

DR.9 BK 64

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

McKNIGHT RD.
From Mailand To Upper Affton Rd.

Road Acc't. No. 68

Date Filed _____

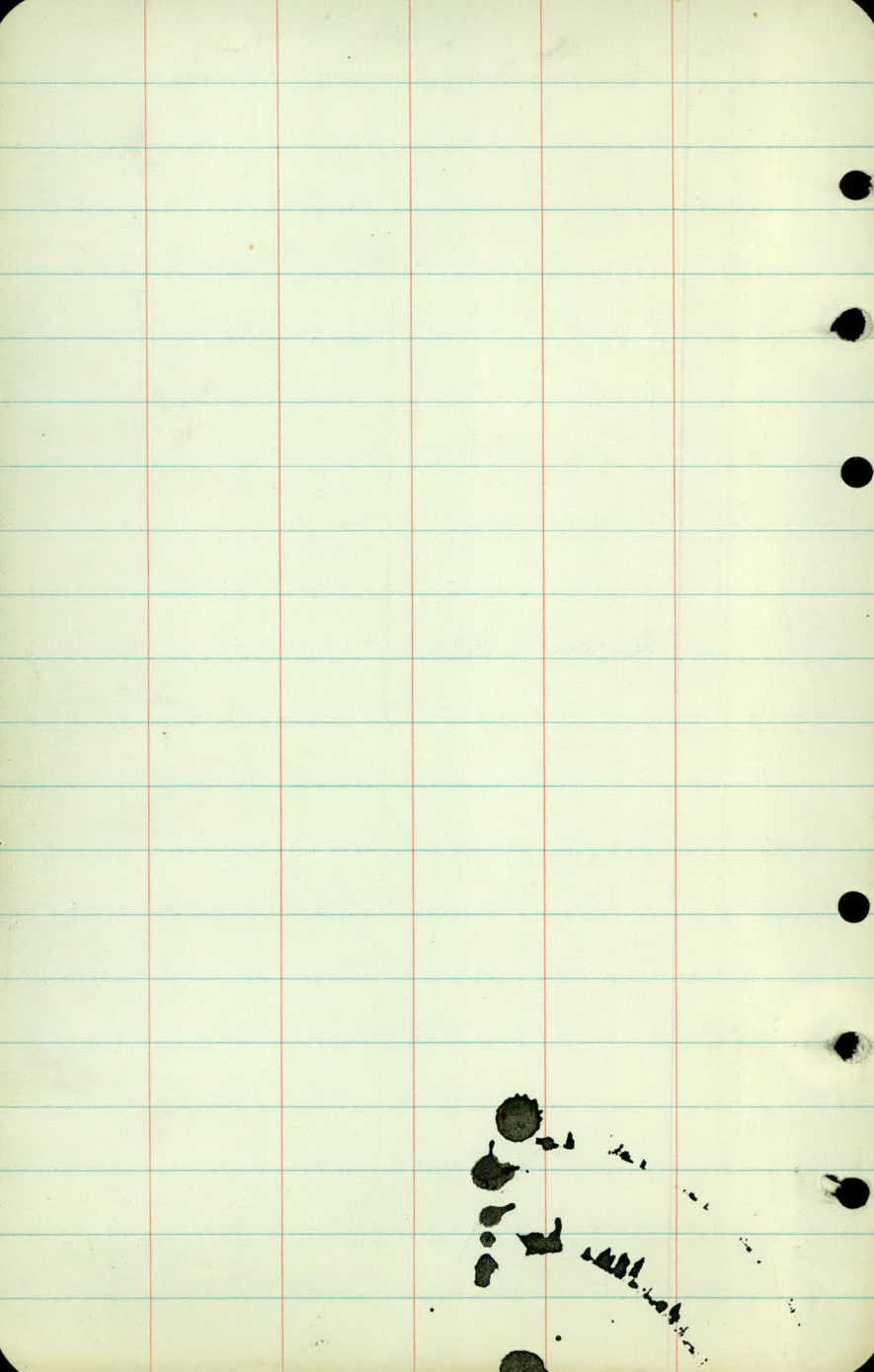
File _____

KP
WM
PK

MC KNIGHT RD.

MAILAND RD TO UPPER AFTON RD.

PLAN SURVEY



UPPER AFTON
ROAD

STONE MONT

W $\frac{1}{4}$ COR
S1-T29-R22

2



2630.71

IRON
NW COR
S12-T28-R22

89°31.0'

312.0

LOWER AFTON
ROAD RR SPIKE

1000.82

88°31.0'

LONDIN LAKE

STONE MONT.
W $\frac{1}{4}$ COR OF
NW $\frac{1}{4}$ S12-T28-R22

IRON
E $\frac{1}{4}$ COR OF
NW $\frac{1}{4}$ S12-T28
R22

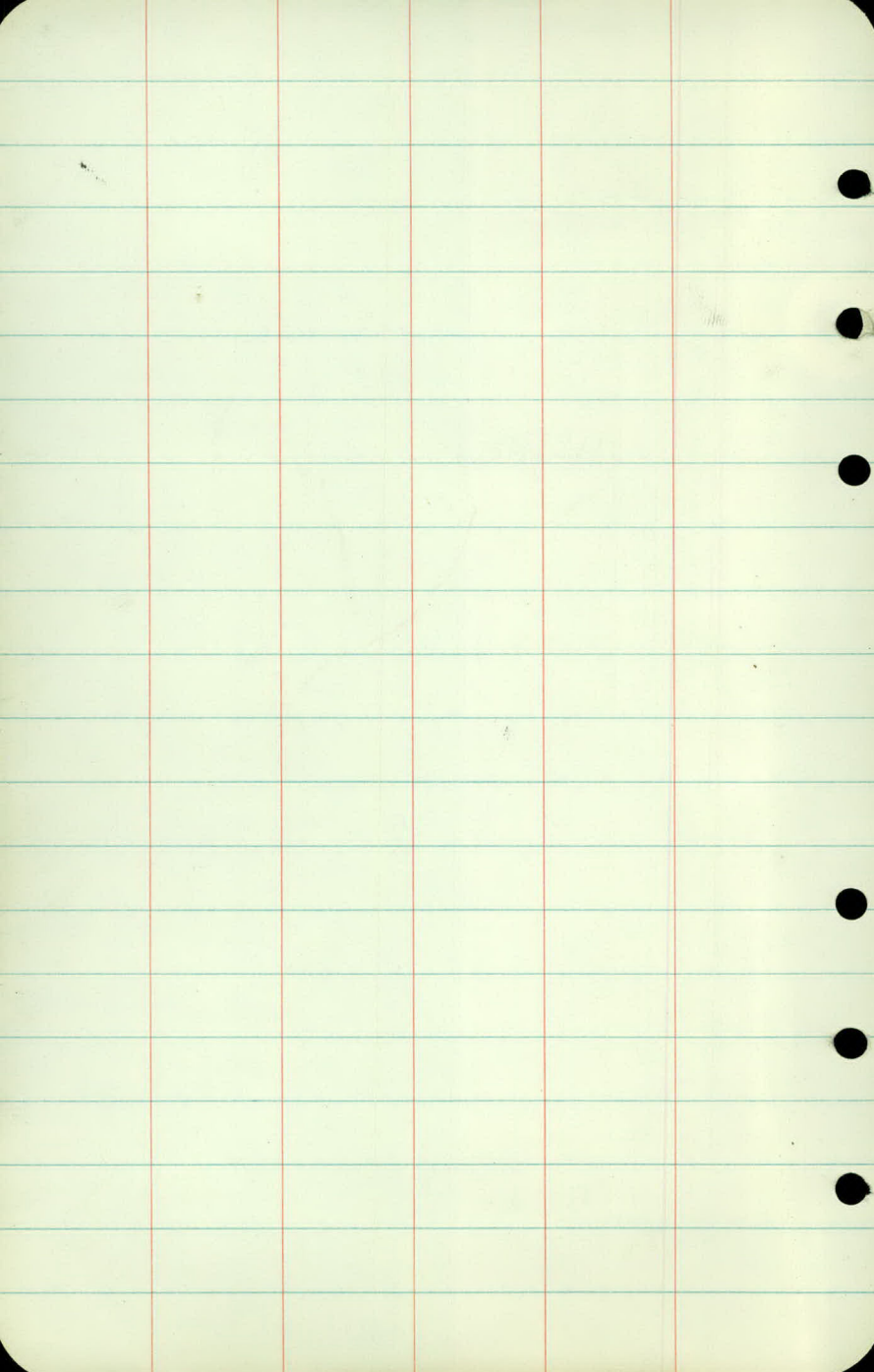
89°43.11"

1312.41

STONE MONT. MAILAND RD.

S $\frac{1}{4}$ COR OF
NE $\frac{1}{4}$ S11-T28-R22

STONE MONT.
W $\frac{1}{4}$ COR S12-T28-R22



ALINEMENT

STA	POINT	ΔL	ΔR	CURVE DATA
-----	-------	------------	------------	---------------

10+00.82	±	LOWER AFTON RD.		
		P.O.T.		

0+00	±	LONDIN LANE		
------	---	-------------	--	--

65+65.17		W $\frac{1}{4}$ COR OF N.W. $\frac{1}{4}$ Sec. 12-T28-R22		
----------	--	---	--	--

59+47.54		P.O.T.		
----------	--	--------	--	--

52+52.92	PI.	0'00.5'	±	MAILAND ROAD
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		W $\frac{1}{4}$ COR. Sec. 12-T28-R22		
--	--	--------------------------------------	--	--

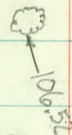
LT

E

RT

4

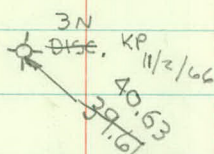
QUAD.
COTT.
(DISC)



HYDRANT

58.93

RR SPIKE



DISC

113.90

STONE MONT.

103.35

87.12

DISC

DISC



DISC.

44.93

PK

10.28

DISC.

FOUND.

99.64

88.55

STONE MONT

156.40

25.24

29.07

DISC

STA	POINT	ΔL	ΔR	CURVE DATA
-----	-------	------------	------------	---------------

39+43.53	±	UPPER	AFTON RD.	
----------	---	-------	-----------	--

	$W\frac{1}{4}$	COR	Sec 1 - T28 - R22	
--	----------------	-----	-------------------	--

17+12.08	P.O.T.			
----------	--------	--	--	--

13+12.82	N.W. COR			
----------	----------	--	--	--

	Sec 12 - T28 - R22			
--	--------------------	--	--	--

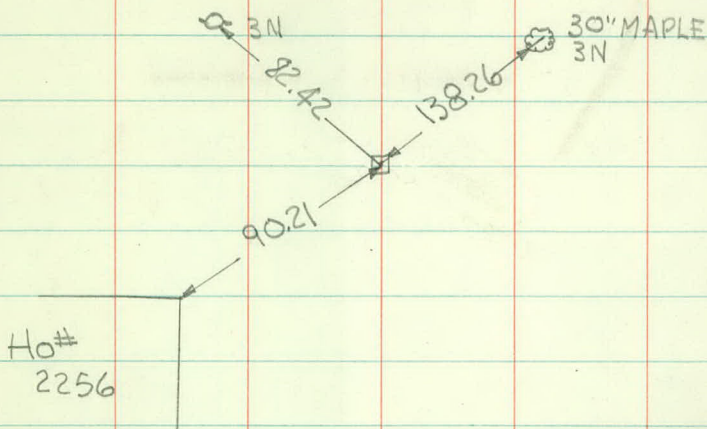
	$0^{\circ}28\frac{1}{2}$			
--	--------------------------	--	--	--

LT

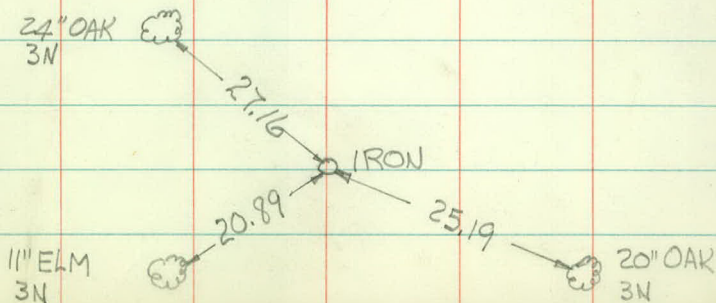
E

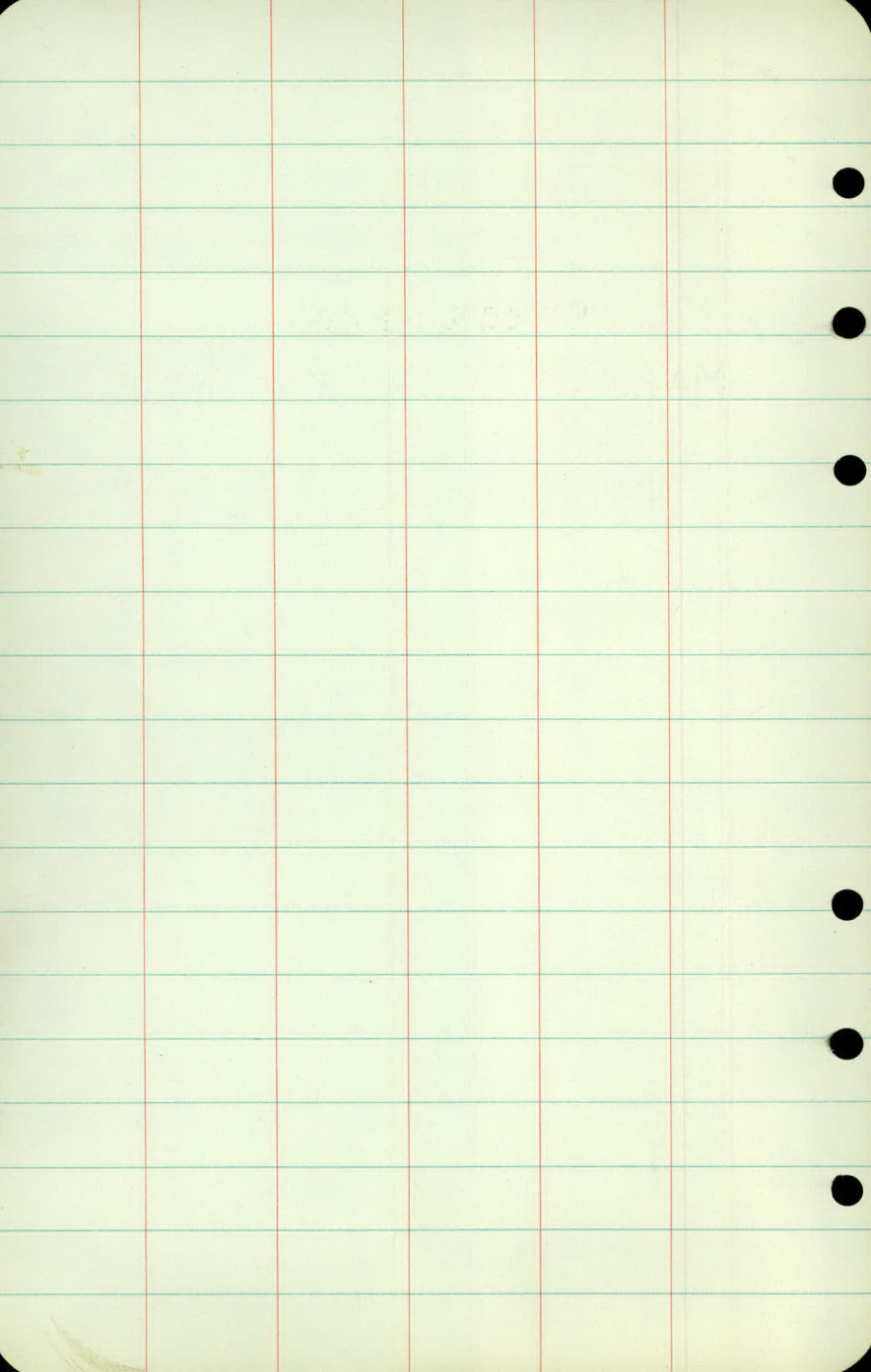
RT

5



SPIKE





KP
WM
PK

14 JAN. 1965

6

McKNIGHT RD
LINWOOD AVE TO MAILAND RD.

ALIGNMENT TIES.

STA	POINT	Δ	LT	DRT
52+52.92	PI		0°00'.5	

49+95.38 P.O.T.

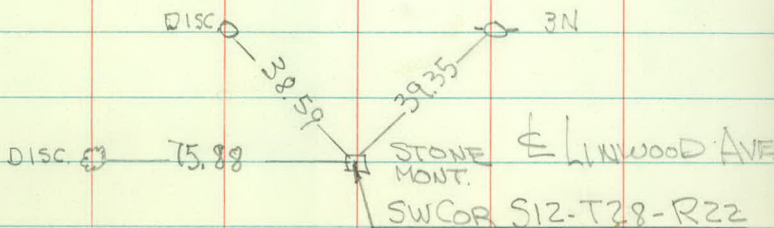
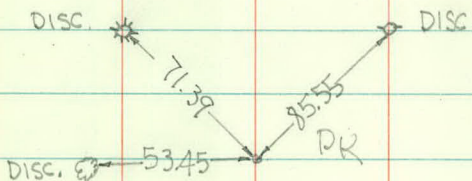
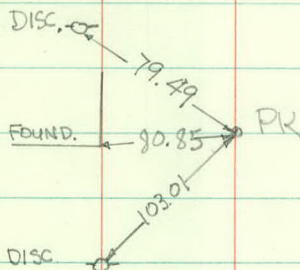
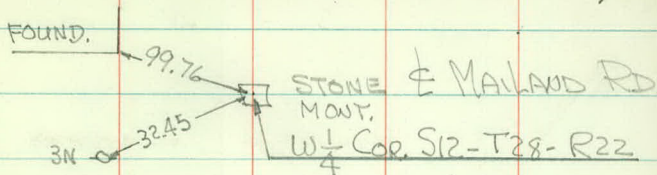
P.O.T.

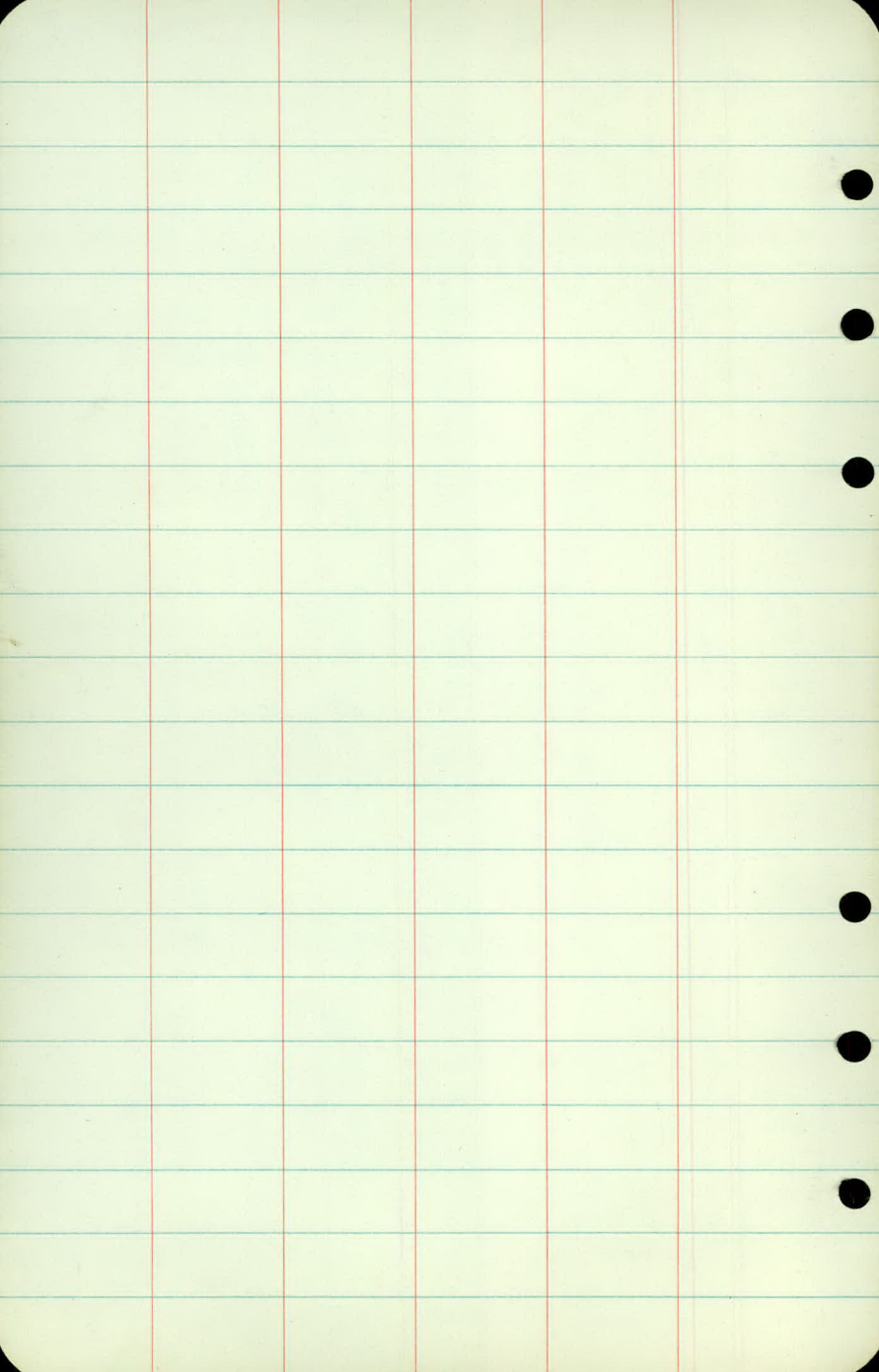
26+28.32 PI

1°03'.0

14 JAN. 1965

7





KP
JS
WM
WS
FS
R

5 MARCH 1963

8

UPPER

39+43.53 AFTON RD.
MONT.
W $\frac{1}{4}$ COR. Sec 1-T29-R22



13+12.82
IRON
NW COR
S12-T28-R22

NEW Lower
89°31'0"
312.2
10+00.82
RR. SPIKE
Afton Rd
McKnight Rd

Old Lower
2400
88°31'0"
1000.82
MONT Afton Rd
W $\frac{1}{4}$ COR NW $\frac{1}{4}$
S12-T28-R22
IRON
E $\frac{1}{4}$ COR NW $\frac{1}{4}$
S12-T28-R22

1312.25

MONT
W $\frac{1}{4}$ COR
S12-T28-R22

STA	POINT	ΔLT	ΔRT
-----	-------	-----	-----

13+12.82			
----------	--	--	--

		0°28'½	
--	--	--------	--

10+00.82 P.O.T. = STA 56+00 NEW LOWER AFTON RD

0+00

6 MARCH 1963

9

LT

≠

RT

N.W. COR. S12-T28-R22

24" OAK

3N

27.16

0.31'

1 KON 20"

25.19

OAK

3N

spike

20.89

4" ELM

3N



~~DISC~~
ROAD, COTT.

106.52

PK iron

HYD.

58.93

58.93

106.52

W 1/4 COR NW 1/4 S12-T28-R22

39.61

MONT

113.90

103.35

87.12

40# 366

STA	Point	ΔL	ΔR	curve data
-----	-------	------------	------------	---------------

39+44.22	11-19-0	R76		
----------	---------	-----	--	--

39+43.53	PI	$0^{\circ}2.5'$		
----------	----	-----------------	--	--

32+50.73	P.O.T.			
----------	--------	--	--	--

17+12.08	P.O.T.			
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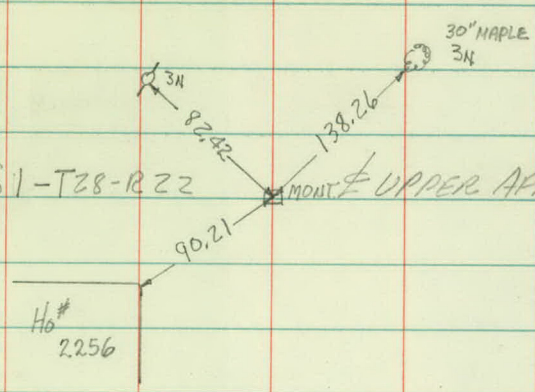
13+12.82	PI			
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7 MARCH 1963

10



W 1/4 Cor. S1-T28-R22



• SPIKE

MISSING
11/19/64
C78

• SPIKE

OK

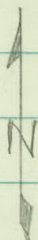
S.W. Cor S1-T28-R22

• iron

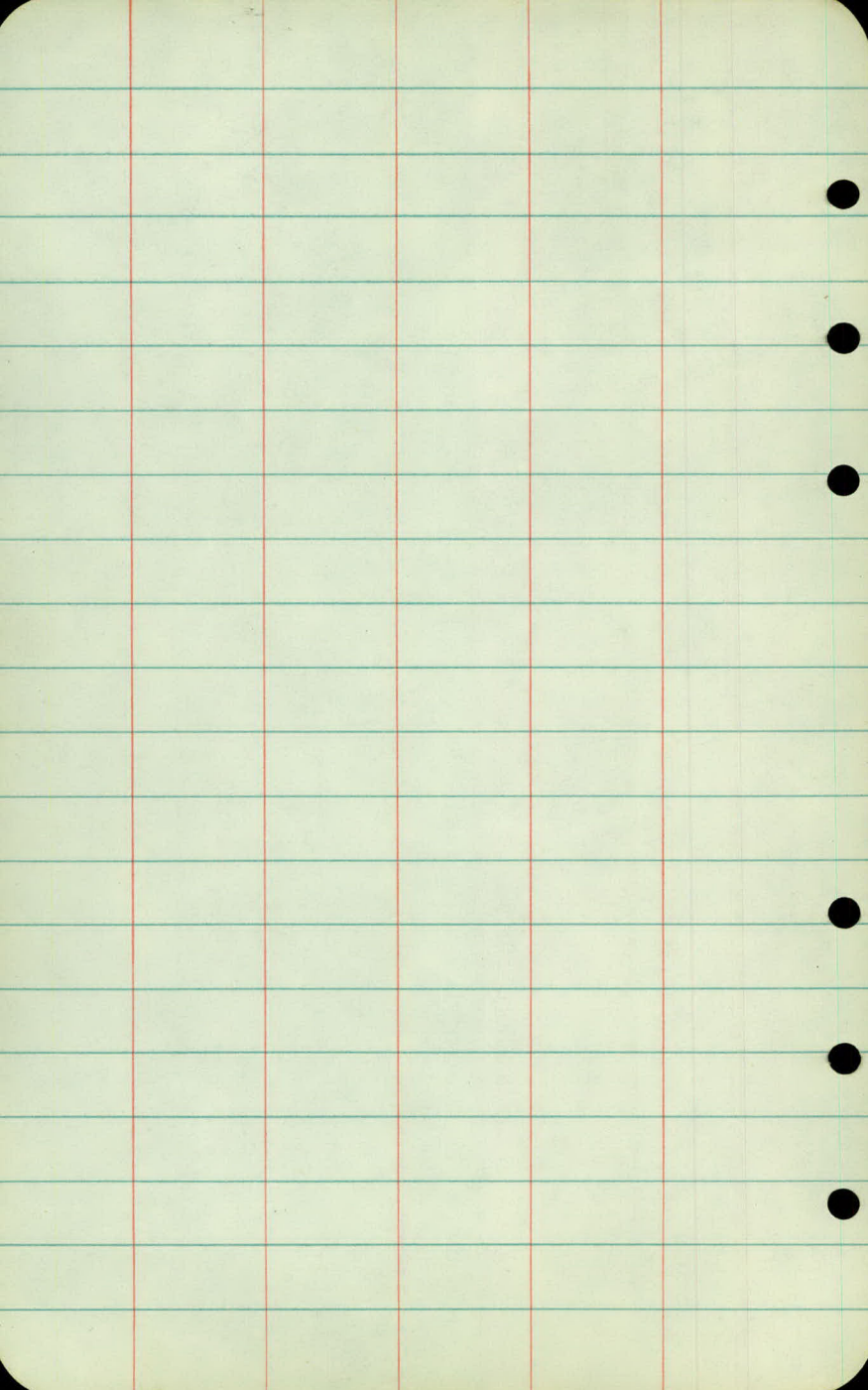
39+43.53 P.I.

£

11



Upper Afton Rd.



RG
FS
PK
LPD

Apr. 18, 1965
Cloudy, Lt. rain 45° 12
1

McKnight Rd.

Additional Topog.
(South of Mailand Rd.)

Sta 48 to Sta 49

2 pages

Lt.

Rt

BT

49+00	+96 $\frac{PP}{28}$	+96 $\frac{E.Fe}{33}$	89	+97 $\frac{12' Oak}{38}$
+91	$\frac{2' Pine}{37}$	+92 $\frac{E Ent}{93}$		
+81	$\frac{1' Pine}{38}$	+73 $\frac{4' Maple}{39}$		
+97	$\frac{Stone Wall}{49-78}$	+92 $\frac{SE Cor Gar}{82}$		
+63	$\frac{2' Maple}{38}$	+60 $\frac{E Ent}{93}$		+67 $\frac{Stp}{26}$
+49	$\frac{E Ent}{79}$			
+44	$\frac{24' Oak}{38}$	+40 $\frac{B.Fe}{32}$		+40 $\frac{Stp}{26}$
+34	$\frac{E 10' Ent}{10}$	+34 $\frac{E Ent}{43}$		+33 $\frac{24' Oak}{44}$

BT

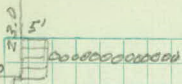
48+00

10 13

April 8, 1965

13
2

SAR.
27.0



X
X

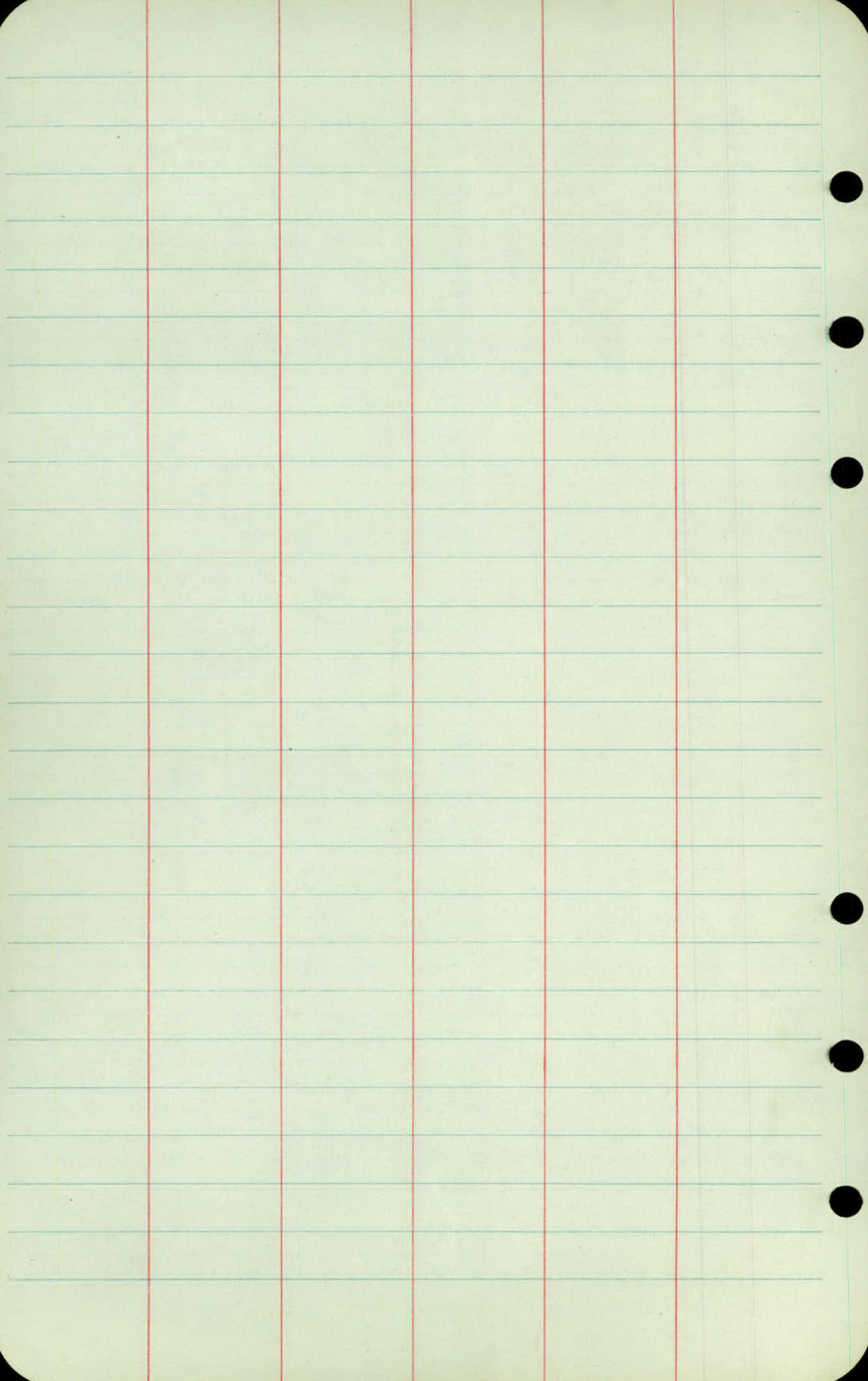
60
60

Sandy Drive

7

7

23

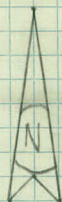


KP
WM
DS
PK

12 JAN. 1965
COLD & CLEAR
4°

14

MCKNIGHT RD.
MAILAND RD TO LONDIN LANE
TOPOGRAPHY



Rec. - 2-17-65

+50

BT
12

BT
9

+50

SPRUCE
34

+45 10' COTT 68 +39 N.E. COR 1/4 90

+28 TWIN 8" WILLOW 39 34 x 29.5

+05 S.E. COR 1/4 90

+43 PINE 35

+15 STR 20 +20 END CEDARS 29

+00 TWIN 6" COTT 35

51+00

BT
10

BT
8

+00 BEGIN CEDARS 29

+76 1/2 10'0 ENT 10

+83 END CEDARS 31 +90 6-6"0 32

+70 PP 27 (14.3 x 20.5)

+81 N.E. COR GA 83

+69 1/4" TWO 62

+97 BUSH 20

+67 S.E. COR GA 83

+69 STR 60

+65 BEGIN CEDARS 31

+56 N.E. COR SHED 93

+56 24"0 29 +58 BUSH 21

+50

+56 BUSH 21

+50 BUSH 23

+51 END CEDARS 31

(8.3 x 10.4)

+45 BUSH 23

+54 WALL 26

+27 BUSH 21

+48 S.E. COR SHED 93

+25 BUSH 21

+26 BUSH 23

+28 BUSH 23

+09 3" ASH 52

+10 PINE 46

+13 SW COR 1/4 84

+21 14"0 55

+07 BEGIN CEDARS 31

+06 PINE 57 +13 BUSH 23

50+00

(46.5 x 27.3)

BT
9

BT
9

+00 10" COTT 39 +03 BUSH 22

+71 S.E. COR 1/4 77 +98 4" SW 16-76

+73 SW COR GA 61

+88 16"0 49 +94 BUSH 22

+59 PINE 56 +66 END FE (WOOD) 33

+69 END LILACS 24

+72 16"0 35

+60 PINE 36 +61 PINE 46

+65 RT ENT 53

+63 12"0 53

+53 PINE 39 +54 BUSH 28

+51 1/2 10'0 ENT 9

+52 BEGIN LILACS 50

+50

+36 BUSH 28

+48 1" BIRCH 48

+20 3" APPLE 58

+32 PINE 41

+17 BEGIN FE (WOOD) 33 (42 x 27) +20 3" APPLE 43

+27 4" ELM 47

+15 S.E. COR 1/4 77

+18 1/2 80 DRIVE 44

+29 1/2 80 DRIVE 31

49+00

BT
8

BT
9

+07 PINE 33

12 JAN 1965

15

LT

RT

20.5

43

27.3

HO # 511

46.5

HO # 515

42.0

27.0

π

6 CEDARS

7 CEDARS

12 CEDARS

WILACS

13.1

GA

21.3

28

21.0

5

23.8

44

32.0

48

54+00	+97 APPLE 50	BT 14	BT 6	LOWLAND 23-150	WOODS 37-125
+98 NE COR GA	+91 E 10.0 ENT 69				
	24.4 x 22.4	+79 E 10.0 ENT			
+74 SE COR GA	69			+52 BEGIN LOWLAND	46
	+61 NE COR HO			+52 BEGIN WOODS	46
+50	90				
	35 x 24.5				
+06 SE COR HO	84				
	+01 6" MAPLE				
53+00	42	BT	BT		
	+00 ER	17	7		
+87 POR	21				
	+74 BR				
	33				
+62 E MAILAND RD				+83 ERI	10
	+51 ER			+57 BR	34
	32			+67 POR	19
+50					
		+53 MONT			
+37 BR	18			+32 ER	26
	+46 POR			+45 E MAILAND RD	
	24				
	+25 PP			+29 HEDGE	33-100
	23			+23 POR	15
+19 12" BE	70			+16 SPRUCE	57
	+06 PINE			+17 SPRUCE	65
	71			+01 SPRUCE	47
52+00				+10 SPRUCE	58
		BT 13	BT 8	+12 BR	8
+83 1" APPLE	78			+00 SPRUCE	34
	+93 PINE				
	71			+87 BLUE SPRUCE	34
+81 8" ELM	71			+94 APPLE	27
				+68 STP	21
+55 L. LAC BUSH	70			+77 PINE	34
	+52 4" COTT			+92 SPRUCE	42
	42			+66 BLUE SPRUCE	33
51+50				+58 SPRUCE	35
		BT 12	BT 9	+54 3 PINES	47

RP
FS
WM
PR

LT

18 JAN. 1965
SUNNY 100

16

RT

GA

24.4

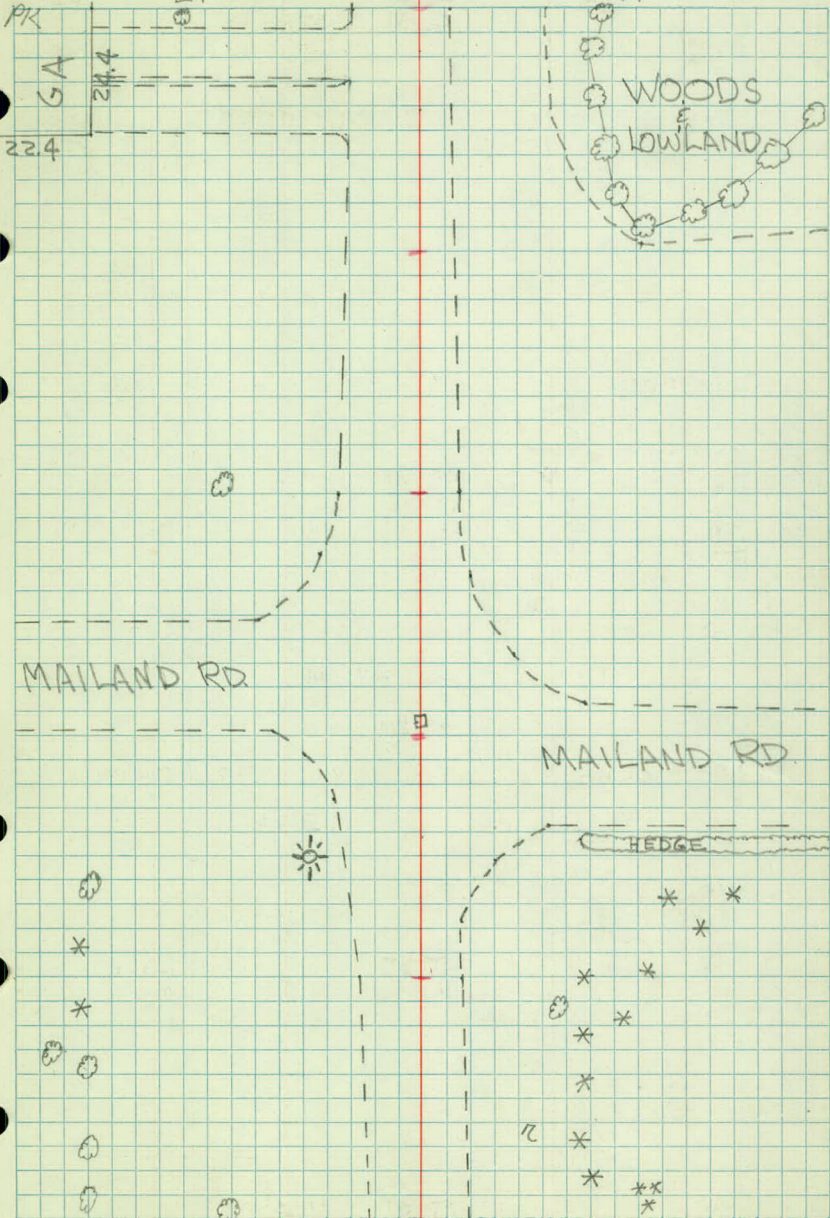
22.4

WOODS
LOWLAND

MAILAND RD

MAILAND RD

HEDGE



+50

BT BT
18 3

56+00

BT BT
18 3

+69 PD
23

+50

BT BT
16 3

+30 1" CE 58 +30 1" CE 58
+25 1" MAPLE 70 +22 1/2 10'0 ENT.

+06 STEPS
62-65

+13 STEPS
62-65
+04 HEDGE
34-60

+10 END LowLAND
20-60
+09 END WOODS
34-85

55+00

SW
62-65

BT BT
14 3

+90 NE COR HO

+91 1" TRIPLE BIRCH
59

+92 COR WOODS

+81 SW
76-79

+75 WOODS
77-96

+75 LowLAND
20-110

+65 SW
80-83

(40.3 X 30.2)

+51 WOOD
82-98

+50

+50 SE COR HO BT BT
14 4

WOODS LowLAND
42-82 20-135

+27 SW
78-82

+41 3" CE
52

+24 S.E. COR SW (30)
47-87

+14 1/2 10'0 ENT

+01 PD
23

54+00

+00 APPLE
38

BT BT
14 6

WOODS
37-125

LowLAND
23-150

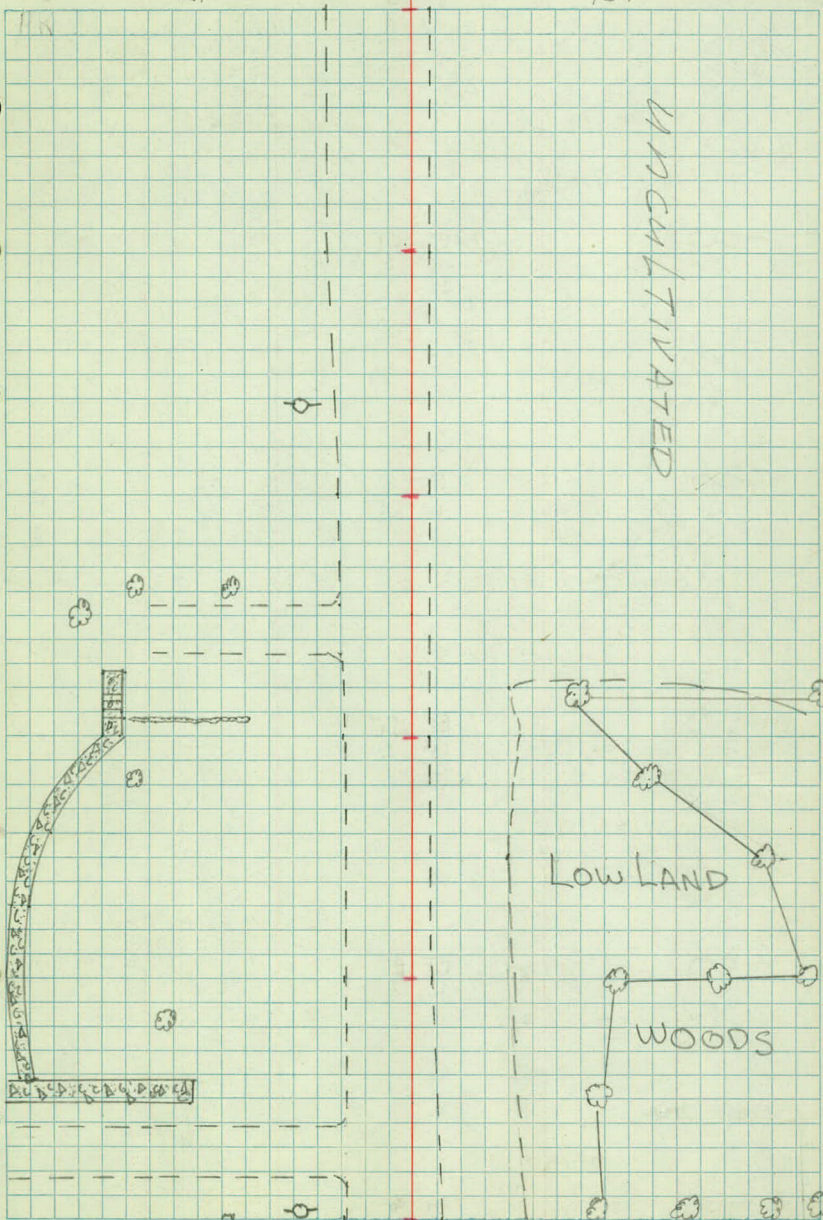
18 JAN. 1965

17

LT

RT

UNCULTIVATED



59+00

BT BT
16 4

+91 PINE
70

+85 PINE
59

+80 PINE
69

+52 4" Willow
42

+50

BT BT
17 3

+37 4" Willow +44 4" Willow No
44 58

+21 HEDGE +26 BUSH No
35-100 48

+15 Fecor
32

58+00

BT BT
17 3

+50

BT BT
18 2

+38 PP
24

57+00

BT BT
18 2

56+50

BT BT
18 3

KP
WM
DS
FS
PR

LT

19 JAN. 1965
cloudy 25°

RT

18

UNCULTIVATED

UNCULTIVATED

HEDGE



+50

42.3 X 26.6

BT BT

15 8

+29 S.E. COR HO

95

+28 6" CE

38

(21.7 X 24.2)

+21 N.E. COR GA

+11 SHRUB

118

64

+04 10.5 CONC. ENT.

16 - 118

61+00

+98 SECOR CONC ENT

+91 SHRUB

BT

6

+78 PINE

+84 SHRUB

50

47

50

+99 SECOR GA

+69 PINE

+72 PINE

118

48

58

+63 PP

+64 PINE

27

53

+54 PINE

+53 PINE

49

58

+50

BT

BT

15

6

+33 PINE

+46 PINE

66

55

+29 12" ELM

+26 PINE

48

65

+05 PINE

+16 10.0 ENT

63

16

+02 8" ELM

40

60+00

BT

BT

3

+61 10" ELM

+93 6" ELM

+79 6" ELM

41

47

+76 PINE

47

+65 PINE

65

+95 PINE

65

64

+55 5" ELM

+56 7" ELM

+85 6" ELM

53

47

59

+50

+42 6" ELM

BT

BT

54

16

4

+45 PINE

+40 6" ELM

72

42

+24 6" MAPLE

+24 PINE

50

85

+15 PP

26

59+00

BT

BT

16

4

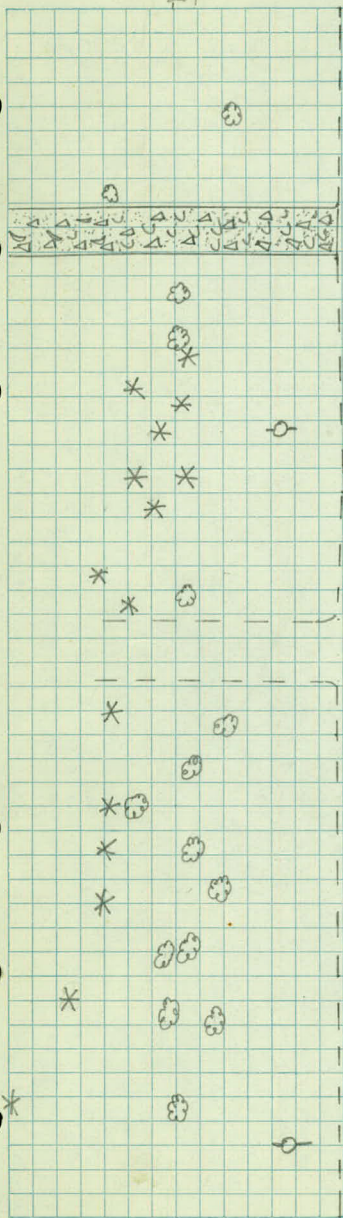
19 JAN. 1965

19

LT

E

RT



UNCULTIVATED

UNCULTIVATED

64100

FE
30

BT BT
10 12

+674" ELM
36

+50

BT BT
11 12

+36 PP
28

63100

FE
33

BT BT
12 11

+87 8" ELM
36

+50

BT BT
12 9

+47 4" ELM
37

+07 4" ELM +00 BT BT +00
37 12 8

62100

+00 PP Fe Cor
28 37

+90 1" ELM
69

+80 JUNIPER Bush +83 JUNIPER Bush

54

43

+84 3-Juniper Bushes

61

+70 3" TWIG BARK +71 NEG COR HO

66

+68 6" ELM
38

61150

BT BT
15 8

19 JAN. 1965

20

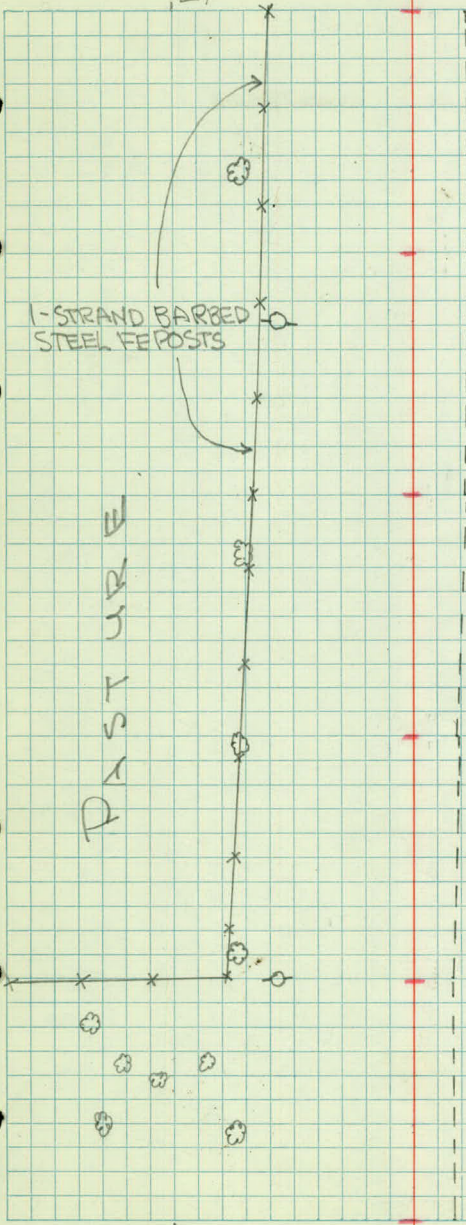
LT

RT

£

1-STRAND BARBED
STEEL FEPOSTS

W
B
J
K
S
A
P



LT

±

RT

66+00

+83 BT
100

+83 BT

+83 BT
100+65.17 STONE MONT
±+54 ER
38+56 ER
48

+50

+39 FE COR
53+43 POR
18+41 POR
27+29 6" ELM
36+30 BR
11+26 1" BIRCH
45+26 1" BIRCH
41+13 FE
31+19 BR
17+03 N.W. COR Ho
62

65+00

FE
29BT
9BT
14+99 ± 2.0 SW
18-57+87 6" ELM
35+99 ± 4x5 STEP
57-62+65 PP
29+62 S.W. COR Ho
63+53 2" BIRCH
39

+50

FE
28BT
10BT
13+45 1" BIRCH
43+47 6" ELM
35+45 1" BIRCH
39+07 5" ELM
36

64+00

FE
30BT
10BT
12

19 JAN. 1965

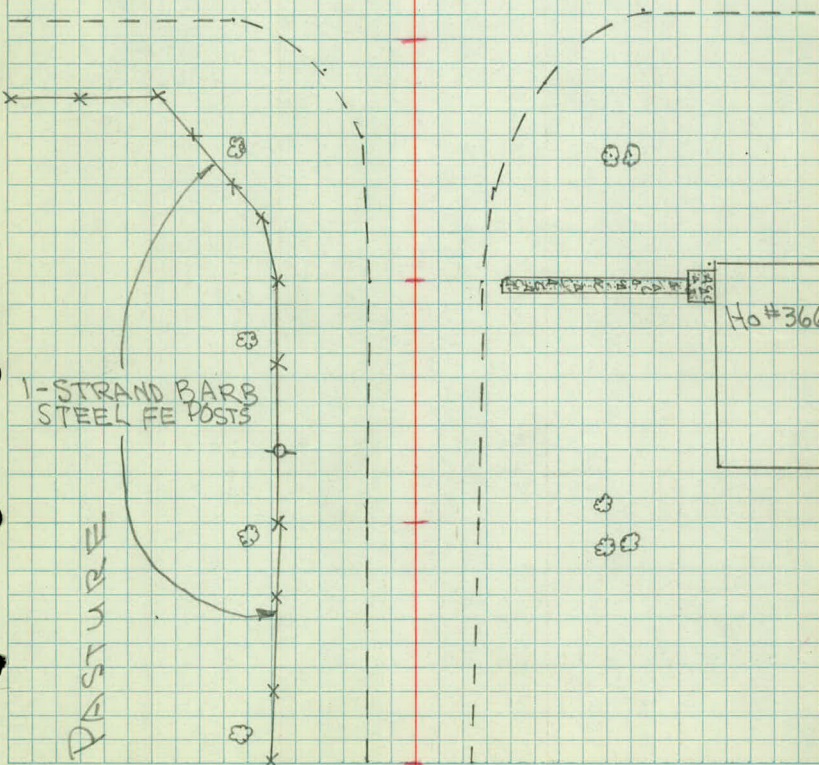
21

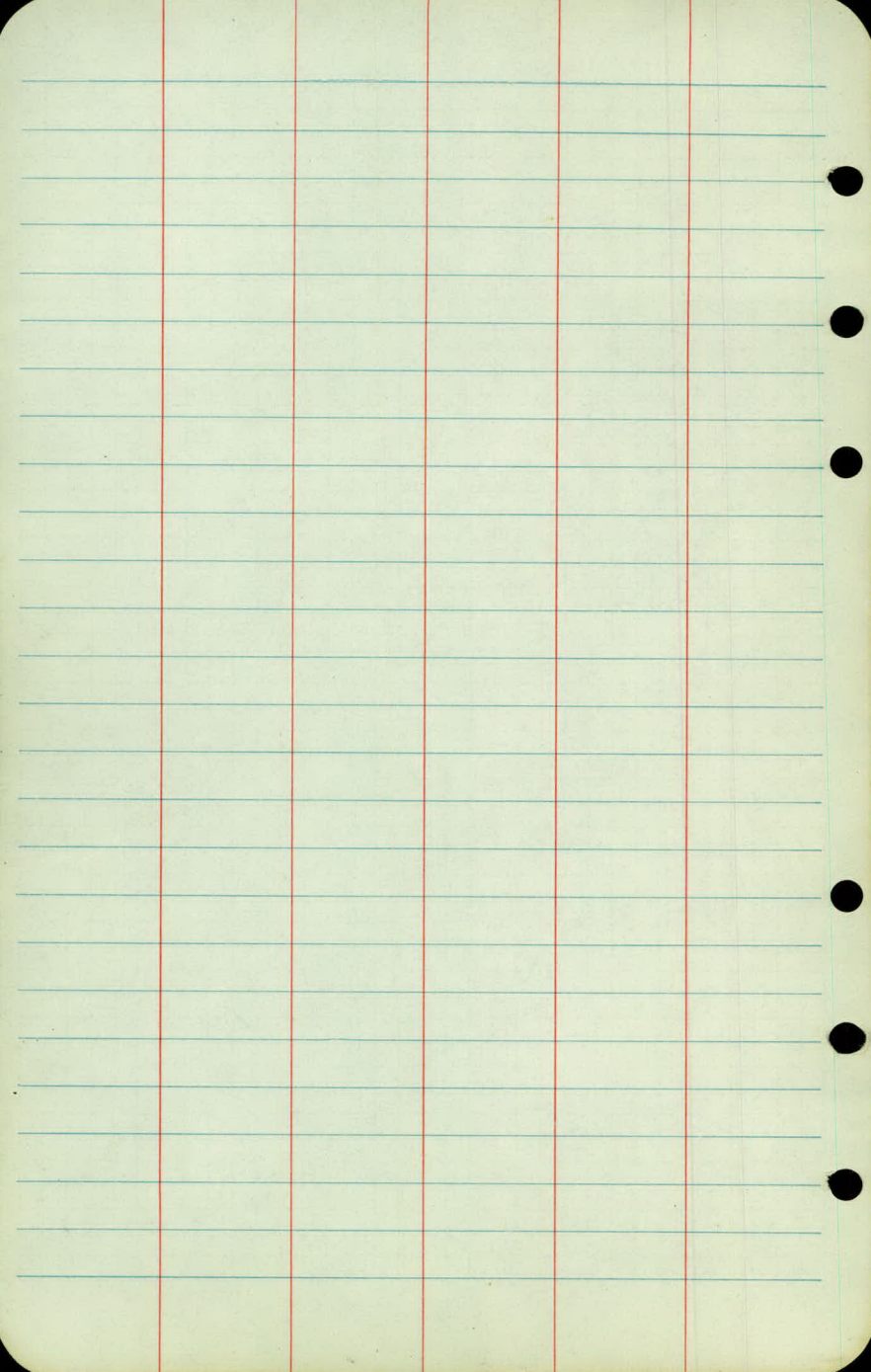
LT

±

RT

LONDIN LANE





RP
WS
DS
R. Boss

29, MARCH 1963 22
Cloudy
45°

Mc Knight Rd.
LONDON LANE
LOWER AFTON TO UPPER AFTON
TOPOGRAPHY

+46 6" ELM
10

+50 SE Cor Conc
Lt

+41 6" ELM
35

+37 6" ELM
146 conc 24

+35 6" BE
59

+29 8" Poplar
33

+25 8" Maple
44

1 + 00

+90 3" Pear
14

+70 5" Balsam
57

+63 3" Balsam
53

+50

+45 5" maple
63

+27 10" BE
65

+27 12" BE
36

+30 EP +21 1/2 DRIVEWAY
5

0 + 00

0-18 POR
23

0-22 POR
17

0-36 BR
12

0-36 6" ELM
36

0-50

0-102 PP
29

Rt.

+46 10" ELM
54

+38 SE Cor Barn
46

+35 TW 6" APPLE
34

+24 10" COTT
60

+15 10" Spruce
51

+23 8" Poplar
36

+19 3" Pear
11

+81 1" MAPLE
47

+64 5" Balsam
48

+63 24" Oak
29

+45 7" ELM
66

+27 12" BE
70

+28 AP
29

+18 BT
100

+30 Begin fc
52

1/2 (1-Strand Barbed Wire)
at Mont #

0-11 ER
39

0-30 POR
13

0-44 BR
17

0-60 1/2 2x2 SW
55-93

0-76 5" ELM
37

0-103 SW Corho
62

24 MARCH 1963

Rt.



17.5
33.0
33.0

401-S-S

3100 N
PAT. 10-13
D.D.

Barn
28.5

1-Strand barbed wire.

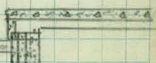
GA.
20
6
14

Five

LOWER Afton
LONDON

Road
LANE

McKnight Rd.



H. #366

4

4+00 Woods 40 Lt Fe 4 Rt Washout 39-42 Woods 71

+50 Woods 40 Fe (3 strand) 1 Woods 77 WA Shout 55-60

+ 32 NE Cor hut

+20 SE Cor hut 9

3+00 Cor Woods 30 Fe 2 Cor Woods 85 WASHOUT 70-79
+72 Cor Woods 83

+50 Fe 1 WASHOUT 95-105

+08 4" ELM 7
+100 FP 20
2+00
+81 Retaining wall 32-48
+58 NE Cor Slob 42-88
+70 NE Cor Barn 11
+67 5" ELM 7
1+50
+27 Cor Woods 25
+13 SECOR SHED 35
+05 6" ELM 50
+99 STD 54
+86 4" ELM 33
+65 14" TW ELM 64
+83 20" TRIPLE BE 13
+54 6" TW ELM 7
+74 4" ELM 24
+74 6" ELM 22
+28 Corner Woods 33
+77 9" ELM 35
+76 8" TW ELM 3
+86 5" ELM 28
+68 2" ELM 27
+54 STD 14
+60 3" ELM 4
+54 3" ELM 39
+96 FP
+77 9" ELM 27
+88 5" ELM 28
+65 9" ELM 3
+65 5" ELM 4
+57 7" TW 6" ELM 3

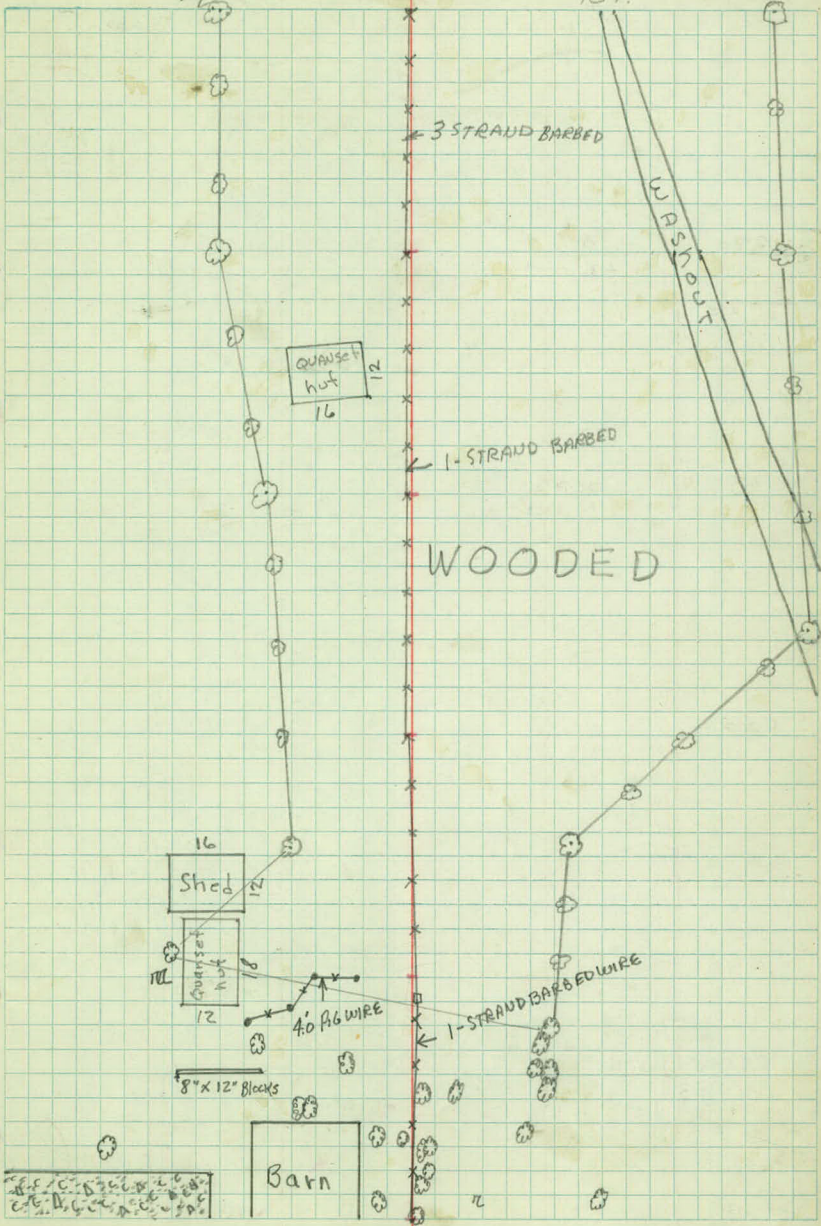
1 APRIL 1963

4

2

RT.

24



+50

Lt Woods
53-100

FE
3

Rt

Woods
-6-57

6+00

WOODS
53-100

FE
4

WOODS
6-57

+65 ~~FE~~ COR
4

+53 Cor Woods
60

+50

WOODS
53-100

+48 Fe
20

5+00

Cor Woods
100

Fe
1

Fe
53

+86 Fe
61-100

+70 Cor Woods
64

+50

+38 Fe
20

+44 COR WOODS
33

+27 Cor Woods
40

+13 Fe
1

4+00

WOODS
40

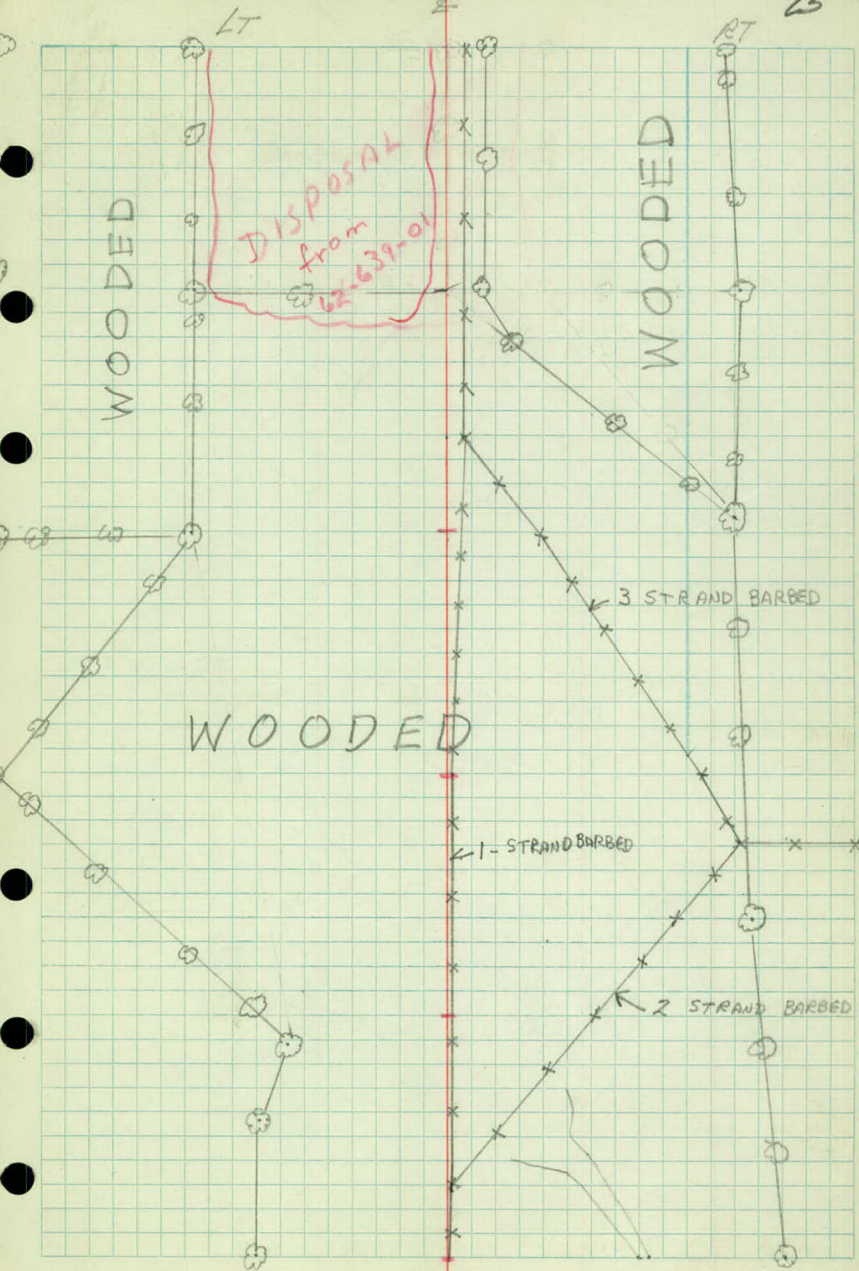
Fe
4

Washout
39-42

WOODS
71

4 APRIL 1963

25



9+00

Lt

E

FE
1

Rt

+50

FE
2

8+00

FE
2

+51 END WOODS
59-93

+50

FE
2

+18 10" APPLE
12

+27 6" ELY
58

7+00

WOODS
53-100

FE
3

END WOODS
0-58

6+50

WOODS
53-100

FE
3

WOODS
6-57

4 APRIL 1963

26

RT

Lt

St

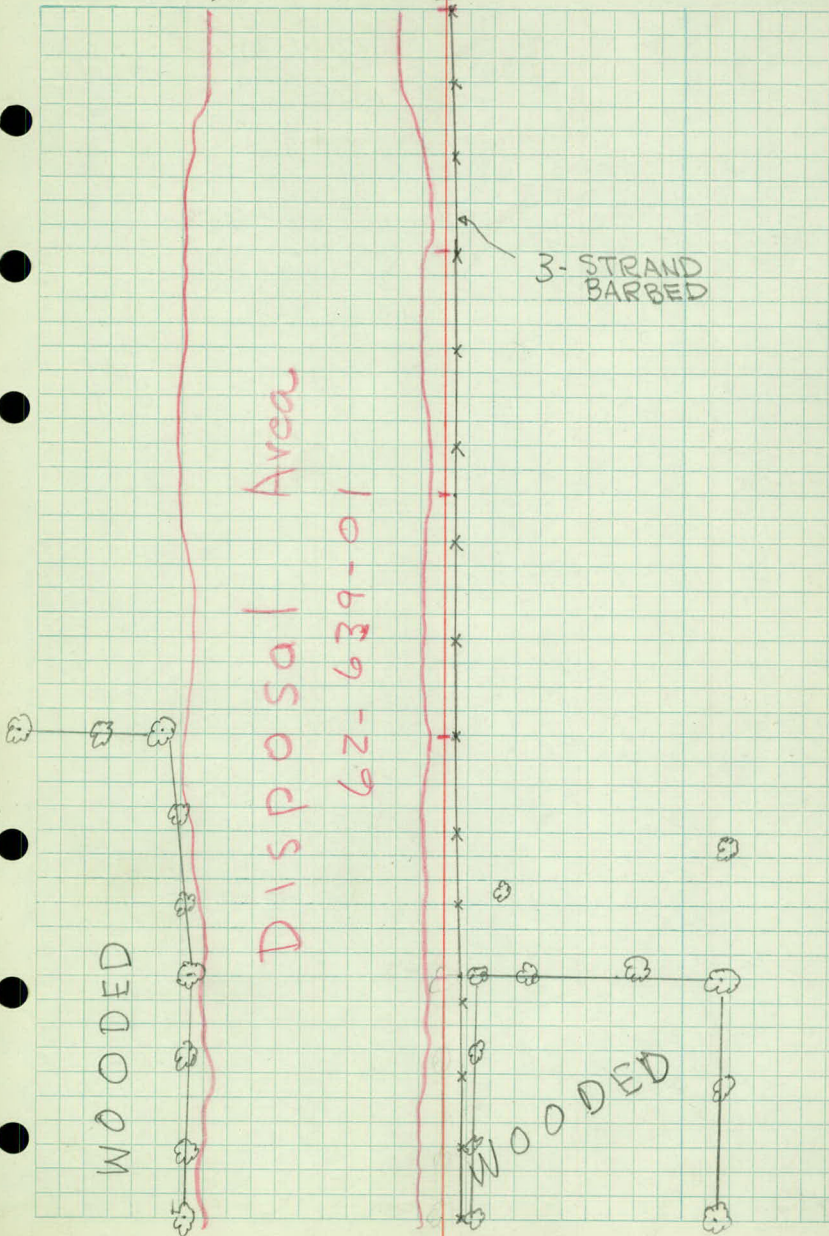
3-STRAND
BARBED

Disposal Area

62-639-01

WOODED

WOODED



+50

Lt

£

+47 Pine
89

+40 Pine
96

+29 Pine
78

+20 12" ELM
20

+17 Pine
67

+15 Pine
64

+100 Pine
63

+95 Pine
70

+88 Norway Pine
70

Rt

+43 6" ELM
18

+32 10" ELM
20

+17 Pine
84

+15 Pine
75

+104 Pine
71

+50 Pine
94

+43 Twin 10" ELM
21

+36 8" ELM
17

+26 Pine
74

+19 5" ELM
20

+10 6" ELM
21

+32 Cor Woods
51

+08 6-14" ELMs
8

11+00 +100 Cor Woods
125

+50

+43 ^V ~~INDENT~~
20

+41 WATER SHUTOFF
40 +25 Shoulder
£

10+00

+100 £ Lower Aften Rd

+77 Shoulder
£

+50

FECOIR
£

+34 FE
90

9+00

FE
1

4 APRIL 1963

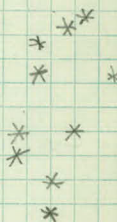
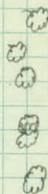
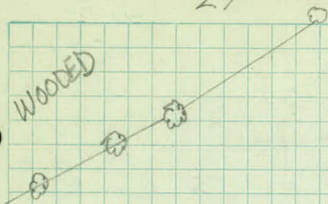
Lt

E

Rt

27

WOODED



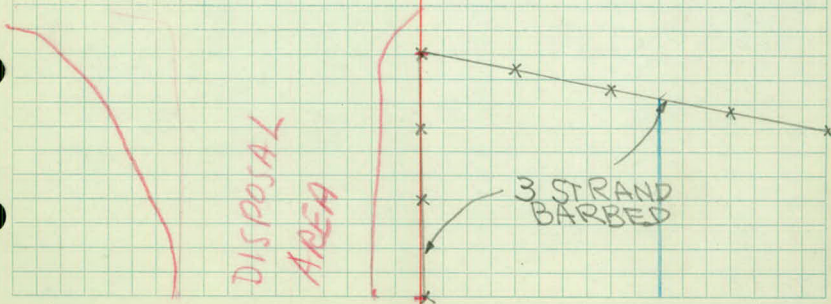
0

LOWER AFTON RD

62-639-01

DISPOSAL
AREA

3 STRAND
BARBED



14+00

Lt

£

Fe
10

Rt

woods
11-49

+72 Begin Fe
2

+54 Cor Woods
4

+50

+20 EDGE WOODS
15

+48 Cor Woods
25

+14 Fe
25-100

+14 END WOODS
15-100

+14 Fe
11-100

+10 Cor Woods
68

+13 Iron mont
£

13+00

+86 Fence Cor
1

+64 Cor Woods
11

+56 Creek
45-100

+50

12+00 Cor Woods
56

Bend in Creek
11

WOODS
100

+93
£ Creek

+65 Begin Fe
3

+59 Cor Woods
83

+62 Cor Wood
7

+52 Cor Woods
22

11+50

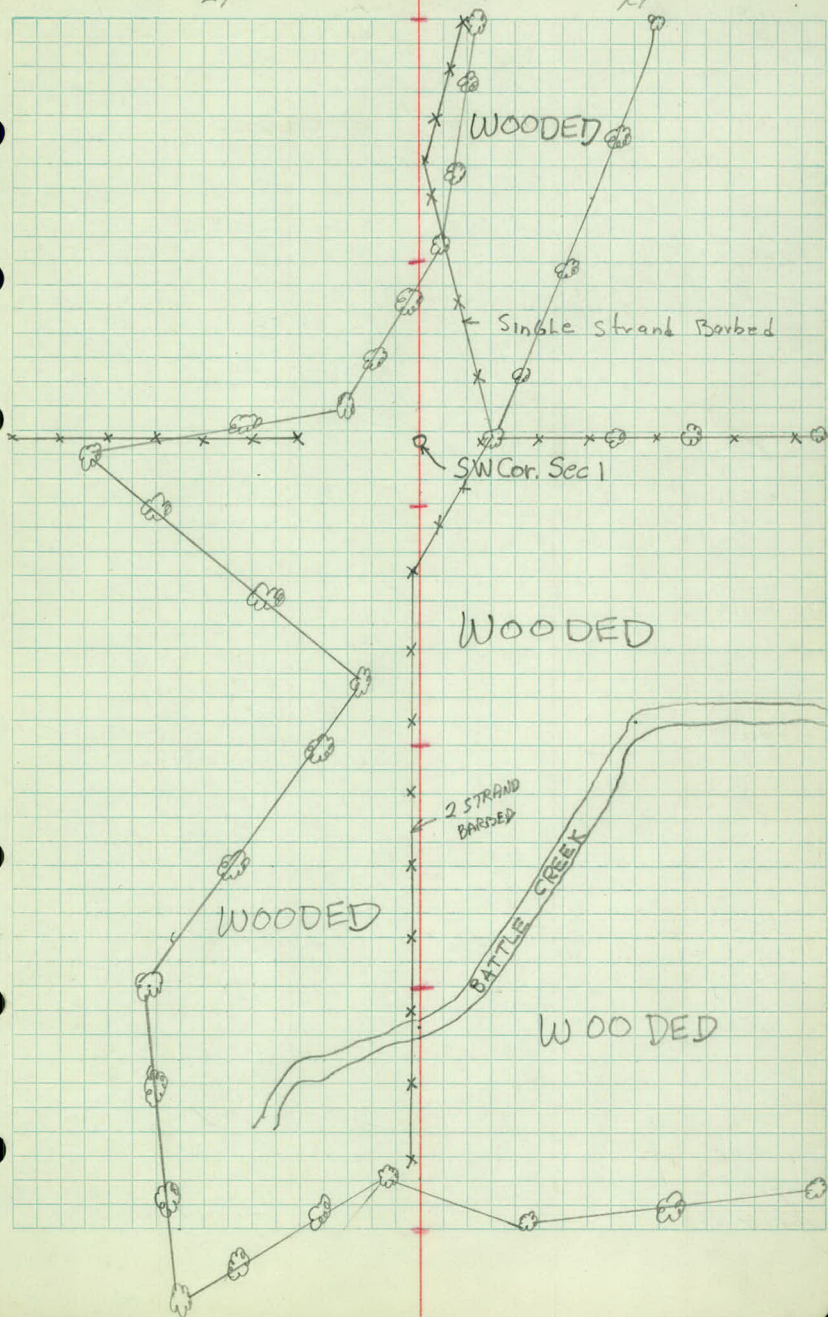
4 APRIL 1963

28

Lt

E

Rt



+50

Lt

±

Fe
41

Rt

16+00

Fe
42

+80 6" BE

+90 4" BE

97

103

+61 Fence Cor

42

+50

+50 Fence corner
66

+50 ENDWOOD
66-86

+34 4" ELM
14

+48 4" ELM
11

15+00

Fe
46

WOODS
46-73

+50

Fe
31

WOODS
23-59

14+00

Fe
10

WOODS
11-49

4 APRIL 1963

Rt

29

Uncultivated

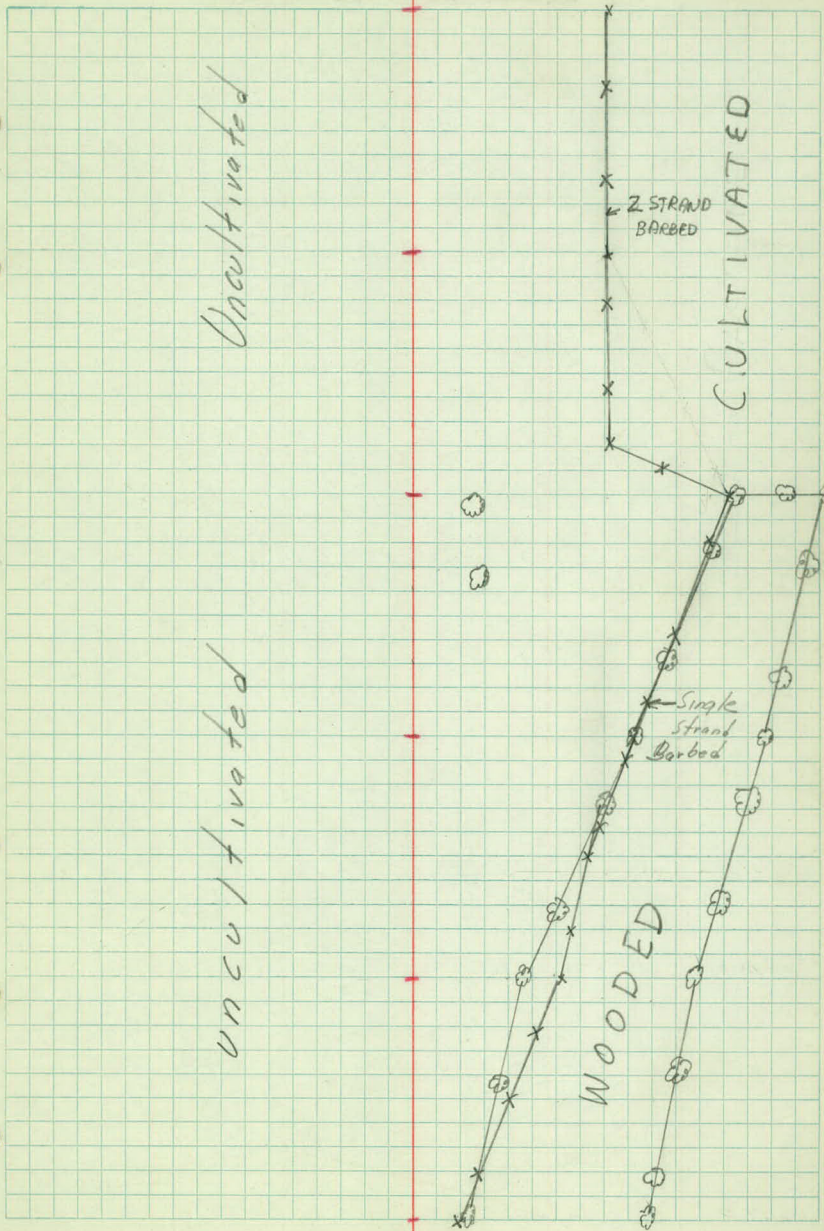
uncultivated

CULTIVATED

2 STRAND
BARBED

Single
Strand
Barbed

WOODED



19+00

Lt

\$ $\frac{Fe}{31}$

Rt

+50

18+00

$\frac{Fe}{35}$

+50

17+00

$\frac{Fe}{40}$

16+50

+50 $\frac{Fe}{41}$

4 APRIL 1963

30

Lt

Lt

Rt

uncultivated

cultivated

← 2 STRAND
BARBED

+50

Lt

£

FE
21

Rt

21+00

Fe
23

+50

20+00

FE
27

+50

19+00

Fe
31

4 APRIL 1963

31

Lt

Lt

Lt

uncultivated

cultivated

← 2-STRAND
BARBED



24+00

Lt

£

Rt

+95 12" OAK
71

+88 16" OAK
43

+53 12" OAK
85

+50 10" OAK
33

+44 RT Fe

+37 Fe Cor
15

+99 12" OAK
88

+98 12" OAK
105

+55 12" OAK
68

+55 24" OAK
93

+47 10" OAK
33

+44 12" OAK
30

+46 12" O
47

+50

23+00

FE

15

+50

22+00

FE

19

21+50

FE

21

4 APRIL 1963

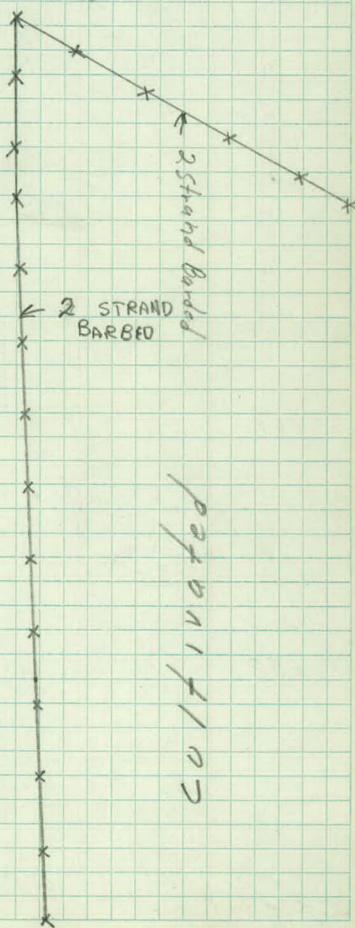
32

Lt

E

Rt

uncultivated



cultivated

+50

26+00

+91 SE GORGA
58

+50

25+00

+99 STP
18

+71 8" OAK
19

+63 6" OAK
25

+50

+43 10" OAK
17

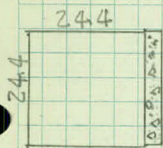
+20 10" OAK
24

+11 10" OAK
33

24+00

4 APRIL 1963

33



uncultivated

12



29+00

Lt

RD
15-39

Fe
37

Rt

+88 PP
43

776 Fe Cor
45

+54 Fe Cor
82

+50

28+00

SE COR HO
60

conc
63-79

+67 N.E. COR SW

+67 CONC
63-79

51 +63 SE COR SW
51

+62 PP
44

+70 ER
41

+58 hyd

+52 BR
52

53 +60 POR
43

+50

+17 POR
41

+20 ER
51

+38 MH
81

+08 BR
37

+11 N.E. COR SW
51

+10 3-7 BE
87

+07 S.E. COR SW
51

27+00

+96 PINE
54

+53 S.E. COR HO
59

26+50

4 APRIL 1963

34

47

34

Rf

io.0
Board fence

39.5

$1\frac{1}{2}-5-5$

28

18.4

710 Road

T

oil Road

*

1111
dirt
Road

44.6

2-S-S

29.6

+50

Lt Fe
50

Rd
18-41

± 50 5' Balcon Rt
18

+17 Fence Cor
50

+17 FC
50-55

+40 PP
40

+39 12" BE

7 +38 30" ELM
20

+30 14" BE
18

31+00

+92 SE Cor Ho
55

Rd
18-40

+69 NW Cor BLDG
75

+77 PP
77

+63 SE Cor SW
50

+67 NE Cor SW
50

+86 SW Cor BLDG
78

+57 POR
40

+67 ER
40

+56 HYD
54

+53 BR
52

+50

+37 ± Rd

+21 ER
51

+14 AD
45

+44 N. END OF TANK
29

+38 PP
74

+18 POR
41

+11 NE Cor SW
50

+26 S. END TANK
28

+35 W. END OF TANK
19

+07 BR
39

+07 SE Cor SW
50

+19 RT BLDG

+16 SW Cor Bldg
75

30+00

RD
17-39

+00 SW Cor Corn Crib
73

+93 SW Cor Corn Crib
73

+83 CTR 2'0 STOPS
51

+82 END WALL
51

+53 BEGIN WALL
51

+48 SW (2.0)
44+

+53 SE Cor Ho
56

+53 NE Cor Flower Box
51

+50

S. E. Cor
+49 Flower Box
51

+43 RT
BLDG

+40 NW Cor BLDG
81

+42 NW Cor Shed
30

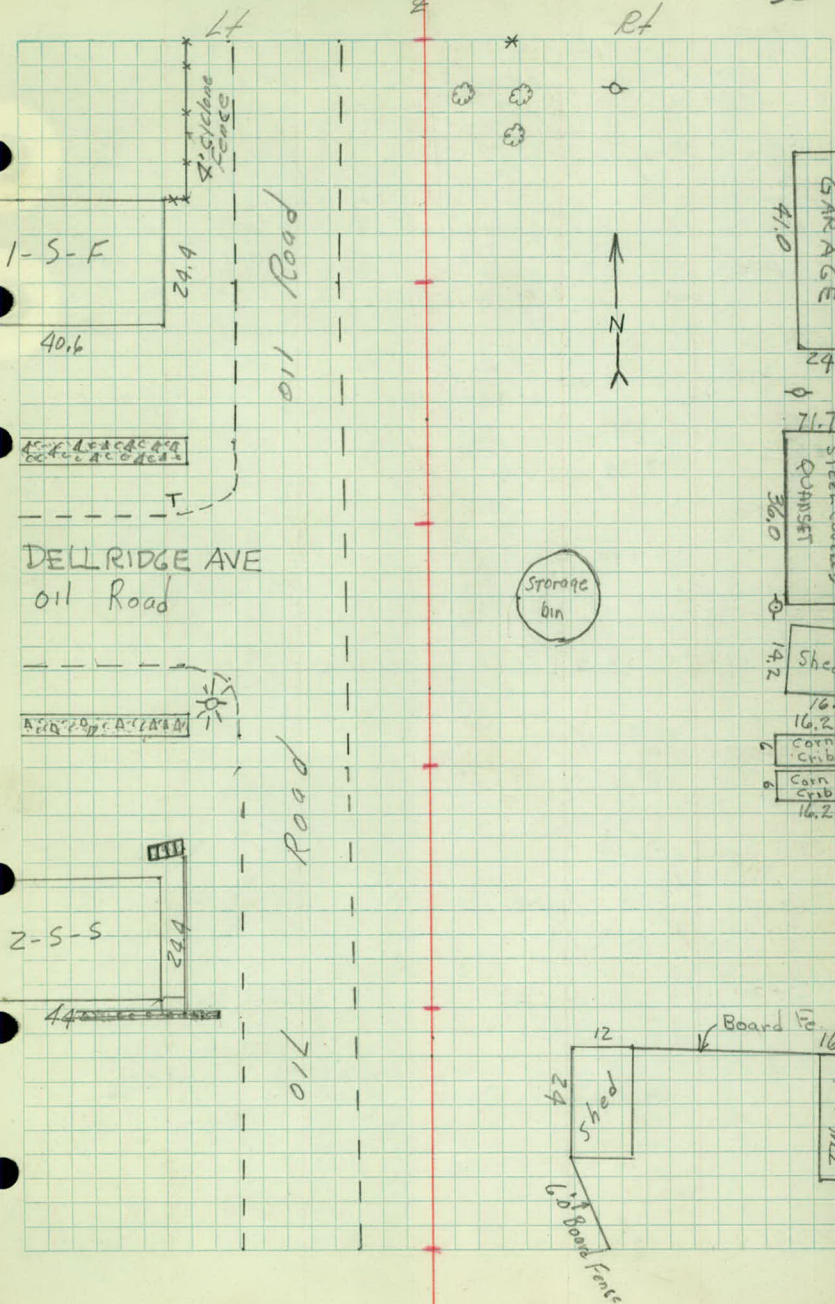
+18 SW Cor Shed
29

29+00

Fe
37

4 APRIL 1963

35



34+00 Lt R+
 +68 SW +97 SE COR HO +97 SW
 63-67 55 63-67
 +63 SE COR SW +68 NE COR SW
 51 50
 +64 ER +57 POR +63 PP
 46 47 47
 +53 BR +53 E END CURB
 50 50

+50
 +37 MH
 29
 +20 GASSHUTTER
 51
 +15 POR +22 ER
 42 50
 +12 NE COR SW
 51
 +07 Conc Driveway
 57-66
 +06 BR +07 SE COR SW
 41 51

33+00 RD
 +90 Pine 21-41
 52
 +85 Pine 52
 +79 Conc Drive
 58-67

+50
 +49 SE COR HO
 55
 +35 Pine +28 4" MAPLE
 58 71

32+00 Rd
 18-41
 +99 Balsam 56
 +88 Fe +88 End Fe +90 PP
 51-100 51 43
 +84 SW COR Greenhouse
 83

31+50

4 APRIL 1963

36

Lt

+

Rt

44.3

45° 45' 45" 45° 45' 45"



CARDINAL PL 0

45° 45' 45" 45° 45' 45"

41

1-5-5

14

27

*



4' cycloae

oil Road

un cultivated

*

186

+50

Lt

£

Rt

+21 ER
55
+17 POR
47
+08 BR
42

+37 MH
39

+12 NE COR SW
52

+14 PD
47

+07 SE COR SW
52

+07 DRIVE
59-75

36+00

71 1" Poplar
50

+46 1" Poplar
50

+41 1" Poplar
50

+87 DRIVE
58-74

+56 1" Poplar
50

+51 SE COR NW
56

+76 1" Poplar
50

+51 1" Poplar
50

+50

+29 1" POP
49

+18 1" POP
50

+13 1" POP
50

+07 1" POP
49

35+00

+34 1" POP
49

+40 1" POP
49

+23 1" POP
49

+45 1" POP
49

+40 1" MAPLE
58

+90 BEGIN BOARD FE
51

+87 BOARD FE
51-110

+87 PD
69

+87 PD
47

+50

+50

+24.5 NE COR SW
51

+21 SE COR SW
51

34+00

RD
23-47

16 APRIL 1963

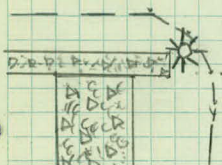
Lt

~~X~~

Rt

37

Berland Plo

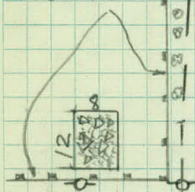


1-5-5

26

46

5'0 BOARD FF



Oil Road

Oil

44.3

1-5-5

24.3

39+00 Lt RD 5-28
+76 Driveway +90 MH
60-77 37

Rt

+76 Sidewalk Cor
56

+76 SW +60 SW
56-60 56-58

+50

+49 S.E. Cor. Ho
59

+44 Cor Woods (END)
26

+45 SW
56-58

38+00

RD
20-40

WOODS
8-54

+50

WOODS
18-59

+08 S. END 9" X 12.0 CM
45

+37 Cor Woods
11

37+00 RD
+99 SE Cor Ho 23-41
56

WOODS
46-67

+67 N to Cor SW +95 1" Pipe
51 55

+63 ER
47

+91 Cor Woods
67

+91 Cor Woods
46

+62 SE Cor SW +55 POR
51 48

+52 BR
53

+77 Cor Woods
33

36+50

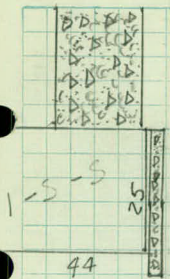
16 APRIL 1963

38

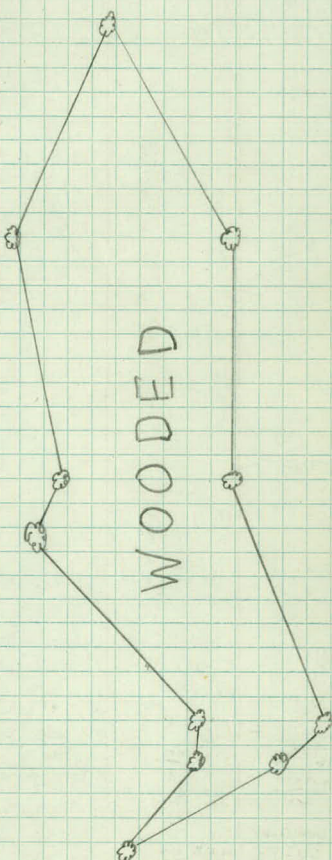
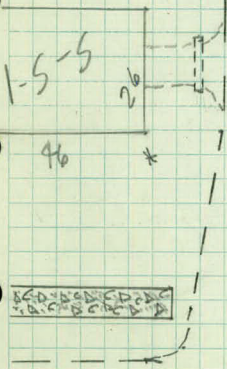
44

24

Rt



Road



WOODED

Lt

2

Rt

40+00

+87 ERC
23+75 PORC
25+66 SRC
42+65 CB
55+44 MH
6

+50

+38 MH
51+27 Shutoff
59+30 Shutoff
50+19 PORC
36+13 Shutoff
40+03 DRIVEWAY
60-77+04 Shutoff
31

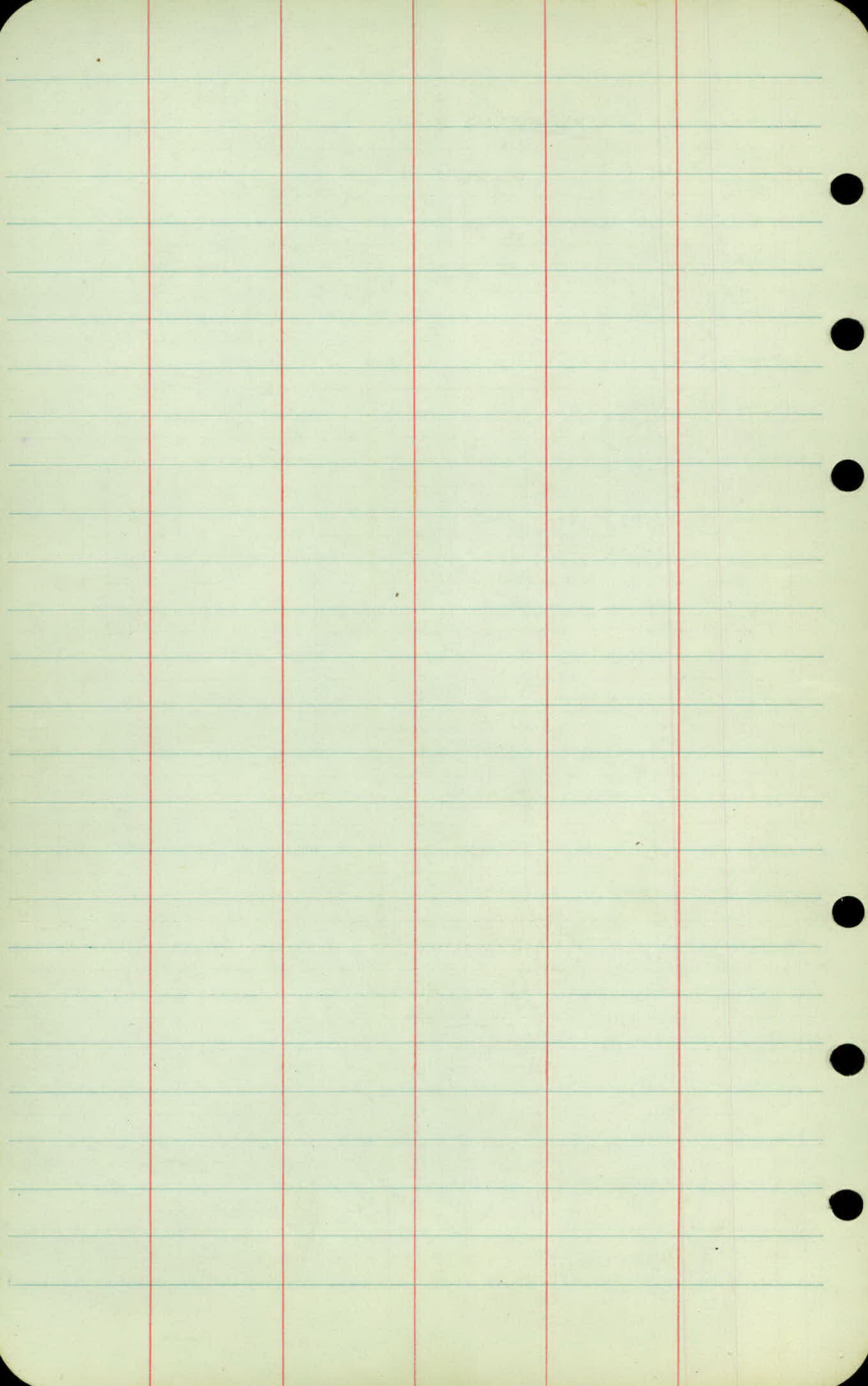
39+00

+22 CB
53+11 HNB
58+09 MH
41+08 SW
50+03 BRC
28+21 ERC
94+12 Shutoff
38+09 Shutoff
39+13 PORC
5+04 BRC
5+03 SECORSW
50

RD

5-28

+76 NEND 15" X SCP
68+84 ER
31+57 OR
66+77 NEND 36" X SCP
89+68 PORC
28+17 S.FND 36" X 60' SCP
96+30 ERC
25



KP
DS
WM

3 MAY 1965

40

MC KNIGHT RD.

MAILAND RD TO UPPER AF100 RD

TOPOGRAPHY

LT

E

RT

40+00

+75

N.END 15' SCP	N.END 30' SCP
<u>70</u>	<u>90</u>

+66 CB
<u>55</u>

+50

+45 MH

7

+38 MH
<u>52</u>

+25

+22 CB
<u>53</u>

+17 S.END 30' SCP
<u>97</u>

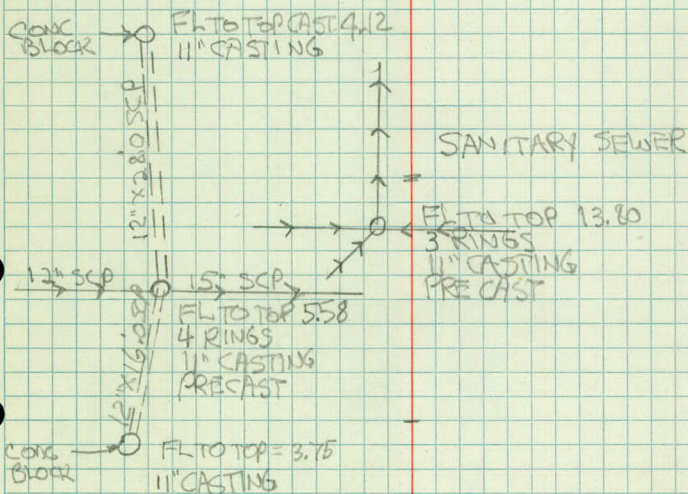
39+00

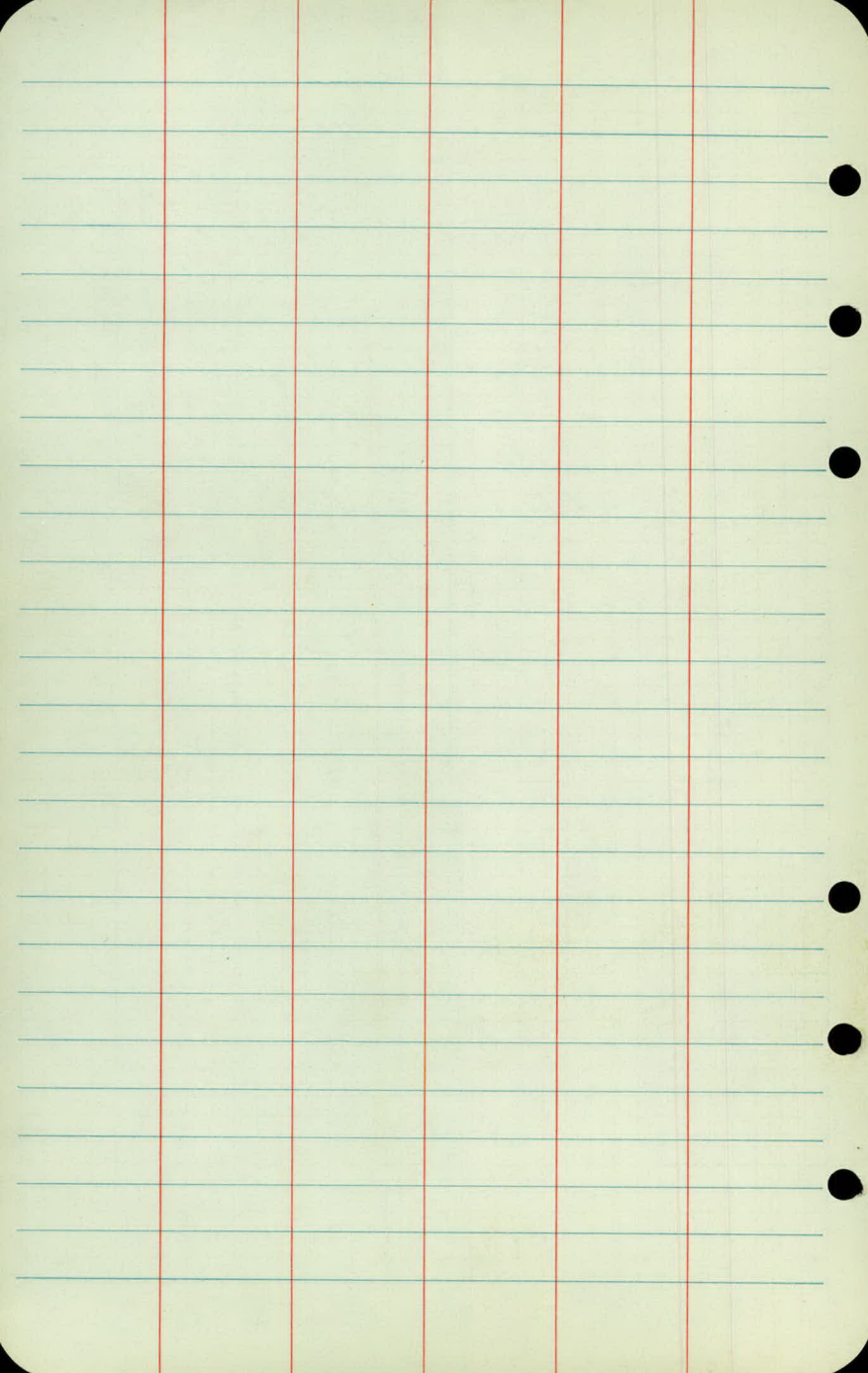
41

LT

4

RT





KP
WM
FS
DS
PK

19 JAN. 1965

42

BENCH LEVELS

MAILAND RD. TO UPPER AFTON RD.

STA	+	π	-	ELEV.
BM	12.47	984.87		972.40
	11.97	995.96	0.88	983.99
			10.46	985.50
	0.85	991.01	5.80	990.16
	4.92	989.73	6.20	984.81
			3.01	986.72
	6.71	991.61	4.83	984.90
			4.89	986.72 (986.72)
			6.79	984.82 (984.82)
	6.33	996.49	1.45	990.16 (990.16)
	0.08	985.58	10.99	985.50 (985.50)
	0.66	973.06	13.18	972.40 (972.40)
	1.36	964.71	9.71	963.35 (963.35)
	0.14	951.74	13.11	951.60 (951.60)
	0.96	939.92	12.78	938.96 (938.96)
	0.70	929.09	11.53	928.39 (928.38)
	1.84	917.51	13.42	915.67 (915.66)
	0.67	912.54	5.64	911.87 (911.85)

19 JAN. 1965

43

DESCRIPTION

TOP N.W. COR LOWER STEP HO# 366 MCKNIGHT

TOP PK $\neq$ STA 62+00

SPIKE IN PP 28.0 LT STA 62+00

SPIKE IN PP 24.0 LT STA 57+38

SPIKE IN PP 23.0 LT STA 54+01

SPIKE IN ARC-LITE POLE SW. COR MCKNIGHT RD
& MAILAND RD.

N.E. COR LOWER STEP HO# 475 MCKNIGHT

SPIKE IN ARC-LITE POLE SW. COR MCKNIGHT
RD & MAILAND RD.

SPIKE IN PP 23.0 LT STA 54+01

SPIKE IN PP 24.0 LT STA 57+38

SPIKE IN PP 28.0 LT STA 62+00

TOP N.W. COR LOWER STEP HO# 366 MCKNIGHT

NAIL IN 2" CE 22.0 RT STA 1+00

SPIKE IN 10" OAK 19.0 RT STA 2+33

SPIKE IN 18" ELM 70.0 RT STA 4+00

SPIKE IN 6" COTT 26.0 RT STA 5+30

SPIKE IN 5" POPLAR 22.0 RT STA 6+85

TOP HYDRANT N.W. COR MCKNIGHT ^{LOWER} AFTON RD

STA + π - ELEV.

912.54

BM 13.33 917.86 7.98 904.56 (904.53)

13.51 929.36 2.01 915.85

12.05 940.66 0.75 928.61

1.01 940.80 0.87 939.79

4.38 935.60 9.58 931.22

12.42 947.90 0.12 935.48

0.31 940.76 7.45 940.45

0.44 927.79 13.41 927.35

1.50 923.10 6.19 921.60

9.16 913.94 (914.05)

BM 13.39 917.92 (904.53)

13.38 929.24 2.06 915.86 (915.85)

12.13 940.74 0.63 928.61 (928.61)

1.02 940.81 0.95 939.79 (939.78)

4.45 935.68 9.58 931.23 (931.22)

12.29 947.77 0.20 935.48 (935.48)

KD
FS
WM
DS
AK

20 JAN. 1965
SUNNY 25°
DESCRIPTION

44

TOP IRON MONT N.W. COR S12-T28-R22

SPIKE IN 4" ELM 20'0 RT STA 14+35

TOP SPIKE E STA 19+00

SPIKE IN 16" OAK 40'0 RT STA 23+60

S.E. COR ENTRANCE SLAB 55'0 LT STA 25+90

SPIKE IN PP 43'0 LT STA 28+88

SPIKE IN ARC-LITE POLE ^{47.0} 45'0 LT STA ³³⁺⁶³ ~~30+14~~

SPIKE IN ARC-LITE POLE 47'0 LT STA 36+14

TOP S.E. COR LOWER STEP BACK ENT.

HO #2256 UPPER AFTON RD

SPIKE IN 24" ELM 130'0 E STA 39+75

TOP IRON MONT N.W. COR S12-T28-R22

SPIKE IN 4" ELM 20'0 RT STA 14+35

TOP SPIKE E STA 19+00

SPIKE IN 16" OAK 40'0 RT STA 23+60

S.E. COR ENT SLAB 55'0 LT STA 25+90

SPIKE IN PP 43'0 LT STA 28+88

STA + π - ELEV.

947.77

0.23 940.⁶⁷68 7.33 940.44 (940.45)

0.50 927.⁸⁴85 13.33 927.³⁴35 (927.35)

1.40 923.^{2.99}00 6.25 921.⁵⁹60 (921.60)

6.33 916.⁶⁶67 (916.66)

9.05 913.⁹⁴95 (913.95)

20 JAN. 1965

45

DESCRIPTION

SPIKE IN ARC-LITE POLE 45.0' LT STA ³³⁺⁶²~~30+14~~

SPIKE IN ARC-LITE POLE 47.0' LT STA 36+14

TOP S.E. COR LOWER STEP BACK ENTRANCE

HO# 2256 UPPER AFTON RD.

SPIKE IN PP NW. COR MCKNIGHT RD.

UPPER AFTON RD.

SPIKE IN 24" ELM 130.0' E. STA 39+75

STA + π - ELEV

Bench Levels

Sta	+	π	-	Elev.
BM.	0.85	973.25		(972.40)
	0.72	964.09	9.88	963.37
	0.09	951.71	12.47	951.62
	0.40	939.38	12.73	938.98
	0.35	928.77	10.96	928.42
	0.00	915.62	13.15	915.62
			3.77	911.85
			11.13	904.49 (904.53)

Description

Top N.W. Cor. Lower step Ho[#] 366 McKnight.

● Nail in 2" Chinese elm 2' Rt Sta 1+00 @ 20'E

Spike in 10" OAK 1.0 Lt Sta 2+33 @ 20'E

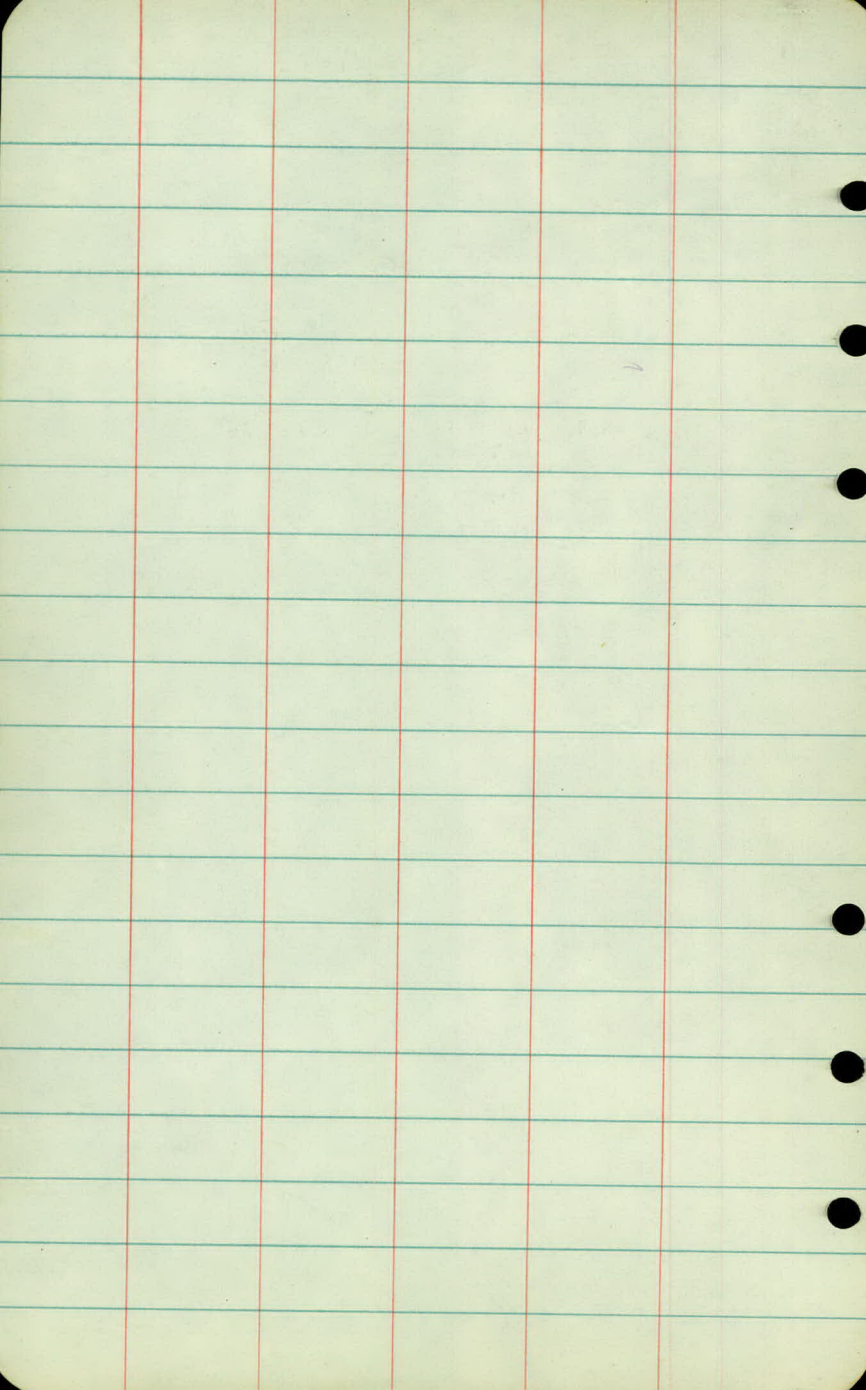
● Spike in 18" Elm 30' Rt Sta 4+00 @ 20'E

Spike in 6" poplar 6' Rt Sta 5+30 @ 20'E

● Spike in 5" poplar 2' Rt Sta 6+85 @ 20'E

Top hydrant N.W. Cor McKnight c'lower Affen Rd

Top iron mont N.W. Cor Sec 12 - T28 - R22



KB
FS
DS
WS
LDD

April 5, 1965
Fair 40°

48

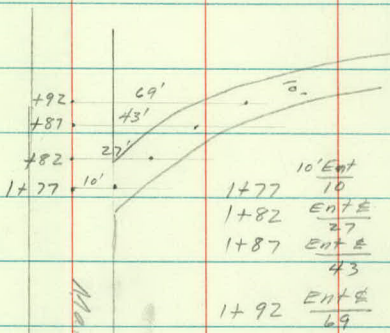
1

Profile

Mailand Road

Lower Afton Rd to 350' East

2 pages



Lower Afton Rd

2

Rd

sta	+	π	-	EIV
BM	13.72	1000.44		986.72
0+00			12.8	
+14			12.2	
+50			9.7	
1+00			6.7	
+50			4.8	
+77			4.0	
2+00			3.3	
+50			1.9	
3+00			0.9	
+50			0.4	
TP	1.58	993.58	8.44	992.00
BM			8.69	984.89 (984.90)

Apr. 5, 1965

49

2

Description

Spike in PP SW Cor M^cKnight $\frac{1}{2}$ Mailand Rd.

Shoulder

$\frac{1}{2}$ Mailand Rd

$\frac{1}{2}$ " "

$\frac{1}{2}$ " "

$\frac{1}{2}$ " "

$\frac{1}{2}$ Ent $\frac{1}{2}$ Mailand Rd

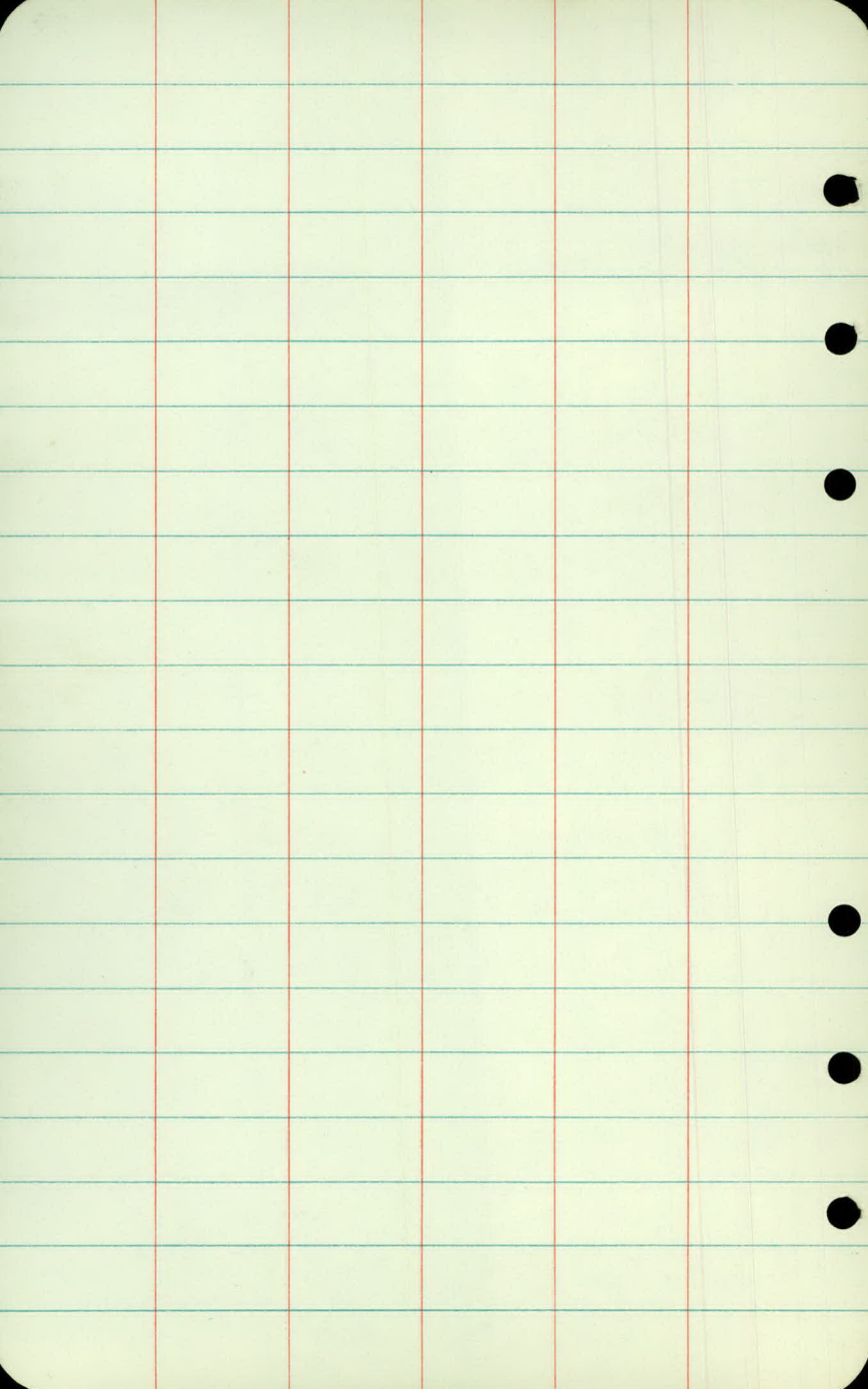
$\frac{1}{2}$ Mailand Rd

$\frac{1}{2}$ " "

$\frac{1}{2}$ " "

$\frac{1}{2}$ " "

Top NE Cor. lower Step Ho. # 475 M^cKnight Rd.



RP
WM
DS
ES
PK

22 JAN. 1965
CLOUDY & WINDY
28°

50

McKNIGHT RD
MAILAND RD TO LONDIN LANE

X- SECTIONS

STA	+	-	ELEV.
BM	19.30	1006.02 1005.5	986.72

49+00

✓

+10 $\nless$ ENTRANCE LT

✓

+51 $\nless$ ENTRANCE RT

LT

E

22 JAN. 1965

RT

51

SPIKE IN ARC - LITE POLE SW COR. MAILAND

RD : MCKNIGHT RD

X

$q2.1$ $q1.1$ $q0.4$ $q9.7$ $q9.8$ $q0.0$ $q0.1$ $q2.0$

13.9 14.9 15.6 16.3 16.2 16.0 15.9 14.0
 42 20 13 8 11 14 19

$q2.9$ $q3.2$

13.1 12.8
 61 75

$q6.1$ $q4.2$ $q3.2$

9.3 11.8 12.8
 75 50 25

$q2.9$ $q2.1$ $q0.9$ $q0.2$ $q0.4$

13.1 13.9 15.1 15.8 15.6 15.4 15.3 13.7 12.5
 54 36 16 8 10 14 17 23

$q3.2$ $q3.2$

12.76 12.8
 72 77
 conc. 40

$q7.4$ $q5.8$ $q5.3$ $q4.0$

8.6 10.2 10.7 12.0
 75 60 45 37

$q3.3$ $q2.5$ $q3.1$ $q2.8$ $q2.4$ $q2.7$ $q2.7$ $q3.4$ $q5.9$

12.7 12.5 12.9 13.2 13.6 13.3 13.3 12.6 10.1
 77 57 33 15 9 12 26 50

Ho

FE

00.0

6.0
 75

STA + π - ELEV.

1006.02

49+65

✓

+72

✓

50+00 = N. EDGE 4.0' SIDEWALK

✓

LT

E

22 JAN. 1965

RT

52

$\overset{\cdot}{92.8}$ $\overset{\cdot}{93.3}$ $\overset{\cdot}{93.0}$ $\overset{\cdot}{93.3}$ $\overset{\cdot}{93.1}$ $\overset{\cdot}{94.4}$ $\overset{\cdot}{95.6}$
 13.2 12.7 13.0 12.7 12.9 11.6 10.4
 32 12 8 13 23 33

$\overset{\cdot}{93.2}$ $\overset{\cdot}{93.6}$ $\overset{\cdot}{93.6}$
 12.8 12.4 12.4
 45 60 75

$\overset{\cdot}{94.4}$ $\overset{\cdot}{94.6}$ $\overset{\cdot}{97.0}$
 1.6 6.4 9.0
 74 52 41

$\overset{\cdot}{94.3}$ $\overset{\cdot}{94.3}$ $\overset{\cdot}{93.6}$ $\overset{\cdot}{93.2}$ $\overset{\cdot}{93.5}$ $\overset{\cdot}{93.4}$ $\overset{\cdot}{94.5}$ $\overset{\cdot}{96.3}$
 11.7 11.7 12.4 12.8 12.5 12.6 11.5 9.7
 36 16 11 8 11 23 32

$\overset{\cdot}{99.6}$ $\overset{\cdot}{94.4}$
 11.4 11.6
 58 77
 40

$\overset{\cdot}{90.4}$ $\overset{\cdot}{90.0}$ $\overset{\cdot}{97.6}$
 5.6 6.0 8.4
 61 49 42
 6A

$\overset{\cdot}{94.41}$ $\overset{\cdot}{94.19}$ $\overset{\cdot}{94.2}$ $\overset{\cdot}{93.7}$ $\overset{\cdot}{94.2}$ $\overset{\cdot}{94.0}$ $\overset{\cdot}{94.6}$ $\overset{\cdot}{95.6}$
 11.61 11.83 11.8 12.3 11.8 12.0 11.4 10.5
 36 17 14 8 12 17 23
 SW SW

$\overset{\cdot}{94.59}$ $\overset{\cdot}{94.72}$
 11.43 11.30
 56 74
 SW SW

$\overset{\cdot}{90.6.8}$ $\overset{\cdot}{94.7}$ $\overset{\cdot}{90.9}$ $\overset{\cdot}{98.9}$
 10.8 1.3 5.2 7.1
 75 54 39 29

STA

+

T

-

ELEV

1006.02

50+31

✓

+37

✓

+50

✓

STA	+	π	-	ELEV.
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		1006.02		
--	--	---------	--	--

50+67				
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✓				
+76	=	ENTRANCE	LT.	

✓				
TP	15.53	1008.27	13.28	992.74

51+00				
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22 JAN. 1965

54

LT

£

RT

91.8 92.7 92.9 93.5 93.9 93.8 95.8 01.1 03.5

14.2 13.3 13.1 12.5 12.1 12.2 10.2 4.3 2.5
44 24 15 9 11 16 26 37

90.8

9.9

06.1

06.4

15.2
6016.1
82+0.7 0.4
76 58

Ho

90.4

91.3

92.2

93.2

93.7

93.4

95.0

00.2

03.1

15.6 14.7 13.8 12.8 12.3 12.6 11.0 5.8 2.9
59 42 17 9 12 16 25 38

99.5

16.5

82
GA

01.4

05.5

+1.4 0.5
77 59

TOP PK £ STA 51+00

89.1

90.9

92.0

92.4

92.8

92.6

94.4

97.2

03.0

05.5

19.2

17.4

16.3

15.9

15.5

15.7

13.9

11.1

5.3

2.8

75

47

17

11

10

16

21

48

70

STA + π - ELEV.

1008.27

TR 8.50 1001.24 15.53 992.74

~~1000.7~~

51+25

✓

+50

✓

STA + π - ELEV.

1001.24

51+75

✓

TP 6.69 995.34 12.59 988.65

BM 10.41 995.31 10.41 984.93 (984.90)

994.8

52+00

✓

LT

E

22 JAN 1965 56

RT

85.8	86.2	87.5	88.9	89.5	89.5	89.4	90.9	92.9
15.4	15.0	13.7	12.3	11.7	11.7	11.8	10.3	8.3
56	28	20	12		8	11	14	27

86.6
14.6
75

97.3 95.2
3.9 6.0
75 46

TOP PR E STA 52400

N.E. COR LOWER STEP HO# 475 MCKNIGHT RD.

85.4	85.5	87.6	88.0	88.6	88.6	88.5	90.8	92.6
9.9	9.8	7.7	7.3	6.7	6.7	6.8	4.5	2.7
52	29	18	13		7	11	16	28

86.3
9.0
75

97.0 93.4
+1.7 1.9
75 40

STA + N - ELEV.

995.31

52+22

+34 = GUTTER LINE (RT)

+46 ± MAILAND RD (RT.)



+53 = GUTTER LINE LT: RT. N. GUTTER RT

S. GUTTER LT

+62 ± MAILAND RD (LT)

LT

S

22 JAN 1965 57

RT

85.9	85.2	85.5	86.1	87.4	88.0	88.3	91.8	93.2	95.3
9.4	10.1	9.8	8.6	7.9	7.3	7.0	3.5	2.1	0.0
75	55	30	17	11		14	23	48	75

85.9	85.0	85.8	86.5	87.2	87.9	88.3	88.8	90.6	92.3
9.4	10.3	9.5	8.8	8.1	7.4	7.0	6.5	4.7	3.0
75	53	26	19	12		15	28	54	75

85.3	85.6	86.3	87.0	87.7	88.1	89.9	92.2	93.9
10.0	9.7	9.0	8.3	7.6	7.2	5.4	3.1	1.4
65	45	25	12		10	37	69	100

85.5
9.8
75

96.8 96.3 95.3 95.1
+1.5 +1.0 0.0 0.2
175 156 131 125

83.5	84.8	85.6	87.0	87.5	87.9	88.8	91.3	92.2
11.8	10.5	9.7	8.3	7.8	7.4	6.5	4.0	3.1
75	49	29	12		8	33	61	75

80.1	80.4	82.0	84.1	85.4	86.8	87.3	87.8	89.8	90.8	91.4	92.1
17.2	14.9	13.3	11.2	9.9	8.5	8.0	7.5	7.5	4.5	3.9	3.0
150	125	100	66	38	13		15	24	31	52	75

STA + π - Elev.

995.31

52+71 = GUTTER LINE (LT)

+80

53+00

BM 4.3 8 989.20 10.49 984.82 (984.82) ✓

53+50

✓

22 JAN. 1965 59

LT

RT

✓ 84.2	84.7	85.1	86.6	87.2	87.1	90.3	91.1	92.2
11.1	10.6	10.2	8.7	8.1	8.2	5.0	4.2	3.1
75	60	34	13		14	23	49	75

✓ 84.5	84.8	85.3	86.4	86.9	87.0	89.7	90.9	91.7
10.8	10.5	10.0	8.9	8.4	8.3	5.6	4.4	3.6
75	55	24	13		12	18	44	75

✓ 84.6	84.7	85.4	86.0	86.4	86.3	87.7	88.8	89.5
10.7	10.6	9.9	9.3	8.9	9.0	7.6	6.5	5.8
75	51	22	14		8	14	41	75

SPIKE IN PP 23'0 LT STA 54+01

✓ 84.5	84.2	84.6	85.2	85.5	85.4	85.4	84.5
4.7	5.0	4.6	4.0	3.7	3.8	3.8	4.7
75	60	36	14		5	10	19

84.6
4.6
90
40

84.8
4.4
75

84.0
5.2
41

STA + π - ELEV.

989.20

53+85 = $\frac{1}{2}$ TWIN ENTRANCES (LT.)

✓

54+00

✓

+14 $\frac{1}{2}$ ENTRANCE (LT.)

✓

25 JAN 1965

60

LT

E

RT

84.20

5.00

69

CONC. APPROX

GA

84.4

4.8

39

84.9

4.3

15

85.1

4.1

84.9

4.3

4

84.5

4.7

10

82.1

7.1

20

81.5

7.7

28

83.1

6.1

75

82.3

6.9

70

81.6

7.6

51

83.8

5.4

75

84.0

5.2

55

84.0

5.2

35

84.9

4.3

15

85.0

4.2

84.8

4.4

4

84.6

4.6

8

83.3

5.9

16

81.2

8.0

20

82.4

6.8

75

81.7

7.5

71

81.0

8.2

47

84.1

5.1

54

84.4

4.8

30

84.7

4.5

17

85.1

4.1

7

84.9

4.3

84.7

4.5

5

84.3

4.9

10

83.2

6.0

15

81.1

8.1

20

83.9

5.3

75

81.8

7.4

75

81.2

8.0

65

80.0

8.4

41

STA	+	K	-	ELEV.
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STA	+	K	-	ELEV.
-----	---	---	---	-------

989.20

STA	+	K	-	ELEV.
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54+50

STA	+	K	-	ELEV.
-----	---	---	---	-------

✓

STA	+	K	-	ELEV.
-----	---	---	---	-------

55+00

STA	+	K	-	ELEV.
-----	---	---	---	-------

✓

STA	+	K	-	ELEV.
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+22 = ~~±~~ ENTRANCE (LT)

STA	+	K	-	ELEV.
-----	---	---	---	-------

✓

25 JAN. 1965 61

LT

RT

84.2	84.3	84.5	85.1	84.9	84.7	84.4	82.2	80.9
5.0	4.9	4.7	4.1	4.3	4.5	4.8	7.0	8.3
75	41	17	6		4	8	15	20

84.14
5.06
83
SW

81.2 80.1
8.0 8.5
75 43

84.3	84.8	85.0	85.3	85.1	85.0	84.8	82.8	82.2
4.9	4.4	4.2	3.9	4.1	4.2	4.4	6.4	7.0
43	22	18	6		4	8	17	23

84.07
5.13
62
CONC.

84.3
4.9
75

83.0 82.4 82.2
6.2 6.8 7.0
75 59 44

83.8	84.6	85.2	85.5	85.4	85.3	85.2	85.2	84.1
5.4	4.6	4.0	3.7	3.8	3.9	4.0	4.0	5.1
35	25	17	7		5	8	13	18

83.0 81.8
6.2 7.4
54 75

83.6 83.0 83.3
5.6 6.2 5.9
75 53 33

STA + π - ELEV.

989.20

55+50

✓

9.45 994.57 4.08 985.12

B.M 4.75 994.91 4.40 990.17 990.16

9.78 985.13 985.12

56+00

25 JAN. 1965 62

LT

≠

RT

84.8	85.5	85.1	85.9	85.7	85.1	85.6	86.0	85.8
4.4	3.7	3.5	3.3	3.5	3.5	3.6	3.2	3.4
29	24	17	7		4	7	11	16
84.3	84.0	82.6	81.4		84.8	84.6	84.7	85.7
4.9	5.2	6.6	7.8		4.4	4.6	4.5	3.5
31	42	37	75		75	63	45	32

TOP PK ≠ STA 55+00

SPIKE IN PP 24.0 LT STA 57+38

TOP PK ≠ STA 55+00.

86.3	81.4	86.3	86.6	86.6	86.5	86.6	88.3	89.3
8.6	7.5	8.6	8.3	8.3	8.4	8.3	6.6	5.6
36	25	21	9		3	6	10	19
84.2	81.8				88.1	88.1	89.2	
10.7	13.1				6.8	6.8	5.7	
55	75				75	55	37	

STA	+	K	-	ELEV.
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		994.91		
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56+25				
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✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

+80				
-----	--	--	--	--

✓				
---	--	--	--	--

KP
DS
FS
WM
PK

LT

26 JAN. 1965 63
SUNNY & WINDY
100 RT

86.6	86.8	86.4	87.0	86.9	86.9	86.9	86.6	89.5
8.3	8.5	8.2	7.9	8.0	8.0	8.0	6.3	5.4
25	22	16	9		3	5	12	27

85.1	82.1	80.1
9.8	12.2	14.8
37	59	75

91.2	90.8	90.0
3.7	4.1	4.9
75	64	47

82.9	86.5	86.1	87.3	87.3	87.3	88.1	89.8	91.9
12.0	8.4	8.2	7.6	7.6	7.6	6.4	5.1	3.0
35	25	19	9		5	12	28	49

81.2	79.2	78.8
13.7	15.7	16.1
46	66	75

92.9
2.0
75

82.0	81.1	81.3	81.9	81.8	81.8	88.1	90.0	90.0
12.9	7.8	7.6	7.0	7.1	7.1	6.2	5.9	4.9
35	23	18	9		6	12	22	34

79.9	77.8	76.9
15.0	17.1	18.0
43	67	75

93.1	93.9	92.9
1.2	1.0	2.6
75	68	49

STA

+

π

-

ELEV.

994.91

57+00

✓

+35

✓

+58

✓

26 JAN. 1965

64

LT

RT

84.2	87.5	87.8	88.5	88.3	88.2	89.0	89.4	90.5
10.7	7.4	7.1	6.4	6.6	6.7	5.9	5.5	4.4
32	25	19	9		5	11	24	36

81.8	79.4	77.5
13.1	15.5	17.4
39	59	75

93.1	93.8	93.1
1.8	1.1	1.8
75	67	55

90.1	89.0	89.5	90.0	89.8	89.8	91.1	92.3	93.8
4.8	5.9	5.4	4.9	5.1	5.1	3.8	2.6	1.1
28	25	18	9		6	13	24	39

90.4	90.4	83.4	82.5
4.5	4.5	11.5	12.4
37	51	68	75

90.6	91.3	91.1	90.6	91.1	90.9	90.9
4.3	3.6	3.8	4.3	3.8	4.0	4.0
50	40	25	19	9		5

90.3	84.6
4.6	10.3
59	75

STA	+	π	-	ELEV.
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		994.91		
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BM	9.58	999.74	4.75	990.16	990.16
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57+35

+58

+83

LT

E

26 JAN. 1965 65

RT

SPIKE IN PP 24.0 LT STA 57+38

94.7	94.7	93.9
5.0	5.0	5.8
56	67	75

93.3	95.2	96.5	96.8
6.4	4.5	3.2	2.9
12	20	36	51

95.1	96.3
4.6	3.4
75	64

92.3	91.7	91.8	92.1	92.0	92.0	93.2	94.0	98.2
7.4	8.0	7.9	7.6	7.7	7.7	6.5	5.7	1.5
28	23	17	9		5	9	13	24

92.4	91.7	95.8
7.3	8.0	13.9
48	62	75

97.9	98.2	98.1
1.8	1.5	1.6
75	60	37

STA + T - ELEV.

999.74

58+00



+29



+62



LT

E

26 JAN. 1965 66

RT

✓ 92.5	92.8	92.3	92.3	92.8	92.6	92.6	93.4	94.3	97.0
7.2	6.9	7.4	7.4	6.9	7.1	7.1	6.3	5.4	2.7
46	29	22	18	8		5	8	13	22
90.7	87.0						98.2	98.1	97.9
9.0	12.7						1.5	1.6	1.8
56	75						75	54	36
✓ 90.7	92.6	92.9	93.4	93.3	93.3	94.4	95.4	95.1	
9.0	7.1	6.8	6.3	6.4	6.4	5.3	4.3	4.6	
36	25	21	11		5	8	17	25	
89.2	87.3	86.3					96.4	96.2	
10.5	12.4	13.4					3.3	3.5	
53	67	75					75	49	
✓ 90.9	93.4	93.3	93.7	93.7	93.7	94.3	94.6	94.9	
8.8	6.3	6.4	6.0	6.0	6.0	5.4	5.1	5.4	
34	25	21	10		6	9	17	23	
89.4	88.0	87.7					94.5	94.4	94.6
10.3	11.7	12.0					5.2	5.3	5.1
53	68	75					75	63	47

STA + T - ELEV.

999.74

59+00

✓

+27

✓

+66

✓

LT

E

RT

26 JAN. 1965 67

92.7	93.7	93.4	93.7	93.6	93.6	94.4	93.9	94.2
7.0	6.0	6.3	6.0	6.1	6.1	5.3	5.8	5.5
38	24	20	9		6	10	21	40

91.2	89.9
8.5	9.8
54	75

92.6	92.8	93.1
7.1	6.9	6.6
75	67	52

93.6	93.9	93.1	93.3	93.2	93.2	94.2	93.9	93.7
6.2	5.8	6.6	6.4	6.5	6.5	5.5	5.8	6.0
35	24	19	9		6	10	20	36

93.0	92.2
6.7	7.5
55	75

92.0	92.6
7.7	7.1
75	58

92.2	92.6	92.0	92.3	92.3	92.1	93.0	92.3	92.0
7.5	7.1	7.7	7.4	7.4	7.6	6.7	7.4	7.7
39	24	18	9		7	13	28	45

91.7	91.6	91.6
8.0	8.1	8.1
54	63	75

90.7	91.0
9.0	8.7
75	64

STA + π - ELEV.

999.74

60400

✓

+16 = $\neq$ ENTRANCE (LT.)

✓

+50

✓

LT

E

26 JAN. 1965

RT

68

90.8

91.2

91.0

91.2

91.2

91.0

91.0

90.4

89.7

8.9

8.5

8.7

8.5

8.5

8.7

8.7

9.3

10.0

41

26

17

8

9

18

34

54

90.6

90.7

89.1

9.1

9.0

10.6

59

75

75

90.4

90.5

90.4

90.7

90.6

90.4

91.0

90.4

90.0

9.3

9.2

9.3

9.0

9.1

9.3

8.7

9.3

9.7

38

20

16

6

9

13

24

37

90.4

90.4

89.5

89.1

9.3

9.3

11.2

10.6

61

75

75

59

89.2

89.3

89.0

89.3

89.3

89.0

89.9

89.4

89.8

10.5

10.4

10.7

10.4

10.4

10.7

10.8

10.3

9.9

30

21

14

7

5

9

12

17

89.0

88.9

88.8

87.8

88.5

89.4

89.1

10.7

10.8

10.9

11.9

11.2

10.3

10.6

50

66

75

75

57

41

31

STA + π - ELEV.

999.74

3.99 991.24 12.49 987.25

BM

5.71 991.21 5.71 985.53

(985.50)

61+00 = CONC. ENT. (LT.)

✓

+50

✓

62+00

✓

LT

E

26 JAN. 1965

RT

69

TOP PR & STA 61+00

SPIRE IN PP 28' 0" LT STA 62+00

87.46	87.22	87.0	87.2	87.2	87.1	87.2	86.8	86.1
3.75	3.99	4.2	4.0	4.0	4.1	4.0	4.4	5.1
31	17	16	6		9	16	27	47
Conc.	Conc.							

87.59	87.15	87.88	87.83		85.3	85.6
3.62	3.46	3.33	3.38		5.9	5.6
46	64	75	117		75	60
Conc.	Conc.	Conc.	Conc.			

85.8	85.7	85.3	85.4	85.5	85.4	84.7	84.0	83.5
5.4	5.5	5.9	5.8	5.7	5.8	6.5	7.2	7.7
28	20	15	5		8	14	24	39
				Approx GA				

86.1	87.0	87.6	87.8		84.2	83.6	82.6
5.1	4.2	3.6	3.4		7.0	7.6	8.6
40	49	68	96		75	63	56
			110				

84.9	84.5	84.0	84.0	84.0	84.0	83.8	83.2	82.1	81.3	81.0
6.3	6.7	7.2	7.2	7.2	7.2	7.4	8.0	9.1	9.9	10.2
25	20	14	9	5		8	14	24	36	43
85.2	85.6	85.9					82.5	81.5		
6.0	5.6	5.3					8.7	9.7		
40	52	75					75	57		

STA	+	π	-	ELEV.
-----	---	-------	---	-------

STA	+	π	-	ELEV.
-----	---	-------	---	-------

991.21

STA	+	π	-	ELEV.
-----	---	-------	---	-------

62+50

STA	+	π	-	ELEV.
-----	---	-------	---	-------

✓

STA	+	π	-	ELEV.
-----	---	-------	---	-------

63+00

STA	+	π	-	ELEV.
-----	---	-------	---	-------

✓

STA	+	π	-	ELEV.
-----	---	-------	---	-------

TP 0.69 980.84 11.06 980.15

26 JAN. 1965

70

LT

RT

83.7	83.3	82.2	82.3	82.4	82.3	81.9	80.7	80.3
7.5	7.9	9.0	8.9	8.8	8.9	9.3	10.5	10.9
38	19	14	6		8	12	21	45

83.5	83.9
7.7	7.8
58	75

80.8
10.4
75

81.5	81.5	80.0	80.1	80.1	80.1	80.0	80.5	79.1
9.7	9.7	11.2	11.1	11.1	11.1	11.2	10.7	12.1
39	18	13	6		9	14	18	34

81.4	81.0
9.8	10.2
59	75

79.2	79.2
12.0	12.0
75	58

TOP PK $\pm$ STA 63400

STA

+

π

-

ELEV.

980.84

63+50

✓

64+00

✓

+50

✓

LT

E

26 JAN. 1965

71

RT

178.4	177.9	177.2	177.4	177.4	177.2	177.2	177.1	176.0
2.4	2.9	3.6	3.4	3.4	3.6	3.6	3.7	4.8
28	18	12	3		10	14	23	36

178.1	178.1
2.7	2.7
47	75

176.8	176.3	175.8	175.0	175.6
40	45	50	58	52
75	67	56	52	48

175.7	175.6	175.4	174.5	174.5	174.3	174.0	173.4	172.6
5.1	5.2	5.4	6.3	6.3	6.5	6.8	7.4	8.2
52	35	17	9		10	16	28	42

176.1
4.7
75

173.3	172.9
7.5	7.9
75	56

172.4	173.1	172.9	171.5	171.5	171.5	171.4	171.3	171.1
8.4	7.7	8.4	9.3	9.3	9.3	9.4	9.5	9.8
43	28	16	9		12	16	24	36

172.7	172.8
8.1	8.0
69	75

171.9	171.4	171.5
9.4	9.4	9.3
75	63	49

FE

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		980.84		
--	--	--------	--	--

64+75				
-------	--	--	--	--

✓				
---	--	--	--	--

65+00				
-------	--	--	--	--

✓				
---	--	--	--	--

BM	1.15	973.55	8.43	972.41	972.40
----	------	--------	------	--------	--------

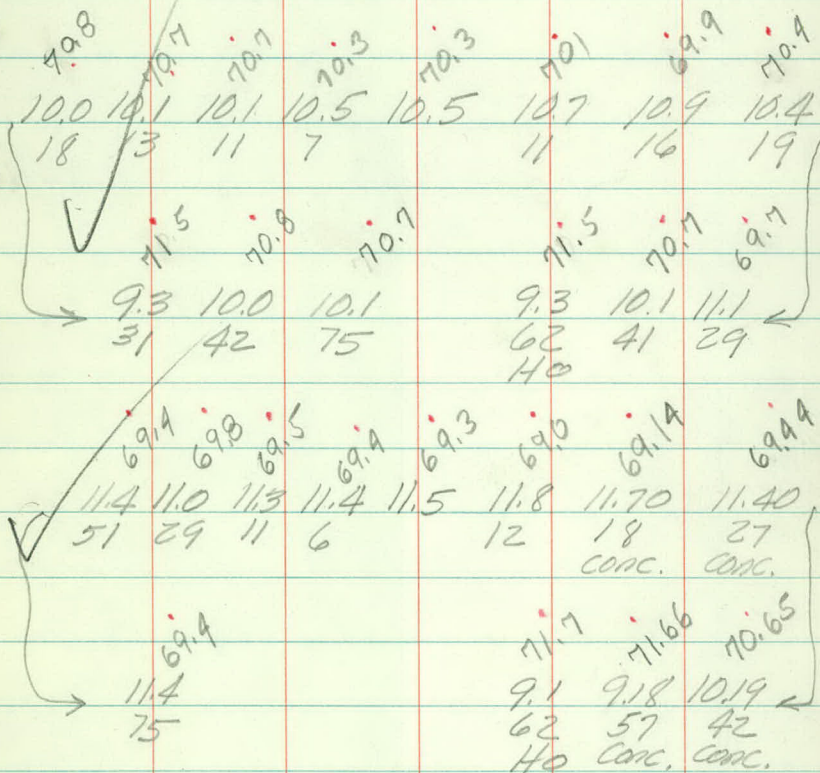
26 JAN. 1965

72

LT

E

RT



TOP N.W. COR LOWER STEP HO# 366
McKNIGHT RD.

STA + π - ELEV.

973.55

65+38

✓

+46 = DITCH LT.

✓

+56 = SHOULDER LT. & RT.

✓

26 JAN. 1965

73

LT

~~E~~

RT

68.2	67.5	67.8	68.1	67.9	67.6	67.9	68.9
5.4	6.1	5.8	5.5	5.7	6.0	5.7	5.2
20	15	9		14	23	32	43

68.3	68.0	68.2
5.3	5.6	5.4
35	47	75

68.8	68.1
4.8	5.2
75	54

66.3	66.6	67.2	67.2	67.5	67.9	67.8	67.9	67.7	67.9
7.3	7.0	6.4	6.4	6.1	5.7	5.8	6.2	5.9	5.7
75	52	29	21	13		13	29	39	59

68.1
5.5
75

67.0	67.1	67.1	67.9	67.7	67.6	67.3	67.3	67.5
6.6	6.5	6.5	6.2	5.9	6.0	6.3	6.3	6.1
75	56	33	14		14	29	49	75

66.9
6.7
100

67.7
5.9
100

STA + π - ELEV.

973.55

65+65 = ~~E~~ LONDIN LANE

BM

10.20 963.35 963.35

FROM STATION 0+00 TO
STATION 4+85 SEE PLAN
SURVEY BOOK #3 / DRAWER #9
PAGES 24 TO 32. DATED 2-16-61.

26 JAN. 1965

74

LT

E

RT

66.6	66.8	67.0	67.2	67.3	67.3	67.3	67.4	67.4
7.0	6.8	6.6	6.4	6.3	6.3	6.3	6.2	6.2
100	75	50	25	25	50	75	100	
66.5	66.4	66.4	66.4		66.1	67.1	67.5	67.5
7.1	7.2	7.2	7.2	5.5	5.9	6.1	6.1	
125	150	175	200	200	175	150	125	

NAIL IN 2" CE 22.0 RT STA 1+00

STA + π - ELEV.

BM 5.75 934.13

928.38

5+00

✓

+20

✓

BM 0.60 928.98 5.76 928.37 928.38

+60

~

RD
DS
PK
W/M

LT

27 JAN. 1965
Choudry 5° RT

75

SPIKE IN 6" COTT. 26'0 RT STA 5+30

20.3	20.3	21.1	21.6	20.7	21.2	30.1	31.0
13.8	13.8	13.0	12.5	13.4	4.9	4.0	3.1
47	36	20	10		20	34	49
							FE

20.3	22.9	22.6	32.1	31.3
13.8	11.2	11.5	1.7	2.8
52	61	75	75	59

21.4	23.8	24.0	25.6	29.1	28.9	29.1	29.8	30.6
12.7	10.3	10.1	8.5	5.0	5.2	5.0	4.3	3.5
51	42	26	8		20	36	56	75
						FE		

22.4	19.9	17.2
11.7	14.2	16.9
55	65	75

SPIKE IN 6" COTT 26'0 RT STA 5+30

24.6	24.7	24.3	24.7	25.4	26.0	26.2	25.9	26.3	27.0	27.3
4.4	4.3	4.7	4.3	3.6	3.0	2.8	3.1	2.7	2.0	1.7
75	51	45	28	12		8	20	41	60	75

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		928.98		
--	--	--------	--	--

6+00				
------	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

BM	3.04	918.70	13.35	915.63	915.66
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7+00				
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LT

E

27 JAN. 1965

76

Rt.

23.0	22.4	22.3	22.5	21.1	21.9	21.4	20.4	22.9
6.0	6.6	6.7	6.5	7.3	7.6	7.6	8.6	6.1
51	49	35	15		5	13	16-18	24
					FE		DITCH	

22.6	22.4
6.4	6.6
66	75

24.1	23.5	23.5
4.9	5.5	5.5
75	54	39

18.2	18.8	18.4	16.6	16.4	16.3	17.1	16.8	17.4
10.8	10.2	10.6	12.4	12.6	12.7	11.9	12.2	11.6
37	20	6	2		3	17	24	36
					FE			

17.9	15.7	14.5
11.1	13.3	14.5
46	53	75

19.9	19.7	16.2
9.1	9.3	12.8
75	64	47-53
		DITCH

SPIKE IN 5" POPLAR 22.0 Rt STA 6+85.

05.4	06.7	08.0	15.4	16.1	16.4	11.6	10.8	11.0	11.8	11.9	13.4	16.5	17.4
13.3	12.0	10.7	3.3	2.6	2.3	7.1	7.9	7.7	6.9	6.8	5.3	2.2	1.3
T5	56	52	41	26	11	3		3	17	29	45	64	75
								FE					

STA

+

K

-

ELEV.

918.70

7+50

✓

8+00

✓

+50

✓

LT

27 JAN. 1965 77

RT

04.6	13.4	14.8	12.1	11.2	11.0	10.2	10.1	12.7
14.1	5.3	3.9	6.6	7.5	7.7	8.5	8.6	6.0
56	42	13	6	2	FE	7	24	39

03.0
15.7
75

17.4
15.6
1.3
3.1
75
58

11.5	13.0	13.2	10.0	09.3	09.4	08.9	10.6	14.3
7.2	5.7	5.5	8.7	9.4	9.3	9.8	8.1	4.4
43	22	11	4	2	FE	15	28	47

00.8
17.9
59

00.3
18.4
75

19.0
18.1
10.3
0.6
75
67

08.5	09.9	10.8	11.3	09.9	09.5	09.5	08.7	10.7	13.3
10.2	8.8	7.9	7.4	8.8	9.2	9.2	10.0	8.0	5.4
70	45	27	12	2	2	FE	15	30	45

05.3
13.4
75

19.3
18.7
17.3
10.6
0.0
1.4
75
69
59

STA + π - ELEV.

918.70

9+00

✓

BM 12.06 923.91 6.83 911.87 (911.85)

9+35

✓

LT

E

27 JAN. 1965

78

RT

08.6	09.0	09.6	09.6	09.6	09.6	09.5	09.8	13.9
10.1	9.7	9.1	9.1	9.1	9.1	9.2	8.9	5.3
62	40	20	8		1	11	24	41
					FE			

08.1
10.6
75

20.7 18.7 17.5
+2.0 0.0 1.2
75 60 56

TOP HYDRANT N.W. COR MCKNIGHT RD &
LOWER AFTON RD.

07.2	08.4	09.3	09.3	09.0	09.3	11.1	14.8
16.7	15.5	14.6	14.6	14.9	14.6	12.8	9.1
75	57	32	13	FE	11	29	44

22.4 18.7
1.5 5.2
75 60

STA + K - ELEV

923.91

9+60 = DITCH LT & RT

+79 = SHOULDER LT & RT

10+00 = ~~E~~ LOWER AFTON RD

BM

11.15

923.00

12.06

911.85

(911.85)

LT

270 AM. 1965
RT

79

07.3	07.4	07.6	08.0	08.1	08.5	08.9	09.4
16.6	16.5	16.3	15.9	15.8	15.4	15.0	14.5
55	43	24	12		15	36	57

06.9
17.0
75

09.7
14.2
75

10.4	10.5	10.6	10.8	11.1	11.2	11.4	11.7
13.5	13.4	13.3	13.1	12.8	12.7	12.5	12.2
75	61	47	26		22	47	65

11.8
12.1
75

09.6	10.2	10.6	10.9	11.0	11.3	11.6	11.8	12.2	12.7
14.3	13.7	13.3	13.0	12.9	12.6	12.3	12.1	11.7	11.2
125	100	75	50	25		25	30	75	100

09.0 08.3 07.4
14.9 15.6 16.5
150 175 200

15.9 15.0 14.2 13.3
8.0 8.9 9.7 10.6
200 175 150 125

TOP HYDRANT N.W. COR MCKNIGHT & LOWER AFTON RD.

STA	+	T.	-	ELEV.
		923.00		

10+25 = SHOULDER LT & RT

10+33 see additions.

+38 = DITCH RT

✓

+75

✓

LT

27 JAN 1965
E

RT

80

10.5	10.7	10.6	10.5	10.6	10.7	11.1
12.5	12.3	12.4	12.5	12.4	12.3	11.9
63	37	13		15	35	57

10.2
12.8
75

11.5
11.5
75

08.2	08.7	08.8	08.8	09.5	10.1	10.6
14.8	14.3	14.2	14.2	13.5	12.9	12.4
56	34	15		24	47	67

08.2
14.8
75

10.8
12.2
75

04.1	05.3	07.1	07.8	08.3	09.0	10.1	15.5
18.9	17.7	15.9	15.2	14.7	14.0	12.9	7.5
75	57	37	15		14	24	43

22.2
19.3
0.8 3.7
75 59

STA	+	π	-	ELEV.
-----	---	---	---	-------

		923.00		
--	--	--------	--	--

11+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+27				
-----	--	--	--	--

✓				
---	--	--	--	--

+43				
-----	--	--	--	--

✓				
---	--	--	--	--

BM				
----	--	--	--	--

	11.16			
--	-------	--	--	--

		911.84		
--	--	--------	--	--

			911.85	
--	--	--	--------	--

LT

27 JAN. 1965 81

RT

03.7	04.4	05.9	07.0	07.7	08.5	10.6	12.2
19.3	18.6	17.1	16.0	15.3	14.5	12.4	10.8
63	48	31	14		13	26	34

02.5
20.5
75

23.0 20.4 15.6
0.0 2.6 7.4
75 63 45

07.1	07.1	08.6	11.9
15.9	15.3	14.4	11.1
	15	27	40

21.7 16.5
1.3 6.5
75 56

03.7	06.3	06.8	09.3
19.3	17.7	16.2	13.7
	10	23	37

18.6 15.3 13.1
4.4 7.7 9.9
75 64 55

TOP HYDRANT N.W. COR. MCKNIGHT & LOWER AFTON RD S

STA	+	π	-	ELEV.
BM	1.17	913.02		911.85

11+27

TP	2.93	906.95	9.00	904.02
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+43

+67

✓

+84

South bank

KG
DS
PK
LPD

LT

E

Feb 10, 1965
Fair RT

82

Top Hyd. NW Cor Lower Alton & McKnight

00.5	00.5	02.4	04.5	05.1	07.1	✓
12.5	12.5	10.6	8.5	7.3	5.9	
75	55	35	24	11		

spike in ground.

97.0	06.9	00.5	02.1	04.0
10.0	10.1	6.5	4.9	3.0
75	64	52	17	

creek
bottom

896.0	897.1	897.6	898.3	901.5	902.6	903.2	904.6	906.3	905.4	912.5
11.0	9.9	9.4	8.7	5.5	4.4	3.8	2.4	0.7	1.6	+6.0
71	68	54	26	11		6	14	20	36	64

inv
creek

915.0
+8.0
75

898.0	895.5	895.5	896.6	898.2	898.3	899.3	901.1	904.8	906.5	903.5
9.0	11.5	11.5	10.4	8.8	8.7	8.2	7.7	5.9	2.2	+3.5
75	70	62	59	43	22	4	12	25	42	41

inv

inv

01.0
+6.0
75

STA	+	T	-	ELEV.
-----	---	---	---	-------

		906.95		
--	--	--------	--	--

11+94	E creek West			
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TP	10.66	913.14	4.47	902.48
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BM			1.29	911.85
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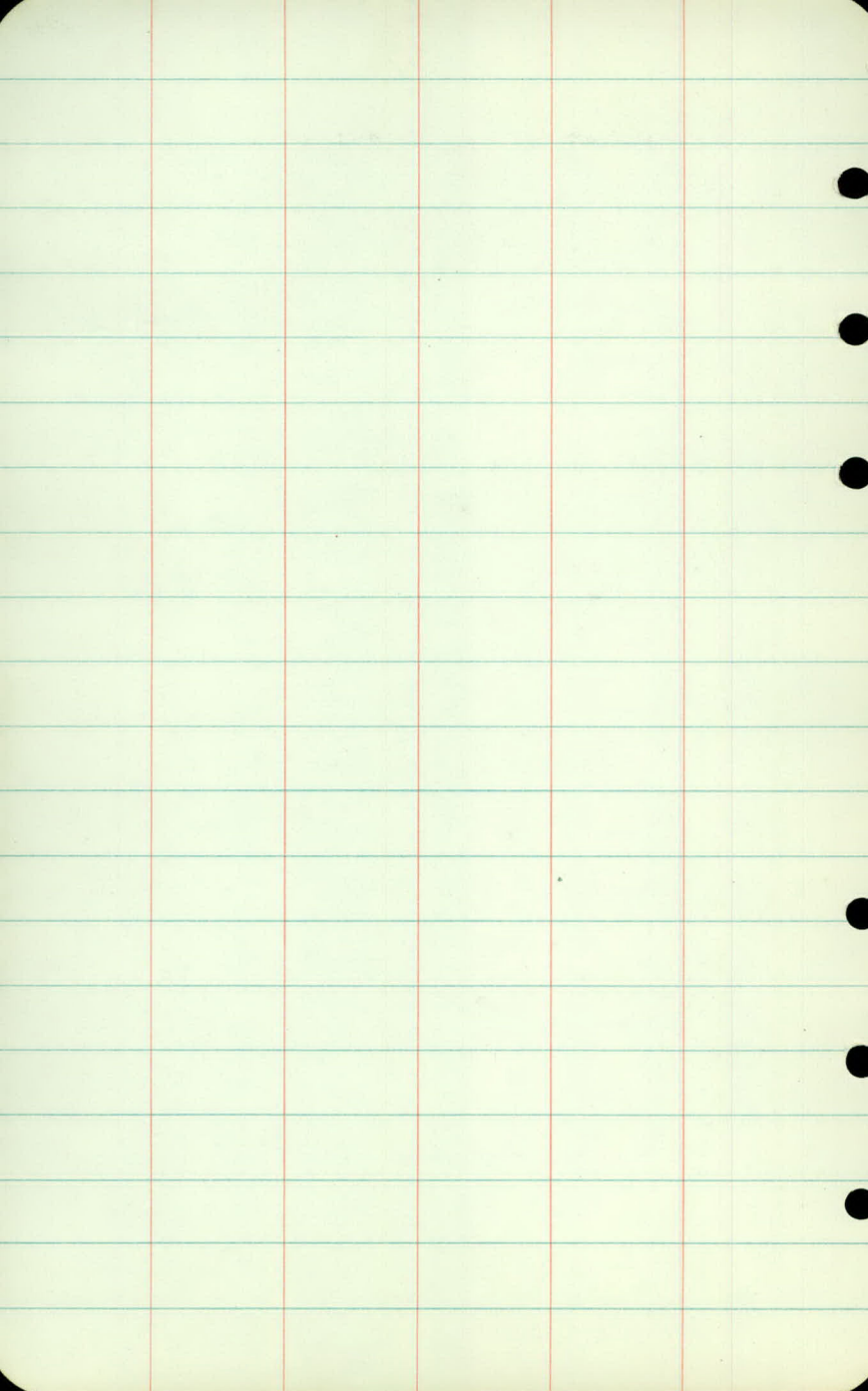
911.85

Feb 10, 1965 83

895.1	895.8	896.0	897.6	898.9	901.4	905.0
11.6	11.2	11.0	9.4	8.1	5.6	2.0
75	52	31		14	21	37
inv.	inv.	inv.	inv.			
Creek						

Top fc post

Top Hyd. L.A. Rd & McKnight



R6
DS
PK
LPD

Feb 10, 1965
Fair, Windy 84

Additional X-Sections

M = Knight Rd

sta 19+50 to sta

Sta	+	π	-	E/V
BM	12.71	941.32		928.61

19+50

20+00

+35

+60

21+00

+50

Feb 10, 1965 85

Lt

E

Rt

Spike & Sta 19+00

936.0	932.9	931.6	929.3	928.1	927.7	926.2	925.4	926.3	927.1	928.2
5.3	8.4	9.7	12.0	13.2	13.6	15.1	15.9	15.0	14.2	13.1
100	75	62	41	19	✓	13	28	42	65	75

931.0	930.0	928.9	928.3	927.6	927.1	926.6	926.6	927.8
10.3	11.3	12.4	13.0	13.7	14.2	14.7	14.7	13.5
100	75	50	25	✓	14	25	50	75

931.6	931.3	931.0	930.7	929.9	928.9	927.8	927.6	927.6
9.7	10.0	10.3	10.6	11.4	12.4	13.5	13.7	13.7
100	69	47	27	✓	11	26	50	75

933.2	932.7	932.3	935.4	934.6	933.6	933.0	930.5	929.4	928.5	928.3
8.1	8.6	9.0	5.9	6.7	7.7	8.3	10.8	11.9	12.8	13.0
100	75	55	50	37	18	✓	15	25	50	75

934.0	932.6	933.7	937.0	936.5	935.3	934.9	932.2	930.8
7.3	8.7	7.6	4.3	4.8	5.4	6.4	9.1	10.5
100	76	54	50	23	✓	26	51	80

933.7	932.3	937.1	937.3	936.4	935.7	933.8	932.7
7.6	8.5	9.0	4.2	4.0	4.9	5.6	7.5
100	68	55	50	22	✓	26	52

Sta + π - E/V

941.32

22+00

+25

BM 2.85 942.64⁶³ 1.53 939.79 939.78 ✓

+61

+61

23+00

✓

Feb 10, 1965

86

L+

L

R+

933.9	933.5	937.6	937.0	937.0	936.5	935.6	934.7	932.9	932.4	932.0
7.4	7.8	3.7	4.3	4.3	4.8	5.2	6.6	8.4	8.9	9.3
55	55	50	39	20	11	✓	21	27	60	75
75										

934.2	934.4	935.0	934.3	934.5	933.5	932.6	932.3	931.9
7.1	6.9	6.3	7.0	6.8	7.8	8.7	9.0	9.4
82	56	48	19	✓	20	35	50	75

Spike in 16" Oak 40' Rt sta 23+60

 RG
 DS
 PK
 LPD
Feb. 11, 1965
cloudy 5°

934.3	934.3	934.6	932.9	932.7	932.2	933.6	933.3	933.0	933.7
8.3	8.3	8.0	9.7	7.9	10.4	9.0	9.3	9.6	8.9
75	58	48	34	24	10	✓	24	45	75

934.9	933.6	933.0	932.6	932.7	933.6	934.4	934.6	936.1	938.1
7.7	9.0	9.6	10.0	9.9	9.0	8.2	8.0	6.5	4.5
48	37	26	20	6	✓	13	34	55	75

934.7	935.1
7.9	7.5
52	75

Sta + π - EIV

942.⁶³64

+28

+50

+71

24+00

TP 7.54 937.^{.11}12 13.06 929.⁵⁷58

+10

+50

Feb 11, 1965
Snow 50 87
RT

935.5 935.0 937.3 935.7 935.2 936.0 935.9 936.6 937.6 938.4 940.2
7.1 7.0 5.3 6.9 7.4 6.6 6.7 6.0 5.0 4.2 2.4
75 50 46 29 10 12 15 30 50 75
Fe

35.2 936.5 938.9 938.3 937.8 938.5 938.1 937.7 939.4 938.9 937.2
7.4 6.1 3.7 4.3 4.8 4.1 4.5 4.9 3.2 3.7 5.4
75 49 43 29 15 4 11 19 44 75

935.0 936.0 937.0 939.8 936.7 938.1 937.3 936.3 937.3 937.3 936.6 933.3 932.0
7.6 6.6 5.6 2.8 3.9 4.5 5.3 6.3 5.3 5.3 6.0 9.3 10.6
75 61 47 41 19 3 3 13 21 39 62 75

934.4 935.3 939.1 939.1 937.5 935.1 933.7 932.9 933.2 931.7 928.3 926.2
8.2 7.3 3.5 3.5 5.1 7.5 8.9 9.7 9.4 10.9 4.3 16.4
75 47 41 33 16 5 4 15 25 47 75

Rock

934.3 934.4 936.1 934.9 934.7 933.4 931.9 932.0 929.1 928.3 926.4 925.7
2.8 2.7 1.0 2.2 2.4 3.7 5.2 5.1 8.0 8.8 10.7 11.4
75 51 44 19 7 6 14 27 38 48 75

933.7 933.5 933.4 934.9 934.7 932.8 931.9 929.9 929.5 926.3 924.9 924.9
3.4 3.6 3.7 2.2 2.4 4.3 5.2 7.2 7.6 10.8 12.2 12.2
75 68 45 42 22 10 6 21 33 53 75

Sta	+	π	-	E/V
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937.12¹¹

BM

5.89

931.23²²

931.22 ✓

BM

4.85

936.07

931.22

25+00

+50

+75

26+00

BM

3.01

934.23

4.05

931.22³

931.22

+50

RG
DS
PK
PLD

Lt

Rt

Feb 15, 1965
Clear 15°
Rt.

88

SE Cor. Ent. Slab 55' Lt Sta 25+90

" " " "

932.9	932.2	931.4	930.6	928.9	928.1	926.4	925.0	924.9
3.2	3.7	4.7	5.5	7.2	8.0	9.7	11.1	11.2
75	47	22	11	✓	14	34	50	75

932.6	932.4	930.1	928.6	927.7	926.7	926.5	925.5	925.4	924.9
3.3	3.7	6.0	7.5	8.4	9.4	9.6	10.6	10.7	11.2
75	56	32	18	✓	11	23	27	50	75

931.3	930.3	929.3	928.2	927.7	926.9	926.4	925.3	925.1	924.9
4.8	5.8	6.8	7.9	8.4	9.2	9.7	10.8	11.0	11.2
75	51	36	21	✓	4	15	25	48	75

931.2	931.2	930.3	928.7	928.0	927.7	926.8	925.7	925.2	924.9
4.86	4.88	5.8	7.4	8.1	8.4	9.3	10.4	10.9	11.2
59	55	40	27	14	✓	15	25	48	75
Gar	conc	slab							

SE Cor Ent Slab 55' Lt Sta 25+90

932.1	931.4	929.9	928.2	928.3	928.5	928.6	927.5	926.4	925.3	924.9	924.9
2.1	2.8	4.3	5.0	5.9	5.7	5.6	6.7	7.8	8.9	9.3	9.3
75	59	45	32	10	✓	14	22	35	41	58	75

Hwy
House

Sta	+	π	-	EIV
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934.23

27+00

+09

4.08 30.15

+21

Gutter Lt.

+36

E Edgebrook Ave.

+51

Gutter Lt

+65

3.78 30.45

28+00

TBM

8.35 940.68 1.90 932.33

Feb 15, 1965

89

LT

E

RT

31.3	31.1	29.9	29.2	29.7	30.0	29.4	27.8	25.8	25.6
2.9	3.1	4.3	5.0	4.5	4.2	4.8	6.4	8.4	8.6
75	58	37	12	✓	17	24	37	48	75

E edge sidewalk LT 51'

29.6	29.7	29.8	29.6	30.1	30.1	29.3	27.0	26.7
4.6	4.5	4.4	4.6	4.1	4.1	4.9	7.2	7.5
75	52	33	14	✓	19	30	43	75

28.7	29.1	29.4	29.8	30.0	29.9	30.3	30.5	30.4	29.7	27.6	27.4	27.4
5.5	5.1	4.8	4.4	4.2	4.3	3.9	3.7	3.8	4.5	6.6	6.8	6.8
200	150	100	63	37	16	✓	15	27	39	44	62	75

29.8	29.9	30.1	30.2	30.6	30.6	29.9	28.1	27.8	27.3
4.4	4.3	4.1	4.0	3.6	3.6	4.3	6.1	6.4	6.9
75	67	42	16	✓	18	35	43	58	75

S. cut
drive
Ent

E. edge sidewalk LT 51'

31.0	31.4	31.8	31.7	31.8	31.8	32.1	31.1	30.3	29.6	29.3	29.1
3.24	2.8	2.4	2.5	2.4	2.4	2.1	3.1	3.9	4.6	4.9	5.1
72	68	40	34	11	✓	20	29	42	51	62	75

& Conc
drive

Top Hyd NW cor Edgebrook & M^c Knight,

Sta + π - EIV

940.68

28+50

29+00

+50

✓

BM 11.61 947.09 5.20 935.48 (935.48)

+83

✓

Feb 15, 1965 90

Lt

Rt

Rt

36.9	35.6	34.0	33.9	33.6	34.3	33.3	32.9	33.7	34.2	34.7	35.2
3.8	5.1	6.7	6.8	7.1	6.4	7.4	7.8	7.0	6.5	6.0	5.5
75	59	40	34	16	✓	23	34	39	45	56	75

37.0	36.7	36.2	35.9	36.2	35.4	34.9	34.6	36.9	37.1	38.6
3.7	4.0	4.5	4.8	4.5	5.3	5.8	6.1	3.8	2.8	2.1
75	60	39	17	10	✓	12	35	53	67	75

Fe

38.4	38.7	38.1	38.8	38.3	39.1	40.3	39.6	37.5	36.9	37.0	37.7	39.3	40.5
2.3	1.9	2.0	1.9	2.4	1.6	0.4	1.1	3.2	3.8	3.7	3.0	1.4	10.2
51	51	44	38	18	13	5	✓	14	22	35	45	58	75

SW S.W. Beg
S.W. Unit
(2')

38.3	37.7	37.8
2.4	3.0	2.9
68	68	80
SW	SW	SW

Spike in PP 43' Lt sta 28+88

44.0	40.5	40.2	39.8	40.2	41.7	41.7	40.6	40.2	39.6	38.6	41.0	39.7
3.1	6.6	6.9	7.3	6.9	5.4	5.4	6.5	6.9	7.5	8.5	6.1	7.4
56	50	35	20	15	7	✓	4	10	17	23	33	44
Top	Bot											
step	steps											

44.1

3.0
75
SW

43.9

3.2
75

43.2

3.9
62

Sta	+	π	-	E/V
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		947.09		
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30+00				
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+09			5.08	42.01
-----	--	--	------	-------

+21	Gutter Lt			
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TBM	5.40	950.47	2.02	945.07
-----	------	--------	------	--------

+37	R Dellridge Ave.			
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+53	Gutter Lt			
-----	-----------	--	--	--

TBM	6.20	951.27	5.40	945.07
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+65			8.74	42.53
-----	--	--	------	-------

+67				
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Feb 15, 1964

91

LT

E

RT

43.1	42.2	41.2	40.6	40.6	42.6	42.2	40.8	41.0	42.8	43.9	45.0
9.0	4.9	5.9	6.5	6.5	4.5	4.9	6.3	6.1	4.3	3.2	2.1
75	51	38	20	15	8	9	25	37	51	71	shed

East edge S.W. Lt 50'

42.4	42.3	41.8	41.3	43.2	43.6	42.9	42.2	42.9	44.1	44.6	45.9	47.1
4.7	4.8	5.3	5.8	3.9	3.5	4.2	4.9	4.2	3.0	2.5	1.2	0.0
75	64	42	19	10	5	5	13	21	41	56	74	shed

Top Hyd. NE cor Dellridge & McKnight

43.1	43.0	42.7	42.1	41.9	42.4	44.6	44.7	43.8	44.0	44.8	46.0	46.7	46.7	47.8
7.7	7.4	7.5	7.8	8.4	8.6	8.1	5.9	5.8	6.7	6.5	6.7	4.5	3.8	3.8
200	150	100	75	39	19	15	5	6	9	15	30	46	58	75

Barn

42.6	42.5	42.5	42.2	43.0	45.0	45.1	45.6	46.0	46.3	47.1	48.0
7.9	8.0	8.0	8.3	7.5	5.5	5.4	4.9	4.5	4.2	3.4	2.5
75	62	42	19	14	5	7	21	38	58	75	Barn

Top Hyd NE cor Dellridge & McKnight

RG
DS
PK
LPDFeb 16, 1965
Clear 0° Windy

E. edge S.W. Lt 50'

43.4	43.1	42.7	42.6	43.3	45.5	45.8	46.6	47.4	48.6
7.9	8.2	8.6	8.7	8.0	5.8	5.5	4.7	3.9	2.7
75	58	40	18	13	5	23	45	72	Bldg

Sta	+	π	-	E/V
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		951.27		
--	--	--------	--	--

30+89				
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31+00				
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+50				
-----	--	--	--	--

32+00				
-------	--	--	--	--

+50				
-----	--	--	--	--

TP	2.98	950.66	3.59	947.68
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+80				
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Sta

+

T

-

E/V

950.66

33+00

+09

8.44

42.22

+22

Gutter Lt.

+37

E Cardinal Place

+53

Gutter Lt

+65

9.74

40.92

+68

34+00

Lt

E

Rt

43.5	42.9	42.8	42.4	42.3	43.5	46.1	47.3	47.6	47.7	47.9
7.2	7.0	7.9	8.3	8.4	7.2	4.6	3.4	3.1	3.0	2.8
75	66	58	42	22	14	5	✓	31	50	75
Conc		Conc								

East edge sidewalk Lt 51'

42.5	41.7	41.8	41.7	43.7	46.8	47.8	47.8	47.8	48.0
8.2	9.0	8.9	9.0	7.0	3.9	2.9	2.9	2.9	2.7
75	61	48	21	11	4	✓	23	46	75
Ent.									

44.1	43.3	42.2	41.6	41.2	41.4	43.0	45.7	47.8	48.5	47.8	47.9	48.0
6.6	7.4	8.5	9.2	9.5	9.3	7.7	5.0	2.9	2.2	2.9	2.8	2.7
200	150	100	54	33	19	12	5	✓	12	26	50	75
				McKnight								

41.6	41.1	40.7	40.6	41.1	43.3	47.0	48.4	47.9	47.9	47.9
9.2	9.6	10.0	10.1	9.6	7.4	2.7	2.3	2.8	2.8	2.8
75	65	49	32	18	5	✓	15	25	48	75
				McK						

East edge sidewalk Lt 51'

41.9	41.1	40.1	40.1	40.8	43.9	47.1	48.6	47.7	47.9	47.8
8.8	9.6	10.6	10.6	9.9	6.8	3.6	2.1	3.0	2.8	2.9
75	51	42	20	15	3	✓	14	27	56	75

42.2	41.6	40.9	38.9	36.4	41.1	43.2	47.4	47.6	48.0	47.8	47.3
8.5	9.1	9.8	11.8	12.1	9.6	7.5	3.3	3.1	2.7	2.9	3.4
75	66	55	36	20	12	3	1	✓	27	53	75
S.W.		HO									

Sta + π - E/V

950.66

BM 6.40 946.85 10.21 940.45 940.45

34+30

+50

35+00

+50

TP 1.20 937.25 10.80 936.05

+82

✓

Feb 16, 1965

94

Lt

F

Rt

Spike in Arc Lt Pole 47' Lt sta 33+63

RG
DS
PK
LPD

Feb 17, 1965

Fair 200

38.6	38.2	37.9	37.6	39.3	42.0	46.8	45.9	45.8	46.8
8.32	8.74	9.0	9.3	7.6	9.9	0.1	+1.0	+1.1	-0.1
75	51	45	19	12	5	✓	15	48	75
S.W.	S.W.								

37.8	37.5	37.0	36.9	38.3	41.3	46.0	45.2	46.1	45.7
9.1	9.4	9.9	10.0	8.6	5.6	0.9	41.7	0.8	1.2
75	65	44	19	12	5	✓	17	50	75

35.7	34.8	34.5	34.2	36.4	39.2	42.6	43.4	41.7	40.1	39.4
11.2	12.1	12.4	12.7	10.5	7.7	4.3	3.5	5.2	6.8	7.5
75	51	43	19	9	3	✓	14	35	61	75
	Fe									

32.2	32.1	31.6	30.9	31.5	33.3	38.3	38.5	38.3	36.1	33.3	32.7
13.7	14.8	15.3	16.0	15.4	13.6	8.6	8.4	8.6	11.8	13.6	14.2
57	52	43	19	9	4	3	✓	15	35	56	75
Ho	Fe										

Nail in PP 47' Lt Sta 34+87

29.8	29.6	28.9	29.1	31.6	35.2	36.5	34.9	31.6	30.5	28.2	27.4
7.5	7.7	8.4	8.2	5.7	2.1	1.8	2.4	5.7	6.8	9.1	9.9
51	41	16	10	5	3	✓	13	26	37	57	75

29.2

Shos

60

Cone

29.3

8.02

75

Cone

Sta

+

π

-

E/V

937.25

36+00

BM

3.96

931.31

9.92

927.33

927.35

+09

3.07

28.24

+21

Gutter Lt.

+36

E Berland Place

+52

Gutter Lt

+64

5.65

25.66

+70

✓

RG M
DS
PK
LPO

Feb 17, 1965
Fair 20°

95

LT

LT

RT

27.9	28.7	29.2	28.5	28.1	30.3	32.3	32.1	31.1	27.6	25.3	24.0
8.36	8.54	8.1	8.8	9.2	7.0	5.9	4.2	6.2	9.7	12.0	13.3
75	59	51	39	16	3	✓	11	18	38	59	75
Conc	Conc										

Spike in Arc Lt. Pole 47' Lt Sta 36+14

East edge sidewalk Lt. 52'

26.0	27.4	27.0	26.6	27.3	28.0	29.9	30.9	30.6	27.7	25.0	23.4	21.7
3.3	3.9	4.3	4.7	4.0	3.3	1.4	0.4	0.7	3.6	6.3	7.9	9.6
75	63	39	16	11	5	2	✓	12	21	34	57	75
Ent												

31.5	28.8	27.2	26.2	25.8	26.4	27.6	29.5	29.7	28.4	25.9	24.0	21.7	20.7
8.0	2.5	4.1	5.1	5.5	4.9	3.7	1.8	1.6	2.9	5.4	7.3	9.6	10.6
145	100	68	37	15	11	4	2	✓	14	19	34	56	75

27.1	26.5	25.3	24.9	25.8	26.6	27.9	28.2	27.5	23.5	21.7	20.1	29.8
4.2	4.8	6.0	6.4	5.5	4.7	3.4	3.1	3.8	7.8	9.6	11.2	11.5
75	64	36	15	12	5	1	✓	14	27	43	67	75

East edge sidewalk Lt 51'

25.8	24.9	24.4	24.0	25.4	27.6	27.6	27.1	24.4	21.9	19.8	18.3
5.5	6.4	6.9	7.3	5.9	3.7	3.7	4.2	6.9	9.4	11.5	13.0
52	48	37	15	7	3		11	17	35	55	75

27.0	27.8
4.3	3.5
63	75

Sta	+	π	-	E/v
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		931.31		
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37+00				
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TP	3.02	927.56	6.77	924.54
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+08			4.91	
-----	--	--	------	--

+20			5.44	
-----	--	--	------	--

+12				
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+24				
-----	--	--	--	--

+60				
-----	--	--	--	--

38+00				
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Feb 17, 1965

96

Lt

E

Rt

29.9	29.9	28.0	25.7	23.4	23.0	22.9	24.9	25.0	24.3	22.6	21.4	19.5	17.1
1.4	1.4	3.3	5.6	7.9	8.3	8.4	6.4	6.3	7.0	8.7	9.9	11.8	14.2
75	72	63	46	50	36	14	4	✓	11	17	32	48	75
			40										

So. inv. 9" CM Lt 45'

No. inv. 9" CM Lt 45'

24.7	24.2	23.0	22.7	22.4	24.6	24.5	22.7	20.9	19.9	18.9	17.1
2.88	3.4	4.6	4.9	5.2	3.0	3.1	4.9	6.7	7.7	8.7	10.5
54	48	40	34	13	5	✓	11	19	39	53	75
Core	BT	BT									

24.2	24.2	21.1	22.4	22.2	22.0	24.0	23.8	22.9	21.2	19.9	18.7	16.8
3.4	3.4	3.5	5.2	5.4	5.6	3.6	3.8	4.7	6.4	7.7	8.9	10.8
75	54	49	43	34	12	4	✓	11	17	30	47	75
		40										

23.4	22.8	21.5	20.9	20.8	22.4	22.5	21.1	19.0	17.3	16.1	15.0
4.2	4.8	6.1	6.7	6.8	5.2	5.1	6.5	8.6	10.3	11.5	12.6
75	54	46	35	13	6	✓	9	18	41	60	75

23.2	21.9	19.8	19.3	19.2	20.3	20.1	19.9	17.9	16.4	14.1
4.4	5.7	7.8	8.3	8.4	7.3	7.5	7.7	9.7	11.2	13.5
75	57	44	35	12	3	✓	6	13	40	75

Sta + π - Elev

927.56

+46

✓

TP 3.69 921.14 10.11 917.45

+74

39+00

+08

4.11

+17

Feb 17, 1965 97

Lt E Rt

21.0	20.9	18.2	17.2	17.5	18.9	19.3	17.7	15.6	13.5	12.8	12.2		
6.60	6.73	9.4	10.4	10.1	8.7	9.3	9.9	12.0	14.1	14.8	15.4		
58	56	47	36	13	5	5	5	12	36	56	75		
Conc		Conc											
(2' slab)													

21.6	23.5	24.6
5.98	4.1	3.0
58	68	75
Conc.		
Top step		

Solarim M.H. 37' Lt 38+94

18.6	18.6	18.5	18.7	17.3	16.9	16.9	15.4	13.5	13.0	12.2
2.52	2.52	2.58	2.4	3.8	4.2	4.2	5.7	7.6	8.1	8.9
75	69	59	50	32	11	16	38	53	75	
Conc		Conc								

17.9	17.5	17.5	16.5	16.3	16.4	15.4	13.8	12.5	13.3
3.2	3.6	3.6	4.4	4.8	4.7	5.7	7.3	8.6	7.8
75	61	51	30	9	16	44	66	75	
Ent		Ent							

East edge sidewalk Lt 51'

17.0	16.7	16.9	16.1	15.7	16.0	15.4	13.9	13.0
4.1	4.4	4.2	5.0	5.4	5.1	5.7	7.2	8.1
75	62	50	31	10		17	45	75
Ent		Ent						

Sta + π - Elev

921.14

+26 Shoulder Lt & Rt

+43 E Upper Afton Rd

BM

4.46

916.68

916.67

Feb 17, 1965 98

LT

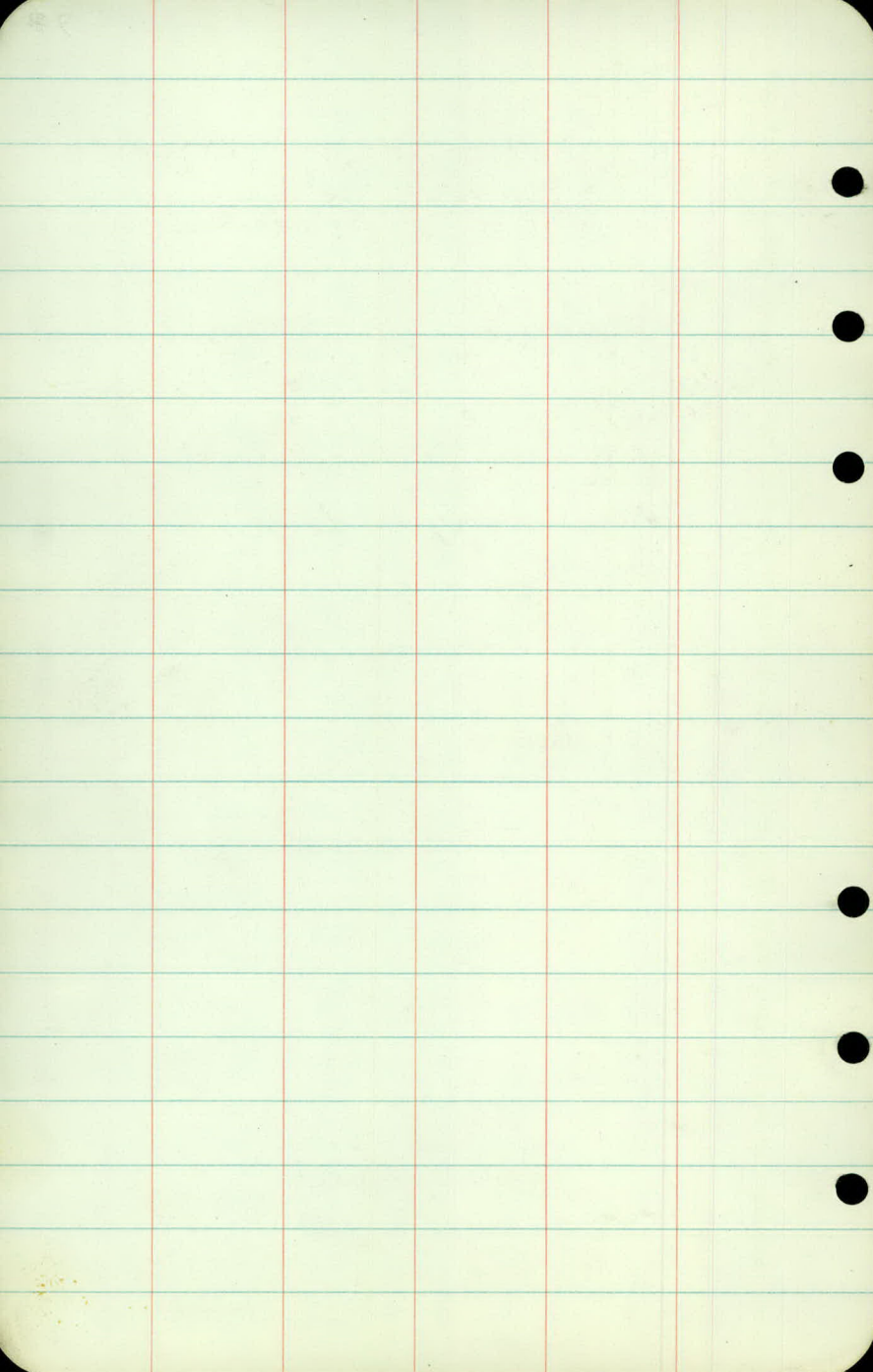
E

RT

16.9	16.3	16.0	15.9	16.0	15.6	15.2	14.9
4.2	4.8	5.1	5.2	5.1	5.5	5.9	6.2
100	75	41	22	✓	23	50	100

20.6	18.6	16.9	15.8	15.6	15.3	15.3	15.3	15.6	15.8
0.5	2.5	4.2	5.3	5.5	5.8	5.8	5.8	5.5	5.3
200	150	100	50		39	79	100	150	200

Spike in PP N.W. Cor. Upper Afton $\frac{1}{2}$ M² Knight



KP
DS
WM

3 MAY 1965
SUNNY 65°

99

MC-KNIGHT RD

MAILAND RD TO UPPER AFTON RD

ADDITIONAL X-SECTIONS

2 TOPO INFORMATION (see topo book)

STA	+	π	-	ELEV.
BM	3.34	920.00		916.66

39+17			12.24	
-------	--	--	-------	--

+22			4.23	915.77
-----	--	--	------	--------

+38			4.11	915.89
-----	--	--	------	--------

+45 = ∇ UPPER AFTON RD.

+62 = SHOULDER LINE RT.

+66			5.18	914.82
-----	--	--	------	--------

LT

£

3 MAY 1965

RT

100

SPIKE IN PP NW COR MCKNIGHT & UPPER AFTON RD

FL S. END 30" SCP 97.0 RT.

TOP CB 53.0 LT

TOP MH 52.0 LT

17.0	16.2	15.9	15.7	15.70	15.7	15.4	15.3	15.4	15.6
3.0	3.8	4.1	4.3	4.30	4.3	4.6	4.7	4.6	4.4
100	75	50	25	7		27	51	100	150

TOP MH

16.6	16.0	15.3	15.4	15.5	15.2	14.7	14.6	14.7
3.4	4.0	4.7	4.6	4.5	4.8	5.3	5.4	5.3
100	82	50	21		22	42	70	100

TOP CB 55.0 LT

STA

+

π

-

ELEV.

92000

39+75 = TOE OF SLOPE RT

✓

BM

6.05

913.95

913.95

LT

E

3 MAY 1965

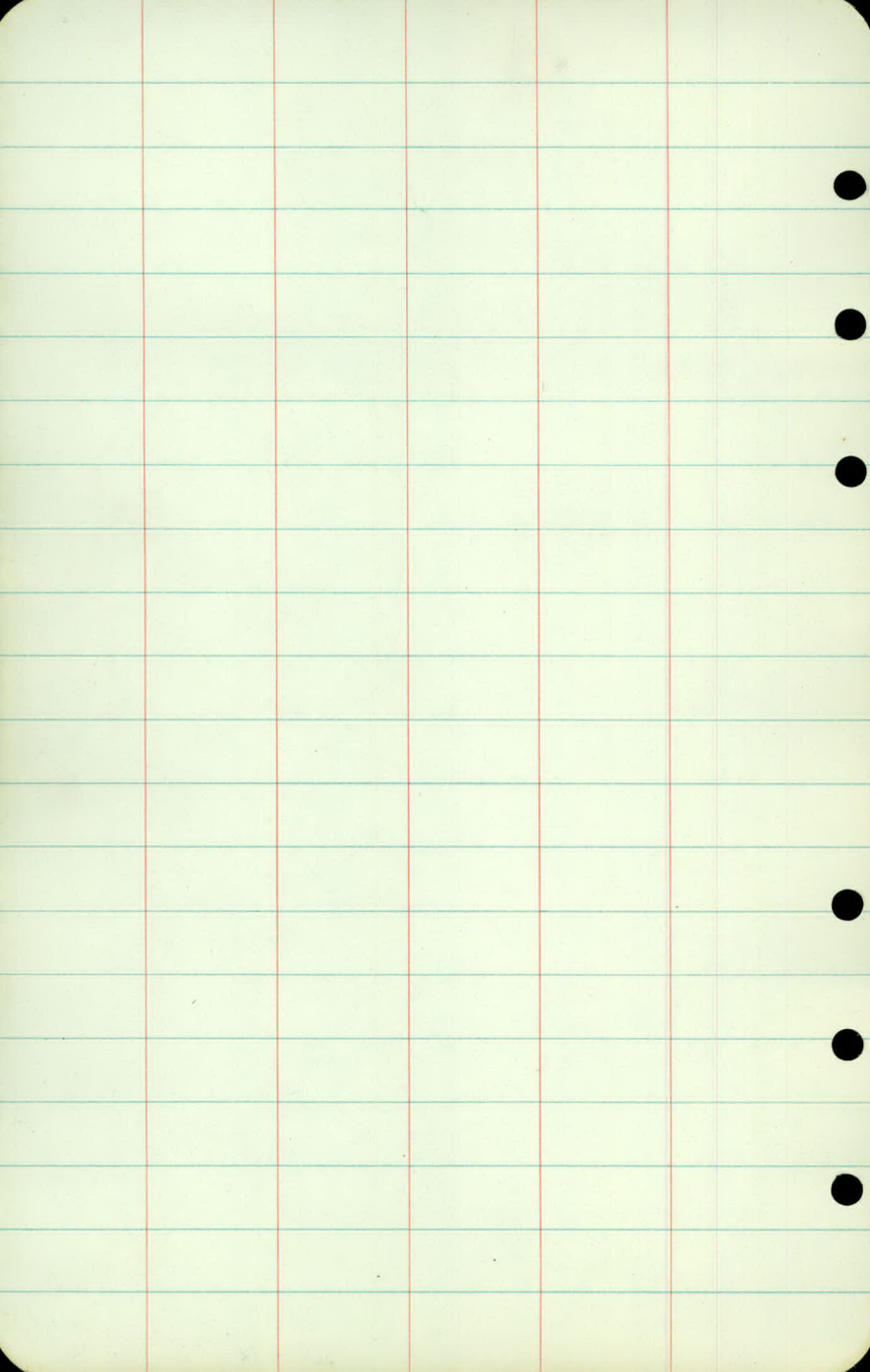
RT

101

15.4	15.0	15.2	14.8	14.6	14.2	8.1
4.6	5.0	4.8	5.2	5.4	5.8	11.9
26	25		22	37	52	68
TOP CURB	BOTTOM CURB					

15.8	16.4	17.1	9.9	6.7	7.8
4.2	3.6	2.9	10.1	13.30	12.20
47	74	100	100	90	70
			FL 30" SCP FL 15" SCP		

SPIKE IN 24" ELM 130.0 E, STA 37+75



April 28, 1965

102

1

McKnight Rd. & Lower Afton Rd.

Additional X-Sections

3 pages

Sta	+	T	-	Elev
B M	4.02	915.87		911.85

91+65

+80

+89

0+12

+22

+36

RG
LPD
PK

LT

£

RT

APR 28, 65
clear 45°
103
2

Top Hyd Lower AFTon & M^cKnight

90.45	07.2	07.7	08.1	08.5	08.8	09.1	09.4	09.9
9.4	8.7	8.2	7.8	7.4	7.1	6.8	6.5	6.0
100	75	50	22	✓	22	50	75	100

09.9	10.3	10.6	10.9	10.9	11.1	11.4	11.9	12.3
6.0	5.6	5.3	5.1	5.0	4.8	4.5	4.1	3.6
100	75	50	22	✓	22	50	75	100

10.0	10.5	10.8	11.0	11.2	11.4	11.7	12.1	12.6
5.9	5.4	5.1	4.9	4.7	4.5	4.2	3.8	3.3
100	75	50	22	✓	22	50	75	100

10.5	10.8	11.0	11.3	11.5	11.8	12.1
5.4	5.1	4.9	4.6	4.4	4.1	3.8
75	50	22	✓	22	50	75

10.2	10.5	10.7	10.9	11.2	11.5	11.9
5.7	5.4	5.2	5.0	4.7	4.4	4.0
75	50	22		22	50	75

08.1	08.4	08.8	08.8	09.0	09.6	10.1
7.8	7.5	7.1	7.1	6.9	6.3	5.8
75	50	22	✓	22	50	75

Sta	+	Σ	-	Elev
		915.87		
10+51				
T. P.	2.93	905.19	13.61	902.26
12+00			8.87	896.32
T. P.	9.41	912.50	2.10	903.09
			0.65	911.85 (911.85)

LT

£

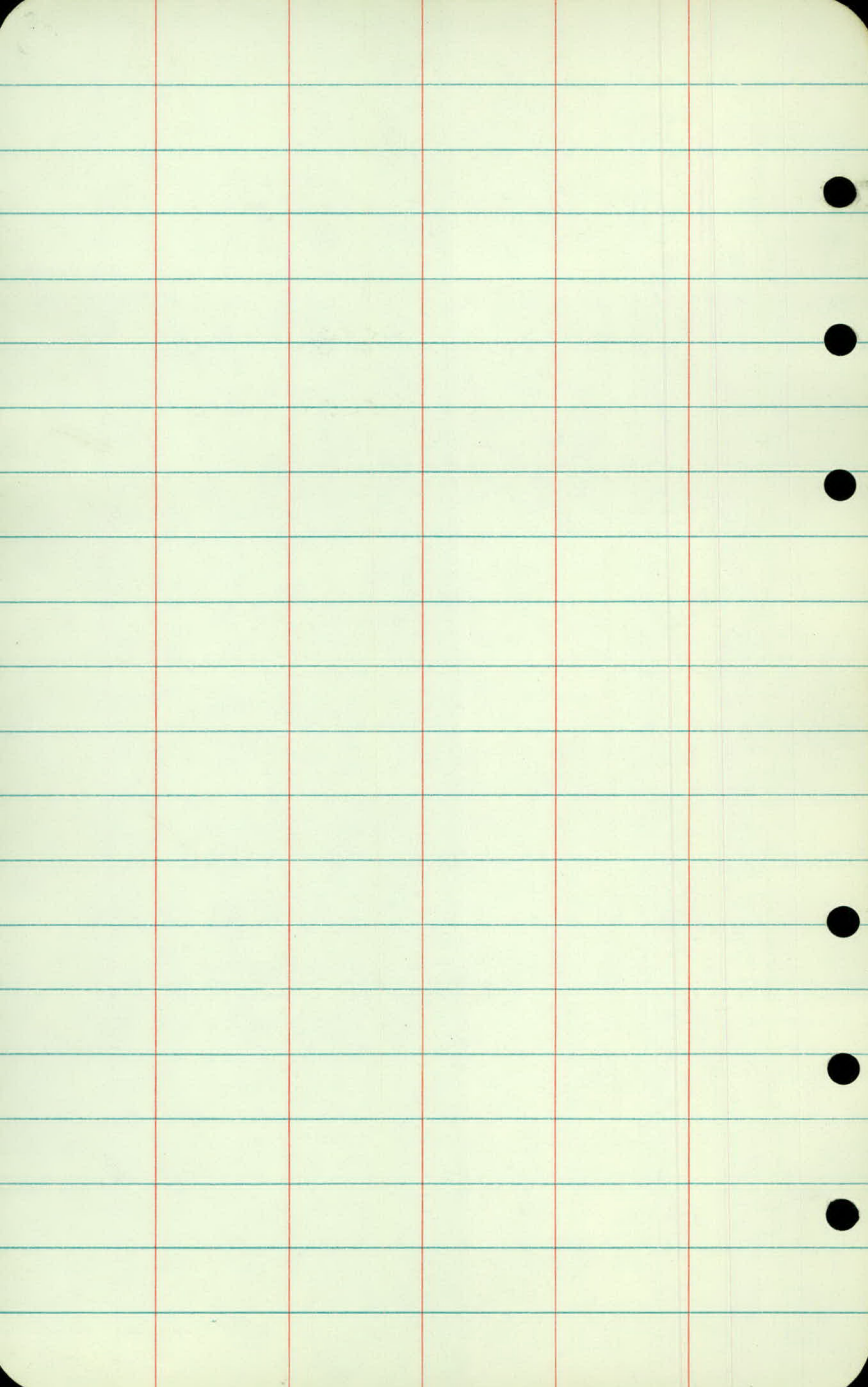
RT

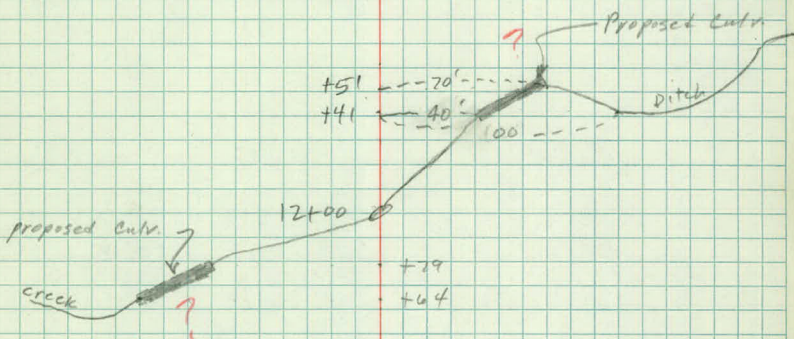
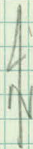
06.8	07.2	07.6	08.5	09.6	12.4	14.6	15.8
9.1	8.7	8.3	7.4	6.3	3.5	1.3	0.1
75	50	21	✓	20	32	48	75

Nail on £

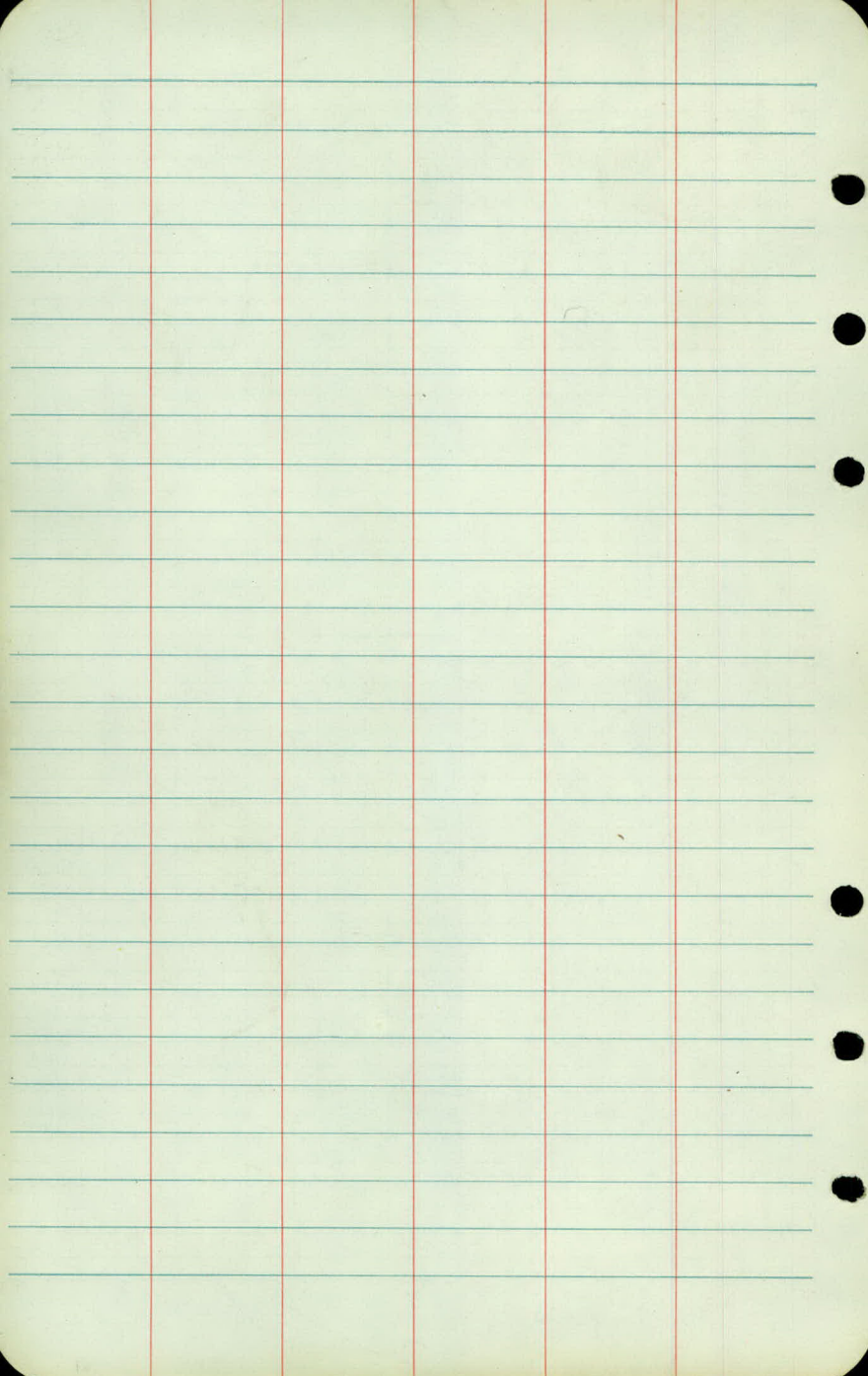
Nail

Top Hyd Lower AFTon & M^cKnight





Lower • Atton Rd



RG
PK
LPD

April 28, 1965
Fair 50°

106

1A

McKnight Rd.

Ditch Stadia

(Sta. 12+00)

4 pages

OBJECT

AZ.

STADIA

Sta 12+00

PI at 12+00

to 11+00

180°

Creek

238° 40'

"

242° 25'

00' LT. STA. 11+64

242° 20'

"

241° 55'

70' LT. STA. 11+79

250° 15'

"

251° 55'

"

252° 05'

"

249° 05'

"

259° 45'

"

199° 50'

"

94° 20'

"

53° 40'

"

48° 20'

"

44° 15'

"

40° 05'

70' AT. STA. 12+51

50° 55'

April 28, 1965 107

DIST.	VERT ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV. 2
-------	---------------	---------------	-----	-------	---------

H.I. = 901.2

896.12

5.1

~~901.2~~

100'

120'

0° 00"

8.5

92.7

114'

"

8.6

92.6

110'

"

8.5

92.7

97'

"

8.5

92.7

77'

"

8.5

92.7

62'

"

7.9

93.3

50'

"

7.5

93.7

40'

"

7.6

93.6

32'

"

7.8

93.4

8'

"

6.6

94.6

11'

"

6.5

94.7

28'

"

6.8

94.4

43'

"

4.5

96.7

56'

"

4.8

96.4

72'

"

3.6

97.6

89'

"

3.5

97.7

OBJECT

AZI

STADIA

T at 12+00

Creek

$56^{\circ} 05'$

"

$62^{\circ} 15'$

"

100' RT. STA. 12+41 $68^{\circ} 10'$

HI 901.2

Apr. 28, 1965 108

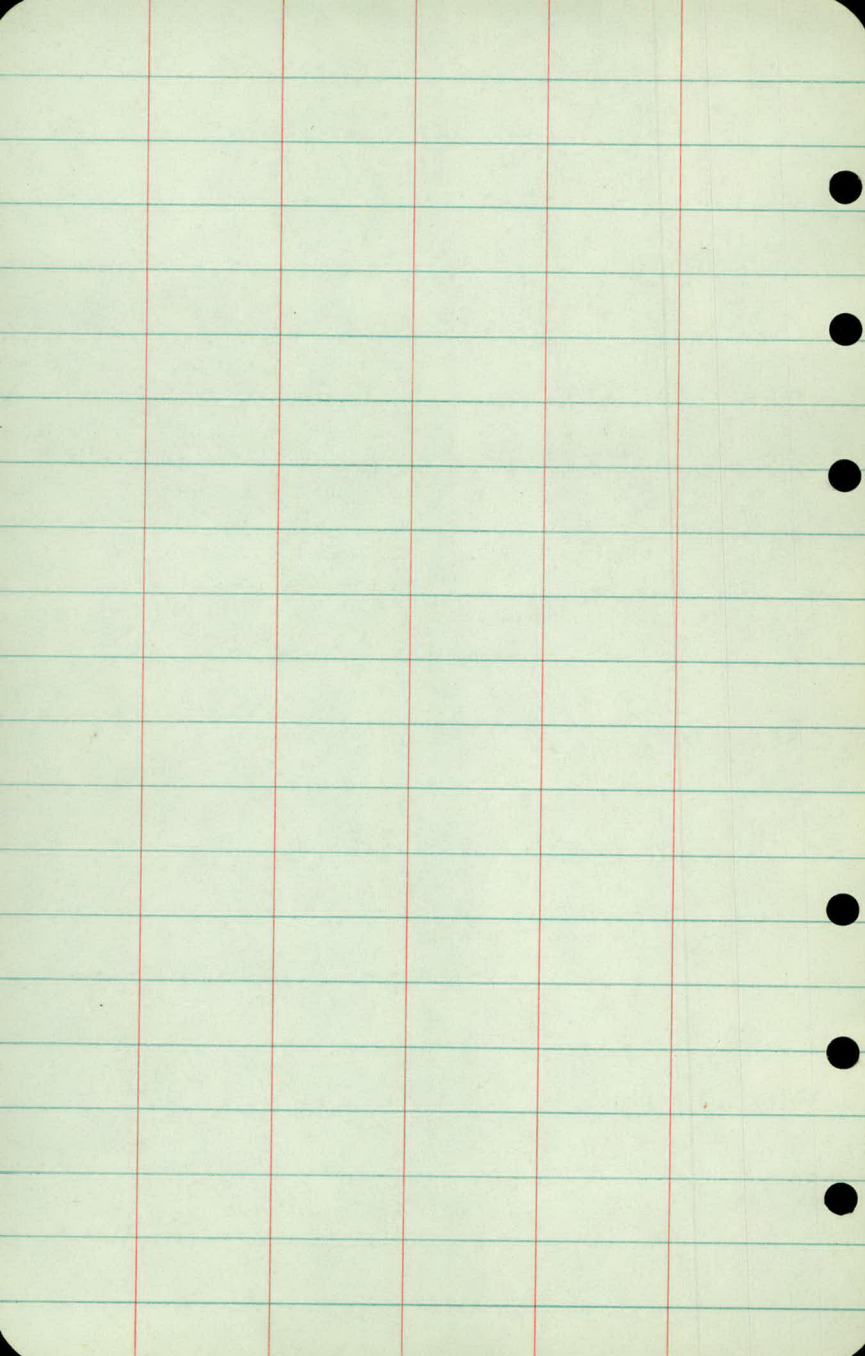
DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
					4

H.I. 901.4

103'	+1° 30'	+2.7	6.1	3.3	97.9
------	---------	------	-----	-----	------

108'	+5° 10'	+9.7	12.1	24	98.8
------	---------	------	------	----	------

115'	+4° 35'	+9.0	12.0	30	98.2
------	---------	------	------	----	------



Mc Knight

Sta + π - Elev.

BM 1.45 913.30 911.85

Size of Pipe at Winthrop 7.35 X 4.50
^{2 pipes} SCP-Arch

10+95

T.P. 2.51 902.39 13.42 899.88

10+95

✓
 TP 13.58 914.26 1.71 900.68

2.10 913.95 2.40 911.86 (911.85)

12+56

TP 6.19 909.39 10.75 903.20

TP 10.09 913.28 6.20 903.19

BM 1.44 911.85 (911.85)

FX
WM
DS
LPD

April 12, 1965 # 110

BM Top of NW Cor McKnight Flower Afton

99.8	93.3	95.1	96.1	
13.5	10.0	8.2	7.2	5.7
100	72	49	25	

90.4	90.4	91.1	90.9	92.8	95.0	96.9
12.0	12.0	11.3	11.5	9.6	7.4	5.5
1228	200	186	157	153	148	124

90.3	90.1	90.0	90.0	89.8
12.1	12.3	12.4	12.4	12.6
252	281	314	336	365

	89.36		89.2		89.3
9.89	13.06	13.2	13.1		
509	509	486	460		

Top S.E. of NW Wall
N Wing

96.6	98.5	96.4	98.0	96.9	93.2
10.8	10.7	13.0	11.4	12.5	16.2
	8	15	24	40	48

90.2	90.5	99.3	98.0	97.2
9.2	8.9	10.1	11.4	12.2
200	170	132	84	66

$\bar{\lambda}$ at 12+00

to 11+00

180° 100'

Creek

160° 7'

"

70° 14'

"

55° 26'

"

47° 40'

44° 57'

38° 71

44° 80'

49° 87'

52° 98'

58° 100

65° 111

237° 9

254° 21

262° 31

251° 41

253° 57'

251° 70'

FK
DS
WM
LPD

Obj
Creek

April 23, 1965

III

Az Dist.

249° 80'

246° 90'

241° 100'

243° 110'

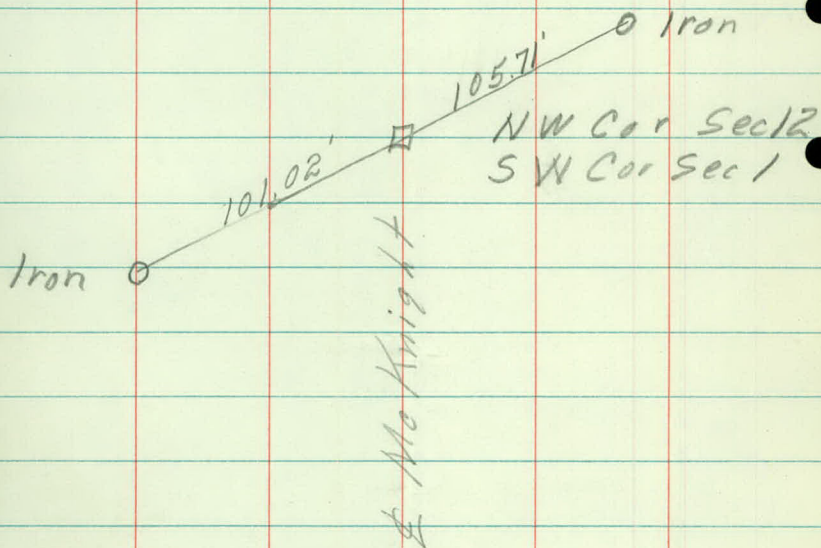
238° 120'

237° 125'

236° 138'

239° 153'

86
1502
101.02



RG
PK
LPD

April 28, 1965
Fair 60°

112
1

Stadia

M=Knight & Edgebrook Area

Pond Location

pages

OBJECT

AZ.

STADIA

BM

2.20

H.I.

934.53

T at Sta 27+00

to sta 24+00

180°00'

Edge Pond

283°50'

"

195°20'

"

174°40'

"

160°25'

"

151°00'

"

140°35'

"

140°10'

"

138°30'

"

126°50'

"

138°10'

"

140°35'

"

129°50'

"

106°50'

"

93°45'

"

80°10'

Apr. 28, 1965

113

2

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
p Hyd. NW Cor. McKnight RT & Edgebrook Ave. 932.33					
300'			1.1		933.4
15'			5.9		928.6
110'			"		"
243'			"		" ✓
330'			"		" ✓
450'			"		" ✓
565'			"		" ✓
687'			"		" ✓
573'			"		" ✓
460'			"		" ✓
440'			"		" ✓
309'			"		" ✓
251'			"		" ✓
270'			"		" ✓
415'			"		" ✓
495'			"		" ✓

OBJECT

AZ.

STADIA

Edge Pond

 $66^{\circ}25'$

"

 $55^{\circ}45'$

"

 $51^{\circ}30'$

"

 $40^{\circ}20'$

"

 $42^{\circ}20'$

"

 $30^{\circ}35'$

"

 $85^{\circ}30'$

"

 $164^{\circ}40'$

114
3

[illegible]

OBJECT.

AZ.

STADIA

A
N

McKnight Rd.

EDGEBROOK AVE

POND

Elev 928.6

935±

POND

man-made ditch

POND

923±

1/2

1/2

1/2

Lowland

1/2

1/2

1/2

RG
PK
LPD
RW

May 11, 1965
Fair 75°

116

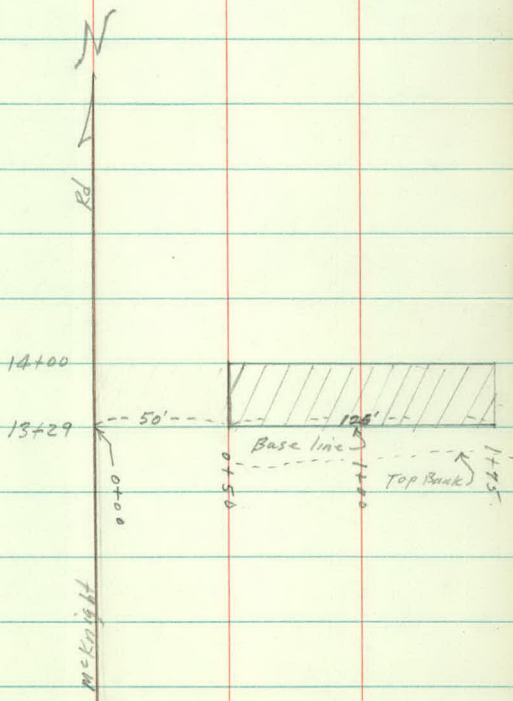
1

McKnight Rd.

Additional X-Sections

Sta 13+29 = baseline = 0+00

2 pages



Sta	+	π	-	Elev.
BM	7.34	923.19		915.85

0+50

+75

1+00

+25

+50

+75

BM			7.34	915.85
----	--	--	------	--------

Lt

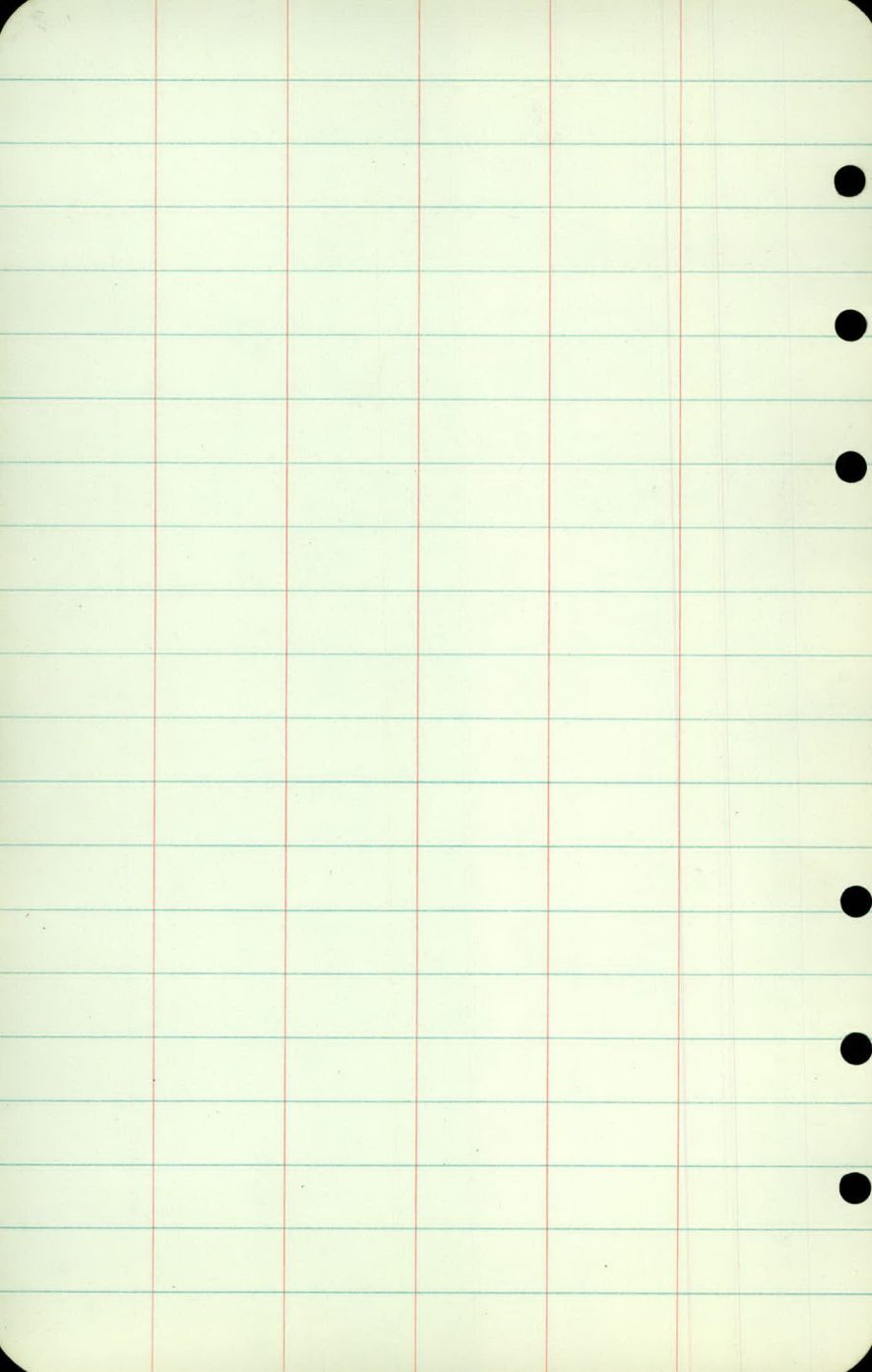
2

Rt

Spike in 4" Elm 20.0' Rt Sta 14+35

14.5	15.0	14.0	12.0	11.7	11.2
8.7	8.2	9.2	11.2	11.5	12.0
71	62	31	11		9
18.6	18.5	17.6	15.9	14.8	13.2
4.6	4.7	5.6	7.3	8.4	10.0
71	63	45	31	25	12
21.0	20.6	19.4	17.1	15.9	13.5
2.2	2.6	3.8	6.1	7.3	9.7
71	61	46	31	26	11
21.9	21.6	20.2	18.1	16.4	14.5
1.3	1.6	3.0	5.1	6.8	8.7
71	59	45	31	21	10
22.4	22.2	21.0	19.2	18.2	16.2
0.8	1.0	2.2	4.0	5.0	7.0
71	65	46	31	24	12
22.6	21.3	19.4	18.7	17.0	16.5
0.6	1.9	3.6	4.5	6.2	6.7
71	47	31	24	13	
					Fe
					17.4
					5.8
					11
					Fe

Above BM



May 17, 1965 118
1

McKnight Rd
Additional X-Sections

2 pages

Sta	+	π	-	E/v.
BM	1.62	986.44		984.82

55+38

TP	0.80	975.47	11.77	974.67
----	------	--------	-------	--------

55+38

✓

TP	12.39	987.24	0.62	974.85
----	-------	--------	------	--------

BM			2.42	984.82	984.82
----	--	--	------	--------	--------

RS
PK
LPD
RW

May 17, 1965
PC 60°

119

LT

2

2

Spk. in PP LT Sta 54+01

75.0	77.0	78.8	79.8	81.6	82.5	84.3	85.2	85.3	85.7	85.5
11.4	9.4	7.6	6.6	4.8	3.9	2.1	1.2	1.1	0.7	0.9
145	125	100	89	68	55	34	26	18	7	

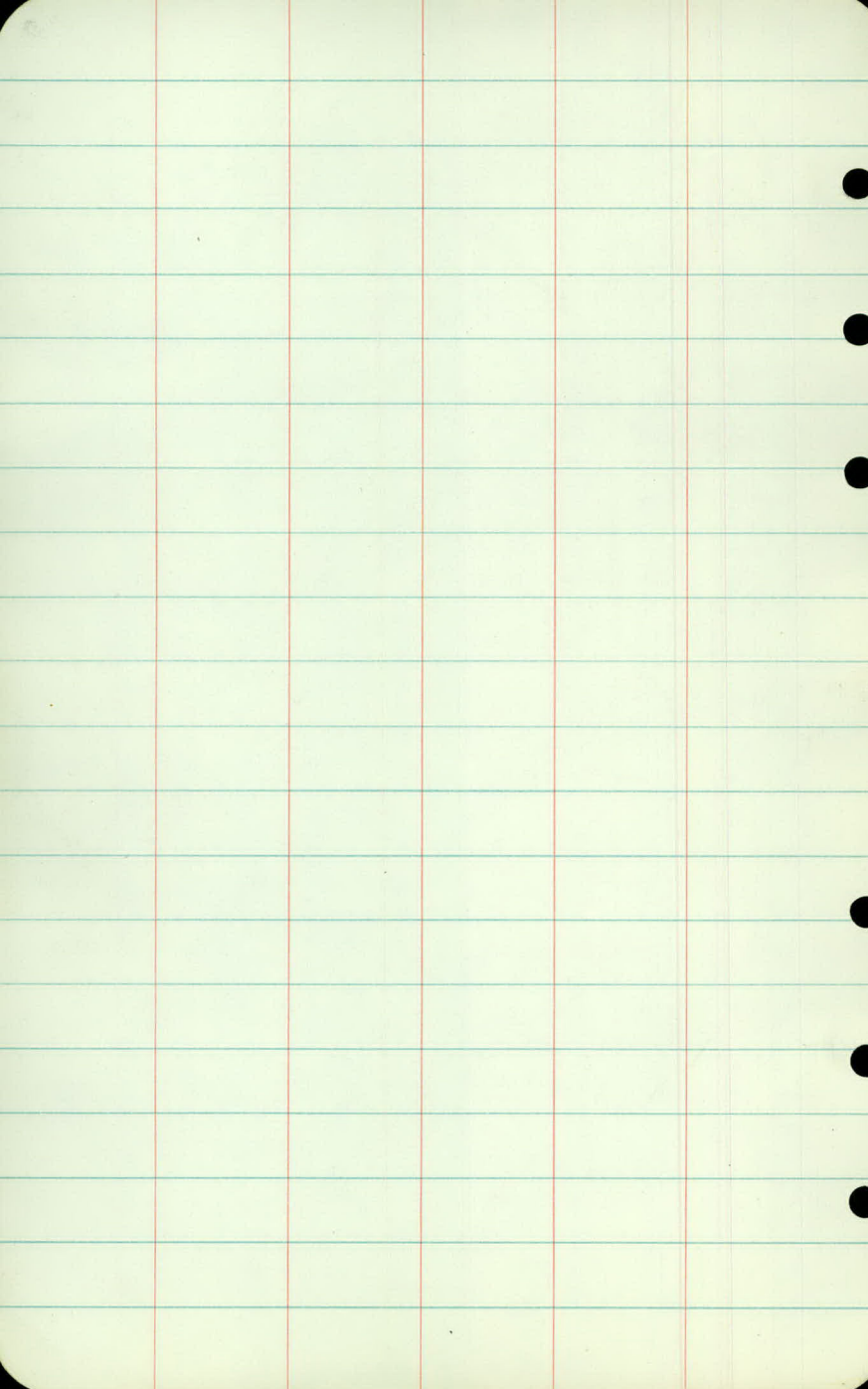
rock

72.8	70.0	68.8	66.5	65.1	64.4	63.8	63.4	63.2
2.7	5.5	6.7	9.0	10.4	11.1	11.7	11.9	12.3
166	188	200	222	242	263	288	300	320

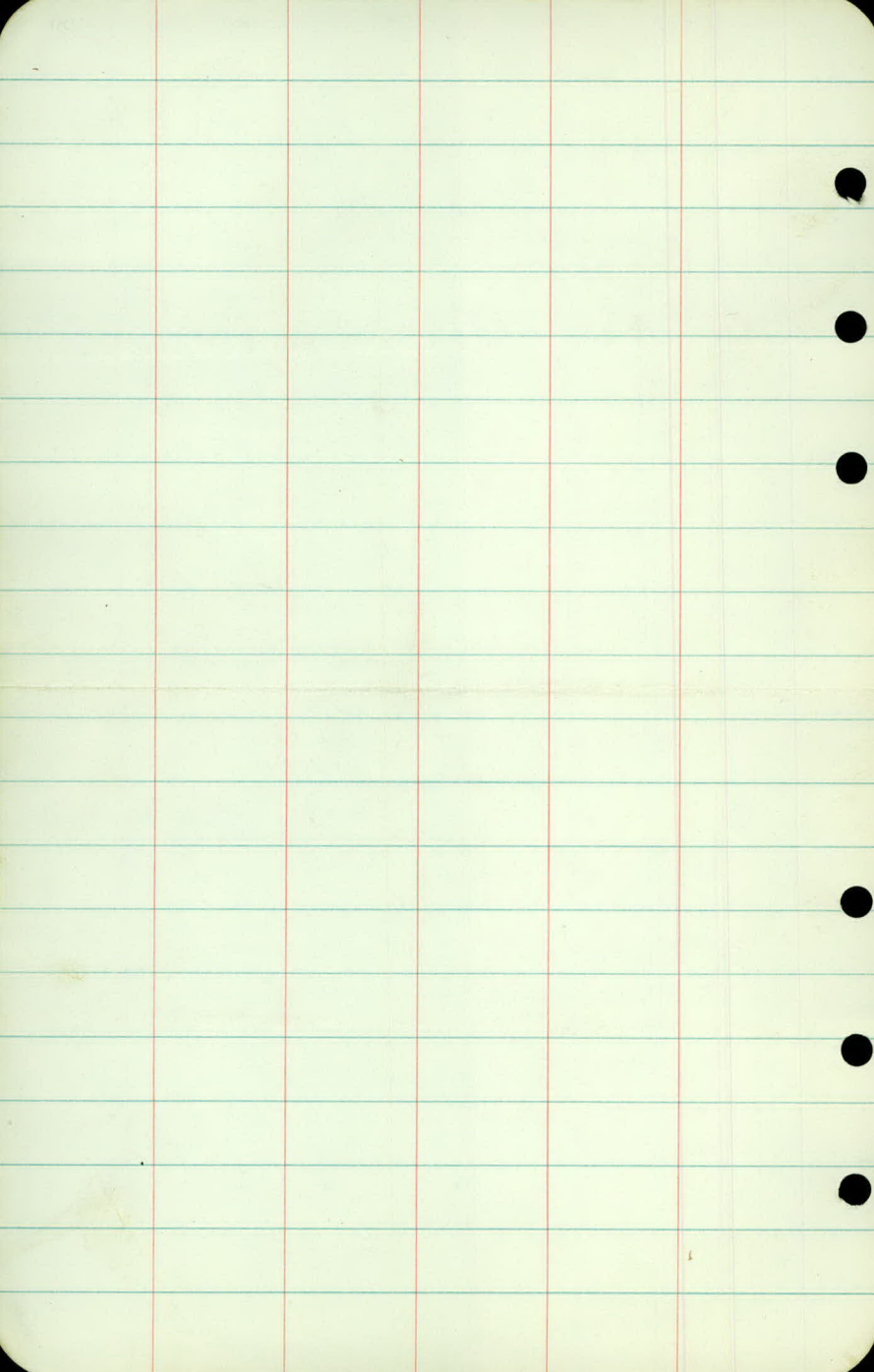
61.5	61.7
14.0	13.8
346	346

rock

Above BM



Sta	+	π	-	Elev.	
BM	5.34	945.79		940.45	Spk. in PP LT Sta 33+63
MH			4.89	940.90	2 Cardinal Pl. LT Sta 33+37
BM	3.15	930.50		927.35	Spk. in PP LT Sta 36+14
MH			4.50	926.00	2 Berland Pl. LT Sta 36+37
BM	4.50	921.16		916.66	Spk. in PP NW Cor M ² Knight & Lower Atten Rd
M.H.			4.27	916.89	LT Sta 39+09
M.H.			3.73	917.43	LT Sta 38+94±



July 13, 1965

121

a

Mc Knight Rd

M. H. Locations &
Elevations

Sta + π - Elev,

B M 1.25 913.10

911.85

10+54 MH Lt. 27 5.95 907.15

10+33 MH Rt. 26' 4.29 908.81

10+00 $\pm$

1.80 911.30

11.3

July 13, 1965

122

6

Top Hyd N.W. Cor McKnight of Lower Atton Rd.

$$\begin{array}{r} 907.15 \\ - 8.40 \\ \hline 898.75 \end{array}$$

7" Casting
1 Adj Ring
4 Eccentric Cone W
Base
FL to Top Cast = 8.4

7" Casting
1 Adj Ring
eccentric Cone
Steps West
4 Cone
1' Ring
Base

$$\begin{array}{r} 908.81 \\ - 8.70 \\ \hline 900.11 \end{array}$$

FL To Top Con = 8.7'

Sta	+	π	-	Elev.
-----	---	-------	---	-------

BM	1.09	912.94		
----	------	--------	--	--

				911.85
--	--	--	--	--------

10+95				
-------	--	--	--	--

✓				
---	--	--	--	--

11				
----	--	--	--	--

✓				
---	--	--	--	--

+27				
-----	--	--	--	--

✓				
---	--	--	--	--

FK
PK
LPD
HL

LT

July 21, 1965 123
C

Top Hyd N.W. Cox McKnight & Lower Aston Rd

00.74	02.54	03.44	05.24	02.3	05.3	06.2	07.6
12.2	10.4	9.5	2.7	10.6	7.6	6.7	5.3
86	81	71	47	45	44	22	

04.6
11.3 13.0
92 100

04.0	01.0	04.6	05.7	06.7	07.5
8.9	11.9	8.3	7.2	6.2	5.4
56	50	46	27	13	

03.2	02.2	01.1	09.9.9	09.9.5
9.7	10.7	11.8	13.0	13.4
66	80	81	89	100

09.9.9	0.6	2.2	4.0	4.9	03.9	05.5	06.8
13.0	12.3	10.7	8.9	8.0	9.0	7.4	6.1
64	50	36	29	19	17	13	

09.9.7 09.9.9
13.2 14.0
83 94

Sta + π - Elev.

912.94

11743

T.P. 3.82 903.75 13.01 899.93

10+95

✓

11

+27

T.P. 613 906.13 3.75 900.00

+43

July 25, 1965

124

96.7 99.8 01.0 01.2 02.0 02.8 03.5
 16.2 13.1 11.9 11.7 10.9 10.1 9.4
 66 54 33 22 12 7

92.8 94.9 96.1 96.0 97.2 98.2 99.2
 11.0 8.9 7.7 7.8 6.6 5.6 4.6
 149 145 138 130 121 116 107

92.6 92.6 92.7
 11.2 11.2 11.1
 150 153 166

93.2 92.8 93.5 94.9 95.8 97.0 99.2
 10.6 11.0 10.3 8.9 8.0 6.8 4.6
 153 149 144 140 131 119 107
 Creek

94.4 94.2 92.7 95.6 97.2
 9.4 9.6 11.1 8.2 6.6
 120 115 109 106 100
 Creek

10495

92.5 92.6 92.9 94.0 95.4 97.0 97.2 98.7
 13.6 13.5 13.2 12.1 10.7 9.1 8.9 7.4
 104 103 101 100 97.9 82 71
 Creek

94.8 95.7 96.1
 11.3 10.4 10.0
 106 112 120

Sta	+	T	-	Elev
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		906.13		
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11+67				
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✓				
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+84				
-----	--	--	--	--

✓				
---	--	--	--	--

+94				
-----	--	--	--	--

✓				
---	--	--	--	--

FK
PK
LPD
HL

LT

July 22 1965
£ 125

94.9 96.5 97.0 97.1 97.4 97.8 98.7 99.4 99.6 99.8
11.2 9.6 9.1 9.0 8.7 8.3 7.4 5.7 4.5 4.3
75 68 63 54 41 24 15 10 4

92.9 95.7 95.9 96.1 98.1 99.2 99.7
13.2 10.4 10.2 10.0 8.0 6.9 6.4
79 84 97 100 108 112 120
£ creek

94.7 93.6 93.6 93.7 94.6 96.8 97.1 97.4 96.9
11.4 12.5 12.5 12.4 11.5 9.3 9.0 8.7 9.2
57 52 42 39 38 31 21 9
£ creek

96.0 99.8 99.6 99.6 99.2 99.6 99.5
10.1 6.3 5.5 5.5 4.9 4.6 4.6
66 75 86 94 100 108 120

91.4 91.0 90.7 99.7 99.7 93.4 93.9 94.4 94.8 95.3
4.7 5.1 5.4 6.4 6.4 12.7 12.2 11.7 11.3 10.8
79 65 55 46 37 32 29 18 7

91.6 91.9 92.1 92.4
4.5 4.2 4.0 3.7
92 100 111 120

Sta	+	π	-	Elev
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		906.13		
--	--	--------	--	--

2+00				
------	--	--	--	--

+06				
-----	--	--	--	--

+25				
-----	--	--	--	--

TP	10.22	916.10	0.25	905.88
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12+25				
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+44				
-----	--	--	--	--

+56				
-----	--	--	--	--

JULY 22 1965

126

LT

£

02.6	02.6	02.4	02.2	02.1	01.5	01.2	00.8	00.3	00.1	00.3
3.5	3.5	3.7	3.9	4.0	4.6	4.9	6.3	8.8	8.0	9.8
120	114	100	92	79	61	43	27	13	5	

03.2	03.1	02.7	02.4	02.1	02.0	00.7	00.5	00.3
2.9	3.0	3.4	3.7	4.0	4.1	5.4	7.6	8.8
120	114	100	81	66	45	25	3	

03.3	02.9	00.9	00.6
2.8	3.2	5.2	5.5
47	27	11	

06.6	06.3	05.9	05.3	04.6
9.5	9.8	10.2	10.8	11.5
120	111	100	83	63

09.3	08.2	08.3	07.9	06.9	06.3	04.4	04.4	03.2	02.4
7.8	7.9	7.8	8.2	9.2	10.8	11.7	11.7	12.9	13.7
120	113	100	84	63	47	33	21	16	

11.3	10.9	10.4	09.7	08.6	07.2	05.8	03.2	03.1
4.8	5.2	5.7	6.4	7.5	8.9	10.3	12.9	13.0
120	114	100	87	68	48	19	10	

Sta + π - Elev

916.10

2+75

BM 5.67 921.34 0.43 915.67

3+00

TP 7.46 926.72 20.8 919.26

+12

+29

BM 10.83 915.89 915.85

TP 0.96 912.64 13.12 913.60

+12

+29

BM 10.03 902.61

JULY 22, 65

127

Lt

£

14.7	13.8	12.8	11.7	10.7	9.7	8.7	7.8	6.9	5.1	5.7
1.4	23	33	44	59	74	83	82	9.0	10.4	
120	100	85	70	54	39	30	21	10		

Top iron witness point to monument

920.5	20.2	19.6	19.2	18.6	17.8	16.6	14.8	10.8	10.0
0.8	11	1.7	2.1	2.7	3.5	4.8	6.5	10.5	11.3
120	116	110	100	88	75	60	46	22	

23.0	22.5	22.3	20.0	19.8	16.8	14.8
3.7	4.2	4.4	6.7	6.9	9.9	11.9
120	105	100	80	65	44	28

24.4	24.1	23.4	22.6	21.6	20.2	17.3	14.3	12.9
2.3	2.6	3.3	4.1	5.1	6.5	9.4	12.4	13.8
120	113	100	91	80	69	51	34	15

11.8	09.3	08.1	02.3
0.8	3.3	4.5	10.3
27	19	7	

10.6	10.1	06.3
1.8	2.5	6.3
14	7	

Top iron Sta 13+12.86

Creek Location

12+58 Rt

+100-3

+100

2

+54

2

+60

2

+64

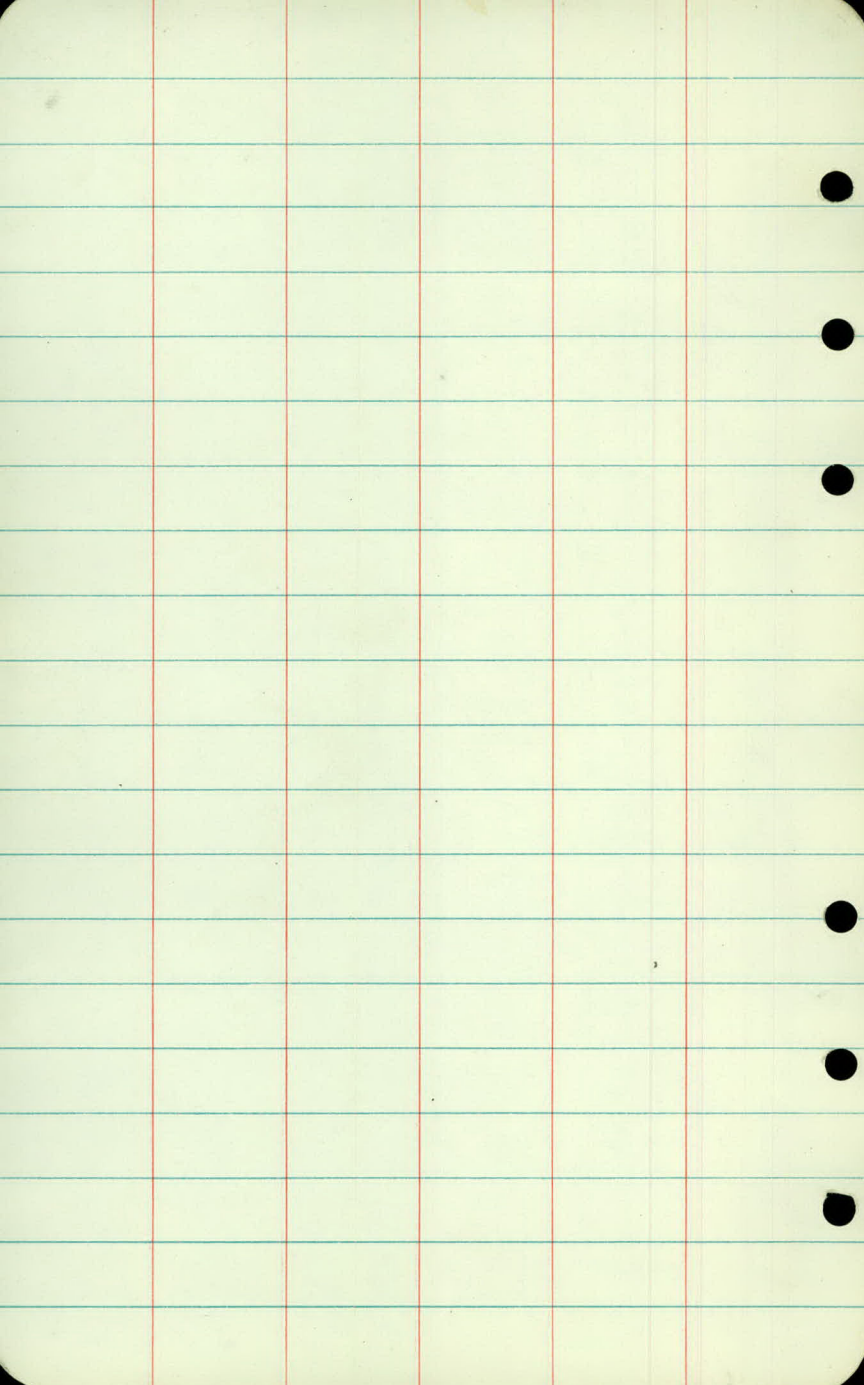
2

+70

2

75

2



PK
LPD
HL

JULY 30 1965
129

X sections

Cattle Pass

Sta	+	T	-	Elev
BM	0.75	912.60		911.85
TP	6.01	910.06	8.55	904.05

0+00

+ 12

+ 25

+ 46

+ 52

+ 63

LT

E

RT

130

Top Hyd NW cor. Lower Aftan + 11th Knight

0 ^{8.8}	0 ^{8.4}	0 ^{1.6}	0 ^{1.1}	0 ^{6.2}
1.3	1.7	2.5	3.0	3.9
10	5		4	10

0 ^{6.9}	0 ^{6.7}	0 ^{6.9}	0 ^{6.5}	0 ^{5.4}
3.2	3.4	3.2	3.6	4.7
10	6		3	10

0 ^{1.4}	0 ^{6.8}	0 ^{5.9}	0 ^{5.0}	0 ^{4.3}
2.7	3.3	4.2	5.1	5.8
12	6		5	10

0 ^{6.6}	0 ^{5.7}	0 ^{5.0}	0 ^{4.1}	0 ^{2.8}
3.5	4.4	5.1	6.0	7.3
10	6		6	10

0 ^{4.7}	0 ^{3.6}	0 ^{2.9}	0 ^{2.3}	0 ^{1.9}
5.4	6.5	7.2	7.8	8.2
10	5		7	10

0 ^{3.8}	0 ^{3.6}	0 ^{3.0}	0 ^{2.5}	0 ^{2.4}
6.3	6.5	7.1	7.6	7.7
10	6		6	10

Sta	+	T	-	Elev
-----	---	---	---	------

		910.06		
--	--	--------	--	--

+ 70				
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+ 75				
------	--	--	--	--

+ 80				
------	--	--	--	--

+ 87				
------	--	--	--	--

+ 01				
------	--	--	--	--

TP	10.95	909.32	11.69	898.37
----	-------	--------	-------	--------

+ 14				
------	--	--	--	--

Lt

£

RT

131

0 ^{3.0}	0 ^{3.3}	0 ^{3.1}	0 ^{2.7}	0 ^{2.3}
7.1	6.8	7.0	7.4	7.8
10	7		5	10

0 ^{1.3}	0 ^{1.3}	0 ^{1.2}	0 ^{1.7}	0 ^{2.4}	0 ^{2.0}
8.8	8.8	8.9	8.4	7.7	8.1
10	6		3	6	10

0 ^{3.3}	0 ^{1.8}	0 ^{0.9}	0 ^{0.2}	0 ^{0.7}
6.8	8.3	9.2	9.9	9.4
10	5		5	10

0 ^{3.4}	0 ^{2.9}	0 ^{2.4}	0 ^{2.0}	0 ^{0.5}	9 ^{9.6}
6.7	7.2	7.7	8.1	9.6	10.5
10	6		4	8	10

0 ^{3.2}	0 ^{1.9}	0 ^{1.4}	0 ^{0.4}	9 ^{8.6}	9 ^{7.4}
6.9	8.2	8.7	9.7	11.5	12.7
	6		3	5	9

£ creek

0 ^{0.4}	9 ^{00.0}	9 ^{8.9}	9 ^{7.6}	9 ^{8.8}	9 ^{9.5}
8.9	9.3	10.4	11.7	10.5	9.8
10	6	1	£ Creek	4	10

Sta	+	π	-	Elev
		909.32		

+20

+33

TP	7.40	910.44	6.28	903.04
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+50

+68

+87

TP	5.90	913.81	2.53	907.91
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2+01

LT

E

RT

132

01.8

900.0

99.0

97.6

98.9

900.0

00.6

7.5
139.3
5

10.3

11.7
2
creek10.4
49.3
78.7
10

02.4

01.4

00.8

99.1

00.2

01.1

8.0
109.0
3

9.6

11.3
410.2
79.3
10

creek

04.6

04.1

03.4

02.1

01.9

99.3

98.2

5.8
266.3
87.0
8

8.3

8.5
511.1
1312.2
15

creek

07.3

06.5

04.8

04.2

03.0

01.9

00.7

98.1

3.1
233.9
185.6
8

6.2

7.4
108.5
189.7
3111.7
34

creek

08.7

07.7

05.7

04.9

02.8

00.9

99.4

1.7
142.7
7

4.7

5.5
68.0
149.5
2211.0
23

creek

11.4

10.4

09.3

08.5

06.6

02.1

00.8

00.1

2.4
233.4
184.5
10

5.3

7.2
1211.7
2013.0
2913.7
34

creek

Sta	+	π	-	Elev
		913.81		

+ 21

+ 33

TP	4.48	907.49	10.80	903.01
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TP	8.96	912.81	3.14	904.35
----	------	--------	------	--------

			0.96	911.88 ⁵	911.85
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Rt

E

Lt

133

11.9	10.8	09.1	04.3	02.0	01.2	00.2
1.9	3.0	4.7	9.5	11.8	12.6	13.6
5		15	25	35	44	47

E creek

12.7	12.3	10.3	04.3	01.4	00.2
1.1	1.5	3.5	9.5	12.4	13.6
5	21	32	50	55	

E creek

Top Hyd NW Cor Lower Afton & ME Knight

Sta

+

π

-

