

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

COUNTY ROAD "H"

From Long Lake Rd To T.H. 10

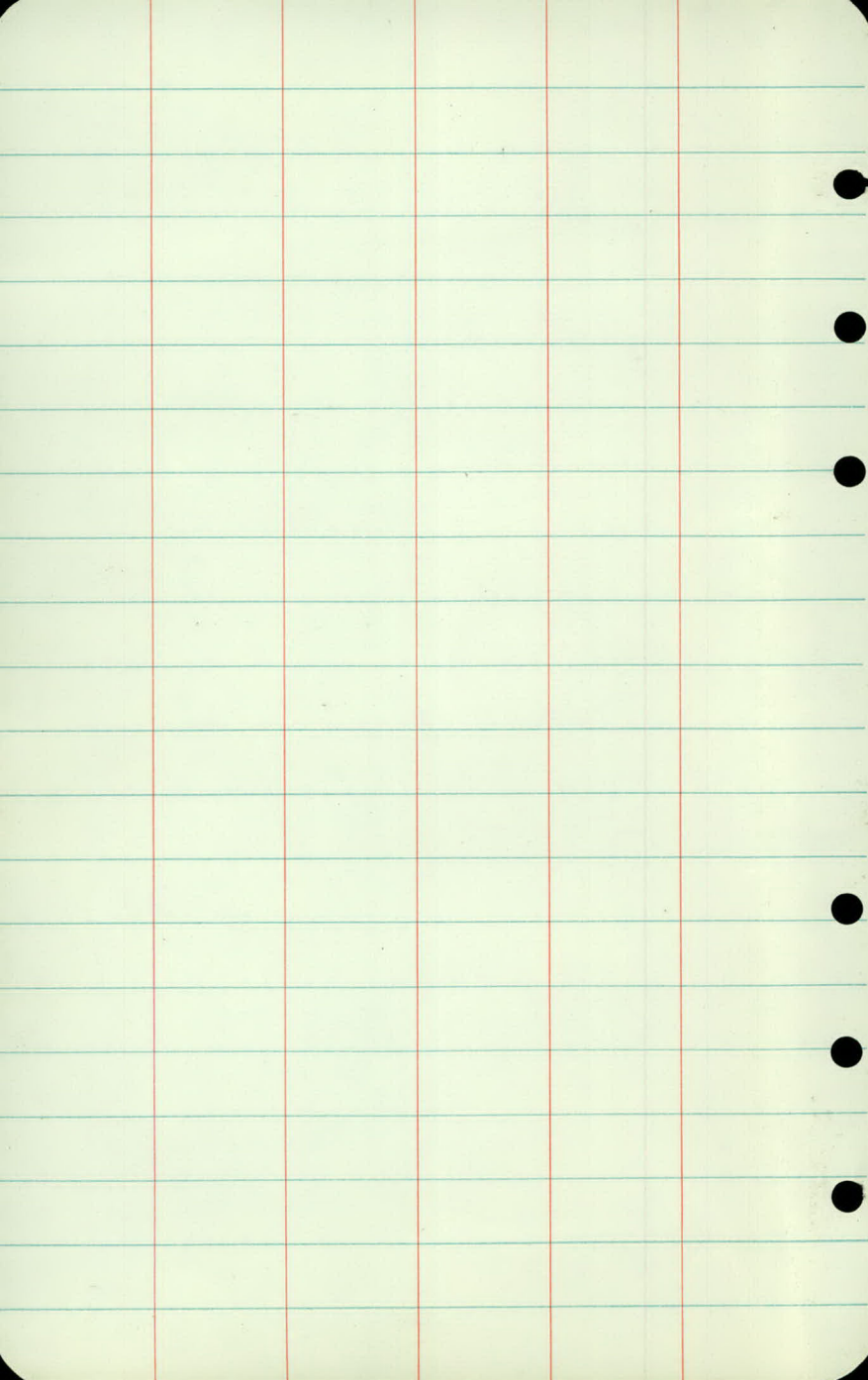
Road Acc't. No. 88 Dr. 9

Date Filed 12-15-66 File Bk. 57

CO. RD. "H"

Long Lake Rd. to T.H. 10

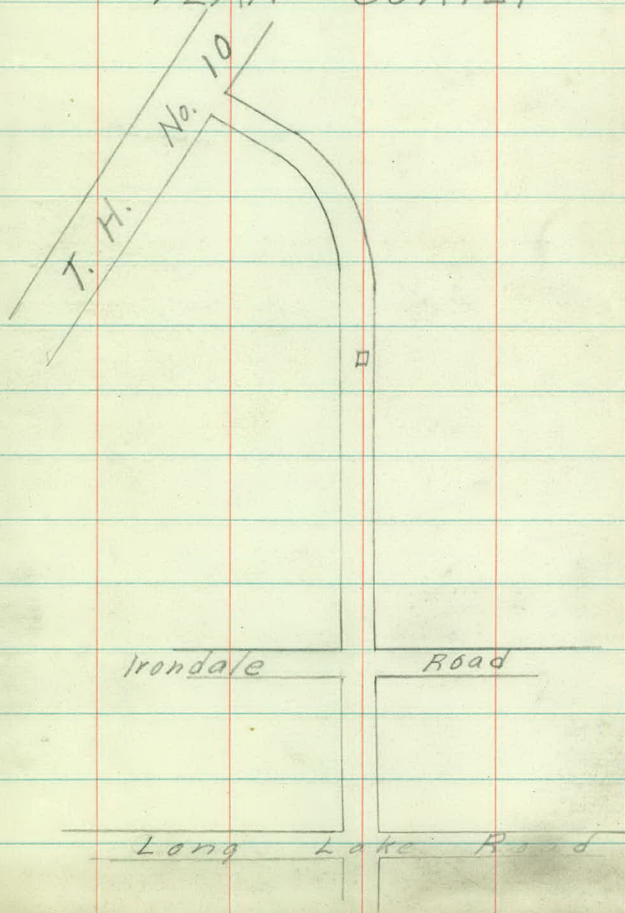
INDEX	PAGE
Alignment	1-9
Topography	10-28
Original X sections	29-80
Misc. Info.	81-86
X sections - New	87-107
Soundings	108-123



CO. RD. "H"

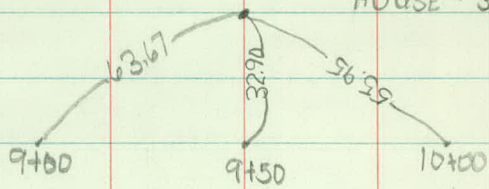
Long Lake Road to T. H. #10

PLAN SURVEY





SOUTHEAST PROPERTY LINE OF
HOUSE # 3409



FK
RG
LD

Jan. 27 1985

2
2

Co. Rd. "H"

Alinement

Sta Point ΔL ΔR

9+86.74

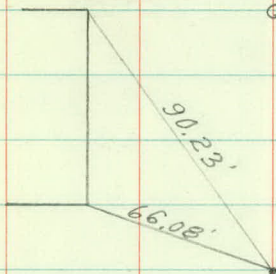
8+25.64 POT

0+00 $\pm$ Long Lake Road

Jan 27, 1965

3

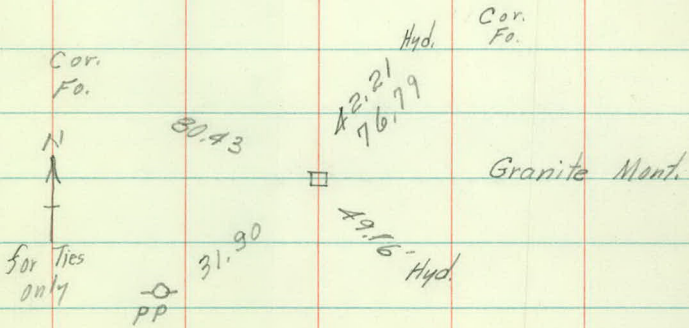
3



21.93 ^{3N}
OPP

Iron

spike



Sta Point ΔL ΔR

38+34.06 P.T.

+25

38

+75

$\Delta = 46^{\circ}16'03''$

+50

D =

37+45.04 P.I.

T = 100.00

+25

L = 189.02

37

R = 234.07

+75

+50

36+45.04 P.C.

Sewer easement Line

31.19 $\frac{26}{26}$
~~26+31.65~~ P.I.

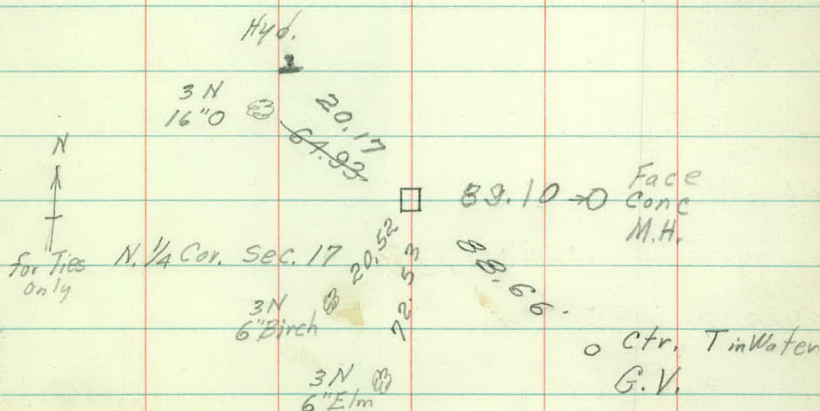
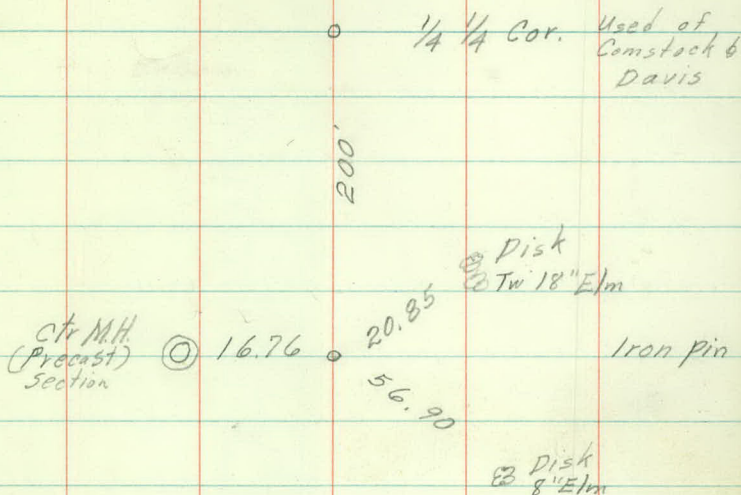
$0^{\circ}17'45''$

5729.48
5729.60
5732.40

FK
WS.
WM
DS
PK
LD

Feb. 5, 1965

4
4



Sta. Point Δ Lt Δ Rt

42+42.44 $\nless$ S.B. Lane T.H. #10

42+30.3 P.O.T P.K. by Edge Conc.

40+98.53 P.T.

+75

+50

40+28.86 P.I.

+25

40

+75

39+58.97 P.C.

Sewer Easement Line

$$\Delta = 11^{\circ} 09' 03''$$

$$D =$$

$$T = 69.89'$$

$$L = 139.56'$$

$$R = 717.08'$$

Feb. 5, 1965

5
5

42+44.44
40 98.53

1 45.91

Spike

Sta Point ΔL

42+26.00 ϕ East of South Bound T.H. #10

¹⁴
42+24 Edge Conc.

+53.73	P.T.	17°23'	
+50		17°11.8'	
38		14°41.8'	$\Delta = 34^\circ 46'$
+50		12°11.8'	$\frac{1}{2}\Delta = 17^\circ 23'$
37		9°41.8'	$D = 10^\circ \text{ Lt.}$
36+85.43	P.I.		$T = 179.37$
+50		7°11.8'	$L = 347.67'$
36		4°41.8'	$R = 572.96'$
+50		2°11.8'	
35+06.06	P.C.	0°00'	

FA
WS
WM

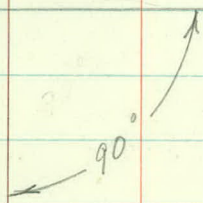
Feb. 10, 1965

6
6

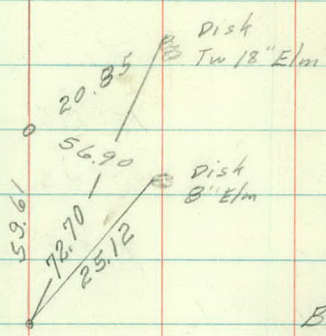
P.K

3745.04
59.61
3685.43

3745.04
3685.43
59.61



sewer line P.I.



Bolt

Sta Point Δ Lt. Δ Rt

40+78.6 $\frac{1}{2}$ R-W
 T.H. # ~~8~~¹⁰ R-W
 T.H. # ~~8~~ R-W

44.58	P.T.	$17^{\circ}35'30''$	
38		$15^{\circ}21'45''$	$\Delta = 35^{\circ}11'$
+50		$12^{\circ}51'45''$	$\frac{1}{2}\Delta = 17^{\circ}35'30''$
37		$10^{\circ}21'45''$	$D = 10^{\circ} Lt.$
36+74.41	P.I.		$T = 181.66$
+50		$7^{\circ}51'45''$	$L = 351.83$
36		$5^{\circ}21'45''$	$R = 572.96$
+50		$2^{\circ}51'45''$	
35		$0^{\circ}21'45''$	
34+92.75	P.C.	$0^{\circ}00'$	

Sept. 3, 1965

7



W. B. L.

0+00

129 60
100 49
35 11

Iron

0

0

Sta. Point ΔL ΔR

40+78.87 R-W Line

+46.66⁵ P.T. $17^{\circ}33\frac{1}{2}'$

38 $15^{\circ}13.5'$

$\Delta = 35^{\circ}07'$

+50 $12^{\circ}43.5'$

$\frac{1}{2}\Delta = 17^{\circ}33'30''$

37 $10^{\circ}13.5'$

$D = 10^{\circ}L$

36+76.77 P.I.

$T = 181.28^{\circ.295}$

+50 $7^{\circ}43.5'$

$L = 351.17^{\circ}$

36 $5^{\circ}13.5'$

$R = 572.96'$

+50 $2^{\circ}43.5'$

35 $0^{\circ}13.5'$

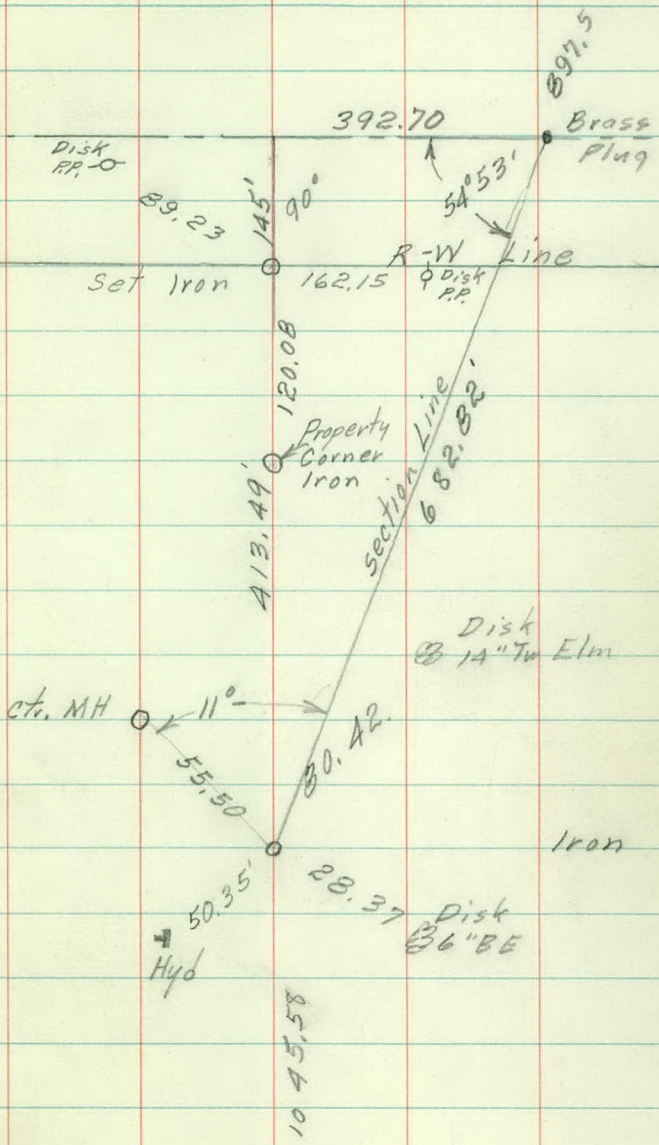
34+95.49⁸ P.C. $0^{\circ}00'$

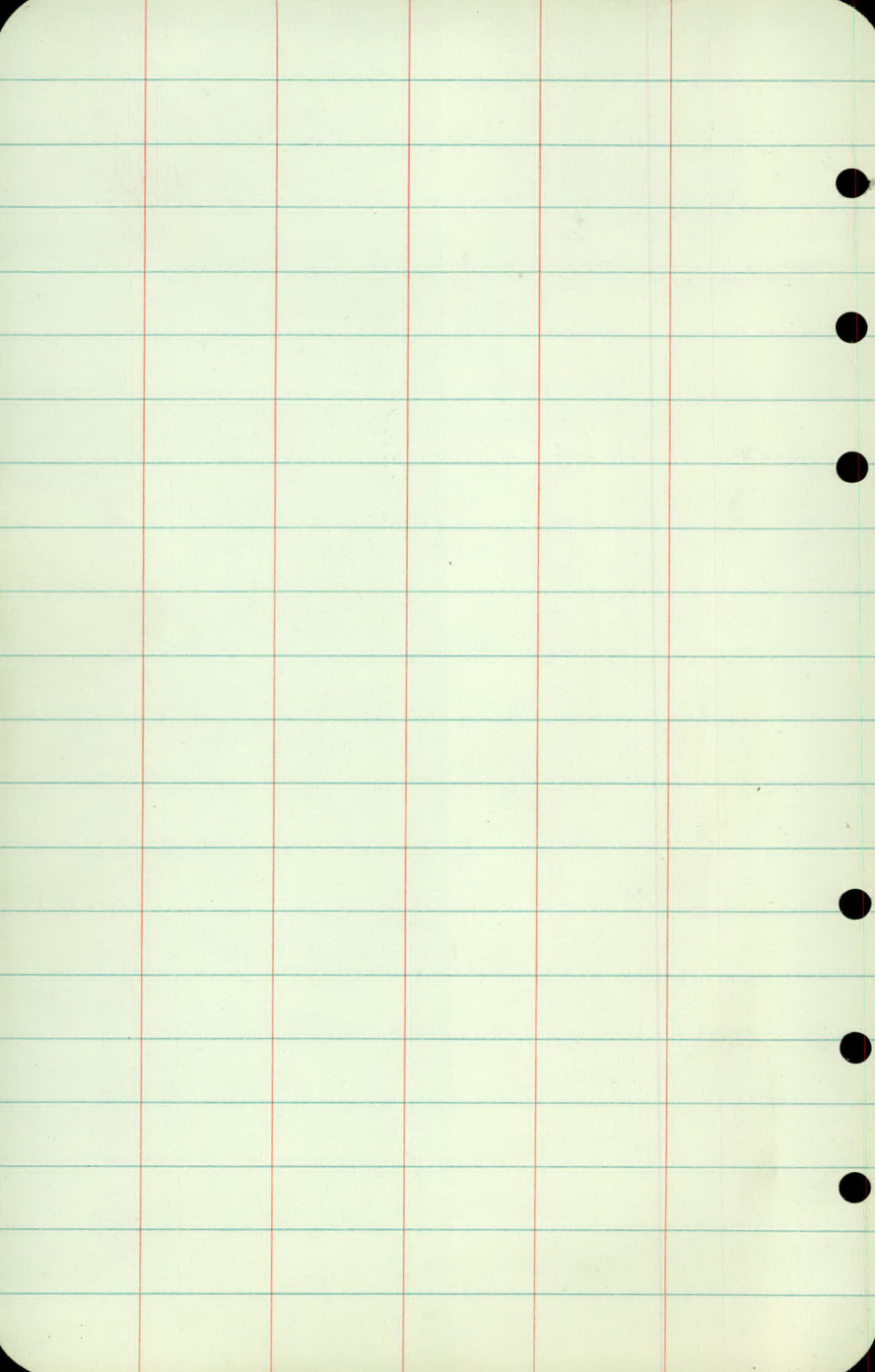
2631.19^{19.2} P.I.

$0^{\circ}17'45''$

Sept. 23, 1965

8

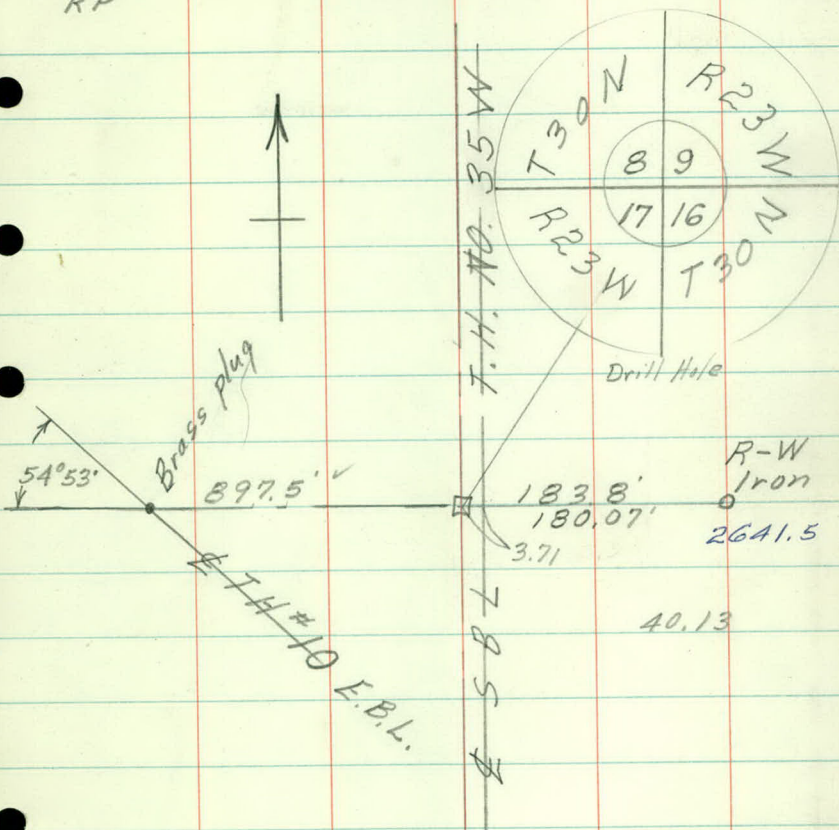




FX
LPD
RW
RP

Sept. 22, 1965

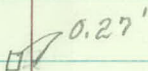
9



Co Rd H²



Co Rd H



Go Rd GP



Co. Rd. "H"

Topography

~~Irondale Rd~~ to T. H. # 10

Long Lake Rd

Lt

+50

+51 ~~En~~ (8')

Conc
20x21
23

C

+50 Hedge Rt
32

+36 94
SW Corner

Bay Hedge (lilacs)

+33 27-64

7" Elm

+12 34

+24 5" Elm
25

+31 8" Elm
31

1+00

+95 6" APPLE J

+82 7" ELMI

24

+62 S.W. COR. HO. ✓
44

+62 14" ELMI ✓
24

✓
BT
15

✓
BT
15

+18 PP
28

+70 M.W. COR. HO. ✓
83

+63 4" PINE
106

+63 18" OAK J
30

+61 10" PINE ✓
88

36" OAK ✓

✓
BT
15

✓
BT
15

+28 24" OAK ✓
86

+28 12" OAK ✓
56

+26 6" VALVE ✓
28

+24 36" ERV ✓
41

+17 1" M.H. ✓
17

-1 1" M.H.
17

400 Hedge ✓
34

+72 15" OAK ✓
38

+80 12" POP ✓
69

+94 BUSH ✓
57

+50

+28 36" (4 PL) ✓
35

+28 6" TW. APPLE ✓
86

+24 HYD ✓
35

+24 36" ERV ✓
26

+17 36" ERV ✓
41

0+00

+43 4" POP ✓
85

+46 12" OAK ✓
35

+41 12" OAK ✓
105

+38 10" POP ✓
85

+38 6" OAK ✓
15

+39 36" ERV ✓
15

+48 BUSH ✓
34

-31 12" ELMI ✓
66

-38 36" ERV ✓
15

-43 18" ELMI ✓
33

-47 3" APPLE ✓
64

-13 36" ERV ✓
41

-25 36" ERV ✓
20

-33 4" PINE ✓
23

-55 4" PINE ✓
33

-28 36" ERV ✓
20

-25 36" ERV ✓
20

-38 36" ERV ✓
15

-+50

-68 TW. COR. HO. ✓
34

-80 12" CHAIN ELMI ✓
34

-88 S.W. COR. HO. ✓
47

-1+00

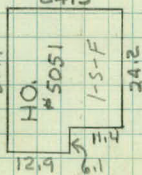
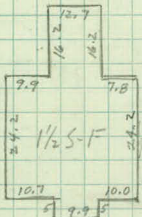
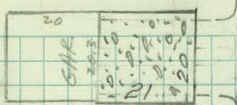
✓
BT
15

✓
BT
15

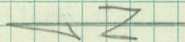
RS
DS
WS
LPD

Feb 26, 1965
cloudy 80

11



M. H.
9' cash.
4 Adj. rings
7.8 to 100.



4100

Lt

BT

Rt

+96 Trl 2" Birch
31

19 11

+76 Ent (16')

+85.5 3' Walk
31

+63 B20
Ent

+64 SW Cor Ho
83

+54 Fe Cor
30-100+

+48 Ent (16')

+38 NW Cor Ho
72
51

+27 MH
14

2 Board
Wood Fe

+15 30

+12 Ent (16')

3+00 +02 SW Cor Ho
80

BT
18 12

+94 B Fe
30

+81 Ent 16'

+71 E. Fe
30

+61 Wood Fe
30-40

~~+60 SW~~ +56 NW Cor Ho
68

62 PP
28

+54 3' Walk CE
35

+46 Mugho Pine
63

+49 PP +48 3' Walk CE
26 38

SW Cor Ho

+11 80
Mugho Pine

BT

2+00 +06 65

16 14

+91 Ent 16' CE
16

+70 30

CE
12

+78 NW Cor Gar
73

+72 Tell Sign
22

+68 Fence +69
36-73 27

+64 11/16 +61 11/16
34 63

+57 Hedge Cor +67 End Hedge
31 72

+52 Tw 8" Elm +54 14" Catt
31 32

March 5, 1965
30° Windy

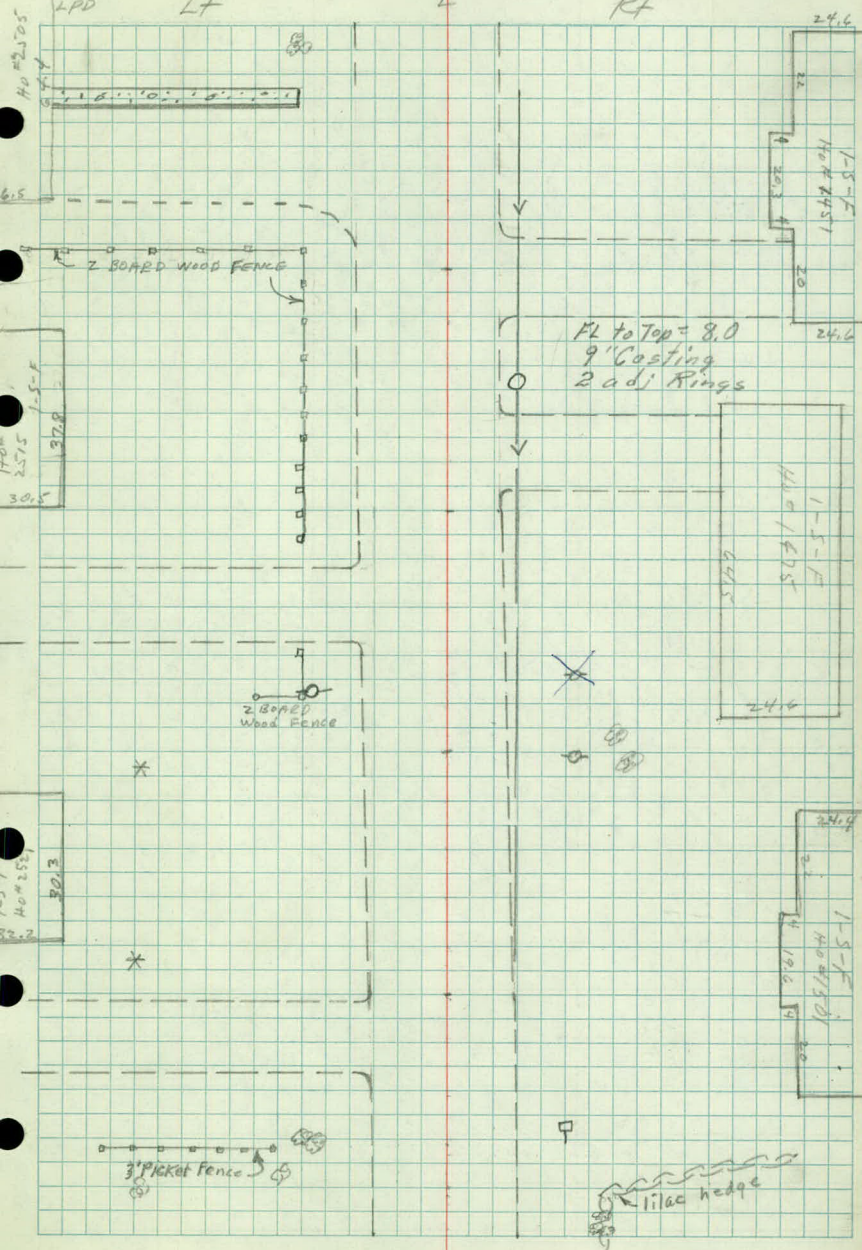
12

RG
DS
RB
PK
LPD

Lf

±

Rt



Lt

E

RT

$$+98 \frac{ER}{57}$$

$$+47 \frac{ER}{30}$$

$$+32 \frac{G.V.}{2}$$

$$+29 \frac{Hyd}{35}$$

$$+36 \frac{POR}{28}$$

$$+34 \frac{POR}{12} +33 \frac{12" Pine}{69}$$

$$+33 \frac{5" Pine}{27} +33 \frac{10" Pine}{40} +33 \frac{10" Pine}{53}$$

$$+04 \frac{6" Pine}{81}$$

$$+18 \frac{BR}{22}$$

$$+19 \frac{Hyd}{12} +19 \frac{BR}{7} +22 \frac{6" Pine}{27}$$

$$6+00 +04 \frac{2" Ash}{46} +04 \frac{1" Ash}{63} BT 23 2$$

$$+09 \frac{3" Pine}{38} +20 \frac{3" Pine}{28}$$

$$+92 \frac{10" Pine}{25}$$

$$+85 \frac{N.W. cor Ho}{66}$$

$$+79 \frac{10" Pine}{29}$$

$$+55 \frac{8" Pine}{65}$$

$$+58 Ent 10'$$

$$+41 \frac{6" Pine}{50}$$

$$+41 \frac{SW cor Ho}{82}$$

$$+45 \frac{12" Pine}{29}$$

$$+10 \frac{12" Dirt Ent}{23}$$

$$+39 \frac{PP}{23}$$

Elm

J.P.

$$+09 \frac{5" Pine}{34}$$

$$+10 \frac{Two App}{41}$$

$$+25 \frac{6" Maple}{35}$$

$$+09 \frac{5" Pine}{46}$$

$$5+00 +00 \frac{1" Pine}{64}$$

$$BT 21 9 +00 \frac{4" Pine}{36}$$

$$+83 Ent 10'$$

$$+69 \frac{SE cor Ho}{67}$$

$$+71 \frac{2" Juniper}{66}$$

$$+59 \frac{SW cor Ho}{81}$$

$$+64 \frac{1" Pine}{64}$$

$$+65 \frac{3" Maple}{35}$$

$$+51 \frac{black hedge}{36-84}$$

$$+51 \frac{4" Maple}{47}$$

$$+50 \frac{2" Pine}{33}$$

$$+51 \frac{PP}{27}$$

$$+41 \frac{Tri 3" Birch}{36}$$

$$+28 \frac{10" Elm}{33}$$

$$+34 \frac{1" Pine}{56}$$

$$+09 \frac{3" Tw. Apple}{45}$$

$$+18 \frac{4" Spruce}{59}$$

$$+10 \frac{PP}{24}$$

$$4+00$$

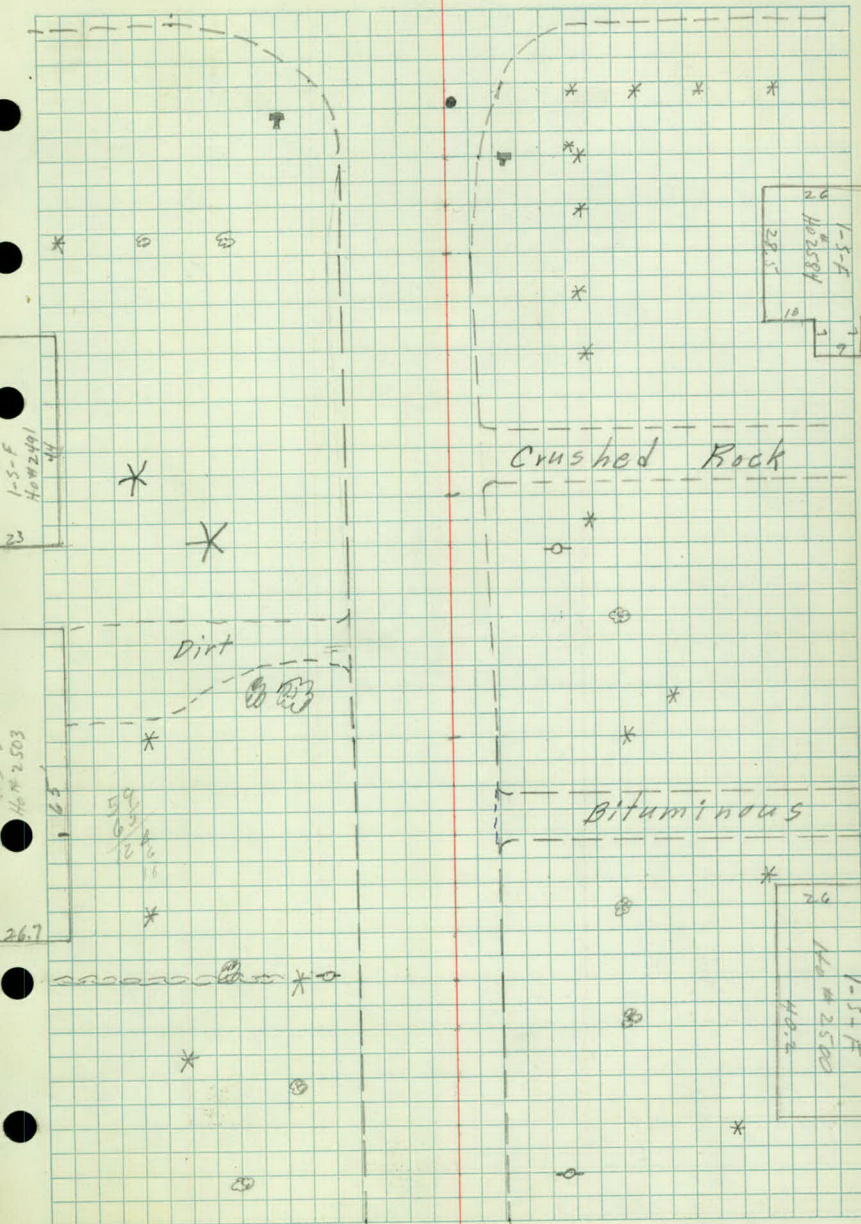
$$BT 19 11$$

March 5, 1965
35° Clear
Rt.

13

Lt.

£



9+00

Lt.

 $\frac{1.4}{Rd.}$
 10-25

Rt.

+86

 $\frac{8ush}{36}$
 $+49 \frac{E. Wolf 3'}{33}$

+38

 $\frac{SW Cor Ho.}{65}$

8+00

 $+99 \frac{12' App}{39}$

+79

 $\frac{4' App.}{39}$
 $+17 \frac{SW Cor House}{63}$

7+00

 $\frac{100}{Rd. 9-25}$

+94

 $\frac{ER}{27}$

+81

 $\frac{ER}{9}$

+77

 $\frac{POR}{3}$

+78

 $\frac{POR}{35}$

+63

 $\frac{ERA}{45}$

+72

 $\frac{BR}{45}$

+50

+52

 $\frac{4' Elm}{34}$

+36

 $\frac{NW Cor 100' Fence}{29}$

+33

 $\frac{Guide Wire}{23}$

+22

 $\frac{P.P.}{23}$
 $+19 \frac{NW Cor Ho.}{50'}$

+81

 $\frac{10' ENH. Cov Conc Ent}{56}$

+77

 $\frac{PP (Arc. Lt.)}{20}$

+73

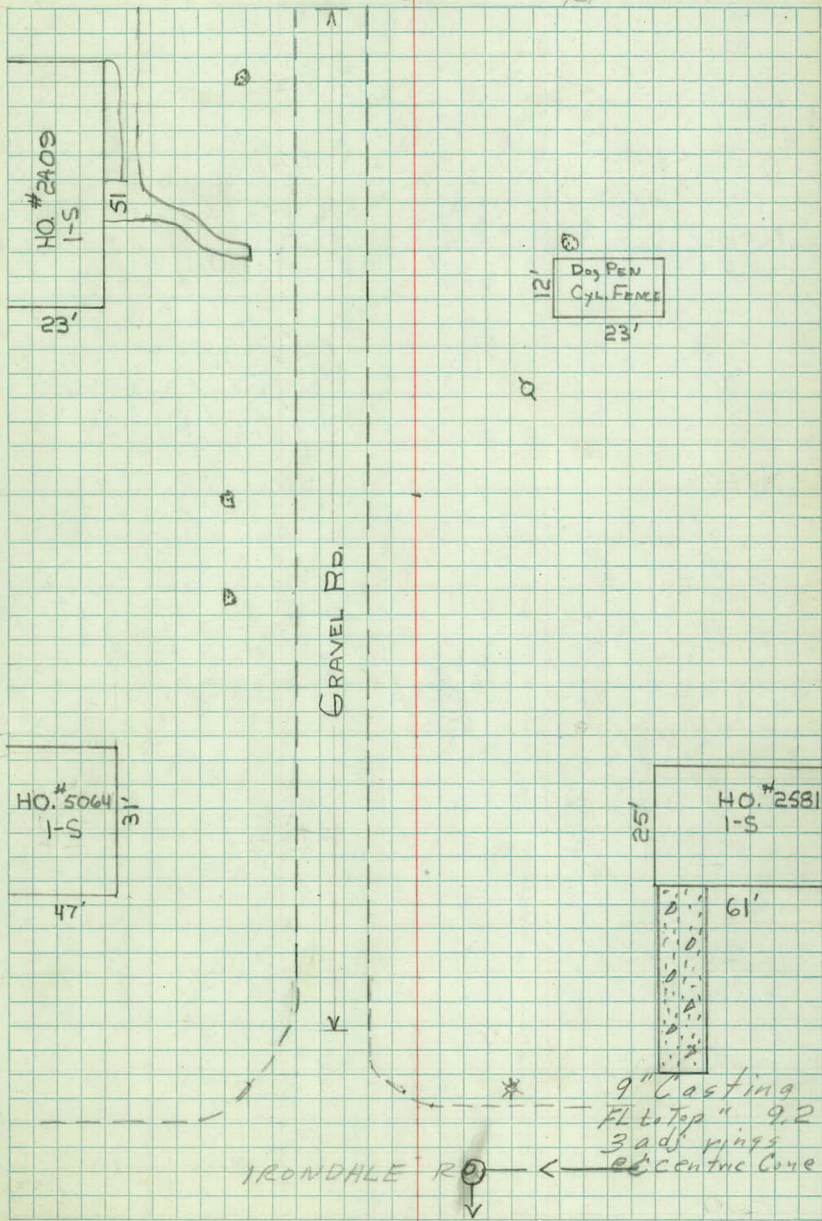
 $\frac{BR}{3}$
 $+60 \frac{MH}{11}$

March 5, 1965
11, 1965 14

Lt

£

Rt



N

1

+50

LT

✗ +50 $\frac{\text{BRUSH}}{20}$ RT ✓

+27 $\frac{\text{BRUSH}}{32}$ ✓

+07 $\frac{\text{Bag. of BRUSH \& TAXES}}{19}$

11+00

+56 $\frac{14" \text{ OAK}}{79}$ ✓

+50

~~+27 $\frac{20" \text{ W. OAK}}{6}$~~

10+00

+07 $\frac{\text{MH}}{226}$

+85 $\frac{\text{MH}}{10}$

+67 $\frac{\text{Hyd}}{27}$

+54 $\frac{\text{COR. LOT IRON}}{33}$ ✓

~~+68 $\frac{36" \text{ TOP OAK}}{8}$~~

+50

+24 $\frac{\text{END RD}}{10-25}$ ✓

~~+22 $\frac{12" \text{ OAK}}{8}$~~

9+00

+00

✓ SW COR. 6" D. ENGL 10-25

+00 Ret. W. H. 1 1/2' WIDE
35'-67 4 High

R.B.
W.S.
F.S.
R.D.

MARCH 11, 1965
CLOUDY 20° 15

LT.

E

RT.

BRUSH & WOODED
AREA
SMALL TREES

N

T

24'

6A.

22'

ENT

GRAVEL
RD



14+00

L.T.

 $\frac{1}{2} + 00$ ✓
 $\frac{\text{WOODS}}{63}$

R.T.

+50

+50

✓
 $\frac{\text{WOODS}}{40}$ ✓
+15 $\frac{\text{M.H.}}{9}$

13+00

+00 $\frac{\text{Basin WOODED AREA}}{27}$

+00

✓
 $\frac{4' \text{ DITCH}}{100}$ +96 $\frac{\text{Hyd}}{31}$

+75

✓
 $\frac{4' \text{ DITCH}}{81}$

+50

+50

✓
 $\frac{4' \text{ DITCH}}{50}$ +50 $\frac{\text{WOODS}}{30}$

+44

✓
 $\frac{4' \text{ DITCH}}{28}$

+37

✓
 $\frac{\text{Ditch R.T.}}{28}$ 28" CONCRETE PIPE
4" OPEN

+18

✓
 $\frac{\text{Brush Woods}}{42}$

12+00

✓
+00 $\frac{\text{B.E.W.}}{70}$

+89

✓
 $\frac{\text{Brush & Woods}}{70}$

+72

✓
 $\frac{\text{B.E. Woods}}{24-50}$

+58

✓
 $\frac{\text{Brush & Woods}}{18}$

+50

+50

✓
 $\frac{\text{B.E. Woods}}{20}$

+50

2

16+00

Trail
30

+50

+50 $\frac{\text{woods} \checkmark}{95}$
+50 $\frac{6' \text{ elm.}}{48}$
+44 $\frac{\text{woods}}{84}$

15+00

+100 Trail
97

+00 $\frac{\text{woods} \checkmark}{63}$
+93 $\frac{8' \text{ window} \checkmark}{42}$

+92 R Tie E
120-132

+50

+50 $\frac{\text{woods} \checkmark}{25}$
+39 $\frac{8' \text{ white}}{36} \checkmark$
+32 $\frac{12' \text{ white}}{30}$

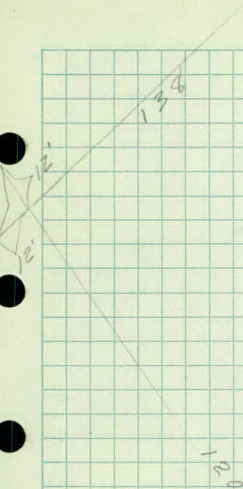
14+00

+00 $\frac{\text{woods} \checkmark}{63}$

MARCH 11, 1965
CLOUDY 20°

17

E



N

WOODED

19+00

£ +00 Woods
45

+90 Woods
60

+50

End
Trail

+55 Woods
64

18+00

Trail
98

+00 Woods
58

+70 Woods
42

+50

+44 Woods
22

17+00

Trail
93

+00 Woods
30

+91 Woods
29

+85 M.H

+71 R Tie Rink 9
138 150

+80 Beg. Woods
51

+50

R.G
R.B
D.S
A.S
P.D
P.K

MARCH 15, 1965
FAIR 20° 18
L. Snow

N

15' RCP
15' RCP

WOODED AREA

+50

$$\begin{array}{r} \checkmark \\ +50 \text{ Woods} \\ \hline 30 \end{array}$$

$$\begin{array}{r} \checkmark \\ +47 \text{ Woods} \\ \hline 31 \end{array}$$

$$\begin{array}{r} \checkmark \\ +17 \text{ Woods} \\ \hline 21 \end{array}$$

21+00

$$\begin{array}{r} \checkmark \\ +00 \text{ Woods} \\ \hline 20 \end{array}$$

$$\begin{array}{r} \checkmark \\ +85 \text{ M.H.} \\ \hline 10 \end{array}$$

$$\begin{array}{r} \checkmark \\ +74 \text{ Woods} \\ \hline 21 \end{array}$$

+50

$$\begin{array}{r} \checkmark \\ +44 \text{ Woods} \\ \hline 25 \end{array}$$

20+00

$$\begin{array}{r} \checkmark \\ +00 \text{ Woods} \\ \hline 26 \end{array}$$

$$\begin{array}{r} +80 \text{ cesspool} \\ \hline 106 \end{array}$$

$$\begin{array}{r} \checkmark \\ +65 \text{ Woods} \\ \hline 28 \end{array}$$

+50

19+00

$$\begin{array}{r} \checkmark \\ +05 \text{ Woods} \\ \hline 32 \end{array}$$
$$\begin{array}{r} \checkmark \\ +00 \text{ Woods} \\ \hline 45 \end{array}$$

MARCH 15, 1965
L. SNOW 20° 19

E

N

0

15" RCP →
→ 15" RCP
3 1/2

WOODED AREA
SMALL TREES

24+00

✓
+00 $\frac{\text{woods}}{13}$

✓
+72 m.H.
10

✓
+66 $\frac{\text{woods}}{14}$

+50

✓
+34 $\frac{\text{woods}}{15}$

23+00

✓
+00 $\frac{\text{woods}}{13}$

✓
+80 $\frac{\text{Ditch 2'}}{77}$

+50

✓
+50 $\frac{\text{woods}}{14}$

✓
+34 $\frac{\text{Ditch 2'}}{43}$

22+00

+00 $\frac{\text{woods}}{17}$

+96 $\frac{\text{SE Cor Lift Sta}}{90}$

✓
+80 $\frac{\text{Ditch 2'}}{15}$

+50

✓
+56 $\frac{\text{Ditch 2'}}{75}$
✓
+50 $\frac{\text{woods}}{30}$

+50

£ +50 $\frac{\text{END WOODS}}{27}$

26+00

+95 $\frac{18'' \text{ OAK}}{52}$

+00 $\frac{\text{(BURN) WOODS}}{21}$

+50

+50 $\frac{\text{WOODS}}{17}$

+17 $\frac{10'' \text{ OAK}}{56}$

25+00

+00 $\frac{\text{WOODS}}{23}$

+50

+50 $\frac{\text{WOODS}}{22}$

24+00

+00 $\frac{\text{WOODS}}{13}$

MARCH 15, 1965
20° 21

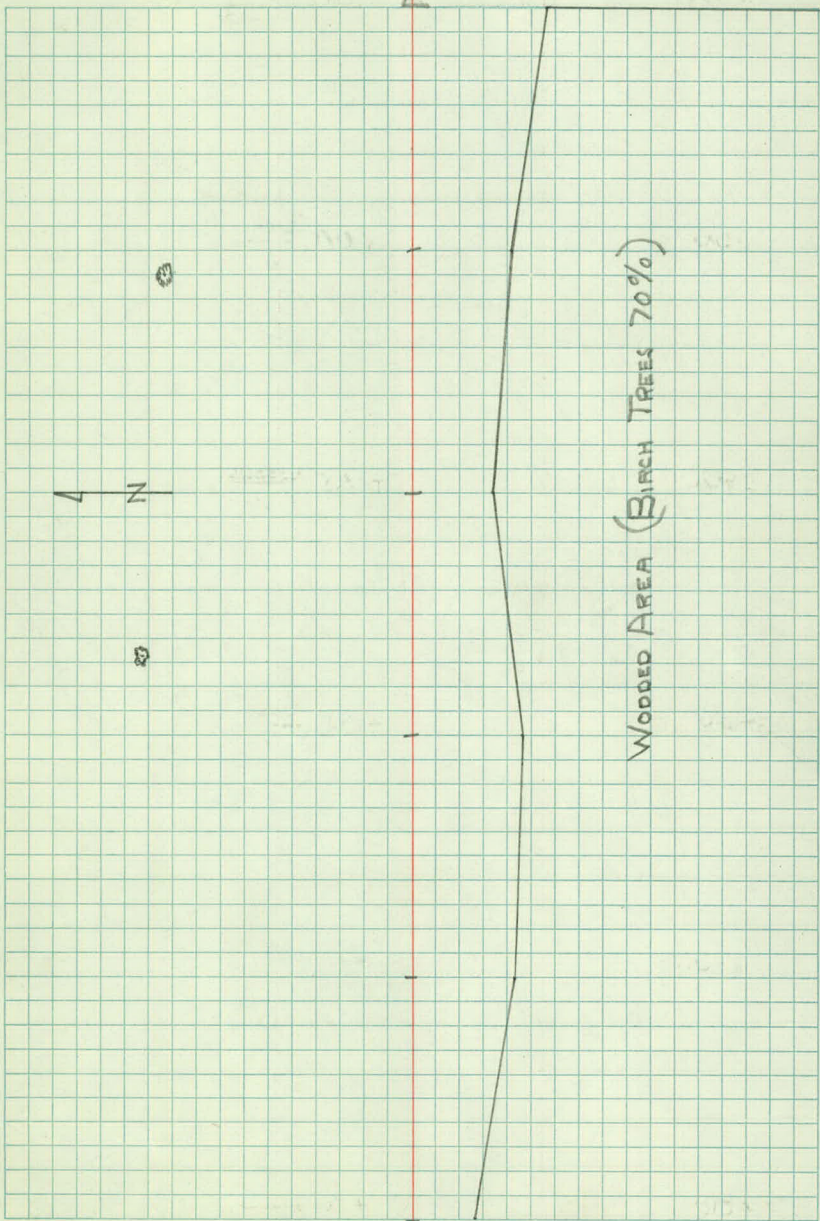
2

7 N

23

20

WOODED AREA (BIRCH TREES 70%)



29+00

+00

+00

2 CREEK
80
FENCE
3

+50

3-STRAND ✓
+15 Beg FENCE
1

28+00

+00 End Sup. ✓

+50

+30 ELM ✓
85

+21 m.H ✓
10

6" ELM ✓ +38 4" ELM ✓
52 63
+28 5" ELM ✓ +35 6" ELM ✓
76 24
+24 4" ELM ✓
48

27+00

+59 STAMP ✓
55

+50

+50 End Wood i Beg. Sup. ✓
27

3/15/65

22



3-S.B.W.
(Poor Cond.)

SWAMP

5" H.C.P.

24 R.C.P.

15" RCP

10 RVC P

9

+50

£

+42 $\frac{\text{£ CREEK } 10'}{30}$ ✓

+13 $\frac{8" \text{ ELM}}{44}$ ✓

31+00

+00 $\frac{27" \text{ OAK}}{27}$ ✓ +00 R. TIE CR

+00 $\frac{\text{CREEK}}{71}$ ✓

+85 $\frac{16" \text{ OAK}}{26}$ ✓ +85 $\frac{\text{ELM}}{23}$ ✓

+62 $\frac{\text{£ CREEK COR. } 10'}{29-75}$ ✓

+50

+51 $\frac{\text{CREEK } 10'}{27}$ ✓

30+00

+00 $\frac{\text{£ CREEK } 10'}{25}$ ✓ +75 $\frac{\text{STUMP}}{32}$ ✓

+72 $\frac{12" \text{ ELM}}{34}$ ✓ +73 $\frac{12" \text{ ELM}}{37}$ ✓

+70 $\frac{10" \text{ ELM}}{38}$ ✓

+50

+33 $\frac{\text{M.H.}}{10}$ ✓

+39 $\frac{\text{£ CREEK } 10'}{27}$ ✓

+10 $\frac{\text{FENCE}}{3}$ ✓

29+00

+00 $\frac{\text{FENCE}}{3}$ ✓

+00 $\frac{\text{£ CREEK } 10'}{80}$ ✓

2

1 2

15
← 2 →

12

Rice Creek

Rice Creek

50 scattered small trees

34+00

$$+00 \frac{\text{CREEK } 9'}{25}$$

$$+63 \frac{\text{CREEK } 9'}{29}$$

+50

$$+40 \frac{\text{CREEK } 10'}{95}$$

$$+50 \frac{\text{CREEK } 10'}{80}$$

$$+23 \frac{10' \text{ ELM}}{25}$$

$$+36 \frac{\text{STUMP}}{17}$$

$$+32 \frac{\text{MH}}{10}$$

$$+20 \frac{12' \text{ ELM}}{6}$$

$$+31 \frac{8' \text{ ELM}}{19}$$

$$+25 \frac{10' \text{ ELM}}{19}$$

$$+02 \frac{8' \text{ ELM}}{31}$$

33+00

$$+90 \frac{10' \text{ ELM}}{36}$$

$$+95 \frac{8' \text{ ELM}}{16}$$

$$+78 \frac{14' \text{ ELM}}{32}$$

$$(\text{STRAND})$$

$$+52 \frac{\text{FENCE}}{36-100}$$

+50

$$+35 \frac{\text{CREEK } 10'}{72}$$

$$+32 \frac{9' \text{ ELM}}{17}$$

32+00

$$+00 \frac{\text{CREEK (R.TIE 31+82)}}{22}$$

$$+88 \frac{\text{CREEK } 10'}{17}$$

$$+75 \frac{\text{CREEK } 9'}{17}$$

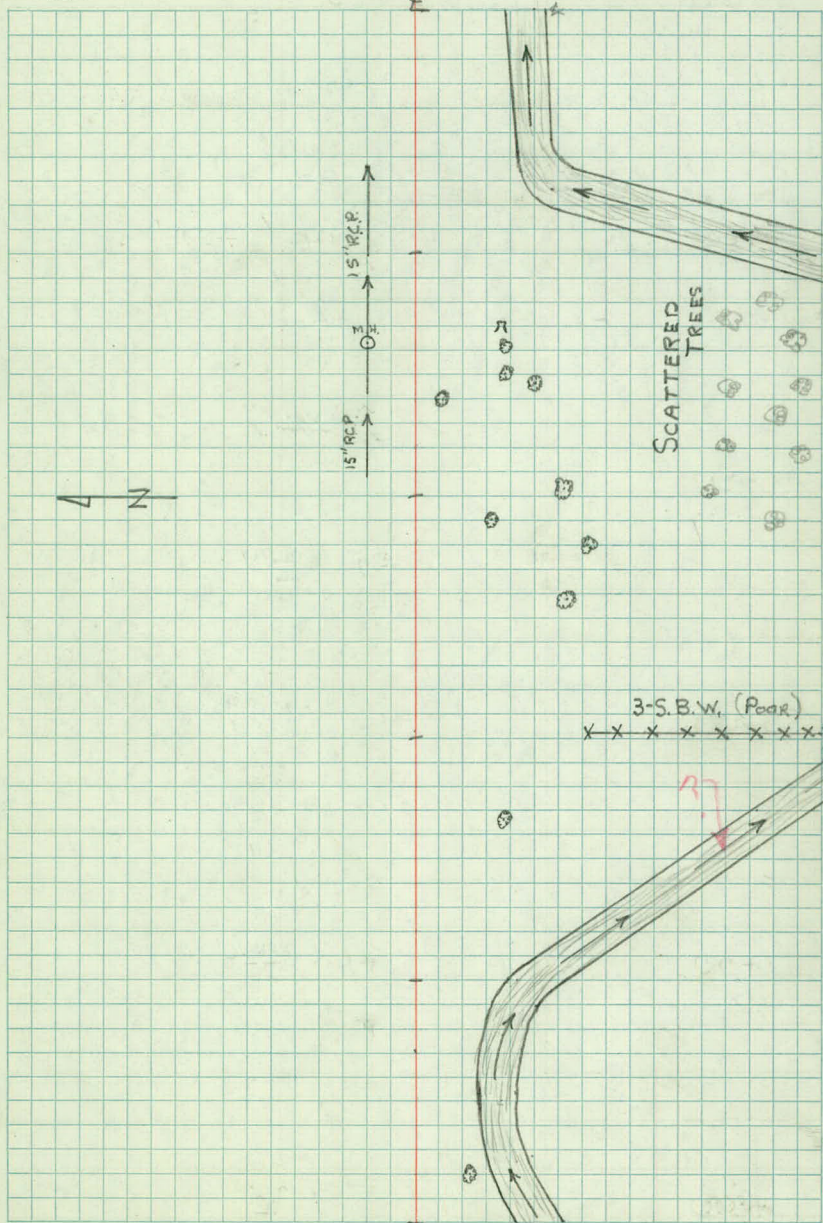
+50

$$+60 \frac{18' \text{ ELM}}{12}$$

$$+60 \frac{\text{CREEK } 10'}{22}$$

R.G.
R.B.
D.S.
F.S.

MARCH, 16, 1965
CLEAR 21° 24



$$+50 \quad +50 \frac{\pounds \text{ DITCH } 10'}{46} \pounds \quad +50 \frac{\text{BRUSH} \checkmark}{50}$$

$$36+00 \quad +00 \frac{\pounds \text{ DITCH } 10' \checkmark}{19} \quad +00 \frac{\pounds \text{ CREEK } 10' \checkmark}{98} \\ +75 \frac{\pounds \text{ DITCH } 15' \checkmark}{4} \quad +75 \frac{\pounds \text{ CREEK } 10' \checkmark}{41} \quad +90 \frac{\text{Bog. BRUSH} \checkmark}{38}$$

$$+50 \quad +54 \frac{\text{DITCH } \pounds 15' \checkmark}{2}$$

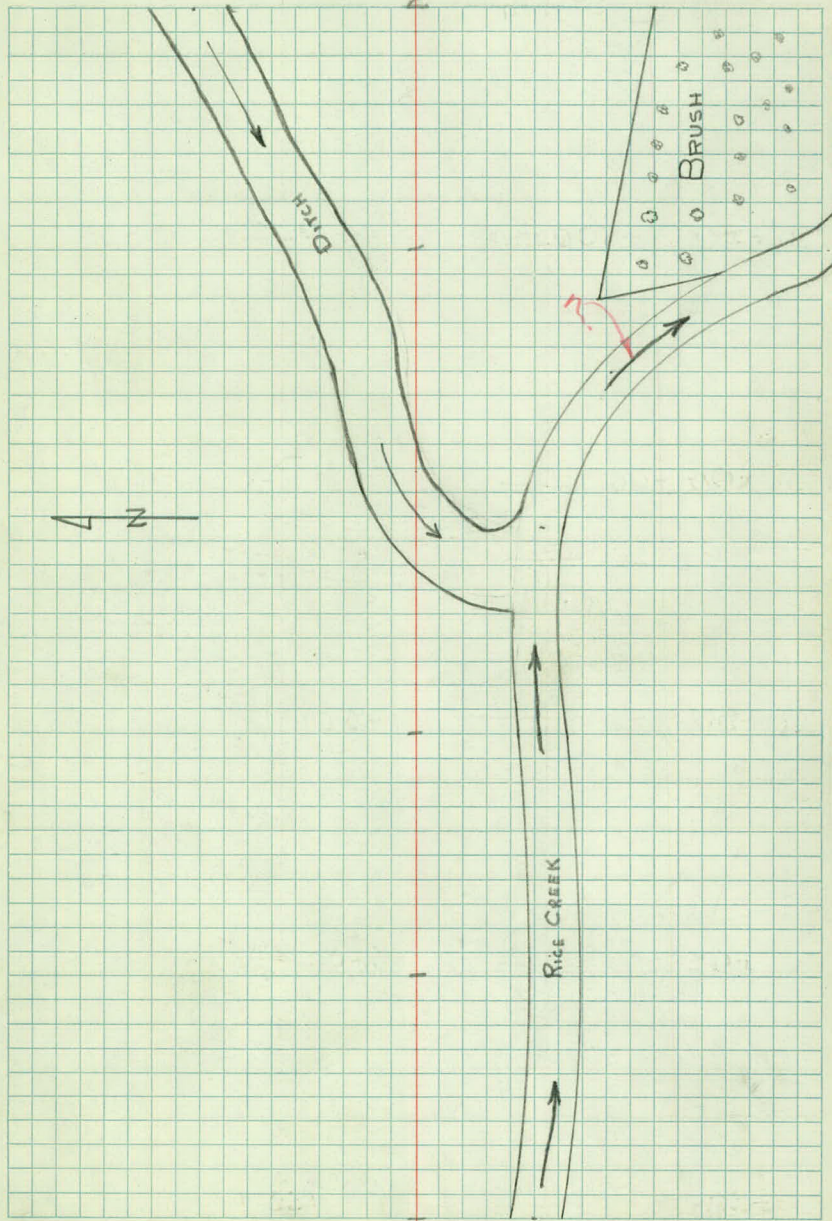
$$+43 \frac{\pounds \text{ CREEK } 10' \checkmark}{26}$$

$$35+00 \quad +00 \frac{\pounds 10' \text{ CREEK} \checkmark}{26}$$

$$+50 \quad +50 \frac{\pounds \text{ CREEK } 10' \checkmark}{28}$$

$$34+00 \quad +00 \frac{\pounds \text{ CREEK} \checkmark}{25}$$

MARCH 16, 1965
21° 25



$$39+00 \quad +00 \quad \begin{array}{r} \checkmark \\ \text{S. Edge Pond} \\ 21 \end{array} \quad \&$$

$$+75 \quad \begin{array}{r} \checkmark \\ \text{8" Cotton} \\ 40 \end{array}$$

$$+50 \quad +50 \quad \begin{array}{r} \checkmark \\ \text{S. Edge Pond} \\ 12 \end{array} \quad +50 \quad \begin{array}{r} \checkmark \\ \text{FENCE} \\ 107 \end{array}$$

$$38+00 \quad +00 \quad \begin{array}{r} \checkmark \\ \text{S. Edge Pond} \\ 9 \end{array} \quad +83 \quad \begin{array}{r} \checkmark \\ \& \text{ DITCH} \\ \& \end{array} \quad +00 \quad \begin{array}{r} \checkmark \\ \text{FENCE} \\ 78 \end{array}$$

$$+68 \quad \begin{array}{r} \checkmark \\ \text{S. Edge Pond} \\ 15 \end{array} \quad +73 \quad \begin{array}{r} \checkmark \\ \& \text{ DITCH} \\ \& \end{array}$$

$$+64 \quad \begin{array}{r} \checkmark \\ \text{S. Edge Pond} \\ 26 \end{array} \quad +63 \quad \begin{array}{r} \checkmark \\ \text{Edge Ditch} \\ \& \end{array}$$

$$+56 \quad \begin{array}{r} \checkmark \\ \text{S. Edge Pond} \\ 35 \end{array} \quad +70 \quad \begin{array}{r} \checkmark \\ \text{Beg. Fence 14-S-Good} \\ 78 \end{array}$$

$$+50 \quad +50 \quad \begin{array}{r} \checkmark \\ \text{S. Edge Pond} \\ 40 \end{array} \quad +50 \quad \begin{array}{r} \checkmark \\ \& \text{ DITCH} \\ 51 \end{array}$$

$$+38 \quad \begin{array}{r} \checkmark \\ 30' \text{ Tec. Willow} \\ 72 \end{array} \quad +40 \quad \begin{array}{r} \checkmark \\ \& \text{ DITCH} \\ 100 \end{array}$$

$$+23 \quad \begin{array}{r} \checkmark \\ \text{M.H.} \\ 34 \end{array} \quad \text{see Alignment}$$

$$+10 \quad \begin{array}{r} \checkmark \\ \text{End BRUSH} \\ 55 \end{array}$$

$$37+00 \quad +00 \quad \begin{array}{r} \checkmark \\ \text{N. Edge Pond} \\ 100 \end{array} \quad +00 \quad \begin{array}{r} \checkmark \\ \text{S. Edge Pond} \\ 52 \end{array}$$

$$+75 \quad \begin{array}{r} \checkmark \\ \text{Beg. Ditch} \\ 60 \end{array} \quad +75 \quad \begin{array}{r} \checkmark \\ \text{BRUSH} \\ 41 \end{array}$$

$$+50 \quad +50 \quad \begin{array}{r} \checkmark \\ \& \text{ DITCH} \\ 46 \end{array} \quad +50 \quad \begin{array}{r} \checkmark \\ \text{BRUSH} \\ 50 \end{array}$$

Myrtle to Ditch

Alinemen^t, H2
at Old B

+50

$$\begin{array}{r}
 +44 \text{ Edge G.R.} \checkmark \\
 \underline{16} \\
 +34 \text{ G.R.} \checkmark \\
 \underline{9}
 \end{array}$$

£

$$\begin{array}{r}
 +32 \text{ B.Top} \checkmark \\
 \underline{2} \\
 +20 \text{ Edge B.T.} \checkmark \\
 \underline{20} \\
 +11 \text{ Edge B.T.} \checkmark \\
 \underline{91} \\
 +05 \text{ E.B. Top} \checkmark \\
 \underline{59} \\
 +00 \text{ G.R.} \checkmark \\
 \underline{60}
 \end{array}$$

41+00

$$\begin{array}{r}
 +95 \text{ M.H.} \checkmark \\
 \underline{26}
 \end{array}$$

$$\begin{array}{r}
 +91 \text{ M.H.} \\
 \underline{19}
 \end{array}$$

+50

$$\begin{array}{r}
 +52 \text{ 1st 3' Elm} \checkmark \\
 \underline{35} \\
 +49 \text{ 2' Elm} \checkmark \\
 \underline{34} \\
 +45 \text{ 3rd Elm} \checkmark \\
 \underline{37}
 \end{array}$$

40+00

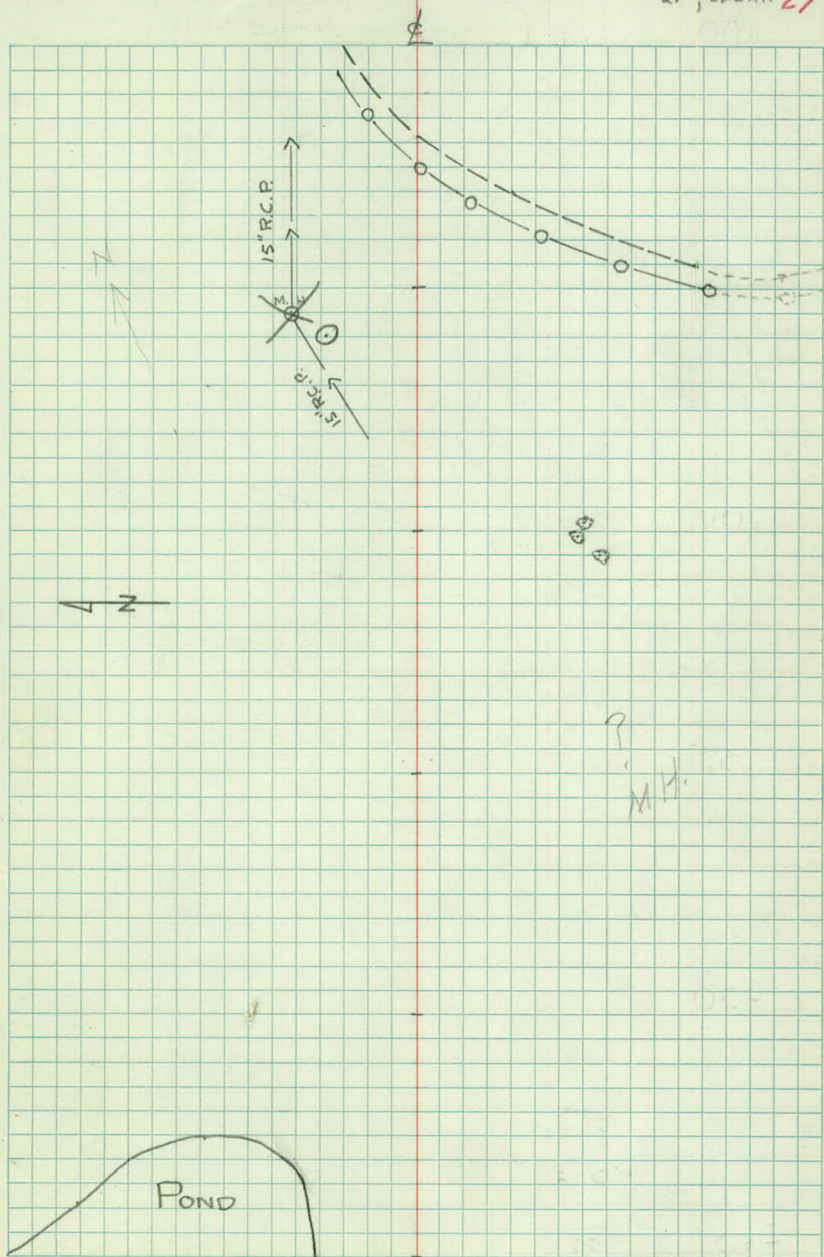
+50

$$\begin{array}{r}
 +20 \text{ N Edge Pond} \checkmark \\
 \underline{40} \\
 +20 \text{ S Edge} \checkmark \\
 \underline{25}
 \end{array}$$

39+00

$$\begin{array}{r}
 +00 \text{ S Edge Pond} \checkmark \\
 \underline{21}
 \end{array}$$

MARCH 16, 1965
21°, CLEAR 27



44+00

+00 $\frac{B.T.}{16}$ LT.

E

+00 $\frac{B.T.}{15}$ RT.+87 $\frac{E.R. \checkmark}{15}$ +74 $\frac{E.R. \checkmark}{17}$ +63 $\frac{Stop Sign \checkmark}{29}$

+50

+50 $\frac{P.R. \checkmark}{44}$ +50 $\frac{P.O.R. \checkmark}{26}$ +67 $\frac{P.O.R. \checkmark}{22}$ +37 $\frac{P.O.R. \checkmark}{34}$ +23 $\frac{P.O.R. \checkmark}{53}$ +14 $\frac{B.R. \checkmark}{78}$ +14 $\frac{Cor. Conc. \checkmark}{59}$ +14 $\frac{Edge Conc. \checkmark}{4}$ +45 $\frac{P.O.R. \checkmark}{34}$ +31 $\frac{P.O.R. \checkmark}{46}$ +23 $\frac{P.O.R. \checkmark}{73}$ +18 $\frac{B.R. \checkmark}{94}$

43+00

+88 $\frac{Edge B.T. \checkmark}{110}$ +88 $\frac{Edge B.T. \checkmark}{96}$ +73 $\frac{P.O.R. \checkmark}{36}$ +64 $\frac{P.O.R. \checkmark}{38}$ +57 $\frac{P.O.R. \checkmark}{46}$ +52 $\frac{B.R. \checkmark}{70}$ +90 $\frac{Edge Conc. \checkmark}{59}$ +90 $\frac{Cor. Conc. \checkmark}{59}$ +82 $\frac{Edge B.T. \checkmark}{69}$ +79 $\frac{E.R. \checkmark}{49}$ +79 $\frac{B.T. \checkmark}{57}$ +73 $\frac{P.O.R. \checkmark}{39}$ +69 $\frac{P.O.R. \checkmark}{30}$ +58 $\frac{P.O.R. \checkmark}{35}$ +53 $\frac{P.O.R. \checkmark}{50}$ +48 $\frac{Edge B.T. \checkmark}{73}$ +44 $\frac{Edge B.T. \checkmark}{91}$ +87 $\frac{B.T. \checkmark}{78}$ +84 $\frac{B.T. \checkmark}{58}$ +64 $\frac{P.R. \checkmark}{38}$

+50

+39 $\frac{Edge Conc. \checkmark}{4}$ +15 $\frac{Edge Conc. \checkmark}{4}$ +08 $\frac{P.O.R. \checkmark}{65}$ +11 $\frac{End B. \checkmark}{94}$

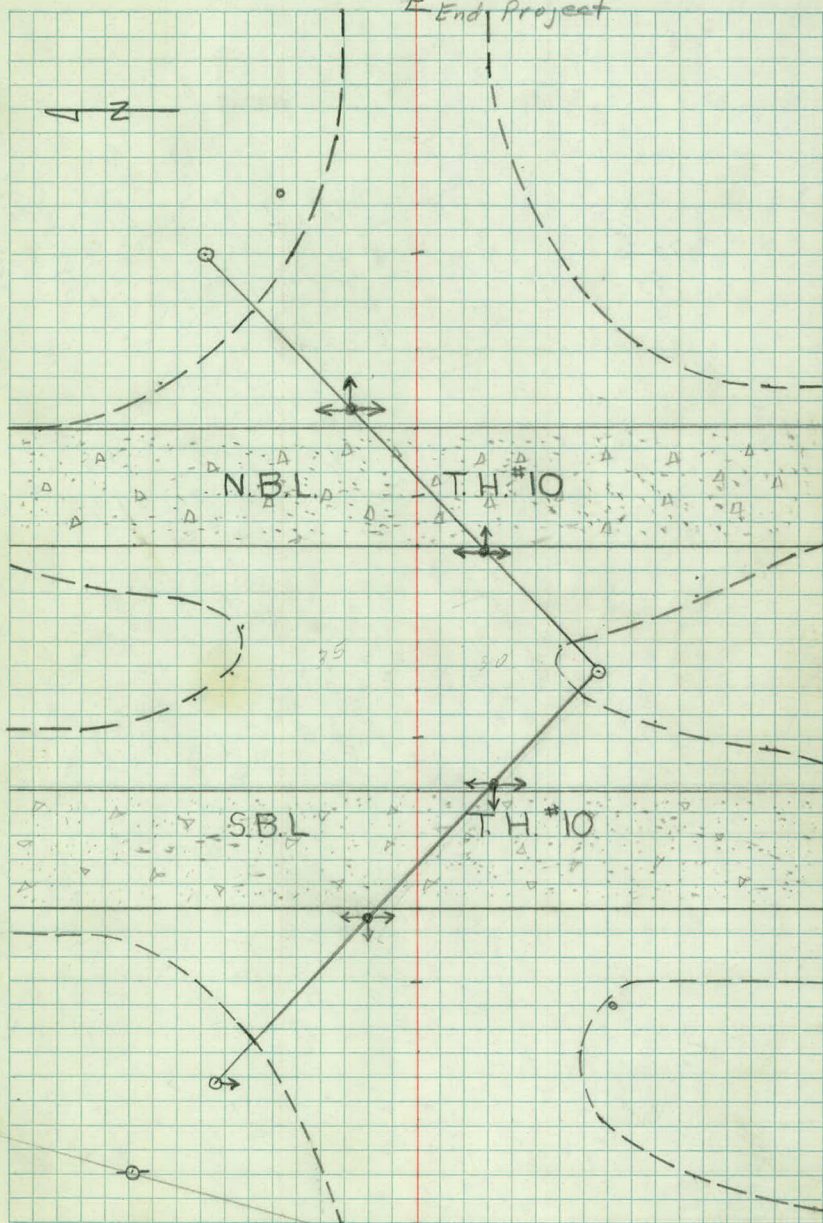
42+00

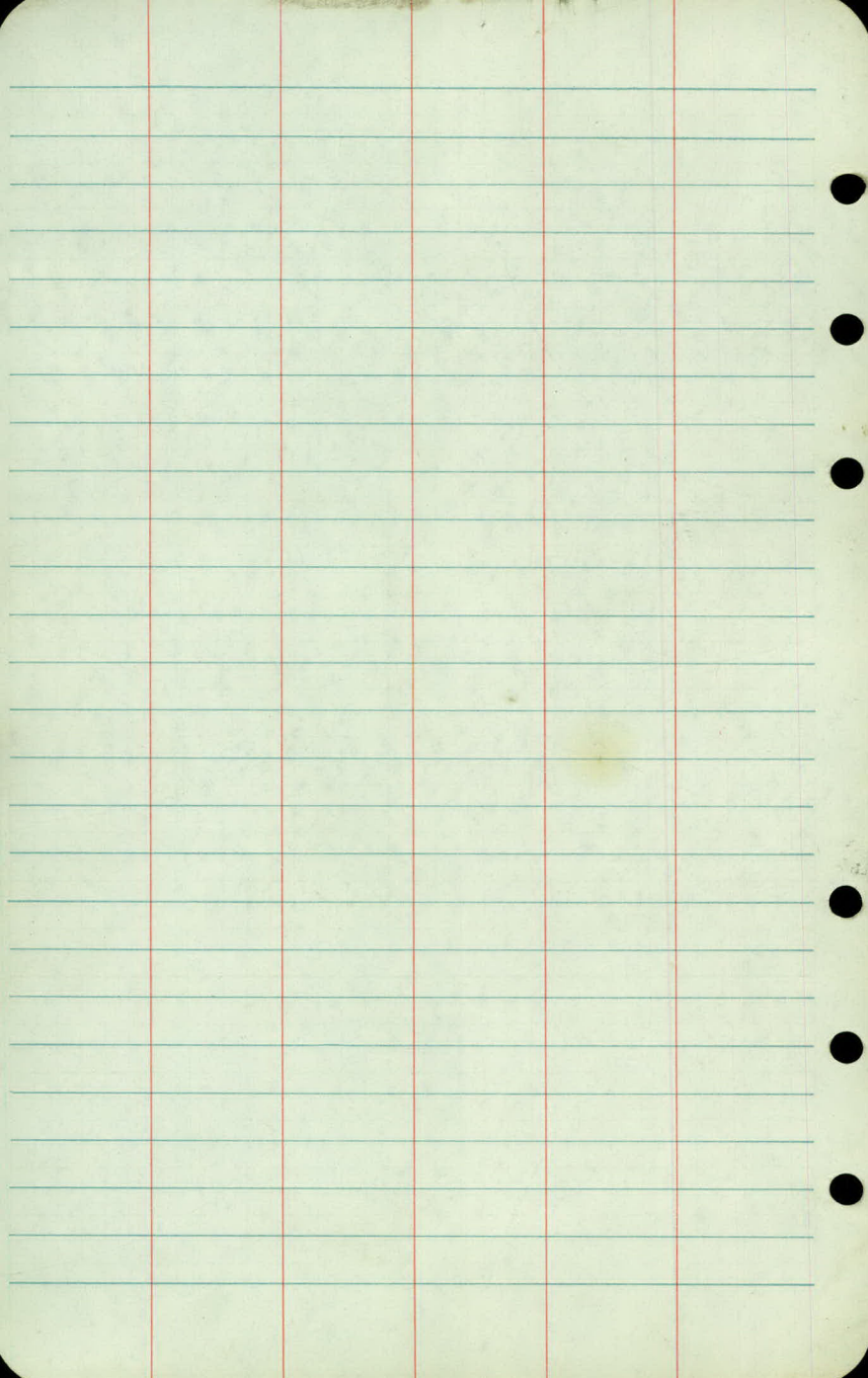
+00 $\frac{P.O.R. \checkmark}{46}$ +00 $\frac{End R.R. \checkmark}{44}$ +85 $\frac{P.O.R. \checkmark}{34}$ +72 $\frac{P.O.R. \checkmark}{38}$ +60 $\frac{P.O.R. \checkmark}{57}$ +53 $\frac{P.O.R. \checkmark}{83}$ +95 $\frac{Stop Sign \checkmark}{42}$ +79 $\frac{Signal Pole \checkmark}{42}$ +88 $\frac{P.O.R. \checkmark}{35}$ +65 $\frac{Edge B.T. \checkmark}{21}$ +61 $\frac{P.R. \checkmark}{59}$

+50

MARCH 16, 1965
CLEAR 21° 28'

End Project





RG
DS
PK
LPD

Feb 18, 1965
cloudy 20°

29

11

X-Sections

Sta	+	π	-	E/V.
BM	3.05	911.10		908.05

0+00 E Long Lake Rd.

0+00 5.56 905.54

+17 shoulder Lt & Rt

+25

+30

+50

+75

Feb 18, 1962

31

44

2

Rt

12

Top Hyd. N.E. Cor. Long Lake Rd $\frac{1}{2}$ Co. Rd. "H"

04.3	04.7	05.0	05.2	05.4	05.4	05.5	05.6	05.7	05.8	05.8	05.8	05.7
6.8	6.4	6.1	5.9	5.7	5.7	5.62	5.5	5.4	5.3	5.3	5.3	5.4
200	150	100	75	50	25	Top	25	50	75	100	150	200
						Mont.						

So. rim M.H. Rt 18'

5.2	5.5	5.4	5.8	5.6	5.6	5.5
5.9	5.6	5.7	5.3	5.6	5.5	5.6
75	49	25	✓ 25	48	75	

05.2	05.9	05.5	05.3	05.8	05.4	05.8	06.0	06.3
5.9	5.2	5.6	5.8	5.3	5.7	5.3	5.1	4.8
75	53	33	16	20	31	54	75	

05.3	05.8	05.7	05.4	05.9	05.3	05.1	06.6	08.0
58	53	54	57	52	58	52	45	31
75	56	26	15	/ 19 31		47	75	

05.7	05.9	06.0	05.7	06.1	06.0	07.2	07.8	08.0	07.9
54	5.20	5.1	5.4	5.0	5.1	3.9	3.3	3.1	3.2
75	55	24	14	✓ 16	26	41	65	75	
	3W								

[illegible]

Sta

+

π

-

Elev.

911.10

1+00

+50

TP

4.96

910.84

5.22

905.88

+

+90

2+00

+50

LT

E

RT

13

06.3	06.5	06.8	06.1	06.4	06.9	07.8	08.2	08.2	08.1	07.7
4.79	4.6	4.3	5.0	4.7	4.7	3.3	2.9	2.9	3.0	3.4
49	37	25	18	✓ 15	15	25	41	60	75	83
SW										HO

06.2	06.1	06.0	06.2	06.3	07.6	07.7	07.7
4.88	4.98	5.1	4.9	4.9	3.5	3.4	3.4
41	23	15	✓ 17	28	45	75	
CONC.	CONC.						

05.0	05.1	05.4	05.4	05.9	05.8	06.5	06.8	07.7
5.8	5.7	5.4	5.4	4.9	5.0	4.3	4.0	3.05
75	62	35	19	✓ 15	22	43		73
			BT					CONC.

05.5	05.4	05.6	05.6	05.9	05.8	06.6	06.9	07.2	07.6
5.3	5.4	5.2	5.2	4.9	5.0	4.2	3.9	3.6	3.2
75	51	31	23	✓ 14	22	38	54	69	
								HO	

05.4	05.1	05.4	05.4	05.8	05.6	06.1	06.3	06.6	06.1
5.4	5.7	5.4	5.4	5.0	5.2	4.7	4.5	4.2	4.7
80	58	34	19	✓ 14	24	48	68	75	

Sta + π - E/V.

910.84

3 + 85

4.89

3+00

TP. 440 911.03 4.21 906.63

+50

+75

5.19

4+00

LT

E

RT

14

Garage ent. slab 89 FT. LT.

05.96	05.4	05.2	05.8	05.5	05.9	06.3	06.78
4.88	5.4	5.6	5.0	5.3	4.9	4.5	4.06
75	43	22		13	26	46	70
SW							conc

Top SW COR Lower Step House 2515 COR H

05.5	05.4	05.1	05.2	05.3	05.9	05.7	05.8	06.2	06.91
55	56	59	58	57	51	5.3	5.2	4.8	4.12
82	75	55	35	21		14	26	41	71
HO									conc

Garage conc ent slab 82 FT. LT.

06.1	05.6	05.5	05.9	05.8	06.0	06.0	06.1
4.9	5.4	5.5	5.1	5.2	5.0	5.0	4.9
83	38	21		13	25	46	72
HO							HO

Sta + π - Elev.

911.03

+50

+83

4.60

5+00

+19

3.80

+50

+59

3.8

BM 3.19 912.65 1.56 909.47 (909.46)

Lt

L

RT

15

05.1 05.3 05.8 05.6 06.0 05.9 06.4 06.4 06.4
 5.9 5.7 5.2 5.4 5.7 5.1 4.6 4.6 4.6
 7.5 54 31 18 11 23 44 68
 HO

Conc Garage ent 95 FT. RT.

07.0 07.0 06.6 06.4 05.9 06.2 06.4 06.9 06.7 07.0
 4.0 39.7 4.4 4.6 5.1 4.8 4.6 4.1 4.3 4.0
 82 76 52 31 21 10 19 42 75
 HO SW

Conc Garage ent Slab 34 FT. LT.

07.9 07.4 07.6 06.4 06.4 06.4 07.0 06.6 07.1 07.1
 21 36 34 4.6 4.6 4.6 4.0 4.4 3.9 3.9
 83 59 33 20 8 16 35 61 75
 HO

PT on Driveway RT. 80 FT.

Top Hyd N.W. Cor. Irondale Rd & Co. Rd. "H"

Sta + π - E/V.

912.65

6+00

+49 Gutter Line Lt & Rt

+60 $\frac{1}{2}$ Irondale RD

+71 Gutter Line Lt & Rt

7+00

+37

4.06

Lt

L

Rt

16

08.2	08.2	08.2	07.8	06.7	06.8	06.8	06.8	08.4	08.5	08.5	08.4
4.5	4.5	4.5	4.9	6.0	5.9	5.9	5.9	4.3	4.2	4.2	4.3
82	75	56	38	22	8	✓	5	14	39	58	66
Ho											Ho

06.8	07.0	07.4	07.6	07.7	07.8	08.2	08.5	08.6
5.9	5.7	5.3	5.1	5.0	4.9	4.5	4.2	4.1
75	56	24	11	✓	8	39	58	75

04.8	05.7	06.5	06.9	07.5	07.6	07.8	07.9	08.0	08.4	08.9	09.4	09.6
7.9	7.0	6.2	5.8	5.2	5.1	4.9	4.8	4.7	4.3	3.8	3.3	3.1
200	150	100	54	24	12	✓	7	24	55	100	150	200

06.7	07.0	07.3	07.4	07.4	07.8	07.8	08.4	07.6	08.9
6.0	5.7	5.4	5.3	5.3	4.9	4.9	4.3	5.1	3.8
75	69	47	25	13	✓	7	32	54	75

08.6	08.0	07.2	07.3	08.1	08.3	08.3	10.1	10.40	10.6
4.2	4.7	5.5	5.9	4.6	3.4	3.4	2.6	2.5	2.1
75	51	32	15	✓	3	2.2	49	58	75

conc
Drill

Edge Conc. S.W. 55 FT. LT.

Sta

+

π

-

E/V

912.65

+46

✓

BM

12.50

913.60

11.55

901.10

901.10

7+71

✓

8+00

FK
WM
WS
PS
LP
PK

Feb. 19, 1965

36

Lt

£

Rt

17

02.13 08.5 08.5 08.4 07.6 07.4 08.4 09.6 10.7 ✓
992 424 424 43 5.1 5.3 4.3 31 2.0
67 59 56 42 27 12 ✓ 21 48
SW SW SW H0

02.0
10.70
75
SW

Top N.E. Cor Lower Step To Garage ±200' E Irondale

07.1 07.3 07.3 07.5 07.9 ✓ 08.9 09.5 10.2 11.0
5.9 6.3 6.3 6.1 5.7 4.7 4.1 3.4 2.6
32 25 18 9 ✓ 14 34 52 75

07.8 02.1 02.2
5.8 11.5 11.4
57 69 75

06.7 06.8 06.2 06.5 06.6 07.9 ✓ 08.8 08.6 09.3 09.5
6.9 6.8 7.4 7.1 7.0 5.7 4.8 5.0 4.3 4.1
54 31 24 17 10 ✓ 14 33 56 75

02.3 01.8
11.3 11.8
65 75

+27 +35
Sta + π - EIV
913.60

8+27

✓

+35

✓

+49 Walk 35' Lt 9.45

+69

✓

Feb. 19, 1965

37

LT

Z

RT

18

5.3	04.8	05.2	05.1	07.1	07.9	07.3	07.5
8.3	8.8	8.4	8.5	6.5	5.7	6.3	6.1
36	24	16	9		22	47	75

05.4	02.9	02.0
8.2	10.7	11.6
54	64	75

05.0	04.2	04.5	04.4	05.4	05.5	06.8	07.0	07.1
8.6	9.4	9.1	9.2	8.2	8.1	6.8	6.6	6.5
35	26	17	10		17	21	29	51

05.2
8.4
59
75
HO

06.8
6.8
75

S.W CORNER OF SIDEWALK HOUSE #2409

04.4	04.4	03.3	02.5	02.6	02.3	02.9	03.1	04.3	03.9	03.8
9.17	9.2	10.3	11.1	11.0	11.3	10.7	10.5	9.3	9.7	9.8
COND. 57	37	30	24	15	8		14	23	51	75

04.4
9.2
63
HO

sta + π - E/V.

913.60

9+00

✓

BM 0.97 902.07 12.50 901.10

+13

+01

✓

+13 & ENT. ON LEFT.

+26

Feb. 19, 1965 38

Lt £ Rt 19

01.1	00.3	00.5	00.2	00.1 ✓	02.1	01.7	01.4
12.5	13.3	13.1	13.4	13.5	11.5	11.9	12.2
32	22	12	6	✓	22	52	75

03.8	01.1	00.4
9.8	12.50	13.16
39	59	67
	CONC	

00.1	00.4	00.3	00.6	00.2	00.1 ✓
2.0	1.7	1.8	1.5	1.9	2.0
47	35	22	13	7	✓

Duplicate sta 9 rt

00.5
1.6
66

00.4	00.1	99.5	99.5	99.2	99.3	99.9	00.6	00.6	00.6
1.65	2.0	2.6	2.6	2.9	2.8	2.2	1.5	1.5	1.5
65	52	33	20	11	✓	17	32	56	75
CONC									

00.0	98.8	98.1	98.1	98.2	00.5 ✓	99.2 ✓	00.2	99.2	99.1
2.1	3.3	4.0	4.0	3.9	1.6	2.9	1.9	2.9	3.0
45	30	19	11	4		15	23	39	59

00.6
1.5
66

00.1
1.4
75

98.5
3.6
75

sta

+

π

-

E/V.

902.07

9+50

9+50

✓

+62

✓

+84 & STREET ON LEFT

✓

Feb. 19, 1965

39

Lt.

E

Rt

20

97.5	96.1	95.4	95.5	95.4	95.1	97.2	97.3	97.1	96.7	96.8
46	60	6.7	66	67	70	4.9	4.8	5.0	5.4	5.3
39	27	18	11	5	✓	8	23	42	65	75

96.8	96.1
5.3	60
60	75

92.7	94.0	94.1	94.1	93.9	93.8	96.2	96.2	95.8	95.5
9.4	81	8.0	8.0	8.2	8.3	5.9	5.9	6.3	6.6
49	31	19	12	6	✓	6	27	53	75

91.9	91.9
10.2	10.2
63	75

91.0	91.6	91.9	92.3	91.3	92.3	92.5	94.4	94.1	94.6
11.1	10.5	10.2	9.8	10.8	9.8	8.6	7.7	8.0	7.5
75	49	32	17	9	✓	9	27	44	75

91.0	88.9	87.8
11.7	13.2	14.3
100	150	200

STA. + I - ELEV.

902.07

10+00

✓

+12

✓

TBM 0.47 892.90 9.64 892.43 (892.43)

+56

✓

Feb. 19, 1965 40

LT.

2

RT.

21

90.8	91.5	92.1	91.8	91.6	91.6	92.4	93.4	93.1	93.6
11.3	10.6	10.0	10.3	10.5	10.5	9.7	8.7	9.0	8.5
64	41	24	16	10	9	27	42	55	

90.8

11.3
75

93.5

8.6
75

90.5	91.0	91.6	91.3	91.0	90.8	91.9	92.3	93.1	93.4	93.1
11.6	11.1	10.5	10.8	11.1	11.3	10.2	9.8	9.0	8.7	8.7
55	37	25	18	11	8	25	44	53	75	

90.2

11.9
75

Bent SPIKE IN TWIN 8" OAK 5' RT

88.1	87.6	87.5	87.7	88.0	89.0	89.1	89.6	89.3	89.2
4.8	5.3	5.4	5.2	4.9	3.9	3.8	3.3	3.6	3.7
38	28	18	5	5	24	43	60	75	

87.8

5.1
51

87.9

5.0
68

87.5

5.4
75

Sta + X - Elev

892.90

11

+31

✓

BM 7.78 888.83 11.85 881.05

+66

✓

12

+26 MH 28' Lt

11.03 877.80

~~2.03~~ 881.80

BM

7.78 881.05 (881.05)

Feb 12, 1965 41 22

Lt

85.9	85.6	84.6	84.4	84.1	83.2	83.6	84.3	83.9	84.0
70	73	8.3	8.5	8.8	9.7	9.3	8.6	9.0	8.9
75	54	37	24	18	✓	8	28	51	75

81.8	81.0	80.1	79.7	80.3	80.3	80.1	80.6	79.8
11.1	11.9	12.8	13.2	12.6	12.6	12.8	12.3	13.1
40	28	23	10	✓	16	37	52	75

82.9	83.5	84.6
10.0	9.4	8.3
46	51	75

Bent Spike N. Side 18" Elm Lt Sta 12+00

79.4	79.0	78.1	77.8	78.4	78.4	78.3	78.3	78.1
9.4	9.8	10.7	11.0	10.4	10.4	10.5	10.5	10.7
36	28	18	7	✓	13	30	48	75

80.1	80.7	82.4
8.7	8.1	6.4
41	46	75

80.5	80.5	79.1	78.2	78.4	76.1	74.1	73.9	74.9	75.6
8.3	8.3	9.7	10.6	10.4	12.7	14.7	14.9	12.9	13.2
75	67	41	32	20	✓	12	39	63	75

Bent Spike N. Side 18" Elm Lt Sta 12+00

Sta	+	π	-	E/V.
BM	6.55	887.60		881.05

12+36 Top Bank Rt

+40 & Ditch Rt

+44 Top Bank Rt

+75

13+00

+15

12.86

73.74

+50

RG
DS
WS
PK

clear 10' 42
23

Lt.

+

Rt.

Bent spike in N. Side 18" Elm Lt. Sta 12+00

78.6	78.0	78.1	78.1	77.6	76.2	76.3	75.4	74.5	74.5	73.2
9.0	9.6	9.5	9.5	10.0	11.4	11.3	12.2	13.1	13.1	14.4
75	56	40	24	15	9		10	25	45	75

78.6	77.6	77.7	77.8	76.2	76.2	76.2	74.0	71.92	70.8	71.2	70.9	70.9
9.0	10.0	9.9	9.8	11.4	11.4	11.4	13.20	15.68	16.8	16.4	13.714	
75	50	35	14	9		10	28	32	36	53	58	7
							Top 30" Apron	Inv.	Ditch	Bank		

78.6	77.6	77.2	78.0	77.7	76.1	75.7	75.0	74.1	73.2	71.4	74.1	73.4
9.0	10.0	10.4	9.6	9.9	11.5	11.9	12.6	14.5	14.4	16.2	13.5	14.2
75	60	43	21	14	9		22	35	49	50-58 ditch	61	75

77.1	76.8	77.3	77.3	75.7	74.7	73.8	73.4	73.9
10.5	10.8	10.3	10.3	11.9	12.9	13.8	14.2	13.7
75	67	38	14		15	42	60	75

78.3	77.2	77.5	76.4	75.9	74.7	73.8	73.4	73.0	72.9
9.3	10.4	10.1	11.2	11.7	12.9	13.8	14.2	14.6	14.7
75	49	26	18		21	33	50	60	75

W. rim MH 10' Lt.

81.6	80.8	80.0	79.4	76.5	75.8	75.1	73.3	73.1	72.6
6.0	6.8	7.6	8.2	11.1	11.9	12.5	14.3	14.5	15.0
100	75	55	29	15		27	40	55	75

Sta	+	π	-	Elev.
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		887.60		
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13+70				
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14+00				
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+50				
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15+00				
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TP	7.83	889.63	5.80	881.80
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15+50				
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16+00				
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March 19, 1965 43
24

2+

8

R+

85.7	85.7	85.3	84.4	80.0	76.8	75.7	74.6	73.2	73.2	73.4
1.9	1.9	2.3	3.2	2.6	10.8	11.9	13.0	14.4	14.4	14.2
100	90	66	39	27	15	✓	30	47	60	75

86.9	85.3	85.2	85.7	85.1	79.3	76.6	76.1	74.3	72.9	73.4
0.7	2.3	2.4	1.9	2.5	8.3	11.0	11.5	13.3	14.7	14.2
150	100	81	56	38	21	9	✓	35	55	75

86.9	85.0	85.0	85.0	85.2	83.6	78.8	75.1	74.9	74.0	72.7	72.3
0.7	2.6	2.6	2.6	2.4	4.0	8.8	11.5	12.7	13.6	14.9	15.3
150	100	75	53	39	29	16	✓	28	55	60	75

87.1	85.6	85.0	85.2	84.5	81.5	78.5	77.4	75.4	74.7	73.6	73.0
0.5	2.0	2.6	2.4	3.1	6.1	9.1	10.2	12.2	12.9	14.0	14.6
150	100	81	53	29	20	9	✓	27	52	64	75

	86.1	85.4	84.7	79.5	75.0	75.7	75.5	74.4
Snowbank	3.5	4.2	4.9	10.1	11.6	13.9	14.1	15.2
	83	55	30	10	✓	31	61	75

	86.5	85.6	85.3	80.9	79.0	77.7	76.7	75.3
Snowbank	3.1	4.0	4.3	8.7	10.6	11.8	12.9	14.3
	96	58	30	13	✓	28	55	75

Sta	+	π	-	Elv.
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		889.63		
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16+50				
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+85				
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		10.11	879.52	
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17+00				
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+50				
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18+00				
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+50				
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19+00				
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Mar. 10, 1965

44
25

Lt.

E

Rt

87.0	86.6	86.3	85.4	84.7	82.1	79.7	79.0	78.3	77.9	77.3
2.6	3.0	3.3	4.2	4.9	7.5	9.9	10.6	11.3	11.7	12.3
125	100	82	57	28	13	✓	30	51	70	75

Top W. rim MH Lt 10'

88.1	87.1	85.8	85.0	83.1	80.7	79.2	79.0	78.4	77.4
1.5	2.6	3.8	4.6	6.5	8.9	10.4	10.6	11.2	12.2
100	75	58	31	26	13	✓	24	42	75

88.1	86.8	85.4	84.3	82.9	79.2	78.0	77.6	77.7	77.5
1.5	2.8	4.2	5.3	8.7	10.4	11.6	12.0	11.9	12.1
100	74	54	31	13	✓	17	43	63	75

87.6	87.2	86.4	84.1	80.6	79.5	80.1	77.7	77.4	76.6
2.0	2.4	3.2	5.5	9.0	10.1	9.5	11.9	12.2	13.0
100	82	64	35	14	✓	10	31	55	75

88.7	88.4	87.3	86.1	84.4	80.8	79.4	80.6	82.4	79.5	77.6	76.2	76.5
0.9	1.2	2.3	3.5	5.2	8.8	10.2	9.0	7.2	10.1	12.0	13.4	13.1
100	85	62	35	27	14	✓	4	5	28	45	62	75

88.2	87.9	86.3	83.9	81.6	79.1	78.3	78.8	80.0	76.5	74.5	74.0
6.4	1.7	3.3	5.7	8.0	10.5	11.3	10.8	9.6	13.1	15.1	15.6
100	78	52	35	25	13	✓	6	7	31	59	75

Sta

+

π

-

E/V

889.63

19+50

20+00

+85

TP

4.42

882.12

11.93

877.20

+50

21+00

+50

+80

Mar. 19, 1965 ⁴⁵
26

LT E RT

87.6	87.4	86.0	82.5	81.3	79.9	77.3	75.1	75.3	74.9	74.5
2.0	2.2	3.6	2.1	8.3	11.7	12.3	14.5	14.3	14.7	15.1
100	82	68	47	27	14		19	30	53	75

83.4	81.1	78.7	77.4	75.9	75.0	75.3	74.5	74.6
6.2	8.5	10.9	12.2	13.7	14.6	14.3	15.1	15.0
84	69	46	19		20	37	64	75

Top W. rim MH Lt 10' Sta 20+85

77.4	76.3	74.8	75.1	74.7	74.6	73.8	73.7
4.7	5.8	7.3	7.0	7.4	7.5	8.3	8.4
75	46	12		17	44	66	75

76.6	75.9	75.6	75.2	74.9	74.6	75.4	74.3	74.5	74.9
5.5	6.2	6.5	6.9	7.2	7.5	6.7	7.8	7.6	7.2
75	50	35	14		15	20	40	61	75

76.3	75.9	74.9	74.2	74.7	74.3	74.1	74.9	73.1	72.9	72.9
5.8	6.2	7.2	7.9	7.4	7.8	8.0	7.2	9.0	9.2	12.7
75	54	31	10		19	12	28	54	85	87

± 2' ditch

76.2	75.7	74.8	74.3	74.5	73.6	71.3	73.7	74.3	73.3
5.9	6.4	7.3	7.8	7.6	8.5	10.8	8.4	7.8	8.8
75	51	32	8		13	17	21	53	75

± 2' ditch

Sta	+	π	-	Elev
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		882.12		
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22+00				
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+50				
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23+00				
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+50				
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+				
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		5.93	876.19	
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BM				
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	5.32			
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		879.75		
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			7.71	
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				874.41
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				874.43
--	--	--	--	--------

24+00				
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+50				
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Mar. 10, 1965 46

Lt

E

Rt

27

75.7	76.0	75.0	74.4	74.7	74.9	73.5	73.3	73.8
6.4	6.1	7.1	7.7	7.4	7.2	8.6	8.8	8.3
75	60	39	15	13	13	32	56	75

75.6	74.6	72.4	75.5	76.7	74.4	75.1	74.5	73.9	73.7	73.6
6.5	7.5	9.7	6.6	5.4	7.7	7.0	7.4	8.2	8.4	8.5
75	61	56	51	44	16	14	14	37	58	75

ditch

75.2	72.8	75.0	76.8	76.0	75.2	75.2	75.3	74.9	74.3	74.6
6.9	9.3	7.1	5.3	6.1	6.9	6.8	6.8	7.2	7.8	7.5
100	93	85	69	40	15	12	12	33	51	75

ditch

76.4	76.3	76.0	74.7	75.0	74.5	73.4	74.0	73.4
5.7	5.8	6.1	7.4	7.1	7.6	8.7	8.1	8.7
75	66	38	19	19	19	40	64	75

Top W. rim MH 10' Lt Sta 23+72

N. edge top step in M.H. Sta 23+72 / +10'

76.7	76.9	74.4	74.4	74.6	74.2	74.1	74.1	73.2
3.1	2.9	5.4	5.4	5.3	5.6	5.7	5.7	6.6
75	55	41	22	13	13	36	59	75

74.0	73.3	73.6	73.9	74.1	73.8	72.8	72.1
5.8	6.5	6.2	5.9	5.7	6.0	7.0	7.7
75	56	35	16	23	23	45	75

Sta

+

 π

-

E/V.

879.75

25+00

+50

26+00

+50

27+25

BM

4.77

874.98

874.96

Mar 10, 1965

47
28

Lt

R

Rt

72.7
7.1
75

72.5
7.3
69

73.8
6.0
57

74.7
5.1
44

73.9
5.9
36

73.8
6.0
14

~~73.3~~
~~5.5~~

73.4
6.4
21

70.7
8.1
46

70.7
8.1
75

73.3
6.5
75

~~74.4~~
5.4
60

74.6
5.2
40

73.3
6.5
28

72.2
6.6
14

~~73.1~~
~~6.7~~

73.3
6.5
14

72.0
7.8
30

70.7
8.1
55

70.5
8.3
75

73.8
6.0
75

74.0
5.8
52

73.1
6.7
29

72.7
7.1
8

~~72.1~~
~~7.1~~

73.2
6.6
20

72.2
7.6
49

71.5
8.3
75

72.9
6.9
75

72.9
6.9
48

72.5
7.3
26

73.2
6.6
4

~~73.0~~
~~6.8~~

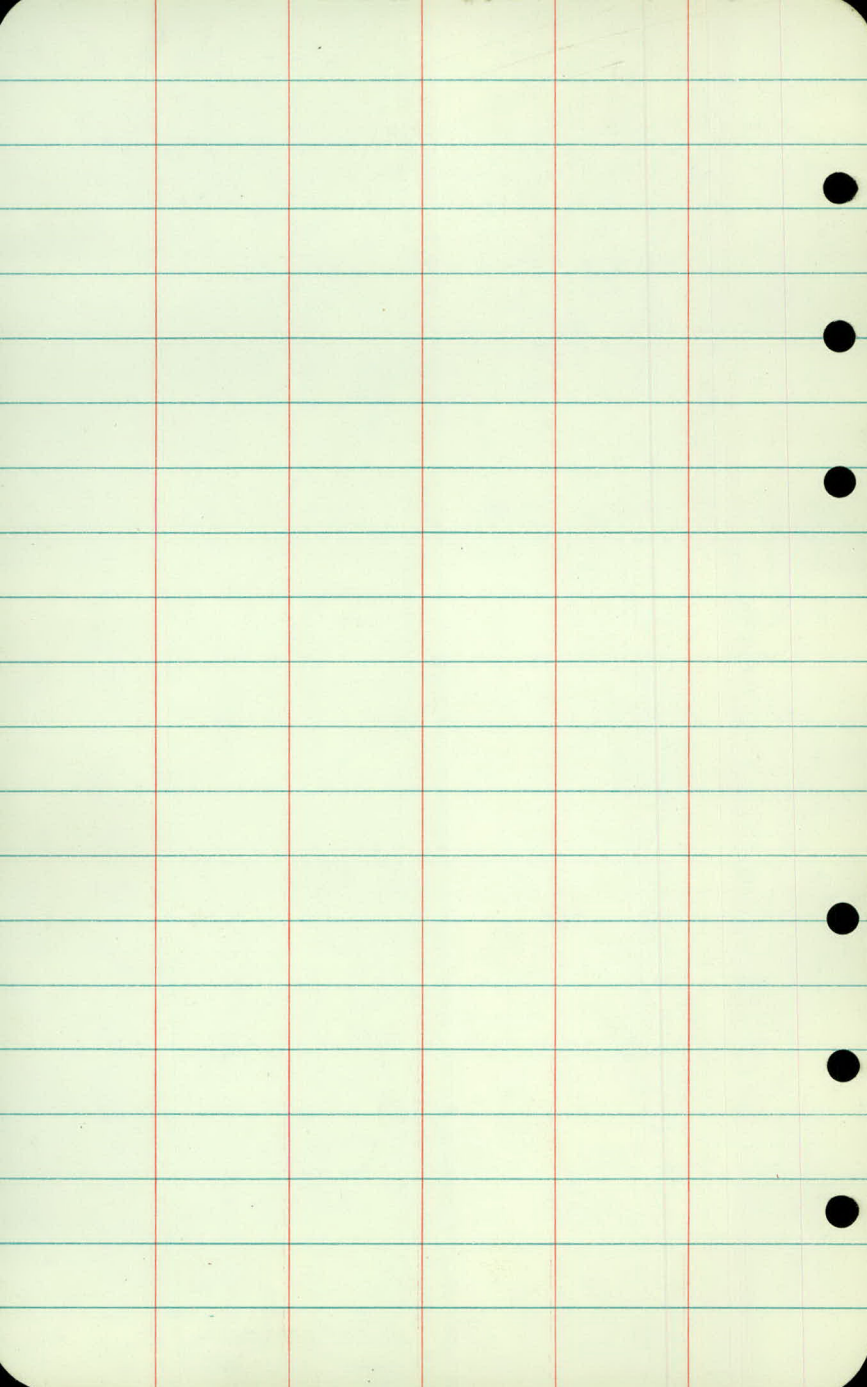
72.9
6.9
26

71.3
8.5
26

71.0
8.8
55

70.8
9.0
75

Top So. rim MH Lt Sta 27+25±



48
29

Sta	+	π	-	Elev.
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B.M.	4.54	879.49		874.95
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27+00

+50

28+00

+50

29+00

+50

TP	5.43	879.19	5.72	873.77	(873.26)
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RG
W44
WS
PK
LPP

Feb 23, 1965
Cloudy 0°

49
30

LT.

£

RT

Top So. Rim M.H. Casting Sta 27+23 LT 10'

873.0	73.3	73.1	72.7	72.4	71.6	71.3	71.3	71.7
6.5	6.2	6.4	6.8	7.1	7.9	8.2	8.2	7.8
75	50	33	24	4	16	45	75	

873.5	72.9	72.3	72.3	72.3	72.2	71.2	71.3	71.3	71.3	71.6	71.6	71.5
6.0	6.6	7.2	7.2	7.2	7.3	8.3	8.2	8.2	8.2	7.9	7.9	8.0
75	58	38	20	2	6	14	24	37	45	59	75	

74.3	73.8	72.7	73.0	73.1	72.3	71.4	71.9	71.9	71.3
5.2	5.7	6.8	6.5	6.4	7.7	8.1	7.6	7.6	8.2
75	57	42	24	5	9	34	56	75	

73.3	74.8	74.0	73.1	72.4	73.8	72.9	72.0	71.4	71.5	71.3
6.2	4.7	5.5	6.4	7.1	5.7	6.6	7.5	8.1	8.0	8.2
75	73	44	38	10	6	3	28	53	75	

74.2	74.7	74.4	73.4	72.9	73.0	72.3	72.4	71.6	71.5	72.3	69.0
5.3	4.8	5.1	6.1	6.6	6.5	7.2	7.1	7.9	8.0	7.2	10.5
75	68	50	31	15	13	12	35	51	69	75	creek

74.0	74.0	73.7	73.0	72.5	72.3	69.1	69.1	71.5	71.5	70.7
5.5	5.5	5.8	6.5	7.2	10.4	10.4	7.6	8.0	8.8	
75	69	43	17	10	18	30	38	40	75	

So. rim M.H. Casting LT Sta 29+30+ creek

Sta

+

T

-

E/V,

879.2
879.19

30+00

+50

✓

+73

East edge creek (Rt)

+78

Top Bank (Rt)

31+00

Feb 23, 1965
P.C. 50

50
31

Lx

2

Rt

74.1	73.4	73.0	73.7	73.9	72.0	67.1	67.1	72.8	72.5	72.0
5.1	5.8	6.2	5.5	5.3	7.2	12.1	12.1	6.4	6.7	7.2
75	43	23	6		12	17	26	32	66	75
						cr.	cr.			

74.6	74.1	73.8	73.1	72.7	73.6	72.4	70.2	67.5	67.2	71.3	70.7
4.6	5.1	5.4	6.1	6.5	5.6	6.8	9.0	11.7	12.0	9.9	9.5
75	52	40	23	10	9	17	22	33	37	42	
							cr.	cr.		Bank	

67.5	68.2
11.7	11.0
75	49
cr.	cr.

74.4	74.3	74.1	73.3	72.1	72.3	73.6	72.3	67.8	67.4	68.3
4.8	4.9	5.1	5.9	7.1	6.9	5.6	6.9	11.4	11.8	10.9
75	50	40	22	6	13	23	31	47	75	
							cr.	cr.	cr.	

74.4	74.5	74.0	73.2	72.1	72.3	72.6	72.4	71.3	71.9	71.8
9.8	9.7	5.2	6.0	7.1	6.9	6.6	6.8	7.9	7.3	7.4
75	57	40	24	7	9	24	40	58	75	

74.9	74.8	74.5	74.4	73.2	72.1	71.9	71.5	72.3	71.5	72.6	72.1	68.4	68.3
4.3	4.4	4.7	4.8	6.0	7.1	7.3	6.9	7.7	6.6	7.1	10.8	10.9	
75	60	46	39	20	10	15	18	25	39	58	61	75	
											cr.	cr.	

Sta

+

π

-

Lt

879.19

31+25

+50

32+00

+25

+50

33+00

BM

2.80

877.40

4.59

874.60

874.60

Feb 23, 1965

51

Lt

\$

12+

32

74.8	74.9	74.8	72.8	72.6	72.3	72.1	71.6	68.3	68.4	72.0	71.9	71.9
4.4	4.3	5.2	6.4	6.6	6.9	7.1	7.6	10.9	10.8	7.2	7.3	7.3
75	58	39	23	16	✓	16	28	35	60	64	75	80
								cr.	cr.			

73.3	73.3	73.3	73.0	72.7	72.5	72.4	68.1	68.5	71.6	71.7
5.9	5.9	5.9	6.2	6.5	6.7	6.8	11.1	10.7	7.6	7.5
75	63	46	38	18	✓	14	21	44	50	75
							cr.	cr.		

72.9	72.1	72.0	72.7	72.4	72.3	72.1	68.4	68.5	72.1	71.7
6.3	7.1	7.2	6.5	6.8	6.9	7.1	10.8	10.7	7.1	7.5
75	48	38	21	15	✓	6	11	33	50	75
							cr	cr		

72.1	72.1	72.1	72.3	72.2	72.1	71.7	70.6	68.4	68.7	72.0	72.1
7.1	7.1	7.1	6.9	7.0	7.1	7.5	8.6	10.8	10.5	7.2	7.1
75	48	38	23	16	✓	10	24	35	62	68	75
								cr.	cr.		

72.7	72.6	72.0	71.9	72.1	72.2	72.2	71.5	70.6	71.0	68.0
6.5	7.2	7.2	7.3	7.1	7.0	7.0	7.7	8.6	8.2	11.2
75	48	38	21	9	✓	14	29	43	66	75
										cr

72.7	72.5	72.4	72.2	71.2	72.3	72.9	71.3	71.8	71.8	71.2
6.5	6.7	6.8	7.0	8.0	6.9	6.3	4.9	7.4	7.4	8.0
75	48	41	21	5	✓	22	28	38	61	75

Top 50. rim MH casting Lt Sta 33+30 ±

Sta + π - Elev

877.40

33+50

+65

+70 Top Bank Rt

34+00

+50

35+00

BM 5.10 879.67 2.83 874.57 874.57

Top MH

2.10
Elev = 876.67

Lt \$ Rt

12.5	12.0	11.9	11.7	11.8	67.9	67.8	67.7	67.7
4.9	5.4	5.5	5.7	5.6	9.5	9.6	9.7	9.7
75	41	23		12	16	31	61	75
				cr.	cr.	cr.	cr.	

12.7	12.0	11.9	11.5	11.8	67.9	67.8	68.0	67.6
4.7	5.4	5.5	5.9	5.6	9.5	9.6	9.4	9.8
75	41	22		14	20	27	47	75
				cr.	cr.	cr.	cr.	

12.6	12.1	11.9	11.7	11.7	67.8	67.8	72.2	72.7	72.6
4.8	5.3	5.5	5.7	5.7	9.6	9.6	5.2	4.7	4.8
75	41	22		15	21	33	38	55	75
				cr.	cr.				

12.7	12.5	12.2	11.9	11.9	11.8	12.0	66.4	66.4	71.9	71.6	70.5
4.7	4.9	5.2	5.5	5.5	5.6	5.4	11.0	11.0	5.5	5.8	6.9
75	65	42	23	11		13	21	33	39	52	75
						cr.					

12.2	12.2	11.8	11.9	12.4	12.5	66.6	66.6	73.1	72.5	72.5
5.2	5.2	5.6	5.5	5.0	4.9	10.8	10.8	4.3	4.9	4.9
75	63	40	15		12	17	31	38	62	75
					cr.	cr.				

12.7	12.6	11.8	11.5	11.4	12.1	11.3	66.8	66.8	71.4	73.3	73.0
4.7	4.8	5.6	5.9	5.9	6.1	10.6	10.6	6.0	4.1	4.4	
75	52	40	24	13	13	19	33	38	61	75	
					cr.	cr.					

No. end Top step in M.H. Rt Sta 37+25

Sta

+

π

-

Elv

879.67

35+37

+43

+60

+82

36+00

+25

RG
WM
PK
LPD

LT

2

Feb 24, 1965
Fair 5°
RT

53
34

12.9	12.6	12.0	12.0	69.5	68.7	69.4	42.9	12.7	12.8
6.8	7.1	7.7	7.7	10.2	11.0	10.3	6.8	7.0	6.9
75	50	28		8	20	30	37	68	75
				cr.	cr.	cr.			

12.1	12.9	12.4	12.7	11.5	69.3	68.1	68.6	12.5	12.8	12.5
6.6	6.8	7.3	7.0	8.2	10.4	11.6	11.1	7.2	6.9	7.2
75	56	36	16	7		12	31	39	62	75
						cr.	cr.			

13.5	13.2	12.9	12.5	69.0	67.9	69.0	71.1	69.0	68.0	68.0	71.6	71.9
6.2	6.5	6.8	7.2	10.7	11.8	10.7	8.6	10.7	11.7	11.7	8.1	7.8
75	56	37	15	6	cr.	6	11	23	35	50	53	75
				cr.		cr.		cr.	cr.	cr.		

13.7	13.7	13.2	13.1	69.0	69.0	71.8	73.1	71.9	71.2	69.0	67.8
6.0	6.0	6.5	6.6	10.7	10.7	7.9	6.6	7.8	8.5	10.7	11.9
75	65	47	25	12	cr.	4	27	39	55	67	75
				cr.						cr.	cr.

13.8	13.8	13.5	11.8	69.0	67.8	69.0	71.2	71.4	72.6	73.3	72.2	72.0	71.5
5.9	5.9	6.2	7.9	10.7	11.9	10.7	8.5	8.3	7.1	6.4	7.5	7.7	8.2
75	68	52	30	22	16	11	4		6	38	51	69	75
				cr	cr	cr							

14.3	14.1	13.7	68.2	69.0	73.9	73.0	73.3	71.8	72.1
5.4	5.6	6.0	11.5	10.7	5.8	4.7	6.4	7.9	7.6
75	63	47	34	30	20		29	54	75
			cr	cr					

Sta

+

π

-

E/V

879.67

36+50

37+00

37+00

37+50

+50

Top Bank Rt

+60

Creek

489

Top Bank Rt

38+00

Feb 25, 1965 54

Lt

♀

Rt

35

15.1	73.8	69.7	68.7	69.6	74.0	73.7	72.7	73.0	72.6	71.6
4.6	5.9	10.0	11.0	10.1	5.7	6.0	7.0	6.7	7.1	8.1
75	58	50	46	40	32	17	✓ 29	48	75	
		cr	cr	cr						

68.1	68.2	72.7	75.1	74.8	72.7	72.9	72.8	71.8	72.6
11.6	11.5	7.0	4.6	4.9	7.0	6.8	6.9	7.9	7.1
75	55	30	16		✓ 9	36	52	71	75
cr	cr								

68.1	68.1	72.3	72.1	72.1	72.5	72.7
11.6	11.6	7.4	7.6	7.6	7.2	7.0
75	40	11	✓ 23	50	75	
cr	cr					

67.5	68.1	68.4	68.4	68.2	70.6	70.7	70.5
12.2	11.6	11.3	11.3	11.5	9.1	9.0	9.2
75	55	25	cr	✓ 26	51	68	75
cr	cr	cr		cr			

67.7	68.2	68.4	68.4	68.9	72.5	73.1	72.9	73.6	73.6	73.6
12.0	11.5	11.3	10.3	10.8	7.2	6.4	6.8	6.1	6.1	5.9
75	55	30	5		✓ 11	25	29	42	58	75
cr	cr	cr	cr							

67.2	67.7	68.1	69.2	71.2	73.0	74.3	74.2	74.3	74.3
12.5	12.0	11.6	10.5	8.5	6.7	5.4	5.5	5.4	5.4
75	55	30	8	✓ 8	23	43	60	75	
cr	cr	cr							

Sta	+	π	-	Elev
-----	---	-------	---	------

		879.67		
--	--	--------	--	--

38+50				
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BM	1.52	880.37	0.81	878.86	878.85
----	------	--------	------	--------	--------

39+00	edge water Lt.				
-------	----------------	--	--	--	--

+50					
-----	--	--	--	--	--

40+00					
-------	--	--	--	--	--

40+30					
-------	--	--	--	--	--

+55					
-----	--	--	--	--	--

Feb 25, 1965 55

36

67.2	67.7	68.1	69.1	71.4	73.8	75.1	75.0	74.8	74.9
12.5	12.0	11.6	10.6	8.3	5.9	4.6	4.7	4.9	4.8
75	55	35	15	7	✓	5	30	55	75
cr	cr	cr	cr						

Top West end Headwall Rice Creek Box Culvert.

RB
with
PK

Feb 26, 1965
cloudy 8°

69.0	69.0	69.0	72.6	76.1	75.2	75.3	75.4
11.4	11.4	11.4	28	53	5.2	5.1	5.0
75	50	21	11	X	28	52	75
cr	cr	cr					

13.9	13.3	13.1	15.4	15.7	15.5	15.3	14.9
6.5	7.1	7.3	5.0	4.9	4.9	5.1	5.5
75	42	23	8	25	51	75	

80.1	76.0	75.3	75.3	75.2	75.1	74.9	74.5
0.3	4.4	5.1	5.1	5.2	5.3	5.5	5.9
75	61	31	17		25	58	75
Disposal pile							

80.4	16.1	15.2	14.2	14.1	13.6	13.3	13.8
0.0	4.0	5.2	6.2	6.1	6.8	7.1	6.6
6.2	48	29	13	✓	24	51	75
Disposal pile							

[illegible]

Sta + π - EIV

880.37

BM 5.66 884.63 1.40 878.97 878.97

40+85

41+00

41+50

41+75

42+00

B.T. Shoulder

42+10

Feb 26, 1965 56

Lt

E

Rt

37

East rim MH casting Lt 25' 40+95

82.2	78.5	77.4	76.6	75.8	76.6	77.2	78.3	79.0
2.4	6.1	7.2	8.0	8.8	8.0	7.4	6.3	5.6
75	63	54	37	21	28	53	75	

Disposal
pile

81.0	79.6	78.6	77.4	77.0	77.4	79.8	80.0	80.0
3.6	5.0	6.0	7.2	7.6	7.2	4.8	4.6	4.6
75	71	61	41	25	24	44	75	

Disposal
pile

BT BT

84.1	78.9	78.3	78.3	80.0	80.1	80.1	79.9	79.9	80.0	80.1
5.0	5.7	6.3	6.3	4.6	4.5	4.5	4.7	4.7	4.6	4.5
75	72	54	40	23	13	50	100	150	200	

BT BT BT BT BT BT

79.8	79.6	78.8	80.3	80.4	80.0	80.0	79.4	79.4	80.1	79.9
4.8	5.0	5.8	4.3	4.2	4.6	4.6	5.2	5.2	4.5	4.7
75	70	39	25	BT	46	52	75	91	100	132

BT BT BT BT BT BT

81.2	81.0	80.9	80.9	80.8	80.7	80.8
3.4	3.6	3.7	3.7	3.8	3.9	3.8
75	47	25	BT	33	61	75

BT BT BT BT BT BT

Sta + π - Elev

884.63

42+14 W. edge Conc. S.B.L. T.H. #10

+26 $\pm$ S.B.L. (PK nail) T.H. #10

BM

5.77

878.86

878.85

Feb 26, 1965

57
38

Lt

£

Rt

83.12

82.52

81.76

81.29

81.08

~~81.08~~

81.13

81.14

81.19

1.51
200

2.11
150

2.87
100

3.34
50

3.55
✓

~~3.55~~
50

3.50
100

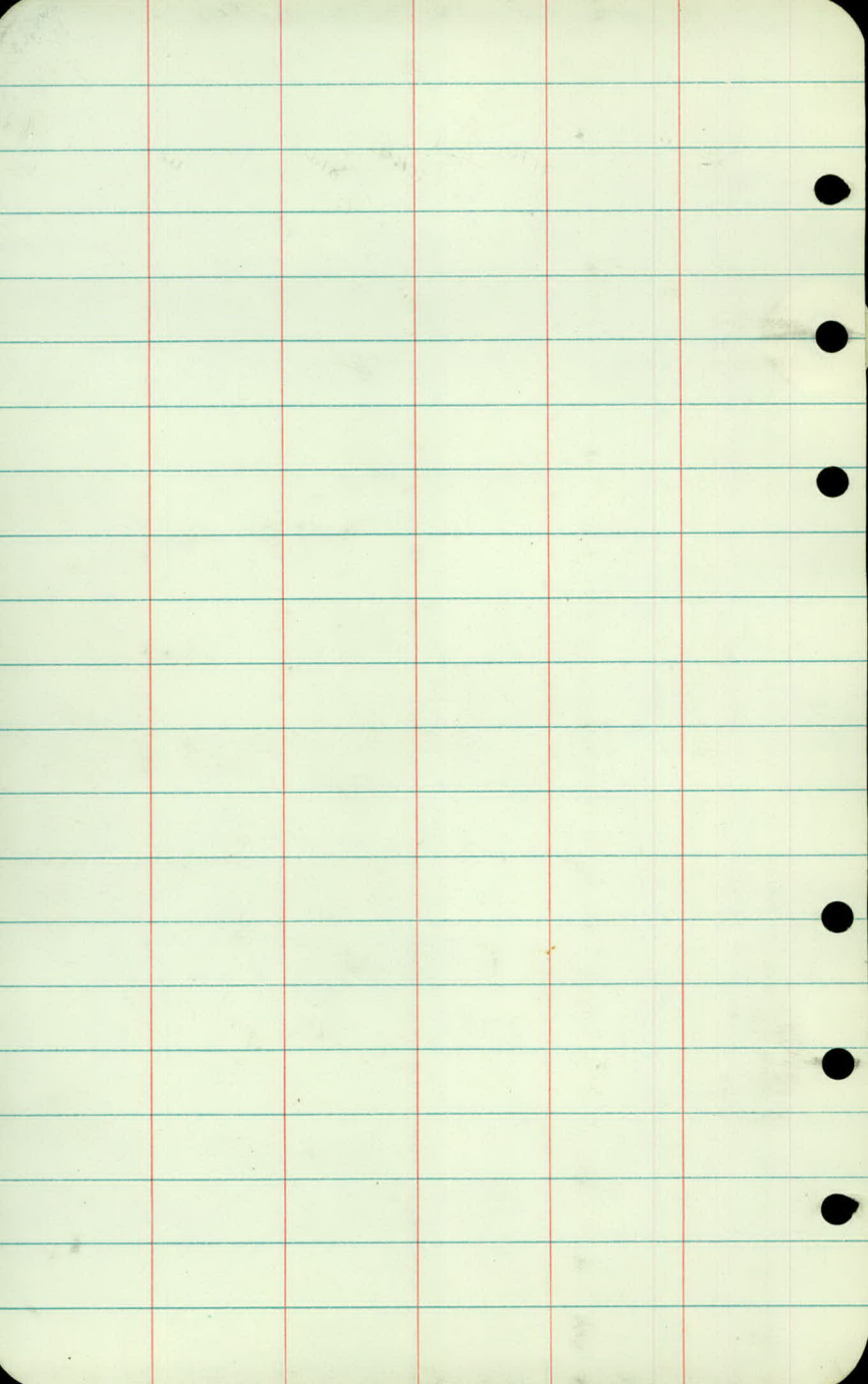
3.49
150

3.44
200

2
81

3.42

Top W. end Wing wall of Box Culvert (Rice Creek)



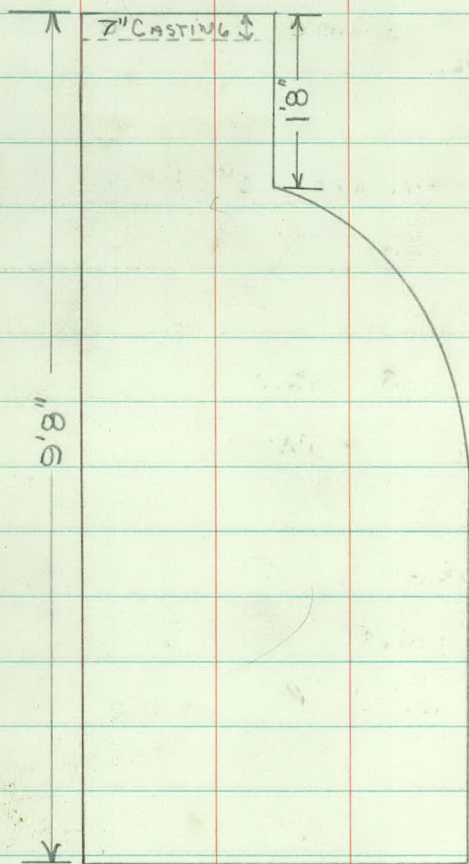
Co. Rd. "H"
Manhole Details

3 pages

Sta. -0+01 RT 17'

MANHOLE #1 SANITARY SEWER 4 RINGS

COMES FROM EAST GOES SOUTH



-0+01 17' RT

13+15

SANITARY SEWER

459
M 2

F.L. TO TOP CASTING 8.4

2' SECTION AT BOT.

4' CONE

3 Rings (Adj.)

7" CASTING

FROM WEST TO EAST 15" (CONCRETE)

FROM NORTH TO EAST 8" (TILE)

16+85

SANITARY SEWER

F.L. TO TOP CASTING

13.65 INVERT

7" CASTING

5 Adj. Rings

W. TO E. 15" RCP

20+85 SANITARY SEWER

4 Adj. Rings

8" CASTING

12.38 TO INVERT

WEST TO EAST 15" R.C.P.

23+72 SANITARY SEWER

8" CASTING

2 Adj. Rings

11.31 TO INVERT

WEST TO EAST 15" R.C.P.

27+21 SANITARY SEWER

4- Adj. Rings

7" CASTINGS

11.39 TO INVERT

WEST TO EAST 15" R.C.P.

29+33 SANITARY SEWER M3 4160

7 Ag. Rings

7" CASTING

9.58 TO INVERT

WEST TO EAST 15" R.C.P.

33+32 SANITARY SEWER

4 Adj. Rings

7" CASTING

10.04 TO INVERT

WEST TO EAST 15" R.C.P.

37+23 SANITARY SEWER

3 Adj. Rings

7" CASTING

11.54 TO INVERT

From WEST TO 30° EAST 15" R.C.P.

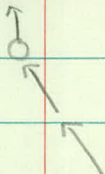
(over)

40+95 SANITARY SEWER

3 Adj. Rings

7" Casting

12.37 TO INVERT



KP
DS
WM
RB
ML

8 JUNE 1965
SUNNY
60°

61
42

LONG LAKE RD
CO. RD H TO WOODCREST
PROFILE

0+00 = SW COR SEC 7-T 30-R 23

59995

REDUCED BY KP
CHECKED BY RB

LONG LAKE RD



CO. RD H 0+00

STA	+	π	-	Elev.
BM	2.37	910.42 102.37		908.05 100.00

0-200

0-150

0-100

0-50

0+00 = $\neq$ Co. Rd H

8 JUNE 1965

LT

E

RT

62.
43

TOP HYDRANT N.E. COR CO. RD. H : LONG LAKE RD.

~~97.7~~
05.1
4.7

~~97.7~~
05.1
4.7

~~97.8~~
05.8
4.6

~~97.7~~
05.7

97.9	98.1	97.8	97.4	97.5	98.0	98.2	98.1	97.9
05.9	06.1	05.8	05.4	05.5	06.0	06.3	06.1	05.9
4.5	4.3	4.6	5.0	4.9	4.4	4.1	4.3	4.5
200	50	100	50	50	100	150	200	

STA + Δ - ELEV.

910.42
102.37

0+58

1+00

TP

4.08

909.11
~~101.06~~

5.39

905.03
~~96.98~~

1+50

+81 = ENTRANCE RT

2+00

LT

E

8 JUNE 1965

RT

63
44~~5.1~~
0.5.15.3
33~~5.3~~
0.5.3

5.1

~~5.6~~
0.5.64.8
33~~5.8~~
0.5.85.6
33~~5.0~~
0.5.0

5.4

~~5.2~~
0.3.27.2
33

TOP OF SPIKE E STA 1100

~~4.2~~
0.4.24.9
33~~4.6~~
0.4.6

4.5

~~4.7~~
0.4.74.4
33~~4.3~~
0.4.34.8
43~~4.4~~
0.4.4

4.7

~~4.5~~
0.4.54.63
33
conc.~~4.4~~
0.4.44.7
43~~4.3~~
0.4.3

4.8

~~4.9~~
0.3.95.2
33

STA + π - ELEV.

909.11
~~101.06~~

+55 = ENTRANCE LT

+65 = ENTRANCE RT

3+00

+33 ENTRANCES LT & RT

+50

4+00 ENTRANCE LT.

8 JUNE 1968

64

LT

E

RT

45

~~9.0~~
~~0 4.0~~

5.1

43

~~9.2~~
~~0 4.2~~

4.9

~~9.3~~
~~0 4.3~~

4.8

33

~~9.1~~
~~0 4.1~~

5.0

43

~~9.1~~
~~0 4.1~~

5.0

~~9.1~~
~~0 4.1~~

5.0

33

~~9.0~~
~~0 4.0~~

5.1

43

~~9.0~~
~~0 4.0~~

5.1

~~9.0~~
~~0 4.0~~

5.1

33

~~9.2~~
~~0 4.2~~

4.9

43

~~9.1~~
~~0 4.1~~

5.0

~~9.4~~
~~0 4.0~~

5.12

33

conc.

~~9.2~~
~~0 4.2~~

4.9

43

~~9.0~~
~~0 4.0~~

5.1

~~9.1~~
~~0 4.1~~

5.0

33

~~9.5~~
~~0 4.5~~

4.6

43

~~9.9~~
~~0 3.9~~

5.2

~~9.8~~
~~0 4.8~~

4.3

33

STA + π -

909.11
~~101.06~~

4+14 = ENTRANCE RT

+50

+79 = ENTRANCE LT

5+00 = ENTRANCE RT.

+50

6+00 = ENTRANCE RT

+60 = $\frac{1}{2}$ WOODCREST DRIVE

BM

1.05

908.06
~~100.00~~

908.05
100.00

8 JULY 1965

65

LT

E

RT

46

~~4.6~~
~~0.0~~

~~4.0~~
~~0.0~~

~~4.1~~
~~0.0~~

4.5
43

5.1

3.92
33
conc.

~~4.6~~
~~0.0~~

~~3.9~~
~~0.0~~

~~5.0~~
~~0.0~~

4.5
43

5.2

4.1
33

~~4.0~~
~~0.0~~

~~3.8~~
~~0.0~~

~~4.9~~
~~0.0~~

5.1
43

5.3

4.4
33

~~4.3~~
~~0.0~~

~~3.1~~
~~0.0~~

~~4.0~~
~~0.0~~

4.8
43

5.4

5.1
33

~~4.0~~
~~0.0~~

~~3.1~~
~~0.0~~

~~3.3~~
~~0.0~~

5.1
43

6.0

5.8
33

~~3.1~~
~~0.0~~

~~2.1~~
~~0.0~~

~~3.1~~
~~0.0~~

5.7
43

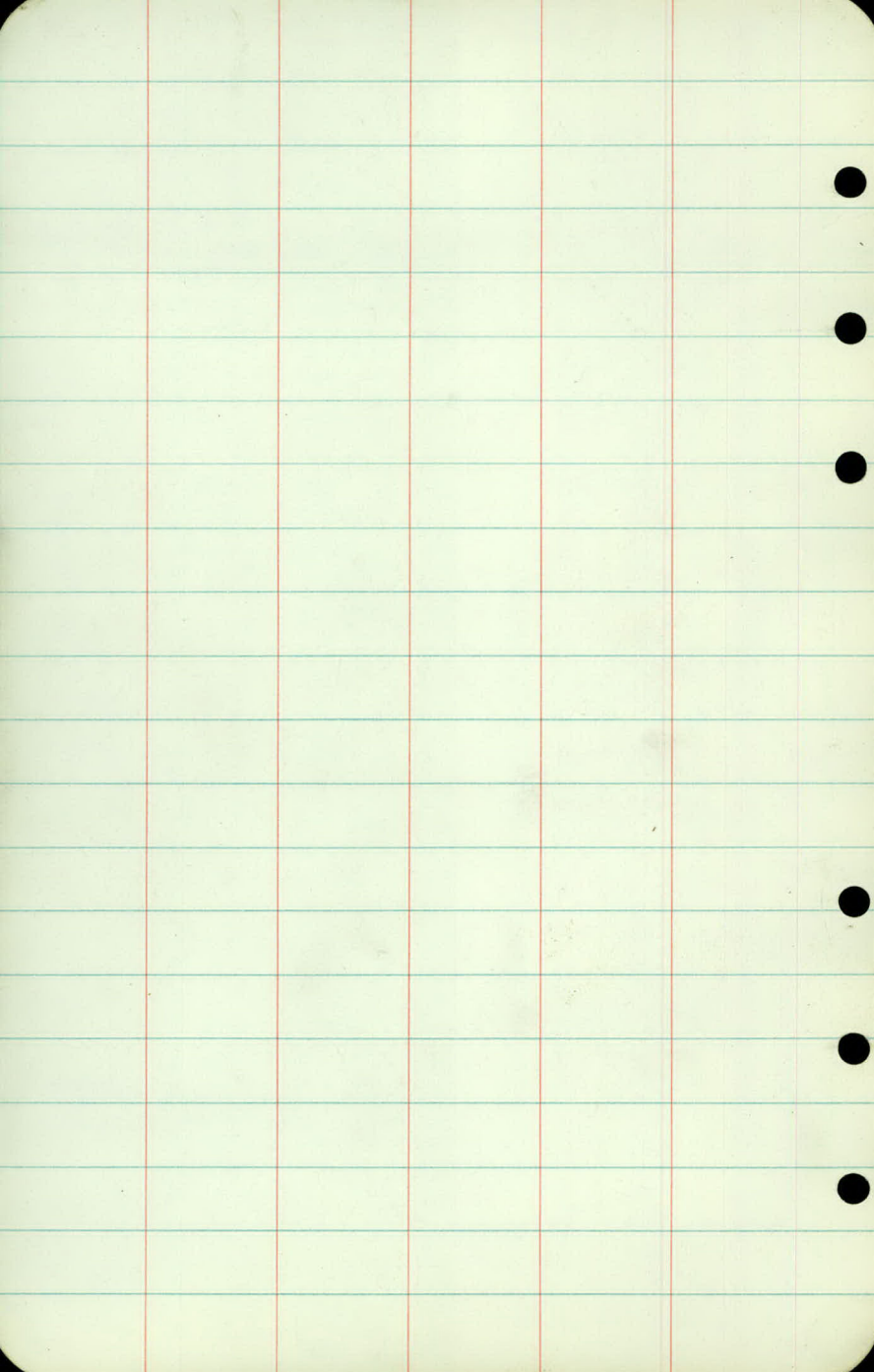
6.7

6.0
33

~~1.6~~
~~0.0~~

7.5

TOP HYDRANT NE COR COR RD 4 LONG LAKE RD.



FK
PK
LPD

June 14, 1965
Clear Cool 55' 66
47

Co Rd "H"

M. H. Elev.

Sta	+	π	-	Elev.
BM	3.45	904.55		(901.10)
BM			9.79	894.76
T.P.	0.72	892.92	12.35	892.20
MH			1.31	891.61
BM	1.06	882.13	11.85	881.07
MH			4.32	877.81
MH			7.37	874.76 13+
MH			0.80	
BM	6.36	884.02	4.47	877.66
TP	6.06	885.65	4.43	879.59
TP	3.28	881.04	7.89	877.76
TP			4.80	876.24

All beyond are inaccessible.

June 14, 1965

4867

2

Top NE Cor Lower Step To Garage

Top Hyd N.W. Cor $9+66$ Lt $32'$
NE Cor Garage $+44$ Lt $32'$
 $9+85$

MH NE Cor. Garage $+63'$ Lt $10'$

NE Garage $+65$ Iron Φ

Lt 27.5 NE Cor Garage $+85'$
 $10+07$

Bent Spike in 18" Elm Lt $75'$ $\pm$

Storm Sewer MH

Lt $8'$ $\pm$ st N

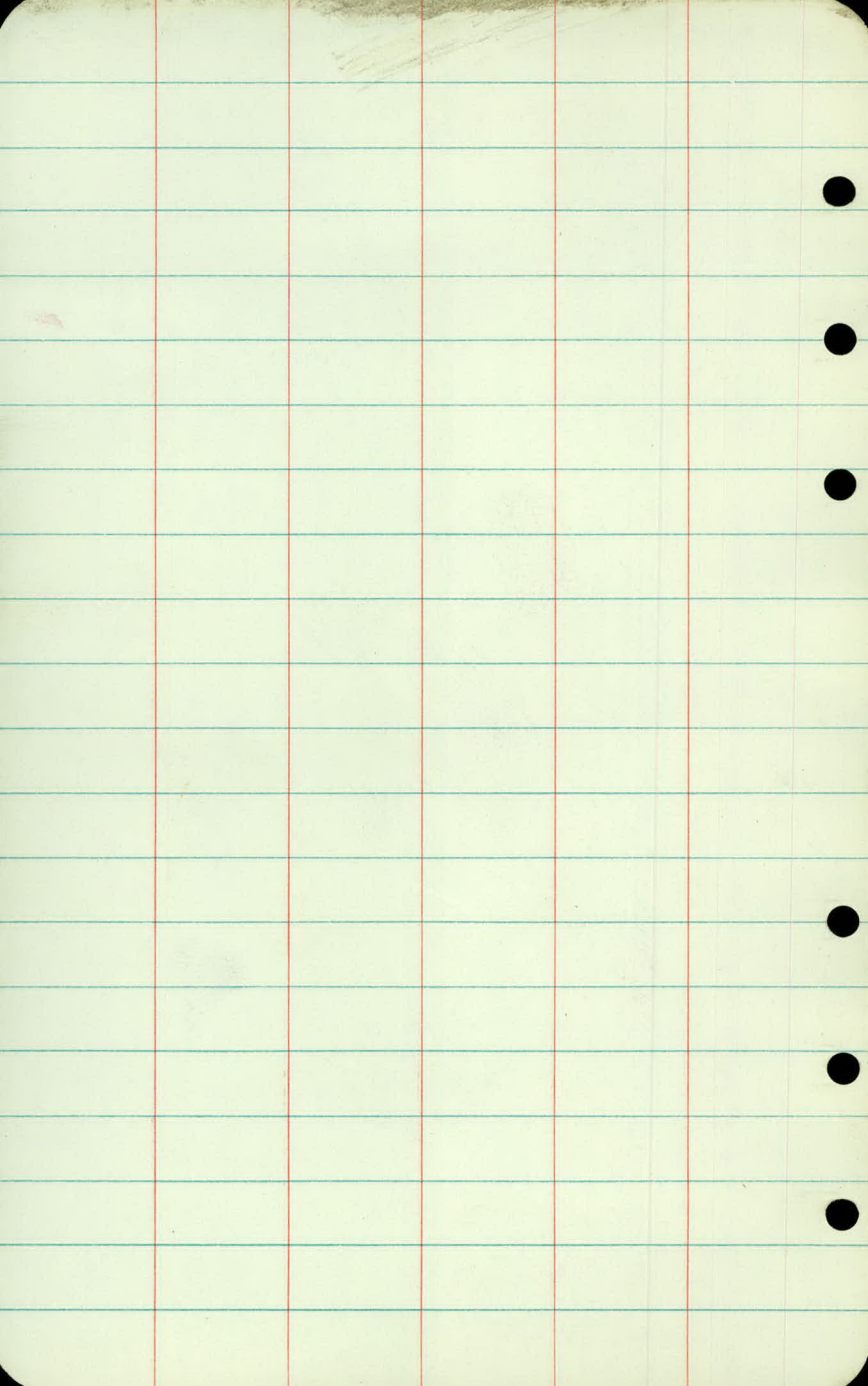
Top MH Lt $118'$ $\pm$ st N

Top Hyd N.W. Cor $+ Co Rd 'H'$ ✓

MH Lt $9'$ at Beg Woods Rt

MH previously used

MH Sta $23+74^{\pm}$



July 7, 1965

~~4968~~
3

Additional x-sections
at
Long Lake Rd.

Long Lake Rd.

Sta + π - Elev

BM 2.09 910.14

908.05

1+58

2+00 = Co. Rd. H

2+42

Co. Rd H

0-22

0-47

0-100'

0-92 Walk 17' Lt 4.16

MH Rt 18' of 0+00 4.61 905.53 905.54

BM 1.85 908.29

PK
PK
LPD
RP
HL

July 7, 1965

5069
4

Top Hyd N.E. Cor. Long Lake Rd & H

04.1	06.1	06.1	05.4	05.1	06.1	06.1	05.3	06.1	07.5	07.1
5.4	4.0	4.0	4.7	4.4	4.0	4.0	4.8	3.4	2.6	2.5
75	50	25	13		14	16	22	31	50	75

East side

06.1	06.3	05.6	05.2	04.7	05.0	05.2	05.1	05.2	05.7	06.0	06.4
4.0	3.8	4.5	4.9	5.4	5.1	4.9	5.0	4.9	4.4	4.14	3.73
75	68	54	40	17	12		14	21	40	56	75

Walk

04.9	05.0	05.4	05.1	05.4	05.1	05.2	05.4
5.2	5.1	4.7	5.0	4.7	5.0	4.9	4.7
75	50	25	19		21	50	75

South side

05.0	05.3	05.4	05.4	05.2	05.2	05.4	05.2	05.3	05.0	05.3
5.1	4.8	4.7	4.7	4.9	4.9	4.7	4.9	4.8	5.1	4.8
75	50	30	16	13	9		17	25	50	75

06.3	06.1	06.0	05.7	05.8	05.5	05.7	04.7	04.9
3.8	4.0	4.1	4.4	4.3	4.6	4.4	5.4	5.2
50	26	14	10		15	25	50	75

South

Top Hyd S.E. Cor. Long Lake Rd & "H"

Sta + Δ - Elev.

BM 4.77 879.20 874.43

21+87 Profile Ditch

66
1.2

Rim MH

2.99 876.21 (876.19)

PA
PK
LPP
RP
HL

11

July 8, 1965
Overcast
Rt

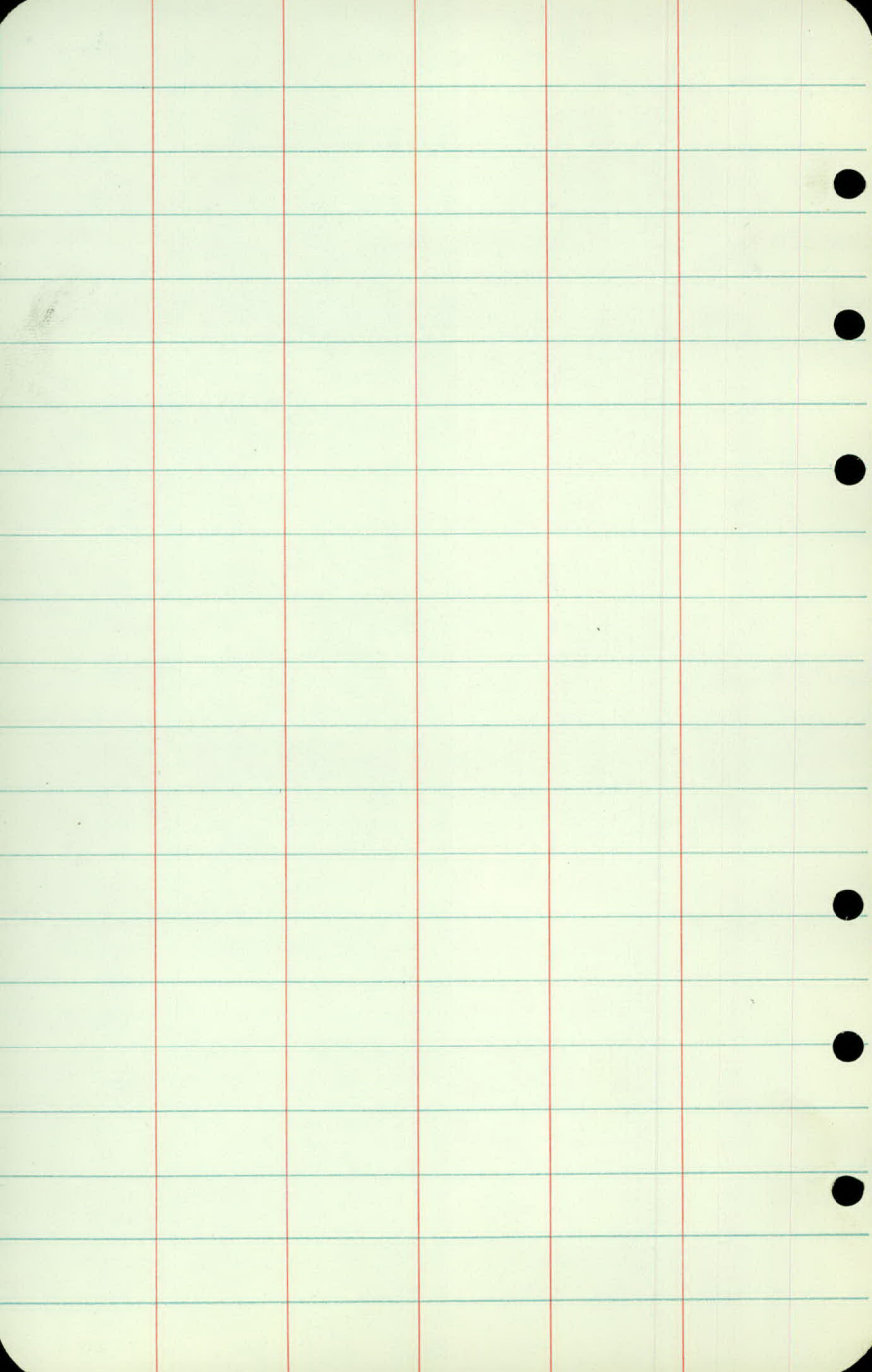
5170

N. Edge Top step M.H. 10' Lt Sta 23+72

71.2	70.8	71.6	72.4	71.6	71.4	71.3	70.3	71.3
8.0	8.4	7.6	6.8	7.6	7.8	7.9	8.9	7.9
100	65	38	19	2	14	25	50	75
infill				Culvert				

71.3	71.4	71.1	71.2	70.9	71.2
7.9	7.8	8.1	8.0	8.3	8.0
125	150	175	200	120	100
				Edge Creek	

10' Lt Sta 23+72



July 8, 1965

~~52~~⁷¹
a

New x-sections

Sta + π - Elev.

BM 2.76 903.86 901.10

9+23

BM 5.66 900.42 9.10 894.76 (894.76)

+36

✓

+47

Lt.

July 8, 1965
Rain Rt.~~5372~~

6

Top N.E. Cor Lower step to Garage

98.1	98.6	98.00	98.1	97.0	98.3	98.6	99.1	99.2	99.1
5.8	5.3	5.9	5.8	6.9	5.6	5.4	4.2	4.7	4.2
26	18	12	7	4		2	6	15	2.1

99.0	99.7	00.4	00.0		98.3	98.6	98.9
4.9	4.2	3.5	3.9		5.6	5.3	5.0
36	45	65	75		75	60	41

Top Hyd N.W. Cor 4th St & Co. Rd. "H"

93.3	96.8	96.6	94.9	96.9	96.9	98.1	98.8	98.3	98.3
7.1	3.6	3.8	5.5	3.5	3.5	2.3	1.6	2.1	2.1
23	18	10	7	4		9	22	50	75

97.2	97.4	97.3	97.5
3.2	3.0	3.1	2.9
27	44	60	75

92.0	95.2	96.3	93.0	94.9	95.8	97.1	97.3	97.8	97.4	97.4
8.4	5.2	5.1	7.4	5.5	4.6	3.3	3.1	2.6	3.0	3.0
22	20	7	5	3		4	10	20	25	50

92.8	96.6	97.1	95.5	96.8	96.3
7.6	3.8	3.2	4.9	3.6	4.1
25	28	45	52	55	75

97.0
3.4
75

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		900.42		
--	--	--------	--	--

9+65				
------	--	--	--	--

✓				
---	--	--	--	--

+85				
-----	--	--	--	--

✓				
---	--	--	--	--

10				
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PK
LPD
RP
HL

Lt

July 9, 1965

5473
C

93.6	93.7	89.8	92.5	93.6	93.9	94.0	94.5	95.9	96.2
6.8	6.7	10.6	7.9	6.8	6.5	6.4	5.9	4.5	4.2
18	12	10	9	6		4	5	6	9

90.2	90.3	93.0	92.4	91.8	91.6	95.1	95.2	95.4	95.8
10.2	10.1	7.4	8.0	8.6	8.8	5.3	5.2	5.0	4.6
20	26	29	42	58	75	75	50	29	21

92.0	88.8	88.7	92.1	92.1	92.4	92.1	93.5	94.3
8.4	11.6	11.7	8.25	8.3	8.0	8.3	6.9	6.1
21	19	12	MH		3	5	17	27
			9					

91.8	91.0	90.4		94.7	94.4
8.6	9.4	10.0		5.7	6.0
40	60	75		75	50

87.7	87.7	91.1	90.2	91.7	91.8	92.2	93.5	93.3	93.7
12.7	12.7	9.3	10.2	8.7	8.6	8.2	6.9	7.1	6.7
19	15	11	7	3		10	26	48	75

90.7	91.6	90.8	90.4
9.7	8.8	9.6	10.0
23	35	59	75

Sta + π - Elev.

900.42

10+05

✓

+21

✓

TBM 0.10 892.5⁵ 7.97 892.45 (892.42)

+57

✓

BM

11.44

881.08

(881.05)

July 9, 1965

5574

1+

4

RT d

89.5	87.4	87.4	91.1	91.5	90.8	91.8	91.7	92.4	92.9
10.9	130	130	9.3	8.9	9.6	8.6	8.7	8.0	7.5
22	20	14	11		2	5	9	14	33

91.7	91.3	90.3	90.1
8.72	9.1	10.1	10.3
MH	41	63	75
27.5			

93.2	93.3
7.2	7.1
75	52

86.5	86.5	88.0	90.0	90.0	90.4	90.6	89.9	91.1
13.9	13.9	12.4	10.4	10.4	10.0	9.8	10.5	9.3
19	15	10	7		2	4	5	13

89.5	89.4	88.9
10.9	11.0	11.5
21	50	75

92.7	92.4	91.0
7.7	8.0	9.4
75	50	26

Bent spike in 8" Tw Out

85.8	86.9	85.6	84.5	84.4	85.9	85.7	85.8	87.1	87.8	86.2	86.4
6.7	5.6	6.9	8.0	8.1	6.6	6.8	6.7	5.4	4.7	6.3	6.1
22	20	17	13	8	6		3	10	15	16	17

87.3	87.9	87.6	87.6
5.2	4.6	4.9	4.9
26	37	60	75

88.3	86.9	87.1	88.1	88.1
4.2	5.6	5.4	4.4	4.4
22	22	20	20	18

88.2	88.8	87.2	88.3	89.1	89.1	87.4	87.1	87.8
4.3	3.7	5.3	4.2	3.4	3.4	5.1	4.8	4.2
75	59	23	25	32	38	39	45	48

Sta + π - Elev

892.52

11+00

✓

+50

✓

BM 2.91 883.99 11.44 881.08

12

✓

July 9, 1965

5625

Lt.

E

Rt

C

83.3	82.5	82.1	82.1	82.5	82.8	83.8	83.8	83.5	84.1
9.2	10.0	10.4	10.4	10.0	9.7	8.7	8.7	9.0	8.4
24	19	13	7		4	16	39	56	61

83.8	84.1	84.6	84.8	83.9		83.1	83.3
8.7	8.4	7.9	7.7	6.8		9.4	9.2
31	34	41	57	75		75	67

80.5	79.5	79.6	80.1	80.2	80.9	82.4	81.1	79.9
12.0	13.0	12.9	12.4	12.3	11.6	10.1	11.4	12.6
41	31	15	11		2	5	8	10

81.5	81.8	82.6	83.4	79.1	79.2	79.3	79.4	79.6	79.4
11.0	10.7	9.9	9.1	13.4	13.3	13.2	13.1	12.9	13.1
46	50	63	75	75	54	41	32	27	15

Beat Spike in 18" film Lt Sta 12+00

77.2	77.8	79.8	81.1	81.3	79.6	78.2	76.3	75.4	73.9	73.7
6.8	6.2	4.2	2.3	2.7	4.4	5.8	2.7	8.6	10.1	10.3
19	12	8	4	2		3	6	26	48	75

77.2	78.2	79.7	80.3	80.7
6.8	5.8	4.3	3.7	3.3
31	36	44	54	75

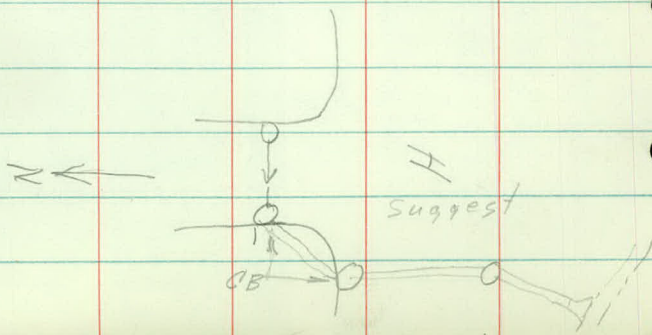
Sta + π - Elev

883.99

12+26

+44

+60 Ditch Line North



July 9, 1965

5776

Lt.

L

BT

F

16.0	16.0	19.4	17.6	18.8	17.9	17.6	16.3	14.6	14.2	13.4
8.0	8.0	4.6	6.4	5.2	6.1	6.4	7.7	9.4	9.8	10.6
17	7	5	3	2		1	6	13	27	39

18.3	17.8	17.8	17.9	18.1
5.7	6.18	4.2	6.1	5.9
21	MH	44	63	75
28				

13.1	13.5
10.9	10.5
75	58

17.6	16.4	16.8	15.2	15.3	16.5	17.0	5.4	16.2	14.7	14.4
6.4	7.6	2.2	8.8	8.7	7.5	7.0	8.6	7.8	9.3	9.58
75	48	28	21	4		4	9	19	25	29

Top Apron

13.1	13.5	11.9
10.9	10.5	12.10
75	57	29

Apron

16.8	15.7	15.0	14.8	14.9	14.6	14.3	13.8	13.3	13.4
7.2	8.3	9.0	9.2	9.1	9.4	9.7	10.2	10.7	10.6
75	71	52	35	23		4	18	30	45

80.0

4.0 for Drainage from North

11.6	11.1	12.8
12.4	12.3	11.2
75	65	56
Ditch		

Sta + π - Elev.

883.99

12+81

+90 Possible G.V. 1436'

13

+14 ϕ 1st St.

+41

BM 9.47 887.13 6.34 877.65 (877.66)

July 9, 1965

5877

Lt

2

RT

9

18.1	17.8	16.9	16.2	15.1	15.2	14.4	14.0	14.0
5.9	6.2	7.1	7.8	8.9	8.8	9.6	10.0	10.0
75	68	65	42	19		20	33	75

16.2	15.1	16.0	16.0	80.1	80.3	8.4	82.3	82.3	19.9	14.9
7.8	8.3	8.0	8.0	3.9	3.7	2.6	1.7	1.7	4.1	9.1
26	19	15	7	2		2	5	9	15	22

11.3	18.0
6.7	6.0
55	75

12.8	13.4	13.5	13.4
11.2	10.6	10.5	10.6
75	47	37	30

17.6	19.1	11.6	16.1	14.8	16.4	16.1	14.5	13.2	13.0
4.6	4.9	6.4	7.3	9.19	7.6	7.3	9.5	10.8	11.0
100	74	42	26	MH	10	2	16	33	38

19.9	81.3	81.9	83.0	84.0	12.5	13.1	13.2
4.1	2.64	2.1	1.0	0.0	11.5	10.9	10.8
116	117	142	165	183	75	63	47

80.2	19.3	19.0	17.6	16.4	16.6	16.8	17.3	14.6	13.6
3.8	4.7	5.0	6.4	7.6	7.4	7.2	6.7	9.4	10.4
75	63	42	21	10		10	14	21	36

11.8	11.9	12.6	11.9
12.2	12.1	11.4	12.1
75	66	59	40

Top Hyd 32' Lt Sta 12+94

Sta + π - Elev.

887.13

13+68

✓

14

+50

15

+50

July 9, 1965

5978

L1

2

R1

h

18.0	16.5	14.8	16.1	16.3	16.5	17.5	18.9	13.0
9.1	10.6	12.3	10.4	10.8	10.6	9.6	13.2	14.1
22	17	16	8	9	15	28	43	

18.8	81.9	85.3	85.1	85.2
8.3	5.2	1.8	20	1.9
37	45	54	69	75

12.5
14.6
57
Water

85.2	84.8	83.9	9.4	11.3	16.3	16.3	14.6	13.8	13.1	12.6
1.9	2.3	3.2	7.7	9.8	10.6	10.8	12.5	13.3	14.0	14.5
75	50	42	31	17	6	14	34	56	75	

84.6	84.6	19.3	11.2	16.1	16.4	14.5	13.9	13.4
2.5	2.5	7.8	9.9	10.4	11.7	12.6	13.2	13.7
75	49	30	9	12	35	59	75	

84.6	84.4	82.3	81.1	19.3	11.3	11.3	16.1	15.1	14.0	13.6
25	2.7	4.8	6.0	7.8	9.8	9.8	11.0	12.0	13.1	13.5
75	64	52	29	16	3	10	25	51	75	

85.3	84.3	81.5	80.3	19.9	19.6	20.8	19.4	15.4	14.4	13.5
1.8	2.0	5.6	6.8	7.2	7.5	6.3	7.7	11.7	12.7	13.6
75	52	46	29	11	6	13	30	55	75	

Sta	+	π	-	Elev
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		887.13		
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16

+50

+83	MH 921		7.54	79.59
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17

T.P.	8.94	888.55	7.52	879.61
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+50

18

+50

18+91 Begin New Sewer Const
Next Week

July 3, 1965

6079

LT

85.6	85.3	81.8	81.5	80.7	81.0	19.6	81.9	16.9	15.0	14.4
1.5	1.8	5.3	5.6	6.4	6.1	7.5	5.2	10.2	12.1	12.7
75	54	43	36	15	8	20	41	64	75	

BT

85.6	85.3	81.8	81.5	81.4	81.8	83.5	80.2	19.0	18.4	17.0
1.5	1.8	5.3	5.6	5.7	5.3	3.6	6.9	8.1	8.7	10.1
75	58	38	24	5	0	21	30	49	75	

85.1	85.2	85.0	81.1	80.3	80.1	80.6	81.0	18.0	18.0	16.2
1.4	1.9	2.1	6.0	6.8	7.0	6.5	4.1	9.1	9.1	10.9
75	55	44	29	18	12	20	28	45	75	

86.5	85.1	82.3	81.5	80.3	80.0	80.0	18.8	17.2	17.0	16.9
2.1	3.5	6.3	7.1	8.3	8.6	8.6	9.8	11.4	11.6	11.7
75	50	40	34	17	7	12	26	48	75	

87.0	85.6	81.2	80.5	80.3	81.1	18.2	16.8	16.1	16.1	16.1
1.6	3.0	7.4	8.1	8.3	7.5	10.4	11.8	11.9	12.2	
75	55	46	13	13	22	38	51	75		

87.6	86.9	81.4	80.5	80.5	80.4	80.4	81.2	19.7	17.5	16.3	15.8
1.0	1.7	7.2	8.1	8.1	8.2	8.2	7.4	8.9	11.1	12.3	12.8
75	49	44	31	14	9	11	27	47	61	75	

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		888.55		
--	--	--------	--	--

19+00				
-------	--	--	--	--

✓				
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B.M.				
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	10.89	877.66		877.66
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July 13, 1965 61⁸⁰

Lt.

Rt

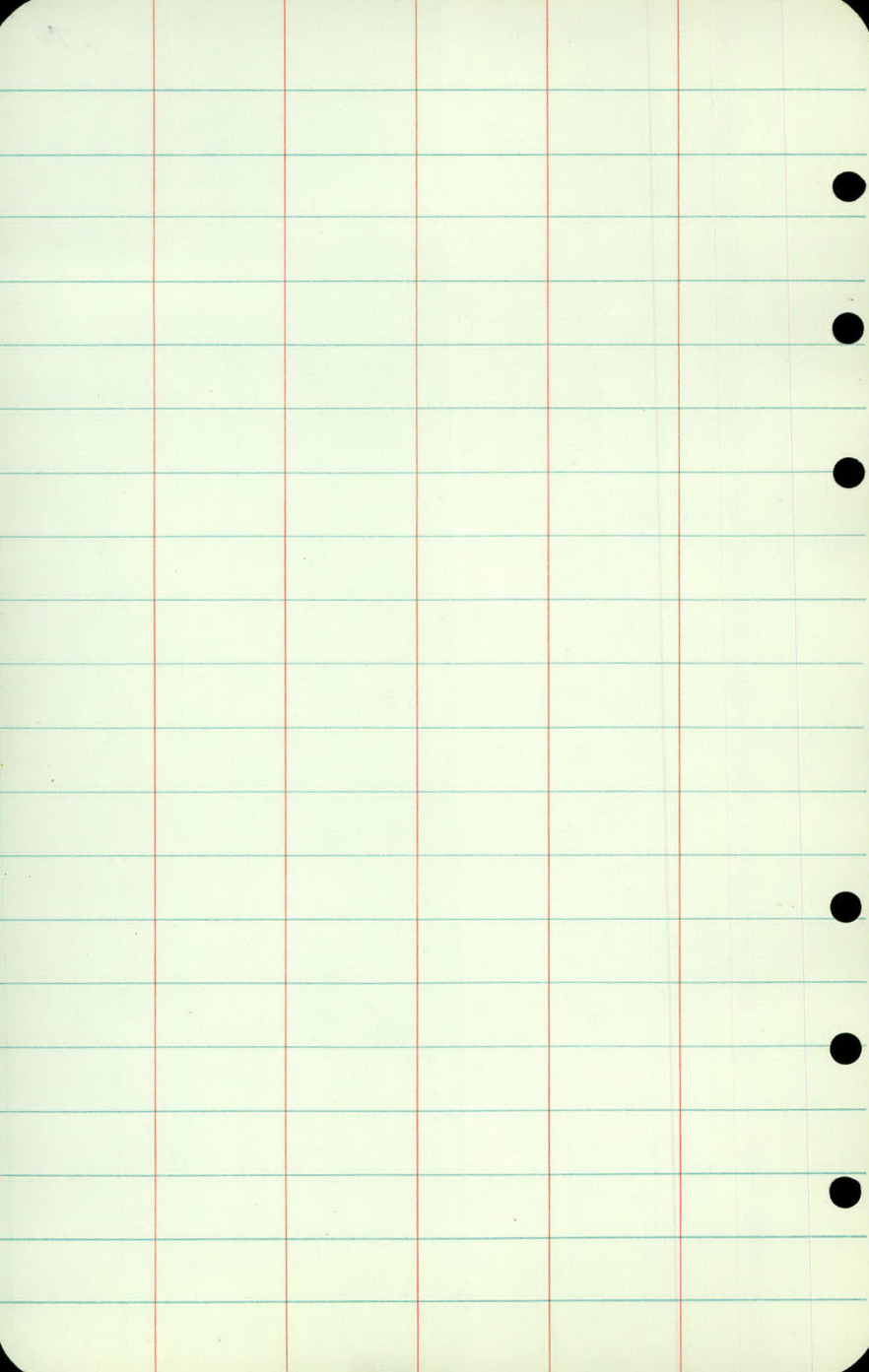
J

26.9	26.4	21.0	19.9	19.5	19.4	19.8	19.0	15.5	14.8	14.0
1.7	2.2	7.6	8.7	9.1	9.2	8.8	9.6	13.1	13.8	14.6
68	50	44	33	16		5	16	31	54	75

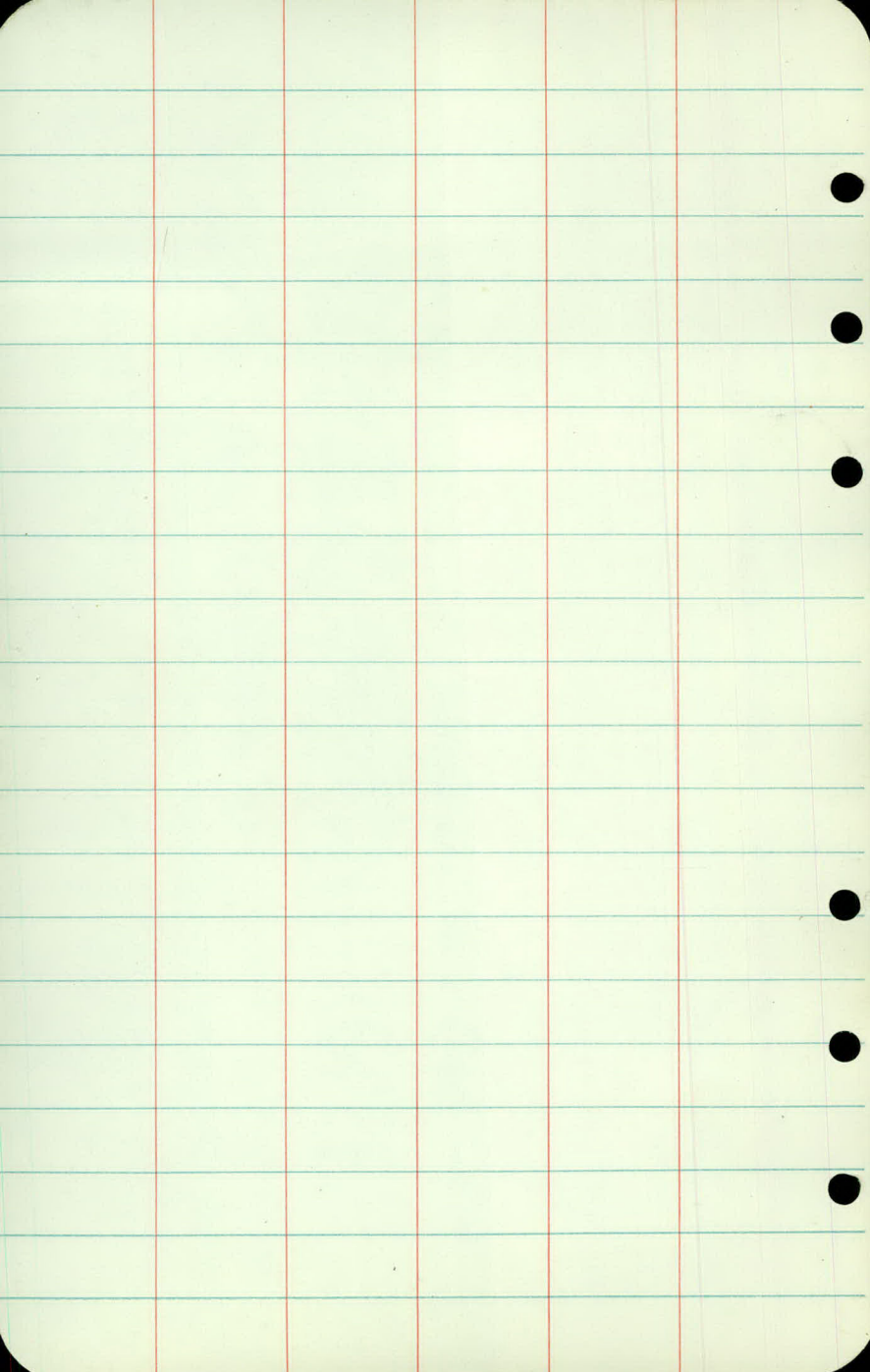
87.3

1.3
75

Top Hyd 32' Lt Sta 12+94



81
~~52~~



August 6, 1963

82

8:30 - 10: AM

Co Rd H Long Lake Rd to East
No Alinement Left
Recently Regraded
Lip of MH Casting Broken off
by Last House on N. Side

Laying pipe Their Stationing
187+81 - 187+31 on fine Sand
area with 1 ft. Gravel for Base

188+31 Begin area where there
was a clay base reported by Engr.
company inspector

N. Pipe Line = 1' N. of Section Line

187+00 3' Peat

186+90 Begin Peat Rt only

In P.M. they were installing Gate Valve

$$21 + 63.6 = \text{Their}$$

$$192 + 03$$

$$\begin{array}{r} 120.3 \\ 16.1 \\ \hline 136.4 \end{array}$$

P.I. S. Line
@ 16'

120.3

P.I. N. Line @ 43'

station 22

$$\begin{array}{r} 23 \\ 136.4 \\ \hline 21 + 63.6 \end{array}$$

station 23

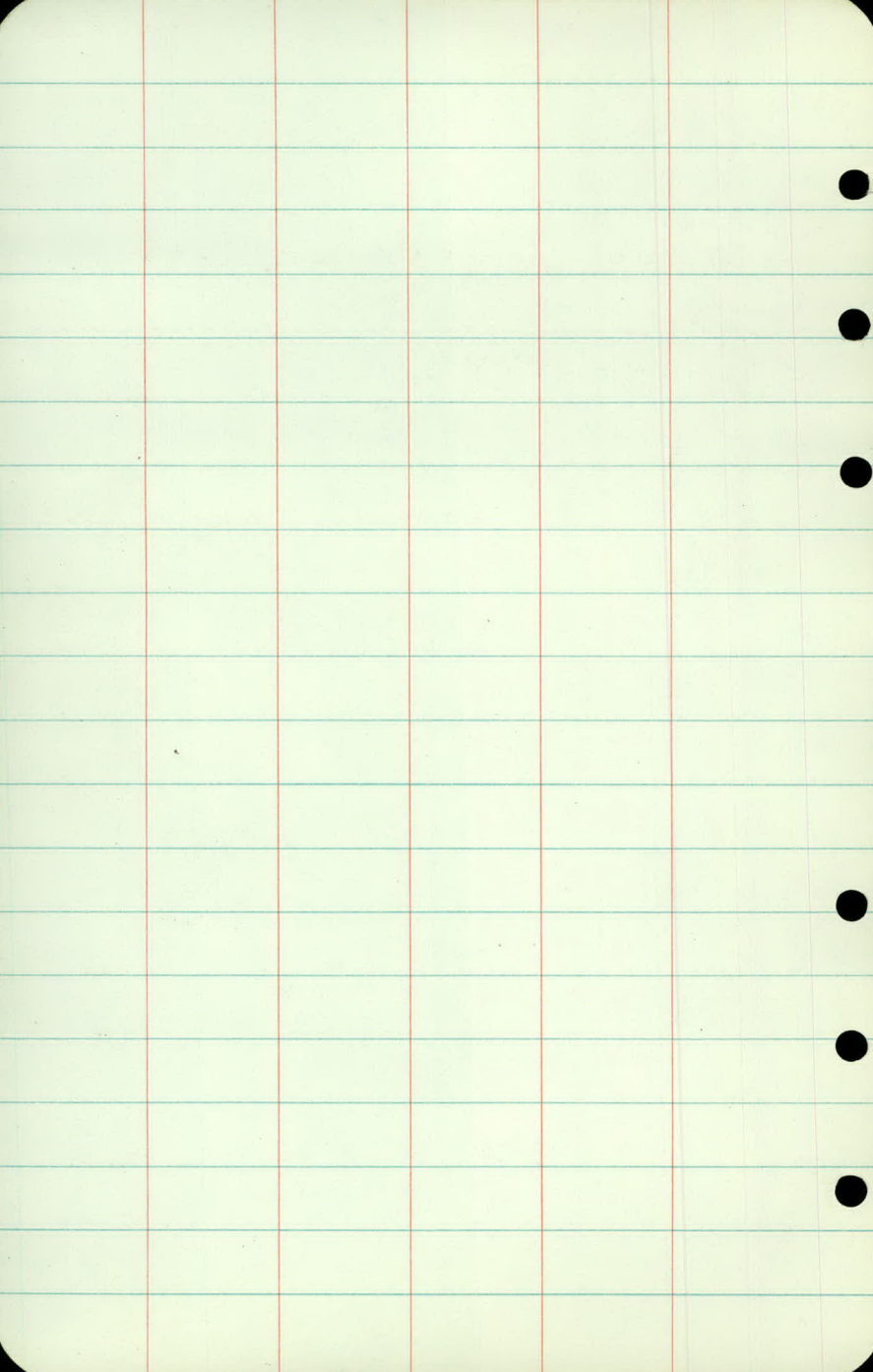
August 9, 1963

83

Checking Right Side there
is a layer of Peat $2\frac{1}{2}$ to 3'
Deep from said beginning to
100' East of Beginning of Woods
Rt. Side. One 5' Deep spot
at this east end.

North Side is all in Sewer Exc.

Their stationing 186 + 60 End Peat Rt.
at " " 185 + 50 to ↑ Peat 2' to 3'



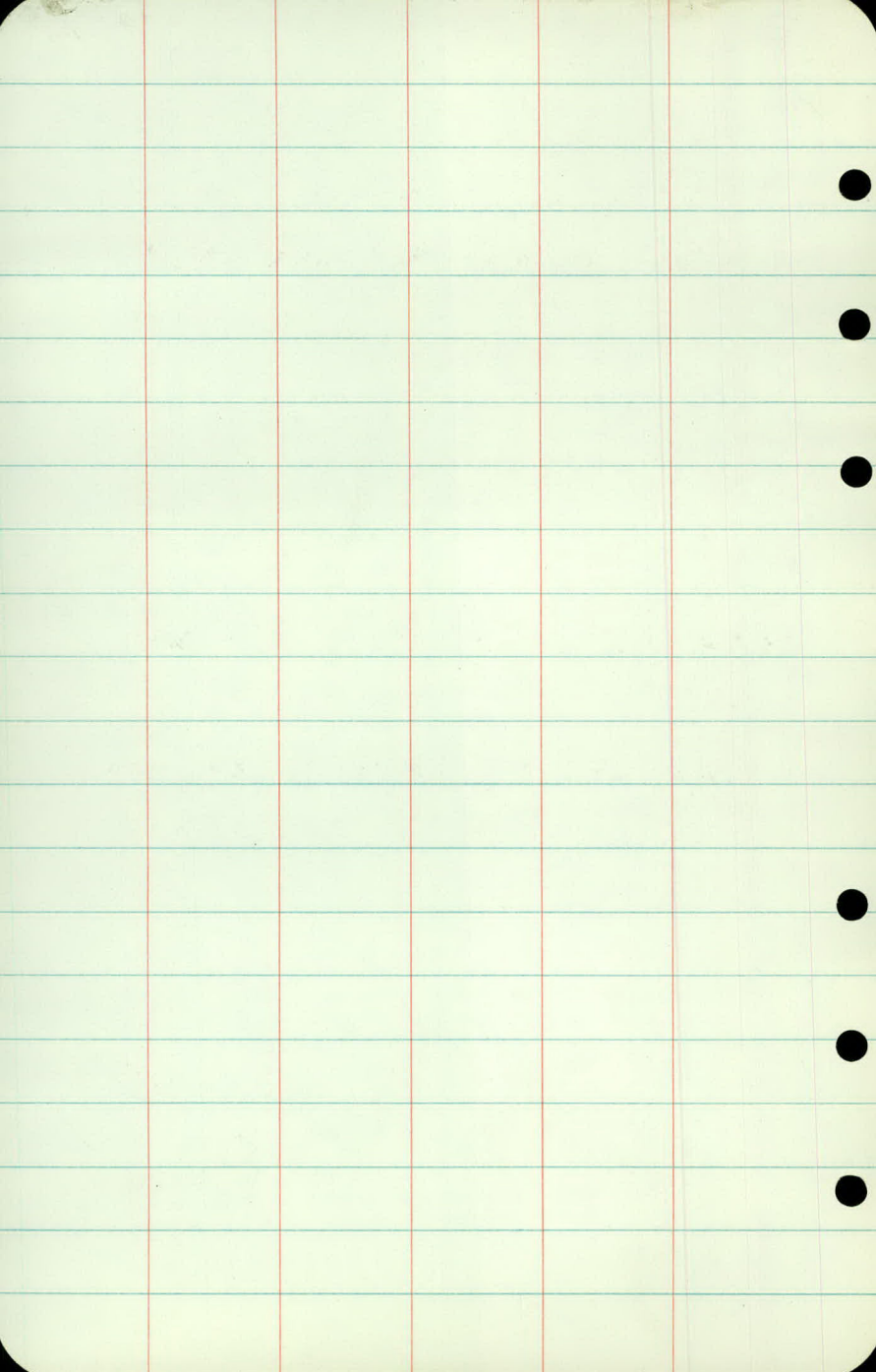
August 10

84

185+50 Peat 2.0' Thick

185+86 to 185+56 Silt 2'
above Bottom of Pipe to
about 1' Below Pipe

185+00 Trace of Peat or Topsoil
to 184+00 " " " " "



August 11, 1965⁸⁵

181+60 Peat 4' Thick

For some reason the
small drag-line had dug a
hole

Sta 10+11.2 = Their 180+50

Sta 184+00 Peat 1.5' Thick

184+35 Peat 2.5' Thick

Laying pipe 184+30 to 184+00

August 12., 1965

Digging around Storm Sewer
1 to 1 1/2' Black Topsoil
Down 3 feet
Sand below

August 13, 1965

182+75	2' Peat Down 2-4'
182+50	Peat to 5' Down
182+00	Peat 8' Deep

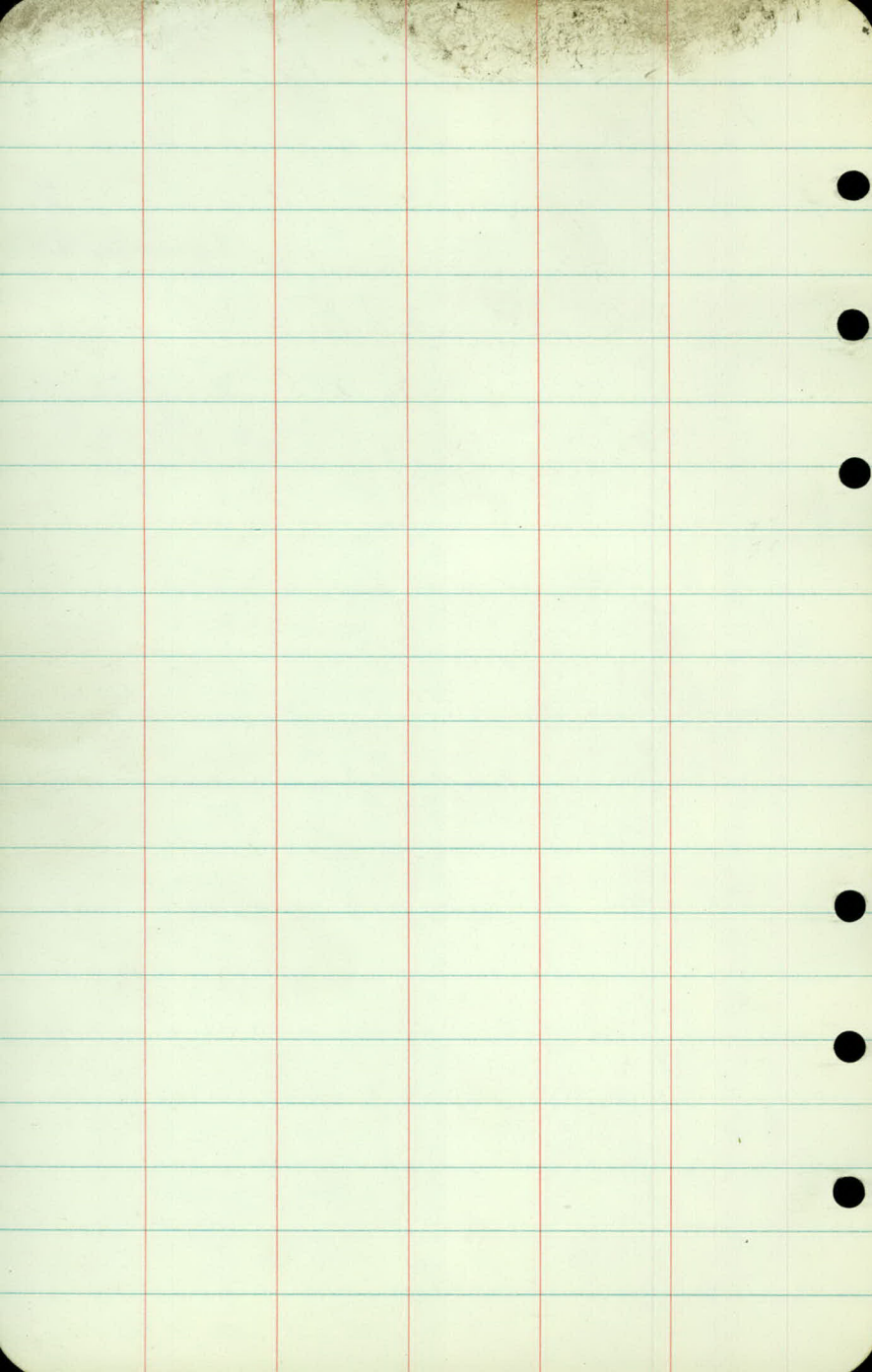
August 16, 1965

86

Laying Pipe 181+50

End Peat 181+50

Peat to 3' Below pipe
at one point



FK
LPD
JG

9-7-65

87

a

Co Rd H

X-sections

for

Channel Change

Sta + π - Elev.

BM 4.39 879.34

874.95

28+00

✓

+50

✓

29+00

✓

TP

4.13

877.89

558

873.76

873.76

2

9-7-65

88
b

S. Rim MH Sta 27+25

71.5	70.5	70.0	70.0	70.3	70.6	71.4	71.1
78	8.8	8.9	8.9	9.0	8.7	7.9	8.2
	9	20	39	59	82	100	114

71.9	71.7	71.8	71.5	70.9
74	7.6	7.5	7.8	8.4
200	179	167	153	134

72.2	71.0	70.6	70.5	70.4	71.0	71.3	71.6
7.1	8.3	8.7	8.8	8.9	8.3	8.0	7.7
	14	28	44	66	77	95	114

68.9	69.5	70.3	71.6	72.1
10.4	9.8	9.0	7.7	7.2
200	193	174	155	136

72.4	71.7	72.6	70.8	71.7	71.6	69.0 72.8
6.9	7.6	6.7	8.5	7.6	7.7	10.3
	10	23	36	53	70	76

70.48
WS
8.86

71.2	71.3	71.1	69.6	68.8 61.8
8.1	8.0	8.2	9.7	10.5
200	176	134	126	96

S. Rim MH Lt. Sta

£
Creek

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		877.89		
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29+42				
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TP	10.14	883.90	4.13	873.76
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+42				
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+70				
-----	--	--	--	--

✓				
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30+00				
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✓				
---	--	--	--	--

FK
LPD
RP
JG

2

9-8-65

BT

89
C

71.7	71.4	67.7	68.6	71.2	72.3	70.6
6.2	6.5	10.2	9.3	6.7	5.6	7.3
7	19	30	49	73	99	

71.7	71.7	73.1	71.9	71.8
12.2	12.2	10.8	12.0	12.1
138	150	165	178	200

76.4	76.1	69.7	67.4	70.2	71.7	72.0
7.5	7.8	14.2	16.5	13.7	12.2	11.9
7	15	22	30	34	60	

69.5	69.3	68.5	67.3	71.5	72.1	71.7	71.7
14.4	14.6	15.4	16.6	12.4	11.8	12.2	12.2
200	177	146	135	131	117	96	79

73.0	71.5	68.1	70.2	71.9	71.9	71.6
10.9	12.4	15.8	13.7	12.0	12.0	12.3
13	17	29	32	57	81	

71.4	71.0	71.9	70.6	67.2	72.1
12.5	12.9	12.0	13.3	16.7	11.8
200	173	148	145	114	108

Sta + π - Elev.

883.90

30+50

✓

TP 6.07 878.60 11.37 872.53 (872.51)

+73

✓

+78

✓

TP 6.77 879.30 6.07 872.53 (872.51)

9-8-65

90

2

R1

69.6	70.2	68.3	72.0	69.1	69.3	70.3
14.3	13.7	15.6	11.9	14.2	14.6	13.6
15	23	36	60	86	109	

72.9	72.3	72.7	72.0
11.0	11.6	11.2	11.9
200	173	149	128

Rock

71.3	71.9	71.8	69.3	69.1	72.0	71.9	72.2	73.5
7.3	6.7	6.8	9.3	9.5	6.6	6.7	6.4	5.1
15	29	34	53	71	85	99	112	

72.1	72.2	72.3	72.3
6.5	6.4	6.3	6.3
200	179	156	126

71.4	71.7	72.1	72.9	71.6	72.3	71.6	72.0	68.9
7.2	6.9	6.5	5.7	7.0	6.3	7.0	6.6	9.7
7	21	38	44	64	79	96	113	

69.3	69.6	69.6
9.3	9.0	9.0
200	150	132

ROCK

STA + π - ELEV

TP 879.30 6.27

31.00

✓

+25

✓

B.M. 5.26 5.50 873.80 (872.76)

B.M. 5.36 877.87 872.51

+50

✓

FK
LPD
RP
JG

E

8-SEP-65 91
Sept. 9, 1965
RT E

11.1	11.2	13.0	12.6	12.5	65.6	65.8	66.8
8.2	8.1	63	6.7	6.8	13.7	13.5	12.5
7	10	37	52	72	75	80	

11.1	10.6	11.3	10.3	69.9
8.2	8.7	8.0	9.0	9.4
200	180	164	136	108

11.4	12.2	11.1	69.0	67.3	68.3	70.8	72.3
7.9	7.1	8.2	10.3	12.0	11.0	8.5	7.0
18	29	33	38	48	68	74	

12.2	11.1	12.2	11.8	11.2	12.1
7.1	8.2	7.1	7.5	8.1	7.2
200	179	160	136	118	92

5 R in MH/Lt. Sta 29+30

11.7	12.6	67.7	68.0	11.0	12.9	11.6	11.7	12.1
6.2	5.3	10.2	9.9	6.9	5.0	6.3	6.2	5.8
12	22	31	48	57	82	104	124	

12.0	11.4	11.7	12.0
59	6.5	6.2	5.9
200	189	170	147

Sta + π - Elev.

872.87

32+00

✓

+25

✓

+50

✓

✓

TP

3.16

877.76

3.27

874.60

2

9-9-65

92

RT

f

✓ 72.0	71.1	70.1	67.5	70.8	72.7	71.8	71.4
5.9	6.8	7.8	10.4	7.1	5.2	6.1	6.5
	4	9	23	39	54	76	100

	77.6	76.6	72.9	71.7
+30.0	0.3	1.3	5.0	6.2
←	141	139	134	121

✓ 71.4	70.8	70.9	69.4	68.0	69.4	72.4	71.7
6.5	7.1	7.0	8.5	9.9	8.5	5.5	6.2
	13	34	44	57	69	74	98

77.6	76.4	74.0	72.3	71.3
0.3	1.5	3.9	5.6	6.6
136	133	128	120	107

✓ 71.3	73.1	70.9	72.8	71.3	70.1	70.6	71.1
6.6	4.8	7.0	5.1	6.6	7.8	7.3	6.8
	9	17	24	27	40	55	63

72.4	68.1	68.1	68.6	70.6	71.3	70.7	70.6
5.5	9.8	9.8	9.3	7.3	6.6	7.2	7.3
129	126	120	114	105	95	87	77

75.5	77.9
2.4	0.0
135	138

Sta + π - Elev.

877.76

33

✓

+50

✓

T.P. 3.47 878.06 3.17 874.59

34

✓

Sept. 9, 1965

93

2

8+

9

✓ 13.0 13.0 12.3 12.3 12.8 12.7 11.8 9.4 6.6
4.8 4.8 5.5 5.5 5.0 5.1 6.0 8.4 10.8
17 40 62 85 100 111 117 125

11.8 14.5 11.2 10.0 11.1 11.2 10.3
0.0 3.3 6.6 7.8 6.7 6.6 7.5
200 193 190 178 164 133 131

✓ 12.6 12.4 12.7 12.7 12.8 10.6 10.8 12.3 12.4
5.2 5.4 5.1 5.1 5.0 7.2 7.0 5.5 5.4
17 30 51 61 71 84 92 116

15.9 13.0 11.9 11.7 12.2
S.S. 1.9 4.8 5.9 7.6 6.1 5.6
204 200 199 174 149 140

✓ 12.2 12.9 12.3 10.3 12.2 12.2 10.6 12.6 12.4
5.9 5.2 5.8 7.8 5.9 5.9 7.5 5.5 5.7
14 29 35 50 73 91 99 123

15.1 12.5 10.7 11.1
S.S. 3.0 5.6 7.4 7.0
200 191 167 147
creek

Sta + π - Elev.

878.06

34+50

✓

35

✓

+50

✓

BM 2.99 879.65 1.40 876.66

Sept. 9, 1965

94

RT

✓ 71.8	72.1	70.5	70.9	72.9	72.2	71.7	72.0
6.3	6.0	7.6	7.2	5.2	5.9	6.4	6.1
	11	21	35	37	56	80	102

72.00	71.0	74.2	71.8	70.9	72.1	71.1	70.4
6.07	1.1	3.9	6.3	2.2	6.0	7.0	7.7
W.S. 200	191	189	163	139	127	112	

✓ 71.6	71.5	70.3	72.1	71.3	72.4	73.3	72.8	71.0
6.5	6.6	7.8	6.0	6.8	5.7	4.8	5.3	7.1
	12	22	34	48	61	81	94	128

74.0	72.7	71.6
4.1	5.4	6.5
200	186	158

✓ 68.3	66.9	67.6	71.7	73.3	73.2	72.7
9.8	11.2	10.5	6.4	4.8	4.9	5.4
	4	17	32	35	58	75

71.7	71.7	73.2	72.5	71.2
6.4	6.4	4.9	5.6	6.9
200	170	128	110	92

S. Rim M.H.

Sta + π - Elev.

879.65

36

✓

+ 50

✓

TBM 5.40 882.06 2.99 876.66

37

37

✓

Sept. 9, 1965

95

BT

10.9	12.2	12.7	12.2	9.4	12.3	10.3	12.9
8.8	7.5	7.0	7.5	10.3	7.4	9.4	6.8
10	23	52	80	105	109	114	

12.4	13.3	12.8	11.3	12.0
7.30	6.4	6.9	8.4	7.7
W.S.	200	188	159	134

12.5	13.0	12.4	11.6	12.9	13.6	12.1	9.0	8.7
7.2	6.7	7.3	8.1	6.8	6.1	7.6	10.7	11.0
21	45	68	74	83	85	97	106	

10.1	10.5	10.7	11.3	12.9	12.2	9.8
9.6	9.2	9.0	8.4	6.8	7.5	10.9
200	186	165	150	125	122	111

Rim MH

14.3	14.2	12.4	13.0	13.4	13.2	13.0	12.4
7.8	7.9	9.7	9.1	8.7	8.9	9.1	9.7
6	11	35	60	73	90	107	

97.2
W.S.

12.5	12.7	13.4	12.9	12.1	9.5	8.9
9.6	9.4	8.7	9.2	10.0	12.6	13.2
200	193	180	170	157	145	129

Sta + π - Elev

882.06

37+50

✓

BM

3.19 878.87 878.85

Sept. 9, 1965

96

~~2~~

St.

~~1~~

✓ 13.2	12.8	12.5	12.4	12.1	13.4	12.9	12.8
8.9	9.3	9.6	9.7	9.4	8.7	9.2	9.3
19		44	57	86	100	116	148

11.1	8.3	9.4	12.4
✓ 10.4	13.8	12.7	9.72
200	185	169	WS
New Channel			155

Top W. Cor. Headwall Rice Creek Box Culvert

Sta	+	π	-	Elev.
-----	---	-------	---	-------

BM	2.98	911.03		908.05
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0+00

+22

+33

+50

1

T.P.	4.37	910.46	4.94	906.09
------	------	--------	------	--------

+50

FX
LPO
BP
50

Lt.

Sept. 10, 1965 97
Rt. 10

Top Hyd N.E. Cor Long Lake Rd + H

04.5	04.7	05.0	05.4	05.2	05.6	05.7	05.5	05.6
6.5	6.3	6.0	5.6	5.8	5.4	5.3	5.46	5.4
50	80	50	28	18		14	MH	24
1007							17	

05.5	05.3	05.5	05.6	05.2
5.5	5.7	5.5	5.4	5.8
24	17		12	30

05.5	05.6	05.3	05.6	05.5	05.6	05.9
5.5	5.4	5.7	5.4	5.5	5.4	5.1
23	19	8		9	19	22

05.6	05.8	05.4	05.5	05.7	06.1	06.7
5.4	5.2	5.6	5.5	5.3	4.9	4.3
25	19	8		9	16	19

06.3	06.2	05.8	05.9	06.2	06.3	06.9
4.7	4.8	5.2	5.1	4.8	4.7	4.1
24	20	10		7	15	20

S.W. Cor. Conc Ent Lt.

06.1	06.1	06.0	05.9	06.2	06.2	06.2
4.36	4.4	4.5	4.6	4.3	4.3	4.3
Conc	22	12		7	15	21
23						

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		910.46		
--	--	--------	--	--

2				
---	--	--	--	--

	+50			
--	-----	--	--	--

3				
---	--	--	--	--

	+50			
--	-----	--	--	--

4				
---	--	--	--	--

✓				
---	--	--	--	--

Sept. 10, 1965

98

Lt

Lt

Rt

05.6	05.5	05.7	06.0	05.9	06.0	06.3
4.9	5.0	4.8	4.5	4.6	4.5	4.2
25	20	9		7	14	19

05.6	05.4	05.6	05.7	05.8	05.6	06.0
5.0	5.1	4.9	4.8	4.7	4.9	4.5
27	21	12		10	16	23

05.2	05.4	05.8	05.6	05.4	05.5	05.8
5.3	5.1	4.7	4.9	5.1	5.0	4.7
27	23	14		8	19	26

05.3	05.4	05.7	05.8	05.6	05.3	05.5
5.2	5.1	4.8	4.7	4.9	5.2	5.0
28	25	15		9	17	23

05.5	05.7	05.8	05.6	05.6	05.6
5.0	4.8	4.7	4.9	4.9	4.9
25	23	10		10	16

05.9	05.7	06.1	06.0	05.9	05.9
4.6	4.8	4.4	4.5	4.6	4.6
25	20	11		8	11

Sta	+	π	-	Elev
-----	---	-------	---	------

		910.46		
--	--	--------	--	--

5

T.P.	6.42	912.54	434	906.12
------	------	--------	-----	--------

+50

6

+33

+45 Gutter Rt

+60

14

Sept. 10, 1965

99

Rt

an

06.4	06.2	06.9	06.4	06.2	06.7
4.1	4.3	4.1	4.1	4.3	3.8
32	27	16		8	12

07.1	06.7	06.7	06.4	06.9	06.6
5.4	5.8	5.8	4.1	6.1	5.9
29	24	14		8	11

07.2	07.0	06.9	06.5	06.8	07.2
5.3	5.5	5.6	6.0	5.7	5.3
29	26	15		7	10

07.4	07.0	06.8	07.0	07.4	08.1	08.7	08.8
5.1	5.5	5.7	5.5	5.1	4.4	3.8	3.7
50	33	23		10	18	37	50

07.1	07.0	06.8	07.1	07.3	07.4	07.8
5.4	5.5	5.7	5.4	5.2	5.1	4.7
50	37	22		10	15	36

06.8	06.7	06.9	07.4	07.6	07.7	07.8
5.7	5.8	5.6	5.1	4.9	4.82	4.7
50	37	17		8	MH	17
					11	

Sta + π - Elev.

912.54

6+70 Gutter Line Rt.

+75

7

+50

BM 3.13 912.54 3.13 909.39⁴¹ (909.46)

TP 4.04 909.65 6.98 905.61

8

8.55

901.10

+27

Sept. 10, 1965 100

Lt

Lt

Rt n

06.9	07.0	06.6	07.2	07.4	07.6	07.9	08.1	08.3	08.4
56	55	59	53	51	49	46	44	42	41
50	42	26	14		6	19	27	43	50

07.1	07.3	06.7	07.2	07.4	07.5	07.7	08.3
54	52	58	53	51	50	48	42
50	45	29	15		7	14	17

07.6	07.1	06.9	06.9	06.8	07.0	07.6	07.2
49	54	56	56	57	55	49	33
38	34	26	13		9	13	15

07.9	07.9	07.0	06.7	06.1	06.2	06.3	07.2
46	46	55	58	64	63	62	33
40	38	22	11		8	13	20

Top Hyd N.W. Cor. Irondale Rd & "H"

07.2	06.4	05.7	05.7	05.3	08.5
25	33	40	40	44	12
35	25	8		13	19

05.3	05.0	05.0	04.6	04.4	04.5	07.3
44	47	47	51	53	52	24
34	29	15		11	19	21

Sta + π - Elev.

909.65

8+35

+69

BM 0.69 901.79 8.55 901.10 (901.10)

9

+01

+23

+36

11

Sept. 10, 1965

101

51

0

04.2	04.4	04.4	04.2	04.0	04.1	04.6
5.5	5.3	5.3	5.5	5.7	5.6	3.2
36	31	16		11	18	22

04.0	02.8	02.2	01.7	01.2	01.5	03.6
5.7	6.9	2.5	8.0	8.5	8.2	6.1
35	29	16		10	19	27

Top N.E. Cor. Bottom Step to garage

01.2	00.2	00.0	99.5	99.4	00.0	01.2	01.8
0.6	1.6	1.8	2.3	2.4	1.8	0.6	0.0
33	24	14		9	16	19	21

00.5	00.4	00.1	99.9	99.4	99.4	99.9	01.2	01.8
1.3	1.4	1.7	1.9	2.4	2.4	1.9	0.6	0.0
50	35	24	14		9	16	19	21

00.1	98.8	98.9	98.2	97.8	97.7	98.0	99.4
1.7	3.0	2.9	3.6	4.0	4.1	3.8	2.4
50	34	19	12		12	15	20

97.5	97.2	97.5	97.2	96.8	96.6	96.8	96.3
4.3	4.6	4.3	4.6	5.0	5.2	5.0	3.5
50	40	18	12		10	14	21

Sta	+	π	-	Elev
-----	---	-------	---	------

		901.79		
--	--	--------	--	--

9+47				
------	--	--	--	--

BM				
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	7.02	894.77		
--	------	--------	--	--

+65				
-----	--	--	--	--

+85				
-----	--	--	--	--

10				
----	--	--	--	--

+05				
-----	--	--	--	--

TP	0.82	891.03	11.58	890.21
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+21				
-----	--	--	--	--

Lt.

Sept. 10, 1965 102

Rt.

p

95.3	96.4	96.0	95.8	95.8	96.3	97.1
6.5	5.4	5.8	6.0	6.0	5.5	4.1
50	41	18		10	16	21

Top Hyd Lt Sta 9+50±

93.2	93.0	92.9	94.0	94.2	94.0	94.4	95.8
8.6	8.8	8.9	7.8	7.6	7.8	7.4	6.0
50	39	21	9		9	15	20

91.8	91.9	91.8	91.5	92.6	92.0	92.2	92.4	93.5
10.0	9.9	10.0	10.3	9.2	9.8	9.6	9.4	8.3
50	41	28	15	10		8	11	16

91.0	90.8	90.9	90.2	90.2	90.5	90.8	92.8
10.8	11.0	11.4	11.6	11.6	11.3	11.0	9.0
50	44	26	11		7	10	16

90.5	89.8	91.5	90.0	89.7	89.3	90.1	92.0	92.6
11.3	12.0	10.25	11.8	12.1	12.3	11.7	9.8	9.2
50	37	26	24	10		10	13	17

89.6	88.9	88.6	87.9	88.0	88.2	88.3	90.6
1.5	2.1	2.4	3.1	3.9	2.8	2.7	0.4
50	40	25	15		7	10	14

Sta + π - Elev.

891.03

10+57

11

+50

BM 9.95 891.00 9.95 881.08 881.05

TP 3.48 880.68 13.80 877.20

12

+26

+44

Sept. 10, 1965

103

11

2

RT

8

86.8	86.3	85.9	86.0	85.2	85.2	85.1	85.3	87.6
4.2	4.7	5.1	5.0	5.8	5.8	5.9	5.7	3.4
50	38	29	20	11	7	11	16	

84.3	83.5	83.4	82.5	82.6	82.5	82.8	84.2
6.7	7.5	7.6	8.5	8.4	8.5	8.2	6.8
50	35	23	11	9	13	20	

79.0	78.6	81.4	80.2	80.0	80.1	79.7	79.6	79.6
12.0	12.4	9.6	10.8	11.0	10.9	11.3	11.4	11.4
35	22	15	12	5	17	22	24	

77.7	77.5	78.0	77.5	77.2	76.8	76.4	74.6
3.0	3.2	2.7	3.2	3.5	3.9	4.1	6.1
50	34	18	11	11	18	23	

78.0	77.8	78.0	76.7	76.4	76.3	75.6	74.5
2.7	2.9	2.7	4.0	4.3	4.4	5.1	6.2
50	31	17	11	8	18	25	

76.9	76.3	76.5	76.1	76.0	75.8	74.4
3.8	4.4	4.2	4.6	4.7	4.9	6.3
50	28	10	10	18	25	

Sta + π - Elev.

880.68

12+60

+81

BM

3.05 877.63

13

+14

+41

TP 10.25 885.65 5.28 875.40

+68

Sept. 10, 1965

104

Lt.

E

Rt.

n

16.8	16.3	16.0	16.2	15.9	15.5	15.4	13.9
3.9	4.4	4.7	4.5	4.8	5.2	5.3	6.8
50	40	26	12		8	19	26

16.5	15.8	16.0	15.7	15.6	15.5	15.4	14.3
4.2	4.9	4.7	5.0	5.1	5.2	5.3	6.4
50	31	18	11		12	20	27

Top Hyd Lt Sta 12+95

16.7	16.3	15.9	15.7	15.3	15.2	15.5	16.6	14.6
4.0	4.4	4.8	5.0	5.4	5.5	5.2	4.1	6.1
50	39	20	7		10	19	25	28

16.6	14.73	14.6	14.4	15.7	14.3
4.1	5.95	5.1	5.3	5.0	6.4
17	MH	7		18	28
	9				

18.4	17.4	17.2	16.8	15.2	15.6	16.3	15.4
2.3	3.3	3.5	3.9	5.5	5.1	4.4	5.3
50	31	26	12		14	21	27

13.3	10.1	18.5	16.5	16.0	15.6	15.3	14.3
2.4	5.6	7.2	9.2	9.7	10.2	10.4	11.4
50	35	28	14		11	17	30

Sta + π - Elev.

885.65

14

+50

15

+50

16

+06 MH 6' Lt No Casting 8.56 sewer force Main Gate Valve

+50

+66 MH $\neq$ No Casting 8.40

Sept. 10, 1965

105

$\frac{1}{t}$ $\frac{1}{t}$ $\frac{1}{t}$ $\frac{1}{t}$ $\frac{1}{t}$ $\frac{1}{t}$ $\frac{1}{t}$ $\frac{1}{t}$
 $\frac{82.6}{3.1}$ $\frac{79.4}{6.3}$ $\frac{76.9}{8.8}$ $\frac{76.1}{9.6}$ $\frac{75.5}{10.2}$ $\frac{75.0}{10.7}$ $\frac{74.3}{11.4}$ $\frac{73.9}{11.8}$
 45 29 15 8 10 22 36

$\frac{83.2}{2.5}$ $\frac{82.2}{3.5}$ $\frac{81.3}{4.4}$ $\frac{80.6}{5.1}$ $\frac{79.8}{5.9}$ $\frac{78.1}{7.6}$ $\frac{76.4}{9.3}$ $\frac{76.2}{9.5}$ $\frac{76.3}{9.4}$ $\frac{75.8}{9.9}$ $\frac{75.0}{10.7}$
 50 46 44 33 30 15 5 14 20 33

$\frac{82.4}{3.3}$ $\frac{80.1}{5.6}$ $\frac{78.3}{7.4}$ $\frac{76.6}{9.1}$ $\frac{76.1}{9.6}$ $\frac{76.9}{8.8}$ $\frac{77.1}{8.6}$ $\frac{74.9}{10.8}$
 50 27 11 9 15 18 38

$\frac{82.7}{30}$ $\frac{82.4}{45}$ $\frac{81.2}{26}$ $\frac{79.1}{10}$ $\frac{77.8}{7.9}$ $\frac{76.8}{8.9}$ $\frac{77.2}{8.5}$ $\frac{79.0}{6.7}$ $\frac{78.8}{6.9}$ $\frac{75.3}{10.4}$
 50 45 26 10 2 14 17 22 33

$\frac{83.8}{1.9}$ $\frac{82.4}{3.3}$ $\frac{80.9}{4.8}$ $\frac{79.6}{6.1}$ $\frac{78.9}{6.8}$ $\frac{77.5}{8.2}$ $\frac{77.8}{7.9}$ $\frac{80.1}{5.6}$ $\frac{78.9}{6.8}$ $\frac{77.2}{8.5}$
 50 32 18 9 4 14 21 31 39

$\frac{84.7}{1.0}$ $\frac{83.2}{2.5}$ $\frac{83.2}{2.5}$ $\frac{80.9}{4.8}$ $\frac{78.3}{7.4}$ $\frac{77.3}{8.4}$ $\frac{77.2}{8.5}$ $\frac{78.8}{6.9}$ $\frac{79.0}{6.7}$
 50 31 19 8 4 15 18 36

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		885.65		
--	--	--------	--	--

17+00

TP	9.32	887.44	7.53	878.12
----	------	--------	------	--------

+50

18

+50

19

+50

Sept. 10, 1965

106

Lt.

E

Rt. t

8 ^{4.4}	8 ^{4.1}	8 ^{2.6}	8 ^{1.3}	8 ^{0.2}	18 ⁰	18 ¹	17 ⁰	17 ⁹	19 ⁰	19 ⁰	18 ⁵
1.3	1.6	3.1	4.4	5.5	7.7	7.6	8.7	7.8	6.7	6.7	7.2
50	44	29	19	6	4	6	15	19	23	27	

State 17:00 E

8 ^{2.2}	8 ^{3.9}	8 ^{1.6}	8 ^{2.1}	8 ^{0.4}	18 ¹	18 ²	17 ³	17 ³	18 ²	
3.2	5.1	3.5	3.8	5.3	7.0	8.7	9.2	10.1	10.1	9.2
50	31	28	21	15	6	3	5	10	18	28

8 ^{4.0}	8 ^{2.2}	18 ¹	17 ⁵	17 ⁰	17 ²	19 ¹	17 ⁹
3.4	5.2	8.7	9.9	10.4	10.2	8.3	9.5
50	36	8	4		14	16	30

8 ^{3.7}	8 ^{1.6}	19 ⁴	17 ⁸	16 ⁰	16 ⁴	15 ³	16 ⁵	8 ³	8 ⁹	18 ⁸
3.7	5.8	8.0	9.6	11.4	12.0	12.1	10.9	7.1	6.5	8.6
50	40	22	8	5		7	14	19	31	35

8 ^{1.2}	8 ⁹	18 ³	18 ¹	16 ⁵	16 ⁴	14 ⁹	16 ⁰	18 ²	17 ⁹	15 ¹
6.2	8.5	9.1	9.3	11.9	12.0	12.5	11.4	9.2	9.5	11.7
50	33	26	17	7		7	13	16	26	33

18 ¹	17 ⁴	17 ³	16 ⁹	15 ⁶	15 ²	14 ⁹	16 ¹	17 ⁰	17 ¹	
8.7	10.0	10.1	10.5	11.8	12.2	12.5	11.3	10.4	9.7	10.6
50	30	22	11	5		5	13	17	25	30

Sta + π - Elev.

887.44

20

TP 1.82 879.65 9.61 877.83

+50

21

+50

22

BM

5.17 874.48 874.45

FX
RP
RW

Lt

Sept. 10, 1965
Sept. 13, 1965

107

RT M

17.2

17.2

17.2

16.2

15.8

15.4

15.6

16.8

16.1

15.1

10.2

10.2

10.2

11.2

11.6

12.0

11.8

10.6

11.3

11.7

50

30

21

8

6

16

19

24

28

Top E. Rim MH Lt

16.1

15.1

16.0

16.0

15.2

15.2

14.9

14.2

3.6

4.6

3.7

3.7

4.5

4.5

4.8

5.5

50

30

27

15

12

24

31

15.1

15.4

15.0

14.8

15.0

14.6

14.8

16.0

14.1

4.0

4.3

4.7

4.9

4.7

5.1

4.9

3.7

5.6

50

40

14

4

7

18

21

25

15.9

15.5

15.0

14.4

14.4

14.9

13.4

3.8

4.2

4.7

5.3

5.3

4.8

6.3

50

39

18

6

16

31

17.2

14.1

14.5

15.3

14.9

14.9

14.6

14.9

13.1

2.5

5.0

5.2

4.4

4.8

4.8

5.1

4.8

6.0

50

44

32

20

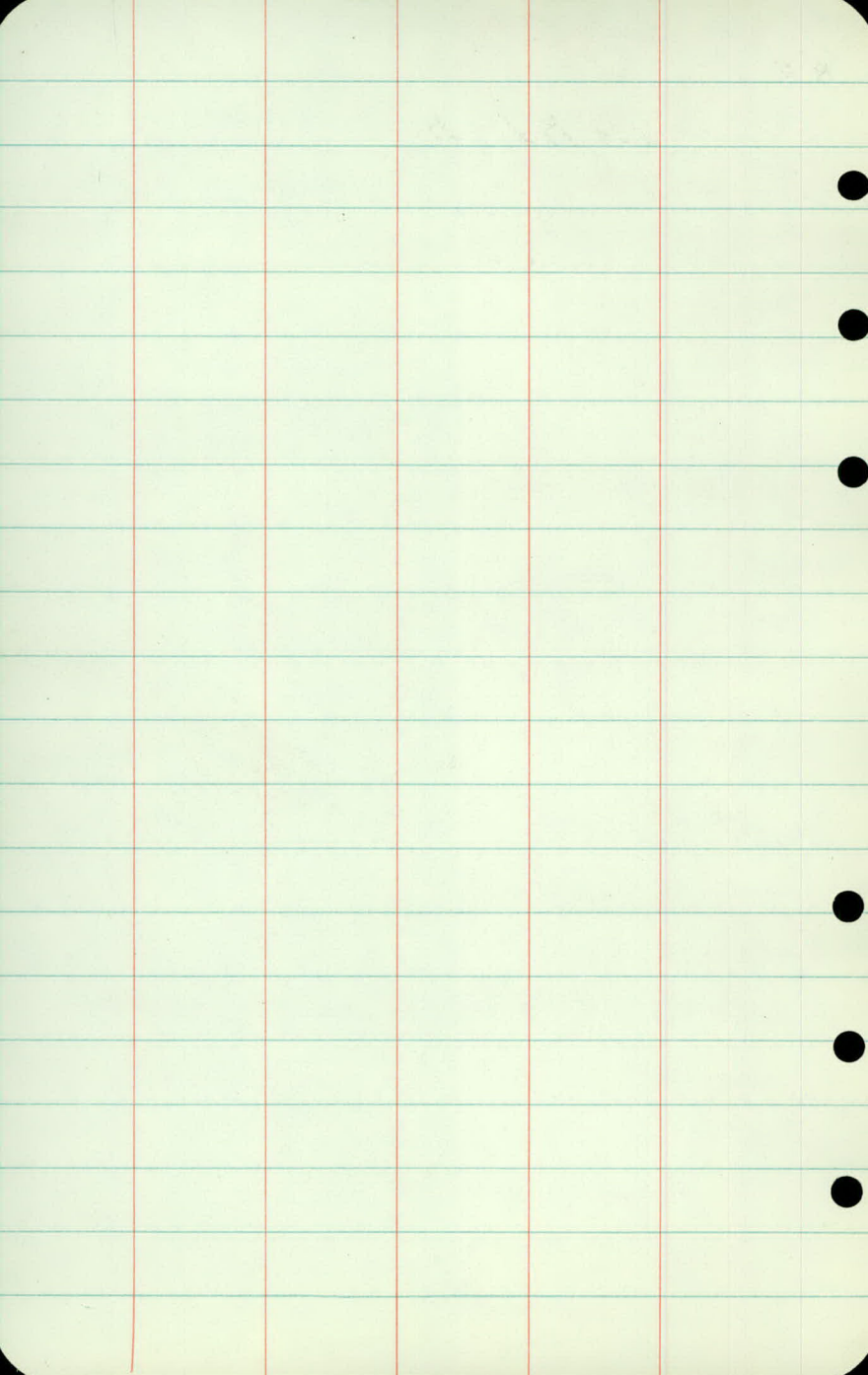
6

11

15

19

N. Edge Top Step MH Sta 23+



FK
RP
RW

108
v

Co. Rd. "H"

Soundings

Sta 11+80 Lt 10' El.=878.3

Feet	Blows	Material
0-1		
1-2		
2-3		
3-4		
4-5		
5-6		
6-7		
7-8		
8-9		
9-10		

Auger soundings
sand



sewer

Sta 11+80 Lt 24' El.=879.1

Feet	Blows	Material
0-1		
1-2		
2-3		
3-4		

Auger soundings
sand



Pipe

Water?

Sta 11+80

Lt 33' El: 880.8

109

Feet

Blows

Material

0-1

Sand

1-2

2-3

Peat

3-4

Gravel

4-5

~~Natural Ground~~ →

5-6

sand
Li

6-7

Natural Ground →

7-8

Topsoil

8-9

Peat

9-10

10-11

11 + 68

15' Lt El. = 878.6

Feet

Blows

Material

0-1

1-2

2-3

3-4

4-5

5-6

6-7

7-8

8-9

9-10

Auger Soundings

Sand
Fill

Peat
+
sand mixture

Peat

Sta 12+13 Lt 15' El= 877.6 ¹¹⁰

Feet Blows Material

0-1

1-2

2-3

3-4

4-5

5-6

6-7

7-8

8-9

9-10

Auger Soundings

Sand
Fill

Peat

Sand

Grey
sand

Sta 12 +13 Lt 24' El. = 878.1

Feet	Blows	Material
0-1		
1-2		
2-3		
3-4		
4-5		
5-6		
6-7		
7-8		
8-9		
9-10		

Auger Soundings

Sand
Fill

Peat
Topsoil

Brown
Fibrous
Peat

Grey
Sand

Sta 12+13 Lt. 33'

III
E/-878.1

Feet

Blows

Material

0-1

1-2

2-3

3-4

4-5

5-6

6-7

7-8

8-9

9-10

Sand
Fill

Peat
Topsoil

Brown
Fibrous
Peat

Grey
Sand

Sta 13+00 Lt 15' El. = 876.5

Feet	Blows	Material
------	-------	----------

0-1		
-----	--	--

1-2		
-----	--	--

2-3		
-----	--	--

3-4		
-----	--	--

4-5		
-----	--	--

5-6		
-----	--	--

6-7		
-----	--	--

7-8		
-----	--	--

8-9		
-----	--	--

9-10		
------	--	--

10-11		
-------	--	--

11-12		
-------	--	--

Auger Soundings
Sand & Gravel layers
of Fill

87

Sta 13+00 Lt. 30' El. = 876.9 ¹¹²

Feet Blows Material

0-1

1-2

2-3

3-4

4-5

5-6

6-7

7-8

8-9

9-10

10-11

11-12

Auger Soundings
Loose Sand Backfill
and Possible Water Main



Sta 12+70 Lt. 30' El. = 876.6

Feet	Blows	Material
------	-------	----------

0-1		
-----	--	--

1-2		
-----	--	--

2-3		
-----	--	--

3-4		
-----	--	--

4-5		
-----	--	--

5-6		
-----	--	--

6-7		
-----	--	--

7-8		
-----	--	--

8-9		
-----	--	--

9-10		
------	--	--

10-11		
-------	--	--

11-12		
-------	--	--

Auger Soundings

Fill Sand

Peat
Topsoil

Grey Sand

FK
LPD
RP

Sept. 15, 1965

± 2.5

113

Sta 14+00 Lt. 15' El. = 878.0

Feet	Blows	Material
0-1		Sand Fill
1-2		
2-3		
3-4		
4-5		
5-6		Topsoil
6-7		
7-8		Grey Sand
8-9		

± 3.4

Sta. 14+00 Lt. 25' El. = 878.9

Feet	Blows	Material
0-1		
1-2		
2-3		
3-4		
4-5		
5-6		
6-7		
7-8		
8-9		
9-10		
10-11		
11-12		

Auger Soundings

Sand Fill

Trace of Topsoil

Grey Sand

Sta $E = 876.6$ ± 2.4 114
 15+00 Lt. 15' El. = 879.0

Feet	Blows	Material
0-1		
1-2		
2-3		
3-4		
4-5		
5-6		
6-7		
7-8		
8-9		
9-10		
10-11		
11-12		
12-13		
13-14		
14-15		

Auger Soundings

Sand Fill

Peat at

Least 10'

Caved in

$\phi = 816.6$ $\pm + 3.4$

Sta 15+00 Lt. 25' El = 880.0

Feet	Blows	Material
0-1		Mixed Sand
1-2		Fill
2-3		
3-4		Brown Sand
4-5		
5-6		
6-7		Black sand
7-8		Grey sand
8-9		
9-10		
10-11		peat ? depth
11-12		
12-13		
13-14		
14-15		

FA
LPD
RW
RP

Sept. 16, 1965 $\pm - 2.7$ 115

Sta 12+00 R+20' E1=

Feet	Blows	Material
0-1		Sand
1-2		Peat
2-3		
3-4		
4-5		Grey Sand

Sta 13+00 R+22' E1= $\pm + 0.2$

Feet	Blows	Material
0-1		Fill
1-2		Sand
2-3		
3-4		Peat
4-5		Grey Sand
5-6		

±-1.0

Sta 14+00 Rt. 17' El. =

Feet	Blows	Material
0-1		Fill Sand
1-2		
2-3		
3-4		Peat
4-5		Grey Sand
5-6		
6-7		

Sta 15+00 Rt 20' El. = ±+0.1

Feet	Blows	Material
0-1		Sand Fill
1-2		
2-3		
3-4		Peat
4-5		
5-6		
6-7		Grey Sand

Sta 20+00 ϕ El =

Feet Blows Material

0-1

1-2

2-3

3-4

Fine Sand
Black

Sta 20+00 Lt. 25' El =

Feet Blows Material

0-1

1-2

2-3

3-4

4-5

5-6

Sand
Fill
Topsoil
Grey sand

Sta 20+00 Rt. 25' El =

Feet Blows Material

0-1

1-2

2-3

sand.
Topsoil
sand

Sta 21 ± El. =

Feet	Blows	Material
0-1		Dark Sand
1-2		
2-3		
3-4		

Sta 21+00 Lt. 30' El. =

Feet	Blows	Material
0-1		Sand
1-2		
2-3		
3-4		
4-5		Peat sand
5-6		

Sta 21+00 Rt 25' El. =

Feet	Blows	Material
0-1		Topsoil
1-2		Sand
2-3		
3-3½		

Sta 22+00 Lt El. =

Feet	Blows	Material
0-1		Sand
1-2		Peat Fill
2-3		
3-4		Mixed sand Fine
4-5		
5-6		Grey Sand
6-8		Silt Grey Sand

Sta 22+00 Lt 30' El. =

Feet	Blows	Material
0-1		Sand Fill
1-2		
2-3		
3-4		
4-5		
5-6		Topsoil
6-7		silt
		Sand

Sta 22+00 Rt. 30' El. =

Feet	Blows	Material
0-1		Fibrous
1-2		Peat
2-3		
3-4		
4-5		Sandy silt
5-6		Brown Sand

Sta 23+00 £ El. =

Feet	Blows	Material
0-1		Mixed Sand
1-2		
2-3		
3-4		Grey Sand
4-5		Brown Sand
5-6		

Sta 23+00 Lt. 30' El. 118

Feet	Blows	Material
0-1		Sand
1-2		Top Soil
2-3		Loam
3-4		Peat
4-5		Sand
5-6		Br Peat
		Grey Sand

Sta 23+00 Rt 30' El. =

Feet	Blows	Material
0-1		Topsoil
1-2		Sand
2-3		
3-4		
4-5		Silty Sand

Sta 24+00 L El. =

Feet	Blows	Material
0-1		Sand
1-2		Sand
2-3		Trace Peat
3-4		Sand
4-5		Peat
5-6		Grey Sand
6-		

Sta 24+00 Rt 30' El. = E+0.0

Feet	Blows	Material
0-1		Topsoil
1-2		
2-3		Sand
3-4		Sand
4-5		Grey Sand
5-6		

Sta. 24+00 Lt 30' El. = ^{±0.1} 119

Feet	Blows	Material
0-1		Topsoil
1-2		
2-3		
3-4		Sand
4-5		
5-6		
6-7		

Sta 25+00 ± El. =

Feet	Blows	Material
0-1		Topsoil
1-2		
2-3		Sand
3-4		
4-5		Peat
5-6		Grey Sand
6-7		

Sta 25+00 Lt. 30' El. = ± -0.6

Feet	Blows	Material
0-1		clay Topsoil
1-2		
2-3		
3-4		
4-5		
5-6		

Sta 25+00 Rt 30' El. = ± -1.5

Feet	Blows	Material
0-1		Topsoil
1-2		
2-3		
3-4		
4-5		
5-6		

Sta 26+00 $\pm$ El. = 120

Feet	Blows	Material
0-1		Topsoil
1-2		
2-3		
3-4		
4-5		Grey Sand

Sta 26+00 Lt 30' $\pm$ +0.4 El. =

Feet	Blows	Material
0-1		Topsoil
1-2		
2-3		
3-4		
4-5		Grey Sand

Sta 26+00 Rt. 35' El. = $\pm$

Feet	Blows	Material
0-1		Topsoil
1-2		Sand
2-3		
3-4		Grey Sand
4-5		

Sta 27+00 $\pm$ El. =

Feet	Blows	Material
0-1		Sand
1-2		
2-2 $\frac{1}{2}$		

Sta 27+00

Lt. 30' El. = ± 1.0
121

Feet

Blows

Material

0-1

Topsoil

1-2

2-3

Brown
Fibrous
Peat

3-4

4-5

5-5½

Grey
Sand

Sta 27+00

Rt. 30' El.

 ± -0.5

Feet

Blows

Material

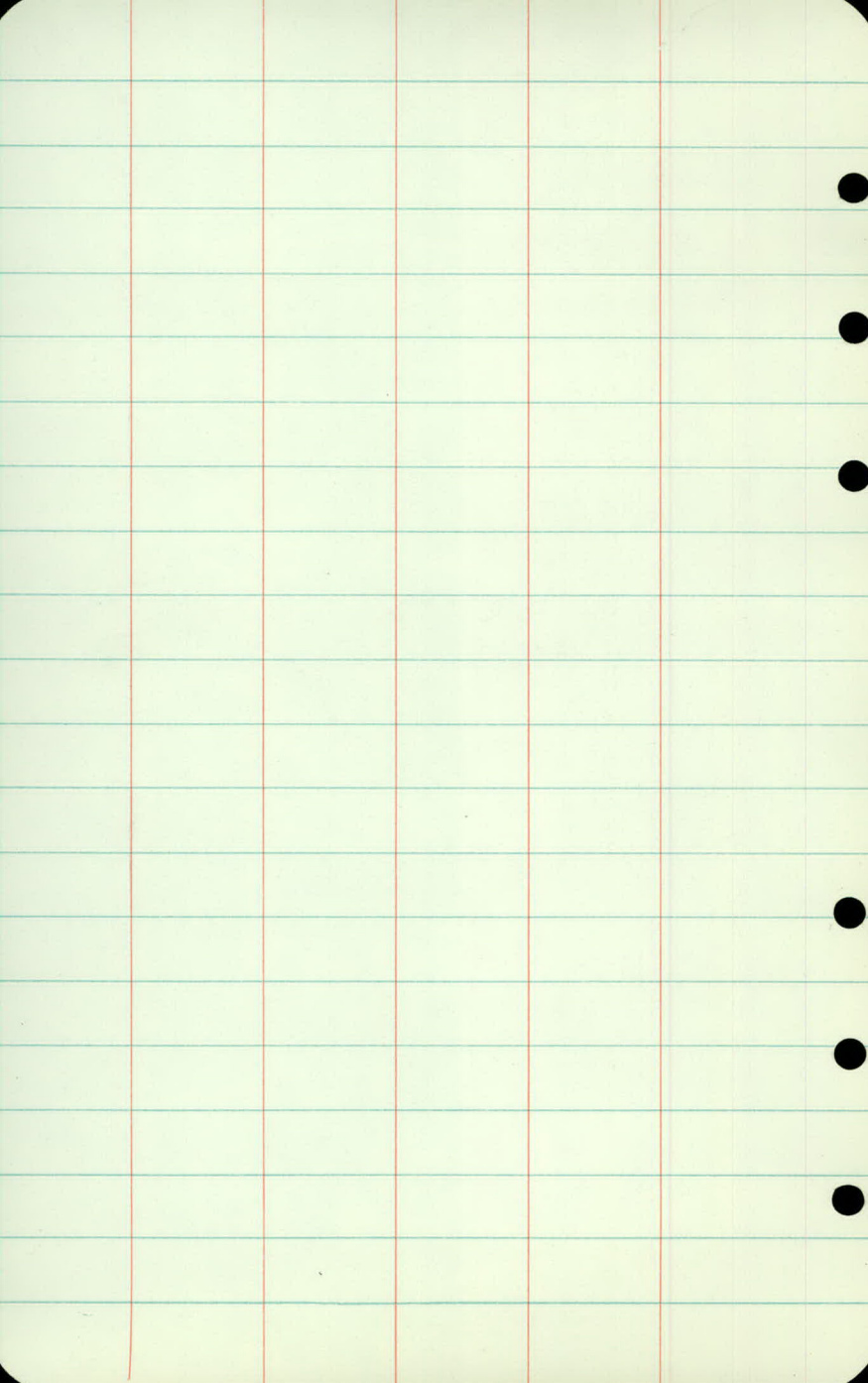
0-1

Topsoil

1-2

Grey
Sand

2-3



Sta 28+00

122

Feet	Blows	Material
0-1		sand
1-2		clay
2-3		Br Fibrous
3-4		Peat
4-5		sand

Sta 28+00 Lt 30'

Feet	Blows	Material
0-1		sand
1-2		sand
2-3		Peat
3-4		sand

Sta 29+00 E

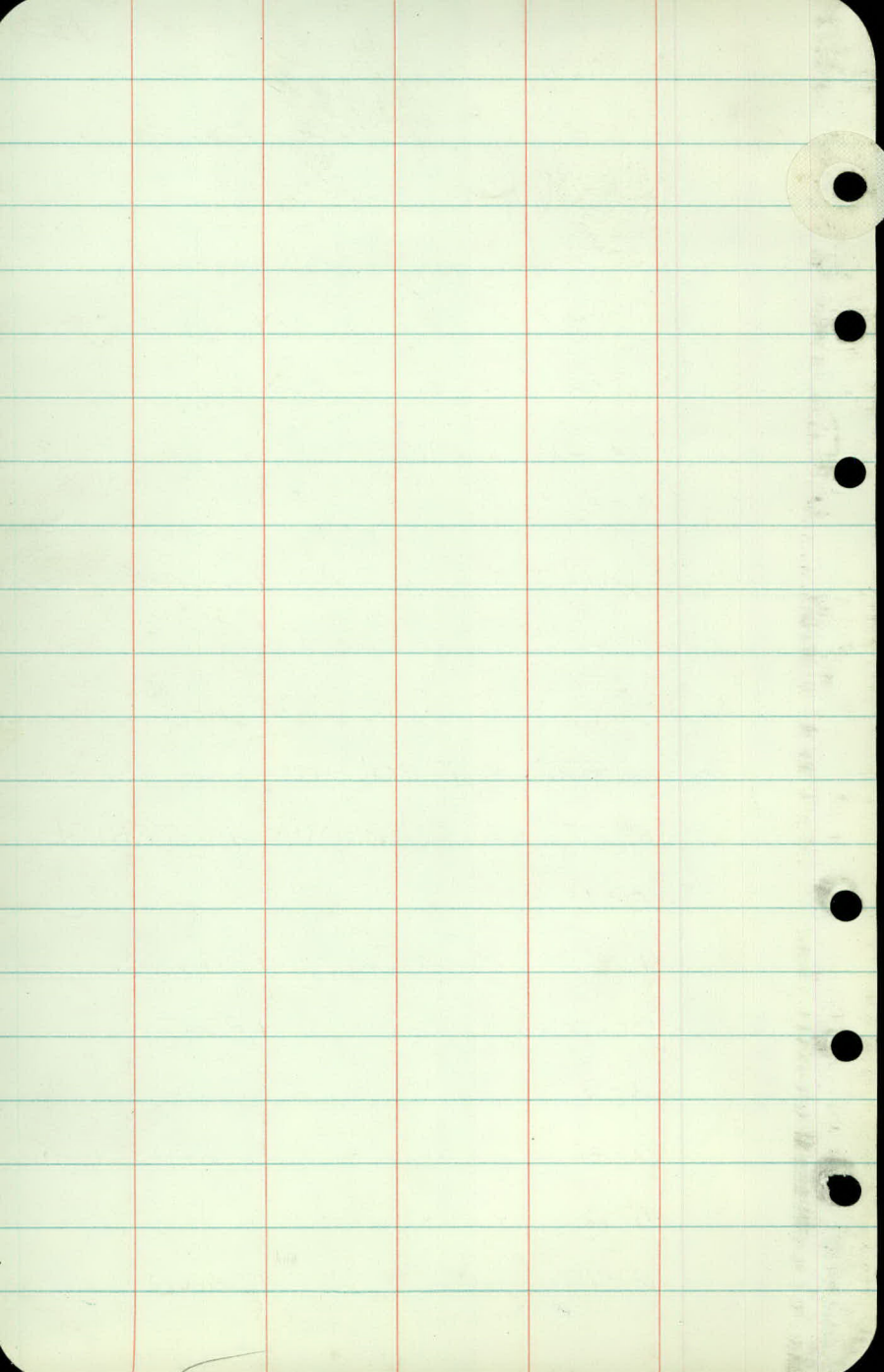
Feet	Blows	Material
0-1		sand
1-2		clay
2-3		Peat
3-4		sand

Sta 29+00 Lt 25'

Feet	Blows	Material
0-1		sand
1-2		peat
2-3		
3-4		sand

Sta	30+00	±		
Feet		Blows	Material	
0-1				
1-2				SAND
2-3				
3-4				PEAT
4-5				
5-6				
6-7				SAND

STA.	30+00	LT 30'		
FEET		BLOWS	MATERIAL	
0-1				
1-2				SAND
2-3				PEAT
3-4				
4-5				
5-6				
6-7				SAND



KP
DS
WS

2 NOV. 1967

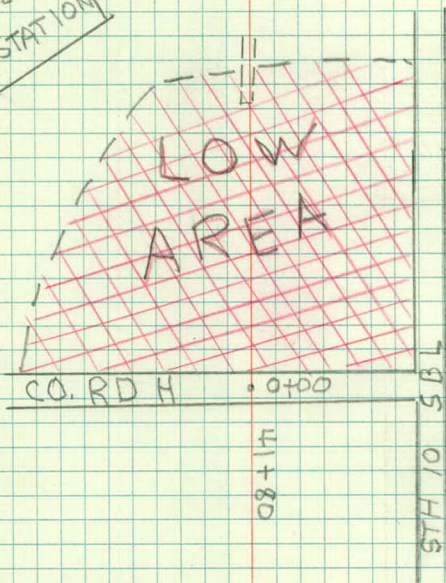


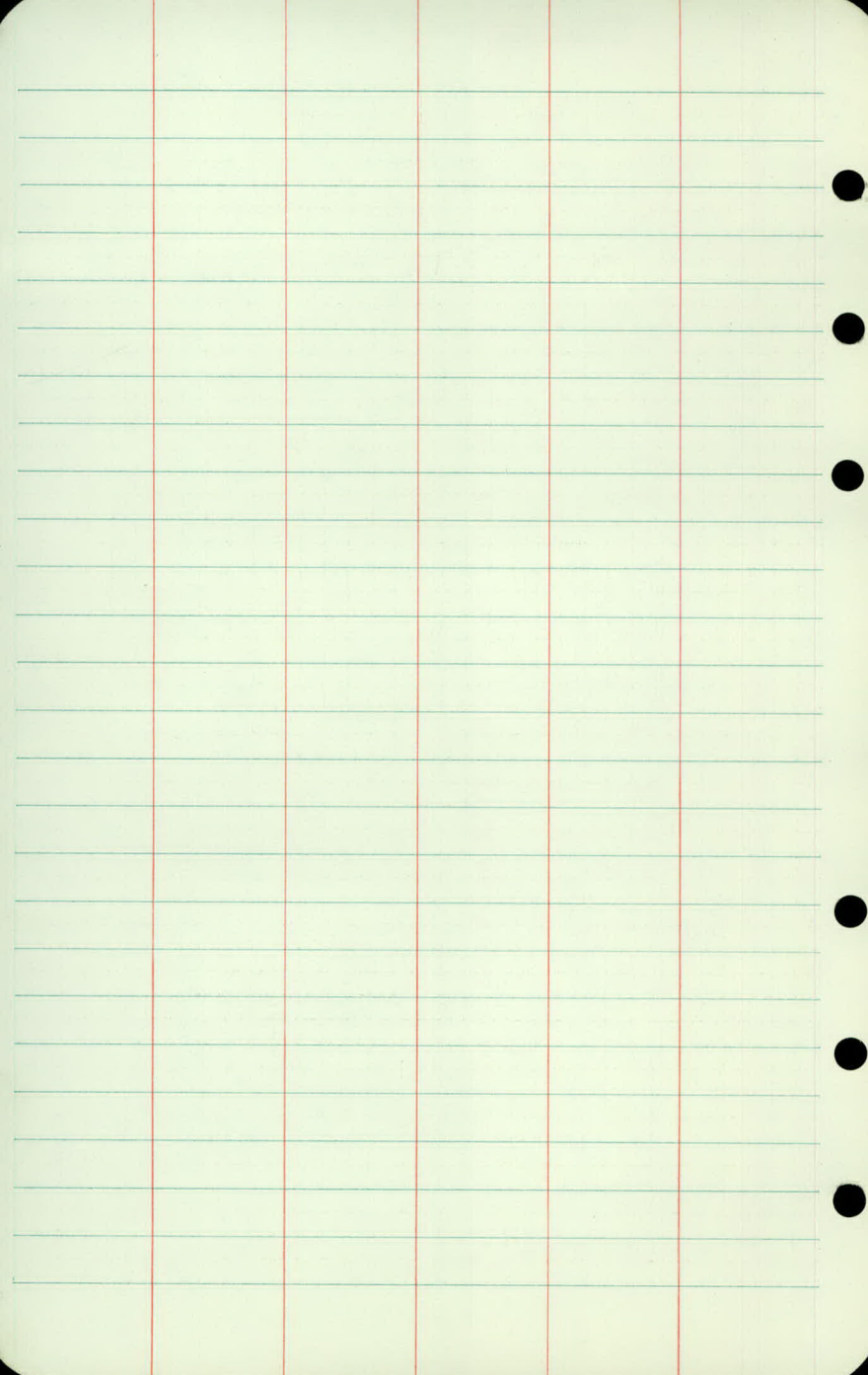
CO. RD H

STH 10 to west

DRAINAGE

SKELLY
STATION





2 NOV 1967

X- SECTIONS

0+00 - 1+63

STA + T - ELEV

BM 6.65 885.50

878.85

0+00 = C.O.R.D.H STA 41+80

✓

0+21 = GUTTER LINE

✓

0+22 = TOP OF BERM

✓

2 NOV. 1967

LT

±

RT

TOP SW COR HEADWALL OF BOX CULVERT

19.8	19.8	20.1	20.6	21.10
5.7	5.7	5.4	4.9	4.40
150	100	50		32

19.5	19.3	19.1
6.0	6.2	6.4
200	250	300

19.4	19.5	19.7	20.5	21.20
6.1	6.0	5.8	5.0	4.30
150	100	50		32

19.3	19.0	18.1	17.8
6.2	6.5	6.8	7.7
200	250	300	440
		FL CB	

20.1	20.6	20.6	21.20
5.4	4.9	4.9	4.30
50	25		32

STA	+	π	-	ELEV
-----	---	-------	---	------

		88550		
--	--	-------	--	--

0+33				
------	--	--	--	--

✓				
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0+37				
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✓				
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0+50				
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✓				
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LT

RT

2 NOV 1967

RT

80.5	81.2	80.8	80.8	81.24
5.0	4.3	4.7	4.7	4.26
50	25		11	32

80.5	81.9	81.9	80.3	81.0	81.28
5.0	6.7	6.7	5.2	4.5	4.22
50	27	17		15	30

81.1	81.2	81.2	81.5	81.1	81.34
4.4	6.3	6.3	6.0	4.4	4.16
50	30	21		22	30

STA	+	π	-	ELEV
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		885.50		
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0+75				
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✓				
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1+00				
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✓				
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+50				
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✓				
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+6				
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+63	= FL	S. END	20" SPAN	CMP
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2 Nov. 1967

LT

♀

RT

82.3	82.6	80.1	80.0	80.9	81.19
3.0	3.0	4.8	5.5	5.1	3.71
50	37	25	12		28

81.06
4.44

