

LK. 7 BK. 72

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

RED Fox RD.

From HAMLIN To LEXINGTON

Road Acc't. No. 131

Date Filed 12-1-69 File _____

13 FEB 1969

1

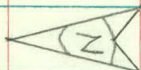
0+00 = 181.26 E. OF CTR OF SECTION

RED FOX RD.
HAMLINE TO LEXINGTON
PLAN SURVEY

24+50

LEXINGTON AVE

263034



2449.80
181.24
2631.06

2450.00

40.0 iron 40.0

iron
122.12

0+00

27.99

181.26

0-181.26

HAMLINE AVE

LT

E

RT

2

26 + 31.26

□ E $\frac{1}{4}$ Ctr 527 T30 R23

2450.00

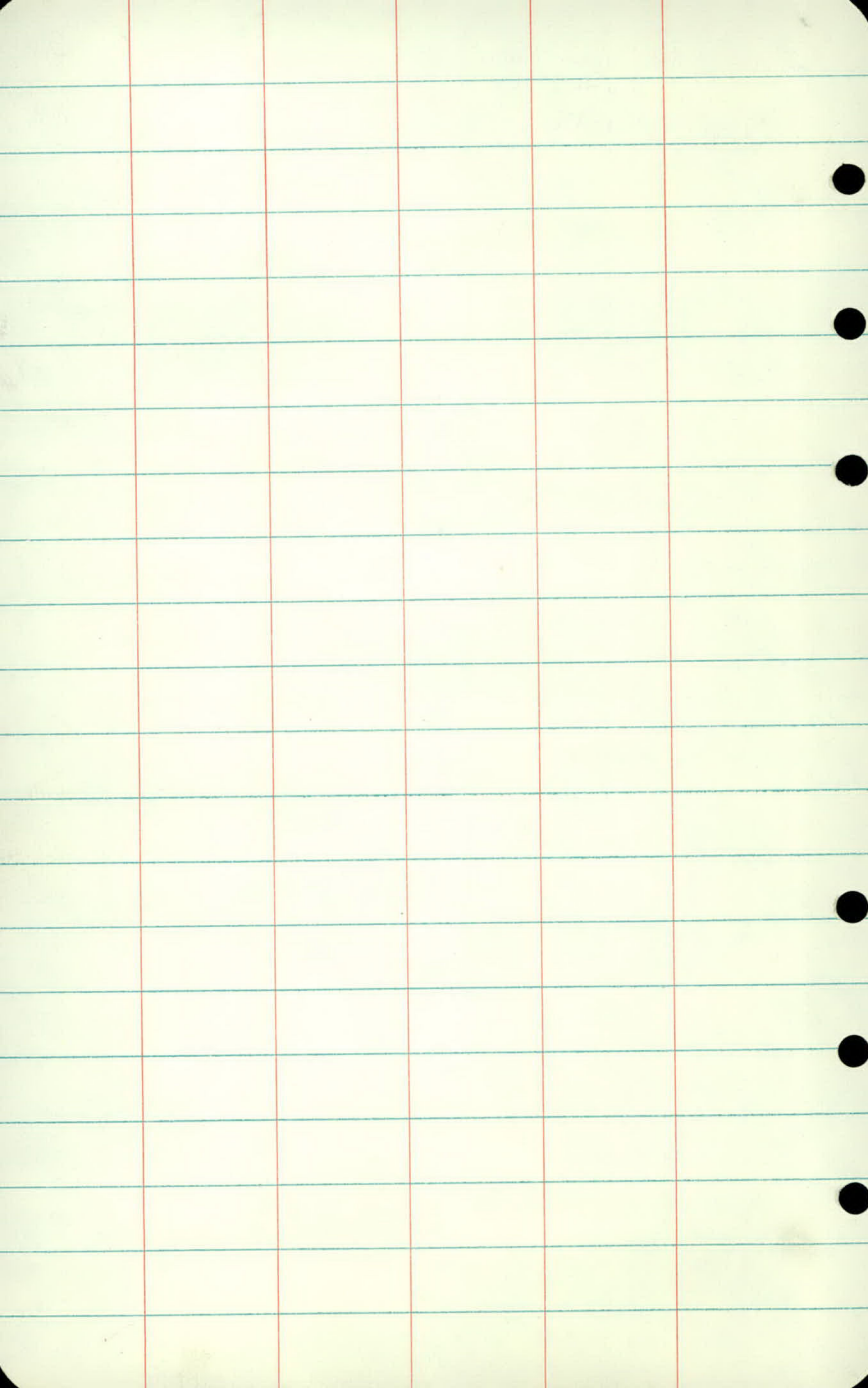
40.00 Iron 122.12

1100
100
Iron

0400

18126
27.97

□ CTR 527 T30 R23



FK
PK
CM
AS

June 27, 1969

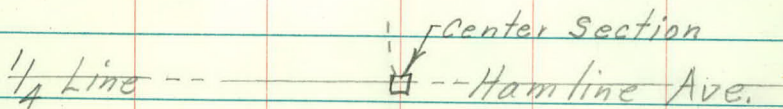
3

Alinement

Sta	Point	$\Delta Lt.$	$\Delta Rt.$
0+00			

0+00

4



Sta	Point	ΔLt	ΔRt
-----	-------	-------------	-------------

P.O.T.

POT

E Dunlap

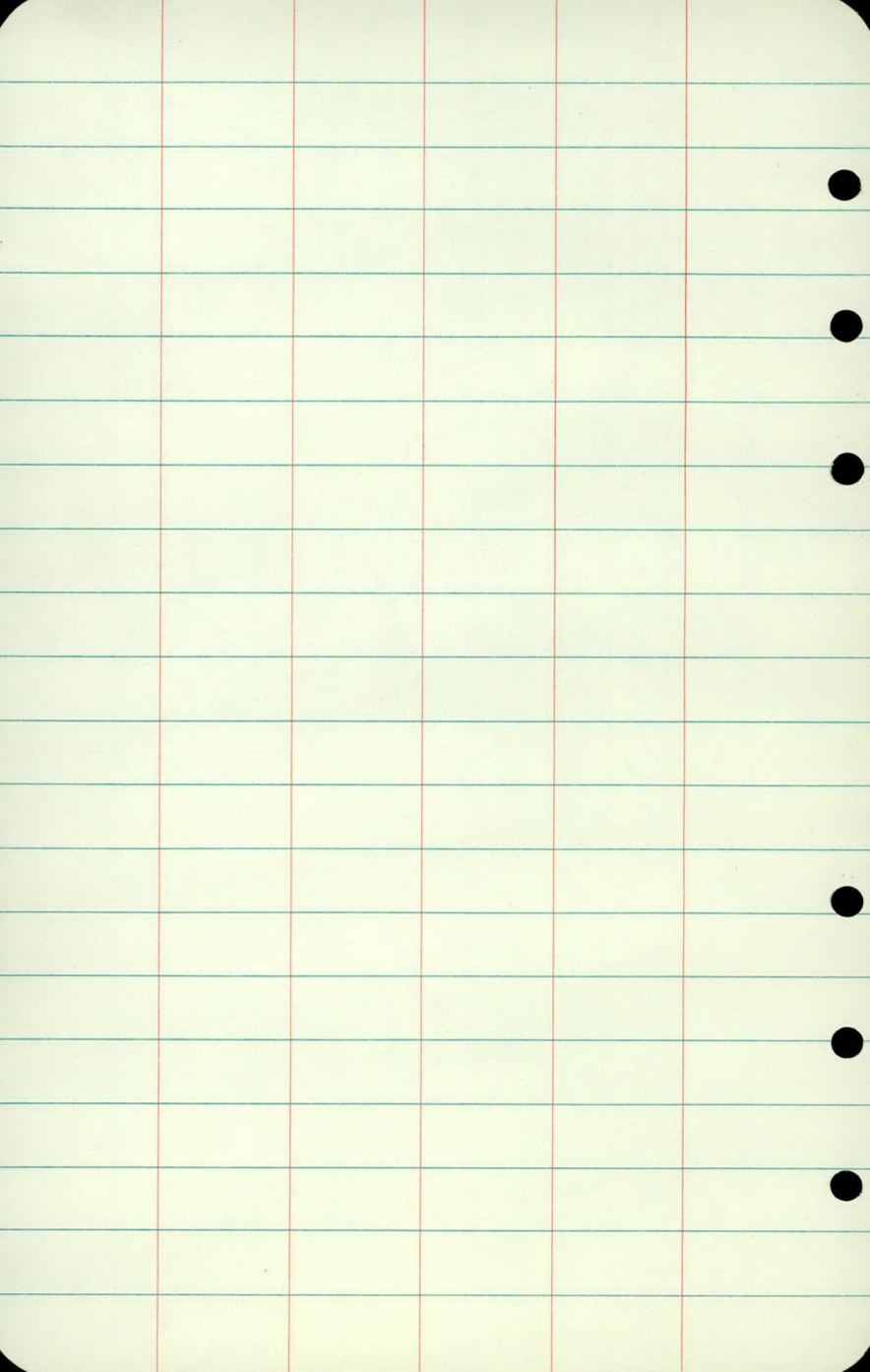
24+49.80 P.O.T.

FK
PK
CM
AS

June 30, 1969

6

£ Lexington



PROFILE

HAMLIN TO LEXINGTON

STA	+	π	-	ELEV
BM	4.25	941.21		936.96
0-71				
0-61				
0-41	$\neq$	DITCH		
0-23				
0+00				
+50				
1+00				
+50				
2+00				
		12.08	929.13	929.12

LT

£

RT

8

TOP HYD LT 0-12

33.5

7.66

33.1

8.1

29.8

11.4

31.9

9.3

32.3

8.9

31.2

10.0

29.5

11.7

29.3

11.9

28.6

12.6

TOP HYD LT 24 23

STA	+	π	-	ELEV
		941.21		
2+50				
3				
+50				
4				
+50				
5				
+50				
6	10.86	944.61	7.46	933.75
BM		9.90	934.71	934.72

LT

~~4~~

RT

9

29.5
11.7

30.3
10.9

32.1
9.1

32.6
8.6

32.9
8.3

32.6
8.6

32.5
8.7

33.7
7.5

~~4~~ STA 6

TOP HYD

LT 5x85

STA	+	π	-	ELEV
-----	---	-------	---	------

		944.61		
--	--	--------	--	--

6+50				
------	--	--	--	--

7				
---	--	--	--	--

+50				
-----	--	--	--	--

8				
---	--	--	--	--

+50				
-----	--	--	--	--

9				
---	--	--	--	--

BM				
----	--	--	--	--

	4.87	939.74	939.73	
--	------	--------	--------	--

+50				
-----	--	--	--	--

LT

~~E~~

RT

10

35.3
9.3

37.3
7.3

39.1
5.5

39.5
5.1

40.0
4.6

39.9
5.2

TOP HYD LT STA 9

39.5
5.1

STA	+	T	-	ELEV
-----	---	---	---	------

		944.61		
--	--	--------	--	--

10				
----	--	--	--	--

+50				
-----	--	--	--	--

11				
----	--	--	--	--

+50				
-----	--	--	--	--

12				
----	--	--	--	--

+50				
-----	--	--	--	--

13				
----	--	--	--	--

+50				
-----	--	--	--	--

14				
----	--	--	--	--

BM	2.14	941.02	5.73	938.88
----	------	--------	------	--------

L_T

£

R_T

11

5.3^{39.3}5.0^{39.6}4.7^{39.9}5.4^{39.2}6.0^{38.6}7.0^{37.6}7.4^{37.2}7.6^{37.0}7.9^{36.7}

TOP HYD SW Cor DUNLAP

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		941.02		
--	--	--------	--	--

14+50				
-------	--	--	--	--

15				
----	--	--	--	--

+50				
-----	--	--	--	--

16				
----	--	--	--	--

+50				
-----	--	--	--	--

17				
----	--	--	--	--

+50				
-----	--	--	--	--

18				
----	--	--	--	--

+50				
-----	--	--	--	--

LT

E

RT

12

37.0
4.0

36.3
4.7

36.1
4.9

36.0
5.0

36.1
4.9

36.0
5.0

35.7
5.3

35.1
5.9

34.8
6.2

STA	+	K	-	ELEV
-----	---	---	---	------

		941.02		
--	--	--------	--	--

19				
----	--	--	--	--

+50				
-----	--	--	--	--

20				
----	--	--	--	--

+50				
-----	--	--	--	--

21				
----	--	--	--	--

+50				
-----	--	--	--	--

22				
----	--	--	--	--

+50				
-----	--	--	--	--

23				
----	--	--	--	--

TP	10.85	946.96	11.91	936'.11
----	-------	--------	-------	---------

LT

E

19 FEB 1969

RT

13

6.1
34.96.5
34.56.7
34.36.9
34.17.0
34.07.1
33.96.9
34.16.4
34.64.9
36.1

E STA 23

STA	+	π	-	ELEV
-----	---	-------	---	------

		946.96		
--	--	--------	--	--

23+50				
-------	--	--	--	--

24				
----	--	--	--	--

+50	TOP	MONT		
-----	-----	------	--	--

BM				
----	--	--	--	--

	2.50	944.46		
--	------	--------	--	--

LT

~~LT~~

RT

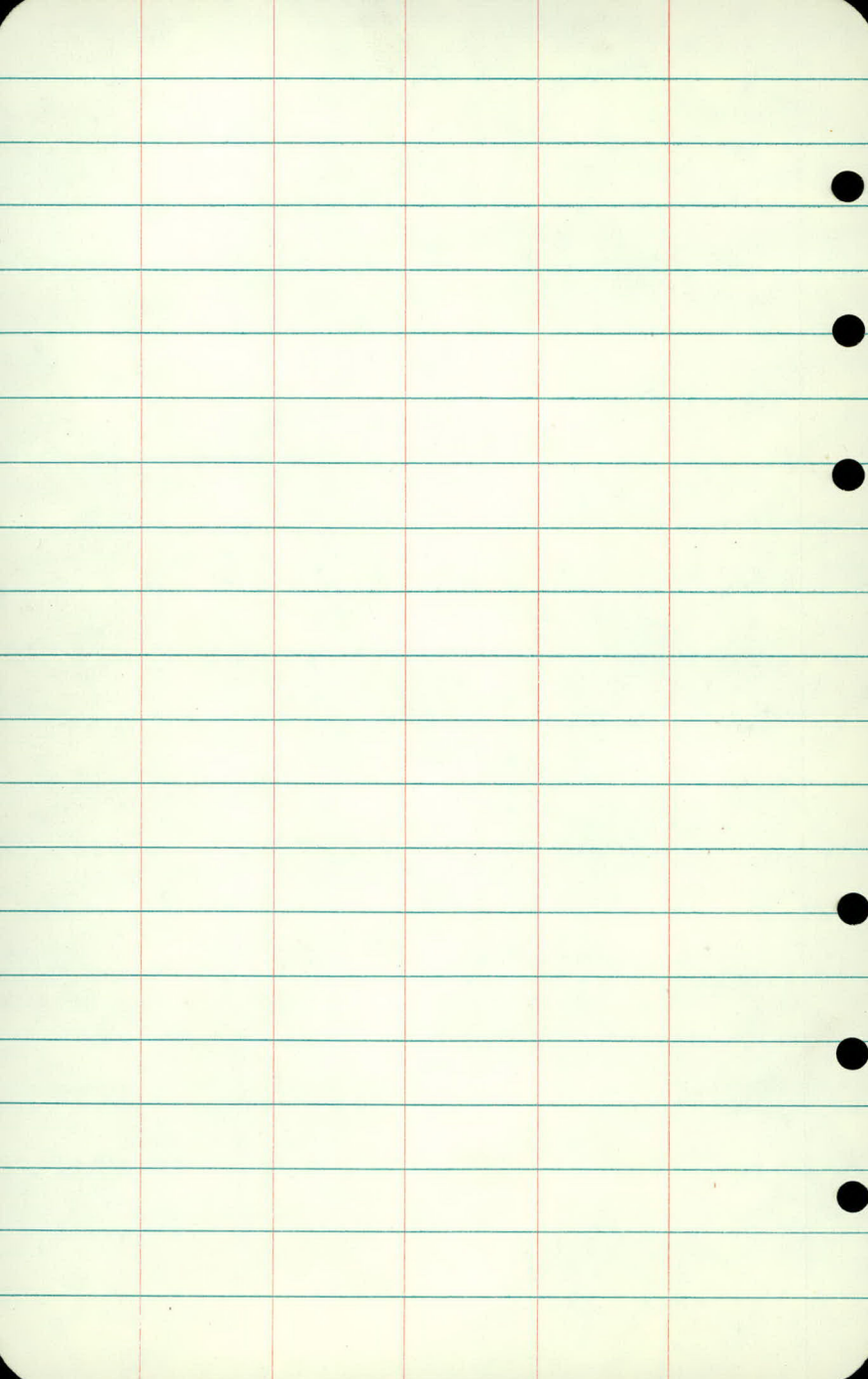
14

~~38.6~~
8.9

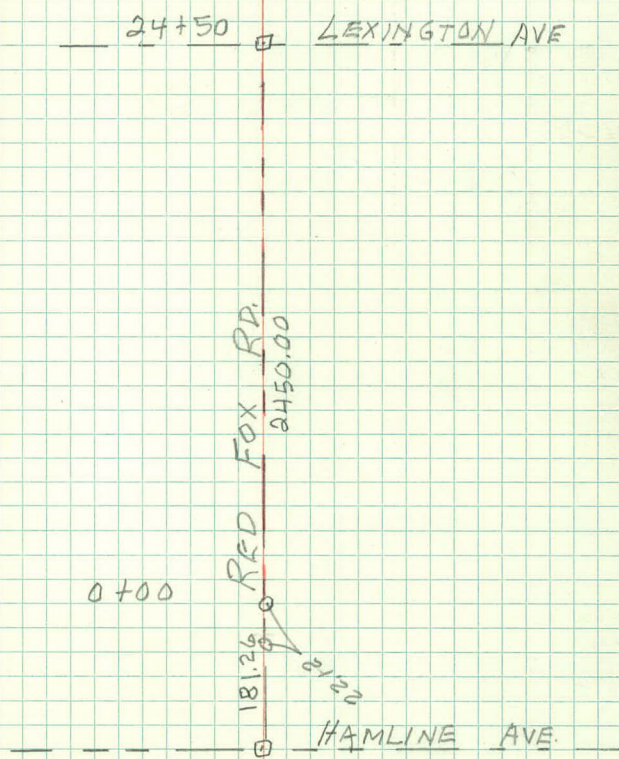
~~40.9~~
6.1

~~42.43~~
4.53

↳ SPIKE IN PP NE COR LEX.



TOPOGRAPHY



0+00

LT

 $\frac{RD}{4}$ $\frac{RD}{21}$

RT

0-07 PP
280-12 HYD
270-07 BR
260-06 POR
280-19 $\frac{1}{2}$ Service drive0-31 BR
53

0-31 wedge BT

0-50

0-61 E EDGE BT

0-71 E. EDGE CONC.

0-95 WEDGE CONC.

0-100

0-150

0-200

0-250

16

○
T



BIT Shoulder

694

$\begin{array}{r} \downarrow +50 \\ +33 \text{ 6" Poplar} \\ \hline 32 \\ +32 \text{ 6" Poplar} \\ \hline 33 \\ +28 \text{ F.P.} \\ \hline 54 \end{array}$	$\begin{array}{r} \downarrow \\ \text{LT} \end{array}$	$\begin{array}{r} \text{F.E.} \\ \hline 28 \end{array}$	$\begin{array}{r} \downarrow \\ \text{RT} \end{array}$	$\begin{array}{r} +44 \text{ FE Cor} \\ \hline 34 \end{array}$
$\begin{array}{r} +35 \text{ P.P.} \\ \hline 28 \\ +35 \text{ FE Cor} \\ \hline 28 \end{array}$	$\begin{array}{r} +26 \text{ F.P.} \\ \hline 31 \\ +23 \text{ Hyd} \\ \hline 28 \end{array}$			

2+00

RD
9

RD
9

+73 N. End Culvert 18" x 44.0 CM
22

150

$$\begin{array}{r} \downarrow +28 \text{ 1" Birch} \\ \hline 60 \\ +27 \text{ 2" Birch} \\ \hline 61 \end{array}$$

$$\begin{array}{r} +07 \text{ PINE} \\ \hline 65 \\ +04 \text{ PINE} \\ \hline 80 \end{array}$$

1+00

+04 House Cor.
74

RD
13

RD
9

+67 8" ELM
21

450

+34 E 10' ENT

+24 +24 SW Cor 140
70

+16 6" PINE
68

+06 6" PINE
54

0+00

RD
4

+28 Iron
40

+22 ER
12

RD
21

3

 R_T

17

1-5-F #1315

iron

iron

5+00

$\frac{FE}{27}$ LT

$\frac{Rd}{9}$

$\frac{Rd}{9}$

$\frac{FE}{33}$

RT

+50

$\frac{FE}{28}$

$\frac{FE}{34}$

4+00

$\frac{FE}{29} + 94 \frac{PP}{28}$

$\frac{Rd}{9}$

$\frac{Rd}{9}$

$\frac{FE}{34}$

+50

$\frac{FE}{29}$

$\frac{FE}{34}$

3+00

+06 6" Plumb
 $\frac{FE}{28}$ 33

$\frac{Rd}{9}$

$\frac{Rd}{9}$

$\frac{FE}{34}$

2+50

$\frac{FE}{28}$

$\frac{Rd}{9}$

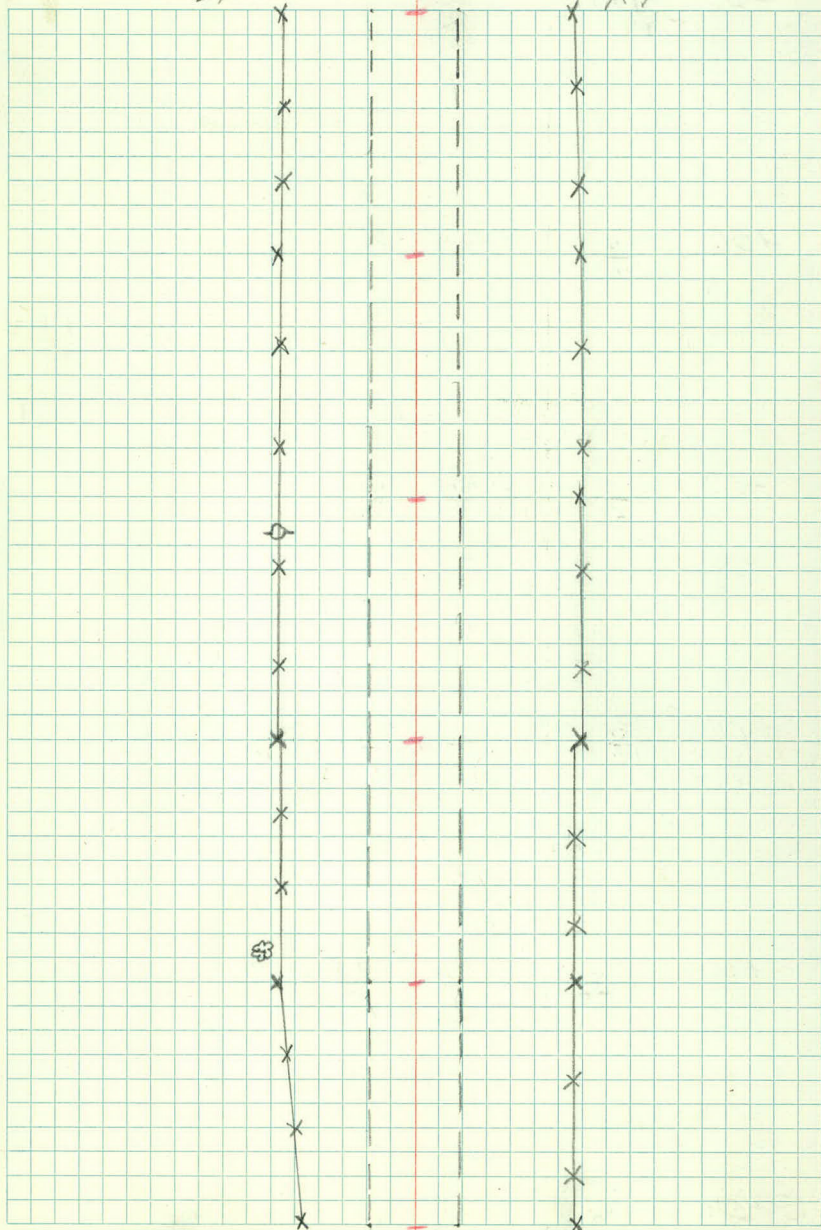
$\frac{Rd}{9}$

$\frac{FE}{34}$

LT

E

RT



+50

LT $\frac{FE}{28}$

~~F~~

RT

↓
+14 $\frac{P.P.}{28}$

7+00

$\frac{FE}{28}$

$\frac{Rd}{9}$

$\frac{Rd}{9}$

+50

$\frac{FE}{28}$

6+00

$\frac{FE}{29}$

$\frac{Rd}{9}$

$\frac{Rd}{9}$

✓
+18 $\frac{END FE}{31}$

$\frac{FE}{31}$

$\frac{4" PLUMB}{31}$

+85 $\frac{Hyd}{27}$

↓
+54 $\frac{P.P.}{28}$

+50

5+00

$\frac{FE}{27}$

$\frac{Rd}{9}$

$\frac{Rd}{9}$

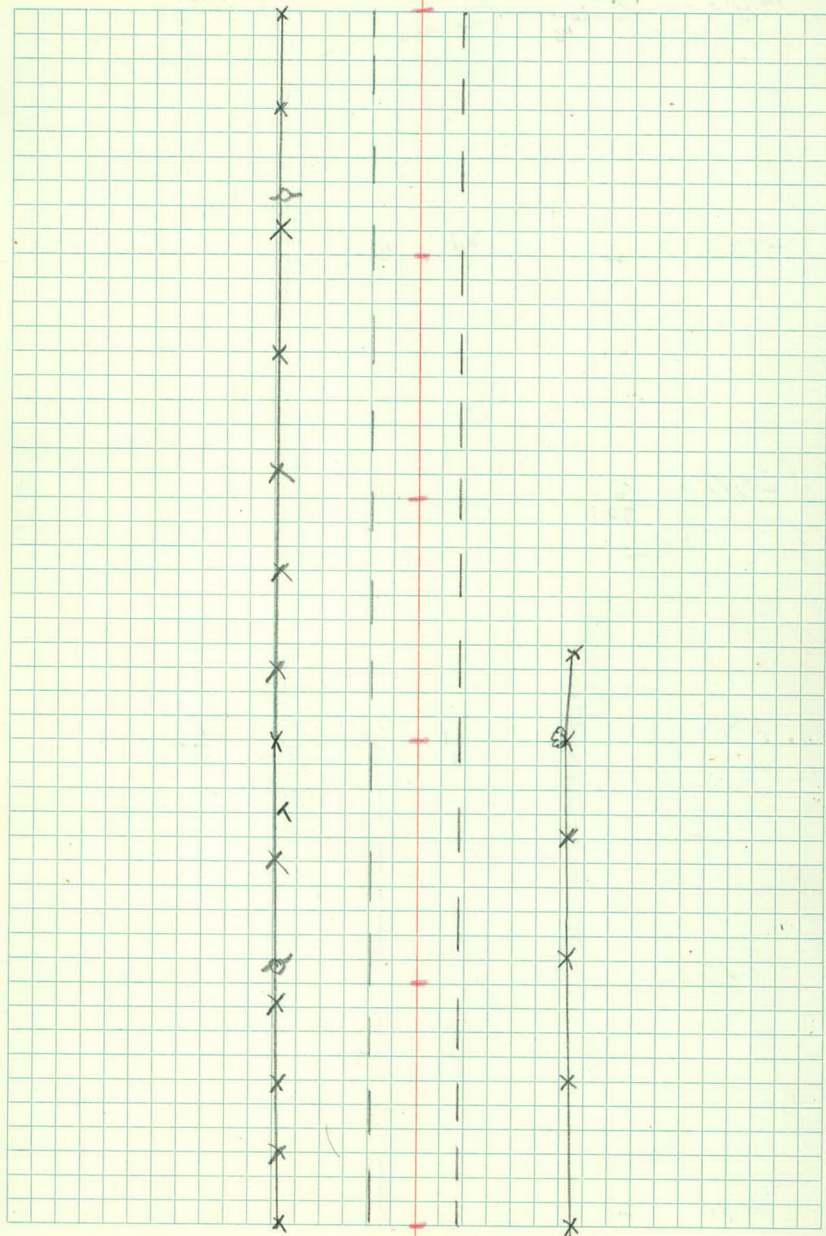
✓
 $\frac{FE}{33}$

LT

E

RT

19



10+00 $\frac{FE}{27}$ $\frac{LT}{27}$ $\frac{4" Willow}{26}$

$\frac{E}{27}$

$\frac{LILAC}{28}$ RT
 $\frac{+82}{37}$ $\frac{24" Oak}{37}$
 $\frac{+70}{41}$ $\frac{8 Ash}{41}$
 $\frac{+58}{37}$ $\frac{16" Cott Wood}{37}$
 $\frac{+54}{29}$ $\frac{BEGIN LILAC}{29}$

+50

$\frac{FE}{29}$
 $\frac{+31}{29}$ $\frac{TWIN APPLE}{29}$

$\frac{+16}{27}$ $\frac{4" Cott W}{27}$
 $\frac{+103}{28}$ $\frac{Hyd}{28}$

9+00

$\frac{FE}{30}$ $\frac{Rd}{9}$ $\frac{Rd}{9}$
 $\frac{+80}{28}$ $\frac{4" ELM}{28}$ $\frac{+75}{25}$ $\frac{P.P}{25}$

$\frac{+10}{26}$ $\frac{36" Maple}{26}$

$\frac{+71}{31}$ $\frac{TWIN Cott W.}{31}$

+50

$\frac{+46}{38}$ $\frac{14" C.W}{38}$
 $\frac{+38}{38}$ $\frac{31" C.W}{38}$

8+00

$\frac{FE}{28}$ $\frac{Rd}{9}$ $\frac{Rd}{9}$

$\frac{Triple}{34}$ $\frac{14" B.E}{34}$

$\frac{+89}{30}$ $\frac{10" B.E}{30}$

$\frac{+55}{38}$ $\frac{4" ELM}{38}$

7+50

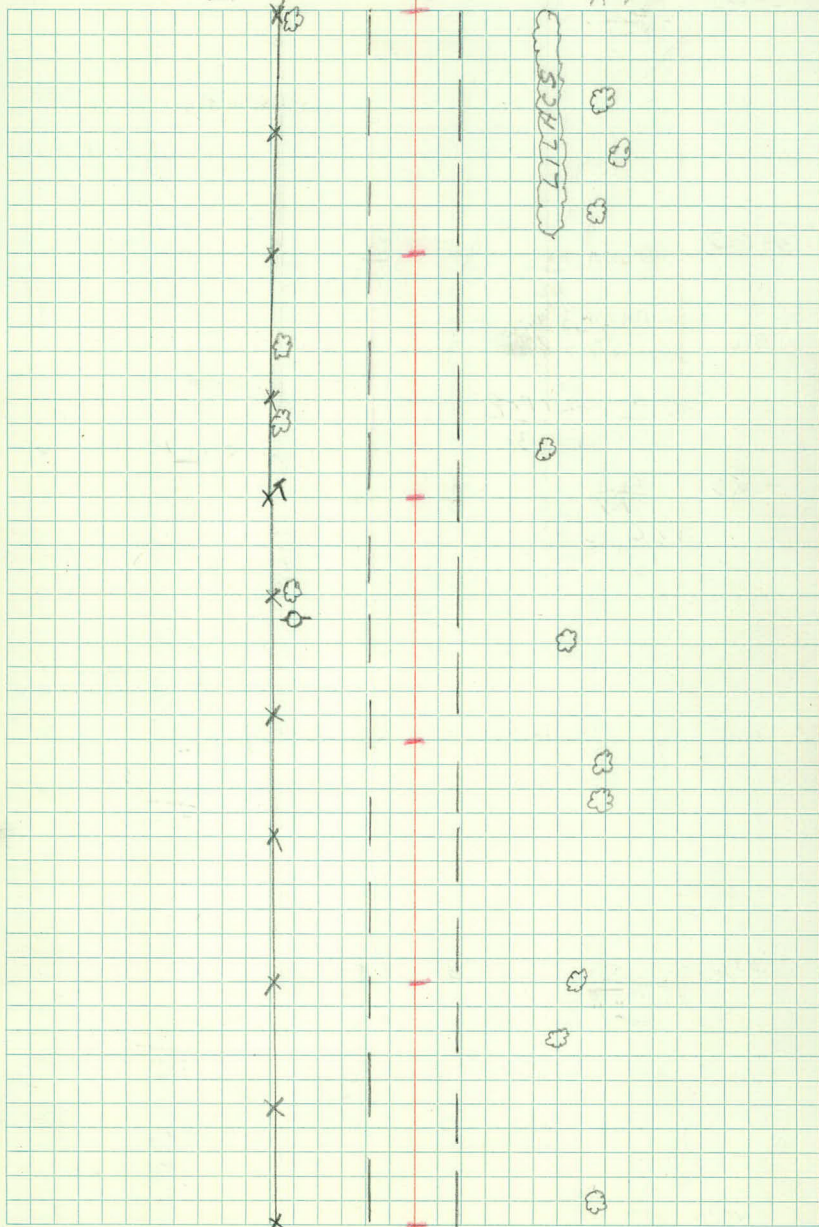
$\frac{FE}{28}$

LT

~~E~~

RT

20



+50

 $\frac{FE}{92}$ LTWOODS
54-90

E

RT

12+00

 $\downarrow$
+99 $\frac{PP}{28}$ $\frac{Rd}{9}$ $\frac{Rd}{9}$ $\downarrow$
+80 $\frac{FE}{90}$ +80 $\frac{BEGIN WOODS}{54-90}$ $\downarrow$
+67 $\frac{FE}{31-NORTH}$ +67 $\frac{FEP}{31}$

+50

+66 $\frac{Hyd}{24}$ $\downarrow$
+35 $\frac{MH}{2}$ $\downarrow$
+52 $\frac{FEP}{38}$ $\downarrow$
+30 $\frac{FEP}{36}$ $\downarrow$
+06 $\frac{FEP}{36}$ +08 $\frac{WGV}{16}$ 11+00 $\frac{FE}{27}$ $\frac{END TREE}{39}$ $\frac{Rd}{9}$ $\frac{Rd}{9}$ $\downarrow$
+80 $\frac{PP}{30}$
+77 $\frac{END LINE}{30}$ $\downarrow$
+52 $\frac{24" B.E.}{35}$ $\downarrow$
+50 $\frac{TREES FE}{30-40}$ 29 $\downarrow$
+39 $\frac{PP}{28}$ $\downarrow$
+16 $\frac{TREES}{25-40}$ $\downarrow$
+41 $\frac{24" B.E.}{35}$

10+00

+06 $\frac{NW Cor Bldg}{90}$ BrickTransformer B₉ NE Cor.
Possible Pump House

LT

E

RT

21

d

TREES

N 20.1 E
E 34.7 W

15+00

$$\begin{array}{r} \text{Woods T} \\ 39-66 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 15 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 20 \end{array}$$

+91

+80

+75

$$\begin{array}{r} \text{RT} \\ \text{E.R.} \end{array}$$

$$\begin{array}{r} \text{P.O.R.} \\ 22 \end{array}$$

$$\begin{array}{r} \text{B.R.} \\ 34 \end{array}$$

+62

$$\begin{array}{r} \text{2 DUN LAP ST} \end{array}$$

$$\begin{array}{r} \text{+50 E.R.} \\ 30 \end{array}$$

$$\begin{array}{r} \text{+44 Hyd} \\ 37 \end{array}$$

+46

$$\begin{array}{r} \text{P.O.R.} \\ 14 \end{array}$$

$$\begin{array}{r} \text{+36 B.R.} \\ 9 \end{array}$$

+50

$$\begin{array}{r} \text{FE} \\ 69 \end{array}$$

14+00

$$\begin{array}{r} \text{FE Woods} \\ 92 54-95 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 9 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 9 \end{array}$$

$$\begin{array}{r} \text{+58 PP} \\ 28 \end{array}$$

+50

$$\begin{array}{r} \text{FE} \\ 96 \end{array}$$

13+00

$$\begin{array}{r} \text{FE Woods} \\ 90 54-95 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 9 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 9 \end{array}$$

12+50

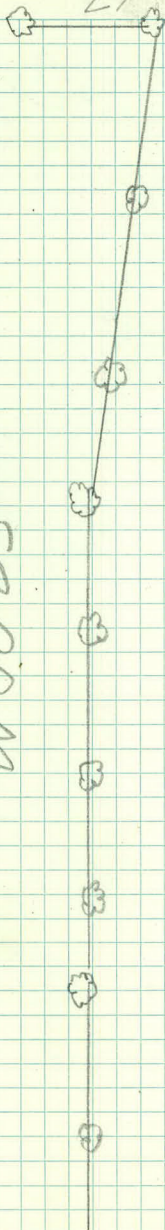
R_T

E

L_T

DUNLAP

WOODS



+50

$\frac{FE}{30}$ ✓

$\frac{RD}{13}$

$\frac{RD}{21}$ ✓

R_T

17+00

$\frac{FE}{29}$ ✓

$\frac{Pond}{110-28}$ ✓

$\frac{Rd}{13}$ ✓

$\frac{Rd}{22}$ ✓

+89 $\frac{FE COR}{29}$

+77 $\frac{P.P.}{28}$

+50

$\frac{FE COR}{34}$ ✓

+47 $\frac{Cor Pond}{28}$

+26 $\frac{Cor Pond}{100}$

16+00

$\frac{FE}{39}$ ✓

$\frac{Rd}{15}$ ✓

$\frac{Rd}{20}$ ✓

+78 $\frac{FE}{64}$ ✓

+78 $\frac{Endwoods}{36-74}$ ✓

+50

$\frac{FE}{62}$ ✓

+77 $\frac{P.P.}{29}$ ✓

15+00

$\frac{FE}{67}$ ✓

$\frac{WOODS}{39-66}$

$\frac{Rd}{15}$ ✓

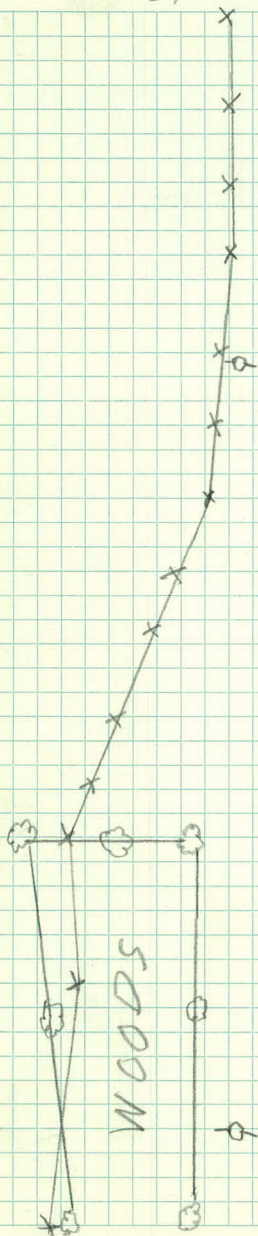
$\frac{Rd}{20}$ ✓

LT

#

R_T

23



20+00

LT

$$\begin{array}{r} \cancel{Rd} \quad \cancel{Rd} \\ 12 \quad 19 \end{array}$$

RT

$$\begin{array}{r} +72 \text{ END FENCE} \\ 31 \end{array}$$

+50

$$\begin{array}{r} FE \\ 30 \end{array}$$

$$\begin{array}{r} +08 \text{ End Low land Pond} \\ LT \quad 85 \end{array}$$

19+00

$$\begin{array}{r} FE \\ 30 \end{array}$$

$$\begin{array}{r} Rd \\ 13 \end{array}$$

$$\begin{array}{r} Rd \\ 19 \end{array}$$

$$\begin{array}{r} +69 \text{ Begin Lowland Pond} \\ LT \quad 85 \end{array}$$

+50

$$\begin{array}{r} FE \\ 30 \end{array}$$

$$\begin{array}{r} +39 \text{ P.P} \\ 29 \end{array}$$

18+00

$$\begin{array}{r} FE \\ 30 \end{array}$$

$$\begin{array}{r} Rd \\ 13 \end{array}$$

$$\begin{array}{r} Rd \\ 20 \end{array}$$

$$\begin{array}{r} +52 \text{ End Pond} \\ 85 - 29 \end{array}$$

17+50

$$\begin{array}{r} FE \\ 30 \end{array}$$

$$\begin{array}{r} Hyd \\ 24 \end{array}$$

L_T

~~E~~

R_T

24

x

x

x

x

x

σ

x

x

x

x T

+50

LT

RD
10

~~E~~

RD
22

RT

22+00

✓
Rd
10

✓
Rd
23

✓
+58 P.P
29

+50

21+00

Rd
10

Rd
20

+62 Hyd
25

+50

20+00

✓
+03 P.P
29

✓
Rd
12

✓
Rd
19

L7

£

R7

25

0

+

0



Drains

25+00 LT £ RT

+50

MONT
£

✓
+38 ER
37
✓
+22 ROR.
13

✓
+38 ER
40
✓
+25 ROR.
21

24+00

28
+03 BR ✓
118 Rd ✓
12 Rd
19

✓
+03 BR
16

✓
+90 WENDGM 48" ✓
55
+90 WENDGM 48" ✓
55

+50

✓
+13 PR
28

23+00

✓
Rd ✓
10 Rd
21

+59 PR
27

22+50

Rd ✓
10 Rd
22

LT

£

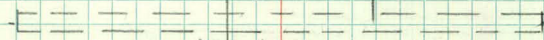
RT

26

LEXINGTON



AVE



110

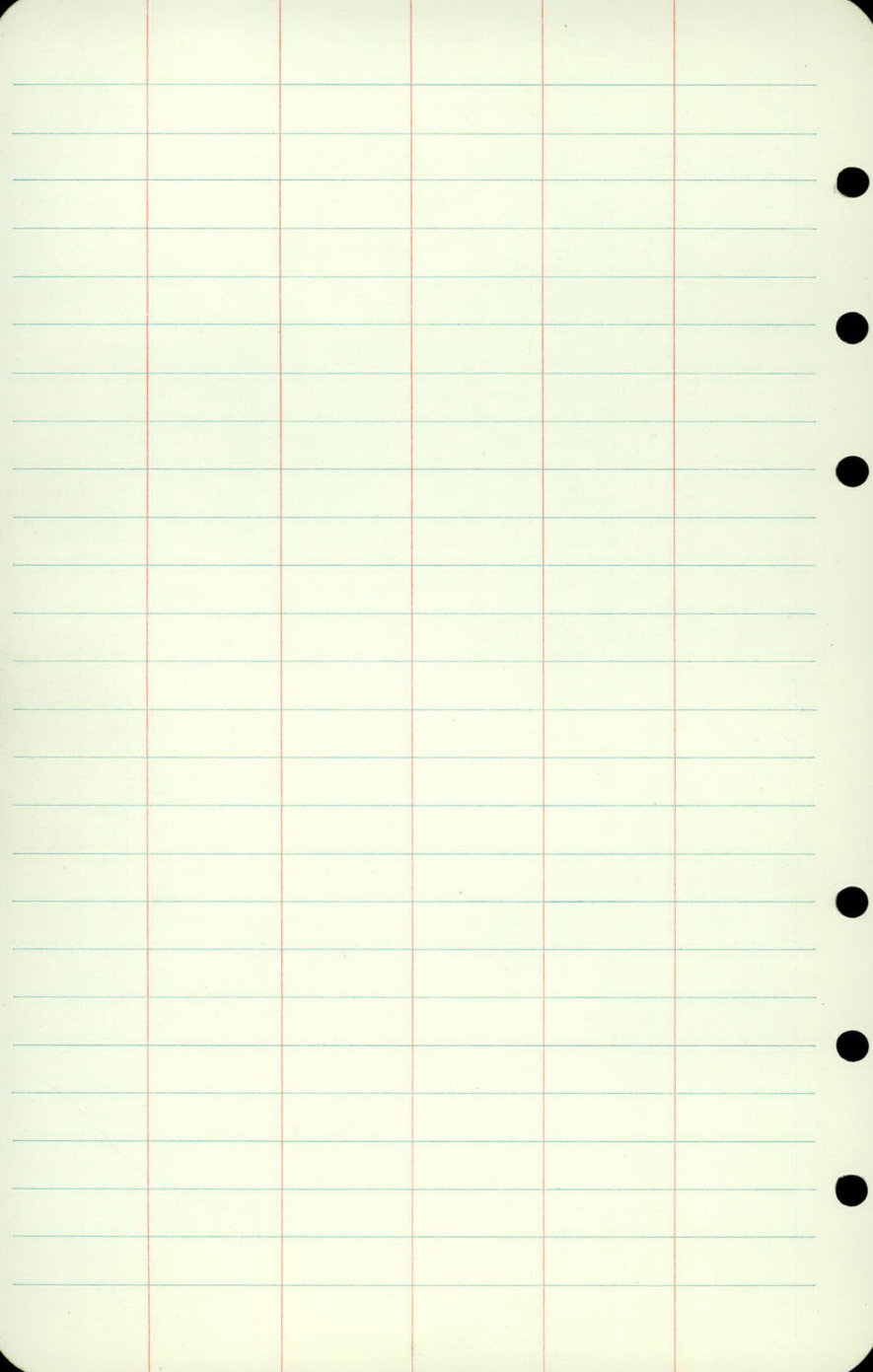
X

~~18~~

CMP

60"





BENCH LEVELS

STA	+	π	-	ELEV.
BM				936.96

BM				929.12
----	--	--	--	--------

BM				934.73
----	--	--	--	--------

BM				939.73
----	--	--	--	--------

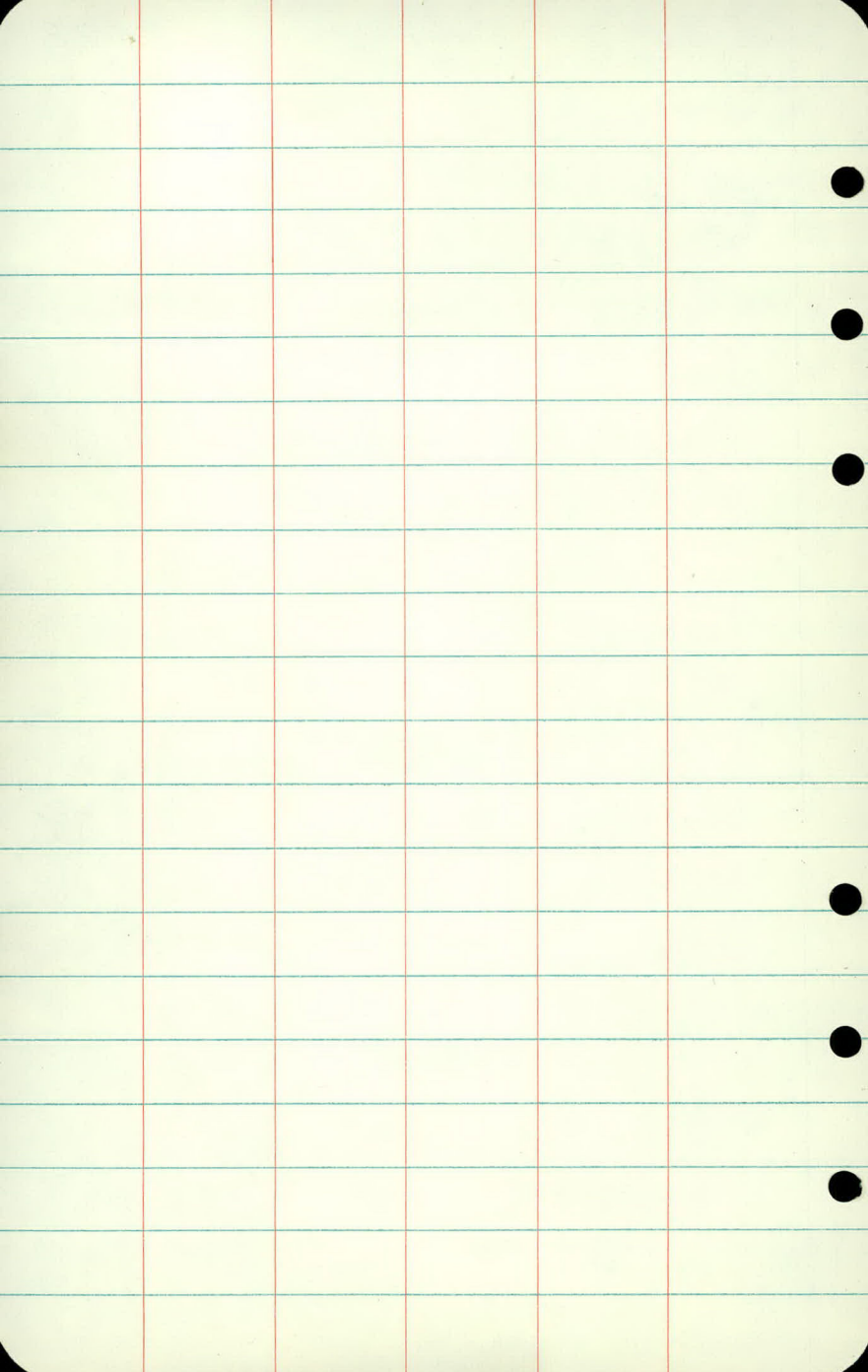
DESCRIPTION

TOP HYD LT STA 0+15

TOP HYD LT STA 2+20

TOP HYD LT STA 5+75

TOP HYD LT STA 9+00



STA	+	Σ	-	ELEV	
B.M.	5.06	944.79			939.73
B.M.	2.44	941.32	5.91	938.88	
B.M.	3.60	941.26	3.66	937.66	
T.P.	12.77	946.91	7.12	934.14	
			2.47	944.44	944.46

D.S.
G.A.
J.A.
C.M.

30

Top Hyd LT STA 9

Top Hyd COR Red Fox Rd $\frac{1}{2}$ DUNLAP

Top Hyd LT STA 16+50

T.P. & OF STA 22+00

Spike with Red in P.P. N.E. COR LEX. $\frac{1}{2}$ Red Fox Rd

STA	+	II	—	ELEV	
BM	2.52	941.40			938.88
B.M.	3.43	941.11	3.72	937.68	
B.M	5.99	945.37	1.73	939.38	
B.m	2.27	946.73	1.00	944.37	944.46
B.m.	1.98	941.61	7.10	939.63	939.63
T.P.	6.21	942.75	5.07	936.54	
B.M.			3.85	938.90	938.88
B.m.					

L

E

RT

31

TOP HYD AT DUNLAP

Top Hyd STA 16+50

SPIKE IN P.P. N.W. COR. LEX & Red Fox Rd

SPIKE WITH RED IN P.P. N.E. COR. LEX. & Red Fox Rd

SPIKE IN P.P. N.W. COR. LEX & Red Fox Rd.

TOP BELL TELEPHONE PIPE

B.M. ^{TOP} Hyd AT DUNLAP

Sp

STA

+

万

[illegible]

ELEV

B m

7.07

946.70

939.63

 $23 + 90$

24+00

 $24 + 38$ $24 + 50$

of LEX.

2.24

944,46

944.46

67

LT

E

RT

32
68

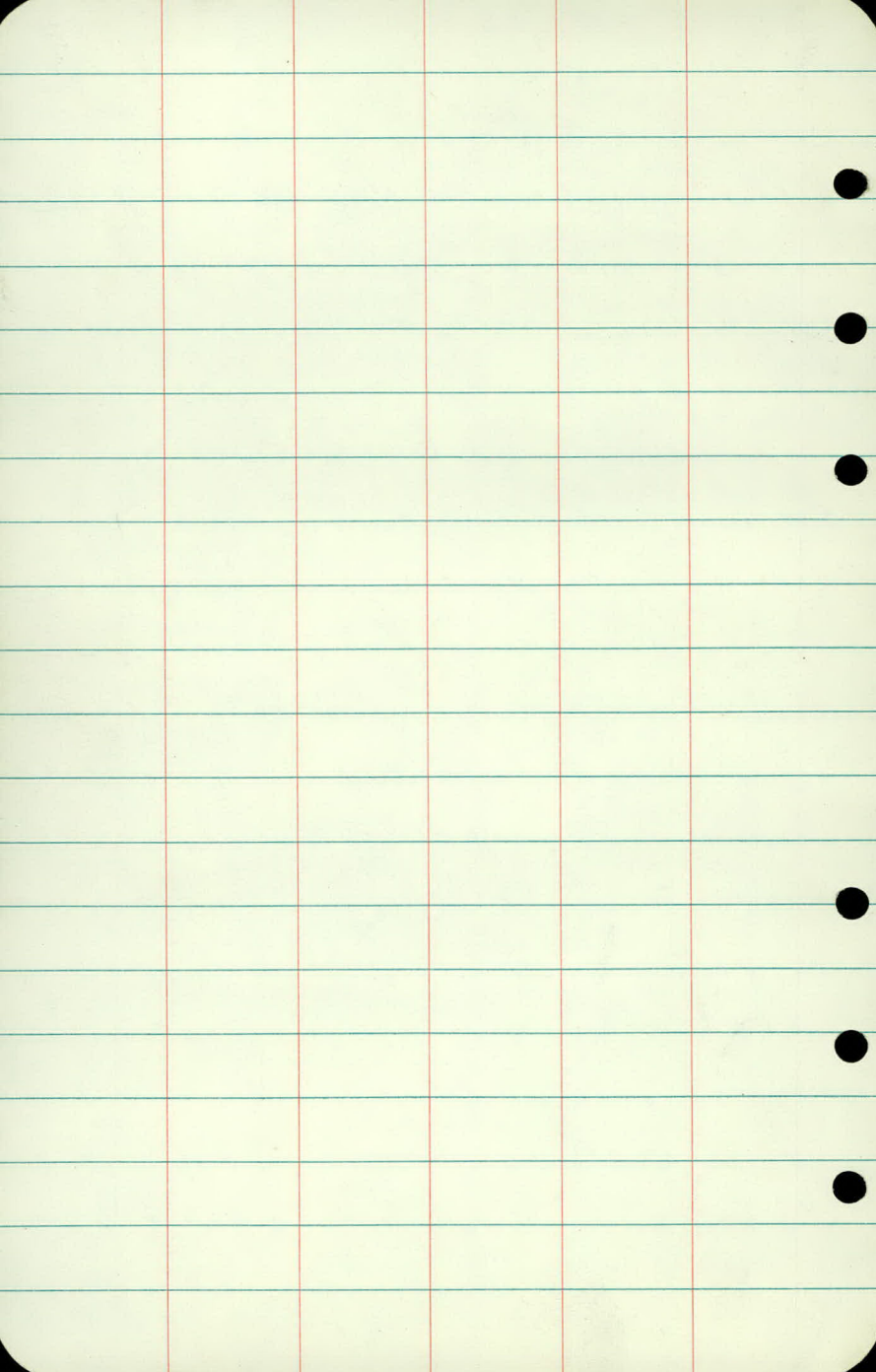
^{29.3} <u>17.4</u> 75	^{21.4⁵} <u>19.25 (CMP)</u> 54 (FL)	^{38.1} <u>120.9</u> 42	^{37.4} <u>9.3</u> 31	^{39.1} <u>7.0</u> 16	^{40.2} <u>6.5</u> E	^{39.5} <u>7.2</u> 18	^{36.3} <u>10.4</u> 33	^{34.0} <u>12.7</u> 43	^{27.2⁵} <u>19.75 (MA)</u> 51 (FL)	^{28.2} <u>8.5</u> 75
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^{32.4} <u>14.3</u> 75	^{33.4} <u>13.3</u> 53	^{39.9} <u>6.8</u> 25	^{40.9} <u>5.8</u> 15	^{40.9} <u>5.8</u> E	^{40.4} <u>6.3</u> 15	^{40.0} <u>6.7</u> 20	^{33.2} <u>12.9</u> 35	^{29.1} <u>17.6</u> 59	^{28.8} <u>17.9</u> 75
--------------------------------------	--------------------------------------	-------------------------------------	-------------------------------------	------------------------------------	-------------------------------------	-------------------------------------	--------------------------------------	--------------------------------------	--------------------------------------

^{44.1} <u>2.0</u> 100	^{43.1} <u>3.3</u> 50	^{42.1} <u>4.0</u> 16 Bit	^{42.4} <u>4.3</u> E	^{42.1} <u>4.6</u> 17	^{41.3} <u>5.4</u> 47	^{40.2} <u>6.5</u> 100
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^{44.8} <u>1.9</u> 100	^{44.3} <u>2.4</u> 75	^{43.8} <u>2.9</u> 50	^{43.1} <u>3.6</u> 25	^{42.4³} <u>4.27</u> E MONT	^{42.1} <u>4.6</u> 25	^{41.5} <u>5.2</u> 50	^{40.9} <u>5.8</u> 75	^{40.4} <u>6.3</u> 100
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Spike with Red in P.P. N.E. of Lex & Red Fox Rd.

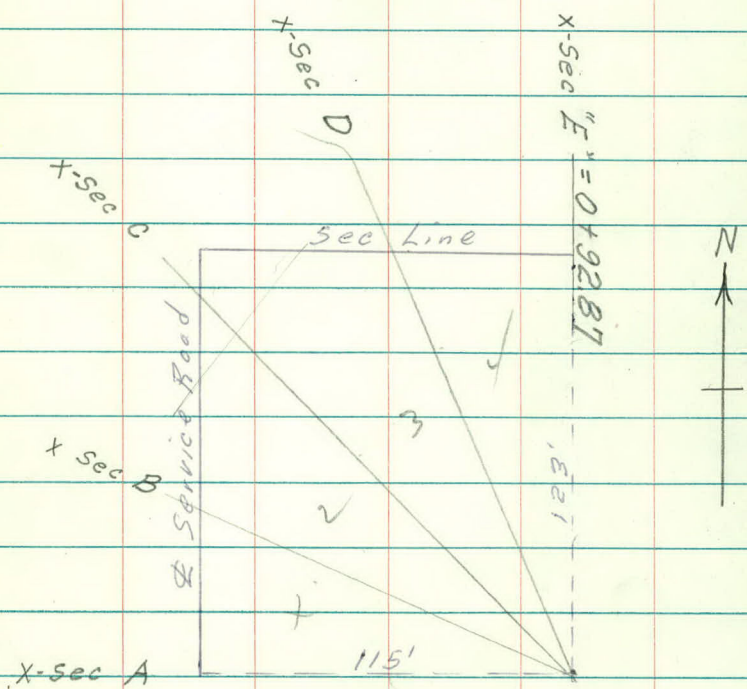


FK
PK
CM
AS

June 27, 1969

33

X - SECTIONS



STA + π - ELEV.

BM 0.04 937.00

936.96

X-Sec. "A"

✓

✓
119
2212
9259

✓

X-Sec "B"

✓

June 27, 1969

Lt. from Center

Ctr. 34

Left Sta 0-12
TOP HYD NW COR SERVICE DRIVE

23.4	24.0	24.7	26.3	27.8	29.1	30.9
13.6	13.0	12.3	10.7	9.2	7.9	6.1
53	49	47	38	27	14	

23.3	23.2	21.5	23.1	22.1	22.3
13.7	13.8	15.5	13.9	14.9	14.7
56	58	59	63	66	74

26.6	28.7	28.5	28.3	27.2	24.0	22.9
8.4	8.3	8.5	8.7	9.8	13.0	14.1
125	113	101	100	95	86	82
	£	Bit				

28.3	24.2	27.7	32.1	32.5	32.7
8.7	12.8	9.3	4.9	4.5	4.30
130	141	150	164	166	167
					Bit

22.9	24.0	25.4	26.4	27.8	29.4	30.9
14.1	13.0	11.6	10.6	9.2	7.6	6.1
58	50	45	41	28	14	

22.5	22.6	23.4	27.9
14.5	14.4	13.6	9.1
68	80	84	100

STA	+	π	-	ELEV.
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		937.00		
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X-Sec "B"				
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✓				
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X-Sec "C"				
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✓				
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✓				
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X-Sec "D"				
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June 27, 1969

Lt. from center

ctr

35

28.0	30.2	30.3	30.2	29.8	29.4
9.0	6.8	6.7	6.8	7.2	7.6
151	142	136	123	110	105
Bit					

32.8	33.0
4.2	4.0
173	175
Bit	

23.1	23.5	24.4	26.1	27.3	28.4	29.6	30.9
13.9	13.5	12.6	10.9	9.7	8.6	7.4	6.1
87	78	62	50	40	28	14	

23.7	25.2	30.4	30.8	31.3	31.6	31.9	32.0
13.3	11.8	6.6	6.2	5.7	5.4	5.1	5.0
100	108	127	134	141	143	153	162
Bit							

33.2	33.0	32.4	30.7	30.2	30.9	31.8
3.8	4.0	4.6	6.3	6.8	6.1	5.2
223	221	217	210	202	183	170

24.5	24.8	26.3	27.4	28.0	28.7	29.8	30.9
12.5	12.2	10.7	9.6	9.0	8.3	7.2	6.1
80	70	59	52	40	28	14	

Sta + π - Elev

937.00

X-Sec. "D"

✓

X-Sec E

T.P. 0.34 932.60 4.74 932.26 0+00 $\pm$
32.3

Lt. from Center

June 27, 1969

Cfr.

36

31.0	31.0	30.5	27.6	25.3	24.5	23.8
6.0	6.0	6.5	9.4	11.7	12.5	13.2
125	123	119	113	106	100	92
Bit						

31.2	31.5	31.7	32.5	33.5	33.9	35.3	36.6
5.8	5.5	5.3	4.5	3.5	3.10	1.66	0.35
133	142	145	153	160	164	175	187
Bit		Ent			Conc.		

24.4	26.7	27.9	28.2	28.7	29.6	30.1	30.90
12.6	10.3	9.1	8.8	8.3	7.4	6.9	6.1
79	69	62	54	42	28	14	

24.7	25.2	26.9	29.6	29.7	29.7
12.3	11.8	10.1	7.4	7.3	7.3
87	100	105	111	114	122

36.2	34.4	31.8	30.0	29.5	29.6
0.8	2.6	5.2	2.0	2.5	7.4
174	162	150	138	134	131

36.7
0.3
180

Ditch Profile Rt
along East Side Service Rd

932.60

5 0+10± Rt

✓

0 - 22.13 ± Service Road (Profile)

✓

✓

Ctr. of Radius

1.73 930.87 (930.9)

1.73

June 27, 1969

37

L

RT

21.6	21.6	21.3	21.0	20.7
11.0	11.0	11.3	11.6	11.9
162	212	236	253	270

18.8	19.1	19.4	19.8	20.4
13.8	13.5	13.2	12.8	12.2
362	340	332	319	292

31.8	31.8	31.3	30.4	29.7	28.7	27.8
0.8	0.8	1.3	2.0	2.9	3.9	4.8
25	47	70	96	123	149	

22.3	23.3	24.1	25.0	26.0	27.0
10.3	9.3	8.5	7.6	6.6	5.6
311	278	254	229	200	173

21.5	20.9	20.4
11.1	11.7	12.0
341	370	400

Sta	+	π	-	Elev.
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BM	0.99	943.42		
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942.43

BM			3.26	940.16
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22+00

✓

+50

✓

✓

Lt.

June 27, 1969
£

Rt.

38

Top Monument & Lexington

Top Hyd S.W. Corner Lexington

39.7	36.1	35.1	34.2	33.8	33.6	33.5	33.6	34.0
3.7	7.3	8.3	9.2	9.6	9.8	9.9	9.8	9.4
28	20	14	12		11	28	42	51

40.0	39.2	39.1		37.4	37.5
3.4	4.2	4.3		11.0	9.9
32	53	75		75	58

36.6	35.6	35.3	34.6	34.6	34.2	34.6	34.8	35.4
6.8	7.5	8.1	8.8	8.8	9.2	8.8	8.6	8.0
25	19	13	11		16	18	22	30

37.0	37.1	36.6	37.2	36.8	36.2	36.5	35.8
6.4	6.3	6.8	6.2	6.6	7.2	6.9	7.6
31	38	42	45	45	42	38	32

38.6	38.8	38.7	38.1	37.6
4.8	4.6	4.7	5.3	5.8
75	62	57	52	49

36.1	36.1
6.7	5.3
51	100

Hole
under construction

Sta + π - Elev.

943.42

23

✓

+50

✓

24

for check

2.53 940.89 (40.9)

Lt.

June 27, 1969

39

Rt.

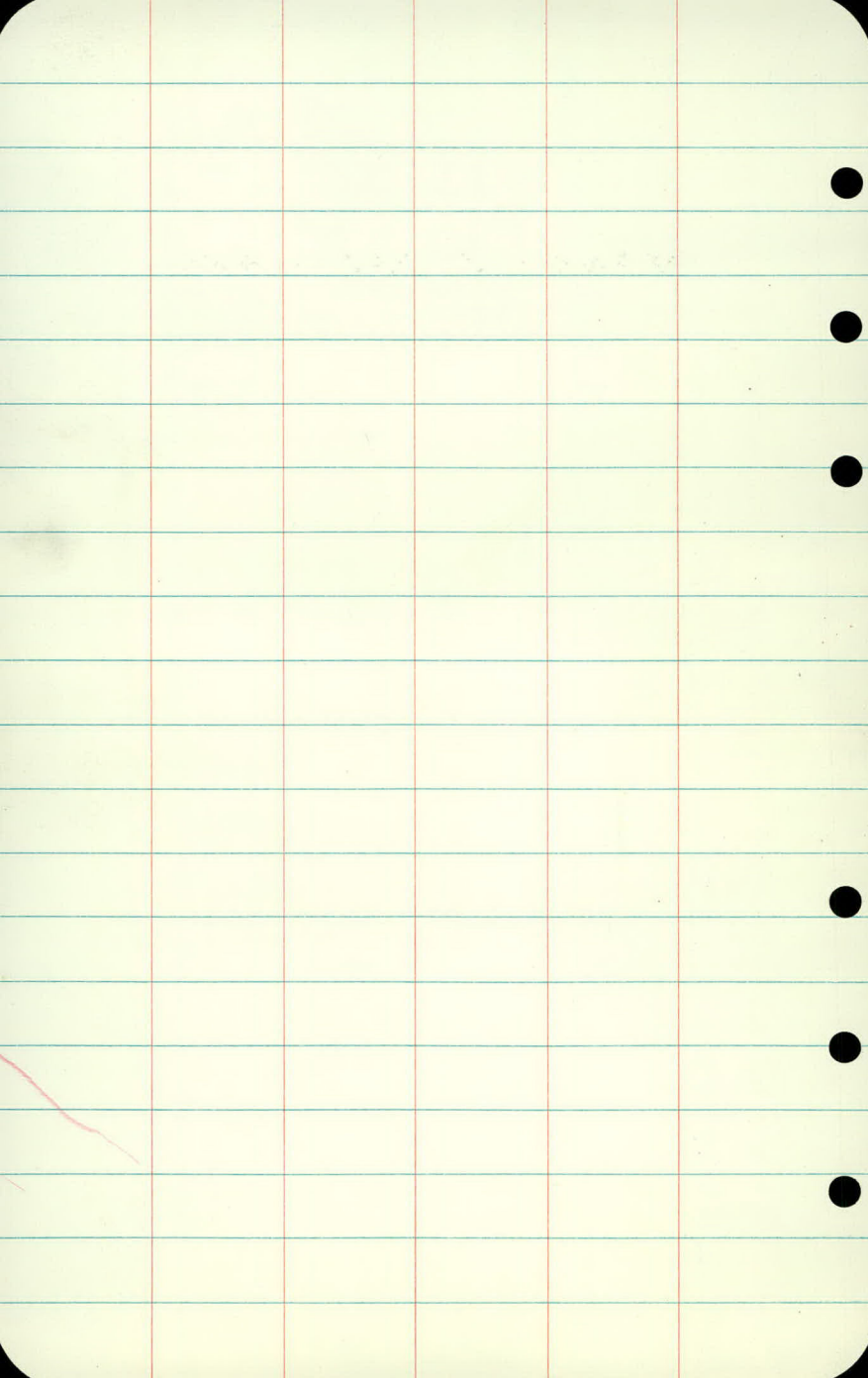
38.1	36.9	36.6	36.1	36.1	35.4	36.8	37.7	38.4
5.3	6.5	6.8	7.3	7.3	8.0	6.6	5.7	5.0
25	20	15	11		16	26	39	54

38.8	38.3	38.3	38.0		39.1	38.8
4.6	5.1	5.1	5.4		4.3	4.6
30	50	68	75		85	71

38.2	38.2	38.1	38.0	38.3	38.1	37.6	38.3	39.3	40.0
5.2	5.2	5.3	5.4	5.1	5.3	5.8	5.1	4.1	3.4
69	52	36	22	11		17	26	48	63

38.1
5.3
85

39.9
3.5
75



FK
PK
CM
AS

June 30, 1969

40

BENCH LEVEL CHECK

Sta	+	π	-	Elev.
BM	3.37	940.33		936.96
BM	8.10	937.22	11.21	929.12
BM	9.66	944.37	2.51	934.71
BM	4.36	944.09	4.64	939.73 939.73
BM	2.85	942.78	4.16	939.93
BM	2.62	941.49	3.91	938.87 938.88
BM	1.74	939.40	3.83	937.66
BM	7.58	944.82	2.16	937.24
BM			4.73	940.09 944.65
BM			0.16	944.66 944.46
BM			8.79	936.03
BM	2.14	941.01		938.87
BM	1.87	939.51	3.37	937.64 937.65
BM	7.73	944.94	2.30	937.21 937.23
BM			4.87	940.07 940.08
BM			0.31	944.63 944.65

June 30, 1969

41

Top Hyd Lt Sta 0-12

Top Hyd Lt Sta 2+23

Top Hyd Lt Sta 5+85

Top Hyd Lt Sta 9+03

Top Hyd Lt Sta 11+66

Top Hyd S.W. Corner Dunlap & Red Fox Rd

Top Hyd Lt Sta 17+50

Top Hyd Lt Sta 20+62

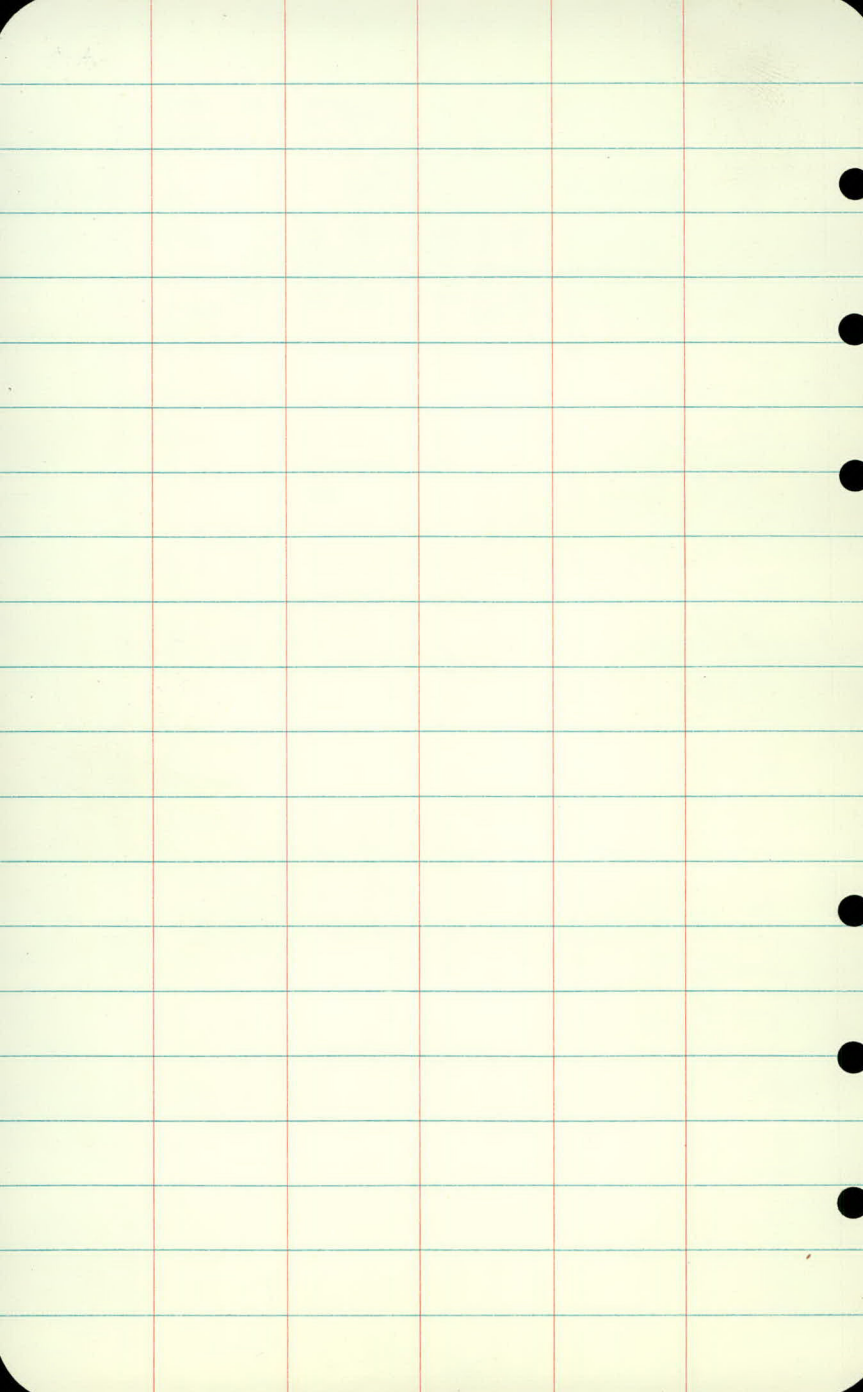
Top Hyd S.W. Corner Lexington & Red Fox
Spike in Arc Light NE Corner Lexington
Sta 23 E

Top Hyd S.W. Corner Dunlap & Red Fox Rd.

Top Hyd Lt Sta 17+50

Top Hyd Lt Sta 20+62

Top Hyd S.W. Corner Lexington & Red Fox
Spike in Arc Light NE Corner Lexington



July 7, 1969

42

Lexington Ave x-sections

Sta	+	π	-	Elev
BM	5.25	945.33		940.08

52.5' North of Red Fox Rd

✓

✓

51' South of Red Fox Rd

0.68

BM

0.68 944.65 944.65

FA
CM
AC

July 1, 1969

Left

43

Top Hyd S.W. Corner Lexington & Red Fox

35.33	37.03	38.73	40.73	42.33	42.83	43.53	43.73
10.0	8.3	6.6	4.6	3.0	2.5	1.8	1.6
46	42	35	29	25	23	12	

32.53	24.93	30.73	31.44	30.53	32.03
12.5	15.4	14.6	13.89	14.8	13.3
51	55	58	62	67	72

Top 60" Culvert

33.13	38.13	37.83	36.93	34.73	33.53
7.2	7.2	7.5	8.4	10.6	11.5
100	94	89	84	79	75

32.83	32.83	35.83	37.63	39.13	40.83	41.13	41.33
12.5	11.5	9.5	7.7	6.2	4.5	4.2	4.0
46	42	38	34	29	23	13	

33.13	30.53	29.53	31.23	30.93	34.53
13.6	14.8	15.5	14.5	14.4	10.8
49	51	55	60	67	71

Top 60" Culv

39.43	39.13	37.53	37.03	35.63
5.9	6.2	6.8	8.3	9.7
100	96	89	82	75

Spike in PP NE Corner Lexington & Red Fox Road

Sta + π - E/ev

BM 0.52 940.60 940.08

N. End inv. 9.22
4.90
14.12 926.48

South End inv. 9.47
4.93
14.40 926.20

FH
PK
CM
AC

July 8, 1969

44

