

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

COUNTY ROAD B

From Hamline Av. To Dale St.

Road Acc't. No. 25 Dr. 9

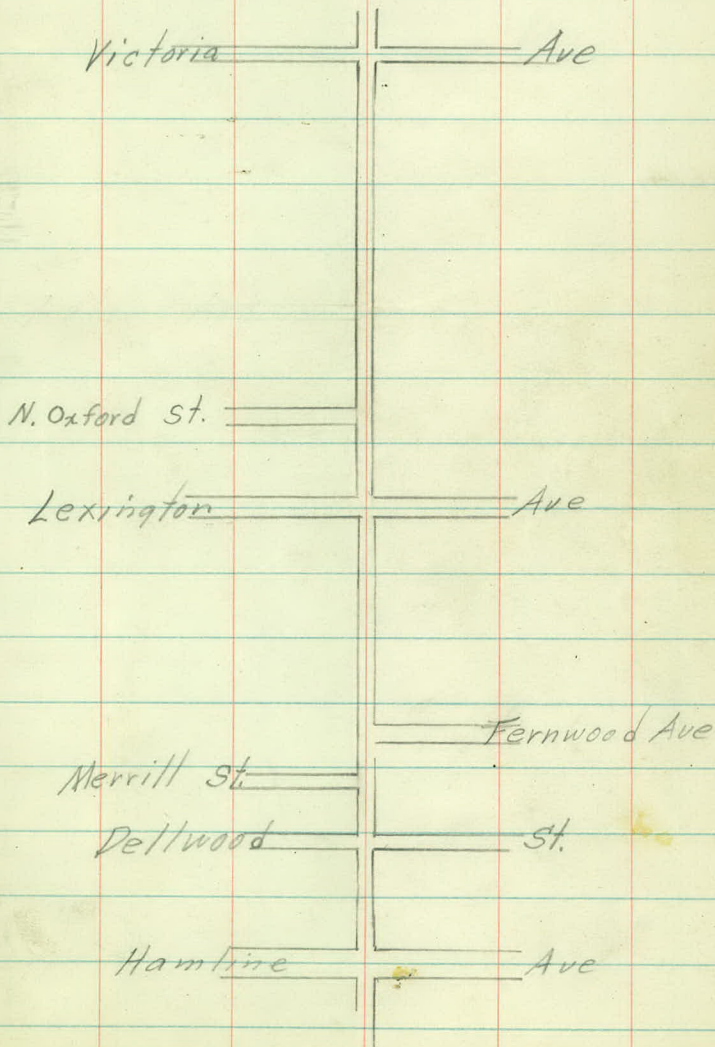
Date Filed 12-15-66 File BK. 56

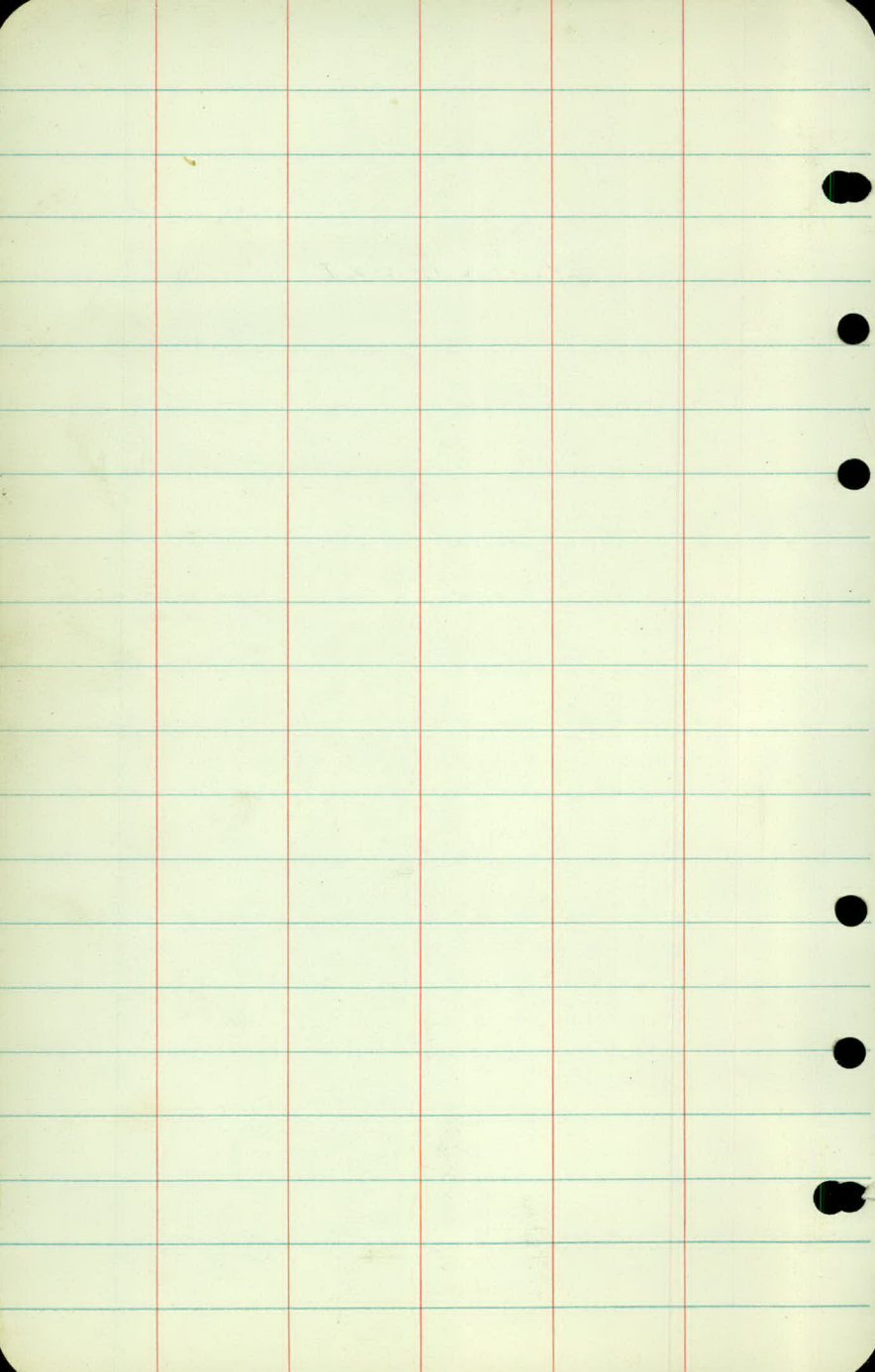
1

Co. Rd. "B"

Hamline to Victoria

PLAN SURVEY





July 9, 1965

2

Alinement

Sta Point Δ Lt. Δ Rt.

2634.40 P.I.

658.60

13+17.14 $\pm$ Fernwood Ave.

9+89.06 $\pm$ Merrill St.

^{.75}
6+58.57 $\pm$ Dellwood St.

0+00 Beginning

FK
PK
LPD
RP
HL

July 9, 1965

3

£ Lexington

Granite

Base Signal

Base Signal

40.94

43.54

42.63

47.02

Disk
PP

Hyd.

Cor. Ga. Fo.

69.93'

46.14

Iron

38.55

Iron

Hyd

3 N
PP

Cor.
Cone.

P.K. Nail

30'

60.33

43.00

30'

92.85

Iron

Cor. Wood.

Hyd.

44.55

31.02

BM

P.K. Nail

Cor. Garage

108.14

New Library

Base
Pure oil Sign

£ Hamline

Granite

131.60

48.23

55.91

Hyd

Sta	Point	$\Delta Lt.$	$\Delta Rt.$
-----	-------	--------------	--------------

52+55.40	End.		
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35+13.52	± N Oxford		
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FA
PK
LPD
RP
HL

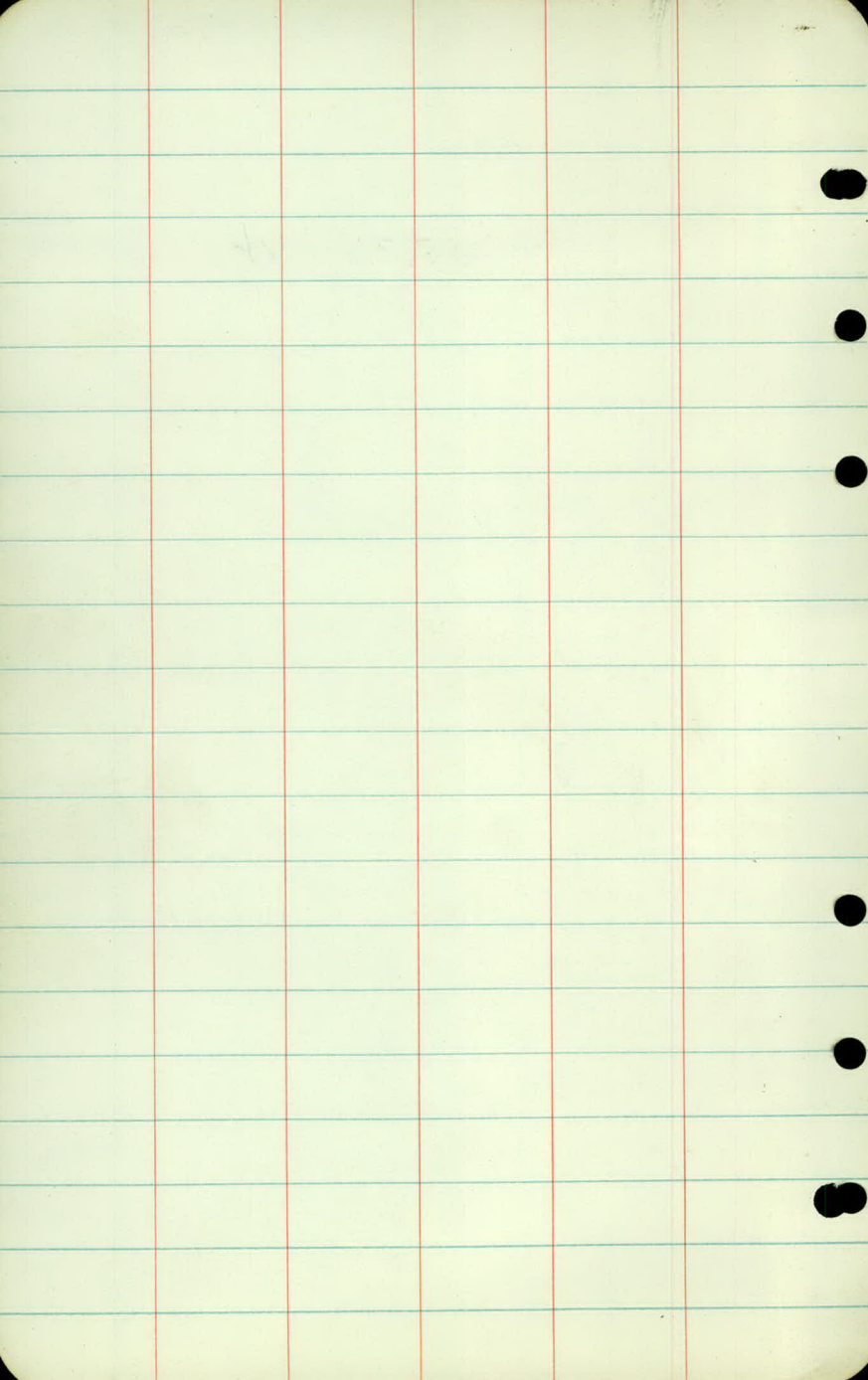
July 12, 1965

A

£ Victoria ϕ 94.97.
61.
118.90' $\square$ C.I. Mont.
60.24' Hyd.

Hyd $\square$ Top Cor.
W. Pillar
102.55
50.73
41.7A
33.11 ϕ Fe Post Iron
75.56
Hyd $\square$

H₀ #1026



Hyd.

+

6 PP

78+73.87

2 Dale

47.99

48.62

Manhole

P.P.

6

53.09

38.22

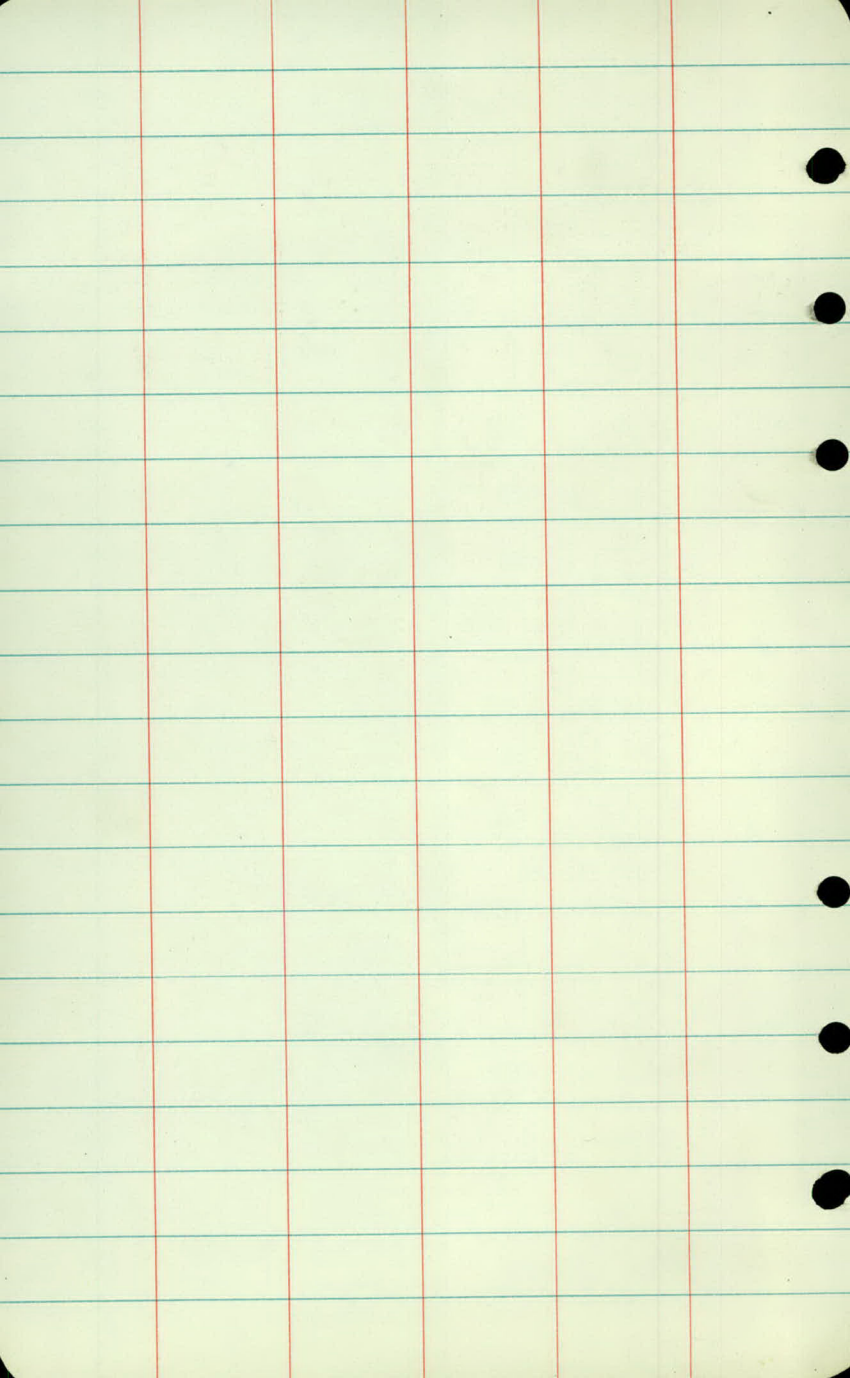
6 PP

52+36.56 DALE

61+45.9A P.O.T.

W. Edge Ho # 781
38.28' N

Victoria 52+55.40



TOPOGRAPHY

	Walk to	Bit	Fe
2	29	24 26	34
+93	2" P		
	56		
+73	2" P		
	57		
+61	2" P		
	71		
	ER	Cor Bit	Cor Bit
	72 24	41 25	28 32
	BR	R Tie	NW Cor Ga
	65 29	76 Garage	74 71
+50		Fe	Tap 14" BE
		43 35-65	57
			NW Cor Store
		29 71	
	ER	4" P	3" P
	40 29	15 65	13 70
+28	BR	Underground	24" Elm
	22	33 X-ing	11 63
		10 49	Old sign Base
	Bit Curb		107 Curb
	22		51 →
1	G.V.		Cor. Bit
+91	23		108 35
	SW Cor Library	Gas Tank openings	
	73 110	82 60-68-76	
	MH	NW Cor. Station	
	80 18	78 87	
		Underground	
		77 X-ing	
+50	MH	Pump Island	
	65 18 NSP	54 78-109	
N Edge Walk		E Edge Bit	Sign
27 Bit		33 Walk LT	36 36
+35	ER	BR	
	23	0+30 29	
0+00			

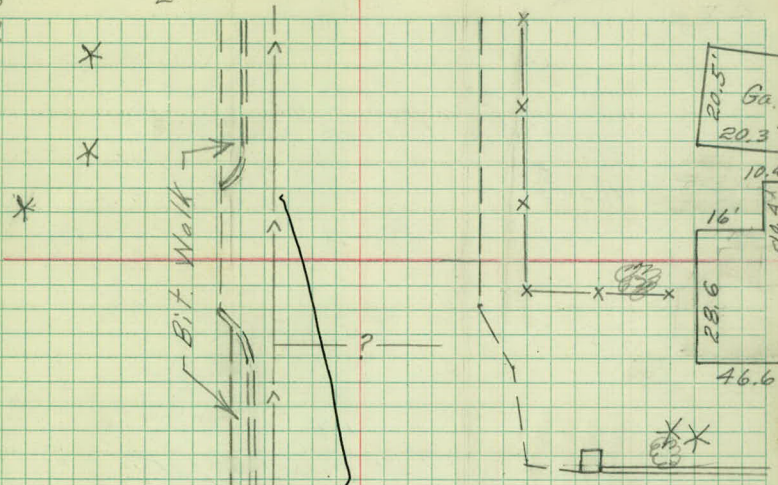
FK
PK
LPD
RP
HL

July 14, 1965

Rt.

6

Lt.



34.5 E-W
180.4 N-S

11" Casting
2 Adj. Rings
eccentric Cone N.
FL to Top 8.36'

10.4 0 0 0

28 E-W
48 N-S

9" Casting
4 Row Brick
FL to Top 7.84'

Granite Monument



Lt.

E

Rt.

+50

+45 Pond
92+53 E Ent
36+54 WE 12"x16" CM
22+20 Pond
50+36 Pond
68+29 E Ent
41+41 2"P
56+05 Pond
36+15 2"P
55+05 10"O
33+14 NW Cor Ho
81+13 E Ent
394 12"O
30Pond
39Bit
19 19+02 E Ent
24+02 4"O
56+88 D. Oak Pond
44 45+94 WE 12"x16" CM
23+68 Cor Pond
42

2

+70 Bit
18+60 E. Bit Apron
40+55 Bit
25+56 Bit
20

+50

+63 Trip 14"O
23+64 12" Gravel Ent
23 - 12"x16" CM

?

+39 NE Cor Ho
84+49 6"P
36+46 E Apron
32+03 SD
25+14 5"P
36+39 ER
16+07 5"P
36+09 Hvd
29+21 Por + Pitch
26+35 MH
16+07 4"P
44

3

+15 BR
37+03 MH
10Bit
26+02 SD
25+03 5" FE
70+95 ER
34+89 B.R
24+82 E 4 Walk
32+74 2"P
57+87 Underground
X-ing

+50

+46 NW Cor Ho
24+46 4" Maple
34+43 2"P
58+58 2"P
71+36 E 10' Ent
34 Dirt+23 2"P
57+11 Underground
X-ing+29 Fe Cor
34

2

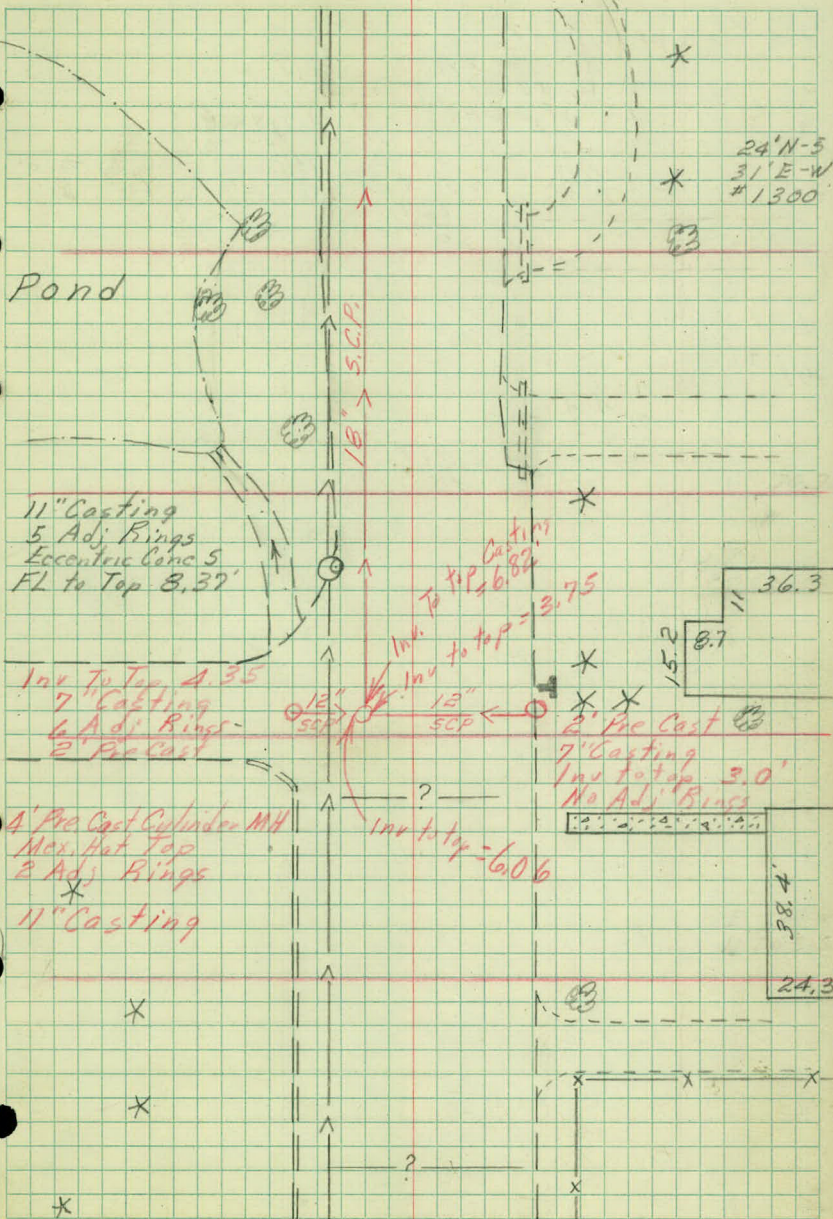
+03 2"P
72

Lt.

July 14, 1965

Rt.

7



7 $\checkmark$ GV 24 $\checkmark$ MH 11 $\checkmark$ Bit 18 15
 +94 24 +634 11 +92 GV 22
 +93 Hyd 27 +98 ER 18 +84 Are Lt 28
 +72 BR 42 +78 POR 29 +83 6"0 41
 +146 SP 30 +59 MH 18 +58 MH 19 +75 16" E/m 74
 +50 +27 SE Cor Ent slab 68 (15') +61 E-Gr 32
 +44 ER 45 +49 Underground X-119
 +24 BR 19 +36 POR 27
 +19 Bush 32 +24 Bush 32 +27 Bush 35 +36 B-GR 33 +29 6" Coff 48
 +19 4 Ash 50 +25 MH 22
 6 Bit 18 17
 +95 6" E/m 37

+435 SP 26.7
 +75 E Lilac 31
 +50 +55 6" M 37
 +40 SW Cor Ho 77 +435 S.P. 21.2
 +47 B. Lilac 32 +43 MH 10
 +17 NE Cor. Ho 78 +28 12' Ent 23
 +13 4' Walk 33 +12'x16' Gravel

5 +100 18"0 28 Bit 19 16
 +95 8"0 29 +90 Underground X-119
 +68 10" BE 43 +78 6"0 36 +89 36" Coff 42
 +50 8" BE 53 +57 8" BE 41 +55 18"0 54

4 +50 +51 18" E 29

July 14, 1965

8

Lt.

Rt.

6 Adj. Rings
24" Pre Cast CB
Inv. to top = 4.25
7" Casting

Inv. N to top = 9.90
2 Adj. Rings
eccentric Cone N
11" Casting

11" Casting
6 Adj. Rings
eccentric Cone E
FL to top 12.87'

11" Casting
FL to top = 12.48
eccentric W
7 Adj. Rings

11" Casting
No Adj. Rings
Concentric Cone
FL to top 9.85'

1 1/2' 5'-5"
23.4
10'
494

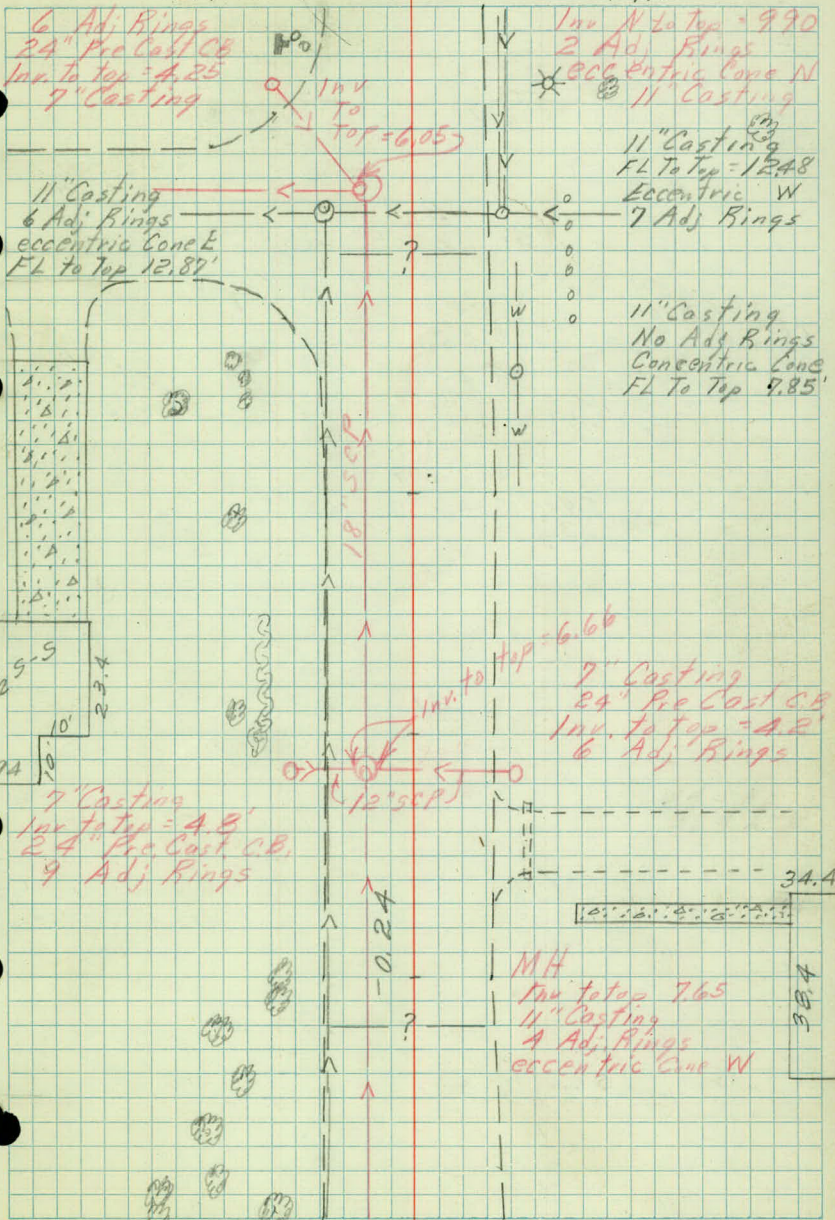
7" Casting
Inv. to top = 4.8'
24" Pre Cast CB
9 Adj. Rings

Inv. to top = 6.66
7" Casting
24" Pre Cast CB
Inv. to top = 4.2'
6 Adj. Rings

MH
Inv. to top 7.65
11" Casting
4 Adj. Rings
eccentric Cone W

34.4

38.4



2

+50

+42 $\frac{28''0}{50}$
Tw 18" BE
+24 $\frac{66}{66}$

+23 Tw 4" Birch
38

Bit
20 18

9

+81 SW Cor Ho
69

+86 $\frac{W50}{36}$
+71 6" Birch
38

+70 NW Cor Ho
80

+56 2" 10' Dirt
Ent

+67 $\frac{24''0}{26}$

+42 $\frac{20''0}{58}$

+42 Tw 14" S. Maple
41

+50

+65 R. Tie
Rt

+34 Honey Sack
97

+44 2" 9+12' Conc Ent
33

+31 10" Willow
78

+31 Tw 18" S. Maple
31

8

+100 SW Cor Ho
73

Bit
20 18

+80 N.W. Cor Ho
93

+83 Wall
29

+85 $\frac{W50}{37}$

+82 $\frac{24''N}{69}$

+67 5" Maple
37

+50

+54 Beg Ent Crushed Rock
Rt

+22 SW Cor Ho 1275
74

+46 4" Elm
44

+01 10" Elm
89

+16 NW Cor Ho
74

+27 $\frac{22''0}{62}$

7

+00 6" Elm
50

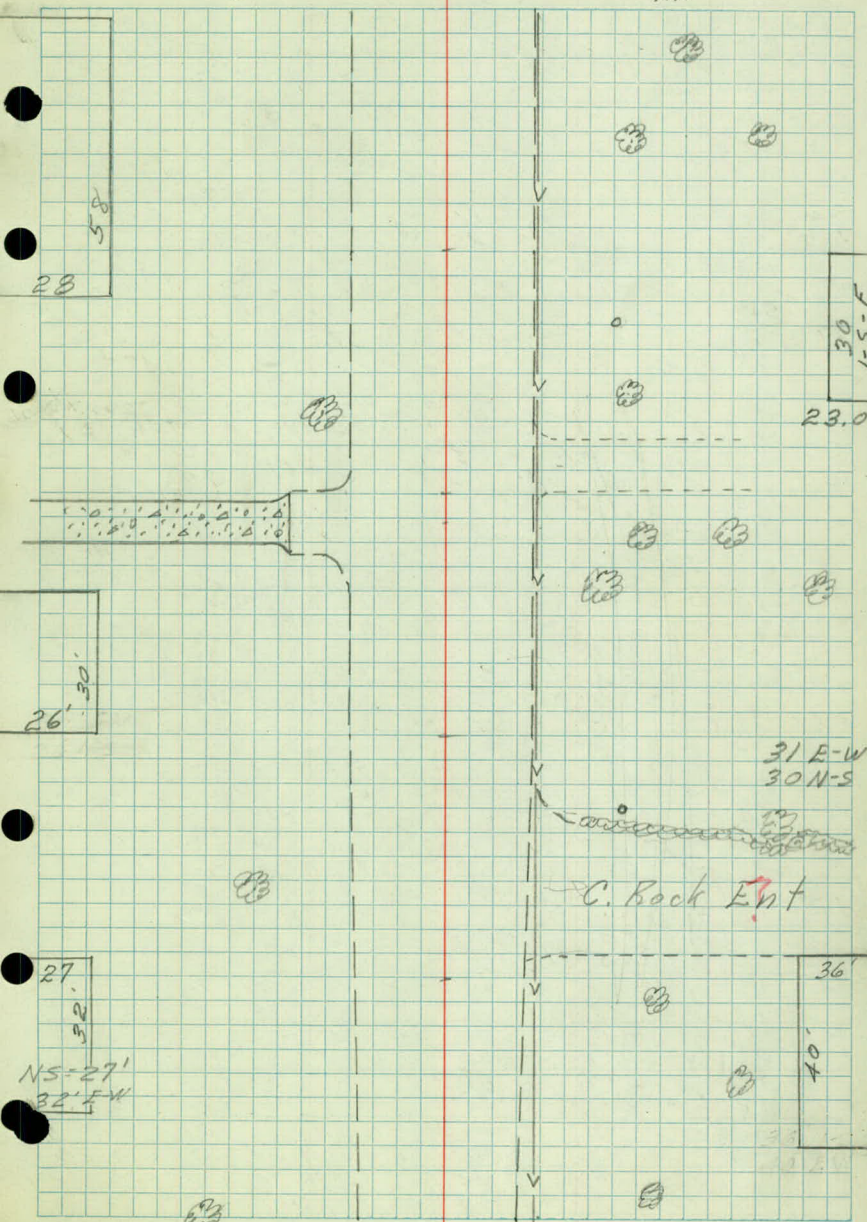
+05 $\frac{8''0}{43}$

Lt.

July 14, 1965

Rt.

9



12 Bit
23 15

+94 SW Cor Ho
83

+93 B Fe + Hedge
34

+82 Ed Ent
41

+85 8" Conc Ent
34

+72 Ed Ent
59

+73 16" O
70

+82 30" C. off
100

+61 Juniper
66

+69 X-Fe
34

+69 10" O
41

+56 Cedar
61

+63 8" W. F.
62

+51 5" P
40

+50 2" P
60

+46 E. Hedge
31

+20 10" Elm
35

+43 5" P
36

+48 6" P
40

+13 SW Cor Ho
68

+24 Underground
X-ing 103 36

+106 B. Hedge
31

+36 Sex 10" W. Willow
57

11 +11 SE Cor. 15" Conc Bit
56 Ent 24 16

+01 NW Cor Ho
70

+92 Fe Cor
34

+96 2" 10" Bit
Ent

+63 26" O
30

+86 Bush
30

+91 Hedge
32

+49 SW Cor Ho
69

+56 Underground
X-ing 183 59

+4 Red Tree
59

+29 MH
20

+78 8" Birch
36

+65 2" P
50

+31 6" Elm
36

+24 1" P
67

+55 20" W. Willow
33

+20 6" Elm
41

+46 8" Elm
49

+18 B Fe 40" CL
34

+14 Underground
X-ing 131 69

+31 NW Cor Ho
69

+20 ER
20

+109 10" Elm
55

+29 Bush
41

+31 Top 25
51

+10 Arc Lt
28

+13 Hyd
35

+121 2" 11" Bit
Ent

10 +103 BR
39

+13 G.V. Bit
33 16

+61 BT
81

+62 EE 3" W. H.
67

+75 BT
104

+78 ER
34

+66 E. Hedge
54

+78 BT
52

+64 Hedge
30

+68 4" Elm
52

+69 Hedge
45

+50 24" O
28

+63 BR
21

+59 MH
17

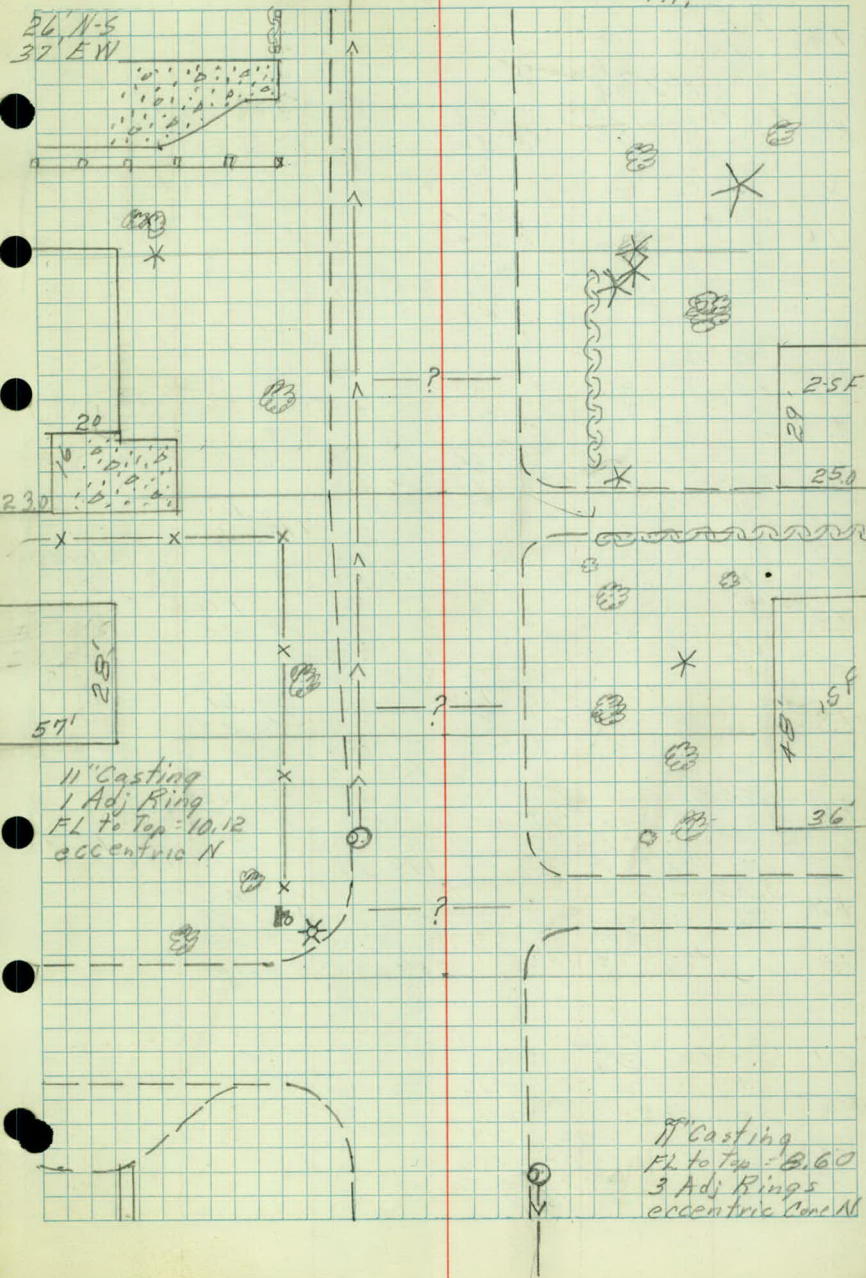
July 14, 1965

10

Lt.

♀

Rt.



				+40	NW Cor Ga 84	21' Bit Ent ± 15' x 25' CM
+42	± Ent RT Angle					+52 23
		+34	E Hedge 34		x-Fe	+37 5P 46
+26	± Ent 77	+20	8" P 52	+26	14" CE 95	+23 12" Elm 40
+11	Tu 30' Coll 29					
				+26	5P 50	
14		+02	10" Mt. Ash Hedge Bit 80	34	215-17	
+73	S.W. Cor Ho 112			+89	Sewer Xing	
		+47	5P 44	+95	W.S.O 35	
+39	Flon Ent 73			+47	8" P 51	
		+32	B. Hedge 34			
+28	10" CE 75			+28	20" CE 69	
+64	M.H 33	+24	± Ent 28			
+22	16" CE 71			+22	12" CE 78	
+63	S.O 21	+22	18" CE 65			
+17	M.H 19			+20	10" Catulpa 51	
13		+04	± 10" Cing Ent Bit 27	22		
+88	5" Mt. Ash 80			+77	BR 17	
		+79	1" Maple 42			
+60	3" Ash 57			+79	6" Coll 35	
+50		+54	S.W. Cor Ho 83			
				+74	4" Coll 59	
				+94	POR 24	
		+42	Fe Car 34			
+37	E. Hedge 36			+34	4" P 34	
		+23	3" Maple 58			

M.H.
11" Casting
15.75 Top to Inv
42" Pipe
Inv to Top = 6.0
4 Adj. Rings
Mex Hat Top

169

+38.6 SP
39.6

+52 Hyd
31

+38 POR
24

+209 ER
46

+72 12" Elm
40

+57 ER
17

+32 BR
43

+209 ER
46

+77 BR
17

+79 4" Coll
61

+79 6" Coll
35

+80 4" Coll
57

+93 Amt Lt
30

+28.7 M.H
40

+96.5 SP
39

FX
PK
LPD
RP
HL

July 15, 1965

Lt.

Rt.

11

EW = 28.5'
NS = 26'

5 Adj. Rings
Pre Cast C.B.
24" 7" Casting
Inv to Top 4.1'

11" Casting
1 Adj. Ring
FL to Top = 9.24'
Eccentric N

39
142

13'

42.3

34.5'
15.5'
74'

7 Adj. Rings
7" Casting
24" Pre Cast C.B.
Inv to top = 4.3'

Inv to Top = 6.2
Inv. to Top = 6.55

3 Adj. Rings
Inv. to top = 4.56
7" Casting
24" Pre Cast C.B.

MH
Inv to top = 14.65
4 Adj. Rings
11" Casting
Mex. Hat Top

17

$$\frac{\text{Bit}}{15 \ 15}$$

$$+93 \frac{6'' \text{CE}}{45}$$

$$+89 \frac{8'' \text{Cott}}{49}$$

$$+83 \frac{2 \ 12'' \times 17 \text{cm Conc}}{22 \ \text{Bit} \ 44}$$

$$+169 \frac{14'' \text{CE}}{34} +52 \ 43 \ \text{WSO}$$

$$+73 \frac{15'' \text{Elm}}{40}$$

$$+50 \frac{\text{MH}}{20}$$

$$+35 \frac{\text{NW Cor Ho}}{78}$$

$$+31 \frac{8'' \text{P}}{74}$$

$$+23 \frac{12'' \text{Elm}}{40}$$

$$+11 \frac{\text{Bush}}{46}$$

$$+11 \frac{\text{Bush}}{50}$$

$$+10 \frac{\text{E. Trees}}{50}$$

$$+125 \frac{28'' \text{CE}}{35}$$

$$+07 \frac{\text{Bush}}{46}$$

$$16 +00 \frac{\text{E. Trees}}{36} +5$$

$$\text{Bit} \ 15 \ 15$$

$$+00 \frac{8'' \text{P}}{69}$$

$$+91 \frac{2 \ \text{Ent} + 15'' \times 20'' \text{CA}}{22 \ \text{Cn Rock} \ 43}$$

$$+73 \frac{14'' \text{Elm}}{40}$$

$$+51 \frac{\text{WSO}}{43}$$

$$+50 +62 \frac{\text{WSO}}{40}$$

$$+40 \frac{\text{B. Trees}}{63} -34 +5$$

$$+49 \frac{\text{Triple Bitel}}{55}$$

$$+40 \frac{\text{NW Cor Ho}}{79}$$

$$+32 \frac{6'' \text{P}}{69}$$

$$+13 \frac{2 \ \text{C.R. Ent} 10''}{25}$$

$$+39 \frac{\text{Sewer Xing}}{46}$$

$$+32 \frac{\text{Bush}}{46}$$

$$+36 \frac{\text{Bit}}{16}$$

$$+28 \frac{\text{Bush}}{46}$$

$$+28 \frac{\text{Bush}}{50}$$

$$15 +20 \frac{\text{Bit}}{23}$$

$$\text{Bit} \ 23 \ 16$$

$$+24 \frac{20'' \text{Elm}}{39}$$

$$+99 \frac{2'' \text{P}}{59}$$

$$+98 \frac{15'' \text{CE}}{34}$$

$$+82 \frac{\text{WSO}}{44}$$

$$+64 \frac{2'' \text{Mt. Ash}}{41}$$

$$+73 \frac{\text{Tr. 3'' Bitel}}{52}$$

$$+73 \frac{14'' \text{Elm}}{40}$$

$$+58 \frac{\text{SW Cor Ho}}{84}$$

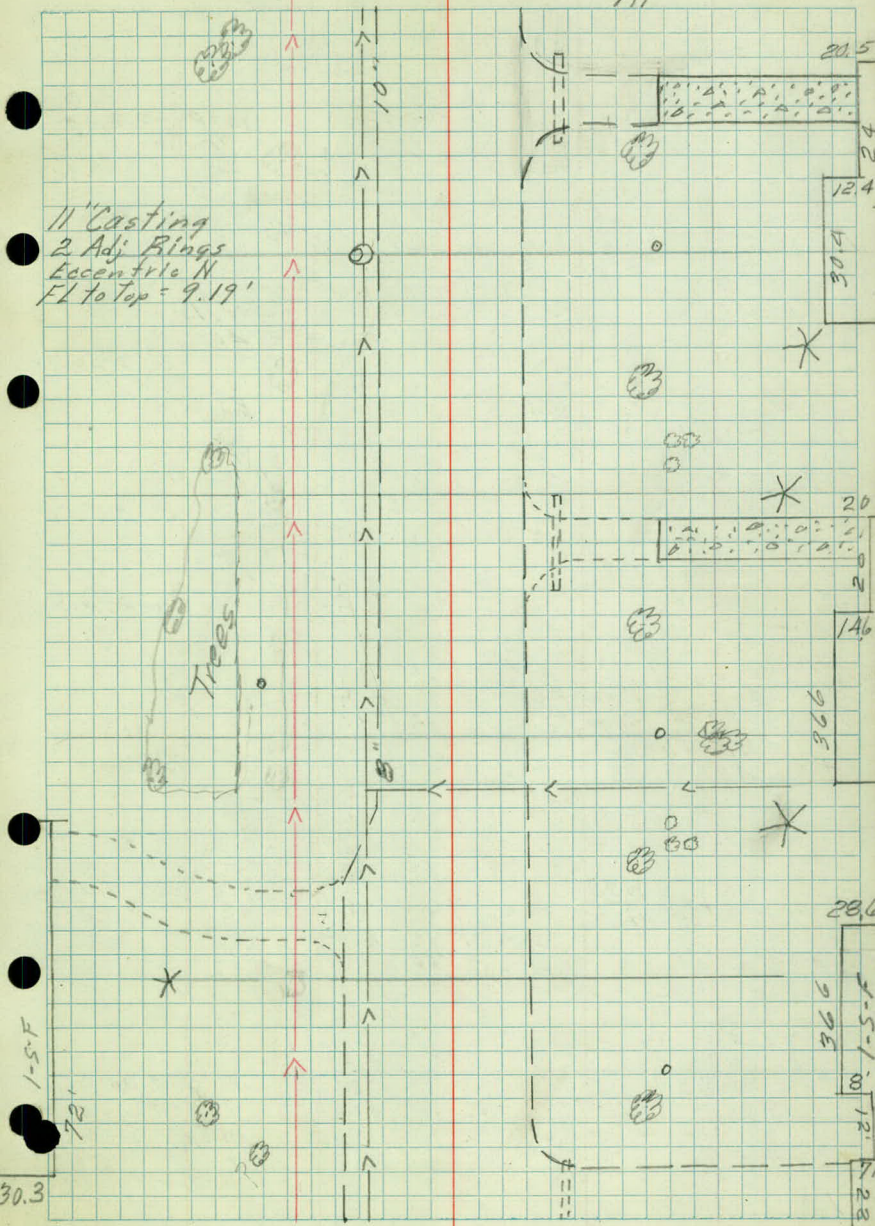
July 15, 1965

12

Lt.

Rt

11" Casting
2 Adj. Rings
Eccentric N.
FL to Top = 9.19'



+50

+36 WSO
44
15" Elm
+23 40
+06 N.W. Cor Garage
99

19 ~~EP~~ ~~PK~~ Bit 17 15 +08 ± 18.5' Conc Ent
23 (Bit)

12" Elm
+74 40

+70 Bush
36

+50

+62 9' Conc Ent
33 (Bit)

+54 Bush
35

+01 MH
49'

+01 SD +29 Gas Connection
20 RT

+01 SD
25

+13 N.W. Cor Ho +23 12" Elm
78 40

18 ~~3~~ ~~51~~ ~~22~~ Bit 16 15 +01 6" P
+85 ~~B. For Trees~~ 43 +92 Hyd 29 +92 Hedge 32

+69 5" Fe
37

+88 6" P
33

+92 6" V
27

+38 WSO
43

+78 12" x 16" CM 8' Conc
22 C.R. 43

+50

+66 6" P
33

+60 10" Elm
40

+40 WSO
43

+14 Sewer +23 N.W. Cor Ho
Xing 78

+23 16" Elm
40

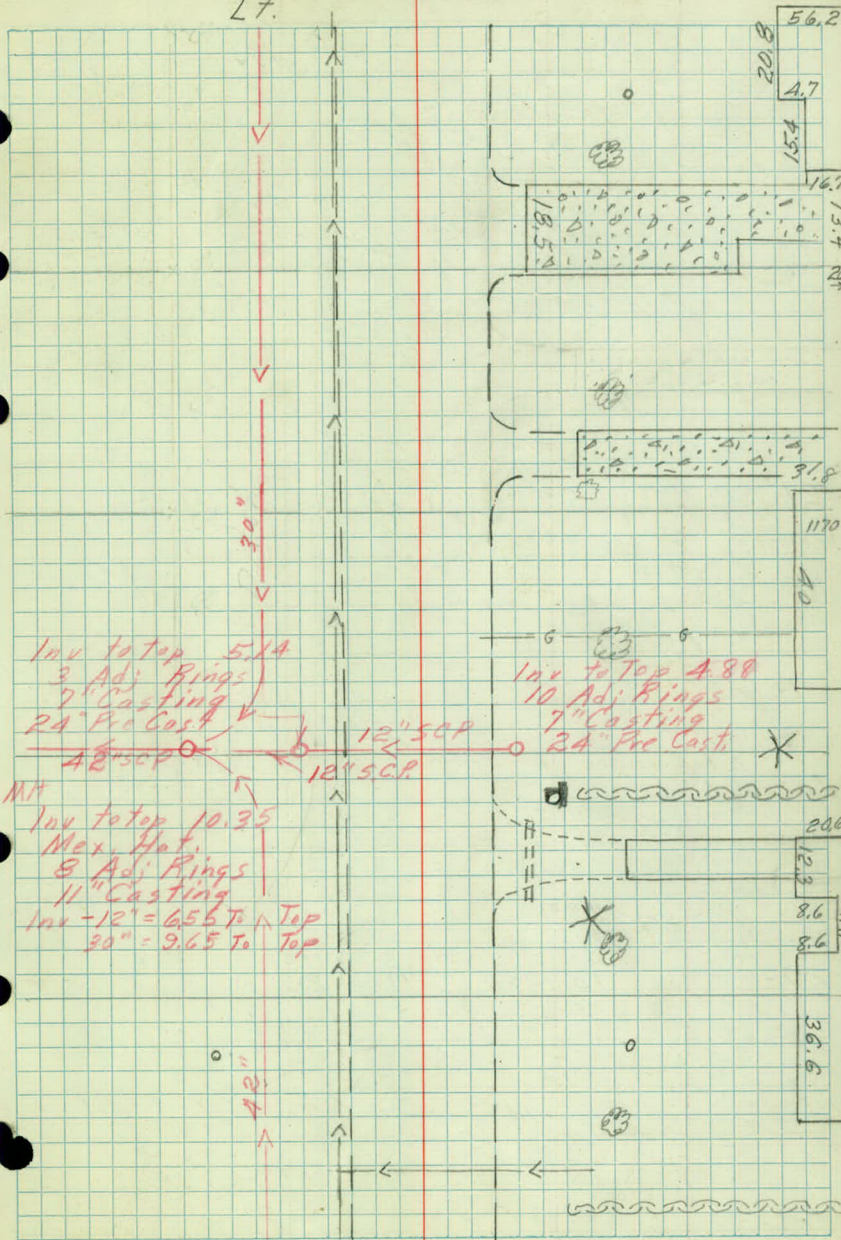
+06 Hedge
31

17.

July 15, 1965

13

Lt.



22		Road Ditch	Fe
	18 16 22		33
+78	S.E. Cor Ho.	+76 SP	N.W. Cor Ditch
	96	22	33 - 46
+76	M.H.	+9.5 11" Bit Ent	Rip Rap
	33	15" x 20" CM 24"	
+85	62	+85 14" Coll	+76 SP
	62	78	21
+51	16" Elm	Tn 5" S. Maple	
	44	A5	+84 14" Elm
	44		40
+29	Cor Conc	+27 S.W. Cor Garage	12" Elm
	62	98	+44 40
		15" x 20" CM 4 1/2 - 11"	
	+35	20 Conc Ent 23	+40 B. Fe
			34
+16	8" Coll.	+16 Cor Conc	+15 Cor B.T.
	82	85	46
		+16 12" Coll.	+38 Con B.T.
		45	46
	+14	Curb	+07 W 2 15" x 33 CM
		26	20
+10	Curb	+15 3" P	+09 E. Fe
	43-59	53	33
		+04 15" x 20" Road	+06 15" Elm
		22 Bit 18 16	40
21			Ditch Fe
	+04		24 33
+98	Curb	+92 14" Elm	
	43	26	45
	14" Maple	SW Cor Ho.	
+58	75	62 93	+94 N.W. Cor Walk
			97.3
	+51	1" P	
		91	
	X Fe 36" Coll	+45 15" Elm	
+45	45	44	
	+23	4" P	+57 B Fe
		87	34
+33	10" Conc Ent	15" x 20" CM	+64 12" Elm
	50	22	40
	+23	4" Ent	+60 E. Fe
		41	39
+03	Juniper	+15 Juniper	+52 B. Fe
	58	59	39
	+09	4" Walk	+25 10" Elm
		54	40
	+09	4" Ent	+16 Dry Well
		B.T. Ditch Road	22
20		43 26 17 17	25
+86	15" x 24" CM	+90 4" Maple	
	24 C. Rock	67	
+89	M.H.	+82 SW Cor Ho.	
	20	94	+85 E.E 15" CM
			22
+75	Fe Cor	+75 X Fe	+84 12" Elm
	43	43	39
	+73	Fe Cor	+74 Fe Cor
		+89 Underground	34
		Crossing	
+90	4" Ent	+65 E. Trees	M.H.
	34	43	19

July 15, 1965

Rt. 14

M.H.
Inv. 30" to Top 7.50
Inv. 12" to Top 5.88
11" Casting

1 Adj Ring
eccentric East

24" Pre Cast
Inv. to Top 2.20
1 adj. Ring
7" Casting
Bit.

50.2 EW Inv. To top 40.3
24.0 NS 7" Casting
No Adj Rings
24" Pre Cast

PARKING

Portable
Curb

23.8'

10' School

32.2 EW
26.2 NS

30" SCP

36" Chain Link

Bit Ditch Filled

55.6'

Playground

56.2 EW
28 N-S

48" Chain Link

6" Casting
FL To top = 9.09
No Adj Rings
eccentric N

6" Casting
Brick construction
FL to Top = 3.93

Abandon

+44 74 B Fe
 Walk
 +45 63 -70
 +44 32 B. Guard Rail
 +45 74 SECoy Bldg
 +31 35 E.R. Curb
 +27 73 Dry Wall
 +30 34 End Wall
 +22 45 BR
 +21 40 10" Elm
 +13 33 BT
 +16 31 PP
 24 24 20 Bit
 +01 44 B. Curb

+60 20 BT
 +42 73 S.W. Cor. Bldg
 +37 62 -69 B. Walk
 +25 98 20" Cat
 +25 79 18" Cat
 +10 19 MH
 +105 74 4" Walk
 +105 74 15" Elm
 +105 66 -A4 Cor Hedge
 23 20 17
 +99 83 1" P
 +84 67 6" Maple
 +70 57 1" P
 +70 79 SW Cor Ho
 +79 33 B Fe
 +78 42 Cor BT
 +66 44 B. Hedge
 +55 62 20" Cat
 +55 44 16" Elm
 +47 20 WE 12" X 34 CM
 +47 33 E Fe
 +55 46 Cor BT
 +44 30 Hyd
 +42 59 8" Maple
 +38 23 6V
 +44 28 GV
 +21 45 12" Elm
 +23 39 14" Elm
 +12 59 8" Apple
 22 +04 94 SW Cor. Ho

FK
PK
LPD
RP
H2

Lt.

July 16, 1965

15

6 Chain Link

Bt

81.6

103.4

108.

Rock Parking Area

7'

9 Casting
1 Adj Ring
Eccentric N
FL to top = 8.91

30 EW
24 NS

20 EW
38.4 NS

Parking

[illegible]

FX
PK
LPD (shrubs)

Lt.

July 16, 1965
July 19, 1965
Rt.

16

+83 - 34
+79 - 34
+79 - 36
+72 - 39
+68 - 43
+69 - 45
+68 - 48

C.B.
+79 20

CONC

9" Casting

4 Adj. Rings

Eccentric Cone S

FL to Top C = 11.29

Est FL Inv. to Top = 8.29

10" Casting

4.2' Bottle Top

4' NS X 3' EW

1 row Brick Adj

9" Casting

4 Adj. Rings

Eccentric S

FL to Top C = 10.79

C.B.
+56 43

C.B.
+13 50

12" SCP

24" SCP

97'

Service Sta

30.5'

Parking

SEE P. 27A FOR M.H. & C.B. INFO.

Sta +43 56 +50 55
 +21 Ent 123 29 +25 24 +49 End Port. Curb 34
 +24 42 +23 SW Cor. Ho 88 +25 4 Birch 51
 +06 4 Birch 62 +14 28.5 Conc Ent 34 +16 B. Portable Curb 35
 +07 Ent 30 +10 Ent 37 +107 2" P 43 +110 Post 35
 29 +00 Cor Ent 23 +23 20 +100 2 Ent
 +84 51 Const 73 +79 Hedge 33
 +83 6 Elm 39 +77 Wall 33 +89 Post 35
 +75 LTP 34 +78 Fe 33 +88 GR 43 +90 Fe 43
 +63 2 Ent 20
 +47 E.G.R. 32

28 B.T. 22
 +98 Cesspool 19 +71 E.C. 22 +71 End Walk 27-32
 +73 M.H. 22.3 +74 Cor Walk 48 +69 Fe 36 +78 NW Cor Bldg 55
 +75 S.W. Cor. Store 158 +65 E.Curb 55 +61 Curb 35
 +59 Sign 35
 +59 ER 22 +57 LTP 35
 +47 2 Ent 29 +53 BC 33
 +37 Pumps 55-68 +54 BR 27
 +29 ER 27 +30 E.Curb 34
 +20 Curb 36 +16 ER 22 +25 BF 22
 +11 BBC 27 +10 B.C.C 33 +14 Pumps 69-82

27

Lt

July 19, 1965

Rt

17

27.7'EW
24.2'NS

Parking

Stone & Concrete

Cement Block

PARKING

3" Casting
6 Row Brick
4" Casting
6" Block Construction
Inv to top = 7.1
Bottom to top = 16'

Brick
+
Block

53.5

41.8'

PARKING

11" Casting
2 Adj Rings
Eccentric N

stone wall

B. t.
14 16

32
+70 96
+70 47
+74 44
+50 40
+86 66
+70 73
+59 41
+10 49
+2 44
+54 22
+10 49
+32 40
+25 40
+107 39
+107 34
+107 34
+16 16
+94 68
+92 95
+78 22
+73 52
+50 98
+10 29
+106 38
+20 17
+83 65

+99 Hedge
52

+47 Flower Box
53

+28 NW Cor Garage
83

+33 40
+123 43
+109 44

+123 43
+109 44

+109 44

31
+95 40
+92 95
+78 22
+73 52
+50 98
+10 29
+106 38
+20 17
+83 65

+92 NW Cor Ho
73

+73 45
+58 38
+46 78
+46 37
+46 35
+26 51
+98 NW Cor Ho
78
+95 52
+77 41
+64 34

+10 29
+106 38
+20 17
+83 65

+92 NW Cor Ho
73

+73 45
+58 38
+46 78
+46 37
+46 35
+26 51
+98 NW Cor Ho
78
+95 52
+77 41
+64 34

+10 29
+106 38
+20 17
+83 65

+92 NW Cor Ho
73

+73 45
+58 38
+46 78
+46 37
+46 35
+26 51
+98 NW Cor Ho
78
+95 52
+77 41
+64 34

+10 29
+106 38
+20 17
+83 65

+92 NW Cor Ho
73

+73 45
+58 38
+46 78
+46 37
+46 35
+26 51
+98 NW Cor Ho
78
+95 52
+77 41
+64 34

+10 29
+106 38
+20 17
+83 65

+92 NW Cor Ho
73

+73 45
+58 38
+46 78
+46 37
+46 35
+26 51
+98 NW Cor Ho
78
+95 52
+77 41
+64 34

FK
PK
LPD
HL

21.

July 20, 1965
2 Cloudy Rt.

18

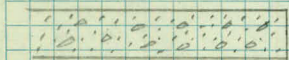
34.3' EW
32.6' NS

11" Casting
5 Adj. Rings
Eccentric Cone A
FL to Top 10.98'
Inv to Top 9'

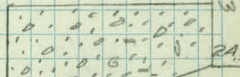
11" Casting
2 Adj. Rings
Eccentric S
FL to Top C = 8.39'

31.6' N-S
28.6' EW

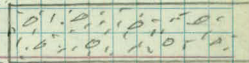
27.7' EW
24.1' N-S



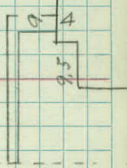
20.2
12.1
8.3



36.3
30.3



24.2
5.6
4
5.6



2

+45 NW Cor. Ho
69

+43 Tw 6" P
68

+20 SW Cor. Ho
95

+45 5" Ash
43

+31 Tw 4" Birch
36

+23 4" P
67

+11 5" Birch
75

+22 4" Ash
44

+22 12" Bit ent 6" x 14" Cl. Pipe
24

34

+11 6" P
58

+16 16
16

+13 Tw 4" Birch
37

+97 8" Elm
44

+85 18" Maple
78

+99 8" WP
79

+71 6" Elm
46

+79 SE Cor. Ho
94

+69 1" P
59

+67 NW Cor. Ho
69

+51 8" Hackberry
71

+56 1" P
46

+62 4" Maple
35

+40 1" P
59

+26 8" Conc Ent
27

+40 4" Elm
45

+15 4" Elm
56

+12 5" WP
42

+37 18" Ent
43 Gravel

3

+103 4" P
66

+17 15

+107 WSO
44

+90 NW Cor. Ho
67

+96 Hedge
64

+76 16" Elm
75

+74 Cedar
32

+79 Hedge
59

+55 22" Elm
50

+62 4" Ash
41

+44 SW Cor. Ho
98

+34 NW Cor. Ho
76

+50 WSO
43

+40 6" P
95

+34 Good 1" Birch
41

+29 18" Double Ent
36 Cedar

+25 Arb. birds
31

+29 Cedar
51

32

+10 4" P
42 +109 2" Ash
65

+113 1/4" Ent
Gravel

July 20, 1965

Lt

37.0 19

24.5

27.0 NS
29.5 EW

X

⊗

X

⊗

XX

30' NS
46.3 EW

X

⊗

X

⊗

X

⊗

27.0 NS
29.5 EW

⊗

X

X

~~~~~

⊗

⊗

32.6' EW  
37.3' NS

⊗

X

⊗

⊗

⊗

o

o

⊗

o

⊗

⊗

⊗

36.3

24.3

34

1.5

266

35

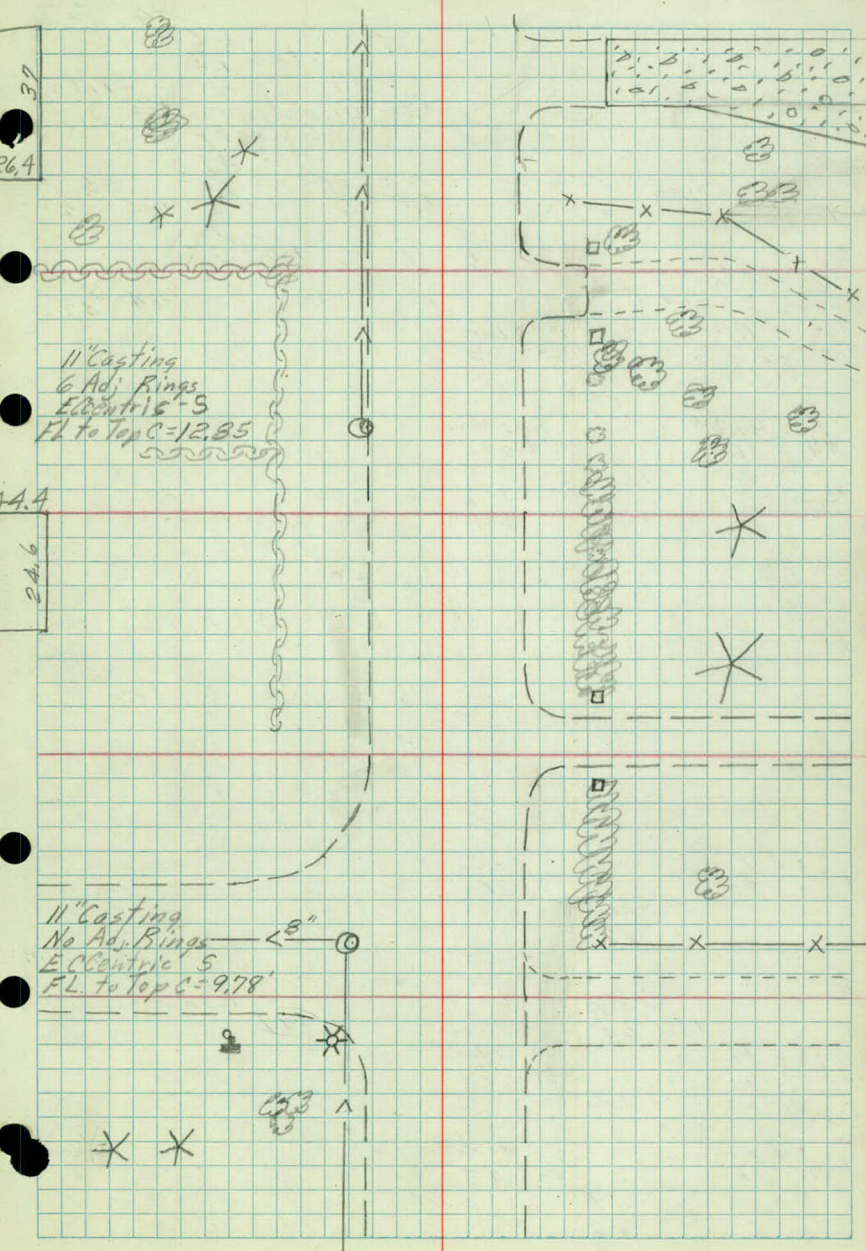
24

|                          |                  |             |                |                           |                 |
|--------------------------|------------------|-------------|----------------|---------------------------|-----------------|
| 37                       |                  | 16 15       | 191            | 2 14' Cor Ent             | 34 Bit          |
|                          |                  | +56 20"O    | 166 24"O       | +62 Fe                    |                 |
|                          |                  | +45 Fe      | +46 10' Ent    | +55 Pillar                |                 |
| +80 5" Birch             | +99 3" Elm       | +75 2" P    | +39 18" Oak    | +39 P.O. Dr               | +34 P.O. Drive  |
| 59                       | 59               | 42          | 50             | 77                        | 90              |
|                          | +69 S.W. Cor. Ho |             | +66 6"O        | +37 Pillar                | +75 10"O        |
|                          | 84               |             |                | 32                        | 26              |
| +65 4" P                 |                  | +62 2" P    | +31 15"O       | +65 E Fe                  | +28 24"O        |
| 48                       |                  | 59          | 34             | 30                        | 41              |
|                          | +59 2" Calulpa   |             | +76 Edge Conc  | +28 Lilac                 | +84 Edge Conc W |
|                          | 75               |             |                | 32                        | 52              |
| +51 Cor Hedge            |                  | +51 Lilac   | +17 Lilac      |                           | +23 12" Oak     |
| 33-100                   |                  | 33          | 32             |                           | 54              |
|                          | +18 MH           |             |                | +19 10"O                  |                 |
|                          | 76               |             |                | 72                        |                 |
| +16 5" Apple             |                  | +13 Bushes  | +12 10"O       |                           | +06 End Trees   |
| 62                       |                  | 35-67       | 56             |                           | 32              |
|                          | +Hedge           |             |                | +10 Lilac                 |                 |
| 36                       | 34               | 15          | 17             | 31                        |                 |
|                          |                  |             |                |                           |                 |
|                          | +SW Cor Ho       |             |                |                           | +93 Lilac       |
| +76                      | 83               |             |                |                           | 32              |
|                          |                  |             |                | +97 10" P                 |                 |
|                          |                  |             |                | 62                        |                 |
|                          |                  |             |                | +69 12" P                 |                 |
|                          |                  |             |                | 60                        |                 |
| +53 B. Hedge             |                  |             |                | +53 10' Bit               |                 |
| 35                       |                  |             |                | Ent                       |                 |
|                          | +47 ER           |             | +44 2x2 Pillar |                           | +62 2x2 Pillar  |
|                          | 16               |             | 32             |                           | 32              |
| +29 POR                  |                  | +23 BR      |                | +23 12" Elm               |                 |
| 25                       |                  | 43          |                | 56                        |                 |
|                          | +12 MH           |             | +11 X-Fe       |                           |                 |
|                          | 19               |             | 33             |                           |                 |
| 35                       |                  |             | Bit            | +11 Begin Buckthorn Trees |                 |
|                          |                  |             | 17             | 32                        |                 |
| +83 BR                   | +92 POR          | +97 ER      |                | +97 14' C. Rock           |                 |
| 17                       | 20               | 33          |                | Ent                       |                 |
| +91 Arc Lt               |                  | +91 GV      |                |                           |                 |
| 23                       |                  | 44          |                |                           |                 |
| <del>+76 SW Cor Ho</del> | +89 Hyd          |             |                |                           |                 |
| 83                       | 44               |             |                |                           |                 |
| +74 4" P                 |                  | +77 24" Oak |                |                           |                 |
| 49                       |                  | 33          |                |                           |                 |
|                          | +74 8" P         |             |                |                           |                 |
|                          | 56               |             |                |                           |                 |

20

11" Casting  
6 Adj. Rings  
Eccentric - S  
FL to Top C = 12.85

11" Casting  
No Adj. Rings  
Eccentric S  
FL. to Top C = 9.78

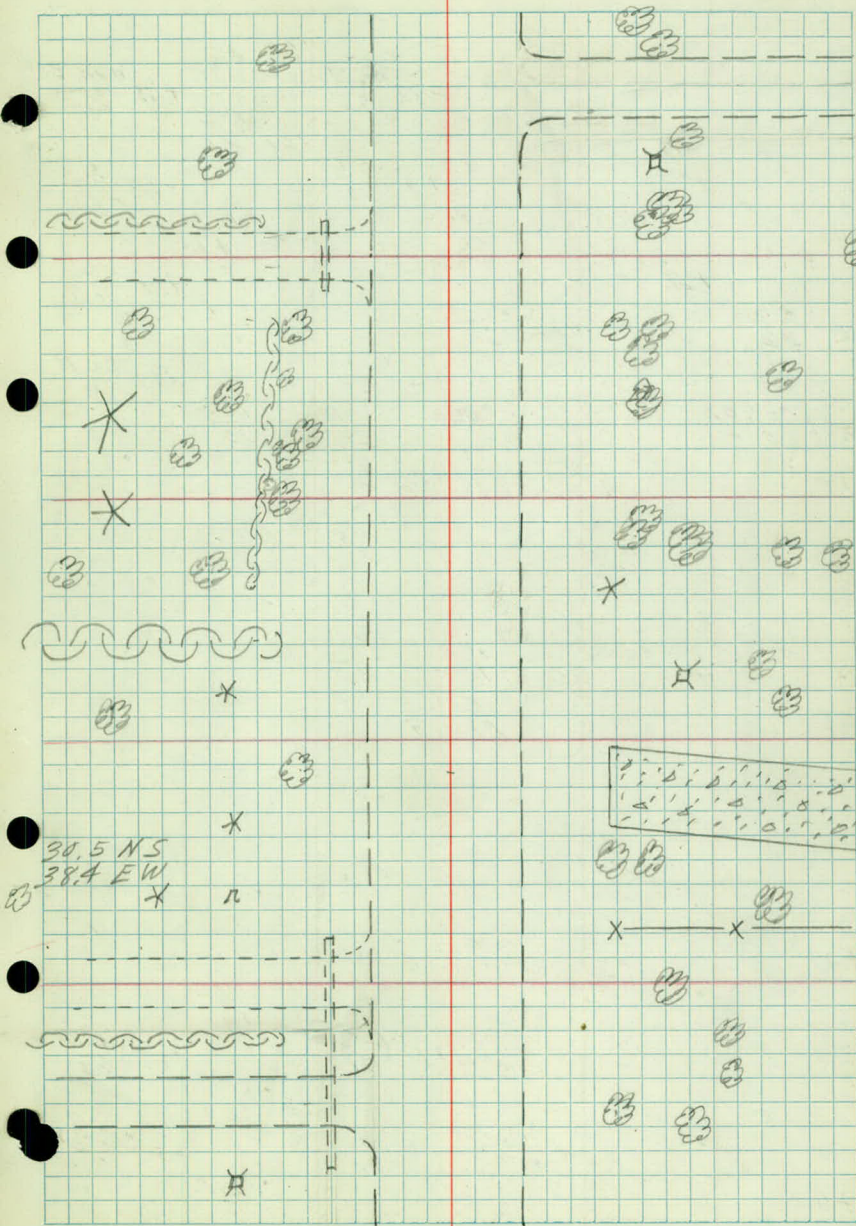






July 20, 1965

21

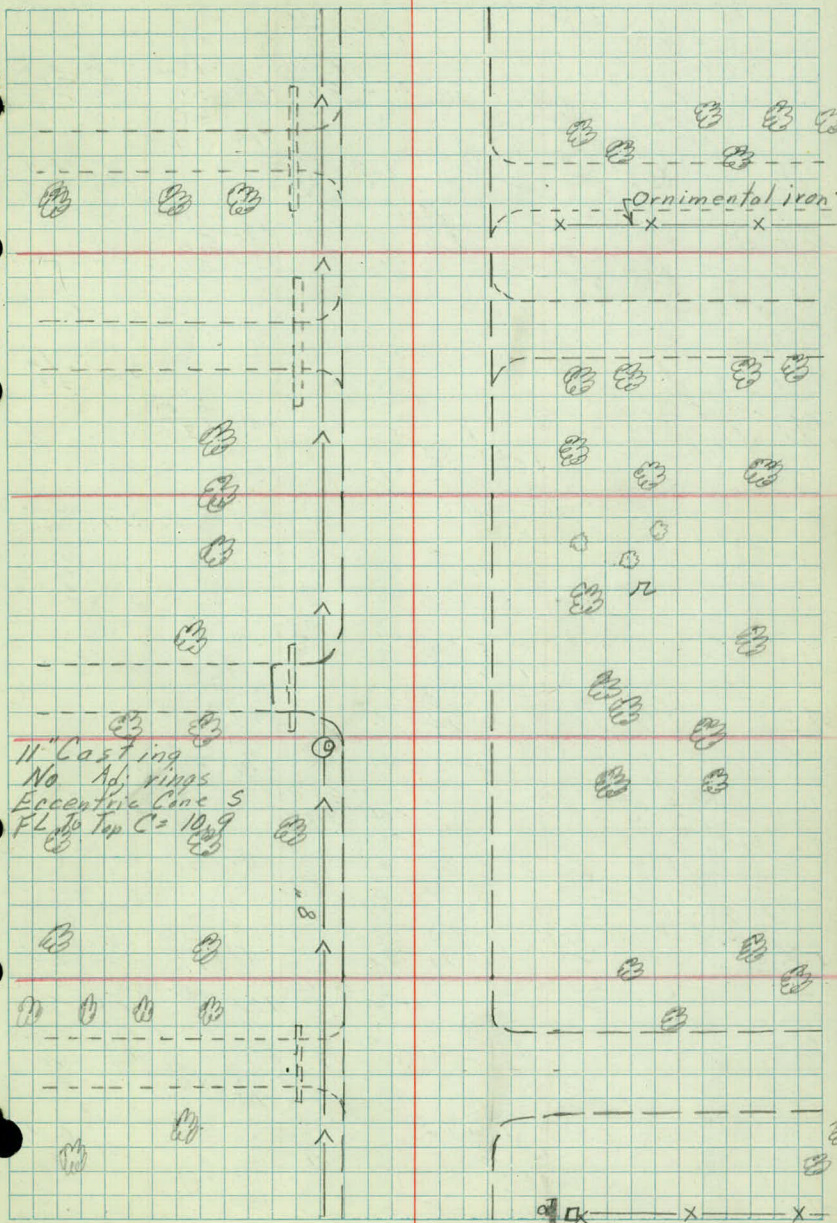






July 20, 1965

22





FK  
LPD  
HL

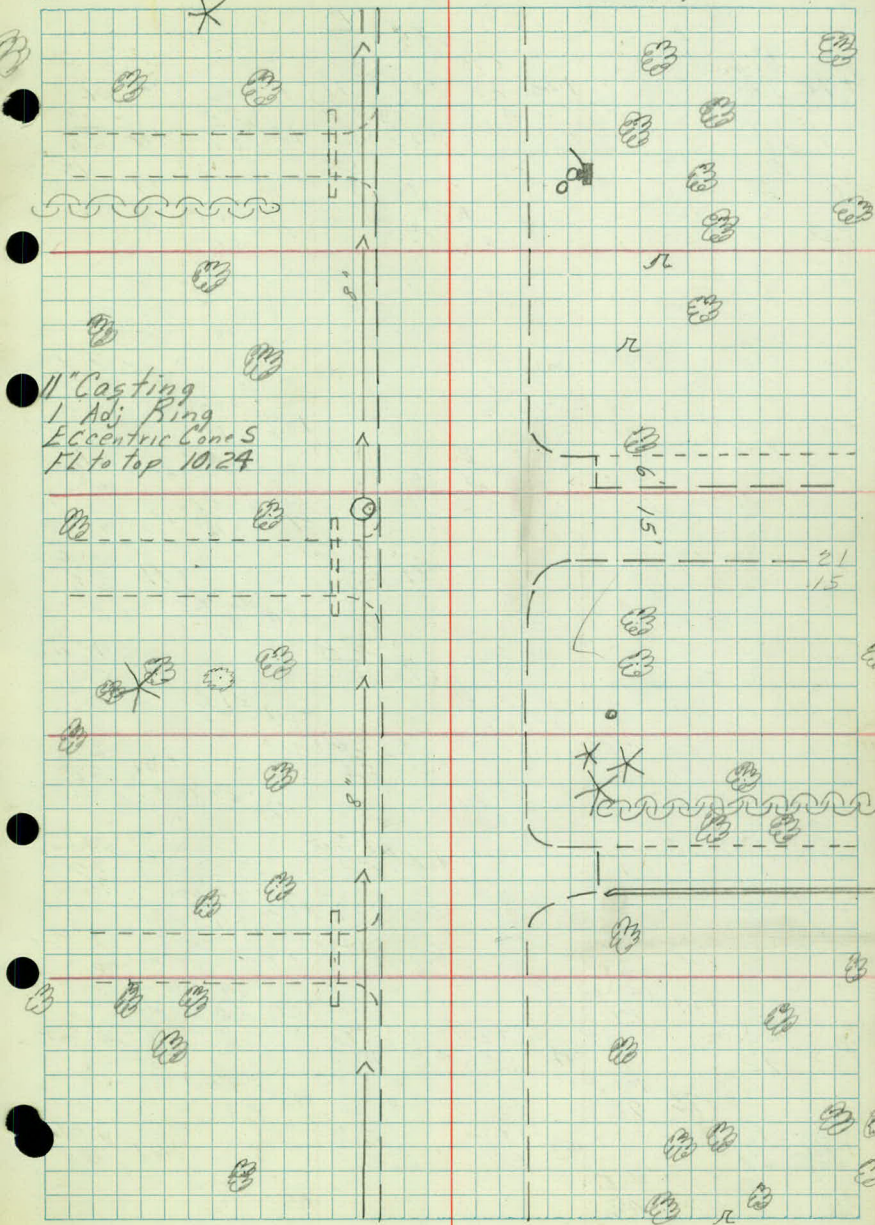
Lt.

August 5, 1965  
£

Rt.

23

11" Casting  
1 Adj Ring  
Eccentric Cone S  
FL to top 10.24





|                 |                |            |               |
|-----------------|----------------|------------|---------------|
| Bit             |                |            |               |
| 47              | 15             | 15         |               |
| +83 12"x14"CM   | +83 28 Ent     | +85 1" P   | +84 1" P      |
| +83 22 R.T      | +83 Dirt       | +85 36     | +84 42        |
| +92 30 Cotulpa  | +92 3" P       | +96 4" P   | +96 28 Ent    |
| +92 39          | +92 82         | +96 65     | +96 18 Ent    |
| +71 3" P        | +71 4" P       | +53 5" P   | +45 7" P      |
| +71 66          | +71 81         | +53 35     | +45 89        |
| +46 MH          | +71 12" P      | +90 2" P   | +37 18 Oak    |
| +46 19          | +71 39         | +90 63     | +37 58        |
| +50 2" P        | +59 20 Cotulpa | +43 5" P   | +127 5" P     |
| +50 48          | +59 40         | +43 35     | +127 34       |
| +37 2" P        | +17 4" P       | +17 33     | +191 16 Oak   |
| +37 48          | +17 33         | +191 80    | +36 5" P      |
| +23 8 Cotulpa   | +30 18 Oak     | +85 12 Oak | +113 4" P     |
| +23 40          | +30 33         | +85 94     | +113 82       |
| +21 Quad 10 Oak | +113 4" P      | +96 12 Oak | +113 4" P     |
| +21 30          | +113 65        | +96 49     | +113 72       |
| +12 2 10 Ent    | +12 12x20 CM   | +93 1" P   | +07 20 Oak    |
| +12 C. Rock     | +12 21         | +93 37     | +07 52        |
| 46              | Bit            | 14         | 15            |
|                 |                |            | +07 5" P      |
|                 |                |            | +99 2 10 Ent  |
|                 |                |            | +99 C. Rock   |
|                 |                |            | +91 4" Oak    |
|                 |                |            | +91 51        |
|                 |                |            | +84 26 Oak    |
|                 |                |            | +77 4" Pine   |
|                 |                |            | +77 35        |
|                 |                |            | +69 18 Oak    |
|                 |                |            | +77 14 Elm    |
|                 |                |            | +77 36        |
|                 |                |            | +59 24 Oak    |
|                 |                |            | +55 2" M Ash  |
|                 |                |            | +55 34        |
|                 |                |            | +42 6" Pine   |
|                 |                |            | +42 98        |
|                 |                |            | +53 14 Elm    |
|                 |                |            | +42 24 Oak    |
|                 |                |            | +42 65        |
|                 |                |            | +16 14 Oak    |
|                 |                |            | +16 54        |
|                 |                |            | +25 14 Oak    |
|                 |                |            | +17 12 Elm    |
|                 |                |            | +17 99        |
|                 |                |            | +02 24 Oak    |
|                 |                |            | +02 81        |
| 45              | Bit            | 14         | 16            |
|                 |                |            | +03 4" Pine   |
|                 |                |            | +03 37        |
|                 |                |            | +99 12x15 CM  |
|                 |                |            | +99 21 Bit    |
|                 |                |            | +97 Light Hle |
|                 |                |            | +97 50        |
|                 |                |            | +85 2 11 Ent  |
|                 |                |            | +78 20 Oak    |
|                 |                |            | +92 14 Oak    |
|                 |                |            | +92 79        |
|                 |                |            | +85 2 8 Birch |
|                 |                |            | +85 76        |
|                 |                |            | +85 10 Birch  |
|                 |                |            | +85 57        |
|                 |                |            | +71 2 10 Ent  |
|                 |                |            | +71 C. Rock   |
|                 |                |            | +67 WSO       |
|                 |                |            | +67 34        |
|                 |                |            | +54 4" Pine   |
|                 |                |            | +54 42        |
|                 |                |            | +56 14 Oak    |
|                 |                |            | +56 53        |

August 5, 1965

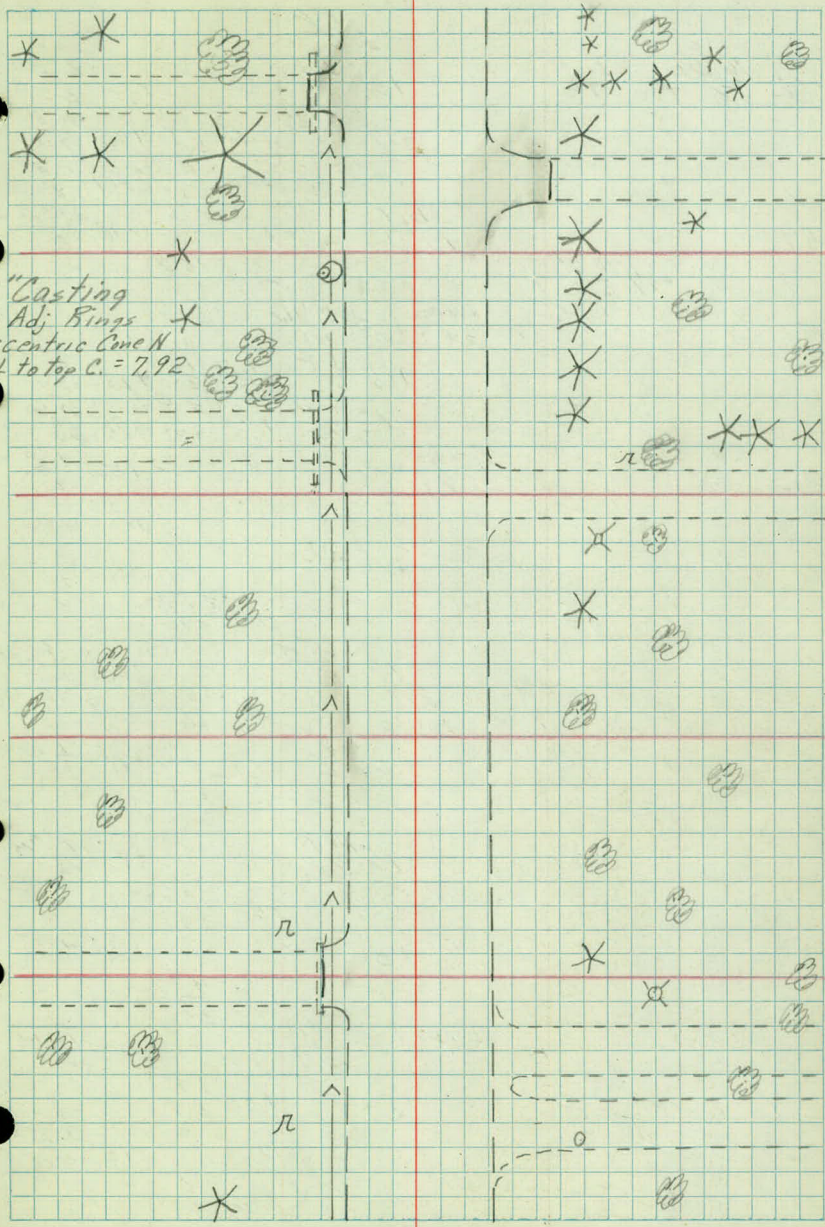
24

Lt.

£

Rt.

11 "Casting"  
No Adj. Rings  
Eccentric Cam N  
FL to top C. = 7.92



[illegible]



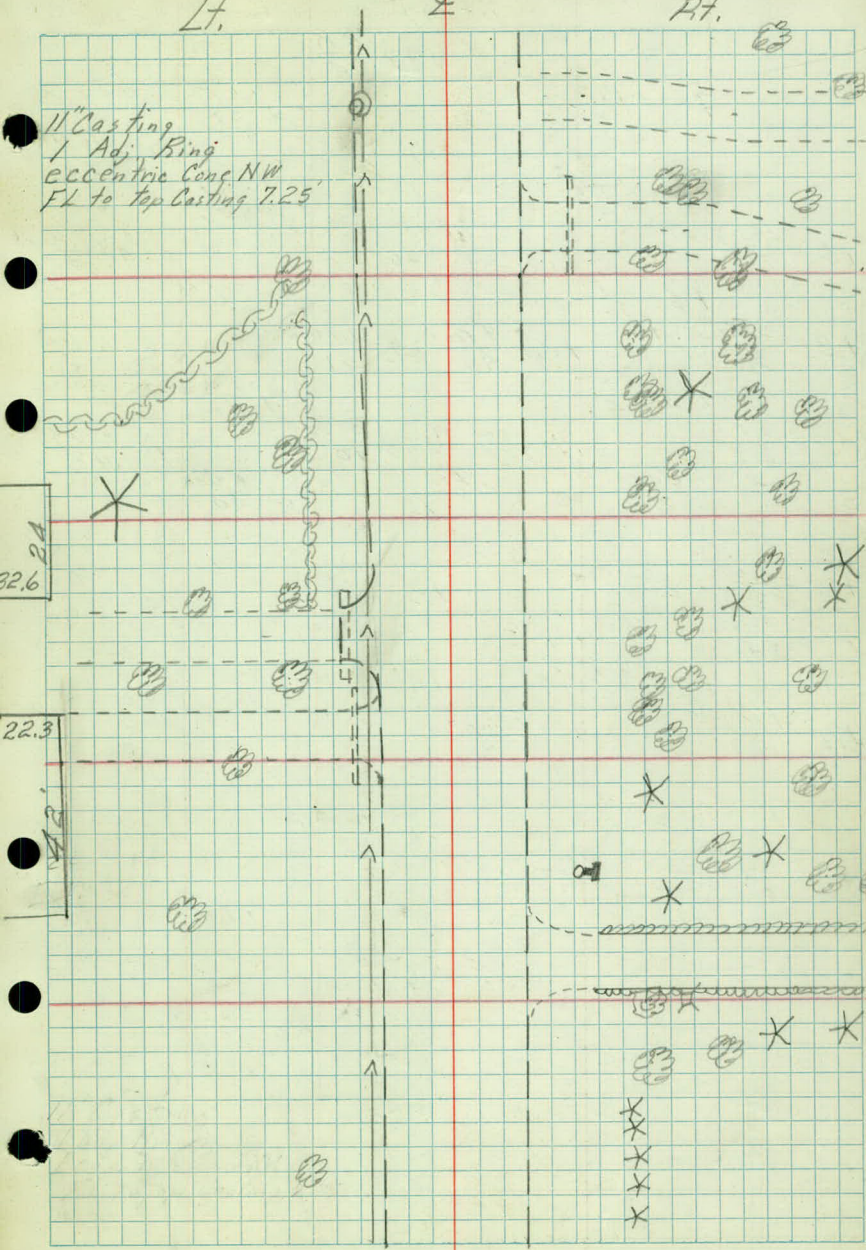
August 5, 1965 25  
 Lt. Rt.

11" Casting  
 1 Adj. Ring  
 eccentric Conc. NW  
 FL to Top Casting 7.25'

24  
 32.6

22.3

12



52

$$\frac{\text{Bit}}{23 \ 17}$$

$$+93 \frac{\text{BR}}{14}$$

$$+86 \frac{\text{MH}}{17}$$

$$+80 \frac{1''\text{P}}{51}$$

$$+78 \frac{2''\text{P}}{63}$$

$$+93 \frac{16''\text{O}}{74}$$

$$+82 \frac{1''\text{Pine}}{35}$$

$$+90 \frac{2''\text{P}}{56}$$

$$+66 \frac{\text{Pine Bush}}{57}$$

$$+73 \frac{6''\text{Ash}}{49}$$

$$+56 \frac{16''\text{Oak}}{49}$$

$$+84 \frac{18''\text{Oak}}{40}$$

$$+63 \frac{1''\text{P}}{34}$$

$$+58 \frac{14''\text{Oak}}{43}$$

$$+25 \frac{\text{S.W. Con Ho}}{56}$$

$$+44 \frac{3''\text{Pine}}{44}$$

$$+45 \frac{\text{Tw 6'' Oak}}{51}$$

$$+38 \frac{4''\text{Oak}}{47}$$

$$+22 \frac{33''\text{Oak}}{34}$$

$$+34 \frac{18''\text{Oak}}{41}$$

$$+20 \frac{\text{ER}}{23}$$

$$+11 \frac{\text{Curb}}{33}$$

$$+33 \frac{20''\text{Oak}}{40}$$

$$+18 \frac{16''\text{Oak}}{48}$$

$$51 \frac{\text{Conc}}{70}$$

$$\frac{\text{Bit}}{13}$$

$$+15 \frac{8''\text{Oak}}{44}$$

$$+93 \frac{6''\text{Oak}}{39}$$

$$+88 \frac{\text{Curb}}{33}$$

$$+88 \frac{\text{Car Conc}}{32}$$

$$+93 \frac{10''\text{Oak}}{34}$$

$$+93 \frac{12''\text{Oak}}{36}$$

$$+79 \frac{\pm 4' \text{ Conc Spillway}}{34}$$

$$+85 \frac{\pm \text{Spill}}{31}$$

$$+83 \frac{\text{Cor Rip Rap}}{35}$$

$$+70 \frac{A''\text{Maple}}{59}$$

$$+78 \frac{\text{Rip Rap}}{34}$$

$$+70 \frac{A''\text{Maple}}{44}$$

$$+50 \frac{\text{Tw 4'' BE}}{20}$$

$$+18 \frac{\pm 7' \text{ Spillway}}{\text{Bit } 32-22}$$

50

$$\frac{\text{Bit}}{20 \ 14}$$

$$+99 \frac{24''\text{Oak}}{58}$$

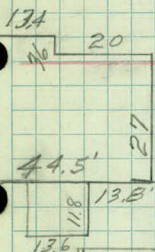
$$+64 \frac{6''\text{Oak}}{61}$$

$$+69 \frac{6''\text{Elm}}{35}$$

$$+55 \frac{4''\text{BE}}{34}$$

August 6, 1965

26



11' Casting  
25 Adj Rings  
eccentric Cone S  
FL to Top C = 9.0

\*

\*

\*

223

223  
223  
223  
223

223

223

223

223

223

223



14 - 2

Rt

+35 8" Ash  
45

+30 4" Ent  
33

+45 4" Mt. Ash  
43

+22 6" Maple  
68

+30 S.W. Cor Ho  
77

+18 X-Fe  
34

+13 4" Ent  
Ent

+14 PP  
28

+11 4" Ent  
70

54

+100 Pine Bush  
35

+17 B. L.  
15

+100 4" Ent  
45

+194 4" Ent  
31

+85 Cor Ho as  
32

+80 4" Ent  
69

+75 18" O  
40

+87 End Hed  
36

+72 14" Maple  
54

+93 10" Russian  
46 olive

+57 8" O  
58

+150 14" Elm  
46

+127 12" O  
42

+53 10" O  
54

+32 4" Walk  
64

+43 E. Walk  
22

+25 N.W. Cor. Ho  
69

+16 12" Elm  
46

+107 T. 12" O  
60

+10 12" BE  
70

+11 5" P  
60

+15 S.W. Cor. Ho  
73

+106 12" Oak  
32

+107 ER  
19

+104 Cor Lilac  
31

5.3

+100 ER  
19

+92 10" Maple  
79

+90 Cor Lilac  
46

+92 10" Maple  
53

+78 Pine Bush  
47

+87 S. End 15" Elm  
33

+93 18" Oak  
47

+75 PP  
60

+55.4 Mont.  
4

+85 Arc Lt  
29

+75 POR  
32

+69 BR  
54

+74 BR  
47

+84 POR  
29

+64 MH  
9

+54 MH  
2

+105 12" Elm  
58

+28 POR  
51

+30 ER  
79

+103 1" P  
35

+24 GV  
23

+35 ER  
61

+20 POR  
31

+106 PE  
29

+20 POR  
33

52

+105 BR  
23

+102 GV  
26

+102 H4  
28

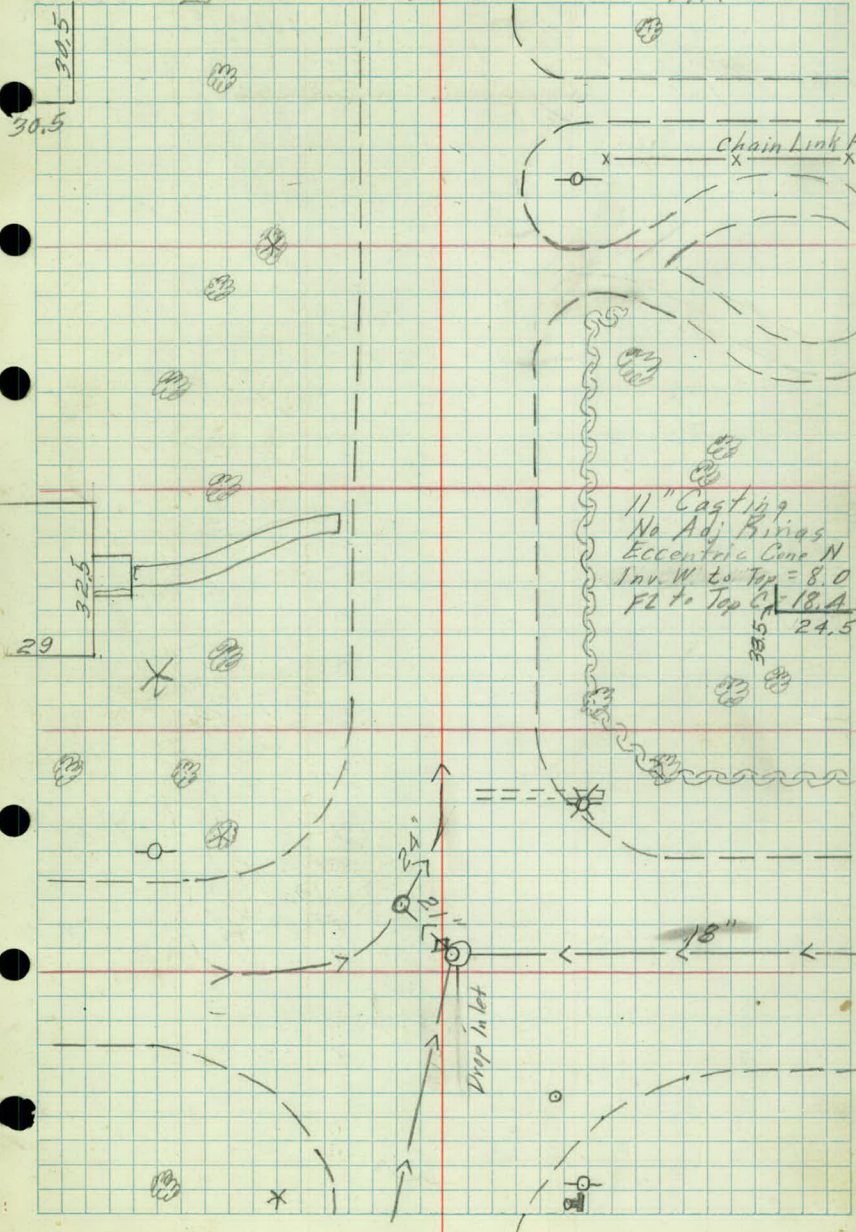
FK  
DS  
PK  
WJ

August 6, 1963  
Feb. 1, 1966

27

Lt.

Rt.



57

B.t.  
17 18

100 3"P  
30

+91 MH  
1

+99 28 BE  
43

+99 26 BE  
69

+97 S.W. Cor Ho  
102

+89 E Ent  
27

+79 PP  
24

+79 6 M  
44

+84 59

+79 16 LE  
59

+63 10 P  
83

+67 24 P  
90

+34 R. Tie  
Ent Lt.

+49 12 P  
80

+45 E Ent  
36

+46 14 M  
45

+44 24 P  
90

+15 3 P  
56

+26 10 Conc Ent  
40

+43 NW Cor Ho  
93

56

+12 3 Ash  
46

+17 14 Elm  
92

+35 6 P  
89

56

B.t.  
17 18

+17 12 M  
44

+77 S.W. Cor Ho  
80

+92 Trip Birch  
55

+91 Lilac Hedge  
28

+74 14 M  
45

+63 14 Maple  
77

+81 E Ent  
74 & 28

+66 Hyd  
29

+65 8 Elm  
66

+48 PP  
28

+48 E Ent  
29

+32 Willow  
54

+47 E Ent  
84

+38 12 M  
46

+12 12 M  
45

B.t.  
17 15

+11 14 Maple  
79

55

+91 S.W. Cor Ho  
74

+95 4 Mode  
56

+78 E Ent  
25

+92 Hedge  
34

+59 17 Ash  
45

+68 12 L. For  
72

+50 NW Cor Ho #842  
70 E 34.5  
N 26.5



65 + 1  
56 + 2  
38 .76  
27 .00

Feb. 1, 1966

28

E 22.3 W  
N 44.3 S

11" Casting  
4 Adj. Rings  
eccentric Cable  
Mighty Deep

9

X

#824  
E 26.2 W  
N 30.4 S

X

#825

34.5

24

#835  
24.3  
62.7

1-5-5  
34.5  
26.5

|                                 |                                   |                               |                                |                              |
|---------------------------------|-----------------------------------|-------------------------------|--------------------------------|------------------------------|
|                                 |                                   |                               | +32 $\frac{4 \text{ Ent}}{29}$ | +46 $\frac{3 \text{ P}}{55}$ |
|                                 |                                   | +20 $\frac{1 \text{ Fe}}{31}$ |                                | +20 $\frac{PP}{24}$          |
| +31 $\frac{10 \text{ Elm}}{76}$ | +46 $\frac{\text{Cor Hedge}}{37}$ |                               | +18 $\frac{16 \text{ M}}{61}$  |                              |
|                                 | +29 $\frac{\text{Pine}}{46}$      | +11 $\frac{8 \text{ P}}{67}$  |                                | +14 $\frac{1 \text{ P}}{48}$ |
| 59                              |                                   | Bit $\frac{16}{17}$           | +14 $\frac{1 \text{ P}}{33}$   |                              |

|                                   |                                           |                                   |                                    |                             |
|-----------------------------------|-------------------------------------------|-----------------------------------|------------------------------------|-----------------------------|
| +88 $\frac{\text{SW Cor Ho}}{81}$ |                                           |                                   |                                    |                             |
|                                   | +69 $\frac{4 \text{ Ent Conc } 8.5'}{37}$ |                                   | +76 $\frac{\text{NW Cor Ho}}{79}$  |                             |
|                                   |                                           | +72 $\frac{20 \text{ Elm}}{33}$   |                                    | +57 $\frac{\text{Ent}}{32}$ |
|                                   | +59 $\frac{PP}{31}$                       |                                   | +45 $\frac{\text{Hedge}}{34}$      |                             |
|                                   |                                           | +26 $\frac{10 \text{ Elm c}}{43}$ |                                    | +107 $\frac{PP}{24}$        |
| 58                                |                                           | Bit $\frac{18}{17}$               | +100 $\frac{\text{NW Cor Ho}}{79}$ |                             |

|                                    |                                |                                        |                                   |                                 |
|------------------------------------|--------------------------------|----------------------------------------|-----------------------------------|---------------------------------|
|                                    |                                |                                        | +86 $\frac{5 \text{ P}}{42}$      |                                 |
|                                    |                                | +77 $\frac{4 \text{ Ent}}{\text{Bit}}$ |                                   | +67 $\frac{5 \text{ Ash}}{65}$  |
|                                    |                                |                                        | +66 $\frac{4 \text{ P}}{78}$      |                                 |
|                                    |                                | +62 $\frac{12 \text{ O}}{31}$          |                                   | +59 $\frac{4 \text{ P}}{54}$    |
|                                    | +68 $\frac{4 \text{ Ent}}{30}$ |                                        | +59 $\frac{2 \text{ P}}{40}$      |                                 |
| +58 $\frac{10 \text{ Ash}}{53}$    | +59 $\frac{12 \text{ O}}{45}$  | +34 $\frac{10 \text{ O}}{31}$          |                                   | Post $\frac{29 \times 3.2}{25}$ |
|                                    | +57 $\frac{12 \text{ M}}{83}$  |                                        | +19 $\frac{\text{NW Cor Ho}}{80}$ |                                 |
| +108 $\frac{\text{Flag Pole}}{64}$ | +31 $\frac{24 \text{ BE}}{78}$ | +10 $\frac{4 \text{ Ent}}{28}$         |                                   | +18 $\frac{\text{G. Post}}{28}$ |
| 57                                 | +04 $\frac{PP}{23}$            |                                        | +102 $\frac{\text{G. Post}}{27}$  |                                 |

Feb. 1, 1966

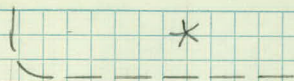
29



13

\*

E 30.2 W  
N 26.4 S

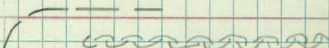


\*



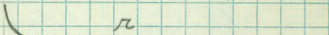
13

E 28.3 W  
N 35.4 S



13

E 36.4 W  
N 32.2 S



13

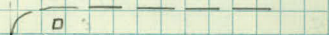
\*

\*

13

\*

N 24.5 S  
E 38.5 W





62

Bit  
16-18+96 10"P  
40+97 Wall  
38+91 Yard Lite  
35+85 PP  
35+45 SW Cor Ho  
89+75 4"P  
40+91 16"CE  
53+29 10"P  
47+59 PP  
28+27 10"P  
41+50 N.W. Cor Ho  
81+32 MH  
1+50 1"P  
41+21 4"Ent  
34+29 Hedge  
33

61

Bit  
18 18+10 4"P  
59+99 Cor Hedge  
34+99 18"Elm  
76+94 2"P  
37+58 5"M  
36+71 2"P  
51+83 6"M  
37+97 12"Elm  
41+47 4"Conc Ent  
34+41 SW Cor Ho  
81+78 14"Elm  
41+36 B.Hedge  
35+29 12"Elm  
49+38 1"P  
38+60 NW Cor Ho  
70+29 Hyd  
29+29 14"Elm  
76+40 PP  
23+57 8"Elm  
42+28 X Fe  
34+18 4"Conc Ent  
34+38 12"Elm  
41

60

+27 PP  
33Bit  
17 19+98 Hedge  
33+83 4"P  
69+69 SW Cor Ho  
82 #795+84 2"P  
56+52 6"CE  
60+55 4"M  
42+83 6"Elm  
42

30

E 26.2W  
N 34.2S

11" Casting  
4 Adj. Rings  
eccentric Cone  
Deep X.V

N 42.8 S  
E 36.3 W

27  
2-5-18  
45

E 27 W  
N 45 S

#795

E 32 W  
N 31.3 S

+39  $\frac{2^{\circ} \text{Eh}}{39}$

+37  $\frac{\text{Hyd}}{28}$

+15  $\frac{\text{Wall}}{33}$

+16  $\frac{\text{Wall}}{33}$

+59  $\frac{\text{S.W. Cor Ho}}{81}$

+22  $\frac{3^{\circ} \text{P}}{68}$

+22  $\frac{4^{\circ} \text{P}}{41}$

+10  $\frac{\text{R Tie}}{\text{Ent}}$

+107  $\frac{\text{Ent}}{31}$

+92  $\frac{8^{\circ} \text{P}}{39}$

+62  $\frac{\text{S.W. Cor Ho}}{79}$

+35  $\frac{6^{\circ} \text{P}}{39}$

+12  $\frac{\text{Ent}}{31}$

+12  $\frac{\text{Ent}}{31}$

+42  $\frac{3^{\circ} \text{P}}{47}$

+20  $\frac{\text{PP Arch'd}}{28}$

+60  $\frac{2^{\circ} \text{M}}{53}$

+57  $\frac{\text{BR}}{20}$

+39  $\frac{2^{\circ} \text{Birch}}{41}$

+18-18  $\frac{\text{B.T.}}{18-18}$

+25  $\frac{10^{\circ} \text{Ash}}{58}$

+25  $\frac{\text{N.W. Cor. Ho}}{82}$

+25  $\frac{\text{Ent}}{82}$

+25  $\frac{\text{Ent}}{82}$

+25  $\frac{\text{Ent}}{82}$

+25  $\frac{\text{Ent}}{82}$

+25  $\frac{\text{Ent}}{82}$

+30  $\frac{3^{\circ} \text{P}}{47}$

+29  $\frac{\text{ER}}{18}$

+109  $\frac{\text{BR}}{45}$

+85  $\frac{\text{ER}}{51}$

+107  $\frac{\text{PP}}{28}$

+74  $\frac{\text{Hedge}}{34}$

+53  $\frac{4^{\circ} \text{M}}{58}$

+25  $\frac{\text{N.W. Cor. Ho}}{82}$

+25  $\frac{\text{Ent}}{82}$

+25  $\frac{\text{Ent}}{82}$

+25  $\frac{\text{Ent}}{82}$

+25  $\frac{\text{Ent}}{82}$

+25  $\frac{\text{Ent}}{82}$

64

+90  $\frac{1^{\circ} \text{M}}{41}$

+10  $\frac{\text{R Tie}}{\text{Ent}}$

+22  $\frac{4^{\circ} \text{P}}{59}$

+10  $\frac{\text{R Tie}}{\text{Ent}}$

+10  $\frac{\text{R Tie}}{\text{Ent}}$

+10  $\frac{\text{R Tie}}{\text{Ent}}$

+10  $\frac{\text{R Tie}}{\text{Ent}}$

+10  $\frac{\text{R Tie}}{\text{Ent}}$

+10  $\frac{\text{R Tie}}{\text{Ent}}$

+10  $\frac{\text{R Tie}}{\text{Ent}}$

+10  $\frac{\text{R Tie}}{\text{Ent}}$

63

+10  $\frac{\text{R Tie}}{\text{Ent}}$

+10  $\frac{\text{R Tie}}{\text{Ent}}$

+10  $\frac{\text{R Tie}}{\text{Ent}}$

+10  $\frac{\text{R Tie}}{\text{Ent}}$

+10  $\frac{\text{R Tie}}{\text{Ent}}$

+10  $\frac{\text{R Tie}}{\text{Ent}}$

+10  $\frac{\text{R Tie}}{\text{Ent}}$

62

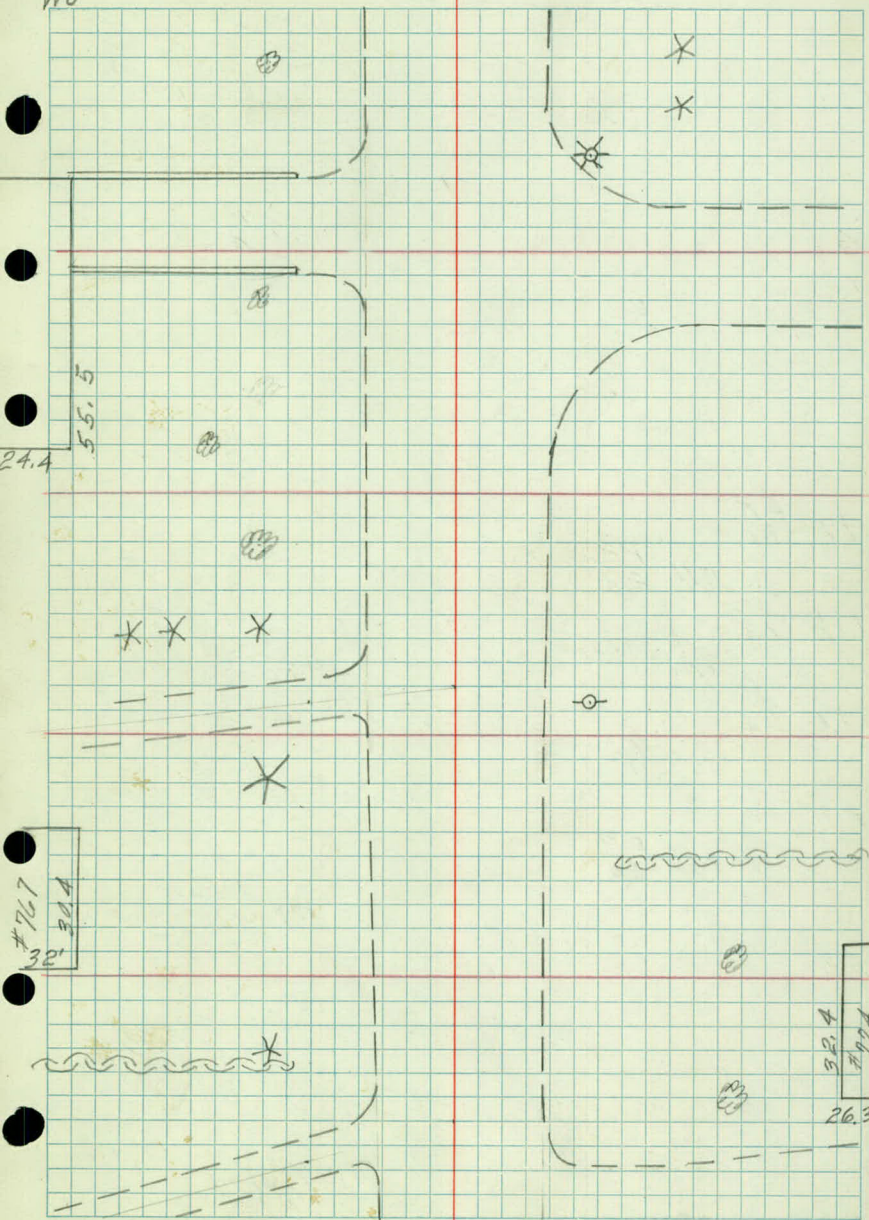
+10  $\frac{\text{R Tie}}{\text{Ent}}$



FK  
Ds  
PK  
WJ

Feb. 2, 1966

31



67

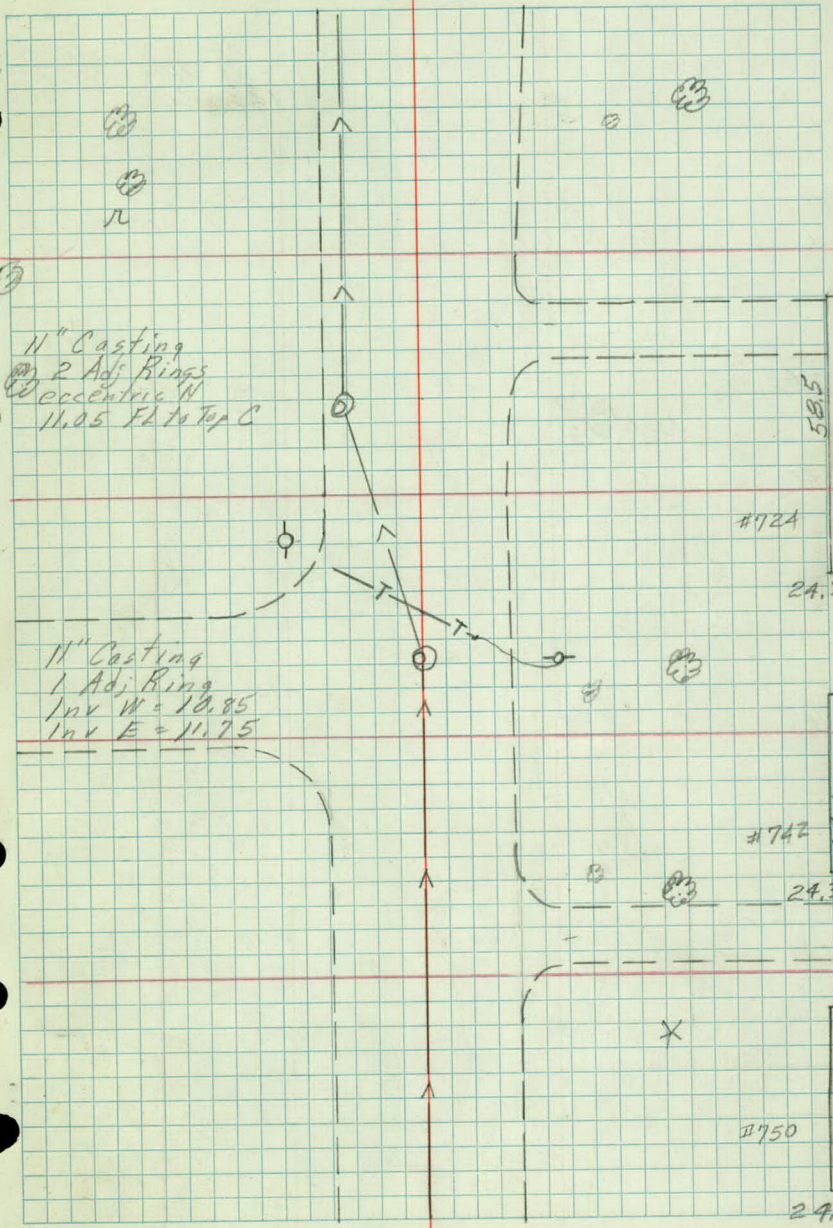
B.T.  
20 18+84  $\frac{Tn 18^0}{92}$ +87  $\frac{NW Cor Ho}{110+}$ +77  $\frac{18^0}{62}$ +82  $\frac{14^0 Lh}{58}$ +65  $\frac{12^0}{59}$ +77  $\frac{Rose Bush}{41}$ +58  $\frac{5TP}{63}$ +47  $\frac{20^0}{87}$ +18  $\frac{MH}{17}$ +35  $\frac{2^0 Lh}{26}$ +24  $\frac{16^0}{83}$ B.T.  
20 18+93  $\frac{ER}{20}$ +91  $\frac{PP}{28}$ +83  $\frac{NW Cor Ho}{86}$ +85  $\frac{T cable}{18}$ +66  $\frac{PP}{28}$ +75  $\frac{T cable}{Xing}$ +64  $\frac{6^0 CE}{55}$ +75  $\frac{BR}{44}$ +59  $\frac{Bush}{35}$ +70  $\frac{T cable}{12}$ +67  $\frac{MH}{1}$ +48  $\frac{ER}{39}$ +21  $\frac{NW Cor Ho}{85}$ +29  $\frac{BR}{20}$ +21  $\frac{Bush}{35}$ +17  $\frac{6^0 CE}{53}$ +08  $\frac{2^0 Lh}{27}$ 

65

B.T.  
19 20+88  $\frac{3^0 P}{51}$ +55  $\frac{NW Cor Ho}{84}$

Feb. 2, 1966

32





+23  $\frac{PP}{26}$

69

$\frac{B.T.}{17 \ 17}$

+63  $\frac{18''0}{43}$

+69  $\frac{3-8''BE}{44}$

+57  $\frac{18''0}{46}$

+70  $\frac{4''BE}{43}$

+51  $\frac{Cor. B.S.}{85}$

+53  $\frac{10''BE}{42}$

+36  $\frac{Cor. B.S.}{99}$

+44  $\frac{PP}{26}$

+35  $\frac{14''0}{43}$

+27  $\frac{12''0}{40}$

+13  $\frac{8''0}{40}$

+00  $\frac{10''BE}{51}$

+06  $\frac{16''BE}{40}$

68

+00  $\frac{Tw 12''BE}{39}$

$\frac{B.T.}{17 \ 18}$

+

+95  $\frac{STP}{39}$

+94  $\frac{16''BE}{41}$

+85  $\frac{Tw 12''0}{74}$

+93  $\frac{Trip 10''0}{52}$

+76  $\frac{Trip 12''BE}{35}$

+81  $\frac{12''BE}{43}$

+44  $\frac{EE 12''x25' CM 12+55 79}{14''0}$

+68  $\frac{16''BE}{33}$

+35  $\frac{E 8''CN}{44}$

+34  $\frac{14''0}{47}$

+38  $\frac{14''BE}{38}$

+17  $\frac{8''0}{44}$

+19  $\frac{WE 12''CM}{24}$

+28  $\frac{E Ent}{23}$

+32  $\frac{26''CE}{52}$

+41  $\frac{EFC}{36}$

+12  $\frac{16''0}{44}$

+33  $\frac{10''E}{36}$

+05  $\frac{10''0}{84}$

+09  $\frac{6''0}{42}$

+20  $\frac{E Ent}{23}$

+12''x22''CM

+28  $\frac{BFC}{35}$

67

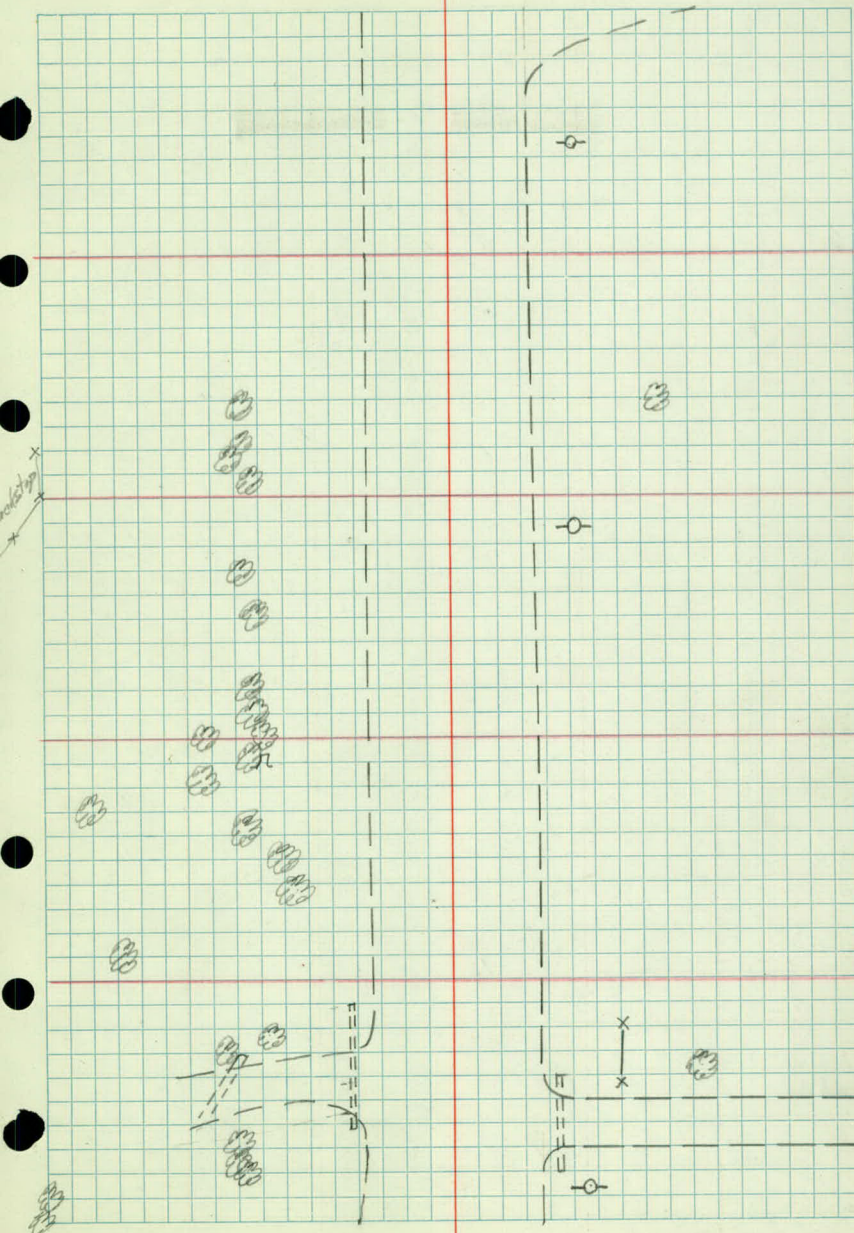
+00  $\frac{14''0}{85}$

+07  $\frac{PP}{28}$

Feb. 2, 1966

33

rocket stop



72

$$\begin{array}{r} \text{Road} \\ 15 \quad 17 \end{array}$$

$$+86 \quad \begin{array}{r} \text{Iron} \\ 34 \end{array}$$

$$+55 \quad \begin{array}{r} \text{Begin} \\ \text{Lowland} \end{array}$$

$$+27 \quad \begin{array}{r} \text{PP} \\ 26 \end{array}$$

71

$$\begin{array}{r} \text{Gutter} \\ 15 \quad 18 \end{array}$$

$$+02 \quad \begin{array}{r} \text{Hyd} \\ 27 \end{array}$$

70

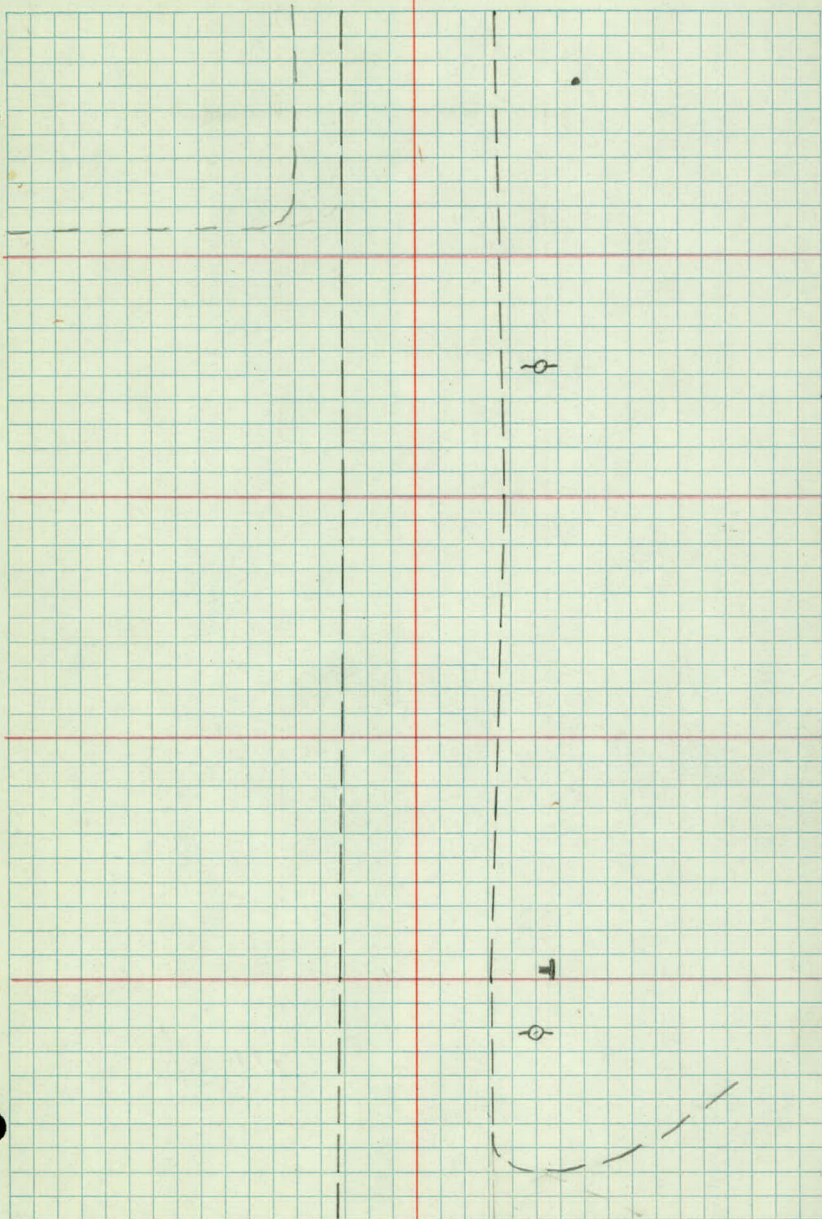
$$\begin{array}{r} \text{Gutter} \\ 16 \quad 16 \end{array}$$

$$+89 \quad \begin{array}{r} \text{PP} \\ 25 \end{array}$$

$$+53 \quad \begin{array}{r} \text{Large} \\ \text{Ent} \end{array}$$



Feb 2, 1966 34



+44

+26

10 Trees  
65

74

Road  
15 18

+90 PP  
27

+90

+66

14 Trees  
63

73

Road  
15 17

+17 Begin Swamp  
BT

+61 PP  
27

+35 Begin Swamp  
BT

+34 Ent  
BT

72

Feb. 2, 1966

35

SWAMP

SWAMP

SWAMP

0

0



77

$$\frac{\text{Road}}{16 \ 18}$$

+80 End Smp

+71

$$\frac{6-4 \text{ " Willow}}{40}$$

+51

$$+48 \frac{PP}{28}$$

X-Culvert Burried

+27 Spillway B. F

+04 Bit Spillway

25-15

76

$$\frac{\text{Road}}{15 \ 17}$$

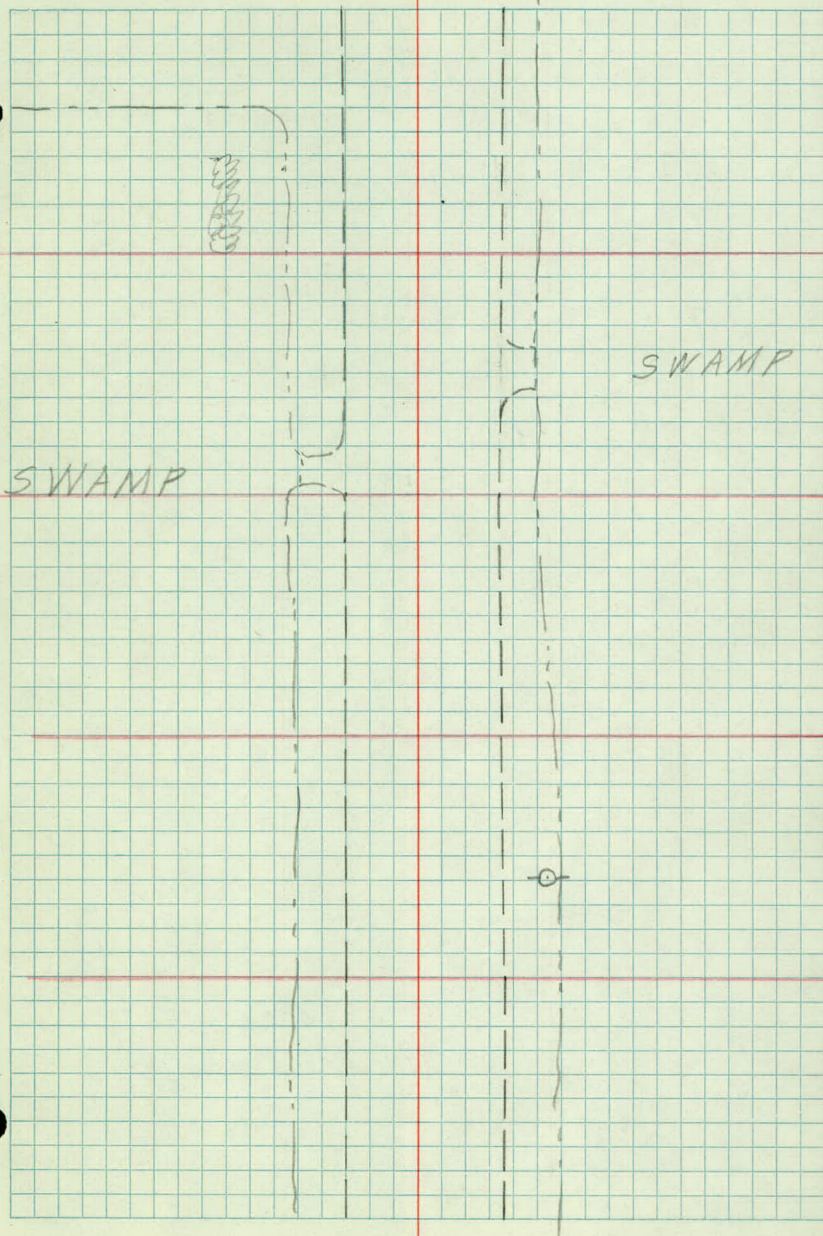
$$+21 \frac{PP}{27}$$

75

$$\frac{\text{Road}}{15 \ 18}$$

Feb 2, 1966

36



79

+54  $\frac{GV}{33}$

+51  $\frac{ER}{44}$

+48  $\frac{PP}{46}$

+51  $\frac{ER}{35}$

+48  $\frac{PP}{28}$

+40  $\frac{BR}{22}$

+30  $\frac{B.Conc Curb}{22}$  B-R

+30  $\frac{B.Conc Curb}{22}$

78

$\frac{Curb}{21}$  21

+51  $\frac{PP}{28}$

+44  $\frac{Curb}{21}$

+38  $\frac{B.Curb}{17}$

+32  $\frac{B.Curb Bit}{18}$

+15 End Swp  
Rt

+15 End Lowland

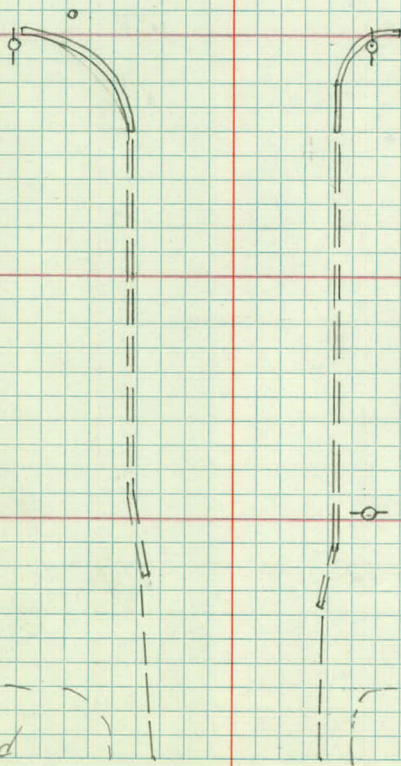
77

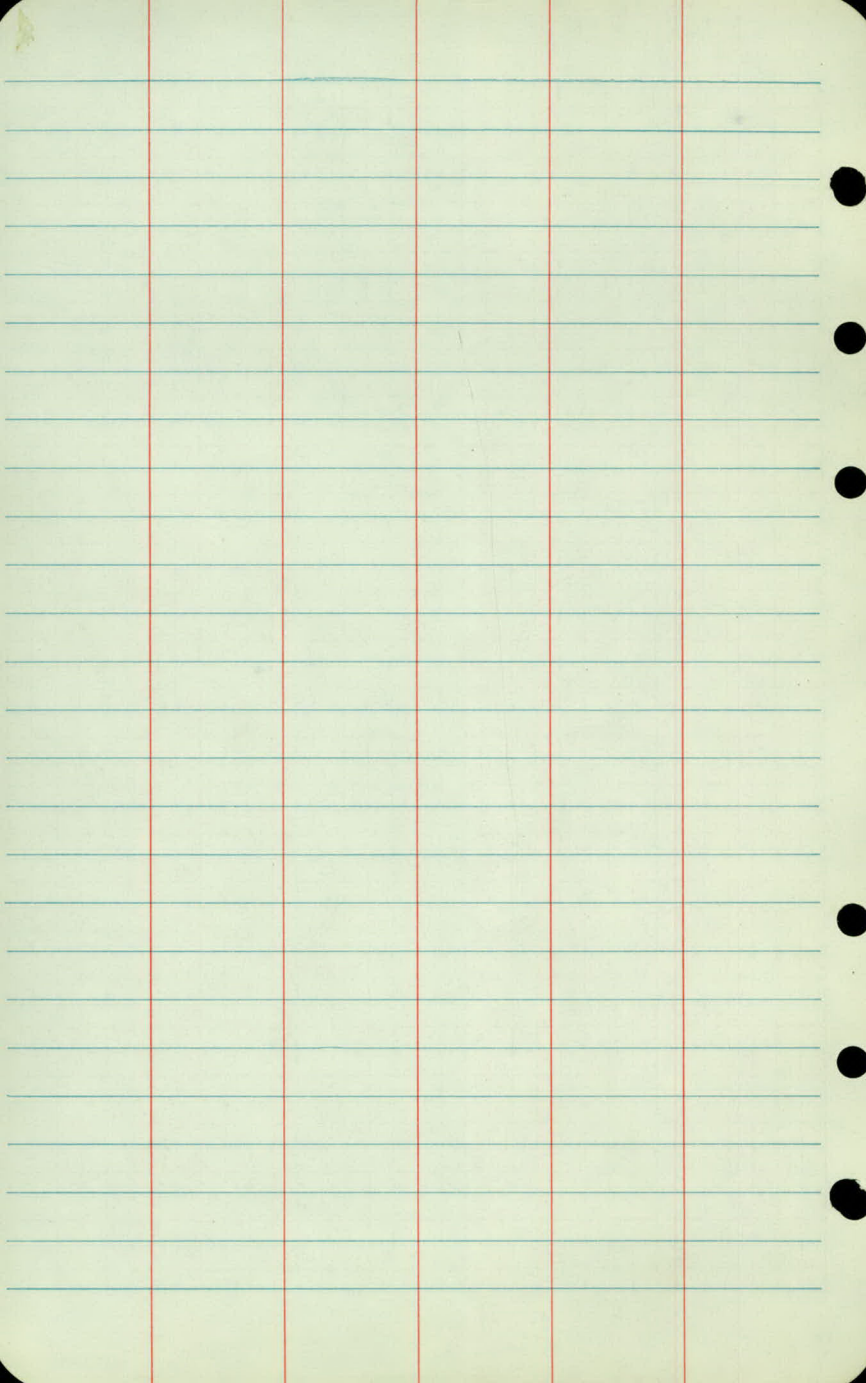


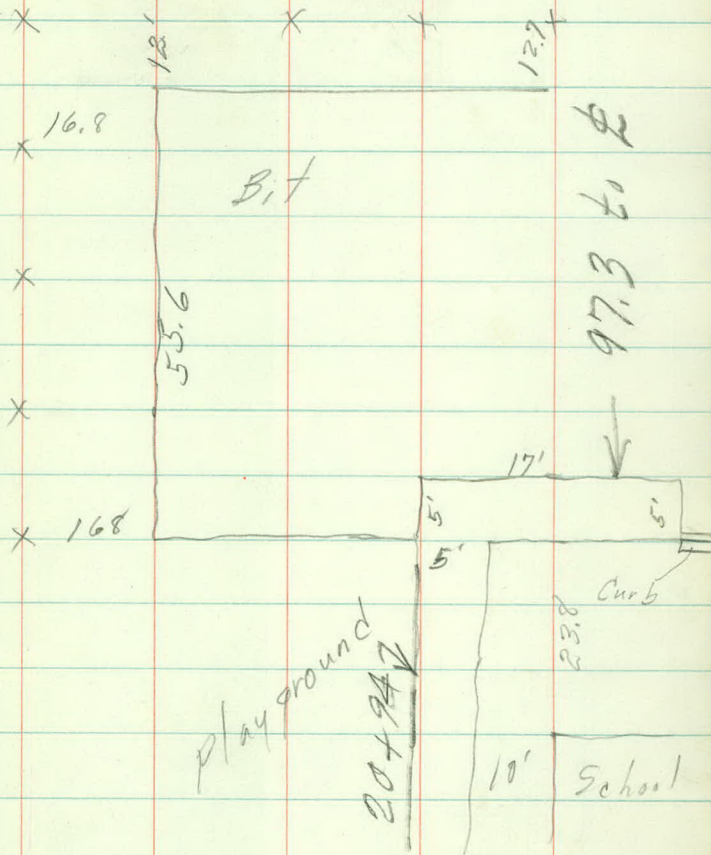
Feb. 2, 1966

37

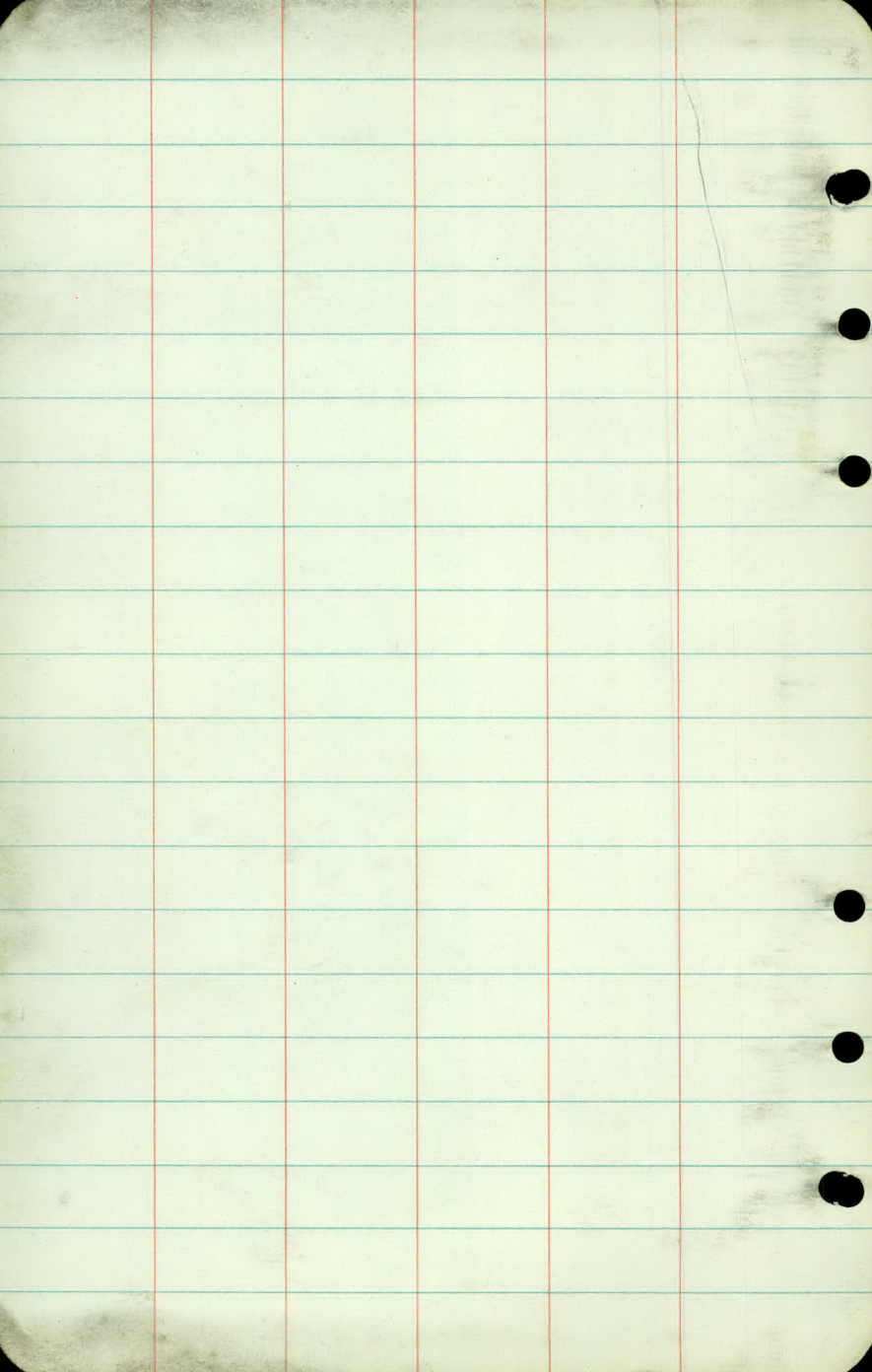
DALE ST.











26+56 B+A3' CB

Inv to top 3.84

12" SCP N

5 Adj Rings

10" Casting w Carb

24" Pre Cast

26+79 CB 20' Rt

Inv to Top 2.92

2 Adj Rings

Block Const

10" Casting w Carb

26+56 MH  $\Phi$ 7" Casting With  
30" Opening

4 Adj Rings

Mex Hat

Inv to Top 6.24

21" West

" " " 5.0

12" N

" " " 5.0

12" NE

" " " 5.1

12" SE

" A " 4.6

12" S

48" Pre Cast

26+79 CB 20' Lt

Inv to top 4.52

7 Adj Rings

10" Casting - Carb inl

24" Pre Cast

26+56 CB Lt 46'

Inv to top - 4.89

5 Adj Rings

10" Casting Carb inl

24" Pre Cast

25+85 CB 21' Rt 5 Adj Rings  
Inv to Top N- 5.04  
11" Casting  
Short Pre cast Cone

25+84 SD 23' Lt 2 Adj Rings  
Max Hat - 48" Pre Cast  
Inv to top 6.25 - 24" N. W.  
" " " 5.75 21" S. E.  
" " " 5.25 - 12" S.  
" " " 4.5 12" E. N. E.  
7" Casting

26+13 CB 40' Lt Inv to Top = 4.26  
24" Pre Cast  
5 Adj Rings  
10" Casting side Inlet

26+13 CB 50' Rt Inv to top = 3.9  
10" Casting  
24" Pre Cast  
4 Adj Rings



HAMLIN AVE.

12

£

+81 ERC  
50

+68 Hyd  
46

+54 B.R.C  
25

+52 Arc. Lite  
28

+41 MH  
13

+30 Gas GV  
14

+13 Serv sta  
78

+05 Lite Pole  
34

1

23

+65 S.W. Cor Serv. Sta  
81

22

+37 Lite Pole  
34

+35 G Rail  
27

+34 Cor. Bit  
18

+34 PP  
28

+34 PP  
27

+15 Cor Hedge  
43

0

Hedge Bit  
43 21 18

Conc.

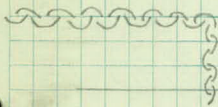
CO.

RD

"B"



B<sup>1</sup>





2

4

18 25

+50  $\frac{G. Rail}{45}$  →

+53  $\frac{Cor B. t}{18}$  28

+51  $\frac{Sign}{45}$

+73  $\frac{£ 10' Conc Ent}{43}$  Walk

3

+97  $\frac{S.E. Pump Island (13)}{65}$  34

+10  $\frac{SW Cor Library}{73}$

+96  $\frac{Sign}{50-67}$

+48  $\frac{PCC}{24}$

+63  $\frac{NSP M.H.}{12}$

+54  $\frac{EC}{29}$  35

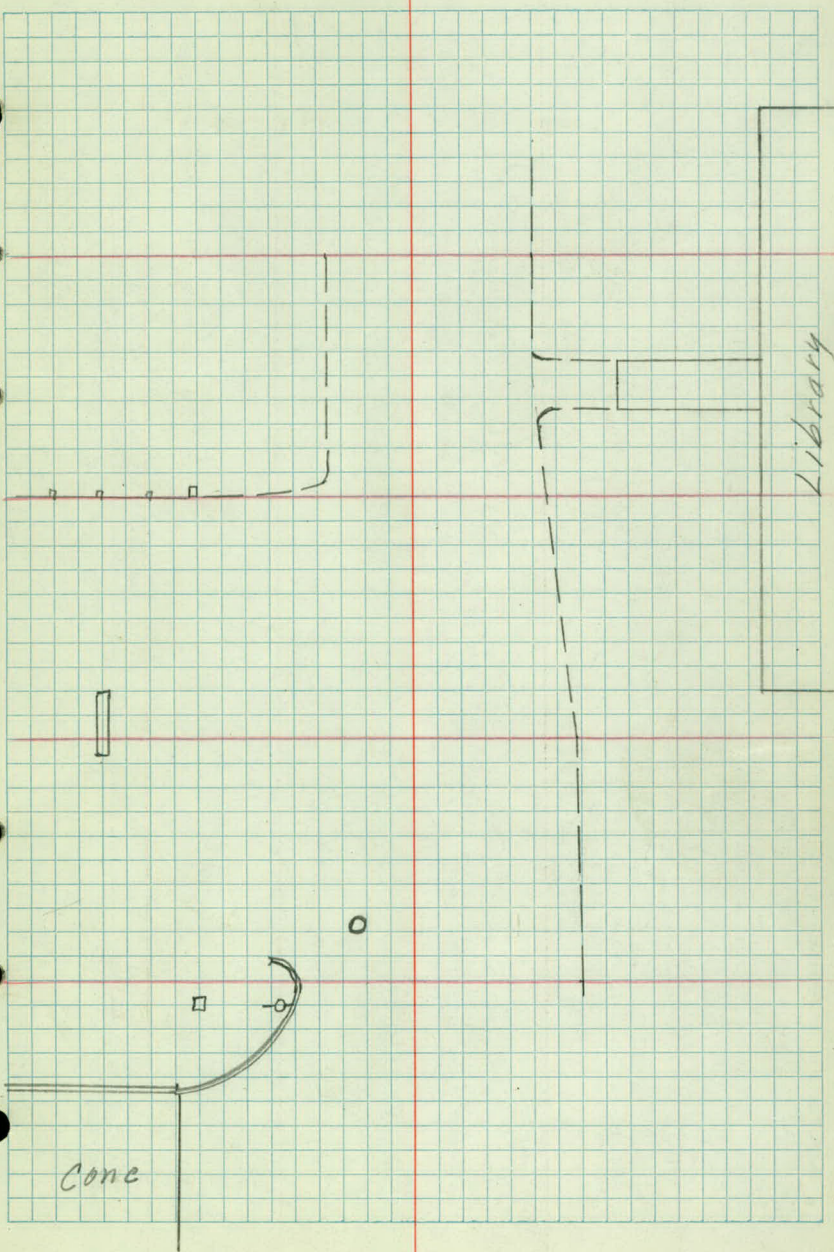
+45  $\frac{Sign}{45}$

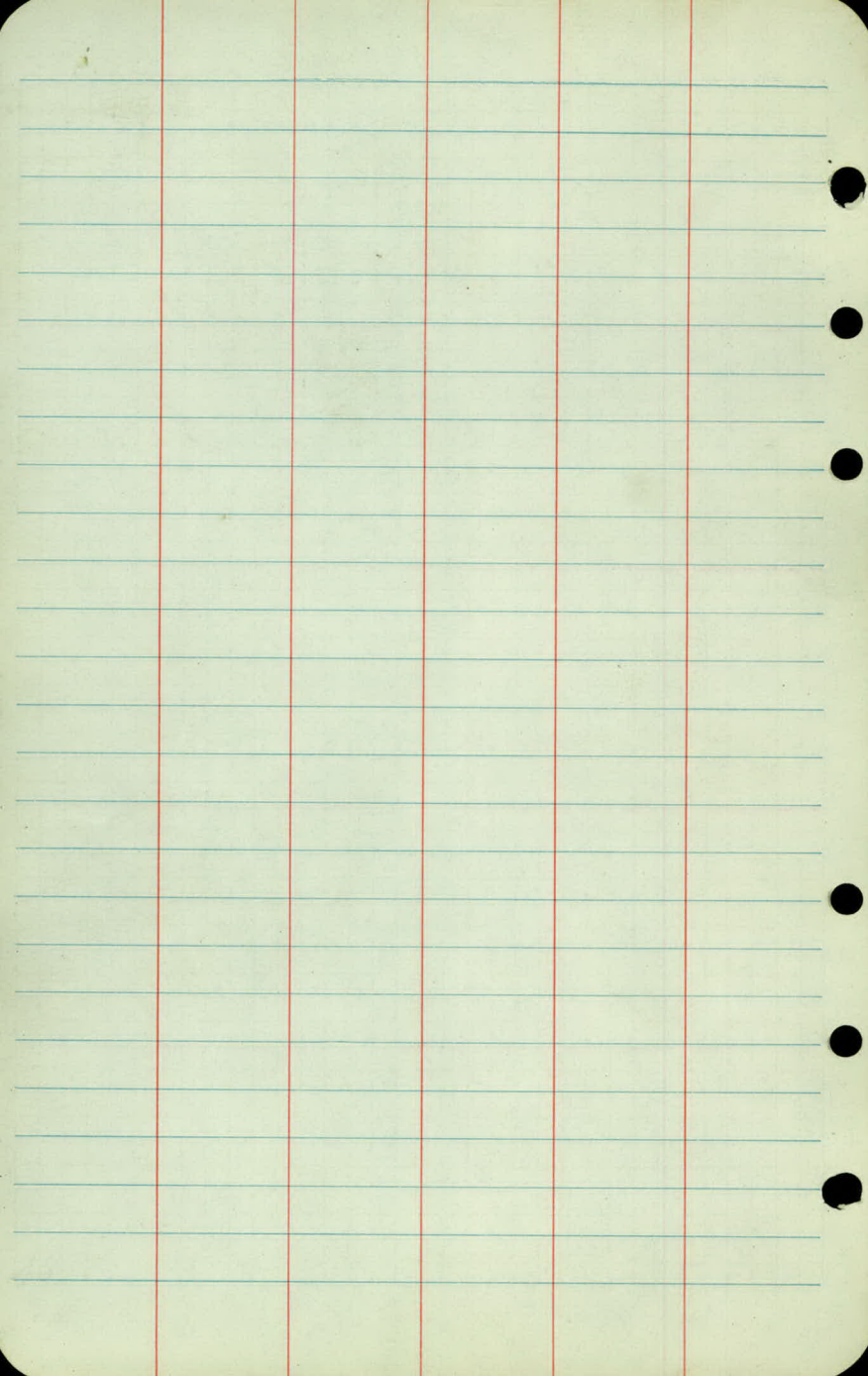
+45  $\frac{PP}{28}$

+29  $\frac{BRC}{50}$

2

Library







Oct. 25, 1965

1

Hamline Ave  
Eldridge to Burke

House Locations

51

50

+15 S.E. Cor. A.H. Garage  
+ House 53.5

49

+67 S.E. Cor. Ho  
86.4

48

+35 S.E. Cor. Ho  
84.3

47

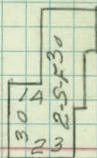
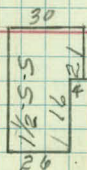
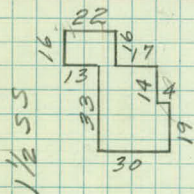
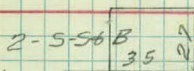
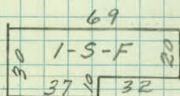
+02 N.E. Cor. H  
84

+96 S.W. Cor. Ho  
112.6

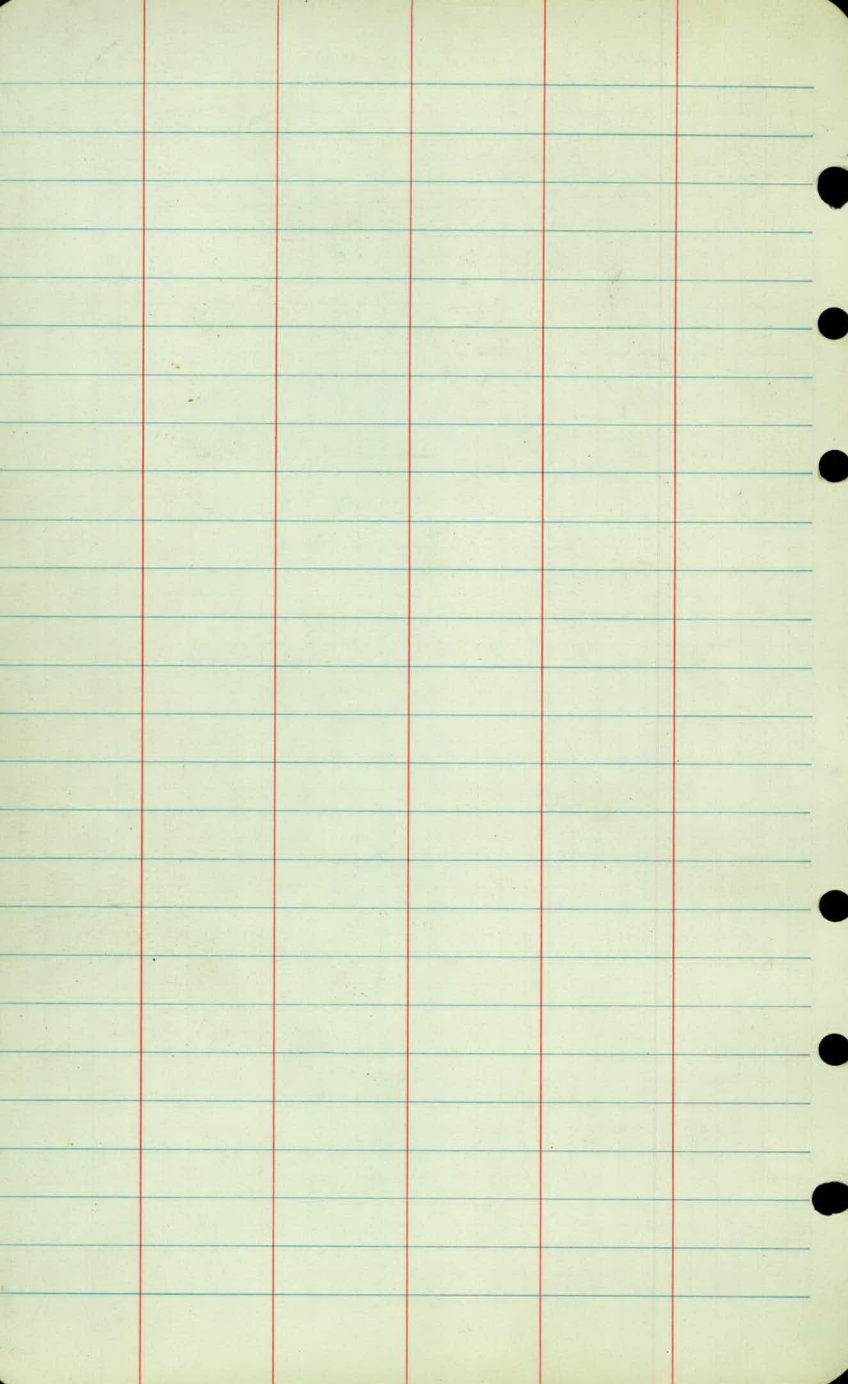
46

Oct. 25, 1965

2







199 SE Cor B + Hartline  
SW. Cor Base Pure oil  
Sign 955.620

106 SE Cor DeHwood + B  
Mont 956.981

203 NW Cor Fernwood + B  
SE Cor Top Landing H.  
#1225 El = 957.895

107 N.W. Cor Lex + Sandhurst  
El 947.415 Mont,

32 S. Side B. by H. #982  
El 941.860

31 SE Cor Gro H. + B  
El 923.950

65 Chev Blue Wagon



x-Sections

PCC. 10-4-65

K.A.

| Sta | + | $\pi$ | - | Elev. |
|-----|---|-------|---|-------|
|-----|---|-------|---|-------|

|    |      |        |  |  |
|----|------|--------|--|--|
| BM | 4.07 | 959.69 |  |  |
|----|------|--------|--|--|

|  |  |  |  |         |
|--|--|--|--|---------|
|  |  |  |  | 955.620 |
|--|--|--|--|---------|

|      |  |  |  |  |
|------|--|--|--|--|
| -200 |  |  |  |  |
|------|--|--|--|--|

|  |  |  |      |  |
|--|--|--|------|--|
|  |  |  | 7.80 |  |
|--|--|--|------|--|

|      |  |  |  |  |
|------|--|--|--|--|
| -175 |  |  |  |  |
|------|--|--|--|--|

|  |  |  |      |  |
|--|--|--|------|--|
|  |  |  | 7.06 |  |
|--|--|--|------|--|

|      |  |  |  |  |
|------|--|--|--|--|
| -150 |  |  |  |  |
|------|--|--|--|--|

|  |  |  |      |  |
|--|--|--|------|--|
|  |  |  | 6.40 |  |
|--|--|--|------|--|

|      |  |  |  |  |
|------|--|--|--|--|
| -125 |  |  |  |  |
|------|--|--|--|--|

Sec Line

|  |  |  |      |  |
|--|--|--|------|--|
|  |  |  | 5.71 |  |
|--|--|--|------|--|

|      |  |  |  |  |
|------|--|--|--|--|
| -100 |  |  |  |  |
|------|--|--|--|--|

|  |  |  |      |  |
|--|--|--|------|--|
|  |  |  | 5.16 |  |
|--|--|--|------|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| -75 |  |  |  |  |
|-----|--|--|--|--|

|  |  |  |      |  |
|--|--|--|------|--|
|  |  |  | 4.79 |  |
|--|--|--|------|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| -50 |  |  |  |  |
|-----|--|--|--|--|

|  |  |  |      |  |
|--|--|--|------|--|
|  |  |  | 4.53 |  |
|--|--|--|------|--|

|       |  |  |  |  |
|-------|--|--|--|--|
| -49.5 |  |  |  |  |
|-------|--|--|--|--|

✓

|     |  |  |  |  |
|-----|--|--|--|--|
| -24 |  |  |  |  |
|-----|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| -12 |  |  |  |  |
|-----|--|--|--|--|

|    |  |  |  |  |
|----|--|--|--|--|
| BM |  |  |  |  |
|----|--|--|--|--|

|  |  |  |      |        |
|--|--|--|------|--------|
|  |  |  | 1.50 | 958.19 |
|--|--|--|------|--------|

FX  
LPD  
RP  
HL

11

8-20-65  
Cool Clear 65°  
RT

29

B<sub>4</sub>

Top S.W. Cor. Base Pure oil Sign S.E. Cos Hamlin

+

|      |      |       |       |       |       |      |      |
|------|------|-------|-------|-------|-------|------|------|
| 55.7 | 55.4 | 55.04 | 55.17 | 55.16 | 55.04 | 55.1 | 55.6 |
| 4.0  | 4.30 | 4.65  | 4.52  | 4.53  | 4.65  | 4.20 | 4.1  |
| 37   | 27   | 26    | 4     |       | 17    | 18   | 37   |
|      | C    | G     |       |       | G     | C    |      |

|      |      |      |      |
|------|------|------|------|
| 55.6 | 55.6 | 55.6 | 55.4 |
| 4.1  | 4.1  | 4.1  | 4.3  |
| 41   | 43   | 50   | 50   |

|       |      |      |      |      |      |      |      |      |       |
|-------|------|------|------|------|------|------|------|------|-------|
| 55.65 | 55.1 | 55.1 | 55.3 | 55.6 | 55.6 | 55.5 | 55.4 | 55.4 | 55.23 |
| 4.04  | 4.6  | 4.6  | 4.4  | 4.1  | 4.1  | 4.2  | 4.3  | 4.3  | 3.76  |
| C     | G    | 35   | 22   | 4    |      | 15   | 25   | G    | C     |
| 50    |      |      |      |      |      |      |      | 44   | 50    |

|       |      |      |      |      |      |      |      |
|-------|------|------|------|------|------|------|------|
| 55.26 | 55.2 | 55.3 | 55.4 | 55.6 | 55.6 | 55.6 | 55.9 |
| 4.43  | 4.5  | 4.4  | 4.3  | 4.1  | 4.1  | 4.1  | 3.8  |
| NSPMH | 50   | 33   | 15   |      | 13   | 31   | 50   |
| 62    |      |      |      |      |      |      |      |

Top Hyd S.W. Cor. Hamline & "B"



Sta +  $\pi$  - Elev.

95969

0+00  $\neq$  Hamline

✓

+14

+29

+35

+65

8-20-65

21

2

51

30

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 55.6 | 55.5 | 55.6 | 55.5 | 55.6 | 55.7 | 55.9 | 56.1 | 56.2 | 57.8 |
| 4.1  | 4.2  | 4.2  | 4.2  | 4.1  | 4.0  | 3.8  | 3.6  | 2.8  | 1.9  |
| 100  | 71   | 50   | 37   | 17   |      | 23   | 50   | 100  | 150  |

|      |      |      |      |      |
|------|------|------|------|------|
| 55.4 | 54.9 | 54.4 | 54.0 | 53.5 |
| 4.3  | 4.8  | 5.3  | 5.7  | 1.2  |
| 150  | 200  | 250  | 300  | 200  |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 55.1 | 55.1 | 55.2 | 55.4 | 55.4 | 55.4 | 55.7 |
| 4.6  | 4.6  | 4.5  | 4.3  | 4.3  | 4.3  | 4.0  |
| 50   | 35   | 16   |      | 20   | 38   | 50   |

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| 55.2 | 54.9 | 54.7 | 54.8 | 55.1 | 54.8 | 54.6 | 55.5 |
| 4.5  | 4.8  | 5.0  | 4.9  | 4.6  | 4.9  | 5.1  | 4.2  |
| 50   | 34   | 22   | 13   |      | 12   | 25   | 50   |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 54.9 | 54.8 | 55.0 | 54.6 | 54.7 | 55.1 | 54.7 | 54.8 | 55.7 |
| 4.8  | 4.9  | 4.7  | 5.1  | 5.0  | 4.6  | 5.0  | 4.9  | 4.0  |
| 50   | 32   | 23   | 22   | 14   |      | 11   | 29   | 50   |

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| 55.0 | 54.6 | 54.6 | 54.6 | 54.4 | 54.5 | 55.0 | 54.9 |
| 4.7  | 5.0  | 5.10 | 5.1  | 5.1  | 5.3  | 5.2  | 4.8  |
| 23   | 22   | MH   | 12   |      | 10   | 23   | 50   |
|      |      | 17   |      |      |      |      |      |

|      |      |      |
|------|------|------|
| 54.9 | 55.1 | 55.5 |
| 4.8  | 4.6  | 4.2  |
| 30   | 50   | 70   |

3

Sta +  $\pi$  - Elev.  
959.69

0+81

(Gas)  
+92 G.V. Lt 23' 4.89

1

+50 Abandon Ent Lt.

TP 4.39 958.41 5.67 954.02

2

✓

+35  $\neq$  Ent Rt.



8-20-65

RT 31

55.2  
4.5 55.0 54.9 54.5 54.4 54.4 54.2 54.3 55.1 55.8  
47 48 52 521 5.3 5.2 5.3 5.5 5.4 4.6 3.9  
50 39 23 22 MH 11 7 15 23 36 50  
41 = 55.6  
70  
17.5

54.8 54.2 54.5 54.8 54.4 54.3 54.4 54.3 54.2 54.3 55.2 55.9  
39 4.5 5.2 4.9 5.3 5.4 5.3 5.4 5.5 5.4 4.5 3.8  
70 50 28 23 22 11 8 16 24 35 50

54.9 54.0 53.8 53.7 54.0 54.3 54.1 54.0 54.4 55.3  
4.8 5.7 5.9 6.0 5.7 5.4 5.6 5.7 5.3 4.4  
50 30 29 24 11 9 24 29 50

53.8 53.6 53.7 53.3 53.5 54.0 53.8 53.9 54.0 54.4  
4.6 4.9 4.7 5.1 4.9 4.4 4.6 4.5 4.4 4.0  
40 29 25 24 11 8 14 26 31

54.0  
4.4  
50

55.0 54.5 54.29  
3.4 3.9 4.12  
50 36 33.5  
WSO

53.8 53.0 53.0 62.9 53.2 54.0 53.8 53.8 53.9 54.6  
4.6 5.4 5.3 5.5 5.2 4.4 4.6 4.6 4.5 3.8  
50 29 24 23 12 12 18 27 50

| Sta | + | $\pi$ | - | Elev. |
|-----|---|-------|---|-------|
|-----|---|-------|---|-------|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 958.41 |  |  |
|--|--|--------|--|--|

|      |  |               |  |  |
|------|--|---------------|--|--|
| 2+83 |  | $\pm$ Walk Rt |  |  |
|------|--|---------------|--|--|

|   |  |         |  |  |
|---|--|---------|--|--|
| 3 |  | Ent Lt. |  |  |
|---|--|---------|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +35 |  |  |  |  |
|-----|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

|     |  |         |  |  |
|-----|--|---------|--|--|
| +65 |  | Ent Rt. |  |  |
|-----|--|---------|--|--|

|   |  |         |  |  |
|---|--|---------|--|--|
| 4 |  | Ent Rt. |  |  |
|---|--|---------|--|--|

|    |      |        |      |        |
|----|------|--------|------|--------|
| BM | 1.79 | 959.03 | 1.17 | 957.24 |
|----|------|--------|------|--------|

8-20-65

Lt.

Rt 32

|     |     |     |     |     |     |     |     |     |      |       |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|-------|
| 540 | 531 | 530 | 528 | 533 | 541 | 539 | 539 | 538 | 5452 | 53717 |
| 4.4 | 5.3 | 5.4 | 5.6 | 5.1 | 4.3 | 4.5 | 4.5 | 4.6 | 3.89 | 3.24  |
| 50  | 28  | 24  | 23  | 16  |     | 9   | 19  | 25  | Walk |       |
|     |     |     |     |     |     |     |     |     | 33   | 50    |

|      |      |      |      |      |     |     |     |      |      |      |
|------|------|------|------|------|-----|-----|-----|------|------|------|
| 53.5 | 52.6 | 52.5 | 52.6 | 53.4 | 540 | 539 | 537 | 53.5 | 53.7 | 54.9 |
| 4.9  | 5.8  | 5.9  | 5.8  | 5.0  | 4   | 4   | 4.5 | 4.7  | 4.9  | 4.7  |
| 50   | 30   | 26   | 24   | 13   |     |     | 10  | 20   | 25   | 27   |
|      |      |      |      |      |     |     |     |      | 38   | 50   |

|      |      |      |       |      |     |     |      |      |       |      |
|------|------|------|-------|------|-----|-----|------|------|-------|------|
| 52.2 | 52.2 | 53.3 | 53.55 | 53.6 | 541 | 539 | 53.5 | 53.2 | 54.20 | 54.9 |
| 6.2  | 6.2  | 5.1  | 4.86  | 4.8  | 4.3 | 4.5 | 4.9  | 5.2  | 4.20  | 3.5  |
| 31   | 29   | 22   | MH    | 13   |     | 13  | 19   | 25   | W50   | 50   |
|      |      |      |       |      |     |     |      |      | 33    |      |

|     |      |      |
|-----|------|------|
| 530 | 54.4 | 54.7 |
| 5.4 | 4.0  | 3.7  |
| 32  | 42   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |        |       |
|------|------|------|------|------|------|------|------|------|------|------|--------|-------|
| 50.7 | 50.1 | 51.5 | 53.4 | 53.5 | 53.6 | 54.0 | 53.7 | 53.6 | 53.9 | 54.0 | 54.6   | 55.57 |
| 7.7  | 8.3  | 6.9  | 5.0  | 4.9  | 4.8  | 4.4  | 4.7  | 4.8  | 4.5  | 4.4  | 3.8    | 2.84  |
| 50   | 41   | 35   | 21   | 17   | 12   |      | 13   | 19   | 28   | 50   | Garage |       |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 48.4 | 52.9 | 53.1 | 53.4 | 53.9 | 53.6 | 53.5 | 53.9 | 53.9 | 54.0 | 54.0 |
| 10.0 | 5.5  | 5.3  | 5.0  | 4.5  | 4.8  | 4.9  | 4.5  | 4.5  | 4.5  | 4.4  |
| 50   | 35   | 23   | 17   |      | 11   | 17   | 26   | 41   | 50   |      |

Top Hyd by H<sub>0</sub> #1316 C. R. B



Sta +  $\pi$  - Elev.

959.03

4+29 Walk Rt

✓

+65 Ent Rt

+72

✓

5

Lt.

8-20-65

RT

33

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 51.8 | 52.7 | 53.5 | 53.9 | 53.5 | 53.4 | 52.4 | 52.4 | 53.8 |
| 7.2  | 6.3  | 5.5  | 5.1  | 5.5  | 5.6  | 6.6  | 6.6  | 5.2  |
| 50   | 35   | 17   |      | 16   | 18   | 22   | 24   | 28   |

|       |       |       |
|-------|-------|-------|
| 54.50 | 54.24 | 54.29 |
| 4.50  | 4.79  | 4.74  |
| House | 50    | 46    |
|       | Walk  |       |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 51.6 | 52.4 | 53.2 | 53.5 | 54.1 | 53.7 | 53.7 | 54.0 | 54.1 |
| 7.4  | 6.6  | 5.8  | 5.5  | 4.9  | 5.3  | 5.3  | 5.0  | 4.9  |
| 50   | 33   | 20   | 17   |      | 16   | 22   | 33   | 50   |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 50.7 | 51.6 | 53.6 | 53.6 | 54.1 | 53.8 | 53.6 | 52.7 | 52.7 |
| 8.3  | 7.4  | 5.5  | 5.4  | 4.9  | 5.2  | 5.4  | 6.3  | 6.3  |
| 50   | 34   | 20   | 18   |      | 15   | 19   | 22   | 24   |

|      |      |      |
|------|------|------|
| 54.2 | 53.9 | 53.7 |
| 4.8  | 5.1  | 5.3  |
| 50   | 33   | 26   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 51.8 | 52.5 | 53.7 | 54.0 | 54.2 | 53.8 | 53.7 | 52.5 | 52.5 | 54.0 |
| 7.2  | 6.5  | 5.3  | 5.0  | 4.8  | 5.2  | 5.3  | 6.5  | 6.5  | 5.0  |
| 50   | 32   | 21   | 18   |      | 15   | 17   | 22   | 24   | 27   |

|      |      |
|------|------|
| 55.3 | 54.3 |
| 3.7  | 4.7  |
| 50   | 33   |

Sta +  $\pi$  - Elev.

959.03

5+13 Walk Rt

✓

+28 Ent Rt

+50

+60

+70



Lt

£

8-20-65

Rt

34

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 62.3 | 62.1 | 53.7 | 53.9 | 54.3 | 53.9 | 53.7 | 52.5 | 52.5 |
| 6.7  | 6.3  | 5.3  | 5.1  | 4.7  | 5.1  | 5.3  | 6.5  | 6.5  |
| 50   | 33   | 19   | 17   |      | 15   | 18   | 21   | 24   |

|       |       |       |      |
|-------|-------|-------|------|
| 56.36 | 54.29 | 54.48 | 54.0 |
| 2.67  | 4.74  | 4.55  | 5.0  |
| House | 50    | 33    | 28   |
|       | walk  |       |      |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 52.9 | 52.9 | 53.0 | 53.6 | 53.8 | 54.4 | 54.0 | 53.7 | 53.6 | 53.9 | 54.9 |
| 6.1  | 6.1  | 6.0  | 5.4  | 5.2  | 4.6  | 5.0  | 5.3  | 5.4  | 5.1  | 4.1  |
| 50   | 42   | 26   | 18   | 17   |      | 16   | 17   | 22   | 26   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 53.4 | 53.4 | 52.7 | 53.8 | 53.9 | 54.7 | 54.2 | 53.6 | 52.6 | 52.4 | 53.9 | 54.7 |
| 5.6  | 5.6  | 6.3  | 5.2  | 5.1  | 4.3  | 4.8  | 5.4  | 6.4  | 6.6  | 5.1  | 4.7  |
| 50   | 37   | 27   | 19   | 17   |      | 15   | 18   | 22   | 27   | 34   | 50   |

|       |      |      |      |      |      |      |      |      |      |      |      |
|-------|------|------|------|------|------|------|------|------|------|------|------|
| 53.6  | 53.6 | 53.4 | 52.8 | 53.8 | 53.9 | 54.8 | 54.4 | 54.2 | 53.8 | 52.6 | 51.5 |
| 5.38  | 5.4  | 5.6  | 6.2  | 5.2  | 5.1  | 4.2  | 4.6  | 4.8  | 5.2  | 6.5  | 7.5  |
| House | 50   | 37   | 25   | 18   | 17   |      | 16   | 19   | 25   | 30   | 50   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 53.6 | 53.4 | 53.0 | 53.7 | 54.1 | 54.9 | 54.4 | 53.7 | 53.7 | 54.0 |
| 5.4  | 5.6  | 6.0  | 5.3  | 4.9  | 4.1  | 4.6  | 5.3  | 5.3  | 5.0  |
| 50   | 32   | 27   | 19   | 15   |      | 14   | 23   | 42   | 50   |

Sta +  $\pi$  - Elev.

959.03

6+00

+25

+35 Ditch No

+45 Shoulder No

+58<sup>+</sup>  $\pm$  Dellwood

+73 Shoulder Line

BM 8.66 965.65 2.04 956.99

BM

7.98

957.67

956.981

Looks Tipped

Lt

Z

8-20-65

BT

35

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 53.4 | 53.6 | 53.2 | 54.0 | 54.8 | 55.3 | 54.9 | 54.8 | 54.1 | 54.7 |
| 5.6  | 5.5  | 5.8  | 4.7  | 4.2  | 3.7  | 4.1  | 4.2  | 4.6  | 4.3  |
| 50   | 36   | 28   | 19   | 14   |      | 12   | 16   | 25   | 50   |

|      |      |      |      |      |      |      |      |       |      |      |
|------|------|------|------|------|------|------|------|-------|------|------|
| 53.0 | 53.3 | 54.1 | 54.7 | 55.3 | 55.6 | 55.3 | 55.0 | 55.27 | 55.4 | 55.6 |
| 6.0  | 5.7  | 4.9  | 4.3  | 3.7  | 3.4  | 3.7  | 4.0  | 3.76  | 3.6  | 3.4  |
| 50   | 32   | 26   | 20   | 14   |      | 15   | 20   | MH    | 32   | 50   |
|      |      |      |      |      |      |      |      | 23    |      |      |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 52.6 | 53.1 | 53.8 | 54.8 | 54.0 | 55.5 | 55.7 | 55.4 | 55.2 | 55.5 | 55.8 |
| 6.4  | 5.9  | 5.2  | 4.2  | 4.0  | 3.5  | 3.3  | 3.6  | 3.8  | 3.5  | 3.2  |
| 50   | 39   | 32   | 26   | 20   | 14   |      | 15   | 17   | 31   | 50   |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 53.7 | 54.5 | 55.3 | 56.4 | 56.7 | 56.5 | 56.6 | 56.1 | 56.3 |
| 5.3  | 4.5  | 3.7  | 3.6  | 3.3  | 3.5  | 3.4  | 2.9  | 2.7  |
| 50   | 36   | 21   | 16   |      | 15   | 20   | 37   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 52.1 | 53.2 | 54.3 | 54.7 | 55.5 | 56.0 | 55.7 | 55.9 | 56.1 | 56.6 | 56.3 |
| 6.9  | 5.8  | 4.7  | 4.3  | 3.5  | 3.33 | 3.3  | 3.1  | 3.4  | 2.9  | 2.4  |
| 100  | 75   | 50   | 40   | 20   | 19   | 15   |      | 16   | 30   | 42   |
|      |      |      |      |      | MH   |      |      |      |      | 50   |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 53.9 | 55.7 | 55.6 | 55.9 | 56.1 | 55.8 | 55.9 | 56.2 | 57.9 |
| 5.1  | 4.3  | 3.5  | 3.1  | 2.9  | 3.2  | 3.1  | 2.8  | 1.1  |
| 50   | 36   | 20   | 13   |      | 15   | 20   | 27   | 31   |

Roseville Mont SEC, Dellwood &amp; B

Top Hyd NE Co, Dellwood &amp; B



| Sta | + | $\pi$ | - | Elev. |
|-----|---|-------|---|-------|
|-----|---|-------|---|-------|

965.65

6+73

+87 Ditch Line

+92 G.V. Lt 22' 10.26

+94 G.V. Lt 25' 10.52

7

+48

+56 Entry

+80 Entry

Lt.

~~4~~

8-20-65

Rt.

34

54.2  
6.0 5.3  
38 50

52.8 53.3 54.6 55.4 55.7 56.3 56.0 56.1 56.4 57.8 57.1 57.1  
12.9 12.4 11.1 10.3 10.0 9.4 9.7 9.6 9.3 7.9 4.0 4.3  
50 38 28 21 15 16 22 26 31 40 50

55.6 54.9 55.8 55.7 56.5 56.3 56.1 56.7 58.6 61.6 61.6  
10.1 10.8 9.9 10.0 9.2 9.4 9.6 9.0 7.1 4.1 4.3  
50 27 19 17 11 22 26 32 39 50

55.76 55.5 55.6 56.4 56.6 56.9 56.7 56.6 56.9 58.8 61.2 61.9  
9.89 10.2 10.1 9.3 9.2 8.8 9.0 9.1 8.8 6.9 4.5 3.8  
House 50 30 19 15 15 17 25 32 37 50

56.3 55.4 56.4 56.4 56.5 56.9 56.9 56.8 57.5 58.3  
10.4 10.3 9.3 9.3 9.2 8.8 8.8 8.9 8.2 6.9  
50 36 21 17 15 13 18 27 50

56.1 55.3 56.0 56.5 57.0 57.1 57.2 57.7 58.6 58.9  
10.6 10.4 9.7 9.2 8.7 8.6 8.5 8.0 7.1 6.8  
50 37 20 18 15 20 28 41 50

Sta +  $\pi$  - Elev

965.65

7+84 Top Wall

+85 WSO 30' Rt

8

+18

✓

+44  $\phi$  Ent Lt

+55 Ent Rt

BM 2.11 961.17 6.59 959.06 (959.05)



Lt

Lt

8-20-65

Rt

37

55.3  
10.4  
50

55.3  
10.4  
41

55.9  
9.8  
20

55.5  
9.2  
19

57.0  
8.7  
14

57.1  
8.6  
14

57.2  
8.5  
21

57.9  
7.8  
29

57.9  
5.8  
34

57.9  
4.7  
42

55.9  
9.8  
50

55.8  
9.9  
39

56.1  
9.6  
23

56.3  
9.4  
19

56.6  
9.1  
15

57.0  
8.7  
13

57.0  
8.7  
20

57.4  
8.3  
27

57.8  
7.9  
32

59.5  
6.2  
41

61.5  
4.2  
50

55.01  
9.64  
House  
walk

55.9  
9.8  
50

55.8  
9.9  
29

56.2  
9.5  
21

56.4  
9.3  
18

57.1  
8.6  
12

57.3  
8.4  
16

57.1  
8.6  
25

57.3  
8.4  
26

57.5  
8.2  
31

59.4  
6.3  
31

62.1  
3.6  
50

61.4  
4.3  
38

55.67  
9.98  
50

55.49  
10.16  
33

55.8  
9.9  
28

56.2  
9.5  
19

56.4  
9.3  
15

57.2  
8.5  
15

57.3  
8.4  
15

57.2  
8.5  
19

57.3  
8.4  
25

58.6  
7.1  
30

60.7  
5.0  
36

61.4  
4.3  
50

Conc

55.4  
10.3  
50

55.5  
10.2  
42

55.4  
10.3  
29

56.2  
9.5  
19

56.5  
9.2  
15

57.3  
8.4  
13

57.4  
8.3  
22

57.6  
8.1  
34

58.0  
7.7  
50

59.1  
6.6  
50

Top Hyd. NE Cor Merrel St &amp; "B"

Sta +  $\pi$  - Elev.

961.17

8+65

9

+30

+59

+78 Gutter Line

✓

LK  
 LPD  
 RP  
 HL

8-23, 65

Lt

Rt 38

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 55.1 | 55.2 | 56.1 | 56.3 | 56.7 | 56.9 | 57.4 | 57.3 | 57.8 | 57.6 | 57.4 |
| 6.0  | 5.1  | 4.9  | 4.5  | 4.3  | 3.8  | 3.9  | 3.9  | 3.6  | 1.8  |      |
| 50   | 30   | 20   | 17   | 14   | 12   |      | 6    | 17   | 27   | 50   |

|       |      |      |      |      |      |      |      |      |      |      |      |
|-------|------|------|------|------|------|------|------|------|------|------|------|
| 55.6  | 55.4 | 55.9 | 56.6 | 56.7 | 57.0 | 57.5 | 57.5 | 57.3 | 57.6 | 58.2 | 59.6 |
| 5.56  | 5.8  | 5.3  | 4.6  | 4.5  | 4.2  | 3.7  | 3.7  | 3.9  | 3.6  | 3.0  | 1.6  |
| House | 50   | 30   | 23   | 19   | 14   |      | 9    | 17   | 20   | 31   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 55.4 | 55.8 | 56.2 | 56.5 | 56.6 | 57.0 | 57.4 | 57.5 | 57.3 | 57.4 | 58.3 | 59.0 |
| 5.8  | 5.4  | 5.0  | 4.7  | 4.6  | 4.2  | 3.8  | 3.7  | 3.9  | 3.8  | 2.9  | 2.2  |
| 50   | 44   | 29   | 24   | 19   | 15   |      | 11   | 17   | 25   | 37   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 56.8 | 56.1 | 56.6 | 56.6 | 57.0 | 57.3 | 57.4 | 57.4 | 57.1 | 57.0 | 57.9 | 58.3 |
| 5.4  | 5.1  | 4.6  | 4.6  | 4.2  | 3.9  | 3.8  | 3.8  | 4.1  | 4.2  | 3.3  | 2.9  |
| 50   | 32   | 24   | 19   | 15   | 9    |      | 8    | 15   | 23   | 40   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 56.3 | 56.3 | 57.1 | 57.0 | 57.3 | 57.5 | 57.3 | 57.1 | 57.3 | 57.1 | 57.1 |
| 5.9  | 4.9  | 4.1  | 4.2  | 3.9  | 3.7  | 3.9  | 4.1  | 3.9  | 4.1  | 4.1  |
| 50   | 31   | 21   | 16   | 10   |      | 12   | 17   | 19   | 36   | 50   |

54.3  
 53.3  
 6.9 7.9  
 72 100



Sta +  $\pi$  - Elev.

961.17

9+89  $\pm$  Merrill St.

✓

10

29

57.3

✓

+19 Ent Rt

+50

BM

0.87

959.94

2.10

959.07

8-23-65

11

2

BT 39

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 54.6 | 55.7 | 56.2 | 56.7 | 57.2 | 57.3 | 57.3 | 57.3 | 57.1 | 57.3 | 57.2 | 57.2 |
| 6.7  | 5.5  | 5.0  | 4.5  | 4.0  | 3.9  | 3.7  | 3.9  | 4.1  | 3.9  | 4.0  | 4.0  |
| 78   | 50   | 38   | 26   | 15   | 9    |      | 8    | 16   | 18   | 33   | 50   |

|      |      |      |
|------|------|------|
| 53.6 | 52.7 | 51.8 |
| 7.6  | 8.5  | 9.4  |
| 100  | 125  | 150  |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 56.0 | 55.7 | 56.5 | 56.7 | 57.2 | 57.4 | 57.2 | 57.1 | 57.4 | 57.1 | 57.2 |
| 6.2  | 5.5  | 4.7  | 4.3  | 4.0  | 3.8  | 4.0  | 4.1  | 3.8  | 4.1  | 4.0  |
| 55   | 42   | 29   | 20   | 13   |      | 8    | 15   | 18   | 30   | 50   |

|      |      |
|------|------|
| 54.2 | 53.2 |
| 7.0  | 8.0  |
| 75   | 100  |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 55.4 | 56.0 | 56.3 | 56.4 | 56.8 | 57.2 | 57.1 | 57.1 | 57.2 | 57.4 | 57.6 |
| 5.8  | 5.2  | 4.4  | 4.6  | 4.4  | 4.0  | 4.1  | 4.1  | 4.0  | 3.8  | 3.6  |
| 50   | 36   | 24   | 20   | 16   |      | 10   | 16   | 22   | 36   | 50   |

|          |      |      |      |      |      |      |      |      |      |      |
|----------|------|------|------|------|------|------|------|------|------|------|
| 55.4     | 55.7 | 56.3 | 56.1 | 56.2 | 57.0 | 56.8 | 56.5 | 56.4 | 56.8 | 57.3 |
| 5.8      | 5.5  | 4.9  | 5.1  | 5.0  | 4.2  | 4.4  | 4.7  | 4.7  | 4.4  | 3.9  |
| House 50 | 24   | 20   | 17   |      |      | 11   | 15   | 18   | 26   | 39   |

Top Hyd NE Cor. Merrill + B

|       |      |
|-------|------|
| 56.4  | 57.9 |
| 4.8   | 3.3  |
| House | 50   |

Sta +  $\pi$  - Elev.

959.94

9+57 MH Rt 2.90

11+00 Ent Rt & Lt

+42

+72

+88 Ent Lt

✓

12



Lt.

8-23-65

RT 40

<sup>55.50</sup>  
<sup>55.1</sup>  
<sup>55.4</sup>  
<sup>55.1</sup>  
<sup>55.1</sup>  
<sup>55.8</sup>  
<sup>55.3</sup>  
<sup>55.9</sup>  
<sup>55.3</sup>  
<sup>55.8</sup>  
<sup>57.8</sup>  
<sup>57.93</sup>  
 444 44 43 43 44 41 36 40 36 31 21 201  
 55 50 43 25 21 14 13 17 34 56 House  
 Come

<sup>56.1</sup>  
<sup>55.5</sup>  
<sup>55.3</sup>  
<sup>55.0</sup>  
<sup>55.8</sup>  
<sup>55.1</sup>  
<sup>55.4</sup>  
<sup>55.2</sup>  
<sup>56.4</sup>  
<sup>57.2</sup>  
 3.8 4.4 4.6 4.9 4.1 4.8 4.5 4.7 3.5 2.7  
 50 36 24 21 16 18 21 38 50

<sup>54.3</sup>  
<sup>54.3</sup>  
<sup>54.4</sup>  
<sup>55.0</sup>  
<sup>54.7</sup>  
<sup>55.4</sup>  
<sup>54.7</sup>  
<sup>54.7</sup>  
<sup>53.5</sup>  
<sup>52.6</sup>  
<sup>52.1</sup>  
 5.6 5.6 5.5 4.9 5.2 4.5 5.2 5.2 6.4 7.3 7.8  
 50 33 26 23 21 16 18 27 33 50

<sup>54.65</sup>  
<sup>54.44</sup>  
<sup>54.19</sup>  
<sup>54.8</sup>  
<sup>54.6</sup>  
<sup>55.2</sup>  
<sup>54.5</sup>  
<sup>54.4</sup>  
<sup>53.8</sup>  
<sup>53.0</sup>  
 5.29 5.50 5.75 5.1 5.3 4.7 5.4 5.5 6.1 6.9  
 50 41 34 24 22 15 18 24 33

<sup>54.89</sup>  
<sup>55.14</sup>  
<sup>55.62</sup>  
 5.05 4.80 4.32  
 60 70 79

<sup>52.9</sup>  
 7.0  
 50

412

<sup>55.82</sup>  
<sup>54.7</sup>  
<sup>54.1</sup>  
<sup>54.1</sup>  
<sup>54.5</sup>  
<sup>54.5</sup>  
<sup>55.1</sup>  
<sup>54.9</sup>  
<sup>54.4</sup>  
<sup>54.3</sup>  
<sup>53.9</sup>  
<sup>53.1</sup>  
 4.12 5.2 5.8 5.8 5.4 5.4 4.8 5.0 5.5 5.6 6.0 6.8  
 House 50 39 29 24 18 8 15 17 21 26

<sup>53.1</sup>  
<sup>53.5</sup>  
<sup>52.9</sup>  
 6.8 6.4 7.0  
 50 35 30

Sta +  $\pi$  - Elev.

959.94

12 + 44

✓

BM 2.02 959.92 2.02 957.92 (957.895)

2.02

959.94

+89

✓

13 Ent Lt Ditch Rt

+06 Shoulder Line

8-23-65

Lt.

E

Rt.

41

|      |      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 55.0 | 54.5 | 54.2 | 54.5 | 54.3 | 54.2 | 54.7 | 54.5 | 54.1 | 53.8 | 52.4 | 52.7 | 52.1 |
| 49   | 54   | 57   | 54   | 56   | 57   | 52   | 54   | 58   | 61   | 75   | 72   | 62   |
| 50   | 37   | 27   | 24   | 22   | 18   |      | 7    | 15   | 18   | 29   | 36   | 39   |

53.3  
6.6  
50

S.E. Cor. Top Landing H<sup>o</sup> 1225 N.W. Cor Fernwood

|       |      |      |      |      |      |      |      |      |      |      |
|-------|------|------|------|------|------|------|------|------|------|------|
| 56.22 | 55.7 | 54.3 | 54.5 | 54.2 | 54.5 | 53.6 | 53.4 | 53.4 | 53.1 | 52.4 |
| 3.2   | 4.2  | 5.6  | 5.4  | 5.7  | 5.4  | 6.3  | 6.5  | 6.5  | 6.8  | 7.5  |
| House | 50   | 27   | 24   | 22   |      | 16   | 19   | 23   | 28   | 34   |

53.1  
6.8  
50

53.0  
6.9  
42

|        |       |       |       |      |      |      |      |      |      |      |      |
|--------|-------|-------|-------|------|------|------|------|------|------|------|------|
| 57.08  | 55.43 | 54.97 | 54.50 | 54.1 | 54.4 | 54.5 | 53.9 | 53.7 | 53.1 | 52.7 | 52.4 |
| 28.4   | 44.9  | 49.5  | 54.2  | 5.8  | 5.5  | 5.4  | 6.0  | 6.2  | 6.8  | 7.2  | 7.5  |
| Garage | 45    | 37    | 28    | 20   | 12   |      | 15   | 20   | 29   | 43   | 50   |

Conc

|       |       |       |      |      |      |      |      |      |
|-------|-------|-------|------|------|------|------|------|------|
| 55.44 | 54.98 | 54.50 | 54.1 | 54.1 | 54.4 | 53.8 | 53.0 | 53.1 |
| 44.8  | 49.4  | 54.2  | 5.8  | 5.8  | 5.5  | 5.1  | 6.9  | 6.8  |
| 45    | 37    | 28    | 22   | 20   |      | 17   | 42   | 50   |

Conc



Sta +  $\pi$  - Elev.

959.92

13+17  $\neq$  Fernwood

✓

+32 Shoulder Line

+47 E.P.L.

BM 2.47 957.57 4.82 955.10 (955.10)

+70

✓

FK  
LPD  
RP  
HL

11

8-23-65  
8-24-65 Rt. 42

|      |      |      |       |       |      |      |      |      |
|------|------|------|-------|-------|------|------|------|------|
| 55.8 | 54.3 | 54.0 | 54.13 | 54.14 | 54.8 | 53.5 | 53.4 | 53.3 |
| 4.1  | 5.6  | 5.9  | 5.74  | 5.5   | 6.1  | 6.4  | 6.5  | 6.6  |
| 50   | 29   | 23   | NH    |       | 17   | 39   | 50   | 75   |
|      |      |      | 19    |       |      |      |      |      |

|      |      |      |      |      |
|------|------|------|------|------|
| 53.9 | 53.7 | 53.6 | 53.5 | 53.3 |
| 6.0  | 6.2  | 6.3  | 6.4  | 6.6  |
| 200  | 175  | 150  | 125  | 100  |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 55.4 | 54.6 | 54.2 | 53.9 | 54.3 | 53.9 | 53.7 | 53.1 | 53.0 |
| 4.5  | 5.4  | 5.7  | 6.0  | 5.6  | 6.0  | 6.2  | 6.8  | 6.9  |
| 50   | 33   | 24   | 22   |      | 13   | 19   | 37   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 55.6 | 55.2 | 54.4 | 54.0 | 54.0 | 53.7 | 54.2 | 53.7 | 52.9 | 52.1 | 52.3 | 52.8 |
| 4.3  | 4.7  | 5.5  | 5.9  | 5.9  | 6.2  | 5.7  | 6.2  | 7.0  | 7.8  | 7.6  | 7.1  |
| 50   | 45   | 36   | 32   | 24   | 22   |      | 13   | 21   | 25   | 31   | 50   |

Top Hyd S.E. Cor Fernwood 48

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 54.1 | 54.8 | 53.7 | 53.5 | 54.0 | 53.3 | 53.0 | 52.5 | 51.7 | 52.1 |
| 1.5  | 2.8  | 3.9  | 4.1  | 3.6  | 4.3  | 4.6  | 5.1  | 5.9  | 5.5  |
| 50   | 38   | 23   | 20   |      | 15   | 18   | 21   | 24   | 28   |

|      |      |      |
|------|------|------|
| 54.5 | 54.4 | 53.1 |
| 3.1  | 3.2  | 4.5  |
| 50   | 40   | 32   |

Sta +  $\pi$  - Elev.

957.57

14+00

+42 Ent Rt + Lt.

+78

✓

15

✓

8-24-65

43

Lt

E

Rt

55.5 54.7 53.6 53.2 53.0 53.1 52.6 52.2 52.1 53.5 54.5  
 2.1 2.9 4.0 4.4 3.8 4.5 5.0 5.4 5.5 4.1 3.1  
 50 37 23 21 15 18 22 28 33 41 50

54.6 53.8 53.2 53.0 53.4 53.0 53.2 53.6 53.8 54.4  
 3.0 3.8 4.4 4.6 4.2 4.6 4.4 4.0 3.8 3.1  
 50 36 22 21 16 22 38 50 Garage

55.72 54.6 53.8 52.8 52.9 52.5 53.2 52.4 52.0 51.7 52.1 53.1  
 1.85 3.0 3.8 4.8 4.7 5.1 4.4 5.2 5.6 5.9 5.5 3.9  
 House 50 42 31 23 22 16 19 23 27 35

55.04 54.5  
 2.53 3.1  
 House 50

54.0 52.3 52.4 52.1 53.1 52.4 52.1 51.6 51.7 52.4  
 3.6 5.3 5.2 5.5 4.5 5.2 5.5 6.0 5.9 5.2  
 50 31 24 22 15 18 22 26 28

54.4 53.4  
 3.2 4.2  
 50 33



Sta +  $\pi$  - Elev.

957.57

15+18 Ent Lt

✓

+29

✓

+40

Lt

L

8-24-65

Rt

44

|        | 55.45 | 53.5 | 52.6 | 53.2 | 53.0 | 52.9 | 52.1 | 51.9 | 51.1 | 51.1 | 52.2 |
|--------|-------|------|------|------|------|------|------|------|------|------|------|
|        | 2.12  | 4.1  | 5.0  | 4.4  | 4.6  | 4.7  | 5.5  | 5.7  | 6.5  | 6.5  | 5.4  |
| Garage | 50    | 38   | 27   | 22   |      |      | 15   | 17   | 22   | 25   | 28   |

|  | 53.9 | 52.9 |
|--|------|------|
|  | 3.7  | 4.7  |
|  | 50   | 32   |

|  | 53.0 | 52.3 | 51.9 | 51.7 | 51.9 | 52.8 | 52.0 | 51.6 | 51.2 | 50.9 | 51.9 |
|--|------|------|------|------|------|------|------|------|------|------|------|
|  | 4.6  | 5.3  | 5.7  | 5.9  | 5.7  | 4.8  | 5.6  | 6.0  | 6.4  | 6.7  | 5.7  |
|  | 50   | 39   | 25   | 23   | 18   |      | 16   | 18   | 21   | 23   | 27   |

|  | 53.9 | 52.9 |
|--|------|------|
|  | 3.7  | 4.7  |
|  | 50   | 32   |

|  | 49.5 | 50.3 | 51.2 | 51.9 | 52.4 | 52.6 | 52.2 | 51.9 | 51.4 | 51.1 | 52.3 |
|--|------|------|------|------|------|------|------|------|------|------|------|
|  | 8.1  | 7.3  | 6.4  | 5.7  | 5.2  | 5.0  | 5.4  | 5.7  | 6.2  | 6.5  | 5.4  |
|  | 50   | 35   | 23   | 17   | 12   |      | 15   | 16   | 21   | 24   | 29   |

|  | 54.2 | 53.1 |
|--|------|------|
|  | 3.4  | 4.5  |
|  | 50   | 33   |

Sta +  $\pi$  - Elev.

957.57

15+70

✓

+91 Ent Rt

✓

T.P. 4.62 956.40 5.79 951.78

16

+50

✓

8-24-65

Lt.

E

Rt 45

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 49.7 | 49.2 | 49.5 | 50.6 | 51.6 | 52.1 | 52.4 | 51.9 | 51.5 | 50.9 | 51.9 |
| 79   | 8.4  | 8.1  | 7.0  | 6.0  | 5.5  | 5.2  | 5.7  | 6.1  | 6.7  | 5.7  |
| 38   | 35   | 32   | 24   | 16   | 11   |      | 13   | 17   | 22   | 27   |

49.0  
8.6  
50

55.25  
2.32 3.4 4.7  
House 50 32

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 50.3 | 50.2 | 50.9 | 50.5 | 51.8 | 52.1 | 52.2 | 52.0 | 52.2 | 52.8 | 53.2 |
| 7.3  | 7.4  | 6.7  | 6.1  | 5.8  | 5.5  | 5.4  | 5.6  | 5.4  | 4.8  | 4.4  |
| 35   | 30   | 25   | 20   | 15   | 11   |      | 13   | 20   | 31   | 38   |

49.5  
8.1  
50

55.23  
2.24 3.78 4.06  
Garage 50 43

Top E. End Culvert Rt 15+01

Conc

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 49.8 | 50.2 | 50.8 | 51.8 | 51.9 | 52.2 | 51.9 | 50.8 | 52.2 | 53.2 | 53.4 |
| 6.6  | 6.2  | 5.6  | 4.6  | 4.5  | 4.2  | 4.5  | 5.6  | 4.2  | 3.2  | 2.5  |
| 50   | 36   | 29   | 18   | 15   |      | 14   | 21   | 27   | 32   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 49.0 | 49.5 | 50.3 | 51.0 | 51.2 | 51.9 | 51.2 | 50.3 | 50.3 | 51.4 | 52.7 |
| 7.4  | 6.9  | 6.1  | 5.3  | 5.2  | 4.5  | 5.2  | 6.1  | 6.1  | 5.0  | 3.7  |
| 50   | 35   | 27   | NH   | 17   |      | 15   | 20   | 22   | 26   | 30   |

21

54.78  
1.62 3.1  
House 50



Sta +  $\pi$  - Elev.

956.40

16+83  $\angle$  Ent Rt.

17

✓

+43

✓

+22

BM 0.69 954.99 2.10 954.30 (954.31)

Lt.

8-24-65

R1 46

| 49.0 | 49.1 | 48.9 | 50.2 | 51.2 | 51.6 | 51.4 | 52.2 | 52.62 | 53.02 | 54.8  |
|------|------|------|------|------|------|------|------|-------|-------|-------|
| 7.4  | 7.3  | 7.5  | 6.2  | 5.2  | 4.8  | 5.0  | 4.2  | 3.78  | 3.38  | 1.59  |
| 50   | 43   | 35   | 21   | 17   |      | 15   | 34   | 43    | 50    | Gauge |

Conc

| 49.0 | 49.3 | 50.0 | 51.1 | 51.2 | 51.6 | 51.1 | 50.8 | 50.6 | 50.1 | 51.2 |
|------|------|------|------|------|------|------|------|------|------|------|
| 7.4  | 7.1  | 6.4  | 5.3  | 5.2  | 4.8  | 5.3  | 5.6  | 6.4  | 6.3  | 5.2  |
| 50   | 37   | 29   | 18   | 15   |      | 14   | 18   | 21   | 23   | 29   |

| 52.5 | 51.8 |
|------|------|
| 3.9  | 4.6  |
| 50   | 35   |

| 48.9 | 48.7 | 50.0 | 50.7 | 51.1 | 51.4 | 51.0 | 50.1 | 49.3 | 50.1 | 51.6 |
|------|------|------|------|------|------|------|------|------|------|------|
| 7.5  | 7.7  | 6.4  | 5.7  | 5.3  | 5.0  | 5.4  | 6.3  | 7.1  | 6.3  | 4.8  |
| 50   | 37   | 26   | 17   | 13   |      | 14   | 19   | 22   | 25   | 31   |

| 53.58          | 52.6 | 51.9 |
|----------------|------|------|
| 2.82           | 3.8  | 4.5  |
| H <sub>0</sub> | 50   | 40   |

| 49.4 | 49.5 | 50.4 | 51.1 | 50.7 | 51.3 | 51.8 | 51.88 | 52.2 |
|------|------|------|------|------|------|------|-------|------|
| 7.0  | 6.9  | 6.0  | 5.3  | 5.7  | 5.1  | 4.6  | 4.52  | 4.18 |
| 29   | 23   | 19   |      | 15   | 26   | 39   | 43    | 50   |

SA.16 Conc  
2.24  
garage

Top Hyd by Ho #1178 C. Rd "B"

| Sta  | +     | $\pi$  | -     | Elev.  |                            |
|------|-------|--------|-------|--------|----------------------------|
|      |       | 954.99 |       |        |                            |
| BM   | 1.51  | 952.92 | 3.58  | 951.41 | (951.42)                   |
| BM   | 3.53  | 954.64 | 1.81  | 951.11 | (951.13)                   |
| BM   | 0.42  | 954.18 | 0.88  | 953.76 | (953.78)                   |
| BM   | 1.64  | 949.44 | 6.38  | 947.80 | (947.80)                   |
| BM   | +7.52 | 949.43 | 7.53  | 941.91 | <sup>91</sup><br>(941.860) |
| B.M. | -6.41 | 954.21 | -1.63 | 947.80 |                            |
| BM   | 0.80  | 954.59 | 0.42  | 953.79 |                            |
| BM   | 1.17  | 952.31 | 3.45  | 951.14 |                            |
| BM   | 2.98  | 954.41 | 0.88  | 951.43 | (951.42)                   |
| BM   | 2.37  | 956.68 | 0.10  | 954.31 | ✓                          |
| BM   | 4.09  | 959.19 | 1.58  | 955.10 | ✓                          |
| BM   |       |        | 1.31  | 957.88 | (957.895)                  |

Lt.

£

8-24-65

Rt

47

Top Hyd By School

Top Hyd S.W. Cor. Lexington + B

Top Hyd Sta 30+45

Top Hyd N.W. Cor Oxford + "B" 6.38

Roseville B.M. by Ho # 982 Co Rd "B"

Top Hyd by Ho # 1178 Co Rd "B"

Top Hyd S.E. Cor. Fernwood + "B"

S.E. Cor. Top Landing Ho # 1225 N.W. Cor. Fernwood



Sta +  $\pi$  - Elev.

BM 5.42 960.52

955.10

12+96

13

+06

+17

+29 MH 40' Rht. 7.06 953.46

+32

+38

BM 3.88 958.98 5.42 955.10

FK  
DS  
LPD  
ML

11-16-65

11

4

81

48

Top Hyd S.E. Cor. Fernwood 4 "B"

|      |      |      |       |      |      |
|------|------|------|-------|------|------|
| 54.5 | 53.9 | 52.9 | 51.65 | 52.6 | 52.9 |
| 6.00 | 6.6  | 7.6  | 8.87  | 7.9  | 7.6  |
|      | 14   | 29   | 39    | 55   | 87   |

Castings

|      |      |      |      |      |
|------|------|------|------|------|
| 54.4 | 53.9 | 53.0 | 52.6 | 52.8 |
| 6.1  | 6.6  | 7.5  | 7.9  | 7.7  |
|      | 14   | 32   | 52   | 79   |

|      |      |      |      |      |
|------|------|------|------|------|
| 54.4 | 53.9 | 53.1 | 52.8 | 52.8 |
| 6.1  | 6.6  | 7.4  | 7.7  | 7.7  |
|      | 13   | 34   | 53   | 79   |

|      |      |      |      |      |      |
|------|------|------|------|------|------|
| 54.3 | 53.9 | 53.4 | 53.1 | 53.0 | 53.0 |
| 6.2  | 6.6  | 7.1  | 7.4  | 7.5  | 7.5  |
|      | 13   | 29   | 59   | 79   | 100  |

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| 54.7 | 54.0 | 54.1 | 54.2 | 53.9 | 53.4 | 53.1 | 53.1 |
| 5.8  | 6.5  | 6.4  | 6.3  | 6.6  | 7.1  | 7.4  | 7.4  |
| 39   | 24   | 15   |      | 13   | 27   | 51   | 75   |

|      |      |      |      |       |      |      |
|------|------|------|------|-------|------|------|
| 54.2 | 53.7 | 53.2 | 52.6 | 51.70 | 52.4 | 52.6 |
| 6.3  | 6.8  | 7.3  | 7.9  | 8.82  | 8.1  | 7.9  |
|      | 13   | 26   | 35   | 39    | 46   | 65   |

Castings 52.7  
53.0  
7.5 7.8  
93 Ent

Top Hyd SE Cor. Fernwood 4 "B"

| Sta | + | $\Delta$ | - | Elev |
|-----|---|----------|---|------|
|-----|---|----------|---|------|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 958.98 |  |  |
|--|--|--------|--|--|

|       |  |  |  |  |
|-------|--|--|--|--|
| 13+47 |  |  |  |  |
|-------|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +64 |  |  |  |  |
|-----|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +70 |  |  |  |  |
|-----|--|--|--|--|

|    |  |  |  |  |
|----|--|--|--|--|
| 14 |  |  |  |  |
|----|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +42 |  |  |  |  |
|-----|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +78 |  |  |  |  |
|-----|--|--|--|--|

FK  
DS  
LPD  
ML

11-17-63

LT

E

BT

49

|    |      |      |      |      |      |      |      |      |
|----|------|------|------|------|------|------|------|------|
|    | 55.1 | 54.1 | 54.1 | 54.2 | 53.7 | 52.5 | 53.1 | 53.5 |
| NG | 39   | 49   | 49   | 48   | 53   | 65   | 59   | 55   |
|    | 42   | 24   | 15   |      | 13   | 22   | 44   | 68   |

|      |      |         |      |      |      |      |      |      |      |      |
|------|------|---------|------|------|------|------|------|------|------|------|
| 55.6 | 55.4 | 54.4    | 53.5 | 53.8 | 54.1 | 53.5 | 52.3 | 52.4 | 54.2 | 54.8 |
| 34   | 36   | 464     | 583  | 5.2  | 4.9  | 55   | 6.7  | 66   | 4.8  | 42   |
| 50   | 45   | 33      | 21   | 15   |      | 12   | 25   | 29   | 41   | 64   |
| MH   |      | Casting |      |      |      |      |      |      |      |      |

|      |      |      |      |      |      |
|------|------|------|------|------|------|
| 55.8 | 55.2 | 53.1 | 53.4 | 53.7 | 54.1 |
| 32   | 38   | 53   | 56   | 53   | 4.9  |
| 50   | 42   | 26   | 22   | 16   |      |

|      |      |      |      |      |      |
|------|------|------|------|------|------|
| 55.3 | 54.9 | 53.8 | 53.4 | 53.5 | 53.8 |
| 37   | 4.1  | 5.2  | 56   | 5.5  | 5.2  |
| 47   | 40   | 26   | 21   | 16   |      |
| NG   |      |      |      |      |      |

|      |      |      |      |      |
|------|------|------|------|------|
| 54.9 | 54.0 | 53.2 | 53.3 | 53.5 |
| 4.1  | 50   | 5.8  | 57   | 5.5  |
| 54   | 33   | 21   | 15   |      |

|      |      |      |      |      |      |
|------|------|------|------|------|------|
| 54.6 | 53.7 | 53.0 | 52.5 | 52.9 | 53.2 |
| 44   | 53   | 6.0  | 6.5  | 6.1  | 5.8  |
| 52   | 39   | 25   | 21   | 15   |      |



Sta +  $\pi$  - Elev

958.98

15

+18

+29

+40

+70

+91

TP 3,80955.61 7.17 951.81

11

11-17-65

84 50

54.3 53.3 52.7 52.4 52.7 53.1  
4.7 5.7 6.3 6.6 6.3 5.9  
53 41 24 21 15

53.4 52.8 52.3 52.5 53.0  
5.6 6.2 6.7 6.5 6.0  
47 34 23 14

54.3 53.4 52.8 52.1 52.4 52.8  
4.7 5.6 6.2 6.9 6.6 6.2  
59 48 36 23 14

49.9 51.1 52.0 51.7 52.3 52.7  
9.1 7.9 7.0 7.3 6.7 6.3  
53 45 30 25 14

49.4 50.4 51.7 51.1 52.1 52.4  
9.6 8.6 7.3 7.9 6.9 6.6  
50 40 32 25 13

49.5 49.9 51.3 51.1 52.0 52.3  
9.5 9.1 7.7 7.9 7.0 6.7  
50 40 32 26 14

E. E Cn/v.

Sta +  $\pi$  - Elev

955.61

16 + 00

+ 50

+ 83

17

+ 43

+ 77

Nov. 13, 1965

2+

51

49.9 49.9 51.5 51.0 52.0 52.2  
5.7 5.7 4.1 4.6 3.6 3.4  
50 40 32 26 13

49.0 49.2 50.8 50.5 51.1 51.5 51.9  
6.6 6.4 4.8 5.1 4.4 4.1 3.7  
53 43 32 26 MH 14  
21

48.9 49.4 50.8 50.3 51.4 51.6  
6.7 6.2 4.9 5.3 4.2 4.0  
50 40 32 26 13

48.9 49.4 50.5 50.2 51.4 51.6  
6.8 6.2 5.1 5.4 4.2 4.0  
50 41 32 26 13

49.1 50.1 50.0 51.2 51.4  
6.5 5.5 5.6 4.4 4.2  
51 36 26 13

49.2 49.6 49.3 50.5 50.8 51.1  
6.4 6.0 6.3 5.1 4.8 4.5  
50 37 27 19 12



Sta +  $\pi$  - Elev

955.61

18+00

BM 0.06 954.3<sup>9</sup>~~3~~ 1.28 954.33 (954.31)

+40

+62 Ent Rt

+88

19

+40

T.P. 5.20 952.4<sup>3</sup>~~4~~ 6.96 947.4<sup>3</sup>~~4~~ (947.44)

Nov. 12, 1965

LT

RT

52

|      |      |      |         |      |      |         |      |      |      |      |
|------|------|------|---------|------|------|---------|------|------|------|------|
| 48.3 | 48.8 | 49.1 | 48.3    | 50.5 | 50.8 | 50.5    | 49.3 | 50.5 | 51.5 | 52.3 |
| 7.3  | 6.8  | 6.5  | 7.3     | 5.1  | 4.8  | 5.1     | 6.28 | 5.1  | 4.1  | 3.3  |
| MH   | 54   | 41   | 25      | 11   |      | 11      | 20   | 26   | 30   | 54   |
| 49   |      |      | Casting |      |      | Casting |      |      |      |      |

Top Hyd by H<sub>2</sub> #1178

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 49.1 | 49.0 | 49.2 | 49.8 | 50.1 | 49.9 | 49.6 | 49.9 | 51.3 | 51.9 |
| 5.3  | 5.4  | 5.2  | 4.6  | 4.3  | 4.5  | 4.8  | 4.5  | 3.1  | 2.5  |
| 51   | 41   | 23   | 12   |      | 10   | 19   | 25   | 33   | 50   |

|      |      |      |      |      |      |      |      |             |      |      |
|------|------|------|------|------|------|------|------|-------------|------|------|
| 49.2 | 49.2 | 49.1 | 49.4 | 49.7 | 49.6 | 49.8 | 49.5 | 51.1        | 51.5 | 52.0 |
| 5.2  | 5.2  | 5.3  | 5.0  | 4.7  | 4.8  | 4.6  | 4.9  | 3.31        | 2.89 | 2.43 |
| 53   | 43   | 25   | 14   |      | 11   | 22   | 28   | 34          | 45   | 57   |
|      |      |      |      |      |      |      |      | Conc Joints |      |      |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 49.1 | 49.2 | 49.0 | 49.0 | 49.3 | 49.2 | 48.9 | 49.4 | 50.2 | 50.7 |
| 5.3  | 5.2  | 5.4  | 5.4  | 5.1  | 5.2  | 5.5  | 5.0  | 4.2  | 3.7  |
| 53   | 41   | 24   | 13   |      | 11   | 21   | 29   | 43   | 53   |

|      |      |      |      |      |      |      |      |       |      |
|------|------|------|------|------|------|------|------|-------|------|
| 48.9 | 48.9 | 48.8 | 48.9 | 49.2 | 49.0 | 48.9 | 49.0 | 50.1  | 50.4 |
| 5.5  | 5.5  | 5.6  | 5.5  | 5.2  | 5.4  | 5.5  | 5.40 | 4.33  | 4.00 |
| 53   | 42   | 24   | 14   |      | 11   | 20   | 24   | 43    | 50   |
|      |      |      |      |      |      |      |      | Conc. |      |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 49.0 | 48.1 | 48.4 | 48.7 | 48.8 | 48.5 | 48.1 | 47.8 | 48.4 | 48.9 | 50.5 |
| 5.4  | 5.7  | 6.0  | 5.7  | 5.6  | 5.9  | 6.3  | 6.6  | 4.0  | 5.5  | 3.9  |
| 52   | 36   | 25   | 15   |      | 12   | 18   | 24   | 28   | 37   | 53   |

Top CB, RT +65

Sta +  $\pi$  - Elev.

952.1<sup>3</sup>~~6~~

19+65

+86

20

+34

+62

21

Ent Lt.

Nov. 17, 1965

LT

RT

53

| 48.2 | 48.0 | 48.3 | 48.4 | 48.6 | 48.3 | 47.6 | 47.2 | 47.7 | 49.2 | 50.1 |
|------|------|------|------|------|------|------|------|------|------|------|
| 44   | 46   | 43   | 42   | 40   | 43   | 50   | 54   | 49   | 34   | 25   |
| 55   | 39   | 22   | 14   |      | 13   | 17   | 22   | 27   | 36   | 53   |

| 48.2 | 48.1 | 48.1 | 48.9 | 48.6 | 48.3 | 47.9 | 47.6 | 48.1 | 49.5 | 50.1 | 49.6 |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 44   | 45   | 45   | 42   | 40   | 43   | 47   | 50   | 45   | 31   | 25   | 30   |
| 52   | 40   | 24   | 14   |      | 11   | 19   | 22   | 27   | 34   | 41   | 51   |

Fe

| 49.1 | 48.9 | 48.0 | 47.9 | 48.2 | 48.5 | 48.3 | 47.8 | 47.8 | 49.1 | 49.9 | 48.9 | 49.9 |
|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 3.5  | 4.20 | 4.6  | 4.7  | 4.4  | 4.1  | 4.3  | 4.8  | 4.8  | 3.5  | 2.7  | 2.8  | 2.7  |
| 93   | 54   | 34   | 23   | 16   |      | 11   | 19   | 24   | 33   | 42   | 45   | 53   |

House Walk Fe

| 48.5 | 48.1 | 47.9 | 47.6 | 48.0 | 48.3 | 48.1 | 47.8 | 47.7 | 48.1 | 49.2 | 49.8 | 49.6 | 49.1 |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 4.11 | 4.46 | 4.7  | 5.0  | 4.6  | 4.3  | 4.5  | 4.8  | 4.9  | 4.5  | 3.4  | 2.8  | 3.0  | 2.7  |
| 63   | 50   | 31   | 23   | 15   |      | 11   | 19   | 25   | 29   | 34   | 42   | 45   | 55   |

Conc Fe

| 48.7 | 48.4 | 48.1 | 47.4 | 47.2 | 47.7 | 48.1 | 47.9 | 47.6 | 48.2 | 49.2 | 49.7 | 49.4 | 48.5 |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 3.9  | 4.2  | 4.5  | 5.2  | 5.4  | 4.9  | 4.5  | 4.7  | 5.0  | 4.4  | 3.4  | 2.9  | 3.2  | 3.1  |
| 33   | 62   | 40   | 27   | 23   | 16   |      | 12   | 17   | 26   | 33   | 43   | 45   | 51   |

House Fe

| 48.1 | 47.9 | 47.8 | 47.3 | 47.1 | 47.6 | 48.0 | 47.7 | 47.4 | 48.2 | 49.2 | 49.7 | 48.7 | 48.8 |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 4.5  | 4.7  | 4.8  | 5.3  | 5.5  | 5.0  | 4.6  | 4.9  | 5.2  | 4.4  | 3.4  | 2.9  | 3.9  | 3.8  |
| 75   | 52   | 38   | 29   | 23   | 16   |      | 11   | 21   | 27   | 33   | 43   | 46   | 51   |

Fe



Sta +  $\pi$  - Elev.

<sup>3</sup>  
952.4~~X~~

21+30 Ent Rt + Lt

+76

|      |      |                                     |      |                                     |        |
|------|------|-------------------------------------|------|-------------------------------------|--------|
| BM   | 3.80 | <sup>19</sup><br>955.2 <del>2</del> | 1.24 | <sup>39</sup><br>951.4 <del>0</del> | 951.42 |
| T.P. |      |                                     | 2.78 | <sup>1</sup><br>947.4 <del>4</del>  | ✓      |
| BM   |      |                                     | 0.90 | <sup>29</sup><br>954.3 <del>2</del> | 954.31 |

Nov. 17, 1965

LT

RT

54

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 48.9 | 48.1 | 47.4 | 47.1 | 47.6 | 47.9 | 47.7 | 47.5 | 47.7 | 48.0 | 48.6 | 48.8 |
| 3.73 | 4.52 | 5.2  | 5.5  | 5.0  | 4.7  | 4.9  | 5.1  | 4.9  | 4.6  | 4.0  | 3.8  |
| 63   | 43   | 28   | 23   | 16   |      | 11   | 17   | 23   | 30   | 46   | 59   |

conc

|      |      |      |      |      |      |      |      |      |         |      |      |
|------|------|------|------|------|------|------|------|------|---------|------|------|
| 48.5 | 48.0 | 47.2 | 45.7 | 47.3 | 47.4 | 47.9 | 47.6 | 46.7 | 46.7    | 47.5 | 48.9 |
| 4.1  | 4.6  | 5.4  | 6.92 | 5.3  | 5.2  | 4.7  | 5.0  | 5.9  | 5.9     | 5.1  | 3.7  |
| 55   | 42   | 27   | 22   | 18   | 15   |      | 12   | 21   | Casting | 25   | 33   |

Casting

47.4

5.18  
33  
MH

|      |      |      |
|------|------|------|
| 48.8 | 48.7 | 49.6 |
| 3.8  | 3.9  | 3.0  |
| 51   | 46   | 41   |

Top Hyd by School  
C.B.

Top Hyd by Ho #1178

Sta +  $\pi$  - Elev

B.M 1.00 952.42

951.42

22+00 Ent Lt

✓

+04 Gutter Rt

+50

✓

+66  $\neq$  Ent

8-24-64

55

Top Hyd. By School

RT a

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 48.6 | 47.8 | 47.6 | 47.5 | 47.5 | 47.9 | 47.4 | 46.6 | 46.7 | 47.5 | 48.5 |
| 4.8  | 4.6  | 4.8  | 4.9  | 4.9  | 4.5  | 5.0  | 5.8  | 5.7  | 4.9  | 3.9  |
| 50   | 37   | 32   | 18   | 15   | 18   | 21   | 26   | 33   |      |      |

at House

|      |      |      |
|------|------|------|
| 48.7 | 48.6 | 49.5 |
| 3.7  | 3.8  | 2.9  |
| 50   | 36   | 42   |

|      |      |
|------|------|
| 47.9 | 48.6 |
| 4.5  | 3.8  |
| 33   | 45   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 47.7 | 47.4 | 47.4 | 47.2 | 47.6 | 47.4 | 47.5 | 48.1 | 49.2 | 49.3 |
| 4.7  | 5.0  | 5.0  | 5.2  | 4.8  | 5.0  | 4.9  | 4.3  | 3.2  | 3.1  |
| 50   | 40   | 24   | 20   | 15   | 19   | 29   | 33   | 40   |      |

|      |      |
|------|------|
| 48.7 | 48.4 |
| 3.7  | 4.0  |
| 50   | 44   |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 47.8 | 47.5 | 47.5 | 47.2 | 47.6 | 47.4 | 47.9 | 48.6 | 48.9 |
| 4.6  | 4.9  | 4.9  | 5.2  | 4.8  | 5.0  | 4.5  | 3.8  | 3.5  |
| 50   | 40   | 25   | 21   | 14   | 27   | 43   | 50   |      |



Sta +  $\pi$  - Elev.

95242

22+82

✓

23

✓

+14 Ent Lt.

✓

Lt

8-2465 56  
RT 6

| 48.8  | 47.5 | 47.9 | 47.7 | 47.1 | 47.5 | 47.2 | 46.9 | 46.9 | 47.5 | 48.4 |
|-------|------|------|------|------|------|------|------|------|------|------|
| 3.65  | 4.9  | 4.5  | 4.7  | 5.3  | 4.9  | 5.2  | 6.0  | 6.0  | 4.9  | 4.0  |
| House | 14   | 50   | 42   | 23   | 17   | 19   | 21   | 23   | 33   |      |

| 48.9 | 48.7 | 49.2 |
|------|------|------|
| 3.5  | 3.7  | 3.2  |
| 50   | 42   | 40   |

| 47.6 | 47.6 | 47.2 | 47.0 | 47.5 | 47.5 | 47.2 | 48.8 | 47.2 | 48.3 |
|------|------|------|------|------|------|------|------|------|------|
| 4.8  | 4.8  | 5.2  | 5.4  | 4.9  | 4.9  | 5.2  | 5.6  | 5.2  | 4.1  |
| 50   | 43   | 34   | 24   | 13   |      | 15   | 22   | 23   | 33   |

| 48.8 | 48.7 | 49.1 |
|------|------|------|
| 3.6  | 3.7  | 3.3  |
| 50   | 42   | 41   |

| 47.6 | 47.5 | 47.2 | 47.4 | 47.5 | 47.1 | 47.4 | 47.4 | 48.4 | 49.0 |
|------|------|------|------|------|------|------|------|------|------|
| 4.8  | 4.9  | 5.2  | 5.0  | 4.9  | 5.3  | 5.4  | 5.0  | 4.0  | 3.4  |
| 50   | 35   | 23   | 15   |      | 15   | 21   | 24   | 33   | 42   |

| 48.8 | 48.6 |
|------|------|
| 3.6  | 3.8  |
| 50   | 45   |

Sta +  $\pi$  - Elev.

952.48

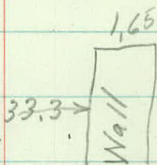
23+50

✓

+57 Gutter Rt

24

T.P. 1.90 952.74 1.58 950.84



+31 Ent Rt

✓

Lt.

8-24-65 Rt 57  
0

4.3 4.9 4.9 4.7 4.4 4.6 4.6 4.3 4.0 4.4 4.1  
4.13 4.5 4.5 4.7 5.0 4.8 4.8 5.1 5.4 5.0 4.3 3.3  
Walk 50 44 32 20 8 14 21 24 32 41

4.6 4.4  
3.8 4.0  
50 45

4.0 4.3  
4.4 4.1  
33 42

4.3 4.1 4.8 4.3 4.6 4.7 4.3 4.1 4.6 4.3 4.1  
4.12 4.3 4.6 4.9 4.8 4.7 4.9 5.3 4.8 3.7  
Walk 50 37 24 14 13 22 33 50  
N.W. Cor wall

4.1 4.9 4.3 4.6 4.7 4.9 4.1 4.3 4.8  
4.6 4.8 5.2 5.1 5.0 5.2 5.6 5.4 4.9  
50 41 23 11 13 22 23 32

4.6 4.3 4.5 4.0  
4.1 4.4 4.22 4.72  
50 45 0 0  
35



Sta +  $\pi$  - Elev.

952.74

24+50

✓

25

+28 Walk Lt.

+50

26

✓

BM

2.22

953.35

1.65

951.09

951.13

8-24-64

58

Lt.

Rt.

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 48.2 | 47.9 | 47.6 | 47.6 | 47.7 | 47.5 | 47.2 | 47.9 | 47.9 | 47.5 |
| 4.5  | 4.8  | 5.1  | 5.1  | 5.0  | 5.2  | 5.5  | 4.8  | 4.8  | 4.2  |
| 50   | 32   | 21   | 11   |      | 15   | 21   | 33   |      |      |

G C  
wall 35

|      |      |      |
|------|------|------|
| 48.8 | 48.6 | 48.3 |
| 3.9  | 4.1  | 4.4  |
| 55   | 50   | 42   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 48.3 | 48.1 | 47.6 | 47.6 | 47.6 | 47.5 | 47.4 | 48.1 | 48.3 | 48.8 |
| 4.4  | 4.6  | 5.1  | 5.1  | 5.1  | 5.2  | 5.3  | 4.6  | 4.4  | 3.9  |
| 50   | 37   | 21   | 11   |      | 15   | 21   | 33   | 35   | 50   |

Wall

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 48.3 | 48.4 | 47.9 | 47.6 | 47.5 | 47.5 | 47.5 | 48.1 | 48.3 | 48.6 | 48.8 |
| 4.19 | 4.3  | 4.8  | 5.1  | 5.2  | 5.2  | 5.2  | 4.6  | 4.35 | 4.08 | 3.88 |
| 8/09 | 50   | 33   | 15   |      | 15   | 21   | 33   | 33   | 41   | 50   |

Walk

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 48.3 | 48.2 | 48.1 | 47.5 | 47.7 | 47.5 | 47.6 | 48.1 | 48.4 | 48.9 |
| 4.4  | 4.5  | 4.6  | 5.2  | 5.0  | 5.2  | 5.1  | 4.6  | 4.3  | 3.8  |
| 50   | 42   | 31   | 13   |      | 14   | 25   | 33   | 35   | 50   |

Wall

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 47.9 | 47.8 | 48.0 | 47.6 | 47.6 | 47.8 | 47.6 | 47.5 | 48.0 | 48.0 |
| 4.8  | 4.9  | 4.76 | 5.12 | 5.1  | 4.9  | 5.1  | 5.2  | 4.71 | 4.71 |
| 50   | 44   | C    | G    | 15   |      | 15   | G    | C    | GV   |

23

23

27

|      |      |
|------|------|
| 48.2 | 48.1 |
| 50.3 |      |
| 4.5  | 4.6  |
| 50   | 33   |

Wall

Top Hyd S.W. Cor Lex. 4B

Sta +  $\pi$  - Elev.

953.35

26+12

+04 MHL 5.52 947.83

25+84 Lt. 24' MH <sup>Storm</sup> Sewer 5.70 47.65

✓

+21

+35  $\pm$  Lexington

✓

+48

+52 MHL 21' 5.50 947.85

8-2465

59

Lt

✓

Rt

e

|      |      |      |      |      |      |                |      |      |      |      |      |
|------|------|------|------|------|------|----------------|------|------|------|------|------|
| 48.1 | 47.7 | 47.6 | 47.8 | 47.6 | 47.8 | 47.9           | 47.7 | 47.7 | 47.7 | 47.9 | 47.8 |
| 5.26 | 5.7  | 5.8  | 5.6  | 5.8  | 5.6  | 5.5            | 5.7  | 5.7  | 5.7  | 5.50 | 5.6  |
| C    | G    | 50   | 39   | 32   | 16   |                | 17   | 32   | 42   | C    | 50   |
| 72   |      |      |      |      |      | 42 Carb Broken |      |      |      |      |      |

|      |      |      |      |   |      |      |
|------|------|------|------|---|------|------|
| 47.4 | 48.1 | 47.4 | 48.1 |   | 47.9 | 47.8 |
| 6.0  | 5.30 | 5.95 | 5.33 |   | 5.5  | 5.6  |
| G    | C    | G    | C    |   | 100  | 72   |
| 91   |      | 100  |      | ✓ |      |      |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 47.8 | 47.9 | 47.9 | 47.9 | 48.0 | 47.9 | 47.9 |
| 5.6  | 5.5  | 5.5  | 5.5  | 5.4  | 5.5  | 5.5  |
| 50   | 25   | 9    |      | 8    | 25   | 50   |

✓

|      |      |      |      |      |       |      |      |      |      |      |
|------|------|------|------|------|-------|------|------|------|------|------|
| 48.1 | 48.1 | 48.2 | 48.2 | 48.2 | 48.1  | 48.3 | 48.3 | 48.3 | 48.3 | 48.3 |
| 5.3  | 5.3  | 5.2  | 5.2  | 5.2  | Hole  | 5.1  | 5.1  | 5.1  | 5.1  | 5.1  |
| 100  | 75   | 50   | 25   | 6    | Patch | 6    | 18   | 35   | 50   | 77   |

|      |      |      |
|------|------|------|
| 48.1 | 48.1 | 48.1 |
| 5.3  | 5.3  | 5.3  |
| 125  | 150  | 200  |

|      |      |      |      |
|------|------|------|------|
| 48.5 | 48.4 | 48.4 | 48.4 |
| 4.9  | 5.0  | 5.0  | 5.0  |
| 200  | 150  | 125  | 100  |

✓

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 47.9 | 47.9 | 47.9 | 47.9 | 48.0 | 48.1 | 48.1 | 48.1 | 48.0 | 47.9 | 48.2 | 48.2 |
| 5.5  | 5.5  | 5.5  | 5.5  | 5.4  | 5.3  | 5.3  | 5.3  | 5.4  | 5.5  | 5.2  | 5.2  |
| 100  | 75   | 50   | 46   | 26   | 11   |      | 10   | 38   | 50   | 82   | 100  |



Sta +  $\pi$  - Elev.

953.35

26+56

+66

✓

BM 3.33 954.46 2.22 951.13 (951.13)

+

ICB

6.76

27+00

+45

+71

✓

Lt

8-24-64 60  
RT f

|      |      |      |      |      |      |      |     |      |      |     |      |
|------|------|------|------|------|------|------|-----|------|------|-----|------|
| 11.1 | 11.6 | 8.02 | 11.7 | 11.7 | 11.9 | 8.2  | 8.0 | 8.27 | 11.9 | 8.0 | 8.4  |
| 5.7  | 5.8  | 5.33 | 5.7  | 5.7  | 5.5  | 5.2  | 5.4 | 5.07 | 5.5  | 5.4 | 4.97 |
| 100  | 75   | C    | G    | 38   | 20   | N.H. | 16  | Curb | 50   | G   | C    |
|      |      | 50   |      |      |      |      |     | 46   |      |     | 76   |

Top Hyd SW. Cor Lex + B

|      |      |      |
|------|------|------|
| 11.8 | 11.5 | 11.2 |
| 5.57 | 4.90 | 5.2  |
| A3   | C    | G    |
| CB   | 100  |      |

|     |     |     |     |     |     |     |      |      |      |
|-----|-----|-----|-----|-----|-----|-----|------|------|------|
| 9.0 | 8.5 | 7.8 | 7.9 | 8.2 | 8.0 | 7.9 | 8.4  | 8.6  | 8.8  |
| 55  | 6.0 | 6.7 | 6.6 | 6.3 | 6.5 | 6.6 | 6.05 | 5.92 | 5.67 |
| 50  | 34  | 22  | 16  |     | 14  | 21  | 27   | 33   | 50   |
| BT  | BT  |     |     |     |     |     | conc | conc | conc |

|     |     |     |     |     |     |     |      |      |      |
|-----|-----|-----|-----|-----|-----|-----|------|------|------|
| 8.5 | 8.4 | 8.1 | 8.3 | 8.4 | 8.2 | 8.0 | 8.7  | 8.8  | 9.1  |
| 6.0 | 6.1 | 6.5 | 6.2 | 6.1 | 6.3 | 6.5 | 5.80 | 5.72 | 5.44 |
| 50  | 31  | 21  | 15  |     | 15  | 21  | 27   | 33   | 50   |
| BT  | BT  |     |     |     |     |     | conc | conc | conc |

|     |     |     |     |     |     |     |     |      |      |      |
|-----|-----|-----|-----|-----|-----|-----|-----|------|------|------|
| 8.6 | 8.8 | 9.1 | 8.3 | 8.4 | 8.7 | 8.5 | 8.2 | 8.8  | 8.9  | 8.9  |
| 6.0 | 5.7 | 5.4 | 6.2 | 6.1 | 5.8 | 6.0 | 6.3 | 5.7  | 5.62 | 5.56 |
| 50  | 34  | 32  | 24  | 16  |     | 13  | 21  | 22   | 27   | 32   |
| BT  | BT  |     |     |     |     |     |     | CURB | SW   | SW   |

|     |     |
|-----|-----|
| 8.7 | 8.5 |
| 5.8 | 6.0 |
| 50  | 37  |

| Sta | + | T | - | Elev |
|-----|---|---|---|------|
|-----|---|---|---|------|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 954.46 |  |  |
|--|--|--------|--|--|

|       |  |  |  |  |
|-------|--|--|--|--|
| 28+00 |  |  |  |  |
|-------|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +40 |  |  |  |  |
|-----|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +64 |  |  |  |  |
|-----|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +76 |  |  |  |  |
|-----|--|--|--|--|

|    |      |        |      |        |
|----|------|--------|------|--------|
| TP | 3.50 | 957.31 | 0.65 | 953.81 |
|----|------|--------|------|--------|

|     |  |  |  |  |
|-----|--|--|--|--|
| +87 |  |  |  |  |
|-----|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ↓ |  |  |  |  |
|---|--|--|--|--|

LT

E/

RT

61

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 49.3 | 49.1 | 49.1 | 48.9 | 48.6 | 48.8 | 49.1 | 48.8 | 48.5 | 48.7 | 49.3 |
| 5.2  | 5.4  | 5.4  | 5.6  | 5.9  | 5.69 | 5.4  | 5.7  | 6.0  | 5.8  | 5.18 |
| 50   | 34   | 29   | 24   | 22   | 20   |      | 14   | 22   | 30   | conc |

MH

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 49.5 | 49.6 | 50.0 | 49.1 | 49.5 | 49.7 | 49.4 | 49.2 | 49.0 | 49.6 | 49.0 |
| 5.0  | 4.9  | 4.5  | 5.4  | 5.0  | 4.8  | 5.1  | 5.3  | 5.5  | 5.5  | 5.5  |
| 50   | 34   | 32   | 21   | 14   |      | 13   | 22   | 23   | 43   | 50   |

BT

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 49.9 | 50.2 | 49.9 | 50.0 | 50.1 | 49.9 | 49.7 | 49.8 | 49.6 |
| 4.6  | 4.3  | 4.6  | 4.5  | 4.4  | 4.6  | 4.8  | 4.7  | 4.9  |
| 50   | 30   | 21   | 15   |      | 13   | 22   | 35   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 50.0 | 50.3 | 50.3 | 50.1 | 50.2 | 50.3 | 50.1 | 49.9 | 49.9 | 50.1 | 50.1 | 49.8 |
| 4.5  | 4.2  | 4.2  | 4.4  | 4.3  | 4.2  | 4.4  | 4.6  | 4.7  | 4.4  | 4.4  | 4.7  |
| 50   | 34   | 27   | 21   | 16   |      | 14   | 21   | 23   | 25   | 33   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 51.0 | 51.3 | 50.4 | 50.3 | 50.2 | 50.3 | 50.3 | 50.1 | 50.0 | 49.9 | 50.0 | 49.9 |
| 6.3  | 6.0  | 6.9  | 7.0  | 7.1  | 7.0  | 7.0  | 7.2  | 7.3  | 7.4  | 7.3  | 7.4  |
| 33   | 30   | 27   | 24   | 22   | 15   |      | 14   | 21   | 22   | 34   | 50   |

|      |      |      |
|------|------|------|
| 13.8 | 13.7 | 13.6 |
| 5    | 5    | 5    |
| 3.5  | 3.6  | 3.7  |
| 37   | 40   | 50   |



| Sta | + | T. | - | Elev |
|-----|---|----|---|------|
|-----|---|----|---|------|

| Sta | + | T.     | - | Elev |
|-----|---|--------|---|------|
|     |   | 957.31 |   |      |

| Sta   | + | T. | - | Elev |
|-------|---|----|---|------|
| 29+00 |   |    |   |      |

| Sta | + | T. | - | Elev |
|-----|---|----|---|------|
| +15 |   |    |   |      |

| Sta | + | T. | - | Elev |
|-----|---|----|---|------|
| +27 |   |    |   |      |

| Sta | + | T. | - | Elev |
|-----|---|----|---|------|
| +80 |   |    |   |      |

| Sta   | + | T. | - | Elev |
|-------|---|----|---|------|
| 30+00 |   |    |   |      |

| Sta | + | T. | - | Elev |
|-----|---|----|---|------|
| +15 |   |    |   |      |

L T

E

R +

62  
h

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 52.1 | 52.1 | 51.3 | 51.5 | 50.7 | 50.7 | 50.5 | 50.3 | 50.4 | 50.4 |
| 4.8  | 5.2  | 6.0  | 6.8  | 6.6  | 6.6  | 6.8  | 7.0  | 6.9  | 6.9  |
| 50   | 41   | 25   | 22   | 14   |      | 11   | 20   | 36   | 50   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 52.8 | 52.2 | 51.9 | 50.8 | 51.0 | 50.9 | 50.6 | 50.4 | 50.9 | 50.4 |
| 4.47 | 5.13 | 5.4  | 6.5  | 6.3  | 6.4  | 6.7  | 6.9  | 6.4  | 6.9  |
| 50   | 34   | 30   | 21   | 12   |      | 14   | 22   | 33   | 50   |

conc conc

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 51.0 | 51.5 | 51.9 | 50.9 | 51.2 | 51.0 | 50.8 | 50.6 | 50.9 | 50.4 |
| 4.3  | 4.8  | 5.4  | 6.4  | 6.1  | 6.3  | 6.5  | 6.7  | 6.4  | 6.9  |
| 50   | 38   | 27   | 21   | 14   |      | 13   | 21   | 34   | 50   |

|       |      |      |      |      |      |      |      |      |      |      |
|-------|------|------|------|------|------|------|------|------|------|------|
| 54.3  | 52.4 | 51.2 | 51.8 | 51.3 | 51.6 | 51.7 | 51.4 | 51.4 | 51.0 | 51.0 |
| 3.03  | 4.70 | 5.08 | 5.48 | 6.0  | 5.7  | 5.6  | 5.9  | 5.9  | 6.3  | 6.3  |
| House | 50   | 40   | 27   | 22   | 13   |      | 15   | 18   | 37   | 50   |

conc conc conc

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 52.6 | 52.5 | 51.9 | 51.4 | 51.8 | 51.5 | 51.5 | 50.9 | 51.2 | 51.2 |
| 4.7  | 4.8  | 5.4  | 5.9  | 5.5  | 5.8  | 5.8  | 6.4  | 6.1  | 6.1  |
| 50   | 38   | 26   | 22   |      | 16   | 18   | 27   | 46   | 50   |

|       |      |      |      |      |      |      |      |      |      |      |       |
|-------|------|------|------|------|------|------|------|------|------|------|-------|
| 53.1  | 52.6 | 52.5 | 52.5 | 51.5 | 51.5 | 51.7 | 51.5 | 51.4 | 51.2 | 51.2 | 51.3  |
| 4.15  | 4.7  | 4.8  | 4.8  | 5.8  | 5.8  | 5.6  | 5.8  | 5.9  | 6.1  | 6.1  | 5.98  |
| House | 50   | 42   | 31   | 23   | 17   |      | 15   | 20   | 37   | 50   | House |

| Sta | + | 1      | - | Elev |
|-----|---|--------|---|------|
|     |   | 957.31 |   |      |

30+45

+58

|    |      |        |      |        |          |
|----|------|--------|------|--------|----------|
| TP | 1.57 | 955.35 | 3.49 | 953.82 | (953.78) |
|----|------|--------|------|--------|----------|

+79

31 Good for Ent Lt

+33

+54

[illegible]



Sta +  $\pi$  - Elev

955.35

32

+15 Ent Rt.

23  
24

TP 4.24 953.08 6.51 948.84

+28 Ent Lt.

+44

+83

33

Sept. 27, 1965

64

LT

✓

RI

✓

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 51.7 | 51.4 | 49.9 | 49.8 | 49.7 | 49.6 | 49.3 | 49.0 | 48.5 | 48.3 | 49.2 | 49.3 |
| 3.7  | 4.0  | 5.5  | 5.6  | 5.7  | 5.8  | 6.1  | 6.4  | 6.9  | 7.1  | 6.2  | 6.1  |
| 50   | 38   | 25   | 21   | 15   |      | 14   | 17   | 23   | 27   | 36   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 42.2 | 41.5 | 41.2 | 50.0 | 49.6 | 49.7 | 49.5 | 49.1 | 48.8 | 48.4 | 48.5 | 48.2 |
| 3.2  | 3.9  | 4.2  | 5.4  | 5.6  | 5.7  | 5.9  | 6.3  | 6.6  | 7.0  | 6.9  | 6.8  |
| Ho   | 50   | 39   | 29   | 23   | 14   |      | 14   | 20   | 27   | 40   | 50   |

Top N.W. Cor Bottom Step Ho #1044

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 50.1 | 50.1 | 49.8 | 49.6 | 49.6 | 49.4 | 49.0 | 48.8 | 48.1 | 48.3 | 48.3 |
| 3.0  | 3.0  | 3.3  | 3.5  | 3.5  | 3.7  | 4.1  | 4.3  | 5.0  | 4.8  | 4.8  |
| 50   | 43   | 28   | 18   | 15   |      | 13   | 18   | 24   | 37   | 60   |

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 51.6 | 51.8 | 51.4 | 49.6 | 49.4 | 49.4 | 49.3 | 48.7 | 48.6 | 48.8 | 48.1 | 48.3 |
| 1.50 | 1.3  | 1.7  | 2.5  | 3.7  | 3.7  | 3.8  | 4.4  | 4.5  | 5.3  | 5.0  | 4.8  |
| 10   | 50   | 36   | 25   | 21   | 16   |      | 14   | 18   | 25   | 33   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 51.8 | 51.6 | 49.1 | 49.1 | 49.1 | 49.2 | 48.4 | 48.3 | 47.3 | 47.6 | 47.6 |
| 1.3  | 1.5  | 4.0  | 4.0  | 4.0  | 3.9  | 4.7  | 4.8  | 5.8  | 5.5  | 5.5  |
| 50   | 43   | 26   | 21   | 17   |      | 15   | 18   | 26   | 32   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 48.7 | 48.9 | 49.6 | 48.9 | 49.0 | 48.4 | 48.2 | 47.3 | 47.6 | 47.7 | 47.7 |
| 4.4  | 4.2  | 4.5  | 4.2  | 4.1  | 4.7  | 4.9  | 5.8  | 5.5  | 5.4  | 4.4  |
| 50   | 31   | 21   | 17   |      | 14   | 17   | 25   | 31   | 50   | Ho   |

Sta + x - Elev.

953.08

33+27 Ent Rt & Lt

+67

BM 3.63 951.43 5.26 947.82 (947.80)

34

+22 Ent Rt

+60

+84

FX  
LPD  
RW  
RP

Lt.

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Sept. 28, 1965 RT -6

48.6 47.9 49.0 49.0 48.4 48.6 48.7 48.1 47.1 47.4 47.1 47.9  
4.5 4.20 4.14 4.12 4.7 4.5 4.4 5.0 5.4 5.7 5.4 5.2  
Ho 50 43 31 20 17 13 18 27 41 50

Canc

48.4 48.3 48.1 47.9 48.0 48.1 48.3 47.8 47.6 46.6 47.1 47.3  
4.7 4.8 5.0 5.2 5.1 5.0 4.8 5.3 5.5 6.5 6.0 5.8  
50 41 29 23 20 16 13 16 25 33 50

Top Hyd N.W. Cor. Oxfordy + "B"

47.0 47.2 47.1 47.4 48.1 47.3 46.6 47.0 47.4 47.4  
4.4 4.2 4.3 4.0 3.3 4.1 4.8 4.4 4.0 4.04  
50 33 24 14 14 24 32 50 House

47.0 46.9 46.9 46.7 47.3 47.9 47.2 47.0 47.0 47.1  
4.38 4.5 4.5 4.7 4.3 3.5 4.2 4.4 4.4 4.3  
Ho 50 36 26 16 14 22 33 50

46.4 46.5 46.4 46.9 47.5 46.9 46.7 46.0 46.5 46.9  
50 49 50 4.5 3.9 4.5 4.7 5.4 4.9 4.5  
50 37 26 15 15 18 25 34 50

45.4 46.1 45.8 46.5 47.0 46.4 45.4 46.2 46.7 47.0  
6.0 5.3 5.6 4.9 4.4 5.0 5.8 5.2 4.7 4.4  
50 35 26 15 15 24 31 50 Ho



Sta +  $\pi$  - Elev

951.43

35 Ent. Rt Gutter Lt

+14  $\phi$  Oxford

✓

+23 Shoulder Lt

+44 P.L. Lt.

+55  $\phi$  Ent Rt

T.P. 4.59 949.47 6.55 944.88

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Lt Rt

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| x2.9 | x4.4 | x5.4 | x6.4 | x6.7 | x6.2 | x5.9 | x4.3 |
| 75   | 70   | 60   | 50   | 47   | 52   | 55   | 51   |
| 50   | 44   | 30   | 20   |      | 13   | 26   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| x2.6 | x4.1 | x5.0 | x6.0 | x6.2 | x6.5 | x6.0 | x5.2 | x3.6 | x2.9 | x2.6 |
| 88   | 73   | 64   | 54   | 52   | 49   | 54   | 62   | 78   | 86   | 88   |
| 75   | 50   | 36   | 20   | 16   |      | 12   | 22   | 29   | 47   | 50   |

MH

|      |      |      |
|------|------|------|
| x1.2 | x3.9 | x3.8 |
| 10.2 | 11.5 | 12.6 |
| 100  | 125  | 150  |

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| x4.3 | x5.3 | x6.2 | x6.4 | x5.9 | x5.2 | x3.9 | x2.8 |
| 71   | 61   | 52   | 50   | 55   | 62   | 75   | 86   |
| 50   | 29   | 13   |      | 12   | 21   | 29   | 50   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| x2.2 | x2.4 | x3.3 | x5.6 | x5.8 | x6.2 | x5.8 | x5.2 | x4.2 | x2.9 |
| 92   | 90   | 81   | 58   | 56   | 52   | 56   | 62   | 72   | 85   |
| 50   | 33   | 24   | 17   | 14   |      | 11   | 19   | 30   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| x2.1 | x2.2 | x2.7 | x5.6 | x5.9 | x6.1 | x5.6 | x5.3 | x4.2 | x3.8 | x3.6 |
| 89   | 92   | 87   | 58   | 55   | 53   | 58   | 61   | 72   | 76   | 78   |
| 50   | 35   | 25   | 16   | 13   |      | 13   | 18   | 30   | 39   | 50   |

N. Rim M.H. Lt 36 + 20 +

Sta +  $\pi$  - Elev.

949.47

36

+19

+46 Ent Rt

+69

37

BM 5.86 947.77 7.56 941.91 (941.91)

+25 Ent Lt.

FK  
LPD  
RW

Lt.

Sept. 28, 1965  
Oct. 1, 1965  
RT.

67  
m

| 43.3 | 42.1 | 43.0 | 45.4 | 45.7 | 45.9 | 45.4 | 45.0 | 43.3 | 43.2 |
|------|------|------|------|------|------|------|------|------|------|
| 6.2  | 6.8  | 6.5  | 4.1  | 3.8  | 3.6  | 4.1  | 4.5  | 6.2  | 6.3  |
| 50   | 33   | 26   | 17   | 15   |      | 13   | 19   | 29   | 50   |

| 43.3 | 42.7 | 44.9 | 45.5 | 45.8 | 45.3 | 45.1 | 45.5 | 43.0 |
|------|------|------|------|------|------|------|------|------|
| 6.2  | 6.8  | 4.59 | 4.0  | 3.7  | 4.2  | 4.4  | 6.0  | 6.5  |
| 50   | 29   | 17   | 12   |      | 14   | 18   | 30   | 50   |

MM

| 43.6 | 42.9 | 45.2 | 45.4 | 45.7 | 45.3 | 44.5 | 44.5 | 43.9 |
|------|------|------|------|------|------|------|------|------|
| 5.9  | 6.6  | 4.3  | 4.1  | 3.8  | 4.2  | 5.0  | 5.0  | 5.6  |
| 50   | 27   | 16   | 13   |      | 13   | 25   | 31   | 50   |

| 44.1 | 43.8 | 42.9 | 45.0 | 45.2 | 45.5 | 45.2 | 44.9 | 44.3 | 44.6 | 44.1 |
|------|------|------|------|------|------|------|------|------|------|------|
| 5.4  | 5.7  | 6.6  | 4.5  | 4.3  | 4.0  | 4.3  | 4.6  | 5.2  | 4.9  | 5.4  |
| 50   | 34   | 26   | 16   | 13   |      | 14   | 18   | 25   | 31   | 50   |

| 44.3 | 43.7 | 43.1 | 44.6 | 45.0 | 45.2 | 45.0 | 44.6 | 44.2 | 44.5 | 44.4 |
|------|------|------|------|------|------|------|------|------|------|------|
| 5.2  | 5.8  | 6.4  | 4.9  | 4.5  | 4.3  | 4.5  | 4.9  | 5.3  | 4.9  | 5.10 |
| 50   | 33   | 25   | 16   | 12   |      | 10   | 17   | 25   | 34   | 50   |

Roseville BM By H. H. 922 C. R. B. Cond Ent

| 44.2 | 44.1 | 44.3 | 44.7 | 44.9 | 44.7 | 44.4 | 43.8 | 44.6 | 44.5 |
|------|------|------|------|------|------|------|------|------|------|
| 3.6  | 3.7  | 3.5  | 3.1  | 2.9  | 3.1  | 3.4  | 4.0  | 3.2  | 3.3  |
| 50   | 26   | 18   | 11   |      | 11   | 18   | 24   | 33   | 50   |



Sta + X - Elev

947.77

37+50 Ent Lt.

+82 Ent Rt.

38

+27

+57

39 Ent Lt

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RT n

1+

| $\Delta 3.5$ | $\Delta 3.6$ | $\Delta 4.0$ | $\Delta 4.4$ | $\Delta 4.7$ | $\Delta 4.4$ | $\Delta 4.2$ | $\Delta 3.7$ | $\Delta 4.2$ | $\Delta 4.2$ |
|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| 4.3          | 4.2          | 3.8          | 3.4          | 3.1          | 3.4          | 3.6          | 4.1          | 3.6          | 3.6          |
| 50           | 29           | 17           | 12           |              | 12           | 17           | 24           | 31           | 50           |

| $\Delta 3.5$ | $\Delta 3.1$ | $\Delta 2.7$ | $\Delta 3.9$ | $\Delta 4.1$ | $\Delta 4.3$ | $\Delta 4.1$ | $\Delta 3.6$ | $\Delta 3.4$ | $\Delta 3.5$ | $\Delta 3.7$ |
|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| 4.3          | 4.7          | 5.1          | 3.9          | 3.7          | 3.5          | 3.7          | 4.2          | 4.4          | 4.25         | 4.11         |
| 50           | 29           | 26           | 18           | 13           |              | 10           | 18           | 25           | 32           | 50           |

Conc.

| $\Delta 3.5$ | $\Delta 3.2$ | $\Delta 2.6$ | $\Delta 3.6$ | $\Delta 3.9$ | $\Delta 4.2$ | $\Delta 3.9$ | $\Delta 3.5$ | $\Delta 3.2$ | $\Delta 3.5$ | $\Delta 3.7$ |
|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| 4.3          | 4.6          | 5.2          | 4.2          | 3.9          | 3.6          | 3.9          | 4.3          | 4.6          | 4.3          | 4.1          |
| 50           | 29           | 25           | 17           | 11           |              | 11           | 18           | 24           | 31           | 50           |

| $\Delta 3.0$ | $\Delta 2.9$ | $\Delta 2.3$ | $\Delta 2.5$ | $\Delta 3.7$ | $\Delta 3.9$ | $\Delta 3.7$ | $\Delta 3.4$ | $\Delta 3.0$ | $\Delta 2.4$ | $\Delta 2.5$ |
|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| 4.8          | 4.9          | 5.5          | 4.3          | 4.1          | 3.9          | 4.1          | 4.4          | 4.8          | 4.4          | 4.3          |
| 50           | 30           | 26           | 18           | 11           |              | 10           | 18           | 23           | 32           | 50           |

| $\Delta 3.1$ | $\Delta 3.1$ | $\Delta 2.3$ | $\Delta 3.0$ | $\Delta 3.3$ | $\Delta 3.5$ | $\Delta 3.7$ | $\Delta 3.6$ | $\Delta 3.2$ | $\Delta 2.8$ | $\Delta 2.5$ | $\Delta 2.5$ |
|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| 4.7          | 4.7          | 5.5          | 4.8          | 4.5          | 4.3          | 4.1          | 4.2          | 4.6          | 5.0          | 5.3          | 5.3          |
| 50           | 29           | 25           | 21           | 17           | 11           |              | 11           | 17           | 23           | 35           | 50           |

| $\Delta 3.0$ | $\Delta 3.0$ | $\Delta 2.1$ | $\Delta 2.9$ | $\Delta 3.1$ | $\Delta 3.3$ | $\Delta 3.1$ | $\Delta 2.8$ | $\Delta 2.4$ | $\Delta 2.5$ | $\Delta 2.5$ |
|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| 4.8          | 4.8          | 4.7          | 5.0          | 4.7          | 4.5          | 4.7          | 5.0          | 5.4          | 5.2          | 5.3          |
| 50           | 39           | 25           | 16           | 10           |              | 11           | 17           | 24           | 31           | 50           |

Sta +  $\pi$  - Elev

947.77

39+35 Ent. Rt.

✓

+ 81 Ent. Rt. 427

40

✓

TP 0.12<sup>+</sup> 945.12 2.77 945.00

+ 50

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RT 0

11

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 42.4 | 41.4 | 42.1 | 42.5 | 42.8 | 42.9 | 42.7 | 42.4 | 42.2 | 42.5 | 42.5 |
| 5.4  | 6.4  | 5.7  | 5.3  | 5.0  | 4.9  | 5.1  | 5.4  | 5.6  | 5.3  | 5.3  |
| 29   | 24   | 19   | 14   | 10   |      | 10   | 16   | 23   | 30   | 50   |

42.9 43.0  
→ 4.9 4.8  
3.5 5.0

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 42.7 | 42.6 | 42.5 | 42.1 | 42.3 | 42.3 | 42.3 | 41.9 | 42.2 | 42.1 |
| 5.1  | 5.2  | 5.3  | 5.7  | 5.5  | 5.5  | 5.5  | 5.9  | 5.6  | 5.7  |
| 50   | 35   | 22   | 16   | 11   |      | 11   | 25   | 32   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 41.7 | 41.0 | 41.9 | 42.0 | 42.1 | 42.2 | 42.1 | 41.9 | 41.6 | 41.6 | 41.7 |
| 6.1  | 6.8  | 5.9  | 5.8  | 5.7  | 5.6  | 5.7  | 5.9  | 6.2  | 6.2  | 6.1  |
| 28   | 24   | 17   | 14   | 10   |      | 11   | 18   | 26   | 32   | 50   |

42.1 41.9  
→ 5.7 5.9  
3.8 5.0

Hyd RT B<sub>4</sub> BM

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 41.9 | 41.4 | 41.0 | 41.4 | 41.4 | 41.6 | 41.7 | 41.7 | 41.5 | 40.9 | 41.2 | 41.4 |
| 3.2  | 3.7  | 4.1  | 3.7  | 3.7  | 3.5  | 3.4  | 3.4  | 3.6  | 4.2  | 3.9  | 3.7  |
| 40   | 29   | 24   | 21   | 15   | 12   |      | 12   | 15   | 24   | 32   | 50   |

41.7  
→ 3.4  
5.0



Sta +  $\pi$  - Elev.

945.12

40+62 Ent Lt.

+87

41

+31

+67 Ent R4L

42

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 Lt. 81 p

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 41.8 | 41.6 | 41.5 | 41.5 | 41.6 | 41.6 | 41.4 | 40.8 | 41.0 | 41.2 |
| 3.3  | 3.5  | 3.6  | 3.6  | 3.5  | 3.5  | 3.7  | 4.3  | 4.1  | 3.9  |
| 50   | 29   | 21   | 13   | 14   | 17   | 26   | 32   | 50   |      |

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 41.4 | 41.5 | 41.2 | 40.1 | 41.1 | 41.2 | 41.5 | 41.5 | 41.3 | 40.6 | 40.4 | 40.6 |
| 3.7  | 3.6  | 3.9  | 4.4  | 4.0  | 3.9  | 3.6  | 3.6  | 3.8  | 4.5  | 4.7  | 4.5  |
| 50   | 38   | 29   | 24   | 17   | 13   | 12   | 17   | 26   | 42   | 50   |      |

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 41.2 | 41.2 | 41.1 | 40.2 | 40.9 | 41.1 | 41.5 | 41.4 | 41.3 | 40.6 | 40.6 | 40.6 |
| 3.9  | 3.9  | 4.0  | 4.9  | 4.2  | 4.0  | 3.6  | 3.7  | 3.8  | 4.5  | 4.6  | 4.5  |
| 50   | 38   | 29   | 24   | 19   | 13   | 11   | 16   | 25   | 36   | 50   |      |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 41.1 | 40.8 | 40.9 | 40.7 | 41.1 | 41.3 | 41.2 | 40.9 | 40.5 | 40.6 |
| 4.0  | 4.3  | 4.2  | 4.4  | 4.0  | 3.8  | 3.9  | 4.2  | 4.6  | 4.5  |
| 50   | 33   | 23   | 18   | 13   | 12   | 16   | 25   | 50   |      |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 40.9 | 40.9 | 40.9 | 40.9 | 41.0 | 41.1 | 41.0 | 40.7 | 40.3 | 40.2 | 40.1 |
| 4.2  | 4.2  | 4.2  | 4.2  | 4.1  | 4.0  | 4.1  | 4.4  | 4.8  | 4.9  | 5.0  |
| 50   | 32   | 25   | 17   | 13   | 13   | 16   | 24   | 33   | 50   |      |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 40.6 | 40.4 | 39.8 | 40.6 | 40.7 | 40.8 | 40.7 | 40.5 | 39.7 | 40.2 | 40.2 |
| 4.5  | 4.7  | 5.3  | 4.5  | 4.4  | 4.3  | 4.4  | 4.6  | 5.4  | 4.9  | 4.9  |
| 50   | 30   | 23   | 16   | 14   | 14   | 17   | 25   | 31   | 50   |      |

Sta    +     $\pi$     -    Elev

945.12

42+25

+55 Ent Lt

+68 Ent Rt

✓

43

+35 Ent Lt

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Lt

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 40.4 | 40.2 | 39.6 | 40.5 | 40.6 | 40.5 | 40.2 | 39.4 | 39.3 | 39.2 |
| 4.7  | 4.9  | 5.5  | 4.5  | 4.5  | 4.6  | 4.9  | 5.7  | 5.8  | 5.8  |
| 50   | 28   | 24   | 15   |      | 12   | 17   | 24   | 32   | 50   |

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| 40.6 | 40.4 | 40.2 | 40.6 | 40.1 | 39.2 | 39.2 | 39.3 |
| 4.5  | 4.7  | 4.9  | 4.6  | 5.0  | 5.9  | 5.9  | 5.8  |
| 50   | 25   | 15   |      | 16   | 25   | 35   | 50   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 40.4 | 40.1 | 39.0 | 40.0 | 40.1 | 40.5 | 40.0 | 39.3 | 39.4 | 39.6 |
| 4.7  | 5.0  | 6.1  | 5.1  | 5.0  | 4.7  | 5.1  | 5.8  | 5.7  | 5.45 |
| 50   | 28   | 23   | 17   | 14   |      | 14   | 25   | G    | C    |
|      |      |      |      |      |      |      |      | 35   |      |

|      |      |
|------|------|
| 39.8 | 39.6 |
| 5.30 | 5.5  |
| C    | G    |
| 50   |      |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 40.4 | 39.9 | 39.0 | 39.6 | 39.7 | 40.3 | 39.8 | 39.4 | 39.1 | 39.2 | 39.1 |
| 4.7  | 5.2  | 6.1  | 5.5  | 5.4  | 4.7  | 5.3  | 5.7  | 6.0  | 5.9  | 6.0  |
| 50   | 29   | 23   | 17   | 15   |      | 14   | 20   | 24   | 29   | 50   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 40.4 | 40.1 | 40.0 | 39.8 | 40.3 | 39.9 | 39.5 | 39.3 | 39.5 | 39.4 |
| 4.7  | 5.0  | 5.1  | 5.3  | 4.8  | 5.2  | 5.6  | 5.8  | 5.6  | 5.7  |
| 50   | 36   | 25   | 14   |      | 14   | 21   | 26   | 32   | 50   |



Sta +  $\Delta$  - Elev

945.12

43+46

+70

44

BM 0.00 942.42 2.70 942.42

+25

(Both)  
+75 Ent S Rt.

45 Ent Lt

2 Oct. 1965 72

Lt

Rt

| 40.3 | 40.0 | 39.2 | 39.1 | 39.8 | 40.2 | 39.8 | 39.3 | 39.4 | 39.3 |
|------|------|------|------|------|------|------|------|------|------|
| 4.8  | 5.1  | 5.9  | 5.4  | 5.3  | 4.9  | 5.3  | 5.8  | 5.7  | 5.6  |
| 50   | 29   | 24   | 20   | 14   |      | 16   | 26   | 36   | 50   |

| 40.2 | 40.0 | 39.1 | 39.5 | 39.6 | 40.2 | 39.6 | 39.4 | 39.0 | 39.2 | 39.2 |
|------|------|------|------|------|------|------|------|------|------|------|
| 4.9  | 5.1  | 6.0  | 5.6  | 5.5  | 4.9  | 5.5  | 5.7  | 6.1  | 5.9  | 5.9  |
| 50   | 30   | 23   | 18   | 14   |      | 14   | 18   | 25   | 30   | 50   |

| 40.3 | 39.6 | 39.6 | 39.2 | 39.4 | 40.0 | 39.5 | 39.2 | 38.9 | 39.2 | 39.0 |
|------|------|------|------|------|------|------|------|------|------|------|
| 4.8  | 5.5  | 6.5  | 5.9  | 5.7  | 5.1  | 5.6  | 5.9  | 6.2  | 5.9  | 6.1  |
| 50   | 29   | 23   | 17   | 14   |      | 14   | 19   | 27   | 34   | 50   |

Top Hyd Rt Sta 44+

| 39.8 | 39.1 | 39.8 | 39.6 | 39.8 | 39.9 | 39.1 | 39.4 | 38.6 | 39.2 | 39.1 |
|------|------|------|------|------|------|------|------|------|------|------|
| 2.6  | 2.7  | 2.6  | 2.8  | 2.6  | 2.5  | 2.7  | 3.0  | 3.8  | 3.2  | 3.2  |
| 50   | 41   | 25   | 16   | 13   |      | 11   | 17   | 24   | 31   | 50   |

| 39.3 | 39.1 | 38.4 | 38.1 | 38.9 | 39.2 | 39.6 | 39.4 | 39.1 | 38.8 | 38.7 | 38.8 |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 3.1  | 3.3  | 3.6  | 4.3  | 3.5  | 3.2  | 2.8  | 3.0  | 3.3  | 3.6  | 3.7  | 3.6  |
| 50   | 38   | 26   | 22   | 16   | 12   |      | 11   | 17   | 26   | 38   | 50   |

| 39.1 | 39.0 | 38.8 | 39.0 | 39.4 | 39.2 | 39.0 | 38.4 | 38.7 | 38.5 |
|------|------|------|------|------|------|------|------|------|------|
| 3.3  | 3.4  | 6.6  | 3.4  | 3.0  | 3.2  | 3.4  | 4.0  | 3.7  | 3.9  |
| 50   | 24   | 17   | 12   |      | 12   | 17   | 25   | 31   | 50   |

Sta +  $\pi$  - Elev.

942.42

45+50

46 Ent Rt.

+12 Ent Rt

+62 Ent Rt

+83 Ent Lt

47

± Oct. 1, 1965

73

2+

R1

L

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 37.9 | 38.9 | 37.9 | 38.2 | 38.5 | 38.9 | 38.1 | 38.3 | 37.1 | 37.9 | 37.1 |
| 3.5  | 3.5  | 4.5  | 4.2  | 3.9  | 3.5  | 3.7  | 4.1  | 4.7  | 4.5  | 4.7  |
| 50   | 30   | 21   | 15   | 10   | 11   | 16   | 24   | 30   | 50   |      |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 38.0 | 38.0 | 36.8 | 37.2 | 37.1 | 38.1 | 37.9 | 37.7 | 37.7 | 38.0 |
| 4.4  | 4.4  | 5.6  | 5.2  | 4.7  | 4.3  | 4.5  | 4.7  | 4.7  | 4.4  |
| 50   | 33   | 22   | 15   | 12   | 11   | 15   | 27   | 50   |      |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 37.9 | 37.9 | 37.8 | 37.3 | 37.5 | 37.9 | 37.7 | 37.4 | 37.2 | 37.5 | 38.0 |
| 4.5  | 4.5  | 4.6  | 5.1  | 4.9  | 4.5  | 4.7  | 5.0  | 5.2  | 4.9  | 4.4  |
| 50   | 36   | 22   | 16   | 12   | 11   | 16   | 23   | 30   | 50   |      |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 37.0 | 36.4 | 35.5 | 36.1 | 36.4 | 36.8 | 36.7 | 36.4 | 37.1 | 37.6 |
| 5.4  | 6.0  | 6.9  | 6.3  | 5.8  | 5.6  | 5.7  | 6.0  | 5.3  | 4.8  |
| 50   | 27   | 22   | 19   | 12   | 12   | 23   | 34   | 50   |      |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 36.5 | 36.5 | 36.2 | 36.3 | 36.3 | 36.4 | 36.3 | 36.1 | 36.6 | 38.2 | 38.2 |
| 5.9  | 5.9  | 6.2  | 6.1  | 5.9  | 6.0  | 6.1  | 6.3  | 5.8  | 4.2  | 4.0  |
| 50   | 43   | 23   | 13   | 11   | 16   | 23   | 29   | 34   | 50   |      |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 36.6 | 36.4 | 35.1 | 35.8 | 36.0 | 36.2 | 36.2 | 36.0 | 36.3 | 38.1 | 38.6 |
| 5.8  | 6.0  | 7.3  | 6.6  | 6.4  | 6.2  | 6.2  | 6.4  | 6.1  | 4.3  | 3.8  |
| 50   | 30   | 21   | 17   | 12   | 11   | 18   | 29   | 34   | 50   |      |



Sta +  $\pi$  - Elev.

942.42

47+50

+59 for Ent Rt only

BM 2.12 940.52 4.02 938.40

48 Ent Lt

+27 Ent Lt.

+60

49

TP 2.58 935.95 7.15 933.37

Lt.

Oct. 1, 1965 74  
Bt

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 36.3 | 36.3 | 35.1 | 34.8 | 35.4 | 35.7 | 35.6 | 35.0 | 35.8 | 34.5 | 34.1 |
| 6.1  | 6.1  | 6.7  | 7.6  | 7.0  | 6.7  | 6.8  | 7.4  | 6.6  | 3.9  | 3.7  |
| 50   | 39   | 29   | 19   | 13   |      | 12   | 22   | 29   | 36   | 50   |

|      |      |      |      |      |
|------|------|------|------|------|
| 35.6 | 35.4 | 34.1 | 34.4 | 34.9 |
| 6.8  | 7.0  | 7.7  | 7.6  | 7.5  |
| 13   | 25   | 44   | 50   |      |

Top Hyd Bt Sta 47

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 35.7 | 35.6 | 35.0 | 34.6 | 35.1 | 34.7 | 34.6 | 33.9 | 34.8 | 34.6 | 34.5 |
| 4.8  | 4.9  | 5.5  | 5.9  | 5.4  | 5.8  | 5.9  | 6.6  | 3.7  | 1.9  | 2.0  |
| 50   | 39   | 22   | 15   |      | 13   | 17   | 25   | 36   | 39   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 34.7 | 34.3 | 34.3 | 34.3 | 34.6 | 34.4 | 34.1 | 33.6 | 34.1 | 34.4 | 34.5 |
| 6.3  | 6.2  | 6.2  | 6.2  | 5.9  | 6.1  | 6.4  | 6.9  | 3.4  | 2.1  | 2.0  |
| 50   | 30   | 20   | 15   |      | 13   | 18   | 25   | 35   | 38   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 33.9 | 33.8 | 33.8 | 33.2 | 33.4 | 33.7 | 34.0 | 33.8 | 33.5 | 33.0 | 34.9 | 34.4 | 34.5 |
| 6.6  | 6.7  | 6.7  | 7.3  | 7.1  | 6.8  | 6.5  | 6.7  | 7.0  | 7.5  | 3.6  | 2.1  | 2.0  |
| 50   | 40   | 27   | 23   | 20   | 16   |      | 13   | 18   | 24   | 34   | 39   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 30.8 | 31.0 | 32.1 | 32.9 | 32.3 | 32.8 | 33.3 | 33.4 | 33.2 | 33.0 | 34.3 | 34.5 |
| 9.7  | 9.5  | 7.8  | 7.6  | 8.2  | 7.7  | 7.2  | 7.1  | 7.3  | 7.5  | 4.2  | 4.0  |
| 50   | 46   | 37   | 29   | 22   | 18   |      | 13   | 18   | 25   | 37   | 50   |

49

Sta +  $\pi$  - Elev.

935.95

A9+09 Ent Rt.

✓

+36

✓

+68

✓

Lt

Oct. 1, 1965 75  
Rt

| 32.1 | 32.7 | 32.5 | 31.9 | 33.2 | 32.2 | 32.5 | 34.2 | 34.5 |
|------|------|------|------|------|------|------|------|------|
| 3.9  | 3.3  | 3.5  | 3.1  | 2.8  | 2.8  | 2.5  | 1.8  | 1.5  |
| 23   | 20   | 19   | 11   |      | 14   | 22   | 40   | 50   |

31.6 29.6  
→ 4.4 6.4  
34 50

| 31.3 | 32.0 | 31.8 | 31.9 | 32.3 | 32.4 | 32.3 | 31.9 | 31.4 | 32.4 | 33.0 |
|------|------|------|------|------|------|------|------|------|------|------|
| 4.7  | 4.0  | 4.2  | 4.16 | 3.7  | 3.6  | 3.7  | 4.1  | 4.6  | 3.6  | 3.0  |
| 21   | 19   | 18   | 17   | 10   |      | 11   | 17   | 27   | 40   | 50   |

MT

29.2 29.3 25.6  
→ 6.8 8.7 10.4  
25 36 50

| 28.3 | 30.9 | 31.4 | 31.0 | 31.4 | 31.6 | 31.7 | 31.4 | 31.6 | 29.0 |
|------|------|------|------|------|------|------|------|------|------|
| 7.7  | 5.1  | 4.6  | 5.0  | 4.6  | 4.4  | 4.3  | 4.6  | 5.4  | 7.0  |
| 28   | 23   | 20   | 19   | 12   |      | 10   | 16   | 24   | 26   |

25.2 23.5  
→ 10.8 12.5  
32 50

28.5 29.7 30.9 29.2  
7.5 6.3 5.1 6.8  
50 48 32 29



Sta + A - Elev.

935.95

50

✓

+50

+76

36.0  
5.1  
—  
30.9  
2

+89

LT

Oct. 1, 1965

76

RT

76

27.5

30.4

30.1

30.3

31.0

31.2

31.1

30.8

30.6

27.9

8.5 5.6 5.3 5.7 5.0 4.8 4.9 5.2 5.4 8.2  
28 23 21 20 13 13 19 24 30

24.9

27.9

11.2 13.7  
33 50

22.2

24.8

13.8 11.2  
50 36

25.8

26.0

28.1

30.1

31.0

30.6

30.9

31.1

30.6

30.0

26.2

23.0

14.5

10.2 10.0 7.9 5.3 5.0 5.4 5.1 4.9 5.4 6.0 9.8 13.0 16.5  
50 34 31 26 22 21 14 13 21 27 34 50

28.3

28.1

30.6

30.8

30.6

31.0

31.2

30.7

30.0

26.1

22.2

19.6

7.7 7.9 5.5 5.2 5.4 5.0 4.8 5.3 6.0 9.9 13.8 16.4  
50 32 25 23 22 12 13 22 29 37 50

30.6

29.9

29.9

30.6

30.9

31.3

30.8

30.5

26.8

22.5

20.3

5.40 6.06 6.1 5.4 5.1 4.7 5.2 5.5 9.2 13.5 15.7  
34 33 31 19 17 13 20 29 40 50

C G

30.4

30.8

30.6

31.0

5.60 5.16 5.42 4.96

G C G C

42

50

Sta +  $\pi$  - Elev

935.95

51

31.59  
31.04  
30.90  
C G  
73 69

+12

Garage floor 931.08

✓

BM 1.73 937.60 0.08 935.87

+39

+74

+87

Lt

Oct. 1, 1965 77  
RT W

|       |      |      |      |      |      |      |      |      |      |      |
|-------|------|------|------|------|------|------|------|------|------|------|
| 30.48 | 30.5 | 30.2 | 30.1 | 30.9 | 31.3 | 31.0 | 30.8 | 30.9 | 24.4 | 22.2 |
| 5.50  | 5.77 | 5.9  | 5.1  | 4.7  | 5.0  | 5.2  | 9.1  | 11.6 | 13.8 |      |
| 51    | 50   | 34   | 31   | 18   |      | 11   | 22   | 31   | 37   | 50   |

Cone.

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 30.6 | 30.3 | 30.3 | 30.6 | 31.1 | 31.4 | 31.2 | 31.0 | 28.8 | 25.8 |
| 5.35 | 5.65 | 5.7  | 5.4  | 4.9  | 4.6  | 4.8  | 5.0  | 7.2  | 10.2 |
| C    | G    | 32   | 23   | 14   |      | 13   | 23   | 29   | 35   |
| 35   |      |      |      |      |      |      |      |      |      |

|      |      |  |  |  |  |  |  |  |  |
|------|------|--|--|--|--|--|--|--|--|
| 30.6 | 30.9 |  |  |  |  |  |  |  |  |
| 5.35 | 5.08 |  |  |  |  |  |  |  |  |
| G    | C    |  |  |  |  |  |  |  |  |
| 50   |      |  |  |  |  |  |  |  |  |

Top Hyd 50 S.W. Con. Victoria +18

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 30.4 | 30.4 | 33.3 | 31.4 | 31.3 | 31.5 | 31.8 | 31.6 | 31.5 | 28.6 | 27.2 | 25.4 |
| 1.2  | 4.3  | 6.2  | 6.3  | 6.1  | 5.8  | 6.0  | 6.1  | 9.0  | 10.4 | 12.0 |      |
| 0.50 | 35   | 24   | 22   | 15   |      | 13   | 26   | 32   | 41   | 50   |      |

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 30.0 | 31.4 | 33.4 | 32.1 | 31.9 | 32.1 | 32.3 | 32.0 | 31.8 | 32.5 | 30.8 | 30.4 |
| 1.6  | 2.2  | 4.2  | 5.5  | 5.7  | 5.5  | 5.3  | 5.6  | 5.8  | 5.1  | 6.8  | 7.2  |
| 50   | 44   | 33   | 24   | 22   | 13   |      | 14   | 23   | 28   | 44   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 33.1 | 32.4 | 32.1 | 32.4 | 32.4 | 32.5 | 32.2 | 31.9 | 32.9 | 33.3 | 32.4 |
| 4.5  | 5.2  | 5.5  | 5.2  | 5.2  | 5.1  | 5.4  | 5.7  | 4.7  | 4.3  | 5.2  |
| 29   | 25   | 23   | 16   | 12   |      | 14   | 23   | 28   | 40   | 50   |

MAH

|      |      |  |  |  |  |
|------|------|--|--|--|--|
| 33.4 | 35.5 |  |  |  |  |
| 2.5  | 2.1  |  |  |  |  |
| 42   | 50   |  |  |  |  |



Sta +  $\pi$  - Elev.

937.60

52

+20

+36 Gutter Line

+54 MH Rt 1' 4.24 933.35

+55

+64 MH 9' Lt 4.11 933.49

Lt

Oct 1, 1965

78

Rt

X

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 35.2 | 34.1 | 32.8 | 32.1 | 32.6 | 32.7 | 32.3 | 32.1 | 32.1 | 32.1 | 32.1 | 32.1 |
| 24   | 35   | 48   | 49   | 50   | 49   | 53   | 55   | 49   | 52   | 52   |      |
| 50   | 35   | 26   | 23   | 14   |      | 15   | 23   | 25   | 39   | 50   |      |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 34.6 | 33.9 | 32.0 | 32.8 | 33.0 | 32.8 | 32.7 | 32.2 | 31.6 | 31.6 |
| 3.0  | 37   | 46   | 48   | 46   | 48   | 49   | 54   | 60   | 60   |
| 50   | 33   | 30   | 27   | 16   |      | 12   | 23   | 35   | 38   |

|      |      |
|------|------|
| 30.4 | 31.2 |
| 72   | 64   |
| 50   | 41   |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 33.4 | 33.3 | 33.2 | 33.2 | 33.0 | 32.9 | 32.2 | 31.5 | 31.3 |
| 4.2  | 43   | 44   | 44   | 46   | 47   | 54   | 61   | 63   |
| 50   | 46   | 32   | 18   |      | 13   | 32   | 47   | 50   |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 34.1 | 33.7 | 33.6 | 33.5 | 33.3 | 33.0 | 32.4 | 31.7 | 30.2 |
| 3.5  | 3.9  | 4.0  | 4.1  | 4.3  | 4.6  | 5.2  | 5.9  | 7.4  |
| 100  | 50   | 35   | 18   |      | 19   | 39   | 50   | 75   |

|      |      |
|------|------|
| 34.2 | 34.3 |
| 3.4  | 3.3  |
| 150  | 200  |

|      |      |      |
|------|------|------|
| 23.8 | 26.1 | 28.1 |
| 13.8 | 11.5 | 8.9  |
| 200  | 150  | 100  |

| Sta | + | x | - | Elev |
|-----|---|---|---|------|
|-----|---|---|---|------|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 937.60 |  |  |
|--|--|--------|--|--|

|       |  |  |  |  |
|-------|--|--|--|--|
| 52+69 |  |  |  |  |
|-------|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +89 |  |  |  |  |
|-----|--|--|--|--|

|    |  |  |  |  |
|----|--|--|--|--|
| 53 |  |  |  |  |
|----|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +50 |  |  |  |  |
|-----|--|--|--|--|

|  |  |     |  |  |
|--|--|-----|--|--|
|  |  | 3.4 |  |  |
|--|--|-----|--|--|

|  |  |  |      |  |
|--|--|--|------|--|
|  |  |  | 34.2 |  |
|--|--|--|------|--|

|    |  |  |  |  |
|----|--|--|--|--|
| 54 |  |  |  |  |
|----|--|--|--|--|

|  |  |     |  |  |
|--|--|-----|--|--|
|  |  | 2.6 |  |  |
|--|--|-----|--|--|

|  |  |  |      |  |
|--|--|--|------|--|
|  |  |  | 35.0 |  |
|--|--|--|------|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +50 |  |  |  |  |
|-----|--|--|--|--|

|  |  |     |  |  |
|--|--|-----|--|--|
|  |  | 2.1 |  |  |
|--|--|-----|--|--|

|  |  |  |      |  |
|--|--|--|------|--|
|  |  |  | 35.5 |  |
|--|--|--|------|--|

|    |  |  |  |  |
|----|--|--|--|--|
| 55 |  |  |  |  |
|----|--|--|--|--|

|  |  |     |  |  |
|--|--|-----|--|--|
|  |  | 1.4 |  |  |
|--|--|-----|--|--|

|  |  |  |      |  |
|--|--|--|------|--|
|  |  |  | 36.2 |  |
|--|--|--|------|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +50 |  |  |  |  |
|-----|--|--|--|--|

|  |  |     |  |  |
|--|--|-----|--|--|
|  |  | 0.9 |  |  |
|--|--|-----|--|--|

|    |  |  |  |  |
|----|--|--|--|--|
| TP |  |  |  |  |
|----|--|--|--|--|

|  |      |  |  |  |
|--|------|--|--|--|
|  | 4.88 |  |  |  |
|--|------|--|--|--|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 942.45 |  |  |
|--|--|--------|--|--|

|  |  |  |      |  |
|--|--|--|------|--|
|  |  |  | 0.03 |  |
|--|--|--|------|--|

|  |  |  |  |        |
|--|--|--|--|--------|
|  |  |  |  | 937.57 |
|--|--|--|--|--------|

|    |  |  |  |  |
|----|--|--|--|--|
| BM |  |  |  |  |
|----|--|--|--|--|

|  |  |  |      |  |
|--|--|--|------|--|
|  |  |  | 2.11 |  |
|--|--|--|------|--|

|  |  |  |  |        |
|--|--|--|--|--------|
|  |  |  |  | 940.34 |
|--|--|--|--|--------|

Oct. 1, 1965

79

17

✓

RT.

2

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 33.9 | 33.8 | 33.1 | 33.6 | 33.6 | 33.4 | 33.1 | 32.3 | 31.8 |
| 3.7  | 3.8  | 3.9  | 4.0  | 4.0  | 4.2  | 4.5  | 5.3  | 5.8  |
| 50   | 38   | 23   | 14   |      | 13   | 22   | 41   | 50   |

✓

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 35.8 | 35.4 | 34.1 | 33.9 | 33.8 | 33.7 | 33.6 | 33.2 | 33.4 | 31.1 | 30.9 | 31.1 |
| 1.8  | 2.2  | 2.5  | 3.7  | 3.8  | 3.9  | 4.1  | 4.4  | 4.2  | 6.5  | 7.0  | 5    |
| 50   | 41   | 26   | 22   | 12   |      | 13   | 23   | 26   | 34   | 47   | 50   |

✓

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 36.2 | 36.2 | 35.0 | 34.1 | 33.9 | 33.8 | 33.6 | 33.2 | 33.4 | 33.2 | 31.0 | 31.0 |
| 1.4  | 1.4  | 2.6  | 3.5  | 3.7  | 3.8  | 4.0  | 4.4  | 4.2  | 4.4  | 0.6  | 0.6  |
| 50   | 45   | 33   | 20   | 15   |      | 14   | 18   | 20   | 25   | 33   | 50   |

Top Hyd



| Sta | +     | $\pi$  | -     | Elev.  |          |
|-----|-------|--------|-------|--------|----------|
|     |       | 942.45 |       |        |          |
| BM  | 0.29  | 941.13 | 1.61  | 940.84 |          |
| BM  | 0.49  | 934.11 | 7.51  | 933.62 |          |
| BM  | 10.02 | 934.06 | 10.07 | 924.04 | 923.95   |
| BM  | 7.80  | 941.41 | 0.45  | 933.61 |          |
| BM  | 1.23  | 942.57 | 0.57  | 940.84 |          |
| TP  | 1.91  | 939.47 | 5.01  | 937.56 |          |
| BM  | 0.20  | 936.07 | 3.60  | 935.87 | (935.87) |
| TP  | 6.90  | 942.47 | 0.50  | 935.57 |          |
| BM  |       |        | 4.06  | 938.41 | 40       |
| BM  | 3.07  | 945.52 | 0.02  | 942.45 | 44 42    |
| BM  |       |        | 3.60  | 941.92 | 941.91   |

Oct. 1, 1965

80

3

Top Hyd by Ho #

Top Hyd by <sup>759</sup>~~# 1059~~

Roseville BM, S.E. Cor. Grotto + "B"

Top Hyd By Ho <sup>759</sup># ~~1059~~

Top Hyd By Ho #

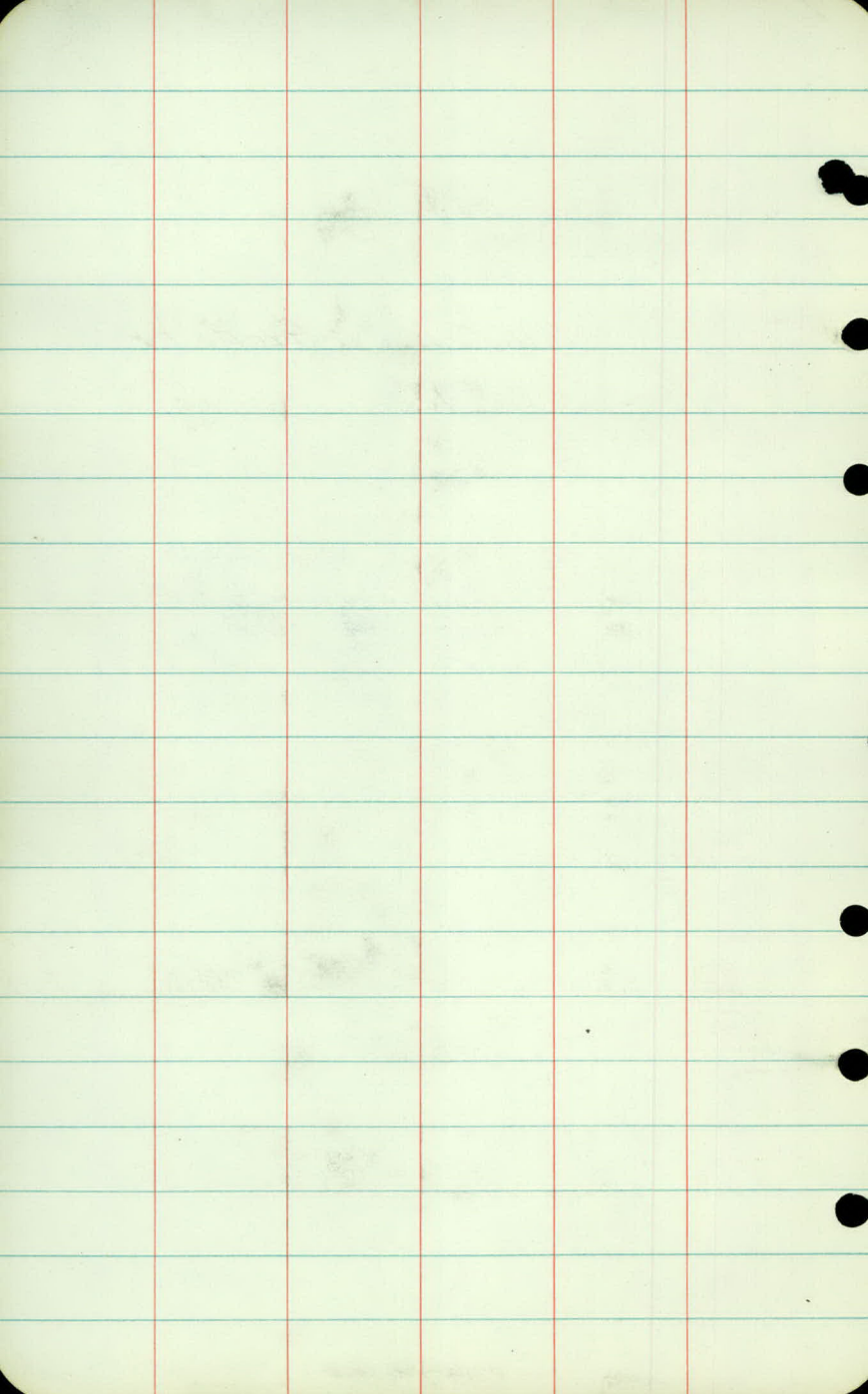
rock

Top Hyd SW. Cor. Victoria + "B"

Top Hyd Rt Sta 47+

Top Hyd Rt Sta 48-

Roseville BM



FK  
FS  
LPD

Dec. 29, 1965  
Overcast 25°

96  
a

Co Rd B

at

Victoria



| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

|    |      |        |  |        |
|----|------|--------|--|--------|
| BM | 3.58 | 939.45 |  | 935.87 |
|----|------|--------|--|--------|

53+39 Walk Left

✓

+50

✓

+92 Ent Rt

54

Dec. 20, 1965

9.7  
6

Top Hyd S.W. Cor Victoria + B

|       |      |      |      |      |      |      |      |      |
|-------|------|------|------|------|------|------|------|------|
| 35.35 | 34.6 | 34.3 | 34.2 | 34.1 | 33.9 | 33.9 | 34.0 | 34.3 |
| 4.10  | 4.9  | 5.2  | 5.3  | 5.4  | 5.6  | 5.6  | 5.5  | 5.2  |
| 33    | 22   | 18   | 13   |      | 10   | 17   | 19   | 26   |

Conc  
walk

|       |      |      |  |      |      |      |
|-------|------|------|--|------|------|------|
| 36.02 | 36.6 | 37.2 |  | 37.5 | 37.1 | 36.9 |
| 343   | 2.9  | 2.3  |  | 2.0  | 2.4  | 2.6  |
| 41    | 50   | 40.  |  | 50   | 41   | 33   |

Conc

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 36.3 | 35.1 | 34.4 | 34.2 | 34.3 | 34.1 | 34.1 | 34.2 | 36.6 |
| 3.2  | 4.4  | 5.1  | 5.3  | 5.2  | 5.4  | 5.4  | 5.3  | 2.9  |
| 42   | 25   | 19   | 13   |      | 10   | 17   | 22   | 33   |

|      |  |      |      |
|------|--|------|------|
| 36.6 |  | 37.5 | 37.2 |
| 2.9  |  | 2.0  | 2.3  |
| 50   |  | 50   | 43   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 36.4 | 35.3 | 34.8 | 34.6 | 35.0 | 34.9 | 34.9 | 35.7 | 36.6 | 37.1 |
| 3.1  | 4.2  | 4.7  | 4.9  | 4.5  | 4.6  | 4.6  | 3.8  | 2.9  | 1.8  |
| 50   | 31   | 19   | 13   |      | 10   | 16   | 30   | 42   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 36.2 | 35.9 | 35.3 | 34.8 | 34.7 | 35.1 | 35.0 | 34.9 | 35.1 | 36.6 | 36.1 | 37.2 |
| 3.3  | 3.6  | 4.2  | 4.7  | 4.8  | 4.4  | 4.5  | 4.6  | 3.4  | 2.9  | 3.4  | 2.3  |
| 50   | 42   | 29   | 19   | 14   |      | 10   | 17   | 24   | 29   | 36   | 50   |

| Sta | + | $\pi$ | - | Elev. |
|-----|---|-------|---|-------|
|-----|---|-------|---|-------|

|    |      |        |  |        |
|----|------|--------|--|--------|
| BM | 5.86 | 941.73 |  | 935.87 |
|----|------|--------|--|--------|

|       |        |  |  |  |
|-------|--------|--|--|--|
| 54+13 | Ent Lt |  |  |  |
|-------|--------|--|--|--|

|     |        |  |  |  |
|-----|--------|--|--|--|
| +30 | Ent Rt |  |  |  |
|-----|--------|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +50 |  |  |  |  |
|-----|--|--|--|--|

|     |        |  |  |  |
|-----|--------|--|--|--|
| +77 | Ent Lt |  |  |  |
|-----|--------|--|--|--|

|       |  |  |  |  |
|-------|--|--|--|--|
| 55+00 |  |  |  |  |
|-------|--|--|--|--|

|     |        |  |  |  |
|-----|--------|--|--|--|
| +48 | Ent Lt |  |  |  |
|-----|--------|--|--|--|

RG  
WM  
RB  
LPD

14

2

Feb 1, 1966  
Clear 0°  
RT

98

Top Hyd SW Cor Victoria  $\frac{1}{2}$  "B"

|                |                  |                |                  |                |                  |                  |                  |                  |                  |
|----------------|------------------|----------------|------------------|----------------|------------------|------------------|------------------|------------------|------------------|
| 3 <sup>8</sup> | 3 <sup>5.6</sup> | 3 <sup>0</sup> | 3 <sup>4.8</sup> | 3 <sup>2</sup> | 3 <sup>6.0</sup> | 3 <sup>1.9</sup> | 3 <sup>5.9</sup> | 3 <sup>7.9</sup> | 3 <sup>7.8</sup> |
| 5.9            | 6.1              | 6.7            | 6.9              | 6.5            | 6.7              | 6.6              | 5.8              | 3.8              | 3.9              |
| 50             | 38               | 22             | 16               |                | 13               | 19               | 29               | 33               | 50               |

|                |                |                |                |                  |                  |                |                  |                |
|----------------|----------------|----------------|----------------|------------------|------------------|----------------|------------------|----------------|
| 3 <sup>8</sup> | 3 <sup>6</sup> | 3 <sup>8</sup> | 3 <sup>4</sup> | 3 <sup>6.0</sup> | 3 <sup>5.2</sup> | 3 <sup>3</sup> | 3 <sup>5.9</sup> | 3 <sup>6</sup> |
| 4.9            | 5.1            | 5.9            | 6.3            | 6.7              | 6.3              | 6.5            | 6.4              | 5.8            |
| 50             | 43             | 32             | 23             | 15               |                  | 10             | 18               | 32             |

|                |                |                |                  |                  |                |                  |                  |                  |                |
|----------------|----------------|----------------|------------------|------------------|----------------|------------------|------------------|------------------|----------------|
| 3 <sup>9</sup> | 3 <sup>6</sup> | 3 <sup>9</sup> | 3 <sup>6.6</sup> | 3 <sup>5.3</sup> | 3 <sup>6</sup> | 3 <sup>5.2</sup> | 3 <sup>6.1</sup> | 3 <sup>6.8</sup> | 3 <sup>5</sup> |
| 4.8            | 5.0            | 5.8            | 6.1              | 6.4              | 6.1            | 6.3              | 6.0              | 4.9              | 4.2            |
| 50             | 44             | 31             | 22               | 15               |                | 18               | 23               | 31               | 50             |

|                |                  |                |                  |                |                |                |                |                 |                |
|----------------|------------------|----------------|------------------|----------------|----------------|----------------|----------------|-----------------|----------------|
| 3 <sup>3</sup> | 3 <sup>6.3</sup> | 3 <sup>0</sup> | 3 <sup>5.6</sup> | 3 <sup>9</sup> | 3 <sup>6</sup> | 3 <sup>9</sup> | 3 <sup>8</sup> | 3 <sup>10</sup> | 3 <sup>5</sup> |
| 5.4            | 5.4              | 5.7            | 6.1              | 5.8            | 6.1            | 5.8            | 5.9            | 4.7             | 4.2            |
| 50             | 44               | 28             | 17               |                | 14             | 19             | 25             | 35              | 50             |

|                  |                |                  |                  |                  |                  |                |                |                  |                |
|------------------|----------------|------------------|------------------|------------------|------------------|----------------|----------------|------------------|----------------|
| 3 <sup>7.2</sup> | 3 <sup>3</sup> | 3 <sup>6.1</sup> | 3 <sup>7.1</sup> | 3 <sup>6.2</sup> | 3 <sup>5.9</sup> | 3 <sup>9</sup> | 3 <sup>4</sup> | 3 <sup>6.6</sup> | 3 <sup>5</sup> |
| 4.5              | 5.4            | 5.6              | 6.0              | 5.5              | 5.8              | 5.8            | 5.3            | 5.1              | 5.2            |
| 50               | 32             | 23               | 16               |                  | 12               | 22             | 30             | 43               | 50             |

|                  |                  |                |                  |                  |                  |                  |                  |                |
|------------------|------------------|----------------|------------------|------------------|------------------|------------------|------------------|----------------|
| 3 <sup>7.3</sup> | 3 <sup>7.1</sup> | 3 <sup>7</sup> | 3 <sup>6.4</sup> | 3 <sup>6.6</sup> | 3 <sup>6.5</sup> | 3 <sup>6.4</sup> | 3 <sup>6.3</sup> | 3 <sup>5</sup> |
| 4.4              | 4.6              | 5.0            | 5.3              | 5.1              | 5.2              | 5.3              | 5.4              | 5.2            |
| 50               | 43               | 29             | 15               |                  | 14               | 26               | 41               | 50             |



| Sta | + | $\pi$ | - | EIV |
|-----|---|-------|---|-----|
|-----|---|-------|---|-----|

941.73

|       |        |  |  |  |
|-------|--------|--|--|--|
| 55+70 | Ent Rt |  |  |  |
|-------|--------|--|--|--|

56+00

|     |        |  |  |  |
|-----|--------|--|--|--|
| +26 | Ent Lt |  |  |  |
|-----|--------|--|--|--|

+50

|     |        |  |  |  |
|-----|--------|--|--|--|
| +88 | Ent Rt |  |  |  |
|-----|--------|--|--|--|

+91

4.15

57+00

Feb 1, 1966 99

Lt

Rt.

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| 37.8 | 37.2 | 36.9 | 36.6 | 36.9 | 36.7 | 36.6 | 36.5 |
| 3.9  | 4.5  | 4.8  | 5.1  | 4.8  | 5.0  | 5.1  | 5.2  |
| 50   | 31   | 21   | 13   |      | 13   | 23   | 50   |

|     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|
| 8.1 | 7.6 | 7.2 | 7   | 7.0 | 8   | 8   | 8   |
| 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 3.6 | 4.1 | 4.5 | 5.0 | 4.7 | 4.9 | 5.3 | 5.3 |
| 50  | 33  | 22  | 16  |     | 14  | 25  | 50  |

|      |      |     |     |     |     |     |     |
|------|------|-----|-----|-----|-----|-----|-----|
| 7.1  | 7.6  | 7.1 | 6.9 | 7.2 | 6.8 | 7.1 | 6.6 |
| 3    | 3    | 3   | 3   | 3   | 3   | 3   | 3   |
| 3.96 | 4.08 | 4.6 | 4.8 | 4.5 | 4.9 | 5.0 | 5.1 |
| 50   | 40   | 31  | 17  |     | 15  | 28  | 50  |

conc

|     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 7.3 | 7.3 | 7.3 | 7.1 | 7.1 | 7.0 | 6.8 | 6.9 | 7.0 |
| 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 4.4 | 4.4 | 4.4 | 4.6 | 4.3 | 4.7 | 4.9 | 4.8 | 4.7 |
| 50  | 45  | 26  | 17  |     | 14  | 26  | 39  | 50  |

Ent Ent

|     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|
| 7.9 | 7.5 | 7.2 | 7.6 | 7.3 | 7.0 | 6.9 | 6.9 |
| 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 3.8 | 4.2 | 4.5 | 4.1 | 4.4 | 4.7 | 4.8 | 4.8 |
| 50  | 28  | 15  |     | 14  | 22  | 40  | 50  |

MH W.rim

|     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 6.9 | 6.9 | 7.0 | 7.4 | 7.6 | 7.3 | 7.0 | 6.9 | 6.9 |
| 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 4.8 | 4.8 | 4.7 | 4.3 | 4.1 | 4.4 | 4.7 | 4.8 | 4.8 |
| 50  | 41  | 23  | 14  |     | 14  | 22  | 40  | 50  |

| Sta | + | $\pi$ | - | EIV |
|-----|---|-------|---|-----|
|-----|---|-------|---|-----|

941.73

942.74

|    |      |                   |      |        |        |
|----|------|-------------------|------|--------|--------|
| TP | 3.58 | <del>942.72</del> | 2.59 | 939.14 | 939.16 |
|----|------|-------------------|------|--------|--------|

57+10 Ent Rt

+50

+69 Ent Lt

+77 Ent Rt

58+00

+30

Lt

E

Rt

Top NW cor planter Ho 818 W Co Rd "B" (3' x 3')

|                  |                  |                  |                  |                  |                  |                  |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| 3 <sup>1.8</sup> | 3 <sup>1.5</sup> | 3 <sup>1.1</sup> | 3 <sup>1.5</sup> | 3 <sup>1.2</sup> | 3 <sup>1.0</sup> | 3 <sup>1.0</sup> |
| 4.9              | 5.2              | 5.6              | 5.2              | 5.5              | 5.7              | 5.7              |
| 50               | 29               | 15               |                  | 13               | 30               | 50               |

|                  |                  |                  |                  |                  |                  |                  |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| 3 <sup>1.8</sup> | 3 <sup>1.4</sup> | 3 <sup>1.3</sup> | 3 <sup>1.6</sup> | 3 <sup>1.3</sup> | 3 <sup>1.2</sup> | 3 <sup>1.3</sup> |
| 4.9              | 5.3              | 5.4              | 5.1              | 5.4              | 5.5              | 5.4              |
| 50               | 35               | 17               |                  | 13               | 26               | 50               |

|                  |                  |                  |                  |                  |                  |                  |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| 3 <sup>1.0</sup> | 3 <sup>1.5</sup> | 3 <sup>1.4</sup> | 3 <sup>1.6</sup> | 3 <sup>1.4</sup> | 3 <sup>1.6</sup> | 3 <sup>1.3</sup> |
| 4.7              | 5.2              | 5.3              | 5.1              | 5.3              | 5.1              | 5.4              |
| 50               | 30               | 14               |                  | 13               | 28               | 50               |

|                  |                  |                  |                  |                  |                  |                  |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| 3 <sup>1.8</sup> | 3 <sup>1.4</sup> | 3 <sup>1.4</sup> | 3 <sup>1.6</sup> | 3 <sup>1.4</sup> | 3 <sup>1.3</sup> | 3 <sup>1.2</sup> |
| 4.9              | 5.3              | 5.3              | 5.1              | 5.3              | 5.4              | 5.5              |
| 50               | 30               | 15               |                  | 13               | 25               | 50               |

|                  |                  |                  |                  |                  |                  |                  |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| 3 <sup>1.8</sup> | 3 <sup>1.4</sup> | 3 <sup>1.4</sup> | 3 <sup>1.8</sup> | 3 <sup>1.6</sup> | 3 <sup>1.1</sup> | 3 <sup>1.8</sup> |
| 4.9              | 5.3              | 5.3              | 4.9              | 5.1              | 5.0              | 4.9              |
| 50               | 32               | 14               |                  | 13               | 23               | 50               |

|                  |                  |                  |                  |                  |                  |                  |                  |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| 3 <sup>1.3</sup> | 3 <sup>1.2</sup> | 3 <sup>1.4</sup> | 3 <sup>1.4</sup> | 3 <sup>1.8</sup> | 3 <sup>1.5</sup> | 3 <sup>1.5</sup> | 3 <sup>1.9</sup> |
| 5.4              | 5.5              | 5.3              | 5.3              | 4.9              | 5.2              | 5.2              | 4.8              |
| 50               | 31               | 23               | 13               |                  | 14               | 25               | 50               |



Sta

+

+

-

Elev.

942.74

~~942.72~~

58+57

Ent Rt

+69

Ent Lt

59+00

+33

Ent Rt

+50

60+00

Feb 1, 1966

101

LT

RT

RT

| 37.6 | 2    | 4    | 4    | 37.9 | 6    | 9    | 9    |
|------|------|------|------|------|------|------|------|
| 37.1 | 37.1 | 37.1 | 37.1 | 37.1 | 37.1 | 37.1 | 37.1 |
| 5.1  | 5.5  | 5.3  | 5.3  | 4.8  | 5.1  | 4.8  | 4.8  |
| 50   | 31   | 29   | 14   | 14   | 35   | 50   |      |

| 5    | 4    | 4    | 5    | 37.9 | 6    | 9    | 9    |
|------|------|------|------|------|------|------|------|
| 37.1 | 37.1 | 37.1 | 37.1 | 37.1 | 37.1 | 37.1 | 37.1 |
| 5.16 | 5.30 | 5.3  | 5.2  | 4.8  | 5.1  | 4.8  | 4.8  |
| 50   | 39   | 29   | 14   | 14   | 35   | 50   |      |

conc

| 8.1 | 8.0 | 1.6 | 1.6 | 8.0 | 1.1 | 1.1 | 1.9 | 8.1 |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 4.6 | 4.7 | 5.1 | 5.1 | 4.7 | 5.0 | 5.0 | 4.8 | 4.6 |
| 50  | 30  | 19  | 14  | 13  | 18  | 25  | 50  |     |

| 8.1 | 8.0 | 1.1 | 1.5 | 8.0 | 1.8 | 1.1 | 1.3 |
|-----|-----|-----|-----|-----|-----|-----|-----|
| 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 4.6 | 4.7 | 5.0 | 5.2 | 4.7 | 4.9 | 4.6 | 4.4 |
| 50  | 34  | 24  | 16  | 13  | 26  | 50  |     |

| 8.1 | 8.1 | 1.1 | 1.4 | 8.0 | 1   | 1.1 | 8.4 | 8.1 |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 4.6 | 4.6 | 5.0 | 5.3 | 4.7 | 5.0 | 5.0 | 4.3 | 4.6 |
| 50  | 32  | 24  | 14  | 14  | 18  | 26  | 50  |     |

| 8.6 | 8.3 | 1.6 | 1.3 | 1.1 | 1.3 | 1.4 | 1.5 | 8.4 |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 4.1 | 4.4 | 5.1 | 5.4 | 5.0 | 5.4 | 5.3 | 5.2 | 4.3 |
| 50  | 32  | 23  | 13  | 13  | 19  | 25  | 50  |     |

| Sta | + | $\pi$ | - | E/V |
|-----|---|-------|---|-----|
|-----|---|-------|---|-----|

942.74

~~942.72~~

60+19 Ent Lt

+29

1.91

940.83

940.85

+50 Ent Lt

61+00

+22 Ent Rt

Mt

5.84

rim

+50

62+00 Ent Rt

TP

5.04

940.96

940.89

6.89

.85

935.83

935.92

Feb 8, 1966

102

LT

RT

RT

|      |      |     |     |     |     |     |     |     |     |
|------|------|-----|-----|-----|-----|-----|-----|-----|-----|
| 8.1  | 7.9  | 7.7 | 7.3 | 7.6 | 7.2 | 7.1 | 7.1 | 8.1 | 8.1 |
| 3    | 3    | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 4.55 | 4.82 | 5.0 | 5.4 | 5.1 | 5.5 | 5.6 | 5.6 | 4.6 | 4.6 |
| 50   | 33   | 27  | 13  |     | 14  | 19  | 26  | 31  | 50  |
| conc |      |     |     |     |     |     |     |     |     |

Top Hyd 30' LT

|      |      |       |     |     |     |     |     |     |     |
|------|------|-------|-----|-----|-----|-----|-----|-----|-----|
| 8.3  | 8.1  | 7.7   | 7.2 | 7.4 | 7.1 | 7.0 | 7.2 | 8.1 | 8.2 |
| 3    | 3    | 3     | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 4.41 | 4.60 | 5.0   | 5.5 | 5.3 | 5.6 | 5.7 | 5.5 | 4.6 | 4.5 |
| 50   | 34   | 27    | 13  |     | 13  | 19  | 25  | 30  | 50  |
| conc |      | conc. |     |     |     |     |     |     |     |

|     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 7.9 | 7.3 | 7.1 | 6.9 | 7.0 | 6.8 | 6.8 | 6.2 | 8.1 |
| 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 4.8 | 5.4 | 5.6 | 5.8 | 5.7 | 5.9 | 5.9 | 4.5 | 4.3 |
| 50  | 31  | 23  | 12  |     | 14  | 24  | 32  | 50  |

|     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 7.7 | 8.1 | 7.1 | 6.8 | 6.8 | 6.6 | 6.9 | 6.5 | 7.9 |
| 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 4.0 | 4.6 | 5.6 | 5.9 | 5.9 | 6.1 | 5.8 | 5.2 | 4.8 |
| 50  | 31  | 21  | 13  |     | 13  | 21  | 34  | 50  |

1' RT Sta 6424 (2/4/66)

|     |     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 8.4 | 7.8 | 8.8 | 8.1 | 7.4 | 6.2 | 6.1 | 6.3 | 7.7 | 8.2 |
| 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 4.3 | 4.9 | 5.9 | 6.3 | 6.3 | 6.5 | 6.3 | 6.4 | 5.0 | 4.5 |
| 50  | 31  | 23  | 14  |     | 14  | 18  | 23  | 38  | 50  |

|     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 7.6 | 7.2 | 5.9 | 6.7 | 6.8 | 5.6 | 5.9 | 7.0 | 7.1 |
| 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 5.1 | 5.5 | 6.8 | 7.0 | 6.9 | 7.1 | 6.8 | 5.7 | 5.6 |
| 50  | 28  | 20  | 12  |     | 12  | 23  | 43  | 50  |

E Sta 62



Sta

+

$\pi$

-

E/V.

940.96

~~940.87~~

62+13 Ent Lt

+50

63+00

+06 Ent Lt (only)

+50 Top Bank Rt

+64

Feb 1, 1964

103

$\frac{L}{\frac{R}{R}}$

|     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 1.0 | 6.1 | 6.1 | 5.6 | 5.7 | 5.5 | 5.9 | 6.1 | 7.3 |
| 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 4.0 | 4.3 | 4.9 | 5.4 | 5.3 | 5.5 | 5.1 | 4.3 | 3.7 |
| 50  | 41  | 21  | 12  |     | 13  | 20  | 33  | 50  |

|     |     |     |     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 3.1 | 1.8 | 1   | 1   | 1   | 1.9 | 6.1 | 1.7 | 1.7 | 1.9 | 6.5 | 7.7 |
| 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 2.9 | 3.2 | 4.3 | 5.6 | 6.1 | 5.9 | 6.3 | 6.3 | 6.1 | 4.5 | 3.3 |     |
| 50  | 36  | 29  | 21  | 12  |     | 12  | 14  | 21  | 33  | 50  |     |

|     |     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 1.9 | 5.5 | 1.0 | 3.8 | 3.8 | 3.8 | 1.3 | 1.3 | 1.5 | 6.1 |
| 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 3.6 | 5.5 | 7.0 | 7.2 | 7.2 | 7.6 | 7.2 | 6.7 | 5.5 | 4.3 |
| 50  | 29  | 21  | 12  |     | 12  | 18  | 24  | 37  | 50  |

|     |     |     |     |     |
|-----|-----|-----|-----|-----|
| 1.9 | 5.0 | 3.8 | 3.6 | 3.6 |
| 3   | 3   | 3   | 3   | 3   |
| 4.2 | 6.0 | 7.2 | 7.4 | 7.4 |
| 50  | 30  | 20  | 12  |     |

|     |     |     |     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 3.2 | 3.2 | 1.4 | 2.9 | 3.2 | 3.2 | 3.8 | 3.2 | 1.0 | 3.8 | 3.7 | 5.2 |
| 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 3.8 | 4.8 | 6.6 | 8.1 | 8.9 | 8.8 | 9.2 | 8.9 | 8.0 | 7.2 | 7.3 | 5.8 |
| 50  | 40  | 29  | 21  | 12  |     | 13  | 19  | 23  | 29  | 40  | 50  |

|     |     |     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 3.4 | 3.5 | 3.7 | 3.7 | 3.7 | 3.8 | 3.4 | 3.5 | 3.5 | 3.2 | 3.9 |
| 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 3.6 | 5.2 | 7.3 | 8.4 | 9.3 | 9.2 | 9.6 | 9.5 | 8.5 | 8.9 | 9.1 |
| 50  | 37  | 27  | 21  | 12  |     | 13  | 20  | 25  | 35  | 50  |

Sta +  $\pi$  - EIV

940.96

940.87

63+81 Berm Rt

+85 Gutter Rt

+95 E Avon St.

64+00 Ent Lt

935.52

TP

1.89

935.43

7.33

933.63

933.63

+10 Gutter Rt

+15 Berm Rt.

Feb 1, 1966

Rt.

104

$\frac{14}{36.2}$   $\frac{2}{4.9}$   $\frac{2}{3.8}$   $\frac{2}{3.6}$   $\frac{2}{3.2}$   $\frac{2}{3.1}$   $\frac{2}{3.1}$   $\frac{2}{3.1}$   $\frac{2}{3.1}$   $\frac{2}{3.1}$   
 4.8 6.1 8.2 9.4 9.8 9.7 9.9 10.4 10.3  
 50 38 28 21 12 11 32 50

$\frac{14}{36.6}$   $\frac{2}{4.7}$   $\frac{2}{3.7}$   $\frac{2}{3.5}$   $\frac{2}{3.1}$   $\frac{2}{3.1}$   $\frac{2}{3.1}$   $\frac{2}{3.1}$   $\frac{2}{3.1}$   $\frac{2}{3.1}$   
 4.4 6.3 8.3 9.5 9.9 9.8 10.0 10.4 10.5 10.5  
 50 37 27 21 12 12 28 40 50

$\frac{14}{31.8}$   $\frac{2}{3.2}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   
 9.2 9.8 10.0 10.3 10.2 10.3 10.6 10.7 10.9  
 50 33 22 12 12 35 50 100

$\frac{14}{31.5}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   
 9.5 10.2 10.4 10.5 10.3 10.3 10.6 10.7  
 50 31 21 12 12 35 50

Top Hyd 30±L+ 64+40±

$\frac{14}{31.8}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   
 3.7 5.0 5.3 5.4 5.2 5.4 5.8 5.5  
 50 30 21 11 12 28 50

$\frac{14}{31.8}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   $\frac{2}{3.0}$   
 3.7 5.0 5.3 5.4 5.3 5.6 5.8 5.1 5.1  
 50 30 21 11 12 27 38 50



Sta

+

$\pi$

-

EIV

935.52

935.43

67 +20

+40

+75

55+00

65+00

+07 Ent. Rt.

+41 Berm Lt.

Feb 1, 1966  
Rt. 105

✓  
 $\begin{matrix} 2 & 0.1 & 0.0 & 0.7 & 0.0 & 0.7 & 0.7 & 0.2 & \Delta \\ 3 & 3 & 3 & 2 & 3 & 2 & 2 & 3 & 1 \\ 2.3 & 4.8 & 5.5 & 5.8 & 5.5 & 5.8 & 5.8 & 5.3 & 5.1 \\ 50 & 28 & 21 & 11 & & 12 & 23 & 33 & 50 \end{matrix}$

✓  
 $\begin{matrix} 2.8 & 0 & 0.3 & 0.3 & 0.0 & 2.3 & 0.0 & 0.9 & 0.5 & 0.6 & 0.6 \\ 3 & 1 & 3 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 \\ 2.7 & 3.5 & 5.2 & 6.2 & 6.5 & 6.2 & 6.5 & 6.6 & 6.0 & 5.9 & 5.9 \\ 50 & 39 & 28 & 11 & 11 & & 12 & 17 & 24 & 38 & 50 \end{matrix}$

✓  
 $\begin{matrix} 1.1 & 0.8 & 0.1 & 0.2 & 0.1 & 0.3 & 0.0 & 0.1 & 0.9 & 0.1 & \Delta \\ 3 & 3 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 \\ 3.8 & 4.7 & 6.4 & 7.3 & 7.4 & 7.2 & 7.5 & 7.7 & 6.6 & 6.4 & 6.1 \\ 50 & 37 & 27 & 20 & 10 & & 13 & 18 & 24 & 33 & 50 \end{matrix}$

✓  
 $\begin{matrix} 2.1 & 0.5 & 2.6 & 2.1 & 2.7 & 2.8 & 2.1 & 0.9 & 1.1 & 0.0 \\ 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 \\ 6.4 & 7.0 & 7.9 & 8.8 & 8.8 & 8.7 & 8.8 & 8.6 & 7.8 & 7.5 \\ 50 & 32 & 26 & 19 & 12 & & 12 & 24 & 40 & 50 \end{matrix}$

✓  
 $\begin{matrix} 2.5 & 2.3 & 2.1 & 2.5 & 2.3 & 2.5 & 2.3 & 2.5 & 2.3 \\ 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 \\ 7.0 & 7.2 & 8.4 & 9.0 & 9.2 & 9.0 & 9.2 & 9.0 & 8.2 \\ 50 & 41 & 26 & 20 & 11 & & 12 & 24 & 50 \end{matrix}$

✓  
 $\begin{matrix} 2.3 & 2.5 & 2.1 & 2.9 & 2.0 & 2.8 & 2.0 & 2.6 & 2.5 & 2.0 \\ 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 \\ 10.2 & 10.1 & 10.8 & 10.6 & 10.5 & 10.7 & 10.5 & 9.9 & 9.0 & 8.5 \\ 50 & 34 & 20 & 11 & & 13 & 19 & 26 & 36 & 50 \end{matrix}$

| Sta | + | $\pi$ | - | E/V |
|-----|---|-------|---|-----|
|-----|---|-------|---|-----|

935.52  
935.43

65+49 Gutter Lt

+64 E Grotto St.

+65

11.58

TBM

12.63

922.87  
922.80

922.87

TBM

8.41

931.28  
~~931.21~~

922.87  
922.80

+75 Gutter Lt

+80

Berm Lt

66+00

+19

10.70

Feb 1, 1966

Lt

Rt

Rt.

106

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 24.8 | 24.4 | 24.6 | 24.7 | 24.5 | 24.6 | 25.3 | 26.4 | 26.9 |
| 10.7 | 11.1 | 10.9 | 10.8 | 11.0 | 10.9 | 10.2 | 9.1  | 8.6  |
| 50   | 31   | 10   |      | 13   | 17   | 25   | 39   | 50   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 25.9 | 24.2 | 23.8 | 23.8 | 23.9 | 23.4 | 24.0 | 24.2 | 25.4 | 26.4 |
| 9.6  | 11.3 | 11.7 | 11.7 | 11.6 | 12.1 | 11.5 | 11.3 | 10.1 | 9.1  |
| 100  | 50   | 26   | 13   |      | 13   | 19   | 25   | 33   | 50   |

MH 1' Lt

Top NW Cor lower step H<sub>2</sub>O #724 W. Cor'd "B"Rt  
Wm  
RB  
LPPFeb 2, 1966  
Clear 100

Above TBM.

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 23.9 | 23.5 | 23.3 | 23.2 | 23.5 | 23.1 | 23.5 | 23.6 | 23.6 |
| 7.4  | 7.8  | 8.0  | 8.1  | 7.8  | 8.2  | 7.8  | 7.7  | 7.7  |
| 50   | 37   | 22   | 14   |      | 15   | 24   | 41   | 50   |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 24.5 | 23.8 | 23.5 | 23.8 | 23.2 | 23.8 | 23.9 | 23.7 | 23.6 |
| 6.8  | 7.5  | 7.8  | 8.5  | 8.1  | 8.5  | 8.4  | 8.6  | 8.7  |
| 50   | 39   | 27   | 14   |      | 15   | 24   | 36   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 29.1 | 28.4 | 25.4 | 23.7 | 22.6 | 21.6 | 21.7 | 22.1 | 21.6 | 21.7 | 21.9 |
| 1.2  | 2.9  | 5.9  | 7.6  | 8.7  | 9.7  | 9.6  | 9.2  | 9.7  | 9.6  | 9.4  |
| 77   | 65   | 50   | 38   | 26   | 17   | 12   |      | 13   | 25   | 50   |

No rim MH Lt 15'



| Sta | + | $\pi$ | - | E/V. |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

931.28

~~931.21~~

66+34 Ent Rt (BT)

+50

+68

TP

0.34

919.05

~~918.98~~

12.57

918.71

~~918.64~~

+82

67+00

+09

5.15

+19

6.49

+31

6.34

+46

7.51

Feb 2, 1966

107

Lt

Rt

Rt

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 31.3 | 29.2 | 26.5 | 26.8 | 20.6 | 19.8 | 20.4 | 19.9 | 20.3 | 20.8 | 21.2 |
| 0.0  | 2.1  | 4.8  | 8.5  | 10.7 | 11.5 | 10.9 | 11.4 | 11.0 | 10.5 | 10.1 |
| 71   | 62   | 50   | 36   | 26   | 15   | ✓    | 14   | 25   | 33   | 50   |
|      |      |      |      |      |      |      | 135  |      |      |      |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 29.5 | 29.6 | 25.3 | 22.1 | 19.4 | 18.9 | 19.3 | 19.2 | 19.1 | 21.2 | 20.1 |
| 1.8  | 1.7  | 4.0  | 9.2  | 11.9 | 12.4 | 11.8 | 12.1 | 11.6 | 10.1 | 10.6 |
| 73   | 62   | 50   | 38   | 25   | 16   | ✓    | 14   | 24   | 37   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 26.7 | 26.6 | 24.3 | 21.1 | 18.8 | 17.8 | 19.5 | 18.1 | 18.1 | 17.5 | 17.3 | 16.4 |
| 4.6  | 4.7  | 2.0  | 10.2 | 12.5 | 13.5 | 12.8 | 13.2 | 13.2 | 13.8 | 14.0 | 14.9 |
| 75   | 60   | 50   | 39   | 27   | 18   |      | 16   | 25   | 43   | 50   | 75   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 14.4 | 16.3 | 17.4 | 18.1 | 17.0 | 17.5 | 17.8 | 17.3 | 17.0 | 16.2 | 16.0 |
| +4.7 | +2.8 | +1.7 | 1.0  | 2.1  | 1.6  | 1.3  | 1.8  | 2.1  | 2.9  | 3.1  |
| 63   | 50   | 43   | 27   | 19   | 12   |      | 15   | 25   | 41   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 17.8 | 19.0 | 18.3 | 16.6 | 15.6 | 16.4 | 16.7 | 16.3 | 15.2 | 15.7 | 14.8 |
| +1.3 | 0.1  | 0.8  | 2.5  | 3.5  | 2.7  | 2.4  | 2.8  | 3.9  | 3.4  | 4.3  |
| 66   | 41   | 34   | 25   | 20   | 12   |      | 13   | 22   | 27   | 50   |

W inv 12" CM Rt

W inv 12" CM Lt

E inv 12" CM Rt

E inv 12" CM Lt

Sta

+

.X

-

E/V

919.05

918.98

67+09

✓

+19

Ent Rt

.07

917.08

TP

0.31

917.01

2.28

916.76

916.76

+31

+36

3.00

+46

+60

Feb 2, 1966

Lt

2/

Rt

108

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 16.4 | 15.2 | 14.6 | 15.1 | 15.6 | 16.2 | 15.8 | 15.4 | 14.7 | 14.0 | 15.3 |
| 2.7  | 3.9  | 4.5  | 4.0  | 3.5  | 2.9  | 3.3  | 3.5  | 4.4  | 5.1  | 3.8  |
| 30   | 25   | 19   | 15   | 11   |      | 13   | 18   | 22   | 23   | 26   |

18.6

0.5

50

14.4

15.1

4.7

4.0

50

32

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 16.8 | 16.3 | 15.0 | 13.9 | 14.4 | 15.4 | 15.5 | 15.2 | 14.9 | 14.3 | 14.4 | 14.2 |
| 2.3  | 2.8  | 4.1  | 5.2  | 4.7  | 3.7  | 3.6  | 3.9  | 4.2  | 4.8  | 4.7  | 4.9  |
| 50   | 40   | 25   | 21   | 20   | 11   |      | 13   | 23   | 40   | 50   | 75   |

Ent

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 16.1 | 15.2 | 15.1 | 14.8 | 14.7 | 14.8 | 14.4 | 14.3 | 13.6 | 14.6 | 13.8 | 13.1 |
| 1.0  | 1.9  | 2.0  | 2.3  | 2.4  | 2.3  | 2.7  | 2.8  | 3.5  | 2.6  | 3.3  | 3.4  |
| 50   | 46   | 30   | 24   | 13   |      | 11   | 18   | 22   | 25   | 44   | 50   |

Ent Ent

SE inv 9" CM Lt 45'

|      |      |      |      |      |      |      |      |      |      |      |      |      |     |
|------|------|------|------|------|------|------|------|------|------|------|------|------|-----|
| 13.2 | 13.2 | 14.0 | 14.1 | 11.5 | 13.7 | 13.8 | 13.8 | 13.5 | 13.1 | 11.9 | 12.8 | 10.5 | 8.7 |
| 3.3  | 3.9  | 3.1  | 3.0  | 5.6  | 3.4  | 3.3  | 3.3  | 3.6  | 4.0  | 5.2  | 4.3  | 6.6  | 8.4 |
| 50   | 40   | 29   | 26   | 23   | 18   | 12   |      | 13   | 20   | 24   | 28   | 33   | 50  |

|      |      |      |      |      |      |      |      |      |      |     |      |
|------|------|------|------|------|------|------|------|------|------|-----|------|
| 12.2 | 11.4 | 12.8 | 11.0 | 12.6 | 12.1 | 12.9 | 12.5 | 12.2 | 11.3 | 9.3 | 8    |
| 4.9  | 5.7  | 4.3  | 6.1  | 4.6  | 4.4  | 4.2  | 4.6  | 4.9  | 5.8  | 7.8 | 11.3 |
| 50   | 41   | 31   | 25   | 17   | 12   |      | 14   | 19   | 25   | 32  | 50   |



Sta

+

 $\pi$ 

-

EIV

917.07

917.01

68+00

✓

TP

1.45

910.76

~~910.70~~

7.76

909-31

~~909.25~~

+50

✓

69+00

✓

Feb. 2, 1966

LT

RT

RT

109

|      |      |      |      |      |      |      |      |      |      |      |       |
|------|------|------|------|------|------|------|------|------|------|------|-------|
| 05.7 | 10.0 | 10.3 | 10.2 | 10.1 | 10.2 | 09.5 | 09.1 | 05.1 | 01.2 | 00.7 | 899.1 |
| 11.4 | 7.1  | 6.8  | 6.9  | 7.0  | 6.9  | 7.6  | 8.0  | 12.0 | 15.9 | 16.4 | 18.0  |
| 30   | 19   | 16   | 15   | 11   |      | 14   | 22   | 30   | 40   | 50   | 75    |

spillway

|      |      |      |
|------|------|------|
| 06.8 | 04.5 | 04.2 |
| 10.3 | 12.6 | 12.9 |
| 33   | 50   | 75   |

|     |     |     |     |     |     |     |     |     |     |       |       |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------|-------|
| 3.0 | 1.2 | 0.9 | 0.5 | 0.7 | 0.7 | 0.2 | 0.8 | 0.3 | 0.2 | 897.2 | 895.8 |
| 0   | 0   | 0.6 | 0   | 0.6 | 0.7 | 0.6 | 0   | 0.2 | 0   | 8     | 8     |
| 7.8 | 3.6 | 3.9 | 4.3 | 4.1 | 3.8 | 4.1 | 4.6 | 5.0 | 8.5 | 13.6  | 15.0  |
| 29  | 22  | 18  | 16  | 12  |     | 7   | 17  | 21  | 31  | 41    | 60    |

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 897.5 | 896.7 | 898.5 | 898.6 | 895.0 |
| 13.3  | 14.1  | 12.3  | 12.2  | 15.8  |
| 39    | 50    | 59    | 75    | 75    |

|      |      |      |     |      |      |      |      |      |       |       |
|------|------|------|-----|------|------|------|------|------|-------|-------|
| 00.1 | 03.6 | 03.6 | 03  | 03.6 | 03.8 | 03.1 | 03.2 | 02.5 | 899.0 | 894.0 |
| 0    | 0    | 0    | 0   | 0    | 0    | 0    | 0    | 0    | 8     | 8     |
| 10.7 | 7.2  | 7.3  | 7.5 | 7.2  | 7.0  | 7.7  | 7.6  | 8.3  | 11.8  | 16.8  |
| 28   | 20   | 17   | 16  | 11   |      | 15   | 16   | 21   | 30    | 42    |

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 895.7 | 893.4 | 894.7 | 891.8 | 893.1 |
| 15.1  | 17.4  | 16.1  | 19.0  | 17.7  |
| 39    | 50    | 75    | 75    | 50    |

| Sta | + | T      | - | E/v |
|-----|---|--------|---|-----|
|     |   | 910.76 |   |     |
|     |   | 910.70 |   |     |

69+14

✓

|     |      |                   |       |        |        |
|-----|------|-------------------|-------|--------|--------|
|     |      | 903.36            |       |        |        |
| TBM | 3.59 | <del>903.30</del> | 10.99 | 899.77 | 899.77 |

+24

+29 M.H. LT 15' 901.79

✓

+50 Ent Rt

✓

Feb 2, 1966

L+

2/

R+

110

|       |      |      |      |      |      |      |      |      |       |       |       |
|-------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 897.9 | 02.6 | 03.0 | 02.8 | 02.9 | 03.0 | 02.2 | 02.5 | 01.4 | 897.4 | 894.1 | 891.4 |
| 12.9  | 8.2  | 2.8  | 8.0  | 7.9  | 2.8  | 8.6  | 8.3  | 9.4  | 13.4  | 16.7  | 19.4  |
| 30    | 21   | 16   | 16   | 12   |      | 16   | 17   | 23   | 34    | 43    | 75    |

→ 889.5.0    893.0    894.4    893.9

|      |      |      |      |
|------|------|------|------|
| 15.8 | 17.8 | 16.4 | 16.9 |
| 37   | 47   | 54   | 75   |

Top Hyd Rt Sta 70±

|       |       |       |      |      |      |      |      |      |      |       |       |       |
|-------|-------|-------|------|------|------|------|------|------|------|-------|-------|-------|
| 893.5 | 893.9 | 897.6 | 02.3 | 02.4 | 02.2 | 02.4 | 01.8 | 01.9 | 00.9 | 899.6 | 897.6 | 896.4 |
| 9.9   | 9.5   | 5.8   | 1.1  | 1.0  | 1.2  | 1.0  | 1.6  | 1.5  | 2.5  | 3.8   | 5.8   | 7.0   |
| 45    | 40    | 31    | 22   | 17   | 14   |      | 14   | 17   | 25   | 41    | 60    | 75    |

→ 892.4    891.6    893.1

|      |     |      |
|------|-----|------|
| 11.0 | 9.8 | 10.3 |
| 49   | 51  | 75   |

|       |       |       |       |       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 896.2 | 900.9 | 902.0 | 902.1 | 901.9 | 902.1 | 901.6 | 901.7 | 900.3 | 902.1 | 902.4 |
| 8.2   | 3.5   | 2.4   | 2.3   | 2.5   | 2.3   | 2.8   | 2.7   | 4.1   | 6.3   | 8.0   |
| 30    | 24    | 26    | 16    | 15    |       | 15    | 16    | 27    | 46    | 75    |

→ 893.9    893.4    892.6    893.9    893.4

|      |      |      |      |      |
|------|------|------|------|------|
| 10.5 | 10.6 | 11.8 | 10.5 | 11.0 |
| 36   | 43   | 47   | 50   | 75   |



Sta

+

 $\pi$ 

-

E/V.

903.36

903.30

70+00

✓

+50

71+00

✓

TBM

0.19

892.46

~~892.45~~

892.40

11.09

2.27

892.21

892.26

71+50

Feb 2, 1966

LT

RT

RT.

111

|       |       |       |       |       |       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 891.2 | 894.5 | 897.4 | 897.8 | 897.9 | 898.4 | 898.0 | 898.2 | 897.6 | 896.5 | 894.3 | 893.6 |
| 12.2  | 8.9   | 6.0   | 5.6   | 5.5   | 5.0   | 5.4   | 5.2   | 5.8   | 6.9   | 9.1   | 9.8   |
| 36    | 28    | 24    | 20    | 16    |       | 15    | 17    | 20    | 28    | 50    | 75    |

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 891.1 | 890.5 | 890.4 | 890.7 | 890.6 |
| 12.3  | 12.9  | 13.0  | 12.7  | 12.8  |
| 50    | 58    | 61    | 67    | 75    |

|       |       |       |       |       |       |       |       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 889.4 | 889.3 | 889.5 | 889.8 | 889.0 | 889.7 | 889.8 | 889.9 | 889.4 | 889.5 | 889.0 | 889.9 | 889.6 | 889.9 |
| 14.0  | 14.1  | 13.9  | 9.6   | 8.4   | 7.7   | 7.6   | 7.5   | 8.0   | 7.9   | 9.4   | 10.5  | 11.8  | 12.5  |
| 75    | 50    | 33    | 26    | 20    | 17    | 14    |       | 15    | 17    | 22    | 31    | 50    | 75    |

|       |       |       |       |       |       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 888.0 | 890.1 | 892.7 | 893.4 | 893.3 | 893.7 | 893.4 | 893.7 | 893.1 | 890.3 | 889.8 | 889.8 |
| 15.4  | 13.3  | 10.7  | 10.0  | 10.1  | 9.7   | 10.0  | 9.7   | 10.3  | 13.1  | 13.6  | 13.6  |
| 33    | 27    | 21    | 16    | 15    |       | 15    | 17    | 20    | 28    | 50    | 75    |

|       |       |
|-------|-------|
| 887.5 | 887.8 |
| 15.9  | 15.6  |
| 50    | 75    |

Spk. in PP RT Sta 71+30 ±

RG  
WM  
RB  
LPD

Feb 3, 1966

10' Lt Snow

|       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 886.6 | 887.1 | 886.6 | 889.0 | 891.1 | 891.5 | 891.5 | 891.7 | 891.6 | 891.9 | 891.5 | 890.7 | 888.6 | 888.5 | 888.5 |
| 5.9   | 5.4   | 5.9   | 3.5   | 1.4   | 1.0   | 1.0   | 0.8   | 0.9   | 0.6   | 1.0   | 1.8   | 3.9   | 4.0   | 4.0   |
| 25    | 50    | 32    | 25    | 20    | 15    | 11    |       | 14    | 17    | 18    | 23    | 29    | 43    | 75    |

Sta

+

$\pi$

-

EIV

~~892.45~~  
~~892.46~~  
~~892.40~~

72+00

+30

Ent R4.

+65

73+00

+31

M.H. LT. 16'

885.30

+50

74+00

TP

4.09

888.48

~~888.42~~

8.07

884.39

~~884.33~~

884.39

Feb 3, 1966

| Lt    |       |       |       |       | Q     |       |       |       |       | Rt    |       |       |       |       | 112 |  |  |  |  |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-----|--|--|--|--|
| 884.4 | 884.5 | 885.6 | 887.3 | 889.2 | 889.4 | 89.8  | 889.4 | 889.7 | 889.3 | 890.1 | 887.5 | 887.4 | 887.5 |       |     |  |  |  |  |
| 8.1   | 8.0   | 6.9   | 5.2   | 3.3   | 3.1   | 2.7   | 3.1   | 2.8   | 3.2   | 4.4   | 5.0   | 5.1   | 5.0   |       |     |  |  |  |  |
| 75    | 50    | 32    | 25    | 17    | 12    | 15    | 17    | 18    | 25    | 36    | 50    | 75    |       |       |     |  |  |  |  |
| 882.9 | 884.3 | 887.3 | 888.1 | 888.5 | 888.3 | 88.6  | 888.2 | 884.3 | 887.2 | 886.6 | 886.5 | 887.2 |       |       |     |  |  |  |  |
| 8.6   | 8.2   | 5.2   | 4.4   | 4.0   | 4.2   | 3.9   | 4.3   | 4.2   | 5.3   | 5.9   | 5.6   | 5.3   |       |       |     |  |  |  |  |
| 75    | 34    | 26    | 20    | 16    | 14    | 14    | 16    | 26    | 40    | 50    | 75    |       |       |       |     |  |  |  |  |
| 882.3 | 882.5 | 882.6 | 886.1 | 887.2 | 887.5 | 887.2 | 887.4 | 887.1 | 887.3 | 886.7 | 886.6 | 885.9 | 885.8 |       |     |  |  |  |  |
| 10.2  | 10.0  | 9.9   | 6.4   | 5.3   | 5.0   | 5.3   | 5.1   | 5.4   | 5.2   | 5.8   | 5.9   | 6.6   | 6.7   |       |     |  |  |  |  |
| 75    | 50    | 36    | 27    | 21    | 15    | 14    | 15    | 17    | 21    | 31    | 50    | 75    |       |       |     |  |  |  |  |
| 882.7 | 882.5 | 882.4 | 884.7 | 886.3 | 886.3 | 886.3 | 886.0 | 886.3 | 886.0 | 884.1 | 884.5 | 884.4 | 884.5 |       |     |  |  |  |  |
| 9.8   | 10.0  | 10.1  | 7.8   | 6.2   | 6.2   | 6.2   | 6.5   | 6.2   | 6.5   | 8.4   | 8.0   | 8.1   | 8.0   |       |     |  |  |  |  |
| 75    | 50    | 35    | 26    | 19    | 13    | 14    | 16    | 20    | 28    | 34    | 50    | 75    |       |       |     |  |  |  |  |
| 881.5 | 881.8 | 882.2 | 884.2 | 885.2 | 885.5 | 885.4 | 885.3 | 884.9 | 885.1 | 884.8 | 883.2 | 881.2 | 881.1 |       |     |  |  |  |  |
| 11.0  | 10.7  | 10.3  | 8.3   | 7.3   | 7.0   | 7.1   | 7.2   | 7.6   | 7.4   | 7.7   | 9.3   | 11.3  | 11.4  | 11.1  |     |  |  |  |  |
| 75    | 50    | 34    | 27    | 19    | 15    | 13    | 15    | 16    | 21    | 26    | 31    | 50    | 75    |       |     |  |  |  |  |
| 881.5 | 881.3 | 881.4 | 883.6 | 884.4 | 884.7 | 884.6 | 884.4 | 884.1 | 884.4 | 884.1 | 882.6 | 880.4 | 880.2 | 880.3 |     |  |  |  |  |
| 11.0  | 11.2  | 11.1  | 8.9   | 8.1   | 7.8   | 7.9   | 8.1   | 8.4   | 8.1   | 8.4   | 9.9   | 12.1  | 12.3  | 12.2  |     |  |  |  |  |
| 75    | 50    | 35    | 28    | 19    | 16    | 13    | 15    | 18    | 22    | 26    | 34    | 50    | 75    |       |     |  |  |  |  |

PK Nail &amp; Sta 74400



| Sta | + | T.     | - | E/V |
|-----|---|--------|---|-----|
|     |   | 888.48 |   |     |
|     |   | 888.42 |   |     |

74+50

75+00

|    |      |        |      |        |
|----|------|--------|------|--------|
|    |      | 888.66 |      |        |
| TP | 5.40 | 888.60 | 5.22 | 883.20 |
|    |      |        |      | 883.26 |

+42

+47 E ditch Lt

✓

+52

Feb 3, 1966

LT

R

RT

113

|      |      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 80.5 | 80.7 | 80.7 | 82.7 | 84.1 | 83.9 | 83.9 | 83.6 | 83.9 | 83.3 | 81.4 | 80.4 | 79.7 |
| 8.0  | 7.8  | 7.8  | 4.8  | 4.4  | 4.6  | 4.6  | 4.9  | 4.6  | 5.2  | 6.9  | 8.1  | 8.8  |
| 75   | 50   | 30   | 21   | 16   | 13   |      | 13   | 18   | 23   | 31   | 50   | 75   |

|      |      |      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 80.1 | 80.1 | 80.2 | 82.2 | 82.5 | 83.7 | 82.6 | 83.6 | 83.3 | 83.4 | 82.8 | 80.0 | 79.1 | 79.1 |
| 8.4  | 8.4  | 8.3  | 5.3  | 5.0  | 4.8  | 4.9  | 4.9  | 5.2  | 5.1  | 5.7  | 8.5  | 9.4  | 9.4  |
| 75   | 50   | 30   | 23   | 19   | 15   | 13   |      | 15   | 19   | 23   | 31   | 50   | 75   |

PK Nail R Sta 76+00

|      |      |      |      |      |      |      |      |      |      |      |      |      |    |
|------|------|------|------|------|------|------|------|------|------|------|------|------|----|
| 79.9 | 80.0 | 82.3 | 83.4 | 83.5 | 83.6 | 83.5 | 83.3 | 83.3 | 82.6 | 80.8 | 79.7 | 79.1 |    |
| 8.8  | 8.7  | 6.4  | 5.3  | 5.2  | 5.2  | 5.2  | 5.4  | 5.3  | 6.1  | 7.9  | 9.0  | 9.6  |    |
| 75   | 50   | 32   | 25   | 20   | 16   | 13   |      | 14   | 17   | 24   | 29   | 40   | 75 |

|      |      |      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 78.4 | 78.9 | 80.1 | 83.2 | 83.5 | 83.5 | 83.4 | 83.2 | 83.3 | 82.6 | 80.8 | 79.7 | 79.1 | 79.0 |
| 10.3 | 9.8  | 8.0  | 5.5  | 5.2  | 5.2  | 5.3  | 5.5  | 5.4  | 6.1  | 7.9  | 9.0  | 9.6  | 9.7  |
| 34   | 30   | 25   | 19   | 15   | 10   |      | 14   | 17   | 24   | 28   | 35   | 50   | 75   |

|      |      |      |      |
|------|------|------|------|
| 78.5 | 78.8 | 78.8 | 79.1 |
| 10.2 | 9.9  | 9.9  | 9.6  |
| 47   | 73   | 100  | 150  |

|      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 80.2 | 79.7 | 78.4 | 78.9 | 80.6 | 83.6 | 83.5 | 83.4 | 83.2 | 83.3 | 82.6 | 80.8 | 79.7 | 79.1 | 79.0 |
| 8.5  | 9.0  | 10.3 | 9.8  | 8.1  | 5.3  | 5.1  | 5.2  | 5.3  | 5.5  | 5.4  | 6.1  | 7.9  | 9.0  | 9.6  |
| 75   | 44   | 34   | 30   | 26   | 20   | 16   | 14   |      | 14   | 17   | 24   | 28   | 35   | 50   |

ditto

Sta

+

. T

-

EIV

888.66

888.60

76+00

✓

436 End ditch Lt

✓

+41

+75

✓

Feb 3, 1966

Lt

Rt

Rt.

114

| 4    | 6    | 2    | 5   | 8   | 3.3  | 3.0 | 3.2 | 9   | 5    | 9.6 |
|------|------|------|-----|-----|------|-----|-----|-----|------|-----|
| 18.4 | 40.6 | 83.2 | 4.5 | 8.4 | 83.3 | 8.3 | 8.2 | 8.1 | 19.6 |     |
| 10.3 | 29   | 5.5  | 5.2 | 5.3 | 5.4  | 5.7 | 5.5 | 5.8 | 7.2  | 9.1 |
| 29   | 25   | 19   | 14  | 12  |      | 15  | 17  | 22  | 28   | 32  |

ditch

| 4    | 4    | 7    | 0    |  |  |  |  |  |  |
|------|------|------|------|--|--|--|--|--|--|
| 18.4 | 19.4 | 19.7 | 80.0 |  |  |  |  |  |  |
| 10.3 | 9.3  | 9.0  | 8.7  |  |  |  |  |  |  |
| 36   | 41   | 50   | 75   |  |  |  |  |  |  |

ditch

| 19.0 | 19.1 |  |  |
|------|------|--|--|
| 9.7  | 9.6  |  |  |
| 75   | 50   |  |  |

| 2    | 0    | 3    | 5    | 4    | 4    | 0    | 2    | 0    | 1    | 5    |
|------|------|------|------|------|------|------|------|------|------|------|
| 18.2 | 81.0 | 83.3 | 83.5 | 83.4 | 83.4 | 83.0 | 80.2 | 79.0 | 78.5 | 78.5 |
| 10.5 | 7.7  | 5.4  | 5.2  | 5.3  | 5.3  | 5.7  | 8.5  | 9.7  | 10.2 | 10.2 |
| 30   | 25   | 19   | 16   | 10   |      | 17   | 22   | 27   | 50   | 75   |

ditch

| 2    | 7    | 0    |
|------|------|------|
| 18.2 | 79.7 | 80.0 |
| 10.5 | 9.0  | 8.7  |
| 39   | 45   | 75   |

ditch

| 1    | 9    | 8    | 0    | 5    | 6    | 5    | 5    | 1    | 2    | 0    | 5    | 6    |
|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 80.1 | 79.9 | 79.8 | 83.0 | 83.5 | 83.6 | 83.5 | 83.5 | 84.1 | 80.2 | 79.0 | 79.5 | 78.6 |
| 8.6  | 8.8  | 8.9  | 5.7  | 5.2  | 5.1  | 5.2  | 5.2  | 5.6  | 8.5  | 9.7  | 10.2 | 10.1 |
| 75   | 50   | 33   | 25   | 19   | 16   | 13   |      | 17   | 22   | 28   | 50   | 75   |

| 8    | 5    | 2    | 7    | 1    | 1    | 2    | 7    | 6    | 2    | 2    | 1    | 1    | 5 |
|------|------|------|------|------|------|------|------|------|------|------|------|------|---|
| 80.8 | 80.5 | 81.2 | 83.7 | 84.1 | 84.1 | 84.2 | 83.7 | 83.6 | 82.9 | 81.2 | 80.1 | 79.5 |   |
| 7.9  | 8.2  | 7.5  | 5.0  | 4.6  | 4.6  | 4.5  | 5.0  | 5.1  | 5.8  | 7.5  | 8.6  | 9.2  |   |
| 75   | 50   | 41   | 23   | 17   | 11   |      | 15   | 18   | 23   | 28   | 34   | 50   |   |

79.9  
8.8  
75



Sta

+

.T

-

EIV

888.66  
~~888.60~~

77+00

+10

+25

TP

8.89

894.25

~~894.09~~

3.40

.26  
885.20

885.36

+50

78+00

Feb 3, 1966

LT

RT

RT

115

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 81.1 | 82.1 | 82.8 | 83.6 | 84.5 | 84.6 | 84.7 | 84.2 | 83.6 | 81.9 | 80.8 | 80.4 |
| 7.6  | 6.6  | 5.9  | 5.1  | 4.2  | 4.1  | 4.0  | 4.5  | 5.1  | 6.8  | 7.9  | 8.3  |
| 75   | 50   | 31   | 23   | 18   | 11   |      | 15   | 22   | 29   | 50   | 75   |

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 81.0 | 82.3 | 83.0 | 83.7 | 84.7 | 84.8 | 85.0 | 84.5 | 83.9 | 82.2 | 81.0 | 80.6 |
| 7.7  | 6.4  | 5.7  | 5.0  | 4.0  | 3.9  | 3.7  | 4.2  | 4.8  | 6.5  | 7.7  | 8.1  |
| 75   | 50   | 31   | 23   | 18   | 11   |      | 15   | 22   | 29   | 50   | 75   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 86.0 | 85.7 | 85.3 | 85.4 | 86.4 | 85.3 | 84.9 | 84.8 | 84.3 | 81.9 | 81.4 |
| 2.7  | 3.0  | 3.4  | 3.3  | 3.3  | 3.4  | 3.9  | 3.9  | 4.4  | 6.8  | 7.3  |
| 50   | 40   | 26   | 18   | 13   |      | 15   | 21   | 29   | 50   | 75   |

Top Curb 18' RT 77+33+

|      |      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 86.1 | 86.7 | 86.3 | 86.0 | 86.1 | 85.5 | 85.7 | 85.6 | 85.4 | 86.2 | 85.3 | 84.8 | 84.8 |
| 7.6  | 7.6  | 8.0  | 8.3  | 8.2  | 8.8  | 8.6  | 8.7  | 8.4  | 8.1  | 9.0  | 10.5 | 11.5 |
| 50   | 35   | 20   | 19   | 13   |      | 12   | 19   | 19   | 24   | 36   | 45   | 50   |

T.Curb

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 87.4 | 87.9 | 87.8 | 87.3 | 87.4 | 87.7 | 87.4 | 87.3 | 87.8 | 88.0 | 87.9 | 86.2 |
| 6.9  | 6.5  | 6.5  | 7.0  | 6.9  | 6.6  | 6.9  | 7.0  | 6.5  | 6.3  | 6.4  | 8.1  |
| 50   | 28   | 21   | 21   | 14   |      | 15   | 20   | 20   | 26   | 36   | 50   |

T.C.

|     |   |        |   |       |
|-----|---|--------|---|-------|
| Sta | + | $\pi$  | - | Elev. |
|     |   | 894.25 |   |       |
|     |   | 894.09 |   |       |

78+38

+52 Gutter Lt. & Rt.

+73 E Dale St

|    |  |  |      |        |        |
|----|--|--|------|--------|--------|
| BM |  |  | 0.09 | 894.20 | 894.22 |
|----|--|--|------|--------|--------|

|    |      |        |  |        |  |
|----|------|--------|--|--------|--|
| BM | 1.04 | 895.26 |  | 894.22 |  |
|----|------|--------|--|--------|--|

78+57 Top Curb Lt. & Rt.

|    |  |  |      |        |  |
|----|--|--|------|--------|--|
| BM |  |  | 1.04 | 894.22 |  |
|----|--|--|------|--------|--|

Feb 3, 1966

LT

RT

RT

116

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 89.3 | 89.5 | 89.3 | 89.9 | 89.2 | 89.3 | 89.1 | 89.0 | 89.3 | 90.2 | 91.2 |
| 5.0  | 4.8  | 5.0  | 5.4  | 5.1  | 5.0  | 5.2  | 5.3  | 5.0  | 4.1  | 3.1  |
| 50   | 34   | 24   | 24   | 12   |      | 19   | 24   | 24   | 34   | 50   |
|      |      | TC   |      |      |      |      |      | T.C. |      |      |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 89.4 | 89.5 | 89.7 | 89.9 | 90.1 | 90.7 | 90.4 |
| 4.9  | 4.8  | 4.6  | 4.4  | 4.2  | 3.6  | 3.0  |
| 75   | 50   | 25   |      | 25   | 50   | 75   |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 89.7 | 89.7 | 89.8 | 90.1 | 90.3 | 90.6 | 91.1 | 91.7 | 92.4 |
| 4.6  | 4.6  | 4.5  | 4.2  | 4.0  | 3.7  | 3.2  | 2.6  | 1.9  |
| 100  | 75   | 50   | 25   |      | 25   | 50   | 75   | 100  |

Top Hyd NE Cor Data + "B"

" " " " " "

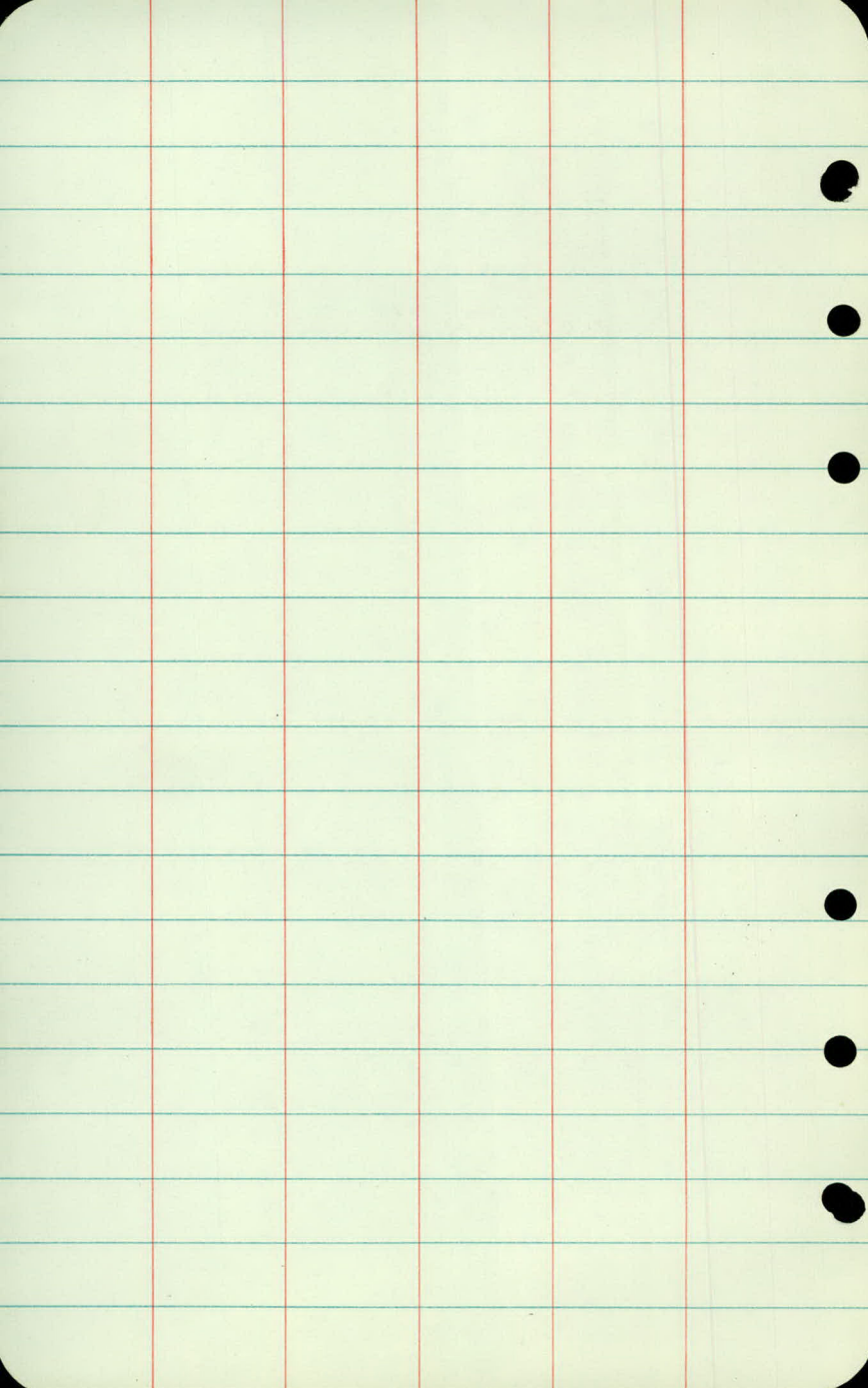
|      |      |      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 89.9 | 89.5 | 90.1 | 89.6 | 89.6 | 89.8 | 89.9 | 90.0 | 90.3 | 91.1 | 91.3 | 91.5 | 92.0 | 92.4 |
| 5.36 | 5.8  | 5.21 | 5.7  | 5.7  | 5.5  | 5.4  | 5.3  | 5.0  | 4.64 | 4.0  | 3.78 | 3.3  | 2.87 |
| 66   | 66   | 42   | 42   | 33   | 13   |      | 15   | 34   | 34   | 60   | 60   | 92   | 92   |
| T.C. | B.C. | T.C. | B.C. |      |      |      | BC   | T.C. | BC   | T.C. | BC   | T.C. | BC   |

|      |      |      |      |
|------|------|------|------|
| 89.4 | 89.9 | 89.6 | 90.0 |
| 5.9  | 5.36 | 5.8  | 5.31 |
| 90   | 90   | 115  | 115  |
| B.C. | T.C. | B.C. | T.C. |

|      |      |
|------|------|
| 93.2 | 92.1 |
| 2.08 | 2.6  |
| 122  | 122  |
| T.C. | BC   |

Above B.M.





K6  
WM  
FS  
RB  
LPD

Feb 4, 1966 PM  
40 Clear

Co Rd "B"

Bench Levels

Victoria St. to Dale St.

| Sta | +    | -      | E/v    |               |
|-----|------|--------|--------|---------------|
| BM  | 4.72 | 940.59 | 935.87 |               |
| TP  | 3.67 | 942.83 | 1.43   | 939.16 939.16 |
|     |      | 1.98   | 940.85 | 940.77        |
|     |      | 5.95   | 936.88 |               |
| TP  | 4.91 | 940.83 | 6.91   | 935.92 935.83 |
| TP  | 2.10 | 935.73 | 7.20   | 933.63 933.54 |
| TBM | 1.17 | 924.04 | 12.86  | 922.87 922.80 |
| TP  | 0.86 | 917.62 | 7.28   | 916.76 916.70 |
| TP  | 1.38 | 906.86 | 12.14  | 905.48        |
| TBM | 0.35 | 900.12 | 7.09   | 899.77 899.71 |
| TBM | 0.60 | 892.86 | 7.86   | 892.26 892.21 |
| TP  | 4.12 | 888.51 | 8.47   | 884.39 884.33 |
| TP  | 5.77 | 889.03 | 5.25   | 883.26 883.20 |
| TP  | 9.85 | 895.21 | 3.67   | 885.36 885.20 |
| BM  |      | 1.04   | 894.17 | 894.22        |

Feb 4, 1966

Top Hyd SW Cor B + Victoria

Top NW cor planter Ho #818 Co Rd B (3'x3')

rim MH Sta 61+24 E

PK nail E 62+00

Top Hyd 30' Lt Sta 64+40 (NE Cor Aven + B)

Top NW corner lower step Ho #724 W Co Rd B

Top Hyd Rt Sta 70 ±

Spk in PP Rt Sta 71+30 ±

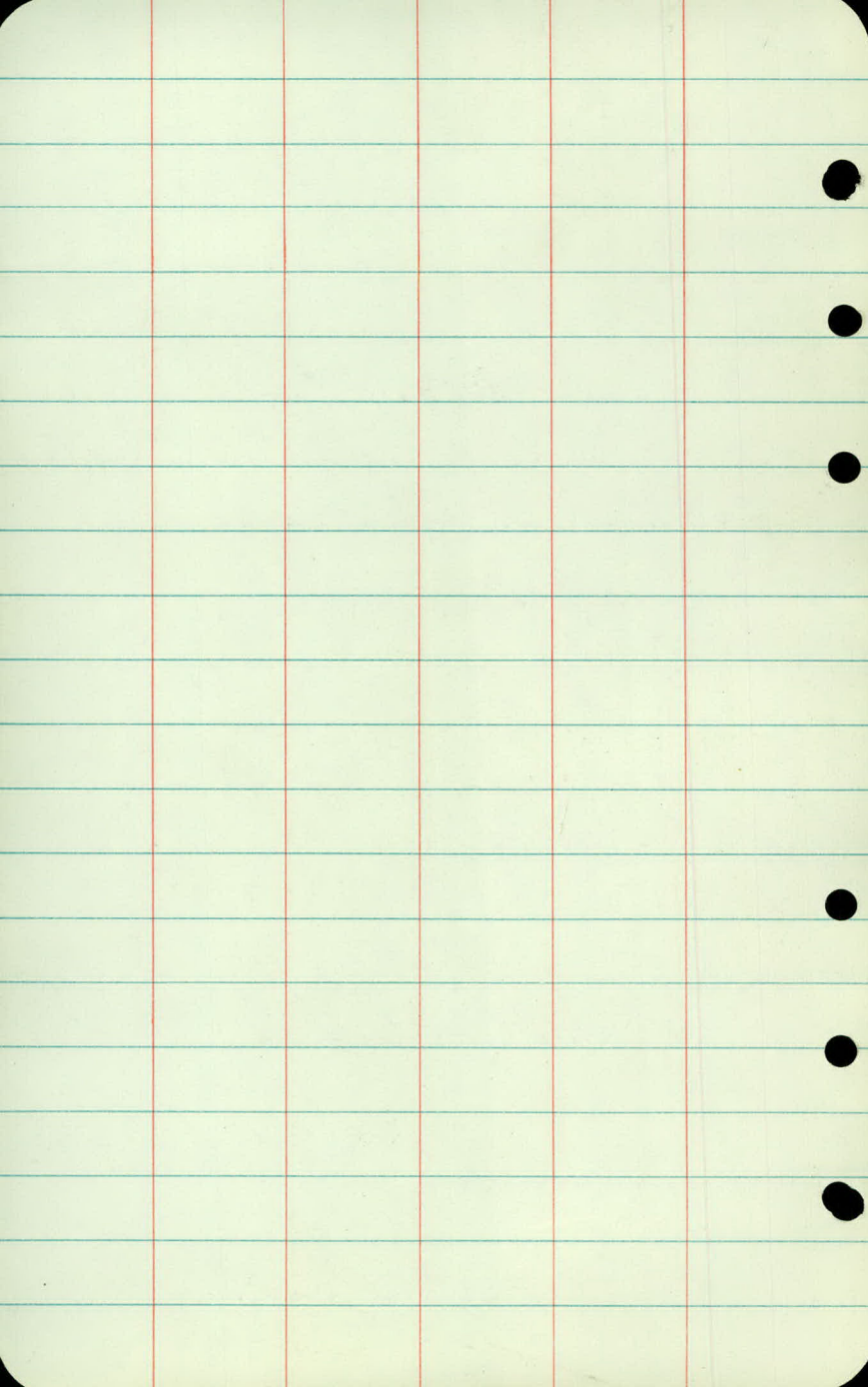
PK nail Sta 74+00 E

PK nail Sta 76+00 E

Top Curb Rt Sta 77+33 ±

Top Hyd NE Cor Dale, E B





Hamline Ave

x-sections

Sta +  $\pi$  - Elev.

BM 3.96 962.15

958.19

2+50  
0+50

3+50  
1+50

TP 3.75 959.64 6.20 955.89

4+00  
~~2+00~~ =  $\angle$  Co Rd B

4+50  
+50

✓

5+50  
3+50

BM

1.47

958.17 958.19

FX  
RV

Lt.

±

Oct. 25, 1965

Rt

82  
6

Top Hyd S.W. Cor. Hamline & "B"

|    |    |      |      |      |      |      |      |      |      |      |
|----|----|------|------|------|------|------|------|------|------|------|
| 36 | 56 | 57.5 | 57.6 | 57.4 | 57.1 | 57.8 | 57.7 | 57.6 | 57.9 | 57.8 |
| 60 | 62 | 4.7  | 4.6  | 4.8  | 4.5  | 4.4  | 4.5  | 4.6  | 4.3  | 4.4  |
| 50 | 36 | 28   | 21   | 21   | 16   |      | 16   | 18   | 34   | 50   |
|    | C  | G    |      |      |      |      |      |      |      |      |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 55.5 | 56.1 | 55.9 | 55.6 | 55.7 | 55.9 | 56.1 | 55.9 | 55.5 | 55.6 | 55.8 |
| 6.7  | 6.1  | 6.6  | 6.5  | 6.3  | 6.1  | 6.3  | 6.7  | 6.6  |      | 6.4  |
| 50   | 28   | 24   | 24   | 21   | 12   |      | 8    | 18   | 32   | 50   |
|      | C    | G    |      |      |      |      |      |      |      |      |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 55.4 | 55.6 | 55.0 | 55.2 | 55.5 | 55.1 | 54.9 | 55.1 | 55.2 | 55.2 |
| 42   | 40   | 46   | 44   | 41   | 45   | 47   | 45   | 44   | 44   |
| 33   | 24   | 24   | 12   |      | 12   | 21   | 30   | 30   | 35   |
|      | C    | G    |      |      |      |      | G    | C    |      |

55.6  
40  
50

54.8  
48  
50

54.9  
47  
36

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 55.5 | 55.4 | 54.9 | 54.3 | 54.6 | 55.0 | 55.3 | 55.1 | 55.1 | 55.4 | 55.6 | 56.0 |
| 4.1  | 4.2  | 4.7  | 5.3  | 5.0  | 4.6  | 4.3  | 4.5  | 4.5  | 4.2  | 4.0  | 3.6  |
| 50   | 44   | 34   | 24   | 19   | 13   |      | 9    | 24   | 25   | 29   | 50   |

Top Hyd. S.W. Cor Hamline & B



Sta +  $\pi$  - Elev.

BM 2.32 953.45

951.13

25+84

✓

59

67

78

26+59

✓

+67

✓

FK Nov. 2, 1965 83  
 LPD Lt E BT C

Top Hyd S.W. Cor ✓

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 47.9 | 47.5 | 47.1 | 47.1 | 47.9 | 47.1 | 47.4 | 48.1 | 48.1 |
| 5.6  | 6.0  | 5.8  | 5.8  | 5.6  | 5.8  | 6.05 | 5.43 | 5.4  |
| 34   | 23   | 22   | 13   |      | 13   | 22   | 22   | 33   |
|      | CB   |      |      |      |      | CB   | Curb |      |

48.0  
 5.5  
 50

48.9 48.4  
 4.6 5.1  
 50 36

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 47.9 | 47.7 | 47.8 | 48.0 | 48.0 | 48.0 | 47.7 | 48.2 | 48.3 |
| 5.6  | 5.8  | 5.7  | 5.5  | 5.5  | 5.5  | 5.8  | 5.27 | 5.2  |
| 31   | 31   | 20   | 13   |      | 13   | 30   | 32   | 40   |
| Carb | G    | MH   |      |      |      |      | Curb |      |

48.0 48.1  
 5.5 5.4  
 37 50

48.1  
 5.4  
 50  
 Curb Ent

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| 47.9 | 47.7 | 47.8 | 48.2 | 47.9 | 47.8 | 48.2 | 48.4 |
| 5.57 | 5.8  | 5.7  | 5.3  | 5.6  | 5.7  | 5.26 | 5.11 |
| 24   | 24   | 13   |      | 13   | 24   | 24   | 32   |
| Curb | G    |      |      |      | G    | Curb | Walk |

48.1 48.6 48.6  
 5.4 4.9 4.9  
 30 39 50

48.5 48.5  
 5.02 5.04  
 50 43  
 Walk

Sta +  $\pi$  - Elev

953.45

26+78

✓

✓

M 11

561 947.84 947.85

BM 0.88 954.66

(953.78)

31+20

32+05

LT  $\frac{1}{2}$  Nov. 2, 1965 84  
BT d

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| 48.0 | 47.5 | 47.8 | 48.2 | 47.9 | 47.6 | 48.3 | 48.4 |
| 5.45 | 5.99 | 5.7  | 5.3  | 5.6  | 5.92 | 5.24 | 5.1  |
| 22   | 20   | 14   |      | 13   | 21   | 22   | 25   |
| Curb | CB   |      |      |      | CB   | Curb |      |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 48.2 | 49.2 | 49.3 | 49.0 | 48.6 | 48.5 | 48.3 |
| 5.3  | 4.3  | 4.2  | 4.52 | 4.9  | 5.04 | 5.15 |
| 28   | 34   | 41   | 43   | 41   | 32   | 28   |
|      |      |      | Curb |      | Walk |      |

|      |      |      |      |
|------|------|------|------|
| 48.8 | 48.7 | 48.5 | 48.6 |
| 4.7  | 4.8  | 5.00 | 4.97 |
| 50   | 45   | 43.5 | 50   |

$\frac{1}{2}$  BT

Top Hyd by sta 30+45

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 50.4 | 50.0 | 49.7 | 49.6 | 49.8 | 49.8 | 49.9 | 49.6 | 49.3 | 49.1 |
| 4.3  | 4.7  | 5.0  | 5.1  | 4.9  | 4.9  | 4.8  | 5.1  | 5.4  | 5.6  |
|      | 15   | 19   | 28   | 39   | 58   | 70   | 82   | 94   | 100  |

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| 49.6 | 49.2 | 48.5 | 48.3 | 48.1 | 48.0 | 47.7 | 47.6 |
| 5.1  | 5.5  | 6.2  | 6.4  | 6.6  | 6.7  | 7.0  | 7.1  |
| 14   | 29   | 44   | 59   | 77   | 94   | 100  |      |



Sta +  $\pi$  - Elev.

954.66

32+80

✓

TP 4.11 952.76 6.01 948.65

33+55

✓

34+40

✓

BM

4.98 947.78 (947.80)

£

Nov. 2, 1965

85

BT

2

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 49.2 | 48.5 | 48.2 | 47.2 | 47.5 | 47.6 | 47.8 | 47.6 | 46.6 |
| 5.5  | 6.2  | 6.5  | 7.5  | 7.2  | 7.1  | 6.9  | 7.1  | 8.1  |
|      | 14   | 19   | 26   | 39   | 56   | 68   | 74   | 87   |

78  
58=71

43.5

11.2

100

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| 48.5 | 47.7 | 47.6 | 46.8 | 47.2 | 47.4 | 47.4 | 47.4 |
| 4.3  | 5.0  | 5.2  | 6.0  | 5.6  | 5.4  | 5.4  | 5.4  |
|      | 14   | 19   | 27   | 32   | 47   | 63   | 78   |

43.9

47.0

8.9

5.8

100

88

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| 47.7 | 47.1 | 46.9 | 46.3 | 46.5 | 46.7 | 46.9 | 47.0 |
| 5.1  | 5.7  | 5.9  | 6.5  | 6.3  | 6.1  | 5.9  | 5.8  |
|      | 14   | 18   | 24   | 30   | 45   | 59   | 74   |

42.0

46.6

10.8

6.2

107

83

Top Hyd N.W. Cor Oxford & B

Sta HAMLINE AVE.  
+  $\pi$  - Elev.

BM 3.34 961.53

958.19

~~3+00~~  
~~1+00~~

~~5+00~~  
~~3+00~~

Co. Rd "B"

0+24

+44

✓

FX  
LPD

4100 & 6022-B

Nov. 5, 1965

86

Top Hyd S.W. Cor Hamline + B

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 54.1 | 56.3 | 54.8 | 56.6 | 56.6 | 56.9 | 56.7 | 56.5 | 57.0 | 57.1 | 57.2 |
| 64   | 5.2  | 47   | 49   | 49   | 4.6  | 4.8  | 5.0  | 4.5  | 44   | 4.3  |
| 50   | 35   | 23   | 22   | 14   |      | 12   | 18   | 30   | 40   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 56.6 | 56.5 | 55.6 | 55.3 | 55.0 | 55.3 | 55.6 | 55.3 | 55.4 | 55.5 | 55.6 | 55.7 | 55.8 |
| 5.9  | 6.0  | 5.9  | 6.2  | 6.5  | 6.2  | 5.9  | 6.2  | 6.1  | 6.0  | 5.9  | 5.8  | 5.7  |
| 50   | 44   | 37   | 28   | 22   | 14   |      | 13   | 22   | 30   | 31   | 37   | 50   |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 55.0 | 54.9 | 54.7 | 54.9 | 55.1 | 55.0 | 54.7 | 54.9 | 55.6 |
| 6.5  | 6.6  | 6.8  | 6.6  | 6.4  | 6.5  | 6.8  | 6.6  | 5.9  |
| 50   | 37   | 21   | 13   |      | 13   | 28   | 34   | 55   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 54.8 | 55.0 | 54.7 | 54.5 | 54.9 | 54.4 | 54.3 | 54.8 | 55.6 | 56.5 |
| 6.7  | 6.5  | 6.8  | 7.0  | 6.6  | 7.1  | 7.2  | 6.7  | 5.9  | 5.0  |
| 30   | 23   | 22   | 13   |      | 13   | 21   | 32   | 51   | 69   |

|      |      |      |
|------|------|------|
| 54.9 | 55.5 | 55.8 |
| 6.6  | 6.0  | 5.7  |
| 50   | 75   | 97   |

|      |      |
|------|------|
| 57.1 | 56.8 |
| 4.4  | 4.7  |
| 100  | 80   |



Sta +  $\pi$  - Elev.

967.53

0+65

+81

1

+15

+50

2

Lt

Z Nov. 5, 1965

RT

87

56.1 55.7  
54 58  
100 75

56.6 55.70 56.8 57.2  
6.94 5.84 4.7 4.3  
50 75 100

56.6 56.2 55.9  
4.9 5.3 5.6  
Library 100 75  
110

56.8 57.2 57.4 57.5  
4.7 4.3 4.1 4.0  
75 84 conc 100  
84

56.3 55.9  
5.2 5.6  
100 75

56.0 56.8 57.0  
5.5 4.7 4.5  
57 75 85

54.3 54.1 54.2 54.7 55.3 56.3 56.9  
7.2 7.4 7.3 6.8 6.2 5.2 4.6  
13 23 34 50 60 80

56.3 55.2  
5.2 6.3  
100 75

55.5 54.8  
6.0 6.7  
100 75

Sta + X - Elev.

961.53

2+35

+83

3+05

B.M. 0.12 935.99 (935.87)

51+00 Lt

Garage Lt 4.91 31.08

B.M. 3.13 939.00 (935.87)

52+77

52 ± 6.29 932.71 (32.7)

Nov. 5, 1965

£

88

Lt

|      |      |
|------|------|
| 55.3 | 54.6 |
| 6.2  | 6.9  |
| 100  | 75   |

|      |      |
|------|------|
| 55.0 | 54.6 |
| 6.5  | 6.9  |
| 100  | 75   |

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| 55.2 | 54.7 | 54.3 | 53.7 | 52.6 | 52.2 | 53.4 | 54.0 |
| 6.3  | 6.8  | 7.2  | 7.8  | 8.9  | 9.31 | 7.9  | 7.5  |
| 150  | 100  | 81   | 60   | 32   | 50   | 13   |      |
|      |      |      |      |      | 24   |      |      |

Top Hyd S.W. Cor Victoria

|           |       |       |       |
|-----------|-------|-------|-------|
| 31.59     | 31.04 | 30.90 | 30.48 |
| 4.40      | 4.95  | 5.09  | 5.51  |
| C         | G     | 69    | 51    |
| <u>73</u> |       |       |       |

£

Top Hyd S.W. Cor Victoria + B

|      |      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 35.1 | 34.8 | 33.4 | 33.8 | 33.8 | 33.7 | 33.7 | 33.5 | 32.7 | 32.9 | 31.7 | 31.6 | 31.3 |
| 39   | 42   | 56   | 52   | 52   | 5.3  | 5.3  | 5.5  | 6.3  | 6.1  | 7.3  | 74   | 77   |
| 65   | 50   | 37   | 31   | 23   | 13   |      | 12   | 32   | 37   | 45   | 50   | 60   |



| Sta    | +    | $\pi$     | -    | Elev.           |
|--------|------|-----------|------|-----------------|
| BM     | 2.29 | 959.53    |      | (957.24)        |
| 3+03   | MH   | 10' Lt    | 5.87 | 53.46           |
| 3+02   | SD   | Rt 25'    | 6.17 | 53.36           |
| 3+03   | SD   | 25' Lt.   | 7.28 | 52.25           |
| 5+43   | MH   | 10' Lt.   | 5.61 | 53.92           |
| 5+43.5 | SD   | 26.7' Lt  | 7.04 | 52.49           |
| 5+43.5 | SD   | 21.2' Rt. | 7.70 | 51.83           |
| 6+63.4 | MH   | 11' Lt    | 3.71 | 55.82           |
| 6+84.6 | S.D. | 30' Lt    | 4.77 | 54.76           |
| BM     |      |           | 1.86 | 957.67 (957.67) |

FK  
DS  
LPD  
ML

TH  
7  
7  
1

Nov. 17, 1965

89

Top Hyd By Ho #1316 Co Rd "B"

Top Hyd NE Cor Dellwood & B

| Sta   | +      | $\pi$  | -    | Elev        |
|-------|--------|--------|------|-------------|
| BM    | 1.80   | 952.93 |      | 951.13      |
| 25+84 | S.D.   | Lt 23' | 5.49 | 47.44       |
| 25+85 | CB     | 21' Rt | 5.53 | 47.40       |
| 26+13 | CB     | 30' Rt | 5.54 | 47.39       |
| 26+13 | CB     | 40' Lt | 5.38 | 47.55       |
| 26+56 | MH     | $\neq$ | 4.94 | 47.99       |
| 26+56 | CB     | 43' Rt | 5.26 | 47.67       |
| 26+56 | CB     | 46' Lt | 5.54 | 47.39       |
| 26+79 | CB     | Rt 20' | 5.39 | 47.54       |
| +79   | CB     | Lt 20' | 54.6 | 47.47       |
| 25    | $\neq$ |        | 5.26 | 947.67 47.6 |

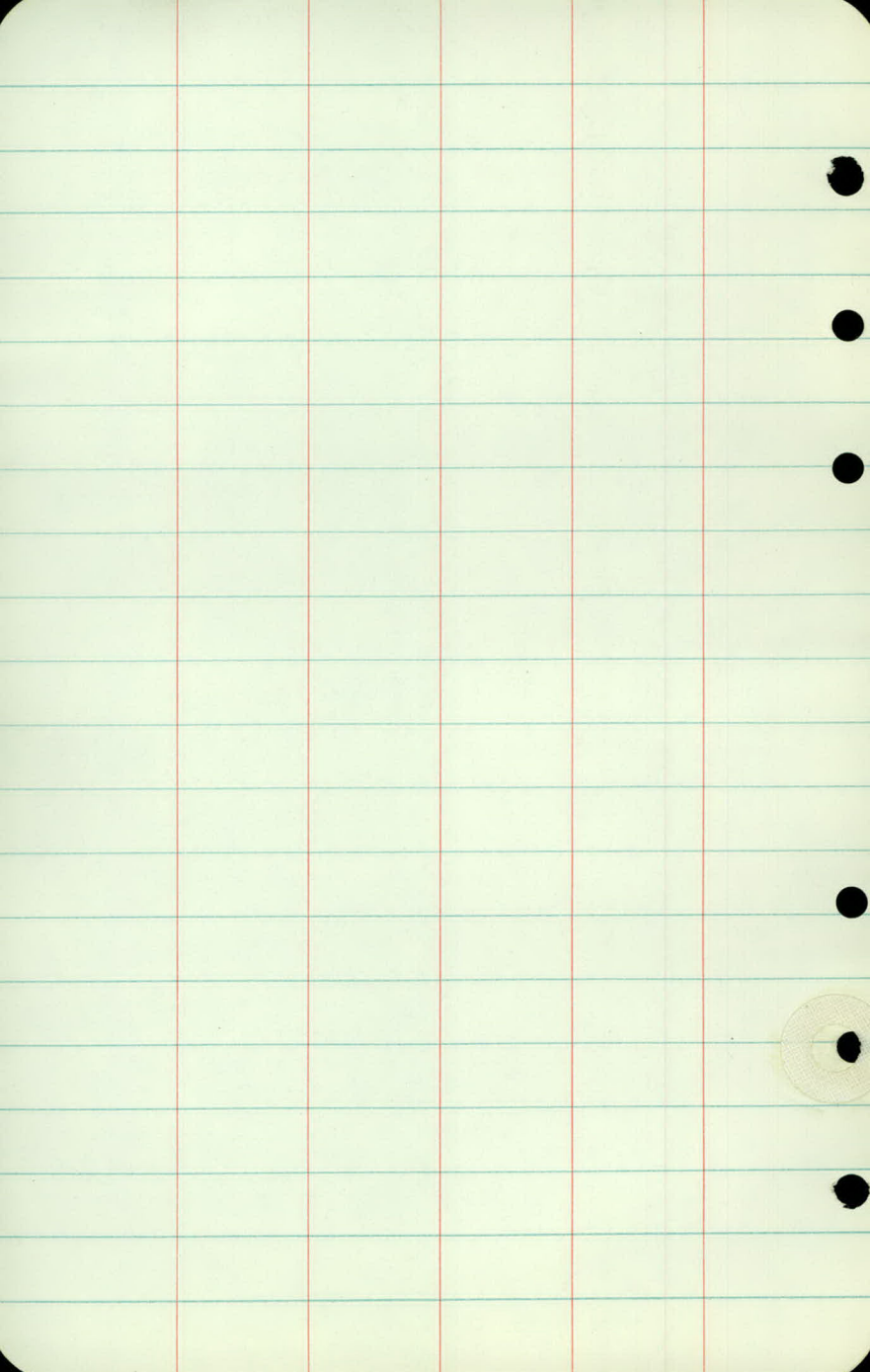
FK  
FS  
LPD

Nov. 18, 1965

90

Top Hyd S.W. Cor. Lexington + "B"





FK  
FS  
LPD  
ML

Nov. 23, 1965

91  
a

M. H. Elevations  
on  
Co Rd "B"  
Hamline to Victoria

Rec. 11-23-65

| Sta   | +          | $\pi$  | -    | Elev   |
|-------|------------|--------|------|--------|
| BM    | 2.40       | 961.45 |      | 959.05 |
| 10+29 | MH 20' Lt. |        | 5.16 |        |
| 10    | $\pm$      |        | 4.18 |        |

|       |              |        |      |        |
|-------|--------------|--------|------|--------|
| BM    | 0.66         | 954.97 |      | 954.31 |
| 19+65 | S.D. 19' Rt. |        | 2.54 |        |
| 19+89 | MH 20' Lt.   |        | 6.98 |        |
| 20    | $\pm$        |        | 6.42 |        |

|       |            |        |      |        |
|-------|------------|--------|------|--------|
| BM    | 1.72       | 953.14 |      | 951.42 |
| 23+10 | MH 19' Lt. |        | 6.01 |        |
| 23    |            |        | 5.62 |        |

|       |              |        |      |        |
|-------|--------------|--------|------|--------|
| BM    | 2.53         | 953.66 |      | 951.13 |
| 27+73 | MH 22.5' Lt. |        | 5.47 |        |
| 28    | $\pm$        |        | 4.65 |        |

|       |             |        |      |        |
|-------|-------------|--------|------|--------|
| BM    | 1.80        | 946.80 |      | 945.00 |
| 40+48 | MH. 18' Lt. |        | 5.60 |        |
| 40    | $\pm$       |        | 4.64 |        |

Nov. 23, 1965 92

b

Top Hyd N.E. Cor. Merrill & B

Top Hyd by Ho # 1178 Co Rd B West

Top Hyd by School

Top Hyd S.W. Cor. Lexington & "B"

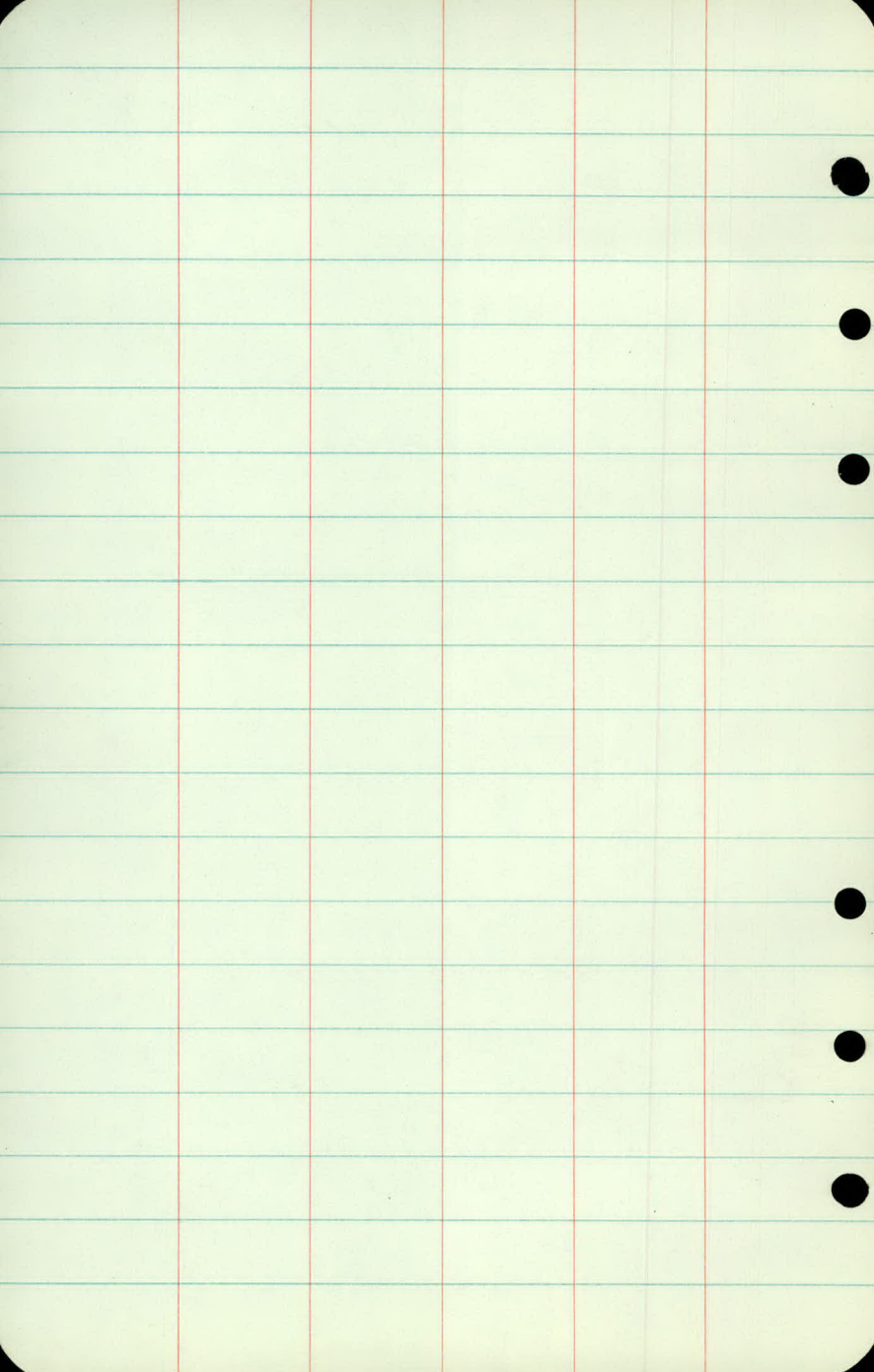
Top Hyd by Ho # 982 Co Rd "B" West



| Sta   | +         | $\pi$  | -    | Elev   |
|-------|-----------|--------|------|--------|
| BM    | 1.08      | 943.52 |      | 942.44 |
| 43+47 | MH 17' Lt |        | 3.96 | 939.56 |
| 46+46 | MH 19' Lt |        | 7.14 | 936.38 |
| 46    | $\Sigma$  |        | 5.36 |        |

Nov. 23, 1965 93  
C

Top Hyd Rt sta 44+16



FK  
LPD  
ML

Nov. 23, 1965

94

a

x-section Extensions

PEC- 11-29-65

plotted 11-29-65



| Sta | +    | $\pi$ | - | Elev. |
|-----|------|-------|---|-------|
| TP  | 0.22 |       |   | 931.2 |

50+00

+50

+76

+89

51

+12

51+00 £

0.12 931.3

Nov. 23, 1965

95

BT

b

sta 50

|      |      |      |
|------|------|------|
| 22.5 | 21.9 | 21.5 |
| 8.9  | 9.5  | 9.9  |
| 55   | 71   | 85   |

✓

|      |      |      |
|------|------|------|
| 19.6 | 17.6 | 16.7 |
| 13.0 | 14.0 | 14.7 |
| 55   | 65   | 80   |

✓

|      |      |      |
|------|------|------|
| 18.0 | 17.1 | 16.1 |
| 13.4 | 14.3 | 15.3 |
| 55   | 70   | 83   |

✓

|      |      |      |
|------|------|------|
| 20.1 | 18.6 | 17.6 |
| 11.3 | 13.0 | 13.8 |
| 54   | 68   | 80   |

✓

|      |      |      |
|------|------|------|
| 21.4 | 20.0 | 19.2 |
| 10.0 | 11.4 | 12.2 |
| 55   | 70   | 80   |

✓

|      |      |      |
|------|------|------|
| 22.0 | 21.1 | 19.9 |
| 9.4  | 10.3 | 11.5 |
| 61   | 76   | 88   |

✓

Man wants not of  
what he knows not.

Hamline

0100 = 4 CO. R. D. B



Sta + \* - Elev.

B M 3.45 961.64

958.19

£ £ Hamline + B 5.92 955.72

2+00  
0+00

6+00  
4+00

FM  
RG  
WNI  
WJ

March 29/1966

2

Top Hyd S.W. Cor Hamlinet B

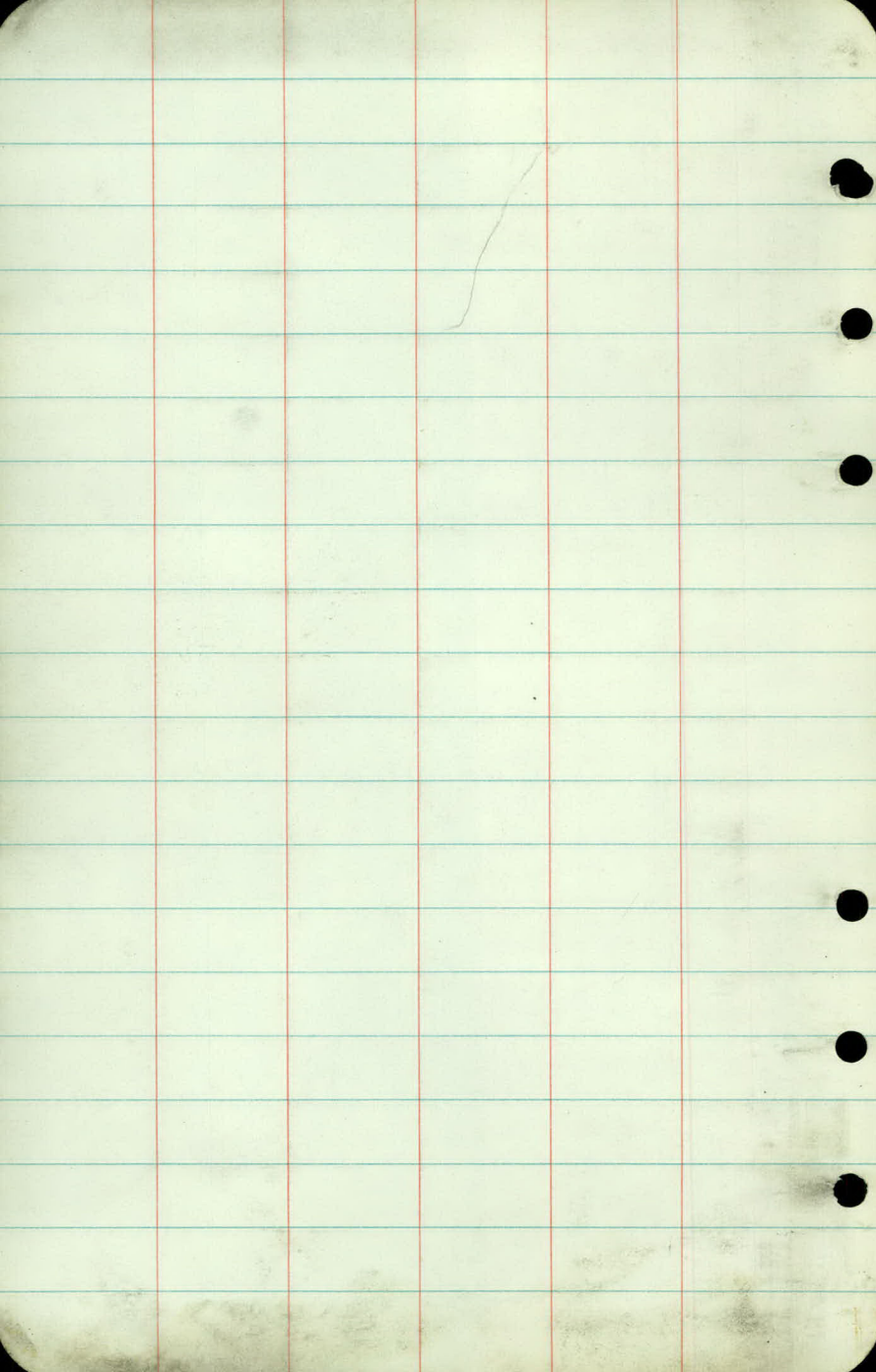
54.98  
43 58.87 58.51 58.44

2.40 2.77 3.13 3.20  
Garage 13 24 26  
53.5 40 30 Edge  
27.5

~~4~~

58.54 58.3 57.9 58.4 58.5 58.1 57.8 57.9 57.6 57.0  
2.1 3.3 3.7 3.2 3.1 3.5 3.8 3.7 3.8 4.6  
57 42 26 17 16 22 37 45 62

53.4 52.4 53.8 54.6 54.9 54.9 55.6 56.2 56.9  
8.2 8.2 7.8 7.0 6.7 6.7 6.0 5.4 4.7  
62 48 27 14 20 30 47 78  
Library



86 +

49 +

26 + 59

25 + 84



33 + 20

34 + 40

33 + 55

+ 80

32

31 + 20

31

big

31

M



FK  
RG  
WM  
WJ

March 24, 1966

1

Hamline Ave

Profile & X-sections

4+00 = Co Rd B

Sta +  $\pi$  - Elev.

|    |      |        |        |
|----|------|--------|--------|
| BM | 5.44 | 963.63 | 958.19 |
|----|------|--------|--------|

|     |       |      |
|-----|-------|------|
| 7.9 | 5 5.7 | 55.7 |
|-----|-------|------|

|      |      |      |
|------|------|------|
| 0400 | 5.42 | 58.2 |
|------|------|------|

|     |  |  |      |      |
|-----|--|--|------|------|
| +50 |  |  | 5.02 | 58.6 |
|-----|--|--|------|------|

1

+50

|    |      |        |
|----|------|--------|
| BM | 2.86 | 960.77 |
|----|------|--------|

March 24, 1966

Lt.

£

Rt

2

Top Hyd S.W. Cor. Hamline + "B"

58.9

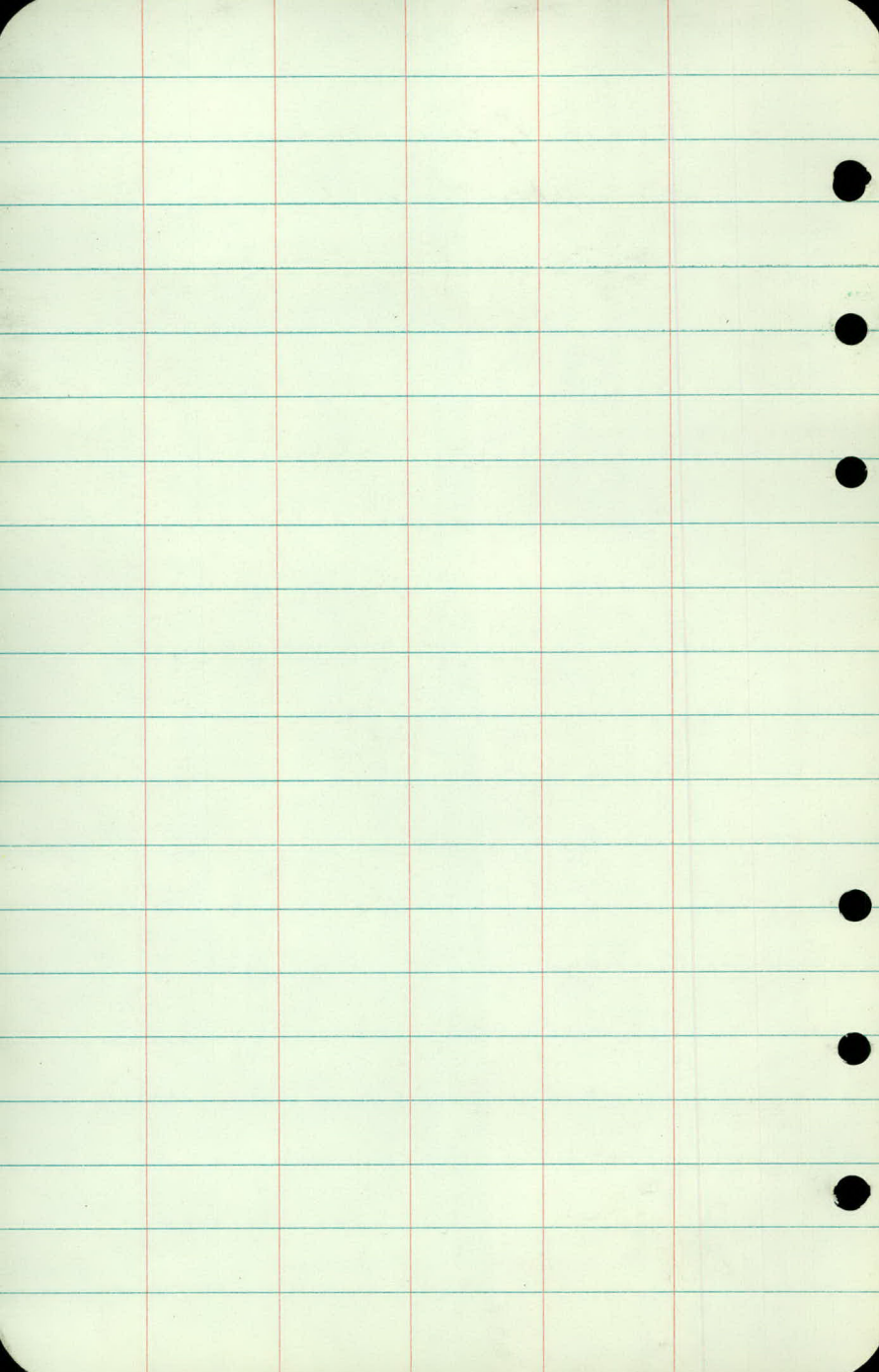
|     |     |     |     |     |      |     |     |     |     |
|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|
| 5.3 | 5.3 | 5.0 | 4.8 | 4.8 | 4.72 | 5.0 | 5.2 | 5.9 | 7.4 |
| 50  | 42  | 29  | 23  | 15  |      | 12  | 20  | 29  | 50  |
| Fe  |     |     |     |     |      |     |     |     |     |

58.9

|       |     |     |     |     |     |     |     |     |      |
|-------|-----|-----|-----|-----|-----|-----|-----|-----|------|
| 4.4   | 4.6 | 4.9 | 4.8 | 4.7 | 5.2 | 5.8 | 8.2 | 9.9 | 10.6 |
| 53.5  | 50  | 41  | 22  | 17  | 14  | 20  | 24  | 30  | 50   |
| House |     | Fe  |     |     |     |     |     |     |      |

Top Hyd NE Cor. Burke + Hamline





1  
Victoria Avenue

Parker to "B"

Plan Survey

Rec. 11-22-65

| Sta | Point | Δ Lt | Δ Rt |
|-----|-------|------|------|
|-----|-------|------|------|

58

~~52~~ + 04.55

45+50.13 P.O.T.

FK  
FS  
LPD

Nov. 18, 1965

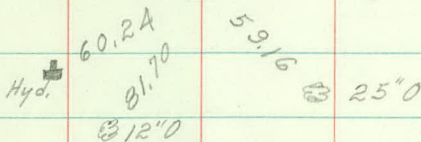
2

S. E. Cor.  
Stucco Ho.

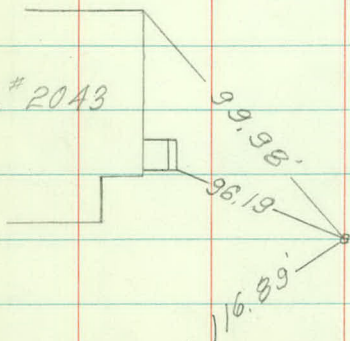
SW. Cor.  
Brick Ho.

N  $\frac{1}{4}$  Cor. Sec. 14

Co. Rd. "B"



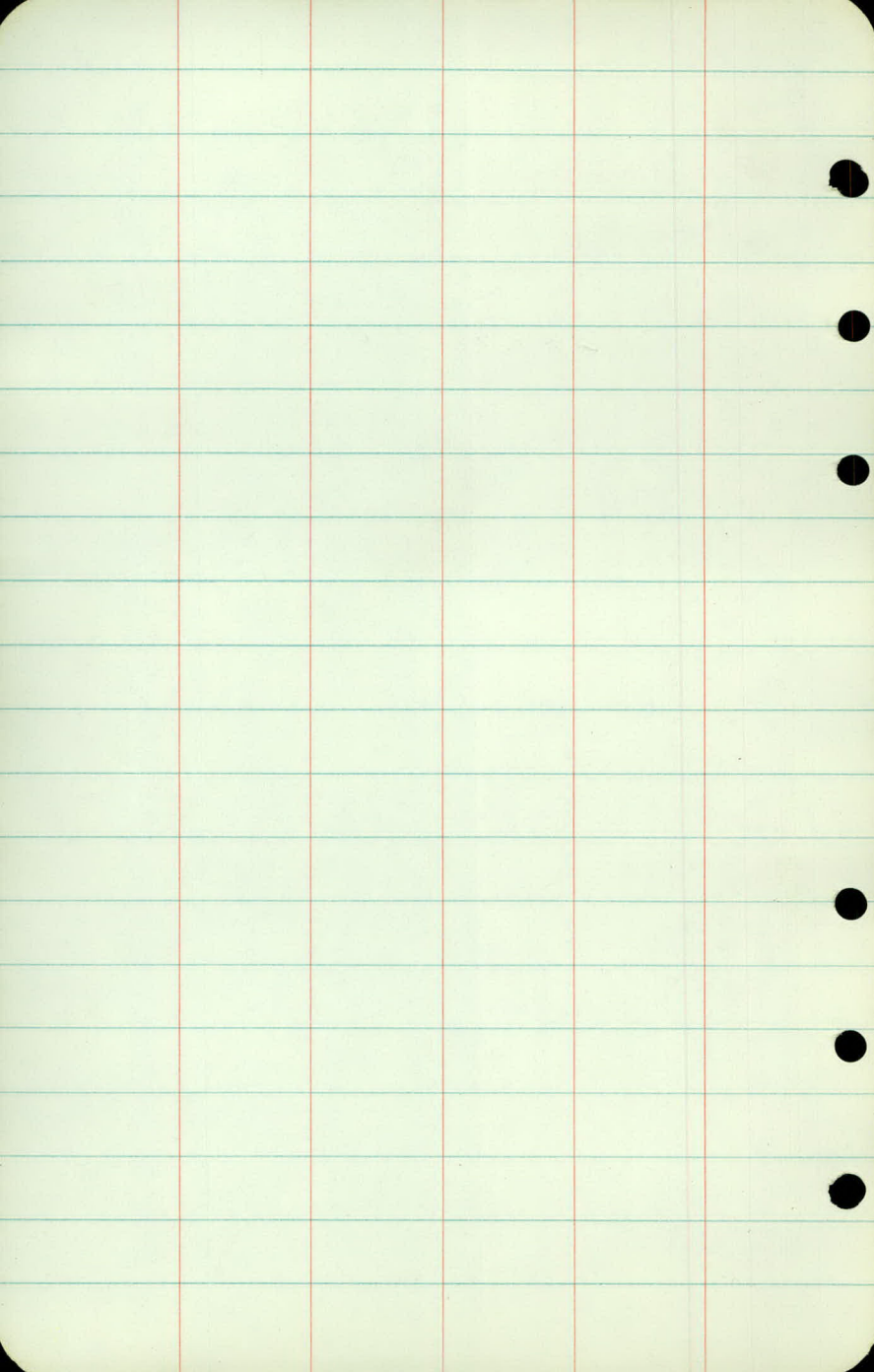
Ho. # 2043



Boat Spike

Ho # 2035





Nov. 18, 1965

3

# TOPOGRAPHY

49

$$\begin{array}{r} \text{Bit} \\ 25 \end{array}$$

$$+98 \frac{18 \text{ Elm}}{61}$$

$$+92 \frac{4 \text{ Pine}}{45}$$

$$+72 \frac{18 \text{ Elm}}{38}$$

$$+91 \frac{12 \text{ Elm}}{38}$$

$$+47 \frac{\text{SE Cor. Ho}}{101}$$

$$+44 \frac{10 \text{ Elm}}{38}$$

$$+47 \frac{8 \text{ Elm}}{55}$$

$$+32 \frac{\text{Ent 10 Elm}}{\text{RT Dirt}}$$

$$+24 \frac{\text{Hedge}}{56}$$

$$+24 \frac{18 \text{ Coll}}{44}$$

$$+106 \frac{6 \text{ Pine}}{56}$$

$$+20 \frac{\text{PP}}{29}$$

48

$$\begin{array}{r} \text{Bit} \\ 23 \ 20 \end{array}$$

$$+72 \frac{8 \text{ Pine}}{46}$$

$$+73 \frac{\text{SE Cor. Ho}}{116}$$

$$+57 \frac{6 \text{ Pine}}{46}$$

$$+53 \frac{30 \text{ Coll}}{43}$$

$$+35 \frac{\text{Ent 12" x 20 CM}}{21}$$

$$+22 \frac{20 \text{ Coll}}{69}$$

$$+108 \frac{\text{Quad 6" Maple}}{41}$$

$$+23 \frac{8 \text{ Pine}}{47}$$

$$+103 \frac{8 \text{ Maple}}{70}$$

$$+12 \frac{28 \text{ Coll}}{46}$$

47

$$\begin{array}{r} \text{Bit} \\ 22 \ 19 \end{array}$$

$$+84 \frac{10 \text{ Mt. Ash}}{52}$$

$$+83 \frac{8 \text{ Coll}}{41}$$

$$+76 \frac{\text{Tw 6 Cedar}}{70}$$

$$+76 \frac{\text{SE Cor. Ho}}{102}$$

$$+62 \frac{6 \text{ Apple 5" A}}{45} \frac{5 \text{ A}}{62}$$

$$+67 \frac{\text{MH}}{16}$$

$$\begin{array}{r} \text{Bit} \\ 21 \ 19 \end{array}$$





50

+49 SE 15" x 20' CM  
20 CR

+33 ER  
20

+39 3" Pine  
33

+20 8" Ash  
47

+24 PP  
28

+22 GV  
11

+14 POR  
30

+06 BR  
49

51

BIT  
22

+01 MH  
44

12" Walnut  
+85 51

+61 SE Cor Ho  
71

+52 4" Maple  
52

+12 Cor Bit  
22

+20 5" Maple  
64

+13 PP  
52

+13 B.M.  
41

+79 ER  
53

+66 POR  
28

+12 Hyd  
35

+14 ER  
18

+49 BR  
22

+11 NE 18' SCP  
20

+46 3" Pine  
53

+05 POR  
25

+06 8" Maple  
85

50

+00 BR  
42

BIT  
20

+05 SW Cor Ho  
107

+91 10' Bit  
Ent

+98 MH  
30

+81 PP  
28

+88.5 MH  
1 Lilac

+72 Cor Bit  
40

+78 7' Xing

+77 STP  
36

+66 Cor Bit  
25

+74 STP  
37

+65 Ent 12" x 20' CM  
26 Bit to 29'

+60 SE 18' x 4' CM  
22

+44 16' Elm  
50

+21 SW Cor Ho  
104

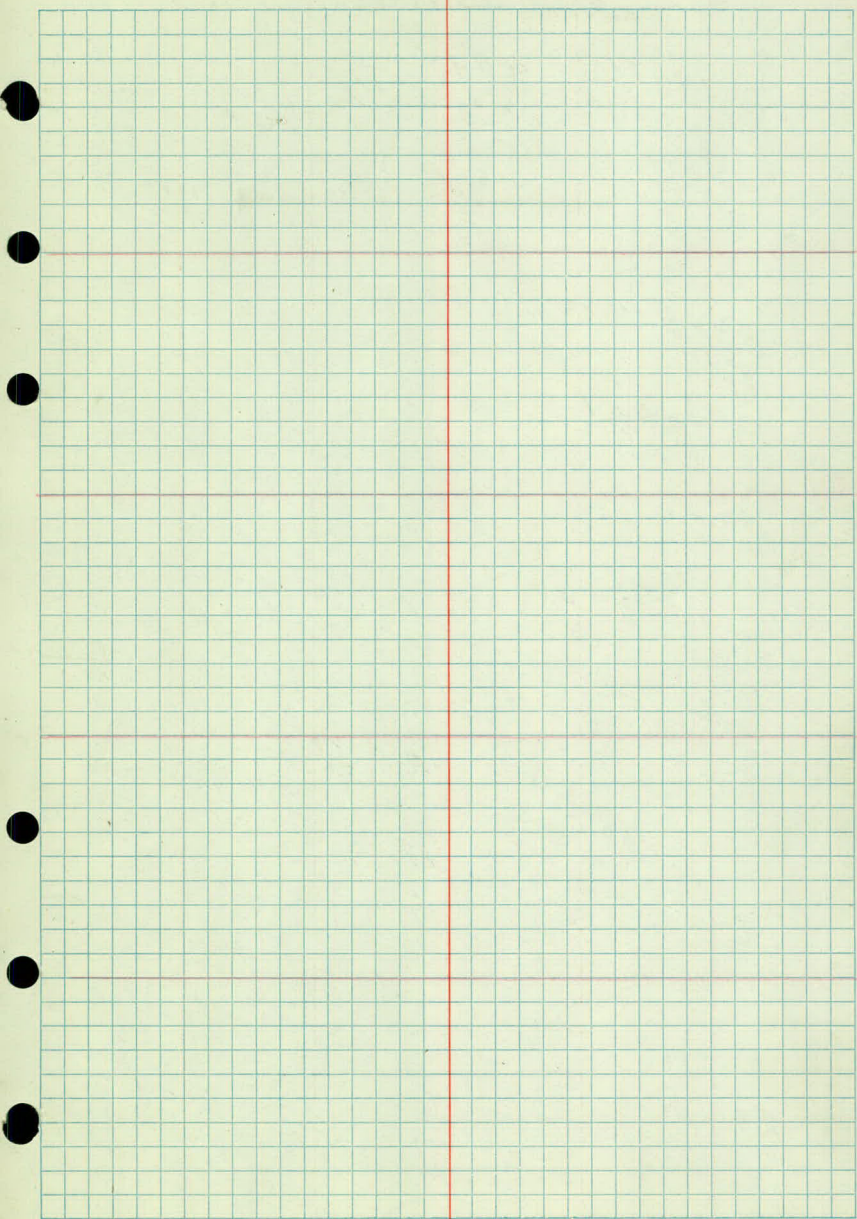
+27 WSO  
33

+32 MH  
17

+12 8' S. Maple  
50

BIT  
25 20

49



54

Pothole Bit  
36 20 19

100 Spillway Pothole  
Bit 35 47

+92 Cluster 6-6" BE  
27

Pothole Begins at  
Edge Woods

+62 Cor Woods  
43

+11 Pothole  
36

+34 Woods  
33

+05 MH  
1.5

+01 Cor Woods  
37

53

+00 Pothole  
100

Bit  
19 19

+01 TP  
29

+94 Cluster 9-4" BE  
25

+96 Lilac Hedge  
35

+51 5" Cotulpa  
75

+41 4" Pine  
46

+46 SW Cor Ho  
113

+25 12" X 23" CM Bit to 33  
33 Dirt

+20 PP  
69

+19 Cor Wall  
29

+20 PP  
29

+16 53" Cott.  
32

+13 B. Wall  
29

52

Bit  
18 18

+00 End Bit  
Ent

+66 3" P  
34

+84 Edge Bit  
33

+78 B. Bit-Ent  
20

+51 SW Cor Ho  
76

50



11" Casting  
 1 Adj. Ring  
 Inv to top = 6.2  
 eccentric Cens W

18" Sensor

Pothole

Woods

CHIEF

Dirt

Bit



5-4"BE

+43 51

+40 R Tie Garage

+38 Tw 20"O  
+33 SW Car Garage

NS = 24.5  
EW = 21.1

+22 3-8"BE  
48

+44 2-4"BE  
32

+35 80

29 28"O  
92

+14 5"BE  
46

+16 10"BE  
51

+20 10"BE  
53

+30 R Tree  
76

+11 9"BE  
38

+12 6"BE  
29

+12 6"BE  
44

+23 28"BE  
29

+20 28"BE  
37

+104 5"BE  
37

+106 4"BE  
37

+110 8"BE  
37

+19 TP  
30

56

Woods  
28

Bit  
21 18

+99 30"BE  
32

+92 4"BE  
41

+88 12"BE  
34

+97 30"BE  
40

+160 Cor Woods  
41

+88 6"BE  
31

+79 12"BE  
38

+160 Cor Pothole  
41

+66 20"BE  
26

54

+71 4"BE  
31

+61 12"BE  
36

+64 5"W  
42

+65 5"W  
38

+62 10"W  
42

+43 Tw 22"Willow  
34

+59 5"W  
40

+61 5"W  
38

+61 5"W  
36

+37 26"Willow  
30

+35 4"BE  
36

+11 4"Cell  
35

+104 Cor Pothole  
41

55

+100 Pothole  
49

Bit  
20 18

+58 TP  
31

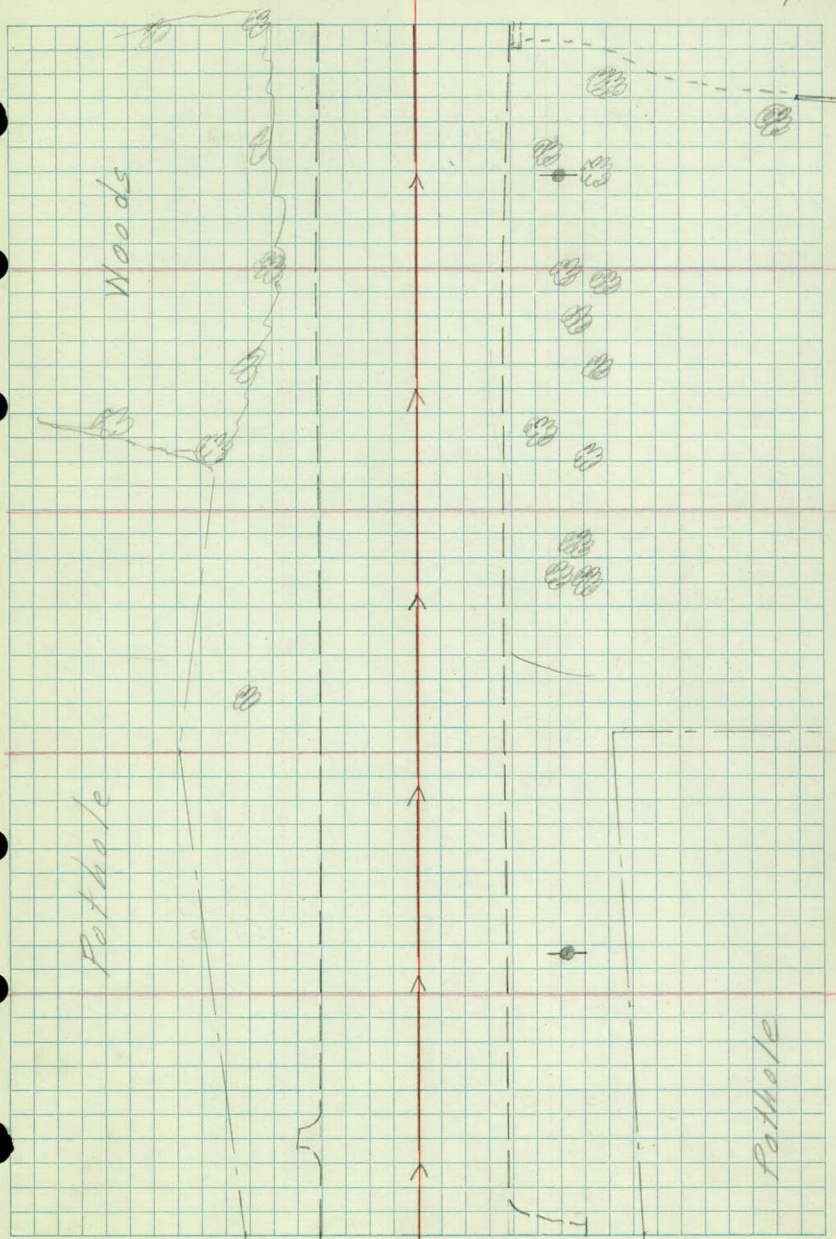
+21 Spillway  
25-19

54

Bit  
20 19

Nov. 22, 1965

7



4

5B

|                |                   |                       |
|----------------|-------------------|-----------------------|
| +89 ER<br>61   | +82 GV<br>34      | +86 ER<br>45          |
| +80 POK<br>46  | +81 GV<br>55      | +71 SE 15' CM<br>32   |
| +78 Hrd<br>55  | +74 POK<br>27     | +78 PP<br>30          |
| +67 24"0<br>74 | +76 PP<br>50      | +59 BR<br>20          |
| +64 POK<br>33  | +58 18"0<br>38    | +73 16"0<br>50        |
| +33 20"0<br>65 | +51 2" Pine<br>69 | +45 Tw 14"0<br>51     |
| +34 Bit<br>27  | +31 12" CK<br>39  | +58 Cor Hedge<br>38   |
| +15 18"0<br>57 | +22 6-5" BE<br>41 | +13 S.W. Cor Ho<br>68 |
| +12 16"0<br>55 | +4 24" BE<br>47   | +35 14" BE<br>54      |

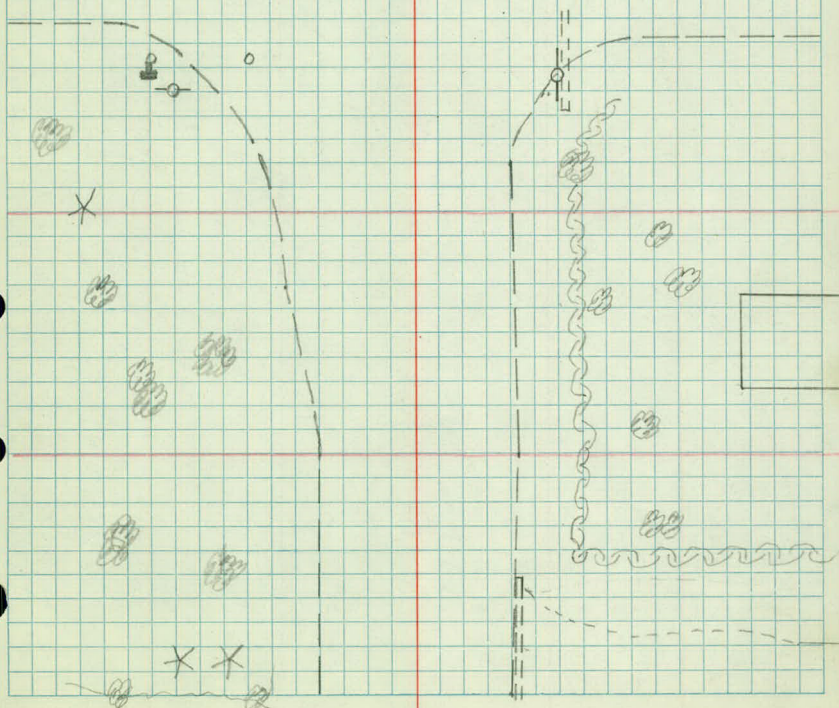
57

|                     |                            |                     |
|---------------------|----------------------------|---------------------|
| +81 Tw 24"0<br>62   | +75 Summit 4" BE<br>39     | +85 10"0<br>59      |
| +57 3" Pine<br>49   | +59 15" x 30" CM Ent<br>21 | +85 14"0<br>49      |
| +50 Cor Woods<br>63 | +51 Cor Woods<br>31        | +78 Cor Lilac<br>23 |

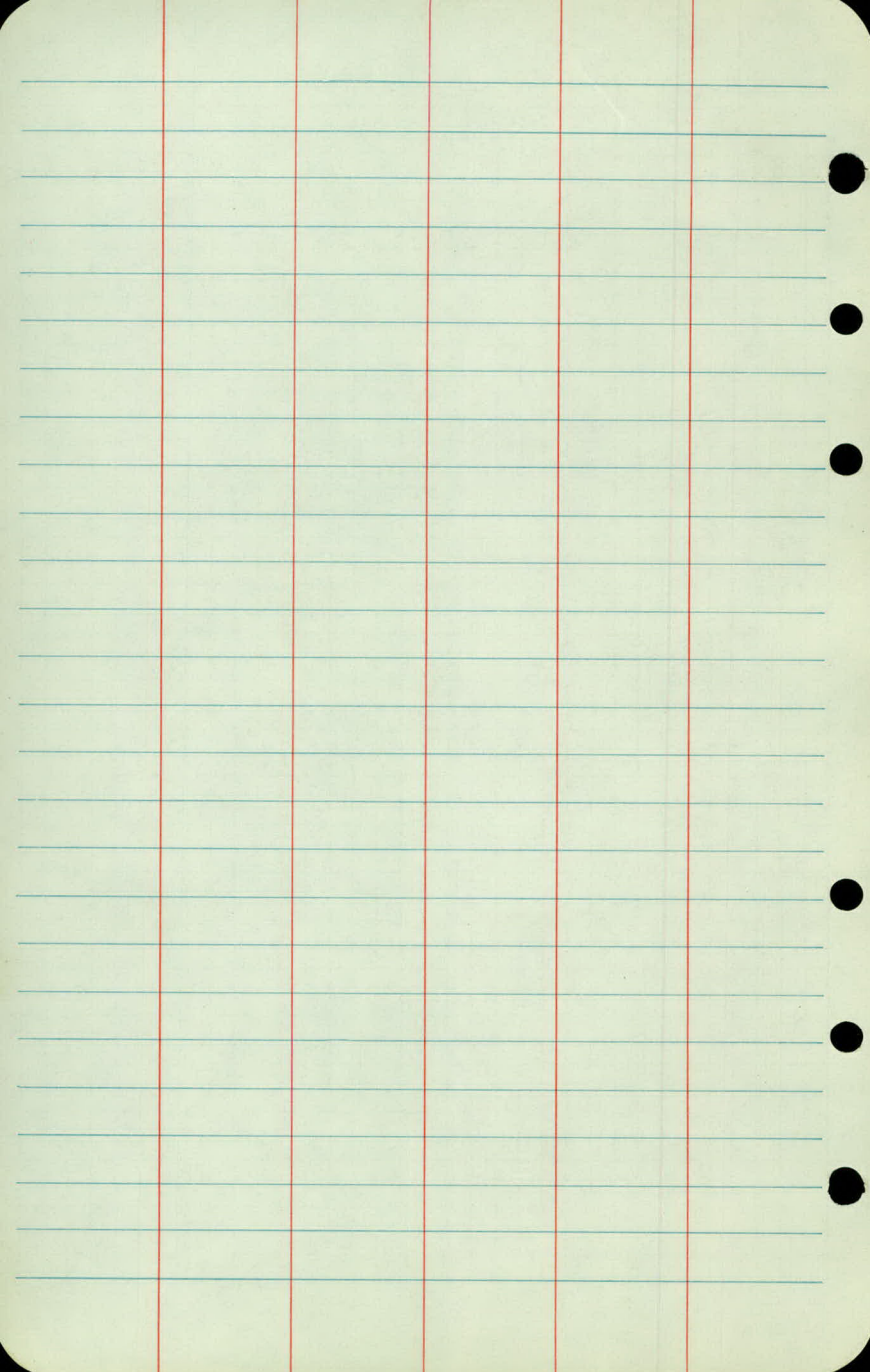


Nov 22, 1965

8







X-Sections

| Sta | +    | $\pi$  | -     | Elev   |
|-----|------|--------|-------|--------|
| BM  | 1.54 | 937.41 |       | 935.87 |
| TP  | 1.00 | 924.61 | 13.80 | 923.61 |
| TP  | 9.25 | 931.65 | 2.21  | 922.40 |
| BM  | 9.12 | 939.20 | 1.57  | 930.08 |
| BM  |      |        | 4.10  | 935.10 |
| BM  |      |        | 2.38  | 936.82 |

|      |       |        |       |        |
|------|-------|--------|-------|--------|
| B.M  | 1.91  | 937.78 |       | 935.87 |
| T.P. | 0.40  | 925.28 | 12.90 | 924.88 |
| T.P. | 13.60 | 938.28 | 0.60  | 924.68 |
| BM   |       |        | 7.20  | 931.08 |
| BM   |       |        | 2.08  | 936.20 |
| BM   |       |        | 0.36  | 937.92 |

|    |      |        |       |        |
|----|------|--------|-------|--------|
| BM | 0.11 | 935.98 |       | 935.87 |
| TP | 1.38 | 924.93 | 12.43 | 923.55 |
| TP |      |        | 2.60  | 922.33 |
| TP | 9.03 | 933.68 | 0.28  | 924.65 |
| TP | 7.51 | 938.54 | 2.65  | 931.03 |

FK  
FS  
LPD

Nov. 19, 1965

10

Top Hyd. S.W. Cor. Victoria & "B"

Sta 56+00 ±

Sta 53+00 ±

Staple in P.P. NE Cor Parker Ave & Victoria  
Roseville

Top Hyd N.W. Cor Parker

Top Hyd. S.W. Cor. Victoria & "B"

Staple in PP N.E. Cor Parker

Roseville BM N.W. Cor Parker & Victoria

TOP HYD. S.W. COR. VICTORIC & "B"

STA 56+00

STA 53+00

STAPLE IN PP NE COR. PARKER AVE - VICT.



|        | +     | $\Sigma$ | -     | ELEV         |
|--------|-------|----------|-------|--------------|
| BM     |       | 938.54   |       |              |
| BM     |       |          | 2.40  | 936.14       |
| BM     | 10.68 | 948.53   | 0.69  | 937.85       |
| 46 +50 |       |          | 0.4   | 48.1<br>38.1 |
| 47     |       |          | 1.5   | 47.0<br>37.0 |
| +50    |       |          | 2.9   | 45.6<br>35.6 |
| 48     |       |          | 1.6   | 43.9<br>33.9 |
| +50    |       |          | 6.3   | 42.2<br>32.2 |
| 49     |       |          | 8.6   | 39.9<br>29.9 |
| +50    |       |          | 10.9  | 37.6<br>27.6 |
| 50     |       |          | 13.4  | 35.1<br>25.1 |
| BM     | 1.73  | 937.87   | 12.39 | 936.14       |

Nov. 19, 1965

11

STAPLE IN PP N.E. COR. PARKER + VICT.

ROSEVILLE

TOP HYD N.W. COR PARKER

Roseville BM N.W. Cor Parker + Victoria

Sta +  $\pi$  - Elev.

937.87

50+50

✓

+62

✓

+80 Gutter Rt

✓

Lt

Nov. 13, 1965

Rt

12

|                     |                     |                     |                     |                     |                     |                     |                     |                     |                     |
|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|
| <sup>33.6</sup> 5.3 | <sup>32.8</sup> 6.1 | <sup>32.8</sup> 6.1 | <sup>33.5</sup> 5.4 | <sup>33.8</sup> 5.1 | <sup>33.5</sup> 5.4 | <sup>33.1</sup> 5.8 | <sup>33.4</sup> 5.5 | <sup>33.5</sup> 5.4 | <sup>36.2</sup> 2.7 |
| 22                  | 20                  | 18                  | 16                  |                     | 12                  | 21                  | 22                  | 26                  | 35                  |

|                     |                     |                     |
|---------------------|---------------------|---------------------|
| <sup>33.7</sup> 5.2 | <sup>36.9</sup> 2.0 | <sup>38.1</sup> 0.2 |
| 24                  | 34                  | 39                  |

|                     |                     |
|---------------------|---------------------|
| <sup>37.9</sup> 1.0 | <sup>37.5</sup> 1.4 |
| 67                  | 51                  |

|                     |                     |                     |                     |                     |                     |                     |                     |                     |                     |                     |
|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|
| <sup>35.5</sup> 3.4 | <sup>32.9</sup> 6.0 | <sup>32.2</sup> 6.7 | <sup>32.2</sup> 6.7 | <sup>33.0</sup> 5.9 | <sup>33.3</sup> 5.6 | <sup>33.1</sup> 5.8 | <sup>32.4</sup> 6.5 | <sup>33.1</sup> 5.8 | <sup>35.8</sup> 3.1 | <sup>37.4</sup> 1.5 |
| 30                  | 23                  | 21                  | 19                  | 16                  |                     | 12                  | 23                  | 26                  | 36                  | 53                  |

|                     |
|---------------------|
| <sup>37.3</sup> 1.6 |
| 36                  |

|                     |
|---------------------|
| <sup>36.9</sup> 2.0 |
| 72                  |

|                     |                     |                     |                     |                     |                     |                     |                     |                     |                     |                     |                     |
|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|
| <sup>34.4</sup> 4.5 | <sup>32.2</sup> 6.7 | <sup>31.6</sup> 7.3 | <sup>31.6</sup> 7.3 | <sup>32.3</sup> 6.6 | <sup>32.7</sup> 6.2 | <sup>32.6</sup> 6.3 | <sup>32.3</sup> 6.6 | <sup>31.8</sup> 7.1 | <sup>31.6</sup> 7.3 | <sup>31.4</sup> 7.5 | <sup>31.2</sup> 7.7 |
| 29                  | 22                  | 21                  | 19                  | 16                  |                     | 12                  | 24                  | 43                  | 63                  | 82                  | 100                 |

|                     |                     |
|---------------------|---------------------|
| <sup>36.4</sup> 2.5 | <sup>38.7</sup> 0.2 |
| 35                  | 43                  |



Sta +  $\pi$  - Elev.

937.87

50+93  $\pm$  Parker A/E

✓

51

✓

+05 Gutter Line

✓

Lt. Nov. 19, 1965 Rt 13

| 32.0 | 31.2 | 31.2 | 31.8 | 32.2 | 32.2 | 31.9 | 31.6 | 31.7 | 31.5 |
|------|------|------|------|------|------|------|------|------|------|
| 6.9  | 7.7  | 7.7  | 7.1  | 6.7  | 6.7  | 7.0  | 7.3  | 7.2  | 7.4  |
| 23   | 20   | 18   | 16   | 12   | 26   | 48   | 70   | 100  |      |

| 35.2 | 37.9 | 38.8 |
|------|------|------|
| 3.7  | 1.0  | 0.1  |
| 32   | 42   | 47   |

| 30.9 | 31.1 |
|------|------|
| 8.0  | 7.8  |
| 200  | 150  |

| 31.8 | 31.0 | 31.0 | 31.4 | 31.9 | 31.9 | 31.6 | 31.5 | 31.3 |
|------|------|------|------|------|------|------|------|------|
| 7.1  | 7.9  | 7.9  | 7.5  | 7.0  | 7.0  | 7.3  | 7.4  | 7.6  |
| 22   | 20   | 18   | 16   | 12   | 30   | 51   | 73   |      |

| 35.4 | 37.5 | 38.1 |
|------|------|------|
| 3.5  | 1.4  | 0.2  |
| 33   | 44   | 55   |

| 34.7 | 31.9 | 31.0 | 31.0 | 31.2 | 31.7 | 31.7 | 31.3 | 31.3 | 31.2 |
|------|------|------|------|------|------|------|------|------|------|
| 4.2  | 7.0  | 7.9  | 7.9  | 7.7  | 7.2  | 7.2  | 7.6  | 7.6  | 7.7  |
| 31   | 22   | 20   | 19   | 17   | 12   | 28   | 49   | 76   |      |

| 36.6 | 37.9 |
|------|------|
| 2.3  | 1.0  |
| 40   | 56   |

Sta +  $\pi$  - Elev.

937.87

51+20

✓

G.V. Lt 8.07

+52 Ent Lt

✓

+69

✓

T.P. 4.16 930.37 11.66 926.21

+70 NE Culv 20' Lt <sup>273</sup> 3.98 26.39

Lt

E Nov. 13, 1965

Rt.

14

| 31.1 | 30.3 | 30.3 | 30.7 | 31.2 | 31.0 | 30.7 | 31.4 | 32.2 | 32.3 |
|------|------|------|------|------|------|------|------|------|------|
| 7.8  | 8.6  | 8.6  | 8.2  | 7.7  | 7.9  | 8.2  | 7.5  | 6.7  | 6.6  |
| 23   | 20   | 18   | 16   |      | 12   | 21   | 30   | 44   | 57   |

| 34.6 | 35.7 | 36.4 | 37.0 |
|------|------|------|------|
| 4.3  | 3.2  | 2.5  | 1.9  |
| 37   | 49   | 62   | 72   |

Ent

| 34.4 | 32.7 | 30.7 | 29.9 | 29.3 | 29.6 | 29.4 | 29.1 | 29.5 | 29.7 | 31.7 |
|------|------|------|------|------|------|------|------|------|------|------|
| 4.5  | 6.2  | 8.2  | 9.0  | 9.6  | 9.3  | 9.5  | 9.8  | 9.4  | 9.2  | 7.2  |
| 65   | 47   | 33   | 20   | 16   |      | 12   | 18   | 19   | 25   | 40   |

| 32.08 | 32.2 | 32.0 |
|-------|------|------|
| 6.79  | 6.7  | 6.9  |
| 71    | 70   | 54   |

Walk

| 30.7 | 30.0 | 29.1 | 28.5 | 28.7 | 28.5 | 28.2 | 28.7 | 30.1 | 31.5 |
|------|------|------|------|------|------|------|------|------|------|
| 8.2  | 8.9  | 9.8  | 10.4 | 10.2 | 10.4 | 10.7 | 10.2 | 8.8  | 7.4  |
| 33   | 24   | 19   | 16   |      | 12   | 17   | 19   | 31   | 44   |

| 33.0 | 34.6 |
|------|------|
| 5.9  | 4.3  |
| 52   | 70   |

| 31.9 |
|------|
| 7.0  |
| 61   |



Sta + X - Elev.

930.37

51 + 82 S. Edge Ent Rt

✓

52

✓

+18

✓

Nov. 19, 1965

LT

RT

15

| 25.6 | 27.2 | 27.1 | 26.9 | 27.1 | 26.9 | 26.6 | 26.9 | 27.5 | 29.5 |
|------|------|------|------|------|------|------|------|------|------|
| 4.8  | 3.2  | 3.3  | 3.5  | 3.3  | 3.5  | 3.8  | 3.5  | 2.9  | 0.9  |
| 25   | 21   | 17   | 16   |      | 11   | 17   | 18   | 28   | 43   |

24.9 25.9  
→ 5.5 4.5  
38 55

30.4  
0.0  
52

| 23.8 | 25.0 | 26.0 | 25.8 | 26.2 | 26.0 | 25.7 | 26.2 | 27.4 | 29.3 | 30.3 |
|------|------|------|------|------|------|------|------|------|------|------|
| 6.6  | 5.4  | 4.4  | 4.6  | 4.2  | 4.4  | 4.7  | 4.2  | 3.0  | 1.1  | 0.1  |
| 26   | 20   | 17   | 16   |      | 11   | 17   | 18   | 30   | 46   | 55   |

Ent

23.5 22.5  
→ 6.9 7.9  
41 62

| 23.0 | 24.0 | 25.3 | 24.9 | 25.4 | 25.2 | 24.7 | 25.0 | 23.5 | 23.4 |
|------|------|------|------|------|------|------|------|------|------|
| 7.4  | 6.4  | 5.1  | 5.5  | 5.0  | 5.2  | 5.7  | 5.4  | 6.9  | 7.0  |
| 24   | 19   | 17   | 16   |      | 11   | 16   | 18   | 24   | 27   |

21.4 21.2 21.0 20.2  
→ 9.0 9.2 9.4 10.2  
32 39 53 71

25.9 25.8 25.2 24.2  
4.5 4.6 5.2 6.2  
76 62 42 28

Wall

Sta +  $\pi$  - Elev.

930.37

32+19

✓

+23 SE 12" 1/4 33' RT 10.02 20.35

+33 Ent RT

✓

+47

✓

T.P. 2.16 924.50 8.03 922.34

Lt

Nov. 19, 1965

St

16

25.4

25.0

24.5

23.3

22.9

22.3

Duplicate + 18

5.0 5.4 5.9 7.1 7.5 8.1  
13 17 25 29 37

22.8

22.7

7.6

7.7

74

54

19.8

20.3

22.2

24.6

24.2

24.8

24.6

24.3

23.0

22.8

22.8

23.0

106 10.1 8.2 5.8 6.2 5.6 5.8 6.1 7.4 7.6 7.6 7.4  
49 34 22 18 16 11 17 28 47 70 100

19.3

18.5

11.1  
64

11.9  
81

18.5

20.2

24.0

23.5

24.3

24.1

23.6

23.9

23.1

20.2

11.9 10.2 6.4 6.9 6.1 6.3 6.8 6.5 7.3 10.2  
41 25 17 16 11 17 18 21 30

18.3

17.7

16.8

23.47

22.9

22.2

21.8

20.7

19.81

12.1 12.7 13.6 6.90 7.5 8.2 8.6 9.7 10.56  
62 84 100 103 86 62 42 36 32  
FL Culv

No Walk

532



Sta +  $\pi$  - Elev,

924.50

52+84

✓

53

✓

53+05 MH 4.5' Lt 2.35 22.15

+50

✓

Nov. 13, 1965

Lt.

RT

17



|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 17.7 | 21.4 | 22.1 | 22.4 | 22.9 | 22.5 | 22.1 | 22.3 | 21.5 | 19.1 |
| 6.8  | 2.1  | 2.4  | 2.1  | 1.6  | 2.0  | 2.4  | 2.2  | 3.0  | 5.4  |
| 28   | 18   | 16   | 11   |      | 11   | 17   | 18   | 22   | 31   |

|      |      |      |      |  |      |      |      |      |
|------|------|------|------|--|------|------|------|------|
| 15.6 | 15.3 | 13.5 | 14.8 |  | 21.8 | 21.4 | 20.7 | 19.0 |
| 8.9  | 9.2  | 10.0 | 9.7  |  | 2.7  | 3.1  | 3.8  | 5.5  |
| 43   | 58   | 80   | 100  |  | 29   | 68   | 49   | 38   |



|      |      |      |      |      |       |      |      |      |      |      |
|------|------|------|------|------|-------|------|------|------|------|------|
| 14.9 | 21.1 | 21.9 | 21.6 | 21.8 | 22.34 | 21.9 | 21.5 | 21.9 | 21.3 | 20.7 |
| 96   | 34   | 26   | 29   | 2.7  | 2.16  | 2.6  | 3.0  | 2.6  | 3.2  | 3.8  |
| 36   | 23   | 18   | 16   | 11   |       | 11   | 17   | 18   | 21   | 25   |

|      |      |      |  |      |      |      |      |      |
|------|------|------|--|------|------|------|------|------|
| 12.4 | 13.5 | 13.4 |  | 17.8 | 17.1 | 16.8 | 17.0 | 17.6 |
| 11.1 | 11.0 | 11.1 |  | 6.7  | 7.4  | 7.7  | 7.5  | 6.9  |
| 57   | 80   | 100  |  | 100  | 78   | 60   | 46   | 32   |



|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 19.3 | 20.2 | 20.0 | 20.3 | 20.4 | 20.4 | 20.0 | 20.3 | 19.9 | 15.0 | 13.9 |
| 52   | 43   | 45   | 4.2  | 3.7  | 4.1  | 4.5  | 4.2  | 4.6  | 9.5  | 10.6 |
| 25   | 18   | 16   | 11   |      | 11   | 17   | 18   | 21   | 30   | 38   |

|      |      |      |      |      |  |      |      |      |
|------|------|------|------|------|--|------|------|------|
| 12.5 | 11.7 | 11.4 | 11.4 | 11.5 |  | 12.8 | 12.7 | 13.4 |
| 12.0 | 12.8 | 13.1 | 13.1 | 13.0 |  | 11.7 | 11.8 | 11.1 |
| 38   | 40   | 52   | 75   | 100  |  | 100  | 75   | 54   |

Sta +  $\pi$  - Elev.

924.50

54+00

✓

TP 4.28 924.15 4.63 919.87 sta 55

+50

✓

55

✓

Nov. 18, 1965

L4

RT

18

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 19.1 | 19.3 | 18.9 | 19.3 | 19.8 | 19.5 | 19.0 | 19.2 | 14.1 | 11.6 |
| 5.4  | 5.2  | 5.6  | 5.2  | 4.7  | 5.0  | 5.5  | 5.3  | 10.4 | 12.9 |
| 23   | 18   | 16   | 11   |      | 11   | 17   | 18   | 32   | 44   |

|            |      |      |      |      |  |            |      |      |
|------------|------|------|------|------|--|------------|------|------|
| 12.4       | 10.5 | 10.8 | 09.9 | 09.8 |  | 10.3       | 11.1 | 11.2 |
| 12.1       | 14.0 | 13.7 | 14.6 | 14.7 |  | 14.2       | 13.4 | 13.3 |
| 36         | 50   | 69   | 86   | 100  |  | 100        | 95   | 55   |
| 12.1 = 1cc |      |      |      |      |  | 13.0 = 1cc |      |      |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 12.5 | 19.1 | 19.1 | 18.8 | 19.2 | 19.6 | 19.1 | 18.8 | 19.1 | 18.6 | 12.8 |
| 11.7 | 5.1  | 5.1  | 5.4  | 5.0  | 4.6  | 5.1  | 5.4  | 5.1  | 5.6  | 11.4 |
| 42   | 29   | 19   | 17   | 11   |      | 11   | 16   | 17   | 22   | 35   |

|            |      |      |  |            |      |      |      |
|------------|------|------|--|------------|------|------|------|
| 10.5       | 09.9 | 09.4 |  | 09.0       | 09.1 | 09.5 | 11.5 |
| 13.7       | 14.3 | 14.4 |  | 15.2       | 15.1 | 14.7 | 12.7 |
| 56         | 80   | 100  |  | 100        | 80   | 62   | 43   |
| 11.7 = 1cc |      |      |  | 1cc = 12.7 |      |      |      |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 18.8 | 19.5 | 19.1 | 19.6 | 19.9 | 19.6 | 19.2 | 19.6 | 19.4 | 12.2 |
| 5.4  | 4.7  | 5.1  | 4.6  | 4.3  | 4.6  | 5.0  | 4.6  | 4.8  | 12.0 |
| 29   | 19   | 18   | 11   |      | 11   | 16   | 17   | 19   | 39   |

|      |      |      |      |  |      |      |      |      |
|------|------|------|------|--|------|------|------|------|
| 12.6 | 10.9 | 10.0 | 09.7 |  | 10.9 | 11.5 | 10.9 | 11.5 |
| 11.6 | 13.3 | 14.2 | 14.5 |  | 13.3 | 12.7 | 13.3 | 12.7 |
| 47   | 55   | 80   | 100  |  | 100  | 78   | 55   | 50   |



Sta +  $\pi$  - Elev.

924.15

55+50.

11.7 =  
100

✓

56

✓

TP 6.41 929.99 0.57 923.58 56 ±

+33

✓

Nov. 13, 1965

Lt.

Rt.

19

| 20.3 | 20.9 | 20.3 | 20.8 | 21.3 | 21.3 | 21.1 | 21.7 | 20.8 | 19.2 |
|------|------|------|------|------|------|------|------|------|------|
| 3.9  | 3.3  | 3.9  | 3.4  | 2.9  | 2.9  | 3.1  | 2.5  | 3.4  | 5.0  |
| 26   | 20   | 18   | 11   |      | 11   | 16   | 18   | 22   | 29   |

| 13.5 | 12.5 | 10.8 | 10.1 | 10.2 | 18.2 | 17.6 | 17.9 |
|------|------|------|------|------|------|------|------|
| 10.7 | 11.7 | 13.4 | 14.1 | 14.0 | 6.0  | 6.6  | 6.3  |
| 39   | 47   | 70   | 85   | 100  | 100  | 80   | 51   |

| 23.0 | 23.5 | 23.0 | 23.3 | 23.6 | 23.6 | 23.3 | 23.6 | 20.9 | 20.0 |
|------|------|------|------|------|------|------|------|------|------|
| 1.2  | 0.7  | 1.2  | 0.9  | 0.6  | 0.6  | 0.9  | 0.6  | 3.3  | 4.2  |
| 26   | 20   | 19   | 11   |      | 11   | 16   | 17   | 23   | 52   |

| 16.6 | 14.1 | 12.6 | 11.4 | 19.2 | 19.8 |
|------|------|------|------|------|------|
| 7.6  | 10.1 | 11.6 | 12.8 | 5.0  | 4.4  |
| 37   | 63   | 87   | 100  | 100  | 78   |

| 19.1 | 24.4 | 25.1 | 24.6 | 24.8 | 25.1 | 25.1 | 24.8 | 25.2 | 24.3 | 23.6 | 26.7 |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 10.9 | 5.6  | 4.9  | 5.4  | 5.2  | 4.9  | 4.9  | 5.2  | 4.8  | 5.7  | 6.4  | 3.8  |
| 37   | 27   | 22   | 20   | 13   |      | 11   | 16   | 17   | 20   | 24   | 31   |

| 16.0 | 14.9 | 13.7 | 27.4 | 26.3 | 25.8 | 25.8 | 24.8 | 26.1 |
|------|------|------|------|------|------|------|------|------|
| 14.0 | 15.1 | 16.3 | 2.6  | 3.7  | 4.2  | 4.2  | 5.2  | 3.9  |
| 54   | 88   | 100  | 91   | 79   | 68   | 52   | 43   | 38   |

Garage

Sta +  $\pi$  - Elev

929.99

56+44

✓

+58  $\pm$  Elev

✓

+75

✓

TP 9.69 938.11 1.57 928.42 57  $\pm$

Nov. 19, 1965

✓

20

250

257

25.5

25.6

25.2

25.3

25.5

25.7

25.4

25.7

25.3

4.5 4.4 4.8 4.7 4.5 4.3 4.6 4.3 4.7

28 22 21 12 10 16 17 20 21

Culv

19.5

17.3

15.4

14.7

27.5

26.8

26.3

26.5

26.2

25.0

→ 10.5 12.7 14.6 15.3 2.5 3.2 3.7 3.5 3.8 5.0

39 62 85 100 91 76 53 36 28 24

Garage

25.8

26.3

25.8

26.0

26.2

26.4

26.3

26.5

26.2

26.7

4.2 3.7 4.2 4.0 3.8 3.6 3.7 3.5 3.8 3.3

28 23 22 14 10 17 18 24 51

21.1

20.5

19.3

15.8

29.4

27.7

→ 8.9 9.5 11.7 14.2

37 55 73 100

0.6 2.3

82 69

✓

24.5

26.9

27.0

26.7

26.8

27.0

27.3

27.1

33.5

27.6

28.7

5.5 3.1 3.0 3.3 3.2 3.0 2.7 2.9 2.4 1.3

(47 29 23 22 12 12 16 21 25 29

Culv

23.1

20.2

19.8

33.0

33.0

32.5

→ 6.9 9.8 10.2

65 84 100

+3.0 +3.0 +2.5

79 64 47



Sta +  $\pi$  - Elev.

938.11

57+00

✓

+35

✓

+62

✓

Nov. 19, 1965

14

B1

21

✓

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 27.7 | 28.2 | 27.8 | 28.0 | 28.4 | 28.6 | 28.1 | 28.7 | 32.0 | 35.3 |
| 10.4 | 9.9  | 10.3 | 10.1 | 9.7  | 9.5  | 10.0 | 9.4  | 6.1  | 2.8  |
| 34   | 24   | 23   | 14   |      | 10   | 20   | 21   | 28   | 37   |

|      |      |      |      |  |      |      |
|------|------|------|------|--|------|------|
| 25.6 | 27.4 | 25.4 | 23.1 |  | 36.3 | 36.7 |
| 9.5  | 10.7 | 12.7 | 15.0 |  | 1.8  | 1.7  |
| 41   | 57   | 79   | 100  |  | 62   | 50   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 28.8 | 29.9 | 30.1 | 29.8 | 30.1 | 30.5 | 30.7 | 30.4 | 31.0 | 34.1 | 37.8 |
| 9.3  | 8.2  | 8.0  | 8.3  | 8.0  | 7.6  | 7.4  | 7.7  | 7.1  | 4.0  | 0.3  |
| 37   | 33   | 27   | 26   | 13   |      | 10   | 20   | 21   | 29   | 35   |

|      |      |      |      |      |      |  |      |      |
|------|------|------|------|------|------|--|------|------|
| 30.4 | 32.3 | 32.3 | 30.2 | 27.9 | 26.3 |  | 37.4 | 37.8 |
| 7.2  | 5.8  | 5.8  | 7.9  | 10.2 | 11.8 |  | 0.2  | 0.3  |
| 39   | 48   | 61   | 74   | 85   | 100  |  | 62   | 53   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 30.3 | 31.1 | 31.6 | 31.2 | 31.7 | 32.1 | 32.2 | 32.1 | 32.6 | 31.7 | 34.7 |
| 7.8  | 7.0  | 6.5  | 6.9  | 6.4  | 6.0  | 5.9  | 6.0  | 5.5  | 6.4  | 3.4  |
| 44   | 34   | 32   | 31   | 13   |      | 13   | 19   | 21   | 26   | 35   |

|      |      |      |  |      |      |      |
|------|------|------|--|------|------|------|
| 32.3 | 32.9 | 31.6 |  | 37.1 | 37.0 | 37.3 |
| 5.8  | 5.2  | 6.5  |  | 1.0  | 1.1  | 0.8  |
| 47   | 65   | 83   |  | 78   | 58   | 42   |

Sta

+

$\pi$

-

Elev

938.11

58+46

+73

BM

2.21 935.90 935.52

11

2

Nov. 19, 1965

Rt

22

| 35.2 | 35.0 | 33.6 | 33.1 | 33.5 | 33.7 | 33.9 | 34.1 | 34.6 | 35.6 | 36.0 |
|------|------|------|------|------|------|------|------|------|------|------|
| 29   | 31   | 45   | 50   | 46   | 44   | 42   | 40   | 35   | 25   | 21   |
| 60   | 39   | 26   | 25   | 12   |      | 15   | 16   | 23   | 39   | 61   |

| 36.0 | 34.9 | 34.0 | 33.5 | 33.8 | 34.0 | 34.3 | 34.1 | 35.4 | 33.7 | 36.8 |
|------|------|------|------|------|------|------|------|------|------|------|
| 2.1  | 3.2  | 4.1  | 4.6  | 4.3  | 4.1  | 3.8  | 3.6  | 2.7  | 4.4  | 1.22 |
| 61   | 29   | 23   | 22   | 12   |      | 13   | 14   | 27   | 48   | 60   |

Walk

Top Hyd S.W. Cor. Victoria & "B"



11+17 & VICTORIA

11+00

31.2