

Dr. 9 BK. 5

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

LAKE JOHANNA BLVD.

From Co. Rd. E To S.T. H. #10

Road Acc't. No. _____

Date Filed 2-6-59

File Dr 9 BK 5

1955-09-30

1
Lake Johanna Blvd

New Alignment

Sta Point ΔL ΔR

1+28.52

0-114.32 PC

0-159.35 = 0+00 New Line

$\Delta = 31^{\circ}04'$

$D = 20^{\circ}$

0-194.35 P.I.

$T = 80.03$

$L = 155.33$

$R = 287.94$

Cor. Rd E post.

14+98.36
30.22 Rt

26.20

PI = 0+82.53 o/d

0+00 o/d

Cor.
Ho.

50.02

35.87 28" Elm

25.500 PP

65° 53' 16"

124° 21'

52.57

25.24

R.R. Spike

85.82

101.36

SW. Cor
Gov. Lot 2

101.36
85.82
15.54

Sta Point ΔL ΔR

+05.08

$33^{\circ} 42'$

9

$33^{\circ} 20.7'$

+50

$29^{\circ} 50.7'$

8

$26^{\circ} 20.7'$

+50

$22^{\circ} 50.7' \Delta 67^{\circ} 24' R$

7

$19^{\circ} 20.7' D = 14^{\circ}$

6+97.27 P.I.

$67^{\circ} 24' T = 273.62$

+50

$15^{\circ} 50.7' L = 481.43$

6

$12^{\circ} 20.7' R = 410.28$

+50

$8^{\circ} 50.7'$

5

$5^{\circ} 20.7'$

+50

$1^{\circ} 50.7'$

+23.65

$0^{\circ} 00'$

4

Nov. 2, 1955

3

16"0

85.33

8" Elm 3 39.63

1"x2"x18"

Sta Point ΔL ΔR

15+36.39 P.O.T. Exact

+81.32 PT

3°00'

+50

2°41.2' Δ 6°00' Rt

14

2°11.2' D-2°

+50

1°41.2' T- 150.14'

13+31.46 P.I.

6°00' L=300.00'

13

1°11.2' R=2864.93'

+50

0°41.2'

12

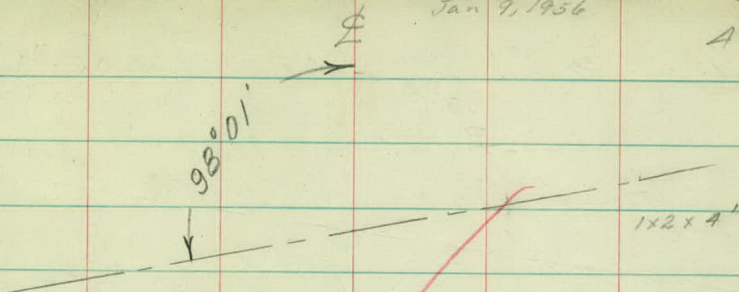
0°11.2'

11+81.32 PC

0°00'

Jan 7, 1956

A



~~VOID See "B" Line~~

~~P. 57-61~~

8" Ash

24" 0

8

56.16

□

1x2"x18"

~~81.86~~

73.98

8" Trip 8" Cherry

1536.39

1481.32

53.07

150.14

203.21

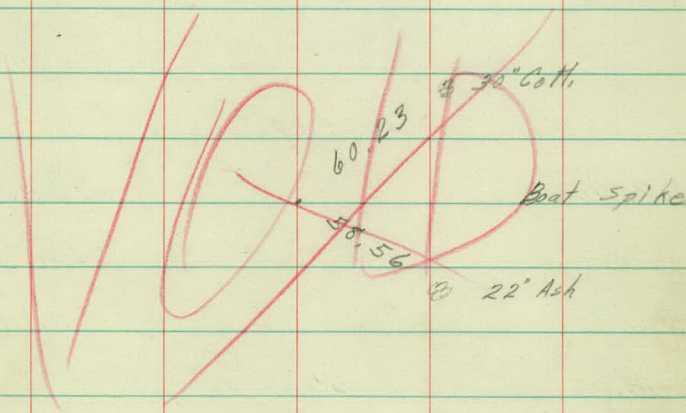
Temp

205.25

Sta	Point	ΔL	ΔR
190.73		$23^{\circ} 57' 22\frac{1}{2}''$	
+50		$21^{\circ} 55'$	
23		$19^{\circ} 25'$	
+50		$16^{\circ} 55'$	$\Delta = 47^{\circ} 54' 45''$ Lt.
22		$14^{\circ} 25'$	$D = 10^{\circ}$
21+66.51	PI	$47^{\circ} 54'$	$T = 254.90$
+50		$11^{\circ} 55'$	$L = 479.12$
21		$9^{\circ} 25'$	$R = 573.69$
+50		$6^{\circ} 55'$	
20		$4^{\circ} 25'$	
+50		$1^{\circ} 55'$	
19+11.61		$0^{\circ} 00'$	

Nov 2, 1955

5



Sta Point ΔL ΔR

+31.82 P.T.

$12^{\circ} 49\frac{1}{2}'$

25

$10^{\circ} 55' \Delta = 25^{\circ} 39' R$

+50

$7^{\circ} 55' D = 12^{\circ}$

24+26.96 P.I. (611)

$25^{\circ} 39' T = 108.89$

24

$4^{\circ} 55' L = 213.75$

+50

$1^{\circ} 55' R = 478.34$

~~Equation 25+40.50~~

~~= 23+18.07 P.C. Survey 7/8/40 $0^{\circ} 00'$~~

~~23+18.07 - 1990SUNNY~~

~~25+40.5 P.C. = } Equa~~

Jan 10, 1956

6

$$\begin{array}{r} 149.77 \\ 24 \overline{) 11.82} \\ \underline{2561.59} \end{array}$$

$$\begin{array}{r} 24 + 11.82 \\ 23 + 90.73 \\ \underline{121.09} \end{array}$$

$$\begin{array}{r} 100 \\ 40.5 \\ 9.27 \\ \hline 149.77 \\ 6.10 \\ \hline 155.87 \end{array} \quad 25 + 40.5$$

$$\begin{array}{r} 24 + 11.82 \\ 24 + 05.72 \\ \hline 6.10 \end{array}$$

$$\begin{array}{r} 24 + 05.72 \\ 155.87 \\ \hline 2561.59 \end{array}$$

WPP

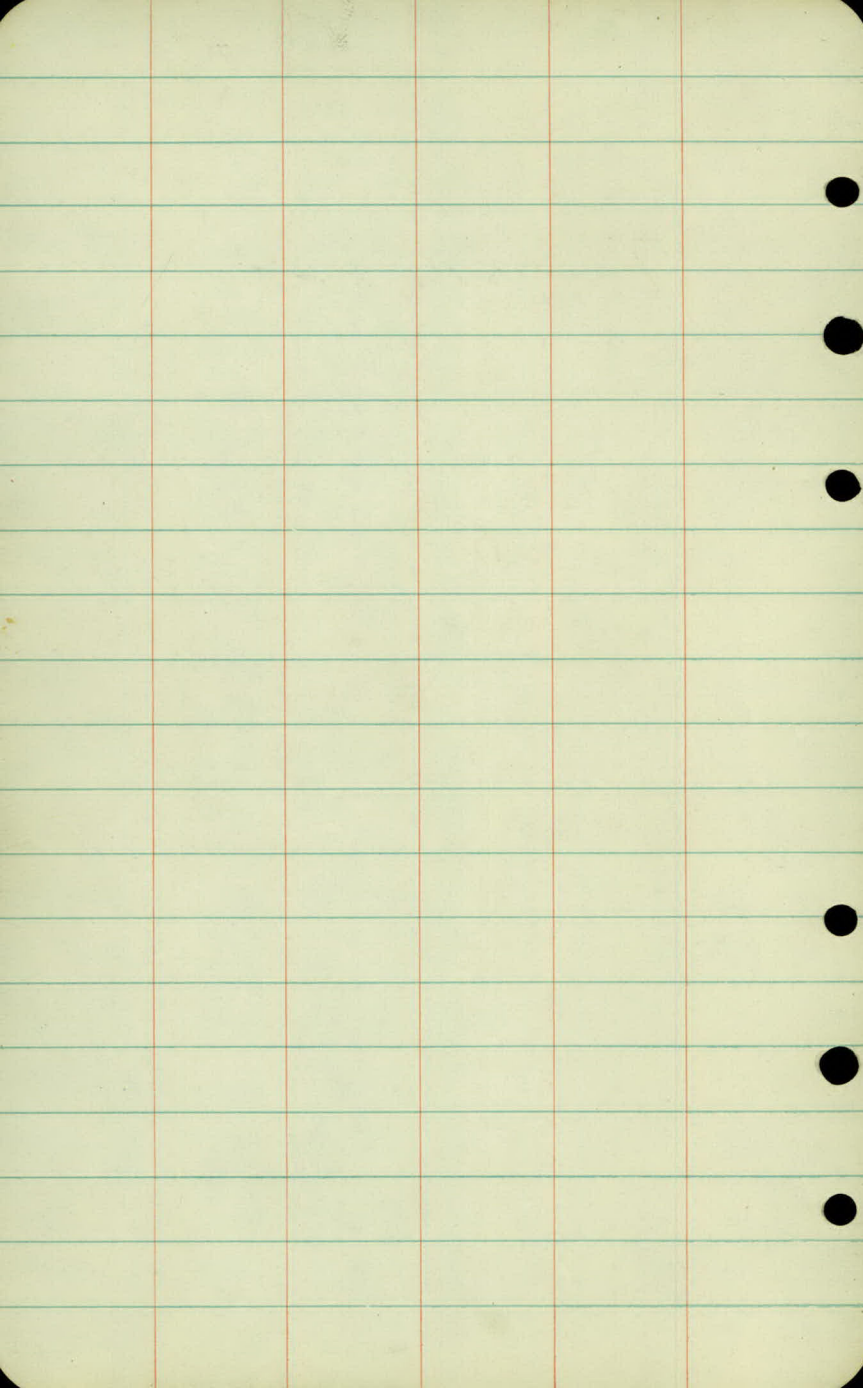
TP0 29.22

38.33

OPP

Spike

$$\begin{array}{r} 25 + 40.5 \\ 21.08 \\ \hline 2561.58 \end{array}$$



Jan 10, 1956

7

TOPOGRAPHY

4

$+85 \frac{18''A}{37}$ $+98 \frac{10''E}{43}$ $+75 \frac{Parkies}{35}$
 $+65 \frac{18A}{38}$ $+66 \frac{20''A}{32}$ $+67 \frac{26A}{25}$
 $+38 \frac{Rtie}{Ent}$ $+57 \frac{26''A}{31}$ $+59 \frac{24A}{24}$
 $+120 \frac{28Ent}{26}$ $+27 \frac{Cor Park}{30}$
 $+100 \frac{Road}{44}$

$+82 \frac{12''O}{27}$ $+99 \frac{T-8''E}{39}$

$+47 \frac{14''O}{39}$ $+66 \frac{20''Ash}{35}$ $+70 \frac{16''O}{36}$

$+17 \frac{16''Ash}{18}$

$+24 \frac{8''O}{4}$

$+13 \frac{5''BE}{5}$

$+98 \frac{20''Ash}{33}$

$+84 \frac{26''W}{51}$ $+85 \frac{5''Cott}{12}$

$+51 \frac{14''E}{4}$ $+73 \frac{5TP}{33}$ $+82 \frac{18''Cott}{44}$ $+70 \frac{Road}{26}$

$+37 \frac{18BE}{46}$

$+33 \frac{Rd}{E}$

$+59 \frac{A-elt}{9}$

2

$+53 \frac{Road}{14}$ $+62 \frac{P.Rm}{3}$ $+68 \frac{Road}{E}$

$+49 \frac{T14''W}{20}$ $+52 \frac{B.Post Rm}{15}$ $+63 \frac{Post Rm}{E}$

$+35 \frac{T14''W}{33}$ $+43 \frac{Doub 12''W}{27}$ $+65 \frac{Road}{19}$ $+50 \frac{Post Road Fe}{6 12-40 44}$ $+60 \frac{Post Rm}{5}$

$+80 \frac{Road}{44}$ $+25 \frac{14''W}{48}$

$+29 \frac{PV}{T}$

1

$Post Rm$
3

$Guard Fe$
22

$Road$
3-25 $+10 \frac{18''E}{43}$

$+98 \frac{16''E}{39}$ $+50 \frac{Road}{18}$ $+100 \frac{Road}{11''W}$

$+78 \frac{10''W}{49}$ $+89 \frac{26''E}{36}$ $+91 \frac{14''W}{30}$

$+100 \frac{Road}{14}$

$+50 \frac{Post Rm}{14}$

$+66 \frac{22''E}{8}$

$+50 \frac{Road}{9}$

$+150 \frac{Guard Fe}{21}$

$+63 \frac{14''W}{45}$

$+76 \frac{24''E/m}{33}$

0

$+18 \frac{2Ent}{21}$

$+06 \frac{Rtie}{Ent}$

$+15 \frac{Guard Fe}{14.5}$

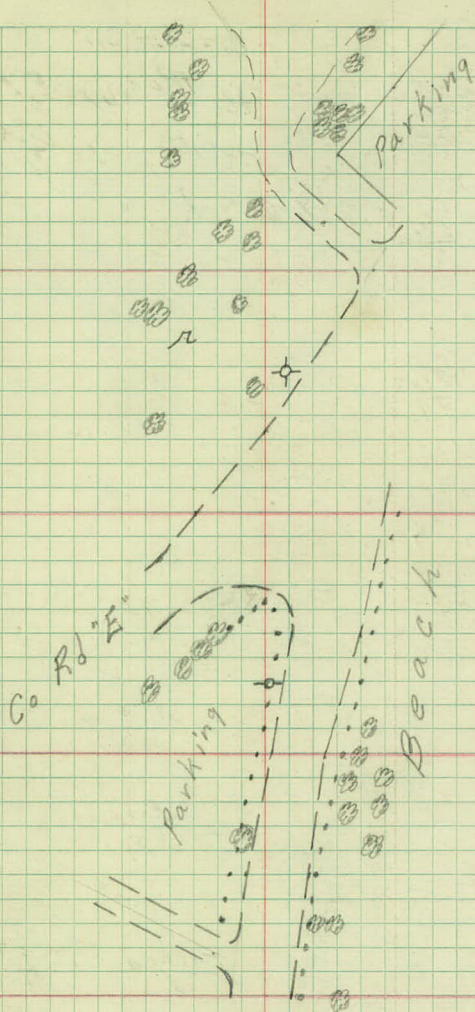
$+29 \frac{12''W}{29}$

$+30 \frac{29''Ent}{21}$

$-01 \frac{20''W}{31}$

Jan 10, 1956

8



9

+95 $\frac{14}{38}$ "Cott
 +60 $\frac{7.12}{4}$ "Cott +65 $\frac{8}{9}$ "A
 +44 $\frac{4}{31}$ "A +52 $\frac{6}{2}$ "A +58 $\frac{8}{4}$ "A
 +50 $\frac{5atL}{90}$
 +65 $\frac{J 8}{12}$ "Cott

+23 $\frac{14}{15}$ "Cott +41 $\frac{16}{10}$ "Cott
 +22 $\frac{13}{10}$ "Cott

+12 X-Pitch

+37 $\frac{29}{10}$ "W
 +17 $\frac{7}{2}$ "W

+88 $\frac{12}{39}$ "Cott
 +98 $\frac{6}{28}$ "W

150 to 8 $\frac{7 T. W 8}{30-50}$

+77 $\frac{12}{34}$ "Cott

150 Scattered T.L. 90

+27 Cor Parking $\frac{37-120}{123}$

+33 Cor Parking

+100 $\frac{38-1}{123}$ Parking

7

+150 $\frac{45-126}{126}$ Parking TL

6

+100 $\frac{40-116}{116}$ Parking TL

+150 $\frac{29-98}{98}$ Parking TL

5

+100 $\frac{14}{86}$ Parking PK+TL

+11 $\frac{30}{30}$ Cor. Parking

+61 $\frac{20}{20}$ Parking

+150 $\frac{74}{74}$ PK+TL

+44 $\frac{16}{36}$ "E

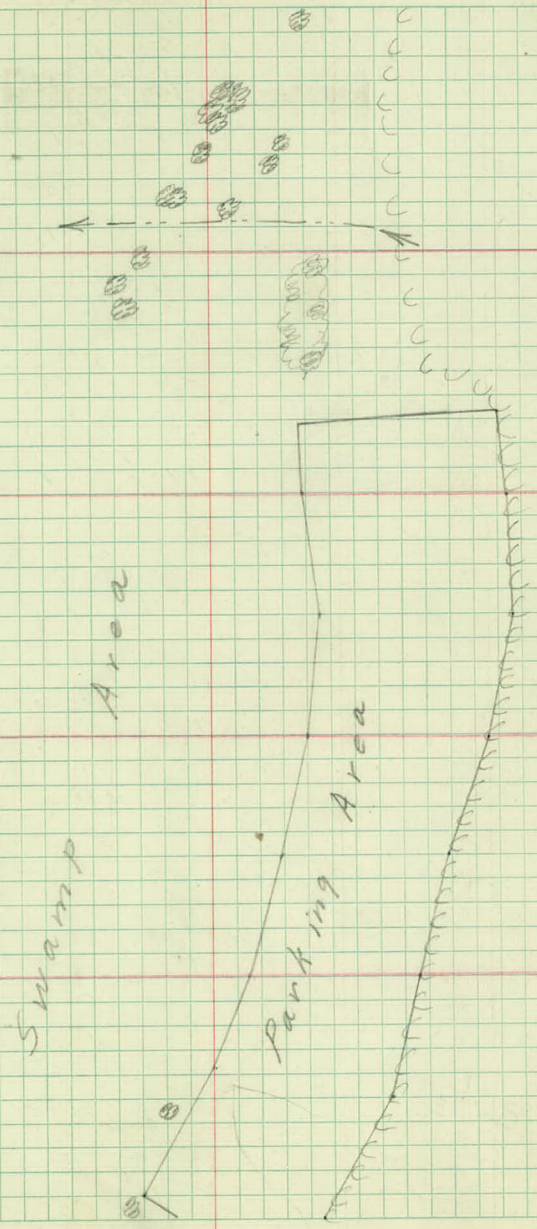
Parking + Tree Line
 26

4

+105 $\frac{16}{36}$ "E

Jan 10, 1956

9



14

+80 Beg Marsh

+50 $\frac{\text{Ditch}}{27}$ +53 $\frac{22 \text{ Cut}}{5}$

13

+100 $\frac{\text{Ditch}}{22}$ +96 $\frac{\text{STP}}{32}$ +84 $\frac{\text{STP}}{2}$ +86 $\frac{20''0}{22}$ +93 $\frac{\text{STP}}{17}$ +56 $\frac{14''0}{7}$ +82 $\frac{12''0}{3''0}$ +58 $\frac{7-8''0}{9}$ +59 $\frac{\text{STP}}{6}$ +73 $\frac{\text{Trim Cherry}}{42}$ +25 $\frac{18''0}{6}$ +35 $\frac{14''0}{11}$ +50 $\frac{\text{Ditch}}{27}$ +42 $\frac{20''0}{33}$

12

+101 $\frac{7-12'' Bas}{14}$ +100 $\frac{\text{Ditch}}{33}$ +11 $\frac{\text{STP}}{2}$ +107 $\frac{4''A}{28}$ +113 $\frac{4''0}{5}$ +75 $\frac{\text{STP}}{9}$ +89 $\frac{10''0}{25}$ +94 $\frac{12''0}{15}$ +95 $\frac{16''0}{8}$ +99 $\frac{2-6''0}{39}$ +48 $\frac{12''0}{11}$ +60 $\frac{12''0}{26}$ +72 $\frac{16''0}{22}$ +61 $\frac{14''0}{15}$ +65 $\frac{8''0}{28}$ +85 $\frac{6''A}{38}$ +31 $\frac{\text{W End Cul}}{41}$ +61 $\frac{15 \times 30 \text{ E. Cul}}{33}$ +19 $\frac{\text{Road}}{2}$ +29 $\frac{20''0}{14}$ +55 $\frac{16''0}{37}$

11

+100 $\frac{\text{Ditch}}{50}$ +12 $\frac{16''A}{32}$ +100 $\frac{\text{Road}}{20}$ +22 $\frac{12''0}{25}$ +42-6 Sta $\frac{17 \text{ Trees}}{10-55''}$ +84 $\frac{16''A}{45}$

10

+107 $\frac{12''A}{48}$ +101 $\frac{10''A}{50}$ +100 $\frac{\text{STL}}{75}$

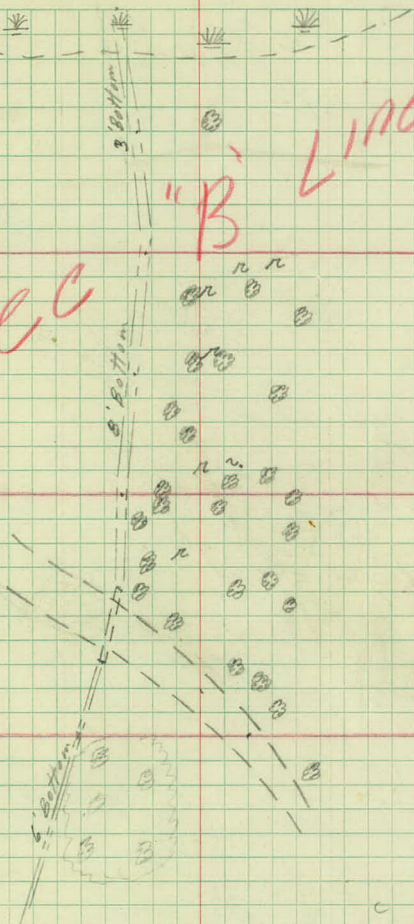
9

+100 $\frac{\text{S. TL}}{80}$

Jan 11, 1956

10

Sec "B" Line



C
C
C
C
C
C
C
C
C
C

19

Road
54

18

17

16

+10 $\frac{Fe}{\#}$ 15 +100 $\frac{\# \text{ Pitoh + Fe}}{58'}$ +50 $\frac{\# \text{ Pit}}{49}$

14

+100 $\frac{\# \text{ Pitoh}}{36}$

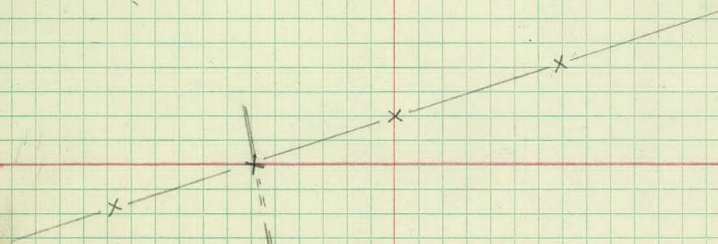
Jan 11, 1956

11

See "B" Line

March

g. Buffon



24

+100 $\frac{\text{Road}}{2-22}$ +98 $\frac{18 \text{ Cat}}{28}$ +72 $\frac{\text{P.P.}}{6}$ +50 $\frac{\text{Road}}{8-28}$ +144 $\frac{16 \text{ Cat}}{21}$ +29 $\frac{\text{STP}}{7}$

23

+100 $\frac{\text{Road}}{25-47}$ +25-54 $\frac{15 \text{ trees}}{30-45}$ +68 $\frac{\text{STP}}{10}$ +66 $\frac{\text{PP}}{26}$ +50 $\frac{\text{Road}}{42}$ +11 $\frac{\text{STP}}{3}$ +18 $\frac{\text{STP}}{9}$ +22 $\frac{\text{STP}}{22}$

22

+106 $\frac{\text{STP}}{8}$ +17 $\frac{\text{STP}}{9}$ +100 $\frac{\text{Road}}{51}$ +89 $\frac{\text{STP}}{12}$ +91 $\frac{\text{STP}}{1}$ +98 $\frac{\text{STP}}{32}$ +83 $\frac{\text{STP}}{6}$ +50 $\frac{\text{Road}}{53}$ +79 $\frac{\text{Sign}}{31-37}$

21

Road
48+50 $\frac{\text{Road}}{36}$

20

Road
36+50 $\frac{\text{Road}}{38}$

19

Jan 11, 1956

12

566

March to Bird

π
 π
 π

π
 π
 π

π

π

"B"

Line

B

π

π

π

π

π

B

B

B

25

+87 $\frac{PP}{26}$

+69 $\frac{Ent 15 \times 20 CM R. 10}{22}$ +66 $\frac{Ent}{Ent}$

Road
10-11

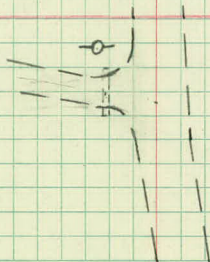
+50 $\frac{Road}{8-14}$

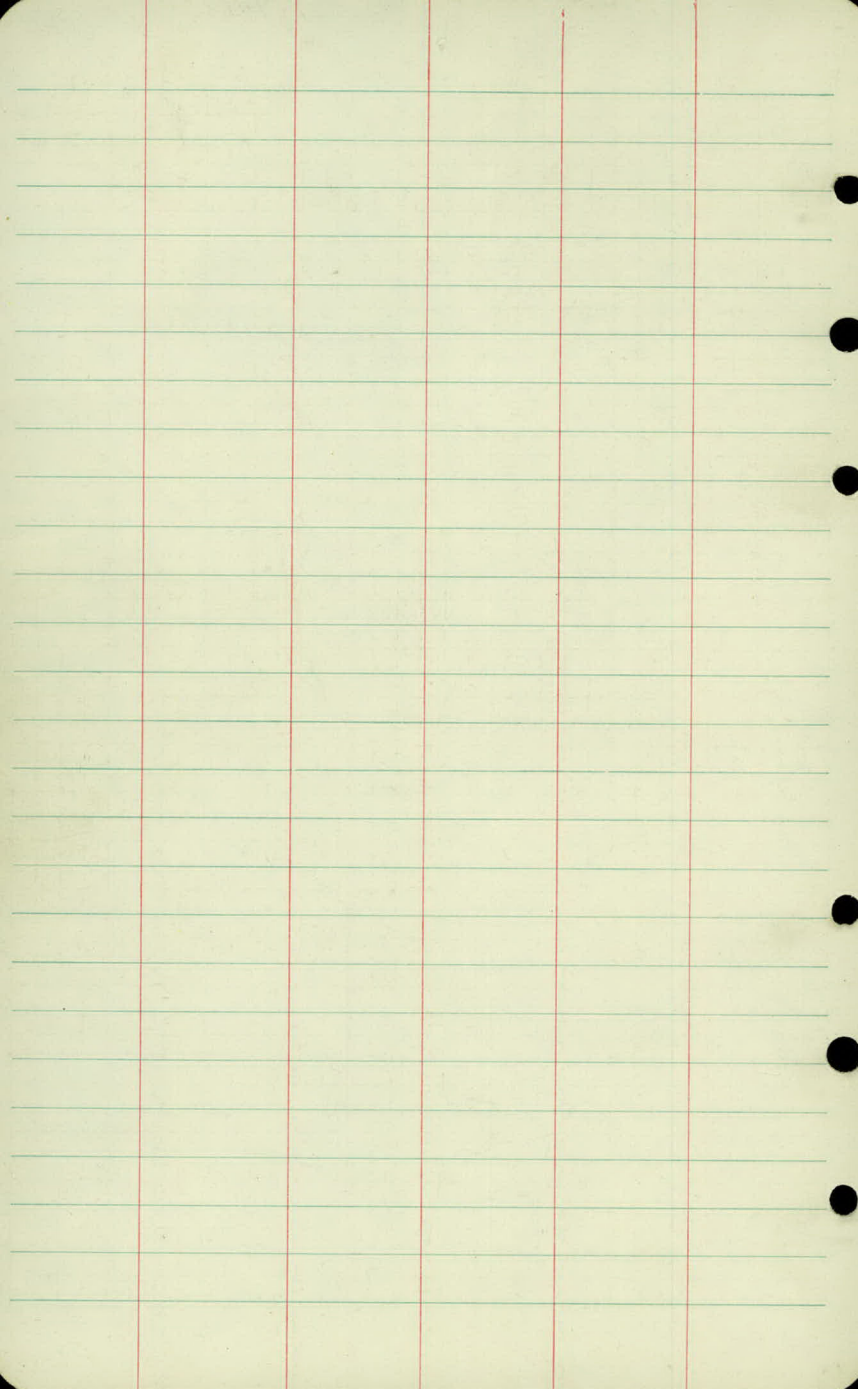
+50

24

Jan 11, 1956

13





Jan 11, 1956

14

Bench Levels

Sta	+	π	-	Elev
B.M.				gone 884.17
B.M.	7.76	889.58		881.82
BM			11.00	878.58
T.P.	4.97	894.12	0.43	889.15
BM			9.23	884.89 (883.41)
TP	4.16	886.24	12.04	882.08
BM			3.92	882.32 (882.33)

Jan 11, 1956

15

Lt.

Rt.

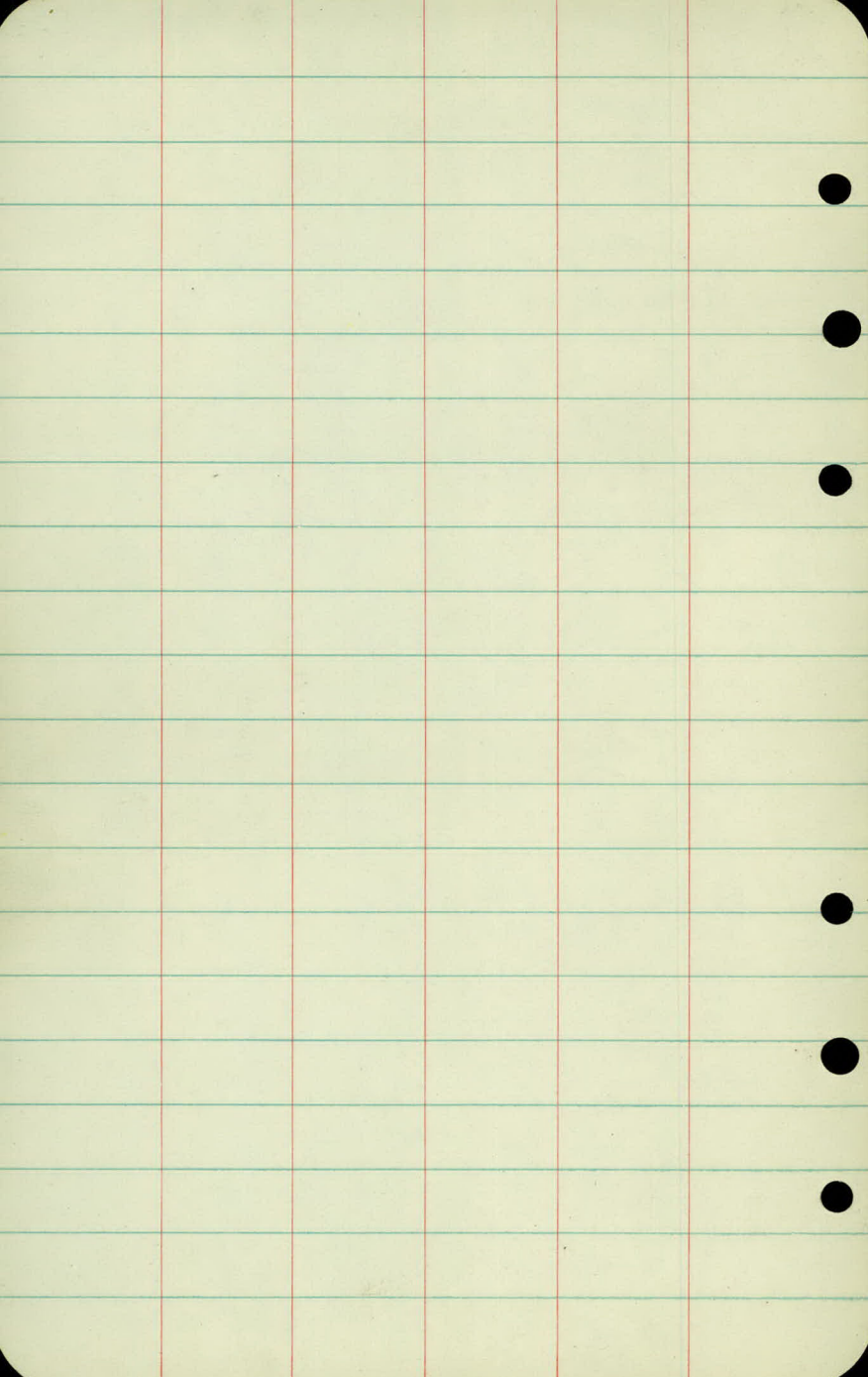
~~Spike in Arc Light Pole 30' Lt sta 0+87 (ok)~~

Top S.W. Cor of Conc. Wall of Spillway Lake outlet ^{Johanna}

Spike in 12" Oak Lt sta 11+60

Garage floor Myers Garage. Edge Apron

Spike in P.P. at Ent to Prince of Wales Club.



FK
LC
AB
CW

Jan 12, 1956

16

X-Sections

Sta	+	π	-	Elev.
BM	6.72	888.54		881.82

0-100

0-50

0+00

+50

1

+50

Jan 12, 1956

17

17

54

S.W. Cor. Conc. Wall at Spillway Lake Johanna Outlet

85.7
2.8

85.7
2.8

✓ 88.0	87.6	85.6	85.0	85.0	84.6	84.7	82.7	79.7
0.5	0.9	2.9	3.5	3.5	3.9	3.8	5.8	8.8
40	Wall	24	10		11	15	24	40
24								

✓ 84.1	84.1	84.0	84.5	84.6	84.4	84.6	80.3	78.2
44	44	45	4.0	3.9	4.1	3.9	82	10.3
50	26	15	7		16	21	36	50

✓ 83.6	83.7	83.7	83.9	84.1	84.4	84.2	84.6	81.4	80.5
49	48	48	4.6	4.4	4.1	4.3	3.9	7.1	8.0
50	38	25	8		17	26	33	42	50

✓ 85.5	85.6	85.4	84.1	83.5	83.5	83.9	84.3	83.9	84.0	82.5
3.0	2.9	2.8	4.4	5.0	5.0	4.6	4.2	4.6	4.5	6.0
50	40	29	23	15		14	26	39	46	50

Sta + π - Elev

888.54

1+78

2

+30

+65

✓

T.P. 0.35 885.69 3.20 885.34

3

2 Dec. 12, 1956

18

11

BT

✓	83.0	83.9	84.7	84.7	84.3	84.2	83.9	82.7	✓
	5.5	4.6	3.8	3.8	4.2	4.3	4.8	5.7	
	50	39	22		17	32	46	50	

✓	81.8	82.5	83.0	84.0	84.2	84.3	84.2	84.0	✓
	6.7	6.0	5.5	4.5	4.3	4.2	4.3	4.5	
	50	41	27	13		26	39	50	

✓	81.6	81.9	82.6	82.8	83.0	83.6	83.8	84.0	✓
	6.9	6.6	5.9	5.7	5.5	4.9	4.7	4.5	
	50	37	19	12		19	34	50	

	78.2	79.5	82.0	82.7	83.2	83.6	83.0	83.7	83.8	✓
	10.3	9.0	6.5	5.8	5.3	4.9	5.5	4.8	4.7	
	33	27	21	15		12	27	44	50	

	77.2	76.8
→	11.3	11.7
	42	50

Post

✓	77.6	78.0	78.4	79.1	79.2	82.8	83.2	83.3	83.4	83.5	✓
	8.1	7.7	7.3	6.6	6.5	2.9	2.5	2.4	2.3	2.2	
	50	35	23	12	7		18	31	46	50	

Sta + π - E/ev

885.69

3 + 43

+58

4

+24

+50

Jan 12, 1956 19

Lt

Rt

✓ 79.4	79.2	79.4	80.3	81.3	81.7	83.3	83.6	83.5
6.3	6.5	6.3	5.4	4.4	4.0	2.4	2.1	2.2
50	33	16		15	23	30	46	50

✓ 78.3	78.7	79.1	79.8	80.0	79.9	80.7	82.0	83.3
7.4	7.0	6.6	5.9	5.7	5.8	5.0	3.7	2.4
50	34	17		12	24	35	43	50

✓ 74.3	75.0	76.7	77.4	78.1	78.3	78.3	78.6	79.6
11.4	10.7	9.0	8.3	7.6	7.4	7.4	7.1	6.1
50	40	35	29	19		24	38	50

73.6	73.8	74.8	76.4	77.3	77.7	77.8	78.1	78.3	78.3
12.1	11.9	10.9	9.3	8.4	8.0	7.9	7.6	7.4	2.4
50	40	31	23	15		15	32	45	50

73.1	73.8	75.8	76.5	77.0	77.3	77.5	78.1
12.6	11.9	9.9	9.2	8.7	8.4	8.2	7.6
22	15	8	4		18	32	50

73.8	73.5	72.9
11.9	12.2	12.8
27	35	50

Sta	+	π	-	Elev
-----	---	-------	---	------

		885.69		
--	--	--------	--	--

5+00				
------	--	--	--	--

+50				
-----	--	--	--	--

6

T.P.	3.16	880.48	8.37	877.32
------	------	--------	------	--------

+50				
-----	--	--	--	--

7

+50				
-----	--	--	--	--

Sta + π - Elev

880.48

7+85

8

+ 05

+ 10

+ 18

+ 50

Jan 12, 1956

21

✓ 73.2
23
50

74.0
65
35

74.9
56
25

75.2
53
16

75.6
4.9
8

75.2
53
8

74.2
6.3
50
Ditch

73.5-
70
17

73.7
6.8
21

74.8
5.7
80

74.3
6.2
29

75.1
5.4
40

75.1
5.4
50

✓ 73.0
25
50

73.5-
70
36

74.0
6.5
24

73.4
7.1
10

73.4
7.1
10

73.5-
70
10

73.5-
70
18

74.7
5.8
30

75.1
5.4
39

74.7
5.8
50

✓ 73.0
25
50

73.5-
70
36

73.0
7.5
27

73.4
7.1
17

73.4
7.1
10

73.5-
70
10

73.6
6.9
17

74.7
5.8
25

75.1
5.4
37

74.7
5.8
50

✓ 73.1
74
50

73.0
75
33

73.5-
70
23

75.5
50
12

75.5-
50
18

75.1
5.4
18

75.0
5.5
31

74.8
5.7
42

74.9
5.6
50

✓ 73.7
6.8
50

73.8
6.7
34

74.0
6.5
20

74.7
5.8
10

75.7
4.8
15

75.8
4.7
15

75.5-
50
27

75.5-
50
42

74.0
4.5
50

✓ 74.0
4.5
50

Sta + π - Elev

880.48

9

+50

10

+50

11

BM 6.39 884.97 1.87 878.61 (878.58)

+31

2 Jan 12, 1956

22

74.4	74.7	75.2	75.6	76.4	76.7	77.0	77.7	77.9
6.1	5.8	5.3	4.9	4.1	3.8	3.5	2.8	2.6
50	43	28	15		16	29	44	50

73.9	74.2	75.1	75.9	76.6	76.9	77.1	77.7	77.9
6.6	6.3	5.4	4.6	3.9	3.6	3.4	2.8	2.6
50	42	30	18		12	28	41	50

74.7	74.1	74.9	75.6	76.0	76.6	77.1	77.9
5.8	6.4	5.6	4.9	4.5	3.9	3.4	2.6
50	38	25	11		15	30	50

74.7	75.1	75.6	76.2	76.7	77.1	77.6
5.8	5.4	4.9	4.3	3.8	3.4	2.9
50	34	15		16	30	50

73.1	74.6	76.4	76.1	76.3	77.0	77.4	78.1	79.0
7.4	5.9	4.1	4.4	4.2	3.5	3.1	2.4	1.5
50	39	32	19		18	31	42	50

Spike in 12" Oak Lt Sta 11+60

72.91	76.9	77.1	77.2	77.5	78.9	79.4	80.1	81.5
12.06	8.1	7.9	7.8	7.5	6.1	5.6	4.9	3.5
41	36	31	21		13	24	34	50

Fl 15 KM

73.2	75.1	75.9
11.8	9.9	9.1
AT	45	50

Sta + π - Elev

884.97

11+61

✓

BM 10.22 888.80 6.41 878.56 878.58

+81.32 PC.

✓

12

FK
2C
AB
CW

2

Jan 12, 1956
Jan 13, 1956

23

BT

73.03

14

76.6

77.6

79.7

80.3

81.4

83.1

83.8

84.5

86.1

11.95 8.4 7.4 5.3 4.7 3.6 1.9 1.2 0.5 +1.1

33 26 21 14 12 22 30 38 50

FL 15" CM

72.8

75.0

77.5

77.7

11.2 10.0 7.5 2.3

33 36 43 50

Spike in 12" oak 14 sta 11.60

73.2

73.6

77.3

79.1

80.8

82.4

83.0

82.3

83.2

85.3

86.1

15.6 15.2 11.5 9.7 8.0 6.4 5.8 6.5 5.6 3.5 2.7

34 29 24 17 9 6 8 14 22 31

74.0

76.2

76.9

88.2

87.1

14.8 12.6 11.9 0.6 1.7

38 43 50 50 38

73.5

77.0

78.3

79.8

80.9

82.8

84.5

83.8

84.6

85.7

15.3 11.8 10.5 9.0 7.9 6.0 4.3 5.0 4.2 3.1

28 26 21 14 8 11 13 16 22

73.5

74.2

75.4

76.8

88.8

88.3

86.8

15.3 14.6 13.4 12.0 0.0 0.5 2.0

33 38 43 50 50 44 30

Sta + Δ - Elev

888.80

12+50

✓

TP 0.65 881.80 7.65 881.15

13

✓

+16

T.P 11.00 887.14 5.66 876.14

± Jan 13, 1956

24

Lt. Pt.
 73.4 77.0 78.8 80.2 81.3 82.7 83.9 84.2 84.2

154 118 100 86 75 61 49 46 46 ✓
 21 16 12 7 14 24 39 50

73.3 73.1 74.6 75.7 78.2

155 157 142 131 106 ✓
 24 30 34 37 50

73.6 73.3 74.4 75.8 76.9 77.5 78.0 78.7 79.5

82 85 74 60 49 43 38 31 23
 28 22 16 11 24 23 42 50

75.9 78.2 79.3

59 36 25
 36 45 50

72.4 73.1 73.9 75.6 75.8 76.0 77.0 77.2 78.8

84 87 79 62 60 55 48 46 30
 28 21 14 8 12 23 37 50

75.3 78.5

65 33 ✓
 36 50

Stake at P1.

Sta + π - Elev.

882.14

13 + 50

✓

14

✓

+ 50

15

FK
LO
AB
CW

Jan 17, 1956
Cool 10° Lt. Snow

25

73.1	73.7	74.7	75.6	76.0	76.0	76.3	77.1	77.3
14.0	13.4	12.4	11.5	11.1	11.1	10.8	10.0	9.8
27	20	16	14		21	35	47	50

74.0	75.9	76.6
13.1	11.2	10.5
32	42	50

73.6	73.6	74.9	75.1	75.1	75.1	75.1	75.7	75.3
13.5	13.5	12.2	12.0	12.0	12.4	12.0	11.4	11.8
39	35	28	15	13	26	44	50	

74.7	74.8
12.4	12.3
45	50

73.4	74.4	74.3	74.6	75.0	74.9	74.8	74.8
13.7	12.7	12.8	12.5	12.1	12.2	12.3	12.3
50	43	33	18		21	37	50

73.8	73.9	74.1	74.7	74.6	74.6	74.6	74.7	74.7
13.3	13.2	13.0	12.4	12.5	12.5	12.5	12.4	12.4
50	45	31	14		14	29	45	50

Sta + π - Elev

887.14

15+50

16

+50

17

+50

18

Jan 17, 1956

26

11

B+

73.9	7A.1	7A.1	7A.5	7A.8	7A.5	7A.6
13.2	13.0	13.0	12.6	12.3	12.6	12.5 ✓
50	32	17		17	32	50

7A.1	7A.1	7A.3	7A.6	7A.1	7A.6	7A.6
13.0	13.0	12.8	12.5	12.7	12.5	12.5 ✓
50	35	16		18	37	50

7A.3	7A.2	7A.2	7A.4	7A.6	7A.3	7A.4
12.8	12.9	12.9	12.7	12.7	12.8	12.7 ✓
50	32	19		20	34	50

7A.1	7A.3	7A.3	7A.3	7A.5	7A.5	7A.7
13.0	12.8	12.8	12.8	12.6	12.6	12.4 ✓
50	40	22		19	37	50

7A.0	7A.2	7A.3	7A.5	7A.8	75.0	75.0
13.1	12.9	12.8	12.6	12.3	12.1	12.1 ✓
50	33	19		22	38	50

7A.1	7A.5	7A.7	75.2	75.1	75.2	75.7
13.0	12.6	12.4	11.9	12.0	11.9	11.4 ✓
50	34	22		17	33	50

Sta + π - Elev

887.14

18+50

19

3.75 883.39 (883.41)

TP

✓

TP 8.91 885.17 10.88 876.26

+50

20

Jan 13 1956

27

14

B1

7A.9

75.0

75.5

75.5

75.6

76.0

76.5

12.2

12.1

11.6

11.6

11.5

11.1

10.6

50

36

20

20

34

50

75.3

75.3

75.7

76.4

76.5

76.9

76.0

79.7

11.8

11.8

11.4

10.7

10.6

20.2

9.1

2.4

50

39

21

22

34

40

45

PC

VOID

See

80.6

65

50

75.2

75.6

76.2

76.8

77.2

77.6

80.0

80.0

10.0

9.6

9.0

8.4

8.0

7.6

5.2

5.2

50

33

19

18

24

29

34

82.4

80.4

80.7

81.1

81.0

28

4.8

4.5

4.1

4.2

67

64

62

50

42

75.4

75.5

75.6

76.6

76.8

77.2

77.7

80.5

9.8

9.7

9.6

8.6

8.4

8.0

7.5

4.7

50

35

18

13

21

26

32

81.6

80.9

81.0

81.3

81.1

3.6

4.3

4.2

3.9

4.1

65

61

56

46

36

Sta + π - Elev

885.17

20+50

✓

21

✓

+50

BM

2.81

882.36

882.38

Jan 17, 1956

28

14

RT

75.3	75.6	75.4	76.3	76.9	78.6	79.5	80.3
9.9	9.6	9.8	8.9	8.3	6.6	5.7	4.9
50	33	18		14	22	27	33

81.7	81.1	81.2	81.4	80.9
3.5	4.1	4.0	3.8	4.3
69	65	61	50	39

75.2	75.0	75.5	76.1	77.2	79.2	80.1	80.3
10.0	10.2	9.7	9.1	8.0	6.0	5.1	4.9
50	38	19		18	27	36	44

82.6	81.1	81.2	81.5	81.5	80.6
2.6	4.1	4.0	3.7	3.7	4.6
84	80	75	69	59	49

75.2	75.1	75.4	76.0	76.4	76.7	78.9	79.7
10.0	10.1	9.8	9.2	8.8	8.5	6.3	5.5
50	35	20		17	26	33	40

81.7	81.4	81.5	81.9	81.4	80.3	80.0
3.5	3.8	3.7	3.3	3.8	4.9	5.2
100	96	89	82	69	57	48

Spike in P.P. at ent to Prince of Wales Club

Sta + π - Elev

885.17

22

17.4

✓

+50

✓

23

2 Jan 22, 1956

29

$\frac{15.2}{10.0}$ $\frac{15.2}{10.0}$ $\frac{15.8}{9.4}$ $\frac{16.7}{8.5}$ $\frac{17.1}{8.1}$ $\frac{17.4}{7.8}$ $\frac{19.5}{5.7}$ $\frac{19.8}{5.4}$
 50 43 24 17 30 38 47

$\frac{82.5}{2.7}$ $\frac{81.8}{3.4}$ $\frac{80.8}{4.4}$ $\frac{80.1}{5.1}$
 100 80 66 55

$\frac{75.6}{9.6}$ $\frac{75.8}{9.4}$ $\frac{76.4}{8.8}$ $\frac{76.5}{8.7}$ $\frac{77.9}{8.4}$ $\frac{78.3}{6.9}$ $\frac{79.4}{5.8}$ $\frac{79.8}{5.4}$ $\frac{80.3}{4.9}$
 50 42 29 17 16 25 35 43

$\frac{80.7}{4.5}$ $\frac{81.6}{3.6}$ $\frac{81.6}{3.6}$ $\frac{81.1}{4.1}$
 85 73 65 55

$\frac{75.7}{9.5}$ $\frac{76.0}{9.2}$ $\frac{76.8}{8.4}$ $\frac{77.9}{7.3}$ $\frac{78.9}{6.3}$ $\frac{79.5}{5.7}$ $\frac{80.3}{4.9}$ $\frac{81.0}{4.2}$
 50 38 20 10 16 20 25

$\frac{80.8}{4.4}$ $\frac{81.2}{4.0}$ $\frac{81.5}{3.7}$ $\frac{81.6}{3.6}$
 63 55 49 36

Sta	+	x	-	Elev
-----	---	---	---	------

		885.17		
--	--	--------	--	--

23+50				
-------	--	--	--	--

✓				
---	--	--	--	--

BM	3.74	886.10	2.81	882.36 882.38
----	------	--------	------	---------------

24				
----	--	--	--	--

+50				
-----	--	--	--	--

£ Jan 17, 1954 30

76.0	76.6	77.5	78.8	80.1	80.7	81.3	81.5	81.3	81.0
9.2	8.4	7.7	6.4	5.1	4.5	3.9	3.7	3.9	4.2
50	37	22	9		4	9	19	32	38

Spike in PP at Ent to Price of Water Club

76.3	77.2	78.5	79.8	81.1	81.6	81.7	81.1	80.8	80.6	80.4
9.8	8.9	7.6	6.3	5.0	4.5	4.4	5.0	5.3	5.5	5.7
50	35	21	13	6		9	18	24	35	50

77.9	80.00	81.2	81.8	82.0	82.0	81.3	81.2	81.1	81.3
8.2	6.1	4.9	4.3	4.1	4.1	4.8	4.9	5.0	4.8
22	16	12	7		4	13	20	29	42

77.1	76.8
9.0	9.3
37	50

Top 7.02
W End Calvert Ent

Top 6.84
E. End Calvert Ent

Sta + π - Elev.

886.10

25

✓

+50

BM

3.74 882.36 882.38

Jan. 17 1956

31

11

84

78.1	78.9	81.2	82.0	82.2	81.6	81.2	81.2	80.6
8.0	7.2	4.9	4.1	3.9	4.5	4.9	4.9	5.5
26	21	16	11		11	15	24	30

40

✓

78.1	78.1
8.0	8.0
38	50

- B L 1110

79.3	80.4	82.2	82.6	82.7	82.1	81.6	81.6	80.7	80.7
6.8	5.7	3.9	3.5	3.4	4.0	4.5	4.5	5.4	5.4
26	19	15	9		9	16	20	27	35

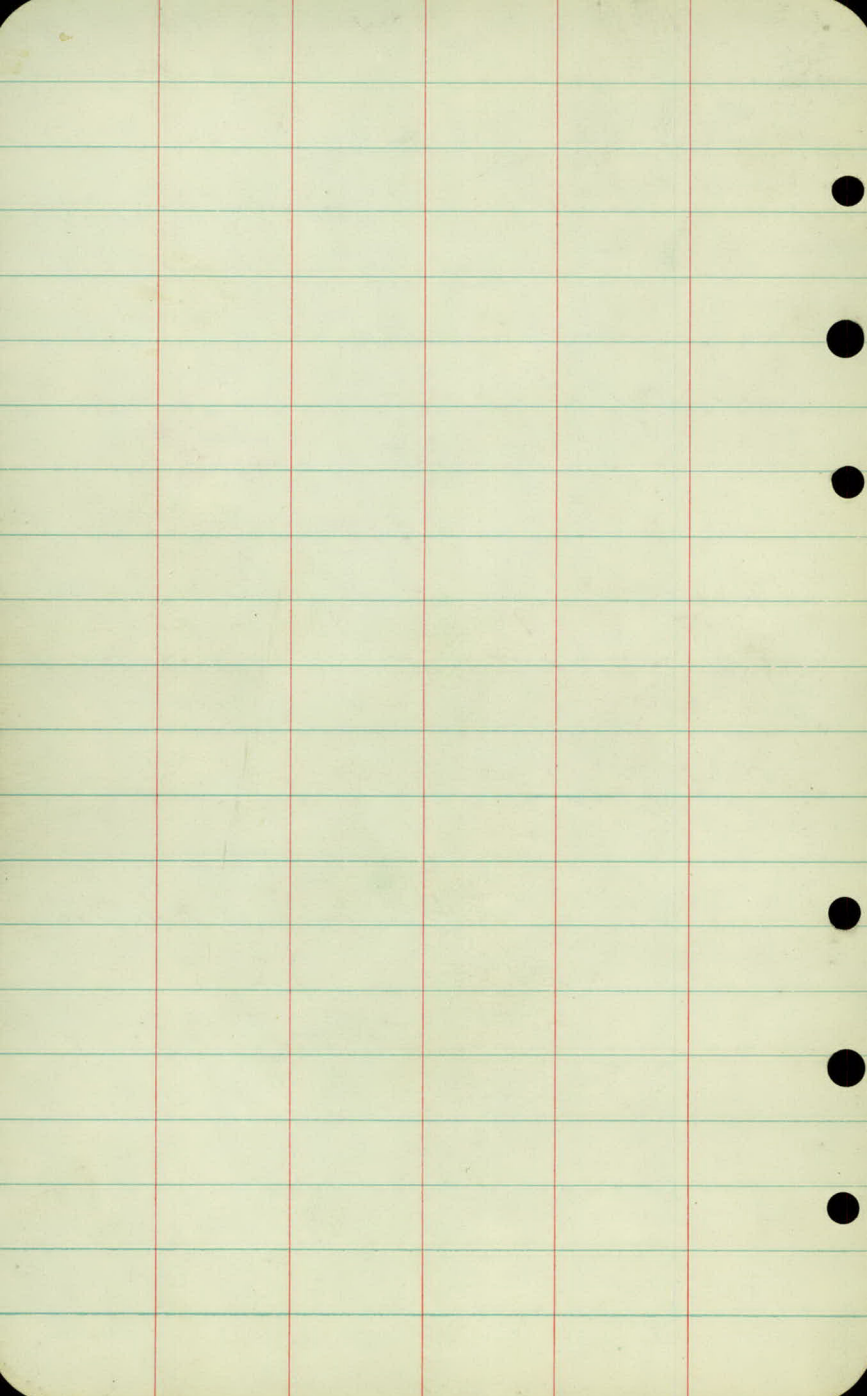
79.4	79.9
6.7	6.2
39	50

walk

✓

Spike in P.P. at Ent to Prince of Wales Club

25 160.56
2 13.72
27 54.92



FK
LC
AB
CW

Jan 24, 1956
Cold 12°

32

X-section Extensions

Void see 'B' Line

Sta	+	Σ	-	Elev
BM	7.08	888.90		881.82

0+00

+50

+50

+78

2

2

Jan 24, 1956

33

st

Top Conc Headwall Outlet N. End Lake Johanna

78.3	77.1	76.1	75.9
10.6	11.8	12.8	13.0
50	65	82	90

✓

77.4	76.3	75.9
11.5	12.4	13.0
60	95	94

✓

78.9	77.0	76.1	75.9
10.0	11.9	12.8	13.0
60	76	90	100

✓

80.6	79.9	78.5	77.1	76.4	75.9
83	90	10.4	11.8	12.5	13.0
64	73	78	90	100	114

✓

81.0	80.2	78.1	77.1	76.1	75.9
7.9	8.7	10.8	11.8	12.8	13.0
69	79	85	98	114	127

✓

82.4	82.2	80.2	78.2	76.8	75.9
5.5	6.7	8.7	10.7	12.1	13.0
56	68	82	95	112	123

✓

TL

Sta	+	π	-	Elev
-----	---	-------	---	------

Sta	+	π	-	Elev
		888,90		

Sta	+	π	-	Elev
2+30				

Sta	+	π	-	Elev
+65				

Sta	+	π	-	Elev
✓				

Sta	+	π	-	Elev
3				

Sta	+	π	-	Elev
✓				

Sta	+	π	-	Elev
+43				

Jan 24, 1956

34

RT

12
£

83.9	82.8	81.4	79.8	78.0	76.6	75.9
5.0	6.1	7.5	9.1	10.9	12.3	13.0
63	72	86	95	109	124	137
TL						
84.0	83.5	83.3	82.1	81.6	79.2	77.3
4.9	5.4	5.6	6.8	7.3	9.7	11.6
55	73	78	90	95	112	129
£		TL				

✓ 75.8	76.1
131	12.8
157	146
62	51

83.8	84.0	83.5	83.2	82.6	80.3	78.4
5.1	4.9	5.4	5.7	6.3	8.6	10.5
60	65	72	86	92	95	118
£	£		TL			

✓ 75.9	76.4
13.0	12.5
170	154

130
TL

83.3	83.8	84.0	83.5	83.0	81.9	80.6
5.6	5.1	4.9	5.4	5.9	7.0	8.2
62	82	92	99	110	121	133
		£			TL	
✓ 75.9	77.1	78.3				
13.0	11.8	10.6				
182	166	150				

Sta + π - Elev

888.90

3 + 58

✓

4

✓

+23.65

BM

6.39

888.21

7.09

881.81

881.82

\$

Jan 24, 1956

35

ST

40
TL

84.5	83.5	83.9	84.1	83.6	83.0	81.6
4.4	5.4	5.0	4.8	5.3	5.9	7.3
57	70	88	100	110	120	133
			\$		TL	

✓ 75.9	76.3	77.3	79.3
13.0	12.6	11.6	9.6
200	187	172	150

82.5	83.4	83.5	83.6	84.2	83.9	83.4
6.4	5.5	5.4	5.3	4.7	5.0	5.5
64	80	89	100	114	130	144
	TL		\$			

✓ 75.9	76.0	76.3	77.3	79.1	81.3
13.0	12.9	12.6	11.6	9.8	7.6
228	221	214	200	178	159
					TL

80.7	83.2	83.4	83.3	84.2	84.0	83.6
8.2	5.7	5.5	5.6	4.7	4.9	5.3
65	84	91	100	127	142	155
		TL		133		
				\$		

✓ 75.9	76.9	78.0	79.1	81.8
13.0	12.0	10.9	9.8	7.1
234	217	200	190	172
				TL

Top Conc Headwall Outlet NE End Lake Johanna

Sta	+	π	-	Elev
-----	---	-------	---	------

		888.21		
--	--	--------	--	--

4+50				
------	--	--	--	--

	π			
--	-------	--	--	--

✓				
---	--	--	--	--

5				
---	--	--	--	--

✓				
---	--	--	--	--

+ 50				
------	--	--	--	--

FA
LC
AB
CW

£

Jan 25, 1956

36

BT

78.1	79.3	81.9	81.3	83.2	83.6	84.2
10.1	8.9	6.3	4.9	5.0	4.6	4.0
55	77	88	100	115	127	143
			TL			£

75.9	75.9	76.9	77.8	79.5	81.6	83.5	84.0
12.3	12.3	11.3	10.4	8.7	6.4	4.7	4.2
100	246	232	219	200	187	173	157
				TL			

77.4	78.6	81.1	83.2	83.4	83.2	84.0	84.2
10.8	9.6	7.1	5.0	4.8	5.0	4.2	4.0
70	89	100	110	119	129	148	156
			TL				£

75.9	76.3	77.0	78.4	81.1	82.7	83.9	84.0
12.3	11.9	11.2	9.8	6.8	5.5	4.3	4.2
266	250	238	221	200	191	178	167
					TL		

77.0	78.1	78.6	80.1	83.0	83.1	84.3
11.2	10.1	9.6	7.8	5.2	4.8	3.9
66	93	100	110	127	144	169
				TL		£

75.9	76.0	77.2	78.7	81.2	83.1	84.0
12.3	12.2	11.0	9.5	7.0	5.1	4.2
278	263	246	228	214	200	181
					TL	

Sta + π - Elev

888.21

6 + 50

✓

7 + 50

✓

7

£

Jan 25, 1956

37

81

76.9	77.8	79.1	82.4	83.4	83.5
11.3	10.4	9.1	5.8	4.8	4.7
70	97	116	131	148	155
		TL			

75.9	76.9	78.1	81.5	83.6	83.7	84.3
12.3	11.3	10.1	6.7	4.6	4.5	3.9
281	257	241	223	200	191	178
			TL			£

76.8	77.7	78.4	80.0	82.3	83.5	83.1
11.4	10.5	9.8	8.2	5.9	4.7	5.1
75	100	113	126	137	148	162
				TL		

75.7	76.1	77.4	79.5	83.2	83.6	84.2	83.9
12.5	12.1	10.8	8.7	5.0	4.6	4.0	4.3
292	275	255	237	216	200	188	175
			TL			£	

76.8	77.6	78.9	80.3	82.4	83.0	83.0
11.4	10.6	9.3	7.9	5.8	5.2	5.2
76	100	116	127	138	152	166
				TL		

76.9	78.4	78.9	82.7	83.5	84.1	84.0
11.3	9.8	8.3	5.5	4.7	4.1	4.2
264	244	234	219	205	193	183
			TL		£	

→ 75.9
12.3
284

Sta + π - Elev

888.21

7+50

✓

✓

+94

8

2

Jan 25, 1956

38

ST

74.9	74.8	75.2	76.2	78.3	79.9
13.3	13.4	13.0	12.0	9.9	8.3
53	67	85	100	114	126

78.5	82.7	83.1	84.2	83.8	83.0	83.1	82.1
9.7	5.5	A.8	A.0	A.4	5.2	5.1	5.8
242	224	213	200	188	174	160	141
	TL		£				

77.0	75.9
11.2	12.3
261	279

75.3
12.78
FL 24 SCP
122

75.4	75.6	76.2	78.3	80.0	82.3
12.8	12.6	12.00	9.9	8.2	5.9
60	84	100	114	127	139
					TL

77.6	78.5	81.8	83.4	84.1	83.7	83.0	83.0
10.6	9.7	6.4	A.8	A.1	4.5	5.2	5.2
252	234	223	213	200	192	179	165
				£			

76.2	75.8
12.0	12.4
273	289

Sta + π - Elev

888.21

8401

+50

✓

9

✓

+50

£

Jan 25, 1956

39

RT

Hdwall Lake Outlet 223

75.9	76.1	76.9	79.1	82.1	82.8	83.5
12.3	12.1	11.3	9.1	6.1	5.4	4.7
60	78	100	117	126	261	180
				TL		

75.9	76.6	78.8	82.9	83.6	84.2	83.9	83.2
12.3	11.6	10.0	5.3	4.6	4.0	4.3	5.0
285	265	243	224	215	200	194	186
		TL			£		

77.5	77.6	78.2	79.9	81.9	82.8	83.3
10.7	10.6	10.0	8.3	6.3	5.4	4.9
58	79	100	116	131	155	169
				TL		

75.9	76.2	77.2	79.8	82.3	83.7	84.2	83.6	83.3
12.3	12.0	11.0	8.4	5.9	4.5	4.0	4.6	4.9
283	266	249	233	221	212	200	190	181
		TL				£		

78.5	78.9	79.2	80.4	80.2	81.2	82.9
9.7	9.3	9.0	7.8	8.0	7.0	5.3
66	86	100	129	150	163	174
					TL	

75.9	77.1	79.9	83.5	84.0	84.5	83.8
12.3	11.1	8.3	4.7	4.2	3.7	4.4
257	238	219	207	200	191	182
			TL			

Sta + π - Elev

888.21

10

BNI 10.08 891.90 6.39 881.82 881.82

259
16

150

✓

✓

11

FK
AB
CW

£

Jan 25, 1956
Feb 7, 1956
BT

40

77.9	78.4	79.6	80.6	81.9	83.6	84.6
10.3	9.8	8.6	7.6	6.3	4.6	3.6
57	77	100	121	143	165	175

TL

75.9	76.2	77.5	80.6	83.1	84.1	84.9
12.3	12.0	10.7	7.6	5.1	4.1	3.3
257	247	228	215	200	197	185

Top Conc Headwall Outlet N. End Lake Johanna £

77.9	78.7	79.1	79.7	80.3	81.3
14.0	13.2	12.8	12.2	11.6	10.6
61	77	94	100	160	131

82.7	84.7	85.6	85.2	83.7	82.7	82.3
9.2	7.2	6.3	6.7	8.2	9.2	9.6
200	195	184	174	165	157	148

TL £ TL

80.9	78.3	77.0	76.0	75.9
11.0	13.6	14.9	15.9	16.0
210	219	233	247	258

80.2	80.8	81.4	82.3	83.2	84.6
11.7	11.1	10.5	9.6	8.9	7.3
60	78	100	124	150	168

TL

Sta + π L - Elev

891.90

11

✓

+31

✓

✓

+61

£

Feb 7, 1956

41

BT

85.3	85.8	86.2	85.9	85.5	82.6
6.4	6.1	5.7	6.0	6.4	9.3
180	186	195	200	208	216

£

75.9	76.0	76.9	78.6
16.0	15.9	15.0	13.3
273	257	242	229

TL

83.0	84.6	85.8	87.0	87.8	86.0	86.0
8.9	7.3	6.1	4.9	4.1	5.9	5.9
61	81	100	119	133	151	172

TL

83.1	86.2	86.8	87.0	86.3	86.3	85.7
8.8	5.7	5.1	4.9	5.4	5.6	6.2
228	221	216	204	196	191	182

TL

80.4	77.6	76.1	75.9
11.5	14.3	15.8	16.0
240	253	272	288

86.6	88.0	89.4	89.8	89.3	88.1	87.7
5.3	3.9	2.5	2.1	2.6	3.8	4.2
60	75	95	100	128	149	169

TL

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		891.90		
--	--	--------	--	--

11+61				
-------	--	--	--	--

✓				
---	--	--	--	--

+8/32	P.C.			
-------	------	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

12				
----	--	--	--	--

£

Feb 7, 1956

42

RT

87.1	87.0	87.1	87.6	87.5	87.0	83.3
4.8	4.9	4.8	4.3	4.4	4.9	8.6
185	196	200	211	222	227	236
£						

75.7	76.1	77.9	80.0
16.2	15.8	14.0	11.9
300	284	264	253
TL			

89.2	89.7	90.5	90.5	89.4	88.3	87.5
2.7	2.2	1.4	1.4	2.5	3.6	4.4
60	79	100	123	140	163	187
TL						

82.9	87.1	87.8	87.9	87.3	87.1
9.0	4.8	4.1	4.0	4.6	4.8
249	238	230	219	209	200
£					

80.5	78.1	76.6	76.1	75.8
11.4	13.8	15.3	15.8	18.1
268	281	291	300	314
TL				

88.9	89.3	90.4	90.5	89.2	88.3	87.5
3.0	2.6	1.5	1.4	2.7	3.6	4.4
60	82	100	124	128	169	195
TL						

Sta

+

π

89/90

12

✓

+50

✓

✓

10
8
10
10
8

7
5
10
10

13

£

Feb 7, 1956

43

81

87.3	87.5	88.1	88.0	87.6	83.7	81.6
46	4.4	38	39	4.3	8.2	10.3
204	213	222	235	246	256	276
		£			TL	

75.9	77.5
16.0	14.4
314	297

84.5	85.0	85.3	85.6	84.8	83.8	85.3
7.4	6.9	6.6	6.3	7.1	8.1	6.6
60	87	100	121	142	160	191

89.1	88.5	88.1	87.5	86.3
2.5	2.8	3.4	3.8	4.4
250	240	229	218	210
	£			

89.2	89.1	86.0	84.3	82.3	77.9	76.3	75.8
2.7	2.8	5.9	7.6	9.6	14.0	15.6	16.1
259	269	278	291	299	313	328	342
	TL						

80.4	81.0	81.7	82.6	84.3	84.0	85.5
11.5	10.9	10.2	9.3	7.6	7.9	6.4
60	83	100	126	155	174	200
						£

Sta + π - E/ev.

891.90

13

✓

TP 4.97 893.60 3.27 888.63

+50

✓

✓

14

2

RT

44

86.8	88.6	89.0	89.4	90.0	90.2
5.1	3.3	2.9	2.5	1.9	1.7
218	229	236	243	254	264
TL				E	

75.8	76.6	78.5	81.4	87.0	88.7
16.1	15.3	13.4	10.5	4.9	3.2
360	343	329	321	304	294

78.2	79.5	81.7	83.7	85.3	86.9	87.5
15.4	14.1	11.9	9.9	8.3	6.7	6.1
60	85	110	136	160	194	215

89.0	90.8	90.6	90.1	90.0	91.1	89.6
4.6	2.8	3.0	3.5	3.6	2.5	4.0
303	281	268	259	253	246	240
			E			TL

89.5	80.4	77.3	76.0	75.4	75.4
4.1	13.2	16.3	17.6	18.2	18.2
317	334	344	359	375	385

76.1	76.9	78.5	80.9	82.9	84.4
17.5	16.7	15.1	12.7	10.7	9.2
60	92	116	155	186	200

Sta + π - Elev

893.60

14

✓

TP 2.97 892.66 3.91 889.69

+50

885.66

✓

✓

15

FX
LC
AB
CW

£

Feb. 7, 1956
Feb 14, 1956
RT

45

86.8	88.8	91.1	90.1	90.2	90.8
6.8	48	2.5	3.5	3.4	2.8
226	238	252	258	262	273
	TL				£

75.8	76.2	78.1	82.3	86.5	90.4	90.5	91.0
17.8	17.4	15.5	11.3	7.1	3.2	3.1	2.6
370	351	333	323	317	310	300	281
Top 1x2x4' W Red at 1/4 1/4 line N Edge Johnson Blvd.							

75.5	75.5	75.5	76.2	78.5	80.5
17.2	17.2	17.2	16.5	14.2	12.2
67	87	100	123	154	177

90.4	90.4	89.8	88.2	86.9	83.7	81.7
2.3	2.3	2.9	4.5	5.8	9.0	11.0
292	279	269	256	244	222	200
	£			TL		

89.9	88.9	83.8	77.3	75.7	75.7
2.8	3.8	8.9	15.4	17.0	17.0
298	312	321	343	366	392
			TL		

75.1	75.1	75.4	77.3	79.4	81.5
17.6	17.6	17.3	15.4	13.3	11.2
78	100	130	158	180	200

Sta + π - Elev

892.66

15

✓

+49.2 along $\frac{1}{4}$ $\frac{1}{4}$ Line

7.70 884.96 889.89

2

Feb 14, 1956

46

Rt

86.2	89.6	90.4	89.3	89.7	90.3	90.4
6.5	31	23	3.4	3.0	2.4	23
223	247	260	268	272	282	290
	TL				£	

75.7	75.9	77.9	84.2	90.5	89.6	89.9
17.0	168	14.8	8.5	2.2	3.1	2.8
375	352	334	319	307	300	296
			TL			

74.8	74.8	74.8	75.0	75.5	76.2
17.9	17.9	17.9	17.7	17.2	16.5
83	100	133	153	173	195

88.3	87.4	87.0	86.5	84.3	80.6	79.2
4.4	5.3	5.7	6.2	8.4	12.1	13.5
285	275	271	259	252	239	219
£				TL		

88.3	88.0	88.0	79.1	76.1	75.9	75.7
4.4	4.7	4.7	13.6	16.6	16.8	17.0
298	300	310	331	351	372	391
			TL			

Garage floor Myers Garage

Sta	+	π	-	Elev
BM		4.62	887.00	882.38

25+50			4.3	82.7	82.7
-------	--	--	-----	------	------

+72.5

26+22.5

+72.5

27+22.5

+54.25 P.T.

28

Feb 14, 1956

47

Spike in P.P. at Ent to Lakeview Terrace Club.

83.0

7.0

83.6

3.4

84.9

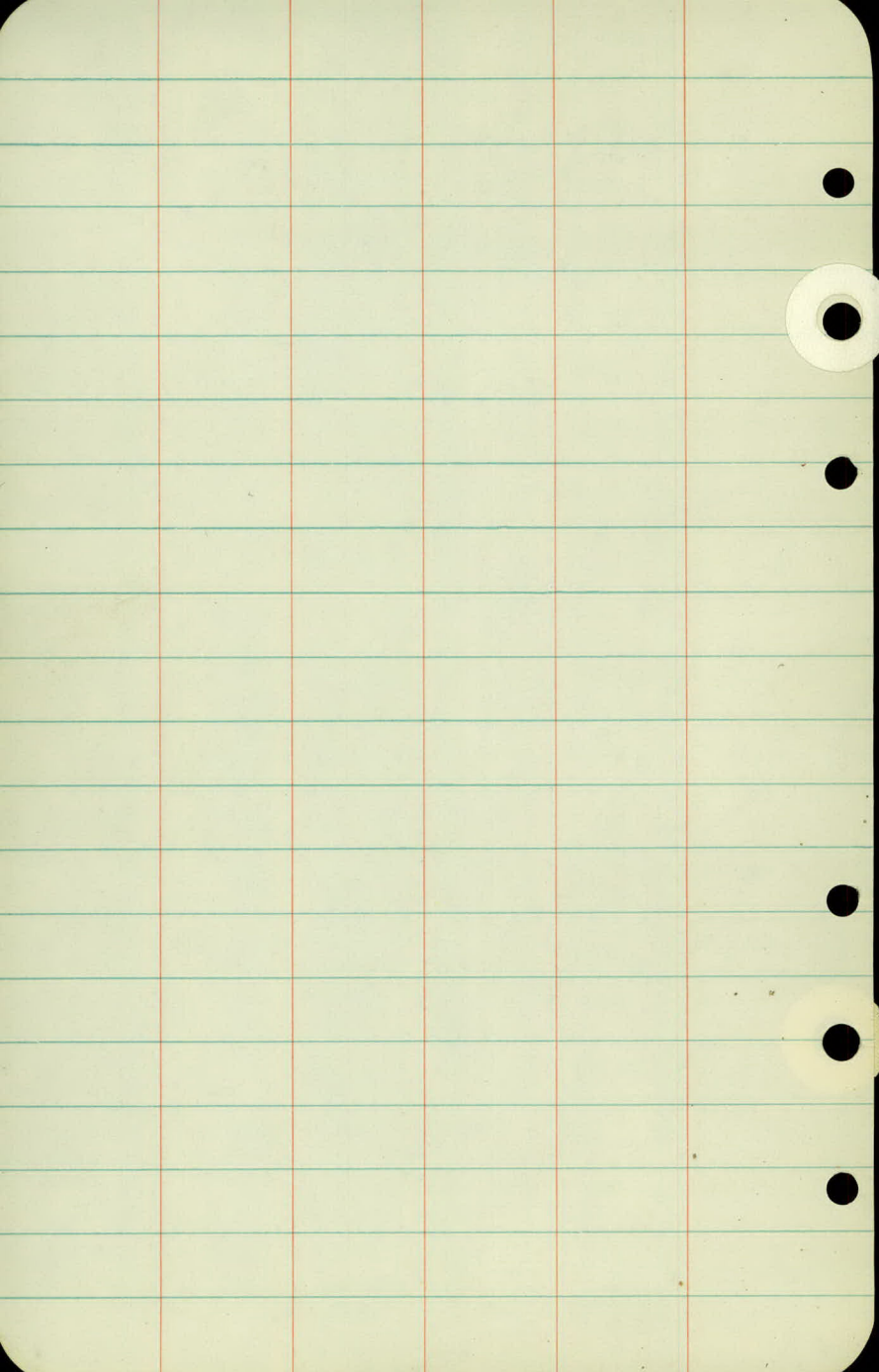
2.1

86.2

0.8

87.0

0.0



Schmidt Park
Soundings

Push Rod

Sta	Depth	at
4+50	3'	20' left
5+50	13'	£
6+50	6'	£
7	5'	£
14	7'	£
15	33'	£
16	25' Object?	£
17	35'	£
18	34'	£

FX
LC
AB sta
CW

Feb. 20, 1956
Depth Cold Clear 70

49,
b

19

6'

£

20

8'

£

21

5'

£

22

3'

£

14+50

7'

50' RT

15

11'

50' RT

16

28'

50' RT

16

26'

100' RT

17

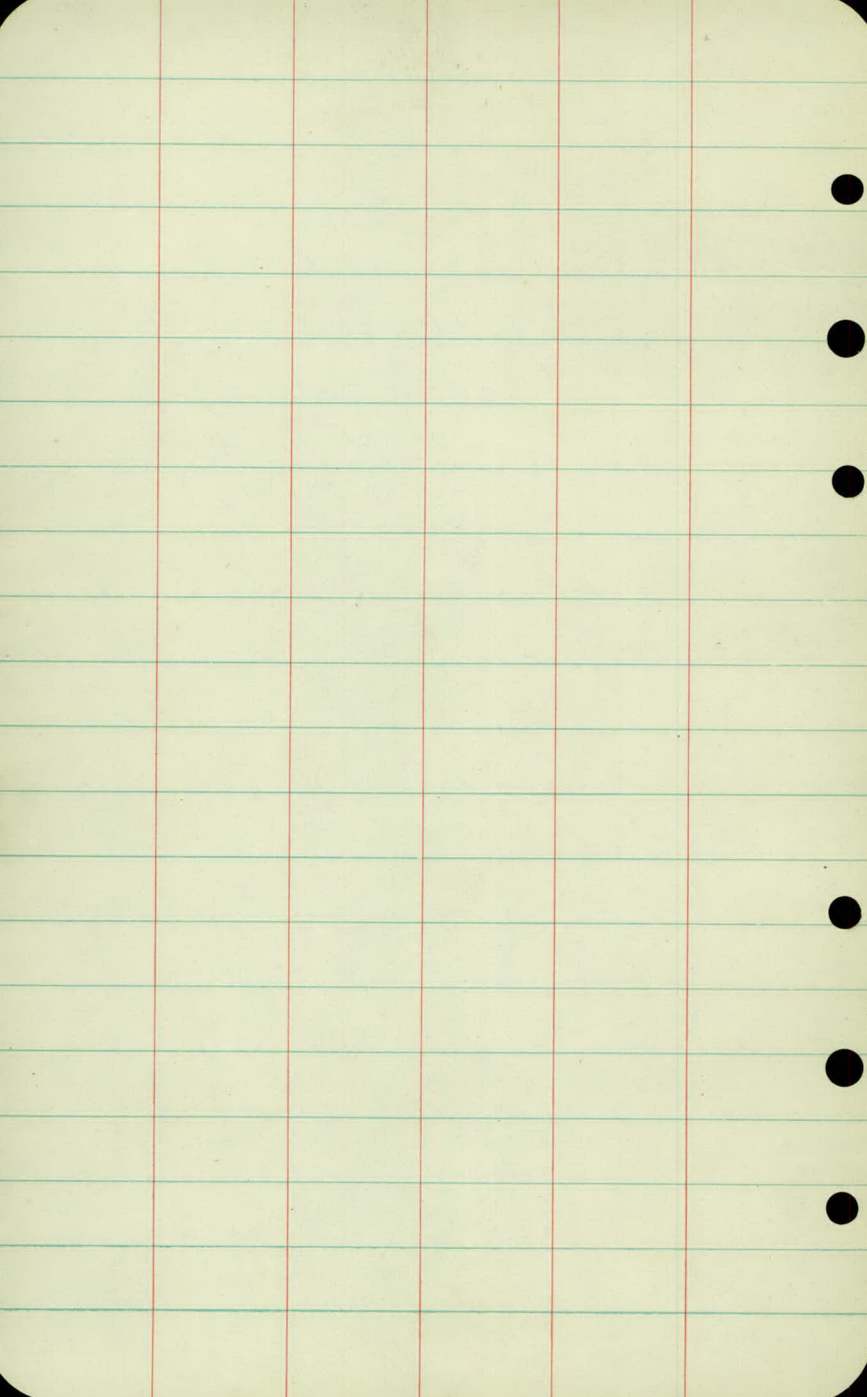
32+

50' RT

17

21'

100' RT



Feb 20, 1956

50c

Schmidt Park

Soundings

Push Rod

Sta

Depth

Loc.

4+50

8'

40' Lt

5

16'

12' Rt

5

20'

40' Lt

5+50

24'

40' Lt

6

22'

40' Lt

+50

13'

40' Lt

7

6'

40' Lt

7

4'

40' R

6+50

8'

35' R

Feb 20, 1956

56

Sta

Depth

Loc

6

8'

30' R

5+50

11'

25' R

18

10'

50' R

Object

AZ Stadia

X at P.T. Sta 9+05.08

to P.L. Sta 7+ 180°00'

to Sta 12+50 0°00'

L P.P. 265°40' 534

N End Lake Outlet Culvert 120°51' 155 ✓

S " " " & Headwall 101°40' 233 ✓

P.P. 134°30' 445 ✓

" 130°10' 295 ✓

" 98°50' 185 ✓

" 58°20' 233 ✓

" 45°05' 304 ✓

G.P. 39°05' 297 ✓

P.P. 38°00' 427 ✓

" 33°40' 558 ✓

" 29°05' 652 ✓

FK
Lc
DIST.

VERT.
ANGLE

ROD
EQUIV.

Feb 20, 1956
Feb 28, 1956
ROD DIFF.

52
ELEV.

H.I. = 5.4

+5°08'

6.9

130°
349
950

OBJECT

Sta 5 6' Lt.

Feet

Material

0 -15

15-16

16-17

17-18

Auger Soundings

Peat

Sand

Gumbo

FK
LC
AB

Jan. 23, 1956

54

Sta 6

Feet

Material

Auger Soundings

Peat

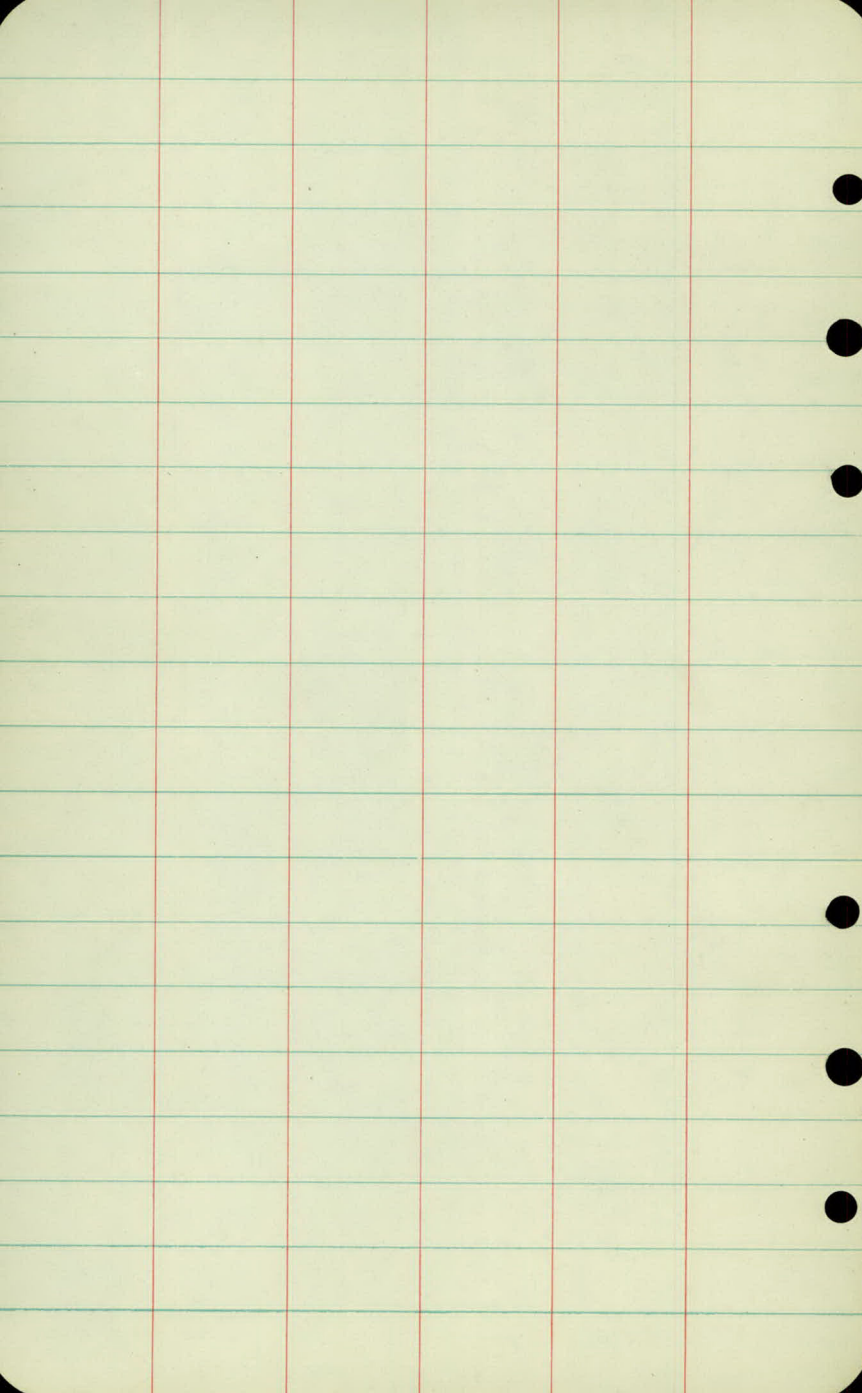
10-11

11-12

12-13

Sand

~~Sta 6 40 ft~~



DIST.

VERT.
ANGLEROD
EQUIV.

ROD

DIFF.

ELEV.

55

Lake Johanna Blvd.

Meyers House & Garage

Location

OBJECT

AZ.

STADIA

K at sta 17+00

to sta 19+00

0°00'

N.W. Cor. Gar.

61°38' 221'

N.E. " "

56°01' 217'

N.E. Cor H0

55°06' 239'

N.W. " "

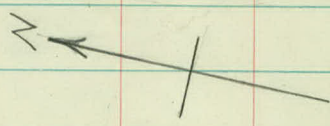
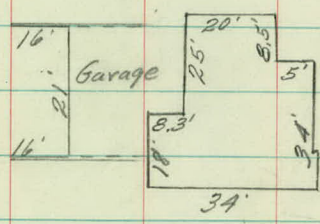
65°20' 235'

Feb 25 1956

56

FA
LC
AB
CW

VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
----------------	---------------	-----	-------	-------



OBJECT

AZ.

STADIA

Johanna Blvd No

Alignment Change

"B" Line

Sta Point ΔL ΔR

POST

15+49.20 P.O.T. $\frac{1}{4}$ $\frac{1}{4}$ Line

157.27' P.T.

7° 55'

+50

7° 44'

13

6° 29'

+50

5° 14' $\Delta = 15050'$

12

3° 59' $D = 5'$

12+00 P.I.

15° 50' $T = 159.40'$

+50

2° 44' $L = 316.67'$

11

1° 29' $R = 1146.28'$

+50

0° 14'

10+40.60 P.C. V

0° 00'

FX
LC
AB
CW

Feb 21, 1956

58

Iron
0' 22.1

14" Line

P.O.T. 1955 Survey

1/4 1/4 Line

74.42

10' 10 3/4

73.12 14"0

Boat spike

93.00

83.21

84"0

12' 4.0

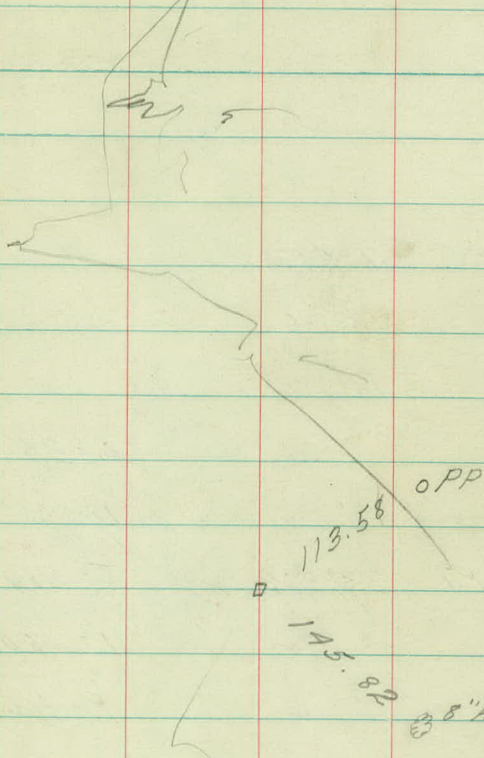
Sta Point ΔL ΔR

+01.92 ^{ok.} P.T.		12° 01'	
+01.92			
19		11° 57½'	
+50		10° 27½'	
18		8° 57½'	$\Delta = 24° 02'$
+50		7° 27½'	$D = 6°$
17+04.72	P.I.	24° 02'	$T = $ ^{ok.} 203.36 ✓
17		5° 57½'	$L = $ ^{.56} 400.55
+50		4° 27½'	$R = 955.37$
16		2° 57½'	
+50		1° 27½'	
15+01.36 ^{ok.} P.C.		0° 00'	↓

FX
LAC
AB
CW

Feb 21, 1956
Feb 24, 1956
Wet Drizzle 32°

593



2x2 Hub

8" Ash

Sta Point ΔH ΔBt

~~2410502~~

~~+05.72~~
~~+05.73~~

24

P.T. $16^{\circ} 49 \frac{3}{4}'$

$16^{\circ} 36'$

+50

$14^{\circ} 36'$

23

$12^{\circ} 36'$

$\Delta = 33^{\circ} 39 \frac{1}{2}'$

+50

$10^{\circ} 36'$

$D = 8^{\circ}$

~~2210210~~

~~2+01.80~~

P.I. $33^{\circ} 39 \frac{1}{2}'$

$T = 216.81$ ✓

22

$8^{\circ} 36'$

$L = 420.73$

+50

$6^{\circ} 36'$

$R = 716.78$

21

$4^{\circ} 36'$

+50

$2^{\circ} 36'$

20

$0^{\circ} 36'$

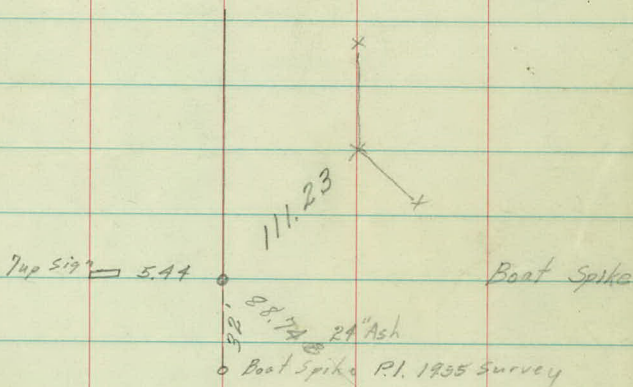
~~1915507~~

~~19+84.99~~

P.C. $0^{\circ} 00'$

85.00

Feb 24, 1956 604



Sta Point ΔL ΔR

~~175.33~~

+75.34 PT

+50

27

~~26170.28~~

~~26+70.48~~ P.I.

+50

26

~~25+61.59~~

~~25+61.59~~ PC

6.58

$12^{\circ} 49' \Delta = 25^{\circ} 39' R$

$11^{\circ} 18' D = 12^{\circ}$

$8^{\circ} 18' T = \overset{108.90}{\cancel{108.89}}$

$L = 213.75'$

$5^{\circ} 18' R = 478.34'$

$2^{\circ} 18'$

$0^{\circ} 00'$

FK
LC
AB
MH

March 1, 1956

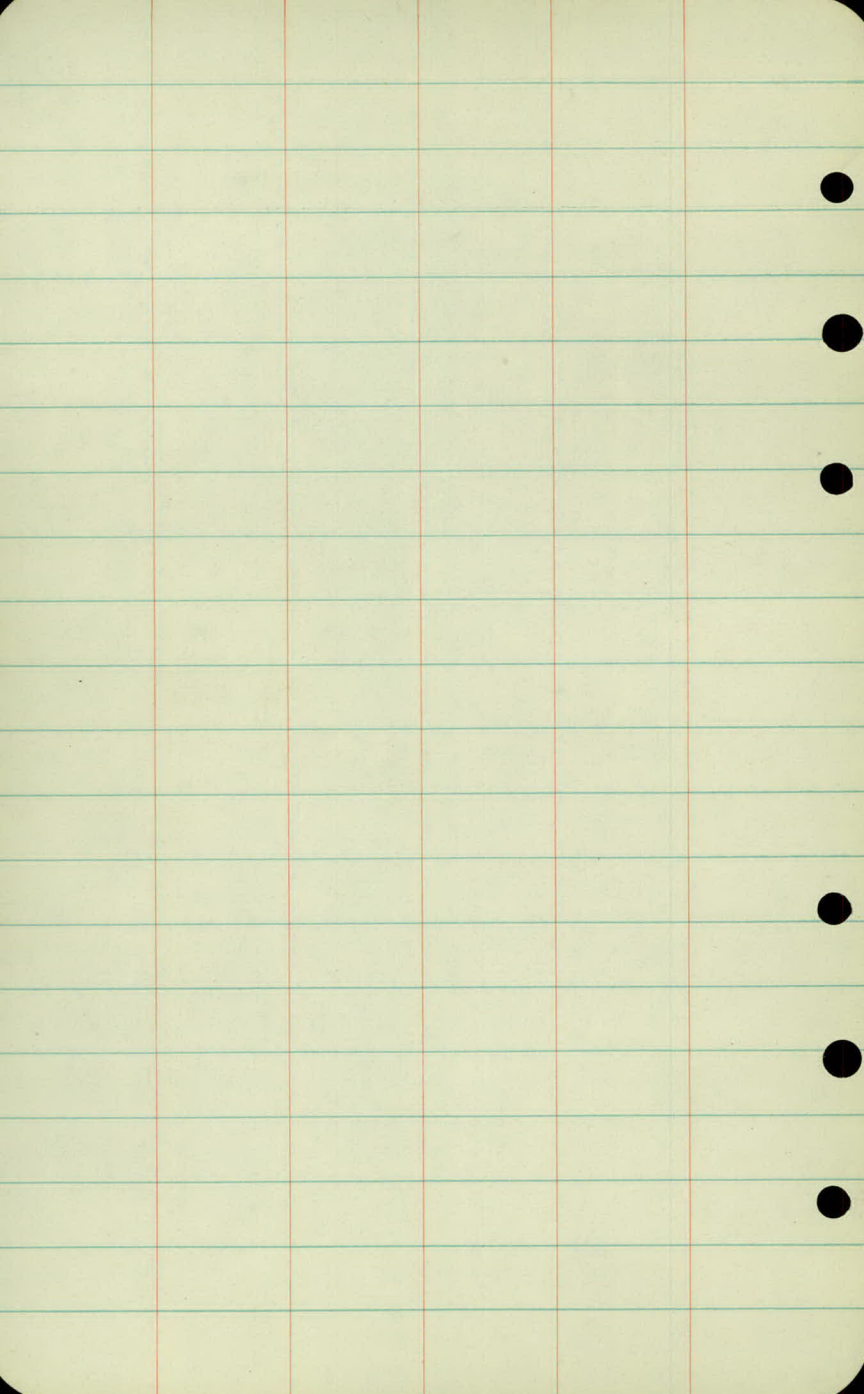
60a

TP 29.22

38.33

OPP

Spike



£ "B" Line Distances

from

old £ (1955 Survey)

Sta

Dist. Rt.

10+50

0.1'

11

1.2'

+31*

3.5

+50

5.6

+61*

7.0

+91*

9.5'

12

11.0

+50

18.2

13

26.8

+16*

30.0

+50

36.8

14

47.1

+50

57.3

15

65.1

FK
LC
AB
CW

Feb 28, 1956
Cold Clear 5°
Feb 29, 1956

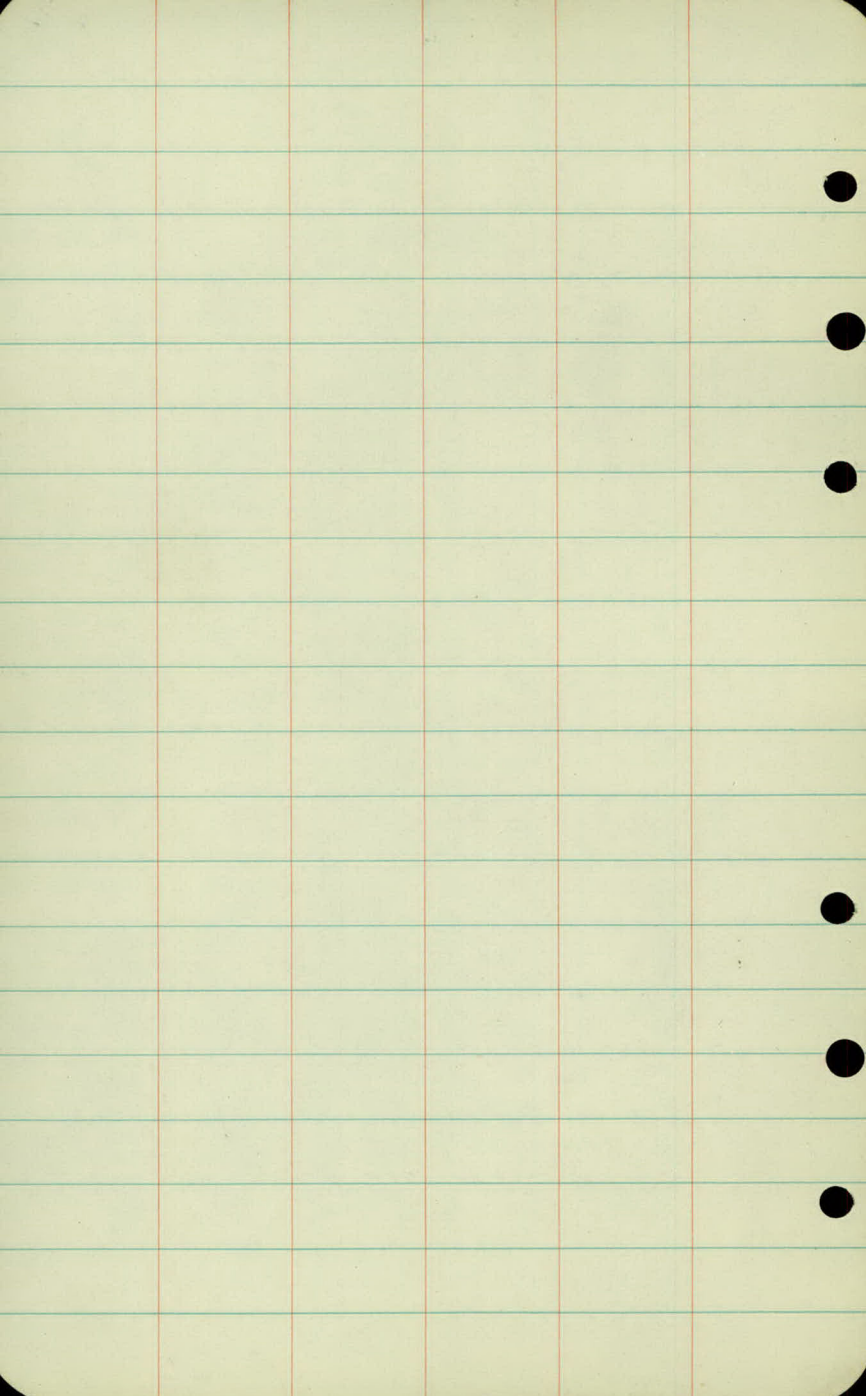
626

+31

+61

181

+16



Feb 27, 1956

637

TOPOGRAPHY

"B" Line

$$+94 \frac{PP}{181}$$

$$+06 \frac{PP}{225}$$

$$+49.20 \frac{X-Fe 113' Bl}{at Rth Ang to Post}$$

$$+18.5 \frac{Fe}{\cancel{2}} 4-5-8$$

$$+00 \frac{Swp}{60} \frac{Woods}{82}$$

$$+00 \frac{Swp}{34} +00 \frac{Woods}{67}$$

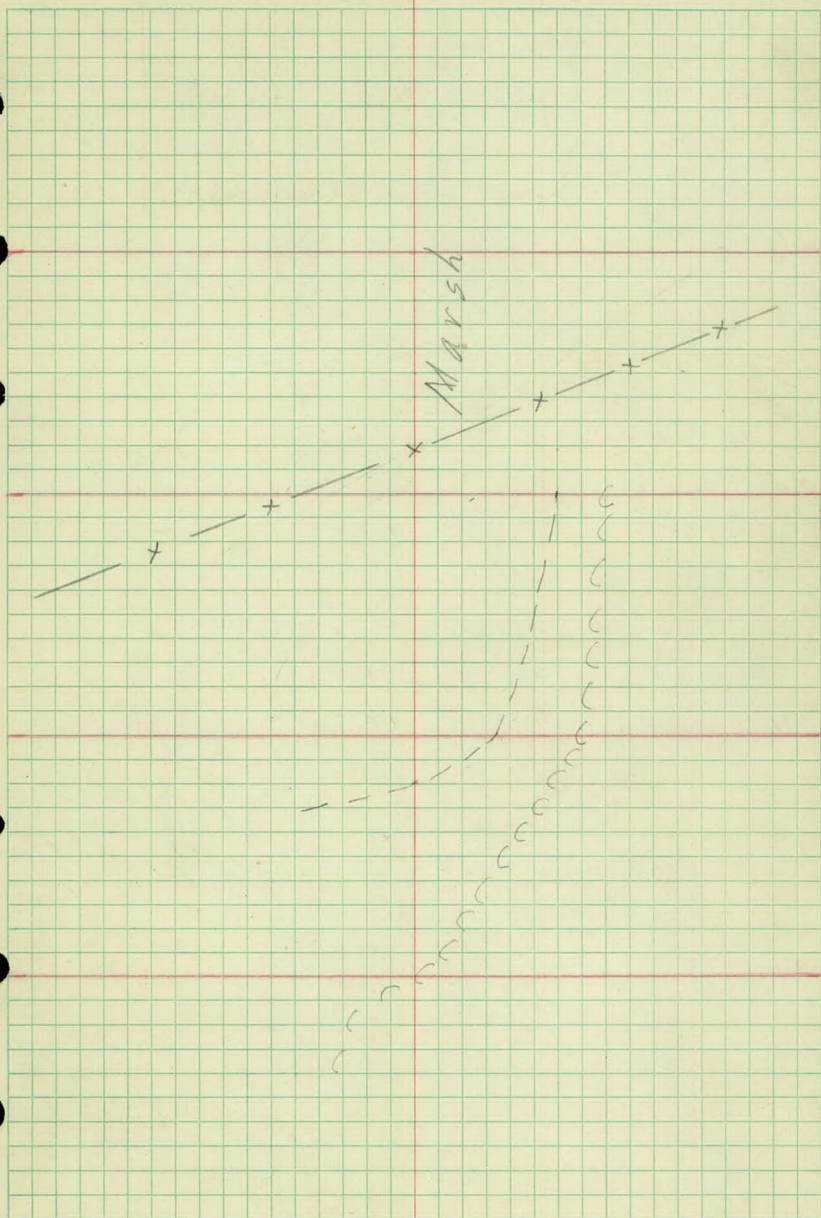
$$+80 \frac{Edge Swp}{\cancel{2}}$$

$$+50 \frac{Woods}{34}$$

$$\frac{Edge Woods}{\cancel{2}}$$

Feb 27, 1956

648



$$+53 \frac{PP}{83}$$

$$+50 \frac{Road}{39-56}$$

21

$$+100 \frac{Road}{27-50}$$

$$+50 \frac{Road}{14-36}$$

$$+13 \frac{PP}{37}$$

20

$$\frac{Road}{3-26}$$

$$+50 \frac{Road}{3-24}$$

$$+28 \frac{R Tie Fe}{RT}$$

$$+16 \frac{PP}{37}$$

19

$$\frac{Road}{+7}$$

$$+100 \frac{NECn B1/2}{51}$$

$$+38 \frac{PP}{64}$$

$$+50 \frac{BT}{22-44}$$

$$+52 \frac{NW Bldg}{658} \& Rangetie$$

18

$$+100 \frac{BT}{47}$$

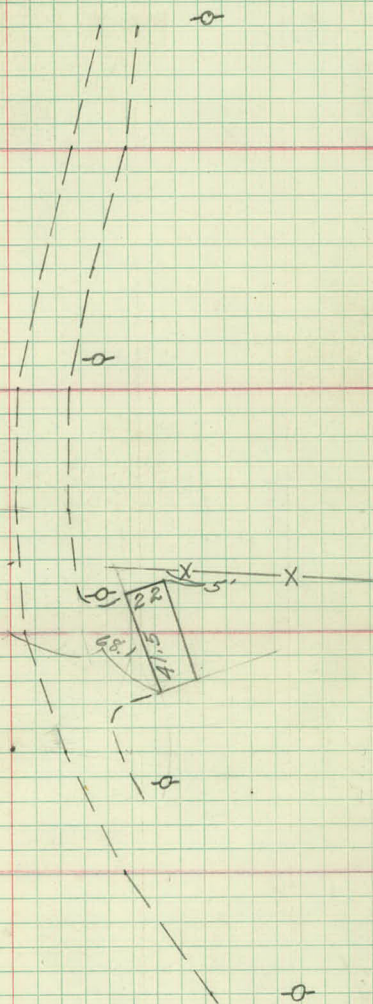
$$+50 \frac{PP}{119}$$

$$+50 \frac{Road=BT}{83}$$

17

Feb 27, 1956

65



$$+12 \frac{PP}{97}$$

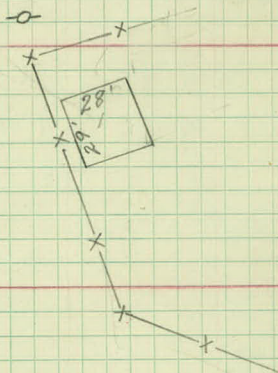
$$+184 \frac{RTic}{Fe} + 95 \frac{Fe Cor}{99}$$

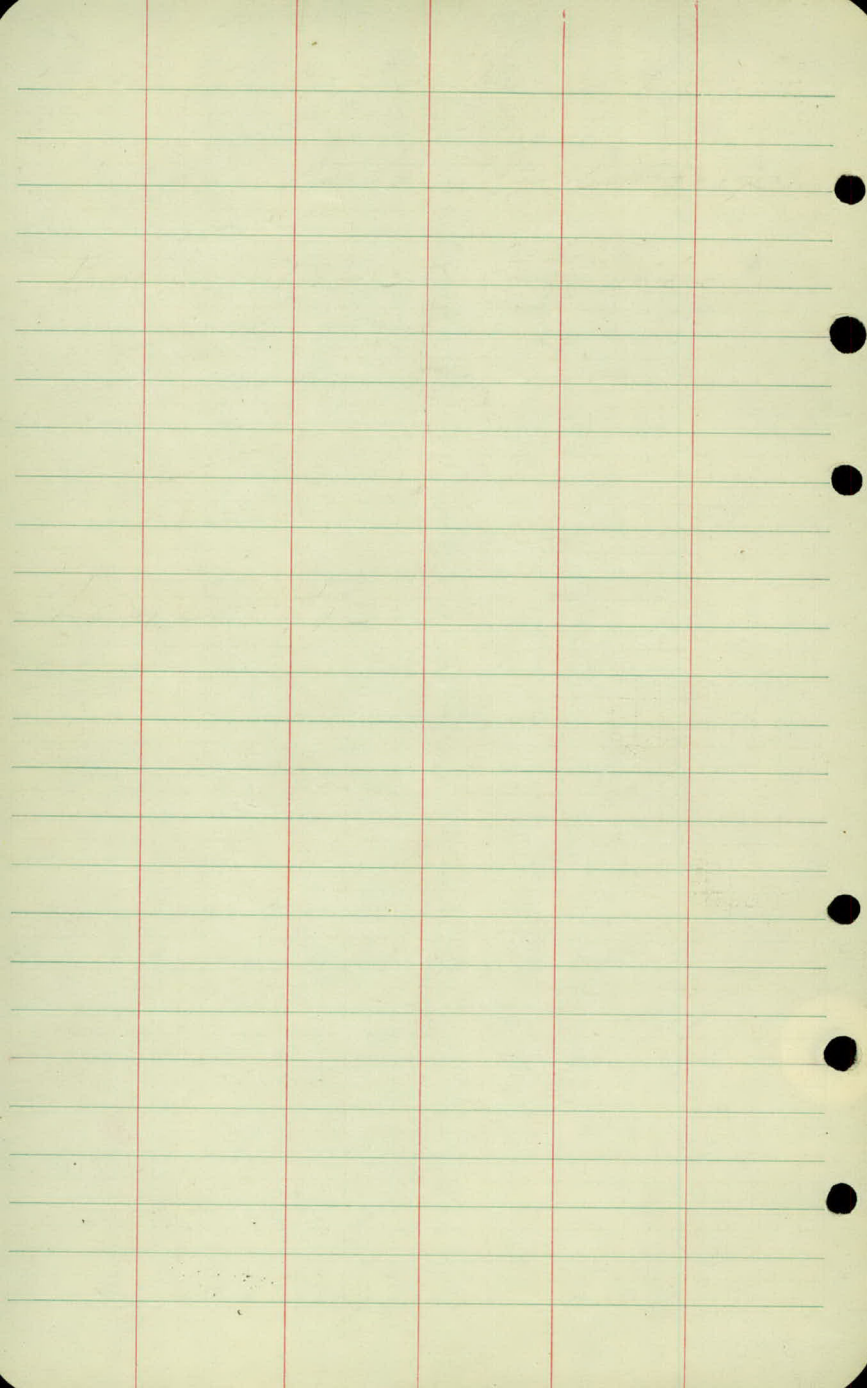
$$+30 \frac{RTic}{Ho}$$

$$+19 \frac{RTic}{Fe}$$

$$+50 \frac{NW Cor Ho}{62}$$

$$+89 \frac{Fe Cor}{76}$$





FK
LG
AB
CW

Feb 29, 1956
Cool Clear 15° a

67

x-sections

"B" Line

pages a-e

Sta	+	π	-	Elev
BM	2.09	884.47		882.38

16

+50

17

+50

18

Feb 29, 1956

68

Lt

E

Rt

Spike in PP at Entko Lakeview Terrace Club

74.7	74.7	74.7	74.7	74.7	74.5	74.7	74.6	74.8
9.8	9.8	9.8	9.8	9.8	10.0	9.8	9.9	9.7
50	39	27	15		9	21	32	50

74.6	74.6	74.5	74.6	74.9	74.7	74.7	74.7
9.9	9.9	10.0	9.9	9.6	9.8	9.8	9.8
50	40	27	12		17	32	50

74.5	74.6	74.7	74.9	75.0	75.1	75.2	75.0	75.0
10.0	9.9	9.8	9.6	9.5	9.4	9.3	9.5	9.5
50	38	26	14		9	21	34	50

74.8	75.0	75.1	75.1	75.2	75.4	75.7	76.0	76.5
9.7	9.5	9.4	9.4	9.3	9.1	8.8	8.5	8.0
50	36	34 24	14		13	26	40	50

82.3	82.4	82.2	81.1
2.2	2.1	2.3	3.4
97	85	75	65

75.0	75.0	75.4	75.5	75.9	76.4	76.2	79.9	81.3	81.8
9.5	9.5	9.1	9.0	8.6	8.1	8.3	4.6	3.2	2.7
50	39	27	15		13	25	36	44	53

81.7
28
62

Sta + π - Elev

884.47

18+50

19

+50

20

+50

21

TP

2.67 885.04

2.10

882.37

Feb 29, 1956

69

11

2

C

84

75.3	75.7	75.9	76.1	76.7	79.5	80.9	81.3	81.1	81.1
9.2	8.8	8.6	8.4	7.8	5.0	3.6	3.2	3.2	3.2
50	34	24	14		14	22	32	40	5

76.2	76.1	76.7	76.9	77.8	79.6	80.4	80.8	81.1	80.9	81.0
8.3	8.4	7.8	7.6	6.7	4.9	4.1	3.7	3.4	3.6	3.5
50	42	29	18	10		5	9	19	28	33

76.2	76.9	77.0	77.3	80.1	80.7	81.0	81.1	80.8	80.5	81.9
8.3	7.6	7.5	7.2	4.4	3.8	3.5	3.4	3.7	4.0	2.6
50	36	27	15	6		4	14	22	26	31

75.7	76.9	77.1	77.9	80.2	81.0	81.4	81.1	81.0	82.7
8.8	7.6	7.4	6.6	4.3	3.5	3.1	3.4	3.5	1.8
50	31	20	10		6	16	27	30	38

75.3	75.8	76.1	76.7	77.9	79.6	80.3	80.9	81.4	81.0	82.0
9.2	8.7	8.4	7.8	6.6	4.9	4.2	3.6	3.1	3.5	2.5
50	39	28	15	7		5	15	24	39	44

75.2	75.3	75.9	76.7	77.1	79.1	80.3	80.6	81.4	81.5
9.3	9.2	8.6	7.8	7.4	5.4	4.2	3.9	3.1	3.0
50	33	23	12		8	20	29	38	51

82.0	81.1	81.1
2.5	3.4	3.4
70	66	59

Sta + π - Elev

885.04

21+50

22

✓

+50

Feb 29, 1956

60

11

£

d R 70

74.8	74.9	75.2	75.6	76.2	76.7	77.3	79.0	80.1	80.4	81.3
102	10.1	9.8	9.4	8.8	8.3	7.7	6.0	4.9	4.6	3.7
50	42	33	23	7		12	19	29	41	51
										2

82.8	81.8	81.4	81.7
2.2	3.2	3.6	3.3
86	78	70	60

75.2	75.4	75.2	75.5	76.0	76.2	76.8	77.0	79.3	79.9
9.8	9.6	9.8	9.5	9.0	8.8	8.2	8.0	5.7	5.1
50	44	35	24	11		10	19	28	36

81.4	80.8	80.1
3.6	4.2	4.9
100	66	57
		47
		2

75.9	76.2	76.7	77.3	77.6	78.4	79.4	79.8	80.1
9.1	8.8	8.3	7.7	7.4	6.6	5.6	5.2	4.9
50	30	20	10		14	23	34	44

81.5	81.4	80.9
3.5	3.6	4.1
74	64	54
		2

Sta + π - Elev

885.04

23

✓

+50

24

24 (old) 1955

BM

2.67

882.37

Feb 29, 1936

71

H

L

0 84 71

75.7	76.4	76.4	77.9	77.5	78.0	80.1	81.0	81.4
93	86	86	71	75	70	49	40	36
50	41	24	10		9	22	31	40

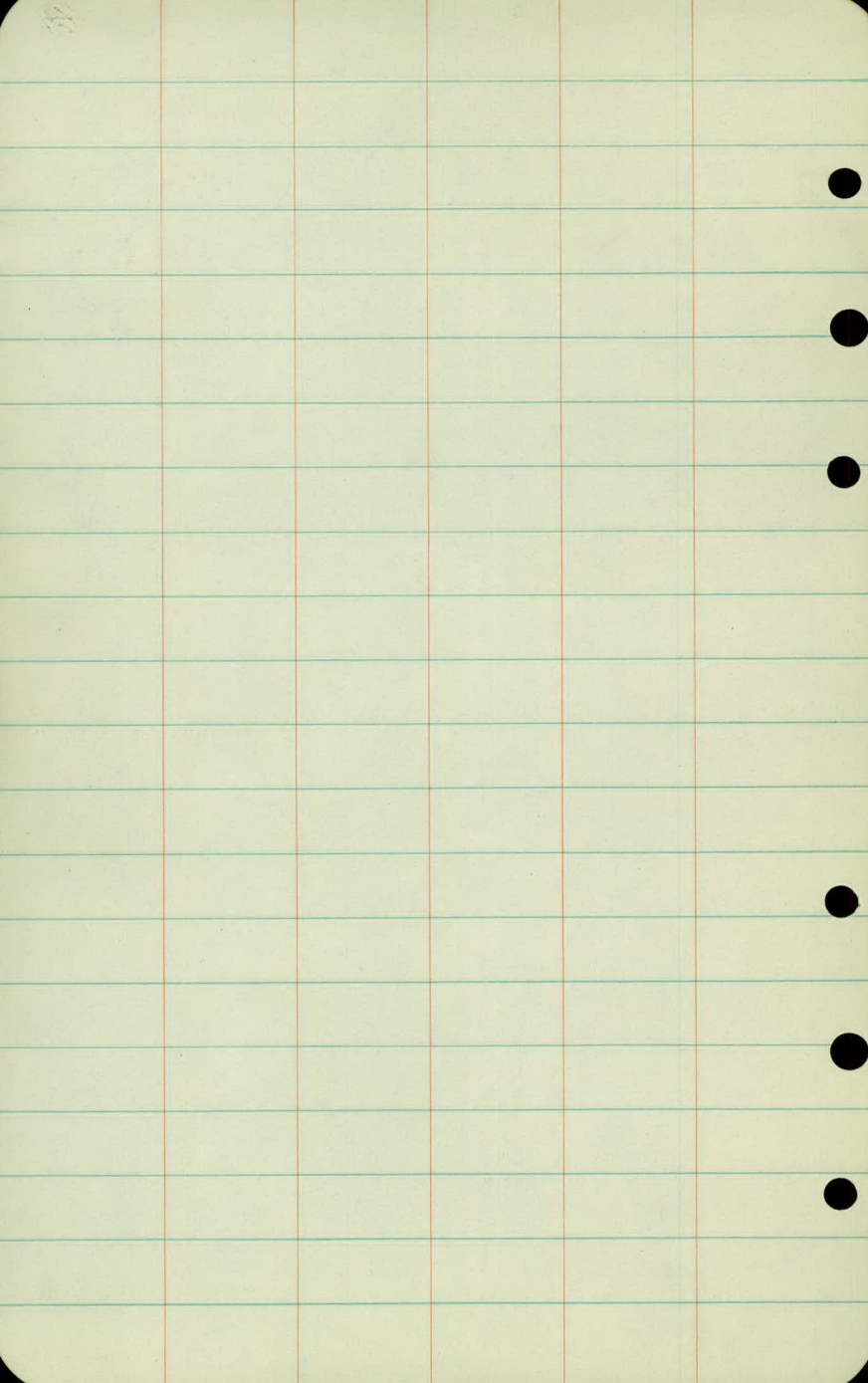
80.5	81.2	81.7
45	38	33
65	59	50

75.8	76.3	76.9	77.7	78.5	81.3	81.5	81.3	81.0	81.8
92	87	81	73	65	37	35	37	40	32
50	37	23	10		14	25	34	42	48

76.3	77.4	78.0	79.5	80.8	81.1	81.3	81.4	81.0	80.8	80.9
87	76	70	55	42	39	37	36	40	42	41
50	35	22	13	5		3	13	21	30	42

81.6
3.4

spike in PP at Ent to Lakeview Terrace Club



March 1, 1956

72

b

Profile

+

X-Section

Sta	+	π	-	Elev.
BM	5.52	887.90		882.38

24

+50

25

+50

+

26

+50

27

+50

+75.34

15+49.2 X-section Level to North

March 1, 1956

73

L

spike in PP at Ent to Lakeriew Terrace Club

81.1

6.8

81.8

6.1

82.1

5.8

82.45

5.45

83.0

4.9

83.6

4.3

85.0

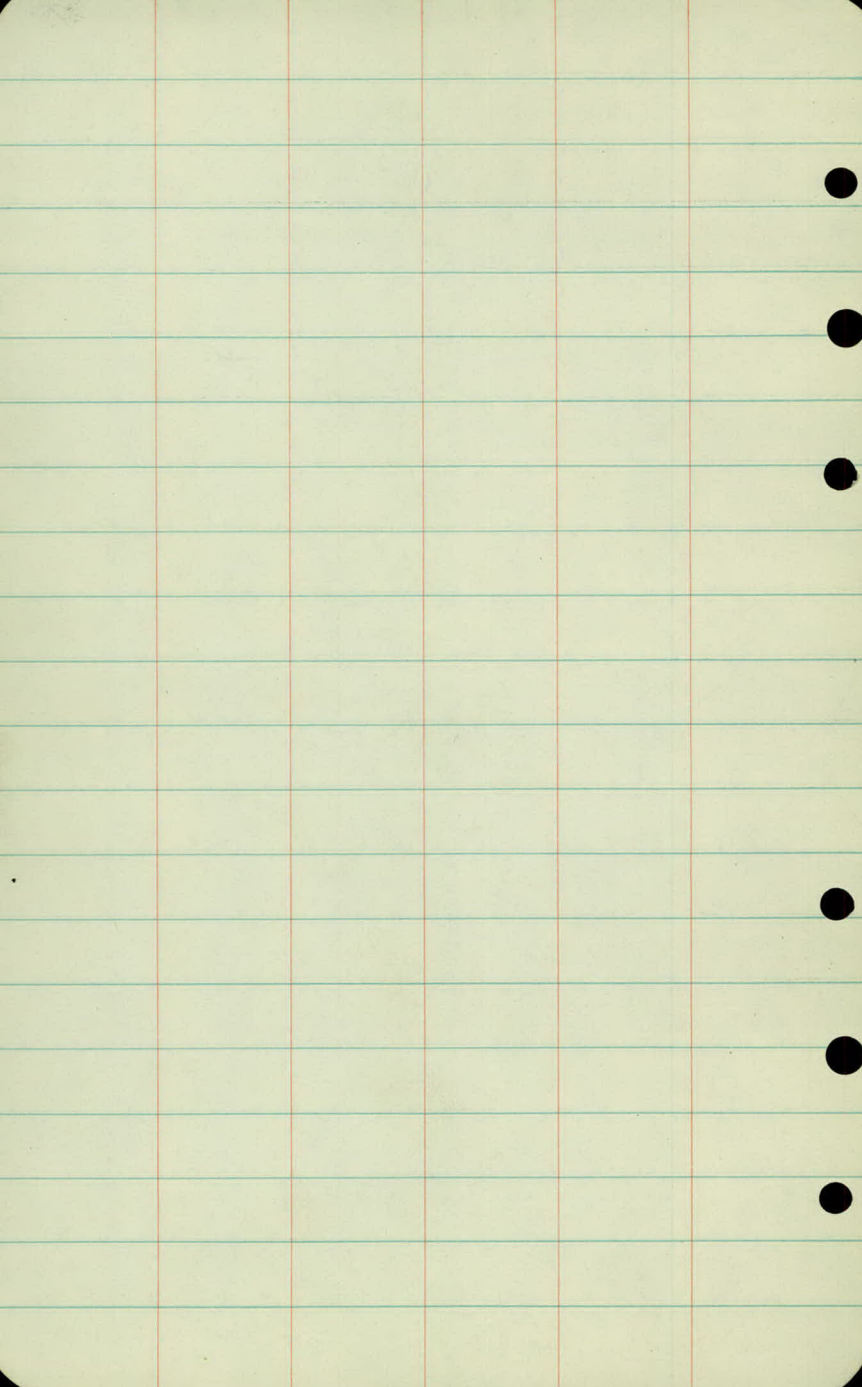
2.9

86.3

1.6

86.9

1.0



FX
LC
AB
CW
HAW

March 2, 1956
100% Relative Humidity
25°F

a

74

Soundings

Equipment: Standard

20# Hammer

Sta	4+50	22' Lt
Fect		Blows
0-1		3
1-2		2
2-3		5
3-4		6
4-5		8
5-6		10
6-7		6
7-8		5
8-9		10
9-10		12
10-11		15
11-12		15

March 2, 1956

75

Sta 4+50

46' Lt

b

Feet

Blows

0-1

3

1-2

2

2-3

3

3-4

5

4-5

8

32

5-6

9

6-7

8

7-8

7

8-9

18

9-10

23

10-11

11

11-12

9

12-13

10

13-14

20

14-15

26

Sta	5+00	8' Lt
Feet		Blows
0-1		1
1-2		2
2-3		0
3-4		0
4-5		1
5-6		2
6-7		2
7-8		3
8-9		6
9-10		8
10-11		9
11-12		12
12-13		11
13-14		21

March 2, 1956

76

Sta 5400 40' Lt C

Feet Blows

0-1 3

1-2 2

2-3 2

3-4 2

4-5 3

5-6 4

6-7 7

7-8 8

8-9 7

9-10 10

10-11 9

11-12 10

12-13 11

13-14 16

14-15 18

16-17 19

17-18 24

Sta 5+50 at 2

Feet	Blows
0-1	1
1-2	1
2-3	1
3-4	1
4-5	1
5-6	1
6-7	2
7-8	2
8-9	5
9-10	12
10-11	11
11-12	15
12-13	17
13-14	26

March 2, 1936

77

Sta 5+50 40' Lt 2

Feet Blows

22'

0-1 2

1-2 2

2-3 2

3-4 2

4-5 3

5-6 5

6-7 3

7-8 3

8-9 6

9-10 6

10-11 5

11-12 7

12-13 10

13-14 11

14-15 11

15-16 12

16-17 16

17-18 18

18-19 14

19-20 15

20-21-16.

Sta 6+00 3' Lt

Feet Blows

0-1 0

1-2 1

2-3 2

3-4 4

4-5 3

5-6 3

6-7 4

7-8 5

8-9 8

9-10 11

10-11 11

11-12 15

12-13 13

13-14 8

14-15 14

15-16 20

16-17 24

March 2, 1956

78

Sta 6700

40' Lt

Feet

Blows

0-1

3

1-2

3

2-3

2

3-4

2

4-5

4

5-6

4

6-7

5

7-8

4

8-9

5

9-10

6

10-11

7

11-12

8

12-13

9

13-14

10

14-15

12

15-16

14

16-17

17

17-18

14

18-19

12

Sta 6+00 40' Lt (Cont)

Feet	Blows
19-20	11
20-21	13
21-22	21
22-23	23

March 2, 1956

79

Sta 6+50

4' Lt

F

Feet

Blows

0-1

4

1-2

3

2-3

1

3-4

4

4-5

8

5-6

11

6-7

14

7-8

31

Sta 6+50 40' Lt

Feet	Blows
------	-------

0-1	2
-----	---

1-2	1
-----	---

2-3	0
-----	---

3-4	1
-----	---

4-5	3
-----	---

 521

5-6	4
-----	---

6-7	5
-----	---

7-8	9
-----	---

8-9	9
-----	---

9-10	8
------	---

10-11	10
-------	----

11-12	5
-------	---

12-13	9
-------	---

13-14	13
-------	----

14-15	13
-------	----

15-16	17
-------	----

16-17	17
-------	----

17-18	21
-------	----

18-19	29
-------	----

Sta 7+00 at L 9

Feet	Blows
------	-------

0-1	4
-----	---

1-2	10
-----	----

2-3	18
-----	----

3-4	4
-----	---

4-5	7
-----	---

5-6	13
-----	----

6-7	13
-----	----

7-8	17
-----	----

8-9	19
-----	----

9-10	17
------	----

10-11	17
-------	----

11-12	26
-------	----

Sta 7+00 40' Lt

Feet

Blows

0-1

3

1-2

2

2-3

12

3-4

8

4-5

13

5-6

16

6-7

27

March 2, 1956

81

Sta 14+00 at E h

Feet	Blows
------	-------

0-1	7
-----	---

1-2	4
-----	---

2-3	4
-----	---

3-4	3
-----	---

4-5	8
-----	---

5-6	22
-----	----

6-7	19
-----	----

7-8	20
-----	----

Sta 14+00 40' Lt

Feet Blows

0-1 3

1-2 3

2-3 2

3-4 1

4-5 1

5-6 16

6-7 22

7-8 40

Sta 14+50 at E in

Feet	Blows
------	-------

0-1	3
-----	---

1-2	2
-----	---

2-3	1
-----	---

3-4	2
-----	---

4-5	5
-----	---

5-6	11
-----	----

6-7	11
-----	----

7-8	18
-----	----

8-9	15
-----	----

9-10	14
------	----

10-11	26
-------	----

Sta 14 + 50 40' Lt

Feet Blows

0-1 0

1-2 1

2-3 1

3-4 1

4-5 2

5-6 4

6-7 6

7-8 5

8-9 9

9-10 8

10-11 17

11-12 19

12-13 13

13-14 12

14-15 12

15-16 10

16-17 14

17-18 23

Sta 14+50 4.0' RT j

Feet	Blows
------	-------

0-1	8
-----	---

1-2	10
-----	----

2-3	4
-----	---

3-4	9
-----	---

4-5	18
-----	----

5-6	23
-----	----

31
<u>12</u>
19

Sta 15+00 at £

Feet Blows

0-1 1

1-2 1

2-3 0

3-4 2

4-5 5

5-6 5

42

32

6-7 11

7-8 21

8-9 25

9-10 14

10-11 18

11-12 18

12-13 28

Sta 15+00 at 40' Lt h

Feet Blows

0-1 2

1-2 2

2-3 2

3-4 1

4-5 0

5-6 1

6-7 0

7-8 2

8-9 2

9-10 4

10-11 5

11-12 6

12-13 7

13-14 10

14-15 10

15-16 7

16-17 7

17-18 12

16
14

Sta 15+00 40' Lt (Cont.)

Feet	Blows
18-19	16
19-20	14
20-21	21
21-22	28

Sta 15+00

40' RT

L

Feet

Blows

0-1

4

1-2

3

2-3

3

3-4

3

4-5

9

5-6

10

6-7

18

7-8

27

Sta 15+50 at E

Feet	Blows	
0-1	3	
1-2	2	
2-3	2	
3-4	2	
4-5	2	
5-6	2	
6-7	3	10
7-8	3	
8-9	5	
9-10	7	
10-11	7	3 1/2
11-12	12	
12-13	13	
13-14	14	
14-15	16	
15-16	23	

Sta 15+50

40' Lt

m

Feet

Blows

0-1

1

1-2

0

2-3

0

3-4

0

4-5

1

5-6

0

6-7

1

7-8

1

8-9

2

9-10

2

10-11

2

11-12

3

12-13

7

13-14

9

14-15

6

15-16

7

16-17

12

17-18

13

Sta 15+50 40' Lt

Feet	Blows
------	-------

18-19	16
-------	----

19-20	18
-------	----

20-21	20
-------	----

Sta 15+58 40' RT m

Feet Blows

0-1

2

1-2

2

2-3

2

3-4

2

4-5

4

5-6

6

6-7

8

7-8

14

8-9

7

9-10

16

10-11

18

11-12

14

12-13

22

Sta 16+00 at ϕ

30°

Feet	Blows
------	-------

0-1	1
-----	---

1-2	0
-----	---

2-3	2
-----	---

3-4	1
-----	---

4-5	0
-----	---

5-6	0
-----	---

6-7	2
-----	---

7-8	2
-----	---

8-9	3
-----	---

9-10	4
------	---

10-11	4
-------	---

11-12	4
-------	---

12-13	8
-------	---

13-14	8
-------	---

14-15	8
-------	---

15-16	8
-------	---

16-17	12
-------	----

17-18	14
-------	----

Sta 16+00 at E (Cont.) m

Feet	Blows
18-19	12
19-20	13
20-21	14
21-22	17
23-24	16
24-25	13
25-26	23
26-27	16
27-28	18
28-29	22

Sta 16+00 40' Rt

Feet	Blows
0-1	3
1-2	3
2-3	2
3-4	1
4-5	3
5-6	2
6-7	2
7-8	2
8-9	8
9-10	6
10-11	9
11-12	9
12-13	13
13-14	12
14-15	10
15-16	11
16-17	12
17-18	12
18-19	

Sta 16+00 40' Rt (Cont.) 0

18-19 12

19-20 10

20-21 12

21-22 14

22-23 14

23-24 16

24-25 12

25-26 18

26-27 18

27-28 21

Sta 16+00 40' Lt

Feet	Blows
------	-------

0-1	2
-----	---

1-2	1
-----	---

2-3	1
-----	---

3-4	2
-----	---

4-5	3
-----	---

5-6	2
-----	---

6-7	2
-----	---

7-8	3
-----	---

8-9	3
-----	---

9-10	3
------	---

10-11	2
-------	---

11-12	2
-------	---

12-13	3
-------	---

13-14	3
-------	---

14-15	5
-------	---

15-16	5
-------	---

16-17	5
-------	---

17-18	7
-------	---

Sta 16+00 40' Lt (Cont) p

Feet	Blows
------	-------

18-19	8
-------	---

19-20	9
-------	---

20-21	13
-------	----

21-22	13
-------	----

22-23	16
-------	----

23-24	13
-------	----

24-25	11
-------	----

25-26	12
-------	----

26-27	13
-------	----

27-28	18
-------	----

28-29	21
-------	----

Sta 17+00 at ♀

Feet	Blows
0-1	1
1-2	1
2-3	0
3-4	1
4-5	2
5-6	2
6-7	1
7-8	2
8-9	2
9-10	2
10-11	2
11-12	4
12-13	4
13-14	4
14-15	4
15-16	4
16-17	7
17-18	8

March 2, 1956

91

Sta 17+00 at 2 Cont g

Feet	Blows
------	-------

18-19	7
-------	---

19-20	9
-------	---

20-21	11
-------	----

21-22	10
-------	----

22-23	11
-------	----

23-24	12
-------	----

24-25	13
-------	----

25-26	15
-------	----

26-27	15
-------	----

27-28	16
-------	----

28-29	17
-------	----

29-30	16
-------	----

30-31	22
-------	----

Sta 17+00 40' Rt

Feet	Blows
------	-------

0-1	1
-----	---

1-2	2
-----	---

2-3	1
-----	---

3-4	1
-----	---

4-5	3
-----	---

5-6	4
-----	---

6-7	4
-----	---

7-8	4
-----	---

8-9	8
-----	---

9-10	16
------	----

10-11	11
-------	----

11-12	10
-------	----

12-13	5
-------	---

13-14	7
-------	---

14-15	9
-------	---

15-16	6
-------	---

16-17	9
-------	---

17-18	12
-------	----

18-19	20
-------	----

19-20	25
-------	----

FK
LC
AB
CW
HAW

March 5, 1956

92

Sta 17+00 40' Fog Lt 27° n

Feet	Blows
0-1	1
1-2	1
2-3	1
3-4	1
4-5	4
5-6	2
6-7	2
7-8	2
8-9	3
9-10	3
10-11	3
11-12	3
12-13	4
13-14	4
14-15	3
15-16	4
16-17	5
17-18	6

Sta 17+00 40' 21" (Cont)

Feet	Blows
18-19	5
19-20	6
20-21	8
21-22	9
22-23	10
23-24	13
24-25	14
25-26	12
26-27	12
27-28	15
28-29	21
29-30	18

March 5, 1956

93

Sta 17+50 at # 2

Feet	Blows
------	-------

0-1	2
-----	---

1-2	2
-----	---

2-3	0
-----	---

3-4	0
-----	---

4-5	2
-----	---

5-6	3
-----	---

6-7	5
-----	---

7-8	5
-----	---

8-9	10
-----	----

9-10	9
------	---

10-11	6
-------	---

11-12	13
-------	----

12-13	26
-------	----

13-14	
-------	--

14-15	
-------	--

15-16	
-------	--

Sta 17+50 40' Lt

Feet	Blows
0-1	0
1-2	8
2-3	2
3-4	1
4-5	1
5-6	1
6-7	1
7-8	2
8-9	3
9-10	3
10-11	6
11-12	5
12-13	7
13-14	7
14-15	8
15-16	10
16-17	10
17-18	11

March 5, 1956

94

Sta 17+50 40' H (Cont.)

Feet	Blows
------	-------

18-19	11
-------	----

19-20	12
-------	----

20-21	9
-------	---

21-22	11
-------	----

22-23	14
-------	----

23-24	14
-------	----

24-25	13
-------	----

25-26	10
-------	----

26-27	16
-------	----

27-28	12
-------	----

28-29	14
-------	----

29-30	12
-------	----

30-31	15
-------	----

31-32	19
-------	----

Sta 17+50 48' Pt

Feet	Blows
------	-------

0-1	2
-----	---

1-2	4
-----	---

2-3	2
-----	---

3-4	2
-----	---

4-5	6
-----	---

5-6	20
-----	----

6-7	9
-----	---

7-8	12
-----	----

8-9	17
-----	----

9-10	21
------	----

March 5, 1956

95

Sta 18+00 at #

m

Feet	Blows
------	-------

0-1	2
-----	---

1-2	2
-----	---

2-3	2
-----	---

3-4	3
-----	---

4-5	3
-----	---

5-6	5
-----	---

6-7	9
-----	---

7-8	7
-----	---

8-9	12
-----	----

9-10	24
------	----

Sta 18+00 40' Lt

Feet	Blows
------	-------

0-1	0
-----	---

1-2	0
-----	---

2-3	2
-----	---

3-4	3
-----	---

4-5	1
-----	---

5-6	2
-----	---

6-7	3
-----	---

7-8	4
-----	---

8-9	5
-----	---

9-10	4
------	---

10-11	4
-------	---

11-12	5
-------	---

12-13	6
-------	---

13-14	10
-------	----

14-15	8
-------	---

15-16	9
-------	---

16-17	10
-------	----

17-18	11
-------	----

March 3, 1956

96

Sta 18+00 40' Lt 25

18-19 9

19-20 9

20-21 14

21-22 17

22-23 15

23-24 9

24-25 13

25-26 22

Sta 18+00 25' BT

Feet

Blows

0-1

5

1-2

5

2-3

4

3-4

2

4-5

7

5-6

12

6-7

15

7-8

20

March 5, 1956.

97

Sta 18+50

£

sw

Feet

Blows

0-1

4

1-2

3

2-3

3

3-4

1

4-5

1

5-6

6

6-7

17

7-8

12

8-9

25

Sta 18+50 40' Lt

Feet	Blows
------	-------

0-1	1
-----	---

1-2	1
-----	---

2-3	1
-----	---

3-4	1
-----	---

4-5	2
-----	---

5-6	4
-----	---

6-7	4
-----	---

7-8	4
-----	---

8-9	6
-----	---

9-10	8
------	---

10-11	5
-------	---

11-12	9
-------	---

12-13	18
-------	----

13-14	15
-------	----

14-15	16
-------	----

15-16	25
-------	----

16-17	
-------	--

17-18	
-------	--

March 5, 1956

98

Sta 19+00

15"

X

Feet

Blows

0-1

6

1-2

7

2-3

5

3-4

1

4-5

7

5-6

8

6-7

9

7-8

22

Sta 19+00 40' LA

Feet

Blows

0-1

7

1-2

1

2-3

1

3-4

2

4-5

4

5-6

16

6-7

18

7-8

9

8-9

21

9-10

10-11

11-12

March 5, 1956

99

Sta 19+50 20' Lt y

0-1

1-2

2-3

3-4

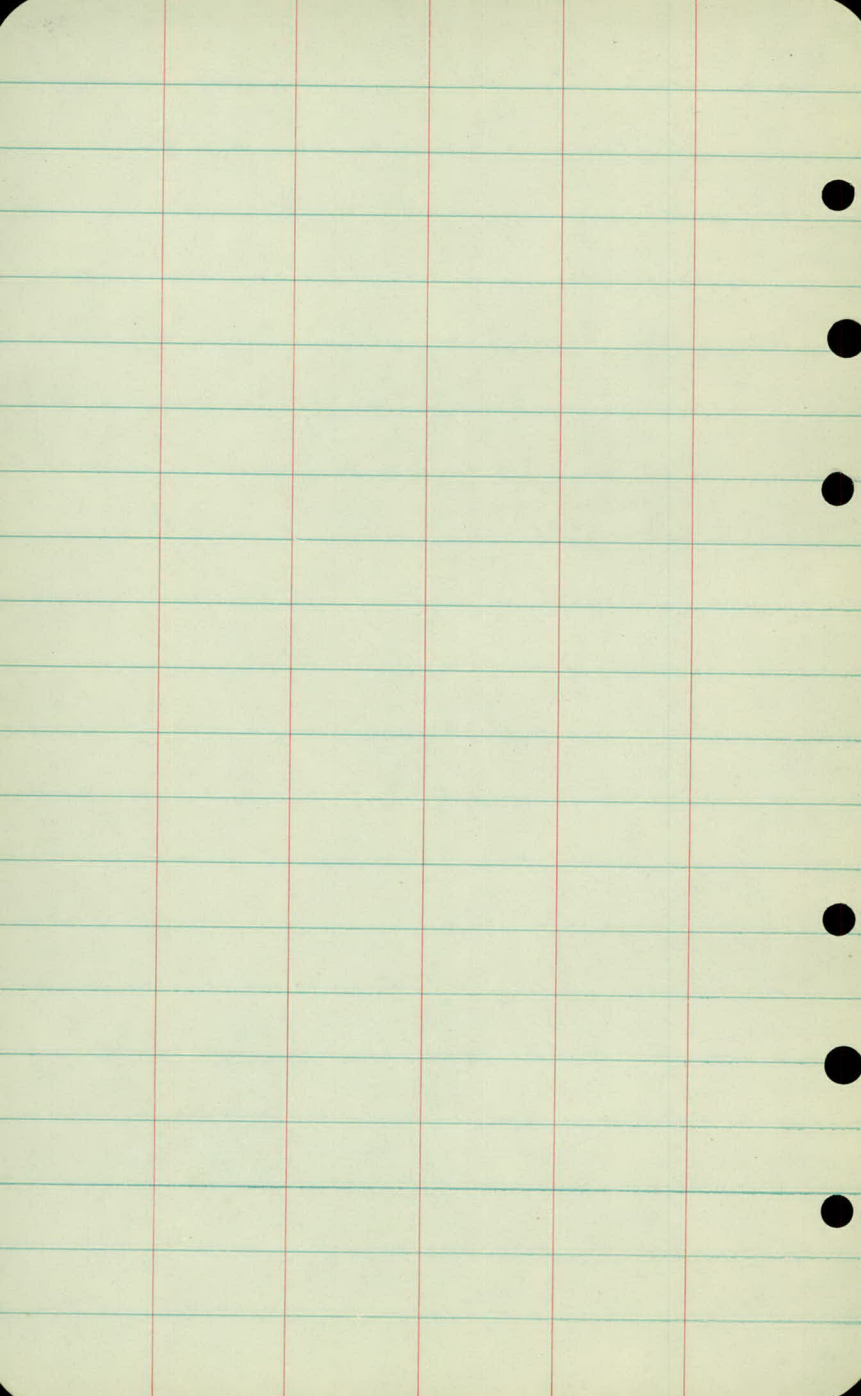
4-5

5-6

17

6-7

29



FX
LC
AB
CW

Feb 29, 1956

f

100

Soundings

pages F-6 + 1

Sta

4+00 No Swamp

4+50

⌀

Feet

Material

0-1

1-2

2-3

3-4

4-5

5-6

6-7

Auger sounding

Clay

Peat

Sand

Depth

5+00 Push Rod 10' Lt

14'

5+00 Push Rod 60' Lt

15'

5+50 Push Rod 20' Lt

19'

5+50 Push Rod 60' Lt

23'

Feb 29, 1956.

101

Sta

9

Depth

6+00 Push Rod L 17'

6+00 Push Rod 20' Lt 14' ? Layer of sand

6+00 Push Rod 60' Lt 22'

6+50 Push Rod 60' Lt 11'

6+50 Push Rod 20' Lt 12'

6+50 Push Rod 20' Rt 6'

7+50 Push Rod L 0.0'

7+50 Push Rod 30' Lt 0.5'

7+50 Push Rod 30' Rt 4'

Sta

5+00 20' Bt

0-4 Clay

Push Rod to 21'

18+50 Push Rod £ 5'

18 Push Rod £ 9'

17+50 Push Rod £ 12'

17 Push Rod £ 24'

16+50 Push Rod £ 39'

16 Push Rod £ 33'

15+50 Push Rod £ 19'

FK
LC
AM
MH.

Feb 29, 1956
March 1, 1956

102

15 Push Rod £ 8'

14+50 Push Rod £ 8'

14 Push Rod £ 5'

13+50 Push Rod £ 1.0'

14 Push Rod 25' Rt 1.5'

14 Push Rod 25' Lt 4.0'

14+50 Push Rod 25' Rt 5'

14+50 Push Rod 25' Lt 8'

15 Push Rod 25' Rt 8'

15 Push Rod 25' Lt 17'

Sta

15+50 Push Rod 32' Rt 10'

15+50 Push Rod 25' Lt 20'

15+50 Push Rod 50' Lt 25'

16 Push Rod 25' Rt 29'

16 Push Rod 50' Rt 18'

16 Push Rod 25' Lt 34'

16 Push Rod 50' Lt 34'

16+50 Push Rod 50' Lt 31'

16+50 Push Rod 50' Rt 26'

March 1, 1956

103

Sta

i

²¹
17 push Rod 50' Rt 18'

17 push Rod 25' Rt = old 17-100' Rt

17 push Rod 25' Lt = old 17-50' Rt

¹²
17+50 push Rod 25' Rt 9'

17+50 push Rod 50' Rt 5'

17+50 push Rod 25' Lt 23'

17+50 push Rod 50' Lt 32'

18 push Rod 20' Lt = old 18-50' Rt

18 push Rod 50' Lt 28'

18 Push Rod 25' Rt 8'

Sta

18+50 push Rod 25' Lt 9'

19 push Rod 12' Lt 7'

19 push Rod 28' Lt 9'

+50 push Rod 16' Lt 6'

+50 push Rod 31' Lt 6'

20 push Rod 12' Lt 6'

20 push Rod 28' Lt 9'

+50 push Rod 8' Lt 6'

+50 push Rod 25' Lt 7'

j

21 push Rod 25' Lt 9'

21 push Rod £ 5'

21+50 push Rod 25' Lt 5'

21+50 push Rod 14' Rt 4'

21+50 push Rod 23' Lt 7'

22 push Rod £ 6'

22 push Rod 16' Rt 3'

22 push Rod 25' Lt 8'

22+50 push Rod £ 2'

22+50 push Rod 25' Lt 4'

Sta

23 push Rod $\frac{1}{2}$ 4'

23 push Rod 25' Lt 5'

23+50 push Rod $\frac{1}{2}$ 7'

23+50 push Rod 25' Lt 8'

16+00 Fibrous Peat Down to 5.0'

17+00 Fibrous Peat & Roots 3.0'

15+00 Fibrous Peat Down to 5'

OBJECT

AZ.

STADIA

At P.I. Sta 17+?

to P.I. Sta. 22± 90° -

AZ.

check N.E. Cor. Meyer's Ho 139° 35'

N.W. Cor. Ho.

135° 42' 222'

S.W. " "

138° 38' 240'

S.W. Cor. Bldg.

109° 17' 242'

N.W. " "

105° 28' 237'

N.W. Cor Bldg.

101° 38' 301'

N.E. " "

100° 50' 340'

22+00 ± Ent 80' Rt

22+00 P.I. Ent 143' Rt 40' Radius

Tan to 15' so of Garage $\left. \begin{matrix} 18.3 \\ 38.3 \end{matrix} \right\}$

FX
LO
AB DIST.
CW
HAW

VERT.
ANGLE

ROD
EQUIV.

ROD

DIFF.

ELEV.

March 5, 1956

106

Size 21.5' N. + S. 35.0' E. + W. ✓

Size 16.5 N. + S. 24.3 E. + W. ✓

Size 18.3 N. + S. 38.3 E. + W. ✓

OBJECT

AZ.

STADIA

March 8, 1956

107

a

Johanna Blvd. No.

Borrow Pit #2

Pages a-i

Sta Point

26+23.08

7+82.43 $\angle$ N.S. P. R//W

6+91.43 P.O.T.

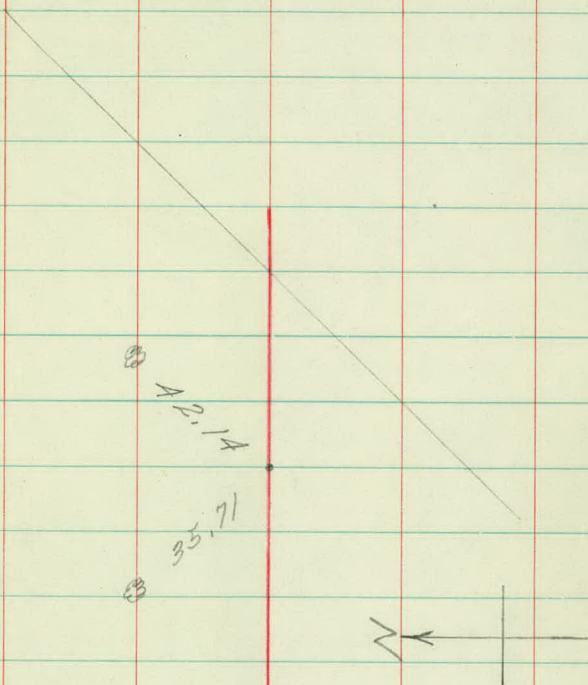
0+00 N $\frac{1}{4}$ Cor Sec 33-30-23

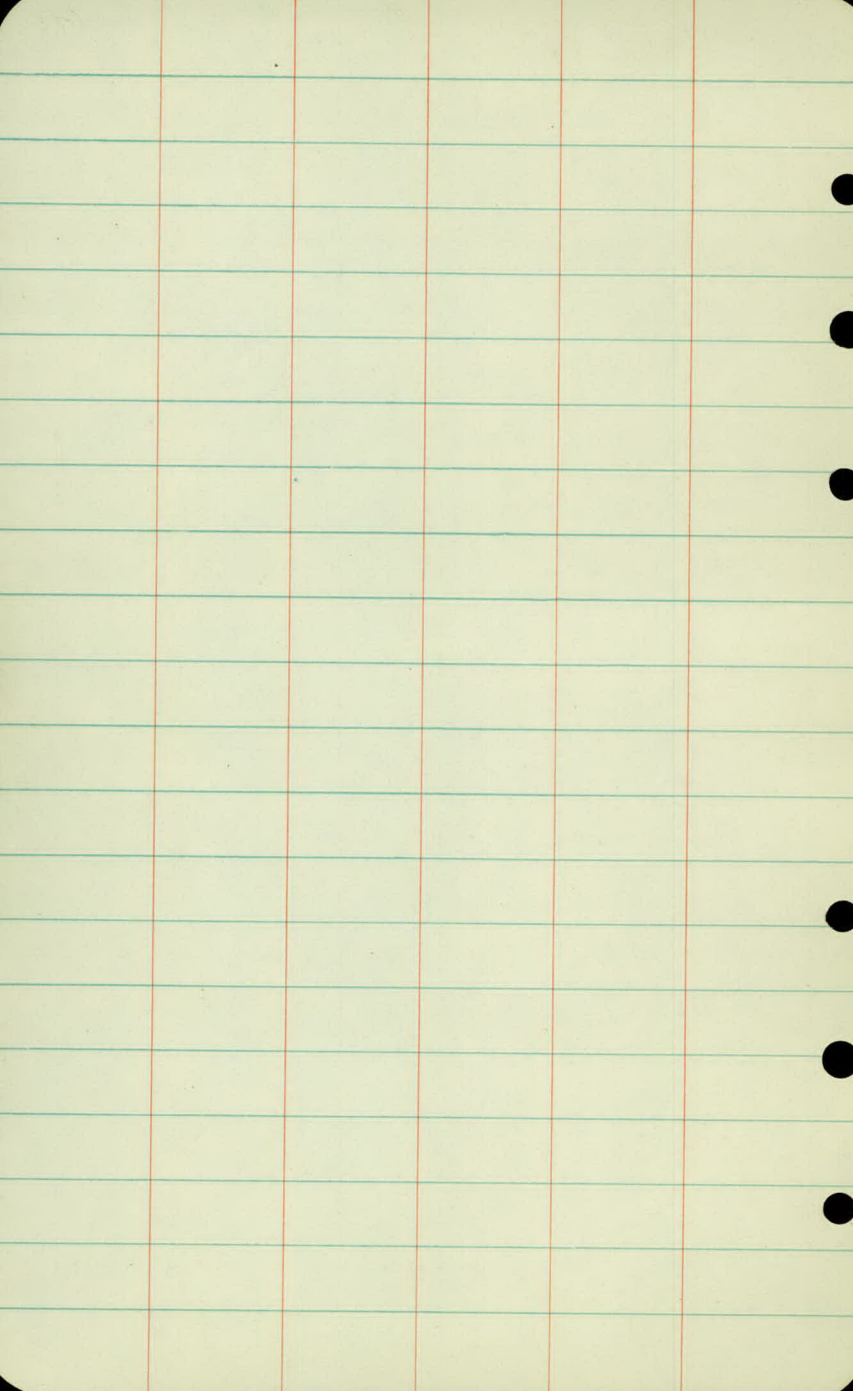
FK
LC
CW

March 8, 1956
Cold Clear 10°

108

N.E. Cor. Sec. 23-30-23





March 10, 1956

109

C

X-sections

Sta	+	π	-	Elev.
BM		4.70930.68		925.98

6

+50

+53 8.1
 103

FX
LO
AB
CW

March 9, 1956 110
Clear Cold 12°
Rd

Spike in PP #19 Schmidt Park Stadia

18.9	18.6	18.9	18.7	18.0	18.0	18.6
11.8	12.1	11.8	12.5	12.7	12.7	12.1
68	44	23		18	39	62

18.5	18.1	17.6	16.7	16.1	15.1	17.0
12.2	12.6	13.1	14.0	14.6	15.6	13.7
90	100	120	141	153	100	79

Trees

13.3	14.2
17.4	16.5
200	185

22.0	22.7	23.7	24.7	24.5	24.9	24.7	23.9	24.3
8.7	8.0	7.0	6.0	6.2	5.8	6.0	6.8	6.4
95	65	38	18		15	35	55	73

21.1	20.5	15.3	17.5	19.0	20.3	22.8
9.6	10.2	15.4	13.2	11.7	10.4	7.9
123	142	175	137	140	123	100

19.7	19.8	19.4	19.9	16.2	12.3
11.0	10.9	11.3	12.8	14.5	18.4
165	189	200	226	239	256

Sta + π - Elev

930.68.

+ 53

+ 71

+ 73

✓

+ 75

7

2 March 9, 1956 III

14

54 c

22.6

8.1

23.7

103
P.P

2.0
12.5
P.P

23.9	24.6	25.4	25.2	26.0	26.0	26.8	27.1	27.1	27.2
6.8	6.1	5.3	5.5	4.7	4.7	3.9	3.5	3.5	3.5
100	95	74	48	21		21	43	67	87

13.2	15.6	17.1	17.8	18.9	20.5	22.2	24.2	26.1
17.5	15.1	13.6	12.9	11.8	10.2	8.5	6.5	4.6
241	220	200	186	166	146	35	118	100

19.9	20.0	20.2	21.9
10.8	10.7	10.5	8.8
188	160	136	113

20.9	20.1	19.3	15.3	13.7
9.8	10.6	13.4	15.4	17.0
200	219	238	252	2.62

23.6	25.4	26.4	27.0	27.3	27.3	27.7	27.8	27.6
2.1	5.3	4.3	3.7	3.4	3.4	3.0	2.9	3.1
89	68	42	19		18	38	62	100

Sta + π - Elev

930.68

+25

March 9, 1956 112

14

2

8+ 9

186 182 179 196 235 212 201 180
 12.1 12.5 12.8 11.1 + 7.2 9.5 10.6 12.7
 176 155 134 114 + 133 135 174 200

205 201 168 157 147 139 136 151

10.2 10.6 13.9 15.0 16.0 16.8 12.1 15.6
 200 223 242 264 284 300 248 227

220 261 265 261 263 262 264 258 252

8.7 4.6 4.2 4.6 4.4 4.5 4.3 4.9 5.5
 86 62 38 18 21 41 61 81

12.7 14.5 161 18.0 196 205 225 244

18.0 16.2 14.6 12.7 11.1 10.2 8.2 6.3
 242 222 200 180 160 140 121 100

199 17.7 176 185 19.7 201 204

10.8 13.0 13.1 12.2 11.0 10.6 10.3
 100 124 146 169 189 200 222

133 141 159 181

17.4 16.6 14.8 12.6
 300 290 269 247

Sta + π - Elev

930.68

7+50

✓

✓

✓

+75

2 March 9, 1956 113

LT

RT

22.4 25.2 25.1 24.1 23.2 23.4 23.6 23.9 22.9

8.1 5.5 5.6 6.6 7.5 7.3 7.1 6.8 7.8
81 61 37 19 18 35 53 71

13.4 15.5 15.3 17.0 18.1 19.1 20.6 22.1

17.3 15.2 15.4 13.7 12.6 11.6 10.1 8.6
245 222 193 169 146 123 100 85

18.7 15.8 15.9 16.1 17.9 19.5 18.4

12.0 14.9 14.8 14.6 12.8 11.2 12.3
100 125 147 171 192 224 247

12.9 14.4 15.8

12.8 16.3 14.9
300 291 269

21.2 23.7 22.5 21.9 21.0 20.4 19.8 19.5

9.5 7.0 8.2 8.8 9.7 10.3 10.9 11.2
76 56 35 19 23 43 62

16.3 16.7 16.1 16.4 15.7 14.6 15.2 17.2

14.4 14.0 14.6 14.3 15.0 16.1 15.5 13.5
218 200 190 166 143 120 100 84

Sta + + - Elev

930.68

7+75

TP 4.99 925.80 9.87 920.81

8

TP 5.04 925.84 5.00 920.80

+25

FK
AB.
CW

March 9, 1956 114
March 13, 1956
RT h

12.4 14.5 18.1 14.5 12.7
18.3 16.2 12.6 16.2 18.0
135 114 94 237 255

17.3 20.2 21.9 21.5 20.6 20.2 19.7 17.9 14.6
8.5 5.2 3.9 4.3 5.2 5.6 6.1 7.9 11.2
84 65 38 19 18 36 54 71

084 10.9 15.1 15.7 15.7 13.5 11.3 11.9
17.4 14.9 10.7 10.1 10.1 12.3 14.5 13.9
259 238 200 176 154 136 119 92

14.4 13.0 10.8
11.4 12.8 15.0
100 110 124
1x2 & Power Line 4 Sec Line

18.1 21.7 23.0 22.4 20.7 20.1 19.0 15.8 12.4
7.7 4.1 2.8 3.2 5.1 5.7 6.8 10.0 13.4
78 61 44 22 20 40 61 80

14.5 12.4
11.3 13.2
93 100
11.7 14.5 14.3 14.8 12.8 11.0
14.1 11.3 10.5 11.0 13.0 14.8
226 200 179 154 131 100

Sta + π - Elev

925.84.

+50

✓

+75

+79

9

Trees Beyond

T.P. 5.57 929.32 2.09 923.75

3.36 925.96

2 March 13, 1956 115

4

RT 1

19.3 21.6 22.9 22.2 20.5 19.7 18.1 16.8 12.4
6.5 4.2 2.9 3.6 5.3 6.1 7.7 10.0 13.4
79 59 37 19 18 39 62 83

16.5

14.3

11.8

10.6

→ 9.3 11.5 14.0
92 100 110

15.2
96

19.7 20.8 21.0 21.0 19.8 20.0 17.8 15.2 11.1
6.1 5.0 4.8 4.8 6.0 5.8 8.0 10.6 14.7
80 58 42 24 22 45 64 90

15.1

11.6

→ 10.7 14.2
100 112

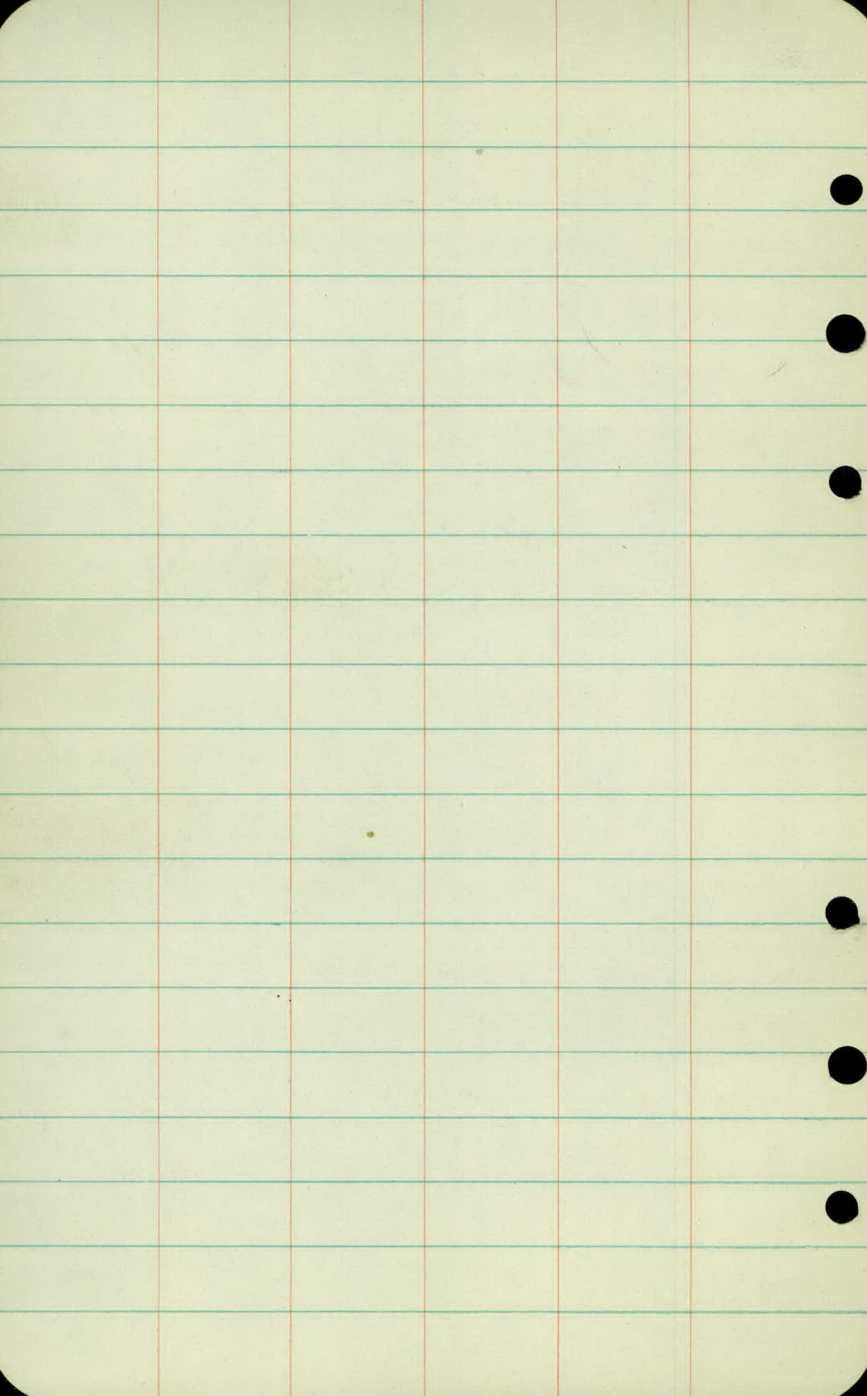
088

17.0
122
PP

16.3 16.0 17.0 17.1 17.0 16.2 15.1 12.6 10.4
9.5 9.8 8.8 8.6 8.8 9.6 10.7 13.2 15.4
63 48 29 16 18 37 57 73

17.5 14.7

→ 8.3 11.1
76 92



PK
LC
AB
CW

VERT.
ANGLE

ROD
EQUIV.

March 5, 1956
ROD

DIFF.

ELEV. 1/16

Borrow Pit #1

• 1/4 1/4 Cor.

10" 15.97 • 3+00
7.97
24" 100'

spike

• 2+00 Iron ~~the~~
4/66

• 1+00 spike

• 0+00

spike

300'

New Road

P.O.S.T.

Sta	OBJECT	+	X	AZ.	STADIA LED
BM	10.87	889.45			878.58
0+00					
✓					
+25					
✓					
✓					
+50					

DIST. VERT. ANGLE ROD EQUIV. ~~2~~ March 5, 1956 ROD DIFF. ELEV. ~~2~~ 117

Spike in 12" Oak 75' 41" Sta 11760 ±

77.5	16.5	75.8	75.4	75.1
12.0	13.0	13.7	14.1	14.4
72	50	33	17	

78.7	80.0	80.0	79.4	80.6	82.9	✓
10.8	9.5	9.5	10.1	8.9	6.6	
100	127	148	168	187	200	

80.5	78.5	77.9	77.1	76.1
90	11.0	11.6	12.4	13.4
65	49	33	20	

81.0	83.0	84.3	84.4	83.7	82.3	82.6	84.1
8.5	6.5	5.2	5.1	5.8	7.2	6.9	5.4
84	100	117	134	150	167	184	200

81.5	84.3	84.9
8.0	5.2	4.6
270	245	224

86.6	84.4	82.3	80.0	77.8
2.9	5.1	7.2	9.5	11.7
100	24	51	28	

Sta OBJECT +

Δ

AZ

STADIA
Elev

889.45

0+50

✓

T.P. 5.09 894.31 0.23 889.22

+75

✓

✓

1

DIST. VERT. ROD ROD March 5, 1956 118
 ANGLE EQUIV. ROD DIFF. ELEV. 9

85.3 86.3 87.3 87.3

4.2 3.2 2.2 2.2
 177 155 137 118

84.8 84.8 84.4 83.2 81.0 79.3

→ 4.7 4.7 5.1 6.3 8.5 10.2
 191 200 218 235 252 263

86.6 86.6 84.9 81.1 79.5

7.7 7.7 9.4 13.2 14.8
 60 44 27 13

87.1 88.3 89.2 89.8 89.2 88.4 87.1 86.0

→ 7.2 6.0 5.1 4.5 5.1 5.9 7.2 8.3
 78 100 119 135 154 169 185 200

79.9 81.0 81.5 84.4

14.4 13.3 12.8 9.9
 248 239 228 217

88.2 87.9 88.4 87.3 82.1

6.1 6.4 5.9 7.0 12.2
 71 49 33 17

89.9

4.4
 100

Sta OBJECT +

π

AZ

STADIA
Elev

894.31

1

✓

+35

✓

✓

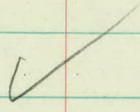
+70

March 5, 1956

DIST. VERT. ANGLE ROD EQUIP. ROD DIFF. ELEV. 4

87.3 89.5 91.4 91.1
7.0 4.8 2.9 3.2
196 174 148 123

86.7 84.0 80.3
7.6 10.3 14.0
200 218 235



89.6 90.1 90.0 89.2 87.2 81.8 80.3
4.7 4.2 4.3 5.1 7.1 12.5 14.0
50 36 22 14 20 28

90.6 91.5 92.1 92.2 92.0 90.4 90.1
3.7 2.8 2.2 2.1 2.3 3.9 4.2
81 100 114 128 143 163 179



80.2 80.9 82.0 84.5 87.0 88.4
14.1 13.4 12.3 9.8 7.3 5.9
234 230 222 212 200 192

90.6 90.3 90.8 90.7 89.1 85.7 82.2 81.4 79.9
3.7 4.0 3.5 3.6 5.2 8.6 12.1 12.9 14.4
78 51 31 13 21 35 41 50

90.9
3.4
100



Sta OBJECT + 1 AZ. Station

894.31

1+70

✓

2

✓

TP 1.31 894.23 1.39 892.92

+25

FK
LC
AB
CW

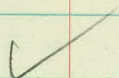
VERT.
ANGLE

ROD
EQUIV.

March 5, 1954 119
March 6, 1954 119
DIFF. ELEV.

88.7 90.8 90.7 90.8
56 35 36 35
182 167 147 131

85.5 83.1 81.6
8.8 11.2 12.7
200 215 228



92.3 92.1 92.2 91.3 90.2 88.1 86.7 84.9 82.0
20 16 21 30 41 62 76 94 123
66 44 30 13 19 33 44 63

91.1 90.4 89.5 89.3 88.6 87.5 86.4 83.7
32 39 48 50 57 68 79 106
86 100 115 129 146 165 178 200
Top of Stake Sta 2+00.70

90.0 90.9 91.2 91.0 90.2 88.4 86.9 86.3
42 33 30 32 40 58 73 79
77 55 34 16 23 46 55

89.0 86.9 85.3 83.8 82.7 82.5 82.2
52 73 89 104 115 117 120
100 134 151 165 179 194 200

Sta	OBJECT	π	AZ.	Elev	STADIA
-----	--------	-------	-----	------	--------

		894.23			
--	--	--------	--	--	--

2+50					
------	--	--	--	--	--

T.P.	3.35	886.07	11.51	882.72	
------	------	--------	-------	--------	--

+75					
-----	--	--	--	--	--

✓					
---	--	--	--	--	--

3					
---	--	--	--	--	--

✓					
---	--	--	--	--	--

BM					
----	--	--	--	--	--

		1.50			
--	--	------	--	--	--

			884.57		
--	--	--	--------	--	--

				884.63	
--	--	--	--	--------	--

DIST. VERT. ANGLE ROD EQUIV. ROD DIFF. ELEV. ¹²⁰

March 6, 1956

87.9 88.0 87.8 87.8 87.8 87.0 86.9 87.7

6.3 6.2 6.4 6.4 6.4 7.2 7.3 6.5
68 50 28 13 21 34 50

87.6 87.0 85.4 84.4 83.3 81.9 80.7 81.3

6.6 7.2 8.8 9.8 10.9 12.3 13.5 12.9
86 100 117 131 145 159 173 194

83.5 82.9 82.6 83.0 83.3 84.0 84.9 86.0

2.6 3.2 3.5 3.1 2.8 2.1 1.2 0.1
67 49 34 18 16 33 50

83.2 82.9 82.3 81.2 80.5 80.1 80.9 81.6

2.9 3.2 3.8 4.9 5.6 6.0 5.2 4.5
85 100 119 135 153 164 176 188

79.2 78.3 78.1 78.4 78.9

6.9 7.8 8.0 7.7 7.2 4.0
75 52 32 15

79.5 79.9 79.3 78.7 79.8 80.8

6.6 6.2 6.8 7.4 6.3 5.3
95 102 116 131 148 161

Nail in stump BM #1 Schmidt Park Stadium

OBJECT

AZ.

STADIA

24 + 05.23

420 73

19 + 85.00

1.92

23.08

Johanna Blvd.

^{1' 5 7/8}
overload fill

6°

12610

3°/100'

180°/100'

1.8°/100'

48.5

90°/50'

87 1/2

1301.36

1357.27

144.09

139.40

1AA 07

153

73

8

				1.5
Sta	PG	PGR	SBGGR	
BM	4.42	883.00		878.58
13+50	79.5	3.5	5.0	✓
14	79.3	3.7	5.2	✓
+50	79.2	3.8	5.3	✓
15	79.3	3.7	5.2	✓
+50	79.4	3.6	5.1	✓
16	79.6	3.4	4.9	✓
+50	79.7	3.3	4.8	✓
17	79.8	3.2	4.7	✓
+50	80.0	3.0	4.5	✓

Spike in 12" Oak Lt of Sta 11+60

2.5
C 2.0

Sta PG PGR SSGGR Elev
1.5
883.00

18 80.1 2.9 4.4

+50 80.3 2.7 4.2

19 80.4 2.6 4.1

+50 80.5

BM 4.51 886.89 882.38

Lt 17+60 3.40 883.49

17+50 4.16 882.73

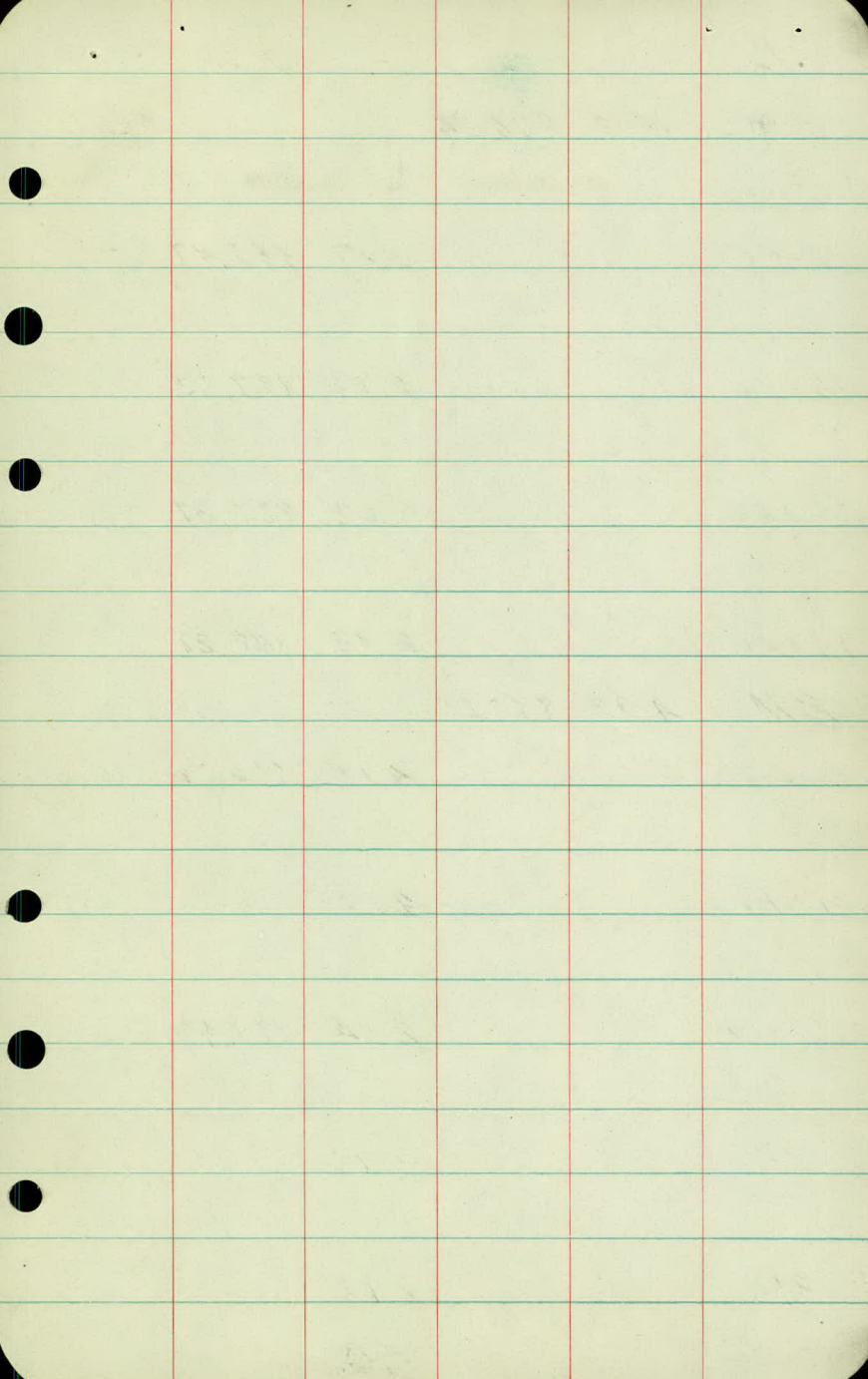
Lt 17+00 3.31 883.58

16+50 4.63 882.26

FK
RG
RH
JD

July 18, 1956
Clear 68°

Sta	+	-	Elev
BM	4.16	886.54	882.38
Lt 17+60		3.07	883.47 -0.2
17+50 P		3.79	883.75
Lt 17+00		3.02	883.52 -0.6
16+50 P		4.32	882.22
BM	4.83	887.21	
Lt 17+60		3.77	883.44 -0.3
17+50 P		4.50	
Lt 17+00		3.74	883.47 -0.05
16+50 P		5.03	
Lt 16+75		3.90	
16+50 RI		5.08	



Sta	+	-	Elev
BM	7.98	890.36	882.38
about			

16+50	RT	3.44	886.92
			$\frac{26}{16}$

16+75	LT	2.87	887.49
			$\frac{25}{21}$

17+00	RT	1.47	888.89
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17+40	LT	2.15	888.21
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BM	4.92	890.87	4.41	885.95
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16+50	RT	(890.69)	4.08	886.79	-12.61
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16+75	LT	3.55	887.32	.17
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17+00	RT	2.14	888.73	.16
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17+40	LT	2.78	888.09	.12
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BM	3.68	886.06	8.31	882.56	882.38
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BM			0.10	885.96	
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July 12, 1956

4:PM

Spike in PP

N. Cor West Ent Wall Meyer Garage

July 13 9 AM

Spike in PP

Wall

Sta	+	-	Elev
BM	4.61	890.56	885.95

16+50	RT	3.78	886.78 -13
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16+75	LT	3.25	887.34 -17
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17+00	RT	1.83	888.73 -15
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17+40	LT	2.49	888.09 -13
-------	----	------	------------

BM	5.24	891.19	885.95
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16+50	RT	4.43	886.76 .02
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16+75	LT	3.91	887.28 .03
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17+00	RT	2.49	888.70 .03
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17+40	LT	3.13	888.06 -0
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July 13, 1956

9 AM

N. Cor West Wall Ent to Meyers Garage

A PM July 13, 1956

4.69 86.50 $\begin{array}{r} 25 \\ 16 \\ \hline 41 \end{array}$

4.16 87.03 $\begin{array}{r} 25 \\ 28 \\ \hline 53 \end{array}$

2.97 88.22 $\begin{array}{r} 24 \\ 19 \\ \hline 43 \end{array}$

3.62 88.57 $\begin{array}{r} 43 \\ 14 \\ \hline 57 \end{array}$

Sta	+	π	-	Elev.
BM	5.06	891.01		885.95

15+25	RT		10.54	47
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15+50	LT		9.93	81.08
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15

16+50	RT		4.69	86.32 - .18
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16+75	LT		4.15	86.86 - .17
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17+00	RT		2.96	88.05 - .17
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17+40	LT		3.54	887.47 - .10
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July 16, 1956 8 A.M.

N. Cor West Wall Ent to Meyer's Garage

Sta	+	π	-	Elev
BM	4.54	890.51		885.95

14+50	LT		11.50	879.01
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15+25	RT		10.04	.47
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+50	LT		9.43	81.08
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16+50	RT		4.20	86.31 -.01
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+75	LT		3.67	86.84 -.02
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17+00	RT		2.48	88.03 :.02
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+40	LT		3.05	87.46 -.01
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July 16, 1956 4 PM

N Cor W. Wall Ent to Meyer Garage

Sta	+	π	-	Elev
BM	4.83	890.78		885.95

14+50	Lt		11.77	79.01	0.00
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15+25	Rt		10.32	80.46	-0.01
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+50	Lt		9.73	81.05	-0.03
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16+50	Rt		4.53	86.25	-0.06
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+75	Lt		4.00	86.78	-0.06
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17+00	Rt		2.80	87.98 ^{8.32}	-0.05 _{.24}
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+40	Lt		3.35	87.43	-0.03
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2 P/M July 17, 1956

Top N. Cor. W. Wall Ent Meyer Garage

-0.00

-.01

-03

-.11

-.46

-.43

-.39

Sta	+	π	-	Elev
BM	4.78	890.73		885.95

14+50	Lt		11.72	79.01	0.00
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15+25	Rt		10.27	80.46	0.00
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+50	Lt		9.69	81.04	-01
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16+50	Rt		4.51	86.22	-03
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+75	Lt		3.99	86.74	-04
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17+00	Rt		2.78	87.95	-03
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+40	Lt		3.32	87.41	-02
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8 AM July 18, 1954

Top N. Cor W. Wall Ent to Meyer Garage

0.00

- 0.01

- 0.04

- 0.44

- 0.50

- 0.46

- 0.41

Sta	+	π	-	Elev
BM	4.87	890.82		885.95

14+50	Lt		11.81	89.01	.00
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15+25	Rt		10.38	44	.02
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+50	Lt		9.81	81.01	.03
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16+50	Rt		4.65	86.17	.05
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+75	Lt		4.13	86.69	.05
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17	Rt		2.92	87.90	.05
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+40	Lt		3.44	87.38	.03
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1.28	884.20				
	6.35				
	887.85				
				882.92	

8 Am July 19, 1956

Top N. Cor. W. Wall Ent to Meyer Garage

0.00

-0.03

0.07

0.49

0.55

-0.51

-0.44

Check Day Rd
for stakes

Sta	+	π	-	Elev	
BM	4.77	890.72			885.95
14+50	Lt		11.71	79.01	0.00
15+25	Rt		10.28	80.44	0.00
+50	Lt		9.73	80.99	-.02
16+50	Rt	4	4.59	86.13	-.04
+75	Lt	2	4.07	86.65	-.04
17	Rt	3	2.85	87.87	-.03
+40	Lt	1	3.35	87.37	.01

8 AM July 20, 1956

Top N. Cor. West Wall Ent to Meyer Garage

0.00

-0.03

-0.09

-0.53

-0.59

-0.54

-0.45

St	+	Δ	-	Elev	
BM	4.68	90.63			885.95
14+50	Lt		11.63	79.00	0.01
15+25	Rt		10.20	80.43	-0.01
+50	Lt		9.71	80.92	-0.7
16+50	Rt		4.61	86.02	-.11
+75	Lt		4.11	86.52	-.13
17	Rt		2.87	87.76	-.11
+40	Lt		3.33	87.30	-.07

8 AM July 23, 1956

Top N. Cor. West Wall Ent to Meyer Garage

0.01

0.04

0.16

- 0.64

- 0.72
69

- 0.65

0.52

Sta New Grado SAGGR				
Sta	+	x	-	Elev
	1.56	887.51		885.95
13+50	79.5	8.0	9.5 ✓	
14	79.3	8.2	9.7 ✓	
+50	79.4	8.1	9.6 ✓	
15	79.8	7.7	9.2 ✓	
+50	80.05	7.46	8.96 ✓	
16	80.5	7.0	8.5	6.5 ✓ C20 63 C2.0
+50	80.4	7.1	8.6	36 C5.0 66 C2.0 85.0
17	80.3	7.2	8.7	27 ✓ C6.0 5.7 C3.0
+50	80.2	7.3	8.8	2.8 C6.0 4.8 C4.0

Lake Johanna

876.44 = 4/15/53

W.S. Rad = 7.7

