

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

COUNTY ROAD "C"

From OXFORD To DALE

Road Acc't. No. 23

Date Filed 12-3-74

Dr. 9

File BK 76

LT

E

August 20, 1970

RT

X-4

4.5	8.5	12.0	12.3	12.4	12.2	11.6	6.9	3.2
14.8	10.8	7.3	7.0	6.9	7.1	7.7	12.4	16.1
<u>63</u>	<u>50</u>	<u>39</u>	<u>24</u>		<u>24</u>	<u>43</u>	<u>53</u>	<u>62</u>

6.9	10.5	14.2	14.7	14.7	14.5	14.6	10.9	06.2	6.5
10.4	8.8	5.1	4.6	4.6	4.8	4.9	8.4	11.1	12.8
<u>66</u>	<u>56</u>	<u>43</u>	<u>29</u>		<u>27</u>	<u>45</u>	<u>55</u>	<u>60</u>	<u>63</u>

12.3	12.5	13.5	15.9	15.4	15.9	15.7	15.5	13.5	10.6	06.1	06.2
70	6.8	5.8	3.4	3.5	3.4	3.6	3.8	5.8	8.7	11.2	13.1
<u>75</u>	<u>63</u>	<u>52</u>	<u>39</u>	<u>23</u>		<u>23</u>	<u>43</u>	<u>49</u>	<u>56</u>	<u>60</u>	<u>64</u>

16.7	15.4	15.0	17.0	16.4	17.2	17.1	16.7	09.9	03.9
2.6	3.5	4.3	2.3	2.5	2.1	2.2	2.6	9.4	15.4
<u>82</u>	<u>69</u>	<u>56</u>	<u>39</u>	<u>21</u>		<u>24</u>	<u>44</u>	<u>58</u>	<u>70</u>

16.6	17.3	16.3	16.4	16.2	16.2	12.9	09.2	06.7
0.7	2.0	1.0	0.9	1.1	1.1	6.5	10.1	12.6
<u>81</u>	<u>54</u>	<u>24</u>		<u>30</u>	<u>43</u>	<u>54</u>	<u>62</u>	<u>70</u>

20.2	19.1	19.0	19.6	19.5	19.3	18.9	13.4	10.9
8.4	9.5	9.6	9.0	9.1	9.3	9.7	15.2	17.7
<u>79</u>	<u>59</u>	<u>42</u>	<u>23</u>		<u>28</u>	<u>44</u>	<u>56</u>	<u>71</u>

STA + π - Elev.

928.63

+75

66

+25

+50

✓

BM

0.64

927.99

927.96 ✓

LT

E

August 20, 1970

RT x5

21.1	20.0	21.0	20.9	20.6	20.4	15.5	14.6
<u>7.5</u>	<u>8.6</u>	<u>7.6</u>	<u>7.7</u>	<u>8.0</u>	<u>8.2</u>	<u>13.1</u>	<u>13.8</u>
70	47	26		23	38	55	74

23.8	22.1	22.9	22.0	21.7	22.2	16.7	15.4
<u>4.8</u>	<u>6.5</u>	<u>5.7</u>	<u>6.6</u>	<u>6.9</u>	<u>6.4</u>	<u>11.9</u>	<u>13.2</u>
82	57	30		22	36	45	69

24.7	24.0	24.3	23.2	23.1	21.2	18.6	17.7	16.1
<u>3.9</u>	<u>4.6</u>	<u>4.3</u>	<u>5.4</u>	<u>5.5</u>	<u>7.4</u>	<u>10.1</u>	<u>10.9</u>	<u>12.5</u>
82	62	30		24	31	46	58	68

23.3	20.1	25.3	24.6	24.4	22.6	22.0	25.5	25.7	26.4
<u>5.3</u>	<u>3.5</u>	<u>3.3</u>	<u>4.0</u>	<u>4.2</u>	<u>6.0</u>	<u>6.6</u>	<u>2.98</u>	<u>2.96</u>	<u>2.19</u>
71	54	30		8	14	23	28	27	27

conc conc

5
24.3
21.3
32
conc

Top Wing Wall SE Cor North Abutment

STA	+	π	-	Elev
BM	2.22	928.38		926.16

69+20

+50

+75

70

TP	0.60	918.95	10.03	918.35
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+50

71

LT

E

8-20-1970

RT

X-6

Bench Mark Plate in SE Wing Wall

27.1	27.0	26.3	26.4	24.0	24.7	24.8	24.6	23.8	19.5	14.9
1.29	1.35	2.12	1.97	4.4	5.7	3.6	3.8	4.6	8.9	13.5
31	26	26	11	10		9	30	39	47	57
SW	SW	GL	conc							

26.3	21.2	24.3	24.3	24.1	23.3	17.9	13.0
2.06	7.2	4.1	4.1	4.3	5.1	10.5	15.0
27	27	19		20	34	49	58
SW							

14.6	18.6	22.9	23.4	23.1	23.0	22.6	17.6	12.9
13.8	9.8	5.5	5.2	5.3	5.4	5.8	10.8	15.5
53	43	26	20		22	34	46	56

11.2	16.5	20.4	21.2	21.3	21.7	20.6	14.6
17.2	12.9	8.0	7.7	7.1	6.7	7.8	13.8
60	48	34	21		18	38	49

09.9	13.1	16.6	16.1	15.2	18.1	17.4	11.4	08.1
9.1	4.9	2.4	0.90	0.8	0.9	1.6	7.6	11.9
56	4.9	39	21		28	36	50	57

08.2	11.1	14.6	15.2	15.4	16.2	14.5	09.1	04.6
11.8	7.9	4.4	3.8	3.6	3.8	4.5	9.9	14.4
57	49	36	25		26	38	51	60

STA + π - Elev

918.95

+50

TP 2.34 913.99 7.30 911.65
2.34

72

+50

73

+50

74

TP 6.86 908.31 12.54 901.45
6.86

LT

E

RT

X-7

8-20, 1970

$\begin{array}{cccccccc} 05.2 & 10.1 & 12.0 & 12.5 & 13.0 & 12.9 & 12.7 & 07.3 & 03.2 \\ 13.8 & 8.6 & 7.0 & 6.5 & 6.0 & 6.1 & 6.3 & 11.7 & 15.8 \\ \hline 55 & 46 & 39 & 23 & & 24 & 36 & 49 & 59 \end{array}$

$\begin{array}{cccccccc} 00.8 & 4.4 & 08.6 & 9.1 & 10.3 & 10.6 & 10.4 & 10.2 & 05.0 & 01.0 \\ 13.2 & 9.6 & 5.4 & 4.3 & 3.7 & 3.4 & 3.6 & 3.8 & 9.0 & 13.0 \\ \hline 62 & 53 & 44 & 38 & 22 & & 19 & 35 & 45 & 56 \end{array}$

$\begin{array}{cccccccc} 99.5 & 01.8 & 04.5 & 01.3 & 07.9 & 06.3 & 08.0 & 07.5 & 04.1 & 00.5 \\ 14.5 & 12.2 & 9.5 & 6.7 & 6.1 & 5.7 & 6.0 & 6.5 & 9.9 & 13.5 \\ \hline 59 & 51 & 46 & 41 & 26 & & 27 & 37 & 48 & 63 \end{array}$

$\begin{array}{cccccccc} 99.3 & 99.4 & 02.1 & 04.8 & 05.5 & 06.2 & 05.8 & 05.6 & 02.4 & 00.4 \\ 14.7 & 14.6 & 11.9 & 9.2 & 8.5 & 7.8 & 8.2 & 8.4 & 11.6 & 13.6 \\ \hline 66 & 52 & 44 & 39 & 26 & & 19 & 37 & 47 & 64 \end{array}$

$\begin{array}{cccccccc} 99.3 & 99.8 & 03.6 & 03.3 & 03.7 & 03.2 & 02.9 & 01.0 & 00.8 \\ 14.7 & 14.2 & 10.4 & 10.7 & 10.3 & 10.8 & 11.1 & 13.0 & 13.2 \\ \hline 67 & 50 & 39 & 29 & & 26 & 38 & 53 & 72 \end{array}$

$\begin{array}{cccccccc} 02.1 & 00.9 & 00.6 & 00.9 & 01.5 & 01.5 & 00.9 & 01.5 & 02.0 & 01.9 & 01.8 \\ 11.9 & 13.1 & 13.4 & 13.1 & 12.5 & 12.5 & 13.1 & 12.5 & 12.0 & 12.1 & 12.2 \\ \hline 70 & 55 & 48 & 25 & & 16 & 30 & 38 & 45 & 54 & 62 \end{array}$

STA + π - Elev

908.31

+50

75

+46

BM

10.53 897.78 897.68

LT

E

8-20-70

RT

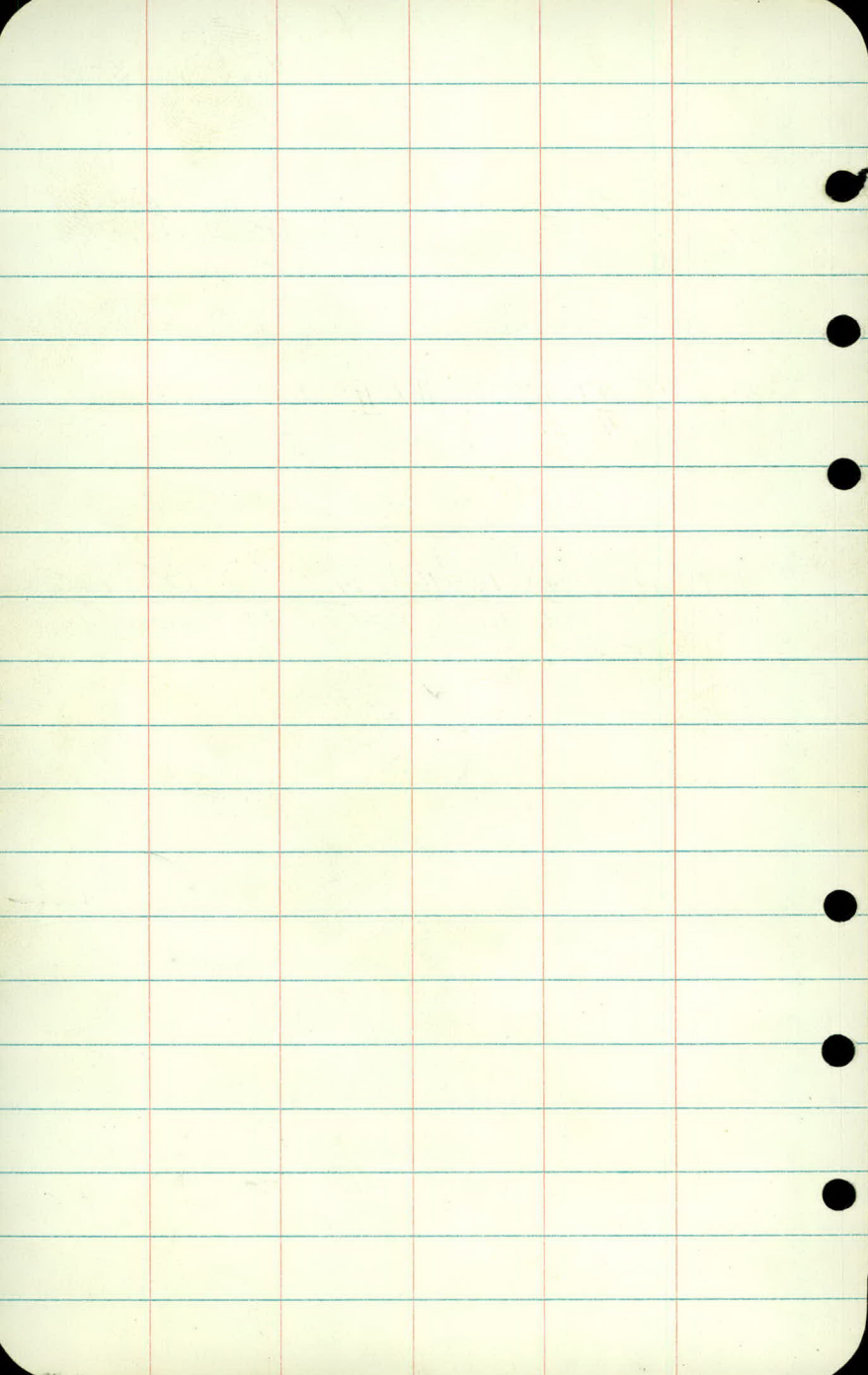
x-8

96.3	98.4	99.2	98.2	98.6	99.0	98.9	98.0	98.5	01.3	01.6	01.4
10.0	9.9	9.1	10.1	9.7	9.3	9.4	10.3	9.8	7.0	6.7	6.9
<u>78</u>	<u>64</u>	<u>48</u>	<u>38</u>	<u>25</u>	<u>18</u>	<u>25</u>	<u>29</u>	<u>32</u>	<u>47</u>	<u>65</u>	

96.7	96.7	96.6	96.3	96.0	96.4	96.4	96.4	98.1	98.1	98.0
11.6	11.6	11.7	12.0	12.3	11.9	11.9	11.9	10.2	10.2	10.3
<u>73</u>	<u>59</u>	<u>41</u>	<u>31</u>	<u>23</u>	<u>23</u>	<u>32</u>	<u>36</u>	<u>58</u>	<u>80</u>	

94.9	94.3	94.0	93.8	93.9	93.6	94.7	94.7	94.0
13.4	14.0	14.3	14.5	14.4	14.7	13.6	13.6	14.3
<u>89</u>	<u>63</u>	<u>39</u>	<u>12</u>	<u>19</u>	<u>36</u>	<u>62</u>	<u>82</u>	
BT	BT	GL	Victoria					

Top Hyd Co Rd C & Victoria



X Sections and
Profiles

23-1971

Co Rd C

STA + π - ELEV

2.18 99.86

897.68

2.18

75+72 $\neq$ Victoria

+83 G.L. Victoria Edge of Mat

76+04

✓

PK
CM
CP
BP

LT

E

June 22 '70

RT

1

10p Hyd SW cor Victoria & "C"

96.7	96.1	95.4	95.2	94.9	94.6	94.4	93.6	93.5	93.3	92.8	92.6	92.4	92.4
3.2	3.8	4.5	4.7	5.0	5.3	5.5	6.0	6.4	6.6	7.1	7.3	7.5	7.5
200	161	125	100	75	50	25		25	50	100	125	150	175

RR Tracks

94.9	94.9	94.9	94.9	94.4	93.7	93.3	92.9	92.7	92.3	92.1	91.9
5.0	5.0	5.0	5.0	5.5	6.2	6.6	7.0	7.2	7.6	7.8	8.0
125	112	100	75	98	25		25	50	75	100	125

M.H. M.H.

95.7

4.2

159

RR Tracks

89.7	93.9	94.3	94.9	93.7	93.0	92.4	91.9	91.5	90.8	90.5
10.2	6.0	5.6	5.0	6.2	6.9	7.5	8.0	8.4	9.1	9.4
130	110	100	75	50	25		25	50	75	100

Bit Bit

94.2 95.1

5.7

4.8

147

159

RR Tracks

STA + π - Elev

99.86

76+25

✓

76+50

✓

+75

✓

TP 9.91 902.05 7.72 92.14

LT

Z

RT

2

94.1	94.6	93.4	93.4	96.4	93.8	92.9	91.9	92.2	88.1	87.3
<u>5.8</u>	<u>5.3</u>	<u>6.5</u>	<u>6.5</u>	<u>3.5</u>	<u>6.1</u>	<u>7.0</u>	<u>8.0</u>	<u>7.7</u>	<u>11.8</u>	<u>12.6</u>
86	73	52	28	20		25	50	75	86	100
Bit	Bit	Bit								

93.6	90.9	88.5	88.0	93.6	94.6
<u>6.3</u>	<u>9.0</u>	<u>11.4</u>	<u>11.9</u>	<u>6.3</u>	<u>5.3</u>
93	100	109	128	140	150
					RR Tracks

92.6	93.6	94.0	92.8	96.2	98.6	97.2	95.4	94.6	94.9	87.1	86.7
<u>7.3</u>	<u>6.3</u>	<u>5.9</u>	<u>7.1</u>	<u>3.7</u>	<u>1.3</u>	<u>2.7</u>	<u>4.5</u>	<u>5.3</u>	<u>5.0</u>	<u>12.8</u>	<u>13.2</u>
90	79	67	50	29	21		25	50	87	100	120
Bit	Bit	Bit									

88.5	87.3	87.1	92.3	94.1
<u>11.4</u>	<u>12.6</u>	<u>12.8</u>	<u>7.6</u>	<u>5.8</u>
100	106	124	134	148
				RR Tracks

93.2	93.7	92.6	91.5	96.7	98.5	97.2	98.3	94.4	86.9	86.5
<u>6.7</u>	<u>6.2</u>	<u>7.3</u>	<u>8.4</u>	<u>3.2</u>	<u>1.4</u>	<u>2.7</u>	<u>1.6</u>	<u>5.5</u>	<u>13.0</u>	<u>13.4</u>
75	62	46	36	20		25	49	85	100	120
Bit	Bit	Bit								

92.0	87.5	87.1	92.7	93.9
<u>7.9</u>	<u>12.4</u>	<u>12.8</u>	<u>7.2</u>	<u>6.0</u>
86	100	121	134	145
				RR Tracks

Spike in PP STA 77± LT

STA + $\bar{A}$ - Elev

902.05

920

77

✓

+20

✓

TP 3.36 96.18 9.23 9282

3.35

+29

✓

PK
CM
CP
BP

LT

£

June 23 '70
Clear 89°
RT

3

³
^{92.8} ^{89.6} ^{89.3} ^{90.0} ^{95.1} ^{98.4} ^{80.2} ^{96.5} ^{93.8} ^{96.4} ^{86.5}
^{9.8} ^{12.5} ^{12.8} ^{12.1} ^{7.0} ^{3.7} ¹⁹ ^{5.6} ^{8.3} ^{15.7} ^{15.6}
³⁹ ³¹ ²⁶ ²⁰ ¹¹ ²² ³⁷ ⁵⁴ ⁶⁸ ¹⁰⁰
 Bit

^{93.2} ^{92.7} ^{91.9} ^{88.4} ^{96.7} ^{97.0} ^{92.2} ^{93.4}
^{8.9} ^{9.4} ^{10.2} ^{14.7} ^{15.4} ^{15.1} ^{9.9} ^{8.5}
⁵⁷ ⁶⁹ ⁷⁷ ⁹² ⁹⁹ ¹²³ ¹³¹ ¹⁴²
 Bit Bit RR Tracks

^{91.8} ^{92.4} ^{93.0} ^{92.2} ^{86.7} ^{86.8} ^{92.0} ^{89.5} ^{86.7} ^{86.9} ^{86.5} ^{96.6}
^{10.3} ^{9.7} ^{9.1} ^{9.9} ^{15.4} ^{15.3} ^{10.1} ^{12.6} ^{15.4} ^{15.2} ^{15.6} ^{15.5}
⁷⁴ ⁶⁷ ⁵³ ³⁸ ²⁰ ¹¹ ²⁶ ³⁹ ⁶⁴ ⁸⁶ ¹⁰⁰
 Bit Bit Bit

^{86.4} ^{86.9} ^{87.2} ^{92.4} ^{93.4}
^{15.7} ^{15.2} ^{14.9} ^{9.7} ^{8.7}
⁹⁴ ¹⁰⁶ ¹¹⁶ ¹²⁷ ¹⁴⁰
 RR Tracks

^{87.1} ^{86.7} ^{91.6} ^{92.2} ^{92.7} ^{92.0} ^{86.9} ^{86.0} ^{85.2} ^{86.1} ^{86.6} ^{86.6}
^{9.1} ^{9.5} ^{4.6} ^{4.0} ^{3.5} ^{4.2} ^{9.4} ^{11.2} ^{11.0} ^{10.1} ^{9.6} ^{9.6}
¹⁰³ ⁸⁹ ⁷¹ ⁶⁴ ⁵⁰ ³³ ¹⁹ ³⁰ ⁵⁰ ⁷⁰ ¹⁰⁰
 Bit Bit Bit

^{91.2} ^{91.8} ^{93.2}
^{9.0} ^{4.4} ^{3.0}
¹¹ ² ¹²⁴ ¹³⁷
 RR Tracks

STA + $\bar{A}$ - Elev

896.18

678

90

77+75

✓

BM 5.81 895.21 6.78 889.40 (889.40)

581

78

✓

78+50

Lt

L

Rt

4

91.7	91.2	91.3	89.9	86.5	86.3	86.7	86.1	86.5	86.5
4.5	4.0	4.9	6.3	9.7	9.9	9.5	9.8	9.7	9.7
58	45	30	22	13		25	50	75	100
B.T	B.T	B.T							

58

90.8	86.6	86.5	86.9	91.5	92.9
5.4	9.6	9.7	9.3	4.7	3.3
66	77	100	113	123	135

RR Tracks

96 08
87 40
76 8

Spike in PP STA 78+80 RT

86.7	86.1	90.2	91.1	91.8	90.8	86.9	85.3	87.2	86.6	86.6	86.5
8.5	8.8	5.0	3.8	3.4	4.4	8.3	9.9	8.0	8.6	8.6	8.7
92	80	61	52	39	23	11		25	50	75	100

B.T B.T B.T

87.0	91.5	92.1
8.2	3.7	2.5
112	121	133

RR Tracks

86.3	86.7	89.0	90.9	91.3	90.7	86.8	86.1	86.5	86.7	86.5	86.5
8.9	8.5	6.2	4.3	3.7	4.5	8.4	9.1	8.7	8.5	8.7	8.7
83	57	51	42	28	14		1	27	50	70	100

B.T B.T B.T

86.4	91.2	91.3
8.8	4.0	2.9
107	117	129

RR Tracks

STA.

+

K

-

Elev

895.21

6.48

79+00

✓

79+50

✓

T.P. 8.82 897.55 6.48 888.73

8.82

79+92 END PIPE
49+ 92 END PIPE
51

80 + 17

Range Tie to Ditch

LT

E

RT

5

86.1	86.8	89.1	90.1	91.0	90.6	89.4	86.5	85.9	86.3	86.3	86.1
9.1	8.4	6.1	4.8	9.2	9.7	5.8	8.7	9.3	8.9	8.9	9.1
78	48	94	34	20	6		8	25	50	75	100
			B.T	B.T	B.T						

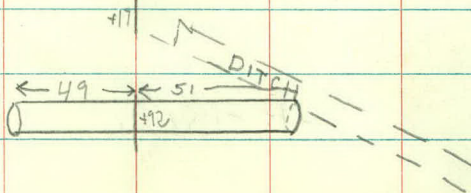
94.2	86.0	90.4	91.8
10	92	48	3.4
100	106	113	123

RR Tracks

89.8	86.2	86.0	86.5	89.4	90.7	91.3	90.7	86.5	85.9	86.5	86.5	86.3
5.4	9.0	9.2	8.7	5.8	4.5	3.9	9.5	8.7	9.3	8.7	8.7	8.9
114	107	68	44	37	28	14		12	26	50	75	100
					B.T	B.T	B.T					

91.5
3.7
128

RR Tracks



STA + π - Elev

897.55
2.85

79
+ 92

✓

4-17 & Ditch Profile RT

Ditch

+ 50

✓

TP 8.12 902.82 2.85 894.70

LT

£

Rt

6

8A.9 87.7 88.7 91.3 91.7 91.1 91.0 88.6 87.1 8A.11 8A.6
 1256 9.82 8.82 6.3 5.9 6.5 6.6 9.0 10.5 13.4 13.0
 50 49 40 25 10 4 25 51 51 66

FL Conc Conc Bit Bit Bit Bit Top Pipe FL Ditch
 Pipe

85.9 8A.8 88.7 90.4 91.2 86.5 85.9
 11.7 12.87 8.9 7.2 6.4 11.1 11.7
 77 108 108 117 130 100 80
 Top Culvert RR Tracks
 FL Culvert under Tracks

£ 92.1 91.8 90.8 Rt 86.6 85.5 85.0 8A.5 8A.4 8A.1
 5.5 5.8 6.8 11.0 12.1 12.6 13.1 13.2 13.5
 £ 7 12 19 21 50 75 100 125
 Bit Bit

86.51

ELEV H₂O = 11.04

86.6 86.6 92.1 93.2 93.4 93.2 93.1 87.6 86.8 86.5 86.7
 11.2 10.9 5.5 4.3 4.2 4.3 4.5 10.0 10.8 11.1 10.9
 81 41 28 19 6 8 20 50 78 107
 Bit Bit Bit Bit

86.6 89.4 91.6
 11.0 8.4 6.0
 112 119 143
 RR Tracks

STA + π - Elev

402.82

81

✓

+56

✓

+63

+78

€ HEINEL Dr

LT

E

RT

7

86.9	87.6	87.8	94.3	95.6	96.4	94.9	94.7	88.6	86.9	86.6	86.9
<u>15.9</u>	<u>15.2</u>	<u>15.0</u>	<u>8.5</u>	<u>7.3</u>	<u>7.4</u>	<u>7.9</u>	<u>8.1</u>	<u>14.3</u>	<u>15.9</u>	<u>16.2</u>	<u>15.9</u>
130	79	44	28	18		10	70	26	50	75	100

B.T B.T B.T

90.0 92.0

→ 12.8 10.8

136 145

RR Tracks

90.8	91.9	92.2	96.9	97.8	98.0	97.4	88.3	87.0	86.9
<u>12.0</u>	<u>10.9</u>	<u>10.6</u>	<u>5.9</u>	<u>5.0</u>	<u>4.8</u>	<u>5.4</u>	<u>14.5</u>	<u>15.8</u>	<u>15.9</u>
105	80	50	35	26		10	38	68	110

B.T

89.7

→ 13.1

143

91.5	95.1	97.3	99.2	97.4	88.4	87.0	86.7
<u>8.3</u>	<u>7.7</u>	<u>5.5</u>	<u>4.5</u>	<u>5.2</u>	<u>14.4</u>	<u>15.8</u>	<u>16.1</u>
100	83	35		12	42	72	106

B.T B.T

95.2	95.3	95.5	96.6	99.1	99.2	88.4	86.9	86.7
<u>7.6</u>	<u>7.5</u>	<u>7.3</u>	<u>6.2</u>	<u>3.2</u>	<u>3.7</u>	<u>4.6</u>	<u>14.4</u>	<u>15.9</u>
150	125	100	50	18		13	45	75

113

STA + π - Elev

902.82

80

2.02

81+98

82+50

+75

+92

BM 13.00 915.03 0.80 902.02 (902.03)

82+10

SW cor Leg Highline Pole

LT

E

RT

8

95.5	95.3 ⁶	96.1	97.9	96.7	98.1	98.3	98.0	98.9	8.1	87.9	99.5
7.3	7.7	6.4	4.9	5.9	4.7	2.5	2.8	3.9	13.4	14.9	13.3
113	83	65	49	39	28	13		12	45	72	110

B.T B.T B.T

02.0	01.0	92.7	90.9	89.7
0.2	1.2	10.1	11.9	13.1
15	45	76	115	

02.1	99.0	97.8	96.2	95.0	94.8
0.7	3.8	5.0	6.6	7.8	8.0
18	35	57	82	106	118

11.08

3.95

37

MH

Top Hyd C & Heinel

PK	02.1	02.3	02.3	99.8	99.4	00.8	00.6	June 24 '70
CD	02.1	02.3	02.3	99.8	99.4	00.8	00.6	cloudy windy 60°
BP	12.9	12.7	12.7	15.2	15.6	14.2	14.4	
	114	92	73	54	29	14		

B.T B.T

902.82

12.21

STA + $\bar{A}$ - Elev

915.03

82+50

+75

83+00

Equation

$$83 + 47.83 = 8400.03$$

+30

+42 $\notin$ ENT RT

8+06 P.W.

LT

-

RT

9

0.2 0.3 0.8 0.8 0.5 0.2
12.3 11.4 12.2 13.2 12.5 12.4
106 80 57 29 12

Bit Bit

0.8 0.2 0.5 0.2 0.4 0.9
10.2 9.8 10.5 11.8 11.6 11.1
107 48 41 31 17

0.3 0.4 0.5 0.3 0.0 0.4 0.5 0.4 0.9 0.1 0.3 0.1 0.9 0.1
8.7 6.6 7.5 10.7 11.0 10.4 10.0 10.6 10.1 10.9 16.7 15.9 16.1 17.9
106 80 37 27 21 15 18 18 19 34 41 67 110

Cur

0.6 0.5 0.4 0.9 0.2 0.5 0.9 0.4 0.5 0.7 0.1 0.1 0.3
4.4 5.5 5.6 9.1 8.8 8.5 9.1 8.6 9.3 13.3 13.9 14.7
100 74 48 25 14 19 19 21 36 61 88

Bit Bit

0.2 0.8 0.0 0.6 0.7 0.1 0.5 0.4 0.1 0.8 0.0
3.8 4.2 5.0 8.4 8.3 7.9 8.5 9.6 12.9 13.2 14.0
100 70 46 22 12 20 29 51 66 85

0.4 0.0 0.7 0.6 0.2 0.7 0.0 0.2 0.2 0.1
3.6 3.0 4.0 8.0 7.6 7.4 7.8 7.3 8.0 12.1 12.4 13.3
106 75 53 23 17 26 20 22 36 45 67

Bit Bit

0.6
13.4
86

STA + π - Elev

915.03
210

8+21

+46

TP 9.84 922.77 2.10 912.93
989

+76

✓

+82

+92 WGL Fisk

Lt

E

Rt

10

12.4	13.2	12.2	08.0	08.4	08.4	08.0	08.5	07.6	03.0	03.8	03.6
<u>2.6</u>	<u>1.8</u>	<u>2.8</u>	<u>7.0</u>	<u>6.6</u>	<u>6.6</u>	<u>7.0</u>	<u>6.5</u>	<u>7.4</u>	<u>12.0</u>	<u>11.2</u>	<u>11.4</u>
108	8.9	48	20	11		21	21	23	36	39	54

Curb

HOUSE

14.8	14.2	13.7	09.7	09.6	09.8	09.3	09.9	09.0	05.3	08.5	10.2
<u>0.2</u>	<u>0.8</u>	<u>1.3</u>	<u>5.3</u>	<u>5.4</u>	<u>5.2</u>	<u>5.7</u>	<u>5.1</u>	<u>6.0</u>	<u>9.7</u>	<u>6.5</u>	<u>4.84</u>
104	80	45	22	10		12	12	14	24	33	45

BIT

BIT Curb

HOUSE
CONC

18.4	17.6	16.2	14.4	11.4	11.5	11.6	11.1	11.6	11.0	10.7	09.4	09.3
<u>4.4</u>	<u>5.2</u>	<u>6.6</u>	<u>8.4</u>	<u>11.4</u>	<u>11.3</u>	<u>11.2</u>	<u>11.7</u>	<u>11.2</u>	<u>11.8</u>	<u>12.1</u>	<u>13.4</u>	<u>13.5</u>
114	100	75	43	13	10		22	22	23	25	28	30

Curb

10.1	10.7	10.7	10.5
<u>12.7</u>	<u>12.11</u>	<u>12.11</u>	<u>12.3</u>
80	65	55	35

CONC

CONC

20.0	18.1	16.5	14.2	11.9	11.9	11.9	11.5	12.0	11.3	11.0	10.9	10.2
<u>2.8</u>	<u>4.7</u>	<u>6.3</u>	<u>8.6</u>	<u>10.9</u>	<u>10.9</u>	<u>10.9</u>	<u>11.3</u>	<u>10.8</u>	<u>11.5</u>	<u>11.8</u>	<u>11.9</u>	<u>12.6</u>
114	91	70	41	12	9		24	24	44	53	65	86

BIT

BIT Curb

22.1	20.5	19.4	17.6	12.8	12.4	12.5	11.9	11.7	11.0	09.8	08.9
<u>0.7</u>	<u>2.3</u>	<u>3.4</u>	<u>5.2</u>	<u>10.0</u>	<u>10.4</u>	<u>10.3</u>	<u>10.93</u>	<u>11.1</u>	<u>11.8</u>	<u>13.0</u>	<u>13.9</u>
119	96	76	54	19	8		28	40	60	85	100

BIT

CB

STA + π - Elev

922.77

8.62

1415

9

BM

8.62 914.15 914.15

LT

£

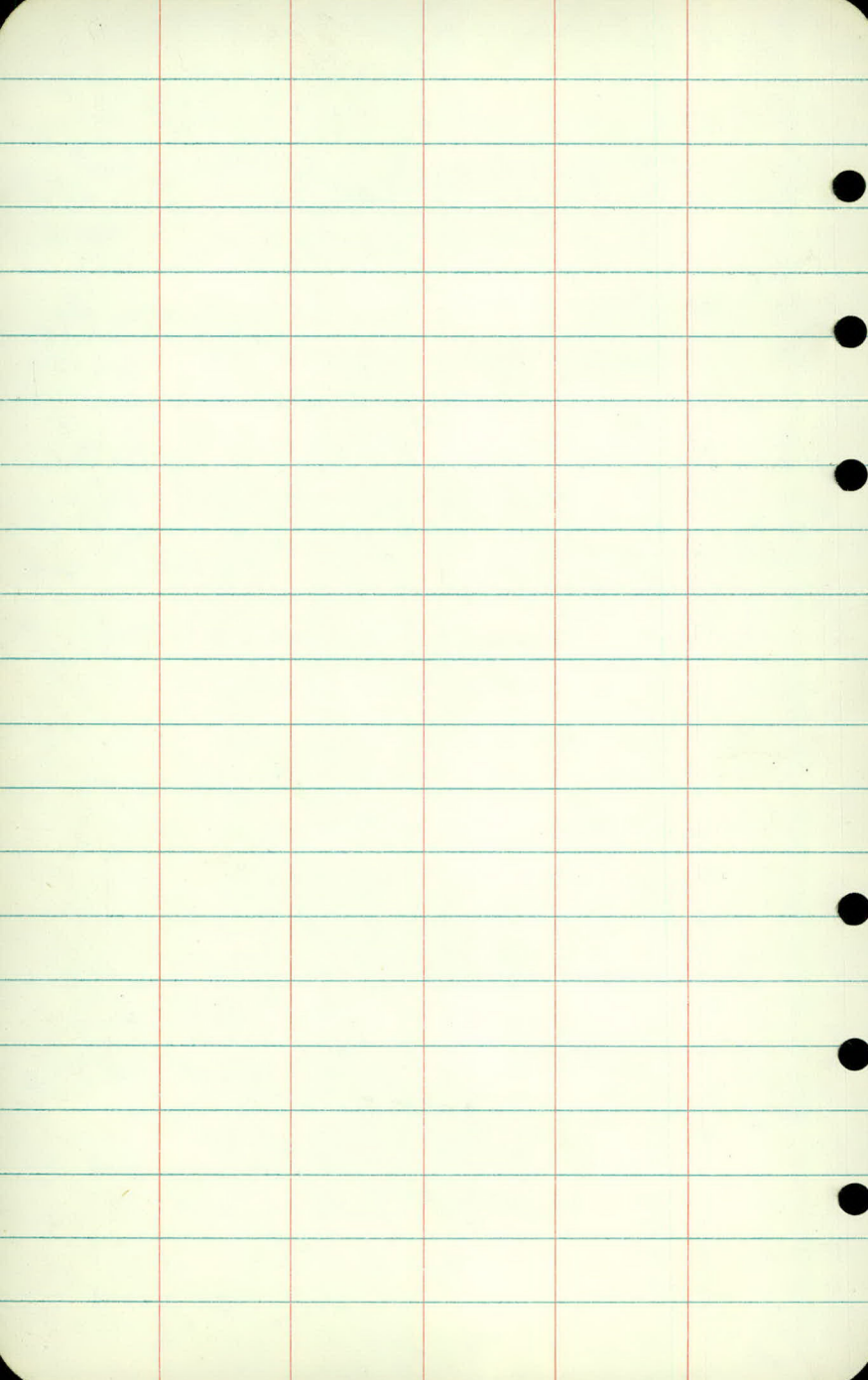
RT

11

13.0

9.8

Top Hyd SW Cor Fisk & C



STA + π - Elev

BM 1.02 915.17
0.70

914.15

9+07

+34

TP 11.95 926.42 0.70 914.47
" " " "

+50

+75

10

+17

PK
CM
CD
BP

LT

£

June 19 1970 13
Fair 70° RT

Top Hyd SW cor Fisk & C

£ Fisk

13.3	12.9	12.6	11.5	09.7	08.4	07.1
1.9	2.3	2.7	3.7	5.5	6.8	8.1
	27	36	60	100	125	150
		MH				

14.8	14.5
0.4	0.7
	24
	ER

15.6

10.8

11.9

9.5

18.4

8.0

21.96	52	21.17	21.00	20.82	20.0	19.4	19.2
4.46	490	5.25	5.60	6.4	7.02	7.2	
100	79	55	33	22	10		
				MH			

GL B618 CURB

Terrace

STA + T - ELEV

926.42

+49

+75

11

11

+25

+50

TP 12.54 38.36 0.60 925.82

12.54

+75

TP

LT

£

RT

14

$\begin{array}{r} 21.98 \\ 4.44 \\ \hline 160 \end{array}$
 $\begin{array}{r} 21.61 \\ 4.81 \\ \hline 75 \end{array}$
 $\begin{array}{r} 21.17 \\ 5.25 \\ \hline 50 \end{array}$
 $\begin{array}{r} 20.98 \\ 5.44 \\ \hline 31 \end{array}$
 $\begin{array}{r} 20.8 \\ 5.6 \\ \hline 18 \end{array}$

Terrace

5.4 GL BG18 Conc CURB

$\begin{array}{r} 22.3 \\ 4.1 \end{array}$

$\begin{array}{r} 23.5 \\ 2.9 \end{array}$

$\begin{array}{r} 24.1 \\ 1.7 \end{array}$

$\begin{array}{r} 25.8 \\ 0.6 \end{array}$

$\begin{array}{r} 26.9 \\ 11.5 \end{array}$

STA + $\nearrow$ - E/EV

938.36

12+92

12

+14

+25

+50

+74

LT

£

RT

15

£ ENT

$\begin{array}{r} 21.5 \\ 10.9 \\ \hline 12 \end{array}$
 $\begin{array}{r} 27.9 \\ 10.5 \\ \hline 26 \end{array}$
 $\begin{array}{r} 27.6 \\ 10.8 \\ \hline 41 \end{array}$
 $\begin{array}{r} 27.0 \\ 11.4 \\ \hline 55 \\ \text{conc} \end{array}$
 $\begin{array}{r} 25.1 \\ 11.85 \\ \hline 75 \end{array}$
 $\begin{array}{r} 25.8 \\ 12.52 \\ \hline 75 \end{array}$

$\begin{array}{r} 27.9 \\ 10.5 \end{array}$

$\begin{array}{r} 21.62 \\ 6.74 \\ \hline 74 \end{array}$
 $\begin{array}{r} 31.45 \\ 6.91 \\ \hline 57 \end{array}$
 $\begin{array}{r} 30.91 \\ 7.42 \\ \hline 43 \\ \text{conc.} \end{array}$
 $\begin{array}{r} 30.1 \\ 8.3 \\ \hline 25 \end{array}$
 $\begin{array}{r} 28.4 \\ 10.0 \\ \hline 4 \end{array}$
 $\begin{array}{r} 28.4 \\ 10.0 \end{array}$

£ ENT

$\begin{array}{r} 28.9 \\ 9.5 \end{array}$

$\begin{array}{r} 30.0 \\ 8.4 \end{array}$

£ ENT

$\begin{array}{r} 31.1 \\ 7.3 \\ \hline 11 \end{array}$
 $\begin{array}{r} 31.3 \\ 7.1 \\ \hline 25 \end{array}$
 $\begin{array}{r} 30.9 \\ 7.5 \\ \hline 41 \end{array}$
 $\begin{array}{r} 30.7 \\ 7.7 \\ \hline 45 \end{array}$
 $\begin{array}{r} 30.8 \\ 7.6 \\ \hline 75 \end{array}$
 $\begin{array}{r} 31.4 \\ 7.0 \\ \hline 75 \end{array}$

STA + π - Elev

938.36

13

+25

+50

BM 867 945.90 1.10 937.26 937.23
867

+71

14

+25

LT

E

RT

16

$$\begin{array}{r} 32.2 \\ 6.2 \end{array}$$

$$\begin{array}{r} 33.4 \\ 5.0 \end{array}$$

$$\begin{array}{r} 34.5 \\ 3.9 \end{array}$$

Top Hyd SW cor Avon & C

 PK
 CM
 CP
 BP

June 22 '70

Clear 700

E AVON ST

35.5	35.8	35.6	34.9	34.1	33.1
10.4	10.1	10.3	11.0	11.8	12.8
	<u>11</u>	<u>26</u>	<u>50</u>	<u>75</u>	<u>100</u>

$$\begin{array}{r} 37.1 \\ 8.8 \end{array}$$

$$\begin{array}{r} 38.3 \end{array}$$

7.6

STA + $\bar{A}$ - Elev
945.90

14+50

+75

15

+03

+11

+25

LT

£

RT

17

39.4

6.3

A0.8

5.1

A1.8

4.1

A1.9

A2.0

A1.7

A0.0

39.6

39.6

£ ENT

4.0

3.9

4.2

5.9

6.3

6.31

10

21

50

75

105

conc

44

A

AA.2

A3.7

A2.7

A2.2

653

1.71

2.18

3.2

3.7

£ ENT

69

56

43

25

conc

A2.7

3.2

STA + π - Elev

945.90

2.56

933.34

+51

+75

16

+25

+50

+75

TP 2.94 946.28 2.56 943.34

LT

£

RT

18

£ ENT

A ^{3.3}	A ^{3.4}	A ^{3.1}	A ^{3.6}	A ^{4.1}	A ^{4.4}
2.6	2.5	2.8	2.4	1.72	1.50
	10	22	50	67	88
				CONC	

A^{3.6}

2.3

A^{3.7}

2.2

A^{3.8}

2.1

A^{3.8}

2.1

A^{3.7}

2.2

STA + π - Elev

946.28

1.72

17

+ 25

+ 34

+ 50

+ 80

BM

1.72 944.56 (944.56)

18

+ 25

LT

¢

RT

19

3.4

~~A1.0~~

2.9

¢ ENT

A3.3

A3.5

A3.6

A3.6

A3.0

A2.6

3.0

2.8

2.8

2.8

3.3

3.7

8

20

24

50

67

BIT

A3.2

3.1

A3.6°

A3.A

A2.9

A2.8

A3.1

A3.0

2.68
97
CONC

2.9
75

3.4
50

3.5
30

3.2
4

3.3

¢ ENT

Top Hyd STA 17+99

A2.8

3.5

A2.6

3.8

STA + π - Elev

946.28

+50

+75

+82

19

+25

+50

Lt

E

Rt

20

A_{2.3}

4.0

A_{2.1}

4.2

E ENT

A_{2.1}

4.2

A_{2.3}

4.0

A_{2.1}

4.2

A_{2.2}

4.1

A_{2.1}

4.2

A_{2.3}

4.0

A_{2.2}

4.1

7

17

42

56

75

100

A_{1.9}

4.4

A_{1.7}

4.6

A_{1.4}

4.9

STA + π - Elev

946.28
594
4034

+75

20

+05

+16

BM 2.72 943.09 5.94 940.34 (940.37)

+25

+50

Lt

£

Rt

21

$$\begin{array}{r} A1.1 \\ 5.2 \end{array}$$

$$\begin{array}{r} A0.8 \\ 5.5 \end{array}$$

£ ENT

$A0.6$	$A0.8$	$A0.9$	$A1.1$	$A2.0$
5.7	5.5	5.4	4.9	4.3
	<u>4</u>	<u>15</u>	<u>33</u>	<u>49</u>

$A1.9$	$A1.5$	$A0.9$	$A0.6$	$A0.4$	$A0.5$	
4.4	4.8	5.4	5.7	5.9	5.8	£ ENT
<u>100</u>	<u>75</u>	<u>50</u>	<u>30</u>	<u>4</u>		

Roseville BM # 37.3

$$\begin{array}{r} A0. \\ 2.8 \end{array}$$

$$\begin{array}{r} A0.9 \\ 3.2 \end{array}$$

STA + π - Elev

43.09

+75

21

+06

+25

+50

+75

LT

- £

↗

R+

22

39.6

3.5

39.3

3.8

39.2

39.3

38.9

39.3

39.5

39.8

£ ENT (BIF)

3.9

3.8

4.2

3.8

3.6

3.3

5

15

38

60

75

39.0

4.1

38.7

4.4

38.5

4.6

STA + π - Elev

943.09

+ 82

22

+ 25

BM

2.70 940.39 (940.41)

+ 50

+ 75

23

Lt

£

RT

23

£ ENT (Crushed Rock)

	⁵ 38.6	⁶ 38.6	³ 38.3	¹ 38.1	⁷ 37.7	⁶ 37.6	⁰ 38.0
	46	46	48	50	54	55	51
		<u>5</u>	<u>15</u>	<u>21</u>	<u>50</u>	<u>75</u>	<u>100</u>

^A38.
3
4.7

£ ENT (Bit)

	³ 38.3	³ 38.3	⁰ 38.0	⁵ 37.5	⁸ 36.8	² 36.2	⁶ 35.6	³ 37.3
	4.8	4.8	5.1	5.6	6.3	6.7	7.5	8.8
		<u>5</u>	<u>15</u>	<u>30</u>	<u>50</u>	<u>75</u>	<u>100</u>	<u>175</u>

TopH9d STA 22+40 Lt

	³ 38.3
	4.8

¹38.1
3
5.0

⁹37.9
3
5.2

STA + π - Elev

943.09

4.28

39.81

+25

+45

+75

24

+25

+36

TP

1.27

940.08

4.28

938.81

L.T

£

RT

24

37.8

5.3

37.4

37.6

37.3

9

A

A

A

A

6

£ ENT (crushed Rock) 5.5

5.5

5.8

6.2

6.7

6.7

6.6

5

14

25

50

78

84

37.2

5.9

36.9

6.2

36.8

6.3

38.39

37.53

36.87

36.63

36.2

36.5

36.6

4.70

5.56

6.22

6.46

6.9

6.6

6.5

£ ENT (conc)

9.4

6.9

5.1

4.0

2.5

9

conc.

STA + $\bar{T}$ - Elev

940.08

+44

+75

25 25

+25

+50

+75

LT

Σ

RT

25

	36.5	36.6	36.3	36.0	36.2	36.3	36.3
Σ ENT (Bit)	3.6	3.6	3.8	4.1	3.9	3.9	3.8
	$\frac{2}{2}$	$\frac{13}{13}$	$\frac{26}{26}$	$\frac{4.6}{4.6}$	$\frac{70}{70}$	$\frac{90}{90}$	
			Bit				

36.2

3.9

36.0

4.1

36.7

4.4

$3A.9$ $3A.9$ $3A.8$ $3A.7$ $3A.6$ $3A.6$

$\frac{5.2}{90}$ $\frac{5.2}{62}$ $\frac{5.3}{41}$ $\frac{5.4}{25}$ $\frac{4.7}{10}$ 4.5 Σ ENT (Bit stabilized)

$3A.4$?

5.7

STA + π - Elev

940.08
306

26

+27

+50

BM 1.92 938.97 3.06 937.02 37.05
1.92

+75

27

+10

LT

Σ

RT

26

Σ ENT (Dirt)

$\begin{array}{r} 35.1 \\ 35.2 \\ 3A.2 \\ 33.3 \\ 33.2 \\ 33.1 \end{array}$
 $\begin{array}{r} 4.7 \\ 4.9 \\ 5.9 \\ 6.8 \\ 6.9 \\ 7.0 \end{array}$
 $\begin{array}{r} 11 \\ 30 \\ 50 \\ 75 \\ 100 \end{array}$

$\begin{array}{r} 35.3 \\ 35.2 \\ 3A.8 \\ 35.1 \\ 35.3 \end{array}$
 $\begin{array}{r} 4.8 \\ 4.9 \\ 5.3 \\ 5.0 \\ 4.8 \end{array}$
 $\begin{array}{r} 75 \\ 60 \\ 30 \\ 11 \end{array}$

Σ ENT BIT

$\begin{array}{r} 35.2 \\ 35.1 \\ 4.9 \end{array}$

Top Hyd STA 26+43

$\begin{array}{r} 3A.7 \\ 4.3 \end{array}$

$\begin{array}{r} 3A.2 \\ 4.8 \end{array}$

$\begin{array}{r} 35.5 \\ 35.1 \\ 35.0 \\ 3A.8 \\ 3A.3 \\ 3A.1 \\ 3A.1 \end{array}$
 $\begin{array}{r} 3.32 \\ 3.56 \\ 3.89 \\ 4.20 \\ 4.7 \\ 4.9 \\ 4.9 \end{array}$
 $\begin{array}{r} 100 \\ 75 \\ 50 \\ 25 \\ 15 \\ 15 \end{array}$

Σ ENT (conc)

STA + π - Elev

38.97

+16

+50

+75

+96

~~28+25~~

28+25

+50

LT

£

RT

27

£ ENT (Bit)

$\begin{array}{ccccccc}
33.9 & 33.8 & 33.0 & 33.10 & 33.9 & 33.4 \\
5.1 & 5.2 & 5.0 & 4.4 & 4.1 & 3.6 \\
15 & 15 & 28 & 60 & 100
\end{array}$

33.5

5.5

32.9

6.1

$\begin{array}{ccccccc}
36.1 & 36.7 & 36.6 & 36.7 & 36.4 & 36.3 & 32.4 \\
2.9 & 3.3 & 4.3 & 5.3 & 6.6 & 6.7 & 6.6 \\
100 & 86 & 62 & 36 & 15 & 15
\end{array}$

£ ENT (Bit)

31.5

7.5

30.5

8.5

STA + π - Elev

938.97
12,96

+75

28488

29

+19

+50

+75

1.49 927.56 12.90 926.07
149

LT

£

RT

28

29.6

9.4

£ ENT

29.0	29.0	29.1	29.5	29.9	31.7
10.0	10.0	9.9	9.5	9.1	7.3
	<u>16</u>	<u>16</u>	<u>26</u>	<u>33</u>	<u>52</u>
			BIT	BIT	Gravel

28.5

10.5

36.3	31.1	32.1	29.5	28.1	28	27.8	
5.7	4.9	6.9	9.5	10.9	11.2	11.2	£ ENT
<u>100</u>	<u>74</u>	<u>53</u>	<u>31</u>	<u>16</u>	<u>16</u>		
Gravel	Gravel	BIT	BIT				

26.5

12.5

26.4

13.6

STA + π - Elev

927.56

+96

30+22 Begin conc curb

+50

+74 Begin Radius

+89

+92 ^{in Elev} GL Dale ST

LT

Z

RT

29

ENT (BIT)

2 ^{A3}	2 ^{A2}	2 ^A	2 ^{A8}	2 ⁵⁰
3.3	3.4	3.2	2.7	2.5
23	24	39	5.0	

2 ^{1.6}	2 ^{1.5}	2 ^{1.6}	2 ^{1.1}	2 ^{1.9}	2 ^{3.1}	2 ^{3.3}	2 ^{3.37}	2 ^A	2 ^{1.8}	2 ^{1.2}	2 ^{1.2}	2 ^{A.5}	2 ^{A.6}
0.0	0.1	0.0	2.5	3.77	4.25	4.19	4.2	4.38	4.44	3.94	3.1	3.0	
62	49	38	28	24	24	22		24	25	25	33	54	

CONC CONC

2 ^{5.6}	2 ^{1.3}	2 ^A	2 ^{1.6}	2 ^{1.8}	2 ^{2.7}	2 ^{1.5}	2 ^{1.6}	2 ^{1.0}	2 ^{3.58}	2 ^{1.6}	2 ^{3.8}
2.0	2.3	4.2	4.90	5.38	5.29	5.1	5.40	5.46	3.98	4.0	3.8
60	38	28	24	24	22		23	24	24	30	54

CONC CONC

2 ^{A.3}	2 ^{A1}	2 ^{1.1}	2 ^{1.9}	2 ^{1.6}	2 ^{1.33}	2 ^{1.8}	2 ^{1.15}	2 ^{0.98}	2 ^{1.6}	2 ^{2.7}	2 ^{2.6}
3.3	3.5	4.5	5.77	6.30	6.23	5.8	6.41	6.58	6.0	4.9	5.0
67	49	36	25	25	23		23	25	25	32	55

CB

2 ^{1.00}	2 ^{1.6}
6.56	6.0
36	
CB	

2 ^A	2 ^{3.0}	2 ^{1.5}	2 ^{2.0}	2 ^{1.28}	2 ^{1.1A}	2 ^{1.6}	2 ^{0.60}	2 ^{0.36}	19 ^A	17 ³	15 ⁸	11 ²
3.2	4.6	5.1	5.6	6.28	6.42	6.0	6.96	7.21	8.2	10.3	11.8	13.4
200	125	100	75	48	40		37	45	61	100	130	152

END ER POR POR ER END
 BIT CONC CONC CONC CONC BIT
 CURB CURB

STA + π - Elev

927.56
2.58
98

30+97

31+15 ∇ Dale ST

✓

BM

2.58 924.98 924.98
2.58
927.56

LX

E

RT

30

21.5

21.05

6.1

6.51
21
MH

22.8 22.6 22.1 21.6 21.4 21.4 21.1 20.5 17.4 15.9

4.8 5.0 5.5 6.0 6.2 6.2 8.5 7.1 8.7 10.2 11.7
11 100 75 50 22 22 44 75 100 125

23.6 21.2 21.7

13.16 11.5

4.0 3.4 2.9
153 180 200

14.4 13.1
175 149

Top Hyd NE cor C & D 1/2

STA + π - Elev

RAB.
B.W
H.H.H
D.S.

MAY. 12-1971

X- SECTION 5
FISK to DALE

STA	+	π	-	Elev
	7.78	921.93		914.15

9+21 E. Gutter line Fisk

+23

+50

10+00

+15 MH. H 10' 2.58 919.35

+17 West Gutter

Lt

£

Rt

2

TOP Hyd S.W. Cor. Fisk & C

20.9	19.5	17.4	15.2	13.7	14.1	13.8	11.7	10.7
1.0	2.4	4.5	6.7	8.2	7.8	8.1	10.2	11.2
73	52	35	23	8		24	52	75

Same

14.2	13.9	13.3	12.0	11.7	11.3
7.7	8.0	8.6	9.9	10.2	10.6
	25	42	53	67	75

21.8	20.3	16.6	15.3	15.6	15.4	15.9	15.2	12.8	13.3	13.2
0.1	1.6	5.3	6.6	6.3	6.5	6.0	6.7	9.1	8.6	8.7
60	43	21	8		25	25	26	35	46	75

T.C

21.7	21.1	20.1	18.2	18.3	18.3	18.8	18.2	15.0	14.7	14.0
0.2	0.8	1.8	3.7	3.6	3.6	3.1	3.7	6.4	7.2	7.23
60	44	26	7		24	24	26	33	54	75

T.C

Conc

21.4	21.3	21.0	20.4	19.8	19.1	19.2	19.3	19.8	19.1	15.7	15.0	15.26
0.5	0.6	0.9	1.5	2.1	2.8	2.7	2.6	2.1	2.8	6.2	6.9	6.67
75	65	44	28	18	3		24	24	27	35	52	65

T.C

STA	+	π	-	Elev
-----	---	-------	---	------

		921.93		
--	--	--------	--	--

10+30	E	TERRACE DR		
-------	---	------------	--	--

+34	MH. Rt 30'	2.39	919.54	
-----	------------	------	--------	--

+49	East Gutter Line			
-----	------------------	--	--	--

T.P.	13.33	932.70	2.56	919.37
------	-------	--------	------	--------

+62				
-----	--	--	--	--

+92				
-----	--	--	--	--

11+00				
-------	--	--	--	--

Lt

E

Rt

3

21.9	21.6	20.9	20.0	19.9	20.1	20.6	20.2	16.3	15.2	15.6A
0.0	0.3	1.0	1.9	2.0	1.8	1.3	1.7	5.4	6.7	6.29
75	53	28	4		24	24	28	36	52	67

21.0	21.3	21.0	20.8	20.9	21.0	21.2	21.6	21.1	17.9	16.4	15.8
0.3	0.6	0.9	1.1	1.0	0.9	0.7	0.3	0.8	4.0	5.5	6.1
75	61	40	20	3		24	24	28	34	44	56

25.3	23.7	23.0	22.4	21.3	21.7	21.9	22.4	22.1	19.1	18.1	16
9.4	9.4	9.7	10.3	11.4	11.0	10.8	10.3	10.6	13.4	14.6	16
75	61	43	24	7		25	25	27	35	44	5

T.C

25.7	25.5	25.1	22.7	23.1	23.5	24.0	23.7	21.8	22.5	22.3
7.0	7.2	7.6	10.0	9.6	9.2	8.7	9.0	10.9	10.2	10.4
62	44	29	6		25	25	28	34	42	75

T.C

26.5	25.8	23.2	23.5	23.8	22.7	22.0	22.6	22.7	22.7
6.2	6.9	9.5	9.2	8.4	10.4	10.7	10.1	10.0	10.0
43	27	6		25	31	35	42	60	75

Fe

Sta	+	π	-	Elev
		932.70		

+50

+75

+90 $\frac{1}{2}$ Ent Rt 20' Conc.

12+00

+14 $\frac{1}{2}$ Ent Lt.

T.P.	10.26	942.75	0.21	932.49
------	-------	--------	------	--------

+50

L+

E

R+

4

✓

29.4	28.9	28.1	25.6	25.8	25.7	25.1	24.0	24.2	24.3
33	38	4.6	7.1	6.9	7.0	7.6	8.7	8.5	8.4
43	32	23	5		26	28	36	48	69
Fe									

✓

29.8	30.5	29.6	26.6	25.8	26.8	26.3	25.7	25.8	25.5
1.9	2.2	3.1	6.1	5.9	5.9	6.4	7.4	6.9	7.2
63	49	30	5		25	29	36	51	60

✓

29.2	31.1	30.3	27.3	27.4	27.4	26.49
1.5	1.6	2.4	5.4	5.3	5.3	6.21
66	53	31	4		25	55
					conc.	

✓

31.4	31.2	30.5	27.7	27.8	27.9	26.5	26.8	26.5	26.3
1.3	1.5	2.2	5.0	4.9	4.8	6.2	5.9	6.2	6.4
60	52	32	3		26	34	46	54	60

✓

31.47	30.95	29.7	28.4	28.4	28.3	28.2	26.7	27.5	26.8
1.23	1.75	3.0	4.3	4.3	4.4	4.5	6.0	5.2	5.9
59	43	19	3		23	26	35	47	62

✓

37.4	34.7	31.5	30.4	29.9	30.0	30.1	29.9	28.4	29.0	29.0	29.1
5.1	8.1	11.3	12.4	12.9	12.8	12.7	12.9	14.4	13.8	13.8	13.1
58	39	21	9	3		23	26	33	43	52	60

Sta + π - Elev.

942.75

rt.

12+74 $\pm$ Ent. Δ f. - 2 Ribbons

13+00

+45

+53

+60 West Gutter Avon St

+69 $\pm$ Avon

Lt

E

Rt⁵

34.0	31.8	30.3	35.8	31.2	30.9	31.1	31.0	30.6	30.73	31.1
4.8	5.0	6.5	9.0	11.6	11.9	11.7	11.8	12.2	12.02	11.7
75	66	45	28	10	3		23	36	42	56
									conc	

40.1	39.9	35.5	32.3	32.1	32.2	32.1	31.6	30.9	31.5	31.8
2.7	2.9	7.3	10.5	10.7	10.6	10.7	11.2	11.9	11.3	11.0
75	53	30	10	2		23	28	34	43	60

41.2	41.1	38.1	34.8	34.0	34.3	33.9	33.0	33.1	32.7
1.6	1.7	4.7	8.0	8.8	8.5	8.9	9.8	9.7	10.1
75	56	36	15	5		27	34	46	60

41.2	41.2	36.4	34.3	34.7	34.6	34.9	35.0	34.9
1.6	1.6	6.2	8.5	8.1	8.2	7.9	7.8	7.9
75	55	25	6		25	35	57	60

41.2	41.0	34.9	34.6	35.0	35.0	34.6	34.2
1.6	1.8	3.9	8.0	7.8	7.8	8.2	8.6
75	54	35	7		25	47	62

41.0	41.5	36.6	35.3	35.6	35.6	35.2	34.5
1.8	1.3	4.2	7.5	7.3	7.2	7.6	8.3
75	57	32	9		23	41	61

STA + π - ELEV

942.75

+78 MH. Rt. 29' 7.23 935.52

13+84 East Cutter Line

14+00

+50

BM 10.66 947.89 5.52 937.23 (937.23)

15+00 4 ENT Rt. Gravel/C. Rock

+12 4 ENT Lt 16" Conc.

Lt

E

Rt. 6

41.1 41.2 36.9 35.9 31.3 36.2 35.4 34.1
 1.7 1.6 3.9 6.9 6.5 6.6 7.4 8.7
 75 54 28 7 26 40 63

41.5 41.6 31.9 36.9 31.1 37.1 37.5 31.3 34.6
 1.3 1.2 2.9 5.9 5.7 5.7 5.3 5.5 6.2
 75 51 30 8 23 30 43 61

43.1 42.4 41.3 39.4 37.6 39.5 37.2 38.3 38.7 39.2
 40.3 0.4 1.5 3.4 3.2 3.3 3.6 4.5 4.1 3.6
 60 43 26 6 21 27 34 43 60

Top Hyd. S.W. Cor. Avon & C

44.0 43.7 42.6 41.5 41.8 41.6 40.8 40.1 39.8
 3.9 4.4 5.4 6.4 6.1 6.3 7.1 7.8 8.1
 60 40 23 5 21 32 49 60

44.28 43.73 42.5 41.9 42.2 42.1 41.0 40.3 40.0
 3.6 4.4 5.4 6.0 5.7 5.8 6.9 7.6 7.9
 61 43 19 6 22 36 51 58

STA	+	π	-	Elev
-----	---	-------	---	------

STA	+	π	-	Elev
-----	---	-------	---	------

947.89

STA	+	π	-	Elev
-----	---	-------	---	------

15+50 $\nless Ent Rt. C. Rock$

STA	+	π	-	Elev
-----	---	-------	---	------

16+00

STA	+	π	-	Elev
-----	---	-------	---	------

+50

STA	+	π	-	Elev
-----	---	-------	---	------

17+00

STA	+	π	-	Elev
-----	---	-------	---	------

+34 $\nless Ent Rt B.T$

STA	+	π	-	Elev
-----	---	-------	---	------

+79 $\nless Ent Lt. Gravel$

L1

E

R1 7

$\begin{matrix} 43.2 & 43.5 & 43.8 & 42.9 & 43.3 \\ 4.7 & 4.4 & 4.5 & 5.0 & 4.6 \\ 60 & 46 & 28 & 6 & \end{matrix}$
 $\begin{matrix} 43.2 & 42.9 & 43.3 & 43.6 \\ 4.7 & 5.0 & 4.6 & 4.4 \\ 21 & 29 & 43 & 50 \end{matrix}$

$\begin{matrix} 44.1 & 44.6 & 44.3 & 43.9 & 43.1 & 43.1 & 43.1 & 43.9 & 43.1 & 43.2 & 42.3 & 42.9 & 43.3 \\ 3.2 & 3.3 & 3.6 & 4.0 & 4.8 & 4.2 & 4.2 & 4.0 & 4.2 & 4.7 & 5.6 & 5.0 & 4.6 \\ 60 & 53 & 34 & 23 & 11 & 2 & & 10 & 21 & 27 & 31 & 38 & 62 \end{matrix}$

$\begin{matrix} 40.4 & 44.1 & 44.1 & 43.8 & 43.8 & 43.8 & 43.9 & 43.6 & 43.3 & 42.4 & 43.0 & 42.1 & 42.1 \\ 2.5 & 3.2 & 3.8 & 4.5 & 4.1 & 4.1 & 4.0 & 4.3 & 4.6 & 5.5 & 4.9 & 5.2 & 5.8 \\ 60 & 41 & 23 & 12 & 2 & & 10 & 21 & 26 & 31 & 37 & 49 & 60 \end{matrix}$

$\begin{matrix} 44.0 & 44.0 & 43.1 & 42.9 & 43.6 & 43.6 & 43.1 & 43.6 & 43.1 & 42.4 & 43.3 & 43.1 \\ 3.9 & 3.9 & 4.2 & 5.0 & 4.3 & 4.3 & 4.2 & 4.4 & 4.8 & 5.5 & 4.6 & 4.8 \\ 60 & 44 & 23 & 10 & 3 & & 9 & 20 & 26 & 31 & 43 & 60 \end{matrix}$

$\begin{matrix} 43.4 & 43.3 & 43.1 & 42.3 & 43.3 & 43.3 & 43.3 & 43.6 & 43.6 & 43.4 & 43.0 & 42.4 \\ 4.5 & 4.6 & 4.8 & 5.6 & 4.6 & 4.6 & 4.6 & 4.4 & 4.4 & 4.5 & 4.9 & 5.1 \\ 60 & 40 & 22 & 13 & 7 & 3 & & 8 & 20 & 37 & 52 & 60 \end{matrix}$

$\begin{matrix} 43.1 & 42.8 & 42.9 & 43.1 & 43.1 & 43.0 & 43.1 & 42.9 & 42.5 & 41.8 & 42.4 & 42.4 \\ 4.8 & 5.1 & 3.0 & 4.8 & 4.8 & 4.9 & 4.8 & 5.0 & 5.4 & 6.1 & 5.5 & 5.5 \\ 60 & 45 & 27 & 14 & 4 & & 8 & 18 & 24 & 29 & 39 & 60 \end{matrix}$

Sta + π - Elev.

94789

18+00

M.H. 17+95 Rt. 26' 4.68 943.21

BM 1.50 946.05 3.34 944.55 (944.56)

+50

+83 $\notin$ ENT. Rt. DIRT

19+00

+50

Lt

E

Rt

8

42.6	41.9	41.9	41.4	42.5	42.7	42.8	43.0	42.5	42.2	41.5	42.1	42.2	42.2
5.3	6.0	6.0	6.5	5.4	5.2	5.1	4.9	5.4	5.7	6.4	5.8	5.7	5.7
60	33	22	14	9	5		7	18	24	29	36	54	60

TOP Hyd Sta. 17+99 Lt

42.2	42.2	41.8	41.6	40.9	42.0	42.2	42.6	42.0	41.7	41.2	42.0	43.0
3.8	3.8	4.2	4.4	5.1	4.0	3.8	3.5	4.0	4.3	4.8	4.0	3.0
60	50	35	21	14	7		7	18	24	29	36	60

42.1	41.8	41.2	41.6	40.6	41.9	41.9	42.0	42.2	42.0	42.0	42.1
3.9	4.2	4.8	4.5	5.4	4.1	4.1	4.0	3.8	4.0	4.0	3.9
60	51	34	22	14	8	4		7	18	37	59

42.3	41.9	41.1	40.4	41.6	41.8	41.9	42.0	41.7	41.1	42.0	41.9
5.7	4.1	4.9	5.6	4.4	4.2	4.1	4.0	4.3	4.9	4.0	4.1
60	51	22	15	8	3		7	20	28	52	60

42.5	41.7	40.9	39.6	41.2	41.2	41.3	41.5	41.3	41.4	41.0	42.2	42.4
3.5	4.3	5.1	6.4	4.8	4.8	4.7	4.5	4.7	4.6	5.0	3.8	3.6
60	43	24	15	8	4		6	16	22	32	36	60

Sta	+	π	-	Elev
		946.05		

20+00 $\neq$ Ent Rt (Dirt)

+15

+50

+73 $\neq$ Ent Lt (Bit)

21+00 $\neq$ Ent Rt (Bit)

+34 Ent Lt Conc^{16'}, 6.53

+50

Lt

E

Rt

9

~~21.3 40.1 40.5 40.6 40.7 40.8 40.8 41.3 42.2
 4.7 5.4 5.5 5.4 5.3 5.2 5.2 4.7 3.8
 60 36 18 5 5 16 30 60~~

~~41.1 40.6 40.4 40.3 40.4 40.5 40.7 40.2 41.8 42.2 42.5
 4.9 5.4 5.6 5.7 5.6 5.5 5.3 5.8 4.2 3.8 3.5
 60 29 13 5 6 16 27 37 51 60~~

~~40.1 39.6 39.1 39.7 39.8 39.9 39.8 39.7 39.0 40.1 41.2
 5.9 6.2 6.9 6.3 6.2 6.1 6.2 6.3 7.0 5.9 4.8
 60 43 22 5 5 15 21 28 38 60~~

~~40.0 39.8 39.4 39.3 39.6 39.4 39.3 39.2 39.5 40.4 40.9
 6.0 6.2 6.6 6.7 6.5 6.4 6.7 6.8 7.5 5.6 5.1
 60 50 25 7 5 15 21 29 44 60~~

~~39.9 39.6 39.8 39.2 39.2 39.9 39.2 39.3 39.5
 6.1 6.4 7.2 7.0 6.8 6.8 7.1 6.8 6.7 6.5
 60 47 20 5 5 14 25 47 60~~

~~40.2 39.9 39.3 39.5 39.4 39.7 39.3 39.0 39.5 39.0 39.1
 5.8 7.0 7.7 7.5 7.4 7.3 7.7 8.0 8.5 8.0 7.3
 60 38 21 5 4 14 20 28 40 60~~

Sta + π - Elev

946.05

+81 $\nless$ Ent Pt (Gravel)

22+00

+16 $\nless$ Ent Lt Conc ^{16'} 6.89

B.M.

5.71

940.34

940.41

B.M.

0.34

40.75

940.41

+25 $\nless$ Ent Pt V.F.W Bit

+50

Lt

L

Rt 10

40.0	39.1	38.1	37.2	36.4	36.5	36.6	37.8	37.1	37.5
6.0	6.9	7.9	7.8	7.6	7.5	7.9	8.2	8.3	8.5
65	40	20	5		4	14	26	41	60

40.0	38.9	38.2	37.1	36.3	36.3	37.9	37.1	36.8	36.8
6.0	7.1	7.8	7.9	7.7	7.7	8.1	8.9	9.2	9.2
71	40	25	6		4	14	26	47	60

Top Hyd 22+40 Lt.

Top Hyd 22+40 Lt.

40.1	39.7	38.8	37.8	36.2	36.4	36.4	37.6	36.9	36.6
0.7	1.1	2.0	3.0	2.8	2.4	2.4	3.2	3.9	4.2
61	53	38	19	6		4	29	49	60

39.9	38.7	37.8	36.3	36.1	36.3	37.6	37.5	37.1	37.0
0.9	2.1	3.0	2.5	2.4	2.5	3.3	3.3	3.7	3.8
60	40	18	6		5	22	33	52	60

STA + π - Elev

940.75

23+00 $\nless Ent. Lt. Conc 16'$

+45

+64

24+00

+43 $\nless Ent. Rt. B. + \nless Ent. Lt. Conc$

+55

L+

±

R+ 11

^{39.4³} ^{38.8⁴} ^{38.4} ^{37.4} ^{37.9} ^{36.0} ^{37.6} ^{36.6} ^{36.6} ^{37.1} ^{36.1}
 1.32 1.9 2.4 3.4 2.9 2.8 3.2 4.2 4.2 4.1 4.1
 62 43 39 19 7 15 28 40 46 60
 Conc

^{39.1} ^{37.9} ^{37.0} ^{37.7} ^{37.6} ^{37.1} ^{37.5} ^{37.2} ^{36.9} ^{36.7} ^{36.6}
 1.7 2.9 3.8 3.1 3.2 3.1 3.3 3.6 3.9 4.1 4.2
 60 40 20 10 7 13 23 35 54 60

^{37.3} ^{37.0} ^{36.6} ^{37.4} ^{37.4} ^{37.5} ^{37.3} ^{36.4} ^{36.6} ^{36.6} ^{36.7} ^{36.7}
 3.5 3.8 4.0 3.4 3.4 3.3 3.5 4.4 4.0 4.2 4.14
 60 39 20 8 4 12 23 30 43 506

^{37.1} ^{37.1} ^{36.6} ^{36.9} ^{36.9} ^{37.0} ^{37.0} ^{36.8} ^{36.1} ^{36.0} ^{37.1} ^{36.6} ^{36.1}
 3.7 4.1 4.2 3.9 3.9 3.8 3.8 4.0 4.7 4.8 4.1 4.2 4.1
 60 27 20 15 8 3 12 20 22 34 52 60

^{37.5} ^{36.7⁰} ^{37.1} ^{36.6} ^{36.6} ^{36.5} ^{36.2} ^{36.3} ^{36.4}
 3.6 4.1 4.7 4.2 4.2 4.3 4.6 4.5 4.4
 60 34 19 8 12 25 41 60
 Conc.

^{37.9} ^{35.6} ^{35.0} ^{37.1} ^{37.1} ^{37.1} ^{36.3} ^{36.2} ^{35.3} ^{34.7}
 4.9 5.0 5.0 5.1 4.4 4.3 4.5 4.6 5.5 6.1
 62 42 32 18 8 11 20 36 60

STA + T - ELEV
940.75

24+74

25+00

+50 $\neq$ Ent Lt (Bit)

+72

+91

26+00 $\neq$ Ent Rt (Dir+)

Lt

4

Rt 12

~~35.6~~ ~~35.4~~ ~~35.2~~ ~~35.9~~ ~~35.2~~ ~~35.3~~ ~~36.1~~ ~~36.0~~ ~~34.1~~ ~~33.6~~ ~~33.0~~
 5.0 5.4 5.6 4.9 4.6 4.5 4.7 4.8 6.1 7.2 7.8
 68 29 20 15 9 11 17 23 39 55

~~35.4~~ ~~35.4~~ ~~35.1~~ ~~34.9~~ ~~35.5~~ ~~35.4~~ ~~36.0~~ ~~35.4~~ ~~35.1~~ ~~34.2~~ ~~33.2~~ ~~33.0~~ ~~32.6~~ ~~31.1~~
 5.4 5.4 5.7 5.9 5.3 5.0 4.8 5.0 5.1 6.6 7.6 7.8 8.2 9.1
 60 48 32 21 14 10 11 17 27 39 50 62 75

~~35.0~~ ~~34.9~~ ~~34.9~~ ~~35.0~~ ~~35.6~~ ~~35.6~~ ~~35.6~~ ~~35.1~~ ~~34.3~~ ~~32.4~~ ~~32.1~~ ~~30.2~~
 5.8 5.9 5.9 5.8 5.3 5.2 5.3 5.7 7.5 8.4 8.7 10.6
 60 47 28 17 10 11 17 27 41 51 75

~~35.0~~ ~~34.8~~ ~~34.6~~ ~~34.0~~ ~~35.4~~ ~~35.3~~ ~~35.6~~ ~~35.3~~ ~~34.8~~ ~~33.4~~ ~~32.8~~ ~~32.0~~ ~~30.9~~ ~~30.6~~
 5.8 6.0 6.3 6.8 5.4 5.5 5.3 5.5 6.0 7.2 8.0 8.8 9.9 10.3
 60 40 28 20 13 10 11 17 26 33 49 64 75

~~35.1~~ ~~34.7~~ ~~33.9~~ ~~34.9~~ ~~35.2~~ ~~35.6~~ ~~35.3~~ ~~34.1~~ ~~34.1~~ ~~33.9~~ ~~33.9~~
 5.7 6.1 6.9 5.9 5.6 5.3 5.5 6.1 6.7 6.9 6.9
 60 41 24 14 9 11 28 49 66 78

~~35.0~~ ~~34.7~~ ~~34.6~~ ~~34.0~~ ~~35.0~~ ~~35.2~~ ~~35.3~~ ~~35.3~~ ~~34.1~~ ~~33.6~~ ~~33.1~~ ~~33.2~~
 5.8 6.1 6.3 6.8 5.8 5.6 5.3 5.5 6.4 7.2 7.7 7.6
 60 44 29 23 13 9 10 26 43 63 82

Sta	+	π	-	Elev
		940.75		

BM	0.61	937.67	3.69	937.06	937.05
----	------	--------	------	--------	--------

+25 $\pm$ Ent Rt (Bit)

+50

27+00

+09 $\pm$ Ent Lt (Canc)

+15 $\pm$ Ent Rt (B.t)

Lt

- E -

Pt

13

TOP Hyd STA. 26+43 Lt.

35.1	35.1	35.0	34.8	35.2	35.0	35.2	34.9	34.2	34.1	34.2
26	2.6	2.7	2.9	2.5	2.3	2.5	2.8	3.5	3.6	3.5
58	45	30	17	10		11	19	25	42	64

35.0	35.1	34.8	34.0	34.4	34.9	35.2	34.9	35.2	34.6	35.0	35.6
2.7	2.6	2.9	3.7	3.3	2.8	2.5	2.8	2.5	2.9	2.1	2.1
65	48	32	24	20	15	15	20	32	49	61	

35.2	35.0	34.5	34.8	34.2	34.2	34.1	34.7	35.1	34.6	35.0	35.4
2.5	2.7	3.2	2.9	3.5	3.5	3.6	3.0	2.6	3.1	2.7	2.3
55	43	30	15	15		15	15	22	31	40	60

7F. T.C.

35.12	35.08	34.91	34.6	34.1	34.1
255	261	276	313	36	3.6
53	46	31	21	12	

Cone

35.1	35.0	35.0	34.5	34.0	34.0	33.9	34.2	34.6	34.9
26	2.7	2.9	3.2	3.7	3.7	3.8	3.5	3.1	2.8
52	44	32	20	12		15	20	40	60

STA + T - Elev

937.67

+50

+95 @ Ent Lt Bit

28+00

+50

+87 @ Ent Rt Diet

29+00

Lt

- E -

Rt

14

3.9 3.5 3.2 3.9 3.2 3.2 3.3 3.9 3.2 3.2 3.2
2.2 2.7 5.5 3.8 4.3 4.3 4.4 3.8 3.3 3.3 5.0
60 46 27 15 15 15 15 29 41 60
T.C.

3.13 3.18 3.3 3.2 3.2 3.2 3.2 3.2 3.2 3.2 3.2
3.4 2.9 3.4 4.2 5.4 5.8 5.5 4.9 4.5 4.0 3.7 3.3
58 62 47 29 15 15 15 20 31 44 56
T.C.

3.7 3.2 3.2 3.2 3.2 3.2 3.2 3.2 3.2 3.2 3.2
3.0 3.5 4.2 5.5 5.4 5.6 5.1 4.7 4.0 3.7
60 49 30 15 15 15 20 30 44
T.C.

3.18 3.1 3.0 3.2 3.2 3.2 3.2 3.2 3.2 3.2 3.2
2.9 4.0 3.7 6.5 7.1 7.1 7.4 6.9 6.5 5.4 4.8
60 50 20 15 15 15 15 20 33 60
T.C.

3.13 3.1 3.2 3.2 3.2 3.2 3.2 3.2 3.2 3.2 3.2
3.2 4.1 5.2 7.1 8.0 8.6 8.7 8.7 7.8 6.7 5.3
66 44 29 20 16 16 15 23 46 60
T.C.

3.1 3.1 3.1 3.0 3.2 3.2 3.2 3.2 3.2 3.2 3.2
3.9 4.6 5.8 7.7 8.5 9.0 9.1 9.3 8.7 8.2 6.1 5.3 5.1
60 45 29 20 16 16 15 15 20 33 48 60
T.C.

STA + π - Elev.

937.67

+20 4 Ent Lt Gravel

+37

+85

+88 Ent Rt. Dirt

30+00

BM

12.67 925.00

924.97

4

E

Rt 15

34.2	32.4	31.3	29.6	27.9	27.8	27.6	27	29.0	31.2	32.4	32.7
8.5	4.9	6.4	8.1	9.9	9.9	10.1	9.5	8.7	6.5	4.9	5.0
75	60	46	32	16		17	17	22	29	43	60
							TC				

34.9	33.7	32.1	29.9	27.7	27.1	27.1	26.8	27.5	29.8	31.7	31.9	31.9
28	40	5.6	7.8	10.0	10.2	10.6	10.9	10.2	8.9	6.0	5.8	5.8
75	60	37	27	17	17		19	19	26	35	49	60
			TC					TC				

30.0	29.8	29.6	25.4	24.8	24.6	24.7	25.2	27.2	27.0	26.9
7.7	7.9	8.1	12.3	12.9	12.9	13.0	12.5	10.5	10.7	10.8
65	50	37	22	22		22	22	29	46	60
			TC				TC			

Same

24.7	24.5	25.1	25.2
13.0	13.2	12.6	12.5
22	36	53	

28.8	29.0	28.4	24.6	23.9	24.1	24.1	24.9	24.9
8.9	8.7	9.3	13.1	13.8	13.6	13.6	12.8	12.8
68	46	34	22	22		23	41	60
			TC					

TOP HYD N.E.C. & DAIR E.C

STA

+

π

-

Elev.

Co Rd "C"

62-623-10

Sewer Profile N
or Lt.

Sta + π - Elev

BM 3.33 940.37

937.04

25-~~42~~

4.8 35.6

17 5.1 35.3

21 6.3 34.1

27 5.8 34.6

59 5.7 34.7

89 5.2 35.2

112 5.0 35.4

132 4.7 35.7

147 4.5 35.9

20.9 5.4 35.0

25 4.41 936- 36.0 ✓

23-71. CR 4-5-11

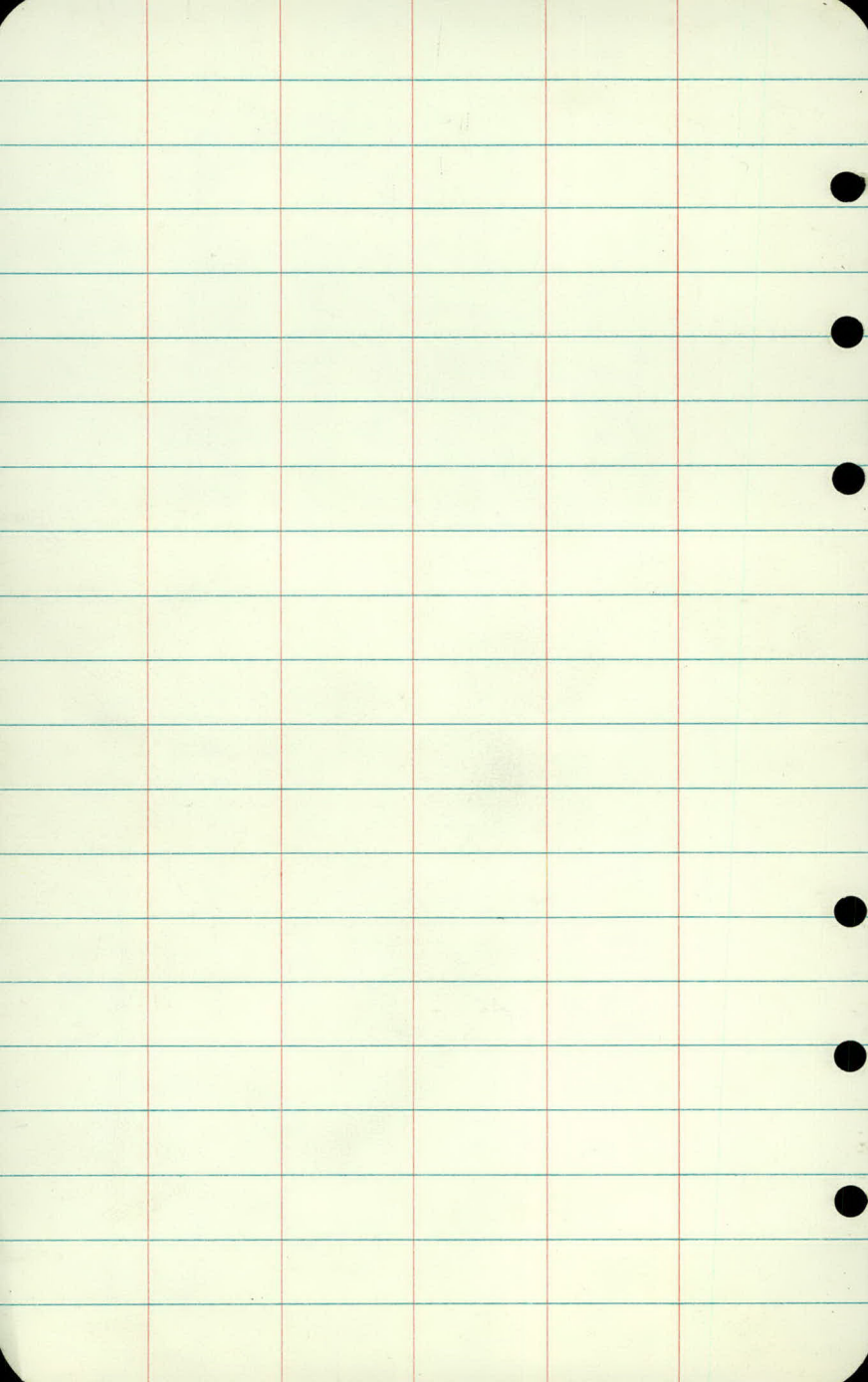
County Road "C" Oxford to Dale

- BM¹ Elev. 895.25¹⁹ ✓ ²³ ^{Settling} Top Hyd N.E. Corner, Oxford + "C"
- BM² Elev. 897.71 ✓ Top Hyd on Victoria Between "C" + RR
- BM³ Elev. 905.53 ✓ Top S.E. Corner NE Pier Crash Rail ^{Bridge} 625
- BM⁴ Elev. 926.16 ✓ B.M. Plate S.E. Wing Bridge No 625
- BM⁵ Elev. 924.97 ✓ Top Hyd. N.E. Corner Dale + Co. Rd. "C"
- BM⁶ Elev. 902.04 ✓ Top Hyd. N.E. Corner Heinel Drive + "C"
- BM⁷ Elev. 914.16 ✓ Top Hyd. S.W. Corner Fisk + Co. Rd "C"
- BM⁸ Elev. 932.27 ✓ Top Hyd. S.W. Corner Avon + Co Rd "C"
- BM⁹ Elev. ^x 944.57 ✓ ¹⁷⁺⁷⁹ Top Hyd. by House # 743 County Rd "C"
- BM¹⁰ Elev. ^x 940.40 ✓ ²²⁺⁴⁰ Top Hyd by House # 701 County Rd "C"
- BM¹¹ Elev. 937.04 ✓ ²⁶⁺⁴³ Top Hyd by House # 667 County Rd "C"
- BM¹² Elev. 924.97 ✓ Top Hyd N.E. Corner Dale St + Co Rd "C"
- BM¹³ Elev. 940.37 ✓ ²⁰⁺ Roseville BM #37 By House # 720

FK
GA

March 22, 1972

Top Hyd by H₂ # 667 Co Rd "C"



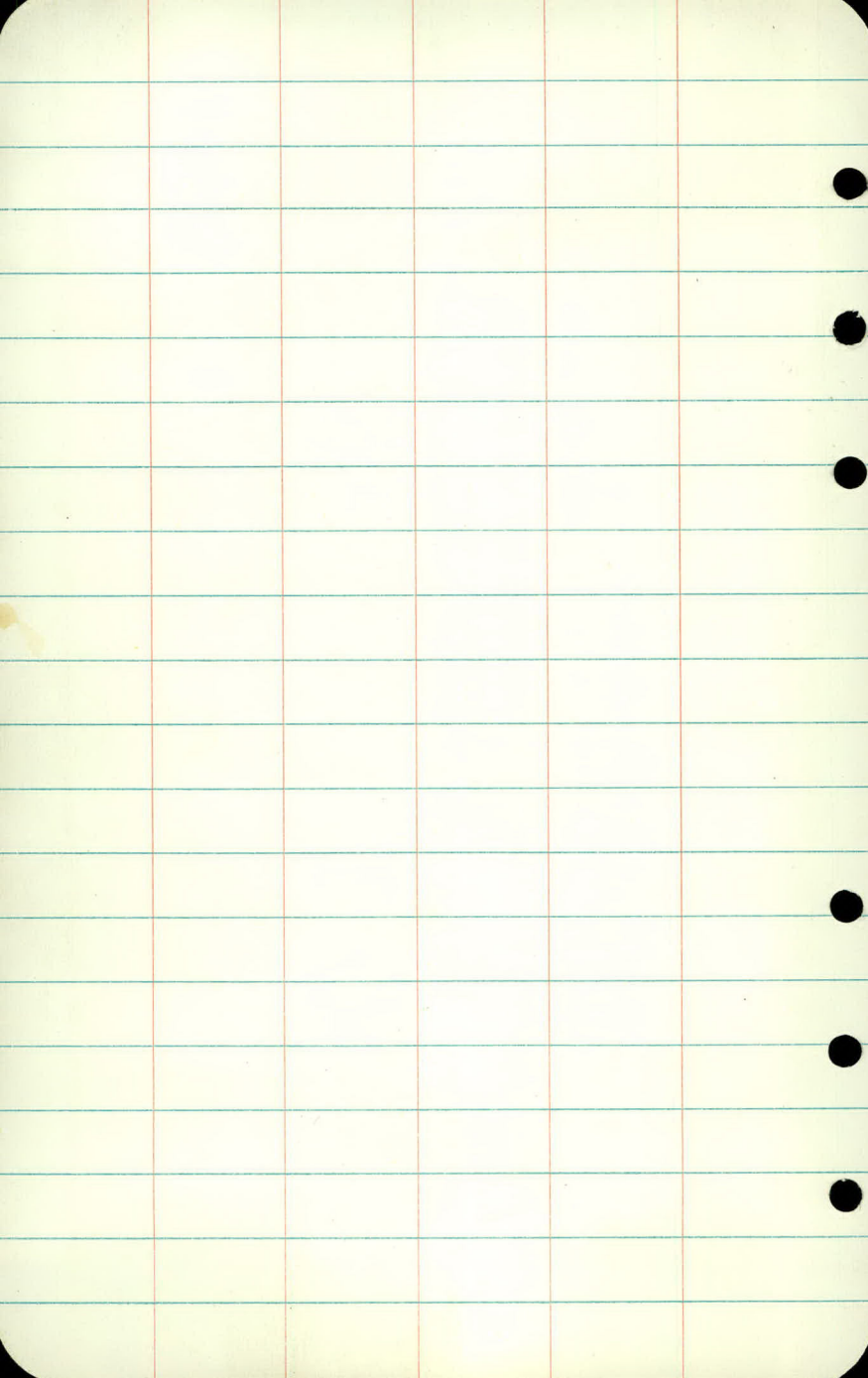
August 19, 1970

1

COUNTY ROAD "C"

Oxford to Dale

PLAN SURVEY



August 19, 1970

2

Alinement

Sta Point ΔL ΔR

66+58.58 P.T.

$$\Delta = 34^{\circ} 28' 30''$$

$$D = 6$$

$$D = 6^{\circ}$$

63+80.29 P.I.

$$T = 296.29'$$

$$L = 574.58'$$

$$R = 954.93$$

60+84.00 PC

PK
CP
CM
BP

August 19, 1970

3

2x2 hub



99.53

54.93

3 Disk

2x2 hub



46.38

2x2 hub



112.00

std



165.85'

N.W.
Cor.



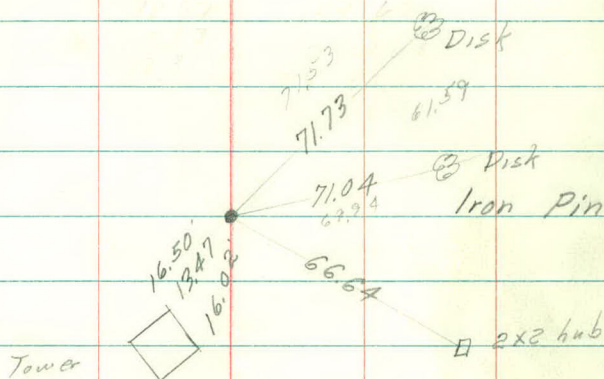
Chimney

Backstop

Sta	Point	ΔL	ΔR	
+48.23	P.T.	$28^{\circ}03'$		
74		$25^{\circ}38.3'$		
+50		$23^{\circ}08.3'$		
73		$20^{\circ}38.3'$	$\Delta = 56^{\circ}06'$	
+50		$18^{\circ}08.3'$	$\frac{1}{2}\Delta = 28^{\circ}03'$	
72		$15^{\circ}38.3'$	$D = 10'$	
71+92.52	P.I.		$T = 305.29'$	
+50		$13^{\circ}08.3'$	$L = 561.00'$	
71		$10^{\circ}38.3'$	$R = 572.96'$	
+50		$8^{\circ}08.3'$		
70		$5^{\circ}38.3'$		
+50		$3^{\circ}08.3'$		
69		$0^{\circ}38.3'$		
68+87.23	P.C.	$0^{\circ}00'$		
67+89.74	P.O.T.	$\nsubseteq$ Railroad Track		

August 19, 1970

4

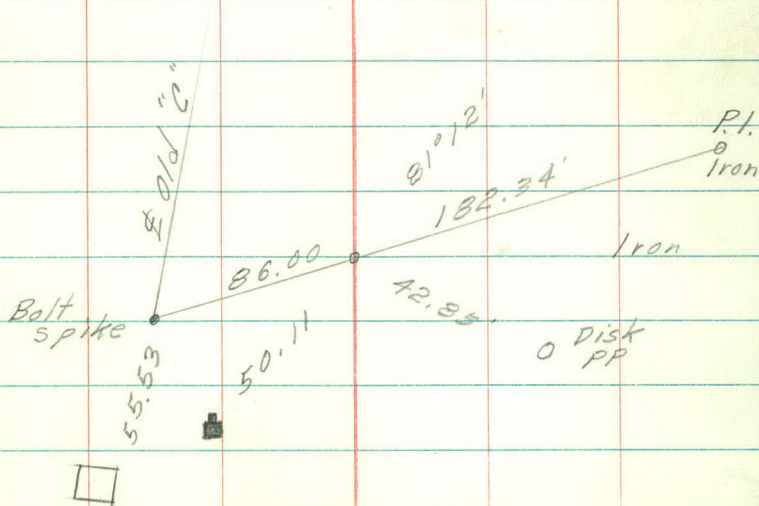
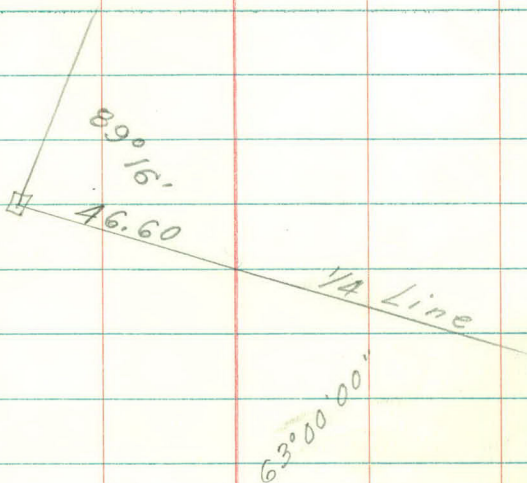


80+21.20 P.O.T. Tie to Section Line

75+71.84 P.O.T. $\pm$ Victoria

August 19, 1970

5



Sta	Point	ΔL	ΔR
-----	-------	------------	------------

8+00.03	P.T.		
---------	------	--	--

Equation =			
------------	--	--	--

+47.82	P.T.		
--------	------	--	--

		13° 52'	
--	--	---------	--

B3		12° 26'	
----	--	---------	--

+50		10° 56'	
-----	--	---------	--

B2		9° 26'	$\Delta = 27° 44'$
----	--	--------	--------------------

+50		7° 56'	$D = 6°$
-----	--	--------	----------

B1+21.33			$T = 235.37$
----------	--	--	--------------

B1		6° 26'	$L = 462.22$
----	--	--------	--------------

+50		4° 56'	$R = 954.93$
-----	--	--------	--------------

B0		3° 26'	
----	--	--------	--

+50		1° 56'	
-----	--	--------	--

79		0° 26'	
----	--	--------	--

7B+85.60	P.C.		
----------	------	--	--

		0° 00'	
--	--	--------	--

August 19, 1970

6



$$\begin{array}{r} 5764.30 \\ - 235.73 \\ \hline 5528.57 \end{array}$$

Iron

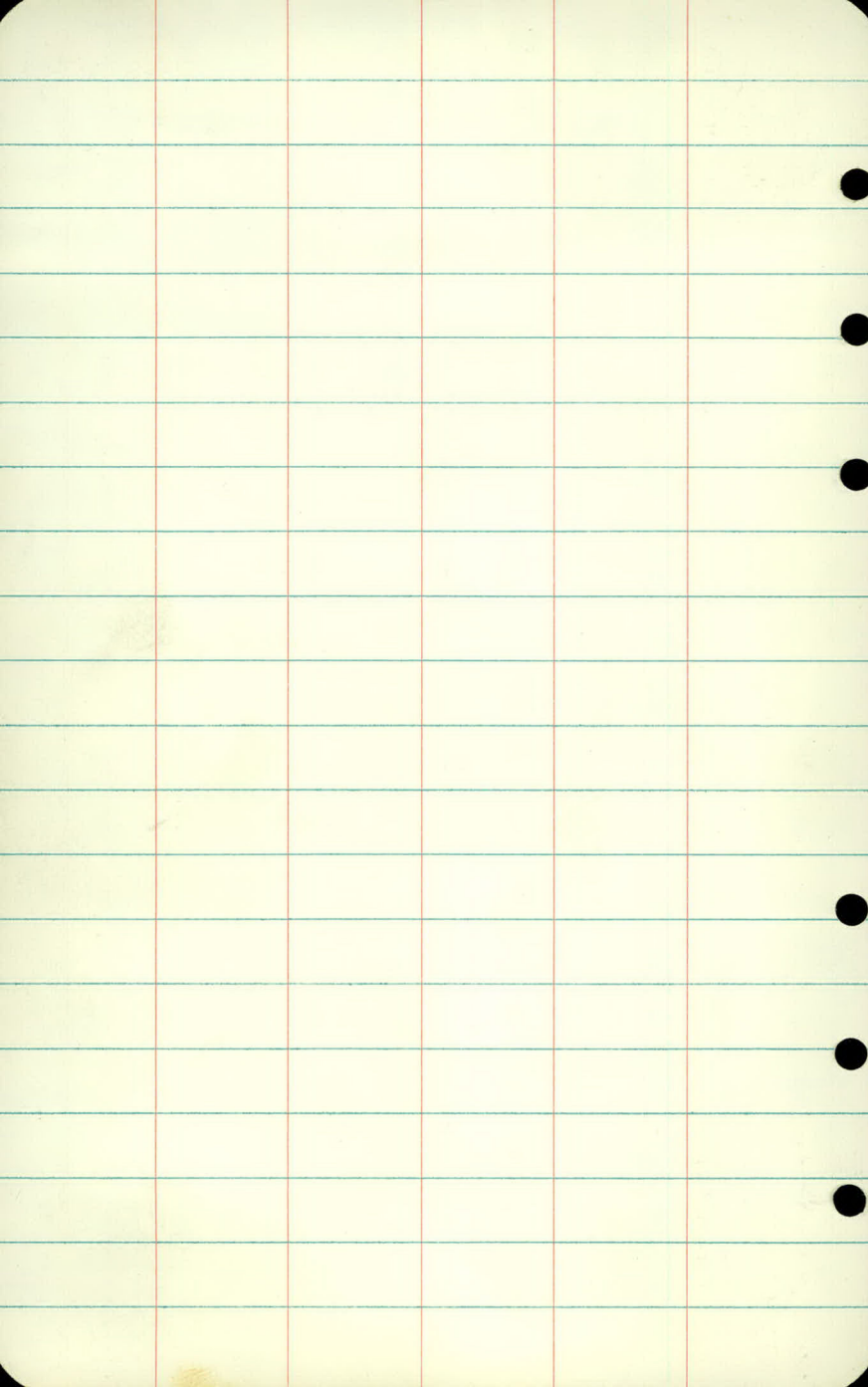
Sta Point Δ Lt. Δ Rt

P.O.T.

P.O.T.



Broken off
C. I. Monument



Topography

14
13 14

+21 chd
28

+21 ER
14

+17 PP
29

+107 POR
28

+19 TF ✓
29

22

+105 BR
54

Road
11

+93 ER
66

+81 MH
12

+78 POR
33

+67 BR
16

+65 R.T. Tower
Road
16 10

3000
+42 R.T. Tower
54

81

Road
19 10

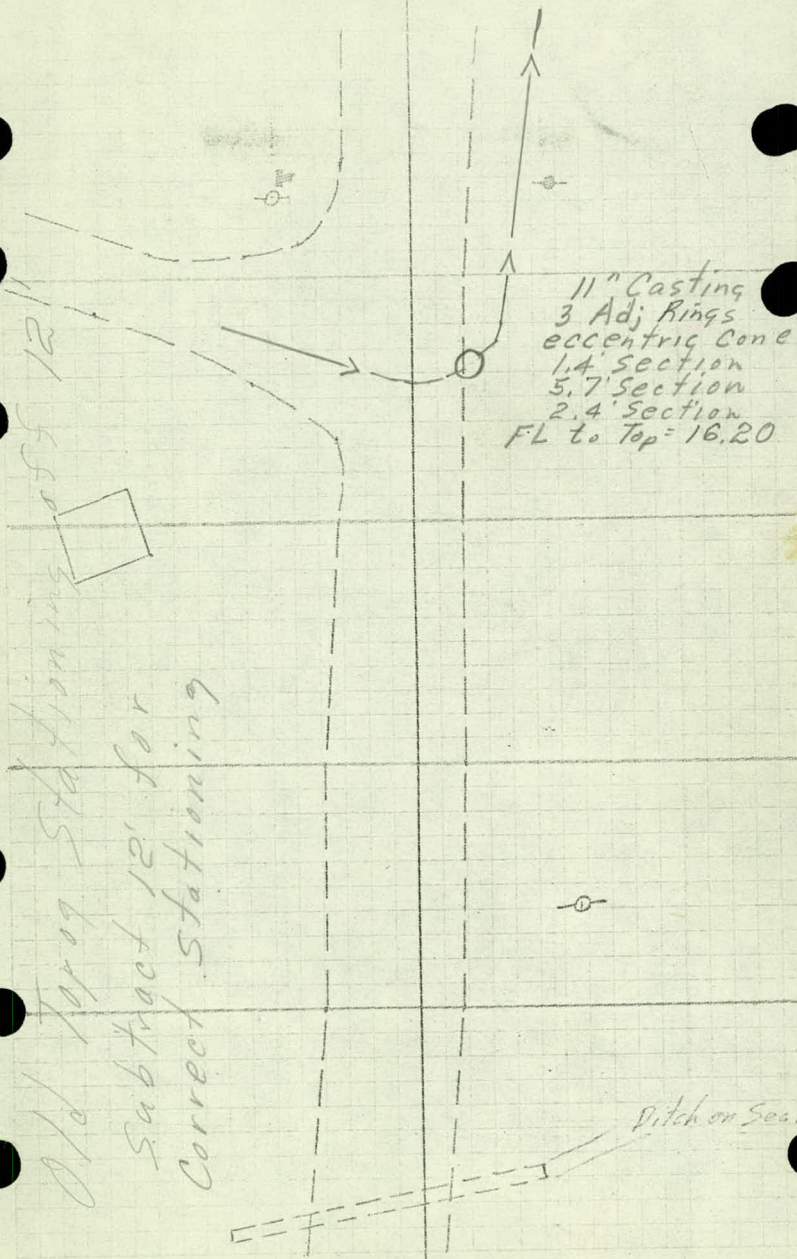
+71 PP ✓
33

Road
20 8

80

+104 NE 36' CM
40

+17 NE 36' CM
25



11" Casting
3 Adj Rings
eccentric Cone
1.4' Section
5.7' Section
2.4' Section
FL to Top = 16.20

Old Topog Stationing of 55 12'
Subtract 12' for
Correct Stationing

Ditch on Sec Line

Hand
5 24

35

+47 2nd Cor
65

+48 E.L. 18" CM
29

+49 MH
58

+44 ER
24

+06 MH
36

9

+07 W.L. 15' 20' 20'
16 Calc

+85 3"
75

+34 BR
30

+93 SD
29

+88 WE 18" CM
28

+95 41"
42

+88 2 10' Conc
Int 60

84 15 PP
~~19~~

+03 ER
44

+44 POR
26

+83 ER
22

24

Road
6 21

+65 TP
35

+13 Road
7 20

+28 E.L. 18" CM
36

+43 Cor. Ent
51

+42 45' Cor. Ent
51

+27 Cor. Ent
59-60

Road
7 20

+05 E. Ent TP
C-Ent

+81 NW. Cor. Ent
54

+65 Cor. Ent
53

+62 B. Spine
41

+75 E. Spine
41

+37 E. Spine
41

+34 W.L. 18" CM
37

+07 B. Spine
40

Road
10 17

+05 MH
38

+03 TP
31

+00 E.L. 18" CM
36

83

82+93

+81 WE 12" x 18" CM
36

FX
FS
FV
DO

Oct. 10, 1966
Oct. 23, 1966

54
37

Subtract 12 feet from
Red for correct stationing

11" Casting
4 Adj. Rings
eccentric Cone
1' Section

SP
Plugged

C. Rock

5'

11" Casting
2 Adj. Rings
ecc. Cone
2' section
36" RCP



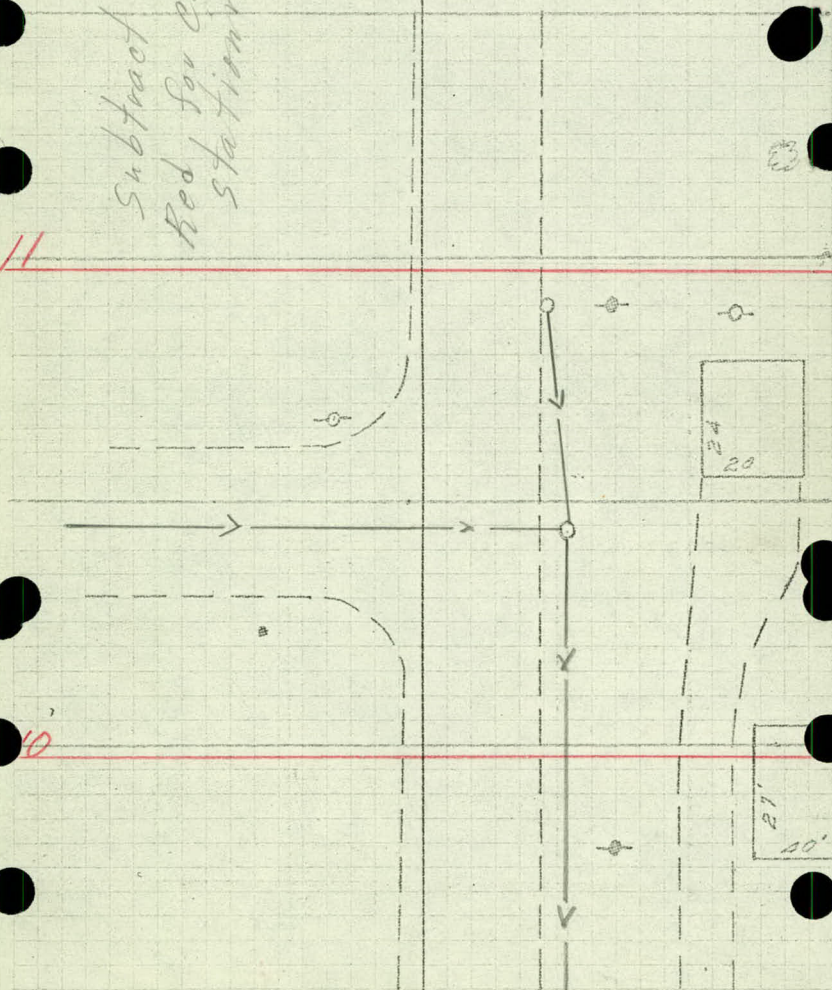
Oct. 28, 1966

53
78

Subtract 12' from
Red, for correct
stationing

11

10



+47

Road
2 25

11 +24 6" Cedar
74

10 +91 PP
65

10 +93 TP
39

+98 MH
26

+70 14
PP

+82 ER
3

+58 NW Cor Garage
58

+64 BR
20

Road
3 24

+47

+47 MH
30
+34 new

+33 ER
23

+16 MH
10

+66 BR
4

+26 GG
33

+80 NW Cor. Ho
68

+82 TP
40

35

5 24

KP
RG
DK

9 FEB 1972
CLEAR
2°

1.

COUNTY RD. "C"

Oxford to Dale

topography

+50

LT

~~L~~

RT

+34 MH
+47 30

W. Dept.
M.H.
+16 10

10 + 00

+50

+69 TP
40

+21 SW Cor. Ho
74

9 + 00

+06 MH
36 ♀ Fisk St.

+50

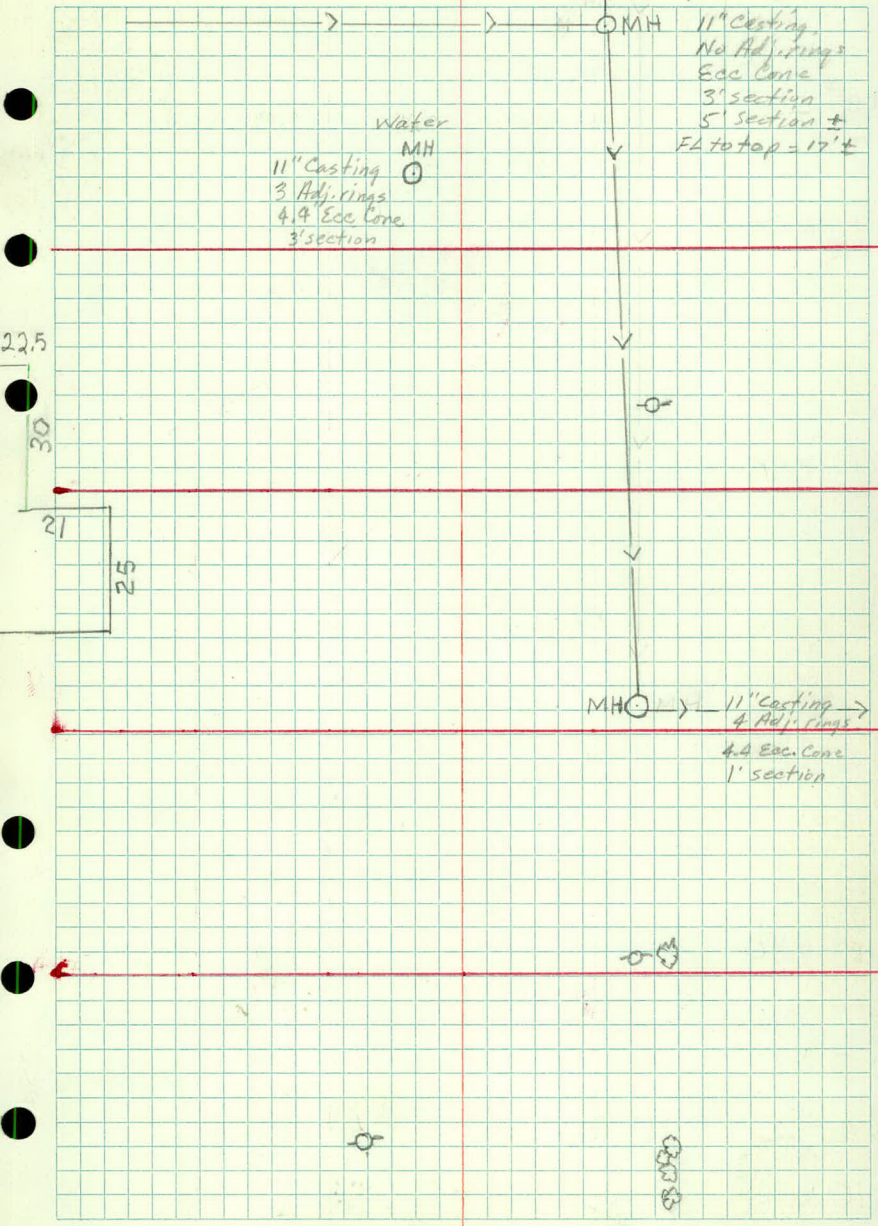
+55 3' Birch
44
+54 TP
36

+16 PP
20

8 + 00

+12 Bush
43
+05 Bush
43
+15 Bush
42
+09 Bush
43

LT E R



13+00

LT

E

RT

+50

+33 $\frac{PP}{17}$ +26 $\frac{TP}{40}$

12+00

+01 $\frac{SW Cor Ho}{74}$ +59 $\frac{Fe Cor}{44-}$

+50

11+00

+93 $\frac{SW Cor Ho}{75}$ +82 $\frac{PP}{46}$ +93 $\frac{Cor Fe}{44-75}$ +74 $\frac{TP}{65}$ +81 $\frac{MH}{27}$ +58 $\frac{LP}{18}$

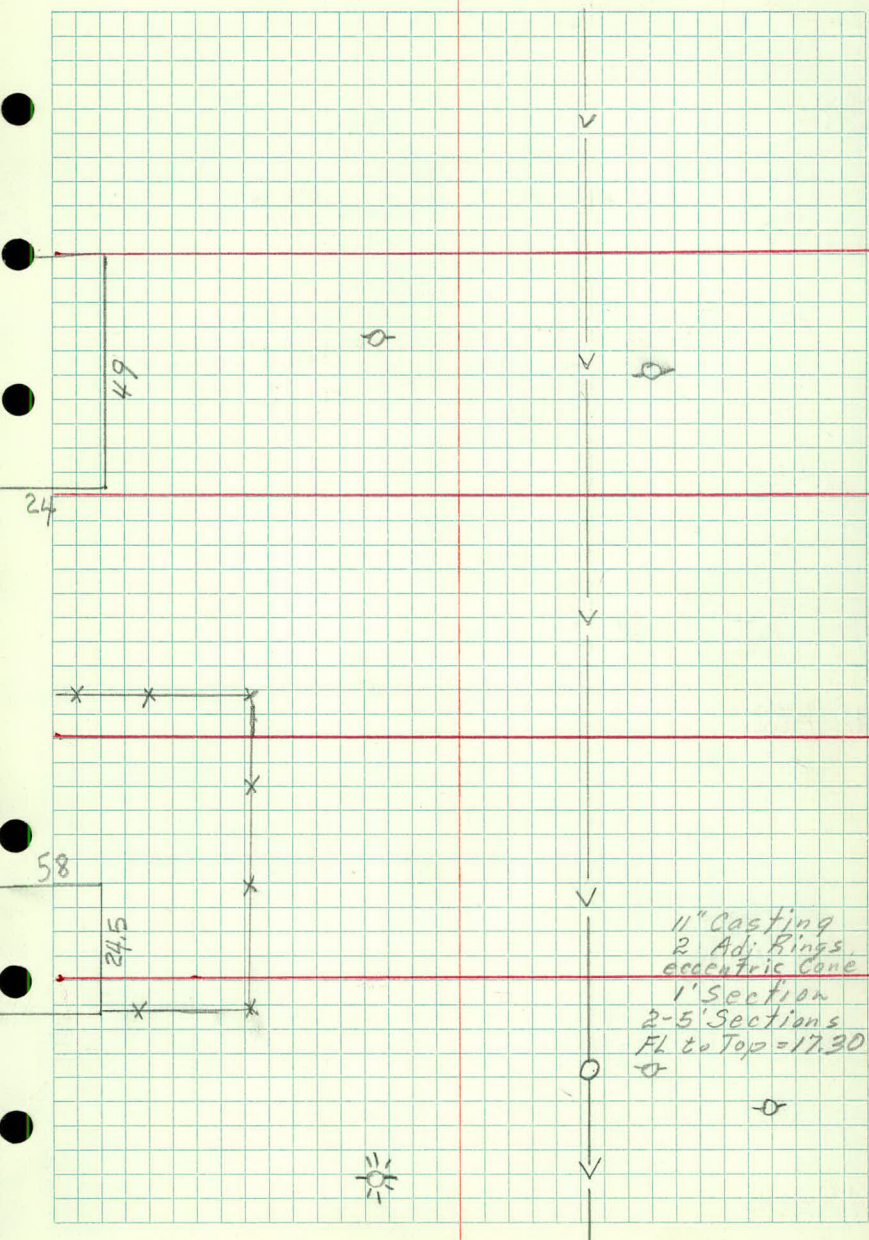
10+50

LT

E

RT

3.



+50

LT

£

RT

+30 $\frac{PP}{19}$

+33 $\frac{PP}{38}$

+31 FE Cor
44 to

+19 $\frac{1"P}{43}$

15+00

+91 SEEDLING
37

+81 Seedling
36

+74 SEEDLING
36

+71 $\frac{4" M}{44}$

+68 SEEDLING
36

+57 SW Cor Ho
75

+59 Seedling
37

+50

+41 $\frac{2"P}{47}$

+41 $\frac{PP}{39}$

+46 FE Cor
44 to

+02 $\frac{1"P}{46}$

14+00

+91 $\frac{PP}{17}$

+7A $\frac{MH}{29}$

+51 $\frac{Hyd}{46}$

+50

+41 $\frac{2"P}{47}$

+31 $\frac{2"P}{46}$

+20 $\frac{PP}{40}$

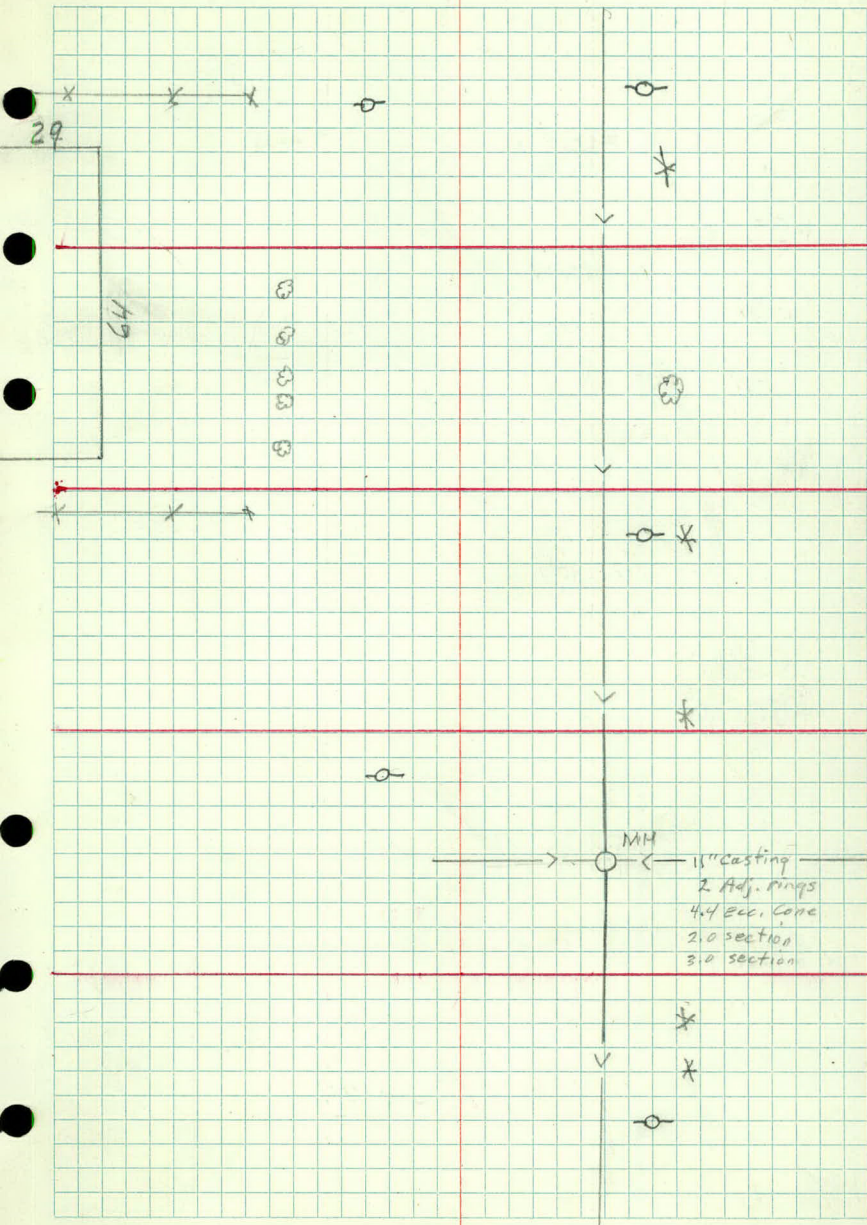
13+00

LT

E

RT

4.



18+00

LT

E

RT

+91 $\frac{18''E}{25}$ +68 $\frac{14''E}{24}$ +97 $\frac{PP}{37}$ +96 L LAC HEDGE
36-+94 $\frac{MH}{26}$

+50

+49 $\frac{18''E}{37}$ +19 $\frac{6''P}{21}$ +15 $\frac{3''P}{26}$ +46 $\frac{14''E}{38}$ +11 $\frac{10''E}{31}$ +20 $\frac{12''E}{38}$

17+00

+00 FE Cor (WOOD RAIL)
33.5 to+59 $\frac{PP}{38}$

+50

+31 E DRIVE

+22 $\frac{3''P}{47}$ +26 SW Cor Ho.
74+18 $\frac{PP}{18}$ +06 $\frac{1''P}{43}$ +00 NE Cor Ho
89

16+00

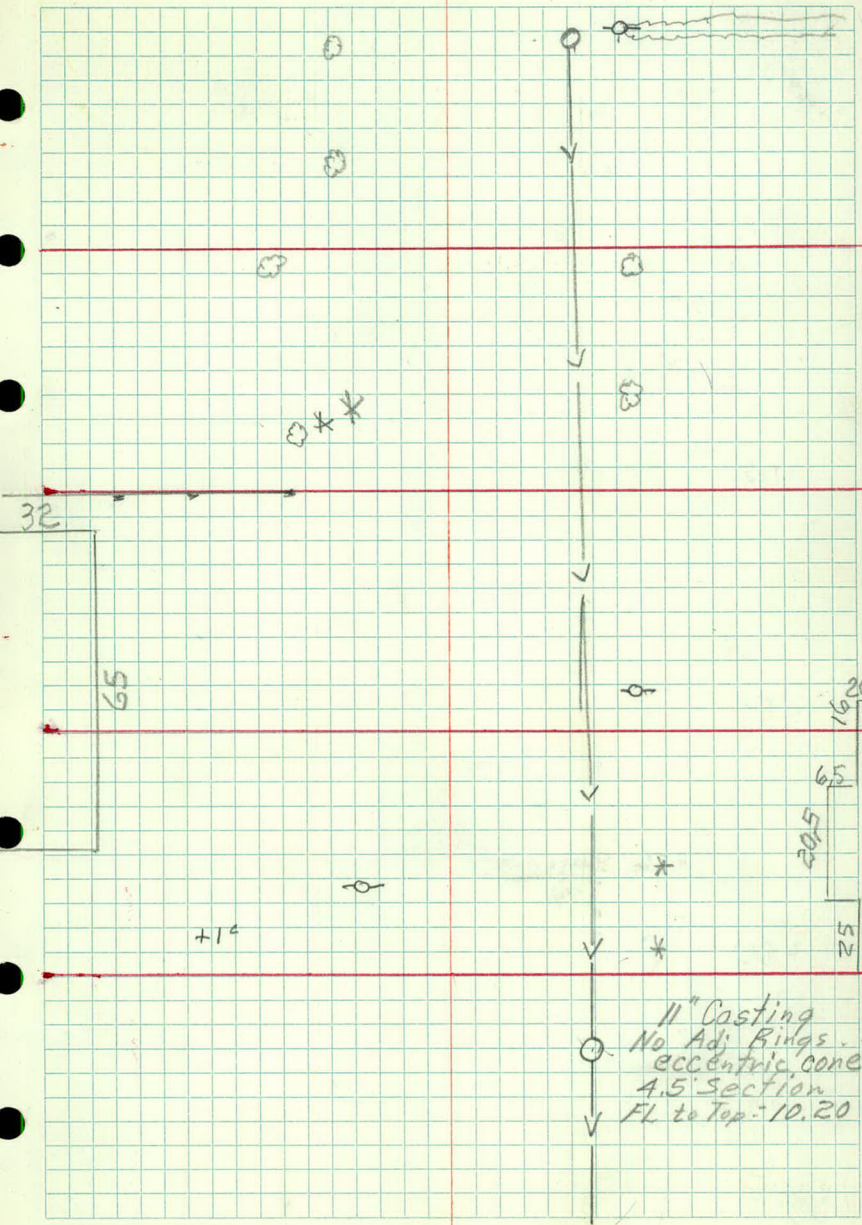
+85 $\frac{MH}{29}$

15+50

LT

£

RT



11" Casting
 No Adj. Rings.
 eccentric cone
 4.5" section
 FL to Top: 10.20

+50

LT

E

RT

+46 SW Cor Parking Lot
42 to+19 $\frac{PP}{36}$ +02 $\frac{PP}{22}$ +19 $\frac{L/LMS}{36-}$

20+00

+00 $\frac{10'0''}{31}$ ✓+90 BUSH
36+98 $\frac{10'0''}{36}$ +84 BUSH
36

36

+75 $\frac{16'0''}{36}$ +70 BUSH
36+77 BUSH
36+67 $\frac{8'0''}{36}$

+55 BUSH

+61 BUSH
36+61 $\frac{24'0''}{31}$ ✓+51 BUSH
37

+50

PP

+29 $\frac{22}{22}$ +23 $\frac{10'0''}{26}$ +21 $\frac{PP}{34}$

19+00

+02 $\frac{L/LAC}{37}$ +92 $\frac{18'E}{36}$ +77 $\frac{1'ASH}{9}$ +69 BUSH
39

+50

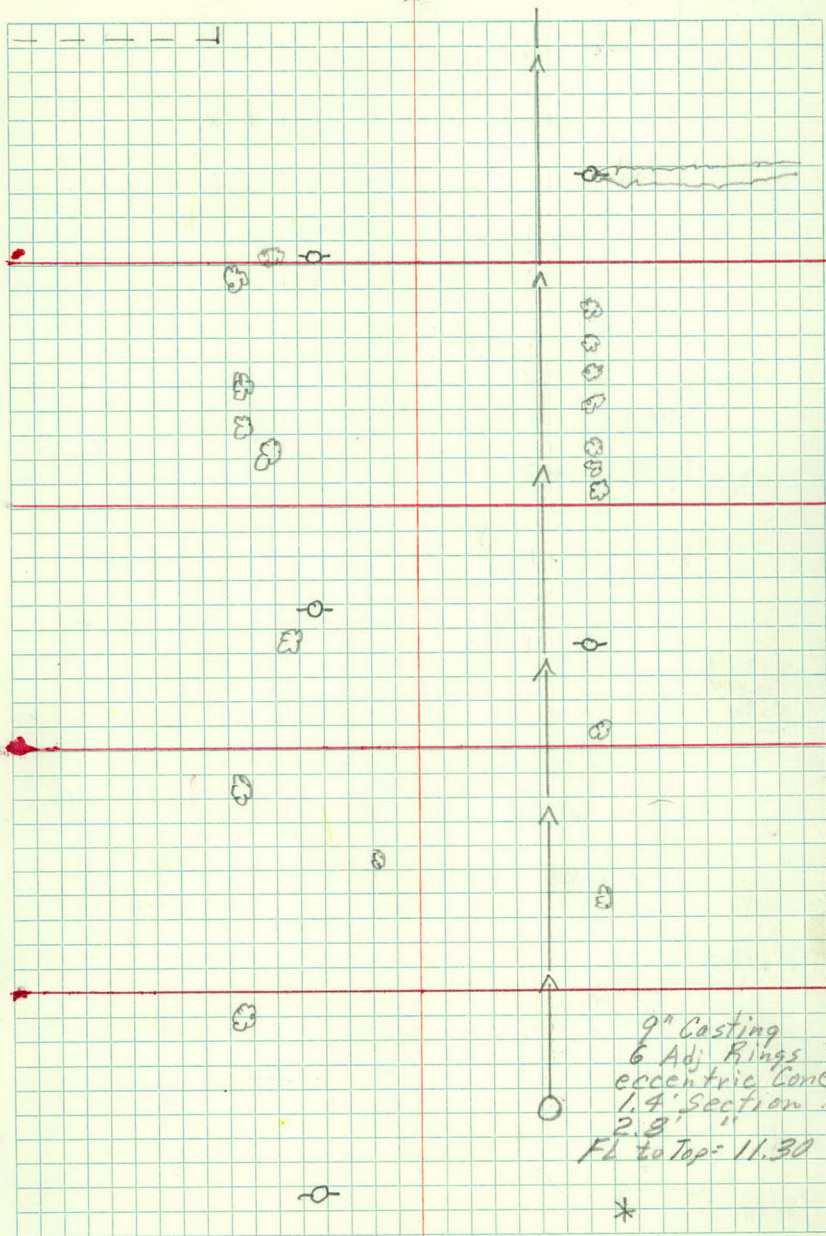
+45 $\frac{16'0''}{37}$ +26 $\frac{MH}{27}$ 18+00 +09 $\frac{PP}{21}$ +05 $\frac{4'P}{42}$

LT

E

RT

6.



23+00

LT

£

RT

+95 SW Cor Ho
83

+50

+14 £ 16' CONC ENT

+04 SW Cor Ho
85

22+00

+02 PP
23

+02 PP
59

+67 PP
35

+50

+26 SW Cor Ho 160.5 +36 £ 16' CONC ENT
41

+05 S.E. Cor Parking Lot
41

+05 SW Cor FE
41

+19 3" COT
37

21+00

+94 SE Cor Ho
83

+95 1" ELM
28

+96 L. lac
40

+73 £ 20' BIT ENT

+75 MH
25

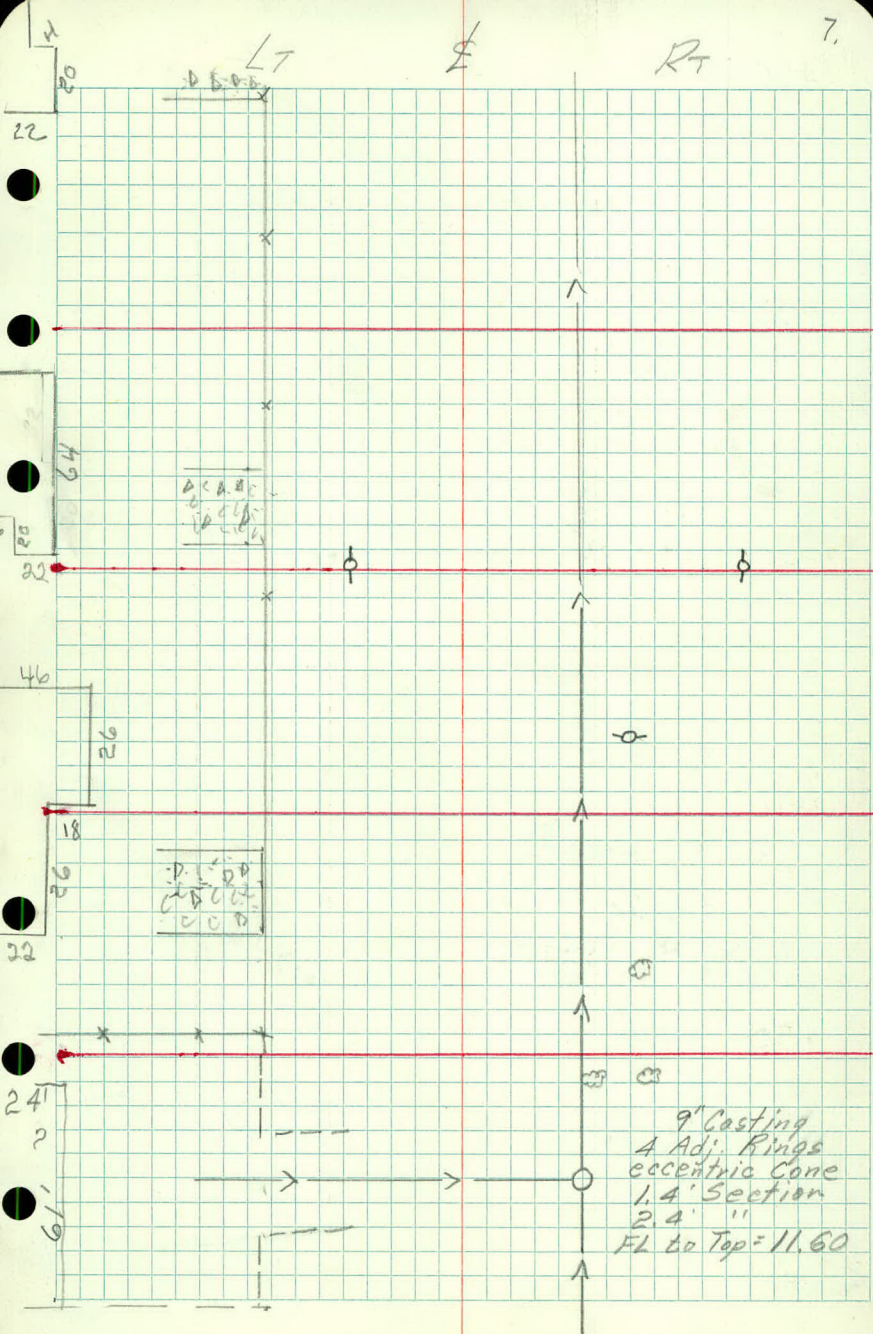
20+50

+46 SW Cor Parking Lot
42 to

R_T

£

LT



+50

LT

2

RT

25+00

+55 $\frac{PP}{28}$
+51 3"ASH
40
+51 1"ASH
43
+50

+69 Bush
31

+66 3"ASH
33

+27 $\frac{PP}{33}$
+21 Bush
34

24+00

+77 SW Cont'd
+66 $\frac{PP}{26}$ 89
+64 SE Cor Fe
39

+56 $\frac{PP}{33}$

+50

+54 $\frac{MH}{20}$

+22 Two Ash
44

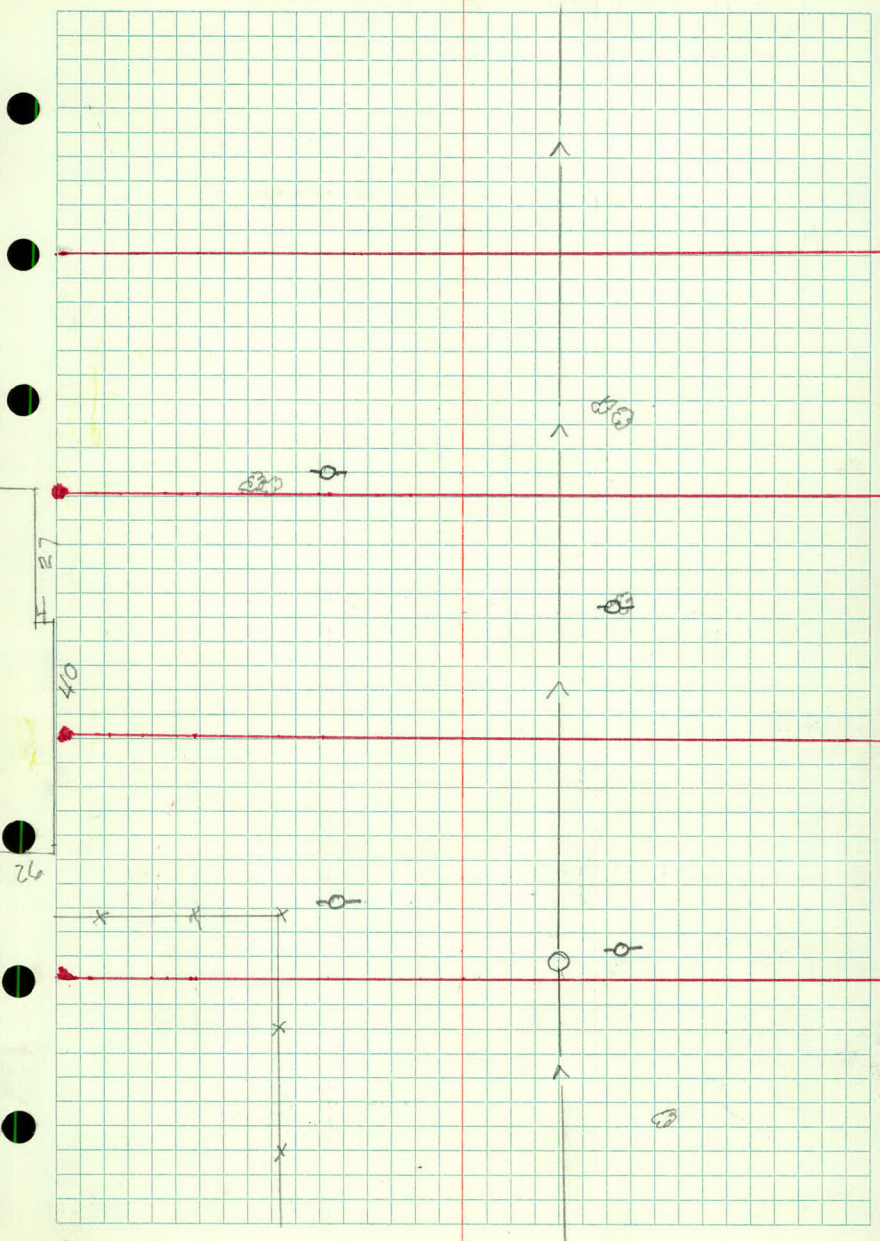
23+00

LT

$\frac{1}{2}$

R₇

8.



28+00

LT

L

RT

+50

$$+61 \text{ N.E. Cor Ho}$$

$$+51 \frac{PP}{31} \quad 84$$

$$+42 \text{ SW Cor Ho}$$

$$110$$

27+00

$$+00 \frac{PP}{28}$$

$$+94 \frac{PP}{31}$$

$$+88 \text{ N.E. Cor Ho}$$

$$81$$

$$+65 \frac{5''M}{42}$$

+50

+44 END HEDGE

+14 14''M +37 10'E 32

42 +19 HEDGE

$$+10 \frac{PP}{27} \quad 34$$

26+00

$$+87 \frac{M17}{19}$$

$$+65 \text{ Begin hedge}$$

$$32$$

$$+65 \frac{PP}{32}$$

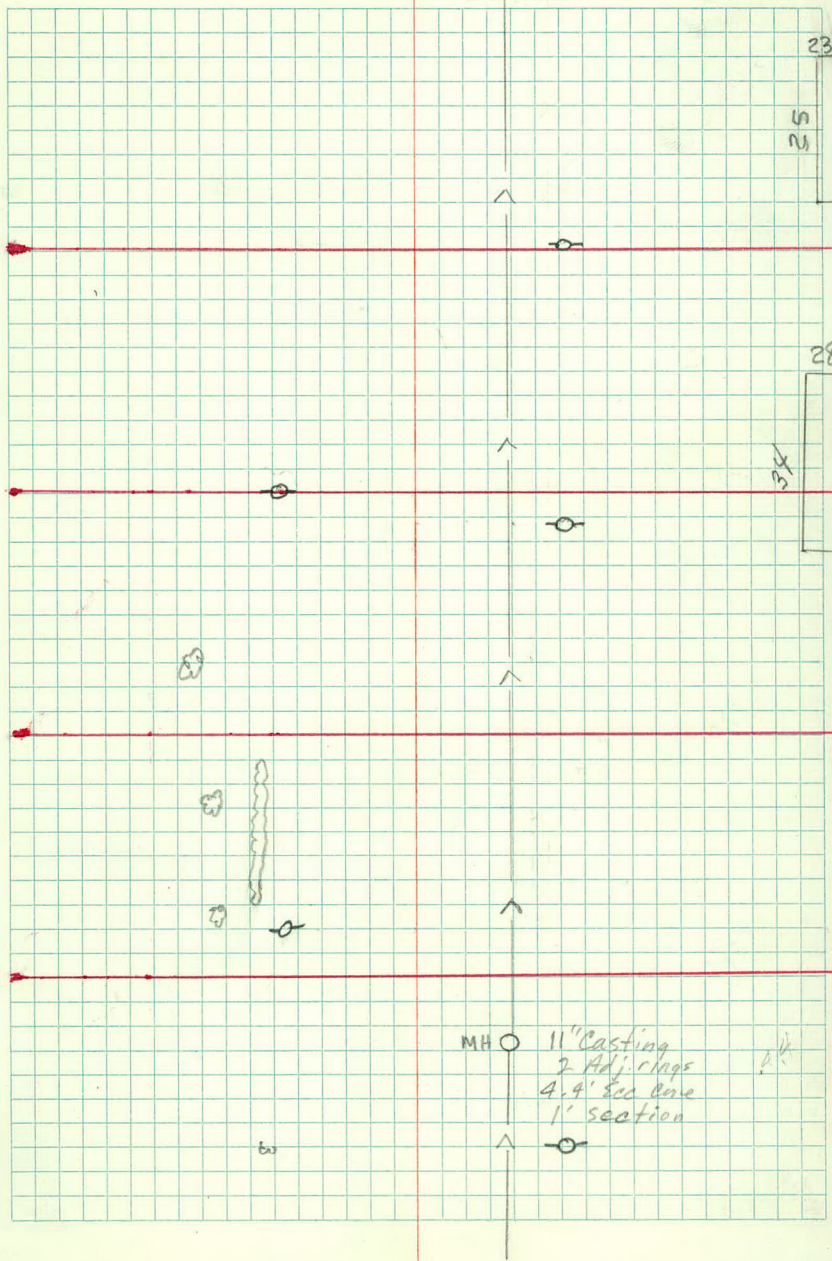
25+50

LT

E

RT

9.



+50

LT

E +50 6" P
4

RT +50 8" P
37

+32 5-2"E
43
+49 TW 4"E
43
+16 PP
29

+47 8" M
44
+09 NN Cor H₀
67

+03 3"E
42

30+00

+75 2"E
38

+50

+82 Bushes END
31

+56 PP
34

+08 Bush Bc G₁₁
32

29+00

+95 PP
28

+65 NE. Cor H₀
87

+50

+26 Bush +29 6" Cor
35 32

28+00

+19 Bush +23 1" M
41
+18 PP
31

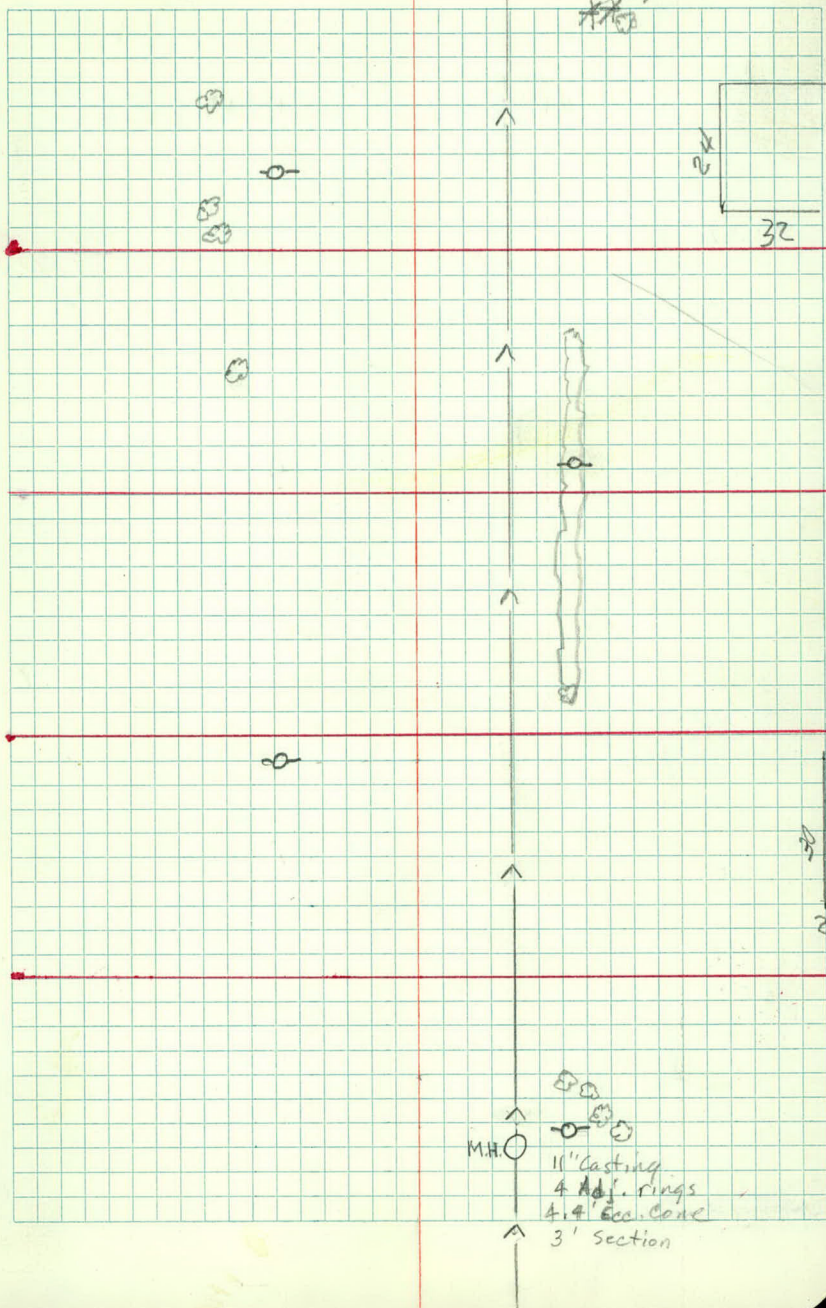
38+15 MH
20

Lt

E

10.

Rt
~~***~~



33+00

LT

£

R₇

+50

32+00

+50

31+00

+97 $\frac{MH}{21}$

+95 $\frac{MH}{26}$

+87 $\frac{CB}{30}$

+81 $\frac{MH}{23}$
Water Depth

+86 $\frac{TW 4" F}{37}$

+74 $\frac{PF}{28}$

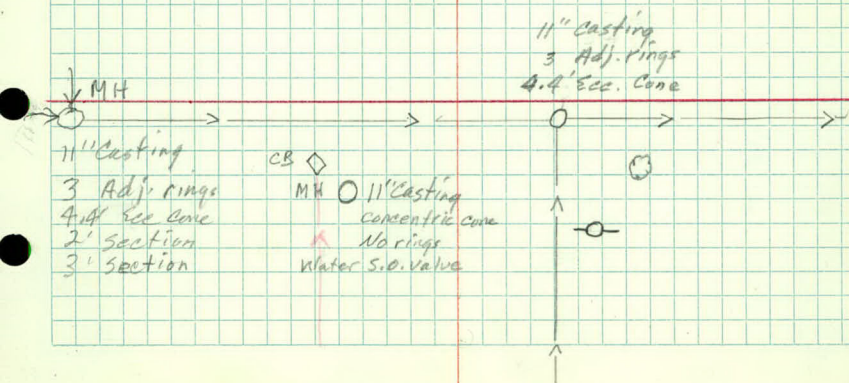
30+50

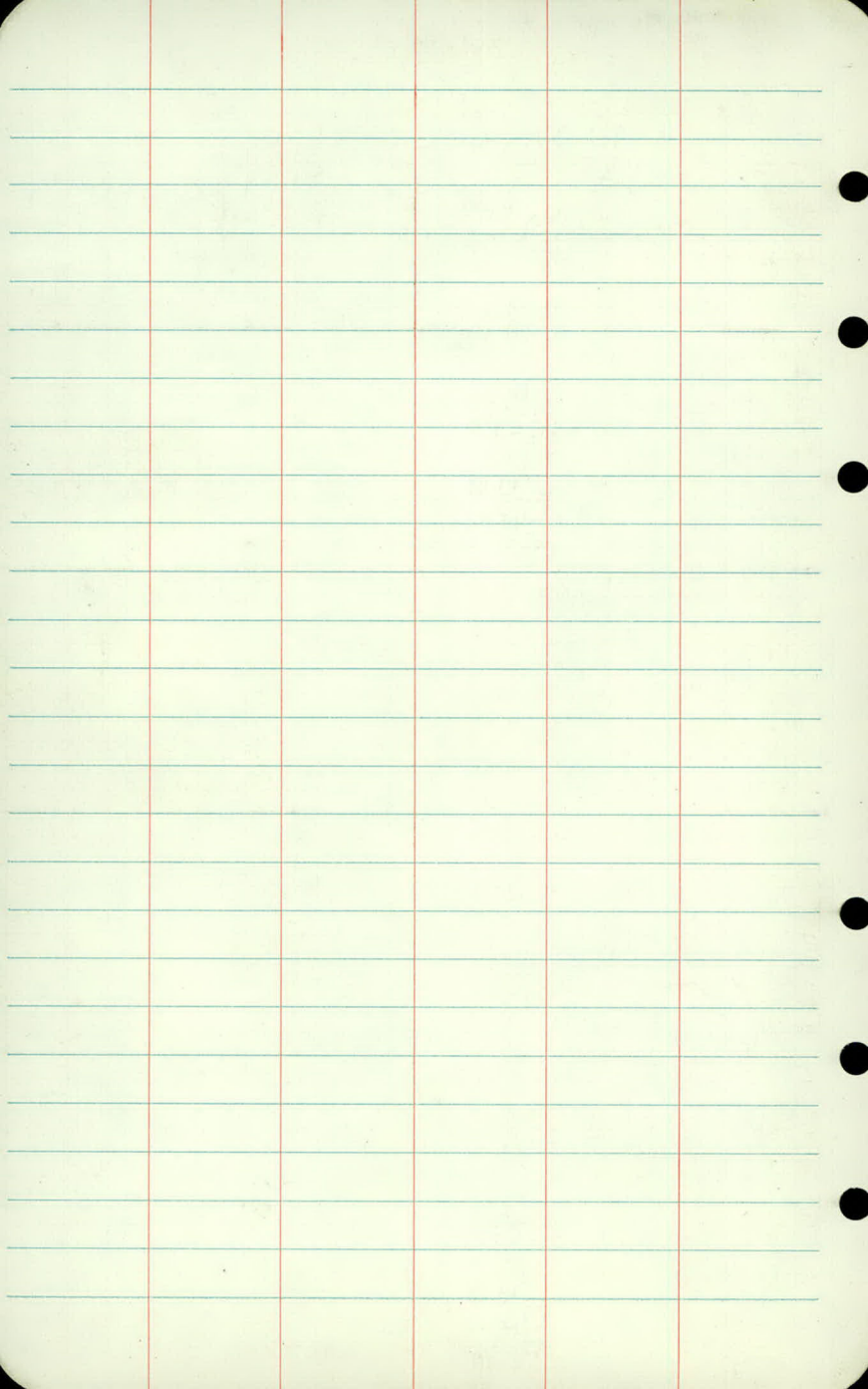
LT

⊥

RT

11.





BENCH LEVELS

Co Rd C - Victoria to Dale

23-1971

STA	+	π	-	Elev
BM				895.23
BM				926.16
BM	0.47	98.15		897.68
BM		8.75		897.71
TP	12.90	902.30	8.75	889.40
TP	13.77	15.80	0.27	902.03
TP	13.75	27.90	1.65	914.15
TP	13.12	39.54	1.48	926.42
TP	10.75	47.98	2.31	937.23
TP	1.80	46.36	3.42	944.56
BM	3.48	43.85	6.02	940.34 (940.37)
TP	0.92	41.33	3.44	940.41
TP	0.09	37.14	4.28	937.05
TP	11.32	36.30	12.16	924.98 (924.97)
TP	4.93	40.11	1.12	935.18
TP	6.22	42.95	3.38	936.73
BM			2.56	940.39 (940.37)

PK
CM
CP
BP

June 19 '70
Partly Cloudy 70°

Top Hyd NE Cor Oxford & C

BM Plate SE wing of Bridge

Top Hyd SW Cor Victoria & C

Top SE Cor Conc Base SE Leg PP#90

Spike in PP STA 78+80 RT

Top HYD NE Cor Heinel drive & C

Top HYD SW Cor Fisk & C

NW Cor Conc Drive Ho #800 Co Rd "C"

Top HYD SW Cor Avon & "C"

Top HYD STA 17+99 LT

Roseville BM #37 IN Front of Ho #720

Top Hyd STA 22+40 LT

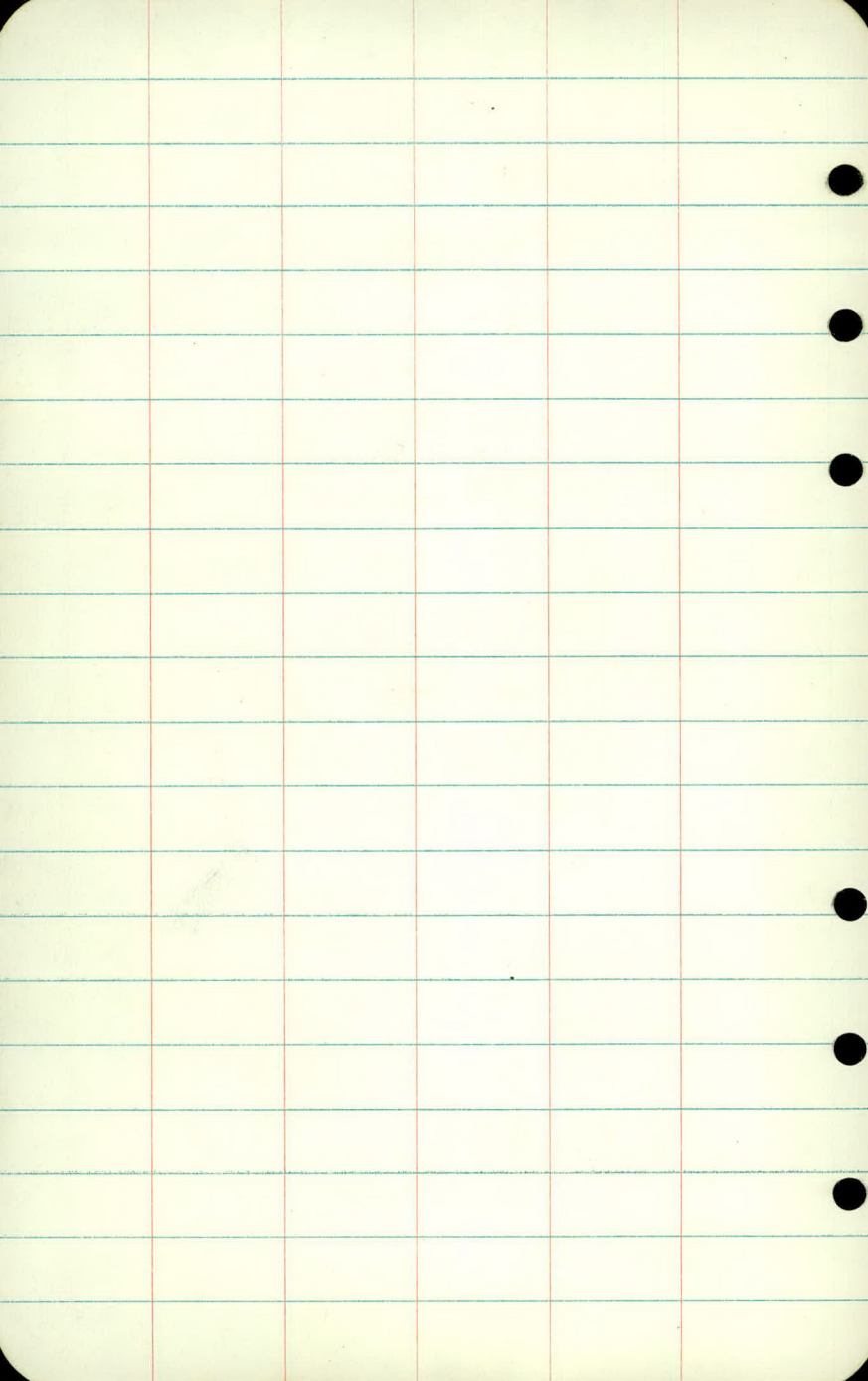
Top Hyd STA 26+43 LT

Top Hyd NE Cor Co Rd C & Dale

Spike in PP #429 STA 26+95 RT

SW Cor Conc Drive STA 24+50 LT

Roseville BM #37



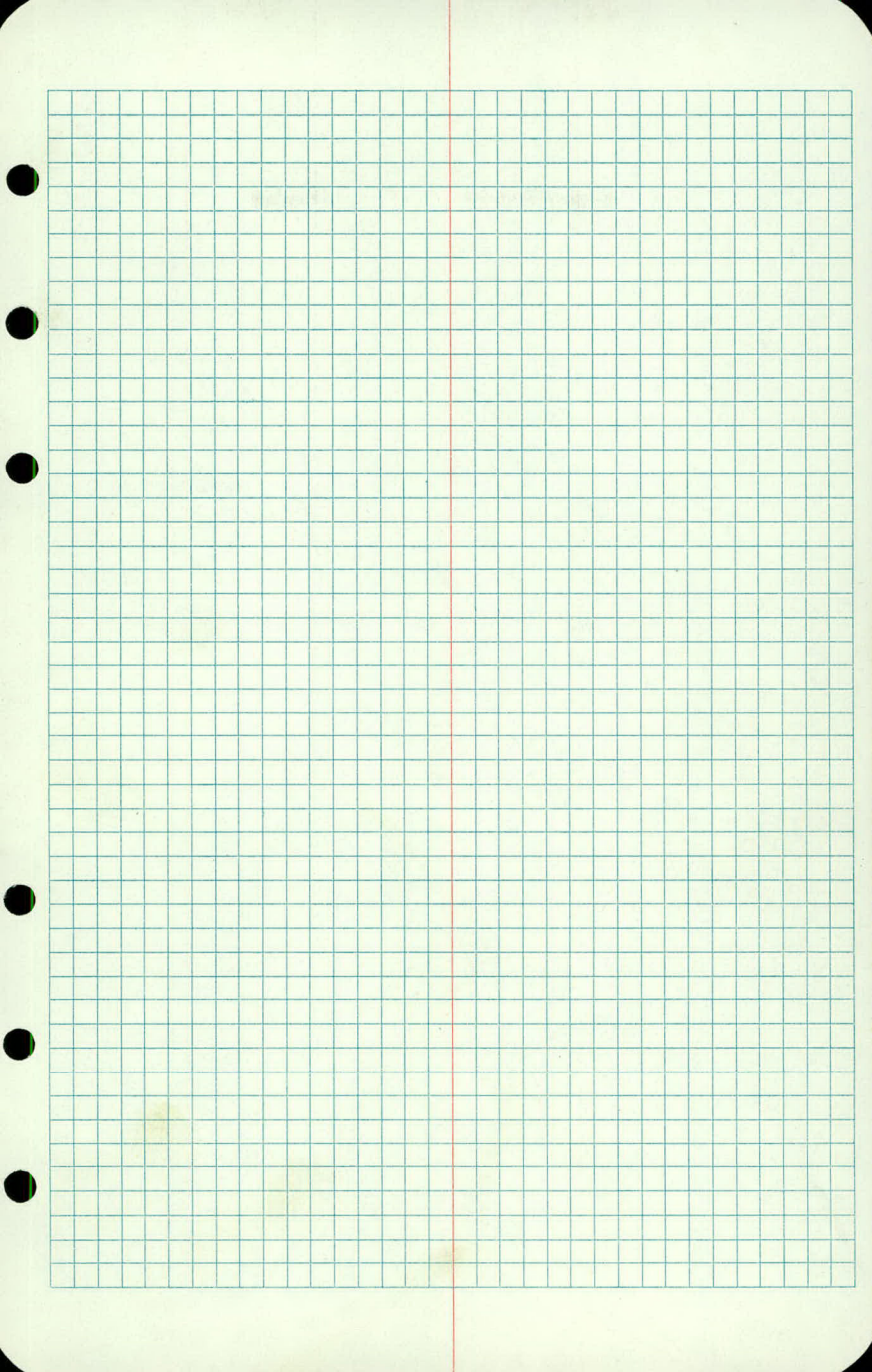
July 30, 1970

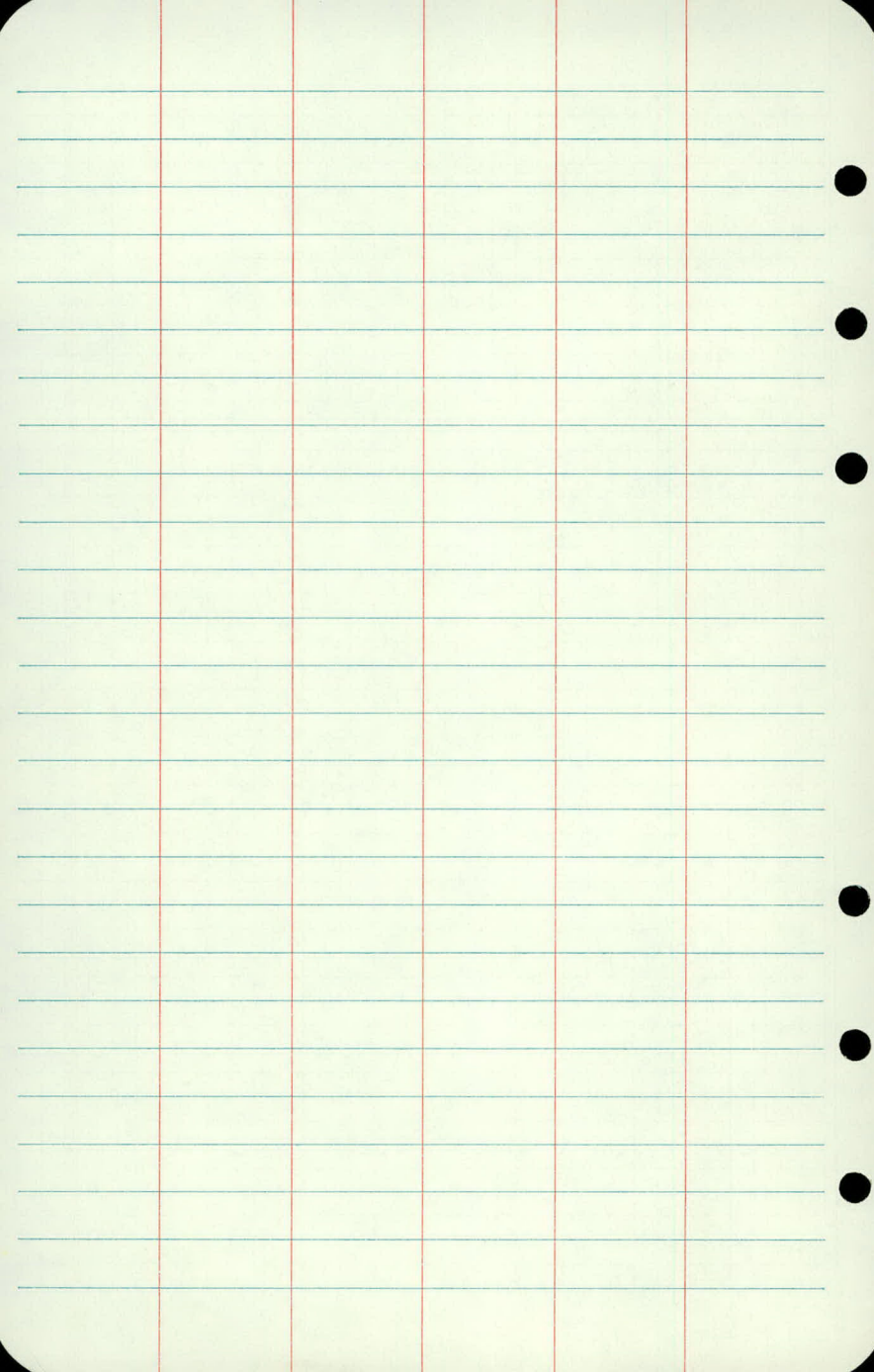
1

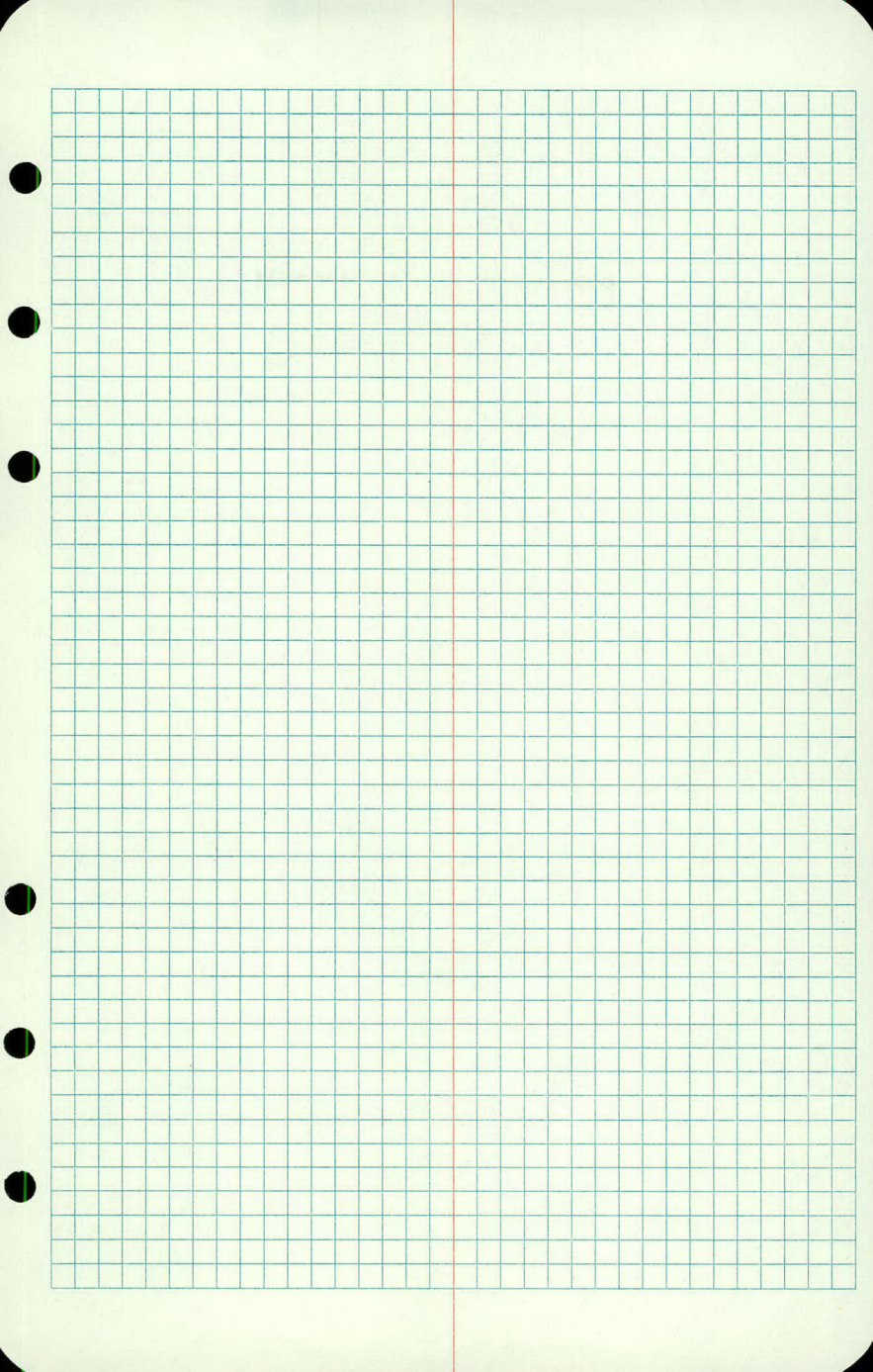
Bench Data Check

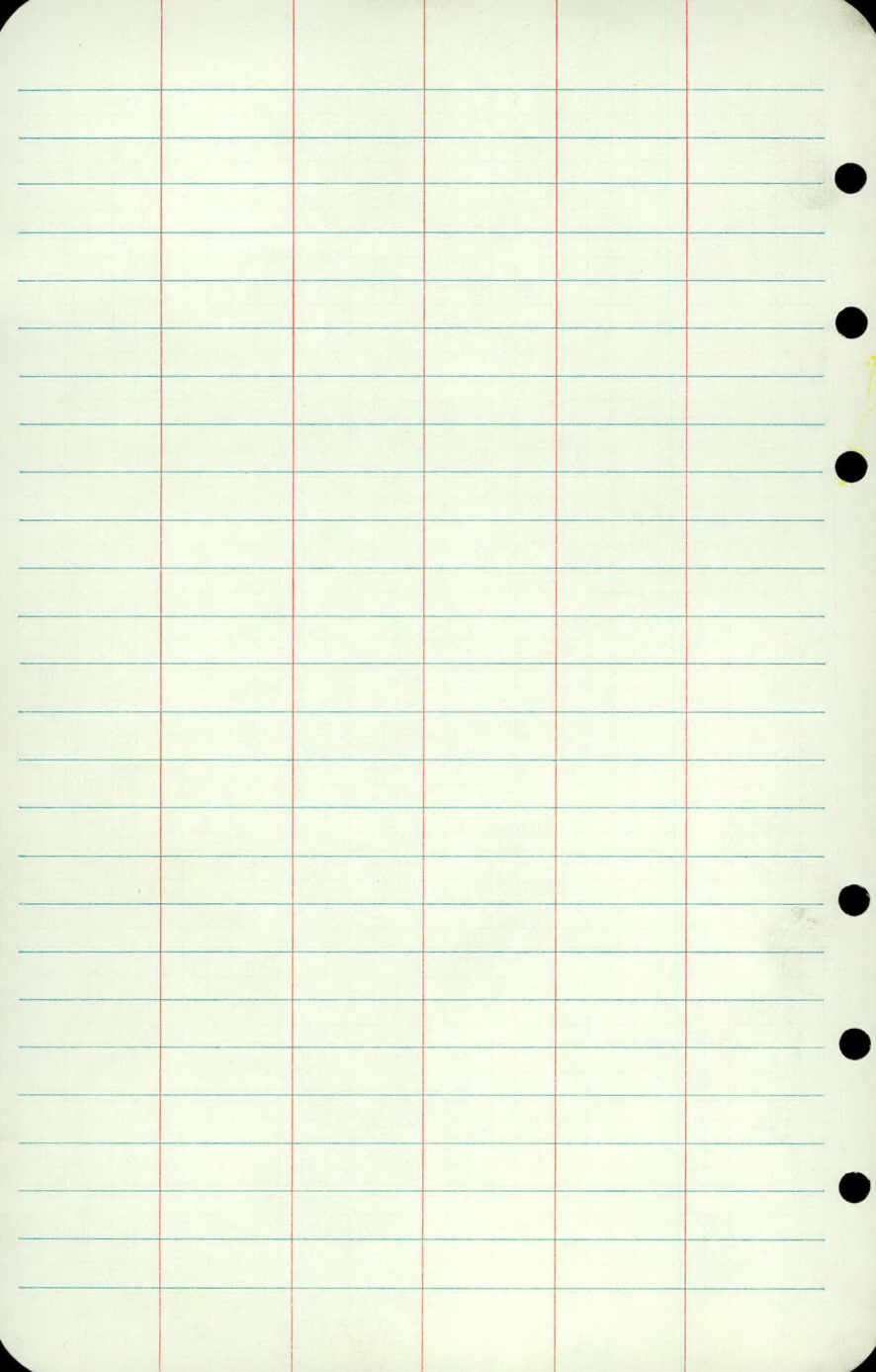
Conclusion: 1938 Notes
elevations are 0.26' higher
than found by 1966 Notes
which are Roseville Plane.

Sta	+	π	-	Elev.
BM	7.90	948.27		940.37
19+84	Ent Lt			
BM		3.71	944.56	
17+32				
17		4.53	43.74	43.53
18		5.30	42.97	42.75
1st step		4.66	943.61	
BM		5.19	943.08	943.34
				Low 0.26
BM	2.56	962.59	960.03	
£	£	Rice f'C"	4.26	958.33
				New Bit Surface 957.91
BM		11.80	962.59	950.79









FX
CM
BP
CP

L

July 30, 1970

2

Roseville BM

Low, 25
40.95
41.90

40.95

41.12

High, 17

6.57
50

7.15

Hyd Lt Sta 18+00

43.93

43.52

4.75

43.03

43.54

4.73

23

On New Bit.

42.81

42.81

5.46

50

North End, Top of Lower concrete
Step of dwelling Rt Sta 16+80

Walk

Top Hyd NW. Corner C & Rice

Top Hyd by playground

Sta	+	π	-	Elev.	
BM	0.48	902.52			
Top N. End $\angle$ Iron		$\begin{array}{r} 12.62 \\ 4.87 \\ \hline 17.49 \end{array}$	885.03	890.89	
81+00		7.12			
BM	2.26	899.98	4.80		(897.72)
S. Rail $\angle$ Victoria		3.83	896.15		Raised (95.84)
0+00		5.16	94.82		Low 0.22 (95.04)
0+00 S Rail Rt Angle		4.14	95.74		(95.84)
0+15					
0+43		5.02	94.96		(94.44)
water		14.24	85.74		

July 30, 1970

3

Top Hyd N.E. Corner Heinel Drive & "C"

on N.W. Corner tow Leg

Top Hyd on Victoria Between C & RR

& Victoria

94.44

94.46

5.52

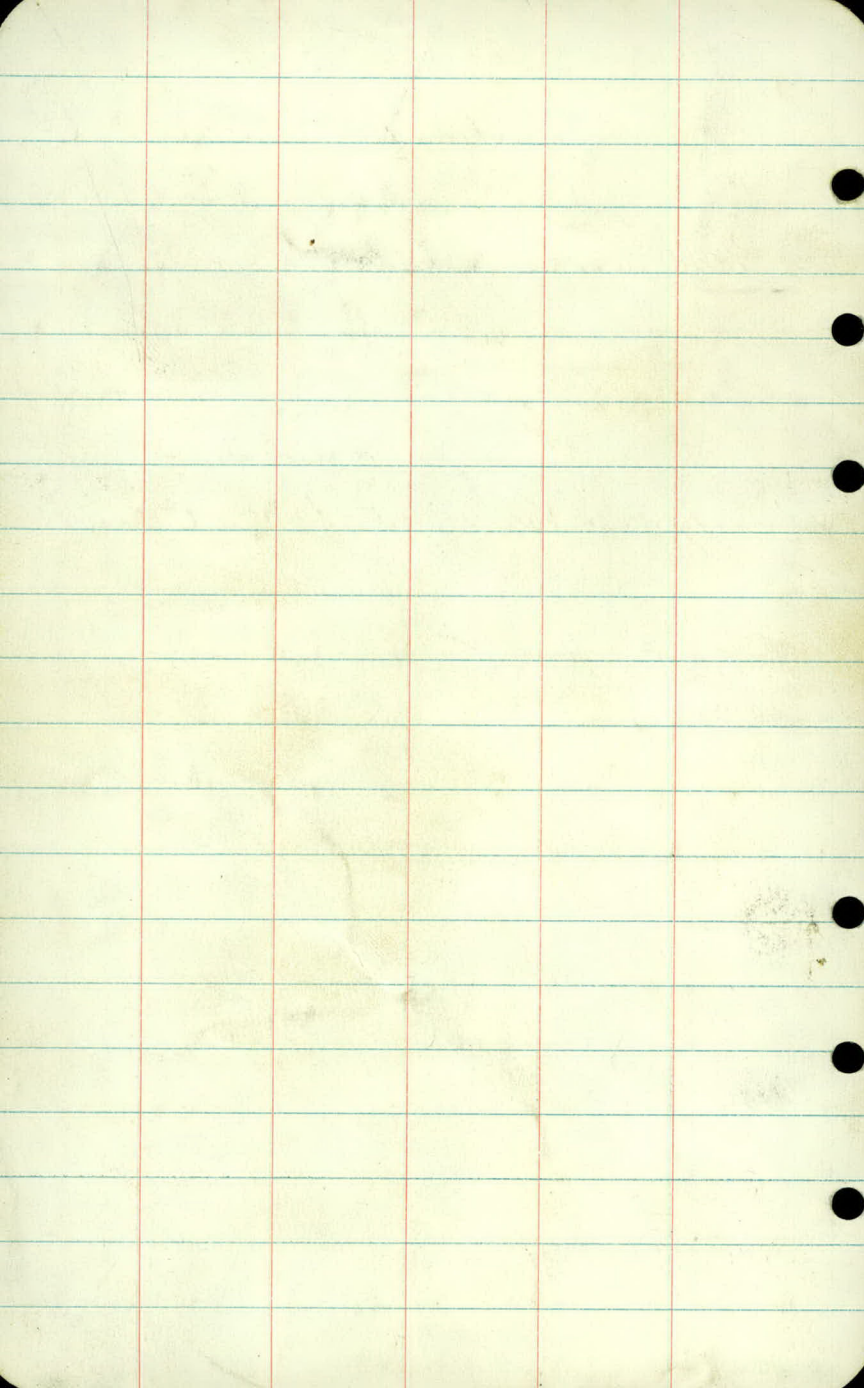
50

93.40

93.38

6.64

123



RGM
GAT
DKP

March 8, 1971
Fair 20°

County Rd "C"

Oxford to Dale

Bench Levels

Proj. 62-623-70

Sta	+	A	-	EIV	
BM	13.32	908.55		895.23	
TP	13.22	921.47	0.30	908.25	
TP	13.11	933.23	1.35	920.12	
BM	0.62	926.81	7.04	926.19	926.12
TP	0.62	914.15	13.28	913.53	
TP	1.14	903.24	12.05	902.10	
BM	0.21	897.98	5.47	897.77	
BM	4.24	896.46	5.76	892.22	
BM	8.91	898.35	7.02	889.44	
TP	6.35	904.16	0.54	897.81	
BM	12.32	914.42	2.06	902.10	
BM	13.42	927.65	0.19	914.23	
TP	10.46	937.67	0.44	927.21	
BM	11.52	948.87	0.32	937.35	
TP	4.65	947.33	6.17	942.68	
BM	1.33	945.97	2.67	944.64	944.57
BM	1.60	942.06	5.51	940.46	
BM	0.15	937.26	4.95	937.11	
BM			12.22	925.04	
	+ 117.17		- 87.38	895.23	
	- 87.38			29.81	
	29.81	← check			

RG M
GA K
DK ϕ

Description

Mar. 8, 1971
Mar. 9, 1971
cldy 18°

2

Top Hyd NE Cor Oxford $\frac{1}{2}$ "C"

Top stake

nail

Disk in SE Wing Wan Bridge 62519

NAIL

Top stake ϕ 74400

Top Hyd SW Cor Victoria $\frac{1}{2}$ "C"

Spike in PP Sta 77 $\pm$ Lt

" " " " 79 $\pm$ Rt

Rock

Top Hyd NE Cor Heinel Dr. $\frac{1}{2}$ "C"

Top Hyd SW Cor Fisk $\frac{1}{2}$ "C"

rock

Top Hyd SW Cor Aram $\frac{1}{2}$ "C"

rock

Top Hyd Ho # 743 Co Rd "C"

Top Hyd Ho # 701 Co Rd "C"

Top Hyd Ho # 667 Co Rd "C"

Top Hyd NE Cor Dale $\frac{1}{2}$ "C"

Sta	+	-	EIV	
BM	12.31	937.35	925.04	
BM	4.44	941.55	0.24	937.11 (937.11)
BM	5.70	946.16	1.09	940.46 (940.46)
BM	3.92	948.56	1.52	944.64 (944.64)
BM	0.71	938.04	11.23	937.33 (937.35)
TP	0.52	927.72	10.84	927.20 (927.21)
BM	0.18	914.41	13.49	914.23 (914.23)
BM	0.60	902.72	12.29	902.12 (902.10)
BM	7.07	896.53	13.26	889.46 (889.44)
BM	6.87	899.12	4.28	892.25 (892.22)
BM	10.91	908.70	1.33	897.79 (897.77)
TP	11.89	919.85	0.74	917.96
TP	10.10	927.40	2.55	917.30
BM	7.15	933.37	1.18	926.22 (926.19)
TP	0.56	920.44	13.49	919.88
TP	0.30	908.57	12.17	908.27 (908.25)
BM				895.12
		13.32	895.25	(895.23)
	+ 83.23	- 113.02		
		83.23	925.04	
		29.79	895.25	
			29.79	
		check		

R6 M
GA T
DK P

Mar. 9, 1971
cldy 18° Snow PM

Description

3

Top Hyd NE Cor. Dale $\frac{1}{2}$ "C"

Top Hyd Ho # 667 Co Rd "C"

Top Hyd Ho # 701 Co Rd "C"

Top Hyd Ho # 743 Co Rd "C"

Top Hyd SW Cor. Avon $\frac{1}{2}$ Co Rd "C"
rock

Top Hyd SW Cor. Fisk $\frac{1}{2}$ "C"

Top Hyd NE Cor. Heinal Dr. $\frac{1}{2}$ "C"

spike in PP Rt sta 79 ±

" " " Lt sta 77 ±

Top Hyd SW Cor Victoria $\frac{1}{2}$ "C"

rock

rock

BM Disk SE Wingwall Bridge 62519

rock

Top stake

Top Hyd. NE Cor. Oxford $\frac{1}{2}$ "C"

Sta	+	π	-	EIV
BM	1.53	946.17		944.64
BM			5.73	940.94 940.37
BM			5.72	940.45 940.46

High 0.7

Sta	+	π	-	EIV
BM,	2.66	897.89		895.23
TP	6.46	903.24	1.11	896.78
BM,	3.59	898.31	8.52	894.72 (894.61)
TP	1.76 ⁵	898.53 ⁵	1.54	896.77
BM,			3.31	895.225 (895.23)

W 1st BM

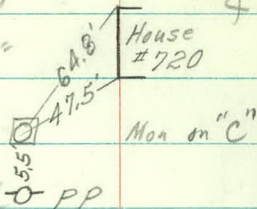
RG
LPD

Mar. 11, 1971
cldy 25°

Top Hyd Ho # 743 Co Rd "C"

Roseville BM # 37

Top Hyd Ho # 741 Co Rd "C" PP



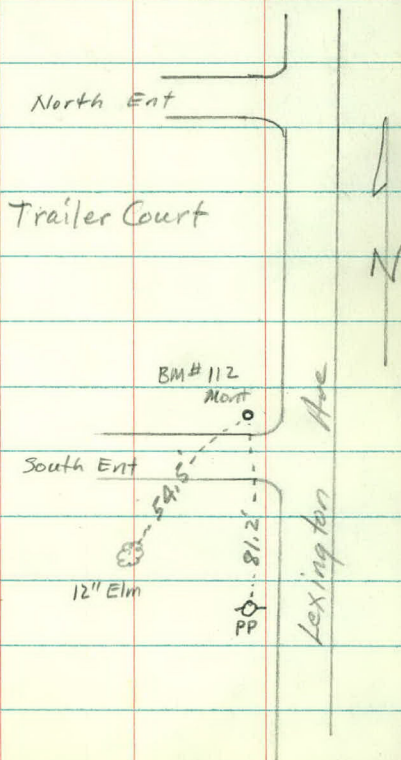
RG
GA

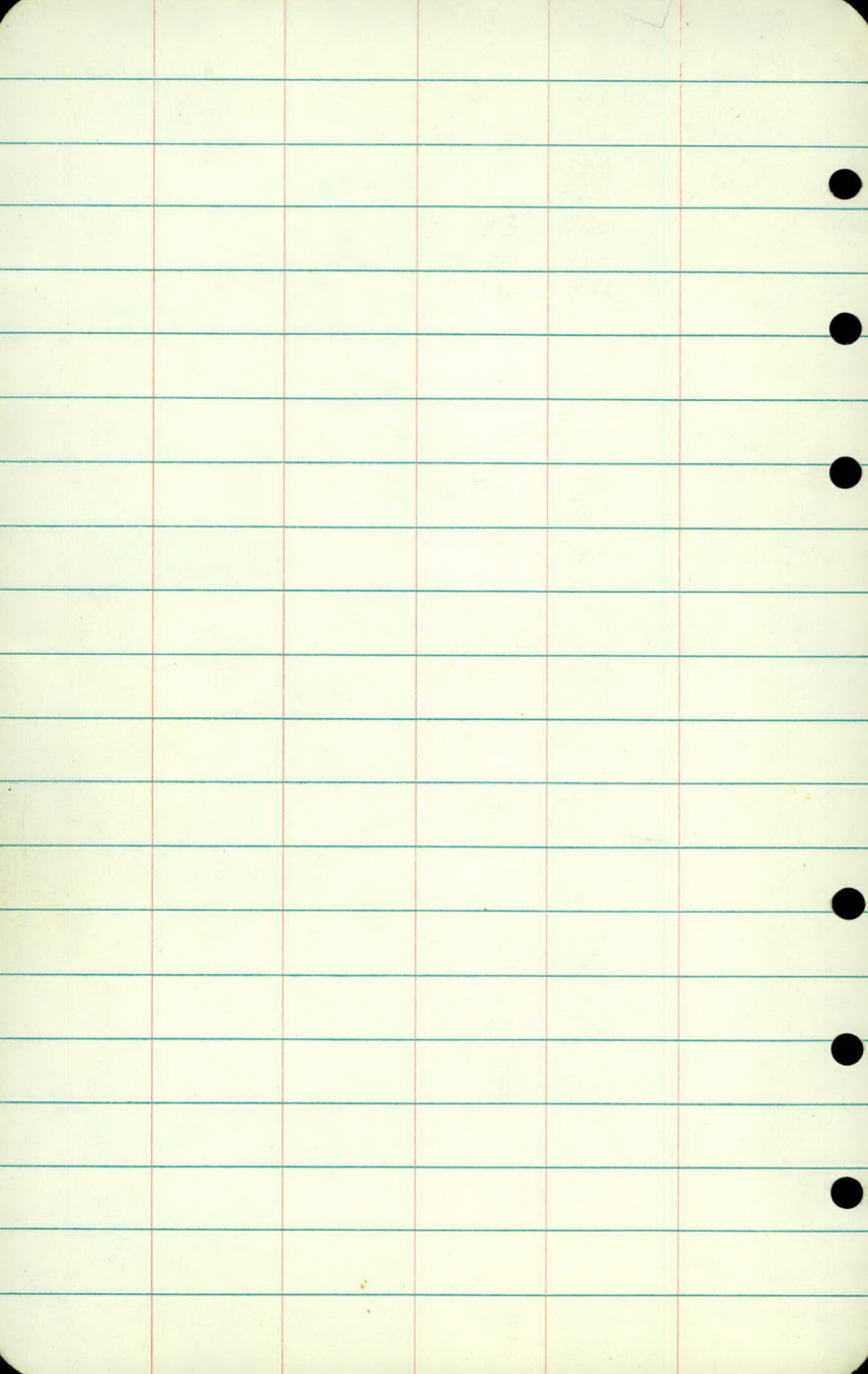
Mar. 23, 1971
Clear 130

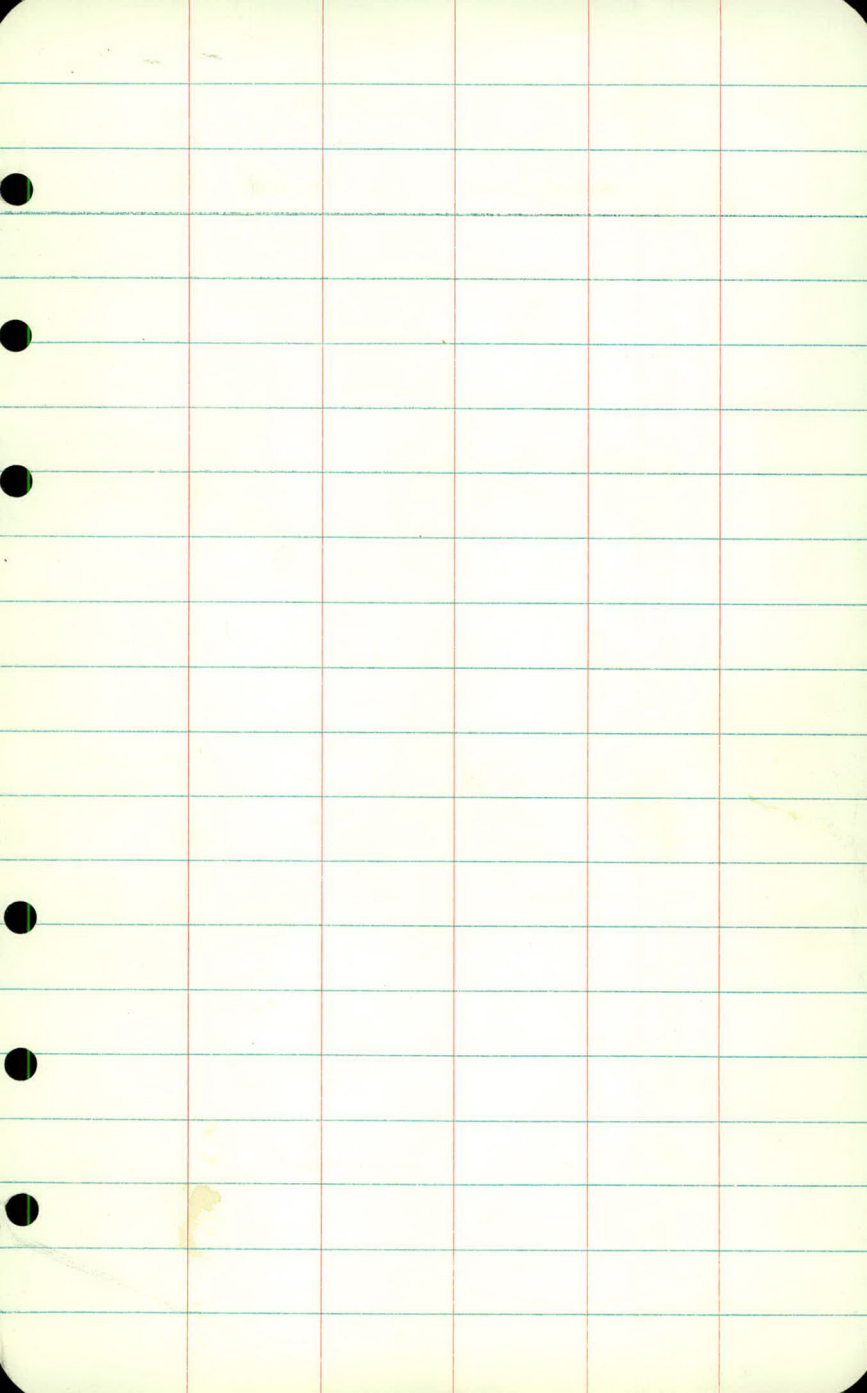
Top Hyd NE Cor Oxford & "C"

NP RTracks
|||||

Roseville BM #112







STA	T	T	-	Elev
BM	7.17	933.33		926.16 7.17

1			7.72	925.61
2			6.46	926.87
3			6.33	927.00
4			5.98	927.35
5			7.90	925.43
6			6.64	926.69
7			6.51	926.82
8			6.08	927.25

BM			6.41	926.92	926.90
----	--	--	------	--------	--------

July 30 '71 PK
LPD
DIB
BIB

Bench Mark SE Wing of Bridge G Rd
"C" and Victoria

Gutter Line SE cor Bridge

Gutter Line MEDIAN SE side

Gutter Line MEDIAN SW side

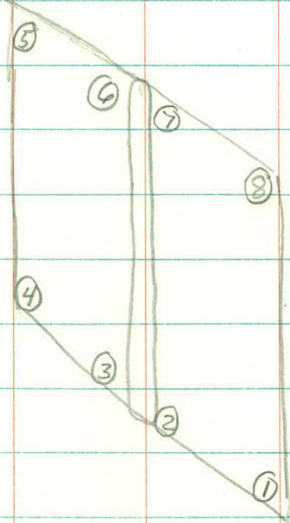
Gutter Line SW cor Bridge

Gutter Line NW cor Bridge

Gutter NW side

Gutter NE Side

Gutter NE corner



Spike in Twin 5" Elm North of Bridge

Sta + π - Elev

BM 2.43900.11

897.68
2.43

111+17.6 South Rail

111+22.7 North Rail

BM 2.48 897.6 3 897.62

LT

±

July 30 '71

RT

P/K
LPD
BP
DR

Top Hyd SW Cor Victoria and Cord C

96.60	96.33	96.10	95.75	95.52
3.51	3.78	4.01	4.36	4.59
<u>50</u>	<u>27</u>		27	50

Top Rail

96.53	96.29	95.99	95.62	95.43
3.58	3.87	4.12	4.49	4.68
<u>50</u>	<u>27</u>		27	50

Top Rail

Top Bolt in High Line Pole

899.50 Top Hyd. SW. Cor. RR Tracks & Lex

897.71 Top Hyd Lt. Sta 75+49

(Top Hyd on Victoria Between C & RR)

895.25 Top Hyd NE Corner, Oxford & "C"

RG
HL

Nov 4, 1970
PC 40°

Co. Rd. C
Proj. 23-71

Culvert Borings

79+67 45'

- 0-1 B.T. (8") & CL Gray pl.
1-2 SIL Gray pl.
2-3 LS Bwn NP
3-4 SIL Gray pl.
4-5 pl. SL Gray
5-9 SIL Gray pl.
9-12 SL Gray se. pl. fluid at 12'
12-13 S Gray pl.
13-17 + Fibrous peat

80+13 2

0-1 8"± BT LCL Gray pl.

1-3 pl. SL Bwn.

3-4 LS/FG Bwn NP

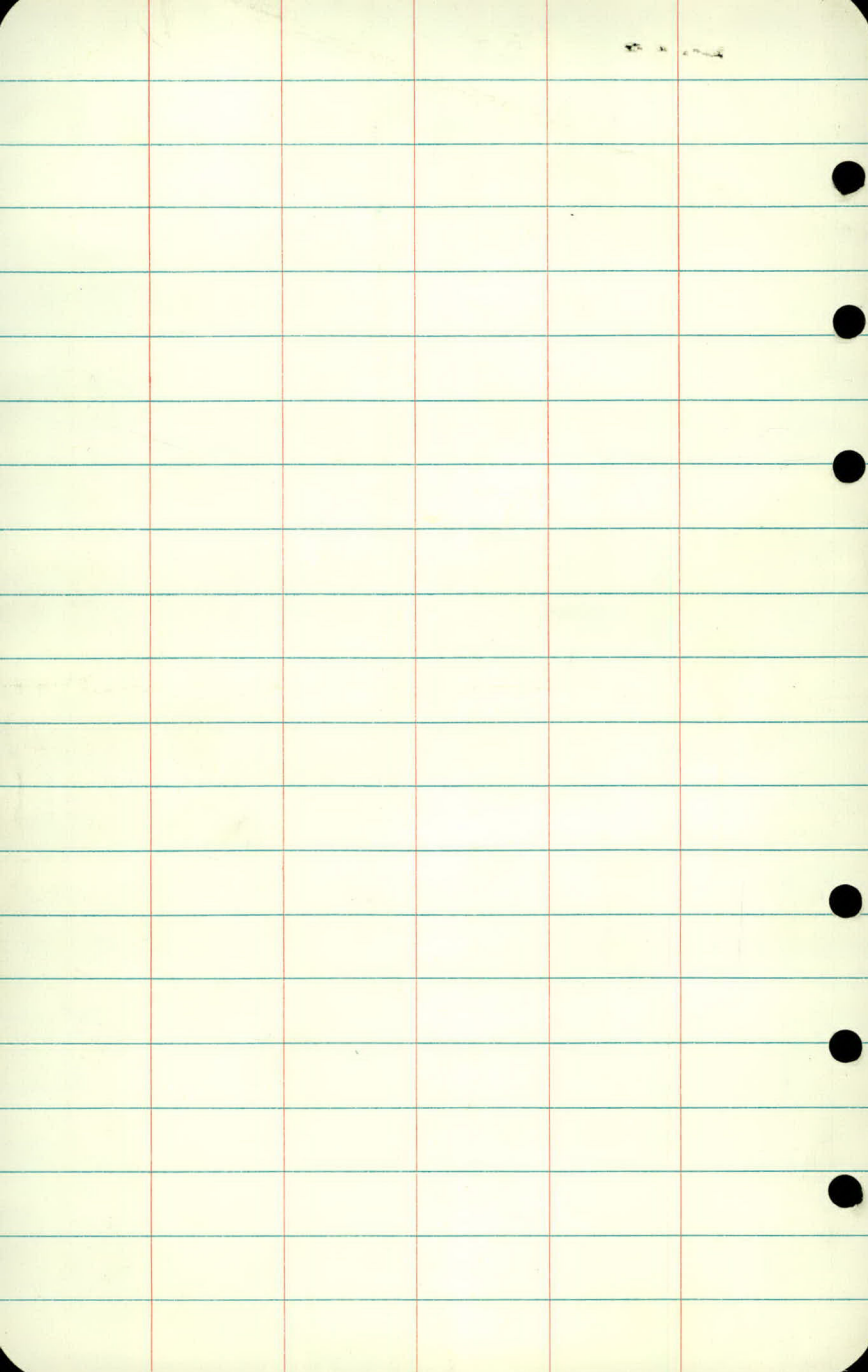
4-10 SL Bwn pl.

10-14 SL Gray sl. pl.

14-18 Fibrous peat

18-23 CrS/G Gray NP

23-27 C Gray pl. v. stiff



County Road C

Oxford to Dale

x-sections

Lordon Christensen
N

Sta	+	π	-	Elev.
BM	2.14	897.37		895.23

Apron Invert			7.38	887.85
--------------	--	--	------	--------

59

Inr E, End 15" x 34' CM		5.41		891.98
-------------------------	--	------	--	--------

4.16
103
41

+50

+68

60

+50

T.P.	11.20	907.24	1.33	896.04
------	-------	--------	------	--------

FA
PK
BP
CM

August 20, 1970

X-2

Top Hyd NE Corner Oxford & "C"

Culvert Between C & R.R. East Side of Lex.

90.4	92.6	93.3	93.1	93.2	92.7	93.2	93.2	92.8
6.93	4.8	4.1	4.3	4.2	4.66	4.22	4.2	4.6
Inv. 79	64	43	21		6	23	41	63
WE 15" CM					22	C		

92.2	94.5	94.3	93.8	94.1	93.7	94.2	94.3	93.3
5.2	2.9	3.10	3.56	3.3	3.68	3.24	3.10	4.155
45	31	23	22		22	23	38	59
Water		C	G		G	C		

92.2	94.4	94.8	94.3	94.5	94.2	94.7	94.8	93.8
5.2	3.0	2.57	3.06	2.9	3.21	2.71	2.6	3.6
40	31	23	22		22	23	35	57
Water		C	G		G	C		

92.2	93.3	93.6	93.9	94.7	94.9	93.5
5.2	4.1	3.8	3.5	2.7	2.5	3.7
41	39	19		23	45	67
Water					95.4	92.5

92.3	95.0	95.5	95.4	96.4	95.4	95.4	94.2
5.1	2.4	1.9	1.6	1.0	1.6	2.0	3.2
42	36	22		22	45	64	67

Tie Hub 11.

Sta + π - Elev.

907.24
1.04

61

+50

62

+50

TP 13.07 919.27 1.04 906.20
13 07

63

+50

Lt.

August 20, 1970

Rt

X-3

93.5	96.7	97.1	97.9	97.7	97.6	96.7	97.3
13.7	10.5	10.1	9.4	9.5	9.4	10.5	9.9
45	35	24		24	52	70	79

93.9	94.7	96.1	98.9	99.4	99.9	99.6	99.4	95.5
13.3	12.5	11.1	8.3	7.8	7.3	7.6	8.8	11.7
52	48	44	37	25		2.3	52	66

96.5	97.9	91.3	91.4	92.4	91.9	91.3	97.8	95.0
10.7	9.3	5.9	5.8	4.8	5.3	5.9	9.4	11.7
57	45	35	22		25	40	51	60

97.6	90.0	93.8	94.1	94.7	94.5	93.7	99.3	96.2
9.6	7.2	3.4	3.1	2.5	2.7	3.5	7.9	11.0
61	44	36	23		21	38	49	60

92.1	95.7	96.2	97.1	97.3	97.0	96.9	92.7
17.2	13.6	13.1	12.2	12.0	12.3	12.4	16.6
46	40	36	28		21	34	45

94.2	96.7	97.4	99.7	99.9	99.8	99.2	94.2
15.1	12.6	9.9	9.6	9.4	9.5	10.1	15.1
50	43	36	19		26	40	50

STA + $\bar{\Delta}$ - Elev

919.27
67

64

+50

+75

65

+25

10.03 928.63 0.67 918.60

+50

RG
LPD
DK

Mar. 1, 1972
10° Windy, Snow

1

62-623-10

CO. RD. "C" "

Victoria St. TO DALE ST,

MH ELEVATIONS

STA	+	π	-	ELEV.	
BM.	6.70	908.74			902.04
MH			11.07	897.67	
MH			10.90	897.84	?
BM	7.92	922.08			914.16
MH			9.60	912.48	
MH			2.73	919.35	
MH			2.54	919.54	
TP	6.30	928.20	0.18	921.90	
MH			5.62	922.58	
BM	11.94	949.21			937.27
MH			13.64	935.57	
MH			6.85	942.36	
MH			7.74	941.47	
MH			8.15	941.06	
BM	4.33	944.73			940.40
MH			6.57	938.16	
MH			8.45	936.28	
BM	3.57	940.61			937.04
MH			5.93	934.68	

LT

E

RT

2

TOP HYDRANT NE Cor. Heinel Dr.

Sta 81+81 Rt 12'

Sta 82+93 Rt 38

Top Hyd SW Cor Fisk

Sta 9+06 Rt 36' & Fisk St.

Sta 10+16 Lt 10' (Water Dept.)

Sta 10+³⁴~~47~~ Rt 30'

Sta 10+81 Rt 27'

Top Hyd SW Cor. Avon St.

Sta 13+74 Rt 29' & Avon St

Sta 15+85 Rt 29'

Sta 17+94 Rt 26'

Sta 18+26 Rt 27'

Top Hyd Lt Sta 22+40

Sta 20+75 Rt 25'

Sta 23+54 Rt 20'

Top Hyd Lt Sta 26+43

25+87 Rt 19

STA	+	π	-	ELEV.
BM	2.81	940.21		937.40
MH			8.17	932.04
BM	1.99	926.96		924.97
MH			5.61	921.35
MH			4.99	921.97
MH			5.95	921.01

LT

~~E~~

RT

3

Top Hyd Lt Sta 26+43

Sta 28+15 Rt 20'

Top Hyd NE Cor Dale St # "C"

Sta 30+81 Lt 23' (Water Dept.)

Sta 30+95 Lt 86'

Sta 30+97 Rt 21'

STA

+

π

-

ELEV.

RG
GA
DK

April 26, 1972
PC 45

1

Stock pile X-Sections

sta	+	π	-	E/v
BM	0.48	926.64		926.16

71+00

+15

✓

+30

+50

72+00

TP	3.95	918.87	11.72	914.92
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LT

P

Apr. 26, 1972

RT

2

BM Disc SE Wingwall Bridge 62519

17.1 ⁶⁴	17.2 ¹⁴	17.2 ¹⁴	17.2 ³⁴	16.9 ⁸⁴	14.7 ⁶⁴
9.0	9.5	9.5	9.3	9.8	12.0
43	32	15		14	27

NG section

17.2 ¹⁴	26.3 ²⁴	2.7 ¹⁴	26.1 ³⁴	26.7 ⁶⁴	26.5 ⁴⁴	1.9 ⁸⁴	1.9 ⁸⁴
9.5	0.4	10.5	0.3	0.0	0.2	11.8	12.8
62	53	36	16		9	26	30

NG

64
13.7
13.0
69
NG

89.9 ³⁴	15.7 ⁶⁴	19.7 ⁶⁴	25.7 ⁶⁴	18.1 ⁰⁴	18.1 ³⁴	18.1 ⁶⁴	15.6 ⁵⁴	13.1 ¹⁴
27.3	13.0	7.0	1.0	8.6	8.3	8.0	11.1	13.2
94	73	63	45	22		14	20	29

NG

NG

89.9 ³⁴	25.8 ¹⁴	19.8 ¹⁴	17.6 ⁵⁴	17.7 ⁸⁴	17.6 ⁵⁴	12.9 ⁸⁴
27.3	1.5	6.9	9.1	8.8	9.1	13.8
94	60	52	43		12	20

NG

NG

89.9 ⁸⁴	13.7 ⁶⁴	22.8 ¹⁴	17.5 ²⁴	15.5 ⁴⁴	16.1 ⁰⁴	16.8 ¹⁴	10.7 ⁶⁴
27.8	13.0	3.9	9.4	11.2	10.4	10.5	16.0
93	73	61	50	32		10	19

NG

NG

rock

Sta + π - E/V

918.87

72+50

73+00

✓

TP 1.77 908.60 12.04 906.83

73+50

74+00

+50

BM

10.86

897.74

897.68

Apr. 26, 1972

LT

F

RET

3

00.2	05.6	18.1	19.9	12.2	12.3	12.0	07.8
18.7	13.3	0.8	41.0	6.7	6.6	6.9	11.1
100	92	72	51	41		14	23
NG						NG	

07.6	15.0	16.3	09.4	08.9	09.2	08.6	06.1
11.3	3.9	2.6	9.5	10.0	9.7	10.3	12.8
76	65	54	43	25		20	27
						NG	

899.9
19.0
88
NG

Nail & Sta 73+50

99.4	05.3	05.4	04.4	04.8	06.7	06.8	06.6	03.1
9.2	3.3	3.2	4.2	3.8	1.9	1.8	2.0	5.5
64	55	47	37	28	22		25	32
NG							NG	

00.5	01.7	00.9	01.3	06.5	06.5	04.9	04.9	06.2	01.0
8.1	6.9	7.7	2.3	2.1	2.1	3.7	3.7	2.4	7.6
49	37	33	19	9		2	11	17	25
NG									NG

99.2	99.6	98.8	99.3	99.1	99.5	98.8
9.4	9.0	9.8	9.3	9.5	9.1	9.8
47	33	30	15		12	19
NG					NG	

Top Hyd. @ Victoria

