

DR. 9 Bx 99

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

OWASSO BLVD. NO.

From OWASSO ST. To Chandler Ave.

Road Acc't. No. 18

Date Filed _____

File _____

1965-1966

Dec. 6, 1965

OWASSO BLVD. NORTH

Arbogast to
Chandler Drive

New Alinement
1965

Not Constructed

INDEX	PAGE
Alignment	1-12
	13-22
Topography	70-86
	26-67
X Sections	
	23-25
Bench Levels	101-105
West Owasso Blvd	88-91

Dec. 12-13-65

Sta Point Δ Lt. Δ Rt.

64+20.41 P.T. $18^{\circ}08'$

64 $16^{\circ}54.5'$

+75 $15^{\circ}24.5'$

$\Delta = 36^{\circ}16'$

+50 $13^{\circ}54.5'$

$\frac{1}{2}\Delta = 18^{\circ}08'$

+25 $12^{\circ}24.5'$

$D = 12^{\circ}$

63 $10^{\circ}54.5'$

$T = 156.36'$

+75 $9^{\circ}24.5'$

$L = 302.22'$

62+74.55 P.I. $36^{\circ}16'$

$R = 477.46$

+50 $2^{\circ}54.5'$

+25 $6^{\circ}24.5'$

62 $4^{\circ}54.5'$

+75 $3^{\circ}24.5'$

+50 $1^{\circ}54.5'$

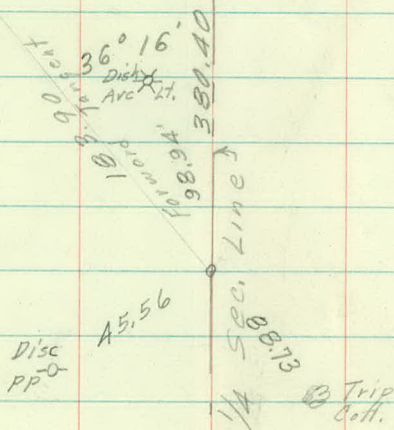
+25 $0^{\circ}24.5''$

61+18.19 P.C. $0^{\circ}00'$

Dec. 6, 1965

2
2

W $\frac{1}{4}$ Cor. $\square$ Sec. 36



P.K. nail

Sta Point Δ Lt. Δ Rt.

+05.45 P.T. $9^{\circ} 27'$

66 $9^{\circ} 07.4'$

+75 $7^{\circ} 37.4' \Delta = 18^{\circ} 54'$

+50 $6^{\circ} 07.4' \frac{1}{2} \Delta = 9^{\circ} 27'$

65+27.42 P.I. $18^{\circ} 54' \cdot D = 12^{\circ}$

+25 $4^{\circ} 37.4' T = 79.47'$

65 $3^{\circ} 07.4' L = 157.50'$

+75 $1^{\circ} 37.4' R = 477.46'$

64+47.95 P.C. $0^{\circ} 00'$

FK
LPD
ML

Dec. 3, 1963

3
3

Disk
pp-o

99.88

spike

Al. 17

Disk
pp-o
With Transformer

Sta Point ΔL ΔR

68+65.33 P.T. $11^{\circ}17'15''$

+50 $10^{\circ}35.9'$

+25 $9^{\circ}28.4'$

68 $8^{\circ}20.9'$

+75 $7^{\circ}13.4' \Delta = 22^{\circ}34'30''$

+50 $6^{\circ}05.9' \frac{1}{2}\Delta = 11^{\circ}17'15''$

67+41.55 P.I. "A" Line $22^{\circ}34\frac{1}{2}' D = 9^{\circ}$

+25 $4^{\circ}58.4' T = 127.06'$

67+01.55 P.O.S.T. $L = 250.835'$

67 $3^{\circ}50.9' R = 636.62'$

+75 $2^{\circ}43.4'$

+50 $1^{\circ}35.9'$

+25 $0^{\circ}28.4'$

66+14.49 PC $0^{\circ}00'$

66+09.37 P.T.
0/0

65+51.69 P.I. $29^{\circ}46'$

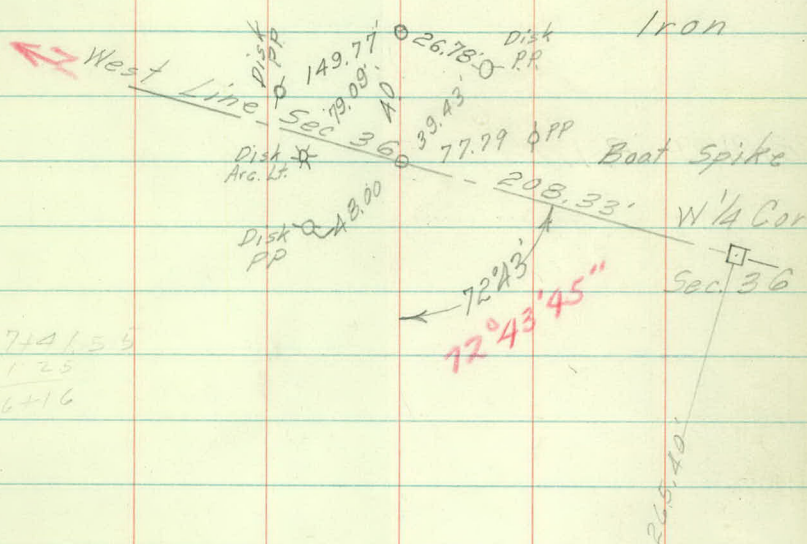
(1937 Survey)

OK for Line "A"
see Page 6
for Line "B"
Changed

FK
LPD
ML

12-2-65
Clear 40°

4
4



6741.55
1.25
66+16

Sta 65+27.42 P.I.

115' - old P.O.T.
to New
P.I.

Sta Point ΔL ΔR

78+91.39 P.I.
= 79+27.85 P.I. = 1937 Survey

$15^{\circ}22'30''$

$\Delta = 15^{\circ}22'30''$

$\frac{1}{2}\Delta = 7^{\circ}41'15''$

$D = 3^{\circ}$

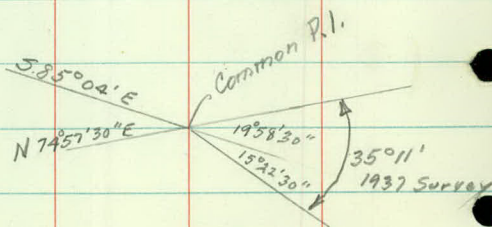
$T = 257.80$

$L = 512.36$

$R = 1909.86$

R. Clark

From Lat. & Dep. Sheet.



FK
LPD
ML

Dec. 3, 1965
Cloudy Windy 36°

5
5

"B" Line
Sta Point ΔL ΔR

+50.76 P.T. $9^{\circ}53.7'$ $9^{\circ}55.75'$
2.05

+25 $8^{\circ}46.2'$

68 $7^{\circ}38.7\Delta = 19^{\circ}51'30'' R$

+75 $6^{\circ}31.2\frac{1}{2}\Delta = 9^{\circ}55'45''$

+50 $5^{\circ}23.7' D = 9^{\circ} \text{ Arc}$

67+41.55 P.I. $T = 111.44$

+25 $4^{\circ}16.2' L = 220.65$

67 $3^{\circ}08.7 R = 636.62$

+75 $2^{\circ}01.2'$

+50 $0^{\circ}53.7'$

66+30.11 P.C. $0^{\circ}00'$

March 31, 1966
April 1, 1966

6
6

from

Ties on page 4

Sta Point ΔL ΔR

✓ +88.99 P.T.	12° 25' 15"	540.87
+50	11° 15' 07"	
80	9° 45'	
+50	8° 15' $\Delta = 24° 50' 30"$	
79	6° 45' $\frac{1}{2}\Delta = 12° 25' 15"$	
78+85.28 P. I.	D = $\frac{6^\circ \text{Arc}}{4^\circ \text{Arc}} = 210.32$	
76+74.96	5° 15' T = 315.48	
78	3° 45' L = 621.04	
+50	2° 15' R = 1432.40	
77	0° 45' 07"	
✓ 76+74.96 P.C.	0° 00'	

3/100
130/50

FK
DS
PK
WJ

March 31, 1966

7
7

→ Z

Disk
A" Ash

19.72'
P.I.

18" line

Disk
7" Oak

37.94'

63.04'

Disk
PP
Up 7'

Iron

55'

P.I. 78+91.39

81°

Sta. Point ΔL ΔR

38+56.67 P.I.

+55.29 P.T. $14^{\circ}27'37.5''$

+50 $14^{\circ}18'09.6''$

86 $12^{\circ}48'$

+50 $11^{\circ}18'$

85 $9^{\circ}48'$

$\Delta = 28^{\circ}55'15''$

+50 $8^{\circ}18'$

$\frac{1}{2}\Delta = 14^{\circ}27'37.5''$

34+19.54 P.I.

$D = 5^{\circ}$ Arc
246.26'

84 $6^{\circ}48'$

$T = 295.51$
482.01

+50 $5^{\circ}18'$

$L = 578.42'$

83 $3^{\circ}48'$

$R = 1145.92'$

+50 $2^{\circ}18'$

82 $0^{\circ}48'09.6''$

31+73.28 P.C. $0^{\circ}00'$.616

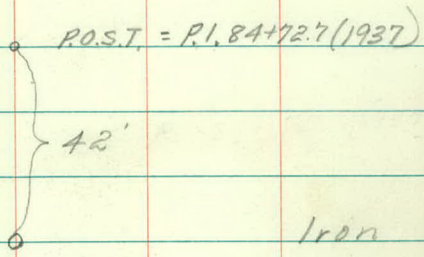
FK
PK
WJ

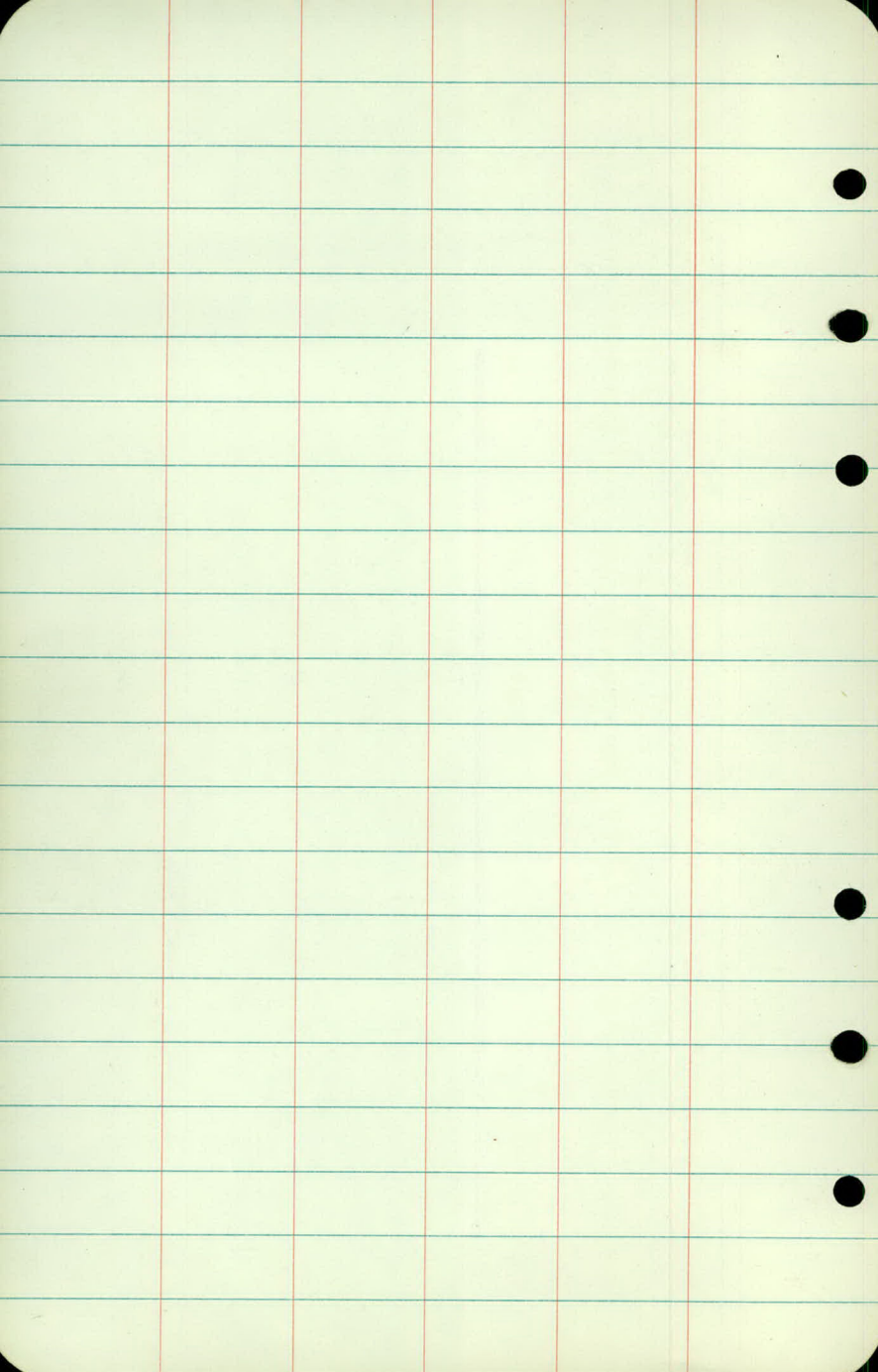
April 1, 1966
April 4, 1966

8
8

Sta 88+70.75
1937 Survey

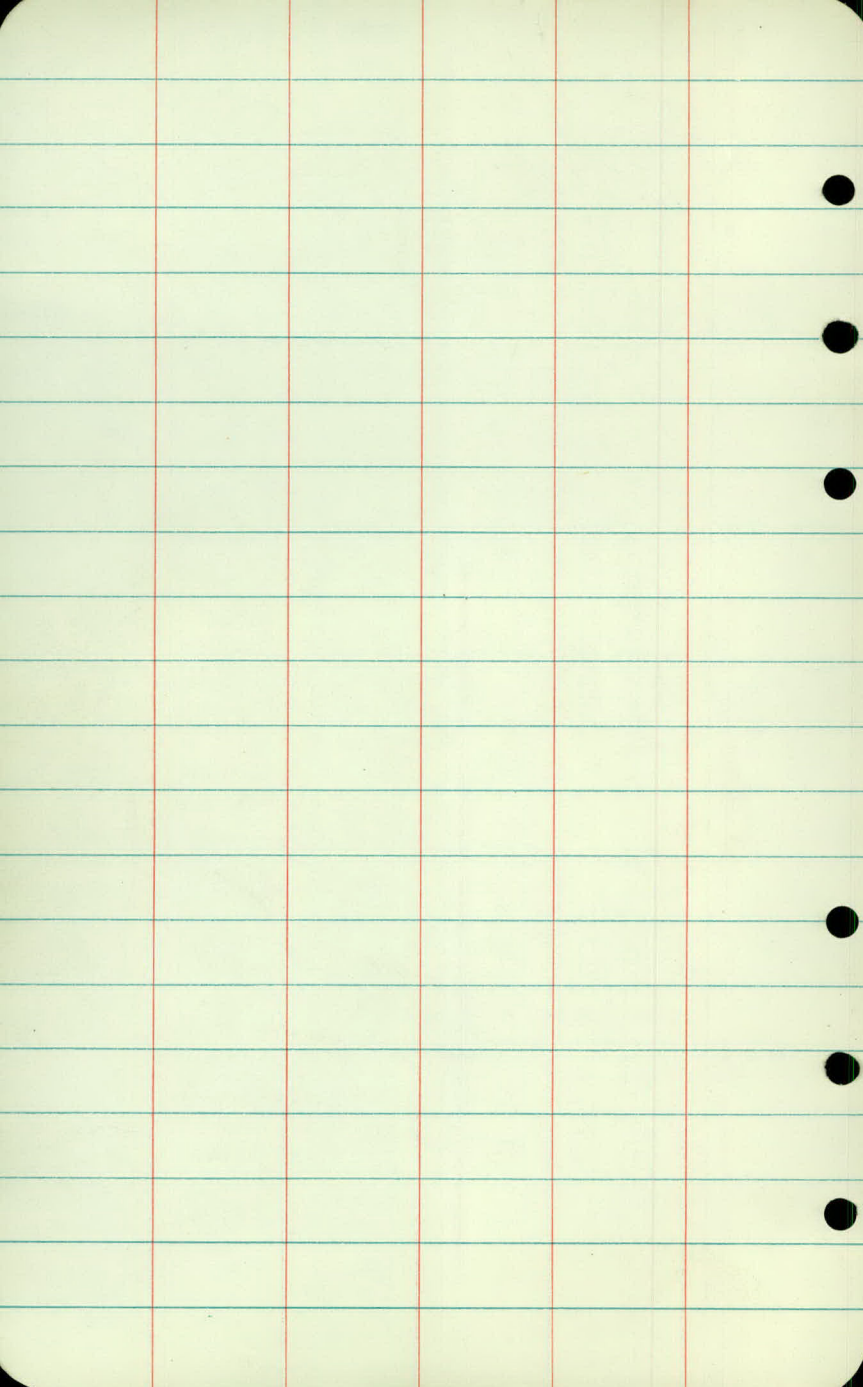
• P.K. Nail at P.I.





OWASSO BLVD. NORTH

Received March 11, 1966



March 11, 1966

10

92 43
72 43 ³/₄

290 35
28 12
10 175
8 16
15
12
3

61 22
245 28.5
24 88.5
5
4
1

89 53
359 32
32 18
39 212
36 20
12

P.I.

Dale St Boat Spike

W 1/4 Cor.
36-30-23

61° 22' 07"

89° 53'

72° 43' 45"

161° 05' 15"

Make 161° 05' 45"

161 05

184 21
360
11

2 464 21

284 21 161 05' 15"

360
4 644 21
4
29
29 4

36° 17' 30"

Arbogast St.

89° 53'

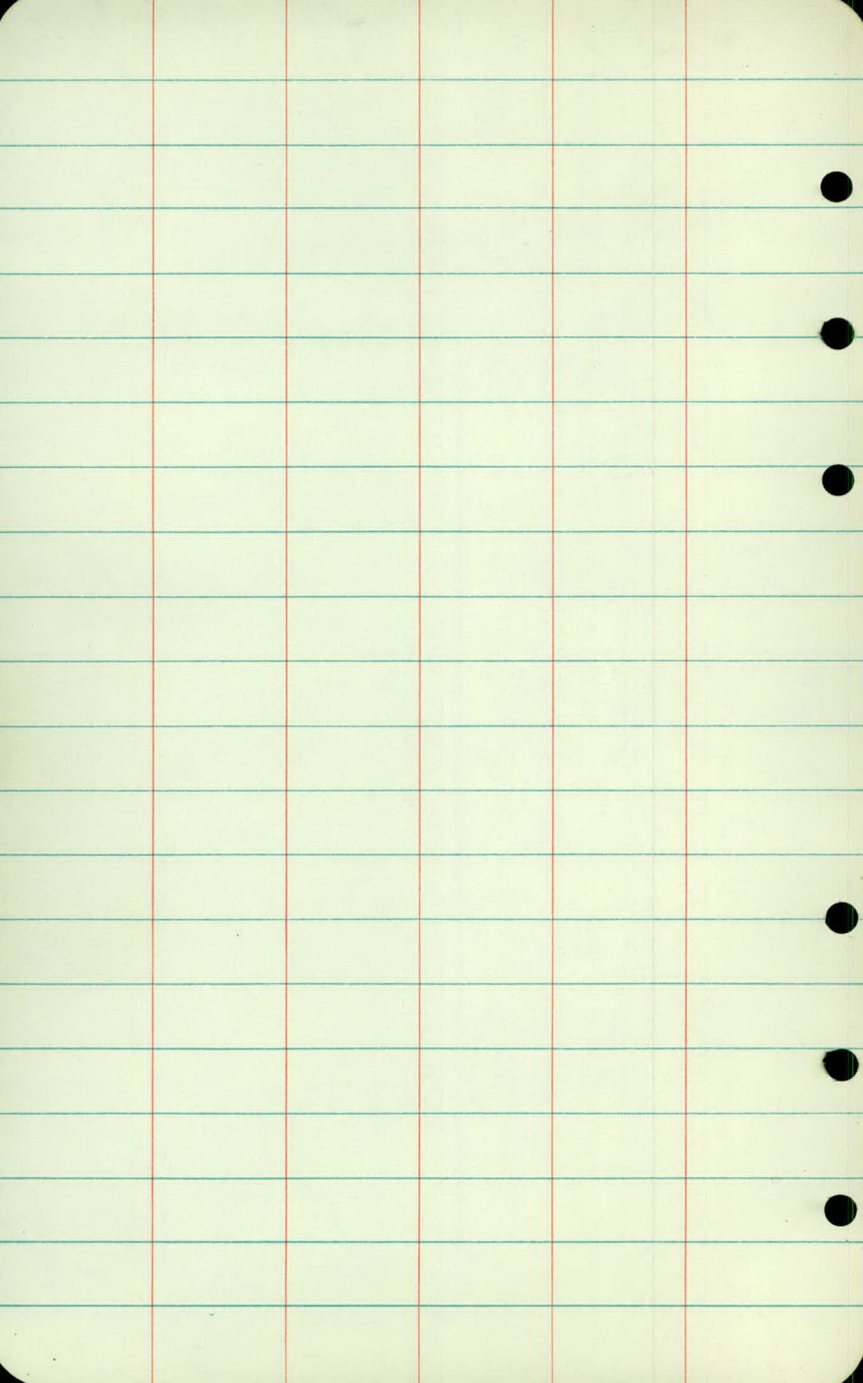
36° 17' 30"

72° 43' 45"

161° 05' 15" 45

358° 118 90"

359° 59' 30"



FK
LPD
WJ

Feb 28, 1966

//
/

182 23
360
 542° 23

183.33
360
 543 33

24.50

90° 24'

90 22

6 542 23

54

0143

12

13

12

N

↑

↑

↑

↑

↑

↑

↑

↑

↑

↑

↑

↑

↑

↑

↑

↑

90° 35' 1/2"

9 343

6 543 33

54 180

219

18

33

30

30

90° 22'

90° 35' 1/2"

65.15

46'

136.30"

89° 82'

90° 22'

32

89° 50'

90° 35' 30"

32

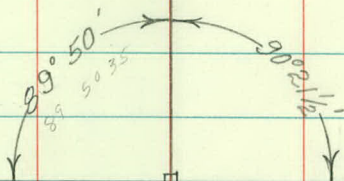
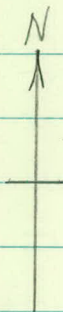
90° 67' 30"

46

90° 21' 30"

Feb. 28, 1966

12
2



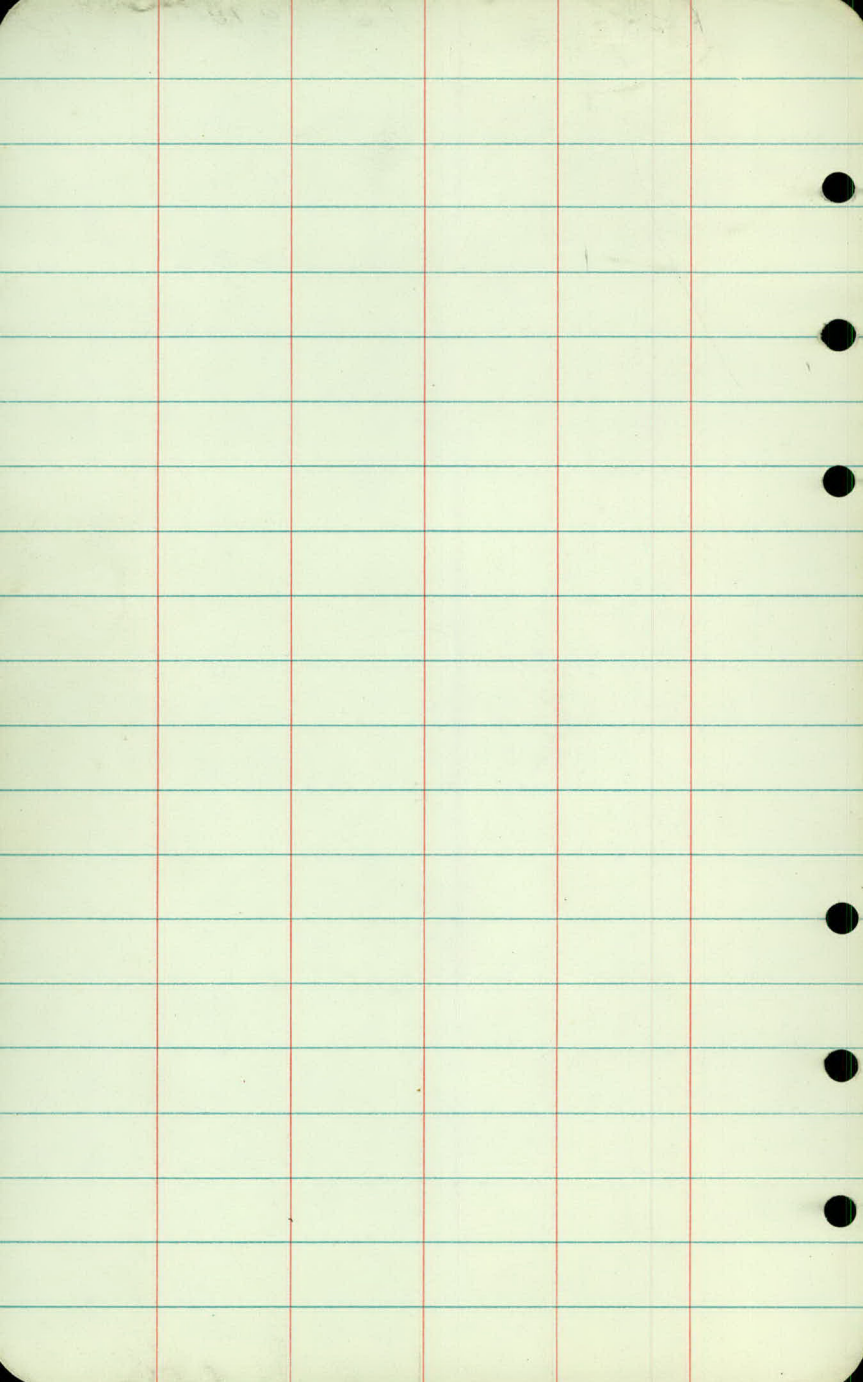
W 1/4 Cor.

Sec. 36 - 30 - 23

90° 06'
10-21-37

89° 38'
10-21-37

90	06	
89	50	
89	38	
90	21	30
358	115	30



RB
RB
LPD

Feb 9, 1966 13
cloudy 48°
T-1

TOPOGRAPHY
OF
OWASSO BLYD. NORTH
FROM
ARBOGAST TO CHANDLER DRIVE
(STA. 61+18.19 to STA. 78+91.39)
"A" Line

Lt.

Rt.
+50 BT
4-33

Rt.

PP
+43 13

+39 BT
0 28

10" C.H.
+09 42

62+00 +00 12" C.H.
32

9 19

12" C.H.
+13 38

8" C.H. (3)
+84 30

20" C.H. 8" C.H.
+81 37 +84 38

+75 BT
12 16

+50 B.T
14 14

PP
+21 28

+12 Ent(10') RT+09
W. end 12"x20" CH 24

+25 B.T
15 13

61+00 +02 24

15 14

60+00

RG
WM
FS
LPD

Feb 10, 1965

14

T-2

2

0

0

0

0

0

0

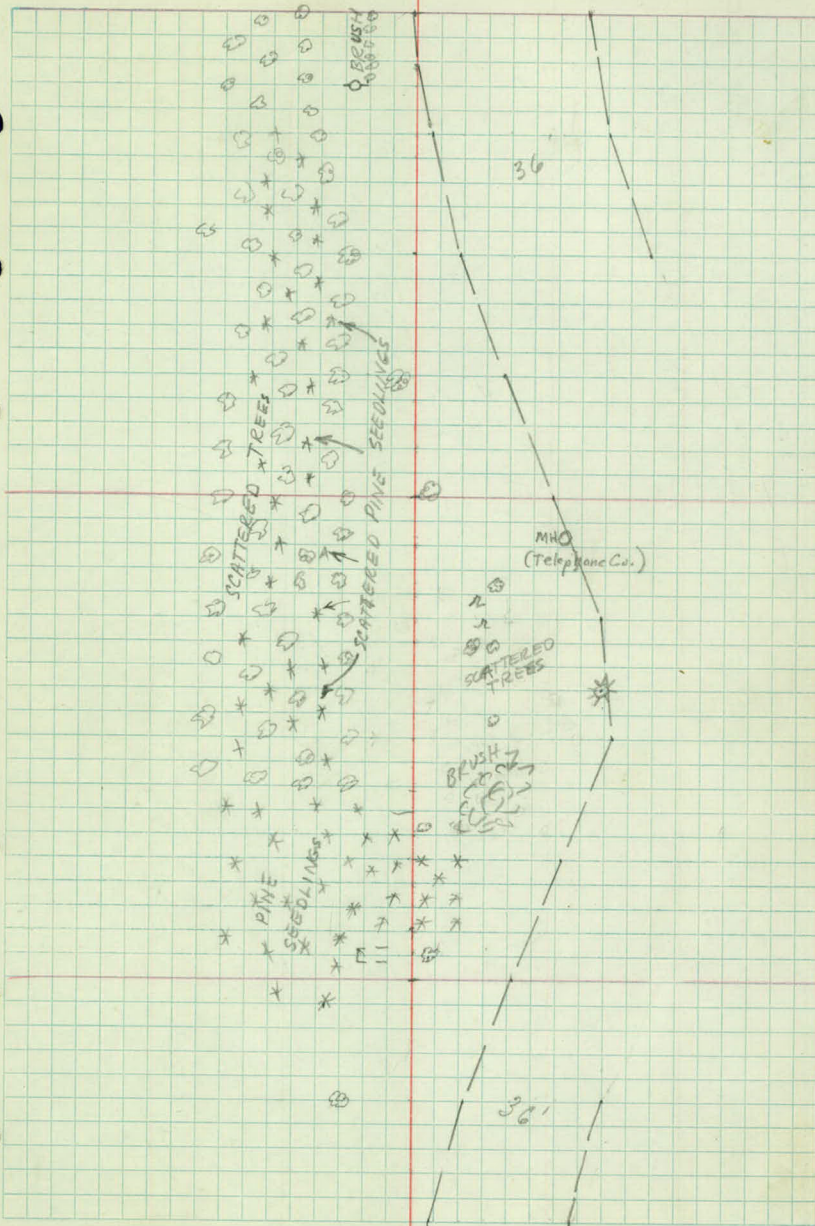
0
1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
52
53
54
55
56
57
58
59
60
61
62
63
64
65
66
67
68
69
70
71
72
73
74
75
76
77
78
79
80
81
82
83
84
85
86
87
88
89
90
91
92
93
94
95
96
97
98
99
100

65+00 Lt. P. Rt.
 +00 Brush 10-25 +00 Trees 25
 Brush +85 PP +89 BT
 12-23 14 2
 +75 Trees 20
 +75 BT 3-40
 +50 Trees 14
 +50 BT 9-48
 +25 Trees 15 +24 24" Cott. 4 +25 BT 18
 64+00 +00 Trees 13 +01 22" Cott. 2 +00 BT 29
 +75 Trees 13 +73 Bell Telep. Mt. 31
 +79 51P 13 +83 18" Oak 16
 +75 ER 39 +70 End Trees 13
 +60 40 40 +74 51P 15
 +39 Scattered Trees 0-75 +39 Trees 2 +50 POR 42 +50 Trees 10
 +30 Pine Seedlings 4 +31 Beg. Scattered Sm. Cott. 1-20
 +25 BTR 32
 +06 4" Cott. 3 +12 to +25 scattered Pine seedlings 2-10'
 63+00 +06 N. end 24" RCP x 88' +00 BT 22'
 +94 Beg Small Pine Seedlings 18
 +75 3" Oak 15 +75 BT 11-40
 +62 S. end 24" RCP 66
 BT 4-33

Feb 10, 1965

15
7-3

2



Lt

E

Rt

$$+50 \frac{BT}{36-79}$$

$$+36 \frac{PP}{79}$$

$$+25 \frac{ER}{19} +25 \frac{BT}{63}$$

$$\frac{POR}{10}$$

$$67+00$$

$$+00 \frac{BIR}{50}$$

$$+00 \frac{POR}{29}$$

$$+00 \frac{PP}{69}$$

$$+04 \frac{CorrEnt}{46}$$

$$+94 \frac{EdgeEnt}{69}$$

$$+82 \frac{ER}{55} +86 \frac{E Dalest}{34} Rt+78$$

$$+69 \frac{End Trees}{61} +71 \frac{stop sign}{49}$$

$$+67 \frac{POR}{34} +67 \frac{Arc Lt}{41}$$

$$+40 \frac{BIR}{16} +69 \frac{End Brush}{61}$$

$$+40 \frac{BR}{23} +50 \frac{ER}{37}$$

$$+42 \frac{SE Cor Conc. TP}{30} +43 \frac{Telep MH}{17}$$

$$+19 \frac{TP}{37} +33 \frac{SW Cor Conc.}{28}$$

$$66+00 \quad +00 \frac{Trees}{45} \quad BT \quad 18 \quad 22$$

$$+00 \frac{Brush}{35-45}$$

$$+50 \frac{Trees}{37} +50 \frac{Brush}{25-37} \quad BT \quad +50 \quad 15 \quad 23$$

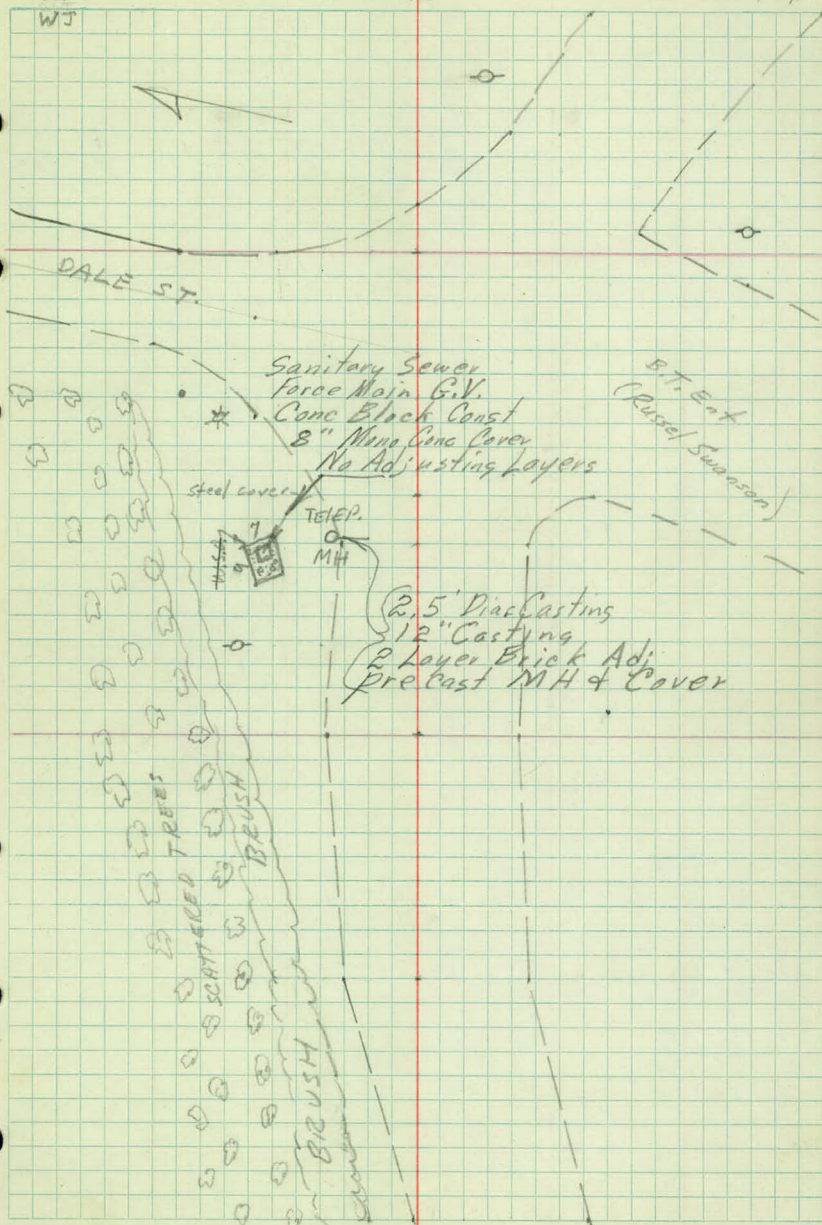
$$65+00$$

$$1 \quad 36$$

L^o

16
T-4

WT



70+00

Lt

L

Rt

$$+98 \frac{12''0}{4}$$

$$\begin{array}{r}
 +84 \frac{12''0ak}{44} +91 \frac{5''0.}{46} +93 \frac{12''0}{39} \\
 +68 \frac{12''0ak}{42} +77 \frac{9''0ak}{43} \\
 +53 \frac{28}{10''0ak} \\
 +41 \frac{26}{10''0ak}
 \end{array}$$

$$+41 \frac{15''0ak}{42}$$

$$+27 \frac{20''0ak}{56}$$

69+00

$$+93 \frac{10''0ak}{30}$$

$$+51 \frac{8''0ak}{2}$$

$$+50 \frac{PP}{76} +50 \frac{BT}{90}$$

68+00

$$+00 \frac{BT}{67}$$

$$+95 \frac{BT}{51}$$

$$+50 \frac{BT}{36-79}$$

Feb 21, 1965

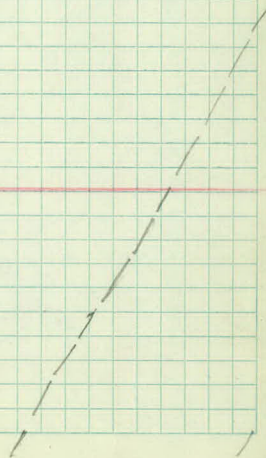
17

T-5

4
E

Uncultivated

Uncultivated



Lt.

£

Rt.

72+00

71+00

$$+10 \frac{\text{STP}}{2}$$

$$70+00 + 00 \frac{10''0}{24} + 04 \frac{12''0}{2}$$

$$\begin{array}{r}
 +31 \frac{22''0}{32} \\
 +21 \frac{12''0}{5} \\
 +11 \frac{\text{STP}}{23}
 \end{array}
 +
 \begin{array}{r}
 +28 \frac{\text{STP}}{12''0} \\
 +11 \frac{12''0}{31}
 \end{array}
 +
 \begin{array}{r}
 +15 \frac{10''0}{40}
 \end{array}$$

Feb 21, 1965

18

T-6

£

Uncultivated

Uncultivated



75+00

Lt.

$\frac{1}{2}$

Rt.

+64 $\frac{MH}{80}$

74+00

73+00

Feb 21, 1965

19

T-7

1/2



9" Cast
1 ring MH
over 14' to top

Uncultivated

Uncultivated

LT

Q

RT

$$+50 \frac{BT}{35}$$

77+00

$$+00 \frac{BT}{48}$$

$$+55 \frac{PP}{46}$$

$$+55 \frac{BT}{62}$$

76+00

$$+00 \frac{BT}{77}$$

$$+73 \frac{Tele. MH}{84}$$

$$+41 \frac{12" Oak}{41} \quad +47 \frac{10" BE}{38}$$

$$+13 \frac{5 BE 8"}{81}$$

$$+40 \frac{Nudge 30" X 55' SCP}{81} \quad RT+12$$

$$+25 \frac{PP}{75}$$

Edge Rd

$$+00 \frac{BT}{99}$$

75+00

R6
WM
DS

Feb 25, 1966
clear 15°

20

T-8

Lt

Rt

Rt

Uncultivated

Uncultivated

Temp.

M.H.

30" x 55" 50"

80+00

Lt

F

Rt

+96 $\frac{PP}{23}$

+83 $\frac{PP}{66}$

+50 $\frac{BT}{629}$ Fe 36

+15 $\frac{6" Oak}{37}$

+12 $\frac{5" BE}{28}$

+13 $\frac{6" BE}{28}$

+05 $\frac{PP}{5}$

+00 $\frac{BT}{10-41}$

+00 $\frac{Fe 5' chks.}{51}$

79+00

+00 $\frac{5" BE}{29}$

+89 $\frac{5" BE}{28}$

+91 $\frac{5" BE}{25}$

+78 $\frac{Two 7" BE}{27}$ +82 $\frac{4" BE}{25}$

78+00

+00 $\frac{BT}{23-58}$

+00 $\frac{Fe}{69}$

+80 $\frac{Arc Lt.}{79}$

77+50

+50 $\frac{BT}{35}$

Lt

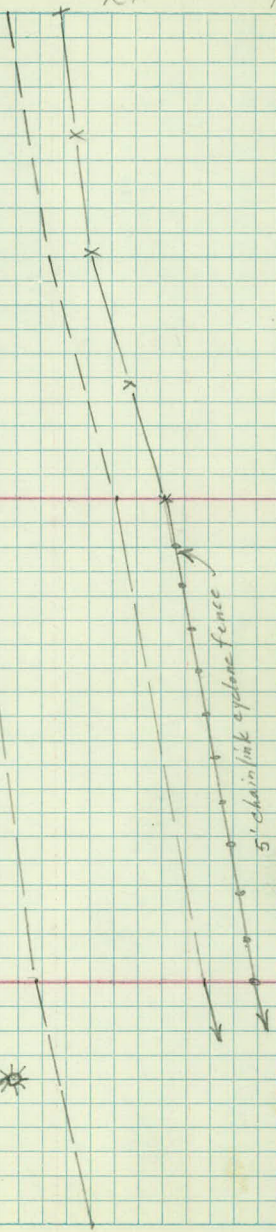
Q'

Rt

Q

Q

Uncultivated



BT	Fe
19 14	28

164	Ent
	Bit

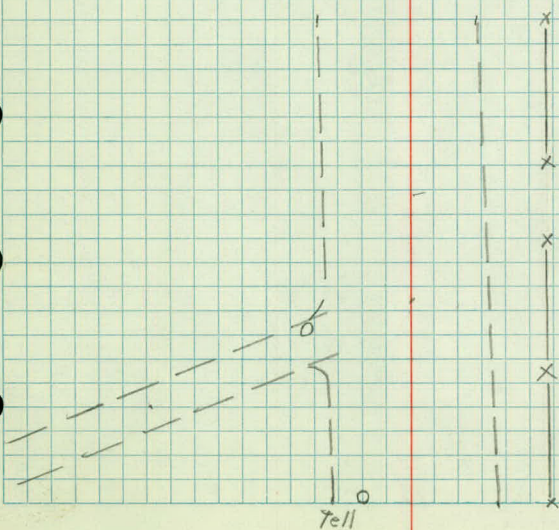
10'
2 Rd
+20 54

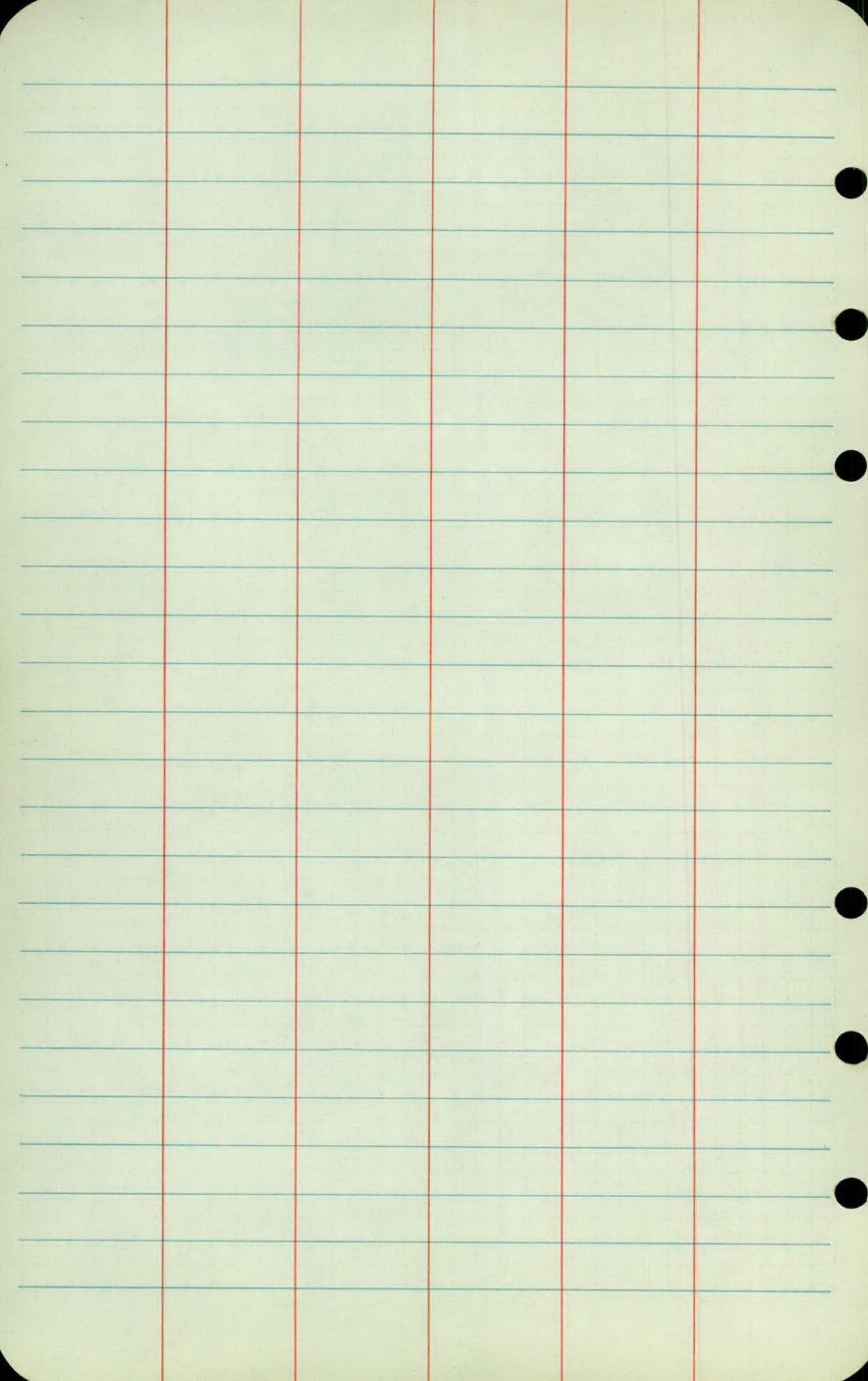
1A2	Blue
	Rd

+36	MH
22	

+35	28" Ash
68	

101	MH	Bit	Fe
10	16	18	29





Owasso Blvd. No.

Bench Levels

Sta	+	π	-	E/V.	
		937.10			<u>927.29</u>
BM ₁	9.81	937.53			927.72 ?
		.17		936.56	
TP	7.61	944.60	0.54	936.99	
		.15		940.65	
BM ₂	7.50	948.58	3.52	941.08	
		.27		.11	
TP	8.16	956.28	0.04	948.54	
		.55		.33	
BM ₃	0.22	954.98	1.94	954.76	
		943.58		.31	
TP	2.27	944.01	13.24	941.74	
		.24		929.89	
BM ₄	1.35	931.67	13.69	930.32	
		919.64		918.90	
TP	0.74	920.07	12.34	919.33	
		.33		907.57	
TP	0.76	908.76	12.07	908.00	
		898.88		.54	
BM ₅	1.34	899.31	10.79	897.97	
		897.69		891.74	
TP	5.95	898.12	7.14	892.14	
		900.02		894.52	
TP	5.50	900.45	3.17	894.95	
		.00		895.26	
BM ₆	4.74	900.43	4.76	895.69	<u>895.26</u>
		0.78		1.74	
TP	9.04	901.21	8.26	892.17	892.17
		10.68		.55	
BM ₇	13.13	911.11	3.23	897.98	897.97
		.43		07.58	
T.P.	11.85	919.86	3.10	908.01	908.00
		30.81		18.92	
T.P.	11.89	931.24	0.51	919.35	919.33
		43.64		29.91	
BM ₈	13.73	944.07	0.90	930.34	930.32
		54.71		.33	
TP	13.38	955.14	2.31	941.76	941.74

RG
WM
DS

Feb 25, 1966 24
Clear 20°-35°
14

Description

R.R.

Spk. in 24" Oak SW Cor. Arbogast $\frac{1}{2}$ Owasso St.

Spk. in Guy Pole SE Int. Arbogast $\frac{1}{2}$ Owasso Blvd No.

Spk. in Arc. Lt. Pole NW Cor. Dale $\frac{1}{2}$ Owasso Blvd. No.

Spk. in Arc. Lt. Pole N. of Int Owasso Hgts. Rd $\frac{1}{2}$ Owasso Blvd. No.

Top So. Rim MH 80' Rt Sta 74+64

Spk. in Arc. Lt. Pole 19' Rt Sta 77+80

Horseshoe Drive $\frac{1}{2}$ Owasso Blvd. No.

Spk. in R.P. used as Wabasso Lake Elev. Control B.M. ©

Sta	+	π	-	E/V.	
		954.71 955.14 54.97			
BM ₃	0.62	955.40	0.36	954.78 ..35	954.76
TP	2.61	947. 53 ^{.10}	10.48	944.92 ..49	
BM ₂	1.33	942. 46 ^{.03}	6.40	941.13 40.70	941.08
TP	2.51	935. 48 ^{.05}	9.49	932.97 ..54	
BM ₁			7.74	927. 71 ^{.31}	927.72

BM	6.20	901.46			(895.26)
T.P.	0.63	898.57	3.52	897.94	
BM			7.05	891.52	(891.51)

6.20 901.89 895.69

0.63 999.00 3.52 998.37

7.05 991.95 (891.51)

0.44 diff

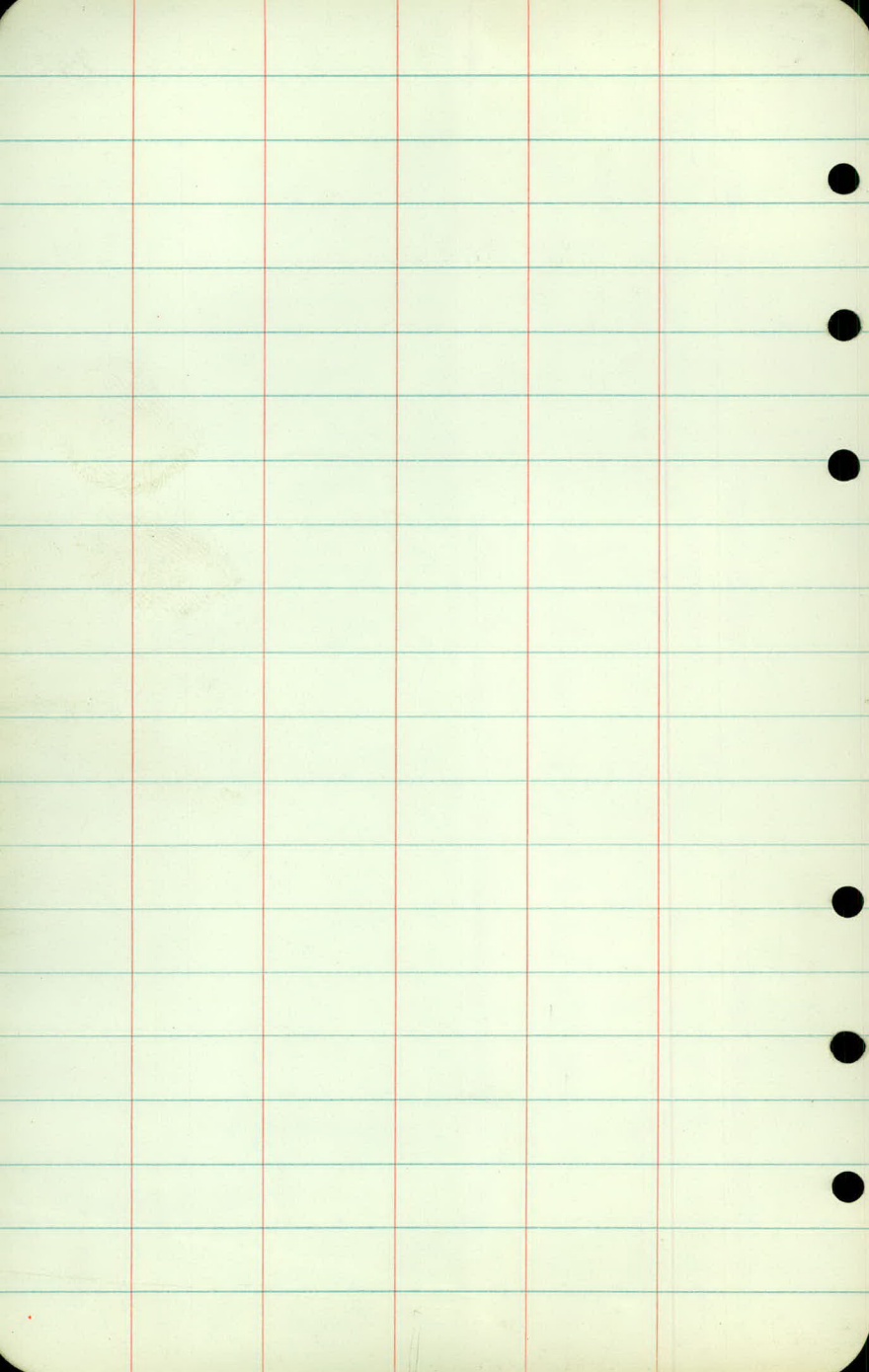
checked - R.B. 3-14-66

K6
wm
DS
RB

Description

Feb 25, 1966 25
Mar. 2, 1966
Overcast 34° 15

Spike in P.P. Lake Mabassa BM E. Horseshoe Drive & N.O. Blvd
& Door sill pump House Lake Okauchie



FX
WM
LPD

March 9, 1966

26
16

X-Sections

Sta	+	π	-	Elev
BM	9.39	36.68 937.11		927.29 927.72

8+80 59			7.3	29.8 ^{.4}
------------	--	--	-----	--------------------

+50 9+80 60			7.6	29.1 ^{.2}
-------------------	--	--	-----	--------------------

+50 10+50 61			6.7	30.0
--------------------	--	--	-----	------

+92

+12 Ent/Lt.

11+05

+25

✓

11+30

+50

March 9, 1966

27

Lt

♀

Rt

17

Owago St.

R.R. Spike in 24" Oak S.W. Co. Arbogast &

31.2 31.1	30.6 30.5	30.1 30.0	26.8 26.7	30.5 30.4	30.8 30.7	30.6 30.5	27.4 27.3	25.1 25.0	20.4 20.3
5.5	6.1	6.6	9.90	6.2	5.9	6.1	7.3	11.6	16.4
75	48	31	24	14		13	25	33	shore
FL15"CM									45

29.7 29.6	20.4 20.3	30.7 30.6	31.0 30.9	30.8 30.7	30.4 30.3	25.2 25.1	20.2 20.1
6.0	6.3	6.0	5.7	5.9	6.7	11.5	16.5
75	36	15		14	25	32	43

29.9 29.8	26.3 26.2	27.2 27.1	30.0 29.9	31.4 31.3	31.0 30.9	30.5 30.4	24.8 24.7	20.2 20.1
6.8	10.40	9.5	6.7	5.7	5.4	5.7	6.2	11.9
30	Onlv	23	19	13		14	24	32
								42

30.3 30.2	30.2 30.1
6.4	6.5
42	75

29.4 29.3	27.2 27.1	26.4 26.3	27.0 26.9	31.5 31.4	31.8 31.7	31.5 31.4	31.3 31.2	26.8 26.7	20.2 20.1
7.3	9.5	10.3	9.7	5.2	4.9	5.2	5.4	9.9	16.5
75	64	39	24	13		14	24	30	41

Sta + π - Elev

36.68
~~937.11~~

11+80
62

12+30
+50

✓

12+80
63

1266
226
98

✓

12+96

+06 FL N.E. 24" SCP 14.92 21.76

13+05
+25

✓

March 9, 1966

28

26.8 26.1	25.7 25.1	25.7 25.1	29.6 30.0	32.7 31.1	33.2 33.6	33.2 33.6	32.1 35.1	32.3 35.1	26.5 26.9	20.2 20.6
99	11.0	11.0	7.1	4.0	3.5	3.5	4.0	4.4	10.2	16.5
75	45	23	15	8		8	19	29	38	49

25.3 25.1	24.1 24.5	24.5 24.9	29.9 30.3	33.7 34.1	34.6 35.0	34.9 35.3	34.8 35.2	34.1 34.5
11.4	12.7	12.2	6.8	3.0	2.1	1.8	1.9	2.6
43	28	18	7		4	20	32	43

27.8 27.2	28.7 28.1
8.9	8.0
68	75

28.2 28.6	26.1 26.5	23.6 24.0	22.7 23.1	27.6 27.9	30.9 31.3	33.4 33.8	36.1 36.5	36.4 36.8	36.4 36.8
8.5	10.6	13.1	14.0	9.2	5.8	3.3	0.6	0.3	0.3
75	62	42	13		8	15	20	36	48

28.4 28.8	35.9 36.3
8.3	0.8
75	60

23.1 23.5	22.7 23.1	21.9 22.3	22.7 23.1	23.6 24.0	26.3 26.7	21.8 22.2	36.2 36.6
13.6	14.0	14.8	14.0	13.1	10.4	4.9	0.5
42	24	21	10		7	18	28

25.2 25.6	27.3 27.7
11.5	9.4
62	75

Sta	+	Σ	-	Elev
-----	---	----------	---	------

Sta	+	Σ	-	Elev
		36.68 937.11		

Sta	+	Σ	-	Elev
63+50				

Sta	+	Σ	-	Elev
63+50				
✓				

Sta	+	Σ	-	Elev
+ 75				

Sta	+	Σ	-	Elev
+ 75				
✓				

Sta	+	Σ	-	Elev
64				

Sta	+	Σ	-	Elev
64				
✓				

Sta	+	Σ	-	Elev
TP	11.72	.28 944.71	4.12	56 932.99

March 9, 1966

29
19

Lt

Rt

22.8 22.2	23.0 22.4	25.0 25.4	25.9 25.3	28.1 27.5	30.2 30.6	34.4 34.8
13.9	13.7	11.7	10.8	8.6	6.5	2.3
39	25	13		17	25	34

21.7 22.1	22.7 23.1	22.9 23.3	23.9 24.3
15.0	14.0	13.8	12.8
41	43	59	75

2 Ditch

23.1 23.5	23.4 23.8	24.2 24.6	27.0 27.4	27.8 28.2	30.2 30.6	34.0 34.4	36.4 36.8
13.6	13.3	12.5	9.7	8.9	6.5	2.7	0.3
52	37	23	12		9	22	28

22.1 22.5	22.9 23.3	23.3 23.7
14.6	13.8	13.4
53	60	75

2 Ditch

24.1 24.5	25.1 25.5	27.1 27.5	29.9 30.3	31.0 31.4	34.9 35.3
12.6	11.0	9.0	6.8	5.7	1.8
46	30	16	9		13

23.0 23.4	22.3 22.7	25.3 25.7
13.7	14.4	13.4
73	74	79

2 Ditch

boulder

Sta	+	π	-	Elev
-----	---	-------	---	------

~~944.71~~ ^{.28}

13+05
63+25

63+50

+75

+93 M.H. 31' RT

4.37

^{39.91}

~~940.34~~

64+00

TP

7.11

^{47.78}

~~948.21~~

3.61

^{40.67}

~~941.10~~

12.0

+30

✓

FX
DS
LPD
WJ

Lt

March 9, 1966 Rt
March 12, 1966 Rt

30
20

✓
~~37.2~~
2.1
31
~~37.6~~
6.7
48
~~37.6~~
6.7
64
~~37.2~~
7.1
75

✓
~~38.1~~
6.5
42
~~38.9~~
5.4
59
~~38.9~~
5.4
75

✓
~~38.4~~
5.9
33
~~38.9~~
5.4
39
~~39.4~~
4.9
57
~~38.9~~
5.4
75

✓
~~40.6~~
3.7
22
~~40.1~~
4.2
27
~~39.8~~
4.5
42
~~38.9~~
5.4
64
~~39.6~~
4.7
67
~~41.4~~
7.3
75

Nail in G.P

~~23.4~~
244
65
~~26.3~~
215
44
~~29.7~~
181
19
~~32.0~~
158
8
~~35.9~~
12.3
7
~~38.4~~
9.4
7
~~40.5~~
7.3
11
~~41.0~~
6.8
17
~~40.5~~
7.3
36

→ ~~23.1~~
24.7
75
Ditch
86

~~44.2~~
3.6
75
~~42.9~~
4.9
69
~~40.2~~
7.6
54
~~39.6~~
8.2
51

Sta + π - Elev.

47.78

~~948.21~~

64+55

✓

+83

✓

65

✓

March 10, 1966

3/21

LT

RT

RT

23.7 24.1	27.8 28.2	32.4 32.8	35.7 36.1	42.2 42.6	42.6 43.0	41.8 42.2	40.9 41.3	41.2 41.6	43.7 44.1
24.1	20.0	15.4	12.1	5.6	5.2	6.0	6.9	6.6	4.1
57	42	27	15		7	28	43	44	58

22.9
~~23.3~~

47.7
~~48.1~~

47.2
~~47.6~~

24.90

65

Pond

0.1 0.6
75 73

28.6
~~29.0~~

33.1
~~33.5~~

37.6
~~38.0~~

42.9
~~43.3~~

43.5
~~43.9~~

43.7
~~44.1~~

42.9
~~43.3~~

41.8
~~42.2~~

42.1
~~42.5~~

43.4
~~43.8~~

19.2	14.7	10.2	4.9	4.3	4.1	4.9	6.0	5.7	4.4
37	26	15	5		2	22	38	39	47

24.3
~~24.7~~

23.0
~~23.4~~

23.1
~~23.5~~

47.7
~~48.1~~

46.9
~~47.3~~

23.5
~~23.9~~

24.8

24.7

5.5

0.1

0.9

48

54

Rock

In Pond

68

64

25.3
~~25.7~~

30.6
~~31.0~~

35.7
~~36.1~~

44.0
~~44.4~~

44.5
~~44.9~~

43.8
~~44.2~~

42.5
~~42.9~~

42.8
~~43.2~~

44.5
~~44.9~~

22.5	17.2	12.1	3.8	3.3	4.0	5.3	5.0	3.3
43	31	20	5		18	36	37	45

23.0
~~23.4~~

47.7
~~48.1~~

46.9
~~47.3~~

24.8

54

Pond

5.5

0.1

0.9

60

57

Sta	+	π	-	Elev.
-----	---	-------	---	-------

47.78
~~948.21~~

65+25

✓

+50

936.2
 9.38
 926.82
 9.55
 936.37

✓

TP	10.45	^{.39} 957.82	0.84	^{46.94} 947.37
----	-------	-------------------------------------	------	---------------------------------------

65+25

+50

March 10, 1966 32
RT 22

LT

32.8 32.9 15.0 28	37.8 38.2 10.0 20	45.2 45.6 2.6 8	45.5 45.9 2.3 5	45.6 46.0 2.2	45.0 45.4 2.8 16	43.7 44.1 4.1 32	44.4 44.8 3.8 33	45.7 46.1 2.1 41	46.7 47.1 1.1 47	47.8 48.2 0.0 54
---------------------------------------	---------------------------------------	-------------------------------------	-------------------------------------	--------------------------------	--------------------------------------	--------------------------------------	--------------------------------------	--------------------------------------	--------------------------------------	--------------------------------------

28.1 28.5 19.7 39	24.6 25.0 23.2 50	23.0 23.4 24.8 Pond 58
---------------------------------------	---------------------------------------	---

30.2 30.6 17.6 45	36.9 37.3 10.9 29	46.5 46.9 1.3 13	47.0 47.4 0.8 9	47.0 47.4 0.8	46.3 46.7 1.5 12	45.0 45.4 2.8 28	45.3 45.7 2.5 29	47.0 47.4 0.8 39	47.6 48.0 0.2 42
---------------------------------------	---------------------------------------	--------------------------------------	-------------------------------------	--------------------------------	--------------------------------------	--------------------------------------	--------------------------------------	--------------------------------------	--------------------------------------

26.2 26.6 21.6 56 65+30 ±	24.4 24.8 23.4 62	23.0 23.4 24.8 68 Pond
--	---------------------------------------	---

49.2 49.6 8.2 60	53.1 53.5 4.3 75
--------------------------------------	--------------------------------------

51.3 51.7 6.1 58	54.9 55.3 2.5 68	55.6 56.0 1.8 75
--------------------------------------	--------------------------------------	--------------------------------------

Sta + π - Elev.

^{.39}
957.82

65+75

959.82
936.37
21.5

✓

66

✓

+25

✓

+43 MH 17' Lt 5.21 952.6⁻¹⁸

G.V.

+40 Top Conc MH Lt 5.01 952.8^{-.38}

March 10, 1966

33

23

Lt

£

Rt

~~35.7~~
~~36.1~~

~~44.2~~
~~44.6~~

~~48.4~~
~~48.4~~

~~48.5~~
~~48.9~~

~~48.1~~
~~48.5~~

~~47.3~~
~~47.7~~

~~46.5~~
~~46.9~~

~~46.8~~
~~47.2~~

~~48.9~~
~~49.3~~

21.7
42

132
27

94
23

89
14

9.3

10.1
13

10.9
24

10.6
25

8.5
36

~~51.1~~
~~51.5~~

~~25.6~~
~~26.0~~

~~23.4~~
~~23.8~~

~~23.0~~
~~23.4~~

~~57.3~~
~~57.7~~

~~54.3~~
~~54.7~~

~~51.6~~
~~52.0~~

26.3
51

31.8
66

34.0
75

34.4
77

Pond

0.1
72

3.1
61

58
48

~~44.8~~
~~45.2~~

~~47.5~~
~~47.9~~

~~50.2~~
~~50.6~~

~~48.9~~
~~49.3~~

~~49.9~~
~~50.3~~

~~49.4~~
~~49.8~~

~~48.4~~
~~48.8~~

~~47.9~~
~~48.3~~

~~48.2~~
~~48.6~~

~~50.5~~
~~50.9~~

~~52.8~~
~~53.2~~

12.6
43

9.9
40

7.2
34

7.5
19

7.5
11

8.0
14

9.0
22

9.5
23

6.9
35

4.6
44

~~35.2~~
~~35.6~~

~~30.9~~
~~31.3~~

~~27.7~~
~~28.1~~

~~24.2~~
~~24.6~~

~~57.4~~
~~57.8~~

~~55.4~~
~~55.8~~

22.2
59

26.5
65

29.7
75

33.2
93

Pond
100

0.0
66

2.0
57

~~44.5~~
~~44.9~~

~~48.0~~
~~48.4~~

~~52.0~~
~~52.4~~

~~51.3~~
~~51.7~~

~~51.4~~
~~51.8~~

~~50.6~~
~~51.0~~

~~49.7~~
~~50.1~~

~~49.0~~
~~49.4~~

~~49.7~~
~~50.1~~

~~53.1~~
~~53.5~~

~~55.3~~
~~55.7~~

~~56.1~~
~~56.5~~

12.9
60

8.4
52

5.4
43

6.1
21

6.0
15

6.8
12

7.7
23

8.4
25

7.7
40

4.3
56

~~35.9~~
~~36.3~~

~~33.8~~
~~34.2~~

~~56.3~~
~~56.7~~

21.5
79

23.6
100

1.1
75

Sta + π - Elev. all stakes

^{.39}
~~957.82~~

66+50

+ 75

+75 Profile Dale St

67

+25

+50

BM 6.16 ^{.52} 960.92 303 ^{.36} 954.77 954.76
954.35

she would pull all stakes
 declared
 MGM - 742
 1960 Chevrolet Brown + Cream
 Bellair Wagner

License Plates

March 10, 1966

34
24

47.9 42.3	50.8	53.4	53.4	52.5	52.5	52.0	50.9	50.7	51.4	52.4	52.6
9.5	51.2	51.8	51.8	52.9	52.9	52.1	51.3	51.1	51.8	52.8	52.0
66	40	40	49	49	54	65	67	60	50	48	
75	66	52	39	27	14	16	28	51	71	75	

53.8	54.7	53.7	53.3	53.6	53.4	52.1	51.4	51.3	52.0	53.3
51.2	51.1	54.1	52.7	54.0	53.7	52.5	51.8	51.7	52.4	53.7
3.6	2.7	3.7	4.1	3.8	4	5.3	6.0	6.1	5.4	4.1
75	61	51	38	15		20	36	50	70	75

52.5	53.2	53.6	53.8
52.9	51.6	54.0	54.2
4.9	4.2	3.8	3.6
200	150	100	50

53.7	53.7	53.8	53.6	53.6	53.6	52.8	51.9	52.1	54.2
54.1	54.1	54.2	54.0	54.0	54.0	53.2	52.3	52.5	54.4
3.7	3.7	3.6	3.8	3.8	3.8	4.6	5.5	5.3	3.2
75	70	47	15		13	26	45	53	65

55.1	55.2	55.1	54.9	54.9	53.3	53.3	52.9	51.6	51.4
55.5	55.6	55.5	55.3	55.3	52.7	53.7	53.3	52.0	51.8
2.3	2.2	2.3	2.5	2.5	4.1	4.1	4.5	5.8	6.0
75	51	35	14		18	22	40	61	66

55.7	55.9	55.4	54.9	53.8	52.3	52.6	52.5	50.7
56.1	54.3	55.8	55.3	54.2	52.7	53.0	52.9	51.1
1.7	1.5	2.0	2.5	3.6	5.1	4.8	4.9	6.7
75	48	20		25	36	39	51	75

Spike in Arc Lite Pole N.W. Cor Daley/Dwasso Blvd. North

Sta + π - Elev.

~~960.92~~
960.92

68+00

+50

69

✓

T.P. 4.20 ~~953.34~~ 2.94 11.78 ~~949.14~~ 48.74

+36

+77

March 10, 1966

35
25

L1

E, 3

E

R1

55.6 56.0	55.9 56.3	56.2 56.6	56.3 56.7	56.3 56.7	56.3 56.7	56.3 56.7	56.3 56.7	56.3 56.7	56.3 56.7
4.9	4.6	4.3	4.6	6.2	8.6	9.9	10.0	9.9	
75	51	24		25	48	62	63	79	
72	48	21	E, 5	3	28	51	65		

53.9 54.3	54.1 54.5	54.5 54.9	56.1 56.5	57.7 58.1	57.7 58.1	56.0 56.4	52.6 53.0	50.1 50.5	50.3 50.7
6.6	6.4	6.0	4.4	2.8	2.8	4.5	7.9	10.4	10.2
75	63	44	20		8	31	52	68	75
70	58	39	15	E, 5	13	36	57	73	

46.6 47.0	49.0 49.4	50.9 51.3	51.7 52.1	51.9 52.3	53.1 53.5	53.0 53.4	54.1 54.5	54.3 54.7	51.8 52.2	52.9 53.3
13.9	11.5	9.6	8.8	8.6	7.4	7.5	6.4	6.2	5.7	5.6
100	76	53	34	16		11	18	29	36	43
69	46	27	9	7	18	25	36	43	50	

49.6 50.0	50.9 51.3	51.8 52.2
10.9	9.6	6.7
75	66	53

44.7 45.1	44.5 44.9	45.9 46.3	46.5 46.9	47.4 47.8	48.9 49.3	49.0 49.4	49.7 50.1	50.0 50.4	49.0 49.4	49.5 49.9
8.2	8.4	7.0	6.4	5.5	4.0	3.9	3.2	2.9	3.9	3.4
100	89	64	40	19		8	21	39	67	75
80	55	31	10	11	9	17	30	48	76	

44.1 44.5	43.6 44.0	43.4 43.8	43.6 44.0	44.1 44.5	44.7 45.1	45.4 45.8	45.7 46.1	45.8 46.2
8.8	9.3	9.5	9.3	8.8	8.2	7.5	7.2	7.1
100	75	46	22		21	46	65	75
64	35	11	11	32	57	76		

Sta + π - Elev.

52.94
~~953.34~~

70

+17

+35

TP 1.67 943.^{.21}~~61~~ 11.40 941.^{.54}~~94~~

+62

71

+50

TP 1.81 934.^{.50}~~90~~ 10.52 933.^{32.69}~~09~~

March 10, 1966

36

26

Lt

Rt

43.5 43.9	43.2 43.6	41.9 42.2	43.1 43.5	44.6 45.0	46.6 47.0	46.9 47.2	45.7 46.1	42.8 43.2
9.4	9.7	10.0	9.8	8.3	6.3	6.0	7.2	10.1
100	80	58	33	15		21	45	75
	68	46	21	34	12	33	57	
42.3 42.7	42.3 42.7	42.7 43.1	43.7 44.1	43.9 44.3	47.5 47.9	47.3 47.7	46.1 46.5	44.1 44.5
10.6	10.6	10.2	9.2	7.0	5.4	5.4	6.8	8.8
100	79	53	31	14		19	38	58
	66	40	18	14	13	32	51	71
42.0 42.4	42.0 42.4	41.8 42.2	42.0 42.4	43.0 43.4	44.0 44.4	45.6 46.0	43.0 43.4	41.8 42.2
10.9	10.9	11.1	10.9	9.9	8.9	7.7	8.4	9.9
100	86	65	30	17	10		25	49
	51	16	3	4	14	39	63	75
40.0 40.4	39.6 40.0	40.2 40.6	40.2 40.6	39.5 39.9	40.6 41.0	40.7 41.1	40.1 40.5	39.2 39.6
32	30	30	3.2	3.7	3.1	2.6	2.5	3.1
100	96	75	56	28		8	32	50
	60	41	134	15	23	47	65	
38.9 39.3	36.9 37.3	37.2 37.6	36.5 36.9	36.6 37.0	36.4 36.8	36.3 36.7	36.5 36.9	35.4 35.8
4.3	6.3	6.0	6.7	6.6	6.8	6.9	6.7	7.8
100	80	50	23		18	39	53	70
	63	33	64	35	56			
33.1 33.5	33.2 33.6	33.2 33.6	33.6 34.0	33.0 33.4	33.0 33.4	32.7 33.1	33.1 33.5	31.8 32.2
10.1	10.0	10.0	9.6	10.1	10.2	10.2	10.5	10.1
100	90	67	41	21		26	52	64
	71	48	22	2	19	45	71	

Rock

Sta + π - Elev.

^{.50}
934.90

72

+50

BM

^{.00}
4.50 930.43 930.32

73

TP

^{.20}
1.23 922.60 ^{20.97} 13.53 ~~921.37~~ 921.31

TP

^{07.66}
14.54 ~~908.06~~ (908.00)

TP

^{.55}
0.58 921.89 ^{20.97} 921.31 921.31

+50

74

+40

FK
DS
L PD
WJ

March 10, 1966
March 11, 1966

37
27

11.

k.

RT

(29.6)

28.7	28.4	28.2	29.7	29.1	29.1	29.0	29.4	28.7
29.1	28.8	29.6	30.1	29.5	29.5	29.4	29.8	29.1
5.8	6.1	5.3	4.8	5.4	5.4	5.5	5.1	5.8
100	72	48	27	25	50	60	75	
	50	26	5	22	47	72		

(25.0)

26.3	25.3	24.0	25.0	25.0	25.1	24.9	24.7	24.2
26.7	25.7	24.4	25.4	25.4	25.5	25.3	25.1	24.6
8.2	9.2	10.5	9.5	9.5	9.4	9.6	9.8	10.3
100	76	54	26	20	46	62	75	
	52	30	2	24	44	70		

(20.5)

22.0	21.0	20.6	20.5	20.6	20.8	20.6	21.0	20.8
22.4	21.4	21.0	20.9	21.0	21.2	21.0	21.1	21.2
12.5	13.5	13.9	14.0	13.9	13.7	13.9	13.5	13.7
100	78	54	29	17	41	56	75	
	52	28						

Nail in transformer P.P. 26 43 67

Nail in Transformer P.P.

(17.1)

21.6	20.9	20.1	17.5	16.9	15.8	17.2	17.4	17.6	17.1
21.4	21.0	20.4	17.8	17.2	16.1	17.5	17.7	17.9	17.4
0.0	0.7	1.5	4.1	4.7	5.8	4.4	4.2	4.0	4.5
100	89	69	45	22	12	34	53	75	
	60	40	16	31	7	29	41	63	

(14.6)

21.6	19.8	15.9	13.9	13.0	12.5	12.7	12.9	12.9	13.3	12.9
21.4	19.7	15.2	14.2	13.3	12.8	13.0	13.2	13.2	13.6	13.3
0.0	2.8	5.7	7.7	8.6	9.1	8.9	8.7	8.7	8.3	8.1
100	71	46	23	10	17	34	51	64	75	
	69	40	1.5	8	31	41	48	65		

(13.0)

17.5	16.0	14.5	13.0	11.6	10.6	10.3	09.3	10.6	11.3
17.8	16.3	14.8	13.3	11.9	10.9	10.6	09.6	10.9	11.6
4.1	5.6	7.1	8.6	10.0	11.0	11.3	12.3	11.0	10.3
100	75	54	33	17	14	17	19	35	
	67	42	21	0	16	33	47	50	

Sta + π - Elev

^{.55}
921.89

74 + 40

+ 71

✓
TP 5.89 ^{15.71} ~~916.05~~ 11.73 ^{09.82} ~~912.16~~

75

✓

+ 16

12.3
5.8
6.5

Lt.

L

March 11, 1966

Rt.

38
28

(11.4)

15.9 16.2	13.6 13.9	11.5 11.8	10.2 10.5	9.2 9.5	8.8 9.1	6.6 6.9	6.6 6.9
5.7	8.0	10.1	11.4	12.4	11.8	15.0	15.0
89	65	37	8	10	13	21	55
55	31	3	26	34	44	47	55

15.5
15.86.1
100

Rock

07.8
08.113.8
7508.7
09.012.9
5509.8
10.111.8
3909.5
09.812.1
24

12.5 12.9	11.9 12.3	10.9 11.3	9.7 10.1	9.1 9.5	8.3 8.7	7.2 7.6	5.7 6.1	5.6 6.0	7.9 8.3
3.2	3.8	4.8	6.0	6.6	7.8	8.5	10.0	10.1	7.8
100	86	65	40	19	7	12	21	25	
50	29	4	17	36	43	48	57		

(09.6)

06.4
06.893
7506.8
07.289
6307.1
07.58.6
42

09.3 09.7	8.2 8.6	8.1 8.5	6.5 6.9	5.9 6.3	2.5 2.9	5.9 6.3	4.6 5.0
6.4	7.5	8.6	9.3	9.6	9.8	13.2	9.8
69	55	48	19	18	21	24	41
31	17	10	19	38	56		

10.2
10.65.5
90
5310.6
11.05.1
10089.6
89.017.1
81
30.30P00.9
01.314.8
7800.5
00.915.2
6203.4
03.812.3
56

Sta + π - Elev

15.71
~~916.05~~

75+66

✓

76

✓

TP 6.22 11.76 ~~912.10~~ 10.17 .54 ~~905.88~~

+50

✓

March 11, 1966

39

06.6

29

07.5 07.9	06.6 07.0	39 06.5	06.4 06.8	07.6 08.0	06.4 06.8	04.9 05.3	04.0 04.4	03.6 04.0
82	91	92	93	81	93	108	117	121
51	43	30	11	9	27	48	58	
12	4	9	28	39	48	66		

08.3 08.7	09.2 09.6	10.3 10.7
74	65	54
68	86	100
29	47	61

02.6 03.0	01.8 02.2
13.1	13.9
75	67

08.1 08.5	07.8 08.2	07.5 07.9	40 07.6	07.2 07.6	05.8 06.2	04.6 05.0	03.4 03.8	02.1 02.5	00.8 01.2
76	79	82	81	85	99	111	123	136	149
85	62	43	29	17	15	38	51	66	
45	22	3	11	23	40	55			

07.3

08.8

01.9

6.9
100
rock 60

13.8
75

08.9 09.3	08.3 08.7	07.5 07.9	43 06.3	05.1 05.5	04.1 04.5	02.9 03.3	02.6 03.0	01.7 02.1	00.8 01.2	89.8 90.2
2.9	3.5	4.3	5.5	6.7	7.7	8.9	9.3	10.1	11.0	12.0
100	92	68	42	20	19	30	37	50	54	
57	49	25	1	23	43	62				

06.3

01.0
01.3
10.8
75

00.7
01.0
11.1
65

Sta + π - Elev.

11.76
912.10

77

✓

+50

12,20
280
9.4
1

✓

78

TP	2.88	902.71 ^{.37}	12.27	899.49 ^{.49}
BM3	8.54	906.51 ^{.14}	4.77	897.94 ^{.60}
				(897.97)

March 11, 1966 40
30

11

05.3

07.3
02.6

06.5
06.8

05.3 45'
05.6

04.1
04.4

02.5
02.8

00.6
00.9

89.3
89.6

89.6
89.8

89.6
89.9

45 53 65 77 9.3 11.2 12.5 13.2 12.2
88 70 46 21 18 37 41 54
43 25 1 24 45 63

902.8
902.1

899.1
899.4

898.6
898.9

899.1
899.4

899.4
899.7

4.0
100
55

12.7 13.2 12.7 12.4
106 100 87 69
Fence

906.8
907.2

906.4
906.4

904.7 45'
905.10

903.6
903.9

902.2
902.5

900.2
900.5

899.1
899.4

898.5
898.8

897.6
897.9

4.9 5.7 7.0 8.2 9.6 11.6 12.7 13.3 14.2
100 88 67 44 18 13 24 27
55 43 22 1 27 45 58

03.7

896.3
896.6

897.1
897.4

897.7
898.0

897.3
897.6

15.5 14.7 14.1 13.8
86 70 52 38
Fence

906.0
906.30

905.4
905.7

904.7 42'
905.0

903.2
903.5

901.3
901.6

898.9
899.2

897.7
898.0

896.1
896.4

896.3
896.6

896.8
897.1

5.8 6.4 7.1 8.6 10.5 12.9 14.1 15.7 14.5 15.0
100 88 70 45 22 8 15 27 40
58 46 28 3 20 42 50 57

02.4

895.8
896.1

896.0
896.3

16.0 15.8
67 55
Fence

Sta + Δ - Elev.

906.¹⁴~~51~~

78+50

✓

+ 75

✓

78+91.39 P.I. = 1937 P.I.

79

+ 50

Sta + π - Elev

906.⁻¹⁴~~51~~

79+67

✓

TP 3.45 ^{96.65}~~897.02~~ 12.94 ^{.20}~~893.57~~

+79

121.47
78+91.39
80+12.86
= 80+40.95
12
121.47

✓

80

✓

March 16 1966

42
31

893.4

LT.

893.5

BT.

892.5
892.9

894.4
894.8
893.1

892.5
892.9
893.0

892.6
893.0

893.5
893.9

893.5
893.9

893.3
893.7

892.7
893.1

117 136 135 12.6 12.6 12.8 13.4 13.6
34 24 17 6 9 22 32
3 7' 14' 25' 31' 40' 53' Fe

896.1
895.5

895.6
896.0

895.0
895.4

894.3
894.7

894.1
894.5

10.0 10.5 11.1 11.8 12.0
46 60 73 86 100
15 29 42 55

892.7
893.0

892.4
892.7

892.5
892.8

893.2
893.5

893.4
893.7

893.3
893.6

892.7
893.0

892.5
892.8

4.0 4.3 4.2 3.5 3.3 3.4 4.0 4.2
47 29 18 9 7 20 31
16 2' 13' 22' 31' 38' 51' Fence

893.6
894.1

893.4
893.7

893.6
893.9

29 3.3 3.1
68 87 100
37 56

892.9
893.2

892.7
893.0

892.4
892.7

892.6
892.9

893.1
893.4

893.0
893.3

892.5
892.8

892.2
892.5

3.8 4.0 4.3 4.06 3.6 3.7 4.2 4.5
66 43 21 10 5 17 28
36 13 9' Tell M4 30' 35' 47' Fe 58'

893.2
893.5

893.2
893.5

3.5 3.5
87 100
57

Sta + π - Elev.

96.65
~~897.02~~

80+33

+42

+45 Profile Chandler Ave.

+64 Ent Rt.

81

+50

March 15, 1966

43

32

14

891.2	91.0	91.8	92.2	92.1	92.2	92.7	92.6	92.2	92.6	91.6
55	57	49	45	46	45	40	41	45	45	51
100	96	79	60	43	29	14	15			28F
68	51	32	15	1	14'	28'	43'			56'

90.7	91.3	91.8	91.1	90.9	91.7	92.6	92.5	92.1	91.5
6.0	5.4	4.9	5.6	5.8	5.0	4.1	4.2	4.6	5.2
100	77	63	48	34	26	15		16	28
73	50	36	21	7	1'	12'	27'	43'	55'

91.7	91.1	94.5	93.1	92.4	92.3	92.4
0.0	0.6	2.2	3.6	4.3	4.4	4.3
218	200	150	100	50	24	

90.1	93.1	92.5	90.7	90.9	90.8	91.6	91.8	92.2	92.3	92.0	90.3	90.8
6.6	3.6	4.2	6.0	5.8	5.9	5.1	4.5	4.4	4.7	6.4	7.8	9.2
100	93	83	70	50	35	31	16		14	28	46	70
38	45	25	10	6	9'	25'	39'		53'			Lake

91.8	89.7	90.1	90.5	90.6	92.0	92.2	92.0	91.2
4.9	7.0	6.6	6.2	6.1	4.7	4.5	4.7	5.5
100	93	74	53	38	17		13	27
72	53	32	17	4'	21'	34'	48'	

89.1	90.1	90.2	90.2	90.7	91.5	92.1	91.8	90.7
7.6	6.6	6.5	6.5	6.0	5.2	4.6	4.9	6.0
100	74	54	40	33	17		12	28
59	39	25	18	2	15'	27'	43'	

Sta + π - Elev.

96.65
~~897.02~~

81 + 7.91

Equals 82+00 - of 1937 Survey

BM 5.56 896.^{.12}~~49~~ 6.09 890.^{.56}93

81 + 7.91 4.10 892.^{.02}~~35~~

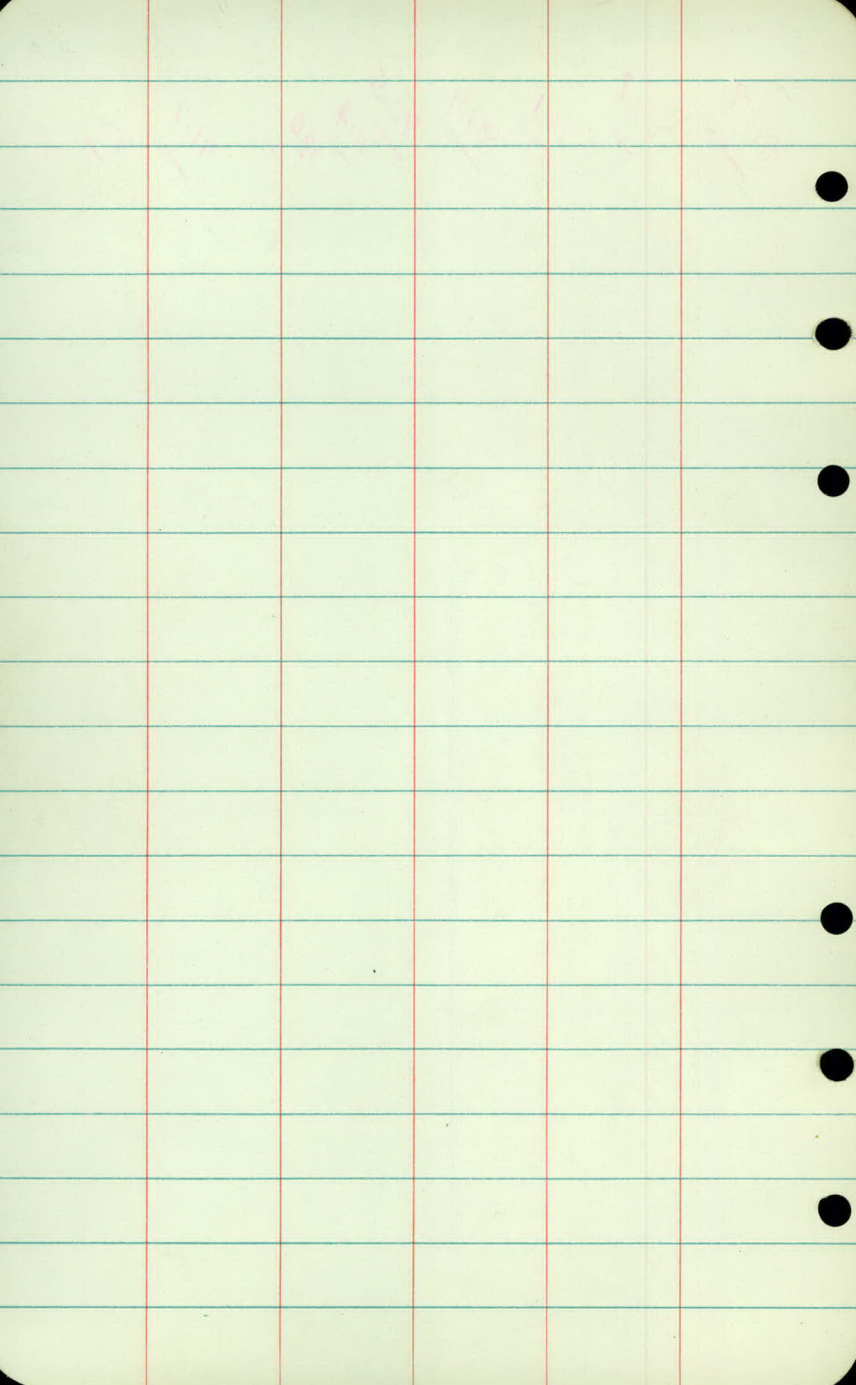
March 11, 1966

44
33

Lt

88.9	89.7	90.1	89.9	90.5	91.4	92.0	91.7	90.5	90.5
81.2	90.0	90.4	90.4	90.8	91.7	92.3	92.0	90.4	90.8
7.8	7.0	6.6	6.6	6.2	5.3	4.7	5.0	6.2	6.2
100	82	54	39	30	18	13	13	25	29
69	41	26	17	5	13'		26'	38'	42

Top S. Rim MH



FK
WJ
HL
JT

June 6, 1966

45
34

"B" Line X-Sections

Starting 82+00 of "B" Line
started April 4, 1966

Sta	+	π	-	Elev.
BM	5.56	896. ^{.12} 49		890. ^{.56} 93

82

+50

+76 M.H. 25' Lt

83

Sta	+	Span	Top	Arch	Elev.
+29	47.5	Rt	3.45'	7.83	2.32
				10.15	

+50

Sta	+	Span	Inv. Arch	Elev.
+80	41.5	Inv.	3.45'	10.16

84

+37 MH 36.3' Lt 5.91

+50 Good for E Horseshoe Drive

+51 MH 36' Rt. 3.69 92.80

24

2

June 6, 1966 46

Rt 35

Top S. Rim M.H.

89.3	90.0	89.7	89.9	91.1	91.5	91.9	91.6	90.9	90.5
89.7	90.4	90.1	90.3	91.5	91.9	92.3	92.0	91.3	90.9
6.8	6.1	6.4	6.2	5.0	4.6	4.2	4.5	5.2	5.6
63	44	32	20	7		11	23	31	40

Fe

88.7	89.6	89.1	90.1	90.7	91.2	91.6	91.7	91.0	90.4
89.1	90.0	89.5	90.5	91.1	91.6	92.0	92.1	91.4	90.8
7.4	6.5	7.0	6.0	5.4	4.9	4.5	4.4	5.1	5.7
60	45	36	21	11		6	19	29	40

Fe

88.5	89.4	89.9	90.4	90.7	90.9	91.3	90.9	90.1
88.9	89.8	90.3	90.8	91.1	91.3	91.7	91.3	90.5
7.6	6.7	6.2	5.7	5.4	5.2	4.8	5.2	6.0
60	40	25	14		4	16	32	46

Fe

87.5	88.6	89.5	90.4	90.9	91.1	90.7	90.4
87.9	89.0	89.9	90.8	91.3	91.5	91.1	90.8
8.6	7.5	6.6	5.7	5.2	5.0	5.4	5.7
60	48	29	16		19	43	60

88.5	89.6	90.4	91.1	91.4	91.3	91.1	91.0
88.9	90.0	90.8	91.5	91.8	91.7	91.5	91.4
7.6	6.5	5.7	5.0	4.7	4.8	5.0	5.1
60	37	20		9	23	42	65

87.4	88.5	90.1	89.8	90.6	91.3	91.8	92.3	93.1	94.6	96.6
87.8	88.9	90.5	90.2	91.0	91.7	92.2	92.7	93.6	95.0	97.6
8.7	7.6	6.0	6.3	5.5	4.8	4.3	3.8	3.0	1.5	10.5
60	45	40	32	22		9	29	53	77	100

Sta + π - Elev.

^{.12}
~~896.49~~

85

+50

T.P. 391 ^{.56} 897.95 2.45 ^{893.65} ~~894.04~~

86

+50

86+8400 B Line =

87+00 1937

Continued on 1937 Alignment

+50

June 6, 1966

47

LL

X

RT

36

87.0

~~87.4~~

90.2

~~90.6~~

91.0

~~91.4~~

92.0

~~92.4~~

92.5

~~92.9~~

92.1

~~92.6~~

92.7

~~93.1~~

93.1

~~93.5~~

93.1

~~93.5~~

91

5.9

5.1

4.1

3.6

3.9

3.4

1.0

1.0

45

36

23

18

28

43

50

60

Water

X

87.1

~~87.5~~

90.8

~~91.2~~

91.6

~~92.0~~

92.3

~~92.7~~

92.5

~~92.9~~

92.7

~~93.1~~

92.0

~~92.4~~

93.9

~~94.3~~

94.5

~~94.9~~

9.0

5.3

4.5

3.8

3.6

3.4

4.1

2.2

1.6

48

35

24

3

15

26

47

52

Nail in PP SE. Cor W. Horseshoe Drive + N. Ovasso

87.3

~~87.7~~

88.1

~~88.5~~

91.6

~~92.0~~

92.3

~~92.7~~

93.0

~~93.4~~

93.1

~~93.5~~

93.1

~~93.5~~

92.6

~~93.0~~

94.1

~~94.5~~

96.0

~~96.4~~

96.9

~~97.3~~

10.3

9.5

6.0

5.3

4.6

4.5

4.5

5.0

3.5

1.6

+1.3

60

41

35

23

3

13

24

38

47

54

X

88.7

~~89.1~~

88.2

~~89.6~~

92.1

~~92.5~~

93.0

~~93.4~~

93.8

~~94.2~~

93.9

~~94.3~~

92.7

~~93.1~~

94.2

~~94.6~~

96.9

~~97.3~~

98.1

~~98.5~~

8.9

8.4

5.5

4.6

3.8

3.7

4.9

3.4

0.7

+1.0

60

51

34

22

13

21

33

38

44

up 1.12

86.6

~~87.0~~

86.8

~~87.2~~

92.4

~~92.8~~

93.4

~~93.8~~

94.2

~~94.6~~

94.0

~~94.4~~

92.8

~~93.2~~

94.9

~~95.3~~

96.8

~~97.2~~

11.0

10.8

5.2

4.2

3.4

3.6

4.8

2.7

0.8

1.1

1.1

1.1

1.1

47

40

28

21

13

24

34

37

exp

out

1.12

86.6

~~87.0~~

86.7

~~87.1~~

88.2

~~88.6~~

92.9

~~93.3~~

94.0

~~94.4~~

94.5

~~94.9~~

94.1

~~94.5~~

93.3

~~93.7~~

95.0

~~95.4~~

96.6

~~97.0~~

98.0

~~98.4~~

99.0

~~99.4~~

11.0

10.9

9.4

4.7

3.6

3.1

3.5

4.3

2.6

+3.0

52

43

34

26

19

14

24

35

43

1.1

1.2

1.1

1.2

1.1

Sta + Δ - Elev.

^{.56}
897.95

88

+50

BM 3.24 ^{.59}897.98 3.21 ^{.35}894.74

+82 Tell M.H. 17' Lt. 2.87

89

+17 MH 27' Rt 3.24

+50

90

+50

June 6, 1966 48
 Lt Rt 37

86.7	88.2	93.3	94.3	94.7	94.2	93.1	94.8	902.3
87.1	88.4	93.7	94.7	95.1	94.6	93.5	95.2	902.7
10.9	9.4	4.3	3.3	2.9	3.4	4.5	2.8	+4.7
39	33	23	18		13	23	36	49

86.6	88.9	94.2	94.9	94.7	94.2	93.2	94.9	902.6
87.0	89.3	94.6	95.3	95.1	94.6	93.6	95.3	903.0
11.0	8.7	3.4	2.7	2.9	3.4	4.4	2.7	+5.0
50	37	23	12		13	22	37	48

R.R. Spike in PPH sta 88+48

85.8	88.9	94.1	94.9	94.9	94.2	93.2	94.9	96.6
86.2	89.3	94.5	95.3	95.3	94.6	93.6	95.3	97.0
11.8	8.7	3.5	2.7	2.7	3.4	4.4	2.7	+1.6
58	36	23	11		14	24	38	53

86.1	87.9	93.7	94.6	94.6	93.9	92.8	94.4	96.3
86.5	88.3	94.1	95.0	95.0	94.3	93.2	94.8	96.7
11.5	8.7	3.9	3.0	3.0	3.7	4.8	3.2	1.3
52	33	20	8		18	26	46	60

85.9	92.5	93.8	94.1	93.7	92.3	94.2	95.9
86.3	92.9	94.2	94.5	94.1	92.7	94.6	96.3
11.7	5.1	3.8	3.5	3.9	5.3	3.4	1.7
32	20	9		18	27	46	60

84.3	92.0	93.3	93.5	93.0	91.8	92.7	95.3
84.7	92.4	93.7	93.9	93.4	92.2	93.1	95.7
13.3	5.6	4.3	4.1	4.6	5.8	4.9	2.3
36	22	6		17	28	41	60

Sta + π - E/ev.

^{.59}
~~897.98~~

91

BM

^{.28}
2.31 895.~~67~~ (895.69)

June 6, 1966

49

Lt.

Rt.

38

~~86.3~~
~~86.7~~

~~91.7~~
~~92.1~~

~~92.6~~
~~93.0~~

~~92.9~~
~~93.3~~

~~93.0~~
~~93.4~~

~~92.6~~
~~93.0~~

~~91.6~~
~~92.0~~

~~92.2~~
~~92.6~~

~~93.4~~
~~93.8~~

11.3

5.9

5.0

4.7

4.6

5.0

6.0

5.4

4.2

37

22

15

7

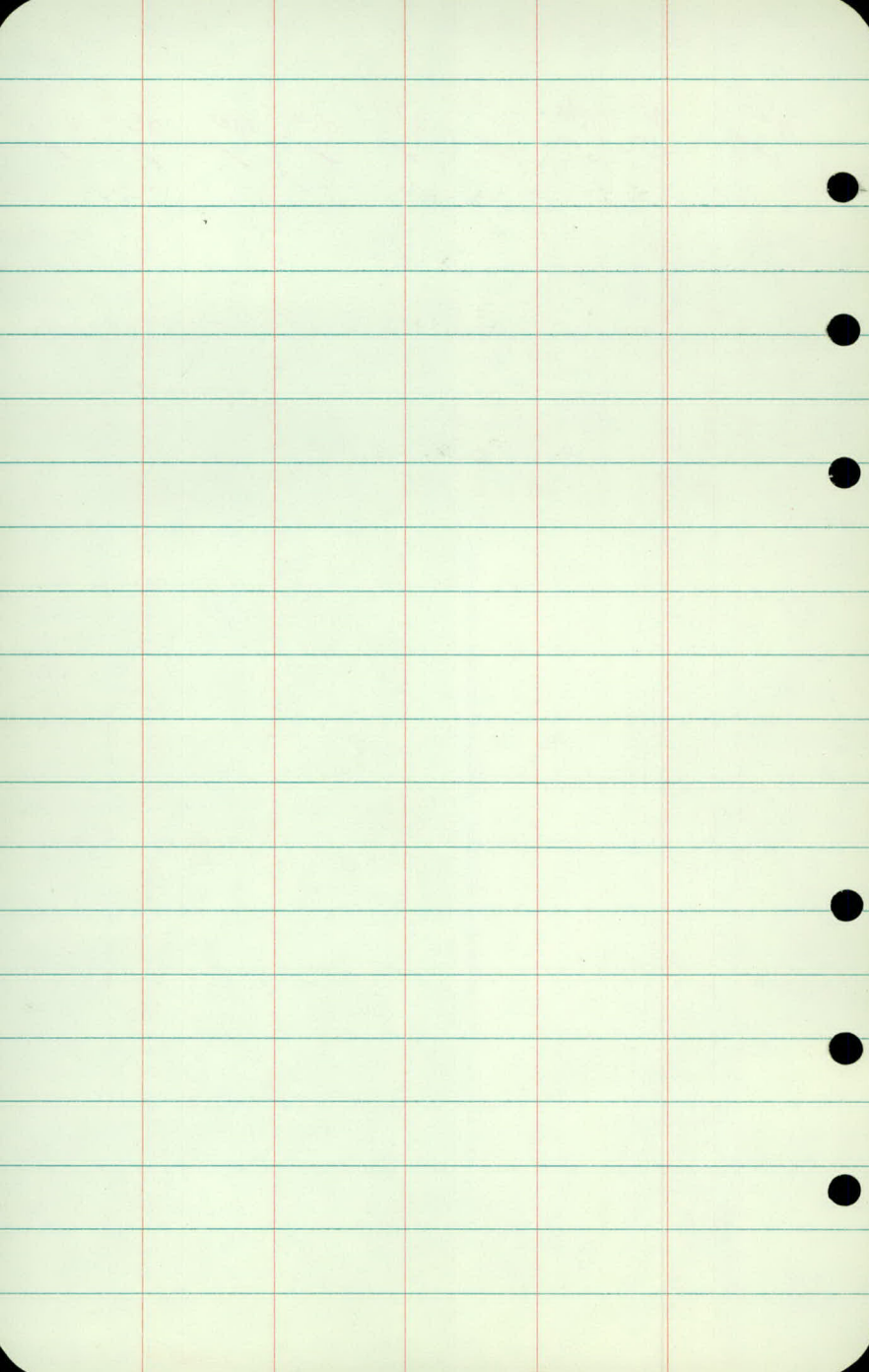
17

25

40

60

Spike in P.P. E. Horseshoe Drive & N. Owasso



Additional x-sections
and
Profile of

ARBOGAST ST

Sta	+	π	-	Elev.
BM	7.11	934.83 ^{.40}		927.29 (927.72)
4			0.1	934.73 ^{.30}
5			1.5	933.90
6			2.85	931.55
7			3.5	930.90
8			4.3	930.10
9			5.2	929.20

✓

+26

✓

June 24, 1966 51/40
 Lt. BT

RR Spike S.W. Corner Arbogast + Orasso St

✓

31.9	28.8	27.9	29.0	29.2	28.9	28.4	27.4	27.4
25	5.6	6.6	5.4	5.2	5.5	6.0	7.0	7.0
45	26	20	15	13	20	24	25	

33.8	27.2	29.8	31.3
0.6	7.2	4.6	3.1
60	60	46	32

✓

34.2	31.2	28.6	25.6	29.0	29.1	28.7	29.1	27.1	28.7
92	3.2	5.8	8.8	5.4	5.3	5.7	6.3	7.3	5.7
68	45	26	22	13		13	22	26	29

24.2	26.2
10.2	8.2
60	46

Sta + T - Elev

^{.40}
~~934.88~~

9+39

✓

+47

✓

T.P. 7.41 ^{.48} 935.91 6.33 ^{.07} 928.50

+59

173.5 & Onassis St

+59 +78

+92

10

✓

FK
JT
JS
PA

11.

June 24, 1966
June 23, 1966

52
41

31.6 28.6 27.8 29.9 29.1 29.0 28.6 27.3 28.5 27.9
28 58 66 55 53 54 58 61 59 65
60 27 23 17 13 11 20 24 33

22.1 22.6 23.4 25.5
12.3 11.8 11.0 8.9
80 70 60 45

29.6 29.8 27.4 27.6 28.9 29.0 28.5 28.2 26.6 28.3
48 56 69 56.8 5.5 54 59 62 78 61
37 26 FL 18 in 22 16 13 22 26 29
20.4

30.6 31.1
3.8 33
54 60
Top S.P.

24.1 25.9 27.8
10.3 8.5 6.6
60 50 35

29.5 29.1 28.9 29.2 29.0 29.6 27.9 26.6 28.2
6.0 6.4 6.6 6.3 6.5 6.9 7.6 8.9 7.3
50 35 20 10 13 21 25 30

30.0
5.5
60

26.9 27.9 28.2
8.6 7.6 7.3
60 54 44

Sta + π - Elev.

935.⁴⁸91

9+73.5 $\pm$ Oniasco St. Lt.

✓

+78 M.H. 22.5 Rt. 7.41

+92

✓

10

✓

June 27, 1966 53
RT 42

Lt.

~~29.1~~
~~29.5~~

30.5 30.0 29.5 29.2 28.7 28.3 27.7 26.2
5.0 5.5 6.0 6.3 6.4 6.8 7.2 7.79 9.3
60 45 28 10 13 23 26.5 27
(RimCB)

31.2 33.2 35.3
4.3 2.3 0.2
70 106 45

28.7 28.7 28.1
6.8 6.8 7.4
60 50 32

29.8 29.3 29.1 29.2 29.3 29.1 28.0 28.4 28.8
5.7 6.2 6.4 6.3 6.2 6.4 7.5 7.1 6.7
45 29.7 25 10 12 28 37 50
GGV.

30.5
5.0
55

29.4 29.2
6.1 6.3
74 60
Ho

30.6 29.9 28.8 29.2 29.4 29.1 28.7 28.1 28.2
4.9 5.6 6.7 6.3 6.1 6.4 6.8 7.4 7.3
45 31 22 13 12 21 25 34

30.7
4.8
52

29.2 28.6
6.3 6.9
60 45

Sta + π - Elev

^{.48}
935.91

10 + 44

✓

+ 80

4.76

11 + 05

4.35

+ 05

4.26

+ 30

3.7

+ 80

2.4

12

1.8

+ 30

2.0

+ 80

8.1

13

10.7

+ 05

11.9

F.L. Culr Ent
E. End

7.92
^{1.30}
9.22

9.22

²⁶
926.69

(926.71)

June 27, 1966 54

LT

✓

BT 43

30.4

28.8

28.3

29.6

30.1

29.9

29.4

28.1

28.1

5.1	6.7	7.2	5.9	5.4	5.6	6.1	7.4	7.4
30	27	22	14		11	19	24	CB
								32

31.0

31.3

32.1

21.9

23.2

25.4

27.2

4.5	4.2	3.4			13.6	12.3	10.1	8.3
41	48	66			66	63	55	45

Difference

Sta

"B" Line of A Line

66+50	0.57	Lt.
67	1.9	Lt.
+50	3.1	Lt.
68	4.3	Lt.
+50	5.5	Lt.
69	7.7	Lt.
70	12.3	Lt.
71	17.2	Lt.
72	21.9	Lt.
73	26.6	Lt.
74	31.0	Lt.
75	36.3	Lt.
76	40.8	Lt.
77	45.3	Lt.
+50	44.5	Lt.
78	42.4	Lt.
+50	37.3	Lt.
79	31.8	Lt.
+50	31.5	

Sta

B Line of A line

55
44

80

30.1' Lt

+50

27.0

81

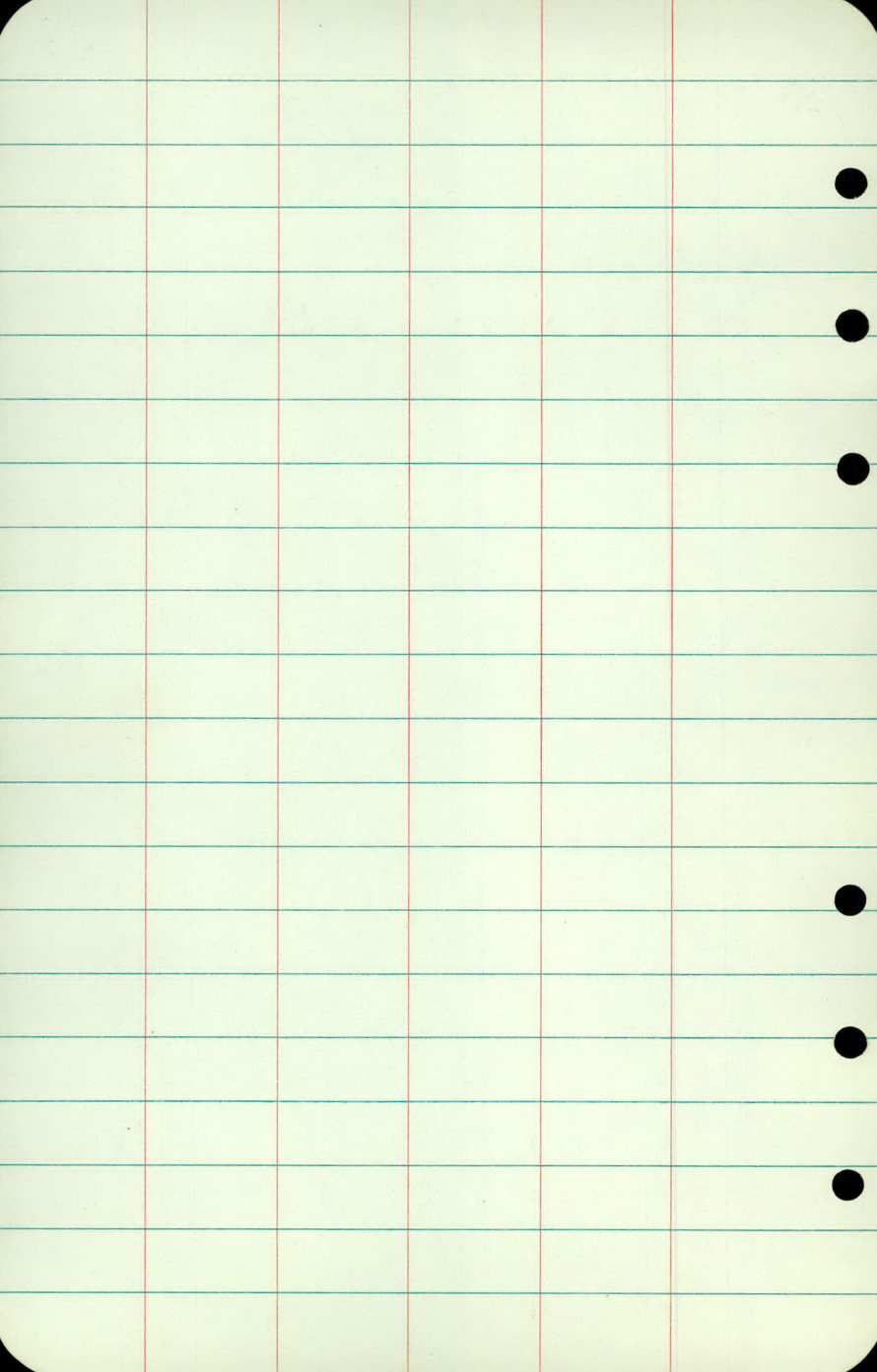
21.4' Lt

+50

15.2' Lt

+71.91

13.2' Lt



FK
JT
JS
PA

June 29, 1966

56
45

Profile "B" Line Check

Sta 68 to 75

Sta	+	Δ	-	Elev.
BM	6.92	961.68		954.35 <u>954.76</u>

68			5.07	956.61
----	--	--	------	--------

A line +50 check			53.57	58.1 ✓ 58.1
------------------	--	--	-------	-------------

69			8.49	
----	--	--	------	--

TP	0.31	960.58	11.41	960.27
----	------	--------	-------	--------

+77			5.97	
-----	--	--	------	--

70			5.31	
----	--	--	------	--

+17			4.3	
-----	--	--	-----	--

71			13.59	
----	--	--	-------	--

TP	1.66	948.66	13.58	947.00
----	------	--------	-------	--------

71 $\neq$

72			8.91	
----	--	--	------	--

T.P.	0.97	935.90	13.73	934.93
------	------	--------	-------	--------

June 29, 1966

57

46

£

Spike in Arc Light pole NW Cor Dale St

Rock

stone

Sta + X - Elev.

935.90

73

5.17

74

11.16

75

15.77

BM

4.61 930.29 (930.32)

Arbogast

4

10.54 945.27

(934.73)

3

9.13

2

7.31

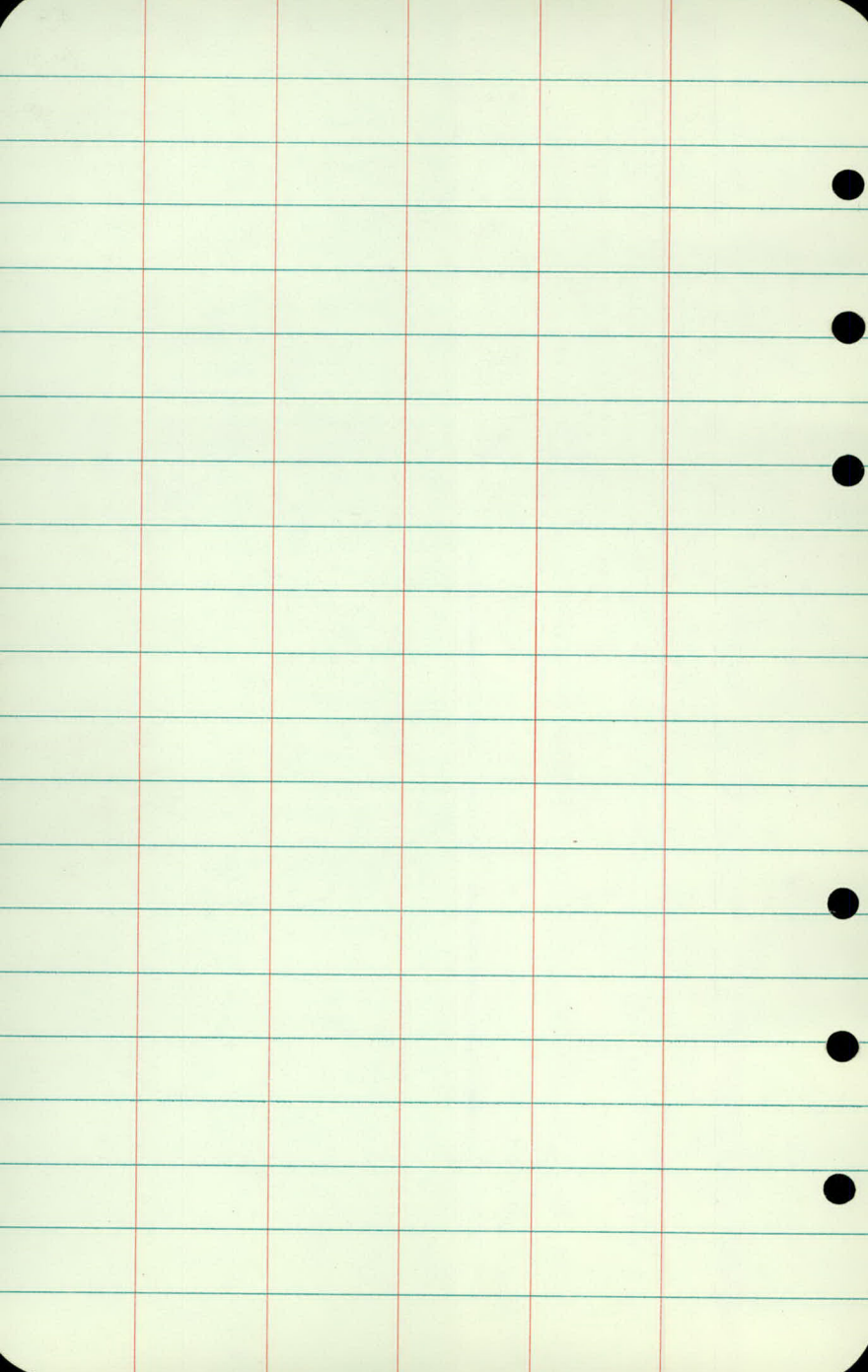
1

4.31

0 £ Victoria 1.26 944.0

June 29, 1966 58
47

Spike in PP



Owasso Blvd West

Alignment

Sta	Point	ΔL	ΔR
-----	-------	------------	------------

+85.97	P.T.	$12^{\circ}50'$	
--------	------	-----------------	--

+75		$12^{\circ}03.9'$	
-----	--	-------------------	--

+50		$10^{\circ}18.9'$	
-----	--	-------------------	--

+25		$8^{\circ}33.9'$	
-----	--	------------------	--

63		$6^{\circ}48.9'$	
----	--	------------------	--

62+95.87	P.I.		
----------	------	--	--

+75		$5^{\circ}03.9'$	
-----	--	------------------	--

+50		$3^{\circ}18.9'$	
-----	--	------------------	--

+25		$1^{\circ}33.9'$	
-----	--	------------------	--

62+02.64	P.C.	$0^{\circ}00'$	
----------	------	----------------	--

			P.I. = 62+95.87
--	--	--	-----------------

			$\Delta = 25^{\circ}40'$
--	--	--	--------------------------

			$\frac{1}{2}\Delta = 12^{\circ}50'$
--	--	--	-------------------------------------

			$D = 14^{\circ}00'$
--	--	--	---------------------

			$T = 93.23'$
--	--	--	--------------

			$L = 183.33'$
--	--	--	---------------

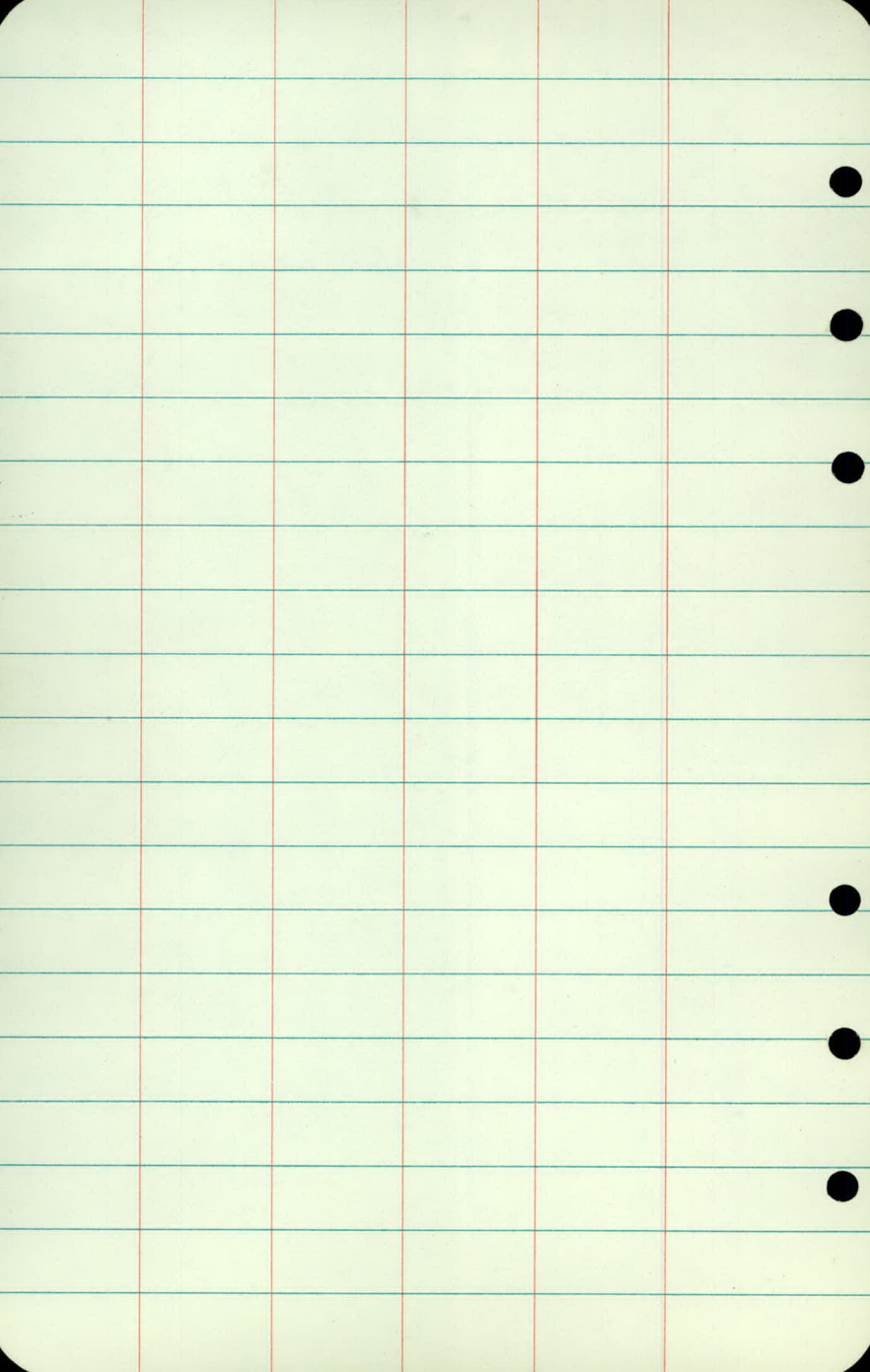
			$R = 409.26$
--	--	--	--------------

June 29, 1966

60

49

Reinforcing Rod



x-sections

Ovasso Blvd West

Elev. Checked & Changed
7-28-66 JH

Sta + π - Elev.

46.79

940.57

TP 6.12 ~~947.22~~

~~941.10~~

39.94

6.85 ~~940.27~~

61+00

+50

62

FK
JT
JS
PA

June 30, 1966

62
51

Nail in G.P. N.E. Cor Arboretum W. Owasso

39.0	40.6	42.0	43.3	43.7	44.0	43.8	44.9	48.8
7.8	6.3	4.8	3.5	3.08	2.8	3.0	1.9	+2.0
20	16	13	8		8	23	32	43

35.1
11.7
30
Fe

39.9	38.1	41.4	42.6	43.0	43.3	43.2	47.2	50.4
12.9	8.7	5.4	4.2	3.8	3.5	3.6	+0.4	+3.6
21	16	10	5		9	25	33	44

30.4
16.4
29
Fe

53.8
+7.0
56

32.9	33.6	40.9	41.6	42.6	42.6	42.6	43.0	43.6
13.9	13.2	5.9	5.2	4.6	4.2	4.2	3.8	3.2
29	26	13	5		10	24	6	C
							32	

46.7	46.0	44.5
0.1	0.8	2.3
50	48	42

Sta + Δ - Elev
46.79
~~947.22~~

62+25 Ent Rt

✓

+50

✓

TP 3.67 ^{44.56} ~~944.99~~ 5.90 ^{40.89} ~~941.23~~

+75

✓

June 30, 1966

63
52

Lt

£

Fr

33.6 35.5 40.8 41.3 41.6 42.0 41.8 43.5 45.9 46.0
132 113 6.0 5.5 52 4.8 50 3.3 0.9 0.2
24 19 12 5 11 24 41 59 63
£

32.3
14.5
30
Fe

33.0 35.4 40.1 40.7 40.9 41.0 40.6 40.8 41.5
13.8 11.4 6.7 6.1 59 5.8 6.2 5.9 5.3
21 17 10 4 14 27 6 C
£ 32

31.6
15.2
34

45.0 43.6
1.8 3.0
55 49

32.4 33.0 34.4 39.2 39.4 39.8 40.2 40.1 39.5 39.9
12.0 11.6 10.2 5.4 5.2 4.8 4.4 4.5 5.1 4.7
21 18 17 9 6 10 17 34 35
£

32.0 31.5 31.3
12.6 13.1 13.3
27 34 37

44.2 41.6
04 3.0
58 46

Sta + π - Elev.
 944.56
~~944.99~~

63

✓

+10 Top 24" SCP 8.80 35.76 1' 1/4"
 $\frac{225}{33.51}$

+25

✓

+50

✓

June 30, 1964 64
RT. 53

14

✓

33.1 33.8 34.4 37.6 38.3 39.1 39.3 38.8 38.6

11.5 10.8 10.2 7.0 6.3 5.5 5.3 5.8 3 6.0
20 12 9 3 11 24 37 43
GGV

32.8

32.1

42.9

41.0

38.4

39.0

→ 11.8 12.5
23 30

1.7 3.6 6.15 5.6
71 63 50 45
53

30.1

32.4

35.3

36.5

37.2

38.2

38.6

39.2

38.9

14.5 12.2 9.3 8.1 7.4 6.4 6.0 5.4 5.7
21 16 10 4 3 9 24 43

27.7

40.5

38.8

38.5

38.5

→ 16.9
27

4.1 5.8 6.1 6.1
78 67 63 55
Burn

35.2

36.2

36.9

37.7

38.6

39.3

39.2

38.7

38.6

9.4 8.4 7.7 6.9 6.0 5.3 5.4 5.9 6.0
56 47 35 17 24 46 66 76

40.5

39.2

4.1 5.4
86 80
Burn

Sta + π - Elev
~~44.56~~
~~944.99~~

63+75

✓

± W. Onosso at ± Arbogast 5.2 939.8

BM

3.91 ~~940.65~~
~~39.65~~ 940.67
~~4.91~~ 940.08 ~~940.10~~

BM 0.89 928.18

927.29
~~927.72~~

WS.

9.61 918.57

BM 4.19 958.95

954.76

66+60

+75 ±

5.30 953.65

June 30, 1966 65
RT 54

11

36.2 36.8 37.5 37.5 37.3 37.2 37.4 37.9 39.0
8.4 7.8 7.1 7.1 7.3 7.4 7.2 6.7 5.6
54 35 15 4 9 19 30 45

35.4

9.2
75

39.6

5.0
62

Spike in GP

R.R. Spike in 24" Oak S.W. Cor. Omass. St. & Arden
Lake Emily

Spike in Arc Light N.W. Cor. Pale + Omass.

52.9 53.0 51.3 51.1
6.03 7.06 7.73 7.86
14 25 31

52.9 52.1 51.3
6.10 6.85 7.72
77 59 41

Sta	+	π	-	Elev.
WS.	13.8	932.4		918.57

61

+50

62

+25

+50

+75

June 30, 1966

66
55

Lt

Lake Emily

✓
18.6 29.6
13.8 2.8
58 41
Lake

✓
18.6 27.0
13.8 5.4
50 36

✓
18.6 23.8 28.7
13.8 86 3.7
70 61 48

✓
18.6 27.0 28.9 30.4
13.8 5.4 3.5 2.0
83 67 62 55

✓
18.6 27.8 30.8 30.6
13.8 4.6 1.6 1.8
88 68 55 44

✓
18.6 26.3 25.5 30.2
13.8 6.1 3.9 2.2
86 70 62 52

Sta + K - Elev

932.4

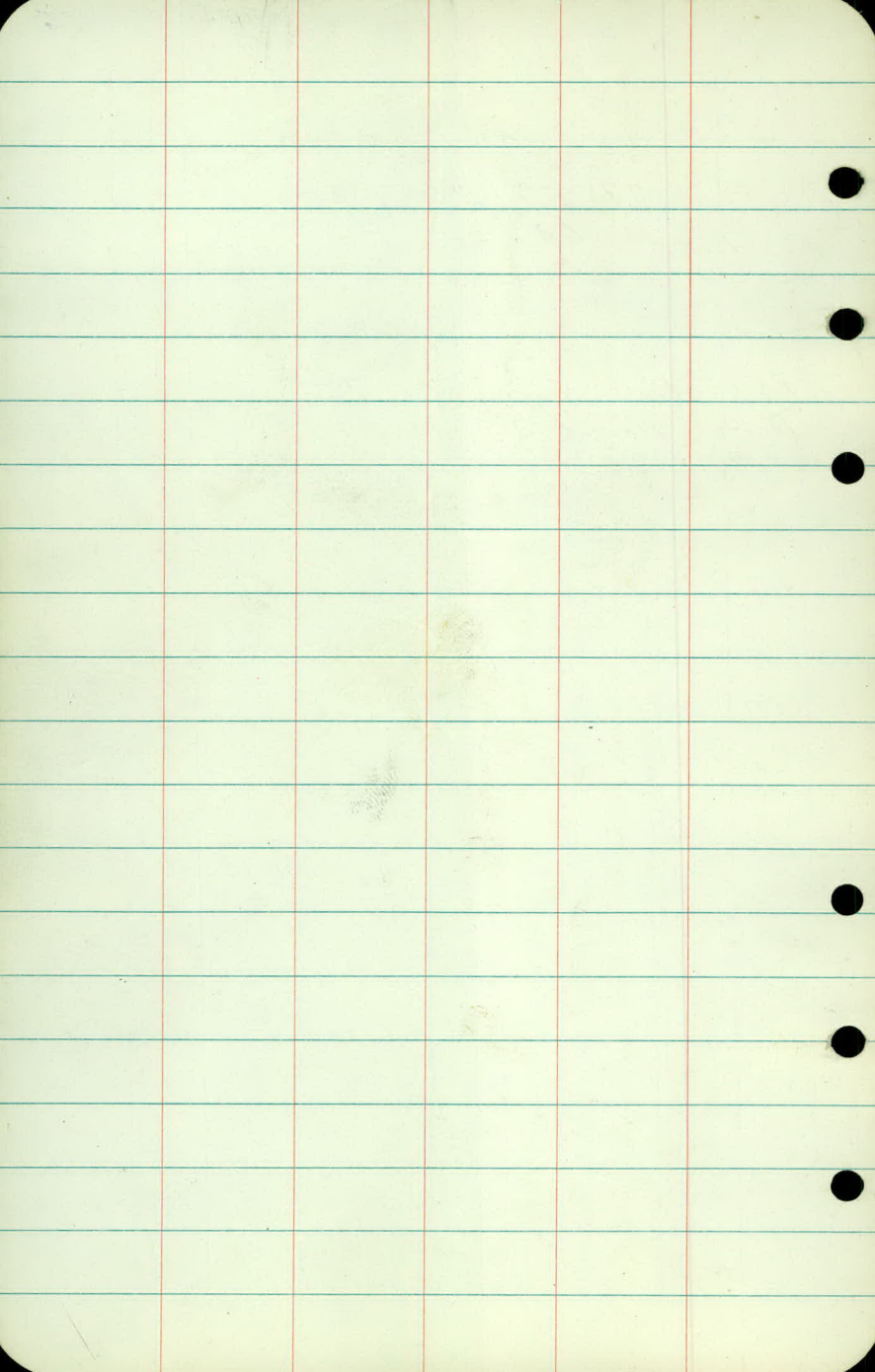
63

+25

June 30, 1966 67
56

14 18.6 24.7 26.7 28.8 30.4
13.8 7.7 5.7 3.6 2.0
94 71 64 55 43

18.6 22.0 22.3 24.0 24.6
13.8 10.4 10.1 8.4 7.8
104 76 62 51 39



68

/

Arbogast to East

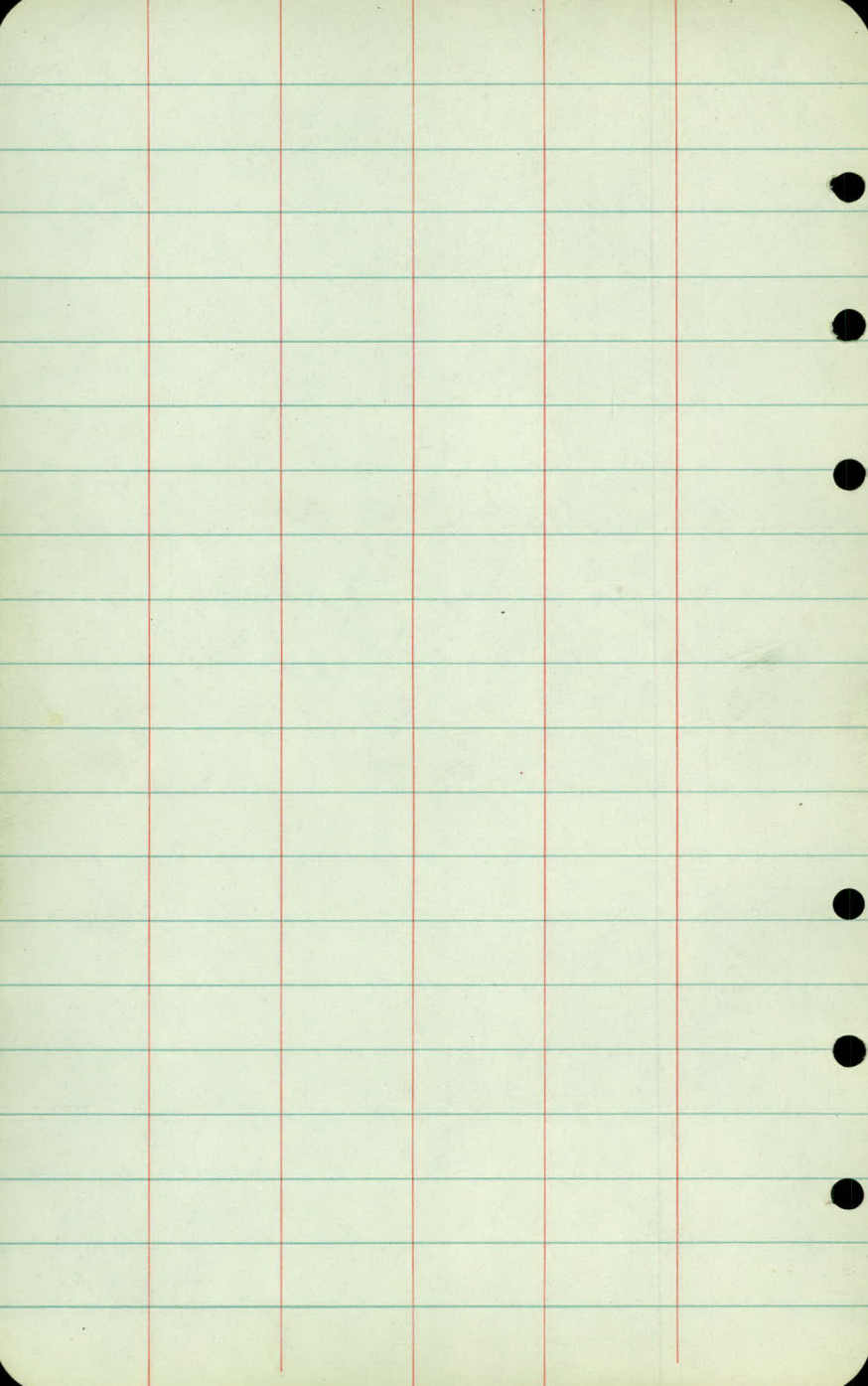
INDEX

Alignement 2

Topography 3-16

Dec. 6-15-64

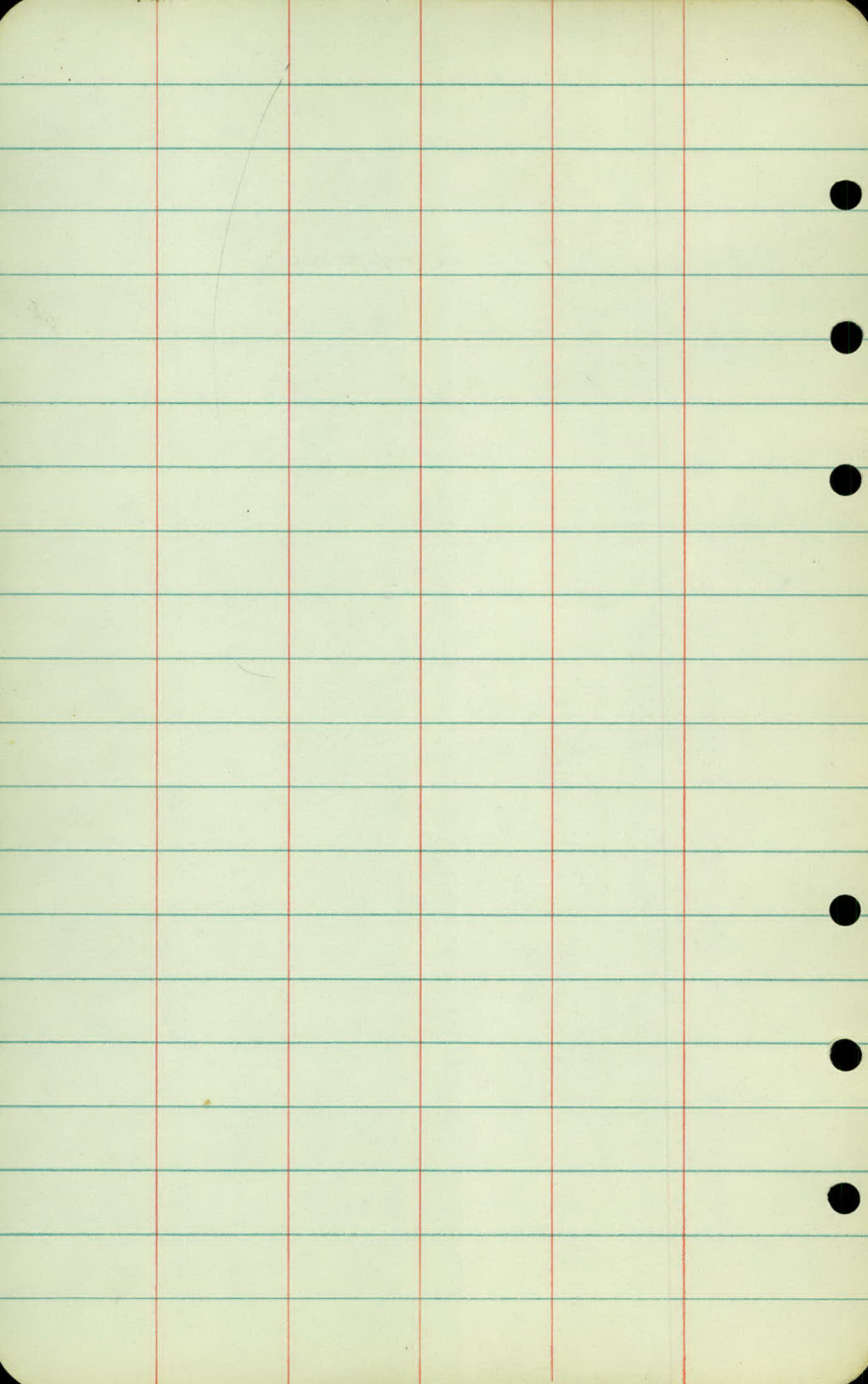
W. H. Johnson



Alinement

Same as Plan Survey

Pages 1-7 6/1937



Topography

+50

BT
13 23

+25 BT
14 23

65

+96 PP
29

BT
16 20

+50

BT
17-19

+25 BT
16-19

+105 MH (Tall)
16

64

BT
18-20

+91 Arch Ltr
32

+95 OP
29

+85 ER
20

+68 POR
31

+55 BR
49

+50

Road
23

+33 ER
34

Gas Main Angle

+41.5 14

+25 POR
21

+38 Gas M
2

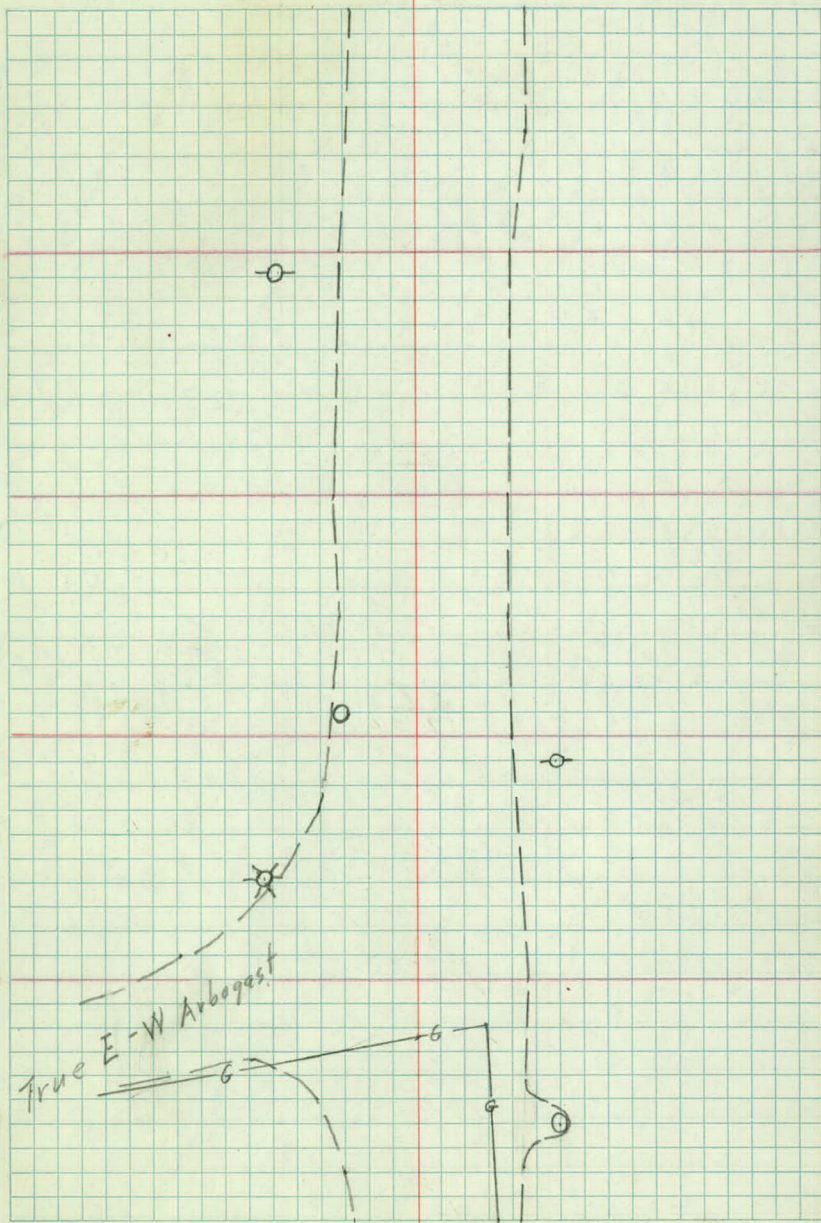
+20 C.B
30

+10 B.R
15

63

Road
13 22

Gas Main
17



68

$$\frac{BT}{19-17}$$

+50

$$\frac{B.T.}{16-18}$$

$$+25 \frac{BT}{16-25}$$

$$+15 \frac{PP}{51}$$

$$+25 \frac{PP}{24}$$

$$\frac{BT}{17}$$

$$\frac{Edge Ent}{63}$$

+14

Rtic E Edge Ent

2

67

$$+90 \frac{POR}{23}$$

$$+80 \frac{BR}{53}$$

$$+59 \frac{PP}{44}$$

$$+65 \frac{ER}{56}$$

$$+60 \frac{BT}{37}$$

$$+52 \frac{Begin Ent Rt}{31}$$

+50

$$\frac{BT}{19-24}$$

$$+42 \frac{SEC Ch List Pump}{28}$$

$$+42 \frac{MH (coll)}{18}$$

$$+40 \frac{BR}{19}$$

$$+25 \frac{BT}{20-23}$$

$$+20 \frac{PP}{37}$$

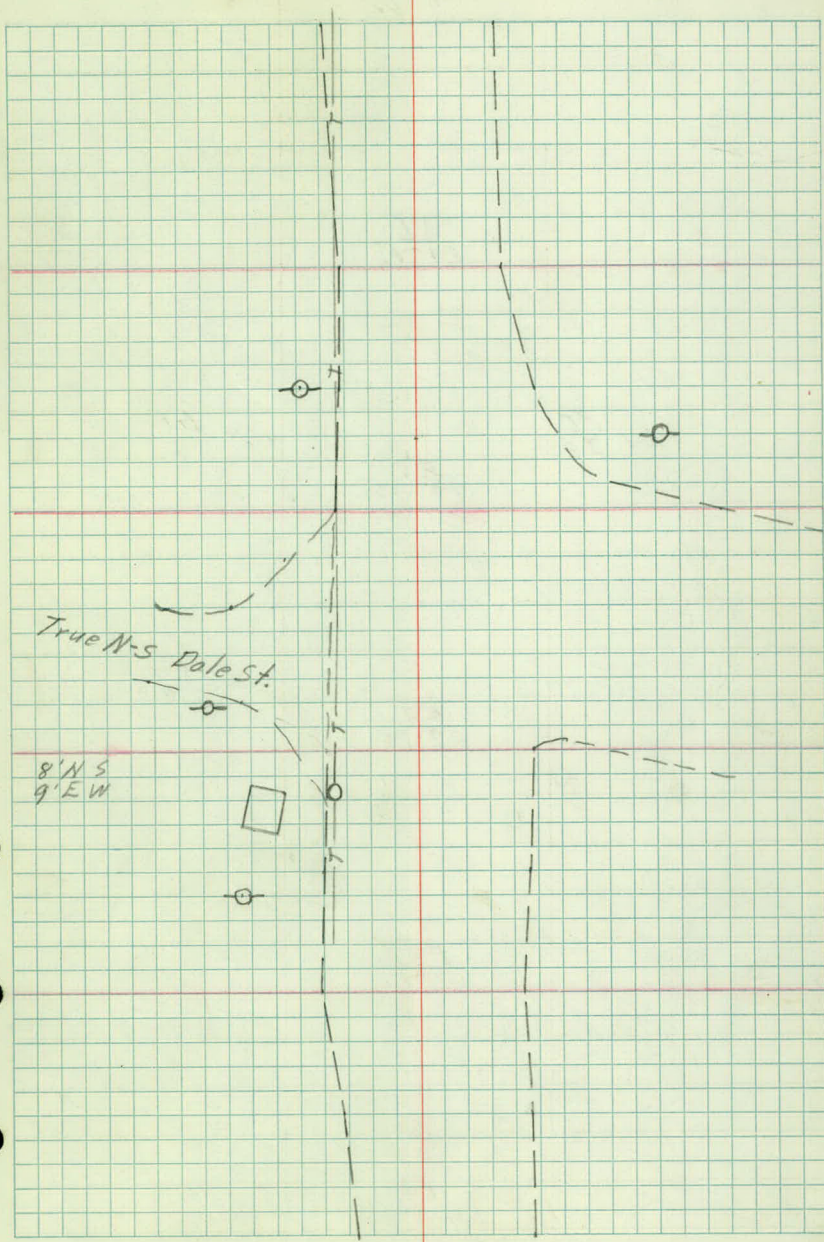
66

$$\frac{BT}{20-22}$$

$$+75 \frac{BT}{16-23}$$

65 + 50

$$\frac{BT}{13-23}$$



True N-S Dale St.

8' N S
9' E W

+50

BT
19 14

70

BT
21-13'

+66 MH (cell)
18

+60 PP
35

+60 GP
26

+50

BT
22-13

+03 R tie Ent R
BT
22-16

+10 Ent
34

69

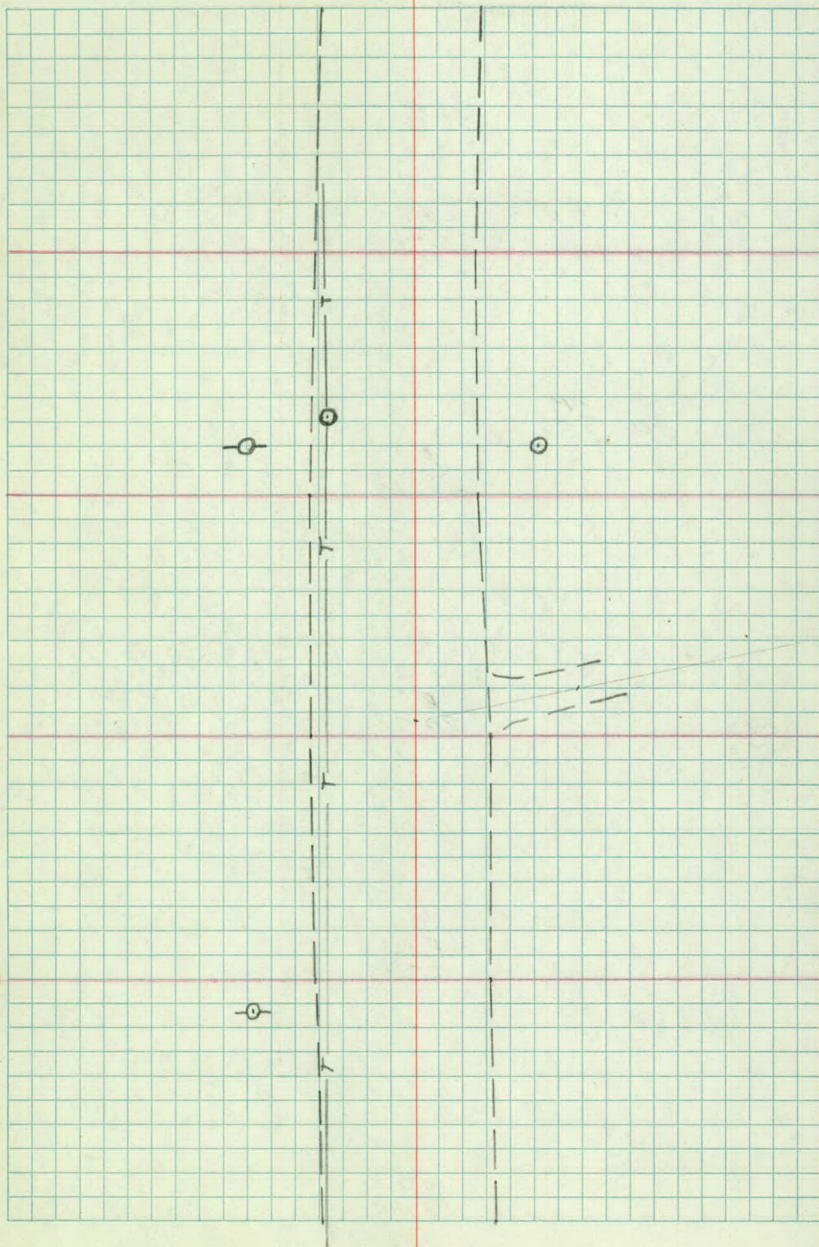
+50

BT
21-16

+43 PP
34

68

BT
19 17



73

$$\frac{BT}{24-12}$$

$$+90 \frac{PP}{46}$$

+50

$$\frac{BT}{24-11}$$

$$+02 \frac{PP}{32}$$

$$\frac{BT}{22-12}$$

72

$$+86 \frac{ER}{14}$$

$$+73 \frac{BR}{26}$$

+50

$$\frac{BT}{20-12}$$

$$+53 \frac{2 \text{ Keed}}{57}$$

$$+44 \frac{ER}{54}$$

$$+40 \frac{POR}{33}$$

$$+27 \frac{PB}{15}$$

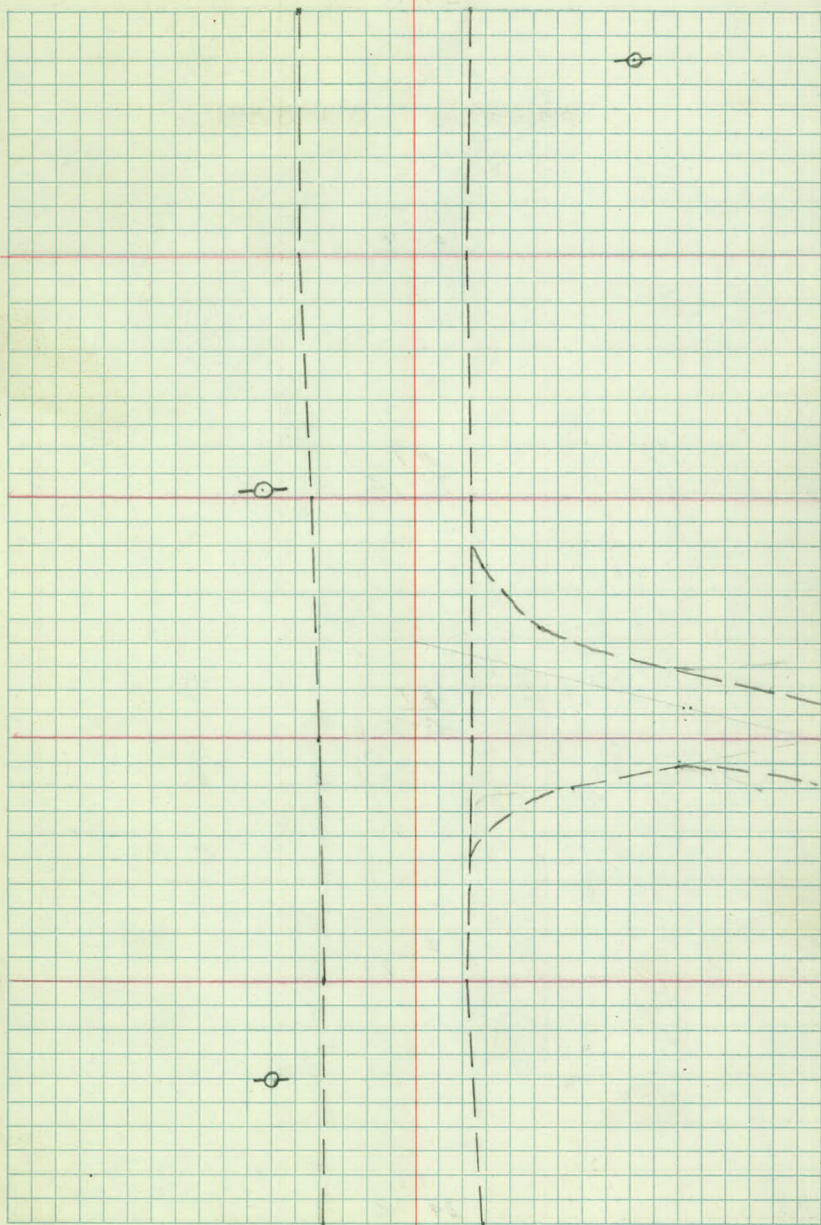
71

$$\frac{BT}{19-11}$$

$$+80 \frac{PP}{30}$$

$$\frac{BT}{19-14}$$

70+50



+50

B.T.
26 6

75

B.T.
24-8
+93 ^{MH} 44 ^{San}

PP
+50 32

74

BT
23-9

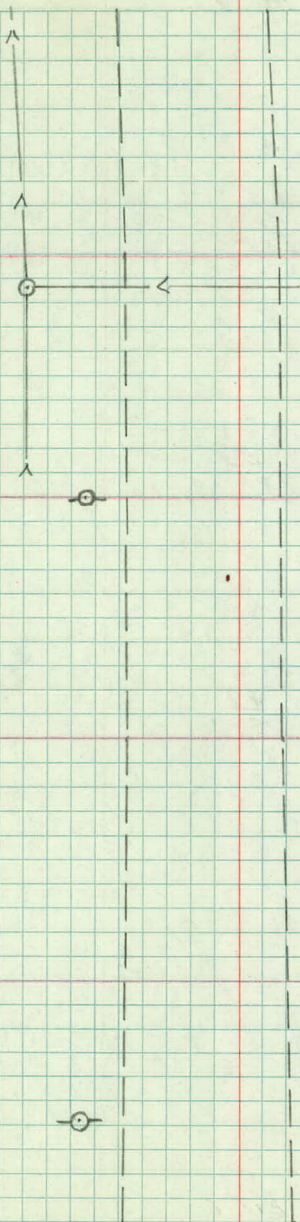
+50

PP
+21 33

73

24-12

8" Casting
Exc Cone
No. Ring



78

BT Fe Lake
14-19 38 67

+50

Fe
32

77

BT Fe Lake
22-14 35 62

+89 PP
37

+50

BT Lake
25-10 76

+55 Fe
39

Begin (72' chain link)

+06 MH (Tel)
23

76

BT Lake
26-7 100

+59 PP
23

S.E. 30' S.C.P.

+55 PP
42

+77 20

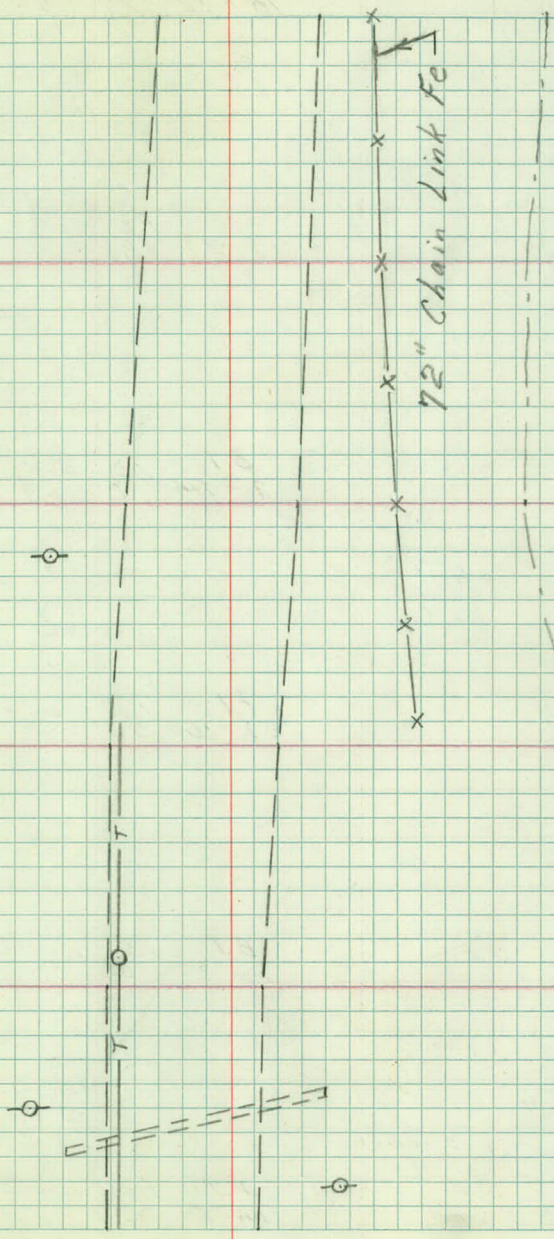
+66 NE 30' x 55' S.C.P.
34

BT Lake
26 6 110

75+50

Lake O WASSO

72" Chain Link Fe



BT	Fe	Lake
14-22	28	84

170 30
+ 36 $\overline{22}$ POR

$$+25 \overline{) BB}$$
$$+27 \frac{PV}{23}$$

80

10-21	Fe	Lake	
29		88	✓

450

BT	<u>Fe</u>	<u>Lake</u>
7-24	32	89

$$+36 \frac{PF}{1.3}$$

79

BT	Fe	<u>Loke</u>
7.24	30	86

+50

BT	Fe	Loko
9-24	30	79

#17 Arc Light
21

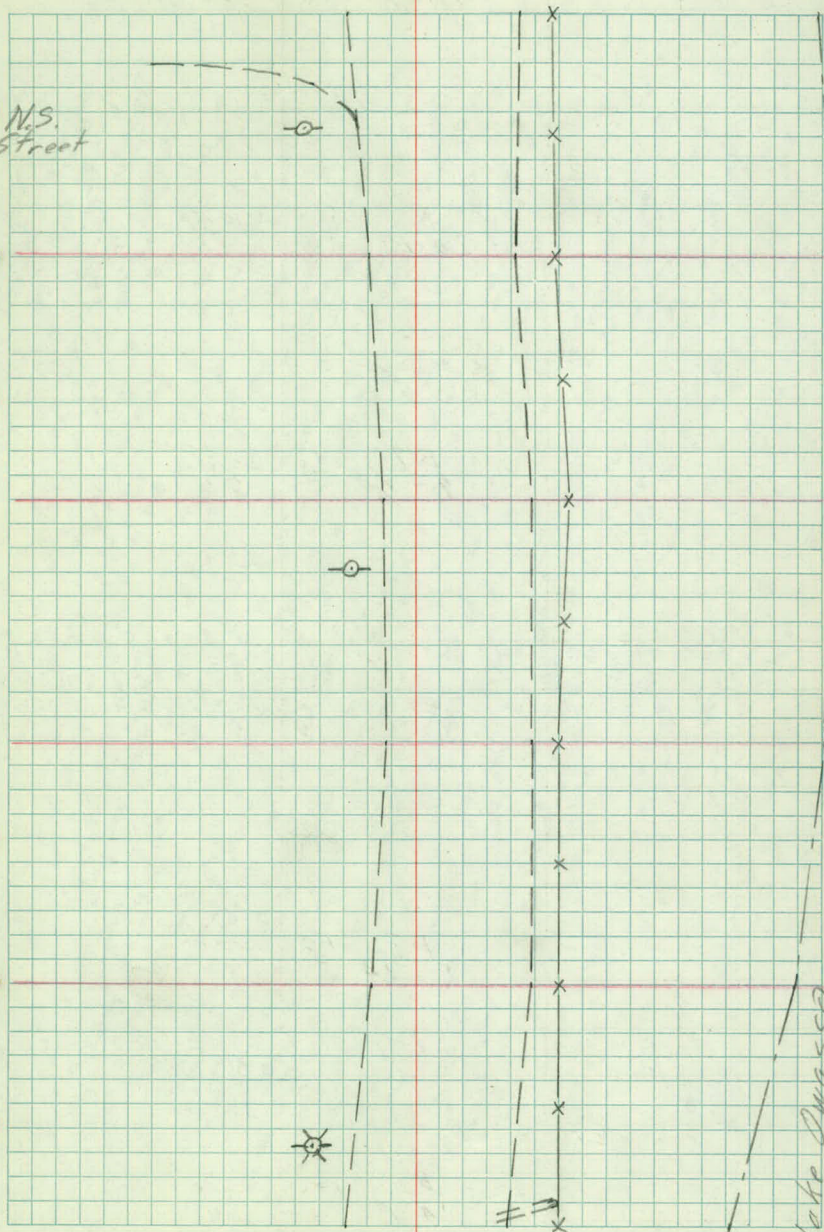
N. End Burried
12" CM

105 $\frac{SE12C}{30}$ M

78

BT	Fe	Lake
14-19	30	67

N.S.
Street



Let's Dress

83

✓

<u>BT</u>	Fe	Lake
21 16	38	88

✓
 +93 MH
 32

✓

+88 PP
 42

+50

<u>BT</u>	Fe	Lake
20 13	31	81

82

<u>BT</u>	Fe	Lake
20 14	29	76

+63 PP
 35

+50

81

<u>BT</u>	Fe	Lake
19 14	28	81

✓ +83 ER
 18

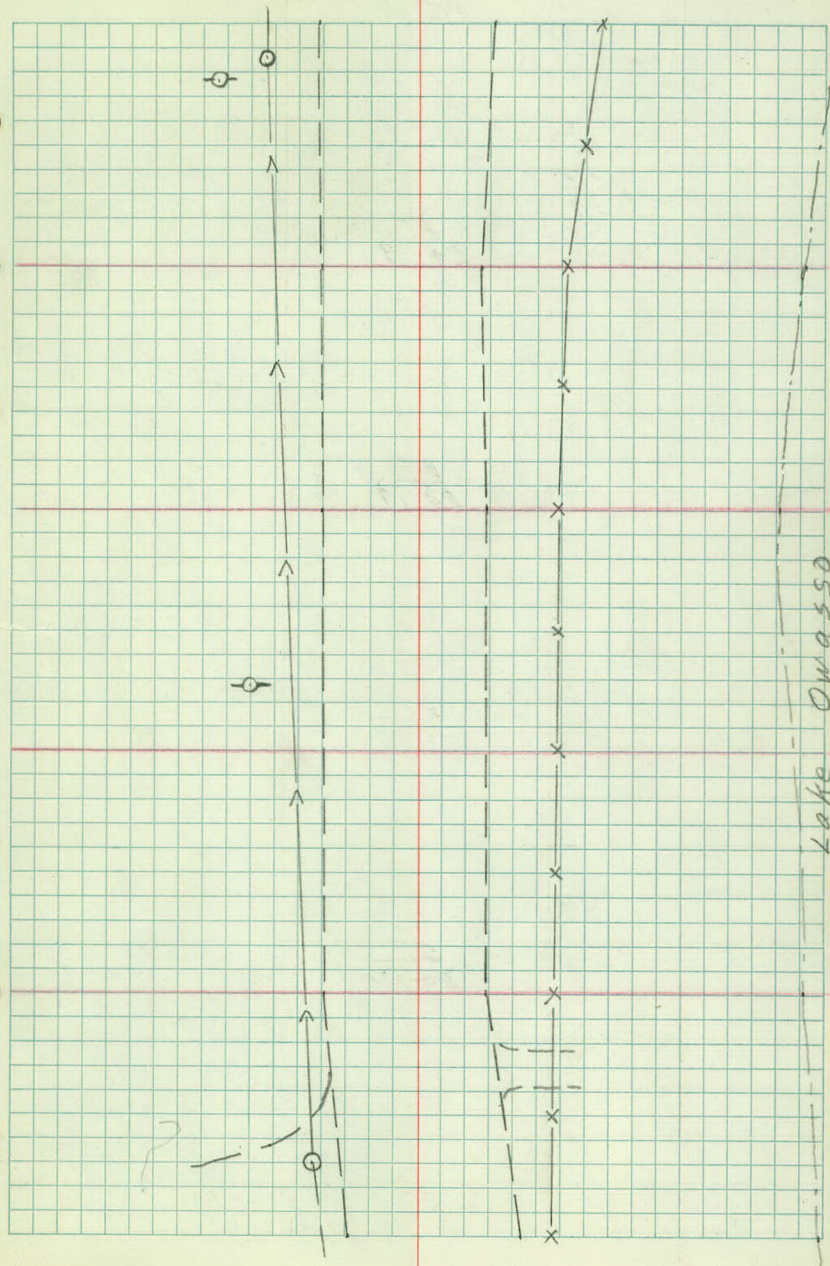
+84 Ent
 RT

+65 MH
 22

+68 BR
 31

80+50

<u>BT</u>	Fe	Lake
14 22	28	84



Lake Owasso

+50

Lake BT
80 25-17

+28 ER
19

+101 PP
39

+104 POR
29

85

Lake BT
69 24-19

+196 BR
88

+194 POR
59

+168 MH
36.5

+166 ER
83

+154 MH
38

+50

Lake BT
89 22-19

+159 POR
49

+40 POR
30

+18 POR
20

84

Lake BT
106 22-18

+75 Begin Lake
300

+94 MH
32

+79 Arc. Lite
43

+50

BT
22-16

+133 NWCR Bldg
45

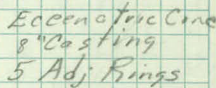
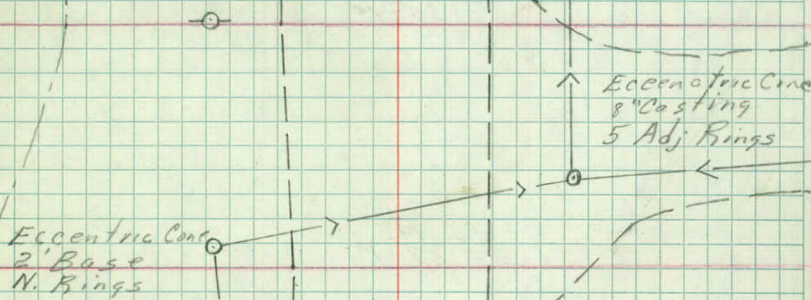
+23 PP
42

+29 End Fe Lake
44 97

BT Fe Lake
21-16 38 88

83

Lake Wabasso



88

Lake BT
60 21 14

+50

Lake BT
60 20-14

+32 $\frac{PP}{33}$

87

Lake BT
64 23-14

+79 $\frac{\text{Ent}}{17}$

+50

Lake BT
118 23 14

+06 $\frac{PP}{45}$

86

Lake BT
115 24-15

85+50

Lake BT
80 25-17

Late Mabase

0

11

0

+50

Lake
28

90

Lake BT
46 16-18

+68 PP
28

+50

Lake BT
60 17-18

+19 MH
225

89

Lake BT
57 20-14

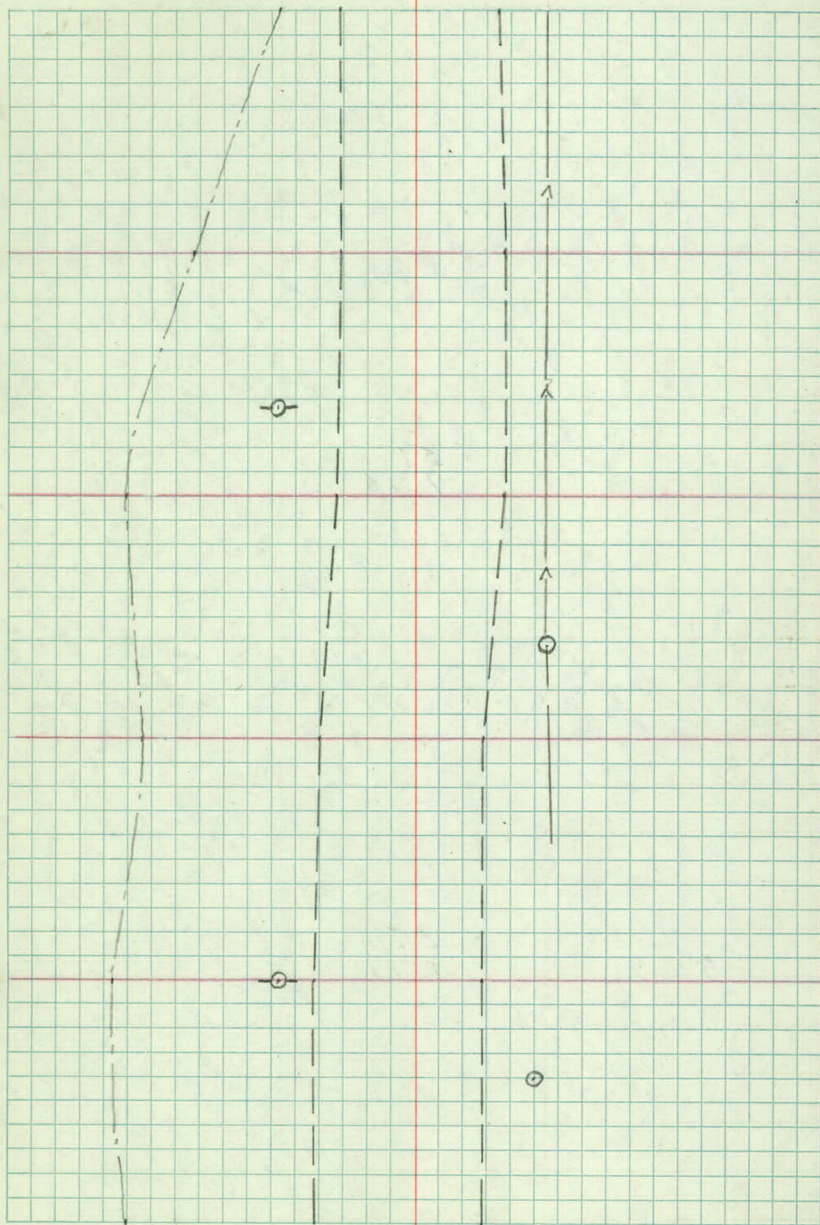
+50 PP
28

Lake BT
63 21-14

+30 GP
25

88

Lake BT
60 21-14



93

17-19

+71 $\frac{251}{82}$ E. Horseshoe

+50

+45 $\frac{Rtie}{St. Rt}$

+55 $\frac{PP}{87}$
+45 $\frac{MH}{26.5}$

92

+15 $\frac{PP}{23}$

$\frac{BT}{17}$ 18

+65 $\frac{Ent}{44}$

+77 $\frac{Rtie}{Ent \& Lt}$

+50

+17 $\frac{NE 24" CM}{27}$

H/A $\frac{SE 24" \times 53" CM}{25}$
+02 Ent + Rt

91

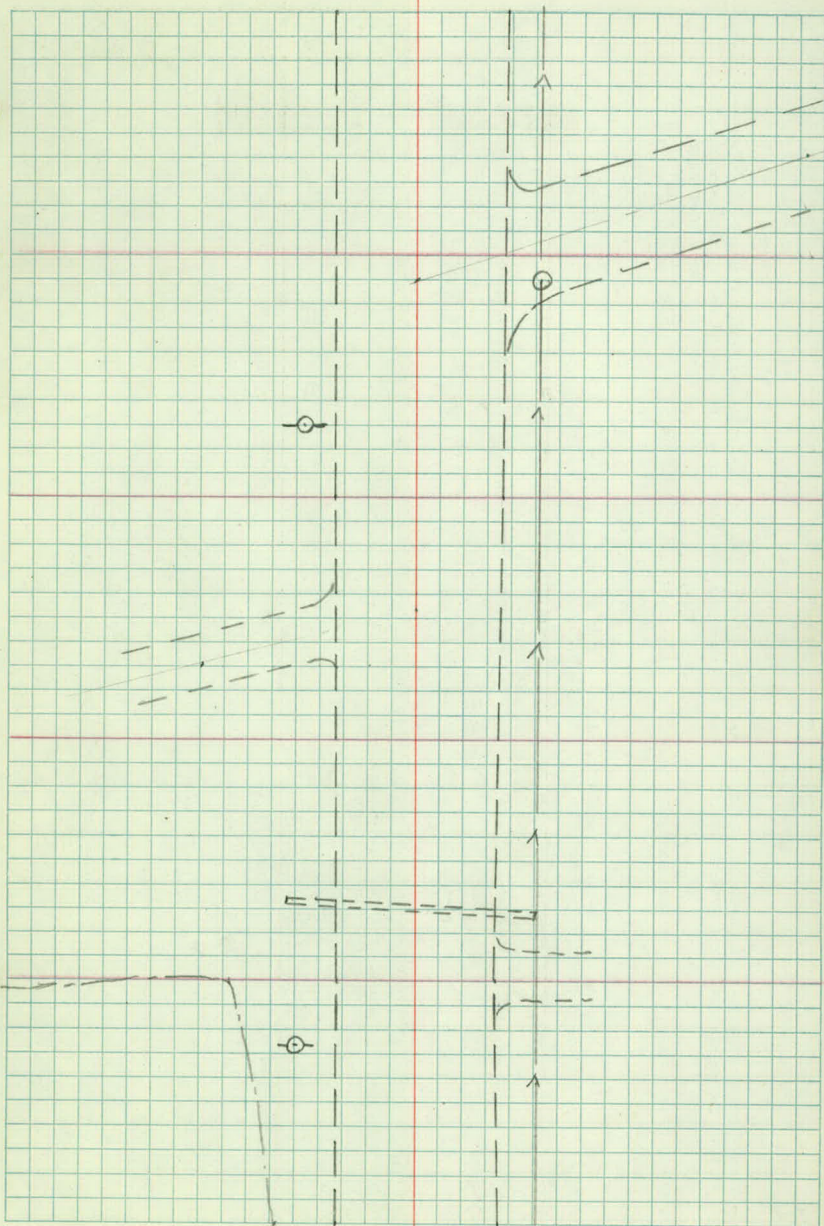
+00 $\frac{End Lake}{38}$

$\frac{BT}{16}$ 17

+87 $\frac{PP}{25}$

90+50

$\frac{Lake}{28}$



94

Road
22-19

+98 $\frac{RTie}{Ent}$

+86 $\frac{Ent}{37}$

+60 $\frac{MH(Tell)}{15}$

+27 $\frac{PP}{22}$

+26 $\frac{GP}{24}$

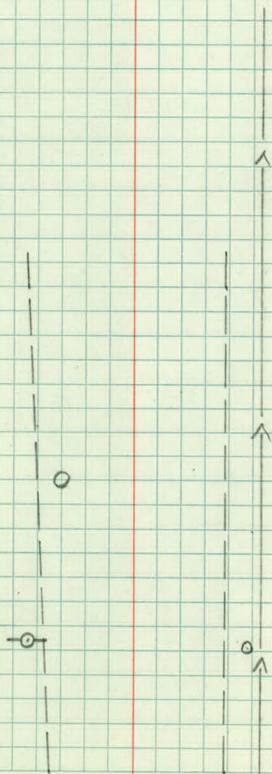
93

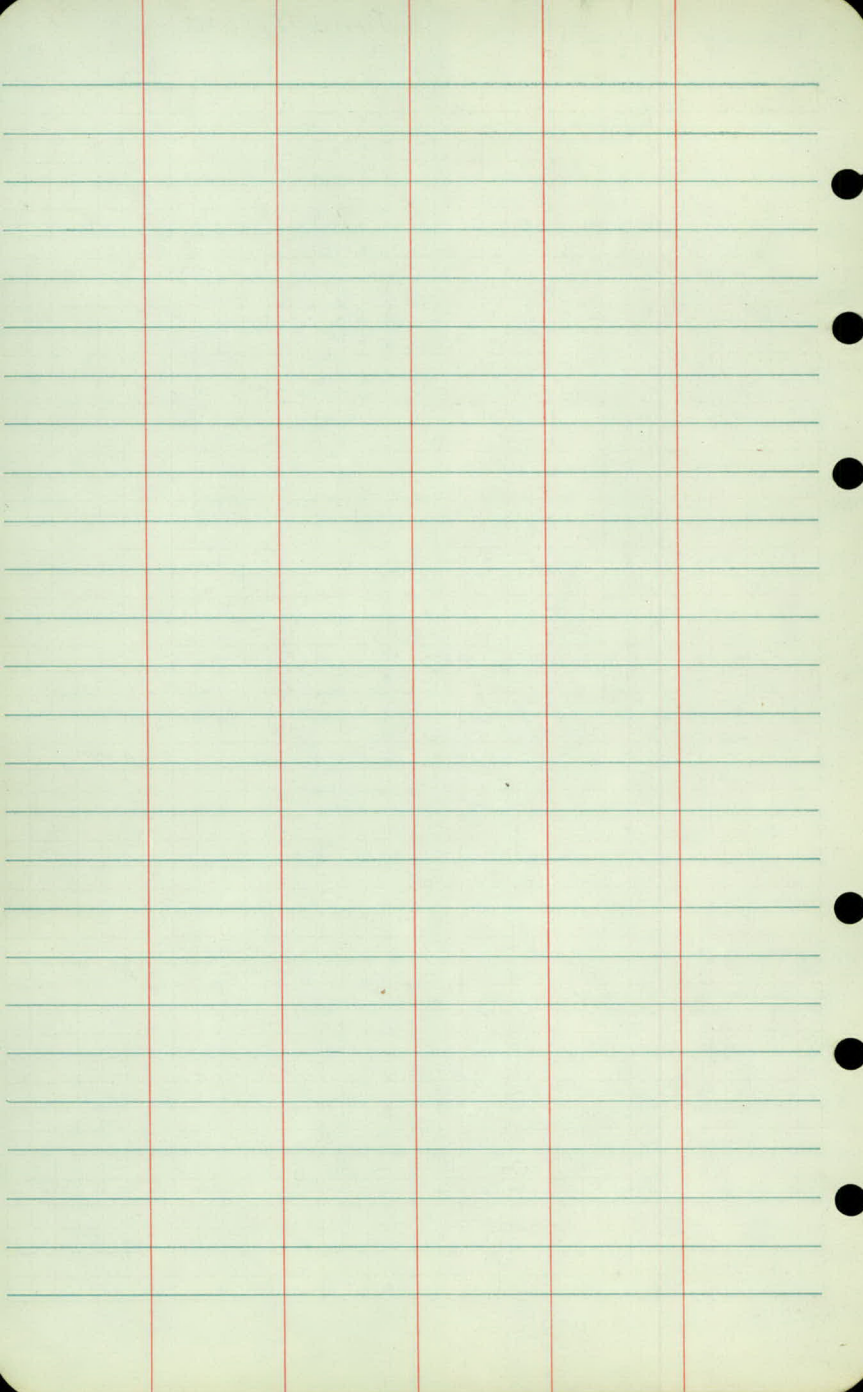
Road
17-19

FK
DS
TL
FK

June 15, 1964

83
16





June 19, 1964

84

NORTH OWASSO BLVD.

House Location

67+66

R. Tie Ho.

67+33

R. Tie Ho.

67+00	E. Cor. Ho
	133.6
67+00	N. Cor. Ho
	123.4

65+63

R. Tie Ho.

65+00	N. Cor. Ho
	118
65+00	W. Cor. Ho
	102.5

65+00

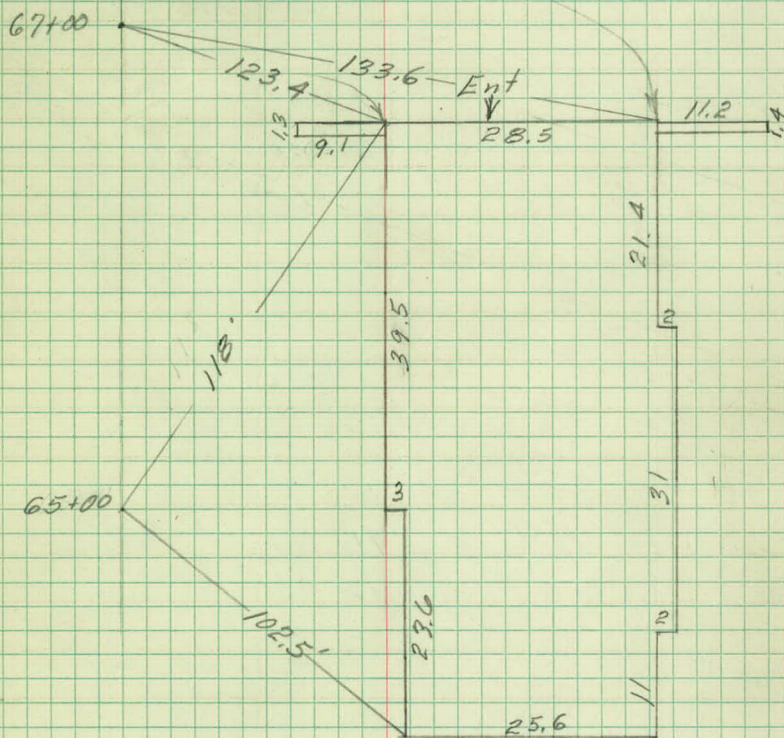
64+99

R. Tie Ho.

FK
TL
FK
H Lother

June 19, 1964

85
2

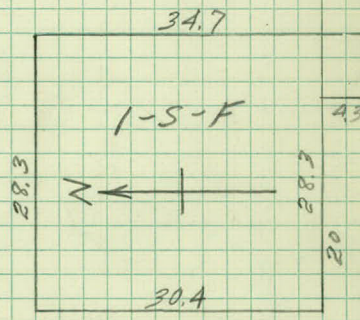
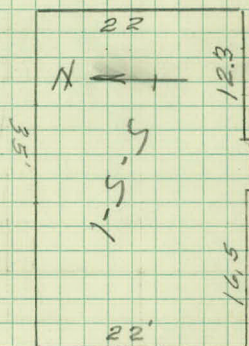


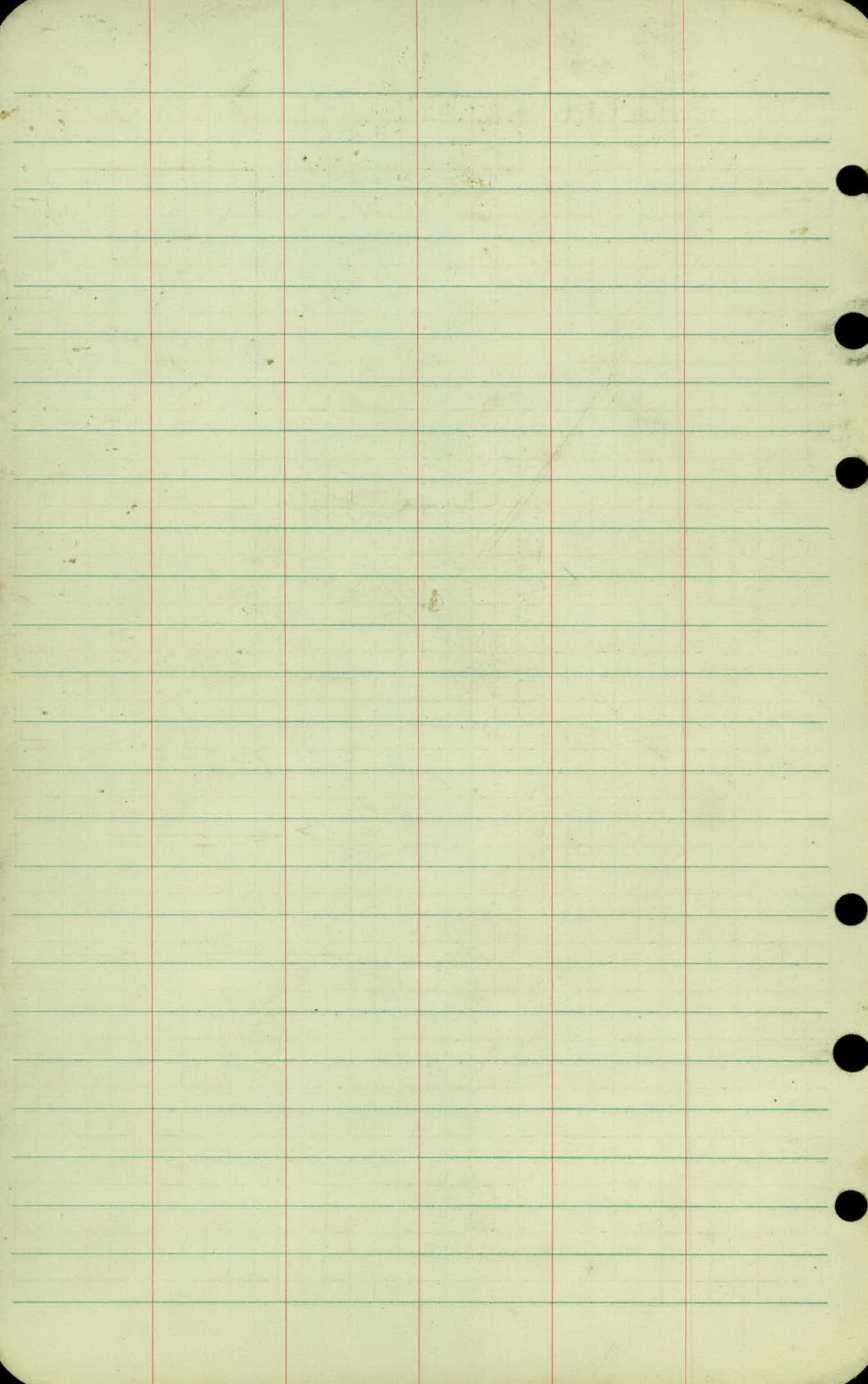
Az

X at PT
Sta 90+04.74
to Sta 93 0°00'

N.E. Cor Ho	62°45'	146'
N.W. Cor Ho	76°40'	141'
S.W. Cor Ho	76°50'	163'

NE Cor. Ho	125°30'	208'
SE Cor. Ho	119°50'	228'
NW Cor Ho	130°45'	230'





Locate House N.E. Omasso S
and

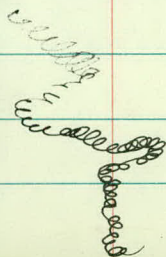
61+18.19

storm. sewer

61+27 S.E. Cor. Ho. Lt. 132.5

N - 38.3' - S

E - 38.5' - W





ELK RIVER CONCRETE PRODUCTS

DIVISION OF THE CRETEX COMPANIES, INC.

R. Terry Tambornino

Res. 943 Summit Avenue
Phone: 225-3650 (612)

Plant: 881-2615

OFFICE: 650 Builders Exchange
Phone: 336-2678

X-Section $\neq$ Ent
Rt Sta 66+60⁺

June 16, 1966 88

1

West Owasso Blvd.

~~ARBOGAST ST.~~ 63+51.87

33'

63

43' 30'

62

61

60

AZ Dist

π at PC 60+68.35
to E $\frac{1}{4}$ Co. Sec 35 90°

Lake shore of

Lake Emily! ~~151°~~^{209°} 127

" 207°40' 113

" 208°30' 95

" 200° 76

" 191° 65

" 182°30' 48

" 169°40' 46

" 137°20' 60

" 119° 93

" 109°30' 148

" 119°30' 202

" 124°40' 215

" 128° 232

" 129°30' 252

" 131°10' 276

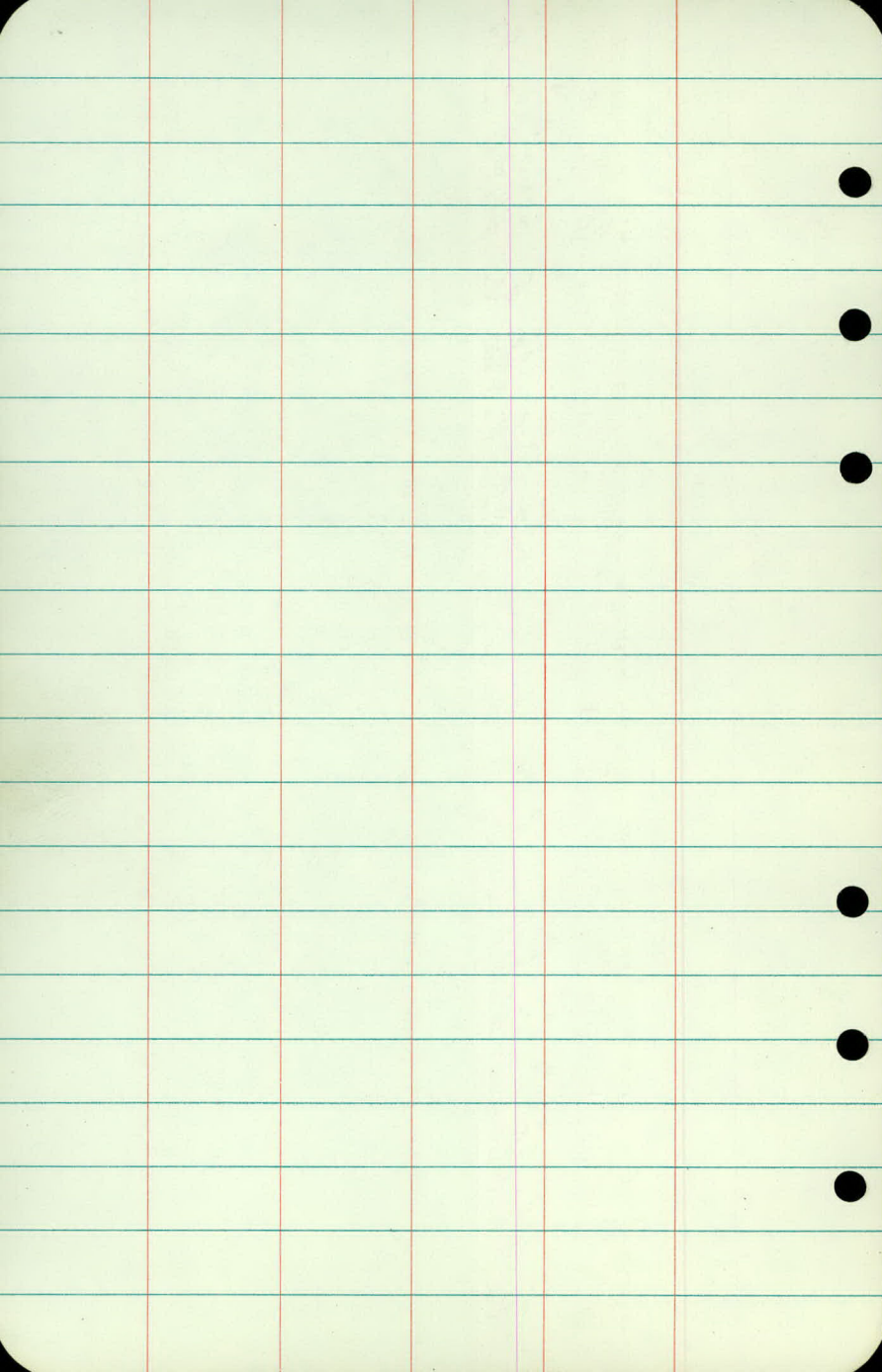
135°30' 305

FK
WJ
JT
JS

June 16, 1966 89
AZ Dist 2

Shore Line

140°	323
" 145°	350
" 148° 50'	373
" 154° 10'	428
" 158°	490
159° 20'	510
160° 20'	557
161°	588
161° 30'	616'
162° 10'	655
162° 20'	695
163° 05'	735



FK
WJ
JT
JS

June 17, 1966

90
3

TOPOGRAPHY

+50

Road
37

+40 ER
34

+38 Gas
3

+38 Cor Gas Main
36

+26 POB
11

+14 BR
7

+08 W. E 24" SCP
16

+22 CB
38

Shoulder Road
12 6 30

+12 Gas GV
25

63

+64 PP
17

+57 EC
27

+45 Curb
35

+38 BRC
54

+21 POC
50

Shoulder Road Curb
10 5 30

Gas M
23

62

+79 Begin Curb
26

+51 PP
16

Shoulder Road
11 8 23

61

+24 PP
16

Shoulder Road
13 9 23

60

+24 Wall
29

+06 Wall
29

+15 EG
45

59

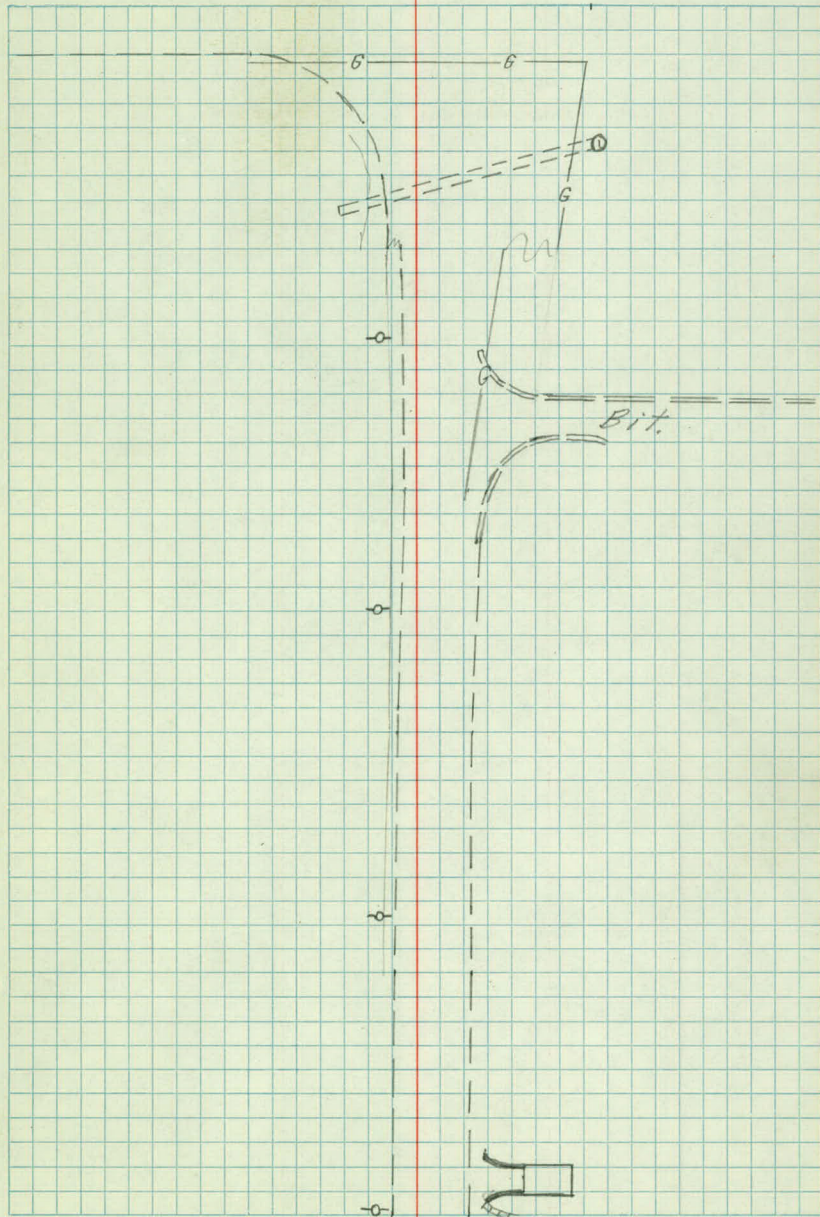
+02 PP
17

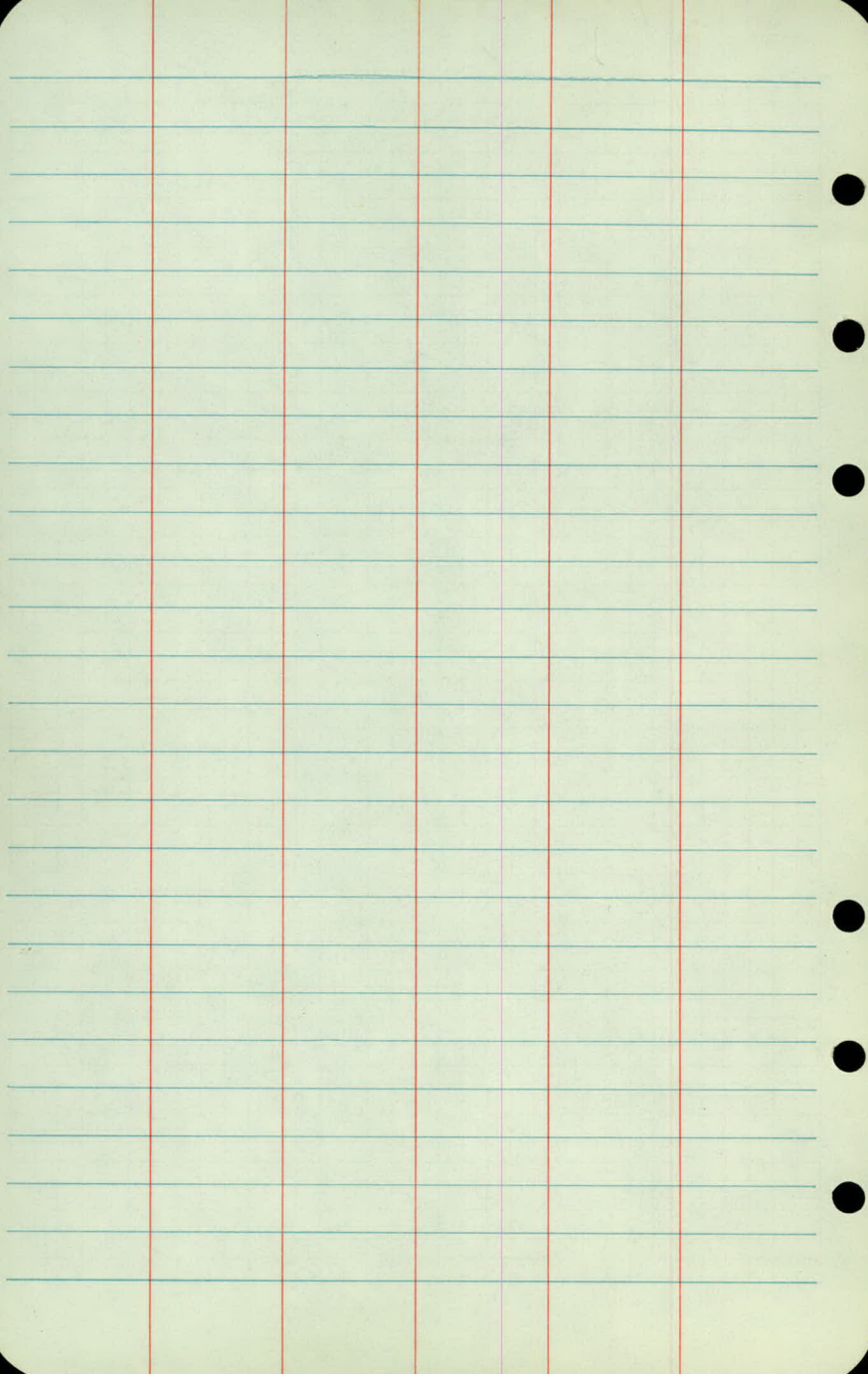
Rd
10 22

+04 Walk
28

June 17, 1966

91
4





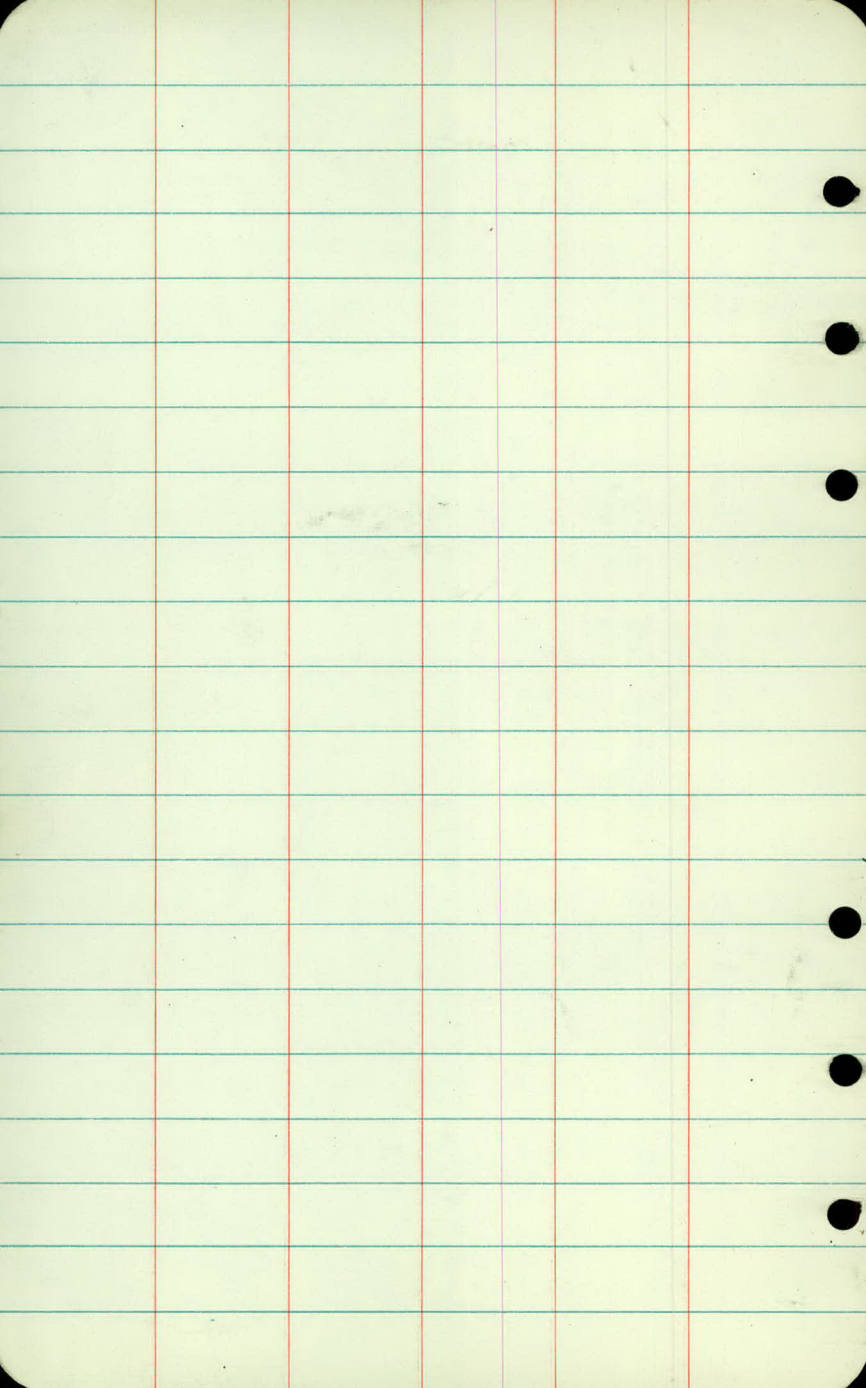
1937

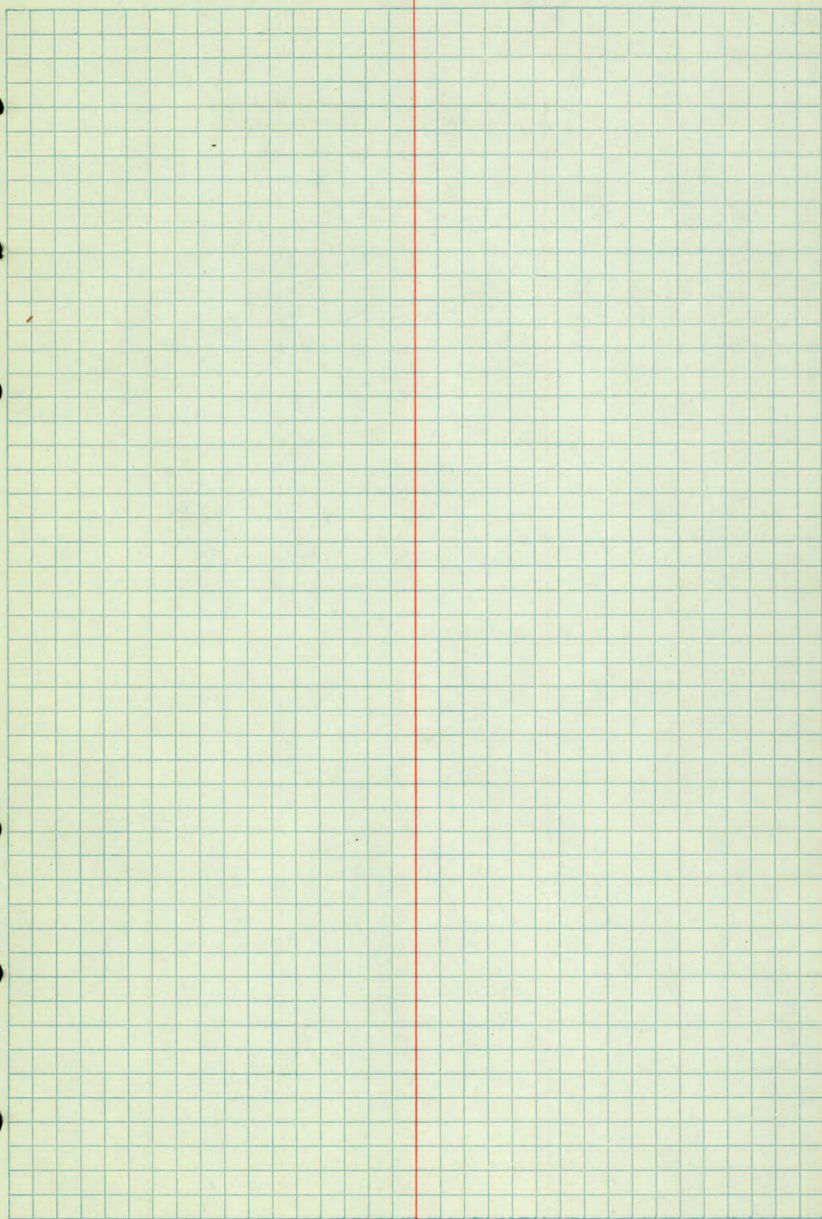
X-Section R&L 82+00 to 91

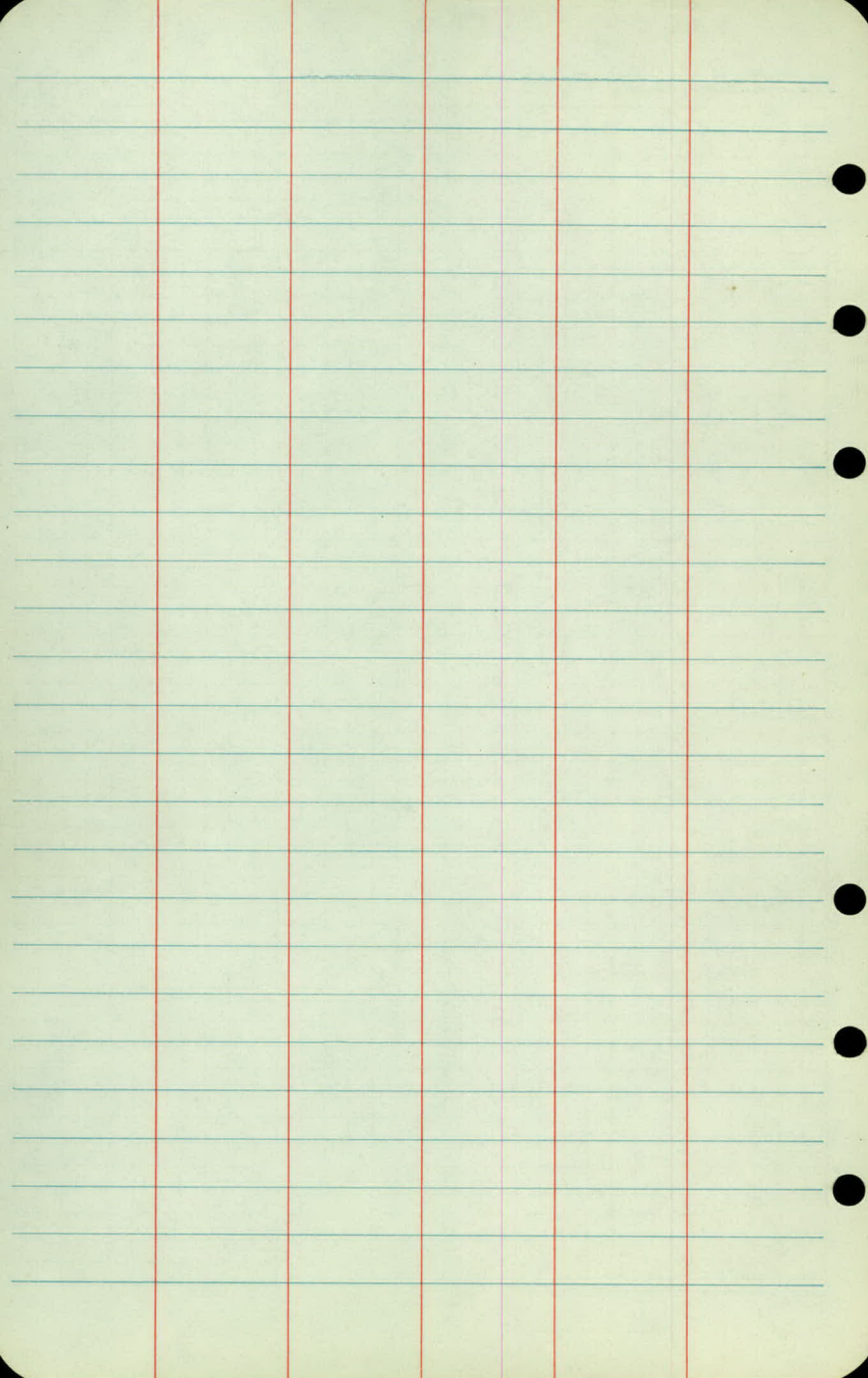
or 81+7191 "A" Line

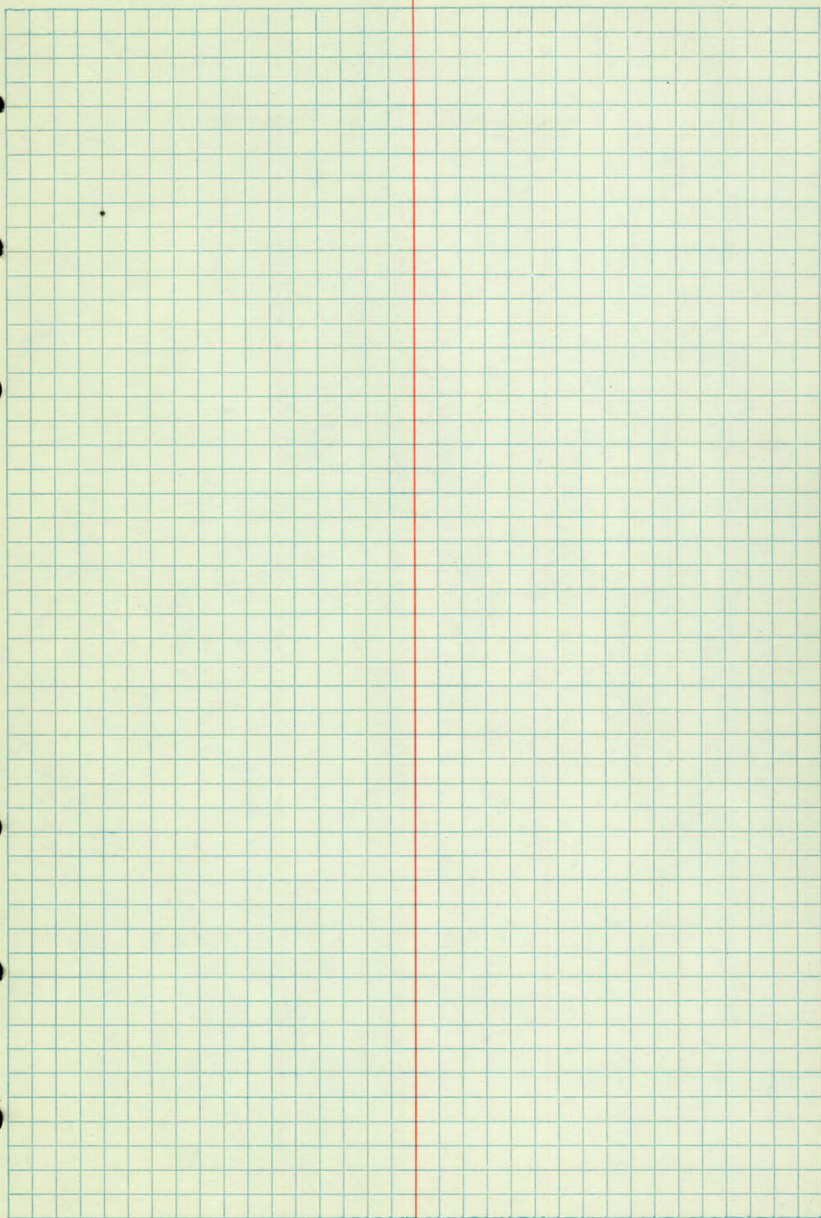
Elev of floor Barn

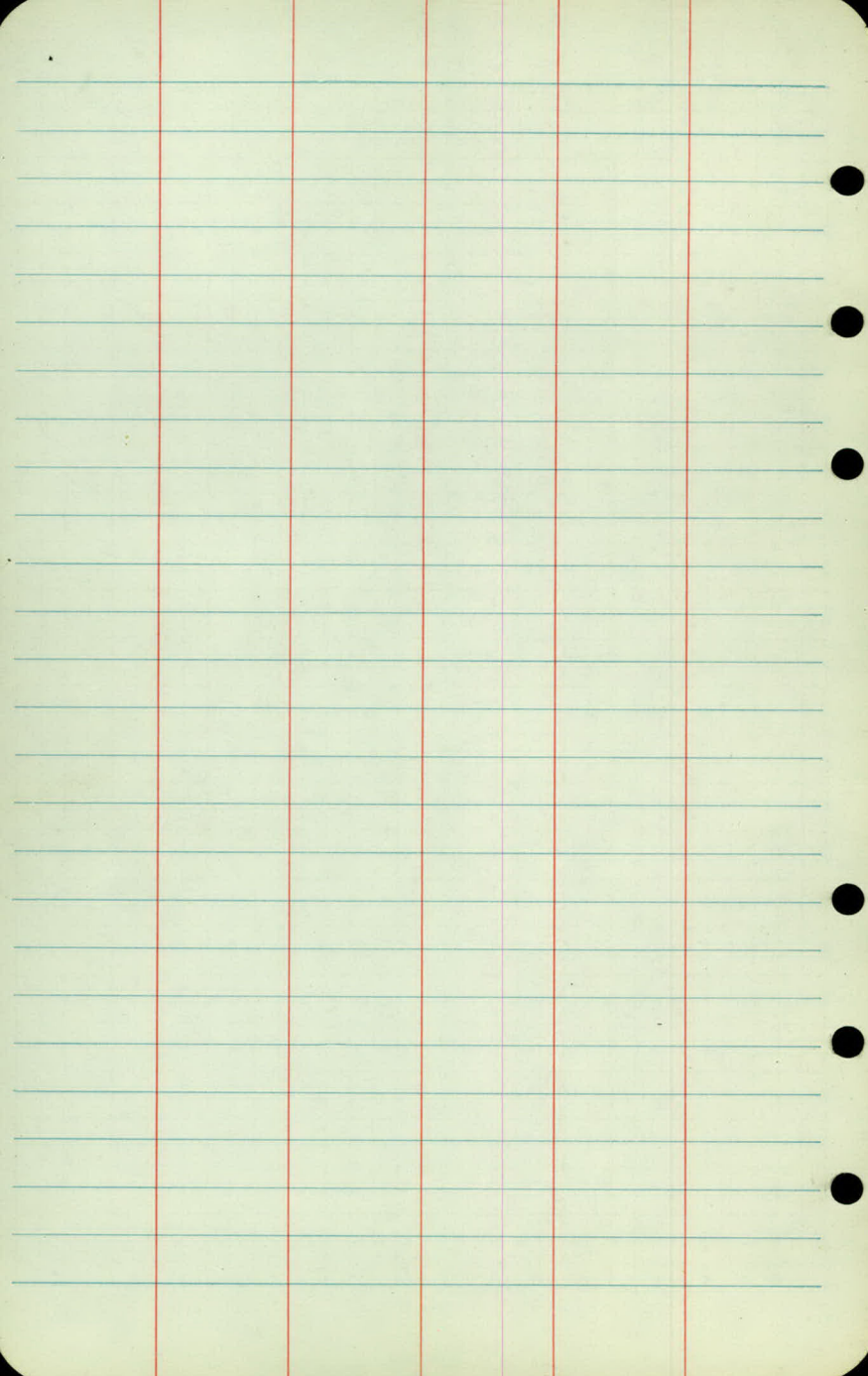
Elev of Pipe in barn

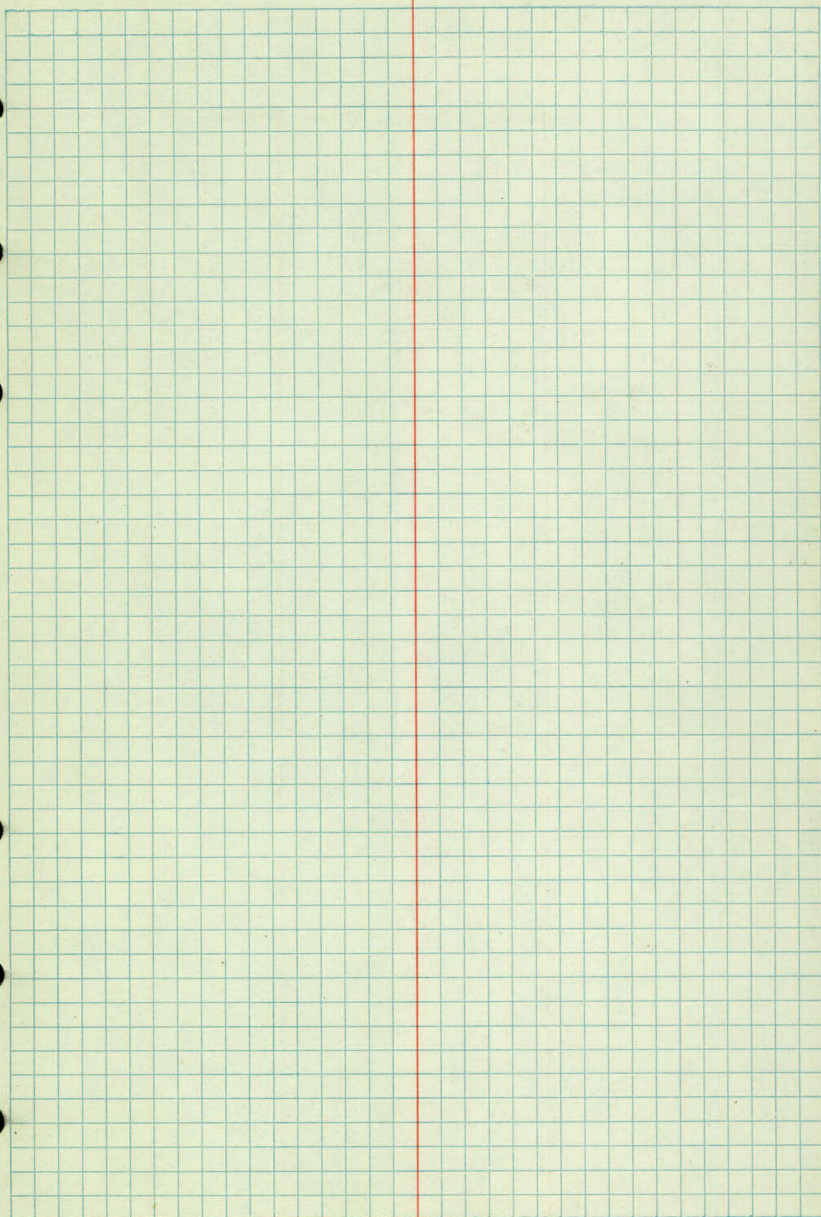


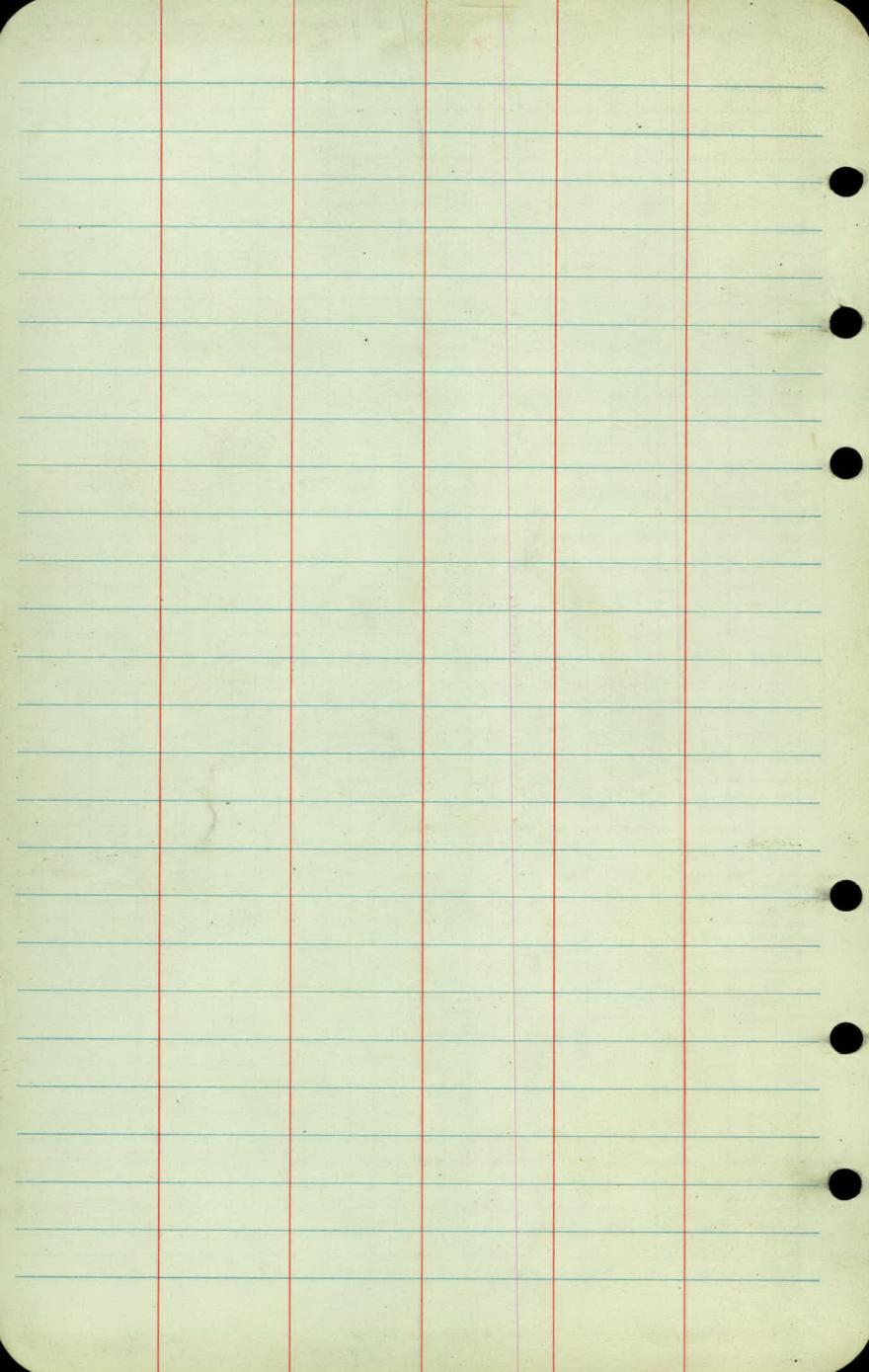












$$\begin{array}{r} 222.63 \\ 42 \\ \hline \end{array}$$

$$\begin{array}{r} 264.63 \\ 43.52 \\ \hline 308.15 \end{array}$$

$$(84 + 72) \text{ area} \quad 96$$

$$\begin{array}{r} 28 \ 54 \ 750 \\ 55 \ 15 \end{array}$$

$$L \quad 28^{\circ} 55' 15''$$

$$\begin{array}{r} 28 \\ 40 \\ \hline 1680 \\ 55.25 \\ \hline 1735.25 \end{array}$$

$$\begin{array}{r} 7.2302 \\ 240 \overline{) 1735.25} \end{array}$$

$$\begin{array}{r} 1680 \\ \hline \end{array}$$

$$87 + 39.26$$

$$\begin{array}{r} 86 + 89.24 \\ 43.52 \end{array}$$

$$\begin{array}{r} 552 \\ 480 \end{array}$$

$$\begin{array}{r} 725 \\ 720 \end{array}$$

$$\begin{array}{r} 500 \\ 480 \\ \hline 200 \end{array}$$

$$\begin{array}{r} 28 \quad 9.411615 \\ 1427 \quad 9.411092 \\ 327 \end{array}$$

$$\text{Log } \frac{725}{720} = 9.411419$$

$$1432 = 15 \ 59 \ 43$$

$$121$$

$$\begin{array}{r} \text{Log } R \quad 3.156064 \\ 9.411419 \end{array}$$

$$\begin{array}{r} 37.5 \\ 8.72 \\ 750 \\ 2625 \\ 3000 \\ \hline 327.000 \end{array}$$

$$\begin{array}{r} 2.567483 \\ 7379 \\ \hline 104 \end{array} = 369.39$$

$$\begin{array}{r} 540.87 \\ 210.32 \end{array}$$

$$\begin{array}{r} 26.72 \\ 53 \\ \hline 1.8 \end{array}$$

$$330.55$$

$$80 + 88.99$$

$$84 + 19.54$$

$$246.26$$

$$81573.28$$

$$\begin{array}{r} 482.01 \\ 445.52 \end{array}$$

over for 50

$$\begin{array}{r} 5.29 \\ 2.529 \\ \hline 5.29 \\ 5.29 \\ \hline 9.522 \end{array}$$

$$\begin{array}{r} 213.76 \\ 26.72 \\ \hline 48.096 \end{array}$$

059185
30

Log R = 3.059155

5°R = 1145.92 Log 1/2 = 9.411419

2.470574
27
14

295.51

28
+ 60
1680
55.25
1735.25

2
578.416

300 | 1735.25
1500
2352
2100

9.411419
2.979973
2.391392
246.26

2525
2400
1250
1200
500
300
2000

482014
360 | 1735.250
1440
2952
2880
725
720
500
360
360.250

$$\begin{array}{r}
 22^{\circ} 34' 30'' \quad 526 \\
 80 \quad 43 \quad 2^{\circ} 43' \\
 \hline
 190 \quad 51 \quad 30 \quad (67 + 41.55) \quad (62)
 \end{array}$$

$$R = 636.62$$

$$\begin{array}{r}
 636.6 = 803867 \\
 \quad \quad 136 \\
 \hline
 8038806
 \end{array}$$

$$\text{Log } R = 2.803881$$

$$\text{Log Tan } 9^{\circ} 55' = 9.242610$$

$$\begin{array}{r}
 9.243178 \\
 2.803881 \\
 \hline
 2.047059 \\
 6885 \\
 \hline
 174
 \end{array}$$

$$\begin{array}{r}
 12.4 \\
 45 \\
 \hline
 420 \\
 492 \\
 \hline
 568.0 \\
 142 \\
 \hline
 710
 \end{array}$$

$$111.44$$

$$\begin{array}{r}
 \Delta \\
 L \quad D \quad \frac{60}{54}
 \end{array}$$

$$\begin{array}{r}
 19 \\
 60 \\
 \hline
 1140 \\
 51.5 \\
 \hline
 1191.5'
 \end{array}$$

$$\begin{array}{r}
 2.20648 \\
 540 \overline{) 1191.5} \\
 \underline{1080} \\
 111.5 \\
 \underline{1080}
 \end{array}$$

$$67 + 41.55$$

$$111.44$$

$$66 + 30.11$$

$$220.65$$

$$6850.76$$

$$3500$$

$$3240$$

$$2600$$

$$2160$$

$$4400$$

$$4320$$

29.89

9' 1" K

2.7

20923

5978

80.703

4° 30' / 100'

2° 15' / 50

1° 7.5' / 25

1.26

2.7

532

152

2.052

19.89

6' 2.7

13923

3978

53.703

$$1225 = 9.342757$$

150

$$9.342907$$

$$\log R = 3.156064$$

$$9.342907$$

$$12.498971$$

28

$$315.5_2$$

$$T = 315.48$$

$$10.02$$

15

$$5010$$

$$1502$$

$$150.30$$

6.

12

60

720

1440

50.5

$$1490.5$$

$$78+85.28$$

$$315.48$$

$$75+69.80$$

$$621.04$$

$$81+90.84$$

$$240 \overline{) 6,210.40}$$

$$1440$$

$$505$$

$$480$$

$$250$$

$$240$$

$$1000$$

$$480$$

$$200$$

$$315.48$$

$$295.51$$

$$610.99$$

$$295.51$$

$$252.38$$

$$547.89$$

$$3.059155$$

$$9.342907$$

$$2.402062$$

$$252.4$$

$$252.38$$

$$2.979959$$

$$2.979973$$

$$9.342907$$

$$2.979973$$

$$2.322880$$

$$210.32$$

$$76+74.96$$

$$414.03$$

$$80+88.99$$

24 50 30
60

29
1440

13.36

4.60 } 170.0
1380
3200

414.03
360 } 1490.5

1440
505
360
1450
1440
1000
1080

25
B 36
150.24
7572
90.144

1.8
3.6
40
144.0 2024'

31.8
40
72.0

25.04
1.8
20032
2504
45.072

414.03
1.8
331220
41403
745.254

12
60 } 745.25
60
145
120
252

27
38.99
1.8
31192
3899
70482

1.8
340
72.0
60
12

6"
30'/100
1°30'/50'
45'/25'

Owasso Blvd. North

Sta + π - Elev.

BM 3.83

80+13 MH 4.44

+29 MH 5.10

+49 MH 4.74

+49 F.L. Culv 7.45

+14 F.L. Culv 6.74

81+00 "A" Line 4.85

82+00 "A" Line 5.05

82+00 "B" Line 5.49

FK
JT
JD
PA

July 15, 1966

100
2

Spike in R.P. N.W. Cor. Chandler Dr.

Rt 20'

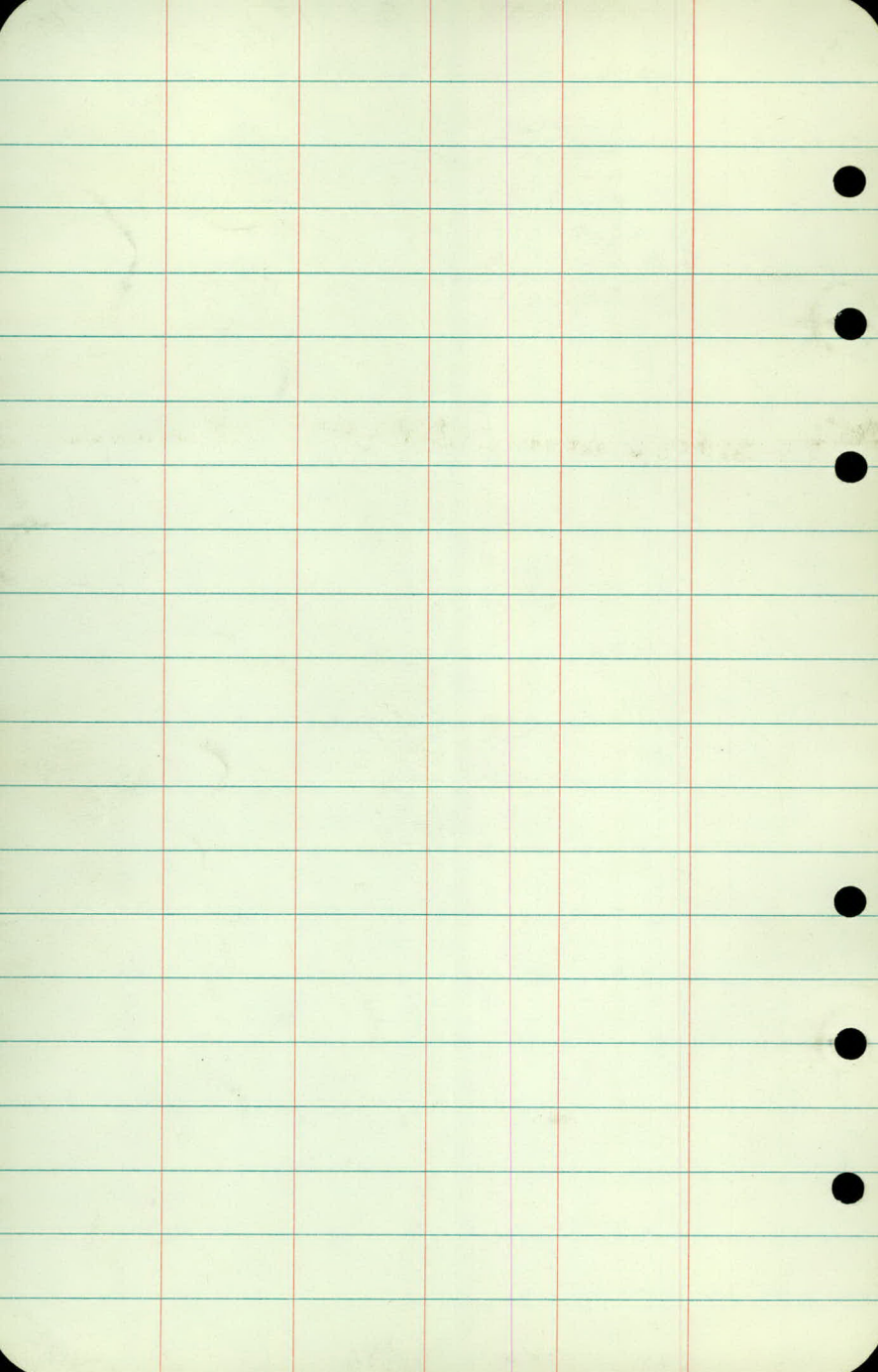
Rt 8'

Rt 6.5

Lt 10'

13.5
6.5
20.0

Lt 2'



Bench Levels

Victoria & E

to

Lake Owasso Pump

The levels herein for Owasso Pump
No. are raised 0.97' to conform to
Lake Owasso Lake Improvement datum.

K.A. - 7-8-66

Rec. 7-7-66

Sta	+	-	Elev
BM	4.69	958.68	953.99
T.P.	11.34	969.45	958.11
T.P.	3.78	970.54	966.76
T.P.	2.44	964.97	962.53
T.P.	1.14	953.38	952.24
T.P.	4.07	947.03	942.96
T.P.	1.26	943.81	942.55
T.P.	1.81	935.12	933.31
T.P.	4.93	933.09	928.16
BM		6.77	926.32
T.P.	8.61	938.75	930.14
T.P.	10.59	949.01	938.42
T.P.	7.70	956.06	948.36
BM		2.68	953.38
T.P.	0.01	942.50	942.49
T.P.	0.96	930.17	929.21
T.P.	0.83	917.99	917.16
T.P.	0.97	905.95	904.98

FX
JT
JS
PA

July 6, 1966

102

2

Top of S.W. Bolt on Crossing Signal
SE. Cor. Victoria & R.R. at "E."

center line of Harriet & Victoria

center line of Arbogast & Victoria

Owasso St. 100' North of E Arbogast

R.R. Spike in 24" Oak S.W. Cor. Owasso St & Arbogast

center line of W. OWASSO BLVD. E' ARBOGAST

66 + 00

Spike in Archlight, N.W. corner
of DALE ST. & OWASSO BLVD

STA	+	Δ	-	ELEV.
		905.95		
		12.40		
T.P.	1.34	894.89	12.40	893.55
		3.90		17.34
T.P.	6.76	897.75	3.90	890.99
		3.45		10.10
T.P.	5.87	900.17	3.45	894.30 895.26
		5.81		5.87
T.P.	2.51	896.87	5.81	894.36
		6.33		2.51
BM			6.33	890.54 891.51

891.51

JULY 6, 1966

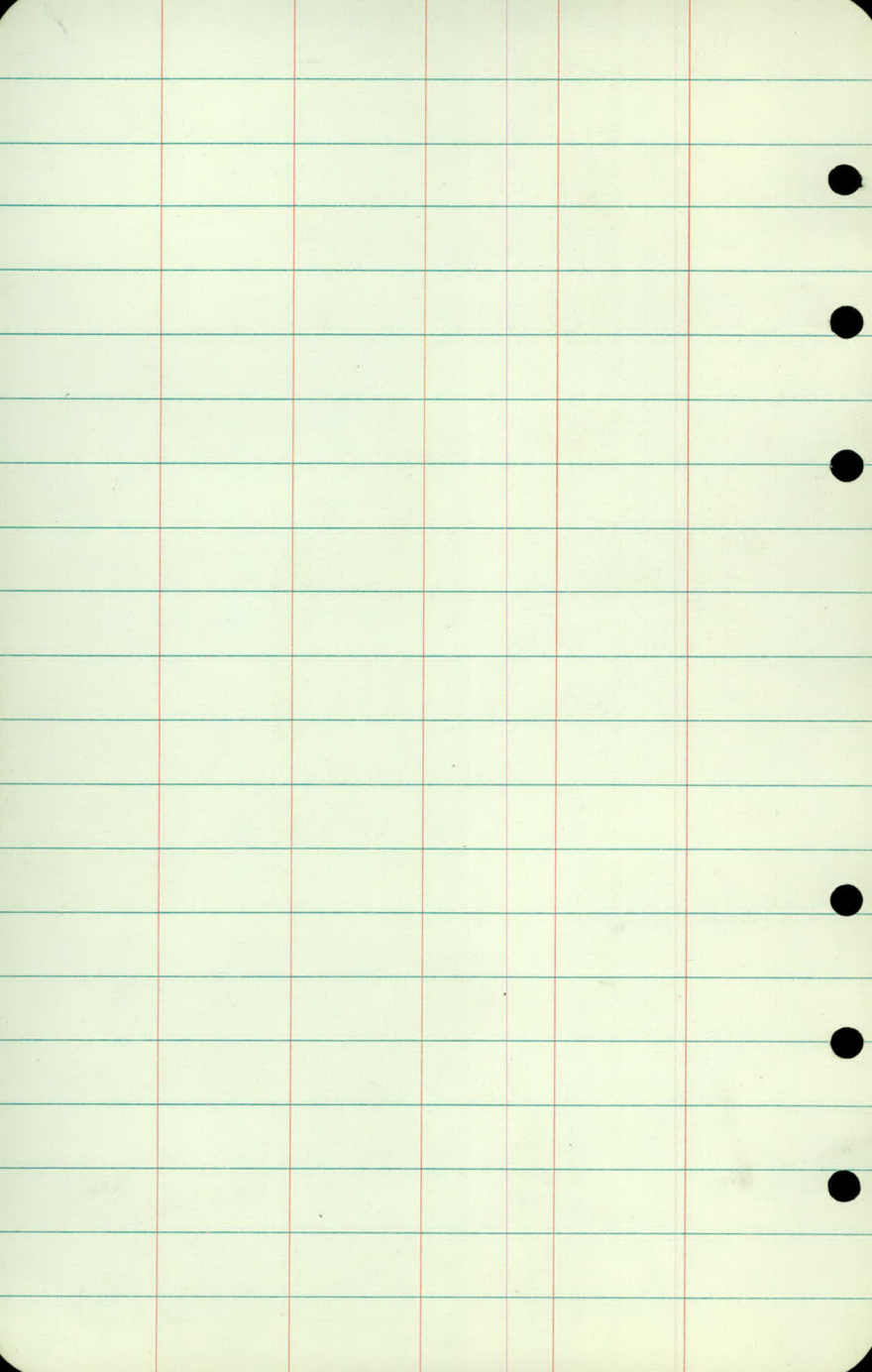
103

3

85+00 E center line

LK WABASSO BENCH - POWER Pole

Ctr. Door sill Pump Ho #14 at Lake Quasso



Owasso Blvd. North

Sta + π - Elev.

BM 1209966.44 954.35

Monument 4.87 961.57

80' W 3.6 62.8

80' E 4.9 61.5

$\pm$ Dale & New Line 12.7 53.7 (53.6)

FK
FS
WJ

Jan. 26, 1967

105
2

Spike in Arc Light Pole NW. Cor. Dale

from P. 34

