

OFFICE OF COUNTY ENGINEER
RANSEY CO. MO.

Road Map Survey

LARPENTEL AVE.

From W. Co. Line to Hamline Ave.

Road A. C. No. 14

From Hamline Ave. to Dale St.

Road Acc't. No. 50

Date Filed 9-19-30 File

Webb
Beaton
Stragg, lun.
Bell

(Topography)

Larpenteur Ave.

W. County line To Dale St.

0+00 To

6+00

5+00

4+00

3+00

2+00

1+00

0+00

12

11

10

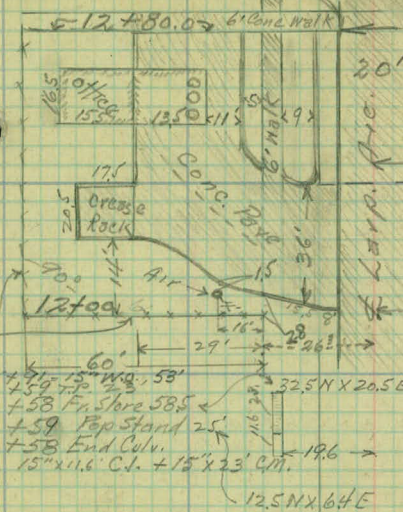
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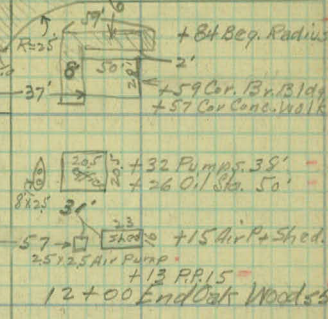
7

12+00 End S.W. 4

5-11-30



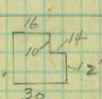
Euslis St. Bve.



Picket Fence

- +59 Fr. Bldg. 58.5
- +59 Pop Stand 25
- +58 End Culv.
- 15" x 11.6' C.I. + 15' x 23' C.M.
- 12.5' N x 6.4' E

- +59 Guy P. 13'
- +58 P.P. 16'



- +71 T.P. 23'
- +65 Fr. Bldg. 59'

- +68 P.P. 16'

10

- +73 M.H. 11.5'
- +79 Rd Sq. 29'
- +95 Ctr 12' x 40' C.M. 21'
- +57 Br. Pier 33'
- +40 T.P. 22'
- +32 Br. Pier 35'
- +28.5 Br. Sw. 33'
- +25 Br. Pier 33'
- +18 Cor. House 57'
- +05 = 2-4" Apple Trees 51'-65'
- +79 Br. Pier 33' - 15' x 15'
- +96 End Garden 26'



- +43 P.P. 16.5'
- +37 Rd Sq. 18'

9

- +28 Cor. Garden 25'
- +Ctr 12' Dr.
- +12 T.P. 22'

- +11 P.P. 17'

8

- +29 Cor. 4' S.W. 30'
- +24 Car House 57'



7

- +03 = 6" C.M. 33'

17

16

15

14

13

12

3-1-30

- +64 Cor House 59' 1st Stucco.
- +72 Ctr. Walk 34'
- +61 End F. 22' Running N.
- +44-4" Maple 36'
- +30 Cor. House 51'
- +30-5" Tree 36' 33' 1st Stucco

17

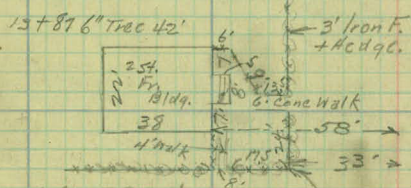
- +92 Cor House 51'
- +85 Pr. Dr. 8' wide
- +78 End Garden
- +79-12 X 146 C.M. 25'
- +73 T.P. 22'
- +30 Rd Sq. 15'
- +23 T.P. 53'
- +17.5 Cor. Iron + Garden 33'
- +16 P.R. 53'

16

- +77 Stop Sq. 36'
- +58 G.V.P. 22'
- +46-2-12" B.E. 30'
- +42 T.P. 22'
- +27 Ctr. 3 C.M. Walk 30'
- +19 Cor House 56.5'
- +15 Ctr. 10' Pr. Dr.
- +07.4" B.E. 30'

- +73 Cor House 51'
- +65 M.H. 15'
- +65-12" W.O. 40'
- +52-18" Oak 65'
- +36 Cor. Ice. H. 42'
- +21-6" Tree 43'
- +18-15" Oak 78'
- +12 T.P. 22'

14 + 30 End F. 32' → 32' →



- +42 P.R. 100'
- +52-2-10 Elms 42'
- +42 F. Cor + Hedge 33'
- +37 C.B. 33'
- +15 Stop Sq. 18'
- +07.1 M.H. 13'
- +91 Stop Sq. 35'
- +89 Rd Sq. 25'
- +82 T.P. 23'

Nursery Grounds

- +43 P.R. 15'
- +38 End Hedge 20'
- +20' End Hedge 20'
- +16-20" Tree 51'
- +16 " " 76'

- +93-10" Birch 4'
- +90 " " 54'
- +84-10" Birch 44'
- +83-4" Tree 23'
- +65-12" Tree 41'
- +65-6-5" Tree 41'
- +53-10" Tree 22'
- +21-8" Tree 22'
- +17 P.R. 14'

- +90 Ctr. of S-8' E. 91' 4'
- +74-Bush 44'
- +55-8" Tree 21'
- +50 Beag Hedge 18'
- +42 Apple Tr. 66'
- +25 " " 65'
- +14 " " 59'
- +08 Apple tree 43'
- +03 P.R. 16' 57'
- +98 Apple tree 43'
- +90-Apple trees 56-70'

- +60-10" Pop. 26'
- +54-Line 10" Pop. 25-50-65-71'
- +50-Beag laun. 52-10 Pop. 20'
- +40-8" Birch 23'
- +38-P.R. 16'
- +31 Evergreen 18'

- +70-6" Birch 24'
- +58 6" Pop 23'
- +56-6" Pop. 28'
- +51 Line 6" Pop. 39-70-80-8'
- +49 Cor. Flow. Gax. 22'
- +41 P.R. 17'
- +39 Rd Sq. 30'
- +36 Stop Sq. 33'
- +37-12" C.M. Cul. 46'
- +08 Water Cut out 33'
- +07 Water Cut out 4'
- +00 Hyd. 36'

Ensle St. Brick

- +84-Beag 25' R.

23

22

21

20

19

18

3-11-30 Windy

+89 P.P. 17'

- 415 T.P. 22'

+47 Rd Sq. 16'

+17 P.P. 17'

- 488 T.P. 22'

+77 P.P. 17'

- 457 T.P. 22'

- 416 Cor. Nursery 47'

+10 - T.P. 65'

- 489 1/2 Pleasant Ave.

+67 Rd Sq. 45'

+34 - 12" Oak 40'

+31 T.P. 22'

+25 - 12" Oak 47'

+23 - 12" Oak 41'

+16 - 2 Evergreens 23'

+14 - 15 Oak 70'

+49 P.P. 16'

+85 Cor. 254 Stocco House

+83 - 3" Evergreen 21'

+72 - 30" W.O. 88'

+72 - 24" W.O. 38'

+27 - 15" Oak 39'

+25 - 15" Oak 35'

+19 - 12" Oak 32'

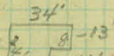
+13 Cor. 4 Walk 25'

+09 - 12" Oak 39'

+12 - 12" Oak 32'

+04 - 2 - 12" Oak 36'

+01 T.P. 22'



18 + 0.50

Nursery Grounds

+52 P.P. 15'

30

29

28

27

26

25

24

3-12-30 Fair little windy

- +98 T.P. 24'

- F = 39'

- +68 T.P. 22'
+47 Rd Sp. 17'

- F. 41

- +38 T.P. 22'

- F. = 40'

- +02 T.P. 22'

- +74 Cr F. 36.5

- +39.91 = £ Fulham.

+25 stop 59. 46'

+17 Rd Sp. 25'

- +18-24 x 56' p3 22.5'

- +06. End Nursey Grd. 38'

- +78 T.P. 22'

- +53 = H. Polo. 20-24
T.P.

+79 - R.P. 24'

+40 = End Oak Woods

+35 - 12" T.P. 30

+13 - 12" B.O. 30

F = 46

+49 - R.P. 23'

F. 44

+33 R.P. 22'

F. = 39'

+06 R.P. 21

+74 F. Cr. 33'

+38 Sp. 15'

F/m.s. 000000 +93-6. 4" f/m.s. 50'

+87 End Nur. 40'

+77 R.P. 20'

+67 H. Polo 15-24
R.P.

Golf Links

Oak Woods

37

36

35

34

33

32

31

3-12-30

- +46 T.P. 235

- F = 33'

- +00 End Sand traps 75'

- +36 Water Hyd. 49'

- +17 T.P. 225

- F = 33.5' to 0.0 Sand traps 50'

- +80 Edge of Sand traps 100'

- +60 Cr. Dr. P.O. 15'

- F = 33

- +90 H. Pole 20-24

- +38 End Swamp 33'

- F 33'

- +62 T.P. 23'

- +05. Edge Swamp 33'

- F. 33

- +77 = 15" x 56' Conc. Culv.

- +28 = T.P. 24

- F = 33'

- F = 36'

+88 P.P. 27'

+39 = 4" W.O. 60'

+10 End. Woods 60'
F = 38'

+78 = H. pole 23'-52'

F = 40'

+78 = 4" Water main
+53 P.P. 26'

F = 42'

+38 P.P. 26'

F. 43

+21 P.P. 25'

F. 45' - +00 Beg. Oak Works 45'

+34 End Oaks.

+00 = P.P. 25'
F = 45'

+29 Beg. Oaks

F = 46'

Wood Line 30 to 33' E.H.

x Scattered Oaks

44

43

42

41

40

39

38

3 12 - 30

- +97-12" B.E. 46'
- +95-12" Oak 31'
- +93-6" Oak 33'
- +91-12" Oak 32'
- +76 TP 23
- +60 Clump Willows 50'

+100-12" B.E. 33' F-30'

- +90-18" B.E. 36'
- +76-6" Oak 27'
- +47 TP 23

+89 F. Cor. 30'

+43-18" B.E. 34'

+18 TP 23'

+06-15" B.E. 34'

+75 Ch. Pr. Dr.

+48 Bush 43'

+32-12" B.E. 34'

+89 TP 23'

+04-15" 53' Conc. Cur.

+83 TP 23'

+60 End H.F. 33.5'

F 33'

+78 TP 23.5'

+17-12" B.O. 37'

F 33'

Pasture

Cultivated

PARK

PARK

27 2.4
35000
35

Ch. Pr. Dr.

- +90 Cor. House 70'
- +68 PP 29'
- +53-12" 1/2 W.O. 25'
- +37-6" B.E. 39'
- +37-10" Oak 33'
- +30 Clump 5.8 Oak 75'
- +25-3-6" B.E. 40'
- +23-13" Oak 32'
- +16-6" Oak 31'
- +08-10" B.E. 33'
- +85-10" Oak 27'
- +62 TP 10" B.E. 32'
- +55 PP 28'
- +50-6" B.E. 26'
- +46 TP 10" B.E. 36'
- +33-8" B.E. 28'
- +30-15" W.O. 25'
- +30-2-6" B.E. 33'

+56 PP 29'

+44 TP 28'

+35 Ch. 12 Dr.

+24 Edge Swamp

+33 PP 27.5'

+60 Edge Swamp

+60 End F 32'

+18 PP 27'

F 35'

+88-12" Oak 39'

+65-12" Oak 55'

+40 Ch. Dr.

+26-15" W.O. 75'

F 36'

Low uncultivated land

14 Gate

51

50

49

48

47

46

45

58

57

56

55

54

53

52

- +94 T.P. 24
 - +59 T.P. 22'
 +47 School Sq 23

- +60 T.P. 23'

- +81 T.P. 22'
 +61 Rd Sq 14'
 - +32 T.P. 23.5

- +09 T.P. 21.5
 - +96 T.P. 23'

- +00 T.P. 23'

- +52 T.P. 21'

- +14 T.P. 22.5

- +80.75
 - +63 Rd Sq. 42'
 - +53 T.P. 62'
 - +51 Rd Sq. 30'
 - +50 F. cov 33'
 - +30-34" C.W. 26'
 - +10 T.P. 15'
 - +07 T.P. 29'
 - +05 Guy Pole 16'

Cultivated Field

33'
 33'
 33'
 33'
 33'
 33'

+08 P.P. 23'

+89 P.P. 23'

+66 P.P. 22'

+43 H. Pole 18 +27
 P.P.

Cultivated Field

+29 P.P. 23.5
 +14 F. cov 33'
 +12 Rd Sq. 29
 +06 T.P. 52'
 +98 Rd Sq. 11 +15'

+57 T.P. 54'
 +54 End Cdv. 42'
 +40-24" Maple T. 56'
 +37-12"x20 C.M. 30'
 +16 P. 10' R'
 +25 P.P. 22'

& Cleve. Ave.

20

65

64

63

62

61

60

59

65

+45 H. Pole 21-26
T.P.

Cultivated

+60 Ctr. P. Dr.
12" X 32 CM. 27'



+14 T.P. 23'

Yard.

+85 T.P. 23'

+55 To +70 Hedge 35'
+48 Fence 34'

3

+83 T.P. 23'

+12 P.P. 22'

+52 T.P. 22.5

+35 Ctr. P. Dr.
12" X 20' CM. 25'

2

+53 T.P. 23'

+90 P.P. 22'

+78 T.P. 23'

Cultivated

Cultivated

+51 P.P. 23'

+24 T.P. 23'

60

+96 = 12' F.E.
+85 Sta. Sq. 20'

+46 = 12" X 42
Conc. Cu/v.
+30 - P.P. 22'

72

71

70

69

68

67

66

- +81 Row Ev Gr.
- +77 Row Ev Gr.
- +72-12" W. Ash 39' Path
- +65-12" X 8' C.M. 27'
- +49-8" W. Ash 41'
- +36 Row Apple 51' →
- +21 Row 6 App/c. trees 51' →
- +20 End Cult. beg. yard.

+62 R.P. 23' -

+81-T.P. 23

+40 R.P. 22.5' -

Cult.

+50 T.P. 23'

Cultivated.

+13 R.P. 22.5' -

- +25 End Yard Beg. Cult.
- +20 T.P. 23.5'
- +10 Ctr P.R. Dr.
- 12" X 20' C.M. 26.5'

+95 R.P. 22' -

+61 Cor Ho. 37' 25ft. Stucco 88' →

+48 Ctr P.R. Dr.

+60 Cor Ho. 40' 25ft. Stucco 88' →

- +94 T.P. 23.5'
- +90 End Cult. Beg. yard.

+75 R.P. 21' -

Cultivated

Cultivated

+73 T.P. 23'

+50 R.P. 22' -

+30 Stop 59.27

+20 Ctr F.E. -

78

77

76

75

74

73

Yard.

- + 72 Pery Bush 40 30'
- + 67 6" WASH 40'
- + 67 T.P. 21'
- + 64 P.P. 21'
- + 65 N+S. F. 30'
- + 58 End Cult.

+ 32 H.P. 21-25'

3-20-30'
15° F

Pasture

- 105' End F 31'
- 198 T.P. 24'
- + 72 Plum T. 48'
- + 58 18" B.E. 36' +
- + 57 F. Cor. 32.5'
- 148 Ctr. P.D.
- 12" x 20 C.M. 26'
- + 30 Bush 37'
- + 36-18" B.E. 70'
- + 06. Bush 55'

- + 96 = 3-4" B.E. 4 Guy P. 21'
- + 85 Edge Shrub 45'
- + 72 Edge Shrub 45'
- 170 T.P. 23'
- 156 End Cult. Beg. Yard.
- + 56 = 18" B.E. 60'
- + 32-8" B.E. 41'

+ 90-8" B.E. 40'

Cult.

- 141 T.P. 23'
- + 40 12" B.E. 40'
- + 18 = 18" B.E. 35'
- 113 = Beg. Cultivation
- 103 Ctr. Pr. Dr. 12" x 20 C.M. 25'
- + 90-10" Elm 57'
- + 90 = 8" B.E. 40'
- + 60-24" Elm. 72' Yard
- + 55 20" B.E. 40'
- + 37-2-12" B.E. 41' + 67'
- 110 T.P. 23.5'

Cult.

- + 41 F. Cor. 32.7'
- + 41 P.P. 22'
- + 25 T.P. 22'
- + 25 End Orch. 48'

+ 77 T.P. 22.5'

+ 20 T.P. 25'

+ 98 Gr. Orch. 48'

+ 97 T.P. 55'

+ 97 P.P. 22'

+ 92 End Cult.

+ 94 P.P. 31'

12" x 20 C.M. 26'

+ 86 F.E.

+ 76 Rd Sq. 30'

+ 79 Guy Pole 25'

Cult.

+ 79 P.P. 22'

33

33

33

84

82

81

80

79

3-20-30 - Windy
15° F.

25 Stucco.
196.5" P.R. 72'
+96 Cor. Ho. 82'
35' +86 End Cult.
+77 T.P. 20'

+51 T.P. 23
+30 Dead B/E 23

+51 P.P. 20'

+80 Ctr. F. Ent.
+70 Rd 59.53'
+70 T.P. 50

+69 H/B/E 16-23
T.P.

+22 T.P. 23'

+29 P.P. 20'
+17 T.P. 20'

Cultivated

+91 T.P. 23

+16 T.P. 20'
+14 P.P. 20'

+16 Bush 35'
+25 Beg. Cult. F.
+11-12" Plum 45'
+05.12" B.E. 88'

Cultivated

+61 T.P. 24'

+94 T.P. 20'
+88-18" B.E. 37'
+87 P.P. 20
+81.15" B.E. 85'
+76.12" Elm 53'
+65 Wind Mill 95'
+31 Cor. Ho. 52'
12" x 20" Oak 21'
+20 Ctr. F. Oak
+09-2 B.E. 10" x 15" 10
+09-18 B.E. 41'
+07 E Bushes 20'

+06 T. End F.

90

89

88

87

86

85

84

+105 T.P. 23

Nursery

+90-10" Stump 33'
+52-20" Stump 33'
+44-15" Stump 33'
+33 T.P. 19
+32-15" Stump 53
+14-15" Stump 33
+04 Hedge 33
+04 P.P. 20

12" x 20" C.M. 25'
+84 Ctr. P.Dr.
+75 Cor Hedge 30

Yard
+73-20" Stump 33'
+50-20" Stump 33'
+41 Stump 20" 33'
+10 Cor. Hedge 30
15" x 20" C.M. 22'
+02 Ctr. P. Dr.

+96 Row Bushes 40

+92 T.P. 19
+80 P.P. 19
+77-20 Map 32

12" x 20" C.M. 23
254 Fr. +55 Pr. Dr.
34' +27 18" Map 32
+17 Cor. Ho. 82

+74 T.P. 19
+65 15" Map 31
+46 T.P. 19
+32 18" Map 31
+27 Row 6-4 Elms 46
12" x 20" C.M. 24
+16 P.Dr.
+03 2" B.E. 40

35'
+75 Cor Ho. 81
+73-8" B.E. 71
+73-8" B.E. 51
254 Fr. +73-4" W. Rd. 43
+66 End of Out.
+34 T.P. 20
+31 P.P. 20

+43 T.P. 23

Cultivated

+12 T.P. 23

Cultivated

+81 T.P. 23

+38-14" F.E.

+05 T.P. 19
+02 P.P. 20

+50 B.O. Cult.
+41 12" Elm 38
12" x 20" C.M. 24
+33 Ctr. P.Dr.
+00-4" Elm 38

97

96

95

94

93

92

91

+99-24" Map. 39'

+94-T.P. 23'

+77=24" Map. 39'

+58-15" Map. 39'

+37-24" Map. 39'

+18-30" Map. 39'

+98-30" Map. 39'

+82 T.P. 23'

+82 Cor. F. Beg. Pasture 33'

+76-Ctr. Pr. Dr. = 12" x 20" C.M. 26'

+70 End Cult.

Pasture.

Cultivation.

+30 T.P. 23'

+72 End Yard Beg. Cult.

+34-3-8" Apple Tr. P. 51-63-75'

8 x 16 Bridge Plank

+25 Ctr. Pr. Dr.

+14 End Hedge 30'

+98-Row Trees 15" 12" 15" 50'

+98 T.P. 23'

+85-8" Box 36'

+73-10" Elm 36'

+60 Row 13" Elm - 50-65-75-85'

+60 Cor. Hedge 30'

+52 End Cult. Beg. Yard.

+63 T.P. 22'

Cultivated

+35-H. Pole 20'-25'
T.P.

+90 P.P. 19'

+72 T.P. 19'

+26-30" Map. 33'

+11-24" Map. 33'

+94-30" Map. 33'

+85-P.P. 19'

+62-24" Map. 33'

+57-12" x 44" Cor. C.M.

+50 T.P. 19' x Dr.

+00-30" Map. 33'

+78-24" Map. 33'

+78-P.P. 19'

+49-18" Map. 33'

+22 T.P. 19'

+11-18" Map. 33'

+99-24" Map. 33'

+63 P.P. 19.5'

+16-18" Map. 33'

+07-T.P. 19.5'

+43 P.P. 19'

+81-Cor. Pole 19'

+78-H. Pole 16-22'

+72-24" Maple 33'

+20 F. Cor. 31'

12" x 20" C.M. 25'

+87 Ctr. F.E. 2'

+67-24" Stump 33'

+61-T.P. 20'

+51-30" Stump 33'

+40-12" Stump 33'

+24 P.P. 19'

+21-15" Stump 33'

+05-15" Stump 33'

Pasture.

Pasture

Nursery

101

100

99

98

+92-24" Map. 38'
 +76-T.P. 23'
 +52-18" Map. 38'
 +32-25" Map. 38'

+75-18" Map. 39'
 +54-18" Map. 38'
 +45 T.P. 23'
 +34-15" Map. 39'
 +16-15" Map. 39'
 +07 F.E. 12" X 20" C.M. 25'

+77-24" Stump 40'
 +55-20" Map. 40'
 +37-24" Map. 40'
 +23 T.P. 23'
 +17-12" Stump 40'
 +97-18" Map. 39'

+77-12" Stump. 40'
 +57 18" Map. 39'
 +48 C.F. F.E. 12" X 20" C.M. 25'
 +37-18" Map. 39'
 +33 End Pasture
 +33 End F. 33'
 +17-18" Map. 39'

Pasture.

+80 Rd. Sp. 15'
 +90-10" Map. 50'
 +88 F. Cor. 385'
 +38 Bushes 55'
 +62 End Clump Bu.
 +58-20" Map. 34'
 +58-8" F.R. 77'
 +52 End Bush 55'
 +55-8" Elm 50'
 +38-10" C.W. 50'
 +36-30" Stump 34'
 +32 F.P. 13-16-22'
 +19-12" Elm 50'
 +03-12 C.W. 50'

+87-24" Stump. 34'
 +84-8" Elm 50'
 +66 E. Bushes 60'
 +66-4" Pop. 50'
 +60 Fir Tree 77'
 +43- Fir Tree 77'
 +42-24" Map. 34'
 +21 Edge Bushes 55'
 +21 T.P. 19'
 +15 Row Elms. 50-689'
 +15-PP 19'
 +13-15" Stump 36'
 +16 F.A. 38'
 +06 Hedge 48'

+87 Hedge. 48'
 +87 Cor. 3 X 3 F.R.
 +80-24" Stump 34'
 +79 End Bushes.
 +79-2-12" Trees-50-85'
 +79-F. Cor. 39'
 +61-24" Map. 34'
 +50 Edge Bushes 55'
 +20-15" Map. 34'
 +00-24" Stump. 33'
 +93 T.P. 19'
 +80 PP 19'
 +64-24" Map. 34'
 +61 F. Jog. 37'
 +61 End F. 32'

Pasture.

105

104

103

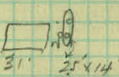
102

+74 T.P. 23'
 +60 P.P. 39'
 +59 R.L. 39' 31'
 +10-12" x 62" C.M. 57'
 +10-1' Conc. Culv. 37'
 +08-G.P. 93

+66 G.P. 32'
 +59-P.P. 54'
 +55 Hyd. 65'
 +08-1' C.M. 60'
 +01 = F. Cor. 40'

C.M. on 80, + Conc. on N. End.

+98-15" Map 93'
 +82 = 2' x 3' Stone Light Base.
 +46 End Pump 69" + Ctr. 40R
 +45 W. Cor. Bldg. 86
 +98-30" Map 36
 +78-15" Map 36
 +59-15" Map 36
 +40 T.P. 33
 +38-24" Map 36
 +20-15" Map 36



+98 Rm Tr. 64-80-96
 +92 T.P. 19'
 +88 G.P. 20'
 +78-30" Radius 1'
 +67 8" Elm 50'
 +59 Stump 35'
 +33 8" Elm 50'
 +29-10" BE 36'
 +14 End Bush 56'
 +14-24" Elm 35'

← End F = 105400



+84 Board F 33'
 +63-30" Map 36
 +23-6" BE 41'
 +06 T.P. 23'

+97-6" Elm 50'
 +97 Edge Bush 56'
 +86-30" Map 83'
 +80-24" Stump 35'
 +63-12" Elm 50'
 +61 T.P. 20'
 +55-30" Stump 34'
 +31-30" Stump 35'
 +25 Clump 6" Elms 75'
 +28-12" BE 50'
 +25 End Bush 58'
 +05 Edge Bush 58'

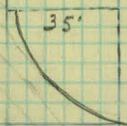
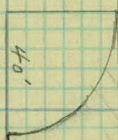
+88-18" Map 37 Gate Ent. =
 +70 15" Map 37 same as sk
 +50-18" Map 37 at Sta 99+89
 +31-18" Map 37
 +10-12" Map 37

+98-24" Stump 36'
 +92-8" Elm 50'
 +73-18" C.W. 36'
 +56-8" Elm 50'
 +54 T.P. 19'
 +50-24" Stump 36'
 +33-24" Stump 36'
 +18-24" Stump 36'
 +50 Edge Bush 60'
 +24 Edge Bush 60'
 +24 F. Δ
 +02 Hedge. 60' South
 +00 Cor. Stone 16. 45'

105+32⁹⁵ £ Snelling Ave.

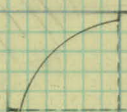
21

20'



Pave 20'

40 Pave.



20'

112

111

110

109

108

107

106

+24 T.P. 23'

+54 T.P. 29'

F=46.5

+84 P.P. 17'

+27 T.P. 29'

F=46.5

+92 T.P. 23'

+55 P.P. 17'

F=46.5

+95 P.P. 28.5'

+35 P.P. 17'

+11 Dr. 2
12" x 32' C.M. 19'

+82 Beg. Fat Bldg.
R 47'

+66 T.P. 27.5'

+20 P.P. 17'

+18 Cr Bldg. 47'

+00 Cr Dr.

+92 F. End 47'

+36 T.P. 27'

+13 P.P. 16.5'

+17 F. Cor. 47'

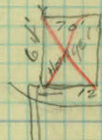
+08 T.P. 26'

+03 P.P. 17'

Uncultivated Field & Pasture.

Air Field.

Pasture



119

118

117

116

115

114

113

+ 75 T.P. 23'
+ 60 Beg. Cult Field 27'

+ 45 T.P. 23'

+ 16 T.P. 23'

+ 85 T.P. 23'

+ 81 G.P. 23'
+ 55 T.P. 22.5'

Pasture

+ 90 End F 45.5
+ 82 P.P. 17'

+ 85 T.P. 28.5
F = 45.5

+ 52 P.P. 16'

F = 46'

+ 80 T.P. 29'

+ 44 G.P. 19'

+ 17 P.P. 16.5

Flying Field

+ 48 T.P. 29'

F. 46.5

+ 91 P.P. 17'

+ 18' T.P. 29'

+ 53 P.P. 17'

+ 81 T.P. 29'

+ 18 P.P. 17'

126

125

124

123

122

121

120

- +55 T.P. 23'

- +38 G.P. 24'

As/wood

- +65 Hyd 23'

- +27 End Cult.

+41 Ctr. Rd. = 15" x 30' C.M. 20'

+30 Stop Sq. 25'

- +24 T.P. 23'

+61 P.P. 16'

+39 T.P. 28'

F 47'

+18 T.P. 29'

+11 P.P. 17'

- +95 T.P. 23'

+28 End Yard Beg. Cult. 28'

+25-12" B.E. 84'

+17 Ctr. P.D. 15" x 30' C.M. 25'

+03-12" B.E. 44'

+82-4" Elm 44'

+66 T.P. 235'

+66 Cor. No. 85'

+58-6" Hook T. 46'

+43-8" Hook T. 89'

+39 End Cult. Beg. Yard 24'

Flying field

+94 T.P. 29'

+71 P.P. 17'

F = 46'

+75 T.P. 29'

+31 P.P. 165'

+95 Beg F 46'

+47 T.P. 28'

+09 P.P. 17'

+25 T.P. 29'

- +35 T.P. 23'

- +07 T.P. 23'

133

132

131

130

129

128

127

4 Woc

+ 25 Bird House 34'
+ 25 Sq. Posts - 18'-2"
+ 12 P.P. 17'
+ 08 Rd. Sq. 24'

4.75 Stop Sq. 38'
+ 65 T.P. 2nd
+ 64 Rd Sq. 33'
+ 62 Beg. 15" x 54" C.M. 20'

+71 Hyd. 39'
+63 G.P. 30' cm. 20'
+62 Ead. 15' 20" 13' 20"
+62 Row Tr. 38-56-77'
+54 T.P. 27'
+48 End F. 47'

Pasture.

A 25 T. P. 28'

250

2 St. Stucco.

Pasture

Field

Flying

+32 P.P. 16'

F 46.5

+90 T.R. 28'

+ 12 Ctr. Dr. 12" x 16' C.M. 20'

F. 46'

+ 86 T.P. 23'
+ 60 End Yard
+ 55 Ctr. Pl. Dr.
15' x 20' C.M. 25.
26' E
15' W
11' S

+92 P.P. 16'
+83 Rd 59. 16'
+64 T.P. 28'

28' N
154
Ft.

5.

100' $\rightarrow$

137

136

135

134

133

132

A97 T.R. 18'

F57

+ 73 Rd 59 20'

754 T.P. 23'

+ 67 TP 17'

F 50'

+25 T.P. 23'

+ 28 - T.P. 17' -

$$F = 44'$$

+90 F. Int

+70 - PP 53'

461-P.P. 39.5

407 Bag. 6" Cone. Curb. 10"
407 End Curb.

$$F = 35'$$

494 T.F. 23'

+70 out 74.7k
Site # +976.P.19
2' Com. +94 T.P.20

+ 43 Edge Pumps
stand 41.5

+ 36 Edge Pump
+ 31 Stand. 57.5

+26

+ 22 End 6" Curb 10

+ 12 Cor. Pave 39'

Mont. $131 + 94,80$

132

143

142

141

140

139

138

137

143

+35 H.P. 10' 21'-26' T.P.

+70 Beg. F 38'

142

+81 Ctr. Spillway 10' x 10' C.M.

+60 G.P. 25'

+35 F. Cor. 41'

141

+80 X Drain 18" dia.

+74 T.P. 22'

140

F. 44'

139

Beg. Potholes
Best
F = 46'

138

+17 T.P. 23'

F. 47

137

+32.5 Ctr. Spillway
+13.6" Maple 30'

68' 44' +57 Con. Cor.

+20 East End Dump

+08 T.P. 19'

This curb is in
deplorable
condition

+81 Ctr. Spillway
10' C.M. covered

+60 T.P. 18'

Dump
C.H.

This end has
been covered

+21 T.P. 18'

+71.5 Ctr. Spillway
15' x 40' C.M.

+00 Beg. Dump 100'

+68 T.P. 18'

150

149

148

147

146

145

144

1-15"x24" V. 27' II
 - +08 Field Ent Ctr.
 - 2-Side drains-1-12"x30" V. 25'

+68 T.P. 23'

+72 T.P. 20'

+39 T.P. 23'

+41 T.P. 19'

+10 T.P. 23'

+16 T.P. 19'

+56 P.P. 36'

+98 P.P. 40'

+98=2 Side drains 1-18"x22" C.M. 25'
 +98=Ctr. 12" Dr. 1-12"x20" V. 27'

+80 T.P. 23

Cultivated.

Un-cultivated

Cultivated

+97 End F. 37'

+63 T.P. 23'

+24 End Curbing

F. 37'

6'x5' Head wall.

6' walk

24'x81" C.M.

6'x5' Head wall.

6' walk

6'x5' Head wall.

6' walk

6'x5' Head wall.

6' walk

6'x5' Head wall.

6' walk

6'x5' Head wall.

6' walk

+85 T.P. 19'

+68 Ctr. Cem. SW. 26'

+67 P.P. 32'

+62 RA. 54 29'

+58 RA. 50. 35'

+24 Hyd. 39'

+14 Ctr. Cem. SW. 26'

+01 End Culvert. 26'

+57 T.P. 19'

+25 Cor. House

+24 End Curbing

+00=12" Elm 49'

1st. Space.
 4.5' 25'

45' 25'

157

156

155

154

153

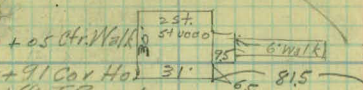
152

151

+77 Rd Sq. 23.5
 +76 T.P. 22.5
 +67 Beg. Rad. 18
 +63.18" N. Ash 36'



+78 Water Plug 27.5
 +93 Mt. 45
 +91 Water Plug 25
 +85 End. Cur 6.25
 +69 End. Cur 6.15
 +79 E. Loc. 39.26
 +52 V. Edge Pump
 +51 Cor. Bldg.



+05 Cor. House,

+91 Cor. Hoi 31'
 +69 T.P. 22'
 +72 Lilac Bushes 35-77'
 +60 Lilac Bush 35'
 +43-15" Map. 37'
 +35 Lilac Bushes 59-68-76'
 +30 Lilc. Bush 36'
 +25-12" B.F. 92'
 +22 Ctr. Pz. Dr.
 12" x 34" G.M. 18'



+22 T.P. 19'

+68-H-Pole T.P.-21-25

Un-cultivated

Cultivated

+00 T.P. 19'

+91 Rd Sq. 19'

+60 T.P. 23'

+07 Rd Sq. 25'
 +100 Ctr. Dr.

+95 Ctr. Dr. = 30'

+65 T.P. 19'

+59 T.P. 23'

Cultivated

Un-cultivated

+47 H. Yd. 19'
 +40 T.P. 20'

+30 T.P. 22'

+00 T.P. 22'

+06 T.P. 19'

163

162

161

160

159

158

+12 T.P. 22'

+00 Ctr. Dr.

+70 End Cult. Beg. Greenhouse Yard.

+33 Rd Sp. 19'

+77 T.P. 22'

+70 Rd Sp. 15'

+42 T.P. 22'

+00 Cor. Rep Stand

+54 Cor. conc. Slab.

+04 T.P. 22'

+85 Cor. Bldg. 103'

+65 Tank Pipe. 44'

+61.5 " " 46.5'

+58 Tank Pipe 49'

+41 Elec. Sq. 36' Rd. Cntr.

+24 Edge Id. 24'

+39 Rd Sp. 36'

+33 P.R. 83'

Greenhouse Yard

Cultivated

Cultivated

+98 T.P. 20'

+76-2-4' B.E. 47'-67'

+89 Ctr. P. Dr.

+42 Water Plug 27'

+35 Cor. Ho. 77'

+30 6" B.E. 26' 40'

+22 End Cult Beg. Yard 22'

+67 T.P. 19'

+62 X Drain

= 15" x 45" C.M.

+84 Beg. Cult.

+84 End Berry Ptd 30'

+69 Berry Ptd 30'

+52 Row 6 Elms 42-76'

+44 Ctr. P. Dr.

+38 End Hedge 22'

+35 T.P. 19'

+15 Cor. Brd 77'

+10 Hedge 24'

+02 End Berry 17'

+58 Berry Patch 35'

+50 6" M. Ash 25'

+35 Ctr. P. Dr.

+27 5" Ash 25'

+16 T.P. 19.5'

+96 4" Elm Lumber 26'

+68 Cor. Ho. 87'

+64 6" App. Tr. 43'

+64 10" Elm 25'

+57 Hyd 24'

+42 Edge Garden 24'

+39 12" Maple 83'

+35 T.P. 20'

+31 Rd Sp. 24'

+26 T.P. 47'

+12 M.H. 45'

169

168

167

166

165

164

+79-6" Ev. Gr 36'

+71-6" Ever Green 36'

+59-6" Ev. Gr. 36'

+55-3" Cent. 11.31'

+53-T.P. 23'

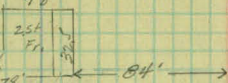
+40-6" Ev. Gr. 36'

+38 Cor. Portak

+34-15" B.W. 78'

+27 Ctr. Fr. Dr. = 1-12" x 20' Vit.

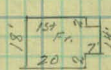
+17 Row 20' Basswood 4-40-63-85-90-100'



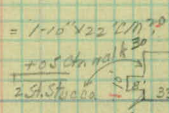
- +1-12" x 22' C.M. 20'
- +38 Ctr. Fr. Dr.
- +34 Hodge 70'
- +27-12" x 20' 74'
- +27-12" x 20' 36'
- +27 T.P. 18'
- +25-8" x 20' 44'
- +23 End Orch. 58'
- +23-12" x 20' 27'
- +23 Hyd 23'

11

+99 Row Fruit Trees
+2-56-76'



- +174 Cor. House 78'
- +68 End Orch. 42'
- +25 T.P. 23'
- +03 Beg. Apple Orch. 41'
- +96 F. 31'
- +88 End Cultivated.
- +96-2-6" Elm 538'



- +93-10" x 20' 65'
- +93-12" x 20' 53'
- +88-8" x 20' 42'
- +78 Beg. H. Orch. 58'
- +70-15" x 20' 33'
- +62-15" x 20' 58'
- +64-10" x 20' 58'
- +54-12" x 20' 34-44'
- +48-12" x 20' 60'
- +40 Ctr. Fr. Dr.
- +21-12" x 20' 36'
- +12-10" x 20' 53'
- +00 Cor. Ho. 75'
- +92 T.P. 18'
- +86 Beg. Yard
- +75-12" x 20' 35'

- +03. T.P. 23'
- +58 Beg. Cultivation.
- +78 Ctr. Fr. Dr.
- +60 End Orch.
- +33 Cor. Apple Orchard 45'
- +05 Clump Bushes 37-10's square.
- +83 Fruit Trees - 36' 74' 85'
- +75 End Cult. Beg. Yard.
- +71 T.P. 23'

+70 T.P. 23'

Cultivated

Cultivated

+43 T.P. 20'

- +60 Ctr. Fr. Dr. = 10" x 21' Vit 18'
- +65 Beg. Cult.
- +45 End Greenhouse Yard
- +42 T.P. 23'

- +42 G.P. 20'
- +20 T.P. 19'

174

173

172

171

170

170

169

+ 71 T.P. 23'

+60 T.F. 19' -

+ 42 T.P. 23'

+ 24 T.P. 19'

+ 84 Rd. 59. 13'

4147.P. 23

+ 79'H - Pole - 16' - 22'

472 Beg. Cst.

+ 73 End Yard.

+ 73 End Hedgezi

100

+ 23 Rev 4" Fruit Trs. 59-8

+18 - Twin 4" Pp. 72'

 $+16 = 6^{\circ} \text{B.E. } 52'$

+ 33 End X Drain 21'

453 Beg. Cultivation

+ 27 to 30' Road

4/6 Rd. 59, 25

4037 P. 52

+ 07 End X Drawn 10'

+83 H-Pole T.P. 20-25'

← 81' → 25' 10" + 78' Cor. House

+ 62 Beg. Hedge 20' -

+ 54-30" K.O. 67

+ 50 End 4' Stone SW. 57'

+ 48 Cl. Dr.

+40 End Hedoe 25'

$$+ 14 - 1.5'' \text{ LKO} = 47'$$
 $+16 - 12'' \text{ H.P. } 27'$

+ 11 = water plug 27

+06-6" Elm 52'

+06-15'' W.O. 31'

+ 32 End Yard Bcg. Cultivation

+07-6" E v. Gr. 36'

405.15 N.O. 27

cent.
1924. 1925. 1926.

+ 85-12" W.O. 47

+77 Co House

11

+ 72-12 W.A. 75

+ 66-6" Elm 47'

+ 62-12-14.0.55

750 / 241.01 27
A 15 [B 00 1100 27]

445-1224 Key 23
445-151100 1-1

445-15" 24.0-60
445-15" 20.0-55

180

180

179

178

177

176

175

- + 97 12" M.A. 43'
- + 78 G.P. 17'
- + 76-10" Tree 43'
- + 68 Rd Sq. 19'
- + 68 8" W.I. 39'
- + 66-12" W.I. 39'
- + 58 M.H. 20'
- + 50-6" W.I. 41'
- + 49 T.P. 50'
- + 31 12" B.E. 50'
- + 20-00 R. 32'
- + 16-8" B.E. 36'
- + 11-8" B.E. 45'
- + 08-12" Oak 36'
- + 98-12" W.I. 35'
- + 88 T.P. 23'
- + 64 24" B.O. 30'
- + 57 T.P. 54'
- + 40-10" B.E. 42'
- + 11-12" Elm 39'

+ 73-12" Elm 39'

+ 57 T.P. 23'

+ 29-12" Map. 40'

+ 82 12" Map 40'

+ 81 P.F. 60'

+ 30 T.P. 23'

+ 74 Shrubory 35' 8" wide

+ 66 T.P. 50'

+ 408 Victoria

+ 25 Rd Sq. 45'

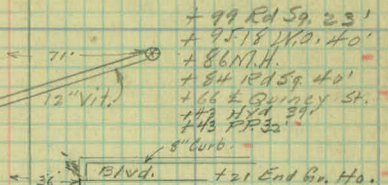
+ 17 P.F. 63'

+ 07 Rd Sq. 32'

+ 00 End Cultivation

+ 00 T.P. 23'

10' x 12' x 5' 1/2'



Greenhouse = 5 Units

+ 85 T.P. 20'

+ 54 T.P. 20'

+ 20 Cor. Gr. House 36'

+ 27 T.P. 20'

+ 90 F.E. = 12" x 140 M. 19'

+ 40 Reflector 19'

+ 99 T.P. 19'

+ 00-End Cult. Beg. Hay Hd.

186

185

184

183

182

181

[illegible]

- + 99 T.P. 191
+ 80 = Hyd — 24
+ 80 = Water Plug 11'
+ 75 End Cuit.

- + 82 H-Pole - 16-22

- +78 T.P. 22'

+45.15" Elm 37'

- +83 15" B.O. 29'
+79 10" W.O. 29'
+70 T.P. 19'
+47 12" B.O. 28'
+42 12" B.O. 28'

+ 46 - 24" B.O. 37'
+ 41 T.R. 19
+ 30' 12" W.O. 30'

- + 41 T.P. 19
+ 30' 12" W.O. 30'

+93 18" B.O. 31"
+83- 24" B.O. 28"
+58-18 B.O. 26"
+32-24" W.O. 32"
+15 T.P. 19"
+06 Beg. Cult.

+93 18" B.O. 31'
+83- 24" B.O. 28'
+ 58-18 B.O. 26'
+ 32-24" W.O. 32'
+15 T.P. 19'
+06 Beg. Cult.

- +18 T.P 23'
+00-8" BE 38'



1.5
6.3
81

///

167 + 44 End 15' x 80' C.M. 20

+ Cor. Pier.

187 + 40' End Wall 33'

33'

15' x 79' C.M.

5' Cem. Walk

2'10" x 2'10" Pier

20' R.

Catch Basin 186 + 63 C.B.

30'

3' En. Gutters

18' x 34' C.M.

+ 15' Beg. Radius
186 + 27 = 15' x 15' C.B.

5' Cem. Walk

2'10" x 2'10" Pier

27' R.

2' wide 2.5' High Wall
STONE

40'

15' x 86' C.M.

2' x 2' Pier

+ 42' Cor. Pier 32.5'
185 + 41' End Side Drain 21' Lt.

192

191

190

189

188

187

186

+97-10" Tree. 45'

+65 T.P. 22.5
+60-12" Tree 42'

+39-10" Tree 35'

+03-20" Elm 39'

+98-10" Tree 35'
+87-12" Will 36'
+82-12" Will 37'
+63-15" Elm 40'
+44-15" x 40" X Drain
+34-10" Tw. BE 44'
+28 T.P. 22.5
+17-15" Will 44'
+12-15" Will 44'

+82-18" Willow. 35'
+59 RT 59. 17'
+46-10" Ash 40'

+12-10" BE. 36'
+00 Tr. 10" BE 39'
+96 T.P. 22.5
+96 Map. 38'

+45-12" BE 43'

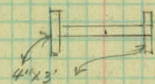
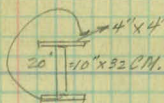
+75-15" Elm 38'
+68 T.P. 22.5

+25-15" Elm 38'

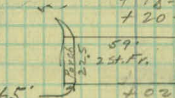
+98-15" Elm 99'
+91-15" Elm 63'

+59-15" Elm 39'
+40 Row Brush 35'
+39 T.P. 22'
+17-18" Elm 55'

+84-18" Elm 80.1'



Headwall



+93 T.P. 19'
+08 Beg. Cult.
+00 Cr. P. Dr.

+78-20" Map 91'
+78-24" Map 77'
+78-15" Map 64'
+78-8" Map 55'
+20-18" BE. 27'

+10 Gr. House.
+02 T.P. 14.5

+84-30" Map. 57'
+63-15" Map 56-63
+50 End Cult. 76
Beg. yard. 88

+99 Gr. P. 18.
+86-T.P. 19.5

+57-T.P. 19'

+22 T.P. 19'

Cemetery Grounds

Grass

Cultivation

199

198

197

196

195

194

93

F 26

+ 70 H. Pole. 16-23

- +65 Beg. Cult.
- +65 End Berry Patch
- +58 Berry Patch
- +51 End Orchard 33'
- +41 T.P. 22.5
- +15 Cor. Orchard 33'
- +07 F. Dr. = 12" x 16" C.M. 18'
- +93-10" App. Tr. 38-52
- +82-10" App. Tr. 38-52
- +72 = 10" App. Tr. 53
- +72 = 8" App. Tr. 38'
- +72 Cor. Ho. = 60'
- +72 End Cult.

F 35
26'

+41 T.P. 19.5

- +04 Beg. F. 23'
- +04 T.P. 23'

- +02 Gully Pole 22'
- +81 = Beg. N. Dale. Pk. Road.
- +81 = Rd 39 27'
- +73 E. Rd.
- +62 End Cult.

- +62 Beg. Cult.
- +62 End Cemetery Property.
- +55 F.E. = 10" x 16" C.M.
- +44 Gully Pole 21.5
- +40 18" Pop 39'
- +40 End Brush line

- +42 T.P. 33'
- +28 T.P. 19.5

- +01-2-12" Willows 40'
- +95-48" Willow 36'

- +68 T.P. 22'
- +31 15" Tr. Will. 39'
- +28 10" Willow 42'
- +22 15" Willow 43'

+08 T.P. 19.5

+33 T.P. 22.5

+89 T.P. 19.5

- +15-8" Ash 35'
- +13-20" BE 40'
- +00-6" Tree 36'
- +99 T.P. 22.5
- +92 = 8" Tree 45'

+59 T.P. 19'

206

205

204

203'

202

201

200

+77-15' BE. 68'

+70-15' B.O.B.

+55-18' Top 53'

+50 Cor. 40.

+50-6' BE. 33'

+40 Low BE. 12'



+10 T.P. 22'

Cultivated

+76 T.P. 22.5

+20 End F. 27'

Cultivated

+22 T.P. 23

27

+15 Beg. Cult.

+11 F.E. = 12 x 13' v. 1.19'

+95 T.P. 22.5

Hay Field

+91 F. Int. 27'

+72 T.P. 22.5

F. 26'

+50
-52

+37 T.P. 19' -
+04 Wood line Jog.

+06 T.P. 19.5
+00 Beg. Woods. 32

+91-24' C.W. 26'

+65 T.P. 19' -

+22 T.P. 19' -

+92 T.P. 19' -

210

209

208

207

206

+62 T.P. 62'
 +51 Guy Pole 84'
 +27 F.P. = 38
 +27 C.B. = 33'

+22 T.P. 22'
 +17 End. Cul. = 23' = 15' x 4' = Vit.
 +12 Beg. Cut. Back Pass. 5' x 5' Headwall
 +98 End F 24

4' x 3' Headwall
 +43 End Cul. 17'
 = 15' x 40' C.M.

+84 T.P. 22.5

Cultivated

F 27'

+47 Beg. Cult.
 +50 T.P. 23'
 +47 F. Int 27'
 +38 End Orch. 44'

+66 Beg. Orchard 44'
 +60 Ctr. Fr. Dr. 12" x 16" C.M. 20'
 +98 Floor 27'
 +98 12" B.E. 35' - 50' - 60' - 70' 23'

Dale St.
 +66 Edge Ave.
 +40 F.P. 33'
 +46 Hyv. 25'
 +44 Kasp. 25'
 +42 " " 23'
 +39 T.P. 18'
 +35 Cor. Woods. 64'
 +22 Beg. Δ

+50 Tree line 50

+24 End Cul. 19.5

+03 T.P. 19'

+82 Tree line 72'

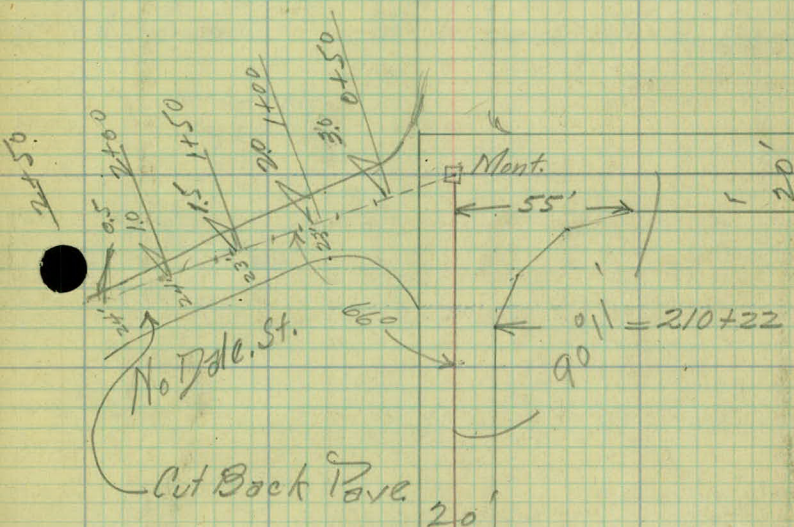
Tree line 48'

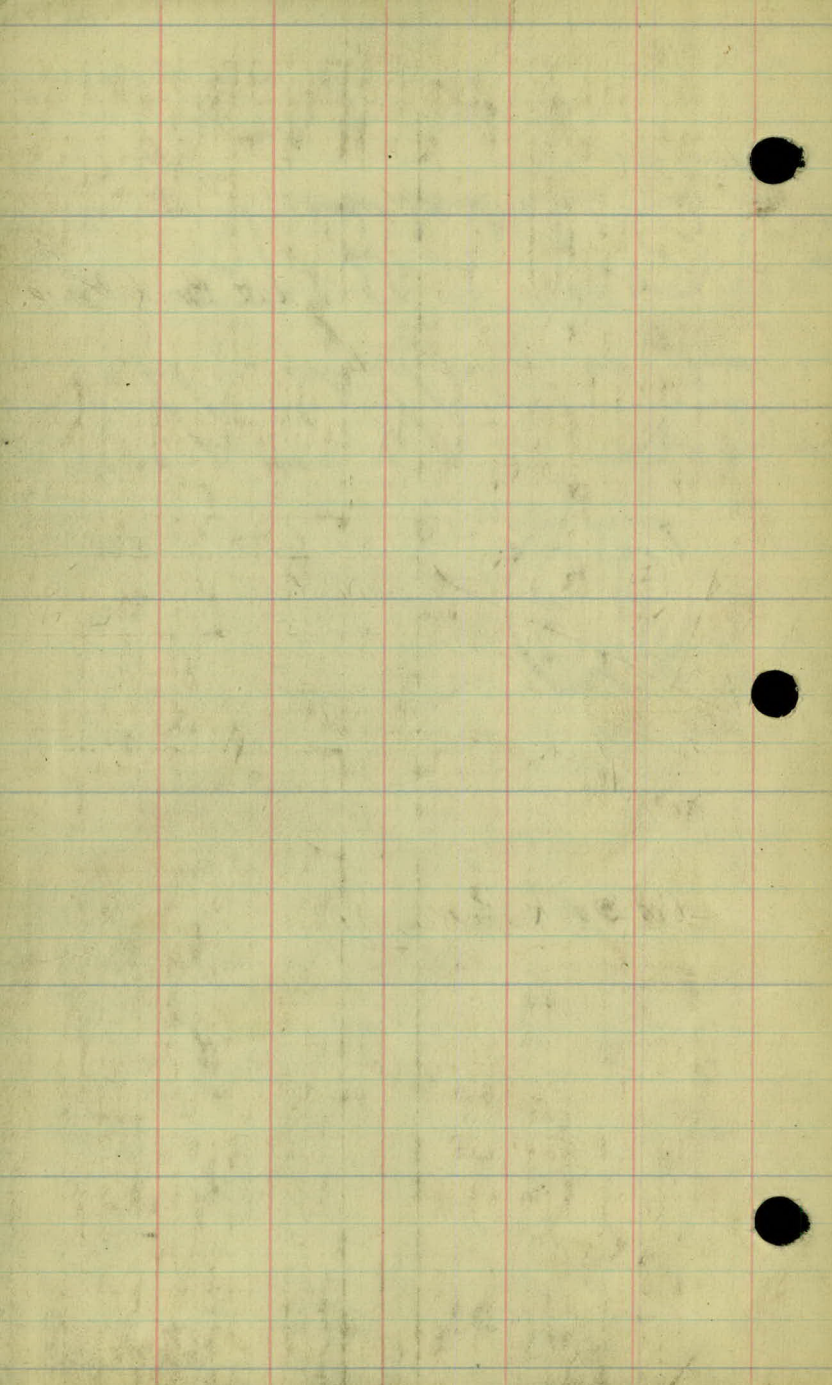
+74 T.P. 19'

Tree line 50'

210

Cut Back Pave.





Larpenteur

1160

159

158

157

143

142

+92 Hamburger Sq. 30'

+85 Bulletin Board 47'

+52 Elect. Light 39'

+48 Stop Sq. 21'

+63-1' Conc Curb
Around Tree

+35 Veg. House 42'
8'x29'



+80-Hyway Sq. 21'

+33-Tourist Sq. 24'

+28 Hyway Sq. 24'

+83-Hyway Sq. 25'

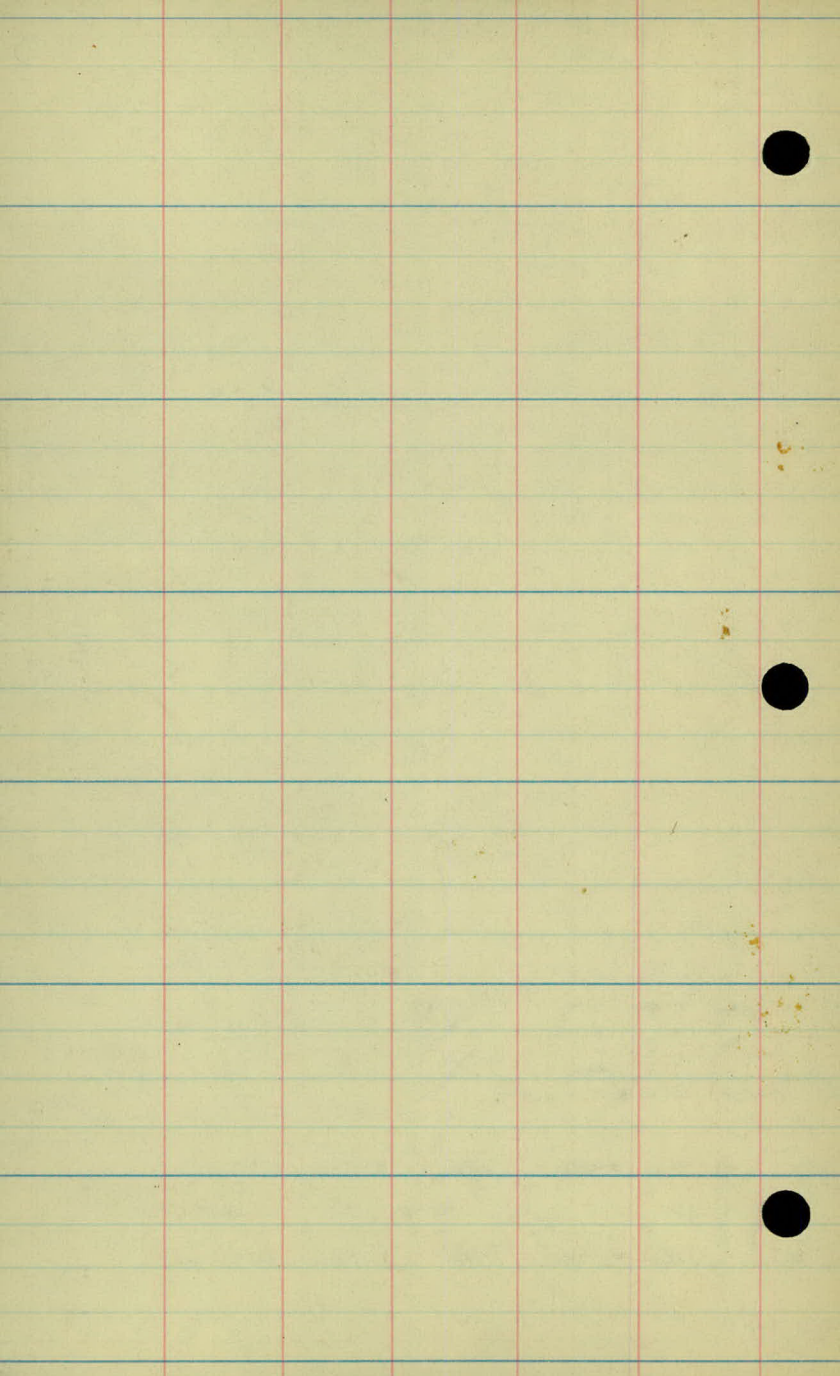
+60 Stop Sq. 16'

+04 Gas Sign 33'

+02 M.B. 18'



+74 Shack 35'



Lexington

7

6

5

4

3

2

1

Q Larpenteur

0+00

+14-T.P. 28'

+10-P.P. 28'

+46-X-Rd. Sq. 15'

+43-Cen. Lane Sq. 22'

+52-Slow Sq. 21'

+46-G.P. 29'

+43-T.P. 29'

+54-Beer Sq. 27'

+46-P.P. 28'

+35-Hamburger Sq. 23'

+27-Hyway Sq. 21'

+62-18" Tr. 71' 30°
+46-Cor. Gar. 95' 20.5'

+30-18" Maple 34'

+04-18" Maple 36'

+94-Rd. Sq. 25'

+90-T.P. 27'

+86-Sign 80'

+51-Sandwich
Shop 80'

+33-Cor. Ice Ho. 80'

+25-End of Curb

18' 18'

+89 Cor. Ice Ho. 31'

+82 Hyway Sq. 21'

+74 Water Dept. Sq. 21'

+43 P.P. 64'

+32 & Drive

+22 Stone Flower Vm 22'

+06 Bird Bath 60'

+05 Cor. Gar. 80'

+85 End Curb Rad. 38'

+13-M.B. 21'

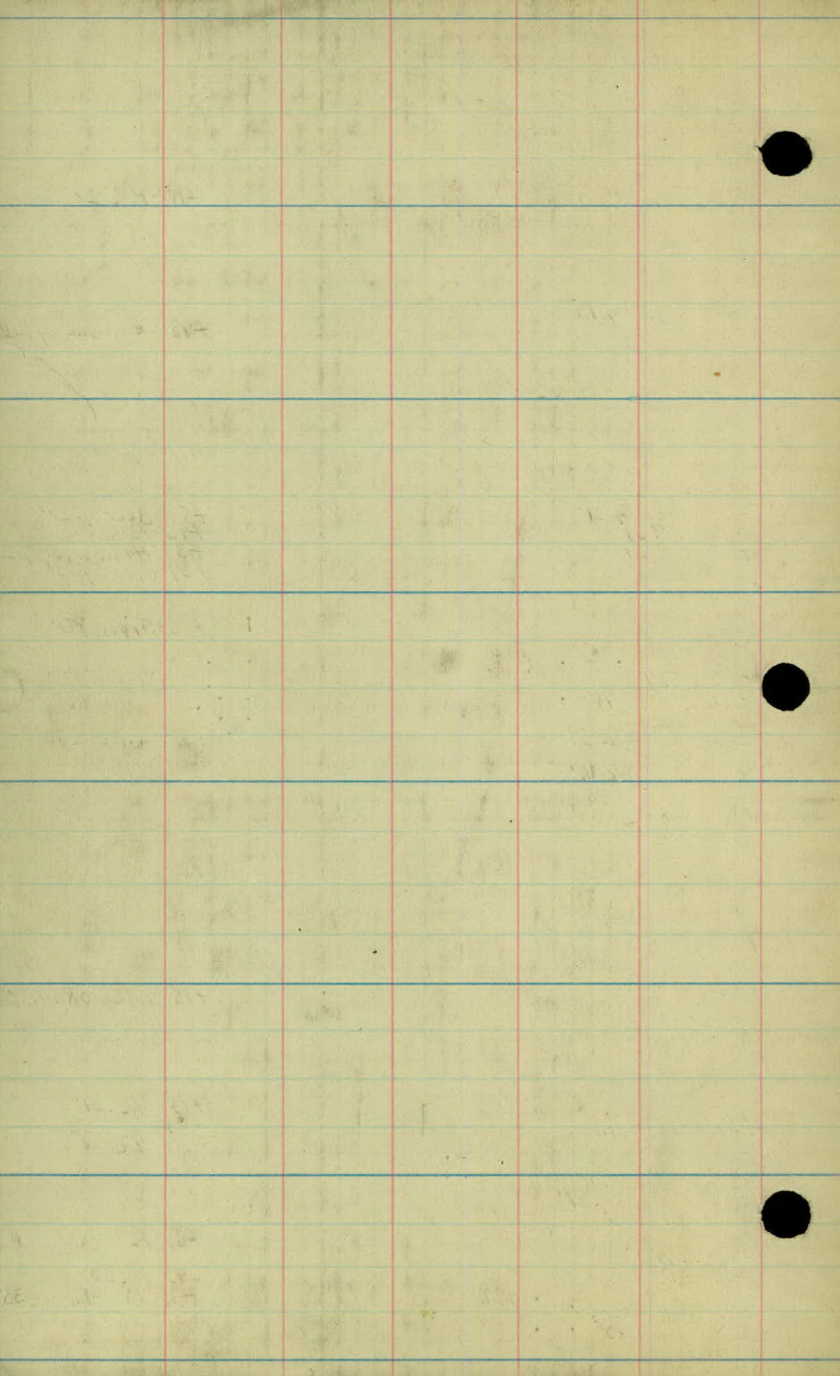
+09 2" Tree 22'

+04-4" Cone Walk 31'

+68-12" Maple 33'

+43-P.P. 20'

+31-15" Maple 33'



Larpenteur Ave.

Transit Notes

W. County line To Dale Street.

0+00 To 210+75.75

Mar. 1930

{ Weber
Boston
Skoglund
Bell }

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed 9.10.30

File No.

Station Point	Deflection
	Left Right

79+06.20 So. $\frac{1}{4}$ Sec. 16-27-23. 0°05'

52+80.15 $\angle$ Cleve. Ave. 0°10'

26+39.21 $\angle$ Fulham St. 0°01'

13+19.93 $\frac{1}{4}$ $\frac{1}{4}$ Cor. 0°05'

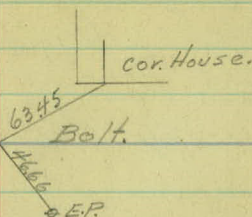
13+09.93 $\angle$ Eustis St. North.

3+53.2 Ctr. Bridge over Belt line tracks

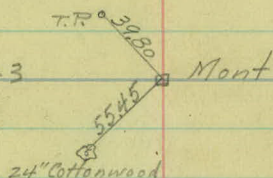
0+00 W. County line & Harp. Ave.

3-8-30 Fair 25° F

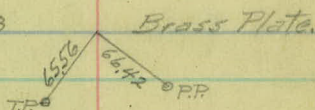
Weber
Beaton
Skoglund
Bell



SE. cor. Sec. 17-29-23

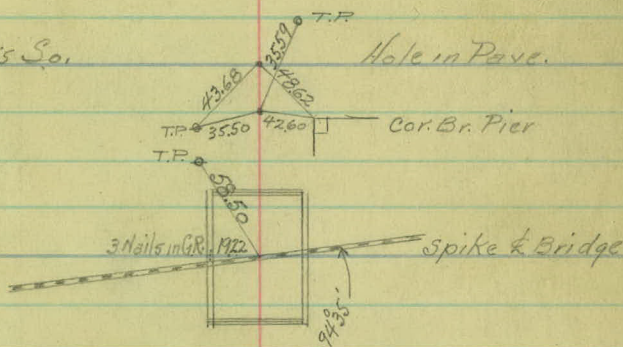


So. 1/4 Cor. Sec. 17-29-23

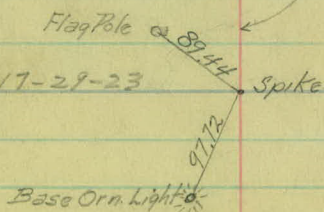


E. Eustis So.

Hole in Pav.



SW. cor. Sec. 17-29-23



Deflection
Left Right

184+47.90 So. $\frac{1}{4}$ Cor. Sec. 14

0°11'

169+82.65 P.O.T.

R.R. spike in Exp. Joint

158+06.05

141'

145+01.10 $\frac{1}{4}$ $\frac{1}{4}$ cor.

131+94.80 So. $\frac{1}{4}$ cor. Sec. 15 0°30'

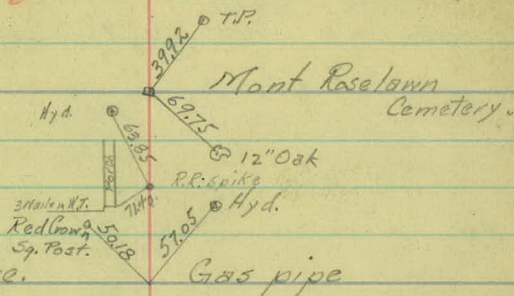
06.30

105+32.95 S.E. cor. Sec. 16 0°18'

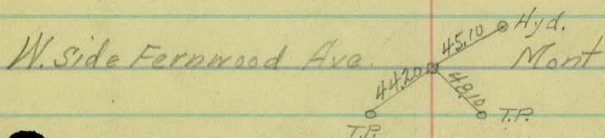
92+20.0 $\frac{1}{4}$ $\frac{1}{4}$ corner

$\frac{1}{4}$ mi. W of S. 1/2

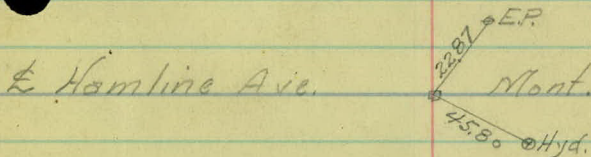
7273.55



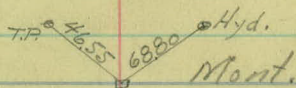
£ Lexington Ave.



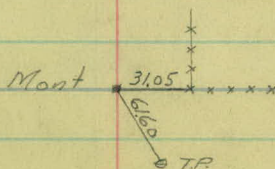
W. Side Fernwood Ave.



£ Hamline Ave.



£ Snelling Ave.

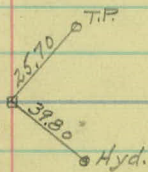


210 + 75.⁷⁵

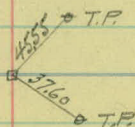
End of Project.

197 + 61.7

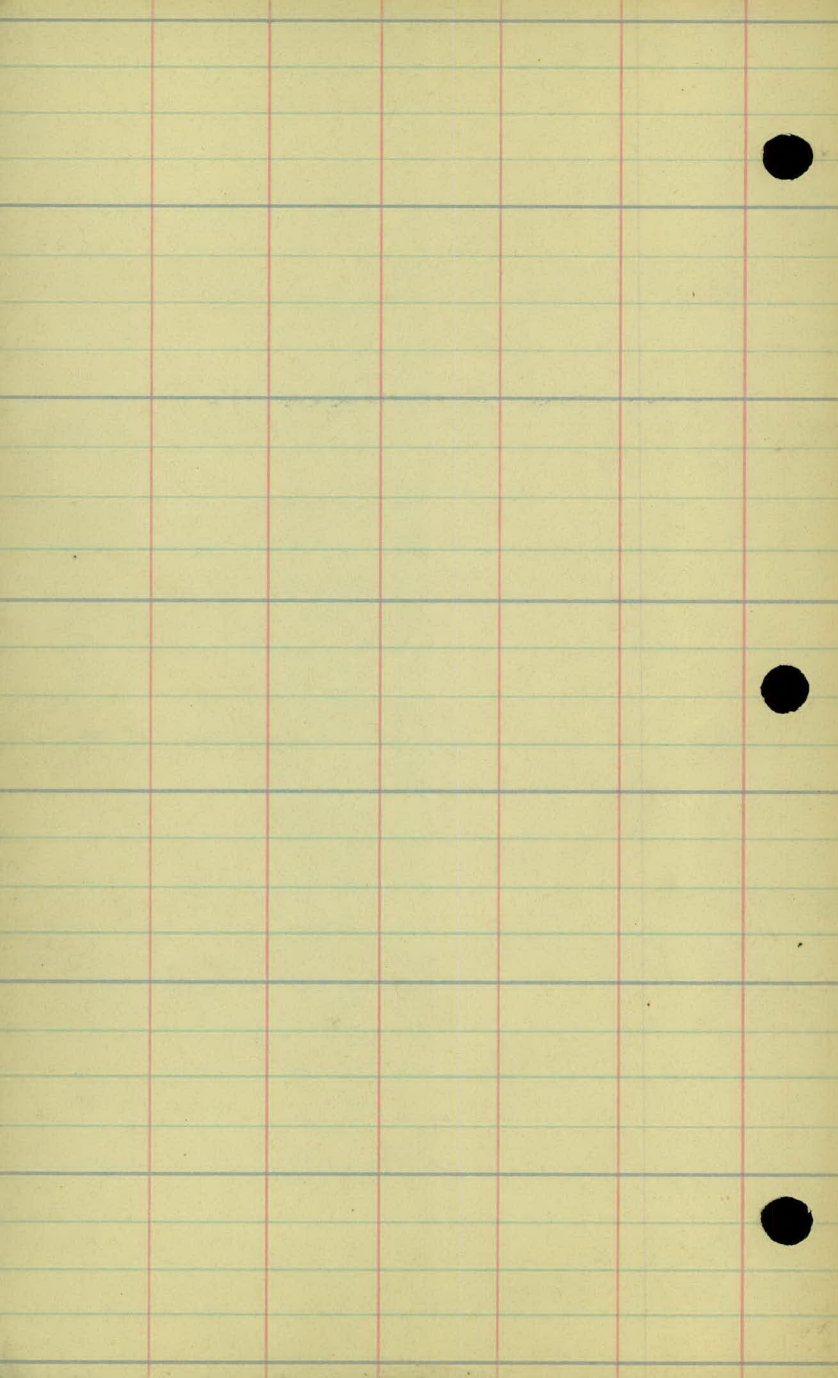
E Dale St. (south)



1/4 1/4 Cor.



Mar. 26-30-21°F



Larpentur Ave.

Bench Levels

Dale St. To - W. County line.

3-13-30

{ Weber
Beaton
Skoglund
Bell. }

	+	H.I.	-	Elev.
B.M.	5.30	924.23		918.93
T.P.	6.72	926.24	4.71	919.52
B.M.			4.27	921.97
T.P.	1.47	923.71	4.00	922.24
B.M.			3.72	919.99
T.P.	5.17	923.10	5.78	917.93
B.M.			3.09	920.01
T.P.	5.01	927.96	0.15	922.95
T.P.	11.58	939.10	0.44	927.52
" "	7.67	946.41	0.36	938.74
B.M.			0.70	945.71
T.P.	1.85	946.80	1.46	944.95
B.M.	5.91	945.29	7.42	939.38 (939.40)
B.M.			3.47	941.82
T.P.	0.88	939.24	6.93	938.36
" "	0.04	929.92	9.36	929.88
" "	1.61	919.64	11.89	918.03
B.M.			9.72	909.92
T.P.	2.11	910.49	11.26	908.38
" "	8.87	913.10	6.26	904.23
" "	12.39	925.16	0.33	912.77
" "	11.78	936.46	0.48	924.68
" "	12.44	948.90	0.00	936.46
B.M.	5.81	951.16	3.55	945.35
T.P.	6.75	954.76	3.15	948.01
B.M.	4.96	956.33	3.39	951.37
T.P.	6.47	957.66	5.14	951.19

3-13-30 20° F.

Top of Mont. Dale & Larpenteur.

Ctr. Mont 14 1/4 cor. Sta. 197+61.2

Nail in TP N. side

R.R. spike in TP #15935 23' Lt Sta. 194+00

S.W. cor. Mont Sta. 184+47.2 S.W. cor. Sec. 14.

Top Hya. Sta. 169+23 = 22' Rt.

Spike in T.P. 500' E of Lex. Ave N. side

Top of Gas pipe Int. Lex. & Larp. Ave.

Ctr. Mont. at Fernwood. Ave. Sta. 145+01.1

N.W. cor. Mont Hamline & Larp. Ave.

spike in T.P. 23' Lt Sta. 118+75

Nail in T.P. 23' Lt Sta. 112+24

	+	H.I.	-	Elev.	
		957.66			
B.M.	6.43	963.07	1.02	956.64	
C.K. B.M.			7.45	955.62	(955.54)
T.P.	6.77	961.96	7.88	955.19	
B.M.	6.27	965.75	2.48	959.48	
T.P.	5.97	968.68	3.04	962.71	
B.M.	8.75	975.23	2.20	966.48	
T.P.	7.78	981.43	1.58	973.65	
B.M.	5.03	981.08	5.38	976.05	
T.P.	6.45	983.24	4.29	976.79	
B.M.			2.50	980.74	
T.P.	6.70	989.27	0.67	982.57	
" "	3.03	984.09	8.21	981.06	
B.M.			6.03	978.06	
T.P.	1.97	981.73	4.33	979.76	
T.P.	4.65	980.94	5.44	976.29	
B.M.			5.37	975.57	
			6.08	974.87	✓
			6.60	968.86	
T.P.	17.4	975.46	7.22	973.72	
" "	0.78	967.66	8.58	966.88	
			3.31	964.35	
B.M.	0.11	957.64	10.13	957.53	
T.P.	0.02	947.06	10.60	947.04	
	0.36	938.39	9.03	938.03	
" "	0.29	926.78	11.90	926.49	
B.M.			11.98	914.80	

3-13-30 - 20°F

N.W. cor. Mont. & Larp. & Snelling Aves.
spike in T.P. S.E. cor. Larp. & Snell.

N.E. cor. Mont at $\frac{1}{4}$ cor. Sta. 92+20.2 ✓

Top Bolt $\frac{1}{4}$ cor. N. of Snelling Sta. 79+06.90

Boat Spike in T.R. 20' Lt Sta. 64+15

Ctr. Mont & of Larp. & Cleveland Ave.

Boat spike in T.R. 20' Lt Sta 40+90

R.R. spike in T.P. 20' Lt. Sta. 27+03. (Fulham St)

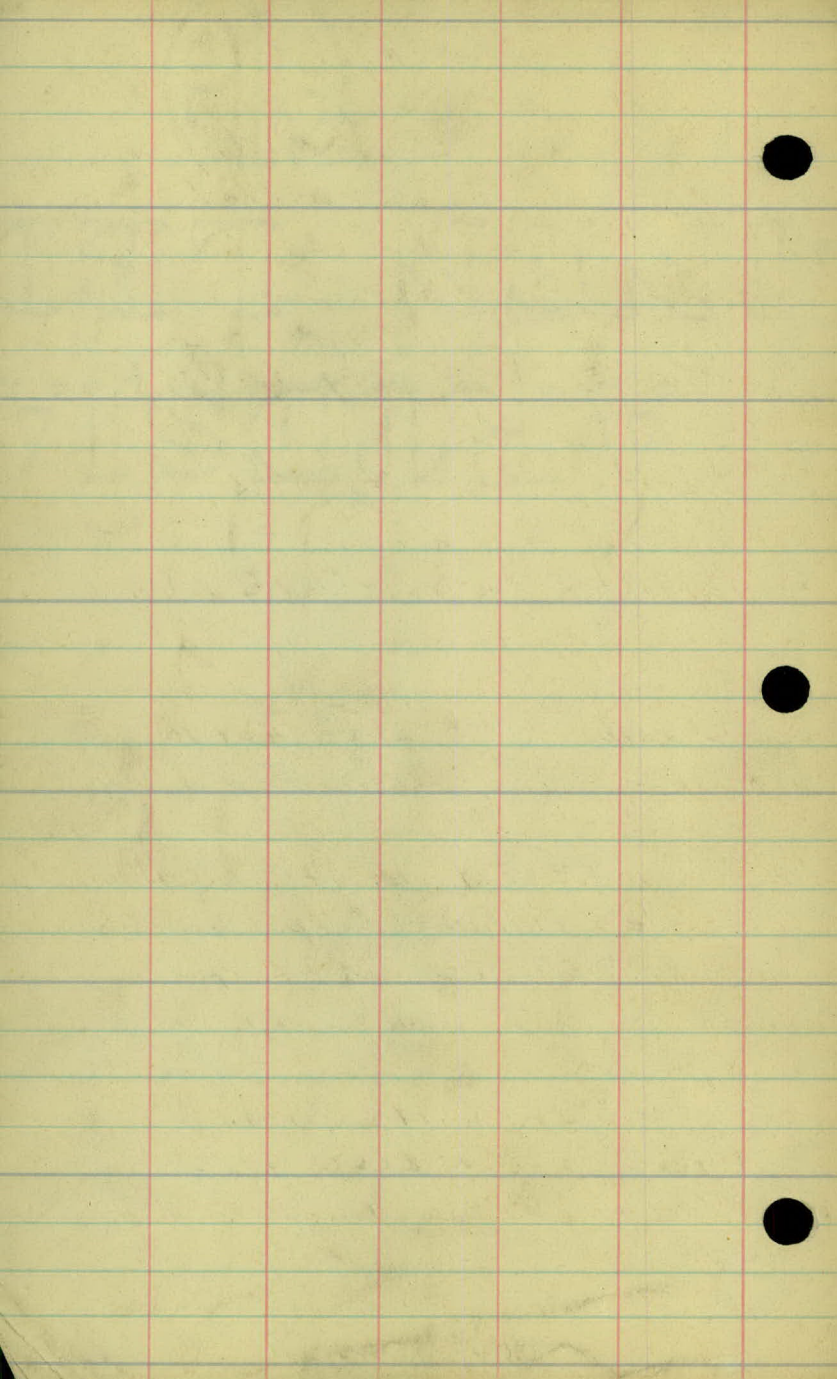
Iron plate & Fulham & Larp.

spike in P.P. Int. Pleasant & Larp.

spike in P.P. Int. Carl & Larp.

R.R. spike in P.P. 15' Rt Sta. 12+12

Top Fire Hyd. 0.0-100 and 20' Lt.



3-14-30

Larpenteur Ave

- Original -

X. Sections

W. Co. line To Dale St.

{ Weber
Beaton
Skoglund
Bell. }

Sta.	+	H.I.	-	Elev.
B.M.	3.71	918.51 ✓		914.80

0+00				17.93
------	--	--	--	-------

+06				18.16
-----	--	--	--	-------

+18				
-----	--	--	--	--

+34				
-----	--	--	--	--

+65				
-----	--	--	--	--

T.P.	12.35	930.14 ✓	0.72	917.79 ✓
------	-------	----------	------	----------

0+00				
------	--	--	--	--

+06				
-----	--	--	--	--

+18				18.79
-----	--	--	--	-------

+34				19.74
-----	--	--	--	-------

+65				22.09
-----	--	--	--	-------

+92				23.64
-----	--	--	--	-------

1+00				24.14
------	--	--	--	-------

3-14-30 Lt £ Rt

Top Fire Hyd. 0.0 - 100' 20 Lt.

0.58 0.95 1.2 7.0 9.6 12.0 16.2
19 20 45 65 89 103

0.35 0.65 1.4 4.2 8.8 12.2
17 31 50 91 100

11.3
- 1.3 1.2 3.8 7.6 9.6
32 50 76 100

- 1.2 5.7 8.2 9.5
34 55 100

Face of Gar. -3.6 2.6 5.8 9.4 10.0 10.8 14
32 41 42 60 91 100

Bldg. Corb 12.2
100 10.9 11.5 12.4 12.3
78 50 25 24 19

Bldg. 12.0
9.8 10.6 11.35 12.05 12.05
78 50 20 20 18

Bldg.
9.5 10.0 11.0 11.35 11.35 11.55
78 50 30 46 15

Bldg.
9.2 9.4 9.7 10.7 10.25 10.4 10.5 11.0
78 50 36 20 12 13 21

Bldg.
9.0 9.0 8.7 8.15 8.05 8.1 8.1 9.0 9.0 8.5
78 50 23 10 10 14 15 17 18

Bldg. Wall.
8.0 8.0 7.4 6.6 6.5 6.5 6.3 7.0 7.0 6.2 5.7 11.6
78 50 25 10 10 14 15 17 18 30 40

Bldg. Bldg.
7.2 7.2 7.0 6.5 6.7 6.1 6.0 6.1 5.8 6.5 6.5 5.7 5.0
78 50 37 36 17 10 10 14 15 17 18 41

930.14 ✓

+50

27.11

+71

28.39

+83

29.19

2+00

29.94 ✓

T.P

10.52 940.08 ✓ 0.58 929.56 ✓

+50

32.93

+90

35.03

3+05.

Sections on Lt = Top R.R. Cut. 35.98

+22

Sections on Lt. come in Ctr. of fill 36.83

T.P

432 943.17 ✓ 1.23 938.85 ✓

+63

Top of Bridge 38.30

+90

Top R.R. Cut on Rt. only 37.67

+96

= End of Bridge + Top of R.R. Cut on Lt. 37.47

4+50

37.97

5+00

38.37

Lt ~~E~~ Pt.

$\frac{1.6}{100}$ $\frac{37}{50}$ $\frac{37}{32}$ $\frac{3.0}{70}$ $\frac{3.05}{10}$ $\frac{3.1}{26}$ $\frac{3.5}{50}$ $\frac{3.1}{50}$ $\frac{3.6}{100}$

$\frac{1.80}{100}$ $\frac{34}{50}$ $\frac{34}{24}$ $\frac{2.0}{18}$ $\frac{1.75}{10}$ $\frac{1.75}{10}$ $\frac{1.85}{10}$ $\frac{2.5}{16}$ $\frac{3.0}{50}$ $\frac{3.8}{100}$

$\frac{9.8}{100}$ $\frac{103}{60}$ $\frac{9.8}{40}$ $\frac{7.5}{31}$ $\frac{1.0}{19}$ $\frac{1.0}{10}$ $\frac{0.95}{10}$ $\frac{1.0}{10}$ $\frac{0.8}{14}$ $\frac{1.5}{15}$ $\frac{1.5}{17}$ $\frac{1.0}{18}$ $\frac{3.5}{53}$ $\frac{3.5}{100}$

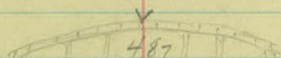
$\frac{10.2}{100}$ $\frac{112}{60}$ $\frac{10.6}{45}$ $\frac{8.4}{33}$ $\frac{0.0}{19}$ $\frac{0.25}{10}$ $\frac{0.2}{10}$ $\frac{0.2}{10}$ $\frac{0.0}{14}$ $\frac{0.5}{15}$ $\frac{0.7}{17}$ $\frac{0.0}{18}$ $\frac{2.4}{63}$ $\frac{3.4}{100}$

$\frac{16.2}{100}$ $\frac{118}{53}$ $\frac{7.8}{39}$ $\frac{9.0}{35}$ $\frac{9.0}{29}$ $\frac{7.1}{23}$ $\frac{7.2}{10}$ $\frac{7.15}{10}$ $\frac{7.3}{14}$ $\frac{7.3}{15}$ $\frac{7.8}{17}$ $\frac{7.8}{18}$ $\frac{7.3}{50}$ $\frac{9.1}{75}$ $\frac{11.7}{100}$

$\frac{9.2}{100}$ $\frac{6.8}{75}$ $\frac{3.7}{38}$ $\frac{5.7}{31}$ $\frac{4.6}{24}$ $\frac{4.9}{14}$ $\frac{5.05}{15}$ $\frac{5.1}{33}$ $\frac{5.6}{74}$ $\frac{10.0}{74}$ $\frac{11.2}{100}$

$\frac{3.7}{100}$ $\frac{1.7}{65}$ $\frac{0.0}{46}$ $\frac{3.8}{26}$ $\frac{4.0}{17}$ $\frac{4.1}{18}$ $\frac{4.2}{31}$ $\frac{4.7}{70}$ $\frac{8.6}{70}$ $\frac{9.4}{100}$

Bridges SH.
 $\frac{3.25}{20}$ $\frac{3.2}{21}$ $\frac{3.6}{29}$ $\frac{10.0}{35}$ $\frac{8.7}{70}$ $\frac{9.2}{90}$ $\frac{9.6}{100}$



Lt. side come on Cut. $\frac{5.5}{26}$ $\frac{7.2}{54}$ $\frac{10.8}{75}$ $\frac{12.0}{100}$ $\frac{10.5}{100}$

$\frac{1.0}{100}$ $\frac{2.8}{50}$ $\frac{3.7}{32}$ $\frac{5.5}{26}$ $\frac{5.4}{19}$ $\frac{5.7}{19}$ $\frac{5.7}{50}$ $\frac{10.0}{100}$ $\frac{13.3}{100}$

$\frac{2.4}{100}$ $\frac{4.0}{60}$ $\frac{5.0}{34}$ $\frac{6.0}{32}$ $\frac{6.5}{26}$ $\frac{5.2}{22}$ $\frac{5.2}{10}$ $\frac{5.2}{10}$ $\frac{5.3}{17}$ $\frac{5.4}{25}$ $\frac{6.7}{60}$ $\frac{9.4}{100}$ $\frac{12.6}{100}$

$\frac{5.0}{100}$ $\frac{6.0}{60}$ $\frac{6.5}{34}$ $\frac{7.7}{31}$ $\frac{7.6}{24}$ $\frac{5.6}{20}$ $\frac{4.7}{10}$ $\frac{4.8}{10}$ $\frac{5.0}{15}$ $\frac{5.0}{22}$ $\frac{8.5}{60}$ $\frac{10.0}{78}$ $\frac{10.4}{100}$ $\frac{13.0}{100}$

Sta.

943.17

5+50

38.87

+77

12" x 40' C.M.

6

39.72

+50

40.87

+57

W. Toe Shoulder Dr. on Lt 41.12

T.P.

10.02 951.36 ✓ 1.83 941.34 ✓

+61

41.21

+78

41.71

+82

41.81

+94

42.16

7

42.31

+50

43.61

+54

43.76

8

45.06

Lt.

E

Rt

4.8	6.6	7.2	4.5	4.25	4.3	4.45	4.6	10.4	12.6	15.0
<u>100</u>	<u>60</u>	<u>22</u>	<u>15</u>	<u>10</u>		<u>10</u>	<u>15</u>	<u>25</u>	<u>50</u>	<u>100</u>

← Floor line

7.5	10.65
<u>19</u>	<u>21</u>

3.7	6.4	6.4	3.6	3.55	3.45	3.7	3.8	9.5	12.6	13.0	10.
<u>100</u>	<u>46</u>	<u>29</u>	<u>15</u>	<u>10</u>		<u>10</u>	<u>15</u>	<u>25</u>	<u>46</u>	<u>60</u>	<u>100</u>

1.0	3.0	4.3	3.7	2.5	2.3	2.5	2.8	7.2	9.4	9.8	9.
<u>100</u>	<u>60</u>	<u>38</u>	<u>19</u>	<u>16</u>	<u>10</u>	<u>10</u>	<u>15</u>	<u>22</u>	<u>41</u>	<u>70</u>	<u>100</u>

0.0	3.2	3.2	2.2	2.1	2.5	2.35	2.5	7.3	8.5	9.6	8.8
<u>100</u>	<u>50</u>	<u>24</u>	<u>19</u>	<u>10</u>		<u>10</u>	<u>15</u>	<u>24</u>	<u>34</u>	<u>71</u>	<u>100</u>

8.0	9.6	10.3	10.15	10.15	10.45	10.7	15.5	17.6	16.8
<u>100</u>	<u>60</u>	<u>24</u>	<u>10</u>		<u>10</u>	<u>15</u>	<u>25</u>	<u>60</u>	<u>100</u>

8.0	9.0	10.1	9.7	9.65	10.0	10.1	13.7	16.0	17.5	17.
<u>100</u>	<u>60</u>	<u>23</u>	<u>10</u>		<u>10</u>	<u>14</u>	<u>22</u>	<u>30</u>	<u>60</u>	<u>100</u>

8.0	9.0	9.6	10.3	11.0	9.7	9.6	9.55	9.8	10.0	14.0	16.0	17.0
<u>100</u>	<u>80</u>	<u>60</u>	<u>45</u>	<u>18</u>	<u>15</u>	<u>10</u>		<u>10</u>	<u>15</u>	<u>22</u>	<u>29</u>	<u>100</u>

8.0	8.4	9.0	11.0	10.6	9.3	9.35	9.2	9.4	9.7	15.0	16.5	16.5
<u>100</u>	<u>76</u>	<u>60</u>	<u>33</u>	<u>17</u>	<u>15</u>	<u>10</u>		<u>10</u>	<u>15</u>	<u>25</u>	<u>60</u>	<u>100</u>

7.7	8.7	9.7	9.2	9.05	9.2	9.5	14.6	16.0	16.0
<u>100</u>	<u>60</u>	<u>24</u>	<u>10</u>		<u>10</u>	<u>15</u>	<u>25</u>	<u>60</u>	<u>100</u>

7.0	7.4	8.1	7.85	7.8	7.75	7.85	8.0	12.7	14.0	15.0
<u>100</u>	<u>60</u>	<u>15</u>	<u>10</u>			<u>10</u>	<u>15</u>	<u>24</u>	<u>60</u>	<u>100</u>

4.7	8.4	9.0	8.0	7.7	7.6	7.65	8.0	12.2	13.5	14.5
<u>100</u>	<u>54</u>	<u>18</u>	<u>14</u>	<u>10</u>		<u>10</u>	<u>15</u>	<u>25</u>	<u>60</u>	<u>100</u>

4.6	7.2	8.0	7.8	6.4	6.4	6.3	6.4	6.5	10.0	10.5	11.2
<u>100</u>	<u>60</u>	<u>36</u>	<u>17</u>	<u>15</u>	<u>10</u>		<u>10</u>	<u>16</u>	<u>24</u>	<u>60</u>	<u>100</u>

8		951.36 ✓			
+25					45.86
+50					46.61
T.P.	6.87	957.88 ✓	0.35	951.01 ✓	
9					48.0
+50					49.4
+77					W. Toe of Shoulder Malvern 50.1
+80					Top Shoulder 50.4
+94					E. Malvern 50.7
10 + 08.0					Top Shoulder ✓ 51.2
T.P.	10.82	963.16 ✓	5.54	952.34 ✓	
+14					E Toe Shoulder 51.3
+21					Reg. Ditch on Lt. 51.5
+63					52.8
11					53.9
+50					55.2
T.P.					
T.P.		561		957.55 ✓	53

Lt.

±

RT

4.7	6.5	6.7	5.6	5.5	5.5	5.6	5.6	7.8	7.7	7.5	9.2	9.2
100	60	17	14	10		10	15	20	41	68	71	75

4.2	5.5	5.7	5.0	4.8	4.75	4.95	5.1	6.8	7.0	4.5	4.0	5.8
100	60	17	15	10		10	15	19	29	31	60	65

9.9

8.2	9.2	9.3	10.2	11.2	9.7	9.7	9.85	10.1	10.0	11.7	11.8	4.4	4.4	5.7	5.5
100	60	23	21	17	15	10		10	15	21	27	33	47	50	55

8.5

8.0	8.1	8.5	9.0	9.0	8.5	8.45	8.45	8.55	8.6	9.8	9.8	5.1	4.8	8.6	9.4
100	60	22	21	18	16	10		10	16	20	28	33	42	47	84

Flowline $\xrightarrow{\text{Culvert}}$

8.0	8.6	9.3	7.7	7.7	7.8	7.8	7.8	9.2	9.2	6.8	7.7	8.2	3.0	1.0
100	26		21	10	10	16	19	27	31	35	68	75	100	

7.1	7.6	7.4	7.55	7.5	7.65	8.0	9.0	9.0	6.5	7.8	8.0	2.4
100	60	28	10		10	16	20	28	31	33	67	74

N

5.8	6.7	7.15	7.15	7.3	7.4	8.4	8.6	6.8	7.4	2.0	0.2
100	50	10		10	15	19	28	30	60	70	100

6.0	6.8	6.7	6.7	6.9	6.9	7.8	7.1	6.1	6.2	1.2	1.2
100	60	10		10	15	17	28	30	53	61	100

Flowline $\xrightarrow{\text{Culvert}}$

12.0	13.6	13.0	13.5	12.0	11.8	11.85	11.95	12.0	12.5	12.5	11.2	11.5	5.8	4.0
100	60	26		19	10		10	20	22	28	29	47	60	100

12.6	13.2	12.0	12.5	12.0	11.65	11.7	11.75	12.0	12.6	12.6	10.8	7.1	6.5	5.5
100	60	27	20	17	10		10	18	20	27	29	42	48	60

12.0	12.0	10.0	11.5	10.2	10.4	10.4	10.5	10.6	11.4	5.4	5.5	5.5
100	60	26	20	16	10		10	17	26	32	60	100

9.7	11.3	8.4	10.0	9.8	9.3	9.2	9.3	9.4	9.6	9.4	4.8	5.8	6.8
100	67	27	22	17	15	10		10	15	25	29	60	100

6.2	8.2	7.7	7.1	8.5	8.1	8.0	7.95	8.05	8.0	8.0	4.6	4.7	7.7
100	58	46	24	22	15	10		10	15	25	28	54	100

R.R spike in R.P. 15' RT 54.2 12+12

4.33 961.86

957.53 ✓

12+00

56.4

+22

57.1

+50

57.7

7.67 ✓ 965.20

4.33

957.53 ✓

+95

W. side of Euslis No. Edge S.W. So. 58.8

13+05.0

W. Edge of Rd. bed So.

59.1

+09.93

E Euslis St. No.

59.1

+19.93

E " " So.

59.4

+32

E. Edge of Pav. So.

59.7

+37

E Ditch So.

59.8

+50

60.1

14

61.0

+29.5

Toe Wall on Lt.

61.5

+31

61.5

3-15-20 Lt

Rt.

RR spike in RR 15' Rt 12+12

5.3	4.8	4.8	5.4	5.45	5.45	5.55	5.2	4.2	5.0	7.0
100	60	33	18	10	10	10	29	32	60	100

Fence Edge SW.

4.6	3.0	3.6	4.3	5.1	4.8	4.8	4.9	4.5	5.0	6.5	Shed.
100	92	49	27	17	10	10	10	46	60	88	

Bldg.

Curb.

Bldg.

2.95	3.6	4.5	4.25	4.2	4.2	4.0	4.5
60	19	18	10	10	10	20	44

Spike in RR 15' Rt 5+12 12+12.

5.1	5.8	6.4	6.4	6.35	6.5	7.0	6.6	9.9	11.2
100	60	23	10	10	10	29	41	82	100

4.7	5.5	6.2	6.1	6.25	8.2	10.5	12.0
100	46	10	10	10	43	75	100

4.7	5.3	6.05	6.1	6.05	6.2	7.9	10.1	11.7
100	50	10	10	10	10	39	76	100

4.7	5.3	5.8	5.8	5.9	8.2	11.4
100	50	10	10	10	50	100

5.0	5.4	5.5	5.5	5.65	8.3	11.5
100	50	10	10	10	50	100

Top Catch Basin

Edge of R.

Flowline
Culv.

5.1	5.3	5.9	5.35	5.4	5.55	6.45	8.2	9.4	9.8	12.7
100	60	10	10	10	10	22	46	60	60	100

4.6	4.6	5.0	5.4	5.15	5.1	5.3	4.8	5.2	6.4	12.2
100	60	33	23	10	10	12	16	41	60	100

4.4	4.2	4.5	4.15	4.2	4.3	4.2	6.0	7.2	14.5
100	60	24	10	10	10	17	37	60	100

4.0	3.6	4.2	4.7	4.1	3.7	3.65	3.8	4.0	6.2	10.8	14.2
100	60	32	23	17	10	10	10	14	28	60	100

2.4	2.4	3.0	4.6	4.8	4.0	3.7	3.65	3.5	4.0	6.6	11.0	14.2
100	60	34	31	23	15	10	10	10	14	31	60	100

14 965.20 ✓
 + 64 ✓ 62.0
 10.93 968.46 ✓ 7.67 ✓ 957.53 ✓

15 62.5

+16 62.7

+50 63.1

+57 63.2

+77 63.5

+84 63.7

+8737 = ± Carl St.

16 63.8

+06. 63.9

+15 64.0

+28 64.3

+50 64.6

+78 65.0

LT.

\$

RT

1.2 15 2.5 4.0 4.4 3.6 3.2 3.2 3.4 3.5 10.0 11.8 12.3
 100 60 34 31 23 18 10 10 13 26 44 100
 RR spike 10 RR 15' RT 34.12-12

3-17-30 - 30° F. A.M.

4.3 4.8 6.0 7.7 7.7 6.4 5.95 5.95 6.25 6.3 13.2 14.2 14.0 100
 100 60 34 30 22 18 10 10 14 25 40 60 100

5.0 5.4 6.2 7.2 7.2 6.1 5.7 5.75 5.95 6.1 12.6 13.0 10.1
 100 60 32 29 23 17 10 10 15 27 37 100

5.3 5.6 6.4 7.0 6.2 5.6 5.4 5.35 5.45 6.4 6.5 6.5
 100 60 30 28 19 17 10 10 35 60 100

5.4 10.6 6.7 6.1 6.7 6.7 6.0 5.3 5.3 5.4 6.4 5.8 5.7
 100 54 49 30 28 20 17 10 10 19 60 100

11.2 11.4 6.9 5.5 5.0 5.2 6.0 5.5 5.4
 100 44 37 10 10 20 60 100

11.1 11.6 7.7 5.0 4.95 5.5 6.0 5.5 5.5
 100 76 52 10 10 20 60 100

9.7 8.0 7.0 4.7 4.7 4.8 5.7 5.4 5.4 5.0
 100 60 33 10 10 21 32 60 100

9.4 8.1 9.2 8.4 6.3 4.7 4.6 4.7 5.6 5.4 5.0
 100 60 50 37 30 10 10 20 60 100

9.2 11.2 10.3 6.7 5.6 6.2 5.8 4.8 4.6 4.5 4.6 5.4 5.3 5.0
 100 82 60 43 29 27 20 17 10 10 21 60 100

11.1 6.9 3.7 4.6 5.8 5.6 4.3 4.3 4.2 4.3 5.3 5.3 5.0
 110 83 42 29 26 18 15 10 10 21 60 100

21.5 7.5 7.4 4.7 4.7 3.9 3.8 3.8 4.1 5.2 5.4 5.2
 100 24 29 26 25 24 18 15 10 10 21 60 100

4.5 2.0 1.6 2.4 5.2 5.2 4.0 4.1 3.5 3.4 3.45 3.75 5.0 5.6 5.6
 100 83 60 31 25 24 23 18 15 10 10 21 60 100

968.46 ✓

17

T.P. 5.98 ✓ 970.99 3.45 965.01 ✓ 65.2

+38 65.7

+41 65.7

+50 65.8

18 66.3

+36 66.9

+41 67.0

+77 67.4

+81 67.5

19 67.7

+50 68.2

+69 N. Edge of Pleasant ✓ 68.5 ✓

T.P. 9.09 977.46 ✓ 2.62 968.37 ✓

T.P. 7.43 976.29 ✓ 8.60 968.86 ✓

+89.92 = 2 Pleasant. 68.9

L+

K

K+

Porch → $\frac{2.2}{51} \frac{2.5}{31} \frac{3.7}{27} \frac{4.0}{17} \frac{3.1}{15} \frac{3.1}{10} \overset{3.3}{3.25} \frac{3.55}{10} \frac{3.8}{13} \frac{5.3}{25} \frac{6.2}{60} \frac{6.2}{100}$

Porch → $\frac{4.8}{51} \frac{5.7}{19} \frac{5.2}{15} \frac{5.2}{10} \frac{5.3}{10} \frac{5.55}{10} \frac{5.5}{14} \frac{7.6}{28} \frac{9.0}{60} \frac{10.0}{100}$

Porch → $\frac{4.8}{51} \frac{5.8}{50} \frac{5.2}{15} \frac{5.2}{10} \frac{5.3}{10} \frac{5.55}{10} \frac{5.3}{14} \frac{9.0}{33} \frac{10.2}{60} \frac{11.0}{100}$

House → $\frac{4.8}{59} \frac{5.4}{22} \frac{5.2}{15} \frac{5.05}{10} \frac{5.2}{10} \frac{5.5}{10} \frac{5.5}{14} \frac{7.8}{18} \frac{9.1}{33} \frac{10.2}{60} \frac{11.2}{100}$

$\frac{4.4}{100} \frac{4.7}{60} \frac{5.0}{23} \frac{4.7}{16} \frac{4.6}{10} \overset{4.7}{4.65} \frac{4.9}{10} \frac{5.1}{14} \frac{7.7}{19} \frac{9.3}{26} \frac{10.7}{60} \frac{11.8}{100}$

$\frac{4.0}{100} \frac{4.3}{60} \frac{4.1}{15} \frac{4.05}{10} \overset{4.1}{4.05} \frac{4.3}{10} \frac{4.4}{14} \frac{9.0}{27} \frac{10.0}{60} \frac{11.7}{100}$

$\frac{6.0}{100} \frac{6.5}{60} \frac{6.1}{24} \frac{4.1}{15} \frac{4.0}{10} \frac{4.0}{40} \frac{4.2}{10} \frac{4.4}{15} \frac{8.2}{25} \frac{10.0}{60} \frac{11.7}{100}$

$\frac{4.7}{100} \frac{6.0}{60} \frac{6.0}{25} \frac{3.7}{15} \frac{3.6}{10} \frac{3.60}{10} \frac{3.8}{10} \frac{3.9}{14} \frac{5.7}{18} \frac{7.2}{27} \frac{9.0}{60} \frac{11.6}{100}$

$\frac{3.6}{100} \frac{3.6}{60} \frac{4.5}{17} \frac{3.8}{15} \frac{3.5}{10} \frac{3.5}{10} \frac{3.7}{10} \frac{3.9}{15} \frac{6.2}{19} \frac{7.1}{27} \frac{9.0}{60} \frac{11.5}{100}$

Porch → $\frac{3.6}{57} \frac{4.0}{16} \frac{3.3}{15} \frac{3.3}{10} \frac{3.3}{10} \frac{3.45}{10} \frac{3.5}{14} \frac{6.3}{22} \frac{8.7}{60} \frac{11.2}{100}$

$\frac{0.8}{100} \frac{2.5}{60} \frac{4.3}{33} \frac{3.0}{18} \frac{2.8}{10} \frac{2.8}{10} \frac{3.0}{10} \frac{3.0}{15} \frac{5.0}{19} \frac{6.2}{45} \frac{7.7}{60} \frac{11.0}{100}$

$\frac{1.7}{100} \frac{2.2}{82} \frac{2.5}{50} \frac{2.5}{10} \frac{2.5}{10} \frac{2.6}{10} \frac{2.7}{15} \frac{4.7}{22} \frac{6.4}{51} \frac{10.0}{85} \frac{11.0}{100}$

spike in P.P. Int. Pleasant and Larp. Ave.

$\frac{6.2}{100} \frac{6.8}{50} \frac{7.4}{10} \frac{7.4}{10} \frac{7.6}{10} \frac{7.7}{15} \frac{9.6}{23} \frac{11.2}{43} \frac{15.5}{100}$

20

976.29 ✓

+ 09.

69.1

+ 15

69.2

+ 50

69.7

21

70.4

+ 55

71.0

22

71.3

+ 50

71.7

23

72.2

+ 50

72.5

+ 75

72.6

24

72.7

+ 31

73.0

+ 50

73.2 ✓

T.P.

7.01

982.03 ✓

1.27

975.02 ✓

L+

L

R+

$$\begin{array}{r} 6.4 \quad 7.0 \quad 7.2 \quad 7.05 \quad 7.12 \\ \hline 100 \quad 60 \quad 16 \quad 10 \quad 7.15 \end{array} \quad \begin{array}{r} 7.35 \quad 7.5 \quad 9.2 \quad 10.0 \quad 11.8 \quad 15.5 \\ \hline 10 \quad 14 \quad 20 \quad 29 \quad 55 \quad 100 \end{array}$$

$$\begin{array}{r} 52 \quad 6.0 \quad 62 \quad 75 \quad 7.0 \quad 6.85 \quad 7.1 \\ \hline 100 \quad 82 \quad 40 \quad 17 \quad 15 \quad 10 \quad 7.05 \end{array} \quad \begin{array}{r} 7.2 \quad 7.4 \quad 8.8 \quad 10.0 \quad 11.8 \quad 15.5 \\ \hline 10 \quad 14 \quad 18 \quad 29 \quad 55 \quad 100 \end{array}$$

$$\begin{array}{r} 4.0 \quad 5.5 \quad 63 \quad 8.0 \quad 8.0 \quad 6.7 \quad 6.6 \\ \hline 100 \quad 41 \quad 34 \quad 30 \quad 19 \quad 15 \quad 10 \end{array} \quad \begin{array}{r} 6.6 \quad 6.7 \quad 7.0 \quad 9.5 \quad 10.8 \quad 15.0 \\ \hline 10 \quad 16 \quad 17 \quad 26 \quad 48 \quad 100 \end{array}$$

$$\begin{array}{r} 8.0 \quad 7.7 \quad 62 \quad 6.0 \quad 5.9 \quad 6.0 \quad 6.2 \quad 8.2 \quad 12.0 \quad 14.2 \\ \hline 30 \quad 20 \quad 15 \quad 10 \quad 10 \quad 16 \quad 28 \quad 60 \quad 100 \end{array}$$

$$\begin{array}{r} 4.3 \quad 5.0 \quad 7.0 \quad 6.9 \quad 5.2 \quad 5.3 \quad 5.3 \\ \hline 36 \quad 32 \quad 28 \quad 20 \quad 14 \quad 10 \quad 5.25 \end{array} \quad \begin{array}{r} 5.4 \quad 5.8 \quad 7.0 \quad 12.0 \quad 13.6 \\ \hline 18 \quad 15 \quad 19 \quad 60 \quad 100 \end{array}$$

$$\begin{array}{r} 6.0 \quad 6.5 \quad 4.9 \quad 5.0 \quad 5.0 \quad 5.05 \quad 5.1 \quad 7.0 \quad 8.3 \quad 11.4 \quad 13.2 \\ \hline 30 \quad 18 \quad 14 \quad 10 \quad 10 \quad 14 \quad 23 \quad 27 \quad 53 \quad 100 \end{array}$$

$$\begin{array}{r} 6.4 \quad 6.2 \quad 4.4 \quad 4.55 \quad 4.6 \quad 4.7 \quad 4.8 \quad 7.2 \quad 8.8 \quad 11.0 \quad 12.15 \\ \hline 29 \quad 19 \quad 14 \quad 10 \quad 10 \quad 15 \quad 24 \quad 28 \quad 50 \quad 78 \quad 100 \end{array}$$

$$\begin{array}{r} 5.8 \quad 5.6 \quad 4.4 \quad 4.15 \quad 4.1 \quad 4.2 \quad 4.4 \quad 6.8 \quad 9.8 \quad 11.7 \quad 11.0 \\ \hline 29 \quad 20 \quad 16 \quad 10 \quad 10 \quad 15 \quad 21 \quad 33 \quad 69 \quad 100 \end{array}$$

$$\begin{array}{r} 4.4 \quad 4.6 \quad 3.8 \quad 3.7 \quad 3.8 \\ \hline 31 \quad 18 \quad 15 \quad 10 \quad 3.75 \end{array} \quad \begin{array}{r} 3.90 \quad 4.0 \quad 6.0 \quad 7.2 \quad 9.0 \quad 10.2 \\ \hline 10 \quad 15 \quad 19 \quad 27 \quad 31 \quad 100 \end{array}$$

$$\begin{array}{r} 4.9 \quad 4.9 \quad 3.8 \quad 3.6 \quad 3.65 \quad 3.85 \quad 3.9 \quad 5.3 \quad 6.3 \quad 8.3 \quad 10.0 \quad 9.4 \\ \hline 30 \quad 19 \quad 15 \quad 10 \quad 10 \quad 15 \quad 18 \quad 27 \quad 35 \quad 67 \quad 100 \end{array}$$

$$\begin{array}{r} 4.9 \quad 4.6 \quad 3.5 \quad 3.55 \quad 3.55 \quad 3.7 \quad 3.8 \quad 5.4 \quad 5.7 \quad 7.4 \quad 9.4 \quad 8.8 \\ \hline 29 \quad 19 \quad 15 \quad 10 \quad 10 \quad 10 \quad 15 \quad 20 \quad 26 \quad 33 \quad 66 \quad 100 \end{array}$$

$$\begin{array}{r} 5.0 \quad 5.0 \quad 4.1 \quad 3.3 \quad 3.3 \quad 3.25 \quad 3.4 \quad 3.5 \quad 4.5 \quad 7.0 \quad 8.5 \quad 7.2 \\ \hline 27 \quad 25 \quad 23 \quad 16 \quad 10 \quad 10 \quad 15 \quad 18 \quad 33 \quad 63 \quad 100 \end{array}$$

$$\begin{array}{r} 4.6 \quad 4.6 \quad 3.4 \quad 2.9 \quad 3.1 \quad 3.1 \quad 3.3 \quad 3.3 \quad 4.3 \quad 7.0 \quad 8.0 \quad 6.2 \\ \hline 28 \quad 26 \quad 24 \quad 16 \quad 10 \quad 10 \quad 16 \quad 18 \quad 34 \quad 60 \quad 100 \end{array}$$

Next Page

982.03 ✓

21

+55

22

+50

23

+50

+75

24

+31

+50

T.R

469

979.71 ✓

7.01

975.02 ✓

25

73.5

+50

74.0

+75

74.2

LT

~~+~~

RT

$$\frac{6.2}{100} \quad \frac{10.0}{48} \quad \frac{9.8}{34} \quad 11.6$$

$$\frac{2.7}{100} \quad \frac{3.6}{80} \quad \frac{5.4}{49} \quad \frac{5.4}{40} \quad 11.0$$

$$\frac{4.0}{100} \quad \frac{6.4}{44} \quad \frac{7.2}{34} \quad 10.8$$

$$\frac{4.7}{100} \quad \frac{7.4}{42} \quad \frac{7.8}{33} \quad 10.3$$

$$\frac{6.2}{100} \quad \frac{6.8}{88} \quad \frac{8.5}{42} \quad \frac{8.0}{33} \quad 9.8$$

$$\frac{8.0}{100} \quad \frac{9.0}{40} \quad \frac{9.0}{32} \quad 9.5$$

$$\frac{9.0}{100} \quad \frac{9.0}{40} \quad \frac{9.0}{32} \quad 9.4$$

$$\frac{9.4}{100} \quad \frac{7.6}{60} \quad \frac{8.0}{41} \quad \frac{7.6}{32} \quad 9.3$$

$$\frac{9.2}{100} \quad \frac{7.4}{76} \quad \frac{6.2}{60} \quad \frac{6.6}{40} \quad \frac{6.6}{32} \quad 9.0$$

$$\frac{10.0}{100} \quad \frac{8.0}{73} \quad \frac{7.2}{47} \quad \frac{7.6}{38} \quad \frac{7.2}{32} \quad 8.8$$

$$\frac{9.5}{100} \quad \frac{8.6}{68} \quad \frac{8.4}{33} \quad \frac{7.7}{17} \quad \frac{6.2}{14} \quad \frac{6.2}{10} \quad 6.2 \quad \frac{6.3}{10} \quad \frac{6.4}{15} \quad \frac{8.2}{18} \quad \frac{10.0}{35} \quad \frac{10.6}{50} \quad \frac{9.2}{100}$$

$$\frac{10.0}{100} \quad \frac{10.6}{77} \quad \frac{9.0}{33} \quad \frac{7.5}{18} \quad \frac{5.9}{14} \quad \frac{5.8}{10} \quad 5.7 \quad \frac{5.8}{10} \quad \frac{5.8}{14} \quad \frac{7.2}{18} \quad \frac{9.4}{36} \quad \frac{10.0}{55} \quad \frac{9.2}{100}$$

$$\frac{10.0}{100} \quad \frac{9.5}{60} \quad \frac{8.8}{35} \quad \frac{7.8}{29} \quad \frac{7.0}{18} \quad \frac{5.8}{14} \quad \frac{5.6}{10} \quad 5.5 \quad \frac{5.6}{10} \quad \frac{5.8}{15} \quad \frac{7.2}{19} \quad \frac{10.1}{44} \quad \frac{10.1}{60} \quad \frac{9.4}{100}$$

979.71
4.14
975.57

26

74.5

+10

74.6

+14

74.6

+22

74.6

+26

74.6

+39.91 = £ Fulham.

74.8

+55

74.9

+59

75.0

+66

75.0

+70

75.1

2.68 978.25 4.14 975.57

27

75.2

+50

75.6

28

75.9

L1

L2

R1

92
 $\frac{92}{100}$ 7.0 6.1 5.6 7.4 7.2 5.5 5.4 5.2 5.3 5.3 9.1 10.6 10.2 9.5
 60 46 32 29 21 16 10 10 14 29 47 86 100

8.5 5.0 5.0 7.5 7.5 5.3 5.3 5.1 5.2 5.4 8.8 11.0 11.0 9.5
 $\frac{8.5}{100}$ 55 34 32 23 20 10 10 15 28 50 73 100

7.8 7.2 6.8 7.2 5.2 5.3 5.1 5.2 5.5 9.0 10.8 11.6 9.8
 $\frac{7.8}{100}$ 78 52 31 24 10 10 15 29 50 75 100

7.2 7.0 6.7 5.2 5.2 5.1 5.1 5.2 9.5 11.2 11.7 9.6
 $\frac{7.2}{100}$ 75 44 33 10 10 15 30 47 82 100

5.1
 $\frac{4.4}{100}$ 50 5.2 5.5 5.1 5.5 9.2 11.3 12.9 10.2
 50 10 10 15 29 50 72 100

4.0 4.3 5.0 4.9 5.0 5.4 9.1 12.0 12.7 10.6
 $\frac{4.0}{100}$ 50 10 10 15 21 50 70 100

4.8
 $\frac{4.2}{100}$ 4.6 4.9 4.75 4.8 5.1 9.0 10.2 12.5 13.0 12.5
 50 10 10 14 22 29 60 75 100

6.2 6.2 4.7 4.9 4.7 4.5 5.2 8.8 12.0 13.4 11.4
 $\frac{6.2}{100}$ 44 34 10 10 15 22 50 75 100

6.2 6.2 6.6 4.6 4.8 4.7 4.7 5.2 7.8 12.0 13.2 11.6
 $\frac{6.2}{100}$ 60 28 19 10 10 15 19 50 75 100

5.0 3.0 3.7 6.8 7.0 4.8 4.8 4.6 4.6 5.2 11.7 10.2 13.0 11.6
 $\frac{5.0}{100}$ 77 33 29 22 17 10 10 15 19 33 75 100
 R.R. in F.R. 20' L1 Sta. 27+03.

3-18-30 23° F. A.M. Snowing Clear P.M.

3.1
 $\frac{4.6}{29}$ 4.0 3.1 3.05 3.05 3.1 3.1 5.7 8.8 10.6 10.6 9.6
 17 15 10 10 15 22 43 64 82 100

4.6 4.2 2.9 2.8 2.7 2.7 2.9 6.1 8.1 10.0 10.0 7.4
 $\frac{4.6}{28}$ 20 15 10 10 15 20 35 60 82 100

3.6 3.6 2.4 2.5 2.4 2.4 2.7 6.0 8.0 9.2 9.2 4.8
 $\frac{3.6}{28}$ 20 15 10 10 15 21 37 53 73 100

978.25

+ 43

76.1

+ 80

76.2

29

76.3

+ 50

76.4

30

76.3

+ 50

76.1

31

76.1

1224 987.81 ✓ 2.68 975.57 ✓

27 T.P.

5.36 991.50 ✓ 1.67 986.14 ✓

27

~~+ 50~~

+ 50

~~28~~

28

~~+ 43~~

+ 43

~~+ 80~~

+ 80

~~29~~

29

Lt

≠

Rt

$$\begin{array}{cccccccccccc} & & & & & & & & & F & & & & \\ \frac{2.5}{26} & \frac{2.8}{20} & \frac{1.9}{16} & \frac{2.3}{10} & 2.2 & \frac{2.2}{10} & \frac{2.4}{15} & \frac{5.2}{20} & \frac{7.2}{41} & \frac{8.2}{51} & \frac{8.2}{67} & \frac{5.2}{100} \end{array}$$

$$\begin{array}{cccccccccccc} & & & & 2.1 & & & & & F & & & \\ \frac{3.8}{28} & \frac{4.3}{20} & \frac{2.1}{16} & \frac{2.1}{10} & 2.05 & \frac{2.05}{10} & \frac{2.2}{16} & \frac{4.2}{20} & \frac{5.2}{28} & \frac{7.4}{44} & \frac{10.1}{86} & \frac{12}{100} \end{array}$$

$$\begin{array}{cccccccccccc} & & & & & & & & & F & & & \\ \frac{4.0}{27} & \frac{4.5}{20} & \frac{2.3}{16} & \frac{2.05}{10} & 2.0 & \frac{2.0}{10} & \frac{2.1}{16} & \frac{5.0}{21} & \frac{5.8}{27} & \frac{4.6}{29} & \frac{6.6}{44} & \frac{10.1}{68} & \frac{12}{100} \end{array}$$

$$\begin{array}{cccccccccccc} & & & & & & & & & F & & & \\ \frac{3.0}{26} & \frac{3.0}{18} & \frac{2.0}{15} & \frac{2.0}{10} & 1.9 & \frac{2.0}{10} & \frac{2.1}{17} & \frac{5.0}{22} & \frac{5.7}{28} & \frac{1.6}{33} & \frac{3.3}{46} & \frac{8.6}{90} & \frac{10.5}{100} \end{array}$$

$$\begin{array}{cccccccccccc} & & & & & & & & & F & & & \\ \frac{4.0}{27} & \frac{4.0}{18} & \frac{2.3}{15} & \frac{2.1}{10} & 2.0 & \frac{2.1}{10} & \frac{2.2}{16} & \frac{4.5}{20} & \frac{6.4}{33} & \frac{7.2}{46} & \frac{8.4}{68} & \frac{9.5}{100} \end{array}$$

$$\begin{array}{cccccccccccc} & & & & & & & & & F & & & \\ \frac{4.2}{26} & \frac{4.7}{19} & \frac{2.5}{15} & \frac{2.2}{10} & 2.2 & \frac{2.4}{10} & \frac{2.7}{15} & \frac{9.7}{26} & \frac{10.7}{46} & \frac{10.7}{77} & \frac{9.7}{100} \end{array}$$

$$\begin{array}{cccccccccccc} & & & & 2.2 & & & & & F & & & \\ \frac{5.0}{31} & \frac{5.5}{25} & \frac{2.5}{15} & \frac{2.2}{10} & 2.15 & \frac{2.3}{10} & \frac{2.4}{14} & \frac{8.7}{25} & \frac{10.0}{46} & \frac{11.0}{75} & \frac{11.3}{100} \end{array}$$

R.R. spike in T.R. 20 kt star, 27+03.

$$\begin{array}{cccc} 15.0 & 136 & 142 & 142 \\ 100 & 84 & 50 & 33 \end{array} \quad 16.3$$

$$\begin{array}{cccc} 14.8 & 126 & 127 & 132 \\ 100 & 87 & 50 & 33 \end{array} \quad 15.9$$

$$\begin{array}{cccc} 11.5 & 9.8 & 9.2 & 10.4 \\ 100 & 86 & 50 & 34 \end{array} \quad 15.6$$

$$\begin{array}{cccc} 3.3 & 16 & 4.5 & 5.2 \\ 100 & 73 & 50 & 38 \end{array} \quad 15.4$$

$$\begin{array}{cccc} 2.6 & 3.3 & 5.7 & 6.5 \\ 100 & 78 & 50 & 38 \end{array} \quad 15.3$$

$$\begin{array}{cccc} 4.0 & 5.0 & 6.5 & 7.2 \\ 100 & 75 & 50 & 38 \end{array} \quad 15.2$$

991.50 ✓

+50

30

+50

31

T.P. 0.28 980.14 ✓ 11.64 ✓ 979.86 ✓

+50

76.0

32

75.9

+50

75.7

T.P. 9.57 982.22 ✓ 7.49 ✓ 972.65 ✓

+77 = 15" x 56 Conc. Culv.

33

75.8

+50

76.0

34

76.3

+50

76.9

35

77.7

Lt

Rt

$$\frac{5.6}{100} \quad \frac{6.5}{80} \quad \frac{7.5}{50} \quad \frac{8.0}{37} \quad 15.1$$

$$\frac{5.8}{100} \quad \frac{6.3}{75} \quad \frac{7.3}{50} \quad \frac{7.8}{37} \quad 15.2$$

$$\frac{5.3}{100} \quad \frac{5.0}{84} \quad \frac{6.8}{64} \quad \frac{12.2}{42} \quad \frac{12.5}{39} \quad 15.4$$

$$\frac{4.2}{100} \quad \frac{9.8}{75} \quad \frac{15.5}{50} \quad \frac{16.7}{35} \quad 15.4$$

$$\frac{9.8}{100} \quad \frac{4.0}{77} \quad \frac{6.2}{60} \quad \frac{7.3}{34} \quad \frac{7.5}{25} \quad \frac{4.3}{15} \quad \frac{4.15}{10} \quad 4.1 \quad \frac{4.25}{10} \quad \frac{4.4}{15} \quad \frac{9.7}{22} \quad \frac{10.1}{28} \quad \frac{10.1}{30} \quad \frac{11.7}{32} \quad \frac{9.7}{32} \quad \frac{9.8}{46} \quad \frac{12.3}{76} \quad \frac{3.0}{100}$$

$$\frac{2.8}{100} \quad \frac{5.4}{82} \quad \frac{8.0}{86} \quad \frac{9.0}{44} \quad \frac{8.7}{26} \quad \frac{4.4}{15} \quad \frac{4.2}{10} \quad 4.2 \quad \frac{4.3}{10} \quad \frac{4.3}{14} \quad \frac{8.0}{20} \quad \frac{8.5}{27} \quad \frac{11.5}{30} \quad \frac{8.5}{34} \quad \frac{12.0}{100}$$

$$\frac{3.7}{100} \quad \frac{5.8}{70} \quad \frac{8.0}{53} \quad \frac{9.0}{38} \quad \frac{8.6}{26} \quad \frac{4.4}{15} \quad \frac{4.4}{10} \quad 4.4 \quad \frac{4.6}{10} \quad \frac{4.6}{15} \quad \frac{10.0}{24} \quad \frac{9.5}{45} \quad \frac{9.0}{77} \quad \frac{9.7}{100}$$

8.9 ← Flowline → 9.9

$$\frac{9.6}{100} \quad \frac{9.0}{77} \quad \frac{10.6}{44} \quad \frac{10.5}{27} \quad \frac{6.5}{15} \quad \frac{6.4}{10} \quad 6.4 \quad \frac{6.6}{10} \quad \frac{6.8}{14} \quad \frac{11.8}{22} \quad \frac{11.2}{27} \quad \frac{10.2}{45} \quad \frac{8.2}{88} \quad \frac{9.2}{100}$$

$$\frac{11.0}{70} \quad \frac{10.0}{41} \quad \frac{11.8}{37} \quad \frac{10.0}{34} \quad \frac{10.0}{29} \quad \frac{6.2}{15} \quad \frac{6.2}{10} \quad 6.15 \quad \frac{6.4}{10} \quad \frac{6.4}{14} \quad \frac{6.4}{20} \quad \frac{9.8}{30} \quad \frac{10.8}{33} \quad \frac{9.6}{34} \quad \frac{9.3}{44} \quad \frac{4.2}{100}$$

← into the swamp

$$\frac{11.2}{62} \quad \frac{9.8}{28} \quad \frac{5.8}{15} \quad \frac{5.9}{10} \quad 5.9 \quad \frac{6.0}{10} \quad \frac{6.1}{15} \quad \frac{9.5}{21} \quad \frac{9.8}{30} \quad \frac{7.6}{33} \quad \frac{5.8}{70} \quad \frac{2.6}{100}$$

$$\frac{10.6}{100} \quad \frac{9.4}{50} \quad \frac{8.7}{27} \quad \frac{5.4}{16} \quad \frac{5.3}{10} \quad 5.3 \quad \frac{5.4}{10} \quad \frac{5.4}{14} \quad \frac{9.0}{21} \quad \frac{9.0}{32} \quad \frac{7.2}{34} \quad \frac{6.3}{60} \quad \frac{2.2}{100}$$

$$\frac{6.4}{100} \quad \frac{5.6}{50} \quad \frac{5.4}{33} \quad \frac{6.5}{31} \quad \frac{6.5}{25} \quad \frac{4.8}{17} \quad \frac{4.7}{10} \quad 4.5 \quad \frac{4.5}{10} \quad \frac{4.6}{15} \quad \frac{8.6}{21} \quad \frac{8.8}{31} \quad \frac{7.0}{34} \quad \frac{6.5}{50} \quad \frac{3.8}{100}$$

35

982.22 ✓

+50

78.3

36

78.9

+50

79.5

37

79.7

+38

79.8

+50

79.8

4.23

983.60 ✓

2.85

979.37 ✓

38

79.7

+50

79.7

39

79.6

+50

79.5

40

79.3

+04

15" x 53"

Lono. Calv.

LT £ RT

$\frac{6.5}{100}$ $\frac{5.5}{50}$ $\frac{4.8}{36}$ $\frac{4.2}{33}$ $\frac{5.2}{30}$ $\frac{4.9}{21}$ $\frac{4.1}{17}$ $\frac{3.9}{10}$ $\frac{3.9}{10}$ $\frac{3.9}{10}$ $\frac{3.8}{15}$ $\frac{7.0}{21}$ $\frac{7.0}{25}$ $\frac{5.5}{28}$ $\frac{6.3}{50}$ $\frac{8.7}{100}$

$\frac{2.8}{100}$ $\frac{2.8}{87}$ $\frac{3.8}{41}$ $\frac{3.1}{33}$ $\frac{5.2}{29}$ $\frac{5.2}{26}$ $\frac{3.4}{16}$ $\frac{3.3}{10}$ $\frac{3.3}{10}$ $\frac{3.4}{15}$ $\frac{3.4}{19}$ $\frac{5.7}{24}$ $\frac{6.2}{28}$ $\frac{5.2}{40}$ $\frac{7.2}{50}$ $\frac{8.6}{100}$

$\frac{2.2}{100}$ $\frac{1.2}{70}$ $\frac{1.2}{33}$ $\frac{5.7}{29}$ $\frac{5.4}{20}$ $\frac{2.9}{16}$ $\frac{2.8}{10}$ $\frac{2.7}{10}$ $\frac{2.8}{10}$ $\frac{2.6}{15}$ $\frac{5.4}{20}$ $\frac{5.5}{24}$ $\frac{6.0}{32}$ $\frac{5.8}{40}$ $\frac{3.6}{50}$ $\frac{5.2}{100}$

$\frac{3.7}{100}$ $\frac{1.2}{50}$ $\frac{0.8}{33}$ $\frac{4.8}{27}$ $\frac{5.0}{22}$ $\frac{2.8}{16}$ $\frac{2.6}{10}$ $\frac{2.5}{10}$ $\frac{2.6}{10}$ $\frac{2.6}{15}$ $\frac{5.8}{20}$ $\frac{6.2}{24}$ $\frac{5.6}{25}$ $\frac{6.8}{38}$ $\frac{5.0}{45}$ $\frac{0.8}{50}$

$\frac{5.2}{100}$ $\frac{4.5}{78}$ $\frac{2.2}{50}$ $\frac{2.5}{29}$ $\frac{4.2}{21}$ $\frac{2.6}{15}$ $\frac{2.5}{10}$ $\frac{2.4}{10}$ $\frac{2.5}{10}$ $\frac{2.5}{15}$ $\frac{6.0}{21}$ $\frac{6.0}{29}$ $\frac{7.3}{37}$ $\frac{6.2}{44}$ $\frac{2.7}{53}$ $\frac{2.7}{63}$

$\frac{5.7}{100}$ $\frac{5.2}{83}$ $\frac{2.3}{41}$ $\frac{4.0}{26}$ $\frac{3.7}{19}$ $\frac{2.6}{15}$ $\frac{2.4}{10}$ $\frac{2.4}{10}$ $\frac{2.4}{10}$ $\frac{2.5}{15}$ $\frac{6.0}{21}$ $\frac{5.8}{27}$ $\frac{6.8}{42}$ $\frac{2.6}{68}$ $\frac{6.0}{100}$

$\frac{8.2}{100}$ $\frac{6.8}{72}$ $\frac{7.4}{60}$ $\frac{6.8}{23}$ $\frac{4.0}{14}$ $\frac{3.9}{10}$ $\frac{3.9}{10}$ $\frac{3.9}{10}$ $\frac{4.0}{15}$ $\frac{8.4}{20}$ $\frac{6.6}{23}$ $\frac{3.8}{28}$ $\frac{7.0}{36}$ $\frac{8.0}{46}$

→ $\frac{7.1}{62}$ $\frac{3.5}{73}$ $\frac{5.8}{100}$

$\frac{8.6}{100}$ $\frac{9.6}{55}$ $\frac{8.5}{25}$ $\frac{4.2}{16}$ $\frac{3.9}{10}$ $\frac{3.9}{10}$ $\frac{4.0}{10}$ $\frac{4.0}{14}$ $\frac{6.8}{20}$ $\frac{5.8}{35}$ $\frac{5.7}{57}$ $\frac{6.6}{100}$

$\frac{8.2}{100}$ $\frac{9.6}{80}$ $\frac{10.0}{60}$ $\frac{8.4}{24}$ $\frac{4.2}{16}$ $\frac{4.0}{10}$ $\frac{4.0}{10}$ $\frac{4.1}{10}$ $\frac{4.1}{15}$ $\frac{7.4}{21}$ $\frac{8.5}{59}$ $\frac{8.0}{100}$

$\frac{7.8}{100}$ $\frac{9.2}{50}$ $\frac{8.5}{25}$ $\frac{4.4}{16}$ $\frac{4.2}{10}$ $\frac{4.1}{10}$ $\frac{4.3}{10}$ $\frac{4.4}{15}$ $\frac{9.0}{22}$ $\frac{10.2}{50}$ $\frac{10.8}{100}$

$\frac{7.7}{100}$ $\frac{9.2}{38}$ $\frac{8.7}{27}$ $\frac{4.3}{15}$ $\frac{4.3}{10}$ $\frac{4.3}{10}$ $\frac{4.6}{10}$ $\frac{4.7}{15}$ $\frac{9.6}{22}$ $\frac{11.0}{60}$ $\frac{11.4}{100}$

9.25 ← Flowline → 10.3

40
+50

983.60

79.2

41

79.2

+16

79.2

+29

Mar. 19-

27°F ✓ Fair. 79.2

B.M.

7.43

985.49 ✓

5.54

978.06 ✓

+38

79.3

+43

79.2

+55

79.2

+65

79.3

+85

79.4

+92

79.4

42

79.4

+50

79.5

43

79.7

Lt.

Lt

Lt

<u>8.6</u>	<u>9.3</u>	<u>8.7</u>	<u>4.5</u>	<u>4.3</u>	<u>4.4</u>	<u>4.7</u>	<u>4.8</u>	<u>9.5</u>	<u>11.0</u>	<u>11.4</u>
100	38	28	15	10		10	14	22	60	100

<u>5.8</u>	<u>7.0</u>	<u>8.0</u>	<u>4.5</u>	<u>4.5</u>	<u>4.4</u>	<u>4.5</u>	<u>4.6</u>	<u>9.6</u>	<u>11.2</u>	<u>11.8</u>
100	47	24	15	10		10	15	22	60	100

<u>5.0</u>	<u>6.7</u>	<u>7.7</u>	<u>4.6</u>	<u>4.4</u>	<u>4.4</u>	<u>4.5</u>	<u>4.7</u>	<u>8.8</u>	<u>11.0</u>	<u>11.6</u>
100	50	23	15	10		10	15	22	60	100

<u>4.7</u>	<u>6.0</u>	<u>7.5</u>	<u>4.5</u>	<u>4.4</u>	<u>4.4</u>	<u>4.5</u>	<u>4.6</u>	<u>8.0</u>	<u>8.7</u>	<u>9.0</u>
100	50	22	15	10		10	15	36	60	100

Boat spike in T.P. 20' Lt 5th. 40 + 90

<u>6.8</u>	<u>7.8</u>	<u>8.5</u>	<u>9.1</u>	<u>9.1</u>	<u>6.5</u>	<u>6.3</u>	<u>6.2</u>	<u>6.4</u>	<u>6.4</u>	<u>9.8</u>	<u>10.5</u>	<u>10.8</u>
100	50	30	26	21	14	10		10	15	41	60	100

<u>6.8</u>	<u>7.8</u>	<u>8.4</u>	<u>9.1</u>	<u>9.1</u>	<u>6.4</u>	<u>6.3</u>	<u>6.25</u>	<u>6.4</u>	<u>8.0</u>	<u>11.2</u>	<u>11.4</u>	<u>12.7</u>
100	50	30	26	21	15	10		10	27	42	75	100

<u>6.8</u>	<u>7.8</u>	<u>8.2</u>	<u>8.8</u>	<u>8.8</u>	<u>6.6</u>	<u>6.3</u>	<u>6.25</u>	<u>6.4</u>	<u>6.6</u>	<u>9.7</u>	<u>11.0</u>	<u>11.6</u>	<u>10.2</u>	<u>12.7</u>
100	50	30	27	20	14	10		10	15	20	38	50	68	100

<u>7.2</u>	<u>7.7</u>	<u>8.0</u>	<u>6.2</u>	<u>6.2</u>	<u>6.3</u>	<u>6.6</u>	<u>10.0</u>	<u>10.8</u>	<u>10.8</u>	<u>10.2</u>	<u>12.5</u>
100	50	20	10		10	15	21	36	50	70	100

<u>8.5</u>	<u>8.5</u>	<u>7.7</u>	<u>6.2</u>	<u>6.1</u>	<u>6.2</u>	<u>6.2</u>	<u>9.8</u>	<u>10.6</u>	<u>10.2</u>	<u>11.2</u>
100	50	31	10		10	15	21	35	50	100

<u>8.8</u>	<u>8.8</u>	<u>8.4</u>	<u>9.4</u>	<u>6.5</u>	<u>6.2</u>	<u>6.1</u>	<u>6.2</u>	<u>6.4</u>	<u>9.8</u>	<u>10.4</u>	<u>10.0</u>	<u>10.5</u>
100	50	36	20	15	10		10	15	22	36	60	100

<u>9.3</u>	<u>9.3</u>	<u>8.8</u>	<u>9.6</u>	<u>6.3</u>	<u>6.2</u>	<u>6.1</u>	<u>6.2</u>	<u>6.2</u>	<u>9.2</u>	<u>9.6</u>	<u>9.6</u>	<u>10.5</u>
100	50	40	19	14	10		10	15	22	35	66	100

<u>10.6</u>	<u>10.4</u>	<u>10.5</u>	<u>6.1</u>	<u>6.0</u>	<u>6.0</u>	<u>6.1</u>	<u>6.2</u>	<u>9.0</u>	<u>9.8</u>	<u>8.8</u>	<u>9.2</u>	<u>9.6</u>
100	50	21	15	10		10	15	20	28	38	60	100

<u>11.0</u>	<u>11.6</u>	<u>11.5</u>	<u>10.1</u>	<u>5.8</u>	<u>5.9</u>	<u>5.8</u>	<u>5.9</u>	<u>6.0</u>	<u>10.8</u>	<u>11.0</u>	<u>11.8</u>
100	50	29	21	14	10		10	14	22	60	100

43

985.49 ✓

+50

80.0

44

80.5

+44

81.2

+50

81.2

+62

81.5

+65

81.5

45

82.1

+50

82.9 ✓

T.P.

9.01

991.62 ✓

2.88

982.61 ✓

✓

+60

82.9

+63

83.0

+92

83.3

46 ✓

83.3

+50

83.6

Lt

L

Rt

11.7	10.4	10.8	10.4	9.2	5.5	5.6	5.5	5.5	5.5	9.0	10.2	12.4
100	72	50	30	22	15	10	10	15	21	52	100	

10.7	9.2	9.0	8.7	5.2	5.1	5.0	5.0	5.0	8.6	10.6	12.0	12.0
100	66	47	20	14	10	10	15	21	50	83	100	

10.6	10.8	11.6	10.6	4.6	4.6	4.3	4.3	4.4	8.0	8.7	7.7	
100	62	42	23	14	10	10	15	21	60	100		

10.6	10.8	11.5	10.6	4.6	4.5	4.3	4.25	4.2	5.5	5.8	7.4	7.0
100	62	42	23	14	10	10	15	22	53	63	100	

10.3	10.5	11.2	10.0	4.4	4.3	4.0	4.0	4.1	4.7	4.3	7.4	7.4
100	62	42	22	14	10	10	15	24	74	89	100	

10.3	10.5	11.2	10.0	4.4		4.0	3.9	4.0	5.0	4.4	4.0	
100	62	42	22	14		10	15	20	60	100		

9.2	8.7	8.4	7.4	3.8	3.7	3.4	3.4	3.4	4.4	4.4	4.0	3.0
100	45	32	21	14	10	10	14	18	33	36	70	

6.7	3.7	2.8	2.8	2.6	2.6	2.6	3.3	2.8	2.2	2.2	1.8	
100	50	22	10	10	10	15	20	30	34	60	100	

11.5	8.8	8.0	10.1	8.8	8.7	8.7	8.7	8.8	7.7	8.0	8.0	4.2	4.2
100	50	22	18	16	10	10	28	36	60	76	91	100	

11.5	8.6	8.1	9.9	8.9	8.8	8.6	8.6	9.0	6.5	6.2	5.8	1.9	2.0
100	50	22	18	15	10	10	26	31	60	76	90	100	

10.4	7.1	5.8	9.2	9.2	8.4	8.5	8.3	8.3	8.3	3.5	2.4	1.5	1.5
100	50	26	19	17	15	10	10	20	32	60	71	100	

House

9.8	6.4	5.6	9.0	9.0	8.1	8.4	8.3	8.3	8.3	3.0	2.1	1.6	2.7
100	50	26	19	17	15	10	10	17	33	60	70		

7.5	6.7	5.3	8.7	8.7	8.0	8.0	8.0	8.2	2.4	1.8	2.4		
100	50	27	18	16	15	10	10	15	34	60	100		

46

991.62 ✓

+ 95

84.1

47

84.1

+ 22

84.3

+ 50

84.4

+ 95

84.4

T.F.

4.42

988.85 ✓

7.19

984.43 ✓

48

84.4

+ 08

84.4

+ 11

84.3

+ 50

84.2

49

84.1

+ 50

84.0

50

83.8

+ 50

83.4

Lt.

L

Rt

$\frac{4.9}{100}$	$\frac{4.5}{44}$	$\frac{5.0}{27}$	$\frac{8.2}{18}$	$\frac{8.2}{17}$	$\frac{7.6}{15}$	$\frac{7.6}{10}$	7.5	$\frac{7.5}{10}$	$\frac{7.5}{17}$	$\frac{4.2}{32}$	$\frac{4.5}{46}$	$\frac{6.0}{53}$	$\frac{5.2}{75}$	$\frac{5.0}{100}$
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$\frac{5.0}{100}$	$\frac{4.5}{45}$	$\frac{5.0}{27}$	$\frac{8.3}{18}$	$\frac{8.3}{17}$	$\frac{7.5}{15}$	$\frac{7.5}{10}$	7.5	$\frac{7.5}{10}$	$\frac{7.3}{17}$	$\frac{6.1}{45}$	$\frac{5.7}{60}$	$\frac{6.0}{100}$
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$\frac{4.7}{100}$	$\frac{4.4}{50}$	$\frac{4.8}{27}$	$\frac{8.2}{18}$	$\frac{8.2}{17}$	$\frac{7.4}{15}$	$\frac{7.3}{10}$	7.3	$\frac{7.3}{10}$	$\frac{6.8}{22}$	$\frac{5.2}{26}$	$\frac{5.3}{37}$	$\frac{6.7}{60}$	$\frac{7.6}{100}$
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$\frac{4.6}{100}$	$\frac{4.6}{50}$	$\frac{5.1}{28}$	$\frac{8.1}{18}$	$\frac{8.1}{17}$	$\frac{7.2}{16}$	$\frac{7.3}{10}$	7.2	$\frac{7.2}{10}$	$\frac{7.8}{23}$	$\frac{6.8}{29}$	$\frac{8.2}{60}$	$\frac{8.8}{100}$
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$\frac{6.1}{100}$	$\frac{6.6}{60}$	$\frac{6.8}{28}$	$\frac{7.2}{19}$	$\frac{7.3}{10}$	7.2	$\frac{7.3}{10}$	$\frac{7.8}{19}$	$\frac{9.4}{42}$	$\frac{9.7}{60}$	$\frac{10.6}{100}$
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P.M. Windy

$\frac{3.5}{100}$	$\frac{4.0}{50}$	$\frac{4.3}{21}$	$\frac{4.5}{10}$	4.5	$\frac{4.6}{10}$	$\frac{5.0}{16}$	$\frac{6.7}{43}$	$\frac{7.2}{60}$	$\frac{8.2}{100}$
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$\frac{3.6}{100}$	$\frac{4.3}{50}$	$\frac{4.6}{20}$	$\frac{4.6}{10}$	4.5	$\frac{4.6}{10}$	$\frac{4.6}{15}$	$\frac{5.7}{19}$	$\frac{7.3}{60}$	$\frac{8.2}{100}$
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$\frac{3.6}{100}$	$\frac{4.3}{50}$	$\frac{4.5}{22}$	$\frac{5.5}{18}$	$\frac{4.7}{16}$	$\frac{4.6}{10}$	4.6	$\frac{4.7}{10}$	$\frac{4.6}{15}$	$\frac{5.8}{19}$	$\frac{6.2}{39}$	$\frac{7.0}{44}$	$\frac{8.2}{100}$
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$\frac{4.1}{100}$	$\frac{4.5}{50}$	$\frac{4.8}{37}$	$\frac{5.2}{23}$	$\frac{4.7}{10}$	4.7	$\frac{4.8}{10}$	$\frac{4.8}{16}$	$\frac{6.0}{19}$	$\frac{6.5}{41}$	$\frac{7.4}{45}$	$\frac{8.7}{100}$
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$\frac{4.2}{100}$	$\frac{4.7}{60}$	$\frac{4.8}{20}$	$\frac{5.4}{17}$	$\frac{4.8}{10}$	4.8	$\frac{4.9}{10}$	$\frac{5.0}{15}$	$\frac{5.7}{18}$	$\frac{6.2}{41}$	$\frac{7.2}{45}$	$\frac{8.0}{60}$	$\frac{8.7}{100}$
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$\frac{3.7}{100}$	$\frac{4.3}{60}$	$\frac{4.8}{22}$	$\frac{5.7}{19}$	$\frac{5.0}{14}$	$\frac{4.9}{10}$	4.9	$\frac{5.0}{10}$	$\frac{4.9}{14}$	$\frac{5.5}{17}$	$\frac{5.8}{37}$	$\frac{6.7}{39}$	$\frac{7.3}{60}$	$\frac{8.4}{100}$
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$\frac{4.0}{100}$	$\frac{4.5}{40}$	$\frac{4.3}{22}$	$\frac{5.7}{19}$	$\frac{5.2}{15}$	$\frac{5.1}{10}$	5.1	$\frac{5.2}{10}$	$\frac{5.2}{14}$	$\frac{6.5}{22}$	$\frac{6.7}{27}$	$\frac{5.5}{30}$	$\frac{5.8}{38}$	$\frac{6.1}{44}$
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$\frac{4.5}{100}$	$\frac{4.8}{60}$	$\frac{4.5}{30}$	$\frac{5.0}{21}$	$\frac{6.3}{19}$	$\frac{5.8}{15}$	$\frac{5.5}{10}$	5.5	$\frac{5.8}{10}$	$\frac{5.5}{14}$	$\frac{6.8}{23}$	$\frac{6.8}{29}$	$\frac{5.7}{31}$	$\frac{5.7}{39}$	$\frac{6.7}{41}$	$\frac{6.8}{74}$
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$\frac{6.8}{71}$	$\frac{8.2}{100}$
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988.85

51

82.8

+50

82.2

52

81.7

+50

81.2

+56

Ditch Lt. Pt. W. Edge Bottom ^{81.1}

+60

" " " E. " ^{81.1}

+64

81.0

+80.75

± Cleveland Ave. ^{80.8}

B.M.

2.65

983.39 / 8.11

980.74 Mar. 24

+97

Snowing 30° F. ^{80.5}

53

80.4

+05

80.3

+07

80.3

+11

80.3

LH

E

RH

$\frac{5.1}{100}$	$\frac{5.4}{50}$	$\frac{5.5}{21}$	$\frac{6.7}{18}$	$\frac{6.1}{16}$	$\frac{6.1}{10}$	6.1	$\frac{6.2}{10}$	$\frac{6.2}{15}$	$\frac{7.5}{26}$	$\frac{7.5}{28}$	$\frac{6.5}{30}$	$\frac{6.3}{38}$	$\frac{7.5}{60}$	$\frac{8.5}{100}$
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$\frac{6.2}{100}$	$\frac{6.2}{41}$	$\frac{6.5}{21}$	$\frac{7.7}{19}$	$\frac{6.8}{15}$	$\frac{6.8}{10}$	6.7	$\frac{6.8}{10}$	$\frac{6.7}{15}$	$\frac{8.0}{25}$	$\frac{8.0}{29}$	$\frac{7.0}{31}$	$\frac{7.0}{38}$	$\frac{8.7}{100}$
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$\frac{7.0}{100}$	$\frac{6.8}{31}$	$\frac{7.2}{21}$	$\frac{8.0}{20}$	$\frac{7.2}{15}$	$\frac{7.2}{10}$	7.15	$\frac{7.3}{10}$	$\frac{7.3}{14}$	$\frac{8.4}{25}$	$\frac{8.4}{30}$	$\frac{7.5}{31}$	$\frac{7.7}{40}$	$\frac{9.2}{100}$
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$\frac{7.2}{100}$	$\frac{7.8}{60}$	$\frac{8.0}{27}$	$\frac{8.8}{21}$	$\frac{8.1}{17}$	$\frac{7.8}{10}$	7.7	$\frac{7.9}{23}$	$\frac{8.3}{30}$	$\frac{9.3}{70}$	$\frac{9.5}{100}$
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$\frac{100}{100}$	$\frac{100}{60}$	$\frac{9.6}{27}$	$\frac{8.3}{22}$	$\frac{7.85}{10}$	7.8	7.75	$\frac{8.25}{29}$	$\frac{8.6}{40}$	$\frac{9.8}{45}$	$\frac{10.7}{100}$
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$\frac{9.8}{100}$	$\frac{9.8}{60}$	$\frac{9.7}{37}$	$\frac{8.0}{22}$	$\frac{7.9}{10}$	7.8	$\frac{8.4}{36}$	$\frac{8.7}{46}$	$\frac{10.0}{57}$	$\frac{10.6}{100}$
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$\frac{7.5}{100}$	$\frac{7.8}{60}$	$\frac{7.9}{10}$	7.9	$\frac{8.6}{44}$	$\frac{9.1}{75}$	$\frac{9.7}{100}$
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$\frac{7.4}{100}$	$\frac{7.6}{50}$	$\frac{8.1}{10}$	8.1	$\frac{8.2}{10}$	$\frac{8.6}{50}$	$\frac{9.45}{100}$
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Ctr. Mon. Larp + Clev. Ave.

$\frac{2.1}{100}$	$\frac{2.6}{40}$	$\frac{3.0}{10}$	2.9	$\frac{3.2}{42}$	$\frac{4.0}{84}$	$\frac{4.1}{100}$
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$\frac{4.7}{100}$	$\frac{4.7}{75}$	$\frac{4.7}{45}$	$\frac{2.7}{33}$	$\frac{3.0}{10}$	3.0	$\frac{3.2}{36}$	$\frac{4.8}{53}$	$\frac{5.6}{100}$
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$\frac{4.8}{100}$	$\frac{5.0}{75}$	$\frac{4.7}{27}$	$\frac{3.0}{26}$	$\frac{3.1}{10}$	3.1	$\frac{3.2}{29}$	$\frac{4.8}{43}$	$\frac{5.7}{100}$
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$\frac{5.0}{100}$	$\frac{5.1}{75}$	$\frac{4.8}{34}$	$\frac{3.2}{25}$	$\frac{3.2}{10}$	3.1	$\frac{3.2}{27}$	$\frac{4.2}{43}$	$\frac{4.6}{100}$
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$\frac{5.0}{100}$	$\frac{5.0}{75}$	$\frac{5.0}{32}$	$\frac{3.2}{24}$	$\frac{3.2}{10}$	3.1	$\frac{3.1}{22}$	$\frac{3.4}{28}$	$\frac{4.2}{36}$	$\frac{4.5}{60}$	$\frac{4.5}{100}$
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53

983.39

+13

80.2

+50

79.7

54

79.1

+50

78.6

55

78.1

+50

77.7

56

77.5

+50

77.3

57

77.2

+50

77.2

58

77.1

3.93

980.70 ✓

6.62

976.77 ✓

+50

77.0

59

76.8

Cloudy Windy Cold. 30°F

Mar 24-30

Lt.

±

Rt

3.2	3.6	3.4	5.1	5.1	3.3	3.3	3.2	3.2	3.4	4.2	4.6	4.5
100	60	33	30	24	19	10		22	26	33	60	100

4.4	4.8	4.8	6.5	5.8	3.8	3.7	3.7	3.9	3.7	5.8	6.2	5.2	5.5
100	60	37	30	19	14	10		10	14	19	29	31	50

4.8	4.8	5.6	7.4	6.4	4.6	4.4	4.3	4.4	4.5	6.8	7.4	6.4	6.5	6.8
100	60	37	28	19	15	10		10	15	20	28	30	50	100

5.2	5.3	6.0	7.7	6.8	5.1	4.9	4.8	4.9	5.0	7.3	8.2	7.0	7.1	7.7
100	60	38	25	18	14	10		10	15	19	29	30	50	100

6.0	6.0	6.4	8.0	7.0	5.3	5.3	5.25	5.4	5.5	8.4	8.8	7.4	7.5	7.8
100	60	38	27	18	14	10		10	15	21	28	30	50	100

6.6	6.6	7.2	8.3	7.2	5.8	5.7	5.7	5.8	5.8	8.4	8.8	7.7	7.8	8.6
100	60	37	28	18	14	10		10	15	22	28	29	50	100

7.0	7.1	7.5	8.4	7.7	5.8	5.9	5.9	6.0	6.1	8.4	9.0	7.8	8.0	9.0
100	60	37	28	21	15	10		10	15	19	27	30	50	100

7.1	7.1	7.5	8.4	7.4	6.1	6.1	6.1	6.2	6.2	8.7	9.4	8.2	8.4	9.2
100	60	39	29	17	15	10		10	15	21	27	29	50	100

6.8	7.0	7.4	8.1	7.4	6.2	6.2	6.15	6.2	6.3	8.0	9.2	8.2	8.4	9.6
100	60	39	29	18	15	10		10	15	19	27	29	50	100

6.8	7.0	7.4	8.4	7.5	6.2	6.2	6.2	6.3	6.3	8.5	9.0	8.0	8.4	9.7
100	60	38	27	18	14	10		10	15	20	28	30	50	100

6.8	6.8	7.2	8.2	6.2	6.3	6.3	6.4	6.3	8.0	9.0	7.7	8.1	9.4
100	60	37	24	15	10		10	15	19	28	30	50	100

4.4	4.4	4.7	5.5	5.7	3.8	3.7	3.8	3.8	6.3	6.3	4.8	5.4	6.2
100	60	37	27	14	10		10	16	23	27	29	50	100

5.0	5.0	5.2	6.0	4.0	3.95	3.9	4.1	4.1	7.5	7.5	6.0	6.2	7.0
100	60	37	27	14	10		10	15	22	27	29	50	100

59

980.70 ✓

+ 46 = 12" x 42' Conc. Cross Drain

+ 50

76.4

60

76.2

+ 50

76.1

61

76.0

+ 50

75.9

62

76.0

+ 50

76.1

63

76.1

+ 50

76.3

64

76.5

+ 50

76.7

65

B.M. 5.24 981.26 ✓ 4.68 976.02 ✓ 76.9 976.05

Mar 24-30 H L RT

6.65 ← Flow line → 7.7

<u>4.8</u>	<u>5.1</u>	<u>5.5</u>	<u>6.0</u>	<u>4.4</u>	<u>4.4</u>	<u>4.3</u>	<u>4.4</u>	<u>4.4</u>	<u>7.2</u>	<u>7.2</u>	<u>6.4</u>	<u>7.7</u>	<u>7.7</u>
100	60	33	19	14	10		10	14	22	28	29	50	100

<u>4.8</u>	<u>5.1</u>	<u>5.4</u>	<u>4.6</u>	<u>4.5</u>	<u>4.5</u>	<u>4.5</u>	<u>4.7</u>	<u>7.7</u>	<u>7.7</u>	<u>6.4</u>	<u>7.5</u>	<u>8.5</u>
100	60	29	16	10	10	16	22	28	29	50	100	

<u>4.7</u>	<u>5.2</u>	<u>5.6</u>	<u>4.7</u>	<u>4.6</u>	<u>4.6</u>	<u>4.7</u>	<u>4.8</u>	<u>7.2</u>	<u>7.7</u>	<u>6.0</u>	<u>6.8</u>	<u>8.5</u>
100	60	19	17	10	10	16	21	27	29	50	100	

<u>4.8</u>	<u>5.0</u>	<u>5.5</u>	<u>5.8</u>	<u>4.7</u>	<u>4.8</u>	<u>4.7</u>	<u>4.8</u>	<u>4.7</u>	<u>7.7</u>	<u>7.7</u>	<u>6.5</u>	<u>7.1</u>	<u>7.8</u>
100	60	31	19	16	10	10	15	21	28	29	50	100	

<u>5.2</u>	<u>5.3</u>	<u>5.3</u>	<u>5.7</u>	<u>4.7</u>	<u>4.8</u>	<u>4.8</u>	<u>4.9</u>	<u>5.0</u>	<u>7.4</u>	<u>7.7</u>	<u>6.8</u>	<u>7.2</u>	<u>7.8</u>
100	60	33	19	16	10	10	16	20	28	29	50	100	

<u>5.1</u>	<u>5.2</u>	<u>5.4</u>	<u>6.0</u>	<u>6.0</u>	<u>4.6</u>	<u>4.7</u>	<u>4.7</u>	<u>4.8</u>	<u>4.7</u>	<u>7.8</u>	<u>7.8</u>	<u>6.6</u>	<u>6.6</u>	<u>8.2</u>
100	60	34	28	19	16	10	10	15	23	27	29	50	100	

<u>4.8</u>	<u>5.2</u>	<u>6.2</u>	<u>5.8</u>	<u>4.9</u>	<u>4.6</u>	<u>4.6</u>	<u>4.7</u>	<u>4.7</u>	<u>7.8</u>	<u>7.8</u>	<u>6.3</u>	<u>6.5</u>	<u>7.7</u>
100	60	26	20	17	10	10	16	22	28	30	50	100	

<u>5.2</u>	<u>5.6</u>	<u>6.6</u>	<u>6.0</u>	<u>4.6</u>	<u>4.6</u>	<u>4.5</u>	<u>4.7</u>	<u>4.7</u>	<u>7.5</u>	<u>7.5</u>	<u>6.6</u>	<u>6.6</u>	<u>7.5</u>
100	60	26	19	16	10	10	16	22	28	30	50	100	

<u>4.7</u>	<u>5.4</u>	<u>5.6</u>	<u>6.7</u>	<u>6.0</u>	<u>4.4</u>	<u>4.5</u>	<u>4.4</u>	<u>4.5</u>	<u>4.7</u>	<u>7.8</u>	<u>7.8</u>	<u>7.2</u>	<u>6.8</u>	<u>7.8</u>
100	60	32	21	19	16	10	10	17	22	28	30	50	100	

<u>4.2</u>	<u>4.8</u>	<u>4.8</u>	<u>6.2</u>	<u>5.8</u>	<u>4.5</u>	<u>4.3</u>	<u>4.2</u>	<u>4.4</u>	<u>4.4</u>	<u>7.2</u>	<u>7.6</u>	<u>6.7</u>	<u>6.7</u>	<u>7.0</u>
100	60	32	27	19	16	10	10	16	22	28	29	50	100	

<u>3.8</u>	<u>4.1</u>	<u>4.4</u>	<u>5.4</u>	<u>5.0</u>	<u>4.0</u>	<u>4.0</u>	<u>4.1</u>	<u>3.8</u>	<u>5.6</u>	<u>6.4</u>	<u>5.1</u>	<u>5.8</u>	<u>6.6</u>
100	60	31	28	18	10	10	10	15	20	27	29	50	100

<u>5.0</u>	<u>5.0</u>	<u>5.3</u>	<u>3.8</u>	<u>3.8</u>	<u>3.8</u>	<u>3.8</u>	<u>3.7</u>	<u>6.1</u>	<u>6.1</u>	<u>4.6</u>	<u>5.2</u>	<u>6.8</u>
100	60	24	19	10	10	16	22	27	29	50	100	

Boat spike in TR 20' Lt Sta 64+15

65		981.26		
+50			77.1	
66			77.1	
+50			77.1	
67			76.8	
+50			76.7	
68			76.5	
+50			76.2	
69			75.8	
+50			75.3	
70			74.8	
+50			74.4	
71			74.0	
+50			73.8	
T.P.	2.14	975.79 ✓	7.61	973.65 ✓

Mar. 24-30 Lt

±

Rt.

$\frac{5.7}{100}$	$\frac{5.7}{60}$	$\frac{5.7}{26}$	$\frac{4.4}{16}$	$\frac{4.2}{10}$	$\frac{4.1}{10}$	$\frac{4.3}{10}$	$\frac{4.2}{16}$	$\frac{6.1}{22}$	$\frac{6.1}{27}$	$\frac{5.2}{29}$	$\frac{5.8}{50}$	$\frac{6.1}{100}$
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$\frac{5.2}{100}$	$\frac{5.5}{60}$	$\frac{5.7}{23}$	$\frac{4.0}{15}$	$\frac{4.2}{10}$	$\frac{4.2}{10}$	$\frac{4.2}{10}$	$\frac{4.3}{16}$	$\frac{5.7}{23}$	$\frac{5.7}{27}$	$\frac{5.0}{29}$	$\frac{6.1}{50}$	$\frac{7.1}{100}$
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$\frac{4.8}{100}$	$\frac{4.8}{60}$	$\frac{5.3}{25}$	$\frac{4.2}{15}$	$\frac{4.2}{10}$	$\frac{4.2}{10}$	$\frac{4.3}{10}$	$\frac{4.3}{17}$	$\frac{6.2}{24}$	$\frac{6.2}{28}$	$\frac{5.3}{29}$	$\frac{6.2}{50}$	$\frac{7.1}{100}$
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$\frac{4.8}{100}$	$\frac{5.2}{60}$	$\frac{5.4}{21}$	$\frac{4.4}{16}$	$\frac{4.7}{10}$	$\frac{4.5}{10}$	$\frac{4.6}{10}$	$\frac{5.0}{19}$	$\frac{6.2}{22}$	$\frac{6.6}{27}$	$\frac{5.7}{28}$	$\frac{6.4}{50}$	$\frac{7.1}{100}$
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$\frac{4.8}{100}$	$\frac{5.0}{60}$	$\frac{5.5}{22}$	$\frac{4.5}{15}$	$\frac{4.6}{10}$	$\frac{4.6}{10}$	$\frac{4.8}{10}$	$\frac{4.8}{17}$	$\frac{6.6}{22}$	$\frac{7.1}{27}$	$\frac{5.8}{28}$	$\frac{6.8}{50}$	$\frac{7.1}{100}$
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$\frac{4.3}{100}$	$\frac{4.3}{60}$	$\frac{4.6}{36}$	$\frac{5.5}{25}$	$\frac{4.7}{16}$	$\frac{4.8}{10}$	$\frac{4.8}{10}$	$\frac{4.9}{10}$	$\frac{4.9}{18}$	$\frac{6.2}{21}$	$\frac{7.1}{27}$	$\frac{5.8}{28}$	$\frac{6.7}{50}$	$\frac{7.1}{100}$
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$\frac{4.8}{100}$	$\frac{5.0}{60}$	$\frac{5.2}{34}$	$\frac{6.2}{34}$	$\frac{6.4}{23}$	$\frac{5.4}{21}$	$\frac{5.1}{10}$	$\frac{5.1}{10}$	$\frac{5.2}{19}$	$\frac{5.4}{24}$	$\frac{7.1}{27}$	$\frac{7.1}{27}$	$\frac{6.0}{28}$	$\frac{6.6}{50}$	$\frac{7.1}{100}$
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$\frac{5.2}{100}$	$\frac{5.2}{60}$	$\frac{5.8}{33}$	$\frac{6.8}{27}$	$\frac{6.8}{24}$	$\frac{5.8}{21}$	$\frac{5.5}{10}$	$\frac{5.5}{10}$	$\frac{5.7}{20}$	$\frac{5.7}{24}$	$\frac{7.3}{27}$	$\frac{7.3}{27}$	$\frac{6.5}{28}$	$\frac{6.8}{50}$	$\frac{7.1}{100}$
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$\frac{6.1}{100}$	$\frac{6.1}{60}$	$\frac{7.0}{24}$	$\frac{6.0}{17}$	$\frac{6.0}{10}$	$\frac{6.0}{10}$	$\frac{6.1}{10}$	$\frac{6.2}{17}$	$\frac{7.8}{23}$	$\frac{7.8}{27}$	$\frac{7.0}{29}$	$\frac{7.6}{50}$	$\frac{8.1}{100}$
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$\frac{7.5}{100}$	$\frac{7.4}{60}$	$\frac{7.3}{20}$	$\frac{6.5}{15}$	$\frac{6.5}{10}$	$\frac{6.5}{10}$	$\frac{6.6}{10}$	$\frac{6.6}{17}$	$\frac{8.4}{22}$	$\frac{8.4}{28}$	$\frac{7.8}{29}$	$\frac{8.8}{50}$	$\frac{8.1}{100}$
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$\frac{7.6}{100}$	$\frac{7.6}{60}$	$\frac{8.0}{27}$	$\frac{7.0}{16}$	$\frac{6.9}{10}$	$\frac{6.9}{10}$	$\frac{7.1}{10}$	$\frac{7.1}{15}$	$\frac{8.9}{22}$	$\frac{8.9}{28}$	$\frac{8.3}{29}$	$\frac{8.7}{50}$	$\frac{9.2}{100}$
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$\frac{8.0}{100}$	$\frac{8.0}{60}$	$\frac{8.3}{28}$	$\frac{7.3}{15}$	$\frac{7.3}{10}$	$\frac{7.3}{10}$	$\frac{7.4}{10}$	$\frac{7.4}{17}$	$\frac{9.4}{23}$	$\frac{9.4}{28}$	$\frac{8.7}{29}$	$\frac{9.0}{50}$	$\frac{9.1}{100}$
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$\frac{8.2}{100}$	$\frac{8.2}{60}$	$\frac{8.6}{22}$	$\frac{7.5}{15}$	$\frac{7.5}{10}$	$\frac{7.5}{10}$	$\frac{7.7}{10}$	$\frac{7.8}{16}$	$\frac{9.5}{21}$	$\frac{9.8}{28}$	$\frac{9.0}{29}$	$\frac{9.2}{50}$	$\frac{10.0}{100}$
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✓
975.79

72

73.5

+50

73.3

73

73.0

+50

72.3

74

71.7

+50

71.2

75

70.7

+50

70.2

76

69.8

+50

69.4

77

69.0

+

+50

68.5

78

67.9

B.M.

9.33

✓ 966.46 ✓ 966.48

Mar. 24.30

Lt

Rt.

Rt.

3.2	3.2	3.7	2.2	2.3	2.3	2.4	2.5	4.7	4.7	3.5	3.8	4.7
100	60	29	16	10	10	16	22	27	29	50	100	

2.7	3.0	3.2	4.5	4.5	2.5	2.5	2.5	2.6	2.6	4.2	4.7	3.7	4.0	5.0
100	60	31	29	24	16	10	10	16	22	28	29	50	100	

2.8	3.0	4.5	2.9	2.9	2.8	2.9	3.0	5.1	5.6	4.0	4.2	4.8
100	60	25	16	10	10	16	20	27	30	50	100	

3.2	3.5	4.5	5.4	5.4	3.5	3.5	3.5	3.5	3.4	5.5	5.5	4.5	4.6	5.4
100	60	30	28	24	15	10	10	16	21	27	29	50	100	

4.0	4.3	4.6	5.3	5.3	4.1	4.1	4.1	4.2	4.1	5.7	5.7	4.9	5.0	5.6
100	60	31	28	22	19	10	10	16	21	28	29	50	100	

4.9	5.2	6.0	4.6	4.7	4.6	4.7	4.6	6.7	6.7	5.6	5.4	6.0
100	60	24	17	10	10	16	23	29	30	50	100	

5.6	5.9	6.2	7.0	5.1	5.2	5.1	5.1	5.1	7.2	7.2	6.2	5.7	6.7
100	60	29	25	16	10	10	16	22	29	30	50	100	

5.8	6.3	6.7	7.4	5.8	5.6	5.6	5.7	5.7	7.3	7.3	6.5	6.2	6.8
100	60	29	25	16	10	10	16	22	29	30	50	100	

5.5	6.8	7.0	8.0	8.0	6.1	6.1	6.0	6.0	6.2	7.2	7.7	7.0	6.8	7.5
100	60	32	29	25	16	10	10	19	23	28	30	50	100	

6.8	6.9	7.1	8.0	8.0	6.7	6.4	6.4	6.5	6.5	8.4	8.4	7.2	7.3	7.6
100	60	29	27	24	20	10	10	17	25	29	31	50	100	

6.8	7.5	7.8	8.8	8.8	7.0	6.9	6.8	6.9	7.1	8.7	8.7	7.7	7.5	7.8
100	60	30	27	23	19	10	10	18	24	29	30	50	100	

7.4	7.8	7.8	8.2	8.6	7.3	7.3	7.3	7.5	7.6	9.1	9.1	7.6	7.8	8.2
100	60	28	26	22	19	10	10	17	25	29	31	50	100	

7.5	8.1	8.3	10.0	9.7	8.0	7.9	7.9	8.0	8.1	9.2	9.2	8.1	8.4	8.6
100	60	30	27	23	19	10	10	17	22	28	30	50	100	

Top Bolt. at 1/4 cor. Sta 79+06.9

B.M. 4.54 971.02 ✓ 966.48
78+50 67.3

79 66.6

+50 65.8

80 65.2

+50 64.7

81 64.2

+50 63.8

82 63.6

+50 63.5

T.P. 2.62 966.30 ✓ 7.34 963.68 ✓

83 63.5

+50 63.4

84 63.2

+50 62.9

Mar 25-30 25°F Lt North Wind. L R.H.

Top of Bolt. 1/4 Cor. Sta. 79+06.9

3.5	4.0	4.6	5.7	5.9	3.8	3.8	3.7	3.8	3.7	5.6	5.6	4.5	4.4	4.2
100	60	30	28	23	18	10		10	16	22	27	29	60	100

4.0	4.2	5.6	6.8	6.8	4.6	4.6	4.4	4.5	4.8	5.8	5.8	5.2	4.6	4.3
100	60	30	28	23	19	10		10	16	20	25	26	60	100

5.3	5.1	5.8	7.5	6.0	5.1	5.2	5.2	5.3	5.1	6.6	6.6	5.5	4.6	Howe
100	60	32	29	22	19	10		10	16	20	24	27	52	

6.4	6.0	6.2	8.1	7.5	6.0	5.8	5.8	5.9	5.8	7.5	7.5	6.7	6.4	6.7
100	60	33	29	22	19	10		10	15	20	25	27	60	100

7.5	6.8	7.0	8.4	8.4	6.3	6.3	6.3	6.4	6.4	8.4	8.2	8.1	8.1
100	60	32	30	23	19	10		10	16	21	28	60	100

8.4	7.6	7.5	9.0	9.0	6.9	6.8	6.8	6.9	6.7	9.0	8.7	8.4	8.6
100	60	33	30	24	19	10		10	16	22	30	60	100

8.4	8.5	8.7	9.7	9.2	7.3	7.1	7.2	7.4	7.3	9.3	9.0	9.0	9.2
100	60	32	30	24	19	10		10	16	22	28	60	100

8.4	8.4	8.8	9.1	9.1	7.4	7.3	7.4	7.6	7.5	9.5	9.5	10.0	9.7
100	60	32	30	23	19	10		10	16	20	27	60	100

8.5	8.6	8.7	9.3	9.0	8.0	7.5	7.5	7.8	7.5	9.2	9.8	10.0	10.0
100	60	32	30	25	20	10		10	16	19	33	60	100

3.8	3.8	4.1	4.4	2.9	2.8	2.8	2.9	2.8	5.6	5.0	5.2	5.2
100	60	30	24	15	10		10	15	21	29	60	100

5.2 5.2

4.0	3.6	4.2	4.8	4.8	3.1	3.0	2.9	3.0	2.8	9.2	9.2	4.4	4.7	5.0
100	60	32	29	22	17	10		10	16	19	25	27	60	100

3.5	3.3	4.2	5.3	5.1	3.5	3.2	3.1	3.2	3.4	5.4	5.4	4.2	4.2	3.8
100	60	33	28	22	17	10		10	15	20	26	29	60	82

4.2	3.8	4.4	5.8	5.3	3.7	3.5	3.4	3.5	3.8	5.5	5.5	4.8	5.7	6.0
100	60	33	29	23	17	10		10	16	20	26	31	60	100

966.30 ✓

85 62.4

+50 62.0

86 61.7

+50 61.7

+65 61.5

+68 61.5

87 61.5

+50 61.2

88 61.0

+50 60.7

T.R. 6.45 965.18 ✓ 7.57 958.73 ✓

89 60.6

+50 60.3

90 60.0

LT £ RT

Very Windy 10³⁰ A.M. & cold.

4.6 4.6 5.4 6.4 6.4 4.3 3.9 3.9 4.0 4.0 6.3 6.2 6.6 6.7
100 60 32 28 25 16 10 10 15 21 31 60 100

5.1 5.4 5.8 6.5 6.6 4.4 4.3 4.3 4.5 4.8 7.3 6.8 7.2 7.2
100 60 33 29 22 15 10 10 15 21 31 60 100

4.6 5.4 6.2 6.8 6.8 4.8 4.5 4.6 4.8 4.9 7.5 7.3 7.2 7.2
100 60 33 29 24 16 10 10 15 21 31 60 100

3.7 4.8 6.2 7.2 7.5 4.9 4.6 4.6 4.8 4.8 7.7 7.2 7.4 7.4
100 60 33 30 23 16 10 10 15 21 30 60 100

3.4 4.5 5.7 7.0 7.0 4.8 4.7 4.8 4.9 5.0 7.8 7.7 7.7 7.6
100 60 32 29 22 15 10 10 14 20 29 60 100

3.4 4.5 5.7 7.0 7.0 4.8 4.7 4.8 4.8 5.1 7.7 7.8 6.7 6.4 6.2
100 60 32 29 22 15 10 10 14 20 26 30 60 100

3.1 4.1 5.7 7.2 6.7 5.0 4.8 4.8 4.9 5.2 7.7 7.8 6.5 6.0 6.0
100 60 33 30 21 15 10 10 15 20 27 29 60 100

3.8 4.4 5.6 7.4 7.0 5.2 5.1 5.1 5.2 5.0 7.7 7.7 5.8 7.0 7.2
100 60 32 29 20 15 10 10 16 21 26 28 60 100

5.1 5.4 6.7 7.8 7.7 5.5 5.3 5.3 5.4 5.3 7.5 8.0 6.0 7.0 7.4
100 60 32 29 20 16 10 10 16 19 25 28 60 100

6.4 6.4 7.4 8.2 8.0 5.7 5.6 5.6 5.7 6.1 7.7 8.1 6.5 7.1 7.5
100 60 32 29 22 17 10 10 17 20 26 28 60 100
Top of West End Cully. 88+83

Mar. 27-30-22° F Windy.

6.0 6.0 6.8 7.7 7.7 5.0 4.7 4.6 4.7 4.6 7.3 7.3 5.5 6.0 6.2
100 60 32 30 21 15 10 10 16 21 26 28 60 100

6.2 6.3 7.3 8.4 8.0 5.4 5.0 4.9 5.0 5.0 7.8 7.8 6.5 6.5 6.5
100 60 32 30 20 15 10 10 16 23 26 32 60 100

6.3 6.6 7.3 8.3 8.1 5.3 5.2 5.2 5.2 5.6 7.8 7.8 6.6 6.2
100 60 32 30 21 15 10 10 17 21 27 60 100

965.18 ✓

5

+50

59.9

91

59.8

+50

59.6

92

59.5 ✓

B.M.

3.23

962.70 ✓

5.71

959.47 ✓

+50

59.4

93

59.0

+50

58.5

94

57.9

+50

57.3

95

56.8

+50

56.3

96

55.9

+50

55.7

+57 = 12" x 44' Conc. Cross Drain

Lt

E

Rd

64	66	73	84	83	56	53	53	55	55	86	88	72	80	78
100	60	32	29	21	15	10		10	15	20	26	30	60	100

63	63	72	82	82	57	55	54	55	54	92	92	72	82	85
100	60	32	29	21	15	10		10	15	21	27	30	60	100

6.4	6.4	7.2	8.0	7.0	5.7	5.7	5.6	5.7	5.5	8.5	8.5	7.0	7.9	8.4
100	60	32	29	18	15	10		10	15	20	27	30	60	100

6.4	6.5	7.1	7.7	7.5	5.7	5.7	5.7	5.7	5.7	8.7	8.7	6.3	7.4	8.1
100	60	32	29	18	15	10		10	15	22	27	30	60	100

N.E. cor. Mont $\frac{1}{4}$ $\frac{1}{4}$ cor. S40 92 + 20

4.0	4.0	4.5	5.3	4.6	3.6	3.5	3.3	3.4	3.3	6.3	6.3	3.8	4.0	4.8
100	60	31	27	19	15	10		10	16	21	27	29	50	100

3.8	4.3	4.3	4.6	4.6	3.8	3.6	3.7	3.8	3.7	6.4	6.4	4.1	4.4	5.4
100	60	30	27	18	15	10		10	16	22	26	28	50	100

4.2	4.1	4.3	5.2	5.2	4.3	4.4	4.3	4.2	4.3	4.1	7.1	7.1	4.4	4.8	6.0
100	60	27	26	24	23	16	10		10	15	21	26	28	50	100

5.1	5.1	4.8	5.5	5.5	4.8	4.8	4.8	4.9	4.8	7.2	7.2	5.2	5.5	6.6
100	60	27	26	24	24	10		10	16	21	26	30	50	100

5.2	5.6	5.9	6.9	5.7	5.4	5.4	5.4	5.4	5.3	8.0	8.0	5.5	6.0	7.0
100	60	29	28	27	10		10	16	22	28	34	50	100	

6.3	6.8	7.8	6.1	5.9	5.9	6.0	6.2	8.8	8.8	7.9	7.0	7.7
100	60	33	16	10		10	16	22	26	29	50	100

6.3	7.5	7.5	8.4	6.7	6.4	6.4	6.6	6.7	9.5	9.5	8.2	8.2	8.7
100	60	39	32	16	10		10	16	22	26	28	50	100

7.2	7.8	8.0	8.7	7.0	6.8	6.8	6.9	7.1	9.7	9.7	8.6	9.4	9.8
100	60	36	29	16	10		10	16	21	26	28	50	100

8.0	8.2	8.4	9.2	7.3	7.0	7.0	7.8	7.3	9.7	9.7	9.6	10.6	11.5
100	60	37	30	16	10		10	16	20	27	30	50	100

10.1 ← Flow line → 10.9

96		962.70 ✓			
T.P.	5.03	959.43 ✓	8.30 ✓	954.40 ✓	
97					55.2
+50					55.3
98					55.3
+50					55.3
99					55.5
+50					55.9
100					56.5
+50					57.1
101					57.6
T.P.	4.16	963.06 ✓	0.53 ✓	958.90 ✓	
+50					58.2
102					58.4
+50					58.4

Lt

L

Rt.

$\frac{5.2}{100}$	$\frac{5.5}{60}$	$\frac{5.1}{30}$	$\frac{6.0}{27}$	$\frac{4.2}{15}$	$\frac{4.0}{10}$	3.9	$\frac{4.0}{10}$	$\frac{4.2}{17}$	$\frac{7.1}{22}$	$\frac{7.1}{27}$	$\frac{6.5}{28}$	$\frac{6.5}{31}$	$\frac{7.4}{32}$
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 $\frac{7.7}{50}$ $\frac{8.5}{100}$

$\frac{5.5}{100}$	$\frac{5.5}{60}$	$\frac{5.5}{30}$	$\frac{6.2}{28}$	$\frac{5.8}{22}$	$\frac{4.2}{15}$	$\frac{4.2}{10}$	4.1	$\frac{4.2}{10}$	$\frac{4.2}{16}$	$\frac{7.3}{21}$	$\frac{7.3}{27}$	$\frac{6.1}{29}$	$\frac{7.4}{50}$	$\frac{8.4}{100}$
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$\frac{5.0}{100}$	$\frac{5.0}{60}$	$\frac{5.5}{30}$	$\frac{6.2}{28}$	$\frac{6.0}{22}$	$\frac{4.3}{15}$	$\frac{4.2}{10}$	4.1	$\frac{4.1}{10}$	$\frac{4.4}{16}$	$\frac{6.7}{21}$	$\frac{6.7}{27}$	$\frac{5.2}{29}$	$\frac{6.2}{50}$	$\frac{8.0}{100}$
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$\frac{3.6}{100}$	$\frac{4.0}{60}$	$\frac{4.6}{32}$	$\frac{6.0}{29}$	$\frac{5.7}{23}$	$\frac{4.5}{16}$	$\frac{4.2}{10}$	4.1	$\frac{4.1}{10}$	$\frac{3.9}{16}$	$\frac{6.6}{21}$	$\frac{6.6}{28}$	$\frac{5.5}{30}$	$\frac{5.7}{50}$	$\frac{6.0}{100}$
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$\frac{2.5}{100}$	$\frac{3.5}{60}$	$\frac{4.1}{33}$	$\frac{6.5}{29}$	$\frac{5.5}{20}$	$\frac{4.2}{16}$	$\frac{4.0}{10}$	3.9	$\frac{3.9}{10}$	$\frac{3.9}{16}$	$\frac{6.2}{23}$	$\frac{6.2}{27}$	$\frac{5.0}{29}$	$\frac{5.6}{60}$	$\frac{6.0}{100}$
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$\frac{2.4}{100}$	$\frac{2.8}{60}$	$\frac{3.5}{32}$	$\frac{6.0}{29}$	$\frac{5.0}{20}$	$\frac{3.6}{16}$	$\frac{3.7}{10}$	3.5	$\frac{3.5}{10}$	$\frac{3.7}{17}$	$\frac{6.0}{21}$	$\frac{6.0}{27}$	$\frac{4.5}{29}$	$\frac{4.8}{60}$	$\frac{5.4}{100}$
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$\frac{1.4}{100}$	$\frac{2.2}{60}$	$\frac{3.3}{30}$	$\frac{5.2}{28}$	$\frac{4.4}{20}$	$\frac{3.2}{16}$	$\frac{3.1}{10}$	2.9	$\frac{3.0}{10}$	$\frac{3.2}{17}$	$\frac{5.0}{21}$	$\frac{5.0}{26}$	$\frac{4.0}{28}$	$\frac{4.5}{60}$	$\frac{4.8}{100}$
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$\frac{1.3}{100}$	$\frac{1.8}{60}$	$\frac{2.6}{30}$	$\frac{4.5}{28}$	$\frac{3.3}{19}$	$\frac{2.5}{15}$	$\frac{2.4}{10}$	2.3	$\frac{2.4}{10}$	$\frac{2.4}{16}$	$\frac{4.8}{22}$	$\frac{4.8}{26}$	$\frac{3.5}{28}$	$\frac{4.1}{60}$	$\frac{4.7}{100}$
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$\frac{1.0}{100}$	$\frac{1.0}{44}$	$\frac{2.0}{29}$	$\frac{3.6}{27}$	$\frac{2.0}{16}$	$\frac{1.9}{10}$	1.8	$\frac{2.0}{10}$	$\frac{1.8}{16}$	$\frac{4.2}{21}$	$\frac{4.2}{25}$	$\frac{2.6}{27}$	$\frac{3.2}{60}$	$\frac{3.8}{100}$
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$\frac{4.7}{100}$	$\frac{5.0}{60}$	$\frac{4.7}{40}$	$\frac{5.4}{30}$	$\frac{7.2}{28}$	$\frac{7.2}{24}$	$\frac{5.2}{16}$	$\frac{5.0}{10}$	4.9	$\frac{5.0}{10}$	$\frac{5.0}{16}$	$\frac{7.3}{21}$	$\frac{7.3}{26}$	$\frac{5.8}{27}$	$\frac{5.4}{32}$	$\frac{6.0}{60}$	$\frac{6.8}{100}$
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$\frac{5.0}{100}$	$\frac{5.0}{50}$	$\frac{4.6}{47}$	$\frac{5.5}{30}$	$\frac{6.8}{28}$	$\frac{6.8}{24}$	$\frac{4.8}{16}$	$\frac{4.8}{10}$	4.7	$\frac{4.8}{10}$	$\frac{5.0}{16}$	$\frac{7.0}{21}$	$\frac{7.0}{26}$	$\frac{5.7}{27}$	$\frac{6.2}{60}$	$\frac{6.3}{100}$
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$\frac{5.0}{100}$	$\frac{5.4}{60}$	$\frac{4.7}{43}$	$\frac{5.4}{29}$	$\frac{7.2}{27}$	$\frac{7.2}{23}$	$\frac{5.0}{17}$	$\frac{4.7}{10}$	4.7	$\frac{4.65}{10}$	$\frac{4.85}{15}$	$\frac{4.8}{21}$	$\frac{7.2}{26}$	$\frac{7.2}{28}$	$\frac{5.6}{60}$	$\frac{6.3}{100}$
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963.06

103 58.4

956.63

+50 58.3

104 58.2

+50 57.7

105 57.2

+04 Bottom Ditch Rt Top on Lt. 57.1

+08 Top Ditch Rt Bottom Lt. 57.1

+12 Top Ditch Lt. 57.0

+16 Top Ditch No. 56.9

+32⁹⁵ Snelling 56.7

+50 Top Shoulder No. 56.5

+54 Bottom Ditch No. 56.5

+61 So. 56.4

3-27-30 - N.W. wind and How

Lt

L

RT

$\frac{51}{100} \frac{55}{60} \frac{51}{42} \frac{58}{31} \frac{77}{28} \frac{77}{25} \frac{50}{76} \frac{47}{18} \quad 4.7 \quad \frac{4.8}{70} \frac{4.7}{16} \frac{7.4}{21} \frac{7.4}{26} \frac{5.7}{28} \frac{6.0}{60} \frac{6.0}{100}$

$\frac{5.2}{100} \frac{5.6}{60} \frac{5.5}{37} \frac{6.2}{30} \frac{7.7}{28} \frac{7.7}{24} \frac{4.8}{16} \frac{4.8}{10} \quad 4.8 \quad \frac{4.9}{10} \frac{4.8}{16} \frac{7.4}{22} \frac{7.4}{26} \frac{5.7}{28} \frac{5.8}{60} \frac{6.2}{100}$

$\frac{5.4}{100} \frac{5.6}{60} \frac{5.6}{27} \frac{5.0}{70} \quad 4.9 \quad \frac{5.0}{10} \frac{5.0}{16} \frac{7.5}{22} \frac{7.5}{25} \frac{5.8}{27} \frac{5.8}{60} \frac{6.2}{100}$

Bldg. $\rightarrow \frac{5.8}{81} \frac{5.8}{60} \frac{5.8}{23} \frac{5.5}{70} \quad 5.4 \quad \frac{5.5}{10} \frac{5.5}{16} \frac{7.7}{21} \frac{7.7}{25} \frac{5.8}{27} \frac{5.8}{60} \frac{6.2}{100}$

$\frac{6.4}{100} \frac{6.7}{60} \frac{6.6}{34} \frac{6.2}{16} \quad 5.9 \quad \frac{6.5}{20} \frac{6.6}{25} \frac{7.7}{28} \frac{7.7}{30} \frac{6.7}{33} \frac{7.1}{60} \frac{7.1}{100}$

$\frac{6.7}{100} \frac{6.7}{60} \frac{6.4}{30} \frac{6.3}{20} \quad 6.0 \quad \frac{6.8}{23} \frac{6.8}{29} \frac{8.0}{34} \frac{8.8}{60} \frac{9.2}{100}$

$\frac{6.5}{100} \frac{6.5}{60} \frac{8.2}{56} \frac{8.2}{39} \frac{6.5}{31} \frac{6.3}{22} \quad 6.0 \quad \frac{6.9}{28} \frac{7.2}{50} \frac{7.7}{100}$

$\frac{6.4}{100} \frac{6.2}{60} \frac{8.2}{56} \frac{8.2}{38} \frac{6.4}{36} \frac{6.4}{25} \quad 6.05 \quad \frac{7.1}{40} \frac{7.3}{60} \frac{7.7}{100}$

$\frac{6.3}{100} \frac{6.2}{60} \frac{6.4}{31} \quad 6.2 \quad \frac{7.1}{50} \frac{7.65}{100} \frac{8.15}{150}$

$\frac{5.65}{150} \frac{5.9}{100} \frac{6.15}{50} \frac{6.43}{50} \quad 7.1 \quad \frac{7.6}{100} \frac{8.15}{150}$

$\frac{6.1}{100} \frac{6.2}{60} \frac{6.3}{32} \quad 6.6 \quad \frac{7.2}{50} \frac{7.8}{100} \frac{8.3}{150}$

$\frac{7.7}{100} \frac{7.8}{60} \frac{7.2}{32} \frac{6.3}{28} \frac{6.4}{24} \quad 6.6 \quad \frac{7.1}{39} \frac{7.1}{60} \frac{8.0}{100}$

$\frac{7.5}{100} \frac{7.5}{60} \frac{7.5}{31} \frac{6.6}{23} \frac{6.6}{17} \quad 6.7 \quad \frac{6.9}{23} \frac{7.5}{35} \frac{8.2}{60} \frac{8.7}{100}$

105

963.06 ✓

+97

56.0

106+00

56.0

B.M.

0.07

956.71 ✓

6.43

956.63 ✓

956.64

+50

55.3

107

54.8

+50

54.2

108

53.5

+50

53.1

109

52.8

+50

52.5

110

52.2

+50

52.0

111

51.9

T.I.P.

3.85

955.06 ✓

5.50

951.21 ✓

+50

Mar. 28-30 = 22°F 51.9

Stiff N.W. wind and How

3-28-30
"Wary Wary"
Windy.

Left

Lat.

±

±

Right

Rt

$\frac{8.0}{100} \frac{8.0}{60} \frac{7.8}{18} \frac{7.2}{14} \frac{7.1}{10} \frac{7.1}{10} \frac{7.1}{14} \frac{9.0}{19} \frac{9.0}{24} \frac{8.5}{25} \frac{8.6}{60} \frac{9.6}{100}$

$\frac{8.0}{100} \frac{8.0}{60} \frac{7.8}{18} \frac{7.2}{14} \frac{7.1}{10} \frac{7.1}{10} \frac{7.1}{15} \frac{9.0}{19} \frac{9.0}{24} \frac{8.5}{25} \frac{9.2}{38} \frac{10.2}{60} \frac{10.2}{100}$

N.W. cor. Mont Larp. + Snelling Sta. 105 + 32.95

$\frac{2.4}{100} \frac{2.4}{60} \frac{2.2}{29} \frac{3.0}{25} \frac{2.7}{19} \frac{1.5}{15} \frac{1.4}{10} \frac{1.4}{10} \frac{1.6}{15} \frac{3.3}{19} \frac{3.8}{60} \frac{3.8}{100}$

$\frac{2.8}{100} \frac{2.8}{60} \frac{2.5}{27} \frac{3.6}{23} \frac{3.6}{18} \frac{2.0}{14} \frac{2.0}{10} \frac{1.9}{10} \frac{2.0}{14} \frac{2.0}{19} \frac{3.6}{24} \frac{3.6}{26} \frac{3.2}{60} \frac{3.7}{100} \frac{4.1}{100}$

$\frac{3.2}{100} \frac{3.7}{60} \frac{3.4}{26} \frac{4.2}{23} \frac{4.2}{19} \frac{2.7}{14} \frac{2.6}{10} \frac{2.5}{10} \frac{2.6}{14} \frac{2.6}{18} \frac{4.3}{23} \frac{4.3}{26} \frac{3.8}{60} \frac{4.4}{100} \frac{5.8}{100}$

$\frac{4.2}{100} \frac{4.2}{60} \frac{4.4}{27} \frac{5.2}{23} \frac{5.2}{19} \frac{3.4}{15} \frac{3.2}{10} \frac{3.2}{10} \frac{3.3}{15} \frac{3.8}{18} \frac{5.0}{24} \frac{5.0}{27} \frac{4.5}{60} \frac{4.8}{100} \frac{5.7}{100}$

$\frac{4.5}{100} \frac{4.5}{60} \frac{5.0}{24} \frac{5.5}{22} \frac{5.5}{18} \frac{3.8}{14} \frac{3.6}{10} \frac{3.6}{10} \frac{3.7}{15} \frac{3.8}{18} \frac{5.5}{25} \frac{5.5}{27} \frac{5.0}{37} \frac{5.2}{100} \frac{5.8}{100}$

$\frac{5.1}{100} \frac{5.0}{60} \frac{5.1}{24} \frac{5.8}{24} \frac{5.8}{19} \frac{4.1}{14} \frac{4.0}{10} \frac{3.9}{10} \frac{4.1}{15} \frac{4.3}{18} \frac{5.6}{24} \frac{5.6}{27} \frac{5.2}{60} \frac{5.5}{100} \frac{6.0}{100}$

$\frac{5.4}{100} \frac{5.4}{60} \frac{5.3}{24} \frac{5.9}{21} \frac{5.9}{18} \frac{4.3}{14} \frac{4.3}{10} \frac{4.2}{10} \frac{4.3}{14} \frac{4.5}{18} \frac{6.0}{30} \frac{5.5}{60} \frac{6.0}{100} \frac{6.5}{100}$

$\frac{5.4}{100} \frac{5.4}{60} \frac{5.8}{24} \frac{6.2}{22} \frac{6.2}{19} \frac{4.8}{15} \frac{4.6}{10} \frac{4.5}{10} \frac{4.5}{14} \frac{4.6}{18} \frac{6.1}{33} \frac{6.0}{60} \frac{6.1}{100} \frac{7.0}{100}$

$\frac{5.8}{100} \frac{5.8}{60} \frac{6.0}{24} \frac{6.5}{22} \frac{6.5}{19} \frac{4.8}{14} \frac{4.7}{10} \frac{4.7}{10} \frac{4.8}{14} \frac{5.0}{18} \frac{6.5}{39} \frac{6.3}{60} \frac{7.0}{100} \frac{7.5}{100}$

$\frac{6.2}{100} \frac{6.3}{60} \frac{5.8}{23} \frac{6.5}{21} \frac{6.5}{18} \frac{5.0}{15} \frac{4.9}{10} \frac{4.8}{10} \frac{4.9}{14} \frac{4.9}{18} \frac{6.8}{33} \frac{7.8}{60} \frac{8.3}{100}$

Nail in T.P. Sta. 112 + 24 = 23' Lt.

$\frac{4.6}{100} \frac{4.8}{60} \frac{4.6}{25} \frac{5.0}{20} \frac{3.3}{14} \frac{3.3}{10} \frac{3.2}{10} \frac{3.3}{14} \frac{3.5}{19} \frac{5.6}{60} \frac{6.4}{100}$

955.06

112 571.8

+50 571.8

113 571.8

+50 571.7

114 571.6

+50 571.6

115 571.5

+50 571.5

116 571.4

+50 571.4

117 571.3

T.P. 4.17 955.63 ✓ 3.60 951.46 ✓

+50 571.2

118 571.2

Still cold and windy Lt
"Darnit"

£

Right

$\frac{4.6}{100} \frac{4.8}{60} \frac{4.8}{23} \frac{5.6}{22} \frac{5.6}{19} \frac{3.5}{14} \frac{3.3}{10} \frac{3.3}{10} \frac{3.4}{10} \frac{3.7}{16} \frac{5.7}{20} \frac{6.0}{60} \frac{6.0}{100}$

$\frac{4.5}{100} \frac{4.5}{60} \frac{4.3}{27} \frac{5.5}{21} \frac{5.5}{19} \frac{3.5}{14} \frac{3.3}{10} \frac{3.3}{10} \frac{3.4}{10} \frac{3.6}{15} \frac{5.5}{19} \frac{5.8}{60} \frac{6.1}{100}$

$\frac{4.0}{100} \frac{4.0}{60} \frac{4.2}{28} \frac{5.3}{20} \frac{3.7}{14} \frac{3.4}{10} \frac{3.3}{10} \frac{3.4}{10} \frac{3.8}{16} \frac{4.8}{18} \frac{5.5}{60} \frac{6.0}{100}$

$\frac{3.8}{100} \frac{3.7}{60} \frac{4.0}{26} \frac{4.8}{20} \frac{3.6}{15} \frac{3.4}{10} \frac{3.4}{10} \frac{3.5}{10} \frac{3.6}{16} \frac{4.6}{18} \frac{5.0}{60} \frac{5.7}{100}$

$\frac{3.8}{100} \frac{3.8}{60} \frac{4.1}{23} \frac{5.1}{21} \frac{5.1}{18} \frac{3.7}{14} \frac{3.5}{10} \frac{3.5}{10} \frac{3.5}{10} \frac{3.7}{15} \frac{4.7}{18} \frac{4.7}{20} \frac{3.7}{22} \frac{4.7}{60} \frac{5.1}{100}$

$\frac{3.7}{100} \frac{4.0}{24} \frac{5.0}{21} \frac{5.0}{18} \frac{3.8}{14} \frac{3.6}{10} \frac{3.5}{10} \frac{3.6}{10} \frac{3.7}{15} \frac{4.4}{17} \frac{4.4}{20} \frac{3.4}{24} \frac{4.0}{32} \frac{4.5}{100}$

$\frac{4.0}{100} \frac{4.0}{23} \frac{4.5}{20} \frac{4.5}{17} \frac{3.8}{14} \frac{3.6}{10} \frac{3.6}{10} \frac{3.6}{10} \frac{3.8}{14} \frac{4.4}{16} \frac{4.4}{19} \frac{3.5}{21} \frac{4.0}{33} \frac{4.2}{100}$

$\frac{4.0}{100} \frac{4.0}{60} \frac{3.6}{40} \frac{4.4}{19} \frac{3.7}{15} \frac{3.7}{10} \frac{3.6}{10} \frac{3.7}{10} \frac{3.8}{15} \frac{4.5}{17} \frac{4.5}{20} \frac{3.3}{22} \frac{3.6}{37} \frac{3.8}{100}$

$\frac{3.9}{100} \frac{3.9}{24} \frac{4.8}{21} \frac{4.6}{18} \frac{3.9}{16} \frac{3.8}{10} \frac{3.7}{10} \frac{3.7}{10} \frac{3.7}{16} \frac{4.4}{18} \frac{4.4}{22} \frac{3.2}{23} \frac{3.8}{35} \frac{4.0}{100}$

$\frac{4.0}{100} \frac{4.2}{24} \frac{4.6}{17} \frac{4.0}{14} \frac{3.7}{10} \frac{3.7}{10} \frac{3.8}{10} \frac{3.9}{16} \frac{4.9}{17} \frac{4.9}{20} \frac{3.4}{22} \frac{4.0}{33} \frac{4.4}{100}$

$\frac{4.1}{100} \frac{4.1}{24} \frac{4.7}{18} \frac{4.1}{16} \frac{3.8}{10} \frac{3.8}{10} \frac{3.8}{10} \frac{3.9}{15} \frac{5.4}{17} \frac{5.4}{20} \frac{4.0}{22} \frac{4.7}{37} \frac{4.8}{100}$

$\frac{4.5}{100} \frac{5.0}{23} \frac{5.5}{21} \frac{5.5}{18} \frac{4.6}{15} \frac{4.4}{10} \frac{4.4}{10} \frac{4.5}{10} \frac{4.9}{14} \frac{6.0}{16} \frac{6.0}{19} \frac{4.8}{22} \frac{5.4}{38} \frac{5.8}{100}$

$\frac{4.6}{100} \frac{5.0}{35} \frac{5.7}{19} \frac{4.8}{14} \frac{4.5}{10} \frac{4.4}{10} \frac{4.5}{10} \frac{5.0}{14} \frac{6.3}{17} \frac{6.3}{20} \frac{5.4}{21} \frac{5.6}{36} \frac{6.0}{100}$

955.63

+50

B.M.

119

4.24 951.39

51.1

51.1

+50

51.0

120

B.M.

2.15

953.54

4.24

951.39

50.9

+50

50.9

121

50.7

+50

50.4

122

50.0

+50

49.5

123

49.0

+50

48.4

124

48.0

+50

47.6

Very cold on Fingers. 10.30 AM.

Left

±

Right

4.4 5.1 5.2 5.7 4.6 4.5 4.5 4.6 5.1 6.6 6.6 5.4 6.0 5.7
100 60 40 20 15 10 10 15 17 21 22 36 100
 Spike in TP 22' Lt - Sta. 118 + 75

4.7 5.1 5.8 5.8 4.7 4.5 4.5 4.7 5.0 6.6 6.6 5.6 6.0 5.7
100 25 23 19 15 10 10 14 17 20 22 37 100

4.9 4.8 5.3 6.3 6.3 5.0 4.7 4.6 4.7 4.8 6.2 5.6 5.7 5.5
100 28 21 21 18 18 10 10 14 18 22 38 100

4.1 4.4 5.5 6.7 6.7 5.4 4.7 4.7 4.8 5.2 5.8 5.3 4.2 4.2
100 27 22 21 19 18 10 10 15 17 23 39 100
 Lit Smoking Lamp 10.30 out at 10.45 AM.

2.8 1.5 3.0 4.6 4.8 3.0 2.7 2.6 2.7 2.8 3.6 1.3 1.3 1.3
100 27 22 21 19 18 10 10 15 18 37 60 100

2.7 1.6 5.2 5.2 3.4 2.7 2.9 2.8 2.9 2.8 3.5 2.8 0.5 0.5
100 24 21 19 18 14 10 10 15 17 30 37 100

3.4 2.4 5.5 5.5 4.0 3.1 3.1 3.2 3.4 4.1 3.4 1.3 0.6 0.6
100 22 21 19 18 10 10 14 17 22 28 40 100

3.5 3.1 5.8 5.8 4.3 3.5 3.5 3.5 3.6 4.7 1.5 1.5
100 22 21 19 18 10 10 14 17 39 100

3.7 4.3 5.7 5.7 4.4 4.0 4.0 4.1 4.1 5.0 2.6 2.7
100 23 21 19 18 10 10 14 17 37 100

House 3.8 4.6 6.5 6.5 4.8 4.6 4.5 4.6 4.4 5.1 3.0 3.5
8.5 31 27 25 24 10 10 15 19 36 100

6.7 5.8 5.0 7.0 7.0 5.7 5.2 5.1 5.2 5.2 6.0 3.8 4.3 4.5
100 60 25 24 22 21 10 10 15 18 35 60 100

8.0 6.0 7.5 7.5 6.7 5.6 5.6 5.5 5.6 5.6 6.4 4.7 5.4 5.7
100 23 22 20 19 14 10 10 15 18 27 60 100

9.2 6.8 8.0 8.0 7.1 6.2 6.0 5.9 6.0 6.4 7.6 6.2 6.6 7.0
100 22 21 19 18 15 10 10 15 19 23 60 100

✓
953.54

125 47.3

+27 47.2

+31 47.2

+48 47.2

+51 47.1

+59 47.1

T.R 3.10 951.13 ✓ 5.51 948.03 ✓

126 46.9

+50 46.8

127 46.7

+50 46.6

128 46.4

+50 46.3

129 46.2

Still very cold

Left $\pm$ Right

$\frac{9.8}{100} \frac{8.7}{60} \frac{7.2}{24} \frac{8.4}{21} \frac{6.4}{15} \frac{6.2}{10} \frac{6.2}{10} \frac{6.3}{10} \frac{6.8}{15} \frac{8.2}{17} \frac{8.2}{20} \frac{6.7}{22} \frac{8.2}{100}$

$\frac{10.0}{100} \frac{9.3}{60} \frac{8.2}{27} \frac{7.1}{17} \frac{6.4}{10} \frac{6.3}{10} \frac{6.4}{10} \frac{6.6}{16} \frac{8.5}{18} \frac{8.5}{21} \frac{7.3}{23} \frac{8.6}{100}$

$\frac{8.3}{100} \frac{8.2}{60} \frac{7.2}{23} \frac{6.4}{10} \frac{6.3}{10} \frac{6.5}{10} \frac{6.6}{15} \frac{8.5}{18} \frac{8.5}{21} \frac{7.3}{23} \frac{8.6}{100}$

$\frac{8.4}{100} \frac{8.3}{60} \frac{7.4}{23} \frac{6.5}{10} \frac{6.3}{10} \frac{6.5}{10} \frac{6.8}{16} \frac{8.9}{18} \frac{9.0}{21} \frac{7.4}{23} \frac{8.7}{100}$

$\frac{10.0}{100} \frac{9.5}{60} \frac{9.0}{21} \frac{7.0}{16} \frac{6.5}{10} \frac{6.4}{10} \frac{6.5}{10} \frac{6.8}{16} \frac{8.9}{18} \frac{8.9}{21} \frac{7.4}{23} \frac{8.8}{100}$

$\frac{9.7}{100} \frac{7.5}{25} \frac{8.8}{22} \frac{8.8}{19} \frac{6.8}{16} \frac{6.5}{10} \frac{6.4}{10} \frac{6.5}{10} \frac{7.1}{15} \frac{9.0}{18} \frac{9.0}{21} \frac{7.4}{23} \frac{8.8}{100}$
Hyd. Mar. 29-30 Cool but Fair 30°F

$\frac{7.2}{100} \frac{6.0}{60} \frac{5.3}{25} \frac{6.6}{21} \frac{6.6}{19} \frac{4.4}{15} \frac{4.2}{10} \frac{4.16}{10} \frac{4.3}{10} \frac{4.6}{15} \frac{6.4}{18} \frac{6.4}{21} \frac{5.6}{22} \frac{6.8}{100}$

$\frac{6.6}{100} \frac{5.1}{22} \frac{6.8}{20} \frac{6.8}{18} \frac{4.4}{14} \frac{4.4}{10} \frac{4.3}{10} \frac{4.4}{10} \frac{4.4}{15} \frac{6.0}{18} \frac{6.0}{21} \frac{5.3}{23} \frac{7.0}{100}$

$\frac{6.0}{100} \frac{5.0}{25} \frac{7.0}{20} \frac{7.0}{20} \frac{4.4}{14} \frac{4.5}{10} \frac{4.4}{10} \frac{4.5}{10} \frac{4.6}{15} \frac{6.2}{17} \frac{6.2}{21} \frac{5.8}{24} \frac{6.7}{100}$

$\frac{3.6}{100} \frac{4.5}{60} \frac{5.0}{23} \frac{6.8}{22} \frac{6.8}{20} \frac{4.5}{15} \frac{4.6}{10} \frac{4.5}{10} \frac{4.6}{10} \frac{5.2}{16} \frac{6.5}{17} \frac{6.5}{21} \frac{5.4}{23} \frac{6.8}{100}$

$\frac{5.8}{100} \frac{5.6}{60} \frac{5.2}{23} \frac{6.7}{21} \frac{6.7}{19} \frac{4.7}{16} \frac{4.8}{10} \frac{4.7}{10} \frac{4.8}{10} \frac{5.4}{15} \frac{6.7}{17} \frac{6.7}{21} \frac{5.7}{22} \frac{4.8}{33} \frac{6.6}{100}$

$\frac{5.2}{100} \frac{5.5}{34} \frac{4.8}{27} \frac{5.4}{22} \frac{6.6}{21} \frac{6.6}{19} \frac{5.1}{17} \frac{4.9}{10} \frac{4.8}{10} \frac{4.9}{10} \frac{5.1}{15} \frac{6.2}{17} \frac{6.2}{21} \frac{5.5}{22} \frac{4.6}{32} \frac{5.7}{47} \frac{5.8}{100}$

$\frac{5.6}{100} \frac{5.5}{36} \frac{4.9}{27} \frac{5.5}{23} \frac{6.8}{22} \frac{6.8}{20} \frac{5.0}{18} \frac{5.0}{10} \frac{4.9}{10} \frac{5.0}{10} \frac{5.2}{16} \frac{6.2}{18} \frac{6.2}{21} \frac{5.2}{23} \frac{4.6}{31} \frac{5.5}{47} \frac{6.0}{100}$

951.13

+50

46.1

130

46.9

+50

45.8

131

45.6

+50

45.4

B.M. 4.39 949.73 ✓ 15.79

945.34 ✓

+69

45.3

+72

45.3

+75

45.3

+90

45.4

132

45.1

+06

44.9

+08

44.9

+50

43.2

Left £ Right

$\frac{5.7}{100}$ $\frac{6.0}{34}$ $\frac{5.6}{25}$ $\frac{6.8}{22}$ $\frac{6.8}{20}$ $\frac{5.1}{16}$ $\frac{5.1}{10}$ $\frac{5.0}{10}$ $\frac{5.2}{10}$ $\frac{5.7}{14}$ $\frac{6.7}{17}$ $\frac{6.7}{20}$ $\frac{5.6}{21}$ $\frac{4.8}{30}$ $\frac{5.8}{47}$ $\frac{6.2}{100}$

$\frac{5.6}{100}$ $\frac{6.2}{40}$ $\frac{5.6}{23}$ $\frac{7.2}{22}$ $\frac{7.2}{20}$ $\frac{5.5}{16}$ $\frac{5.2}{10}$ $\frac{5.2}{10}$ $\frac{5.3}{10}$ $\frac{5.6}{15}$ $\frac{7.0}{18}$ $\frac{7.0}{22}$ $\frac{5.8}{29}$ $\frac{6.5}{47}$ $\frac{6.4}{100}$

$\frac{6.1}{100}$ $\frac{6.4}{60}$ $\frac{6.2}{23}$ $\frac{7.4}{22}$ $\frac{7.4}{20}$ $\frac{6.2}{16}$ $\frac{5.4}{10}$ $\frac{5.3}{10}$ $\frac{5.5}{10}$ $\frac{5.8}{15}$ $\frac{7.0}{17}$ $\frac{7.0}{21}$ $\frac{6.0}{28}$ $\frac{6.8}{47}$ $\frac{6.8}{100}$

$\frac{6.4}{100}$ $\frac{6.4}{38}$ $\frac{5.8}{26}$ $\frac{7.3}{22}$ $\frac{7.3}{19}$ $\frac{5.6}{15}$ $\frac{5.6}{10}$ $\frac{5.5}{10}$ $\frac{5.6}{10}$ $\frac{6.8}{19}$ $\frac{5.8}{27}$ $\frac{6.8}{47}$ $\frac{7.3}{82}$ $\frac{6.8}{100}$

$\frac{5.6}{100}$ $\frac{6.5}{31}$ $\frac{6.0}{23}$ $\frac{7.3}{21}$ $\frac{7.3}{19}$ $\frac{5.8}{16}$ $\frac{5.8}{10}$ $\frac{5.7}{10}$ $\frac{5.8}{10}$ $\frac{6.9}{20}$ $\frac{6.0}{20}$ $\frac{6.0}{28}$ $\frac{6.9}{37}$ $\frac{5.9}{100}$
N.W. cor Mont Hamling & Larp. Ave.

$\frac{4.2}{100}$ $\frac{4.4}{60}$ $\frac{4.7}{47}$ $\frac{5.4}{34}$ $\frac{4.6}{30}$ $\frac{4.4}{10}$ $\frac{4.5}{10}$ $\frac{4.4}{10}$ $\frac{4.8}{20}$ $\frac{5.3}{27}$ $\frac{4.8}{60}$ $\frac{4.4}{100}$

$\frac{5.4}{100}$ $\frac{5.8}{60}$ $\frac{5.5}{40}$ $\frac{4.5}{30}$ $\frac{4.5}{10}$ $\frac{4.4}{10}$ $\frac{4.4}{10}$ $\frac{4.7}{28}$ $\frac{5.4}{35}$ $\frac{5.6}{60}$ $\frac{5.8}{100}$

$\frac{4.2}{100}$ $\frac{4.5}{15}$ $\frac{4.5}{10}$ $\frac{4.4}{10}$ $\frac{4.4}{10}$ $\frac{4.8}{50}$ $\frac{4.8}{100}$

$\frac{3.6}{100}$ $\frac{4.3}{50}$ $\frac{4.5}{10}$ $\frac{4.3}{10}$ $\frac{4.5}{50}$ $\frac{4.4}{50}$ $\frac{4.2}{100}$

$\frac{4.3}{100}$ $\frac{5.0}{50}$ $\frac{4.7}{10}$ $\frac{4.6}{10}$ $\frac{4.7}{10}$ $\frac{4.7}{50}$ $\frac{4.5}{100}$

$\frac{5.2}{100}$ $\frac{5.5}{50}$ $\frac{5.4}{39}$ $\frac{5.0}{10}$ $\frac{4.8}{10}$ $\frac{5.0}{50}$ $\frac{4.8}{100}$

$\frac{4.0}{100}$ $\frac{4.0}{60}$ $\frac{4.3}{32}$ $\frac{5.5}{28}$ $\frac{5.0}{10}$ $\frac{4.8}{10}$ $\frac{5.1}{50}$ $\frac{4.8}{50}$ $\frac{4.5}{100}$

$\frac{3.3}{100}$ $\frac{2.6}{32}$ $\frac{3.7}{23}$ $\frac{3.7}{18}$ $\frac{6.8}{15}$ $\frac{6.8}{10}$ $\frac{6.5}{10}$ $\frac{6.7}{10}$ $\frac{4.4}{48}$ $\frac{4.0}{65}$ $\frac{3.7}{100}$

133		949.73 ✓		40.6 ✓
B.M.	1.03	946.37 ✓	439 ✓	945.34 ✓
+50				38.1
134				35.7 ✓
T.P.	0.79	935.44 ✓	11.72 ✓	934.65 ✓
+50				33.1
135				30.6
+14				29.9
+38				28.7
+60				27.5
136				25.6 ✓
T.P.	0.12	924.94 ✓	10.62 ✓	924.82 ✓
+50				23.1
137				20.5
+28				19.1
+60				17.4

Lat

Long

Alt.

10 12 10.7 10.7 9.3 9.35 9.1 9.4 6.0 3.3 2.5 2.0
 100 35 20 17 15 10 10 37 60 76 100
 NW. cor. Mont Hamline and Larp. Arc.

100 100 85 85 82.5 84 40
 20 17 15 10 10 34
 Mar 31-30
 2500

123 12.3 10.7 10.9 10.7 10.9 9.2 4.0
 21 18 15 10 10 28 40

3.5 3.5 2.3 2.4 2.3 2.5 2.3 3.6
 21 18 15 10 10 14 19

6.2 6.2 4.8 5.0 4.8 5.0 5.3
 23 19 14 10 10 20

7.2 7.2 5.6 5.7 5.5 5.8 5.6 5.5 5.0 1.0
 22 18 15 10 10 14 17 30 40

8.0 8.0 6.7 6.8 6.7 6.9 6.9 8.2 8.8 5.5 5.5
 22 18 15 10 10 14 17 54 85 100

9.2 9.2 8.0 8.0 7.85 8.1 8.1 9.5 9.8 10.4 12.5
 21 17 15 10 1.9 10 14 20 60 80 100

11.4 11.4 10.0 10.0 9.8 10.1 10.1 12.0 12.5 10.7 12.7
 25 18 15 10 10 14 23 60 87 100

2.2 2.2 1.8 2.0 1.8 1.95 1.8 2.3 2.2 3.7
 29 19 15 10 10 14 18 60 100

7.5 2.8 0.4 5.5 4.6 5.8 4.5 4.5 4.4 4.5 4.2 3.8 4.0 5.0 3.5
 100 60 43 33 26 23 18 10 10 15 24 55 60 100

14.5 100 7.4 9.5 7.0 6.0 5.8 6.0 6.0 3.5 4.5 6.0 4.8 3.0
 100 60 35 32 28 10 10 18 28 41 60 42 100

8.2 7.6 7.5 7.7 7.8 5.7 6.2 6.7 7.2
 25 10 10 18 36 60 76 100

+ 924.94 ✓

+ 87

T.R.	10.61	935.43 ✓	0.12	924.82 ✓	16.1
" "	11.65	946.29 ✓	0.79	934.64 ✓	
B.M.	8.97	954.32 ✓	0.95	945.34 ✓	945.35 ✓

133+50

134

+50

135

+14

+38

+60

136

+50

B.M.		897 ✓	945.35 ✓
T.R.	0.33	925.16 ✓	924.83 ✓

138

15.5

Lt

L

Rt.

9.5	8.9	8.8	9.0	8.8	10.8	11.0	13.8	14.7
25	70		10	14	20	45	60	100

N.W. cor. Mont & Hamline & Larp. Ave.

5.0	5.5	5.0	16.2	6.0	6.4
100	60	39		67	100

4.7	4.7	4.6	18.6	5.2	5.8	6.2
100	60	43		51	71	100

15.7	16.2	16.6		13.7	13.4	12.4
5.5	5.0	4.6	21.2	7.5	7.8	8.8
100	75	48		40	60	100

17.5	18.0	18.1		12.5	15.3	15.5
6.2	5.7	5.6	23.7	11.2	8.4	8.2
100	75	51		40	52	100

17.9	18.9	18.8		14.2	16.4	11.9	
6.5	5.5	5.6	24.4	10.2	8.0	12.5	29.9
100	70	52		56	86	100	

18.1	18.3	19.1					
7.5	7.3	6.5	25.6				28.7
100	75	52					

18.8	18.8	19.5					
8.0	8.0	7.3	26.8				27.5
100	75	52					

18.0	19.0	19.7					
10.7	9.7	9.0	28.7				25.6
100	75	57					

10.7	15.7						
20.5	15.5		31.2				23.1
100	55						

Mont. Hamline & Larp. Ave.

10.4	9.9	9.65	9.8	9.8	12.5	12.5	17.0	17.8
23	10		10	14	24	50	60	100

925.16

138

+50

T.P.

0.62

913.41 ✓

✓ 12.37

912.79 ✓

13.1 ✓

139

10.7

+50

08.4

140

06.6

+50

05.2

141

04.4

+50

03.9

142

04.0

+50

T.P.

5.66

906.75 ✓

12.32

901.09 ✓

04.4 ✓

137+60

+87

138

+50

L4

E

R4

$$\begin{array}{r} 13.5 \\ 21 \end{array} \quad \begin{array}{r} 12.2 \\ 15 \end{array} \quad \begin{array}{r} 12.2 \\ 10 \end{array} \quad 12.1 \quad \begin{array}{r} 12.3 \\ 10 \end{array} \quad \begin{array}{r} 12.4 \\ 14 \end{array}$$

$$\begin{array}{r} 5.5 \\ 22 \end{array} \quad \begin{array}{r} 3.1 \\ 14 \end{array} \quad \begin{array}{r} 2.9 \\ 10 \end{array} \quad 2.7 \quad \begin{array}{r} 2.9 \\ 10 \end{array} \quad \begin{array}{r} 2.9 \\ 14 \end{array}$$

$$\begin{array}{r} 5.2 \\ 17 \end{array} \quad \begin{array}{r} 5.2 \\ 10 \end{array} \quad 5.0 \quad \begin{array}{r} 5.2 \\ 10 \end{array} \quad \begin{array}{r} 7.8 \\ 20 \end{array} \quad \begin{array}{r} 9.0 \\ 46 \end{array} \quad \begin{array}{r} \downarrow \\ 80 \end{array}$$

$$\begin{array}{r} 7.0 \\ 23 \end{array} \quad \begin{array}{r} 7.0 \\ 10 \end{array} \quad 6.8 \quad \begin{array}{r} 6.9 \\ 10 \end{array} \quad \begin{array}{r} 7.5 \\ 37 \end{array} \quad \begin{array}{r} \downarrow \\ 60 \end{array}$$

$$\begin{array}{r} 10.5 \\ 21 \end{array} \quad \begin{array}{r} 8.5 \\ 16 \end{array} \quad \begin{array}{r} 8.3 \\ 10 \end{array} \quad 8.2 \quad \begin{array}{r} 8.3 \\ 10 \end{array} \quad \begin{array}{r} 8.3 \\ 38 \end{array} \quad \begin{array}{r} \downarrow \\ 60 \end{array}$$

$$\begin{array}{r} 9.2 \\ 17 \end{array} \quad \begin{array}{r} 9.2 \\ 10 \end{array} \quad 9.0 \quad \begin{array}{r} 9.2 \\ 10 \end{array} \quad \begin{array}{r} 10.7 \\ 33 \end{array} \quad \begin{array}{r} \downarrow \\ 60 \end{array}$$

$$\begin{array}{r} 9.7 \\ 16 \end{array} \quad \begin{array}{r} 9.7 \\ 10 \end{array} \quad 9.5 \quad \begin{array}{r} 9.6 \\ 10 \end{array} \quad \begin{array}{r} 10.0 \\ 31 \end{array} \quad \begin{array}{r} \downarrow \\ 60 \end{array}$$

$$\begin{array}{r} 9.7 \\ 20 \end{array} \quad \begin{array}{r} 9.6 \\ 10 \end{array} \quad 9.4 \quad \begin{array}{r} 9.6 \\ 10 \end{array} \quad \begin{array}{r} 10.6 \\ 60 \end{array} \quad \begin{array}{r} 13.8 \\ 100 \end{array}$$

$$\begin{array}{r} 8.8 \\ 17 \end{array} \quad \begin{array}{r} 9.2 \\ 10 \end{array} \quad 9.0 \quad \begin{array}{r} 9.2 \\ 10 \end{array} \quad \begin{array}{r} 9.2 \\ 30 \end{array} \quad \begin{array}{r} 10.8 \\ 60 \end{array} \quad \begin{array}{r} 12.0 \\ 100 \end{array}$$

Nail in F.P. 130' L4 Sta. 139+00

$$\begin{array}{r} -13.1 \\ 2.5 \\ 100 \end{array} \quad \begin{array}{r} -10.9 \\ 0.3 \\ 60 \end{array} \quad \begin{array}{r} 9.1 \\ +1.0 \\ 39 \end{array} \quad 10.6$$

(17.4)

$$\begin{array}{r} -16.1 \\ 6.8 \\ 100 \end{array} \quad \begin{array}{r} -14.1 \\ 4.8 \\ 60 \end{array} \quad \begin{array}{r} -11.9 \\ 2.6 \\ 40 \end{array} \quad 9.3$$

(16.1)

$$\begin{array}{r} -16.7 \\ 8.0 \\ 100 \end{array} \quad \begin{array}{r} -14.5 \\ 5.8 \\ 60 \end{array} \quad \begin{array}{r} -12.9 \\ 4.2 \\ 45 \end{array} \quad 8.7$$

(15.5)

$$\begin{array}{r} -18.0 \\ 11.7 \\ 100 \end{array} \quad \begin{array}{r} -16.3 \\ 10.0 \\ 67 \end{array} \quad \begin{array}{r} -9.8 \\ 3.5 \\ 34 \end{array} \quad 6.3$$

(13.1)

These points = Edge of Dump
and Pot hole Elev = 889.85

Sta.

906.75

139

+50

140

+50

+80

= 18" V.P.

141

530 ✓ 909.56 ✓ 2.49

904.26 ✓

138+50

909.56

139

4.09

901.65 ✓

12.0

897.56 ✓

11.8

889.85 ✓

7.11

911.37 ✓

904.26 ✓

141+50

142

+50

143

05.1

Lt.

L

15.6 15.6 -14.6 10.4

$$\frac{11.7}{100} \quad \frac{11.7}{60} \quad \frac{10.7}{47} \quad \frac{6.5}{34}$$

3.9

(10.7)

-13.6 -13.8 -13.4

$$\frac{12.0}{100} \quad \frac{12.2}{60} \quad \frac{11.8}{45}$$

1.6

(08.4)

-10.0 -11.6 -11.3

$$\frac{10.2}{100} \quad \frac{11.8}{60} \quad \frac{11.5}{43}$$

+2

(06.6)

-1.4 -9.5 -9.8 -8.4

$$\frac{3.0}{100} \quad \frac{11.1}{78} \quad \frac{11.4}{46} \quad \frac{10.0}{33}$$

+1.6

(05.2)

11.8 ← X Drain Flowline → This end has been covered.

+2.9 +.7 -7.6 -8.0

$$\frac{+0.5}{100} \quad \frac{1.7}{72} \quad \frac{100}{48} \quad \frac{10.4}{33}$$

+2.4

(04.4)

Nail in T.P. 20' Rt. 141+60'

-3.5

$$\frac{-10.2}{52} \quad \frac{-13.5}{100}$$

(13.1)

-1.1

$$\frac{-6.9}{30} \quad \frac{-6.7}{52} \quad \frac{-15.1}{74} \quad \frac{18.1}{100}$$

(10.7)

= Elev Pot hole.

$$\frac{+1.0}{100} \quad \frac{3.0}{78} \quad \frac{5.2}{60} \quad \frac{5.7}{46} \quad \frac{12.8}{34} \quad \frac{12.8}{28} \quad (7.5)$$

$$\frac{+1.5}{100} \quad \frac{4.2}{60} \quad \frac{5.0}{42} \quad \frac{12.0}{32} \quad \frac{12.0}{28} \quad (7.4)$$

$$\frac{2.2}{100} \quad \frac{5.2}{75} \quad \frac{7.2}{41} \quad \frac{11.8}{32} \quad \frac{11.8}{28} \quad (7.0)$$

$$\frac{5.5}{100} \quad \frac{9.2}{42} \quad \frac{11.5}{32} \quad \frac{11.5}{26} \quad \frac{6.3}{16} \quad \frac{6.5}{10} \quad 6.3 \quad \frac{6.4}{10} \quad \frac{6.2}{26} \quad \frac{8.0}{60} \quad \frac{7.5}{100}$$

911.37 ✓

+50

06.3

144

07.5

+13

Toe of Fill rear of House on Rt. 07.8

+26

Top " " " " " " 08.1

+50

08.7

B.M.

7.95 ✓

917.87

1.43

909.94 ✓

909.92

+26

+50

145

09.9

+08

10.1

+12

10.2

+27

10.6

+42

± Fernwood Ave 11.0

+56

11.4

14 2 24.

$\frac{70}{100} \frac{85}{60} \frac{86}{41} \frac{92}{25} \frac{50}{15} \frac{52}{10} 51 \frac{54}{10} \frac{52}{32} \frac{47}{60} \frac{42}{100}$

$\frac{72}{100} \frac{78}{25} \frac{38}{75} \frac{40}{10} 39 \frac{41}{10} \frac{40}{18} \frac{46}{21} \frac{35}{34} \frac{25}{60} \frac{10}{100}$

$\frac{71}{100} \frac{73}{37} \frac{63}{22} \frac{34}{15} \frac{37}{10} 36 \frac{38}{10} \frac{36}{18} \frac{44}{20} \frac{32}{30} \frac{17}{56} \frac{08}{71} \frac{08}{100}$

$\frac{62}{100} \frac{75}{60} \frac{68}{37} \frac{58}{23} \frac{30}{15} \frac{33}{10} 33 \frac{35}{10} \frac{34}{18} \frac{42}{20} \frac{34}{27}$

$\frac{60}{100} \frac{68}{60} \frac{50}{37} \frac{47}{22} \frac{25}{16} \frac{27}{10} 27 \frac{29}{10} \frac{25}{18} \frac{35}{20} \frac{28}{27}$

Chr. Mont $\frac{1}{4} \frac{1}{4}$ Sta. $145 + 0.1$

9.8

$\frac{26}{39} \frac{28}{81} \frac{62}{100}$

9.2

$\frac{22}{38} \frac{22}{46}$ HOUSE

$\frac{85}{100} \frac{85}{60} \frac{84}{34} \frac{95}{30} \frac{86}{25} \frac{82}{10} 80 \frac{81}{10} \frac{78}{16} \frac{97}{22} \frac{71}{26} \frac{65}{32} \frac{33}{36} \frac{24}{60} \frac{10}{100}$

$\frac{77}{100} \frac{80}{60} \frac{82}{35} \frac{95}{28} \frac{85}{25} \frac{80}{10} 78 \frac{79}{10} \frac{58}{32} \frac{35}{36} \frac{30}{60} \frac{12}{100}$

$\frac{75}{100} \frac{81}{60} \frac{83}{33} \frac{92}{27} \frac{86}{25} \frac{79}{10} 77 \frac{78}{10} \frac{61}{10} \frac{40}{60} \frac{12}{100} \text{ S.W.}$

$\frac{72}{100} \frac{75}{60} \frac{78}{38} \frac{90}{26} \frac{73}{15} \frac{75}{10} 73 \frac{73}{10} \frac{56}{50} \frac{24}{100}$

$\frac{62}{100} \frac{72}{60} \frac{68}{41} \frac{90}{26} \frac{69}{15} \frac{70}{10} 69 \frac{70}{10} \frac{58}{36} \frac{42}{60} \frac{17}{100}$

$\frac{66}{100} \frac{72}{60} \frac{72}{42} \frac{90}{26} \frac{66}{15} \frac{67}{10} 65 \frac{67}{10} \frac{61}{30} \frac{48}{60} \frac{22}{100}$

917.87 ✓

+71

11.7

+79

11.9

T.P.

8.91 921.82 ✓ ↓ 4.96 912.91 ✓ ↓

+87

Top Drive on Lt

12.1

+92

Top " " "

12.2

146

12.4

+08

12.6

+11

9.66 922.57 ✓ ↓ 8.91 912.91 ✓ ↓

12.7

+50

14.0
Apr. 1-30 Fair. warmer.

147

15.4

+50

16.4

148

17.1

+50

18.1

149

19.1

Lt

£

Rt.

<u>6.2</u>	<u>6.8</u>	<u>7.2</u>	<u>8.7</u>	<u>6.3</u>	<u>6.3</u>	<u>6.2</u>	<u>6.4</u>	<u>6.0</u>	<u>3.8</u>	<u>1.0</u>
100	60	42	25	16	10		10	25	60	100

<u>6.5</u>	<u>7.0</u>	<u>7.0</u>	<u>8.6</u>	<u>6.1</u>	<u>6.1</u>	<u>6.0</u>	<u>6.2</u>	<u>5.7</u>	<u>6.8</u>	<u>6.8</u>	<u>0.8</u>	<u>+3.0</u>
100	60	41	26	17	10		10	16	20	25	37	100

R.R. in T.F. 22' Lt + Sta 45 + 79

<u>11.0</u>	<u>11.6</u>	<u>12.5</u>	<u>9.8</u>	<u>9.9</u>	<u>9.7</u>	<u>9.9</u>	<u>9.5</u>	<u>12.4</u>	<u>12.4</u>	<u>9.6</u>	<u>8.5</u>	<u>4.5</u>	<u>9.5</u>
100	34	27	22	10		10	16	21	23	26	33	37	100

<u>8.8</u>	<u>9.2</u>	<u>9.7</u>		<u>9.65</u>	<u>9.8</u>	<u>9.4</u>	<u>12.2</u>	<u>12.2</u>	<u>9.8</u>	<u>8.5</u>	<u>4.5</u>	<u>0.4</u>
100	60	10		10	15	20	22	27	32	36	100	

<u>8.8</u>	<u>9.4</u>	<u>9.5</u>	<u>9.4</u>	<u>9.6</u>	<u>9.4</u>	<u>12.1</u>	<u>12.1</u>	<u>5.2</u>	<u>3.0</u>	<u>0.0</u>
100	60	10		10	15	21	23	31	60	100

<u>8.5</u>	<u>9.0</u>	<u>9.4</u>	<u>9.2</u>	<u>9.2</u>	<u>9.4</u>	<u>9.3</u>	<u>11.8</u>	<u>11.8</u>	<u>4.7</u>	<u>2.7</u>	<u>0.0</u>
100	60	28	10		10	16	21	23	31	60	100

<u>8.5</u>	<u>9.2</u>	<u>9.7</u>	<u>12.2</u>	<u>9.0</u>	<u>9.2</u>	<u>9.1</u>	<u>9.3</u>	<u>9.2</u>	<u>11.8</u>	<u>11.8</u>	<u>4.7</u>	<u>2.7</u>	<u>0.5</u>
100	60	30	25	20	10		10	16	21	23	31	60	100

R.R. spike in T.F. 22' Lt + Sta 45 + 79

<u>8.8</u>	<u>8.8</u>	<u>9.0</u>	<u>11.0</u>	<u>11.0</u>	<u>8.7</u>	<u>8.8</u>	<u>8.6</u>	<u>8.9</u>	<u>8.9</u>	<u>11.2</u>	<u>11.2</u>	<u>2.4</u>	<u>+0.5</u>
100	60	32	29	22	16	10		10	15	20	25	39	100

<u>8.0</u>	<u>6.8</u>	<u>6.7</u>	<u>10.1</u>	<u>10.1</u>	<u>7.4</u>	<u>7.4</u>	<u>7.2</u>	<u>7.4</u>	<u>7.1</u>	<u>9.2</u>	<u>9.2</u>	<u>1.0</u>	<u>+1.5</u>
100	60	33	30	21	16	10		10	15	20	26	34	100

<u>7.0</u>	<u>5.6</u>	<u>6.2</u>	<u>10.0</u>	<u>10.0</u>	<u>6.5</u>	<u>6.4</u>	<u>6.2</u>	<u>6.3</u>	<u>6.4</u>	<u>7.9</u>	<u>7.9</u>	<u>1.2</u>	<u>+0.5</u>
100	60	35	30	22	15	10		10	15	18	25	32	100

<u>6.8</u>	<u>5.5</u>	<u>6.0</u>	<u>9.4</u>	<u>9.4</u>	<u>5.8</u>	<u>5.7</u>	<u>5.5</u>	<u>5.6</u>	<u>5.3</u>	<u>7.0</u>	<u>7.0</u>	<u>1.6</u>	<u>+0.8</u>
100	64	35	29	22	15	10		10	15	19	26	32	100

<u>7.5</u>	<u>6.0</u>	<u>6.2</u>	<u>9.0</u>	<u>9.0</u>	<u>4.6</u>	<u>4.7</u>	<u>4.5</u>	<u>4.7</u>	<u>4.4</u>	<u>5.6</u>	<u>5.6</u>	<u>2.5</u>	<u>1.0</u>
100	64	34	30	24	15	10		10	15	18	26	32	100

<u>8.0</u>	<u>6.6</u>	<u>7.4</u>	<u>8.4</u>	<u>8.4</u>	<u>3.6</u>	<u>3.6</u>	<u>3.5</u>	<u>3.6</u>	<u>3.5</u>	<u>4.4</u>	<u>4.1</u>	<u>3.0</u>	<u>1.2</u>
100	62	33	30	23	15	10		10	15	18	30	33	100

922.57 ✓ ↓

+50

20.3

+91

Toe Fill Drive on Lt.

21.2

150+03.

Top on W. Shoulder

21.5

+11

" " E. " 21.7

+22

Toe " " " 22.0

T.P. 8.39 930.63 ✓ 0.33 922.24 ✓

+50

22.8

151

24.4

+50

26.0

+76

26.9

T.P. 4.16 934.02 ✓ 0.77 929.86 ✓

152

27.7

+05

28.0

+26

28.8

10.06 939.92 ✓ 4.16 929.86 ✓

+37

29.1

Lt

L

Rt.

<u>7.7</u>	<u>7.2</u>	<u>7.2</u>	<u>7.8</u>	<u>2.4</u>	<u>2.5</u>	<u>2.3</u>	<u>2.6</u>	<u>2.5</u>	<u>3.7</u>	<u>4.4</u>	<u>2.8</u>	<u>1.7</u>
100	64	34	24	15	10		10	15	19	30	35	100

<u>8.6</u>	<u>8.5</u>	<u>7.2</u>	<u>1.7</u>	<u>1.6</u>	<u>1.4</u>	<u>1.7</u>	<u>1.5</u>	<u>3.7</u>	<u>3.7</u>	<u>2.8</u>	<u>1.4</u>
100	38	23	14	10		10	15	19	30	32	100

<u>3.8</u>	<u>3.4</u>	<u>2.4</u>	<u>1.3</u>	<u>1.1</u>	<u>1.3</u>	<u>1.2</u>	<u>3.8</u>	<u>3.8</u>	<u>2.8</u>	<u>1.4</u>
100	60	27	10		10	14	19	30	32	100

<u>3.8</u>	<u>3.2</u>	<u>2.1</u>	<u>1.1</u>	<u>0.9</u>	<u>1.1</u>	<u>1.0</u>	<u>3.7</u>	<u>3.7</u>	<u>2.7</u>	<u>1.3</u>
100	60	24	10		10	15	19	30	32	100

<u>7.2</u>	<u>7.7</u>	<u>4.8</u>	<u>1.2</u>	<u>0.8</u>	<u>0.6</u>	<u>0.8</u>	<u>0.8</u>	<u>4.0</u>	<u>4.0</u>	<u>2.8</u>	<u>1.6</u>
100	31	21	15	10		10	14	19	31	33	100

<u>13.7</u>	<u>13.7</u>	<u>14.7</u>	<u>13.7</u>	<u>8.1</u>	<u>8.0</u>	<u>7.8</u>	<u>8.1</u>	<u>8.2</u>	<u>11.2</u>	<u>11.3</u>	<u>10.2</u>	<u>8.4</u>
100	60	31	22	14	10		10	14	19	30	32	100

<u>13.8</u>	<u>13.8</u>	<u>14.2</u>	<u>12.5</u>	<u>6.4</u>	<u>6.5</u>	<u>6.25</u>	<u>6.5</u>	<u>6.2</u>	<u>8.8</u>	<u>9.4</u>	<u>7.8</u>	<u>7.3</u>	<u>5.6</u>
100	60	33	22	14	10		10	15	19	31	33	60	100

<u>12.5</u>	<u>10.8</u>	<u>10.0</u>	<u>6.6</u>	<u>4.9</u>	<u>4.8</u>	<u>4.65</u>	<u>4.8</u>	<u>4.7</u>	<u>6.3</u>	<u>6.5</u>	<u>3.1</u>	<u>3.2</u>	<u>2.6</u>
100	60	33	18	15	10		10	15	19	27	33	60	100

<u>11.3</u>	<u>8.7</u>	<u>7.0</u>	<u>5.7</u>	<u>5.3</u>	<u>4.2</u>	<u>4.0</u>	<u>3.75</u>	<u>3.9</u>	<u>3.6</u>	<u>4.8</u>	<u>4.8</u>	<u>0.5</u>	<u>0.0</u>
100	60	35	28	18	15	10		10	15	18	26	32	100

Nail T.P. 22 Rt. 5 + 2. 152 + 40

<u>12.5</u>	<u>10.0</u>	<u>6.0</u>	<u>8.2</u>	<u>8.2</u>	<u>6.5</u>	<u>6.5</u>	<u>6.3</u>	<u>6.5</u>	<u>6.5</u>	<u>7.6</u>	<u>7.5</u>	<u>1.7</u>	<u>2.0</u>	<u>2.0</u>
100	60	22	20	18	15	10		10	15	18	27	30	60	100

<u>11.8</u>	<u>9.0</u>	<u>5.1</u>	<u>7.6</u>	<u>7.6</u>	<u>6.2</u>	<u>6.3</u>	<u>6.0</u>	<u>6.3</u>	<u>6.3</u>	<u>6.7</u>	<u>7.0</u>	<u>7.7</u>
100	60	23	21	18	14	10		10	15	26	60	100

<u>10.5</u>	<u>7.3</u>	<u>3.3</u>	<u>6.2</u>	<u>6.2</u>	<u>5.5</u>	<u>5.4</u>	<u>5.2</u>	<u>5.5</u>	<u>5.5</u>	<u>6.5</u>	<u>6.0</u>
100	60	23	21	17	14	10		10	15	60	100

<u>14.8</u>	<u>11.7</u>	<u>8.1</u>	<u>11.8</u>	<u>11.8</u>	<u>11.0</u>	<u>10.9</u>	<u>10.8</u>	<u>11.0</u>	<u>10.8</u>	<u>11.2</u>	<u>4.0</u>	<u>4.0</u>
100	60	23	21	17	15	10		10	16	62	70	100

Station

✓
939.92 ✓

+50

29.6

153

31.3

+37

32.3

+53

32.6

154

33.7

+22

34.0

+50

34.5

155

35.5

+50

36.7

T.P.

6.68

✓
945.02 ✓

1.58

✓
938.34 ✓

+95

37.9

156

38.0

+34

38.9

+36

39.0

Left

±

Right

<u>14.2</u>	<u>7.8</u>	<u>11.6</u>	<u>11.6</u>	<u>10.4</u>	<u>10.6</u>	<u>10.3</u>	<u>10.6</u>	<u>10.5</u>	<u>10.8</u>	<u>3.7</u>	<u>3.5</u>
100	24	21	17	15	10		10	15	57	64	100

<u>10.2</u>	<u>7.2</u>	<u>4.8</u>	<u>6.5</u>	<u>10.5</u>	<u>10.5</u>	<u>8.7</u>	<u>8.9</u>	<u>8.6</u>	<u>9.1</u>	<u>8.9</u>	<u>13.0</u>	<u>12.0</u>	<u>2.5</u>	<u>2.5</u>
100	60	29	23	21	17	14	10		10	16	23	40	53	100

<u>10.0</u>	<u>7.0</u>	<u>4.4</u>	<u>9.0</u>	<u>9.0</u>	<u>7.8</u>	<u>7.8</u>	<u>7.6</u>	<u>8.0</u>	<u>8.2</u>	<u>9.6</u>	<u>9.6</u>	<u>2.5</u>	<u>2.0</u>	<u>1.2</u>
100	60	23	21	17	15	10		10	14	16	26	40	60	100

<u>10.4</u>	<u>7.5</u>	<u>5.0</u>	<u>8.5</u>	<u>8.5</u>	<u>7.4</u>	<u>7.5</u>	<u>7.3</u>	<u>7.6</u>	<u>7.6</u>	<u>8.0</u>	<u>4.8</u>	<u>2.5</u>	<u>1.3</u>
100	60	23	20	17	15	10		10	14	25	33	60	100

<u>13.4</u>	<u>10.1</u>	<u>6.8</u>	<u>7.8</u>	<u>7.8</u>	<u>6.4</u>	<u>6.4</u>	<u>6.2</u>	<u>6.4</u>	<u>6.4</u>	<u>6.4</u>	<u>4.5</u>	<u>3.3</u>	<u>1.6</u>
100	60	22	21	18	15	10		10	14	25	27	60	100

<u>13.1</u>	<u>10.1</u>	<u>9.1</u>	<u>7.8</u>	<u>7.7</u>	<u>6.1</u>	<u>6.0</u>	<u>5.9</u>	<u>6.1</u>	<u>6.2</u>	<u>7.3</u>	<u>7.3</u>	<u>4.8</u>	<u>2.2</u>
100	60	31	27	19	15	10		10	14	19	25	28	100

<u>13.4</u>	<u>10.5</u>	<u>10.1</u>	<u>5.5</u>	<u>5.6</u>	<u>5.4</u>	<u>5.6</u>	<u>5.6</u>	<u>6.7</u>	<u>6.7</u>	<u>4.7</u>	<u>2.6</u>
100	60	21	16	10		10	15	20	26	30	100

<u>13.0</u>	<u>10.5</u>	<u>10.0</u>	<u>7.5</u>	<u>4.5</u>	<u>4.6</u>	<u>4.4</u>	<u>4.6</u>	<u>4.6</u>	<u>5.8</u>	<u>5.9</u>	<u>4.6</u>	<u>1.6</u>
100	60	30	21	15	10		10	16	19	27	31	100

<u>9.8</u>	<u>8.2</u>	<u>8.0</u>	<u>5.4</u>	<u>3.4</u>	<u>3.4</u>	<u>3.2</u>	<u>3.5</u>	<u>3.5</u>	<u>4.8</u>	<u>4.8</u>	<u>3.0</u>	<u>1.7</u>	<u>0.0</u>
100	60	29	20	15	10		10	15	19	27	30	60	100

<u>11.8</u>	<u>11.1</u>	<u>10.1</u>	<u>8.5</u>	<u>7.4</u>	<u>7.3</u>	<u>7.1</u>	<u>7.4</u>	<u>7.7</u>	<u>8.7</u>	<u>8.7</u>	<u>6.4</u>	<u>4.6</u>
100	60	30	26	15	10		10	15	19	26	29	100

<u>9.4</u>	<u>8.6</u>	<u>7.6</u>	<u>7.8</u>	<u>7.2</u>	<u>7.0</u>	<u>7.3</u>	<u>7.5</u>	<u>8.4</u>	<u>8.4</u>	<u>6.4</u>	<u>4.6</u>
100	60	25	15	10		10	15	19	26	29	100

<u>7.1</u>	<u>6.5</u>	<u>6.2</u>	<u>6.8</u>	<u>6.3</u>	<u>6.1</u>	<u>6.3</u>	<u>6.3</u>	<u>7.6</u>	<u>7.6</u>	<u>5.2</u>	<u>4.8</u>
100	60	27	20	10		10	15	18	25	28	100

<u>6.9</u>	<u>6.3</u>	<u>7.5</u>	<u>7.5</u>	<u>6.3</u>	<u>6.3</u>	<u>6.0</u>	<u>6.3</u>	<u>6.3</u>	<u>7.6</u>	<u>7.6</u>	<u>5.2</u>	<u>4.8</u>
100	23	20	16	14	10		10	15	18	25	28	100

945.02 ✓

Orig. B.M.

+50

39.3

B.M.

4.90

946.72 ✓

3.27

941.75 ✓

941.82 ✓

157

40.4

+16

40.7

+50

41.2

+74

Top Ditch on Lt.

41.4

+79

Bottom " " "

41.5

+82

" " " "

41.6

+87

Top " " "

41.7

158+06.25

L. Lex. Ave.

41.8

+50

41.5

159

40.9

+50

40.7

T.P.

4.04

944.29 ✓

6.47

940.25 ✓

160

40.5

$\frac{5.8}{100}$ $\frac{5.5}{23}$ $\frac{7.1}{20}$ $\frac{7.1}{76}$ $\frac{5.9}{14}$ $\frac{5.9}{10}$ $\frac{5.7}{10}$ $\frac{6.0}{15}$ $\frac{5.9}{18}$ $\frac{7.3}{23}$ $\frac{7.3}{26}$ $\frac{4.7}{60}$ $\frac{5.2}{100}$

Top Gas pipe Ctc Harp + Lex. Ave.

House. $\frac{4.2}{71}$ $\frac{4.8}{24}$ $\frac{7.0}{19}$ $\frac{7.0}{76}$ $\frac{6.3}{15}$ $\frac{6.5}{10}$ $\frac{6.3}{10}$ $\frac{6.5}{15}$ $\frac{6.5}{24}$ $\frac{7.2}{25}$ $\frac{6.0}{56}$ $\frac{6.7}{100}$

House. $\frac{4.2}{81}$ $\frac{4.2}{60}$ $\frac{4.8}{22}$ $\frac{6.3}{20}$ $\frac{6.2}{10}$ 6.0 $\frac{6.3}{10}$ $\frac{6.5}{15}$ $\frac{6.5}{24}$ $\frac{5.2}{31}$ $\frac{5.3}{52.5}$ House

$\frac{4.4}{100}$ $\frac{4.5}{44}$ $\frac{5.0}{43}$ $\frac{5.7}{10}$ 5.5 $\frac{5.8}{10}$ $\frac{6.2}{33}$ $\frac{5.8}{61}$ $\frac{5.8}{100}$ Filling Sta.

$\frac{4.4}{100}$ $\frac{4.4}{64}$ $\frac{5.4}{5.8}$ $\frac{5.4}{38}$ $\frac{5.4}{12}$ 5.3 $\frac{5.6}{16}$ $\frac{6.0}{60}$ $\frac{6.0}{71}$ Filling Sta.

$\frac{7.6}{100}$ $\frac{7.2}{82}$ $\frac{5.4}{73}$ $\frac{5.3}{37}$ $\frac{5.4}{14}$ 5.2 $\frac{5.6}{19}$ $\frac{6.0}{60}$ $\frac{6.0}{71}$ $\frac{5.8}{100}$

$\frac{7.7}{100}$ $\frac{7.1}{90}$ $\frac{5.5}{83}$ $\frac{5.3}{38}$ $\frac{5.4}{1}$ 5.1 $\frac{5.5}{21}$ $\frac{6.0}{60}$ $\frac{6.0}{71}$ $\frac{5.8}{100}$

$\frac{5.8}{100}$ $\frac{5.5}{84}$ $\frac{5.4}{41}$ $\frac{5.3}{21}$ 5.0 $\frac{5.6}{32}$ $\frac{6.0}{60}$ $\frac{5.9}{100}$

$\frac{5.4}{100}$ $\frac{5.1}{50}$ 4.9 $\frac{5.3}{50}$ $\frac{5.7}{100}$

$\frac{5.7}{100}$ $\frac{5.7}{60}$ $\frac{5.4}{17}$ $\frac{5.4}{10}$ 5.2 $\frac{5.5}{10}$ $\frac{5.5}{16}$ $\frac{6.2}{24}$ $\frac{6.5}{82}$ $\frac{5.2}{85}$ $\frac{4.8}{100}$

$\frac{4.0}{100}$ $\frac{5.3}{60}$ $\frac{6.0}{21}$ $\frac{5.9}{10}$ 5.8 $\frac{6.1}{10}$ $\frac{5.8}{15}$ $\frac{6.4}{18}$ $\frac{5.7}{20}$ $\frac{6.2}{76}$ $\frac{5.0}{87}$ $\frac{4.8}{100}$

$\frac{4.8}{100}$ $\frac{5.2}{60}$ $\frac{6.4}{20}$ $\frac{6.1}{10}$ 6.0 $\frac{6.3}{10}$ $\frac{6.0}{15}$ $\frac{6.5}{18}$ $\frac{5.4}{20}$ $\frac{6.5}{100}$

$\frac{2.8}{100}$ $\frac{3.8}{38}$ $\frac{4.8}{19}$ $\frac{3.8}{15}$ $\frac{4.2}{10}$ 3.8 $\frac{4.1}{10}$ $\frac{3.8}{16}$ $\frac{4.1}{60}$ $\frac{4.1}{100}$

Sta. + H.I. - Elev.
944.29 ✓

+50

40.2

161

39.9

+50

39.7

162

39.6

+50

39.5

163

39.5

+50

39.7

164

40.0

+50

40.6

165

41.3

+50

42.3

T.P. 3.13

946.90 ✓ 10.52

943.77 ✓

166

43.3

+50

44.0

Left

L

Right

$\frac{4.8}{100}$	$\frac{5.0}{47}$	$\frac{5.5}{23}$	$\frac{4.4}{16}$	$\frac{4.3}{10}$	4.1	$\frac{4.4}{10}$	$\frac{4.4}{16}$	$\frac{5.3}{25}$	$\frac{5.3}{60}$	$\frac{5.3}{100}$
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$\frac{6.8}{100}$	$\frac{6.8}{60}$	$\frac{7.4}{20}$	$\frac{4.6}{16}$	$\frac{4.5}{10}$	4.4	$\frac{4.8}{10}$	$\frac{5.2}{16}$	$\frac{7.5}{22}$	$\frac{8.0}{60}$	$\frac{8.6}{100}$
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$\frac{7.7}{100}$	$\frac{7.7}{60}$	$\frac{7.5}{21}$	$\frac{4.8}{15}$	$\frac{4.7}{10}$	4.6	$\frac{5.0}{10}$	$\frac{5.2}{16}$	$\frac{7.7}{20}$	$\frac{8.6}{60}$	$\frac{9.2}{100}$
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$\frac{7.6}{100}$	$\frac{7.6}{60}$	$\frac{7.2}{20}$	$\frac{5.3}{16}$	$\frac{4.9}{10}$	4.7	$\frac{5.0}{10}$	$\frac{5.1}{16}$	$\frac{6.5}{19}$	$\frac{7.5}{60}$	$\frac{9.0}{100}$
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$\frac{7.1}{100}$	$\frac{7.0}{60}$	$\frac{7.0}{21}$	$\frac{5.0}{16}$	$\frac{5.0}{10}$	4.8	$\frac{5.0}{10}$	$\frac{5.0}{16}$	$\frac{5.7}{18}$	$\frac{6.4}{60}$	$\frac{6.4}{77}$
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$\frac{6.6}{100}$	$\frac{6.5}{60}$	$\frac{5.8}{20}$	$\frac{5.0}{17}$	$\frac{5.0}{10}$	4.8	$\frac{5.0}{10}$	$\frac{5.1}{16}$	$\frac{6.1}{19}$	$\frac{6.6}{60}$	$\frac{7.4}{100}$
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Flower Boxes → $\frac{5.3}{95}$	$\frac{6.2}{60}$	$\frac{6.2}{20}$	$\frac{5.0}{17}$	$\frac{4.8}{10}$	4.6	$\frac{4.9}{10}$	$\frac{4.8}{15}$	$\frac{6.3}{18}$	$\frac{6.5}{60}$	$\frac{6.3}{100}$
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→ $\frac{4.2}{95}$	$\frac{5.1}{60}$	$\frac{5.5}{31}$	$\frac{5.7}{19}$	$\frac{4.4}{16}$	$\frac{4.5}{10}$	4.3	$\frac{4.6}{10}$	$\frac{4.8}{15}$	$\frac{6.2}{18}$	$\frac{6.3}{60}$	$\frac{6.1}{100}$
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$\frac{4.0}{100}$	$\frac{4.1}{60}$	$\frac{4.4}{25}$	$\frac{5.4}{19}$	$\frac{3.8}{16}$	$\frac{3.9}{10}$	3.7	$\frac{4.0}{10}$	$\frac{4.0}{15}$	$\frac{5.0}{18}$	$\frac{5.0}{60}$	$\frac{5.7}{100}$
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$\frac{3.4}{100}$	$\frac{3.2}{23}$	$\frac{4.2}{21}$	$\frac{4.2}{18}$	$\frac{3.2}{15}$	$\frac{3.0}{10}$	3.0	$\frac{3.2}{10}$	$\frac{3.0}{16}$	$\frac{3.9}{19}$	$\frac{3.3}{60}$	$\frac{3.8}{100}$
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$\frac{2.7}{100}$	$\frac{2.3}{24}$	$\frac{3.3}{21}$	$\frac{3.3}{18}$	$\frac{2.0}{15}$	$\frac{2.2}{10}$	2.0	$\frac{2.2}{10}$	$\frac{2.0}{16}$	$\frac{2.8}{18}$	$\frac{2.8}{60}$	$\frac{3.3}{100}$
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$\frac{3.4}{100}$	$\frac{3.7}{27}$	$\frac{4.5}{24}$	$\frac{4.5}{17}$	$\frac{3.8}{15}$	$\frac{3.8}{10}$	3.6	$\frac{3.8}{10}$	$\frac{3.8}{16}$	$\frac{4.7}{18}$	$\frac{4.3}{60}$	$\frac{4.8}{100}$
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$\frac{2.8}{100}$	$\frac{2.8}{26}$	$\frac{3.5}{24}$	$\frac{3.0}{16}$	$\frac{3.1}{10}$	2.9	$\frac{3.2}{10}$	$\frac{3.2}{16}$	$\frac{4.2}{18}$	$\frac{3.4}{60}$	$\frac{4.0}{100}$
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✓
946.90

167 44.2

+50 44.0

168 6.25 No. 43.7

+50 43.2

169 42.8

B.M. 1.16 ✓ 945.74 ✓ 945.71 ✓

+50 42.2

170 41.9

T.P. 2.70 ✓ 944.04 ✓ 5.56 ✓ 941.34 ✓

+50 41.5

171 41.0

+09 Toe Shoulder Road on No. 40.9

+18 Top " " " " 40.8

+19 = Ctn. Culvert

+37 Top Shoulder No. 40.7

Left

L

Right

$\frac{25}{100}$	$\frac{26}{28}$	$\frac{33}{18}$	$\frac{26}{16}$	$\frac{29}{10}$	2.7	$\frac{29}{10}$	$\frac{30}{17}$	$\frac{35}{18}$	$\frac{31}{60}$	$\frac{37}{100}$
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$\frac{27}{100}$	$\frac{30}{29}$	$\frac{35}{18}$	$\frac{30}{10}$	2.9	$\frac{31}{10}$	$\frac{32}{15}$	$\frac{40}{18}$	$\frac{36}{27}$	$\frac{37}{100}$
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$\frac{31}{100}$	$\frac{30}{26}$	$\frac{43}{21}$	$\frac{43}{18}$	$\frac{33}{16}$	$\frac{34}{10}$	3.2	$\frac{35}{10}$	$\frac{35}{16}$	$\frac{45}{18}$	$\frac{45}{28}$	$\frac{30}{31}$	$\frac{28}{100}$
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$\frac{29}{100}$	$\frac{31}{30}$	$\frac{47}{21}$	$\frac{47}{18}$	$\frac{36}{16}$	$\frac{38}{10}$	3.7	$\frac{39}{10}$	$\frac{37}{17}$	$\frac{46}{19}$	$\frac{44}{28}$	$\frac{32}{31}$	$\frac{34}{100}$
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$\frac{36}{100}$	$\frac{37}{29}$	$\frac{52}{21}$	$\frac{52}{18}$	$\frac{42}{15}$	$\frac{43}{10}$	4.1	$\frac{44}{10}$	$\frac{43}{16}$	$\frac{52}{18}$	$\frac{47}{28}$	$\frac{38}{31}$	$\frac{44}{100}$
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Top Hyd. 22' Ht. Sta. 169 + 23

House $\frac{26}{84}$	$\frac{38}{60}$	$\frac{41}{30}$	$\frac{55}{27}$	$\frac{55}{20}$	$\frac{48}{18}$	$\frac{48}{10}$	4.7	$\frac{49}{10}$	$\frac{48}{15}$	$\frac{56}{19}$	$\frac{56}{21}$	$\frac{44}{23}$	$\frac{55}{100}$
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$\frac{64}{100}$	$\frac{57}{60}$	$\frac{62}{29}$	$\frac{76}{25}$	$\frac{76}{20}$	$\frac{54}{16}$	$\frac{52}{10}$	5.0	$\frac{52}{10}$	$\frac{53}{15}$	$\frac{62}{18}$	$\frac{62}{21}$	$\frac{57}{23}$	$\frac{50}{69}$ ^{House}
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$\frac{54}{100}$	$\frac{52}{60}$	$\frac{50}{29}$	$\frac{66}{25}$	$\frac{62}{20}$	$\frac{29}{16}$	$\frac{27}{10}$	2.5	$\frac{28}{10}$	$\frac{29}{17}$	$\frac{48}{21}$	$\frac{45}{60}$	$\frac{45}{100}$
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$\frac{58}{100}$	$\frac{60}{60}$	$\frac{60}{32}$	$\frac{66}{30}$	$\frac{62}{18}$	$\frac{33}{14}$	$\frac{31}{10}$	3.0	$\frac{32}{10}$	$\frac{36}{15}$	$\frac{57}{20}$	$\frac{52}{60}$	$\frac{50}{81}$ ^{House}
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$\frac{70}{100}$	$\frac{67}{60}$	$\frac{62}{19}$	$\frac{34}{15}$	$\frac{32}{10}$	3.1	$\frac{33}{10}$	$\frac{40}{17}$	$\frac{58}{20}$	$\frac{54}{60}$	$\frac{57}{81}$ ^{House}
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$\frac{42}{100}$	$\frac{41}{60}$	$\frac{33}{15}$	$\frac{33}{10}$	3.2	$\frac{34}{10}$	$\frac{40}{17}$	$\frac{58}{17}$	$\frac{58}{20}$	$\frac{55}{100}$
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37.9

37.44

6.25

Flowlines

6.6

$\frac{43}{100}$	$\frac{41}{60}$	$\frac{35}{17}$	$\frac{35}{10}$	3.3	$\frac{36}{10}$	$\frac{42}{18}$	$\frac{65}{21}$	$\frac{66}{60}$	$\frac{66}{100}$
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+ H.I. 2
944.04 ✓

+42 40.6
Toe of Rd Bed. on North.

172 40.0

+50 39.5

173 39.0

+50 38.5

174 38.2

+50 37.7

175 37.3

T.P. 3.90 939.02 ✓ 892 935.12 ✓

+50 36.4

176 35.7

+19 £ Ditch No. on Victoria 35.3

+40 £ Victoria 34.7

+66 34.0

Left & Right

$\frac{66}{100}$ $\frac{67}{60}$ $\frac{63}{20}$ $\frac{35}{17}$ $\frac{3.5}{10}$ 34 $\frac{36}{10}$ $\frac{42}{17}$ $\frac{65}{20}$ $\frac{68}{100}$

$\frac{55}{100}$ $\frac{62}{27}$ $\frac{58}{18}$ $\frac{42}{15}$ $\frac{4.2}{10}$ 40 $\frac{4.2}{10}$ $\frac{45}{15}$ $\frac{5.5}{18}$ $\frac{5.1}{25}$ $\frac{63}{100}$

$\frac{5.1}{100}$ $\frac{58}{26}$ $\frac{58}{19}$ $\frac{45}{15}$ $\frac{4.6}{10}$ 45 $\frac{4.8}{10}$ $\frac{4.9}{15}$ $\frac{5.9}{19}$ $\frac{5.0}{21}$ $\frac{5.3}{100}$

$\frac{4.6}{100}$ $\frac{57}{27}$ $\frac{58}{18}$ $\frac{5.1}{16}$ $\frac{5.1}{10}$ 50 $\frac{5.2}{10}$ $\frac{5.0}{16}$ $\frac{57}{19}$ $\frac{47}{22}$ $\frac{4.8}{100}$

$\frac{4.4}{100}$ $\frac{56}{27}$ $\frac{58}{18}$ $\frac{54}{15}$ $\frac{57}{10}$ 55 $\frac{56}{10}$ $\frac{53}{16}$ $\frac{58}{19}$ $\frac{45}{23}$ $\frac{5.0}{100}$

$\frac{4.6}{100}$ $\frac{48}{60}$ $\frac{5.0}{30}$ $\frac{58}{22}$ $\frac{6.1}{10}$ 58 $\frac{6.0}{10}$ $\frac{58}{18}$ $\frac{4.4}{22}$ $\frac{5.0}{100}$

$\frac{6.2}{100}$ $\frac{59}{26}$ $\frac{69}{18}$ $\frac{6.4}{15}$ $\frac{65}{10}$ 63 $\frac{6.5}{10}$ $\frac{63}{18}$ $\frac{45}{22}$ $\frac{5.1}{60}$ $\frac{5.1}{100}$

$\frac{6.0}{100}$ $\frac{7.6}{29}$ $\frac{79}{17}$ $\frac{69}{15}$ $\frac{69}{10}$ 67.5 $\frac{7.0}{10}$ $\frac{68}{19}$ $\frac{6.1}{22}$ $\frac{6.0}{60}$ $\frac{6.0}{100}$
 Nail in T.P. 22' Lt 52.176 + 00 Apr. 2-30.

$\frac{3.8}{100}$ $\frac{38}{60}$ $\frac{38}{18}$ $\frac{25}{15}$ $\frac{25}{10}$ 24 $\frac{2.6}{10}$ $\frac{27}{16}$ $\frac{37}{19}$ $\frac{30}{21}$ $\frac{3.8}{60}$ $\frac{3.4}{100}$

$\frac{4.8}{100}$ $\frac{52}{60}$ $\frac{50}{19}$ $\frac{35}{15}$ $\frac{35}{10}$ 33 $\frac{36}{10}$ $\frac{38}{16}$ $\frac{46}{20}$ $\frac{42}{23}$ $\frac{3.8}{100}$

$\frac{5.8}{100}$ $\frac{54}{75}$ $\frac{50}{44}$ $\frac{56}{33}$ $\frac{44}{30}$ $\frac{39}{10}$ 37 $\frac{40}{10}$ $\frac{40}{16}$ $\frac{50}{19}$ $\frac{45}{21}$ $\frac{3.8}{100}$

$\frac{4.8}{100}$ $\frac{44}{50}$ $\frac{45}{10}$ 43 $\frac{45}{10}$ $\frac{42}{16}$ $\frac{53}{20}$ $\frac{41}{22}$ $\frac{35}{100}$

$\frac{6.4}{100}$ $\frac{60}{60}$ $\frac{54}{33}$ $\frac{52}{18}$ $\frac{50}{10}$ $\frac{52}{10}$ $\frac{50}{17}$ $\frac{60}{20}$ $\frac{44}{23}$ $\frac{42}{100}$

✓
939.02

177 33.1

+50 31.3

178 29.4

+07 29.1

+11 28.9

+18 28.7

+21 28.6

T.P. 129 ✓ 929.86 ✓ 10.45 ✓ 928.57 ✓

+80 26.4

179 25.7

+50 24.2

180 23.0

+21 22.8

+50 22.4

Lt £ Rt

Apr. 2-30- 37°F Clear & windy

5.8 4.6 6.0 7.2 5.8 6.1 5.9 6.1 6.1 6.8 6.8 4.4 4.6
100 33 23 20 17 10 10 17 18 21 25 100

6.4 4.2 6.1 8.6 7.6 7.7 7.7 7.7 8.4 8.4 4.6 6.0
100 34 23 20 16 10 10 16 17 20 24 100

7.7 6.5 5.8 8.0 10.6 9.8 9.9 9.65 9.9 9.7 10.4 10.4 6.1 7.8
100 60 34 22 20 17 10 10 16 17 20 25 100

7.8 6.2 8.4 11.0 10.0 10.2 9.9 10.2 10.0 10.4 10.4 6.6 8.6
100 34 22 19 16 10 10 16 17 21 25 100

8.2 6.5 8.5 11.2 10.2 10.3 10.1 10.3 9.8 11.4 11.7 12.7
100 34 22 20 16 10 10 23 36 60 100

8.4 6.8 9.0 11.4 10.4 10.6 10.3 10.6 10.4 9.7 12.4 12.7
100 34 22 20 16 10 10 16 24 43 100

8.6 7.0 9.0 11.5 10.6 10.7 10.4 10.7 10.5 11.1 11.1 8.0 8.6 11.7
100 34 22 20 16 10 10 15 17 21 25 33 36

2.2 0.8 2.8 4.5 3.5 3.7 3.5 3.7 3.4 4.4 4.4 3.2 3.2 ←
100 34 21 19 16 10 10 16 18 21 23 36

4.0 1.6 3.5 6.2 4.5 4.5 4.2 4.4 4.2 5.2 5.2 3.5 3.5 ←
100 34 21 19 16 10 10 16 18 21 23 36

7.0 6.6 4.6 5.8 6.8 6.1 5.9 5.7 5.9 5.5 6.5 6.5 5.4 5.0 ←
100 56 36 22 20 16 10 10 16 18 21 24 36

9.2 9.2 8.2 8.2 6.6 7.0 6.9 7.1 6.8 7.3 5.6
100 47 34 20 16 10 10 16 18 36

9.2 9.2 8.6 7.0 7.3 7.1
100 48 20 16 10

9.0 8.8 8.9 7.6 7.7 7.5
100 50 20 16 10

Green house

✓
929.86

+66

22.3

+81

22.2

181

22.1

+06

22.1

+50

21.9

T.P.

3.49

✓
926.52

✓
6.83

✓
923.03

✓

180+21

+50

£ Ditch West

+66

£ Quincy St.

+81

£ Ditch East

181

+06

+50

T.P.

12.02

✓
932.05

✓
6.49

✓
920.03

✓

182

21.9

L4

L2

L7

$\frac{7.4}{100} \frac{7.5}{60} \frac{8.3}{23} \frac{9.0}{20} \frac{6.6}{16} \frac{7.8}{10} 7.6$

$\frac{6.0}{100} \frac{6.2}{60} \frac{6.6}{33} \frac{8.0}{28} \frac{8.3}{23} \frac{8.8}{20} \frac{7.8}{16} \frac{7.9}{10} 7.7$

$\frac{4.0}{100} \frac{4.5}{60} \frac{5.2}{32} \frac{8.2}{27} \frac{8.2}{22} \frac{8.9}{20} \frac{7.9}{16} \frac{8.0}{10} 7.8$

$\frac{3.5}{100} \frac{4.7}{32} \frac{8.3}{26} \frac{8.3}{21} \frac{9.0}{19} \frac{8.0}{16} \frac{8.0}{10} 7.8$

$\frac{0.4}{100} \frac{2.2}{33} \frac{7.7}{26} \frac{7.7}{23} \frac{9.2}{20} \frac{8.2}{16} \frac{8.2}{10} 8.0$

(37)

$\frac{-3}{40} \frac{-4}{4.1} \frac{+4}{33} \frac{+5}{3.2} \frac{+1}{3.6}$
 $\frac{7.0}{23} \frac{3.6}{16} \frac{7.0}{100}$

4.1

$\frac{-2}{4.3} \frac{0}{4.1} \frac{-1.4}{5.5} \frac{-2.5}{6.6}$
 $\frac{7.0}{18} \frac{6.0}{60} \frac{100}{100}$

4.2

$\frac{4.5}{10} \frac{4.3}{50} \frac{5.3}{100}$

4.3

$\frac{4.6}{7.0} \frac{4.4}{21} \frac{5.8}{50} \frac{6.4}{100}$

4.4

$\frac{4.6}{10} \frac{5.3}{21} \frac{4.8}{32} \frac{5.0}{60} \frac{5.9}{100}$

4.4

$\frac{4.7}{10} \frac{5.0}{17} \frac{5.8}{23} \frac{7.0}{60} \frac{7.4}{100}$

4.6

$\frac{4.9}{10} \frac{4.8}{15} \frac{6.0}{18} \frac{7.6}{60} \frac{8.0}{91} \frac{7.0}{100}$

Mont $\frac{1}{4}$ cor. Sta. 184 + 47.2

$\frac{1.2}{100} \frac{5.5}{33} \frac{9.8}{27} \frac{9.8}{23} \frac{11.4}{21} \frac{11.4}{18} \frac{10.4}{16} \frac{10.4}{10} 10.2$
 $\frac{10.4}{10} \frac{10.6}{15} \frac{12.0}{18} \frac{11.0}{40} \frac{13.5}{60} \frac{13.5}{100}$

Face of Greenhouse.

Orig. BM.

✓
932.05

+50

21.7

183

21.6

+50

21.2

184

20.6

+27

20.3

+37

✓ 20.1

BM.

2.30

✓ 922.31

12.02

✓ 920.03

920.01

+56

19.9

185

19.3

+40

18.8

+43

18.8

186

18.1

+44 = Chr. Cemetery Entrance 17.7

187

16.9

Lt

±

Pt.

7.3	10.2	10.2	11.7	11.7	10.6	10.5	10.4	10.6	10.7	12.1	12.5	11.8
33	28	22	21	18	16	10		10	15	19	49	100
2.2												
100												

32	8.5	10.0	10.0	11.6	11.6	10.6	10.7	10.5	10.8	10.6	12.2	11.0	10.0	10.0
100	33	29	23	21	19	17	10		10	15	19	40	74	100

1.0	6.5	8.6	10.2	10.4	12.0	12.0	11.1	11.1	10.9	11.1	11.2	12.8	11.2	9.0	8.8
100	60	33	28	22	21	18	17	10		10	15	19	38	82	100

0.7	5.4	8.4	11.2	11.2	12.4	12.4	11.6	11.7	11.5	11.8	11.7	13.5	11.2	10.2	10.0
100	60	34	27	22	21	18	17	10		10	15	19	60	80	100

1.1	5.8	9.2	10.2	10.8	12.5	12.5	11.9	12.0	11.8	12.1	11.8	13.5	11.5	11.2	11.5
100	60	33	31	23	21	18	17	10		10	15	19	60	79	100

5.3	7.7	9.5	10.1	10.6	10.8	12.7	12.7	12.0	12.1	12.0	12.2	12.2	13.7	12.0	11.2	12.0
100	77	60	34	32	22	21	18	16	10		10	16	19	60	73	100

Mont Sta. 184 + 47.9

P.M. Fair + windy

2.0	1.6	2.0	3.4	3.4	2.6	2.7	2.4	2.7	2.7	4.0	2.8	2.8
100	60	23	21	18	17	10		10	16	18	60	100

3.0	3.0	3.2	4.2	4.2	3.3	3.2	3.0	3.3	3.7	5.0	4.3	4.3
100	60	23	21	18	16	10		10	14	18	60	100

Dead cat in pits

2.7	3.1	3.8	5.4	5.4	3.7	3.7	3.5	3.7	3.5	5.0	6.7	6.2	6.8
100	60	23	22	19	17	10		10	15	19	60	79	100

2.7	3.1	3.4	3.7	3.5	3.8	3.6	7.1	7.0	7.3
100	60	30	10		10	15	60	75	100

2.8	3.6	4.3	4.4	4.2	4.4	4.2	5.0	4.7	6.0	7.3
100	60	30	10		10	16	20	25	60	100

2.7	3.8	4.7	4.6	4.6	4.9	5.0	6.0	6.6	7.3
100	60	30	10		10	15	18	60	100

Mall.

3.4	4.0	4.0	5.2	5.6	5.4	5.6	5.4	9.0	8.2	9.4
100	60	33	27	10		10	16	23	29	100

✓
922.31

+41

16.4

+44

16.4

188

T.P.

5.21

✓
920.84

6.68

✓
915.63

16.0

+50

15.8

189

15.6

+50

15.6

190

15.6

+50

15.9

191

16.1

+44

X Drain

+50

14.2

T.P.

7.60

✓
922.72

5.72

✓
915.12

192

16.4

+50

16.9

Lt

E

Pt.

Wall
 $\frac{4.0}{100}$ $\frac{4.4}{60}$ $\frac{4.2}{33}$ $\frac{5.8}{26}$ $\frac{6.1}{10}$ $\frac{5.9}{10}$ $\frac{6.1}{10}$ $\frac{6.0}{15}$ $\frac{10.7}{24}$ $\frac{9.7}{32}$ $\frac{10.7}{100}$

$\frac{4.0}{100}$ $\frac{4.5}{60}$ $\frac{4.6}{33}$ $\frac{7.4}{19}$ $\frac{6.0}{17}$ $\frac{6.1}{10}$ $\frac{5.9}{10}$ $\frac{6.2}{10}$ $\frac{6.1}{15}$ $\frac{10.8}{24}$ $\frac{9.8}{32}$ $\frac{10.8}{100}$

$\frac{5.5}{100}$ $\frac{6.3}{60}$ $\frac{7.0}{28}$ $\frac{7.6}{20}$ $\frac{6.2}{17}$ $\frac{6.5}{10}$ $\frac{6.3}{10}$ $\frac{6.6}{10}$ $\frac{6.6}{15}$ $\frac{10.6}{20}$ $\frac{11.6}{29}$ $\frac{12.6}{100}$

$\frac{4.8}{100}$ $\frac{5.4}{60}$ $\frac{5.8}{29}$ $\frac{6.7}{20}$ $\frac{5.0}{17}$ $\frac{5.2}{10}$ $\frac{5.0}{10}$ $\frac{5.3}{10}$ $\frac{5.3}{15}$ $\frac{6.6}{18}$ $\frac{8.2}{25}$ $\frac{9.7}{100}$

$\frac{4.0}{100}$ $\frac{4.7}{60}$ $\frac{5.2}{32}$ $\frac{6.7}{21}$ $\frac{5.1}{19}$ $\frac{5.4}{10}$ $\frac{5.2}{10}$ $\frac{5.4}{10}$ $\frac{5.4}{16}$ $\frac{6.6}{21}$ $\frac{8.2}{100}$

$\frac{2.0}{100}$ $\frac{3.3}{60}$ $\frac{3.8}{33}$ $\frac{6.0}{29}$ $\frac{6.8}{22}$ $\frac{5.4}{18}$ $\frac{5.4}{10}$ $\frac{5.2}{10}$ $\frac{5.4}{16}$ $\frac{5.2}{20}$ $\frac{6.3}{27}$ $\frac{5.7}{27}$ $\frac{6.7}{100}$

$\frac{5.4}{100}$ $\frac{3.7}{60}$ $\frac{3.5}{33}$ $\frac{7.2}{25}$ $\frac{5.2}{17}$ $\frac{5.3}{10}$ $\frac{5.2}{10}$ $\frac{5.4}{10}$ $\frac{5.0}{16}$ $\frac{5.4}{20}$ $\frac{4.7}{24}$ $\frac{4.6}{60}$ $\frac{5.2}{100}$

$\frac{9.2}{100}$ $\frac{8.0}{60}$ $\frac{6.6}{34}$ $\frac{7.5}{26}$ $\frac{5.0}{16}$ $\frac{5.1}{10}$ $\frac{4.9}{10}$ $\frac{5.1}{10}$ $\frac{5.0}{16}$ $\frac{5.6}{18}$ $\frac{5.6}{21}$ $\frac{4.2}{22}$ $\frac{3.0}{60}$ $\frac{4.0}{100}$

$\frac{9.0}{100}$ $\frac{8.7}{60}$ $\frac{7.8}{22}$ $\frac{4.9}{15}$ $\frac{4.9}{10}$ $\frac{4.7}{10}$ $\frac{5.0}{10}$ $\frac{4.9}{16}$ $\frac{6.0}{18}$ $\frac{6.0}{23}$ $\frac{4.6}{28}$ $\frac{3.1}{60}$ $\frac{2.4}{100}$

7.2 ← Flowlines → 6.95

$\frac{8.3}{100}$ $\frac{7.8}{60}$ $\frac{6.8}{19}$ $\frac{5.0}{15}$ $\frac{4.8}{10}$ $\frac{4.6}{10}$ $\frac{4.8}{10}$ $\frac{4.7}{16}$ $\frac{6.4}{18}$ $\frac{6.4}{22}$ $\frac{5.3}{26}$ $\frac{3.1}{100}$
 Se. End X Drain Sta. 191 + 44

$\frac{9.0}{100}$ $\frac{8.5}{60}$ $\frac{7.8}{28}$ $\frac{8.5}{19}$ $\frac{6.5}{15}$ $\frac{6.5}{10}$ $\frac{6.3}{10}$ $\frac{6.5}{10}$ $\frac{6.4}{16}$ $\frac{7.0}{18}$ $\frac{7.0}{20}$ $\frac{6.6}{28}$ $\frac{6.0}{100}$

$\frac{7.7}{100}$ $\frac{7.2}{60}$ $\frac{6.8}{28}$ $\frac{7.6}{19}$ $\frac{6.1}{15}$ $\frac{6.0}{10}$ $\frac{5.8}{10}$ $\frac{6.1}{10}$ $\frac{6.0}{16}$ $\frac{7.2}{19}$ $\frac{6.6}{21}$ $\frac{5.3}{100}$

✓
922.72

193

17.5

+50

18.2

194

✓ 18.9

5.70

✓ 925.69

2.71

✓ 920.01

919.99

+50

19.8

195

20.4

+50

21.0

196

21.4

+50

21.7

197

21.8

+50

✓ 22.0

B.M.

3.29

✓ 925.26

3.73

✓ 921.96

921.97

198

919.52
22.1

+50

22.1

199

21.9

Lt

L

Rt

$\frac{7.0}{100}$	$\frac{6.6}{60}$	$\frac{5.8}{28}$	$\frac{6.2}{19}$	$\frac{5.2}{16}$	$\frac{5.4}{10}$	5.2	$\frac{5.5}{10}$	$\frac{5.5}{16}$	$\frac{6.2}{19}$	$\frac{5.4}{21}$	$\frac{4.2}{60}$	$\frac{4.7}{100}$
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$\frac{6.7}{100}$	$\frac{5.5}{60}$	$\frac{4.7}{23}$	$\frac{5.5}{19}$	$\frac{4.8}{16}$	$\frac{4.7}{10}$	4.5	$\frac{4.7}{10}$	$\frac{4.5}{19}$	$\frac{3.8}{24}$	$\frac{3.2}{60}$	$\frac{3.6}{100}$
-------------------	------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	-------------------

$\frac{5.3}{100}$	$\frac{4.4}{60}$	$\frac{3.3}{21}$	$\frac{4.3}{19}$	$\frac{3.8}{16}$	$\frac{4.0}{10}$	3.8	$\frac{4.0}{10}$	$\frac{4.2}{18}$	$\frac{3.6}{22}$	$\frac{3.1}{60}$	$\frac{3.4}{100}$
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Spike in T.P. 23' Lt Std. 194+00.

$\frac{6.5}{100}$	$\frac{5.8}{60}$	$\frac{5.4}{21}$	$\frac{6.8}{19}$	$\frac{6.1}{16}$	$\frac{6.2}{10}$	5.9	$\frac{6.2}{10}$	$\frac{6.4}{20}$	$\frac{6.0}{22}$	$\frac{6.0}{60}$	$\frac{6.4}{100}$
-------------------	------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	-------------------

$\frac{5.2}{100}$	$\frac{5.2}{60}$	$\frac{5.2}{21}$	$\frac{6.4}{19}$	$\frac{5.3}{16}$	$\frac{5.5}{10}$	5.3	$\frac{5.4}{10}$	$\frac{5.7}{22}$	$\frac{5.4}{31}$	$\frac{6.2}{60}$	$\frac{7.3}{100}$
-------------------	------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	-------------------

$\frac{4.9}{100}$	$\frac{5.2}{60}$	$\frac{4.9}{22}$	$\frac{5.9}{21}$	$\frac{4.9}{16}$	$\frac{4.9}{10}$	4.7	$\frac{5.0}{10}$	$\frac{5.2}{16}$	$\frac{6.2}{19}$	$\frac{5.5}{23}$	$\frac{6.3}{60}$	$\frac{7.3}{100}$
-------------------	------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------	-------------------

$\frac{4.3}{100}$	$\frac{4.8}{60}$	$\frac{4.9}{22}$	$\frac{5.9}{21}$	$\frac{4.5}{16}$	$\frac{4.5}{10}$	4.3	$\frac{4.6}{10}$	$\frac{4.6}{15}$	$\frac{6.0}{20}$	$\frac{6.2}{60}$	$\frac{6.7}{100}$
-------------------	------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	-------------------

$\frac{4.2}{100}$	$\frac{4.5}{60}$	$\frac{4.6}{23}$	$\frac{6.0}{21}$	$\frac{4.5}{16}$	$\frac{4.2}{10}$	4.0	$\frac{4.3}{10}$	$\frac{4.4}{15}$	$\frac{5.7}{19}$	$\frac{5.7}{60}$	$\frac{6.2}{100}$
-------------------	------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	-------------------

$\frac{3.5}{100}$	$\frac{3.5}{60}$	$\frac{3.7}{22}$	$\frac{5.0}{20}$	$\frac{4.2}{16}$	$\frac{4.1}{10}$	3.9	$\frac{4.1}{10}$	$\frac{4.2}{15}$	$\frac{5.5}{18}$	$\frac{5.0}{25}$	$\frac{5.6}{100}$
-------------------	------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	-------------------

$\frac{2.5}{100}$	$\frac{3.0}{60}$	$\frac{4.1}{23}$	$\frac{4.9}{19}$	$\frac{3.8}{16}$	$\frac{4.0}{10}$	3.7	$\frac{4.0}{10}$	$\frac{4.1}{15}$	$\frac{5.1}{60}$	$\frac{5.8}{100}$
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Ctr. Mont $\frac{1}{4}$ Cor.

$\frac{2.5}{100}$	$\frac{2.5}{22}$	$\frac{4.4}{21}$	$\frac{4.4}{18}$	$\frac{3.6}{16}$	$\frac{3.4}{10}$	3.2	$\frac{3.5}{10}$	$\frac{3.7}{15}$	$\frac{4.7}{19}$	$\frac{3.7}{22}$	$\frac{4.1}{32}$	$\frac{6.5}{100}$
-------------------	------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------	-------------------

$\frac{2.5}{100}$	$\frac{2.8}{22}$	$\frac{4.5}{21}$	$\frac{4.5}{18}$	$\frac{3.5}{16}$	$\frac{3.4}{10}$	3.2	$\frac{3.6}{10}$	$\frac{4.0}{15}$	$\frac{4.8}{19}$	$\frac{3.9}{20}$	$\frac{5.2}{60}$	$\frac{6.8}{100}$
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$\frac{2.4}{100}$	$\frac{3.5}{23}$	$\frac{4.8}{21}$	$\frac{4.8}{17}$	$\frac{3.6}{15}$	$\frac{3.7}{10}$	3.4	$\frac{3.7}{10}$	$\frac{3.8}{15}$	$\frac{4.8}{19}$	$\frac{4.2}{20}$	$\frac{5.4}{60}$	$\frac{7.0}{100}$
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✓
925.26

+50

21.7

200

21.5

+50

21.4

201

21.2

+50

21.1

202

T.P.

3.75

✓
924.54

4.47

✓
920.79

20.9

+50

20.7

203

20.5

+50

20.4

204

20.2

+50

20.1

205

20.0

+50

19.9

Let $\frac{1}{2}$ Rf.

Apr. 3-30 - 40°F wonderful

$\frac{26}{100}$ $\frac{39}{22}$ $\frac{52}{21}$ $\frac{52}{17}$ $\frac{38}{15}$ $\frac{38}{10}$ 3.6 $\frac{3.9}{10}$ $\frac{4.1}{15}$ $\frac{5.4}{18}$ $\frac{4.8}{23}$ $\frac{5.8}{60}$ $\frac{7.0}{100}$

$\frac{26}{100}$ $\frac{42}{23}$ $\frac{55}{21}$ $\frac{55}{18}$ $\frac{40}{15}$ $\frac{3.9}{10}$ 3.8 $\frac{4.0}{10}$ $\frac{4.1}{15}$ $\frac{6.0}{18}$ $\frac{5.3}{22}$ $\frac{6.2}{60}$ $\frac{7.2}{100}$

$\frac{4.2}{100}$ $\frac{4.7}{60}$ $\frac{4.9}{23}$ $\frac{5.9}{22}$ $\frac{5.9}{18}$ $\frac{4.1}{15}$ $\frac{4.1}{10}$ 3.9 $\frac{4.2}{10}$ $\frac{4.2}{14}$ $\frac{6.0}{18}$ $\frac{5.0}{22}$ $\frac{6.0}{60}$ $\frac{6.7}{100}$

$\frac{3.7}{100}$ $\frac{3.8}{60}$ $\frac{4.2}{23}$ $\frac{6.0}{22}$ $\frac{6.0}{18}$ $\frac{4.4}{16}$ $\frac{4.3}{10}$ 4.1 $\frac{4.4}{10}$ $\frac{4.5}{15}$ $\frac{5.7}{18}$ $\frac{5.3}{23}$ $\frac{6.0}{60}$ $\frac{6.7}{100}$

$\frac{3.9}{100}$ $\frac{3.5}{60}$ $\frac{3.7}{23}$ $\frac{5.8}{21}$ $\frac{5.8}{18}$ $\frac{4.3}{16}$ $\frac{4.5}{10}$ 4.2 $\frac{4.5}{10}$ $\frac{4.5}{15}$ $\frac{5.5}{17}$ $\frac{5.0}{22}$ $\frac{4.5}{36}$ $\frac{7.0}{100}$

$\frac{4.4}{100}$ $\frac{4.2}{60}$ $\frac{4.0}{23}$ $\frac{5.8}{22}$ $\frac{5.8}{20}$ $\frac{4.3}{16}$ $\frac{4.6}{10}$ 4.35 $\frac{4.6}{10}$ $\frac{4.6}{15}$ $\frac{5.7}{17}$ $\frac{5.0}{30}$ $\frac{5.8}{60}$ $\frac{6.8}{100}$

$\frac{4.4}{100}$ $\frac{4.4}{23}$ $\frac{5.5}{21}$ $\frac{5.5}{18}$ $\frac{3.8}{15}$ $\frac{3.9}{10}$ 3.8 $\frac{4.1}{10}$ $\frac{4.1}{15}$ $\frac{5.5}{16}$ $\frac{4.8}{31}$ $\frac{5.8}{60}$ $\frac{6.1}{100}$

$\frac{4.8}{100}$ $\frac{4.6}{23}$ $\frac{5.6}{21}$ $\frac{5.6}{18}$ $\frac{4.0}{15}$ $\frac{4.1}{10}$ 4.0 $\frac{4.2}{10}$ $\frac{4.2}{15}$ $\frac{6.2}{18}$ $\frac{5.2}{27}$ $\frac{5.6}{60}$ $\frac{5.8}{100}$

$\frac{4.5}{100}$ $\frac{4.2}{60}$ $\frac{4.6}{23}$ $\frac{6.0}{21}$ $\frac{6.0}{18}$ $\frac{4.2}{16}$ $\frac{4.3}{10}$ 4.1 $\frac{4.4}{10}$ $\frac{4.1}{15}$ $\frac{6.2}{18}$ $\frac{6.2}{22}$ $\frac{5.2}{23}$ $\frac{5.2}{100}$

$\frac{4.4}{100}$ $\frac{4.7}{22}$ $\frac{5.7}{21}$ $\frac{5.7}{18}$ $\frac{4.4}{16}$ $\frac{4.5}{10}$ 4.3 $\frac{4.5}{10}$ $\frac{4.4}{15}$ $\frac{6.0}{17}$ $\frac{6.0}{21}$ $\frac{4.9}{23}$ $\frac{4.2}{100}$

$\frac{5.2}{100}$ $\frac{4.6}{23}$ $\frac{5.6}{21}$ $\frac{5.6}{18}$ $\frac{4.5}{15}$ $\frac{4.6}{10}$ 4.4 $\frac{4.7}{10}$ $\frac{4.4}{15}$ $\frac{5.8}{18}$ $\frac{5.8}{22}$ $\frac{4.4}{23}$ $\frac{4.2}{100}$

$\frac{5.2}{100}$ $\frac{4.6}{23}$ $\frac{5.5}{21}$ $\frac{5.5}{18}$ $\frac{4.8}{15}$ $\frac{4.7}{10}$ 4.5 $\frac{4.8}{10}$ $\frac{4.7}{15}$ $\frac{5.5}{18}$ $\frac{5.5}{22}$ $\frac{4.4}{23}$ $\frac{3.5}{100}$

$\frac{4.8}{100}$ $\frac{4.7}{60}$ $\frac{4.6}{25}$ $\frac{5.8}{20}$ $\frac{4.8}{16}$ $\frac{4.9}{10}$ 4.6 $\frac{4.9}{10}$ $\frac{5.0}{16}$ $\frac{6.1}{18}$ $\frac{6.1}{22}$ $\frac{4.5}{23}$ $\frac{4.2}{100}$

✓
924.54

206

19.7

+50

19.5

207

19.4

+50

19.3

T.P.

3.74

✓ 922.80

5.48

✓ 919.06

208

19.1

+50

19.0

209

18.8

+34

= 15" x 42' C.M. Cross Drain

+50

3.84

96
918.93

18.7

210

18.9

+16

End Ditch on Lt.

18.9

+20

19.0

+54

19.0

Left £ Right

$\frac{5.1}{100}$ $\frac{5.1}{23}$ $\frac{6.1}{21}$ $\frac{6.1}{18}$ $\frac{5.1}{16}$ $\frac{5.0}{10}$ 4.8 $\frac{4.7}{10}$ $\frac{5.0}{16}$ $\frac{6.2}{19}$ $\frac{6.2}{21}$ $\frac{4.5}{22}$ $\frac{4.9}{10}$

→ $\frac{4.4}{72}$ $\frac{4.8}{60}$ $\frac{5.8}{22}$ $\frac{6.7}{21}$ $\frac{6.7}{18}$ $\frac{5.3}{16}$ $\frac{5.2}{10}$ 5.0 $\frac{5.2}{10}$ $\frac{5.1}{15}$ $\frac{6.7}{18}$ $\frac{6.7}{21}$ $\frac{5.0}{22}$ $\frac{5.9}{100}$

Porch $\frac{4.8}{100}$ $\frac{5.6}{23}$ $\frac{6.8}{22}$ $\frac{6.8}{18}$ $\frac{5.5}{15}$ $\frac{5.3}{10}$ 5.1 $\frac{5.4}{10}$ $\frac{5.5}{15}$ $\frac{7.1}{18}$ $\frac{7.1}{21}$ $\frac{5.7}{23}$ $\frac{6.8}{100}$

$\frac{4.8}{100}$ $\frac{5.6}{60}$ $\frac{6.4}{23}$ $\frac{7.6}{21}$ $\frac{7.6}{18}$ $\frac{5.4}{15}$ $\frac{5.4}{10}$ 5.2 $\frac{5.5}{10}$ $\frac{5.5}{15}$ $\frac{7.5}{18}$ $\frac{7.5}{21}$ $\frac{6.8}{22}$ $\frac{7.5}{100}$

$\frac{4.3}{100}$ $\frac{5.0}{60}$ $\frac{5.5}{22}$ $\frac{6.2}{20}$ $\frac{4.0}{15}$ $\frac{3.8}{10}$ 3.7 $\frac{3.9}{10}$ $\frac{4.2}{14}$ $\frac{6.4}{20}$ $\frac{5.6}{22}$ $\frac{6.5}{100}$

$\frac{4.5}{100}$ $\frac{5.2}{60}$ $\frac{5.5}{22}$ $\frac{6.4}{20}$ $\frac{4.0}{15}$ $\frac{4.0}{10}$ 3.8 $\frac{4.1}{10}$ $\frac{4.3}{14}$ $\frac{6.6}{20}$ $\frac{5.8}{22}$ $\frac{6.4}{100}$

$\frac{4.9}{100}$ $\frac{5.2}{60}$ $\frac{5.5}{22}$ $\frac{6.2}{19}$ $\frac{4.2}{15}$ $\frac{4.2}{10}$ 4.0 $\frac{4.3}{10}$ $\frac{4.2}{14}$ $\frac{6.2}{20}$ $\frac{5.6}{22}$ $\frac{5.2}{100}$

6.15 ← ~~Flowlines~~ → 6.05

$\frac{4.7}{100}$ $\frac{5.3}{21}$ $\frac{6.1}{20}$ $\frac{6.1}{18}$ $\frac{4.3}{15}$ $\frac{4.2}{10}$ 4.1 $\frac{4.3}{10}$ $\frac{4.2}{14}$ $\frac{6.5}{19}$ $\frac{5.4}{22}$ $\frac{4.7}{100}$

$\frac{4.2}{100}$ $\frac{4.0}{82}$ $\frac{4.9}{75}$ $\frac{5.5}{33}$ $\frac{4.7}{21}$ $\frac{5.5}{20}$ $\frac{5.5}{17}$ $\frac{4.4}{15}$ $\frac{4.1}{10}$ 3.9 $\frac{4.2}{10}$ $\frac{4.2}{14}$ $\frac{5.6}{17}$ $\frac{5.2}{22}$ $\frac{4.3}{100}$

$\frac{3.4}{100}$ $\frac{3.8}{78}$ $\frac{4.4}{67}$ $\frac{3.9}{45}$ $\frac{4.5}{25}$ $\frac{6.0}{24}$ $\frac{6.0}{21}$ $\frac{4.1}{19}$ $\frac{4.0}{10}$ 3.9 $\frac{4.1}{10}$ $\frac{4.0}{15}$ $\frac{5.5}{19}$ $\frac{5.0}{21}$ $\frac{4.0}{100}$

$\frac{3.4}{100}$ $\frac{3.8}{73}$ $\frac{4.4}{64}$ $\frac{4.0}{51}$ $\frac{4.0}{19}$ $\frac{4.0}{10}$ 3.8 $\frac{4.0}{10}$ $\frac{4.0}{15}$ $\frac{5.5}{19}$ $\frac{5.0}{21}$ $\frac{4.0}{100}$

$\frac{5.2}{100}$ $\frac{4.4}{62}$ $\frac{3.5}{34}$ $\frac{3.9}{10}$ 3.8 $\frac{4.0}{27}$ $\frac{4.0}{36}$ $\frac{4.7}{47}$ $\frac{3.7}{50}$ $\frac{3.5}{100}$

✓
922.80

+56

Ditch on Rt.

19.0

+75²⁵ Mont $\frac{33}{0875}$ $\frac{1}{2}$ Dale St. South. 19.0
Rt.

+96

End of Project - 19.2

+98

19.2

211+08.75 R/W. East side Dale St. South 19.35

B.M. 384 918.96 918.93 (.03)

Left

L

Right

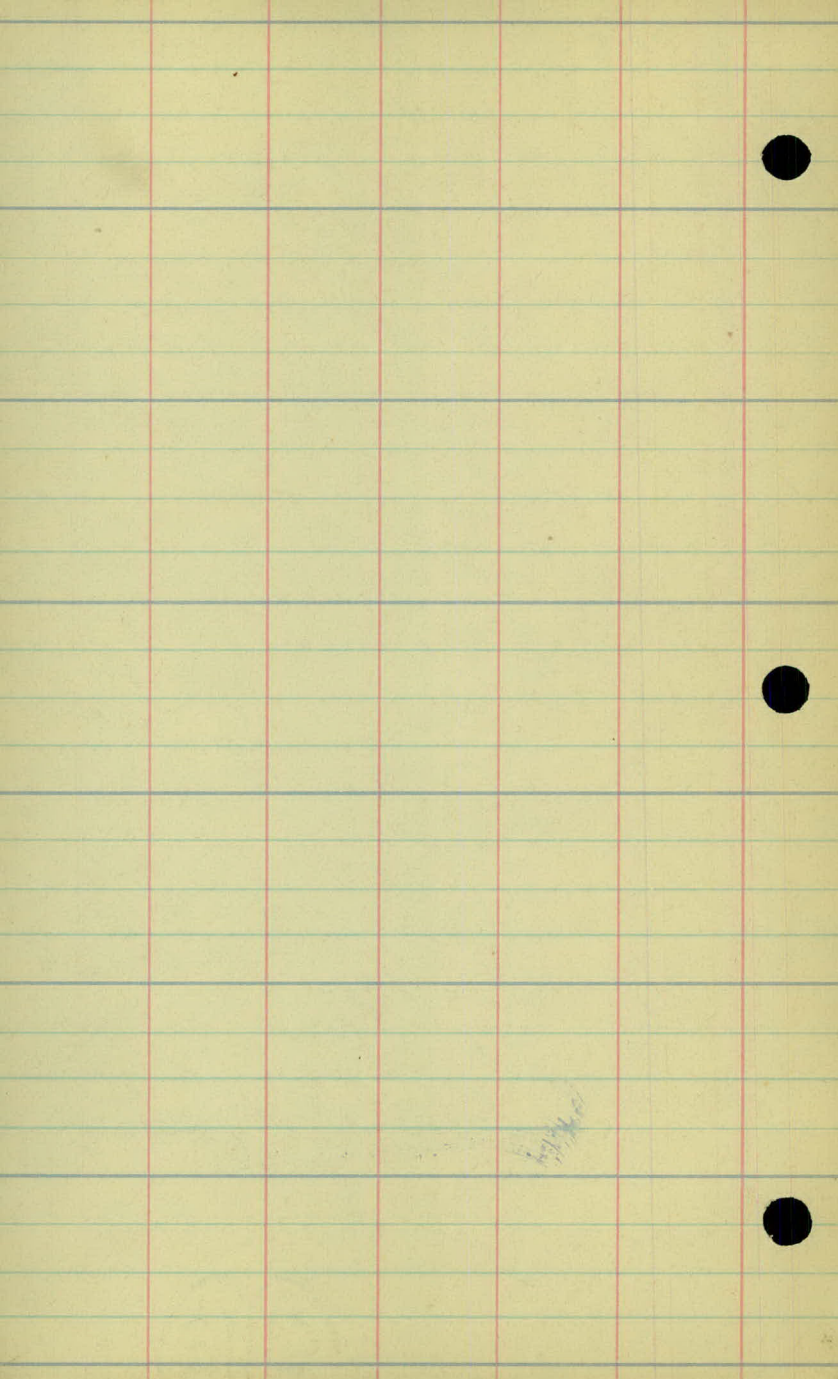
$\frac{5.2}{100}$	$\frac{4.4}{60}$	$\frac{3.5}{34}$	$\frac{3.9}{10}$	3.8	$\frac{4.0}{29}$	$\frac{3.8}{35}$	$\frac{4.7}{48}$	$\frac{4.8}{60}$	$\frac{5.0}{100}$
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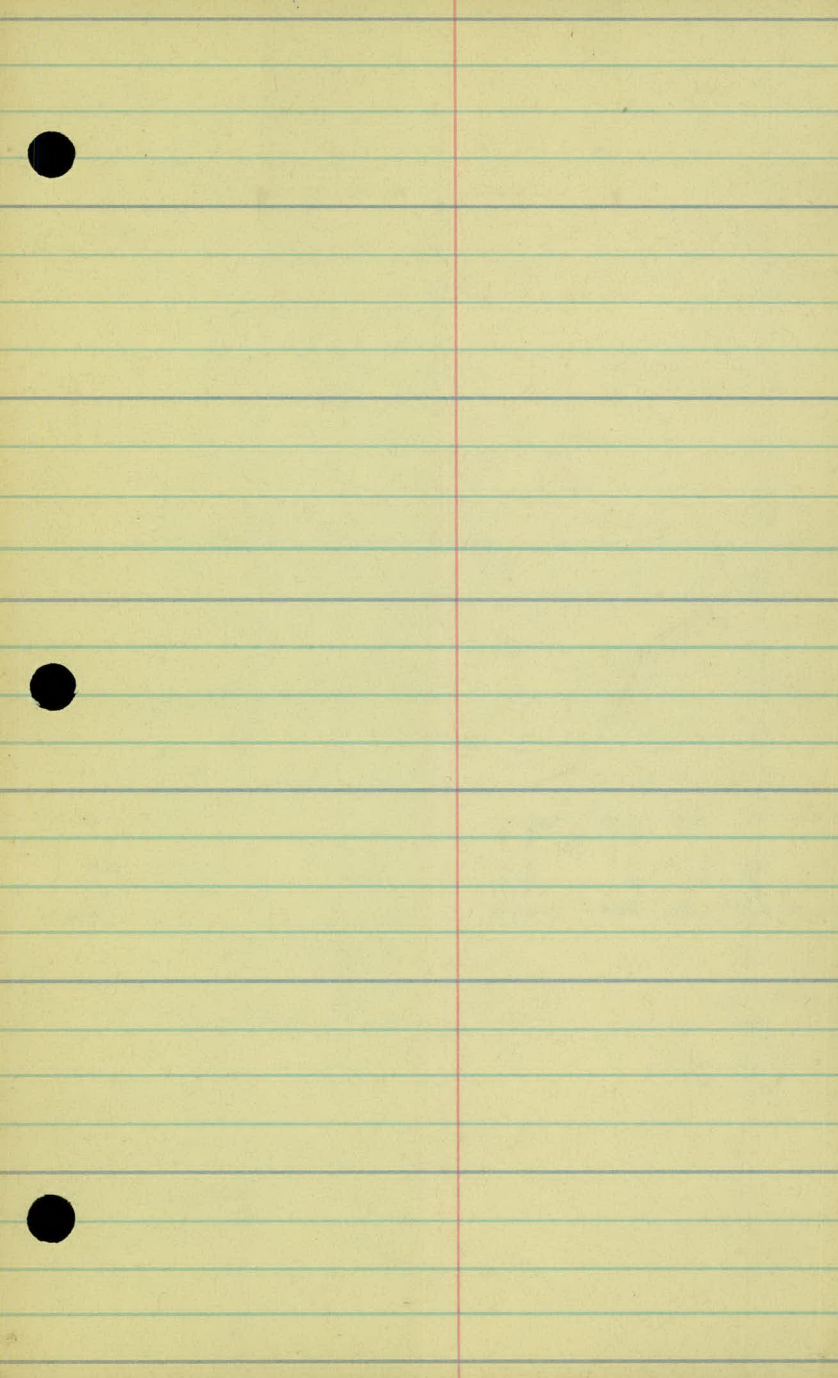
$\frac{5.6}{100}$	$\frac{5.2}{57}$	$\frac{4.4}{50}$	$\frac{3.6}{20}$	$\frac{3.8}{10}$	3.8	$\frac{4.0}{50}$	$\frac{4.15}{100}$
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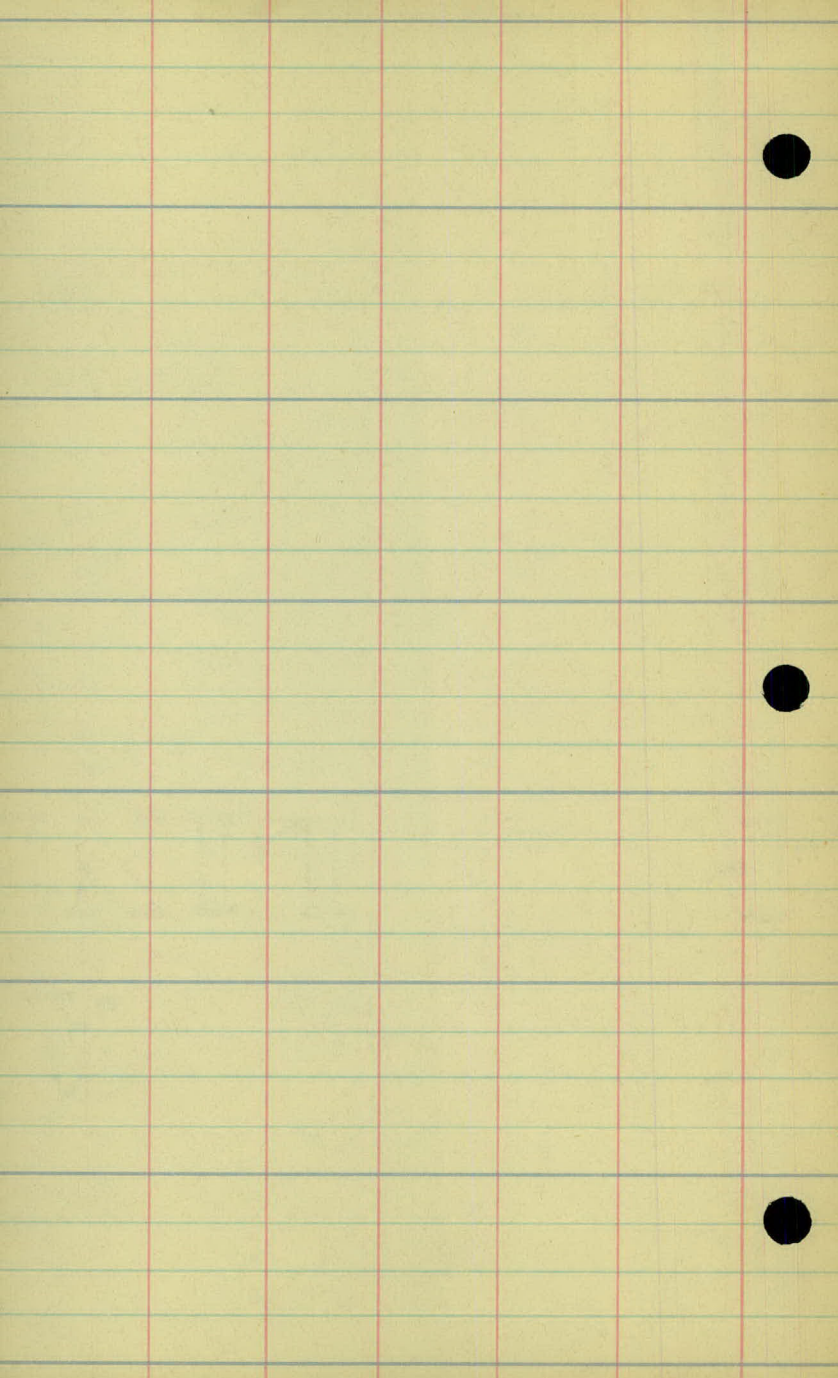
$\frac{5.7}{100}$	$\frac{5.1}{60}$	$\frac{4.7}{25}$	$\frac{3.9}{19}$	$\frac{3.5}{12}$	3.6	$\frac{3.8}{13}$	$\frac{4.3}{28}$	$\frac{4.6}{60}$	$\frac{4.8}{100}$
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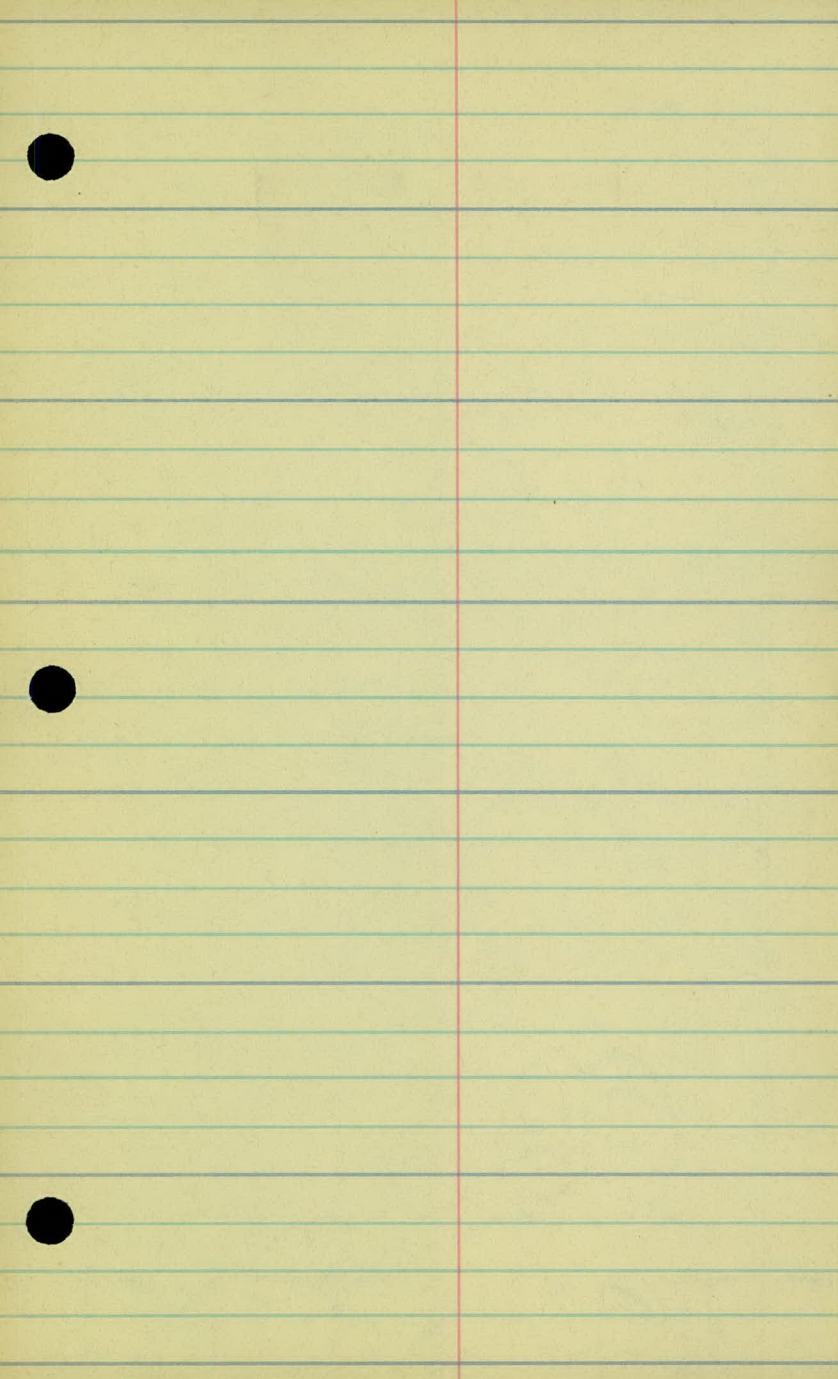
$\frac{5.7}{100}$	$\frac{5.1}{60}$	$\frac{4.7}{25}$	$\frac{3.9}{19}$	$\frac{3.5}{12}$	3.6	$\frac{3.7}{16}$	$\frac{4.5}{20}$	$\frac{4.5}{25}$	$\frac{3.7}{26}$	$\frac{3.5}{60}$	$\frac{3.4}{100}$
-------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------	-------------------

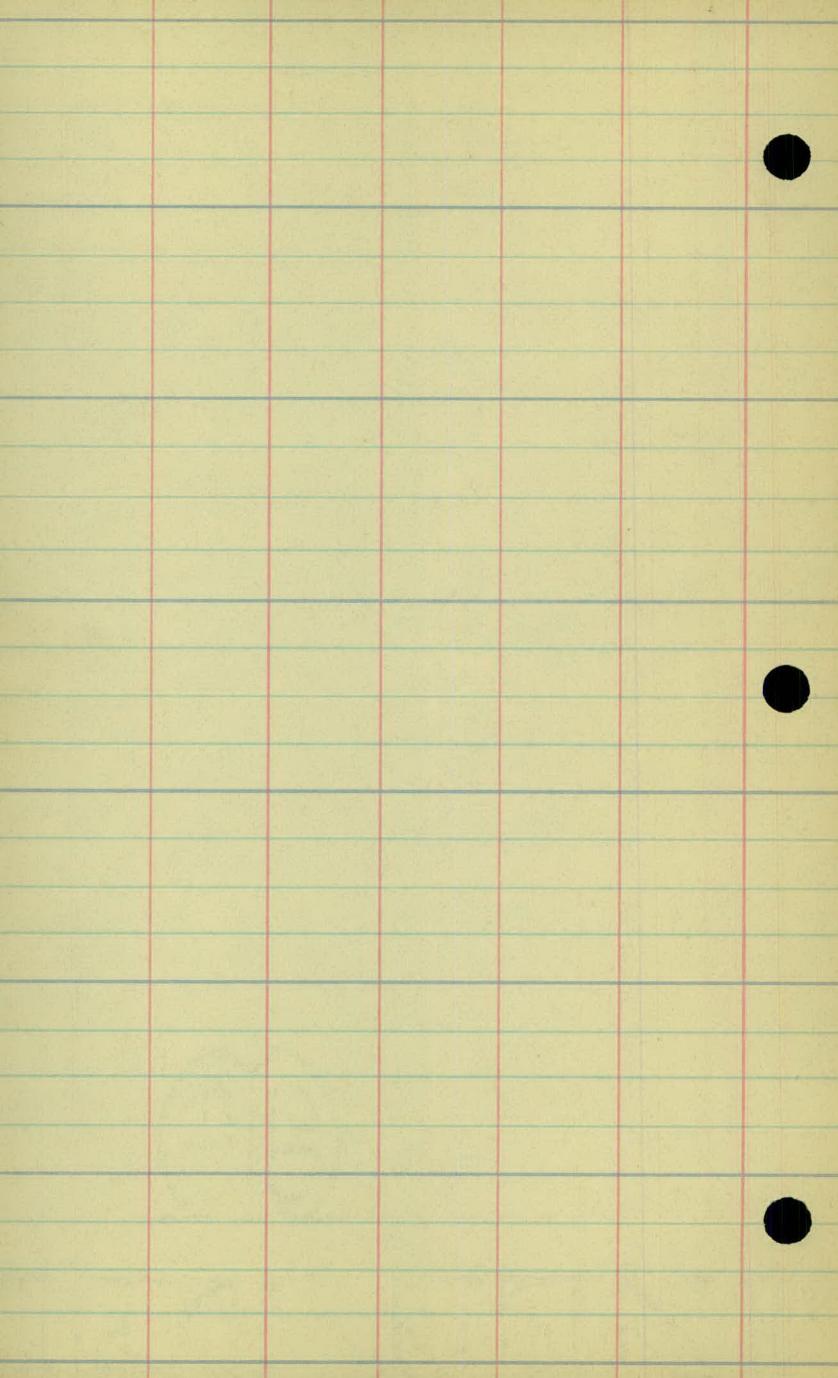
$\frac{5.6}{100}$	$\frac{5.3}{60}$	$\frac{4.9}{24}$	$\frac{3.9}{17}$	$\frac{3.5}{12}$	3.45	$\frac{3.6}{13}$	$\frac{3.9}{14}$	$\frac{4.6}{21}$	$\frac{4.6}{25}$	$\frac{3.8}{26}$	$\frac{3.8}{100}$
-------------------	------------------	------------------	------------------	------------------	------	------------------	------------------	------------------	------------------	------------------	-------------------

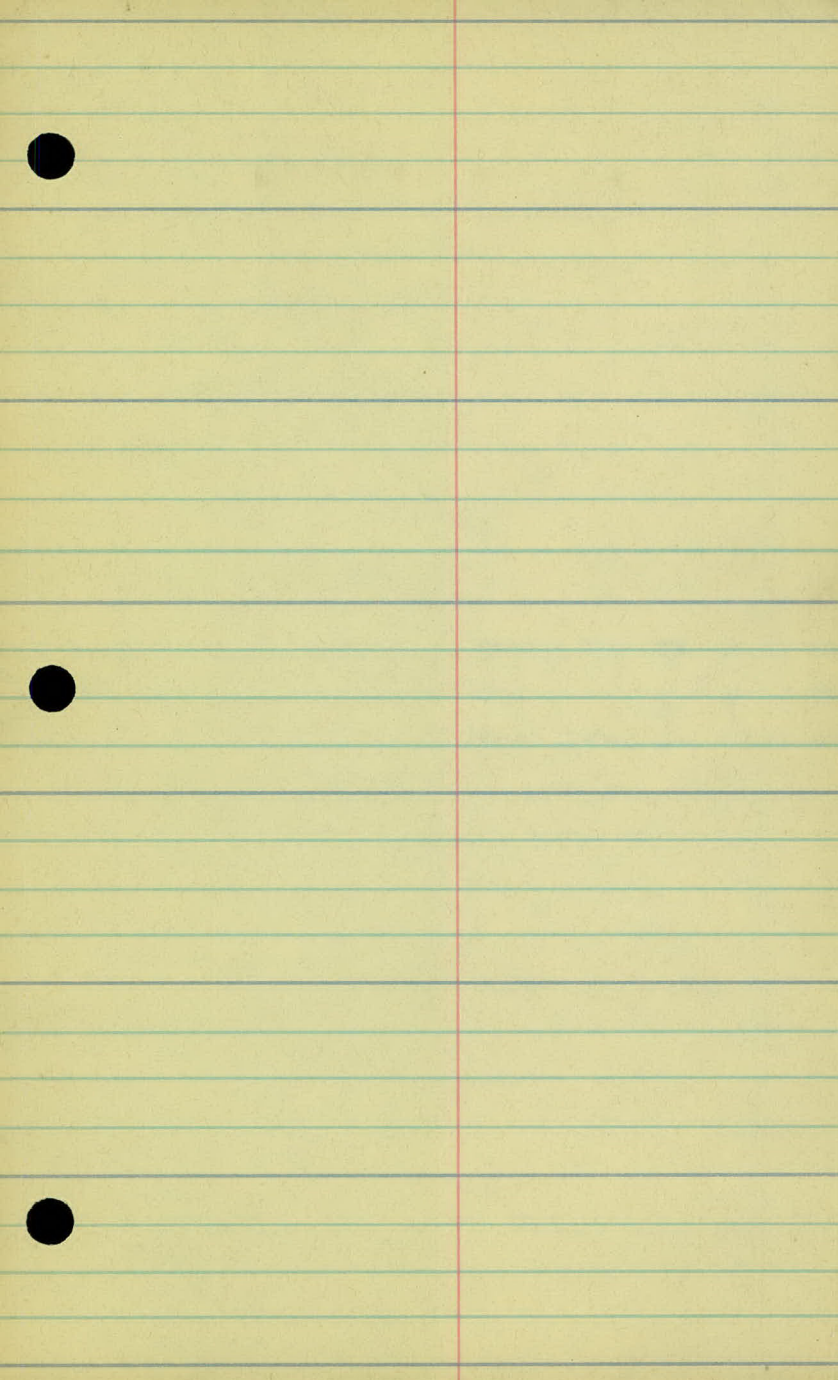


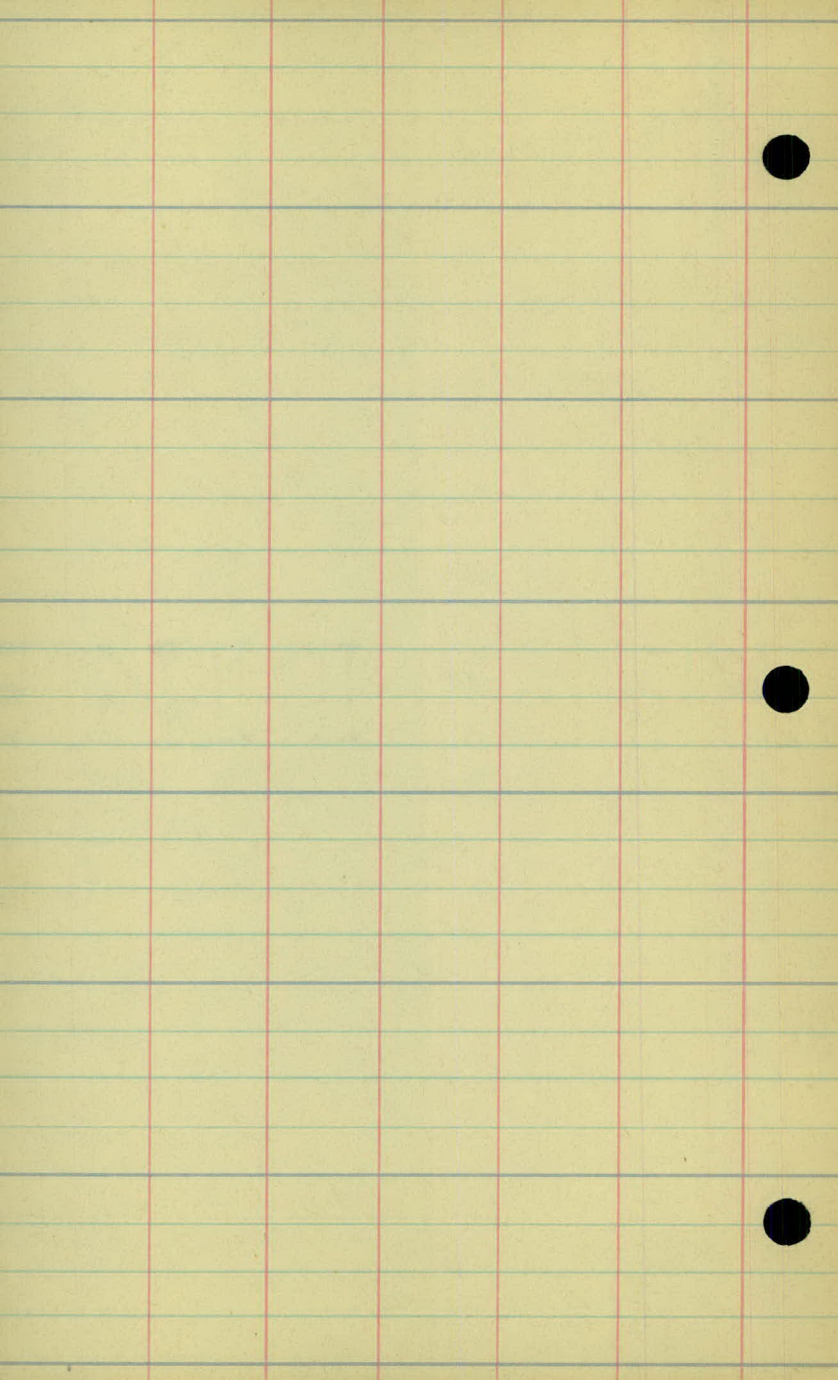


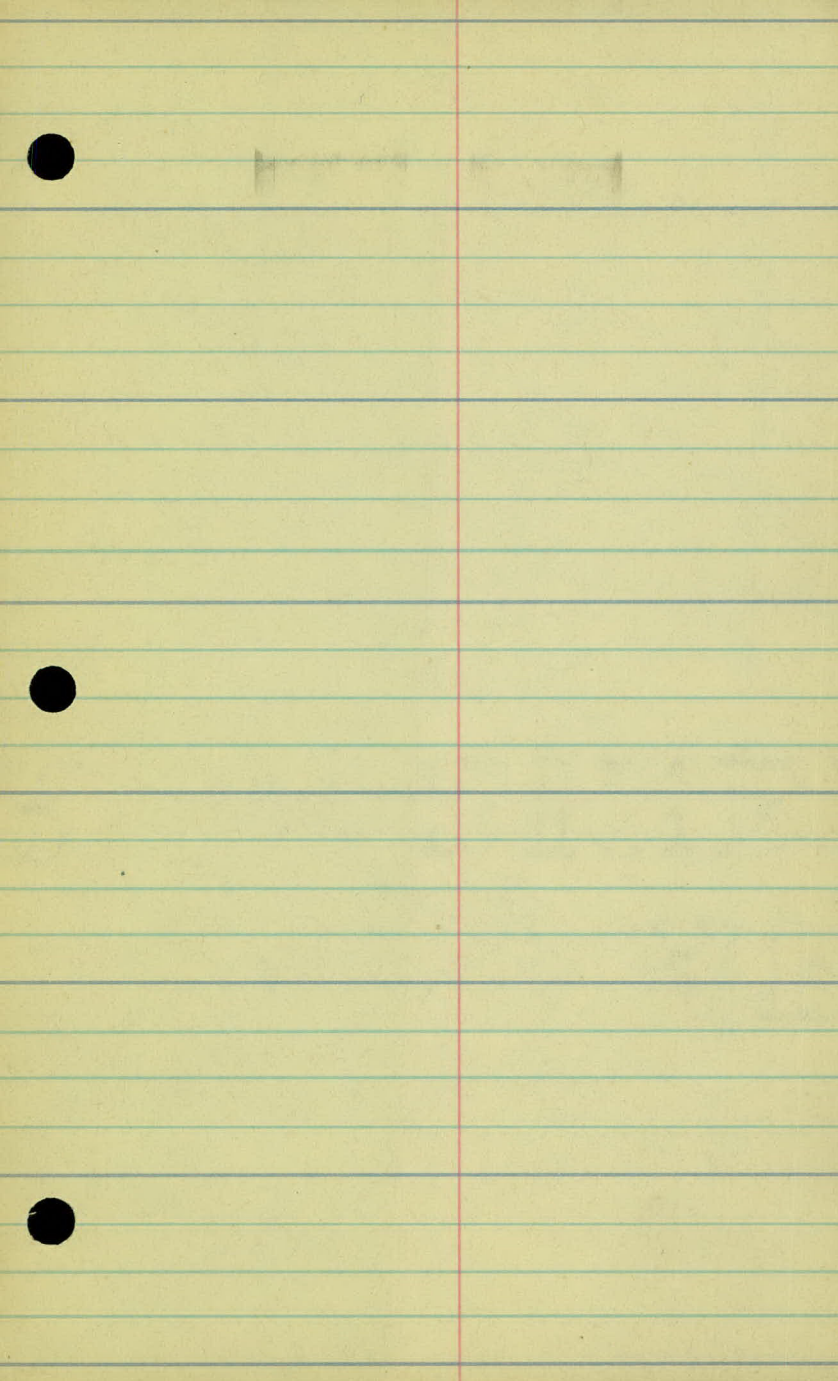


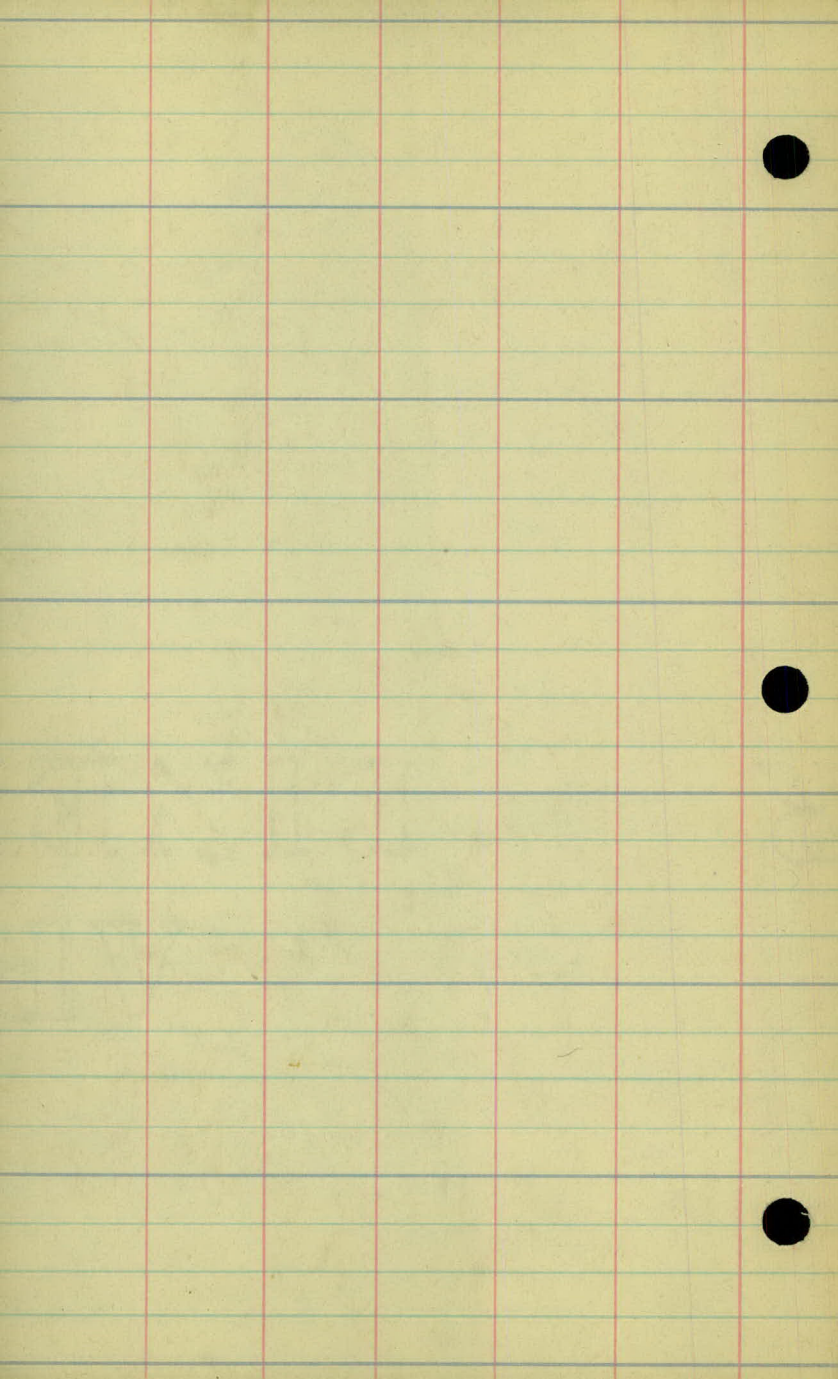


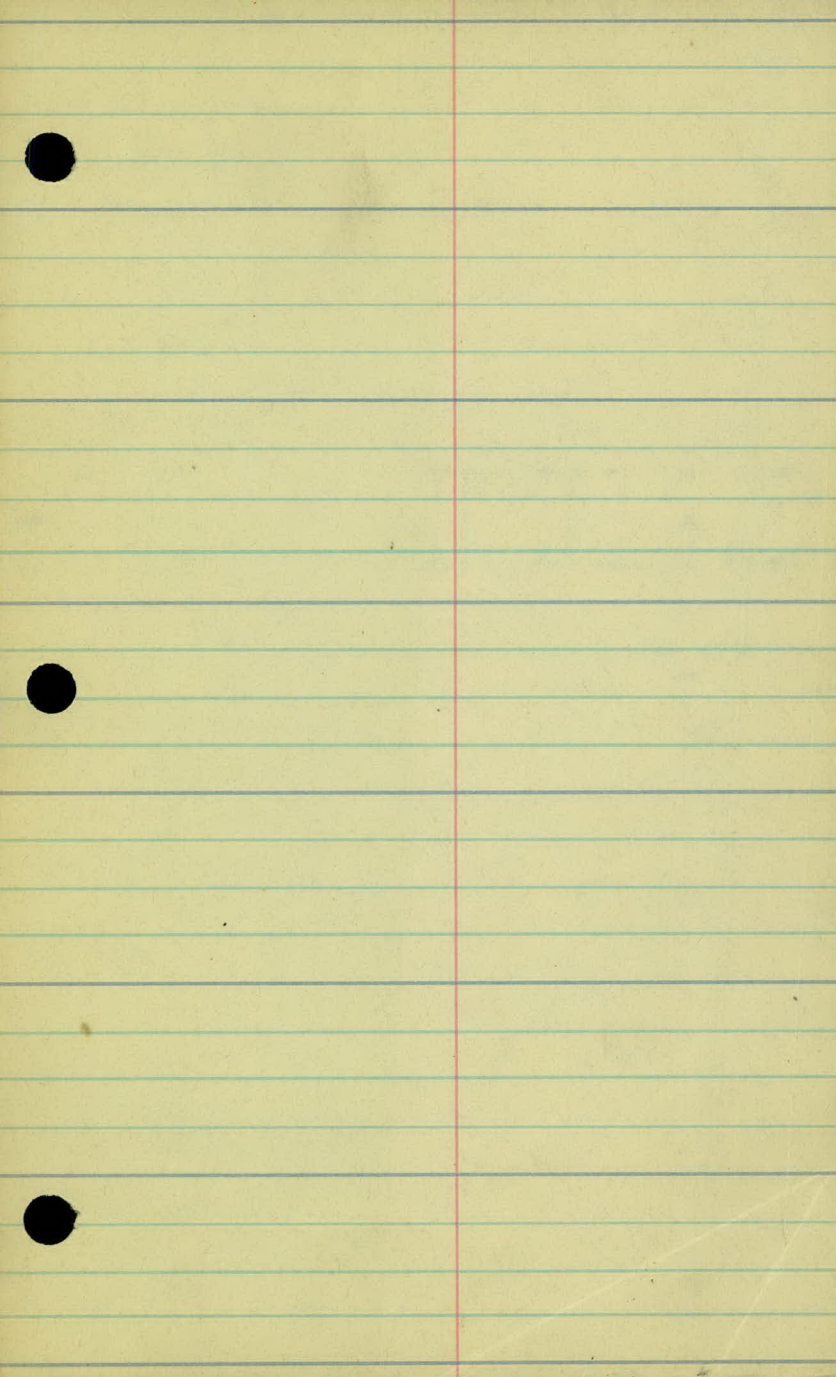


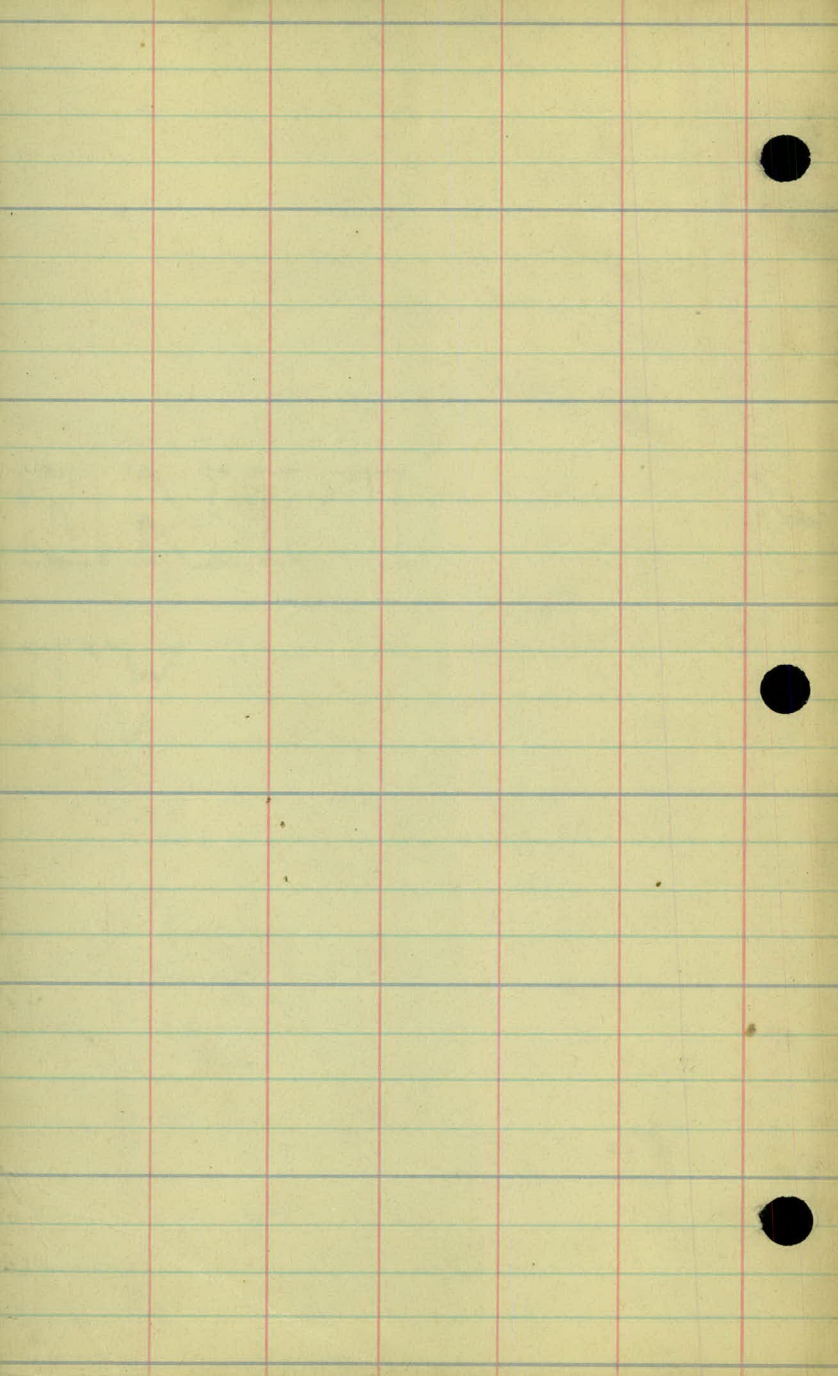












Dale St.
Larp. to 300' North

M.

6.30

918.93

0+00

± Larp

+50

1

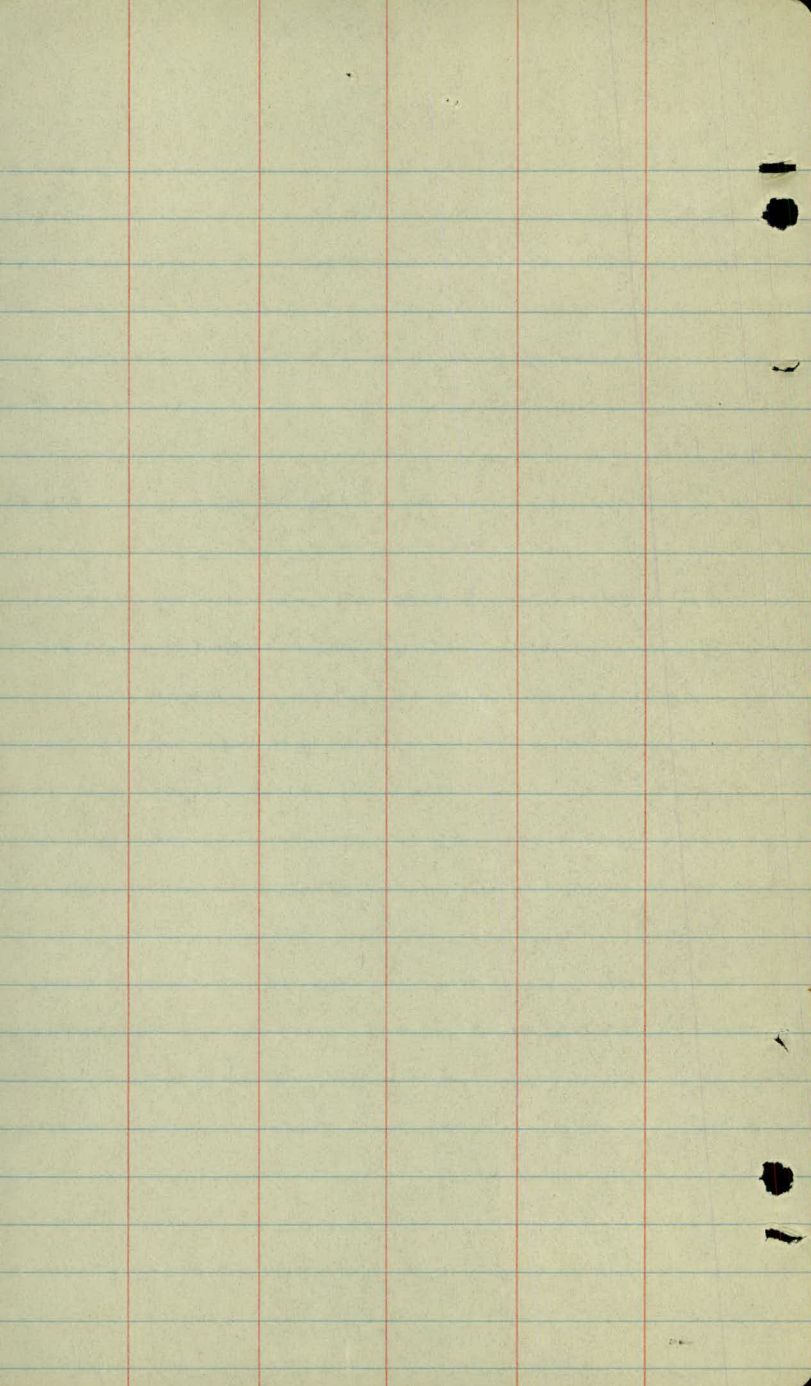
2

3

Note: 00 = 15' West of Larp. to Dale (P.I.)

Δ 112°42' Lt

Rd. 14 & 50



Base Line =
 & Travelled road

EC: Edgeford

Top Mont Dale & Larp

6.3

6.6 6.2 6.3 6.7 7.7 7.4 7.5
 50 13 59 17 23 26-29 31 69

EC: R

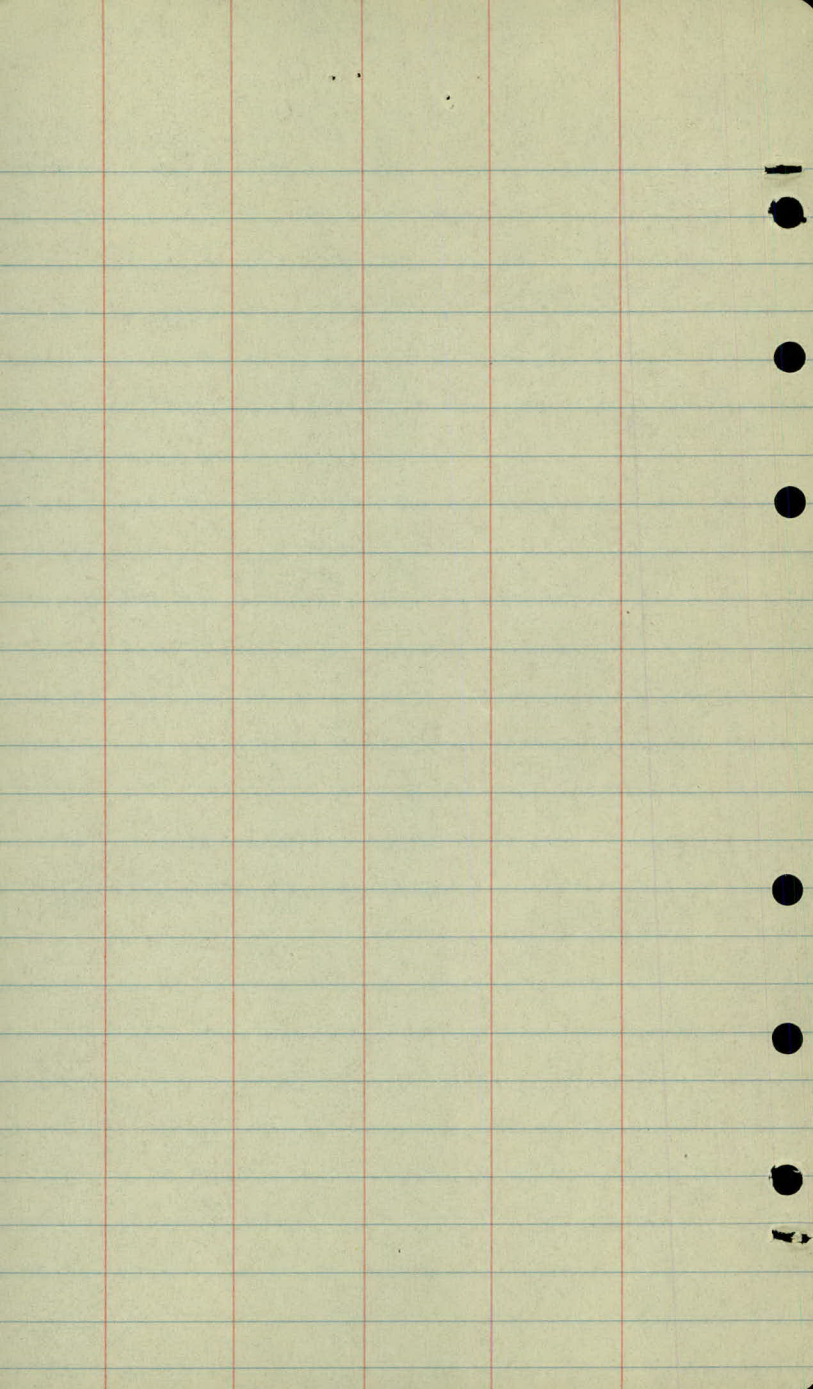
6.3 6.5 6.2 6.1 6.7 7.8 8.0 8.2
 50 18 12 5.7 10 20 23 54 92

EC:

5.9 5.3 6.7 5.4 5.3 5.0 6.2 5.7 6.4 5.8 6.0 6.9
 50 26 22-19 15 12 10 19 22-25 27 71 136

EC

4.9 4.4 5.8 4.7 4.5 4.1 4.6 5.9 4.5 5.5 5.4
 50 27 23-19 16 12 4.1 12-19 22-26 29 48 100



10/12/36

H.T. Porter

Slope Stakes

@

Temple of Aaron
Cemetery

28'

M.

5.49

924.42

918.93

50

+50

28 = Shoulder Width
 3:1 " Slope
 4' Wide Ditch
 1' Deep
 10:1 Fill Slopes + Back Slopes

Top Mont Data & Larp.

5.0 $\frac{22}{35}$ $\frac{2.2}{33}$ $\frac{6.5}{38.24}$ $\frac{4.5}{17}$ 4.0

5.2 $\frac{26.4}{33}$ $\frac{3.8}{33}$ $\frac{6.1}{28}$ $\frac{5.9}{21}$ $\frac{4.5}{17}$ 4.2

5.9 $\frac{28}{66.0}$ $\frac{2.8}{33}$ $\frac{6.7}{27.23}$ $\frac{5.2}{20}$ $\frac{5.3}{15}$ 4.8

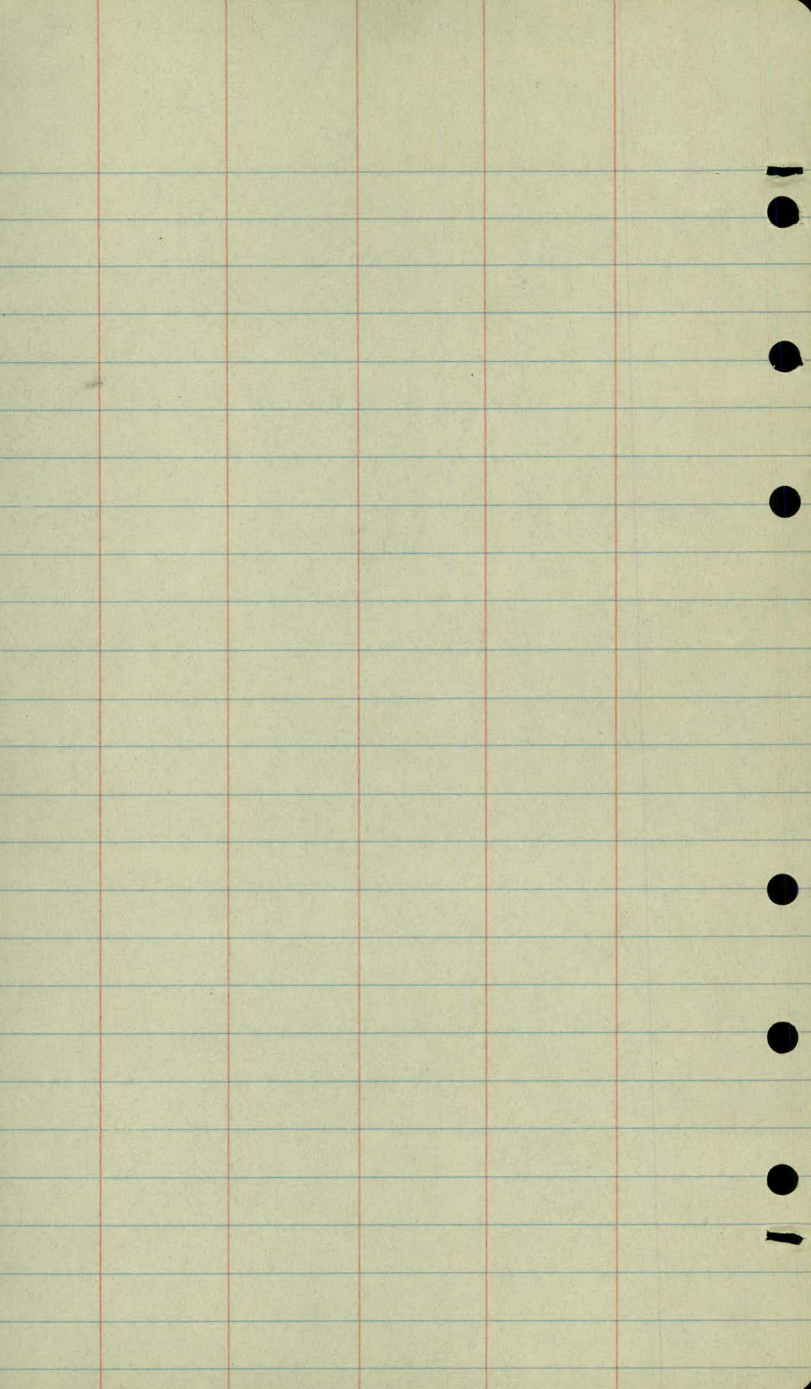
5.8 $\frac{26.7}{62.0}$ $\frac{3.1}{32}$ $\frac{3.7}{27.21}$ $\frac{6.8}{18}$ $\frac{5.4}{18}$ 4.8

5.9 $\frac{F1.2}{61}$ $\frac{6.3}{39}$ $\frac{7.3}{27}$ $\frac{5.4}{22}$ $\frac{5.4}{18}$ 4.9

5.1 $\frac{F2.7}{7.8}$ $\frac{8.2}{22}$ $\frac{5.4}{17}$ 5.1

4.8 $\frac{F3.4}{8.2}$ $\frac{7.8}{21}$ $\frac{5.4}{17}$ $\frac{5.2}{14}$ 4.8

4.9 $\frac{F1.7}{7.6}$ $\frac{6.8}{22}$ $\frac{5.3}{15}$ 4.9



Special X-Section

Larp. + Chatsworth

Sta 169 to 172

Sta + π -

BM 080 946.51

945.71

9+45

$$\begin{array}{r} \frac{+58 \text{ Tr}(4.2)}{27} \\ +86 \text{ Tr}(4.6) \\ \hline 37 \end{array} \quad \begin{array}{r} \frac{+45 \text{ Tr}(4.2) \text{ (Rod)}}{24} \end{array}$$

70

$$\begin{array}{r} \frac{+05 \text{ Tr}(5.1)}{36} \\ +16 \text{ Tr}(5.8) \\ \hline 27 \end{array} \quad \begin{array}{r} \frac{+06 \text{ Tr}(5.2)}{30} \end{array}$$

71

$$\begin{array}{r} \frac{+36 \text{ Tr}(6.9)}{37} \quad \frac{+37 \text{ Tr}(6.9)}{30} \end{array}$$

+75

Top Hyd 22' Rt. Sta. 169+22

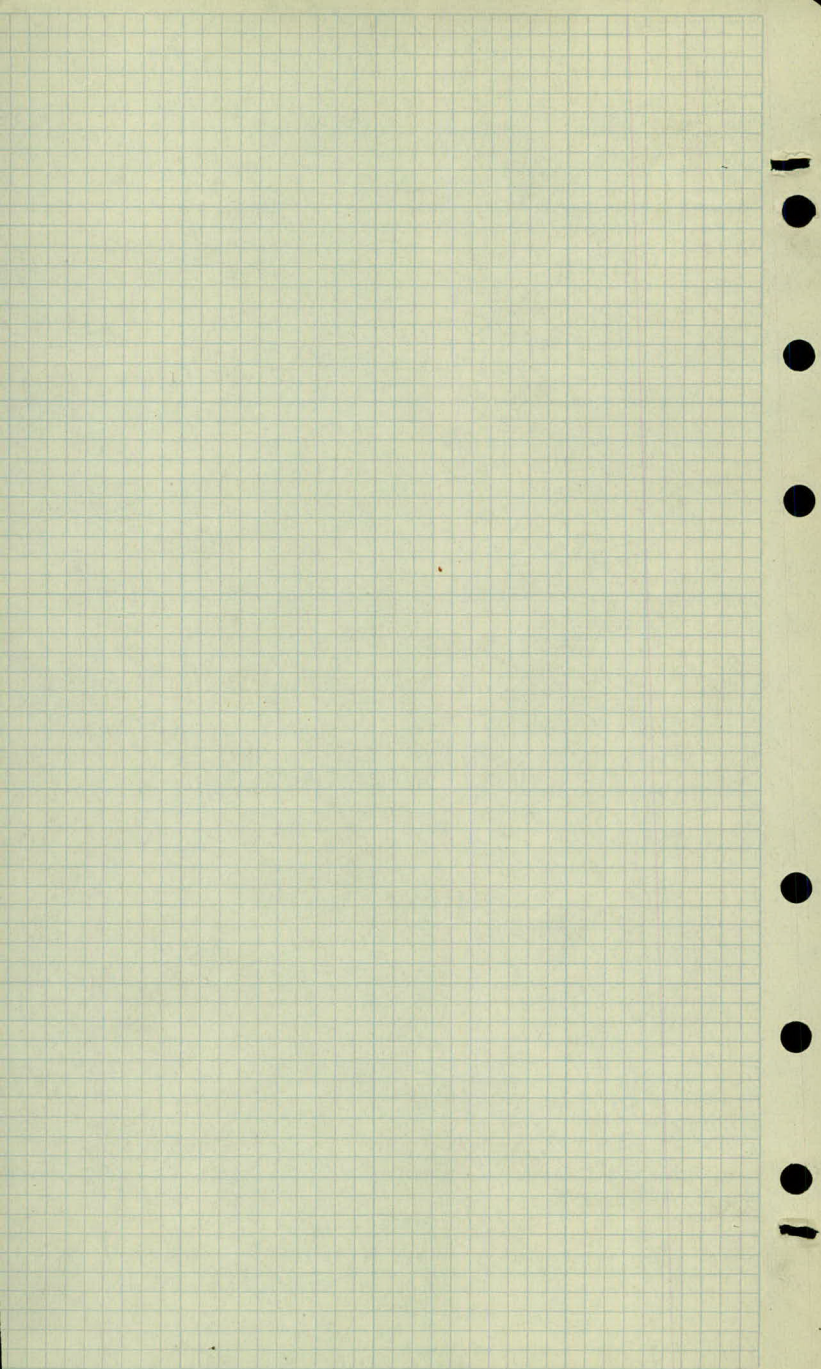
$$4.3 \frac{4.5}{10} \frac{4.5}{19} \frac{4.9}{20} \frac{4.0}{27} \frac{4.2}{38} \frac{4.7}{100}$$

Floor Ho, 2.16

$$4.6 \frac{4.8}{10} \frac{5.4}{17} \frac{5.7}{20} \frac{5.4}{24} \frac{5.1}{46} \frac{4.7}{84-100}$$

$$5.5 \frac{5.8}{10} \frac{6.2}{17} \frac{8.2}{22} \frac{7.7}{75} \frac{\text{Floor Ho}}{6.0}$$

$$6.3 \frac{6.5}{10} \frac{6.8}{19} \frac{7.0}{24} \frac{7.4}{100}$$



Original X-Sections
Larpy Dale St East

5.32 924.25

918.93

+00

± Date

+50

+70

± Gully 18" Conc X 40'

+92

00 Sec Rt.

+94

00 Sec Lt

M

5.32

28 1/2 Top.

10:1

Top Mont Dale - Larp

Taken on Rd (Dealest)

$\frac{4.3}{200}$ $\frac{4.8}{100}$ 5.3 $\frac{5.7}{100}$ $\frac{6.1}{200}$

$\frac{6.9}{200}$ $\frac{7.5}{100}$ $\frac{7.5}{60}$ $\frac{6.8}{22}$ $\frac{5.2}{16}$ 4.7 $\frac{5.0}{13}$ $\frac{6.4}{20}$ $\frac{6.6}{24}$ $\frac{5.6}{26}$ $\frac{5.7}{100}$ $\frac{6.9}{200}$

ER₁

$\frac{6.9}{200}$ $\frac{6.4}{108}$ $\frac{7.8}{95}$ $\frac{8.3}{83}$ $\frac{7.6}{21}$ $\frac{5.4}{17}$ $\frac{5.1}{19}$ 4.6 $\frac{5.1}{9}$ $\frac{5.2}{12}$ $\frac{7.6}{19}$ $\frac{6.7}{29}$ $\frac{7.1}{72}$ $\frac{6.5}{100}$ $\frac{7.9}{200}$

ER₂

FL₁

FL₂

$\frac{6.6}{162}$ $\frac{7.8}{100}$ $\frac{8.2}{52}$ $\frac{8.0}{22}$ $\frac{8.1}{23}$ $\frac{5.2}{14}$ $\frac{5.2}{14}$ 4.9 $\frac{5.3}{9}$ $\frac{8.6}{12}$ $\frac{9.1}{18}$ $\frac{8.4}{18}$ $\frac{7.5}{28}$ $\frac{8.8}{35}$ $\frac{9.0}{88}$ $\frac{9.0}{200}$

ER₁

$\frac{5.9}{160}$ $\frac{7.2}{100}$ $\frac{8.2}{35}$ $\frac{8.0}{22}$ $\frac{5.6}{18}$ $\frac{5.3}{14}$ 5.0 $\frac{5.4}{8}$ $\frac{8.8}{13}$ $\frac{7.5}{19}$ $\frac{7.8}{33}$ $\frac{9.3}{79}$ $\frac{9.3}{100}$ $\frac{9.5}{200}$

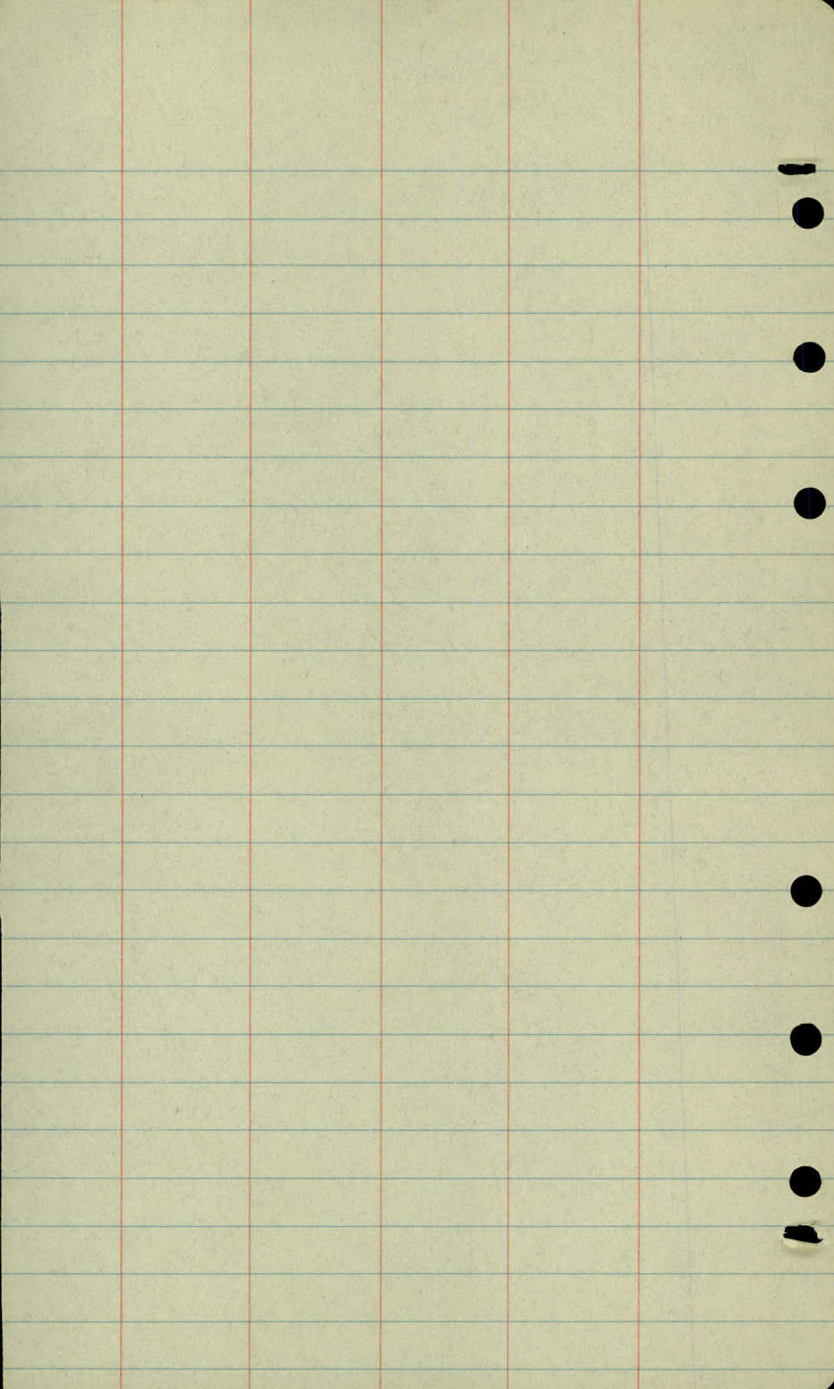
ER₂

$\frac{3.7}{156}$ $\frac{4.7}{100}$ $\frac{5.6}{30}$ $\frac{7.2}{27}$ $\frac{5.3}{18}$ $\frac{5.2}{15}$ 4.7

Bottom @ Ground Line

Top Mont Dale - Larp

Cemetery East Posts 7.00



For Carley

Prelim. X-sec. along Carpenter Av.
thru Roselawn Cemetery.

Sta. + π - Elev.

6.86 926.87 920.01

T.P. 12.59 939.29 0.17 926.70

+50

77

+50

178

+50

179

T.P. 1.43 927.17 13.55 925.74

+50

180

+50

181

T.P. 6.67 928.29 5.55 921.64

+50

Lt.

L

Top Monument Sta. 184+47.9

$$\begin{array}{r} 5.3 \\ 100 \end{array} \quad \begin{array}{r} 4.9 \\ 35 \end{array} \quad \begin{array}{r} 5.2 \\ 10 \end{array} \quad \begin{array}{r} 4.9 \\ \hline \end{array}$$

$$\begin{array}{r} 6.2 \\ 100 \end{array} \quad \begin{array}{r} 5.1 \\ 48 \end{array} \quad \begin{array}{r} 5.2 \\ 34 \end{array} \quad \begin{array}{r} 7.3 \\ 24 \end{array} \quad \begin{array}{r} 7.3 \\ 20 \end{array} \quad \begin{array}{r} 6.4 \\ 15 \end{array} \quad \begin{array}{r} 6.5 \\ 10 \end{array} \quad \begin{array}{r} 6.2 \\ \hline \end{array}$$

$$\begin{array}{r} 6.6 \\ 100 \end{array} \quad \begin{array}{r} 4.7 \\ 45 \end{array} \quad \begin{array}{r} 4.7 \\ 34 \end{array} \quad \begin{array}{r} 9.1 \\ 24 \end{array} \quad \begin{array}{r} 9.2 \\ 19 \end{array} \quad \begin{array}{r} 8.4 \\ 15 \end{array} \quad \begin{array}{r} 8.2 \\ 10 \end{array} \quad \begin{array}{r} 8.4 \\ \hline \end{array}$$

$$\begin{array}{r} 7.8 \\ 100 \end{array} \quad \begin{array}{r} 6.4 \\ 48 \end{array} \quad \begin{array}{r} 6.4 \\ 33 \end{array} \quad \begin{array}{r} 11.0 \\ 24 \end{array} \quad \begin{array}{r} 11.0 \\ 19 \end{array} \quad \begin{array}{r} 10.3 \\ 15 \end{array} \quad \begin{array}{r} 10.2 \\ 10 \end{array} \quad \begin{array}{r} 10.0 \\ \hline \end{array}$$

$$\begin{array}{r} 9.8 \\ 100 \end{array} \quad \begin{array}{r} 9.1 \\ 45 \end{array} \quad \begin{array}{r} 9.4 \\ 34 \end{array} \quad \begin{array}{r} 13.2 \\ 25 \end{array} \quad \begin{array}{r} 13.3 \\ 20 \end{array} \quad \begin{array}{r} 12.3 \\ 16 \end{array} \quad \begin{array}{r} 12.2 \\ 10 \end{array} \quad \begin{array}{r} 11.9 \\ \hline \end{array}$$

$$\begin{array}{r} 12.4 \\ 100 \end{array} \quad \begin{array}{r} 11.9 \\ 69 \end{array} \quad \begin{array}{r} 11.4 \\ 49 \end{array} \quad \begin{array}{r} 11.3 \\ 34 \end{array} \quad \begin{array}{r} 14.7 \\ 25 \end{array} \quad \begin{array}{r} 14.8 \\ 20 \end{array} \quad \begin{array}{r} 14.1 \\ 16 \end{array} \quad \begin{array}{r} 13.9 \\ 10 \end{array} \quad \begin{array}{r} 13.7 \\ \hline \end{array}$$

$$\begin{array}{r} 4.2 \\ 100 \end{array} \quad \begin{array}{r} 4.0 \\ 58 \end{array} \quad \begin{array}{r} 3.8 \\ 46 \end{array} \quad \begin{array}{r} 3.1 \\ 32 \end{array} \quad \begin{array}{r} 4.2 \\ 23 \end{array} \quad \begin{array}{r} 4.2 \\ 19 \end{array} \quad \begin{array}{r} 3.3 \\ 15 \end{array} \quad \begin{array}{r} 3.3 \\ 10 \end{array} \quad \begin{array}{r} 3.1 \\ \hline \end{array}$$

$$\begin{array}{r} 5.5 \\ 100 \end{array} \quad \begin{array}{r} 5.9 \\ 25 \end{array} \quad \begin{array}{r} 5.6 \\ 34 \end{array} \quad \begin{array}{r} 4.9 \\ 32 \end{array} \quad \begin{array}{r} 5.3 \\ 24 \end{array} \quad \begin{array}{r} 5.3 \\ 19 \end{array} \quad \begin{array}{r} 4.4 \\ 15 \end{array} \quad \begin{array}{r} 4.4 \\ 10 \end{array} \quad \begin{array}{r} 4.2 \\ \hline \end{array}$$

$$\begin{array}{r} 4.5 \\ 100 \end{array} \quad \begin{array}{r} 5.4 \\ 73 \end{array} \quad \begin{array}{r} 5.9 \\ 33 \end{array} \quad \begin{array}{r} 6.0 \\ 19 \end{array} \quad \begin{array}{r} 5.2 \\ 15 \end{array} \quad \begin{array}{r} 5.1 \\ 10 \end{array} \quad \begin{array}{r} 4.9 \\ \hline \end{array}$$

$$\begin{array}{r} 1.4 \\ 100 \end{array} \quad \begin{array}{r} 2.3 \\ 46 \end{array} \quad \begin{array}{r} 2.6 \\ 34 \end{array} \quad \begin{array}{r} 6.2 \\ 24 \end{array} \quad \begin{array}{r} 6.3 \\ 20 \end{array} \quad \begin{array}{r} 5.3 \\ 15 \end{array} \quad \begin{array}{r} 5.3 \\ 10 \end{array} \quad \begin{array}{r} 5.1 \\ \hline \end{array}$$

$$\begin{array}{r} 4.0 \\ 100 \end{array} \quad \begin{array}{r} 10.8 \\ 79 \end{array} \quad \begin{array}{r} 0.8 \\ 48 \end{array} \quad \begin{array}{r} 0.8 \\ 34 \end{array} \quad \begin{array}{r} 7.6 \\ 21 \end{array} \quad \begin{array}{r} 7.6 \\ 19 \end{array} \quad \begin{array}{r} 6.7 \\ 15 \end{array} \quad \begin{array}{r} 6.7 \\ 10 \end{array} \quad \begin{array}{r} 6.4 \\ \hline \end{array}$$

Large Trees

Elev. at base.

$$177+82-5.5 \text{ out } 40'$$

$$178+29-40' \text{ Lt. } 8'$$

$$178+74-39' \text{ Lt. } 1'$$

$$179+10-39' \text{ Lt. } 1'$$

$$179+64-38' \text{ Lt.}$$

$$180+07-35' \text{ Lt.}$$

$$180+20-30' \text{ Lt.}$$

Sta. + π - Elev.

182 928.29

+50

183

+50

184

+25

+48

185

+41

+43

186

+40

4.

2

Trees.

$$\begin{array}{r} +0.7 \quad 0.3 \quad 0.3 \quad 0.8 \quad 1.9 \quad 2.7 \quad 7.5 \quad 6.6 \quad 6.7 \quad 6.5 \\ \hline 100 \quad 68 \quad 47 \quad 46 \quad 33 \quad 23 \quad 19 \quad 15 \quad 10 \quad \hline \end{array} \quad 182+37-38'41. \quad 2$$

$$\begin{array}{r} +0.5 \quad 0.8 \quad 2.3 \quad 3.3 \quad 5.6 \quad 7.6 \quad 7.6 \quad 6.7 \quad 6.8 \quad 6.7 \\ \hline 100 \quad 73 \quad 47 \quad 46 \quad 33 \quad 25 \quad 20 \quad 16 \quad 10 \quad \hline \end{array} \quad 187+85-38'41.$$

$$\begin{array}{r} +0.5 \quad 2.1 \quad 3.6 \quad 4.5 \quad 5.1 \quad 7.8 \quad 8.0 \quad 7.1 \quad 7.0 \quad 6.8 \\ \hline 100 \quad 77 \quad 47 \quad 45 \quad 32 \quad 24 \quad 19 \quad 15 \quad 10 \quad \hline \end{array}$$

183+45-38'41.

$$\begin{array}{r} +1.5 \quad 0.1 \quad 2.3 \quad 3.4 \quad 4.3 \quad 4.7 \quad 8.2 \quad 8.5 \quad 7.4 \quad 2.4 \quad 7.2 \\ \hline 100 \quad 81 \quad 67 \quad 46 \quad 45 \quad 34 \quad 23 \quad 19 \quad 15 \quad 10 \quad \hline \end{array}$$

$$\begin{array}{r} +2.1 \quad 0.6 \quad 2.6 \quad 3.0 \quad 4.6 \quad 5.0 \quad 5.0 \quad 7.9 \quad 8.0 \quad 7.8 \\ \hline 100 \quad 70 \quad 48 \quad 47 \quad 34 \quad 23 \quad 19 \quad 15 \quad 10 \quad \hline \end{array} \quad 184+11-38'41.$$

$$\begin{array}{r} +3.3 \quad 0.0 \quad 1.6 \quad 3.0 \quad 4.2 \quad 5.5 \quad 9.3 \quad 9.4 \quad 8.4 \quad 8.3 \quad 8.1 \\ \hline 100 \quad 76 \quad 65 \quad 52 \quad 45 \quad 35 \quad 23 \quad 19 \quad 15 \quad 10 \quad \hline \end{array}$$

$$\begin{array}{r} 7.3 \quad 7.2 \quad 7.4 \quad 7.5 \quad 8.6 \quad 9.7 \quad 8.6 \quad 8.6 \quad 8.3 \\ \hline 100 \quad 65 \quad 46 \quad 33 \quad 24 \quad 19 \quad 15 \quad 10 \quad \hline \end{array}$$

184+87-38'41.

$$\begin{array}{r} 8.8 \quad 8.8 \quad 8.8 \quad 10.5 \quad 10.7 \quad 9.3 \quad 9.2 \quad 9.0 \\ \hline 100 \quad 45 \quad 33 \quad 24 \quad 19 \quad 15 \quad 10 \quad \hline \end{array}$$

$$\begin{array}{r} 9.4 \quad 9.4 \quad 9.5 \quad 11.3 \quad 11.7 \quad 9.6 \quad 9.7 \quad 9.5 \\ \hline 100 \quad 33 \quad 27 \quad 22 \quad 20 \quad 16 \quad 10 \quad \hline \end{array}$$

$$\begin{array}{r} 9.4 \quad 9.4 \quad 9.4 \quad 9.8 \quad 9.7 \quad 9.5 \\ \hline 100 \quad 34 \quad 26 \quad 21 \quad 10 \quad \hline \end{array}$$

$$\begin{array}{r} 9.4 \quad 9.4 \quad 10.2 \quad 10.4 \quad 10.2 \\ \hline 100 \quad 54 \quad 14 \quad 10 \quad \hline \end{array}$$

(Entrance)

$$\begin{array}{r} 9.4 \quad 10.6 \quad 10.7 \quad 10.6 \\ \hline 100 \quad 20 \quad 10 \quad \hline \end{array}$$

Sta. + ∇ - Elev.
187 928.29

+41

+44

T.P. 4.50 920.34 12.45 915.84

188

+50

189

+50

190

+50

191

B.M. 0.29 920.05 (920.01)

4.

2

$\frac{10.0}{100}$ $\frac{10.0}{33}$ $\frac{11.3}{14}$ $\frac{11.6}{10}$ $\frac{11.4}{1}$

Large
Toos
Elev. at base

$\frac{10.2}{100}$ $\frac{10.6}{30}$ $\frac{11.8}{18}$ $\frac{12.0}{10}$ $\frac{11.8}{1}$

$\frac{10.2}{100}$ $\frac{11.1}{29}$ $\frac{13.9}{22}$ $\frac{11.9}{16}$ $\frac{12.0}{10}$ $\frac{11.8}{1}$

187+60-39' Lt.

$\frac{3.8}{100}$ $\frac{4.1}{45}$ $\frac{5.3}{27}$ $\frac{5.6}{20}$ $\frac{4.6}{15}$ $\frac{4.5}{10}$ $\frac{4.3}{1}$

188+27-37' Lt.

$\frac{4.9}{100}$ $\frac{5.2}{80}$ $\frac{5.2}{46}$ $\frac{5.0}{32}$ $\frac{5.7}{34}$ $\frac{5.6}{19}$ $\frac{4.7}{15}$ $\frac{4.7}{10}$ $\frac{4.6}{1}$

188+25-37' Lt.

$\frac{3.2}{100}$ $\frac{4.1}{68}$ $\frac{4.4}{43}$ $\frac{4.9}{31}$ $\frac{5.8}{26}$ $\frac{5.8}{20}$ $\frac{4.8}{15}$ $\frac{4.9}{10}$ $\frac{4.7}{1}$

189+44-43' Lt.

$\frac{1.4}{100}$ $\frac{2.4}{77}$ $\frac{3.5}{33}$ $\frac{6.7}{24}$ $\frac{6.1}{21}$ $\frac{4.9}{15}$ $\frac{4.9}{10}$ $\frac{4.7}{1}$

189+96-38' Lt.

$\frac{6.0}{100}$ $\frac{4.6}{84}$ $\frac{3.8}{66}$ $\frac{2.7}{33}$ $\frac{6.5}{23}$ $\frac{6.4}{21}$ $\frac{4.8}{15}$ $\frac{4.8}{10}$ $\frac{4.6}{1}$

190+10-35' Lt.

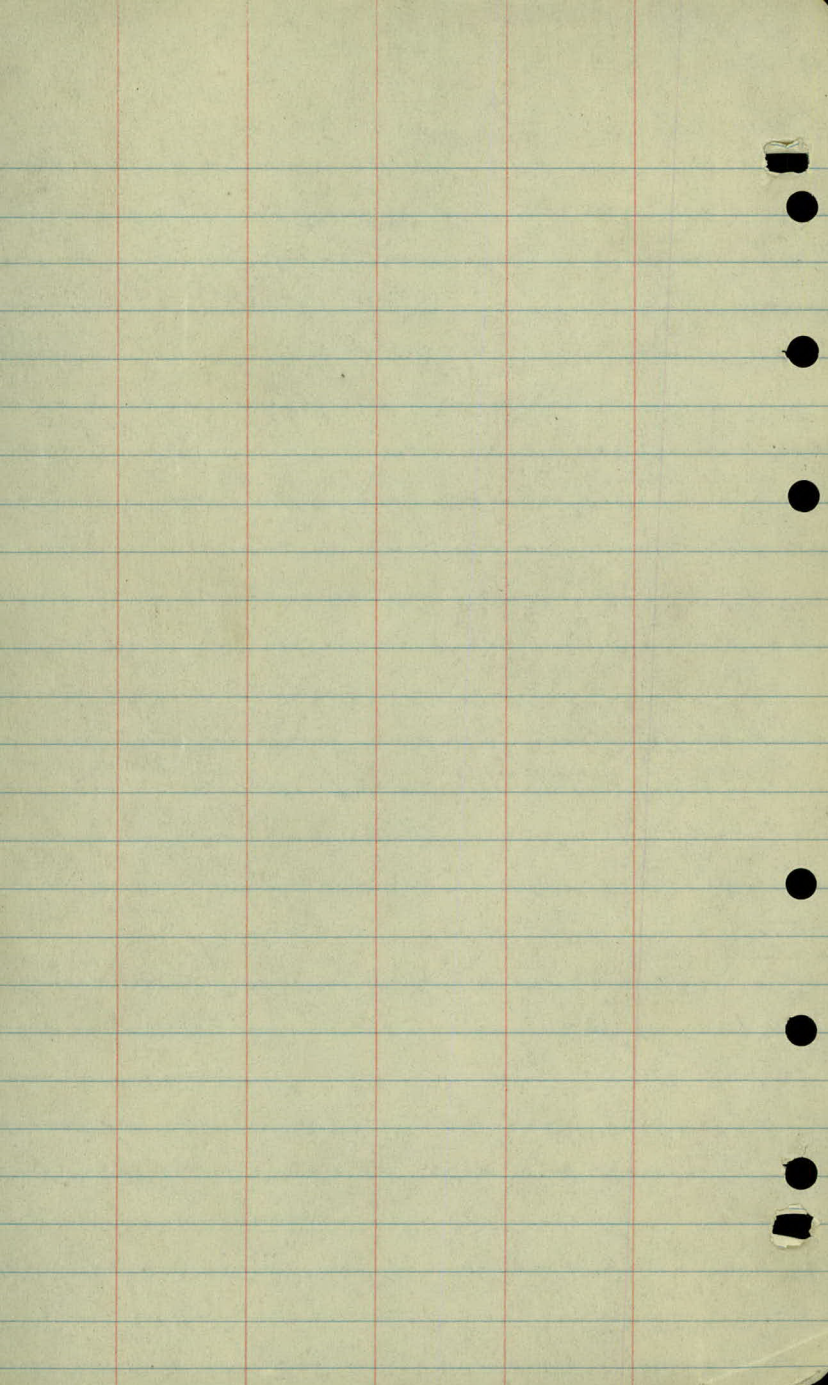
$\frac{8.6}{100}$ $\frac{7.8}{66}$ $\frac{6.8}{50}$ $\frac{5.9}{36}$ $\frac{6.5}{23}$ $\frac{6.5}{19}$ $\frac{4.6}{15}$ $\frac{4.6}{10}$ $\frac{4.4}{1}$

190+48-40' Lt.

$\frac{8.4}{100}$ $\frac{8.4}{59}$ $\frac{7.0}{26}$ $\frac{4.4}{16}$ $\frac{4.4}{10}$ $\frac{4.2}{1}$

190+82-35' Lt.

Top Monument 515. 184+47.9



West Carpenter Ave.

Existing and Required
Culverts between West Co.
Line & Wheelock Parkway.
4/37

Location.	Road or Side Culvert.	Existing Culverts.	
N.W. Cor. Dole + Larpenleur	S		
209+43	R	15" x 66' C.M.	
206+90 Lt.	S		
204+30 Rt.	S		
202+11 Lt.	S		
201+00 Lt.	S		
199+10 Lt.	S		
197+00 Rt.	S		
191+44	R	15" x 40' C.M.	# 50-34
187+00 Lt.	S	15" x 79' C.M.	} Rosebawn Cemetery
186+44 Lt.	S	15" x 34' C.M.	
185+85 Lt.	S.	15" x 84' C.M.	
181+00	R	12" x 48" x -	Conc. Box
180+54	R	12" x 96" V.T.P.	
180+75 Rt.	S.	Quincy St.	
178+30 Rt.	S.		
176+90 Rt.	S.		
171+20	R	{ 18" x 48' C.M. 12" x 14' Conc. Pipe	
170+40 Rt.	S.		
170+00 Rt.	S.		
169+30 Rt.	S.		

Required Culverts

100 Lin. Ft. Spiral Dredge pipe to connect to
culvert @ N.W. Cor. intersection

North end buried connect to proposed spiral
dredge pipe above

15" x 20' C.M.

15" x 20' C.M.

15" x 22' C.M.

15" x 20' C.M.

15" x 20' C.M.

15" x 24' C.M.

15" x 6' Extension on Rt.

Must be completed as per plans on Rt.

12" x 48' C.M. to connect to 17" V.T.P. above.

15" x 18' C.M.

15" x 20' C.M.

18" x 6' C.M. extension on Rt.

15" x 20' C.M.

15" x 8' C.M. under walk

9" x 22' C.M. (pipe at site)

Location	Road or Side Culvert	Existing Culvert
169+10 Lt.	S.	
168+40 Rt.	S.	
168+07 Rt.	S.	12" x 8' C.M.
164+60 Lt.	S.	
167+90 Lt.	S.	
161+67	R.	15" x 45' C.M.
160+44 Rt.	S.	
156+90 Rt.	S.	
157+00 Rt.	S.	
150+00 Lt.	S.	24" x 48' Conc. Pipe
146+00 Lt.	S.	15" x 22' C.M.
145+40 Rt.	S.	24" x 81' C.M.
136+10 Rt.	S.	
135+20 Rt.	S.	
134+10 Lt.	S.	24" x 102' C.M.
131+75	R.	
130+25 Lt.	S.	15" x 20' C.M.
128+10 Lt.	S.	15" x 20' C.M.
127+50 Lt.	S.	15" x 40' C.M.
125+40 Lt.	S.	{ 15" x 30' C.M. 18" x 36' C.M.
125+35 Rt.	S.	
123+20 Lt.	S.	18" x 30' C.M.
122+00 Lt.	S.	18" x 40' Conc. Pipe
118+80 Lt.	S.	
112+25 Lt.	S.	24" x 50' C.M.

Required Culverts.

1304 60
10

9" x 40' C.M. (Rect no head room)

15" x 20' C.M.

15" x 20' C.M.

15" x 40' C.M.

15" x 16' Ext. (8' each end.)

15" x 20' C.M.

12" x 8' C.M. (Walk)

15" x 40' C.M.

Fernwood Ave (Open up West End & Ditch)

15" x 20' C.M.

15" x 20' C.M. (Also Ditch)

Hamm line Ave.

18" x 54' C.M.

Albert St. (Lower this Culvert)

Holton Ave

24" x 24' C.M.

Parcel St.

Reena Ave.

Location	Road or Side	Culvert	Existing Culvert.
114 90		R	24" x 48" x - Conc. Box
108+70 Lt.	}	S	
Hawking Golf. Lt.			
101+60 Rt.		S	
99+85 Rt.		S	
98+50 Lt.		S	15" x 20' C.M.
96+77 Lt.		S	15" x 20' C.M.
96+57		R	30" x 48" x 42' Conc. Box
94+70 Lt.		S	12" x 20' C.M.
94+25 Lt.		S	8' x 12' Plank Xing
93+31		R	30" x 48" x 42' Conc. Box
90+00 Rt.		S	15" x 22' Conc. Pipe
88+55 Rt.		S	15" x 20' C.M.
87+16 Rt.		S	15" x 20' C.M.
85+37 Rt.		S	15" x 20' C.M.
84+34 Rt.		S	15" x 20' C.M.
81+90 Rt.		S	15" x 20' C.M.
81+35		R	24" x 48" x 42' Conc. Box
79+70 Rt.		S	15" x 20' C.M.
79+10 Lt.		S	15" x 66' Conc. Pipe
76+50 Lt.		S	14" x 20' C.M.
75+86 Rt.		S	15" x 20' Conc.
74+04 Lt.		S	12" x 20' C.M.
74+95 Lt.		S	12" x 20' C.M.
72+26 Lt.		S	12" x 20' C.M.

Required Culvert.

Under Construction

15" x 20' C.M.

15" x 28' C.M.

15" x 20'

15" x 22'

Remove & place 15" x 20' C.M. or Pitch to Conc. Box

New Brighton Rd.

Location	Road or Side Culvert	Existing Culverts.
70+88 Lt.	S.	
69+09 Lt.	S.	12" x 20' C.M.
68+50 Lt.	S.	
64+59 Lt.	S.	
67+36 Lt.	S.	12" x 20' C.M.
59+94 Lt.	S.	
59+51	R	24" x 48" x 4' Conc. Box
217+47	R	24" x 40' Conc. pipe
215+38 Rt.	S	15" x 24' C.M.
217+17 Rt.	S.	15" x 24' C.M.
223+90 Rt.	S.	15" x 40' C.M.
225+75 Lt.	S.	{ 12" x 50' C.M. 17" x 42" x 16' Wood Box
226+00 Rt.	S.	{ 12" x 24' C.M. 12" x 42" x 22' Wood Box 3' x 122' Flume of $\frac{3}{4}$ C.M.
228+40 Rt.	S	18" x 24' C.M.
230+44	R	30" x 84' C.M.
231+76	R.	30" x 62' Conc. Pipe
231+96 Rt.	surface Drain	12" x 14' C.M.
232+00 Lt.	S	12" x 12' C.M.
234+00 Rt.	S	30" x 34' C.M.

Required Culverts.

15" x 24' C.M.

15" x 20' C.M.

15" x 36' C.M.

15" x 20' C.M.

24" x 16' Extension

Location	Road or Side Culvert.	Existing Culverts
54+45 Rt.	S.	12" x 20' C.M.
54+04	R	24" x 48" x Conc. Box
51+85 Rt.	S.	12" x 9' C.M.
49+50 Rt.	S.	15" x 20' C.M.
49+30 Lt.	S.	12" x 12' C.M.
48+33 Lt.	S.	12" x 20' C.M.
47+70 Rt.	S.	
47+00 Rt.	S.	
46+25 Rt.	S.	12" x 8' C.M.
45+52 Lt.	S.	12" x 20' C.M.
45+39 Rt.	S.	12" x 8' C.M.
44+64 Rt.	S.	12" x 22' Conc. Pipe.
40+14	R	
35+74 Lt.	S.	
34+89	R	15" x 58' Conc. Pipe.
31+93 Lt.	S.	12" x 38' C.M.
28+39 Lt.	S.	12" x 7' Conc.
26+50 Lt.	S.	24" x 54' Conc.
15+42 Rt.	S.	
10+30	R.	12" x 40' C.M.
6+67 Lt.	S.	18" x 42' C.M.
5+80	R	

Required Culverts.

Lower to meet new box grade,
Under Construction &

15" x 32' C.M.

15" x 20' C.M.

24" Pipe Culvert under construction

15" x 20' C.M.

12" x 20' C.M.

Clean out & extend 20'

18" x 67' C.M.

