

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

WHITE BEAR AVE.

From Co. Rd. "C" To Co. Rd. "D"

Road Acc't. No. 65

Date Filed _____ File _____

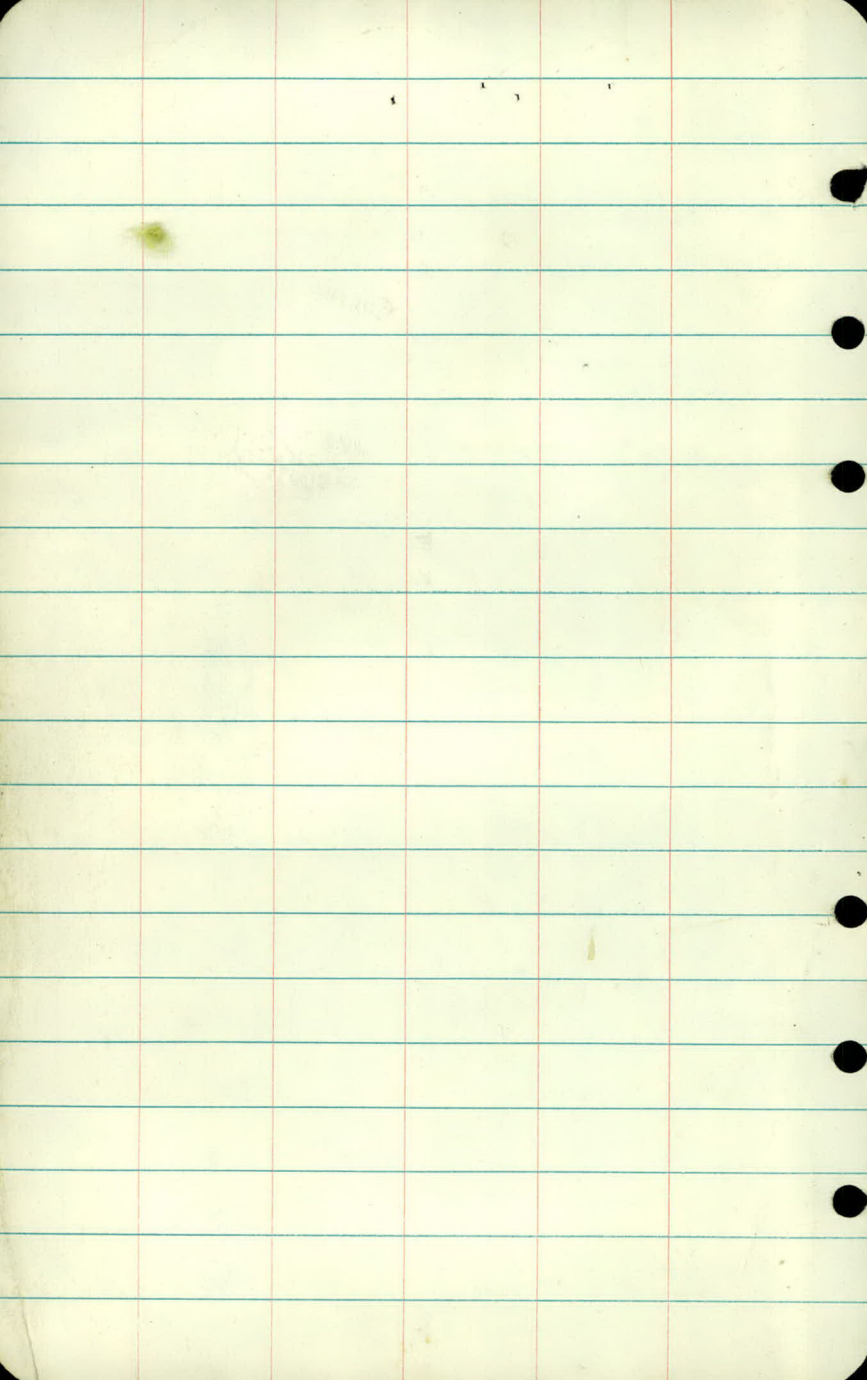
37.82

49.83

1
WHITE BEAR AVE.

Co Rd "C" to Co Rd "D"

PLAN SURVEY



FK
WM
DM
WF

June 10, 1968

A-2

Alinement

Hyd.

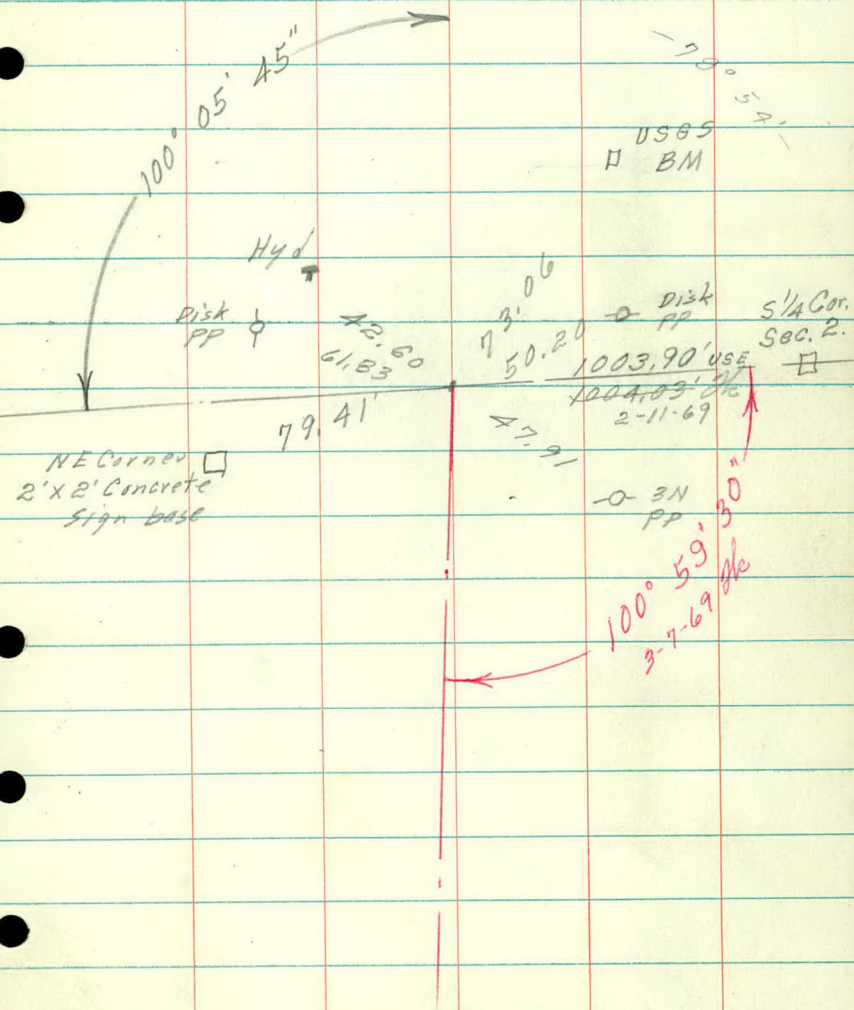
42.60

Sta Point Δ Lt Δ Rt

700 d

0+00.00 $\pm$ C_o Rd C

June 10, 1968 A-3



Sta Point ΔL ΔR

14+53.71 P.T.

+50

40.21

~~134.44 P.T.~~

+25

14

+75

13 7310 P.I.

+50

+25

13105.74 ~~PC~~

13

12+92.18 P.C.

119° 24'
239° 40'
79 54 30

1204.33

100 05 45
79 54
42 24
59 324
36 324
199
199

6 14
50
0.33

3-7-69

8° 04' 35" $\frac{1}{2}$

~~$\Delta = 8^{\circ} 04' 35''$ $\Delta = 8^{\circ} 04'$~~

~~$D = 5^{\circ}$ $D = 6^{\circ}$~~

~~$T = 80.92'$ $T = 67.36'$~~

$B^{\circ} 04' L = 161.53 L = 134.44'$

~~$R = 1146.28$ $R = 955.366'$~~

954.93

June 10, 1968

A-4

3N
PP -

38.95

Drill Hole

54.68

43.17

3N
12" Catalpa

3N
TP

26 + 50.97 P.O.T.

1012

June 10, 1968

A-5

VOID
0.19 N. of P.1. Page A-13

3N
TP

113.52

3N
PP-O 27.12

112.85

3N
TP

Sta Point Δ Lt. Δ Rt.

+61.48	P.T.	$0^{\circ}33'$	$\Delta = 1^{\circ}06'$
+50		$0^{\circ}31.3'$	$D = 0^{\circ}30' \text{ Arc.}$
34		$0^{\circ}23.8'$	$T = 110.00'$
33+51.48	P.I.	$1^{\circ}06'$	$L = 220'$
+50		$0^{\circ}16.3'$	$R = 11,459.16'$
33		$0^{\circ}8.8'$	
+50		$0^{\circ}1.3'$	
32+41.48	P.C.	$0^{\circ}00'$	

FK
DM
WF

July 30, 1968

A-6

VOID

3N
PP - 48.04

Spike

17.20

3N
TP

Sta Point Δ Lt. Δ Rt.

54+74.03 Sec. Line

41.18

54+32.85

52+32.85

+65.62 P. T. $2^{\circ}15'$

+50

$2^{\circ}05.6'$

$\Delta = 4^{\circ}30'$

49

$1^{\circ}35.6'$

$D = 2^{\circ}$ Arc

48+53.18 P. I.

$4^{\circ}30'$

$T = 112.56'$

+50

$1^{\circ}05.6'$

$L = 225.00$

48

$0^{\circ}35.6'$

$R = 2864.79'$

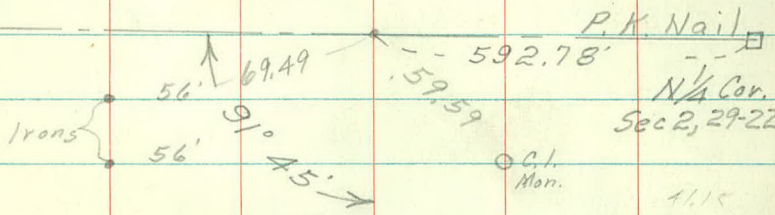
+50

$0^{\circ}5.6'$

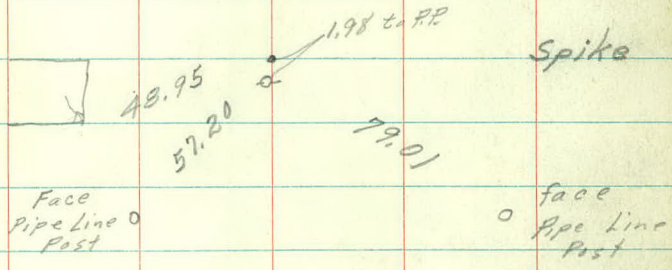
47+40.62 P. C. $0^{\circ}00'$

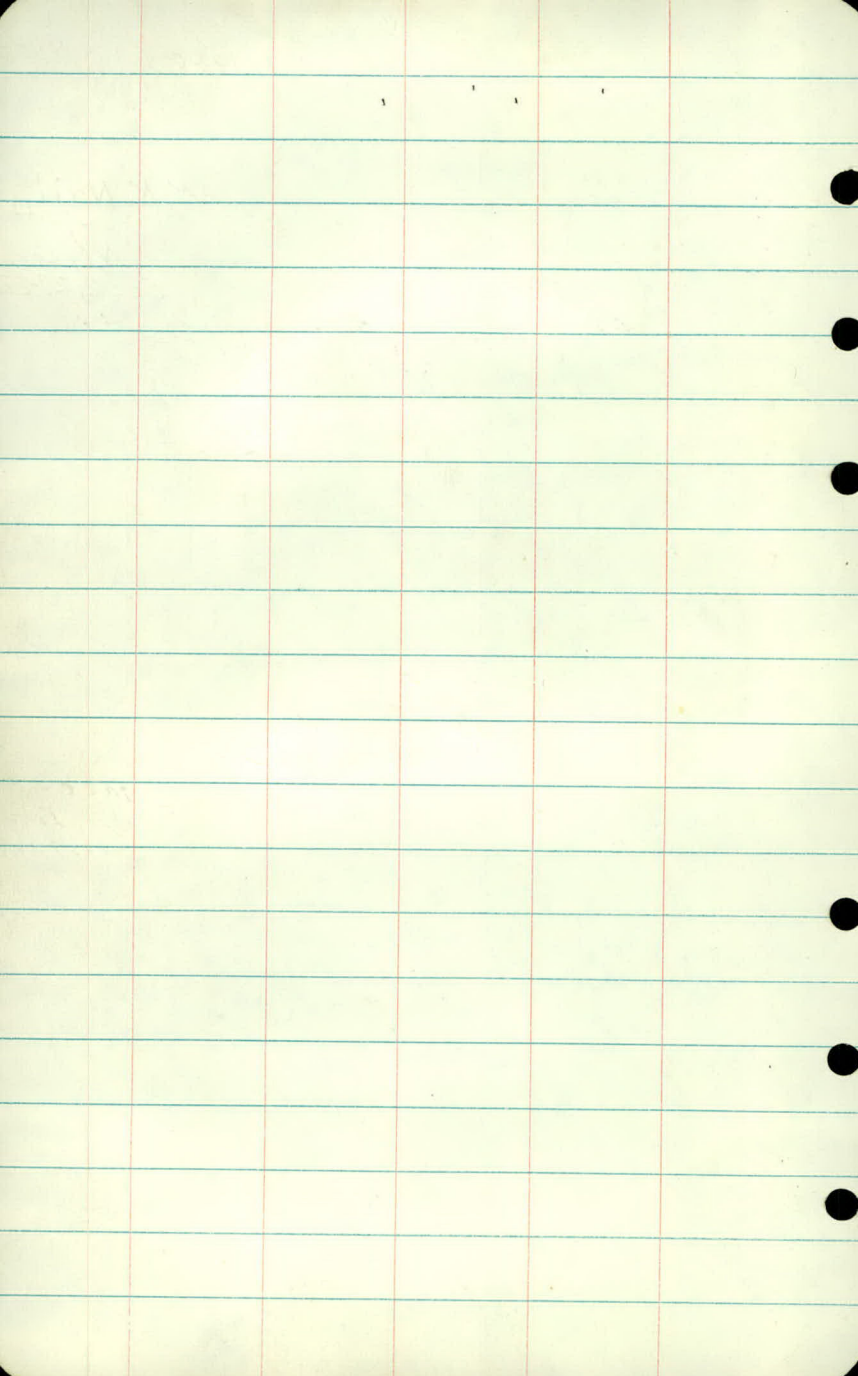
July 30, 1968
August 1, 1968

A-7



VOID





FK
GA
PF

Sept. 4, 1968

A-B

NEW ALIGNMENT

Sta 29+02.22 to "D"

Sta Point ΔL ΔR

+27.22 P.T. 33.75'

+25 33.4'

31 29.65'

+75 25.9'

+50 22.15'

$\Delta = 1^{\circ} 07' 30''$

+25 18.4'

$\frac{1}{2}\Delta = 33' 45''$

30+14.71 P.I.

$D = 0^{\circ} 30' \text{ Arc}$

30 14.65'

$T = 112.49'$

+75 10.9'

$L = 225.00'$

+50 7.15'

$R = 11,459.16'$

+25 03.4'

29+02.22 P.C. $0^{\circ} 00'$

Sept. 4, 1968

A-9

3N
PP ○

40.22'

46.86'

TP
○

Drill hole

68.38'

3N
PP ○

Sta Point ΔL ΔR

+13.41 P.T. $2^{\circ}58'45''$

41 $2^{\circ}50.7'$

+75

+50 $2^{\circ}20.7'$

+25

40 $1^{\circ}50.7'$ $\Delta = 5^{\circ}57'30''$

+75 $\frac{1}{2}\Delta = 2^{\circ}58'45''$

39+64.59 P.I. $D = 2^{\circ} \text{ Arc}$

+50 $1^{\circ}20.7'$ $T = 149.10'$

+25 $L = 297.92'$

39 $0^{\circ}50.7'$ $R = 2,864.79'$

+75

+50 $20.7'$

+25 $05.7'$

38+15.49 P.C. $0^{\circ}00'$

Sept 4, 1968 A-10

BM. Spike in
30" C.H.

70.10'

Iron

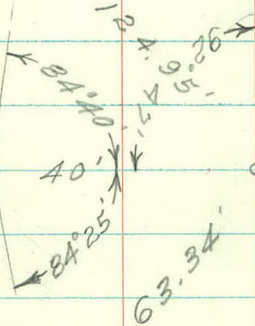
141.20'

Bent Spike
in 28" Oak

P.K. Nail
in O

Transformer P.P.

old P.I.



P.K. Nail
in P.P. O

old P.I.

Sta Point ΔL ΔR

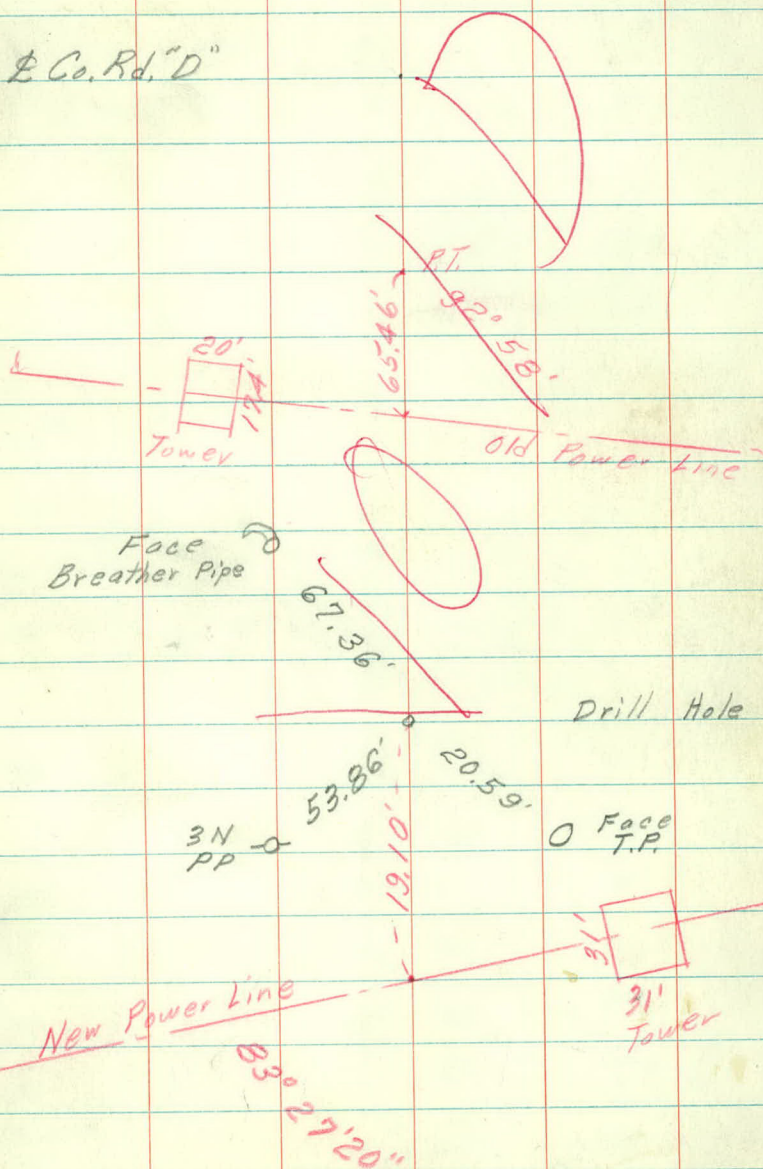
54+77.59 P.O.T. section Line

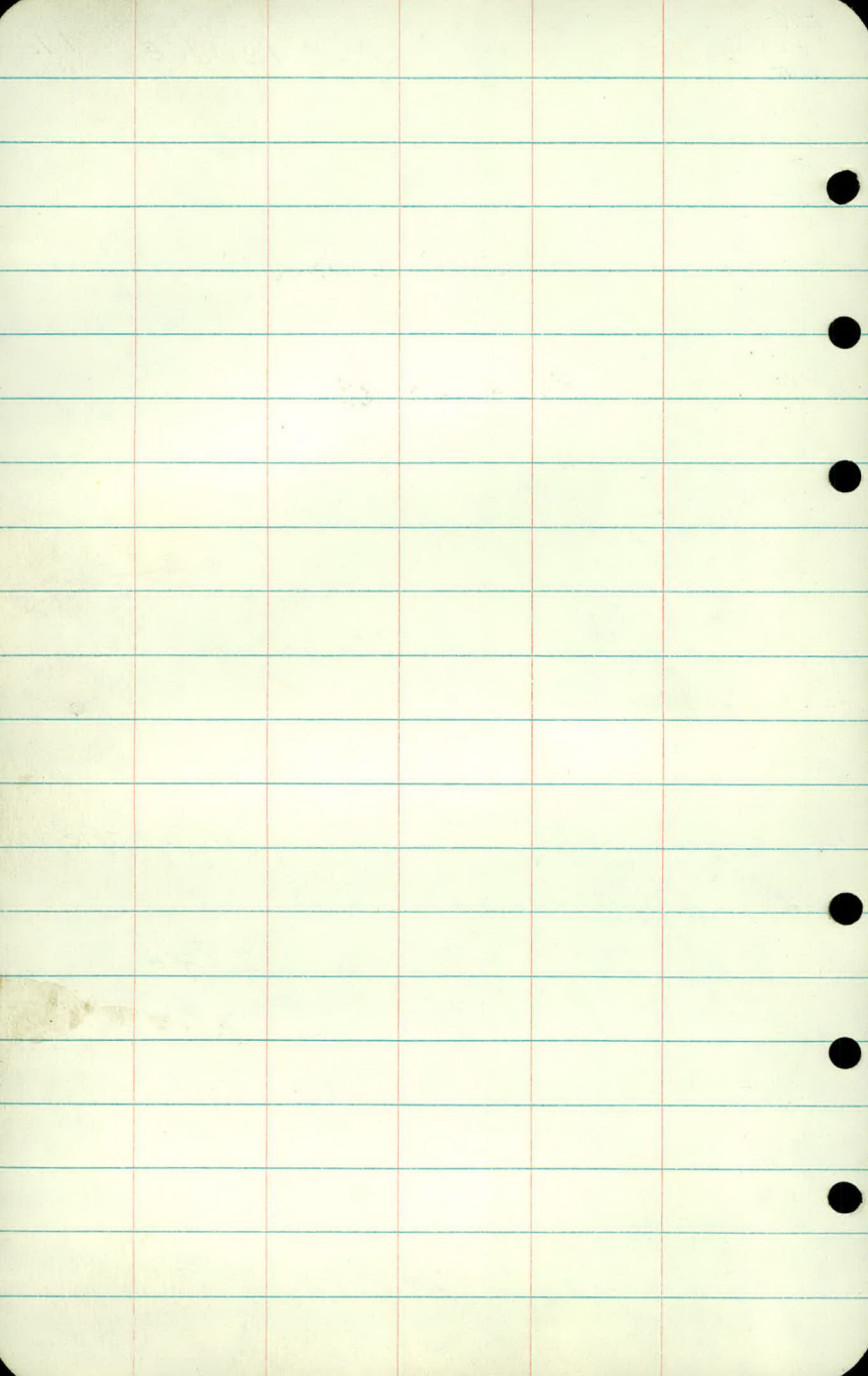
+15.92	P.T.	4° 44'	
50		4° 29.5'	
+75		4° 07'	
+50	POST	3° 44.5'	
+25		3° 22'	
49		2° 59.5'	$\Delta = 9° 28'$
+75		2° 37'	$\frac{1}{2} \Delta = 4° 44'$
48+58.73	P.I.		$D = 3° \text{ Arc}$
+50		2° 14.5'	$T = 158.14'$
+25		1° 52'	$L = 315.33'$
48		1° 29.5'	$R = 1909.86'$
+75	POST	1° 07'	
+50		0° 44.5'	
+25		0° 22'	
47+00.59	P.C	0° 00'	

FK
LPD
PF

Sept. 4, 1968
Sept. 19, 1968 A-11

E Co. Rd. "D"





FK
KG
GA

Dec. 11, 1968

A-12

Revised Alinement

Beam to "D"

33
Sta Point Δ Lt. Δ Rt.

32³⁰ 95.21

+04.79 P.T. $1^{\circ}48'22\frac{1}{2}''$

good

31 $1^{\circ}45.5'$

+75 $1^{\circ}30.5'$

$\Delta = 3^{\circ}36'45''$

+50 $1^{\circ}15.5'$

$\frac{1}{2}\Delta = 1^{\circ}48'22\frac{1}{2}''$

+25 $1^{\circ}00.5'$

$D = 2^{\circ}$ Arc

30+14.50 P.I. $3^{\circ}36'45''$

$T = 90.34'$

30 $0^{\circ}45.5'$

$L = 180.625'$

+75 $0^{\circ}30.5'$

$R = 2864.79'$

+50 $0^{\circ}15.5'$

+25 $0^{\circ}00.5'$

29+24.16 P.C. $0^{\circ}00'$

26+50.78 P.I. $0^{\circ}30'11''$

Frank K.

4/29/74

2:40

can find thing in a.m.

C. O. Surgis

483-4408

Boxwood & McKnight

New C.I. 0.8N
& 0.55 West



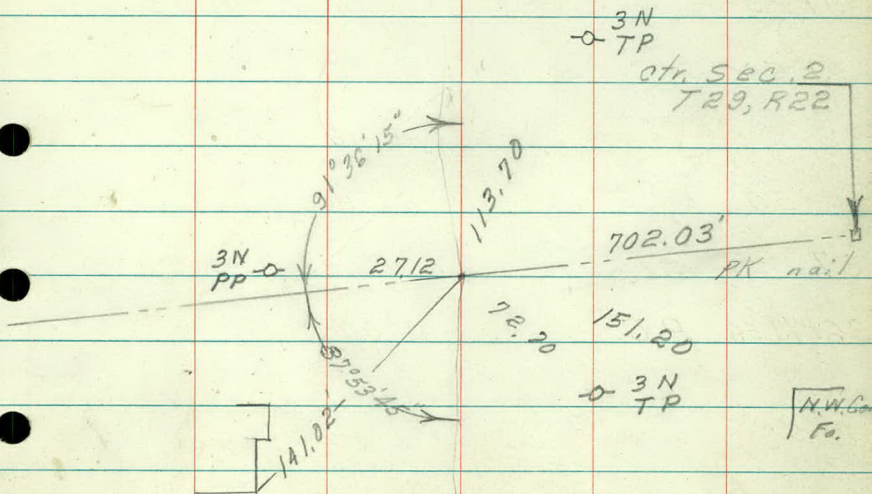
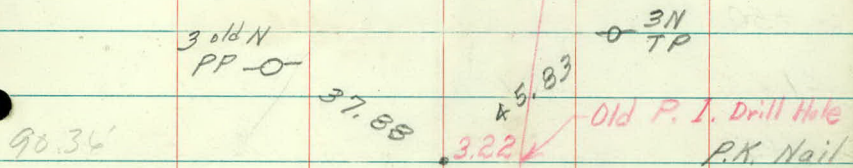
Lewiston Heights^{No. 3}

Leonard Oaks

Beam & W.B.A.

Dec. 11, 1968

A-13



Sta Point ΔL ΔR

42+54.56 P.T.

5° 45'

+50

5° 42' 16"

good

42

5° 12' 16"

+50

4° 42' 16"

41

4° 12' 16" $\Delta = 11° 30' R$

+50

3° 42' 16" $\frac{1}{2}\Delta = 5° 45'$

40

3° 12' 16" $D = 2° Arc$

7.10

39+68.03 P.I.

$T = 288.47'$

+50

2° 42' 16" $L = 575.00'$

39

2° 12' 16" $R = 2864.79'$

+50

1° 42' 16"

38

1° 12' 16"

+50

0° 42' 16"

37

0° 12' 16"

36+79.56 P.C.

0° 00'

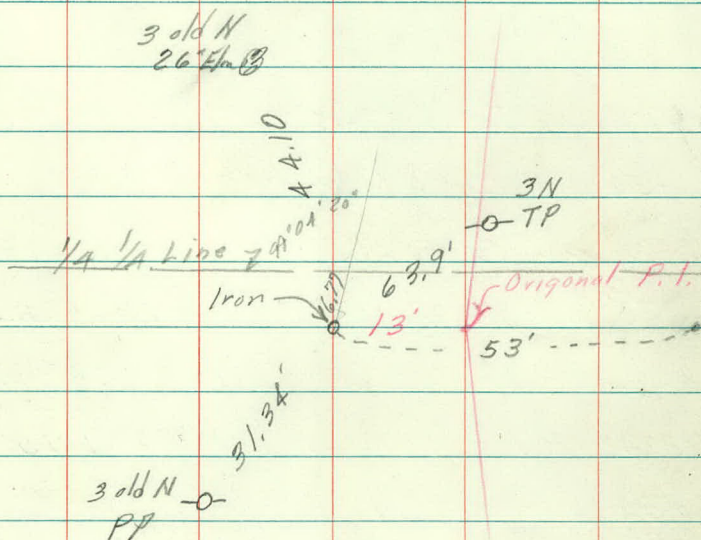
168.03
351.00

468.16
214.00

FK
WS
GA
LPD

Dec. 11, 1968
Dec. 22, 1968

A-14



Sta. Point Δ Lt. Δ Rt.

54+80.42 P.O.T.

54+39.24

52+39.24

good

+59.59 P.T. $5^{\circ}22'45''$

+50 $5^{\circ}14.1'$

49 $4^{\circ}29.1'$

$\Delta = 10^{\circ}45'30''$ H

+50 $3^{\circ}44.1'$

$\frac{1}{2}\Delta = 5^{\circ}22'45''$

48 $2^{\circ}59.1'$

D = 3° Arc

47+80.48 P.I.

180.40

T = 179.50'

+50 $2^{\circ}14.1'$

L = 358.61'

47 $1^{\circ}29.1'$

R = 1,909.86'

+50 $0^{\circ}44.1'$

46+00.98 P.C. $0^{\circ}00'$

PK
KP
KG

12-26-68

A-15

PK Nail
TP

PK Nail
PP

Section Line
E Coi Rd. "D"

Irons {

56'

56'

98.89'
91° 45'
63.69'

96.77'

592.78'

PK nail
Arc Lt.

S.P.P.
PP

42.25

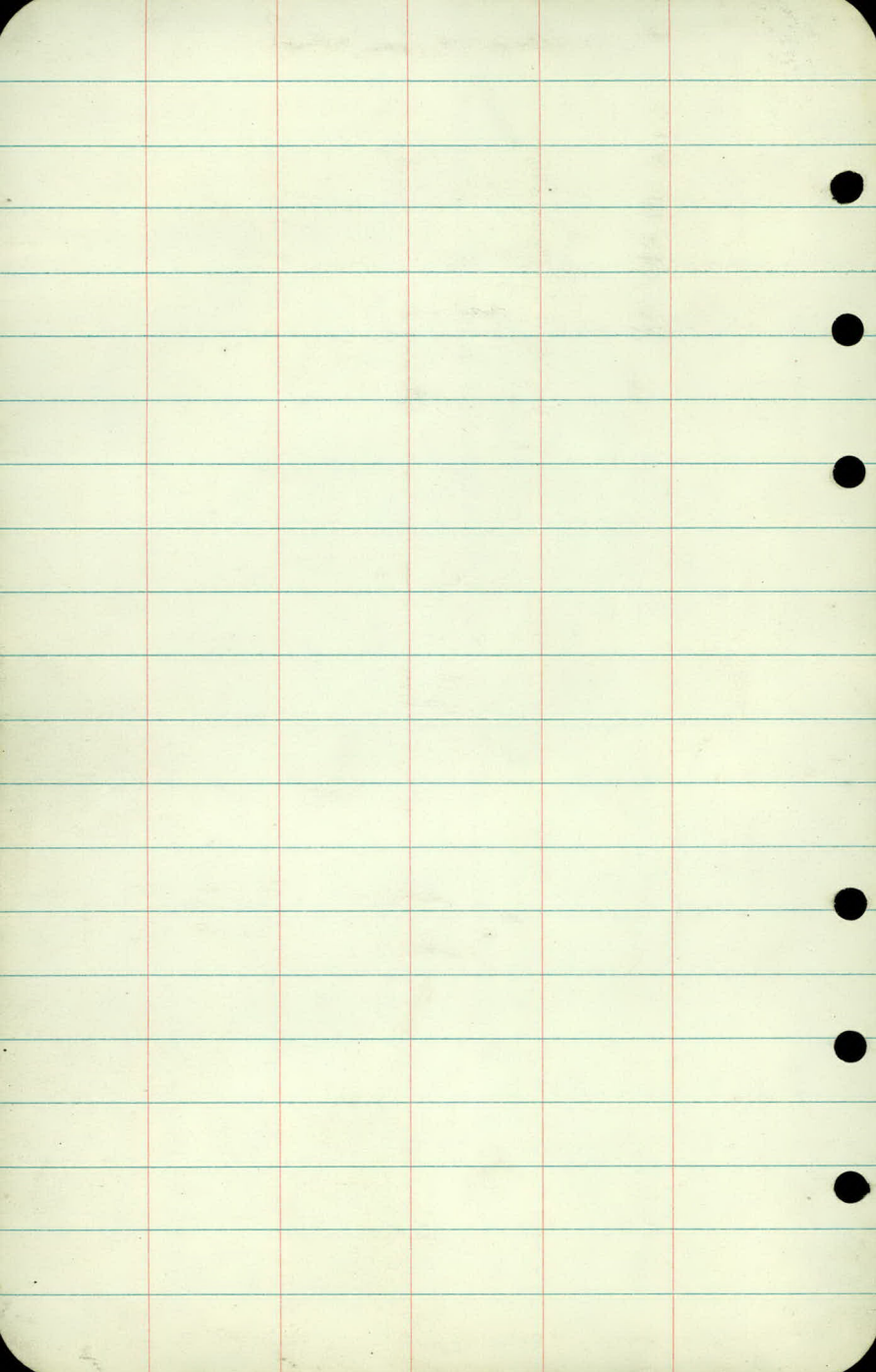
P.K. Nail

3N
12"CE

AA.61

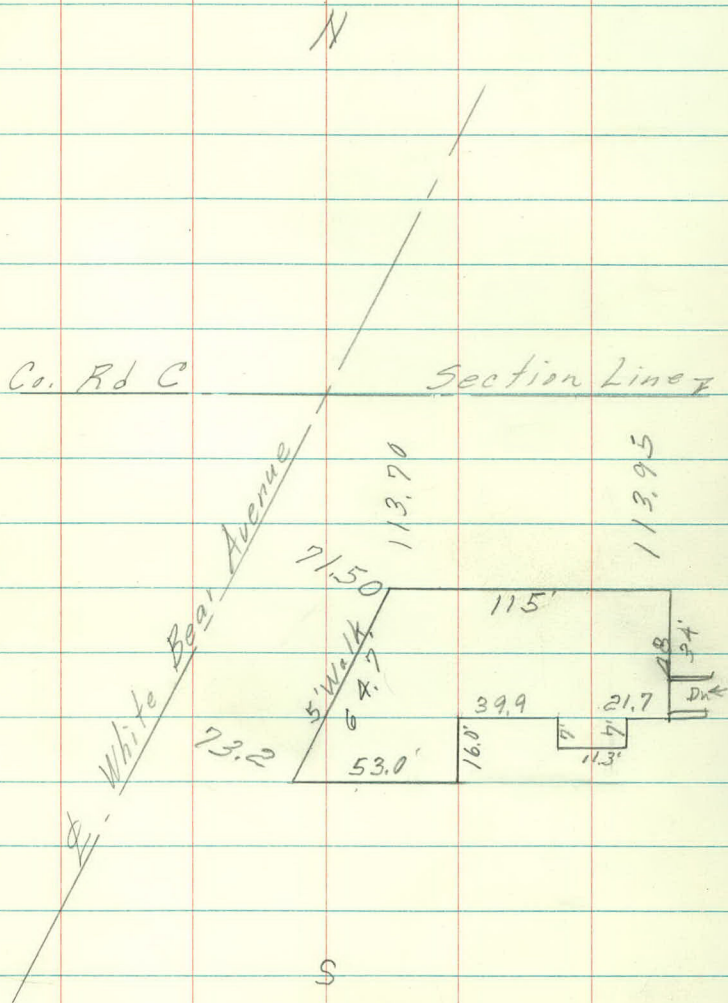
45.10

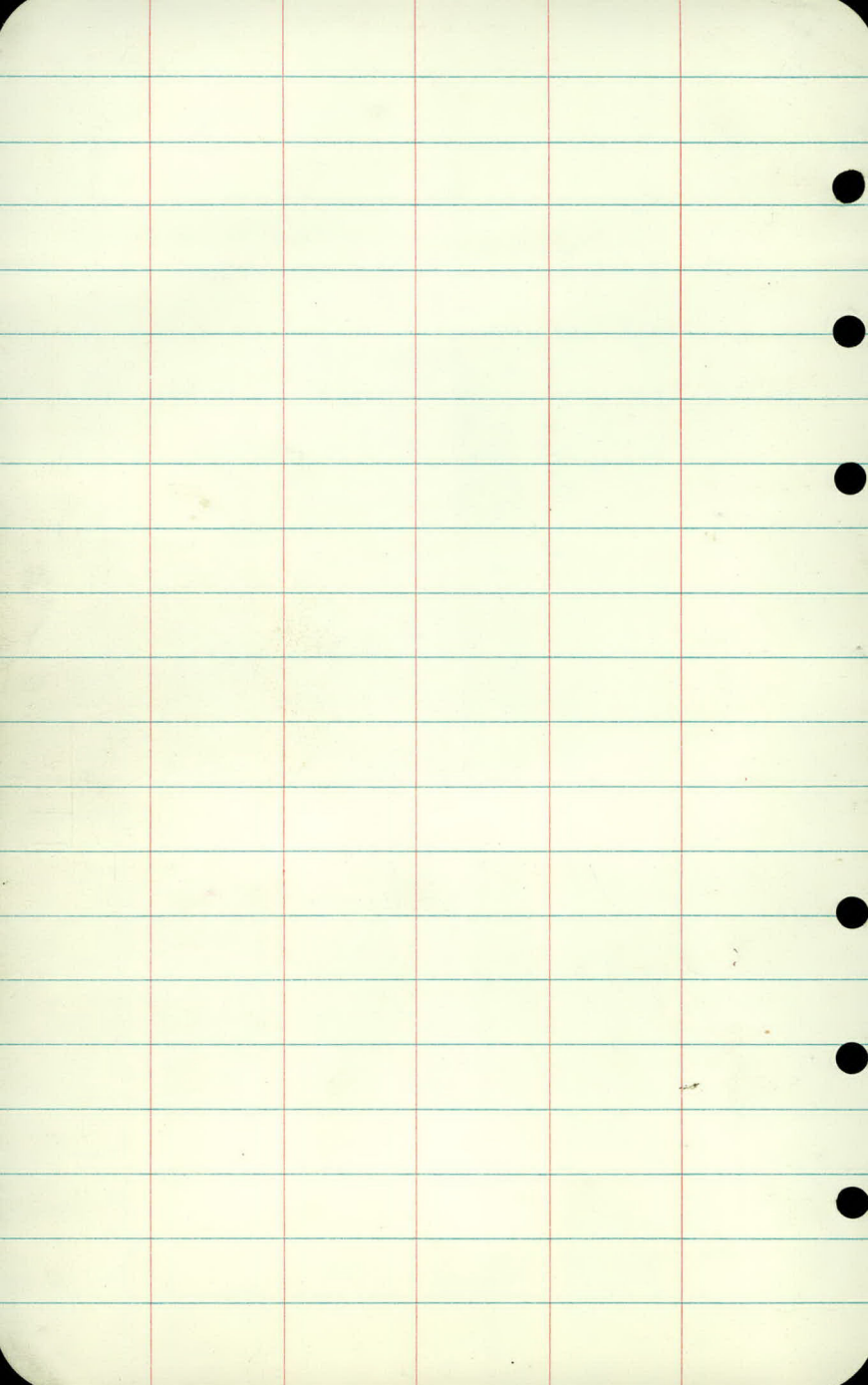
3N
TP



FK
GA
JA
CM

Jan 21, 1969





FK
WM
DM
WF

June 14, 1968

9

TOPOGRAPHY

135 SE Cor Store
 116
 11
 14
 108 POR
 14
 42 POR 18
 103 BR 11
 49 ER 11
 105 Cor Ent 47
 38 BR 29
 108 Cor Bit 47
 51 A Made 72
 37 Cor Bit 47
 102 Cor Ent 29
 25 12" Elm 45
 2
 12 Road 13.5
 197 PP 29
 199 18" Elm 45
 12" x 24" CM 21
 197 Sign 40-47
 89 EG Walk 27-33
 16" Elm 45
 190 Hyd 33
 177 Road 20
 14" Elm 45
 178 Sign 57
 154 SW Corner School 126 65' N-S
 168 Cor Ent 32+46
 10" Elm 45
 226 TP 38
 1
 155 Road 18.5
 227 R Tie 40
 199 14" Elm 45
 72 8" Elm 46
 75 12" Elm 64
 154 PP 29
 222 R Tie 40
 199 USGSEM 32
 47 ER 19
 41 Arc Lt 40
 49 ER 23
 26 POR 29
 19 PP 59
 24 MH 29
 32 BR 44
 21 Hyd 37
 23 Header 24
 15 WBV 31
 0
 16 BR 41
 24 Cgms 24
 101 MH 20

Lt

June 14, 1968

✱

RT

10
B

← Bit. Furnishings

Bit.

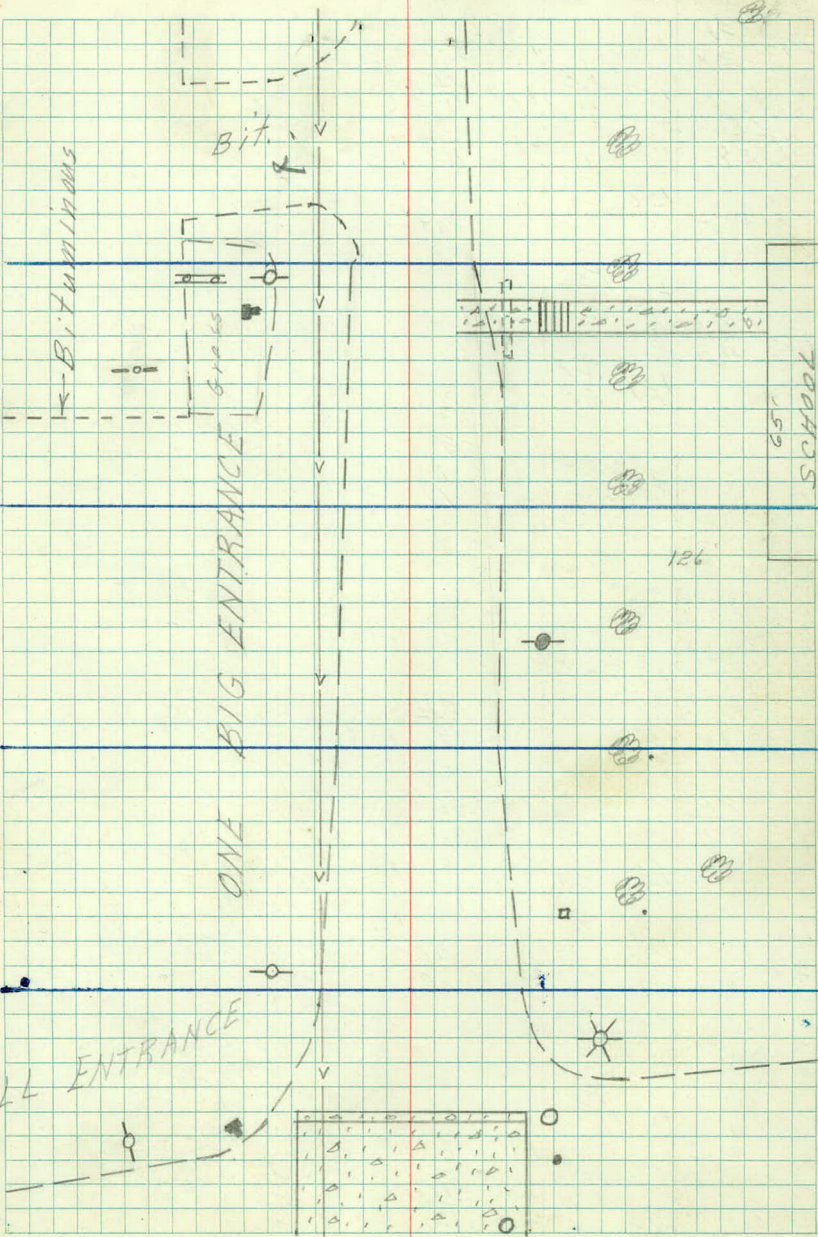
Grass

ONE BIG ENTRANCE

ALL ENTRANCE

65'
SCHOOL

126



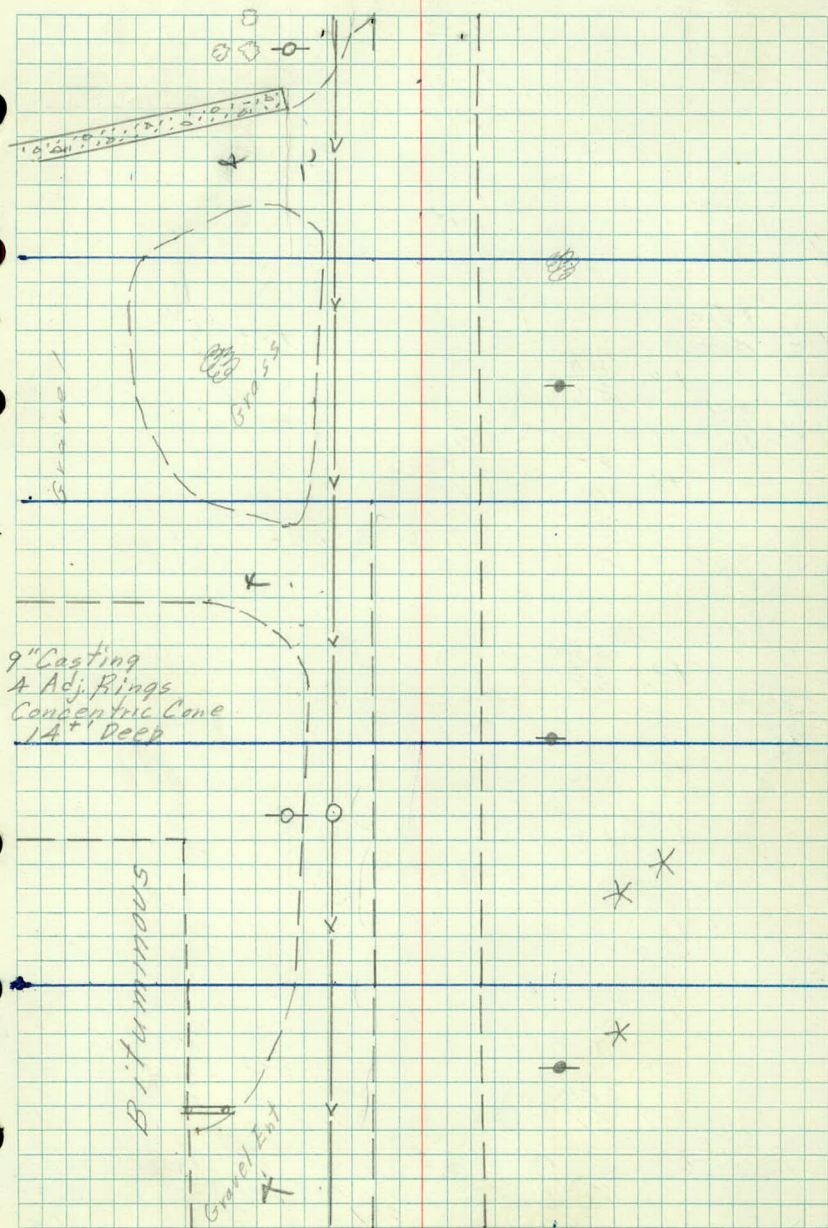
5
 ↓ Road
 10 12
 ↓ PP
 +93 28
 ↓ Spira
 +93 36
 ↓ ER
 +97 15
 ↓ SEC
 +81 28
 ↓ Walk
 +87 20
 ↓ ER
 +56 21
 ↓ POR
 +60 40
 ↓ POR
 +54 51
 ↓ 14" Maple
 +28 42
 ↓ POR
 +21 60
 ↓ POR
 +108 53
 ↓ POR
 +100 46
 ↓ POR
 +50 58
 ↓ 16" Oak
 +49 30
 ↓ TP
 +24 29
 ↓ Road
 11 12

↓ BR
 +95 22
 ↓ E. Ent
 +79 46
 ↓ MH
 +36 19
 ↓ TP
 +51 27
 ↓ Edge Ent
 +73 31
 ↓ Grovel
 +62 24
 ↓ PP
 +35 29
 ↓ B. Ent
 +62 24
 ↓ Car Bit
 +30 50
 ↓ 3" P
 +27 50
 ↓ 3" P
 +19 41
 ↓ Bit
 49
 ↓ Ent
 27
 ↓ Road
 10 12
 ↓ Edge Ent
 +86 32
 ↓ 3" P
 +90 41
 ↓ Car Ent
 +70 47
 ↓ Sign
 +74 41-49
 ↓ R. Tie
 +54 Store
 ↓ TP
 +83 28

3

June 14, 1968

18



↓ Tw 20" Oak
+53 33

↓ R Tie
+14 R.S. Lt

↓ ER
+23 11

↓ BR
+09 30

↓ POR
+14 20

↓ 20" Oak
+21 33

7

↓ MH
+01 18

↓ Road
12

↓ 22" Oak
+08 32

↓ TP
+93 29

↓ R Tie
+85 Road

↓ 12" Oak
+92 36

↓ POR
+76 15

↓ ER
+80 31

↓ BR
+68 10

↓ Arc Lt
+43 27

↓ 28" Oak
+61 35

↓ 3" Maple
+23 57

↓ 26" Oak
+24 35

6

↓ Road
10 12.4

↓ stump
+10 35

↓ 6" Elm
+86 58

↓ 10" Oak
+83 61

↓ 20" Oak
+97 33

↓ B.R. Maple
+74 66

↓ Arbivida
+51 57

↓ TP
+74 30

↓ 8" Apple
+66 62

↓ SE
Corner Church
+56 88

↓ 2" R.L. Maple
+52 32

↓ Conc Apron
+18 61 → 105

↓ Arbivida
+45 56

↓ Well
+40 56

↓ 6" Elm
+29 57

↓ 2" Maple
+20 66

↓ SW Cor. Ho
+36 59

↓ A" Maple
+36 41

↓ Sign
+17 50-56

↓ 6" Elm
+02 56

↓ R Tie
+07 Ent

↓ E 12 Ent
+09 Grove 130

5

↓ N.W. Cor Ho
+01 210'±

↓ 10" Elm
+06 76

June 14, 1968

12

9" Casting
3 Adj. Rings
Concentric Cone
14' Deep

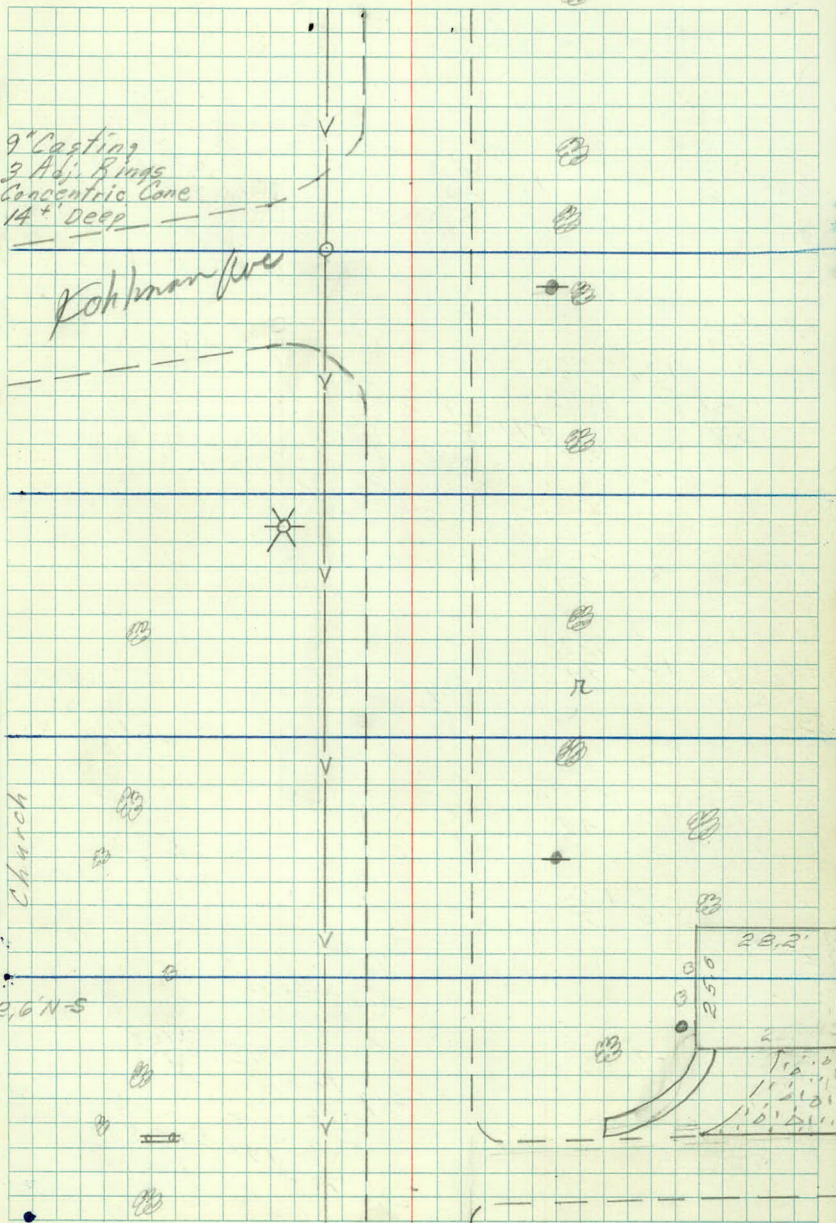
Kohlman Ave

Church

52.6' N-S

28.2'

25.0'



10

Lt.

10-12

Rt.

+97 4' Maple
39

+65 S.E. Cor. Ho
68
+42 Trip 4 Birch
55

+70 R Tie
Ho
+58 6 Maple
40

+67 TP
28

+35 4' Walk
62

+39 PP
28

+38 Yard Lt.
58

+24 26' Double Ent
Gravel

+06 5" Ash
57

+10 18" Walk
28

+36 4" Oak
26

9

+06 Spirea
28

Road
10 12

+03 Stp
35

+88 Bush
28

+91 14" Elm
35

+91 10" Birch
50

+99 Bush
29

+85 S.E. Cor. Ho
69

+71 P. Elm
49

+65 10" LP
33

+61 Lin. Ditch
35

+47 8" LP
33

+53 12" LP
34

+300 R Tie
Pitch Lt

+36 6" LP
34

+40 8" LP
36

+34 R Tie
Pitch Rt

+30 6" Ash
46

+30 10" Birch
61

+29 8" Tree
72

+30 Tw 8" Birch
40

+41 18" Willow
64

+28 W.E. 30" 9CP
29

+30 8" LP
34

+34 E.E. 30" 5CP
29

+05 4" Coll
53

+27 16" Willow
49

8

Road
10 12

+15 TP
28

+99 S.W. Cor. Ho
80

+90 PP
27

+95 27" Oak
34

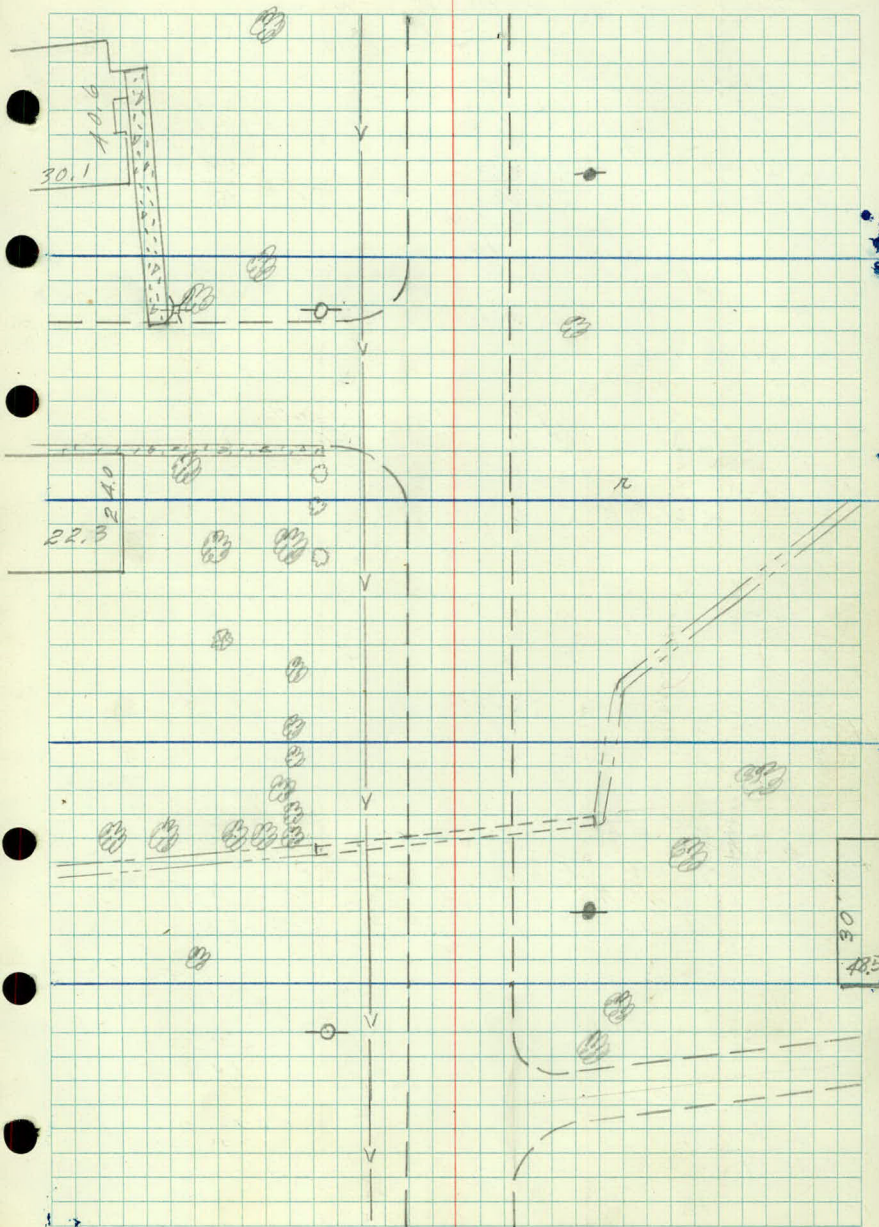
+87 16" Oak
29

+77 12" Ent
B. + 27

+73 R Tie
Ent

June 14, 1968

13



$\downarrow$ Bush
 $+43 \frac{26}{28}$

$\downarrow$ 2" Miller
 $+46 \frac{54}{54}$

$\downarrow$ 10' Ent 15" x 20' CM
 $+35 \frac{Gravel}{19}$

$\downarrow$ Tw 6" Elm
 $+28 \frac{54}{54}$

$\downarrow$ Lilac
 $+27 \frac{45}{45}$

$\downarrow$ Spires
 $+27 \frac{35}{35}$

$\downarrow$ 2" WP
 $+27 \frac{41}{41}$

$\downarrow$ SW Cor Ho
 $+22 \frac{79}{79}$

$\downarrow$ 3' Walk
 $+40 \frac{33}{33}$

$\downarrow$ 26' Oak
 $+23 \frac{51}{51}$

$\downarrow$ 8' Elm
 $+27 \frac{29}{29}$

$\downarrow$ Road
 $10 \frac{12}{12}$

$\downarrow$ TP
 $+09 \frac{28}{28}$

$\downarrow$ 6' Elm
 $+91 \frac{41}{41}$

$\downarrow$ 4' Ent
 $+62 \frac{37}{37}$

$\downarrow$ Rtre
 $+72 \frac{Ent}{Ent}$

$\downarrow$ 24' Oak
 $+66 \frac{61}{61}$

$\downarrow$ S.W. Cor. Ho.
 $+62 \frac{176}{176}$

$\downarrow$ Rtie
 $+68 \frac{Ho}{Ho}$

$\downarrow$ 6' Apple
 $+49 \frac{48}{48}$

$\downarrow$ Road
 $10 \frac{12}{12}$

$\downarrow$ PP
 $+92 \frac{27}{27}$

$\downarrow$ 6' Coll
 $+76 \frac{39}{39}$

$\downarrow$ 4' Coll
 $+71 \frac{37}{37}$

$\downarrow$ TP
 $+86 \frac{28}{28}$

$\downarrow$ 4' Oak
 $+39 \frac{31}{31}$

$\downarrow$ Tw 4" Coll.
 $+21 \frac{39}{39}$

$\downarrow$ MH
 $+27 \frac{20}{20}$

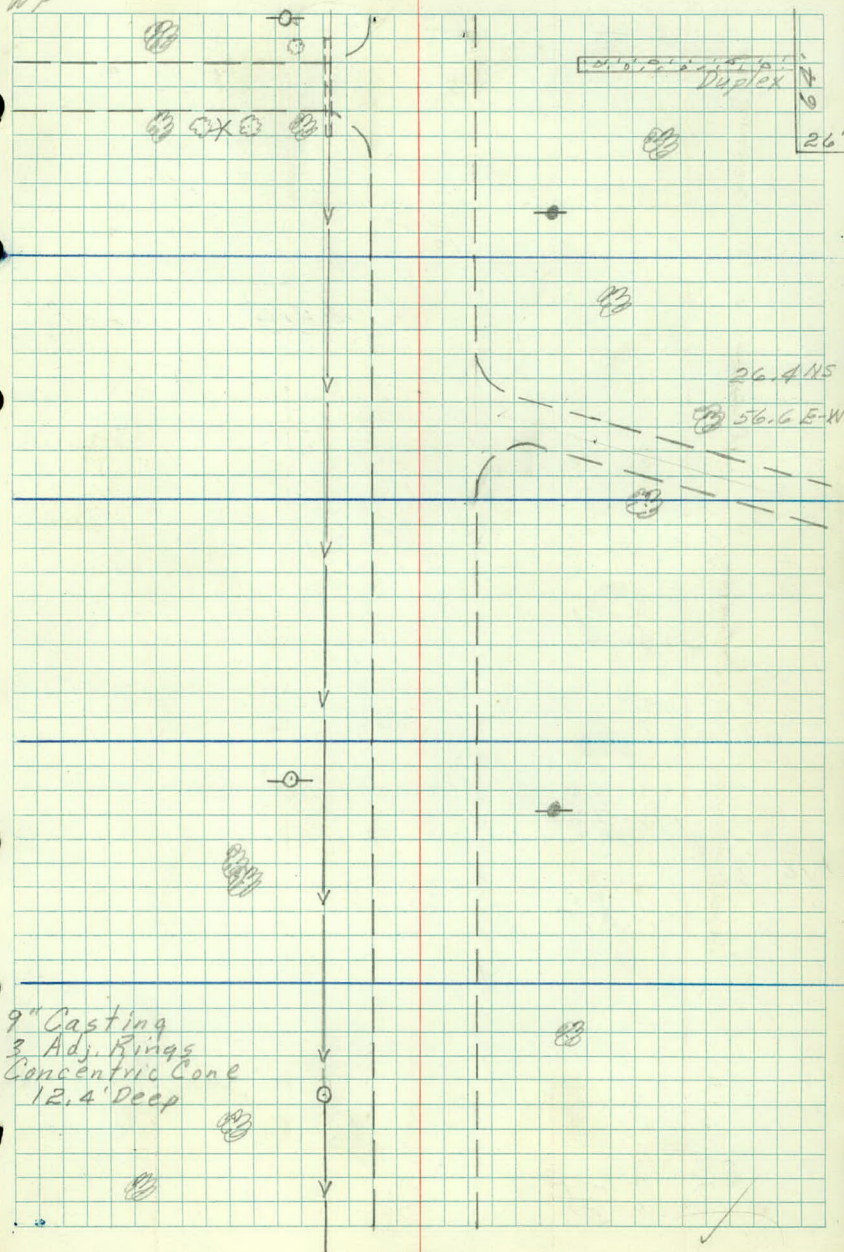
$\downarrow$ Tw 4" Birch
 $+08 \frac{59}{59}$

10

FK
WM
DM
WF

July 2, 1968

14



15
 ↓
 +91 $\frac{\text{Fe Cor.}}{24}$
 +90 $\frac{6'' \text{ Plum Tr.}}{49}$
 ↓
 +79 $\frac{10'' \text{ Apple Tr.}}{49}$
 ↓
 +87 $\frac{\text{R.Tic}}{\text{Fe.}}$
 +99 $\frac{\text{R.Tic ?}}{\text{Ent.}}$
 +73 $\frac{10'' \text{ P}}{64}$
 +67 $\frac{\text{Fe Cor.}}{34}$
 +75 $\frac{8'' \text{ Catalpa}}{42}$
 ↓
 +56 $\frac{\text{Q. 10' Gr Dr}}{39}$
 +47 $\frac{\text{E. Fe}}{24}$
 ↓
 +51 $\frac{\text{R.Tic}}{\text{Ent.}}$

↓
 +37 $\frac{\text{Stump}}{34}$
 ↓
 +39 $\frac{10'' \text{ Apple Tr.}}{50}$
 ↓
 +12 $\frac{\text{Fe Cor.}}{33}$
 +27 $\frac{\text{Any Fe}}{58}$
 ↓
 +07 $\frac{6'' \text{ B.E.}}{45}$
 +117 $\frac{6'' \text{ B.E.}}{50}$
 14
 ↓
 +36 $\frac{8'' \text{ Catalpa}}{39}$
 ↓
 +37 $\frac{\text{MH}}{20}$
 ↓
 +50 $\frac{\text{Fe}}{29}$
 ↓
 +36 $\frac{\text{Fe Cor.}}{29}$
 ↓
 +42 $\frac{\text{R.Tic}}{\text{Fe.}}$
 ↓
 +34 $\frac{4'' \text{ Catalpa}}{40}$
 ↓
 +58 $\frac{\text{Tw 24' Cott}}{45}$
 ↓
 +40 $\frac{\text{Fe Cor.}}{38}$
 ↓
 +40 $\frac{\text{E. Fe}}{45}$
 ↓
 +54 $\frac{\text{E. Fe}}{36}$
 ↓
 +25 $\frac{4'' \text{ Cedar}}{46}$
 ↓
 +25 $\frac{3'' \text{ Cedar}}{40}$
 ↓
 +39 $\frac{\text{IP}}{29}$
 ↓
 +23 $\frac{4'' \text{ Plum}}{65}$
 ↓
 +24 $\frac{\text{Q. 12' Ent.}}{28}$
 ↓
 +30 $\frac{\text{E. Ent.}}{56}$
 ↓
 +17 $\frac{3'' \text{ P}}{60}$
 ↓
 +17 $\frac{3'' \text{ P}}{63}$
 ↓
 +16 $\frac{3'' \text{ P}}{75}$
 ↓
 +15 $\frac{3'' \text{ P}}{82}$
 ↓
 +23 $\frac{4'' \text{ Plum}}{76}$
 ↓
 +17 $\frac{3'' \text{ P}}{67}$
 ↓
 +12 $\frac{\text{Bush}}{63}$
 ↓
 +12 $\frac{\text{Spirea}}{37}$
 13
 ↓
 +64 $\frac{\text{S.E. Cor. Ho.}}{77}$
 ↓
 +66 $\frac{2'' \text{ P}}{59}$
 ↓
 +72 $\frac{\text{P 3' walk}}{33}$
 ↓
 +58 $\frac{3'' \text{ CE}}{34}$
 ↓
 +98 $\frac{3'' \text{ CE}}{35}$

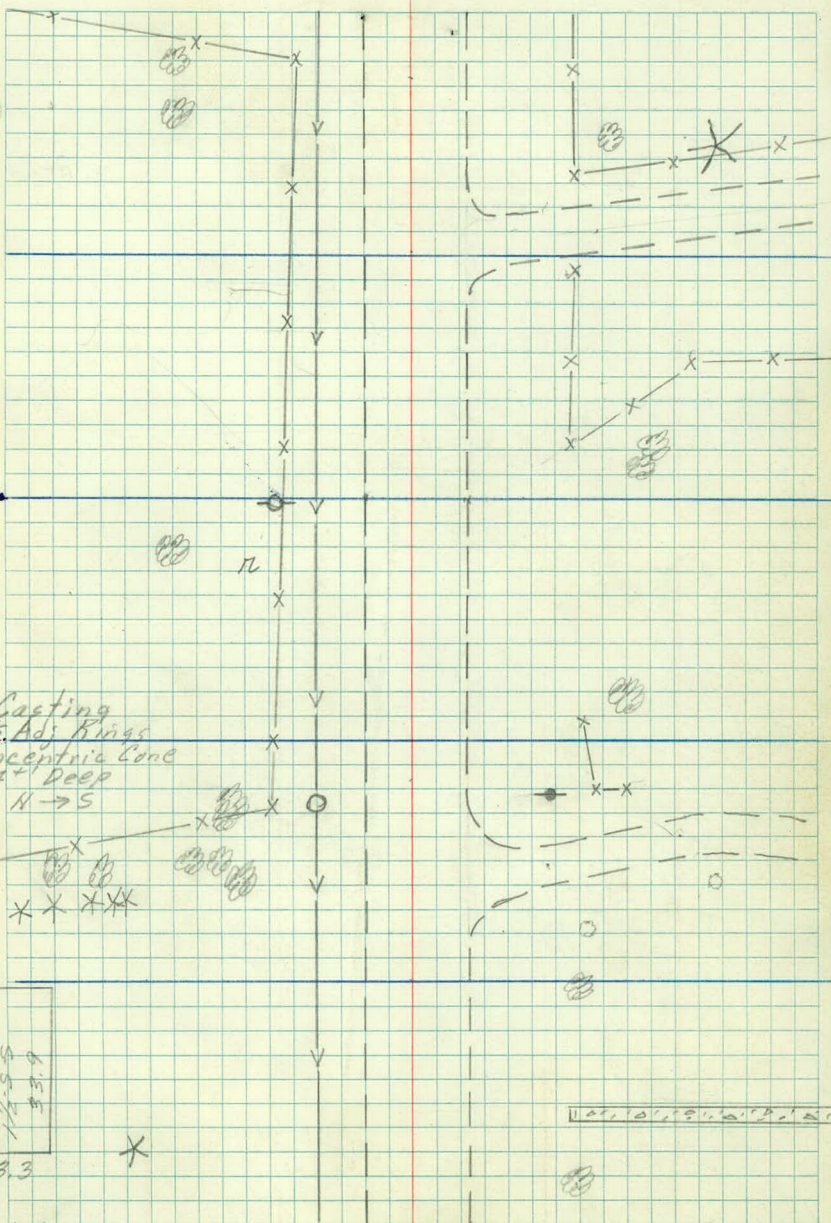
July 2, 1968

15

9" Casting
5 Adj Rings
Concentric Cone
14" Deep
N → S

1 1/2-5 1/2
#3.9

28.3



Lt

L

R4

+35 $\frac{12'' \text{ Elm}}{45}$ +08 $\frac{\text{RP}}{27}$ +04 $\frac{\text{Tw } 4'' \text{ Elm}}{551}$

17

+70 $\frac{4'' \text{ Elm}}{57}$ +55 $\frac{\text{Fc Cor}}{38}$ +53 $\frac{\text{R. Tie}}{\text{Fc}}$ +47 $\frac{9'' \text{ Ent}}{35}$ +45 $\frac{\text{R. Tie}}{\text{Ent}}$ +39 $\frac{\text{Tw } 6'' \text{ Ch Elm}}{42}$ +38 $\frac{8'' \text{ Buck Eye}}{65}$ +33 $\frac{\text{Stamp}}{22}$ +35 $\frac{6'' \text{ Cedar}}{49}$ +39 $\frac{10'' \text{ Ch Elm}}{35}$ +29 $\frac{\text{Stamp}}{26}$ +29 $\frac{8'' \text{ P. Tr}}{30}$ +10 $\frac{\text{Lill Bu.}}{35}$ +22 $\frac{\text{E. Ho}}{26}$ Road
10 12

16

+97 $\frac{\text{SE Cor. Ho}}{69}$ +99 $\frac{14'' \text{ P. Tr}}{35}$ +69 $\frac{\text{Tw } 6'' \text{ M. Ash Tr.}}{47}$ +84 $\frac{2'' \text{ Walk}}{27}$ +50 $\frac{\text{RP}}{28}$ +61 $\frac{4'' \text{ P. Tr}}{36}$ +34 $\frac{\text{Be. Lill. Ho.}}{29}$ +25 $\frac{\text{Stamp}}{45}$ +25 $\frac{6'' \text{ Choke Ch. Tr.}}{54}$ +08 $\frac{\text{Ent}}{31}$ +20 $\frac{\text{Stamp}}{29}$

15

+72 $\frac{14'' \text{ Bit Pr.}}{29}$ +65 $\frac{\text{R. Tie}}{\text{Ent}}$ +63 $\frac{\text{S. Eng } 15'' \text{ C.M. Culv. } \times 20'}{29}$ +16 $\frac{\text{Be. Conc. Curb}}{53}$ +21 $\frac{2'' \text{ P.}}{57}$ +23 $\frac{\text{S.W. Cor. Ho}}{90}$ +10 $\frac{\text{E. Bl. Top } 18'}{\text{Ent}}$ Road
10 12+99 $\frac{\text{S. End } 15'' \text{ C.M. Culv. } \times 26'}{34}$ +96 $\frac{\text{Tele. P.}}{28}$ +64 $\frac{\text{Field Ent}}{}$ +11 $\frac{5'' \text{ P. Tr}}{63'' \text{ P.}}$ +03 $\frac{8'' \text{ P.}}{57}$ +10 $\frac{4'' \text{ Catalpa}}{41}$ +95 $\frac{5'' \text{ P.}}{39}$ +81 $\frac{11'' \text{ Elm}}{50}$ +93 $\frac{8'' \text{ P.}}{51}$ +46 $\frac{8'' \text{ P. Tr}}{56}$ +65 $\frac{7'' \text{ P. Tr}}{44}$ +37 $\frac{\text{Fc Cor}}{33}$ +54 $\frac{\text{N.W. Cor. Ho}}{24}$ +22 $\frac{8'' \text{ Elm Tr.}}{54}$ +18 $\frac{\text{Tele. P.}}{28}$ +06 $\frac{4'' \text{ Willow}}{41}$

July 2, 1968

16

9" Casting
3 Adj Rings
Concentric Cone
14' Deep
N → S

26.2
Perch
48.3
53.8

48.3 NS
38.5 EW

54.4

30.9

Correct

Lt

Rt

20

L

?

		+78 $\frac{\text{End Rad.}}{75}$	+94 $\frac{\text{M.H.}}{19}$
+94 $\frac{\text{M.H.}}{20}$	+69 $\frac{\text{GGV}}{31}$	+72 $\frac{\text{P.O.R.}}{34}$	+71 $\frac{\text{Gas G.V.}}{32}$
+79 $\frac{\text{End Rad.}}{31}$	+72 $\frac{\text{Arch P.}}{27}$	+66 $\frac{\text{Gas Be. Post}}{23}$	
+54 $\frac{\text{Be. Rad.}}{10}$	+70 $\frac{\text{P.O.R.}}{17}$		
+57 $\frac{\text{End P. Bu.}}{51}$	+60 $\frac{\text{Fe}}{48 \text{ to } 59}$		
+61 $\frac{\text{Cor. P. Bu.}}{32}$			
+42 $\frac{\text{Be. P. Bu.}}{35}$	+43 $\frac{\text{End Fe}}{33}$	+41 $\frac{\text{Be. Rad.}}{12}$	+61 $\frac{\text{P.O.R.}}{21}$
+32 $\frac{\text{Be. Fe}}{33}$			

Road

10 12

19
+99 $\frac{\text{S.E. Cor. Ho}}{72}$

+85 $\frac{\text{Tel. P.}}{28}$

+64 $\frac{\text{P.P.}}{28}$
+53 $\frac{\text{For Apt. Tr.}}{41}$

+29 $\frac{6" \text{ Apt. Tr.}}{41}$
+08 $\frac{6" \text{ Apt. Tr.}}{40}$

+11 $\frac{6" \text{ Be. Elm.}}{29}$

18

Road
10 12

+86 $\frac{\text{W End 24" S.C.P.}}{27}$
+76 $\frac{6" P.}{38}$
+68 $\frac{6" P.}{38}$ +68 $\frac{6" P.}{49}$
+59 $\frac{\text{Fe Cor.}}{38}$

Lt.

Rt.

L

$$+47 \frac{6" Elm}{46}$$

$$+18 \frac{Tw 8" M Ash}{64}$$

$$+92 \frac{Bu Old Tr}{62}$$

$$+68 \frac{SE Cor Ho}{80}$$

$$+74 \frac{Arch P.}{28}$$

$$+70 \frac{Ho Wall}{18 to 28}$$

$$+59 \frac{15" Ent 15" x 20" Calu}{22 CR}$$

$$+54 \frac{R. Tie}{Ent}$$

$$+32 \frac{Rose Bu.}{35}$$

$$+30 \frac{8" Ash}{45}$$

$$+104 \frac{NE Cor Ho}{83}$$

$$\frac{Road}{10 \ 10}$$

21

$$+89 \frac{2' Conc Walk}{19}$$

$$+43 \frac{Lil Bu}{46} +52 \frac{10" Ash}{41}$$

$$+17 \frac{PP}{28} +28 \frac{End Rad}{10}$$

$$+20 \frac{Be Rad}{10} +29$$

$$+41 \frac{Honey Se. Bu.}{48}$$

$$+43 \frac{R. Tie}{Ent}$$

$$+18 \frac{12" P.}{56}$$

$$+11 \frac{14" P.}{47}$$

$$+39 \frac{12" x 13" CM Calu}{36}$$

$$+33 \frac{8" D. Ent}{46}$$

$$+19 \frac{14" P}{46}$$

$$+99 \frac{N. W. Cor. Ho}{144}$$

$$+79 \frac{12-6" P. 1-54}{36}$$

$$+65 \frac{8" Ent Gr Dr.}{24}$$

$$+48 \frac{Tele P.}{31} +48 \frac{18" P.}{40}$$

$$+65 \frac{18" CM x 20" Calu}{24}$$

$$+39 \frac{ER.}{11}$$

$$+19 \frac{Tele P.}{24}$$

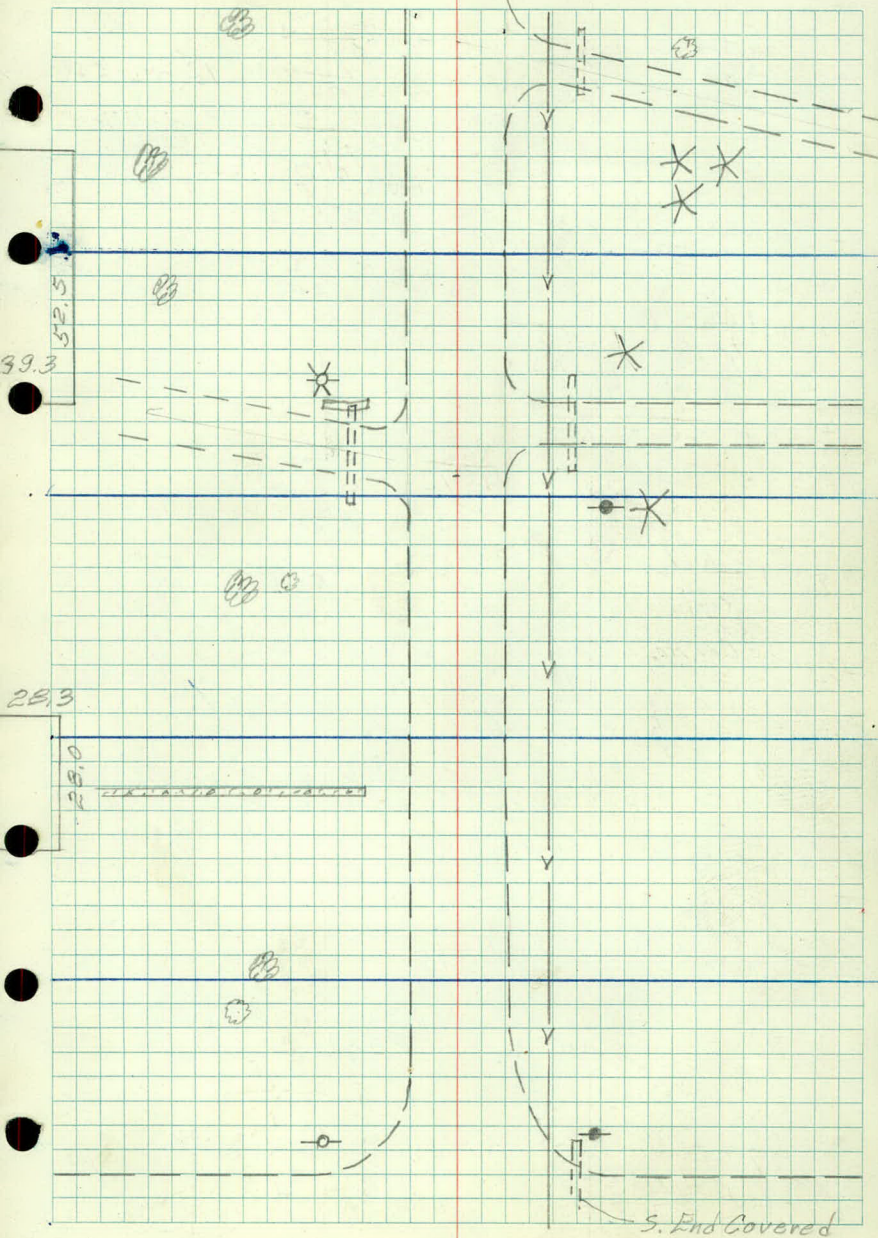
$$+22 \frac{P. QR}{16}$$

$$+17 \frac{No End 15" CM Calu. Plugged}{25}$$

$$+10 \frac{Be Rad}{30}$$

July 2, 1968

18



L.T.

E

R.T.

25

$$+88 \frac{PP}{29} +94 \frac{5''P}{38}$$

$$+80 \frac{SE Cor Ho}{89} +81 \frac{8'' Elm}{66}$$

$$+72 \frac{Conc Curb}{26} +76 \frac{2''P}{37} +80 \frac{Robu}{32}$$

$$+62 \frac{14' Gr Ent 15'' \times 20' cm culv}{29}$$

$$+54 \frac{conc. Curb}{25}$$

$$+34 \frac{3'' P}{64}$$

$$+34 \frac{1'' N.P.}{43} +34 \frac{5'' W.P.}{55}$$

$$+34 \frac{1'' N.P.}{30} +34 \frac{1'' W.P.}{36}$$

$$+15 \frac{15'' \times 20' cm culv}{25}$$

$$+97 \frac{SW Cor Ho}{2''P 86} +97 \frac{10'' Elm}{2''P 54}$$

$$+95 \frac{2''P 86}{44} +98 \frac{2''P 54}{46}$$

$$+81 \frac{Cor Bit Ent}{25} +95 \frac{sign}{36}$$

$$+65 \frac{Con Bit Ent}{45} +70 \frac{Con Bit Ent}{78}$$

$$+69 \frac{Con Bit Ent}{24} +71 \frac{Ed Bit Ent}{36}$$

$$+68 \frac{Tele P}{28}$$

$$+51 \frac{SW Cor Bit P}{51-76}$$

$$+53 \frac{SW Cor EW 6.3' \times 15.8}{33}$$

Road
11 10

24

$$+94 \frac{6'' R. Plum}{64}$$

$$+64 \frac{4'' R. Plum}{64}$$

$$+63 \frac{SE Cor Ho 2855}{85}$$

$$+44 \frac{4'' P}{45} +44 \frac{5'' P}{54} +44 \frac{5'' P}{64}$$

$$+44 \frac{Stump}{37} +44 \frac{1'' P}{38}$$

$$+36 \frac{1'' P}{49} +44 \frac{Stump}{29}$$

$$\frac{NE Cor Ho}{90}$$

$$+23 \frac{PP}{29}$$

$$+29 \frac{PP}{29} +29 \frac{Tw 8'' Bir}{58}$$

$$+22 \frac{M.H.}{19}$$

Road
11 11

23

$$+98 \frac{Tele P}{28}$$

$$+82 \frac{Tw 8'' Bir}{59}$$

$$+77 \frac{2'' P}{46}$$

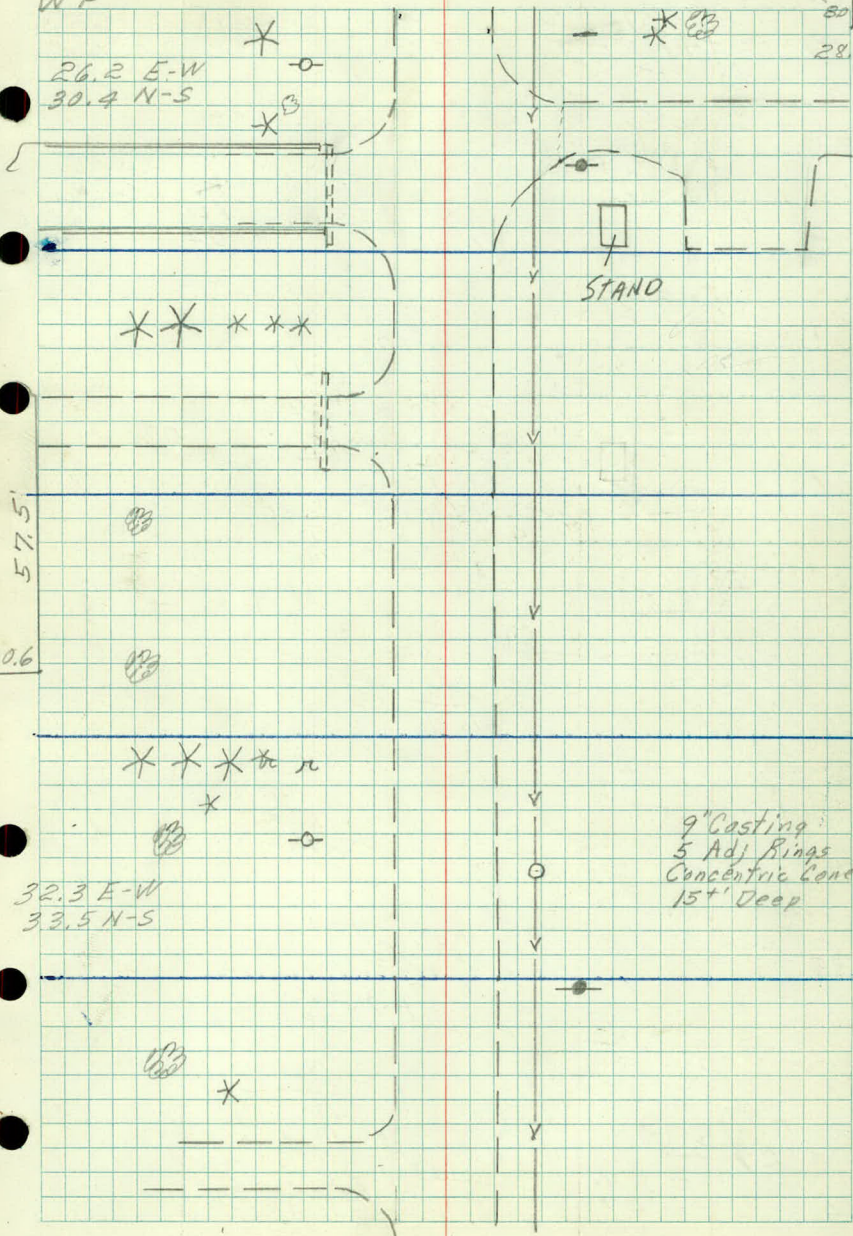
$$+62 \frac{10' Gr Dr}{Ent}$$

FK
WM
DM
WF

July 3, 1968 19

10.2
80
28.1

26.2 E-W
30.4 N-S



Lt.

L

Rt

$$+47 \frac{Tw 4'' O}{23}$$

27

$$\begin{array}{r} \text{Road} \\ 10 \ 10 \end{array} \quad \begin{array}{r} Fe \\ 37 \end{array} \quad +07 \quad \begin{array}{r} 4'' Cot \\ 34 \end{array}$$

$$+99 \frac{3-4'' Oak}{26}$$

$$+50 \quad 24'' \times 48'' SC \times \text{Drain}$$

$$+56 \frac{MH}{20}$$

$$+46 \frac{Tw 10'' BE}{76}$$

$$+46 \frac{Be Cr Fe}{90}$$

$$+54 \frac{Fe Cor}{33}$$

$$+46 \frac{PP}{28}$$

$$+51 \frac{Tw 24'' Cot. Wd}{65}$$

$$+30 \frac{10' Gr Ent}{23}$$

$$+19 \frac{5F 12'' \times 26G M. CW}{23}$$

$$\begin{array}{r} \text{Road} \\ 10 \ 10 \end{array}$$

26

$$+94 \frac{6'' Bir}{53}$$

$$+84 \frac{Tele P}{29}$$

$$+54 \frac{3-4'' Bir}{56}$$

$$+48 \frac{8'' P}{46}$$

$$+46 \frac{S. E. Cor. Ho.}{93}$$

$$+27 \frac{5'' Ash}{98}$$

$$+24 \frac{MP}{47}$$

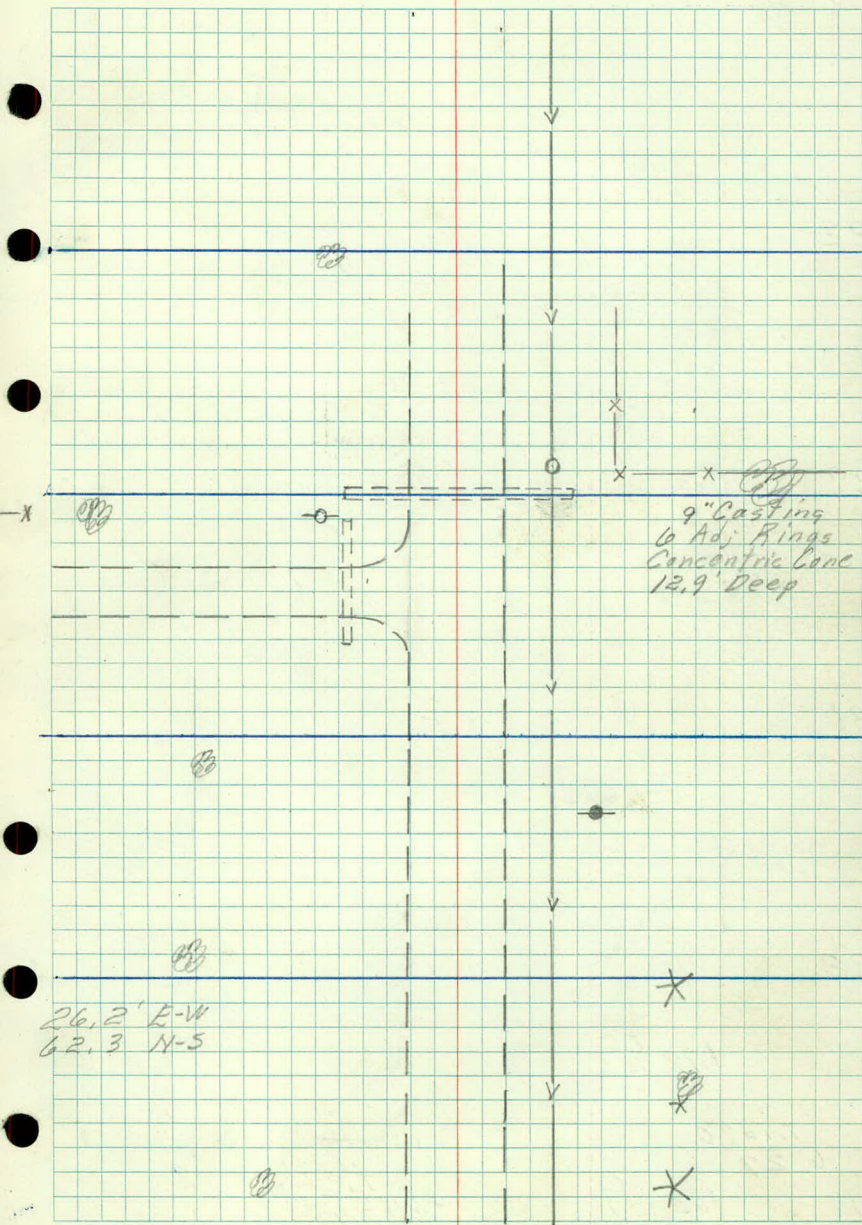
$$+08 \frac{8'' Elm}{41}$$

$$\begin{array}{r} \text{Road} \\ 11 \ 10 \end{array} \quad +07 \quad \begin{array}{r} 8'' P \\ 45 \end{array}$$

25

July 3, 1968

20



30

<u>Road</u>	<u>Fe</u>
11 10	41

 $+59 \frac{Tw}{23} 40$
 $+51 \frac{PP}{26}$

23

29

<u>Road</u>	<u>Fe</u>
10 10	40

 $+09 \frac{T.P.}{28}$

30

 $+70 \frac{4'cott}{39}$

28

<u>Road</u>	<u>Fe</u>
10 10	38

 $+98 \frac{PP}{28}$
 $+66 \frac{Trip}{27} 80$
 $+63 \frac{8'0}{27}$
 $+61 \frac{TP}{29}$

FK
DS
DM
PF

August 1, 1969

21

B

32

$$\begin{array}{r} \text{Fe} \\ 47 \end{array} \quad \begin{array}{r} \text{Road} \\ 22-2 \end{array} \quad \begin{array}{r} \text{Fe} \\ 22 \end{array}$$

$$+90 \quad \begin{array}{r} \text{PP} \\ 40 \end{array}$$

27

$$+93 \quad \begin{array}{r} \text{TP} \\ 15 \end{array}$$

28

31

$$\begin{array}{r} \text{Fe} \\ 40 \end{array} \quad \begin{array}{r} \text{Road} \\ 165 \end{array} \quad \begin{array}{r} \text{Fe} \\ 28 \end{array}$$

?

$$+59 \quad \begin{array}{r} \text{B.B. Fe} \\ 38 \end{array}$$

$$+50 \quad \begin{array}{r} \text{Road} \\ 138 \end{array}$$

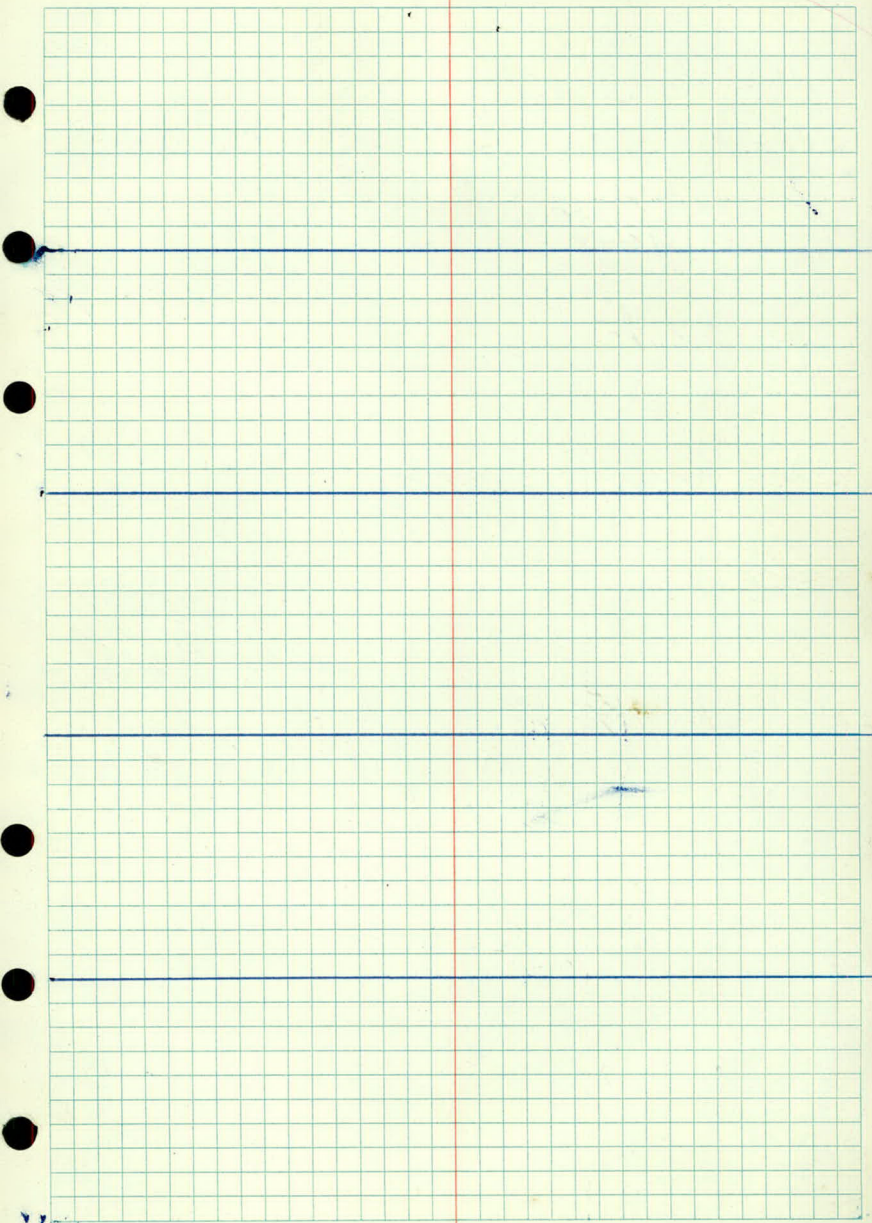
$$+42 \quad \begin{array}{r} \text{PP} \\ 30 \end{array}$$

25

$$+52 \quad \begin{array}{r} \text{TP} \\ 23 \end{array}$$

28

30



35 $\frac{Fe}{4}$ Road 44-24

? +83 $\frac{PP}{61}$ +74 $\frac{Fe}{\cancel{2}}$
 33 +67 $\frac{TP}{1}$

+15 $\frac{E.B. Fe}{60}$

+38 $\frac{\cancel{2} Ent}{Field}$

34 $\frac{Fe}{58}$ 35 $\frac{Road}{-15}$ $\frac{Fe}{9}$

+40 $\frac{PP}{49}$
 23

+37 $\frac{TP}{9}$
 35

33 $\frac{Fe}{52}$ Road 28-8

+10 $\frac{MH}{2}$
 Fe 16

August 1, 1968

23

9" Casting
2 Adj. Rings
Concentric Cone
Very Deep
N → S

$$+150 \frac{\text{Pond}}{40}$$

$$+14 \frac{14^{\circ}0}{11}$$

$$+30 \frac{\text{Pond}}{26}$$

$$+09 \frac{\text{TP}}{21}$$

37

$$\frac{\text{Road}}{61-40}$$

$$\frac{\text{Pond}}{26}$$

$$+82 \frac{20^{\circ}0}{17}$$

$$+70 \frac{20^{\circ}0}{12}$$

$$+50 \frac{\text{EFe}}{5}$$

$$+150 \frac{\text{Pond}}{25}$$

$$+50 \frac{18^{\circ}0}{6}$$

$$+38 \frac{\text{MH}}{25}$$

$$+37 \frac{\text{PP}}{70}$$

$$+35 \frac{16^{\circ}0}{5}$$

36

$$\frac{\text{EFe}}{9}$$

$$\frac{\text{Road}}{53-32}$$

$$\frac{\text{Pond}}{30}$$

$$+91 \frac{\text{TP}}{11}$$

$$+70 \frac{\text{Pond}}{50}$$

$$+86 \frac{24^{\circ}0}{6}$$

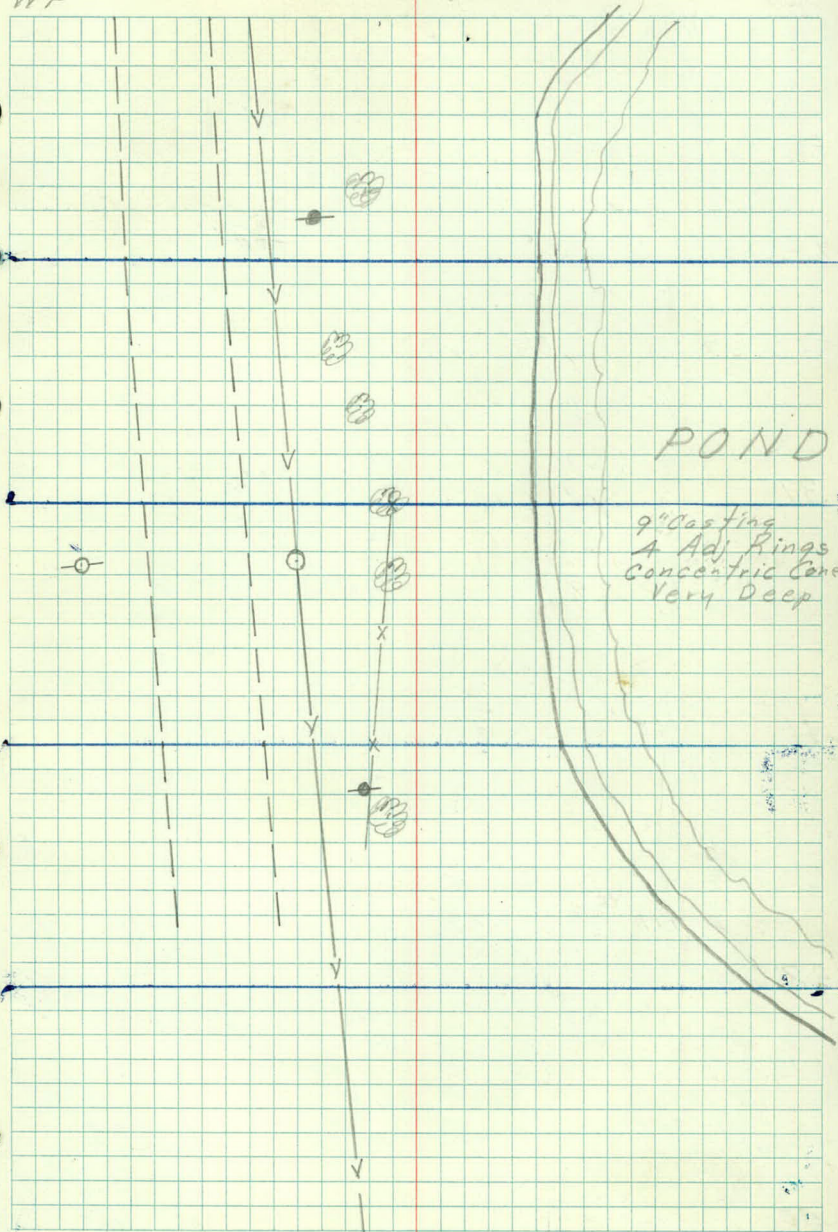
$$+50 \frac{\text{Pond}}{70}$$

35

FK
DM
WF

August 1, 1968
August 2, 1968

24



40

Road
68 49+99 $\frac{EFe}{25}$ +65 $\frac{MH}{41}$ +62 $\frac{B. Fe}{27}$ +54 $\frac{Cor. Garden}{69}$ +36 $\frac{20"O}{27}$ +33 $\frac{PP}{86}$ +18 $\frac{18"O}{28}$

39

Road
68-49Garden
68+95 $\frac{40"Oak}{28}$ +68 $\frac{TP}{32}$ +33 $\frac{Lilac}{27}$ +33 $\frac{Cor. Garden}{68}$ +19 $\frac{NE 15"CM}{3}$ +08 $\frac{E 9'Ent}{X-Gravel}$

38

Road
66-46+97 $\frac{30"Oak}{84}$ +96 $\frac{Stp ?}{45}$ +92 $\frac{S. E 15" X 27"CM}{1}$ +95 $\frac{26" Bassk.}{3}$ +94 $\frac{Stp.}{12}$ +87 $\frac{36"Oak}{20}$ +85 $\frac{PP}{82}$ +65 $\frac{Pond}{95}$ +62 $\frac{E. E 24"SCP}{28-77}$

August 2, 1968

25

9" Casting
2 Adj. Rings
Concentric Casing
Very deep

GARDEN

Pond

$$\downarrow \frac{PP}{+28 \quad 67}$$

$$\downarrow \frac{TR}{+09 \quad 11}$$

$$\downarrow \frac{Road}{35 - 35}$$

$$\downarrow \frac{Fe}{41}$$

42

$$\downarrow \frac{30 \frac{3}{4} \text{ Coll.}}{+50 \quad 39}$$

$$\downarrow \frac{B. Fe}{+45 \quad 42}$$

$$\downarrow \frac{Road}{63 - 43}$$

41

$$\downarrow \frac{E9' \text{ Enl}}{+96 \quad C. Rock}$$

$$\downarrow \frac{20'' \text{ Enl}}{+85 \quad 91}$$

$$\downarrow \frac{PP}{+81 \quad 77}$$

$$\downarrow \frac{22'' \text{ Enl}}{+64 \quad 89}$$

$$\downarrow \frac{18'' \text{ Enl}}{+51 \quad 89}$$

$$\downarrow \frac{16'' \text{ Enl}}{+36 \quad 89}$$

$$\downarrow \frac{26'' \text{ Enl}}{+07 \quad 90}$$

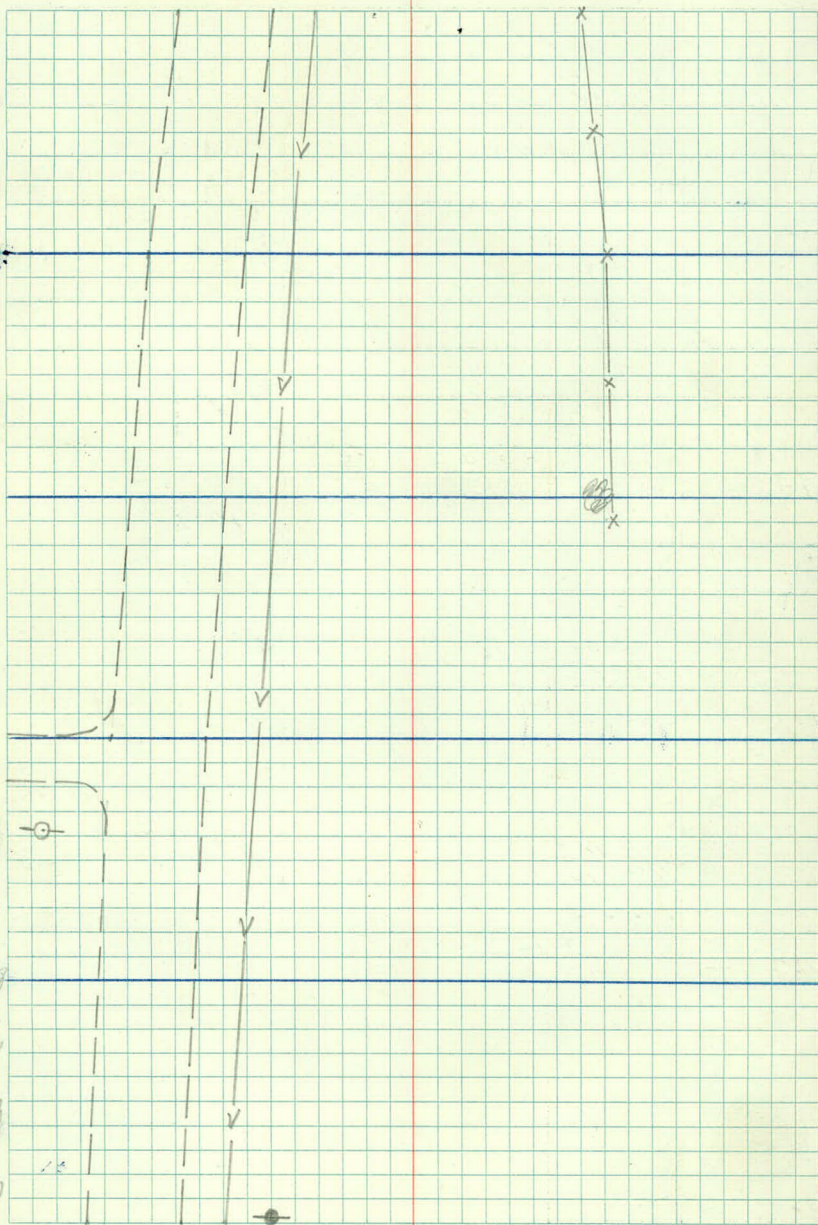
$$\downarrow \frac{18'' \text{ Enl}}{+22 \quad 89}$$

40

$$\downarrow \frac{TP}{+01 \quad 30}$$

August 2, 1968

26



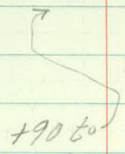
45

44

↓ ↓
Road
33-13

↓
Fe
29

18-6' Trees
18-30



+90 to

↓
+78 PP
52

↓
+71 IP
5

↓
+42 MH
10

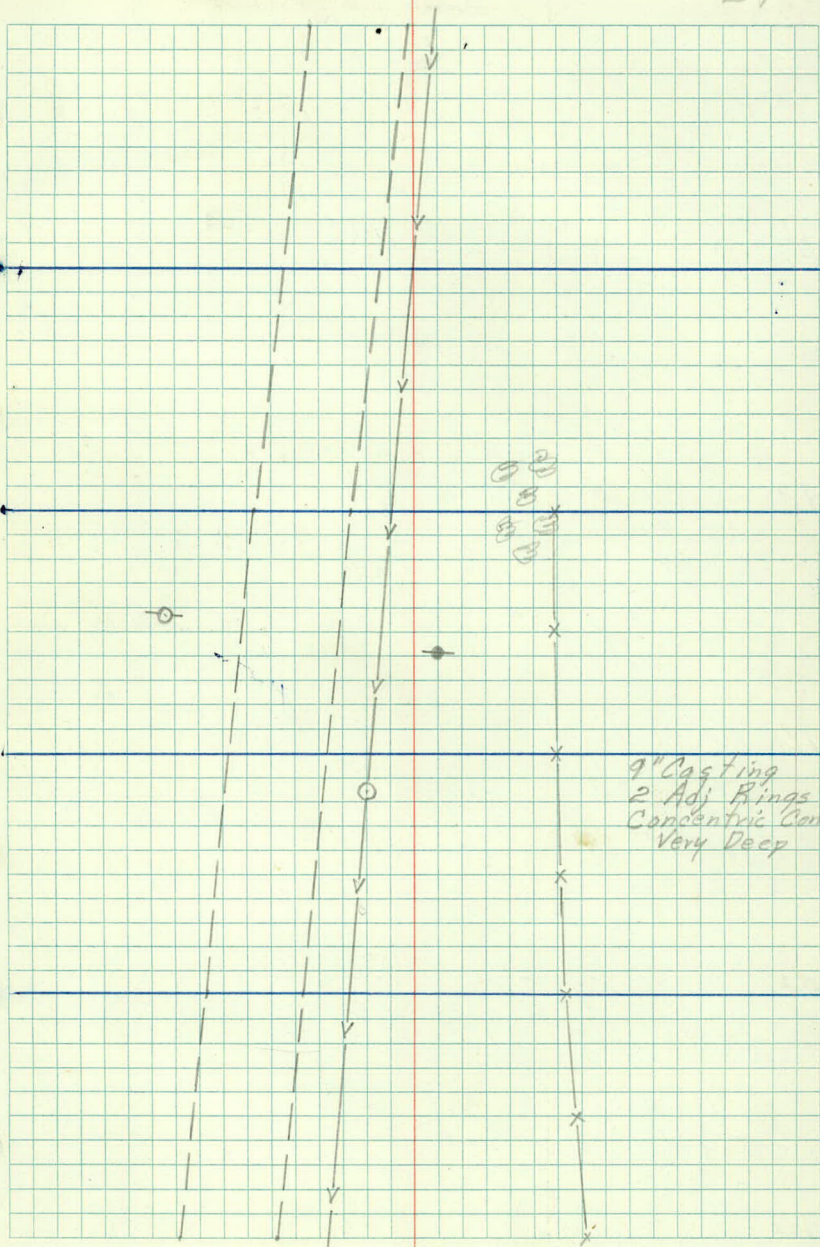
43

↓ ↓
Road
43 23

↓
Fe
32

August 2, 1968

27



↓
TP
+46 43

↓
Libor
+44 42

↓
6" BE
+36 34

↓
Fe Cor
+25 44

↓
12 Ent
+35 35

↓
4" E/m
+17 15

↓
Tw 4" E/m
+10 16

↓
R. Tie
+21 42

↓
Field
+14 Ent

↓
MH
+11 31

↓
Fe
Road
1-21

↓
Fe
42

↓
PP
+71 20

↓
Road
10 10

↓
Fe
33

↓
TP
+65 25

↓
PP
+22 37

↓
WE 24" SCP
+05 38

↓
6" BE
+02 11

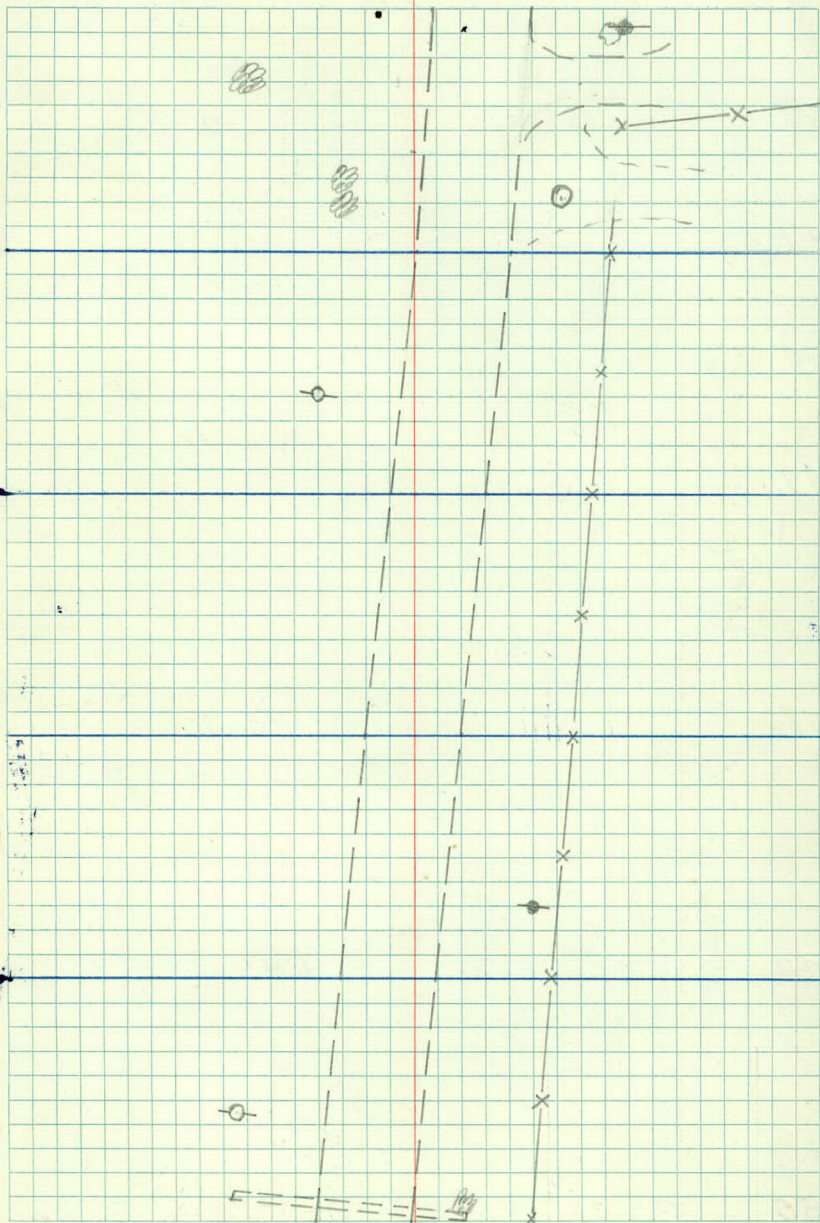
↓
E.E. 24" SCP
+01 11

↓
Road
21.4 - 1.4

↓
Fe
24

August 2, 1968

28



50

↓
Road
14-35

↓
+63 $\frac{PP}{1}$

↓
+58 $\frac{\text{Tower}}{60-41}$

↓
+62 $\frac{TP}{50}$

↓
+39 $\frac{\text{Tower}}{61-42}$

↓
+24 $\frac{6"CE}{76}$

↓
+09 $\frac{G. Main Pipe}{10}$

↓
+07 $\frac{G. Main Pipe}{57}$
↓
Road
13-35

49

↓
+50 $\frac{TP}{51}$

↓
+22 $\frac{8" P}{56}$

↓
+22 $\frac{8" P}{63 \text{ Row}}$

+36 $\frac{E. Power}{\text{Line } \Phi}$

↓
+16 $\frac{6" P}{54}$

↓
+12 $\frac{10" P}{56}$

↓
+14 $\frac{\text{Honey Suck}}{47}$

↓
+15 $\frac{PP}{6}$

↓
+01 $\frac{14" P}{71}$

↓
Road
9-29

48

↓
+53 $\frac{4" E. m}{58}$

↓
+54 $\frac{12" CE}{33}$

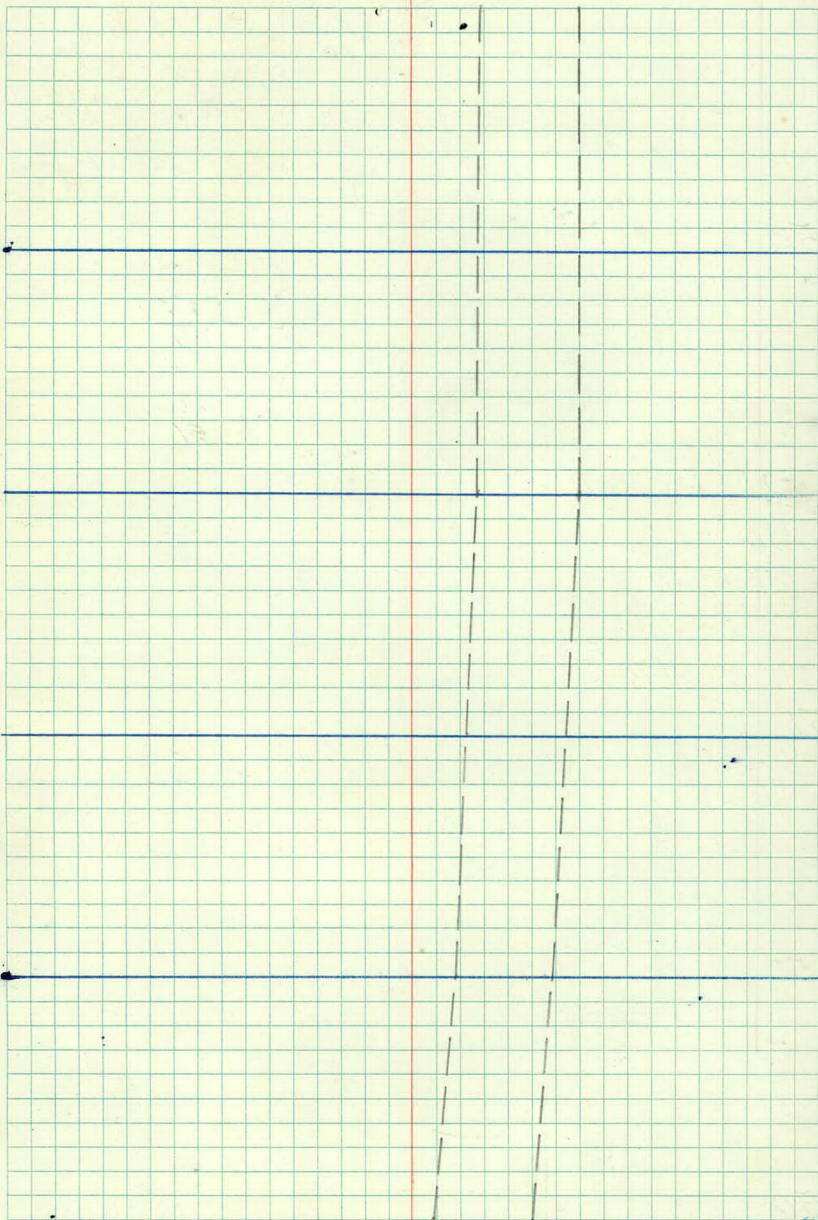
↓
+87 $\frac{14" P}{50}$

↓
+94 $\frac{14" P}{49}$

↓
+77 $\frac{12" P}{47}$

August 2, 1968

29



+43 $\frac{RTie}{Ho}$

+38 $\frac{SWCor Ho}{124}$

+19 $\frac{TP}{45}$

+13 $\frac{\pm 8' Ent}{Bt 46}$

Road
10-38

+100 $\frac{3" P}{62}$

+97 $\frac{3" P}{57}$

+94 $\frac{MH}{40}$

+91 $\frac{3" P}{61}$

+72 $\frac{6" Catalpa}{61}$

+51 $\frac{3" Mt. Ash}{83}$

+39 $\frac{3" P}{62}$

+39 $\frac{3" P}{73}$

+32 $\frac{TP}{47}$

+106 $\frac{PP}{5}$

Road
12-33

+96 $\frac{Tw 6" CE}{52}$

+72 $\frac{RTie}{Ho}$

+66 $\frac{SWCor Ho}{120}$

+16 $\frac{\pm 38' Ent}{Gravel}$

FK
DM
HL
WF

August 5, 1968

30

9" Casting
5 Adj Rings
Concentric Cone
15' Deep

24.2 E-W
32.3 NS

X X

41 NS
30 E-W

55

Road	Conc	Road
7	4-24	34

+87 $\frac{BR}{5}$ +93 $\frac{POR}{41}$ +85 $\frac{BR}{60}$ +74 $\frac{ECORdD}{}$ +63 $\frac{ER}{64}$ +63 $\frac{ER}{29}$ +52 $\frac{MH}{34}$ +45 $\frac{PP}{15}$ +43 $\frac{EE245CP}{38}$ +46 $\frac{POR}{35}$ +49 $\frac{POR}{5}$ +30 $\frac{BR}{31}$

+3

+41 $\frac{WE245CP}{12}$ +33 $\frac{TP}{40}$ +27 $\frac{PP}{13}$ +33 $\frac{BR}{4}$

54

Road
5-32

+99 $\frac{TP}{42}$ +94 $\frac{SLP}{53}$ +70 $\frac{18" Cott}{42}$ +66 $\frac{24" O}{50}$ +85 $\frac{12" O}{52}$ +58 $\frac{16" Cott}{40}$ +55 $\frac{SLP}{50}$ +32 $\frac{30" O}{52}$ +24 $\frac{12 Cott}{19}$ +14 $\frac{TP}{44}$ +03 $\frac{Stub Pole}{9}$

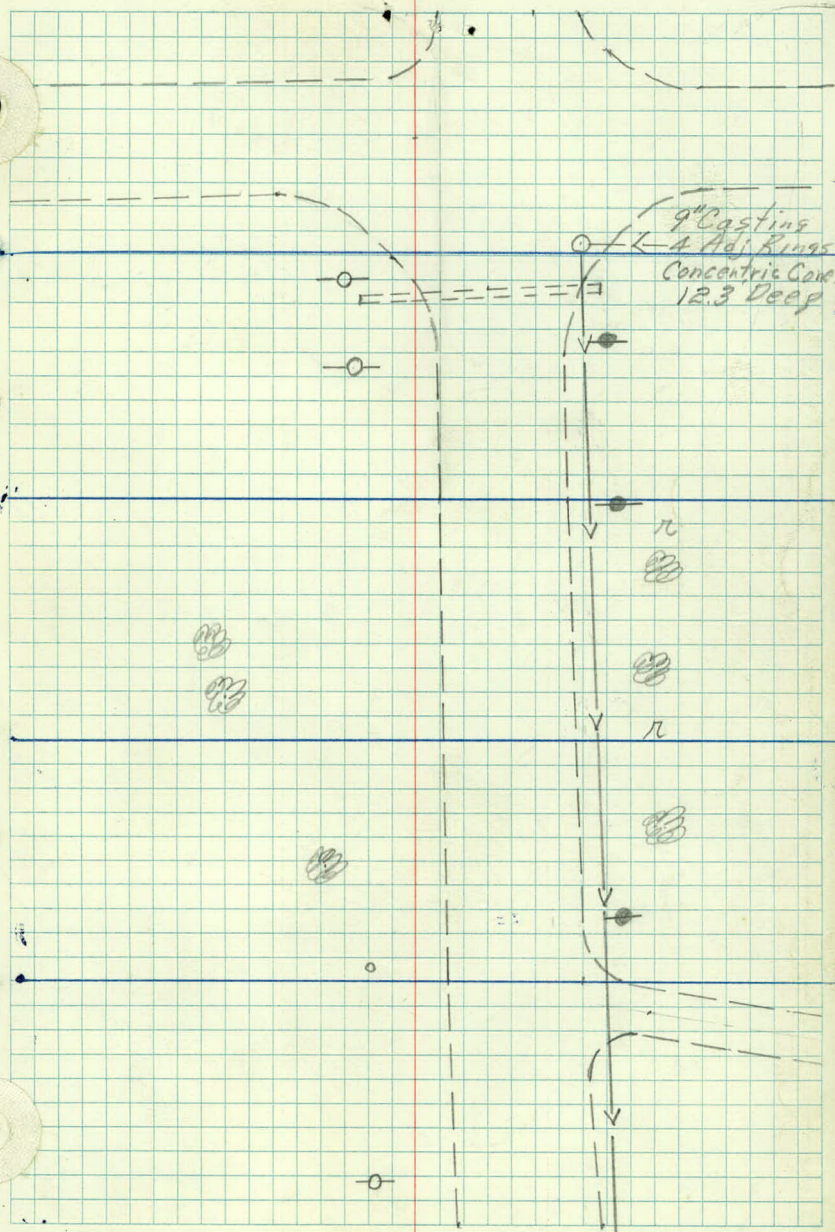
53

Road
7-35

+01 $\frac{R tie}{Ent}$ +94 $\frac{12' Ent}{49}$ Bit.+59 $\frac{PP}{8}$

August 5, 1968

31



12
27980

STA

30

↑ 3.10

29

↑ 2.20

28

1.34

27

.44

KP
DS
LAD
GA
ML

27 FEB 1969
Partly Cloudy
30°

White Bear Ave

additional

Topography

+48 18" MAPLE ✓

+50

+48 8" Pine ⁷⁶

RD

+36 8" ELM ✓

58

+36 24" LOCUST ✓

2-22

28

+27 24" ELM ✓

+26 8" Birch ✓

97

+25 10" Pine ✓

56

41 +100 10' ENT

RD

+83 PP ✓

+90 PP ✓

96

+89 20" ELM ✓

2-22

11

36

+69 20" ELM ✓

24

+54 15" ELM ✓

24

+50

RD

0-21

+38 15" ELM ✓

+28 Trees ✓

23

+25 18" ELM ✓

+23 Trees ✓

53-102

22

54-100

+12 24" ELM ✓

22

51-100

40

RD

1-21

+50

RD

1-20

+39 4" Q

17

+35 PP

17

39

RD

1-20

LT

#

RT



44

RD
3-23

+ 80 PP
14

+50

+47 MH
34

43

RD
3-23

+79 Trees
49-90

+50

+61 Trees
46-90

RD
3-23

+31 PP
13

+49 Trees
47-64

+15 Lombardy poplar
101 02

+ Lilacs
34-100

42

RD
3-23

+8 15" Pine
48

+96 24" Elm
31

+76 24" Oak
30

+61 10" Pine
45

+55 12" Beech
30

41 + 50

LT

£

RT

Q

OMH

TREES

LILACS

*

*

+50

+6

RD
3-23

+50

+26 PP
16

+5

RD

+50

+4

LT

£

RT

0

49

+50

RD
10-32

+22 $\frac{PP}{6}$

48

+54 $\frac{10"ELM}{33}$

+50

RD
5-26

+38 $\frac{4"BE}{32}$

+15 $\frac{4"JWM}{10}$

47

RD
5-26

+75 $\frac{PP}{13}$

46+50

LT

~~E~~

RT



+50

51

+50

50

+50

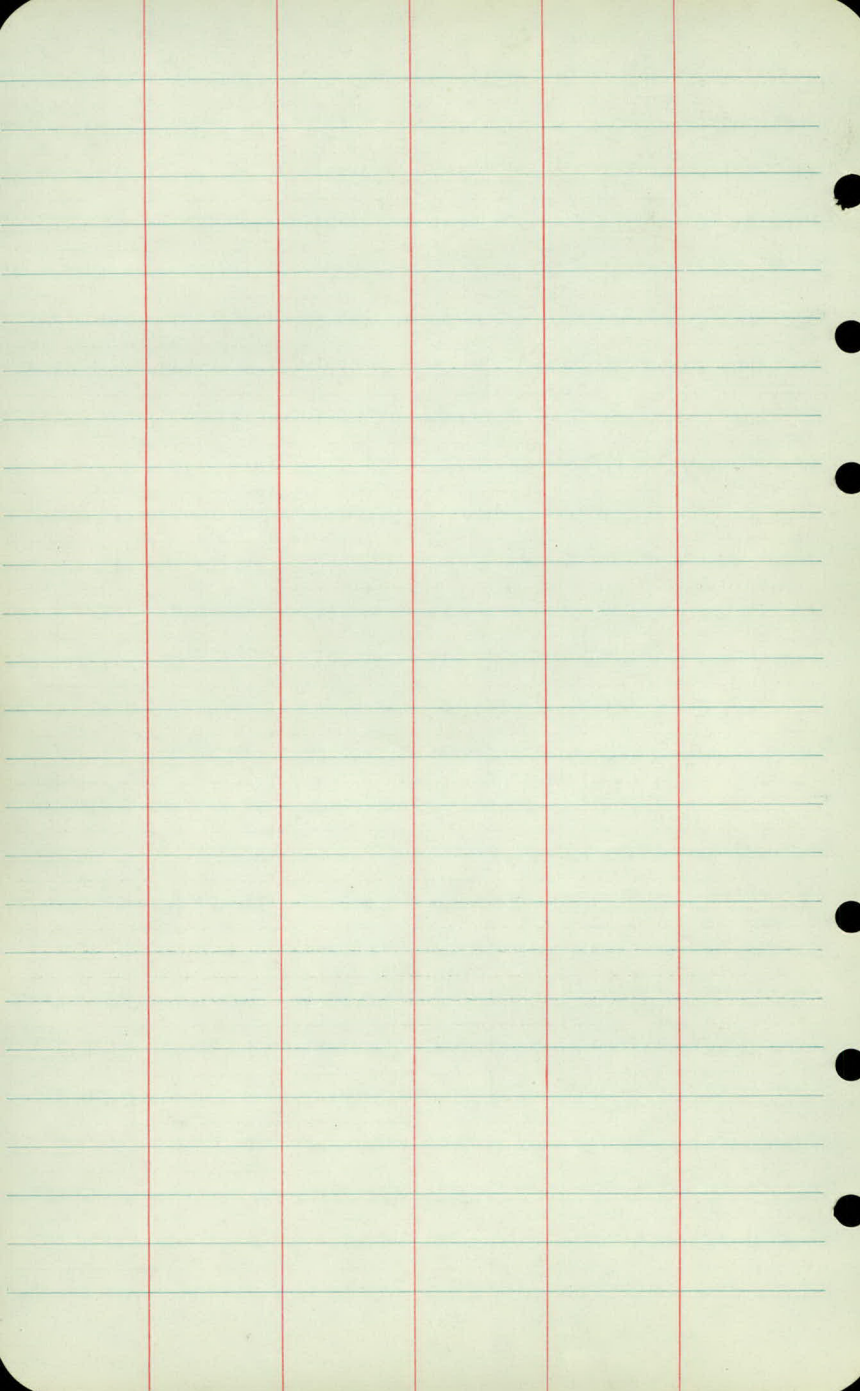
L14 GAS LINE

49

LT

~~£~~
—

RT



July 3, 1968

White Bear Ave.

X-Sections

Co Rd "C" to Co Rd "D"

Sta + π - Elev.

BM 2.99 933.58

930.59

BM 4.65 928.93

0+00 on $\pm$ "C"

✓

+22.5 End Conc.

+27 MH 28'RT 6.39 927.19

+28 W.G.V. 29'Lt

✓

+37

+62

July 3, 1968

Lt.

Rt

1

U.S.G.S. BM. Rt. 0+65

Top Hyd N.W. Corner Co Rd C + W.B. Ave.

26.6	26.8	26.9	27.0	27.4	27.1	27.0	27.7
7.0	6.8	6.67	6.56	6.23	6.51	6.56	5.9
60	47	24	19		20	24	44
			MH		MH		

26.1	25.7
7.5	7.9
89	120

29.9	29.5	29.3	28.6
3.7	4.0	4.3	5.0
121	100	79	60

26.6	26.9	27.0	27.3	27.6	27.2	27.5	28.4	28.9
7.0	6.7	6.60	6.31	6.02	6.39	6.1	5.2	4.7
48	31	24	14		24	36	56	65

26.4	26.2
7.2	7.4
57	65

27.9	27.2	27.4	27.4	27.3	27.6	27.4	27.6	27.8	28.7
5.7	6.4	6.2	6.2	6.3	6.0	6.2	6.0	5.8	4.9
65	49	42	26	23		16	31	44	65

27.5	27.5	27.7	27.9	27.7	27.1	28.9	31.4	31.8	32.2
6.1	6.1	5.9	5.7	5.9	5.5	4.7	2.2	1.8	1.3
65	41	18		17	25	29	40	43	65

Sta + π - Elev.

933.58

1

✓

+50

BM 3.03 933.99 2.62 930.96

+89 $\nless$ Walk Rt,

✓

2

EX
WM
DM
WF

Lt.

July 3, 1968
July 9, 1968 Rt

27.6 27.7 27.6 27.8 27.8 27.8 28.2 28.1 28.0 27.9 28.2 31.9
60 59 60 5.8 5.8 5.8 5.4 5.5 5.6 5.7 5.4 1.7
65 54 39 29 16 12 10 16 22 26 40

33.0 32.4
0.6 1.2
65 49

27.1 27.5 27.7 27.9 28.2 28.0 27.7 27.3 32.1 31.3
6.5 6.1 5.9 5.7 5.4 5.6 5.9 6.3 1.5 0.3
65 46 26 12 15 23 25 43 65
Top Hyd Lt Sta 1+90

27.2 27.5 27.9 28.0 27.8 28.1 28.0 28.2 28.3 30.9
6.8 6.5 6.1 6.0 6.2 5.9 6.0 5.8 5.7 3.07
65 46 42 26 10 12 27 Conc 33
27 Conc
Steps

33.0 32.3
0.97 1.72
65 52

27.6 27.9 28.1 27.8 27.7 28.0 27.9 27.8 27.7 28.9 31.3
6.4 6.1 5.9 6.2 6.3 6.0 6.1 6.2 6.3 5.1 2.7
47 44 30 28 11 12 19 21 30 38

27.1
6.9
65

32.9 32.3
1.1 1.7
65 51

Sta + π - Elev,

933.99

2+28

ENT Lt.

✓

+54

✓

3

+37

T.P.

5.49

932.49

6.99

927.00

MH

Lt.

July 8, 1968

d

27.0	27.4	27.7	27.7	27.9	27.8	27.5	26.4	27.3
7.0	6.6	6.3	6.3	6.1	6.2	6.5	7.6	5.7
65	53	34	11		12	20	25	33

32.4	31.8	30.5
1.6	2.2	3.5
65	55	39

27.1	27.1	27.6	27.6	27.6	27.8	27.8	27.4	26.1	25.2
6.88	6.9	6.4	6.4	6.4	6.2	6.2	6.6	7.9	8.8
building 65	40	24	10		11	18	24	34	

26.8	26.6
7.2	7.4
65	51

27.7	27.7	27.2	27.2	27.4	27.8	27.4	27.6	25.7	25.7	25.4
6.3	6.3	6.8	6.7	6.6	6.2	6.4	6.4	8.3	8.3	8.6
65	49	43	29	10		11	20	23	46	65
Parking										

27.2	26.9	27.2	27.0	27.3	27.6	27.4	27.4	25.2	24.9
6.8	7.1	6.8	(7.00)	6.7	6.4	6.6	6.6	8.8	9.1
31	27	25	(20 MH)	10		10	20	23	34

27.1	26.8
6.9	7.2
59	65

24.7	24.9
9.3	9.1
65	44

Sta + π - Elev,

932.49

3 + 87 Entrance Lt

3 + 72

✓

4

✓

+ 35

✓

TP

6.75

935.05

4.19

928.30

NE Cor Walk

July 9, 1968

Lt

E

Rt e

27.5	27.5	27.3	27.4	27.3	27.2	24.7	24.2	24.2
5.0	5.0	5.2	5.1	5.2	5.3	7.8	8.3	8.3
51	25	10		11	19	36	46	65

27.3	27.3	27.4	27.4	27.3	27.5	27.3	27.2	24.8	24.2
5.2	5.2	5.1	5.1	5.2	5.0	5.2	5.3	7.7	8.3
65	52	34	23	10		11	20	27	34

24.3	24.3
8.2	8.2
65	46

27.3	27.6	27.9	27.5	27.2	27.4	27.3	27.1	25.0	24.5
4.7	4.9	4.6	5.0	5.3	5.1	5.2	5.4	7.5	8.0
65	48	35	21	10		10	18	23	28

23.9	24.0	24.4
8.6	8.5	8.1
65	59	43

27.4	28.0	27.5	27.2	27.4	27.3	27.1	26.5	24.0	21.5
4.1	4.5	5.0	5.3	5.1	5.2	5.4	6.0	8.5	11.0
55	36	23	10		10	17	20	23	44

28.0	28.0
4.5	4.5
61	65

22.0
10.5
65

Sta + π - Elev.
935.05

+66 Entrance Lt.

✓

+84 Walk Lt

✓

5

+14 Entrance Rt.

FK
WM
DM
F

July 18, 1968

11

2

RT

f

28.0	27.8	27.4	27.2	27.2	27.2	27.0	26.2	23.0
7.1	7.3	7.7	7.9	7.7	7.9	8.1	8.9	12.1
65	50	27	10		10	16	20	27

22.2	22.1	21.9
12.9	13.0	13.2
65	55	40

28.9	28.4	28.3	27.8	27.3	27.4	27.2	27.0	26.2	23.5
6.20	6.45	6.82	7.3	7.8	7.7	7.9	8.1	8.9	11.6
65	51	29	29	10		10	17	20	28

Conc

22.2	21.4
12.9	12.7
65	43

30.8	30.3	28.5	27.0	27.3	27.4	27.3	27.1	25.5	23.1	22.4
4.3	4.8	6.6	8.1	7.8	7.7	7.8	8.0	9.6	12.0	12.7
55	59	47	34	20	10	10	17	31	56	65

32.5	32.2	30.5	27.0	27.3	27.4	27.3	27.1	25.5	22.8	22.3
2.6	2.9	4.6	8.1	7.8	7.7	7.8	8.0	9.6	12.3	12.8
65	61	43	22	10		11	17	35	56	65

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		935.05		
--	--	--------	--	--

5+65				
------	--	--	--	--

✓				
---	--	--	--	--

+77				
-----	--	--	--	--

✓				
---	--	--	--	--

6				
---	--	--	--	--

✓				
---	--	--	--	--

July 19, 1968

Lt

£

RT

9

26.9	26.7	27.0	27.1	27.3	27.5	27.3	27.2	26.4	26.3	25.5
8.2	8.4	8.1	8.0	7.8	7.6	7.8	7.9	8.5	9.6	9.6
25	21	18	16	10		11	16	19	30	48

30.2	32.5	33.8		25.1
4.9	2.6	1.3		10.0
39	54	65		65
				House

30.3	27.3	26.7	27.1	27.3	27.5	27.3	27.2	26.7	26.3	27.7
4.8	7.8	8.4	8.0	7.8	7.6	7.8	7.9	8.4	8.8	7.4
42	30	21	18	10		11	17	19	23	28

32.2	33.7		23.8	24.7	26.3	27.3	28.2
2.9	1.4		11.3	10.4	8.8	7.8	6.9
54	65		65	60	49	41	33

30.0	27.1	26.6	27.1	27.4	27.5	27.3	27.2	25.6	26.2	24.9
5.1	8.0	8.5	8.0	7.7	7.6	7.8	7.9	9.5	8.9	10.2
44	31	24	16	10		11	16	24	31	46

31.8	32.8		22.6	23.7
3.3	2.3		12.5	11.4
55	65		65	60

Sta + π - Elev.
935.05

6+30

✓

+60

✓

TP 2.78 930.40 7.43 927.62

+80 Gutter Lt.

✓

July 19, 1968

Lt.

E

Rt

L

29.5	27.2	26.6	26.9	27.3	27.5	27.3	27.2	26.9	25.2	24.4
5.6	7.9	8.5	8.2	7.8	7.6	7.8	7.9	8.2	9.9	10.5
51	31	20	17	10		11	18	19	21	24

30.3
4.8
6.5

22.5 23.0 23.7 24.5 24.7
12.6 12.1 11.4 10.3 10.4
65 49 35 32 26

26.5	26.4	26.4	26.8	27.3	27.5	27.4	27.2	24.9	24.4	24.7
8.6	8.7	8.7	8.3	7.8	7.6	7.7	7.9	10.2	10.7	10.4
52	37	27	17	10		10	17	21	24	26

26.3
8.8
6.5

22.0 22.3 22.9 24.2
13.1 12.8 12.2 10.9
65 57 47 34

Nails in W. Side P.P. S.W. Corner Kohlman

25.1	25.1	26.0	26.7	27.3	27.5	27.4	27.2	25.7	25.2	24.9
5.3	5.0	4.4	3.7	3.1	2.9	3.0	3.2	4.7	5.2	5.5
65	57	37	24	10		10	17	20	22	31

22.0 22.8 23.4
8.4 7.6 6.9
65 53 44

Sta + π - Elev

930.40

7+00 $\pm$ Kohlman Lt.

✓

+16

✓

+41

✓

Lt

July 19, 1968

RT i

25.2	26.2	27.2	27.4	27.5	27.4	27.4	25.2	25.0
5.2	4.2	3.2	3.0	2.9	3.0	3.0	5.2	5.4
65	39	19	12		10	18	23	30

MH

22.4	23.1	23.8	24.9
SS 8.0	7.3	6.6	5.5
58	51	46	36

26.5	26.6	26.5	27.4	27.5	27.5	27.5	25.0	25.0	24.7
3.9	3.8	3.9	3.0	2.9	2.9	2.9	5.4	5.4	5.7
40	32	29	10		10	17	23	29	36

26.0	25.7
4.4	4.7
57	65

22.4	23.2	23.7
SS 7.8	7.2	6.7
60	49	46

26.5	27.0	26.9	27.4	27.6	27.5	27.3	25.4	25.1	25.2
3.9	3.4	3.5	3.0	2.8	2.9	3.1	4.8	5.3	5.2
29	20	19	10		10	17	20	23	30

26.7	26.0	24.7	23.9
3.7	4.4	5.7	6.5
34	39	51	65

24.1	24.2	24.8
6.3	6.2	5.6
65	50	37

Sta π - Elev.

930.40

 $7 + 57$

✓

+ 86

Ent. Rt.

✓

8+00

✓

11

July 19, 1969

RT

j

23.4 22.3 23.9 27.2 27.4 27.4 27.5 27.4 25.6 25.3 25.1
 7.0 7.1 6.5 3.2 3.0 2.8 2.9 3.0 4.8 5.1 5.1
 34 26 23 16 10 10 16 21 23 27

23.4 23.1
 6.8 7.3
 46 65

24.5 24.6 25.5
 5.9 5.8 4.9
 65 49 34

22.3 23.0 27.4 27.5 27.6 27.5 27.1 26.0 25.2
 8.1 7.4 3.0 2.9 2.8 2.9 3.3 4.4 5.2
 27 23 13 9 13 21 42 65

22.1 22.4 19.8
 8.3 8.0 10.6
 43 55 65

21.9 22.0 27.4 27.5 27.6 27.5 27.3 24.4 24.4 25.3 25.1
 8.5 8.4 3.0 2.9 2.8 2.9 3.1 6.0 6.0 5.1 4.8
 29 25 13 9 10 17 26 33 40 65

21.0 20.9 19.6
 9.4 9.5 10.8
 45 55 65

Sta

+

π

-

Elev

930.40

8+20

✓

+24

✓

+30

✓

July 19, 1968

Lt.

E

Rt.

k.

21.4	22.7	27.3	27.5	27.7	27.5	27.2	23.3	24.7	25.1
9.0	7.7	3.1	2.9	2.7	2.9	3.2	7.1	5.7	5.3
37	26	17	10		10	17	27	36	44

21.3	20.4	20.6
9.1	9.8	9.8
49	59	65

25.0
5.4
65

18.6	20.4	27.4	27.5	27.4	27.4	27.0	23.4	22.7	23.3
11.8	9.96	3.0	2.9	2.8	3.0	3.4	6.7	7.7	7.1
29	29	17	10		10	18	24	30	39

Top RC Pipe

18.6	18.1
11.8	12.3
47	61

24.9	24.5
5.5	5.9
65	50

26.8	27.5	27.5	27.6	27.4	27.1	22.7	21.0	21.3
3.6	2.9	2.9	2.8	3.0	3.3	7.7	9.4	9.1
20	17	10		10	17	23	28	32

21.8	21.6	21.0
8.6	8.8	9.4
33	52	65

24.7	24.4	22.2
5.7	5.8	8.2
65	56	38

Sta

+

π

-

Elev

930.40

8+36

✓

+63

✓

+74

✓

July 19, 1968

L+

E

R+ l.

23.0	26.8	27.5	27.5 ✓	27.6	27.4	27.2	20.8	18.4
7.4	3.6	2.9	2.9	2.8	3.0	3.2	9.60	12.0
27	19	17	10		10	17	28	28

TopRSC,pc

22.1	21.8	21.7
8.3	8.6	8.7
33	47	65

24.8	23.7	21.4	20.6
5.6	6.7	9.0	9.8
65	55	35	32

24.2	27.0	27.6	27.8	27.9 ✓	27.7	27.2	21.3	20.4
6.2	3.4	2.8	2.6	2.5	2.7	3.2	9.1	10.0
29	23	18	10		10	18	27	30

23.0	22.4
7.4	7.8
47	62

20.8	18.2	20.0	17.9	20.7
9.6	12.2	10.4	12.5	9.7
65	44	45	37	34

25.2	26.5	27.7	27.9 ✓	28.0	27.8	27.3	22.4	20.4	20.0
5.2	3.9	2.7	2.5	2.4	2.6	3.1	8.0	9.8	10.4
42	28	18	10		10	18	25	31	45

23.4	23.5
6.8	6.9
55	65

20.4	20.9	18.1
10.0	9.5	12.3
66	57	50

Sta + π - Elev

930.40

TP 5.03 932.30 3.13 927.27

8+90

✓

9+00

✓

+ 11

S.W. - Lt

Lt

L

July 19, 1968

Rt m.

North side of S.W. Ho. # 2721 Lt 35 1/2

27.5	27.3	28.0	28.1	28.2	28.0	27.7	27.0	27.8	20.6
4.8	5.0	4.3	4.2	4.1	4.3	4.6	5.3	10.5	11.7
26	24	16	10		10	16	19	29	43

27.4	27.3	26.9	26.8	26.7	18.1	18.1	19.5	20.6
4.7	5.0	5.4	5.47	5.6	14.2	14.2	12.8	11.7
34	44	50	60	65	65	61	59	57

Conc
S.W.

27.0	27.5	27.5	28.1	28.2	28.3	28.0	27.8	27.4	22.4	21.2
5.3	4.8	4.8	4.2	4.1	4.0	4.3	4.5	4.9	9.5	11.1
60	41	25	18	10		11	16	18	26	38

26.9	27.0
5.40	5.3
60	65
Conc	140
S.W.	

20.2	20.5
12.1	11.8
65	55

27.0	27.3	27.2
5.31	5.03	5.08
63	41	30
Conc	Conc	Conc

Sta + π - Elev

932.30

9+25

✓

T.P. 4.5993370 3.19 929.11

+50

✓

10+00

✓

7.49 937.15 4.04 929.66

July 19, 1968
Rt n.

Lt. ~~E~~

27.5	28.2	28.4	28.5	28.3	27.9	28.0	22.7
4.8	4.1	3.9	3.8	4.0	4.4	8.3	9.6
31	16	10		11	18	25	32

26.5	26.4	25.9	20.7	20.7	21.7
5.8	5.9	6.4	11.6	11.6	10.6
44	59	65	66	60	46

P.K Nail in PP Sta 9+35 Lt 28'

27.3	27.4	27.9	28.4	28.4	28.8	28.6	28.4	26.3	23.9	22.7
6.4	6.09	5.8	5.1	5.1	4.9	5.1	5.3	7.4	9.8	10.9
65	60	36	17	9		10	17	27	40	54

SW

21.8
11.9
65

27.5	27.5	27.9	29.0	29.1	29.3	29.1	28.9	26.6	26.8	25.9
6.2	6.2	5.8	4.7	4.6	4.4	4.6	4.8	6.9	6.9	7.8
65	43	21	16	10		11	17	23	31	32

22.8
9.9
65
25.4
8.3
46

SPAKE INAPPLY STA 10+92

STA

+

π

-

ELEV

937.15

10428

9.90

27.25

+50

✓

11400

✓

LT

E

22 July 1968

RT

0

TOP MH19.0 LT

$\begin{matrix} 23.9 & 25.2 & 27.0 & 29.2 & 29.5 & 29.8 & 29.9 & 28.8 & 27.1 & 25.4 \\ 13.3 & 12.0 & 10.2 & 8.0 & 7.7 & 7.4 & 7.8 & 8.4 & 10.1 & 11.6 \\ 65 & 40 & 26 & 19 & 15 & & 15 & 20 & 24 & 47 \end{matrix}$

$\begin{matrix} 25.2 & 25.1 \\ 12.0 & 12.1 \\ 65 & 60 \end{matrix}$

$\begin{matrix} 27.3 & 28.4 & 29.7 & 30.0 & 30.2 & 30.0 & 29.4 & 27.9 & 24.1 \\ 9.9 & 8.8 & 7.5 & 7.2 & 7.0 & 7.2 & 7.8 & 9.3 & 9.1 \\ 33 & 24 & 20 & 15 & & 15 & 20 & 23 & 29 \end{matrix}$

$\begin{matrix} 21.3 & 25.8 \\ 10.9 & 11.4 \\ 48 & 65 \end{matrix}$

$\begin{matrix} 25.5 & 25.4 & 24.3 \\ 11.7 & 11.6 & 10.9 \\ 65 & 53 & 36 \end{matrix}$

STA

+

π

-

ELEV

937.15

11+50

✓

+65

± EXT RT

✓

12+00

✓

22 July 1968

LT

E

RT

P

29.0	28.5	28.8	30.2	30.4	30.8	30.6	30.1	30.2	29.9	28.7
9.3	8.7	8.4	7.0	6.8	6.4	6.6	7.1	7.0	7.3	8.5
51	38	25	19	15		15	20	22	28	38

27.1
10.1
65

27.5 29.0
9.7 9.2
65 56

28.9	28.5	29.4	30.5	30.6	31.0	30.8	30.2	30.3	29.8
8.3	8.7	7.8	6.7	6.6	6.2	6.4	7.0	6.9	7.4
33	32	21	17	15		15	21	24	32

28.3 27.8
8.9 9.4
46 65

28.3 28.6 29.5
8.9 8.6 7.7
65 58 43

29.8	29.5	31.0	31.2	31.4	31.3	31.3	31.6	31.4
7.4	7.7	6.2	6.0	5.8	5.9	5.9	5.6	5.8
29	26	17	14		15	22	49	65

29.9 28.8 28.0
7.3 8.4 9.2
38 50 65

STA	+	π	-	ELEV
-----	---	-------	---	------

		937.15		
--	--	--------	--	--

12+25				
-------	--	--	--	--

		7.34		
--	--	------	--	--

			29.9	
--	--	--	------	--

+34	$\neq$	ENT	LT	
-----	--------	-----	----	--

✓				
---	--	--	--	--

+40				
-----	--	--	--	--

		4.64		
--	--	------	--	--

			32.5	
--	--	--	------	--

+45				
-----	--	--	--	--

		7.08		
--	--	------	--	--

			30.1	
--	--	--	------	--

+50				
-----	--	--	--	--

22 JULY 1968

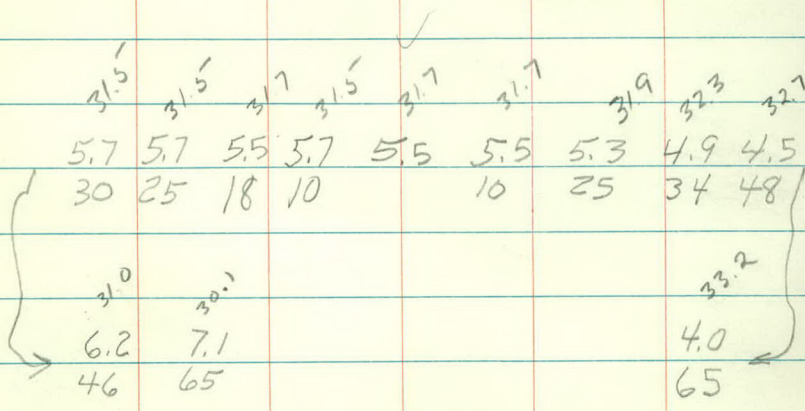
LT

£

RT

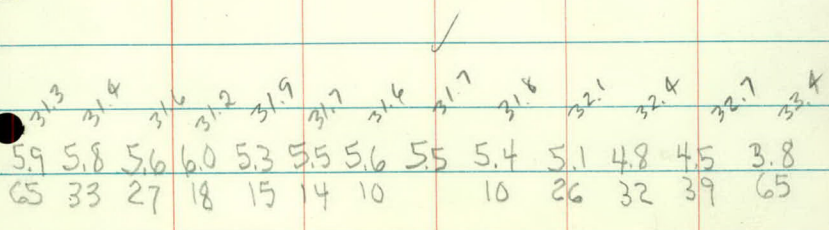
g

FL S End 12" x 20' CM 20' LT



TOP SIDEWALK 33'0 RT

FL N. END 12" x 20' CM 20' LT



STA	+	λ	-	ELEV.
-----	---	-----------	---	-------

		937.15		
--	--	--------	--	--

2+72				
------	--	--	--	--

			4.52	32.6
--	--	--	------	------

3+00				
------	--	--	--	--

+27	±	ENT	RT	
-----	---	-----	----	--

+37				
-----	--	--	--	--

			5.75	31.4
--	--	--	------	------

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

LT

E

22 JULY 1968

RT

n

TOP SIDEWALK 33'0 RT

32.0 31.8 31.7 31.9 31.9 32.3 32.4 32.7 33.0 33.4 33.0

5.2 5.4 5.5 5.3 5.3 4.9 4.6 4.5 4.2 3.8 3.8

65 33 24 18 10 10 30 43 56 65

31.5 31.4 31.9 31.8 32.0 32.4 32.9 32.7 32.2 32.0

5.7 5.8 5.4 5.4 5.2 4.6 4.3 4.5 5.0 7.2

65 41 32 19 10 10 27 43 65

TOP MH 20' LT

30.3 31.4 31.2 31.9 32.3 32.8 33.2 33.1 32.2 30.4

6.8 5.6 6.0 5.3 4.9 4.4 4.0 4.1 5.0 6.8

46 34 29 18 10 10 23 37 65

FE FE

2.9

8.3

65

STA + π - ELEV

937.15

14400

✓

TD 7.79 941.03 3.91 933.24

+54 £ ENT. RT

✓

15400

22 JULY 1968

LT

£

RT

✓

30.0 31.0 31.4 32.1 32.8 33.3 33.7 33.6 33.6 33.3 33.0
 7.2 6.2 5.6 5.1 4.4 3.9 3.5 3.6 3.6 3.9 3.1
 40 37 27 19 10 10 24 37 47 65
 EE

29.6 28.4
 7.6 8.6
 50 65

£ STA 14+00

✓

29.8 30.4 30.9 32.9 33.3 33.6 33.9 33.9 34.1 34.2
 12.2 10.6 10.1 8.1 7.7 7.4 7.1 7.1 6.9 6.8
 52 35 27 18 10 10 26 37 65
 FE

27.1
 13.9
 6.5

✓

27.7 28.4 31.6 32.7 33.9 34.0 33.7 32.5 34.6 35.4
 13.3 12.2 9.4 7.3 7.1 7.0 7.3 8.5 6.5 5.4
 65 50 27 10 10 18 20-22 27 33

DITCH

37.1
 65

STA	+	π	-	ELEV
-----	---	-------	---	------

		941.03		
--	--	--------	--	--

15+07		$\neq$ EOT LT		
-------	--	---------------	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

15+84				
-------	--	--	--	--

		8.68	32.35	
--	--	------	-------	--

16+00				
-------	--	--	--	--

LT

E

23 JULY 1968

RT

x

27.7	30.0	32.4	33.8	34.0	34.0	33.8	32.6	34.6
13.3	11.0	8.6	7.2	7.0	7.0	7.2	8.4	6.4
65	38	20	10		10	18	20-22	27

DITCH

32.5	36.8	35.8
3.5	4.2	5.2
65	49	34

FC

29.4	30.0	32.0	33.8	34.0	34.2	34.2	33.7	32.6	35.1
12.6	11.0	9.0	7.2	7.0	6.8	6.8	7.3	8.2	5.9
65	42	23	16	10		10	18	20-22	27

DITCH

32.9	37.3	36.3
3.1	3.7	4.7
65	47	32

TOP SIDEWALK 27.0 LT

30.9	31.4	33.4	32.9	34.1	34.4	34.4	34.3	33.9	33.4	35.0	35.1	36.3
10.14	9.4	7.6	8.1	6.9	6.6	6.6	6.7	7.1	7.4	6.0	5.3	4.7
63	46	28	17-19	16	10		10	19	22	29	34	48

SW

DITCH

32.2

3.8

65

STA	+ . π -	ELEV.
	941.03	

16+47	$\frac{E}{L}$ ENT LT	
-------	----------------------	--

+56	8.01	33.02
-----	------	-------

TP	5.05	939.98	6.10	934.93
----	------	--------	------	--------

+96		
-----	--	--

17+00		
-------	--	--

✓

23 July 1968

LT

E

RT

W

2 ^{2.6}	3 ^{1.7}	3 ^{3.4}	3 ^{4.4}	3 ^{4.7}	3 ^{4.5}	3 ^{4.0}	3 ^{3.7}	3 ^{4.6}	3 ^{4.1}
12.4	9.3	7.4	6.4	6.3	6.5	7.0	7.3	6.4	6.9
65	38	19	10		10	20	23	31	58

TOP MH 19' LT

E STA 17+00

2 ^{2.4}	2 ^{2.1}	3 ^{0.4}	3 ^{2.4}	3 ^{4.4}	3 ^{4.8}	3 ^{4.9}	3 ^{4.8}	3 ^{4.2}	3 ^{0.8}	3 ^{1.7}	3 ^{2.1}
12.6	10.9	9.6	7.6	5.6	5.2	5.1	5.2	5.8	9.21	8.3	7.9
65	46	39	26	18	10		10	22	35	45	65

FE

FLS. END

15" X 20 CM

2 ^{2.0}	3 ^{0.3}	3 ^{1.8}	3 ^{2.5}	3 ^{4.5}	3 ^{4.8}	3 ^{4.9}	3 ^{4.8}	3 ^{4.4}	3 ^{4.7}	3 ^{5.0}
11.0	9.7	8.2	7.5	5.5	5.2	5.1	5.2	5.6	5.3	5.0
45	38	31	24	17	10		10	23	47	65

FE

27.7
12.3
65

STA

+

π

-

ELEV

939.98

17+21

+26

✓

+57

✓

+65

LT

E

23 JULY 1968

RT

N

^{25.6} ^{29.0} ^{31.4} ^{34.4} ^{34.9} ^{35.0} ^{34.9} ^{34.8} ^{34.9} ^{35.1} ^{35.1}
 14.4 11.0 8.6 5.4 5.1 5.0 5.1 5.2 5.1 4.9 4.9
 65 38 23 16 10 10 19 37 53 65
 FE

^{25.4} ^{29.0} ^{31.4} ^{34.4} ^{34.9} ^{35.0} ^{34.9} ^{34.4} ^{34.2} ^{30.2}
 14.4 11.0 8.6 5.4 5.1 5.0 5.1 5.4 10.8 9.8
 65 38 23 16 10 10 18 31 34
 FC

FLN END

15"CM

^{25.4} ^{34.7} ^{30.6}
 4.2 5.3 9.2
 65 48 40

^{23.7} ^{28.8} ^{34.2} ^{35.1} ^{35.2} ^{35.0} ^{34.4} ^{35.0} ^{29.9} ^{30.3}
 16.3 11.2 5.8 4.9 4.8 5.0 5.4 9.0 11.1 9.7
 65 26 16 10 10 18 25 31 40
 *

^{35.5} ^{34.9}
 4.5 5.1
 65 52

^{23.7} ^{28.8} ^{34.2} ^{35.1} ^{35.2} ^{35.0} ^{35.0} ^{34.9} ^{25.3}
 16.3 11.2 5.8 4.9 4.8 5.0 5.0 5.1 4.7
 65 26 16 10 10 28 45 65

STA

+

π

-

ELEV

939.98

17+82

+86

13.78 26.20

+91

✓

18+00

✓

LT

E

23 JUL 1968

RT

W

^{25.5} 14.5 65
 ^{26.3} 13.7 41
 ^{28.2} 11.8 27
 ^{34.4} 5.6 17
 ^{35.1} 4.9 10
 ^{35.3} 4.7 10
 ^{35.1} 4.9 10
 ^{35.1} 4.9 20
 ^{34.9} 5.2 33
 ^{35.0} 5.0 52
 ^{35.1} 4.9 65

FL 24" SCP 27.0 LT

^{26.1} 13.9 65
 ^{26.5} 13.5 50
 ^{28.3} 11.7 28
 ^{34.5} 5.5 16
 ^{35.1} 4.9 10
 ^{35.3} 4.7 10
 ^{35.1} 4.9 10
 ^{34.9} 5.1 18
 ^{30.0} 9.4 26
 ^{27.0} 13.0 33

^{34.9} 5.1 65
 ^{34.5} 5.5 54
 ^{30.9} 9.1 42

^{26.1} 13.9 65
 ^{26.5} 13.5 50
 ^{28.3} 11.7 28
 ^{34.5} 5.5 16
 ^{35.1} 4.9 10
 ^{35.3} 4.6 10
 ^{35.1} 4.9 10
 ^{34.8} 5.2 18
 ^{28.8} 11.2 27
 ^{28.9} 11.1 40

^{33.9} 6.1 65
 ^{32.4} 7.6 54

STA + π - ELEV

939.98

18+50

0
5
12 6
13

✓

+ 78

✓

TP 7.72 944.16 3.54 936.44

19+00

LT

E

23 JULY 1968
RT

3.7 ^x	3.2 ^x	3.5 ⁷	3.5 ⁸	3.9 ⁹	3.5 ⁶	3.9 ⁹	2.9 ⁹	2.9 ⁹	2.9 ⁶
6.6	7.6	4.3	4.2	4.1	4.4	5.1	10.1	10.1	10.4
31	24-26	14	10		10	18	26	38	50
DITCH									

3.2 ⁷	3.2 ⁶
7.3	7.4
53	65

2.9 ^x
10.6
65

3.5 ⁷	3.5 ⁶	3.4 ¹	3.5 ⁸	3.6 ¹	3.2 ²	3.6 ⁰	3.5 ^x	3.2 ⁴	3.9 ⁹	3.8 ⁸
4.3	4.4	5.9	4.2	3.9	3.8	4.0	4.6	7.6	8.1	8.2
51	33	21-24	15	10		10	19	25	30	41
DITCH										

3.5 ⁸
4.2
65

3.0 ⁰	3.0 ^x
9.0	9.6
65	53

STA 19+00

3.6 ²	3.6 ⁶	3.5 ¹	3.6 ⁰	3.6 ^x	3.6 ^x	3.5 ⁹	3.4 ¹	3.4 ⁷	3.4 ⁷	3.4 ⁹
7.97	7.6	9.1	8.2	7.8	7.8	8.3	10.1	9.5	9.5	6.7
66	34	24	17	10		10	22	24-27	45	59
Conc	DITCH									

STA

+

π

-

ELEV

944/16

19450

+95

± RADATZ

20400

+50

✓

+82

8.79

23 JULY 1968

LT

£

RT

7

37.0	36.9	36.2	36.7	37.0	37.1	37.0	36.6	36.3	37.9	36.7	39.1
7.2	7.3	8.0	7.5	7.2	7.1	7.2	7.6	7.9	6.3	5.5	5.1
65	31	25	18	10		10	21	29	37	55	65

34.9	36.1	36.8	37.5	37.6	37.6	37.5	37.8	36.6	39.4	40.7
9.3	8.1	7.4	6.73	6.6	6.6	6.7	6.38	5.6	4.8	3.5
100	65	43	19	10		10	19	43	65	100
			MH				MH			

36.1	37.0	37.6	37.7	37.6	38.4	39.3
8.1	7.2	6.6	6.5	6.6	5.8	4.9
65	35	10		10	36	65

39.8	37.7	35.7	37.8	38.3	38.1	38.2	38.0	37.7	39.8	39.1
5.4	6.5	8.5	6.4	5.9	5.8	6.0	6.2	6.5	5.4	5.1
65	33	21	15	10		10	22	25	38	58

39.2
5.0
65

FL S. END G" VIT 21' LT

STA	+	π	-	ELEV
-----	---	-------	---	------

		944.16		
--	--	--------	--	--

+88				
-----	--	--	--	--

✓				
---	--	--	--	--

+94				
-----	--	--	--	--

			8.53	
--	--	--	------	--

21+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

23 July 1968

LT

#

RT

2

39.0	37.7	38.4	38.8	38.7	38.9	38.7	38.9	37.7	38.9	39.0
5.21	6.48	5.81	5.4	5.5	5.4	5.5	5.8	6.5	5.3	4.1
65	35	19	15	10		10	21	23-25	34	50
	SW	SW						DITCH		

39.5
47
65

FL N. END 6" VIT 21' LT

38.4	37.3	36.0	38.7	38.8	39.0	38.9	38.5	37.6	38.9
5.6	6.9	8.2	5.5	5.4	5.2	5.3	5.7	6.4	5.3
57	31	21-23	15	10		10	21	22-25	33
		DITCH						DITCH	

38.8
5.4
65

39.6
4.6
65

37.3	38.2	36.1	39.1	39.3	39.4	39.3	39.0	37.3	38.6	39.2	39.4
6.9	6.0	8.06	5.1	4.9	4.8	4.9	5.2	6.90	5.6	5.0	4.8
65	29	22	15	10		10	21	25	30	43	65

FLS. END
15" X 20" CM

FLS. END
15" X 20" CM

STA	+	T	-	ELEV.
-----	---	---	---	-------

		944.16		
--	--	--------	--	--

+60	± ENT LT			
-----	----------	--	--	--

+65	± ENT RT			
-----	----------	--	--	--

+70			8.19	36.0
-----	--	--	------	------

+73			6.30	37.9
-----	--	--	------	------

22+00				
-------	--	--	--	--

✓				
---	--	--	--	--

TP	4.60	944.61	4.15	940.01
----	------	--------	------	--------

LT

23 JULY 1968
RT X-27

38.4	38.9	39.4	39.5
5.8	5.3	4.8	4.7
65	22	10	

39.5	39.4	39.6	39.7	40.1
4.7	4.8	4.7	4.5	4.1
	10	30	44	65

FL N. END 15' X 20' CM 23' LT

FL N. END 15' CM 24' RT

39.0	39.0	39.5	39.4	39.3	39.6	39.7	39.6	39.0	38.3	39.3	39.6
6.2	6.2	6.7	7.8	4.9	4.6	4.5	4.6	5.2	5.9	4.9	4.6
65	51	29	23-25	15	10		10	21	26	45	65

DITCH

Φ STA 23+00

STA + T - ELEV

944.61

22+33

6.50

+38 E ENT RT

✓

+45

6.71 37.9

+62 E ENT LT

23+00

LT

E

24 JULY 1968

RT

X-28

FL S. End 8" C/P 26' RT

37.7	36.7	37.5	39.7	39.9	39.7	39.3	39.2	39.4
6.9	7.9	5.1	4.9	4.8	4.9	5.3	5.4	5.0
28	21-24	15	10		10	29	42	65
DITCH								

37.9
6.7
65

FL N. END 12" CM 26' RT

38.9	38.9	39.3	39.8	39.9	39.7	39.7	38.8	39.1	39.1
5.7	5.7	5.3	4.8	4.7	4.9	4.9	5.8	5.5	5.5
65	56	19	10		10	19	24	40	65

39.0	38.5	38.2	39.5	39.9	40.0	39.9	39.7	39.0	39.2	39.5	39.9
5.6	6.1	6.4	5.1	4.7	4.6	4.7	4.9	5.6	5.4	5.1	5.4
65	38	20	15	10		10	19	20-23	26	44	65
DITCH											

STA	+	Δ	-	ELEV
		944.61		

23+24			5.96	38.65
-------	--	--	------	-------

+50				
-----	--	--	--	--

24+00				
-------	--	--	--	--

+06			7.38	37.23
-----	--	--	------	-------

+15	£	ENT	LT	
-----	---	-----	----	--

+24			7.50	37.11
-----	--	--	------	-------

+40			7.15	37.46
-----	--	--	------	-------

LT

E

24 JULY 1968

RT

X-29

TOP MH 19.0 RT

38.9	38.7	37.8	39.6	39.9	40.0	39.9	39.5	39.0	39.5	39.4
5.8	5.9	6.8	5.0	4.7	4.6	4.7	5.1	5.6	5.1	5.2
65	32	22	15	10		10	18	23	31	65

38.9	38.9	38.3	37.6	39.5	39.8	39.9	39.7	39.1	38.3	38.8	39.1	39.4
5.7	5.7	6.3	7.0	5.1	4.8	4.7	4.9	5.5	6.3	5.8	5.5	5.4
65	52	31	23	16	10		10	19	24	36	57	65

FL S. END 15" X 18' CM 24' LT

39.2	39.4	39.7	39.8	39.7	39.0	38.3	38.8	39.1	39.2
5.4	5.2	4.9	4.8	4.9	5.6	6.3	5.8	5.5	5.4
65	24	10		10	19	24	35	52	65

FL N. END 15' X 18' CM 24' LT

FL S. END 12" X 46' VIT 24' RT

STA	+	π	-	ELEV
-----	---	-------	---	------

		944.61		
--	--	--------	--	--

+ 53				
------	--	--	--	--

		7.40	37.21	
--	--	------	-------	--

+ 62	$\neq$ ENT			
------	------------	--	--	--

+ 73				
------	--	--	--	--

		7.67	36.94	
--	--	------	-------	--

+ 76	$\neq$ ENT RT			
------	---------------	--	--	--

+ 86				
------	--	--	--	--

		7.67	36.94	
--	--	------	-------	--

25+00				
-------	--	--	--	--

TP				
----	--	--	--	--

	3.59			
--	------	--	--	--

		942.85		
--	--	--------	--	--

			5.35	
--	--	--	------	--

				939.26
--	--	--	--	--------

24 July 1968

LT

£

RT

X-30

FL S. END 15" X 20' CM 24' LT

39.0	39.0	39.1	39.5	39.5	39.4	39.0	38.8	39.2	39.4
5.6	5.6	5.5	5.1	5.1	5.2	5.6	5.8	5.4	5.2
65	50	16	10		10	22	33	51	65

FL N. END 15" X 20' CM 25' LT

38.4	38.0	37.7	37.0	37.3	37.3	38.9	38.7	39.3
6.2	6.6	7.4	5.6	5.3	5.2	5.3	5.7	5.9
65	31	24	16	10		10	26	51

FL N. END 12" CM 25' RT

39.3	38.2	37.6	36.9	36.8	36.2	39.1	38.5	37.6	38.1	38.7	39.1
6.3	6.4	7.0	7.7	5.8	5.4	5.3	5.5	6.1	7.0	6.5	5.9
65	54	33	25	16	10		10	20	21-24	30	42

DITCH

£ STA 25+00

STA + π - ELEV

942.85

25+50

26+00

BM 5.87 943.21 5.51 937.34 ~~938.35~~

+29 Ent Lt

✓

+51

+57 M.H. 21' Rt 6.30

FX
WF
PF

LT

24 JULY 1968
August 19, 1969
RT X-31

37.6	37.3	37.0	36.5	38.4	38.9	39.1	38.9	38.3	36.9	37.8	38.8	38.8
5.3	5.6	5.9	6.4	4.5	4.0	3.8	4.0	4.6	6.0	5.1	4.1	4.1
65	51	30	25	16	10		10	18	21-23	31	51	6

DITCH

37.4	37.1	36.7	35.9	35.6	35.7	35.8	37.7	38.3	36.3	35.9	35.2	34.5
5.5	5.8	6.2	7.0	4.3	4.2	4.1	4.2	4.6	6.6	7.0	7.7	8.4
65	42	30	24	15	10		10	18	24	38	55	65

SPIKE IN PP 30' LT 26+48

37.4	37.4	38.2	38.6	38.7	38.5	38.2	37.9	35.0
5.8	5.8	5.0	4.6	4.5	4.7	5.0	5.3	8.2
58	32	16	10		10	18	20	25

37.5
5.7
70

SS 33.4 39.7
9.8 8.5
53 39

38.3	36.9	38.7	38.6	38.6	38.9	38.0	35.95	33.6
8.4	6.32	4.8	4.6	4.60	4.8	5.2	276	9.6
23	22	15	10		10	18	27	27

Top 24 SCP

Top 24 SCP

37.0 38.0
6.2 52
43 60

SS 31.7 32.8
11.5 10.4
53 41

Sta + π - Elev

94321

26 + 71

✓

27

✓

+50

✓

LT

August 9, 1968

RT

X-32

36.0	37.3	38.8	38.6	38.7	38.4	37.9	37.6	31.5
72	5.4	4.8	4.6	4.5	4.8	5.3	9.7	11.7
21	18	15	10		10	18	27	36

35.4	38.6	37.2	38.6	29.2	29.3	30.3
78	4.6	6.0	4.6	14.0	13.9	12.9
25	38	53	80	65	62	46

35.7	35.7	38.5	38.7	38.8	38.5	38.0	32.6	30.5
7.5	7.5	4.7	4.5	4.4	4.7	5.2	10.6	12.7
23	20	15	10		10	17	30	40

38.3	40.4	39.1	37.9	29.9	29.8
4.9	2.8	4.1	5.3	13.8	13.4
27	34	51	65	67	53

37.0	36.9	38.9	39.0	39.1	38.8	38.4	36.8	32.0
6.2	6.3	4.3	4.2	4.1	4.4	4.8	6.4	11.2
25	21	16	10		10	17	20	30

39.5	39.4	35.8	33.9	29.9	29.9	31.4
3.7	3.8	7.4	9.8	13.8	13.8	11.8
30	38	54	67	65	50	35

Sta + * - Elev.

943.21

28+00

✓

+44

✓

✓

TP 3.98 945.74 1.45 941.76 Fe Post

+78

14

A4945 + 9, 1968
R1 X-33

37.4	31.2	39.2	39.4	39.5	39.3	39.1	34.1	32.8
5.8	6.0	4.0	3.8	3.7	3.9	4.1	9.1	10.4
24	22	15	10		10	20	37	43

39.3	39.2	35.3	32.7
3.9	4.0	7.9	10.5
29	32	50	65

31.4
11.8
63

37.6	37.8	39.5	39.7	39.8	39.1	39.3	38.0	38.0
5.6	5.4	3.7	3.5	3.4	3.5	3.9	5.2	5.2
24	21	16	10		10	20	25	27

38.6	38.7	36.3	33.2
4.6	4.5	6.9	10.0
26	27	35	51

38.1	40.0	40.0	38.6
4.5	3.2	3.2	4.6
42	35	32	29

31.6
11.6
65

38.0	37.3	35.5
5.2	5.9	7.7
43	50	65

32.2	33.9	39.5	39.9	40.1	40.0	39.5	27.3	43.9
13.5	11.8	6.1	5.8	5.6	5.7	6.2	7.4	1.8
42	34	17	10		10	20	27	38

30.2
15.5
65

38.8	41.0	42.2	42.7	43.7
6.9	4.7	3.5	3.0	2.0
65	53	45	44	41

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		945.74		
--	--	--------	--	--

29+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+45				
-----	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

+73				
-----	--	--	--	--

TP				
----	--	--	--	--

7.60				
------	--	--	--	--

948.57				
--------	--	--	--	--

4.77				
------	--	--	--	--

940.97				
--------	--	--	--	--

Sta 30				
±				

Lt.

August 19, 1968
Rt. X-34

33.0	34.9	39.8	40.1	40.2	40.1	40.0	39.0	38.6
12.7	10.8	5.9	5.6	5.5	5.6	5.7	6.7	7.1
34	27	17	10		10	17	22	26

32.4	30.6	30.4	39.6	40.6	42.9	43.9	44.3
13.3	15.1	15.3	6.1	5.1	2.8	1.8	1.4
39	53	65	65	59	44	40	37

32.4	34.0	39.8	40.3	40.6	40.6	40.4	40.0	39.1
13.3	11.7	5.9	5.4	5.1	5.1	5.3	5.7	6.6
39	28	16	10		10	17	20	22

31.0
14.7
65

44.7	44.7	40.3	39.1
1.0	1.0	5.4	6.6
43	40	33	27

43.9	42.7
1.8	3.0
53	70

32.9	34.2	40.0	40.3	40.8
12.8	11.5	5.7	5.4	4.9
40	28	16	10	

32.5

13.2
65

Sta + π - Elev

948.57

30

✓

+50

✓

TP ~~5.53~~ 945.90 8.20 940.37 1 iron

5.53 947.38

941.85

Wood stake

31

✓

FK
LPD
PF

Lt.

Sept. 19, 1968
RT

X-35

^{34.3} 14.3	^{35.1} 12.9	^{39.9} 8.7	^{40.5} 8.1	^{40.97} 7.60	^{41.1} 7.5	^{41.1} 7.5	^{40.5} 8.2	^{39.4} 9.2
31	24	16	10		9	13	19	22

^{34.1} 14.5	^{33.3} 15.3	^{33.6} 15.0	^{41.9} 0.7	^{47.8} 0.8	^{47.1} 0.9	^{45.1} 3.5	^{39.0} 9.6
35	58	70	70	57	44	36	28

^{39.1} 9.5	^{38.0} 10.6	^{38.3} 10.3	^{40.4} 8.2	^{40.9} 7.7	^{41.3} 7.3	^{41.3} 7.3	^{41.2} 7.4	^{40.5} 8.1	^{39.4} 9.2
39	29	23	18	11		8	13	17	24

^{38.1} 10.2	^{39.5} 9.1	^{45.8} 2.8	^{45.1} 3.5	^{42.9} 5.7	^{41.4} 7.2	^{39.2} 9.4
54	70	20	62	39	33	27

^{41.0} 3.4	^{38.9} 8.5	^{38.9} 8.5	^{40.8} 6.6	^{41.5} 5.9	^{41.6} 5.8	^{41.6} 5.8	^{41.1} 6.3	^{38.8} 8.6	^{38.5} 8.9
44	35	33	25	16		5	14	23	28

^{43.0} 4.4	^{43.2} 4.2	^{43.3} 4.1	^{42.3} 5.1	^{39.1} 8.3
65	70	70	66	44

Sta + π - Elev.

947.38

31+50

✓

32

✓

+50

✓

TP 5.42 951.99 0.81 946.57 946.57

FX
LPD
GA

11

Sept 23, 1968

RT X-36

39.9	39.9	A1.4	A1.8	A1.8	A1.6	A1.5	38.1	37.9
8.0	7.5	6.0	5.6	5.6	5.8	5.9	9.3	9.5
36	28	25	16		5	13	23	28

Baseline

A2.9	A2.0	A2.4				38.5	37.3
4.5	5.4	5.0				8.9	10.1
45	62	70				70	51

A0.4	A1.6	A2.2	A2.3	A2.1	A2.0	A1.3	38.1	38.2
7.0	5.8	5.2	5.1	5.3	5.4	6.1	8.7	9.2
30	28	18	8		2	10	18	24

39.8	A2.3	A1.3				38.5	38.0
7.6	5.1	6.1				8.9	9.4
38	45	70				70	52

A0.9	A2.3	A2.5	A2.7	A2.5	A1.8	A1.1	A0.8	A1.2
6.5	5.1	4.9	4.7	4.9	5.6	6.3	6.6	6.2
33	30	20	10		9	14	16	18

A0.7	A3.0	A1.6				A2.1	A2.0	A2.2	A2.4
6.7	4.4	5.8				5.3	5.4	5.2	5.0
40	46	70				70	54	27	23

M.H. Guard Post

Sta + π - Elev.

951.99

33

✓

+50

✓

34

✓

Sept 23, 1968

X-37

Lt.

2

RT

A2.A	A2.8	A2.9	A2.9	A2.9	A2.7	A1.9	A1.8
96	92	91	91	91	93	10.1	10.2
32	22	11	3		6	9	12

A1.A	A1.1	A3.9	A2.6	A2.6	A7.A	A8.2	A8.A	A8.A
10.6	10.9	8.1	9.4	9.4	4.6	3.8	3.6	3.6
35	42	49	66	70	70	59	38	21

A1.9	A2.6	A3.1	A3.3	A3.2	A3.1	A3.0	A2.2	A2.3	A8.A
10.1	9.4	8.9	8.7	8.8	8.9	9.0	9.8	9.5	3.6
38	33	23	13	4		5	8	10	17

A1.6	A1.0	A3.0	A2.6	50.1	50.A	A9.7	A9.7
10.4	8.0	9.0	9.4	1.9	1.6	2.3	2.3
43	47	61	70	70	58	38	22

A2.3	A3.0	A3.5	A3.6	A3.5	A3.3	A3.2	A2.5	A2.8	A7.A
97	90	85	8.4	8.5	8.7	8.8	9.5	9.2	4.6
38	36	26	16	6		2	5	8	16

23.3

A1.5	A3.A	A2.9	A2.6	A9.1	A8.9	A8.3	A8.3
10.5	8.6	9.1	9.4	2.9	3.1	3.7	3.7
46	51	61	70	70	53	38	18

Sta + π - Elev.

951.99

34+50

✓

35

✓

BM 2.72 946.90 7.81 944.18 (944.18)

35

+50

FK
LPD
G

LT.

Sept. 23, 1968
Sept. 26, 1968
BT X-38

A3A	A38	A39	A3.8	A3.5	A3.6	A3.7	A3.9	A3.2
8.6	8.2	8.1	8.2	8.5	8.4	8.3	6.1	5.8
37	28	18	9		2	7	13	18

26

A2.2	A1.2	A2.4	A1.2	A0.7	A5.2	A5.5	A6.1
9.8	10.8	9.6	10.8	11.3	6.8	6.5	5.9
40	49	55	64	70	70	53	38

A4.0	AA.2	AA.0	A3.7	A3.3	A2.9	A5.3	A7.1	A3.8
8.0	7.8	8.0	8.3	8.7	9.1	6.7	6.9	8.2
30	21	11	2		4	9	17	36

A3.5	A1.7	A0.9			39.9	A1.8
85	10.3	11.1	stunk		12.1	10.2
38	41	53			70	52

Spike in Arc Light

A0.4	A1.4	A0.7
4.5	5.5	6.2
70	59	55

AA.1	AA.3	AA.2	AA.1	A3.5	A2.9	A3.0	A2.4	A0.9	38.5
2.8	2.6	2.7	2.8	3.4	7.0	3.9	4.5	6.0	8.4
32	23	13	7	4		6	12	26	45

Reed

A3.6	A1.8	A0.9	A2.1	A1.1		35.1	35.9
3.3	5.1	6.0	4.8	5.8		11.8	11.0
39	49	53	59	70		70	62

Sta + π - Elev.

946.90

36+00

✓

+38 M.H. 7' Lt. 4.37 942.53

+50

✓

37

✓

Lt.

Sept 26, 1968 Rt. X-39

AA.5	AA.4	AA.1	A3.5	A1.6	A0.3	3.1	1A	3.8
2.4	2.5	2.8	3.4	5.3	6.6	8.8	11.5	13.1
26	15	10	6		8	20	32	45

Road ————— water

AA.4	A3.9	A2.9	A2.4
2.5	3.0	4.0	4.3
35	43	51	70

AA.8	AA.7	AAA	A2.2	A1.6	A0.8	3.9	3.6.1	3.9
2.1	2.2	2.5	4.7	5.3	6.1	8.0	10.8	13.0
28	17	9	4		8	17	28	45

Road

AA.7	AA.2	A2.9	A3.0	1.3	AA.5
2.2	2.7	4.0	3.9	1.6	2.4
37	46	50	54	58	70

A5.2	A5.2	A2.1	AA.7	AA.1	A1.7	3.9	3.5	1A	3.8
1.7	1.7	1.8	2.2	2.8	5.2	7.0	9.4	11.5	13.1
39	30	20	14	10		6	16	28	45

AA.9	A3.3	A3.1	A5.8	A5.2
2.0	3.6	3.8	1.1	1.7
47	51	56	60	70

Sta + π - Elev.

946.90

37+50

✓

BM

2.72 944.18 (944.18)

T.P. 1.35 943.88

942.53

36+00

+50

37

TP 7.24 949.00 2.12 941.76

4.27 941.73

FX
KG
GA

Lt.

Sept. 26, 1968
Oct 31, 1968 Rt X-40

A ^{5.9}	A ^{5.8}	A ^{5.5}	AA ⁹	A ^{1.7}	3 ^{9.0}	3 ^{7.5}	3 ^{6.7}	3A ⁹	3A ²
10	11	14	20	52	7.9	9.4	11.2	12.0	12.7
41	32	22	14	8		7	15	31	51

A ^{5.7}	A ^{3.5}	A ^{3.2}	A ^{5.7}	A ^{5.1}	
1.2	3.4	3.7	1.2	1.5	
49	53	58	64	70	

Spike in Arc Lt. Pole

33.9
13.0
70

MH 7' Lt Sta 36 + 38

3A.A	33.1	32.9
9.5	10.8	11.0
38	60	70

3A.A	33.1	32.9	32.8
9.5	10.8	11.0	11.1
39	56	65	70

3A.A	33.1	33.1	33.0
9.5	10.5	10.8	10.9
37	53	65	70

Top East End 24" S.C.P. A' Lt Sta 37 + 64

Top West End

Sta + π - Elev.

949.00

37+76

92

✓

+92

✓

38 shoulder of Ent

(41.6)

✓

LH

Oct. 31, 1968
RT X-41

Al.2	Al.1	A5.8	AA.8	A3.9	Al.8	Al.5	A5.9
28	29	32	4.2	9.1	12.2	12.5	13.1
42	32	21	12		17	28	44

Road

Al.1	A3.6	A3.2	Al.0	A5.7		Al.8	Al.1
29	5.4	5.8	3.0	33	✓	13.2	12.9
49	54	58	64	70		70	52

Al. A	Al.3	A3.9	A5.7	AA.5	A3.6	A3.6	A3.2
26	27	31	3.3	4.5	9.4	10.4	10.8
41	31	21	13		14	31	53

Road

Al.3	A3. A	A3.6	Al. A	A5.7		A3.6	A3.9	A3.6
2.7	5.6	5.4	2.6	3.3	✓	9.44	10.1	10.4
48	52	59	64	70		24	70	65

1p. 15" CM

Al.5	Al. A	Al.1	A5.9	AA.3	A3.6	A2.7	A2.1	A2.0
2.5	2.6	2.9	3.1	4.7	5.4	6.3	6.9	7.0
41	32	22	15		19	38	65	70

Road

Al.5	A3. A	A3.9	Al. A	A5.7		Al.2	Al.5	Profile
2.5	5.6	5.1	2.6	3.3	✓	7.8	7.5	Profile
47	53	59	65	70		150	100	

Sta + π - Elev.
949.00

38+13 shoulder Ent Rt.

25

60

✓

+25

✓

150 = 92.05

+60

✓

BM 8.63 952.81 4.81 944.19 944.18

LT

Oct. 31, 1968 X-42
RT.

Al.7	Al.5	Al.2	Al.1	AA.5	A3.1	A2.7	AA.1	A2.5
2.3	2.5	2.8	2.9	4.5	5.9	6.3	6.6	6.5
42	32	22	15		29	49	65	70

Al.7	A3.5	A3.A	Al.3	A5.9
2.3	5.5	5.6	2.7	3.1
47	54	61	65	70

Al.8	Al.7	Al.4	Al.2	A2.8	A1.3	A0.8	A2.3
2.2	2.3	2.6	2.8	6.2	7.7	8.16	6.7
42	33	22	15		19	23	42

Root

Inc 15" CM

Al.7	A3.9	A3.6	Al.7	Al.1	A3.3	A3.1
2.3	5.1	5.4	2.3	2.9	5.7	5.9
47	53	60	65	70	70	65

A7.3	A7.2	Al.8	A5.9	A2.8	A2.5	A3.2	AA.1	A5.3
1.7	1.8	2.2	3.1	6.2	6.5	5.8	4.9	3.7
42	32	22	14		14	33	51	65

Root

A7.1	AA.8	AA.8	A7.1	Al.3	A5.7
1.9	4.2	4.2	1.9	2.7	3.3
47	52	54	60	70	70

Spike in Arc Light.

Sta + π - Elev.

952.81

39+00

42.90

✓

+49

42.90

✓

+65

42.80

✓

FK
KG
GA

Nov. 1, 1968

11

2

ft.

X-43

$\begin{matrix} A7.7 & A7.7 & A7.4 & A6.5 & A5.4 & A5.1 & A5.9 & A6.1 & A7.4 & A8.2 \\ 51 & 51 & 54 & 63 & 74 & 77 & 69 & 61 & 52 & 46 \\ 43 & 33 & 23 & 14 & 8 & & 21 & 41 & 60 & 70 \end{matrix}$
 Road

$\begin{matrix} A7.5 & A5.2 & A5.1 & A6.1 & A5.8 \\ 53 & 76 & 77 & 67 & 70 \\ 48 & 53 & 57 & 62 & 70 \end{matrix}$

$\begin{matrix} A8.2 & A8.0 & A7.8 & A7.2 & A7.2 & A9.8 & A0.6 & A1.1 & A2.3 & A3.2 \\ 46 & 48 & 50 & 56 & 56 & 30 & 22 & 14 & 0.5 & 10.4 \\ 34 & 23 & 18 & 14 & 6 & & 18 & 38 & 60 & 70 \end{matrix}$
 Road

$\begin{matrix} A8.3 & A8.2 & A6.1 & A6.2 & A8.3 & A8.0 & A7.7 \\ 45 & 46 & 67 & 66 & 45 & 48 & 51 \\ 43 & 48 & 53 & 56 & 61 & 66 & 70 \end{matrix}$

$\begin{matrix} A8.4 & A8.2 & A8.0 & A7.7 & A8.0 & A7.8 & A7.9 & A8.9 & A9.8 & A0.4 \\ 44 & 46 & 48 & 51 & 48 & 50 & 49 & 39 & 30 & 2.4 \\ 33 & 22 & 20 & 16 & 13 & & 20 & 39 & 57 & 70 \end{matrix}$
 Road MH

$\begin{matrix} A8.6 & A8.5 & A8.1 & A6.4 & A6.4 & A8.7 & A8.3 \\ 42 & 43 & 47 & 64 & 64 & 41 & 45 \\ 42 & 47 & 50 & 53 & 56 & 61 & 70 \end{matrix}$

Sta + π - Elev.

952.81

40+00

42.76

✓

+ 50

42.98

✓

T.P. 4.03 954.51 2.33 950.48 950.48

41

43.23

✓

TP 2.36 955.65 1.22 953.29 953.29

LT

Nov. 1, 1968

RT X-44

A9.8	A8.6	A8.4	A7.6	A8.1	A7.5	A7.5	A7.4
40	4.2	4.4	5.2	4.7	5.3	5.3	5.4
33	23	17	10		22	49	67

Real

A8.9	A8.8	A8.3	A6.7	A7.1	A8.5	A7.9	A7.3
3.9	40	4.5	6.1	5.7	4.3	4.9	5.5
43	48	50	53	60	68	70	70

A9.5	A9.4	A9.2	A8.9	A6.5	A7.6	A7.1	A6.3	A3.6	A2.5
3.3	3.4	3.6	3.9	6.3	5.2	5.7	6.5	9.2	10.3
43	33	23	18	5		17	29	43	45

Real

A9.5	A7.5	A7.4	A8.8	A8.7	A1.9	A2.2	A3.2
3.3	5.3	5.4	40	4.1	10.9	10.6	9.6
49	53	56	64	70	70	65	47

Nail in Transformer Power Pole

50.0	A9.8	A9.6	A9.3	A8.7	A5.9	A3.5	A1.0	40.9	40.2
4.5	4.7	4.9	5.2	5.8	8.6	11.0	13.5	13.6	14.3
43	32	22	16	12		16	40	56	70

Real

50.1	50.0	50.0	A9.9	50.2
4.4	4.5	4.5	4.6	4.3
48	59	70	100	141

Profile Ent 2+

Top Steel Post LT

Sta + π - Elev.

955.65

41+50

43.09

✓

42

42.37

✓

+50

40.50

FA
KG
GA

LT

NOK 4, 1968

X-45
RT

50.1	49.9	49.7	49.1	45.3	43.8	44.2	43.9
5.6	5.8	6.0	6.6	10.4	11.9	11.5	11.8
31	22	16	13		22	42	63

50.3	50.3	50.2	52.4	52.9		43.0
5.4	5.4	5.5	3.3	2.8		12.7
42	48	56	66	70		70

50.3	49.2	50.0	49.8	49.1	45.9	43.9	43.1	43.3	42.9
5.4	5.5	5.7	5.9	6.6	9.8	11.8	12.6	12.4	12.8
40	29	21	14	11		22	40	53	70

Fe

50.3	48.8	49.3	44.9	45.0
5.4	6.9	6.4	0.8	0.7
46	52	58	67	70

50.3	50.2	50.0	49.7	48.9	46.0	44.0	43.6	44.0	43.8
5.4	5.5	5.7	6.0	6.8	9.7	11.7	12.1	11.7	11.9
38	28	19	13	9		18	35	49	70

50.2	48.2	48.4	45.1
5.5	7.5	7.3	0.6
46	50	58	70

Sta + π - Elev.

955.63

43

38.3

✓

TP 1.44 954.67 2.42 953.23 953.23

+44

36.4

✓

+83

34.7

✓

Nov. 4, 1968
 31 x-46

LT

50.1	50.1	50.2	49.3	46.7	44.2	44.3	44.5	46.0
5.3	5.3	5.5	6.4	9.0	11.5	11.4	11.2	9.7
36	25	17	7		19	25	42	70

Fe

50.1	50.3	49.3	49.0		47.7	47.4
5.6	5.4	6.4	6.7	Profile Ent Lt	8.00	8.28
43	62	70	95		SEnd	NEnd

MH Guard Post 12" Culvert

50.5	50.6	50.4	50.1	48.5	48.2	47.9	46.1	46.9	47.1
4.2	4.1	4.3	4.6	6.15	6.5	6.8	8.6	7.8	7.6
34	22	14	7	4		10	18	38	56

MH Fe

50.0	47.3	45.2	44.6		48.4
4.7	7.4	9.5	10.1		6.3
42	46	61	70		70

50.5	50.7	50.5	50.3	49.2	47.6	50.3	47.0	42.0
4.2	4.0	4.2	4.4	5.5	7.1	4.4	3.7	2.7
32	21	12	5		6	17	30	39

50.1	44.2	42.7		48.8	47.4
4.6	10.5	12.0		1.9	3.3
41	51	70		70	54

Sta + A - Elev.

954.67

44+00

33.96

✓

+38

32.29

✓

+70

30.9

✓

LT,

Nov. 4, 1968

RT X-47

$f_{0.6}$	$f_{0.7}$	$f_{0.6}$	$f_{0.3}$	$A_{9.2}$	$A_{7.8}$	$A_{8.1}$	$f_{0.2}$	$f_{1.0}$
4.1	4.0	4.1	4.4	5.5	6.9	6.6	4.5	3.7
31	20	11	5		5	10	19	29

$f_{0.2}$	$A_{9.8}$	$A_{3.2}$	$A_{2.1}$	$A_{1.3}$	$f_{3.2}$	$f_{1.9}$	$f_{1.3}$
4.5	4.9	11.5	12.6	13.4	1.5	2.8	3.4
37	39	49	58	70	20	60	42

$f_{0.4}$	$f_{0.7}$	$f_{0.9}$	$f_{0.8}$	$f_{0.6}$	$f_{0.2}$	$A_{8.1}$	$A_{9.0}$	$A_{9.5}$	$f_{1.1}$
4.3	4.0	3.8	3.9	4.1	4.5	6.6	6.7	5.2	3.6
35	29	17	9	3		7	11	23	28

$A_{9.8}$	$A_{1.4}$	$A_{1.0}$	$A_{0.4}$	$f_{3.3}$	$A_{1.4}$
4.9	13.3	13.7	14.3	1.4	3.3
37	49	55	70	70	51

$A_{9.8}$	$f_{0.3}$	$f_{0.8}$	$f_{1.0}$	$f_{0.9}$	$f_{0.5}$	$f_{0.2}$	$A_{8.0}$	$A_{9.3}$	$f_{1.2}$
4.9	4.2	3.9	3.7	3.8	4.2	4.5	6.7	5.4	3.5
36	33	28	16	8		2	7	19	25

$A_{1.5}$	$A_{1.2}$	$A_{1.0}$	$f_{1.0}$	$f_{0.3}$	$f_{1.3}$
13.2	13.5	13.7	0.7	2.4	3.4
48	54	70	70	54	40

Sta + π - Elev.

954.67

45

29.58

✓

TP 10.83 955.90 9.60 945.07

+ 50

27.40

✓

46

25.21

✓

Lt

2 Nov. 4, 1968

Rt X-40

$\phi_{0.2}$	$\phi_{0.9}$	$\phi_{1.1}$	$\phi_{1.0}$	$\phi_{0.7}$	$\phi_{0.5}$	$\phi_{0.1}$	$\phi_{0.6}$	$\phi_{0.9}$
45	3.8	3.6	3.7	4.0	8.18	9.6	9.1	6.8
33	26	15	6		7	8	9	14

Top Culv

$\phi_{0.8}$	$\phi_{0.9}$	$\phi_{1.1}$	$\phi_{0.5}$	$\phi_{0.7}$	$\phi_{0.6}$	$\phi_{0.8}$
10.9	12.8	13.0	2.2	3.0	3.2	3.9
43	59	70	70	50	34	22

Top Culv 40' Lt sta 45+08

$\phi_{0.2}$	$\phi_{0.8}$	$\phi_{1.1}$	$\phi_{1.3}$	$\phi_{1.2}$	$\phi_{1.1}$	$\phi_{0.8}$	$\phi_{0.3}$	$\phi_{0.3}$	$\phi_{0.0}$	$\phi_{0.1}$
5.7	5.1	4.8	4.6	4.7	4.8	5.1	5.6	7.6	3.9	3.8
32	30	25	13	5		3	7	12	21	41

$\phi_{1.0}$	$\phi_{1.3}$	$\phi_{1.1}$	$\phi_{1.8}$	$\phi_{0.8}$	$\phi_{0.0}$
14.3	14.6	13.8	14.1	3.1	3.3
46	52	58	70	70	59

$\phi_{0.5}$	$\phi_{1.0}$	$\phi_{1.3}$	$\phi_{1.5}$	$\phi_{1.4}$	$\phi_{1.4}$	$\phi_{1.2}$	$\phi_{0.6}$	$\phi_{0.1}$	$\phi_{0.2}$
5.4	4.9	4.6	4.4	4.5	4.5	4.7	5.3	6.8	6.7
29	27	22	11	3		5	8	13	16

$\phi_{1.3}$	$\phi_{0.2}$	$\phi_{1.0}$	$\phi_{1.5}$	$\phi_{0.0}$	$\phi_{0.1}$	$\phi_{0.3}$	$\phi_{0.0}$
14.6	15.7	14.9	14.4	3.9	3.8	2.6	3.9
42	52	62	70	70	44	26	22

Sta	+	π	-	Elev.
-----	---	-------	---	-------

Sta	+	π	-	Elev.
		955.90		

Sta	+	π	-	Elev.
46+45				24.08

Sta	+	π	-	Elev.
✓				

Sta	+	π	-	Elev.
+90				23.58

Sta	+	π	-	Elev.
✓				

Sta	+	π	-	Elev.
47				23.50

Sta	+	π	-	Elev.
✓				

Nov. 4, 1968

Lt.

~~E~~

X-49

50.9	51.3	51.5	51.8	51.6	51.5	50.6	49.7	50.0
5.0	4.6	4.4	4.1	4.3	4.4	5.3	6.2	5.9
28	26	20	9		6	10	13	16

45.5	43.6	42.6	42.0	41.2	41.2	42.1	41.4	43.6
10.4	12.3	13.3	13.9	4.7	4.7	3.8	1.3	2.3
37	45	59	70	70	61	45	26	19

48.8	41.2	41.5	41.8	42.0	42.0	42.0	41.7	41.0	50.1	50.4
7.1	4.7	4.4	4.1	3.9	3.9	3.9	4.2	4.9	5.8	5.5
32	28	26	19	7		2	7	11	14	17

48.3	45.9	44.6	43.3	41.0	41.0	41.2	40.8	42.9
7.6	10.0	11.3	12.6	4.9	4.9	4.7	3.1	3.3
36	43	56	70	70	59	43	26	22

49.6	51.5	51.8	52.0	52.0	52.1	51.9	51.4	50.5	51.0
6.3	4.4	4.1	3.8	3.9	3.8	4.0	4.5	5.4	4.9
31	26	17	6		3	8	12	15	19

48.4	48.7	45.7	44.5	41.0	50.9	50.9	51.7	52.2
7.3	7.2	10.2	11.4	4.9	5.0	5.0	4.2	3.7
40	52	61	70	70	66	48	31	23

Sta + Δ - Elev

955.90

✓
47+14 Field Ent. Rt.

23.56

✓
+35 Ent. Rt. Abandon Homesite 23.65

✓
+50

23.72

✓

Nov. 4, 1968

X-50

$\begin{matrix} 51.1 & 50.5 & 51.6 & 51.8 & 52.1 & 52.1 & 52.1 & 51.9 & 52.2 & 51.8 \\ 4.8 & 5.4 & 4.3 & 4.1 & 3.8 & 3.8 & 3.8 & 4.0 & 3.73 & 4.1 \\ 42 & 29 & 25 & 16 & 6 & & 4 & 9 & 15 & 29 \end{matrix}$
 MH

$\begin{matrix} 50.5 & 48.9 \\ 5.4 & 7.0 \\ 65 & 70 \end{matrix}$

$\begin{matrix} 51.1 & 51.0 \\ 4.8 & 4.9 \\ 70 & 48 \end{matrix}$

$\begin{matrix} 51.6 & 51.2 & 51.7 & 51.9 & 52.1 & 52.2 & 52.3 & 52.2 & 53.0 & 53.4 \\ 4.3 & 4.7 & 4.2 & 4.0 & 3.8 & 3.7 & 3.6 & 3.7 & 2.9 & 2.5 \\ 34 & 30 & 24 & 16 & 5 & & 4 & 19 & 40 & 58 \end{matrix}$

$\begin{matrix} 51.2 & 50.5 & 50.4 \\ 4.7 & 5.4 & 5.5 \\ 52 & 68 & 70 \end{matrix}$

$\begin{matrix} 51.7 \\ 2.2 \\ 70 \end{matrix}$

$\begin{matrix} 50.9 & 51.7 & 51.9 & 52.2 & 52.3 & 52.3 & 52.4 & 52.6 & 53.1 \\ 5.0 & 4.2 & 4.0 & 3.7 & 3.6 & 3.6 & 3.5 & 3.3 & 2.8 \\ 27 & 23 & 15 & 4 & & 4 & 12 & 20 & 39 \end{matrix}$

$\begin{matrix} 51.8 & 51.6 & 51.3 \\ 4.1 & 4.3 & 4.6 \\ 33 & 51 & 70 \end{matrix}$

$\begin{matrix} 51.1 & 53.4 \\ 1.8 & 2.5 \\ 70 & 54 \end{matrix}$

Sta	+	π	-	Elev
		955.90		
47+70				23.84
✓				
48				24.02
✓				
T.P	7.60	959.97	3.53	952.37 (952.35)
+50				24.40
49				24.82
✓				
Oil Pipe Line				

Nov. 4, 1968

Lt.

RT X-51

51.2	51.9	51.9	52.3	52.3	52.4	52.5	52.1	52.9
4.7	4.0	4.0	3.6	3.6	3.5	3.4	3.8	3.0
27	23	14	2		6	12	16	29

52.3	51.8	51.5	51.6
3.6	4.1	4.4	4.3
34	47	63	70

51.5	53.0
1.4	2.9
70	46

52.1	51.9	52.3	52.6	52.6	52.7	52.5	53.9	51.2
3.2	4.0	3.6	3.3	3.3	3.2	3.4	2.0	1.7
31	21	13	2		8	17	34	56

52.5	52.4
3.4	3.5
50	70
Rock	

51.5
1.4
70

52.8	52.1	52.9	52.0	52.5	52.8	53.1	53.3	53.1	51.3	55.5	51.1
7.2	7.3	7.1	8.0	7.5	7.2	6.9	6.7	6.9	5.7	4.5	2.6
70	47	26	21	17	12		8	16	29	47	70

51.2	51.3	52.2	52.4	53.2	53.6	53.8	53.9	51.9	56.2	51.4
8.7	8.7	7.8	7.4	6.8	6.4	6.2	6.1	5.1	3.8	2.6
41	27	21	18	11		9	19	31	47	60

50.0	49.8
10.0	10.2
58	70

58.6
1.4
70

Sta + π - E/ev.

959.97

49+50

25.08

✓

50

E₀ + R₀

25.12

+50

24.04

✓

51

22.95

BM 9.77 959.88 9.84 950.13

950.11

Nov. 4, 1968

X-52

LT.

✓

RT

12.9	11.8	12.8	13.3	13.8	1A.1	1A.0	1A.6	11.2
7.1	8.2	7.2	6.7	6.2	5.9	6.0	5.4	4.8
29	25	19	10		9	16	19	33

MH

11.5	1A.9	1A.3	1A.3	11.5	11.9	11.9
8.5	10.1	10.7	10.7	2.5	3.1	4.1
32	43	59	70	70	62	47

13.1	12.8	12.5	13.3	13A	13.8	1A.0	1A.7	11.5	11.3
6.9	7.2	7.5	6.7	6.6	6.2	6.0	5.3	4.5	3.7
70	48	35	18	10		10	29	53	70

13.7	13A	12.6	13.5	13.6	13.8	13.7	1A.1	11.0	11.8	11A
6.3	6.6	7.4	6.5	6.4	6.2	6.3	5.9	5.0	4.2	3.6
42	26	22	16	10		10	20	37	55	70

1A.1	1A.0
5.9	6.0
55	70

13.6	13A	13.7	13.1	12.8	13.2	13.3	13.3	13.3	1A.3	13.3	11.7
6.4	6.6	6.3	6.9	7.2	6.8	6.7	6.7	6.7	5.7	4.7	3.3
56	43	27	25	19	11		10	17	27	42	70

13.9

6.1

70

Top Flat iron Connector S.E. Corner #132 of Power Line Tower

Sta + π - Elev

959.88

51+24

22.43

✓

+37

22.15

+67

21.50

✓

+98 MH 18' Rt

2.79 952.09

+

52

20.78

T.P.

3.19 954.54 8.53 951.35

FX
LPD
GA

11

Nov. 6, 1968 X-53
BT

$\beta_{3.4}$	$\beta_{3.6}$	$\beta_{2.0}$	$\beta_{2.1}$	$\beta_{3.0}$	$\beta_{3.1}$	$\beta_{3.0}$	$\beta_{2.9}$	$\beta_{A.2}$	$\beta_{1.8}$
65	63	79	72	69	68	69	70	57	41
49	28	22	17	10		10	17	30	49

$\beta_{3.3}$	$\beta_{3.6}$
66	63
61	70

$\beta_{6.6}$
33
70

$\beta_{2.5}$	$\beta_{3.1}$	$\beta_{3.1}$	$\beta_{2.0}$	$\beta_{2.5}$	$\beta_{2.8}$	$\beta_{2.9}$	$\beta_{2.8}$	$\beta_{2.9}$	$\beta_{A.7}$	$\beta_{6.9}$	$\beta_{A.0}$
74	68	68	79	74	71	70	71	71	52	30	09
70	49	27	22	17	10		10	17	30	48	70

$\beta_{2.5}$	$\beta_{2.9}$	$\beta_{1.3}$	$\beta_{2.1}$	$\beta_{2.4}$	$\beta_{2.5}$	$\beta_{2.4}$	$\beta_{2.5}$	$\beta_{A.8}$	$\beta_{6.6}$	$\beta_{6.8}$
74	70	86	78	75	74	75	74	51	33	11
44	28	21	17	10		10	16	34	51	70

$\beta_{A.2}$	$\beta_{6.1}$
87	98
60	70

$\beta_{0.2}$	$\beta_{1.5}$	$\beta_{0.0}$	$\beta_{1.8}$	$\beta_{1.9}$	$\beta_{2.0}$	$\beta_{1.9}$	$\beta_{1.9}$	$\beta_{3.9}$	$\beta_{5.8}$	$\beta_{6.5}$
97	84	99	81	80	79	80	80	60	41	34
36	29	22	15	10		10	16	37	57	70

$\beta_{9.1}$	$\beta_{7.4}$
108	125
52	70

Sta + π - Elev

954.54

52+16 Ent Rt Bit.

20.44

✓

+30

20.14

✓

+58

19.53

24

Nov 6, 1968

Rt X-54

$\begin{matrix} 50.1 & 49.7 & 51.3 & 51.5 & 51.6 & 51.5 & 51.5 & 52.0 & 52.5 \\ 3.8 & 4.8 & 3.2 & 3.0 & 2.9 & 3.0 & 3.0 & 2.5 & 2.0 \\ 29 & 22 & 16 & 10 & & 10 & 16 & 33 & 53 \end{matrix}$

$\begin{matrix} 49.1 & 47.8 & 46.9 \\ 5.4 & 6.7 & 7.6 \\ 38 & 58 & 70 \end{matrix}$

$\begin{matrix} 52.9 \\ 1.6 \\ 70 \end{matrix}$

$\begin{matrix} 50.0 & 49.3 & 50.8 & 51.0 & 51.2 & 51.3 & 51.2 & 51.1 & 51.8 & 52.9 \\ 4.5 & 5.2 & 3.7 & 3.5 & 3.3 & 3.2 & 3.3 & 3.4 & 2.7 & 1.6 \\ 28 & 22 & 18 & 15 & 10 & & 10 & 16 & 21 & 37 \end{matrix}$

$\begin{matrix} 48.0 & 46.9 & 46.2 \\ 6.5 & 7.6 & 8.3 \\ 39 & 54 & 70 \end{matrix}$

$\begin{matrix} 51.1 & 53.8 \\ 0.1 & 0.7 \\ 70 & 54 \end{matrix}$

$\begin{matrix} 48.5 & 50.1 & 50.5 & 50.7 & 50.7 & 50.7 & 50.6 & 51.3 & 52.0 \\ 6.0 & 4.4 & 4.0 & 3.8 & 3.8 & 3.8 & 3.9 & 3.2 & 2.5 \\ 21 & 19 & 16 & 10 & & 10 & 16 & 20 & 33 \end{matrix}$

$\begin{matrix} 48.2 & 49.1 & 46.7 & 45.2 & 44.2 \\ 6.3 & 5.4 & 2.8 & 9.3 & 10.3 \\ 24 & 28 & 38 & 56 & 70 \end{matrix}$

$\begin{matrix} 51.7 & 53.6 \\ 4.2 & 0.9 \\ 70 & 47 \end{matrix}$

Sta + π - Elev

954.54

53 Ent Rt. Bit.

18.61

✓

+33

19.89

✓

+80

16.87

✓

LT

Nov. 6, 1968
RT X-55

A7.0	A7.3	A9.5	A9.8	A9.9	A9.8	A9.9	10.8	11.9
7.5	7.2	5.0	4.7	4.6	4.7	4.6	3.7	2.6
28	21	15	10		10	17	30	51

A6.5	A7.7	A1.9	12.9
8.0	10.8	12.6	1.6
42	54	70	70

A6.7	A6.7	A8.6	A8.9	A9.1	A9.1	A9.8	A7.8	A8.2
8.8	7.8	5.9	5.6	5.4	5.4	5.7	6.7	6.3
28	21	16	10		10	18	24	33

A6.3	A0.9	10.4	10.6	A9.5
9.2	13.6			5.0
45	70	70	61	46

A6.9	A6.7	A7.8	A8.2	A8.4	A8.3	A8.0	A6.9	A6.7
8.6	7.8	6.7	6.3	6.1	6.2	6.5	7.6	7.8
30	22	20	10		10	18	24	29

A6.1	A4.8	A3.7	A1.9	A9.3	A8.4	A7.8
8.4	9.7	10.8	12.6	5.2	6.1	6.7
37	40	53	70	70	56	40

Sta + π - Elev.

954.54

54

16.44

✓

+25

15.90

✓

+45

15.47

LT

Nov. 6, 1968

RT

X-56

A6.3	A6.7	A7.1	A7.8	A7.9	A7.9	A7.5	A7.9	A6.9
8.2	7.8	7.4	6.7	6.6	6.6	7.0	8.6	7.6
34	26	23	10		10	17	22	35

A7.8	A7.6	A7.3
6.7	6.9	10.2
38	54	70

A8.4	A8.0
6.1	6.5
70	53

A6.9	A5.0	A6.4	A7.4	A7.6	A7.5	A7.1	A6.9	A6.3
7.6	9.5	8.1	7.1	6.9	7.0	7.4	9.6	8.2
38	34	23	10		10	15	22	27

A7.0	A6.4
7.5	7.9
56	70

A8.3	A7.9	A7.3
6.2	6.6	7.2
70	58	42

A2.1	A2.1/1.40	A2.1/1.40	A7.1	A7.3	A7.2	A6.8	A1.77	A6.8
12.4	11.94	8.6	7.4	7.2	7.3	7.7	11.31	7.7
45	28	25	10		10	18	22	29
	inv.						inv.	

A1.4	A0.7
13.1	13.8
58	70

A8.5	A7.3
6.0	7.2
70	44

Sta + π - E/ev.

954.54

54+55 Ditch Rt

15.25

✓

+62 Shoulder

15.10

+77.4 $\angle$ Co RLD

A.TX

BM

2.45 952.09 (952.08)

Nov. 6, 1968

X-57

Lt.

2/

RT

A3.7	AA.8	Ab.3	A7.0	A7.2	A7.2	A7.0	Ab.7	Ab.6
10.8	9.7	8.2	7.5	7.3	7.3	7.5	7.8	7.9
48	31	23	10		10	18	25	31

MH

A3.1

11.4
70

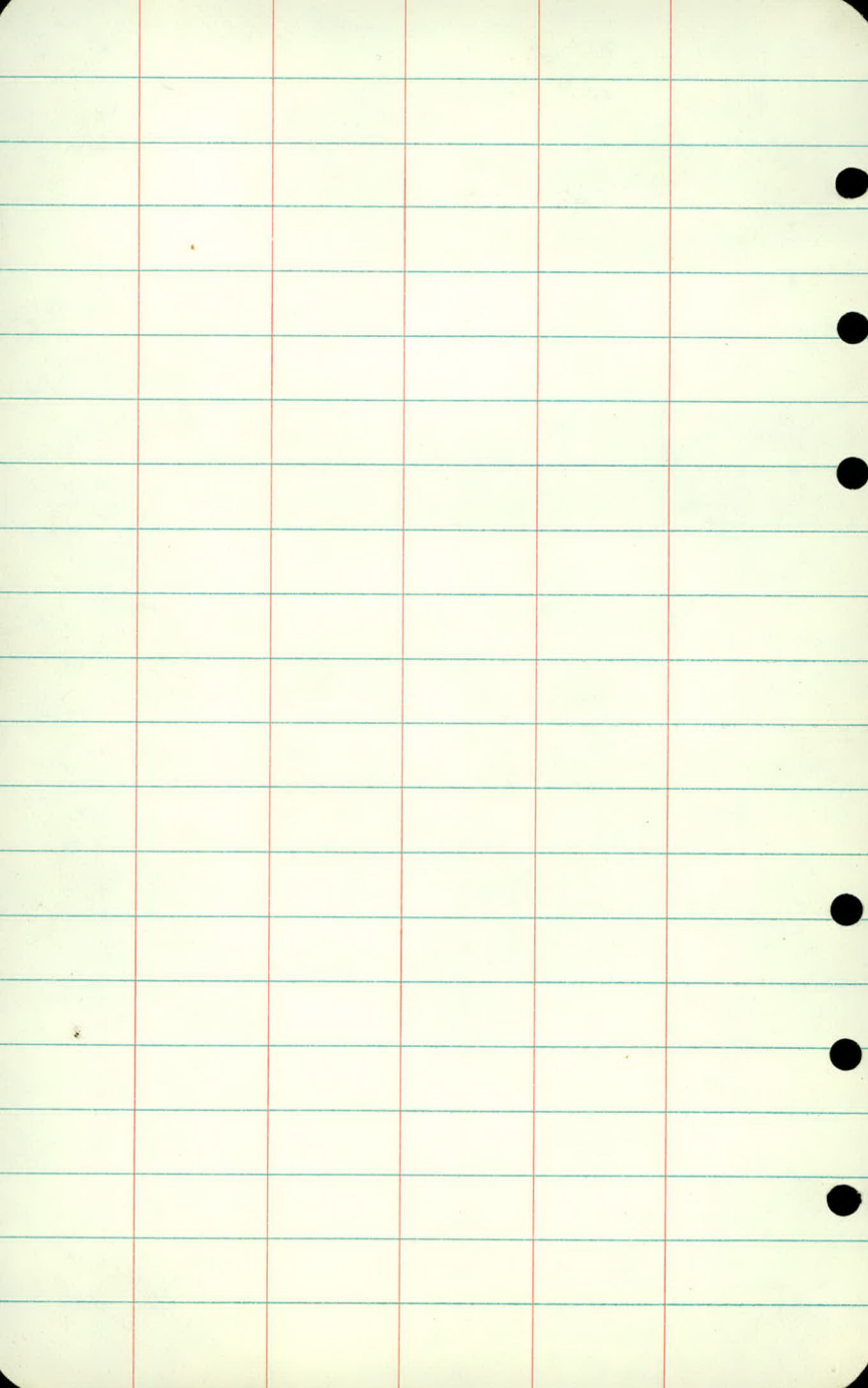
Ab.7 Ab.4 Ab.0 A5.3

7.8 8.1 8.5 9.2
70 60 47 35

AA.7	A5.3	Ab.2	A7.0	A7.2	A7.1	A7.0	A7.4	48.3
9.8	9.2	8.3	7.5	7.3	7.4	7.5	7.1	6.2
70	53	30	10		10	33	49	70

A5.2	A5.0	Ab.3	A7.0	A7.1	A7.1	A7.4	A7.9	48.7
9.3	8.7	8.0	7.5	7.4	7.4	7.1	6.6	5.8
70	54	32	10		10	32	51	77

Top W. Edge MH



Nov. 6, 1968

X-58

Bench Level Check

Sta	+	Σ	-	Elev.
T.P.	5.69	946.66		940.97
			4.81	941.85 ✓
			6.27	940.39 ✓
				1.46
T.P.	7.07	948.82	4.91	941.75 ✓
			? 2.25	946.57 ✓
BM	7.93	952.11	4.64	944.18 ✓
			10.36	.75 ✓
BM	4.29	954.77	1.63	950.48 ✓
			1.48	953.29 ✓
TP	3.27	956.50	1.54	953.23 ✓
TP	7.21	959.56	4.15	952.35 ✓
BM			9.45	950.11 ✓
BM			7.48	952.08 ✓

Nov. 6, 1968

X-59

Sta. 30 $\pm$

wood stake

Iron

MH

Spike in Arc Light Pole

Top E. End 24" S.C.P.

Nail in Transformer P.P.

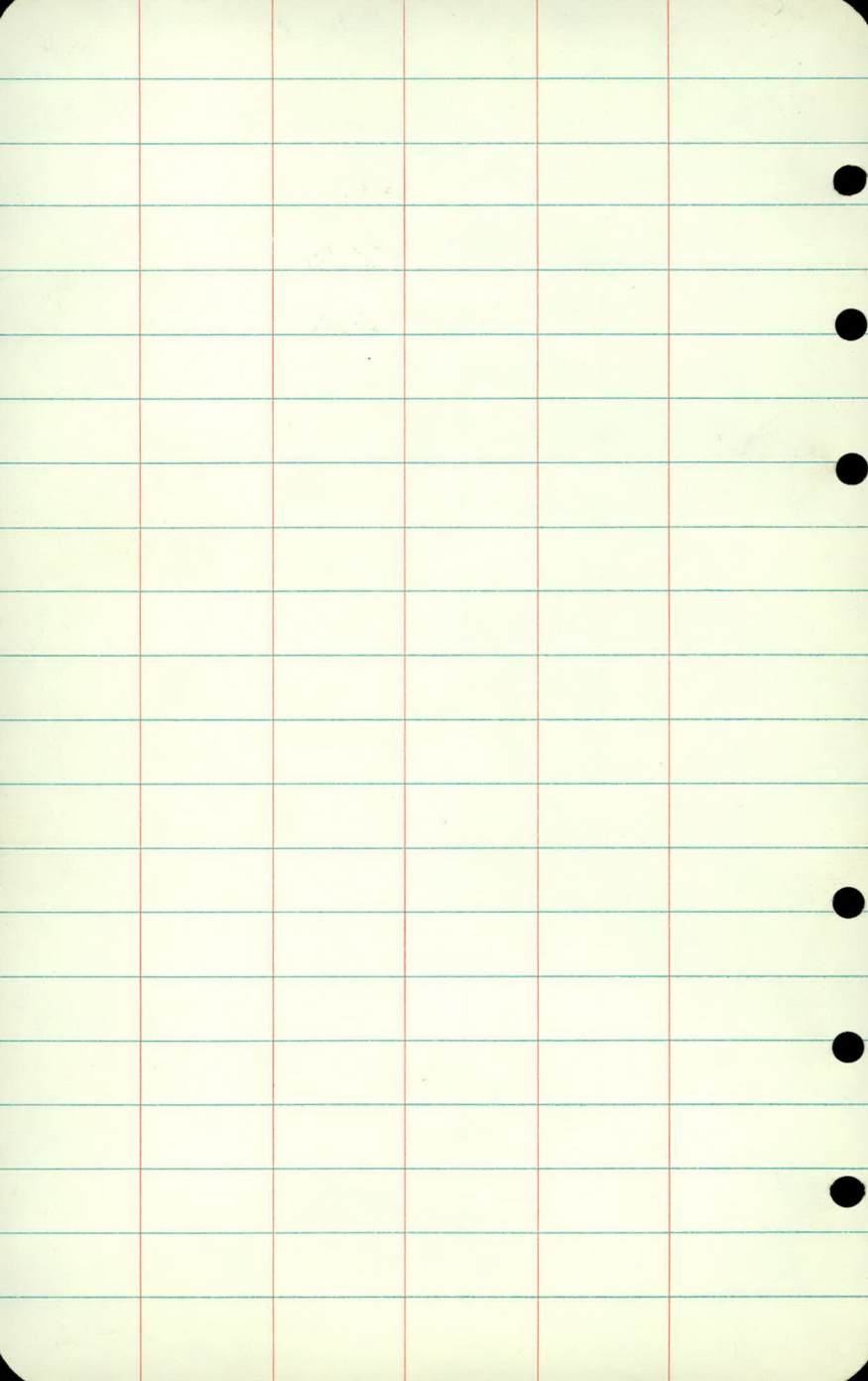
Top steel post Lt.

MH Guard Post Sta 43+40

Rock

Top Flat iron connector SE Corner #132 of Power
Line Tower

W. Edge MH 17' Rt Sta 51+98



White Bear Ave,

x-section Extensions

& Additional x-sections

Sta	+	π	-	Elev.
TP	4.72	944.73		940.01 Sta 23 &

22+38

24+40

5.

T.P.

5.40 939.33 939.26

AK
WS
GA

Lt

Jan. 8, 1968

£ X-61

37.4	37.5	37.8	38.0	37.8	39.8
7.3	7.2	6.9	6.7	6.9	4.9
119	110	91	80	68	£

37.4	37.6	37.6	37.8	38.0	37.7	39.7
7.3	7.1	7.1	6.9	6.7	7.0	5.0
122	100	95	70	48	28	

37.4

7.3

148

Sta 25+00 £

Distances from New L

Sta + π - Elev

TP 5.26 946.23 940.97 $\pm$ sta 30

30

+50

31

+50

32

+50

TP 5.92 948.72 343 942.80 sta 33 $\pm$

TP^v 2.19 948.76 2.19 946.53 (946.57)

FK
GA
JA
CM

LT

£

1-13-69

X-62

34.2

12.0
70

40.1

6.1
70

42.9

3.0 3.3
70 62

42.2

4.0
70

40.7

5.5
70

41.1

5.1
70

Top MH Guard Post

Sta	+	π	-	Elev
-----	---	-------	---	------

		948.76		
--	--	--------	--	--

33				
----	--	--	--	--

+50				
-----	--	--	--	--

34				
----	--	--	--	--

+50				
-----	--	--	--	--

35				
----	--	--	--	--

+50				
-----	--	--	--	--

TP	4.13	951.51	1.38	947.38
----	------	--------	------	--------

BM	7.35	951.53	7.35	944.16 (944.18)
----	------	--------	------	-----------------

Lt

1-13-69 X-63

A2.3

A2.6 ✓

6.4

6.1

70

60

A2.5

A2.6 ✓

6.2

6.1

70

60

A2.7

A2.5 ✓

6.0

6.2

70

60

A1.8

A1.0

6.9

7.7 ✓

70

55

A0.2

39.9

8.5

8.8 ✓

70

55

A1.5

A1.4

A1.4 ✓

7.2

7.3

7.3

70

60

50

Top MH Guard Post
Spike in Arc Light Pole

Sta	+	π	-	Elev
		951.53		

36

+50

37

+50

38

TP	6.90	953.41	5.02	946.51	38 ^{spike} £
----	------	--------	------	--------	-----------------------

+50

24

1-13-69
£ X-64

x2.2

9.3

70

x2.3

9.2

60

x2.6

8.9

45

✓

x2.1

9.4

70

x2.6

8.9

60

x3.1

8.4

50

x3.9

7.6

40

✓

x3.0

8.5

70

x3.6

7.9

60

x4.2

7.3

50

x4.7

6.8

40

✓

x4.0

7.5

70

x4.5

7.0

60

x4.7

6.8

50

x5.0

6.5

40

x5.4

6.1

70

x5.6

5.9

60

x5.7

5.8

50

x5.8

5.7

40

✓

x7.1

6.3

70

x6.8

6.6

60

x6.6

6.8

50

x6.5

6.9

40

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		953.41		
--	--	--------	--	--

37+76				
-------	--	--	--	--

+92				
-----	--	--	--	--

38+13				
-------	--	--	--	--

38+25				
-------	--	--	--	--

+60				
-----	--	--	--	--

39				
----	--	--	--	--

11

1-13-69

~~2~~

x-65

44.6

44.9

45.2

45.4

8.8

8.5

8.2

8.0

70

60

50

40

45.1

45.4

45.5

45.6

8.3

8.0

7.9

7.8

70

60

50

40

45.8

46.0

45.9

45.9

7.6

7.4

7.5

7.5

70

60

50

40

46.3

46.3

46.2

46.2

7.1

7.1

7.2

7.2

70

60

50

40

47.1

46.8

46.5

46.4

6.3

6.6

6.9

7.0

70

60

50

40

45.7

45.6

45.5

45.5

7.7

7.8

7.9

7.9

70

60

50

40

Sta + π - Elev.

953.41

39+49

+65

40

+50

BM 8.99 959.47 2.92 950.49 (950.48)

41+50

42

6.19 959.48 6.19 949.28 (953.29)

1-13-69

Lt

E

X66

Ab.1	Ab.1	Ab.3	Ab.6
7.3	7.3	7.1	6.8
70	60	50	40

✓

A7.2	A7.4	A7.7	A8.3
6.2	6.0	5.7	5.1
70	60	50	40

✓

A7.0	A7.0	A7.2	A7.5
6.4	6.4	6.2	5.9
70	60	50	40

✓

A7.3	A7.3	A7.2	A7.6
6.1	6.1	6.2	5.8
70	60	50	40

✓

Nail in transformer power pole

S2.2	S2.2	S2.2	S2.3
7.3	7.3	7.3	7.2
70	60	50	40

✓

S4.9	S5.2	S5.3	S5.2	S4.9
4.6	4.3	4.2	4.3	4.6
70	60	50	43	33

✓

Top N. Passing Post

Sta + π - Elev

959.48

42+50

TP 1.48 954.71 6.22 953.26 953.23

43+44

+83

44

TP 5.75 956.46 4.00 950.71 $\pm$ Sta 45

+38

+70

EX
JA
GA
CM

Lt

1-13-69
1-14-69 $\frac{1}{2}$

X-67

55.9	55.6	55.9	55.9	55.7
3.6	3.9	3.6	3.6	3.8 ✓
70	60	50	40	33

Top MH Guard Pist

A1.3	A1.2	A1.4	A1.9
10.4	10.5	10.3	9.8 ✓
70	60	50	40

A1.3	A1.2	A1.5	A2.7
13.4	13.5	13.2	12.5 ✓
70	60	50	40

A0.5	A0.7	A1.0	A1.3
14.2	14.0	13.7	13.4 ✓
70	60	50	40

A0.5	A0.7	A0.8
16.0	15.8	15.7 ✓
70	60	50

A1.6	A1.4	A1.6 ✓
14.9	15.1	14.9
70	60	50

Sta + Δ - Elev.

956.46

45

+50

46

+45

+90

A7

BM 6.34 956.45 6.34 950.12 (950.11)

1-14-69

E

X-68

Lt

42.0
~~44.0~~ 96
 4.5
 12.5
 70

42.0
 14.5
 60

41.9
 14.6
 50

✓

43.0
 13.5
 70

42.3
 14.2
 60

42.7
 13.8
 50

✓

42.3
 14.2
 70

42.0
 14.5
 60

41.5
 15.0
 50

✓

41.9
 14.6
 70

41.9
 14.6
 60

41.7
 14.8
 50

✓

42.3
 14.2
 70

42.8
 13.7
 60

43.1
 13.4
 50

✓

43.3
 13.2
 70

43.7
 12.8
 60

44.1
 12.4
 50

✓

Top Flat Iron Connector S.E. Corner #132 of Power
 Line Tower

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		956.45		
--	--	--------	--	--

47+14				
-------	--	--	--	--

+35				
-----	--	--	--	--

+50				
-----	--	--	--	--

+70				
-----	--	--	--	--

48				
----	--	--	--	--

BM	8.49	958.61	6.34	950.12
----	------	--------	------	--------

+50				
-----	--	--	--	--

FK
JA
CM

Lt.

1-14-69
1-1569
~~F~~

X-69

43.9	44.0	45.4	
12.6	12.5	11.1	✓
70	60	50	

44.7	47.1	50.2	
11.8	9.4	6.3	✓
70	60	50	

45.5	48.0	50.7	
11.0	8.5	5.8	✓
70	60	50	

47.3	50.9	51.7	
9.2	5.6	4.8	✓
70	60	50	

52.0	52.2	52.3	
4.5	4.3	4.2	✓
70	60	50	

52.5	52.8	52.9	
6.1	5.8	5.7	✓
70	60	50	

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		958.61		
--	--	--------	--	--

49				
----	--	--	--	--

+50				
-----	--	--	--	--

+59.59	P.T.			
--------	------	--	--	--

50				
----	--	--	--	--

+50				
-----	--	--	--	--

51				
----	--	--	--	--

0.69	958.18	1.12	957.49	
------	--------	------	--------	--

+24				
-----	--	--	--	--

1-15-69

Lt

£

X-70

49.9

49.7

49.5

8.7

8.9

9.1 ✓

70

60

50

49.3

49.2

49.2 ✓

9.3

9.4

9.4 ✓

70

60

50

53.6

53.2

53.0 ✓

5.0

5.4

5.6

70

60

50

53.7

53.6

53.7

4.9

5.0

4.9 ✓

70

60

50

~~3~~
~~54.9~~~~3~~
~~54.9~~~~3~~
~~54.8~~

4.6

4.6

4.7 ✓

70

60

50

~~Dispatch Post~~~~53.7~~~~54.2~~~~54.7~~ ✓

5.8

5.3

4.9 ✓

70

60

50

958.18

51+37

+67

52

TP 1.49 951.95 7.72 950.46

+16

+30

+58

1-15-69

17

£

X-71

50.8 51.8 52.5

7.4 6.4 5.7 ✓

70 60 50

48.8 49.4 50.2

9.4 8.8 8.0 ✓

70 60 50

46.4 46.8 47.8

11.8 11.4 10.4 ✓

70 60 50

Spike in Transformer Power Pole

45.5 46.0

6.5 6.0 ✓

70 60

44.6 45.3 ✓

7.4 6.7 ✓

70 60

43.2 43.9 ✓

8.8 8.1

70 60

Sta	+	π	-	Elev.
		951.95		
53+00				
+33				
+80				
54				
+25				
+45				

1-15-69

X-72

40.3

41.4

11.7

10.6

70

60

39.3

40.3

12.7

11.7

70

60

40.1

41.1

11.9

10.3

70

60

41.5

42.8

10.5

9.2

70

60

43.6

46.1

8.4

5.9

70

60

39.6

40.3

12.4

11.7

70

60

Sta + π - Elev.

951.95

54+55

+62

+774 $\pm$ D

$\pm$ old D + WBA 4.87 947.08 47.1 ✓

Pavement $\pm$ old D + WBA 5.07 946.88

1-15-69

L

X-73

Lt.

~~40.0~~~~40.4~~~~12.0~~~~11.6~~~~70~~~~60~~

43.3

43.8

44.5

8.7

8.2

7.5 ✓

100

80

60

43.8

44.5

45.2 ✓

8.2

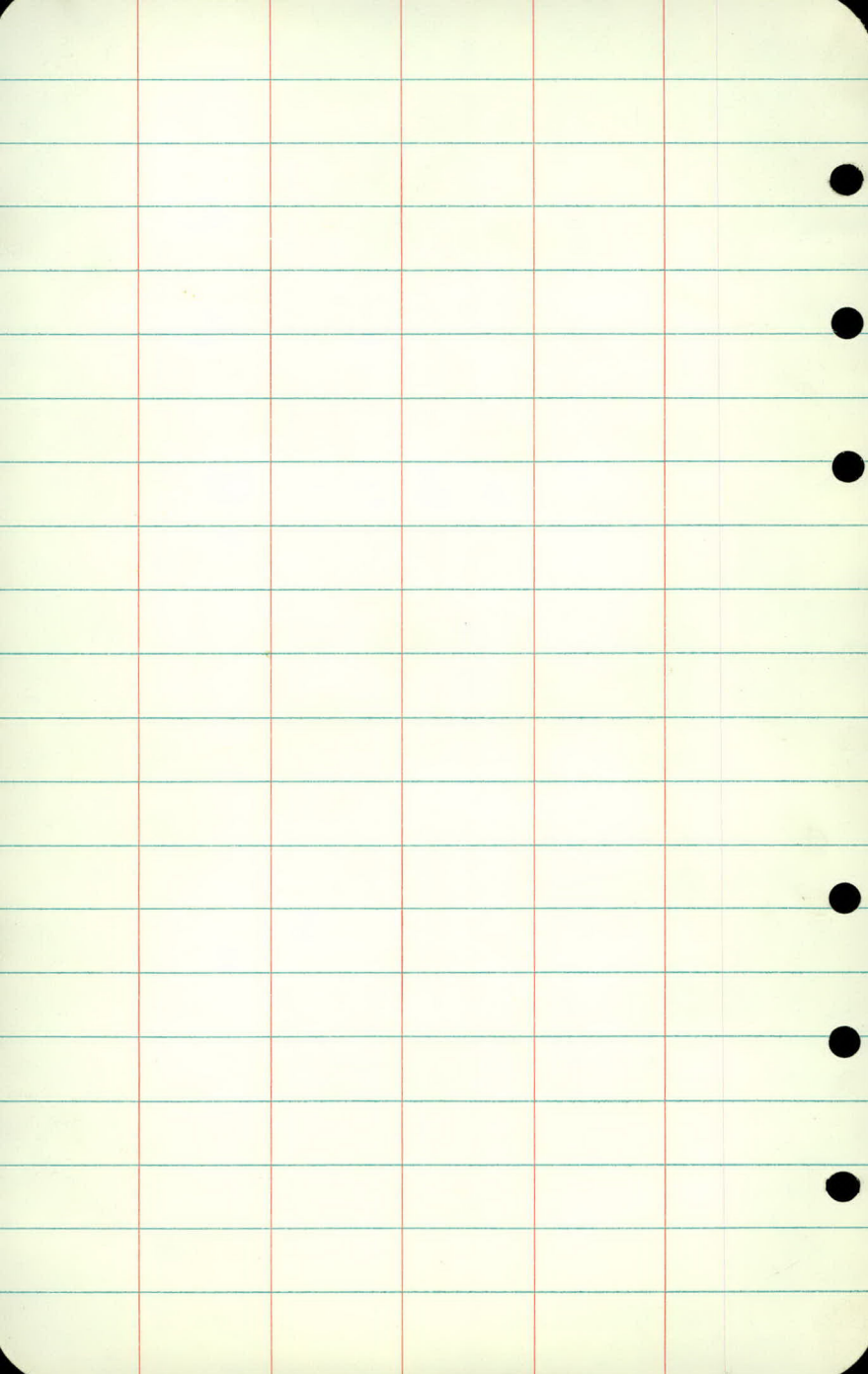
7.5

6.8

100

80

60



Dec. 19, 1968 X-74

Distances Left to New
CENTERLINE
from Σ of X-Section Σ

Sta.	Distance Left
26+71	0.18
27	0.44
+50	0.88
28	1.32
+44	1.71
+78	2.01
29	2.21
+45	2.5
+73	3.1
30	3.7
+50	5.25
31	7.63
+50	10.25
32	12.87
+50	15.48
33	18.09
+50	20.71
34	23.32
+50	25.94

FR
WS
LPD
GA
CM

Dec. 27, 1968

x-75

35

28.55

+50

31.16

36

33.78

+50

36.39

37

39.05

+50

41.05

+76

+92

38

41.60

+13

+25

+50

42.05

+60

39

42.40

+50

42.90 ✓

40

42.76 ✓

+50

42.98

41

43.23

+50

43.09

42

42.37

+50

40.50

Sta	Distance Left
43	38.33
+44	36.40
+83	34.70
44	33.96
+38	32.29
+70	30.90
45	29.58
+50	27.40
46	25.21
+45	24.08
+50	23.92
+90	23.58
47	23.50
+14	23.56
+35	23.65
+50	23.72
+70	23.84
48	24.02
+50	24.40
49	24.82
+50	25.08
50	25.12
+50	24.04
51	22.95

FK
WS
GA
CM

Dec 30, 1968

X-76

Distance Left.

51+24

22.43

+37

22.15

+67

21.50

52

20.78 ✓

+16

20.44

+30

20.14

+58

19.53

53

18.61

+33

17.89

+80

16.87

54

16.44

+25

15.90

+45

15.47

+55

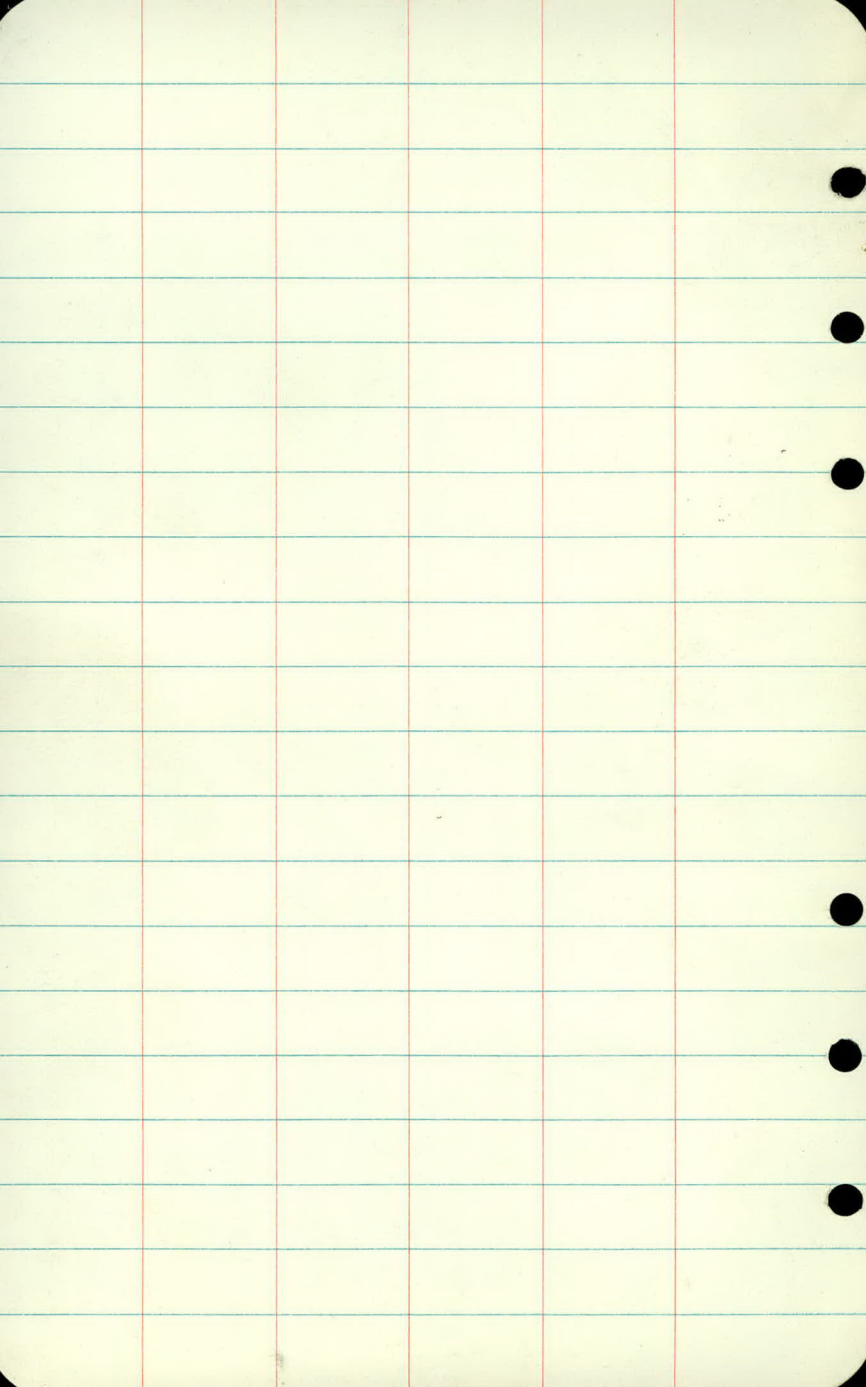
15.25

+62

15.10

+77.4 E D

14.78



X-77¹

White Bear Ave

62-665-08

County Road "C" profile

Sta	+	Δ	-	Elev.
BM	1.32	930.25 931.91		928.93 930.59

10			2.90	927.35 929.01
----	--	--	------	------------------

9+50			3.49	926.76 928.42
------	--	--	------	------------------

9			4.30	925.95 927.61
---	--	--	------	------------------

8+50			4.89	925.36 927.02
------	--	--	------	------------------

8			5.65	924.60 926.26
---	--	--	------	------------------

+50			6.5	923.75 925.4
-----	--	--	-----	-----------------

7			6.9	923.35 925.0
6+96	MH		2.02	923.23 924.89

6+50			7.6	922.65 924.31
6+60	26	L+	9.8	920.95 922.1

6			7.8	922.45 924.1
---	--	--	-----	-----------------

Jan. 22, 1969

X-2.78

Top Hyd N.W. Corner W.B. Ave & "C"

5+28 Double ent Lt

5+70 Hyd Lt

6+45 Ent Lt

7+10 Ent Lt,

7+31 Ent Rt

21.75
8.5
30

20.85
9.4
25

15.5
14.7
44

Sta	+	Σ	-	Elev
		930.25		
		931.91		

5+50

8.0

922.25
923.9

5

8.4

921.85
923.5

4+50

9.0

921.25
922.9

+23

9.47

920.78
922.44

4

9.89

920.36
922.02

BM

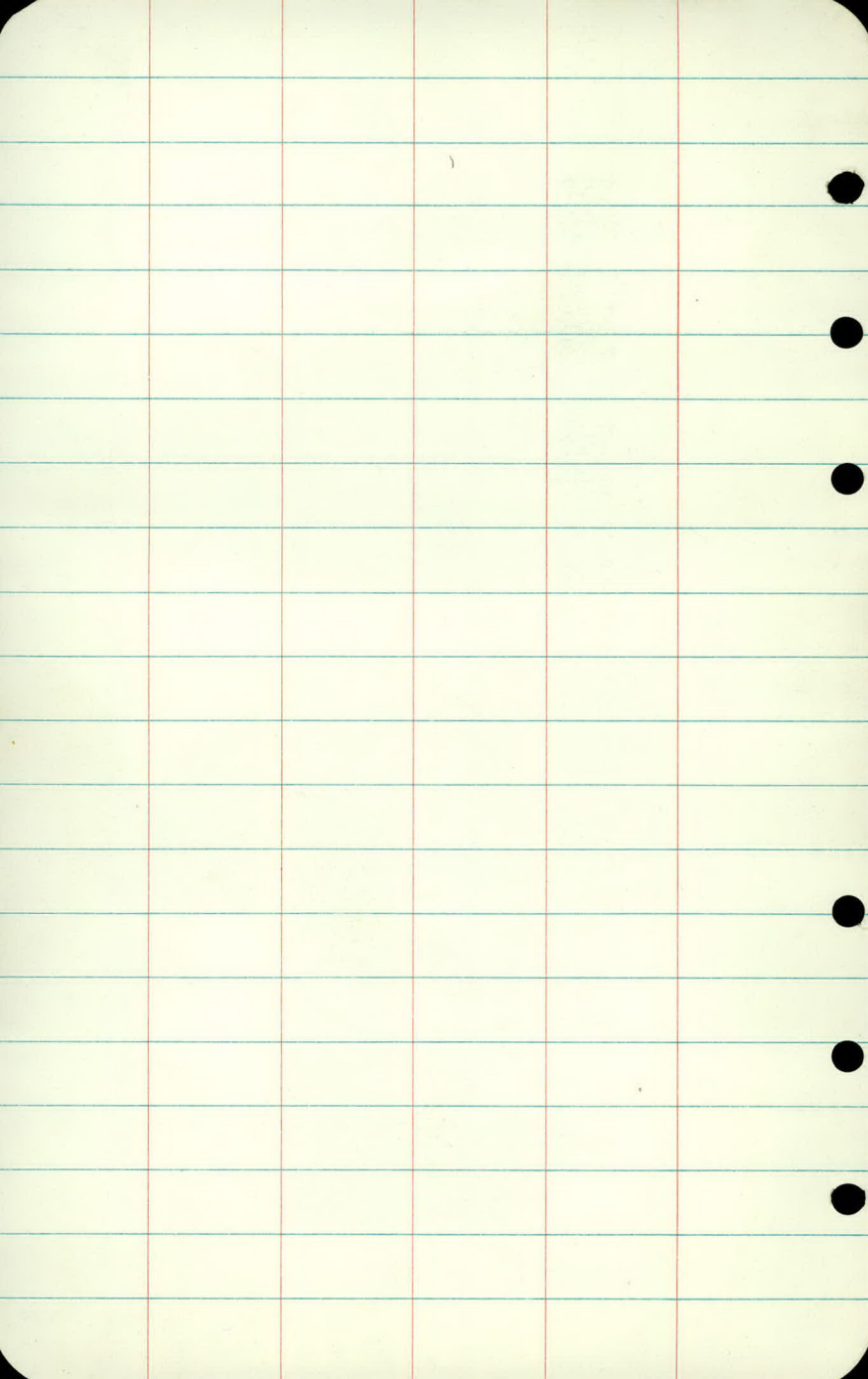
6.21

924.04
925.70

Jan 22, 1969

X-³79

Top Hyd Lt Sta 5+70



1-27-69 X-80
1

White Bear Ave.

X-section Extention

STA + $\bar{\Delta}$ - ELEV

BM 1 5.05 932.67

927.67

5414

5.31 927.36

BM 13.18 950.92

937.74

9.9 941.02

9.86 941.05
911.06

M.H.

8.78 942.14

FK
GA
JA

1-27-69

X-81

Nail P.P.

22.2
10.51
75

21.4
11.31
99

21.2
11.73
130

Nail P.P. 26+40 OR SO.

9.6
14

9.7
23

11.5
30

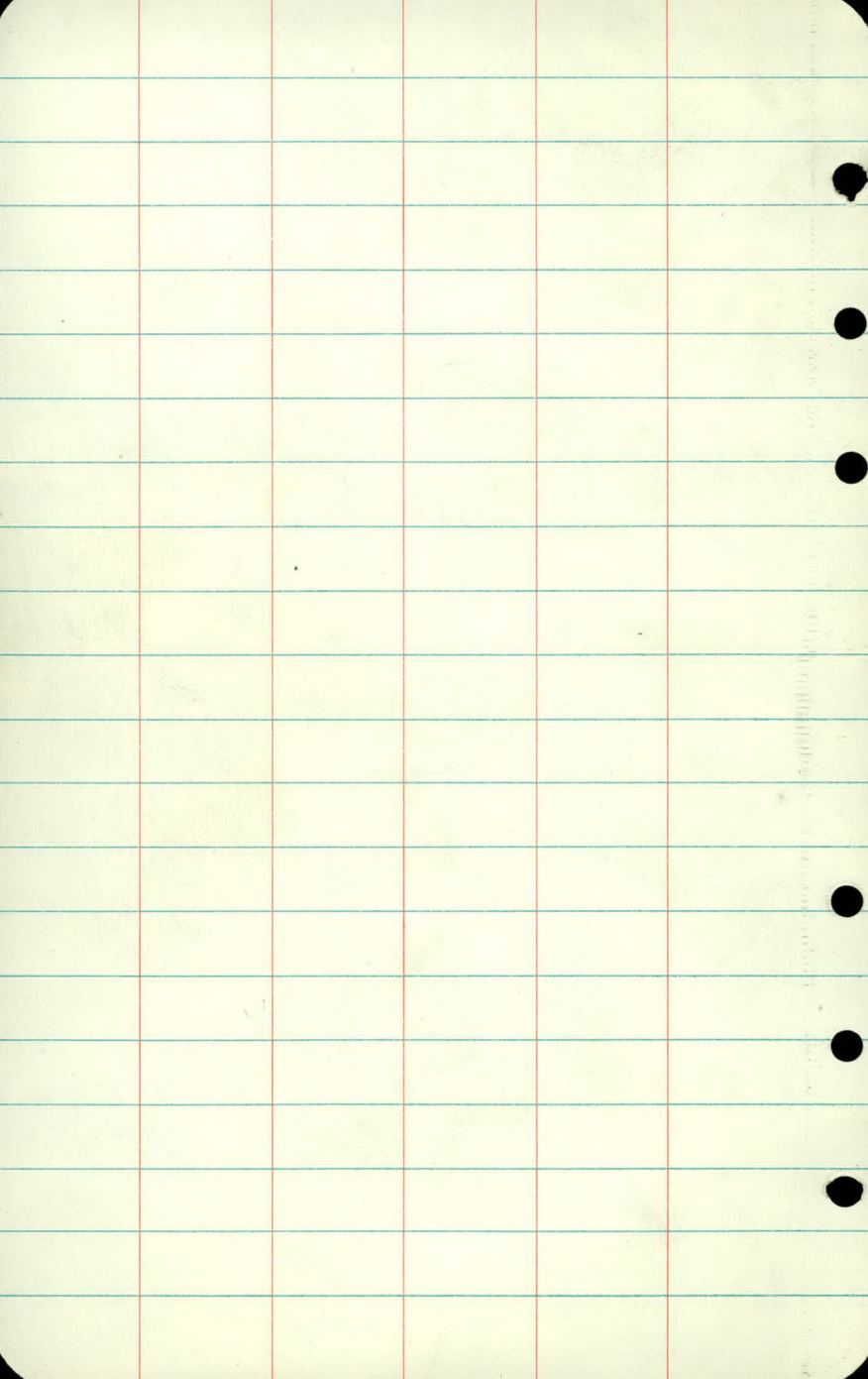
9.1
35

4.4
46

7.3
70

STA 30 P.K.

STA 33+10 M.H.



FK
JA
CM

3-20-69

1

Ditch Location
and
Elevation

62-665-08

Obj	Az	stadia	Red	Elev
π 135' Left of Station 8 + 57 To 13.5' Left Sta 0+00				
H. I. 932.0				
8+00	166°50'	58'	4.40	927.6
Top Pipe	205°35'	33'	11.65	20.35
Ditch	225°-	45'	13.6	18.4
"	236°15'	65'	14.0	18.0
"	240°45'	81'	14.3	17.7
"	243°15'	97'	14.6	17.4
"	246°45'	112'	14.7	17.3
Ditch	94°-	44	13.8	18.2
"	77°45'	53	14.0	18.0
"	69°40'	74	13.7	18.3
"	66°	90	14.0	18.0
	62°25'	116	13.6	18.4
	61°-	138	13.5	18.5
Angle in Ditch	59°30'	160	13.3	18.7
	62°45'	194	12.7	19.3

3-20-69

2

