

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN

Survey

County Road "C"

From Cleveland To Snelling

Road Acc't. No. 23

DR. 9

Date Filed 2-63

File BK. 50

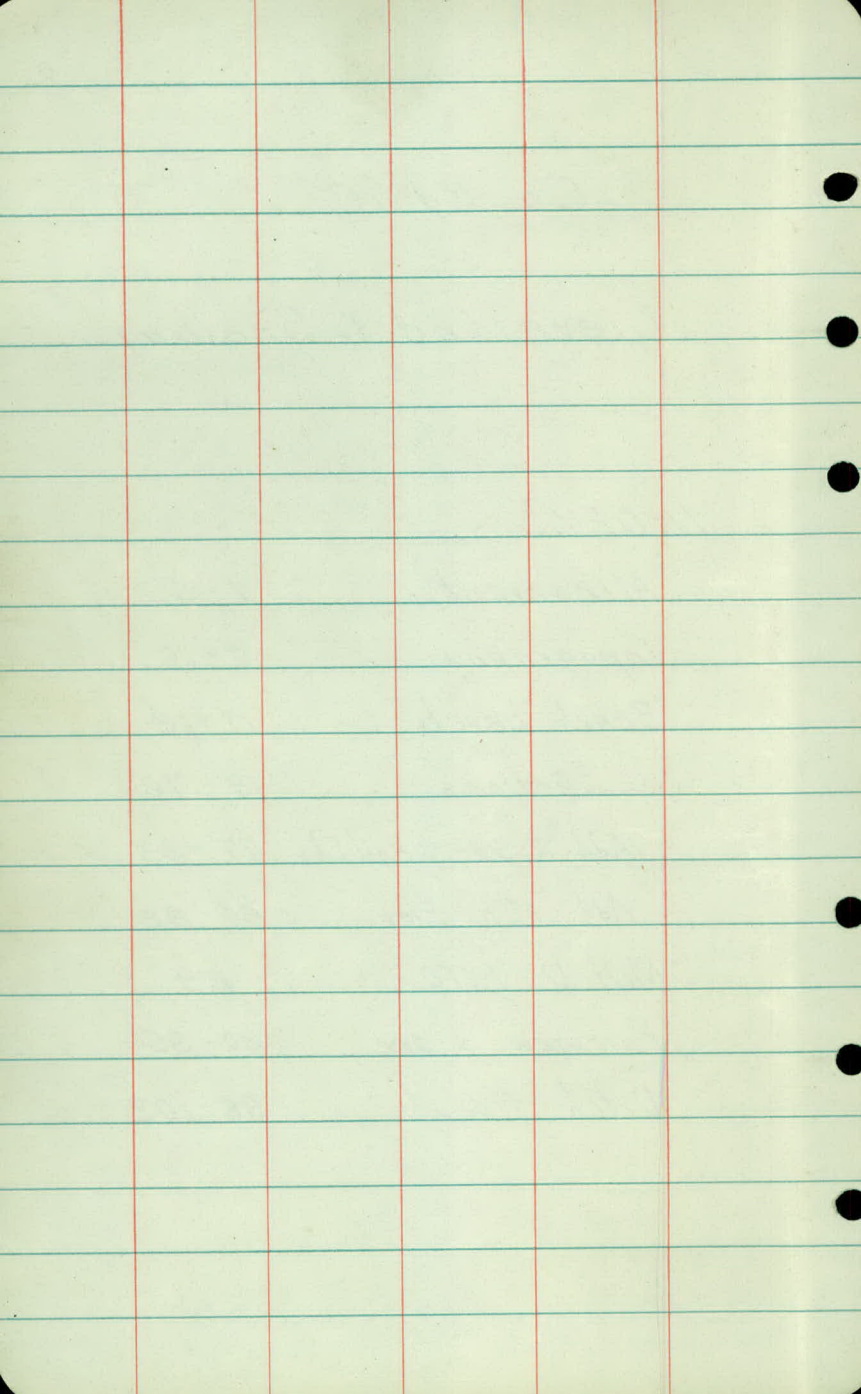
3

Co. Rd. "C"

Cleveland to Snelling

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Co. Rd. "C"

Cleveland to Snelling

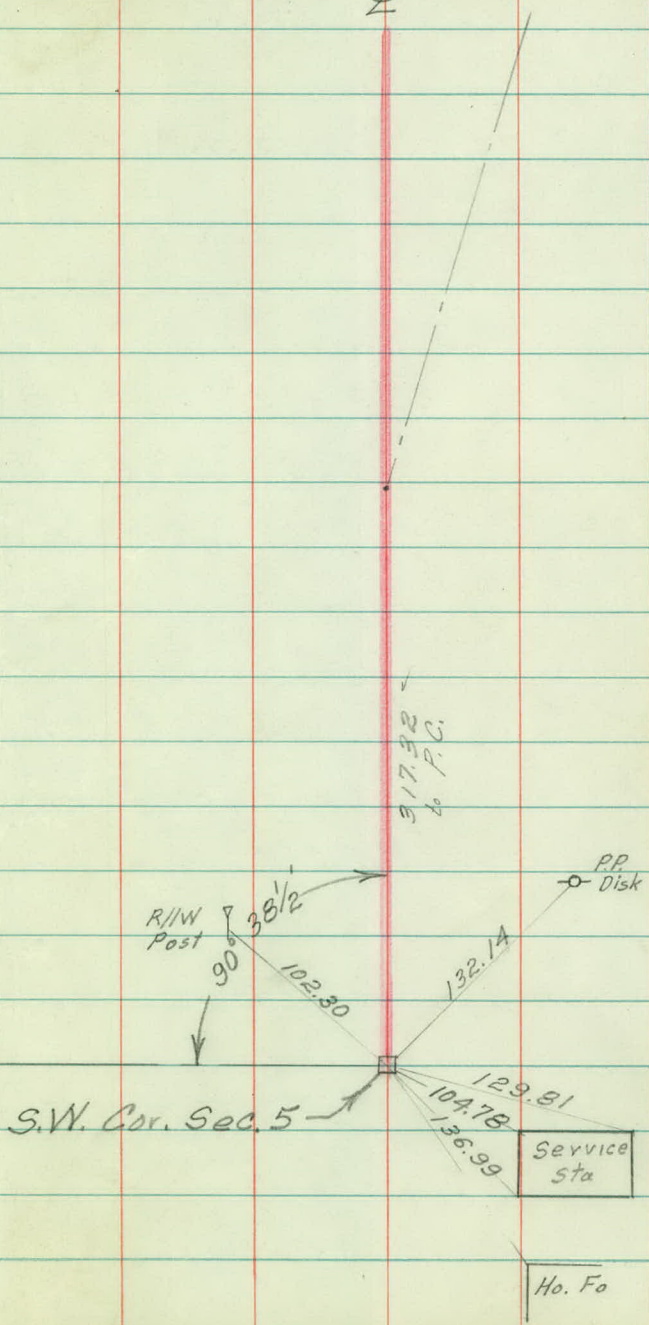
Alinement

5- Pages

Sta	Point	$\Delta Lt.$	$\Delta Rt.$
61+75.76	P.T.	$5^{\circ}33'$	
+50		$5^{\circ}13\frac{1}{2}'$	$P.I. = 58+99.15$
61		$4^{\circ}43\frac{1}{2}'$	$\Delta = 11^{\circ}06' Lt.$
+50		$4^{\circ}13\frac{1}{2}'$	$\frac{1}{2}\Delta = 5^{\circ}33'$
60		$3^{\circ}43\frac{1}{2}'$	$D = 2^{\circ}$
+50		$3^{\circ}13\frac{1}{2}'$	$T = 278.39$
59		$2^{\circ}43\frac{1}{2}'$	$L = 555.00$
+50		$2^{\circ}13\frac{1}{2}'$	$R = 2864.93$
58		$1^{\circ}43\frac{1}{2}'$	
+50		$1^{\circ}13\frac{1}{2}'$	
57		$0^{\circ}43\frac{1}{2}'$	
+50		$0^{\circ}13\frac{1}{2}'$	
56+20.76	P.C.	$0^{\circ}00'$	

53+03.44 ∇ Cleveland

Σ



Sta. point ΔL ΔR

+34.47	P.T.	$4^{\circ} 16\frac{1}{2}'$
73		$3^{\circ} 56.4'$ P.I. = 71+20.62 [✓]
+50		$3^{\circ} 26.4'$ $\Delta = 8^{\circ} 33' R$
72		$2^{\circ} 56.4'$ $\frac{1}{2}\Delta = 4^{\circ} 16\frac{1}{2}'$
+50		$2^{\circ} 26.4'$ $D = 1^{\circ} 59' 42.5''$
71		$1^{\circ} 56.4'$ $T = 214.69'$ [✓]
+50		$1^{\circ} 26.4'$ $L = 428.54$
70		$0^{\circ} 56.4'$ $R = 2871.93$
+50		$0^{\circ} 26.4'$
69+05.93	P.C. [✓]	$0^{\circ} 00'$

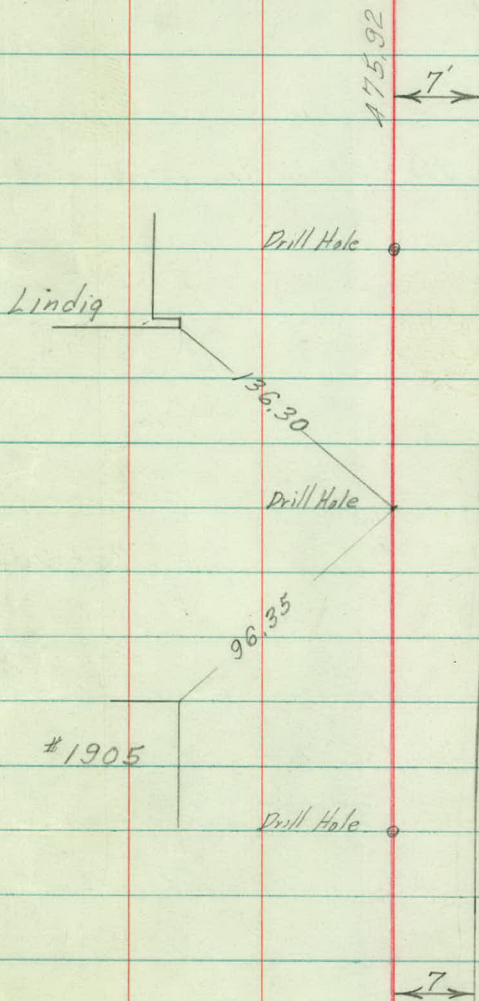
FK
WS
R Boss

Jan. 4, 1962

3

£

A-3



Sta Point Δ Lt. Δ Rt.

79+53.28 P.O.T.

New Brighton Road

P.I. 78+80.70

P.L. = ~~78+83.27~~ ? ✓

+51.96 P.T.

$\Delta = 5^{\circ}36'$

79

$\frac{1}{2}\Delta = 2^{\circ}48'$

+50

$D = 3^{\circ}58^{\circ}50''$

78+11.27 P.C. ←

$T = 70.41$

+10.35 PC Measured =

$L = 140.69$

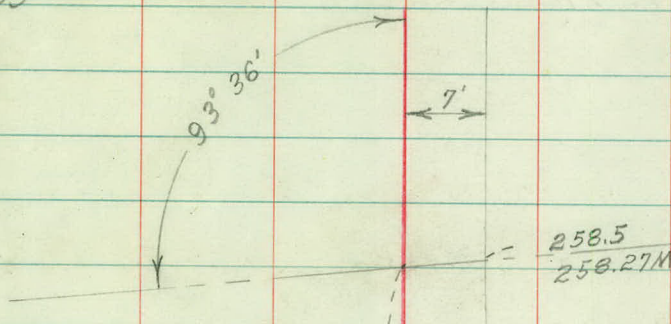
✓ $R = 1439.69$

FK
XP
WS
DS

Jan. 7, 1963

4

A-4

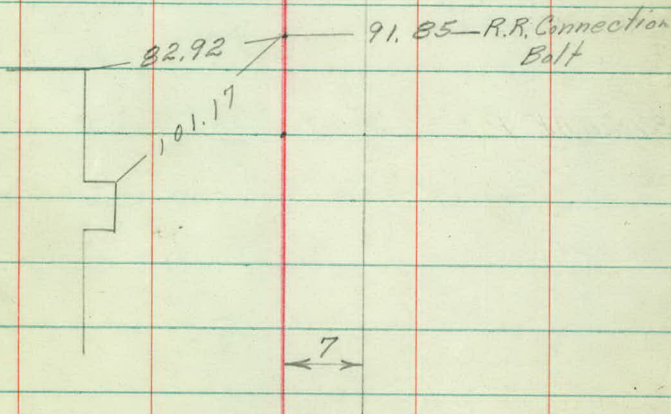


101.22
26.96
112.65

Disk
P.P.

0 27.95

1.32



Sta. Point ΔL ΔR

105+90.58 P.I.

✓
87+24.01 P.I. 0° 04'

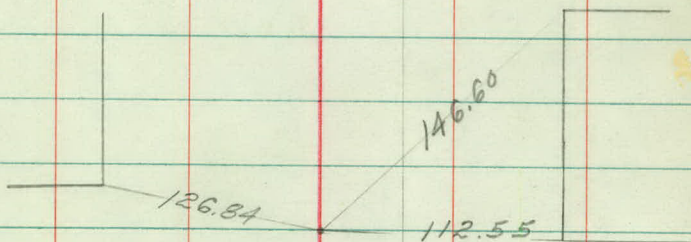
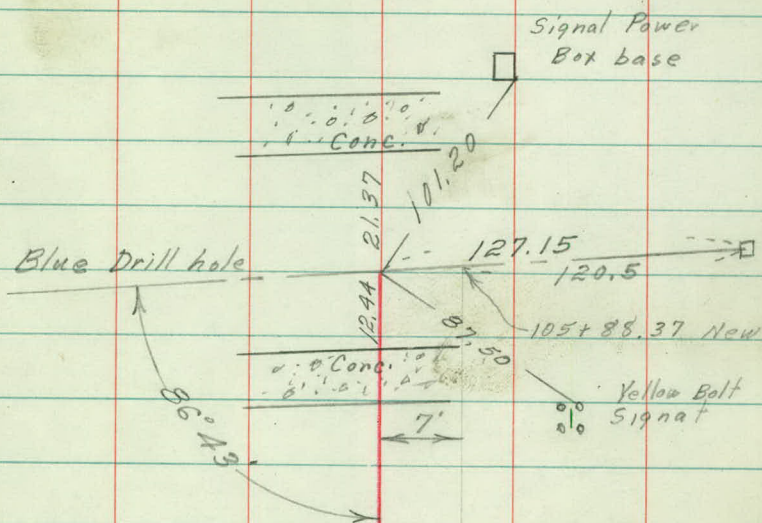
FK
WS
DS

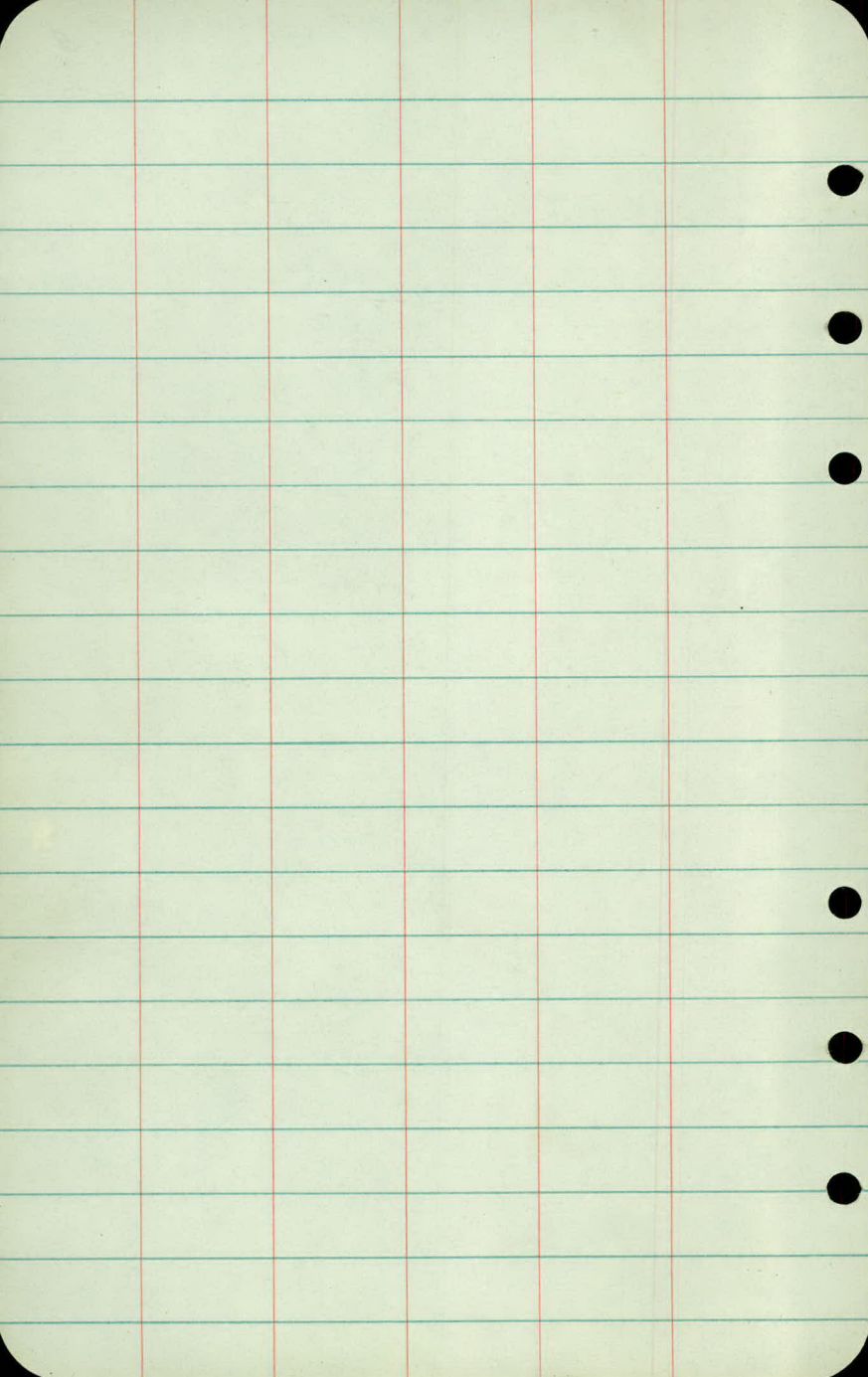
Jan. 8, 1963

£

5

A-5





Co. Rd. "C"

Cleveland to Snelling

Topography

183 Chr. Park Lot Lt 2 Rt
 33 L.E. 15' x 59' CM
 192 22
 174 L. Edge Fe MH
 Ent 140 100 163 17
 131 R tie Beg Ent X-Fe
 Fe 145 116 Fe 134 26
 125 PP N. End 15' x 59' CM
 25 134 22

59+00

185 Possible Ent
Lt

58+00 104 OP PP
 22 22

15' x 28' 50' P
 +63 24

147 P.I. Curb
 29
 +40 End Hedge
 49

147 End Curb
 38

57+00 134 Spruce 4 18
 47 11 11

New E 2' North

3" Pine SECOR Bldg
 +62 62 +59 108.5

2 Tree MH PP
 +48 100 +57 21.5 +53 28

3" Pine 3" Pine Hedge 3" Pine
 +46 52 +46 67 +46 71-107 +48 87

PP Sign
 +10 50 +26 88-97

56+00

11 11

9" Cott Scrub Oak Brush
 +94 53 +94 78-89

End Brush PP
 +25 56-77 +80 42

Beg Brush
 +51 42-94

4" Cott 7" Cott
 +13 52 +22 51

55+00

11 11

5" Cott
 +01 53

RG
WM
NIME
R. Behrens

Nov. 26, 1962
Cl. Cool

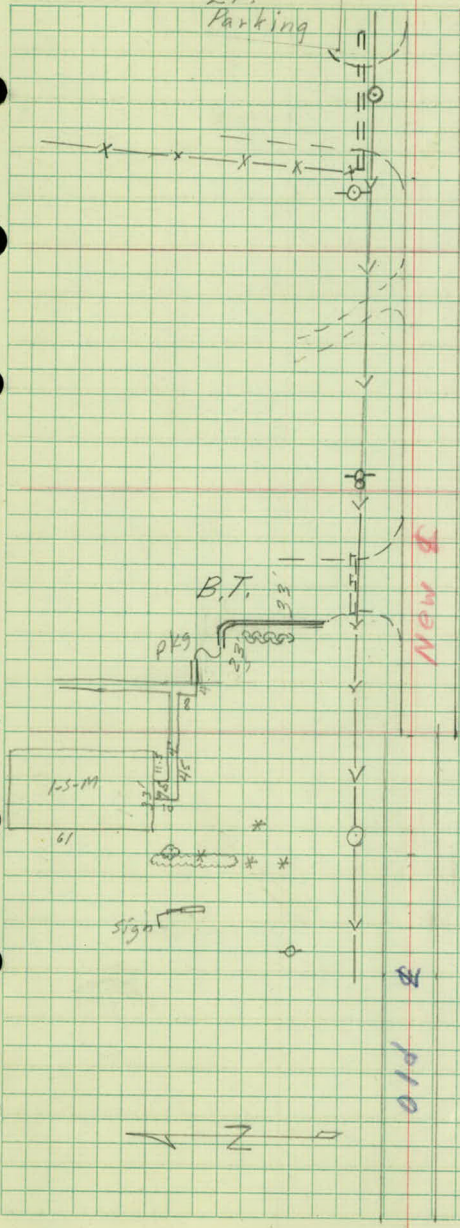
7

T-2

Lt.
Parking

Rt.

Sum. track



Suburban
Ver. Clinic

Top of line - 113

65

Lt

L

Rt

$$+77 \frac{Rt \cdot e}{B \cdot 69}$$

$$+17 \frac{PP}{20}$$

64

$$+143 \frac{Cor. Pk. Lot Fe}{21}$$

$$+144.5 \frac{Rt \cdot e}{B \cdot 69}$$

63

$$+103 \frac{MH}{15}$$

$$+164 \frac{PP}{21}$$

62

$$+145 \frac{Begin Pk. Lot Fe}{23}$$

61

$$+100 \frac{Pk. Lot}{24} +106 \frac{PP}{21}$$

60

T-3

24

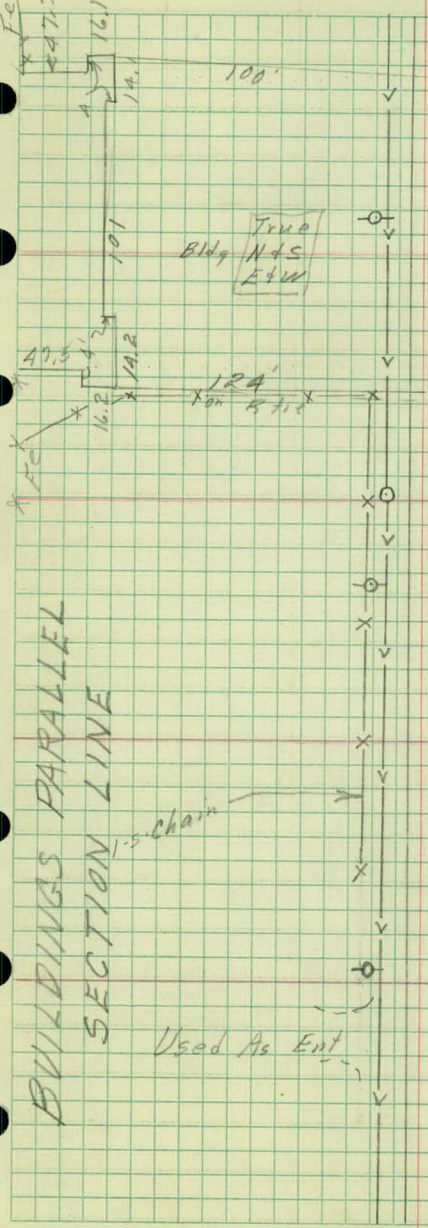
BUILDINGS PARALLEL SECTION LINE

1-5 chain

Used As Ent

Bldg True
N+S
E+W

Inv to Top = 11.66
Top 1.05 below old Φ sta 63



70

Lt

L

Rt

+95 Rtie Bldg
98+98 ER
75+150 B. Ent
Lt+150 BR
18

69

+128 PP
49+93 PP
19+179 N.E. 24" S.C.P. wide
74 30" High+174 S. End 18" S.C.P. 24" x 95" S.C.P.
87 41

53.5" at +63

+32 M.H
14

68

+135 PP
20

67

+95 ER
5+64 E.E. 15" CM
30+154 BR
45+23 E.R.
45+20 PP
65+11 Bench Mont.
28+17 M.H
15

W.E. 15" x 60.5" CM

+104
29

66

+99 Rtie Fe Cor.
Lt 1A.4+94 PP
21+95 B.R.
6

65

Mc

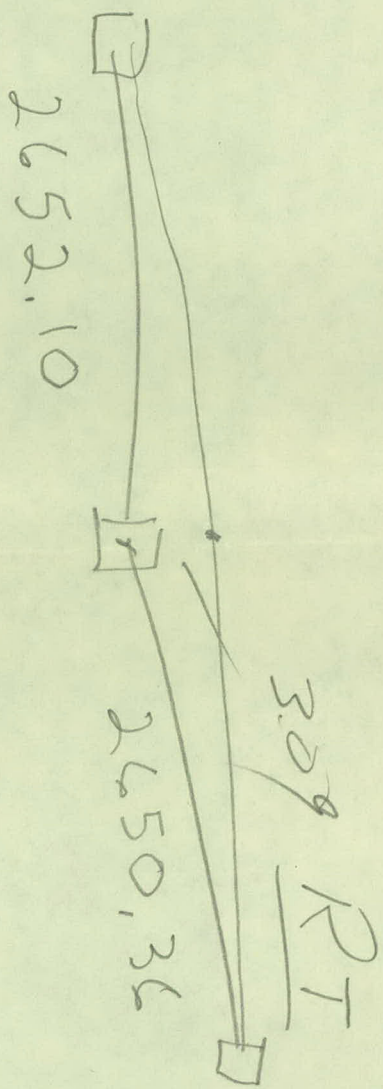
Highwood

Boxwood



.6

//////



Nov 27, 1962

8

30.5

60.7

ϕ

RT

7-4

~~Top to F.L. = 11.6~~

Inv to Top = 10.0

Prior Ave

Stub South
Inv. to Top = 10.26

141

Lt

E

Rt

+89 Cor Parking
32168 E.E 15" CM
22+28 W.E 15" CM 40.4 +84 PP
22 W.C. line 21.574 +13 E.E 15" CM 41 X 9.4
22 Headwall+65 R Tie Bldg
94.2+73 V.E. 15" X 40 CM
22 1.0 X 9.4 Headwall+42 PP +46 M.H.
22 1573 +22 E.E. 15" CM
24+100 E Tracks
93+95 Edge Ent.
32+68 8 E/m +84 E. 4 Walk W.E 15" CM X 37.5
38 78 184 24+23 S.S. Ent +67 S.S. Ent +22 E. 3 Walk
58 54 80+10 9 E/m +14 R. Tie Bldg
39 103.572 +100 Edge Ent +21.5 MH
56 13+90 E 2' Walk
85+91 PP
22+64 Tw 8" Coll
42+62 E 2' Walk
76+21 E 2' Walk
21.5+58 Edge Ent
2671 +105 E Ent + D. Ent
LT+71.5 MH
15.4+63 MH
40+65 PP
21.5+70 ER
18

70

E Track
96+11 RR
25

Nov. 27, 1962

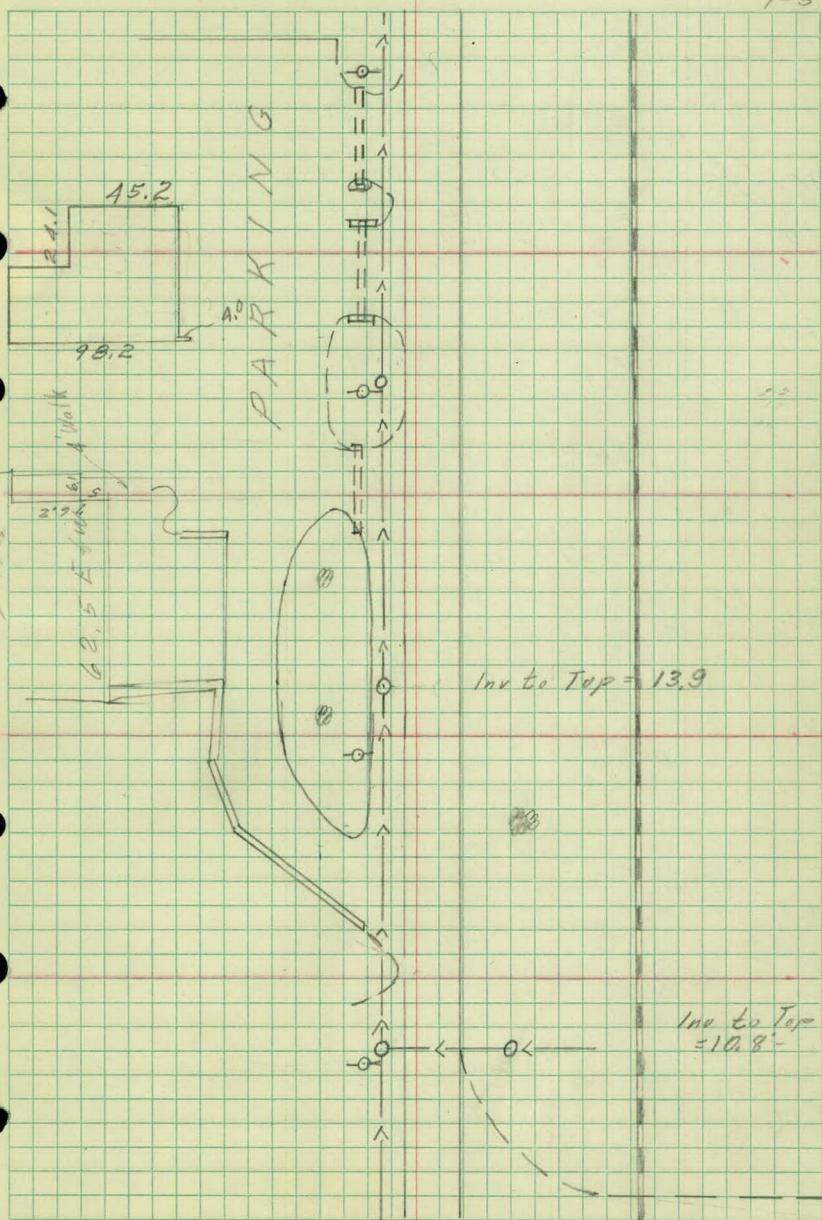
9

Lt

£

Rt

T-5



80
+74 $\frac{MH}{30}$

LT

2

RT

+74 $\frac{Bench\ Mont}{66}$ +80 Possible Gas Main X-ing
+80 $\frac{POR}{37}$

+61 $\frac{BR}{89}$

+23 $\frac{Arc Lt.}{26}$

+42 $\frac{E.R.}{85}$

+62 $\frac{BR}{84}$

+41 $\frac{E.R.}{68}$

+73 $\frac{MH}{41}$

+62 $\frac{2\ Tracks}{91}$

79

+13 $\frac{MH}{14.5}$

+20 $\frac{C.B.}{56}$

+26 $\frac{PP}{49}$

+97 $\frac{BR}{7}$

+96 $\frac{BR}{18}$

78

+67 $\frac{SW. Cor Bldg}{83}$

+66 $\frac{P.P.}{22}$

77

+94 $\frac{12'30\ C.M. Ent.}{25}$

+69 $\frac{Cor Bldg}{87.41}$

+54 $\frac{MH}{15.6}$

+45 $\frac{Cor Parking}{42}$

+31 $\frac{R.P. With Underground}{21.5}$

Leads

76

+08 $\frac{Ent 12' Culv. C.M.}{31}$

+66 $\frac{24" \times 94" SCP X-Drain}{40 - 54}$

+66 $\frac{S.D.}{56}$

75

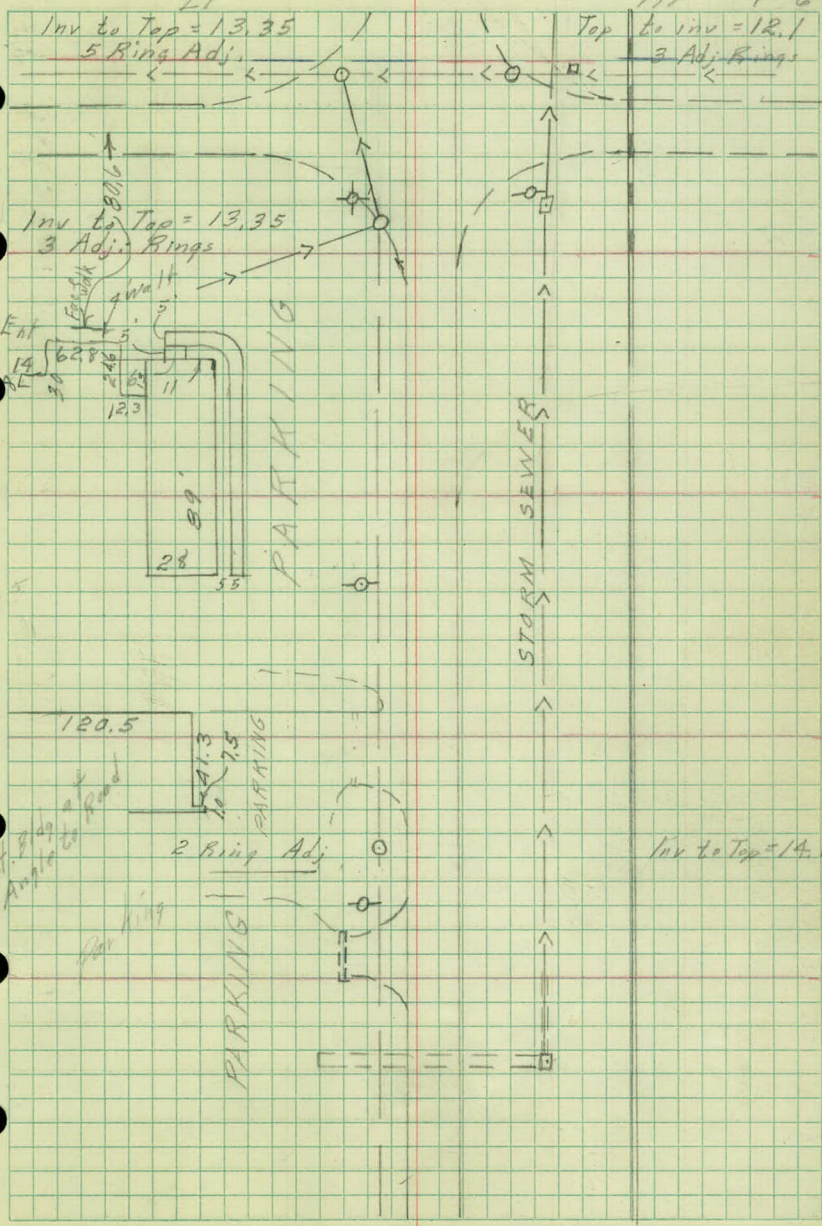
Nov. 27, 1962

10

Lt

Rt

T-6



85

LT

Z

RT

$$+79 \frac{51p}{39}$$

84

$$+59 \frac{EL}{72} \frac{CMCulv}{72}$$

$$+29 \frac{PP}{24}$$

83

82

$$+54 \frac{CB}{64}$$

$$+24 \frac{PP}{26}$$

81

$$+57 \frac{ER}{8}$$

$$+24 \frac{PP}{26}$$

$$+57 \frac{ER}{19}$$

$$+100 \frac{POR}{17}$$

80

FK
WM
MMC

Lt

± Nov. 27, 1962
Nov. 28 Rt

11

T-7

Swamp

about 40 Stumps
35 to 65' in Low Area

Inr.

to Top = 7.8±

36' x 42' x
48 Ft.

90

Lt.

¢

Rt

$$+38 \frac{MH}{31.5}$$

$$+79 \frac{PP}{21}$$

$$+58 \frac{BT}{13} \quad +73 \frac{EBT}{4}$$

$$+29 \frac{Cor BT}{68} \quad +36 \frac{B.T.}{34}$$

$$89 \quad +103 \frac{E.R.}{32} \quad +77$$

$$+76 \frac{BR}{4}$$

88

$$+100 \frac{Service Drive}{36-60}$$

$$+51 \frac{MH}{31} \quad \text{Top to inv} = 7.7'$$

5adr Rings

$$+39 \frac{PP}{23}$$

$$+16 \frac{NW Cor Bldg}{113}$$

 91 735
 92 735
 93

87

$$+100 \frac{Service Drive}{36-60}$$

$$+100 \frac{¢ Tracks}{87}$$

$$+99 \frac{R.Tic Bldg}{164}$$

$$+7A \frac{Edge Ent}{24}$$

$$+69 \frac{W.E. 5\frac{1}{2}' Walk}{120}$$

$$+26 \frac{W.E. 15" \times 60 CM}{23} \quad +21 \quad +83$$

86

$$+100 \frac{Edge Ent}{34}$$

$$+78 \frac{Edge Ent}{52}$$

$$+64 \frac{Edge Ent}{78}$$

$$+38 \frac{R.Tic Bldg.}{156}$$

$$+60 \frac{¢ Ent 15" \times 34 CM.}{RT} \quad 57$$

$$+31 \frac{W.E. 18" SCPX22'}{32} \quad +34 \frac{PP}{24}$$

85

$$+11 \frac{Stb}{40}$$

Nov. 25, 1962

12

T-8

Lt

±

Rt

4 Ring Adj.

1st to Top = 13.10

Parking

Bit Surface

107

80'

41.5

807

41.5

47.2

Bit Surface

Concrete

100

41

Parallel Sec. line

Bit Surface

NO Ent.

2

60.2

90.2

Parallel Sec. line

95

L +

E

Pt.

$$+ 80 \frac{PD}{18}$$

$$+ 79 \frac{BR}{5}$$

$$+ 24 \frac{30'' OAK}{99} + 26 \frac{20'' OAK}{58}$$

$$94 + 00 \frac{29'' OAK}{63}$$

$$+ 00 \frac{Tracks}{92}$$

$$+ 85 \frac{18'' OAK}{78} + 92 \frac{24'' OAK \cdot 12'' OAK}{47 \cdot 99 \frac{66}{66}}$$

$$+ 70 \frac{12'' OAK}{91} + 79 \frac{16'' OAK \cdot 12'' OAK}{79 \cdot 74 \frac{60}{60}}$$

$$+ 37 \frac{24'' OAK}{64} + 46 \frac{18'' OAK}{47}$$

$$+ 18 \frac{20'' OAK}{58}$$

$$93 + 13 \frac{22'' 14'' TW OAK \cdot PP}{85} + 15 \frac{PP}{18}$$

$$+ 00 \frac{Tracks}{91}$$

$$+ 95 \frac{12'' OAK}{92} + 96 \frac{14'' OAK}{100}$$

$$+ 76 \frac{16'' OAK}{97} + 84 \frac{24'' OAK}{45}$$

$$+ 79 \frac{M.H.}{30}$$

$$92 + 12 \frac{12'' OAK}{82}$$

$$+ 00 \frac{Tracks}{91}$$

$$+ 77 \frac{24'' OAK}{65} + 83 \frac{22'' OAK}{92}$$

$$+ 55 \frac{18'' OAK}{62} + 59 \frac{24'' OAK}{94}$$

$$+ 44 \frac{20'' OAK}{66} + 46 \frac{PP}{20}$$

$$+ 29 \frac{S+P}{51}$$

$$91 + 17 \frac{15'' OAK}{58}$$

$$+ 00 \frac{Tracks}{91} + 00 \frac{Tw 6'' Gott}{82}$$

$$+ 81 \frac{24'' OAK}{76}$$

90

$$+ 26 \frac{10'' OAK}{51}$$

WM
M Mc
RB

Nov. 28, 1962
Nov 29, 1962
R.T.

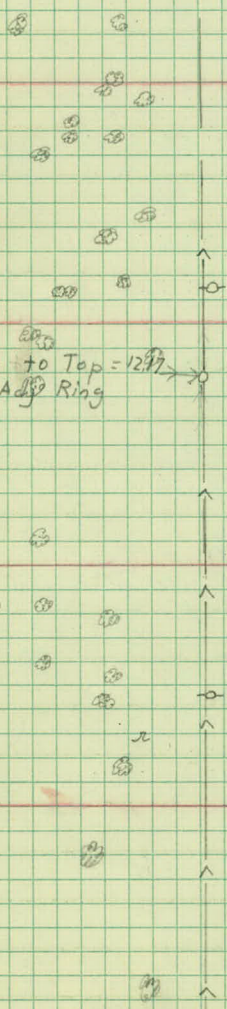
13
T-9

L +

E

Inv to Top = 1277
5 Adj Ring

Scattered Large Oaks



100

5 Adj Kings

Top to FIVE 16.1±

Top to Inv W 9.4'

+157 $\frac{MH}{25}$ +154 $\frac{MH}{40}$

99

+102 $\frac{TP}{16}$ +175 $\frac{GRP}{37}$ +183 $\frac{POR}{14}$ +174 $\frac{E.E.Curb}{29}$ +173 $\frac{GRP}{30}$ +112 $\frac{GRP}{47}$ +113 $\frac{GRP}{40}$ +114 $\frac{GRP}{31}$ +108 $\frac{E.Curb}{59}$ +104 $\frac{RC}{64}$

98

+113 $\frac{W.E 18 \times 60' CM}{29}$ +190 $\frac{R.Tie}{Curb}$ +186 $\frac{Cori.Curb}{64}$ +183 $\frac{BR}{4}$ +182 $\frac{5" C.H.}{72}$ +148 $\frac{5" C.H.}{68}$

97

+197 $\frac{TP}{17}$ +198 $\frac{4" C.H.}{69}$ +197 $\frac{TW 4" C.H.}{70}$ +156 $\frac{End Curb}{68}$ +160 $\frac{R.Tie}{Curb}$ +156 $\frac{Cori Parking}{38}$ +118 $\frac{MH}{31}$

96

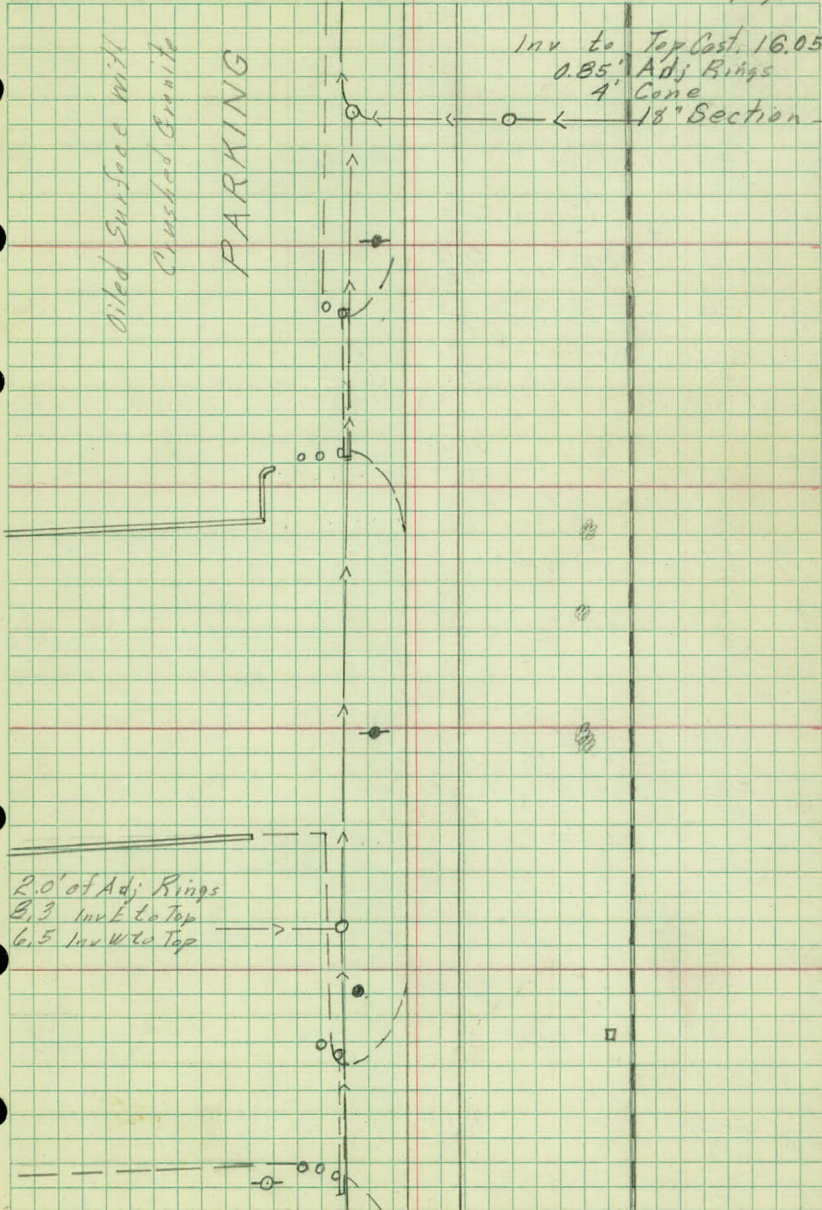
+171 $\frac{POR}{14}$ +191 $\frac{Gas Valve}{26}$ +192 $\frac{ER}{4}$ +173 $\frac{Pull Box 2 \times 2 \times 3}{81'}$ +165 $\frac{GRP}{33}$ +168 $\frac{ER}{35}$ +169 $\frac{GRP}{40}$ +119 $\frac{GRP}{18}$ +166 $\frac{EE Curb}{31}$ +162 $\frac{POR}{25}$ +111 $\frac{PP}{62}$ +115 $\frac{GRP}{33}$ +118 $\frac{GRP+ER}{41}$

95

+107 $\frac{W.E 18 \times 60' CM}{32}$

Oiled Surface with
Crushed Granite
PARKING

Inv to Top Cast. 16.05
0.85' Adj Rings
4' Cone
18" Section



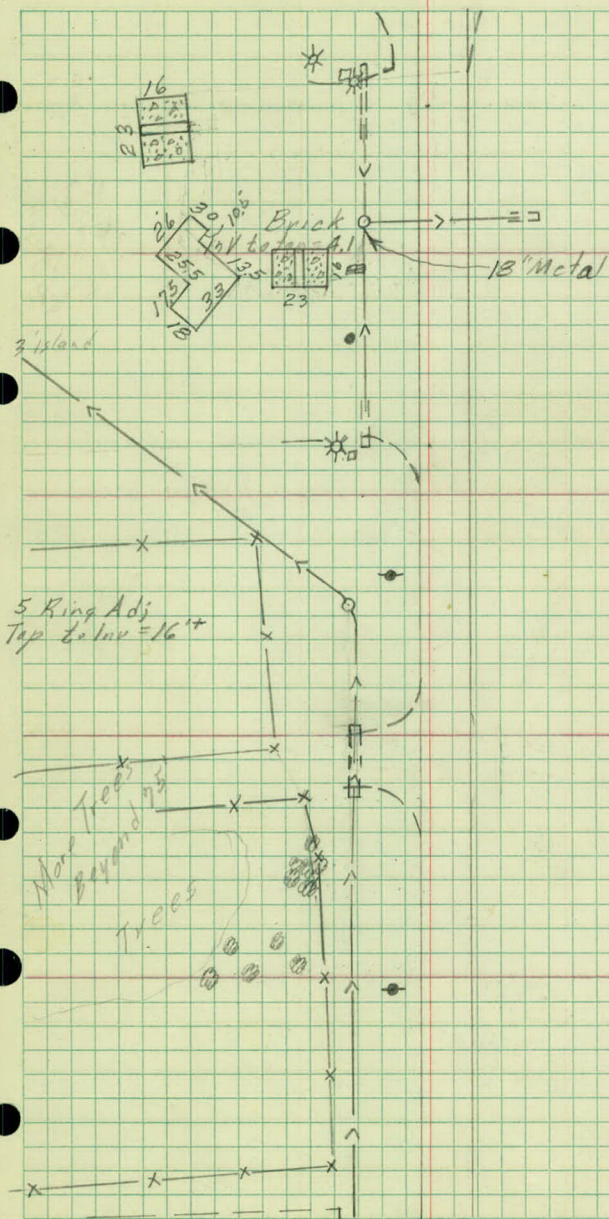
105

Long 1/4

+78 $\frac{EE 15 "SCP}{27}$ +77 $\frac{Cor B.T.}{74}$
 +73 $\frac{Tell B. 1/4}{34}$ +72 $\frac{Light}{31}$ +75 $\frac{BR}{18}$
 +53 $\frac{S.E. Pampalsland}{98}$ +61 $\frac{R Tie}{Island}$ +15 $\frac{S.E. 24 "SCP}{46}$
 104 +103 $\frac{Cor Conc}{42-65}$ +13 $\frac{SD}{27}$
 +86 $\frac{E Island}{54}$ +94 $\frac{Sign}{28}$ +94 $\frac{Sign}{32}$
 +90 $\frac{Cor. Sta}{79}$ +86 $\frac{Cor Conc}{42}$ +86 $\frac{Cor Conc}{65}$
 +25 $\frac{Edge Ent}{26}$ +65 $\frac{G. Filler Cop}{33}$ +20 $\frac{R Tie}{serv sta}$
 +20 $\frac{W.E. 15 "SCP}{27}$ +105 $\frac{B. Ent}{4}$
 103 +116 $\frac{2x2 Sign}{32}$ +20 $\frac{Light}{39}$
 +82 $\frac{Fe Cor}{73}$
 +67 $\frac{T.P.}{16}$ Goes Underground
 +54 $\frac{M.H.}{34}$

102
 +49 $\frac{7" Ash}{47}$ +50 $\frac{Lin Se}{47}$ +53 $\frac{6" Ash}{47}$
 +41 $\frac{Eln}{57}$ +45 $\frac{5" Eln}{51}$ +45 $\frac{12" Eln}{57}$ +91 $\frac{24'x31' CM Ent}{30' 2\frac{1}{2}'}$
 +16 $\frac{10" Eln}{66}$ +45 $\frac{14" Eln}{83}$ +37 $\frac{10" Eln}{50}$ +81 $\frac{R Tie}{Fe Lt.}$
 +06 $\frac{Row Trees}{56}$ +92 $\frac{Fe Cor}{25}$ +77 $\frac{Fe Cor}{54}$
 101 +93 $\frac{Fe Cor}{66}$ +00 $\frac{Fe}{44}$
 +95 $\frac{TP}{16}$

+22 $\frac{Fe Cor}{41}$ +29 $\frac{R Tie}{Fe}$
 100 +04 $\frac{Cor Parking Lot}{37}$



Lt

L

Rt

R. D. G.
 12-11-62

106

Possible Gas Main

57

+22	WE 15" SCP 69	+37	ER 75	+23	Arc Lt 60	+35	SD 53				
		+51	E Conc R 51	+40	Conc 22	+54	ER 75	+40	Conc 30		
		+20	FOR 27			+21	GRP 30	+33	GRP 37	+44	GRP 49
				+03	B. Conc R 4 18			+16	WE 24" SCP 53		
105											

105

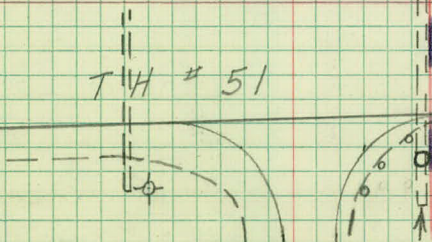
Lt

 $\pm$

Rt

T-12

T/H # 51



92 + 79

KP
US
RB
DS
Richard Boss

26 Nov. 1962

17

18

Co. RDC
CLEVELAND TO SNELLING

BENCH LEVELS

2 pages (B)

STA	+	-	ELEV.
BM	8.64	923.05	914.41
"	5.80	928.47	0.38 922.67
"	5.46	933.58	0.35 928.12
"	4.10	932.40	5.28 928.30
"	4.43	930.68	6.15 926.25
"	3.96	929.75	4.89 925.79
"	2.62	928.51	3.86 925.89
"	2.70	928.07 928.06	3.15 925.36 925.37
"	12.44	931.47 931.46	919.03 919.02
"	0.90	932.26 932.25	931.36 931.35
"	1.36	928.79 928.78	927.43 927.42
"	0.31	923.47 923.46	923.16 923.15
"	2.55	921.22	4.80 918.67
"	5.90	920.10	7.02 914.20
"			2.35 917.75

26 Nov. 1962

18

LT

±

RT

2.B

TOP MONT AT CLEVELAND

S.W. COR ENTRANCE SLAB (VETERINARY CLINIC)

SPIKE IN 30" OAK 120± RT STA 59+50

S.W. COR ENTRANCE SLAB (INDIAN HEAD TRUCK LINE)

SW COR ENTRANCE SIDEWALK (ORRICE BROWN TRAILERS)

N.E. COR HEADWALL IN FRONT OF (ACTON CONST. CO)

TOP S.W. COR DOOR-SILL (BARBER SHOP MACK HOTEL)

TOP MONT. AT NEW BRIGHTON RD. (Fairview)

SPIKE IN PP 33.0' LT STA 83+30

S.W. COR SLAB (ENTRANCE) (Blue truck line)

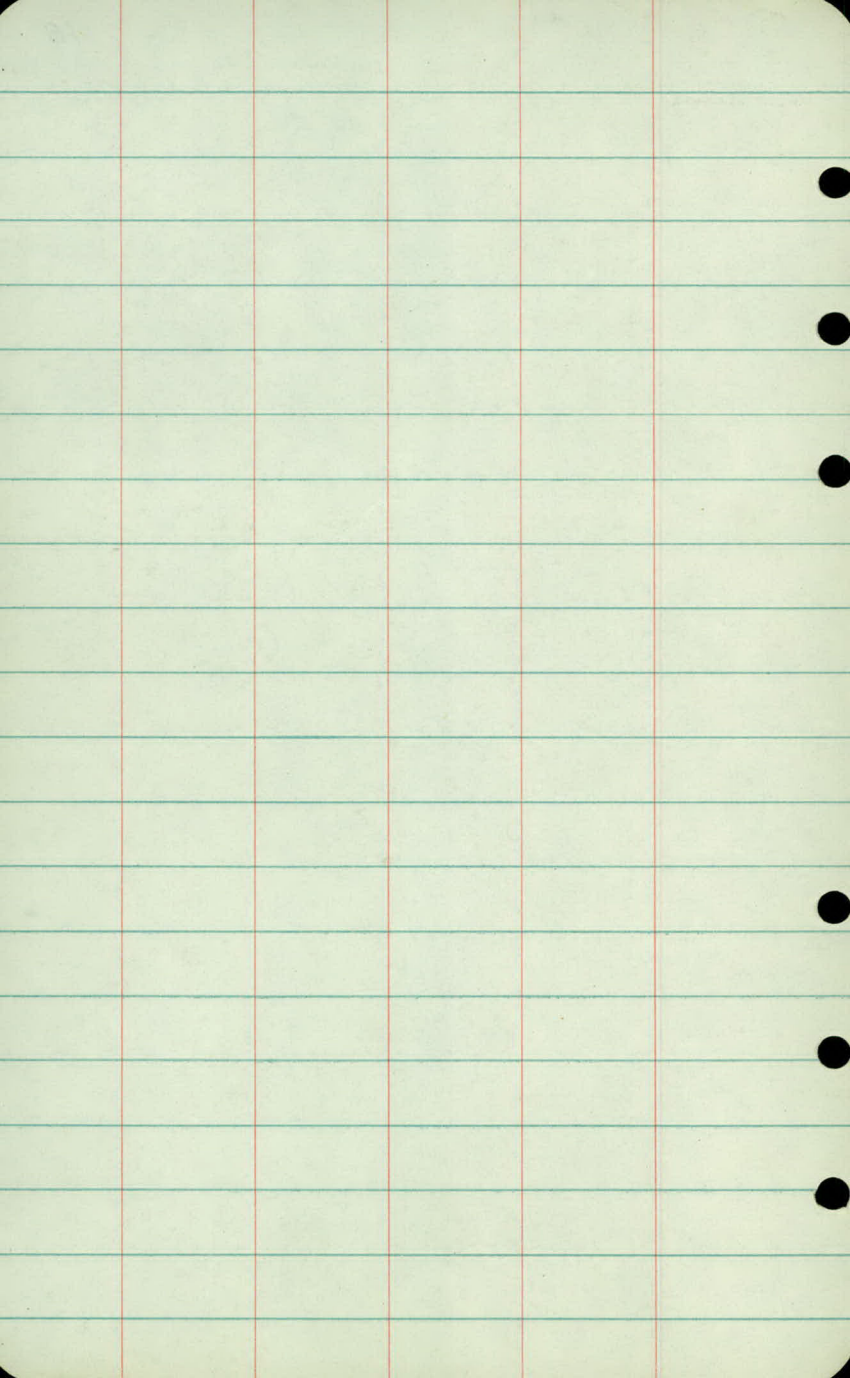
SPIKE IN PP 33' LT STA 91+50

SPIKE IN 36" TWIN OAK 94+30 100' LT

S.E. COR CURB 90' LT STA 96+50

SPIKE IN 10" MAPLE 75± LT STA 101+57

S.W. CORNER-BOLT of LITE STD 50' LT STA 104+70



KP FS
JS WS
RB Richard Bass
DS

27 Nov. 1962
SUNNY 40°

19

1

CO. RD C

CLEVELAND TO SNELLING

X-Sections

58 pages

STA	+	π	-	ELEV.
BM	3.43	926.10		922.67

56400

✓

✓

+50

✓

✓

27 Nov. 1962

20

Lt

E

Rt

2

S.W. COR. ENTRANCE SLAB (VETERINARY CLINIC)

19.0	17.7	19.2	19.89	19.91	19.98	19.75	19.6
7.1	8.4	6.9	6.21	6.19	6.12	6.35	6.5
37	22	13	4		7	18	28

19.8	20.2
6.3	5.9
52	65

13.8	14.3	14.4	15.6
12.3	11.8	11.7	10.5
118	100	80	45

11.6	11.4	21.7
14.5	14.7	4.4
125	129	146

DITCH

18.8	18.8	20.2	20.72	20.84	20.97	20.84	20.6
7.3	7.3	5.9	5.38	5.26	5.13	5.24	5.5
28	23	14	4		7	18	28

21.1	21.9	22.1
5.0	4.2	4.0
44	55	65

16.6	17.1	16.6	15.8
9.5	9.0	9.5	10.3
100	82	57	54

16.1	14.8	14.9	12.3
10.0	11.3	11.2	3.6
111	117	120	138

DITCH

STA	+	π	-	ELEV
		926.10		
56+56			5.66	920.44

57+00

✓

✓

+45 = SHOULDER LT

✓

27 Nov 1962 21

LT

L

RT

3

TOP MH 15.0' LT

Flows Eyo W

FL TO TOP CASTING 16.0

1 ADJUSTMENT RING

1 5.0 PRECAST ECCENTRIC CONE

CASTING = 1.0

22.2	19.8	20.9	21.58	21.74	21.91	21.88	21.7
3.9	6.3	5.2	4.52	4.36	4.19	4.22	4.4
49	25	15	4		7	18	28

12.5
3.6
65

17.8 19.3 18.3 18.3
8.3 6.8 7.8 7.8
88 63 52 48
DITCH

17.9 16.5 23.0
8.2 9.6 3.1
100 108-111 128
DITCH

21.0	21.2	21.9	22.0	22.39	22.54	22.74	22.89	22.7	18.8
5.1	4.9	4.2	4.1	3.71	3.56	3.36	3.21	3.4	7.3
30	24	21	13	4		7	18	29	54

22.0 22.5
4.1 3.6
39 65

23.8 19.7 21.3 21.5
2.3 6.4 4.8 4.6
118 98-102 93 67
DITCH

STA + π - ELEV

926.10

57+47 = GUTTER LT (BT)

✓

+62 = ~~E~~ BT DRIVEWAY LT

✓

+79

5.38 920.72

✓

27 NOV. 1962

22

Lt

E

Rt

4

20.24 22.0 22.41 22.57

5.86 4.1 3.69 3.53 SAME AS +45 ON RT.

24 21 4
FL 12" SCP

21.6 22.12 21.8 22.58

4.5 3.98 4.3 3.52

39 39 65 65

GUTTER CURB GUTTER CURB

21.9 21.9 22.4 22.70 22.86 23.04 23.27 23.0

4.2 4.2 3.7 3.40 3.24 3.06 2.83 3.1

65 52 25 4 7 18 30

23.9 20.5 21.2 22.0 19.2

2.2 5.6 4.9 4.1 6.9

115 96-99 92 70 54

DITCH

FL E. END 12" SCP 25' 0" LT (29' 0" CULVERT)

STA	+	π	-	ELEV
-----	---	-------	---	------

		926.10		
--	--	--------	--	--

+82	=			
-----	---	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

58+00				
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✓				
---	--	--	--	--

✓				
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TP	8.50	932.55	2.05	924.05
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27 Nov. 1962 23
5

Lt

£

Rt

5

21.8	21.4	22.3	23.05	23.23	23.42	23.65	23.4
4.3	4.7	3.8	3.05	2.87	2.68	2.45	2.7
31	25	18	4		7	18	29

21.7 21.8
4.4 4.3
50 65

21.7 22.5 22.2 19.5
4.4 3.6 3.9 6.6
93-95 89 68 52
DITCH

23.5 24.4
2.6 1.7
100 113

23.6	21.9	22.7	23.36	23.54	23.79	23.97	23.7	20.2
2.5	4.2	3.4	2.74	2.56	2.31	2.13	2.4	5.9
46	27	24	4		7	18	29	53

23.9
2.2
65

23.7 21.7 22.5 22.5
2.4 4.4 3.6 3.6
100 90-92 86 71
DITCH

24.4
1.7
111

EDGE CONC.

STA

+

π

-

ELEV.

932.55

58+50

✓

59+00

✓

+32

8.93 923.62

27 Nov. 1962

24
6

LT

£

RT

25.2	23.0	24.0	24.20	24.40	24.60	24.94	24.7	20.6
7.4	9.6	8.6	8.35	8.15	7.91	7.61	7.9	12.0
48	27	12	4		7	18	29	56

25.1
75
65

25.0 21.1 22.2
7.6 11.5 10.4
100 85-87 80
DITCH

25.8	23.7	24.6	25.01	25.21	25.46	25.85	25.8	22.2
6.8	8.9	8.0	7.54	7.34	7.09	6.70	6.8	10.4
50	28	11	4		7	18	29	49

25.8
6.8
65

25.5 24.7 22.4 22.1
7.1 7.9 10.2 10.5
97 86 77 70

FL W. END 15" CM 22.0 LT

STA	+	π	-	ELEV
		932.55		

59+39 = SHOULDER LT

✓

+42 = GUTTER LT (BT)

✓

+60 = ~~E~~ BT ROAD LT

✓

27 Nov. 1962

25

Lt

E

RT

7

26.1	25.6	25.5	25.6	25.88	26.14	26.48	26.6
6.5	7.1	7.1	6.89	6.67	6.41	6.07	6.0
27	22	12	4		7	18	29

26.0	26.0
6.6	6.6
45	65

26.0	21.4	21.8	22.9
6.6	11.2	10.8	9.7
93	70-73	66	47

DITCH

24.6	24.7	25.2	25.6	25.74	25.95
8.0	7.9	7.4	7.0	6.81	6.60
65	52	38	12	4	

SAME AS +39 ON RT

25.9	26.0	26.1	26.08	26.26	26.48	26.82	26.9	33.7
6.7	6.6	6.5	6.47	6.29	6.07	5.73	5.7	8.9
65	38	12	4		7	18	29	45

26.2	21.4	21.8
6.4	11.2	10.8
90	68-70	64

DITCH

STA + π - ELEV.

932.55

59+78 = GUTTER LT (BT)

✓

+93

7.89 924.66

✓

60+00

✓

LT

27 Nov. 1962

L

RT

26

8

25.6	25.9	26.2	26.32	26.53	26.75	27.10	27.2
7.0	6.7	6.4	6.23	6.02	5.80	5.45	5.4
65	41	13	4		7	18	29

26.6	20.8	22.0	23.7
6.0	11.8	10.6	8.9
89	67-69	63	46
DITCH			

FL E. END 15" CM 22.0 LT

26.2	25.4	26.3	26.65	26.85	27.09	27.42	27.5	23.6
6.4	7.2	6.3	5.90	5.70	5.46	5.13	5.1	9.0
38	20-21	12	4		7	18	29	48
DITCH								

26.3
6.3
65

26.7	21.2	22.3
5.9	11.4	10.3
86	67-70	63
DITCH		

STA	+	T	-	Elev.
-----	---	---	---	-------

		932.55		
--	--	--------	--	--

60+50				
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✓				
---	--	--	--	--

61+00				
-------	--	--	--	--

✓				
---	--	--	--	--

61+50				
-------	--	--	--	--

✓				
---	--	--	--	--

BM				
----	--	--	--	--

5.12				
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933.24				
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4.43				
------	--	--	--	--

928.12				
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928.12				
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27 Nov. 1962

27

LT

E

RT

9

26.8	26.2	27.1	27.24	27.43	27.67	28.01	28.0
5.8	6.4	5.5	5.31	5.12	4.88	4.54	4.6
26	19-20	12	4		7	18	29

DITCH

27.1	27.2
5.5	5.4
43	65

27.2	21.6	22.7	23.7
5.4	11.0	9.9	8.9
83	64-67	61	47

DITCH

26.7	27.3	27.4	27.74	27.97	28.18	28.47	28.5
5.9	5.3	5.2	4.81	4.58	4.37	4.08	4.1
24-25	20	12	4		7	18	29

DITCH

27.3	27.6	27.4
5.3	5.0	5.2
32	46	65

27.5	22.1	23.0	24.8
5.1	10.5	9.6	7.8
80	63-67	59	44

DITCH

27.6	26.9	27.8	27.9	28.23	28.37	28.57	28.79	28.5	24.8
5.0	5.7	4.8	4.7	4.32	4.18	3.98	3.76	4.1	7.8
26	24-25	22	12	4		7	18	29	46

DITCH

27.8	27.6
4.8	5.0
50	65

27.8	22.1	23.6
4.8	10.5	9.0
79	62-65	57

DITCH

SPIKE IN 30" OAK 120' RT 59+50

STA.	+	π	-	ELEV
		933.24		
BM			4.94	928.30 (928.30)
102+00				
✓				
+50				
✓				
103+00				
✓				

27 Nov. 1962

28

LT

E

RT

10

S.W. COR ENTRANCE SLAB (INDIAN HEAD TRACK LINE)

27.4	27.7	28.8	28.6	28.7	28.9	29.00	28.8
5.8	5.5	4.4	4.64	4.50	4.28	4.24	4.4
22-23	20	15	4		7	18	28

DITCH

27.9	28.0	28.0
5.3	5.2	5.2
27	47	65

28.5	22.6	24.0	25.0
4.7	10.6	9.2	8.2
69	60-64	54	45

27.6	27.9	28.7	28.9	29.00	29.10	29.02	28.7	25.1
5.6	5.3	4.5	4.32	4.24	4.14	4.22	4.5	8.1
22-23	19	14	4		7	18	29	46

DITCH

28.0	28.1	28.1
5.2	5.1	5.1
26	47	65

28.2	23.4	24.4
5.0	9.8	8.8
80	58-61	53

DITCH

28.1	27.7	28.6	28.99	29.06	29.12	28.95	28.8	25.4
5.1	5.5	4.6	4.25	4.18	4.12	4.29	4.4	7.8
25	20-21	15	4		7	18	29	48

DITCH

28.1	28.2
5.1	5.0
47	65

28.7	23.7	25.1
4.5	9.5	8.1
80	60-63	53

DITCH

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		933.24		
--	--	--------	--	--

63+50				
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✓				
---	--	--	--	--

✓				
---	--	--	--	--

64+00				
-------	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

27 Nov. 1962

29

Lt

Lt

Lt

11

28.3	28.1	28.0	28.6	28.95	29.01	29.13	28.91	28.6
4.9	5.1	5.2	4.6	4.29	4.23	4.11	4.33	4.6
65	47	31	20	4		7	18	29

23.7	24.4	25.5	26.6
9.5	8.8	7.7	6.6
61-64	57	49	43

DITCH

28.7

4.5

80

27.7	27.3	28.4	28.88	28.92	29.00	28.86	28.5
5.5	5.9	4.8	4.36	4.32	4.24	4.38	4.7
47	30	19	4		7	18	29

27.9

28.30

5.3

4.94

65

114

BLDG

23.4

24.4

24.5

25.9

9.8

8.8

8.7

7.3

65-68

57

50

38

DITCH

28.1

5.1

81

STA	+	π	-	ELEV.
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		933.24		
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64+50				
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✓				
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✓				
---	--	--	--	--

65+00				
-------	--	--	--	--

✓				
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TP	4.21	932.63	4.82	928.42
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27 NOV. 1962

30

LT

E

RT

12

27.3	27.0	28.1	28.76	28.82	28.89	28.74	28.4
5.9	6.2	5.1	4.48	4.42	4.35	4.50	4.8
47	29	16	4		7	18	29

27.7

5.5

65

23.7	24.1	25.2	25.7
9.5	9.1	8.0	7.5
59	50	43	40

22.7

27.9

10.5

5.3

63-66

81

DITCH

27.0	26.6	27.5	28.42	28.48	28.53	28.40	28.2	25.6
6.2	6.6	5.7	4.82	4.76	4.71	4.84	5.0	7.6
47	29	16	4		7	18	29	47

27.5

5.7

65

27.9	23.4	24.0
5.3	9.8	9.2
81	64-67	56

DITCH

EDGE CONC.

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		932.63		
--	--	--------	--	--

65+50				
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✓				
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✓				
---	--	--	--	--

66+00				
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✓				
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+02				
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27 Nov. 1962

31

LT

E

RT

13

26.9	26.0	27.5	28.41	28.46	28.47	28.37	28.1
5.7	6.6	5.1	4.22	4.18	4.16	4.26	4.5
51	30	15	4		7	18	29

27.3
5.3
65

23.9 24.8 24.7
8.7 7.8 7.9
64-67 58 46
DITCH

27.9
4.7
79

24.70	26.9	27.6	28.32	28.38	28.39	28.30	28.0
7.93	5.7	5.0	4.31	4.25	4.24	4.33	4.6
29	23	15	4		7	18	29

FLW END
15" CM

27.1 27.3 27.1
5.5 5.3 5.5
34 47 65

28.6 24.9 23.9 25.4
4.0 7.7 8.7 7.2
81 68 51 44

27.1	27.4	27.3	27.5	28.32	28.37
5.5	5.2	5.3	5.1	4.31	4.26
65	47	28	15	4	

SAME AS 6400 ON RT

STA	+	π	-	ELEV.
-----	---	---	---	-------

		932.63		
--	--	--------	--	--

66+17 = SHOULDER LT				
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✓				
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66+17		4.58	928.05	
-------	--	------	--------	--

66+20 = GUTTER LT (RT)				
------------------------	--	--	--	--

✓				
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LT

£

27 Nov. 1962

32

RT

14

27.7

28.05

28.31

28.34

28.36

28.24

28.0 25

4.9

4.58

4.32

4.29

4.27

4.39

4.6 7.2

23

15

4

7

18

29 43

TOP MH

27.3

27.6

5.3

5.0

47

65

28.0

24.6

24.0

4.6

8.1

8.6

80

70

50

TOP MH 15.0 LT

Flows ^{FROM} N TO W

FL TO TOP OF CASTING 10.29

1 ADJUSTING RING

1 5.0 ECCENTRIC CONE (PRECAST)

CASTING = 1.0

27.1

27.4

27.9

28.31

28.34

5.5

5.2

4.7

4.32

4.29

SAME AS +17 ON RT.

51

35

16

4

26.8

5.8

68

STA + π - ELEV

932.43

66+36 = ~~E~~ BT RD LT (PRIOR AVE)

✓

+50 = GUTTER LT (BT)

✓

✓

+54 = SHOULDER LT

27 NOV. 1962

33

LT

E

RT

15

27.3	27.5	28.1	28.30	28.34	28.33	28.16	27.9
5.3	5.1	4.5	4.33	4.29	4.30	4.47	4.7
49	32	13	4		7	18	29

27.0	26.6	26.1	25.7	28.2	24.3	23.7	24.5
5.6	6.0	6.5	6.9	4.4	8.3	8.9	8.1
65	100	150	200	83	70	53	48

27.0	27.5	27.7	28.26	28.31	28.32	28.17	27.9
5.6	5.1	4.9	4.37	4.32	4.31	4.46	4.7
47	27	13	4		7	18	28

26.8
5.8
65

24.3	23.8	24.4
8.3	8.8	8.2
70	61	46

28.2
4.4
81

27.4	27.4	26.9	27.5	28.24	28.30
5.2	5.2	5.7	5.1	4.39	4.33
65	47	27	14	4	

SAME AS +50 ON RT.

STA

+

π

-

ELEV.

932.63

66+66

✓

67+00

✓

+50

✓

27 Nov. 1962

34

Lt

£

Rt

16

24.58	26.6	27.4	28.23	28.28	28.30	28.15	27.7
8.05	6.0	5.2	4.40	4.35	4.33	4.48	4.9
30	23	12	4		7	18	29

FLE. END
15" CM

27.4	27.4	27.3		28.2	23.6	23.8
5.2	5.2	5.3		4.4	9.0	8.8
40	52	65		80	65	47

25.8	23.7	27.9	28.13	28.15	28.20	28.08	27.5
6.8	8.9	4.7	4.50	4.48	4.43	4.55	5.1
43	32	14	4		7	18	29

→ 25.6
7.0
65

28.2 23.2 24.0
4.4 9.4 8.6
81 64 45

22.2	23.0	27.3	27.96	28.00	28.05	27.95	27.5
10.4	9.6	5.3	4.67	4.63	4.58	4.68	5.1
65	42	14	4		7	18	29

28.0 22.8 23.2
4.6 9.8 9.4
82 66 46

STA

+

T

-

ELEV.

932.63

68+00

✓

+31

5.64 926.99

68+50

✓

27 Nov. 1962

35

LT

/

RT

17

20.6	21.0	21.3	21.75	21.81	21.88	21.72	21.4
12.0	11.6	5.3	4.88	4.82	4.75	4.91	5.2
65	44	13	4		7	18	29

21.3	22.4	22.7
5.3	10.2	9.9
82	71	49

TOP MH 14.0 LT

FLOWS FROM S?
WEST TO EAST

1 ADJUSTMENT RING

1 5.0 ECCENTRIC CONE (PRECAST)

FL TO TOP OF CASTING 10.09

CASTING = 1.0

21.73	21.74	21.44	21.0
4.90	4.89	5.19	5.6
	7	18	28

21.1	19.8	21.0	22.7
5.5	12.8	11.6	9.9
84	69	61	47

STA	+	π	-	ELEV
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		932.63		
--	--	--------	--	--

68+62			12.99	919.64
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+65			13.57	919.06
-----	--	--	-------	--------

+65			13.62	919.01
-----	--	--	-------	--------

68+79			12.24	920.39
-------	--	--	-------	--------

BM			4.30	928.33 (928.30)
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BM	5.63	931.88	6.37	926.26 (926.25)
----	------	--------	------	-----------------

68+50				
-------	--	--	--	--

✓				
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69+00				
-------	--	--	--	--

LT

27 NOV. 1962

E

RT

36

18

FL S. END 24" SCP 53.0 RT

● FL N. END 24" SCP 41.0 LT

FL S. END 18" SCP 87.0 LT

● FL N. END 24" SCP 74.0 RT

S.W. COR ENTRANCE SLAB (INDIAN HEAD TRUCK LINE)

S.W. COR ENTRANCE SIDEWALK (BROWN TRAILERS)

20.4	21.6	26.9	27.69	27.74
11.5	10.3	5.0	4.19	4.14
51	37	13	4	

70.7
11.2
65

22.6	23.1	23.9	26.9	27.68	27.71	27.65	27.33	26.6	22.6
9.3	8.8	8.0	5.0	4.20	4.17	4.23	4.55	5.3	9.3
65	51	31	13	4		7	18	29	47

STA.	+	π	-	ELEV.
------	---	-------	---	-------

		931.88		
--	--	--------	--	--

69+00				
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69+50				
-------	--	--	--	--

✓				
---	--	--	--	--

+90				
-----	--	--	--	--

✓				
---	--	--	--	--

+94				
-----	--	--	--	--

KP
FS
RB

Lt

28 Nov. 1962 37
Cloudy 40° ET 19

P. Boss

✓
31.2 19.6 26.6
10.7 12.3 5.3
62 72 86

25.4 25.7 25.3 26.6 27.6 27.6 27.5 27.1 26.7
6.5 6.2 6.6 5.3 4.22 4.22 4.32 4.72 5.2
65 47 26 15 4 7 18 29

✓
26.6 20.5 21.8 22.8
5.3 11.4 10.1 9.1
85 71 61 46

25.8 25.8 25.8 26.8 27.53 27.52 27.44 27.19 27.2
6.1 6.1 6.1 5.1 4.35 4.36 4.44 4.69 4.7
65 47 26 13 4 7 18 31

✓
27.9 22.7 22.7 26.7
4.0 9.2 9.2 5.2
87 78 66 51

SAME AS + 90 ON LT
27.52 27.43 27.17 27.3 26.8
4.36 4.45 4.71 4.6 5.1
7 18 31 57

✓
27.04 27.0 26.8
4.84 4.9 5.1
93 88 78
RTDACK

$70 + 00$

✓

+13



+17

✓

28 NOV. 1962

LT

E

RT

38

20

26.1	26.0	26.0	27.49	27.49	27.42	27.17	27.32
5.8	5.9	5.9	4.39	4.39	4.46	4.71	4.64
65	47	27	4		7	18	36 53

26.2

5.7

95

BLDG

27.07

27.0

4.81

4.9

93

68

TOP N. RR TRACK

26.1	26.2	26.4	26.6	27.36	27.47	27.42	27.12	27.3
5.8	5.7	5.5	5.3	4.52	4.41	4.46	4.76	4.6
65	47	34	21	4		7	18	36

26.16

5.72

82

TOP S. END
SIDEWALK

27.03

26.8 26.7 26.9

4.85

5.1 5.2 5.0

93

83 68 53

TOP RR TRACK

SAME AS +13 ON LT.

27.45	27.41	27.11	27.2	26.6
4.43	4.47	4.77	4.7	5.3
7	18	39	54	

26.6 23.8 24.0

5.3

8.1

7.9

85

78

66

STA	+	π	-	ELEV
-----	---	-------	---	------

		931.88		
--	--	--------	--	--

70+50				
-------	--	--	--	--

✓				
---	--	--	--	--

+71				
-----	--	--	--	--

	5.05	926.73		
--	------	--------	--	--

71+00				
-------	--	--	--	--

✓				
---	--	--	--	--

28 Nov. 1962

39

LT

♀

RT

21

25.8	25.9	25.9	26.3	27.37	27.39	27.33	27.08	26.7
6.1	6.0	6.0	5.6	4.51	4.49	4.55	4.80	5.2
65	47	35	20	4		7	18	29

26.5	23.3	23.6	24.1
5.4	8.6	8.3	7.8
87	77	62	48

TOP MIT 15.0 LT FLOWS FROM S. &
W TO E.

2 ADJUSTING RINGS

FL TO TOPCASTING 13.65

1 5.0 ECCENTRIC CONE

CASTING = 1.0

22.9	25.5	26.5	27.25	27.25	27.18	26.86	26.7
9.0	6.4	5.4	4.63	4.63	4.70	5.02	5.2
65	41	19	4		7	18	29

26.3	23.5	24.2
5.6	8.4	7.7
89	77	48

STA	+	π	-	Elev.
-----	---	-------	---	-------

		931.88		
--	--	--------	--	--

71+20				
-------	--	--	--	--

			5.02	924.86
--	--	--	------	--------

70+63				
-------	--	--	--	--

			7.80	924.08
--	--	--	------	--------

71+50				
-------	--	--	--	--

✓				
---	--	--	--	--

71+62				
-------	--	--	--	--

			7.10	924.78
--	--	--	------	--------

LT

E

RT

40

22

TOP E 2.5' SIDEWALK (S. END) 20.0' LT

TOP MH 40' RT

Flows S TO N

FL TO TOP CASTING 1080

1 5.0' ECCENTRIC CONE

3 ADJUSTING RINGS

CASTING 1.0

25.5 26.0 26.8 27.16 27.13 27.06 26.67 26.6

6.4 5.9 5.1 4.72 4.75 4.82 5.21 5.3

53 40 15 4 7 18 28

25.86

24.0

26.2

21.7

23.3

24.0

6.02

7.9

5.7

10.2

8.6

7.9

55

65

86

77

63

40

E 2.5 SW

SIDE DRAW IN SIDEWALK 74.0' LT

STA	+	+	-	ELEV
-----	---	---	---	------

		931.88		
--	--	--------	--	--

72+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+22				
-----	--	--	--	--

		5.30	926.58	
--	--	------	--------	--

TP	4.93	930.24	6.57	925.31
----	------	--------	------	--------

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23

LT

±

RT

25.3	25.9	25.8	26.3	27.04	27.01	26.86	26.53	26.4
6.6	6.0	6.1	5.6	4.84	4.87	5.02	5.35	5.5
55	55	30	14	4		7	18	29

25.2	25.1	25.31				25.7	21.4	22.2	24.0
6.7	6.8	6.57				6.2	10.5	9.7	7.9
65	82	83				85	74-77	66	42
		± SW.					DITCH		

TOP MH 12.0 LT Flows W TO E

FL TO TOP CASTING 14.00

1 ADJUSTMENT RING

1 5.0 ECCENTRIC CONE (PRECAST)

1 3.0 ADJUSTING SECTION

CASTING = 1.0

S.W. COR SIDE-WALK (ENTRANCE TO LINDIG)

STA	+	π	-	ELEV.
		930.24		

72+50

✓

+83		5.76	924.48
-----	--	------	--------

73+00

✓

+21		5.91	925.05
-----	--	------	--------

28 NOV. 1962

LT

E

RT

42

24

25.6	25.5	26.2	26.93	26.94	26.89	26.48	26.3
4.6	4.7	4.0	3.31	3.30	3.35	3.74	3.9
55	30	15	4		7	18	29

25.2	25.0	25.1	25.3	26.0	25.6	20.9	22.6	23.5
5.0	5.2	5.1	4.9	4.2	4.6	9.3	7.7	6.7
55	60	78	78	100	85	73	63	46

BLOS

FL W. END 15" CM 24.0 LT

25.1	26.0	26.2	26.78	26.76	26.69	26.30	26.0	23.1
5.1	4.2	4.0	3.46	3.48	3.55	3.94	4.2	7.1
65	48	17	4		7	18	29	44

25.6	20.9	21.1
4.7	9.3	9.1
82	75	53

FL E. END 15" CM 24.0 LT. (Filled with dirt)

STA	+	T	-	ELEV
-----	---	---	---	------

		930.24		
--	--	--------	--	--

73+44				
-------	--	--	--	--

			4.43	925.81
--	--	--	------	--------

73+50				
-------	--	--	--	--



+72				
-----	--	--	--	--

			4.28	925.96
--	--	--	------	--------

+72				
-----	--	--	--	--

			6.36	923.88
--	--	--	------	--------

28 NOV. 1962

43

LT

±

RT

25

TOP MH 15.0 LT FLOWS W TO EAST

2 ADJUSTING RINGS

15.0 PRECAST ECCENTRIC CONE

FL TO TOP CASTING 13.65

CASTING = 1.0

24.7	24.8	25.9	26.55	26.56	26.55	26.23	26.0	21.9
5.5	5.4	4.3	3.69	3.68	3.69	4.01	4.2	8.3
43	24	15	4		7	18	29	50

23.8		25.7	20.4	20.3
→ 6.4		4.5	9.8	9.9
65		81	76	64 ←

TOP 1.0 X 6.0 HEADWALL ± = 22.0 LT

FL 15" CM 22.0 LT (W. END)

STA	+	Δ	-	ELEV
-----	---	----------	---	------

		930.24		
--	--	--------	--	--

74+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+12				
-----	--	--	--	--

		4.50	925.74	
--	--	------	--------	--

+12				
-----	--	--	--	--

		6.75	923.49	
--	--	------	--------	--

+28				
-----	--	--	--	--

		6.84	923.40	
--	--	------	--------	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

28 NOV. 1962

44

LT

E

RT

26

24.1	24.4	25.7	26.34	26.38	26.42	26.17	25.8
6.1	5.8	4.5	3.90	3.86	3.82	4.07	4.4
70	41	15	4		7	18	29

24.24

6.00

97

8206

25.6	20.5	20.5	21.3
4.6	9.7	9.7	8.9
81	70	64	52

E 7.5 x 1.0 HEADWALL 22.0 LT

FL E. END 15" CM 22.0 LT

FL W. END 15" CM 22.0 LT

23.4	23.7	25.2	26.09	26.13	26.19	26.02	25.6	21.6
6.8	6.5	5.0	4.15	4.11	4.05	4.22	4.6	8.6
65	45	18	4		7	18	29	48

25.4	20.3	20.2
4.8	9.9	10.0
78	69	59

STA	+	π	-	ELEV
		930.24		
4+67			6.14	924.10
15+00				
✓				
+50				
✓				
+65			11.63	918.61
+65			9.94	920.30
+65			14.59	915.65
BM	4.70	930.59	4.33	925.91 (925.89)

28 Nov. 1962

LT

E

RT

45

27

FL E. END 15" CM 22.0 LT

22.2	22.0	22.0	25.4	25.2	25.9	26.0	25.2	25.9
8.0	8.2	8.2	4.8	4.32	4.25	4.20	4.32	4.3
65	48	31	16	4		7	18	28

25.3	20.4	20.8	21.6
4.9	9.8	9.4	8.6
79	64-67	58	47

DITCH

20.8	20.9	20.6	25.2	25.1	25.8	25.2	25.7	25.6
9.4	9.3	9.6	5.0	4.48	4.42	4.32	4.49	4.6
65	55	38	17	4		7	18	29

21.3	19.5	20.6	21.7
4.9	10.7	9.6	8.5
77	59-61	56	46

DITCH

FL N. END 24" SCP 41.0 LT

CENTER 2.3 X 2.3 WOODEN GRATED CB COVER 55.0 RT.

FLOOR OF CB 55.0 RT. 18.0 SCP RUNS

EASTERLY FROM FLOOR OF CB.

DOOR-SILL MACK HOTEL BARBER SHOP ENTI

STA

+

π

-

F

930.59

75+87

✓

+ 94

✓

76+00

✓

28 Nov. 1962

46

LT

E

RT

28

20.47	24.1	25.2	25.61	25.68	25.69	25.57	25.4
10.12	6.5	5.4	4.98	4.91	4.90	5.02	5.2
33	26	15	4		7	18	29

FL W END

12" CM

20.7	21.1	21.4
9.9	9.5	9.2
40	53	65

25.1	19.6	21.1
5.5	11.0	9.5
77	62-65	51

DITCH

21.8	22.5	24.7	25.1	25.59	25.63
8.8	8.1	5.9	5.5	5.00	4.96
57	46	28	16	4	

SAME AS + 87 ON RT.

21.6
9.0
65

21.1	24.6	25.3	25.56	25.62	25.63	25.53	25.3
8.5	6.0	5.3	5.03	4.97	4.96	5.06	5.3
55	28	15	4		7	18	29

21.6
9.0
65

25.1	19.6	20.7	21.2
5.5	11.0	9.9	9.4
77	61-64	56	49

DITCH

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		930.59		
--	--	--------	--	--

76+17				
-------	--	--	--	--

✓				
---	--	--	--	--

+19				
-----	--	--	--	--

✓				
---	--	--	--	--

+42				
-----	--	--	--	--

✓				
---	--	--	--	--

28 Nov. 1962

47

LT

±

RT

29

22.3	24.2	24.9	25.49	25.53	25.55	25.41	25.2
8.3	64	5.7	5.10	5.06	5.04	5.18	5.4
46	30	18	4		7	18	28

21.7
8.9
65

25.3 20.3 20.9 21.6
5.3 10.3 9.7 9.0
77 61-64 56 47
DITCH

20.58 22.6 24.9 25.47 25.53

10.01 7.0 5.7 5.12 5.06 SAME AS +17 ON RT.
31 25 16 4

PLE. END
12" CM

21.4 21.9 21.8
9.2 8.7 8.8
40 50 65

22.1 24.4 25.0 25.43 25.50 25.51 25.36 24.9

8.5 6.2 5.6 5.16 5.09 5.08 5.23 5.7
26-28 21 14 4 7 18 28
DITCH

25.2 25.9 26.3
5.4 4.7 4.3
40 56 65

25.2 19.9 20.9 21.4
5.4 10.7 9.7 9.2
77 61-63 56 48
DITCH

✓
STA + π - ELEV

930.59

76+54

5.20 925.39

76+78

✓

+85

✓

28 Nov. 1962

48

LT

±

RT

30

TOP MH 16'0 LT Flows W TO E.

FL TO TOP CASTING 13.88

2 ADJUSTING RING

1-5'0 PRECAST ECCENTRIC CONE

1-3'0 ADJUST SECTION

CASTING = 1'0

22.34	24.7	25.2	25.24	25.33	25.38	25.27	24.8
8.25	5.9	5.4	5.35	5.26	5.21	5.37	5.8
25	21	15	4		7	18	29

FL WEND
12" CM

25.4	26.1	26.8	27.0	25.0	19.9	21.1	22.0
5.2	4.5	3.8	3.6	5.6	10.7	9.5	8.6
35	47	65	82	77	62-65	67	44

BLDG DITCH

26.2	26.1	25.1	25.24	25.36	
4.4	4.5	5.5	5.35	5.23	SAME AS +78 ON RT
47	29	16	4		

26.8
3.8
65

STA

+

T

-

ELEV

930.59

77+00

✓

+09

✓

+20

✓

28 NOV. 1962

49

LT

E

RT

31

26.0	25.6	25.1	25.19	25.26	25.31	25.5	24.6
4.6	5.0	5.5	5.40	5.33	5.28	5.44	6.0
47	32	13	4		7	18	29

26.7
3.9
65

24.9 20.0 21.1 21.7
5.7 10.6 9.5 8.9
77 61-64 57 47
DITCH

24.9	22.96	24.6	25.16	25.21	25.29	25.11	24.5
5.7	7.63	6.0	5.43	5.38	5.30	5.48	6.1
32	24	17	4		7	18	29

FL FEED
12" CM

25.8 26.4
4.8 4.2
47 65

24.9 20.0 21.2 21.9
5.7 10.6 9.4 8.7
78 61-64 58 43
DITCH

23.8	23.6	24.4	25.10	25.15	25.23	25.04	24.6
6.8	7.0	6.2	5.49	5.44	5.36	5.55	6.0
47	29	15	4		7	18	29

24.0
6.6
65

24.9 21.2 20.2 21.2 22.3
5.7 9.4 10.4 9.4 8.3
79 69 62-65 58 40
DITCH

STA

+

天

0000000000000000

ELEV.

930.59

 $77+50$

✓

78+00

BM

3.26

929.15

4.70

925.89

925.89

28 NOV. 1962

50

LT

E

RT.

32

24.3	24.3	24.6	24.99	25.05	25.04	24.88	24.4
6.3	6.3	6.0	5.60	5.54	5.55	5.71	6.2
50	27	15	4		7	18	29

24.3
6.3
65

24.9 21.5 20.5 21.2 22.4
5.7 9.1 10.1 9.4 8.2
80 70 63-66 57 39
DITCH

24.9	24.6	24.3	24.1	24.84	24.87	24.79	24.59	24.2
5.7	6.0	6.3	6.5	5.75	5.72	5.80	6.00	6.4
72	55	37	18	4		7	18	29

25.29

25.2

5.30

5.4

72
CONC.82
BLDG.

24.5 21.7 20.3 21.2 22.0
6.1 8.9 10.3 9.4 8.6
81 70 64-67 59 39
DITCH

W. END DOOR-SILL (BARBER SHOP - MACK HOTEL)

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		929.15		
--	--	--------	--	--

78+50				
-------	--	--	--	--

✓				
---	--	--	--	--

79+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+13				
-----	--	--	--	--

		5.41	923.74	
--	--	------	--------	--

28 NOV. 1962

51

LT

E

RT

33

24.2	24.1	24.2	24.64	24.70	24.62	24.34	24.0	21.9
5.0	5.1	5.0	4.51	4.45	4.53	4.81	5.2	7.3
47	33	14	4		7	18	29	42

24.8

4.4

71

24.3 22.3 20.6 21.3

4.9 6.9 8.6 7.9

81 75 64-67 58

DITCH

22.6	22.5	22.6	23.8	24.07	24.15	24.15	24.03	23.6	21.9
5.6	5.7	5.6	5.4	5.08	5.00	5.00	5.12	5.6	7.3
65	49	35	16	4		7	18	29	46

23.1 21.5

6.1 7.7

77 70

TOP MH 15.0 LT

FLOWS FROM N.W.
E.W TO E.

FL TO TOP OF CASTING 13.23

3 ADJUSTING RWGS

1-5.0 PRECAST ECCENTRIC CONE

1-2.0 ADJUSTING SECTION

CASTING = 1.0

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		929.15		
--	--	--------	--	--

79+21				
-------	--	--	--	--

		7.82	921.33	
--	--	------	--------	--

79+21				
-------	--	--	--	--

		14.71	914.44	
--	--	-------	--------	--

79+24				
-------	--	--	--	--

✓

+41 = W. EDGE ^{Fairview Ave.} ~~NEW BRIGHTON RD.~~

✓

28 Nov. 1962

52

LT

E

RT

34

CENTER OF 2.3 X 2.3 WOODEN GRATE 56.0 RT.

TOP FLOOR CB 56.0 RT. 18.0 SCP RUNS
FROM WEST AND 18" SCP RUNS EASTERLY
FROM CB

23.5	23.4	23.6	23.9	24.04	24.08	24.07	23.99	23.71
5.7	5.8	5.6	5.3	5.11	5.07	5.08	5.16	5.44
78	49	23	14	4		7	18	34

23.2	23.2	21.8	23.4
6.0	7.0	7.4	5.8
74	67	54	42

24.1	24.1	23.9	24.11	24.15	24.17	24.23	24.3
5.1	5.1	5.3	5.04	5.00	4.98	4.92	4.9
77	54	25	4		7	18	38

24.16	24.3
4.99	4.9
90	61

RTTRACK

STA + π - ELEV.

929.15

79+51 = $\frac{1}{2}$ Fairview Ave,
~~NEW BRIGHTON RD,~~

✓

✓

79+61 = E. EDGE Fairview Ave,
~~NEW BRIGHTON RD~~

✓

28 NOV. 1962

53

LT

E

RT

35

24.2	24.2	24.1	24.16	24.20	24.21	24.30	24.4
5.0	5.0	5.1	4.99	4.95	4.94	4.85	4.8
100	62	23	4		7	18	39

24.1 24.0
5.1 5.2
150 200

24.5 24.3 24.14 24.5
4.7 4.9 5.01 4.7
150 100 90 65

TOP TRACK

24.9
4.3
200

24.1	24.1	24.0	24.11	24.18	24.24	24.25	24.4
5.1	5.1	5.2	5.04	4.97	4.91	4.90	4.8
85	67	25	4		7	18	64

24.04
5.11
90

RR TRACK

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		929.15		
--	--	--------	--	--

79+73				
-------	--	--	--	--

			5.66	923.49
--	--	--	------	--------

79+73				
-------	--	--	--	--

			5.18	923.97
--	--	--	------	--------

79+90				
-------	--	--	--	--

✓				
---	--	--	--	--

BM				
----	--	--	--	--

			3.76	925.39 (925.37)
--	--	--	------	-----------------

28 NOV. 1962

54

LT

E

RT

36

TOP MIT 30.0 LT

Flows FROM S.W

FL TO TOP CASTING 13.64

" S TO N.

5 ADJUSTING RINGS

1- 5.0 ECCENTRIC CONE

1- 2.0 ADJUSTING SECTION

CASTING = 1.0

TOP MIT 41.0 RT

FL TO TOP CASTING 12.10

Flows S TO N

3 ADJUSTING RINGS

1- 5.0 ECCENTRIC CONE

CASTING = 1.0

23.3	23.3	22.2	22.4	23.95	23.96	23.97	23.88	23.6
5.9	5.9	7.0	5.8	5.20	5.19	5.18	5.27	5.7
65	52	35	20	4		7	18	29

23.0	22.4	21.3
62	68	7.9
79	63	46

Fairview Ave.

TOP MOUNT AT NEW BRIGHT RD

Sta	+	π	-	EIV
BM	2.82	928.19		925.37

80+00

+15

✓

+60

✓

81+00

RG
DS
WS

Nov. 27, 1962
PC Windy 45° 55
RT 37

14.

4

RT

37

Top Mont Fairview 200' SE. of "C"

23.5	23.4	22.1	23.4	23.96	24.0	23.6	22.7	21.2	21.9	23.0	23.4
4.7	4.8	6.1	4.8	4.24	4.2	4.6	5.5	7.0	6.3	5.2	4.8
75	50	26	16	7	26	38	48	59	75	87	
			BT								

23.6	21.7	21.8	22	23.8	23.9	23.8	23.6	22	21.1	23
4.6	6.5	6.4	5.0	4.4	4.3	4.3	4.4	4.6	5.0	7.1
37	28	22	14	4	7	18	25	31	41	54

23.8	23.1
4.4	3.1
53	70

23.4	22.8	22.1
4.8	5.4	6.1
86	79	65

23.6	23.0	20.9	21.1	23.0	23.6	23.7	23.69	23.6	23.1	21.0	23.9
4.6	5.2	7.3	7.1	5.2	4.6	4.5	4.50	4.6	5.1	7.2	7.9
45	38	31	22	14	4	7	18	29	40	47	

24.6	24.1
3.6	4.1
59	78

23.4	22.4	20.7	20.0
4.8	5.8	7.9	8.2
86	74	63	55

21.0	19.4	20.4	23.8	23.3	23.10	23.4	23.1	23.1	19.9	18.4
7.2	8.8	7.8	5.4	4.9	4.79	4.8	4.9	5.1	8.3	9.8
36	29	25	14	4	7	18	28	43	54	

Sta + π - Ely

928.19

(81+00)
✓

81+30

✓

+55

11.64 916.55

+63

✓

82+00

✓

Nov 27, 1962

56

LT

Z

RT

38

22.5 23.3 27.1 20.9
5.7 4.9 5.8 7.3
44 49 65 80

23.5 20.9 18.5
4.7 7.3 9.7
79 70 60

19.8 18.8 18.6 19.6 22.5 27.1 23.3 27.1 27.1 19.4 17.1
8.4 9.4 9.6 8.6 5.7 5.0 4.9 4.86 5.0 5.1 8.8 11.1
50 37 32 24 14 4 7 18 28 46 56

19.8
8.4
75

23.4 17.1
4.8 11.1
79 64

rim of CB RT 64'

14.3 14.1 18.2 27.1 20.0 23.09 27.1 27.1 27.1 27.8 18.4 16.4
13.9 14.1 10.0 5.9 5.2 5.10 5.1 5.2 5.4 9.8 11.8
59 44 29 14 4 7 18 28 48 56

19.8 16.8
10.4 11.4
66 75

23.4 16.4
4.8 11.8
79 68

13.6 13.2 17.5 22.1 22.7 22.80 22.86 22.8 22.5 18.5 16.0
14.6 15.0 10.7 6.1 5.5 5.39 5.33 5.4 5.7 9.7 12.2
60 48 30 14 4 7 18 28 48 60

10.7
75

5.1 12.2
80 68

Sta + π - E/V.

928.19

82+50

✓

TP 6.02 925.05 9.16 919.03 919.03

83+00

✓

+20

✓

Nov. 27, 1962 57

LT.

±

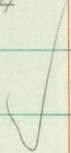
RT

39

11.8	12.1	12.6	21.8	22.1	22.2	22.1	22.0	21.7	18.1	15.5
16.4	15.7	11.6	6.9	6.1	6.0	6.0	6.2	6.5	10.1	12.7
55	49	33	13	4		7	18	28	48	59

16.2	17.2
12.0	11.0
69	75

0	15.7
2.2	15.1
5.2	12.5
82	67

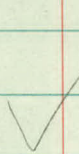


Spike in PP LT Sta 83+30

10.1	10.6	15.9	21.0	21.2	21.30	21.32	21.02	21.0	17.1	14.1
15.0	14.5	9.2	4.1	3.84	3.75	3.73	4.03	4.1	8.0	10.4
62	55	31	14	4		7	18	28	47	57

15.6	15.7
9.5	9.4
75	86

33.0	14.6
2.1	10.5
81	64



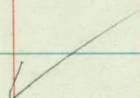
10.0	10.0	14.2	21.1	21.9	21.4	21.6	21.2	21.2	16.5	14.5
15.1	15.1	10.9	4.0	3.8	3.7	3.6	3.9	3.9	8.6	10.6
71	57	38	13	4		7	18	28	49	57

W.S.
(water surface)

0.0	2.2	15.2
16.1	9.9	9.9
71	79	91

GE

2.9	14.6
2.2	10.5
85	64



Sta + π - E/V.

925.05

+40

✓

+70

✓

84+00

✓

sta

+

 π

-

E/V.

925.05

84+50

✓

+84

✓

TP

5.51

929.17

1.39

923.66

3.09

926.08

85+00

✓

Nov. 27, 1962

59

10.4	11.9	12.5	13.3	13.7	13.8	13.8	13.6	13.3	19.1	17.5
14.7	13.2	7.6	1.8	1.4	1.3	1.3	1.5	1.8	6.0	7.6
100	62	36	13	4		7	18	28	50	58

17.5	17.5
1.7	2.6
82	69

14.3	14.0	13.7	16.4	13.7	24.1	24.2	24.3	24.1	23.9	20.1	18.2
10.8	11.1	11.4	8.7	1.4	1.0	0.9	0.8	1.0	1.2	5.1	6.9
100	84	68	44	13	4		7	18	28	48	58

17.9	17.9
1.4	2.2
82	67

Top 18" SCP 27' Lt ± Sta 85+33 ±

14.8	15.1	18.7	23.9	24.3	24.37	24.40	24.26	24.1	20.2	18.2
14.4	13.6	10.5	5.3	4.86	4.80	4.77	4.93	5.1	9.0	11.0
56	48	36	13	4		7	18	29	49	62

15.4	15.7	16.4	15.7
13.8	13.5	12.8	13.5
62	75	90	100

19.2	19.2
5.5	10.0
83	70

Sta	+	π	-	Elev.
-----	---	-------	---	-------

929.17

85+13

✓

+24

Top Bank

+59

& 18' Ent

86+00

+23

3.36 925.81

11

4.61 924.56

RG
DS
RB
WS

Nov 27, 1962 (PM)

60

Lt.

4

Rt.

42

19.4

17.2

19.6

24.1

24.6

24.6

24.6

24.5

24.4

20.1

18.7

9.8

12.0

9.6

5.1

4.6

4.6

4.6

4.7

4.8

9.1

10.5

66

46

35

13

4

7

18

29

50

65

21.1

21.1

8.1

8.1

90

100

23.7

5.5

84

25.5

25.5

20.7

24.3

24.7

24.8

24.8

24.7

24.6

18.9

19.2

23.8

3.7

3.7

8.5

4.9

4.5

4.4

4.4

4.5

4.6

9.3

10.0

5.4

85

53

32

13

4

7

18

29

51

64

83

27.3

26.8

25.8

24.2

25.1

25.4

25.4

25.4

25.3

25.1

24.6

24.5

24.2

1.9

2.4

3.4

5.0

4.1

3.8

3.8

3.8

3.9

4.1

4.6

4.9

5.0

75

58

33

26

13

4

7

18

29

42

65

85

27.9

27.5

27.1

24.8

25.5

26.0

26.05

26.05

26.01

25.8

21.3

20.4

24.0

1.3

1.7

2.1

4.4

3.7

3.16

3.12

3.12

3.16

3.4

7.9

8.8

5.2

75

59

37

27

13

4

7

18

29

50

61

83

BT

BT

BT

Top 15" CM Lt 23'

F.L.

Sta + + - Elev.

929.17

86+50 Ent Lt.

+83

3.62 925.55

TP 6.94 933.74 2.37 926.80

BM

2.37 931.37 (931.36)

87+00

✓

+50

6.30 927.44

+50

88+00

✓

Nov 29, 1962

61

	Lt			E			Rt			43	
26.5	26.1	27.3	26.8	26.9	26.9	26.8	26.6	21.6	20.7	23.9	
0.7	1.1	1.9	2.4	2.3	2.3	2.3	2.4	2.7	2.6	8.5	5.3
75	60	33	13	4		7	18	29	51	65	83

FL 15" CM Lt 22'

Top 15" CM Lt 22'

SW Cor. Ent. Slab Bruce Truck Line

29.7	29.2	28.4	28.1	26.5	27.3	28.02	28.10	28.13	28.02	27.6	23.2	21.1
4.0	4.5	5.3	5.6	7.2	6.4	5.72	5.64	5.61	5.72	6.1	10.5	12.6
75	65	60	36	20	14	4		7	18	29	47	67
	BT		BT									

24.1
9.6
82

E. rim M.H. Lt 30'

29.9	29.5	28.8	28.1	27.4	27.1	27.6	28.4	28.4	28.5	28.4	28.0	23.9	21.3	23.7
3.8	4.2	4.9	5.6	6.3	6.6	6.1	5.3	5.3	5.2	5.3	5.7	9.8	12.4	10.0
75	65	60	36	30	22	14	4		7	18	29	46	67	83
		BT	BT											

28.9	28.4	27.7	28.3	28.96	29.00	29.00	28.86	28.6	24.0	21.8
4.8	5.3	6.0	5.4	4.78	4.74	4.74	4.88	5.1	9.7	11.9
60	36	23	14	4		7	18	29	47	66
	BT									

29.5
4.2
62

30.0
3.7
75

23.9
9.8
83

Sta + π - EIV

933.74

88+50

BM 3.83 935.20 2.37 931.37 931.36

89+00

W. edge Ent. Lt.

+18 E Ent. Lt

+38

7.57 927.63 MH 915.47

1.86
5.52

+55

90+00

+10

✓

RG
DS
WS
R Behrens

Nov 28, 1962
Cl. Cool

62

LT

#

RT

44

79.4	74.8	72	79.5	79.3	79.3	79.4	79.2	78.6	72.9	71.9	74.2
4.3	4.9	5.5	5.2	4.4	4.4	4.3	4.4	5.1	9.8	11.8	9.5
75	61	35	15	4	✓	7	18	29	49	71	84

SW Cor Est. Slab Bruce Truck Line

78.7	78.4	78.4	79.1	79.43	79.48	79.49	79.38	79.0	72.8	71.4	72
6.5	6.8	6.8	6.1	5.77	5.72	5.71	5.82	6.2	11.4	13.8	11
75	52	29	13	✓4		7	18	28	51	20-72	8
BT	BT	BT	BT								

78.7	78.5	78.5	78.9	79.5	79.5	79.5	79.4	78.9	73.8	71.6	73.9
6.5	6.7	6.7	6.3	5.7	5.7	5.7	5.8	6.3	11.4	13.6	11.3
75	56	34	18	4		7	18	28	50	20-73	83

78.5	78.1	77.5	78.7	79.4	79.5	79.5	79.4	78.9	73.7	71.3	73.9
6.7	7.1	7.6	6.5	5.8	5.7	5.7	5.8	6.3	11.5	13.9	11.3
75	50	32	16	4		7	18	29	49	69-73	82
			BT								

77.8	77.6	77.1	78.6	79.20	79.24	79.23	79.13	78.6	73.4	70.8	74.0
7.4	7.6	8.1	6.6	6.00	5.96	5.97	6.07	6.6	11.8	14.4	11.2
75	45	32	13	4		7	18	29	51	69-73	82

76.2	78.1	78.8	77.0	78.4	79.1	79.2	79.2	79.1	78.5	77.90	70.9
7.0	7.1	6.4	8.2	6.8	6.1	6.0	6.0	6.1	6.7	12.3	14.3
75	64	44	32	13	4		7	18	29	53	65

73.9	71.3
11.3	13.9
82	72

Sta

+

π

-

EL

935.20

+25

Top Bank Lt.

+50

91+00

✓

+50

✓

TP

3.65

931.07

7.78

927.42

927.43

LT

Z

RT

45

34.0	34.1	30.8	26.6	28.3	25.0	29.0	29.0	28.9	28.3	29.0	21.1	21.3	21.8
1.2	1.1	4.4	8.6	6.9	6.2	6.2	6.2	6.3	6.9	12.2	14.1	13.9	11.4
75	56	45	29	13	4	7	18	29	52	65	73	87	

33.4	33.7	29.6	26.4	28.1	28.6	28.8	28.8	28.7	28.2	23.3	20.9	23.9
1.8	1.5	5.6	8.8	7.1	6.4	6.4	6.4	6.5	7.0	11.9	14.3	11.3
75	55	42	30	12	4	7	18	29	49	65	72	82

32.8	33.0	29.4	25.7	27.7	28.20	28.15	28.18	28.03	27.6	22.8	21.2
2.4	2.2	5.8	9.5	7.5	7.0	7.05	7.02	7.17	7.6	12.4	14.0
75	54	43	30	13	4	7	18	28	51	62	

24.0	20.7
11.2	14.5
83	72

31.9	31.8	28.9	25.0	26.7	27.2	27.3	27.4	27.2	27.0	26.4	26.1
3.3	3.4	6.3	10.2	8.5	8.0	7.9	7.8	8.0	12.7	14.8	14.8
75	53	42	30	14	4	18	29	50	63	72	

23.6
11.6
82

Spike in PP LT Sta 91450

Sta

+

 π

-

Elev.

931.07

92+00

✓

+50

✓

+79

7.27 923.80

Jk
Top MH. 30' Lt.

93+00

✓

30.3	30.1	27.8	24.0	25.8	26.31	26.35	26.46	26.27	26.9	27.0	20.2
0.8	1.0	3.3	2.1	5.3	4.76	4.71	4.67	4.80	5.2	9.1	10.9
75	50	40	28	13	4		7	18	28	48	62

23.3	20.2
7.8	10.9
82	72

27.0	23.8	23.5	24.3	24.8	25.3	25.3	25.4	25.3	24.9	21.4	19.8
4.1	7.3	7.6	6.8	6.3	5.8	5.8	5.7	5.8	6.2	9.7	11.3
41	30	24	23	14	4		7	18	28	49	62-71

28.8	29.0
2.3	2.1
49	75

23.0
8.1
83

25.7	22.8	22.4	23.2	23.8	24.11	24.16	24.20	24.06	23.7	20.8	19.2
5.4	8.3	8.7	7.9	7.3	6.96	6.91	6.87	7.01	7.4	10.3	11.9
38	28	26	23	14	4		7	18	29	46	60

27.3	27.7	22.9
3.8	3.4	3.2
46	64	75

27.5	19.0
8.5	12.1
83	71

Sta

+

 π

-

EN

931.07

93+50

✓

BM 1.93 925.07 1.93 923.14 (923.16)

92+79 1.31 923.76

94+00

✓

+50

✓

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	Lt.	#	Rt.	47							
	22.2	20.7	21.5	22.6	22.0	23.1	23.1	23.0	22.4	19.9	18.6
	8.9	10.4	9.6	8.5	8.1	8.0	8.0	8.1	8.7	11.2	12.5
	31	28	27	13	4	7	18	28	45	60	
	24.1	25.5	25.5	24.4					22.2	19.2	
	7.0	5.6	5.6	4.7					8.8	11.9	
	38	46	63	85					82	71	

Spike in 36" Tw. Oak Lt. Sta 94+30

M.H.	Lt 30										
21.9	21.2	19.4	20.0	21.5	21.93	21.97	22.01	21.89	21.6	18.8	18.2
3.2	3.9	5.7	5.1	3.6	3.14	3.10	3.06	3.18	3.5	6.3	6.9
40	32	29	27	13	4		7	18	29	45	59
	22.6	22.9	23.2						21.6	18.1	
	2.5	2.2	1.9						3.5	7.0	
	45	64	75						82	69	

	18.3	17.7	16.3	20.5	20.9	20.9	20.9	20.8	20.3	17.7	17.3
	6.8	7.4	6.8	4.6	4.2	4.2	4.2	4.3	4.8	7.4	7.8
	33	30	28	14	4		7	18	29	47	61-69
	19.2	19.7	20.2								21.2
	5.9	5.4	4.9								3.9
	43	60	75								83

Sta + π - E/W

925.07

95+00

+07

8.32 916.75

+20

W. edge ent. Lt.

✓

+41

± Ent.

+62

E. edge Ent

+65

✓

Nov 28, 1962 66

LT	E	RT	48
18.2	17.9	17.6	17.2
6.9	7.2	7.5	7.9
75	62	38	32
		BT	15
			4
			19.1
			19.66
			19.72
			19.76
			19.58
			19.3
			16.6
			16.0
			15.9
			20.6

INV 18" CM LT 32' same section as above LT.

18.6	18.5	18.5	19.3	19.3	19.4	19.2	18.9	16.4	15.6	15.2
6.5	6.6	6.6	5.8	5.8	5.7	5.9	6.2	8.7	9.5	9.9
75	47	31	4		7	18	29	42	57	68
BT	BT	BT								

20.6
4.6
84

18.6	18.4	18.5	18.8	18.9	19.0	19.8	18.5	15.7	15.1	20.4
6.5	6.7	6.6	6.3	6.2	6.1	6.3	6.6	9.4	10.0	4.7
75	39	22	4		7	18	29	45	61-70	83

18.6	18.2	18.1	18.5	18.5	18.6	18.4	18.0	15.5	15.0	20.2
6.5	6.9	7.0	6.6	6.6	6.5	6.7	7.1	9.6	10.1	4.9
75	39	22	4		7	18	29	41	57-69	84

16.7	16.06	16.7	16.9	18.0	18.4	18.4
8.4	9.01	8.4	8.2	7.1	6.7	6.7
32	31	27	25	15	4	

same as above

17.7	18.6	18.5	18.6	18.4
2.4	6.6	6.5		
40	60	75		

Sta + π - EIV

925.07

96+00

✓

1535=Top

+18 M.H. 31' Lt Top 2.5' Below $\pm$ Sta 96

BM 2.74 921.41 6.40 918.67 (918.67)

96+25

+59 E. edge PKg. Lot

✓

97+00

2.58 918.83

Nov. 28, 1962

67

LT

E

RT

49

16.8	16.1	16.2	17.4	17.81	17.85	17.87	17.77	17.3	15.1	14.3
8.3	9.0	8.9	7.7	7.24	7.22	7.20	7.30	7.8	10.0	10.8
36	30	26	13	4		7	18	29	41	59

17.8
7.3
53

18.5
6.6
75

20.0
5.1
83

14.3
10.8
69

Top SE Cor Curb LT 90' Sta 96+59

18.2	17.5	16.4	16.3	16.0	17.1	17.4	17.46	17.5	17.3	17.0	14.5	14.0	14.1	14.5
3.2	3.9	5.0	5.1	5.4	4.3	4.0	3.95	3.9	4.1	4.4	6.9	7.4	7.3	1.9
75	57	37	35	25	13	4		7	18	28	42	60	70	86
BT	BT	BT												

18.67	18.0	16.3	15.7	15.8	16.7	17.0	17.0	17.1	16.8	16.5	14.1	13.5	13.6
2.74	3.4	4.9	5.7	5.6	4.7	4.4	4.4	4.3	4.6	4.9	7.3	7.9	7.8
67	67	38	31	21	12	4		7	18	28	46	39	69
TC	BC	BT											

18.76
2.65
75
TC

18.2
3.2
75
TC

19.2
2.2
85

18.8	17.3	16.3	15.2	16.3	16.59	16.63	16.68	16.52	16.2	13.9	13.1	13.4	19.0
2.6	4.1	6.1	6.2	5.1	4.82	4.78	4.73	4.89	5.2	7.5	8.3	8.0	2.4
75	48	30	22	13	4		7	18	28	41	59	69	85

Rim MH LT 88' Sta 97+29

Sta	+	π	-	E/V.
-----	---	-------	---	------

		921.41		
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97+50

✓

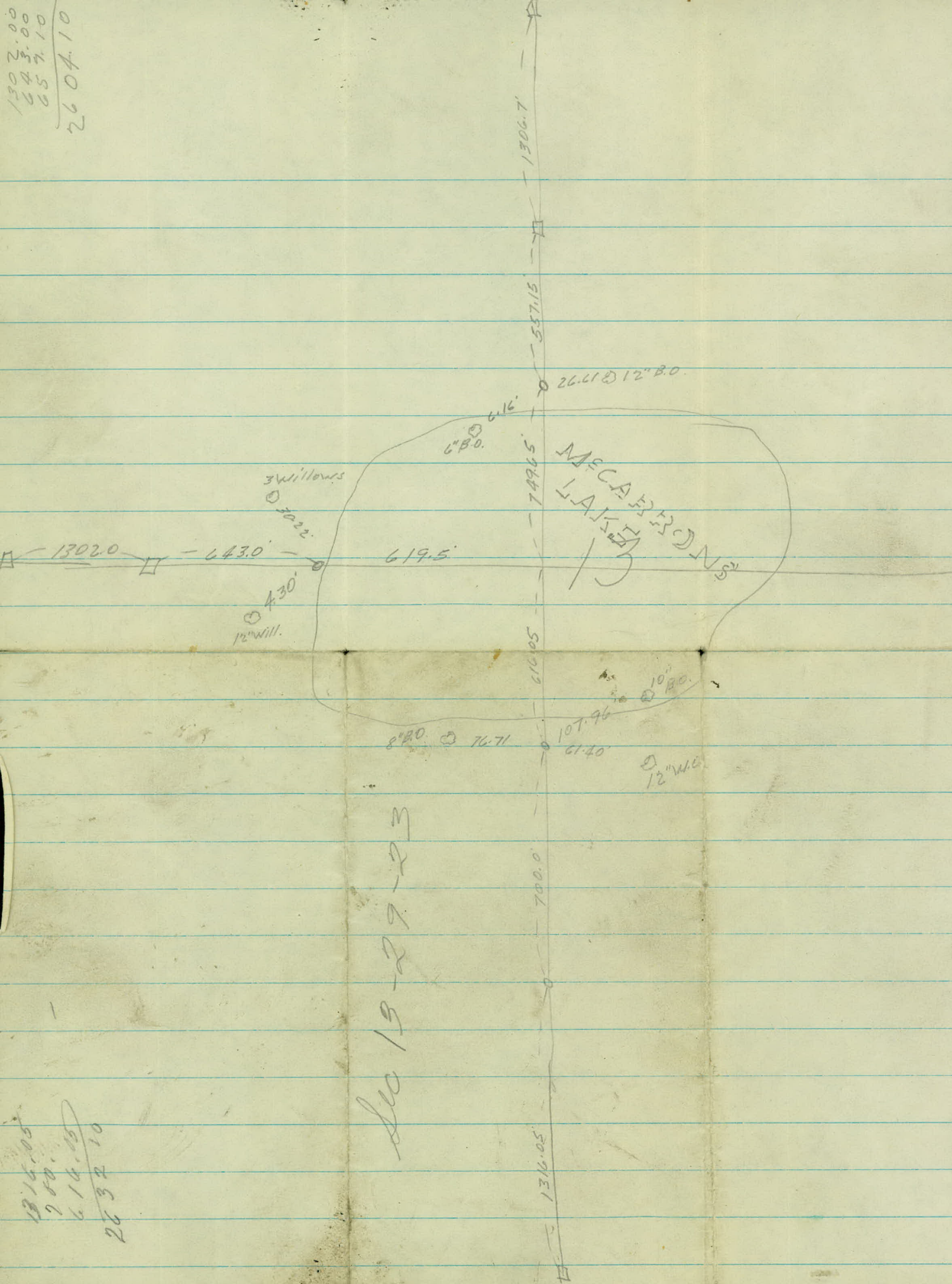
+90 W. edge Pkg. Lot

✓

98+00

TP	1.38	920.56	2.23	919.18
----	------	--------	------	--------

1302.00
 643.00
 657.10
 2604.10



Nov. 28, 1962

68

L+

F

R+

50

17.1	14.8	14.8	16.1	16.2	16.3	16.3	16.2	15.8	13.3	17.1
4.3	6.6	6.6	5.3	5.2	5.1	5.1	5.2	5.6	8.1	8.7
47	39	21	13	4		7	18	28	43	58

Sod

18.1	18.5
3.3	2.9
58	75

18.1	12.9
2.8	8.5
83	66

18.3	16.1	14.4	14.5	15.7	16.1	16.1	16.2	16.1	15.7	13.0	17.1	17.7
3.28	4.8	7.0	6.9	5.7	5.3	5.3	5.2	5.3	5.7	8.4	9.3	8.7
64	47	31	23	15	4		7	18	28	43	60	70

Sod

17.7	17.8	18.27
3.7	3.6	3.14
64	75	75
BC	BC	TC

18.1
3.3
81

17.99	16.7	14.3	14.3	15.7	16.09	16.15	16.18	16.11	15.7	13.0	17.5
3.42	4.7	7.1	7.1	5.7	5.32	5.26	5.23	5.30	5.9	8.4	8.9
64	49	31	23	16	4		7	18	28	42	59

Sod

17.5	17.6
3.9	3.8
64	75
BC	BT

18.2	12.6
3.2	8.8
81	70

Top guard rail post 36' R+ Sta 98+15±

Sta + π - E/V

920.56

98+12 W. edge Ent. Lt.

✓

+43 E Ent. Lt.

+73 E. edge Ent. Lt.

99+00

+50

+54

+57

7.73

7.13

912.83

913.43

RG
WS
DS

Nov. 29, 1962
C.I. Cool

69

LT

4

RT

51

17.1	15.9	13.47	15.9	16.7	16.1	16.2	16.2	16.1	15.8	13.2	12.3
3.5	4.7	7.09	4.7	4.9	4.5	4.4	4.4	4.5	4.8	7.4	8.3
55	30	29	28	20	4	7	18	27	42	55	
BT	BT	inv	BT	BT							
BC		18"CM									
		W-end.									
17.66	17.78	19.1	17.4							18.2	12.6
2.90	2.78	3.5	3.2							2.4	8.0
55	63	63	75							80	70
TC	TC	BC									

17.4	16.9	16.5	16.0	16.1	16.1	16.2	16.1	16.0	13.1	12.0	12.1	18.1
3.2	3.7	4.1	4.6	4.5	4.5	4.4	4.5	4.6	7.5	8.6	8.5	2.5
100	80	64	32	4		7	18	27	40	58	69	81

17.2	14.5	15.8	13.21	15.5	16.1	16.1	16.1	15.7	12.8	12.0	12.2	17.9
3.4	4.1	4.8	7.35	5.1	4.5	4.5	4.5	4.9	7.8	8.6	8.4	2.7
100	67	45	29	29	4		7	18	27	44	54	65
			inv.	BT	BT							81
			E-end.									

16.7	16.1	14.0	14.2	13.8	15.7	16.01	14.06	16.11	16.02	15.8	12.6	11.9	12.1	17.9
3.9	4.5	5.6	6.4	6.8	4.9	4.55	4.50	4.45	4.54	4.8	8.0	8.7	8.5	2.7
75	55	37	32	23	12	4		7	18	28	43	56	67	80
BT	BT	BT												

16.5	15.9	14.6	13.7	13.7	15.4	16.0	16.1	16.1	16.0	15.5	12.0	11.8	12.0	17.6
4.1	4.7	6.0	6.9	6.9	5.2	4.6	4.5	4.5	4.6	5.0	8.6	8.8	8.6	3.0
75	60	37	29	24	13	4		7	18	27	45	61	69	80
BT	BT	BT												

Top M H LT

Sta + π - EIV

920.56

100+00 E. edge Pkg. lot.

✓

+24 Fe. line

+50

101+00

✓

BM 6.03 920.22 6.37 914.19 (914.20)

Nov. 29, 1962 70

Lt				Rt			
15.5	15.1	13.9	13.6	15.97	15.99	15.89	15.6
5.1	5.5	6.7	7.0	4.59	4.57	4.67	5.0
75	61	41	31	7	18	28	44
BT		BT					

17.3
3.3
80

11.7
8.9
67

13.6	13.6	13.2	13.3	13.4	15.6	15.9	16.0	16.0	15.9	15.5	12.6	11.9	11.7	17.0
7.0	7.0	7.4	7.3	7.2	5.0	4.7	4.6	4.6	4.7	5.1	8.0	8.7	8.9	3.6
75	58	41	35	24	12	4		7	18	29	44	61	67	81
		Fe												
		Cor.												

12.8	13.0	13.2	13.4	15.4	15.9	15.9	16.0	15.9	15.5	12.9	11.8	11.9	17.0
7.8	7.6	7.4	7.2	5.2	4.7	4.7	4.6	4.7	5.1	7.7	8.8	8.7	3.6
75	60	41	22	12	4		7	18	28	40	61	66	80
		Fe											

12.9	13.2	13.0	13.0	15.3	15.83	15.87	15.88	15.78	15.3	13.2	12.3	13.0
7.7	7.4	7.6	7.6	5.1	4.73	4.69	4.68	4.78	5.3	7.4	8.3	7.6
75	65	43	22	11	4		7	18	28	40	51	58
		Fe										

17.3
3.3
81

12.3
8.3
65

Spike in 10" Maple Lt Sta 101+57

Sta + π - E/V

~~920.22~~ 920.22

101+50

✓

+77

✓

+90 $\neq$ Ent. / t.

✓

102+00

4.53 915.69

Nov. 29, 1962 71

LT

E

RT

53

13.4	13.5	12.6	12.9	15.4	15.7	15.8	15.8	15.7	15.3	12.6	11.1	11.3
6.8	6.7	7.6	7.3	4.8	4.5	4.4	4.4	4.5	4.9	7.6	9.1	8.9
66	47	38	26	13	4		7	18	28	44	60	64

Fe

13.4
→ 6.8
75

17.2
3.0
81

13.3	11.72	14.6	14.8	15.5	15.6	15.7	15.8	15.6	15.4	12.3	11.6
6.9	8.46	5.6	5.4	4.7	4.6	4.5	4.4	4.6	4.8	7.9	8.6
38	29	29	22	12	4		7	18	28	43	57

INV
wind
241cm

13.6 13.6
→ 6.6 6.6
53 75
Fe

17.3 11.5 10.7 10.8
2.9 8.7 9.5 9.4
81 64 62 59

15.2	14.8	15.0	15.1	15.5	15.7	15.7	15.8	15.6	15.3	12.3	11.6	10.6	11.6
5.0	5.4	5.2	5.1	4.7	4.5	4.5	4.4	4.6	4.9	7.9	8.6	9.6	8.6
100	74	50	25	12	4		7	18	27	40	57	59	67

17.0
3.2
82

Sta	+	π	-	E/V
-----	---	-------	---	-----

		920.22		
--	--	--------	--	--

102+03				
--------	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

+54				
-----	--	--	--	--

		6.95	913.27	
--	--	------	--------	--

				M H 34' LT
--	--	--	--	------------

✓				
---	--	--	--	--

+84				
-----	--	--	--	--

103+00				
--------	--	--	--	--

✓				
---	--	--	--	--

LT

±

RT

54

14.0	11.38	14.2	15.5	15.63	15.69	15.77	15.66	15.3	17.3	10.6
6.2	8.84	6.0	4.7	4.59	4.53	4.45	4.56	4.9	7.9	9.6
39	29	29	12	4		7	18	27	40	59

INV
2nd
24"CM

14.1	14.0
6.1	6.2
66	75
FC	

16.9	11.4
3.3	8.8
81	67

13.7	13.3	13.7	13.2	15.4	15.6	15.7	15.7	15.6	15.1	12.0	11.0	09.9
6.5	6.9	6.95	7.0	4.8	4.6	4.5	4.5	4.6	5.1	8.2	9.2	10.3
68	49	34	21	12	4		7	18	27	42	55	59

13.9
6.3
75

16.7	10.5	09.6
3.5	9.7	10.6
82	67	64

14.3	14.1	13.8	13.6	12.7	13.0	15.2	15.6	15.6	15.7	15.5	15.0	11.2	09.2	10.6	10.6
5.9	6.1	6.4	6.6	7.5	7.2	5.0	4.6	4.6	4.5	4.7	5.2	9.0	11.0	9.6	3.6
75	70	57	38	28	20	12	4		7	18	28	43	61	72	83

FC

14.9	14.2	12.7	12.5	15.1	15.6	15.6	15.7	15.5	14.9	10.9	08.9	09.9
5.3	6.0	7.5	7.7	5.1	4.61	4.56	4.52	4.69	5.3	9.3	11.3	11.3
51	35	28	21	12	4		7	18	28	44	61	67

15.3
4.9
67

15.7
4.5
75

16.5
3.7
82

Sta + π - E/V.

920.22

103+22 W. edge Ent Lt

✓

+50

BM 2.35 920.10 2.47 917.75 917.75

104+00

✓

104+13

10.46 909.64

104+13

4.80 915.30

- 4.1

911.2 = INV.

Nov 29, 1962

73

55

LT

±

RT

15.4	15.1	11.85	14.6	15.7	15.6	15.6	15.6	15.4	14.8	10.3	08.6	16.2
4.8	5.1	8.37	5.6	5.0	4.7	4.6	4.6	4.8	5.4	9.9	11.6	4.0
38	27	27	22	12	4		7	18	28	45	67	82

INV 15"
SCP
W. end

15.8
4.4
52

16.3
3.7
75

17.1	16.6	15.9	15.6	15.4	15.3	15.6	15.4	15.4	14.5	10.3	08.7	08.4	15.9
3.1	3.7	4.3	4.6	4.6	4.7	4.6	4.6	4.8	5.7	9.9	11.5	11.8	4.3
75	58	35	18	12	4		7	18	28	46	55	67	82

SW Cor. Bolt. on Light Std. 50' LT Sta 104+70

17.06	16.98	15.7	15.5	15.45	15.57	15.55	15.38	14.9	10.1	08.6
2.84	3.12	4.4	4.6	4.65	4.58	4.55	4.72	5.2	10.0	11.5
65	42	27	12	4		7	18	29	48	58

conc conc

17.5
17.5
2.6
75

18.5
18.5
4.3
81

INV. 24" SCP

46' RT

MH

26' LT

Sta + π - E/V.

920.10

104+50

✓

+79

✓

E. edge Ent. Lt.

+91

105+00

✓

Nov 29, 1962 74

LT	#	RT	
17.2	16.4	15.7	15.4
2.9	3.7	4.4	4.7
75	45	12	4

16.1
4.0
82

08.6
11.5
69

16.1	12.99	15.3	15.3	15.2	15.6	15.7	15.5	15.2	08.9	08.8
4.0	7.11	4.8	4.8	4.9	4.5	4.5	4.4	4.6	4.9	11.2
38	24	26	21	13	4	7	18	28	52	69

INV
FIELD
15" SCP

16.6
3.5
55

16.8
3.3
75

15.9
4.2
81

14.4	13.0	13.2	15.3	15.5	15.7	15.8	15.8	15.6	15.2	09.0	08.1	08.4	15.6
5.7	7.1	6.9	4.8	4.6	4.4	4.3	4.3	4.5	4.9	11.1	12.0	11.7	4.5
75	47	28	18	12	4	7	18	28	52	60	69	81	

13.0	13.5	15.3	15.5	15.72	15.78	15.82	15.73	15.6	15.3	08.7
7.1	6.6	4.8	4.6	4.38	4.32	4.28	4.37	4.5	4.8	11.4
49	27	18	16 BT	4			18	24 BT	28	56

13.6
6.5
75

15.7
4.4
81

08.7
11.4
69

Sta

+

π

-

EIV

920.10

105+15

12.57

907.53

+15

✓

+25

+32

7.08

913.02

+39

shoulder Lt.

Nov 29, 1962

75

Lt

+

Rt

57

W. inv 24" SCP Rt. 54'

18.5	15.2	15.5	16.0	16.0	16.0	16.1	16.0	15.8	15.7	11.3	11.1
6.6	4.9	4.6	4.1	4.1	4.1	4.0	4.1	4.3	4.4	8.8	9.0
44	27	23 BT	12	4		7	18	26 BT	29	46	54

13.5
13.3
6.6 6.8
63 75

13.6
11.6
4.5 8.5
82 70

14.0	12.52	13.9	15.2	15.6	16.3	16.25	16.3	16.2	16.0	11.7	13.7	15.7
6.1	2.58	6.2	4.9	4.5	3.8	3.85	3.8	3.9	4.1	8.4	6.4	4.4
75	67	55	37	30 BT	10		7	21 conc	28 BT	50	74	82

inv
W. end
15" SCP

Top C. B. Gate Rt. 54'

17.0	16.7	16.3	16.4	16.6	16.5	16.5	16.3	16.0	15.8	14.9	16.2	16.2
3.1	3.4	3.8	3.7	3.5	3.6	3.6	3.8	4.1	4.3	5.2	3.9	3.9
75	65	57	35 BT	20 conc		7	30 conc	41 BT	47	61	68	81

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		920.10		
--	--	--------	--	--

105+54				
--------	--	--	--	--

--	--	--	--	--

BM				
----	--	--	--	--

	2.35			
--	------	--	--	--

		917.75		
--	--	--------	--	--

			917.75	
--	--	--	--------	--

Nov. 29, 1962

76

58

LT

4

RT

17.80

17.36

17.07

16.79

16.67

16.65

16.60

16.55

16.55

16.63

2.30
160

2.74
120

3.03
82

3.31
41

3.43

3.45
7

3.50
18

3.75
59

3.55
82

3.47
91

No. Rail

18.27

1.83
200

16.11

3.99
200

16.43

3.67
173

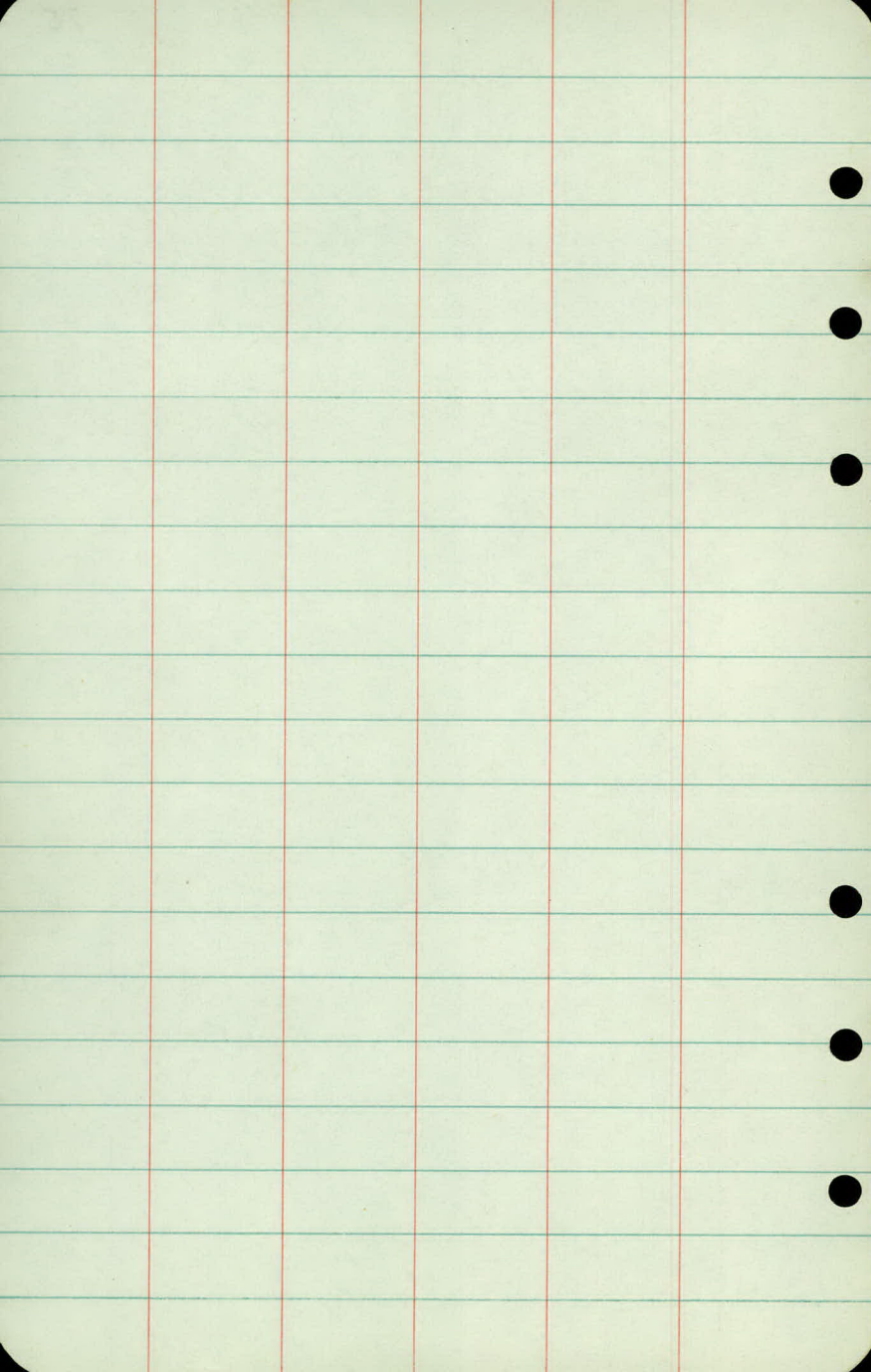
16.53

3.57
130

16.65

3.45
96
So. Rail

SW Cor Bolt on Light Std. 50' Lt std 104+70



Q Rd "C"

X-Sections

sta + π -

B.M 5.62 931.87

926.25

68+68

B.M

4.24 927.63

~~927.63~~
927.71

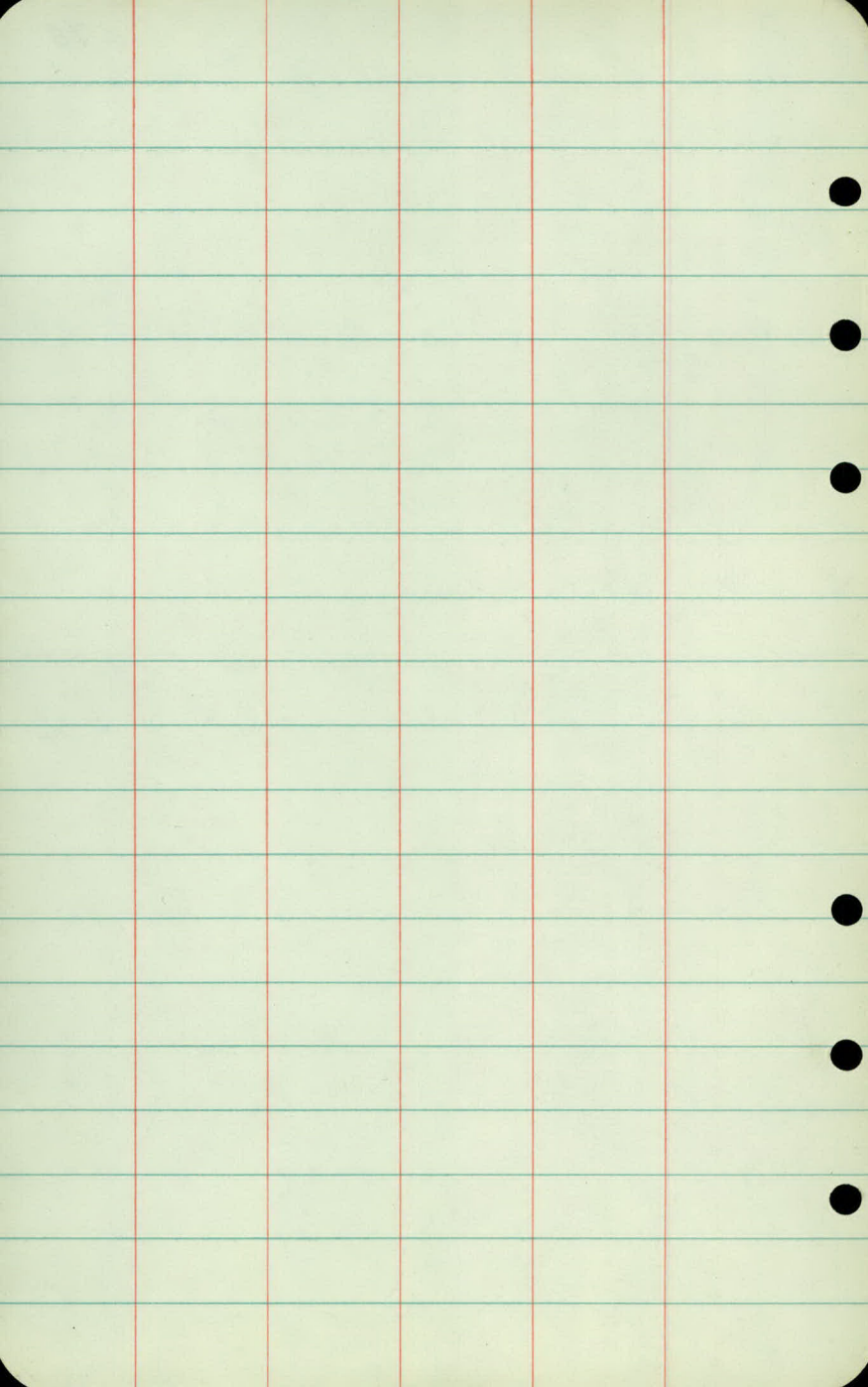
B.M 4.62 930.51

925.89

75+65

4.45 926.06

925.99



KG
WAM
FS
WS

Jan 30, 1963

1° Clear

79

North Rail Elevations

Co. Rd. "C"

(Cleveland to T.H. #51)

Sta	+	π	-	Elev
BM	1.60	924.27		922.67
55+00			2.28	921.99
56+00			1.57	922.70
57+00			0.55	923.72
TP	8.86	932.28	0.85	923.42
58+00			7.30	924.98
59+00			6.25	926.03
60+00			5.04	927.24
61+00			3.95	928.33
62+00			3.36	928.92
63+00			3.51	928.77
TP	4.99	933.43	3.84	928.94
BM			5.13	928.30 (928.30)
64+00			4.85	928.58
65+00			4.85	928.58
66+00			4.55	928.88
67+00 ✓			4.80	928.63
68+00			5.43	928.00
69+00			6.21	927.22

S.W. Cor. Ent. Suburban Vet. Clinic 400' E. of Cleveland

Top North Rail Rt 170' Rt

" "

" " 131' Rt

Top RR Spike

Top No. Rail

" " " 102' Rt

" " "

" " "

89' Rt

" " "

88.5' Rt

" " "

88' Rt

Top R.R. Spike

SW Cor Ent Indianhead Trucking Co.

Top No. Rail 88.5' Rt

" " "

89' Rt

" " "

89' Rt

" " "

89' Rt

" " "

90' Rt

" " "

92' Rt

Sta	+	π	-	Elev	
		<u>933.43</u>			
TP	4.75	931.69	6.49	926.94	
70+00			4.59	927.10	
71+00			4.89	926.80	
72+00			5.20	926.49	
73+00			5.57	926.12	
74+00			5.60	926.09	
75+00 ✓			5.72	925.97	
76+00			5.86	925.83	
77+00			6.18	925.51	
BM	4.52	930.41	5.80	925.89	(925.89)
BM	8.48	927.50	11.39	919.02	(919.02)
78+00			2.61	924.89	
79+00 ✓			3.11	924.39	
80+00			3.57	923.93	
81+00			3.57	923.93	
82+00			3.80	923.70	
83+00			4.09	923.41	
84+00			3.76	923.74	

Top R.R. Spike

Top No. Rail	93' Rt
" " "	94' Rt
" " "	93' Rt
" " "	91' Rt
" " "	91' Rt
" " "	86' Rt
" " "	85' Rt
" " "	86' Rt

Top S.W. Cor. door sill at Barber Shop, Macks Hotel

Spike in PP 33' Lt Sta 83+30

RC
WM
FS
WS
R. Boss

Top No. Rail 89' Rt

Jan 31, 1963
-30 clear

" " "	91' Rt
" " "	88' Rt
" " "	85' Rt
" " "	85.5' Rt
" " "	86' Rt
" " "	86' Rt

Sta	+	π	-	Elev
		927.50		
85+00			3.45	924.05
86+00			3.24	924.26
87+00			3.00	924.50
88+00			2.87	924.63
T.P	8.61	932.85	3.26	924.24
89+00			8.33	924.52
90+00			8.45	924.40
91+00			8.74	924.11
B/M	0.12	927.54	5.45	927.40 927.42
92+00			3.91	923.63
93+00			4.50	923.04
94+00			5.37	922.17
95+00			6.38	921.16
96+00			7.26	920.28
97+00			8.05	919.49
T.P	3.68	922.82	8.40	919.14
98+00			3.92	918.90
99+00			4.36	918.46

Top No. Rail	86' Rt
" " "	87' Rt
" " "	88' Rt
" " "	87.5' Rt

Top R.R. Spike

Top No Rail	87' Rt
" " "	87' Rt
" " "	87' Rt

Spike in P.P. 33' Lt 57 91+50

Top No Rail	87.5' Rt
" " "	88' Rt
" " "	88' Rt
" " "	88' Rt
" " "	88.5' Rt
" " "	89' Rt

Top R.R. spike

Top No Rail	89' Rt
" " "	89' Rt

Sta	+	Δ	-	Elev
		922.82		
100+00			4.67	918.15
101+00			4.94	917.88
102+00			5.18	917.64
103+00			5.49	917.33
104+00			5.93	916.89
105+00			6.17	916.65
105+40±			6.23	916.55
BM			5.08	917.74
				917.75

WM
WS
R. Bass

Jan 31, 1963

83

Top No Rail

" " "

89.5' Rt

" " "

90' Rt

" " "

90' Rt

" " "

90' Rt

" " "

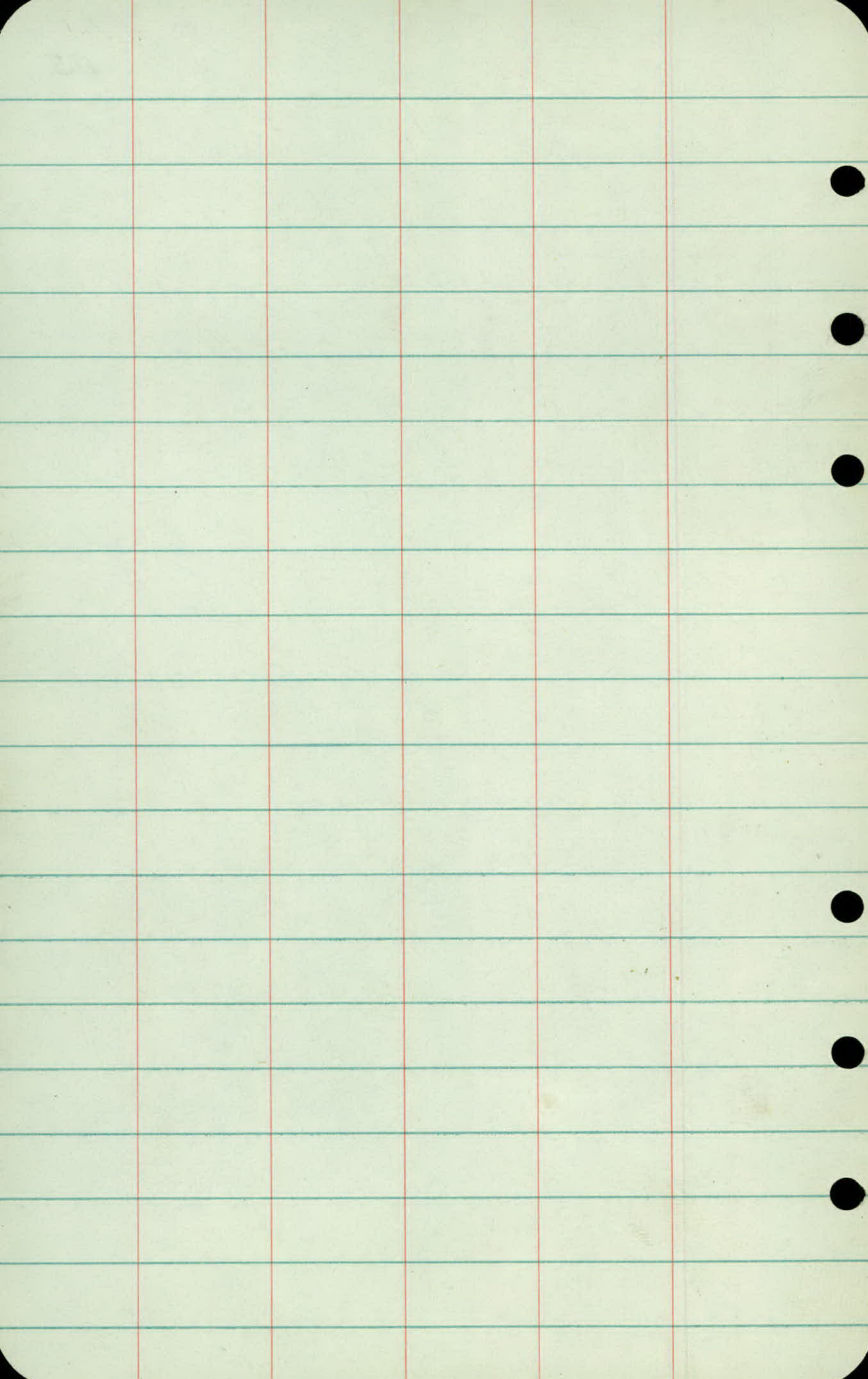
90' Rt

" " "

90' Rt

No Rail & Southbound Lane Snelling Ave

S.W. Cor bolt of light std 50' + stg 104 + 70



Additional

M. H. Elev.

Sta + π - Elev.

BM 5.41 933.71

928.30

59+63

7.70 926.01

63+03

5.69 928.02

62+00

4.90

BM 5.20 931.45

926.25

68+30

4.52 926.93

69+64

No Man hole

70+63

7.44 924.01

70+00

3.98 927.47

FK
KP

Dec. 18, 1962

85

2

S.W. Cor Conc Ent Slab Indianhead office

Top M.H. 17' Lt Casting one Adj Ring

Top M.H. Casting 15' Lt 9" Adj Rings

£ (New)

S.W. Cor. Ent. Walk 1905 W.C. B/C (Brown Trailers)

Top M.H. Casting 17' Lt

Top M.H. Casting 17' Lt

Top M.H. casting 40' Rt

£ New

Az

π at Sta 82+00

23' Rt New π

to Sta 84+00

90°00'

23' Rt New π

Begin
 π Ditch

55°25' 300

π "

51°55' 342'

"

50°— 355

"

45°40' 383

"

36°30' 455

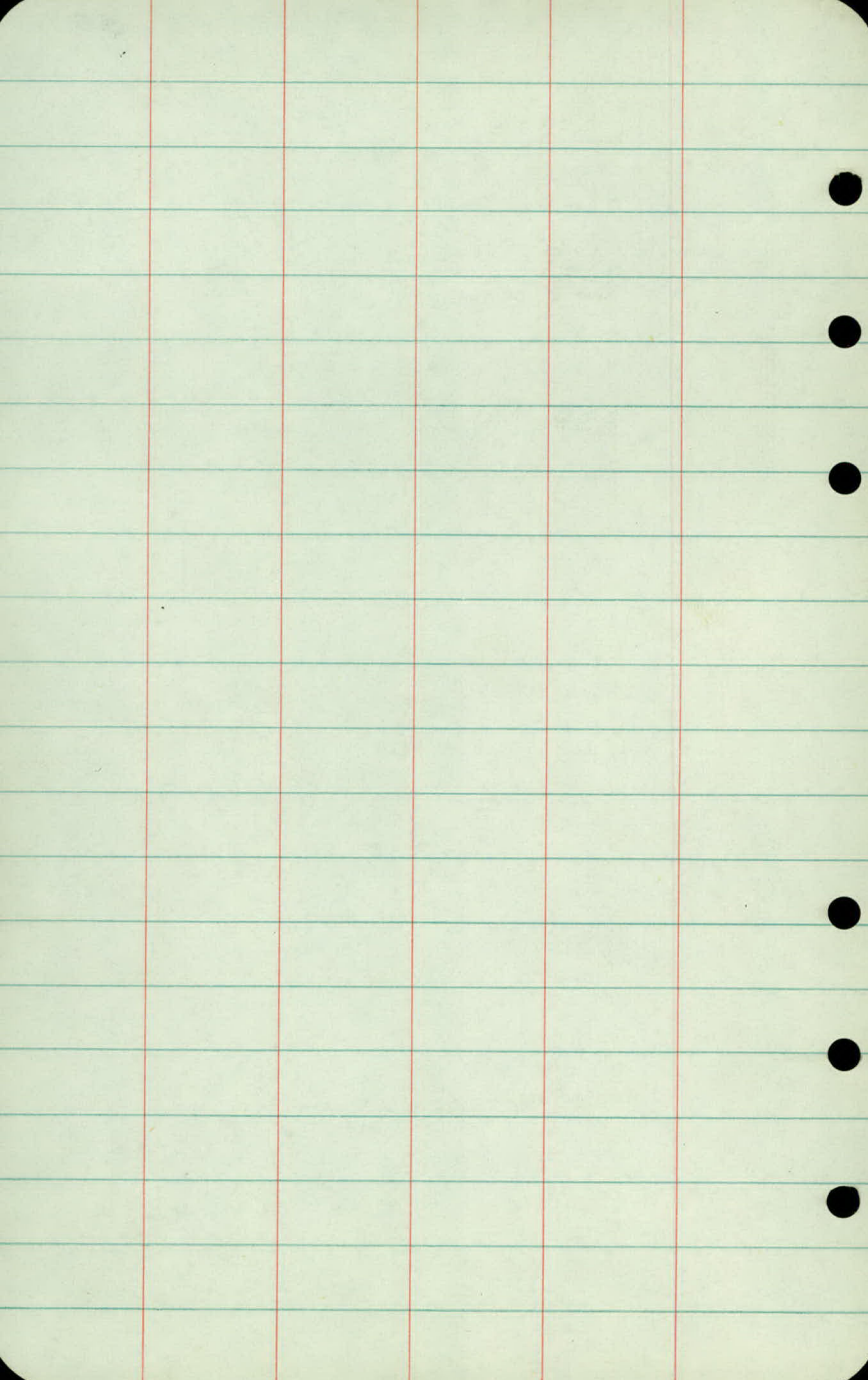
"

29°— 556

Dec. 18, 1962

86 3

279



sfg + π -

B. M. 5.39 931.64

926.25

68+32 14' Lt NEW 4.69

70+63 40' Rt New 7.60

70+71 16' Lt NEW 4.99

B. M. 3.96 924.68 924.71

81+54

Lt

£

Rt

Ent slab S.W. Cor Brown Trailer #1965

10.8 To Flo Line
to Casting

5' Concentric Cone

2 Adjusting Rings

1 Foot Casting
Flow From S to M.
at Sta 70+71

13.8 Flo Line to casting

5' concentric Cone

2 Adjusting Rings

1' Casting

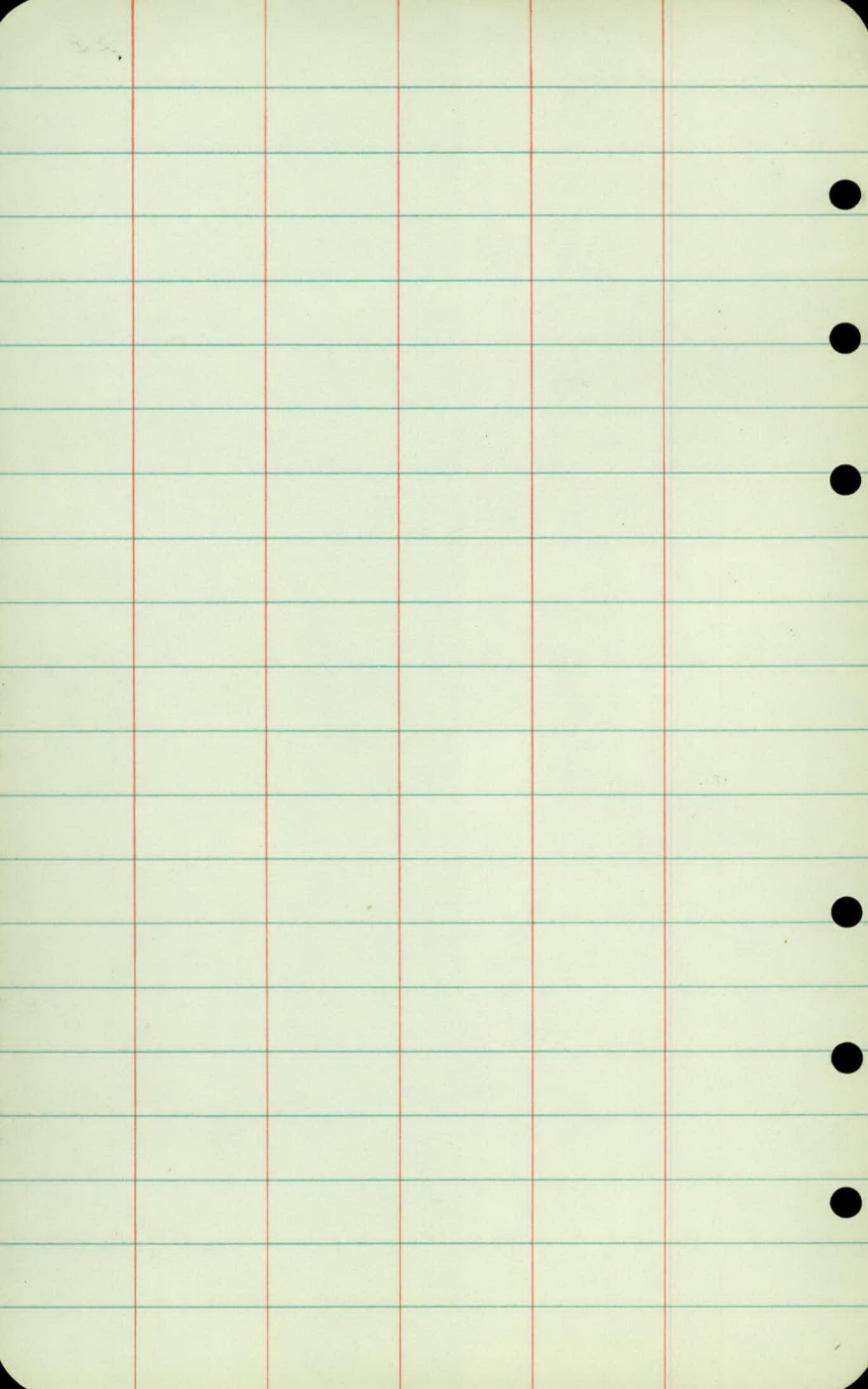
Flows From W. to E
Inlet From S.

£ Sta 69+00 Old £

4' Diameter at Base

2.3 Diameter at Top

All Brick Const.



MHD

$$10 + 00 = \frac{1}{2} \text{ Cleveland } \dot{e} C$$

$$\frac{5 + 89}{411} = \text{END OF Const.}$$

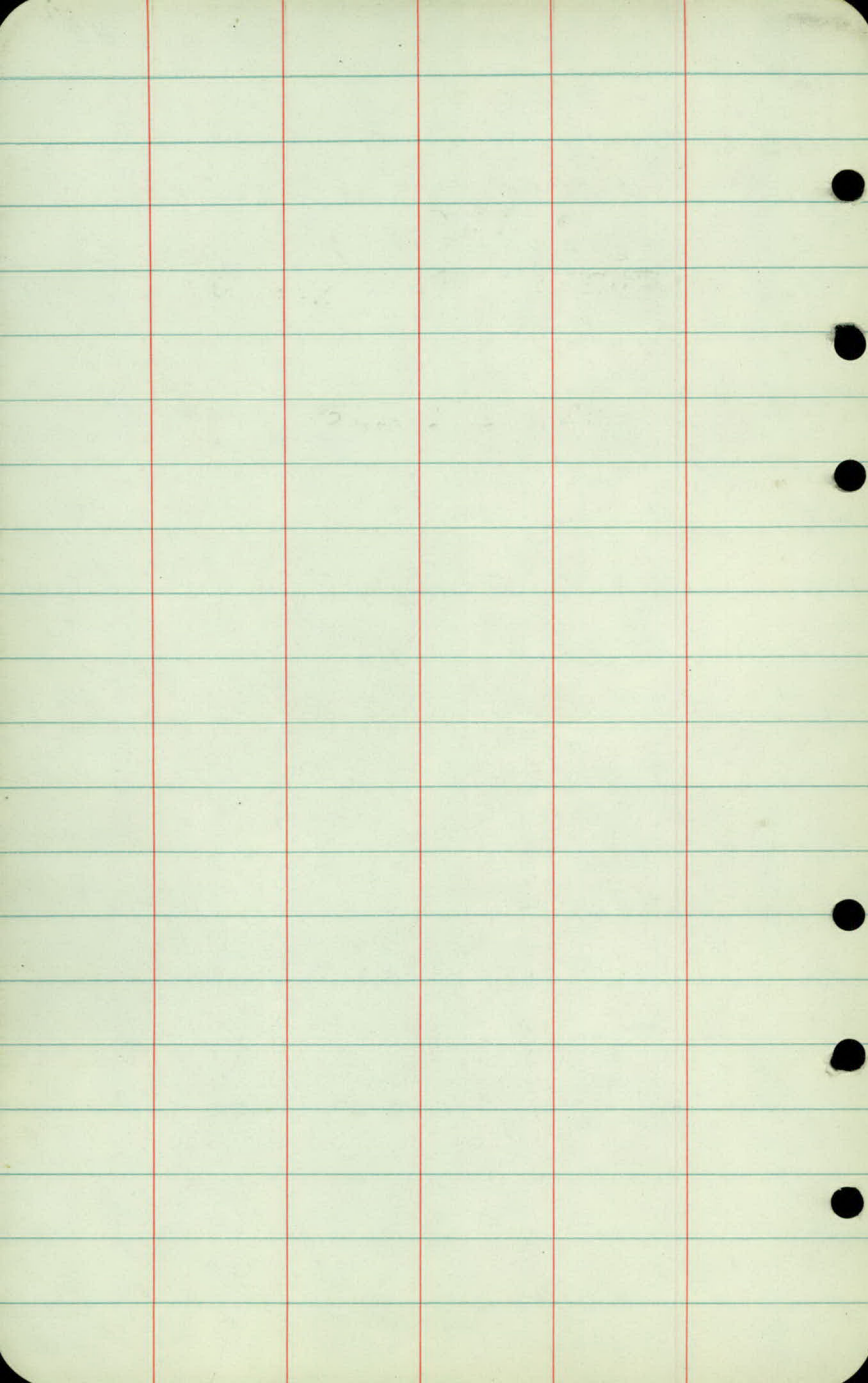
411

R.C.

$$53 + 02.60 = \frac{1}{2} \text{ Cleveland } \dot{e} C$$

$$57 + 13.60 = \text{END OF STD Const}$$

Rec'd. 12-3-62



RG
DS
WS

Nov. 27, 1962 90
PC. Windy 45°
IF

X-Sections

Fairview Ave

0+00 = 300' So. of Existing & Co Rd "C".

6 pages (F)

Sta	+	π	-	Elev.
BM	3.54	929.43		925.89

1+00

✓

+50

+65

6.44 922.99

2+00

+10

+13

So. Rail of RR X-Sing

Lt. & Rt

Top West door sill Barber Shop Mack Hotel Fairview

18.6	21.5	24.0	24.7	24.9	24.8	24.3	23.7	24.2
10.8	7.9	5.4	4.7	4.5	4.4	5.1	5.7	5.2
56	29	16	10		10	19	20-24	30
16.8							24.7	24.8
12.6							4.7	4.6
75							75	50

23.0	23.1	23.1	23.1	23.7	24.3	24.5	24.4	23.7	24.1	21.2	19.6
6.4	6.3	6.3	6.3	5.7	5.1	4.9	5.0	5.7	7.3	8.2	9.8
75	60	33	20	18	10		10	16	32	53	75

Rim Mt 23' Lt

22.0	22.2	20.3	23.9	24.0	24.3	24.0	23.6	19.4	21.4	21.0	21.1
6.9	7.2	9.11	5.5	5.4	5.1	5.4	5.8	10.02	8.0	8.4	8.3
75	39	20	17	9		11	20	23	26	45	70
		FL					FL				
		15" CM					15" CM				

23.6	23.7	23.7	24.1	24.2	24.1	24.0	23.3	23.4
5.8	5.7	5.7	5.3	5.2	5.3	5.4	6.1	6.0
75	46	26	9		11	17	46	75

24.13	24.32	24.22	24.10	24.09	23.88	23.86	23.85	23.77
5.00	5.11	5.21	5.33	5.34	5.55	5.59	5.61	5.66
100	75	50	25		25	50	75	100

Sta	+	π	-	Elev
		929.43		
2+18	No. Rail			
+29				
+43				
+53				
+80				
+89	Edge Conc			
TP	5.65	929.60 929.61	5.48	923.95

Nov 27, 1962 92

24.51	24.40	24.29	24.20	24.14	23.99	23.90	23.85	23.84
4.92	5.03	5.14	5.23	5.29	5.44	5.53	5.58	5.59
100	75	50	25	25	50	75	100	

23.1	23.0	22.9	22.2	22.2	22.14	22.1	22.7	22.9
6.3	6.4	6.1	5.2	5.2	5.0	5.3	6.0	6.7
75	60	33	15	11	17	35	60	75

21.0	21.3	21.6	21.9	21.0	21.4	21.2	21.0	20.7
8.4	8.1	7.8	5.5	5.4	5.0	5.2	6.4	7.5
75	54	32	17	13	18	26	42	61

21.5	21.4	21.33	21.5	21.8	21.4	21.1	21.0	20.4
7.9	8.0	8.10	5.9	5.6	5.0	5.3	6.5	8.3
75	61	34	21	17	18	29	47	68

Top Grate

23.9	23.6	24.1	24.3	24.0	23.6	23.5	23.5
5.5	5.8	5.3	5.1	5.4	5.8	5.9	5.9
75	55	22	20	46	66	75	

24.20	24.14	24.01	23.97	24.27	24.20	23.94	23.80	23.74
5.23	5.29	5.44	5.46	5.16	5.23	5.49	5.63	5.69
75	65	45	25	19	41	60	75	

No. Rim MH SE Cor. Int. Fairview & "C"

Sta	+	π	-	Elev.	
		929.60			
		929.61			
BM			4.23	925.37	<u>925.37</u>
				925.38	
BM	4.23	929.60			925.37
0+00					
✓					
0+25					
0+44					
0+70					
BM			4.23	925.37	✓

£

 $4F$

265.5' So. of Proposed E of "C"

" 27 14

265.5' So. of Proposed E of "C"

0.6	1.6	3.6	4.6	4.0	3.5	3.4	3.9	3.7	4.0	3.8	3.2
65	44	27	26	19	10	1	14	16	23	34	49

$\frac{1}{2}$	$\frac{1}{3}$	$\frac{1}{4}$	$\frac{1}{5}$	$\frac{1}{6}$	$\frac{1}{7}$	$\frac{1}{8}$	$\frac{1}{9}$	$\frac{1}{10}$
2.3	2.4							
72	66							
40								

0.4	1.0	2.1	3.6	4.7	4.0	3/8	4.4	4.2	4.9	4.8	4.7	4.7
76	61	44	31	23	12	1	15	16	23	32	50	75

2.0	2.3	2.7	3.7	5.1	4.3	4.3	4.1	4.8	6.2	11.0	12.0	12.8
80	70	58	34	20	15			15	23	42	62	75

3.3	4.1	4.4	5.5	4.6	4.4	5.2	9.7	11.9	12.7	13.3
75	54	31	21	10		15	32	49	66	75

Above BM

Sta	+	π	-	Elev.
BM	2.31	928.20		925.89

3+07 Prop. & Co. Rd "C"

✓

+57

4+00

+50

5+00

Lt

±

Rt

Top West end door sill of Barber shop Mack Hotel

24.86	24.64	24.37	24.14	24.10	24.19	24.10	23.92	23.92	23.71	23.53
3.34	3.56	3.88	4.06	4.10	4.01	4.10	4.28	4.38	4.49	4.67
125	100	75	50	25		25	50	75	100	125

24.88	24.93	25.02								
3.32	3.27	3.18								
150	175	200								

24.0	23.7	23.5	23.1	23.9	24.1	23.5	23.8	23.6	24.3
4.2	4.5	4.7	5.1	4.3	4.1	4.7	5.4	4.6	3.9
75	65	38	24	15		21	31	46	75

25.21	24.6	23.9	23.6	23.3	24.0	24.1	23.7	23.0	23.6	23.9
2.99	3.6	4.3	4.6	4.9	4.2	4.1	4.5	5.2	4.6	4.3
86	86	69	45	24	10		12	29	58	75

Comp. S.W.

24.5	24.1	23.7	23.3	23.9	24.1	23.8	23.0	23.0	23.7	23.9
3.7	4.1	4.7	4.9	4.3	4.1	4.4	6.2	6.2	7.0	7.3
75	61	45	22	10		10	27	45	66	77

23.5	23.0	23.0	22.6	22.8	23.9	23.7	23.7	23.0	17.1	18.3	18.1
4.7	5.2	5.2	5.6	4.4	4.3	4.5	5.0	7.8	10.5	9.9	9.5
75	50	31	22	10		10	20	25	38	59	75

Sta	+	π	-	Elev
-----	---	-------	---	------

		928.20		
--	--	--------	--	--

5+33				
------	--	--	--	--

✓				
---	--	--	--	--

+57				
-----	--	--	--	--

	12.22	915.98		
--	-------	--------	--	--

+57				
-----	--	--	--	--

+57				
-----	--	--	--	--

	7.57	920.63		
--	------	--------	--	--

6+00				
------	--	--	--	--

BM				
----	--	--	--	--

	2.85	925.35	(925.37)	
--	------	--------	----------	--

Nov 28, 1962

95

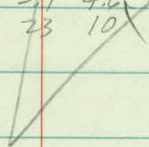
6F

Lt

±

Rt

22.9	22.8	22.8	22.6	23.8	23.5	22.8	19.3	15.7	15.7
5.3	5.4	5.4	5.7	4.6	4.4	4.7	5.4	8.9	12.5
64	44	30	23	10		10	20	28	41

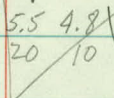


22.8
5.4
75

17.4
17.2
10.8
11.0
75
54

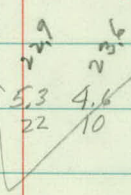
Inv 12" SCP Rt 30'

22.8	22.7	22.7	21.4	22.7	23.4	23.7	23.4	22.8	16.6	15.4	16.3
5.4	5.5	5.5	6.8	5.5	4.8	4.5	4.8	5.4	11.7	12.8	11.9
75	55	39	24	20	10		10	20	37	65	75

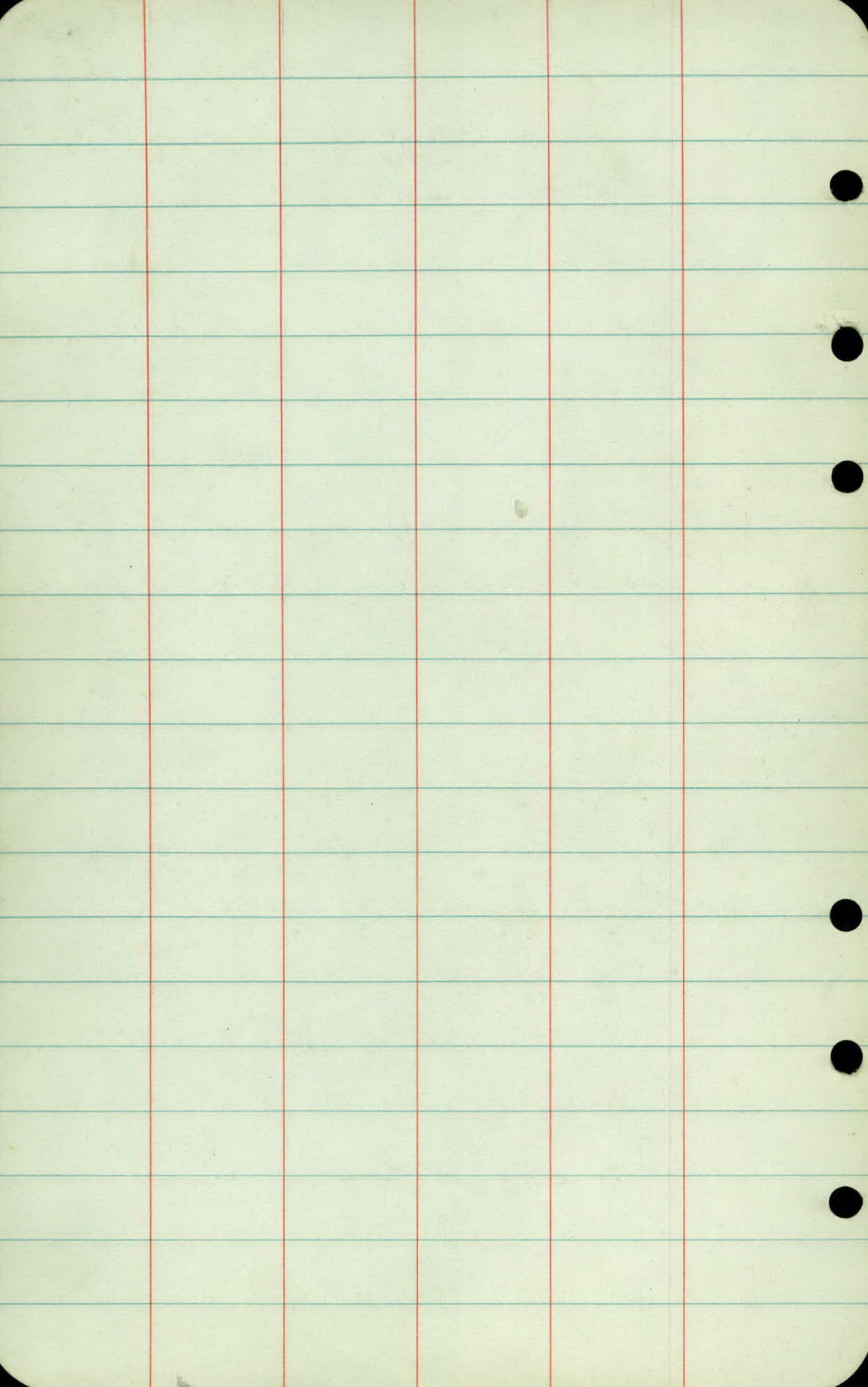


Inv 12" SCP Lt 23'

22.8	22.7	22.8	22.9	23.6	22.7	23.4	22.9	17.6	17.5	16.9
5.4	5.5	5.4	5.3	4.6	4.5	4.8	5.3	10.6	10.7	11.3
75	62	39	22	10		10	18	35	53	75



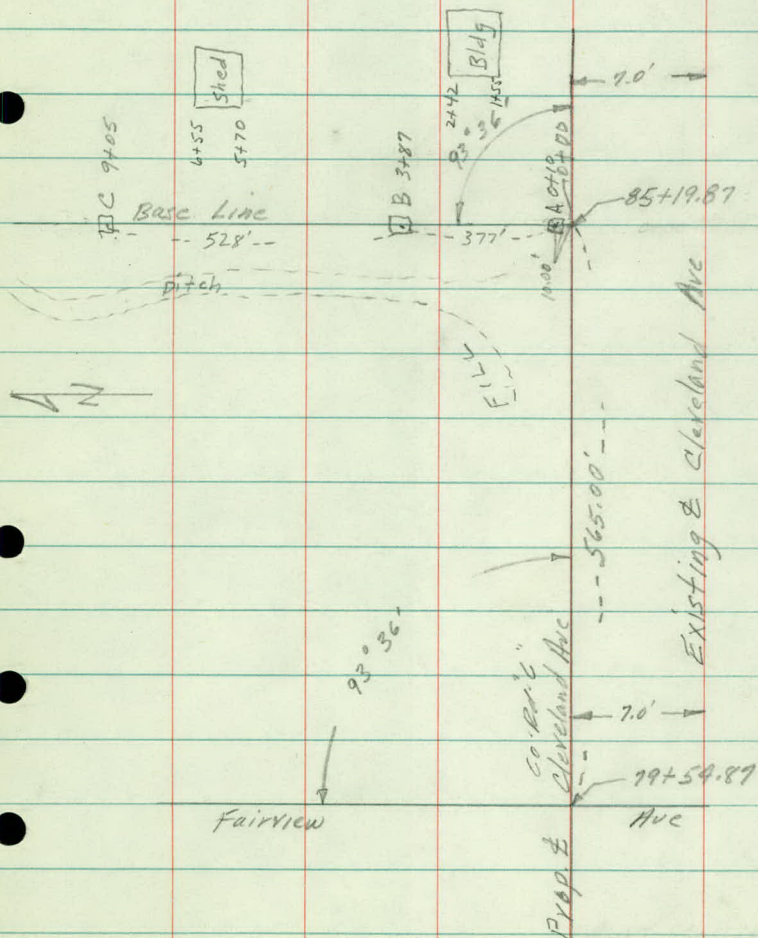
Top Mont on Fairview 265.5 So. of Prop. ± of "C"



Jan 17, 1963
Cold, Snowing 0° 96

Ditch Location by Stadia and X-Sections

565' E. of Fairview = 0+00



OBJECT

AZ.

STADIA

π at 0+00 (565.0' E. of Fairview [Sta 84+19.87 C.P. (C)])

To Sta 92 ("C")

93°36'

To Base Line

0°00'

To $\square A$ (0+10)

0°00'

To $\square A$

H. I. = 929.70

to 0+00

180°00'

to Base Line

0°00'

to $\square B$

0°00'

377'

Not Visible
from $\square A$

to Sta 85+00 ("C") PK nail - old $\square$

Top
Edge Fil

286°20' 250'

"

298°35' 200'

"

311°45' 218'

"

328°20' 193'

"

337°30' 209'

"

344°25' 230'

"

347°25' 280'

$\square$ Ditch

336°10' 155'

"

348°30' 189'

Jan 17, 1963 97
100° Snowing
DIFF. ELEV. 2

RG
WM 2 AM
WS
RG
JS
WM
WS
DJ } PM

VERT. ROD
EQUIV. ROD

10.00'

Elev. from
X-sections 924.43

5.3

5.30

924.40

-

15.05

-15.05

14.65

199

-3°05'

-10.8

5.3

-16.1

13.6

-2°50'

-8.2

5.3

-13.5

16.2

-3°06'

-10.5

5.3

-15.8

13.9

-3°20'

-12.3

5.3

-17.6

12.1

-2°45'

-11.0

5.3

-16.3

13.4

-

15.2

-15.2

14.5

-5°30'

-15.0

5.3

-18.3

911.4

-4°32'

-14.9

5.3

-18.2

911.5

OBJECT

H.I. = 929.70

AZI

STADIA

± Ditch	353°10'	265'
"	355°40'	355'
"	356°40'	438'
"	357°20'	530'

A + B C

H.I. 917.1

to B	180°00'	518'
± Ditch	183°30'	465'
"	185°00'	314'
"	188°00'	231'
"	194°05'	148'
"	221°20'	62'
"	309°20'	61'
"	333°30'	117'

End Ditch 329°00' 155'

Edge Swamp S. 350°15' 115'

" " N. 350°15' 174'

" " S. 14°45' 171'

" " N. 41°46' 234'

Jan 17, 1963 98
ELEV. 3

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
	-3°15'	-14.7	5.3	-20.0	909.7.
	-2°30'	-15.8	5.3	-21.1	908.6.
	-2°00'	-15.7	5.3	-21.0	908.7.
	-1°39'	-15.8	5.3	-21.1	908.6.
			5.25	Elev of El B on X-Section Notes	919.92
	0°00'		9.0		908.7. 916.2.
	-		9.1		08.6.
	-		9.3		08.4.
	-		9.3		08.4.
	-		9.4		08.3.
	-		9.8		07.9.
	-		10.0		07.7.
	-		9.9		07.8.
	-		10.2		07.5.
	-		10.7		07.0.
	-		9.9		07.8.
	-		10.6		07.1.

Object	917.7	Az.	Stadia
--------	-------	-----	--------

Edge Swamp S.		33°10'	228'
---------------	--	--------	------

" " N		26°00'	255'
-------	--	--------	------

" " S.		39°10'	274'
--------	--	--------	------

" " N		31°20'	275'
-------	--	--------	------

Note i Swamp Cont. in Easterly
Direction

Jan 17, 1963 994

Dist	Virt Angle	Rod Equiv	Rod	D. ff	Elev
	-		9.7		08.0.
	-		10.4		07.3.
	-		10.6		07.1.
	-		10.6		07.1.

Sta	+	π	-	EIV
TBM	10.25	929.27		919.02
E14			4.84	24.43

1+55

✓

✓

2+42

✓

✓

R6
JS
WM
DJ
WS

LT

~~LT~~

Jan 17, 1963
Cold
ET

1005

Spike in TP LT Sta 83+30

ET = 0+10
LB = 3+57
WR = 9+45 1+55

0+10

2+42
5+70
6+55

09.6	12.6	14.3	17.0	25.0	25.7	28.0
19.7	16.7	15.0	12.3	4.3	3.6	1.3
56	50	29	15	4		19
						Bldg.

07.7	10.0	09.6	09.6
21.6	19.3	19.7	19.7
56-62	64	88	100

15.4	14.8	11.3	13.3	09.7
13.9	14.5	18.0	16.0	19.6
186	169	154	134	122

07.3	10.3	14.0	14.9	17.1	25.5	27.6	28.0
22.0	19.0	15.3	14.4	12.2	3.8	1.7	1.3
32-37	31	24	20	14		7	19
							Bldg.

11.7	15.4	11.3	10.9	13.1
17.6	13.9	18.0	18.4	16.2
38	44	52	57	62

13.3	14.9	13.6
16.0	14.4	15.7
124	100	77

Sta + π - EIV

929.27

TP 13.67 929.17 13.77 915.50

□ B 9.25 919.92

5+70 So. side of shed

✓

✓

6+55 No. side of shed

✓

□ C

4.58 924.59

Lt

E

Jan 17, 1963
RT 101 6

Rock

3+87 E

10.8

08.4

11.1

11.8

14.2

21.2

26.3

27.0

18.4

20.8

18.1

19.4

15.0

8.0

2.9

2.2

32

23-30

20

14

11

19

31

Bldg.

14.3

10.5

09.4

18.8

14.9

18.7

19.8

10.4

38

46

60

81

19.2

19.2

10.0

10.0

150

100

K

14.1

10.1

08.1

10.6

13.1

15.6

21.2

25.1

24.9

15.1

19.1

21.1

18.6

16.1

13.6

8.0

4.1

4.3

41.43

37

29.36

26

9

11

17

32

Bldg

10.4

09.4

16.2

17.3

17.8

18.8

19.8

13.0

11.9

11.4

49

68

69

100

150

9+05 E

Sta

+

π

-

E/V.

929.17

TBM

10.15

919.02

919.02

Jan 17, 1963

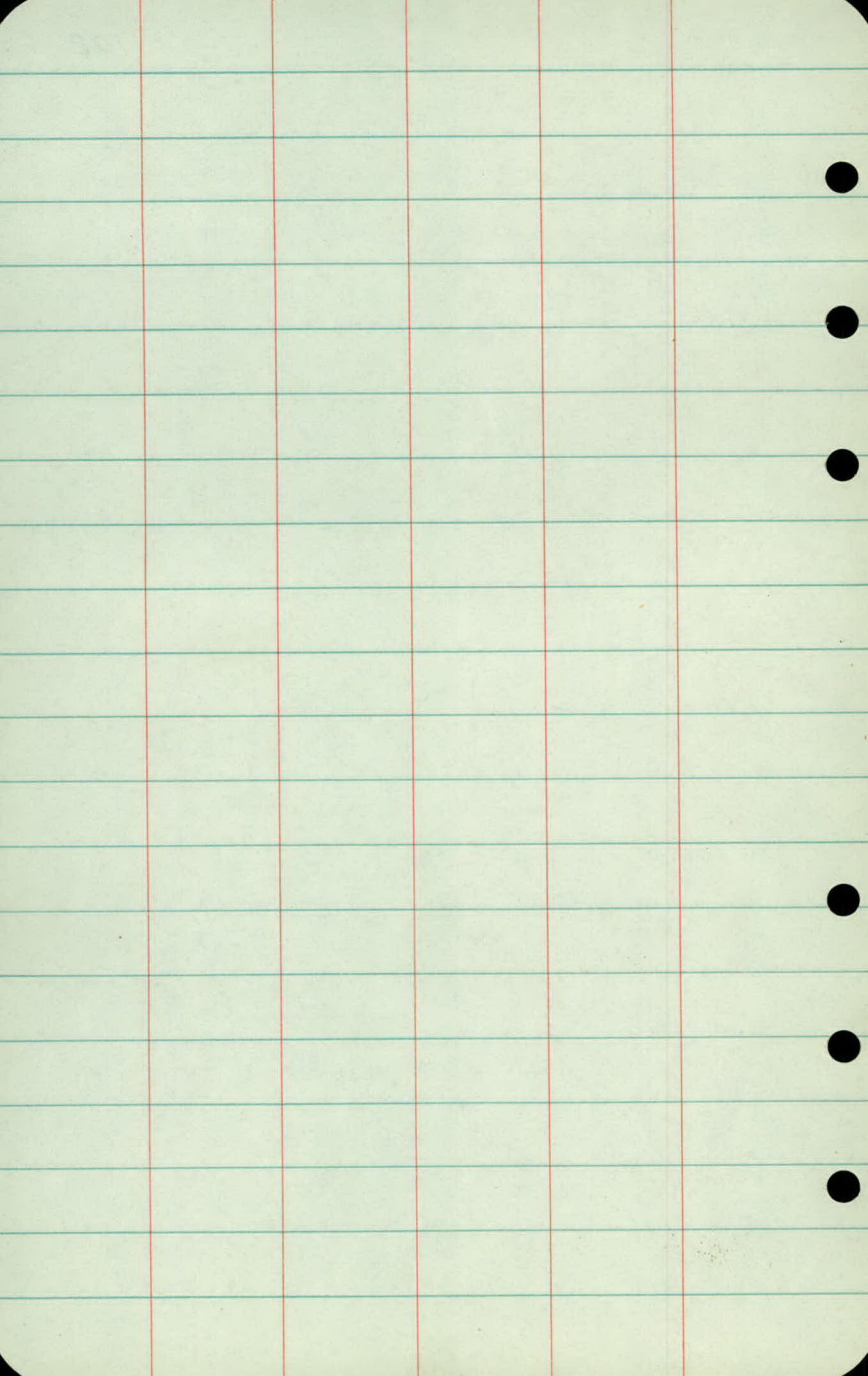
Lt.

E

Rt.

1027

Spike in PP Lt Sta 83 +



KP
WM
R. Boss

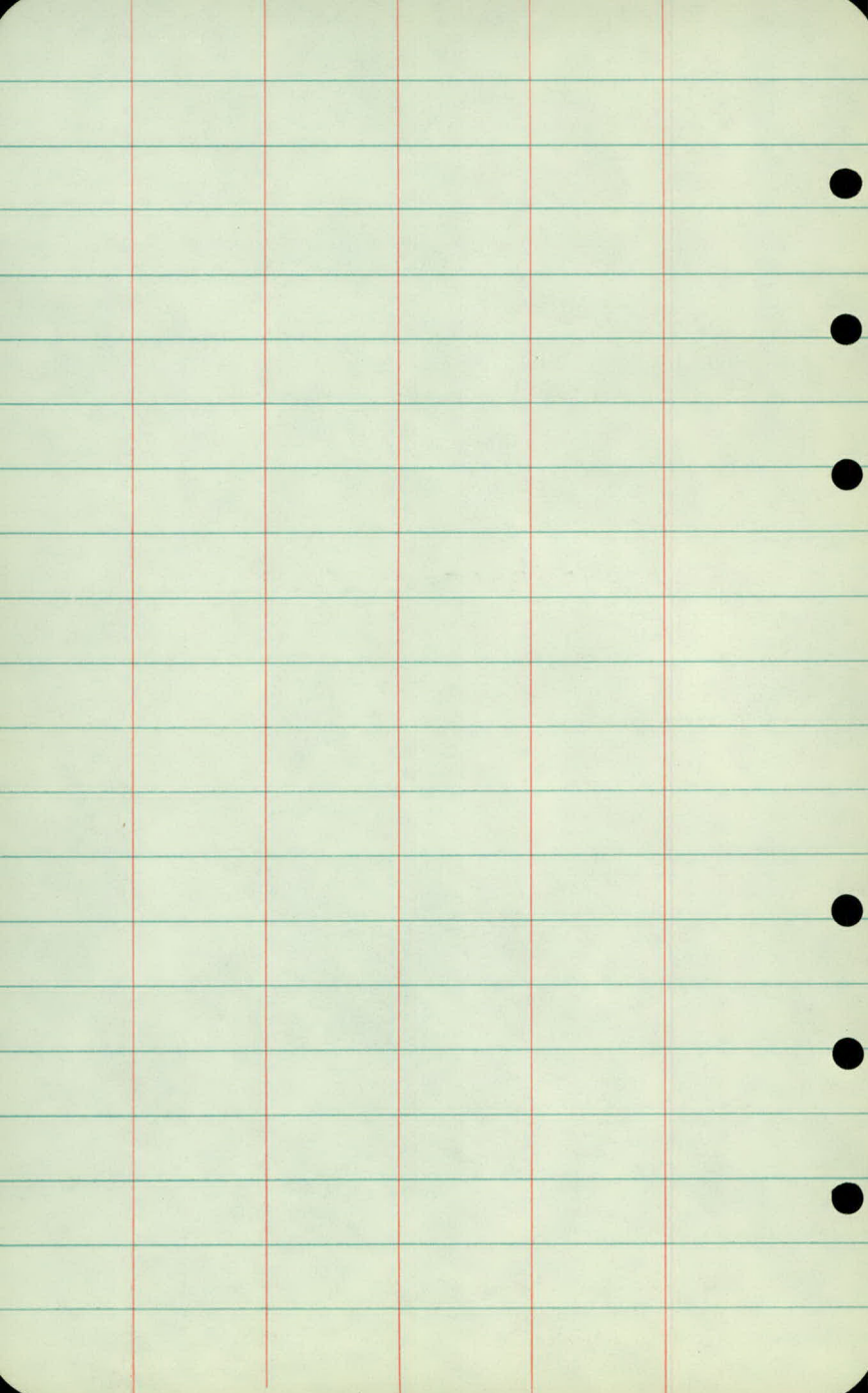
13 FEB. 1963

1.
103

Co. RD. C
CLEVELAND TO SNELLING

MH INFORMATION

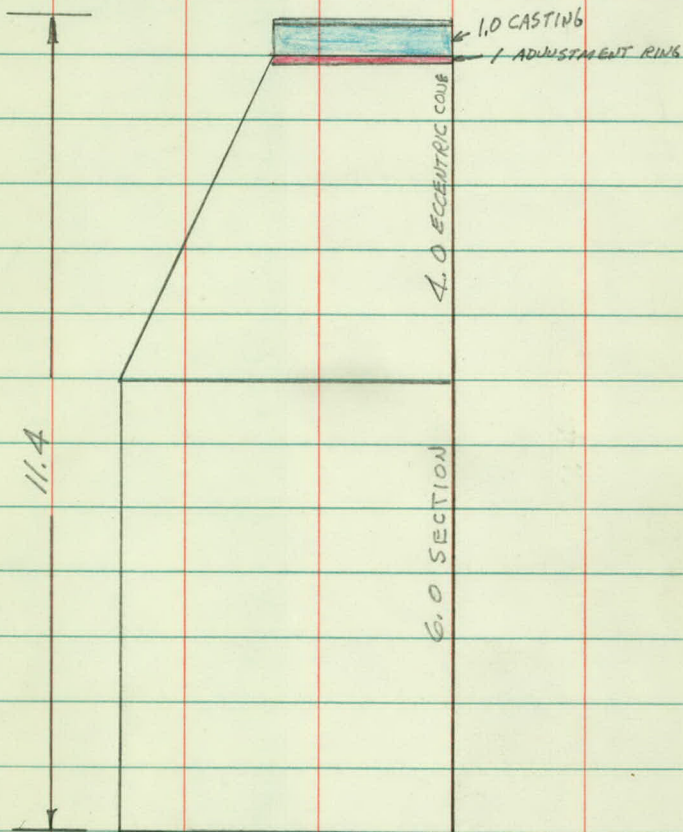
5 PAGES

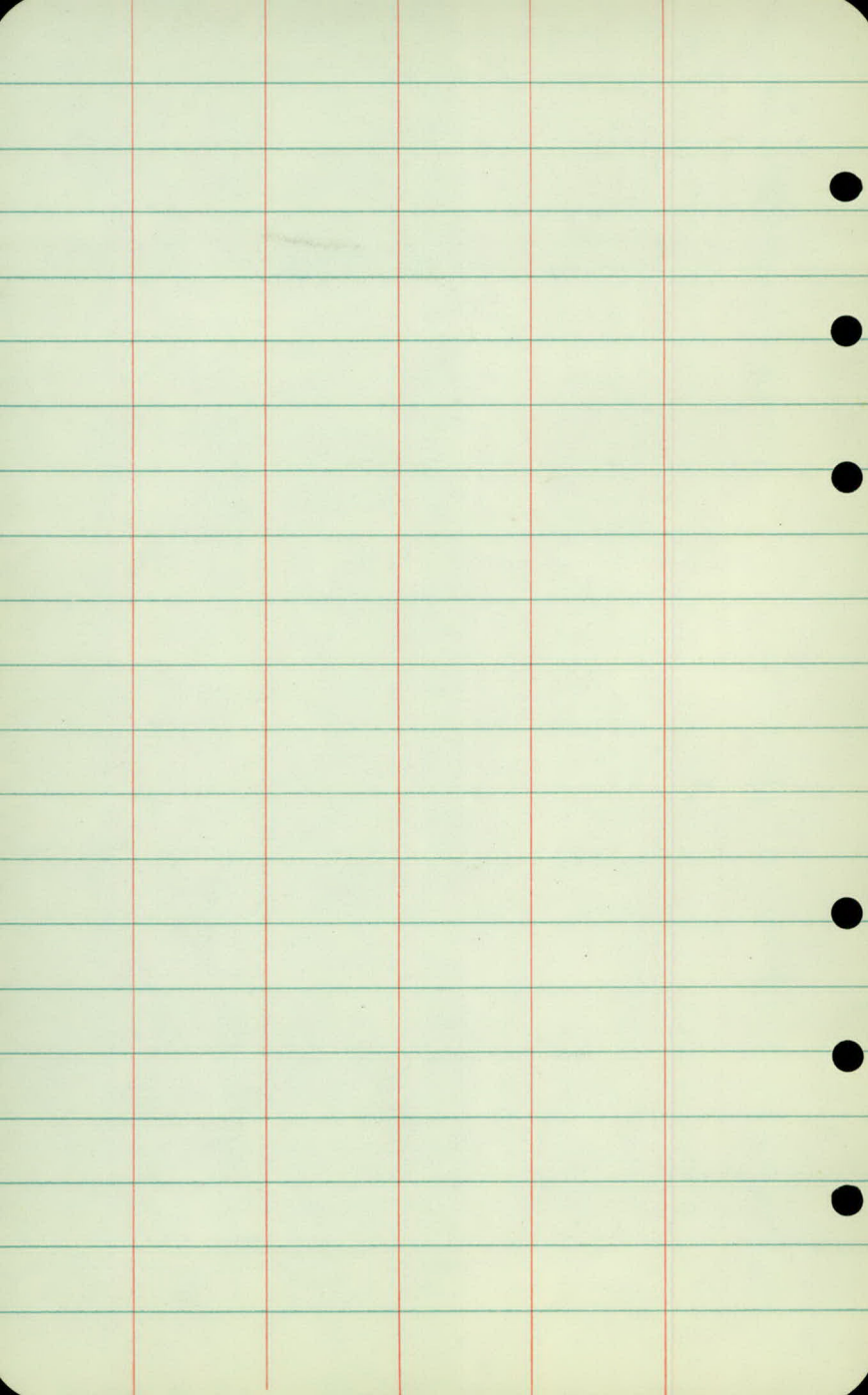


$$59 + 63$$

17.0 LT

2.
104

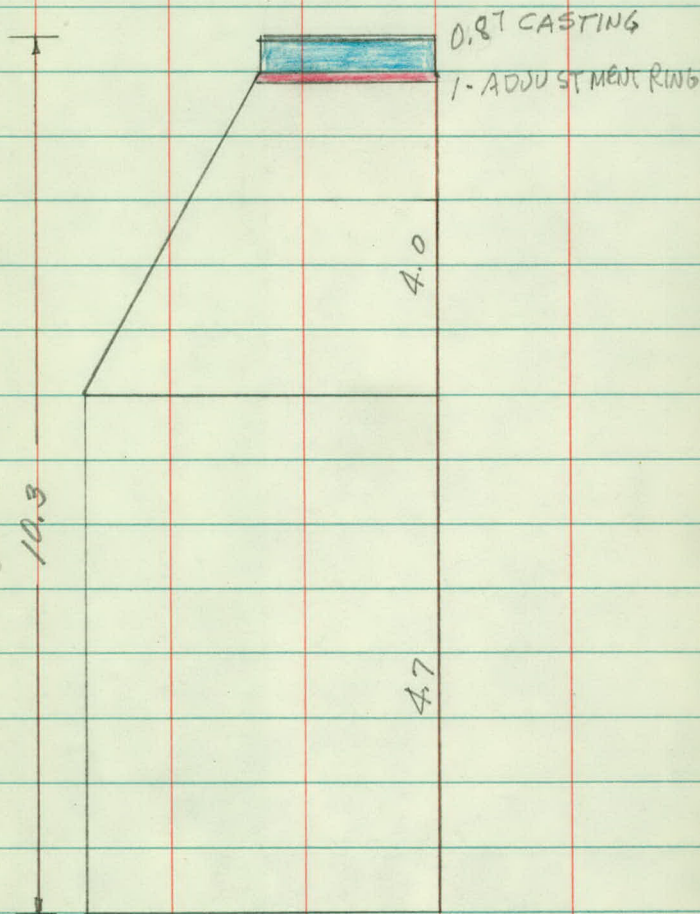


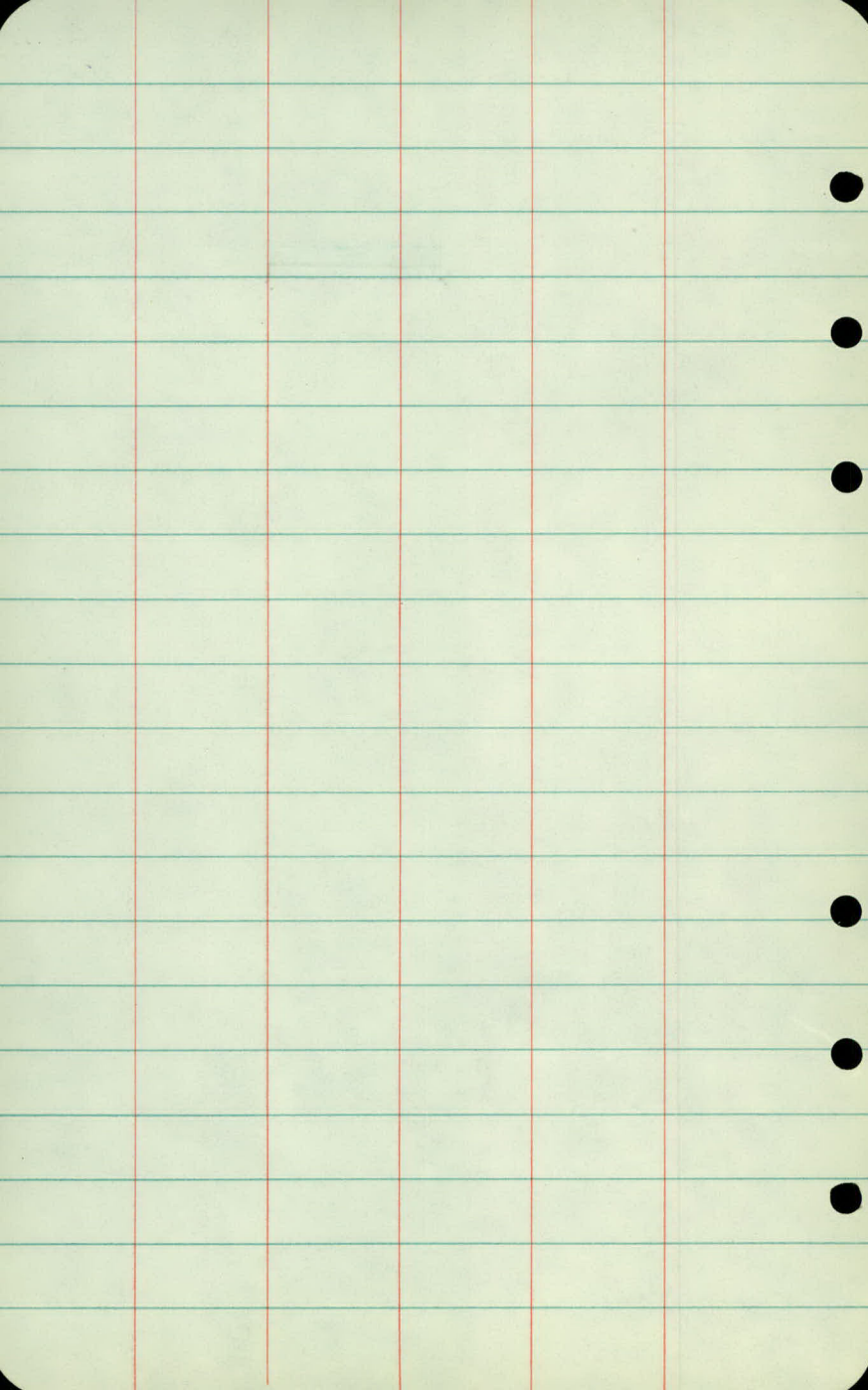


66+17

15.0 LT

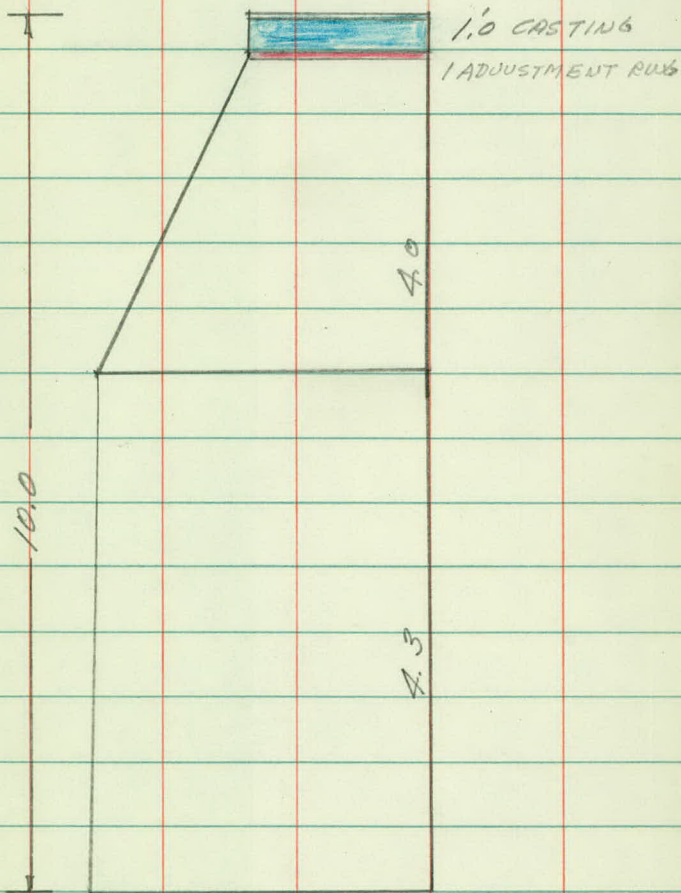
3.
105

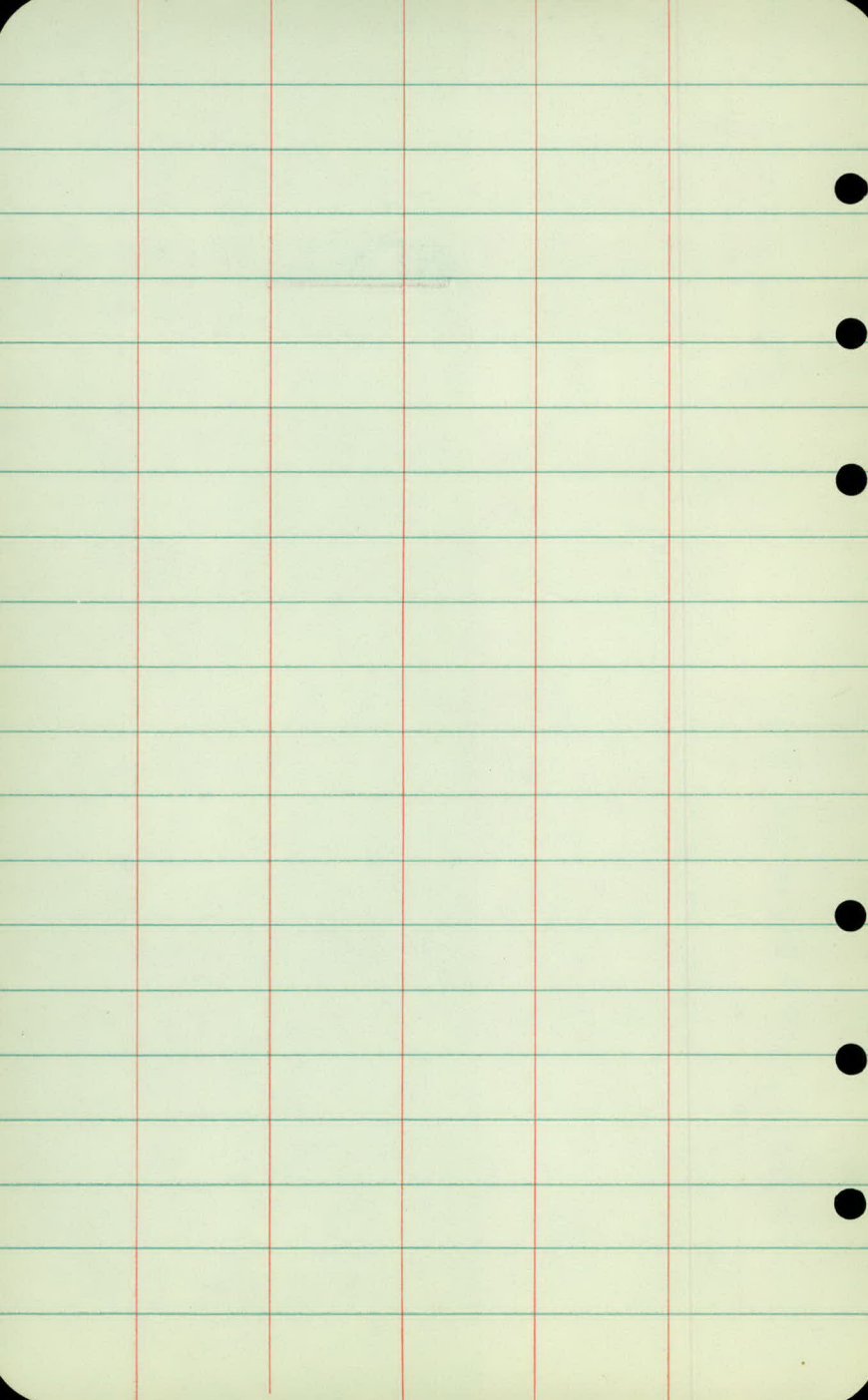




68+32
14.0 LT

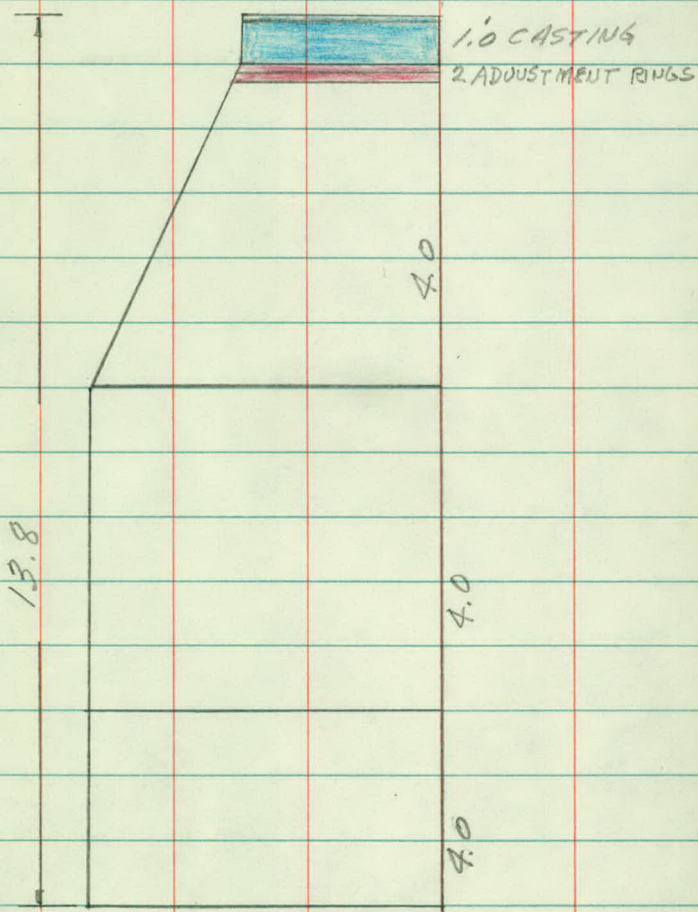
4.
10.6

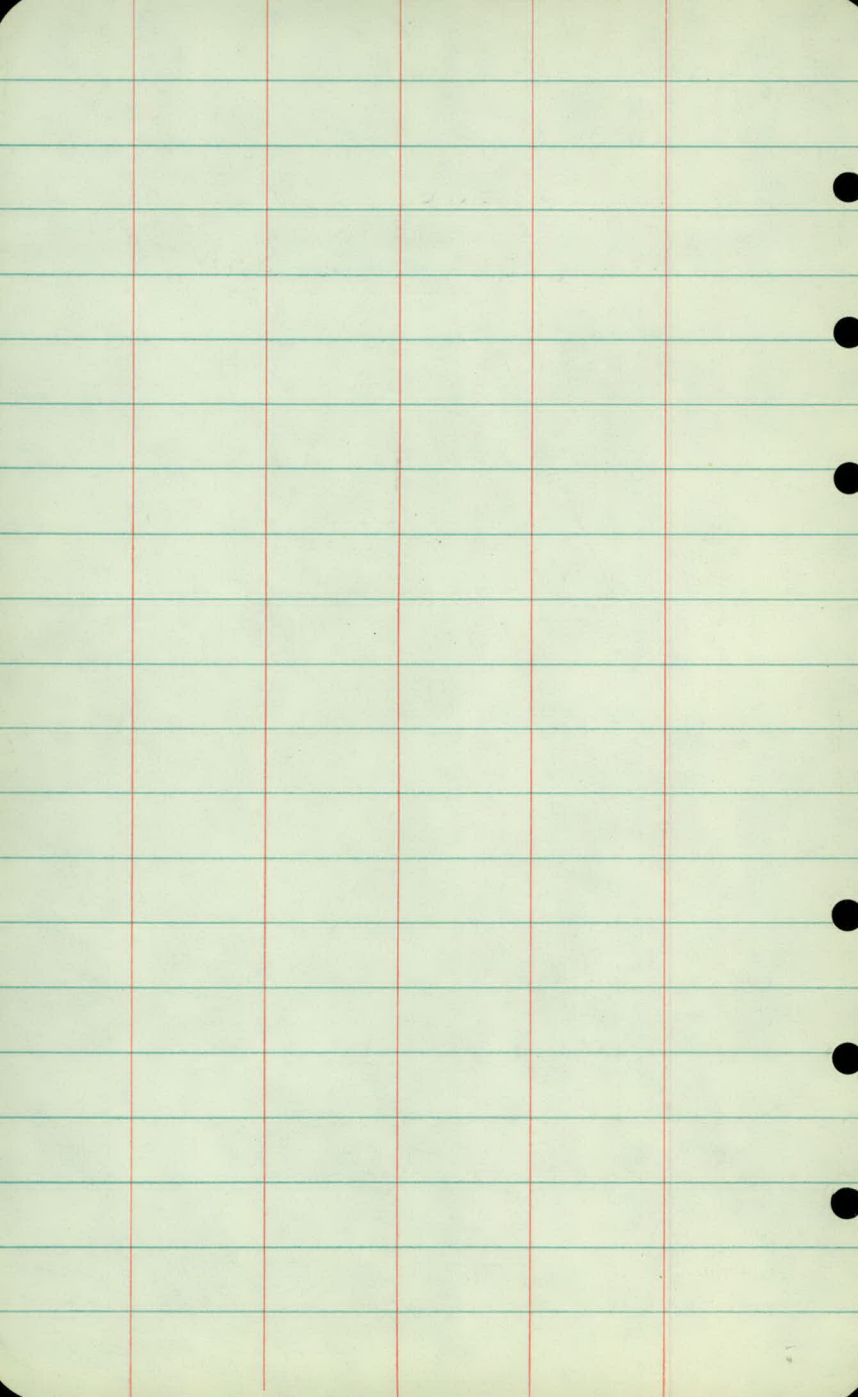




70 + 71.5
15.5 LT

5.
107





Co. Rd. "C"

Cleveland to Snelling

Alinement

5-Pages

Reid
1/8/63

Sta	Point	ΔLt	ΔRt	
61+85.25	P.T.	5°33'		P.I. = 59+35.20
+50		5°09.7'		$\Delta = 11°06'$
61		4°36.5'		$\frac{1}{2}\Delta = 5°33'$
+50		4°03.3'		$D = 2°12'45''$
60		3°30.1'		$T = 251.64$
+50		2°56.9'		$L = 501.69$
59		2°23.7'		$R = 2589.68$
+50		1°50.5'		
58		1°17.3'		
+50		0°44.1'		
57		0°10.9'		
56+83.56	P.C.	0°00'		

53+03.85 $\pm$ Cleveland

FK
WM
DS
R Boss

Dec. 28, 1962
Clear 18°

A2

Fe^m
Post 78.74

156.68

14" Oak
Disk

T=252.32

spike
379.63
631.95

137.63
18" Oak
Disk

36.24
36.24

631.95

R/W
Post

38 1/2

90°

98.58

379.71

116.29

P.P.
Disk

6" Oak
Disk

129.81
104.78
36.99
11.20

Serv.
Sta

Ho, Fo

Sta. point ΔL ΔR

$$P.I. = 71+20.61$$

+37.02 PT

$$4^{\circ}16\frac{1}{2}' \Delta = 8^{\circ}33' \text{ Rt}$$

73

$$3^{\circ}56.4' \frac{1}{2} \Delta = 4^{\circ}16\frac{1}{2}'$$

+50

$$3^{\circ}26.4' D = 1^{\circ}59'42.5''$$

72

$$2^{\circ}56.4' T = 214.68$$

+50

$$2^{\circ}26.4' L = 431.09$$

71

$$1^{\circ}56.4' R = 2871.93'$$

+50

$$1^{\circ}26.4'$$

70

$$0^{\circ}56.4'$$

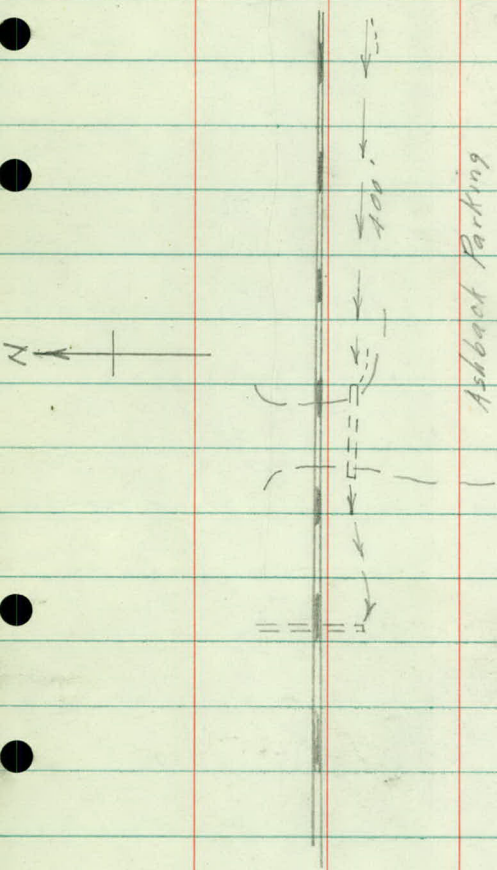
+50

$$0^{\circ}26.4'$$

69+05.93 P.C.

$$0^{\circ}00'$$

C Rd "C"



Sta	+	π	-	Elev.
BM	5.97	932.22		926.25

68

+50

+80

12.25 919.97

69

+50

+85

9.91 922.31

70+15

9.51 922.71

70

4.81 927.41

69

4.59 927.63

Jan. 8, 1962

2

RT

2

1905 W Co Rd C - S.W. Cor, Walk

27.2	25.4	24.4	26.0	27.0	27.3
5.0	6.8	7.8	6.2	5.2	4.9
93	100	111	126	136	149

26.9	25.6	22.7	22.6	24.6	26.8	27.3
5.3	6.6	9.5	9.6	7.6	5.4	4.9
92	100	113	122	131	138	155

inv S End Culv under RR

26.6	24.6	22.1	22.0	24.8	27.0	27.0
5.6	7.6	10.1	10.2	7.4	5.2	5.2
91	100	109	121	131	142	162

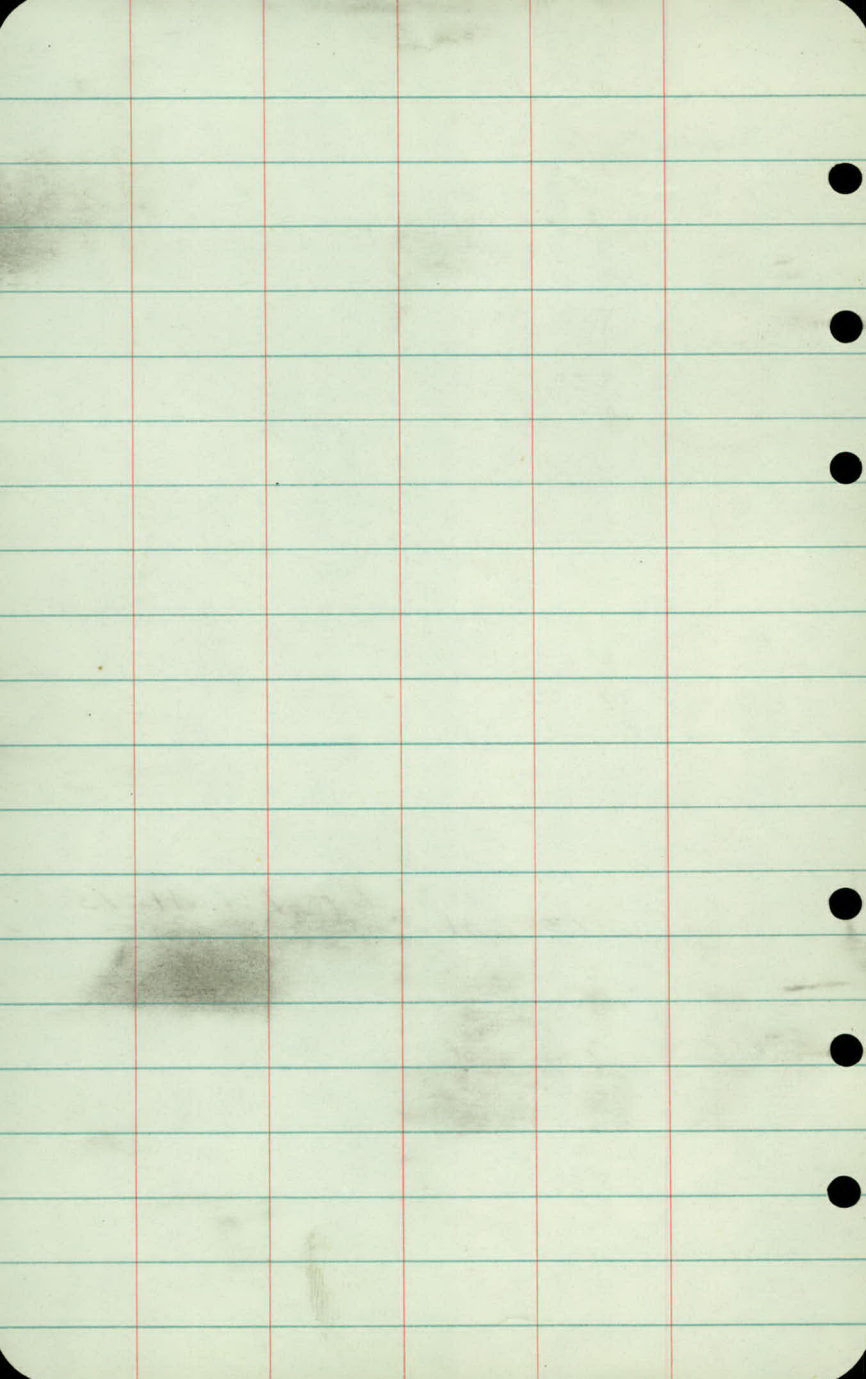
26.4	24.6	22.6	22.5	23.7	26.1	27.1
5.8	7.6	9.6	9.7	8.5	6.1	5.1
91	100	108	119	131	141	154

W. End 12" X 30' CM

E, E 12" X 30' CM

2

2



Co Rd C.

Culvert Elevations

Fairview to SH # 51

Sta

+

n

-

B. M.

9.77

928.79

919.02

85+60

7.42

21.37

+50 +
~~+26~~

9.27

19.52

B. M.

4.36

24.43 ✓

JS
WH
FS
WS
DS
RB

Jan 29. 1963

3° Rt

Lt

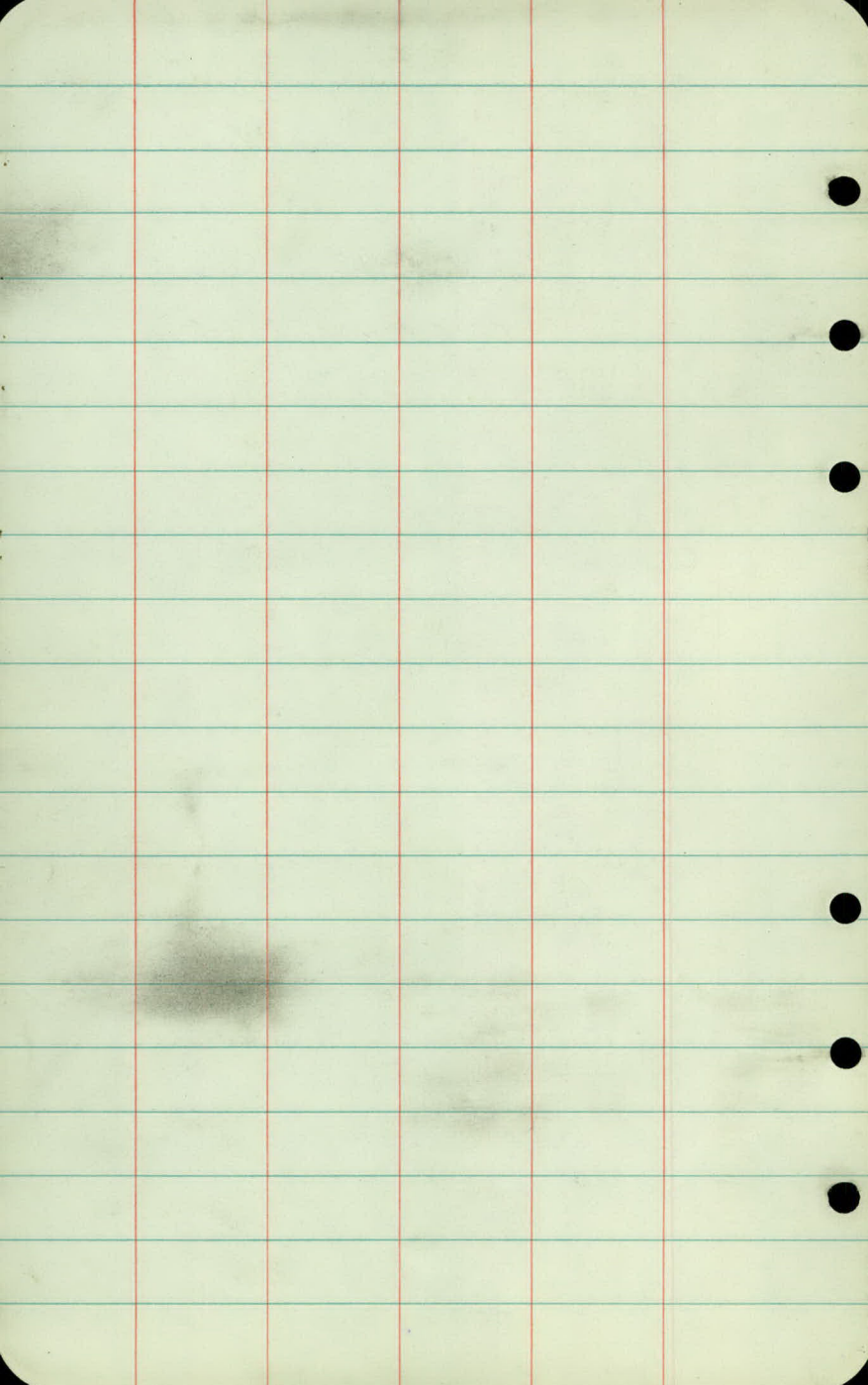
£

P.P. 31' Lt of Sta 83+30

East End 15" CMC 57' Rt

West End 15" CMC 57' Rt

£ Sta 85+00 (old £)



Use For Sod Existing Levee

Avr width
12'

56+07 Lt to 57+46 Lt ✓

63+43 Lt to 66+13 Lt ✓

70+89 Lt to 71+⁴¹2 Lt ✓

⁸⁰71+60 Lt to 72+⁺93 Lt ✓

76+22 Lt to 76+82 Lt ✓

maybe

~~also (76+436) 16x82~~

77+05 Lt to 77+19 Lt. ✓

85+38 Lt to 85+68 Lt or possibly to +78

86+75 Lt to 88+98 Lt ✓

96+58 Lt to 98+06 Lt ✓

98+74 Lt to 100+06 Lt ✓

Special Ditch

sewer Grade

58-60

101+75 - 105

81-86

86-89

94-96

99-102+25

