

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

SILVER LAKE ROAD

From SILVER LAKE To T.H. #100

Road Acc't. No. 44 DR. 9

Date Filed JUNE 26, 1962 File BK 45

KP
JS
FS
RB

28 APRIL 1961

SILVER LAKE ROAD
Co. RD E TO STH #100

REVISED ALINEMENT

STA	POINT	ΔLT	ΔRT	CURVE DATA	MAGNETIC BEARING
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67+86.76	PI	$0^{\circ}29.5'$			
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61+26.33	P.O.T.				
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58+98.42	P.O.T.				
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52+27.57					
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		$1^{\circ}14.0'$			
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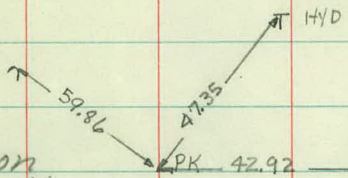
					$N6^{\circ}30'W$
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29 APRIL 1961

4

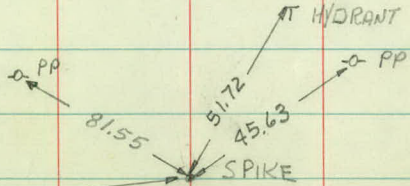
PUNCH MARK
IN TCA VENT

from
3-11-64
Jh



SPIKE

SPIKE



COORD E

5/4 COR. SEC 30 - T30 - R23

STA	POINT	ALT	ΔRT	CURVE DATA
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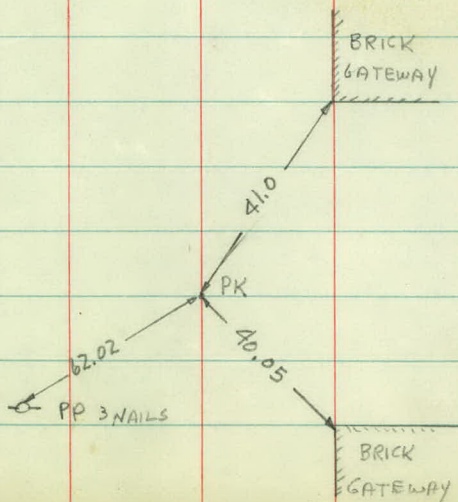
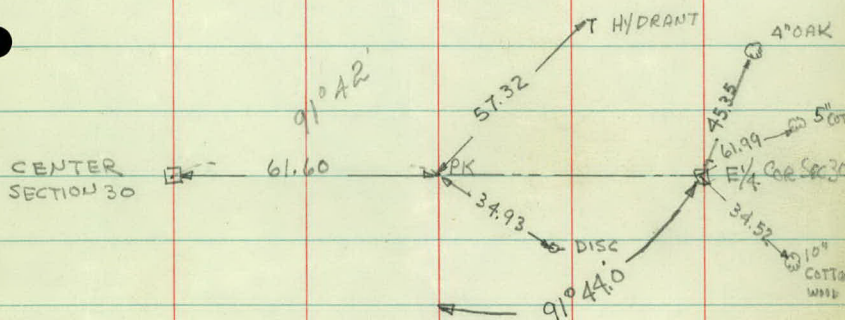
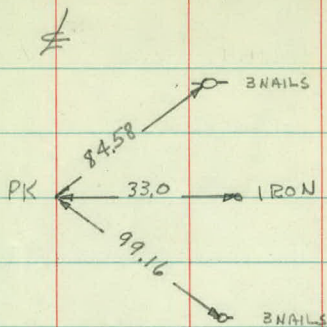
88+44.54	P.O.T.			
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78+56.42	P.O.T.	MH COVER		
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75+64.21	P.O.T.	± INCA DRIVE		
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(4)

24 MAY 1961



STA	POINT	ALT	ΔRT	CURVE DATA
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104+84.9	P.O.T.			
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92+29.11	$\downarrow$ 0°09.5' 0°10' CEMETERY ROAD			
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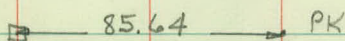
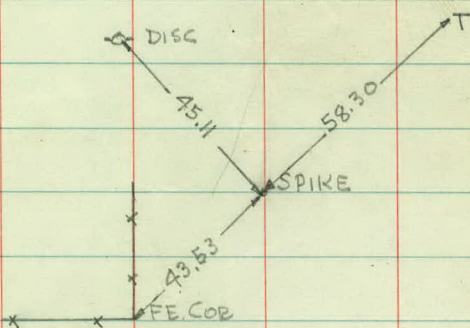
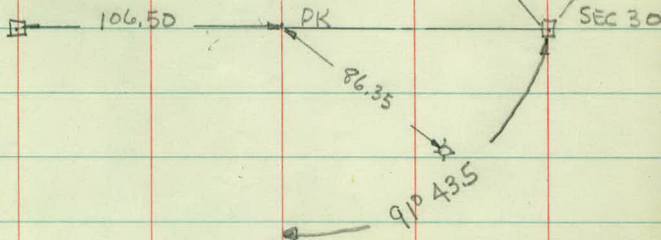
91+67.26	P.O.T.		N 1/4 1/4 LINE	CENTER SEC. 30
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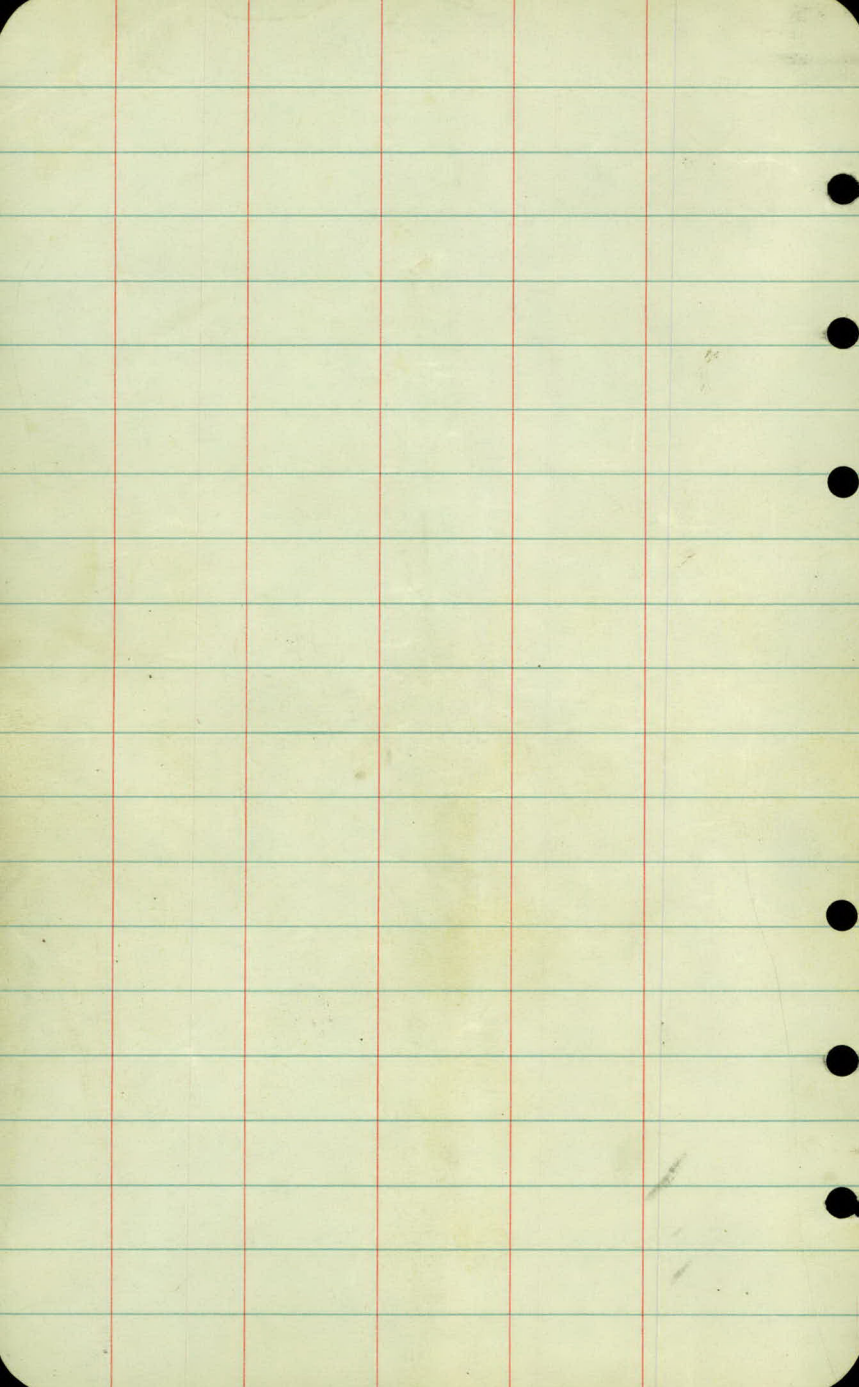
(6)

RP
JS
FS
RB
ERDUR

24 MAY 1961

N 1/4 COR
SEC 30





FX
WM
BS
DS

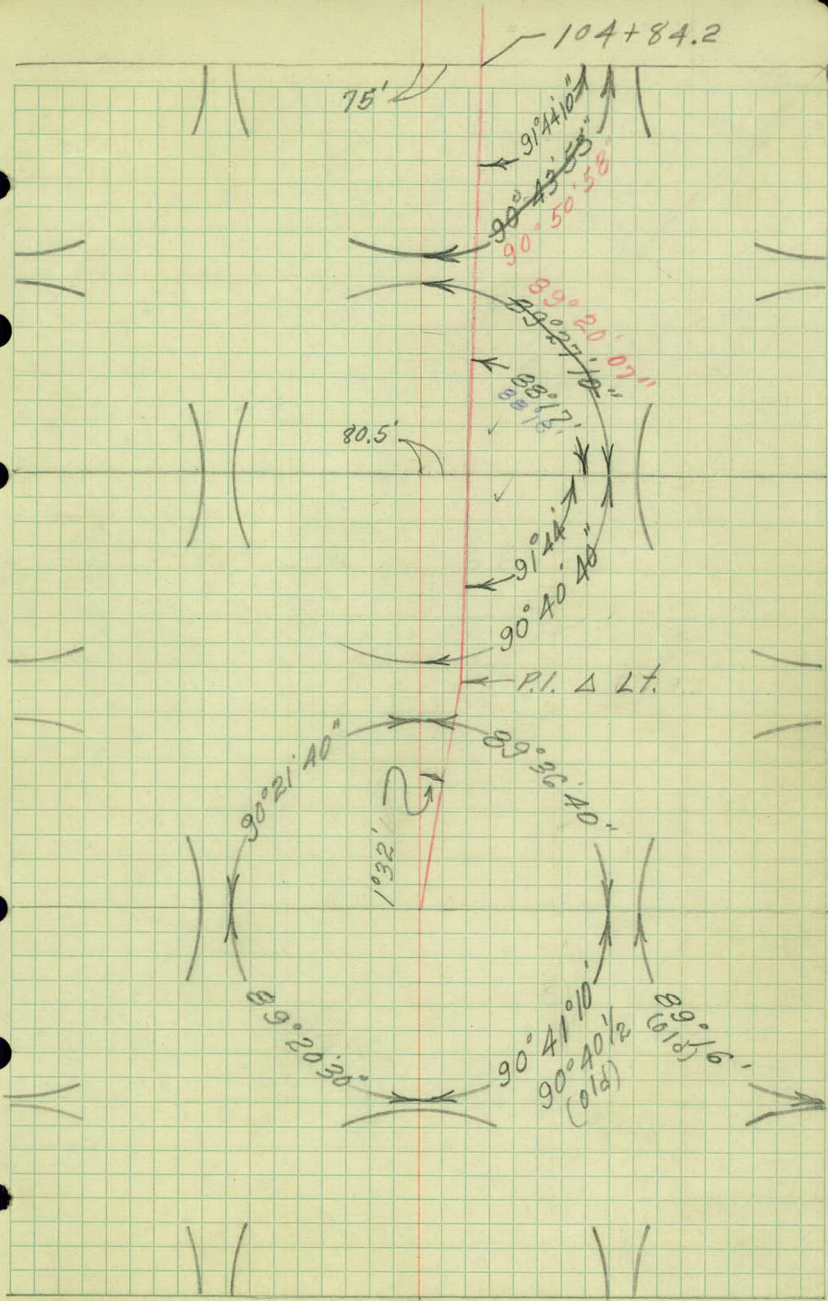
October 1961

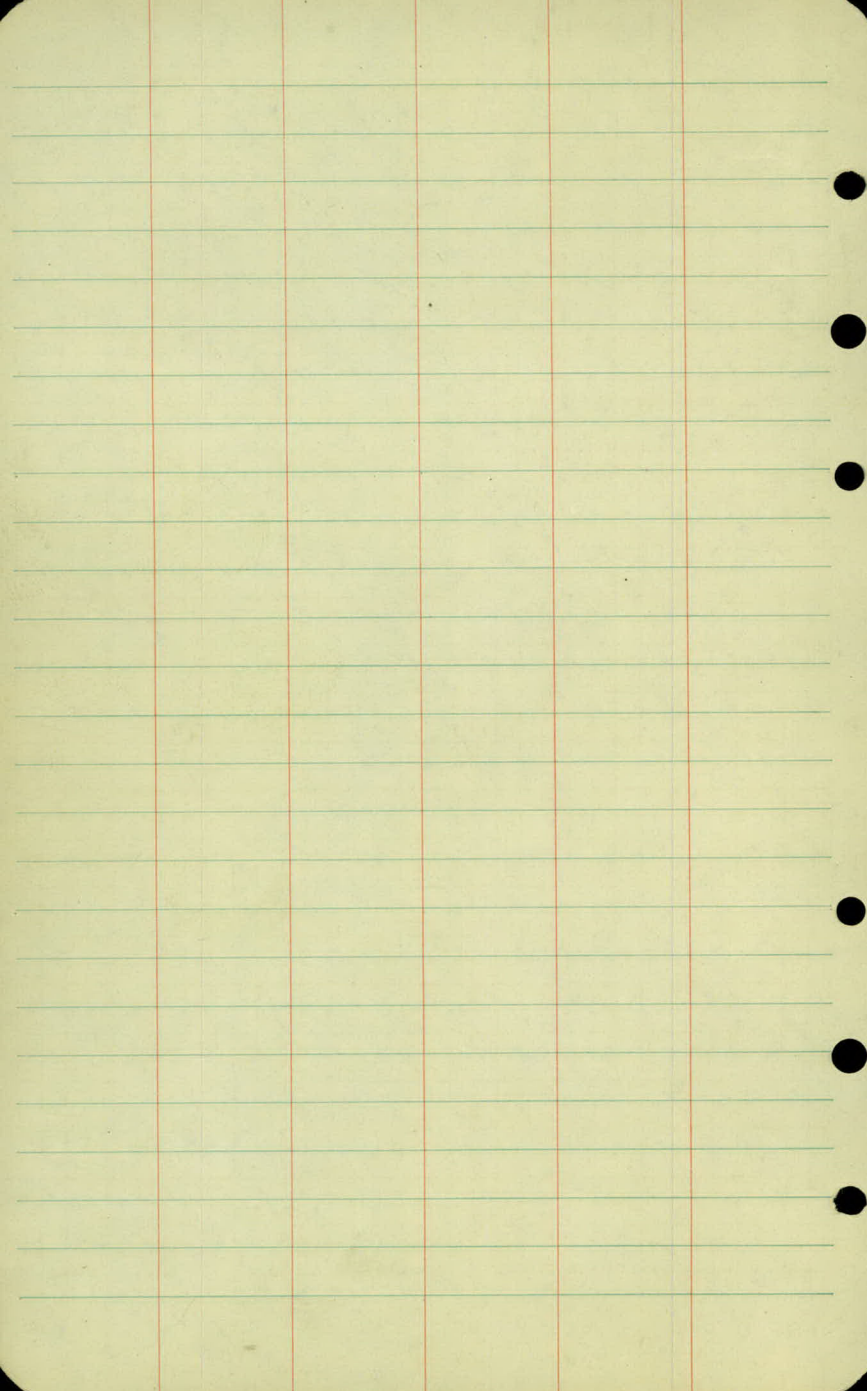
Section Angles

N $\frac{1}{4}$ Cor.

Ctr. Sec. 30

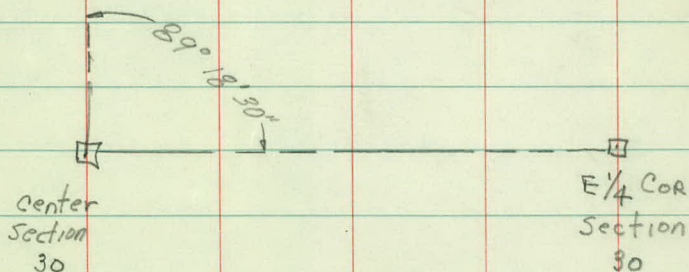
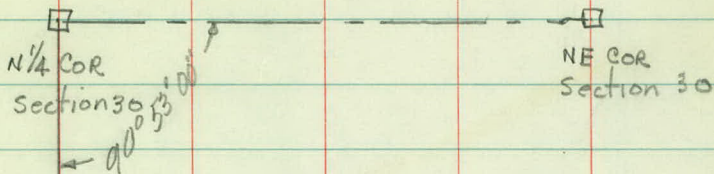
52+27.57 E Co. Rd. "E"

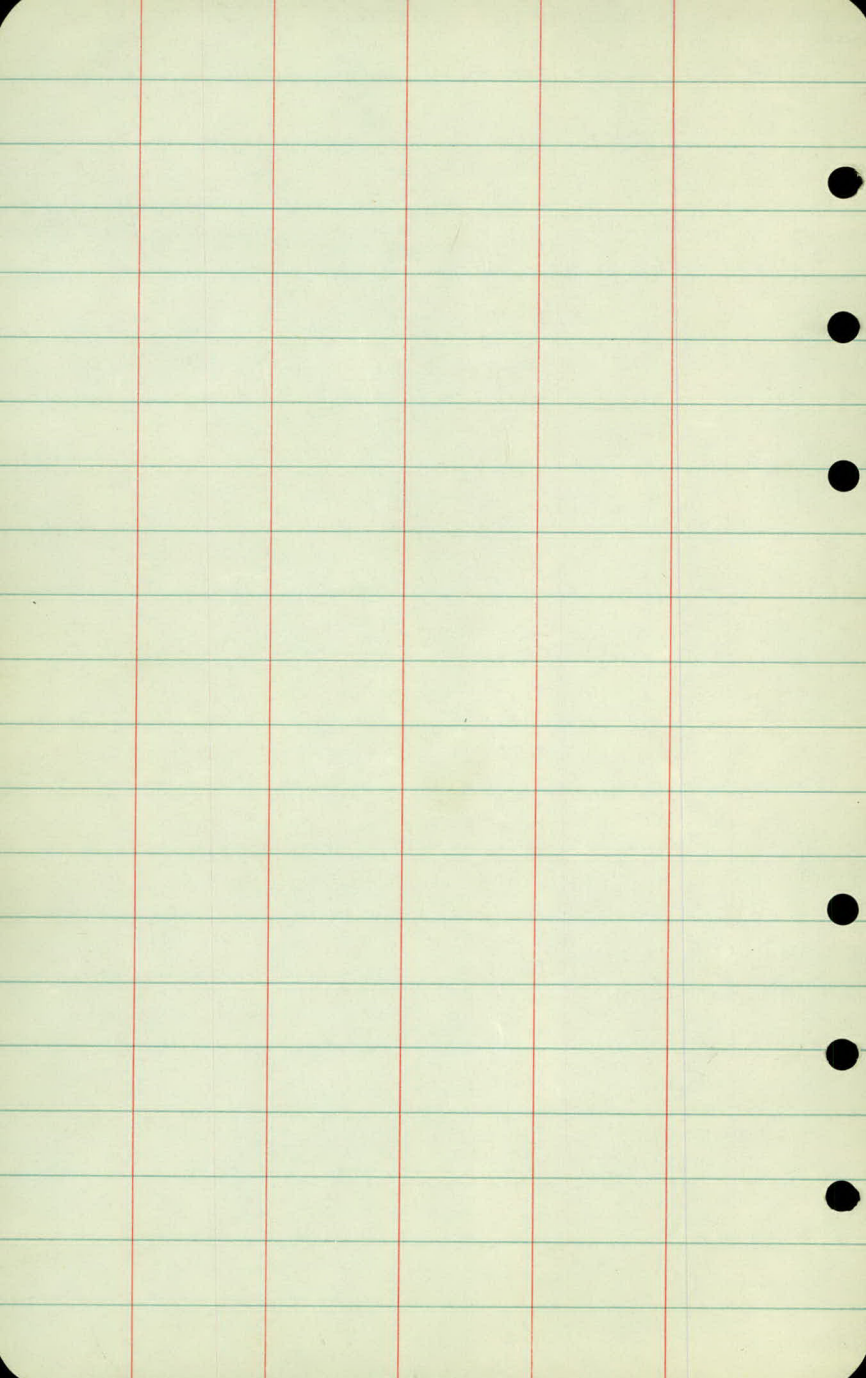




KP
US
FS
LB

3 Nov. 1961





X- sections

Lakeriew Drive to "E"

reduced a chair by R.P. 6/20/60

Sta + K - Elev.

BM 7.24 950.76' 943.52)

26+00

✓

+14 E Lakeview Dr

✓

+26

JS
JL
WM

May 2, 1960

13

LT

RT

Spike in p.p. 100' E. of Lakeview Dr. & S.L.R.

A2.3 A2.0 A1.5 A1.8 A1.8 A1.7 A1.5 A0.9 39.5 39.0

85 8.8 9.3 9.0 9.0 9.1 9.3 9.9 11.3 11.8
77 55 41 26 9 11 18 23 38

A2.8

39.1

39.0

38.8

8.0
100

11.7 11.8 12.0
75 72 59

A2.2 A2.1 A2.4 A2.2 A2.2 A2.1 A1.9 A1.2 A0.2 39.8

75 8.1 8.4 8.5 8.6 8.7 8.9 9.5 10.6 11.0
108 63 40 21 9 11 17 23 32

A4.0

A4.9

A0.2

39.7

39.8

6.8 5.9
150 200

10.6 11.1 11.0
75 61 50

A2.6 A2.1 A2.2 A2.4 A2.4 A2.2 A1.6 A0.6 A0.8

8.2 8.7 8.6 8.4 8.4 8.6 9.2 10.2 10.0
66 43 25 10 11 18 23 27

A2.9 A2.0

A1.3

A1.0

A0.7

A0.7

A0.8

7.9 7.8
91 100

95 9.8 10.1 10.1 10.0
75 70 60 49 40

Sta	+	x	-	Elev
		950.76		

26+33

✓

+47

✓

+64

2 May 2, 1960 146

2x

34

A1.0

A1.1

A1.5

A2.5

A2.5

A2.3

A1.9

A0.7

A0.7

9.8 9.7 9.3 8.3 8.3 8.5 8.9 10.1 10.1
56 39 28 11 14 6 20 24

A1.6

A1.7

A2.5

A2.0

A1.5

A1.6

A1.4

9.2 9.1 8.3 8.8 9.3 9.2 9.4
74 100 75 58 46 36 27

A1.2

A1.5

A1.8

A1.5

A2.5

A2.7

A2.5

A2.1

A0.9

A0.9

A2.6

9.5 9.3 9.0 9.3 8.3 8.1 8.3 8.7 9.9 9.9 8.2
71 47 32 20 11 11 16 20 25 28

A1.0

A0.1

A5.6

A4.1

A3.8

9.8 100 4.7 52 6.4 70
75 58 40 33

A1.1

A1.7

A1.9

A2.1

A2.6

A2.9

A2.7

A2.1

A1.2

A1.2

A2.1

9.4 9.1 8.9 8.7 8.2 7.9 8.1 8.7 9.6 9.6 8.7
70 47 30 16 11 11 17 19 24 28

A0.3

A6.0

A5.5

A4.5

A2.6

A2.8

10.5 100 4.8 5.3 6.3 7.2 8.0
75 63 54 45 36

2 May 2, 1940 15

$\begin{matrix} A1.0 & A2.2 & A2.2 & A2.9 & A3.2 & A3.1 & A2.1 & A1.8 & A2.4 & A3.2 \\ 9.8 & 8.6 & 8.5 & 7.9 & 7.6 & 7.7 & 8.1 & 8.0 & 8.4 & 7.6 \\ 59 & 41 & 19 & 11 & & 11 & 18 & 19 & 26 & 28 \end{matrix}$

$\begin{matrix} 39.4 & 38.7 \\ 11.4 & 12.1 \\ 77 & 100 \end{matrix}$

$\begin{matrix} A6.9 & A6.2 & A3.2 \\ 3.9 & 4.2 & 6.5 \\ 75 & 71 & 36 \end{matrix}$

$\begin{matrix} A0.8 & A2.4 & A2.6 & A3.2 & A3.5 & A3.4 & A2.9 & A2.8 & A2.6 & A3.6 \\ 10.0 & 8.4 & 8.2 & 7.6 & 7.3 & 7.4 & 7.9 & 8.8 & 8.2 & 7.2 \\ 52 & 38 & 19 & 11 & & 11 & 18 & 19 & 24 & 30 \end{matrix}$

$\begin{matrix} 39.2 & 38.3 \\ 11.5 & 12.5 \\ 70 & 100 \end{matrix}$

$\begin{matrix} A6.7 & A5.9 & A4.7 \\ 4.1 & 4.9 & 6.1 \\ 75 & 60 & 37 \end{matrix}$

$\begin{matrix} A1.6 & A2.6 & A2.7 & A3.2 & A3.6 & A3.5 & A3.0 & A2.2 & A2.3 & A3.5 \\ 9.2 & 8.2 & 8.1 & 7.5 & 7.2 & 7.3 & 7.8 & 8.5 & 8.5 & 7.3 \\ 46 & 32 & 19 & 11 & & 11 & 18 & 19 & 21 & 28 \end{matrix}$

$\begin{matrix} A1.7 & 39.1 & 38.4 \\ 9.1 & 11.7 & 12.4 \\ 83 & 91 & 100 \end{matrix}$

$\begin{matrix} A6.8 & A5.9 & A5.6 & A4.6 \\ 4.0 & 4.9 & 5.2 & 6.2 \\ 75 & 60 & 49 & 36 \end{matrix}$

Sta + Δ - Elev

950.76

27+69

✓

28

✓

+50

2 May 2, 1960 16

$A_{2.0}^{2.0}$ $A_{2.8}^{2.8}$ $A_{2.8}^{2.8}$ $A_{3.5}^{3.5}$ $A_{3.7}^{3.7}$ $A_{3.5}^{3.5}$ $A_{3.1}^{3.1}$ $A_{2.7}^{2.7}$ $A_{3.2}^{3.2}$ $A_{3.2}^{3.2}$
 8.8 8.0 8.0 7.3 7.1 7.3 7.7 8.1 7.5 6.5
 44 27 19 11 11 18 23 27 34

$A_{2.0}^{2.0}$ $A_{1.8}^{1.8}$ $A_{2.0}^{2.0}$ $A_{6.1}^{6.1}$ $A_{6.1}^{6.1}$ $A_{5.6}^{5.6}$
 8.8 9.0 8.8 4.1 4.7 5.2
 57 79 100 75 63 47

$A_{2.7}^{2.7}$ $A_{3.0}^{3.0}$ $A_{3.5}^{3.5}$ $A_{3.1}^{3.1}$ $A_{3.6}^{3.6}$ $A_{3.8}^{3.8}$ $A_{3.7}^{3.7}$ $A_{3.4}^{3.4}$ $A_{2.2}^{2.2}$ $A_{2.2}^{2.2}$ $A_{2.2}^{2.2}$
 8.1 7.8 7.3 7.7 7.2 7.0 7.1 7.4 8.5 8.5 6.7
 61 41 30 19 11 11 17 18 21 29

$A_{2.4}^{2.4}$ $A_{2.1}^{2.1}$ $A_{6.6}^{6.6}$ $A_{6.3}^{6.3}$ $A_{5.6}^{5.6}$
 8.4 8.7 4.2 4.5 5.3
 84 100 75 63 40

$A_{4.5}^{4.5}$ $A_{3.9}^{3.9}$ $A_{3.1}^{3.1}$ $A_{3.8}^{3.8}$ $A_{4.0}^{4.0}$ $A_{3.8}^{3.8}$ $A_{3.4}^{3.4}$ $A_{1.8}^{1.8}$ $A_{1.8}^{1.8}$ $A_{4.3}^{4.3}$
 6.3 6.9 7.7 7.0 6.8 7.0 7.4 9.0 9.0 6.5
 33 28 20 11 11 17 19 22 28

$A_{4.1}^{4.1}$ $A_{3.4}^{3.4}$ $A_{3.2}^{3.2}$ $A_{2.6}^{2.6}$ $A_{5.7}^{5.7}$ $A_{6.1}^{6.1}$ $A_{5.8}^{5.8}$ $A_{5.2}^{5.2}$
 6.7 7.4 7.6 8.2 5.1 4.7 5.0 5.5
 49 72 88 92 75 61 43 35

$A_{2.1}^{2.1}$
 8.1
 100

Sta + π - Elev

950.76

29

✓

TP 5,49 949.60 6.65 944.11

+21

✓

+58

✓

May 2, 1960 17

$\Delta 6.8$ $\Delta 2.4$ $\Delta 2.2$ $\Delta 4.1$ $\Delta 4.2$ $\Delta 4.1$ $\Delta 3.6$ $\Delta 2.1$ $\Delta 2.1$
 40 74 76 6.7 66 6.7 72 8.7 8.7 72
 36 25 21 11 11 17 18 22 22

$\Delta 6.1$ $\Delta 5.1$ $\Delta 2.9$ $\Delta 2.6$ $\Delta 6.2$ $\Delta 5.9$ $\Delta 5.7$ $\Delta 4.6$
 4.7 5.7 6.9 7.2 46 49 5.1 6.2
 59 76 95 100 75 59 42 32
 Sta 29

$\Delta 5.5$ $\Delta 6.9$ $\Delta 2.1$ $\Delta 4.0$ $\Delta 4.2$ $\Delta 4.1$ $\Delta 2.7$ $\Delta 2.4$ $\Delta 2.1$
 4.1 2.7 6.5 5.6 5.5 5.5 5.9 7.2 7.2
 56 36 23 11 11 17 18 22

$\Delta 4.5$ $\Delta 2.6$ $\Delta 6.4$ $\Delta 6.4$ $\Delta 6.4$ $\Delta 5.8$ $\Delta 4.1$
 5.1 6.0 3.2 3.2 3.2 3.8 4.9
 76 100 92 75 32 43 32

$\Delta 2.1$ $\Delta 2.8$ $\Delta 3.4$ $\Delta 4.0$ $\Delta 4.2$ $\Delta 4.1$ $\Delta 2.7$ $\Delta 2.6$ $\Delta 2.6$
 6.5 6.8 6.2 5.6 5.4 5.5 5.9 7.0 7.0 5.7
 28 24 19 11 11 19 22 25 29

$\Delta 2.3$ $\Delta 4.7$ $\Delta 1.8$ $\Delta 1.8$ $\Delta 5.9$ $\Delta 5.7$ $\Delta 4.7$
 7.3 7.9 7.8 8.1 3.7 3.9 4.9
 42 53 76 100 75 47 33

Sta + π - Elev.

949.60

29+69

✓

+80

✓

30

4 May 2, 1960 18

Lt

Rt

A1.8

A2.5

A3.2

A2.9

A1.1

A4.0

A3.9

A4.0

A4.2

7.8

7.1

6.3

5.7

5.5

5.6

5.7

5.6

5.4

5.4

5.4

5.4

5.4

34

25

20

11

11

11

11

17

24

24

50

50

50

A0.6

A0.6

A1.2

A1.1

A4.5

9.0

9.0

8.4

8.7

8.7

8.7

8.7

8.7

8.7

8.7

8.7

8.7

8.7

6.4

7.6

8.3

100

100

100

100

100

100

100

100

100

100

100

5

5

1

1

1

1

1

1

1

1

1

1

1

1

A0.5

A0.5

A0.1

A2.4

A2.8

A4.0

A2.9

A2.8

A1.1

A4.2

A4.2

A4.2

A4.2

A4.2

9.1

9.2

8.9

6.2

5.8

5.6

5.7

5.8

5.5

5.4

5.4

5.4

5.4

7.5

5.9

3.7

1.7

1.1

1.1

1.1

1.1

2.1

3.9

6.0

6.0

6.0

A1.0

A1.0

A4.4

8.6

8.6

100

100

100

100

100

100

100

100

100

100

100

A0.5

A0.2

A2.8

A2.5

A2.8

A2.7

A2.4

A1.9

A1.9

A2.1

A2.1

A2.1

A2.1

9.1

9.3

6.8

6.1

5.8

5.9

6.2

7.7

7.7

7.7

5.9

5.9

5.9

4.7

3.0

1.8

1.1

1.1

1.1

1.1

1.7

2.2

2.4

2.8

2.8

2.8

2.8

A0.5

A0.9

A1.0

A2.6

A2.8

A4.0

9.1

8.7

8.6

8.6

8.6

8.6

8.6

8.6

8.6

8.6

8.6

8.6

8.6

5.5

7.3

100

100

100

100

100

100

100

100

100

100

100

100

6.0

5.8

5.6

5.6

5.6

5.6

7.5

6.1

4.3

4.3

4.3

4.3

Sta + π - Elev

949.60

30 + 31

✓

+ 76

✓

31

Sta + π - Elev

949.60

31 + 33

✓

TP 3.55 943.23 9.92 939.68

+60

✓

+86

✓

£ May 2, 1960 20

LT

RT

29.0	20.6	21.2	21.7	21.9	21.7	21.3	29.8	29.8	21.2
10.6	2.0	8.4	7.9	7.7	7.9	8.3	9.8	9.8	7.1
51	31	19	11		11	17	20	23	29

28.2	28.6	20.5
11.4	11.0	9.1
63	70	100

22.1	22.1	22.1
6.5	6.5	6.5
75	65	46

21.4	28.5	20.8	21.3	21.4	21.3	21.0	29.5	29.5	21.6
5.8	4.7	2.4	1.9	1.8	1.9	2.2	3.7	3.7	1.6
46	34	19	11		11	17	20	23	28

26.8	21.5	27.9	26.5	26.2
6.4	5.7	5.3	6.7	7.0
59	7.7	88	96	100

22.6	22.5	22.1
0.6	0.7	1.1
75	65	44

26.6	27.7	20.2	20.8	21.0	20.9	20.9	29.5	29.5	21.5
6.6	5.5	3.0	2.4	2.2	2.3	2.3	3.7	3.7	1.7
33	27	18	11		11	17	20	23	43

25.9	24.3	22.4	22.1
7.3	8.9	9.8	11.1
48	60	80	100

22.5	22.1
0.7	1.1
75	61

Sta + π - Elev.

943.23

32

✓

+36

✓

+68

✓

✓

May 2, 1960 21

LT

RT

34.2	36.5	39.9	40.5	40.8	40.1	40.9	39.6	39.5
8.9	6.7	3.3	2.7	2.4	2.5	2.3	3.6	3.7
36	30	18	11		11	18	20	22

32.0	31.8	31.4	30.9	42.2	42.2	41.5	41.2
10.2	11.4	11.8	12.3	0.9	1.0	1.7	2.0
55	79	97	100	75	69	48	28

32.2	38.4	39.2	39.8	40.1	40.0	39.6	38.2	38.1
10.0	4.8	4.0	3.4	3.1	3.2	3.6	4.9	5.1
32	23	19	11		11	17	20	29

31.8	30.8	29.6	29.3	41.4	41.2	40.4	39.3
11.4	12.4	13.6	13.9	1.8	2.0	2.8	3.9
45	60	79	86	75	65	50	39

Water

35.0	37.2	38.5	39.2	39.5	39.3	38.9	37.8	37.6	38.9
8.2	5.9	4.7	4.0	3.7	3.9	4.3	5.4	5.6	4.4
26	22	17	11		11	17	20	32	47

32.1	32.5	31.9	30.9	41.7	40.8
10.1	10.7	11.3	12.3	1.5	2.4
29	31	32	39	75	65

29.2

14.0
Water

56

Sta + π - Elev

943.23

33

✓

+34

+ 50

✓

34

BM

8.53

947.52

4.24

938.99

938.92

May 2, 1960

22
1

11

31

32.9 31.2 30.2 30.7 29.0 30.9 28.5 26.9 27.0

10.3 6.0 5.0 4.5 4.2 4.3 4.7 6.3 6.2
28 22 18 11 11 17 22 33

30.9 29.2

12.3 14.0
32 42

Water

32.21

9.96
FL 18" CM
27

40.1 38.5 37.3

3.1 4.7 5.9
75 60 47

36.07

2.16
FL 18" CM
20

32.1 25.9 27.1 30.6 28.9 30.7 30.2 26.1 27.0

10.5 7.3 5.5 4.6 4.3 4.5 5.0 6.5 6.2
28 25 18 11 11 19 22 33

31.0 29.2

12.2 14.0
32 44

Water

40.6 39.6 37.7

2.6 3.6 5.5
75 64 53

31.0 32.0 31.4 29.0 29.2 29.1 28.5 27.0 27.8 27.8

12.2 10.2 5.8 4.2 4.0 4.1 4.7 6.2 5.4 5.4
51 32 24 11 11 17 20 33 40

30.5 31.3 31.7

12.7 11.9 11.5
68 93 103

Lake Level Bench

41.1 40.1 38.6

2.1 3.1 4.6
75 66 55

Sta + π - Elev

947.52

34+29

✓

+55

✓

+81

✓

FX
JS
JL
WM
JH

May 4, 1960 23

24.0	28.1	28.9	29.6	29.7	29.5	29.2	29.8	28.1	28.1
135	94	8.6	7.9	78	8.0	8.3	9.7	9.4	9.3
33	26	18	11		11	15	20	33	45

32.6	33.0	32.8	32.2			40.8	40.5	39.1	
13.9	14.5	14.7	14.3			67	70	8.4	
37	52	67	100			75	69	57	

29.8	29.3	29.2	29.6	40.1	40.2	40.1	39.9	28.8	29.3	29.1
9.7	8.2	8.3	7.9	7.4	7.3	7.4	7.6	8.7	8.2	8.4
33	26	22	18	12		11	15	20	33	46

26.9	25.7	25.9	25.6			29.8	29.7		
10.6	11.8	11.6	11.9			7.7	7.8		
43	68	86	100			75	64		

40.1	40.5	29.3	40.1	40.6	40.7	40.5	40.3	29.0	40.5	40.1
7.4	7.0	8.2	7.4	6.9	6.8	7.0	7.2	8.5	7.0	6.8
33	29	25	19	12		11	16	20	25	33

40.4	40.2	29.3	28.1			41.0	41.0		
7.1	7.3	8.2	9.4			6.5	6.5		
40	62	84	100			75	60		

Conc

Sta + π - Elev

947.52

35

✓

+14

✓

+42

May 4, 1960 24

LT

ST

A2.0	A0.7	29.9	A0.5	A0.9	A1.0	A0.8	A0.5	29.5	A0.4	A0.7
45	68	26	70	6.6	6.5	6.7	70	80	7.1	6.79
33	27	24	18	11		12	18	21	24	33

Comp

A2.6	A1.9	A1.2	A0.4		A0.86	A0.90	A0.8
4.9	5.6	6.3	7.1		6.66	6.62	6.7
42	61	84	100		75	61	43

A2.6	29.8	A0.6	A1.2	A1.2	A1.0	A0.7	29.9	29.2	29.2
3.9	7.7	6.9	6.3	6.3	6.5	6.8	7.6	8.3	8.3
33	24	18	11		11	15	18	20	24

A1.8	A1.4	A2.5	A2.4	A2.1		A1.6	A1.5	A0.9	A0.8
2.7	3.1	4.0	4.1	5.4		5.9	6.0	6.6	6.7
39	56	77	83	100		75	69	46	28

A2.8	A0.2	A1.1	A1.5	A1.6	A1.4	A0.9	29.5	29.4	A1.1
3.7	7.3	6.4	6.0	5.9	6.1	6.6	80	8.1	6.4
33	25	18	11		11	17	21	24	27

A2.4	A2.4	A2.2	A1.9
5.1	5.1	5.3	5.6
75	61	45	31

Sta + π - Elev

947.52

35+76

✓

36

✓

+50

✓

+54

4.94 42.58

2 May 3, 1960 25 m

LT

BT

AA.1	AD.6	AI.5	AI.9	A2.1	AI.8	AI.5	AI.1	AD.1	AD.1
34	4.9	6.0	5.6	5.4	5.7	6.0	6.4	7.4	7.4
32	25	18	11		14	16	18	20	23

A2.2	A2.3	A2.6	AD.9
4.3	4.2	3.9	6.6
75	50	32	26

AA.0	AI.1	AI.8	A2.3	A2.4	AI.9	AI.6	AI.2	AD.6	AA.0
3.5	6.4	5.7	5.2	5.1	5.6	5.9	7.3	6.9	3.5
32	25	18	11		14	17	21	26	32

A2.7	A2.2
3.8	3.3
75	54

AI.8	AI.8	A2.6	A2.5	A2.5	A2.7	AI.7	AD.4	AD.4	AI.9
5.7	5.7	4.9	5.0	5.0	5.3	5.8	7.1	7.1	5.6
26	24	19	11		11	17	20	23	26

A2.1	AA.2
5.4	3.3
28	32

A2.7	A2.8	A2.2
3.8	3.7	4.3
75	64	29

Top MH LT

Sta + π - Elev.

947.52

37

✓

+30

/

+60

May 4, 1960 26

$\dot{A}2.1$	$\dot{A}0.2$	$\dot{A}1.4$	$\dot{A}1.9$	$\dot{A}2.1$	$\dot{A}1.8$	$\dot{A}1.4$	$\dot{A}0.0$	$\dot{A}0.0$	$\dot{A}1.3$
3.8	7.2	6.1	5.6	5.4	5.7	6.1	7.5	7.5	6.2
32	24	16	11	11	11	17	20	24	27

$\dot{A}2.2$	$\dot{A}2.7$	$\dot{A}2.1$
4.2	3.8	4.4
75	56	33

$\dot{A}2.8$	$\dot{A}2.5$	$\dot{A}0.9$	$\dot{A}1.4$	$\dot{A}1.6$	$\dot{A}1.2$	$\dot{A}0.9$	$\dot{A}2.9$	$\dot{A}2.9$	$\dot{A}2.9$
3.7	8.0	6.6	6.1	5.9	6.3	6.6	8.6	8.6	7.6
32	52	4	16	11	11	17	20	24	26

$\dot{A}2.4$	$\dot{A}2.2$	$\dot{A}2.5$
5.1	4.2	5.0
75	59	33

$\dot{A}2.1$	$\dot{A}2.6$	$\dot{A}2.9$	$\dot{A}0.7$	$\dot{A}0.9$	$\dot{A}0.6$	$\dot{A}0.2$	$\dot{A}2.0$	$\dot{A}2.0$	$\dot{A}2.6$
4.8	8.9	7.6	6.8	6.6	6.9	7.3	9.5	9.5	8.9
32	6	24	18	11	11	16	20	23	25

$\dot{A}1.4$	$\dot{A}1.9$	$\dot{A}1.3$	$\dot{A}0.6$
6.1	5.6	6.2	6.9
75	53	45	29

Sta + π - Elev

947.52

37+86

✓

38

✓

TP 9.96 952.50 1.98 942.54

35+42

+76

May 4, 1960 27

24

A2.5	28.1	29.9	40.2	40.3	40.1	29.6	31.2	31.2
50	94	76	73	72	74	79	10.2	10.2
324	24	16	11		11	16	20	23

40.2	40.4	29.9	31.2	29.6
73	71	76	82	79
75	53	47	40	28

27.9	27.9	28.4	29.5	29.9	40.0	29.8	29.2	31.2	31.2
96	96	91	80	76	75	77	83	10.3	10.3
25	23	22	16	11	11	17	20	23	

A1.6	A2.1	A2.9	A3.7
5.9	5.4	4.6	3.8
32	42	52	62

29.6	29.5	28.5	29.1
7.9	8.0	9.0	8.4
75	54	38	27

44.9	47.4	48.5	48.5
76	51	40	40
100	73	54	43

46.2	48.0	49.2	49.4
6.2	4.5	3.2	3.1
100	85	66	44

Sta + π - Elev

952.50

36

+50

37

+30

+60

+86

May 4, 1960 28 P

Lt

Z

Ab.9	A7.4	Ab.9	A7.7	50.1
5.6	5.1	3.6	2.8	2.4
100	93	83	68	44

Ab.6	Ab.0	A7.2	50.0
5.9	4.5	3.3	2.5
100	85	66	45

Ab.5	A7.8	Ab.9	Ab.4
6.0	4.7	3.6	3.1
100	82	64	44

A7.2	Ab.7	Ab.0	Ab.0
5.3	3.8	3.5	3.5
100	78	62	44

Ab.9	Ab.4	Ab.7	Ab.7A	Ab.1
5.6	4.1	3.8	5.1	6.4
100	82	70	53	39

Ab.1	Ab.8	Ab.2	Ab.8	Ab.4	Ab.6
7.4	6.7	6.3	6.7	8.1	8.9
100	89	75	62	51	37

Sta	+	π	-	Elev
		952.50		

38

TP	2.28	942.32	12.46	940.04
----	------	--------	-------	--------

+40

✓

✓

+78

✓

✓

May 4, 1960 29

Lt

RT

9

A_{2.2}

A_{4.2}

A_{4.2}

9.2 8.2 8.2
100 89 72

37.0 37.6 38.5 39.1 39.2 39.0 38.6 36.8 36.8
5.3 4.7 3.8 3.2 3.1 3.3 3.7 5.5 5.5
24 23 19 11 11 7 20 22

37.1 38.9 39.7 40.1 38.5 37.5 37.6 37.9
5.2 3.4 2.6 2.2 3.8 4.8 4.7 4.4
25 28 32 44 56 49 43 24

41.2 41.7 41.4 40.8 38.9
1.1 0.6 0.9 1.5 3.4
100 80 67 55 75

36.8 36.7 37.4 38.0 38.5 38.5 38.3 37.9 36.4 36.4 37.7
5.5 5.6 4.9 4.3 3.8 3.8 4.0 4.4 5.9 5.9 4.6
25 24 22 16 11 11 17 19 23 27

37.4 38.4 38.6 39.0 39.3 38.0 37.5 36.3 36.6
4.9 3.9 3.7 3.3 3.0 4.3 4.8 6.0 5.7
28 30 32 41 50 75 68 41 32

41.1 40.9 40.5 39.8
1.2 1.4 1.8 2.5
100 88 76 63

Sta + π - Elev

942.32

39

✓

BM 5.43 941.81 5.94 936.38 936.32

+20

✓

FX
JS
JL
WM

May 4, 1960 30
May 5, 1960 2
RT

37.1 37.1 37.6 38.2 38.2 38.0 37.2 35.8 35.8 36.1
5.2 5.2 4.7 4.1 4.1 4.3 4.6 6.5 6.5 5.6
33 24 16 11 11 17 20 23 26

37.1 38.5 39.0 39.6 41.0 36.6 36.5 35.8 35.9
4.6 3.8 3.3 2.7 1.3 5.7 5.8 6.5 6.4
41 53 69 76 100 75 53 42 30

Top Breather Pipe Lt Sta 40+35

35.8 36.2 37.1 37.9 38.0 37.7 37.5 36.0 35.7 36.1
6.0 5.6 4.9 3.9 3.8 4.1 4.3 5.8 6.1 5.6
51 39 19 11 11 17 20 23 26

36.2 36.9 39.1 40.7 35.5 35.0 34.9
5.6 4.9 2.9 1.1 6.3 6.8 6.9
56 51 81 100 75 59 34

Sta + π - ELEV.

941.81

+34

✓

+45

✓

8.93 932.88

+68

✓

May 5, 1960

31.

LT

Q

RT

35.6	36.1	36.8	37.6	37.8	37.5	37.5	35.6	35.5
6.2	5.9	5.0	4.2	4.0	4.3	4.3	6.2	6.3
51	36	20	11		11	17	21	23

35.7	36.6	38.5	39.3	34.1	34.4	35.1	35.8
6.1	5.2	3.3	2.5	4.7	7.4	6.7	6.0
63	74	88	100	76	50	33	24

35.6	36.2	36.8	37.6	37.7	37.4	37.2	34.8	33.9	33.5
6.2	5.6	5.0	4.2	4.1	4.4	4.6	7.0	7.9	8.3
36	24	17	11		11	16	20	25	32

35.4	35.8	39.5	32.5	32.5	32.9
6.4	6.0	2.3	9.3	9.3	8.9
54	75	105	75	64	42

Water Level Swamp

RT

32.5	33.0	35.7	36.7	37.3	37.4	37.2	36.8	34.0	32.9
9.3	8.8	6.1	5.1	4.5	4.4	4.6	5.0	7.8	8.9
30	28	24	19	11		11	17	20	27

SWAMP

33.0	32.1	32.5	32.7	35.4	35.3	35.8	35.8	36.9
8.8	9.7	9.3	8.1	6.1	6.5	6.0	6.0	4.9
33	36	37	40	47	55	76	98	100

Sta + π - Elev.

941.81

40+00

✓

9.40 932.41

+50

+50

5.96 935.85

41

+50

May 5 1960

LT

E

RT

32.5

32.4 32.7 35.6 36.5 36.9 37.1 36.9 36.4 33.5 33.1 32.0

9.4 9.1 6.2 5.3 4.9 4.7 4.9 5.4 8.3 8.7 9.0
33 30 24 18 11 11 6 21 27 31

Swamp

32.3 33.5 33.4 34.3 35.7 35.7

9.5 8.3 8.4 7.5 7.8 6.1 6.1
40 47 58 64 69 18 100

Water level Swamp Lt.

31.2 32.5 36.0 36.3 36.6 36.4 35.8 33.9 32.9

SWAMP ← 10.6 9.3 5.8 5.2 5.2 5.4 6.0 7.9 8.9 → Swamp
34 28 19 11 11 14 22 28

Top of Man hole 18' Lt.

31.4 32.4 33.5 35.6 36.3 36.4 36.7 35.8 33.8 32.8

10.4 9.4 8.3 6.2 5.5 5.4 5.6 6.0 8.0 9.0
30 27 26 18 11 12 16 20 27

31.8 30.6 31.2 35.5 36.1 36.3 36.6 35.6 35.0 34.0 32.4

10.0 9.2 7.6 6.3 5.7 5.5 5.7 6.2 6.8 7.8 9.0
31 24 23 18 11 11 15 17 19 27

Sta	+	π	-	Elev
		941.81		

42+00

+50

7.75 934.06

T. P.	7.20	941.26	7.75	934.06
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43+00

+50

44+00

May 3 196

LT

E

RT

33

31.9	32.5	34.5	35.6	36.1	36.2	36.0	35.5	34.7	34.2	32.3
9.9	9.3	7.3	6.2	5.7	5.2	5.8	6.3	8.1	8.6	9.5
32	29	22	18	11	5	11	17	21	25	30

32.0	32.6	34.3	35.6	36.1	36.3	36.1	35.5	34.8	32.7	32.2
9.8	9.2	7.5	6.2	5.7	5.3	5.7	6.3	8.0	9.1	9.6
35	29	24	17	11	5	11	17	23	28	31

Top of 15" CMC 26' LT

Top of 15" CMC 26' LT

32.4	32.3	32.7	32.2	34.8	36.0	36.5	36.6	36.4	36.0	34.2	33.6	32.7
8.9	9.0	8.6	8.1	6.5	5.3	4.8	4.7	4.9	5.3	7.1	7.7	8.6
35	32	29	26	22	17	10	4	12	18	21	26	28

32.5	32.9	34.1	36.4	36.9	37.0	36.6	36.0	34.1	33.3	32.1
8.8	8.4	7.2	4.9	4.4	4.3	4.7	5.3	7.2	8.0	9.2
35	29	24	18	10	4	12	19	22	27	31

37.0	37.6	35.4	36.6	37.1	37.2	36.8	36.4	37.4	32.5	32.0
8.3	7.7	5.9	4.7	4.2	4.1	4.5	4.9	7.9	8.8	9.3
32	26	22	18	10	4	12	19	25	28	32

33.1

8.2
35

Sta + π - Elev

941.26

+50

4.5+00

+50

+70

✓

May 5 1960
34

Lt					Z		Rt						
32.6	37.4	37.1	37.4	36.8	37.2	37.3	37.0	36.3	36.8	37.4	37.5	37.1	
29	29	26	6.9	5.8	4.5	4.1	4.0	4.3	5.0	5.5	6.9	7.8	8.6
37	34	30	24	22	18	10		12	18	21	23	28	29

37.0	37.6	37.2	37.1	36.8	37.4	37.5	37.2	36.8	34.8	36.5	37.9	37.2
8.3	7.7	7.1	5.6	4.5	3.9	3.8	4.1	4.5	6.5	7.8	8.4	9.1
31	27	24	21	17	10		12	18	22	27	30	33

37.0	37.9	36.8	37.5	37.9	38.0	37.7	37.0	35.2	34.3	37.9	37.6
8.3	7.4	5.5	3.8	3.4	3.3	3.6	4.3	6.1	7.0	8.4	8.7
31	25	22	16	10		12	18	22	26	30	33

37.2	37.0	36.6	37.7	36.4	38.3	37.9	37.4	35.5	36.4	37.6
8.1	7.3	4.7	3.6	3.2	3.0	3.4	3.9	5.8	5.9	6.7
31	27	21	17	10		12	18	22	26	30

37.0	37.9	37.7	37.5
8.3	8.4	8.6	7.8
75	65	45	34

Sta

+

π

-

Elev

941.26

46+00

✓

T.P

7.40

946.07

2.59

938.67

+ 43

✓

+ 68

✓

DIST. 14 ELEV. 33

37.0	36.5	36.5	36.8
4.3	4.8	4.8	4.5
76	63	42	35

399	376	376	390	393	395	392	388	373	372	390
8.2	8.5	8.5	7.1	6.8	6.6	6.9	7.3	8.8	8.9	7.1
34	23	20	16	11	13	19	21	24	28	

38.0
81
38

$$\begin{array}{r} 43.1 \\ 3.0 \\ \hline 38 \end{array}$$

40.2	39.0	37.9	34.5	34.8	39.9	39.7	39.2	38.1	38.4	40.6	41.3
5.9	7.1	8.2	6.6	6.3	6.2	6.4	6.9	8.0	7.7	5.5	6.8
28	25	21	17	11		12	17	21	24	28	34

42.2	44.1
<u>3.9</u>	<u>2.0</u>
34	38

Sta	OBJECT		AZ.	STADIA
	+	π	-	Flu

946.07

+90

✓

47400

✓

+11

✓

Lt

E

Rt

May 5 1969
36

42.6	39.7	38.3	39.0	39.9	40.2	40.3	40.1	39.6	39.1	40.3	40.8
3.5	6.4	7.8	7.1	6.2	5.9	5.8	6.0	6.5	7.0	5.8	5.3
33	22	22	19	16	10		12	17	20	27	29

44.9

1.2

38

43.9 42.2

2.2 3.9

34 32

42.6	40.1	38.6	39.1	40.0	40.3	40.5	40.3	39.7	38.8	39.7	41.1
3.5	6.0	7.5	7.0	6.1	5.8	5.6	5.8	6.4	7.3	6.4	5.0
32	25	21	20	16	10		13	18	21	26	29

45.1

1.0

38

44.3

1.8

35

45.3	42.1	39.4	38.7	39.9	40.4	40.6	40.5	39.8	38.7	38.7	39.0
0.8	4.0	6.2	7.4	6.2	5.7	5.5	5.6	6.3	7.4	7.4	7.1
39	32	25	22	17	10		12	17	20	23	25

44.4 39.8

1.2 6.3

34 27

Sta + π - Elev

946.07

+40

✓

+70

T.P. 8.09 949.77 4.39 941.68

+70

949.77

48+00

✓

May 31 1960

LX

E

R

37

45.6	42.3	40.4	39.2	40.2	40.8	41.0	40.8	40.3	39.1	38.1	39.1	41.1
0.5	3.8	5.7	6.9	5.9	5.3	5.1	5.3	5.8	7.0	7.4	6.4	1.7
39	32	25	22	17	10		12	14	20	23	25	34

A.8	A.0	A.6	A.6	A.5	A.2	A.4	A.1	A.9	A.7	A.3
1.3	4.1	5.5	6.5	5.6	4.8	4.7	5.0	5.2	5.4	4.8
39	29	25	22	18	10		12	19	25	32

Sta 48+00

A.6	A.7	A.6
8.2	8.1	8.2
75	64	54

A.0	A.2	A.7	A.3	A.2	A.6	A.1	A.4	A.9	A.4	A.6
8.3	9.6	10.1	9.5	8.6	8.2	8.1	8.4	8.9	10.2	10.4
31	26	24	22	17	10		12	17	21	23

A.9	A.6
8.9	8.2
34	39

A.1	A.5	A.1	A.3
10.7	11.3	11.7	10.5
75	58	39	36

Sta	+	π	-	Elev
-----	---	-------	---	------

		949.77		
--	--	--------	--	--

+30				
-----	--	--	--	--

		11.43	938.34	
--	--	-------	--------	--

		9.67	940.10	
--	--	------	--------	--

+60				
-----	--	--	--	--

49+00				
-------	--	--	--	--

+50				
-----	--	--	--	--

50+00				
-------	--	--	--	--

✓				
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May 5-1960

Lt

2

Rt

38

^{29.0} ^{40.9} ^{41.5} ^{42.0} ^{42.1} ^{41.9} ^{42.1} ^{39.7} ^{39.0} ^{38.6} ^{37.6}
 10.8 8.9 8.3 7.8 7.7 7.9 8.6 10.1 10.8 11.2 12.2
 22 22 18 10 13 18 21 25 34 36

Water level Swamp Rt

"

"

"

Lt

^{38.2} ^{39.6} ^{40.5} ^{42.3} ^{42.6} ^{42.1} ^{42.4} ^{42.8} ^{39.6} ^{38.6} ^{38.4} ^{37.4}
 11.5 10.2 9.3 7.5 7.2 7.1 7.4 7.8 10.2 11.2 11.4 12.1 12.2
 26 24 22 17 10 12 18 23 30 34 36 38

^{38.8} ^{40.2} ^{42.8} ^{42.1} ^{42.9} ^{42.6} ^{42.1} ^{39.9} ^{38.6} ^{38.2} ^{37.6}
 11.0 9.5 7.0 6.1 5.9 6.2 6.7 9.9 11.2 11.6 12.2
 27 23 19 10 13 19 24 28 33 36

^{39.2} ^{40.1} ^{42.3} ^{44.6} ^{45.4} ^{45.5} ^{45.4} ^{44.8} ^{42.3} ^{40.1} ^{38.8} ^{38.4}
 10.6 9.1 7.5 5.2 4.4 4.3 4.7 5.0 7.5 9.1 11.0 11.2 11.9
 29 26 22 18 9 13 19 23 27 33 35 38

^{39.5} ^{40.1} ^{42.8} ^{40.8} ^{42.6} ^{42.8} ^{42.5} ^{40.9} ^{42.8} ^{41.0} ^{39.9} ^{39.5}
 10.3 9.1 6.0 3.0 2.2 2.0 2.3 2.9 6.0 8.8 9.9 10.3
 37 34 23 17 9 13 20 24 29 36 42

^{38.2} ^{38.5}
 11.6 11.3
 84 65

Sta + π - Elev

949.77

+ 40

T.P. 6.51 955.88 0.40 949.37

✓

+ 40

955.88

51+00

+ 29

T.P. 10.68 962.15 4.41 951.47

+ 60

962.15

May 5 1960
39

LT

£

RT

39.4	40.2	44.4	44.2	49.5	46.6	49.4	48.7	44.7	41.8	41.8
10.4	9.6	5.4	0.6	0.3	0.2	0.4	1.1	5.1	8.0	8.0
40	37	26	17	9		13	19	26	33	35

50+38 on Road 1' RT £

40.2 40.9
9.5 8.9
25 48

39.6	40.2	44.6	49.7	50.8	51.2	51.2	51.2	50.4	49.2	43.2	42.3
16.3	15.7	11.4	6.2	5.1	4.7	4.7	4.9	5.5	9.6	12.7	13.6
43	40	28	19	16	7		13	19	26	35	56

40.9	42.5	47.8	52.7	53.0	53.0	52.9	51.4	47.4	44.8	44.8	44.7	45.1
15.0	13.4	8.1	3.2	2.9	2.9	3.0	3.5	8.0	11.1	11.1	11.2	10.8
43	37	24	15	7		14	19	27	34	36	51	69

42.4	42.3	46.4	54.3	54.8	54.8	54.6	54.0	49.7	46.2	46.0	45.9
13.5	13.6	9.5	1.6	1.1	1.1	1.3	1.9	6.2	9.7	9.9	10.0
43	41	32	19	6		14	19	27	37	43	65

Top of fence Post

45.1	45.8	55.6	56.2	56.6	56.1	56.4	55.0	50.6	49.7	49.2	48.5
17.1	16.4	6.6	6.0	5.6	5.5	5.8	6.6	11.6	12.5	13.0	13.4
42	37	21	19	9		14	28	29	36	50	65

Sta + π - Elev

96215

+ 87

✓

52+00

✓

11.44 950.71

+ 11

May 3 1960

40

Lt

E

Rt

A1.2	51.2	57.9	59.1	58.2	57.9	57.4	58.9	57.1	57.1
15.0	10.8	4.3	4.1	4.0	4.3	4.8	8.3	9.1	9.1
40	32	20	9		13	21	28	33	36

A1.0
15.2
43

52.4	51.9	52.0
9.8	10.3	9.2
95	54	43

49.6	50.7	56.4	58.4	58.7	58.8	58.6	58.2	55.2	55.2	54.2
12.6	11.5	5.8	3.6	3.5	3.4	3.6	4.0	7.0	7.0	8.0
42	34	28	23	7		4	23	28	37	44

48.7	48.9	50.1	51.5
13.5	13.3	12.1	10.7
59	72	84	100

55.9	54.8
6.3	7.4
77	63

Flowline 15" CMC Lt

58.8	58.8	58.5	59.0	59.2	59.1	58.5	58.1	57.8	57.8
3.4	3.4	3.7	3.2	3.0	3.1	3.7	4.1	4.4	4.4
46	29	1.6	11		14	27	42	59	75

58.2	58.1	58.1
4.0	4.1	4.1
68	82	100

Sta + π - Elev

Approx $\frac{1}{2}$ "E"
+ 27.57

962.15

+ 46

T.P 12.98 974.16 0.97 961.18

+ 66

May 5 1960

41

Lt

£

Rt

58.2

58.5

59.1

59.2

59.7

59.1

59.2

59.2

59.1

58.6

3.9

3.7

3.1

2.9

2.5

2.5

2.9

3.0

3.1

3.6

83

59

31

14

19

44

67

77

100

58.2

58.1

58.0

57.5

57.7

57.2

57.9

3.9

4.1

4.2

4.7

4.5

5.0

4.3

100

150

200

250

300

200

150

57.8

58.2

58.1

58.2

60.2

60.6

60.6

59.9

59.4

59.2

4.4

4.0

3.5

3.0

2.0

1.6

2.3

2.8

3.0

100

72

50

28

10

17

32

48

75

Large Rock left of £ 32' 52' + 50

59.2

59.2

60.4

61.4

61.5

61.5

60.6

61.9

62.7

15.0

15.0

13.8

12.8

12.7

12.7

13.6

12.3

10.5

16

15

13

5

16

26

35

51

60.9

59.9

59.7

61.4

64.6

13.3

14.3

14.5

12.8

9.6

21

36

57

72

75

64.2

64.2

9.9

9.9

100

93

Sta	+	π	-	Elev
-----	---	-------	---	------

		974.16		
--	--	--------	--	--

52+77				
-------	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

53				
----	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

		8.4		
--	--	-----	--	--

54				
----	--	--	--	--

		5.7		
--	--	-----	--	--

May 5/1960
42

LT

E

RT

60.1	60.1	60.1	61.8	62.0	62.1	61.5	62.2	62.1
14.1	14.1	13.5	12.4	12.2	12.1	12.7	12.0	10.5
17	14	13	6		18	27	33	51

62.4	63.5	63.9	63.9	64.8
11.8	10.7	10.3	10.3	9.4
20	25	43	64	75

64.3	64.1
9.9	10.1
100	83

64.8	64.2	63.0	63.2	63.2	63.2	62.7	62.7	62.9
9.4	10.0	11.2	11.0	11.0	11.0	11.5	11.5	11.3
46	27	12	6		17	22	28	34

64.8	64.9	64.9	65.5	65.9	65.5
9.4	9.3	9.3	8.7	8.3	8.7
72	100	75	66	54	42

Edge BT

Sta	+	π	-	Elev
-----	---	-------	---	------

		974.16		
--	--	--------	--	--

54+50				
-------	--	--	--	--

			2.8	
--	--	--	-----	--

55				
----	--	--	--	--

			0.2	
--	--	--	-----	--

BM				
----	--	--	--	--

		11.36	962.80	
--	--	-------	--------	--

BM				
----	--	--	--	--

	3.83	940.21		
--	------	--------	--	--

			936.38	
--	--	--	--------	--

40+50				
-------	--	--	--	--

41				
----	--	--	--	--

+50				
-----	--	--	--	--

42				
----	--	--	--	--

May 5 1960

Lt

E

Rt

43

Top Hyd N.E. Cor Silver Lake Rd & "E"

Top Breather Pipe Lt St 40 + 35

32.0	32.5	32.9	32.1	32.2	31.6	31.7	31.8	31.4
82	77	73	75	80	86	85	84	88
100	89	73	60	43	38	75	52	33

32.9	32.8	32.1	33.1	32.1	32.6	31.6	31.8	31.6
73	74	75	71	65	76	8.6	8.4	8.6
100	88	65	50	44	35	33	54	75

33.2	32.6	32.9	32.8	33.5	31.7	31.5	31.6	31.6
20	76	73	74	67	85	8.7	8.6	8.6
100	84	73	57	45	35	75	47	34

32.0	33.0	32.5	32.1	32.8	31.7	31.3	31.5	31.4
82	72	67	75	74	85	8.9	8.7	8.8
100	83	79	65	48	37	36	60	75

Sta + π - Elev

940.21

42+50

43

+50

40⁰⁰+50

6.32

9429.2

3.61

936.60

44

May 5, 1960

44

LT
~~32.1 32.3 33.3 33.5 33.1 31.9 31.2 31.4 31.2~~
 75 79 69 67 71 83 9.0 8.8 8.9
 100 96 82 70 56 37 75 51 35

~~32.1 33.5 34.2 32.1 33.1 31.9 31.3 31.2 31.1~~
 7.1 6.7 5.9 7.5 7.1 8.3 18.9 9.0 9.1
 100 87 71 63 49 40 37 53 75

~~33.3 34.1 32.3 32.1 33.1 32.3 30.9 30.8 30.1 30.1~~
 6.9 5.5 6.9 7.1 6.5 7.9 9.3 9.4 9.5 9.5
 65 63 54 49 44 40 75 55 46 34

32.6 33.4 34.4 35.5
 6.6 6.8 5.7 4.7
 70 76 90 100

31.8 31.4 31.2
 8.4 8.8 9.0
 37 55 75

~~32.1 34.2 34.2 34.9 34.6 31.0 30.1 30.8 30.6 30.6~~
 9.2 8.6 8.7 8.0 8.3 6.9 12.8 12.1 12.3 12.3
 37 50 58 63 75 88 35 53 67 75
 5.1 5.6
 100 92

STA. + π - ELV

942.92

44+50

45

+50

+70

46

+43

T.P. 13.29 952.61 3.60 939.32

MAY 5, 1960

45

33.0	33.8 Lt	34.5	34.9	36.0	30.6	30.8 Rt	30.9	31.4
9.9	9.1	8.4	8.0	6.7	12.3	12.1	12.0	11.5
42	46	67	83	92	75	55	40	32

31.5
31.2
5.4 5.7

35.5	35.4	34.1	34.8	33.5	31.6	30.7	30.7	30.6	30.5
7.4	7.5	8.2	8.1	9.4	11.3	12.2	12.2	12.3	12.4
100	95	90	82	66	49	37	51	65	70

32.5	31.8	31.5	31.1	31.6	30.9	30.7	31.0	31.7
10.4	11.1	11.4	11.8	11.3	12.0	12.2	11.9	11.2
98	88	66	57	45	75	57	44	35

10.3
100

32.8	32.2	31.1	30.8	31.5
10.1	10.7	11.8	12.1	11.4
100	86	66	49	40

32.3	32.1	32.4	32.2	32.7
10.6	10.8	10.5	10.7	10.2
100	96	75	58	43

36.0	36.5	36.8	31.6
6.9	6.4	6.1	5.3
100	84	69	46

Sta + π - Elev.

952.61

46+68

+90

47

+11

+40

+70

May 5, 1960 46

41

~~43.6. 42.4. 42.9. 42.9. 43.9.~~
~~9.0 9.2 9.7 9.7 8.7~~
~~100 95 88 70 47~~

~~47.9. 48.1. 48.0. 48.8.~~
~~4.7 4.5 4.6 3.8~~
~~100 85 67 47~~

~~50.6. 49.9. 49.2. 49.8.~~
~~2.0 2.7 3.4 2.8~~
~~100 86 70 49~~

~~51.1. 50.6. 50.1. 49.4.~~
~~1.5 2.0 2.4 3.2~~
~~100 87 71 50~~

~~46.7. 46.4. 45.9. 46.5. 46.5.~~
~~5.9 6.2 6.7 6.1 6.1~~
~~100 85 69 60 42~~

~~41.6. 42.0. 43.4. 42.9. 44.1. 43.3.~~
~~11.0 10.6 9.2 9.7 8.5 9.3~~
~~100 90 71 61 54 46~~

Sta + π - Elev

952.61

48

TP 10.66 952.32 10.95 941.66

7.03 955.67 3.68 948.64

46+43

+68

+90

✓

47

TP 1.36 954.31 2.72 947.95

RG
JS
WM
JH

Lt

4

May 5, 1960
May 6, 1960 47
Cold Windy 46°

39.0 41.0 41.7 41.3 42.0
13.6 11.6 10.9 11.3 10.6
100 81 64 59 53
Sta 48+00 E

43.3 48.0 48.2 49.2 50.0
12.4 7.7 7.5 6.5 5.0
38 50 60 75 85

45.4 48.8 52.6 53.1 53.2
10.3 6.9 3.4 2.6 2.5 2.0
41 50 58 64 75 80

44.5 48.3 52.1 54.3 54.6
11.2 7.4 3.6 1.4 1.1
39 47 56 62 64

55.6 54.9 54.8
0.1 0.8 0.9
90 80 65

45.0 48.4 51.9 52.5 52.5
10.7 7.3 3.8 2.2 2.2
39 47 54 58 63

55.4 54.6 54.2
0.3 1.1 1.5
90 80 65

Sta + π - Elev.

954.31

47+11

+40

TP 2.33 943.99 12.65 941.66

48+30

+60

49

May 6, 1960

48

LT

48.0	47.6	45.4	45.2	50.7	52.8	52.8	52.0
6.3	6.7	8.9	9.1	3.6	1.5	1.5	1.3
52	46	39	40	51	56	63	75

52.9	52.6
0.4	0.7
90	85

45.4	47.6	47.5	47.0
8.9	6.7	6.8	7.4
39	46	52	60 75

37.6	37.0	37.0
6.4	7.0	7.0
36	50	61 75

36.9	36.6	36.2	36.5	36.2
7.1	7.4	2.8	7.5	7.7
41	47	56	66	75

37.5	36.9	36.5	36.2
6.5	7.1	7.5	7.7
37	48	70	75

Sta + π - Elev.

943.99

49+50

TP 4.57 946.23 2.33 941.66

48+30

+60

49

+50

50

TP 6.94 947.97 5.20 941.03

LT

May 6, 1960

49

BT

~~27.5
 65
 41~~
~~27.1
 49
 51~~
~~26.9
 2.1
 64~~
~~27.0
 70
 75~~

sta 48

~~28.2
 29
 100~~
~~28.6
 76
 84~~
~~29.9
 6.4
 68~~
~~29.9
 5.7
 61~~
~~28.5
 6.3
 48~~
~~27.9
 7.7
 39~~

~~28.4
 28
 78~~
~~29.4
 6.8
 94~~
~~29.1
 6.1
 76~~
~~28.8
 5.4
 68~~
~~28.0
 6.2
 52~~
~~28.2
 7.9
 45~~
~~27.9
 8.3
 39~~

~~28.1
 5.5
 100~~
~~28.1
 5.5
 82~~
~~29.9
 6.3
 70~~
~~28.6
 7.6
 58~~
~~27.1
 8.5
 48~~
~~27.6
 8.6
 39~~

~~28.5
 5.7
 100~~
~~29.9
 6.3
 94~~
~~29.1
 7.1
 85~~
~~29.9
 6.3
 74~~
~~29.2
 7.0
 62~~
~~27.2
 8.9
 49~~
~~27.8
 8.4
 42~~

~~28.1
 5.5
 100~~
~~28.0
 6.2
 89~~
~~29.4
 6.8
 81~~
~~28.1
 7.5
 70~~
~~28.2
 8.0
 55~~
~~27.1
 8.5
 42~~

Sta + π - Elev

947.97

50 + 40

+ 70

51

+ 29

+ 60

+ 87

Sta 49 ±

4.15 943.82 43.8

2 May 6, 1960 50

LT

29.9.	28.8.	27.8.	29.0.
8.1	9.2	10.2	9.0
100	81	59	42

28.6.	28.2.	29.0.	29.5.
9.4	9.7	9.0	8.5
100	90	66	44

40.0.	40.0.	40.4.	40.1.
8.0	8.0	7.6	7.3
100	82	64	43

41.2.	41.4.	41.8.	42.1.
6.8	6.6	6.2	5.9
100	84	64	44

42.1.	42.1.	42.9.	43.9.	44.6.
5.3	4.9	4.1	4.1	3.4
100	89	69	52	43

47.0.	45.2.	45.8.	46.1.	46.7.
1.0	2.7	2.2	1.9	1.3
100	91	71	55	44

Sta	+	π	-	Elev.
BM	13.27	976.04		962.77

53 + 13

✓

+43

✓

+69

FS
WM

11

May 2, 1960

51

BT

Top Hyd NE Cor Co Rd "E" Silver Lake Rd

61.9	61.9	63.2	63.1	63.8	63.8	63.0	62.9
14.1	14.1	12.8	12.3	12.2	12.2	13.0	13.2
16	14	11	5		18	25	33

63.9	64.9	64.5	64.6	66.3	66.6	66.3
12.1	X	11.5	11.4	9.7	9.4	9.7
23	45	72	100	61	44	

64.0	64.0	64.8	65.3	65.4	65.2	64.6	63.6	63.6
12.0	12.0	11.2	10.7	10.6	10.8	11.4	12.4	12.4
15	13	9	4		18	24	28	32

68.0	67.8	67.6	66.5	66.2	67.0	66.5	66.8
8.0	8.2	8.4	9.5	9.8	9.0	7.5	7.2
33	46	70	83	100	75	59	46

65.4	65.4	66.0	66.5	66.6	66.5	66.1	64.5	64.5
10.6	10.6	10.0	9.5	9.4	9.5	9.9	10.5	11.5
15	12	10	4		18	24	29	32

68.4	70.6	71.0	69.7	67.5	68.5	70.3	70.8	70.2	67.5
7.6	5.4	5.0	6.3	8.5	7.5	5.7	5.2	5.8	8.5
25	33	45	64	75	71	59	53	46	38

68.1	69.1
7.9	6.9
100	83

Sta + π - Elev

976.04

54

✓

✓

TP 12.54 983.88 4.70 971.34

+30

✓

✓

LT

± May 9, 1960

BT

52

72.2	68.4	64.1	67.8	68.3	68.44	68.5	68.3	68.1	66.7
3.8	7.6	8.9	8.8	7.7	7.6	7.5	7.7	7.9	9.3
29	19	11	8	2		8	20	23	27

72.6	71.7	71.8
3.4	3.3	4.2
53	79	100

76.7	73.5	69.8	67.5	66.7
10.7	2.5	6.2	8.5	9.3
56	49	40	33	30

74.3	69.6	66.3
1.7	6.4	9.7
66	84	100

68.7	68.7	69.3	70.1	70.3	70.1	69.6	68.4
15.2	15.2	14.6	13.8	13.6	13.8	14.2	15.5
13	10	8		10	20	26	29

71.1	73.3	73.7	74.1	80.8	74.9	70.2	66.4
12.8	10.6	10.2	9.8	3.1	9.0	13.7	15.5
21	30	45	63	60	48	37	31

74.9	74.6	71.6	73.8
9.0	9.3	6.3	10.1
100	85	77	100

Sta + π - Elev

983.88

54+65

✓

✓

55

✓

✓

May 8 1960

53

LT

RT

73.9	70.7	70.7	71.5	72.1	72.3	72.1	71.4
10.0	13.2	13.2	12.4	11.8	11.6	11.8	12.5
23	13	11	8		10	22	28

75.7	76.0	75.9	76.3	71.9	70.6	70.6
8.2	7.9	8.0	7.6	12.4	13.3	13.3
32	52	71	87	37	34	31

77.6	77.5	83.7	82.7	80.9
6.3	6.4	0.2	1.2	3.0
100	49	61	81	100

75.3	73.1	73.1	73.4	74.0	74.2	74.1	73.7	72.6
8.6	10.8	10.8	10.5	9.9	9.7	9.8	10.2	11.3
20	11	9	6		12	21	29	33

77.1	78.9	78.1	77.4	83.9	80.7	76.9	72.6
6.8	5.0	5.8	6.5	0.0	3.2	7.0	11.3
25	36	55	72	66	55	48	38

81.0	80.5	78.3
2.9	3.4	5.6
100	97	83

Sta + π - Elev

983.88

²⁵
55 + ~~22~~

✓ ✓
TP 6.80 988.96 1.72 982.16

55

+25

+64

✓

± May 9, 1960

54

LT

BT

79.4	76.3	75.6	74.6	74.6	75.3	75.6	75.5	75.1	74.3
45	76	8.3	9.3	9.3	86	8.3	8.4	8.8	9.6
32	19	14	11	8		12	22	29	33

79.9	80.9	82.0	83.9
40	30	19	0.0
42	67	81	100

82.9	79.4	74.8
10	45	91
56	53	42

85.2	85.7	85.4
38	33	36
72	88	100

86.6	86.7	86.5
24	23	25
65	78	100

77.7	74.1	74.1	77.0	77.0	77.1	77.0	76.6	76.0
113	14.9	14.9	120	12.0	11.9	12.0	12.4	13.0
19	9	7	5		13	23	30	35

80.1	81.6	83.2	84.3
8.9	7.4	5.8	4.7
27	61	84	100

86.4	86.4	86.0	83.1	76.3
2.6	2.6	3.0	5.9	12.7
100	83	61	56	43

Sta + π - Elev

988.96

~~+90~~ +75

✓

✓

56

TP 7.28 986.44 9.80 979.16

May 9, 1960 55

14

BT

74.9	74.9	77.0	77.3	77.8	77.6	77.3
14.1	14.1	12.0	11.7	11.2	11.4	11.7
13	11	4		15	24	31

76.2	77.5	80.8	82.1	86.6	84.0	87.3	86.7
10.8	9.5	8.2	6.9	2.4	5.5	1.7	12.3
25	50	75	100	68	60	46	35

87.6	87.9	86.7
1.4	1.1	2.3
79	89	100

75.9	74.6	74.6	77.0	77.4	77.9	77.8	77.2	78.1
13.1	14.4	14.4	12.0	11.6	11.1	11.2	11.8	10.9
19	14	11	4		14	25	32	47

77.5	77.1	77.6	80.6	86.1	87.3	86.6	83.8
11.2	9.9	9.4	8.4	2.3	1.7	2.4	5.2
24	49	68	79	100	77	70	59

81.5

75

100

Nail in PP BT Sta 57

Sta	+	π	-	Elev.
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		986.44		
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56+29				
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✓				
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✓				
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+54				
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✓				
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✓				
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PK
JS
WNI

LT

May 10, 1960

56

RT

74.6	74.3	74.9	74.5	74.8	74.3	74.1	74.5	74.2	74.8
11.8	12.1	11.5	8.9	8.6	8.1	8.3	8.9	9.2	8.6
19	12	9	3		15	25	33	37	45

75.6	76.4	77.8	76.2
10.8	9.5	8.6	8.2
22	29	40	63

73.0	72.1	70.7	70.7
3.4	4.3	5.7	7.7
100	79	64	53

78.4	78.6
8.0	7.8
100	94

74.1	75.6	77.7	77.9	78.7	78.5	77.8	78.0
12.3	10.8	8.7	8.4	7.7	7.9	8.6	8.4
12	8	3		16	26	34	45

74.7	76.8	77.5	78.4	82.3	82.9	81.1	79.6
12.2	9.6	8.9	8.0	4.1	4.4	5.3	6.8
20	26	43	67	100	90	73	57

77.2	78.8
9.2	7.6
100	93

Sta + π - Elev.

986.44

56+82

✓

✓

57

✓

✓

May 10, 1960 57
BT

74.4	74.5	75.1	77.7	78.1	78.6	78.9	78.8	77.9
12.0	11.9	11.3	8.7	8.3	7.8	7.5	7.6	8.5
26	12	9	2		5	17	20	35

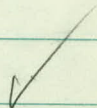
76.5	77.6	76.6	78.0	82.9	81.2	78.9	77.9
9.9	8.8	9.8	8.4	3.5	5.2	7.5	8.5
35	54	73	90	80	62	51	44

77.8	84.0
8.6	2.4
100	100

74.7	74.6	75.4	78.1	78.3	78.9	79.0	76.8	78.2
11.7	11.8	11.0	8.3	8.1	7.5	7.4	7.6	8.2
26	13	9	2		6	16	26	34

74.5	75.1	74.7	76.2	80.5	80.2	79.0	77.5
11.9	11.3	11.7	10.2	5.9	6.2	7.4	8.9
29	36	52	61	75	65	55	41

76.0	76.2	82.4	82.7
10.4	10.2	4.0	3.7
100	85	94	100



Sta + A - Elev.

986.44

57428

✓

✓

+68

✓

✓

2 May 10, 1960 58

Lt

Rt

74.3	74.6	75.7	76.0	78.5	79.0	79.2	78.9	78.5
12.1	11.8	10.7	8.4	7.9	7.4	7.2	7.5	7.9
23	13	7	3		5	17	27	33

73.7	74.2	74.9		81.9	78.9	77.5	77.4
12.7	12.2	11.5		4.5	7.5	8.9	9.0
25	31	41		86	69	57	48

76.2	76.4	74.9	75.4		81.4
10.2	10.0	11.5	11.0		5.0
100	84	70	57		100

74.7	75.0	76.6	78.2	78.5	79.2	79.4	79.2	78.4
11.7	11.4	9.8	8.2	7.9	7.2	7.0	7.2	8.0
17	10	6	2		5	18	28	35

73.4	74.6	74.0		80.6	78.8	77.6	77.7
13.0	11.8	12.4		5.8	7.6	8.8	8.7
27	36	44		69	58	55	48

76.0	75.7	74.8	75.6		81.9	82.8	82.9
10.4	10.7	11.6	10.8		4.5	3.6	3.5
100	91	69	55		75	94	100

Sta + π - Elev

986.44

58

✓

✓

T.P. 6.42 988.29 4.57 981.87

+23

✓

✓

± May 10, 1960 59

LT

RT

73.4	74.9	75.6	76.1	78.7	79.5	79.8	79.6	79.0
130	115	108	83	77	69	66	68	74
29	16	10	3		6	20	28	35

74.2	74.2	74.5	84.4	82.6	81.0	78.5
12.2	12.2	11.9	2.0	38	54	7.9
42	54	68	87	68	57	45

74.5	74.7	74.4	75.2	85.0
11.9	11.7	12.0	11.2	1.4
100	94	85	79	100

✓

74.4	74.9	75.9	78.3	79.1	79.8	80.1	79.9	79.2
13.9	13.4	12.4	10.0	9.2	8.5	8.2	8.4	9.1
23	17	9	3		6	15	28	38

74.6	74.2	74.8	83.5	82.9	81.3	78.6
13.7	14.1	13.5	4.8	54	7.0	9.7
38	46	62	59	54	52	44

74.7	73.8	75.3	85.3	85.7
13.6	14.5	13.0	3.0	2.6
100	84	73	79	100

✓

Sta	+	π	-	Elev.
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		988.29		
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58+46				
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✓				
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✓				
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+67				
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BM	5.06	988.29	5.06	983.23
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± May 10, 1960 60

LT

RT

74.4	74.2	74.9	78.9	79.7	80.7	80.4	80.2	79.9
13.9	14.1	13.4	9.4	8.6	8.0	7.9	8.1	8.4
46	28	16	3		7	18	29	34

74.8	75.0	74.8	85.4	84.8	82.0	78.8
13.5	13.3	13.5	2.9	3.5	6.3	9.5
58	68	90	59	54	51	43

75.3	85.1	85.5	85.4
13.0	3.2	2.8	2.9
100	72	94	100

74.7	75.2	76.6	79.6	80.2	80.6	80.6	80.5	79.9
13.6	13.1	11.7	8.7	8.1	7.7	7.7	7.8	8.4
44	29	12	3		7	19	30	37

75.4	76.5	76.9	85.9	85.4	82.7	79.3
12.4	11.8	11.4	2.4	2.9	5.6	9.0
63	83	100	60	55	52	44

84.8	84.8	84.7
3.5	3.5	3.6
71	90	100

Top Hyd Rt. Sta 59+15

Sta + π - Elev.

988.29

58+77

✓

✓

59

✓

✓

May 10, 1960

61

LT

RT

79.0	78.1	78.6	80.3	80.4	80.1	80.1	80.6	80.3
9.3	10.2	9.7	8.0	7.9	7.6	7.6	7.7	8.0
16	11	6	2		7	18	30	33

78.6	78.1	76.8	85.1	82.3	77.8	79.5
9.7	12.2	11.5	2.6	6.0	8.5	8.8
34	50	68	53	50	44	41

78.2	77.7	85.1	84.7	84.9	84.8
10.1	10.6	2.6	3.6	3.4	3.5
100	90	58	74	90	100

80.3	80.3	79.3	80.3	80.5	80.9	81.0	80.8	80.5
8.0	8.0	9.0	8.0	7.8	7.4	7.3	7.5	7.8
29	10	6	3		7	18	29	35

79.8	78.8	79.9	80.6	84.1	84.2	80.9	79.6
8.5	9.5	8.4	7.7	4.2	4.1	7.4	8.7
46	55	73	92	65	56	41	45

84.1	84.9	85.2
7.2	3.4	3.1
100	87	100

Sta + π - Elev.

988.29

59+31

✓

✓

+60

✓

✓

± May 10, 1960

62

11

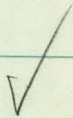
RT

81.5	82.3	82.2	79.7	80.7	81.2	81.2	81.1	80.5
6.8	6.0	6.1	8.6	7.6	7.1	7.1	7.2	7.8
47	30	15	5		7	18	28	36

82.1	82.6	83.0
6.2	5.7	5.3
67	86	100

82.9	81.5	81.8	80.2
5.4	6.8	6.5	8.1
79	60	52	42

84.6
3.7
100

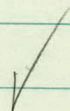


83.2	80.9	79.7	80.6	80.8	81.3	81.4	81.2	80.2
5.1	7.4	8.6	7.7	7.5	7.0	6.9	7.1	8.1
16	10	5	2		7	18	29	41

83.6	82.6	82.5
4.7	5.7	5.8
30	50	69

85.2	83.0	82.0	82.4
3.1	5.3	6.3	5.9
100	74	56	52

82.9	82.6
5.4	5.7
100	94



Sta + π - Elev

988.29

60

✓

✓

+ 24

✓

✓

2 May 10, 1960

63

Lt

Rt

$\delta^{3.2}$	$\delta^{2.2}$	$\delta^{0.4}$	$\delta^{0.4}$	$\delta^{1.3}$	$\delta^{1.6}$	$\delta^{1.6}$	$\delta^{1.4}$	$\delta^{1.1}$
5.1	6.1	7.9	7.9	7.0	6.7	6.7	6.9	7.2
22	12	7	5		6	19	28	35

$\delta^{2.6}$	$\delta^{1.2}$	$\delta^{0.2}$	$\delta^{0.8}$	$\delta^{4.9}$	$\delta^{4.6}$	$\delta^{2.3}$	$\delta^{0.5}$
5.7	7.1	8.1	7.5	3.4	3.7	6.0	7.8
42	65	77	90	67	53	50	44

$\delta^{1.0}$	$\delta^{5.6}$	$\delta^{5.7}$
7.3	2.7	2.6
100	91	100

$\delta^{2.1}$	$\delta^{1.9}$	$\delta^{1.0}$	$\delta^{0.6}$	$\delta^{1.5}$	$\delta^{1.7}$	$\delta^{1.7}$	$\delta^{1.5}$	$\delta^{1.0}$
6.2	6.4	7.3	7.7	6.8	4.6	6.6	6.8	7.3
28	20	12	7		7	18	28	37

$\delta^{1.1}$	$\delta^{1.0}$	$\delta^{0.5}$	$\delta^{6.6}$	$\delta^{5.3}$	$\delta^{5.5}$	$\delta^{0.9}$
7.2	7.3	8.8	1.7	3.0	4.8	7.4
36	54	75	63	52	51	43

$\delta^{0.4}$	$\delta^{0.0}$	$\delta^{0.2}$	$\delta^{5.8}$
8.9	9.3	1.1	2.5
100	89	80	100

Sta + π - Elev

988,29

60+35

✓

✓

+58

✓

✓

May 10, 1960 64

11

81

81.1	81.2	81.0	80.3	81.6	81.7	81.7	81.5
7.2	7.1	7.3	8.0	6.7	6.6	6.6	6.8
55	39	20	6		7	17	27

77.9	77.4	76.2	85.6	83.7	81.3	81.0
10.4	10.9	12.1	2.7	4.6	7.0	7.3
66	76	83	52	51	45	37

77.1	77.5	86.6	87.1	85.0
9.2	10.8	1.7	1.2	3.3
100	93	63	81	100

81.6	80.6	80.6	81.2	81.6	81.7	81.9	81.5	80.8
6.7	7.7	7.7	7.1	6.7	6.6	6.5	6.8	7.5
41	27	10	4		8	17	27	37

81.1	77.6	78.3	85.8	84.3	81.5
7.2	10.7	10.0	2.5	4.0	6.8
65	75	89	53	52	45

77.0	86.7	86.7	84.6
9.3	1.6	1.6	3.7
100	64	81	100

Sta	+	π	-	Elev.
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		988.29		
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60 + 76				
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✓				
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✓				
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61				
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✓				
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✓				
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May 10, 1960

65

21

81

81.4

81.1

80.9

80.6

81.2

81.8

81.8

80.5

80.8

6.9

7.2

7.4

7.7

7.1

6.5

6.5

6.8

7.5

70

49

31

14

7

16

27

36

81.6

80.2

8.7

8.1

80

100

86.5

85.9

84.3

82.4

1.8

2.4

4.0

5.9

64

50

50

47

86.3

84.5

2.0

3.8

79

100

82.1

82.5

81.4

80.6

81.4

81.8

81.7

81.4

80.7

6.2

5.8

6.9

7.7

6.9

6.5

6.6

6.9

7.6

59

42

18

6

6

16

26

38

82.4

82.2

5.9

6.1

79

100

85.8

85.9

83.4

81.9

2.5

2.4

4.9

6.4

59

49

48

45

84.9

83.9

3.4

4.4

81

100

Sta	+	π	-	Elev.
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		988.29		
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61+50				
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✓				
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✓				
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TP	7.25	988.12	7.42	980.87
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+90				
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✓				
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✓				
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May 10, 1960 66
51

83.8	82.8	81.4	80.4	81.1	81.3	81.2	80.9	80.6
4.5	5.5	6.9	7.9	7.2	7.0	7.1	7.4	7.7
56	34	18	6		5	16	26	32

83.6	84.0	85.0		86.3	83.9	80.9	80.0
4.7	4.3	3.3		2.0	4.4	7.4	8.3
70	86	100		50	48	43	38

86.9	85.3	83.6
1.4	3.0	4.7
64	85	100

83.5	82.5	81.6	79.6	80.0	80.1	80.1	79.8	79.4
4.6	5.6	6.5	8.5	8.1	8.0	8.0	8.3	8.7
45	25	15	7		5	15	26	33

84.6	85.0	85.1		82.9	83.0	80.1	78.8
3.5	3.1	2.4		5.2	5.1	8.0	9.3
60	83	100		69	50	45	39

81.9	79.9
6.2	8.2
90	100

Sta + π - Elev.

988.12

62

✓

✓

+18

✓

✓

£ May 10, 1960 67

LT

RT

83.7	82.6	81.6	79.1	79.4	79.7	79.7	79.3	78.9
44	55	65	90	87	84	84	88	92
47	27	15	8		5	15	26	33

84.5	82.9	82.8	83.0	82.3	82.9	79.8	78.2
36	42	53	51	58	58	83	99
55	77	92	100	70	50	45	37

80.9	79.2
72	89
90	100

✓

82.9	81.5	78.1	78.6	78.8	79.0	78.7	78.4
52	66	100	95	93	91	94	97
36	19	9		4	15	26	32

83.9	81.6	80.9	80.9	82.1	81.9	79.7	77.6
42	65	72	72	60	62	84	105
55	73	86	100	70	51	47	37

81.1	78.5
70	96
87	100

✓

Sta + π - Elev.

988.12

62+52

✓

✓

T.P. 1.15 980.46 8.81 979.31

+ 71

✓

63

TP 1.93 974.80 7.59 972.87

£ May 10, 1960 68
R1

Lt

78.8	77.5	76.6	77.1	77.4	77.7	77.4
9.3	10.6	11.5	11.0	10.7	10.4	10.7
28	18	6		4	15	26

76.9	74.0	77.8	77.8	78.8	76.2	77.0
9.2	9.1	10.3	9.3	7.3	11.9	11.1
44	54	64	77	52	37	33

77.7	77.8	76.5	77.4
10.4	10.3	11.6	10.7
100	81	100	97

75.9	75.5	76.3	75.5	76.5	76.9	76.6	76.3	75.4
4.6	5.0	4.2	5.0	4.0	3.6	3.9	4.2	5.1
48	29	14	7		15	26	32	38

76.6	76.6	77.3	72.9	73.8	75.9	79.2
3.9	3.9	3.2	7.6	6.7	4.6	1.3
64	84	100	100	95	70	50

72.6	71.6	72.4	73.8	74.7	75.5	75.6	75.4	75.1	72.8
7.9	8.9	8.1	6.7	5.8	5.2	4.9	5.1	5.4	7.7
49	29	24	16	7	5	15	25	31	39

72.9	73.8	75.2	76.4	64.5	66.8	70.2	72.5
7.6	6.7	5.3	4.1	16.0	13.7	10.3	8.0
62	79	92	100	100	76	53	45

Sta + π - Elev

974.80

63+35

✓

+ 70

✓

64

✓

BM 0.29 972.17 2.92 971.88

2 May 10, 1960 69
BT

LT

71.1	70.8	72.1	73.4	73.7	73.9	74.1	73.8	73.3
3.7	4.0	2.7	1.4	1.1	0.9	0.7	1.0	1.5
41	22	12	5		3	14	24	29

70.8	72.0	73.0
40	2.8	1.8
59	84	100

63.8	65.8	67.4	70.0
11.0	9.0	7.4	4.8
100	80	59	39

69.6	69.1	70.4	71.9	72.2	72.4	72.6	72.4	71.8
5.2	5.7	4.4	2.9	2.6	2.4	2.2	2.4	3.0
40	27	14	4		3	14	24	30

69.3	70.6	72.9
5.5	4.2	1.9
61	84	100

61.8	63.9	65.1	68.3
13.0	10.9	9.1	6.5
100	85	63	42

68.0	69.4	69.9	70.6	71.1	71.2	71.2	70.9	70.6
6.8	5.5	4.9	4.2	3.7	3.6	3.6	3.9	4.3
32	20	10	4		4	13	25	32

68.0	68.0	69.4	71.1	70.8	63.8	65.1	67.9
6.8	6.8	5.4	3.7	14.0	11.0	9.1	6.9
45	57	79	100	100	79	62	40

Spike in PP Rt Sta 63+89

Sta + π - Elev

972.17

64+29

✓

+59

✓

+72

✓

FA
RG
JS
JL
WM

4 May 11, 1960

70

Lt

Rt

69.9	68.2	69.5	70.1	70.4	70.4	70.4	70.1	69.6
7.3	4.0	2.7	2.1	1.8	1.8	1.8	2.1	2.7
59	37	20	5		3	13	23	31

69.3	70.5
2.9	1.7
82	100

67.6	67.1	64.8	66.5	68.1
8.6	8.5	7.4	5.7	4.1
100	96	74	50	37

68.2	68.0	69.0	68.6	69.0	69.0	68.8	68.4	67.9
4.0	4.2	3.2	3.6	3.2	3.2	3.4	3.8	4.3
74	49	27	8		3	13	23	29

69.8	70.1
2.4	2.1
97	100

58.9	59.2	59.1	59.6	64.5
13.3	12.9	14.1	12.6	7.7
100	94	72	51	36

69.4	67.9	67.5	66.3	68.5	68.5	68.3	67.9	67.3
2.8	4.3	4.7	3.9	3.7	3.7	3.9	4.3	4.9
28	17	10	5		3	13	24	30

69.1	67.6	68.0	68.4
3.1	4.6	4.2	3.8
44	60	82	100

57.9	57.5	59.2	63.9
14.3	14.7	13.0	8.3
100	75	50	37

STA

+

π

-

ELV.

972.17

64+93

✓

T.P.

4.08

969.16

7.09

965.08

65+00

✓

+ 30

FK
RG
JS
JL
WM

Lt

Q

MAY 11, 1960

71

Rt

68.0	67.5	66.9	67.4	67.6	67.6	67.5	67.0	66.2
4.2	4.7	5.3	4.8	4.6	4.6	4.7	5.2	6.0
55	36	18	6		3	13	24	30

67.6	68.0	68.3	57.8	57.7	57.7	57.9	62.3
4.6	4.2	3.9	14.4	14.5	14.5	12.5	9.9
70	92	100	100	86	62	44	37

67.5	66.4	63.7	64.5	66.8	67.2	67.2	67.2	66.7	65.8	61.5
1.7	3.8	5.5	4.7	2.4	2.0	2.0	2.0	2.5	3.4	7.7
46	32	21	11	5		3	13	24	31	37

67.1	67.4	67.5	58.4	58.0	57.8	59.2
2.1	1.8	1.7	10.8	11.2	11.4	10.0
66	81	100	100	80	61	44

65.1	64.7	61.4	61.1	65.7	65.9	66.0	65.6	65.2	58.7
4.1	4.5	7.8	7.5	3.5	3.3	3.2	3.6	4.0	10.5
55	35	26	14	8		13	23	30	41

65.0	61.6	62.0	53.7	53.4	54.0	55.5
4.2	7.6	7.2	15.5	15.8	15.2	13.7
76	83	100	100	87	66	57

STA

+

Σ

-

ELV

969.16

65+47

TBM

11.67

969.67

11.16

958.00

65+61

✓

+ 76

✓

RA
 RG
 JS
 JL
 WM

Lt

2

MAY 11, 1960
 Rt. 72

60.0	59.9	60.0	64.1	65.2	65.1	65.2	64.1	59.0
9.2	9.3	9.2	4.5	4.0	3.8	4.2	4.5	10.2
68	44	23	14		13	22	30	3.9

60.6
 8.7 8.2
 86 100

51.4 51.7 52.7 55.3
 17.8 17.5 16.5 13.9
 100 90 72 55

Top Hyd Rt Sta 68+16

59.5	60.0	63.9	64.6	64.9	64.9	64.5	64.3	59.4
10.2	9.7	5.8	5.1	4.8	4.8	5.2	5.4	10.3
45	23	14	9		14	23	29	38

59.7 60.9
 10.0 8.8
 69 100

53.6 53.2 55.2 56.2
 16.1 16.5 14.5 13.5
 100 90 68 54

60.9	60.8	61.7	64.2	64.3	64.4	64.2	63.7	60.0
8.8	8.9	8.0	5.5	5.4	5.3	5.7	6.0	9.7
66	35	13	5		13	23	30	37

60.9
 8.8
 100

56.5 58.6 59.4
 13.2 11.1 10.3
 100 78 52

STA

+

△

-

ELU

969.67

65+91

✓

66+00

✓

+21

✓

RG
JL
JH

Lt

2

MAY 12, 1960

Rt.

73

64.8	65.4	63.8	63.4	63.8	63.9	63.7	63.6	62.0
4.9	4.3	5.9	6.3	5.9	5.8	6.0	6.1	7.7
50	38	31	10		13	22	30	35

65.1	66.5	59.6	62.3	63.2	63.9	63.1	61.9
4.6	3.2	10.1	7.4	6.5	5.8	6.6	7.8
66	100	100	74	55	53	46	39

67.0	66.4	64.0	63.4	63.2	63.7	63.6	63.4	63.3	62.1
2.7	3.3	5.7	6.3	6.5	6.0	6.1	6.3	6.4	7.6
66	42	34	13	5		12	22	29	32

67.3	66.9	60.6	62.7	64.1	65.5	64.9
2.4	2.8	9.1	7.0	5.6	4.2	4.8
86	100	100	87	69	52	44

65.6	64.8	61.9	62.2	63.1	63.1	62.8	62.5	61.7
4.1	7.9	7.8	7.5	6.6	6.6	6.9	7.2	8.0
44	23	15	6		12	22	28	32

65.3	66.7	67.5	68.5	61.1	63.0	64.8	66.9	64.1	62.3
4.4	3.0	2.2	1.2	8.6	6.7	4.9	2.8	2.6	7.4
54	75	93	100	100	88	68	54	52	39

STA.

+

Δ

-

Elev.

969.67

66+51

✓

T.P.

7.78

968.82

8.63

961.04

+84

✓

67+00

RG
JL
JH

Lt.

2

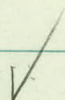
MAY 12, 1960

Rt

74

70.4	64.1	60.5	60.8	62.3	62.3	62.2	62.0	61.8	60.7	60.9
+07	5.0	9.2	8.9	7.4	7.4	7.5	7.7	7.9	9.0	8.8
32	22	12	7	2		13	22	28	33	40

70.3	70.1	70.5
+06	+10	+08
48	92	100



60.6	62.3	64.4	67.0
9.1	7.4	5.3	2.7
100	85	65	54

66+93 SPIKE ON Rt. SHOULDER

64.2	62.8	59.7	59.7	61.4	61.4	61.4	61.3	61.1	59.2
4.6	6.0	9.1	9.1	7.4	7.4	7.4	7.5	7.7	9.6
35	23	15	12	3		11	21	28	37

67.2	68.6	70.5
1.6	02	+1.7
60	81	100

53.5	56.7	59.7	61.9	62.0
15.3	12.1	9.1	6.9	6.8
100	82	61	51	47

62.4	59.9	56.4	60.3	61.1	61.1	60.9	60.4	57.4
6.4	8.9	10.4	8.5	7.7	7.7	7.9	8.4	11.4
44	30	16	9		11	21	31	39

65.6	61.3	68.5
3.2	1.5	03
66	86	100

50.3	54.7	56.5	57.6
18.5	14.1	12.3	11.2
100	70	53	43

STA

+

△

-

Elev.

968.82

67+25

✓

+40

✓

+63

✓

RG
JL
JH

Lt.

Q

MAY 12, 1960

Rt.

75

60.6	56.2	56.4	59.7	60.5	60.5	60.4	59.5	56.2
8.2	12.6	12.4	9.1	8.3	8.3	8.4	9.3	12.6
56	33	27	20		10	21	34	40

63.2	65.2
5.6	3.6
78	100

45.2	47.6	49.0	50.6	53.1
23.6	21.2	19.8	18.2	15.7
100	84	64	53	45

56.0	55.5	59.5	60.3	60.2	60.3	60.1	54.0	54.8
12.8	13.3	9.3	8.5	8.6	8.5	8.7	9.8	14.0
41	30	21	12		10	20	37	43

59.3	61.5	62.5
9.5	7.3	6.3
62	89	100

44.3	44.0	46.3	44.2
25.5	24.8	22.5	20.6
100	92	71	56

58.1	56.3	55.5	59.5	60.0	60.0	59.7	58.6	52.3
10.7	12.5	13.3	9.3	8.8	8.8	9.1	10.2	16.5
72	52	33	25		11	21	42	55

60.1
8.7
100

43.6	44.6	46.5
25.2	24.2	23.3
100	84	65

STA

+

K

-

ELV.

968.82

68+00

✓

+19

✓

TP

11.21

974.63

5.40

963.42

16

68+55

974.63

✓

✓

FK
RG
JS
JL
WM
JH

Lt.

2

MAY 12, 1960

Rt

76

56.3	57.6	59.1	59.8	59.8	59.5	58.0	57.3
10.5	11.3	9.1	9.0	9.0	9.3	10.8	16.5
32	24	18		11	21	40	52

59.4	61.6	63.1
9.4	7.2	5.1
50	76	100

45.4	46.7	49.0
23.4	22.1	19.8
100	88	69

60.1	58.1	58.2	59.6	59.8	59.7	59.5	58.9	59.1	55.1
8.7	10.7	10.6	9.2	9.0	9.1	9.3	9.9	11.4	13.1
20	17	13	9		11	20	27	35	41

60.8	62.0	63.9	65.4
8.0	6.8	4.9	3.4
33	55	79	100

47.6	49.1	49.6	51.4	54.0
21.2	19.7	19.2	17.4	14.8
100	88	78	66	52

68+50 BREATHER PIPE GUARD POST (TOP) Lt.

64.4	64.0	68.5	59.6	59.6	59.7	59.5	59.3	68.0
10.2	10.6	16.1	15.0	15.0	14.9	15.1	15.3	16.6
35	28	17	9		9	20	26	34

65.8	68.9	71.4	72.1
8.8	5.7	3.2	2.5
52	72	88	100

55.1	57.6	57.9	57.1	57.1
19.5	17.0	16.7	17.5	17.5
63	51	41	39	36

53.2	50.3
21.4	24.3
79	100

STA

+

π

-

ELV.

974.63

69+00

✓

✓

+23

✓

+50

✓

MAY 12, 1960

77

FR
RG
JS
JL
wm
JH

Lt.

L

Rt.

61.6	59.0	59.0	59.8	60.1	60.1	59.9	59.3	58.9
13.0	15.6	15.6	14.8	14.5	14.5	14.7	15.3	15.8
24	18	11	7		11	20	27	34

67.7	69.8	70.7	72.5
6.9	4.8	3.9	2.1
37	62	85	100

65.1	56.8	59.3	59.9	58.0
19.5	17.8	15.3	14.7	16.6
78	71	54	46	39

55.1	51.2
21.5	23.4
91	100

67.5	63.5	54.4	54.3	60.0	60.3	60.3	60.1	59.4	58.9
7.1	7.1	15.2	15.3	14.6	14.3	14.3	14.5	15.2	15.7
35	29	20	13	9		10	19	29	41

67.0	65.3	69.1
7.6	6.3	5.5
48	75	100

50.9	52.1	54.0	57.3	58.5
23.7	22.5	20.6	17.3	16.1
100	93	77	65	55

65.6	65.2	64.3	62.8	60.5	60.7	60.7	60.4	60.2	59.4
9.0	9.4	10.3	11.8	14.1	13.9	13.9	14.2	14.4	15.2
100	69	46	22	9		9	19	23	36

50.4	51.5	52.7	56.6	57.8
24.2	23.1	21.9	18.0	16.8
100	89	74	64	59

STA

+

π

-

ELV.

974.63

69+75

✓

70+00

✓

+35

FK
RG
JS

Lt

L

11/4/12, 1960

Rt

28

JL
WM
JH

65.3	64.1	62.6	61.0	61.3	61.1	60.8	60.2	59.2
9.3	10.5	12.0	13.6	13.3	13.5	13.8	14.4	15.4
74	52	31	12		9	19	33	48

65.4

8.7 HOUSE

90

50.6	51.3	56.5	51.5
24.0	23.3	18.1	17.1
100	78	67	59

65.1	64.1	62.5	61.1	61.9	61.7	61.3	60.9	59.8
8.9	10.5	12.1	12.9	12.7	12.9	13.3	13.7	14.8
82	57	34	13		9	18	21	47

65.1

8.9 HOUSE

93

50.6	51.1	50.6	51.6	51.6	51.6
24.0	24.9	24.0	20.0	17.0	16.0
100	91	77	69	64	58

63.1	62.2	61.8	62.6	62.7	62.7	62.6	62.3	61.9	61.2
11.5	12.4	12.8	12.0	11.9	11.9	12.0	12.3	12.7	13.4
60	41	18	9	5		9	18	27	45

63.1	64.9	64.9
10.9	9.7	9.7
77	96	100

51.3	51.1	51.6	56.2	60.8
23.3	23.5	23.0	16.4	13.8
100	90	72	60	52

STA

+

π

-

ELV.

974.63

70 + 50

✓

+ 73

✓

✓

71 + 00

FK
RG
JS
JL
wm
JH

Lt.

2

MAY 12, 1960

79

Rt

56.2	56.0	59.6	63.2	63.1	63.1	63.0	62.7	62.2	61.9
18.4	18.6	15.0	11.4	11.5	11.5	11.6	11.9	12.4	12.7
38	27	18	9	6		9	18	32	46

58.5	59.9	61.5	52.0	52.3	51.9	58.2
16.1	14.7	13.1	22.6	22.3	22.7	16.4
57	79	100	100	86	70	59

55.7	59.7	63.6	63.8	63.9	63.8	63.5	63.0	63.1
18.9	14.9	12.2	10.8	10.7	10.8	11.1	11.6	11.5
27	20	10	8		9	18	32	42

55.1	55.4	55.5	53.2	54.3	53.1	53.0	60.0	
19.5	WATER	19.2	19.1	21.4	20.3	21.5	21.6	14.6
29		68	89	89	82	76	67	55

55.8	53.8
18.8	20.8
100	100

57.0	60.0	64.4	64.8	64.9	64.8	64.5	63.9	61.6	55.4
17.6	14.6	10.2	9.8	9.7	9.8	10.1	10.7	13.0	19.2
26	22	11	6		9	17	33	43	54

55.7	55.3	56.6	56.6	54.4	54.3	
18.9	19.3	WATER	18.0	18.0	20.2	20.3
33	37		100	92	81	71

STA

+

π

-

ELV

974.63

71 + 22

✓

+47

✓

+74

✓

T.P.

13.35

985.24

2.74

971.89

RG
JS
JL
WM
JH

MAY 12, 1960

80

Lt

E

Rt.

57.5	60.5	64.2	65.5	65.9	65.9	65.8	65.5	64.8	63.4	57.2
17.1	14.1	10.7	9.1	8.7	8.7	8.8	9.1	9.8	11.2	17.4
32	26	17	11	5		8	17	29	39	48

57.0	55.3	55.0	
17.6	19.3	19.6	WATER
37	52	53	

58.8	51.0	55.3	55.3
15.8	17.6	19.3	19.3
100	93	82	65

58.6	60.7	63.8	66.8	67.1	69.1	69.0	66.9	67.5	68.6	65.2
16.0	13.9	10.8	7.8	7.5	7.5	7.6	7.7	7.1	6.0	9.4
47	37	26	13	7		8	17	26	31	36

57.1	55.9	54.8	
17.5	18.7	19.8	WATER
56	69	76	

64.2	62.9	62.1	61.9	64.4
10.4	11.7	12.5	12.7	10.2
100	78	60	50	43

66.8	67.7	67.1	68.0	68.4	68.3	68.2	67.6	67.0	67.2
7.8	6.9	7.5	6.6	6.2	6.3	6.4	7.0	7.6	5.4
37	29	19	12	6		17	27	35	49

65.3	63.1	61.0	57.6
9.3	11.5	13.6	17.0
49	65	82	100

69.8	10.2	10.0
4.8	4.4	4.6
100	80	62

72+35 TOP OF WATER SHUT-OFF APP. 35' Rt.

STA

+

△

-

ELV.

985.24

72+00

✓

+35

✓

+58

FK
RG
JS
JL
WM
JH

MAY 12, 1960

81

11.7	11.9	68.0	66.7	69.4	69.6	69.6	69.2	68.2	68.3	12.4
13.5	13.3	17.2	16.5	15.8	15.6	15.6	16.0	17.0	16.9	12.8
63	45	34	26	17		4	11	15	22	30

Rt

Lt

12.6 12.2

12.7 13.0

82 100

13.8 65.0 67.0 70.0 11.8

21.4 20.2 18.2 15.2 13.4

100 87 69 51 37

15.6	10.1	10.2	11.6	11.7	11.6	11.2	10.4	10.5	11.6
9.6	15.1	15.0	13.7	13.5	13.6	14.0	14.8	14.7	7.6
35	22	16	12	5		16	27	34	49

Lt

Rt

15.4 13.4 11.7 69.5

9.8 11.8 13.5 15.7

41 62 83 100

11.1 11.6 11.4 11.1

8.1 7.6 7.8 8.1

100 84 74 56

12.2	11.6	13.1	13.1	13.0	12.6	12.2	11.7	12.0
13.0	13.7	12.1	12.1	12.2	12.6	13.0	13.5	13.2
24	17	13	4		16	23	26	35

Lt

Rt

15.1 16.2 11.6 15.3 13.1

10.1 7.0 7.6 9.9 12.1

30 40 56 70 94

11.9 11.5 11.0 10.0

6.3 5.7 6.2 5.2

100 80 58 49

12.6

12.6

100

STA

+

π

-

ELO

985.24

73+00

✓

+30

✓

TP

12.61

991.48

6.37

978.87

73 +60

981.43

✓

FK
RG
JS
JL
WM
JH

Lt

E

MAY 12, 1960

82

Rt

11.4	14.1	13.6	15.6	15.7	15.6	15.2	14.9	14.2	14.6	81.7
7.3	11.1	11.6	9.7	9.5	9.6	10.0	10.3	11.0	10.7	3.5
32	21	16	11	4		16	22	25	33	47

14.1	80.2	10.7	18.4	17.1
6.1	50	6.5	6.8	8.1
37	55	72	88	100

81.6	81.6	81.2
3.6	3.6	4.0
100	84	69

80.2	14.0	15.8	15.6	11.1	11.4	11.3	11.0	16.7	15.7	16.6	80.5
5.0	6.2	9.4	9.6	8.1	7.8	7.9	8.2	8.5	9.5	8.6	4.7
37	30	21	16	12	6		15	21	25	33	40

80.9	81.2	80.2	80.3	80.0
4.3	4.0	5.0	4.9	5.2
48	64	68	86	100

84.0	83.4	83.5	83.8
1.2	1.3	1.7	1.4
100	87	68	47

73+75 BLACKTOP ON 15' Lt.

80.3	11.7	11.4	18.2	14.1	19.0	18.8	18.4	17.8	19.0
11.2	13.8	14.1	12.7	12.4	12.5	12.7	13.1	13.7	12.5
29	22	18	13	7		14	20	24	32

81.2	82.2	83.7	83.3	83.2
10.3	9.3	7.8	8.2	8.3
36	55	69	81	100

89.6	87.8	87.1	87.5
3.9	3.7	3.8	4.0
100	85	68	49

STA

+

π

-

ELU

991.48

73+80

✓

74+00

✓

+41

✓

FK
RG
JS
JC
JH

Lt

Q

MAY 12, 1960

Rt

83

81.1	18.7	18.3	19.6	80.0	80.0	19.7	19.5	19.0	19.8
10.4	12.8	13.2	11.9	11.5	11.5	11.8	12.0	12.5	11.7
29	22	17	13	8		15	22	25	32

82.2	82.5	85.7	86.3	86.4	85.5	88.9	89.0	89.0	84.1
9.3	8.9	5.8	5.2	5.1	6.0	2.6	2.5	2.5	7.4
35	52	60	81	90	100	100	73	51	39

91.0	19.7	19.3	80.5	81.0	81.0	80.6	80.4	19.8	80.4
9.5	11.8	12.2	11.0	10.5	10.5	10.9	11.1	11.7	11.1
28	22	17	11	5		15	20	23	32

83.2	84.0	85.2	88.9	88.9	88.2	88.8	88.8	88.1	87.9
8.3	7.5	6.3	2.6	2.6	3.3	2.7	2.7	3.4	3.6
35	48	59	72	92	100	100	79	62	46

81.6	81.9	81.1	82.3	82.6	82.7	82.4	81.9	82.1	82.6	84.4
8.0	10.1	10.4	9.2	8.9	8.8	9.1	9.6	9.4	8.9	3.1
30	24	16	11	6		14	23	29	32	48

84.9	86.1	84.2	88.4	88.9	88.6	88.1	88.8
6.6	5.4	4.3	3.1	2.6	2.9	2.8	2.7
38	54	72	85	100	100	83	67

STA

+

π

-

ELV.

991.48

74+69

✓

75+00

✓

+2.5

✓

MAY 12, 1960

84

PG
SS
JC
JH

Lt

Z

Rt

86.1	85.3	85.4	85.0	85.6	85.1	85.4	85.0	85.4	85.1	85.9
4.8	6.2	7.7	8.5	9.9	7.8	8.1	8.5	9.1	8.8	3.6
50	34	23	15	7		14	20	24	30	46

87.9
3.6
74

88.8
2.7
100

88.0 88.2 87.9
3.5 3.3 3.6
100 74 60



87.4	86.5	84.1	84.0	84.3	84.3	84.1	84.1	82.4	85.4	86.9
4.1	5.0	6.8	7.5	7.2	7.2	7.4	7.4	9.1	6.1	4.6
61	45	27	16	7		13	19	25	39	49

87.9 88.5
3.6 3.0
76 100

86.2 86.4 86.5
5.3 5.1 5.0
100 84 67



86.2	85.4	84.2	83.1	84.6	84.6	84.4	83.9	82.7	83.7	85.4
5.3	6.1	7.3	7.8	6.9	6.9	7.1	7.7	8.8	7.8	6.1
41	29	25	16	8		12	22	25	29	43

87.2 87.8 88.5
4.3 3.7 3.0
62 78 100

85.0 85.3 85.8
6.5 6.2 5.7
100 78 61



STA

+

π

-

ELV

991.48

75+33

✓

+46

✓

+47 Gutter Line

✓

BM

4.89 986.59

FK
RG
JS

Lt

Q

MAY 12, 1960 85
Rt

SL

84.8	85.4	84.1	83.8	84.6	84.7	84.5	83.7	84.2	84.9
4.7	6.1	7.4	7.7	6.9	6.8	7.0	7.8	7.3	6.6
54	29	25	19	8		13	23	36	58

84.5 84.8
✓ 4.0 3.7
80 100

✓

84.2 84.4
7.3 7.1
100 78

85.5	84.0	83.6	84.2	84.8	84.8	84.6	84.0	84.0	84.6
6.0	7.5	7.9	7.3	6.7	6.7	6.9	7.5	7.5	6.9
29	25	18	15	8		13	25	36	53

86.8 84.4 84.6
4.7 4.1 3.9
58 81 100

✓

83.6 84.4
7.9 7.1
100 76

Dup. + 46

84.8	84.7	84.0	83.9	83.6
6.7	6.8	7.5	7.6	7.9
	13	25	36	58

✓

82.1 83.2
8.8 8.3
100 77

HYDRANT 30' Rt 75+45 TOP

STA

+

π

-

ELV.

991.48

75+65 $\pm$ Inca Lane

✓

+79 Gutter Line

✓

+80

FK
RG
JS
JL
JH

Lt.

Q

MAY 12, 1960

Rt.

86

84.5	83.5	83.5	84.4	84.8	84.9	84.8	84.2	84.1	83.7	83.3
7.0	8.0	8.0	7.1	6.7	6.6	6.7	7.3	7.4	7.8	8.2
27	23	19	14	7		13	27	46	74	100

85.5 86.2 86.7 87.0

6.0 5.3 4.8 4.5
31 42 79 100

✓

91.3 92.0 92.6
10.2 9.5 8.9
200 162 128

86.2	84.4	83.9	83.9	84.7	84.9	85.0	84.9	84.3	83.6	83.1
5.3	7.1	7.7	7.7	6.8	6.6	6.5	6.6	7.2	7.9	8.4
50	28	22	19	15	7		12	31	54	79

86.4 86.7
5.1 4.8
72 100

✓

82.9
8.6
100

Dup + 79

85.0	84.9	84.1	84.4	83.9
6.5	6.6	7.4	7.1	7.6
	12	37	52	79

✓

83.4
8.1
100

STA

+

 π

-

ELO

991.48

75+95

✓

1.78

988.37

4.89

986.59

76+00

+25

✓

+64

✓

FK
RG
JS
JL
JH

Lt

E

MAY 12, 1960

Rt

87

85.5	83.8	83.8	84.5	85.1	85.1	84.8	84.1	83.1	83.1
6.0	7.7	7.7	7.0	6.4	6.4	6.7	7.4	8.4	8.4
31	26	21	19	7		13	22	24	28

86.4	86.3	86.4	86.2	86.4	84.4	84.1	84.8	85.0	84.5
5.1	5.2	5.1	5.3	5.1	7.1	6.8	6.7	6.5	7.0
51	71	82	94	100	100	80	58	40	33

HYDRANT TOP 30' RT 75+45

85.1
3.3
PROFILE

83.8	83.1	83.1	84.9	85.1	85.1	84.9	84.4	83.6	84.3	85.4	85.7
4.6	5.3	5.3	3.5	3.3	3.3	3.5	4.0	4.8	4.1	3.0	2.7
26	23	21	15	8		12	19	25	31	38	59

85.4	85.6	85.3	84.9	84.5	84.3
3.0	2.8	3.1	3.5	3.9	4.1
30	41	57	73	88	100

85.7
HOUSE 2.7
64

83.6	82.9	82.8	84.7	84.9	85.0	84.9	84.8	83.4	83.4	85.2
4.8	5.6	5.6	3.7	3.5	3.4	3.5	3.6	5.0	5.0	3.2
27	22	21	14	7		12	17	24	27	36

83.8	84.1	84.0	83.2	82.3
4.6	4.3	4.4	5.2	6.1
31	47	62	80	100

85.1
85.4
3.3
3.0
75
55

STA

+

π

-

ELV.

988.37

77+00

✓

TBM

3.17

988.10

3.44

984.93

77+45

✓

+50. Dupl Rt.

✓

FX
RG
JS

Lt

Q

MAY 12, 1960

RE

88

JL
JH

82.4	82.7	82.1	84.0	84.6	84.7	84.6	83.9	82.9	82.9	84.1
60	5.7	6.3	4.4	3.9	3.7	3.8	4.5	5.5	5.5	4.3
31	27	22	14	9		12	17	22	26	33

82.9 82.0 81.3 81.2

5.5 6.4 7.1 7.2
44 60 82 100

84.6 84.5

3.8 3.9
75 51

79+05 TOP OF HYD. 30' RE

81.2	82.8	81.9	83.1	83.4	84.6	84.0	83.5	82.7	82.7	83.2
6.9	5.3	6.2	5.0	4.2	3.5	4.1	4.6	5.4	5.4	4.9
33	26	22	16	9		13	18	23	28	35

81.6 81.2 80.9

6.5 6.9 7.2
53 75 100

83.2 83.4

4.9 4.7
75 58

82.1 83.0 82.14 83.9 84.1

6.0 5.1 5.96 4.3 4.0

51 25 21 11

Top 15" CM

82.3

5.8
100

Sta + π - Elev

988.10

78+00

✓

+44 Berm

+47 Gutter

+57 $\angle$ 5th St N.W

✓

26
JL
WM
JH

May 23, 1960
Warm 90° Clear 89

83.1	82.6	81.6	83.2	83.7	83.5	82.3	82.3	83.2	83.5
5.0	5.5	6.5	4.9	4.4	4.6	5.8	5.8	4.9	4.6
56	31	22	13		11	20	25	36	58

83.5
4.6
78

83.3
4.8
100

83.6
4.5
75

✓

83.4	83.3	83.0	83.5	83.2	83.1	83.8
4.7	4.8	5.1	4.6	4.9	4.4	4.3
14	27	28	45	72	100	

✓

83.4	83.2	83.0	83.0	83.0
4.7	4.9	5.1	5.1	5.1
14	30	62	100	

81.7	81.4	81.1	82.9	83.4	83.1	82.8	82.8	82.9	83.0
8.4	6.7	7.0	5.2	4.7	5.0	5.3	5.3	5.2	5.1
53	37	25	17		18	53	100	150	200

80.0
8.1
78

81.7
8.4
100

✓

Sta + π - Elev

988.10

78 + 74 Gutter

+76 Berm

79 + 00

✓

+50

✓

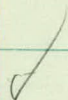
May 23, 1960

Lt

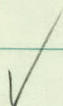
E

Rt

90



83.3	83.0	82.1	82.1	82.1	82.2
4.8	5.1	6.0	6.0	6.0	5.9
	16	33	55	81	100



83.3	83.0	82.1	82.6	82.5	82.6
4.8	5.1	6.0	5.5	5.6	5.5
	16	32	45	76	100

78.3	78.3	78.6	79.0	82.6	83.2	82.8	81.3	81.4	82.6
9.8	9.8	9.5	9.1	5.5	4.9	5.3	6.8	6.4	5.5
100	85	56	30	16		15	22-24	28	50

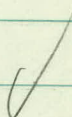


44.3	43.2
3.8	4.9
40.	75

78.4	79.3	80.0	82.4	82.4	82.3	74.28	80.0	82.6
9.7	8.8	8.08	5.7	5.2	5.8	8.82	8.1	5.5
51	28	22.8	15		15	26	23	41

TOP 15" SCP FK 18" SCP

78.8
→ 10.3
75



83.1	83.0
5.0	5.1
75	68

Sta	+	π	-	Elev
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		988.10		
--	--	--------	--	--

+92				
-----	--	--	--	--

✓				
---	--	--	--	--

80+00				
-------	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

+96				
-----	--	--	--	--

T.P	6.38	991.13	3.35	984.75
-----	------	--------	------	--------

May 23, 1960

91

L+

E

R+

18.5	18.6	19.3	82.4	83.0	82.7	80.7	80.7	81.3	83.3
9.6	9.5	8.8	5.7	5.1	5.4	7.4	7.4	6.8	4.8
76	47	29	16		15	23	29	34	58

✓

83.9

4.2

75

16.3	18.6	18.1	19.3	82.4	83.0	82.8	80.9	80.7	83.0	86.2	87.1
9.8	9.5	9.4	8.8	5.7	5.1	5.3	7.2	7.4	5.1	1.9	1.0
100	78	44	30	17		15	21	27	38	72	100

✓

19.1	19.4	19.5	80.3	82.7	83.1	82.7	81.3	81.1	83.1	84.6
9.0	8.7	8.6	7.8	5.4	5.0	5.4	6.8	7.0	5.0	3.5
100	78	44	30	19		13	19	28	36	48

✓

87.94

86.9

0.16

1.2

140 SW

75

80.4	81.0	81.5	81.4	82.9	83.3	83.0	81.8	81.9	82.7	85.9	86.1
7.7	7.1	6.6	6.7	5.2	4.8	5.1	6.3	6.2	4.4	2.2	1.4
100	72	37	28	18		15	24	28	34	62	75

✓

Top iron Lot corner 30' ± RT Sta 81+00

STA.

+

⌒

—

ELV.

58.5

~~6.38~~

991.13

81+00

✓

+08

✓

+50

✓

RG
JC
WM
JH

Lt

L

MAY 24, 1960

Rt.

92

81.2	81.6	81.1	82.9	83.3	83.0	81.4	83.0	85.9	82.7
7.9	9.5	10.0	8.2	7.8	8.1	9.7	8.1	5.2	3.9
83	61	31	18		15	23	30	56	75

80.6
10.5
100

✓

	83.4	83.1	81.5	83.4	85.5
Dup. 81+00 Lt	7.7	8.0	9.6	7.7	5.6
		13	24	31	50

✓

88.0
3.1
75

82.5	81.5	81.2	83.2	83.1	83.3	82.5	82.5	85.0	86.6
8.6	9.6	9.9	7.9	7.4	7.8	8.6	8.6	6.1	4.5
76	49	28	15		13	19	27	36	50

82.7
8.4
100

✓

90.1
1.0
HOUSE
88.6
2.5
75

STA

+

X

-

ELV.

991.13

81+73

✓

+80

✓

82+00

✓

RG
JL
WM
JH

Lt

C

Rt

93

MAY 24, 1960

82.1	81.8	81.1	83.2	84.0	83.4	82.9	83.3	85.0
8.4	9.3	10.0	7.9	7.1	7.7	8.2	7.8	6.1
78	51	29	17		16	21	29	36

82.6
8.3
100

✓

88.8 87.1
2.3 4.0
75 53

83.5	82.1	81.2	83.4	84.0		
7.6	7.0	9.9	7.7	7.1	Dup	81 + 73 Rt.
80	48	30	17			

83.6
7.5
100

✓

82.5	81.6	81.7	83.6	84.3	83.8	83.0	84.7	86.8
8.6	9.5	9.4	7.5	6.8	7.3	8.1	6.4	4.3
52	34	26	16		16	21	34	55

82.8 82.6
8.3 8.5
77 100

✓

87.8
3.3
75

STA

+

⌊

-

ELV.

991.13

2+50

✓

834.00

✓

T.P.

5.40

993.63

2.90

988.23

+50

✓

RG

LT

Q

May 25, 1960
Rt

94

83.5	83.5	83.9	84.1	85.0	84.6	83.9	84.5	84.6
7.6	7.6	7.2	6.4	6.1	6.5	7.2	6.6	4.5 =
75	49	26	16		14	23	29.	48

83.1
7.4
100

90.9 88.1
0.2 2.4
HOUSE 75

84.8	84.8	84.8	85.2	85.6	85.4	85.76	84.6	85.4	86.7
6.3	6.3	6.3	5.9	5.5	5.7	5.37	6.6	5.7	4.4
62	42	25	16		13	23 TCM	23	25	45

84.6
6.6
100

88.4 87.7
2.7 3.4
75 65

LIGHT POST SW CORNER OF SOUTH LIGHT 569 HOUSE NO.

85.1	85.6	85.3	85.1	86.3	86.0	85.3	85.3	86.6	87.6
8.5	8.0	8.3	7.9	7.3	7.6	8.3	8.3	7.1	6.0
36	24	19	15		17	22	26	31	45

85.0 85.1 85.4
8.6 8.5 8.2
53 84 100

91.7 90.0 89.1
1.9 3.6 4.5
109 75 63
HO

Sta + π - Elev

99363

84 +00

✓

+50

✓

85

FK
JS
JL
WM
JH

May 25, 1960

Lt

Rt

95

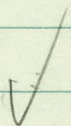
84.2	83.9	84.1	86.5	87.2	86.9	86.1	88.1	87.8	88.1	89.9
94	97	89	71	64	67	75	58	49	37	
54	41	25	16		15	23	36	55	75	

84.0	84.1	85.3
9.6	8.9	8.3
72	89	100



82.4	82.9	86.1	87.3	87.9	87.8	86.9	86.8	87.5	88.5
11.2	10.7	6.9	6.3	5.7	5.8	6.7	6.8	6.1	5.1
43	29	20	17		16	23	26	33	38

82.4	82.1	83.3
11.2	10.9	10.3
65	81	100



84.4	88.6	87.9	88.3
5.2	5.0	5.7	5.3
75	72	54	47

84.0	85.4	85.6	87.9	88.6	88.2	87.2	87.0	88.8	88.5
9.6	8.2	8.0	5.7	5.0	5.4	6.4	6.6	4.8	5.1
29	26	23	18		18	23	34	39	56



83.5	82.8	82.2	81.4
10.1	10.8	11.4	12.2
36	57	75	100

88.8	88.0
48	56
84	64

Sta + π - Elev

993.63

85+22

✓

BM

4.6698897

+69

✓

86

✓

Lt.

L

May 25, 1960

RT

96

82.9	84.0	85.4	86.1	88.3	88.9	88.6	87.3	87.1	87.8	89.3
10.7	9.6	8.2	7.9	5.3	4.7	5.0	6.3	6.5	5.8	4.3
36	31	27	24	17		17	20	25	32	37

82.6	81.9	81.6		88.7	88.4	88.9
11.0	11.7	12.0		4.9	5.2	4.7
54	80	100		75	66	48

Top Hyd Rt sk 85+10

85.4	84.8	85.5	89.2	89.6	89.2	88.7	87.9	88.2	89.3
8.2	8.8	8.1	4.4	4.0	4.4	4.9	5.7	5.4	4.3
46	37	28	16		16	19	22	25	29

84.4	83.4	82.0		89.9	90.1	89.9
9.2	10.2	11.6		3.7	3.5	3.7
60	82	100		75	61	46

86.1	85.3	85.6	89.5	90.1	89.5	88.9	89.9	90.1
8.5	8.3	8.0	4.1	3.5	4.1	4.7	3.7	3.5
49	37	30	16		19	23	29	36

83.1	82.8	82.6		90.1	90.5	90.4
9.9	10.8	11.0		3.5	3.1	3.2
65	90	100		40	75	56

Sta + π - Elev.

993.63

86+31

✓

+ 50

✓

+ 80

✓

May 25, 1960

97

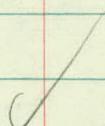
LT

ST

85.3	86.6	86.8	89.9	90.6	90.1	89.1	89.4	90.3	90.6
8.3	7.0	6.8	3.7	3.0	3.5	4.5	4.2	3.3	3.0
55	40	29	17		19	24	26	31	30

84.1	83.8
9.5	9.8
80	100

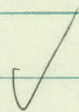
90.4	90.6
3.2	3.0
75	55



86.9	87.1	89.1	90.3	90.9	90.4	89.6	90.5	90.6
6.7	6.5	4.5	3.3	2.7	3.2	4.0	3.1	3.0
51	40	29	17		18	24	31	52

85.3	84.7	84.7
8.3	8.9	8.9
66	81	100

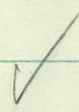
90.4	90.8
3.2	2.8
75	68



89.1	89.6	90.9	90.2	90.8	91.3	90.1	90.0	89.9	90.3	90.0
4.5	4.0	2.8	3.4	2.8	2.3	2.9	3.6	3.7	3.3	3.6
39	35	26	20	17		19	22	26	28	49

88.4	87.0	85.7	85.9	86.0
5.2	4.6	7.9	7.7	7.6
50	56	78	93	100

90.1	90.1
3.5	3.5
75	63



Sta + π - Elev.

993.63

87

✓

TP 7.41 997.59 3.45 990.18

+50

✓

88

✓

Lt

May 25, 1960 98
 Rt

89.4	90.5	91.4	90.6	91.1	91.6	91.0	90.2	90.2	94.6	98.6
42	31	22	30	25	20	26	34	32	40	50
50	36	27	20	16		18	24	29	50	75

88.1	96.1	96.5	96.3
5.5	6.9	7.1	7.3
56	78	93	100

NE Ent Culvert

92.0	91.8	91.4	91.9	92.4	91.8	91.1	91.1	92.3
56	58	62	5.7	5.2	5.8	6.5	6.5	5.3
35	28	21	14		18	21	24	32

91.3	88.1	86.1
6.3	9.5	12.5
48	73	100

91.2	91.8
6.4	5.8
75	56

92.6	93.1	91.9	92.5	92.9	92.3	91.4	92.3	92.2	92.2
50	45	57	5.1	4.7	5.3	6.2	5.3	5.4	5.4
39	28	20	13		17	23	31	57	75

90.5	87.8	84.2
7.1	9.8	13.4
57	75	100

92.4
5.2
Ho

Sta + π - Elev.

997.59

88 + 50

✓

89

✓

TP 5.04 996.89 5.74 991.85

+ 41

✓

May 25, 1960

99

LT

RT

q2.6	q2.6	q2.1	q2.1	q3.3	q2.5	q1.7	q2.3	q1.5
5.1	5.1	5.5	4.9	4.3	5.1	5.9	5.3	6.1
45	29	20	14		17	22	25	35

q0.1	q6.9	q3.6
2.5	10.7	14.0
69	83	100

q0.6	q1.0
7.0	6.6
75	57

q1.6	q3.1	q2.9	q2.3	q3.0	q3.3	q2.8	q1.9	q2.2	q1.4	q0.1
6.0	4.5	4.7	5.3	4.6	4.3	4.8	5.7	5.4	6.2	6.9
62	47	30	19	13		15	23	27	33	54

q8.6	q2.8
9.0	14.8
77	100

q9.56	q1.9
8.04	7.7
Wakat	75

Top Water shut off RT Sta 89+10

q4.3	q4.4	q2.1	q2.7	q3.2	q2.5	q2.2	q2.1	q1.8
2.6	2.5	4.8	4.2	3.7	4.4	4.7	4.2	5.1
46	30	20	15		16	21	27	35

q3.3	q9.9	q6.2	q4.6
3.6	7.0	10.7	12.3
58	76	92	100

q0.1	q1.0
6.8	5.9
75	55

STA

+

Σ

-

ELV.

996.89

89+81

✓

90+00

✓

+37

✓

T.P.

11.84

1003.61

5.12

991.77

MAY 25, 1960

100

Lt

E

Rt

q3.1	q2.6	q1.8	q2.5	q2.0	q2.2	q1.7	q2.3	q1.3
3.8	4.3	5.1	4.4	3.9	4.7	5.2	4.6	5.6
37	27	20	15		18	23	27	35

q3.6	q3.1	88.8
3.3	3.8	8.1
49	72	100

89.3	90.0
7.6	6.9
75	65

q3.6	q3.0	q1.6	q2.6	q2.4	q2.0	q1.6	q1.9	q0.4
3.3	3.9	5.3	4.3	4.0	4.9	5.3	5.0	6.0
38	28	20	13		17	22	28	35

q4.3	q4.1	q2.8
2.6	2.8	7.1
59	85	100

88.3	89.5
8.6	7.4
75	59

q2.7	q1.8	q1.2	q1.4	89.5
4.2	5.1	5.7	5.5	7.4
	18	24	28	34

85.9	87.7
11.0	
75	9.2
75	53

90+50 25' Rt. MAIL BOX FOOTING

STA

+

△

-

ELV₁

1003.61

37
90 + ~~68~~

✓

+68

✓

91+00

✓

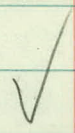
Lt

E

Rt

⁶
¹
^x
 95.6 93.9 92.4 92.7
 80 10.0 11.5 11.2
 49 29 19 13

⁰
⁰
⁶
 98.3 98.3 97.8
 5.6 5.6 6.1
 78 93 100



⁰
¹
⁰
¹
⁶
^{91.9}
 96.3 94.4 92.3 92.4 92.8 92.1
 7.6 9.5 11.6 11.5 11.1 11.7
 31 27 20 14 16

⁶
⁴
 91.9 91.7
 12.0 12.2
 31 54

^{97.8}
⁴
^{1000.0}
^{1000.0}
 98.1 99.7
 5.8 4.2 3.2 3.6
 49 67 80 100

^{91.8}
^{91.5}
 12.1 12.4
 GARGE FLOOR 75



99.6 95.2 92.0 91.9 92.3 91.4 90.8 91.0 90.8
 4.0 8.4 11.6 11.7 11.3 12.2 12.8 12.6 12.8
 37 28 20 15 17 22 30 40

^{1000.1}
^{1000.8}
^{1001.1}
^{1001.8}
^{1001.8}
 3.5 2.8 2.5 1.8 1.8
 46 52 60 72 84

^{90.5}
^{90.7}
^{90.3}
 13.1 13.4 13.5
 HOUSE 75 64



^{1000.9}
 2.7
 100

STA

+

π

-

ELV.

1003.61

91+15

✓

+36

✓

+48

✓

MAY 25, 1960

102

Lt

E

Rt

01.4	1000.6	92.6	91.1	92.1	91.5	90.7	90.7	90.3
2.2	3.0	11.0	11.9	11.5	12.1	12.9	12.9	13.3
50	37	23	16		15	22	34	52

02.0	01.4	01.4
1.6	2.2	2.2
79	96	100

90.4
13.2
75

94.9	93.1	91.6	91.6	91.8	91.2	90.5	90.4	90.3
8.7	10.5	12.0	12.0	11.8	12.4	13.1	13.2	13.3
33	26	20	15		17	26	35	50

94.6	95.1	95.9	96.2
9.2	7.9	7.7	7.7
42	63	84	100

90.0
13.6
75

93.6	91.9	91.4	91.6	91.6	91.0	90.2	90.4	90.2
10.0	11.7	12.2	12.0	12.0	12.6	13.4	13.2	13.4
36	30	20	15		18	25	29	39

94.9	95.4	95.6
8.7	8.2	8.0
55	72	100

90.8	90.1
13.8	13.5
75	60

STA

+

Δ

-

ELV.

1003.61

91+55

✓

+ 67

✓

✓

~~78~~

Lt E Rt

q2.3	q1.4	q1.6	q1.5	q1.1	q0.1	q0.3	q9.4
11.3	12.2	12.0	12.1	12.5	13.5	13.3	13.7
44	23	16		16	23	30	51

↓ q3.2 q4.4 q4.6

10.4	9.2	9.0
69	94	100

✓

89.8
13.8
75

↙

q2.2	q1.2	q1.5	q1.4	q1.2	q0.0	q0.1
11.4	12.4	12.1	12.2	12.4	13.6	13.5
42	22	17		13	25	31

q3.8 q4.8 q5.1 q5.8

9.8	8.8	8.5	7.8
67	90	100	150

✓

89.7	89.6
13.9	14.0
75	55

↙

q4.0

9.6
200

q3.1	q2.0	q0.9	q1.4	q1.2	q1.1	q0.1	q9.9	q9.9
10.5	11.6	12.7	12.2	12.4	12.5	13.5	13.7	13.7
77	45	22	12		11	24	31	36

q4.1

9.5
100

✓

88.8	84.3
14.8	14.3
75	55

STA

+

Δ

-

ELV

1003.61

91+86

✓

92+00

✓

T.P.

4.67

994.77

13.51

990.10

92+14

✓

MAY 25, 1960

104

LT

ⓔ

Rt

95.0	94.1	90.4	91.2	91.2	91.0	90.0	89.4	89.0
8.6	9.5	12.7	12.4	12.4	12.6	13.6	14.2	14.6
55	34	21	15		11	26	43	63

95.5
8.1
81

96.6
7.2
100

✓

88.1
15.5
75

96.1	95.8	90.7	91.0	91.0	90.8	90.2	90.0	86.1
6.9	9.8	12.9	12.6	12.6	12.8	13.4	13.6	14.9
55	31	18	14		13	22	32	53

96.5
5.1
82

99.6
4.0
100

✓

86.5
17.1
75

92+65 Hydrant 50' Rt TOP

93.8	90.7	90.4	90.8	90.8	90.6	89.4	88.4	85.9
1.0	4.1	4.4	4.0	4.0	4.2	5.4	6.4	8.9
32	21	17	12		15	33	45	67

✓

85.1
9.7
75

FENCE

STA

+

K

—

ELV

994.77

92+31

✓

T.P. 0.74 990.84 4.67 990.10

92+51

990.84

✓

+60

✓

Lt

L

Rt.

MAY 25, 1960

105

90.3	90.0	90.5	90.4	90.2	89.8	89.1	89.2
4.5	4.8	4.3	4.4	4.6	5.5	7.7	10.6
21	16	11		14	33	56	85

91.5

93.6

3.3

1.2

26

32

FENCE

91.8

82.6

17.0

12.2

150

100

92+65 HYDRANT 50' RT TOP 7TH ST.

90.7	89.5	89.6	89.9	89.8	89.6	89.0	89.4	85.3
0.1	1.3	1.2	0.9	1.0	1.2	1.8	3.4	5.5
25	22	17	11		14	29	38	70

90.2	89.2	89.4	89.7	89.5	89.4	89.1	88.3	87.1
0.6	1.6	1.4	1.1	1.3	1.4	2.1	2.5	3.7
26	23	20	11		14	29	40	55

85.2

5.6

75

STA

+

π

-

ELV.

990.84

93+00

✓

+50

✓

94+00

✓

MAY 31, 1960

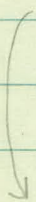
106

Lt

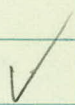
L

Rt

81.5	88.1	88.3	88.3	88.1	89.2	86.4	85.3
3.3	2.7	2.5	2.5	2.7	3.6	4.4	5.5
22	19	11		12	22	40	58



89.3	90.2
1.5	0.6
31	33



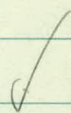
84.2	84.4
6.6	6.4
75	69



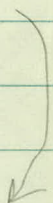
84.9	85.9	86.3	86.3	86.0	84.8	83.8	80.1
5.9	4.9	4.5	4.5	4.8	6.0	7.0	10.1
24	18	11		12	28	36	55



86.1
7.1
33



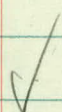
11.3
11.5
75



81.5	82.4	82.9	83.3	83.4	83.2	82.9	19.9	18.4
9.3	8.2	7.9	7.5	7.4	7.6	7.9	11.9	12.4
26	21	18	10		11	18	32	47



82.1	82.2
8.7	8.5
28	34



11.1	18.0	18.2
13.1	12.8	12.6
HOUSE	75	68



STA

+

K

-

ELV.

990.84

94+34

✓

46
+ ~~42~~

✓

T.P.

5.24

985.71

10.37

980.47

94+85

✓

MAY 31, 1960

Lt

E

Rt

107

19.0	19.1	81.5	81.8	81.6	81.3	80.0	78.1	77.4
11.8	11.7	9.3	9.0	9.2	9.5	10.8	12.1	13.4
38	25	19	11		12	21	25	32

82.3	82.5	81.9	90.7
8.5	7.2	2.9	0.1
56	66	85	100

77.1
13.7
75

18.6	19.1	81.0	81.2	81.1	80.8	80.1	78.4	77.1
12.2	12.7	9.8	9.6	9.7	10.0	10.7	12.4	13.7
39	25	18	11	10.4	12	19	24	32

81.6	81.2	85.6	84.0
9.2	6.6	5.2	3.8
57	67	81	100

76.6
14.2
75

Rock 35' Lt STA 44+50

77.7	76.2	79.1	79.7	79.6	79.3	77.6	75.3	75.8
8.0	9.5	6.6	6.0	6.1	6.4	8.1	10.4	9.9
40	23	15	9		13	29	33	37

80.5	84.1	86.2
5.2	1.6	0.5
52	76	92

72.0	73.6	75.3
13.7	12.1	10.4
75	66	47

STA

+

Σ

-

ELV.

985.71

95+00

✓

✓

+11

✓

✓

T.P. +13

9.95

975.76

MAY 31, 1960

108

Lt

E

Rt

15.1	11.1	18.4	17.1	19.0	18.7	17.4	16.3	14.5
10.0	8.6	7.3	6.6	6.7	7.0	8.3	9.4	11.2
29	22	15	10		13	24	29	32

16.5	17.0	18.0	80.6	81.6
9.2	8.7	7.7	5.1	4.1
32	41	44	49	58

12.0	13.9	15.7
13.7	11.9	10.0
75	57	38

85.1	84.4	83.4
0.6	1.3	2.3
100	85	65

14.9	15.6	16.6	18.1	18.7	18.6	18.4	17.3	15.7	15.6
10.8	10.1	9.1	7.6	7.0	7.1	7.3	8.4	10.0	10.1
29	27	22	18	10		12	22	25	27

15.1	16.3	81.0	82.5
10.0	9.4	4.7	3.2
32	39	50	66

11.1	12.0	12.3	13.5
14.1	13.7	12.4	12.2
75	64	43	34

83.1	83.2
2.0	2.5
100	83

9.95
±13
SKIM
MANHOLE

HOUSE

Silver Lake Rd

STA

+

⌋

-

ELV.

985.71

95+50

✓

✓

96+00

✓

MAY 31, 1960

Lt

E

Rt

109

13.8	15.1	11.2	11.1	11.5	11.3	15.4	12.1	12.2
11.9	10.6	8.5	8.0	8.2	8.4	9.8	13.1	13.5
33	27	16	9		12	21	34	48

13.8	15.1	18.1	10.3
11.9	10.0	7.0	5.4
36	45	57	64

✓

10.4	11.6
15.3	14.1
75	58

82.1	81.4
3.6	4.3
91	82

12.1	13.5	15.8	16.5	16.4	16.3	15.3	12.5	11.4
13.0	12.2	9.9	9.3	9.4	9.5	10.5	13.2	13.8
35	25	16	10		13	21	30	41

14.3	16.0	18.1	18.8
11.4	9.7	7.0	6.9
48	67	85	100

HOUSE

✓

11.0	11.4	12.2
14.7	14.3	13.5
75	61	54

STA

+

T

-

ELV

985.71

96+50

✓

✓

TR +85

12.08

973.63

97+00

✓

MAY 31, 1960

Lt

E

Pt.

110

✓ 12.7	✓ 13.2	✓ 14.9	✓ 15.4	✓ 15.3	✓ 15.0	✓ 14.6	✓ 13.7
13.0	12.5	10.8	10.3	10.4	10.7	11.2	12.0
35	23	14	8		14	23	28

✓ 15.1	✓ 16.5	✓ 17.7	✓ 17.9	✓ 13.7	✓ 14.5	✓ 15.6	✓ 14.5
10.6	9.3	8.0	7.8	12.0	11.2	10.1	11.2
52	70	87	100	70	58	45	37

18.9
6.8
HOUSE
13.8
11.9
75

MANHOLE^S Rm 96 + B5 Lt

✓ 13.3	✓ 12.5	✓ 13.4	✓ 14.4	✓ 14.5	✓ 14.3	✓ 14.2	✓ 13.1	✓ 14.5
12.4	13.2	12.3	11.3	11.2	11.4	11.5	12.6	11.3
42	27	19	9		14	22	28	38

✓ 14.8	✓ 15.9	✓ 16.5
10.9	9.8	9.3
61	81	100

✓

✓ 15.9
9.8
75

STA

+

K

-

ELV.

985.71

97+31

✓.

T.P.

2.32

978.52

9.51

976.20

97+50

978.52

✓

+75

✓

MAY 31, 1960

111

Lt

E

Rt

✓
13.7✓
11.8✓
12.5✓
13.6✓
13.7✓
13.4✓
13.0✓
11.6

12.0

13.9

13.2

12.1

12.0

12.3

12.7

14.1

~~14.1~~

51

29

19

9

14

23

29

✓
15.3✓
15.6✓
15.7✓
16.9

✓

✓
16.2✓
16.1✓
13.3✓
~~12.1~~

10.4

10.1

10.0

8.8

9.5

9.6

12.4

13.0

74

92

100

HOUSE

75

54

40

36

WATER SHUT OFF STA 97+31

✓
13.0✓
11.4✓
12.1✓
13.1✓
13.2✓
12.8✓
12.1✓
11.5✓
11.4

5.5

7.1

6.4

5.4

5.3

5.7

6.4

7.0

6.6

41

26

19

9

14

23

31

36

✓
14.3

15.4

✓
15.9

✓

✓
16.4✓
16.3

4.2

3.1

2.6

2.1

2.2

60

84

100

~~100~~

75

56

✓
13.0✓
11.8✓
11.0✓
12.5✓
12.5✓
12.2✓
11.7✓
10.9✓
13.8

5.5

6.7

7.5

6.0

6.0

6.3

6.8

7.6

4.7

46

37

23

9

13

22

31

43

✓
14.0✓
14.7✓
15.4

16.0

✓

✓
16.2✓
16.5

4.5

3.8

3.1

2.5

2.3

2.0

61

76

95

100

75

58

STA

+

π

-

ELV.

978.52

98+00

✓

+23

✓

+50

✓

MAY 31, 1960

112

Lt

E

Rt

✓ 11.8	✓ 10.6	✓ 11.9	✓ 11.9	✓ 11.1	✓ 11.2	✓ 10.4
6.7	7.9	6.6	6.6	6.8	7.3	8.1
42	24	10		13	20	31

✓ 12.6	✓ 12.6	✓ 12.4
5.9	5.9	6.1
60	79	100

✓ 16.6	✓ 16.7	✓ 13.5
1.9	1.8	5.0
75	58	44

✓ 10.7	✓ 10.1	✓ 10.6	✓ 11.3	✓ 11.4	✓ 11.1	✓ 10.7	✓ 10.0	✓ 10.7
7.8	8.4	7.9	7.2	7.1	7.4	7.8	8.5	7.8
35	25	18	9		14	20	28	36

✓ 11.4	✓ 11.8	✓ 11.9	✓ 12.1	✓ 11.1
7.1	6.7	6.6	6.4	6.8
40	55	74	90	100

✓ 11.4	✓ 16.4	✓ 11.1
1.1	2.1	4.4
75	57	47

✓ 11.0	✓ 10.9	✓ 10.0	✓ 10.6	✓ 10.1	✓ 10.4	✓ 10.1	✓ 10.2	✓ 10.7
7.5	8.6	8.5	7.9	7.8	8.1	8.8	9.3	7.8
42	33	19	9		10	22	29	37

✓ 11.1	✓ 11.1	✓ 11.2
7.4	7.4	7.3
66	83	100

✓ 16.3	✓ 15.2
2.2	3.8
75	58

STA

+

⌵

—

ELV.

978.52

78+80

✓

T.P.

9.17

969.35

78+94

✓

99+00

+¹⁸~~00~~

MAY 31, 1960

113

Lt

E

Rt

69.1	68.6	69.2	69.8	69.9	69.8	69.5	68.6	69.3
9.4	9.9	9.3	8.7	8.6	8.7	9.0	9.9	9.2
33	28	18	9		13	19	27	35

68.3	67.1	65.6	65.3		74.9	72.3
10.2	11.4	12.9	13.2		3.6	6.2
56	70	96	100		75	51

MANHATTAN SCIM STATION 98 + 99

68.2	69.4	69.0	69.5	69.6	69.3	69.0	69.3	69.9
10.3	9.1	9.5	9.0	8.9	9.2	9.5	10.2	8.6
50	32	17	10		13	20	28	38

66.6	66.1		74.3	72.4
11.9	12.4		4.2	6.1
80	100		75	54

69.4
9.1
PROFILE

69.2	68.4	67.9	69.1	69.1	68.9	68.3	67.4	69.3
9.3	10.1	10.6	9.4	9.4	9.6	10.2	11.1	9.2
47	31	19	9		13	29	25	34
68.9	68.1	67.1	66.3			73.6	72.1	71.5
9.6	10.4	11.4	12.2			4.9	6.4	7.0
58	72	89	100			75	60	48

STA

+

X

-

ELV.

978.52

99+29

✓

+70

✓

100+00

11/4 31, 1960

Lt

E

Rt

11/4

✓ 67.1	✓ 67.7	✓ 68.2	✓ 68.9	✓ 68.9	✓ 68.1	✓ 68.2	✓ 67.1	✓ 69.6
10.9	10.8	10.3	9.6	9.6	9.8	10.3	11.4	8.9
28	22	16	9		13	20	27	38

✓ 12.9	✓ 11.4	✓ 69.1	✓ 66.8		✓ 73.4	✓ 12.6	✓ 11.8
5.6	7.1	9.4	11.7		5.1	5.9	6.7
47	6.4	82	100		75	68	53

✓ 66.3	✓ 66.2	✓ 67.4	✓ 68.1	✓ 68.1	✓ 68.0	✓ 67.8	✓ 66.4
12.2	12.3	11.1	10.4	10.4	10.5	10.7	12.1
25	20	14	8		12	18	24

✓ 110.0	✓ 113.9	✓ 114.3	✓ 114.0	✓ 113.8	✓ 112.5	✓ 112.0	✓ 111.0	✓ 66.4
8.5	4.6	4.2	4.5	4.7	6.0	6.5	7.5	12.1
38	52	67	85	100	75	67	49	31

✓ 65.4	✓ 65.4	✓ 66.8	✓ 67.5	✓ 67.4	✓ 67.3	✓ 67.0	✓ 66.1	✓ 63.9
13.1	13.1	11.7	11.0	11.1	11.2	11.5	12.4	14.6
25	20	14	8		13	19	24	28

✓ 69.8	✓ 113.6	✓ 113.9	✓ 114.1	✓ 11.0	✓ 11.0	✓ 64.7	✓ 64.3	✓ 66.6	✓ 65.8
8.7	5.0	4.6	4.4	7.5	8.8	10.2	11.9	12.7	
40	53	62	75	75	54	40	34	30	

114.0
 4.5
 100

STA

+

K

-

ELV.

978.52

100+50

✓

✓

T.P.

7.10

976.12

9.50

969.02

101+00

976.12

✓

✓

MAY 31, 1960

115

Lt

R

Rt

✓ 64.1	✓ 65.6	✓ 66.3	✓ 66.3	✓ 66.1	✓ 66.0	✓ 64.8
14.4	12.9	12.2	12.2	12.4	12.5	13.7
21	15	9		14	19	24

✓ 64.2	✓ 10.8	✓ 14.8	✓ 14.9	✓ 64.3	✓ 10.0	✓ 64.8	✓ 64.8	✓ 64.6
14.3	7.7	3.7	3.6	9.2	8.5	8.7	10.7	13.9
25	47	64	75	66	61	57	45	31

✓ 13.6	✓ 14.1	✓ 64.9	✓ 10.1
4.9	3.8	8.6	8.4
100	88	71	75

MAIL BOX STAND 15' RE 99+90

✓ 63.4	✓ 63.0	✓ 64.6	✓ 65.0	✓ 65.1	✓ 64.9	✓ 64.7	✓ 63.2	✓ 63.5
12.7	13.1	11.5	11.1	11.0	11.2	11.4	12.9	12.6
27	21	14	9		14	21	27	32

✓ 69.4	✓ 14.8	✓ 13.9	✓ 12.2	✓ 69.1	✓ 68.4	✓ 64.0	✓ 68.4	✓ 66.4
6.4	1.3	2.2	3.9	7.0	7.7	7.1	7.4	9.7
47	67	80	100	71	67	63	55	41

✓ 68.9
7.2
75

STA + π - ELV

976.12

01+50

✓

✓

102+00

✓

✓

T.P. 5.65 972.20 9.57 966.55

Lt

Q

MAY 31, 1960

Rt

116

✓ 62.4	✓ 61.9	✓ 63.3	✓ 63.8	✓ 63.9	✓ 63.7	✓ 63.4	✓ 62.8
13.7	14.2	12.8	12.3	12.2	12.9	12.7	13.3
28	22	15	9		15	20	26

✓ 64.7	✓ 69.1	✓ 12.2	✓ 13.5	• 13.4	✓ 68.1	✓ 67.5	✓ 65.9	✓ 61.8
11.4	7.0	3.9	2.6	2.7	8.0	8.6	10.2	14.3
35	49	59	68	86	75	54	45	31

12.8
3.3
100

✓ 61.1	✓ 60.4	✓ 62.0	✓ 62.6	• 62.7	✓ 62.6	✓ 62.1	✓ 61.3	✓ 61.2
14.4	15.4	14.1	13.5	13.4	13.6	14.0	14.8	14.9
33	24	16	8		15	22	27	32

✓ 68.0	71.2	71.5	70.8
8.1	4.9	4.6	5.3
51	63	74	92

✓ 68.4	✓ 68.0	✓ 67.7	✓ 66.6	✓ 63.6
7.7	8.1	8.4	9.5	12.5
73	66	58	52	42

70.0
~~61.0~~
5.1
100

✓
68.4
7.7
75

TOP OF NEWSPAPER STAND POST STA. 101+85 12' Lt.

STA

+

X

-

ELV.

972.20

102+50

✓

103+00

✓

+ P.

1.20

961.58

11.82

960.38

103+50

961.58

✓

Lt

R

Rt

117

114 Y 31, 1960

✓ 58.8	✓ 59.2	✓ 60.6	✓ 61.5	✓ 61.5	✓ 61.4	✓ 61.0	✓ 59.8	✓ 59.8
13.4	13.0	11.6	10.7	10.7	10.8	11.2	12.4	12.4
43	24	17	8		14	20	26	34

✓ 59.7	✓ 65.1	✓ 68.6	✓ 69.6		✓ 66.8	✓ 66.5	✓ 64.1	✓ 61.6
12.5	7.1	3.6	2.6		5.4	5.7	8.1	10.8
50	74	93	100		75	73	60	48

✓ 58.1	✓ 57.8	✓ 59.4	✓ 60.3	✓ 60.4	✓ 60.2	✓ 59.7	✓ 58.2	✓ 58.0
14.1	14.4	12.8	11.9	11.8	12.0	12.5	14.0	14.2
43	26	17	8		15	22	29	43

✓ 57.6	✓ 57.7	✓ 58.9				✓ 58.3	✓ 57.9
14.6	14.5	13.3				13.9	14.3
70	93	100				75	69

R STA 103+00

✓ 56.4	✓ 57.1	✓ 59.1	✓ 59.9	✓ 59.6	✓ 59.3	✓ 58.7	✓ 57.3	✓ 57.2
5.2	4.5	2.5	2.3	2.0	2.3	2.9	4.3	4.4
43	26	16	10		14	22	28	43

✓ 56.5	✓ 56.4	✓ 56.5			✓ 56.5	✓ 56.6
5.1	5.2	5.1			5.1	5.0
63	86	100			75	63

Silver Lake Rd.

STA + π - ELV.

961.58

104+00

✓

+23

✓

104+45.7 ETH 100 ?

T.P.

4.95 956.63

Lt

L

MAY 31, 1960

Rt

118

✓ 57.9	✓ 58.3	✓ 59.0	✓ 59.4	✓ 59.0	✓ 58.4	✓ 57.0
3.7	3.3	2.6	3.2 2.2	2.6	3.2	4.6
32	26	17		17	27	33

✓ 56.8	✓ 56.2	✓ 56.0	✓ 55.9	✓ 55.7	✓ 56.2
4.8	5.4	5.6	5.7	5.9	5.9
39	61	79	90	100	75

✓ 58.9	✓ 59.4	✓ 59.2	✓ 59.5	✓ 59.6	✓ 59.4	✓ 58.9	✓ 58.5	✓ 58.4
2.7	2.2	2.2	2.1 2.1	2.0	2.2	2.7	3.1	3.2
61	45	24	10		17	38	56	75

✓ 59.1	✓ 59.0
2.5	2.6
84	100

✓ 60.3	✓ 60.1	✓ 60.0	✓ 59.8	✓ 59.7	✓ 59.5	✓ 59.3	✓ 59.2	✓ 59.1
1.3	1.5	1.6	1.8	1.9	2.1	2.3	2.4	2.5
150	100	65	30		30	58	90	100

60.3
1.3
200

58.4	58.9
3.2	2.7
200	150

GRADE STAKE 60' RT STA 0+00

STA

+

K

-

Elev.

BM

12.06

1002.16

990.10

92+14

+31

+51

+60

93+00

~~+50~~

+50

~~94+00~~

MAY 31, 1960

119

Lt

E

RE.

Top Hyd NE Cor 7th St & Silver Lake Rd

99.6	99.4	98.4	97.1	94.9
2.6	2.8	3.8	5.1	7.3
100	92	72	52	35

→ Cemetery Rd
✓

99.8	99.3	98.0	96.5
2.4	2.9	4.2	5.7
100	81	59	44

✓

99.3	98.8	97.2	94.6
2.9	3.4	5.0	7.6
79	67	50	37

✓

Pump
HOUSES

99.1	98.8	98.0	97.0	94.8
3.1	3.9	4.2	5.2	7.4
80	67	58	48	35

P.H.

✓

99.1	98.6	97.5	95.2	92.8
3.1	3.6	4.7	7.0	9.4
100	85	74	57	43

✓

97.5	94.9	90.1	87.3
4.7	7.3	11.5	14.9
100	87	63	43

✓

STA

+

Δ

-

ELV

1002.16

94+00

BM

12.06

990.10

MAY 31, 1960

Lt

Q

Rt

120

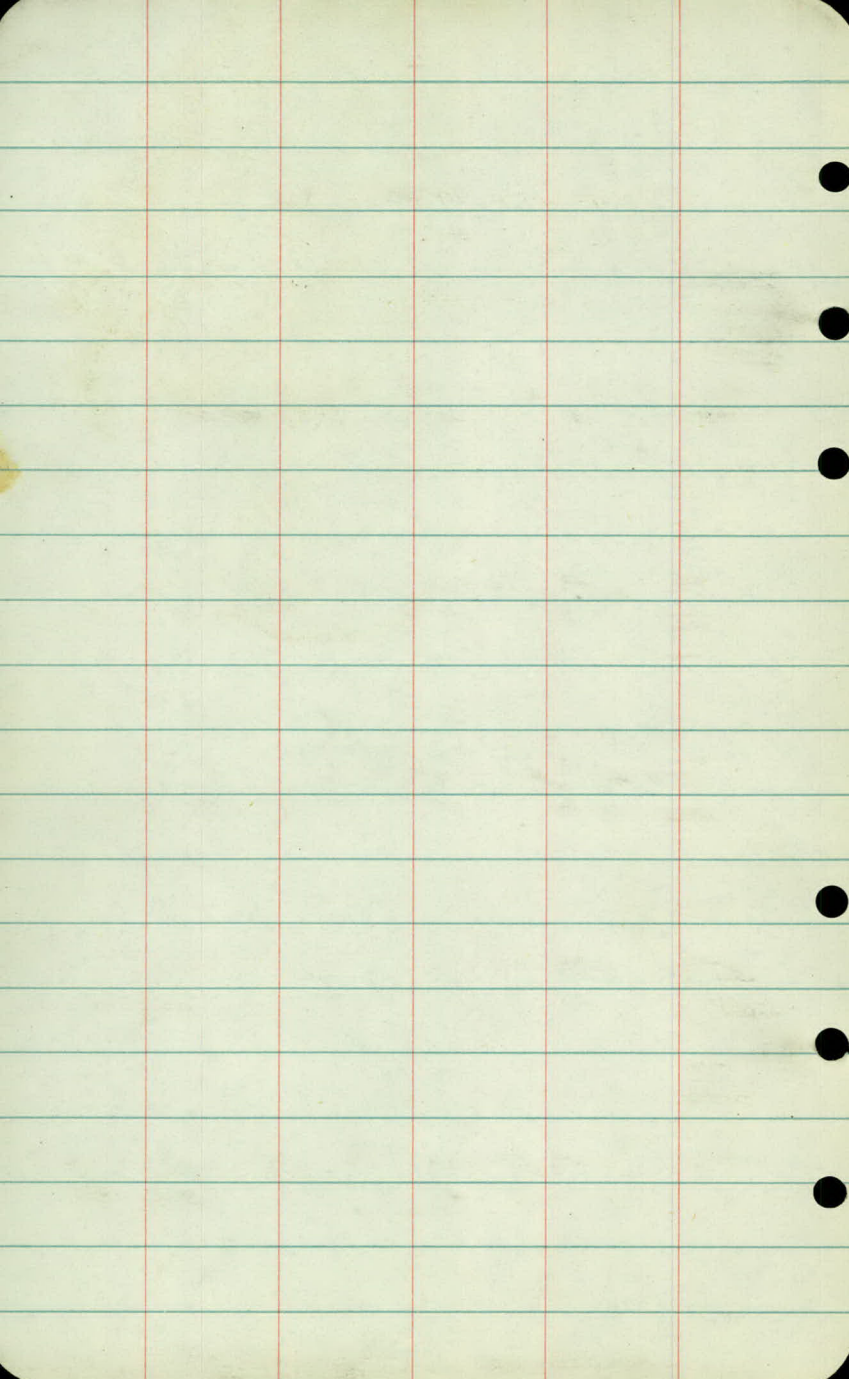
91.8 87.3 83.2

10.4 14.9 19.0

100 72 45



Top Hyd NE Cor 7th St & Silver Lake Rd



SILVER LAKE Rd

T.C.A. M.H. ELEV.

SILVER LAKE

to

S.H. # 100

Bench Levels taken From X-sec.

S + A	T	A	-	CLCO	
B.M.	8.80	947.72			938.92
29+55			11.48	943.24	
33+99			9.71	938.01	
T.P	6.05	945.58	8.19	939.53	
36+55			3.17	942.41	
B.M.			6.65	938.93	938.92
B.M.	3.78	987.01			983.23
60+50			5.69	981.32	
T.P	1.22	976.75	11.48	975.53	
B.M.			4.84	971.91	971.88
T.P	1.85	965.44	13.16	963.59	
8+50			6.17	959.27	
T.P	11.96	976.75	0.65	964.79	
			4.93	971.82	
T.P	11.88	987.29	1.34	975.41	
76+05			2.52	984.77	
B.M.			0.79	986.50	986.59

FS
RB
WS

Lt

E

22 NOV. 1961
FOG & Cloudy 33° 122
Rt

SPike 17 P.P. (SILVER LAKE ^{WEST} LAKE BEACH)

TOP N. RIM TCA M.H. # 17 17' Lt

TOP S. RIM TCA M.H. # 16 16.5' Lt

TOP BREATHER PIPE TCA M.H. # 16 21' Lt

TOP N. RIM TCA M.H. # 15 16.5' Lt

SPike 17 P.P. (SILVER LAKE - W. LAKE BEACH)

TOP HYD Rt STA 59+15

TOP N. RIM TCA M.H. # 13 2' Rt

P.K. STA 63+00 E

SPike 17 P.P. Rt STA 63+89

P.K. STA 66+00 E

TOP N RIM TCA M.H. # 12 9' Lt

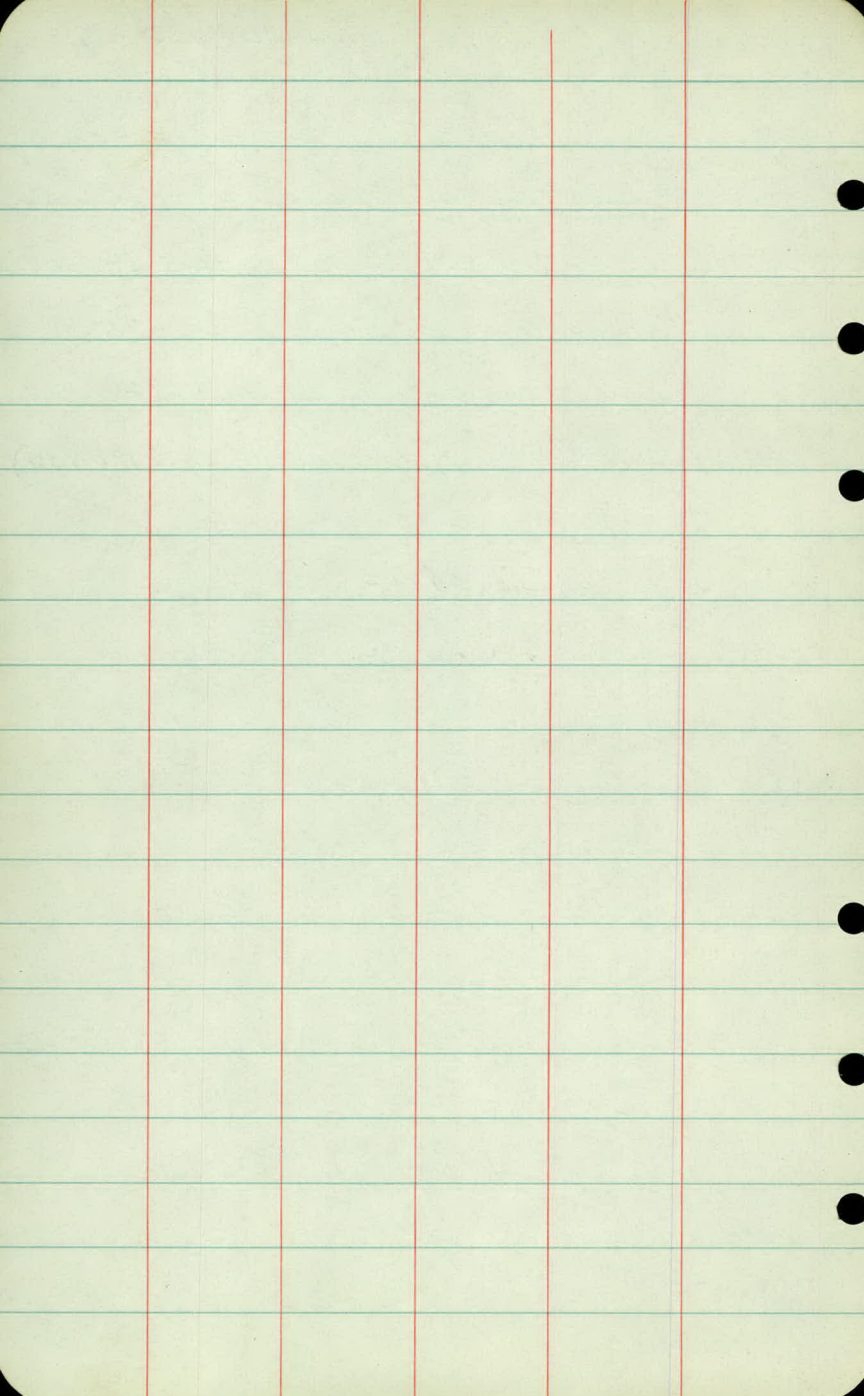
P.K. STA 71+00 E

CHECK SHOT 72+35 TOP WATER SHUT OFF 35' ± Rt

P.K. STA 73+00 E

TOP N RIM TCA M.H. # 11 15' Lt

TOP HYD 30' Rt STA 75+45



Silver Lake Rd.

Standard Oil Pipe Line
locations

3 pages

74+00

+00 $\frac{S.O.P.L}{54.5}$

73+00

+00 $\frac{S.O.P.L}{54.5}$

72+00

+00 $\frac{S.O.P.L}{54.5}$

71+00

+00 $\frac{S.O.P.L}{54.5}$

70+00

+00 $\frac{S.O.P.L}{57.1}$

69+2.1

+21 $\frac{STANDARD OIL MARKING PIPE}{59.1}$

+21 $\frac{S.O.P.L}{57.1}$

JS
FS
RB
WS

22 Nov 1961
cloudy 35° 124

43" Below
Ground

50" Below
Ground

40" Below
Ground

55" Below
Ground

50" Below
Ground 12C

41" Below
Ground

£

$$\begin{array}{r} \text{S.O.P.L.} \\ +74 \text{ MOUNTAIN APC} \\ \hline 27.5 \end{array}$$

$$\begin{array}{r} \text{S.O.P.L.} \\ +70 \text{ EVERETT} \\ \hline 27.5 \end{array}$$

$$+33 \frac{\text{S.O.P.L.}}{52.5}$$

78+00

$$+00 \frac{\text{S.O.P.L.}}{53}$$

77+00

$$+00 \frac{\text{S.O.P.L.}}{53}$$

76+00

$$+00 \frac{\text{S.O.P.L.}}{54}$$

75+00

$$+00 \frac{\text{S.O.P.L.}}{54}$$

74+00

$$+00 \frac{\text{S.O.P.L.}}{54.5}$$

FS
RB
W.S

125

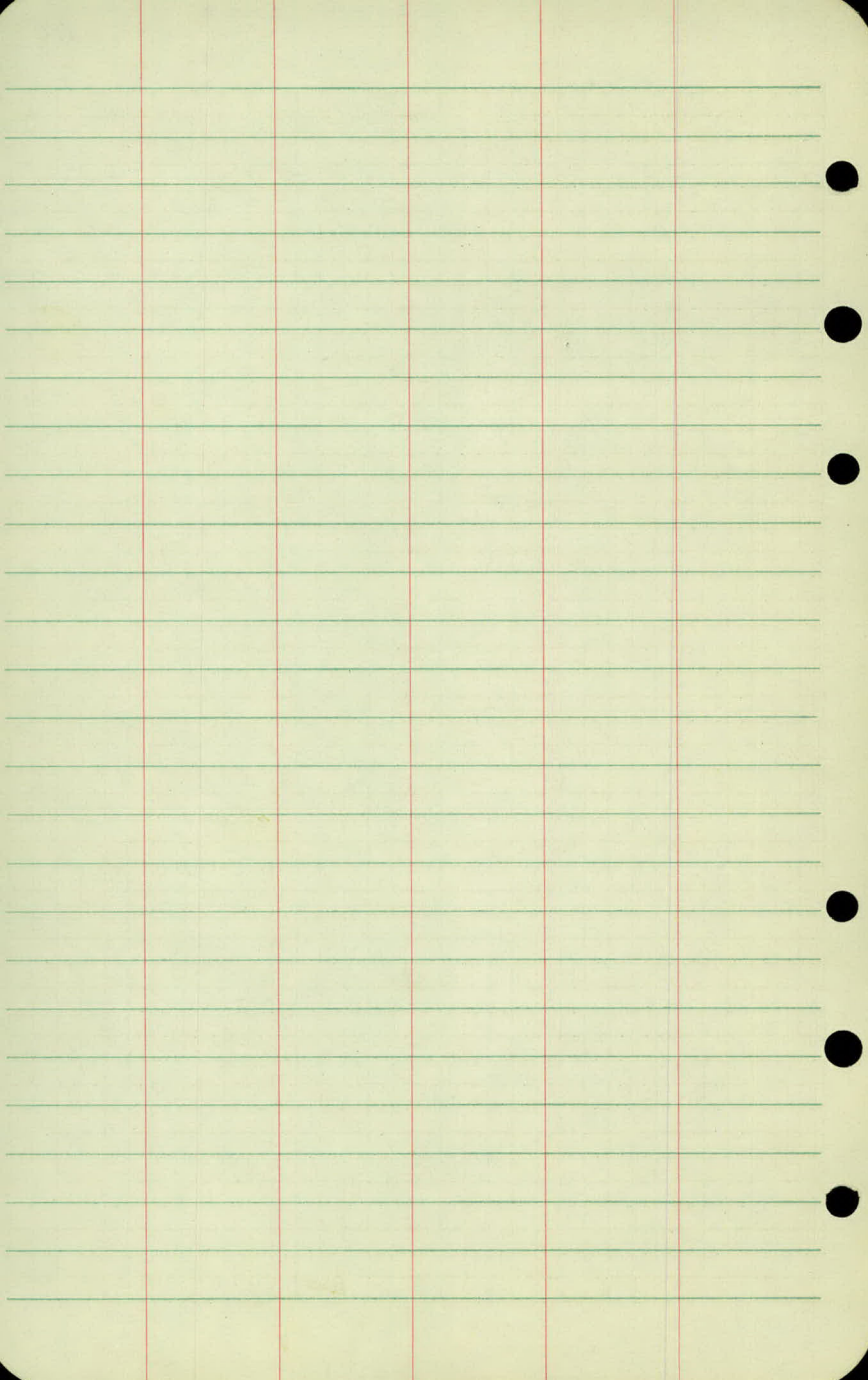


5.0' Below Ground

5.0' Below Ground

5.0' Below Ground

43" Below Ground



SILVER LAKE RD

X- SECTIONS

BENCH Levels taken from X. SEC

Sfg + # - C/EU

B.M. 1.99 988.56

986.59

78+44 LEFT ONLY

~~+46~~

78+47

78+74

78+76

78+92

~~78+30~~

B.M.

3.62 984.94 984.93

25
FS
RB
W.S

L+

24 NOV 1961 127
CLEAR 340
RT

TOP HYD 30' RT 75+45

79.9	80.4	81.0	81.5	81.6	82.2	83.5	83.8	83.9	82.98
8.7	8.2	7.6	7.1	7.0	6.4	5.1	4.8	4.7	
100	80	58	43	27	23	16	14		

79.9	80.4	81.7	81.7	81.6	82.9	83.5	83.8	83.9	5.58 34 (shut off water)
8.7	8.2	6.9	6.9	7.0	5.7	5.1	4.8	4.7	
100	66	52	30	26	20	16	14		

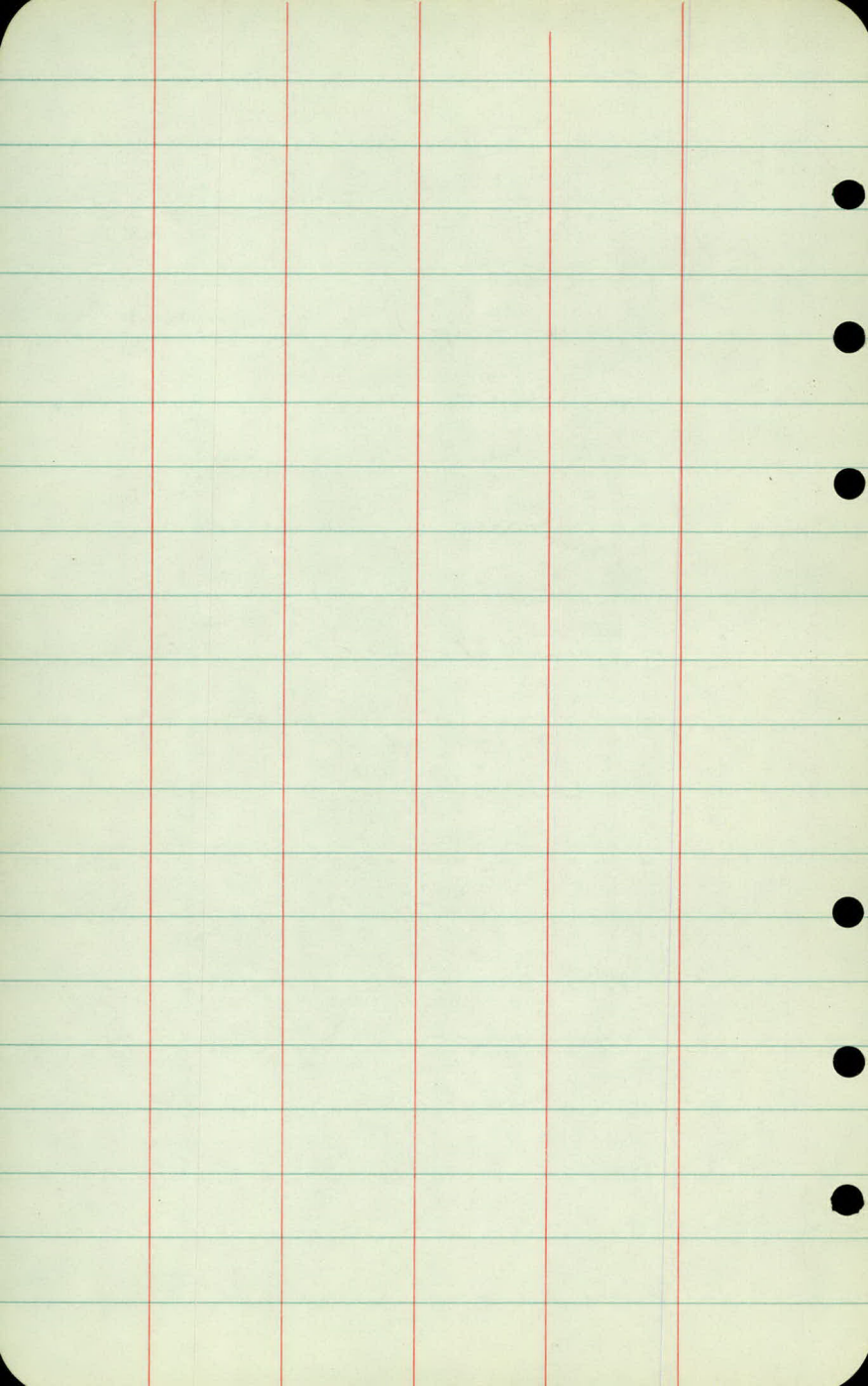
79.1	79.8	79.8	80.0	80.2	82.9	83.3	83.6	83.7
9.5	8.8	8.8	8.6	8.4	6.7	5.3	5.0	4.9
100	88	67	51	21	23	17	14	

79.1	79.1	79.4	79.8	80.6	82.9	83.3	83.6	83.7
9.5	9.5	9.2	8.8	7.0	5.7	5.3	5.0	4.9
100	90	71	48	29	22	17	14	

79.0	79.0	79.1	79.1	80.2	82.5	83.1	83.5	83.6	82.48
9.6	9.6	9.5	9.5	8.4	6.1	5.5	5.1	5.0	
100	83	67	49	29	23	17	14		

6.08 shut off water
30

TOP HYD 30' RT 79+05



28 JULY 1961

138

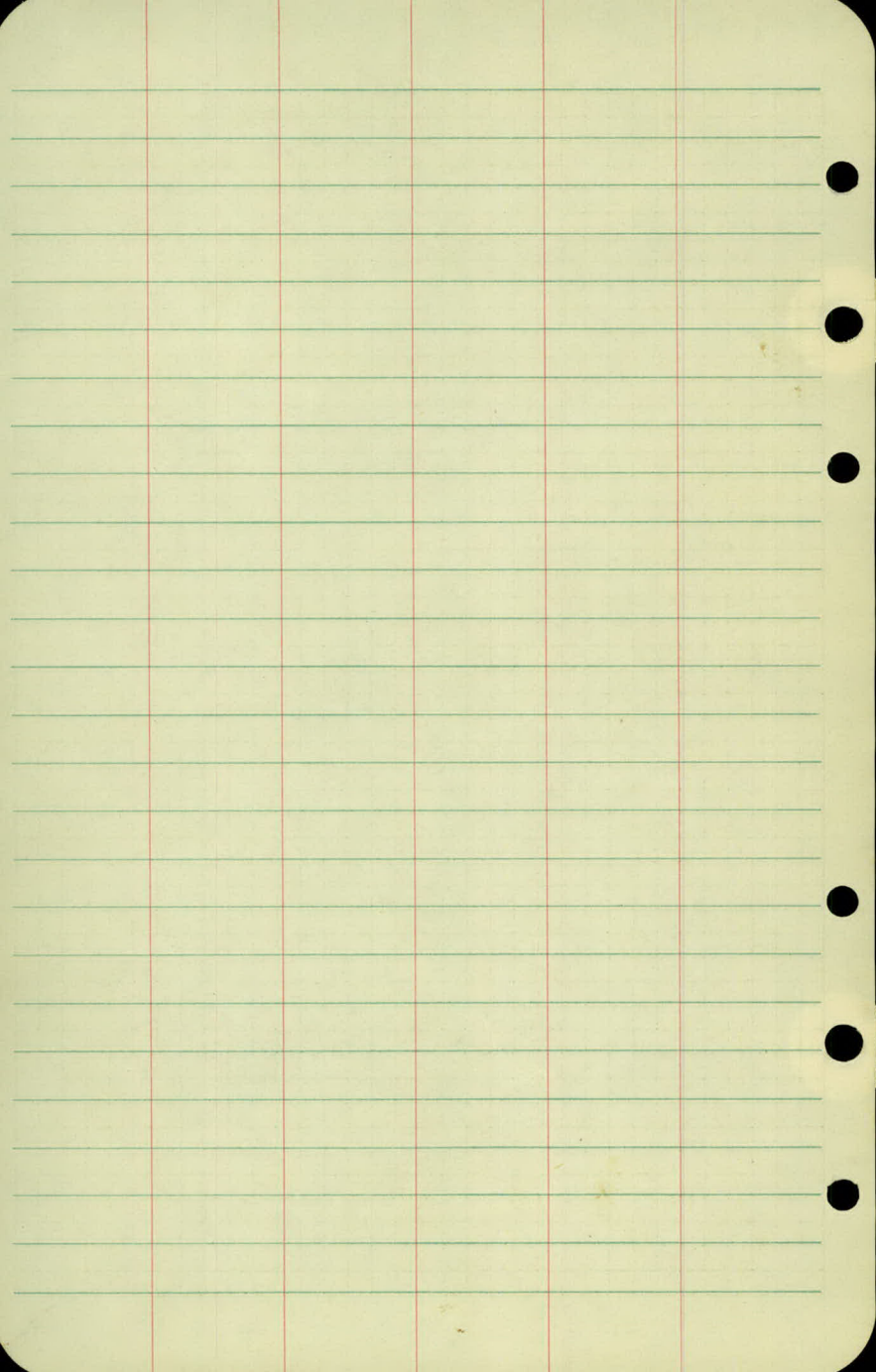
KP
RB
JD
RH

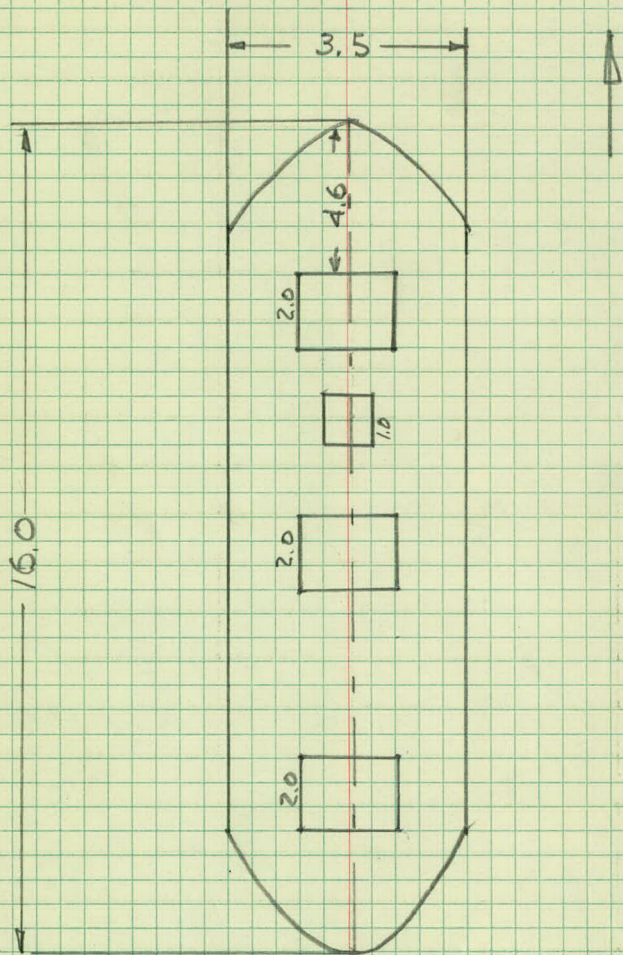
SILVER LAKE RD
CORD E TO STH #100
FILLING STATION
TOPOGRAPHY & ELEVATIONS

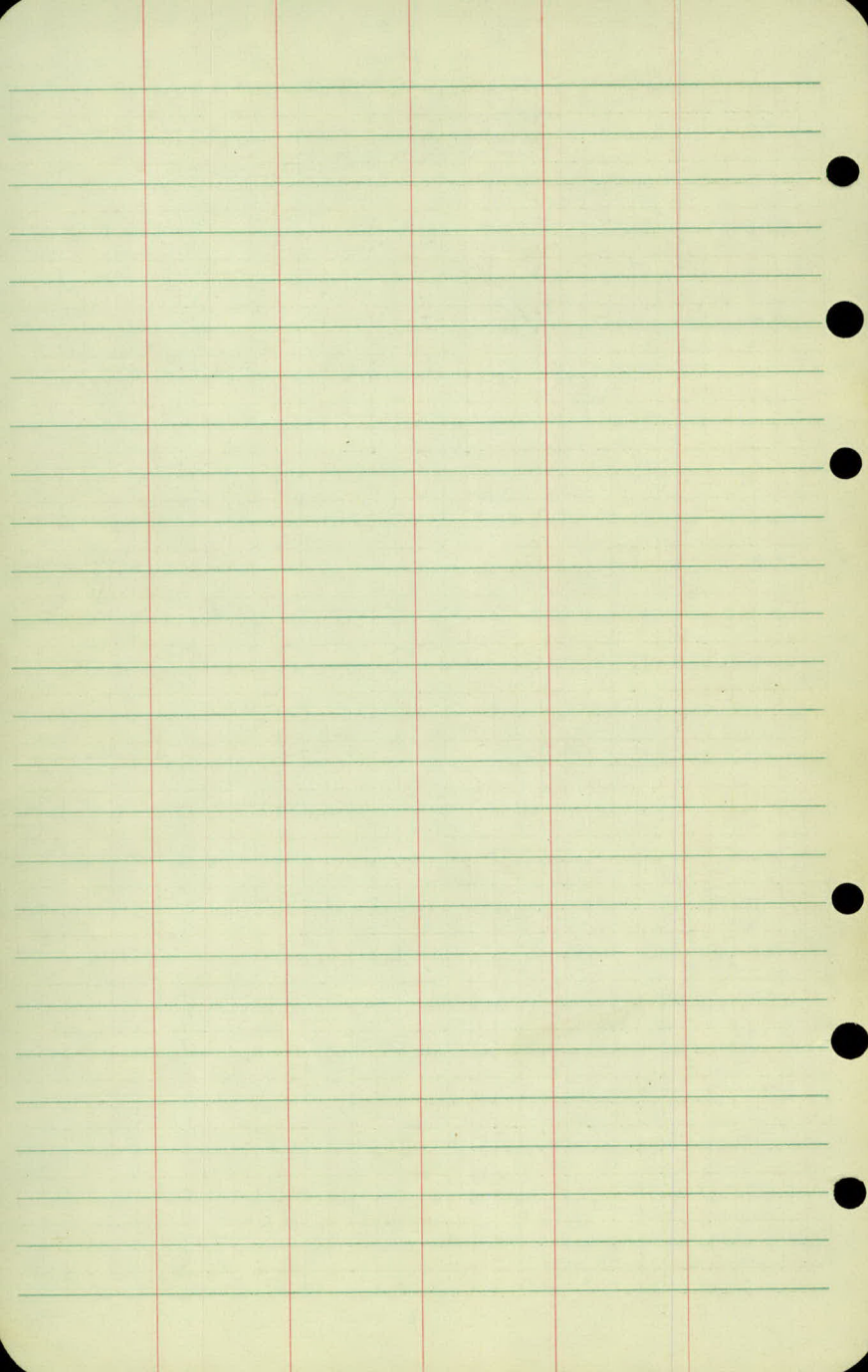
$\pm$ = New Survey line

Plotted
Aug. 30, 1961
H.D.G.

Sta	+	-	ELEV.
BM	5.75	968.52	(962.77)
S.W. COR Slab		8.00	960.52
N.W. COR Slab		3.99	964.53
34	3 19	$\begin{array}{r} +97 \text{ ER} \\ 19 \\ \hline +74 \end{array}$ $\begin{array}{r} 2 \times 2 \text{ STD} \\ \hline 56 \end{array}$	$\begin{array}{r} +94 \text{ N. END 15' CM} \\ 28 \\ \hline +87 \text{ PP} \\ 35 \end{array}$
		+72 NW COR Slab	+58 BR
		55	19
		+55 CONC. SLAB	35
		54	
150		+52' RT BLDG	+54 SEND 15' CM
			29
		+42 $\pm$ N END PUMP BASE	+49 NW COR ST
		69	96
		+26 $\pm$ S. END PUMP BASE	+19 R.T. S.W.
		69	
		+02 ER	+05 BR
		35	17
53	6 17		+16 SW COR Sidewalk
			94
		+75 TEL. BOOTH	+86 $\pm$ W. END PUMP BASE
		53	97.5
		+71 SW COR CONC	+72 1.5X2.0 STD
		52	53
		+61 1.5X2.0 STD	+67 ER
		36	16
			+71 ER
			34.5
150		+51 Archite Pole	+59 Hyd
		39	39.5
			+60 SW COR BT
			34.5
		+28.5 MH	5
52			







SS
W 114
LB
RB
DS
WS

1

Silver Lake Rd

Tree Count

26+14 to 52+21.57

Sta	Clear	Grub
26+32 Rt	1	1
30+07 Lt 25'	1	1
+21 Lt 25'	1	1
+31 Lt 25'	1	1
+39 Rt 45'	1	1
+57 Lt 30'	2	1
+71 Lt 26'	1	1
+72 Rt 45'	1	1
+78 Rt 45'	1	1
31+27 Lt 30'	1	1
32+64 Rt 34'	Bush	
34+17 Lt 37'	1	1
+21 Lt 37'	1	1
+46 Rt 44'	Pine	4' Tall
+57 Rt 44'	Pine	4' Tall
35+08 Rt 42'	Pine	2' Tall
+25 Rt 39'	Pine	2' "
+36 Rt 39'	Pine	2' "
+48 Rt 40'	Pine	2' "
+58 Rt 40'	Pine	2' "

Sta

Clear

Grub

35+68 Rt 40'

Pine

1' Tall

+78 Rt 40'

Pine

1' Tall

+86 Rt 40'

Pine

1' Tall

+96 Rt 40'

Pine

1' Tall

36+24 Lt 38'

1

1

+35 Lt 41'

1

1

+51 Lt 41'

1

1

+68 Lt 37'

1

1

+89 Lt 41'

1

1

37+38 Lt 58'

1

1

+53 Lt 60'

1

1

+64 Lt 45'

1

1

38+35 Lt 46'

1

1

+77 Lt 39'

2

1

+90 Lt 41'

1

1

46+47 Lt 30'

1

1

+66 Lt 42'

1

1

+68 Rt 54'

1

1

+76 Rt 41

1

1

Sta

Clear Grub

46+88 Lt 48'

1 1

47+ 43 Rt 42'

2 1

+ 60 Rt 41'

1 1

+ 64 Rt 37'

1 1

50+00

to

37 37

52+00 Lt

35

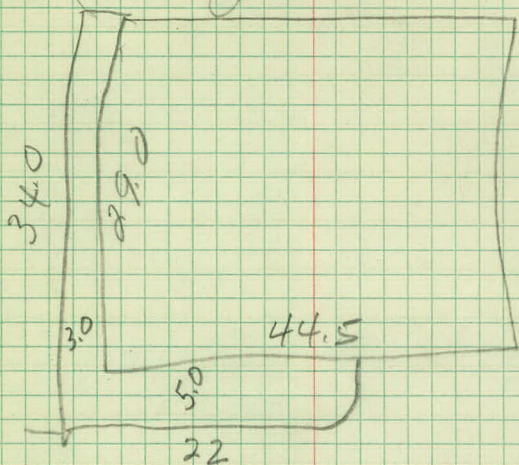
51+20 Rt 46'

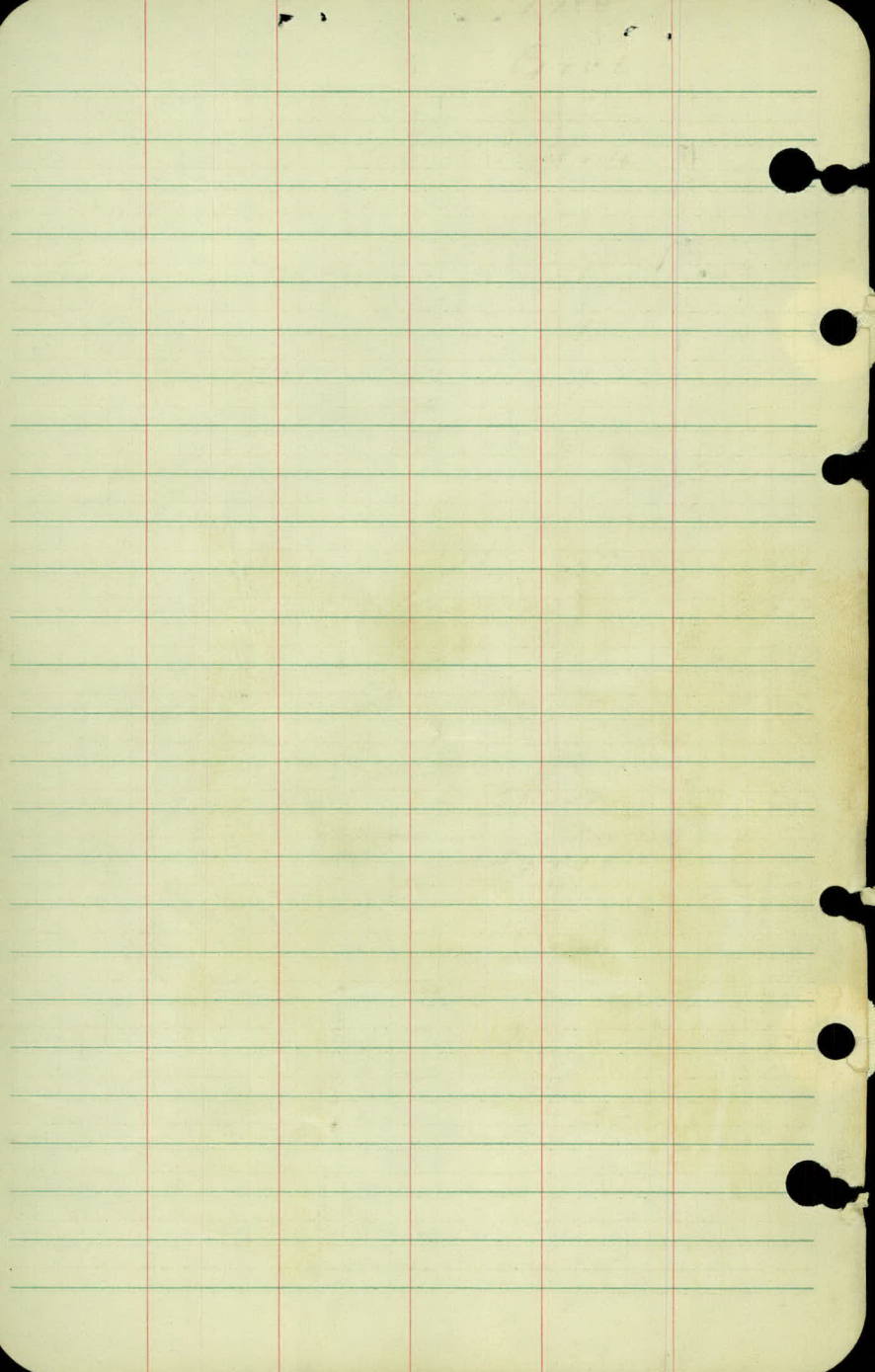
1 1

Total = 42 Trees

Total = 69 Grub

~~Heckon~~





Tree's station	Clear	Grab
CorDE Sta - 1454/37 No.	1	1
4+20 61' Rt	1	1
54+81 69' Rt	1	1
55+09 74' Rt	1	1
55+21 71' Rt	1	1
54+43 to +71 15' to 22' Lt	Brush 1	1
56+17 17' Lt		1
55+63 Lt 34' Plam Tree	1	1
58+75 Rt 54' Twin oak	2	1
60+39 - +96 Lt + 69/26 mid Pt Brush	606 ⁰¹ 5	5 + 3" willows brush
62+77 Rt 52'	1	1
64+78 Lt 9'		1
63+55 - +90 Lt 45' - 52'	4	4 + 3" willows brush
64+20 to +40 Brush 3" willows		
65+54 Lt 33'	3	1
65+75 Lt 24'	2	1
65+46 58' Rt	1	1 12(3")
67+17 Rt 44' ✓	1	1 (4 more check)
69+20 31' Lt	1	1
69+78 Lt 20'		1
70+34 Lt 33'		1
75+33 Rt 38' Upright Juniper		
75+37 Rt 35 Pfitzer Juniper		
75+44 Rt 35 Mugho Pine		
+82 Rt 34 Mugho Pine		
+94 Rt 34 Pfitzer Juniper		
76+00 Rt 38 Upright Juniper		

Stationing		Clear	Grub
81+81	39' Lt	1	1
81+02	46' Lt	1	1
82+15	28' Lt	1	1
82+21	30' Lt	1	1
82+29	53' Lt	1	1
82+53	32' Lt	1	1
82+72	29' Lt	1	1
82+87	42' Lt	1	1
82+95	33' Lt	1	1
83+51	27' Lt	1	1
83+94	27' Lt	1	1
84+07	27' Lt	5	1
85+13	36' Rt	1	1
86+71	34' Rt	1	1
89+55	Lt 27'		1
89+99	Lt 30'		1
90+18	Lt 30'		1
90+55	Lt 32'		1
93+56	Lt 32'		1
94+00	42' Rt	1	1
94+03	42' Rt	5	4
94+11	30' Rt	1	1

94+20	RT 38'	1	1	Grub
94+73	RT 41	3	1	
94+81	RT 41	3	1	
95+96	RT	⁵⁷ 15	10	
95+92	42' LT	1	1	
96+97	RT	⁹³ 27	¹⁵ 12	
100+57'	59' RT	1	1	
100+97	70' RT	1	1	
101+23	55' RT	1	1	
101+42	61' RT	1	1	Pine
101+97	53' RT	1	1	"
102+26	52' RT	1	1	"
102+46	59' RT	1	1	"
102+68	60' RT	1	1	"
102+05	43' LT	1	1	"
102+30	47' LT	1	1	"
102+18	65' LT	1	1	"
102+44	70' LT	1	1	"
102+67	78' LT	1	1	"
102+99	86' RT	1	1	"
		103	80	

Silver Lake Rd. E. 70

Topography

N.S.P. Gas Main

2 pages

91+00

+100 N.S.P Gas Main
25.7

90+00

+100 N.S.P Gas Main
25.8

89+00

+100 N.S.P Gas Main
25.9

88+00

+100 N.S.P Gas Main
25.9

+82.3 Gas Service
21.0
+75.5 R.T. Service
81.1
2

87+00

+100 N.S.P Gas Main
26

+68 N.S.P Gas Main R.T. Service
26.0 116.1

86+00

SS
FS
R13
WS

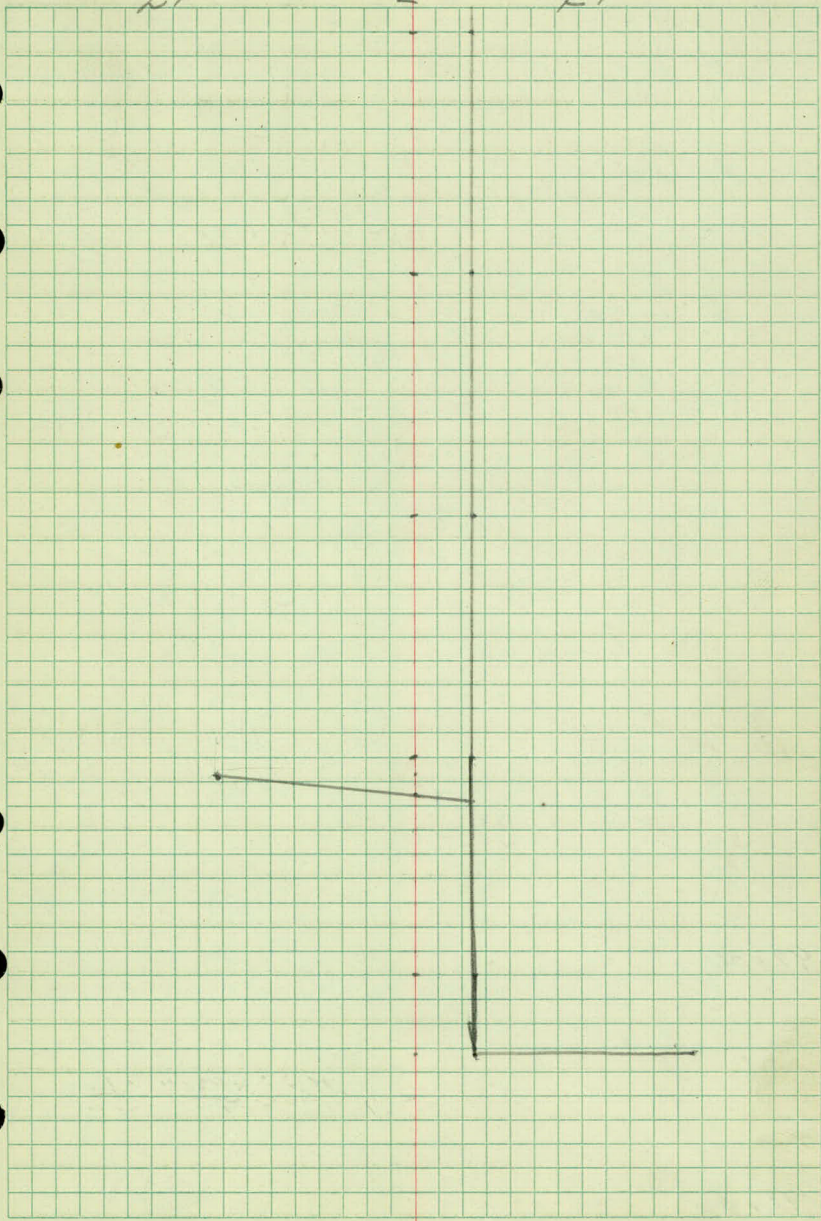
24 Nov 1961
CLEY 138°

129

Lt

$\angle$

Rt



92+00

N.S. DGGS MAIN
+43 SHUT OFF VALVE
25.6

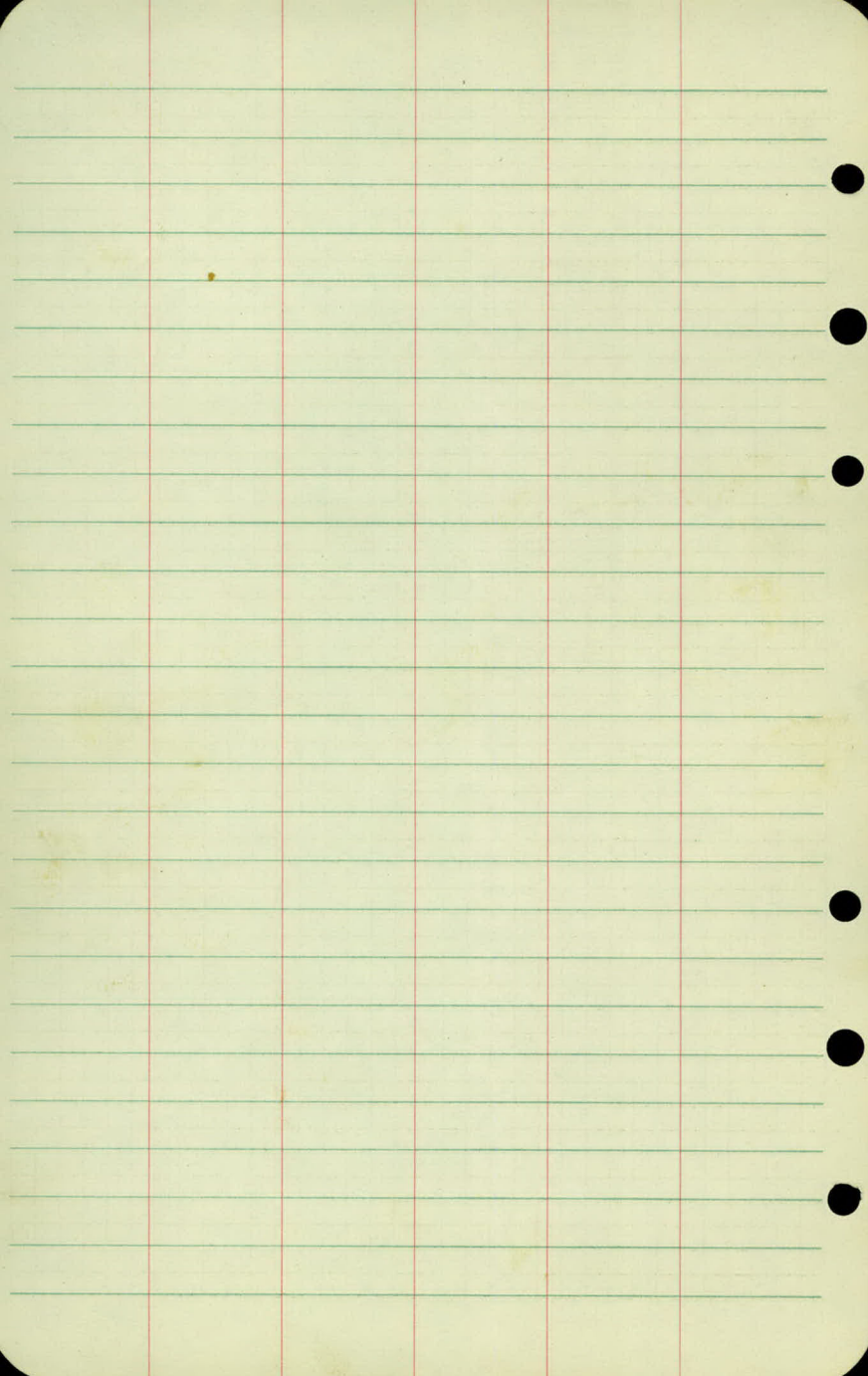
91+00

N.S. DGGS MAIN
+00 25.7

JS
FS
RB
W.S

24 Nov 1961
Clear 38° 130

6



SILVERLAKE RD

Manhole Elevations

FLO. LINE TO TOP OF Casting

adjustment (From Pre Cast to top
of casting)

Casting thickness

Sta	+	π	-	elev
-----	---	-------	---	------

B.M	6.30	969.07		962.77
-----	------	--------	--	--------

52+29			9.25	59.82 <u>10 69</u> 19.13
-------	--	--	------	--------------------------------

52+37			9.48	59.59 <u>10 34</u> 49.25
-------	--	--	------	--------------------------------

			6.30	962.77	962.77
--	--	--	------	--------	--------

B.M.	1.97	988.56			986.59
------	------	--------	--	--	--------

78+56			4.75	83.81	
-------	--	--	------	-------	--

T.P.	6.12	991.06	3.62	984.94	
------	------	--------	------	--------	--

132

24

22

12

TOP HYD N. E COR SILVER LAKE RD & CO. RD. E

TOP N RIM SANITARY SEWER 4.5' RT

10.69 INLET FLOW LINE to top of casting ^{top}

1.57 TOP PRECAST to top of casting

0.80 Casting ^{Height} HEIGHT

"Flows East"

TOP E. RIM sanitary sewer 18.5' LT

10.34 INLET FLOW LINE to TOP of CASTING

2.55 TOP PROCT to top of castine

0.80 HEIGHT of casting

TOP HYD N.E. COR SILVER LAKE, C.B. RD

Flows From West
to E.S. to M.H.
52+29

TOP N.Y.D 30' 124 75+45

TOP "N." RIM SANITARY SCHOOL 4

9.47 FLO LINE TO TOP OF CASTING FROM "N."

941 " " " " " "

Gering L.

1.88 FROM PRECAST to TOP of CASTING

0.80 HEIGHT OF CASTING

TOP HYD 30' RT 79+05

Flows "N" to "E".

Sta	+	π	-	CICU
-----	---	-------	---	------

		991.06		
--	--	--------	--	--

82+71			6.45	84.61
-------	--	--	------	-------

T.P	6.91	995.16	2.81	988.25	988.23
-----	------	--------	------	--------	--------

85+31			5.92	89.24	
-------	--	--	------	-------	--

			2.02	93.14	
--	--	--	------	-------	--

T.P	3.31	996.45	2.02	993.14	
-----	------	--------	------	--------	--

91+06			4.20	92.25	
-------	--	--	------	-------	--

2.5
FS
RB
W.S

Lt

E

24 NOV 1961
CLEAR 34°

Rt

133

TOP "N" RIM SANITARY SEWER 1' RT.

9.09' FLO. LINE TO TOP OF CASTING

1.65' FROM PRECAST M.H TO TOP CASTING

0.80 HIEGHT OF CASTING

TOP S.W. COR. LIGHT POST NO. #569 (SO. LIGHT POST)

TOP "N" RIM SANITARY SEWER &

11.6 FLO. LINE TO TOP OF CASTING

1.75' FROM PRECAST M.H TO TOP OF CASTING

0.80 HIEGHT OF CASTING

TOP "N" RIM SANITARY SEWER

14.2 FLO. LINE TO TOP OF CASTING

1.3 FROM PRECAST M.H TO TOP CASTING

0.80 HIEGHT OF CASTING

TOP "N" RIM M.H & STA 85+31

(OUTLET ONLY)
TOP "N" RIM SANITARY SEWER 1' RT

12.25' FLO LINE TO TOP CASTING

1.02' FROM PRECAST TO TOP "

0.80 HIEGHT OF CASTING

"N" to "S"
FLOWS

"N" to "S"
FLOWS

"N" to "S"
FLOWS

FLOWS FROM THIS
M.H. "S" ONLY
NO INLET

Sta	+	π	-	ELEV
-----	---	-------	---	------

		996.45		
--	--	--------	--	--

T. P.			6.37	990.08 (990.10)
-------	--	--	------	-----------------

95+14

T. P.

96+96

Lt

±

Rt

134

Top HYD 50' Rt STA 92+67 (N. ECOE CEMETARY RD)
SILVER LAKE RD

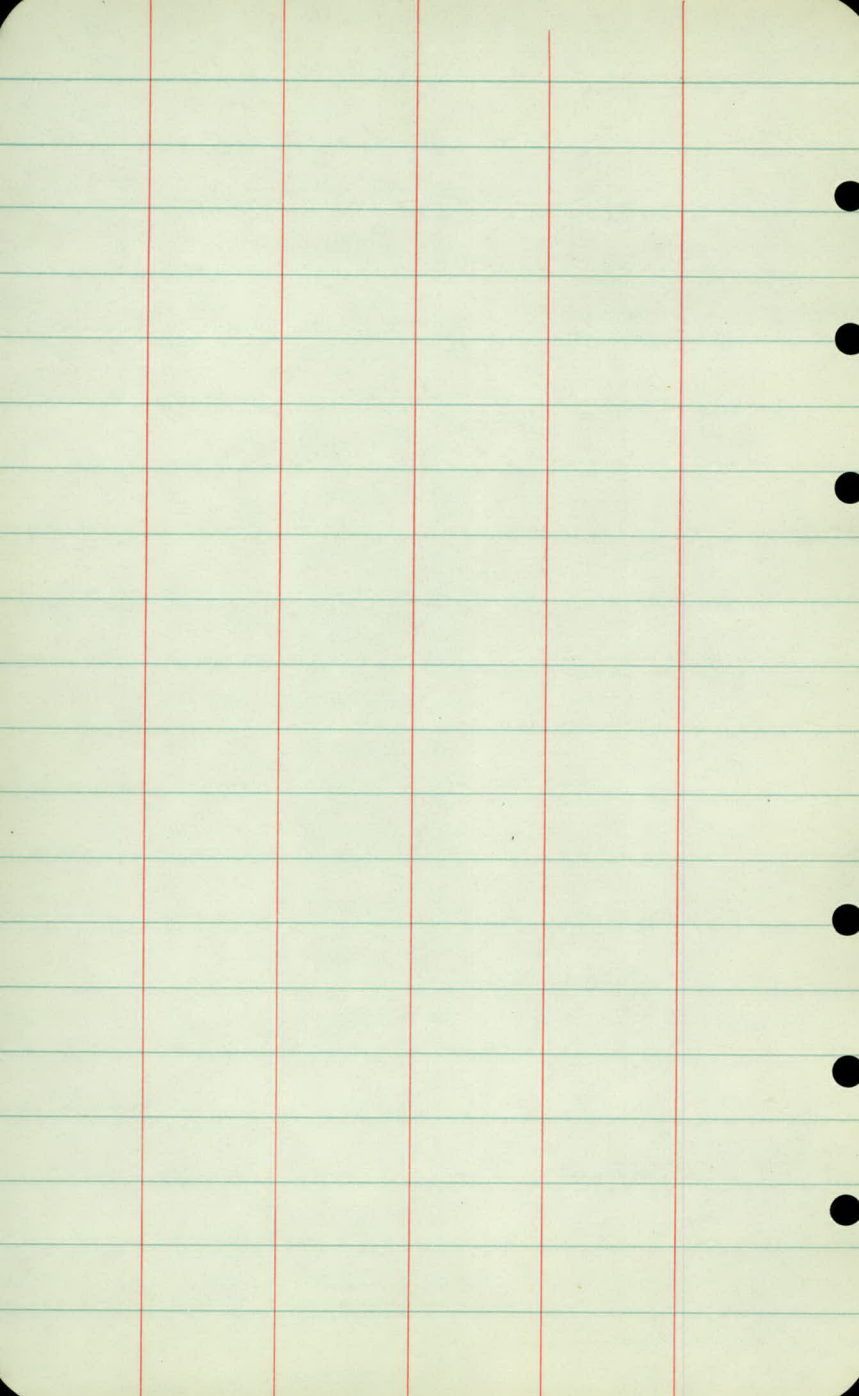
TOP "No." RIM SANITARY SEWER 32' Lt.

8.20 FLO LINE TO TOP OF CASTING

1.35 FROM PRECAST TO TOP "

0.80 HIEGHT OF CASTING

"S" to "N"
FLO



Lt

E

Rt

1350

TOP HYD 50' Rt Sta 92+67

(N.E. Coy Cemetery Rd)
(Silver Lake Rd)TOP "N" RIM SANITARY SEWER 33' ~~Rt~~ Lt.

8.20 FLOW LINE TO TOP OF CASTING

1.35' FROM PRECAST TO TOP OF "

0.80 HIEGHT OF CASTING

96+96

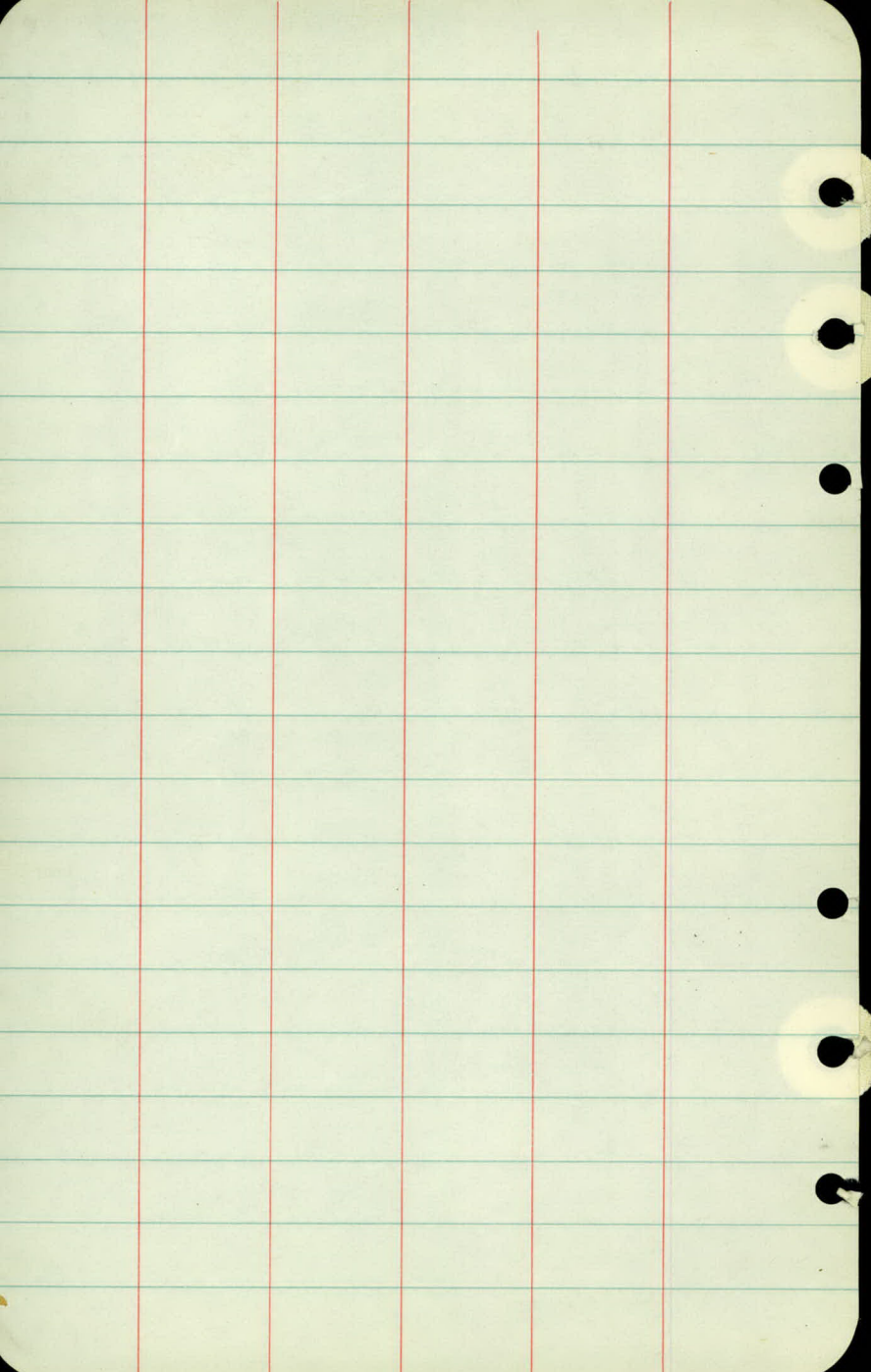
TOP "N" RIM SANITARY SEWER

9.60 FLO. LINE TO TOP OF CASTING

1.40 FROM PRECAST TO TOP OF "

0.80 HIEGHT OF CASTING

S. to N.



XP
US
FS
LB

27 NOV 1961

136

SILVER LAKE RD
CO. RDE TO STH 100

MH & CULVERT ELEVATIONS

Sta	+	Σ	-	Elev.	
BM	0.54	990.64			990.10
95+14			14.83	975.81	
T.P.	2.43	981.59	11.49	979.15	
96+96			7.73	973.85	
98+94			12.71	68.87	
TP	0.96	970.49	12.05	969.53	
104+47			10.72	959.75	
TP	12.57	982.10	0.96	969.53	
TP	11.13	991.95	1.28	980.82	
BM			1.68	990.27	990.10

27 Nov. 1961

1370

Lt

±

Rt

TOP HYDRANT 50.0 RT STA 92+65

TOP MH 32.0 Lt cover broke

TOP PK ± STA 95

TOP MH 34.0 Lt. (S. RIM)

TOP MH (precast)

FL TO TOP ADJ. RING 10.8
NO CASTING.

STW

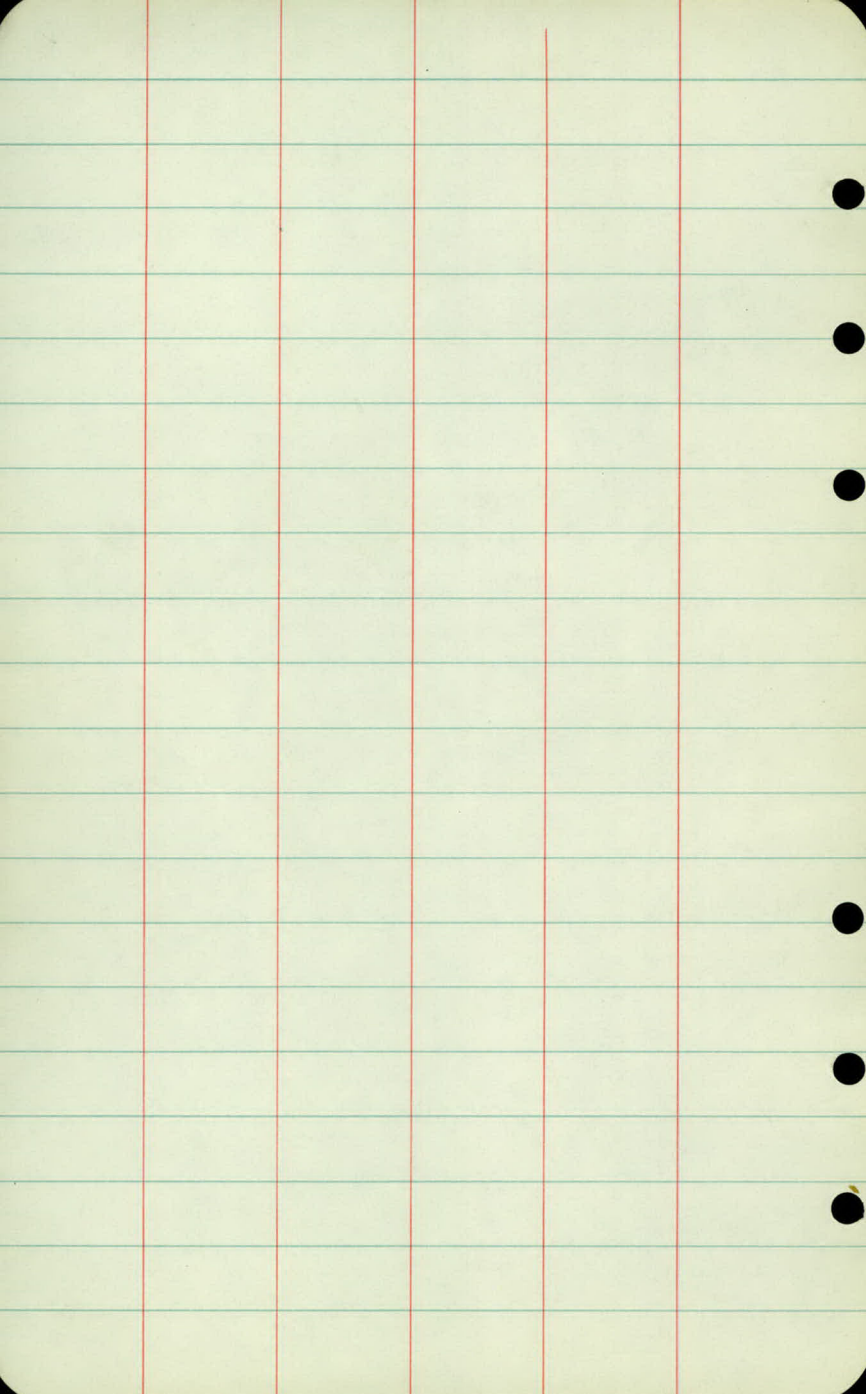
TOP PK ± STA 99

± STA 100

TOP PK ± STA 99

TOP ROCK

TOP HYD. 50.0 RT STA 92+65



Locate and get elev. to following
cross-headers - get new stations if any

	Lt	E	Rt	
57+21 $\frac{12''}{42'}$	2'		21	Can't Find

65+23 $\frac{12''}{40'}$	23'		19'	Can't Find
--------------------------	-----	--	-----	------------

67+67 $\frac{18''}{40'}$			20'	Can't Find
--------------------------	--	--	-----	------------

71+10 = 84' Lt				Can't Find
----------------	--	--	--	------------

70+73 25' Ft.	- $\frac{12''}{Vt}$ -			
---------------	-----------------------	--	--	--

79+52 $\frac{12''}{32'}$	19'		13'	in x sections
--------------------------	-----	--	-----	---------------

98+86 $\frac{12''}{36'}$	19		17'	Can't Find
--------------------------	----	--	-----	------------

104+90 $\frac{12''}{46'}$	26'		20'	Can't Find
---------------------------	-----	--	-----	------------

$$\begin{array}{r}
 76.75 \\
 4.93 \\
 \hline
 971.82
 \end{array}$$

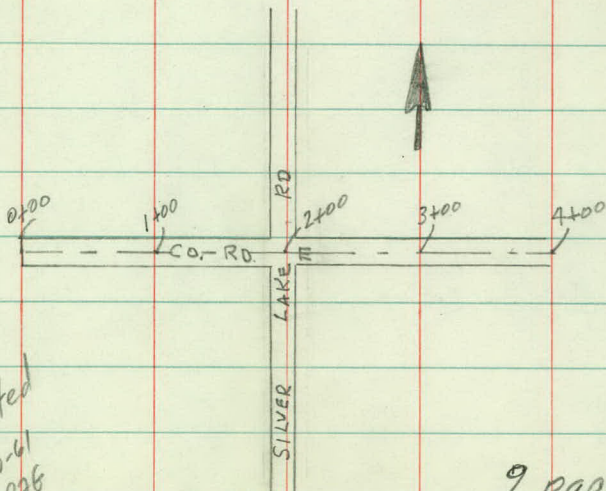
$$\begin{array}{r}
 76.75 \\
 134 \\
 \hline
 975.41
 \end{array}$$

SILVER LAKE RD

X- SECTIONS

ON CO. RD. E 200' E & W OF
SILVER LAKE RD.

0+00 = 200' W. OF SILVER LAKE
RD. ON E OF CO. RD. E.



Plotted
1-10-61
RAG

9 pages

STA	+	π	-	ELEV.
BM	4.14	966.94		962.80
0+28				89.5 1.08 7.87 7.9
✓				
0+00				
✓				
+60				

TOP HYDRANT N.E. COR SILVER LAKE RD & CO. RD. E.

61.2	57.3	57.5	57.9	57.9	57.8	58.1	58.8	54.5
5.7	9.6	9.4	9.0	9.0	9.1	8.8	10.1	12.4
28	21	18	13		9	13	20	26
64.0	65.2	66.4						54.9
2.9	1.7	0.5						12.0
47	50	65						28

60.1	58.7	57.8	57.8	57.8	57.6	58.0	56.9	54.7
6.8	8.2	9.1	9.1	9.1	9.3	8.9	10.0	12.2
27	21	14	9		9	14	20	25
63.8	64.8	66.0						56.2
2.5	2.1	0.9						10.7
43	53	64						28

58.5	57.3	57.8	58.0	58.0	57.9	58.1	54.4	53.6
8.4	9.6	9.1	8.9	8.9	9.0	8.8	12.5	13.3
22	18	14	10		9	15	25	28
63.8	64.8	66.4						
3.1	2.1	0.5						
30	43	68						

STA

+

π

-

ELEV

966.94

1+00

✓

+50

2 = $\neq$ S.L.R.

2+50

✓

Jan 3, 1962

3.

LT

RT

58.7

57.9

58.1

58.2

57.9

58.2

58.2

52.9

8.2

9.0

8.8

8.7

9.0

8.7

10.7

14.0

21

15

10

9

15

20

26

64.5

64.8

65.0

65.0

24

21

1.9

1.9

29

46

56

62

59.1

58.5

58.7

58.8

58.7

58.3

58.7

53.5

7.8

8.4

8.2

8.1

8.2

8.6

8.2

13.4

28

23

17

12

9

15

23

60.4

63.7

64.0

64.9

6.5

3.2

2.9

2.0

40

49

61

75

61.1

60.2

59.7

59.3

59.2

58.8

57.3

54.4

5.8

6.7

7.2

7.6

7.7

8.1

9.6

12.5

58

34

17

10

12

21

28

61.9

5.0

82

49.3

17.6

64

51.8

15.1

44

STA

+

π

-

ELEV

966.24

3

✓

+30

✓

+65

Jan. 3, 1962

4

LT

RT

60.38

57.3

58.8

58.8

58.7

58.5

57.7

57.3

6.56 7.6 8.1 8.1 8.2 8.3 9.2 9.6

44 27 16 10 10 18 27

Conc

60.38

6.40
60

49.5

54.5

17.4 12.4
63 41

57.89

57.1

58.4

58.4

58.4

58.2

57.2

57.9

54.3

7.05 7.8 8.5 8.5 8.5 8.7 9.7 9.0 12.6

45 34 19 10 10 18 25 49

Conc

60.48

6.46
66

Conc

51.3

15.6
70

59.6

58.5

57.9

57.9

57.9

57.6

56.6

53.8

7.3 8.4 9.0 9.0 9.0 9.3 10.3 13.1

47 29 17 10 9 19 27

60.1

6.8
63

50.5

51.2

16.4 15.7
76 49

STA	+	π	-	ELEV.
		966.94		
4+00				
✓				
5+00				
+28				890 1.02 7.88
+60				
/				
+50				
12.11				
A13				962.81
				(962.80)

Jan 3, 1962

5.

LT

RT

51.4

57.8

57.2

57.4

57.5

57.0

55.8

51.7

5.5

9.1

9.7

9.5

9.4

9.9

11.3

15.2

36

25

18

10

10

16

25

64.8

65.7

47.3

48.1

49.5

2.1

1.2

19.4

18.8

17.4

47

70

75

60

40

56.6

56.2

55.2

53.6

10.3

10.7

11.7

13.3

30

42

54

70

54.7

53.8

53.6

48.6

12.2

13.1

15.3

18.3

29

36

52

70

52.3

49.9

46.9

44.4

42.4

14.6

17.0

20.0

22.5

24.5

31

41

53

64

75

49.7

45.9

43.5

41.9

17.2

21.0

23.4

25.0

33

45

57

75

47.9

44.9

43.4

19.0

22.0

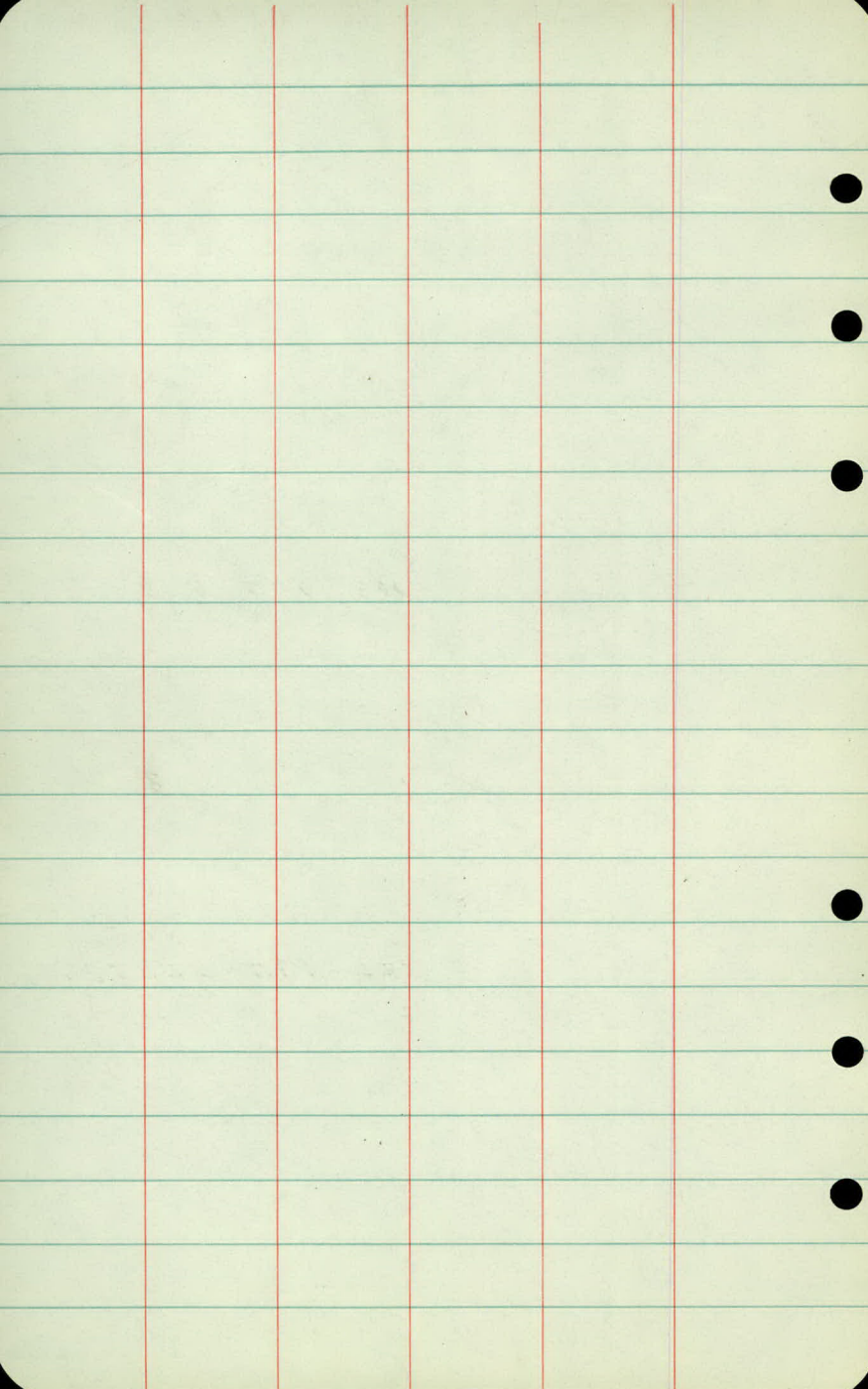
23.5

35

58

75

Top Hyd NECor E + SLR.



KP
RB
LB
DS
WS

29 DEC. 1961
Jan 3, 1962

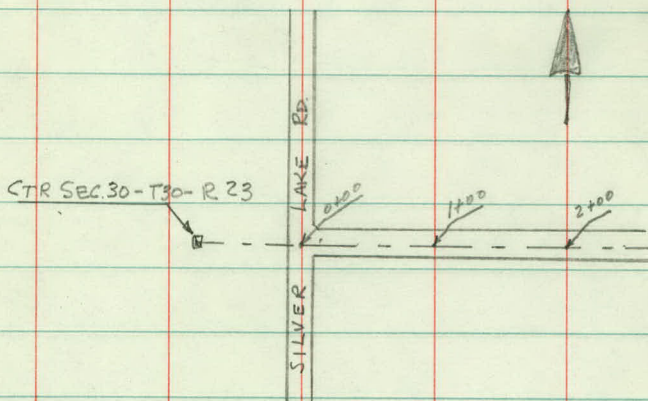
6

SILVER LAKE RD

X- SECTIONS

ON 5TH

FROM SILVER LAKE RD TO 200' E.



STA	+	π	-	ELEV
-----	---	-------	---	------

BM	2.74	987.67		
----	------	--------	--	--

984.93

0+50

+75

1

+50

4.7

2

4.5

+50

4.3

BM

2.74 984.93

LT

E

Jan 3, 1962

7.

RT

TOP HYDRANT RT STA 79+05

82.8	82.7	82.5	82.7	82.5	82.5	83.2	83.2	83.4
4.9	5.0	5.2	5.0	5.2	5.2	4.5	4.5	4.3
50	32	20	15		10	18	39	50

82.5	83.1	82.8	82.5	82.5	82.5	83.2	83.5	83.6
4.2	4.6	4.9	5.2	5.2	5.2	4.5	4.2	4.1
50	38	23	15		12	20	37	50

82.6

5.1

83.0

4.7

83.2

4.5

83.5

4.3

Top Hydrant Rt sta 79+05

STA

+

π

-

Elev.

Jan. 3, 1962

Topography

Sta 25+50 to 28+00

28

$$\frac{BT}{12 \ 12}$$

one free

$$+50 \frac{BT}{16 \ 17}$$

29

$$\frac{BT}{20 \ -20}$$

$$+47 \frac{SP}{49}$$

$$+38 \frac{PP}{70}$$

$$+36 \frac{\text{End Curb}}{56}$$

$$+14 \frac{MH}{42.5}$$

$$+55 \frac{ER}{24}$$

$$+36 \frac{BR}{44}$$

$$+46 \frac{PP}{29}$$

$$+39 \frac{18''}{46}$$

$$+36 \frac{26''}{65}$$

$$+34 \frac{18''}{49}$$

$$+19 \frac{21''}{45}$$

26

$$+89 \frac{E.R.C.}{56}$$

$$+96 \frac{Hyd}{47}$$

$$+02 \frac{MH}{20}$$

$$+93 \frac{S.P.}{50}$$

$$+00 \frac{ERC}{47}$$

$$+79 \frac{B.R.C.}{28.5}$$

$$+62 \frac{B.R.C.}{34.5}$$

$$+71 \frac{E. Island}{4}$$

$$25 + 20$$

$$34.5 + 6.5 + 1 = 27$$

Jan 3, 1962

9

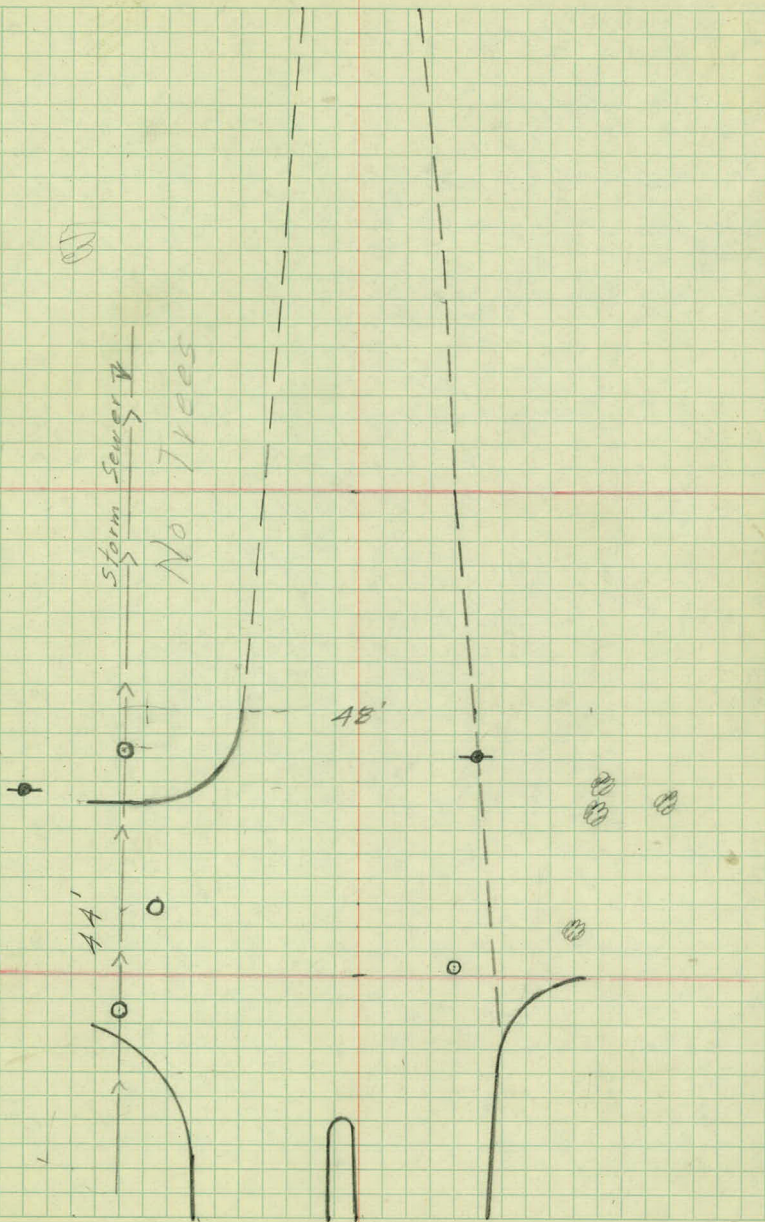
BT

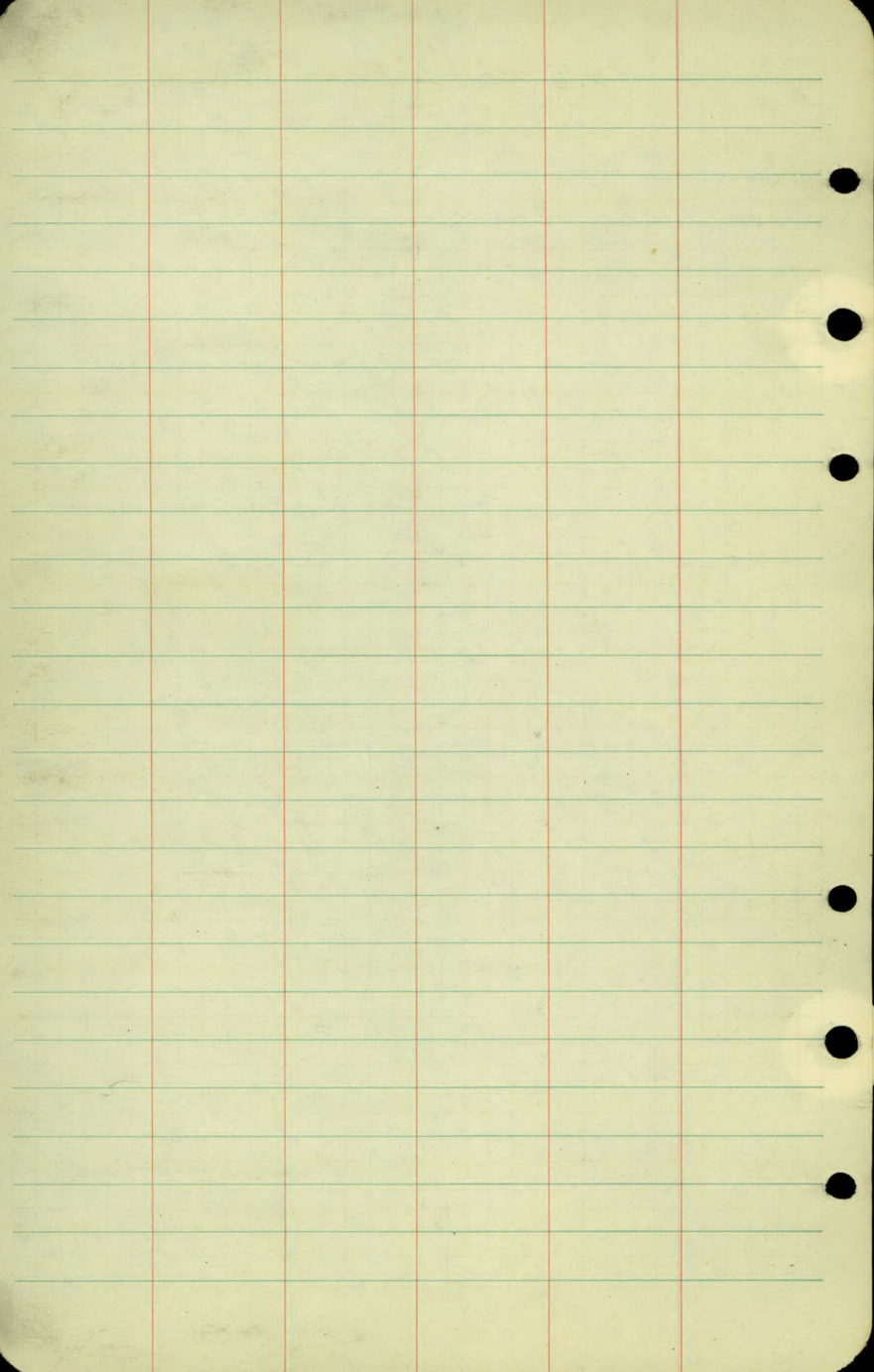
Storm Sewer

No Trees

48'

44'





Silver Lake Rd.

Additional Information

Title Pg. 1

Profiles Pg. 2

X-drain location Pg. 2

Stadia Pg. 3-

Sta	+	π	-	Elev
TBM	13.27	987.27		974.0

55+52

56+57

BM

4.05

982.2

42+54

5.6

941.8

936.2

RG
WM
FS
LB
WS

Lt

£

Jan 24, 1962
19° Overcast
PL

2

Nail & Sta 55+00

8 ^{8.8}	8 ^{7.1}	8 ^{6.2}	8 ^{4.1}	8 ^{2.1}	16 ⁹
+1.5	+0.4	1.1	2.6	5.2	10.4
175	150	125	100	63	

18 ²	19 ⁰	80 ³	81 ⁶	82 ⁶
9.1	8.3	7.0	5.7	4.7
	51	65	80	100

Top Hyd. 42R Sta 59+15 ±

Sta 42 £

Top = 33.8 - Top
8.0 = 32.6 = H.W.

Top = 34.4 - Top
7.4 = 33.0 = H.W.

26.7 17.7

15" X 44.4 CM

OBJECT

AZI

STADIA

 #1 5.36 Sta 33
 944.36

939.0

At Sta 33

to Sta 36

0°00'

to Sta 32 944.4 ✓

3.61

940.80

Lake

312°15' 348'

" 305° - 344'

" 300°20' 245'

" 303°15' 139'

" 328°20' 110'

" 329°35' 72'

" 289°20' 39'

" 222°05' 57'

" 224°50' 99'

" 227°40' 138'

" 225°35' 162'

" 226°45' 214'

" 228°00' 265'

" 229°40' 315'

DIST.

VERT.
ANGLEROD
EQUIV.

ROD

DIFF.

ELEV.₃

13.1

931.3

13.1

31.3

13.3

31.1

13.2

31.2

13.2

31.2

13.1

31.3

13.1

31.3

12.9

31.5

13.1

31.3

13.1

31.3

13.1

31.3

13.1

31.3

13.2

31.2

13.1

31.3

OBJECT	HI	HI	STADIA
X	5.23	943.9	938.7
At sta 46			
to sta 49			0°00'
to sta 45	943.91	6.31	937.6 ✓ 937.5
ES		295°45' 75	
"		215°05' 113	
"		278°55' 127	
"		235°50' 116	
E Ditch		268°35' 134	
ES		252°05' 113	
E Ditch		268°05' 158	
E Ditch		265°25' 226	
ES		269°50' 245	
"		260°05' 248	
"		272°55' 300	
"		257°55' 335	

DIST.

VERT.
ANGLEROD
EQUIV.

ROD

DIFF.

ELEV.

4

9.3

34.6

10.1

33.8

9.3

34.6

10.1

33.8

10.6

33.3

33.3

10.1

33.8

11.0

32.9

10.8

33.1

33.1

10.6

33.3

10.7

33.2

10.3

33.6

10.2

33.7

SWAMP

WEST OF ROAD

OBJECT

AZ

STADIA

HI
5,26

A+Sta 49

943.9

to Sta 46

949.2 180°00'

to Sta 50

1,46

ES

199°00' 96

EDGE
FENCE

204°30' 95

ES

223°45' 104

"

224°20' 145

"

236°05' 176

"

249°00' 205

ES

252°30' 281

"

257°40' 309

"

301°30' 223

"

279°35' 147

"

257°30' 141

"

265°35' 89

"

292°40' 101

321°20' 146

DIST	VERT ANGLE	ROD EQUIV.	ROD	DIFF	⁵ ELEV.
------	---------------	---------------	-----	------	-----------------------

			9.4		39.8
--	--	--	-----	--	------

			8.6		40.6
--	--	--	-----	--	------

			9.0		40.2
--	--	--	-----	--	------

			8.8		40.4
--	--	--	-----	--	------

			9.5		39.7
--	--	--	-----	--	------

			9.5		39.7
--	--	--	-----	--	------

			9.2		40.0
--	--	--	-----	--	------

			9.5	continues N.W.	39.7
--	--	--	-----	----------------	------

			8.9		40.3
--	--	--	-----	--	------

			9.1		40.1
--	--	--	-----	--	------

			9.4		39.8
--	--	--	-----	--	------

			8.3		40.9
--	--	--	-----	--	------

			8.7		40.5
--	--	--	-----	--	------

			9.2		40.0
--	--	--	-----	--	------

OBJECT

AZ

STADIA

ES

325°25' 215

11

326°10' 278

11

337°15' 285

Fe. Con

351°35' 293

Fence

346°05' 177

ES

337°05' 83

ES

268°45' 28

SWAMP EAST OF ROAD

ES.

161°50' 117

11

128°55' 128

11

109°25' 150

11

84°55' 165

11

95°20' 222

11

89°25' 265

11

73°40' 245

11

58°35' 180

11

44°25' 189

11

33°05' 190

DIST	VERT. ANGLE	ROD EQUIV.	ROD	DIFF	5 ELEV
			9.3		39.9
			7.6		41.6
			6.5		42.7
			2.2		47.0
			9.6		39.6
			10.0		39.2
			10.0		39.2
			8.9		40.3
			10.7		38.5
			10.5		38.7
			10.9		38.3
			10.9		38.3
			11.1		38.1
			11.1		38.1
			10.8		38.4
			9.6		39.6
			8.1		41.1

OBJECT

AZ

STADIA

Fen Line

12°10' 174

"

17°40' 120

"

62°35' 41

6

DIST	VERT. ANGLE	ROD EQUIV.	ROD	DIFF	ELEV.
------	----------------	---------------	-----	------	-------

5.9

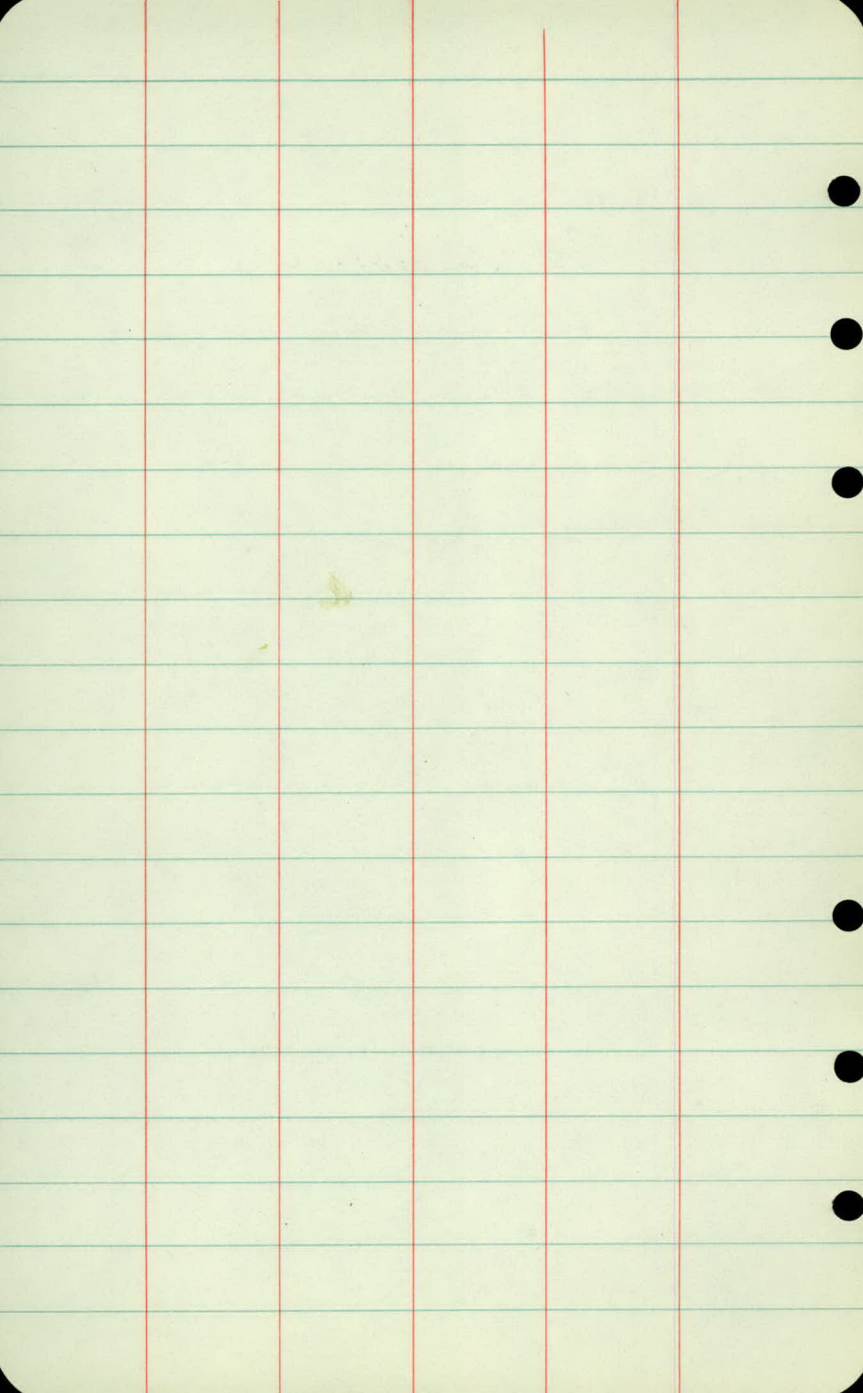
43.3

8.8

40.4

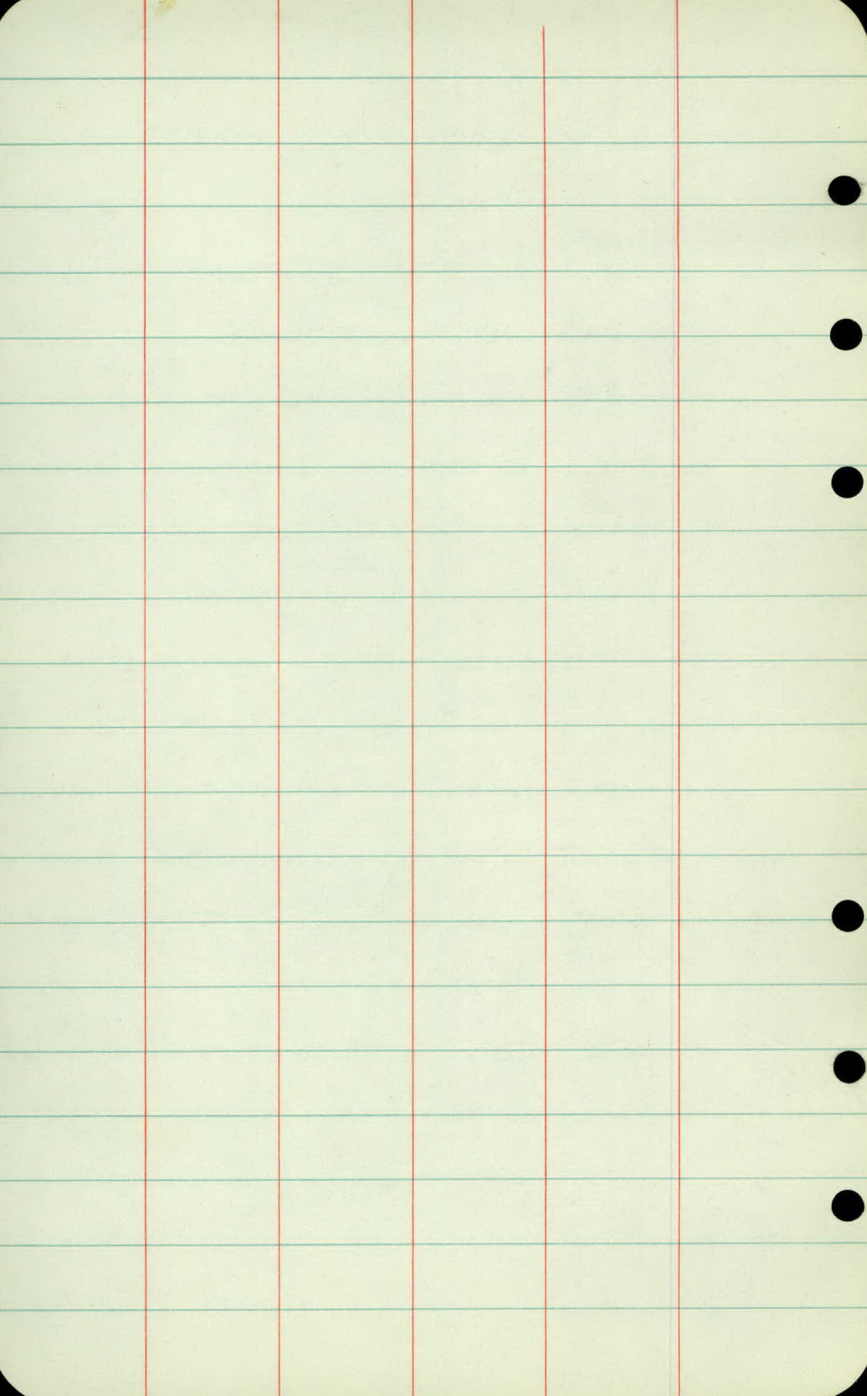
11.4

37.8



Culvert location. $\frac{1}{2}$
flow line elev.

Sta	+/-	π	-	Elev
		950.08		
TBM	7.78	934.52	7.78	942.3
				943.8 $\checkmark$
TBM		937.53	6.27	943.8 $\checkmark$
29+94			8.48	41.6
29+85			8.28	41.8



RG
WM
FS
RB
LB
DS
WS

Jan 26, 1962
Windy Clear 20°

Silver Lake Rd.

Additional Stadia

OBJECT

AZI

STADIA

HI 5.24

At Sta 40

to Sta 36

180°00'

to Sta 41

Lake Shore

222°50' 289 ✓

"

263°35' 420 ✓

"

264°45' 366 ✓

"

219°10' 460 ✓

"

268°30' 307 ✓

"

220°30' 540 ✓

"

266°20' 261 ✓

~~to Sta 39~~

217°20' 540 ✓

"

254°35' 239 ✓

"

244°25' 238 ✓

"

223°20' 289

GE

269°35' 235

"

272°25' 219

4 Rd

252° - 89

CNE

275°45' 136

DIST.

VERT.
ANGLEROD
EQUIV.

ROD

DIFF.

ELEV.

Jan 26, 1962

5.93

11.1

11.1

11.1

11.2

11.1

11.1

11.1

11.2

11.0

11.1

11.1

9.4

7.8

6.5

6.1

OS.
OBJECT

AZI

STADIA

G.E. 274°15' 190

Q Rd. 287°15' 208

G.E. 287°50' 151

Q Rd. 293°40' 285

E.S. 294°15' 142

" 301°30' 135

" 321°40' 204

" 333°20' 263

" 342°55' 335

" 346°10' 345

" 349°15' 390

DIST.

VERT.
ANGLEROD
EQUIV.

ROD

DIFF.

ELEV.

7.0

4.9

6.2

5.4

9.3

10.5

9.6

9.5

9.4

9.2

8.7

OBJECT	AZI	STADIA	Rod Man
		HZ. 5.30	
AT Sta 46			
To Sta 50		360°-	
To Sta 47			
E.S.	257°-	380	✓
"	276°40'	330	✓
"	258°45'	440	✓
"	278°30'	375	✓
"	260°-	510	✓
"	283°35'	440	✓
"	260°45'	580	✓
"	260°50	630	
"	280°50'	615	
"	258°50'	615	
"	275°55'	645	
"	258°15'	580	
"	267°55'	655	
"	263°55'	640	
"	260°35'	680	

DIST.

VERT.
ANGLEROD
EQUIV.

ROD

DIFF

ELEV

3.60

10.1

10.3

10.7

10.9

10.2

10.1

10.5

11.0

9.9

10.6

10.9

10.7

10.7

11.3

11.1

OBJECT	AZI	STADIA
Top E. End 21' C.M.	260°35'	680
E.S.	258°40'	655
"	255°50'	630
Top W End 21' G.M.	259°55'	700
E.S.	251°30'	600 ✓
"	252°30'	570 ✓
Ditch E	257°40'	550 ✓
"	256°40'	495 ✓
"	255°15'	425 ✓
"	254°30'	360 ✓
"	253°25'	305 ✓
"	252°20'	260 ✓
"	250°45'	213 ✓
"	243°35'	172 ✓
"	234°45'	175 ✓
"	228°30'	183 ✓
"	215°00'	217
"	208°40'	257

DIST.

VERT.
ANGLEROD
EQUIV.

ROD

DIFF.

ELEV.

9.5

10.9

10.6

9.45

11.0

11.2

10.4

10.7

10.4

10.4

10.2

10.1

8.9

7.5

7.2

6.4

5.2

5.5

OBJECT

AZI

STADIA

E

Ditch

203°55' 310

||

201°00' 290

||

199°15' 440

DIST.

VERT.
ANGLEROD
EQUIV.

ROD

DIFF.

ELEV.

7.7

9.0

9.8

OBJECT

AZI

STADIA

EG
WM
FS
LB
RB
DS
WS

Jan 29, 1962

Silver Lake Rd

Lake shore locations by Stadia

(3rd Set)

OBJECT	AZI	STADIA	Rodman
	415.29		F.S.
At Sta 32			
to 36		0°00'	
to 34			
L.S.	348°30'	180	F.S.
"	342°40'	210	F.S.
"	326°10'	213	"
"	317°5'	301	"
"	318° -	417	"
"	320°25'	518	✓ "
"	324°40'	537	"
"	329°50'	518	"
"	332°50'	515	"
"	335°35'	535	"

DIST.

VERT.
ANGLEROD
EQUIV.

ROD

DIFF.

ELEV.

Z

6.88

-1°

11.8

"

11.0

"

11.4

"

9.9

"

7.7

"

5.9

"

5.7

"

6.0

"

5.9

"

5.7

OBJECT	AZI	STADIA
	415.30	Rd & road
AT Sta. 41		
To Sta 43		0°00'
To Sta 40		
L.S.	208°5'	⁴¹⁹⁸ 239X2 F.S.
	213°45'	370 W.M.
	222°15'	314 "
	233°45'	288 "
	245°40'	306 "
	248°55'	343 "
	251°55'	420 "
to Rd	276°55'	287 "
"	271°35'	252 "
"	263°45'	218 "
"	254°20'	189 "
"	242°20'	167 "
"	226°35'	154 "
"	202°30'	164 "

DIST.

VERT.
ANGLEROD
EQUIV.

ROD

DIFF.

ELEV.

4.60

10.5

10.6

10.6

10.5

10.6

10.5

10.5

5.0

4.6

4.7

4.9

5.6

5.9

6.1

OBJECT

AZI

STADIA

Additional X-section

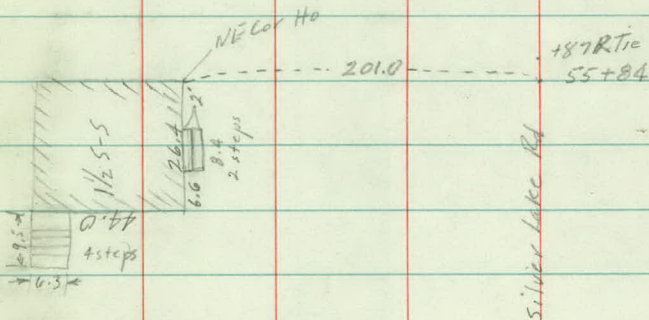
Notes

Silver Lake Road

11 pages

House Location

E



Sta	+	π	-	Elev.
B.M.	9.24	972.04		962.80
52+66				
+77				
53+00	Ent. Rt.			
+13				
+43				

RG
WM
RB
LB
DS

Jan 30, 1961 2

E

RT

Top of Hyd. NE Cor Silver Lake Rd & Co Rd "E"

✓ 61.3 61.4 61.4 61.2 60.69 60.06 54.68
10.7 10.6 10.6 10.8 11.35 11.98 12.36
5 17 24 35 70 100
BT

✓ 61.9 62.0 62.0 62.1 61.3 60.79 60.63 60.38
10.1 10.0 10.0 9.9 10.7 11.25 11.41 11.66
5 16 21 34 56 79 100
BT Conc Conc

✓ 63.2 63.3 63.2 62.9 62.2 62.3 61.39 61.12 60.71
8.8 8.7 8.8 9.1 9.8 9.7 10.65 10.92 11.33
6 16 22 29 34 52 79 100
BT Conc

✓ 63.9 63.9 63.8 63.5 62.5 61.76 61.59 61.23 61.01
8.1 8.1 8.2 8.5 9.5 10.28 10.45 10.81 11.03
6 17 23 43 54 70 91 100
BT Conc

✓ 65.5 65.5 65.3 65.2 63.6 63.8 62.60 62.02 61.48
6.5 6.5 6.7 6.8 8.4 8.2 9.44 10.02 10.56
7 18 22 31 35 55 72 91
BT Conc

61.55 61.48
10.49 10.56
95.98 95
Bldg

Sta	+	π	-	Elev
-----	---	-------	---	------

		972.04		
--	--	--------	--	--

+69				
-----	--	--	--	--

54+00	Ent. Rt.			
-------	----------	--	--	--



+30				
-----	--	--	--	--

	Not Disturbed			
--	---------------	--	--	--

BM				
----	--	--	--	--

		9.24	962.80	
--	--	------	--------	--

Jan 30, 1962

3

✓

	66.7	66.9	66.6	65.8	64.5	63.98	63.15	61.8
5.3	5.1	5.4	6.2	7.5	8.06	8.89	10.2	
6	17	26	42	54	67	91		
			BT		conc			

✓

	68.4	68.6	68.4	68.0	67.4	71.2	72.0	74.3	73.0
3.6	3.4	3.6	4.0	4.6	0.8	0.0	+2.3	+1.0	
8	19	24	30	41	43	53	69		

68.6	69.3
3.4	2.7
100	88

Sta	+	π	-	Elev.
BM	2.74	987.67		984.93
78+35				
+45				
+57				
+75				
79				
+50				
+92				
80				
+59				

Jan 30, 1962

Lt

±

Rt

4

Top Hyd. Rt 79405

83.3

4.4

13

83.4

4.3

13

83.4

4.3

13

83.1

4.6

13

83.0

4.7

13

82.8

4.9

12

83.1

4.7

12

83.1

4.6

12

83.3

4.4

12

83.1

4.0

83.6

4.1

83.6

4.1

83.6

4.1

83.2

4.5

83.1

4.6

83.1

4.6

83.1

4.6

83.3

4.4

83.3

4.4

14

83.4

4.3

14

83.4

4.3

14

83.2

4.5

14

83.1

4.6

14

82.7

5.0

15

83.0

4.7

15

83.0

4.7

15

83.0

4.7

15

Sta	+	π	-	Elev
-----	---	-------	---	------

		987.67		
--	--	--------	--	--

+96				
-----	--	--	--	--

81 +00				
--------	--	--	--	--

+08				
-----	--	--	--	--

+50				
-----	--	--	--	--

TP	6.63	991.29	3.01	984.66
----	------	--------	------	--------

+73				
-----	--	--	--	--

+80				
-----	--	--	--	--

82				
----	--	--	--	--

+50				
-----	--	--	--	--

Jan 31, 1962

Lt £ Rt 5

83.4

4.3

13

83.4

4.3

13

83.4

4.3

13

83.1

4.0

12

83.5

4.2

83.5

4.2

83.6

4.1

83.8

3.9

83.4

4.3

14

83.4

4.3

14

83.5

4.2

14

83.1

4.0

14

Top prep iron Rt Sta 81

83.9

7.4

13

84.0

7.3

13

84.1

7.2

13

85.1

6.2

13

84.0

7.3

13

84.1

7.2

13

84.3

7.0

13

85.1

6.2

13

83.8

7.5

14

84.0

7.3

14

84.2

7.1

14

85.0

6.3

14

Sta	+	π	-	Elev
-----	---	-------	---	------

		991.29		
--	--	--------	--	--

83+00				
-------	--	--	--	--

TP	7.38	996.17	2.50	988.79
----	------	--------	------	--------

+50				
-----	--	--	--	--

84				
----	--	--	--	--

+50				
-----	--	--	--	--

85				
----	--	--	--	--

+22				
-----	--	--	--	--

+69				
-----	--	--	--	--

86				
----	--	--	--	--

RG
WM
LB
WS

Jan 31, 1962
Clear 10°

Lt

E

Rt

6

85.7

5.6

13

85.8

5.5

85.7

5.6

14

✓

Nail in Trans. Pole Rt. Sta 84+15

86.2

10.0

13

86.4

9.8

86.3

9.9

14

✓

87.1

9.1

13

87.2

9.0

87.0

9.2

14

✓

88.0

8.2

13

88.0

8.2

88.0

8.2

14

✓

88.6

7.6

13

88.7

7.5

88.5

7.7

14

✓

88.9

7.3

13

89.0

7.2

88.8

7.4

14

✓

89.7

6.5

13

89.7

6.5

89.6

6.6

14

✓

90.1

6.1

13

90.1

6.1

90.0

6.2

14

✓

sta	+	π	-	Elev
		$\leftarrow$ 996.17		
+31				
+50				
+80				
87				
+50				
88				
+50				
89				
+41				
TP	2.83	997.41	1.59	994.58

Jan 31, 1962

Clear 10°

7

Lt.

E

Rt.

90.5

5.7

12

90.9

5.3

12

91.3

4.9

12

91.6

4.6

12

92.2

4.0

12

92.8

3.4

11

93.1

3.1

11

93.2

3.0

11

93.1

3.1

12

90.6

5.6

12

90.9

5.3

12

91.4

4.8

12

91.7

4.5

12

92.3

3.9

12

92.8

3.4

12

93.1

3.1

12

93.2

3.0

12

93.2

3.0

12

90.6

5.6

14

90.8

5.4

14

91.2

5.0

14

91.4

4.8

14

92.2

4.0

14

92.7

3.5

13

93.1

3.1

14

93.0

3.2

14

92.9

3.3

14

Top 3" Diameter Conc post by Mail Box 625 S. L. Rd

Sta	+	π	-	Elev
-----	---	-------	---	------

		997.41		
--	--	--------	--	--

+81				
-----	--	--	--	--

90				
----	--	--	--	--

+37				
-----	--	--	--	--

+68				
-----	--	--	--	--

91				
----	--	--	--	--

+15				
-----	--	--	--	--

+36				
-----	--	--	--	--

BM	0.11	990.20	7.32	990.09	990.10
----	------	--------	------	--------	--------

TP	6.22	985.37	11.05	979.15	
----	------	--------	-------	--------	--

Jan 31, 1962

8

Lt

E

Rt

92.9

4.5

12

92.9

4.5

12

92.7 ✓

4.7

14

92.9

4.5

12

92.9

4.5

12

92.4 ✓

4.8

14

92.4

4.8

12

92.7

4.7

12

92.4 ✓

5.0

14

92.5

4.9

12

92.5

4.9

12

92.3 ✓

5.1

14

92.3

5.1

12

92.1

5.3

12

92.0 ✓

5.4

14

92.1

5.3

12

91.8

5.4

12

91.8 ✓

5.6

14

91.9

5.5

12

91.8

5.6

12

91.5 ✓

5.9

14

Top Hyd NE Cor. S.L. Rd & Cemetery Rd

Nail in PP Rt. Sta. 94+45

Sta + π - E/er

985.37

94+20 Fe line

+34

+46

+85

95+00

+11

+20 $\frac{1}{2}$ 16' Ent

RF
WM
LB
DS
WS

Feb 1, 1962
Clear 100%

LT

9

✓ 90.6 89.2 86.2 82.8 81.2 81.8 81.0 81.2 81.1
+5.2 +3.8 +0.8 2.6 4.2 3.6 3.4 3.2 3.3
100 88 75 55 36 30 22 14

Fecor

✓ 88.1 83.0 81.6 81.6 81.4
+3.3 2.4 3.8 3.8 4.0
100 56 31 14

✓ 87.1 84.3 81.6 81.0 81.1 81.0
+1.7 1.1 3.8 4.4 4.3 4.4
100 68 51 34 15

✓ 86.4 83.6 80.6 79.5 79.3 74.5 79.3
+1.0 1.8 4.8 5.9 6.1 5.9 6.1
100 72 49 29 17 11

✓ 84.8 83.4 81.1 79.1 78.6 78.7
0.6 2.0 4.3 6.3 6.8 6.7
100 80 39 28 14

✓ 83.7 82.6 80.7 78.8 78.3 78.5
1.7 2.8 4.7 6.6 7.1 6.9
99 78 54 28 15
HO cor.

83.9 83.5 84.3 80.5 78.7 78.3 78.4 78.4
1.5 1.9 3.1 4.9 6.7 7.1 7.0 7.0
HO 99 87 70 50 29 20 13

Sta	+	π	-	Elev
-----	---	-------	---	------

		985.37		
--	--	--------	--	--

+50				
-----	--	--	--	--

96+00				
-------	--	--	--	--

+15	E 16' Ent Lt			
-----	--------------	--	--	--

+50				
-----	--	--	--	--

97+00	4 16' Ent			
-------	-----------	--	--	--

TP	4.77	979.83	10.31	975.06
----	------	--------	-------	--------

+31				
-----	--	--	--	--

Feb 1, 1962

Lt

E

10

✓

83.2	82.4	81.3	79.3	78.2	78.3	77.9	77.9
2.2	2.5	4.1	6.1	7.2	7.1	7.5	7.5
99	80	63	42	25	21	13	
HO							

✓

79.5	78.1	76.8	76.6	76.4	76.3
5.9	6.7	8.6	8.8	9.0	9.1
100	75	42	26	11	

79.0	78.9	88.6	77.2	76.3	76.0	76.1	76.0
6.4	6.5	6.8	8.2	9.1	9.4	9.3	9.4
115	100	89	60	32	18	10	
HO						BT	

✓

79.2	78.4	77.5	76.6	75.2	74.7	75.3	75.2
6.2	7.0	7.9	8.8	10.2	10.7	10.1	10.2
115	100	76	55	34	18	10	
HO						BT	

✓

76.9	76.1	75.3	74.2	74.0	74.4	74.5
8.5	8.7	10.1	11.2	11.4	11.0	10.9
130	100	69	33	15	9	
					BT	

✓

76.95	76.2	75.4	74.3	73.6	73.0	73.6	73.8
2.88	3.6	4.3	5.5	6.2	6.8	6.2	6.0
124	100	76	51	29	18	10	
Cons							
S.W.							

Sta	+	π	-	Elev
-----	---	-------	---	------

		979.83		
--	--	--------	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

98+00				
-------	--	--	--	--

TP	8.81	986.84	1.80	978.03
----	------	--------	------	--------

TP	13.36	992.50	7.70	979.14
----	-------	--------	------	--------

BM			2.42	990.08
----	--	--	------	--------

				990.10
--	--	--	--	--------

Feb 1, 1962

£

11

LT

✓

76.7	76.2	75.5	74.1	72.7	72.4	73.0	73.3
3.1	3.6	4.3	5.7	7.1	7.4	6.8	6.5
124	100	79	52	27	17	11	
140							

✓

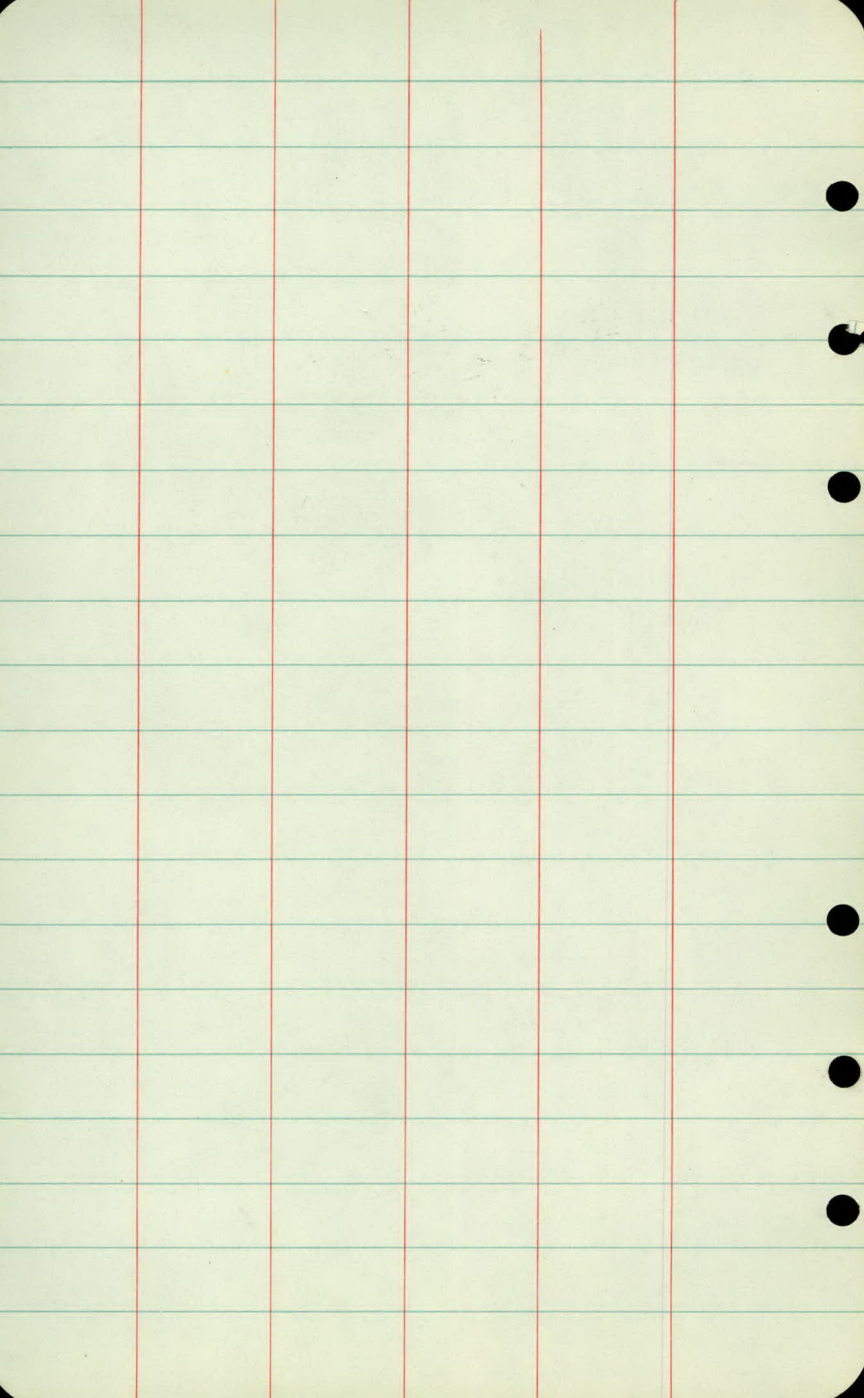
75.8	74.9	74.2	73.4	72.2	72.1	72.5	72.5
4.0	4.9	5.6	6.4	7.6	7.7	7.3	7.3
124	100	69	51	27	17	11	

✓

72.5	72.3	72.0	71.7	71.5	72.0	71.9
7.3	7.5	7.8	8.1	8.3	7.8	7.9
100	69	49	28	17	11	

Nail in PR Rt Sta 94+45

Top Hyd. NE Cor S.L. Rd & Cemetery Rd



Stadia
Silver Lake Road
& Misc.

4 pages

Swamp Location

OBJECT	AZ	STADIA
Sta 42	941.6	936.2
to 47		0°00'
to Sta 43		936.6
to Sta 44		
ES	6°20'	374
"	19°10'	362 ✓
"	26°55'	304 ✓
"	35°30'	203 ✓
"	50°50'	184 ✓ ✓
"	77°00'	203 ✓ ✓
"	102°45'	203 ✓ ✓
"	123°15'	247 ✓ ✓
"	141°30'	283 ✓ ✓
Fe	147°15'	330 ✓
Ge	150°20'	410
"	153°40'	485 ✓
ES	150°40'	283
"	171°25'	262

126

WADIST.

VERT.

ANGLE

ROD

EQUIV.

ROD

Feb 7, 1962

DIFF.

ELEV.

2

FS

RB

LB

DS

WS

4.96

936.64

4.38

37.22

8.2

33.4

8.0

33.6

8.0

33.6

8.2

33.4

8.3

33.3

8.1

33.5

8.2

33.4

8.2

33.4

8.2

33.4

7.9

33.7

7.3

34.3

6.2

35.4

8.4

33.2

8.3

33.3

Profile of Proposed Ditch & Culvert

OBJECT	AZ	STADIA
HI: 941.6		
Sta 42		0°00'
Sta 43		
Sta 46		0°00'
to & prop. culvert	215°16'	
& (0+00) S.L. Road	1.50	
0+18		
0+57		
1+00		
1+38		
1+78		
2+00		
2+22		
2+30 & Rd.		
2+38		
2+61		
3+00		
3+18		
3+34		
3+46		
3+68 Lake		

Feb 7, 1962

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

3

4.96

936.64

5.3

36.3

5.53

36.07

9.7

31.9

9.1

32.5

8.9

32.7

9.6

32.0

8.5

33.1

5.6

36.0

5.4

36.2

5.7

35.9

3.5

38.1

4.1

37.5

4.4

37.2

6.3

35.3

8.8

32.8

10.4

31.2

OBJECT

AZI

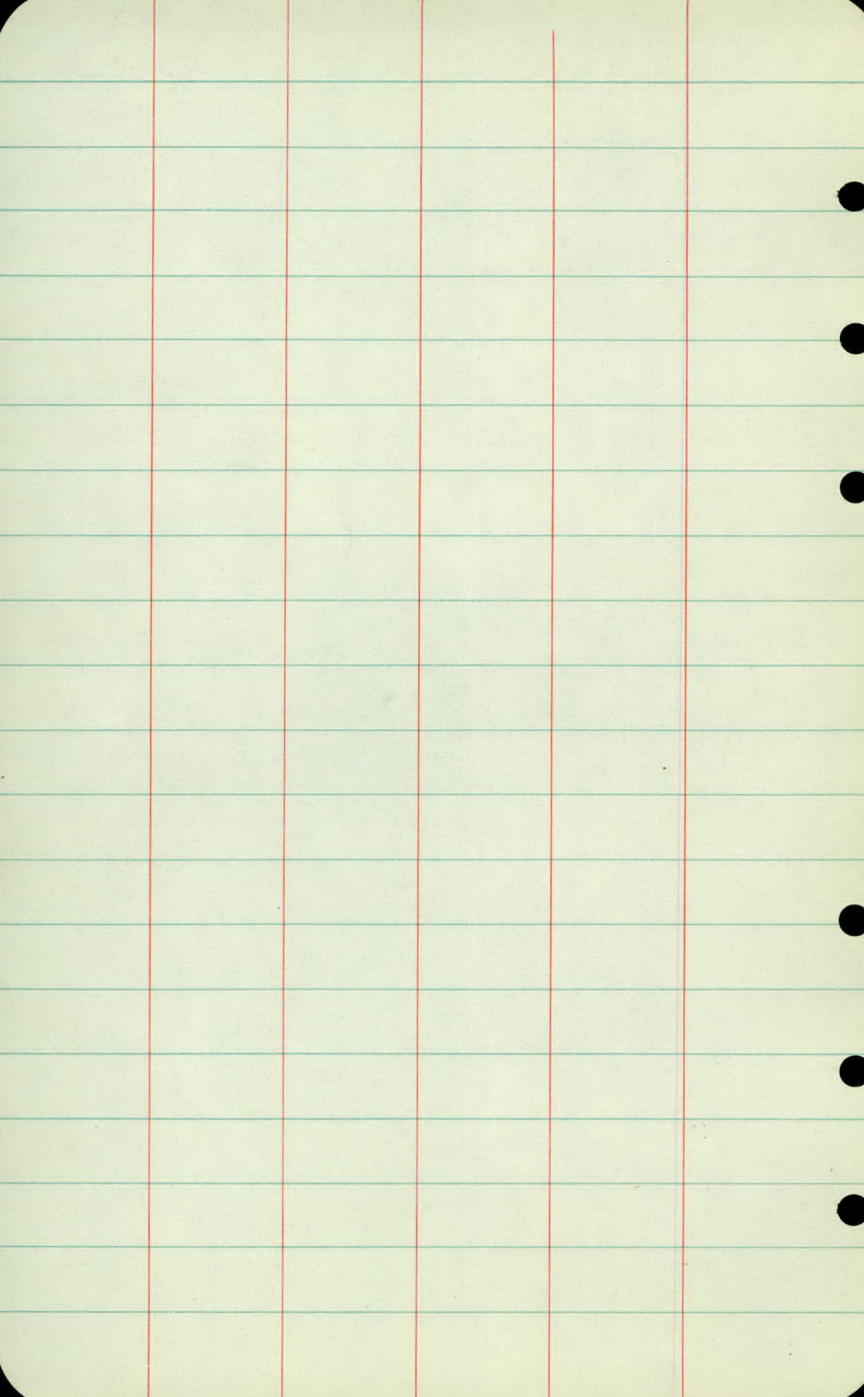
STADIA

Feb. 7, 1962

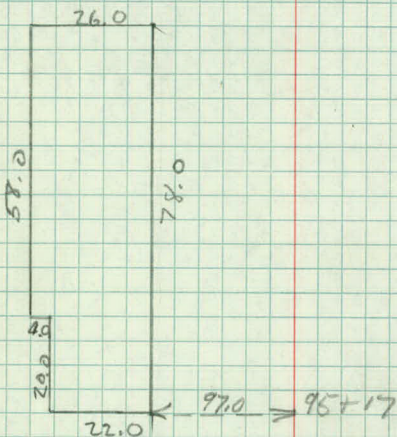
Elevation of Driveway 4 at House 203' Lt Sta 55+50 Silver Lake Rd

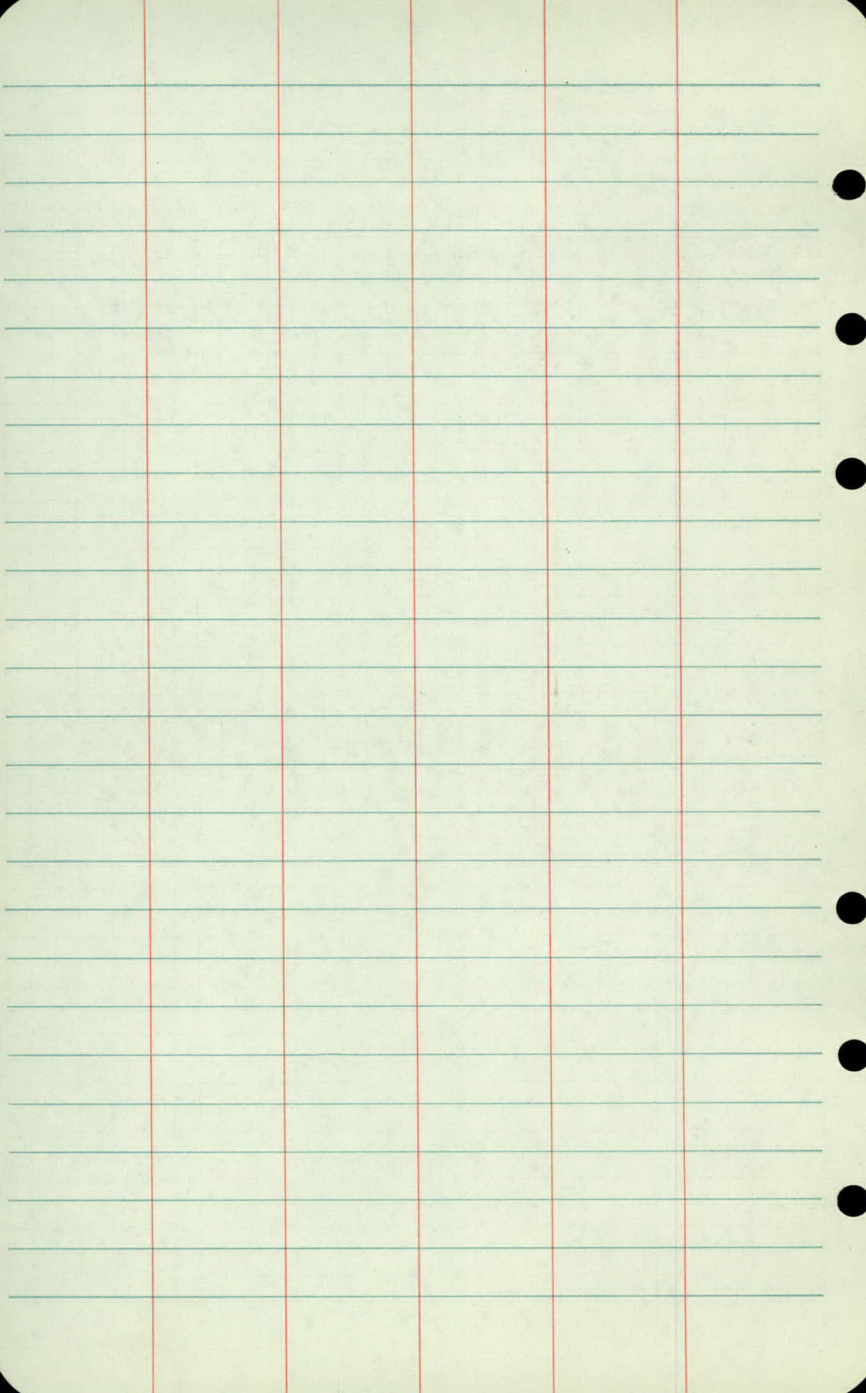
Sta	+	π	-	Elev	
BM 55 &	13.37	987.4			974.0
TP driveway 55+50	5.32	992.7	0.04	987.4	
			3.0	989.7	203' Lt
TP	1.55	981.6	12.65	980.0	
BM Sta 55 &			7.69	974.0	974.0

Prop line = 55+24

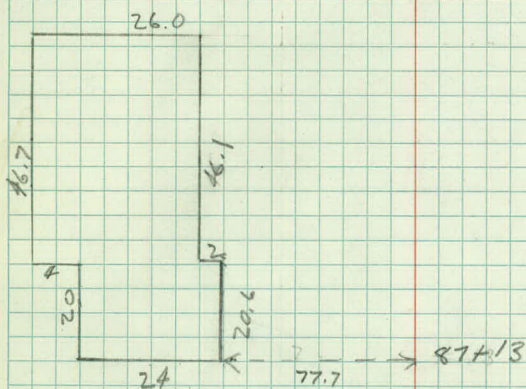


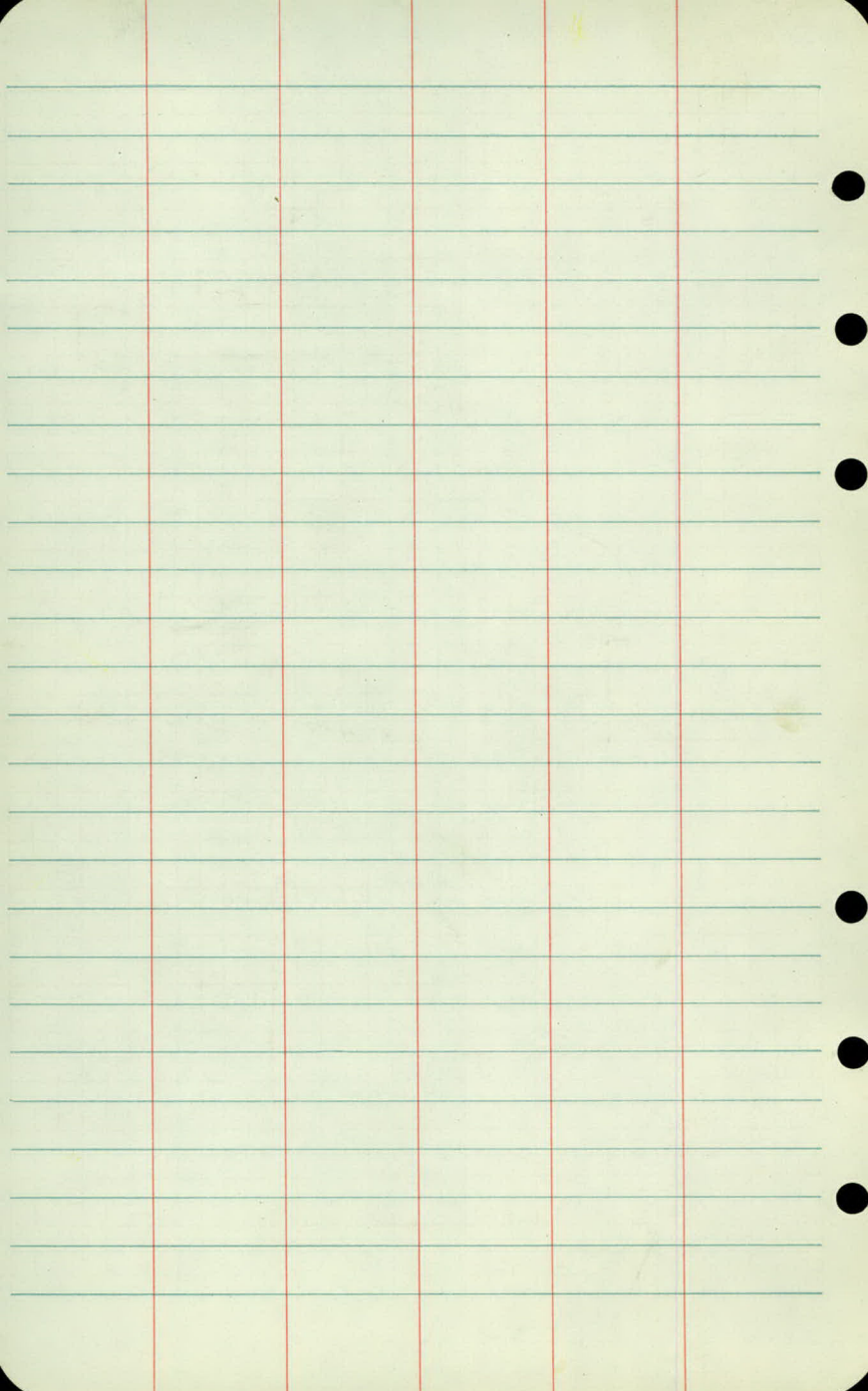
£
Silver Lake Rd





2
Silver Lake Rd





RG
WM
RB
WS

March 5, 1962
Cold, clear

1

Silver Lake Rd.

Curb Elevations

Sta. 26+37 - 46' $\frac{1}{2}$ 50' $\frac{1}{4}$.

Sta	+	π	-	Elev
BM ₁	4.01	946.28		942.27
26+46			4.30	941.98
"			4.91	
"			4.28	942.-
"			4.84	
BM ₁			4.01	
BM ₂			0.57	

March 5, 1962

2

Spike in 24" Oak Rt. Int. Silver Lake Rd $\frac{1}{2}$ Silver Lane

Top carb 46' Lt

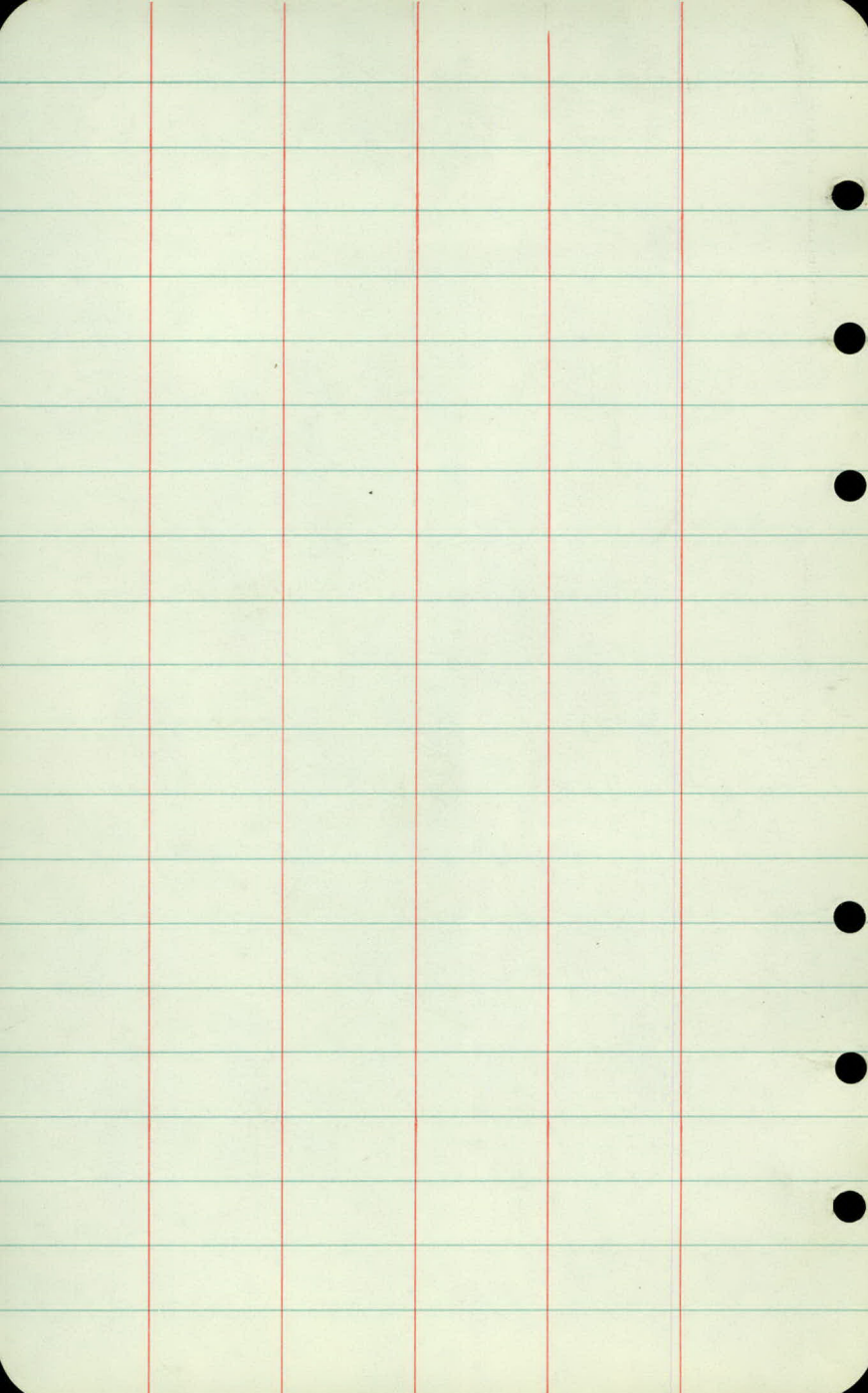
Bottom " "

Top Carb 50' Lt

Bottom " "

Top Hyd SW Cor Silver Lake Rd $\frac{1}{2}$ Silver Lane

0.1 Diff than
1962 Const



Swamp Exc.

Silverlake Road

32+75 to 33+50

x section

Sta + π - elev

BM. 0.412 943.39

942.97

32+50

32+75

33+00

33+50

34+00

0.412 942.97 942.97

Lt

C

~~LT.~~
~~RT~~

S.W. corner Lower step Ho. # 34+26

Natural Ground

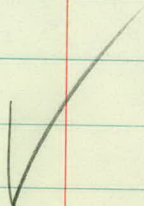
	29.9	29.5	
N.G.	13.5	13.9	W.S.
13	22	38	50

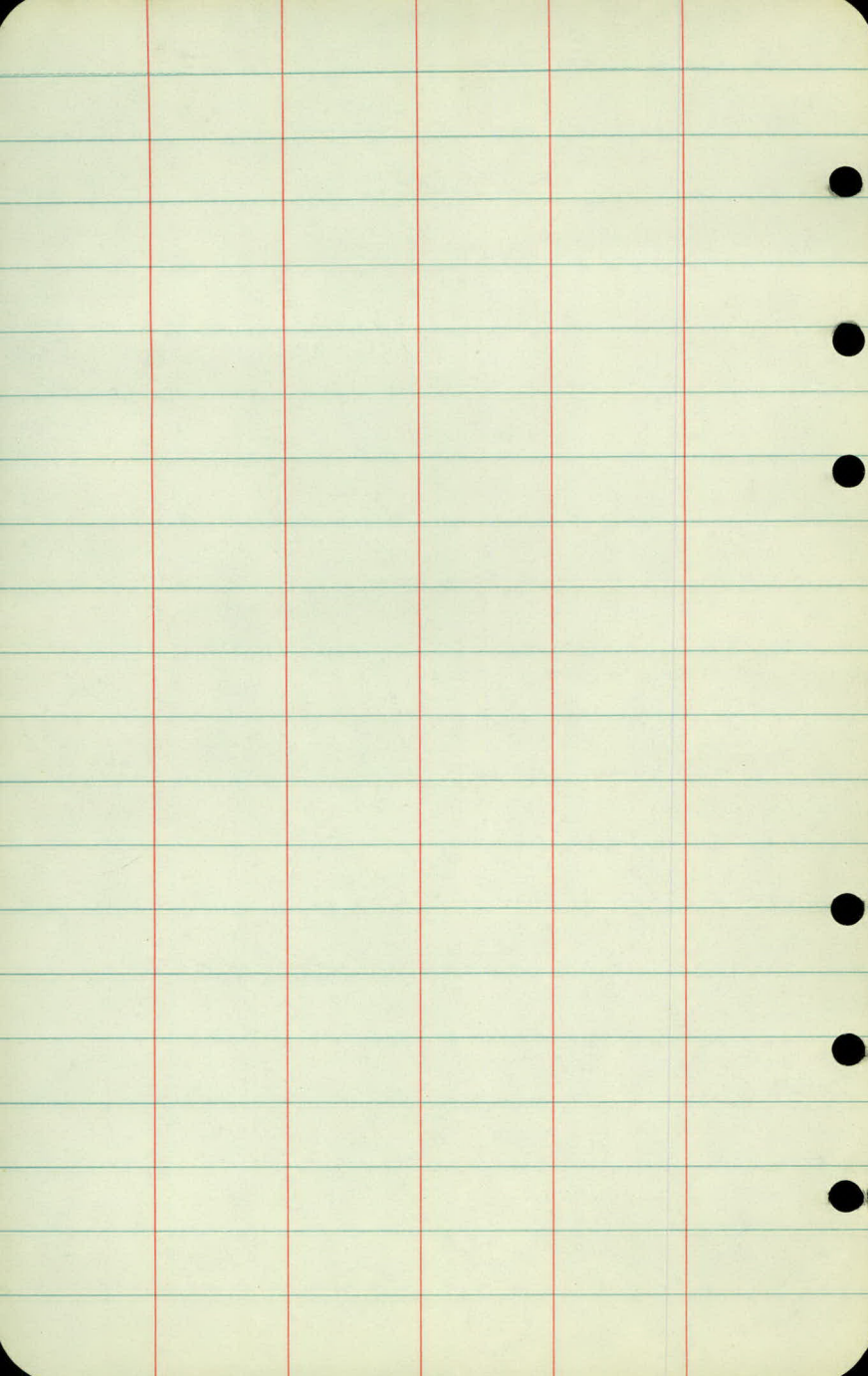
	29.2	29.7	
N.G.	14.2	13.9	W.S.
14	24	39	50

	29.6	29.4	
N.G.	13.8	14.0	W.S.
15	25	39	50

Natural Ground

S.W. corner lower step Ho. # 34+26





Silverlake Road

Swamp Excavation

44 + 50 to 45 + 50

x sections

Sta	+	π	-	elev
-----	---	-------	---	------

B.M.	0.12	940.70		
------	------	--------	--	--

940.58

45+50

45+00

44+50

0.12

940.58

940.58

Lt

L

Rt

Spike in 10" ELM 140' Lt Sta 43+80

28.5	28.1	29.2	
12.2	12.3	12.5	NG.
6		27	29.5



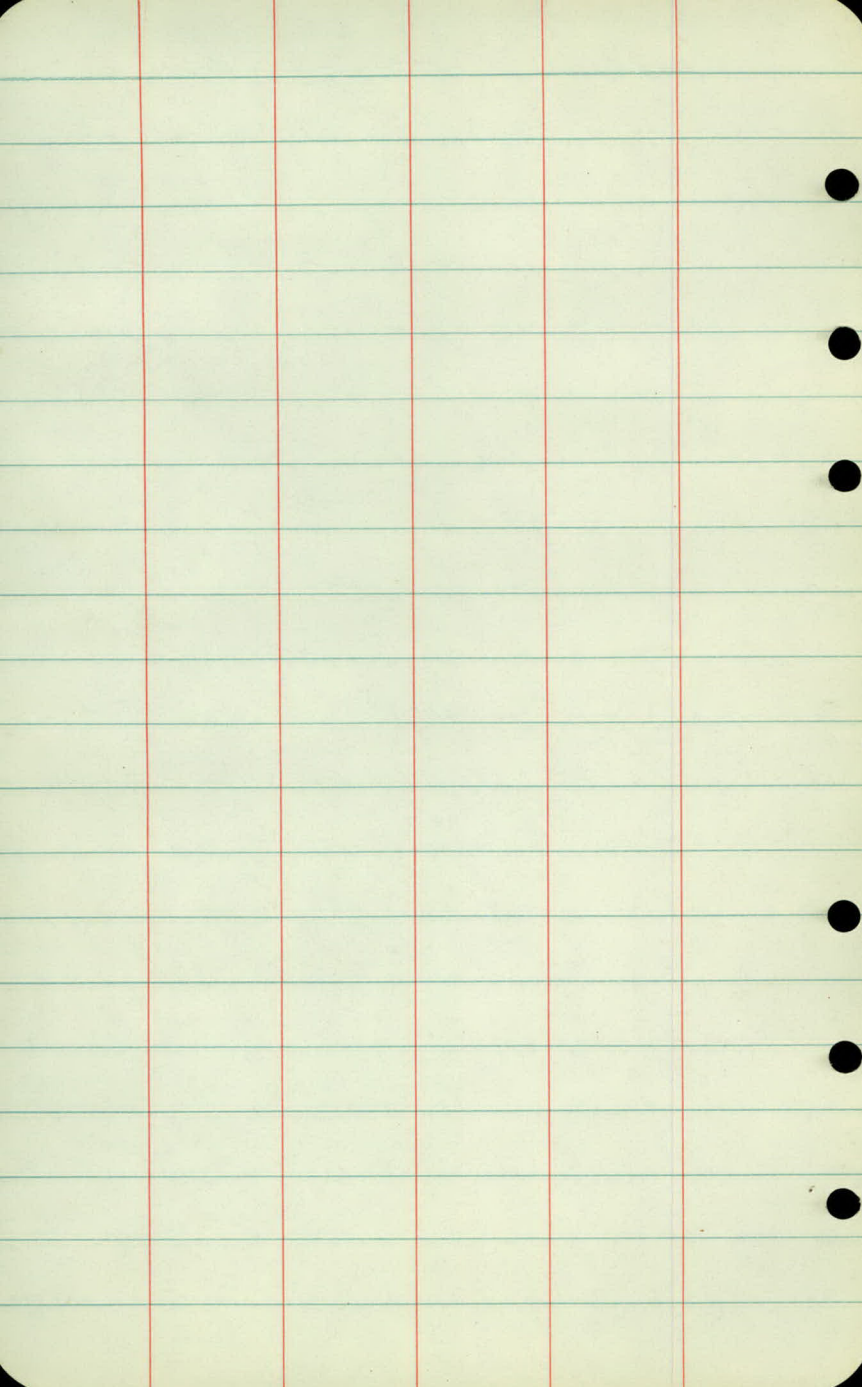
27.3	27.1	26.9	
27.3	13.6	13.8	NG
5		33	36



27.9	27.6	
12.8	13.1	NG
	40.5	42.5



Spike in 10" ELM 140' Lt Sta 43+80



14 JUNE 1962

SILVER LAKE RD

62-644-03

Swamp Excavation X-SECTIONS

39+00 to 46+50

Sta	+	π	-	ELEV
BM	4.68	945.26		(940.58)
B.M.	2.28	937.37	10.17	935.09

45+00 Lt only

44+50 Lt. only

T.P. 10.70 945.80 2.27 935.10

B.M. 5.23 940.57 (940.58)

B.M. 0.54 941.12 940.58

T.P. 1.55 936.59 6.08 935.04

44+00

43+50 Rt. only

19 JUNE 1962

Lt

F

Rt

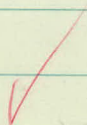
SPIKE IN 10" ELM 140' LT STA 43+80

Top Slope-stake sta 46+00

33.1	29.5	27.7
4.3	7.9	9.7
47	44	22



33.9	31.3	30.4	28.6
3.5	6.1	7.0	8.8
45	40	27	10



Top slope stake sta 46+00

Spike in 10" ELM 140.0' Lt sta 43+80

" " " " " " " "

Top stake 20' Lt sta 43+50

33.9	30.6	29.8	27.2	26.1	31.9
2.7	6.0	6.8	9.4	10.5	4.7
45	38	20		41	44



26.6	25.5	31.3
10.0	11.1	4.3
	41	44.5



sta + π - elev

936.59

43+00 Rt only

T. P. 2.34 937.39 1.54 935.05 (935.04)

42+50 Rt only

T. P. 7.64 941.68 3.35 934.94

B.M. 1.08 940.60 (940.58)

B.M. 0.63 937.01 (936.38)

43+50 Lt only

43+00 Lt only

42+50

B.M. 0.64 936.37 (936.38)

Lt

L

Rt

26.1
10.526.0
10.6
4.332.2
4.4
4.8

Top of stake 20' Lt sta 43+50

26.0
11.424.5
12.9
4.432.5
4.9
4.95

Top of iron pipe 35' Lt sta 42+85

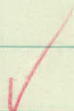
Spike in 10" Elm 140.0' Lt sta 43+80

Top TCH Breather Pipe Lt sta 40+35-

33.6	28.4	28.2	27.8
3.4	8.6	8.8	9.2
4.4	4.0	2.3	1.6



32.3	28.1	27.5	26.3
4.7	8.9	9.5	10.7
4.0	3.6	2.0	1.6



32.2	26.8	26.2	25.4
4.8	10.2	10.8	11.6
4.1	3.8	2.2	1.2



Top T.C.A. Breather Pipe Lt sta 40+35-

Sta + π - elev

B.M. 0.06 936.44 936.38

42+00 Lt only

41+50 Lt only

42+00 Rt only

B.M. 0.14 936.52 0.06 936.38 936.38

41+50 Rt only

41+00 Rt only

B.M. 0.16 936.36 936.38

Lt

L

Rt

Top T.C.A Breather Pipe Lt sta 40+35

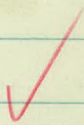
33.0	26.2	24.0	26.0	24.1
3.4	10.2	9.4	10.4	12.3
40	38	19	13	



32.9	26.9	26.4	26.3	25.1
3.5	9.5	10.0	10.1	11.3
41	38	20	15	



25.0	33.0
11.4	3.4
42	47



Top T.C.A Breather Pipe Lt sta 40+35

25.3	31.4
11.2	5.1
41	46



25.3	24.8	24.8	32.2
11.2	11.7	11.7	4.3
41	40	40	47



Top T.C.A. Breather Pipe Lt sta 40+35

Sta + π - elev

0.09 936.117

936.38

40+50 Rt only

+25'
40+00

B.M. 0.30 936.68 0.09 936.38 936.38

39+50 Lt only

41+00 Lt only

T.P. 6.64 941.50 1.82 934.86

B.M. 2.14 938.76 938.72

Lt

L

Rt

Top T.C.A. Breather Pipe Lt sta 40+35

24.6

25.0

33.5 ✓

11.9

11.5

3.0

40

43.

26.1

27.4

26.5 ✓

33.5

10.6

9.1

10.0

3.0

18

42

48

Top T.C.A. Breather Pipe Lt sta 40+35

2

28.1

27.8

27.1

34.3

8.6

8.9

9.0

2.4 ✓

24

42

47

33.0

25.5

26.5

3.7

11.2

10.2

43

39

22

Top N.W. Cor T.C.A. M.H Lt Sta 40+35

Spike in 24" OAK 75.0' Lt Sta 39+15

Sta	+	π	-	elev	
B.M.	1.72	940.44	7.47	932.97	938.72
	4.02	936.99			

40+50 Lt only

40+00 Lt only

T.P	7.45	942.24	2.20	934.79	
B.M.	1.32	940.04	3.52	938.72	938.72

39+50

39+00

	1.32	938.72	938.72
--	------	--------	--------

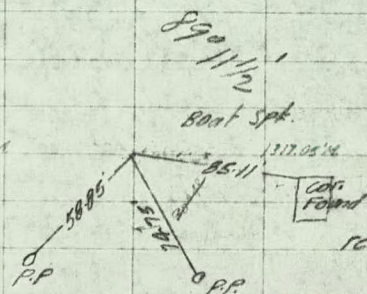
25 + 57.54 P.O.T.

10 + 00 P.O.T.

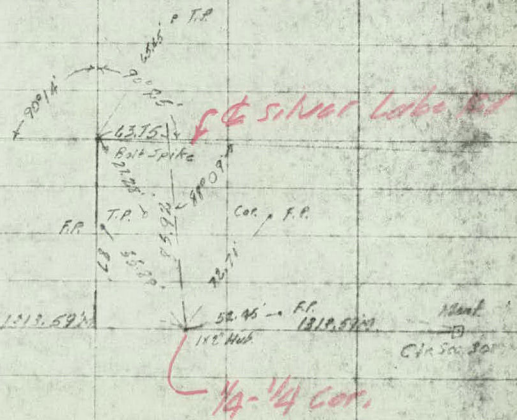
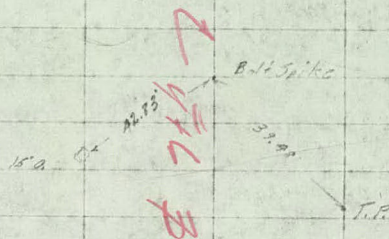
0 + 00 = 1/4 Friedland Ave.

Mont
11.650.30

1317.05' M



Mont 1317.05' M



Mont
11.650.30

1317.05' M

Mont
11.650.30

Lt

C

Rt

spike in 24" Oak 75.0' Lt sta 39+15
Rock

32.9	26.0	25.4	25.1
4.1	11.0	11.6	11.9
43	38	21	15



32.4	27.4	27.6
4.6	9.6	9.4
42	37	20



Top N.W. Cor T.C.A. M.H. Lt sta 40+35

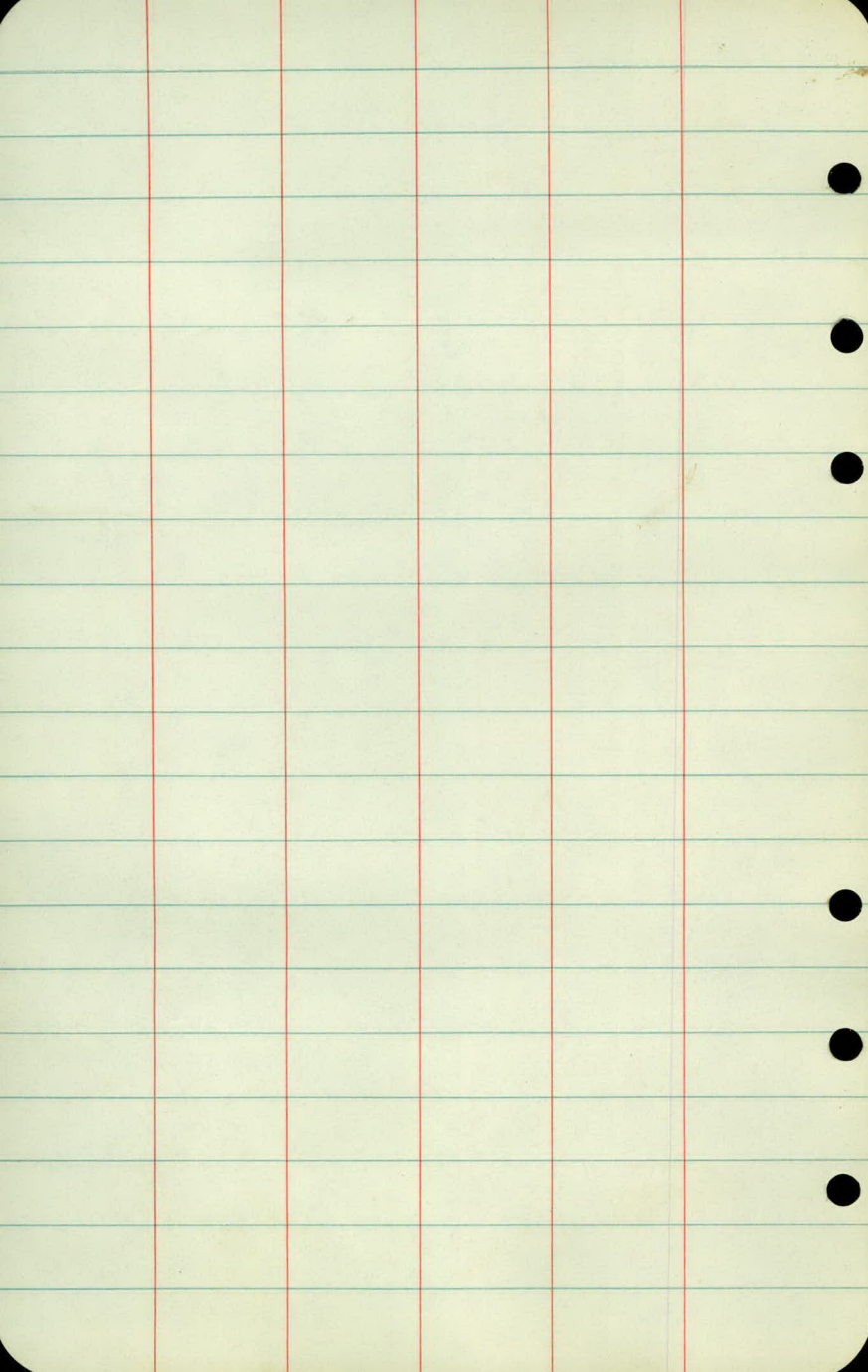
spike in 24" OAK 75.0' Lt sta 39+15

24.6	29.8	29.8	28.2	28.6	24.7
5.2	10.2	10.2	11.8	11.4	53
36	34	20		47	50



Natural Ground (Bottom of sub cut)

spike in 24" oak 75.0' Lt sta 39+15



Silverlake Rd

x sections

47+70 to 51+00

Sta + π - elev

3.80 944.38

946.58

47+00

48+00 Lt only

+30 Lt only

+60 Lt only

49+00 Lt only

+50 Lt only

Lt

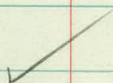
E

Rt

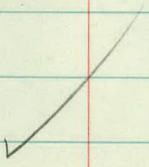
Spike in 10" ELM 140' Lt Sta 43+80

Natural Ground

40.1	39.8	36.1
3.7	5.6	7.7
33	15	
N.G.		



40.1	36.8	36.6	35.3
4.0	7.6	7.6	9.1
41	35	20	



39.2	36.4	34.9	34.8
5.2	8.0	9.5	9.6
42	39	21	



38.2	35.3	34.5	33.6
6.2	9.1	9.9	10.8
49	44	20	



38.8	35.4	34.7	33.5
5.6	9.0	9.7	10.9
51	48	22	



5/9 + π - elev

50+00 Lt only

+40 Lt only

+70 Lt only

51

Lt

E

Rt

39.0	35.9	34.6	
5.4	8.5	9.6	N6 N6
55	52	29	25



39.9	36.2	34.4	
5.5	8.2	7.0	N6
57	54	33	28



39.2	36.8	38.1	
5.2	7.6	6.3	N6
59	53	35	32



Natural Ground

Sta + π -

B.M. 3.81 944.39

940.58

49+50 Rt only

49+00 Rt only

48+60 Rt only

48+30 Rt only

48+00 Rt only

47+70 Rt only

3.81

940.58

940.58

Lt

E

Lt

Spike in 10" ELM 140' Lt sta 43+80

33.4

11.0

10

33.0

11.4

40

38.3

6.1

45



32.9

11.5

5

34.1

10.3

40

39.2

5.2

45



34.2

10.2

5

34.5

9.9

41

38.3

6.1

45



35.0

9.4

42

36.1

7.7

42

38.6

5.8

46

39.5

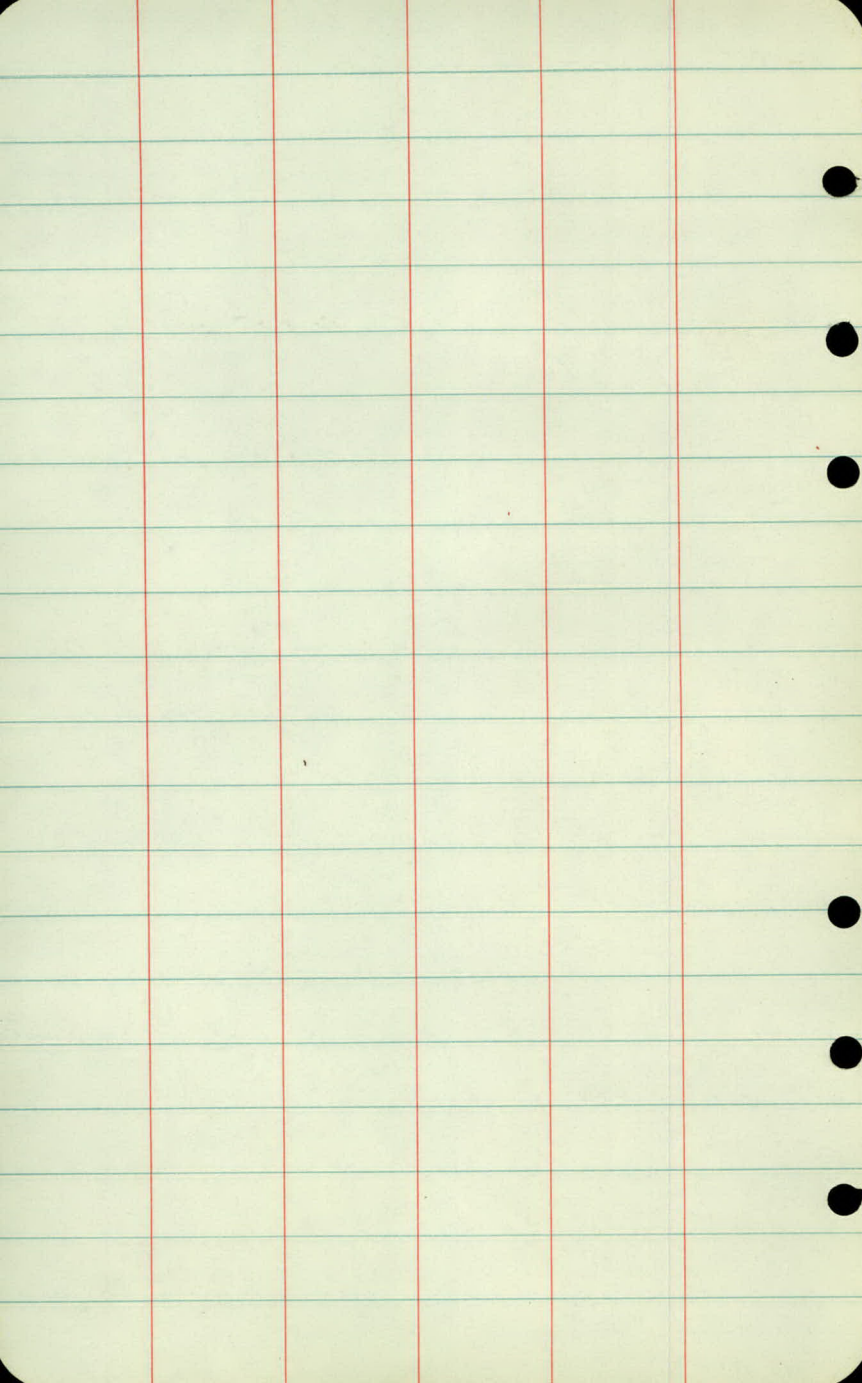
5.9

46



Natural Ground

Spike in 10" ELM 140' Lt sta 43+80



Silver Lake Rd

SWAMP EXC.

x sections

45+50 to 46+50

Sta + π - elev

B.M. 1.74 942.32

940.58

45+50 Lt only

46+00

46+50

B.M.

1.74

940.58

940.58

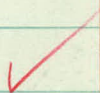
Lt

L

Rt

Spike in 10" ELM 140' Lt Sta 43+80

32.8	29.4	28.1
9.5	14.9	14.2
32	28	15

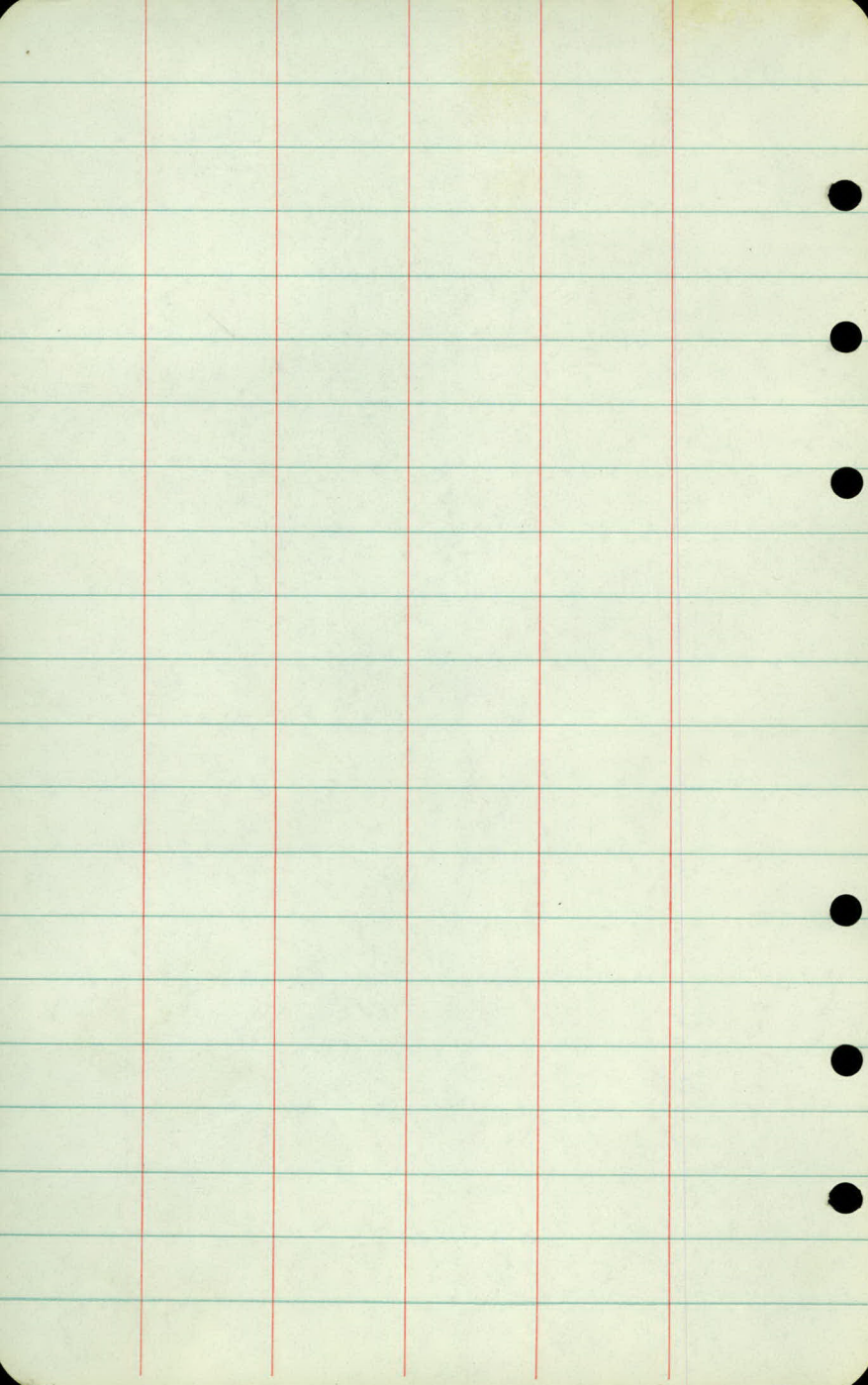


33.6	29.1	31.3	32.4	32.2
8.5	13.2	11.0	9.9	10.1
30	28		25	33



Natural Ground

Spike in 10" ELM 140' Lt Sta 43+80



Silverlake Rd

Swamp Exc.

x - sec.

55+64 to 59+00

S to + π - elev

B.M. 0.39 983.61

983.22

58+75

58+69 Rt. only

58+46 Rt only

58+00 π only

57+68 Rt only

57+28 Rt only

Lt

F

Rt

Top Fire Hyd. 46' Rt Sta 59+16

~~Natural Ground~~

Natural Ground

13.8	15.4	17.4	18.0
9.8	8.2	6.2	5.6
	23	26	30

67.1	67.9	67.4	68.1
15.9	15.7	16.2	4.9
	4	29	34
			N.G.

66.7	66.2	66.6	68.3
16.9	17.4	17.0	5.3
	11	29	35
			N.G.

66.2	66.2	66.6	68.5
17.4	17.4	17.0	5.1
	12	29	35
			N.G.

sta + π - elev

983.61

57+00 Rt only

0.39 983.22 983.22

B.M. 12.50 975.27

962.77

56+82 Rt only

56+54 Rt only

56+29 Rt only

B.M. 12.45 975.22 12.50 962.77 962.77

56+00 Rt only

Lt

£

Rt

66.4 66.7 66.8 18.8
 17.2 16.9 16.8 4.8
 11 29.5 3.5

Top Hyd 46' Rt Stg 59+16 21.6

" " N.E. Cor Silver Lake Rd. S. Co Rd. E

66.4 66.6 66.0 11.6
 8.9 8.7 9.3 35
 9 30

66.8 67.6 67.5 11.6
 8.5 7.7 7.8 33
 10 30

66.9 67.0 69.3 11.6
 8.4 8.3 6.0 33
 13 30

Top Hyd. N.E. Cor Silver Lake Rd. S. Co Rd. E

69.5 69.4 69.1 11.6
 6.7 6.8 6.1 31
 14 27

Sta + π - elev

975.22

55+15 Rt only

58+00 Lt only

B.M.

12.45 962.77

962.77

B.M.

0.68 983.90

983.22

57+68 Lt only

0.68 983.22

983.22

B.M.

12.14 974.91

962.77

57+29 Lt only

12.14 962.77

962.77

Lt

L

Rt

Natural Ground

	66.2	66.3	67.1	✓
N.G.	9.0	8.9	8.1	
33	29	18	8	
Top Hyd N.E. Cor Silverlake Rd. & "E"				
"	"	46'	Rt Sta. 59+16	

	66.8	66.6	66.1	✓
N.G.	17.1	17.3	17.2	
34	31	21	9	
Top Hyd 46' Rt Sta. 59+16				
Top Hyd N.E. Cor Silverlake Rd. & "E"				

	66.2	65.1	66.1	✓
N.G.	8.7	9.2	8.2	
37	32	18	7	
Top Hyd N.E. Cor Silverlake Rd. & "E"				

Sta + π - elev

B.M. 12.37 975.14 962.77

57+00 Lt only

B.M. 12.37 962.77 962.77

B.M. 12.41 975.18 962.77

56+82 Lt only

56+54 Lt only

56+29 Lt only

12.41 962.77 962.77

LT E RT

Top Hyd N.E. Cor. Silverlake Rd. & "E"

	66.6	66.2	66.7	✓
N.G	8.5	8.9	8.4	
32	28	17	7	

Top Hyd N.E. Cor. Silverlake Rd. & "E"

" " " " " " "

	66.6	66.4	67.0	✓
N.G	8.6	8.8	8.2	
32	29	16	8	

	66.8	66.5	67.1	✓
N.G	8.4	8.7	8.1	
33	30	17	7	

	67.9	67.0	67.0	✓
N.G	7.3	8.2	8.2	
38	33	18	9	

Sta + π - elev

B.M. 11.22 973.99

(962.77)

56+00 Lt. only

55+75 Lt only

55+64 Lt. only

T.P 8.18 981.22 0.95 973.04 (973.04)

58+67 Lt only

58+75 Lt only

59+00 Lt only

T.B.N.

8.19 973.03

(973.04)

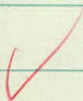
Lt

E

Rt

Top Hyd N.E. Cor. Silver Lake R. d. 'E'

	68.6	64.8	61.1
N.G.	5.4	6.2	6.3
34	30	18	9



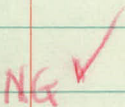
	67.2	66.9	66.6	
N.G.	6.8	7.1	7.4	N.G.
33	28	19	10	



Natural Ground

Top Rock - T.B.M.

	10.2	69.9
N.G.	11.0	11.3
34	31	18

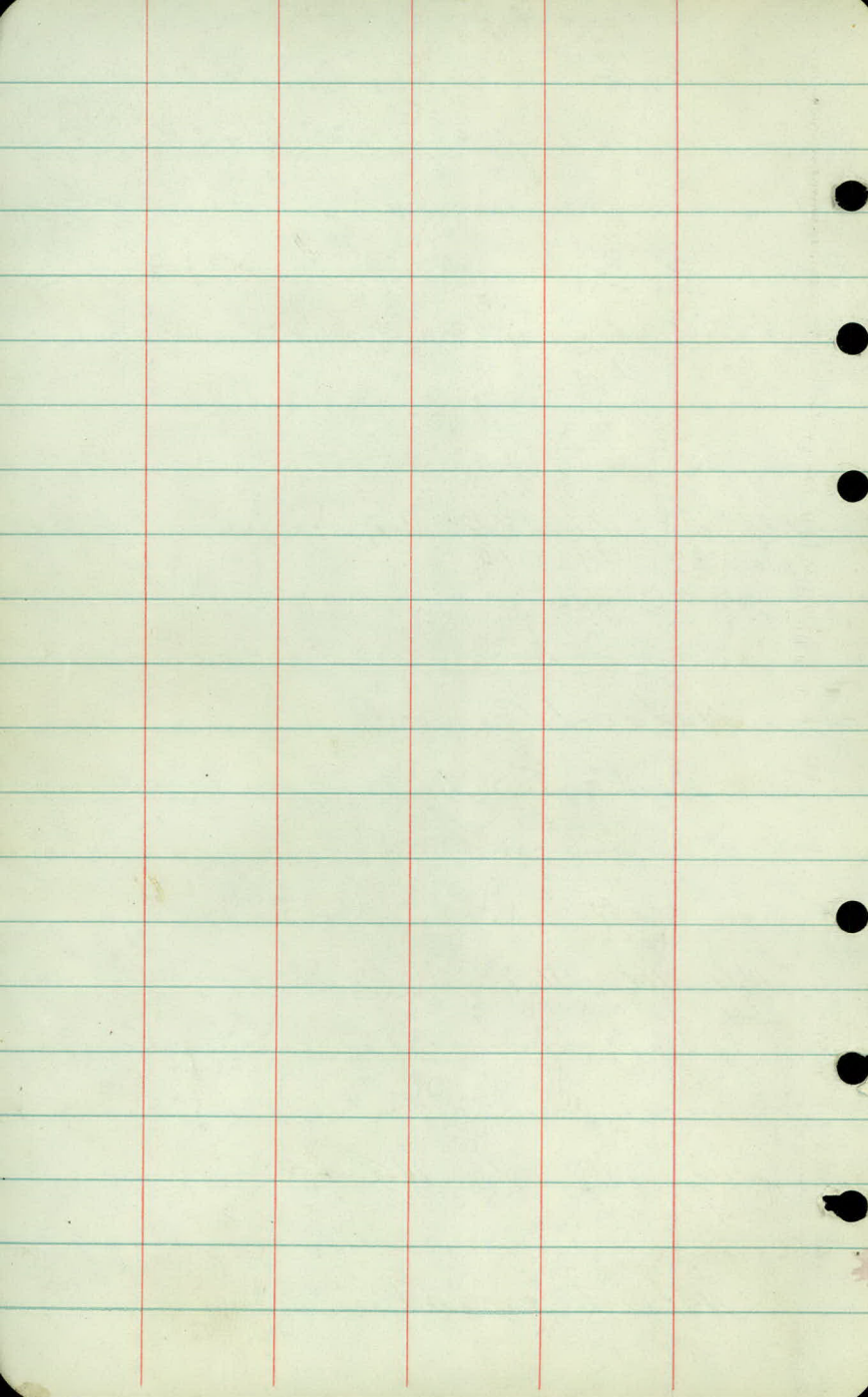


	12.4	13.0
N.G.	9.8	8.2
34	31	18



Natural Ground

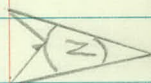
Top Rock



14 JULY 1972
VIVE LE FRANCE

1.

SILVER LAKE RD.
AT GREGORY LANE
(N. of Pine Creek)
(DRAINAGE)



SILVER LAKE RD.

1+00

2+00

3+00

GREGORY LA.

STA + π - ELEV.

BM 2.56 894.97

(892.41)

1+00 = 100' S. ∇ GREGORY LA. E. GUTTER

+25

+62 = C.B.

+74 = BEGIN RADIUS

+85 = GUTTER RT. (S.)

2+00 = ∇ GREGORY LA.

+15 = GUTTER RT (N)

+27 = END. RADIUS

+39

BM

(898.70)

LT

E

14 JULY 1972

RT

2.

HYD. N.W. COR. GREGORY

5.66

5.79

5.80

5.70

5.39	5.49	5.45	5.41
	17	30	50
	CONC. ER		

5.25	5.21	5.29	5.21
	20	40	60

5.21	5.35	5.25	5.27
	18	40	60
	CONC. BR		

5.53

5.42

HYD. S.W. COR. CO. RD. H

STA + π - ELEV.

894.97

+60

+80

3+00

TP 6.66 897.65 3.98 890.99

TP 5.30 899.65 3.30 894.35

BM 0.99 898.66 898.70

LT

~~2~~

14 July 1972 3.

5.31

5.20

5.12

TOP CURB

HYD. N.W. COR. EASTMAN DR.

HYD S.W. COR CO. RD. H

