

Dr. 9 Bk. 4

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

EAST AVENUE

From MARYLAND To 1/2 mi. north

Road Acc't. No. 38A
PROJ. 56-38A.

Date Filed 2-6-59

File Dr. 9 Bk 4

FK
KP

Nov. 29, 1956
Cold Cloudy 14°

a

East Ave
Maryland to Arlington

X-section Extensions
Locations

Locations

6+10 SW Cor Garage 80'

E 21.4 W
N 15.4 S

5+36 8' X 12' shed 217'

5+20 20' X 20' shed 251'

5+14 SW Cor Ho 115' Rt

N 20.5 S

E 31.5 W

3+49 S.W. Cor Ho 159' Rt

N 24.3 S
E 40.8 W

3+06 9' X 12' shed 235' Rt

2+62 S.W. Cor Garage-shed 199' Rt

N 32' S
E 27' W

Nov 29, 1956

b

X-Section Extensions

Sta + π - Elev

BM

992.60

5

EAST AVENUE

Maryland to Arlington

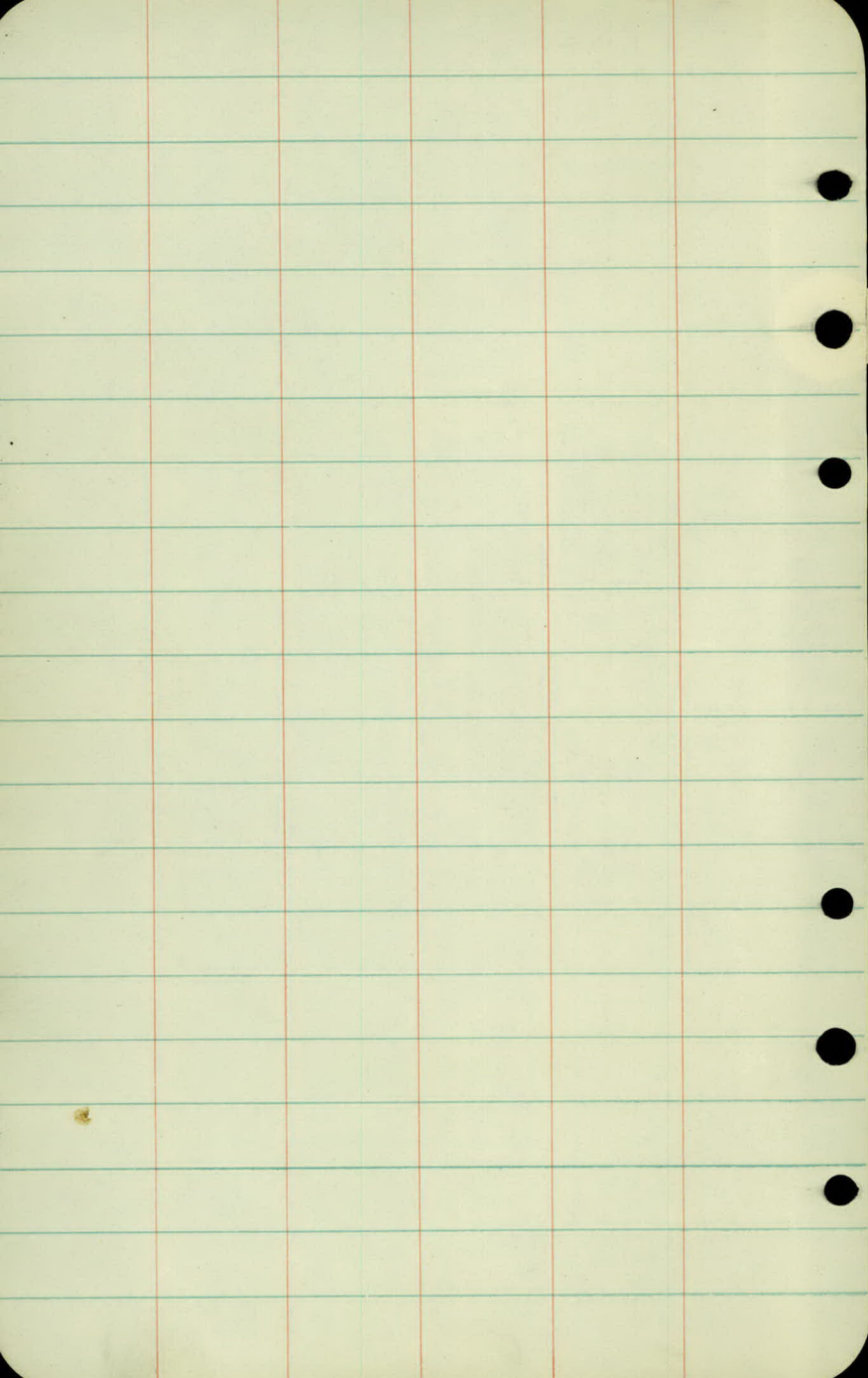
Plan Survey

Alignment 2-5

Topography 6-12

Bench Levels 13-16

X-Sections 18-36



Alignment

Sta Point ΔL ΔR

$\frac{1}{2}$ Ivy
13+17.92 P.I. $0^{\circ}00\frac{1}{2}'$

11+93.97 $\frac{1}{2}$ of East Bound Main Line track

5+34.70 P.O.T.

0+00 $\frac{1}{2}$ Maryland

4

14" T.O.

83

CB

79.56

42.65

51.05

CB

Mont 0.20 East of Straight Line

Mont.

Spiko

64° 03' 3"

51.76

53.82

2.0'

Nail

Gov. Fo.

Hyd &

80.45

42.82

0 PP

119.27

30.04

167.18

PP

9N PP

Mont.

64° 03' 3"

Sta	Point	ΔL	ΔR
-----	-------	------------	------------

26+36.75	± Arlington		
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26+40.00	±		
----------	---	--	--

□

Ment

TOPOGRAPHY

Oct. 28, 1954

FK

AM

LC

MMo

EG

4

Road
19.514" BE Spirea
+91 30 34.39

San

MH
+43 70storm
MH

+30 20

Road

17.5

+80 PP
4.5+80 E. Ent
62+80 GP
25+64 12" x 20 CM Ent
7+61 Range
To Ent 10 ft.+15 14" A
7

Road

16.5

+80 PP
49+70 Alley
11+102 Ent
11+120 PP
3

Road

20.1

79 23.5 165 48
SE. Cor HoHyd
122 36.5+19 3.55g Side Dr.
22+147 End R.
1+103 MH San
70+104 Beg Rad
55

-14 Gutter

-18 9.55g Side Drain
22

-30 Arc Light

planned - KP

Sanitary → ○

storm → ○

○

○

○

○

○

36' 2.5'

N 25 S
E 36 W

T

Sanitary ← ○

D

○

6.21
Deep

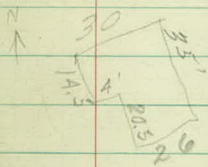
9 Trail 94.83 Fe 2
 +31 TP 1 +75 End Lowland Rt of Fe

8 Trail 67.56 Fe 7
 +90 Beg Lowland Rt of Fe

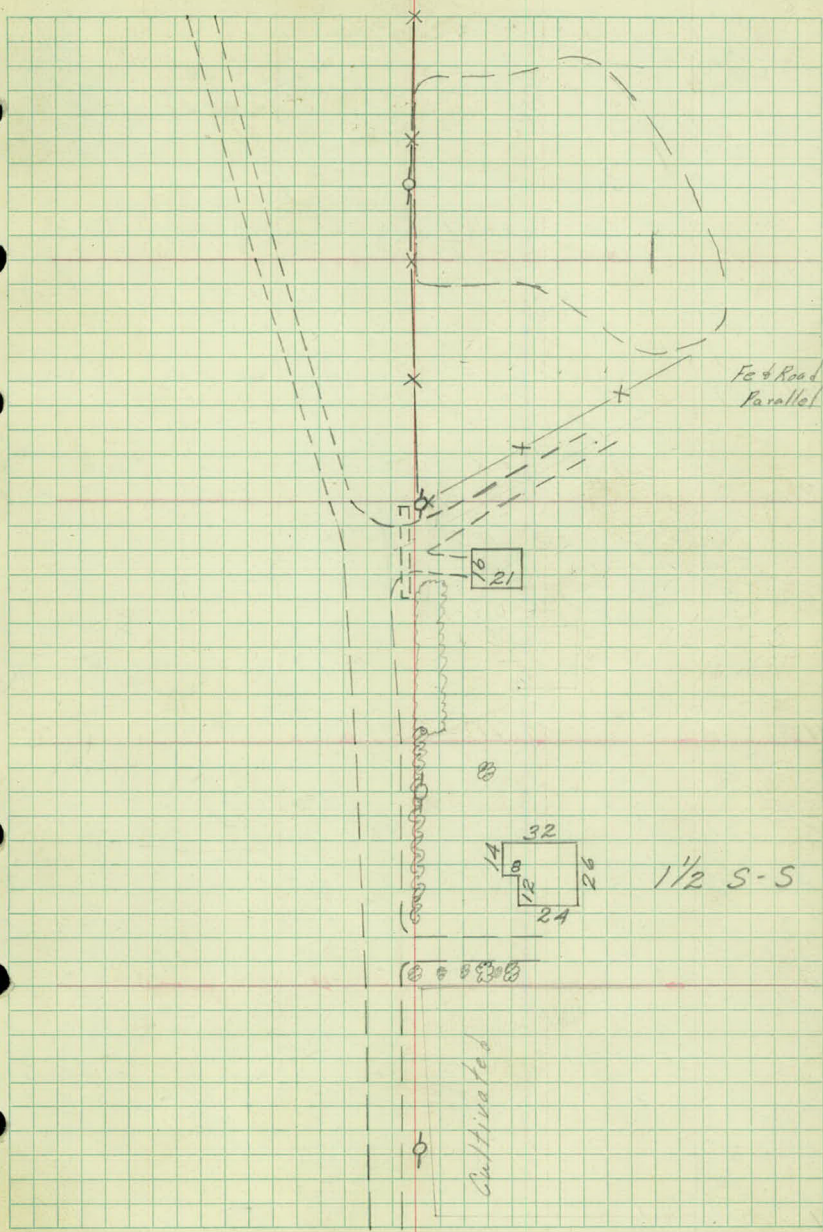
7 Trail 36.27
 +90 End Road +74 Ent Rt +85 Ent Rt +99 T.P. Fe 1-12
 +78 Rt of Fe +67 End SB 1-12 +65 Cor Bar (SW) 24
 S.E. 12" x 37" CM NE 12" x 37" CM
 +60 A Left +97 5' Left
 N.W. Cor Ho End Hedge = Begin R.E.
 +92 74.5 +07 1 1-12
 Road 25.6 Hedge R
 6 Max NW Cor 33.98 +33 S.W. Cor Ho 4890'
 +14 Ent +24 Beg Hedge
 +70 X-Hedge 2 +80 PP +89 5" A
 +04 Hedge Plant Spiraea 6" H. 33
 11; 20; 34; 30; 40

5 Road 21.6
 +99 End Cult 1

4 Road 19.5
 +32 PP 2
 +05 Begin Cult 8



Platted.



14

+99 $\frac{12''0}{6}$ +98 $\frac{12''0}{23}$ +95 $\frac{12''0}{6}$ +94 $\frac{6''0}{9}$
+98 $\frac{14''0}{74}$ +65 $\frac{18''0}{27}$ +27 $\frac{22}{22}$ +69 $\frac{6''0}{42}$
+97 $\frac{12''0}{10}$ +26 $\frac{23}{23}$ +99 $\frac{8''0}{23}$ +60 $\frac{10''0}{49}$
+36 $\frac{C.B.}{41}$ +21 $\frac{T.10''0}{5}$ +20 $\frac{\text{Begin Broken Down Fe } \&}{1}$

13

+18 $\frac{N.H.}{10}$ +103 $\frac{100}{6}$ +105 $\frac{12''0}{5}$
+99 $\frac{C.B.}{49.8}$ +87 $\frac{5''\text{Cott.}}{25}$ +97 $\frac{12''0}{9} \& \frac{12''0}{27}$
+79 $\frac{Pole}{1}$ +67 $\frac{2-14''0}{4}$ +81 $\frac{8''\text{Cott.}}{22}$
+59 $\frac{I.P.}{9}$

+11.29 $\&$ Track W. Bound

12

11+93.97 $\&$ E. Bound Track
11+78.5 $\&$ Side Track
11+62.4 $\&$ " "
11+47.08 $\&$ " "
11+31.95 $\&$ " "
11+16.75 $\&$ " "
11+01.70 $\&$ " "

11

10

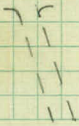
+47 $\frac{\text{End Trail}}{1}$

+70 $\frac{\text{End Fe}}{1}$ +63 $\frac{I.P.}{1}$ +63 $\frac{12''\text{Cott.}}{27}$

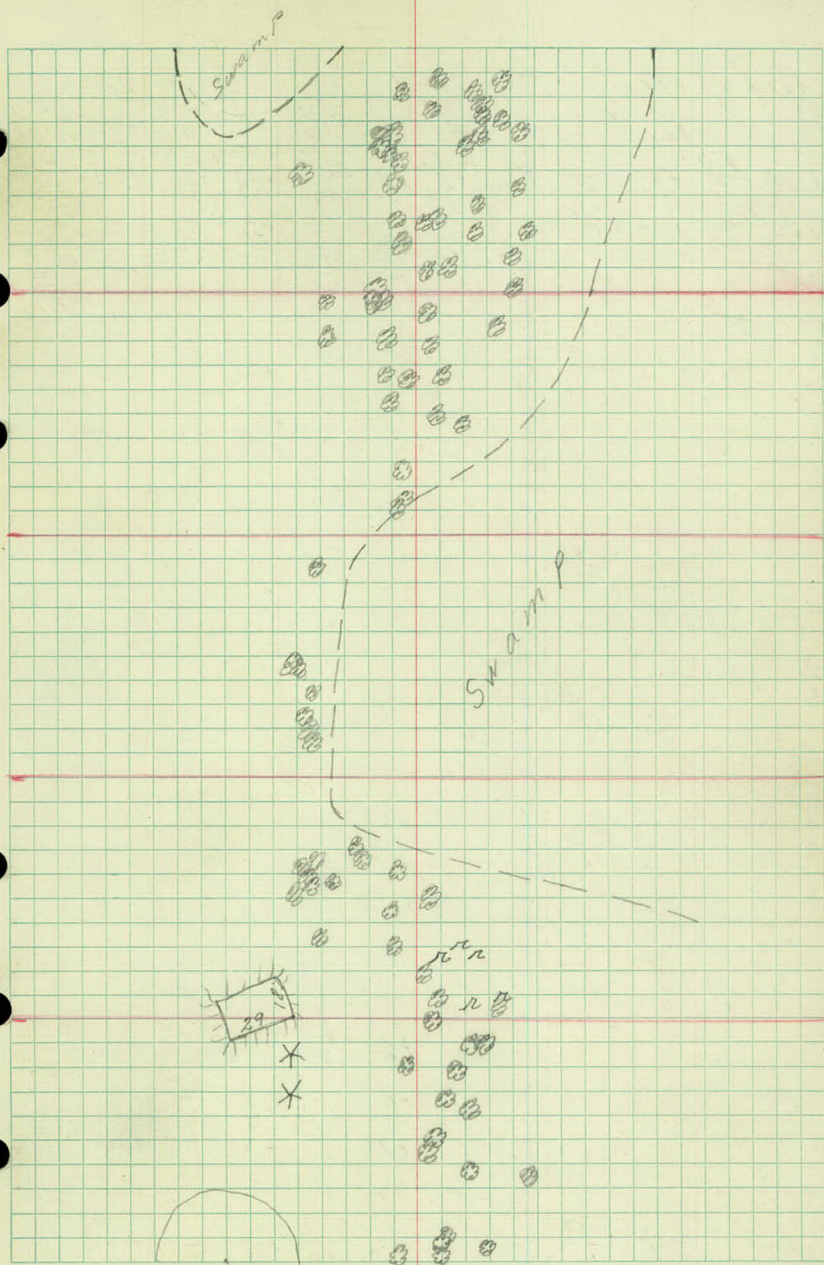
9



144 St.



13	+80 $\frac{50''}{10''}$	+81 $\frac{6''}{5''}$	+86 $\frac{8''}{24''}$	+64 $\frac{27''}{8''}$	+66 $\frac{43''}{32''}$	+70 $\frac{37''}{21''}$	+60 $\frac{2-6''}{21''}$
+58 $\frac{13''}{14''}$	+62 $\frac{10''}{16''}$	+65 $\frac{3-6''}{8''}$	+37 $\frac{12''}{25''}$	+44 $\frac{4''}{44''}$	+60 $\frac{2-6''}{21''}$	+30 $\frac{6''}{9''}$	+23 $\frac{4''}{17''}$
+49 $\frac{14''}{47''}$	+53 $\frac{4''}{6''}$	+56 $\frac{10''}{5''}$	+24 $\frac{8''}{26''}$	+28 $\frac{6''}{3''}$	+30 $\frac{6''}{9''}$	+23 $\frac{4''}{17''}$	+10 $\frac{10''}{15''}$
+44 $\frac{12''}{8''}$	+44 $\frac{10''}{3''}$	+29 $\frac{14''}{9''}$	+09 $\frac{6''}{5''}$	+16 $\frac{3-4''}{41''}$	+23 $\frac{4''}{17''}$	+10 $\frac{10''}{15''}$	+92 $\frac{6''}{6''}$
18	+20 $\frac{2-4''}{7''}$	+01 $\frac{16''}{14''}$	+00 $\frac{5wp}{74''}$	+01 $\frac{10''}{41''}$	+10 $\frac{10''}{15''}$	+10 $\frac{10''}{15''}$	+10 $\frac{10''}{15''}$
+97 $\frac{10''}{13''}$	+98 $\frac{4''}{16''}$	+77 $\frac{4''}{6''}$	+85 $\frac{10''}{34''}$	+92 $\frac{6''}{6''}$	+92 $\frac{6''}{6''}$	+92 $\frac{6''}{6''}$	+92 $\frac{6''}{6''}$
+97 $\frac{8''}{39''}$	+82 $\frac{10''}{37''}$	+80 $\frac{8''}{11''}$	+64 $\frac{10''}{11''}$	+64 $\frac{10''}{11''}$	+64 $\frac{10''}{11''}$	+64 $\frac{10''}{11''}$	+64 $\frac{10''}{11''}$
+63 $\frac{10''}{3''}$	+66 $\frac{14''}{12''}$	+15 $\frac{5wp}{\phi}$	+49 $\frac{8''}{9''}$	+49 $\frac{8''}{9''}$	+49 $\frac{8''}{9''}$	+49 $\frac{8''}{9''}$	+49 $\frac{8''}{9''}$
	+55 $\frac{10''}{9''}$	+27 $\frac{22''}{6''}$	+43 $\frac{6''}{20''}$	+43 $\frac{6''}{20''}$	+43 $\frac{6''}{20''}$	+43 $\frac{6''}{20''}$	+43 $\frac{6''}{20''}$
17	+16 $\frac{7-10''}{5''}$	+10 $\frac{8''}{7''}$					
	+90 $\frac{5wp}{25''}$						
+45 $\frac{6''}{47''}$	+47 $\frac{6''}{30''}$	+87 $\frac{6''}{43''}$					
+23 $\frac{12''}{46''}$		+35 $\frac{5wp}{43''}$					
	+15 $\frac{8''}{42''}$	+21 $\frac{12''}{43''}$					
16	+63 $\frac{16''}{48''}$	+66 $\frac{10''}{42''}$	+66 $\frac{12''}{22''}$				+55 $\frac{5wp}{60''}$
+53 $\frac{6''}{43''}$	+51 $\frac{8''}{48''}$	+58 $\frac{8''}{35''}$					+50 $\frac{12''}{5''}$
+57 $\frac{12''}{35''}$	+44 $\frac{14''}{11''}$	+61 $\frac{12''}{8''}$	+30 $\frac{5wp}{19''}$				+08 $\frac{5wp}{35''}$
+33 $\frac{10''}{40''}$	+71 $\frac{12''}{23''}$	+30 $\frac{12''}{10''}$	+19 $\frac{12''}{2''}$	+25 $\frac{5wp}{10''}$	+26 $\frac{5wp}{26''}$		+26 $\frac{5wp}{26''}$
15	+90 $\frac{5wp}{35''}$	+00 $\frac{5wp}{52''}$	+04 $\frac{8''}{34''}$	+05 $\frac{5wp}{22''}$	+08 $\frac{3-12''}{9''}$		+08 $\frac{3-12''}{9''}$
+85 $\frac{5''}{53''}$			+89 $\frac{8''}{28''}$	+99 $\frac{6''}{7''}$			+99 $\frac{6''}{7''}$
+69 $\frac{8''}{53''}$	+81 $\frac{6''}{4''}$		+67 $\frac{2-4''}{13''}$	+79 $\frac{6''}{16''}$	+88 $\frac{3-12''}{21''}$		+88 $\frac{3-12''}{21''}$
			+45 $\frac{16''}{4''}$	+50 $\frac{10''}{7''}$	+63 $\frac{8''}{21''}$		+63 $\frac{8''}{21''}$
+00 $\frac{Edge Green}{50''}$	+03 $\frac{18''}{7''}$	+02 $\frac{6''}{10''}$	+11 $\frac{4''}{11''}$	+37 $\frac{2-10''}{22''}$	+35 $\frac{12''}{47''}$		+35 $\frac{12''}{47''}$
				+07 $\frac{10''}{29''}$	+09 $\frac{8''}{10''}$		+09 $\frac{8''}{10''}$



+68 to +99	$\frac{12-6''}{0-50'}$						
+61	$\frac{\text{Trip } 6''}{2}$		+93	$\frac{4''}{3}$	+94	$\frac{2-6''}{10''}$	
						+98	
+59	$\frac{8''}{2}$	+36	$\frac{\text{Sto}}{9}$	+31	$\frac{6''}{14}$	+23	$\frac{12''}{8}$
						+30	$\frac{12''}{10''}$
+25	$\frac{8''}{36}$	+24	$\frac{11''}{26'}$			+50	$\frac{\text{SWP}}{24-55}$
						+06	$\frac{12''}{6}$

23	103	100	21, 50	102	1-0
+84	8"0				A
6"0					
49					
+66	4"0	+68	8"0	+70	4"0
49	9	37		23	
End				+72	6"0
+50	6"0	+61	22"0	10	
Swamp	22	11		+80	Swamp
					30-45
+41	10"0	+50	Swamp		
49		10-50			
+32	Trip 8"0				
10					
+43	T-4"0				
14					
				+00	6+40
					13-1-8"0
					0-50'

[illegible]

21

	+15	43	+28	45	+36	45
			Trip 12 ¹ / ₉ p			
	+97	46				
			+90	SUR 50		

[illegible]

12 Trees

SWAMP

13 Trees

Swamp

+98 4"0 27
 +94 3-4"0 18
 +82 2-6"0 21
 +80 8"0 28

+40 12" E 15
 +40 4"0 47
 +34 7-8" W 26
 +29 8" P 12

29

28

27

+60 End R.
10

+35 GP
27

+20 End Pothole
40

+26 +100 Pothole
38

+50 Pothole
70

sta 25
sta 26 Wooded Large
Trees

+25 +00 Pothole 6" 25' 5' +01
90 + 55 + 01

+ +
+68 Cor Pothole 25'
+83 6" W 24' +94 16" W 38' +96 110" W 12'
+00 to +70 24-46 to 8" 0
0-50'

+24 +06 Beg Pothole
100

+70 End R.
12

+17 Beg R.
60

+38 Art Light
30

+06 Beg R.
27

+80 End Broken
Down Fe 2 187 5-8" W
34, 40, 46, 48

+50 SWP
2

+85 End
SWP

+00 SWP
1

+98 16" 0
31

+85 SWP 2 +98 12" W
18

+80 Pothole Drain

+69 GP
20

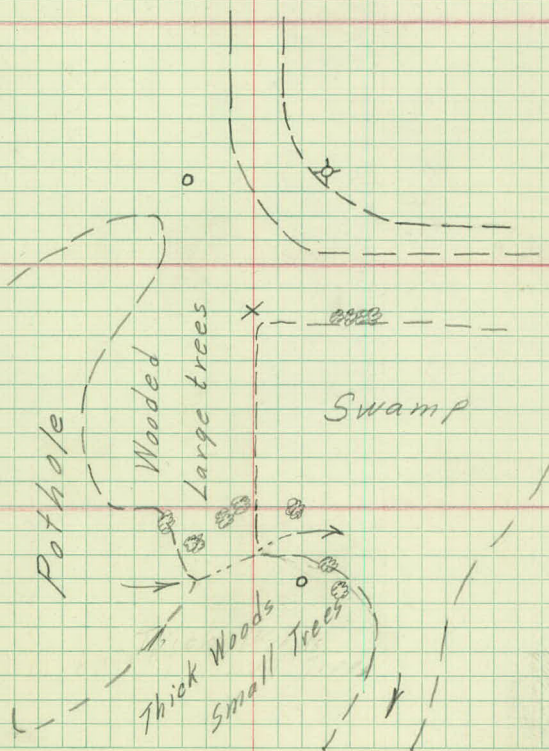
+50 SWP
51-80

+66 22" 0
35

+00 to +70 0-50'

28-46 to 8" trees
0-50'

+00 SWP
29-65



34

33

32

31

30

29

BENCH - LEVELS

EAST - AVE

MARYLAND TO ARLINGTON

STA	+	+	-	ELEV
-----	---	---	---	------

B.M	0.22	965.78		965.56
-----	------	--------	--	--------

1.25	956.95	10.08	955.70	
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7.63	958.72	5.86	951.09	
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10.38	966.24	2.86	955.86	
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7.70	972.21	1.73	964.51	
------	--------	------	--------	--

B.M		1.57	970.64	
-----	--	------	--------	--

Top - Hydt N.W. COR. STILLWATER + EAST AVE

Top - Hydt N.W. - COR. AMES + EDGEWATER - BLVD

Sta	+	-	Elev
BM	2.92	1025.73	1022.81
T.P.	5.07	1025.92	4.88 1020.85
"	12.11	1037.91	0.12 1025.80
old BM		3.98	1033.93 1033.46
TP	8.45	1043.31	0.85 1037.06
"	0.73	1038.80	7.44 1038.07
BM		3.87	1034.93
TP	0.61	1026.37	13.04 1025.76
"	1.15	1013.97	13.55 1012.82
"	2.14	1004.54	11.57 1002.40
BM	8.24	1006.82	5.96 998.58
TP	2.88	1000.82	8.88 997.94
	4.62	1003.29	2.15 998.67
BM		1.66	1001.63 1001.64
TP	2.60	1005.58	0.31 1002.98
BM	3.03	997.57	11.04 994.54 994.59
TP	1.63	992.23	6.97 990.60
"	2.44	983.27	11.40 980.83
BM		7.93	975.34 975.25

Corrected
as of 10-19-55

FK. 41
AM T
WJ Red

Sept. 15, 1955
Cool Clear Windy

15

Top S.W. Cor of Top Step Ent to Store
NW Cor. Laigentour & East Ave.

Top Mast & Sta 39+54.6

Top S. End Ent. Culvert 1506 East Ave

Spike in Arc Light pole N.E. Cor. Arlington & East Ave

Spike in 10" Oak 33' Lt of P.O.T

Top 2' iron 33' Lt Sta 13+40

Top S. End Ent Culvert 4' Rt Sta 6+60

Top Hyd N.W. Cor Maryland & East Ave.

Sta	+	-	Elev	
BM	7.93	983.27	975.34	
TP	12.25	994.01	1.51	981.76
BM			1.33	992.68 (992.60)
TP	6.71	997.34	3.38	990.63 990.60
"	11.24	1005.92	2.66	994.68 1.05 (994.59)
"	4.82	1002.47	8.27	997.65
BM			0.72	1001.75 (1001.64)
TP	11.72	1001.44	12.75	989.72
	9.44	1010.48	0.40	1001.04
BM	13.51	1012.21	11.78	998.70
BM			3.51	1008.70
TP	13.43	1025.32	0.32	1011.89
"	12.93	1037.68	0.57	1024.75
BM	9.75	1044.68	2.69	1034.99 1034.93
T. P	1.46	1033.54	12.60	1032.08
"	4.25	1025.83	11.96	1021.58
				1022.89
B.M			3.00	1022.83 (1022.81)
				1023.79
TP	7.37	997.97		990.60
BM			3.35	994.62
				4.04
				4.05
				4.02

Top Hyd N.W. Cor Maryland & East Ave

Top W. End Front Door Sill Ho #1250 East Ave

Top S. End Ent Culvert 4' BT Sta 6+60

Top 2' Iron 33' Lt Sta 13+40

Spike in 10" Out 33' Lt. of POT

Spike in Arc Light Pole NE Cor Arlington & East Ave

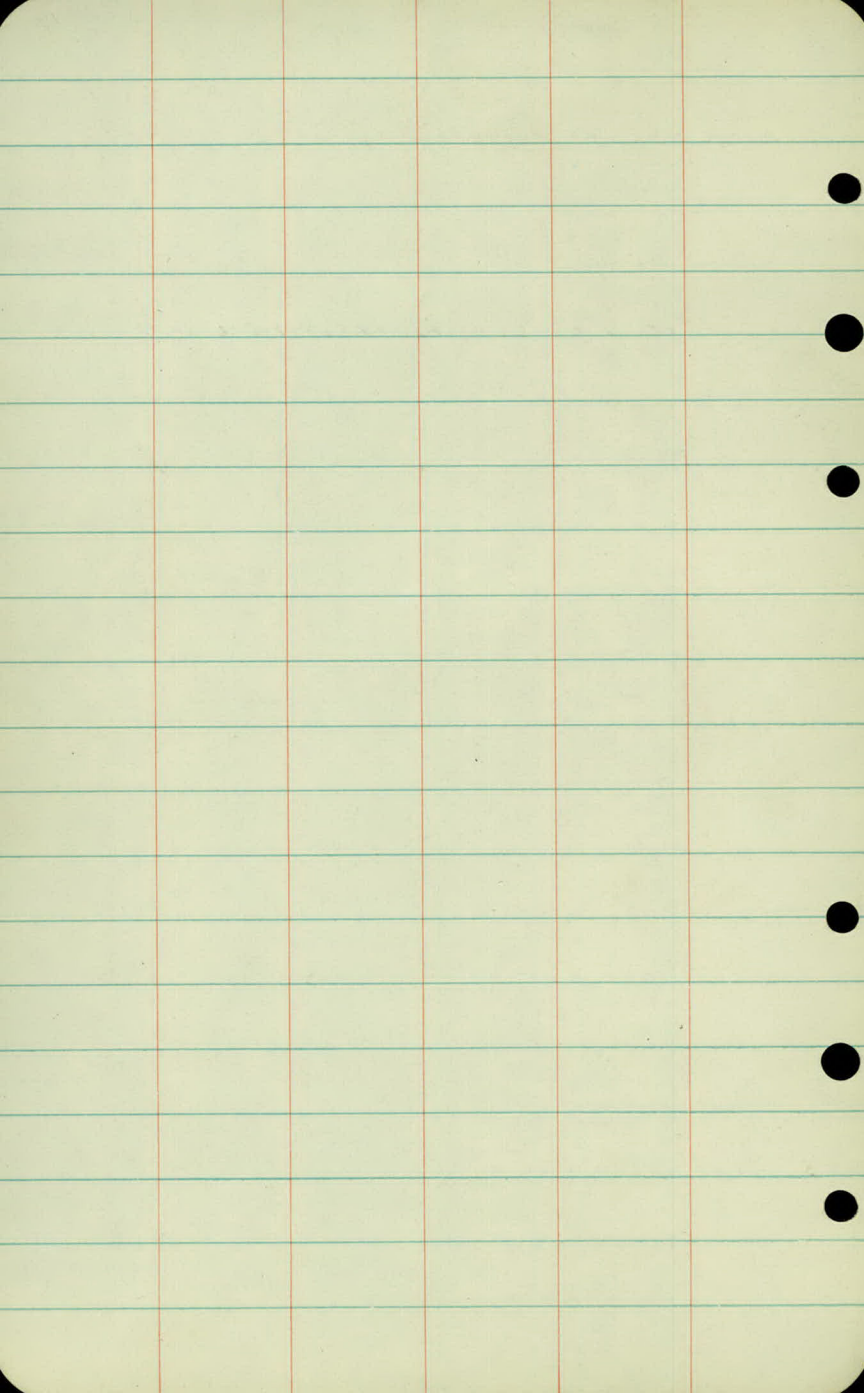
S.W. Cor Apron Golf Course Machine shed

Top S. End Ent. Culvert 1506 East Ave.

Top S.W. COR Top STEP ENT-TO - STORE

S End Ent Culvert 4' BT Sta 6+60

Top of 2' Iron



2+00

0-2 Granular Clay
2-3 Gravel

4+00

Road Bed at 2.5

0-1.5 Topsoil (Very Good)

1.5-4.5 Clay

5+39

N.W. Cor Ho 34.0' RT

6+79

N.W. Cor Garage 23.0' RT

8+00

0-4 Clay

10+00

Somewhat Sandy Soil
RR-Sample

241
1890 12

1890 12

2.6

11 + 78.5

40.1

12 2.5

37.6

11 624

70.6

45.5

151

13 255

68.05

11+3195

655

50.25

5.35

1267

12 5292

11 + 4708

80.65

56

17 83.25

16.75

16.1

15.3

15.1

152

9.0 / 2

1, 2

29

9x

35. 28

$\frac{1}{2} \cdot \frac{1}{2} = \frac{1}{4}$
 $\frac{1}{4} \cdot \frac{1}{2} = \frac{1}{8}$
 $\frac{1}{8} \cdot \frac{1}{2} = \frac{1}{16}$
 $\frac{1}{16} \cdot \frac{1}{2} = \frac{1}{32}$
 $\frac{1}{32} \cdot \frac{1}{2} = \frac{1}{64}$
 $\frac{1}{64} \cdot \frac{1}{2} = \frac{1}{128}$
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 $\frac{1}{562949953421312} \cdot \frac{1}{2} = \frac{1}{1125899906842624}$
 $\frac{1}{1125899906842624} \cdot \frac{1}{2} = \frac{1}{2251799813685248}$
 $\frac{1}{2251799813685248} \cdot \frac{1}{2} = \frac{1}{4503599627370496}$
 $\frac{1}{4503599627370496} \cdot \frac{1}{2} = \frac{1}{9007199254740992}$
 $\frac{1}{9007199254740992} \cdot \frac{1}{2} = \frac{1}{18014398509481984}$
 $\frac{1}{18014398509481984} \cdot \frac{1}{2} = \frac{1}{36028797018963968}$
 $\frac{1}{36028797018963968} \cdot \frac{1}{2} = \frac{1}{72057594037927936}$
 $\frac{1}{72057594037927936} \cdot \frac{1}{2} = \frac{1}{144115188075855872}$
 $\frac{1}{144115188075855872} \cdot \frac{1}{2} = \frac{1}{288230376151711744}$
 $\frac{1}{288230376151711744} \cdot \frac{1}{2} = \frac{1}{576460752303423488}$
 $\frac{1}{576460752303423488} \cdot \frac{1}{2} = \frac{1}{1152921504606846976}$
 $\frac{1}{1152921504606846976} \cdot \frac{1}{2} = \frac{1}{2305843009213693952}$
 $\frac{1}{2305843009213693952} \cdot \frac{1}{2} = \frac{1}{4611686018427387904}$
 $\frac{1}{4611686018427387904} \cdot \frac{1}{2} = \frac{1}{9223372036854775808}$
 $\frac{1}{9223372036854775808} \cdot \frac{1}{2} = \frac{1}{18446744073709551616}$
 $\frac{1}{18446744073709551616} \cdot \frac{1}{2} = \frac{1}{36893488147419103232}$
 $\frac{1}{36893488147419103232} \cdot \frac{1}{2} = \frac{1}{73786976294838206464}$
 $\frac{1}{73786976294838206464} \cdot \frac{1}{2} = \frac{1}{147573952589676412928}$
 $\frac{1}{147573952589676412928} \cdot \frac{1}{2} = \frac{1}{295147905179352825856}$
 $\frac{1}{295147905179352825856} \cdot \frac{1}{2} = \frac{1}{590295810358705651712}$
 $\frac{1}{590295810358705651712} \cdot \frac{1}{2} = \frac{1}{1180591620717411303424}$
 $\frac{1}{1180591620717411303424} \cdot \frac{1}{2} = \frac{1}{2361183241434822606848}$
 $\frac{1}{2361183241434822606848} \cdot \frac{1}{2} = \frac{1}{4722366482869645213696}$
 $\frac{1}{4722366482869645213696} \cdot \frac{1}{2} = \frac{1}{9444732965739290427392}$
 $\frac{1}{9444732965739290427392} \cdot \frac{1}{2} = \frac{1}{18889465931478580854784}$
 $\frac{1}{18889465931478580854784} \cdot \frac{1}{2} = \frac{1}{37778931862957161709568}$
 $\frac{1}{37778931862957161709568} \cdot \frac{1}{2} = \frac{1}{75557863725914323419136}$
 $\frac{1}{75557863725914323419136} \cdot \frac{1}{2} = \frac{1}{151115727451828646838272}$
 $\frac{1}{151115727451828646838$

16/6/19

1/2

2/10/0

1/1/15

X-Sections

Sta	+	π	-	Elev.
BM	2.90	978.15		975.25

0+18 Catch Basin

0+00 $\frac{1}{2}$ Maryland St.

+16 Gutter Line Left

+19 Catch Basin

+23 Shoulder Rt

+30

FK
AM
WJ

Oct. 19, 1955

19

Lt.

Rt.

Top Hyd N.W. Cor East Ave + Maryland

70.88	66.34	66.38	69.91					
7.27	11.81	11.77	8.24					
TOP FL inv S.	FL inv	FL inv	F.L. Side Drain					
12"SCP	N 12"SCP	22						
OUT	IN							
75.2	73.7	71.7	70.4	69.5	68.7	67.3	65.5	64.2
3.0	4.5	6.5	7.8	8.7	9.5	10.9	12.7	14.0
150	100	50	28		23	50	100	150

71.1	70.2	69.8	69.1	67.9	67.1	
7.1	8.0	8.4	9.1	10.3	11.1	
50	22		13	34	50	

71.20	66.85	66.83	70.30					
9.5	11.30	11.32	7.85					
TOP FL inv	FL inv	FL inv	F.L. Side Drain					
N 12"SCP	S. 12"SCP	22						
Stub	OUT							

72.4	71.4	70.4	70.2	70.0	69.2	68.6	67.6	66.8
5.8	6.8	7.8	8.0	8.2	9.0	9.6	10.6	11.4
50	25	22	11		14	26	40	50

72.9	71.9	70.4	70.5	70.3	69.6	68.5	66.6	65.5
5.3	6.3	7.8	7.7	7.9	8.6	9.7	11.6	12.7
50	26	21	9		13	26	40	50

Sta	+	π	-	Elev
-----	---	-------	---	------

		978.15		
--	--	--------	--	--

0+50				
------	--	--	--	--

✓				
---	--	--	--	--

+B1				
-----	--	--	--	--

1				
---	--	--	--	--

+50				
-----	--	--	--	--

TP	8.45	986.25	0.35	977.80
----	------	--------	------	--------

+72	≠ Alley Left			
-----	--------------	--	--	--

Oct. 19, 1955

20

14

RT

74.1	71.7	72.0	72.1	71.8	71.4	72.3	69.3	65.3
4.1	6.5	6.2	6.1	6.4	6.8	5.9	8.9	12.9
29	20	18	9		5	8	21	50

75.7

76.1

2.5
41

2.1
50

78.1

0.1

House
48

75.03

3.12

End Walk
24

77.6	77.5	75.4	75.4	75.2	75.1	73.4	69.9	68.6
0.6	0.7	2.8	2.8	3.0	3.1	4.8	8.3	9.6
50	42	20	10		4	13	32	50

77.9

0.3

50

77.3

0.9

25

77.9

0.3

11

77.6

0.6

78.2

0.0

4

76.6

1.6

15

74.9

3.3

26

71.8

6.4

50

78.0

8.3

100

77.6

8.7

50

77.7

8.6

23

78.4

7.9

20

77.0

7.3

11

78.7

7.6

Drains →

Sta	+	π	-	Elev
-----	---	-------	---	------

		986.25		
--	--	--------	--	--

1 + 80				
--------	--	--	--	--

2

TP	9.97	991.05	5.17	981.08
----	------	--------	------	--------

+50				
-----	--	--	--	--

+54				
-----	--	--	--	--

+74				
-----	--	--	--	--

3

♀

Oct 19, 1955

21

Lt

BT

X 78.3

8.0
50

78.2

8.1
26

78.8

7.5
21

79.4

6.9
10

79.1

7.2
2

78.8

7.5
4

79.8

6.5
24

77.2

9.1
40

74.7

11.6
50

73.9

12.4
50

81.5

X 4.8
50

80.3

6.0
31

79.5

6.8
21

80.0

6.3
10

79.7

6.6
2

79.3

7.0
4

80.3

6.0
16

78.7

7.6
33

76.3

10.0
50

75.3

11.0
50

N. End East Culvert

80.1

X 11.0
50

80.6

10.5
33

80.8

10.3
20

81.1

10.0
10

80.8

10.3
2

80.1

11.0
4

80.8

10.3
26

80.0

11.1
39

79.2

11.9
50

79.1

12.0
50

79.88

11.17

FL 12" x 20" CN

1

80.08

10.97

FL 12" x 20" CN

1

80.1

X 11.0
50

80.5

10.6
30

81.5

9.6
20

81.7

9.4
10

81.1

10.0
2

80.7

10.4
4

81.2

9.9
21

81.5

9.6
34

82.2

8.9
50

83.1

8.0
50

Sta + π - Elev

991.05

3+13 S. Prop. Line Nokomas

+43 $\pm$ Nokomas (Not Graded). Yet

+73 N. Prop. Line Nokomas

✓

A

2 Oct. 19, 1935

22

82.0	81.6	81.8	82.0	81.3	80.2	81.8	82.5	82.8	83.5
9.1	9.5	9.3	9.1	9.8	10.9	9.3	8.6	8.3	7.6
50	30	20	10		2	4	25	38	50

85.5	85.2	84.4	82.4	82.7	82.3	82.4	83.0	84.0	84.6	84.4	85.3
5.6	5.9	6.7	8.7	8.4	8.8	8.7	8.1	7.1	6.5	6.7	5.8
50	43	26	20	10		2	4	10	29	38	50

85.3	83.4	83.4	83.9	83.3	83.5	84.8	85.6	86.6	86.6
5.8	7.7	7.7	7.2	7.8	7.6	6.3	5.5	4.5	4.5
25	22	20	12	3		2	15	31	50

85.5	86.1
5.6	5.0
30	50

86.9	84.6	84.6	85.3	84.9	86.0	87.0	87.4	87.5	87.4
4.2	6.5	6.5	5.8	6.2	5.1	4.1	3.7	3.6	3.7
26	23	21	12	4		1	13	36	50

86.8	87.2
4.3	3.9
40	50

Sta + π - Elev

991.05

+50

✓

5.68 994.87 1.86 989.19

5

✓

2.26 992.61 (992.60)

+50

Oct. 19, 1955

23

87.4	87.9	87.6	88.5-	88.8	88.2	88.3	88.3
3.7	3.2	3.5	2.6	2.3	2.9	2.8	2.8
22	14	5	2		9	27	50

87.4	88.7	88.9	88.9
3.7	2.4	2.2	2.2
24	25	44	50

89.2	89.9	89.7	90.2	90.2	89.7	88.6	87.9
5.7	5.0	5.2	4.7	4.7	5.2	6.3	7.0
25	14	6	2		11	31	50

89.2	90.9	90.5-
5.7	4.0	4.4
26	30	50

Top W. End Front Door Sill H₀ # 1506 East Ave

90.0	90.7	90.0	89.7	90.4	90.6	90.5-	89.8	90.0
4.9	4.2	4.9	5.2	4.5	4.3	4.4	5.1	4.9
26	15	7	4	3		2	16	34.5 H.O.

90.4	91.5-	91.5	91.6
4.5	3.4	3.4	3.3
28	30	41	50

21250

Sta + π - Elev

994.87

6

✓
132 S. prop Line

✓
+62 £

+60 S

FK
AM
LC
HJ

Oct. 19, 1935

24

Lt				Rt			
90.3	90.0	89.4	90.3	90.2	89.9	89.4	87.7
46	49	55	46	47	50	55	7.2
18	10	4	3	2	15	43	50

89.9	90.1	90.9	91.0
50	48	40	39
28	31	32	50

90.2	90.5	89.9	89.5	90.2	90.2	89.6	89.6	88.6	87.5
47	44	50	54	47	47	53	53	63	74
29	19	9	4	3	2	18	34	50	

90.2	91.0	91.6
47	39	33
31	34	50

91.6	91.4	90.9	91.1	90.5	89.9	90.7	90.3	89.7	89.1	88.3
33	35	40	38	44	50	42	46	52	58	66
50	39	33	20	9	6	2		18	37	50

89.57

5.30
FL 12"x37cm
A

Sta + π - Elev.

994.87

6 + 23 $\pm$

+ 92

+ 97

7

✓

TP 7.09 997.04 4.92 989.95

+ 50

2

Oct. 19, 1955

25

Lt

Rt.

89.62

5.25

Gar Ent slab
24

91.1.	91.3.	90.8.	91.1.	91.0.	90.5.	89.2.	88.6.	87.7.
3.8	3.6	4.1	3.8	3.9	4.4	5.7	6.3	7.2
50	45	40	24	10		17	28	50

89.36
5.51
FL 12" x 37" CM

91.1.	90.5.	89.7.	89.7.	91.6.	90.2.	88.7.	87.2.
3.8	4.4	5.2	5.2	3.3	4.7	6.2	7.7
16	8	6	5		5	24	50

90.6.	90.1.	90.1.
4.3	4.8	4.8
29	39	50

86.6.	87.1.	86.9.	87.1.	86.4.	86.3.	85.9.
10.4	9.9	10.1	9.9	10.6	10.7	11.1
50	39	19		14	32	50

Sta + π - Elev

997.04

8

+50

9

+ 50

+ 66

+ 74

Oct. 19, 1955

26

11		BT			
85.0	12.0	50	84.9	12.1	50
85.0	12.0	31	84.6	12.4	19
84.7	12.3	10	84.0	13.0	2
84.1	12.9		83.6	13.4	
			83.3	13.7	18
			83.2	13.8	29
			83.2	13.8	50
85.0	11.0	50	86.0	11.0	50
86.3	10.7	32	86.3	10.7	32
86.4	10.6	10	86.2	10.8	
85.2	11.8	14	85.2	11.8	14
85.4	11.6	29	85.4	11.6	29
85.1	11.9	50	85.1	11.9	50
88.7	8.3	50	88.7	8.3	50
89.4	7.6	36	89.4	7.6	36
89.8	7.2	21	89.8	7.2	21
90.9	6.1	12	90.9	6.1	12
91.9	5.1		91.9	5.1	
90.9	6.1	22	90.9	6.1	22
89.7	7.3	50	89.7	7.3	50
81.7	15.3	50	81.7	15.3	50
86.3	10.7	39	86.3	10.7	39
90.5	6.5	28	90.5	6.5	28
91.6	5.4	12	91.6	5.4	12
92.7	4.3	4	92.7	4.3	4
92.9	4.1		92.9	4.1	
92.3	4.7	11	92.3	4.7	11
83.8	13.2	24	83.8	13.2	24
79.0	18.0	35	79.0	18.0	35
77.3	19.7	50	77.3	19.7	50

92.9
4.1

Sta + π - Elev

992.04

9 + 93

2.3
1.6

10

+50

+97 S. Rail

BM 3.51 998.10 2.45 994.59 (994.59)

+04.4 N. Rail

+16.75 Track

FH
AM
LC
RT

£

Oct 19, 1955
Oct 21, 1955

27

11

RT

81.0	81.0	81.0	80.5	78.5	78.0
15.9	14.0	15.9	16.5	18.5	19.0
50	26		38	43	50

	81.0	
1.0	15.9	1.0

82.2	82.1	82.3
14.8	14.9	14.7
50		50

82.84
14.20
Rail

Top 2 iron 33 1/2 + 56 1/3 + 149 1/5 Rail of South side track

82.82
15.28

83.08
15.02
Rails

294
11.08
15.02

Sta + π - Elev

998.10

11 + 31.95 $\neq$ Track

+47.08 $\neq$ Track

+62.1 $\neq$ Track

+78.5 $\neq$ Track

+93.97 $\neq$ Track

12 + 11.29 $\neq$ Track

£ Oct 21, 1955

28

83.26

14.84
Rails

83.41

14.69

83.60

14.50

83.65

14.45

84.52

13.58
50' Along Track

84.53

13.57

84.52

13.58
50' Along Track

84.19

13.91

Sta + π - Elev

998.10

12+23 Gutter Parallel to Tracks

+25 Rt. Angle

+50

+71

13+18
30
88

+88

13

Oct. 21, 1955

29

82.4	82.1	82.2	81.8	82.0
15.7	16.0	15.9	16.3	16.1
100'P	50'P		50' parallel to road	Tracks
95.6	88.9	82.2		
2.5	9.2	15.9	Tracks	
67	50	19		
	AA			

93.2	94.1	93.8	86.5	85.0	83.5	81.9
4.9	4.0	4.3	11.6	13.1	14.6	16.2
50	39	29	10		15	50

92.3	92.3	93.2	93.6	94.8	84.8	83.6	84.4
5.8	5.8	4.9	4.5	3.3	13.3	14.5	14.7
50	27	20	10		22	33	50

92.2	92.5	92.9	93.8	95.0	89.2	83.1
5.9	5.6	5.2	4.3	3.1	8.9	15.0
50	28	10		17	36	50

93.9
4.2

Sta + π - Elev

998.10

13+17.92

+50

T.P. 7.13 1002.31 2.92 995.18

+50

14

+50

TP 2.70 1004.37 0.64 1001.67

B.M. 1007.57 9.78 994.59

14+75 on next page

15

B.M. 6.61 1007.08 3.90 1000.47

Oct 21, 1955 30

LT			RT		
92.1	92.7	93.3	94.1	95.3	97.0
6.0	5.4	4.8	4.00	2.8	1.1
50	28	14		17	38

94.1
4.0

92.0	92.6	92.1	93.0	94.1	95.4	97.2	98.1
10.3	9.7	10.2	9.3	8.2	6.9	5.1	4.2
50	40	21	3		16	34	50

94.8	96.0	94.5	95.3	95.9	96.5	97.5	98.1
7.5	6.3	7.8	7.0	6.4	5.8	4.8	4.2
50	43	33	12		17	38	50

96.8	98.2	98.8	99.5	99.6	00.3	00.8	01.4
5.5	4.1	3.5	2.8	2.7	2.0	1.5	0.9
50	22	9	7		19	37	50

Nail 10, 12 from Pine

2" IRON LT - STA 13+40

95.6	94.1	91.9	91.2	92.3	90.9	98.0	96.2	94.4
11.2	0.3	2.5	3.2	2.1	3.5	6.4	8.2	10.0
50	45	37	26	12		13	28	50

LT 40' 10" W.O.R

Sta + π - Elev

100708

14+75

15+16

+35

TP 5.80 999.70 13.18 993.90

+73

16

+50

FX
AM
LC
JB

Oct. 24, 1953
cool clear 35°

31

00.1	99.1	99.6	01.9	02.6	01.4	01.1	01.7
7.0	8.0	7.5	5.2	4.5	5.7	6.0	5.4
50	29	11	4		18	38	50

04.8		02.6	98.7	96.9	94.0	91.5	89.3
2.3	4.5	8.4	10.2	13.1	15.6	17.8	
50	27	8		12	29	50	

01.9	99.5	95.2	90.7	89.4	87.1	
5.2	7.6	11.9	16.4	17.7	20.0	
50	32	16		30	50	

89.6	88.5	86.4	87.4	87.5	86.5	
10.1	11.2	13.3	12.3	12.2	13.2	
50	31	16		25	50	

90.0	87.1	86.9	86.3	86.1	86.1
9.7	12.6	12.8	13.4	13.6	13.6
50	25		18	31	50

91.6	90.1	87.5	86.9	86.1	86.0	86.0
8.1	9.6	12.2	12.8	13.6	13.7	13.7
50	47	25		21	33	50

Sta + π - Elev

999.70

17

+50

TP 10.30 1002.09 7.91 991.79

+80

BM 0.46 1001.63 1001.64

18

+50

TP 4.37 994.27 12.19 989.90

19

Oct 24, 1955 32

Lt				Rt			
94.7	91.9	89.5	88.6	87.5	86.8	86.3	86.1
5.0	7.8	10.2	11.1	12.2	12.9	13.4	13.6
4.7	36	24	16		18	38	50

98.0	98.1	95.9	91.4	90.8	88.8	87.3	
1.7	1.6	3.8	8.3	8.9	10.9	12.4	
50	26	16	4		23	50	

96.8	99.7	99.7	98.1	95.7	90.4	88.9	87.3
5.3	24	24	40	6.4	11.7	13.2	14.8
50	36	23	11		26	38	50
Spk. in		10" oak	33'	Lt	P.O.T.		

92.9	95.9	98.6	96.7	94.4	90.6	88.7	88.3
9.2	6.2	3.5	5.4	7.7	11.5	13.4	13.8
50	31	13		15	31	47	50

89.8	91.8	93.1	93.5	91.2	
12.3	10.3	9.0	8.6	10.9	
50	20		21	50	

87.4	87.8	89.1	90.0	90.7	91.7	91.9
6.9	6.5	5.2	4.3	3.6	2.6	2.4
50	25	20		24	36	50

Sta + π - Elev

994.27

19+30

+50

20

TP 5.86 997.85 2.28 991.99

+50

21

+50

11/ 987.14 81
713 74 70 6.1 5.1 4.5
Water 10 17 37 50
Surface

86.9 87.0 87.0 87.0 87.1
74 73 7.3 7.3 72
50 24 25 50

86.9 86.9 86.8 87.0 87.0
74 74 7.5 7.3 73
50 25 24 50

87.3 87.4 87.3 87.2 87.1
10.6 10.5 10.6 10.7 10.8
50 26 23 50

88.1 87.9 87.6 87.4 87.6
9.8 10.0 10.3 10.5 10.3
50 23 17 50

988.80 988.7 988.8 989.6 990.5 991.4 992.1 991.9
905 92 9.1 8.3 7.4 6.5 5.8 6.0
Water 50 38 18 19 37 50
Surface

Sta + π - Elev

997.85

22

+50

TP 6.81 1001.84 2.82 995.03

23

+50

24

+50

TP .542 1002.82 4.44 997.40

Oct 24, 1955 34

Lt		Rt	
90.4	90.9	91.9	92.6
7.5	7.0	6.0	5.3
50	32	27	17
93.7	93.8	92.3	92.0
4.2	4.1	5.6	5.9
23	23	45	50

93.6	93.4	95.2	94.9	93.9	93.3
4.3	4.5	2.7	3.0	4.0	4.6
50	34	26	20	20	50

01.1	98.9	97.3	95.6	94.8	94.0	94.6
0.7	2.9	4.5	6.2	7.0	7.8	7.2
50	27	15	12	12	32	50

02.4	99.1	98.0	96.6	95.7	94.6	94.8
+0.6	2.7	3.8	5.2	6.1	7.2	7.0
50	29	17	10	10	30	50

00.2	00.8	00.3	98.5	97.2	95.4	94.2
1.6	1.0	1.5	3.3	4.6	6.4	7.6
50	46	33	17	23	23	50

95.85	96.7	97.8	98.0	97.2	96.1	95.4
5.99	5.1	4.0	3.8	4.6	5.7	6.4
Water surface	34	20	16	16	32	50
35						

Sta + π - Elev

1002.82

25

+50

+86

26

+10

+36.75

+50

Oct 24, 1955

35

Lt

Fl

97.4	97.4	96.4	95.9	94.4	94.6	94.5
5.4	5.4	6.4	6.9	8.4	8.2	8.3
50	31	15		10	26	50

96.6	96.5	96.2	95.2	94.4	94.3	94.0
6.2	6.3	6.6	7.6	8.4	8.5	8.8
50	38	20		5	22	29

96.8	96.7	96.6	95.6	95.2	94.9
6.0	6.1	6.2	7.2	7.6	7.9
50	32	17		21	50

95.8	96.9	98.1	98.4	97.8	97.6	97.8
2.0	5.9	4.7	4.4	5.0	5.2	5.0
39	19	12		13	37	50

Edge Pond

96.7	98.2	98.3	98.1	98.0	97.9	98.7	98.6	98.1
6.1	4.6	4.5	4.7	4.8	4.9	4.1	3.2	0.1
25	20	12		25	50	75	100	15

Pond 25

97.1	96.5	97.3	98.1	98.3	98.6	98.5	97.4	96.8	96.8
5.7	6.3	5.5	4.7	4.5	4.2	4.3	5.4	6.0	6.0
50	33	22	19	9		10	30	39	50

98.7
41

Sta + π - Elev

1002.82

27

+ 50

+ 72

BM

4.29 998.53 (998.57)

Oct 24, 1955

36

Lt

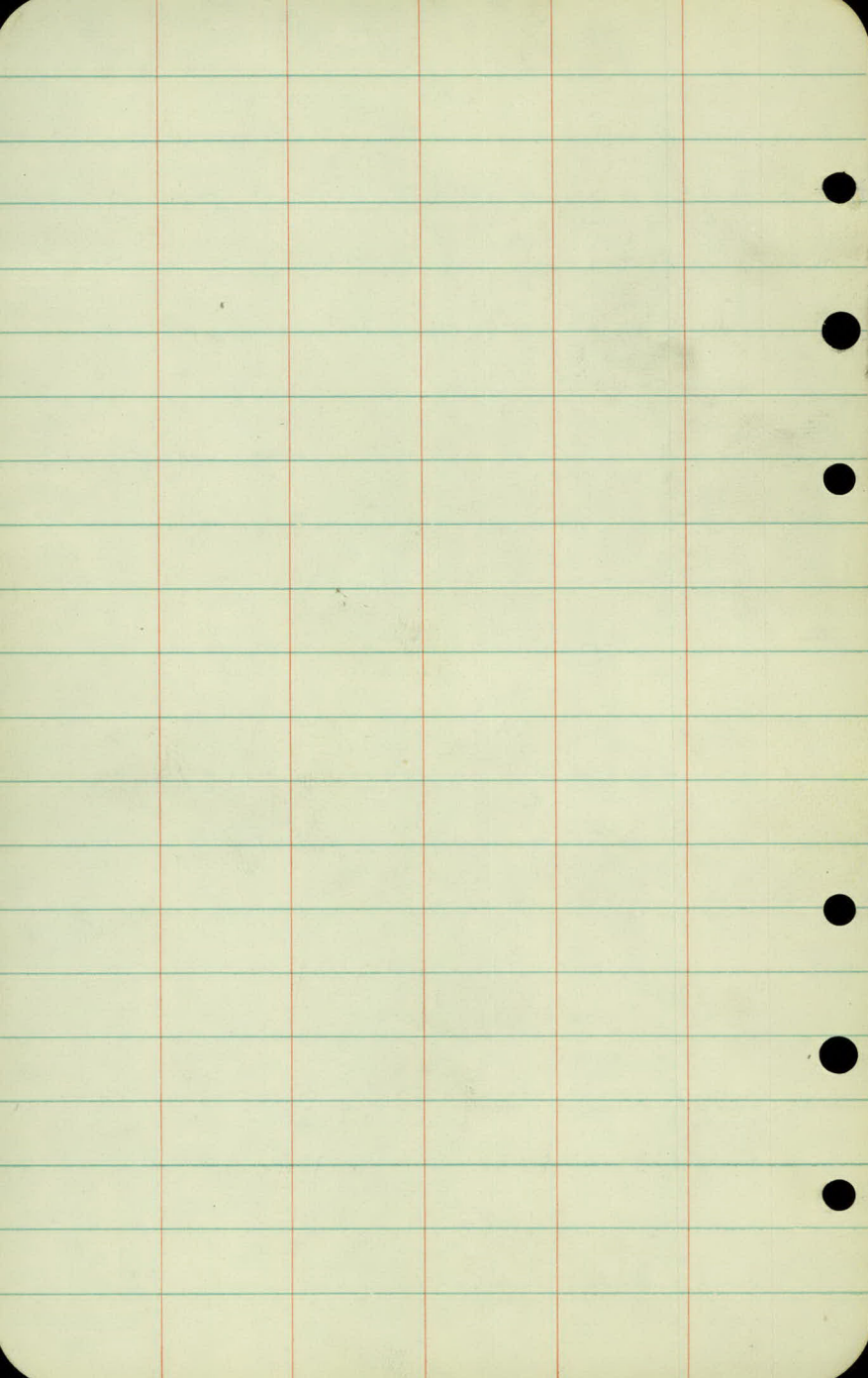
Rt

30
99.8

1.1
01.7

0.0
02.8

Spike in Arc Light Pole N.E. Cor Arlington & East Ave



Auger
Soundings

# 10	Sta 16	£
Feet	Material	
0-1	Peat	
1-2	Peat + Sand	
2-3	Sand	

# 9	Sta 16+50	£
Feet	Material	
0-1	Vegetation	
1-2	sand	

# 8	Sta 17	£
Feet	Material	
0-1	Peat	
1-2	Peat	
2-3	sand	

FX
CW
AB

Feb. 7, 1956
clear 20°

38

#7 Sta 21+32 E

Feet	Material
0-1	Peat
1-2	Gumbo
2-3	sand

#6 Sta 19+24 E

Feet	Material
0-1	Peat
1-2	Gumbo
2-3	Gumbo
3-4	Muck
4-5	Blue Clay
5-6	Sand

#5 Sta 19+60 £

Feet	Material
0-1	Vegetation
1-2	Peat
2-3	Peat
3-4	Muck
4-5	Blue Clay
5-6	Sand

4A Sta 20+47 £

Feet	Material
0-1	Vegetation
1-2	Peat
2-3	
3-4	Muck
4-5	
5-6	
6-7	Sand

#3

Sta 20+97

±

Feet	Material
0-1	Vegetation
1-2	Peat
2-3	Gumbo
3-4	Muck
4-5	Blue Clay
5-6	Sand

#2

Sta 25+00

2' Rt.

Feet	Material
0-1	Peat
1-2	Muck
2-3	Sand

#1 Sta 25+80 2' Rt

Feet

Material

0-1

1-2

2-3

3-4

4-5

5-6

peat

Muck

Sand

FK
AB
CW

Feb 9, 1956

40

EAST AVE.

X-section Extensions

Sta	+	π	-	Elev
BM.	8.52	1003.11		994.59

13+50

14

+50

✓

TP	8.50	1009.49	2.12	1000.99
----	------	---------	------	---------

+75

2

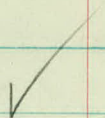
Feb. 9, 1956

41

RT

Top 2' Iron Pipe 33' Lt Sta 13740

97.1	88.1
6.0	15.0
54	71

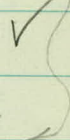


98.5	99.5	99.5	94.1	91.9
4.6	3.6	3.6	2.0	11.2
52	71	87	97	100



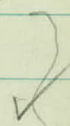
01.7	02.5	01.4	01.8	01.7	01.8
1.4	0.6	1.7	1.3	1.4	1.3
62	79	84	89	100	118

88.6	95.2	97.0	01.2	01.7
14.5	2.9	6.1	1.9	1.4
170	154	148	137	127



02.3	03.0	03.5	03.7	06.3	06.9
7.2	6.5	6.0	5.8	3.2	2.6
60	77	94	100	129	147

93.3	94.9	05.3
16.2	14.6	4.2
200	195	170



Sta + π - Elev

1009.49

15

00.9 ✓

✓
+35

Level out from 50' to 300

BM 5.40 999.99

994.59

13 + 17.92

+50

14

2

Feb. 9, 1956

42

BT

1000.9

	97.0	98.6	98.8	01.1	03.0
8.6	12.5	10.9	10.7	8.4	6.5
	60	82	100	123	140

97.5	99.7	00.0	01.2	02.6	✓
12.0	9.8	9.5	8.3	6.9	
220	210	200	177	160	

Top 2' Iron pipe 33' Lt Sta 13+40

84.8	83.9	
15.2	16.1	✓
57	66	

84.3	81.5	
15.7	18.5	✓
79	93	

84.6	82.7	
15.4	17.3	✓
121	134	

Sta	+	π	-	Elev
-----	---	-------	---	------

		999.99		
--	--	--------	--	--

14+50				
-------	--	--	--	--

+75				
-----	--	--	--	--

15				
----	--	--	--	--

BM				
----	--	--	--	--

	5.40	994.59		
--	------	--------	--	--

£

Feb. 9, 1956

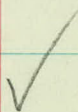
43

RT

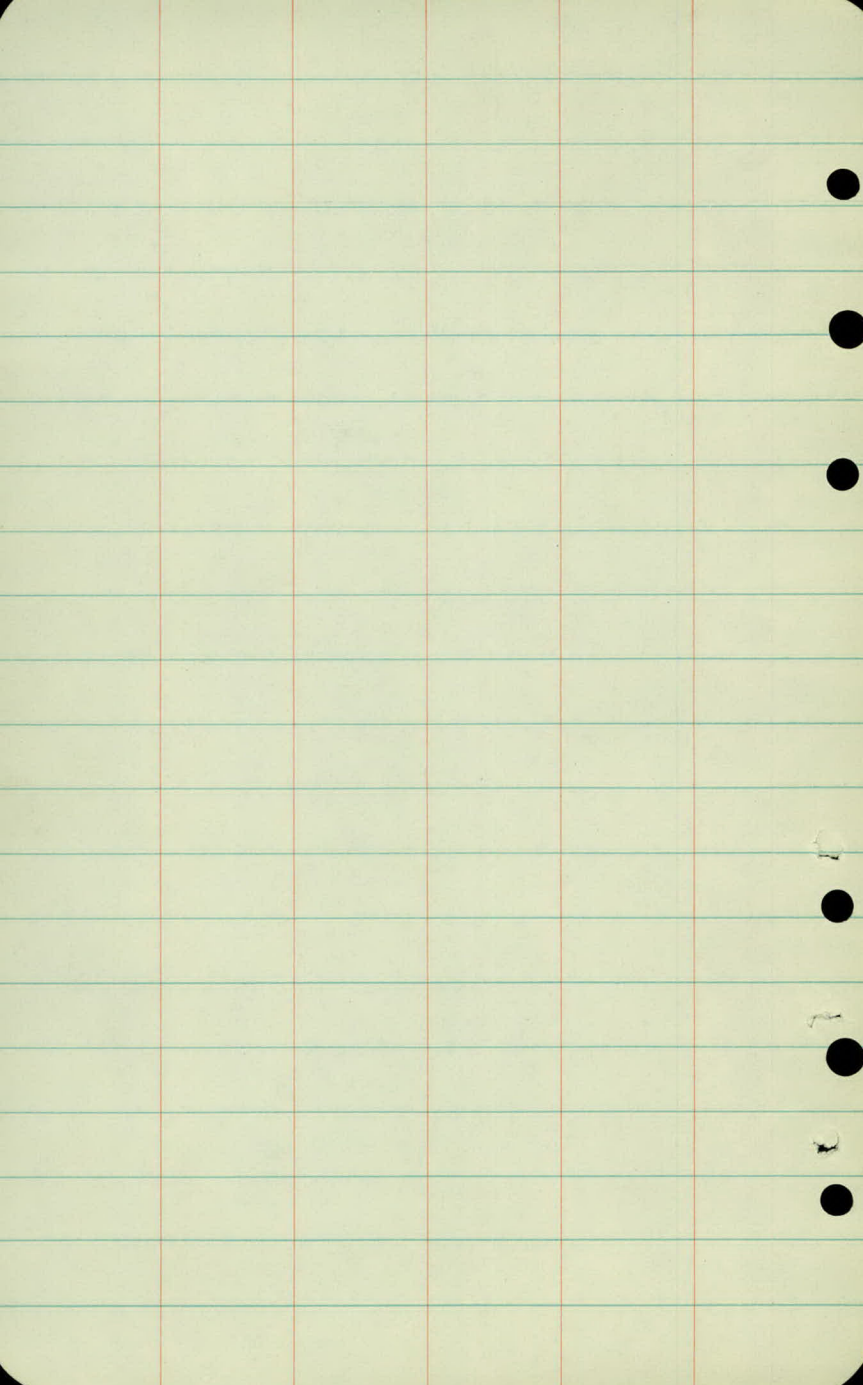
83.6	81.8
16.4	18.2
190	205

90.6	83.6	81.0
9.4	16.4	12.0
223	254	275

90.0	85.1	81.5
10.0	14.9	18.5
254	277	300



Top 2' Iron Pipe 33' Lt Sta 13+40



FR
LC
AB
CW

Feb 9, 1956

44

EAST AVE.

X-section Extensions

Sta	+	π	-	Elev.
-----	---	-------	---	-------

BM	3.70	998.29		
----	------	--------	--	--

				999.59
--	--	--	--	--------

12 +25				
--------	--	--	--	--

✓				
---	--	--	--	--

+ 50				
------	--	--	--	--

✓				
---	--	--	--	--

+ 71				
------	--	--	--	--

+ 88				
------	--	--	--	--

Feb 9, 1956

L

45

Lt

Top 2' Iron pipe 33' Lt Sta 13140

91.0	91.0	90.1	90.1	90.0	94.1
7.3	7.3	8.2	8.2	8.3	42"
173	151	126	100	91	73

✓

90.7	90.7
7.6	7.6
94	200

92.7	92.4	91.9	91.6	91.3	92.0	93.6
5.6	5.9	6.4	6.7	7.0	6.3	4.7
188	161	142	120	100	75	51

✓

92.8
5.5
200

93.1	92.8	92.7	92.4	92.3	92.0	92.2	92.2
5.2	5.5	5.6	5.9	6.0	6.3	6.1	6.1
200	181	158	139	121	100	83	61

92.6	92.3	92.2	92.1	92.1	92.0	92.0
5.7	6.0	6.1	6.2	6.2	6.3	6.3
200	176	150	128	100	80	62

Sta + π - Elev
998.29

13+17.92

X-Sections at Rt. Angle to Tracks

0+00 $\angle$ East Ave & North rail

1

+50

2

Feb. 9, 1956

46

Lt

93.6	93.4	93.1	92.8	92.6	92.5	92.5	92.1
4.7	4.9	5.2	5.5	5.7	5.8	5.8	6.2
200	191	167	143	120	100	82	61

Lt

Rt

84.2	83.4	82.3	85.3	91.4	89.7	89.7
14.1	14.9	16.0	13.0	6.9	8.6	8.6
Rail	5	11	16	30	48	54

84.3	83.8	82.1	85.7	89.7	90.0	90.6	91.0
14.0	14.5	16.2	12.6	8.6	8.3	7.7	7.3
Rail	5	10	16	28	43	62	82

84.3	83.7	82.7	85.0	89.8	89.8	91.2
14.0	14.6	15.6	13.3	8.5	8.5	7.1
Rail	8	10	15	26	46	60

89.5	94.7	94.3
8.8	3.6	4.9
100	8.3	6.7

Stockpile

Sta + A - Elev

998.29

2+50

Additional sections would be similar.

BM

3.71

994.58

994.52

2

Feb 9, 1956

47

RT

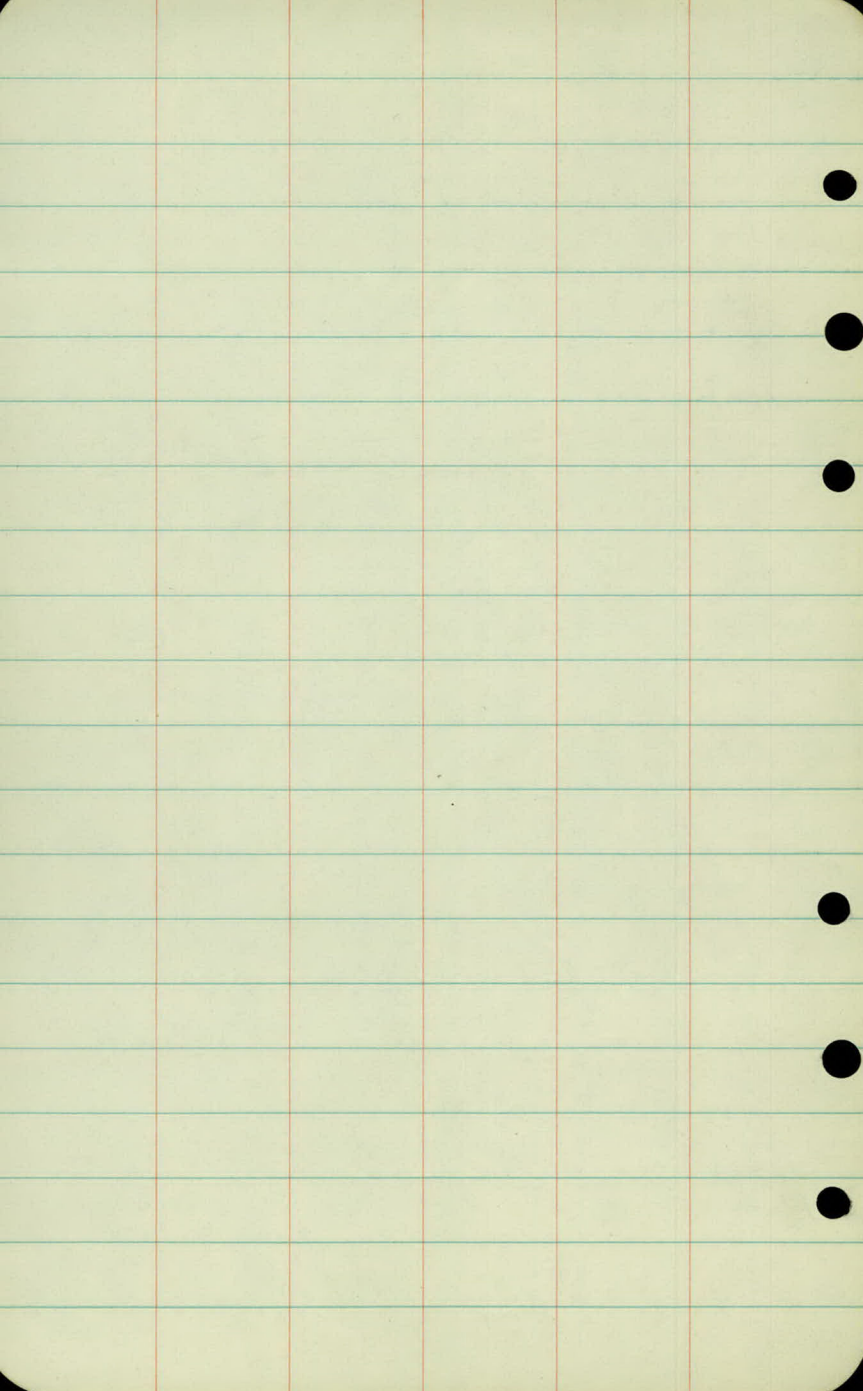
84.3	83.8	82.8	89.6	89.6	90.6	95.0
140	14.5	15.5	8.7	8.7	2.7	3.3
Rail	5	10	27	43	56	67

stockpile

89.8	89.7	95.6
8.5	8.6	2.7
105	95	85

stockpile

Top 2' Iron Pipe 33' Lt. Sta 13+40



FA
RG
RC
RP

Oct 15, 1956
Fair 70°

48

East Ave
Maryland to Arlington

New x-sections

Sta + π - Elev ✓

BM 795 1009.59

1001.64

TP 3.23998.89 12.93 996.66

12 + 71

✓

+ 82

✓

+ 86

Oct. 15, 1956

49

Lt

Rt

Spike in 10" oak 33' Lt of POT 15+16

93.0	94.1	94.5	94.6	93.6	89.7	86.6
6.9	5.8	5.4	5.3	6.3	10.2	13.3
26	16	4		3	9	15

93.7	93.8	93.7		83.9	84.1	84.7
6.2	6.1	6.2		1.0	16.0	15.8
32	46	50		50	41	28

93.4	93.1	93.3	93.5	94.5	93.6	93.1	93.5	92.9
6.5	6.8	6.6	6.4	5.4	6.3	6.8	6.4	7.0
50	41	24	9	4	6	16	28	39

					83.6	87.1	89.5	90.6
					1.0	16.3	12.8	10.4
					65	57	50	47

92.7	92.6	92.7	92.9	92.7	92.6	92.4	90.9
7.2	7.3	7.2	7.0	7.2	7.3	7.5	9.0
50	39	17		16	37	47	50

1.0	17.0	13.7	10.8
72	63	56	

Sta + π - Elev

999.89

13

✓

+02

✓

BM 5.89 999.86 5.92 993.97

10.08

+17.92

Oct. 15, 1956 50

	LT		RT
92.44	92.3	92.4	92.6
7.45	7.6	7.5	7.3
50	44	26	13
CB(Top)			

89.37			
10.52			
50			
FLCB			

91.46	91.6	91.6	91.8	92.1	92.2	92.7	92.9	93.0
8.43	8.3	8.3	8.1	7.8	7.7	7.2	7.0	6.9
50	40	27	12		11	29	44	51
FLinv								

RR Spike 16" Oak 70' Lt sta 13+65

92.1	82.38	92.46	92.2	92.4	92.8	92.9	93.1
7.8	17.48	7.40	7.7	7.5	7.1	7.0	6.8
14	FL	Top MH		15	32	44	50
	TO						

91.8	91.8		
8.1	8.1		
32	50		

Sta + π - Elev

999.86

13+34

✓

✓

+36

+49

2 Oct. 15, 1956 51

91.6
 8.3
 50
 91.35
 8.51
 41
 91.8
 8.1
 28
 91.9
 8.0
 12
 92.0
 7.9
 9
 92.0
 7.9
 17
 92.2
 7.7
 24
 92.3
 7.6
 31
 92.3
 7.6
 FL 10x

90.2
 9.7
 67
 86
 63
 91.3
 9.6
 60
 93.3
 6.6
 59
 93.0
 6.9
 45
 92.7
 7.2
 45
 86.6
 13.3
 71
 82.7
 17.2
 81

89.54
 10.32
 FL
 41
 92.40
 7.46
 7.6
 31
 92.3
 7.6
 16
 92.3
 7.6
 13
 92.6
 7.3
 13
 92.6
 7.3
 29
 92.7
 7.2
 44
 92.6
 7.3
 50
 92.9
 7.0

92.3
 7.6
 50
 82.6
 10.1
 80
 86.4
 13.5
 72
 89.7
 10.2
 68
 92.9
 7.0
 61

92.8
 7.1
 50
 92.8
 7.1
 32
 93.1
 6.8
 14
 93.1
 6.8
 12
 93.1
 6.8
 27
 93.1
 6.8
 43
 92.9
 7.0
 60
 93.3
 6.6

82.0
 10
 17.9
 89
 84.5
 15.4
 74
 90.5
 9.4
 65

Sta + π - Elev

999.86

13+55

Oct 15, 1956

52

LT

RT

92.2	92.4	93.1	92.9	94.6	94.9	95.6	95.6	96.5
7.7	7.6	6.8	7.0	5.3	5.0	4.3	4.3	3.4
50	33	18	6		7	18	22	25

89.2	93.0	98.5	97.4
10.7	6.9	1.4	2.5
66	59	51	34

89.3	85.9	83.8
10.6	14.0	16.1
69	72	81

Sta IVY ST West
+ + - Elev

999.86

0+50

✓

✓

✓

TP 1.94 997.36 7.44 992.42

+50

Oct 15, 1956 53

11

84

92.44	91.7	91.7	91.8	91.9	91.6	92.3	92.8
7.42	8.2	8.2	8.1	8.0	8.3	7.6	7.1
17	17	10		9	16	18	31
Top CB							

92.8	94.1	93.8	94.2
7.1	5.8	6.1	5.7
33	41	48	49

95.7	93.6	92.4	92.1
4.2	6.3	7.5	7.8
65	54	47	35
Cor Green Rim			

92.4	92.2	93.2	94.0
7.5	7.7	6.7	5.9
66	62	59	55

95.9	91.7	86.2
4.0	8.2	13.7
78	85	96

82.3	82.3	83.6	85.6
15.1	15.1	13.8	11.8
119	117	109	100
Di. 4.6			

84.14
13.22
128

Sta + π - Elev

997.36

1

✓

✓

✓

✓

Oct 15, 1954 54

LT

RT

93.2	92.9	92.2	92.0	92.2	92.0	92.6	93.0	92.1
42	45	5.2	54	5.2	5.4	4.8	4.4	5.3
33	19	17	11		16	19	31	35

95.1	94.1	93.9	93.6
23	3.3	3.5	3.8
39	53	67	77

93.9	93.6	92.8
3.5	3.8	4.6
61	51	48

Green Rim Green

93.2	89.5	90.6	91.4
4.2	7.9	6.8	6.0
115	100	90	85

90.7	86.7	82.3
6.7	10.7	15.1
123	132	143

84.16
13.20
153

Sta + π - Elev

997.36

1+50

✓

✓

✓

2

Oct 15/1956 55

R1

11

27	29	40	50	47	51	45	41	39
38	34	19	16		15	18	32	50
94.7	93.5	93.4	92.4	92.7	92.3	92.9	93.3	93.5

25	29	34	59
46	67	79	93
94.9	94.5	94.0	91.5

77	75	71	71
141	130	115	97
89.7	89.9	90.3	90.3

81	115	151	1321
150	159	167	177
89.3	85.9	82.3	84.15

29	35	37	48	44	44	47	42	38
42	37	19	16		7	16	17	33
94.5	93.9	93.7	92.6	93.0	93.0	92.7	93.2	93.6

31	18	46	73					
62	64	72	100			60	47	
94.3	95.6	90.8	90.1			94.4	94.4	

Sta + π - Elev

997.36

2

✓

11 50

Top

4.21

+46.5 MH on L FL

15.71

+50

✓

✓

✓

B M

3.39 993.97

Oct 15, 1956

56

LT

BT

89.6

87.8

89.4

87.6

7.8

7.6

8.0

7.8

164

151

149

120

88.9

86.0

82.9

84.16

85

114

14.5

13.20

177

185

191

201

94.9

94.0

93.8

93.0

93.1

92.9

92.8

93.4

93.6

2.5

3.4

3.6

4.4

4.3

4.5

4.6

4.0

3.8

45

37

20

17

8

16

17

23

94.7

95.4

94.5

90.5

94.6

94.5

93.8

2.7

2.0

6.9

6.9

2.8

2.9

3.6

55

58

66

83

56

45

33

89.2

84.8

87.8

90.1

8.2

7.6

7.6

7.3

163

142

120

100

89.0

90.1

90.4

89.4

8.4

7.3

7.0

8.0

170

172

174

185

84.19

82.6

87.1

89.3

13.17

14.8

14.3

8.1

226

218

207

200

KP	Bob	Ray	FK
----	-----	-----	----

14	0	8	4
----	---	---	---

14	4	11	23
----	---	----	----

14	25	11	28
----	----	----	----

20	26	29	29
----	----	----	----

24	26	48	32
----	----	----	----

46	28	50	32
----	----	----	----

46	54	76	58
----	----	----	----

65	55 18	82 3	58
----	----------	---------	----

65	73	85	63
----	----	----	----

East Ave

Maryland to Arlington

New X-Sections

Sta	+	π	-	Elev
BM	789	983.14		975.25

0+03

2

+50

3

+30

+43

Oct 16, 1956 $\pm$ 58

LT

Top Hyd N.W. Cor Maryland & East Ave

64.44
18.70
FL
10

70.65
12.49
Top MH
10

81.0
2.1
50

80.7
2.4
42

80.1
3.0
29

78.8
4.3
23

77.2
3.9
18

79.4
3.7
10

79.9
3.2

✓

80.4
2.7
50

80.2
2.9
42

80.3
2.8
28

80.5
2.6
19

80.7
2.4

✓

80.2
2.9
50

80.3
2.8
38

81.2
1.9
25

81.0
2.1
10

80.7
2.4

✓

68.39
14.75
FL
20

82.71
0.43
Top MH
20

65.61
17.53
FL
10

82.76
0.38
Top MH
10

Sta + π - Elev

983.14

3+43 $\pm$ Nokamos.

TP 9.24 991.96 0.12 982.72

+73

4

+50

5

+50

Oct 16, 1956

L

59

Lt

81.4	81.5	81.9	82.3	82.8	82.7	82.2
1.7	1.6	1.2	0.8	0.3	0.4	0.9
75	71	52	33	22	10	

83.5	83.6	84.1	84.3	83.8	83.9	83.2
8.5	8.4	7.9	7.7	8.2	8.1	8.8
50	43	34	24	21	11	1

86.2	86.3	86.1	84.7	85.1	85.3
5.8	5.7	5.9	7.3	6.9	6.7
50	34	24	21	18	12

88.4	88.1	88.0	87.4
3.6	3.9	4.0	4.6
50	35	25	24

90.2	90.1	89.7	89.2
1.8	1.9	2.3	2.8
50	45	31	24

90.7	90.7	90.4	89.9
1.3	1.3	1.6	2.1
50	47	31	26

Sta + π - Elev
991.96

6

+ So. P.L. Tilson Dr.

+ £ Tilson Dr

+ £104

+ N.P.L. Tilson Dr

✓

1.43

990.53

990.60

Oct 16, 1956

60
d

W

20.6	90.5	89.9
1.4	1.5	2.1
50	36	29

90.3	90.4	90.3
1.7	1.6	1.7
50	39	31

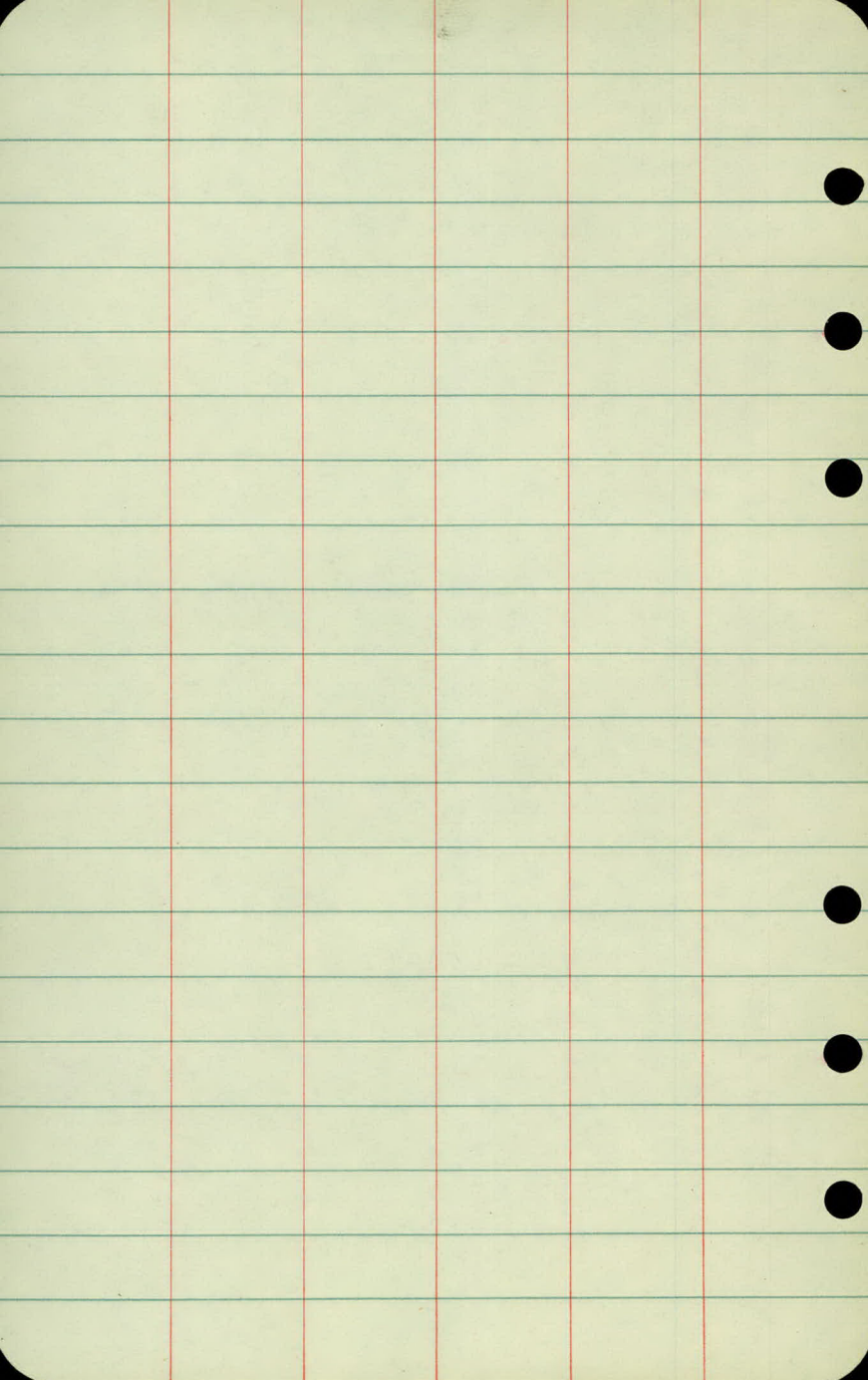
89.8	90.6	91.0
2.2	1.4	1.0
50	39	30

77.17	88.37
14.79	3.59
FL	Top MH
	75

90.1	90.5	90.2	90.6
1.9	1.5	1.8	1.4
50	44	41	35

(Damaged)

Top S. End Ent Culvert Rt 6+65⁺



144 St Topog

2
 17.5
 16.3

2

$$+00 \frac{12''0}{48}$$

$$+39 \frac{29''0}{40}$$

$$+11 \frac{5''0}{42}$$

$$+14 \frac{18''6}{35}$$

$$+09 \frac{3-12''0}{41}$$

$$+00 \frac{5''0}{47}$$

$$+05 \frac{5''0}{46}$$

$$+94 \frac{12''0}{45}$$

$$+85 \frac{10''0}{46}$$

$$+92 \frac{24''0}{41}$$

$$+81 \frac{5''0}{49}$$

$$+60 \frac{15''0}{44}$$

$$+69 \frac{2-16''0}{44}$$

0+00

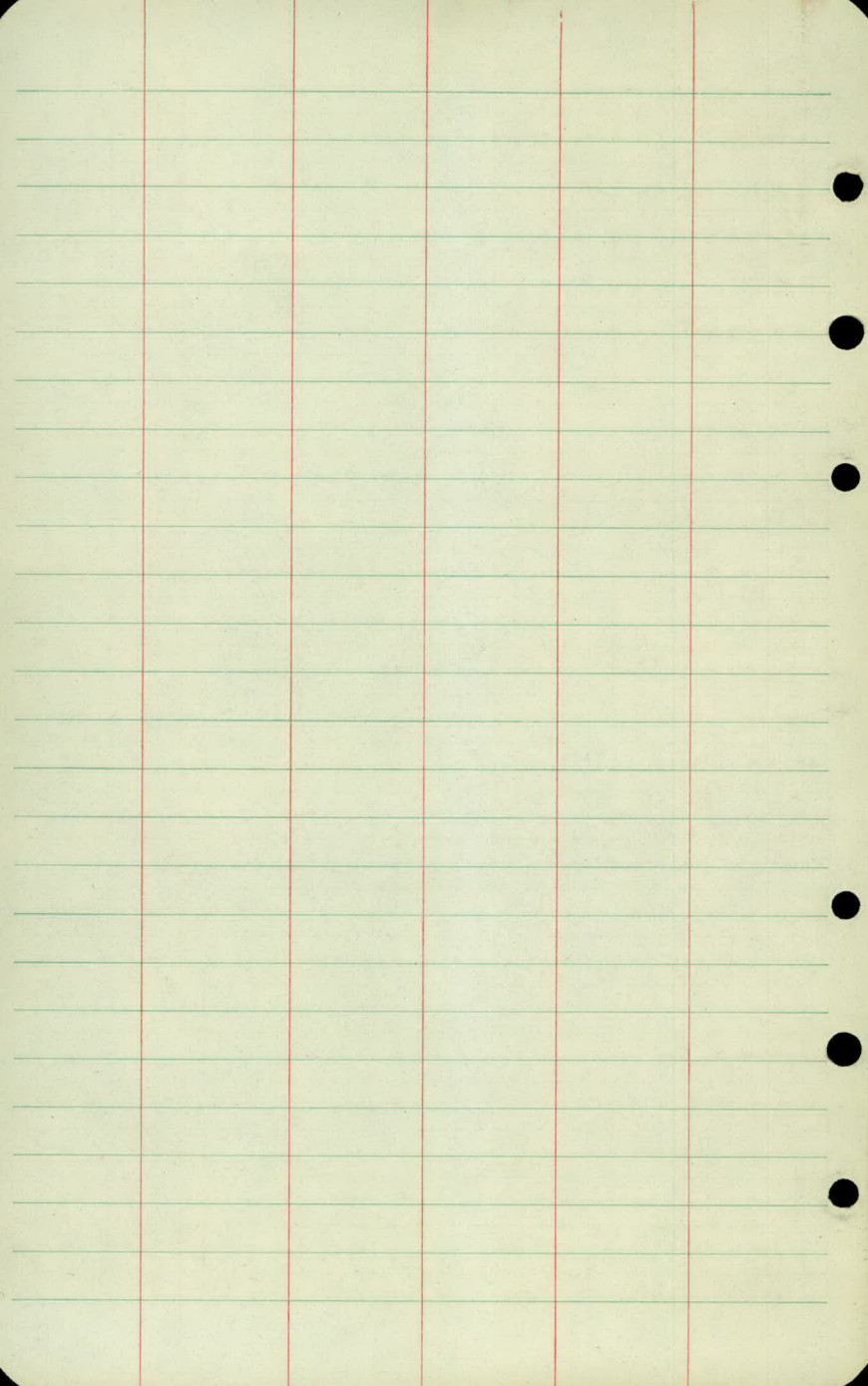
FA
RG
KP
JT

Oct. 11, 1956

62

Fair 74°





FK
RG
KP
CW

Nov 25, 1957 1

East Ave
Maryland to Arlington
Finals

Platted
Comp 12/5/57

Sta + π - Elev

BM 5.60 980.85

975.25

0+00 £ Mary land

+16 Gutter Line

+23

+30

✓

+50

2 Nov. 25, 1957

17

81

2

Top Hyd NW. Cor E. Ave & Maryland

71.6	71.2	70.8	70.4	69.8	69.1	68.8
9.3	9.7	10.1	10.5	11.1	11.8	12.1
50	36	15		17	44	62

✓

71.3	70.8	70.8	70.8	70.2	69.5	69.1
9.6	10.1	10.1	10.1	10.7	11.4	11.8
50	33	18		16	33	50

✓

72.1	71.8	71.4	70.8	70.9	70.2	69.9	70.1	69.6	69.3
8.8	9.1	9.5	10.1	10.0	10.7	11.0	10.8	11.3	11.6
50	40	23	17		19	28	30	40	50

72.4	71.8	71.5	71.2	71.1	71.0	70.9	70.3	70.5	70.1
8.5	9.1	9.4	9.7	9.8	9.9	10.2	10.6	10.4	10.8
50	31	20	18	11		12	21	23	29

Walk

69.4 ✓

11.5 ✓
50

75.1	75.1	75.5	71.9	71.4	71.3	70.7	71.1	70.7	70.2
5.2	5.8	2.4	9.0	9.5	9.6	10.2	9.8	10.2	10.7
38	35	27	19	16		16	18	24	51

S.S.

slope stake

66.1	68.5	69.4
14.2	12.4	11.5
81	77	68

Sta + A - Elev

980.85

1+00

✓

+50

+72

?+82

Nov. 25, 1957

3

LT

£

RT

11.5	11.8	15.0	18.3	12.9	12.89	12.7	12.7	12.9	12.9
34	35	5.9	26	8.0	7.96	8.2	8.2	8.0	8.0
42	36	26	19	15		13	17	19	33

6.8	6.7	12.4
12.5	11.2	8.5
54	45	38

11.8	11.3	15.3	15.0	15.0	14.8	15.4	15.2	13.1	11.1
3.1	3.6	5.6	5.9	5.9	6.1	5.5	5.7	7.8	9.8
34	29	18	15		16	19	33	41	54
5.5									

11.4	11.4	16.6	16.0	16.1	15.9	15.7	16.1	16.0	14.3	14.2
3.5	3.5	4.3	4.9	4.8	5.0	5.2	4.8	4.9	6.6	6.7
50	44	24	17	11		17	20	35	43	50

11.28	11.21	11.3	16.4	16.4	16.1	16.5	16.5	15.1	14.9
3.57	3.64	3.6	4.5	4.5	4.8	4.4	4.4	5.8	6.0
30	25	21	16		17	20	34	42	51

Walk

18.3	19.7
2.6	12
34	43

Garage

Sta	+	π	-	Elev
		980.85		

2+00

✓

T.P.	8.43	988.08	1.20	979.65
------	------	--------	------	--------

+50

3

+13

2 Nov 25 1957

4

21

84

18.1	17.9	17.3	17.2	17.26	16.9	17.4	17.4	17.2	16.1
2.8	3.0	3.6	3.7	3.59	4.0	3.5	3.5	3.7	4.8
30	19	17	14		17	19	29	35	41

19.4 19.1

15.7

1.5 1.2
37 45

5.2
50

81.8	80.3	79.5	79.3	79.1	79.4	78.9	79.4	80.0	79.9	79.2
6.3	7.8	8.6	8.8	9.0	8.7	9.2	8.7	8.1	8.2	8.9
37	30	20	19	15		17	18	26	32	36

82.1

79.0

5.4
46

9.1
50

83.1	82.8	82.3	81.7	80.9	81.12	80.8	81.8	82.0	82.1
5.0	5.3	5.8	6.4	7.2	6.96	7.3	6.3	6.1	6.0
50	40	30	20	18		17	20	30	34

NG

82.8	82.8	82.8	82.0	81.3	81.1	81.2	82.2	82.4	82.5
5.3	5.3	5.3	6.1	6.8	6.4	6.9	5.9	5.7	5.6
50	30	25	19	16		17	20	29	32

NG

Sta	+	π	-	Elev
		988.08		

3+93

+73

4

BM	8.83	994.24	2.67	985.41
----	------	--------	------	--------

+50

✓

5

5+15 Nat. Gravel 20' Rt

2 Nov. 25, 1957

5

11

R1

$g^{3.2}$	$g^{2.9}$	$g^{2.5}$	$g^{2.8}$	$g^{2.4}$	$g^{3.7}$	$g^{2.4}$	$g^{4.5}$	
49	52	56	53	57	49	47	36	✓
50	28	15		17	20	29	32	
							NG	

$g^{3.8}$	$g^{4.1}$	$g^{3.8}$	$g^{3.2}$	$g^{3.8}$	$g^{3.6}$	$g^{4.2}$	$g^{4.2}$	$g^{5.3}$	$g^{6.3}$
4.3	3.7	4.3	4.9	4.3	4.5	3.9	3.9	2.8	1.8
50	30	19	18		18	19	29	31	39
									NG

$g^{5.8}$	$g^{5.5}$	$g^{5.0}$	$g^{4.4}$	$g^{4.2}$	$g^{4.85}$	$g^{4.4}$	$g^{4.6}$	$g^{5.1}$	$g^{5.2}$	$g^{7.6}$
23	26	3.1	3.7	3.9	3.23	3.7	3.5	3.0	2.9	0.5
40	30	20	18	17		17	19	20	30	34
Top Hyd N.W. Cor Nukomis & McKnight										NG

$g^{7.2}$	$g^{7.2}$	$g^{6.7}$	$g^{6.4}$	$g^{6.2}$	$g^{6.6}$	$g^{6.1}$	$g^{6.3}$	$g^{6.5}$	$g^{7.0}$	$g^{8.5}$
7.0	7.0	7.5	7.8	8.0	7.6	8.1	7.9	7.7	7.2	5.7
30	25	20	19	17		16	18	20	29	33
										NG

✓

$g^{5.7}$ $g^{5.9}$

8.5 8.3
41 50

$g^{8.5}$	$g^{8.4}$	$g^{7.6}$	$g^{7.6}$	$g^{8.00}$	$g^{7.6}$	$g^{7.7}$	$g^{8.1}$	$g^{8.6}$	$g^{8.8}$
5.7	5.8	6.6	6.6	6.24	6.6	6.5	6.1	5.6	5.4
30	19	18	16		18	20	22	29	31
									NG

✓

$g^{8.6}$ $g^{8.5}$

5.6 5.7
46 50

Sta + Δ - Elev

994.24

5+50

✓

6

✓

+32

✓

27

Nov. 25, 1957

6

RT

89.9	89.4	89.1	88.5	88.8	88.4	88.8	89.1
4.3	4.8	5.1	5.7	5.9	5.8	5.4	4.5
42	30	20	19		16	18	20
							NG

89.7

4.5
50

89.8	89.5	89.1	88.8	88.95	88.6	88.9	89.4	89.5
4.4	4.7	5.1	5.4	5.29	5.6	5.3	4.8	4.7
30	21	19	17		16	18	19	29

90.2

4.0
42

88.3

5.9
43

89.7	89.6	89.2	88.7	89.0	88.6	88.8	88.8	88.5
4.5	4.6	5.0	5.5	5.2	5.6	5.4	5.4	5.7
30	22	19	17		16	19	22	28

89.4

4.8
50

87.4

6.8
30

88.4

5.8
37

Sta + π - Elev

994.24

6 + 62

+ 92

7

BM

2.31 991.93 (991.91)

1.62 992.62 (992.60)

Nov 25, 1957

7

14

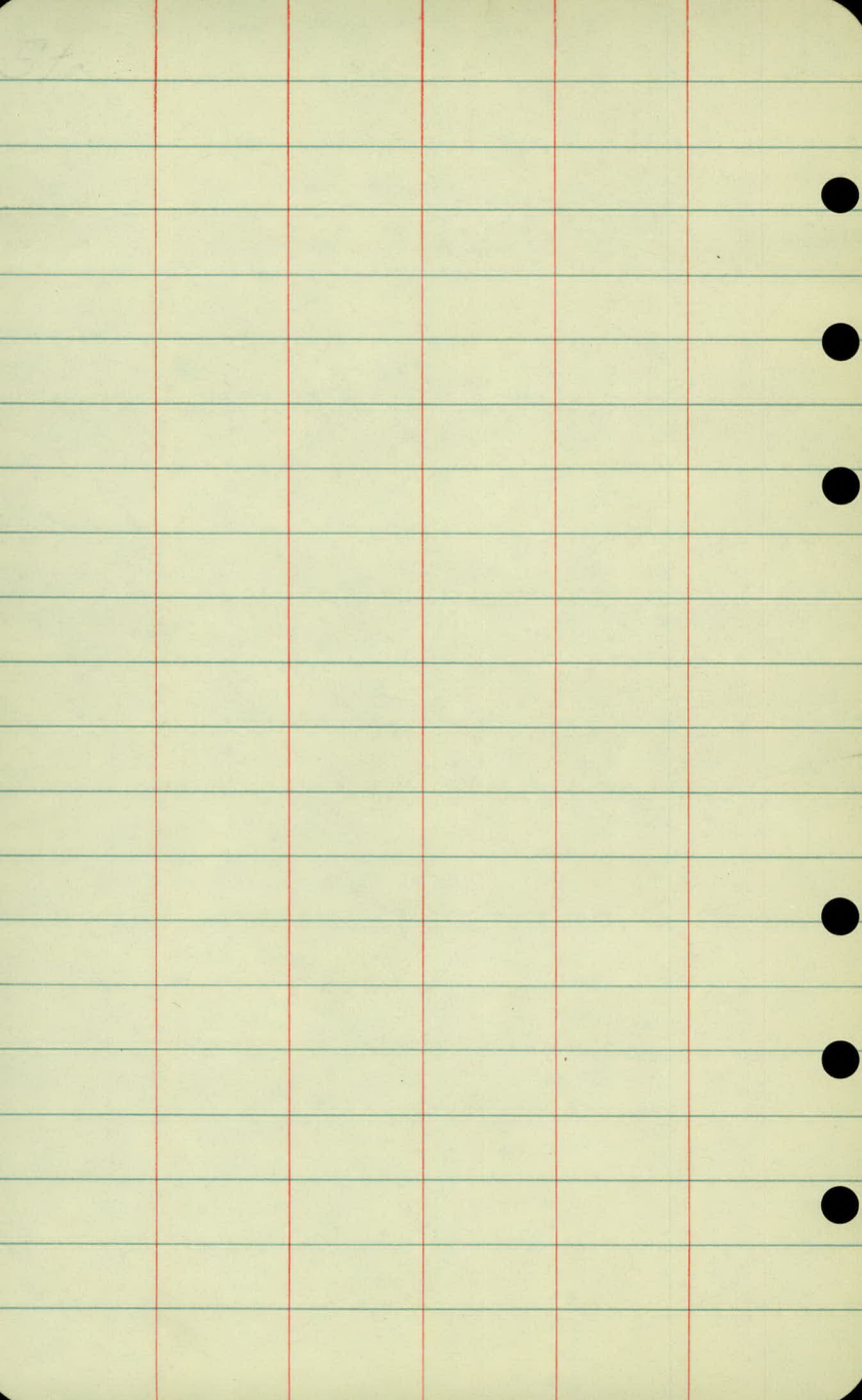
BT

88.1	88.3	88.1	88.8	88.3	88.7	89.4	89.9
6.1	5.9	5.5	5.4	5.9	5.5	4.8	4.3 ✓
50	34	18		16	17	24	32

88.7	89.2	89.1	88.3	88.5	88.0	88.6	89.0	89.0
5.5	5.0	5.1	5.9	5.7	6.2	5.6	5.2	5.2
50	34	21	17		15	17	24	39

89.1	89.2	89.1	88.1	88.44	88.3	88.0	88.6	88.6	88.1
5.1	5.0	5.1	6.1	5.80	5.9	6.2	5.6	5.6	6.1
50	40	21	17		10	14	20	30	40

Tap Hyd N.W. Cor Tilson & McNight Rd
 Tap W. End Door Sill Ho^u 1506 East Ave.



FX LG
RG P
KP T
CW HC

Nov 23, 1957
Overcast 35°

8

Sta	+	π	-	Elev
BM	0.30	992.21		991.91

7+50

✓

8

✓

+50

Nov 27, 1957
Overcast 35° Cold Windy 9
AT

14

Top Hyd N.W. Cor Tilsen & McNight

87.1	87.9	87.4	87.4	87.5	87.8	87.3	87.6	88.0	88.1	87.8
35	43	48	48	47	44	49	46	42	41	44
35	21	19	15	11		15	17	19	27	34

88.9		85.8	86.0	86.3
33		64	62	59
50		50	43	37

87.4	86.6	86.5	86.9	87.02	86.9	86.7	87.0	87.1	87.0
48	56	57	53	519	53	55	52	51	52
20	17	14	6		9	15	17	19	30

87.3	86.4	86.0	87.1	87.2	86.3	86.0	85.8	83.3	84.2	86.6
49	58	62	51	50	59	62	8.4	8.9	80	56
31	33	36	39	43	46	50	50	44	36	34

86.8	86.7	86.2	85.8	86.2	86.3	86.2	85.8	86.3	86.3	86.0
54	55	60	64	60	59	60	64	59	59	62
32	20	16	14	6		8	16	18	29	38

86.2	87.3	87.1		83.1	83.4
60	49	51		91	88
34	44	50		50	43

Sta + π - Elev

992.21

9

✓

+50

✓

+66

✓

T.P. 6.00 989.06 9.15 983.06

11

Nov 29 1957

81

10

85.5

85.4

84.9

85.4

85.49

85.4

85.2

85.1

84.8

6.7

6.8

7.3

6.8

6.72

6.8

7.0

7.1

7.9

20

16

14

6

10

18

20

31

85.4

86.2

86.1

84.0

86.7

88.6

87.9

88.6

6.8

6.0

6.1

6.2

5.5

8.6

9.3

8.6

28

31

41

50

50

40

37

33

87.8

84.0

84.4

84.5

84.6

84.7

84.5

84.4

83.9

83.4

83.0

4.4

8.2

7.8

7.7

7.6

7.5

7.7

7.8

8.3

8.8

9.2

34

27

20

14

8

11

15

19

24

24

27

86.8

86.2

89.8

90.2

87.9

5.4

6.0

2.4

2.0

9.3

42

50

50

41

33

NG

83.3

83.3

84.0

84.3

84.4

84.5

84.3

84.1

83.5

82.9

82.7

8.9

8.9

8.2

7.9

7.8

7.7

7.9

8.1

8.7

9.3

9.5

27

24

19

13

8

10

15

20

27

27

37

83.7

84.6

84.6

82.5

81.6

82.0

8.5

7.6

7.6

9.7

106

102

32

40

47

54

50

45

Sta + A - Elev

98906

9+74 on Ent Rt

✓

+93

✓

10

✓

2 Nov 27, 1957

11

LT

RT

82.1 83.6 84.0 84.2 84.4 84.3 83.8 83.7 83.6

6.4 5.5 5.1 4.9 4.7 4.8 5.3 5.4 5.5
29 27 14 13 10 15 27 50

82.6 84.1 82.8 81.8

→ 6.5 5.0 6.3 7.3
31 36 45 50

82.4 81.9 81.8 83.2 84.0 84.2 83.8 83.8 83.8 82.4 81.1

6.7 7.2 7.3 5.9 5.1 4.9 5.3 5.3 5.3 6.7 8.0
50 37 25 19 12 13 15 17 19 22

80.5 80.7 80.9 ✓

8.6 8.4 8.2
50 37 27

82.5 82.4 82.7 83.6 84.1 84.10 84.0 83.8 82.2 81.4 80.9

6.6 6.7 6.4 5.5 5.0 4.9 6.5 5.1 5.3 6.9 7.7 8.2
50 41 25 15 11 8 12 17 24 32

✓ 80.6

8.5
50

Sta + π - Elev

989.06

10750

11

+50

12

+23

+25

2 Nov 23 1957 12

Lt

Rt

82.3	82.1	82.2	82.9	82.2	82.1	82.8	82.5	82.5
6.8	70	6.9	5.2	4.9	5.0	6.3	6.6	6.6 ✓
38	29	21	13		14	19	24	33

		84.1	84.6	83.9	83.5	82.3	82.0
6.8	70	5.0	4.90	5.2	5.6	6.8	7.1
37	22	14		14	17	22	32

82.9	82.8	83.2	84.2	84.1	84.4	84.2	83.9	82.1	82.7	82.3	82.7
6.2	6.3	5.9	4.9	5.0	4.7	4.9	5.2	6.0	6.4	6.8	6.9
42	27	21	18	14		13	16	18	23	30	42

84.0	84.1	84.5	84.2	84.56	84.0
5.1	5.0	4.6	4.44	4.50	5.1
22	16	14		14	15
	NG				NG

84.4	83.7	84.4	84.5	84.2	84.0
4.7	5.4	4.7	4.6	4.9	5.1
33	21	13		16	26

84.4	83.5	84.4	84.5	84.6	83.9	83.5	83.7
4.7	5.6	4.7	4.6	4.5	5.2	5.6	5.4
33	22	17	13		15	19	22

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		989.06		
--	--	--------	--	--

12+50				
-------	--	--	--	--

TP	3.21	992.11	0.16	988.90
----	------	--------	------	--------

BM			2.16	989.95
----	--	--	------	--------

+71				
-----	--	--	--	--

✓				
---	--	--	--	--

+82				
-----	--	--	--	--

✓				
---	--	--	--	--

Nov 27, 1957

13

11

RT

87.0	85.8	85.9	83.6	84.7	84.9	84.3	83.2	82.9	82.4	83.2 ✓
21	33	52	55	44	42	48	59	63	67	59
50	39	26	20	13		13	18	29	48	50

Top Hy / N.W. Cor Ivy & McNish Rd

84.1	83.9	84.5	84.9	85.2	84.6	84.4	83.0	83.0	82.8
80	82	76	72	69	75	77	91	91	93
26	18	17	11		10	15	18	28	34

85.2	86.2	87.2
69	59	49
37	39	50

82.9	83.6 ✓	83.1
92	85	90
67	51	37

85.5	84.5	84.2	85.1	85.3	84.7	84.2	82.8	82.9	83.7
66	76	79	70	68	74	79	93	92	84
38	28	17	12		12	15	20	34	43

87.1	87.6
50	45
43	50

83.2	84.1 ✓	84.6
89	80	75
83	67	55

Sta	+	π	-	Elev
		992.11		

12+86

✓

BM	7.52	997.47	2.16	989.95	(989.88)
----	------	--------	------	--------	----------

BM			3.43	994.04	(993.97)
----	--	--	------	--------	----------

BM	7.95	997.83			(989.88)
----	------	--------	--	--	----------

13+17.9

✓

+34

FX
RG
LC
KP
CW

± Nov. 27, 1957
Dec 2, 1957 RT

14

LT

85.6	84.9	84.6	85.0	85.3	84.9	84.4	83.0	83.0
65	72	75	71	68	72	77	91	91
37	29	14	12		11	15	20	34

84.5 81.6

83.3 82.8 84.5 ✓

46 45

8.8 8.3 7.6

47 50

91 75 57

Top Hyd NW Cor 1/4 & Mc Night Rd.

RR Spike in 16" Oak 70' Lt Sta 13465

Top Hyd NW Cor 1/4 & Mc Night Rd.

86.5	85.9	85.5	85.7	85.3	84.5	83.1
------	------	------	------	------	------	------

11.1	11.9	12.3	12.1	12.5	13.3	14.7
59	39	13		12	17	21

83.9	84.6	85.2	85.2	84.3	83.6 ✓
------	------	------	------	------	--------

13.9	13.2	12.6	12.6	12.5	14.2
100	78	55	47	38	31

86.5	86.2	85.7	86.0	85.6	84.9	83.4	83.9
------	------	------	------	------	------	------	------

11.3	11.6	12.1	11.8	12.2	12.9	14.4	13.9
50	39	13		13	18	22	31

84.0	84.5	85.2	85.7
------	------	------	------

13.8	13.3	12.6	12.1
100	91	70	54

Sta + Δ - Elev

997.83

13 + 49

✓

+ 55

✓

+ 68

Dec 2, 1937 15

11

BT

87.0	86.9	86.4	85.9	86.2	85.9	85.4	83.8	84.6
10.8	10.9	11.4	11.9	11.6	11.9	12.4	14.0	13.2
50	43	28	18		12	16	24	34

84.8	85.3	85.8	86.0	85.4
130	12.5	12.0	11.8	12.4
100	83	68	50	42

91.3	91.0	85.2	85.2	86.0	86.4	86.0	85.8	84.8
6.5	6.8	12.6	12.6	11.8	11.4	11.8	12.0	13.0
50	31	19	19	17		11	13	23

21
2

84.8	85.5	86.2	86.3	85.5	84.5	83.9
130	12.3	11.6	11.5	12.3	13.3	13.9
100	87	70	52	41	28	25

92.8	93.4	85.3	85.4	86.3	86.5	86.2	85.8	84.5	84.9
50	4.4	12.5	12.4	11.5	11.3	11.6	12.0	13.3	12.9
36	32	20	18	15		12	17	25	27

NG

85.7	86.3	87.4	88.1	87.5	85.7
12.1	11.5	10.4	9.7	10.3	12.1
100	92	81	66	52	35

Sta + 1 - Elev

997.83

14+00

✓

+50

✓

+75

£ Dec 2, 1957

16

24

Rt

91.2 86.0 86.0 86.8 87.18 86.8 86.3 85.5 86.2

66 118 118 11.0 10.65 11.0 11.5 123 11.6
23 21 16 14 12 17 24 28

94.5

96.6

97.0

96.8

94.8

91.3

33

5.5

1.2

0.8

1.0

3.0

6.5

31

100

93

75

61

46

NG

88.1

87.1

86.9

87.8

88.3

89.0

9.7

10.7

10.9

10.0

9.5

8.8

22

20

17

13

13

96.7

87.0

88.5

92.8

97.5

11.1

10.8

9.3

5.0

0.3

24

25

30

40

50

Rt

Side

87.7

87.8

88.5

88.8

88.5

88.0

87.6

87.2

10.1

10.0

9.3

9.0

9.3

9.8

10.2

10.6

21

17

13

13

19

23

25

96.9

92.7

89.2

88.4

0.9

5.1

8.6

9.4

47

39

30

27

Sta	+	X	-	Elev
		997.83		

15

✓

TP	12.23	1005.60	4.46	992.37
----	-------	---------	------	--------

14+50

+75

15

+16

+35

TP	5.12	997.84	12.88	992.72
----	------	--------	-------	--------

Dec 2, 1957

17

LT

RT

88.3	88.3	89.2	89.3	89.1	88.6	87.7	89.8
9.5	9.5	8.6	8.5	8.7	9.2	9.1	8.0
21	17	13		13	18	24	30

94.5	94.8	93.0
3.3	3.0	4.8
50	44	39

97.2	97.5	91.7	91.9
8.4	8.1	3.9	3.7
33	30	58	71

99.2	99.1	91.7	91.8
6.4	6.5	3.9	3.8
33	30	56	67

01.8	01.1
4.5	3.8
35	32

02.9	02.7
2.7	2.9
37	34

95.2	95.0
10.4	10.6
31	28

Sta	+	π	-	Elev
-----	---	-------	---	------

997.84

15+16

+35

+73

16

+50

Dec 2, 1957 18

17

18

88.6	88.1	89.6	89.6	89.3	88.3	89.3	89.6	89.9
9.2	8.8	8.2	8.2	8.5	9.5	8.5	8.2	7.9
21	17	12		14	24	28	37	56

88.8	88.8	89.6	89.9	90.0	89.7	89.0	89.4	89.5	89.1
9.0	9.0	8.2	7.9	7.8	8.1	8.8	8.4	8.3	8.1
22	21	18	12		14	24	27	36	50

90.9	91.0	90.6	90.0	89.9	90.7	90.7	90.4	89.4	89.7	89.8
6.9	6.8	7.2	7.8	7.9	7.1	7.1	7.4	8.4	8.1	8.0
50	38	29	27	19	11		14	24	34	50

90.8	90.7	90.7	89.9	91.1	91.19	90.8	89.7	89.8	90.0	89.7
7.0	7.1	7.1	7.9	6.7	6.65	7.0	8.1	8.0	7.8	8.1
50	46	29	20	13		13	22	28	35	50

91.1	90.3	90.3	91.3	91.6	91.7	91.5	91.0	90.2	90.4	90.9
6.7	7.5	7.5	6.5	6.2	6.1	6.3	6.8	7.6	7.4	7.9
37	23	21	19	11		13	19	24	35	50

92.0	91.7
2.58	6.1
35	50

Sta + π - Elev.

997.84

17

✓

+50

✓ TP

6.49 991.35

+80

✓

18

Dec. 2, 1957

19

14

RT

q^{2.8} q^{1.1} q^{1.7} q^{2.0} q^{2.18} q^{2.2} q^{2.0} q^{1.6} q^{0.6}

5.0 6.7 6.1 5.8 5.66 5.6 5.8 6.2 7.2
34 22 20 11 6 13 18 25

q^{5.6}

2.2
50

q^{0.7} q^{8.2}

71 9.6
50 32

q^{6.2} q^{3.5} q^{2.2} q^{2.0} q^{2.6} q^{2.7} q^{2.7} q^{2.4} q^{2.0} q^{1.1} q^{1.8} q^{0.7}

1.6 4.3 5.6 5.8 5.2 5.1 5.1 5.4 5.8 6.7 6.4 7.1
38 31 21 17 10 6 13 20 26 38 50

q^{3.9} q^{3.1} q^{1.4} q^{1.4} q^{2.5} q^{2.8} q^{2.6} q^{2.5} q^{1.5} q^{1.2} q^{0.6}

3.9 4.7 6.4 6.4 5.3 5.0 5.2 5.3 6.3 6.6 7.2
32 29 21 20 15 13 17 25 35 50

q^{7.2}

q^{9.8}

0.6 +1.6
37 41

q^{5.5} q^{1.7} q^{3.4} q^{1.3} q^{2.7} q^{2.9} q^{2.9} q^{2.7} q^{2.5} q^{1.6} q^{1.3}

2.3 1.1 4.4 6.5 5.1 4.9 4.9 5.1 5.3 6.2 6.5
40 36 30 22 14 6 14 19 25 31

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		997.84		
--	--	--------	--	--

18+50				
-------	--	--	--	--

19				
----	--	--	--	--

+30				
-----	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

20				
----	--	--	--	--

T.P.	2.23	1001.10	3.97	993.87
------	------	---------	------	--------

Dec 2, 1957

20

Lt.

Rt

q1.2	q2.2	q1.3	q2.6	q3.0	q3.2	q3.6	q2.8	q1.9	q2.0	q3.6	q2.5
66	56	65	52	48	46	48	50	59	58	42	53
36	32	25	18	10		14	18	24	39	32	38
NG									29		NG

q1.2	q2.1	q3.0	q3.4	q3.5	q3.2	q2.6	q1.6	q1.3
8.6	5.7	4.8	4.4	4.3	4.6	5.2	6.2	6.5
50	32	19	10		15	18	24	31
								NG

q1.3	q2.5	q3.0	q3.4	q3.6	q3.7	q3.5	q3.3	q2.6	q2.0
8.5	5.3	4.8	4.4	4.2	4.1	4.3	4.5	5.2	5.8
50	31	23	12		6	12	14	18	22

q1.1	q0.4
8.7	24
40	32

q1.4	q2.5	q3.1	q3.6	q3.8	q3.6	q3.3	q2.6	q1.3	q1.8	q1.8
8.4	5.3	4.7	4.2	4.0	4.2	4.5	5.2	6.5	8.0	9.0
50	31	23	11		11	14	19	27	39	41

q0.2	q1.8	q3.6	q4.0	q4.1	q3.9	q3.7	q3.2	q1.9	5.9	q0.7	q0.8
7.6	6.0	4.2	3.8	3.7	3.9	4.1	4.6	6.2	7.1	7.2	
50	35	22	12		11	14	19	27	33	40	

Sta	+	π	-	Elev
-----	---	-------	---	------

Sta	+	π	-	Elev
		1006.10		

Sta	+	π	-	Elev
20+50				

Sta	+	π	-	Elev
21				

Sta	+	π	-	Elev
+50				

Sta	+	π	-	Elev
22				

Sta	+	π	-	Elev
+50				

Sta	+	π	-	Elev
23				

Dec 2, 1957

21

14

RT

90.6	92.2	93.6	94.3	94.5	94.4	94.0	93.1	91.8	91.1
10.5	8.9	7.5	6.8	6.6	6.7	7.1	8.0	9.3	10.0
50	40	26	11		11	15	21	32	43

90.1	91.7	92.7	94.0	94.7	94.8	94.7	94.3	93.5	92.0	90.1
16.0	9.4	8.4	7.1	6.4	6.3	6.4	6.8	7.6	9.1	11.0
50	38	36	24	11		11	14	20	27	41

89.4	90.0	91.2	93.2	94.0	94.8	95.0	94.8	94.6	94.2	93.1	92.5	92.0
11.7	11.1	9.9	7.9	7.1	6.3	6.1	6.3	6.5	6.9	8.0	8.6	9.1
50	43	38	34	27	14		11	14	17	24	27	39

90.8	92.4	91.7	91.7	94.4	95.2	95.3	95.2	94.9	94.0	93.4
1038.7	9.4	9.4	6.7	5.9	5.8	5.9	6.2	7.1	7.7	
4239	36	30	22	12		11	14	23	30	

94.8	94.2	93.4	93.4	94.1	95.1	95.6	95.4	95.2	94.8	93.9	93.5
6.3	6.9	7.7	7.7	7.0	6.0	5.5	5.7	5.9	6.3	7.2	7.6
38	30	28	25	22	13		11	14	24	31	39

94.6	94.1	94.1	95.2	95.5	95.9	96.0	95.7	95.5	94.7	93.8
3.5	7.0	7.0	5.9	5.6	5.2	5.1	5.4	5.6	6.4	7.3
34	27	25	23	13		10	13	23	34	36

99.7	00.9	00.9
14	0.2	0.2
37	44	50

94.5	94.0	93.4
6.6	7.1	7.7
48	46	40

Sta	+	x	-	Elev
-----	---	---	---	------

		1001.10		
--	--	---------	--	--

23 +50				
--------	--	--	--	--

✓				
---	--	--	--	--

24				
----	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

BM	4.10	1002.69	2.53	998.57 (998.59)
----	------	---------	------	-----------------

± Dec 2, 1957

22

11

51

94.1	94.1	95.2	95.8	96.25	96.2	96.0	95.9	95.2
6.4	6.4	5.9	5.3	4.85	4.9	5.1	5.2	5.9
25	22	21	13		11	14	21	33

97.1

90.5

94.9

94.0

95.9

→ 3.4 05 06
33 37 36

6.2 7.1 2.2
45 44 39

96.3	94.1	94.1	95.3	96.1	96.45	96.1	95.9	95.8	94.6
4.8	6.0	6.0	5.8	5.0	4.65	5.0	5.2	5.3	6.5
28	23	21	20	13		14	22	36	41

97.5

90.0

→ 1.6 1.1
33 38

94.8

94.8

95.8

96.6

97.0

97.0

96.7

96.3

95.9

96.2

6.3	6.3	5.3	4.5	4.1	4.1	4.4	4.8	5.2	4.9
22	20	18	14		11	15	21	27	29

97.6

98.0

98.8

98.5

96.3

→ 3.5 3.1 2.3 2.6
26 29 31 36

4.8
41

Spike in Arc Lt. Pale N.E. Co. Arlington & Mc Knight.

Sta

+

$\bar{x}$

-

Elev

1002.69

25+00

✓

+50

+86

26

+35.7

BM

4.10 998.59 (998.59)

Dec 2, 1957

23

11

Rt

97.4	96.5	96.5	97.2	97.6x	97.4	97.3	97.0	96.2	95.6
5.3	6.2	6.2	5.5	5.05	5.3	5.4	5.7	6.5	7.1
27	21	18	14		12	15	19	26	32

98.0	98.5
4.7	4.2
32	50

95.0
2.7
37

98.4	97.8	96.9	96.9	97.7	98.04	97.7	97.6	97.2	96.1	96.2
4.3	4.9	5.8	5.8	5.0	4.65	5.0	5.1	5.5	6.6	6.5
50	29	21	19	15		12	15	22	30	41

98.4	98.0	97.2	97.2	97.9	98.3	98.1	97.9	97.3	96.9
4.3	4.7	5.7	5.5	4.8	4.4	4.6	4.8	5.4	5.8
50	30	20	17	13		14	20	35	48

97.7	98.0	98.0	97.3	98.1	98.44	98.3	98.1	98.0	98.0
5.0	4.7	4.7	5.0	4.6	4.25	4.4	4.6	4.7	4.7
50	38	25	17	13		13	25	41	50

97.2	97.5	98.0	98.6	98.7	98.6	98.4	97.8	97.0
5.5	5.2	4.7	4.1	4.0	4.1	4.3	4.9	5.7
30	22	20	14		13	19	26	34

Spike in Arc Light Pole NE Cor Arlington & McNight

Sta + π - Elev

BM

3.70

993.58

~~995.61~~

989.88

~~991.91~~

0+50

1+00

£ Dec 2, 1957

2A

Lt

Rt

Top Hyd N.W. Cor Ivy + Mc Night Rd

87.1 87.6 86.7 86.1 86.6 86.6 86.5 86.8 87.0 87.0

6.5 6.0 6.9 7.5 7.0 7.0 7.1 6.8 6.6 6.6
42 26 17 16 16 16.5 18 24 30

87.0 86.8 86.2 86.5

92.2

→ 6.6 6.8 7.4 7.1
60 73 76 82

1.4
91
NG

83.6 85.6

10.0 8.0
105 95

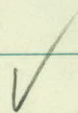


89.0 89.3 88.8 87.9 85.53 88.4 88.9 89.5 89.0 92.2

46 43 4.8 5.7 5.05 5.2 4.7 4.3 4.6 1.4
51 23 173 173 16 17 21 29 38
CR NG

88.4 88.2 87.7 86.1

→ 5.2 5.4 5.9 7.5
79 97 109 118



85.7 83.9 83.9

9.9 9.7 9.7
150 139 130

Sta + Δ - Elev

993.58
~~995.61~~

1+50

✓

2

✓

+50

✓

\$\$\$

7.83 ~~985.75~~
~~87.8~~ 85.73

Dec

25

14

14

89.6 90.3 91.1 89.7 90.4 90.2 90.7 91.1 92.1 93.1

40 33 25 39 32 34 29 25 15 05
101 37 22 16 17 18 28 33 33
NG

89.0

90.0

4.6 3.6
133 135
NG



91.5 92.7 92.7 92.4 91.2 91.8 91.5 92.0 92.2 92.9 93.6

21 09 09 1.2 2.4 1.8 2.1 1.6 1.4 0.7 0.0
58 39 23 20 15 16 18 29 31 34
NG

89.9

89.3

89.7



3.7 4.3 3.9
94 120 150

93.3

93.8

93.6

92.9

93.2

92.6

93.2

93.5

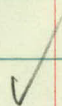
0.3 10.2 0.0 12 0.4 1.0 0.4 0.1 NG
59 47 20 15 17 18 30 33

90.8

90.6

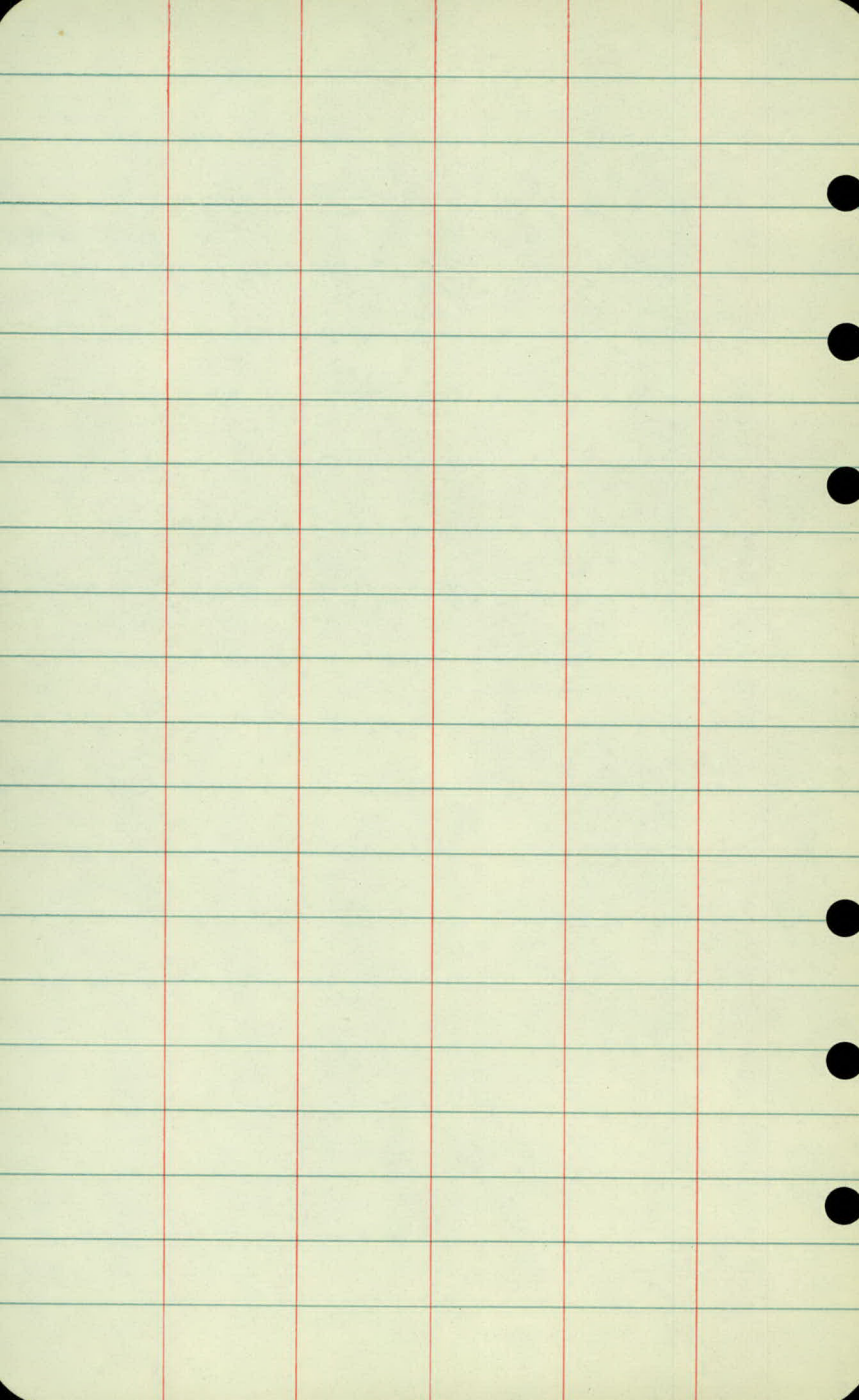
90.1

89.8



2.8 3.0 3.5 3.8
68 86 100 118

Check Sta. 13+17.9



Dec 2, 1957

26

Topography

LT

±

RT

1+00	CB	MH	CB
Ivy Street	19'	±	19'

20+20

24" X 70' CM
35 - 70
→

13+60

15" X 42.5' SCP
18.5' → 24

9+94.5

18" X 48.5' SCP
25 → 23.5

3+43

MH
11

3+31

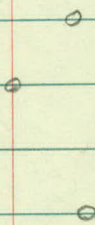
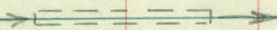
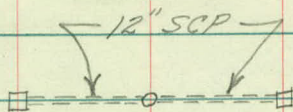
MH
19

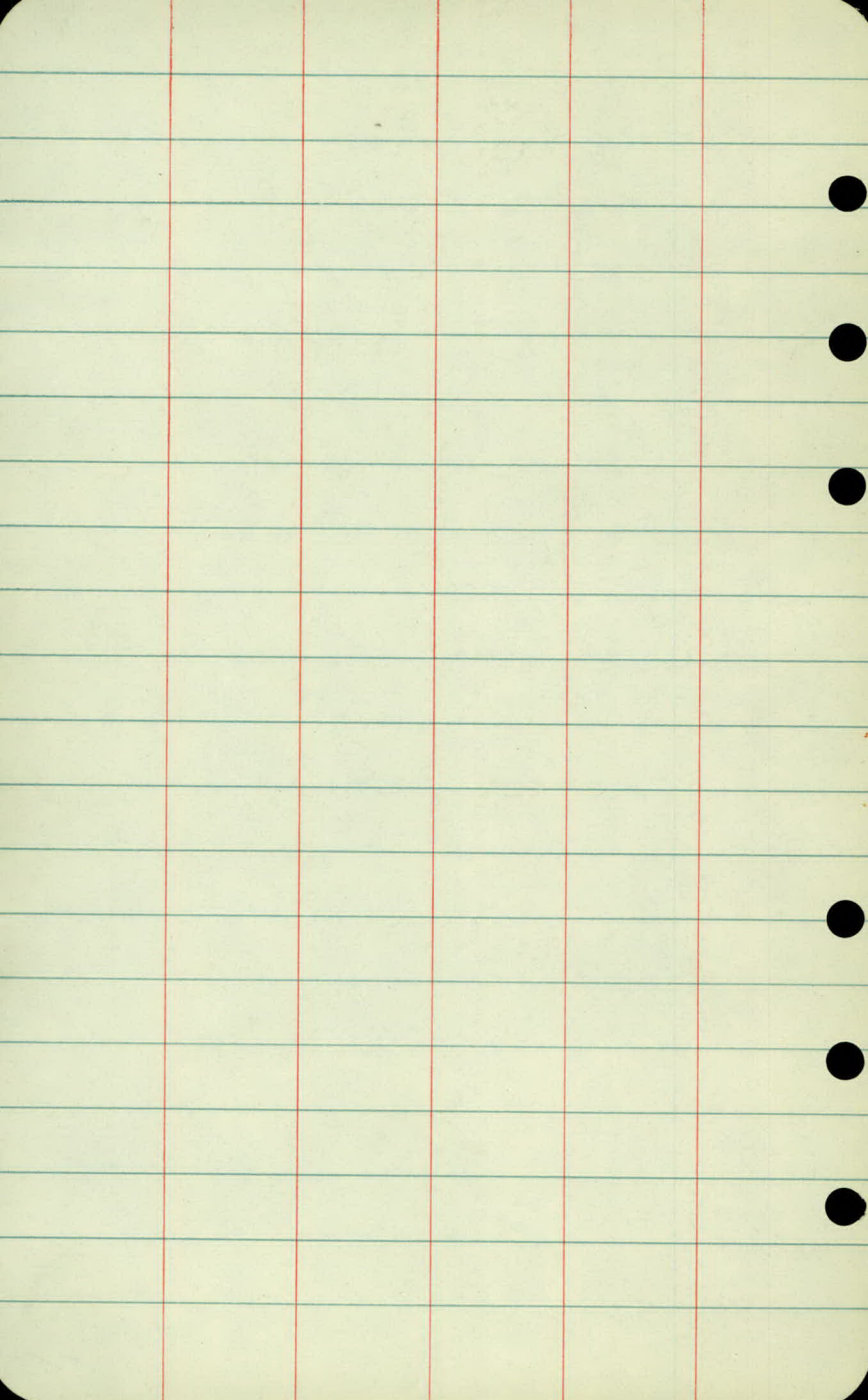
1+7.5

MH
10

Dec 2, 1957

27





FK
RG

Dec 4, 1957

1

McKnight Rd

56-38A

1+00

MH 6.4' Deep
E

1+00

1/4 ST

F.L. to Top
CB = 2.8'

3.2' to Top
From F.L. in v.s.

F.L. to Top
C.B. 2.7'

12+35

E. End 18" x 42.2' SCP
19'

12+17

W. End 18" x 42.2' SCP
19.7

9+94.5

15" x 48.3' SCP
x- Drain

Dec 4, 1957

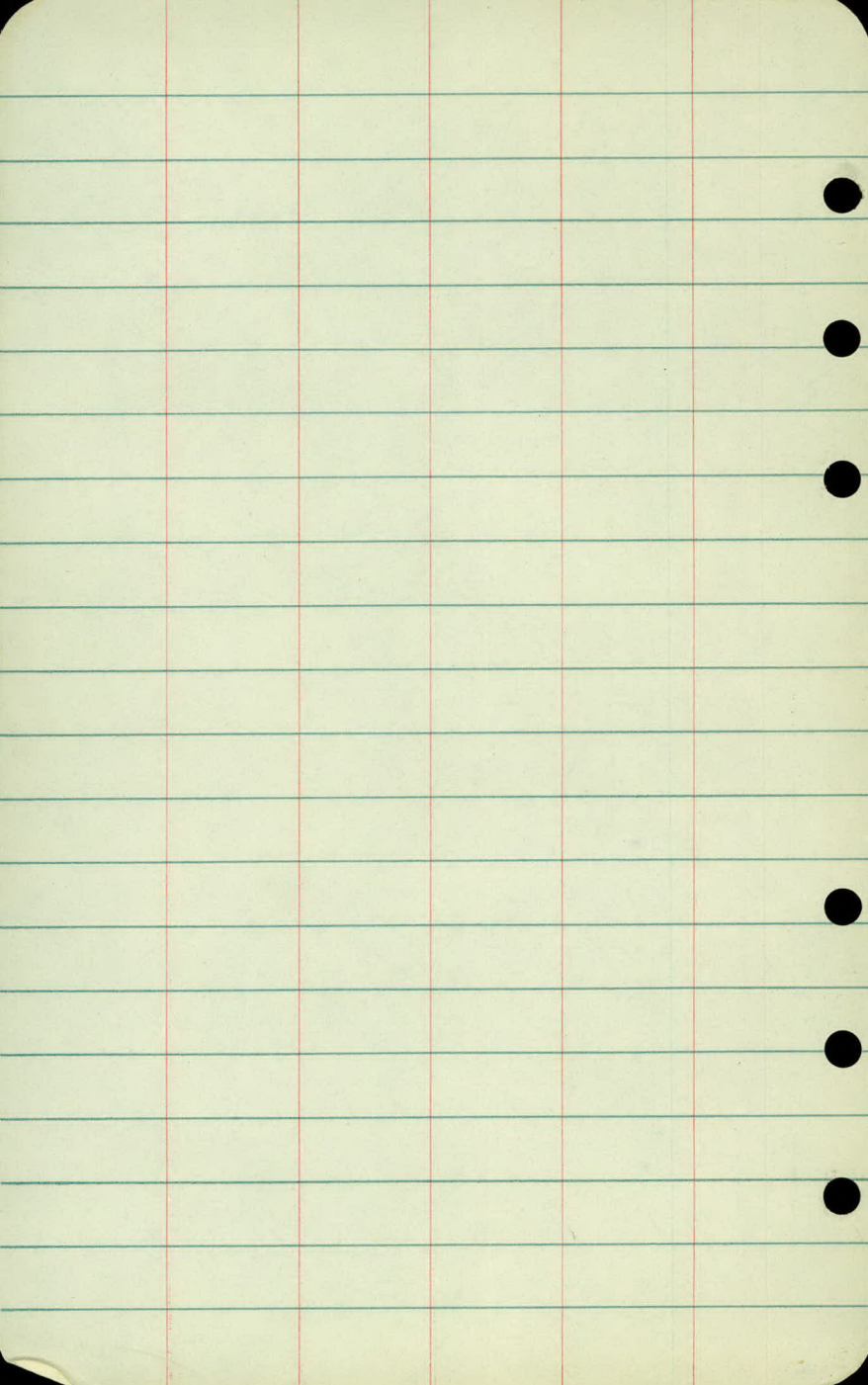
2

M.H. Not Functioning 3.5' of Fill Dirt in it.

North C.B. 0.2 Lower than South C.B.

18" x 42.2' S.C.P.
=====

=====



April 23, 1957

8

14

BT

East Ave Staking & Use

CL
2-11
(1.5)
F30
24.0

7.1
F2.6

(6.5)
10.00
25.0

CL
← 17
49
BT

4.4

4.9
BT

Spike in Arc Lt. Pole N.E. Cor Arlington & East Ave

Sta PG PGR SWGR Elev

BM 3.95 979.20

975.25

0+00

+14

+23

+30 70.6 8.6 8.3

✓

+50 71.3 7.9

130
7.6
51

April 23, 1957

LT

BT

9

Top Hyd NW Cor E. Arc Maryland

71.4	71.3	70.9	70.5	69.8	68.8	68.2	67.4
7.8	7.9	8.3	8.7	9.4	10.4	11.0	11.8
50	45	25	10		17	31	50

71.1	70.8	70.4	70.7	70.5	70.0	69.3	68.4	67.5	67.0
8.1	8.4	8.8	8.5	8.7	9.2	9.9	10.8	11.7	12.2
50	40	19	16	10		9	26	42	50

72.5	71.9	71.5	70.7	70.7	70.3	69.6	68.5	67.9	66.7
6.7	7.3	7.7	8.5	8.5	8.9	9.6	10.7	11.3	12.5
50	38	25	20	10		8	26	34	50

72.9	72.9	72.0	71.0	70.9	70.6	69.4	69.1	67.9	67.1
------	------	------	------	------	------	------	------	------	------

6.3	6.3	7.2	8.2	8.3	8.6	9.8	10.1	11.3	12.1
35	20	25	21	10		14	20	30	38
34.0									

73.4

5.8
50

65.6

13.6
50

67.2

12.0
F3.7
37.4

75.6

74.0

72.1

72.2

71.9

71.5

72.2

70.2

67.7

66.7

36	5.2	7.1	7.0	7.3	7.7	7.0	9.0	11.5	12.5
39	28	20	10	60.6	5	8	16	30	35

3.6

2.8

65.1

14.1
50

66.0

13.2
45

66.2

13.0
15.4
22.8

Sta	PG	PGR	SWGR
-----	----	-----	------

979.20

1+00	73.4	5.8	5.3
------	------	-----	-----

✓

+50	75.6	3.6	3.3
-----	------	-----	-----

6.4
1.6
1.9

✓

+72

T.P.	7.94	985.25	1.89	977.31
------	------	--------	------	--------

April 23, 1957

76.8 74.9 75.1 74.8 74.5 71.2 69.6 69.7

2.4 4.3 4.1 4.4 4.7 8.0 9.6 {9.5
32 18 10 C1.4 6 21 35 F4.0
38}

77.2 77.4 77.6 68.9

2.0 1.8 1.6
C3.5 40 50
37.0

10.3
50

77.6 77.2 77.3 77.5 77.2 77.1 75.2 74.0 72.8

{1.5} 2.0 1.9 1.7 2.0 2.1 4.0 5.2 {6.4
C1.7 23 17 10 C1.6 11 24 28 F3.1
33.4 36.2}

1.5 1.4
37 50

7.9 6.9
50 40

77.9 77.9 78.4 78.2 78.2 77.8 77.9 74.7

1.3 1.3 0.8 1.0 1.0 1.4 1.3 4.5
29 22 10 8 15 29 36

77.7 77.6

1.5 1.6
44 50

73.6
5.6
50

Sta	+	π	-	Elev
-----	---	-------	---	------

985.25

1+82	76.9	8.35	8.0	
------	------	------	-----	--

4.8
4.5

✓

2	72.7	7.5	7.25	
---	------	-----	------	--

4.75
3.5

✓

+50	79.8	5.45	5.15	
-----	------	------	------	--

✓

TP	8.28	989.20	4.33	980.92
----	------	--------	------	--------

April 23, 1957

11

RI

79.0

78.3

78.5

78.9

78.7

78.6

77.0

75.8

75.1

6.3 7.0 6.8 6.4 6.6 6.7 8.3 {9.5} 10.2
28 25 20 10 (C1.7) 13 26 {F1.5} 39
33.0

79.3

79.4

80.1

74.6

→ {6.0} 5.9 5.2 ✓ 10.7
{C2.0} 43 50 50
{34.0}

79.6

79.1

79.3

79.5

79.3

79.1

77.3

76.1

76.1

5.7 6.2 6.0 5.8 6.0 6.2 8.0 9.2 {9.2}
26 24 17 10 (C1.5) 14 27 34 {F2.0}
34.0

80.6

80.50

81.0

81.2

75.3

75.6

→ 4.7 {4.75} 43 4.1 ✓
35 {F2.5} 45 50 10.0 9.7
35.0 50 45

81.0

80.5

80.9

80.8

80.5

80.1

80.1

80.9

80.6

4.3 4.8 4.4 4.5 4.8 5.2 5.2 4.4 4.7
35 27 18 10 C0.6 1 2 3 9

81.3

81.7

78.8

79.2

79.7

80.1

→ 4.0 3.6
46 50 6.5 6.1 {5.85} 5.6 5.2
50 36 {F0.7} 29 24
31.4 ✓

S. End Ent Culvert 1' RI Sta 2+55

Sta	PG	PGR	SWGB	Elev
-----	----	-----	------	------

989.20

3+00	81.9	7.3	7.0	
------	------	-----	-----	--

+13
+43
+73

+13	82.5	6.7	7.9 6.4	
-----	------	-----	------------	--

+43	83.3	5.9	5.6	
-----	------	-----	-----	--

FX
RG
KP
JT

April 24, 1951
Cloudy Windy 40 MPH 12
59°F BT

LT

81.1 81.9 81.9 81.0 81.2 81.1 81.4 81.9

7.8 81 7.3 7.3 8.2 8.0 8.1 7.8 7.3
F0.8 27 19 10 F0.9 4 12 22 28
30.6

81.5 81.6 81.5 83.0 82.7 82.3 82.0

7.7 7.6 7.7 6.2 6.5 6.9 7.2 7.2
37 46 50 50 41 38 32 F0.2 30.4

81.5 81.7 82.3 81.4 81.9 81.9 82.5 82.5

7.8 7.7 7.5 6.9 7.8 7.3 7.3 6.7 6.7
F1.4 28 23 10 F1.1 4 19 28 34
32.8

81.1 81.3 83.5 83.1

8.1 7.9 5.7 6.1 6.8
39 50 50 42 F0.4 30.8

81.9 82.0 82.8 82.8 82.3 82.2 83.0 83.8 83.9

7.3 7.2 6.4 6.4 6.9 7.0 6.2 5.4 5.3
50 37 24 10 F1.0 1 4 9 20

85.0 85.2 84.3 84.5

4.2 4.0 4.9 4.8 4.7
50 45 38 C0.8 30 31.6

Sta	PG	PGR	SWGR	Elev
-----	----	-----	------	------

989.20

3+73	84.0	5.2	4.9	
------	------	-----	-----	--

4	85.1	4.1	3.8	
	1.9			
	<u>3.2</u>			

TP	8.18	⁴ 994.39	2.99	986.21
----	------	---------------------	------	--------

+50	86.9	7.5	7.2	
		3.6	6.6	

BM	1.80	994.40	18.0	992.59 992.60
----	------	--------	------	---------------

April 24, 1957

13

84.1

83.7

83.9

83.8

83.3

84.8

5.1 5.5 5.3 5.4 5.9 4.4
26 19 16 10 (F0.7) 3
NG

(2.8)
C2.1
34.2

84.2

84.0

84.1

→ (5.2) 5.0 5.2 5.1
(F0.3) 31 40 50
(30.6)

85.6

85.0

85.0

85.1

86.1

86.9

87.4

3.6 4.2 4.2 4.1 3.1 2.3 1.8
24 23 18 10 (C1.0) 1 6
NG

(1.8)
C2.0
34.0

85.5

85.5

85.7

→ 3.7 (3.7) 3.7 3.5
30 (C0.1) 40 42
(30.2) 40

87.5

87.8

87.7

87.7

88.8

6.9 6.6 6.7 6.7 5.6
26 19 9 4 C1.9

(6.1)
C1.1
32.2

87.9

87.8

88.1

→ 6.5 (6.6) 6.6 6.3
27 (C0.6) 37 43
(31.2)

Top W. End Door Sill/Hoth 1506 E. Ave.

Sta	PG	PGR	SWGR	Elev.
-----	----	-----	------	-------

994.40

5+00	88.25	6.15 4.3	5.85 3.60	
------	-------	-------------	--------------	--

450

450	89.09	5.3 3.9 1.4	5.0 2.7	
-----	-------	-------------------	------------	--

✓

6	89.46	4.94 4.2	4.64 6.4 1.2	
---	-------	-------------	--------------------	--

BM	4.09	996.05	2.44	991.96
----	------	--------	------	--------

April 24, 1957

14

89.6

89.8

89.8

90.1

4.8 4.6 4.6 4.3
20 10 4 (C1.8)

{ 5.65
C0.2
30.4 }

89.2

89.8

89.7

90.1

90.2

52 { 4.65 } 4.6 4.7 4.3 4.2
26 { C1.2 } 32 38 41 50
32.4

✓

90.6

90.3

89.7

90.4

90.5

38 4.1 4.7 4.0 3.9
15 10 3 2 C1.4

{ 4.7
C0.3
30.6 }

90.3

89.9

90.3

90.3

90.6

41 4.5 { 4.0 } 4.1 4.1 3.8
21 28 { C1.0 } 34 45 50
32.0

✓

90.2

90.0

89.4

90.2

90.2

4.2 4.4 5.0 4.2 4.24
17 10 4 2 C0.7

{ 6.44
F1.8
33.6 }

No Change

Begin New Change

89.9

90.6

90.6

4.5 { 4.24 } 3.8 3.8
28 { C0.4 } 37 50
30.8

✓

Sta	PG	PCR	SWGR	Elev
-----	----	-----	------	------

	996.05			
--	--------	--	--	--

6+32	89.43	6.6	6.3	
------	-------	-----	-----	--

+62	89.24	6.8	6.5	
-----	-------	-----	-----	--

+92	88.87	7.2	6.9	
			5.4	

April 24, 1957

15

2+

8+

90.3

90.5

90.0

89.5

89.2

89.1

88.8

{ 6.0 }
(C03)
30.6

5.8 5.6

6.1 9

6.6 (C0.0)

6.9 7

7.0 18

7.3 29

{ 2.5 }
F1.2
32.4

90.4

90.3

90.1

87.2

88.1

5.7 5.8 6.0
39 47 50

8.9 8.0
50 39

90.5

90.9

91.1

90.5

90.6

89.9

89.7

89.9

5.6 5.2 5.0
41 28 20

5.6 10

5.5 (C1.3)

6.2 6

6.4 15

6.2 28

{ 6.2 }
C0.3
30.6

90.1

90.3

90.1

6.0
50

5.8 6.0
50 43

90.7

90.7

91.0

91.2

90.3

89.1

89.1

88.9

5.4 5.4 5.1
23 C1.5 25

4.9 12

5.8 (C1.4)

7.0 11

7.0 20

7.2 30

{ 7.3 }
F0.4
30.8

90.4

90.1

90.4

89.7

5.7 6.0
41 50

5.7 6.4
50 41

Sta PG PGR SWGR Elev

996.05

7+00 88.74 7.3 7.0

4.8

2.5

+50 87.9 8.15 7.85

1.2

8 87.1 9.- 8.7

+50 86.2 9.85 9.55

TP 7.10 994.55 8.60 987.45

9 85.49 9.06 8.76

86.2

+50 84.95 9.6 9.3

4.9

4.4

TP 2.47 987.69 9.33 985.22

April 24, 1957

16

Lt

Rt

48
No Change in X-Section
 { 5.7 }
 C 1.3
 32.6

{ 7.9 }
 F 0.9
 31.8

{ 9.0 }
 F 1.2
 32.4

8.75
 { F 0.6 }

{ 9.55 }
 F 1.7
 33.4

{ 10.8 }
 F 2.1
 34.2

11.4
 { F 2.4 }

Water

{ 11.15 }
 F 1.6
 33.2

12.1
 { F 2.3 }

16.0

{ 8.21 }
 C 0.5
 31.0

8.5
 { C 0.5 }

{ 9.85 }
 F 1.1
 32.2

{ 5.1 }
 C 4.2
 38.4

2.5
 { C 7.1 }

{ 4.9 }
 C 4.4
 38.8

Rock at Ent

Sta PG PGR SGR Elev

987.69

9+66 84.84

+74 84.78

+93 84.67

10 84.65 3.04 6.2
3.5
2.7

TP 4.79 982.90

BM 4.16 995.61

991.45

Cal. G.R.

Culvert 987.0 9.6 9.0

24" x 70' CM 8.2 8.0

6.53 989.1 989.1

87.0

FK
KF
WJ
L
SR

11

£ April 24, 1957
June 3, 1957 Rt

17

[6.2
F2.7
23.1]

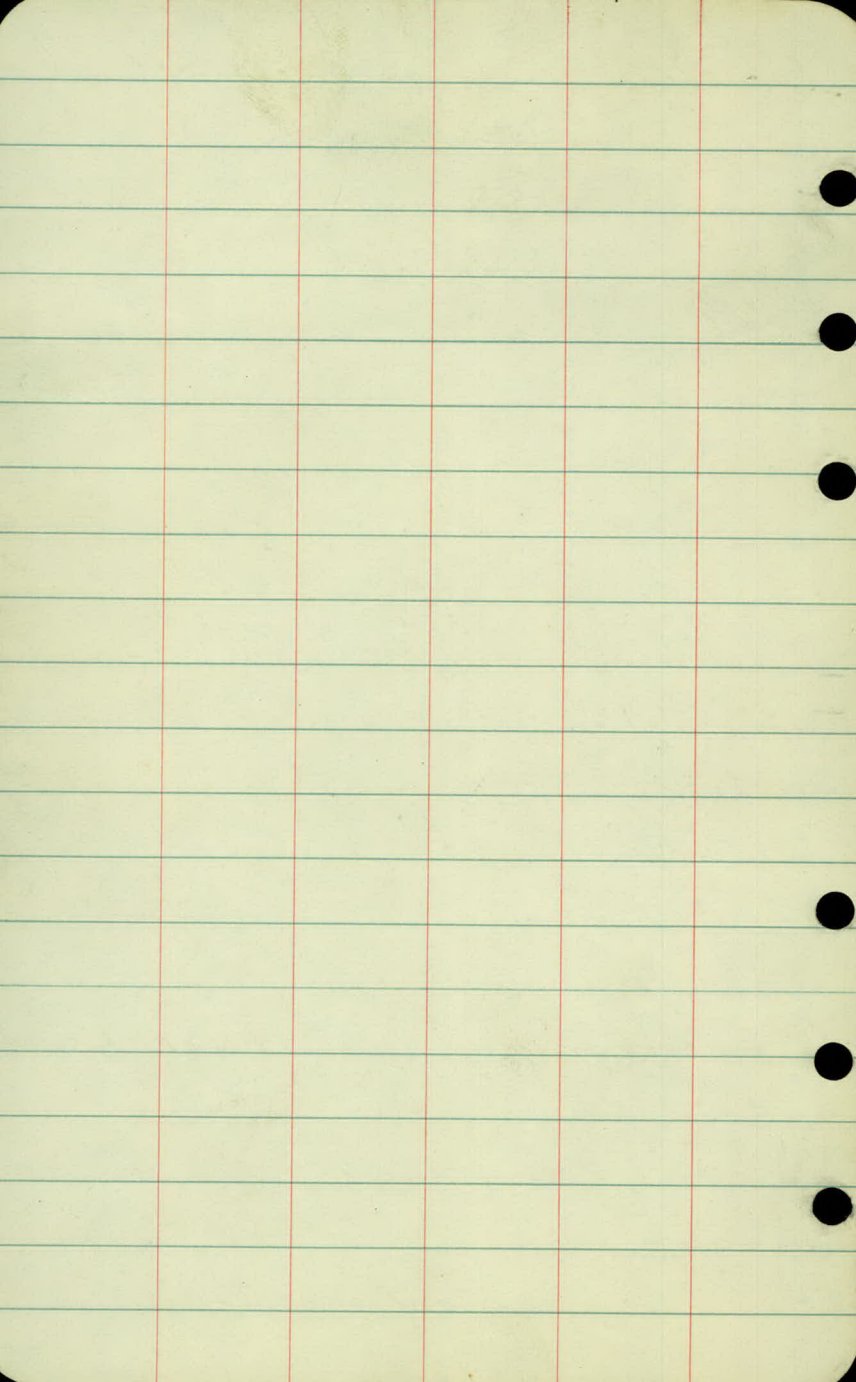
6.4
F3.4

[6.5
F3.0
24.0]

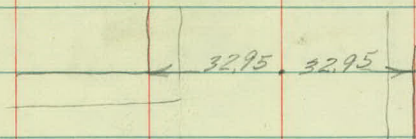
Rail Sta H100 £

1.0
C20
FL 24" x 70' CM
Ø 5.0

7.0
C2.0
FL 24" x 70' CM
⑤
5.0



IVY St Mont



Punch Hole

S.W. Rim M.H.
100' W of X-Street

Punch Hole



248.24'

Mont



± East Ave & Ivy St.

Sta	PG +	PGR +	SGGR -	Elev
BM	2.30	996.27		993.97

13	84.7	11.6	12.6	
----	------	------	------	--

14	86.8	9.5	10.5	
----	------	-----	------	--

15	89.4	6.9	7.9	
----	------	-----	-----	--

16	91.5	4.8	5.8	
----	------	-----	-----	--

17	92.64	3.73	4.7	
----	-------	------	-----	--

TP	5.67	997.23	4.71	991.56
----	------	--------	------	--------

18	93.3	3.93	4.93	
----	------	------	------	--

BM	5.88	997.33	5.88	991.35 991.45
----	------	--------	------	---------------

19	93.9	3.43	4.43	
----	------	------	------	--

T.P	6.29	998.92	4.70	992.63
-----	------	--------	------	--------

20	94.6	4.32	5.32	
----	------	------	------	--

T'

FA
KP
SR
RL

June 10, 1957
Cloudy Sticky 80° 19

R.R. Spike in 16" Oat 70' 24 sta 13+65

2.25

Sta	PG	PGR	SGGR	Elev
		⁸² 998.92		
21	95.2	3.72	4.72	
22	95.8	3.12	4.12	
23	96.5	2.42	3.42	
24	97.1	1.81	2.81	✓
25	97.8	1.12	2.12	
26	98.4	0.52	1.52	
BM			0.20	998.82 998.52

June 10, 1957

20

-1.5 @ 20'				
Sta	PG	PCR	-	Elev
BM	3.28	997.25		993.97
13+49	85.5	11.75 1.5	13.25	12.25 C1.0
14	86.8	10.43 1.5	11.95	10.95 C1.0
+50	88.1	9.15	10.65	9.65 C1.0
15	89.4	7.85	9.35	8.35 C1.0
+50	90.6	6.65	8.15	7.15 C1.0

FX
HP
JD
SK
RL

June 18, 1957

Cloudy

21

Spike in 16 Oak 70' 2f sta 13+65

IVY ST

BM 2.10 996.07

993.97

0+30 986.0 10.07

+50 86.65 9.40 ✓

+65 87.2

1 88.4 7.67 ✓

1.75

4
9
+

+50 90.15 5.92 ✓

1.75

2 91.9 4.17

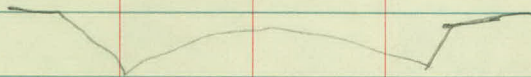
+20 92.6 3.47 ✓

June 18, 1957

22

RR
Spike in 16" Oak 70' 6" Sta 13+65

18.07
Gr



996.07

2+50 93.2 2.87 ✓

2+80 93.9 2.17

BM 1.98 995.95

993.97

Ditch FL 85.0 ~~10.95~~
West

East 84.5 ~~11.45~~

13+60 85.8 10.15 11.65
Left, $\begin{array}{r} 1.5 \\ 84.3 \end{array}$ $\begin{array}{r} 1.5 \\ 12.15 \end{array}$ ✓

Right 85.8 10.15 12.15

3.79
90.65 5.8

Spike in 16" Oak 70' Lt sta 13+65

Blue Top 5

Sta

PG

PGR

-

Elev

BM

8.35 983.60

(975.25)

0+50

71.3

12.3

8.0

75.6

0+84

72.8

10.8

1+25

74.6

7.0

2.3

1

73.4

10.2

+50

75.6

8.0

2

72.7

5.9

TP

5.59

985.45

3.74

979.86

+50

79.8

5.65

PK
AP
JD
SR
RL

June 20, 1931 24

Lt

RT

Top Hyd N.W. Cor East Ave & Maryland

Top slope St 10 Lt Sta 1782

Sta PG FGR - Elev

8 985.43

3 81.9 3.55[✓]

+13 82.5 3.0[✓]

+73 84.0 1.45[✓]

4 83.1 0.35[✓]

TP 8.48 993.58 0.35 985.10

B.M. 0.95 (993.55) 0.95 992.63 992.60

+50 86.9 6.65

5 88.25 5.3[✓]

June 20, 1957

25

Top 9

Top W. End Front Door Sill H₂O 1506

Sta PG PGR - Elev

993.55

5+50 89.09 4.46

6 89.46 4.09

+50 89.25 4.3

7 88.74 4.81

+50 87.9 5.65

TP 3.31 991.22 5.64 987.91

87.1

8 87.1 4.12

JUNE 20, 1957

26

Sta	P6	P6R	-	Elev
-----	----	-----	---	------

		991.22		
--	--	--------	--	--

8 + 50	86.2	5.02		
--------	------	------	--	--

9	85.49	✓ 5.73		
---	-------	-----------	--	--

+ 50	84.95	✓ 6.27		
------	-------	-----------	--	--

10	84.65	+1.5 6.57	56 ShGR ✓ 8.07	
----	-------	--------------	----------------------	--

+50	84.53	+1.5 6.69	✓ 8.19	
-----	-------	--------------	-----------	--

11	84.53	+1.5 6.69	✓ 8.19	
----	-------	--------------	-----------	--

JUNE 20, 1951

Lt

~~Lt~~

Rt

27

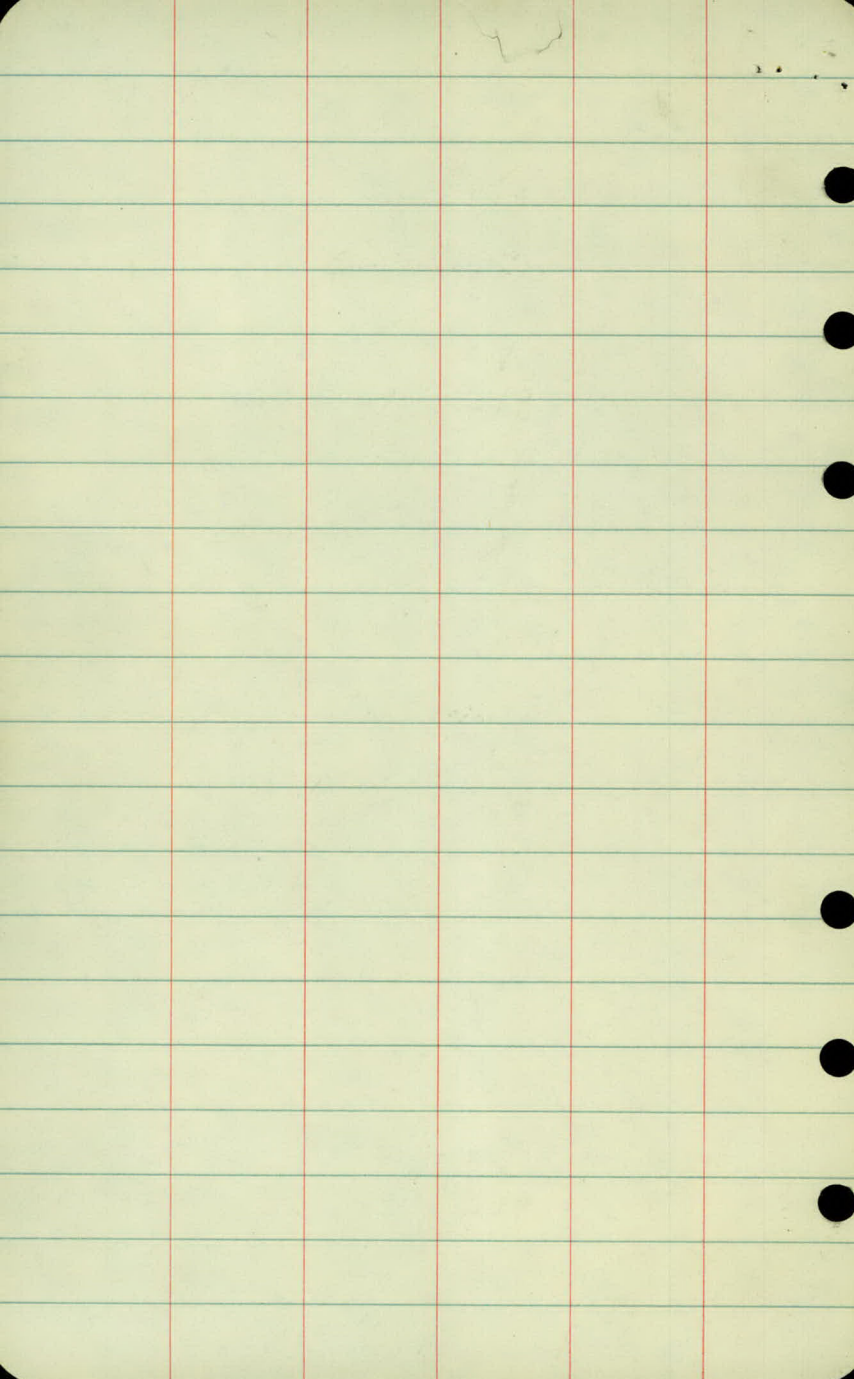
Sta	PL	PLR	-	Elev
-----	----	-----	---	------

		991.22	5.656R	
		+1.5	✓	

11+50	84.53	6.69	8.19	
-------	-------	------	------	--

			6.72	984.50
--	--	--	------	--------

£ THICKS



FX
RG
AP
JT-

April 22, 1951
Clear Perfect 54°

1

East Ave Staking

Sta	PG	PGR	<u>DGR</u> SGR	Elev
-----	----	-----	-------------------	------

BM	2.14	996.11		
----	------	--------	--	--

993.97

12+25	84.20	11.9	5.12 12.4	
-------	-------	------	--------------	--

+50	84.3	11.8	D 13.8	
-----	------	------	-----------	--

+75	84.4	11.7	D 13.7	
-----	------	------	-----------	--

13	84.7	11.4		
----	------	------	--	--

+17.92	85.0	11.1		
--------	------	------	--	--

92.8

+34	85.2	10.9		
-----	------	------	--	--

April 22, 1957

2

14

Rt

RR Spike in 16" Oct 70' Lt Sta 13+65

$$\begin{pmatrix} 13.2 \\ F08 \\ 12.4 \end{pmatrix}$$

456

00.3

11.5

$$\begin{pmatrix} 12.9 \\ 00.9 \\ 22.7 \end{pmatrix} \begin{matrix} 3:1 \\ \\ 1 \end{matrix}$$

+68 2-14" 597'14"

010.3

1.4

$$\begin{pmatrix} 11.7 \\ 52 \\ C0.0 \end{pmatrix} \text{Flat}$$

c7.9

35

$$\begin{pmatrix} 11.4 \\ C0.0 \\ 684 \end{pmatrix} \text{Flat}$$

92' c7.1

4.0

c7

$$\begin{pmatrix} 11.1 \\ C00 \\ 66 \end{pmatrix} \text{Flat}$$

c6.8

4.1

$$\begin{pmatrix} 10.9 \\ 74.1 \\ C00 \end{pmatrix} \text{Flat}$$

Sta

PG

PBR

996.11

13+49 85.5 10.6 8.1 Flat
_{2.5}

10.

+55 85.7 10.4 12.4 13.1
_{1.5}

11.9

3.6

TP 10.66 1003.14 3.63 992.48

+18

14 86.8 16.3 18.3 95.9
_{7.2}
_{1.5}
_{4.9}
_{17.8}
_{26.4}
_{45.1}
_{51.5}

+50 88.1 15.0 17.0
_{1.5}
_{1.5}
_{16.5}
_{31.5}
_{2.5}
_{10.8}
_{30.8}
_{2.5}

+75 88.8 14.3 16.3 14.9
_{0.7}
_{13.6}
_{1.2}
_{15.8}

15 89.4 13.7 15.7
_{1.2}
_{7.9}

16

20

15.8

2.5

20.3

April 22, 1957

LT

RT

3

2.1
CL 7.5

8.1 Flat
CL 0.0
68.4

1.5
CL 8.9
Begin CL
5' RT →

13.1 Flat
CL 0.0
84.4

3.6
30
CL 8.3

996.

8.6
CL 9.2
30

CL 7.98
16 CL 9.1

CL 4.8 2:1
→ CL 13.5
52.0

5.7
CL 10.8
30

CL 3.4
CL 11.6

CL 1.5 2:1
→ CL 15.5
56.0

4.1
CL 11.7
30.0

CL 0.7
5 CL 13.6

CL 1.4 2:1
→ CL 14.9
54.8

1.8
CL 13.4
30.0

CL 2.4
10 CL 11.3

2.8 2:1
CL 7.9
40.8
CL 50

Sta PG PGR DGR

1003.14

15+35 90.3 12.8 14.3
14.8

TP 3.13 996.20 10.07 993.07

+35 90.3 5.9 29
22

+73 91.0 5.2 8.3
5.7 3.1
20
1.5

TP 4.79 994.92 6.07 990.13

16 91.5 3.4 7.6
3.9
3.7

+50 92.2 2.7 7.4
3.2

17 92.64 2.3 6.3
2.8 5.2
87.5

2 April 22, 1957

4

Lt

Rt

CL
35

$\left\{ \begin{array}{l} 6.1 \\ 8.2 \\ 30.0 \end{array} \right\}$

$\left\{ \begin{array}{l} 7.2 \\ 20.7 \\ 26.4 \end{array} \right\}$ ECL
25'

9.8 9.5

End CL
20' $\left\{ \begin{array}{l} 8.3 \\ F2.6 \\ 20.2 \end{array} \right\}$

8.7
 $\left(F3.5 \right)$

$\left\{ \begin{array}{l} 8.7 \\ F3.0 \\ 21.0 \end{array} \right\}$

Rock

17.2

11.3

$\left\{ \begin{array}{l} 7.6 \\ F3.7 \\ 26.1 \end{array} \right\}$

7.7
 $\left(F4.3 \right)$

$\left\{ \begin{array}{l} 7.2 \\ F4.0 \\ 27.0 \end{array} \right\}$

7.8
 $\left(F5.1 \right)$

No
Clearing

$\left\{ \begin{array}{l} 5.8 \\ F3.0 \\ 24.0 \end{array} \right\}$

8.7
7.2
 $\left(F4.9 \right)$

$\left\{ \begin{array}{l} 7.8 \\ F5.0 \\ 30 \end{array} \right\}$

Sta	PP	PCR A	SGR DGR	Elev
		994.92	66	
17+50	93.0	1.9	2.9	
TP	8.22	<u>1002.09</u> 83	1.05	993.87
	93.0	9.1	11.1	1001.64
+80	93.2	8.9	9.4 10.9 2.5 8.4 16.8	36 22 26 25 16.4
18	93.3	8.8	9.3 10.8 5.5	33
BM			10.64	991.45 11.4 106 25 25
+50	93.6	8.5	9.0 10.5 5.5 1.7	
19	93.9	8.2	13.0 8.7	2.4
TP	4.16	995.61	10.2 10.64	991.45 13 12.9
19	93.9	1.7	7.4 2.2 5.9 1.3 17.1 1.2	

£ April 22, 1957

5

14

R1

$$17 + 10 \frac{CL}{£}$$

CL
50

4.3
F2.4

{ 6.6 } CL
F4.2 → 25
27.6

{ 7.0 }
C4.1
33.2 { 2.7 }
C8.2
41.4

6.6
C2.3

{ 9.8 }
F0.4
16.2

CL
41 ←

{ 5.5 }
C5.3
35.6

5.9
C3.4

{ 10.0 } CL
F0.8 → 50'
26.6

Spike in 10" Oak 40' R/ 5' 18+00

CL
15 ← { 10.4 }
F1.4
19.2

8.9
F0.4

{ 8.8 } CL
F17 →
28.4

90.0

12.1
C3.9

{ 11.4 }
F2.4
22.2

CL
33

{ 7.9 }
F5.7
32.1

90.1
3.5

Sta	PG	PCR	SGR	Elev.
		995.61		
19+30	94.1	1.5	20	

TP	7.35	997.39	5.57	990.04
(20) 0	94.6			

21	95.2	2.2	2.7	
----	------	-----	-----	--

+

+50	95.5	1.9	2.4	
-----	------	-----	-----	--

22	95.8	1.6	2.1	(93.7) ✓
----	------	-----	-----	----------

+50	96.2	1.2	1.7	
-----	------	-----	-----	--

TP	7.16	1002.38	2.17	995.22
----	------	---------	------	--------

+50	96.2	6.2	6.7	
-----	------	-----	-----	--

8.3
8.2

09

FX
RG
KP
JT

2 April 23, 1937

6

LT

BT

End CL 7.9
F 6.4

9891
[4.5
F. 4.5
28.5]

Rock 1' LT Sta 19+04

9.4
F 7.2

[9.5
F 6.8
35.4] B. CL
40

+60 B. CL
F

[8.2
F 5.8
32.4
12" C. H
19]

+34

6.7
F 4.9

[5.6
F 3.2
24.6]

CL [5.3
18 F 3.2
24.6]

93.7
3.7
F 2.1

[3.4
F 1.3
18.9] CL
→

~~3.2 [2.3
BT F 0.6
D Grade 16.8
25]~~

~~24
F 1.2~~

~~[3.3
F 1.6
19.8]~~

~~CL [7.4
23 D 0.5
26.0] [7.3
D 0.9
26.8]~~

~~7.4
F 1.2~~

~~[8.5
F 1.8
20.4] [8.4
F 2.0
21.0] CL
22~~

Sta	PG	PGR	DGR SGR	Elev
		1002.38		
23	96.3	5.9	6.4	
			7.9 2.1 5.8 11.6 2.5	12 25
+50	96.8	5.6	6.1	
			7.6 1.6	
24	97.1	5.3	5.8	
			7.3 2.3	5.2 10.4 35.4
+50	97.4	5.0	5.5	
			7.0 5.2	
T.P.	3.65	1002.85	3.18	999.20
25	97.8	5.0		95.9
			7.0 6.3	
+50	98.1	4.7	5.2	15
			6.7	
+75				

April 23, 1957

14

Bt

7

$$\begin{array}{l} \leftarrow CL \\ \leftarrow \left\{ \begin{array}{l} 2.1 \\ \text{R } 5.8 \\ 36.6 \end{array} \right\} \end{array}$$

$$\begin{array}{l} 6.6 \\ \text{FO.7} \end{array}$$

$$\begin{array}{l} \left\{ \begin{array}{l} 7.8 \\ \text{F1.4} \\ 19.2 \end{array} \right\} CL \\ 8 \end{array}$$

$$\begin{array}{l} \leftarrow CL \\ \leftarrow \left\{ \begin{array}{l} 1.6 \\ \text{R } 6.0 \\ 37.0 \end{array} \right\} \end{array}$$

$$\begin{array}{l} 5.8 \\ \text{FO.2} \end{array}$$

$$\begin{array}{l} \left\{ \begin{array}{l} 6.8 \\ \text{FO.7} \\ 17.1 \end{array} \right\} CL \\ 10 \end{array}$$

$$\begin{array}{l} \leftarrow CL \\ \leftarrow \left\{ \begin{array}{l} 2.3 \\ \text{R } 5.0 \\ 35.0 \end{array} \right\} \end{array}$$

$$\begin{array}{l} 5.2 \\ \text{CO.1} \end{array}$$

$$\begin{array}{l} \leftarrow CL \\ 19 \left\{ \begin{array}{l} 6.2 \\ \text{FO.4} \\ 16.2 \end{array} \right\} \left\{ \begin{array}{l} 6.8 \\ \text{R } 0.5 \\ 26.0 \end{array} \right\} \end{array}$$

$$\begin{array}{l} CL \\ 37 \left\{ \begin{array}{l} 4.8 \\ \text{R } 2.2 \\ 29.4 \end{array} \right\} \end{array}$$

$$\begin{array}{l} 4.1 \\ \text{CO.9} \end{array}$$

$$\begin{array}{l} \left\{ \begin{array}{l} 5.7 \\ \text{R } 1.3 \\ 27.6 \end{array} \right\} CL \\ 37 \end{array}$$

$$\begin{array}{l} \leftarrow CL \\ \leftarrow \left\{ \begin{array}{l} 6.2 \\ \text{R } 0.8 \\ 26.6 \end{array} \right\} \end{array}$$

$$\begin{array}{l} 96.05 \\ 6.8 \\ \text{F1.8} \end{array}$$

$$\begin{array}{l} CL \\ 25 \end{array}$$

$$\begin{array}{l} CL \\ \leftarrow \left\{ \begin{array}{l} 6.7 \\ \text{F1.5} \\ 19.5 \end{array} \right\} \end{array}$$

$$\begin{array}{l} 7.3 \\ \text{F2.6} \end{array}$$

$$\begin{array}{l} \leftarrow CL \\ \leftarrow \end{array}$$

Sta	PG	PGR	DGR SSR
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1002.85

25+86	98.3	4.5	5.0 6.5
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26	98.4	4.4	4.9
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BM

4.26 798.59 (998.57)