

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

LAKE JOHANNA BLVD.

From CO. RD. "D" To CO. RD. "E"

Road Acc't. No. 49 Dr. 9

Date Filed 12-15-66 File BK. 58

S.A.P. 62-649-01 1965

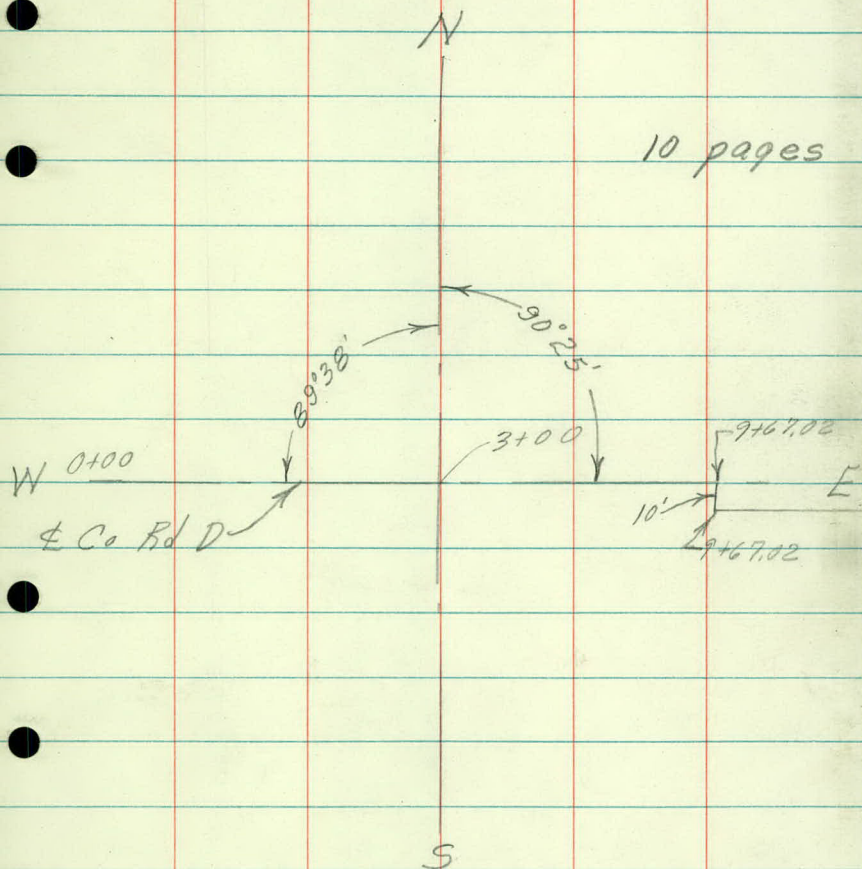
March 16, 1965

1

LAKE JOHANNA BLVD

Co Rd D Profile & X-Sections

10 pages



Sta + π - Elev.

BM 5.03 931.39

926.36

0+00

+50

1

+50

+90

2+10

FA
WM
PK
LD

Lt.

March 16, 1965

Cloudy 10° Rt. 2

Top Mont & Co. Rd. "D" & Lake Johanna Blvd.

27.7	27.3	27.2	27.3	27.4	27.1	26.6	27.1
3.7	4.1	4.2	4.1	4.0	4.3	4.8	4.3
47	32	18	10	✓	11	20	48

27.8	27.3	26.8	27.0	27.0	26.7	26.4	26.6	27.2
36.4	40.6	4.6	4.4	4.4	4.7	5.0	4.8	4.2
56	42	19	11	✓	11	18	32	49

Cont. Ent

26.7	26.6	26.1	26.5	26.6	26.3	25.9	26.4
4.7	4.8	5.3	4.9	4.8	5.1	5.5	5.0
57	36	19	12	✓	11	19	48

26.0	26.1	25.8	26.1	26.2	25.9	25.6	25.9	26.0
5.4	5.3	5.6	5.3	5.2	5.5	5.8	5.5	5.4
50	33	19	12	✓	9	17	35	49

25.8	24.2	25.4	25.9	26.0	25.9	25.5	25.9	26.0
5.6	5.2	6.0	5.5	5.4	5.5	5.9	5.7	5.4
52	35	19	12	✓	11	15	28	40

25.6	25.9	25.4	25.9	26.1	26.0	25.6	26.1	26.6
5.8	5.5	6.0	5.5	5.3	5.4	5.8	5.3	4.8
54	33	17	11	✓	11	16	37	50

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		931.39		
--	--	--------	--	--

2+25				
------	--	--	--	--

2+43				
------	--	--	--	--

513

3.29

184

TP	3.61	931.71	3.29	928.10
----	------	--------	------	--------

5			5.7	26.0
---	--	--	-----	------

TP	1.97	930.37	3.31	928.40
----	------	--------	------	--------

+50			4.3	26.1
-----	--	--	-----	------

6			4.5	25.9
---	--	--	-----	------

+50			5.1	25.3
-----	--	--	-----	------

7			6.4	24.0
---	--	--	-----	------

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3

26.3	25.6	25.3	25.9	26.1	26.0	25.6	25.7	26.5
5.1	5.8	6.1	5.5	5.3	5.4	5.8	5.7	4.9
54	34	22	14	✓	8	14	28	50

27.0	26.7	26.3	26.4	26.3	25.9	25.6	25.8	26.5
4.4	4.7	5.1	5.0	5.1	5.5	5.8	5.6	4.9
58	38	24	16		13	15	39	56

Top Hyd S.W. Cor D + Fairview

Top Hyd 201' E + 20' N. E D + Fairview

130

Sta	+	π	-	Elev.
-----	---	-------	---	-------

930.37

7+50			7.2	23.2
------	--	--	-----	------

BM	3.45	928.74	5.08	925.29
----	------	--------	------	--------

8			6.1	22.6
---	--	--	-----	------

+50			6.6	22.1
-----	--	--	-----	------

9			7.0	21.7
---	--	--	-----	------

+35			7.4	21.3	6.5
-----	--	--	-----	------	-----

+67.02			6.6	22.1	6.0
--------	--	--	-----	------	-----

+67.02	Rt 10' & Esmt		7.4	21.3	6.4
--------	---------------	--	-----	------	-----

10			6.8	21.9
----	--	--	-----	------

+47			6.6	22.1
-----	--	--	-----	------

March 16, 1965

4

Top Hyd S.E. Cor Co Rd "D" & Wheeler

Sta	+	π	-	Elev
		928.74		
10+72			8.2	20.5
11			11.5	17.2
TP	1.71	918.98	11.47	917.27
+25			5.5	13.5
+50			8.6	10.4
+72			12.2	06.8
+80		13.65 125	14.90	5.3 04.08
TP	3.16	908.49	13.65	905.33
12+08		133.4 125 145	14.59	893.90
12+08	$\pm$		17.6	90.9
+30			24.5 ⁺	84.0
T.P.	13.65	918.98	3.16	905.33
T.P.	11.56	928.84	1.70	917.28

March 16, 1965

5

Spike Sta 11

Ink Culvert 10' R1

Inv E. End 15" x 28' C

Top W. E 15" x 28' CM
Sta 11 Z

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		928.84		
--	--	--------	--	--

BM	5.12	930.41	3.55	925.29
----	------	--------	------	--------

BM	3.22	931.62	2.01	928.40	928.50
----	------	--------	------	--------	--------

BM			5.26	926.36	926.36
----	--	--	------	--------	--------

BM			3.52	928.10	928.10
----	--	--	------	--------	--------

1.74

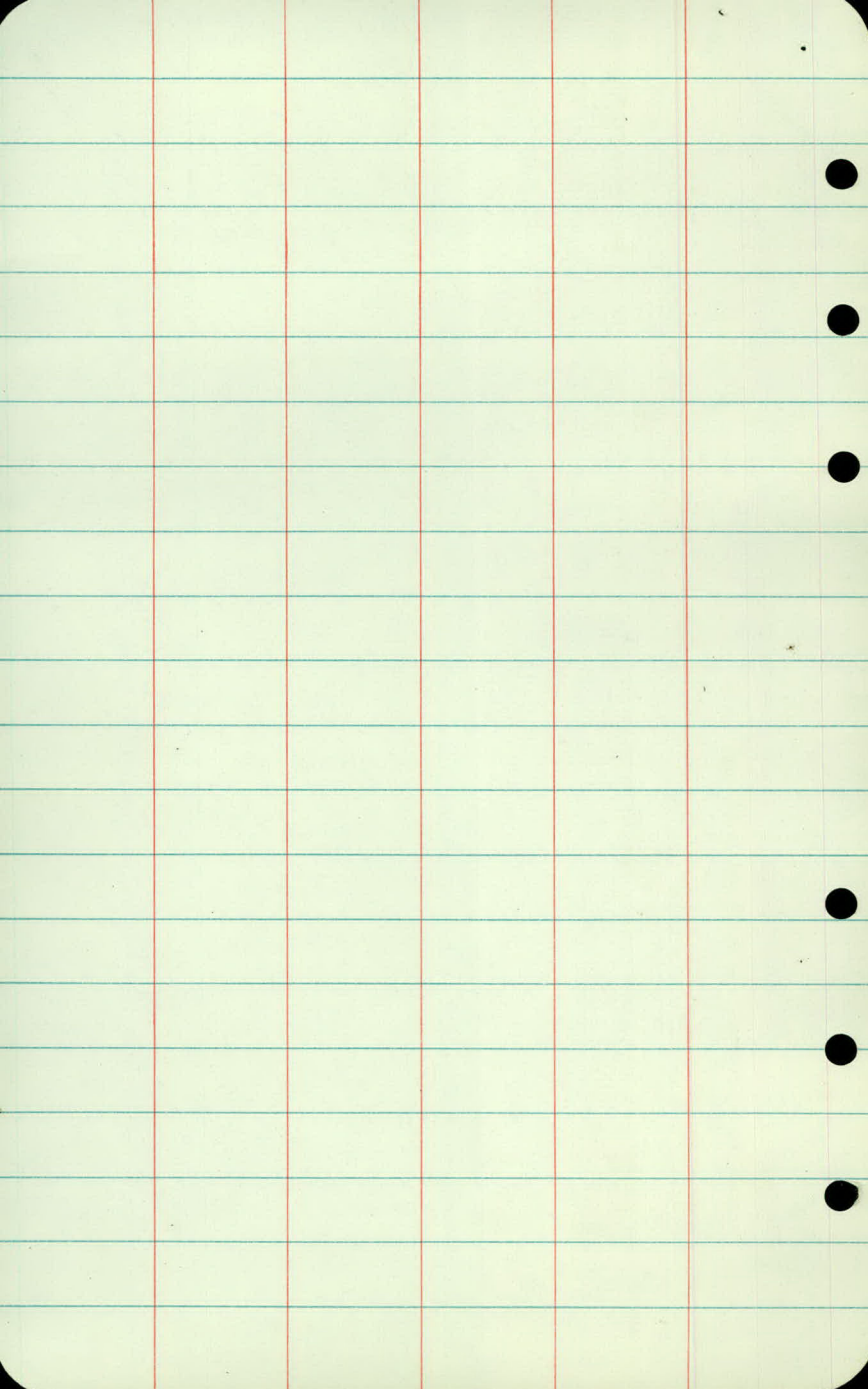
March 16, 1965 6

Top Hyd S.E. Cor Wheeler & Co Rd "D"

Top Hyd 200' E & 20' N of E D & Fairview

Top Mont. & Co Rd "D" & Lake Johanna Blvd.

Top Hyd S.W. Cor D & Fairview



March 16, 1965

7

9

$$+86 \frac{33''0}{25}$$

$$+85 \frac{26''0}{30}$$

$$+66 \frac{PP}{34}$$

$$+49 \frac{End Hedge}{25}$$

8

$$+66 \frac{PP}{14}$$

$$+74 \frac{Hyd}{25}$$

$$+72 \frac{Cor Hedge}{23}$$

7

7

$$+79 \frac{20'' BE}{16}$$

$$+54 \frac{14'' BE}{15}$$

$$+13 \frac{12'' Elm}{36}$$

$$+11 \frac{PP}{17}$$

$$+20 \frac{N.W. Cor Ho}{35}$$

6

$$+96 \frac{12'' Elm}{36}$$

$$+58 \frac{18'' Elm}{36}$$

$$+03 \frac{16'' Elm}{36}$$

5

$$+01 \frac{Hyd}{22}$$

$$+64 \frac{PP}{20}$$

$$+52 \frac{22''0}{18}$$

$$+44 \frac{Cor Walk}{30}$$

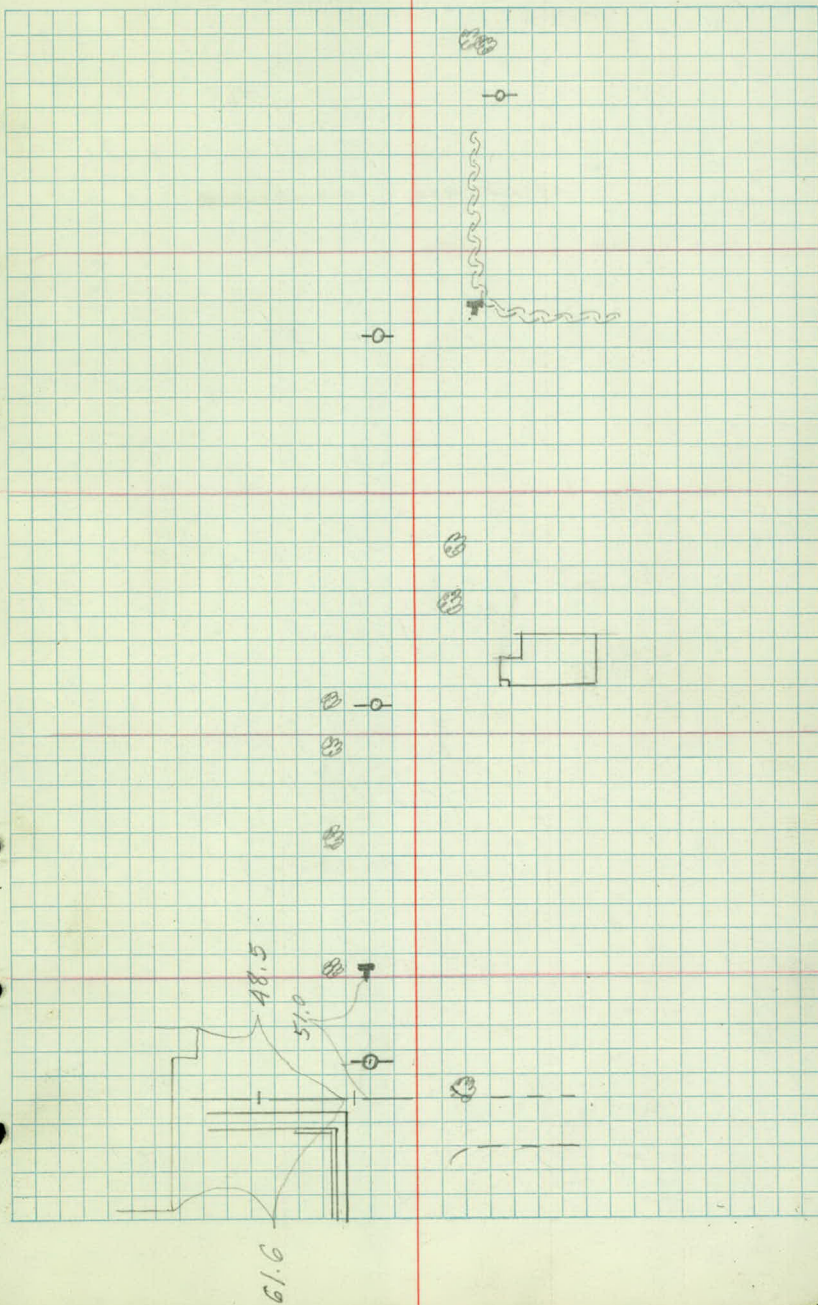
$$+37 \frac{Cor Curb}{34}$$

$$+39 \frac{\pm Double Ent}{}$$

4

March 16, 1965

8



+15 Waters Edge

13

+51 $\frac{\text{Trip 12" Willow}}{3}$

+30 Bottom of slope

12
 +73 $\frac{3" \text{ Maple}}{6}$ +13
 +48 $\frac{\text{Iron}}{10}$ +51 $\frac{3" \text{ Spruce}}{3}$ +78 $\frac{3" \text{ M}}{21}$
 +37 $\frac{4" \text{ Spr}}{2}$ +71 $\frac{\text{Bog Fe}}{21}$ +74
 +108 $\frac{\text{E.E 15" CM}}{10}$ +80 $\frac{\text{WE 15" CM}}{10}$
 +123 $\frac{2" \text{ Spruce}}{4}$

1P
 +75 $\frac{\text{Cor Wall}}{10}$ +89 $\frac{3" \text{ Apple}}{6}$ +89 $\frac{4" \text{ P}}{11}$ +56 $\frac{6" \text{ Apple}}{12}$ +94 $\frac{2" \text{ Apple}}{12}$
 +75 $\frac{5" \text{ Apple}}{7}$ +41 $\frac{10" \text{ LP}}{13}$ +52 $\frac{10" \text{ Elm}}{25}$ +147 $\frac{1" \text{ Birch}}{10}$
 +25 $\frac{10" \text{ LP}}{13}$ +55 $\frac{\text{Tree}}{14}$ +32 $\frac{10" \text{ LP}}{79}$ +36 $\frac{4" \text{ Maple}}{13}$ +42 $\frac{5" \text{ Birch}}{11}$ +45 $\frac{4" \text{ Birch}}{12}$
 +55 $\frac{\text{Fe P}}{10}$ +17 $\frac{14" \text{ LP}}{12}$ +58 $\frac{\text{Fire P}}{11}$ +23 $\frac{4-3" \text{ Birch}}{12}$
 10 +14 $\frac{\text{SW Cor Ho}}{26}$ +09 $\frac{12" \text{ LP}}{13}$ +02 $\frac{3" \text{ MH Ash}}{13}$ +06 $\frac{\text{NW Cor Bldg}}{9}$
 +94 $\frac{4" \text{ Maple}}{17}$

+62 $\frac{\text{Fe Post}}{2}$

+98 $\frac{3" \text{ N. Pine}}{10}$

+94 $\frac{\text{PP}}{23}$

+96 $\frac{8" \text{ LP}}{30}$

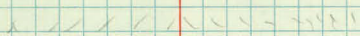
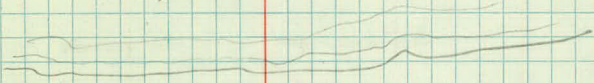
9

+23 $\frac{\text{Arc Lt}}{12}$

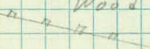
March 16, 1965

9

Pond



Wood Rail Fe



4.5K5

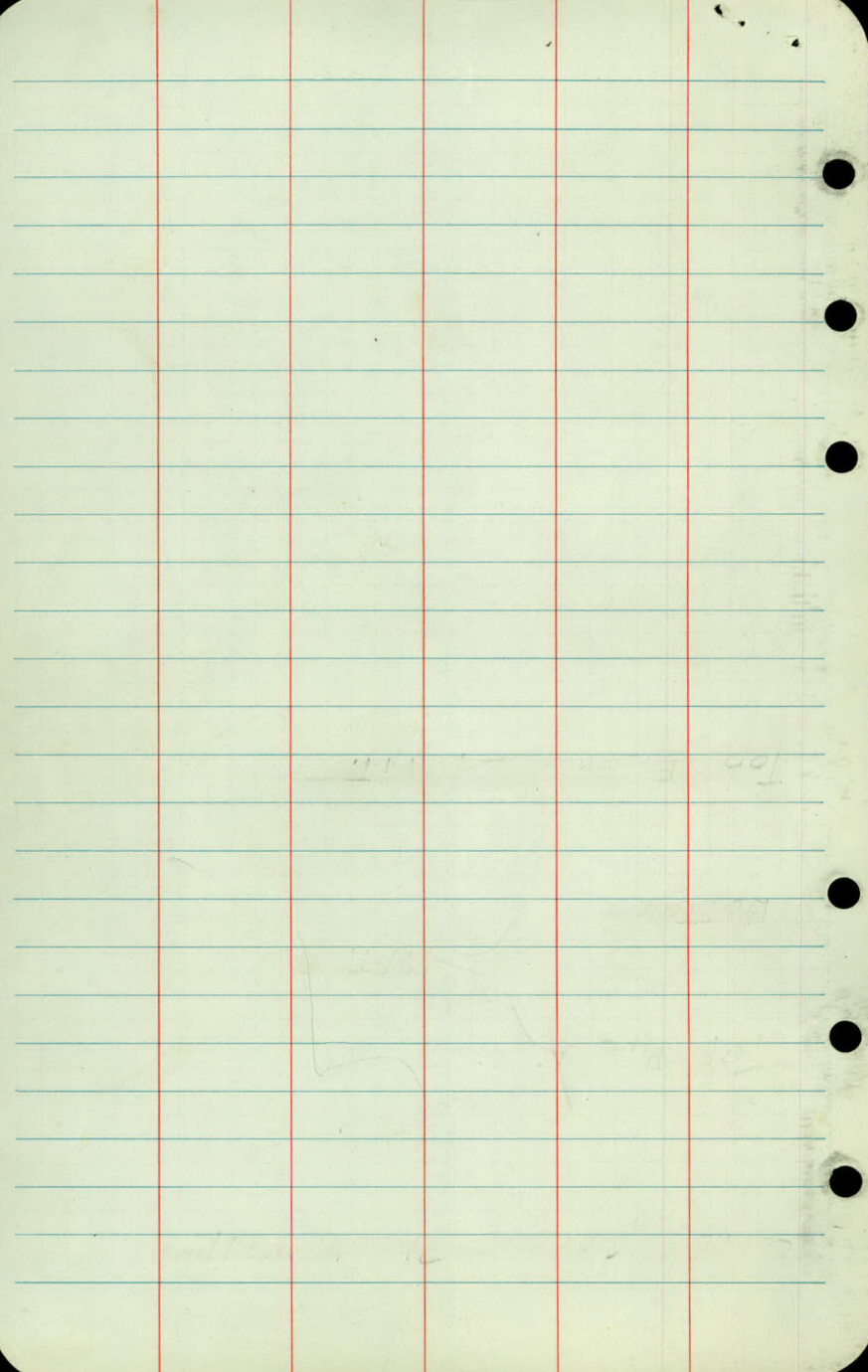
E 3W

N



11x11





30 DEC. 1964

LT

Σ

RT

23

21.3	21.3	21.3	21.4	21.1	20.3	17.4	15.1
4.5	4.4	4.4	4.3	4.6	5.4	8.3	10.6
22	16	10		12	20	31	40

22.1	22.5	23.4	24.1		10.9	12.4
3.6	3.2	2.3	1.6		14.8	13.3
30	38	56	75		75	61

22.0	21.4	21.4	21.4	21.5	21.2	20.4	18.8	16.8
3.7	4.3	4.3	4.3	4.2	4.5	5.3	6.9	8.9
23	20	14	9		14	19	27	34

23.8	25.0	25.7		11.1	13.8
1.9	0.7	0.0		14.6	11.9
34	50	75		75	54

TOP PK Σ STA 12400

26.5	25.2	22.9	22.2	22.1	22.0	21.7	21.1	19.0	16.7	15.4
2.6	3.9	6.2	6.9	7.0	7.1	7.4	8.0	10.1	12.4	13.7
53	34	21	16	10		13	21	32	47	60

26.1
2.4
75

13.2
15.9
75

STA + T - ELEV.

929.08
~~929.10~~

12+17 ± ENTRANCE LT.

✓

+36

✓

+70

✓

LT

30 DEC. 1964

RT

24

23.9	23.46	22.8	22.3	22.1	21.9	21.5	19.9	18.1
5.39	5.62	6.3	6.8	7.0	7.2	7.6	9.2	11.0
50	31	18	9		12	18	26	41
conc.	conc.							

25.67

3.41

75

conc.

14.7

16.1

14.4

13.0

75

60

26.4	24.5	22.6	22.4	22.4	22.0	21.7	19.9	17.9
2.7	4.6	6.5	6.7	6.7	7.1	7.4	9.2	11.2
32	23	17	9		14	19	27	47

27.5

1.6

44

27.6

1.5

60

27.7

1.4

75

15.5

13.6

75

16.6

12.5

63

26.9	25.3	23.0	22.6	22.1	22.4	22.0	21.1	18.6
2.2	3.8	6.1	6.5	6.4	6.7	7.1	8.0	10.5
29	24	18	10		13	21	34	55

27.9

1.2

46

28.3

0.8

62

28.7

0.4

75

16.6

12.5

75

STA + π - ELEV.

~~929.10~~
929.08

13+00

✓

+13

3.69 925.39

+14 DITCH RT

✓

+20 SHOULDER RT

30 DEC. 1964

LT

Z

RT

25

25.1	23.3	22.9	22.8	23.0	22.7	22.2	20.8	18.9
4.0	5.8	6.2	6.3	6.1	6.4	6.9	8.3	10.2
23	18	14	9		15	22	32	52

26.7	27.9	28.1	28.2
2.4	1.2	1.0	0.9
29	43	58	75

17.5
11.6
75

TOP MH 23.0 LT

27.0	25.2	23.6	23.0	23.1	22.6	22.3	22.0	20.1
2.1	3.9	5.5	6.1	6.0	6.5	6.8	7.1	9.0
31	22	18	11		16	26	35	46

28.0	28.4	28.4
1.1	0.7	0.7
47	68	75

17.0	19.0
12.1	11.1
75	66

24.6	27.8	27.1	25.2	23.8	23.3	23.1	22.8	22.2	20.6	18.5
0.6	1.3	2.0	3.9	5.3	5.8	6.0	6.3	6.9	8.5	10.6
64	45	30	22	17	11		15	33	57	75

23.3
0.8
75

STA	+	T	-	ELEV.
-----	---	---	---	-------

~~929.08~~

~~929.10~~

~~929.18~~

~~923.27~~

BM

5.91

~~929.20~~

5.81

~~923.29~~

923.27

13+29

± SANDEEN RD (S)

+38

SHOULDER RT.

+75

30 DEC. 1964

LT

~~E~~

RT 26

SPIKE IN PP 27.0 RT STA 13+45

27.3	27.4	27.4	27.3	27.2	27.9	27.3	27.1	27.6
1.9	4.8	5.8	5.9	6.0	6.3	6.9	8.1	11.6
29	19	14	8		17	33	55	85

27.8
1.4
40

28.3
0.9
75

27.2 27.7 27.5
17.0 16.5 13.7
160 125 100

27.1	27.4	27.6	27.3	27.2	27.0	27.5	27.0	27.9
2.1	4.8	5.6	5.9	6.0	6.2	6.7	7.2	8.3
29	20	16	10		15	23	36	55

27.9
1.3
43

28.4
0.8
75

28.5
10.7
75

26.8	27.5	27.8	27.5	27.4	27.3	27.1	27.5	27.2
2.4	4.7	5.4	5.7	5.8	5.9	6.1	6.7	8.0
28	18	13	8		12	21	30	42

27.5 27.8 27.1
1.7 1.4 1.1
36 53 75

28.2 28.5
11.0 9.7
79 58
40

STA

+

π

-

ELEV.

~~929.18~~
929.20

✓
13+91

± ENTRANCE LT

✓
14+00

✓
+28

± ENTRANCE RT

✓

30 DEC. 1964

LT

#

RT

27

25.7	24.8	24.3	23.6	23.4	23.3	22.9	22.1	21.1
3.5	4.4	4.9	5.6	5.8	5.9	6.3	7.1	8.1
53	31	18	9		12	21	31	38

26.8	27.6	27.77
2.4	1.6	1.41
75	100	118

ONE GA
APRON

18.2	19.7
11.0	9.5
80	54
40	

27.9	26.6	24.4	23.6	23.4	23.4	23.1	22.9	21.0
1.3	2.6	4.8	5.6	5.8	5.8	6.1	6.3	8.2
44	31	21	11		11	19	26	38

28.1	28.4
1.1	0.8
59	75

17.4	19.2
11.8	10.0
78	57
40	

26.8	25.2	23.7	23.2	23.4	23.4	23.1	21.4	19.4
2.4	4.0	5.5	6.0	5.8	5.8	6.1	7.8	9.8
37	25	19	12		11	20	33	50

27.4	27.8
1.8	1.4
60	75

17.58	18.0
11.60	11.2
90	69
CORR.	
GA	
APRON	

STA

+

T

-

ELEV.

929.18
~~929.20~~

14+56

✓

+78

✓

+94 ± ENTRANCE LT

✓

30 DEC. 1964

LT

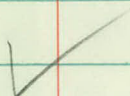
F

RT

28

$\gamma_{6.2}$	$\gamma_{5.1}$	$\gamma_{3.4}$	$\gamma_{3.2}$	$\gamma_{3.3}$	$\gamma_{3.3}$	$\gamma_{3.0}$	$\gamma_{2.4}$	$\gamma_{2.8}$
30	4.1	5.8	6.0	5.9	5.9	6.2	6.8	8.4
49	29	21	13		14	23	31	37

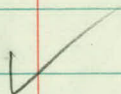
$\gamma_{6.8}$
2.4
75



$\gamma_{6.2}$ $\gamma_{6.6}$
11.0 9.7
80 54
40

$\gamma_{5.3}$	$\gamma_{4.6}$	$\gamma_{3.4}$	$\gamma_{3.2}$	$\gamma_{3.3}$	$\gamma_{3.2}$	$\gamma_{3.1}$	$\gamma_{2.7}$
3.9	4.6	5.8	6.0	5.9	6.0	6.1	6.5
46	27	21	13		16	23	30

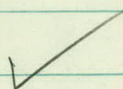
$\gamma_{6.0}$ $\gamma_{6.6}$
3.2 2.6
62 75



$\gamma_{6.2}$ $\gamma_{6.3}$ $\gamma_{6.7}$
11.0 9.9 8.5
75 57 36

$\gamma_{4.1}$	$\gamma_{3.6}$	$\gamma_{3.3}$	$\gamma_{3.1}$	$\gamma_{3.2}$	$\gamma_{3.1}$	$\gamma_{3.2}$	$\gamma_{2.5}$	$\gamma_{2.0}$
5.1	5.6	5.9	6.1	6.0	6.1	6.0	8.7	10.2
56	36	21	11		19	27	37	59

$\gamma_{5.0}$ $\gamma_{5.29}$
4.2 3.89
83 94



$\gamma_{8.4}$
10.8
75

conc.
GAAPRON

STA

+

T

-

ELEV.

929.18
~~929.20~~

15+00

✓

+12

✓

+38

✓

30 DEC. 1964

LT

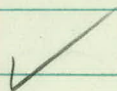
£

RT

29

$\overset{\cdot}{24.2}$	$\overset{\cdot}{23.6}$	$\overset{\cdot}{23.2}$	$\overset{\cdot}{23.1}$	$\overset{\cdot}{23.2}$	$\overset{\cdot}{23.1}$	$\overset{\cdot}{23.0}$	$\overset{\cdot}{23.0}$
50	57	60	61	60	61	62	62
31	22	16	10		14	22	30

$\overset{\cdot}{24.3}$ $\overset{\cdot}{24.1}$ $\overset{\cdot}{24.4}$
 $\rightarrow 4.9$ 5.1 4.8
 45 51 75



$\overset{\cdot}{19.2}$ $\overset{\cdot}{19.7}$ $\overset{\cdot}{21.1}$
 10.0 9.5 8.1
 75 67 44

$\overset{\cdot}{22.4}$	$\overset{\cdot}{22.9}$	$\overset{\cdot}{23.0}$	$\overset{\cdot}{23.1}$	$\overset{\cdot}{23.0}$	$\overset{\cdot}{22.9}$	$\overset{\cdot}{22.8}$	$\overset{\cdot}{22.8}$
5.8	6.3	6.2	6.1	6.2	6.3	6.4	6.4
23	15	9		13	21	31	46

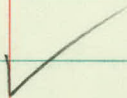
$\overset{\cdot}{24.1}$ $\overset{\cdot}{24.4}$ $\overset{\cdot}{24.7}$ $\overset{\cdot}{24.2}$
 $\rightarrow 5.1$ 4.8 5.0 5.0
 28 48 65 75



$\overset{\cdot}{22.4}$
 6.8
 64
 40

$\overset{\cdot}{22.9}$	$\overset{\cdot}{23.4}$	$\overset{\cdot}{22.5}$	$\overset{\cdot}{22.8}$	$\overset{\cdot}{23.0}$	$\overset{\cdot}{22.9}$	$\overset{\cdot}{22.7}$	$\overset{\cdot}{22.7}$	$\overset{\cdot}{22.7}$
5.3	5.8	6.7	6.4	6.2	6.3	6.5	6.5	6.5
32	24	16	10		13	20	27	44

$\overset{\cdot}{24.1}$ $\overset{\cdot}{23.5}$
 $\rightarrow 5.1$ 5.7
 53 75



$\overset{\cdot}{22.6}$
 6.6
 69
 40

STA

+

T

-

ELEV.

~~929.18~~
~~929.20~~

15+68 ± ENTRANCE RT

✓

4.32 ~~924.72~~ 8.80 ~~920.40~~ 920.37

16+00

✓

30 DEC. 1964

LT

£

RT

30

$\overline{22.6}$	$\overline{22.3}$	$\overline{22.5}$	$\overline{22.8}$	$\overline{22.8}$	$\overline{22.7}$	$\overline{22.7}$
6.6	6.9	6.7	6.4	6.4	6.5	6.5
22	15	11		13	21	29

$\overline{23.4}$	$\overline{23.7}$	$\overline{23.1}$	$\overline{22.6}$
5.8	5.5	6.1	6.6
27	45	62	75

$\overline{22.48}$	$\overline{22.7}$
6.70	6.5
65	54
CONC.	
GA FLOOR	

SPIKE IN PP27.0 RT STA 17+53

$\overline{22.7}$	$\overline{21.9}$	$\overline{22.3}$	$\overline{22.5}$	$\overline{22.6}$	$\overline{22.5}$	$\overline{22.5}$	$\overline{22.5}$	$\overline{22.1}$
2.0	2.8	2.4	2.2	2.1	2.2	2.2	2.2	2.6
24	20	15	10		14	21	27	40

$\overline{23.4}$	$\overline{23.3}$	$\overline{23.0}$
1.3	1.4	1.7
35	48	75

$\overline{20.7}$	$\overline{21.1}$
4.0	3.6
75	60

STA

+

π

-

ELEV.

~~924.70~~
924.72

16+12 ± ENTRANCE Rt.

✓

+23

+32 ± ENTRANCE Lt

✓

KP
WM
DS
FS
PK

LT

4 JAN 1965
SUNNY 30°

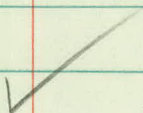
RT

31

23.6	22.9	21.9	22.3	22.5	22.5	22.4	22.0	21.6	21.5
1.1	1.8	2.8	2.4	2.2	2.2	2.3	2.7	3.1	3.19
47	26	21	15	10		13	21	27	37

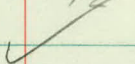
Conc. Apron

23.5	23.9
1.2	0.8
63	75

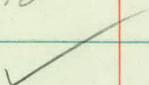


24.4	23.9	22.9	22.5	22.4	22.4	22.2	22.1	21.6	21.66
0.3	0.8	1.8	2.2	2.3	2.3	2.5	2.6	3.1	3.09
75	59	36	20	10		12	20	29	36

Conc. Apron
G4.



23.2	22.9	22.2	22.2	22.3	22.1	21.8	21.7	22.0
1.5	1.8	2.5	2.5	2.4	2.6	2.9	3.0	2.7
70	48	22	10		13	21	25	37



23.3
1.4
75

19.3	19.6	20.7
54	5.1	40
75	68	55

STA

+

T

-

ELEV.

924.70
~~924.72~~

16+44

✓

+75

✓

17+00

✓

4 JAN. 1965

LT

Z

RT

32

21.1	21.8	21.9	22.0	21.8	21.5	21.7	20.7
2.6	2.9	2.8	2.7	2.9	3.2	3.0	4.0
21	15	10		13	19	30	51

22.1	22.9	24.3	24.7
1.6	0.8	0.4	0.0
26	35	57	75

19.0	19.9
5.7	4.8
75	64

22.6	21.4	20.9	21.1	21.3	21.1	20.9	21.2	21.0
2.1	3.3	3.8	3.6	3.4	3.6	3.8	3.5	3.7
27	22	16	11		12	18	21	26

23.2	24.3	24.5
0.9	0.4	0.2
33	55	75

18.9	19.7	20.2	20.9
5.8	5.0	4.2	3.8
75	60	42	37

21.7	20.5	20.2	20.4	20.7	20.6	20.3	20.2	20.6
3.0	4.2	4.5	4.3	4.0	4.1	4.4	4.5	4.1
25	20	15	10		12	19	26	31

22.1	22.8	21.1
1.3	0.9	0.6
32	53	75

18.8	19.1	20.0
5.9	5.6	4.7
75	65	50

STA

+

T

-

ELEV.

~~924.72~~
924.70

17+16

4.41 920.29

+50

✓

18+00

✓

4 JAN. 1965

LT

E

RT

33

TOP MH 23.0 LT

19.2	19.1	19.1	19.2	19.4	19.3	19.1	19.3	19.0
5.5	5.6	5.6	5.5	5.3	5.4	5.6	5.4	5.7
20	18	15	11		12	19	21	26

20.4	22.8	23.7	23.5	✓	18.6	18.9	19.8	20.3
4.3	1.9	1.5	1.2		6.1	5.8	4.9	4.4
25	33	50	75		75	69	50	31

20.9	18.5	18.0	18.1	18.2	18.1	17.9	17.9	20.6
3.8	6.2	6.7	6.4	6.5	6.6	6.8	6.8	4.1
29	22	16	11		12	20	27	34

22.8	23.0	22.8	22.8	✓	19.0	19.2	19.9
1.9	1.7	1.9	1.9		5.7	5.5	4.8
34	49	68	75		75	64	48
							Fe

STA

+

Δ

-

ELEV.

924.70
~~924.72~~

18+39

✓

+59

✓

+65 GUTTER RT

✓

LT

4 JAN. 1965

E

RT

34

18.1	17.4	16.6	17.1	17.3	17.3	17.2	16.8	19.5
6.0	7.3	8.1	7.6	7.4	7.4	7.5	7.9	5.2
26	22	16	10		12	21	28	37

21.4	22.3	23.1
3.3	2.4	1.6
35	51	74

Ho

18.3	19.1
6.4	5.6
75	52

18.3	17.0	16.2	16.4	16.7	16.7	16.4	16.7	18.7
6.4	7.7	8.5	8.3	8.0	8.0	8.3	8.0	6.0
26	23	16	11		13	24	31	36

21.0	22.3	23.0
3.7	2.4	1.7
35	53	74

Ho

16.9	17.3	18.6
7.8	7.4	6.1
75	72	58

18.8	17.2	16.0	16.3	16.5	16.5	16.5	16.6	16.3	16.1
5.9	7.5	8.7	8.4	8.2	8.2	8.2	8.1	8.4	8.6
29	22	16	11		12	27	40	63	75

21.0	22.3	23.1
3.7	2.4	1.6
37	58	75

STA	+	T	-	ELEV.
		924.70		
		924.72		

18+77 E SANDEEN RD RT

✓

+ 89 GUTTER RT

✓

19+00

✓

4 JAN 1965

LT

E

RT

35

18.1	16.2	15.8	16.0	16.2	16.2	16.2	16.2	16.1	16.9	16.1
6.6	8.5	8.9	8.7	8.5	8.5	8.5	8.6	8.8	9.0	
28	22	16	11		12	26	45	69	75	

20.5	21.8	21.6
4.2	2.9	2.1
37	55	75

20.0	17.9	15.9	15.6	15.6	15.8	15.8	15.8	16.3	16.8	16.6
4.7	6.8	8.8	9.1	9.1	8.9	8.9	8.9	8.4	7.9	8.1
38	30	23	16	11		12	24	35	55	75

21.3	21.6
3.4	3.1
61	75

14.2	17.2	15.6	15.2	15.3	15.6	15.5	15.5	15.5	15.2	18.0
65	75	9.1	9.5	9.4	9.1	9.2	9.2	9.2	9.5	6.7
52	32	25	18	11		13	20	23	27	37

18.1
6.0
75

18.6	18.5
6.1	6.2
75	57

STA

+

π

-

ELEV.

~~924.72~~
924.70

19+11

GUTTER LT

✓

+25

± BECKMAN AVE LT.

✓

+40

✓

4 JAN. 1965

LT

✓

RT

36

15.4	15.1	15.0	15.2	15.2	15.2	15.5	15.0	16.1
9.3	9.6	9.7	9.5	9.5	9.5	9.2	9.7	8.6
75	54	29	9		12	22	25-27	30

DITCH

18.7	17.9	18.7
6.0	6.8	6.5
75	62	37

15.4	14.9	14.79	14.9	14.9	14.8	14.9	15.0	14.6
9.3	9.8	9.91	9.8	9.8	9.9	9.8	9.7	10.1
75	51	23	9		12	18	22	25-27

MH

DITCH

16.1	17.5	18.8
8.6	7.2	5.9
100	150	200

18.5	18.5	18.1	16.1
6.2	6.2	6.6	8.6
75	56	36	30

15.2	14.9	14.4	14.3	14.5	14.4	14.3	14.3	14.3	15.1
9.5	9.8	10.3	10.4	10.2	10.3	10.4	10.4	10.4	9.0
75	66	43	25	9		12	19	27	31

19.0	18.7	18.2
5.7	6.0	6.5
75	52	37

STA

+

π

-

ELEV.

924.70
~~924.72~~

19+49

1/2 ENTRANCE RT: GUTTER LT

✓

+60

✓

+79

✓

4 JAN. 1965

LT

≠

RT

37

14.9	14.6	14.2	14.2	14.2	14.1	14.3	16.0	16.7
9.8	10.1	10.5	10.5	10.5	10.6	10.4	9.7	6.0
44	27	18	11		13	26	42	66

14.9	15.0
9.8	9.7
59	75

14.3
5.4
75

15.8	14.8	13.8	13.8	13.8	13.7	13.9	15.4	14.0
8.9	9.9	10.9	10.9	10.9	11.0	10.8	9.3	5.7
41	27	17	12		12	24	32	48

16.8
7.9
75

14.3	14.5
5.4	5.2
75	68

17.0	16.2	13.9	13.3	13.4	13.2	13.4	14.4	18.8
7.7	8.5	10.8	11.4	11.3	11.5	11.3	10.3	5.9
57	36	23	13		14	25	31	47

17.4
7.3
75

14.4	14.1
5.3	5.6
75	64

STA + π - ELEV.

~~924.72~~
924.70

20+00

✓

TP

8.14

~~921.58~~
921.56

11.28

~~913.44~~
913.42

913.42

+01

11.30 910.36

+18 $\pm$ ENTRANCE LT

✓

4 JAN 1965

LT

±

RT

38

16.1	15.6	17.7	12.6	17.8	17.6	17.1	10.8	17.4
8.6	11.1	12.0	12.1	11.9	12.1	12.6	13.9	12.3
34	25	21	13		14	21	24	27
17.2 7.5 47				✓		16.9 7.8 39 Bldg.		
16.1 6.6 75						13.9 10.8 33		

SPIKE WPP 27.0 LT STA 20+03

FL S. END 15" VIT. 23.0 RT

14.0	12.6	17.9	12.1	12.4	12.3	12.0	12.7	12.9
7.6	9.0	9.7	9.5	9.2	9.3	9.6	8.9	8.7
28	24	18	12		10	21	31	37
16.3 5.3 37				✓		GA Floor BT		
17.4 4.2 52						17.7 3.9 61 Ho		

STA + π - ELEV.

~~921.56~~
~~921.58~~

20+54 $\nless$ ENTRANCE RT

✓

+69

13.62 907.94

+75

11.72 909.84

+84 $\nless$ ENTRANCE LT.

✓

39

17.0	16.1	17.1	17.4	17.6
9.1	5.5	4.5	4.2	4.0
29	38	52	67	75

GA FLOW
(DIRT)

TOP MH 24'0 LT.

07.5	04.7	05.7	04.10
19.1	17.4	16.4	17.46
75	64	54	45
FL DRAIN			

STA	+	π	-	ELEV.
-----	---	-------	---	-------

STA	+	π	-	ELEV.
-----	---	-------	---	-------

921.56
~~921.58~~

20+97

14.25 907.31

TP

3.40

913.57
~~913.59~~

11.39

910.17
~~910.19~~

21+00 $\nless$ ENTRANCE RT

✓

+12

✓

5 JAN. 1965

LT

±

RT

40

FL N. END 24' x 32.0 CM 19.0 LT

TOP PR ± STA 21+00

10.0	08.6	09.9	10.1	10.2	10.1	09.8	08.9	08.26
3.6	5.0	3.7	3.5	2.4	3.5	3.8	4.8	5.31
23	20	17	12		11	17	27	35
								COR. GA FLOOR

09.0	09.1	09.1
4.6	4.5	4.5
40	61	75

8.5	9.4	9.6	9.9	10.0	9.9	9.9	7.1	1.1
5.1	4.2	4.0	3.7	3.6	3.7	3.7	6.5	12.5
35	23	18	13		10	21	50	60

08.7	08.5
4.9	5.1
54	75

89.5	92.7	96.7	97.9
22.1	21.4	17.4	15.7
106	90	82	70
H0			

STA

+

T

-

ELEV.

913.57
~~913.57~~

21431

✓

+58

✓

+78

✓

5 JAN 1965

LT

Σ

RT

41

07.2	08.9	09.2	09.2	09.7	09.6	09.0	09.2	06.8
6.4	4.7	4.4	4.4	3.9	4.0	4.6	16.4	16.8
33	20	17	14		11	17	38	49

04.9	05.2	01.6	02.3	03.4
8.7	8.4	22.0	21.3	20.2
51	75	104	82	57
		40		

06.1	08.4	08.9	09.1	09.3	09.2	08.8	03.9	09.5
6.9	5.2	4.7	4.5	4.3	4.4	4.8	9.7	14.1
33	20	17	14		9	16	23	31
								64

03.3	01.7	01.4
10.3	11.9	12.2
43	61	75

03.2	03.6	01.6	08.6	09.0	09.0	08.9	09.1	03.4
10.4	8.0	6.0	5.0	4.6	4.6	4.7	13.9	20.2
40	34	26	16		10	16	30	50

02.2	01.1
11.4	12.5
55	75

00.1	01.0
23.5	22.6
98	75
40	

STA + T - ELEV.

~~913.59~~
913.57

TP 4.30 ~~912.87~~ 912.81 5.02 ~~908.57~~ 908.55 (908.51)

22+00

✓

+26 ≠ ENTRANCE PT.

✓

+38

5.76 907.05

5 JAN 1965

LT

£

RT

42

SPIKE IN PP 27.0 RT STA 23+94

00.6	06.2	07.4	08.3	08.6	08.7	08.6	08.2	01.4	07.1	
12.2	6.6	5.4	4.5	4.2	4.1	4.2	4.6	11.4	15.7	
43	35	28	19	11		11	17	27	36	
99.9		99.5			88.8	99.0	97.6	94.6	94.0	94.5
12.9		13.3			24.0	23.8	20.3	18.2	18.8	18.3
61		75			100	89	75	59	52	46
					40		BT	BT		

06.6	07.9	08.1	08.5	08.5	08.0	02.9	99.1	95.1
6.2	4.9	4.7	4.3	4.3	4.8	9.9	13.7	17.7
33	24	20	11		13	32	47	65
}					}			
00.4		99.6	99.4				91.0	92.6
12.4		13.2	13.4				21.8	20.2
43		67	75				89	78

TOP MH 24.0 LT

STA

+

π

-

ELEV.

~~912.81~~
~~912.87~~

*

22+53

✓

* +46

19.22 893.59

23+00

✓

+12

LT

Z

5 JAN 1965

RT

43

05.5	07.3	08.0	08.2	08.3	08.7	08.0	07.3	07.3
7.3	5.5	4.8	4.6	4.5	4.6	4.8	5.5	9.5
34	25	18	10		7	11	20	35

01.2	02.0	2.1	02.1
11.6	10.8	10.7	10.7
40	52	65	75

92.4	93.6
20.4	19.2
75	69

TOP MH 69.0 RT

06.7	06.6	07.9	08.1	08.1	07.9	07.9	06.8	07.1
6.1	6.3	4.9	4.7	4.7	4.9	4.9	6.0	10.7
34	28-29	18	9		11	18	29	44

07.4	06.0
5.4	4.8
51	75

99.2	99.8	00.6
13.6	13.0	12.2
102	75	58

09.0	0.4	0.2	0.4	0.9	08.0	08.1	08.1	08.0	07.8	06.50	05.23	05.71
3.8	4.0	4.6	5.0	6.0	4.8	4.7	4.7	4.8	5.0	6.31	7.58	7.60
75	61	47	31	27-29	19	9		12	18	25	31	34

DITCH

CB

conc

conc

STA

+

K

-

ELEV.

~~912.81~~
~~912.87~~

23+23

6.17 906.64

+32 ± ENTRANCE LT & RT

✓

+43

6.22 906.59

+56 ± ENTRANCE RT

✓

TP

8.06

~~916.57~~
~~916.63~~

4.30

~~908.51~~
~~908.57~~

(908.51)

5 JAN 1965

LT

£

RT

44

FL S END 12" X 20' CM 25.0 LT

0.3	0.5	0.9	0.0	0.1	0.0	0.9	0.4
3.5	4.3	4.9	4.8	4.7	4.8	5.0	6.4
45	32	18	9		8	17	36
							GA
							FLOOR

1.2	1.1
2.6	2.1
69	75

✓

FL N. END 12" X 20.0 CM 25.0 LT

0.0	0.4	0.8	0.0	0.0	0.0	0.9	0.2	0.3
3.8	5.4	5.0	4.8	4.8	4.8	5.0	5.6	5.5
33	26-28	20	10		8	17	24	37
	DITCH							GA
								FLOOR

10.3	11.3
2.5	1.5
44	75

✓

SPIKE IN PP 27.0 RT STA 23+94

STA

+

π

-

ELEV.

916.57
~~916.63~~

24+00

✓

+34 ± ENTRANCE RT

✓

+50 ± ENTRANCE RT.

✓

5 JAN. 1965

LT

✓

RT

45

11.6	07.9	06.1	08.2	08.2	08.2	08.9	07.4	06.1
5.0	8.7	8.5	8.4	8.4	8.4	8.7	9.2	10.5
40	26-28	20	16		8	23	36	35

DITCH

13.1
3.5
62

13.5
3.1
75

04.7
11.9
75

12.3	08.2	08.3	08.4	08.4	08.2	08.0	06.3	04.77
4.3	8.4	8.3	8.2	8.2	8.4	8.6	10.3	11.80
49	25-26	19	15		9	27	49	75

DITCH

conc.

13.4
3.2
57

13.7
2.9
75

12.6	06.6	06.6	06.7	06.5	08.2	08.2	08.4
4.0	8.1	8.0	7.9	8.1	8.4	8.4	8.2
40		18	15		12	27	53

25-26

GA

DITCH

13.6
3.1
60

13.6
3.1
75

STA + K - ELEV.

916.57
~~916.63~~

24+84

✓

25+00

+17

7.76 908.81

+36 ± ENTRANCE RT.

✓

5 JAN 1965

LT

- E

RT

46

14.1	13.3	9.2	9.0	8.7	8.4	8.4	8.8	8.1
2.5	3.3	7.4	7.6	7.9	8.2	8.2	7.8	8.5
63	41	24-25	15		14	29	57	64
DITCH								

14.1
2.5
75

8.3
8.3
75

14.5	12.2	13.3	9.5	9.1	8.8	8.4	8.4	8.6	8.7
2.1	2.4	3.3	7.1	7.5	7.8	8.2	8.2	8.0	7.9
75	59	40	23-24	14		15	23	29	41
DITCH									

GA

conc. entrance Slab 42.0 RT

14.5	13.4	9.8	9.0	9.0	8.5	8.6	8.8	8.8
2.1	3.2	6.8	7.6	7.6	8.1	8.0	7.8	7.8
57	38	23	13		17	36	57	64

16.1
1.5
75

STA

+

K

-

ELEV.

~~916.57~~
~~916.63~~

+

25+57

7.70 908.87

+450

✓

+85

✓

BM

7.07

~~916.91~~~~916.98~~

6.72

~~909.85~~~~909.91~~

(909.84)

LT

5 JAN. 1965

RT

47

TOP Lower step 29.0 RT.

13.6	9.7	9.7	9.7	9.7	9.6	9.6	9.7	9.3
3.0	6.9	7.5	7.4	7.5	8.0	8.0	7.9	7.3
38	22	13	7		15	28	35	38

14.7 15.3
1.9 1.3
59 75

9.8 9.8 9.8
9.8 9.8 7.8
75 66 63

14.0	13.6	9.6	9.7	9.1	9.5	9.7	10.1	9.5	9.5
2.6	3.0	7.0	7.3	7.5	8.1	7.9	6.5	7.1	8.1
60	43	24	15		15	20	26	46	70

14.64
1.93
75
conc.

9.0 9.7
9.6 9.4
75 72

RR SARE IN PP S.E. COR STOWE AVE
JOHANNA BLVD

STA + π - ELEV.

916.91
~~916.98~~

26+00 GUTTER LINE LT

+11 $\frac{1}{2}$ ENTRANCE RT.

+22 $\frac{1}{2}$ STOWE AVE

5 JAN 1965

LT

E

RT

48

9.8	9.4	9.3	9.2	9.0	8.4	8.3	7.4	7.0
7.1	7.5	7.6	7.7	7.9	8.5	8.6	9.5	9.9
40	23	14	6		14	32	58	75

10.4 11.1
6.5 5.8
61 75

10.7	9.8	9.1	9.1	8.9	8.3	8.1	7.19
6.2	7.3	7.8	7.8	8.0	8.6	8.8	9.72
75	51	26	6		14	34	54

conc. GA Apron

11.8	10.6	9.6	8.81	9.0	8.7	8.1	7.9	7.15
5.1	6.3	7.4	8.10	7.9	8.2	8.8	9.0	9.76
100	75	50	24	7		14	36	52
			MH					GA

13.0 14.0 14.60 15.2
3.9 2.9 2.31 1.7
125 150 173 200
MH

STA + π - ELEV.

~~916.91~~
~~916.98~~

26+42 $\frac{1}{2}$ ENTRANCE RT & GUTTER LT

+50

✓

27+00

✓

TP

12.83

~~904.08~~

~~904.15~~

7.52 917.36

909.84

13.28

904.08

904.08

JOAN 1965

LT

✗

RT

49

10.0	9.3	8.0	8.3	8.5	8.2	8.2	7.6	7.1	6.9
6.9	7.6	7.9	8.6	8.4	8.7	9.4	9.3	9.8	10.0
75	59	38	24	8	✓	13	29	50	75

11.7	10.0	8.1	8.1	8.2	7.1	7.2	7.4	7.1	7.1
5.2	6.9	7.8	8.8	8.7	9.0	9.7	9.5	9.8	9.8
37	37	29	21	7		13	18	46	69

TOP WALL

BOTTOM WALL

13.1	12.1
3.8	1.8
50	62

6.5
10.0
75

11.0	10.3	10.6	10.2	10.1	10.5	10.0	10.5	10.1
5.9	9.6	10.3	10.7	10.8	11.4	10.9	10.4	10.2
34	20	13	6		13	19	23	33

14.4	16.1	16.9
2.5	0.8	0.0
58	69	75

10.0	10.3
10.9	10.6
75	47

S.W. COR. LOWER STEP 23.0 RT STA 27+52

RR. SPIKE IN PP. SECOR. STOWE AVE. BWD

SW. COR. LOWER STEP 23.0 RT STA 27+52

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		917.36		
--	--	--------	--	--

27+30				
-------	--	--	--	--

✓				
---	--	--	--	--

+52	±	ENTRANCE	LT	
-----	---	----------	----	--

✓				
---	--	--	--	--

+64				
-----	--	--	--	--

✓				
---	--	--	--	--

5.72	909.80	13.28	904.08	904.08
------	--------	-------	--------	--------

LT

6 JAN. 1965

RT

50

9.2	06.1	04.5	05.2	05.1	04.6	04.5	05.6
8.2	11.3	12.9	12.2	12.3	12.8	12.9	11.8
35	20	14	8		12	18	23

11.9	12.76	07.22		05.9	05.1
5.5	5.10	10.14		11.5	11.3
49	57	57		75	43

TOPWALL BOTTOMWALL

06.20	05.05	04.5	04.4	04.4	04.0	04.07	05.30
11.16	12.31	12.9	13.0	13.0	13.4	13.29	12.06
52	27	18	9		12	21	24
conc	conc					conc.	conc

TOP STEP

06.43	06.59
10.53	8.77
68	111
conc.	conc. GA

APRON

05.1	05.4	05.1
11.7	11.6	11.7
75	54	30

07.1	05.6	04.4	04.0	03.9	03.5	03.4	04.6	05.6
9.7	11.8	13.0	13.4	13.5	13.9	14.0	12.8	11.8
41	27	20	10		12	18	22	32

10.1	12.1		05.8	05.8	05.31
7.3	4.7		11.6	11.6	11.99
56	75		75	53	47

conc. SW

SW COR LOWER STEP 23' RT STA 274.52

STA

+

π

-

ELEV.

909.80

28400

✓

+40

✓

+60 ± ENTRANCE RT

✓

LT

Z

JUAN. 1965

RT

51

0 ^{5.9}	0 ^{3.8}	0 ^{2.9}	0 ^{2.8}	0 ^{2.8}	0 ^{2.3}	0 ^{2.2}	0 ^{3.8}
3.9	6.0	6.9	7.0	7.0	7.5	7.6	6.0
35	19	14	10		12	18	23

0 ^{7.4}	0 ^{9.0}	0 ^{9.8}		0 ^{6.9}	0 ^{5.7}	0 ^{5.1}
2.4	0.8	0.0		2.9	4.1	4.7
46	60	75		71	52	32

0 ^{4.3}	0 ^{2.8}	0 ^{1.7}	0 ^{1.6}	0 ^{1.6}	0 ^{1.1}	0 ^{1.0}	0 ^{1.5}	0 ^{1.5}
5.5	7.0	8.1	8.2	8.2	8.7	8.8	8.3	8.3
32	19	12	9		13	18	24	47

0 ^{6.0}	0 ^{2.3}	0 ^{9.9}		0 ^{2.5}	0 ^{2.0}	0 ^{2.12}
3.8	2.5	1.9		7.3	7.8	7.68
44	58	75		75	64	58

0 ^{6.2}	0 ^{4.4}	0 ^{2.3}	0 ^{1.0}	0 ^{1.0}	0 ^{1.1}	0 ^{0.5}	0 ^{0.8}	0 ^{1.04}
3.6	5.4	7.5	8.8	8.8	8.7	9.3	9.0	8.76
51	36	20	13	9		13	45	69

0 ^{7.3}	0 ^{7.5}
2.5	2.3
67	75

 CORR. GA
 APRON

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		909.80		
--	--	--------	--	--

28+82				
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✓				
---	--	--	--	--

9.72	909.56	9.96	899.84	
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29+00				
-------	--	--	--	--

✓				
---	--	--	--	--

LT

±

RT

52

01.1	01.4	00.1	00.2	00.4	99.9	99.8	00.5	01.2
6.7	8.4	9.7	9.6	9.4	9.9	10.0	9.3	8.6
35	20	13	9		13	18	24	41

05.0	06.8
4.8	3.0
54	75

01.11
8.69
62
40
conc.

TOP PK ± STA 29400

299.8

03.0	01.0	99.9	99.7	99.6	99.4	99.4	00.3
6.6	8.6	9.7	9.9	10.0	10.2	10.2	9.3
40	23	15	10		14	19	24

04.4	05.8
5.2	3.8
58	75

00.4	00.9
9.2	8.7
55	41
Ho	

STA + π - ELEV.

909.56

29+13

✓

+50 $\neq$ LAKE LAKE LT

✓

+75

✓

LT

E

6 JAN 1965

RT

53

01.9	99.9	99.7	99.3	99.5	99.0	99.6	99.3
7.7	9.7	10.4	10.3	10.1	10.6	10.6	10.3
33	19	16	10		13	18	24

02.6	03.5	02.9	04.6
7.0	6.1	6.7	5.0
48	59	61	80

LAKE
LANE

00.6	00.7
9.0	9.4
49	39

03.3	00.0	98.3	98.1	98.4	98.3	98.7	99.1	98.9
6.3	9.6	11.3	11.5	11.2	11.3	11.4	10.5	10.7
77	44	23	12		12	18	23	44

05.3	07.1	09.6
4.1	1.9	0.0
100	125	150

98.7	98.7
11.4	10.9
75	69

00.6	99.7	99.0	97.7	97.1	97.6	97.4	97.3	98.4	98.3
9.0	9.9	11.6	12.4	12.5	12.0	12.0	12.3	11.2	11.3
60	48	33	24	13		13	20	25	41

00.9
8.7
71

E DRIVE

98.8	98.4	97.1
25.8	19.2	12.5
77	68	55

BLDG

STA

+

π

-

Elev.

909.56

TP

2.66

900.90

11.30

898.26

(898.24)

30+00

✓

+25

✓

+50

✓

LT

E

6 JAN. 1965

RT

54

RR SPIKE IN 24" OAK 46.0 RT STA 30+02

99.1	98.3	97.0	96.0	96.6	96.9	97.0	97.7	96.9
1.8	2.6	3.9	4.9	4.3	4.0	3.9	3.2	4.0
59	40	21	13		11	21	26	44

00.6
0.3
75

81.2 88.8
19.7 12.1
75 60

99.5	97.6	95.6	94.9	95.7	96.2	96.2	96.9	96.5
1.4	3.3	5.3	6.0	5.2	4.7	4.7	4.0	4.4
52	35	20	14		16	23	28	41

00.4 00.9
0.5 0.0
66 75

76.4 77.3 72.5 77.2 91.1
24.5 21.6 18.4 13.7 9.8
84 73 60 54 47
LAKE

00.1	98.6	96.6	94.8	94.0	94.8	95.3	95.6	95.9	95.1	90.1
0.8	2.3	4.3	6.1	6.9	6.1	5.6	5.3	5.0	5.8	10.8
57	40	27	18	13		10	21	26	37	46

00.6
0.3
75

76.4 80.3 80.3
24.5 20.6 20.6
LAKE = 6.9 60 56

STA	+	π	-	Elev.
-----	---	-------	---	-------

		900.90		
--	--	--------	--	--

30+75				
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✓				
---	--	--	--	--

+79				
-----	--	--	--	--

		5.99	894.91	
--	--	------	--------	--

31+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+56				
-----	--	--	--	--

LT

6 JAN. 1965

RT

55

98.5	95.7	94.3	93.3	91.0	91.6	91.6	89.9	86.1
2.4	5.2	6.6	7.6	6.9	6.3	6.3	11.0	14.8
37	25	17	14		14	27	35	44

00.0	00.9
0.9	0.0
54	75

76.4	79.9	87.6
24.5	21.0	18.3
65	55	48

LAKE

TOP M14 18.0 LT

00.3	99.2	94.3	92.7	93.3	93.7	91.0	91.0	93.4
0.6	1.7	6.6	8.2	7.6	7.2	6.9	6.9	7.5
47	36	18	13		14	20	24	29

00.6

0.4

56

Ho

76.4	81.0	81.7	87.3	91.2
24.5	19.9	19.2	13.6	9.7
53	48	44	38	33

LAKE

91.5	91.0	92.2	91.5	91.8
3.4	4.9	8.7	9.4	9.1
48	36	19	14	
Ho				

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		900.90		
--	--	--------	--	--

31+74	$\neq$	ALLEY	Lt	
-------	--------	-------	----	--

+90				
-----	--	--	--	--

32+00				
-------	--	--	--	--

+50				
-----	--	--	--	--

TP	5.42	894.27	12.05	888.85
----	------	--------	-------	--------

+50				
-----	--	--	--	--

6 JAN. 1965

LT

±

RT

56

96.2	94.6	92.5	90.9	89.0	91.4
4.7	6.3	8.4	10.0	9.9	9.5
66	48	30	15	10	

97.1	95.2	93.3	90.5	90.6	91.0
3.8	5.7	9.9	10.4	10.3	9.9
46	30	19	15	10	
Ho	TOP MH				

96.7	95.1	91.6	90.2	90.8
4.2	5.8	9.3	10.7	10.1
49	31	19	15	
Ho				

99.2	98.9	91.9	90.9	89.5	89.9
1.7	2.0	9.0	10.0	11.4	11.0
45	37	24	20	15	

TOP PK ± STA 33+00

STA	+	π	-	Elev.
-----	---	-------	---	-------

		894.27		
--	--	--------	--	--

31+56				
-------	--	--	--	--

+74				
-----	--	--	--	--

+90				
-----	--	--	--	--

32+00				
-------	--	--	--	--

+50				
-----	--	--	--	--

TP	2.60	891.45	5.42	888.85
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LT

±

6 JAN 1965

RT

57

92.1	91.3	91.4	92.8	90.4	16.4
2.2	3.0	6.9	11.5	13.9	17.9
18	22	26	38	53	64

LAKE

91.4	91.1	92.7	90.8	16.4
2.9	3.2	11.6	13.5	17.9
18	24	39	50	68

LAKE

90.9	89.9	93.6	90.9	16.4
3.4	4.4	10.7	13.4	17.9
16	23	35	52	73

LAKE

90.9	89.8	92.9	91.4	16.4
3.4	4.5	11.4	12.9	17.9
16	23	37	52	74

LAKE

89.7	89.0	93.1	90.3	16.4
4.6	5.3	11.2	14.0	17.9
13	21	32	61	75

LAKE

TOP PK ± STA 33+00

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		891.45		
--	--	--------	--	--

33+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

34+00				
-------	--	--	--	--

✓				
---	--	--	--	--

LT

E

7 JAN 1965
FOGGY
360

RT

58

96.2	90.3	88.7	88.7	88.9	88.8	88.8	88.8
+4.7	1.2	2.8	2.8	2.6	2.7	2.7	2.7
34	23	18	13		6	14	19

90.7

+9.2
52

76.4	78.6	83.9
15.1	12.9	7.6
71	60	33

LAKE

95.3	89.3	88.0	88.1	88.3	88.2	88.1	87.7	81.4
+3.8	3.2	3.5	3.4	3.2	3.3	3.4	3.8	10.1
39	23	19	15		5	12	18	29

TOE

96.9

+7.4
55
40

76.4	77.7	79.7
15.1	13.8	11.8
55	45	42

LAKE

90.5	91.2	87.5	87.7	87.7	87.7	87.0	79.5
+11.0	+9.7	4.0	3.8	3.8	3.8	4.5	12.0
60	52	18		5	11	17	29

76.4	78.2
15.1	13.3
46	32

LAKE

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		891.45		
--	--	--------	--	--

34+50				
-------	--	--	--	--

✓				
---	--	--	--	--

+75				
-----	--	--	--	--

		5.79	885.66	
--	--	------	--------	--

+94				
-----	--	--	--	--

		12.02	879.43	
--	--	-------	--------	--

35+00				
-------	--	--	--	--

✓				
---	--	--	--	--

7 JAN. 1965

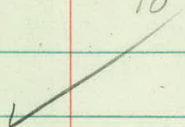
LT

£

RT

59

903.5	91.2	99.0	97.0	97.2	97.1	95.7	90.9	76.2
+12.0	+9.7	2.5	4.5	4.3	4.4	5.8	10.6	13.3
66	48	26	17		10	21	28	39

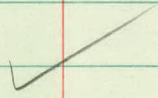


76.4
15.1
50
LAKE

TOP MH 24.0 LT

FL END 24" CM 27.0 RT

903.6	91.9	99.1	96.7	96.7	96.5	96.5	94.6	93.6
+12.1	+7.4	3.4	4.8	4.8	5.0	5.0	6.9	8.1
55	44	25	16		8	17	20	27



95.6
+14.1
59

96.5
+15.0
68
Ho

76.4
15.1
53
LAKE

79.6
11.9
45

91.0
10.5
31

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		891.45		
--	--	--------	--	--

35457				
-------	--	--	--	--

✓				
---	--	--	--	--

+75				
-----	--	--	--	--

		5.03	886.42	
--	--	------	--------	--

+87	£ WASHOUT	LT		
-----	-----------	----	--	--

✓				
---	--	--	--	--

+94				
-----	--	--	--	--

		7.94	883.51	
--	--	------	--------	--

7 JAN 1965

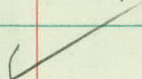
LT

£

RT

60

84.1	81.5	87.1	87.1	86.6	86.5	86.3	81.1	79.0
+12.6	+10.0	4.4	4.8	4.9	5.0	5.2	10.4	12.5
65	54	25	18		7	13	28	33



76.1	77.1
15.1	14.4
54	44

LAKE

TOP MH 25.0 LT

84.2	80.1	87.1	86.1	86.5	86.4	86.2	79.4	77.3
+2.7	1.4	4.4	5.1	5.0	5.1	5.3	12.1	14.2
60	37	26	19		7	21	35	39



86.1
+5.2
75

76.1
15.1
50

LAKE

FL W. END 24" CM 20.0 LT

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		891.45		
--	--	--------	--	--

35+95				
-------	--	--	--	--

	9.40	882.05		
--	------	--------	--	--

+98				
-----	--	--	--	--

	4.99	886.46		
--	------	--------	--	--

36+00				
-------	--	--	--	--

TP				
----	--	--	--	--

	3.84			
--	------	--	--	--

		890.22		
--	--	--------	--	--

	5.07			
--	------	--	--	--

		886.38		
--	--	--------	--	--

36+50				
-------	--	--	--	--

LT

≠

TUAN. 1965

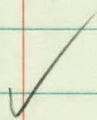
RT

61

Fl E. END 24" CM. 26.0 RT

E. END 18" SCP APRON 27.0 LT

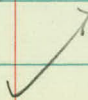
902.5	916.3	928.1	946.7	966.5	966.5	959.9	949.7	966.5
+11.0	+4.8	3.4	4.8	5.0	5.0	5.6	11.8	15.0
61	42	26	19		8	22	30	33



966.5
15.1
49
LAKE

TOP PK ≠ STA 37+00

901.8	911.6	928.5	948.0	966.7	966.4	966.3	966.3	981.0	992.2	991.1	966.2
+11.6	+4.4	0.7	2.2	3.5	3.8	3.9	3.9	9.2	11.0	13.1	14.0
63	36	30	22	17				20	28	35	38



LAKE

STA + T - ELEV.

890.22

36+73

1.06

889.16

~~889.18~~

37+00

✓

TP

1.75

887.05

4.90

885.32

885.30

BM

5.38

881.62

881.82

TP

6.42

891.72

885.30

2.56

889.16

LT

≠

7 JAN 1965

RT

0 62

TOP LOWER STEP 29.0 LT. (CONC.)

95.4	95.2	98.2	96.6	96.4	96.0	94.6	90.2	99.8
+5.2	+5.0	2.0	3.6	3.8	4.2	5.6	10.0	10.4
39	37	25	17		9	18	24	33

BOTTOM
WALL

98.4	98.7
+8.2	+8.5
39	50

TOP WALL

96.2	98.1
14.0	12.1
43	36

LAKE

TOP PK ≠ STA 41+00

TOP SUR. CONTROL STRUCTURE

TOP PK ≠ STA 41+00

TOP LOWER STEP 29.0 LT STA 36+73

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		891.72		
--	--	--------	--	--

37+50				
-------	--	--	--	--

+62				
-----	--	--	--	--

		5.74	885.98	
--	--	------	--------	--

+74				
-----	--	--	--	--

		5.42	886.30	
--	--	------	--------	--

+77				
-----	--	--	--	--

		7.24	884.48	
--	--	------	--------	--

+77				
-----	--	--	--	--

		7.09	884.63	
--	--	------	--------	--

LT

7 JAN, 1965

RT

63

94.2	86.6	86.7	86.0	85.1	84.8	80.4	79.5
+2.5	5.1	5.5	5.7	6.0	6.9	11.3	12.2
43	26	18		10	19	26	35

98.9	90.7
+7.1	+9.0
57	63

15.6	17.4
16.1	14.3
48	38

LAKE

TOP E. END 3'0 SIDEWALK 18.0 TO 24.0 LT

TOP E. END 3'0 SIDEWALK 18.0 TO 23.0 LT

FL W. END 18" CM 20.0 LT

FL E. END 15" CM 22.0 LT

STA

+

K

-

ELEV.

891.72

37+79

13.65 878.07

38+00

✓

✓

+36

5.28 886.44

+50

LT

JUAN 1965

RT

64

FL E. END 18" X 52.0 CM 32.0 RT

86.6	85.8	86.3	85.8	85.5	85.5	84.7	79.5
5.1	5.9	5.4	5.9	6.2	6.2	7.0	12.2
24	20-22	17		9	14	23	35

DITCH

86.9	91.3	91.4	92.7
2.8	0.4	0.3	+1.0
31	32	37	38

BOTTOM TOP WALL
WALL

01.0	94.1
+9.3	+2.4
55	40

85.6	86.7	89.1
16.1	15.0	12.6
56	48	43

LAKE

TOP 12" CONC. GUTTER 21.0 LT

04.8	01.7	90.7	90.8	90.1	85.7	85.5	85.2	84.5	80.3	78.3	75.6
+13.1	+10.0	+4.0	0.9	5.3	6.0	6.2	6.5	7.2	11.4	13.4	16.1
55	45	33	27	19	15		8	19	26	37	61

LAKE

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		891.72		
--	--	--------	--	--

39+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+13				
-----	--	--	--	--

		9.69	882.03	
--	--	------	--------	--

+14				
-----	--	--	--	--

		7.62	884.10	
--	--	------	--------	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

LT

70 AN. 1965

RT

65

93.7	92.8	96.5	95.6	96.5	95.3	95.4	94.1	90.0
+2.0	2.9	5.2	6.1	6.2	6.4	6.3	7.6	11.7
34	27	22	18		8	12	18	25

98.6	92.0	90.1	11.4
+6.9	+10.3	+18.4	+19.7
39	45	59	67

95.6	96.8	98.6
16.1	14.9	13.1
51	40	35

LAKE

FL E, END 15" CM 23.0 RT

FL. W. END 15" CM 17.0 LT

91.5	94.6	98.7	97.0	95.8	95.5	95.4	94.6	97.5	97.4
+9.8	+2.9	3.0	4.7	5.9	6.2	6.3	7.1	9.2	12.3
41	34	23	19	14		9	19	24	27

99.2	13.5	914.2
+17.5	+21.8	+22.5
49	58	67

95.6	97.8
16.1	13.9
57	41

LAKE

STA	+	K	-	ELEV.
-----	---	---	---	-------

		891.72		
--	--	--------	--	--

39+55				
-------	--	--	--	--

40+00				
-------	--	--	--	--

✓				
---	--	--	--	--

5.50	890.80	6.42	885.30	885.30
------	--------	------	--------	--------

+25				
-----	--	--	--	--

✓				
---	--	--	--	--

LT

7 JAN. 1965

RT

66

TOPE END 3.0 SIDEWALK 18.0 - 20.0 LT

91.5	90.3	91.7	95.8	95.5	95.3	93.9	90.0	96.9
+7.8	1.4	4.5	5.9	6.2	6.4	7.8	11.7	14.8
49	26	21	15		9	26	29	46

910.7	14.3
+19.0	+22.6
61	77

75.6
16.1
47
LAKE

TOP PR & STA 41+00

99.0	90.5	91.6	95.8	95.4	95.4	95.1	90.4	99.4
+8.2	0.3	3.2	5.0	5.4	5.4	5.7	10.4	11.4
39	30	23	16		10	23	29	40

906.9	11.4	13.1
+16.1	+20.6	+22.3
50	55	75

76.0
14.8
61
LAKE

STA

+

π

-

ELEV.

890.80

*

40+63

5.20 885.60

2

*
41+50

✓

+75

✓

RP
FS
WM
DS
PK

LT

8 JAN. 1965
CLOUDY - SNOW
10° RT

67

TOP MH 25.0 LT

45.6	49.4	46.7	46.0	45.8	45.6	45.0	44.0
14.8	1.4	4.1	4.8	5.0	5.2	5.8	6.8
49	33	24	16		9	16	25

00.0 11.4 ✓
→ +9.2 +20.6
56 69

76.7 78.9 79.8
14.1 11.9 11.0
64 43 31
LAKE

47.5	46.1	45.3	45.4	45.6	45.3	44.9	44.1	40.3
3.3	4.7	5.5	5.4	5.2	5.5	5.9	6.7	10.5
38	31	25	18		9	17	22	28

49.6
→ 2.2
67

76.7 77.2
14.1 13.6
65 54
LAKE

STA	+	π	-	Elev.
-----	---	-------	---	-------

		890.80		
--	--	--------	--	--

41400				
-------	--	--	--	--

✓				
+50	ENTRANCE	LT		

✓				
BM	4.04	886.75	8.09	882.71

BM				
----	--	--	--	--

			5.06	881.69
				881.82

8 JAN 1965

LT

±

RT

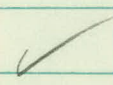
68

46.5 ³	46.1	45.5	45.3	44.8	44.0	43.5	40.0
3.27	4.7	5.3	5.5	6.0	6.8	7.3	10.8
27	27	18		11	16	21	29

TOP WALL

BOTTOM WALL

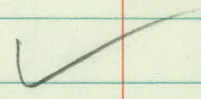
47.8	46.7	48.1
3.0	2.6	2.7
42	63	75



76.7	77.1	78.8
14.1	13.7	12.0
71	60	48

LAKE

45.1	44.8	45.0	44.6	43.7	40.6	38.7
5.7	6.0	5.8	6.2	7.1	10.2	12.1
40	16		15	21	33	50



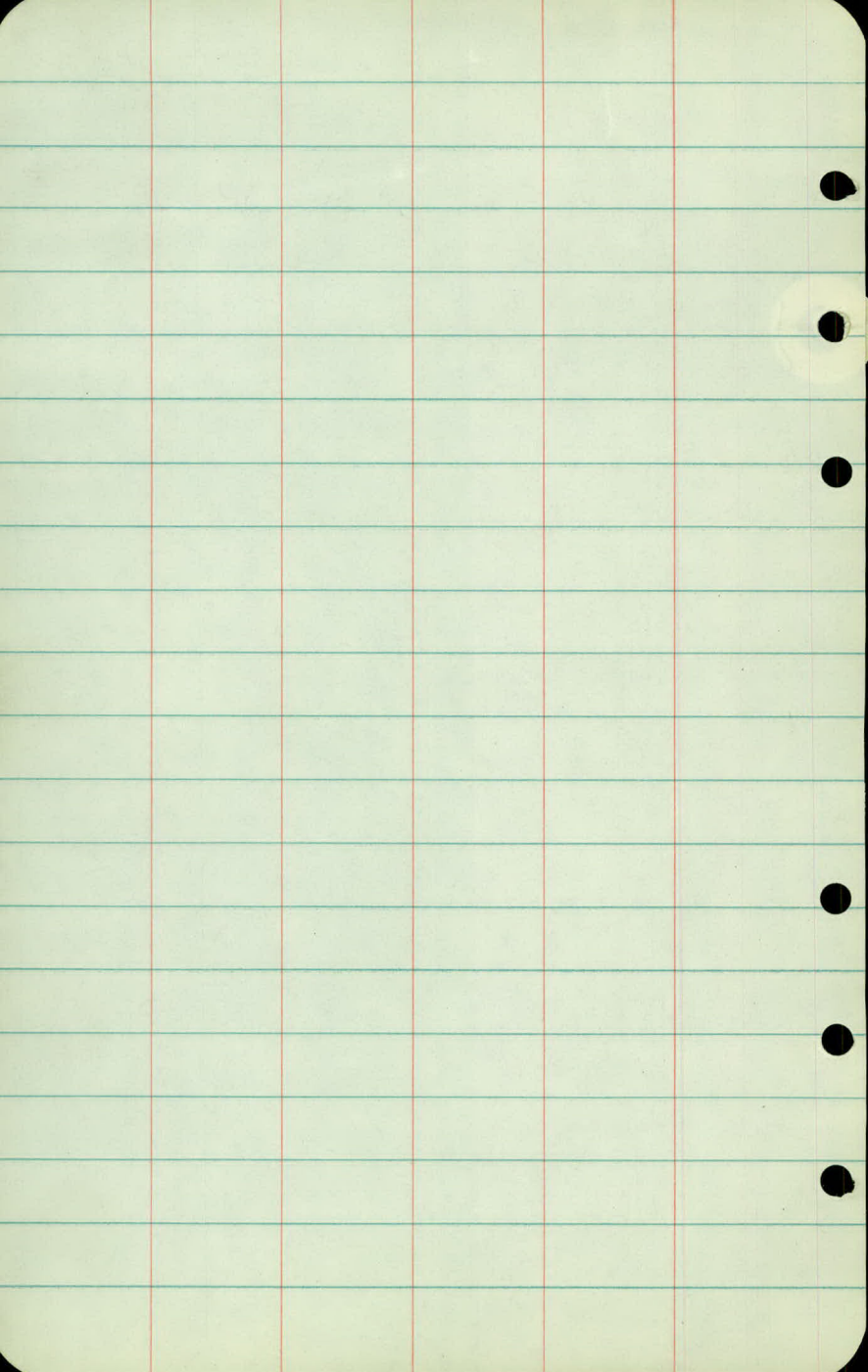
76.7
14.1
74

LAKE

SPIKE IN 48" COTT. S.E. COR. CO. RDE ±

LAKE JOHANNA BAY.

TOP S.W. COR CONTROL STRUCTURE



Feb. 8, 1965

69

Property Line Profile

30' Rt

Sta	+	π	-	Elev.
BM	2.21	910.72		(908.51)
21+00			2.5	
+12			2.8	
+24			8.4	
+41			13.0	
+72			13.3	
22+00			13.5	
+08			11.9	
+18			9.0	
+31			8.0	
+44			6.9	
+66			5.8	6-504.4
+83			6.3	
23+00			4.9	
+07			3.7	
24+00			2.53	908.19

Feb 8, 1965

70

Spike in PP 27' RT Sta 23+94

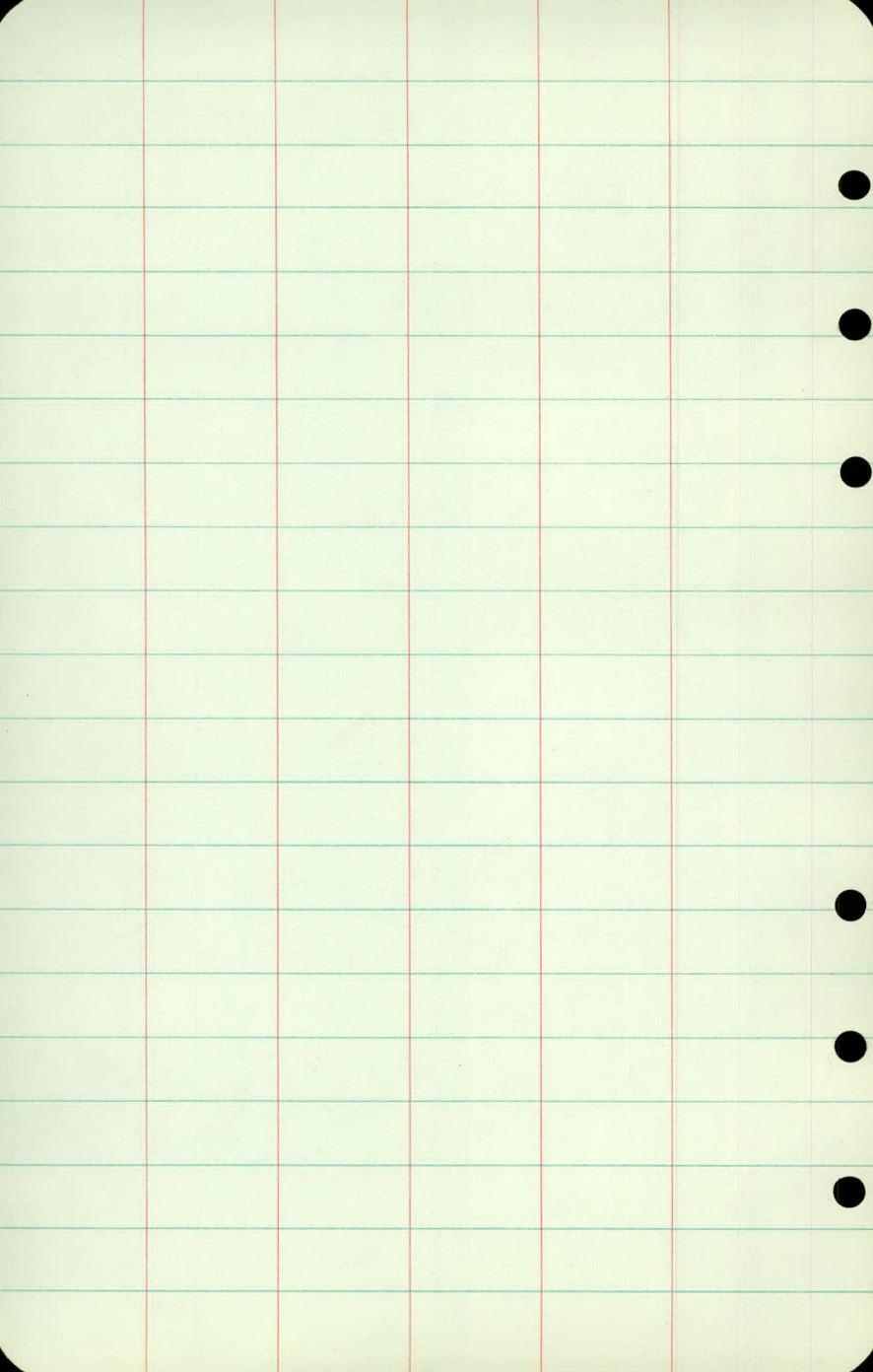
SOUTH SIDE OF GARAGE,

NORTH " " "

BLACKTOP DRIVE SO. SIDE

" " NO. SIDE

TOP WALL BY WALK



Feb. 9, 1965

74

Sidewalk & Gutter Elevations

Sta + π - Elev.

BM 6.50 932.86 926.36

0+28 S. Edge Sidewalk

✓

BM 4.46 928.40

Sewer Crossing S. Side of
Mrs. Kenneth Nelson Property

22+36 ✓ Force Main Sewer Crossing

0-09 ✓ 18' R_T = Sanitary MH

FL to top Casting = 12.3

9" Casting

Eccentric Cone

4 Adjusting Rings

±

x-72

Top Mont ± Co Rd "D" & Lake Johanna Blvd.

26.34	26.32	26.29	26.34	26.50	26.06	25.9
6.52	6.54	6.57	6.52	6.36	6.8	7.0
50	75	100	125	143	150	200

25.1	25.6
7.8	7.30
295	250

Top Hyd 200' Rt Sta 0+20

Sta	+	π	-	Elev.
B.M	4.94	932.05		927.11 ?

1+82.5 N. Edge Walk

✓

BM			A.14	927.91	927.91
----	--	--	------	--------	--------

BM	6.75	889.45			882.71
----	------	--------	--	--	--------

41	$\frac{1}{2}$		A.15	885.31	885.30
----	---------------	--	------	--------	--------

+50

✓

FK
WM
WS

Feb 15, 1965

x-73

Top Hyd SW Cor Co Rd "D" & L.J. Blvd

26.95	27.24	27.64	28.02	28.25
5.10	4.81	4.41	4.03	3.30
33	48.6	65.0	82.5	98.6

28.95
3.10
103.8

N.E. Cor Lower step H₀ #3151 L.J. Blvd.

Spike in 36" CoH. Bt. Sta

85.0

4.3	4.4	4.7	4.6	4.4	4.9	5.0	7.0	10.2
44	27	18	12		13	17	27	43

4.1
63

13.4
80

12.4
67

Sta + π - Elev.

42 ok 889.46

✓

+50

✓

43 Along Aprix $\pm$ Co Rd E

✓

BM 6.76 882.70 (882.71)

Feb 15, 1965
RT X-74

8A.7

0.6

5.4 5.4 5.3 5.1 4.7 5.0 5.4 5.5 7.9
47 27 18 12 13 20 25 37

→ 5.3
75

12.7 12.5 8.9
95 75 48

8A.6

5.4 8.8 5.4 5.2 4.85 5.0 5.3 5.7 7.3
29 25 20 13 15 21 29 47

→ 5.8 5.7
49 69

13.3 12.3 9.4
95 82 60

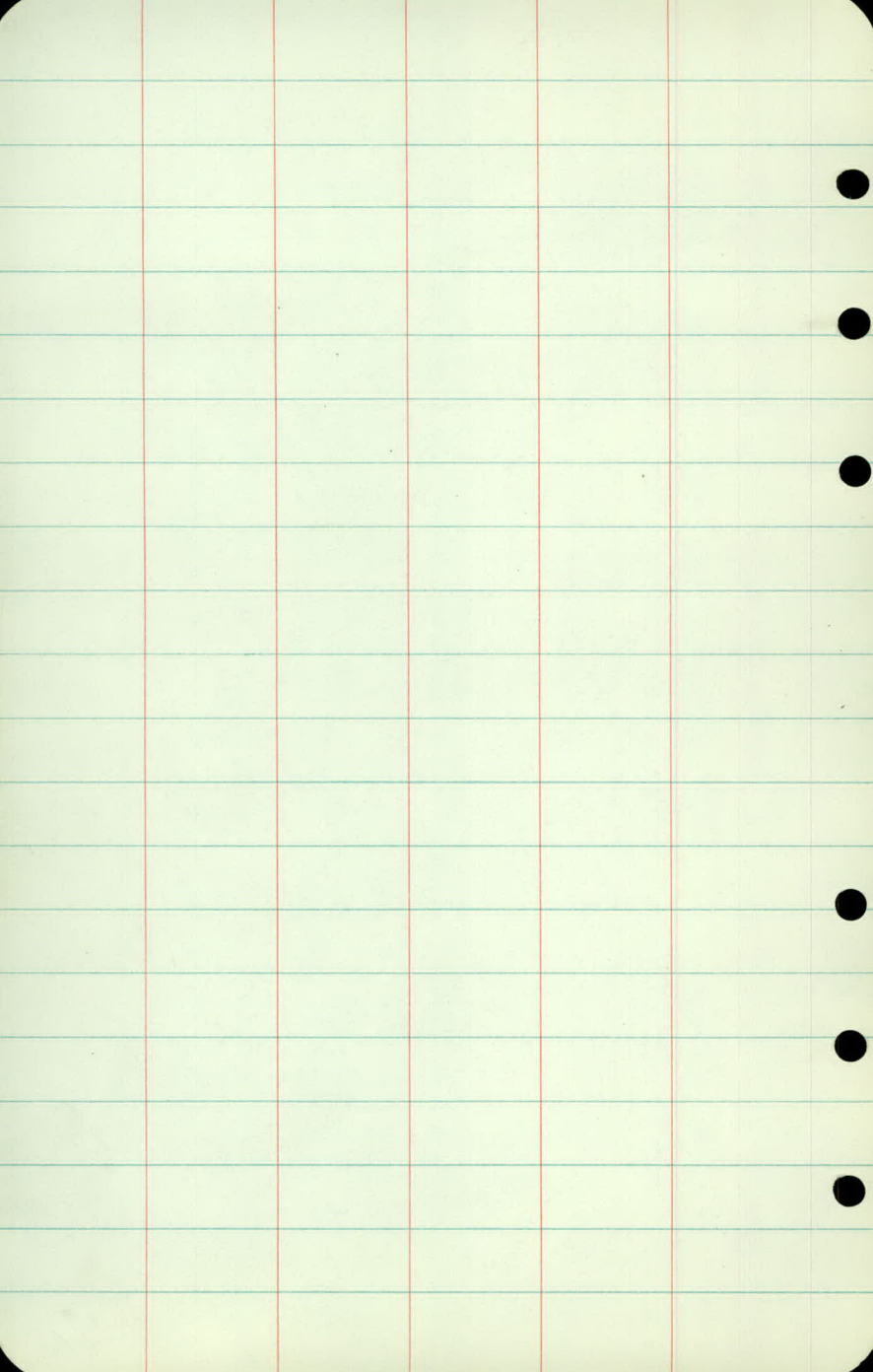
8A.4

3.0 4.6 5.4 5.2 5.0 5.2 5.3 5.2 7.0
100 65 25 19 15 20 27 50

→ 1.5 0.2
127 150

8.9
72

Spike in 36" Coll RT sta



EX
EX
GB

July 29, 1964 X-75
1

JOHANNA BLVD. ~~WEST~~ ^{NORTH}

X-Sections

ctr sec. 33 to North

REC. 7-30-64

Plotted 8-1-64

Sta + π - Elev

0+00 = Ctr Sec 33

5+24.3 S. Side Cabin # 3399

+9.3

✓
6+60.3

✓
7+73 Ho # 3417

12.0

July 29, 1964

X-76

2

	90.1	91.1	90.9	92.2	92.7		92.6	88.6
0.0	+8.9	+4.1	+3.4	+3.9	+3.7	+4.1	0.2	
46	31	16	14			22	30	
Cabin								
					876.3	778	805	817
					12.5	11.0	8.3	7.1
					67	54	50	41
					W5			

99.4	90.9	89.3	89.6	89.2	88.4	80.8	
10.0	0.8	9.3	10.9	10.6	11.0	11.8	19.4
35	17	13		16	24	43	
				87.3	77.2	79.2	
				23.9	23.0	21.0	
				77	70	63	
				WS			

02.7	900.6	899.7	875	876	877	868	780	876.3
07	2.8	13.7	15.9	15.6	15.7	16.6	25.4	27.1
65	34	18	13		15	24	37	47
		12						WS

Sta + π - Elev.

8+85

13

✓

21

10+62.7

10 @ 20

✓

12+44.6

116 20

✓

July 29, 1964

x-77

907.3	902.5	91.9	93.6	87.2	87.2	86.6	86.6	84.1
0.0	4.8	9.9	13.7	20.1	20.1	20.7	20.7	22.6
63	46	36	31	18		13	22	25
HO								

876.3	77.3	79.7	82.5
31.0	30.0	27.6	24.8
62	53	49	33
WS			

92.9	89.4	87.3	86.9	86.4	86.5	85.8	82.1
13.3	14.7	18.8	19.2	19.3	19.6	20.3	23.4
30	22	17	12		11	19	29

96.2	91.9	904.3	05.8	876.3	77.9	80.8	79.9
9.9	8.2	1.8	0.3	29.8	28.2	25.3	26.2
38	39	60	70	46	37	34	31
Wall				WS			

88.8	85.7	85.7	85.0	84.3	82.1
19.2	22.3	22.3	23.0	23.7	25.3
19	13		12	23	28

94.6	900.3	906.5	907.8	876.3	77.1	79.0	79.8
13.4	7.7	1.5	0.2	31.7	30.9	29.0	28.2
27	36	54	67	53	44	38	30
				WS			

Sta + Δ - Elev

13+533

(11) 23.4
22.3
30.3

✓

July 29, 1964

X-78

17.

2

RT

~~7~~

94.0

85.9

85.9

85.4

84.0

80.3

22.6

30.7

30.7

31.2

32.6

36.3

26

12

13

25

30

902.8

078

12.5

14.6

826.3

77.3

13.8

8.6

4.1

2.0

40.3

39.3

36

40

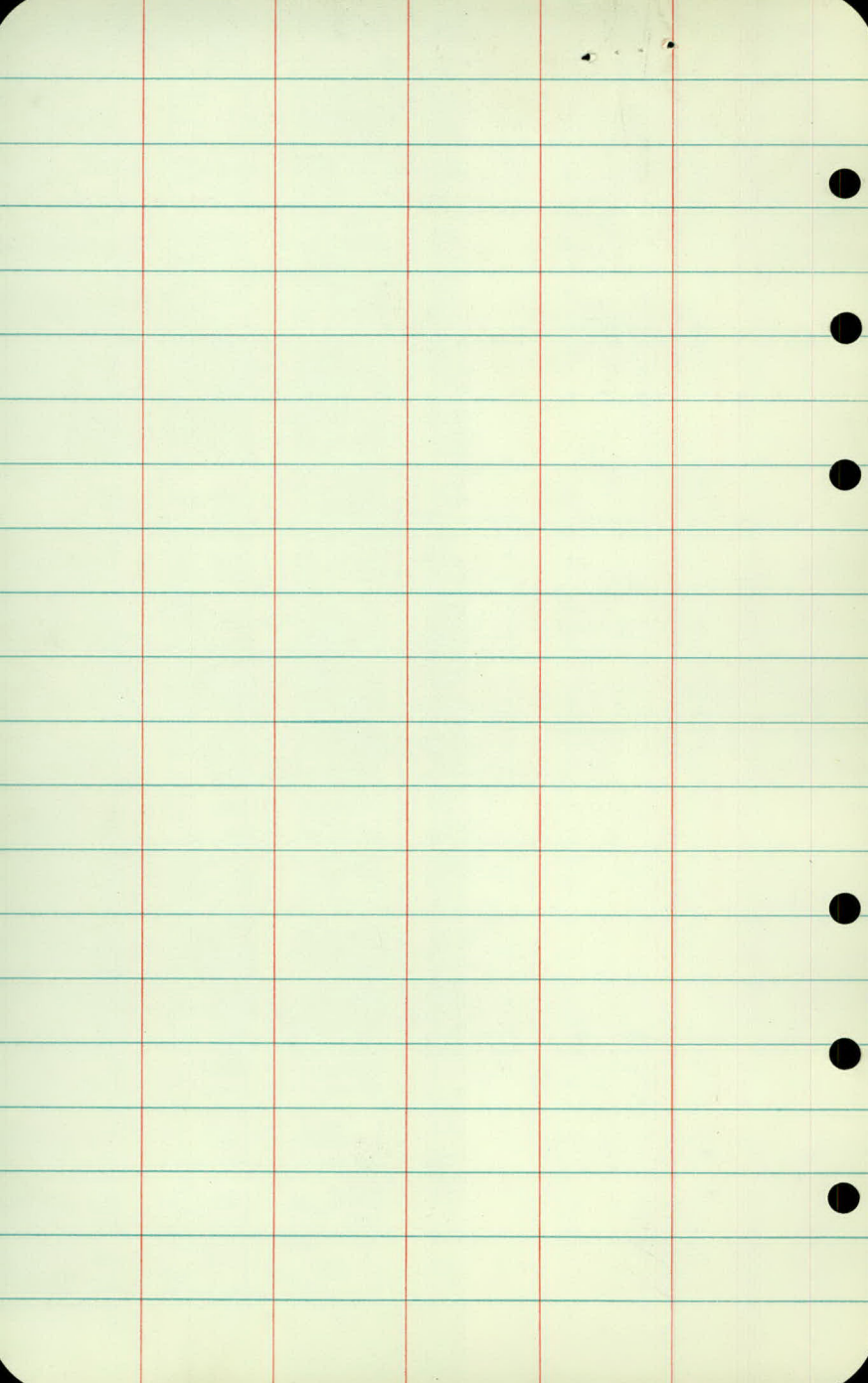
53

71

56.

46

W.S.



KP
WM
DS
FS
PK

21 JAN. 1965

7-1.

SUNNY

X-79

32°

LAKE JOHANNA BLVD.

CO. RD D TO CO. RD E

MISC. ELEVATIONS

STA	+	π	-	ELEV.
BM	5.36	931.72		926.36
0+00			5.69	926.03
+27			7.46	924.26
+66			5.68	926.04
+66			5.64	926.08
2+19			7.60	924.12
BM			3.82	927.90 927.93

21 JAN. 1965 F-2.

DESCRIPTION

X-80

TOP MONT & CO. RD D. JOHANNA BLVD.

TOP CONC. SLAB 10.0 RT.

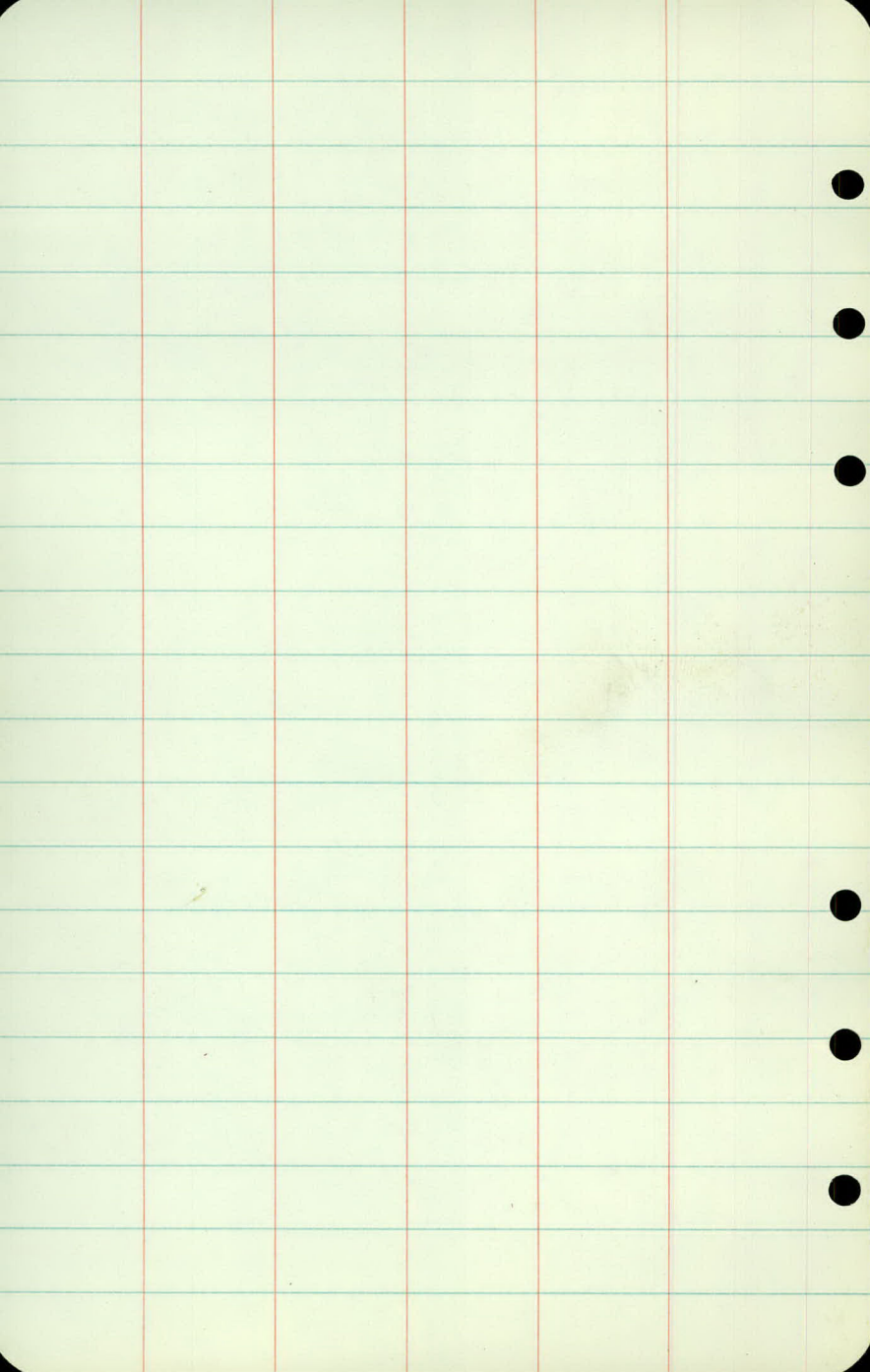
FL CB 22.0 RT

TOP CONC. SLAB 10.0 LT

TOP CONC. SLAB 10.0 RT

FL CB 23.0 RT

N.E. COR LOWER STEP HO# 3151



KP
DS
WM
FS
PK

25 JAN. 1965
DRIZZLE
280

X-81

LAKE JOHANNA BLVD.
Co. RD D TO Co. RD. E.
ADDITIONAL X-SECTIONS

STA	+	π	-	ELEV.
BM	5.82	926.35		(920.73)
			4.30	922.25
			7.15	919.40 (919.40)

BM	0.07	913.49		(913.42)
----	------	--------	--	----------

21+58

✓

BM			4.97	908.52 (908.51)
----	--	--	------	-----------------

25 JAN. 1965

LT

E

RT.

X-82

SPIKE IN PP 28.0 RT STA 6+19.

TOP PK E STA 7+57.16

SPIKE IN PP 28.0 RT STA 10+46

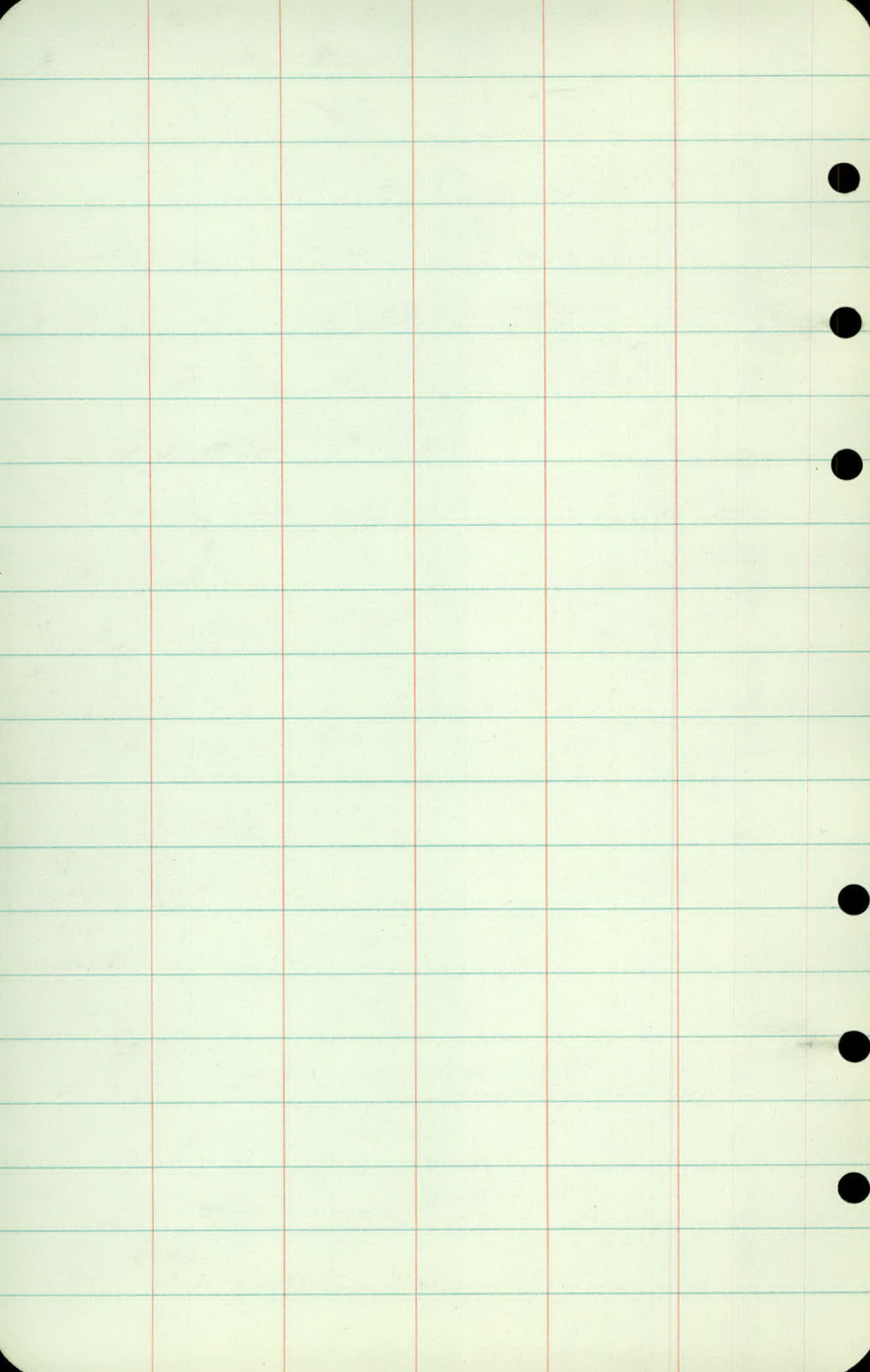
SPIKE IN PP 27.0 RT STA 20+03

			0.3	99.8
4.3	4.3	4.2	6.2	13.7
	9	13	19	30.4
				GA

	91.4	91.1	93.1
22.1	22.4	20.4	
94	71	49	
HO		GA FLOOR	

SPIKE IN PP 27.0 RT STA 23+94

* GARAGE HAS SHEETS OF
TIN FOR SIDING. 4" OVERHANG ON
STREET SIDE.



FK
WM
WS
DS
PK
LD

Feb. 19, 1965 x-83
Cold Cloudy 13° a

Lake Johanna Blvd

Additional x-sections

Sta + π - Elev

BM 4.28 889.58 885.30

4.2 4.85

+30

45
70
90

✓

+39 FL. S.E. 18" CM 79 Lt. 7.80 881.9

6.30
1.5
7.8

+45

✓

+70

✓

Lt.

Feb. 19, 1965 X-84
 Rt. 6

Top P.K. Nail $\pm$ Sta 41+00

83.6	84.0	84.1	84.3	84.7	84.5	84.1	83.6	82.7
60	56	55	53	4.9	5.1	5.5	6.0	6.9
46	26	18	15		16	21	32	41

83.6 83.9
 6.0 5.7
 70 90

76.5 78.8 80.4
 13.1 10.8 9.2
 89 62 56

83.4	84.0	83.9	84.2	84.6	84.5	84.0	83.8	82.2
6.2	5.6	5.7	5.4	5.0	5.1	5.6	5.8	7.4
51	28	18	12		16	21	29	48

84.2 86.1 86.9
 5.4 3.5 2.7
 70 85 94

76.5 78.4 80.4
 13.1 11.2 9.2
 94 68 60

84.3	83.7	83.8	84.1	84.5	84.4	84.1	83.1	81.2
5.3	5.94	5.8	5.5	5.1	5.2	5.5	6.5	8.4
40	MH	20	13		17	22	39	58
	30							

85.1 86.0
 4.5 3.6
 60 82

76.3 78.3 80.2
 13.3 11.3 9.4
 100 77 69

Approx

Sta + π - Elev.

889.58

42+90

✓

7.06
15
8.56

42+83 FL NE 18" CM 92' + 8.56
(18" x 45' CM)

BM

6.90 882.68

11

Feb 19, 1965 X-85
Rt C

85.0	84.2	84.1	84.2	84.4	84.3	84.0	83.5	81.6
4.6	5.4	5.5	5.4	5.2	5.3	5.6	6.1	8.0
70	42	25	11		17	21	37	61

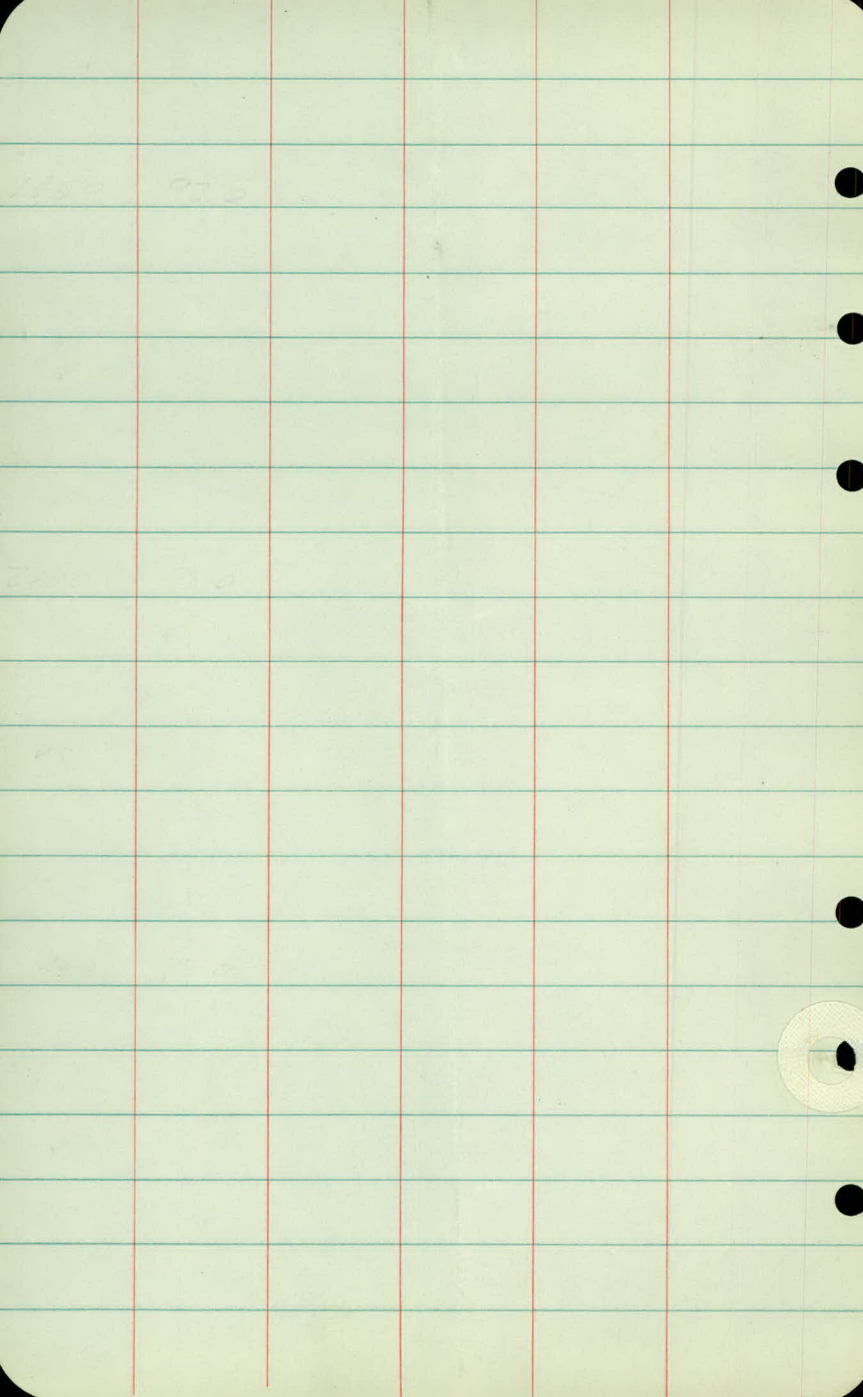
84.1

→ 5.5

84

76.9	78.7	80.4
12.7	10.9	9.2
100	79	75

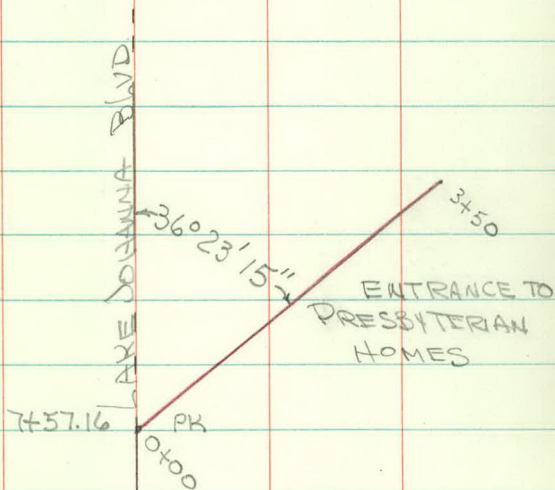
Spike in 36" Cottonwood Rt sta 42+90



KP.
DS.
WM.
FS.
PK.

25 JAN. 1965
DRIZZLE
27°

LAKE JOHANNA BLVD.
Co. RD. D TO Co RD E.
PRESBYTERIAN HOME.
ALIGNMENT & PROFILE
FOR ENTRANCE



Co. RD. D. STONE
0+00 MONT.

STA	+	π	-	ELEV.
BM	2.79	923.52		920.73

0+00 = LAKE JOHANNA BLVD STA.
7+57.16

0+00

+19

+51

+80

1+00

30 JAN. 1965

LT

~~E~~

RT

SPIRE IN PP28.0 RT STA 6+19

2.2

1.3

1.6

3.3

5.6

15.8

7.7

STA	+	T	-	ELEV.
-----	---	---	---	-------

		923.52		
--	--	--------	--	--

1+19		ENTRANCE FORKS TO RT.		
------	--	-----------------------	--	--

+50				
-----	--	--	--	--

+82				
-----	--	--	--	--

2+00				
------	--	--	--	--

+31				
-----	--	--	--	--

+66				
-----	--	--	--	--

25 JAN. 1965

LT

£

RT

14.1

9.4

11.9

11.6 · 10.0 · 11.7

09.8

13.7 · 21.0 · 14.3

08.8

14.7 · 27.0 · 16.0

06.2

16.8 · 41.0 · 19.0

04.1

19.4 · 72.0 23.2

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		923.52		
--	--	--------	--	--

3+00				
------	--	--	--	--

+28				
-----	--	--	--	--

+50				
-----	--	--	--	--

BM				
----	--	--	--	--

	4.12			
--	------	--	--	--

	919.47			
--	--------	--	--	--

		919.40		
--	--	--------	--	--

25 JAN. 1965

LT

~~E~~

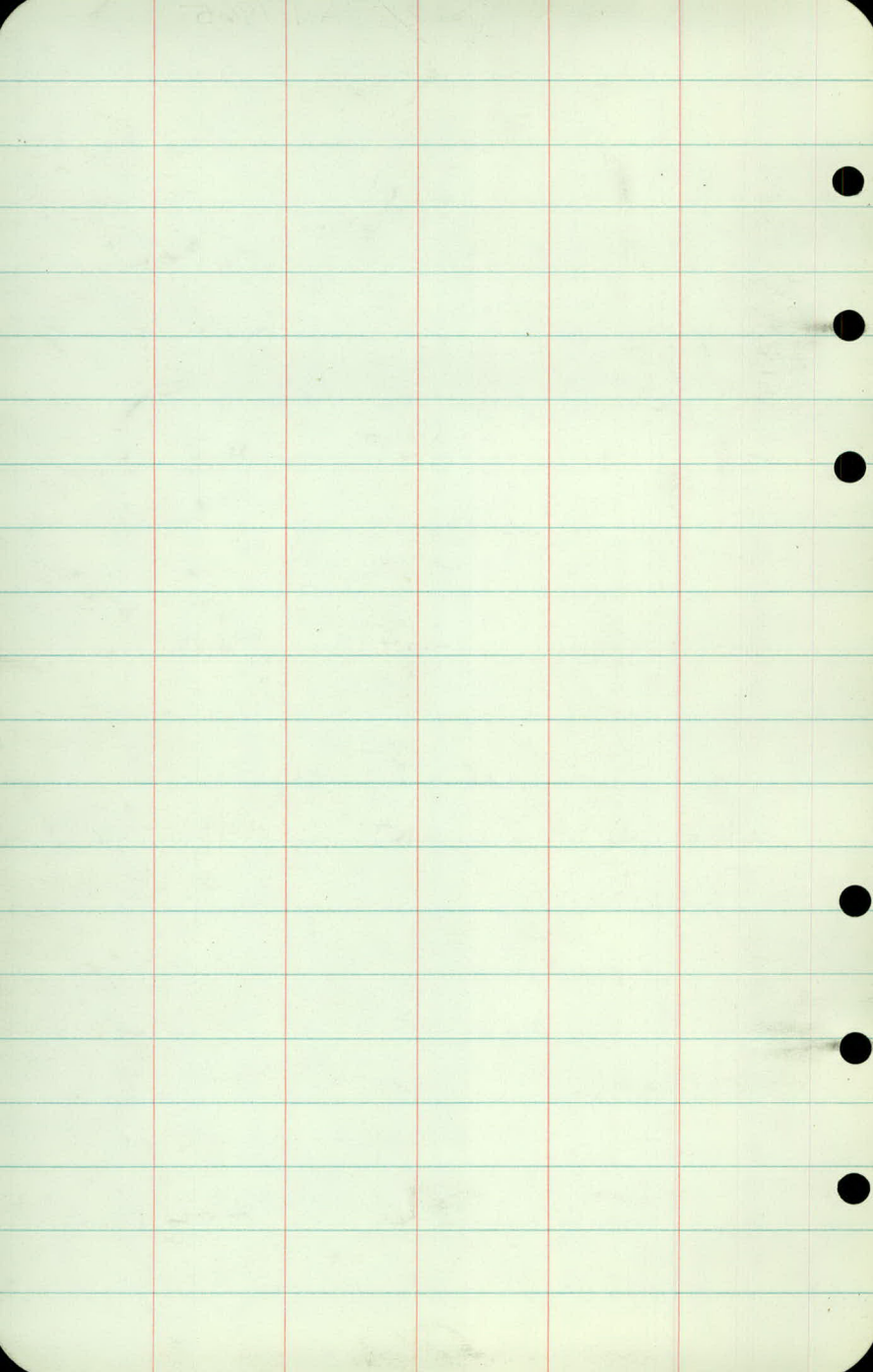
RT

21.8

22.9

23.4

SPIKE IN PP 28.0 RT STA 10+46



RB T
DS ☼
KP ☼
WM
ML

10 JUNE 1965 1.
SUNNY
62°

LAKE JOHANNA BLVD

62-649-01

BM CHECK

2 pages

STA	+	π	-	ELEV.
BM	3.68	931.59		927.91
BM			3.49 *	928.10 927.10
BM			5.23	926.36 926.36
			4.59	927.00 927.1
BM			3.68	927.91 927.91

10 JUNE 1965

2.

DESCRIPTION

TOP N.E. COR LOWER STEP HO# 3151

● TOP HYDRANT S.W. COR Co. RD D

TOP MONT & Co. RD D: JOHANNA BLVD

● TOP PK & STA 3+00

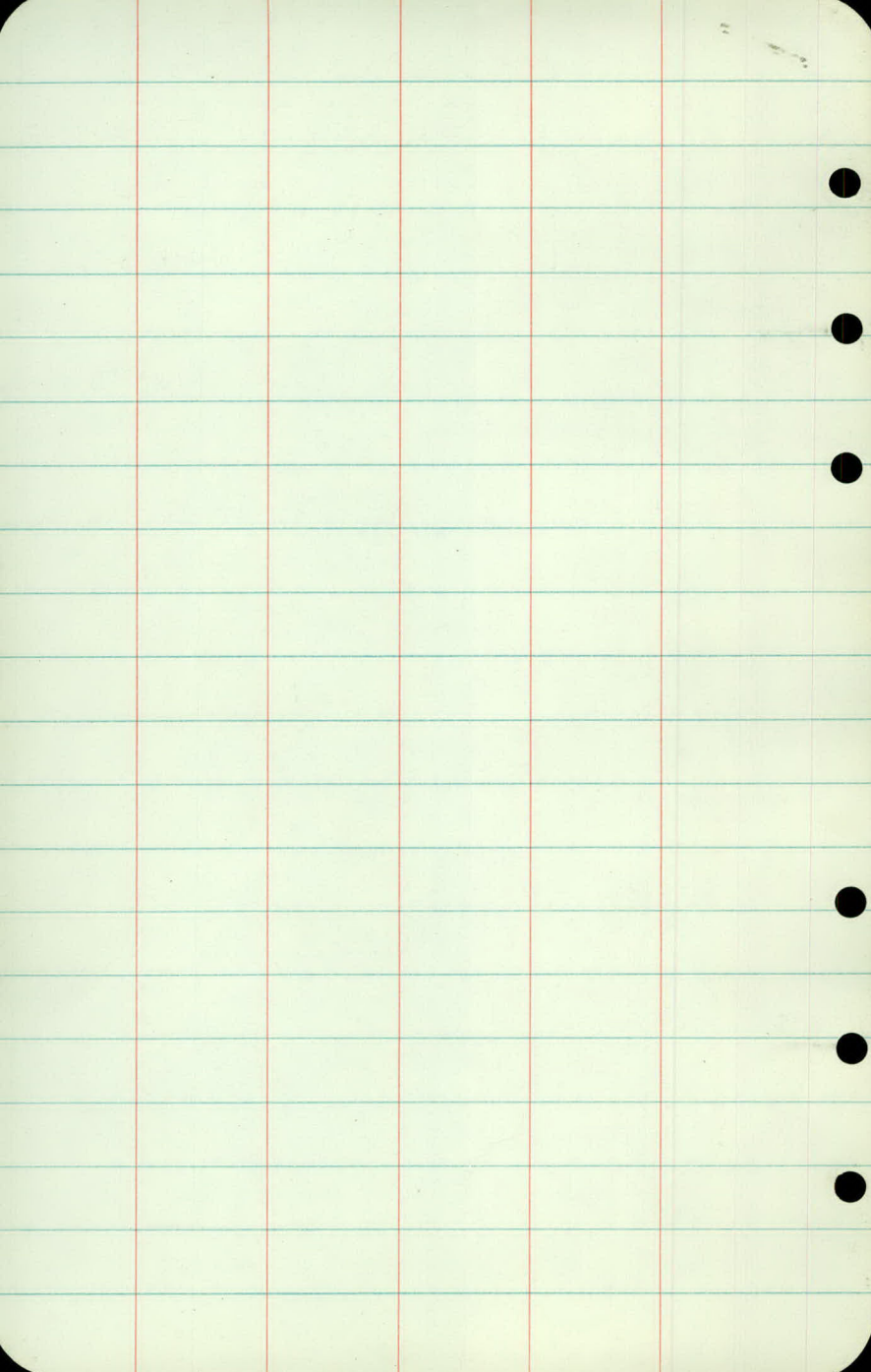
TOP N.E. COR LOWER STEP HO# 3151

●

●

●

●



NOTE: Taper roadway on right from a 22 ft. section at sta. 30+50 to a 14 ft. section at sta. 31+49.14.

Lt Taper from 14 ft. section at entrance sta. 41+25 to a 22 ft. section at beginning of radius at sta. 42+45.

Rt. Taper from 14 ft. section at sta. 41+50 and construct face of curb 4 ft. from guard rail to sta. 42+25, curb not to exceed 22 ft. from ϕ .

11/11/11

FK
WM
PK
WH

Nov. 23, 1964
Clear Cold 22°

A-1

Alignment

Lake Johanna Blvd.

Rec. 1-8-64

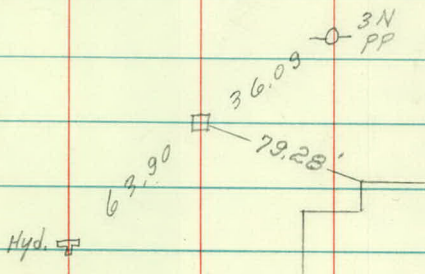
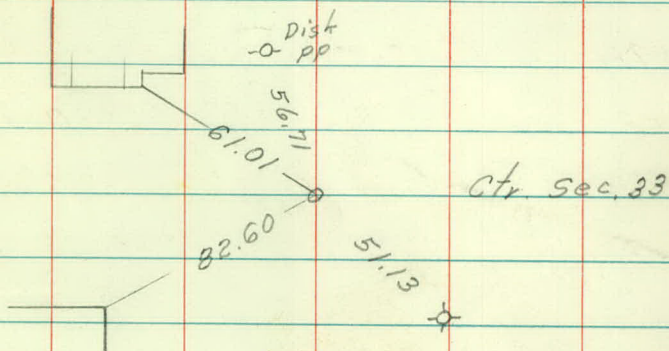
Sta	Point	ΔL	ΔR	
27+30.70	P.T.		22'-	N 44°00'E
+25			21°25.8' $\Delta = 44^\circ$	
27			18°55.8' $\frac{1}{2}\Delta = 22^\circ$	
+75			16°25.8' $D = 20^\circ$ Rt.	
+50			13°55.8' $T = 115.75'$	
26+26.45	P.I.		$L = 220.00'$	
+25			11°25.8' $R = 286.48'$	
26			8°55.8'	
+75			6°25.8'	
+50			3°55.8'	
+25			1°25.8'	
25+10.70	P.C.		0°00'	N 0°00'

0+00 E Co Rd D.

FR
RG
WM
PK

Nov. 25, 1964

A-2



Sta Point ΔL ΔR

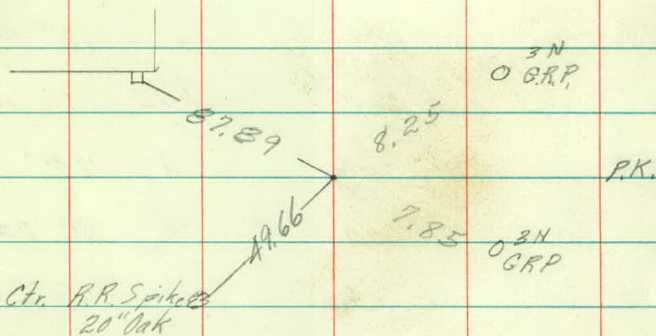
N 6°00'W

+49.17	P.T.	25°00' $\frac{1}{4}$ '	
+25		21°06' $\frac{1}{4}$ '	P.I. = 30+52.14
31		19°06' $\frac{1}{4}$ '	$\Delta = 50°00'\frac{1}{2}$ '
+75		16°06' $\frac{1}{4}$ '	$\frac{1}{2}\Delta = 25°00'15''$
+50		13°06' $\frac{1}{4}$ '	D = 24° Lt
+25		10°06' $\frac{1}{4}$ '	T = 111.34'
30		7°06' $\frac{1}{4}$ '	L = 208.37
+75		4°06' $\frac{1}{4}$ '	R = 238.73'
+50		1°06' $\frac{1}{4}$ '	
29+40.80	PC	0°00'	

N 44°00'E

FK
WM
WH
PK

Dec. 1, 1964
Snowing All Day A-3



Sta Point Δ Lt Δ Rt

106.56	P.T.	$9^{\circ}10'$	
34		$8^{\circ}46.4'$	P.I. = 33+30.83
+75		$7^{\circ}16.4'$	$\Delta = 18^{\circ}20'$
+50		$5^{\circ}46.4'$	$\frac{1}{2}\Delta = 9^{\circ}10'$
+25		$4^{\circ}16.4'$	$D = 12^{\circ} Lt$
33		$2^{\circ}46.4'$	$T = 77.05'$
+75		$1^{\circ}16.4'$	$L = 152.78'$
32+53.78	PC	$0^{\circ}00'$	$R = 477.46'$

33+30.83

1 14.10

32+16.73

2 29.17

34+45.90

Void

see A-5

Dec. 7, 1964

A-4

Sta Point Δ Lt. Δ Rt.

N 24° 20' 30" W

+44.46 P.T. 9° 10'

+25 8° 19.75'

34 7° 19.75'

P.I. 33+30.86

+75 6° 19.75'

$\Delta = 18^\circ 20'$

+50 5° 19.75'

$\frac{1}{2}\Delta = 9^\circ 10'$

+25 4° 19.75'

$D = 8^\circ 14'$

33 3° 19.75'

$T = 115.57'$

+75 2° 19.75'

$L = 229.17' \checkmark$

+50 1° 19.75'

$R = 716.20'$

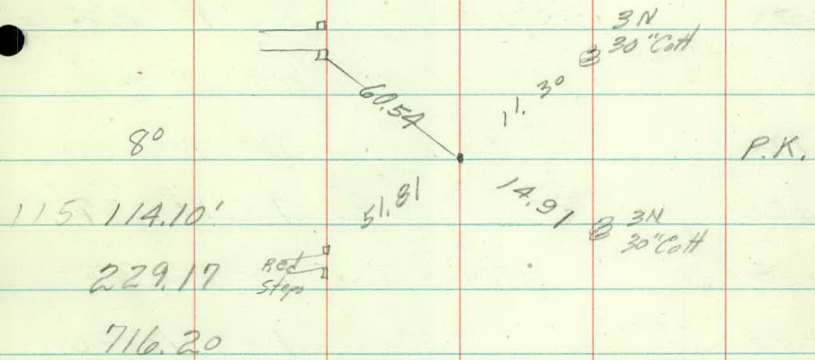
+25 0° 19.75'

32+15.29 P.C. 0° 00'

N 6° 00' $\frac{1}{2}$ W

Dec. 1, 1964

A-5



Sta Point Δ Lt Δ Rt

38+21.78	P.T.	$10^{\circ}56'15''$	N $82^{\circ}28'W$
+75		$10^{\circ}38.6'$	
+50		$9^{\circ}38.6'$	
+25		$8^{\circ}38.6'$ P.I. = 37+46.74	
38		$7^{\circ}38.6'$ $\Delta = 21^{\circ}52\frac{1}{2}'$	
+75		$6^{\circ}38.6'$ $\frac{1}{2}\Delta = 10^{\circ}56'15''$	
+50		$5^{\circ}38.6'$ D = 8° R/L	
+25		$4^{\circ}38.6'$ T = 138.40'	
37		$3^{\circ}38.6'$ L = 273.44	
+75		$2^{\circ}38.6'$ R = 716.20	
+50		$1^{\circ}38.6'$	
+25		$0^{\circ}38.6'$	
36+08.25	P.C.	$0^{\circ}00'$	

Note: Because of change of
Previous Curve-Curve stations are
0.65' Beyond correct location

N $24^{\circ}20'30''W$

Dec. 1, 1964

A-6

P.I.

Post.

Red Brick

41.40

17.53

32.75

32.72

3N
18" Ash

25.59

Black
Wall

3 3N
18" Ash

Sta Point ΔL ΔR

N 24° 24' 30" E

+52.55 P.T.

13° 26' 15"

+50

13° 17.4'

+25

11° 47.4' P.I. = 40 + 42.59

41

10° 17.4' $\Delta = 26° 52\frac{1}{2}'$

+75

8° 47.4' $\frac{1}{2}\Delta = 13° 26' 15"$

+50

7° 17.4' D = 12° Rt

+25

5° 47.4' T = 114.08

40

4° 17.4' L = 223.96

+75

2° 47.4' R = 358.10'

+50

1° 17.4' 477.46

39 + 28.59 P.C.

0° 00'

N 2° 28' W

$\mathbb{Z}$

A-7

28' E/m
Old Tie

Boat Spike

0+00

2550

opp

S. W. Cor.
Gov. Lot 2

C. v.
House

3N

18th Oct.

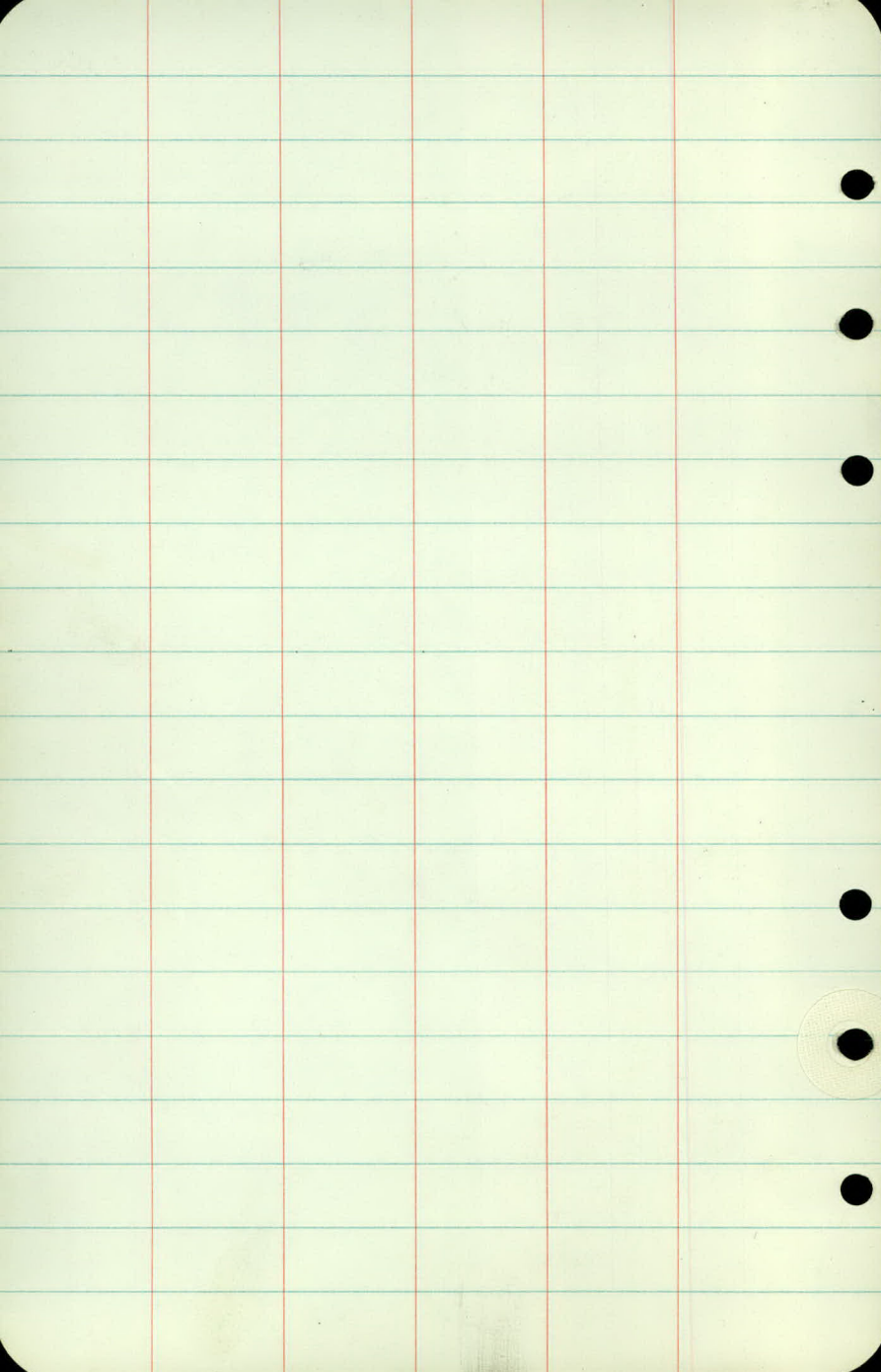
9.5.15

18, 21

P.K. hai

57
25
52
85
3

$$\begin{array}{r} 114.15 \\ 32.68 \\ \hline 81.47 \end{array}$$



FK
WM
WH
PK

Dec. 7, 1964

Cloudy 24°

A-B

Distance Between
New £ and
Used £

Alignment run along
new £.

5fa

Dist. between a new £ and old £

29+50

+75

30

+25

+50

+75

31

+25

+50

32

+25

+50

+75

33

+25

+50

+75

34



0.0

0.1

0.5

0.7

0.2

0.6

1.7

2.7

3.5

3.9

4.3

4.6

4.8

4.9

Dec. 7, 1964

A-9

34 + 25

4.6

+ 50

4.2

35

3.6

+ 50

4.5

36

4.7

+ 25

4.5

+ 50

4.4

+ 75

4.0

37

3.6

+ 25

3.4

+ 50

3.3

+ 75

3.4

38

3.5

+ 25

3.8

+ 50

4.3

+ 75

4.9

39

5.0

+ 25

4.2

+ 50

3.4

Dec. 7, 1964

A-10

Sta

Dist

39+75

3.2

40

3.8

+25

4.7

+50

5.4

+75

5.2

41

4.0

+25

2.6

+50

1.7

42

0

Johanna Blvd.

from

Co. Rd. "D" to Stowe Ave.

TOPOGRAPHY

Pages T-1 to T

0+50

Lt.

POR

POR

+25 80

+34 75

BRd

+17 104

0+00 -26 67

Edge Conc.

Hd

Curb Rad

Conc. Rad

Stop Sign

-26 58

-27 67

-18 60

-9 18

-16 31

MH

DX Sign

6V

6V

WSD

POR

-31 52

-29 64

-30 58

-27 50

-28 28

-20 17

Sign

E. end 18" CM

Cor Bldg

Cor Bldg

Cor Bldg

-41 59

-24 63

-36 50

-30 56

-49 10

-32 10-13

N. end Pump

Curb

Curb

Stop Sign

Beg R

-48 75

-48 58

-49 10

-32 10-13

-52 56

-46 50

S. end 18" Pump

N. end 18" CM

Cor Bldg

Cor Bldg

Cor Bldg

-58 71

-66 68

-52 56

-46 50

-76 48

-76 64

-84 76

Curb

S. end Pump

S. end Pump (3')

E. Rad

BT

BT

-18 41

-30 32

-40 26

-50 23

N. end 12" CM

120 R

E. R

-92 27

-12 56

-60 72

Beg RT Raper

BT Ent + 44 Beg Rad.

-1+00 14

-87 RT to Bldg

-95 34-38

Conc. Curb

B.T.

Bldg

-1+00

-95

34-39

13.5 10

-108 77

-113 35

-115 13

S. end 12" CM

4. BT Ent

Beg. Hedge

PP

-130 41

-130 35

-137 23

-130 31-35

-133 33

-133 28

S. end 12" CM

Beg Rad

End Rad

-141 14

-130 31

Beg RT Raper

BT Ent + 44 Beg Rad.

-1+00 14

-87 RT to Bldg

-95 34-38

-95 34-38

Conc. Curb

B.T.

Bldg

-1+00

-95

34-39

13.5 10

-108 77

-113 35

-115 13

S. end 12" CM

4. BT Ent

Beg. Hedge

PP

-130 41

-130 35

-137 23

-130 31-35

-133 33

-133 28

S. end 12" CM

Beg Rad

End Rad

-141 14

-130 31

Beg RT Raper

BT Ent + 44 Beg Rad.

-1+00 14

-87 RT to Bldg

-95 34-38

-95 34-38

Conc. Curb

B.T.

Bldg

-1+00

-95

34-39

13.5 10

-108 77

-113 35

-115 13

S. end 12" CM

4. BT Ent

Beg. Hedge

PP

-130 41

-130 35

-137 23

-130 31-35

-133 33

-133 28

S. end 12" CM

Beg Rad

End Rad

T-2

 ϕ

Co. Rd.

1000

RIT

12.9'
MH 4 Adj. rings

WSC

005
2 stop
sign

Telep.
MN
O 8.0'

Drive-
14.1n.
18.5

3' 18.5

N

N

14
+50 $\frac{6'' \text{Pine}}{46}$

4 RT

+43 $\frac{4'' \text{Pine}}{72}$

+30 $\frac{24'' \text{Maple}}{70}$ +34 $\frac{8'' \text{Pine}}{45}$
SE Cor Ho 12' BT Ent

+28 83 +20 15
S. end 15' X 20' CM BT
5+00 +09 22 15/15

+97 $\frac{10'' \text{Birch}}{80}$

+90 $\frac{14'' \text{Elm}}{37}$ +94 $\frac{3'' \text{Pine}}{34}$ +73 $\frac{\text{Sign}}{46}$

+77 $\frac{5'' \text{Pine}}{62}$ +80 $\frac{4'' \text{Pine}}{36}$ +83 $\frac{6'' \text{Catalpa}}{45}$ +66 $\frac{\text{PP}}{28}$

+66 $\frac{\text{M.H.}}{22}$ +69 $\frac{12'' \text{Elm}}{36}$ +62 $\frac{7'' \text{BE}}{61}$

RT+48 SE Cor Bar

+50 94 +62 $\frac{12'' \text{BE}}{55}$

S. end 15' X 20' CM

+38 22 +48 15-27 (RT+45)

+24 $\frac{18'' \text{Oak}}{69}$ +26 $\frac{\text{Hedge}}{34}$ +31 $\frac{\text{Lilac}}{36}$

+20 $\frac{20'' \text{Oak}}{36}$ +21 $\frac{20'' \text{Oak}}{52}$

4+00 +03 $\frac{\text{B.T.}}{\text{Ent} (12')}$ BT
16-31 16/14

+84 $\frac{6'' \text{Elm}}{50}$ +92 $\frac{12'' \text{BE}}{34}$

+76 $\frac{\text{SE Cor Ho}}{51}$ +76 $\frac{5'' \text{Pine}}{31}$

+48 $\frac{7'' \text{Pine}}{31}$ +54 $\frac{24'' \text{Oak}}{58}$

+23 $\frac{\text{E Rad}}{18}$ +26 $\frac{\text{PP}}{25}$

3+00 +08 $\frac{\text{POR}}{21}$ +00

N. end 12' SCP

+16 $\frac{23}{\text{PP}}$

+15 $\frac{28}{\text{PP}}$

+12 NW Cor School
120.5

B.T.
30 19

Nov. 9, 1964

LT

4

RT

8+00

BT
12

+00

Curb
15

+00

End Oaks
80-100+

Beg. Hedge

+47

55

MH

+48

23

+55 $\frac{6'' \text{Pine}}{33}$ +47 $\frac{6'' \text{Pine}}{33}$ +47 $\frac{6'' \text{Pine}}{41}$

+36 Ent 12' BT

+25 $\frac{\text{S. end } 15'' \times 20'' \text{cm}}{20}$ +27 $\frac{8'' \text{Pine}}{90}$ +20 $\frac{8'' \text{Pine}}{36}$ +24 $\frac{10'' \text{BE}}{66}$

7+00

BT
13 15+90 $\frac{10'' \text{BE}}{72}$ +93 $\frac{8'' \text{Pine}}{94}$ +98 $\frac{\text{SE Cor Ho}}{102}$ +53 Beg. Ent
15

Beg. Curb

+56

18

+57 $\frac{PP}{28}$ +44 $\frac{\text{Edge Oaks}}{43}$ +14 $\frac{\text{Beg Oaks}}{37-100+}$ +60 $\frac{6'' \text{B.E. (6) scrub}}{75}$ +49 $\frac{4'' \text{Plum.}}{47}$

+34

 $\frac{5'' \text{Apple}}{63}$ +33 $\frac{9'' \text{Apple}}{81}$ +32 $\frac{2'' \text{Elm.}}{39}$

+17

 $\frac{\text{Tw. } 10'' \text{Elm}}{35}$

+28

 $\frac{2'' \text{Plum.}}{38}$

+19

 $\frac{PP}{28}$ +16 $\frac{\text{Tw. } 8'' \text{Pines}}{72}$

+17

 $\frac{12'' \text{Elm.}}{48}$

6+00

BT
14 15

+81 Ent 12' BT

+95 $\frac{10'' \text{Catalpa}}{60}$ +76 $\frac{\text{SE Cor Gar}}{91}$ +70 $\frac{\text{S. end } 15'' \times 24'' \text{cm}}{21}$ +63 $\frac{24'' \text{Oak}}{45}$ +67 $\frac{16'' \text{Maple}}{75}$ 17
19.
23.

+25 $\frac{MH}{24}$

+37 $\frac{\text{E Ent}}{11}$

+46 $\frac{P.P.}{28}$

+22 $\frac{9"P}{92}$

+40 $\frac{3"P}{80}$

+22 $\frac{5"P}{67}$

+22 $\frac{6"P}{78}$

+22 $\frac{320}{45}$

10

$\frac{BT}{13 \ 16}$

+93 $\frac{x\text{-Drain } 18" \times 50' CM}{20 \ 30}$

+69 $\frac{In \ 18" O.}{54}$

+93 $\frac{6" Ash}{64}$

+75 $\frac{4" Ap}{99}$

+60 $\frac{2" Ap}{102}$

+70 $\frac{4" Ap}{76}$

+47 $\frac{2" Apple}{92}$

+07 $\frac{15' \times 20' CM}{21}$

+25 $\frac{Sign \ 1' \times 12' \times 5.5' Brick}{34 \ -46}$

+07 $\frac{\text{E } 8' Conc Ent}{31}$

+01 $\frac{PP}{28}$

9

$\frac{Bit. S.}{14 \ 16}$

$\frac{W. Ent}{91}$

+94 $\frac{12"P}{36}$

+60 $\frac{6" Pine}{37}$

+56 $\frac{4' Cedar}{42}$

+33 $\frac{\text{E } 13' Ent \ 15' \times 20' CM}{20'}$

+37 $\frac{ER}{16}$

+22 $\frac{10"P}{42}$

+22 $\frac{9"P}{33}$

+31 $\frac{BR}{42}$

+14 $\frac{8"P}{33}$

+26 $\frac{POR}{25}$

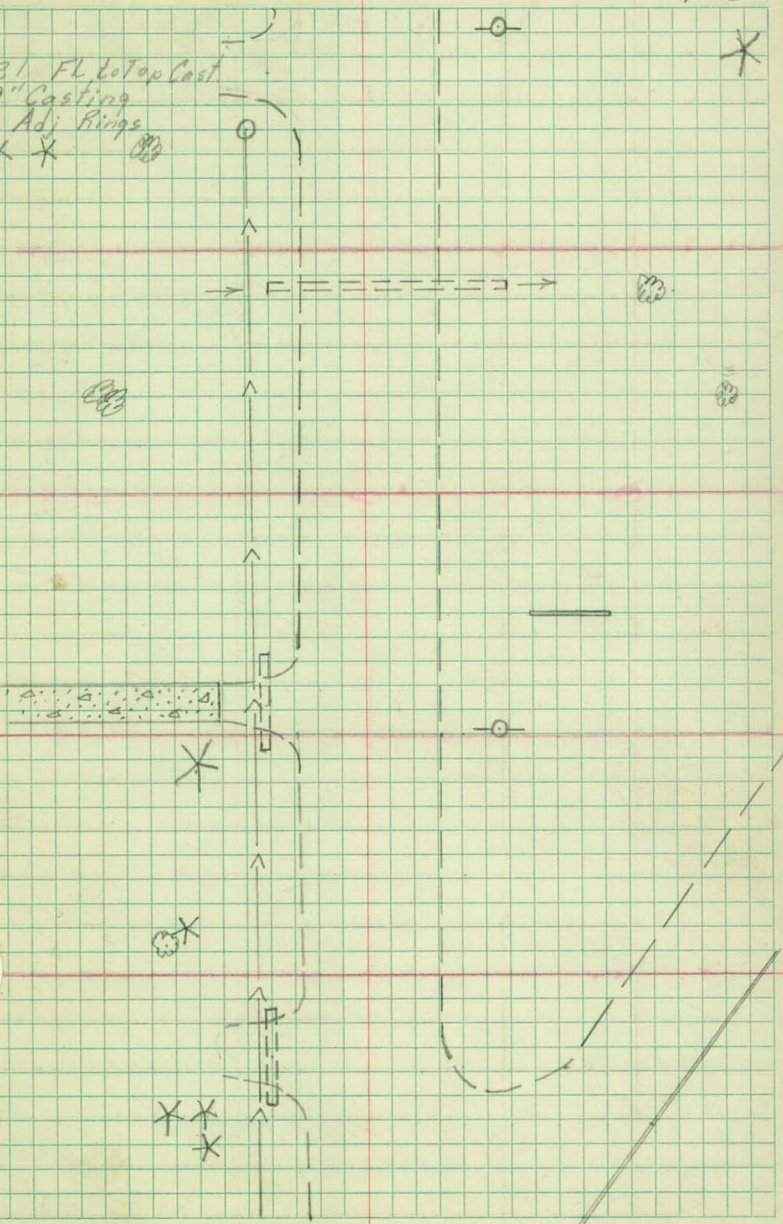
+19 $\frac{B. Curb}{59}$

B+00

T-6

2 Adj Rings

✱ ✱



13

$$\frac{BT}{12 \ 20}$$
 $+99 \frac{10^0}{71}$
 $+93 \frac{9^0}{42}$
 $+58 \frac{5^9 2}{48}$
 $+63 \frac{NE \text{ Car Ho}}{82}$
 $+72 \frac{14^0 P}{74}$
 $+40 \frac{20^0}{44}$
 $+49 \frac{3^0 \text{ Ash}}{60}$
 $+33 \frac{14^0}{49}$
 $+15 \frac{\text{£ } 10^0 \text{ Conc Ent}}{30}$
 $+104 \frac{8^0 P}{59}$

12

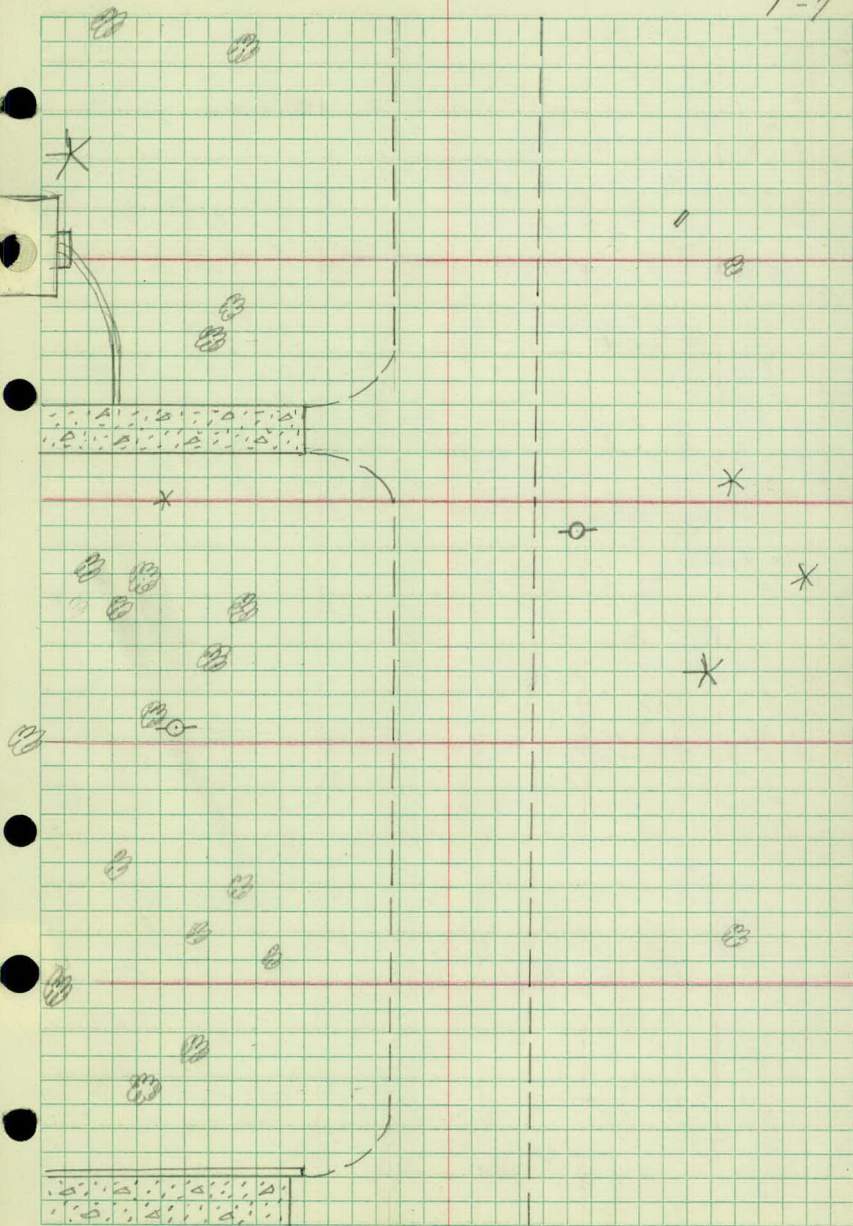
 $+100 \frac{2^0 P}{59}$
 $\frac{B. T.}{12 \ 18}$
 $+86 \frac{14^0}{75}$
 $+77 \frac{14^0}{42}$
 $+78 \frac{4^0 P}{69}$
 $+94 \frac{PP}{27}$
 $+54 \frac{18^0}{61}$
 $+85 \frac{4^0 P}{72}$
 $+53 \frac{PP}{57}$
 $+65 \frac{\text{Cedar}}{82}$
 $+65 \frac{4^0 P}{54}$
 $+51 \frac{10^0}{88}$
 $+66 \frac{6^0 \text{ Maple}}{69}$
 $+67 \frac{6^0 M}{48}$
 $+20 \frac{18^0}{43}$
 $+11 \frac{6^0 \text{ Ash}}{52}$
 $+84 \frac{10^0}{63}$
 $+106 \frac{24^0}{37}$
 $+110 \frac{4^0 \text{ Ash}}{60}$

11

 $\frac{B. T.}{12 \ 17}$
 $+99 \frac{20^0}{82}$
 $+87 \frac{8^0 \text{ Elm}}{53}$
 $+77 \frac{18^0}{64}$
 $+61 \frac{\text{Wall (8" Conc-Block)}}{30}$
 $+56 \frac{\text{£ } 10^0 \text{ Conc Ent}}{33}$

Nov. 16, 1964

T-7



Lt

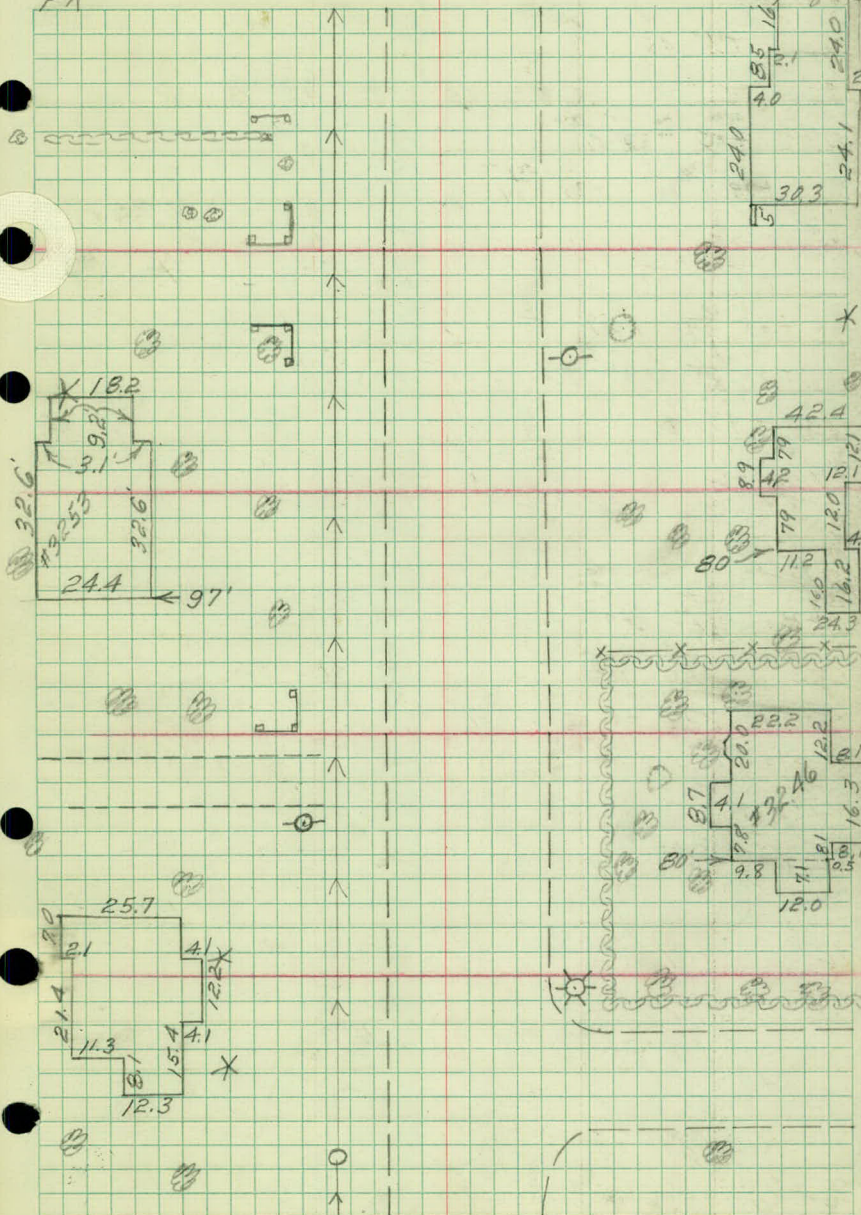
±

Rt

+24	$\frac{Tw 10^0 00''}{87}$	+26	$\frac{Fe Cor}{32-40}$					
+23	$\frac{Hedge}{35-83}$			+18	$\frac{B Fe}{32}$			
		+08	$\frac{18^0 00''}{53}$					
+10	$\frac{E Fe}{32}$			+07	$\frac{24^0 00''}{48}$			
+15		+02	$\frac{Fe Cor}{32-40}$		$\frac{BT}{12-21}$	+09	$\frac{SW Cor Ho}{65}$	
+93	$\frac{E Ent}{17}$				$\frac{Arbivald (tw 5')}{84-38}$	+99	$\frac{12^0 00''}{56}$	
		+85	$\frac{Fe Cor}{32-40}$			+78	$\frac{PP}{27}$	
+82	$\frac{10^0 00''}{61}$	+77	$\frac{B Fe}{32}$	+80	$\frac{16^0 00''}{35}$	86	$\frac{4^0 00''}{84}$	
			$\frac{5^0 00''}{71-79}$			+84	$\frac{4^0 00''}{90}$	
						+73	$\frac{12^0 00''}{87}$	
+47	$\frac{8^0 00''}{36}$			+56	$\frac{28^0 00''}{54}$	+71	$\frac{5^0 00''}{68}$	
		+36	$\frac{20^0 00''}{88}$			+41	$\frac{14^0 00''}{49}$	
						+46	$\frac{16^0 00''}{39}$	
+25	$\frac{Tw 4^0 00''}{34}$		$\frac{SE Cor Ho}{97}$		$\frac{SW Cor Ho}{80}$		$\frac{16^0 00''}{62}$	
		+07	$\frac{Tw 10^0 00''}{67}$			+19	$\frac{12^0 00''}{72}$	
+06	$\frac{30^0 00''}{51}$			+09	$\frac{E Fe}{31}$	+15	$\frac{Cor Hedge}{33}$	
					$\frac{BT}{12-22}$		$\frac{18^0 00''}{47}$	
+14		+01	$\frac{Fe Cor}{31-39}$			+06	$\frac{18^0 00''}{61}$	
+90	$\frac{E Div}{Ent}$			+72	$\frac{PP}{29}$	$\frac{Arbivald}{92-13}$	+96	$\frac{16^0 00''}{55}$
		+68	$\frac{Tw 8^0 00''}{53}$			+80	$\frac{6^0 00''}{42}$	
+63	$\frac{NE Cor Ho}{90}$			+77	$\frac{12^0 00''}{86}$	+69	$\frac{8^0 00''}{53}$	
						+72	$\frac{6^0 00''}{32}$	
						+74	$\frac{SW Cor Ho}{80}$	
						+44	$\frac{12^0 00''}{78}$	
						+46	$\frac{12^0 00''}{44}$	
						+45	$\frac{8^0 00''}{65}$	
						+48	$\frac{ER}{22}$	
+13	$\frac{MA}{23-}$	+54	$\frac{8^0 00''}{47}$			+44	$\frac{Cor Hedge}{33}$	
						+18	$\frac{ER}{30}$	
+16	$\frac{10^0 00''}{78}$					+38	$\frac{BR}{32}$	
				+32	$\frac{6^0 00''}{46}$			
						+13	$\frac{Tw 14^0 00''}{57}$	
+13		+09	$\frac{24^0 00''}{54}$			+11	$\frac{POR}{23}$	

Dec. 8, 1964

FK
WM
WH
PK



FLTO TOPCASTING = 13.65

ADJUSTING RINGS = 4

CASTING = 0.75

18

Lt.

£

Rt.

$$+98 \frac{PP}{45}$$

$$\begin{array}{r} BT \\ 12.5 \end{array} \begin{array}{r} 21.5 \\ +00 \end{array} \begin{array}{r} FC \\ 48 \end{array}$$

$$+85 \frac{Fe Cor}{34-44}$$

$$+82 \frac{Fe Cor for garden}{47} RT+88$$

$$+85 \frac{12''0}{69}$$

$$+79 \frac{36''0}{40} +75 \frac{Bay Fe}{34}$$

$$+53 \frac{PP}{27}$$

$$+42 \frac{16''0}{61} +53 \frac{stp}{46}$$

$$+55 \frac{24''0}{41}$$

$$+48 \frac{16''0}{79} +57 \frac{18''0}{79}$$

$$+31 \frac{24''0}{83} +39 \frac{16''0}{81}$$

$$+25 \frac{stp}{53}$$

$$+13 \frac{14''0}{47} +16 \frac{M4}{23}$$

$$17 +00 \frac{18''0}{46}$$

$$\begin{array}{r} BT \\ 12.22 \end{array} +07 \frac{stp}{42}$$

$$+77 \frac{8''0}{82} +82 \frac{10''0}{45}$$

$$+75 \frac{30''0 Cott}{38} +78 \frac{10''0}{57}$$

$$+78 \frac{SE Cor Pored}{101}$$

$$+77 \frac{14''0}{58}$$

$$+66 \frac{14''0}{47} +66 \frac{15''0}{52}$$

$$+52 \frac{15''0}{40} +50 \frac{12''0}{62} +60 \frac{18''0}{50}$$

$$+43 \frac{3''H Post}{33}$$

$$+41 \frac{14''0}{61}$$

$$+31 \frac{12''Ent}{21} RT+28$$

$$+23 \frac{12''Willow}{48}$$

$$+33 \frac{Bay Fe}{33-63} +33 \frac{Lilac Hedge}{33-63}$$

$$+07 \frac{Sub Cor Garage}{37} +18 Ent 16'$$

$$16 +01 \frac{Tw. 20''0}{86}$$

$$\begin{array}{r} BT \\ 12.5 \end{array} \begin{array}{r} 22 \\ +01 \end{array} \begin{array}{r} TP \\ 28 \end{array}$$

$$+91 \frac{Tip 2'' Birch}{39}$$

$$+99 \frac{16''0}{53}$$

$$+75 \frac{24''0}{52}$$

$$+78 \frac{stp}{59}$$

$$+93 \frac{12'' Elm}{42}$$

$$+61 \frac{12''0}{52}$$

$$+68 \frac{16''0}{43}$$

$$+54 \frac{18''0}{75}$$

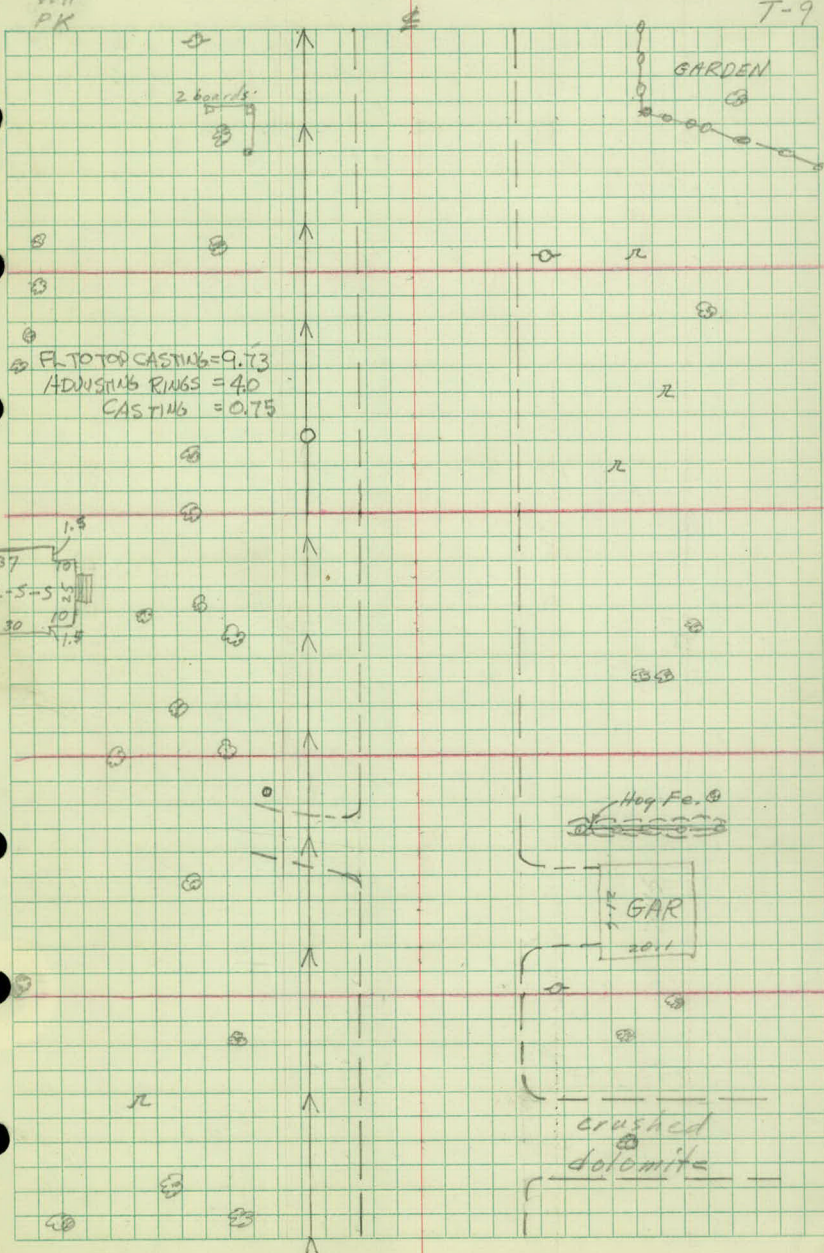
$$+55 \frac{14''0}{39}$$

$$+70 \frac{\text{Crushed Root Ent (16')}}{}$$

RG
WM
WH
PK

Dec 9, 1964
overcast 20°

T-9



Lt.

±

Rt.

+07 SE Cor Ho
61

20

BT
16 18 +03 PP +01 2. end 15" Vit.
27 23
+97 SW Cor Gns
38

+74 2" Maple
51

+53 PP
42

+42 BR +59 ER
44 74

+49 Ent (10')

+28 Beckman Ave

+25 MH
33

+13 ER
43

+25 4" Pine
43

19

+00 POR
165

+90 1" Pine
39

+89 12'0"
83

+85 1" Pine
35

+85 1" Pine
43

+92 Bay Rad
13

+00 ER +02 4" Pine
20 42
+87 B.R. +97 PP +90 PP
35 27 56

+78 ± Sandeen Rd.

+68 End Rad +69.5 Possibly Gas X-ing
40

+45 8" Map
54

+31 SE Cor Ho
74

+34 Quad 5" Maple
62

+48 14" Willow
39

+51 Bay Rad
21

+38 12'0"
87

+30 Fe Cor
49

+37 24" O
61

+06 30" O +11 4" Maple
35 72

+15 Tri 4" Maple
55

18

+03 1" Pine +06 1" Pine .BT
64 55 12.5 21.5

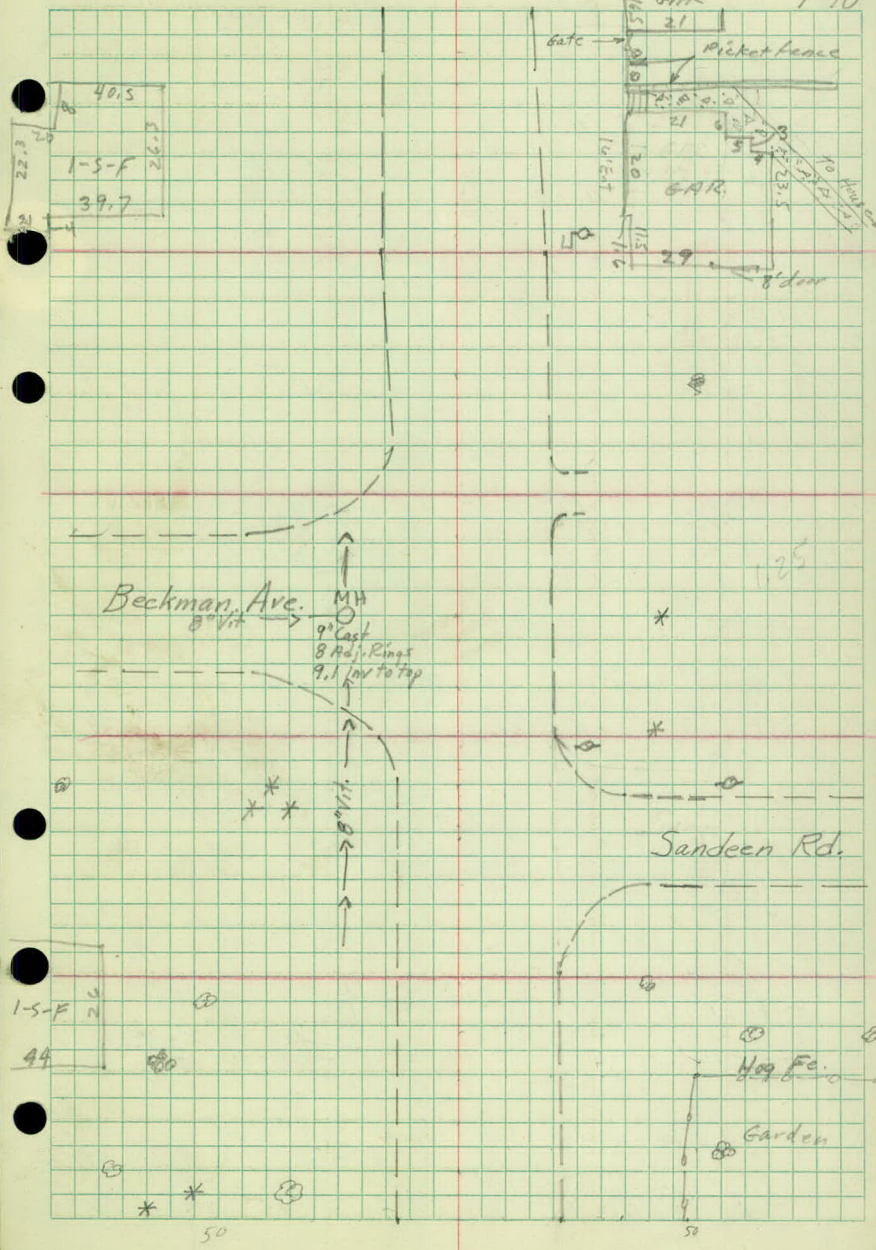
Dec 9, 1964

Lt.

E

Rt.

T-10



23

BT
19 14

Ent 1 BR (6 posts)

+86 $\frac{6" \text{Pine}}{58}$ +79 $\frac{12" \text{Ash}}{39}$ +70 $\frac{12" \text{Ash}}{51}$ +72 $\frac{\text{P. Juniper}}{61}$ +69 $\frac{\text{P. Juniper}}{71}$ +62 $\frac{8" \text{Ash}}{70}$ +63 $\frac{12" \text{Elm}}{45}$ +60 $\frac{4" \text{Pine}}{81}$ +53 $\frac{\text{Fc + Iron pipe}}{34-100+}$ +23 $\frac{\text{Tri 4" BE}}{53}$ +26 $\frac{4" \text{Cott}}{33}$ +30 $\frac{\text{Tw. 4" Cott}}{33}$ +16 $\frac{10" \text{Oak}}{39}$ +38 MH
24

+94

1A
24" Cott+91 $\frac{73}{73}$ +93 $\frac{12" \text{Ash}}{53}$ +76 $\frac{18" \text{Elm}}{69}$

13eg BR

+52 $\frac{14}{14}$ +65 $\frac{14" \text{Ash}}{78}$ +46 $\frac{\text{Tw 8" BE}}{50}$ +46 $\frac{\text{MH}}{68}$ +41 $\frac{\text{PIS}}{28}$ +41 $\frac{\text{Pole}}{36}$ +44 $\frac{\text{ER}}{14}$ +18 $\frac{\text{POR}}{51}$ +31 $\frac{\text{POR}}{31}$ +42 $\frac{\text{BR}}{74}$ +26 $\frac{\text{Tri 8" Elm}}{52}$ +12 $\frac{\text{BR}}{12}$ +17 $\frac{\text{ER}}{16}$ +15 $\frac{\text{POR}}{30}$ +08 $\frac{\text{POR}}{47}$

BT

16.5 13 +02 $\frac{\text{Round 4" Ash}}{27}$ +02 $\frac{\text{Ent BR (8 posts)}}{15}$

22

+88 $\frac{\text{STP}}{44}$ +90 $\frac{\text{STP}}{44}$ +85 $\frac{6" \text{E.}}{38}$ +92 $\frac{\text{STP}}{58}$ +73 $\frac{60" \text{Cott}}{36}$ +88 $\frac{3" \text{Wick}}{75-46}$ +94 $\frac{4" \text{Ash}}{23}$ +83 $\frac{14" \text{Elm}}{37}$ +93 $\frac{12" \text{Elm}}{40}$ +83 $\frac{\text{STP}}{34}$ +73 $\frac{\text{STP}}{37}$ +64 $\frac{20" \text{O}}{50}$ +73 $\frac{\text{Round 5" Ash}}{26}$ (Nocable) +46 $\frac{3" \text{Ash (5)}}{25}$

13eg BR

+37 $\frac{15}{15}$ +37 $\frac{\text{Tri 6" Ash}}{31}$ +41 $\frac{\text{SW Cor Gar}}{30}$ +14 $\frac{\text{PP}}{37}$ +12 $\frac{14" \text{Cott}}{70}$

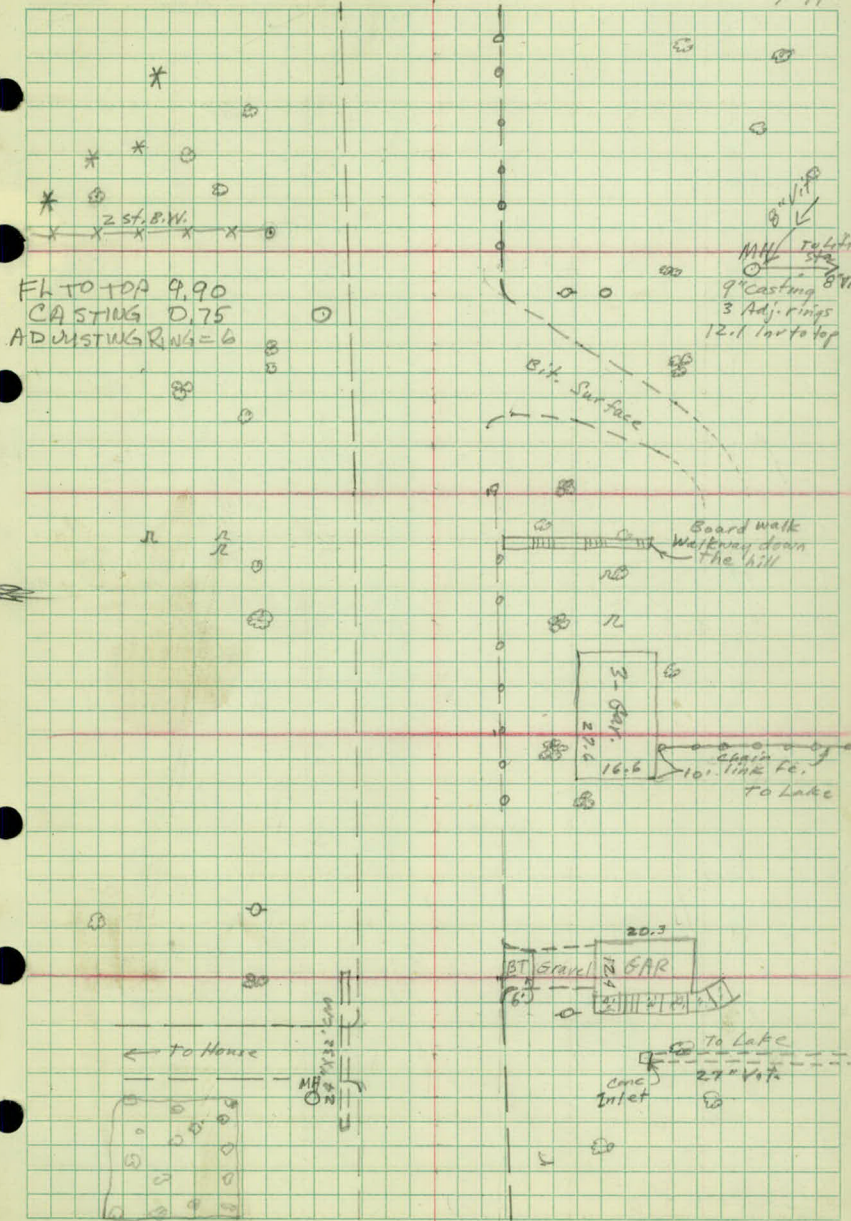
BT

14 14 +03 Ent 10' 6" BT Apron

+79 $\frac{\text{Tri 8" Cott}}{37}$ +93 $\frac{\text{PP}}{27}$ +97 $\frac{\text{SW Cor Gar}}{34}$ +84 Ent 12' +75 $\frac{\text{MH}}{24}$ +75 $\frac{18" \text{Elm}}{59}$ +86 $\frac{3" \text{Cott (2)}}{51}$ +83 $\frac{\text{Open Drain}}{45}$ +65 $\frac{16" \text{Willow}}{36}$ +69 $\frac{\text{Scattered}}{19}$ +50 to +74 $\frac{\text{Cotta}}{41-69}$ +55 $\frac{\text{Ent 14'}}$

Dec 9, 1964

T-11



ADJUSTING RING = 6.0
 FL TO TOP CASTING = 11.75
 CASTING = 0.75

Lt.

E

Rt.

14 Elm
+50 63

Cor. hedge & stone wall
+45 37-100+

6" Oak
+08 35

Edrive +36 50 +39 30 +39 Ent 16'
14" Elm +15 38 +20 31 +21 50
13T +14 23.5 +01 35
14 23.5 +01 35

25

B. Hedge
+94 30

E. Hedge
+77 29

14" Elm
+77 32

+84 E Ent 10'

PP
+95 28

+48 E Ent 10'

B. Hedge
+56 30

+58 12" Elm
+71

Sw. Cor Gar
+97 41

1" Conc. wall
+43 50-81 Rt +44

+45 57

Sw. Cor Gar
+45 57

16" Oak
+49 51

10" Maple
+45 72

12" Maple
+45 90

+41 28-100+

PP
+43 52

Hedge
+41 28-100+

8" BE
+41 36

Quad 4" Hedge
+43 67

14" BE
+28 40

+33 E Ent (10')

+20 12" BE
+70

+27 End Hedge
+27 29

+28 14" BE
+35

+17 16" Oak
+34

+21 41

+20 10" BE
+56

+80 Sw. Cor BT slab (UR33)
+25

+89 78

20" Elm
+89 78

BT
17 22.5 +03 39

4" Pine
+94 Hedge Cor
+27

+98 4" Pine
+44

Tw. 20" Crib
+83 58

+89 53

3" Pine
+89 53

PP
+94 27

B. Cor Fe
+90 36

Fe Cor
+77 26

End Fe
+94 29

3" S.W.
+68 36

NW Cor Gar
+42 35

SW Cor Gar
+47 36

+44 To +60 Pf. Jumper
32 to 44

No. end 12" x 20" cm
+43 25

10' Ent
+34 17

Rt +30

Pf. Jumper
32 to 42

17 SW
30-34

+09 to +26

3" Birch
+06 56

+07 WALL
29

BT
19 14 +09 55

CB 29-35 Sw. Cor Crib
+12 25

+10 36-54

8" Elm
+09 55

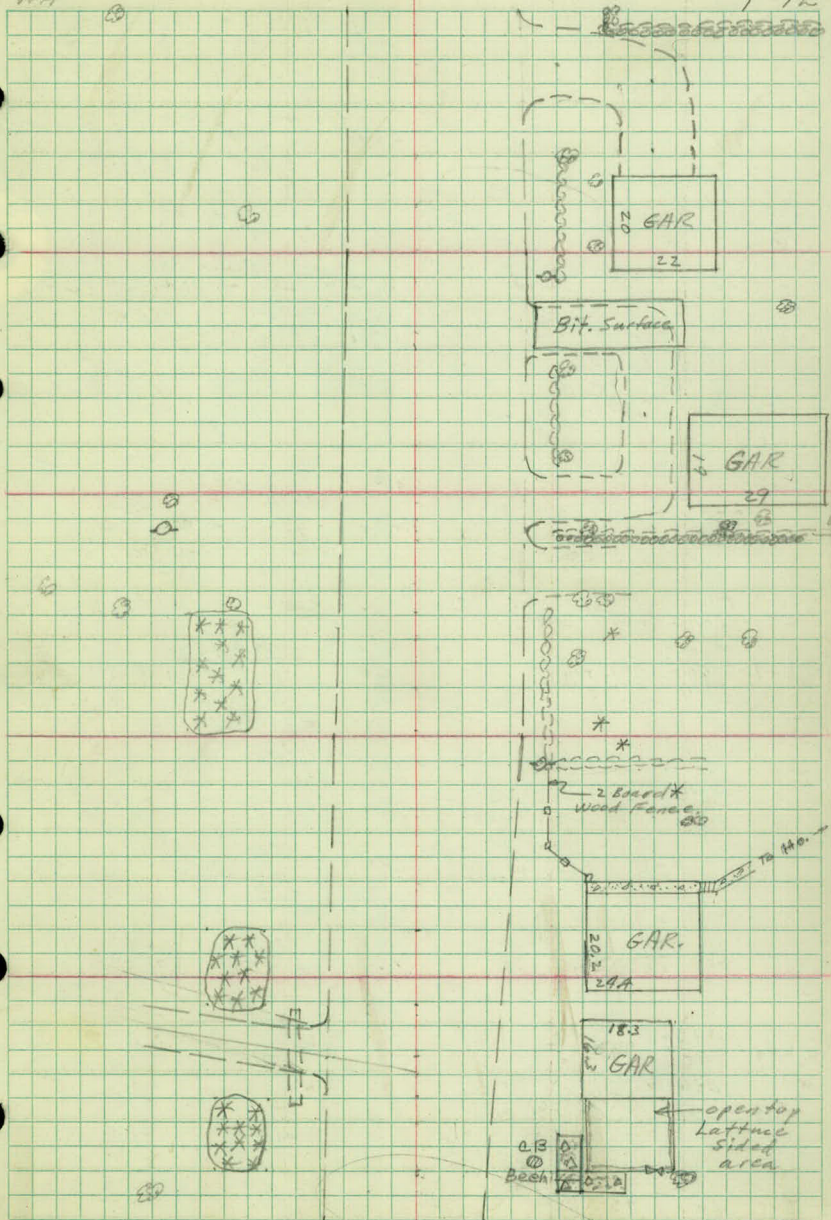
23

23

£

Dec. 9, 1964
Rt. Dec 10, 1964
30° overcast

T-12



Lt.

28

$$\begin{array}{r} \text{BT} + 100 \text{ End Hedge} \\ 13.19 \end{array}$$

+78 Sewer X-1ng

$$\begin{array}{r} \text{Like} \quad 12'' \text{ Spruce} \\ +97 \quad 30 \quad +98 \quad 52 \\ \text{Tri 6" Birch} \quad \text{PP} \\ +84 \quad 45 \quad +92 \quad 30 \\ \text{Sw Cor Ho} \\ +99 \quad 67 \quad \text{RT} + 70 \end{array}$$

$$\begin{array}{r} 8'' \text{ Pine} \\ +62 \quad 66 \\ \text{Conc} \\ +54 \text{ E Ent (18')} \quad \text{RT} + 64 \\ \text{Cor Conc Ent} = \text{Cor Conc Ent} \\ +47 \quad 22 \quad +58 \quad 27 \\ \text{Beg Stone Wall} \\ +32 \quad 46 \quad \text{RT} + 74 \end{array}$$

$$\begin{array}{r} 12'' \text{ Spruce} - \text{Ho} \quad 14'' \text{ Spruce} \\ +50 \quad 78 \quad +50 \quad 89 \quad +38 \quad 85 \\ 2 \text{ steps} + 15 \text{ w.} \quad 4'' \text{ Gate} \\ +52 \quad 23 \quad +52 \quad 26 \\ \text{Hedge} \quad 4'' \text{ Mt Ash} \\ +31 \quad 25 \quad +41 \quad 49 \end{array}$$

27

$$\begin{array}{r} \text{BT} \\ 13.5 \quad 18.5 \end{array}$$

$$\begin{array}{r} \text{E.R.} \quad \text{PP} \quad \text{Tri 3" Birch} \\ +75 \quad 15 \quad +74 \quad 23 \quad +73 \quad 50 \\ \text{SE Cor Ho} \\ +69 \quad 69 \quad \text{RT} + 27 + 4 \end{array}$$

$$\begin{array}{r} 14'' \text{ Maple} \\ +102 \quad 59 \\ 12'' \text{ Pine} \quad \text{Hedge} \\ +91 \quad 42 \quad +00 \quad 25 \\ 12'' \text{ Pine} \quad \text{Hedge} \\ +85 \quad 32 \quad +75 \quad 22 \\ \text{Tri 6" Birch} \quad 12'' \text{ Pine} \\ +68 \quad 29 \quad +74 \quad 42 \\ \text{Fc Cor + Beg Hedge} \quad \text{E Ent} \\ +62 \quad 64 \quad \text{RT} + 28 \quad +62 \quad 50 \end{array}$$

$$\begin{array}{r} \text{POR} \quad \text{POR} \quad 6'' \text{ Pine} \\ +50 \quad 23 \quad +65 \quad 16 \quad +61 \quad 59 \\ \text{Beg Stone Wall} \\ +51 \quad 24 \quad \text{RT} + 66 \quad +39 \quad \text{End Wall} \\ \text{E 18' ENT} \quad \text{POR} \quad \text{POR} \\ +25 \quad 41 \quad +28 \quad 51 \quad +40 \quad 30 \\ \text{MT} \\ +23 \quad 25 \quad +31 \text{ E Stone Arc (RT)} \end{array}$$

$$\begin{array}{r} +45 \text{ E Ent (12')} \quad \text{RT} + 35 \\ +38 \quad \text{B. Hedge} \\ 20 \end{array}$$

+08 RT to So. side Street

$$\begin{array}{r} \text{POR} \quad \text{E. Rad} \\ 26 \quad +00 \quad 30 \quad +00 \quad 48 \end{array}$$

BT

19.5 +08 E 16' Ent RT = 25497

$$\begin{array}{r} \text{End 4' S.W.} \quad \text{B.R.} \\ +89 \quad 75 \quad +91 \quad 14 \\ \text{NE Cor Ho} \quad \text{RT} + 90 \quad +17 \quad 81 \end{array}$$

$$\begin{array}{r} \text{Sw Cor Bar} \quad \text{Stone Wall corner} \\ +99 \quad 59 \quad \text{RT} + 86 \quad +98 \quad 69 \\ \text{Hedge wall Arc Lt.} \quad \text{End hedge e. cor. Wall} \\ +89 \quad 27 \quad +97 \quad 24 \quad +98 \quad 29 \\ 8'' \text{ Elm} \quad 8'' \text{ Elm} \quad 28'' \text{ Cott} \\ +68 \quad 39 \quad +80 \quad 59 \quad +74 \quad 77 \\ 2 \text{ steps (conc)} \quad 2'' \text{ S.W. Angle} \\ +55 \quad 28 \quad +64 \quad 40 \\ \text{Stone Gate Post} \quad \text{Stone Gate Post} \\ +55 \quad 33 \quad +58 \quad 30 \end{array}$$

$$\begin{array}{r} 4'' \text{ SW Cor} \quad \text{SE Cor Ho} \quad \text{RT} + 44 \\ +60 \quad 68 \quad +53 \quad 82 \end{array}$$

$$\begin{array}{r} \text{BT} + 75 \\ 14 \quad 20.5 \end{array}$$

$$\begin{array}{r} 12 \\ 14.5 \end{array}$$

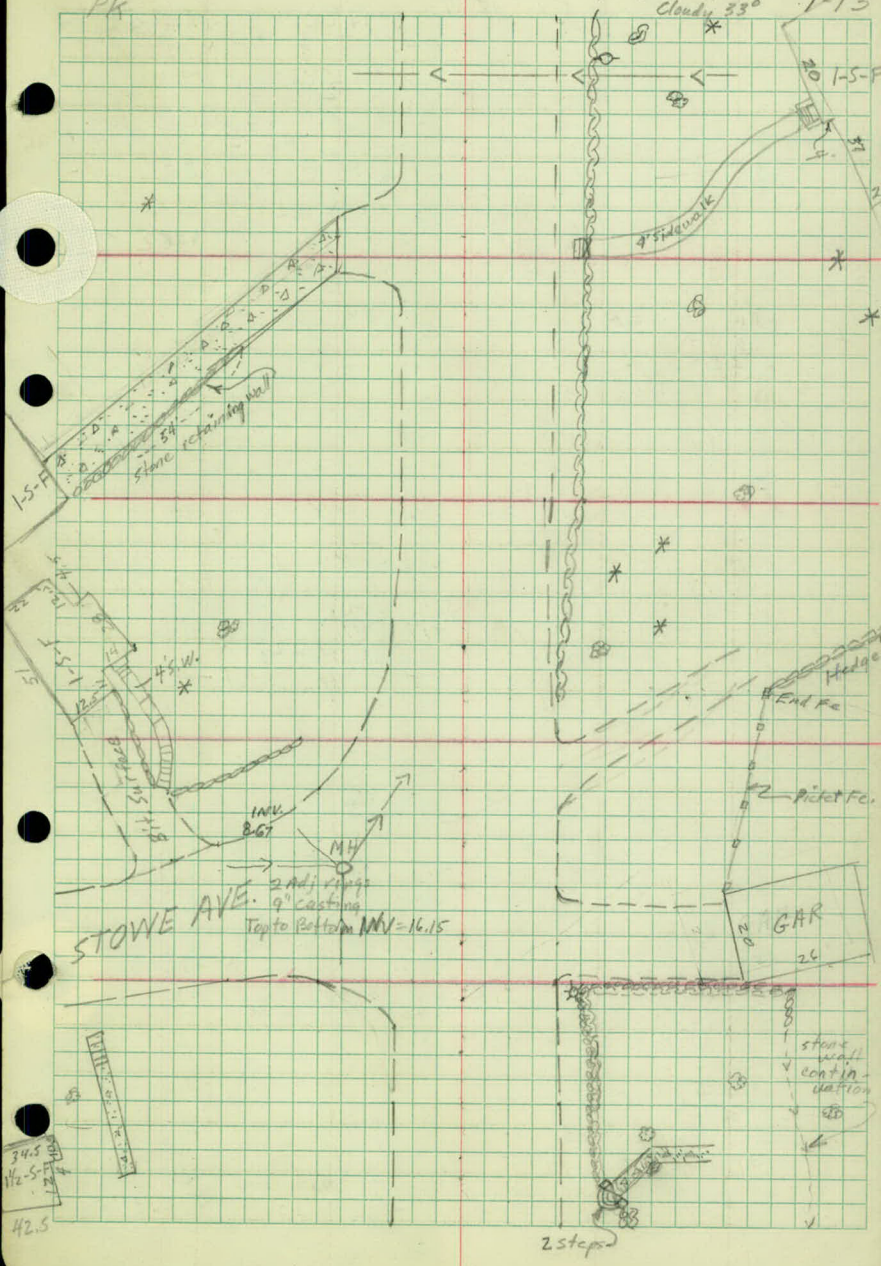
R6
WM
WH
PK

Lt.

A

Dec 10, 1964
Rain PM.
Rt. Dec 11, 1964
Cloudy 33°

T-13
21.3



+50 BT
18 24

+45 14" Cott 58 +50 Lake 73

+39 8" R. post 32

+02 8" BE 73 +01 4" BE 79

+19 6" BE 67 +08 4" BE 79

+08 Bush 32

30

BT 19 25 +02 24" Oak 26 +00 Lake 102

NW cor Cabin

+88 74 RT +73 12" Willow 108

+95 24" Oak 62 +75 BT 22

+64 5" 18" Elm 66 +50 BT 20

+58 3" BE 64 +64 3" Elm 56 +66 12" Cott 100

+51 6" BE 70 +57 3" Steps to Lake 65 RT +11

+61 15" Cott 100 +71 2" 6" Oak 89 +71 5" BE 78

+72 5" Cott 95 +74 4" Cott 92 +76 15" Willow 100

+17 2" Pine 47 +25 2" Pine 56

+16 NW cor Ho 49 RT +01

- BT
16.5 20

+89 4" Elm 29

+60 20' BT Ent - 24' RT +54

+64 SW cor Bar 69 RT +40

+46 SW cor Conc Slab 55 RT +32

+46 Fence 77 +46 Pines 77

+25 6" Spruce 41

+13 6" Spruce 41 +17 4" Spruce 49

28

BT 13 19 +02 Beg 5" Pines 29 RT 27 +79

Dec 11, 1964

T-14

OGR

FL TO TOP CASTING = 10.61
CASTING = 0.75
RINGS = 4

Gravel

LAKE LANE

18" CM

1-S-F

20.6

Picket Fence

Well with Spigot

*

*

33

LX

Z

RT

BT
17 14+00 Lake
69

+93 14" Oak

39
4" Wood Steps

+88 24 37

+54 SE Cedar Ho 76 RT +60 +68 15" Oak 40

+46 Bag Fe 47 to 75 +46 Bag Hedges 30-47

+49 14" Cott 74

+56 12" BE 22

+48 24" Cott 52

+21 18" Cott 27

+18 20" Cott 35

+20 SE Cedar Ho 43 RT +23

+13 10" Oak 22

+00 Lake 75

32

BT
13.5 17

+92 SE Cedar Ho 47 RT +94 +89 MH 20

+87 Stone Wall (1') 37 to 75 RT +91 +64 Steps Sign 23

+85 30" Cott 32

+73 Alley 12' BT 15' Radii

+65 10" BE 44 +65 Stone Wall (1') 38-70 3

+62 20" Cott 35

+49 15" Cott 34 +57 36" Cott 27

+50 8" Cott 35

+40 SE Cedar Ho 47 +42 18" Cott 36

+35 18" Cedar 33

+17 15" Cott 38 +24 15" Cott 38

31 +06 SE Cedar Ho 45 RT +10

BT 16 22 +00 Lake 65

+79 MH 18

+75 Tri 12" Cedar 45

+61 G.R. Post 29 +65 4" Elm 38

+50 G.R. Post 29 +50 3' Wood Steps to Lake 37

RT +42

RS
WM
PK
WH

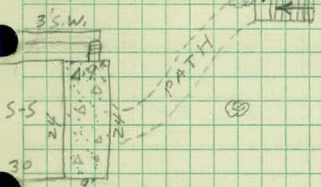
LX

E

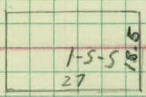
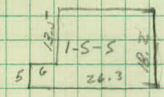
Dec 14, 1964
Rd Cold -5° PC

T-15

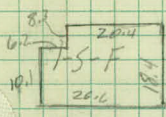
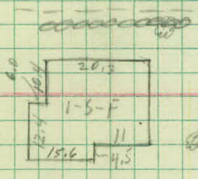
1/2 S-S



8' woven Wood Fe



9' Casting
2ndy Rings
8.62' Inv. to top
MH



11.1.0

MH

9' Casting
4 Adl Rings
10.30 Inv. to top

ORR

GR

LAKE JOHANNA

L4

E

R4

$$+42 \frac{18'' \text{Cott}}{35} +49 \frac{7'' \text{Oak}}{37}$$

$$+47 \frac{\text{End Trees}}{27-40}$$

$$+37 \frac{7'' \text{Oak}}{60}$$

$$+32 \frac{10'' \text{Oak}}{61}$$

$$+19 \frac{10'' \text{BE}}{43} +26 \frac{5'' \text{BE}}{50}$$

BT

Lake

$$17.5 \ 8.5 \ +00 \ 53$$

$$24'' \text{Cott} (20' \text{EXT})$$

$$+99 \frac{18'' \text{Oak}}{49} +96 \frac{\text{Stp}}{46} +75 \frac{\text{MH}}{24}$$

$$+94 \frac{27}{27}$$

$$+90 \frac{8'' \text{BE}}{32} +91 \frac{\text{SE Cor Ho}}{91} \text{ Rt} +83$$

$$+89 \frac{\text{Beg Scattered trees (2-5')}}{29-35}$$

$$+68 \frac{\text{Stp}}{31} +72 \frac{\text{Stp}}{30} +75 \frac{\text{Stp}}{31} +84 \frac{10'' \text{BE}}{32}$$

$$+63 \frac{8'' \text{BE}}{84} +69 \frac{10'' \text{BE}}{33}$$

$$+69 \frac{10'' \text{BE}}{27}$$

$$+45 \frac{6'' \text{BE}}{29} +56 \frac{3'' \text{Wood Steps}}{24-47}$$

$$+28 \frac{4'' \text{Pine}}{71} +49 \frac{6'' \text{Maple}}{75}$$

$$+30 \frac{4'' \text{Wood Steps}}{21-31} \text{ Rt} +33$$

$$+24 \frac{25'' \text{Oak}}{32} +24 \frac{15'' \text{Oak}}{37}$$

$$+14 \frac{14'' \text{BE}}{14}$$

$$+06 \frac{\text{SE Cor Ho}}{81} +19 \frac{16'' \text{Cott}}{47}$$

$$(34) +05 \frac{3'' \text{Pine}}{72} +07 \frac{6'' \text{Rt Post}}{38} \text{ BT } 17.5 \ 10$$

$$+00 \frac{\text{Lake}}{39}$$

$$+99 \frac{6'' \text{Rt Post}}{39} +98 \frac{30'' \text{Cott}}{61}$$

$$+89 \frac{30'' \text{Cott}}{18} +84 \frac{14'' \text{Oak}}{16}$$

$$+75 \frac{\text{SE Cor Ho}}{81} \text{ Rt} +77 \frac{3'' \text{Wood Steps}}{22-46}$$

$$+79 \frac{3'' \text{Wood Steps}}{21-31}$$

$$+68 \frac{\text{Fc Cor Hedge}}{39-100} +73 \frac{4'' \text{Maple}}{39}$$

$$+56 \frac{10'' \text{BE}}{33}$$

$$+47 \frac{4'' \text{Wood Steps}}{27-37}$$

$$+33 \frac{36'' \text{Cott}}{23}$$

$$+25 \frac{\text{Fc Cor}}{37-100} +36 \frac{\text{SE Cor Ho}}{49} \text{ Rt} +37$$

$$+24 \frac{\text{Beg Fc}}{52-100}$$

$$+17 \frac{30'' \text{Cott}}{19}$$

$$+13 \frac{4'' \text{Catalpa}}{40} +24 \frac{\text{Bush}}{40}$$

(33)

BT
17.14

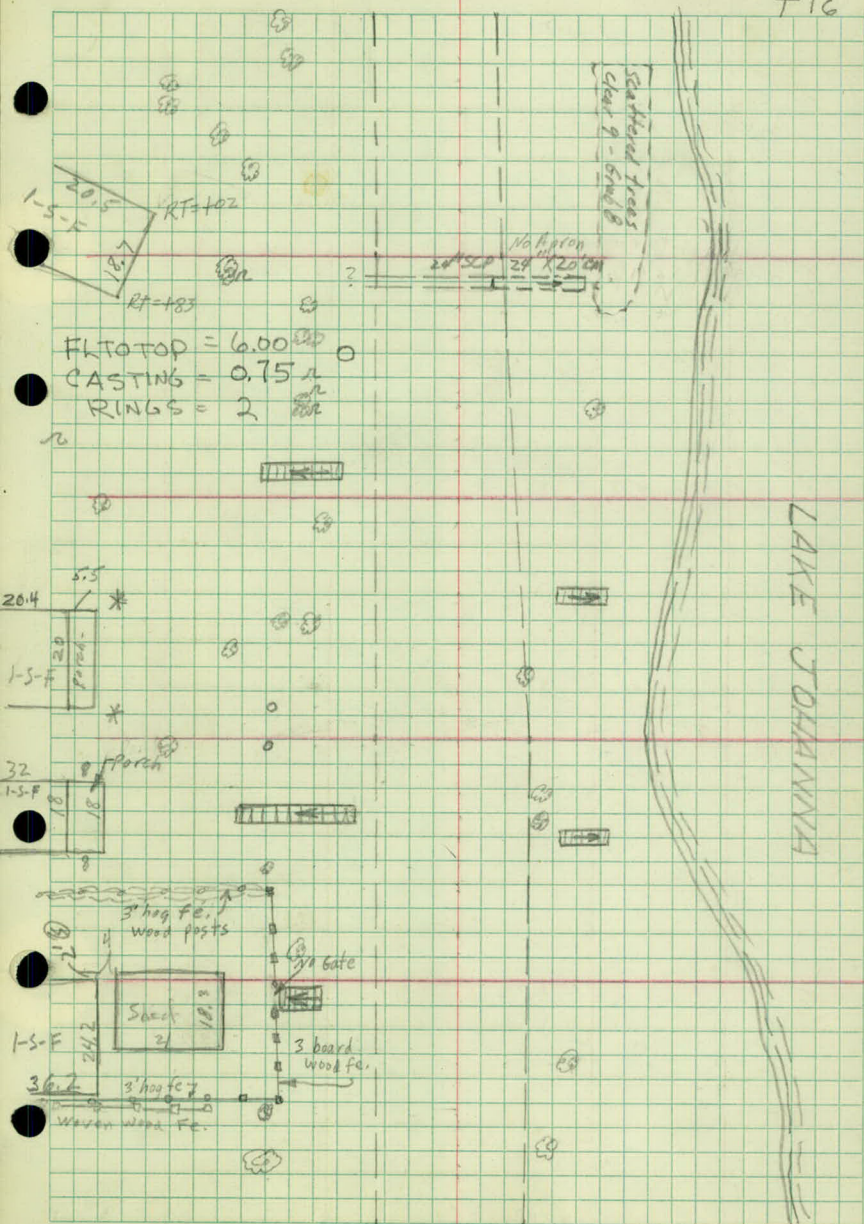
Dec. 14, 1964

24

~~£~~

Rt.

T 16



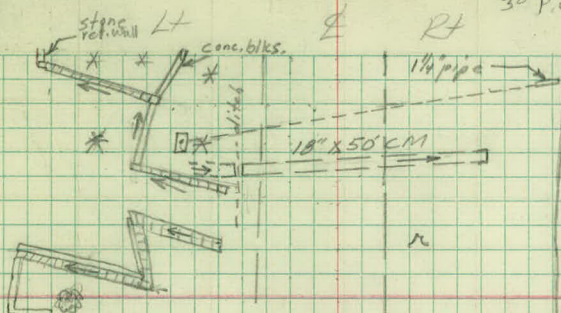
28 Lt RetWall \$
 31 Pine +00 62 BT 1610
 +83 52 +81 28 +80 32 4x3 Pump Well
 " 3' Conc Steps RetWall +00 33
 +89 37-41 Rt+80 33
 18 CM 18 CM 3 Conc Steps
 +77 20 +77 22 +73 23 Rt+69
 Cor RetWall (End) 3 Conc Steps
 +64 44 +62 25 Rt+59
 3 Conc Steps Cor RetWall
 +54 41-68 Rt+51 +54 41-68 Rt+51
 Cor RetWall 60" Coff
 +46 60-68 +49 57
 Bush 3" Pine 1" Pine
 +87 31 +96 27 +97 51
 1" Pine
 +17 38 +19 20 Onk +99 42
 37 Cor RetWall
 +09 50 +10 62 BT
 Cor RetWall 19 9
 39 +06 38
 Lake
 +00 44
 Tri 3" Willow
 +00 25
 13" BE
 +93 14

cor stone wall cor stone wall
 +63 44 Rt+55 +71 40 +76 24" Coff
 5'p 2" Pine top steps 15
 +55 32 +59 46 +69 56 Rt+61
 2" Pine 2" Pine
 +47 62 +48 46
 Quad 15" Coff 2" Pine
 +31 64 +40 54
 12" Coff 12" Coff
 +24 50 +24 55
 Cor RetWall 3 Conc Steps
 +69 46 +76 18-45 Rt+65 +16
 4" Ash 10" Coff 30
 +08 38 +09 41 +23 39 BT
 18 7

36 Quad 10" BE 18" RCP Apron
 +93 48 +98 27 Rt+85
 Apron 18 RCP 24" CM
 +98 33 Rt+84 +94 20
 MTH
 +95 25
 40" Coff
 +90 34
 30" Coff
 +52 10

R6
WM
PK
WH

Dec 15, 1964
30 P.C. Windy



T17

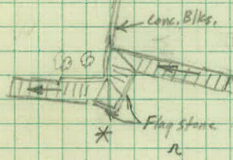
12.15
1.30

LAKE JOHANNNA

5.84

1.28

3.4



MH
29\"/>

8.11

4

Lt
+44 18" Cott
31

Rt
+49 12" Cott
13

40

BT
15 10.5

+100 Lake
47

+100 Brush
31-40

+96 12" Elm
14

+89 6" Ash
39
+90 StP
29
+92 12" Cott
59
Car Steel Steps
End Steel Steps

+69 33
Beg. 3' SW steps
+65 45
Beg. Steel Steps (L')

+55 21-28 +57 26

+45 42
4" Maple
+53 14" Cott
40

+65 Beg Brush
29-38

+57 30" Cott
15

+35 41
+39 45
4" Plum
+43 32

+18 15" Cott
55

+28 40" Cott
11

+13 EAD 15" CM
23

+114 W. EAD 15" CM

39 17

BT
17.5 7

+100 Lake
50

+98 6" Cott
43

Tri 10" BE

+91 45

+83 12" BE

+47 52
10" BE
+86 52
10" BE
+81 StP
36
+49 43
StP
+55 31
StP

+46 21-51
End Ret Wall

+155 to +77 Brush
23-34

+33 59
6" Pine
+42 51
End Ret Wall

+33 38 +36 29

+36 12" CONC. GUTTER
21-175

+23 41
1" Pine

+13 43 +24 49
P.D. RW
End Ret Wall
1" Pine

+20 18" Cott
12

38 +01 52 +06 44
P.D. RW
End Ret Wall

R6
WM
WH
PK

Dec. 16, 1964
5° Windy clear

T 18

4

Willow Brush

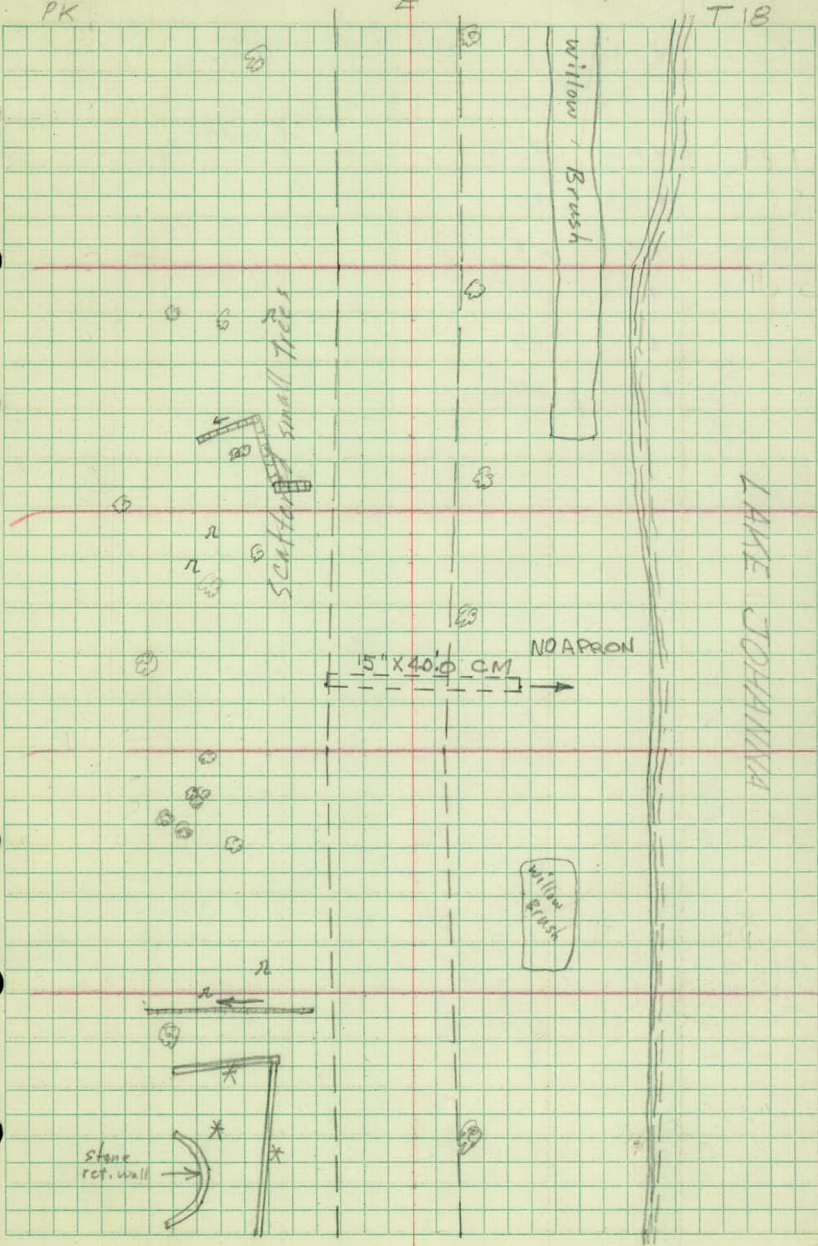
LAKE JOHANNNA

12 ft. long small trees

15' x 40' 0" CM NO APRON

Willow Brush

Stone
rect. wall



44 - 18
+58 23 Lt
43 +27 -37

RT

New Edge Bit

+96 - 65

+77 - 100

+75 - 30

+73 - 40

+70 - 29

+63 - 61

+60 - 20

+57 - 86

Continued

(42) +00 GR 24

BT 17.5 19 +00 GR 25 for 25" Cott Lake 80
+93 12" Willow 45

+54 30" Cott 21 +66 Beg Conc GR 15

+57 Beg Wood GR 22

+32 GR (1) 24 +37 NE 49 Cor to RT +12
+36 End Wall + Hedge 41

+15 Wall 26 +28 Cor Wall 24 RT +14 +07 PP (barwires) 18 +20 20" Willow 30

(41) +04 15" Oak 47 +00 Wall hedge BT 17 11.5 +00 Lake 62
+94 Cor conc wall hedge 29 +95 Beg Wall 34

+99 lilac 36
+84 End Hedge 34

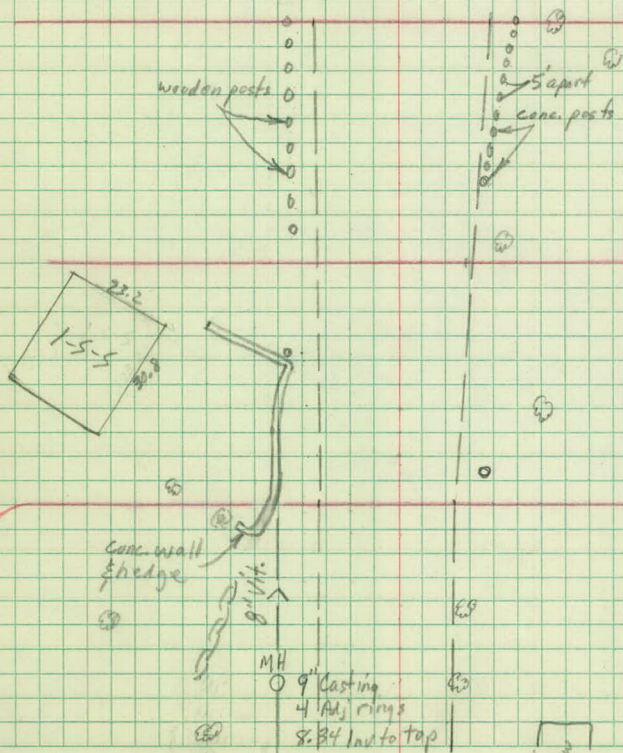
+63 MH 25 +64 Beg Hedge 42 +76 10" BE 60 +64 20" Cott 13 +78 16" Cott 14
+53 15" Cott 40 +55 End Brush 29 -11

Dec 16, 1964

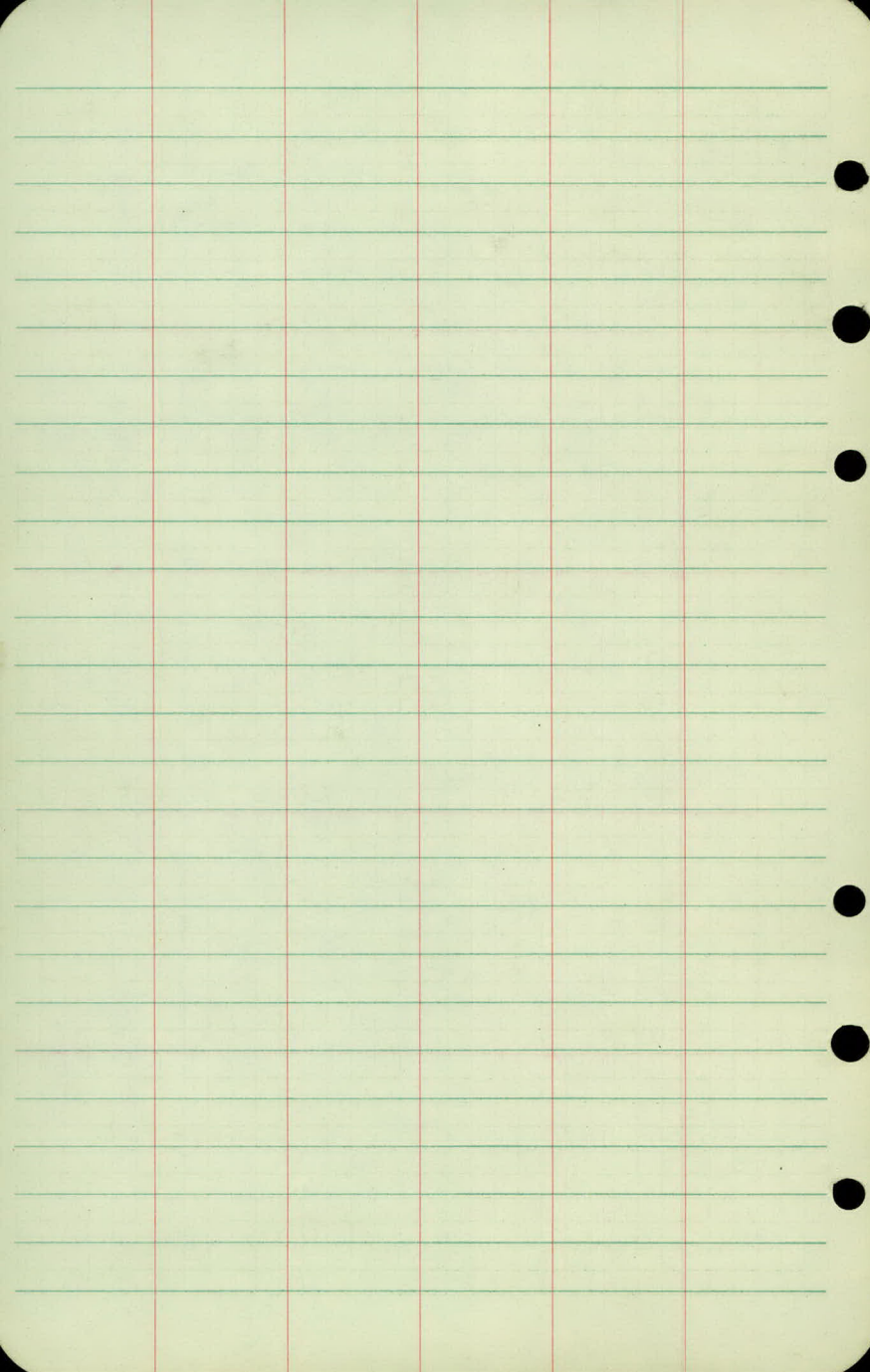
#

T19

Continued



LAKE JOHNNA



TOPOGRAPHY

JOHANNA BLVD.

FROM

Co. Rd. D - Co. Rd. E

EXTENSIONS FROM
STA. 42+00 - 44+00

44+00

+01 R.T. TO LIFT

+84 PP
60'+00 BT
18'+00 BT
14'+00 GR
26'+72 LIFT STATION SECTOR
73'+69 E. RAD.
19'

+50

+21 P.A.R.
35'+12 BT TO L.O. RD E+02 B. RAD.
29'+14 24" ASH
74'

43+00

+04 PP
66'+77 P.O.R.
37'+70 M.H.
29'+00 BT
22'+00 GR
26'+75 E. RAD.
43'+86 36" COT. WOOD
62'+66 BRAD.
19'+55 E. GR. RAIL
24'+62 GUIDE POLE
33'+62 36" COT. WOOD
53'+54 20" WILLOW
49'

42+00

+45 18" WILLOW
71'+40 TWIN WILLOW 20"
77'+34 18" ELM
44'+21 14" ELM
40'+10 24" ELM +12 12" WILLOW
38' 51'

42+00

BT BT
15 20+00
+92+00 CONC. GR. POST +00 6" WILLOW
21' 49'+92 18" COT. WOOD +99 30" ELM
45' 34'

42+00

+67 BE CONC. GR. POST (6' APART)
19'+61 BE GR. RAIL (WOOD) (5' APART)
21'+54 30" COTTON WOOD
22'

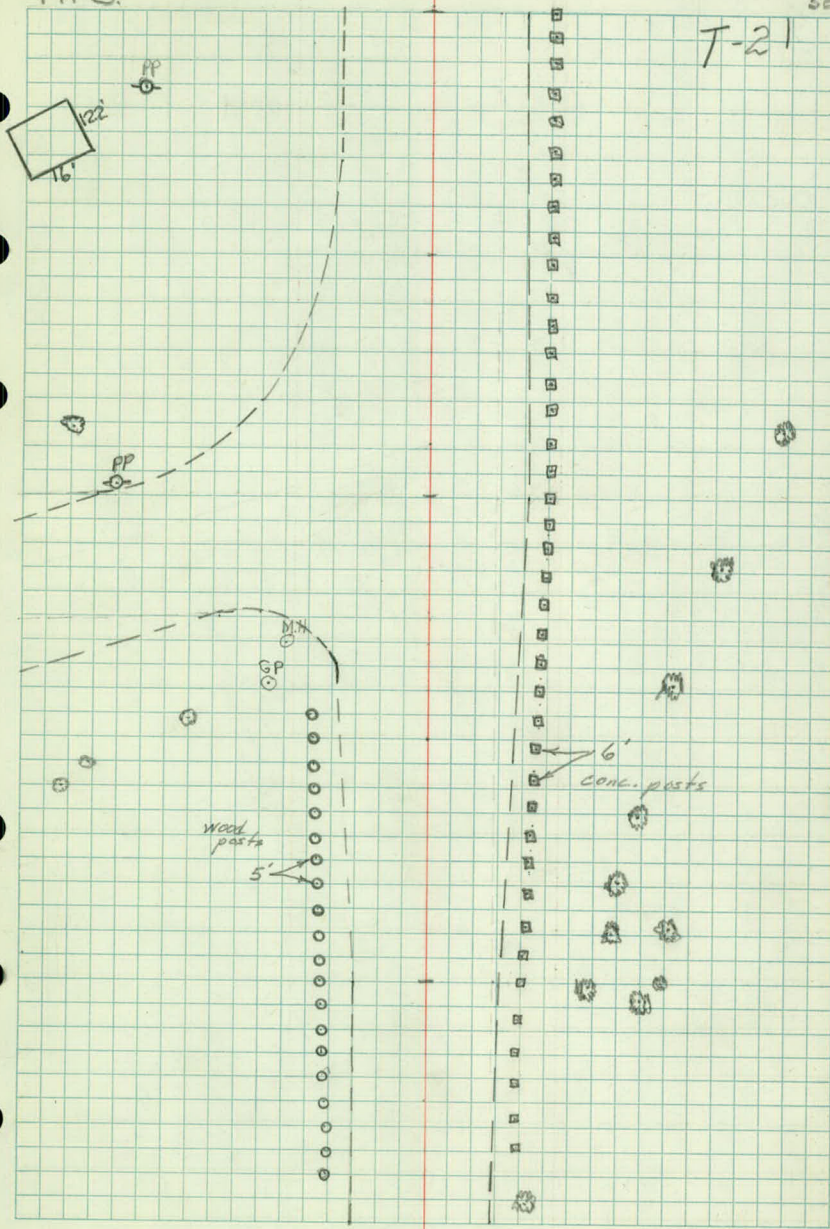
41+50

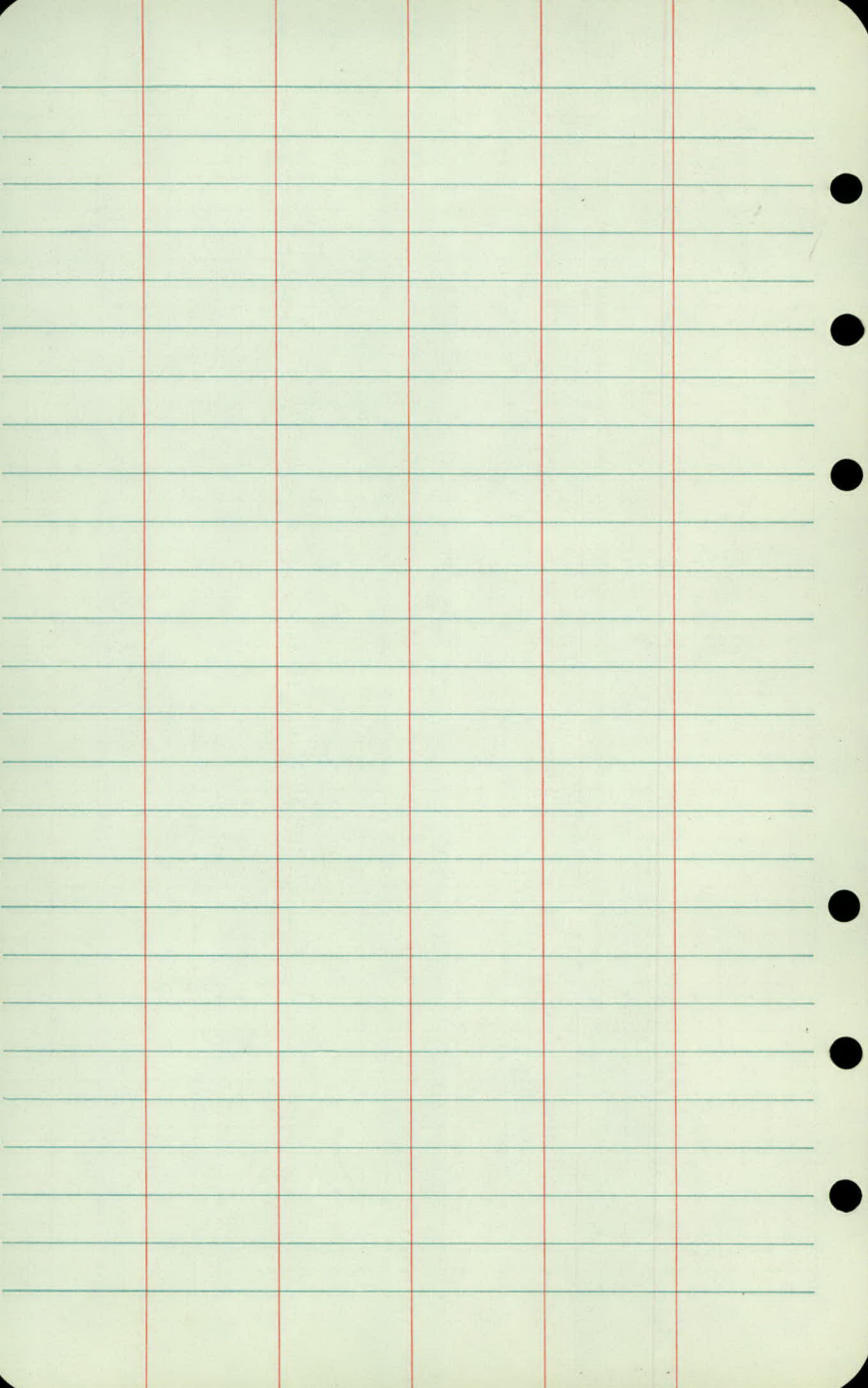
BT BT
15 14

W.S.
W.M.
R.B.

FEB. 17, 1965
SUNNY & WARM
32°

T-21





Feb. 8, 1965

T-22

Sta	+	π	-	Elev
-----	---	-------	---	------

BM	5.03	890.33		885.30
----	------	--------	--	--------

MH			4.70	885.63
----	--	--	------	--------

40			4.77	85.56
----	--	--	------	-------

+25			4.65	85.68
-----	--	--	------	-------

+50			4.53	85.80
-----	--	--	------	-------

+75			4.75	85.58
-----	--	--	------	-------

A1			5.03	885.30
----	--	--	------	--------

BM			7.63	882.70 (882.71)
----	--	--	------	-----------------

A2+70	32' Lt		6.70	883.63
-------	--------	--	------	--------

			7.63	
--	--	--	------	--

PK
WS
WM
PK
LD

Feb. 8, 1965
Cold Clear 3°

T-23

P.K. Nail @ Sta 41+00

Lt. Sta 40+63

Bent.
Spike in 48" Coll S.E. Cor Co. Rd. E & L.J.P.

MH

Sta 42+70 MH 32' LT

FL to top = 8.66

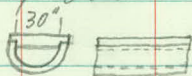
9" Casting

Concentric Cone

4 Adjusting Rings

20+01 Seems to be 2-2' x 15" Vit which empties into 15" CM. This CM is connected to a Manhole which we did not open as it is located on private property at Sta 20+95 Rt 85'

20+84 1/2 - 30" Round culvert to Same Manhole Mentioned above. Property Owner Says MH is 15' deep

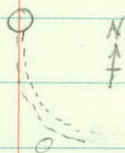


Feb 8, 1965

Sta 22+53

T-24

9/ 15" CM By Lake Johanna is
connected by pipe in an irregular
line to Bee-Hive C.B. Sta 23+12
26' Rt.



Sta 24+74 MH 24' Lt

9" Casting

1.1' of Adjusting Rings

FL to Top = 12.2

Eccentric Cone

Sta 27+04 Rt 21 = MH

9" Casting

3 Adjusting Rings

FL to Top = 14.9'

Eccentric Cone

Sta	+	π	-	Elev
BM	4.63	914.47		909.84

25	£		5.69	
----	---	--	------	--

24+74			6.01	908.46
-------	--	--	------	--------

27+04			7.73	906.74
-------	--	--	------	--------

27	£		8.40	906.07	06.1
----	---	--	------	--------	------

29+34 Patch as sewer Crossing

Sta 33+50 Lt 23' MH

9" Casting

FL to Top Casting = 7.9'

1.5' Adjusting Rings

Eccentric Cone

Feb. 8, 1965

T-25

Top MH Lt 24'

Top MH Lt 21'

Sta 37+25 MH 27' Lt. ✓

9" Casting

F.L. to top = 8.55

1.1' Adjusting Rings

Eccentric Cone

Sta 38+8.6 MH 26' Lt. ✓

9" Casting

FL to top = 9.5

4 Adjusting Rings

Eccentric Cone

STA.	+	Σ	-	ELEV.
B.M.	3.88	891.58		(887.70)
33+50			3.34	888.24
37+25			4.27	887.31
			4.27	
T.P.	3.45	890.76	4.27	887.31
38+86			3.15	887.61
B.M.			5.46	(885.30)

Σ at sta 31+74

to sta 32 0°00'

MH Lt sta 31+90± 308°30' 24'

± 10' Alley 274°45' 16

" " 269°10' 33

" " 270°50' 58

" " 270°55' 59

" " 272°30' 149

FEB 8, 1965

T-26

TOP PK & STA. 34+00

TOP M.H. LT. 23.0'

TOP M.H. LT. 27.0'

TOP NE RIM OF M.H. STA. 37+25

TOP M.H. LT. 26.0'

TOP PK & STA. 41+00

Sta 28+60 Rt is Bit Ent ✓

Sta 34+94 X-Drain

about 14.5' x 24" CM on E. End

28' x 21" Vit xing Road

42.5' Total West End X-Drain

34+93 West End 17' Lt

Sta 36+12 MH 59' Lt ✓

24" x 46' CM No Aprons

RG
WM
DS
PK
LPD

Feb 26, 1965
cloudy 12°

T-27

Johanna Blvd.

Additional M. H. Information

Pages 1-3

Sta	+	-	Elev.
B.M.	5.22	931.58	926.36
M.H.		5.98	926.10
I+00		4.97	926.61
			23.63
B.M.	5.26	903.50	898.24
M.H.		5.93	897.57
30+00		6.88	896.62
			✓ 96.6

Feb 26, 1965

Description

T-28

Top Mont. Co. Rd. "E" & Johanna Blvd.

Top, South rim M.H. Sta 0+24 Rt 12'

P.K. nail &

R.R. Spike in 24" Oak Rt. Sta. 30+25 +

Top East rim M.H. Sta 29+64 Lt. 21'

PK nail &

Description

M. H. Sta. 4+66 Lt 22'

Note: Eccentric type cone, with
vertical side nearest center
line of road.

M. H. Sta. 7+48 Lt. 22'

Note: Eccentric type cone, with
vertical side nearest center
line of road.

M. H. Sta. 17+16 Lt. 23'

Note: Eccentric type cone, with
vertical side to the North.

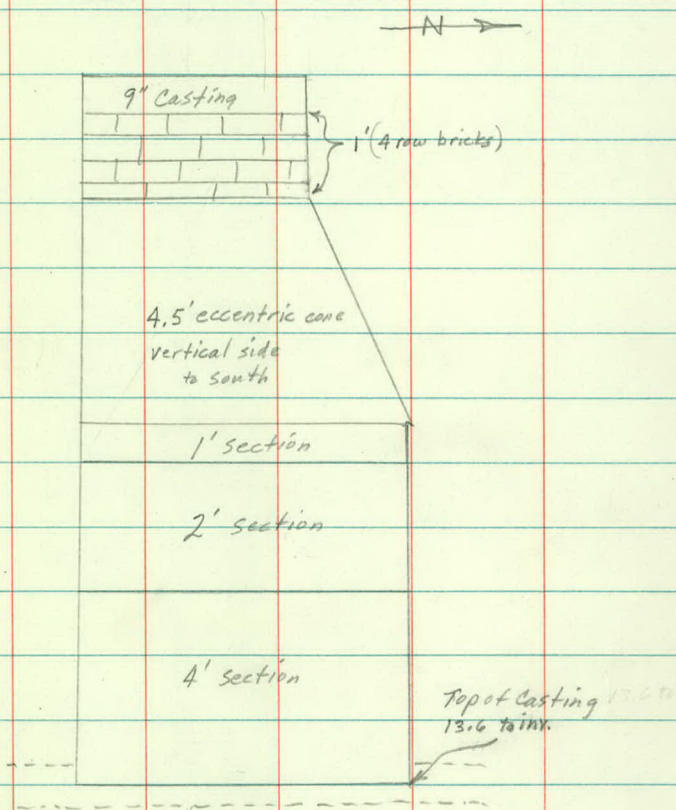


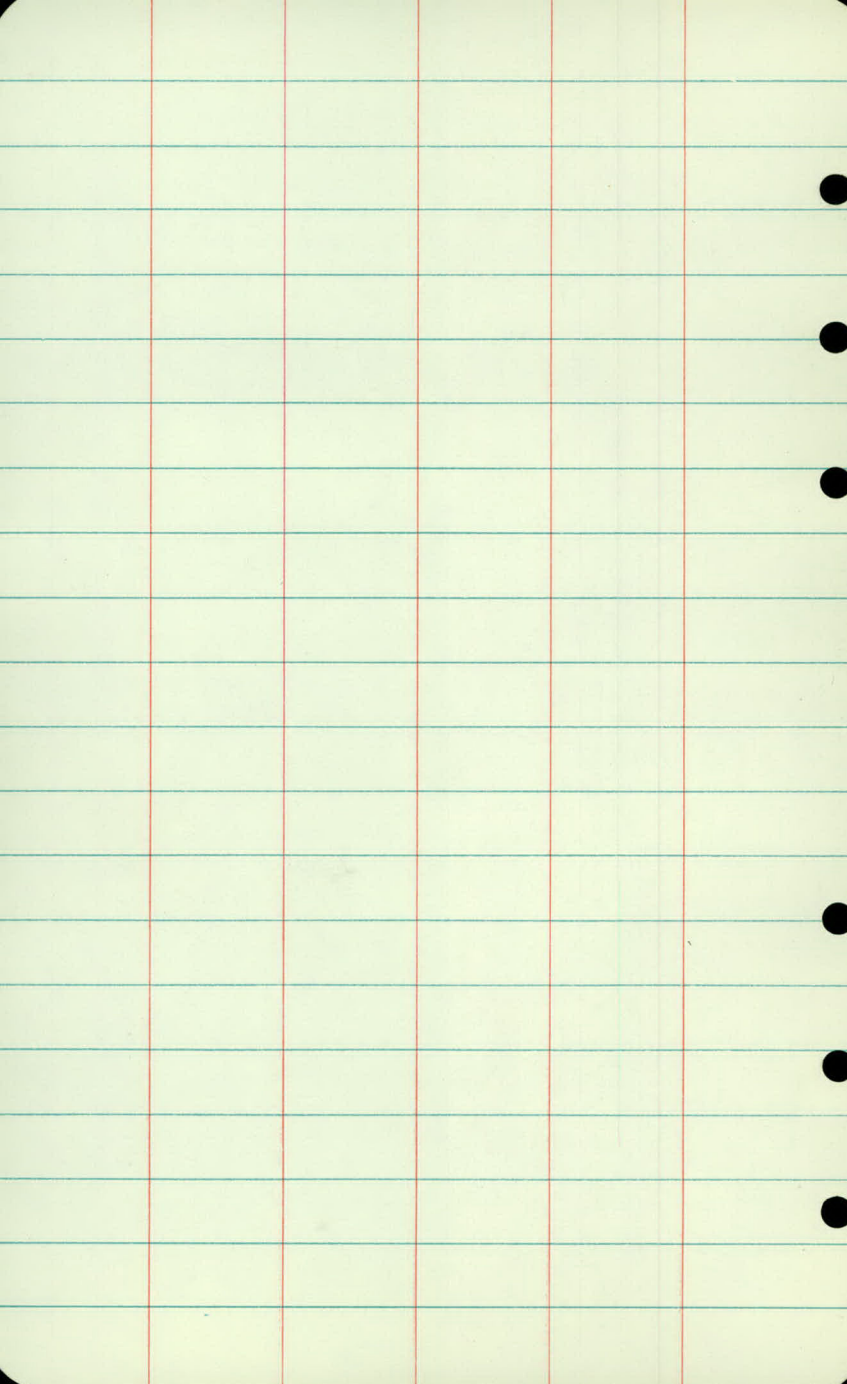
Feb 26, 1965

Description

T-29

M. H. Sta 13+13 Lt 23'





LAKE JOHANNA BLVD.

TOPOGRAPHY

¹/₂
PROFILE

of

STORM SEWER

Sta 20+83 Rt. to Lake Johanna

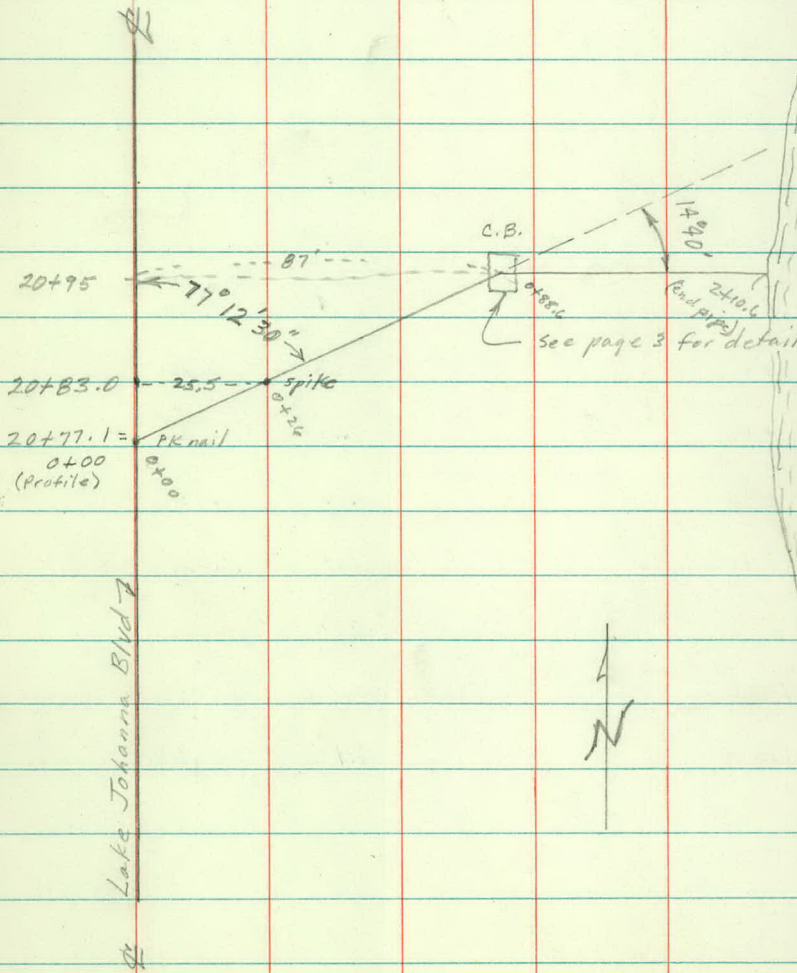
5 pages

Sta	+	π	-	Elv.	Description
BM ₁	1.18	914.60		913.42	
0+00			4.0	910.6	
+09			4.1	10.5	
+19			4.8	09.8	
+26			5.5	09.1	
			9.04	905.56	Top 30" SCP
+47			10.41	904.19	inv 30" SCP
+54			9.9	04.7	
+66			12.3	02.3	
+81			15.4	99.2	
TP ₁	0.48	901.48	13.60	901.00	
+86			5.45	896.03	inv. 22" Vit
+86			4.22	897.26	inv. 30" SCP
+88			3.2	898.3	Top C.B.
+90			5.84	895.64	inv 24" CM ✓
+95			2.9	98.6	
1+00			5.5	96.0	
+14			6.9	94.6	Top Wall
+25			7.7	93.8	Top Wall
+35			7.7	93.8	Top Wall
+35			9.5	92.0	N 6

RG
WM
DS
PK

March 11, 1965
PC 20°

Spike in R.P. 27' Rt Sta 20+03



Sta	+	π	-	Elev
		901.48		
1+58			10.4	91.1
+59			13.5	88.0
TP ₂	0.76	891.78	10.46	891.02
+92			3.9	87.9
+92			5.9	85.9
2+00			6.1	85.7
+05			7.4	84.4
+11			8.38	83.40
+11			10.53	881.25
+16			11.2	80.6
+30			14.8	77.0
+49			15.7	76.1
TP ₂	10.47	901.49	0.76	891.02
TP ₁	13.62	914.61	0.50	900.99
BM ₁			1.18	913.43

913.42

Mar. 12, 1965

Description

3

Top Wall

Bottom Wall

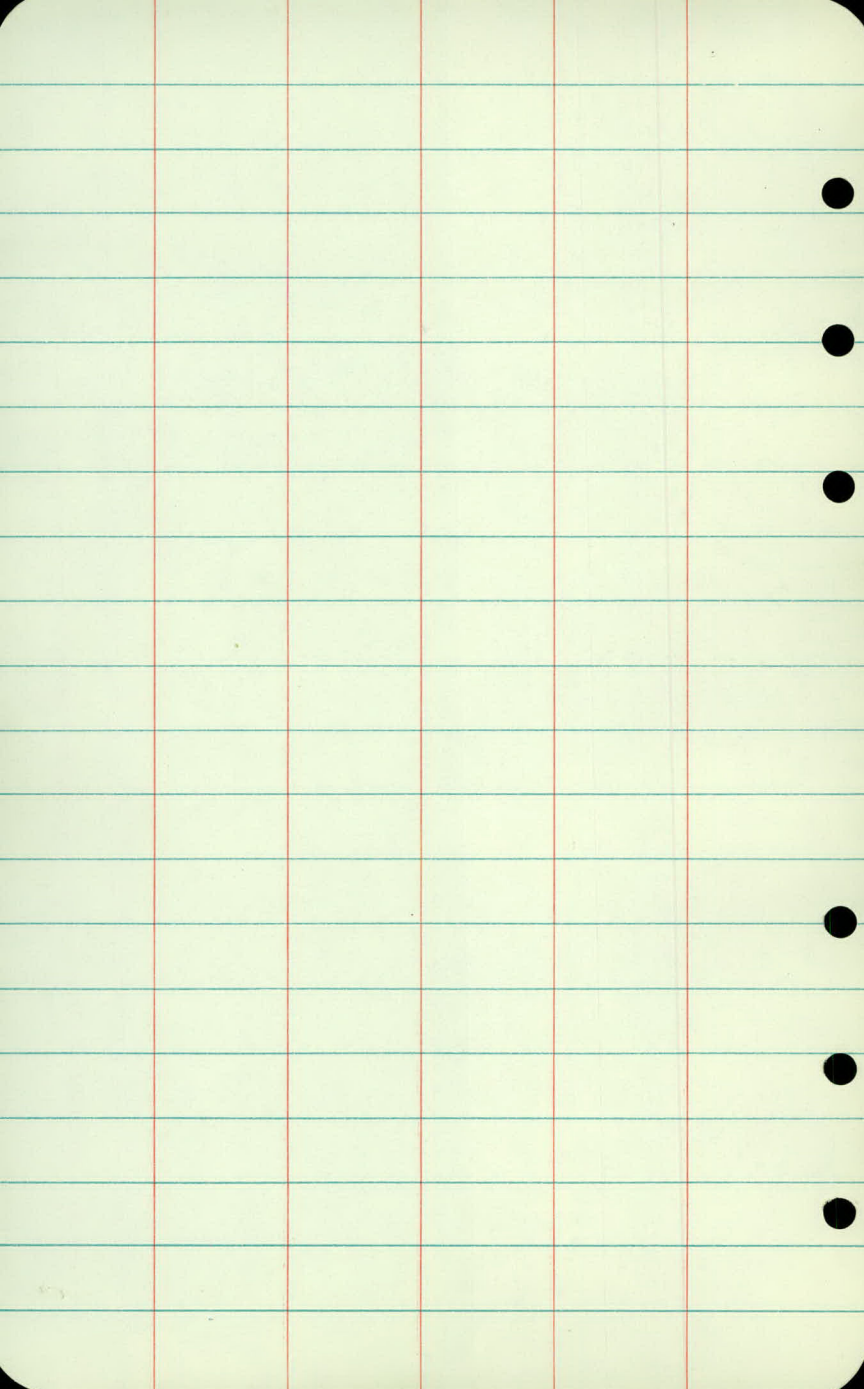
Top Wall

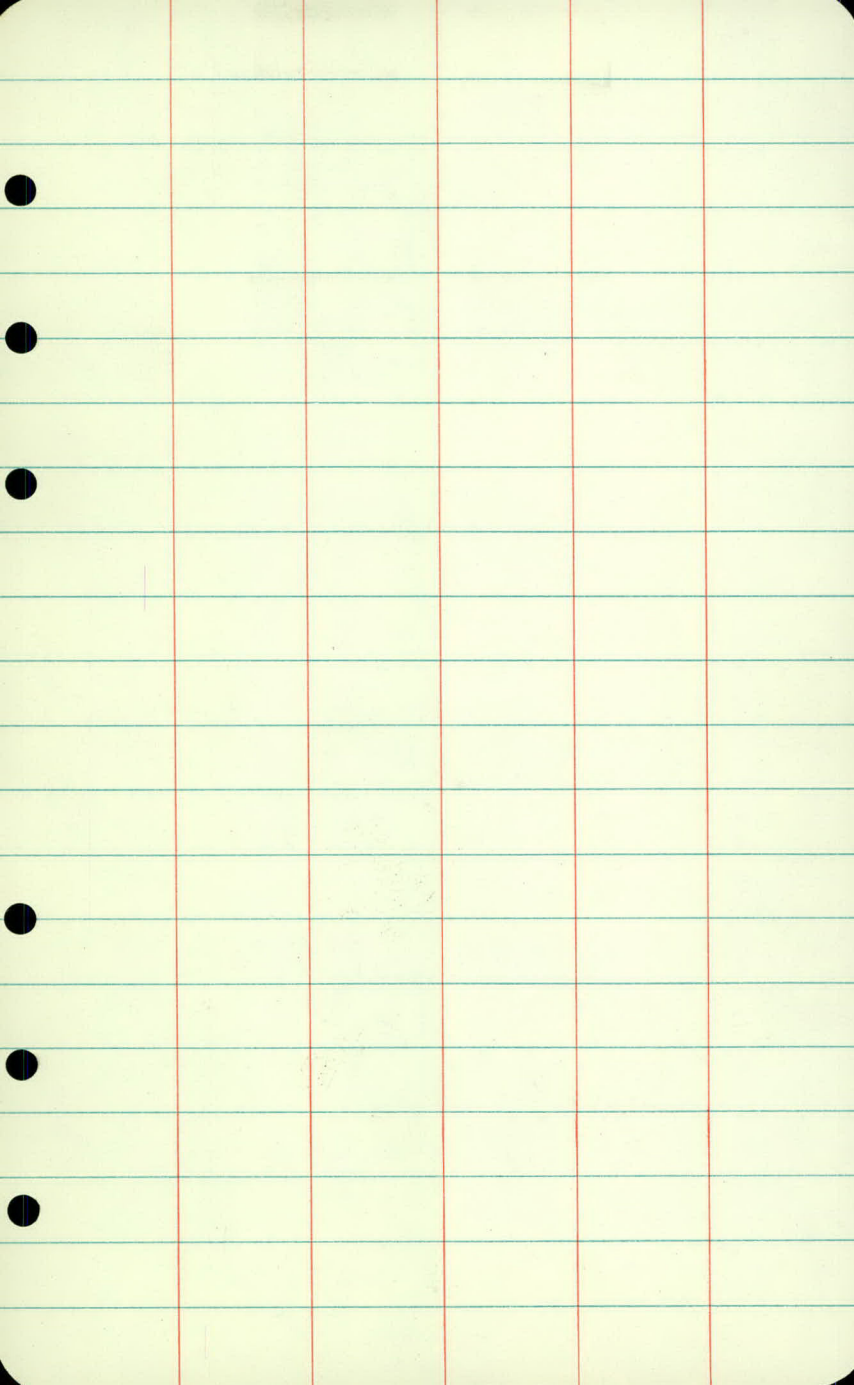
Bottom Wall

Top 24" Vit pipe

Inv. 24" Vit pipe

Lake





March 16, 1965

Sta + T - Elev

T. P. 5.22 896.24 891.02

4.32 91.92

4.06
1.26
2.80
6.32

8.32 87.92

12.84 883.40

TP 5.36 896.38 891.02

6.53 889.85

8.32 888.06

13.00 883.38

CORNER Conc. Block Wall

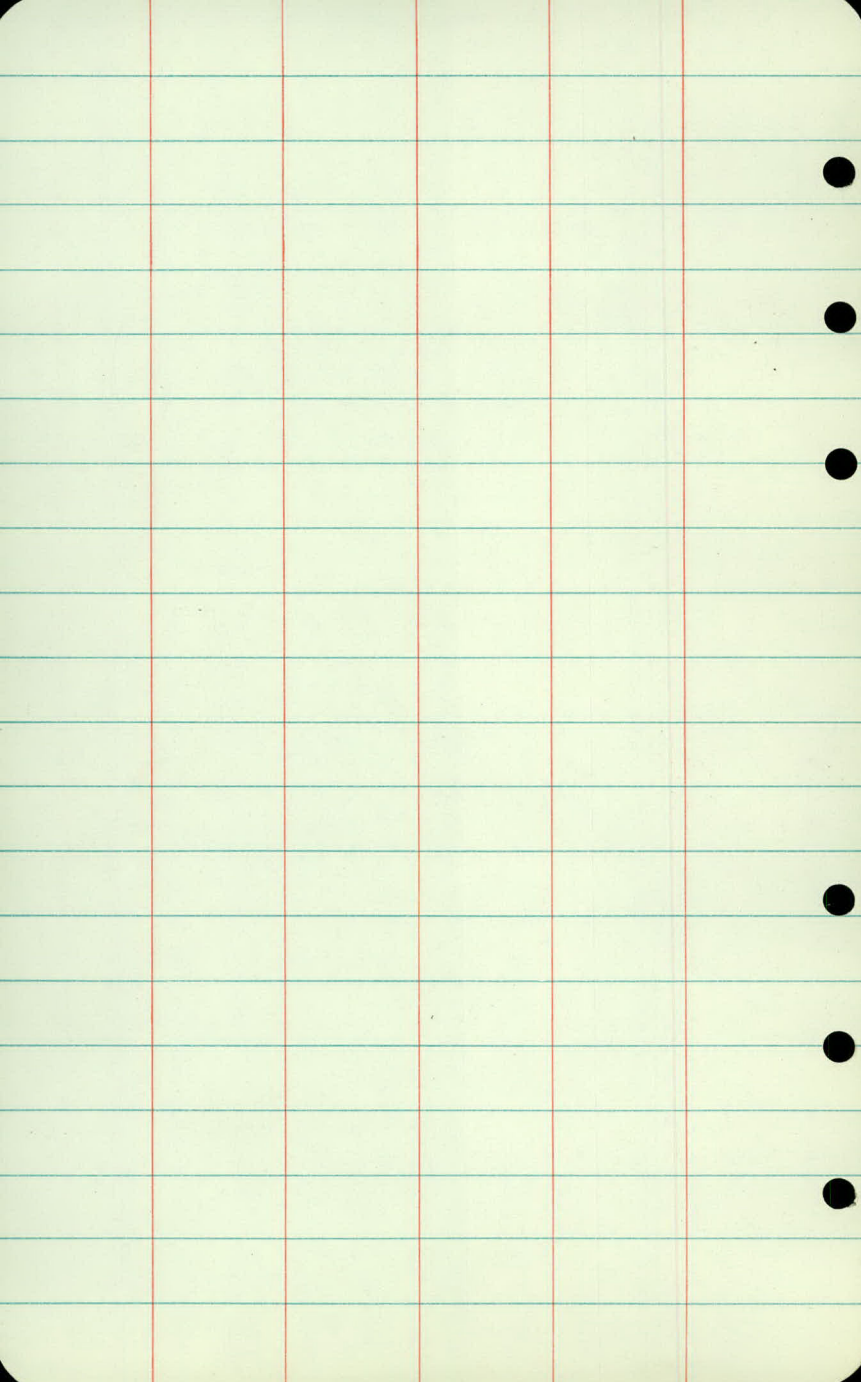
Top of Pipe

Bottom of Catch Basin

Top E. End 24" VIT.

} 77F

Cor. Conc Block wall

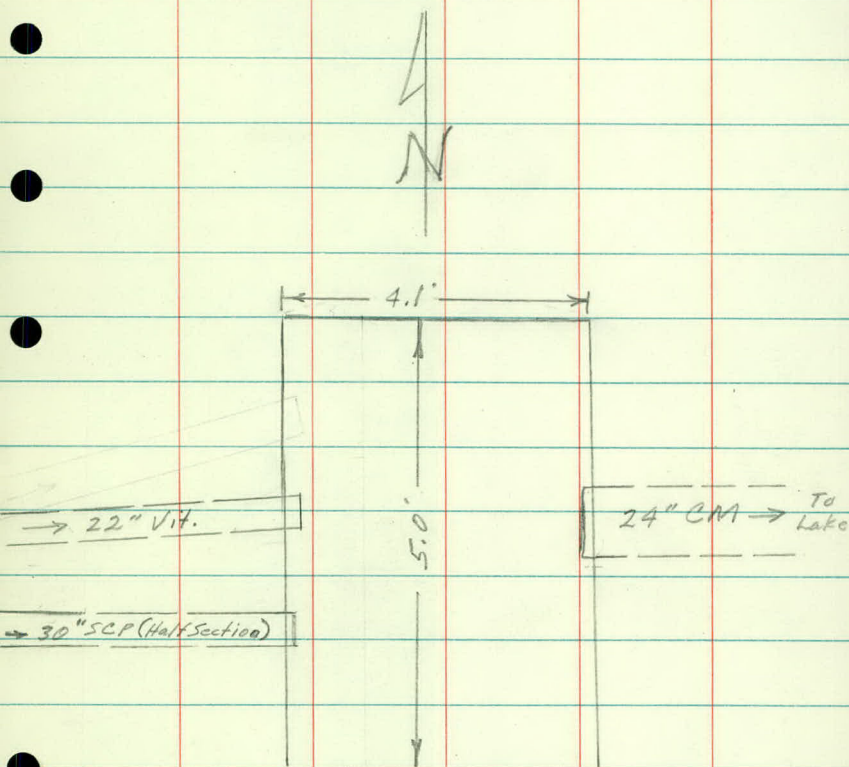


March 11, 1965

Sta. 20+95 Rt. 87'

4

Catch Basin Detail



Note: All brick construction; 6 course high (1.4')

Wooden plank covering.

L+

E

RT

Lake
+46 E

+23 Tw 20" Willow

+10.6 End 24" Vit

+00 Brush

2+00

+00 Wall +07 End Wall

+95 Tw 6" Apple

+93 Prup iron

+44 3' steps +58 Wall cor

+57 24" Cott +00 Wall

+36 SE Cor Ho +36 Req ret. wall

+35 End Wall

+43 12" Oak +56 18" Cott +73 12" Willow

+31 4" Ash

+41 NE Cor Ho +05 NW Cor Ho

+08 SW Cor Ho +10 Wall

+09 12" Elm +09 Wall

1+00 +00 Wall +00 3' SW Cor

+00 Wall

+79 2" Pine +82 3' SW +88 C.B.

+86 6" end 30" Sep +90 24" CM

+76 14" Oak +73 SW +67 End 4 steps

+70 Tw 3" Elm +70 4" Ash +90 5" Apple

+64 3' SW +58 SE Cor Gar +89 SW

+52 4" Elm +53 3" Elm +58 16" Elm

+38 3' SW +58 SW +83 Req Wall

+47 Wend 30" Sep (half section)

+51 PP +39 SW Cor Gar RT+36

+33 NW Cor Gar +52 SE Cor Gar

+86 6" end 22" Vit +96 Wall 5" SW (G)

+13 BT

+29 Tw 12" Willow +96 Req Wall

0+00 +00 BT

+00 BT

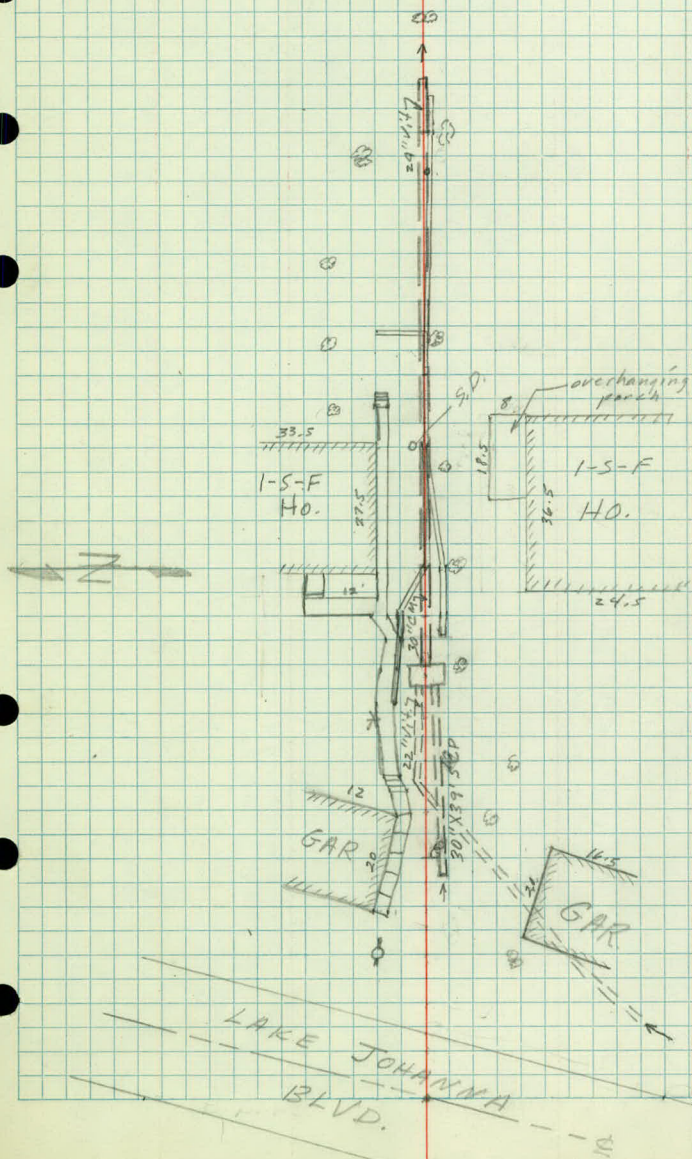
RG
FS
WS
DS
PK

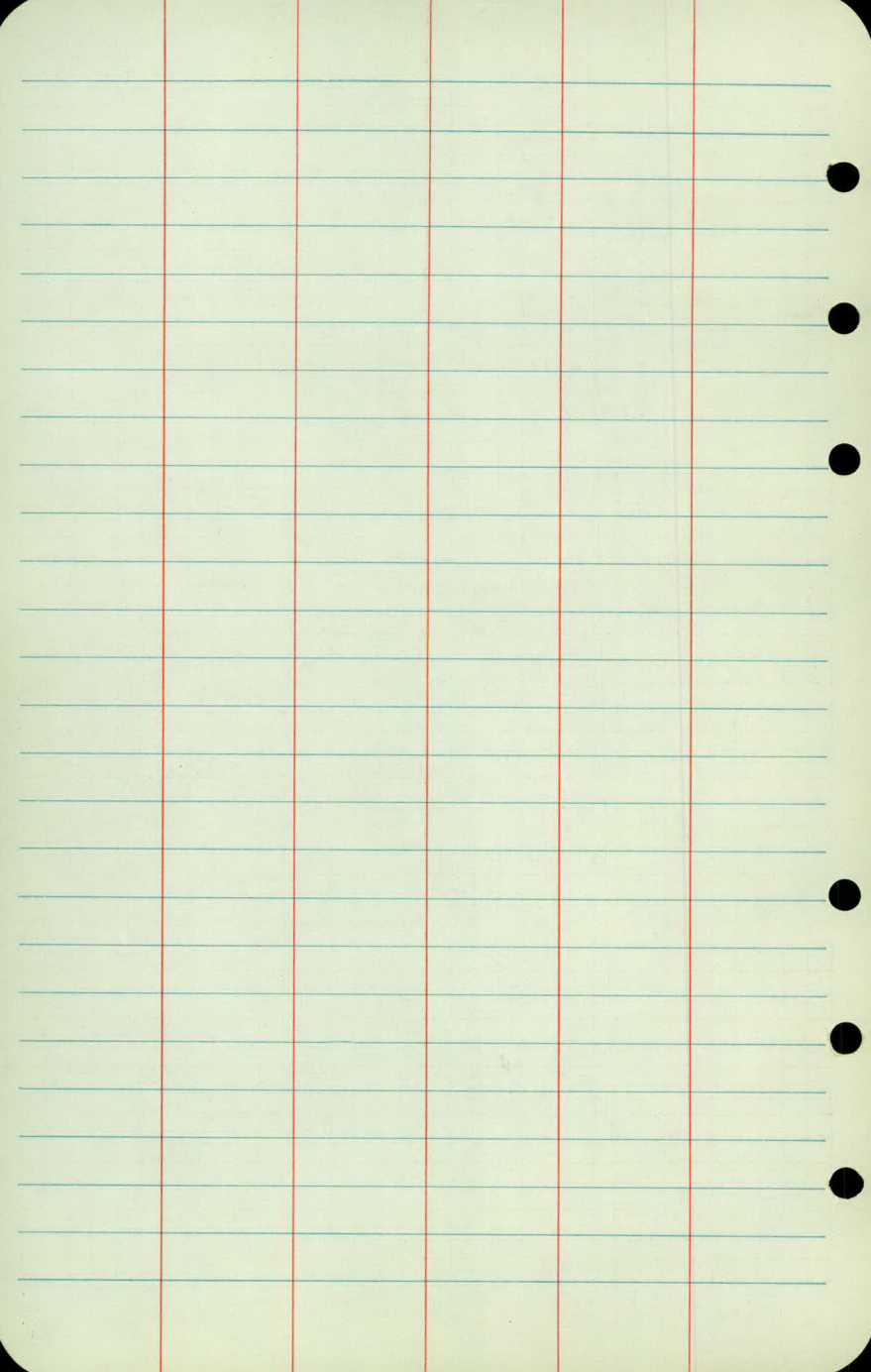
24

LAKE

JOHANNA ^{Rt} -

5





RG
FS
DS
LPD

March 30, 1965
Clear 35°

1

Lake Johanna Blvd.

Proposed Storm Sewer Profile

4 pages

Received & Plotted
3-31-65
Jk

Sta

Pt

23+00

E

+48.5

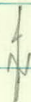
E 10' Easement

22+00

E

March 30, 1965

2



PK nail

87° 26' 15"

Lake Johanna Blvd

20x00

PK nail

PK nail

Sta	+	π	-	EIV
BM	4.91	913.42		908.51
0+00			5.1	08.3
+11			5.2	08.2
+15			5.5	07.9
+28			7.9	05.5
+40			11.2	02.2
+46			13.3	00.1
TP	0.74	900.85	13.31	900.11
+60			5.2	95.6
+79			8.7	92.1
1+00			11.2	89.6
TP	1.55	892.10	10.30	890.55
+18			3.8	88.3
+37			4.8	87.3
+62			5.2	86.9
+75			5.95	86.15
+78			6.0	86.1
+83			6.6	85.5
+83			9.7	82.4
2+00			11.2	80.9

March 30, 1965

3

Spike in PP 27' Rt Sta 23+94

E Lake Johanna Blvd

Top MH 14' RT

Top Wall

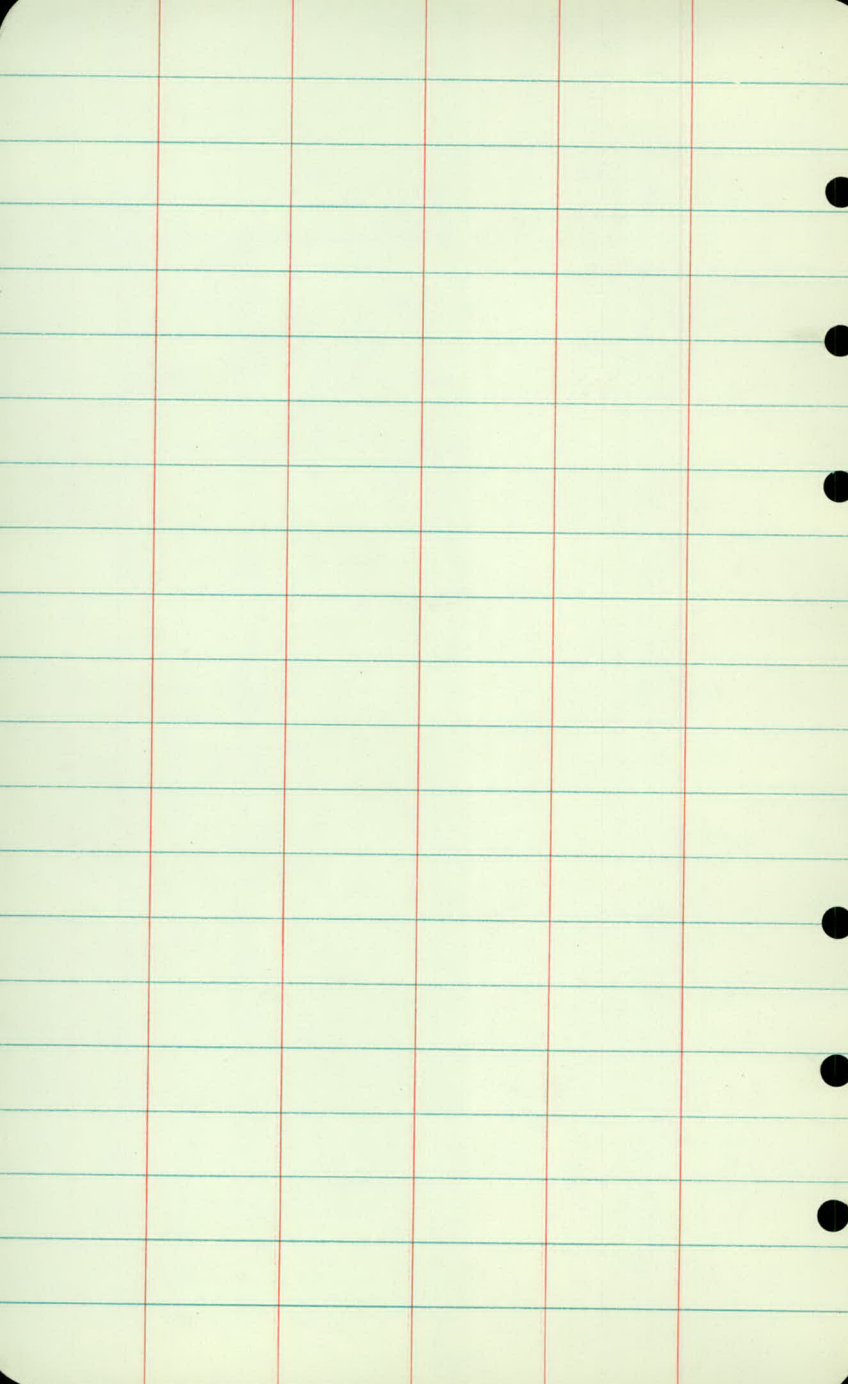
bottom wall

Sta	+	π	-	Elv
		892.10		
2+03			12.52	879.58
TP	12.51	903.06	1.55	890.55
TP	11.79	913.35	1.50	901.56
BM			4.84	908.51
				908.56 (908.51)

March 30, 1965

4

Top 15" CM



KP WH
WM PK
FS
DS

21 DEC. 1964
CLOUDY
25°

3

JOHANNA BLVD.
Co. RD D TO Co. RDE.

X- SECTIONS

0+00 = $\frac{1}{2}$ Co. RD. D & JOHANNA BLVD

STA + π - ELEV.

BM 4.61 930.97

926.36

1+00
0-200

✓

1+50
0-150

✓

1+63
0-137

7.04 923.93

1+85
0-115

4.78 926.19

21 DEC. 1964

LT

£

RT

4

TOP MONT £ CO. RD D & JOHANNA BLVD.

26.3	24.5	25.5	26.0	25.1	25.7	27.1
4.7	6.5	5.5	5.0	5.3	5.3	3.9
29	20-22	13		13	22	33
DITCH						

27.2 26.9
3.8 4.1
51 75

26.6 27.0
4.4 4.0
75 52

26.0	25.0	25.6	26.0	26.1	25.7	26.3	26.1
5.0	6.0	5.4	5.0	4.9	5.3	4.7	4.9
27	22-24	13		13	25	38	62
DITCH							

26.0 26.0
5.0 5.0
50 75

25.8
5.2
75

FL SEND 12" x 45.0 CMP 23.0 LT

TOP TEL MH 13.0 RT

STA

+

K

-

ELEV.

930.97

2+00
0-100

✓

2+08
0-92

6.72 924.25

2+50
0-50

✓

2+69
0-31

5.58 925.39

21 DEC. 1964

LT

±

RT

5

24.9	26.6	25.6	26.3	26.2	25.4	25.0
4.1	4.4	5.4	4.7	4.8	5.6	6.0
63	37	18		14	39	58

27.2

3.8

82

BLDG

24.8

6.2

75

FL N. END 72" X 45.0 CMP 27.0 LT.

24.4	25.5	26.0	26.4	26.2	26.1	25.8
6.6	5.5	5.0	4.6	4.8	4.9	5.2
37-40	35	24		15	39	49
DITCH						BLDG.

26.81

26.42

26.69

27.01

4.16

4.55

4.28

3.96

57

58

77

94

TOP CURB

CONC.

CONC.

CONC.

BLDG

TOP MH 52.0 LT

STA	+	π	-	ELEV.
-----	---	-------	---	-------

930.97

2+70
0-30

5.56 925.41

2+72
0-28

5.01 925.96

2+73
0-27

4.68 926.29

2+76
0-24

7.22 923.75

2+76
0-24

7.39 923.58

2+84
0-16

SHOULDER LINE RT

21 DEC. 1964

LT

£

RT

6

TOP GATE VALVE 58.0 LT

TOP WATER SHUT-OFF VALVE 28.0 RT.

TOP GATE VALVE 50.0 RT.

FL. E. END 18" X 40.0 CMP 63.0 LT

FL W. END 18" X 40.0 CMP 103.0 LT

25.1	26.1	26.7	26.5	26.0	25.8	25.7
5.3	4.9	4.3	4.5	5.0	5.2	5.3
75	37	24		27	53	75

✓

STA	+	π	-	ELEV.
-----	---	-------	---	-------

930.97

0-9			4.90	926.07
-----	--	--	------	--------

BM	5.88	932.24	4.62	926.35	926.36
----	------	--------	------	--------	--------

²⁺⁹⁰
0-10 SHOULDER LINE LT

³⁺⁰⁰
0+00 = $\neq$ CO. RD D

⁺
+19 GUTTER line Ht. Rt.

BM	3.44	931.37	4.31	927.93
----	------	--------	------	--------

21 DEC. 1964

LT

E

RT

7

TOP MH 18.0 RT.

TOP MONT E CO. RD D & JOHANNA BLVD.

26.8	26.0	26.1	26.7	26.5	26.1	25.8	25.6	25.5
6.4	6.2	5.8	5.5	5.7	6.1	6.4	6.6	6.7
75	53	33	18	✓	18	35	58	75

26.1	26.1	26.3	26.8	26.6	26.0	25.7	25.6	25.5
6.1	6.1	5.9	5.4	5.6	6.2	6.5	6.6	6.7
100	75	50	25		25	50	75	100

26.1	26.2	26.6	26.6	26.0	25.9	25.8	25.6
6.1	6.0	5.6	5.6	6.2	6.3	6.4	6.6
125	150	175	200	200	175	150	125

25.6	26.1	26.9	26.7	26.5	26.3	26.0	25.6	25.7
6.6	6.1	5.3	5.5	5.7	5.9	6.2	6.6	6.5
75	64	38	17	✓	12	25	53	75

N.E. COR LOWER STEPHO # 3151 JOHANNA BLVD.

STA

+

 π

-

ELEV.

931.37

BM

4.99 926.38

926.38

0+22

6.85 924.52

0+28

✓

+50

✓

KPPK
FS WH
WM
DS

LT

28 DEC. 1964
CLLOUDY 26° RT 8

TOP MOUNT E CO. RD D; JOHANNA BLVD.

FL 12" CM 36'0 RT

26.6	26.9	26.7	26.6	26.3	26.0	26.37	26.37
4.9	4.5	4.7	4.8	5.1	5.4	5.00	5.05
59	45	18		11	16	28	45
E NEW BRIGHTON RD						CONC.	CONC.

25.2
6.2
75

26.30
5.07
75
CONC.

27.0	26.7	26.7	26.5	26.4	26.1	26.43	26.49
4.4	4.7	4.7	4.9	5.0	5.3	4.94	4.88
54	32	14		12	18	30	33
E NEW BRIGHTON RD						6 CONC	BOTTOM WALL

25.7
5.7
75

27.14
4.0
75

27.14
4.0
47

27.13
4.24
34
TOP WALL

STA

+

π

-

ELEV.

931.37

↓
1+00

✓

↓
+50

✓

↓
+75

✓

28 DEC. 1964

LT

E

RT

9

27.0	27.2	27.0	26.7	26.7	26.4	26.4	26.60	26.65
4.4	4.2	4.4	4.7	4.7	5.0	5.0	4.77	4.72
77	53	25	13		13	18	30	33
ENEW BRKHTON RD						G	CONC	BOTTOM OF WALL

27.7	27.6	27.27
3.7	3.8	4.10
75	54	34
TOP WALL		

28.21	27.5	27.2	27.0	27.1	26.7	26.6	26.88	26.94
3.16	3.9	4.2	4.4	4.3	4.7	4.8	4.49	4.43
47	46	32	15		13	18	30	33
CONC DUMP 15.						G	CONC.	BOTTOM WALL

27.6	27.6
3.8	3.8
62	75

28.0	27.8	27.5
3.4	3.6	3.81
75	57	34
TOP WALL		

27.86	27.81	27.5	27.1	27.2	26.8	26.8	26.72	27.20
3.51	3.56	3.9	4.3	4.2	4.6	4.6	4.65	4.17
49	32	32	14		13	18	29	46
CONC.		CONC.					CONC.	CONC.

27.74
3.63
CONC.
69

STA

+

π

-

ELEV.

931.37

✓
2+00

✓

+19

4.81 926.56

✓
+50

✓

28 DEC. 1964

LT

E

RT

10

26.04	27.6	27.3	27.3	26.9	26.9	26.9	27.3
3.33	3.8	4.1	4.1	4.5	4.5	4.5	4.1
37	31	13		15	28	51	62

TOP ALL
PIPE

28.08	27.96
3.29	3.41
41	43
	BLDG

27.9
3.5
75

TOP CB 22.0 RT

27.6	27.6	27.4	27.0	27.3	26.9	26.7	26.2	26.0
3.8	3.8	4.0	4.4	4.1	4.5	4.7	5.2	4.9
49	42	25	12		11	16	22	39

27.7	28.4	28.26	28.4
3.7	3.0	3.11	3.0
53	63	69	75
		CONC.	

27.8	26.8
3.6	4.6
75	62

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		931.37		
--	--	--------	--	--

3400				
------	--	--	--	--

✓				
---	--	--	--	--

+16				
-----	--	--	--	--

		7.19	924.18	
--	--	------	--------	--

BM				
----	--	--	--	--

	2.08			
--	------	--	--	--

		929.98		
--	--	--------	--	--

		930.01		
--	--	-------------------	--	--

		3.45		
--	--	------	--	--

			927.92	
--	--	--	--------	--

				927.90
--	--	--	--	--------

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

28 DEC. 1964

LT

E

RT

11

27.7	27.3	26.7	26.7	27.1	26.7	26.1	25.9	25.7
3.7	4.1	4.7	4.7	4.3	4.7	5.3	5.5	5.7
62	42	21	11		12	25	49	75

27.9
3.5
75

5.3
2
6.1
118
BLDG

FL 12" SCP 23.0 RT

N.E. COR LOWER STEP HO# 3151 JOHANNA BLVD.

26.1	26.2	26.4	26.3	26.6	26.2	26.1	23.8
3.9	3.8	3.6	3.7	3.4	3.8	3.9	6.2
43	28	18	12		11	17	22-26 DITCH

26.6
3.5
75

5.1
4.9
75

5.7
4.3
47

5.9
4.1
32

STA

+

K

-

ELEV.

929.98
~~930.01~~

3+75

3.6

926.38

4+00

✓

+38

4.34 925.64

+50 ± ENTRANCE LT

✓

28 DEC. 1964

LT

E

RT

12

GROUND AT. 46 # 3155 51.0 LT.

26.2	25.7	25.9	26.0	26.3	26.0	25.1	23.6	24.9
3.8	4.3	4.1	4.0	3.7	4.0	4.3	6.4	5.1
52	29	22	15		11	17	22-26	30

DITCH

26.2
3.8
75

24.6
5.4
75

25.0
5.0
53

FL 15" X 20" CM 22.0 LT (S. END)

25.9	25.9	25.8	25.6	25.9	25.4	24.2	24.3	24.3
4.1	4.1	4.2	4.4	4.1	4.6	7.6	5.7	5.7
74	55	27	14		14	24-28	34	55

DITCH

26.09
3.92
94
conc.
GA APRON

24.1
5.9
75

STA

+

T

-

ELEV.

~~929.98~~
~~930.01~~

4+58

4.89 925.09

+66

5.50 924.48

5+00

✓

+09

6.62 923.36

+20

± ENTRANCE LT

13

26.57	26.0	26.0	26.6	26.8	26.3	26.9	26.4	26.8
3.44	3.6	4.0	5.0	5.4	5.2	5.7	9.1	10.6
128	69	41	17	11		14	26	48
conc.								
GA APR 01								

STA

+

T

-

ELEV.

~~929.98~~
~~930.01~~

5+29

6.94 923.04

+50

✓

+70

7.61 922.37

+82 ⊥ ENTRANCE LT

✓

28 DEC. 1964

LT

E

RT

14

FL 15" X 20' CM 22.0 LT

26.0	23.8	24.1	24.0	24.3	24.0	20.3	18.2	17.2
4.0	6.2	5.9	6.0	5.7	6.0	9.7	11.8	12.8
32	21-23	20	11		13	30	43	58

DITCH

26.9

26.74

27.2

17.1

3.1

3.27

2.8

12.9

64

73

79

75

S.W.

40

FL S. END 15" X 24.0 CM 21.0 LT

27.14

25.4

24.0

23.7

22.9

23.9

23.2

19.0

16.5

287

4.6

6.0

6.3

6.1

6.1

6.8

11.0

13.5

91

43

18

11

12

17

30

43

Conc
GA. APRON

14.4

14.9

15.6

15.1

75

64

STA	+	π	-	ELEV.
-----	---	-------	---	-------

STA	+	π	-	ELEV.
-----	---	-------	---	-------

~~929.98~~
~~930.01~~

STA	+	π	-	ELEV.
-----	---	-------	---	-------

5+94

STA	+	π	-	ELEV.
-----	---	-------	---	-------

8.20 921.76

STA	+	π	-	ELEV.
-----	---	-------	---	-------

TP

STA	+	π	-	ELEV.
-----	---	-------	---	-------

6.27

STA	+	π	-	ELEV.
-----	---	-------	---	-------

~~927.00~~
~~927.03~~

STA	+	π	-	ELEV.
-----	---	-------	---	-------

9.25

STA	+	π	-	ELEV.
-----	---	-------	---	-------

~~920.73~~
~~920.76~~

STA	+	π	-	ELEV.
-----	---	-------	---	-------

(920.73)

STA	+	π	-	ELEV.
-----	---	-------	---	-------

6+00

STA	+	π	-	ELEV.
-----	---	-------	---	-------

✓

STA	+	π	-	ELEV.
-----	---	-------	---	-------

+40

STA	+	π	-	ELEV.
-----	---	-------	---	-------

✓

28 DEC. 1964

LT

E

RT

15

FL N. END 15" x 24.0 CM 21.0 LT

SPIKE IN PP 28.0 RT STA 6+19

23.9	22.9	23.0	23.3	23.6	23.4	23.1	17.0	15.1
3.1	4.1	3.5	3.7	3.4	3.6	3.9	10.0	11.9
28	21-23	17	11		10	16	32	45
DITCH								

25.3	26.4	26.9
1.7	0.6	0.1
46	63	75

12.7	14.2
14.3	12.8
75	63

23.1	22.5	22.8	22.8	23.0	22.8	22.4	17.0	15.6
3.9	4.5	4.2	4.2	4.0	4.2	4.6	9.4	11.4
32	22-24	18	10		10	17	30	38
DITCH								

24.2	25.3
2.8	1.7
50	75

11.9	13.5
15.1	13.5
75	54

STA

+

π

-

ELEV.

927.00
~~927.03~~

6+76

✓

7+00

✓

+25

5.50

437 ± ENTRANCE AT

28 DEC. 1964

LT

E

RT

16

22.5	22.6	22.6	22.8	22.6	22.2	22.0	16.1
4.5	4.4	4.4	4.2	4.4	4.8	8.0	10.3
21-23	17	9		10	18	28	45
DITCH							

22.1	24.2	25.4
3.9	2.8	1.6
29	53	75

13.9
13.1
75

23.1	22.1	22.4	22.5	22.7	22.5	22.1	18.7	18.4
3.9	4.9	4.6	4.5	4.3	4.5	4.9	8.3	8.6
27	20-22	17	10		9	16	28	46
DITCH								

24.1	25.1	26.0
2.9	1.9	1.0
34	57	75

15.0	16.7
12.0	10.3
75	62

S. END 15" X 20' CM 20.0 LT

23.3	22.3	22.9	22.9	22.1	22.1	22.3	22.0	22.7	22.7	22.9	22.9
0.7	1.7	3.1	4.1	4.6	4.6	4.7	5.0	7.3	8.3	7.7	9.2
94	65	30	16	9		12	18	27	30-34	36	52
DITCH											

12.5
75

STA

+

T

-

Elev.

927.00
927.03

7+45

5.89 921.11

+48

4.82 922.18

+70

✓

8+00

✓

28 DEC. 1964

LT

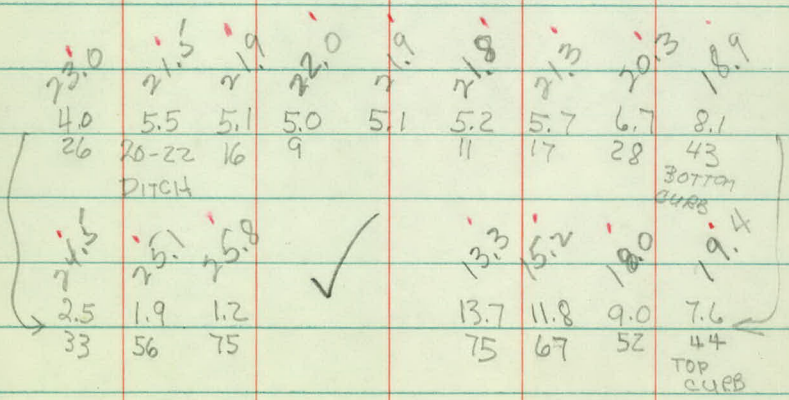
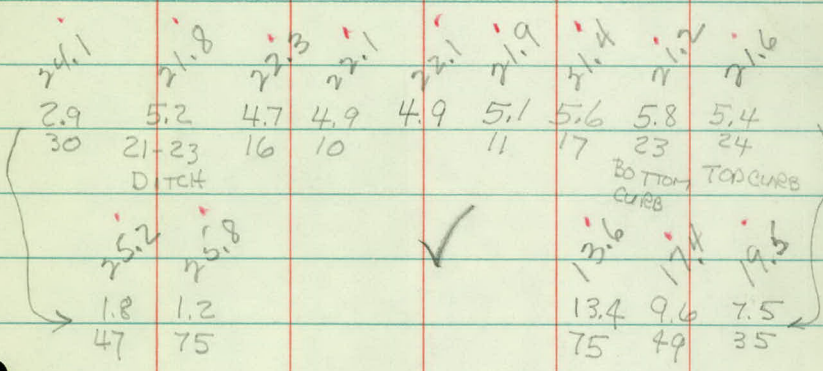
E

RT

17

N. END 15" X 20' CM 20.0 LT

TOP MH 22.0 LT



STA

+

T

-

ELEV.

~~927.00~~~~927.03~~

8+23

6.35 920.65

+33

⊥ ENTRANCE LT

✓

+43

6.56 920.44

TP

6.47

~~925.87~~~~925.89~~

7.61

~~919.39~~~~919.42~~

(919.40)

+66

28 DEC. 1964

LT

±

RT

18

FL 15" X 20.0 CM 20.0 LT

73.8	73.3	72.4	71.9	71.8	71.6	71.4	70.6	70.1
3.2	3.7	4.6	5.1	5.2	5.4	5.6	6.4	9.3
55	36	21	11		10	17	26	43

71.6
7
2.4
75

✓

13.9 15.6 15.2 16.7
13.1 11.4 11.8 10.3
75 70 69 52
TOP BOTTOM ± EUT.
CURB CURB

FL N.END 15" X 20.0 CM 20.0 LT

SPIKE IN PP 28.0 RT STA 10+46

25.0	24.0	22.3	21.0	21.7	21.6	21.6	21.5	21.3	21.1	20.8	20.7	20.6
0.9	1.9	3.6	4.9	4.2	4.3	4.3	4.4	4.6	8.8	8.1	9.2	10.4
75	46	27	20-22	15	11		10	16	31	38	49	55
			Ditch									
										13.5	14.2	
										12.4	11.7	
										76	63	

STA

+

T

-

ELEV.

~~925.89~~
925.87

8+97

5.82 920.05

9+07 ± ENTRANCE LT

✓

+17

6.24 919.63

+29

✓

TD

6.36

~~925.76~~~~925.78~~

6.47

919.42

(919.40)

28 DEC. 1964

LT

E

RT

19

FL S.END 15"X20.0 CM 21.0 LT

23.30	22.10	21.6	21.4	21.4	21.2	21.0	16.6	16.4
259	379	43	45	45	47	49	93	95
49	30	19	12		11	16	30	33
conc.	conc.							

24.75		12.8	14.3	15.5	16.1
1.14		13.1	11.6	10.4	9.8
75		75	61	48	44

FL N.END 15"X20.0 CM 21.0 LT

20.5	19.9	20.3	20.9	21.0	21.3	21.1	20.9	16.7	15.4	14.3
5.4	6.0	5.6	5.0	4.9	4.6	4.8	5.0	9.2	10.5	11.6
32	24	26	23	15	10	11	16	28	33	52

DITCH

21.9	23.5	12.2
4.0	2.4	13.7
54	75	75

SPIKE IN PP 28.0 RT STA 10+46

STA

+

T

-

ELEV.

925.76
925.78

9+63

✓

+93 = 18" CM LT & RT

✓

6.29 925.69 925.71 6.36 919.42 919.40

KPPK
WM WH
FS
DS

LT

29 DEC 1964
FOGGY 29°
RT

20

20.0	18.7	20.4	20.1	20.9	20.8	20.6	16.3	13.4
5.8	7.1	5.4	5.1	4.9	5.0	5.2	10.5	12.4
45	24	16	10		10	16	28	35

21.8	23.1	10.3	11.0
4.0	2.7	15.5	14.8
6	75	75	60

16.43	18.0	20.3	20.6	20.6	20.5	20.2	16.3	12.20
9.35	7.8	5.5	5.2	5.2	5.3	5.6	9.5	13.58
21.4	21	16	7		10	16	25	30

FL W. END

18" X-CULVERT

FL E. END

18" X-~~DR~~ CULVERT

17.5	18.7	20.6	21.8
8.3	7.1	5.2	4.0
25	42	61	75

09.9	12.0
15.9	13.8
75	45

SPIKE IN PP 28.0 RT STA 10+46

ck by

W.M.
F.S.

STA

+

π

-

ELEV.

925.69
~~925.71~~

10+00

✓

+25

6.65 919.04

+38 ENTRANCE LT

✓

KP
WM
WH
PK

LT

E

30 DEC. 1964
SNOW
30°

RT

21

18.5	20.3	20.5	20.6	20.4	20.1	16.6	13.8
7.2	5.4	5.2	5.1	5.3	5.6	9.1	11.9
23	16	12		11	15	23	31

17.9	18.5	20.3	21.5		9.7	11.4
7.8	7.2	5.4	4.2		16.0	14.3
26	39	58	75		75	51

TOPMAH 24.0 LT

21.3	20.5	20.4	20.8	20.8	20.4	20.3	16.8	13.3
4.4	5.2	5.3	4.9	4.9	5.3	5.4	8.9	12.4
68	40	18	11		11	16	24	33

21.5	22.4	23.39	23.64		24.2	10.2
4.2	3.3	2.30	2.05		17.5	15.5
75	100	120	131		75	53

conc con
SA APRON

STA

+

T

-

ELEV.

~~925.71~~
925.69

10+61

✓

6.29

~~925.71~~
925.69

6.29

919.42

(919.40)

11+00

✓

30 DEC. 1964

LT

±

RT

22

20.6	20.5	20.6	20.8	20.9	20.6	20.5	17.1	17.8
5.1	5.2	5.1	4.9	4.8	5.1	5.2	8.6	12.9
34	27	20	12		10	18	28	37

BOTTOM WALL

22.26	20.9	22.56	21.3	22.95	8.1	10.1
3.43	4.8	3.13	4.4	2.74	17.6	15.6
34	56	56	75	75	75	58

TOP WALL BOTTOM WALL TOP WALL BOTTOM WALL TOP WALL

SPIKE IN PD 28.0 RT STA 10+46

20.9	20.8	20.7	20.9	21.1	20.8	20.2	17.1	13.7
4.8	4.9	5.0	4.8	4.6	4.9	5.5	8.6	12.0
32	25-27	17	10		13	19	27	37

DITCH

22.4	23.5	23.9	07.8	10.7
3.3	2.6	1.8	17.9	15.0
36	56	75	75	59

STA.	+	Σ	-	ELEV.
------	---	----------	---	-------

		925.69		
		925.71		

11+45				
-------	--	--	--	--

✓				
---	--	--	--	--

+58				
-----	--	--	--	--

✓				
---	--	--	--	--

TP	7.14	929.08		921.94
		929.10	3.75	921.96

12+00				
-------	--	--	--	--