

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN

Survey

Old Co. Rd. "C"

From Rice

To Lake Stone

Road Acc't. No. —

Date Filed —

File —

DE. 9 BK 73

KP
RG
DS
GA

27 DEC. 1972 1.
☼ CLOUDY 30°

C.O. RD. "C"

RICE ST. TO LAKESHORE DR.

TOPOGRAPHY

+50

LT

R_T

10" Elm

8" Elm

+33 46 +41 46

1" Pine

+30 38

1" Pine

+43 34

PP

+44 28

22" Elm

NW Cor Ho (1-S-F)

+26 64

+28 69

2" Maple

6" Elm

+25 38

+26 57

5" Elm

+12 42

297 +00 $\frac{Fe}{35}$

12 12

6" Pop

+90 42

187 $\frac{PP}{32}$

+71 2 10' Ent.

+64 $\frac{3" B.E.}{32}$

+79 $\frac{5" Elm}{32}$

4 woven wire steel posts

Fe Cor

6" Poplar

+55 35

+55 46

8" Tr. Poplar

3" Apple

+50

+55 $\frac{38}{38}$

+54 $\frac{51}{51}$

Fe Cor

+22 69

NW Cor Ho (1-S-F)

NE Cor Ho

+22 69

+47 69

8" Apple

PP

1" Pine

+02 43

+11 28

+22 58

ER

8" Birch

+00 12

+01 62

4 Cyclone Fe

+90 32 +

296

PP

+78 18

BR

+69 33

+50

+56 Stark St

ER

+44 33

PP

+31 31

PP

+30 17

12P

+31 73

PP

BR

+12 29

+16 12

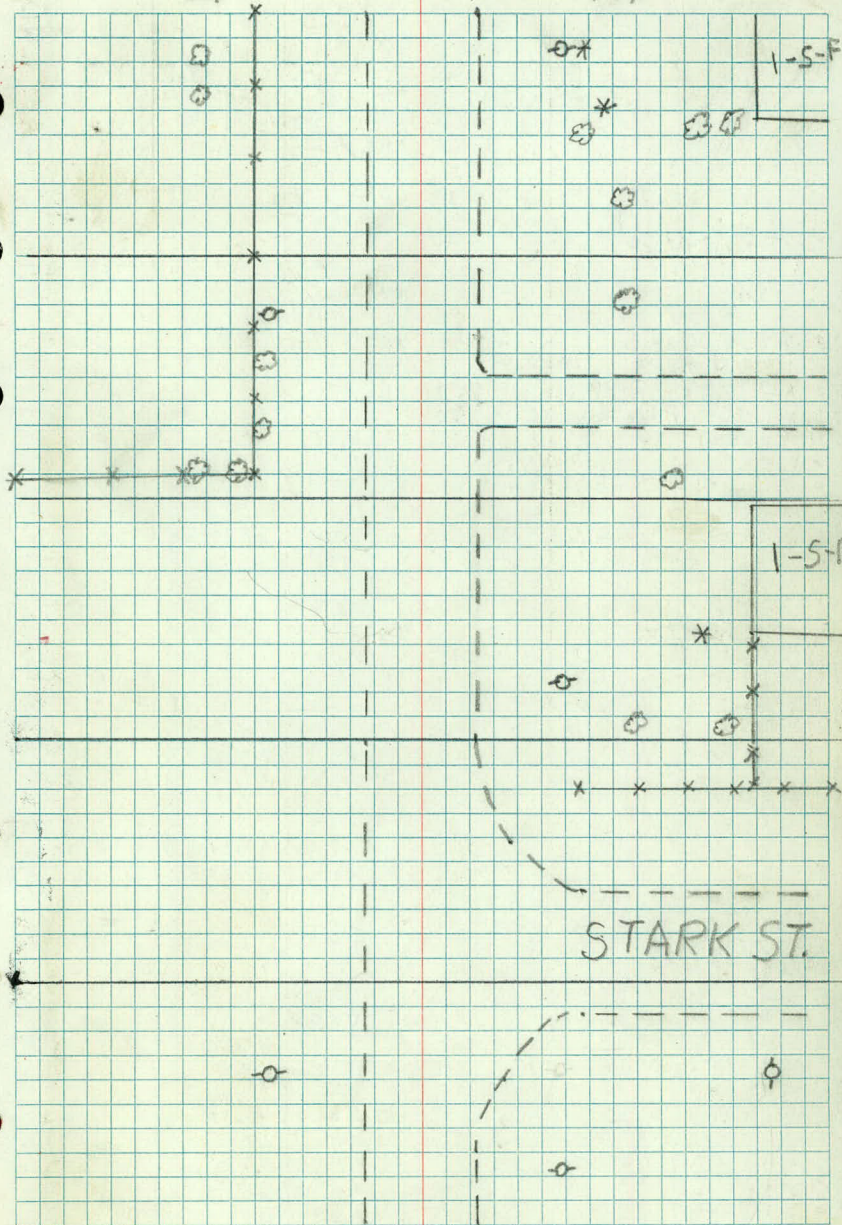
295

12 12

27 DEC. 1972 2.

LT

RT



300

LT

 $\frac{12}{12}$

RT

 $+90 \frac{\text{Bush}}{45}$

3-13" oak

+62-64 ~~83~~ 41
 $+50 +60 \frac{\text{SE Cor Ho}}{99}$

Tw 13" oak

 $+43 \frac{44}{44}$
 $+43 \frac{\text{PP}}{27}$
 $+47 \frac{\text{Tw 4" Elm}}{30}$

4" wire-steel posts

1-5-St.

+41

 $+23 \frac{\text{Beg Fe}}{35}$
 $+29 \frac{\text{SWE Cor Ho}}{100} \text{ RT+31}$
 $\frac{\text{Quint 6" Elm}}{32-34}$
 $+23 \frac{\text{Bush}}{45}$
 $+29 \frac{4" \text{ Elm}}{23}$
 $+29 \frac{4" \text{ Elm}}{27}$
 $+33 \frac{6" \text{ Elm}}{23}$

299

 $+92 \frac{15" \text{ Ent RT+00}}{20}$
 $+65 \frac{\text{PP}}{31}$
 $+75 \frac{15" \text{ Ent}}{72}$

RT+68

+50

 $+59 \frac{\text{Fecor}}{36}$
 $+59 \frac{\text{Tw 12" Coff}}{51}$
 $+40 \frac{29 \text{ SE Cor Ho}}{88}$
 $+44 \frac{10" \text{ oak}}{42}$
 $+42 \frac{\text{PP}}{27}$
 $+40 \frac{\text{RT+40}}{88}$
 $+35 \frac{3-4" \text{ Elm}}{21}$
 $+42 \frac{\text{PP}}{27}$
 $+01 \frac{\text{Beg Fe}}{35}$

(1-5-St.)

SWE Cor Ho

298

+00

81

RT+08

+82

 $\frac{12" \text{ Elm}}{58}$
 $+98 \frac{15" \text{ Ent RT+06}}{58}$

+77

 $\frac{\text{Fecor}}{36}$
 RT+83

+86

 $\frac{14" \text{ Elm}}{52}$
 $+67 \frac{12" \text{ Pop}}{47}$
 $+70 \frac{10" \text{ Ent}}{52}$

297+50

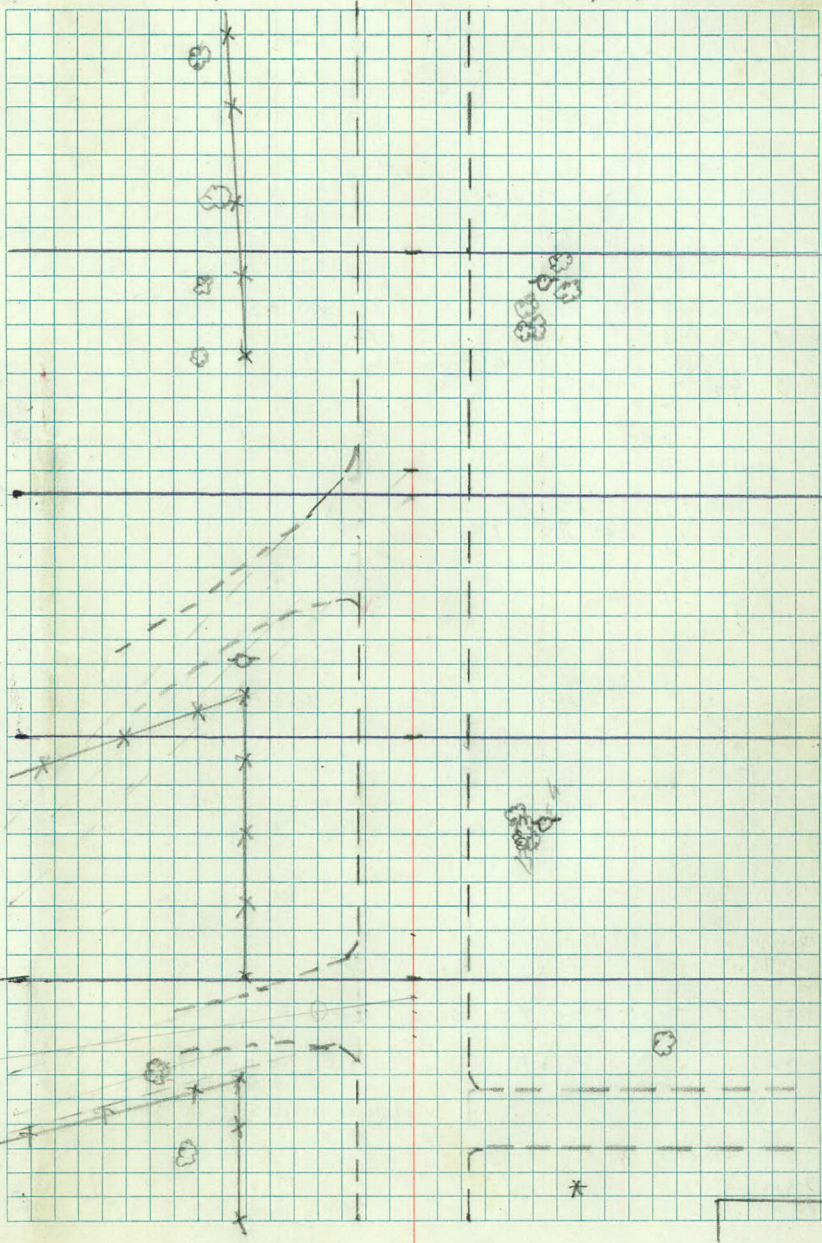
 $+53 \frac{\text{NE Cor Ho}}{69}$
 $+56 \frac{15" \text{ Pine}}{35}$

27 DEC, 1972

3.

LT

RT.



+50

£

+49 EUG & PP
42 POR
+43 23
BIR
+31 40

302

+93 8" Oak 39 +85 24" Elm 29
+74 Two 6" BE 42 +94 5" Oak 41
+98 3-4" Elm 57 +95 4-6" Elm 57
+60 4-4" Oaks 38

+50

+41 6" Elm 51 +47 5" Apple 47 End.
+92 Bridge

PP
+39 23

301

+92 E RR tracks

+50

GR=13 13=GR

+48 Bridge £ +48 PP 24

+14 20" Elm 48 +29 £ 15" Ent
+08 End Ec 40

+14-13 8-4" Elm 31-33

+01 5" Elm 25

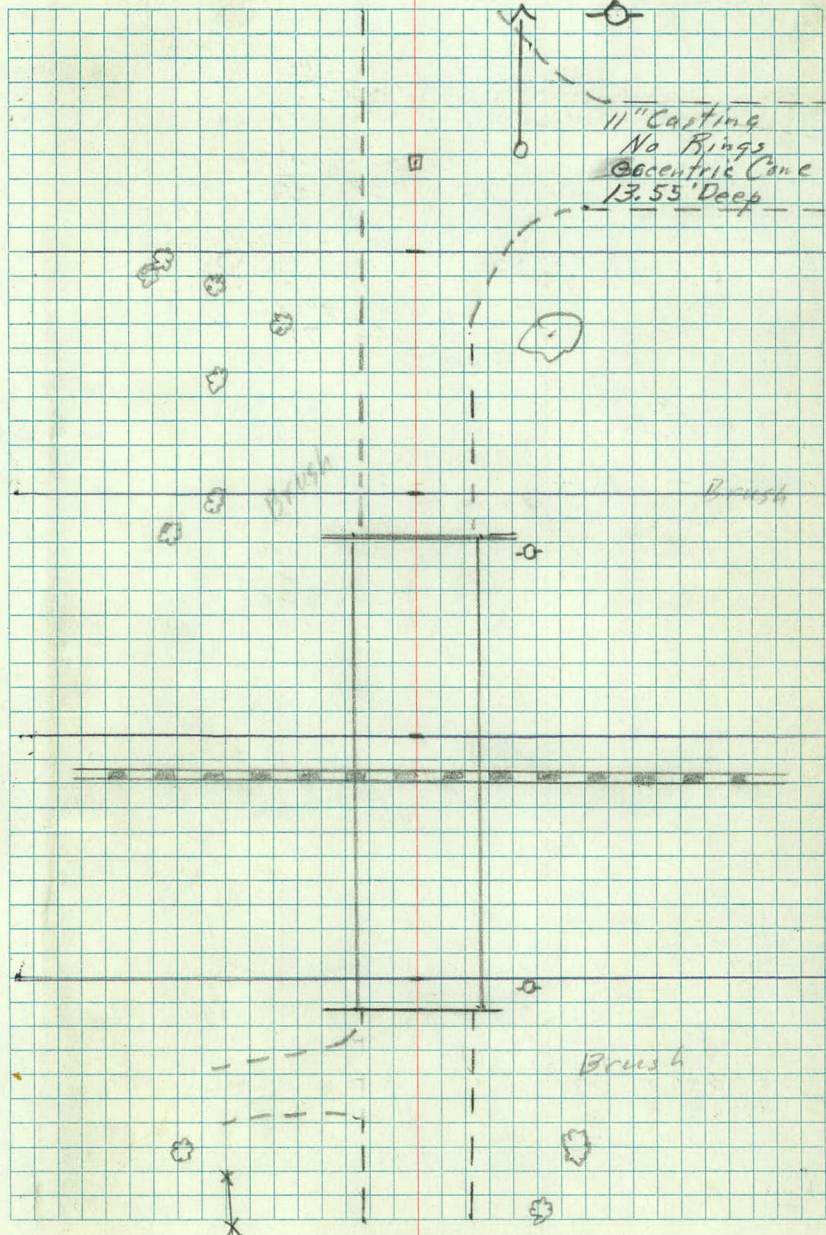
300

LT

E

27 DEC 1972 4.

RT



11" Casting
No Rings
Eccentric Cone
13.55' Deep

Brush

Brush

Lt

2

Rt

30.5

+87	4" B. Spr 53	+97	4" B. Spr 53		
	4" B. Spruce		4" B. Spr.	+86	Cor Ho 63
+74	53	+81	53		6" Cott
	Swan Ho (1-5-F)		C.I. Pipe	+64	27
+67	81	+67	32		N.W. Cor Ho
+58	4" S. Spruce 53		3" Juniper	+59	24
		+52	53	+70	sewer xing
+50			5" B. Spruce 53	+50	EUG 22
	+40		53		

+29	4" Blue Spruce 53	+34	53		N.E. Cor Ho 71
			2" Juniper	+106	WSD 33
	7" N. Pine 53	+24	53		Cor Ho
+14	Hedge			+105	63-71
			5" N. Pine		EUG 29
304	+100 41	+03	53		12 12
	Bag Hedge		3" Norway Pine		

+95	41	+93	53		PP 27
	3" Juniper		3" Pine	+94	sewer xing
+74	53	+82	53		N.W. Cor
	3" Norway Pine			+82	63
+98	53		3" Jun		

		+60	56		EUG 34
+50	+55		56		

	+48	3" S. Juniper 56		Gas +20 X-ing
+15	S.E. Cor Ho 81		3" Juniper 56	
	2" Pine	+36	56	+14
+17	55			sewer xing

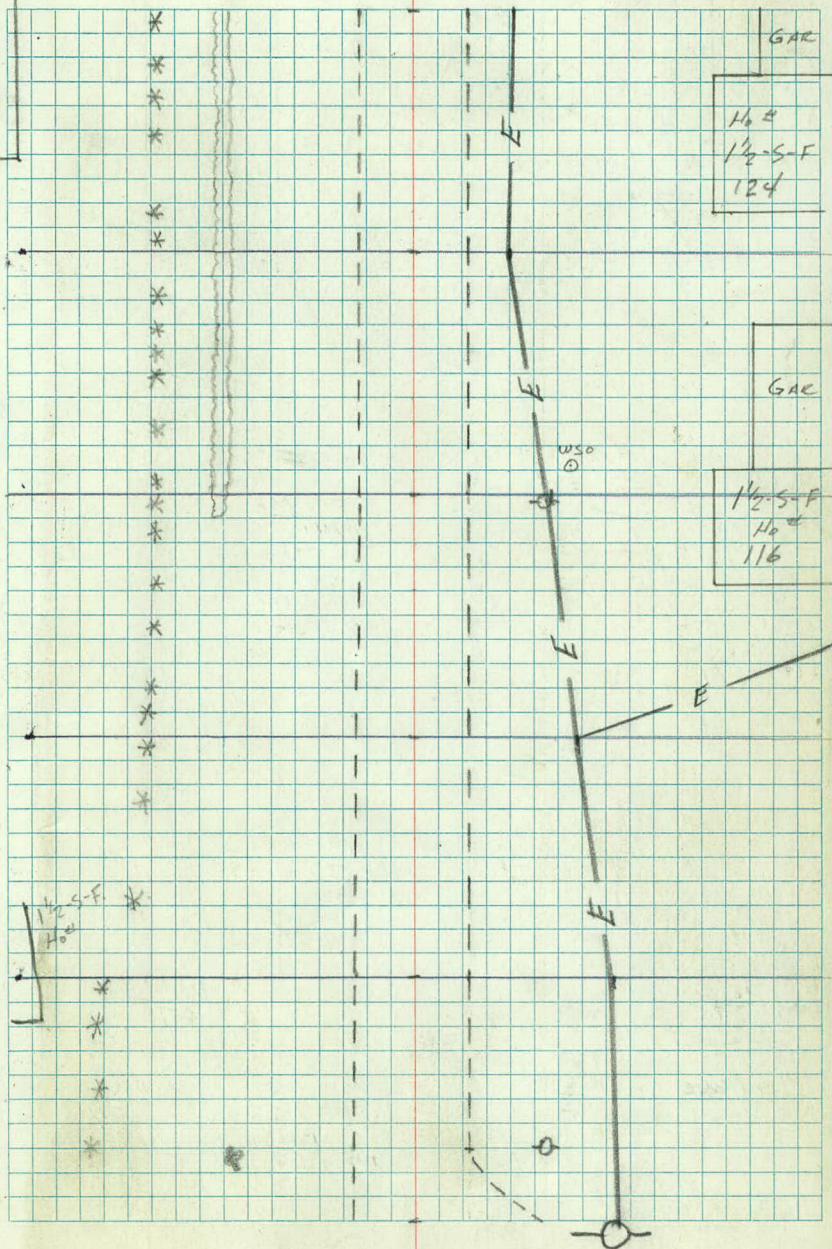
303					EUG 42
+91	Cor Ho 79	+98	2" Pine 60	+72	R.Tie 60
	2" Pine		2" Pine	+65	SW Cor Ho 97
+77	63	+90	68		R.Tie
	Hedge		3" Pine	+99	N-side Ho
+63	38	+65	63		ER 12
					PP 27
				+64	
				+45	

+50

LT

27 DEC. 1972
RT

5.



R-

+50 Prop Iron
33

$$\begin{array}{r}
 5-6'' \text{ Ash} \\
 + 34 \quad 41 \\
 \hline
 6'' \text{ Ash} \\
 + 20 \quad 55 \\
 \hline
 \text{N.E. COR Ho} \\
 + 08 \quad 65
 \end{array}$$

306 + 00 Hedge
35

1212
Sewer
+98 X-ing

$$\begin{array}{r} 485 \overline{) 19000} \\ \underline{1930} \\ 100 \\ \underline{970} \\ 300 \\ \underline{295} \\ 50 \end{array}$$

Сок. Но.
+85 65-47

Hedge Cor

+50	+51	35
-----	-----	----

+34 $\frac{12'' \text{ CMP.}}{25}$ +38 $\frac{12'' \text{ Ash}}{47}$

$+40$ N.W. Core Ho
67

+13	83	+22	Ent (Bit 14')
-----	----	-----	---------------

End Hedge +10 35 Tw 8" Maple +12 12" Ch 25

$$+30 \quad \frac{P^2}{23.5} \quad +19 \quad \frac{N.E. \text{ COR HO}}{74}$$

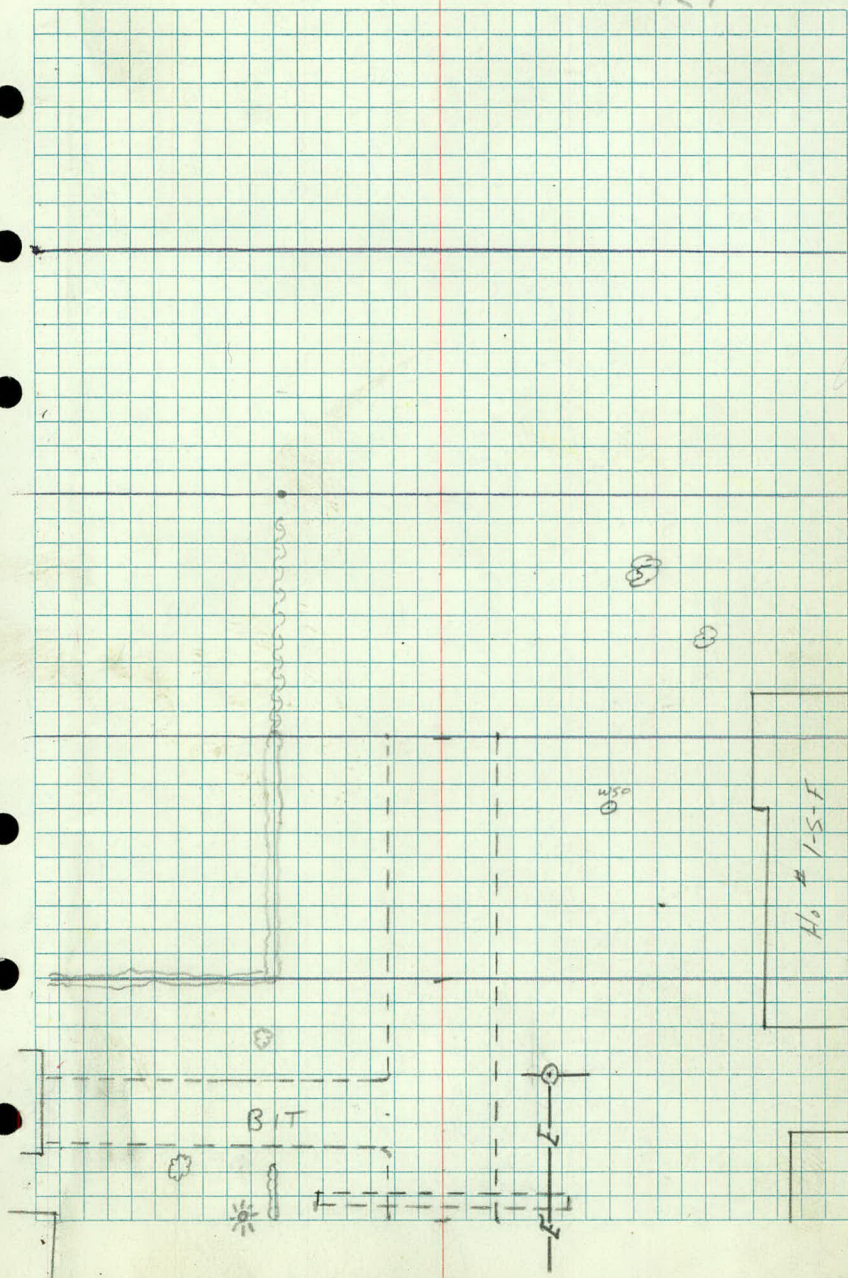
$+04$ 55 $+04$
 Yd. Litz 26
 52

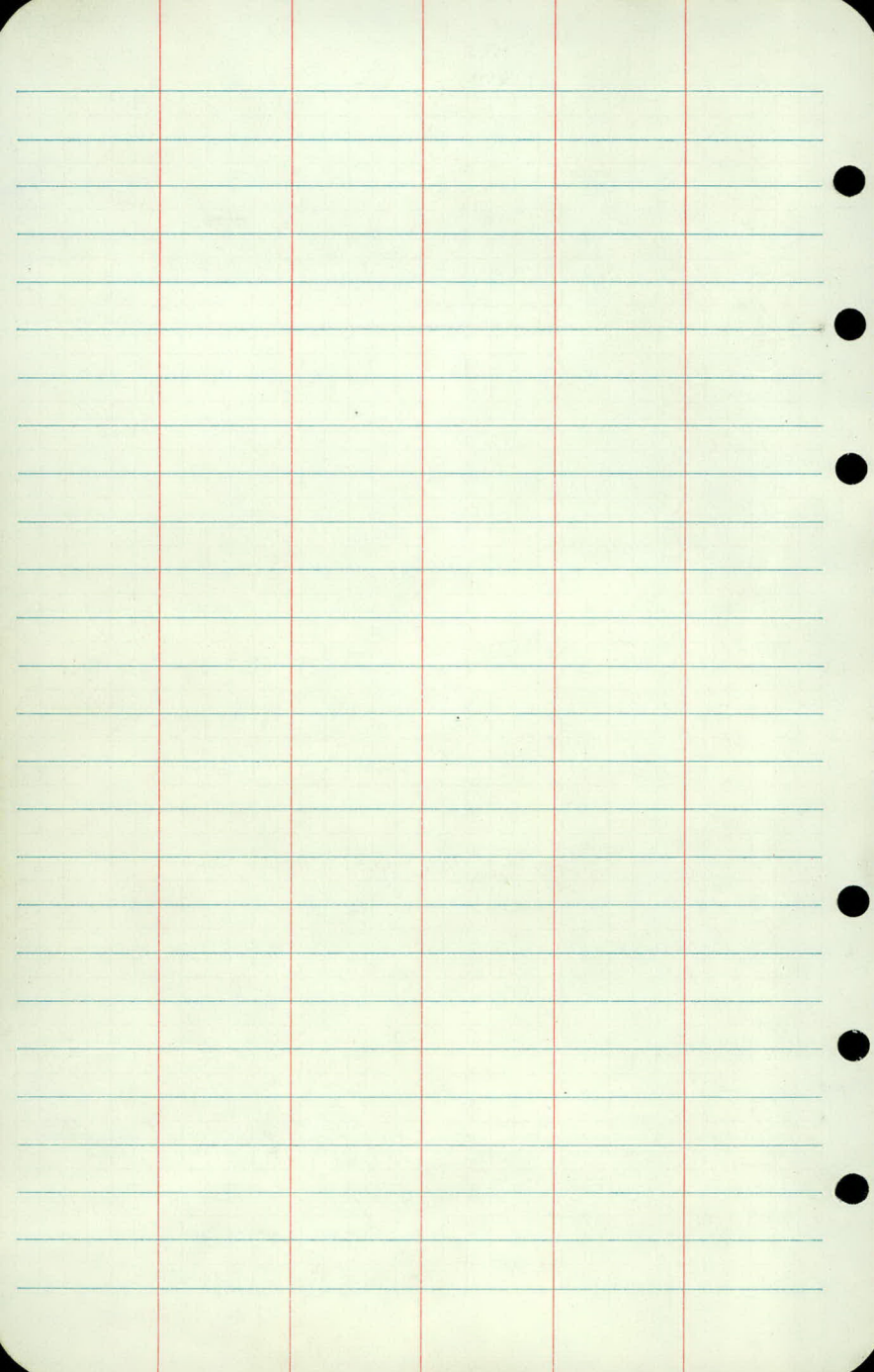
305 401 42 402 81 12 12

LT

27 DEC. 1972
RT

6.





J.A.
L.P.D.
D.S.
B.W.

March 25, 1977
Windy

9

Additional Cross-Sections

Old Co Rd "C" from Jackson St

to LAKE SHORE AVE

Sta	+	π	-	ELEV	
B.M.	12.71	945.02			932.31
302+80			10.12	934.90	
B.M.	2.04	938.69	8.37	936.65	
304+27			8.29	930.40	
305+00			10.79	927.90	
305+90			9.64	929.05	
T.P.	1.20	929.47	10.42	928.27	
B.M.			4.57	924.90	
T.P.	13.57	939.81	3.23	926.24	
B.M.			7.47	932.34	932.31
			3.14	936.67	936.65
TP				927.90	
305+04				923.84	
305	$\angle$			930.27	
+04				923.90	
+04				926.14	
+04				926.08	

J.A.
LPD
D.S.

MARCH 25, 1977
Windy 45° 10

Top Hyd N.E. Cor E. ROSE & DEXMONT

Top GARAGE SLAB Lt.

Top Hyd JACKSON & OLD Co Rd "C" (North of "C")

Top GARAGE SLAB Rt Ho^e 116

Top GARAGE SLAB Rt Ho^e 124

No FLOOR in YET

PROP IRON 306+50 Lt

Top Hyd LAKESHORE & OLD Co Rd "C"

Top 24" RCP 305+50 ±

Top Hyd N.E. Cor E ROSE & DEXMONT

Top Hyd "C" & JACKSON (Side shot)

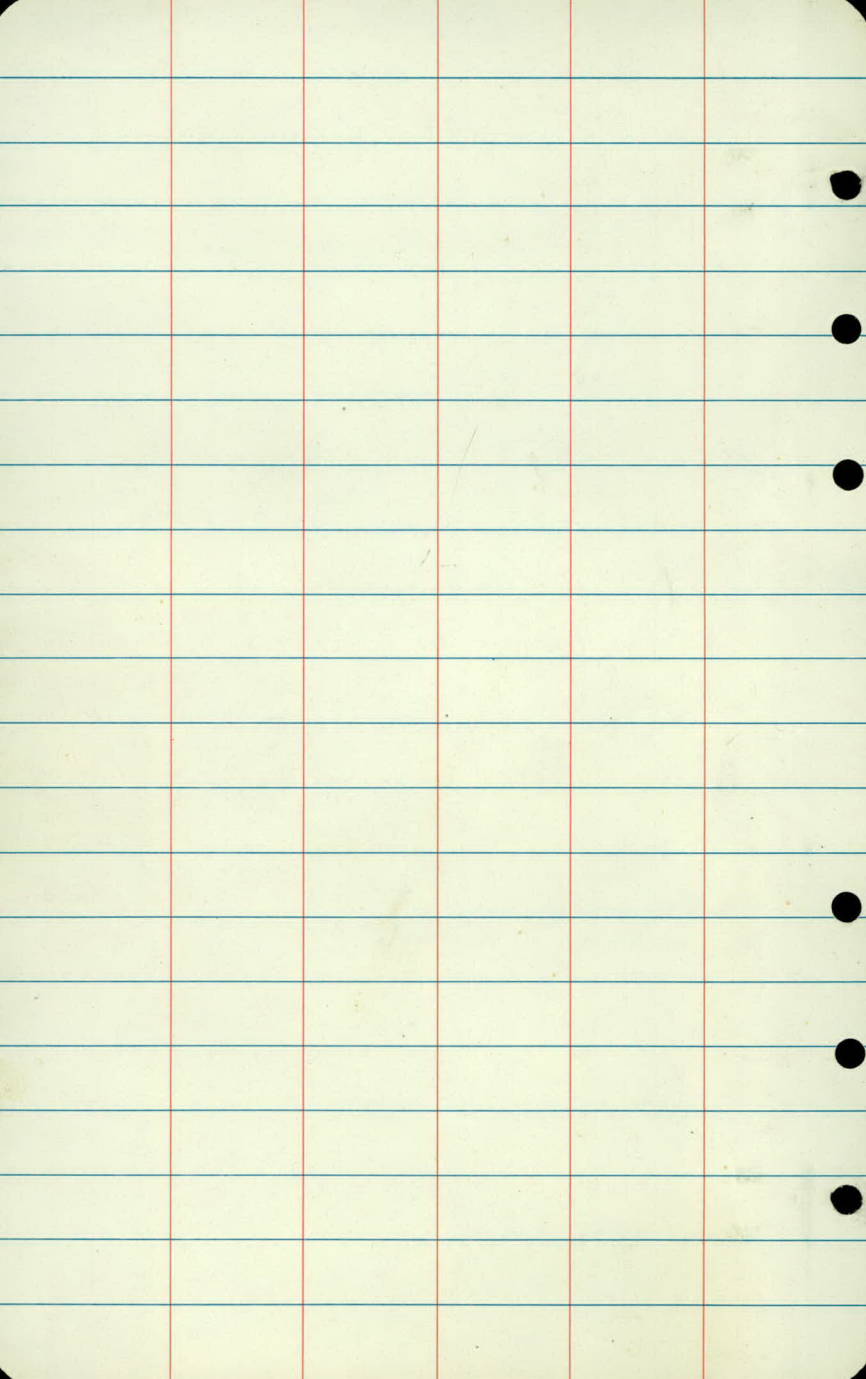
Garage slab #124

Inv S. End

Inv N End

Top N End

Top S End



KP
DS
LPD
GA

28 DEC, 1972
CLOUDY 25° 3

CO. RD C

RICE ST. TO LAKESHORE DR.

X- SECTIONS

Pages 3-13

STA + T → ELEV.

BM 9.31 95830

948.997

295

✓

+44 = GUTTER RT (W)

✓

+56 = £ STARK

✓

LT

L

28 DEC. 1972

RT

4

SPIKE IN PP N.W. COR. STARK

8 A ^{5.8}	A ^{6.1}	50.1	50.1	50.6	50.6	50.0	54.3	55.2
12.5	11.9	8.2	7.6	7.7	7.7	8.3	4.0	3.1
50	32	18	12		11	23	44	50

7 A ^{10.7}	3 A ^{11.0}	50.1	2 51.2	51.4	51.8	8 51.8	1 52.1	0 52.1
11.6	11.0	7.6	7.1	6.9	6.8	6.5	5.6	4.7
50	36	18	12		11	28	50	82

7.1 A ^{11.1}	0 A ^{11.0}	50.1	51.4	51.7	51.8	3 52.1	0 53.0	7 53.1
11.2	10.7	7.8	6.9	6.6	6.5	6.0	5.3	4.6
50	37	18	12		11	35	59	100

STA + π - ELEV.

958,30

+69 = GUTTER RT (E.)

✓

+90

✓

296

✓

LT

28 DEC. 1972

RT

5

A7.2

A7.9

51.0

51.6

51.9

52.2

52.4

52.9

53.3

11.1

10.4

7.3

6.7

6.4

6.1

5.9

5.4

5.0

50

36

18

12

12

34

60

79

8

A7.5

A7.9

51.5

52.3

52.5

52.5

52.5

52.9

53.4

10.5

7.6

6.8

6.0

5.8

5.8

5.8

3.4

2.9

50

35

18

12

12

23

40

50

A

5

0

A8.5

A9.5

52.0

52.6

52.7

52.7

52.7

52.8

52.8

53.0

9.9

8.8

6.3

5.7

5.6

5.6

5.6

5.5

3.5

2.7

50

34

18

12

11

17

24

37

50

STA + π - ELEV.

958.30

+50

✓

+71 $\neq$ ENT. RT.

✓

297

✓

LT

28 DEC. 1972

RT

C

8.7	5.1	5.5	5.9	5.6	5.7	5.7	5.9	5.4	5.0
9.6	8.2	6.8	5.4	4.8	4.6	4.6	4.4	2.9	2.3
50	32	28	18	12		12	21	34	50

4.0	5.5	2.6	2.0	5.0	5.8	5.0	5.9	5.1	5.5
4.3	4.8	5.7	6.3	5.2	4.5	4.3	4.4	4.2	2.8
50	37	34	28	20	12		12	26	50

5.8	5.5	5.8	5.6	5.4	5.1	5.3	5.2	5.1	5.4	5.6
4.5	4.9	5.5	5.7	4.9	4.2	4.0	4.1	4.2	2.9	1.7
50	35	32	26	18	11		12	22	32	50

STA + TP - ELEV.

958.30

+50

TP

3.20 955.10

TP

4.27

959.37

955.10

471

Left Rt

+94

Left Lt

298

LT

E

28 DEC 1972

RT

7

5A.2	5A.8	5A.2	5A.9	5A.4	5A.7	5A.6	5A.6	5A.6	5A.7
4.1	4.5	5.5	4.4	3.9	3.6	3.7	3.7	2.7	1.6
50	35	27	18	11		12	25	38	50

TOP PK E STA 298

 RG
 DS
 LPD
 GA

 Jan 2, 1973
 Clear 10°

5A.3	5A.0	5A.3	5A.2	5A.7	5A.9	5A.9	5A.1	5A.2
5.1	5.4	6.1	5.2	4.7	4.5	4.5	4.3	3.2
43	35	28	18	11		9	28	57

5A.0	5A.1	5A.2	5A.9	5A.1	5A.0	5A.9	5A.4	5A.0
5.4	5.3	5.2	4.5	4.3	4.4	4.5	4.0	3.4
66	50	27	11		9	24	38	50

5A.0	5A.0	5A.4	5A.9	5A.1	5A.0	5A.8	5A.4	5A.1
5.4	5.4	5.0	4.5	4.3	4.4	4.6	4.0	3.3
50	32	22	11		9	24	39	50

STA + π - ELEV.

959.37

298+40

+60

299

TP

2.39 957.51 4.25 955.12

298+95 = ∇ ENT LT

✓

L7

E

Jan. 2, 1973

RT

8

52.9	52.1	51.0	51.7	55.2	55.3	55.2	55.2	51.9	51.3	51.4
6.5	7.3	8.4	4.7	9.2	4.1	4.2	4.2	7.5	8.1	8.0
50	39	32	17	10		10	14	26	43	50

50.1	50.3	52.1	54.4	55.2	55.3	55.2	55.2	49.7	48.1
9.3	9.1	7.3	5.0	4.2	4.1	4.2	4.2	9.7	11.3
50	39	30	18	11		10	16	29	50

49.8	51.6	51.8	51.1	55.2	55.0	55.2	45.3	44.0
9.6	7.8	4.6	4.3	4.2	4.4	4.2	14.1	15.4
50	38	19	11		10	16	38	50

PK no. 1 & sta 299400

47.8	48.8	51.4	54.1	54.9	55.2
9.7	8.7	6.1	3.4	2.6	2.3
75	59	40	25	16	

47.2
10.3
100

STA + π - ELEV.

957.51

299+50

300

+29 = $\neq$ ENT LT

+43 = W. ABUTMENT

TP 0.95 953.79 4.67 952.84

301+42 = E. ABUTMENT

53.6

FK
KP
LPD
GR

LT

10 JUN. 1973
CLOUDY
0°

PT

9

A ^{8.1}	A ^{7.9}	A ^{8.6}	A ^{8.6}	A ^{8.8}	A ^{8.8}	A ^{8.6}	A ^{8.1}	A ^{8.5}	A ^{8.9}
9.4	9.6	8.9	2.9	2.7	2.7	2.9	6.4	12.0	14.1
50	36	30	18	10		14	24	37	50
45.9	45.9	48.8	5 ^{2.2}	5 ^{4.6}	5 ^{4.6}	5 ^{4.6}	5 ^{4.2}	A ^{4.2}	A ^{2.9}
11.6	11.6	8.7	4.3	3.0	2.9	2.9	3.1	3.3	13.2
50	39	32	24	17	11		9	15	37
A ^{7.5}	A ^{8.6}	A ^{8.8}	A ^{8.1}	A ^{8.6}	A ^{8.8}	A ^{8.5}	A ^{8.2}	A ^{8.1}	A ^{7.9}
10.5	8.9	6.7	5.8	3.9	2.9	3.0	3.3	3.4	10.1
100	75	50	43	24	10		10	15	30
A ^{9.1}	A ^{8.2}	A ^{8.1}	A ^{8.9}	A ^{8.5}	A ^{8.3}	A ^{8.3}	A ^{8.6}	A ^{8.2}	A ^{8.9}
7.8	6.3	5.4	3.6	3.0	3.2	3.2	3.9	11.3	13.6
50	36	28	17	10		11	14	28	38

PK & STA 301

A ^{1.0}	A ^{1.4}	A ^{5.8}	A ^{5.7}	A ^{5.6}	A ^{5.5}	A ^{8.9}	A ^{2.0}	A ^{0.9}
12.8	12.4	8.0	2.1	2.2	2.3	9.9	11.8	12.9
50	44	26	10		11	28	41	50

STA + π - ELEV.

953.79

301+30

302

+10 = GUTTER RT (W)

+20 $\pm$ JACKSON

+33 = GUTTER RT (E)

+50

BM 0.83 943.37 11.24 942.55 (942.54)

K10

DS

LT

 11 JAN 1973 10,
 CLEAR 00 RT

LWD

GA

~~80.7~~
 80.7

x1.2

x5.7

x1.2

x1.2

x1.2

x1.2

x0.9

x5.0

x0.5

13.1 12.6 8.1 2.6 2.5 2.6 2.6 2.9 8.8 13.3

50 41 30 16 11 10 14 29 50

38.4

x0.6

x4.5

x7.2

x7.5

x7.7

x7.5

x6.8

x0.9

x9.5

15.4 13.2 9.3 6.6 6.3 6.1 6.3 7.0 12.9 14.3

50 40 29 18 11 11 19 41 50

x0.0

x1.8

x6.5

x6.7

x7.0

x6.7

x4.6

x2.1

x0.3

x8.4

13.8 12.0 7.5 7.1 6.8 7.1 9.2 11.7 13.5 15.4

50 38 22 12 11 32 55 75 100

x8.1

x0.0

x4.8

x6.1

x6.2

x6.0

x5.7

x3.0

x1.0

x8.7

15.7 13.8 9.0 7.7 7.6 7.8 8.32 10.8 12.8 15.1

50 35 22 12 12 19 46 70 100

MH

x4.4

x6.4

x4.7

x5.2

x5.4

x5.1

x4.5

x1.1

x8.2

19.4 17.4 9.1 8.6 8.4 8.7 9.3 12.7 15.5

50 37 16 11 10 31 66 100

x3.2

x3.7

x3.2

x4.2

x4.2

x3.7

x3.1

x9.7

x5.9

20.6 20.1 10.6 9.6 9.6 10.1 10.7 14.1 17.9

50 40 16 11 11 19 34 50

SPIKE IN PP S.E. COR JACKSON C

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		943.37		
--	--	--------	--	--

303				
-----	--	--	--	--

+50				
-----	--	--	--	--

304				
-----	--	--	--	--

TP	1.87	936.39	8.85	934.52
----	------	--------	------	--------

+50				
-----	--	--	--	--

LT

11 JAN 1973 11.
RT

31.7	32.0	39.4	40.3	40.3	40.1	39.4	32.4	30.4
11.7	11.4	4.0	3.1	3.1	3.3	4.0	11.0	13.0
50	34	17	11		10	19	39	50

29.4	29.8	35.7	36.8	36.9	36.6	35.9	29.4	29.4
14.0	13.6	7.7	6.6	6.5	6.8	7.5	14.0	13.6
50	32	17	11		11	20	43	50

28.8	28.4	33.3	34.3	34.6	34.3	34.1	29.3	28.3
14.6	15.0	10.1	9.1	8.8	9.1	9.3	14.1	15.1
50	28	17	11		11	17	31	50

PK & STA 304

28.0	28.0	27.3	31.2	32.5	32.5	32.3	31.8	28.2	27.1
8.4	8.4	9.1	5.2	3.9	3.9	4.1	4.6	8.2	9.3
50	38	26	17	11		11	17	31	50

STA + π - ELEV.

936.39

305



+21 = $\neq$ ENT LT BIT

+50

+50

306

306

+50

LT

11 JAN. 1973 12.
RT

28.1	26.3	26.1	29.3	30.3	30.4	30.2	29.8	24.9	23.5
8.3	10.1	10.3	6.9	6.1	6.0	6.2	6.6	11.5	12.9
38	32	26	18	11		11	16	29	50

28.1

8.3

50

30.6	29.4	29.3	29.7	29.7	29.5	28.6	24.9	22.9
5.8	7.0	7.1	6.7	6.7	6.9	7.8	11.5	13.5
82	51	24	12		10	17	25	50

GA

28.7

7.7

27.5

8.9

26.6

9.8

STA + π - ELEV

936.39

307

TP 7.23 941.75 1.87 934.52

5.07 936.68 (936.67)

BM 1.86 936.38 (934.52)

307 10.5 25.9

+50 11.3 25.1

308 12.2 24.2

+50 13.2 23.2

BM 8.43 942.95 1.86 934.52

BM 0.42 942.53 (942.54)

LT

11 JAN 1973 13.
RT

25.9

10.5

STA 304

TOP HYD LT STA 302+60

PK STA 304

PK STA 304

SPIKE IN PP S.E. COR JACKSON C

STA

+

π

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ELEV.