

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

LOCATION Survey

LOWER AFTON ROAD

From McKNIGHT To E. Co. Line

Road Acc't. No. _____

Date Filed 4-19-61

Dr 9
File BK 36

COUNTY

97195

1
LOWER AFTON ROAD

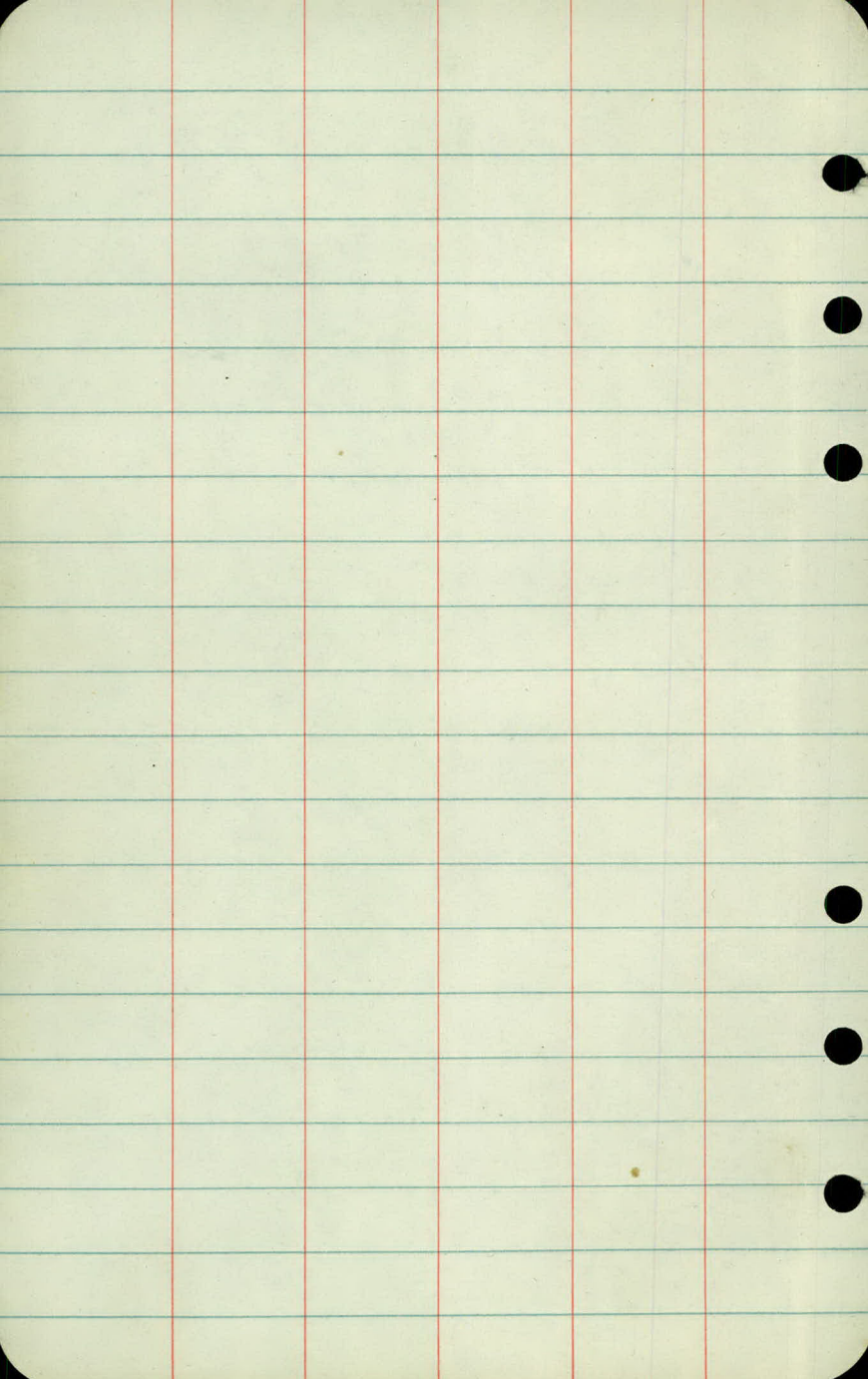
McKNIGHT to EAST COUNTY LINE

LOCATION SURVEY

INDEX:

Alignment

Line 2



FK
RG
KJ
JH

Dec. 15, 1959 a
Cloudy 40°

2

LOWER AETON (County)
Alinement

Line 3

Sta Point ΔL ΔR

+21.70

+21.79 P.T.

16° 10'

26

+50

15° 50.4

15° 05.4

25

+50

14° 20.4

13° 35.4

24

+50

12° 50.4

12° 05.4

23

+50

11° 20.4

10° 35.4

Note

Balance of project
based on chord basis

Not on Arc Method.

W.J.B

22

+50

9° 50.4' $\Delta = 32° 20'$ ✓

9° 05.4

21

8° 20.4 $D = 3'$ ✓

$T = 553.73$

$T = 553.64$

20+97.65 P.I. ✓

+50

7° 35.4

20

+50

6° 50.4 $L = 1077.78$ ✓

6° 05.4

19

+50

5° 20.4 $R = 1909.86$

4° 35.4

18

+50

3° 50.4 $R = 1910.08$ ✓

3° 05.4

17

+50

2° 20.4

1° 35.4

16

+50

0° 50.4

0° 5.4

15+44.01 PC

0° 00'

15+3.92 P.C

0+00 P.I. 136° 25"

FK
JS
KJ
JH

Dec 15, 1959 b.

Dec 16, 1959

27 + 60.00

26 + 21.90

48.30

spike

14" CoH.

52.52

3 Nails

76.74

8" CoH

Disk

88° 35' 30" →

□ ↓ 312

± McKnight Rd

spike

Sta	Point	ΔL	ΔR
-----	-------	------------	------------

57+63.57

57+63.75 $\pm$ E. Co Line Road

31+42.70 P.O.T.

Dec 16, 1959 C

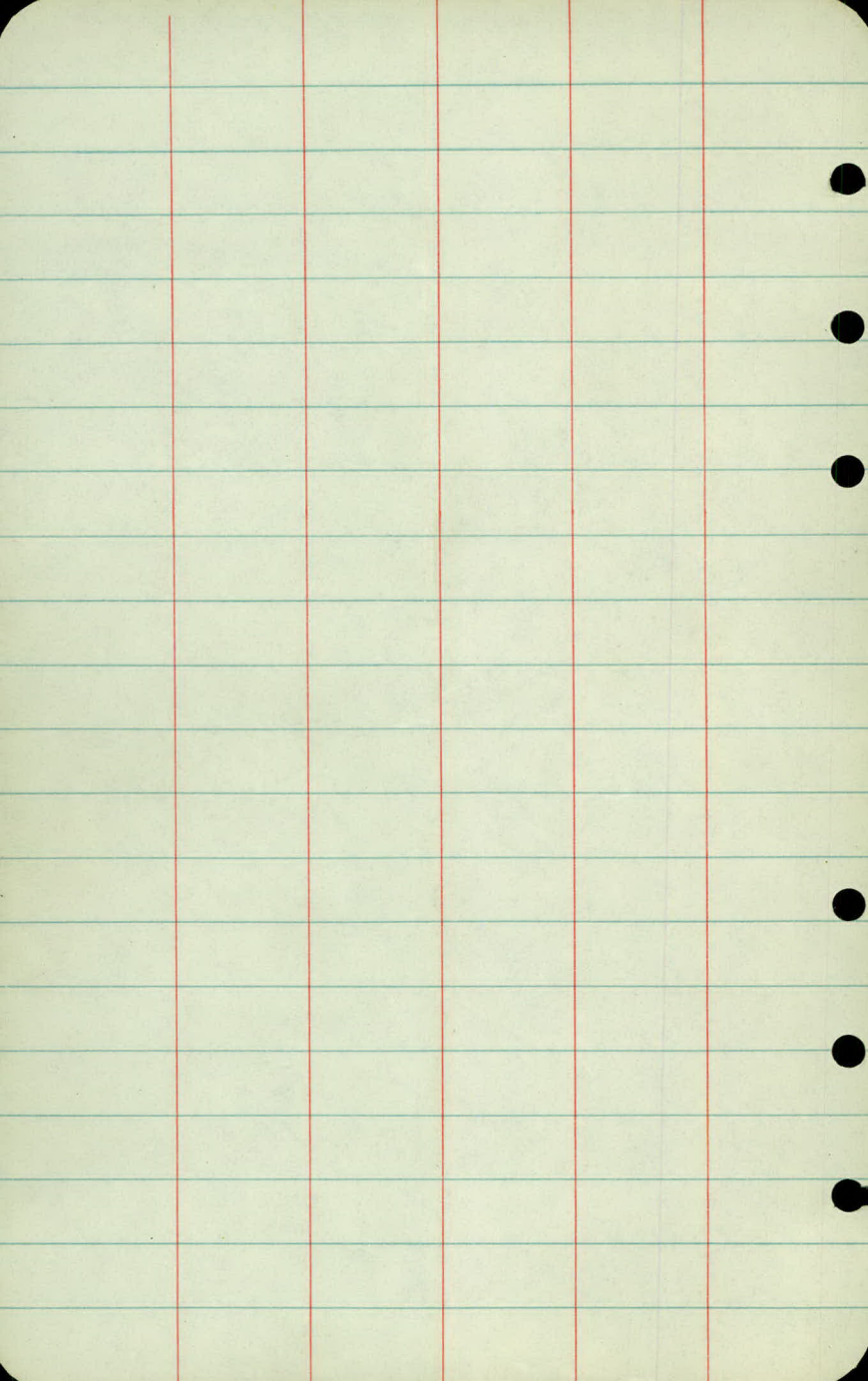
E' 1/4 Cor

Sec 12-28-22

Boat spike

58° 58'

spike



Topography

5

4

3

2

1

0

10	100	<u>Trees</u> 127 - 8	101	<u>£ Creek</u> 9
176			176	<u>£ Creek</u> 4

	177	<u>£ Creek</u> 18		
160	<u>£ Creek</u> 20		160	<u>Trees</u> ← 5

	146	<u>£ Creek</u> 50		
9	<u>Trees</u> 42-139	100	<u>£ Creek</u> 58	

	170	<u>£ Creek</u> 68		
	160	<u>£ Creek</u> 110-76		

130	<u>Begin Trees</u> 100 - 150			
8		100	<u>£ Creek</u> 136	

7

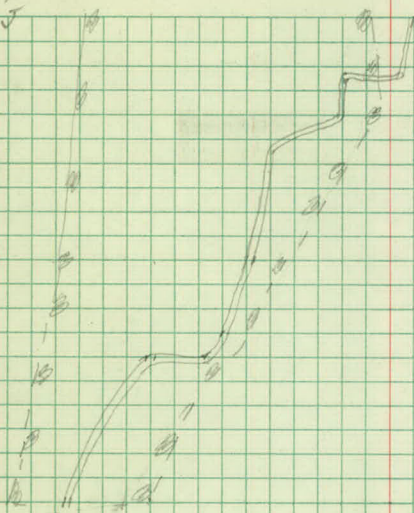
6

5

FK
RG
TD
AJ

Dec 11, 1959

7



15

10

14

13

End Trees
+90 225-65

12

Trees
+100 200 - 77

+100 Trees
195 - 45

11

100 Begin Swamp Drainage
3 ft Lt

+75 Trees
22

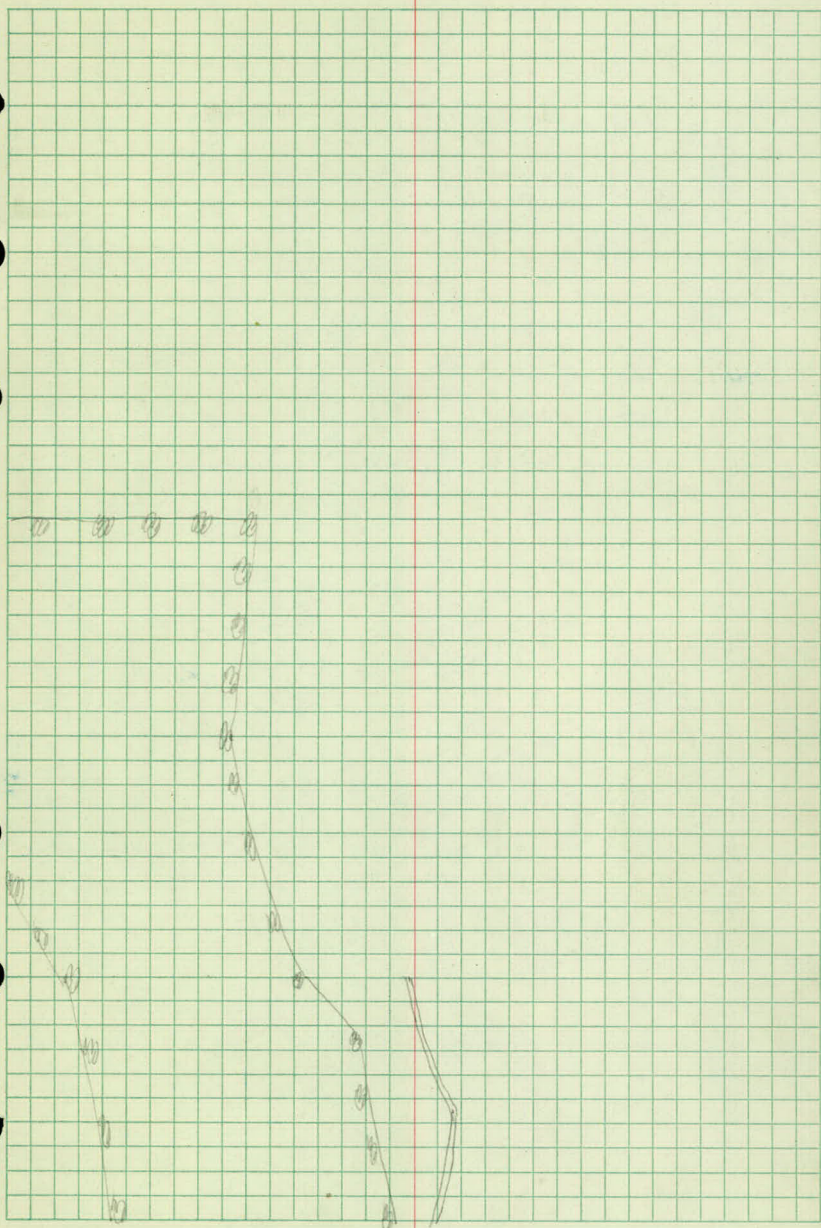
+82 2 Laispot
2

+44 2 Creek
17

10

Dec 11, 1959

8



20

19

18

17

16

15

November 20, 1959 9

00.0

Topography

Sta 20-30

25

24

$$+10 \frac{12''A}{34}$$

$$+97 \frac{6''A}{67}$$

$$+71 \frac{10''A}{61}$$

$$+29 \frac{10''A}{70}$$

$$+23 \frac{10''A}{45}$$

$$+46 \frac{12''A}{52}$$

23

$$+02 \frac{10''A}{60}$$

$$+17 \frac{12''A}{61}$$

$$+92 \frac{12''A}{35}$$

$$+68 \frac{12''A}{29}$$

$$+54 \frac{8''A}{70}$$

$$+21 \frac{10''A}{60}$$

$$+43 \frac{8''A}{44}$$

22

$$+03 \frac{10''A}{77}$$

$$+10 \frac{12''A}{35}$$

$$+43 \frac{12''A}{62}$$

$$+49 \frac{12''A}{16}$$

$$+13 \frac{12''A}{52}$$

$$+27 \frac{12''A}{10}$$

$$+29 \frac{12''A}{57}$$

21

$$+00 \frac{10''A}{24}$$

$$+03 \frac{12''A}{2}$$

$$+30 \frac{14''A}{12}$$

20

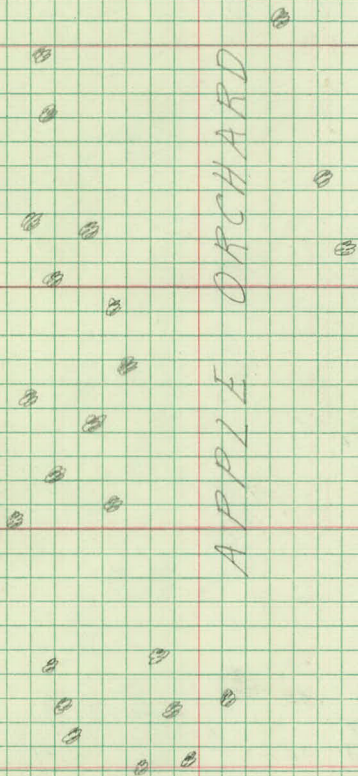
FK
KP
JH

November 20, 1959
Overcast 30°

10

6071

APPLE ORCHARD



30

29

28

27

+78

26

+155

+26

+18

25

+29 X-Fe

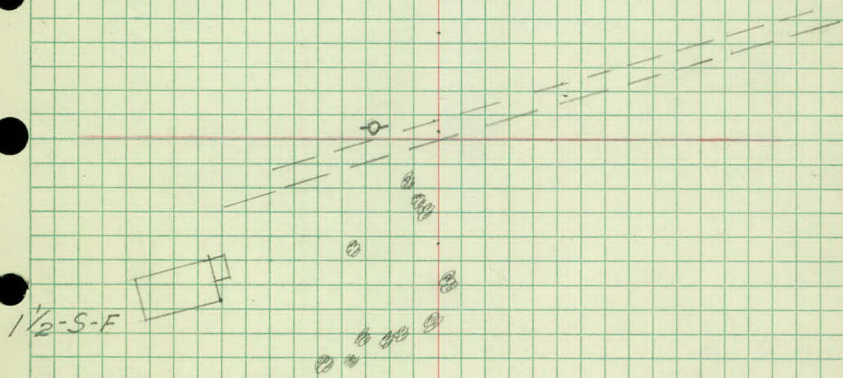
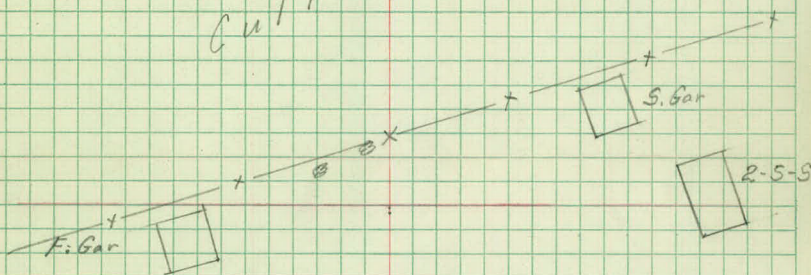
+24 $\frac{4''P}{9}$ +14 $\frac{4''P}{29}$ +99 $\frac{Rtie}{Cor Lt}$ +99 $\frac{Rtie}{Cor Rt}$ +29 $\frac{NW Cor Gar}{87}$ +88 $\frac{NW Cor Ho}{132}$ +44 $\frac{Rtie}{Ho Rt}$ +103 $\frac{PP}{27}$ +102 $\frac{L Ent}{L}$ +18 $\frac{L Ent}{54}$ +171 $\frac{6''C}{5}$ +77 $\frac{6''C}{8}$ +34 $\frac{SW}{90}$ +20 $\frac{5''E}{16}$ +57 $\frac{Rtie}{Ho Lt}$ +19 $\frac{10''E}{31}$ +20 $\frac{5''E}{16}$ +41 $\frac{34 BE}{3}$ +107 $\frac{36''M}{48}$ +109 $\frac{Lilac}{36}$

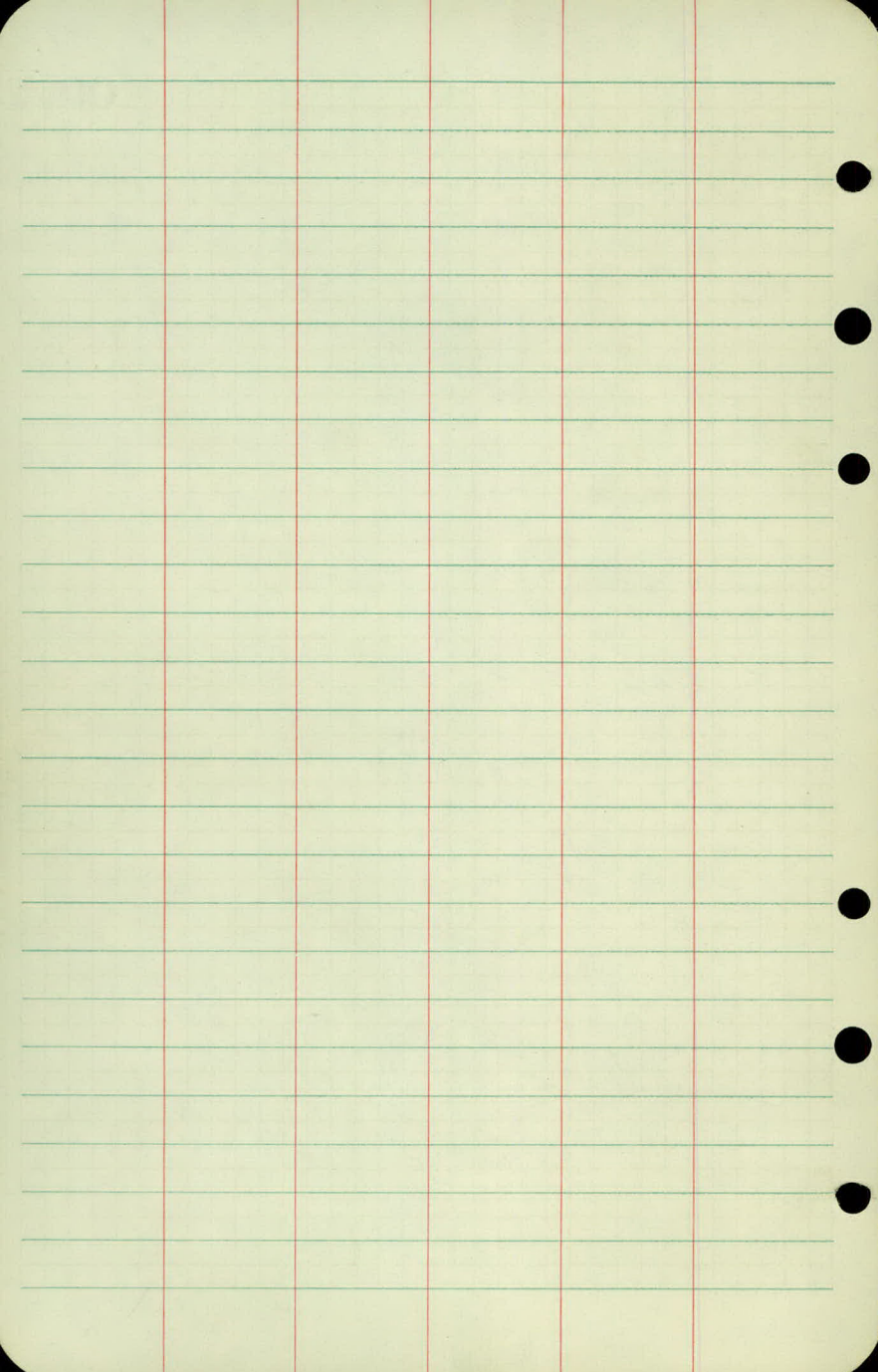
November 20, 1959

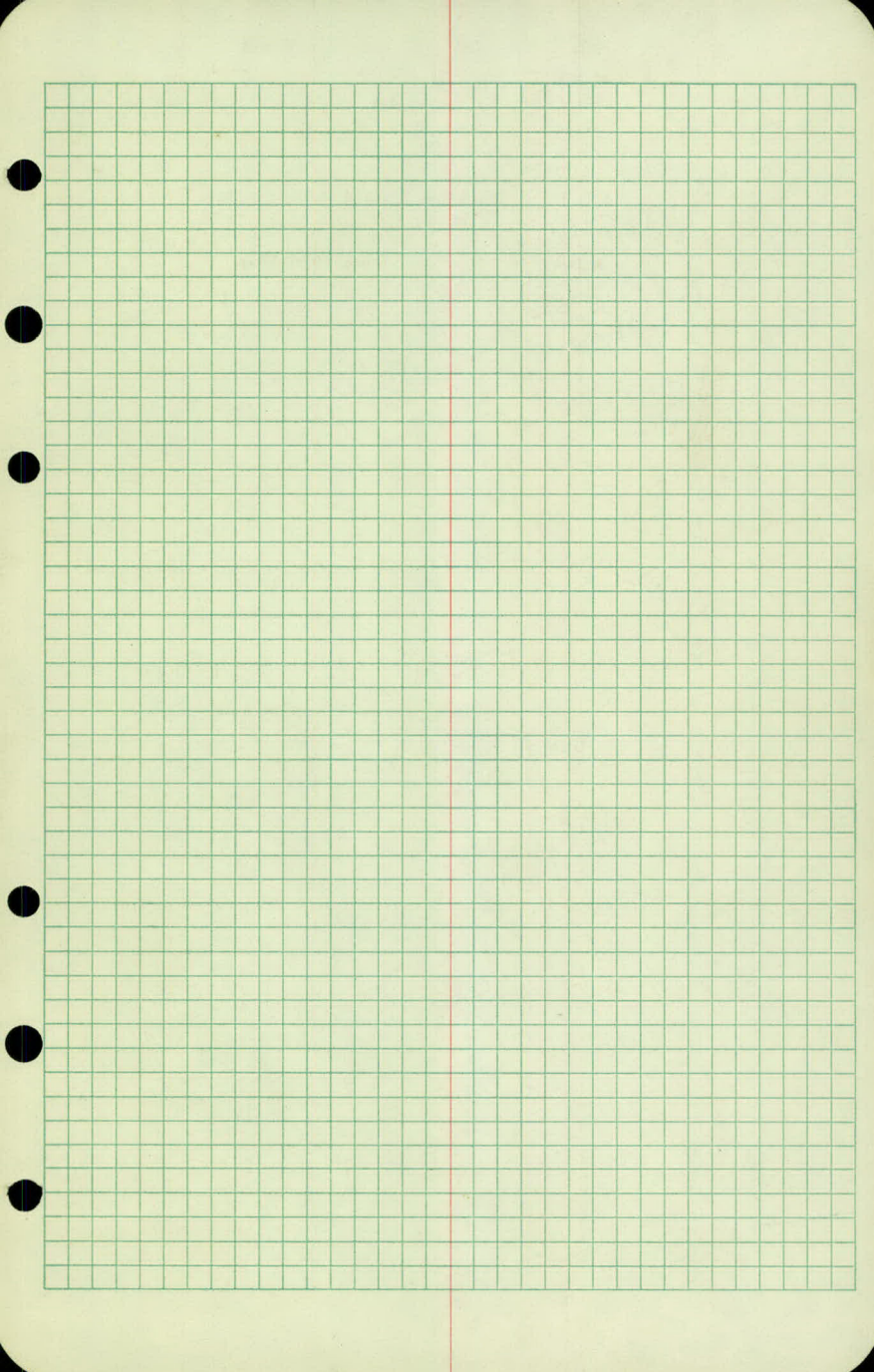
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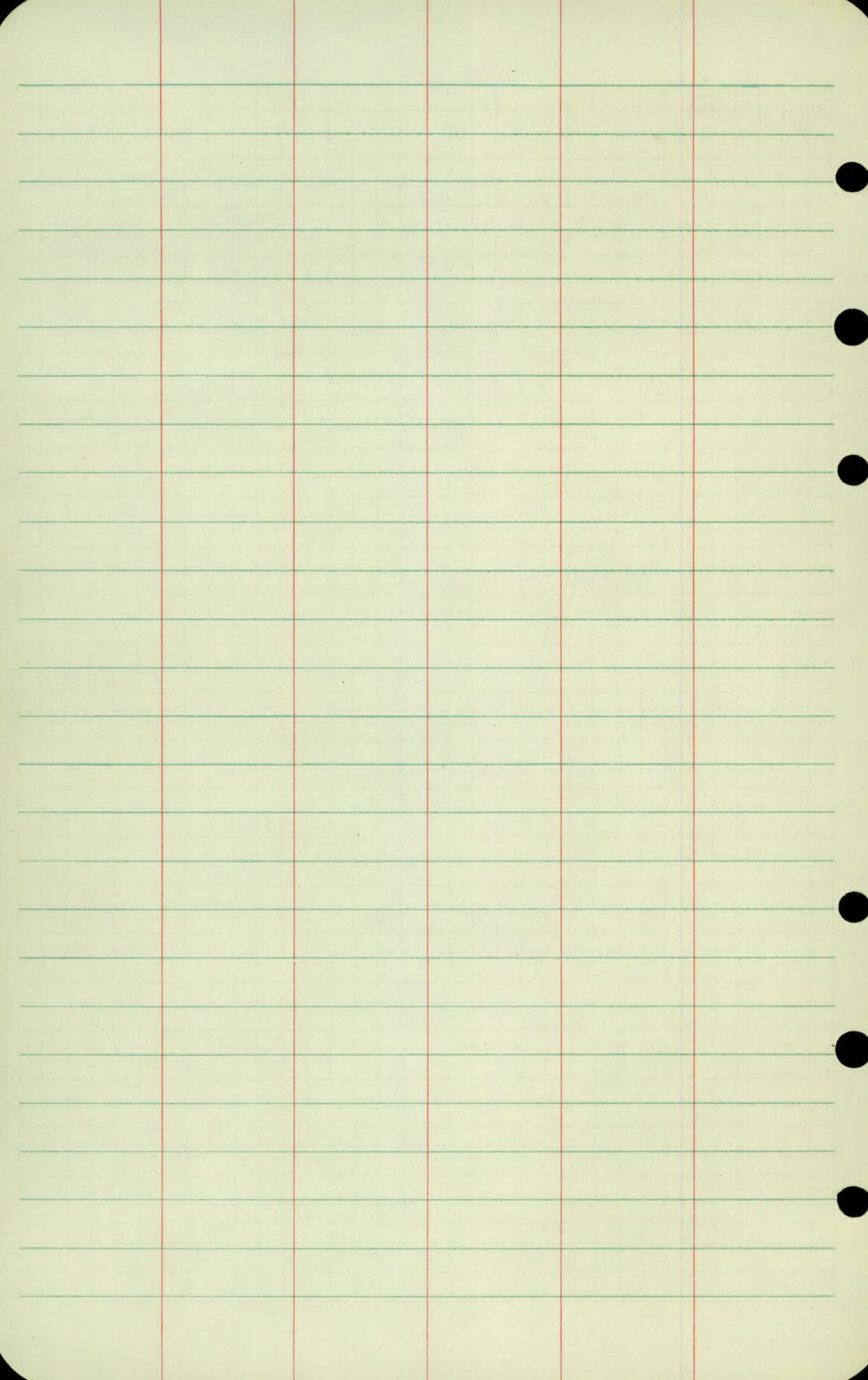
0072

Cultivated









1
Ditch Locations

Stadia

from Line 3

Obj	Az	Sta dia	
At Δ P4 A			1
to Sta 2 Line 3	237°35'	208'	
to Sta 4 Line 3	164°57'	88'	
to Sta 5 Line 3	120°27'	141'	
to BM Spike in 12" oak 74' Lt Sta 5+54			
± Ditch	69°35'	244'	✓
"	58°00'	194'	✓
"	61°00'	160'	✓
"	34°30'	106'	✓
"	41°05'	87'	✓
"	21°20'	67'	✓
"	337°25'	109'	✓
"	312°25'	120'	✓
"	309°00'	165'	✓
"	303°15'	195'	✓
"	296°30'	311'	✓
"	293°00'	305'	✓
"	291°00'	320'	✓

PK R6 KP KT JS JH	Dist	V. Angle	Rod Diff	Dec 17, 1954 Cool, 28° Rod	Elev	2
				1.7		
				2.1		
				2.3		
				2.59		
		-6°03'		9.0		
		-8°06'		8.0		
		-8°12'		13.0		
		-17°20'		6.0		
		-17°20'		11.7		
		-24°55'		10.0		
		-15°26'		10.0		
		-15°26'		8.0		
		-12°00'		6.0		
		-9°49'		7.0		
		-6°09'		8.0		
		-6°00'		10.0		
		-5°28'		12.0		

Sta.

6+80 E Creek 90' Lt.

7+25 E Creek 58' Lt.

7+45 E Creek

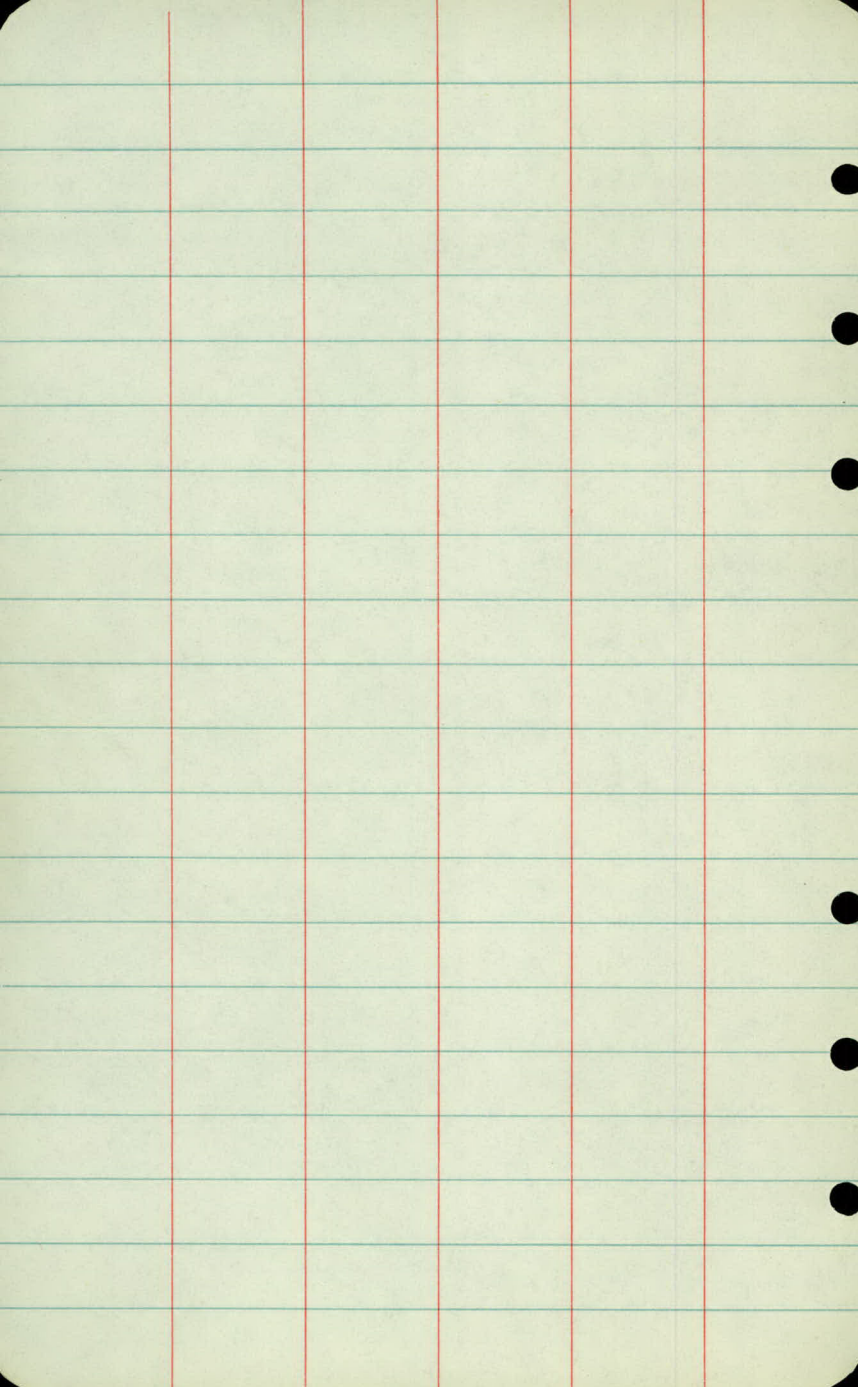
8+00 E Creek 10' Rt.

+24 E Creek 30' Rt.

+80 E Creek 76' Rt To 120'

Dec 17, 1959

3



New Line

Lower Hinton Rd.

Sta 25+00 + 26 +
New Line
Lower Afton Rd.

26 + 79 - N.W. Cor. Ho out 132'
26 + 44 Range Tie to N.W. Cor. Ho

26 + 58 - S.W. Cor. Gar. + 78 Range Tie to S.W. Cor. Gar.
67

+ 20 Range Tie to S.W. Cor. Barn

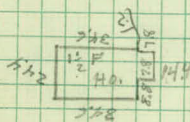
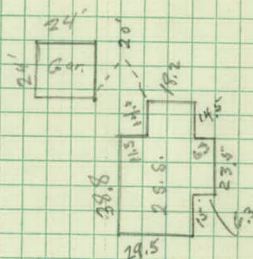
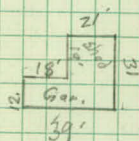
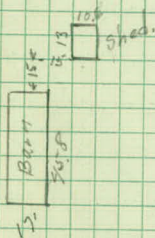
+ 15 - S.W. Cor Barn
304'

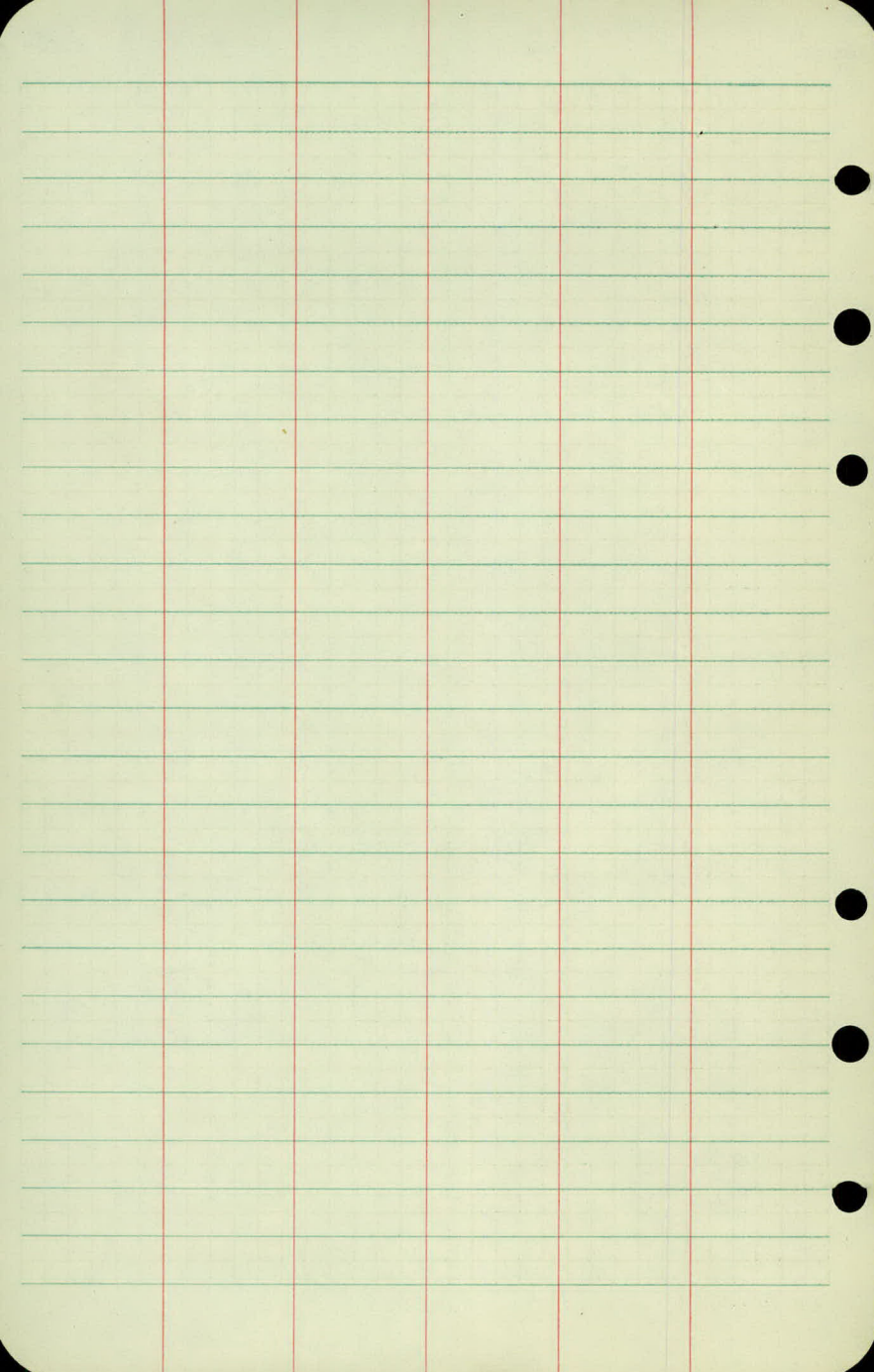
+ 59 S.E. Cor Ho
88
+ 36 - S.W. Cor Ho
90.

25+00

25400 To 26+

15'





New line
lower 17 ft on
work base prop.

Bldgs. removed except barn.
1/10/62 per F.K.
by K.J.

+46 S.W. Cor Ho Range Tie +95 to S.W. Cor
50+00 110'

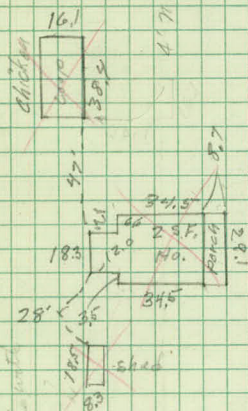
+82-Range Tie S.W. Cor, Barn

+45-S.W. Cor Barn
184'

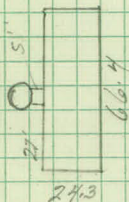
4/8+00

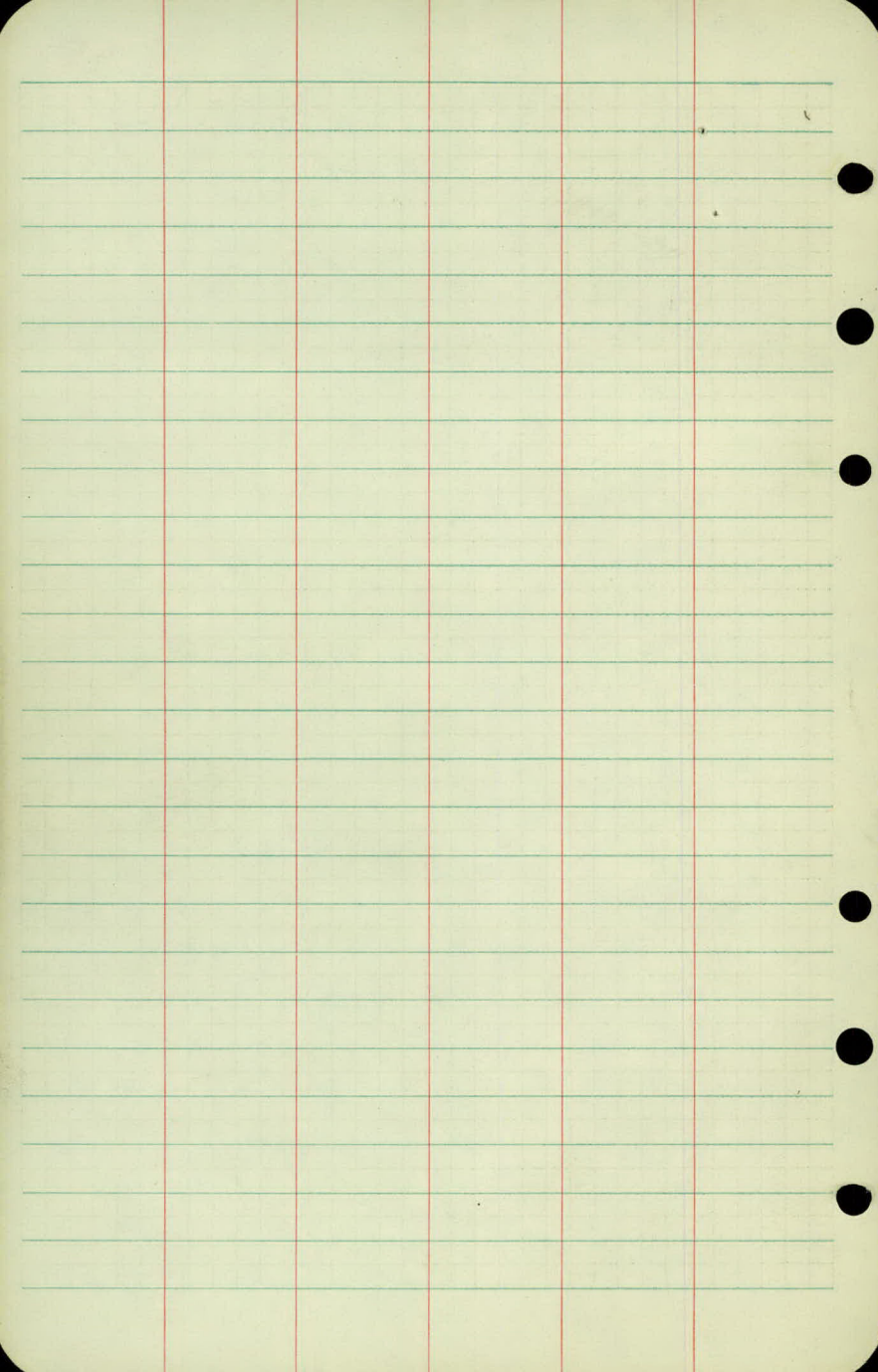
work house prop

12' Holar



6 1/8 13' dia





Oct 21, 1959

~~2005~~

Lower Aften Rd (county)

Alignment
(New)

Line 1

INDEX:

Alignment 1-2

Swamp Loc 3-5

Sta.	Point	ΔL	ΔR
------	-------	------------	------------

9+00			
------	--	--	--

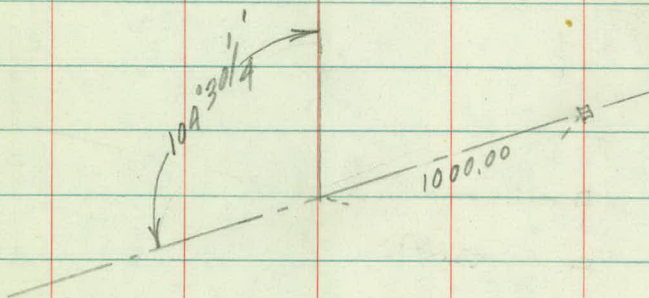
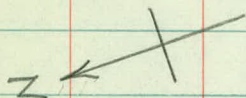
P.O.T.			
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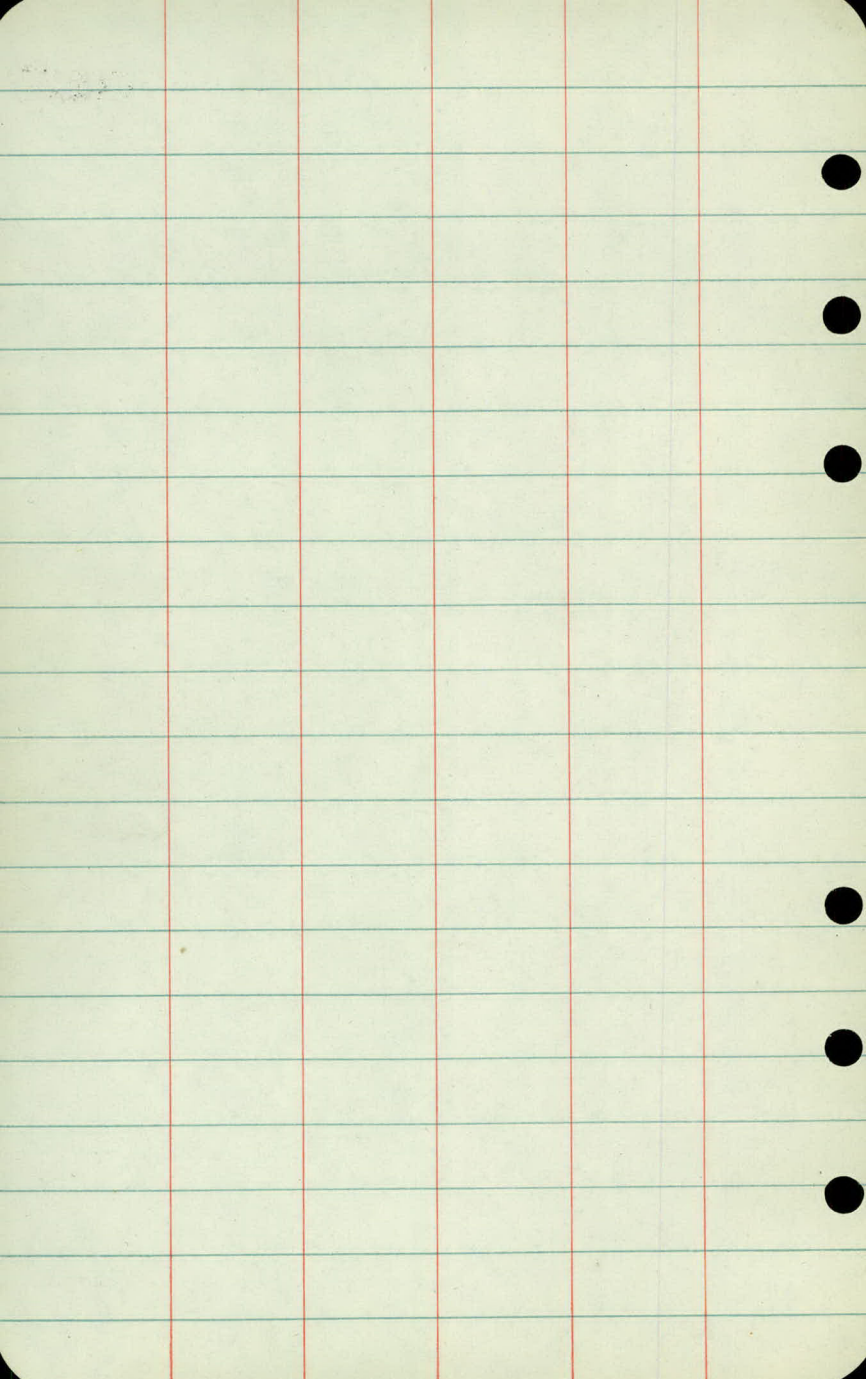
0+00	± McKnight		
------	------------	--	--

FK
RG
KP
HJ
HAW
LC

Oct. 21, 1959

~~0025~~





DIST.

VERT
ANGLE

ROD
EQUIV.

ROD

DIFF.

ELEV
~~6027~~

October 21, 1959

Lower Aston Rd (County)

Stadia

Swamp Location

3 pages

OBJECT

AZ.

STADIA

 π at Sta 9+00

to Sta 5+00

270°00'

 Δ P + A

100°23' 1/2 575

✓

Edge Marsh

90° - 44

✓

" "

122°09' 81

✓

" "

122°55' 128

✓

" "

116°55' 171

✓

" "

103°10' 172

✓

" "

99°16' 238

✓

" "

93°52' 306

✓

" "

94°26' 360

✓

" "

93°21' 460

✓

" "

 π at Δ P + A

to sta 9+00

280°23' 1/2

Edge Marsh

287°05' 530

✓

" "

327°33' 144

✓

" "

06°4' 157

✓

KF 1
LC 1
RG 1
KJ 1
HAW
FK 1

VERT.
ANGLE

ROD
EQUIV.

October 21, 1959
ROD

DIFF.

ELEV.

~~3023~~

OBJECT	AZ.	STADIA	
Edge Marsh (Cor.)	24°40'	152	✓
Low Draw	83°06'	88	
Gully	106°—	141	
"	83°41'	141	
Edge Marsh	57°49'	220	✓
" "	61°38'	282	✓
End Marsh			
Edge Marsh	306°34'	440	✓
" "	320°50'	430	✓
" "	329°02'	403	✓
" "	345°11'	307	✓
" "	358°02'	300	✓
" "	21°35'	248	✓
" "	43°28'	268	✓
" "	49°46'	241 341	✓
SE Cor. Barn	69°30'		

October 21, 1959

DIST.

VERT.
ANGLE

ROD
EQUIV.

ROD

DIFF.

ELEV.

0020

OBJECT

AZI

STADIA

FK
RG
KP
JH

November 18, 1959

2
006

Alignment

Lower Afton Rd. (New Alignment)

Mc Knight to E. Co. Line

Line 2

Sta Point ΔL ΔR

27+29.21 POT

5.73° 48½'E

4+95.38 P.T.

7° 52'

+50

6° 57A

4

5° $\Delta = 15° 44'$

+50

4° $D = 4°$

3+00 P.I.

T = 197.95

3

3° L = 393.33

+50

2° 57.6 R = 1432.69

2

1° 57.6

+50

0° 57.6

1+02.05 PC

0° 00'

5.89° 32½'E

0+00

± Mc Knight

November 18, 1959

3
0063

S.E. Cor.

OF N.E. 1/4 OF
NW 1/4
Sec. 12

255.70

5.00° 12 1/4' W.

74° 00 3/4' →

spike

89° 32 1/2' →

N.W. Cor Sec 12
T28 - R22

312'

999.60

Sta Point ΔL ΔR

56+28.73 $\neq$ STH[#]100

S. 59° 07' E

+85.52 PT	7° 20.75
+50	
44	6° 29.5'
+50	
43	5° $\Delta = 14^{\circ} 41\frac{1}{2}'$
+50	
42	4° $D = 2^{\circ}$
+50	
41+20.28 P.I.	T = 369.34
41	3° L = 734.58
+50	
40	2° R = 2864.93
+50	
39	1°
+50	
38	0° 29.5'
37+50.94 PC	0° 00'

S. 73° 48½' E

FK
RG
KP
JH

November 19, 1959

4

0069

E 1/4 Cor

Sec 12-28-22

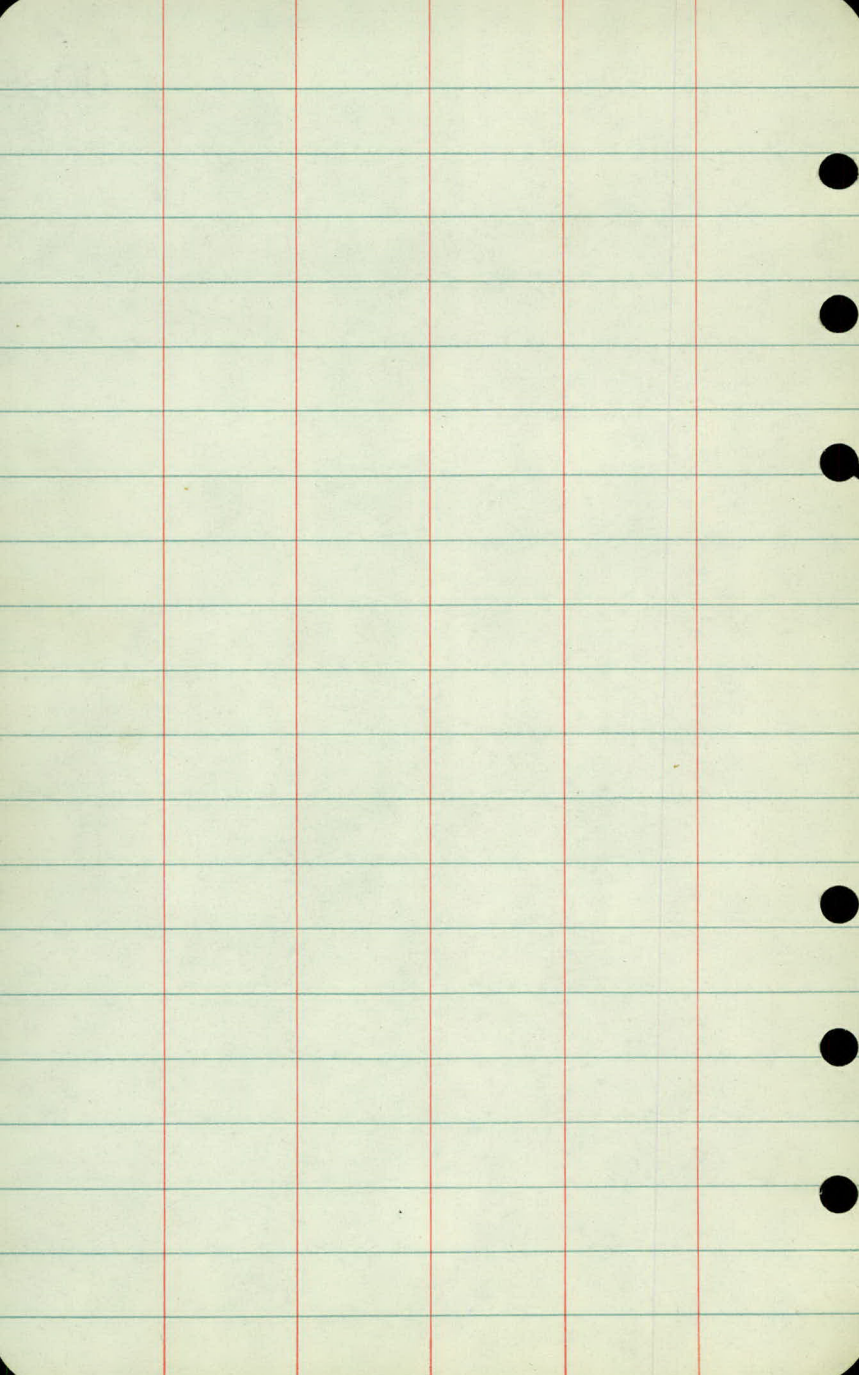
344.22

Boat Spike

5.00° 09' E

58° 58'

Spike



Traverse Line Alignment

McKnight Rd. to Century Ave. T.H. 100

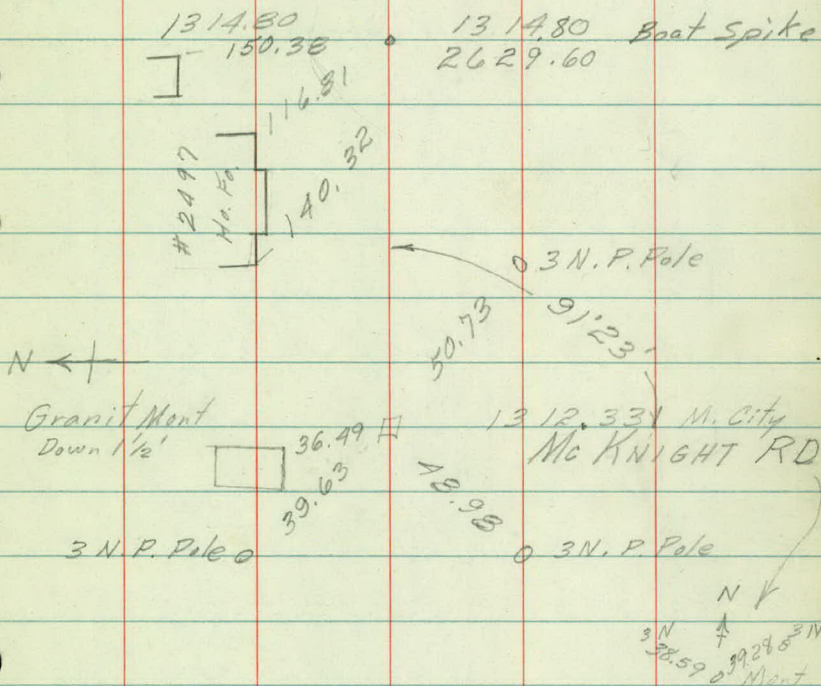
Sta	Point	ΔL	ΔR
-----	-------	------------	------------

26+35.47	P.O.T.	$\frac{1}{4}$	$\frac{1}{4}$ Cor.
----------	--------	---------------	--------------------

0+00	P.I.		
------	------	--	--

Sept. 3, 1959

0004



Sta Point Δ Lt Δ Rt.

+61.78	Pt	$4^{\circ}12'$	
+50		$3^{\circ}46.8'$	$\Delta = 8^{\circ}24'$
+01.92	Pt		$D = 7^{\circ}00'$
33		$2^{\circ}01.8'$	$T = 60.14'$
+50		$0^{\circ}16.8'$	$L = 120.00'$
32+41.78	PC	$0^{\circ}00'$	$R = 819.02'$
+71.58	P.T.	$12^{\circ}25'$	
+50		$10^{\circ}53.5'$	$\Delta = 24^{\circ}50'$
31		$7^{\circ}23.5'$	$D = 14^{\circ}$
+84.53	P.I.		$T = 90.32'$
+50		$3^{\circ}53.5'$	$L = 177.37'$
30		$0^{\circ}23.5'$	$R = 410.27'$
29+94.21	PC	$0^{\circ}00'$	

FX
RL
RR
JF

Sept 4, 1957
Clear 80°
£

~~COO5~~

Boat Spike

Boat Spike

Sta.	Point	ΔL	ΔR
------	-------	------------	------------

+57.64	P.T.	$5^{\circ} 55'$	
--------	------	-----------------	--

+50		$5^{\circ} 45.8'$	
-----	--	-------------------	--

36		$4^{\circ} 45.8'$	
----	--	-------------------	--

 $\Delta = 11^{\circ} 50'$

+50		$3^{\circ} 45.8'$	
-----	--	-------------------	--

 $D = 4^{\circ}$

35+10.29	P.I.		
----------	------	--	--

 $T = 148.48'$

35		$2^{\circ} 45.8'$	
----	--	-------------------	--

 $L = 295.83'$

+50		$1^{\circ} 45.8'$	
-----	--	-------------------	--

 $R = 1432.69'$

34 +50		$0^{\circ} 45.8'$	
--------	--	-------------------	--

33 +61.81	P.C.	$0^{\circ} 00'$	
-----------	------	-----------------	--

FA
RL
RR

Sept 14, 1959

~~CC06~~

24.5°

8°12'
11.50
17.42
20.0°

Boat Spike

Sta Point ΔL ΔR

54+90.00 $\neq$ $STH \#100$

+06.74 PT

$13^{\circ}45'$

42

$13^{\circ}28.8'$

+50

$11^{\circ}28.5'$

41

$9^{\circ}28.8' \Delta = 27^{\circ}30'$

+50

$7^{\circ}28.8' D = 8^{\circ}00'$

+38.37 P.I.

$T = 175.38$

40

$5^{\circ}28.8' L = 343.75$

+50

$3^{\circ}28.8' R = 716.78$

39

$1^{\circ}28.8'$

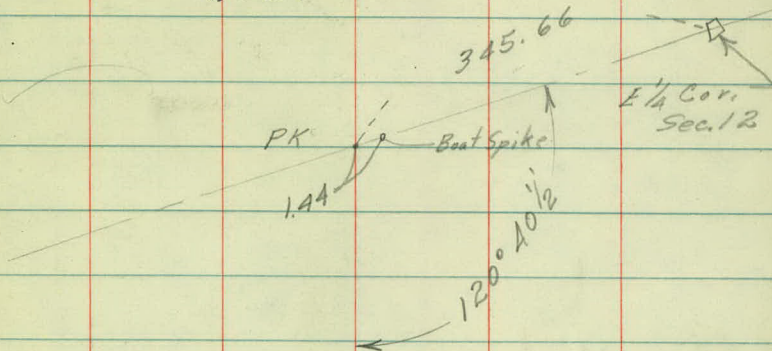
38+62.99 PC

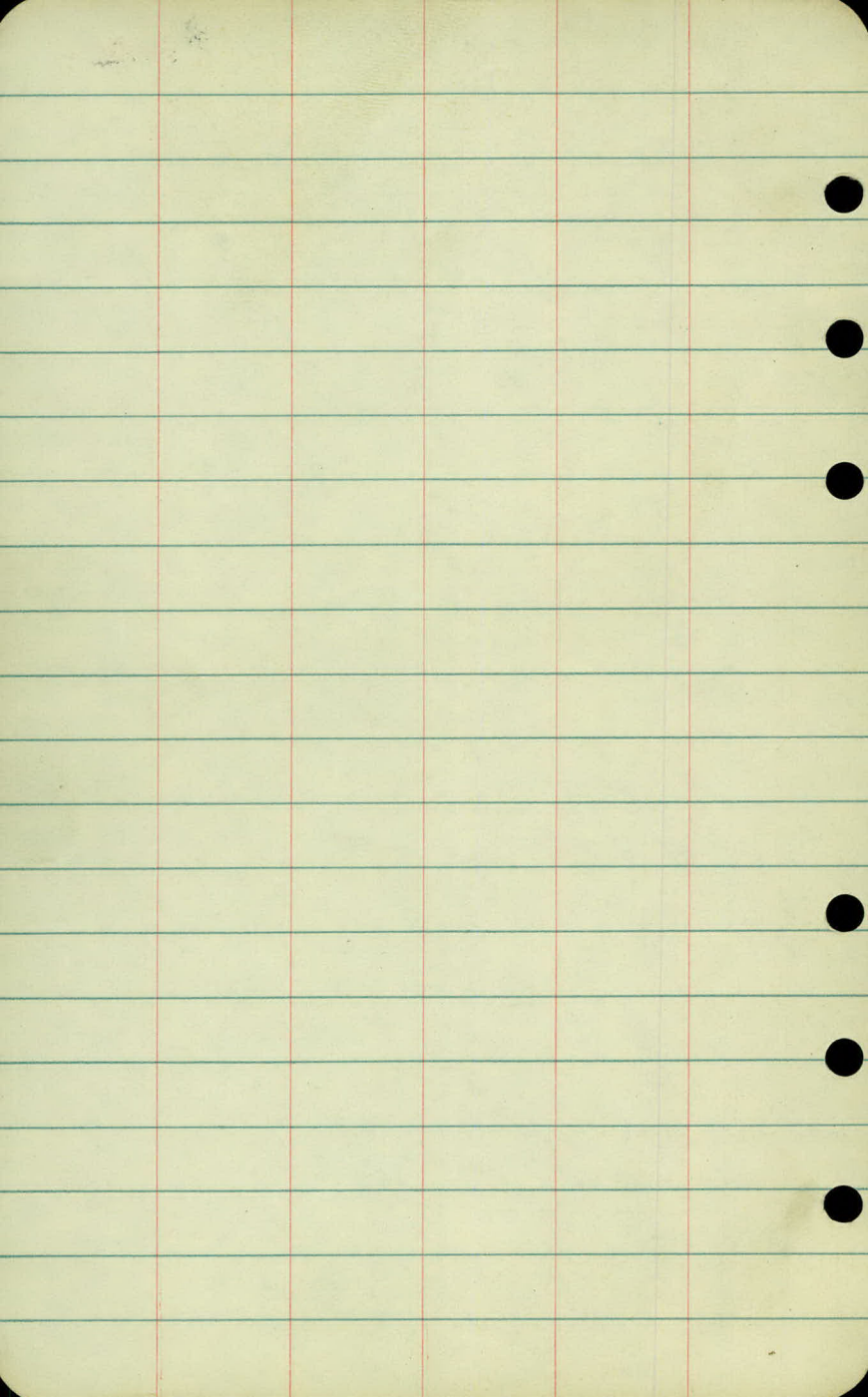
$0^{\circ}00'$

0007

Sept. 14, 1959

3





Building Locations

Stadia

Obj.

Az.

Stadia

T at Sta 47+00

to Sta 54+90

$120^{\circ}40\frac{1}{2}'$

S.W. Cor Barn

$35^{\circ}22'$ 185

N.W. Cor Barn

$33^{\circ}47'$ 217

S.E. Cor Barn

$153^{\circ}12'$ 210

$53^{\circ}12'$

N.W. Cor Ho.

$83^{\circ}-$ 248

S.W. Cor Ho.

$95^{\circ}40'$ 237

S.E. Cor Ho.

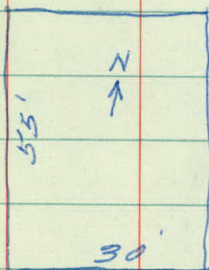
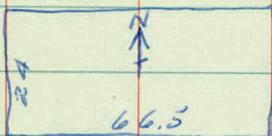
$96^{\circ}-$ 268

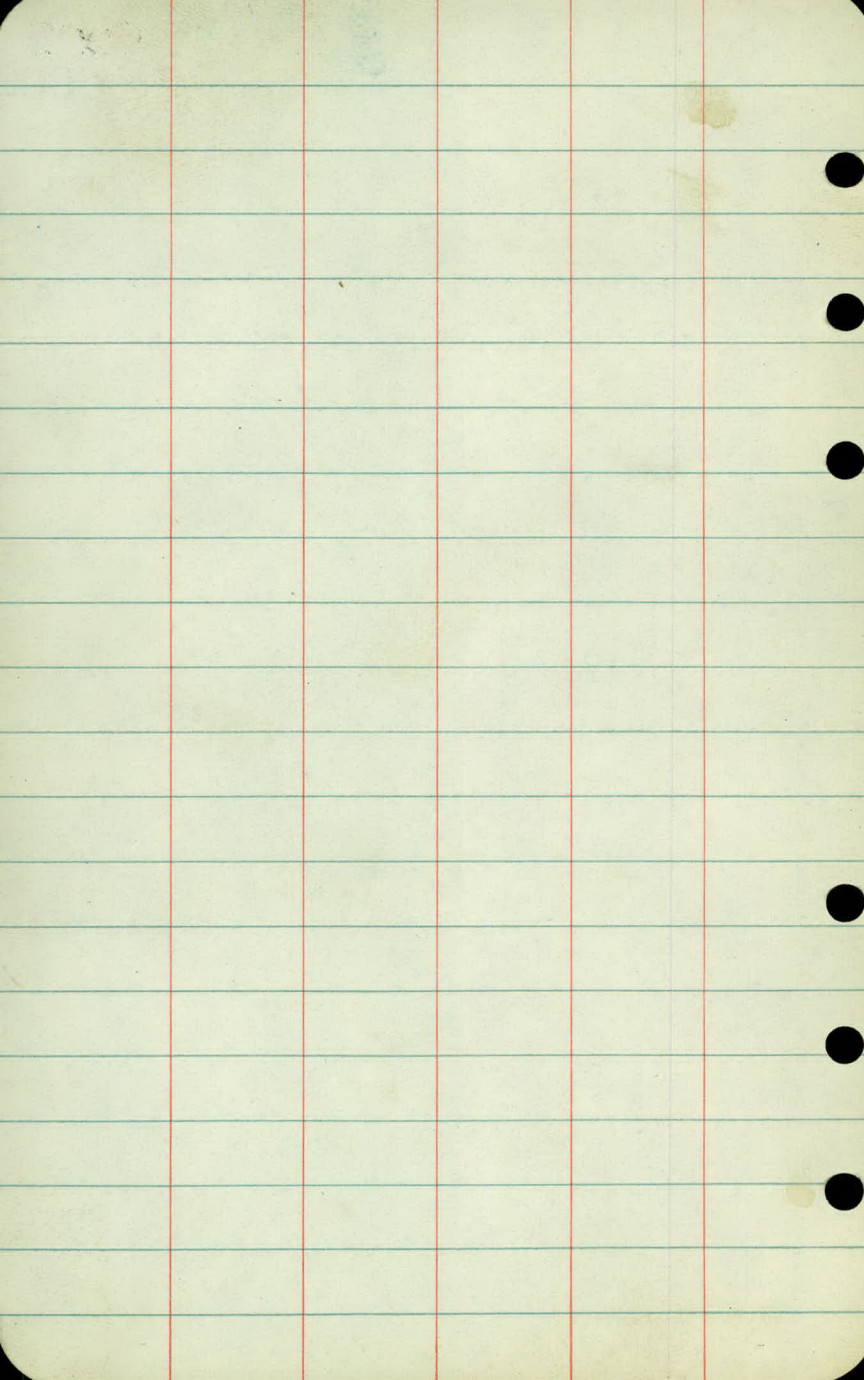
FK
RL
RR

Sept 14, 1959

b

CCCC





FK
KP
UH
KJ

28 Sept. 1959
clear and cool
65°

~~6023~~

Lower Afton Road
StH #100 to McKnight Rd.
Stadia
2 pages.

Object	Az.	Stadia
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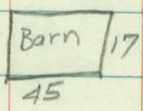
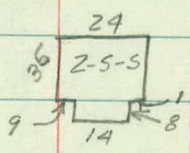
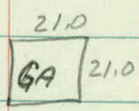
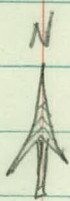
π at sta 24+90 to sta 0+00	270°	
--	------	--

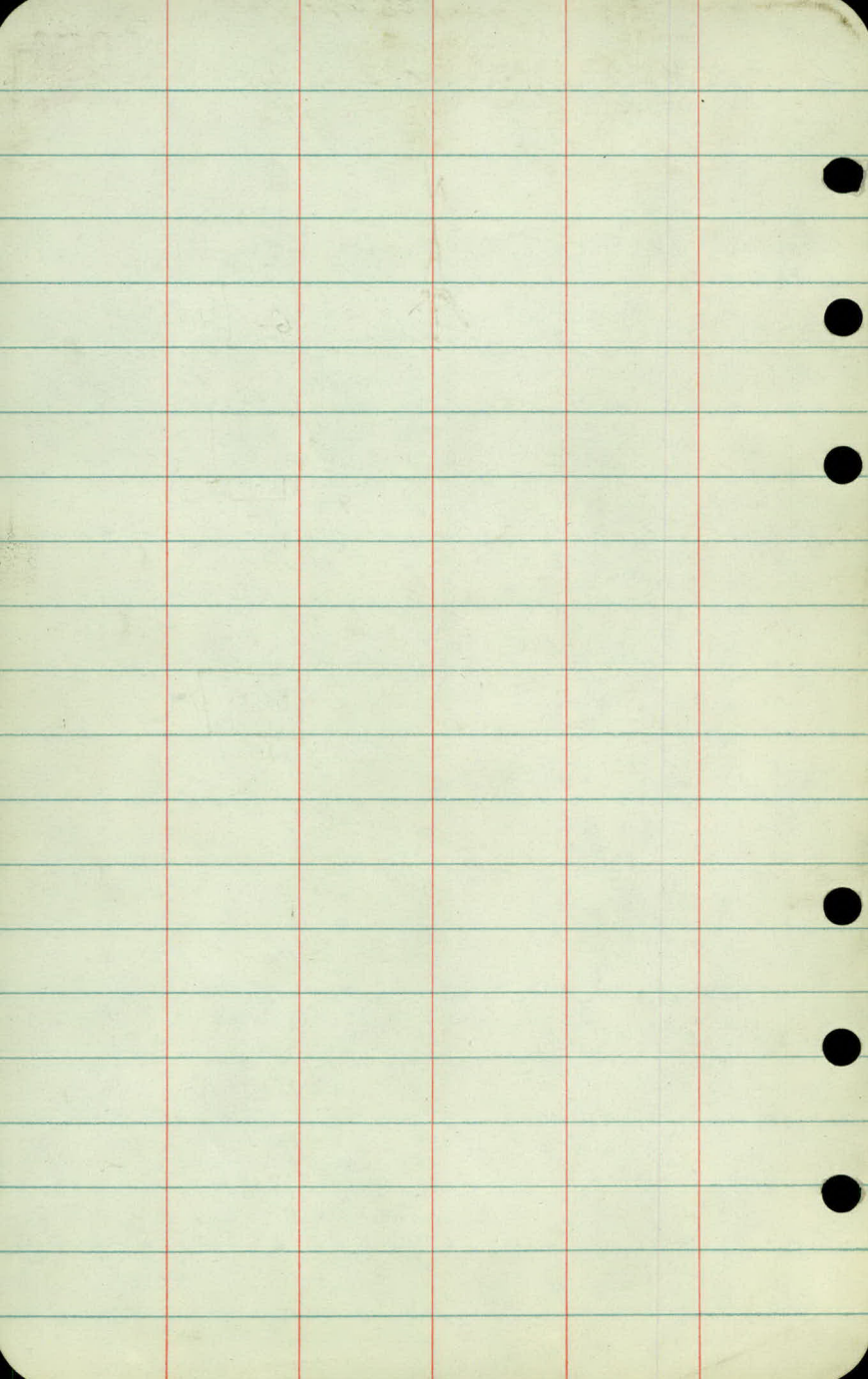
SE. Cor Garage	23°02'	366
S.W. Cor Garage	20°16'	362
NW Cor Garage	19°19'	381
S.E. Cor House	2°42'	392
S.W. Cor House	359°12'	400
SE. Cor. Barn	10°25'	595
S.W. Cor. Barn	6°10'	
N.E. Cor Barn	10°40'	611

28 Sept. 1959

~~0024~~
Elev

Dist.	Vert. angle	ROD EQUIV	ROD	DIFF
-------	----------------	--------------	-----	------





FK
KP
JH

9 October 1959 16
cloudy & cold 40°

~~0045~~

Lower Aston Rd

Profile

McKnight - Lower Aston
to 1000' North

4 PAGES

Sta	+	π	-	Elev.
BM	6.69	957.61		(950.92)
TP1	13.38	970.93	0.06	957.55
TP2	13.32	983.38	0.87	970.06
TP3	2.37	982.73	3.02	980.36
TP4	13.77	991.31	5.19	977.54
TP5	6.14	996.03	1.42	989.89
TP6	10.73	994.62	12.14	983.89
TP7			7.19	987.43
	66.40		29.89	
-	29.89			950.92
	36.51			36.51
	0.59	988.02		987.43
TP8	2.10	978.94	11.18	976.84
BM	0.01	972.01	6.90	972.04 (972.00)
0+00			5.3	66.7

9 Oct. 1959
Cloudy & Cold
45°

17

~~0046~~

P.R. Spike in 18" Oak N.W. Cor McKnight & Linwood
point in road

top 18" stake 40' rt. E 35' SE PP. $\frac{526}{5}$

Spike in Arc light pole Lt. Sta 36+00
reset old BM to 980.26

point in road

top fence post

top S.E. Cor bottom stop Ho #461 McKnight
point in road.

TP 7

point in road

top N.W. Cor Lower stop Ho #366 McKnight

E McKnight & Lower Aston Rd

Sta:	+	π	-	Elev.
		972.01		

0+50			7.6	64.4
------	--	--	-----	------

1			9.4	62.6
---	--	--	-----	------

+33			10.6	61.4
-----	--	--	------	------

+50			12.5	59.5
-----	--	--	------	------

TP	2.73	961.38	13.36	958.65
----	------	--------	-------	--------

2			9.6	51.8
---	--	--	-----	------

+21			11.7	49.7
-----	--	--	------	------

TP	3.07	951.05	13.40	947.98
----	------	--------	-------	--------

+79			0.7	50.4
-----	--	--	-----	------

3			2.4	48.7
---	--	--	-----	------

+50			5.8	45.3
-----	--	--	-----	------

+77			8.6	42.5
-----	--	--	-----	------

4			13.2	37.9
---	--	--	------	------

TP	2.41	940.31	13.15	937.90
----	------	--------	-------	--------

+41			9.0	31.3
-----	--	--	-----	------

+75			10.7	29.6
-----	--	--	------	------

5			10.8	29.5
---	--	--	------	------

+50			13.4	26.9
-----	--	--	------	------

TP	3.28	930.24	13.35	926.96
----	------	--------	-------	--------

FK
KP
JH

October 13, 1959
Overcast 35°

18

~~COAT~~

Sta	+	Σ	-	Elev
-----	---	----------	---	------

930.24

6+00			9.0	21.2
------	--	--	-----	------

+28			11.6	18.6
-----	--	--	------	------

+50			13.7	16.5
-----	--	--	------	------

TP	2.49	919.04	13.69	916.55
----	------	--------	-------	--------

7			8.7	10.3
---	--	--	-----	------

+50			9.8	09.2
-----	--	--	-----	------

8			11.7	07.3
---	--	--	------	------

+50			12.9	06.1
-----	--	--	------	------

9			14.3	04.7
---	--	--	------	------

TP	8.91	916.82	11.13	907.91
----	------	--------	-------	--------

+50			12.4	04.4
-----	--	--	------	------

10			13.0	03.8
----	--	--	------	------

BM	8.00	916.82	8.00	908.82 (908.77)
----	------	--------	------	-----------------

TP	13.38	929.45	0.75	916.07
----	-------	--------	------	--------

TP	13.03	941.77	0.71	928.74
----	-------	--------	------	--------

TP	13.73	955.47	0.03	941.74
----	-------	--------	------	--------

TP	13.01	967.98	0.50	954.97
----	-------	--------	------	--------

TP	6.28	972.67	1.59	966.39
----	------	--------	------	--------

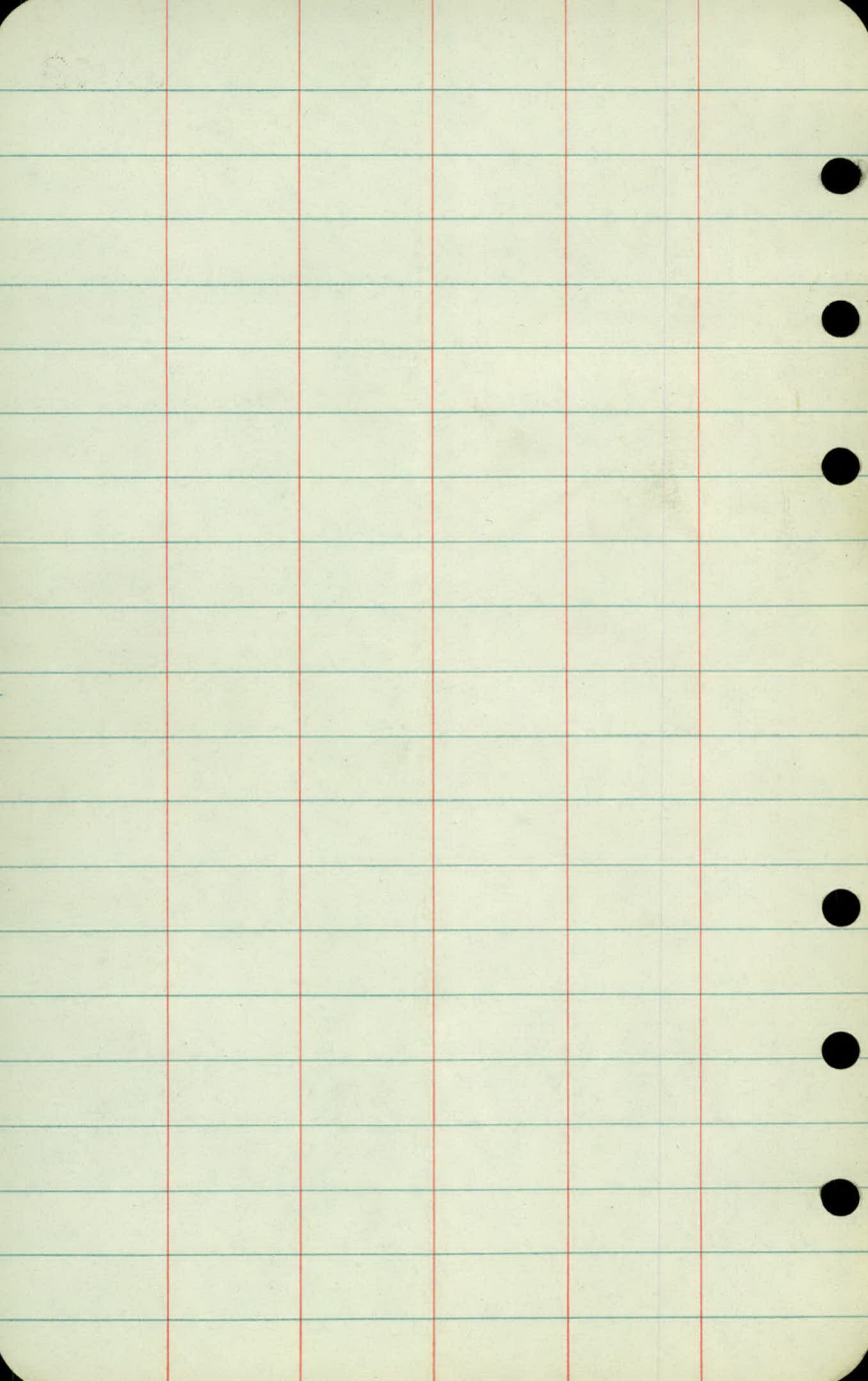
BM			0.57	972.10 (972.00)
----	--	--	------	-----------------

Oct. 13, 1959

~~0048~~

Nail in 14" Oak 8+80

Top N.W. Cor Lower Step #366 Mc Knight



LOWER AFTON ROAD

Profile Levels

McKnight Rd East to Hwy 100

3-12-15-59

LC, KP & JS

Sta	+	π	-	Elev
B.M.	12.91	915.85		902.94
0 + 00			12.0	903.85
+ 11			9.7	06.2
+ 23			6.3	09.6
+ 38			0.9	15.0
T.P.	13.41	928.64	0.62	915.23
+ 54			8.4	20.2
+ 57			6.8	21.8
+ 80			2.4	26.2
T.P.	12.61	941.24	0.01	928.63
1 + 00			10.1	31.1
+ 22			5.9	35.3
+ 50			2.2	39.0
+ 64			1.5	39.7
+ 82			1.4	39.8
2			1.6	39.6
+ 20			1.4	39.8
+ 49			3.0	38.2

Dec 15, 1959

1

SPK in 18" oak 60' Rt. 0-12

910

Sta	+	π	-	Elev
-----	---	-------	---	------

		941.24		
--	--	--------	--	--

2+77			8.2	33.0
------	--	--	-----	------

3			12.2	29.0
---	--	--	------	------

+08			12.8	28.4
-----	--	--	------	------

+36			10.3	30.9
-----	--	--	------	------

+72			4.5	36.7
-----	--	--	-----	------

4			2.1	39.1
---	--	--	-----	------

T.P.	5.16	944.32	208	939.16
------	------	--------	-----	--------

+26			4.3	40.0
-----	--	--	-----	------

+50			4.4	39.9
-----	--	--	-----	------

+78			5.0	39.3
-----	--	--	-----	------

5			5.3	39.0
---	--	--	-----	------

+30			5.2	39.1
-----	--	--	-----	------

B.M			5.65	938.67
-----	--	--	------	--------

+54			4.7	39.6
-----	--	--	-----	------

+76			6.7	37.6
-----	--	--	-----	------

6			12.4	31.9
---	--	--	------	------

T.P.	0.30	932.20	12.42	931.90
------	------	--------	-------	--------

+25			6.1	26.1
-----	--	--	-----	------

Dec 15, 1959

2

SPK in 10" Elm 74' Lt. Sta 5+50 ±

Sta	+	Σ	-	E/ea
		932.20		
6 + 52			11.4	20.8
+ 71			13.5	18.7
T.P.	8.59	927.31	13.48	918.72
7			12.1	15.2
+ 40			13.2	14.1
+ 46			16.3	11.0
+ 53			creek 17.4	09.9
+ 87			15.8	11.5
+ 95			12.2	15.1
8			12.1	15.2
+ 28			9.5	17.8
+ 47			6.8	20.5
+ 76			4.6	22.7
9			1.7	25.6
T.P.	13.31	940.61	0.01	927.30
+ 26			11.1	29.5
+ 40			8.1	32.5
+ 56			5.0	35.6

Dec 15, 1959

3

Sta	+	Σ	-	Elev
		940.61		
9+71			1.2	39.4
T.P.	9.24	949.84	0.01	940.60
10			5.7	44.1
+36			3.6	46.2
+72			2.4	47.4
11			1.6	48.2
+33			2.6	47.2
+72			4.5	45.3
12			4.9	44.9
+28			5.5	44.3
+67			8.1	41.7
+85			9.4	40.4
13			9.3	40.5
+11			9.7	40.1
+26			11.5	38.3
+44			12.8	37.0
+61			12.3	37.5
+81			8.9	40.9

Dec. 15, 1959

4

Sta	+	Σ	-	Elev.
		949.84		
14	+00		5.5	44.3
	+21		1.4	48.4
T.P.	13.40	963.14	0.10	949.74
	+55		8.0	55.1
	+62		6.4	56.7
15			3.2	59.9
	+34		0.4	62.7
T.P.	11.66	974.34	0.46	962.68
	+69		10.8	63.5
	+93		10.5	63.8
16			9.6	64.7
	+14		7.6	66.7
	+50		5.9	68.4
	+75		4.5	69.8
17			3.3	71.0
	+25		2.0	72.3
	+50		0.5	73.8
T.P.	8.16	982.06	0.44	973.90

Dec 15, 1959

5

Sta	+	π	-	Elev
		982.06		
18 + 00			6.1	76.0
+ 36			5.4	76.7
+ 50			5.5	76.6
+ 75			6.4	75.7
19			7.9	74.2
+ 22			10.2	71.9
+ 50			11.3	70.8
+ 75			12.4	69.7
20			13.4	68.7
T. P.	3.38	972.13	13.31	968.75
B. M			8.50	963.63
+ 50			4.9	67.2
+ 58			5.4	66.7
+ 80			4.3	67.8
21			3.7	68.4
+ 34			2.5	69.6
+ 50			2.8	69.3
+ 79			4.2	67.9

Dec 15, 1959

6

76

76

910

66

3/5

4

92

SPK in 10" Coll. 100 ± Lt. Sta. 20+15

Sta	+	π	-	Elev.
		972.13		
22+00			4.8	67.3
+50			6.3	65.8
23				
BM	11.25	974.88		963.63
22+50			9.1	65.8 ✓
+82			10.0	64.9
23			10.6	64.3
+35			10.9	64.0
+50			10.5	64.4
+80			10.0	64.9
24			9.5	65.4
+27			9.1	65.8
+50			8.2	66.7
+80			2.6	67.3
25			6.8	68.1
+29			4.0	70.9
+50			1.6	73.3
TP	13.13	981.42	1.59	973.29

FK
JS
KJ
JH

Dec 15, 1959

Dec 16, 1959

7

Spike in 10" C.A. 100' $\pm$ Lt Sta 20+15

Sta	+	π	-	Elev	
		986.42			
25+80			9.9	76.5	
26			8.6	77.8	
+22			7.6	78.8	
+48			6.0	80.4	
+79			1.6	84.8	
TP	13.65	999.88	0.19	986.23	
27			12.3	87.6	
+28			13.0	86.9	
+70			14.0	85.9	
28			14.4	85.5	
+30			13.4	86.5	11.5
+68			15.1	84.8	
29			16.1	83.8	
+17			16.1	83.8	
+64			12.4	87.5	
30			5.4	94.5	
+39			0.2	99.7	
TP	8.35	1005.32	2.91	996.97	

~~4~~ Dec. 16, 1959

8

style

Nail in Fe Post

Sta	+	Δ	-	Elev
		1005.32		
30+70			4.5	00.8
31			3.8	01.5
+43			2.9	02.4
+75			3.0	02.3
32			2.8	02.5
+45			3.1	02.2
+70			3.2	02.1
33			3.3	02.0
+38			5.5	99.8
+73			7.5	97.8
34			8.5	96.8
+40			10.1	95.2
+75			11.3	94.0
35			11.9	93.4
+35			13.0	92.3
TP	11.07	1004.57	11.82	993.50
+70			14.2	90.4
36			15.2	89.4

± Dec. 16, 1959

9

Sta	+	π	-	Elev
		1004.57		
36+50			15.5	89.07
37			15.5	1006.07
+50			15.5	
38			14.7	89.9
+32			13.7	90.9
+59			12.9	91.7
39			11.2	93.4
+40			9.7	94.9
+63			8.8	95.8
+90			6.4	98.2
+93			5.1	99.5
40			4.6	00.0
+36			2.7	01.9
+61			0.8	03.8
BM	12.76	1016.81	0.52	1004.05
41			11.6	05.2
+27			10.7	06.1
+58			8.2	08.6
			0.52	

Dec 16, 1959

10

Spike in PPLT Sta 39+80

Sta	+	X	-	Elev
		1016.81		

42			5.1	11.7
----	--	--	-----	------

+33			4.9	11.9
-----	--	--	-----	------

+54			4.0	12.8
-----	--	--	-----	------

+80			5.7	11.1
-----	--	--	-----	------

+91			7.4	09.4
-----	--	--	-----	------

+97			7.2	09.6
-----	--	--	-----	------

43			8.0	08.8
----	--	--	-----	------

+34			7.1	09.7
-----	--	--	-----	------

+60			6.4	10.4
-----	--	--	-----	------

44			5.0	11.8
----	--	--	-----	------

45			2.4	14.4
----	--	--	-----	------

46			0.1	16.7
----	--	--	-----	------

TP	11.55	1028.30	0.06	1016.75
----	-------	---------	------	---------

47			9.5	18.8
----	--	--	-----	------

48			7.4	20.9
----	--	--	-----	------

49			5.3	23.0
----	--	--	-----	------

50			3.4	24.9
----	--	--	-----	------

51			1.6	26.7
----	--	--	-----	------

TP	10.98	1038.55 938.55	0.73	1027.57
----	-------	------------------------------	------	---------

Dec 16, 1959

11

Sta + π - Elev.

~~1038.55~~
~~938.55~~

52 9.7 28.9

53 7.6 31.0

54 6.0 32.6

55 4.7 33.9

56 3.8 34.8

57 2.5 36.1

+63.75 2.1 36.5

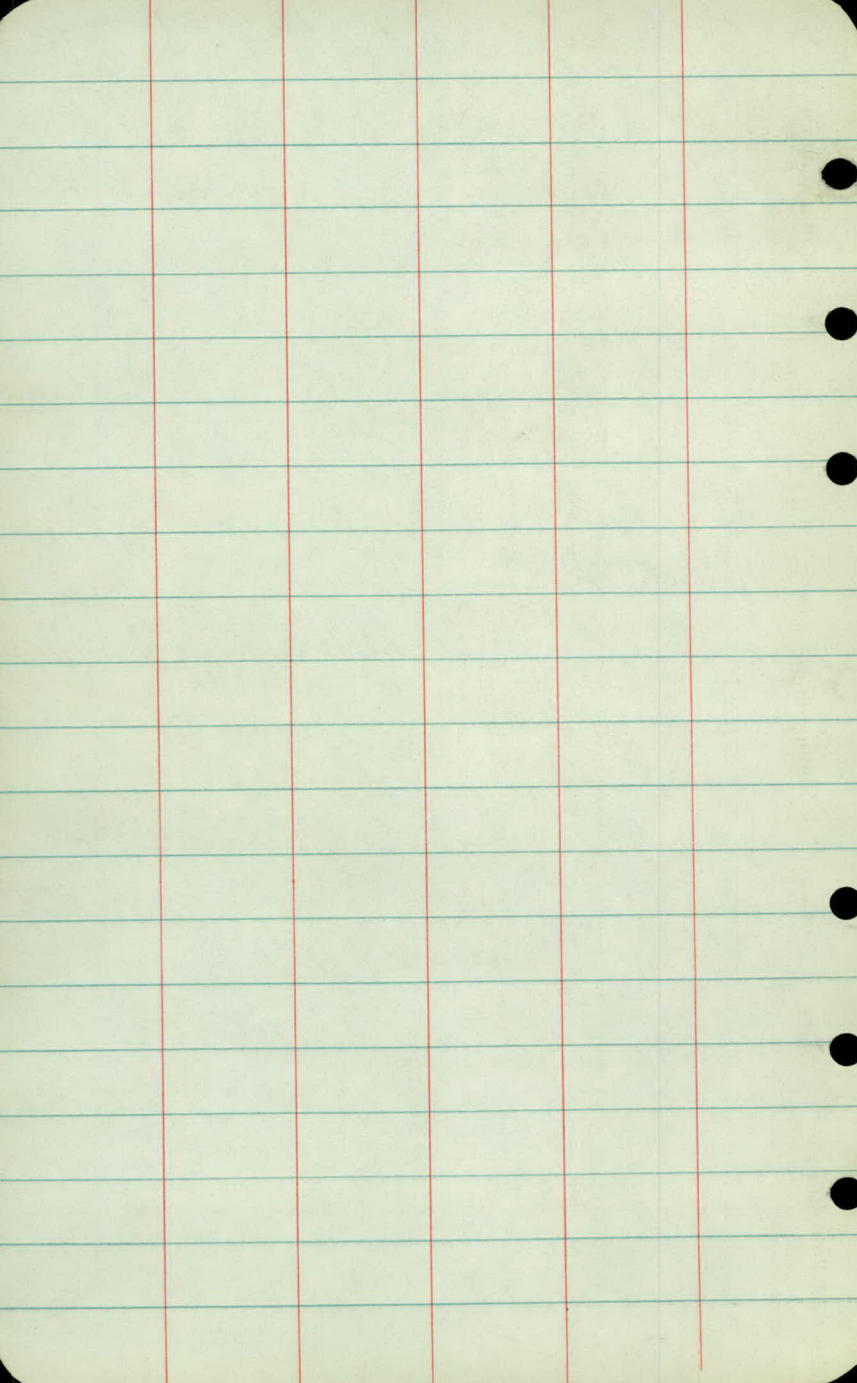
BM 1.97 ~~1036.58~~
936.58

Dec 16, 1959

12

£ STH #100

Spike in PP N.W. Cor Lower Aston Rd & STH #100



R6
JS
JL
WM
FS

March 22, 1961
Cool 35°, cloudy

Lower Afton Road

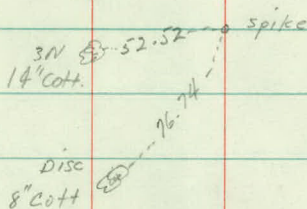
Line # 3

McKnight Rd. to E. Co. Line (Hwy. #100)

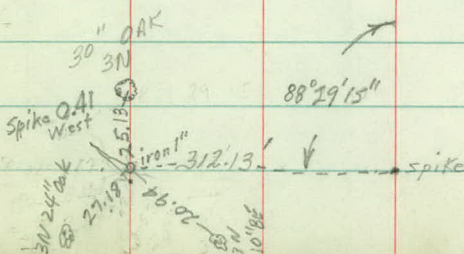
Title	Page	1
Alinement	"	2-3
Topography	"	4-28
Bench Levels	"	29-31
X-sections	"	32-69
Profiles	"	70-72
Bench Level rerun	"	73-76

Sta	Point	DefL	DLT	ΔPT
22	78+00	9°50.5'		
+50		9°05.5'		
21+00	77+00	8°20.5'		
76+97.65				
20+97.65	PI			
+50		7°35.5'		Chord Method
20	76+00	6°50.5'		Δ = 32°20' RT.
+50		6°05.5'		D = 3°
19	75+00	5°20.5'		T = 553.73
+50		4°35.5'		L = 1077.78
18	74+00	3°50.5'		R = 1910.08
+50		3°05.5'		
17	73+00	2°20.5'		
+50		1°35.5'		
16	72+00	0°50.5'		
+50		0°05.5'		
71+43.92				
15+43.92	PC	0°00'		0°00'
56+00				
0+00				

NW Cor Sec 12
Twp 28 Rge 22



2 - 1 -



McKnight Rd

Sta	Point	Defl	ΔL	ΔR
113+64.54				
57+64.54	E Hwy 100			

100+00				
44+00	POT			

82+21.70				
+21.70	PT	16°10'00"		

26 82+00		15°50.5'		
----------	--	----------	--	--

+50		15°05.5'		
-----	--	----------	--	--

25 81+00		14°20.5'		
----------	--	----------	--	--

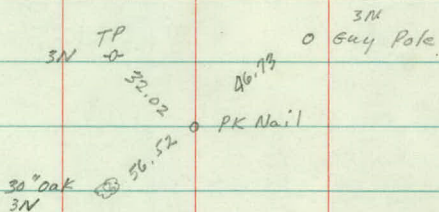
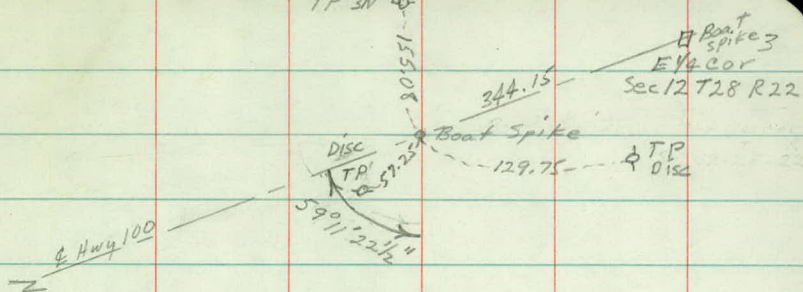
+50		13°35.5'		
-----	--	----------	--	--

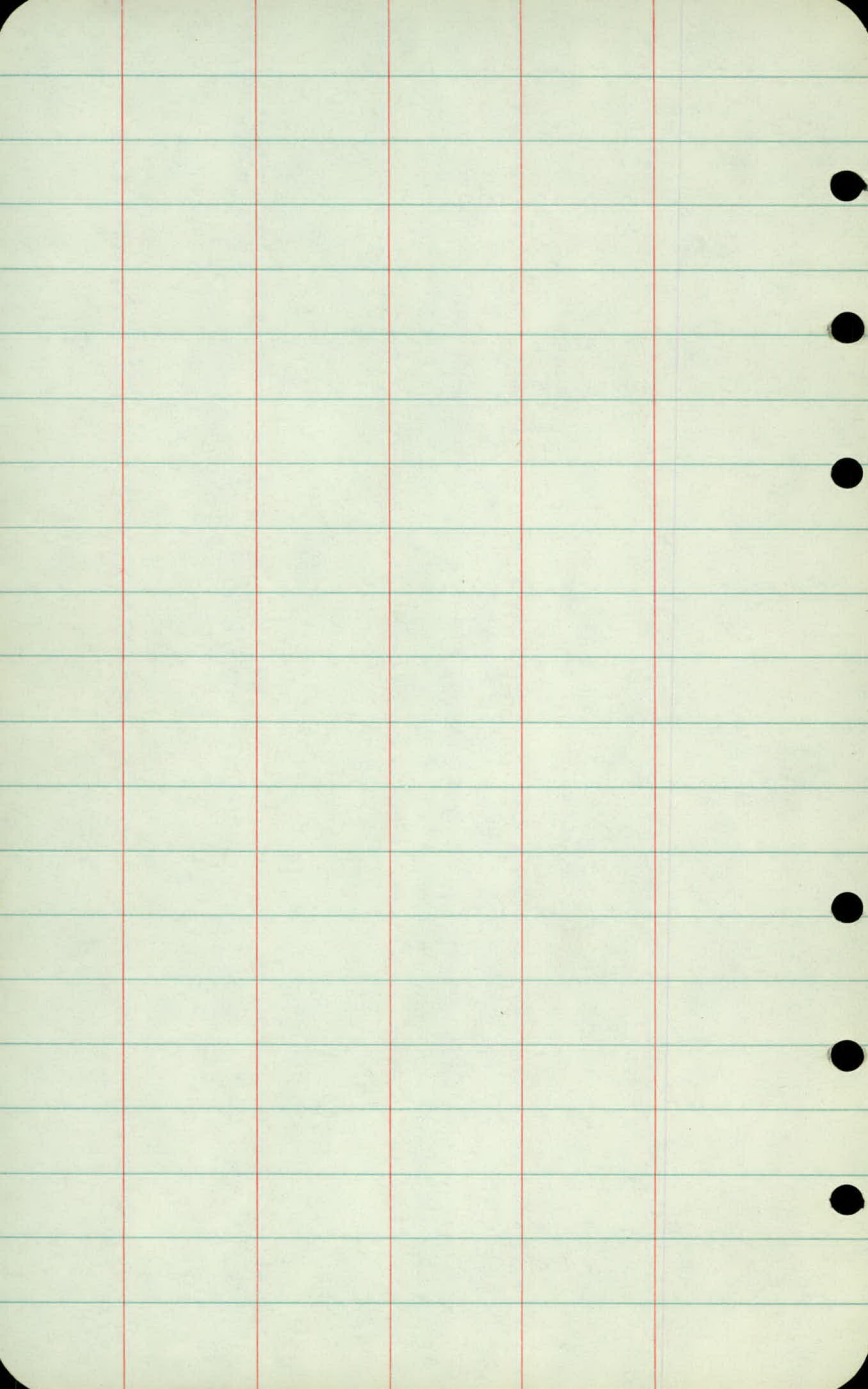
24 80+00		12°50.5'		
----------	--	----------	--	--

+50		12°05.5'		
-----	--	----------	--	--

23 79+00		11°20.5'		
----------	--	----------	--	--

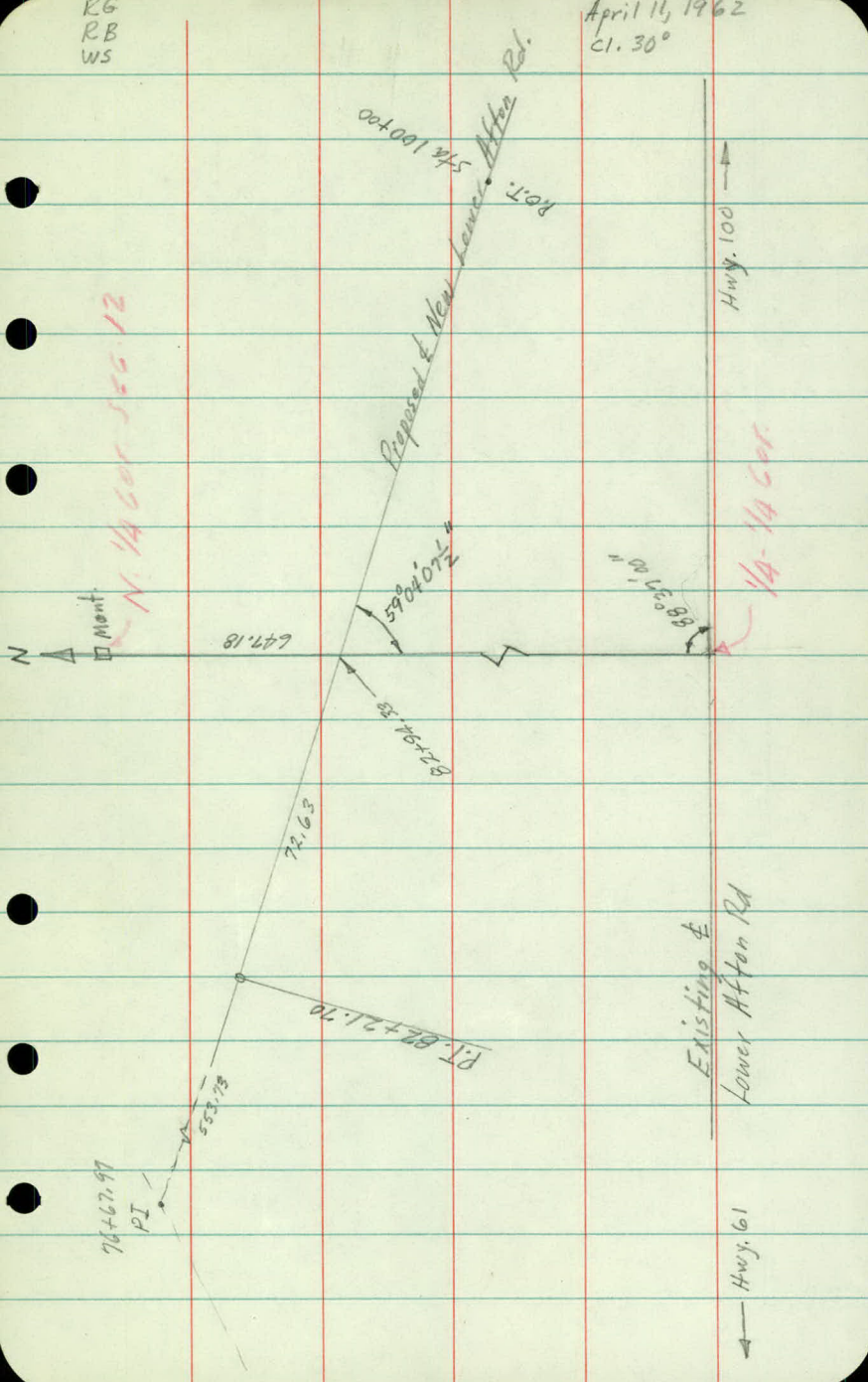
+50		10°35.5'		
-----	--	----------	--	--





KG
RB
WS

April 11, 1962
Cl. 30°



Reg. 7/11/62

MARCH 17, 1961

4

TOPOGRAPHY

LOWER AFTON Rd.
McKNIGHT TO E. Co. Line

pages 4-28

Lt

Q

Rt +49 1' NOR

+44 1' NOR
1
58+00
2+00

+48 J.P. 7'
14

+43 J.P. 7'
7

+41 JACK PINE 7'
10

+37 4' NORWAY
22

+29 1' NORWAY
20

+25 2' NORWAY
29

+19 2' NORWAY
34

+07 4' NORWAY
22

+49 1' NOR
3

+47 2' NOR
30

+47 3' NOR
35

+47 3' NOR
62

+41 3' NOR
48

+98 4' NORWAY
35

+88 3' NORWAY
86

+85 3' NORWAY
89

+77 3' NORWAY
39

+46 3' NORWAY
9

+11 2' NORWAY
43

57+00
1+00

+79 END Hazel Brush
0-100'

+91 4' NORWAY
40

+90 4' NORWAY
36

+79 4' NORWAY
36'

+69 5' NORWAY
4' x 11"

+68 4' NORWAY
32

+63 2' NORWAY
1'

+80 END Norways (39)
100

+61 Beg Norway
100

+22 OAK 18"
32

+20 OAK 15"
74

+17 ELM 10"
81

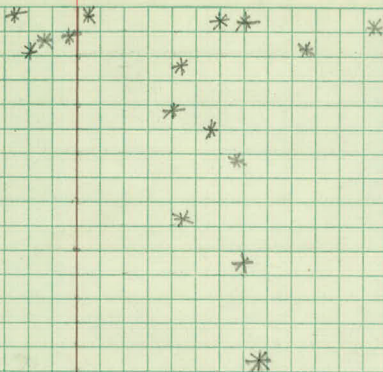
56+00
0+00

+60 END Hazel Brush
0-100'

+02 Beg Hazel Brush
0-100' Rt & Lt

5 MARCH 17, 1961

5



*

* * * * *

34 NORWAYS

* * * *

* * *

Hazel
Brush

Hazel
Brush

61+00

5+00

14

2

12+

+58 $\frac{\text{WOOD AREA}}{73}$

60+00

4+00

+00 $\frac{\text{WOOD AREA}}{93 -}$
Beg Birch & Brush

59+00

3+00

+72 $\frac{\text{JP 8'}}{10}$

+70 $\frac{\text{JP 8'}}{13}$

+67 $\frac{\text{JP 7'}}{18}$

+54 $\frac{\text{JP 6'}}{6'}$

+91 $\frac{\text{3' NOR}}{35}$

+54 $\frac{\text{1' NOR}}{36}$

8 MARCH 17, 1961

6

Wardell
4754

*

*

*

*

Lt

L

Rt

$$+46 \frac{5'' \text{ BIRCH}}{42} +46 \frac{7'' \text{ TWID BIRCH}}{43}$$

$$+48 \frac{4'' \text{ BIRCH}}{41} +25 \frac{\text{QUAD ELM}}{70}$$

$$+25 \frac{\text{E CREEK}}{65} +10 \frac{6'' \text{ ELM}}{77}$$

$$63+00$$

$$+100 \frac{\text{E CREEK}}{71}$$

$$+90 \frac{\text{ENDWOODS}}{23-100+}$$

$$+84 \frac{\text{E CREEK}}{75}$$

$$+61 \frac{\text{Brush}}{8-100}$$

$$+29 \frac{\text{Brush}}{30-100}$$

$$+100 \frac{\text{Brush}}{44-100}$$

$$63+00$$

$$+22$$

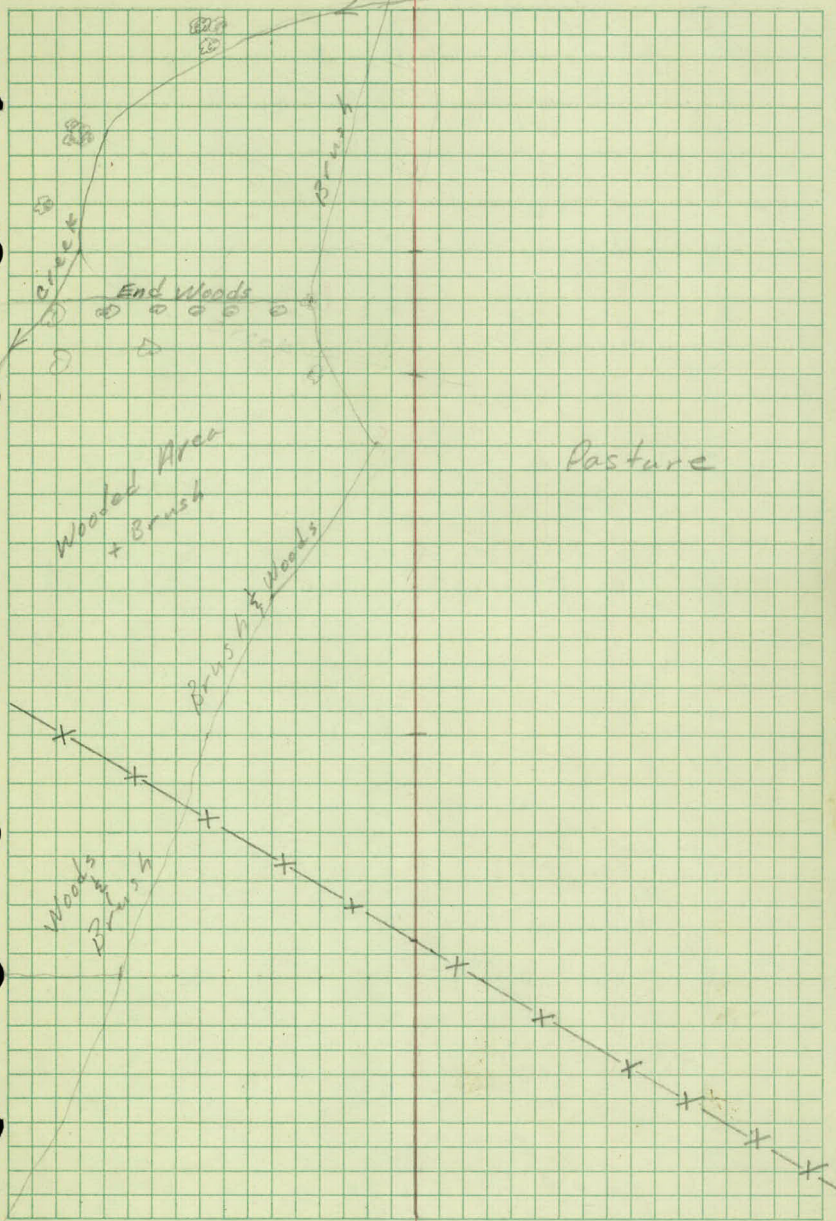
$$+50 \text{ Big Brush} \\ 62-$$

$$+57 \text{ Fence} \\ 0$$

$$61+00 \\ +5+00 +100 \frac{\text{WOOD AREA + BRUSH}}{87}$$

$$+100 \frac{\text{Fence 3rd wire}}{100}$$

7



66+00
10+00

Lt

E

Rt

2" Pine
57

+95

+85 ^{3" Birch}
58

78 ^{4" Birch}
68

+82

(2) 4" Birch
71

+62 ^{(3) 1/6" Willows}
79

End Sumac Brush

+58 50+

65+00

9+00

+00 BRUSH
20-100'

+05 ^{4" Birch}
56

+00 Woods & BRUSH

+00 47-100

+95 ^{Twin Birch}
26

+57 ^{Q CREEK}
54

+80 ^{Q CREEK}
76-120

+57 ^{Beg WOOD AREA & BRUSH}
42-100

+24 ^{Twin ELM}
20

+00 ^{BRUSH}
3-25

+00 ^{Q CREEK}
13

+00 ^{Brush}
0-100

64+00

8+00

+98 ^{8" Twin Birch}
15

+92 ^{10" Quad Willow}
2

+52 ^{Q CREEK}
0

+51 ^{QUAD BRUSH}
10'

7+50

+74 ^{Beg Brush}
4

E MARCH 17, 1961

8

*

Brush

Brush

Brush

Brush

Brush

Stack

creek

Brush

Brush + Woods

Brush + Woods

+50

L+

E

R+

~~68+00~~
~~17+00~~

+25 Sumac Brush
65 - 100 +

+00 Sumac Brush
47

+63 2" Plum Tree
40

+65 Sumac Brush
36

+08 2" Pine
~~67+00~~ 24
~~11+00~~ 2" Pine
+06 26

+35 Sumac Brush
46 +
Reg Sumac Brush
+14 68 - 100 +
+09 2" Pine
9.

+86 1" Pine 21 1" Plum
+89 31

+68 1" Pine
7

+37 2" Plum
9

~~66+00~~
~~10+00~~ +00 2" Pine
54

+00 woods
90 +

RO
JS
IL
WH
FS

Mar 20, 1961

L

9

Brush

Brush

Brush

*

*

*

-

B

*

*

B

*

71+00
15+00

Lt

£ +02 $\frac{Fe}{35}$ Rt

$\frac{Fe}{+58 \frac{1}{2}}$

70+00
14+00

$\frac{Fe}{+00 \frac{1}{2}}$

+23 $\frac{Fe \text{ Cor}}{96}$ +23 $\frac{\text{Twin Oak}}{97}$
+19 $\frac{16" \text{ Oak } \& \text{ Fe}}{62}$

+16 $\frac{Fe (N\&S)}{4}$

+16 $\frac{\text{End Samac's}}{15-95}$

+03
69+00
13+00

$\frac{1" \text{ Plum}}{22}$

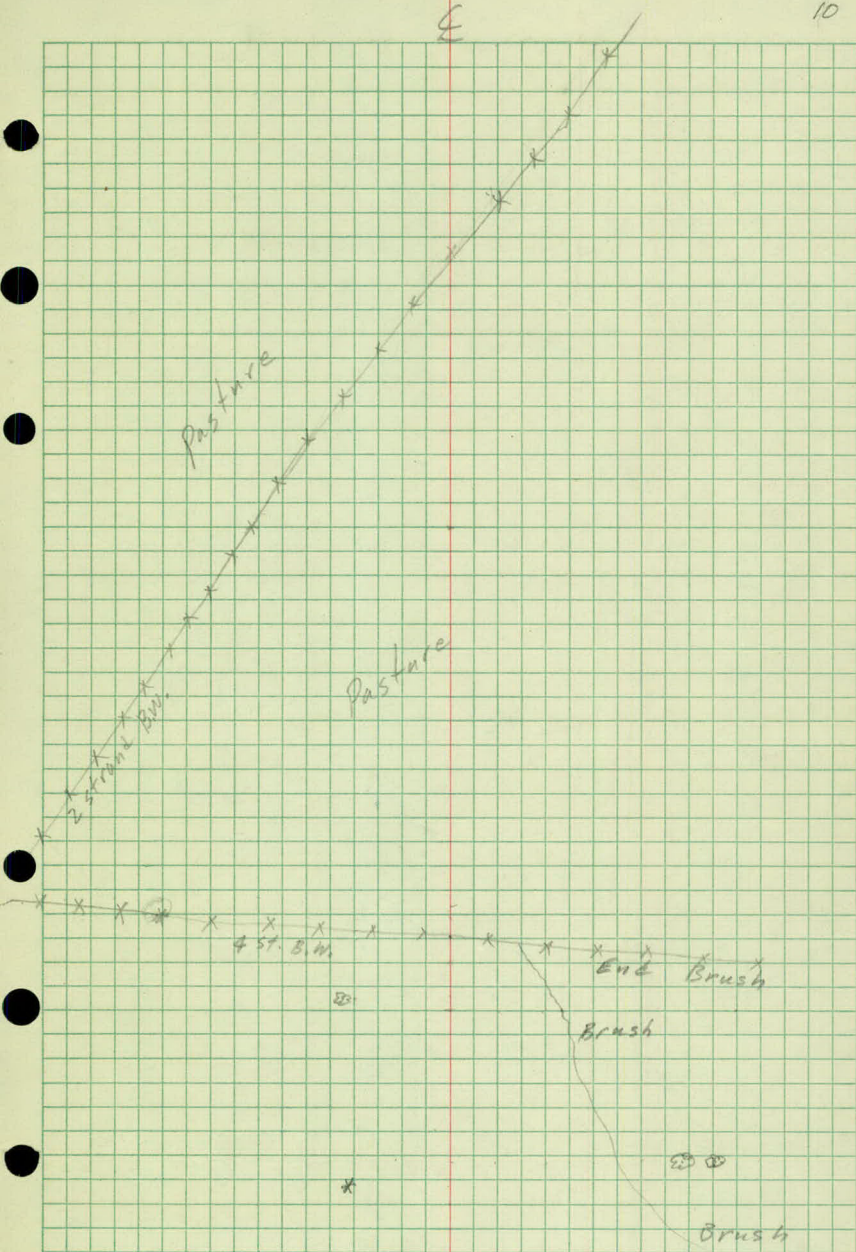
+00 $\frac{\text{Sumac Brush}}{23}$

+63 $\frac{1" \text{ Pine}}{21}$

+69 $\frac{3" \text{ Plum}}{49}$ +69 $\frac{3" \text{ Plum}}{55}$

+50

E



Lt

E

Rt

73+00

~~19+00~~

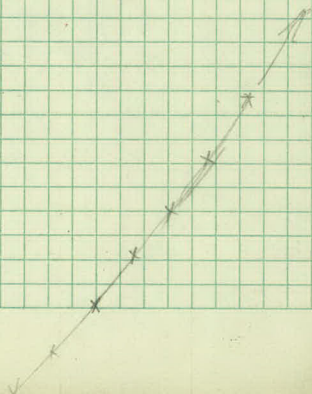
72+00

~~16+00~~+43⁷²PC+44 $\frac{Fc}{67}$

71+00

~~15+00~~+00 $\frac{Fc}{35}$

Posture



~~76+00~~
~~20+00~~

Lt

Q

R+

~~75+00~~
~~19+00~~

+16 $\frac{(3)3^{\circ}8E}{2.9}$

~~74+00~~
~~18+00~~

+07 $\frac{2^{\circ}Cott}{37}$

Pasture

100

Lt

E

Rt

78+00
~~22+00~~

77+00
~~21+00~~

~~76+00~~ + 12 to 68 (10) 6" willows + (14) Cott. 4"-12"
~~20+00~~ 110+125

Pasture

81+00
~~25+00~~

Lt
End Trees
50-71

Q

RT
Fe
45

+00

+00

+50 Trees
35-68
+42 8" Willows 10 42 (3) 8" Willows 15

+25 Beg Trees
65

80+00
~~24+00~~

+00 Fe
81

79+00
~~23+00~~

+50

£

Pasture

Lt

Q

RT

83+00

27+00

$$+88 \text{ Buried gas main } \frac{Fe}{34} +94 \frac{Fe}{2}$$

$$+81 \frac{Fe Cor}{31}$$

$$+00 \frac{24" Oak}{88}$$

$$\text{win } 12" BE$$

$$+76 \frac{14" B.E.}{21}$$

$$+72 \frac{18" BE}{43}$$

$$+61 \frac{18" BE}{22}$$

$$+55 \frac{24" BE}{20}$$

$$+07 \frac{30" Oak}{88}$$

$$\text{NE Cor Barn}$$

$$+86 \frac{18" BE}{81}$$

$$+71 \frac{20" BE}{27}$$

$$+64 \frac{10" BE}{23}$$

$$+59 \frac{20" BE}{15}$$

$$RT = +71$$

$$+76 \frac{20" BE}{30}$$

$$+67 \frac{10" BE}{17}$$

$$+34 \frac{12" F.E.}{3}$$

$$+21.7 \text{ RT}$$

$$+22 \frac{Fe}{2}$$

$$+22 \frac{Beg Fe}{2}$$

$$+00 \frac{Fe}{9}$$

$$+11 \frac{18" E. at}{5} \text{ RT} = +08$$

$$Fe Cor \text{ RT} = 264.00$$

82+00

26+00

$$+80 \frac{(8) 4" Trees}{78-83}$$

$$+65 \frac{\text{clump (5) 4" Trees}}{81-87}$$

$$+45 \frac{\text{clump Brush}}{67}$$

$$+30 \frac{(2) 12" Cott}{66} +35 \frac{12" Cott}{68}$$

81+00

25+00

$$+00 \frac{Fe}{45}$$

March 23, 1961
cloudy 35°

15

KG
JS
JA
WM
FS

L

cultivated

Pipe Line

3 strand B.W.

ENT

3 strand B.W. connects to
H.W. cur. Barn

3 strand
B.W.

17
Barn
50

86+00
~~30+00~~

Lt

E

Rt

85+00
~~29+00~~

84+00
~~28+00~~

+50

cultivated

10

Lt

E

Rt

$$\begin{array}{r} 88+00 \\ 32+00 \end{array}$$

$$400 \frac{Fe}{48}$$

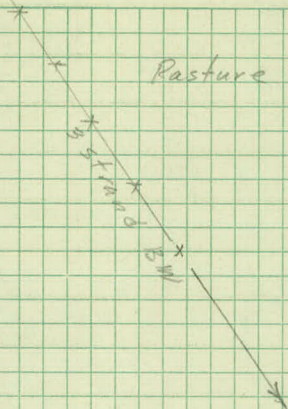
$$\begin{array}{r} 87+00 \\ 31+00 \end{array}$$

$$\begin{array}{r} 86+00 \\ 30+00 \end{array}$$

E

Pasture

Cultivated



91+00

~~35+00~~

2+

Fe

R+

+94 Fe
4

+50 Fe
62

+63 water
4

+28 Fe Cor
104

90+00

~~34+00~~

+00 Fe
87

89+00

~~33+00~~

+00 Fe
14

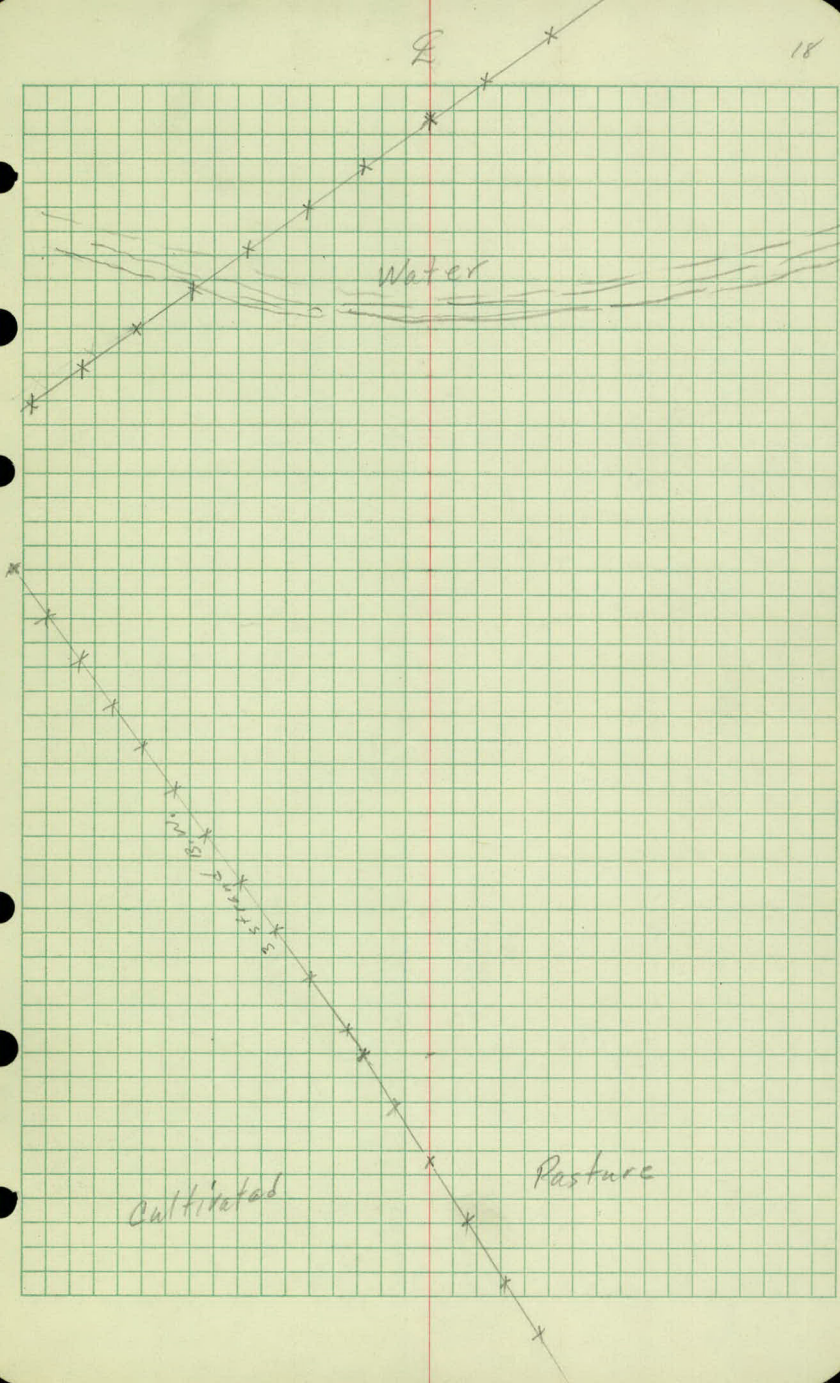
+97 Fe
4

E

Water

Cultivated

Pasture



150

Lt

2

Rt

93+00
~~37~~

92+00
~~36~~

91+00
~~35~~

water

water

96+00
40

Lt

E

Rt

$$\begin{array}{r} +78 \\ \hline \text{pp \frac{1}{2} ent Fe} \\ 24 \end{array}$$

$$\begin{array}{r} +84 \text{ Fe Cor} \\ \hline 27 \end{array}$$

$$\begin{array}{r} +50 \\ \hline \text{Fe} \\ 6 \end{array}$$

$$\begin{array}{r} +41 \text{ Fe} \\ \hline \end{array}$$

$$\begin{array}{r} +41 \text{ Fe} \\ \hline \end{array}$$

$$\begin{array}{r} +30 \text{ Water} \\ \hline \end{array}$$

95+00
34

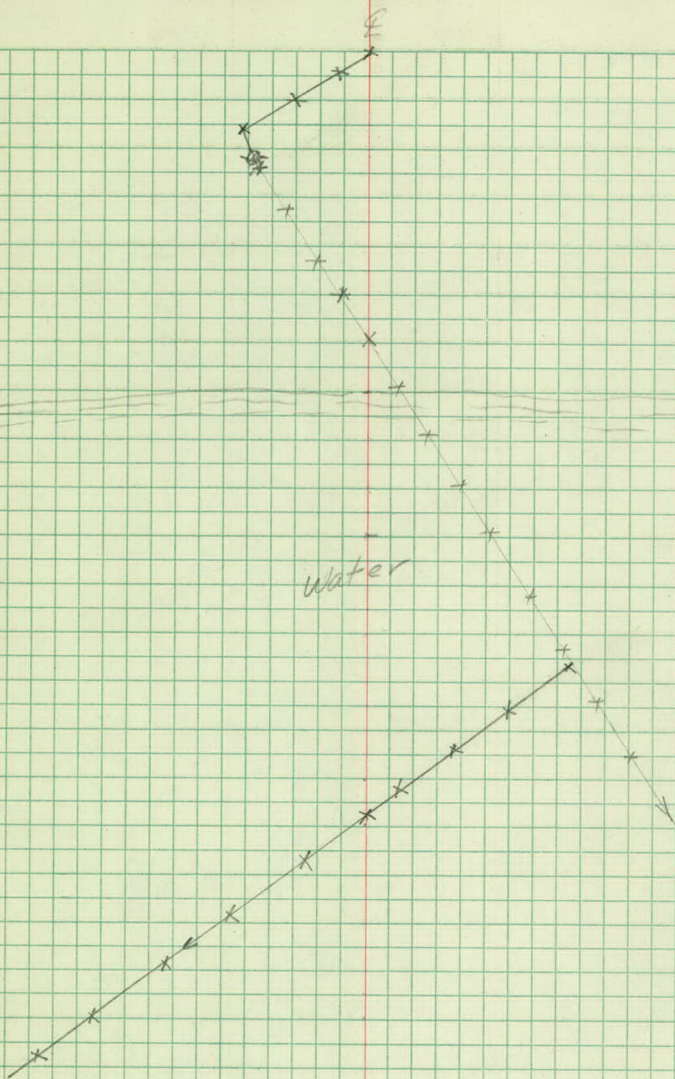
$$\begin{array}{r} +73 \text{ Fe Cor} \\ \hline 42 \end{array}$$

$$\begin{array}{r} +43 \text{ Fe} \\ \hline \end{array}$$

94+00
38

+50

Water



+50

Lt

E

Rt

98+00
42+94 $\frac{IP}{27}$ +100 Fe
21

+100

E Road
62

+100

F.C
8997+00
41+100 Fe
74

+100

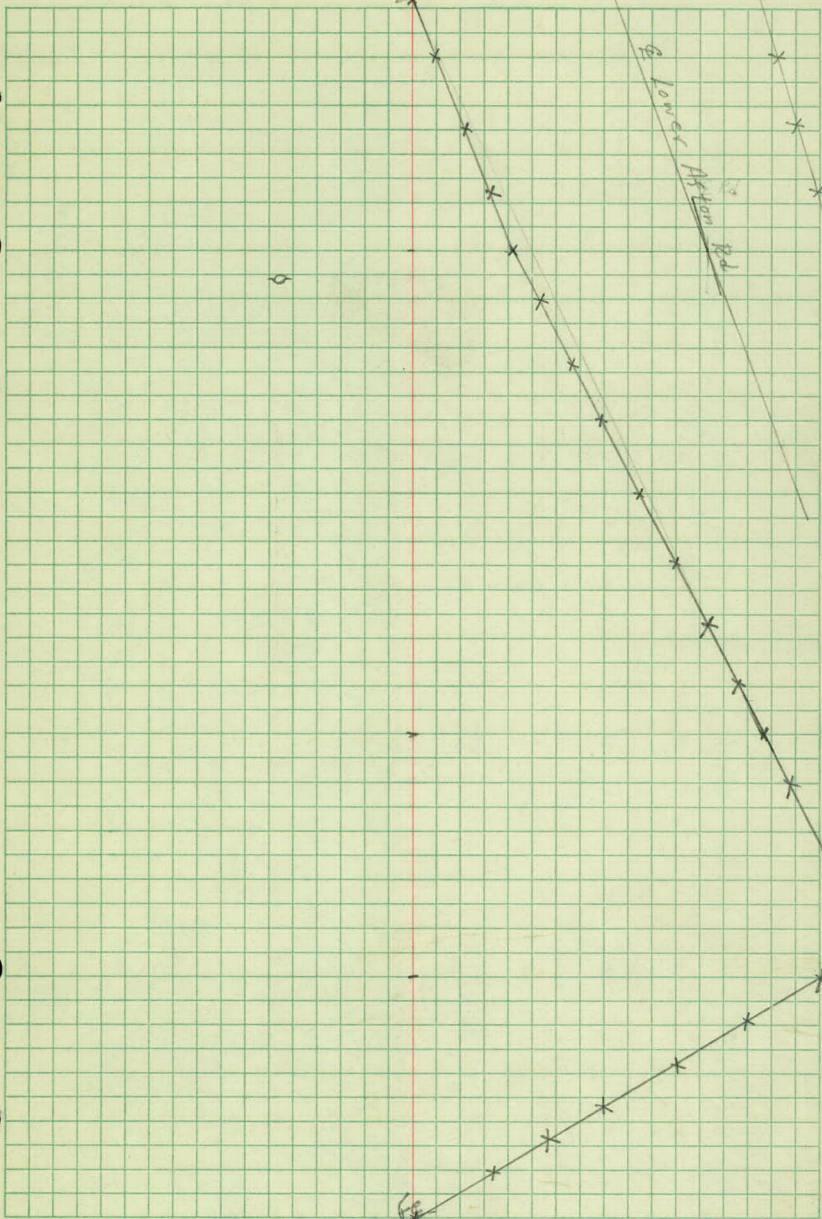
E Lower Aston Rd
113+56 Fe Cor
9796+00
40

Q Lower Astoria Rd.

0

10

10



101+00

48

LT

Q.
11 9

RT

+45 $\frac{1}{2}$ Road

+39 $\frac{TP}{28}$

+05 $\frac{TP}{32}$
100+00
44 +01 $\frac{E. end Culv}{22}$

BT
8 15

+00 $\frac{1}{2}$ Road

+83 RT Fe

+83 Ent RT=44+00

+65 $\frac{30" oak}{47}$ +90 $\frac{Wend 15" \times 32' dm}{19}$

+41 $\frac{12" oak}{26}$

+59 $\frac{Fe Cor}{42}$

99+00

43

+00 $\frac{5' p}{7}$

+00 $\frac{Fe}{19}$

+00 $\frac{1}{2}$ Road
25

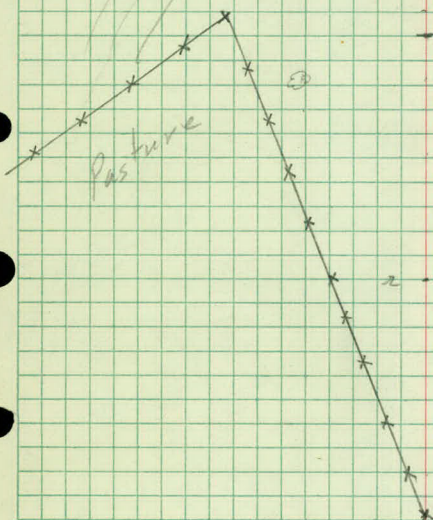
+63 $\frac{Fe Cor}{63}$

+60 $\frac{Fe Cor}{63}$ RT+28

+52 $\frac{Fe}{6}$

E

Cultivated



4 strand

150

Lt

E

Rt

103+00

~~47~~

128

732 $\frac{TP}{33}$

103+00

~~46~~

119

101+00

~~45~~

119

0

cultivated

cultivated

106+00

~~50~~

Lt

2

Rt

+00

$\frac{Fe}{37}$

10 10

105+00

~~49~~

+00

$\frac{Fe}{37}$

11 9

$\frac{TP}{+61 \ 35}$

+61

$\frac{FeCor}{37}$

RT+80

104+00

~~48~~

12 8

450

4 strand B.W.

Cultivated

4 strand B.W.

Cultivated

Lt

E

Rt

$$+41 \cdot \frac{stP}{29}$$

$$+16 \cdot \frac{24" Maple}{29}$$

$$-16 \cdot \frac{Maple}{28}$$

$$+07$$

$$108+00$$

$$52$$

$$+98 \cdot \frac{15" Maple}{29}$$

8 11

$$+83 \cdot \frac{14" Maple}{29}$$

$$+51 \cdot \frac{8" Cott}{28}$$

$$+58 \cdot \frac{20" Elm}{54}$$

$$+30 \cdot \frac{26" oak}{28}$$

$$107+00$$

$$51 +00 \cdot \frac{16" B.E}{27}$$

10 10

$$+85 \cdot \frac{24" Maple}{27}$$

$$+90 \cdot \frac{T.P.}{37}$$

$$+98 \cdot \frac{12" Maple}{23}$$

$$+72 \cdot 10' Ent$$

$$+74 \cdot \frac{stP}{23}$$

$$+65 \cdot \frac{Fc Cor}{38}$$

$$106+00$$

$$50$$

$$+00 \cdot \frac{Fc}{37}$$

10 10

2



Cultivated



← stop 2h



2

4 strand B.W.



114+00

55

Lt

+00

Fe

32

E
11 10

Rt

110+00

54

+00

Fe

33

10 10

109+00

53

Fe Cor

33

Rt +85

10 10

+73

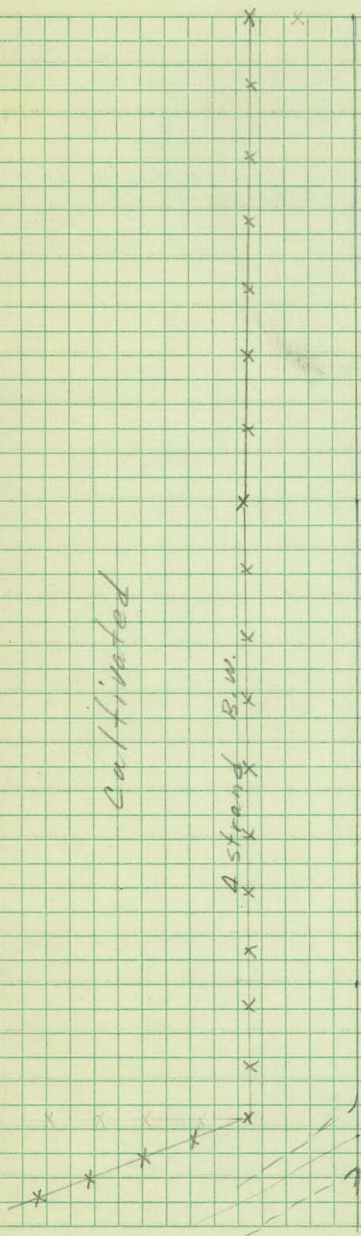
+68 10' Ent Rt +74

+50

cultivated

cultivated

stand B.W.



Lt

E

Rt

+45

$$\frac{POR}{17}$$

$$+28 \quad \frac{E. Rad}{48} \quad RT+50$$

$$+17 \quad \frac{PP}{30} \quad +17 \quad \frac{POR}{32}$$

$$+08 \quad \frac{Fe Post Cor}{38} \quad RT+27$$

$$+20 \quad \frac{Beg Rad}{10}$$

113+00

Beg Rad

57 +00

11

11

112+00

56

9 11

Beg Fe Posts

+51 31

$$+51 \quad \frac{Fe Cor}{31} \quad RT+68$$

111+00

55

$$+00 \quad \frac{Fe}{32}$$

11 10

2

Hwy 100

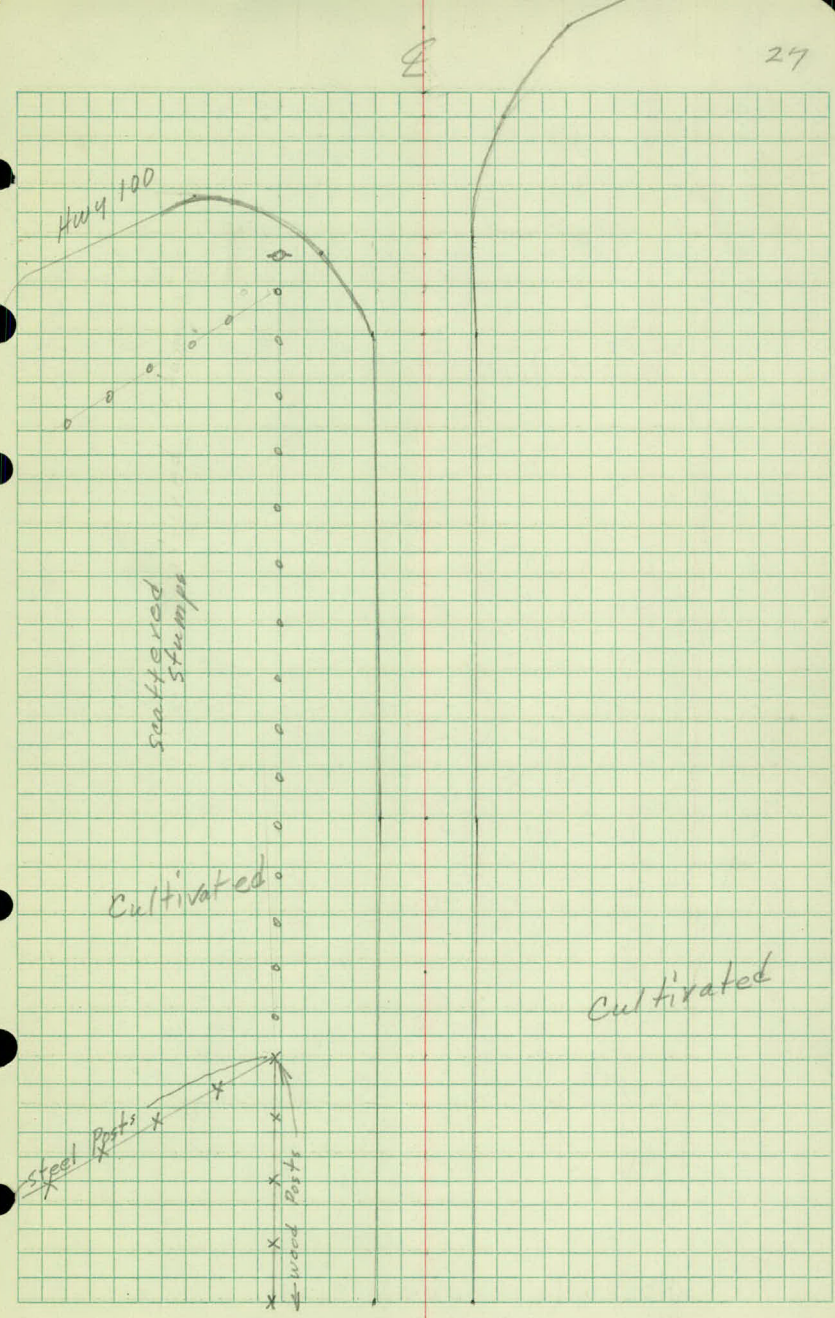
scattered
stumps

Cultivated

Cultivated

steel posts

wood posts



Lt

£

RT

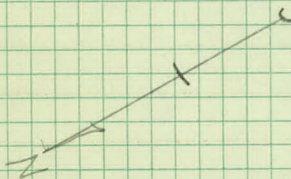
114+00
58

+645 & Hwy 100 +66 ^{E. Rd} 29

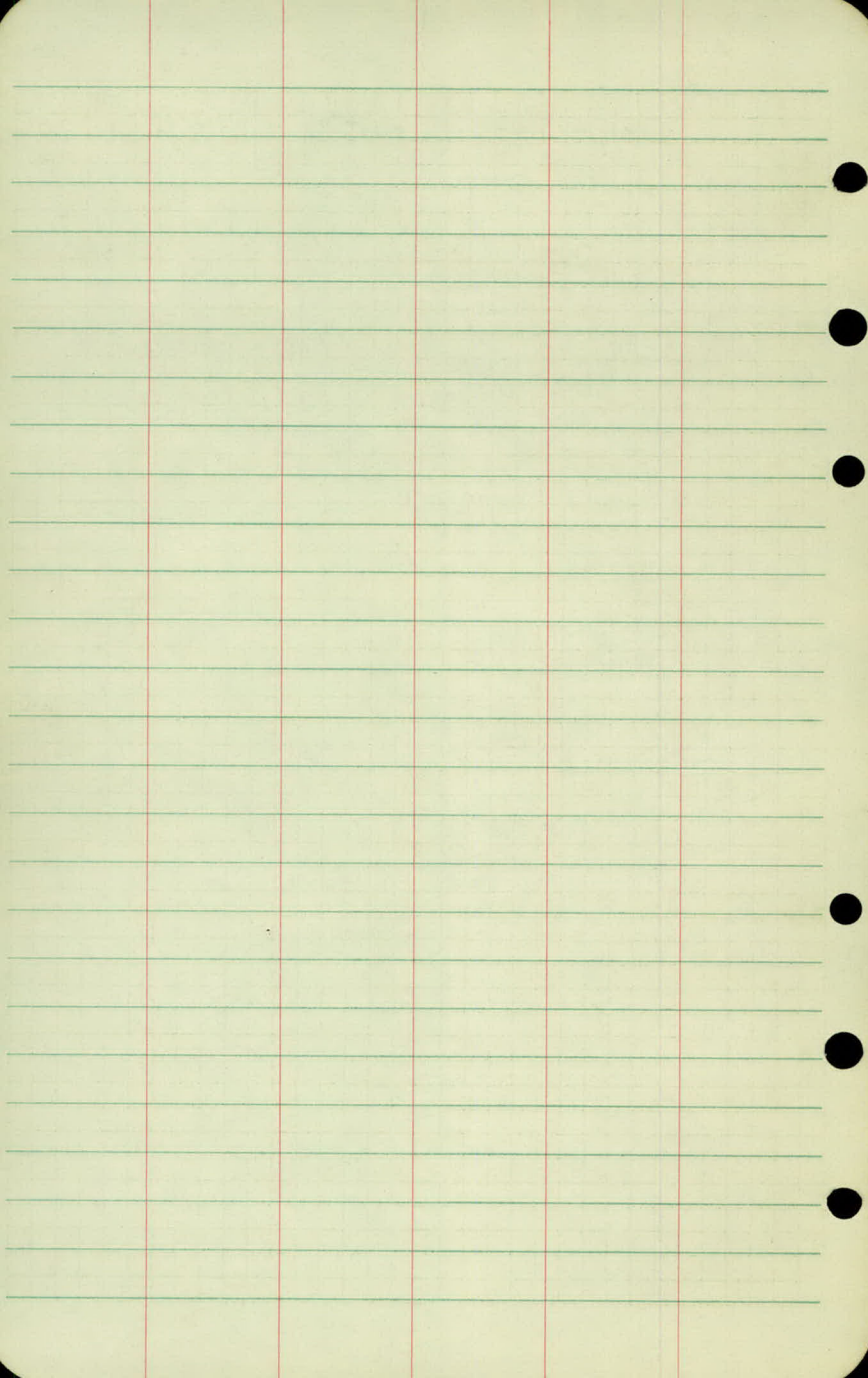
57+50 RT+50 Wedge Hwy 100

March 23, 1961
warm 40° clear 28

£



Hwy 100



RG
JS
JL
WM
FS

April 4, 1961
overcast 35°

29~

Bench Levels

pages 29-31

Sta	+	π	-	E/cr	
BM ₁	13.47	916.41			902.94
TP	12.85	928.78	0.48	915.93	
TP	13.03	941.75	0.06	928.72	
TP	5.78	944.45	3.08	938.67	
BM ₂	1.99	940.64	5.80	938.65	
TP	4.16	932.47	12.33	928.31	
BM ₃	13.11	945.02	0.56	931.91	
TP	13.75	956.94	1.83	943.19	
BM ₄	12.93	967.23	2.64	954.30	
TP	6.97	972.58	1.62	965.61	
BM ₅	9.40	972.96	9.02	963.56	
TP	13.16	984.94	1.18	971.78	
BM ₆	12.97	996.54	1.37	983.57	
TP	8.08	1003.17	1.45	995.09	
BM ₆	8.95	1007.18	4.94	998.23	
BM ₇	13.73	1017.55	3.36	1003.82	
BM ₈	3.19	1019.01	1.73	1015.82	
BM ₉	10.49	1027.56	1.94	1017.07	
BM ₁₀	8.32	1033.97	1.91	1025.65	

Apr. 4, 1961

30

Spike in 18" Oak 60' RT Sta ~~55+88~~ ~~55+12~~

Spike in ground

" " "

rock

Spike in 10" Elm 74' LT Sta ~~61+50~~ ~~5+50~~

Spike in ground

rock

top lge. boulder 15' LT Sta ~~68+75~~ ~~13+75~~ 9

Spike in Quad Oak 100' LT Sta ~~69+25~~ ~~13+25~~

rock

Spike in 10" Cotton 100' LT Sta ~~76+12~~ ~~20+12~~

rock

Spike in 24" Oak 88' RT Sta ~~83+07~~ ~~27+07~~

rock

Gray Barn on Lower Attonk

Bent Spike in root of 20" Oak 33' East of Culvert by

Spike in PP 21' LT Sta ~~95+80~~ ~~39+80~~

Spike in 30" Oak 47' LT Sta ~~99+65~~ ~~43+65~~

Spike in PP LT Sta ~~102+35~~ ~~46+35~~

iron in Stamp 24' RT Sta ~~106+74~~ ~~50+74~~

Sta	+	π	-	Elev	
		1033.97			
TP	6.07	1038.20	1.84	1032.13	
BM			2.31	1035.89	
BM ₁₁			1.98	1036.22	
BM			2.01	1036.19	(1036.20)
BM ₁₁	1.28	1037.50			1036.22
BM ₁₀	3.74	1029.35	11.89	1025.61	1025.65
BM ₈			13.59	1015.76	1015.82

see Bench Level re-run Pages 73-76

Apr. 4, 1961

31

110+00

nail $\in$ Sta 54+00

Double spike in PP NW cor Hwy 100 $\frac{1}{2}$ Lower Afton

yellow painted spike " " " " "

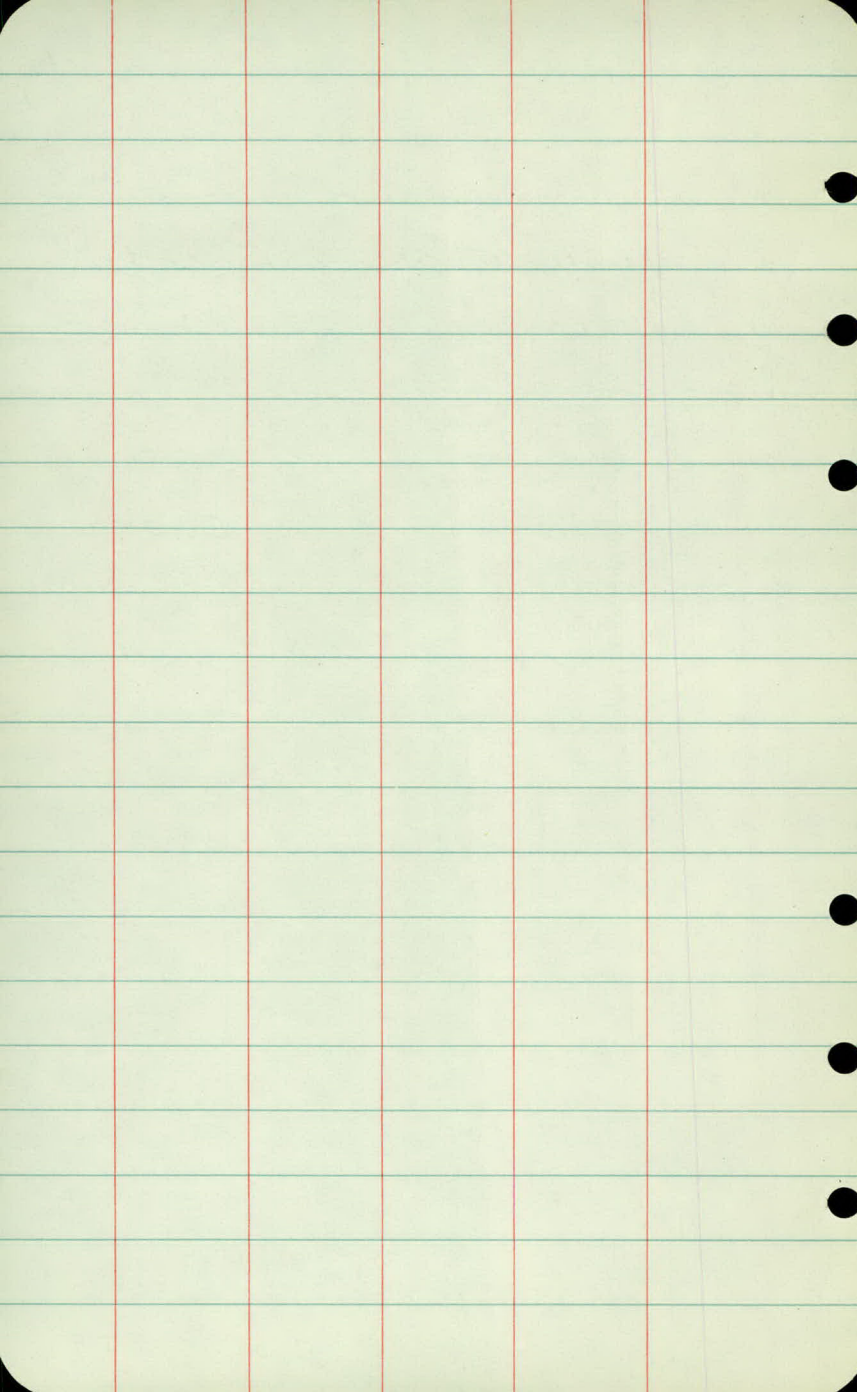
spike with red flagging " " " " "

106+74

iron in stump 24' Rt Sta 50+74

99+65

Spike in 30" oak 47' Lt Sta 43+65



Lower Aften Rd Line 3

X-Sections

McKnight Rd (0+00) to Hwy 100 (57+6454)

pages 32-69

sta	+	π	-	E/cv
-----	---	-------	---	------

BM	12.97	915.91		902.94
----	-------	--------	--	--------

56+00

~~0+00~~

+30

T.P	12.63	924.87	0.67	915.24
-----	-------	--------	------	--------

+57

T.P	13.12	940.44	0.55	927.32
-----	-------	--------	------	--------

57+00

~~+100~~

+30

RG
JS
JL
WM

Lt

L

24 March 1961
Clear

32

Spike in 18" oak 60' Rt Sta. 0-12

903.6	903.8	903.9	903.7	905.8	904.1	904.1	905.0	905.6
12.4	12.1	12.0	12.2	12.1	11.8	11.8	10.9	10.3
100	70	42	21		20	47	76	100

910.3	911.4	911.3	911.7	911.9	911.9	911.8	911.6
5.6	4.5	4.6	4.2	4.0	4.0	4.1	4.3
100	68	37	16		30	63	100

Spike in ground

917.6	919.4	920.6	921.8	921.3	920.5	918.5	918.4
10.3	8.5	7.3	6.1	6.6	7.4	9.4	9.5
100	54	22		31	58	80	100

Spike in ground

928.0	928.8	929.8	931.0	930.6	929.7	929.2
12.4	11.6	10.6	9.4	9.8	10.7	12.2
100	63	37		30	63	100

933.1	933.2	935.1	936.5	936.6	935.5	934.2
7.3	7.2	5.3	3.9	3.8	4.9	6.2
100	73	36		30	62	100

Sta	+	π	-	ELEV
-----	---	-------	---	------

		940.44		
--	--	--------	--	--

+50				
-----	--	--	--	--

+74				
-----	--	--	--	--

T.P.	4.11	9440.5	0.50	939.94
------	------	--------	------	--------

58+00				
-------	--	--	--	--

2+00				
-----------------	--	--	--	--

+37				
-----	--	--	--	--

+66				
-----	--	--	--	--

RG
J5
J2
W19

26 MARCH 1961
CIRAV 34

Lt

£

Rt

35.0	35.0	36.4	37.8	39.0	39.6	39.1	37.3
5.4	5.4	4.0	2.6	1.4	0.8	1.3	3.1
100	83	54	28		27	65	100

✓

35.4	35.9	37.5	39.8	40.1	40.9	40.2	40.4
5.0	4.5	2.9	0.6	0.3	10.5	0.2	0.0
100	60	31		25	41	92	100

Spike in ground

✓

33.1	32.1	33.6	37.1	39.5	40.6	41.7	41.0	39.7
11.0	12.1	10.5	7.0	4.6	3.5	2.4	3.1	4.4
100	74	50	22		16	48	73	100

✓

25.4	26.1	30.6	30.6	39.0	41.1	42.5	40.5	30.6
18.7	18.0	13.5	7.5	5.1	3.0	1.6	3.6	7.5
100	71	41	14		17	41	71	100

✓

23.4	24.3	26.6	32.0	35.3	37.4	38.8	39.4	30.6
20.7	19.8	17.5	12.1	8.8	6.4	5.3	6.2	7.6
100	80	44	17		23	50	83	100

✓

Sta + π - ELEV

944.05

59+00

~~3+00~~

+50

+75

60+00

~~4+00~~

+50

61+00

~~5+00~~

B.M.

5.41 938.64

938.64

RG
JS
JL
W17

Lt

E

Rt

24 March 1961
Clear 35

26.8	25.3	26.4	29.1	31.8	35.5	36.3	36.1
17.3	18.8	17.7	15.0	12.3	8.6	7.8	7.4
100	65	26		22	52	80	100

✓

33.5	35.4	34.4	33.5	33.0	34.0	35.4	37.0
10.6	8.7	9.2	10.6	11.1	10.1	8.7	7.1
100	95	66	33		29	61	100

✓

30.9	37.6	37.9	37.4	37.3	37.1	37.1	37.8	38.1
13.2	6.5	6.2	6.7	6.8	7.0	7.0	6.3	6.0
100	87	57	27		29	58	93	100

✓

28.6	32.0	34.2	34.4	39.5	39.1	38.6	38.5	39.1
15.5	12.1	4.9	4.7	4.6	5.0	5.5	5.6	5.0
100	95	73	52	31		30	29	100

✓

22.8	29.0	36.3	40.4	40.7	40.4	39.9	39.6	39.2	39.6	40.2
21.3	15.1	7.8	3.7	3.4	3.7	4.2	4.5	4.9	4.5	3.9
100	87	70	54	47	23		29	53	88	100

✓

27.6	32.0	36.9	40.7	40.0	39.6	38.9	38.6	38.0	39.1	39.3
16.5	12.1	7.9	3.4	4.1	4.5	5.2	5.5	6.1	5.0	4.8
100	90	79	64	47	22		20	51	89	100

~ SPIKE IN 10" ELM 74' STA 5+50±

✓ Lt

Sta	+	π	-	ELEV
BM	2.35	940.99		938.64 (938.64)

61+50

~~5+50~~

+70

62+00

~~6+00~~

TP	0.67	928.24	13.42	927.57
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+35

+60

63+00

~~7+00~~

21.2 18.5
7.0 9.7
118 108
Top
Bank

RG
JS
JL
FS
WM

Lt

E

March 28, 1961
Cool, Windy, R2. 34
Rt

Spike in 10" Elm 74' Lt. Sta 5+50 ±

30.9	35.2	37.4	39.1	39.6	39.6	38.6	36.1	34.1	32.2	32.9	29.2
10.1	5.8	3.6	1.3	1.4	1.4	2.4	4.3	6.9	8.8	8.1	11.8
100	83	73	60	29		18	41	57	65	71	100

✓

27.1	29.2	33.1	36.5	38.2	31.4	38.4	38.5	36.5	32.4	29.2	27.5	27.5	25.5
13.9	11.8	7.9	4.5	2.8	3.6	2.6	2.5	4.5	8.6	11.8	13.5	13.5	15.
100	91	80	65	57	44	26		23	48	66	74	80	100

✓

26.5	26.0	30.3	31.3	31.5	31.8	28.7	25.2	21.1
18.5	15.0	10.7	9.7	9.5	9.2	12.3	15.8	19.9
100	83	63	45	25		28	62	100

✓

Spike in ground

15.3	18.1	21.6	23.6	24.2	22.6	21.5	19.7	18.8
12.9	9.5	6.6	4.6	4.0	5.6	6.7	8.5	9.4
100	80	53	24		34	52	74	100

✓

10.0	13.1	16.3	18.0	20.1	19.9	19.6	19.8	18.6	18.2	18.2
18.2	15.1	11.9	10.2	8.1	8.3	8.6	8.4	9.6	10.0	10.0
96	80	69	48	31	21		31	60	82	100

✓

Top edge creek
bank

12.6	10.8	11.6	12.5	14.4	15.3	15.1	15.9	16.5	17.3	19.2	20.6
15.7	17.4	20.6	15.7	13.8	12.9	13.1	12.3	11.7	10.9	9.0	7.6
100	96	79-88	68	41	18		22	42	63	86	100

✓

Creek Top
Bank

Sta	+	π	-	Elev
-----	---	-------	---	------

		928.24		
--	--	--------	--	--

+42	Top Bank			
-----	----------	--	--	--

✓				
---	--	--	--	--

+54				
-----	--	--	--	--

+86				
-----	--	--	--	--

✓				
---	--	--	--	--

64+00				
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81+00				
------------------	--	--	--	--

March 28, 1961

LT

E

RT

57

22.6	18.5	16.0	11.3	11.9	12.1	13.5	14.9	17.2	20.2	23.0
5.7	9.7	12.2	16.9	20.3	15.5	14.7	13.3	11.0	8.0	5.2
78	70	63	47	40	26		11	34	64	100

creek



24.1
3.5
100

28.0	25.0	22.2	17.2	15.6	11.1	10.1	9.6	11.3	13.8	16.1	19.4	22.4	24.5
0.2	3.2	6.0	11.0	12.6	16.5	17.5	18.6	16.9	14.4	12.1	8.8	5.8	3.7
100	85	62	50	40	25	5	creek	7	11	23	55	83	100



28.2	23.0	20.8	17.9	14.9	12.2	11.8	9.8	12.0	14.6	18.3	20.0	22.1
0.0	5.2	7.4	10.3	13.3	16.0	16.4	18.4	16.2	13.6	9.9	8.2	5.5
79	56	33	22	16	5		17	19	21	50	67	85

creek

top
Bank



33.3
+ 5.1
100

24.2
4.0
100

34.1	28.2	22.1	20.6	16.0	15.0	13.1	11.1	12.1	14.8	16.6
76.5	0.0	5.5	7.6	12.2	13.2	15.1	17.1	16.1	13.4	11.6
100	71	47	24	6		8	9-13	15	31	46

creek



23.1	22.4	19.3
5.1	5.8	8.9
100	91	69

Sta + π - ELEV

928.24

+50

✓

TP 12.29 940.05 0.48 927.76

65+00

9400

✓

+50

✓

March 28, 1961

LT

±

RT

38

34.2	28.2	26.0	23.3	22.0	20.6	17.4	14.9	15.9	15.5
+6.0	0.0	2.2	4.9	6.2	7.6	10.8	13.3	12.3	12.7
68	46	36	29	11		13	26	44	51

✓

38.6	41.2	42.8
+10.4	+13.0	+14.6
81	92	100

17.8	17.0	15.2	12.7
10.4	11.2	13.0	15.5
100	78	60	52-55

Creek

spike in ground $9+13 \pm 4$

50.4	43.0	34.1	33.1	28.6	25.4	23.2	22.4	19.4	18.1
+10.8	+2.9	1.0	6.4	11.5	14.7	16.9	17.7	20.7	22.0
93	70	55	35	16		16	31	48	69

✓

17.6
22.6
100

58.8	51.1	40.1	36.0	34.4	30.9	28.9	27.2	24.9
+18.7	+11.0	0.0	4.1	5.7	9.2	11.2	12.9	15.2
100	73	23	7		15	24	36	56

✓

18.8	19.7	21.5
21.3	20.4	18.6
100	82	68

Sta	+	K	-	ELEV
-----	---	--------------	---	------

		940.05		
--	--	--------	--	--

66+00 10+00				
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+50				
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✓				
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67+00 11+00				
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✓				
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TP	11.82	950.65	1.22	938.83
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+50				
-----	--	--	--	--

RG
JS
JL
W.M

Lt

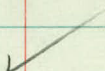
E

March 28, 1961
P. Cloudy
TS 39

61.8	59.0	52.1	46.7	44.1	38.8	33.3	26.6	25.1	22.9	20.6
+ 21.7	+ 18.9	+ 12.0	+ 8.6	+ 4.0	1.3	6.8	13.5	15.0	17.2	19.5
100	73	40	24		20	35	61	74	82	100



61.5	60.5	57.1	52.1	46.5	43.2	39.1	36.9	33.3	29.9	26.1
+ 21.4	+ 20.4	+ 17.0	+ 12.0	+ 6.4	+ 3.1	1.0	3.2	6.8	10.2	14.0
100	84	57	30		16	31	41	51	64	93



23.7
16.4
100

56.6	57.1	56.2	52.1	49.2	45.3	41.2	39.2	34.3	30.2
+ 16.5	+ 17.0	+ 16.1	+ 12.0	+ 9.1	+ 5.2	+ 1.1	0.9	5.8	9.9
100	76	66	25		22	42	50	59	72



25.5
26.1
14.6
100
91

Rock

51.5	52.0	50.7	48.7	46.2	43.8	41.2	38.1	29.5	26.4
+ 0.8	+ 1.3	0.0	2.0	4.5	6.9	9.5	12.6	21.2	24.0
100	64	36	21		18	35	50	77	100



Sta	+	π	-	ELEV
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68+00		950.65		
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12+00				
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+50				
-----	--	--	--	--

✓				
---	--	--	--	--

69+00				
-------	--	--	--	--

13+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+25				
-----	--	--	--	--

453				
-----	--	--	--	--

RG
JS
JL
WM
FS

28 May 1961
Dct 600/170
RT

	LT												
51.2	50.7	49.5	48.5	47.1	44.9	43.4	39.5	36.3	30.2	27.8	26		
+0.5	0.0	1.2	2.2	3.6	5.8	7.3	11.2	14.4	20.5	22.9	24		
100	98	63	41	19		12	31	48	69	84	100		

48.2	48.3	48.3	48.2	45.7	43.0	40.6	38.9	35.1	30.2	28.3			
2.5	2.4	2.4	2.5	5.0	7.7	10.1	11.8	15.6	20.5	22.4			
108	90	64	36	14		15	25	39	61	85			

25.3

25.4
100

50.3	48.1	47.1	43.2	40.6	39.1	35.6	33.9	29.0	27.1				
0.4	2.6	3.6	7.5	10.1	11.6	15.1	16.8	21.7	23.6				
100	63	40	15		7	18	31	59	85				

25.9

24.8
100

50.7	49.5	47.9	43.7	38.4	35.3	32.2	29.4	27.1					
0.0	1.2	2.8	7.0	12.3	15.4	18.5	21.3	23.6					
100	74	48	23		15	44	81	100					

Sta + π - ELEV

950.65

~~69+53~~

~~13+53~~

+ 64

~~70+00~~

~~14+00~~

T.P 13.06 956.27 7.44 943.21

T.B.M. 1.93 954.34 (954.30)

+ 30

+ 59

T.B.M. 13.29 967.59 1.93 954.30 (954.30)

RG
JS
JL
WM
FS

Lt

L

28 March 1961
P. Cloudy
Rt 41

49.9	49.3	46.2	47.0	44.9	40.2	37.3	33.9	32.0	28.2
0.8	1.4	2.5	3.7	5.8	10.5	13.4	16.8	18.7	22.5
100	83	76	61	55	27		31	58	100

Fe line ✓

50.1	49.1	48.3	46.1	41.8	38.4	34.7	32.0	29.9	28.5
0.6	1.6	2.4	4.6	8.9	12.3	16.0	18.7	20.8	22.2
100	73	64	45	19		30	66	93	100

Fe line ✓

51.0	49.9	50.7	49.5	47.7	44.4	40.4	35.6	32.4	31.0
±0.3	0.8	0.0	1.2	3.0	6.3	10.3	15.1	18.3	19.7
100	71	41	36	19		22	53	88	100

Fe line ✓

Top large Rock 15' Lt of Sta 13+75±

Top Spike in Quad oak 100' Lt of Sta 13+25

51.4	50.4	51.6	52.5	52.5	51.6	51.6	50.8	48.1	45.2	38.4	35.1
4.9	5.9	4.7	3.8	3.8	4.7	4.7	5.5	8.2	13.1	17.9	21.2
100	69	39	27	23	19	12		19	42	70	100

Fe line ✓

53.0	53.0	53.9	55.4	56.8	55.9	55.2	54.2	51.5	38.6
3.3	3.3	2.4	0.9	±0.5	0.4	1.1	7.1	14.8	17.7
100	72	42	10		4	13	45	81	100

Top spike in Quad oak 100' Lt of Sta 13+25

✓

Sta	+	π	-	ELEV
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		967.59		
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70+85				
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14+85				
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✓				
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71+00				
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15+00				
------------------	--	--	--	--

✓				
---	--	--	--	--

+44				
-----	--	--	--	--

✓				
---	--	--	--	--

RG
JS
JL
WNY
FS

Lt

2

Rt

42

52.6	54.1	56.7	58.1	59.6	60.1	58.9	54.6	52.9
15.0	13.5	10.9	8.9	8.0	7.5	8.2	13.0	14.7
100	59	24		13	23	29	59	69

✓

44.4	48.5
23.2	19.1
100	86

52.2	53.5	56.1	59.9	61.1	62.2	61.6	60.4	56.8
15.4	14.1	11.5	7.7	6.5	5.4	6.5	7.2	10.8
100	69	34		15	35	39	47	67

Feline

✓

49.7	52.9
17.9	14.7
100	90

52.6	54.2	56.0	58.0	63.0	65.5	66.4	66.1	63.8
15.0	13.4	11.6	9.6	4.6	2.1	1.2	1.5	3.8
100	73	47	25		16	38	70	78

2

60.0	61.7
7.6	5.9
100	91

Sta + π - ELEV

967.59

+61

~~72+00~~

~~16+00~~

TP 13.76 979.92 1.43 966.16

+17

+50

~~73+00~~

~~17+00~~

+50

RG
JS
JL
WMI
FS

24 March 1961
cool, clear 4/3
RT

LT

Σ

52.0	54.8	54.0	54.2	63.5	66.3	67.6	67.7	66.3	63.2	61.5
14.8	12.8	10.6	8.4	4.1	1.3	0.0	+0.1	1.3	4.4	6.1
100	74	46	21		16	34	51	79	90	100

✓

57.3	60.3	62.3	63.7	64.6	67.6	70.1	70.9	69.1	67.2
10.3	7.3	5.3	3.9	3.0	0.0	+2.5	+3.3	+1.5	0.4
100	81	50	20		18	41	52	81	100

✓

spike in ground

54.2	60.6	62.4	64.3	65.6	66.8	68.3	70.0	70.9	69.5	66.7
20.7	19.3	17.0	15.6	14.3	13.1	11.6	9.9	9.0	10.4	13.2
100	90	72	51	31		18	36	60	80	100

✓

62.6	63.5	65.0	66.6	67.4	68.3	69.1	70.9	71.8	70.6	68.4
17.3	16.4	14.9	13.3	12.5	11.6	10.8	9.0	8.1	9.3	11.5
100	86	63	46	22		15	38	62	84	100

✓

65.7	66.4	67.0	68.8	69.9	70.9	71.9	73.2	74.2	73.9	73.0
14.2	13.5	12.9	11.1	10.0	9.0	8.0	6.7	5.7	6.0	6.9
100	88	68	44	21		20	43	69	93	100

✓

64.9	65.7	67.7	70.4	72.0	73.7	74.4	75.5	76.5	76.3	75.6
15.0	14.2	12.2	9.5	7.9	6.2	5.5	4.4	3.4	3.6	4.3
100	90	65	44	26		18	41	66	88	100

✓

St + π - ELEV

979.92

~~74+00~~

~~18+00~~

+50

TP 12.50 981.18 11.24 968.68

+83

~~75+00~~

~~19+00~~

+30

+50

March 29, 1961

Clear

Lt

E

Rt

44

65.2	66.1	69.3	72.9	74.3	75.8	77.0	78.3	79.2	79.0	78.3
14.7	13.8	10.6	7.0	5.6	4.1	2.9	1.6	0.7	0.9	1.6
100	91	66	40	23		22	45	71	92	100



64.7	67.4	70.9	74.2	74.8	76.3	78.0	79.9	81.1	81.1	81.0
15.2	12.5	9.0	5.7	5.1	3.6	1.9	0.0	+1.2	+1.8	+1.1
100	83	63	39	24		21	45	71	89	100



Rock

64.3	67.8	70.2	72.2	73.5	75.4	77.6	79.0	79.9	80.5	81.0	80.9
16.9	13.4	11.0	9.0	7.7	5.8	3.6	2.2	1.3	0.7	0.2	0.3
100	79	63	47	25		22	37	56	72	87	100



63.8	66.9	68.9	70.1	71.7	72.6	74.1	77.3	78.8	79.7	80.4	80.5
17.4	14.3	12.3	11.1	9.5	8.6	7.1	3.9	2.4	1.5	0.8	0.7
100	75	60	47	30	12		27	48	66	85	100



62.5	64.4	65.4	66.9	68.5	72.1	74.4	76.9	78.3	79.1	79.3
18.7	16.8	15.8	14.3	12.7	9.1	6.8	4.3	2.9	2.1	1.9
100	77	58	36	19		17	40	63	88	100



62.6	63.5	63.5	65.4	67.2	70.7	73.2	75.5	77.2	78.0	78.1
18.6	17.7	17.7	15.8	14.0	10.5	8.0	5.7	4.0	3.2	3.1
100	82	71	44	24		18	38	59	79	100



Sta	+	π	-	ELEV
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981.18

76+00

~~20+00~~

+50

77+00

~~21+00~~

+50

T.P.	1.35	972.61	9.92	971.26
------	------	--------	------	--------

B.M.			8.98	963.63	963.58
------	--	--	------	--------	--------

B.M.	8.98	972.56			963.58
------	------	--------	--	--	--------

78+00

~~22+00~~

LT

E

RT

45

61.5	62.1	63.6	64.5	66.5	68.6	71.5	75.5	75.2	74.5	74.6
19.7	19.1	17.6	15.7	14.7	12.6	9.7	7.5	6.0	6.7	6.6
100	84	54	40	19		25	50	77	91	100



61.4	61.8	63.1	63.7	64.8	66.6	67.1	69.2	71.1	72.4	71.3	70.6
19.8	19.4	18.1	17.5	16.4	14.6	14.1	12.0	10.1	8.8	9.9	10.6
100	88	71	56	28	10		32	42	65	85	100



61.0	63.0	63.6	65.2	67.4	68.3	70.1	71.5	71.9	70.0	69.6
20.2	18.2	17.6	16.0	13.8	12.9	11.1	9.7	9.3	11.2	11.7
100	99	60	38	16		23	43	65	90	100



63.0	63.8	64.8	66.2	68.1	69.2	69.2	70.2	71.2	70.1	68.8
18.2	17.4	16.4	15.0	13.1	12.0	12.0	11.0	10.0	11.1	12.0
100	88	60	43	19		20	39	62	86	100



Rock

spike in 10"cott 100' LT sta 20+12

66.0	66.2	67.2	67.6	67.3	67.7	67.0	67.9	68.1	68.9	67.3	66.9
6.6	6.4	5.4	5.0	5.3	5.4	5.6	4.7	3.9	4.3	5.3	5.7
100	84	61	41	21		11	31	52	74	95	100



Sta + π - ELEV

972.56

78+50

~~22+50~~

79+00

~~23+00~~

79+20

~~23+20~~

Ditch

✓

79+36

~~23+36~~

✓

+50

	LT							RT		46
67.0	68.0	67.8	67.3	66.2	65.7	65.6	65.9	65.7	64.1	63.3
5.6	4.6	4.8	5.3	6.4	6.9	7.0	6.7	6.9	8.2	9.3
100	71	46	25	12		25	47	64	83	100

	69.2	69.5	68.5	66.8	65.9	64.4	63.6	63.0	61.9	60.1	59.0
	3.4	3.1	4.1	5.8	7.3	8.2	9.0	9.6	10.7	12.5	13.6
	100	96	69	41	21		18	42	66	89	100

	68.9	68.1	65.9	64.7	64.2	63.7	63.3	61.7	59.4	58.9	58.5
	3.7	4.5	6.7	7.9	8.4	8.9	9.3	10.9	13.2	13.7	14.1
	100	84	57	35	16		20	47	50	63	68

	68.6	67.6	66.6	65.0	64.6	64.2	63.3	63.4	61.4	60.8	63.0	63.1
	4.0	5.0	6.0	7.6	8.0	8.4	9.3	9.7	11.2	11.8	9.6	9.5
	100	82	60	34	17		18	31	32	39	39	48

	68.0	60.3	62.2	62.2
	14.6	12.3	10.4	10.4
	100	87	69	59

	68.5	66.9	65.1	64.9	64.5	64.0	63.7	63.5	61.4	60.3	59.4
	4.1	5.7	7.5	7.7	8.1	8.6	8.9	9.1	11.2	12.3	13.2
	100	80	55	30		25	47	69	8.9	93	100

Sta	+	π	-	Elev
-----	---	-------	---	------

		972.56		
--	--	--------	--	--

80+00				
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24+00				
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✓

+50				
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✓

T.P.	13.24	982.31	3.49	969.07
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81+00				
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25+00				
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Lx

z

Et

44

67.3	66.8	66.5	66.5	65.4	64.8	65.2	65.8	64.8	65.6	67.2
5.3	5.8	6.1	7.1	7.2	7.8	7.4	6.8	6.8	7.0	7.4
100	85	59	25		22	38	47	60	80	91



66.1
8.1
100

67.1	67.5	66.5	66.4	66.9	66.4	66.8	69.2	11.3	11.2	11.3	69.7
4.9	5.1	6.1	6.2	5.7	6.2	5.8	3.4	1.3	1.4	1.3	2.9
100	91	69	49	22		18	40	60	67	78	92



Se

64.0
3.6
100

Rock

69.0	68.7	68.1	67.3	67.9	68.5	69.1	10.9	12.9	13.5
13.3	13.6	14.2	15.0	14.4	13.8	13.2	11.4	9.5	8.8
100	95	52	29		7	20	39	48	55



14.0	14.6	15.3	14.1
8.3	7.7	7.0	7.6
100	91	73	60

Sta + π - ELEV

982.31

81+50

~~25+50~~

+ 88

82+00

~~26+00~~

T.P. 9.07 989.30 2.08 980.23

Lt

L

Rt

L8

11.7	10.4	11.0	10.1	11.0	12.3	13.0	14.6	15.8	16.3	17.2	18.3	19.3
10.6	11.9	11.3	11.6	11.3	10.0	9.3	7.7	6.5	6.0	5.1	4.0	3.0
90	71	57	47	25	16		18	32	37	54	74	88

11.8

10.5
100

18.2

4.1
100

13.1	12.5	12.8	12.5	15.3	17.0	18.6	20.0	21.5	21.7	21.9	22.1
9.2	9.8	9.5	9.8	7.0	5.3	3.7	2.3	0.8	0.6	0.4	0.2
100	72	57	38	11		12	18	27	33	58	70

20.5 21.1

1.8 0.6
100 82

13.8	13.1	13.4	14.3	16.1	17.7	18.7	22.1	22.3	22.5	22.1	20.9
8.5	9.2	8.9	8.0	6.2	4.6	3.6	0.2	0.0	0.2	0.2	1.4
100	80	55	32	19		8	30	44	65	82	100

Fe

26+50
10' Lt

Rock.

Sta + π - EICU

989.30

82+16

~~26+16~~

+55

✓

+80

✓

83+00

~~27+00~~

TBM

5.78 983.52

983.57

TBM

12.15

995.02

983.57

March 29, 1961

LT										
74.4	73.5	74.9	77.5	77.9	80.5	82.4	82.9	82.5	81.2	
14.7	15.8	14.4	11.8	11.4	8.8	6.9	6.4	6.8	8.1	
100	68	42	18	✓	18	31	50	74	100	

79.5	79.3	76.0	77.3	77.6	80.6	80.9	81.7	81.2	80.9	81.1	82.2	81.0
9.8	10.0	13.3	12.0	9.7	8.7	8.4	7.6	7.0	8.4	7.6	7.1	8.3
100	84	67	49	28	15		17	24	42	69	93	95
					fc							

Cor. Brn

80.0
9.3
100

82.0	82.2	83.5	83.9	84.1	84.9	84.6	82.8	81.1	
7.3	7.1	5.8	5.4	4.6	4.4	4.7	6.5	7.6	
87	58	41	27		10	24	41	61	

Fe
COR.

82.5
6.8
100

83.1
82.1
6.2
6.6
89
80
Barn

85.2	84.5	86.0	86.5	87.3	87.6	86.6	86.4	84.0	82.3
4.1	4.8	4.3	2.8	2.0	1.7	2.7	3.9	5.3	7.0
100	82	52	28	✓	12 fc	17	38	59	75

spike in 24" oak 88' Rt sta 27407

" " " " " "

81.3
8.0
85
Barn

Sta	+	π	-	ELEV
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		995.72		
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+50				
-----	--	--	--	--

84+00				
28+00				

+35				
-----	--	--	--	--

+70				
-----	--	--	--	--

85+00				
29+00				

+50				
-----	--	--	--	--

TP	11.06	1004.96	1.82	993.90
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KG
JS
JK
FS

March 30, 1961
Cool, Windy, R.R.
RT 50

89.4	88.8	89.1	86.1	86.0	85.6	85.3	83.9	82.8	82.5
6.3	6.9	8.0	9.0	9.7	10.1	10.4	11.8	12.9	13.2
100	78	58	32		31	49	78	95	100

FC

93.2	90.9	87.6	86.6	85.5	84.1	83.7	81.4	80.0
2.5	4.8	8.1	9.1	10.2	11.6	12.0	14.3	15.7
100	70	35	17		30	58	84	100

93.8	92.1	89.8	88.4	86.6	84.1	81.8	80.1	79.1
1.9	3.6	5.9	7.3	9.1	11.6	13.9	15.6	16.6
100	77	52	30		24	48	77	100

94.1	92.2	89.3	86.6	84.8	83.4	81.2	80.0	79.4
1.6	3.5	6.4	9.1	10.9	12.5	14.5	15.7	16.3
100	81	50	23		27	51	82	100

94.7	89.2	86.2		83.7	82.1	81.0	80.3	80.2
1.0	6.5	9.5		12.0	13.6	14.7	15.4	15.5
100	68	34		30	61	95	100	

95.1	90.4	88.5	87.0	85.5	83.9	82.7	82.3	82.1
0.6	5.3	7.2	8.7	10.2	11.8	13.0	13.4	13.0
100	75	48	24		25	51	77	100

Sta	+	π	-	ELEV
-----	---	-------	---	------

		1004.96		
--	--	---------	--	--

86+00				
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38+00				
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+30				
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+70				
-----	--	--	--	--

87+00				
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37+00				
------------------	--	--	--	--

+50				
-----	--	--	--	--

88+00				
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32+00				
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TP	3.94	1006.88	2.02	1002.94
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30 11/6 rch 1961
P. 2100019 51

LT			±						
03.1	01.5	00.9	93.9	90.3	89.6	91.1	89.1	88.8	
1.9	3.5	6.1	11.1	14.7	15.4	13.9	15.3	16.2	
100	65	27	0	26	45	65	91	100	

05.1	05.3	04.1	03.4	01.4	98.5	96.7	95.5	94.0	91.9
+0.7	+0.3	0.9	1.6	3.6	6.5	8.3	9.5	11.0	13.1
100	90	67	44	24		20	44	73	100

09.0	06.2	05.0	03.1	00.5	98.0	95.5	93.5		
+4.0	+1.2	0.0	1.9	4.5	7.0	9.5	11.5		
100	71	46	28		37	69	100		

09.4	07.3	04.4	02.5	01.1	99.4	96.9	95.0	94.0	
+4.4	+2.3	0.6	2.5	3.9	5.6	8.1	10.0	11.0	
100	73	43	16		28	57	83	100	

09.2	08.9	06.5	05.0	03.3	02.2	00.6	99.6	97.8	97.6	96.4	95.8
+4.2	+3.9	+1.5	0.0	1.7	2.8	4.4	5.4	7.2	7.4	8.6	9.2
100	93	61	37	20		21	49	69	79	85	100

Fe

09.5	07.2	04.5	03.0	02.3	01.5	00.7	01.1	99.6	97.4		
+4.5	+2.2	0.5	2.0	2.7	3.5	4.3	3.9	5.4	7.6		
100	80	50	24		20	40	49	66	100		

Fe

rock

Sta + π - ELEV

1006.88

88+50

32+50

89+00

33+00

+50

90+00

34+00

+50 Lt only Water Pond to Right

B.M.

2. 98 1003.90 (1003.85)

B.M.

8.71 1012.56

1003.85

90+50

95+60 - SEE PAGE 77

34+50 to 39+60 skipped because of water

95+60

39+60

RG
JS
JL
FS

Lt

9

Lt

52

30 March 1961
P. Cloudy

05.9	03.8	02.8	02.1	02.1	02.4	01.8	01.6	00.9	00.6
1.0	3.1	4.1	4.8	4.8	4.5	5.1	5.3	7.0	10.0
100	69	46	22		17	32	49	70	100

Feline

✓

03.5	03.4	03.2	03.0	02.8	01.7	01.9	01.0	00.2	00.4
3.4	3.5	3.7	3.9	4.1	5.2	5.0	5.9	7.7	9.5
100	94	67	36	14		30	67	87	100

✓

02.1	02.9	02.3	02.1	00.1	00.8	00.1	00.8	00.3	00.1	00.3
4.8	4.0	4.6	4.8	6.8	8.1	8.8	8.1	7.6	7.8	9.6
100	84	60	45	25		24	45	65	83	100

Fe

✓

00.3	02.3	00.5	00.7	00.6	00.4	00.2	00.2	00.8
6.6	4.6	6.4	9.2	10.3	11.5	11.7	11.4	12.1
100	74	41	10		28	59	96	100

Fe

✓

water

01.0	00.7	00.6	00.1	00.6
5.9	6.2	7.3	10.8	12.3
100	98	66	29	

Water Pond

Spike 12 P.P. 39+80 21' Lt-

" " " " " "

04.4 04.1 03.9 03.7

01.7	01.8	01.6	00.4	00.2	00.4	00.1	00.1	00.1	00.1	00.1
4.9	10.8	15.0	16.2	17.4	18.2	18.5	18.7	18.9	18.9	18.9
100	70	43	12		11	29	40	58	93	100

✓

Sta	+	π	-	ELEV
-----	---	-------	---	------

		1012.56		
--	--	---------	--	--

96+00				
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40+00				
-------	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

97+00				
-------	--	--	--	--

41+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

R6
J5
J6
R5

LT

R

30 March 1961
P. C. 100 d/4
RT 58

11.0	09.4	05.9	01.4	99.8	99.5	96.9	96.7	97.2
1.6	3.2	6.7	11.2	12.8	13.1	15.7	15.9	15.4
100	85	56	32		11	36	61	100

13.6	13.6	12.6	09.2	04.6	02.6	00.6	00.0	00.0
+1.0	+1.0	0.0	3.4	8.0	10.0	12.0	12.6	12.6
100	86	73	43	14		15	40	74

00.6	99.8
12.0	12.8
100	91

13.8	13.6	12.2	09.6
+1.2	+1.0	0.4	5.0
100	72	48	18

04.9	02.1	02.8	04.0	02.8
7.7	10.5	9.8	8.6	9.8
	27	52	44	79

03.2	02.8	01.8	01.8	02.9
9.4	9.8	10.8	10.8	9.7
102	98	94	92	90

E.
Ad.

13.9	13.6	12.4	11.6	09.0	07.4	07.8	08.1	04.2	04.1
+1.3	+1.0	0.2	1.0	3.6	5.2	4.8	4.5	8.4	8.5
100	91	59	49	18		26	42	51	59

03.1	04.6	04.8	04.9	04.3	03.5	03.5
8.9	8.0	7.8	7.7	8.3	9.1	9.1
100	90	81	70	63	62	60

SE E NE
Ad Ad Ad

Sta	+	π	-	ELCV
-----	---	-------	---	------

1012.56

T.P.	6.02	1017.67	0.91	1011.56 1011.65
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~~98+00~~
~~42+00~~

✓

✓

+30

✓

March 30, 1961

LT

E

RT

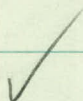
54

Rock

Sta. 43+95

13.1	12.4	12.5	11.9	11.7	11.5	12.4	05.6	05.3	04.4
4.6	5.3	5.2	5.8	6.0	6.2	5.3	12.1	12.4	13.3
63	40	30	26	19		22	33	39	40

14.2	14.3
3.5	3.4
86	100



04.4	05.4	05.9	06.1	05.6
13.3	12.3	11.8	11.6	12.1
83	75	64	52	45
	S.E. Rd.	E Rd.	N.E. Rd.	

04.5
13.2
92
Fe

13.8	14.3	14.5	13.1	12.1	11.4	11.8	10.7	06.7	06.4	05.2	06.1
3.9	3.4	3.2	4.6	5.6	6.3	5.9	7.0	11.0	11.3	12.5	11.6
100	87	68	43	20		9	12	19	26	27-29	30



05.1	05.6	06.4	06.5	06.9
12.6	12.1	11.3	11.2	10.8
79	64	62	50	38
Fe		S.E. Rd.	E Rd.	N.E. Rd.

Sta	+	π	-	ELEV
-----	---	-------	---	------

		1017.67		
--	--	---------	--	--

+57				
-----	--	--	--	--

✓				
---	--	--	--	--

99+00				
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43+00				
------------------	--	--	--	--

✓				
---	--	--	--	--

+40				
-----	--	--	--	--

NOTE: THIS SECTION IS
REVERSED.

✓				
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March 30, 1961

Lt

E

Rt

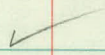
55

14.9	15.9	15.4	13.0	12.3	12.5	07.4	07.3	06.2	07.1	07.6
2.8	1.8	2.3	4.7	5.4	5.2	10.3	10.4	11.5	10.6	10.2
100	77	64	35	11		9	15	17-19	21	28
								Sitch		N.E. Rd



06.0	06.4	07.1	07.1
11.7	11.3	10.6	10.6
65	54	52	41
Fe		S.E. Rd	E Rd

16.2	15.4	15.9	14.3	13.6	10.6	08.1	08.3	07.3	08.1	08.1	08.6	08.0
1.5	2.3	1.8	3.4	4.1	7.1	9.0	9.4	10.4	9.6	9.0	9.2	9.7
39	21	16	14	10	5		2	3-5	6	13	26	38
								Sitch		Wedge Rd		Sledge Rd



17.9	17.3	17.0	15.7
10.2	0.4	0.7	2.0
53	69	91	100

04.9	05.0	07.0	07.4
12.8	12.7	10.7	10.3
100	66	51	40

05.6	07.6	08.2	08.9	09.2	09.7	09.5	09.1	08.7	10.0	11.6	12.5	15.1
12.1	10.1	9.5	8.8	8.5	8.0	8.2	8.6	9.0	7.7	6.1	5.2	2.6
67	41	29	27	17	4		8	9-11	13	18	23	26
			S.E. Rd		E	N. Edge Rd						

05.3	05.3
12.4	12.4
91	100



14.5	15.2	15.2	15.9
3.2	2.5	2.5	1.8
100	87	66	41
			Wedge Service Road

Sta + π - ELEV

1017.67

+68

✓

TBM

1.81

1015.86

1015.88

TBM

3.88

1019.76

1015.88

+73

✓

+82

driveway

✓

Rd
J3
JK
WMI
FS

March 30, 1961
April 3, 1961 cool, cloudy

Lt

R

Rt

SE

16.3	14.3	11.6	10.5	9.7	10.2	10.5	10.3	10.0	9.8	9.3	9.9
1.4	3.4	6.1	7.2	8.0	7.5	7.2	7.4	7.7	8.9	8.4	10.8
49	33	27	20	14	18	12	10	20	26	32	55

E Rd Sedge Rd

13.6	13.9	14.1	15.4
4.1	3.8	3.6	2.3
61	79	93	100

Wedge E Edge
Service Rd S Rd

9.4	9.1
11.3	11.0
100	83

Spike in 30" Oak 47' Lt Sta 43 + 65

10.9	10.4	9.1	9.1	10.3	10.5	10.7	10.3	9.1	9.4	9.4
8.9	9.4	10.7	10.7	9.5	9.3	9.1	9.5	10.7	10.4	12.4
26	20	18	18	14	9		18	24	27	50

FL 15' only

10.6	12.6	14.2	15.3	16.4	16.5
9.2	7.2	5.6	4.5	3.4	3.3
31	52	80	81	89	100

9.5	9.9
13.3	12.9
100	70

17.5	12.0	16.6	13.7	12.6	10.4	10.9	10.9	10.8	10.5	9.3	10.0	9.4
2.3	2.8	3.2	6.1	7.2	9.1	8.9	8.9	9.0	9.3	10.5	9.8	11.4
100	81	57	52	41	16	7		7	18	23	28	40

bank E Rd

9.6	9.2
13.2	12.6
100	70

Sta	+	π	-	ELEV
-----	---	-------	---	------

		1019.76		
--	--	---------	--	--

100+00				
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44+00				
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✓				
---	--	--	--	--

+50				
-----	--	--	--	--

101+00				
--------	--	--	--	--

45+00				
------------------	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

Sta + π - ELEV

1019.76

102+00

~~46+00~~

✓

TBM

2.64 1017.12

1017.15

TBM

10.56

1027.71

1017.15

102+50

~~46+50~~

✓

103+00

~~47+00~~

April 13, 1961

LT

2

RT

58

16.0	15.7	15.4	14.8	15.6	16.1	16.5	16.2	15.9	15.8	15.9	16.3
3.8	4.1	4.4	5.0	4.2	3.7	3.3	3.6	3.9	4.4	3.9	3.5
54	33	27	23	17	12		9	15	18	21	36

16.8	18.0	20.2
3.0	1.8	0.4
71	84	100

15.1	15.9	16.6
4.7	3.9	3.2
100	85	69

Spike in TP LT Sta 46 + 35±

18.7	16.7	16.7	15.7	17.2	17.7	17.4	17.1	16.7	17.0
9.0	11.0	11.0	12.0	10.5	10.0	10.3	10.6	11.0	10.7
91	58	31	22	11		8	14	19	22

20.1
7.6
100

17.3	18.0	17.9
10.4	9.7	9.8
100	76	50

17.3	16.9	17.1	16.6	17.7	18.1	18.5	18.3	18.2	18.0	17.4	17.7
10.4	10.8	10.6	11.1	10.0	9.6	9.2	9.4	9.5	9.7	10.3	10.0
57	38	25	21	15	12		8	11	14	19	21

18.2	19.2
9.5	8.5
88	100

17.8	18.2	18.0
9.9	9.5	9.7
100	75	44

Sta t π - ELEV

103+50 1027.71

~~47+50~~

✓

104+00

48+00

✓

+50

April 3, 1961

LT

E

RT

59

18.0	18.2	17.7	18.6	19.0	19.6	19.4	19.1	18.5	18.1
9.7	9.5	10.0	9.1	8.7	8.1	8.3	8.6	9.2	9.0
54	30	22	15	11		8	13	17	25

18.3
✓ 9.4 8.5
81 100

✓

18.4 18.8 19.1
9.3 8.9 8.6
100 80 52

19.6	19.6	19.1	19.1	20.1	20.6	20.4	20.0	19.4	19.6	19.9
8.1	8.1	8.0	8.6	7.6	7.1	7.3	7.7	8.3	8.1	7.8
79	53	30	21	12		9	15	17	26	55

19.6
✓ 8.1
100

✓

19.2 19.1
8.5 8.0
100 80

22.0	21.5	21.0	20.5	21.0	21.2	21.6	21.3	21.1	20.3	20.1
5.7	6.2	6.7	7.2	6.7	6.5	6.1	6.4	6.6	7.4	7.0
69	57	30	21	15	11		8	12	18	36

21.8
✓ 5.9
100

✓

20.2 20.4 20.6
7.5 7.3 7.1
100 85 64

Sta	+	π	-	ELEV
-----	---	-------	---	------

105+00		1027.71		
49+00				

✓

+50

✓

106+00

~~50+00~~

April 3, 1961

LT

4

RT

60

21.7	22.1	21.7	22.3	22.1	22.4	21.9	21.3	21.5
6.0	5.6	6.0	5.4	5.0	5.3	5.8	6.4	6.2
38	24	20	11		9	15	19	31
Fe.								

22.1	22.2	22.4
5.6	5.5	5.1
52	77	100

20.9	21.0	21.3
6.8	6.7	6.4
100	80	58

22.7	23.0	22.7	23.3	23.6	23.2	22.6	22.2	22.2
5.0	4.7	5.0	4.4	4.1	4.5	5.1	5.5	5.5
37	28	22	10		11	17	19	38
Fe								

22.7	22.2	21.4
5.0	5.5	6.3
51	71	100

21.1	21.7
6.0	6.0
100	80

24.3	24.4	23.8	24.2	24.5	24.3	23.8	23.1	22.7
3.4	3.3	3.9	3.5	3.2	3.4	3.9	4.6	5.0
37	30	21	10		11	15	19	30
Fe.								

24.3	23.8	22.3
3.4	3.9	5.4
52	72	100

22.2	22.6	23.2
5.5	5.1	4.5
100	84	60

Sta + X - ELV.

1027.71

106+50
50+50

✓

T.BM 10.69 ~~1036.40~~ 2.00 1025.71 ^{1025.65}
1025.76

+67

✓

+69

April 3, 1961

Lt

L

Rt

66

25.1	24.9	25.0	24.9	25.5	25.2	24.8	24.2	24.0
2.0	2.8	2.7	2.8	2.2	2.5	2.9	3.5	3.7
38	27	18	10		11	15	20	30

26.3	27.6	27.6		23.1	23.5	24.2
1.4	0.1	0.1	✓	4.6	4.2	3.5
66	96	100		100	77	54

iron in stump sta. 50+74 24' Rt

27.6	26.4	25.6	25.2	25.5	26.0	25.7	25.3	24.7	24.9
8.9	10.1	10.9	11.3	11.0	10.5	10.8	11.2	11.8	11.6
67	38	31	19	11		12	16	25	41

29.4	31.2		✓	23.1	24.3
7.1	5.3			12.8	12.2
86	100			100	75

29.1	27.0	25.7	25.3	25.5	26.0	25.7	25.3	24.7	24.9
7.4	9.5	10.8	11.2	11.0	10.5	10.8	11.2	11.8	11.6
90	68	37	20	11		12	16	26	43

30.5			✓	23.7	24.3
6.0				12.8	12.2
100				100	73

Sta + π - ELV.

1036.45

~~1036.40~~

106+77

~~50+77~~

✓

+79

✓

107+00

~~51+00~~

April 3, 1961

Lt

E

Rt

62

27.2	26.2	25.5	25.6	26.1	25.9	25.5	25.9	24.9
9.3	10.3	11.0	10.9	10.4	10.6	11.0	10.6	11.6
70	47	21	10		11	18	28	40

✓
29.0
7.5
90
30.0
6.5
100

23.8
12.7
100
24.5
12.0
75

27.1	27.1	25.4	25.7	26.2	26.0	25.6	25.9	25.0
9.4	9.4	11.1	10.8	10.3	10.5	10.9	10.6	11.5
46	29	22	10		11	18	30	42

✓
28.9
7.6
72
31.2
5.3
100

23.9
12.6
100
24.5
12.0
75

25.9	26.0	25.8	26.2	26.5	26.4	26.1	25.6	26.5
10.6	10.5	10.7	10.3	10.0	10.1	10.4	10.9	10.0
20	14	11	9		11	17	22	29

✓
28.4
8.1
26
28.4
8.1
47
30.0
6.5
74
31.9
4.6
100

24.6
11.9
100
24.9
11.6
82
25.6
10.9
61
25.9
10.6
34

Sta + ∇ - ELV.

~~107+50~~
~~51+50~~

~~1036.45~~
~~1036.40~~

✓

~~108+00~~
~~52+00~~

✓

+50

✓

April 3, 1961

Lt

L

Rt

63

30.4	26.9	27.0	27.2	27.1	27.3	26.7	27.0	26.9
6.1	9.6	9.5	9.3	8.8	9.2	9.8	9.5	9.6
27	21	14	10		10	17	20	41

31.0 32.4 34.6
 5.5 4.1 1.9
 47 74 100

25.5 26.7
 11.0 9.8
 100 62

35.7	33.4	31.6	28.1	28.3	28.6	28.2	27.8	28.2	27.4
0.8	3.1	4.9	8.4	8.2	7.9	8.3	8.7	8.3	9.1
85	58	28	22	9		11	18	28	46

36.5
 0.0
 100

25.9 26.4 27.4
 10.6 10.1 9.1
 100 85 59

32.6	32.1	31.2	29.5	29.4	29.7	29.1	28.6	28.6	27.6
3.9	4.4	5.3	7.0	7.1	6.8	7.4	7.9	7.9	8.9
61	49	28	23	10		11	18	43	72

32.0 32.7 34.8
 4.5 3.8 1.7
 64 78 100

26.5
 10.0
 100

Sta + Δ - ELEV.

~~1036.45~~

~~1036.40~~

~~1081.75~~

~~521.75~~

✓

T.P.

8.75

~~1041.05~~

~~1041.00~~

4.15

~~1032.30~~

~~1032.25~~

(1032.25)

~~1091.00~~

~~531.00~~

✓

+ 50

✓

April 3, 1961

Lt

Q

Rt

64

31.4	30.9	30.5	29.9	29.7	30.2	29.7	29.3	28.2
5.1	5.6	6.0	6.6	6.8	6.3	6.8	7.2	8.3
46	32	23	18	12		12	18	55

32.5 34.2
4.0 2.3
67 100

£ STA 54+00

26.5 27.4
10.0 9.1
100 79

31.7	30.9	30.5	30.5	30.8	30.3	29.9	29.3	28.1
9.4	10.2	10.6	10.6	10.3	10.8	11.2	11.8	13.0
52	33	24	9		11	19	24	57

32.5 33.1
8.6 7.4
75 100

26.8 27.2
14.3 13.9
100 87

31.6	30.9	30.8	30.6	31.2	31.7	31.2	30.7	29.6	28.3
9.5	10.2	10.3	10.5	9.9	9.4	9.9	10.4	11.5	12.8
71	50	33	19	10		10	15	22	44

32.3 32.8
8.8 8.3
92 100

27.1 27.4
14.0 13.7
100 69

Sta

+

π

-

ELV.

1041.05

~~1041.00~~

110+00

~~54+00~~

✓

+50

✓

111+00

~~55+00~~

✓

April 3 1961

Lt

E

Rt

65

31.1	31.0	31.5	31.8	32.3	31.9	31.1	29.9	28.8
10.0	10.1	9.6	9.3	8.8	9.2	10.0	11.2	12.3
33	19	14	10		10	16	20	33

31.2	31.8	32.8
9.9	9.3	8.3
51	73	100

26.6	26.9	27.5
14.5	14.2	13.6
100	92	65

31.1	31.3	31.4	32.1	32.3	32.0	32.4	32.0	29.8	28.1
9.4	9.8	9.7	9.0	8.8	8.1	8.7	9.1	11.3	12.4
27	22	19	14	10		10	16	22	45

31.6	31.8	32.5	33.4	33.6
9.5	9.3	8.6	7.7	7.5
33	51	73	92	100

27.3	28.0
13.8	13.1
100	78

32.3	32.2	32.0	32.5	33.0	33.6	33.0	32.6	30.1	29.4
8.8	8.9	9.1	8.6	8.1	7.5	8.1	8.5	10.4	11.7
33	26	20	16	10		10	15	22	50

32.8	33.5	34.2	35.0
8.3	7.6	6.9	6.1
50	72	91	100

28.2	28.8
12.9	12.3
100	79

Sta

+

△

-

ELV.

1041.05
~~1041.00~~

111+50

~~55+50~~

✓

112+00

~~56+00~~

✓

+50

✓

April 3, 1961

Lt

E

Rt

66

34.3	33.8	33.0	33.1	34.0	33.4	33.0	32.0	31.0
6.8	7.3	8.1	7.4	7.1	7.7	8.1	9.1	10.1
31	24	18	10		11	16	22	45

34.9	35.8	36.8
6.2	5.3	4.3
42	73	100

28.8	29.1
12.3	11.4
100	77

34.1	35.8	34.1	33.8	34.0	34.5	33.9	33.4	33.0	32.2
3.4	5.3	6.4	7.3	7.1	6.6	7.2	7.7	8.1	8.9
53	31	20	16	9		11	17	24	45

38.1	39.6
2.4	1.5
80	100

29.1	30.2
12.0	10.9
100	79

36.4	35.6	34.5	34.1	34.8	35.1	34.5	34.0	33.6	33.0
4.7	5.5	6.6	6.4	6.3	6.0	6.6	7.1	7.5	8.1
26	21	15	14	10		11	18	24	35

38.4	39.9	41.0
2.7	1.2	0.1
48	169	100

29.2	30.8
11.9	10.3
100	68

Stg + 天 - ELV

1091.05

~~1041.00~~

~~112+75~~

~~56+75~~

✓

~~113+00~~

~~57+00~~

✓

+10

April 3, 1961

26

2

26

67

39.0	36.4	35.1	34.8	35.2	35.5	34.9	34.5	34.1	33.4
2.1	4.7	5.4	6.3	5.9	5.6	6.2	6.6	7.0	7.7
49	26	20	16	9		10	16	22	30

40.4	40.1	38.8	38.2
0.7	0.4	2.3	2.9
71	90	97	100

✓

29.2	31.1
11.9	10.0
100	66

38.1	37.3	36.1	34.9	35.4	35.8	35.3	34.8	34.0	32.4
2.4	3.8	5.0	6.2	5.7	5.3	5.8	6.3	7.1	8.7
48	33	26	18	11		10	15	23	50

36.4	36.5	36.5	38.3	39.0
4.2	4.6	4.6	2.8	2.1
61	67	73	80	90
			82	81

✓

24.4	30.5
11.7	10.6
100	79

35.9	35.5	34.9	35.0	35.5	36.0	35.5	35.0	33.9	33.2
5.4	5.6	6.2	6.1	5.6	5.1	5.6	6.1	7.2	7.9
42	33	25	17	14		9	14	23	32

35.9	34.1	38.2	39.0
5.2	4.0	2.9	2.1
48	56	68	89

✓

29.5	30.1	32.1
11.6	11.0	9.0
100	87	54

Sta

+

K

-

ELV.

1041.05
~~1041.00~~

113+26

57+26

✓

+45

✓

+65

Apr. 3, 1961

Lt

E

Rt

68

38.8	37.6	36.3	35.6	36.1	36.2	35.4	35.0	32.7	31.9
2.3	3.5	4.8	5.5	5.0	4.9	5.7	6.1	8.4	9.2
85	54	38	29	15		12	19	32	52
ERd #100	ERd #100	BT	BT	BT					

39.2

1.9
100
BT

29.5

11.6
100

30.2

10.9
86

36.4	37.6	37.7	37.4	36.4	36.3	35.6	34.8	34.5	33.1	31.8
4.7	3.5	3.4	3.7	4.7	4.8	5.5	6.3	6.6	8.0	9.3
79	74	62	38	9		10	16	23	32	42
		ERd Hwy 100	ERd #100	BT						

41.1

0.0
95

29.5

11.6
100

30.2

10.9
86

31.5

9.6
54

38.2	36.4	35.9	36.6	36.8	36.2	34.6	33.6	31.6	30.1
2.9	4.7	5.2	4.5	4.3	4.9	6.5	7.6	9.6	10.4
73	60	44	40	26	2	33	50	62	66
				ERd 100	100	ERd 100			

39.7

1.4
80

29.6

11.5
100

sta + π - Elev

1091.05

1041.00

1141.00

~~581.00~~

✓

BM

5.05

1036.00

1035.95

(1036.01)

BM

4.71

1036.34

1036.29

(1036.35)

BM

4.75

1036.30

1036.25

(1036.31)

April 3, 1961

LT

E

RT

69

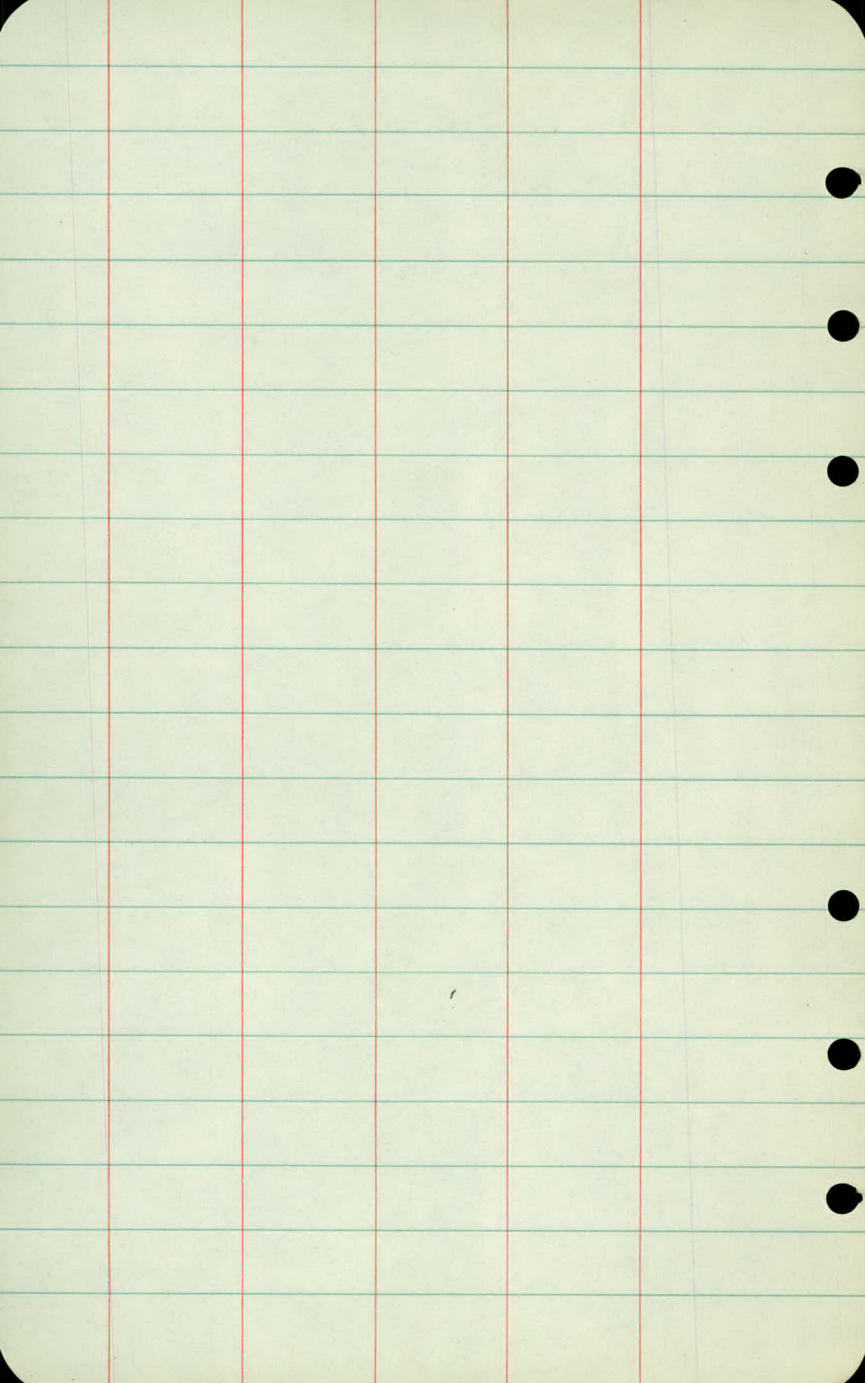
38.0	37.0	34.6	34.5	35.6	35.6	35.4	34.7	33.9	34.0
3.1	4.1	6.5	6.6	5.6	5.5	5.7	6.4	7.2	7.1
59	29	22	17	13		10	15	38	47
									ERL 100

32.1	32.6	33.6
9.0	8.6	7.6
100	95	70
	ERL 100	ERL 100

Double spike in PP NW Cor. Lower Afton + Hwy 100

yellow spike " " " "

slope w/red flagging " " " "



R6
JS
JK
WM
FS

April 3, 1961

70

Profile Levels

Hwy 100 From Lower Afton North Pg 67-68

Hwy 100 " " " South Pg 67-68

Lower Afton from Hwy 100 East Pg 68-69

pages 70-72

sta	+	π	-	Elev
BM	8.64	1044.99		1036.35
0+00	North		8.9	1036.1
+50			7.4	1037.6
1			6.1	1038.9
+50			4.5	1040.5
2			3.0	1042.0
+50			1.6	1043.4
3			0.4	1044.6
		1044.99		
-50	South		10.8	1034.2
+100			12.2	1032.8
-1+50			13.2	1031.8
-2+00			13.9	1032.1
-2+50			14.0	1031.0
-3+00			14.2	1030.8
		1044.99		
+50			9.5	1035.5
1			9.2	1035.8
+50			9.0	1036.0

April 3, 1961

715

Hwy 100 from Lower Afton North

Yellow spike in PP NW cor Lower Afton & Hwy 100

Hwy 100 from Lower Afton South

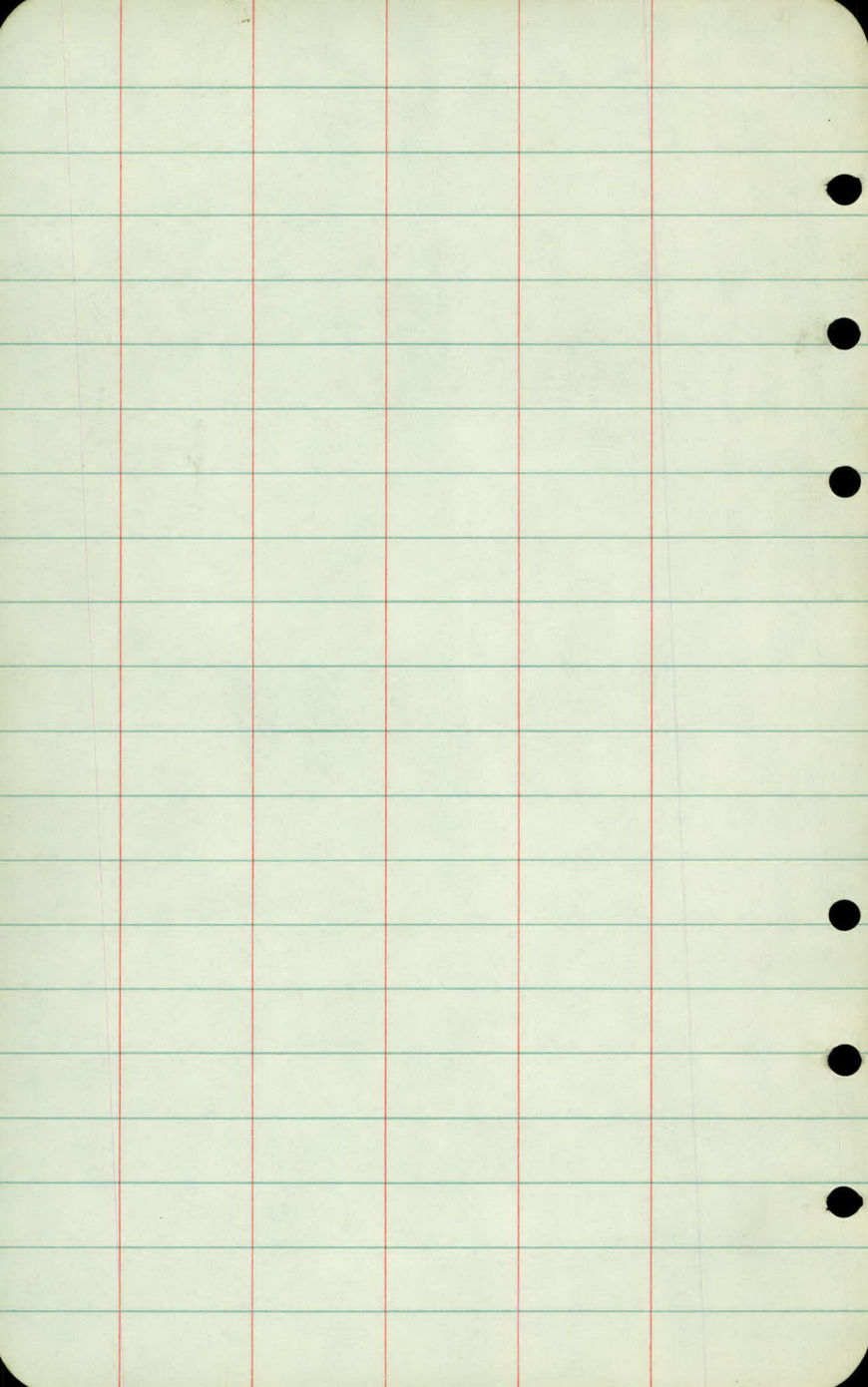
Lower Afton Rd East of Hwy 100

Sta	+	π	-	Elev
		1044.99		
2+00			8.7	1036.3
+50			7.9	1037.1
3+00			6.8	1038.2
BM			8.64	1036.35 (1036.25)

April 3, 1961

721

Yellow spike in PP NW cor Hwy 100 & Lower Afton



Lower Aston Road

73

Bench Level re-run

Lower Aston Road

McKnight to Hwy 100

4 pages 73-77

Sta	+	Σ	-	Elev
BM ₁	13.26	916.20		902.94
TP ₁	13.37	929.05	0.52	915.68
TP ₂	12.63	941.48	0.20	928.85
TP ₃	5.62	944.28	2.82	938.66
BM ₂	9.64	948.28	5.64	938.64
TP ₄	13.65	957.69	4.24	944.04
BM ₃	10.03	964.33	3.39	954.30
TP ₅	5.45	969.57	0.21	964.12
BM ₄	11.65	975.23	5.99	963.58
TP ₆	13.13	986.23	2.13	973.10
BM ₅	12.35	995.92	2.66	983.57
TP ₇	8.28	1003.56	0.64	995.28
BM ₆	9.28	1007.51	5.33	998.23 <i>644</i>
BM ₇	6.10	1009.95	3.66	1003.85
TP ₈	10.35	1017.46	2.84	1007.11
BM ₈	2.53	1018.41	1.58	1015.88
BM ₉	10.65	1027.80	1.26	1017.15
BM ₁₀	8.20	1033.96	2.04	1025.76
TP ₉	6.37	1038.62	1.71	1032.25

R6
JS
JL
WM

Description

April 24, 1961
Cloudy 40° Windy

74

Spike in 18" oak 60' Rt Sta 0-12

root

root

rock

Spike in 10" Elm 74' Lt Sta ~~5+50~~ ⁶¹⁺⁵⁰

nail E Sta 10+00

Spike in Quad Oak 100' Lt Sta ~~13+25~~ ⁶⁹⁺²⁵

rock

Spike in 10" Cott 100' Lt Sta ~~70+12~~ ⁷⁶⁺¹²

Spike in 24" oak 88' Rt Sta ~~29+07~~ ⁸³⁺⁰⁷

rock

Bent

KP 3-16-62 (put in new spike)

~~Spike in root 20" oak 33' E. of Culvert by Gray Barn on~~
Lower Aston Rd.

Spike in PP 21' Lt Sta ~~39+80~~ ⁹⁵⁺⁸⁰

Rock

Spike in 30" oak 41' Lt Sta ~~43+65~~ ⁹⁹⁺⁶⁵

Spike in P.P. Lt. Sta. ~~46+35~~ ¹⁰²⁺³⁵

Iron in stump 24' Rt Sta. ~~50+74~~ ¹⁰⁶⁺⁷⁴

Sta. 54+00 E

Sta	+	Σ	-	Elev.	
		1038.62			
TBM			2.61	1036.01	
B.M. ₁₁			2.27	1036.35	
TBM			2.31	1036.31	
B.M. ₁₁	2.13	1038.48			1036.35
TP ₉	2.17	1034.43	6.22	1032.26	1032.25
B.M. ₁₀	1.94	1027.71	8.66	1025.77	1025.76
B.M. ₉			10.56	1017.15	1017.15
B.M. ₈	1.39	1017.27	11.83	1015.88	1015.88
B.M. ₇	3.76	1007.61	13.42	1003.85	1003.85
B.M. ₆	5.23	1003.46	9.38	998.23	998.23
T.P.	0.00	995.25	8.21	995.25	
B.M. ₅	0.78	984.36	11.67	983.58	983.57
T.P.	0.18	971.23	13.31	971.05	
B.M. ₄	3.94	967.50	7.67	963.56	963.58
T.P.	1.86	959.67	9.69	957.81	
B.M. ₃	1.00	955.29	5.38	954.29	954.30
TP	10.66	954.69	11.26	944.03	
T.P.	1.81	944.96	11.94	942.75	

RG
JL
LB
WM

Description

April 28, 1961
cloudy 35° windy 75
MAY 5, 1961
cloudy windy 50°

- Double spike in PP NW Cor. Hwy 100 & Lower Altton
- yellow painted spike " " " " " "
- slope w/red flagging " " " " " "

Rock

Rock

Rock

9 STA. 10+00

Top Fence Post

Sta	+	∓	—	ELV.	
		944.56			
M ₂			5.94	938.62	938.64
T.P.	1.55	940.94	5.17	939.39	
T.P.	0.11	928.14	12.91	928.03	
T.P.	0.05	916.73	11.46	916.68	
B.M. ₁			13.80	902.93	902.94

RG
JL
WM
LB

Description

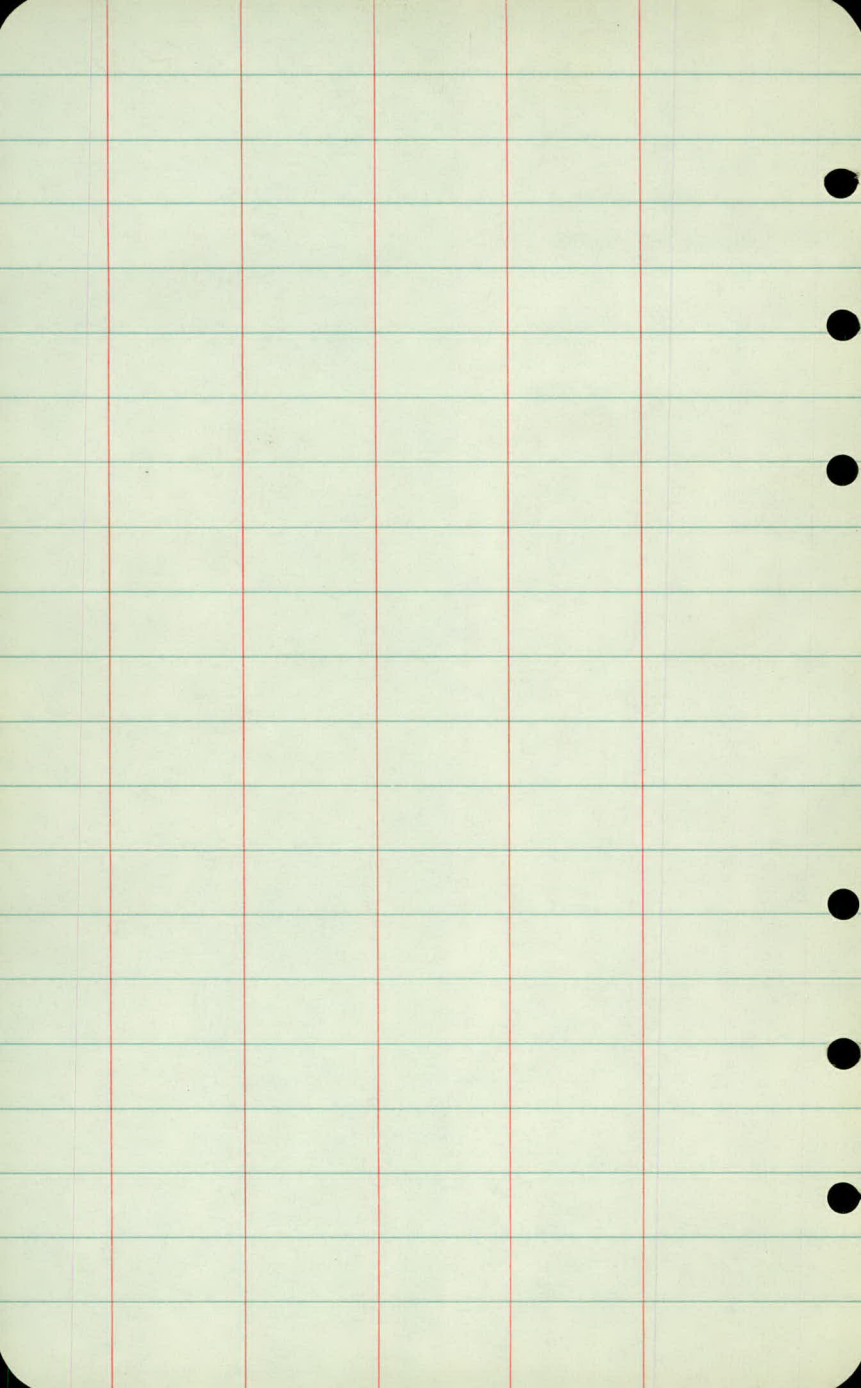
MAY 5, 1961
Cloudy - cool 50° - 76°

E STA 2+00

Rock

Stump

Spike in 18" oak 60' RT Sta 0-12



X-sections

Sta 90+50 to 95+30

Sta + π - Elev

BM 1.30 1005.12

1003.82

1/6

5.35

99.77

99.8

40
Now 96

Ice on pond

11.54

993.58

993.58

90+50

91

+50

92

+50

FX
WM
RB
DS
BS

Nov. 29, 1961

78

Spike in PP 21' Lt Sta 39+80

$\begin{matrix} q4.3 \\ 10.7 \\ 32 \end{matrix}$
 $\begin{matrix} q4.0 \\ 10.4 \\ 32 \end{matrix}$
 $\begin{matrix} q3.9 \\ 10.3 \\ 57 \end{matrix}$
 $\begin{matrix} q3.9 \\ 10.3 \\ 75 \end{matrix}$

$\begin{matrix} q4.2 \\ 10.4 \\ 75 \end{matrix}$
 $\begin{matrix} q4.3 \\ 10.7 \\ 57 \end{matrix}$
 $\begin{matrix} q4.1 \\ 10.5 \\ 37 \end{matrix}$
 $\begin{matrix} q3.6 \\ 0.0 \\ 15 \end{matrix}$
 $\begin{matrix} q3.0 \\ 0.6 \end{matrix}$
 $\begin{matrix} q2.9 \\ 0.7 \\ 25 \end{matrix}$
 $\begin{matrix} q3.1 \\ 0.5 \\ 50 \end{matrix}$
 $\begin{matrix} q2.9 \\ 0.7 \\ 75 \end{matrix}$

$\begin{matrix} q2.0 \\ 1.6 \\ 75 \end{matrix}$
 $\begin{matrix} q2.0 \\ 1.6 \\ 50 \end{matrix}$
 $\begin{matrix} q1.6 \\ 2.0 \\ 25 \end{matrix}$
 $\begin{matrix} q1.5 \\ 2.1 \end{matrix}$
 $\begin{matrix} q1.3 \\ 2.3 \\ 25 \end{matrix}$
 $\begin{matrix} q1.0 \\ 2.6 \\ 50 \end{matrix}$
 $\begin{matrix} q0.4 \\ 3.2 \\ 75 \end{matrix}$

$\begin{matrix} q9.8 \\ 3.8 \\ 75 \end{matrix}$
 $\begin{matrix} q9.5 \\ 4.1 \\ 50 \end{matrix}$
 $\begin{matrix} q9.3 \\ 4.3 \\ 25 \end{matrix}$
 $\begin{matrix} q9.4 \\ 4.2 \end{matrix}$
 $\begin{matrix} q9.1 \\ 4.5 \\ 25 \end{matrix}$
 $\begin{matrix} q8.7 \\ 4.9 \\ 50 \end{matrix}$
 $\begin{matrix} q8.7 \\ 4.9 \\ 75 \end{matrix}$

$\begin{matrix} q8.8 \\ 4.8 \\ 75 \end{matrix}$
 $\begin{matrix} q8.6 \\ 5.0 \\ 50 \end{matrix}$
 $\begin{matrix} q8.4 \\ 5.2 \\ 25 \end{matrix}$
 $\begin{matrix} q8.2 \\ 5.4 \end{matrix}$
 $\begin{matrix} q8.2 \\ 5.4 \\ 25 \end{matrix}$
 $\begin{matrix} q8.3 \\ 5.3 \\ 50 \end{matrix}$
 $\begin{matrix} q8.4 \\ 5.2 \\ 75 \end{matrix}$

Sta	+	T	-	Elev
		993.58		

93

+50

94

+50

95

TP	11.59	1005.12	0.00	993.58
----	-------	---------	------	--------

+30

BM

1.30

✓ Nov. 29, 1961 79

LT

RT

89.4	88.9	88.5	88.4	88.2 ✓	88.5	88.3
4.2	4.7	5.1	5.2	5.4	5.1	5.3
75	50	25		25	50	75

90.2	89.3	88.6	88.5	✓ 88.4	88.5	88.6
3.4	4.3	5.0	5.1	5.2	5.1	5.0
75	50	25		25	50	75

91.7	90.8	90.1	89.6 ✓	89.0	88.9	89.3
1.9	2.8	3.5	4.0	4.6	4.7	4.3
75	50	25		25	50	75

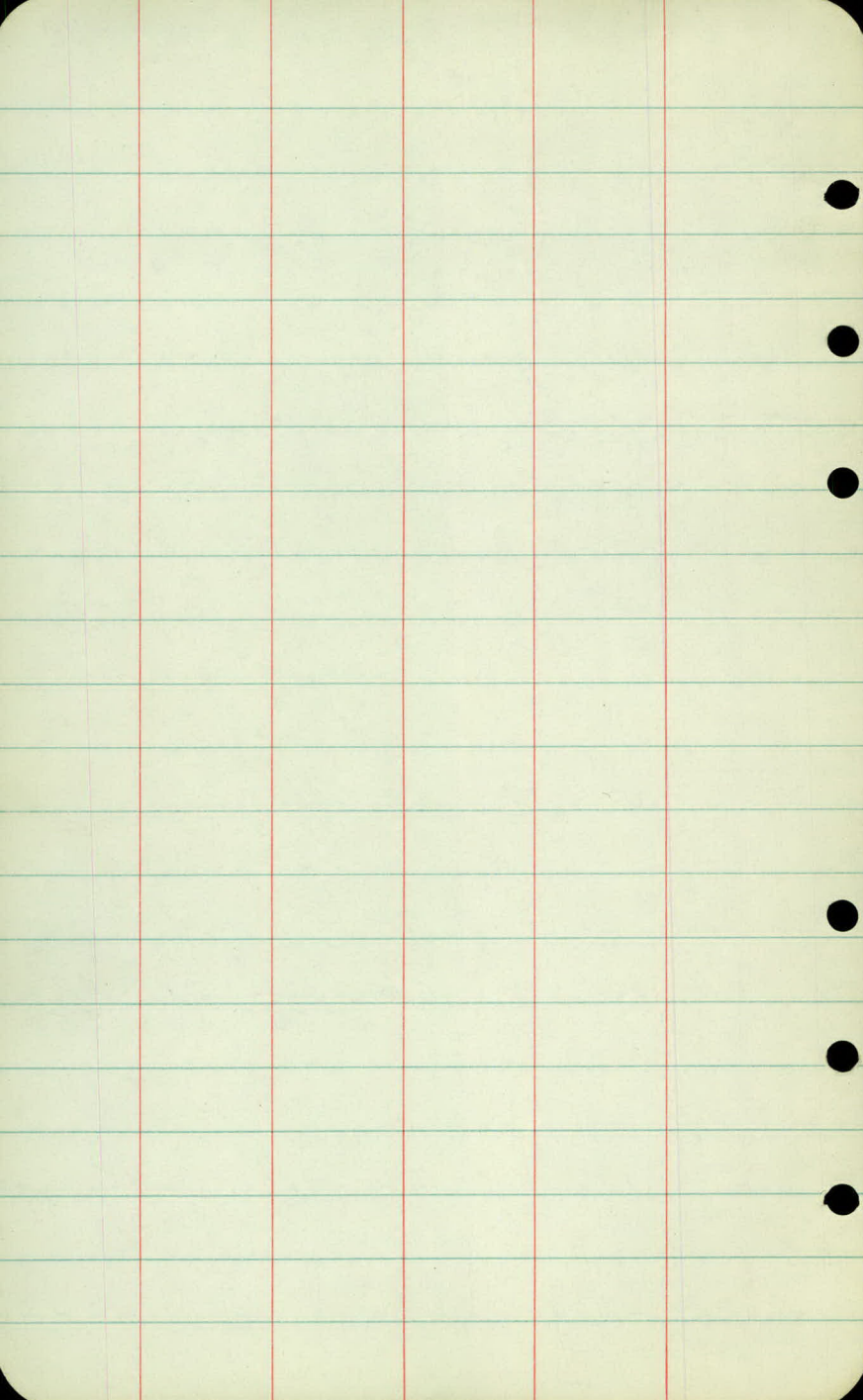
93.8	92.6	91.6	91.4 ✓	90.6	90.3	90.2
10.2	1.0	2.0	2.2	3.0	3.3	3.4
75	50	25		25	50	75

98.1	95.2	94.0	93.6	93.0 ✓	92.2	91.5	91.6
+4.5	+1.6	+0.4	0.0	0.6	1.4	2.1	2.0
75	50	25	14		25	50	75

92.4	92.9	92.9	91.0 ✓	95.4	96.6	97.9	100.8
12.7	12.2	12.2	11.1	9.7	8.5	7.2	3.3
39	23	13		27	46	57	75

92.5	92.1
12.6	13.0
64	75

Reverse
This section



Lt

£

Lower Afton Rd.

LINE REVISION

Bench levels

East Co. Line - to 1 mile East

Sta	+	Σ	-	Elev.	
B.M.	5.90	1003.00			<u>997.50</u> 79.7/10
T.P.	13.48	1014.66	1.82	1001.18	
T.P.	13.32	1026.36	1.62	1013.04	
T.P.	12.63	1038.14	0.85	1025.51	
B.M.			2.32	1035.82	<u>1036.22</u>

Washington Co.

B.M.	11.45	1047.27			<u>1036.22</u> 1035.82
T.P.	3.32	1047.08	3.51	1043.76	
T.P.	8.27	1045.40	9.95	1037.13	
T.P.	6.90	1049.47	2.83	1042.57	
B.M.			5.69	1043.78	
T.P.	13.62	1061.69	1.40	1048.07	
T.P.	12.91	1074.16	0.44	1061.25	
T.P.	10.19	1084.23	0.12	1074.04	<u>1074.44</u>
T.P.	12.25	1088.89	2.59	1076.64	
T.P.	2.81	1083.50	8.20	1080.69	
B.M.			6.62	1076.88	<u>1080.48</u>

Hiway

Spk. in pp. N.W. Cor Lower Afton Rd @ Century Ave.

Spk. in pp. Same as above

12" Elm Tree Lt. 30" Know where it is

Spk. in pp. Lt Side Lower Afton Rd.

Top Conc. base S.W. Cor. Hi. Line Tower. N. Side
of Rd.

+ π - E/eo

1074.44

B.M. 11.09 1085.13

1074.04

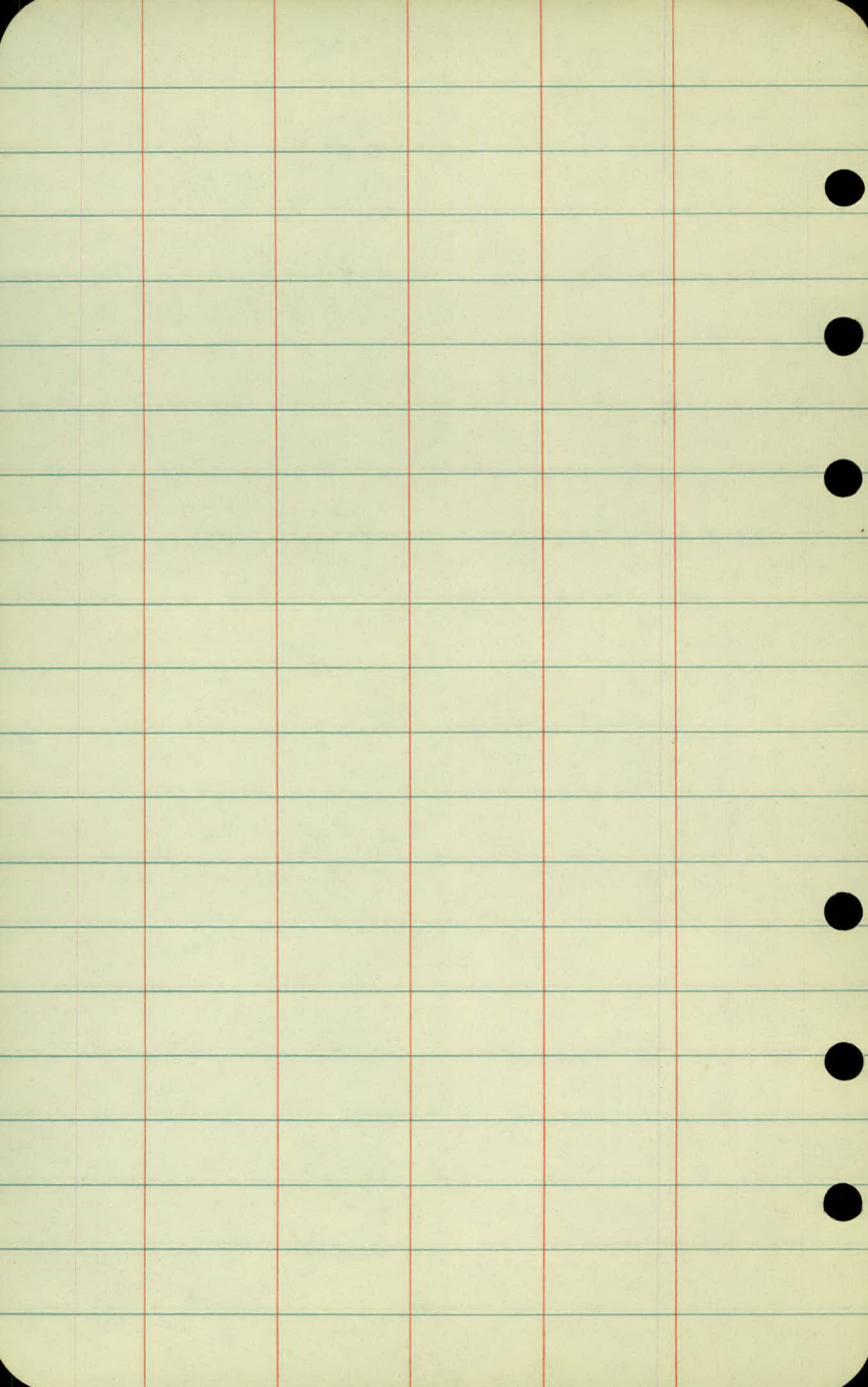
T.P. 0.11 1080.85 4.39 1080.74

B.M. 0.74 1080.11 1080.48

1080.51

Spk. in P.R. Lt of R. (Lower R.F. 50)

Spk in Elm 35' Lt of S.B.L. Sta 619. + 35
(Hiway Dept.)



Lower Afton Rd.

LINE REVISION

Profile Levels

No. of Lower Afton Rd. From
McKnight Rd to E. G. Line Rd.

Sta	+	Δ	-	Elev
B.M.	10.48	913.02		902.94 902.54

0+00				03.4
------	--	--	--	------

+19				07.8
-----	--	--	--	------

+32				12.0
-----	--	--	--	------

T.P.	13.02	925.98	0.06	912.96
------	-------	--------	------	--------

+55				18.7
-----	--	--	--	------

+60				21.5
-----	--	--	--	------

+77				25.1
-----	--	--	--	------

T.P.	12.93	938.54	0.37	925.61
------	-------	--------	------	--------

1+00				30.8
------	--	--	--	------

+27				35.8
-----	--	--	--	------

+42				37.6
-----	--	--	--	------

✍

5 pk. in 18" oat 60' Lt. Sta. 0-12 (west)

9.6

5.2

1.0

6.3

4.5

0.9

7.7

2.7

0.9

Sta	+	π	-	Elev.
		938.54		

T. P.	6.59	944.44	0.69	937.85
-------	------	--------	------	--------

1 + 50				39.0
--------	--	--	--	------

+ 70				39.9
------	--	--	--	------

2				39.9
---	--	--	--	------

+ 35				40.6
------	--	--	--	------

+ 50				39.6
------	--	--	--	------

+ 68				36.6
------	--	--	--	------

+ 88				33.1
------	--	--	--	------

3				32.0
---	--	--	--	------

+ 20				30.6
------	--	--	--	------

~~E~~

5.4

4.5

4.5

3.8

4.8

7.8

11.3

12.4

13.8

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		944.44		
--	--	--------	--	--

3 + 39				32.3
--------	--	--	--	------

+ 50				33.5
------	--	--	--	------

+ 73				36.2
------	--	--	--	------

4				37.8
---	--	--	--	------

+ 25				38.3
------	--	--	--	------

+ 58				38.8
------	--	--	--	------

+ 75				38.5
------	--	--	--	------

5			✓	38.3
---	--	--	---	------

+ 17				38.2
------	--	--	--	------

~~2~~

12.1

10.9

8.2

6.6

6.1

5.6

5.9

6.1

6.4

sta + π - Elev

944.44

36.9

5 + 32

~~5 + 13.38 = 4195.38~~

+ 49

33.2

T.P.

0.00

931.12

13.32

931.12

+ 82

25.3

6 + 25

19.9

+ 53

18.3

+ 82

17.7

+ 88

17.3

7 + 04

18.3

+ 20

20.2

~~£~~

7.5

11.2

5.8

11.2

12.8

13.3

13.8

12.7

10.9

sta + π - Elev

931.12

7 + 51

22.9

8 + 82

25.8

8 + 09

28.1

+ 27

25.9

+ 52

23.0

+ 74

19.9

+ 82

18.9

9 + 19

18.5

+ 40

Edge of Swamp

18.0

$\neq$

8.2

5.3

3.0

5.2

8.1

10.2

11.2

12.6

13.1

sta + π - Eleo

931.12

9+73

17.5

T.P. 8.94 928.84 11.22 919.90

+75

ditch

15.1

+79

17.3

10

18.4

+26

19.0

+63

19.3

+82

begin ditch

19.1

11

20.0

+50

21.3

$\frac{1}{2}$

13.6

Sta. 8+82

13.8

11.6

10.5

9.8

9.5

9.7

8.8

7.5

sta	+	$\bar{A}$	-	Elev
		928.84		
12			6.9	21.9
+50			6.3	22.5
13			5.9	22.9
+50			4.9	23.9
14			3.8	25.0
T.P.	13.60	938.62	3.82	925.02
+50			12.7	25.9
15			10.4	28.2
+50			8.6	30.0
16			8.4	30.2
B.M.			3.78	934.84
				935.34

£

30

spk. in 12" willow 75' R4 sta 16+25

Sta	+	Δ	-	Elev
-----	---	----------	---	------

939.02
938.62

16+50

7.1

31.5

17

6.0

32.6

+29

4.6

34.0

+64

1.0

37.6

T. P.	13.35	951.22	0.75	937.87
-------	-------	--------	------	--------

18

12.6

38.6

+44

9.9

41.3

+85

6.4

44.8

19

3.8

47.6

+13

2.7

48.5

~~E~~

Sta	+	π	-	Elev.
		951.22		
19+23			1.0	50.2
T.P.	13.36	963.65	0.93	950.29
+44			12.9	507
+75			11.3	523
20			8.7	54.9
+14			7.3	56.3
+26			4.8	58.8
+51			1.0	62.6
T.P.	12.67	976.04	0.28	963.37
21			7.5	69.5
+50			4.6	72.4

\$

35

Sta	+	π	-	Elev.
-----	---	-------	---	-------

976.04

21+81			3.2	72.8
-------	--	--	-----	------

22			2.1	73.9
----	--	--	-----	------

+35			0.9	75.1
-----	--	--	-----	------

T. P.	12.95	988.54	0.45	975.59
-------	-------	--------	------	--------

+64			12.1	76.4
-----	--	--	------	------

23			10.2	78.3
----	--	--	------	------

+50			8.3	80.2
-----	--	--	-----	------

24			6.2	82.3
----	--	--	-----	------

+50			4.5	84.0
-----	--	--	-----	------

25			2.7	85.8
----	--	--	-----	------

£

Sta	+	π	-	Elev
		988.54		
25+50			1.6	86.9
+82			1.4	87.1
T.P.	13.63	999.92	2.25	986.29
26			12.8	87.1
+50			12.8	87.1
27			12.5	87.4
+28			13.0	86.9
+32			14.8	85.8
+74			16.9	83.0
28			16.1	83.8

L+

±

34

ground 3.6 at Ho. 5 to 25+50 ± S.W. Cor.

Sta	+	Δ	-	Elev
-----	---	----------	---	------

999.92

28+50

15.2

84.7

29

13.0

86.9

+50

8.2

91.7

30

3.7

96.2

+38

1.9

98.0

+73

2.2

97.7

31

2.9

92.0

+50

4.9

95.0

32

6.9

93.0

~~E~~

Sta	+	T	-	E/cu
-----	---	---	---	------

999.92

32+50

8.4

91.5

33

9.0

90.9

+50

9.7

90.2

34

10.0

89.9

T. P.

12.31

1002.23

ok.
10.00

989.92

B. M

5.10

997.13

997.50

997.10

+50

13.0

88.2

35

13.5

88.7

+50

13.5

88.7

36

13.3

88.9

+50

13.0

89.2

£

36

(old Rd. Sta.)
N.E. cor Conc. Garage Apron 33+05±

Sta	+	π	-	Elev.
		1002.23		
37+00			12.3	89.9
+51			10.9	91.3
38			9.5	92.7
+50			7.2	95.0
+88			4.2	98.0
+93			2.9	99.3
39			2.8	99.5
+45			1.7	00.5
T. P.	12.67	1014.49	0.43	1001.80
40			6.9	07.6

~~4~~

Sta	+	Δ	-	Elev
-----	---	----------	---	------

		1014.47		
--	--	---------	--	--

40 + 31		1014.47	3.7	108
---------	--	---------	-----	-----

+ 45			4.7	098
------	--	--	-----	-----

+ 63			7.4	071
------	--	--	-----	-----

41			6.3	082
----	--	--	-----	-----

+ 50			5.0	095
------	--	--	-----	-----

42			4.0	105
----	--	--	-----	-----

+ 50			2.5	120
------	--	--	-----	-----

43			0.8	137
----	--	--	-----	-----

T. P.	12.93	1024.82	2.58	1011.89
-------	-------	---------	------	---------

+ 50			10.4	144
------	--	--	------	-----

£

38

sta	+	π	-	Elev
-----	---	-------	---	------

		1024.82		
--	--	---------	--	--

44+00				
-------	--	--	--	--

			9.1	
--	--	--	-----	--

				15.7
--	--	--	--	------

+50				
-----	--	--	--	--

			7.8	
--	--	--	-----	--

				17.0
--	--	--	--	------

45				
----	--	--	--	--

			6.6	
--	--	--	-----	--

				18.2
--	--	--	--	------

+50				
-----	--	--	--	--

			5.7	
--	--	--	-----	--

				19.1
--	--	--	--	------

46				
----	--	--	--	--

			4.8	
--	--	--	-----	--

				20.0
--	--	--	--	------

+50				
-----	--	--	--	--

			3.7	
--	--	--	-----	--

				21.1
--	--	--	--	------

47				
----	--	--	--	--

			2.7	
--	--	--	-----	--

				22.1
--	--	--	--	------

+50				
-----	--	--	--	--

			1.6	
--	--	--	-----	--

				23.2
--	--	--	--	------

48				
----	--	--	--	--

			0.6	
--	--	--	-----	--

				24.2
--	--	--	--	------

T.P.				
------	--	--	--	--

	9.66			
--	------	--	--	--

		1032.60		
--	--	---------	--	--

			1.88	
--	--	--	------	--

				1022.94
--	--	--	--	---------

~~4~~

Sta	+	T	-	Elev
-----	---	---	---	------

1032.60

48 + 50

9.0 23.6

49

8.1 24.5

+ 50

7.1 25.5

50

6.0 26.6

+ 50

5.0 27.6

51

4.0 28.6

+ 50

2.9 29.7

52

1.9 30.7

+ 50

1.2 31.4

£

40

sta	+	Δ	-	Elev
-----	---	----------	---	------

1032.60

53+00			0.6	32.0
-------	--	--	-----	------

T. P.	6.70	1038.89	0.41	1032.19
-------	------	---------	------	---------

+50			6.4	32.5
-----	--	--	-----	------

54			5.9	33.0
----	--	--	-----	------

+50			5.4	33.5
-----	--	--	-----	------

55			4.9	34.0
----	--	--	-----	------

+50			4.2	34.7
-----	--	--	-----	------

56			3.5	35.5
----	--	--	-----	------

+28			3.6	35.3
-----	--	--	-----	------

B 11			3.11	1035.78
------	--	--	------	---------

1036.22

~~4~~

41

Approx. ~~2~~ Century Ave.

Nail in R.P. N.W. Cor. Lower Alton Rd
at Century Ave

sta + π - Eleo

PA
RG
JH

October 6, 1959
Fog 49°

2

Bench Levels

Lower Afton Rd.

LINE REVISION

Raise Elevations 0.40'
to conform to M.H.D.
datum. Use elevations
as shown by red figures.
for all future work.

Sta	+	π	-	Elev
BM	10.84 ⁵	887.305		876.86 (876.46)
Sta 21+00			9.65	
Sta 20			2.83	
TP	13.57	900.765	0.11	887.195
Sta 19			9.36	
BM			1.67	
Sta 18			4.1	
TP	13.38	913.59	0.55 ⁵	900.21
Sta 17			8.56	
TP Sta 16	10.38	922.26	1.71	911.88
BM			5.10	
Sta 15			3.36	
TP	13.52 ⁵	935.035	0.75	921.51
Sta 14			10.5	
Sta 13			2.79	
TP	13.685	948.34	0.38	934.655
Sta 12			9.7	
Sta 11			3.7	
TP	13.555	961.575	0.32	948.02

KG
KJ

October 9, 1959
cold 33° Windy

6

Top S.E. Cor Lower Step Ho #2081 Lower Afton Rd

Rock

Top SE Cor lower step Ho #2169 Lower Afton Rd
in ditch

Rock

£

Top SE cor lower step Ho #2185 Lower Afton Rd

Rock

in Ditch

Rock

in ditch

in ditch

Rock

Sta	+	π	-	Elev
		961.575		
BM			5.63	
Sta 10			8.26	
BM			4.75	
BM			0.59	
Sta 9			3.27	
TP	7.795	968.64	0.73	960.845
Sta 8			6.90	
Sta 7			5.75	
Sta 6			5.22	
Sta 5			4.93	
BM			6.72	
Sta 4			3.92	
Sta 3			3.48	
TP				
Sta 2	5.405	971.165	2.88	965.76
Sta 1			5.11	
TP	6.63	972.39		965.76
BM			0.42	971.99
				972.40
				972.00

R6
KJ

Oct 9, 1959

C

Top NE Cor lower Step Ho #2194 Lower Afton Rd

Top SE Cor lower Step Ho #2201 Lower Afton Rd

NW Cor Conc Apron Ho #2200 Lower Afton Rd

Rock

Top SW Cor Lower Step Ho #2217 Lower Afton Rd

±

Sta 2 ±

Top NW Cor Lower Step Ho #366 McKnight Rd.

Sta	+	π	-	Elev
BM	0.05	972.05		972.00 972.00
57+00 Sta 1			5.35	
58+00 Sta 2			4.47	
59+00 TP Sta 3	8.48	976.86	3.67	968.38
60+00 Sta 4			7.48	974.59?
BM			2.67	974.19 974.49
61+00 Sta 5			6.65	
62+00 Sta 6			5.67	
63+00 Sta 7			5.08	
64+00 Sta 8			5.40	
65+00 TP Sta 9	3.15	974.28	5.73	971.13
66+00 Sta 10			3.94	
67+00 Sta 11			5.40	
68+00 Sta 12			7.12	
69+00 Sta 13			8.09	
70+00 TP Sta 14	13.53	979.58	8.23	966.05
71+00 Sta 15			12.51	
72+00 Sta 16			9.95	
73+00 Sta 17			6.55	

R6
KT

Oct 13, 1959
40°, Cloudy

d

Top NW cor Lower Step Ho #366 McKnight Rd

£

Top SE cor Lower Step Ho #2299 Lower Aston Rd

Sta	+	π	-	Elev
		979.58		
74+00 Sta 18			2.72	
TP	12.40	991.58	0.40	979.18
75+00 Sta 19			11.00	
BM			1.91	989.67 (990.07)
76+00 Sta 20			7.51	
77+00 Sta 21			4.32	
78+00 Sta 22			1.38	
TP	8.43	1000.01	0.00	991.58
79+00 Sta 23			8.02	
80+00 Sta 24			6.63	
81+00 Sta 25			5.56	
82+00 Sta 26			4.94	
83+00 Sta 27			4.31	
84+00 Sta 28			3.89	
85+00 Sta 29			3.32	
TP 86+00				
Sta 30	5.27	1002.63	2.65	997.36
87+00 Sta 31			4.45	
88+00 Sta 32			4.20	

RG
KJ

Oct 13, 1959
Cloudy 40°

e

Rock

Top NE Cor Porch Ho# 2450 Lower Atton Rd

pavement

Sta	+	π	-	Elev
		1002.63		
89+00 Sta 33			4.62	
BM			5.53	997.10 <u>997.50</u>
90+00 Sta 34			4.03	
91+00 Sta 35			3.51	
92+00 Sta 36			2.76	
93+00 TP Sta 37	13.63	1014.76	1.50	1001.13
94+00 Sta 38			12.12	
95+00 Sta 39			9.87	
96+00 Sta 40			7.45	
97+00 Sta 41			5.00	
TP 98+00 Sta 42	12.80	1025.82	1.74	1013.02
99+00 Sta 43			10.34	
100+00 Sta 44			8.18	
101+00 Sta 45			6.24	
102+00 Sta 46			4.15	
103+00 Sta 47			2.22	
104+00 +P Sta 48	11.75	1037.28	0.29	1025.53
105+00 Sta 49			9.64	

RG
KJ

13 Oct, 1959
40° Cloudy

f

NE Cor Gar Conc Apron Rt Sta 33+05±

4

5

6

Sta + π - Elev

1037.28

~~106+00~~

~~Sta 50~~

7.59

~~107+00~~

~~Sta 51~~

5.85

~~108+00~~

~~Sta 52~~

4.54

~~109+00~~

~~Sta 53~~

3.53

~~110+00~~

~~Sta 54~~

2.32

BM

0.42

1035.82

1036.86

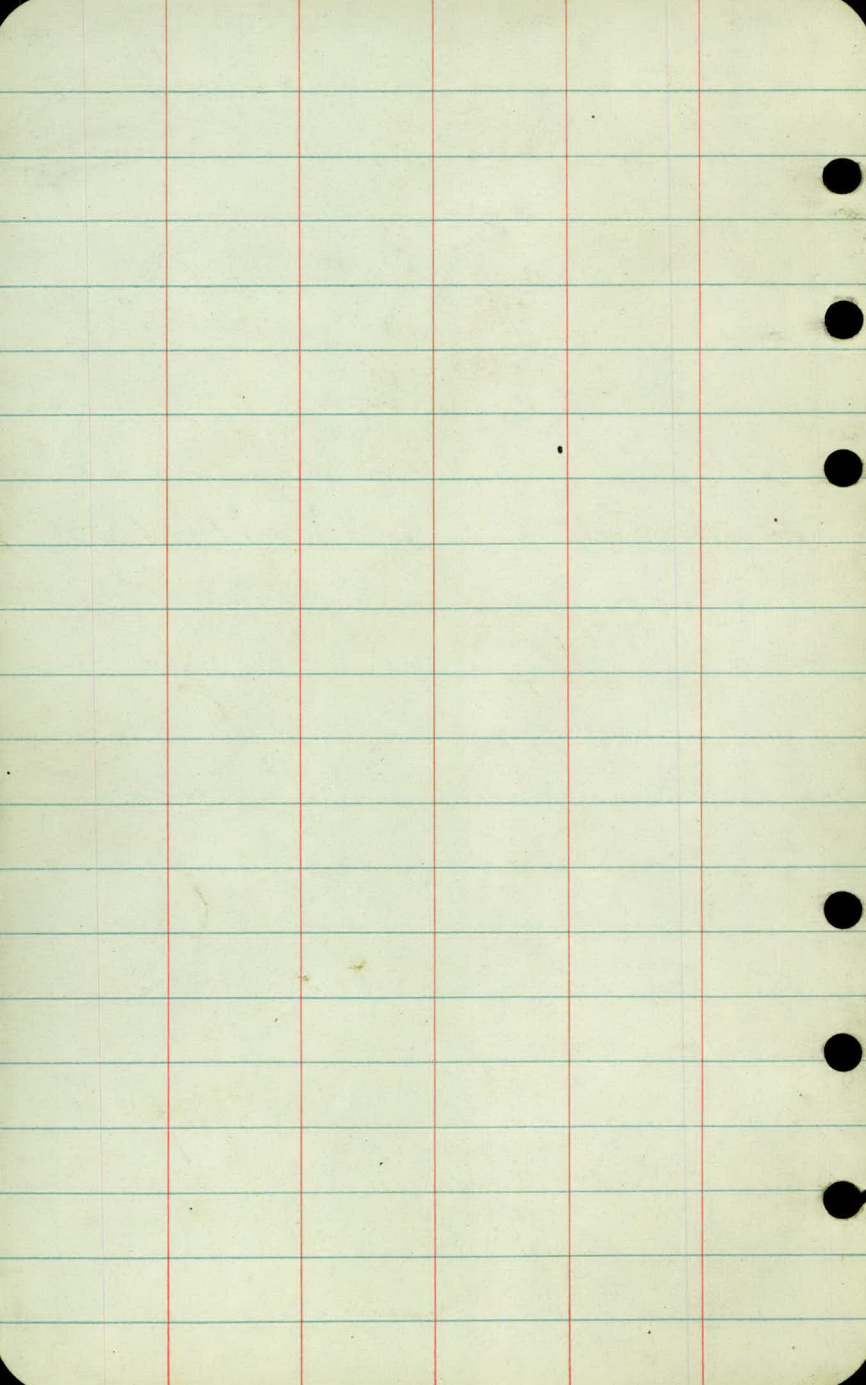
1036.22

KG
KJ

OCT 13, 1959
40° Cloudy

9

Spike in PP NW Cor Hwy 100 + Lower Afton Rd



Lower Afton

S.H.#61 to SH#100

OBJECT/
object

AZ.

STADIA

π at sta 90+00 55°00'
to sta 96+00

Shore line

118°-

1'

148°35'

1'

162°-

1'

160°15'

1'

149°-

1'

138°-

1'

126°-

1'

115°50'

1'

108°30'

1'

100°15'

1'

93°30'

1'

88°20'

1'

82°15'

1'

77°-

1'

73°-

1'

68°30'

FX
RB
DS

Jan. 2, 1962

DIST.

VERT.
ANGLE

ROD
EQUIV.

ROD

DIFF.

6
ELEV.

120 ✓

142 ✓

179

223

253

270

273

284

320

338

379

406

445

483

513

537

OBJECT

AZ.

STADIA

Shore Line

 $62^{\circ}50'$

"

 $57^{\circ}20'$

Sta. 96+00

 $55^{\circ}00'$

Shore Line

 $53^{\circ}30'$

"

 $48^{\circ}20'$

"

 $42^{\circ}-$

"

 $35^{\circ}40'$

"

 $29^{\circ}10'$

"

 $21^{\circ}45'$

"

 $15^{\circ}25'$

"

 $8^{\circ}10'$

"

 $6^{\circ}20'$

"

 $5^{\circ}45'$

"

 $19^{\circ}30'$

"

 $44^{\circ}-$

"

 $78^{\circ}-$

"

 $101^{\circ}-$

"

Jan 2, 1962

c

DIST.

VERT.
ANGLEROD
EQUIV.

ROD

DIFF.

ELEV:

543

539

600

500

463

434

514

400

379

353

306

250

190

142

116

108

107

OBJECT

AZ.

STADIA

Profile

50' Lt & Rt

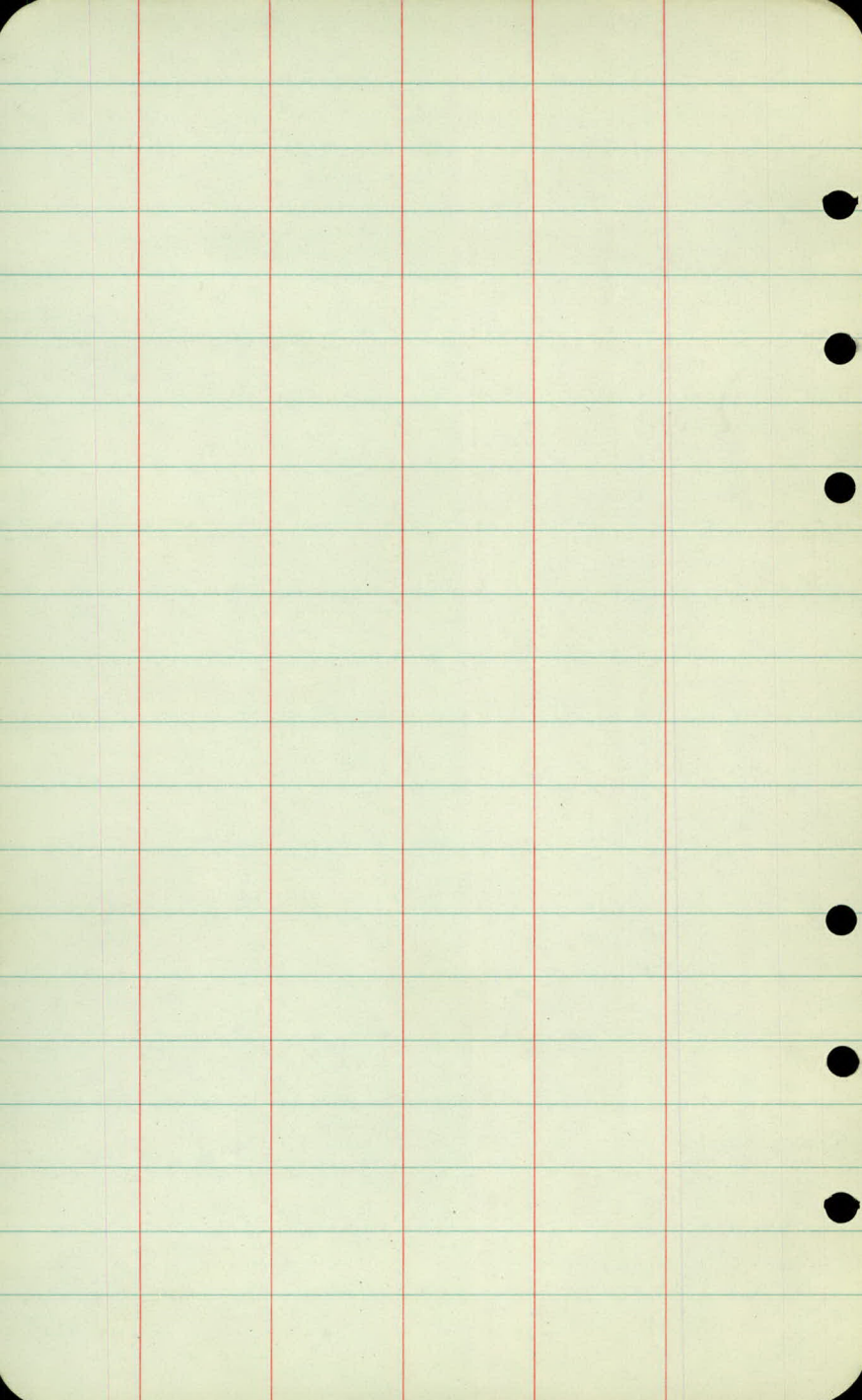
Sta 63 to Sta 65

Sta	+	Σ	-	Elev.	
63 $\pm$	8.24	923.24 ^{923.3}	50' Lt		915.1 ✓
63			9.5	13.8 13.7	
+20			10.7	12.6	
+29			13.1	10.2	
+33			14.6	08.7	
+41			11.2	12.1 12.0	
+50			8.7	14.6 14.5	
+62			2.4	20.9	
+83			1.3	22.0 21.9	
64			+0.2	23.5 23.4	5.4 1.0
64 $\pm$			8.3	914.94 ✓	4.4 = 3 15.0 8.3 23.3
64			50' Rt 5.4	17.9 17.8	
+17			6.7	16.6	
+30			7.6	15.7	
+35			11.5	11.8	
+41			10.0	13.3 13.2	
+61			10.3	13.0	
+66			7.6	15.7	
+76			7.8	15.5	
65			5.4	17.8	23.30
65 $\pm$			+2.1	925.44 ✓	25.40

Jan 2, 1962

LT

RT



April 4, 1962

1

Lower Afton Rd
Swamp $\frac{1}{2}$ Creek Elevations

Sta 66+00

2 pages

Sta	+	T	-	Elev
TBM	6.1	31.5		925.4
W.S.			10.9	920.6
G.E.			10.5	921.0
W.S.			11.7	919.8
G.E.			12.5	919.0
W.S.			14.2	917.3
W.S.			16.2	915.3
GE			+0.1	931.6 931.8

R6
WM
RB
WS

April 4, 1962
cloudy 35°

2

Ground - Sta 65+00

Creek thru swamp opposite Sta 68+

Swamp

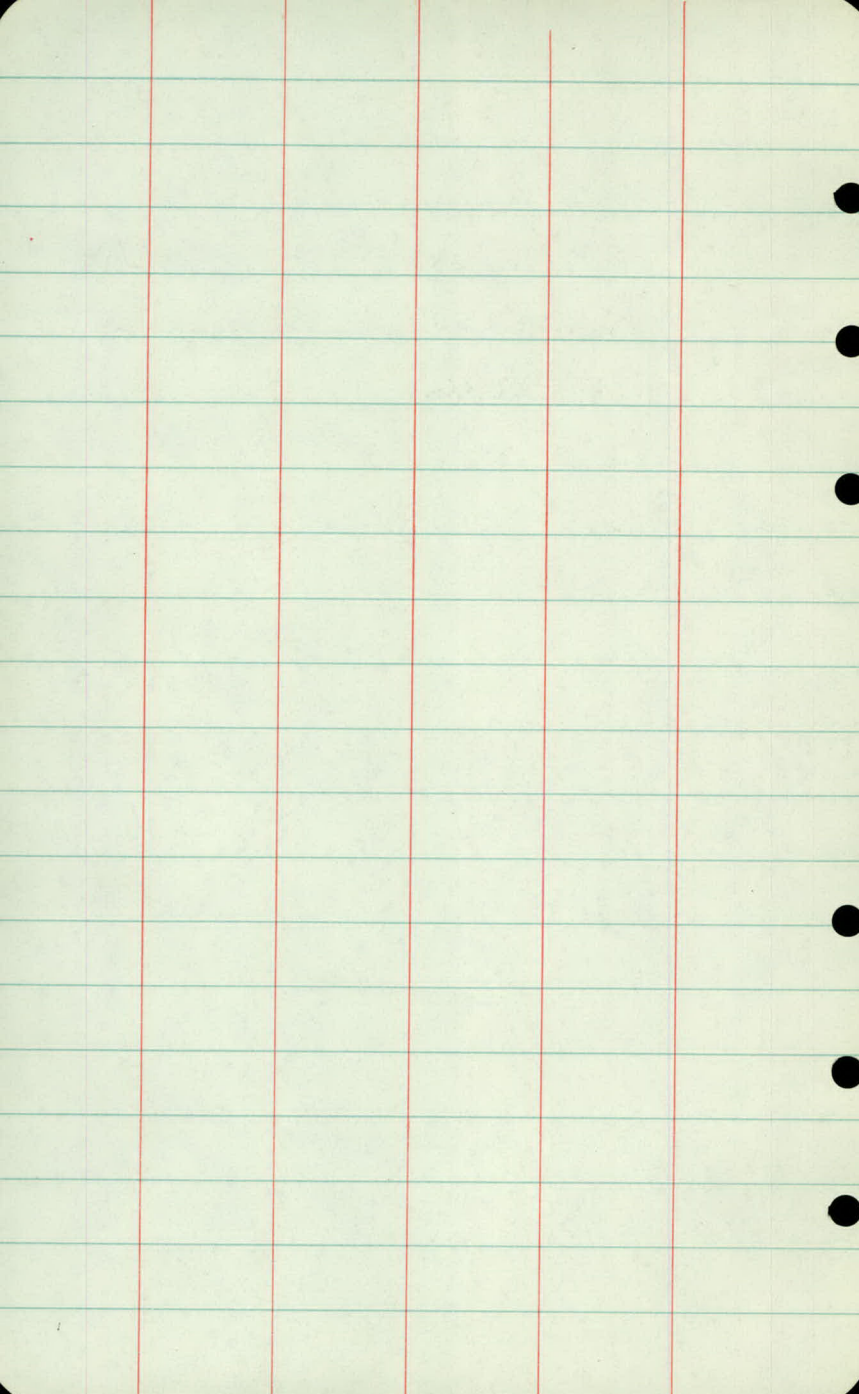
Creek
opposite 67+50±

" 67+00

Creek " "

Creek outlet edge of swamp opposite Sta 66+

Sta 62+00



R6
LB
WS

April 30, 1962
Cl. 45°

1

Lower Afton Rd

Bench Levels

Sta 83 to E. Co. Line.

Sta	+	-	-	Elev.	
BM ₁	11.20	994.77			983.57
TP ₁	10.59	1004.35	1.01	993.76	
BM ₂	5.65	1003.22	6.78	997.57	X
BM ₃	12.03	1013.69	1.56	1001.66	
BM ₄	10.48	1022.54	1.63	1012.06	
TP ₂	7.50	1029.28	0.76	1021.78	
BM ₅	10.06	1036.33	3.01	1026.27	
TP ₃	5.06	1039.53	1.86	1034.47	
BM ₆	3.87	1040.13	3.27	1036.26	
BM ₇	76.44 27.68 52.76		2.80	1037.33	X
BM ₇	2.92	1040.25	check 22.68	983.57 52.76	1037.33
TP ₃	1.42	1035.89	5.78	1034.47	(1034.47)
BM ₅	1.55	1027.82	9.62	1026.27	(1026.27)
TP ₄	1.46	1020.02	9.26	1018.56	
BM ₄	1.61	1013.67	7.96	1012.06	(1012.06)
BM ₃	2.22	1003.87	12.02	1001.65	(1001.66)
BM ₂	1.58	999.14	6.31	997.56	(997.57)
TP ₅	4.05	990.73	12.46	986.68	
BM ₁	16.87		7.17 10.58	983.56	(983.57)

RG
LBT
WS

April 30, 1962
May 1, 1962
Clear, 50°

2

Spike in 24" Oak 88' Rt Sta 83+07

rock

Rt. Sta 93±

Top NE Cor. conc. Garage Ent. Apron So. side L. Atton Rd

Spike in Fe Post So. side L. Atton Rd Rt Sta 97±

Spike in Guy Pole Rt Sta 100+50±

nail in ground

iron by stump Rt Sta 107

PK nail & sta 112

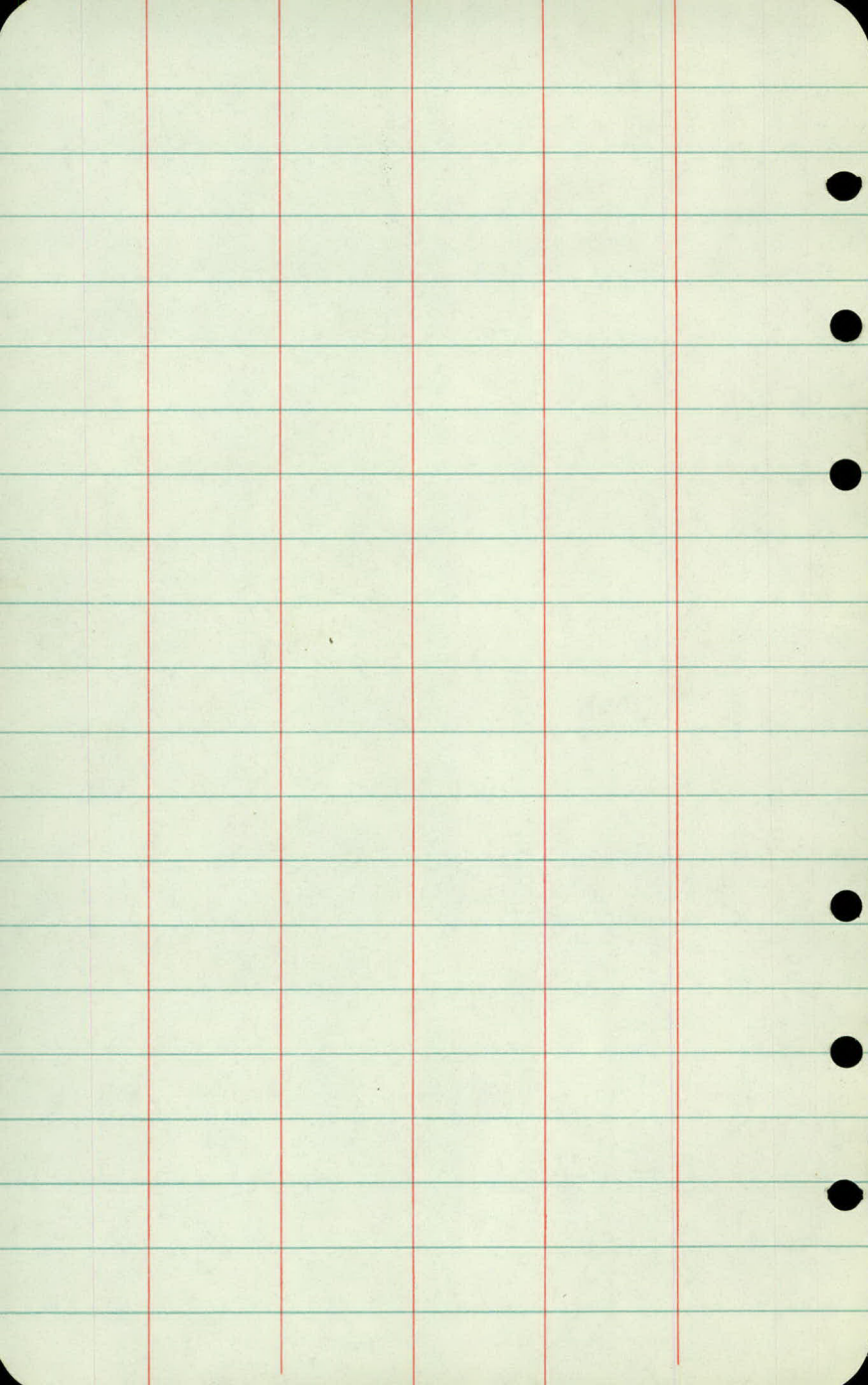
yellow spike in PP NW Cor Hwy 100 & Lower Atton Rd.

spike in PP NE Int. Hwy 100 & Wash Co. Rd. #26

PK nail & sta 103

rock

1037.33	70.58
983.56	16.81
53.77	53.77
OK	

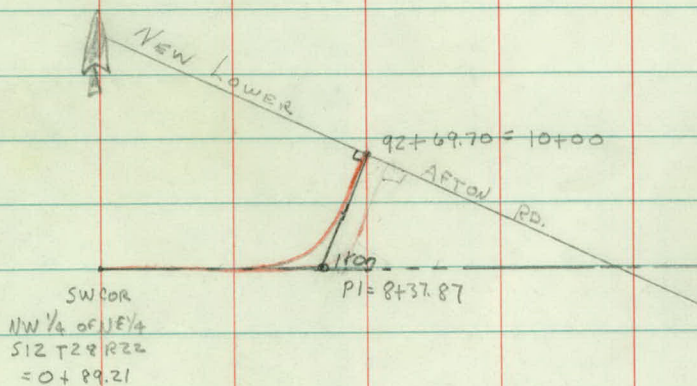


KP
FS
TB
DS

13 APRIL 1962

LOWER AFTON RD PT. DOUGLAS RD TO STH#100

CONNECTION ALIGNMENT



REC. 4/16/62
K.J.

STA POINT ΔL ΔR CURVE

DATA

$+ 71.70$
10+00 = STA 92+69.70 LOWER AFTON RD.

$+ 90.37$
8+88.06 PT

$\Delta 57^{\circ}41.5'$

D 51.9

T 60.59

$+ 40.23$
8+37.87 PI $57^{\circ}41.5'$

L 110.73

R 110.00

79.64
7+77.28 PC

28.25
5+25.89 P.O.T.

91.57
0+89.21 P.O.T = SW Cor of NW $\frac{1}{4}$ of NE $\frac{1}{4}$ S 12-28-22

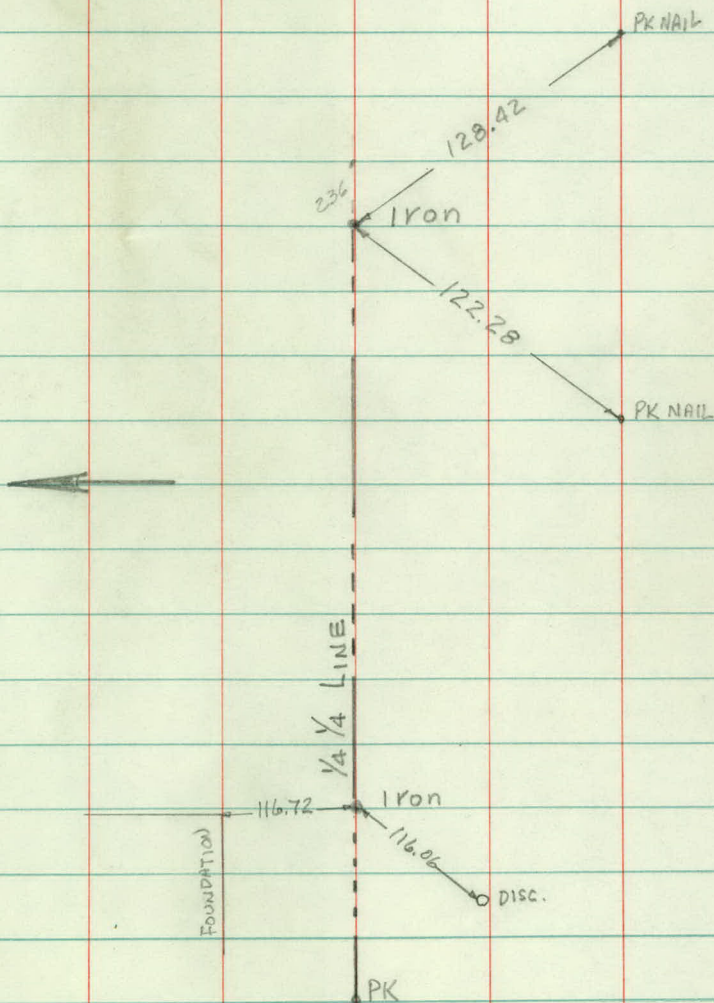
0+00

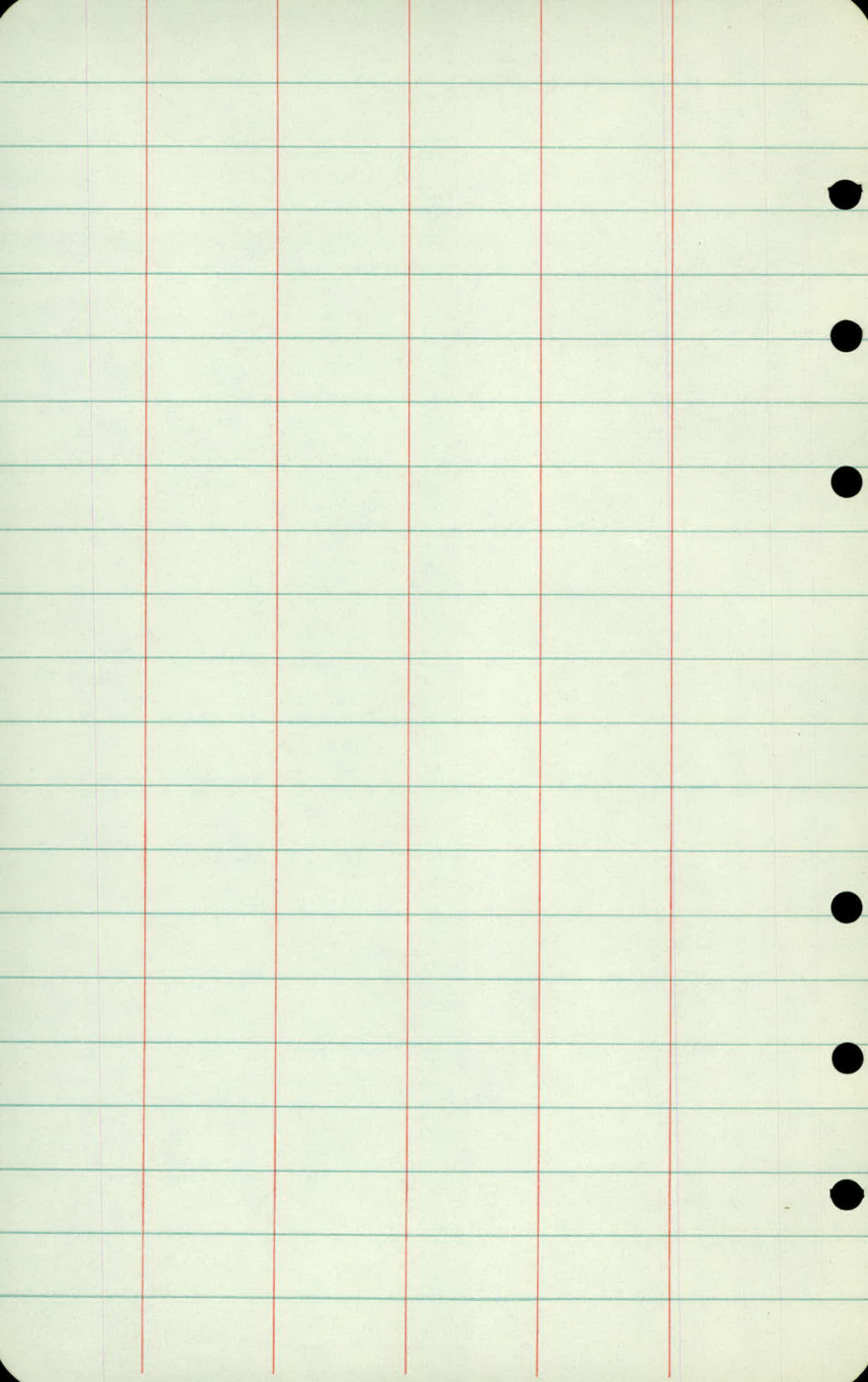
13 APRIL 1962

LT

E

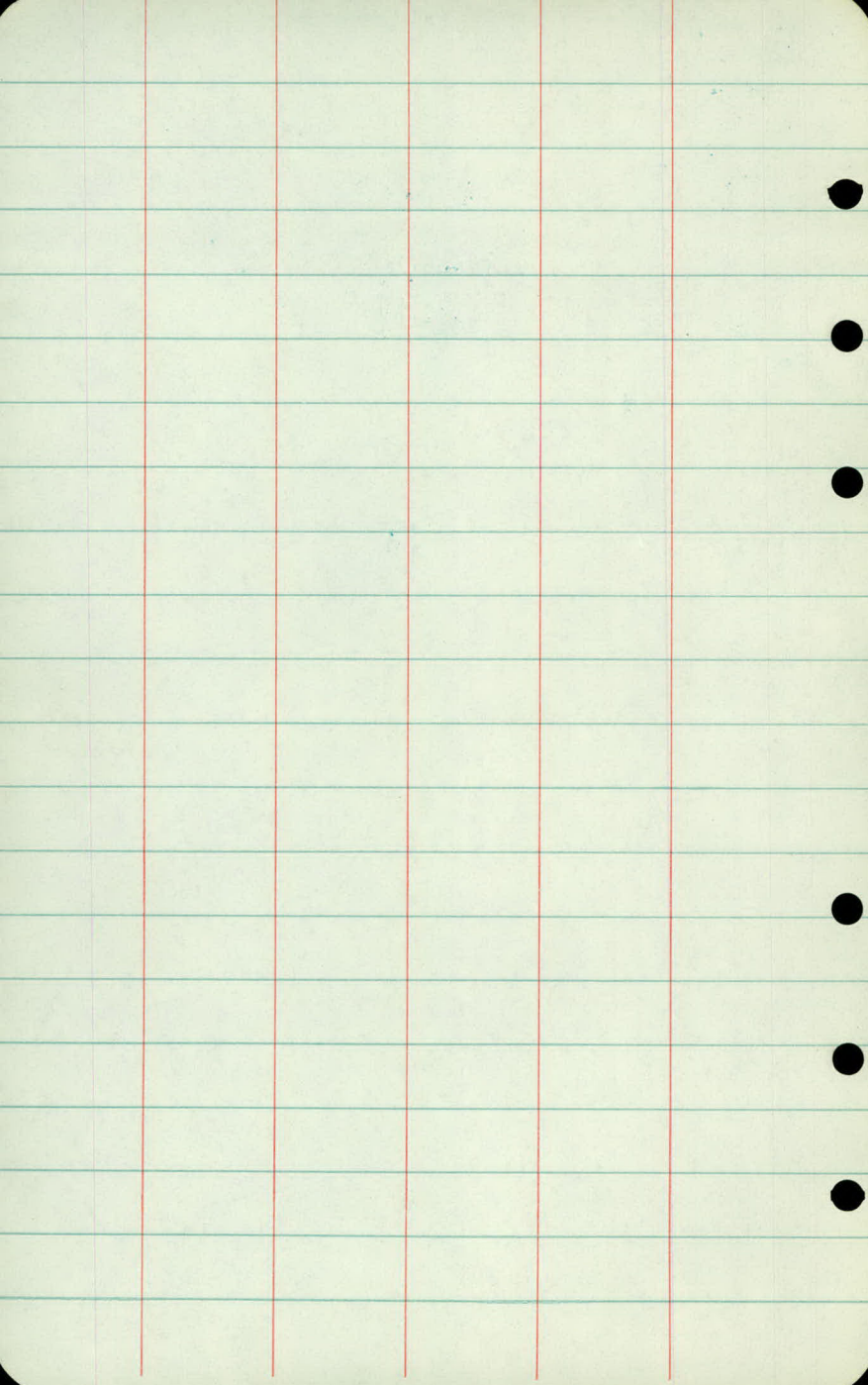
RT





LOWER AFTON RD
PT DOUGLAS RD TO S.T.H. #100

X- SECTIONS



KP
WM
WS

16 APRIL 1962

LOWER AFTON RD

PT. DOUGLAS RD TO STH #100

CONNECTION

X-SECTIONS

STA	+	+	-	ELEV.
BM	1.30	1037.52		1036.22
	0.91	1028.86	9.57	1027.95
	4.38	1021.53	11.70	1017.16
			5.64	1015.89
	0.00	1007.92	13.61	1007.92
	4.93	1003.15	9.70	998.22
			6.53	996.62

16 APRIL 1962

LT

E

RT

SPIKE IN P.D. NW. COR LOWER AFTON RD; "100

TOP ROCK AT OLD WORKHOUSE FARM ENTRANCE

SPIKE IN P.D. LT STA 102+35

SPIKE IN 30" OAK 47' LT STA 99+65

MARK ON RD

SPIKE IN ROOT 20" O 33' S. Culvert by Gray GABLE AFTON RD ^{on Lower}

SPIKE IN FE POST 25' O LT of SW COR of NW 1/4 of NE 1/4

STA	+	π	-	Elev
-----	---	-------	---	------

BM	4.14	1000.76		
----	------	---------	--	--

				996.62
--	--	--	--	--------

0+00				
------	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

+58				
-----	--	--	--	--

			6.21	
--	--	--	------	--

				94.55
--	--	--	--	-------

+65				
-----	--	--	--	--

			5.82	
--	--	--	------	--

				94.94
--	--	--	--	-------

16 APRIL 1962

LT

E

RT

SPIKE IN FE POST 25.0. LT $\frac{1}{4}$ $\frac{1}{4}$ Cor

95.6	93.3	94.8	94.9	95.4	95.3	94.9	94.0	96.1	95.4
5.2	7.5	6.2	5.9	5.4	5.5	5.9	6.8	4.7	5.4
28	20-22 DITCH	15	11 BT	BT	11 BT	15	21-23 DITCH	28	48

95.0
5.8
44

94.8
6.0
60

94.5
6.3
60

✓

95.5	95.0	93.9	95.0	95.1	95.8	95.9	95.4	94.4	76.0	95.6
5.3	5.8	6.9	5.8	5.7	5.2	5.1	5.6	6.6	4.8	5.2
43	26	19-21	16	11 BT	BT	10 BT	17	22-24 DITCH	28	48

95.6
5.2
60

95.8
5.2
60

✓

TOP 12" CM 21.0 LT

TOP 15" CM 22.0 RT

STA	+	π	-	ELEV
-----	---	-------	---	------

		1000.76		
--	--	---------	--	--

0+78				
------	--	--	--	--

0+85				
------	--	--	--	--

			5.71	
--	--	--	------	--

				95.05
--	--	--	--	-------

1+00				
------	--	--	--	--

✓				
---	--	--	--	--

1+50				
------	--	--	--	--

✓				
---	--	--	--	--

2+00				
------	--	--	--	--

16 APRIL 1962

LT

E

RT

TOP 15" CM 22.0 RT

96.2

4.6

27

Fe

96.2

4.6

25

Fe

95.1

5.7

19

Fe

95.1

5.7

15

Fe

95.7

5.1

10

BT

96.1

4.7

BT

96.0

4.8

12

BT

95.4

5.4

16

Fe

94.8

6.0

21-23

DITCH

95.5

5.3

26

Fe

95.9

4.9

52

95.7

5.1

60

95.4

5.4

60

95.6

5.2

49

94.9

5.9

44

Fe

96.2

4.6

26

Fe

94.4

6.4

18-20

DITCH

95.5

5.3

14

Fe

95.8

5.0

10

BT

96.2

4.6

BT

96.0

4.8

12

BT

94.9

5.9

19

Fe

94.2

6.4

24-25

DITCH

94.4

6.4

26

Fe

94.6

6.2

38

Fe

94.3

6.5

60

94.0

6.8

60

90.5

10.3

60

93.1

7.7

38

94.6

6.2

24

Fe

94.0

6.8

19-21

DITCH

95.3

5.5

16

Fe

96.0

4.8

8

BT

96.4

4.4

BT

96.0

4.8

13

BT

94.9

5.9

22

Fe

94.3

6.5

27

Fe

93.3

7.5

41

Fe

92.5

8.3

60

Sfa	+	π	-	Elev
		1000.76		
2+50				
3+00				
3+50				
4+00				
+50				
5+00				
TP	6.45	1002.07	5.14	995.62

16 APRIL 1962

Lt

E

Rt

88.3	89.8	92.5	95.8	96.3	96.7	96.3	95.4	94.2	93.6	93.6
12.5	11.0	8.3	5.0	4.5	4.1	4.5	5.4	6.6	7.2	7.2
60	45	24	15	8	BT	14	22	27	40	60
		Fe		BT	✓	BT		Fe		

88.8	91.2	93.1	95.7	96.4	96.8	96.4	95.4	95.3	96.3	97.6
12.0	9.6	7.7	5.1	4.4	4.0	4.4	5.4	5.5	4.5	3.2
60	31	21	17	7	BT	14	20	27	43	60
		Fe		BT	✓	BT		Fe		

90.9	91.1	93.9	96.3	97.0	97.3	96.7	96.0	95.4	95.7	96.0	96.5
9.9	9.7	6.9	4.5	3.8	3.5	4.1	4.8	5.4	5.1	4.8	4.3
60	45	19	15	6	BT	16	18	22	27	43	60
		Fe		BT	✓	BT			Fe		

95.2	93.9	94.8	97.3	97.5	97.6	96.9	95.5	95.8	95.2	94.6
5.6	6.9	6.0	3.5	3.3	3.2	3.9	5.3	5.0	5.6	6.2
60	31	18	13	4	BT	17	22-24	28	45	60
		Fe		BT	✓	BT	DITCH	Fe		

97.6	97.4	97.8	97.9	98.0	96.9	96.0	96.3	95.8
3.2	3.4	3.0	2.9	2.8	3.9	4.8	4.5	5.0
60	34	14	2	BT	20	29	43	60
		Fe	BT	✓	BT	Fe		

96.6	98.1	98.4	98.3	98.2	97.3	96.4	96.9	97.9
4.2	2.7	2.4	2.5	2.6	3.5	4.4	3.9	2.9
60	36	13	7	BT	24	32	37	60
		Fe		✓	BT		Fe	

Top NAVL & STA 6400

STA

+

 π

-

Elev.

1002.07

5+15

5.26

996.87

+39

5.07

997.0

5+50

✓

6+00

✓

16 APRIL 1962

LT

Z

RT

TOP 15' CM 38.0 RT

TOP 15' CM 41.0 RT

94.4	95.1	97.2	98.0	97.6	98.8	98.8	98.6	97.9	97.1	96.6	99.5
7.7	7.0	4.9	4.1	4.5	3.3	3.3	3.5	4.2	5.0	5.5	2.6
60	45	13	7	5		11	22	33	38	41-43	48
			Fe	DITCH		BT	BT	BT		DITCH	

✓

1000.0
2.1
60

92.9	92.9	94.4	95.7	95.6	96.1	98.5	98.9	98.8	98.1
9.2	9.2	7.7	6.4	6.5	6.0	3.6	3.2	3.3	4.0
60	52	19	1		6	15	25	35	47
			Fe				BT	BT	

✓

98.6	96.8	97.4
3.5	5.3	4.7
64	57-59	51
	DITCH	

STA

+

π

-

Elev

1002.07

6+50

✓

7+00

+50

+77.28

16 APRIL 1962

LT

✱

RT

92.5

9.6
60

92.4

9.7
52

92.9

9.2
34

94.0

8.1
12

94.9

7.2
Fe

95.6

6.5
10

97.7

4.4
25

97.0

5.1
31

98.2

3.9
34

99.0

3.1
45
BT

✓

98.8

3.3

67
BT

99.0

3.1

60
BT

99.1

3.0

54
BT

92.0

10.1
60

92.4

9.7
38

92.9

9.2
9

94.0

8.1
Fe

94.1

8.0
9

95.1

7.0
40

95.9

6.2
53

97.8

4.3
58

98.5

3.6
68

✓

91.0

11.1
60

90.8

11.3
40

91.8

10.3
16

92.3

9.8
Fe

92.6

9.5
13

93.3

8.8
39

94.0

8.1
56

94.1

8.0
60

✓

90.8

11.3
60

91.0

11.1
46

91.3

10.8
23

91.7

10.4
Fe

92.8

9.3
23

94.1

8.0
44

94.4

7.7
60

93.9

8.20
83

✓

TOP N. END

15" vit

93.8

8.24

126

FL SEND

15" vit

STA + π -

100207

8400

✓

+50

9400

+50

10400 = LOWER AFTON RD STA 92+69.70

BM

3.78

998.29 (998.22)

16 APRIL 1962

LT

✓

RT

89.9	89.9	90.3	90.9	90.8	91.0	91.2	92.6
12.2	12.2	11.8	11.2	11.3	11.1	10.9	9.5
60	41	20		2	9	22	47
				Fe			

✓

93.3
8.8
60

89.4	89.3	89.4	89.4	90.0	90.6	90.6
12.1	12.8	12.7	12.7	12.1	11.5	11.5
60	49	22		25	54	60
				Fe		

✓

89.1	88.7	88.7	88.6	88.8	88.9
13.0	13.4	13.4	13.5	13.3	13.2
60	45	17		32	60

✓

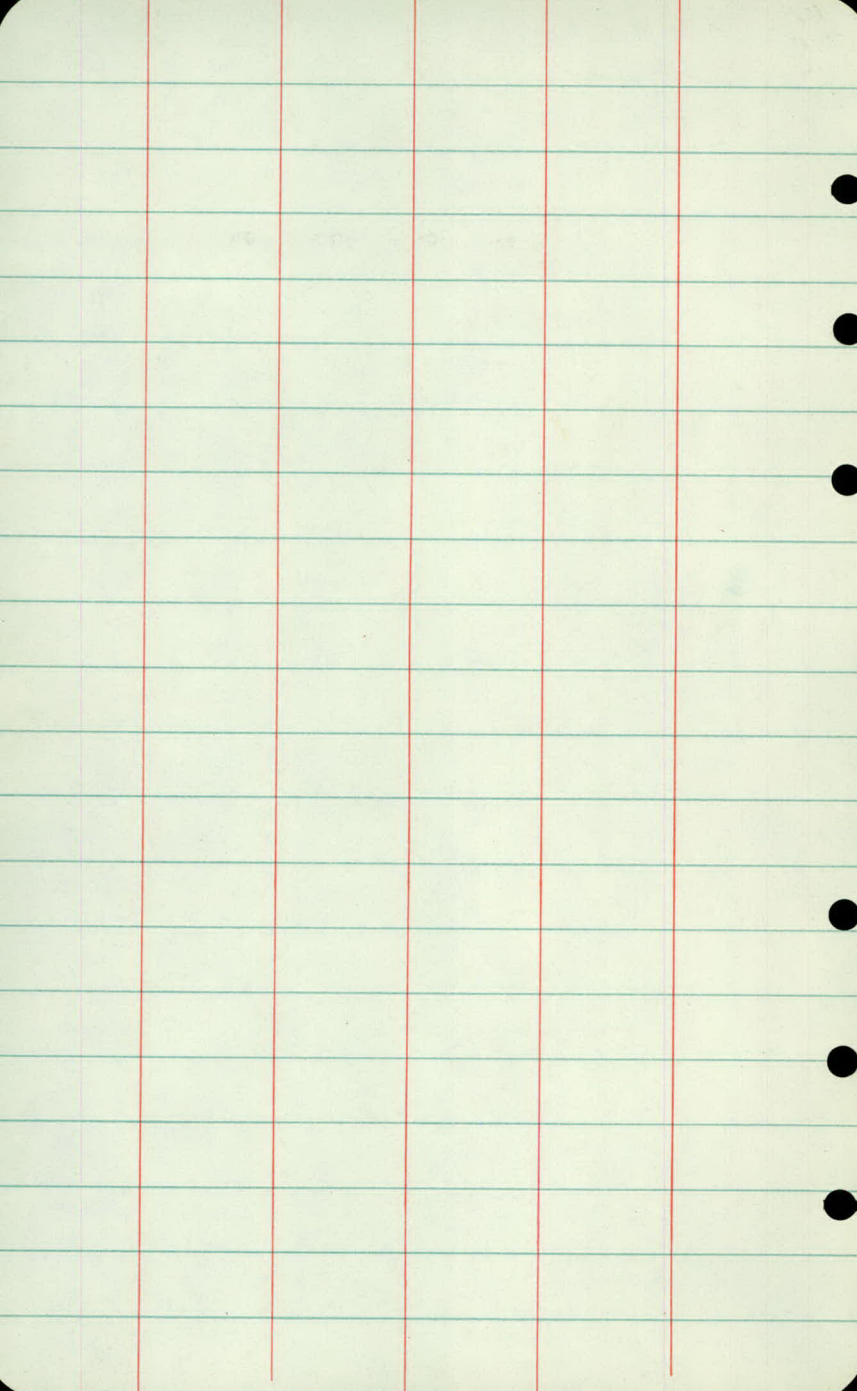
89.1	89.0	88.7	88.5	88.7	88.8	96.1
13.0	13.1	13.4	13.6	13.4	13.3	60
60	50	23		20	45	13.2

88.8

✓

13.3

SPIKE IN ROOT 20" 0 33' 0 5 Culvert



16 APRIL 1962

KP
WM
FS
LB
DS
WS

LOWER AFTON RD

CONNECTION
STA 92+69.70

TOPOGRAPHY

LT

~~E~~

RT

3+00

3+00

Fe
21

7

14

Fe
27

+ 86 PD
14 1/2

2+00

Fe
25

8

13

Fe
26 1/2

+ 49 TP
28

1+00

10

12.5

0+89.21 = 1/4 1/4 Cor

Fe Cor
26

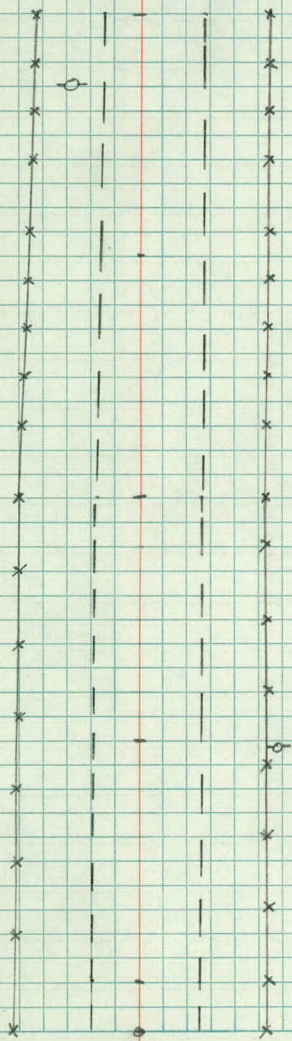
Fe Cor
26

16 APRIL 1962

LT

$\neq$

RT



LT

Z

RT

5+00

$$\frac{Fe}{12}$$

$$\frac{RD}{1-24}$$

$$\frac{Fe}{36}$$

$$+94 PP$$

$$39$$

4+00

$$\frac{Fe}{17}$$

4

17

$$\frac{Fe}{28}$$

$$+44 PP$$

$$29$$

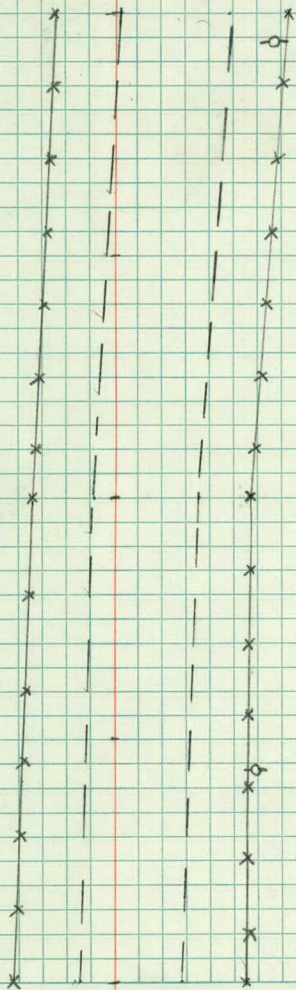
3+00

16 APRIL 1962

L7

E

RT



LT

±

RT

7+00

Fe RD
65-88

+50 RD
44-65

6+00

Fe
2

ROAD
26-47
+90 TP
1

Triple Elm
67

+33 30° ELM
51

+50 ROAD
12-34

+33 END 15° CM
40

+23 ± 6.0 DRIVE
28

+15 36° E
47

+14 W END 15° CM
34

+11 Fe Cor
38

+04 RT Fence

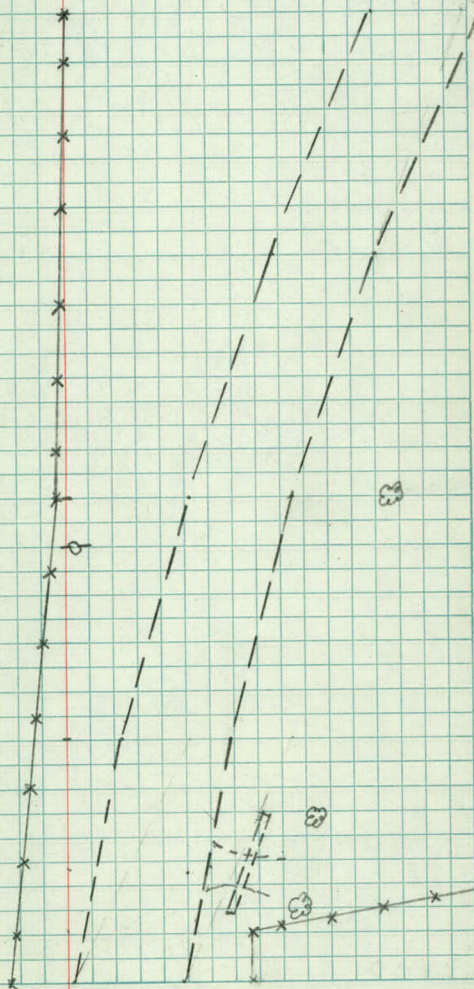
5+00

LT

$\neq$

16 APRIL 1962

RT



+50

LT

E

RT

9+00

Fe
110

+68 PP
51

+58 Fe
32

+33 Fe
15

8+00

Fe

+88 8" SE
13

+93 TW 10" SE
12

+83 QUAD 8" SE
62

+85 STR
15

+79 QUAD. APPLE

+77 NEW 15" (42')
83

+71 Fe line

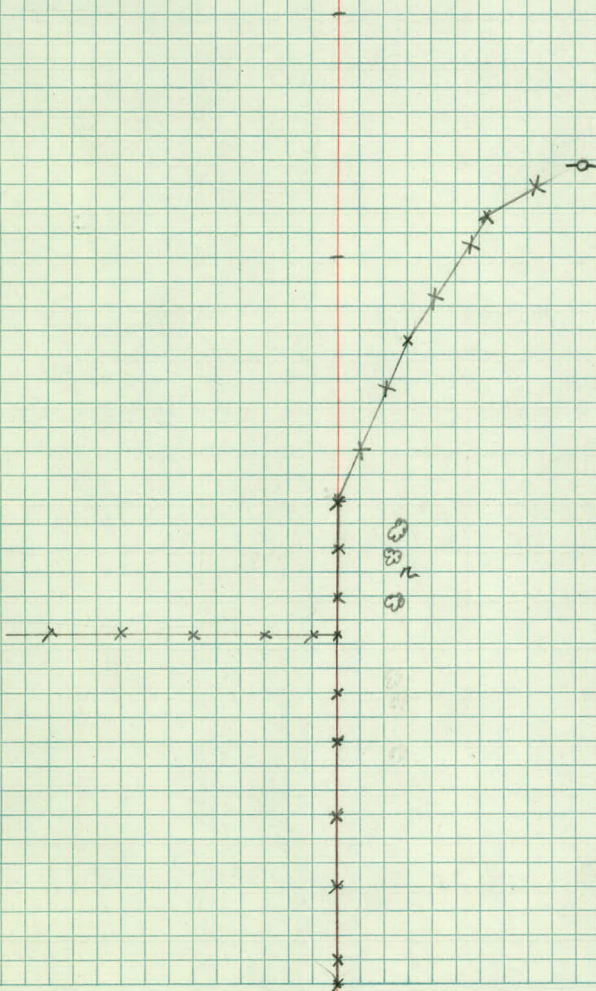
7+00

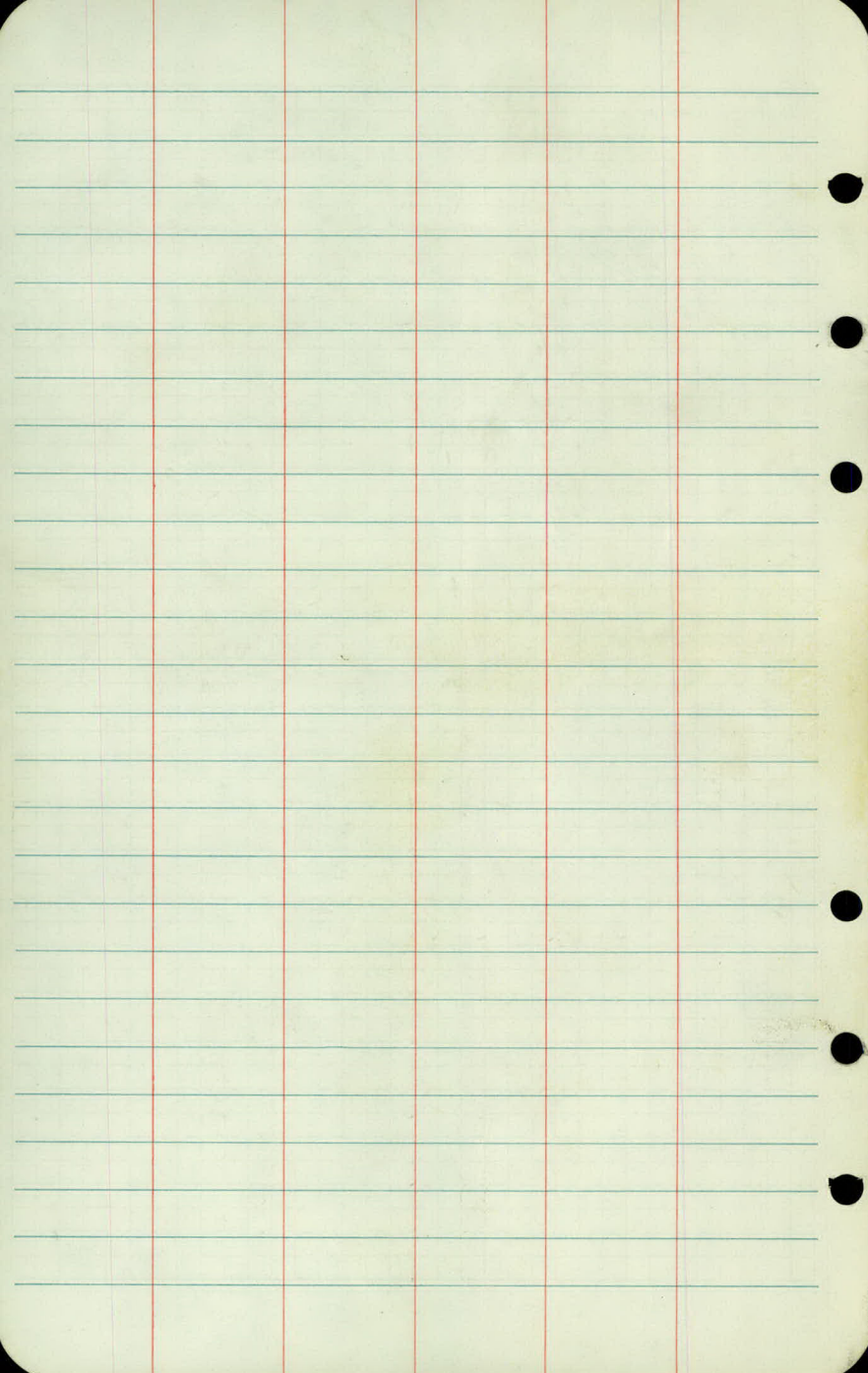
16 APRIL 1962

LT

E

RT





May 9, 1962

1

Drainage tile
Stadia

Lower Afton Rd.

HI 4.95

Obj

Az

Stadia

At Sta 92+00

to Sta 95+00

0°00'

Beg. tile drain (F.L.)

89°55'

100'

✓

" " " Top tile

"

"

✓

Top tile

98°05'

113'

✓

"

104°15'

125'

✓

"

108°00'

135'

✓

"

112°45'

151'

✓

"

117°50"

173'

✓

TP

8.76

0.42

BM

5.02

$\begin{array}{ccccccc}
 \text{///} & \equiv & \text{///} & \equiv & \text{///} & \equiv & \text{///} \\
 & & & & & & \text{///} \\
 & & & & & & \equiv & \text{///}
 \end{array}$

HI 5.5

At Sta 83+00

to Sta 82+21.70 (PT)

180°00'

to outlet

43°25'

385'

✓

"

48°35'

346'

✓

RG 0.75 inside dia.
WM 0.90 outside dia.
LB
WS

Rad

May 9, 1962
63° Windy

2

1.16

7.16

6.35

6.73

6.50

6.66

6.70

6.88

Sta 7400 on Proposed curve at old Lower Afton Rd.
conc.

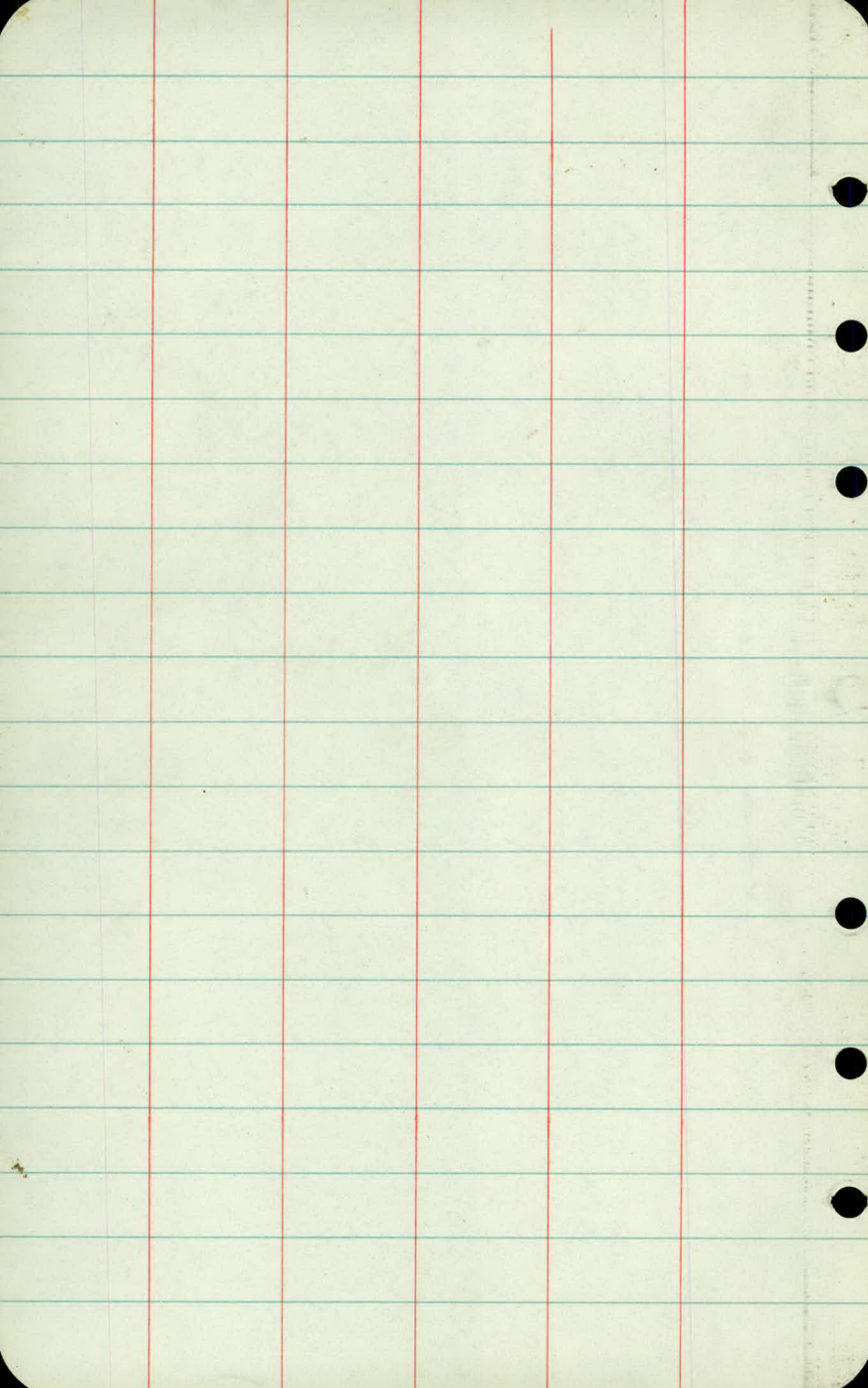
NE Cor, Ent Slab Garage So. Side Lower Afton

111 = 111 = 111 = 111 = 111 = 111 = 111

14.05

8.0

10.8



RG
LB
WS

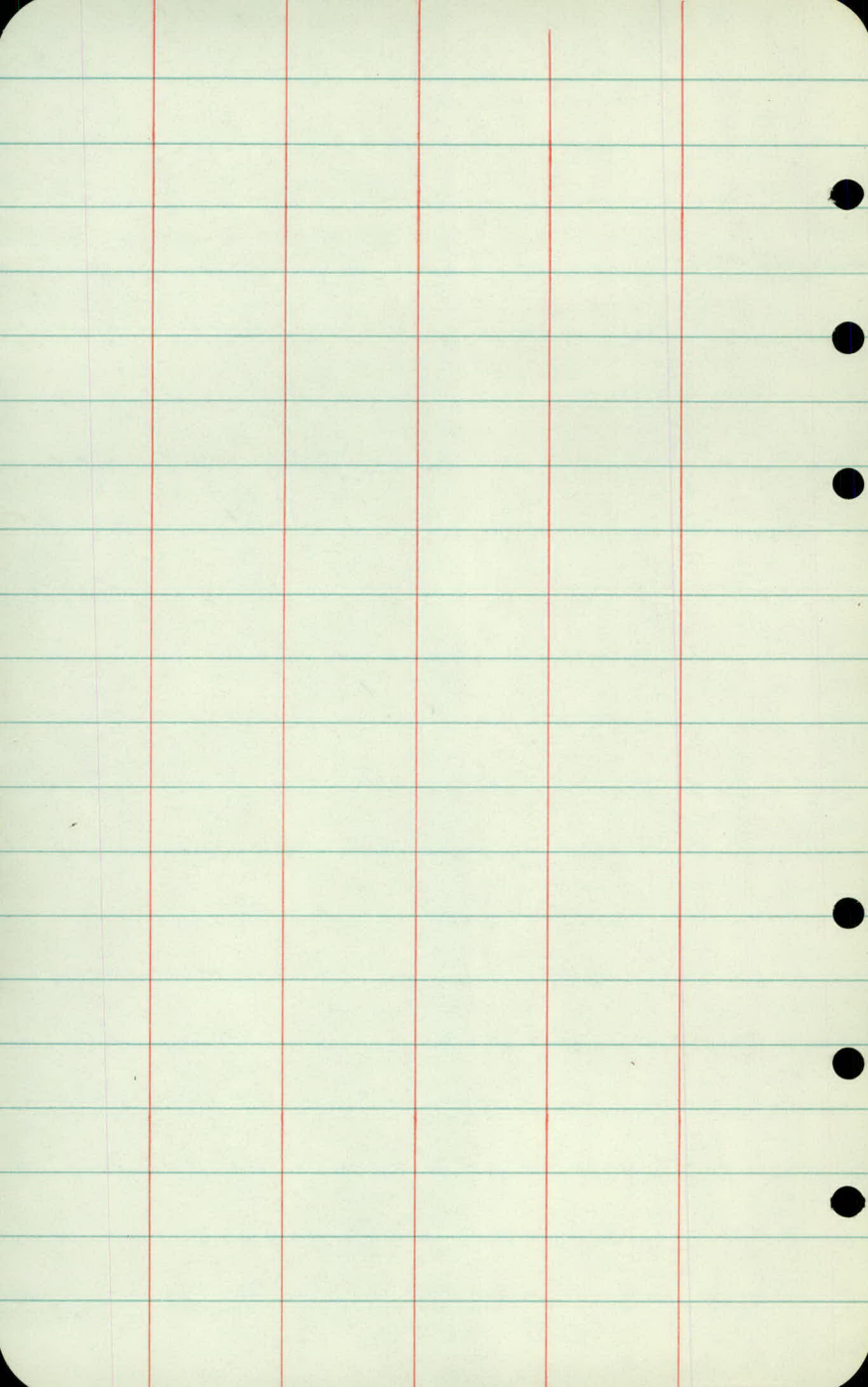
May 3, 1962

1

Lower Afton Rd
Culvert survey

9 pages

Dr. 9, BK 36

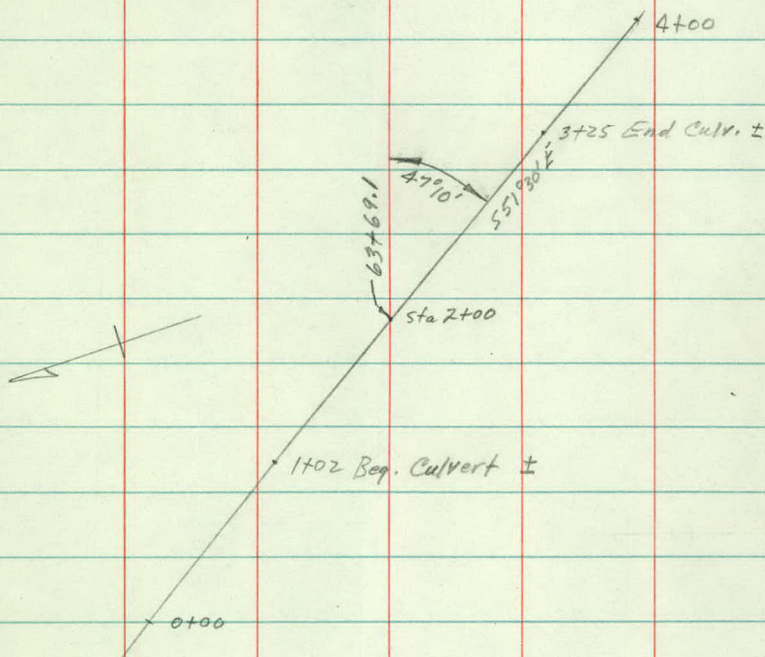


RG
LB
WS

May 3, 1962
Clear 75°

2

Prop. Lower Afton Rd



Profile

Sta	+	π	-	Elev
BM	7.25	922.35		915.1
0+00			9.1	13.3
+15			9.0	13.4
+26			8.0	14.4
+35			6.0	16.4
+43			7.1	15.3
+50			7.2	15.2
+59			7.5	14.9
+63			11.5	10.9
+76			12.7	09.7
+78			13.7	08.7
+90			13.6	08.8
1+00			13.2	09.15
1+00			13.5	08.9
+13			13.8	08.6
+21			11.6	10.8
+32			10.0	12.4
+38			11.5	10.9
+45			11.8	10.6

R6
LB
WS

May 5, 1962

3

£ sta 63+00 (L. After)

Bank

creek bottom

"

W.S.

creek bottom

bank

Sta	+	π	-	E/v.
-----	---	-------	---	------

922.35

1+50			12.8	09.6
+51			14.0	08.4
+53			14.0	08.4
+59			12.9	09.5
+70			12.2	10.2
+83			11.4	11.0
+88			9.8	12.6
+96			9.4	13.0
2+00			10.9	11.5
+03			11.5	10.9
X +04 to +06			12.8	09.6
+04 to +06			12.3	10.1
+08			11.6	10.8
+15			12.4	10.0
+26			12.3	10.1
+27			11.3	11.1
+31			7.5	14.9
+50			6.7	15.7

May 3, 1962

4

bank

creek bottom

"

bank

bank

creek bottom

W.S.

bank

bank

creek bottom

bank

Top bank

Sta	+	π	-	E/V.
-----	---	-------	---	------

92235

2+75			5.5	16.9
------	--	--	-----	------

3+00			4.7	17.7
------	--	--	-----	------

+19			5.0	17.4
-----	--	--	-----	------

+33			5.9	16.5
-----	--	--	-----	------

+37			7.6	14.8
-----	--	--	-----	------

+41			8.9	13.5
-----	--	--	-----	------

+41			8.4	13.95
-----	--	--	-----	-------

+43			6.1	16.3
-----	--	--	-----	------

+50			5.7	16.7
-----	--	--	-----	------

+62			5.2	17.2
-----	--	--	-----	------

+67			4.3	18.1
-----	--	--	-----	------

+76			5.8	16.6
-----	--	--	-----	------

+87			6.8	15.6
-----	--	--	-----	------

+92			7.4	15.0
-----	--	--	-----	------

+92			7.2	15.15
-----	--	--	-----	-------

4+00			7.6	14.8
------	--	--	-----	------

4+00			7.3	15.05
------	--	--	-----	-------

Sta			7.34	915.01
-----	--	--	------	--------

May 3, 1962

5

bank

creek bottom

W.S.

bank

bank

creek bottom

W.S.

creek bottom

W.S.

Sta 64+00 (Lower Afton)

X-Sections

Sta	+	π	-	Elev.
BM	6.74	921.84		915.1

0+75

+85

1+00

+22

+33

+50

R6
LB
WS

May 4, 1962
Clear 70°
Pt.

1st

2nd

3rd

Sta. 63+00 (Lower Afton Rd.)

21.5	15.6	12.5	11.2	09.6	08.0	08.8	08.9	09.5
0.3	6.2	9.3	10.6	12.2	13.8	13.0	12.9	12.3
20	15	13	7		2	4	9	15
15.2	11.4	09.5	07.9	09.0	09.9	10.3	11.0	
6.4	10.4	12.3	13.9	12.8	11.9	11.5	10.8	
15	11	6	3		2	8	15	
	13.8	12.5	10.5	08.8	07.4	09.9	12.1	13.3
	8.0	9.3	11.3	13.0	14.4	11.9	9.7	8.5
	15	12	5		3	5	10	15
13.1	10.1	08.5	09.5	10.7	12.2	13.2	13.8	
8.7	11.7	13.3	12.3	11.1	9.6	8.6	8.0	
15	9	7	5		3	9	15	
14.2	13.0	09.8	08.7	09.8	13.0	13.3	13.9	
7.6	8.8	12.0	13.1	12.0	8.8	8.5	7.9	
15	12	8	6	4	3	9	15	
12.7	12.1	10.7	09.5	08.5	10.0	11.7	13.4	13.8
9.1	9.7	11.1	12.3	13.3	11.8	10.1	8.4	8.0
15	12	7	5	2		3	6	15

Sta

+

π

-

Elev

921.84

1+63

+67

+79

+90

✓

2+00

May 4, 1962

Lt

Rt

Rt

7

14.5	13.0	11.3	09.8	08.8	09.5	10.8	12.1
7.3	8.8	10.5	12.0	13.0	12.3	11.0	9.7
15	11	6		3	4	9	15

14.7	12.7	10.5	10.0	08.8	09.4	10.5	10.7
7.1	9.1	11.3	11.8	13.0	12.4	11.3	11.1
15	10	4		3	5	10	15

15.2	13.7	11.5	10.5	10.1	09.3	09.9	10.6	11.9
6.6	8.1	10.3	11.3	11.7	12.5	11.9	11.2	9.9
15	11	6		2	4	7	12	15

16.0	15.5	14.2	12.2	11.6	10.9	10.4	09.1	10.4
5.8	6.3	7.6	9.6	10.2	10.9	11.4	12.7	11.4
15	13	7		3	9	11	11.5	12

10.9
10.9
15

12.8	12.2	11.6	11.5	10.9	09.3	10.7	10.9	11.7
9.0	9.6	10.2	10.3	10.9	12.5	11.1	10.9	10.1
15	13	7		7	8	11	14	15

Sta

+

π

-

E/v.

921.84

2+15

+35

+57

+76

+93

3+00

May 4, 1962

21.

4

PT

8

11.5	11.4	11.4	09.8	12.4	14.1	15.2	16.1
10.3	10.4	10.4	12.0	9.4	7.7	6.4	5.7
15	12	4	2		3	10	15

11.7	11.8	12.9	14.3	14.3	16.2	17.0
10.1	10.0	8.9	7.5	7.5	5.6	4.8
15	12	8		3	9	15

12.9	14.0	15.7	16.4	17.6	18.2
8.9	7.8	6.1	5.4	4.2	3.6
15	7		3	10	15

12.5	11.4	14.8	16.1	16.5	17.6	18.5	18.6	18.9
9.3	10.4	7.0	5.7	5.3	4.2	3.3	3.2	2.9
15	13	11	6		4	8	12	15

12.8	14.1	16.1	17.1	18.1	19.0	19.4
9.0	7.7	5.7	4.7	3.7	2.8	2.4
15	11	5		4	10	15

15.5	15.7	16.2	17.3	18.0	18.9	19.5
6.3	6.1	5.6	4.5	3.8	2.9	2.3
15	12	10		5	9	15

Sta

+

π

-

Elev

921.84

3+16

+30

BM

6.85

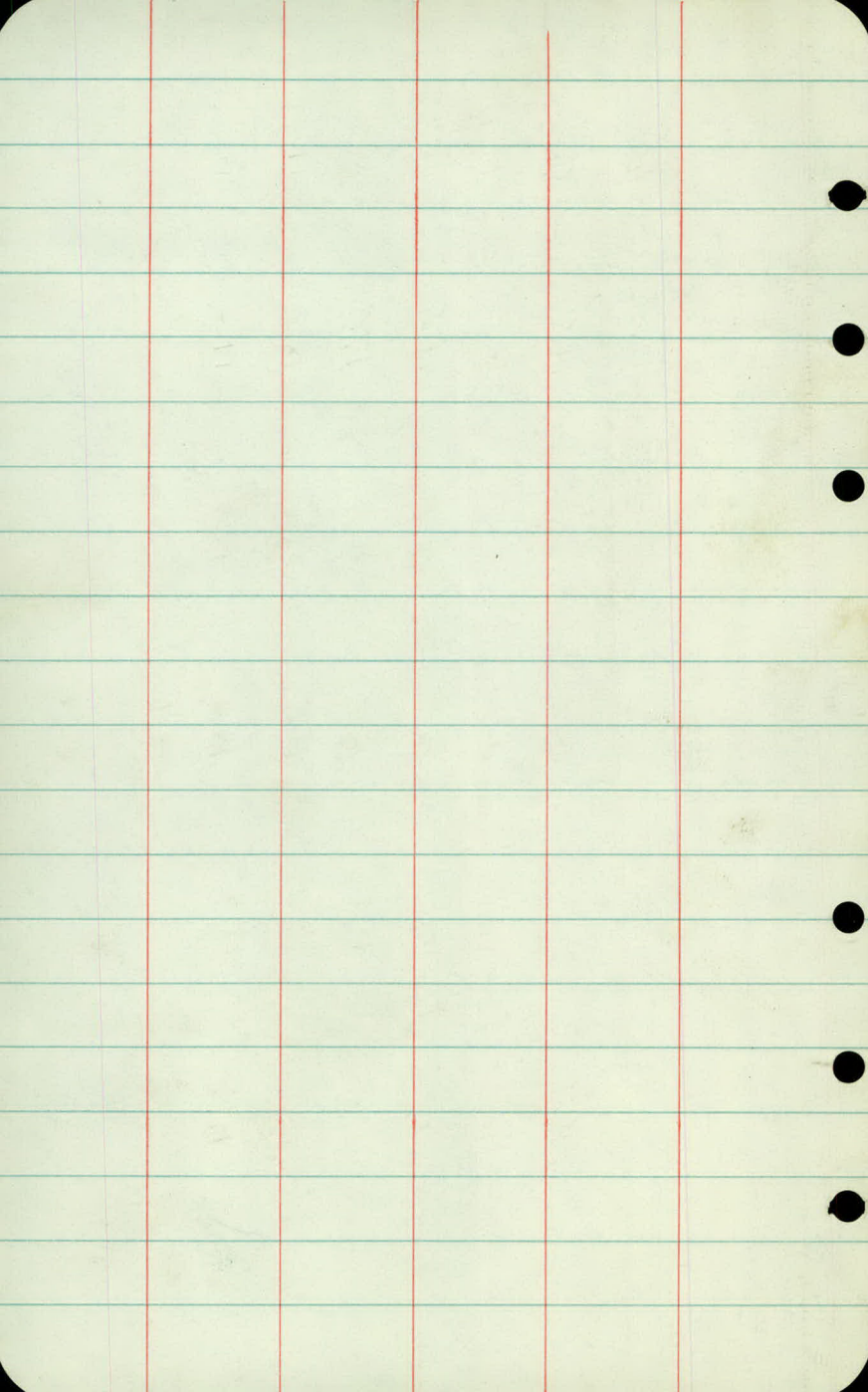
914.99

May 4, 1962

9

Lt	+	Rt
16.6	17.3	17.1
5.2	4.5	4.7
15	11	3
17.3	18.2	19.0
4.5	3.6	2.8
7	12	15
19.9		
13.6	14.5	16.3
8.2	2.3	5.5
15	9	6
16.5	17.5	18.5
5.3	4.3	3.3
4	11	15
19.2		
2.6		
work.		

± Sta 64+00 (Lower Afton Rd.)



1
Lower Afton Road

x-sections

FOR STORM SEWER

Sta	+	π	-	Elev.
BM	1.19	984.76		983.57

81+55

82+29
~~81+29~~

+51

+77

TP	10.86 11.86	994.47	1.15	983.61	93.7
----	---------------------------	--------	------	--------	------

TP	12.19	1004.74	1.92	992.55	92.6
----	-------	---------	------	--------	------

87

✓

FK
JS
FB
LB
BZ

Sept. 13, 1963

LT Clear, Cool 45° 2

Spike in 24" Oak Rt. Sta 83+07

11.3	11.9	12.1	12.4	12.1	12.1	12.6	11.0	11.2	✓
12.5	12.9	12.7	12.4	10.7	8.7	8.2	7.8	7.6	
100	78	58	45	34	25	22	13		

15.5	15.1	15.4	14.0	16.1	11.9	18.1	11.0	11.1	✓
9.3	9.1	9.4	10.8	8.7	6.9	6.1	5.8	5.7	
64	49	39	36	35	27	22	13		

11.1	11.9	11.5	16.6	15.6	16.1	18.1	11.3	11.6	11.8	✓
7.1	6.9	7.3	8.2	9.2	8.1	6.7	5.5	5.2	5.0	
57	49	42	38	35	31	30	22	13		

11.6	18.6	16.5	15.9	16.6	11.2	18.8	11.8	80.2	80.6	✓
3.2	6.2	8.3	8.9	8.2	7.6	6.0	5.0	4.6	4.3	
50	43	41	38	35	32	28	22	13		

Sta 88±

87.3	85.8	85.2	85.8	87.5	90.5	90.1	91.0	91.2	
17.4	18.9	19.5	18.9	17.2	14.2	14.0	13.7	13.5	
45	43	41	38	36	24	23	13		

92.0	99.9	90.4
12.7	4.8	4.3
54	67	79

Sta + π - Elev

1004.24

88

✓

89

✓

90

91

TP 8.21 1003.67 9.28 995.46

Sept. 13, 1963

Lt

£

3

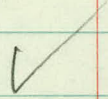
86.9	87.1	88.1	90.5	92.0	92.3	92.54
17.8	17.6	16.0	14.2	12.7	12.4	12.2
44	42	39	30	23	13	

87.2	88.5	93.9	91.7	92.6
17.5	16.2	10.8	3.0	2.1
46	48	57	71	80

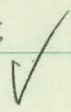


88.1	87.9	88.1	89.3	91.7	92.8	93.1	93.3
16.6	16.8	16.6	15.4	13.0	11.9	11.6	11.4
48	46	44	42	30	22	13	

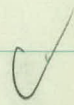
89.5	94.2	92.4	93.3
15.2	10.5	2.3	1.4
49	58	74	83



91.1	95.7	90.7	89.3	89.9	92.3	93.7	94.0	94.1
3.0	9.2	14.0	15.4	14.8	12.4	11.0	10.7	10.6
73	60	49	44	41	31	22	13	



96.7	96.1	93.4	90.4	90.4	92.2	94.3	94.7	94.9
8.0	8.6	11.3	14.3	14.3	12.6	10.3	10.0	9.8
73	63	55	50	41	34	22	13	



Sta 92 + 00 £

Sta + π - Elev
1003.67

92

+60

10.84 992.83

93

12.94

+32



94

95

Sept. 13, 1943 4

LT

q6.0	q4.7	q2.0	q1.0	q1.2	q4.1	q5.1	q6.3	q5.5
7.7	9.0	11.7	12.7	12.5	9.6	8.6	8.4	8.2
83	68	59	53	41	29	22	13	

N End Culvert 300' ± RT

q4.8	q5.0	q1.7	q2.1	q1.8	q3.8	q6.1	q6.3	q6.6
8.9	8.7	12.0	11.6	11.9	9.9	7.6	7.4	7.1
80	69	56	48	41	33	22	13	

q5.1	q2.1	q2.4	q2.2	q0.8	q3.0	q4.6	q6.4	q6.8	q7.0
8.6	11.6	11.3	11.5	13.22	10.7	9.1	7.3	6.9	6.7
66	55	48	41	FL	39	31	22	13	
Culv. 41'									

q5.7	q1.84	q0.73	q3.0	q4.0	q6.2	q6.8
8.0	11.83	12.94	10.7	9.7	7.5	6.9
76	(Water) Right Side			38	25	18
41		FL 41	40			

q5.7	q4.0	q2.8	q2.0	q3.5	q5.6	q7.8	q8.0	q8.3
8.0	9.7	10.9	10.8	10.2	8.2	5.9	5.7	5.4
73	59	46	43	42	34	22	13	

q0.0	q7.9	q5.3	q5.2	q7.8	q0.2	q0.6	q0.7
3.7	5.8	8.4	8.5	5.9	3.5	3.2	3.0
90	65	48	44	34	22	13	

Sta + π - Elev

1003.67

95+28

+45

TP 9.56 1012.91 0.32 1003.35

96

97

98

99

+54 3.69 09.22

+80 3.28 09.63

+53 $\angle$ Ent. Lt 76'

+83 Range tie Ent Lt.

Sept. 13, 1963

5

LT

±

00.7	06.8	05.8	05.9	07.1	08.9	01.0	01.3	01.42
3.0	6.9	7.9	7.8	6.6	4.8	2.7	2.4	2.25
58	44	43	40	39	32	22	13	

✓

02.7	04.9	07.6	06.4	07.0	08.9	01.5	01.7	01.9
1.0	3.8	6.1	7.3	6.7	4.8	2.2	2.0	1.8
61	48	43	41	36	35	22	13	

Sta 96 ±

✓

08.0	06.2	00.7	08.7	08.6	02.0	02.9	03.2	03.35
4.9	6.7	12.2	14.2	14.3	10.9	10.0	9.7	9.56
61	51	37	35	33	28	22	13	

✓

12.0	07.5	03.5	01.5	03.2	04.6	05.5	05.7	06.0
0.9	5.4	9.4	11.4	9.7	8.3	7.4	7.2	6.9
56	46	36	35	33	29	22	13	

✓

12.9	10.5	06.4	05.4	05.1	06.1	06.1	08.0	08.2	08.4
0.0	2.4	6.5	7.5	7.8	6.8	6.8	4.9	4.7	4.5
52	46	38	37	34	34	31	22	13	

✓

12.5	08.8	08.5	07.6	07.9	07.6	10.1	10.3	10.6
0.4	4.1	4.4	5.3	5.0	3.3	2.8	2.6	2.3
48	36	33	32	28	25	22	13	

FL W. End 18" CM 34' LT.

✓

FL E End 18" CM 34' LT.

