

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

CO. ROAD "I"

From Hamline To Lexington

Road Acc't. No. _____

Date Filed 2-23-61

Dr. 9
File BK. 33

COUNTY ROAD "I"

Hamline Ave to Lexington Ave.

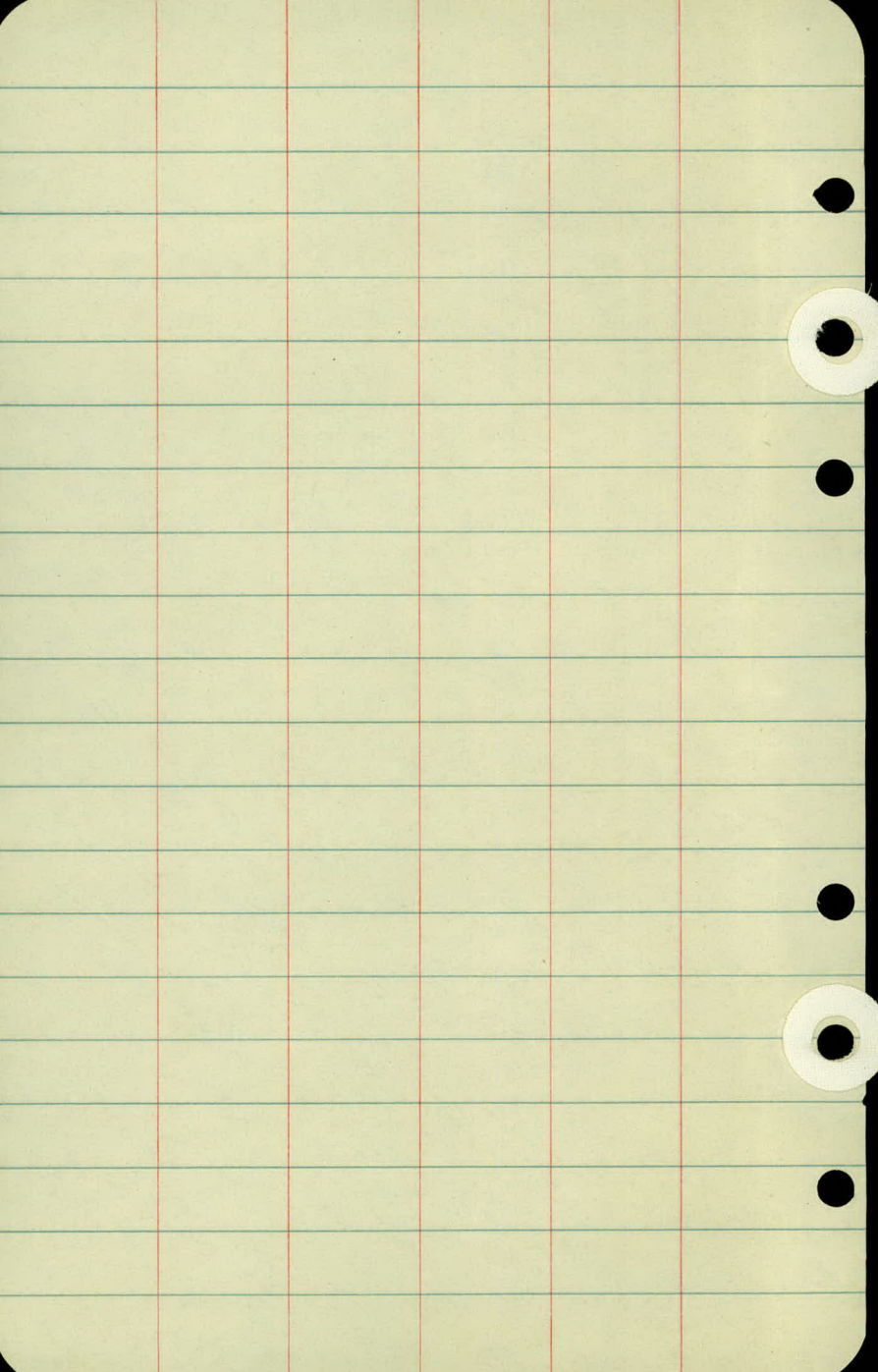
PLAN SURVEY

S.P. 62-603-01

Fed. Proj. D.S. 6360 (1)

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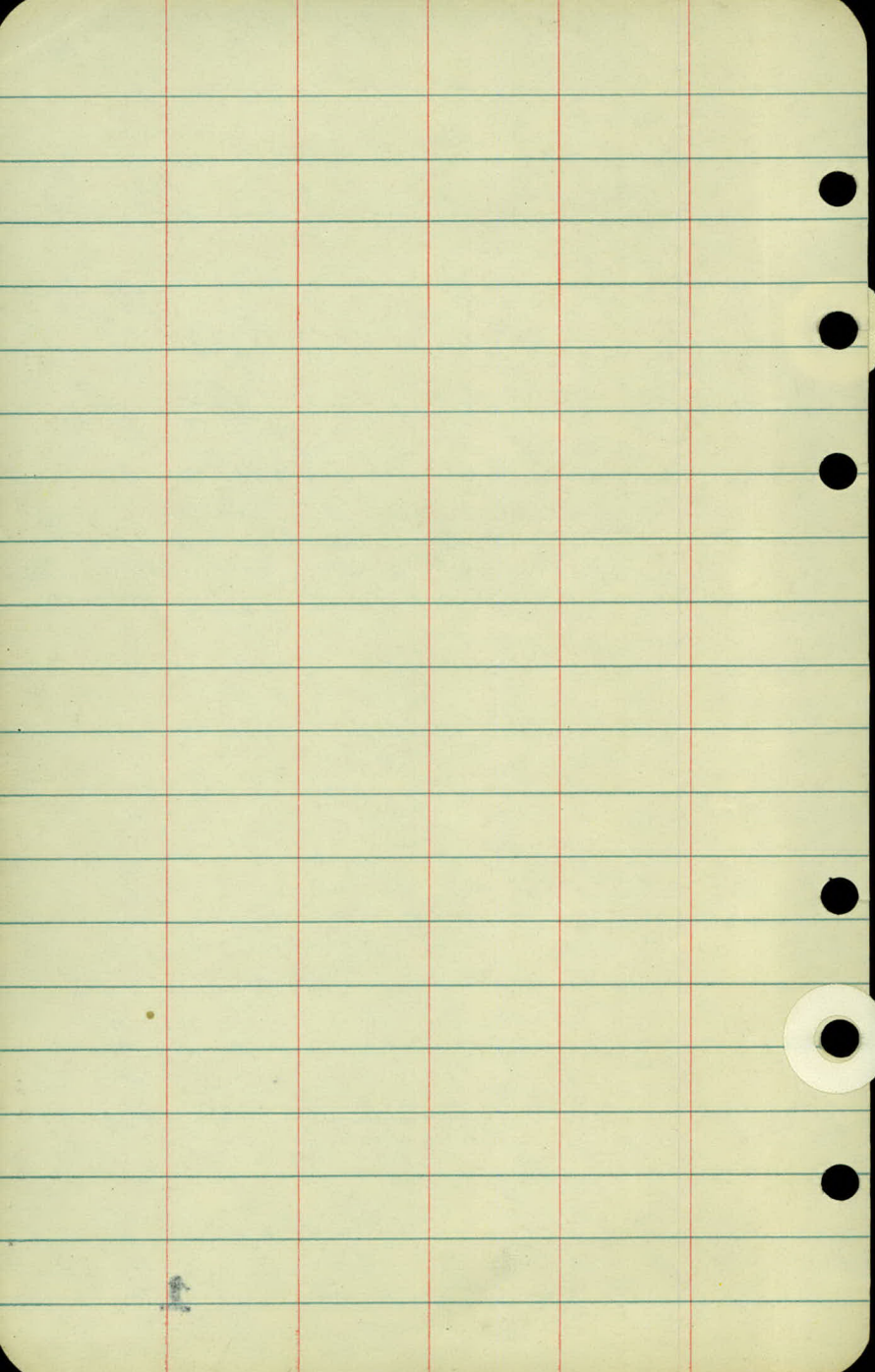


Started April 28, 1958

Co. Rd I

Hamline to Lexington

Plan Survey



FK
KP
AB

May 8, 1958

2

Alignment

4a-Ad

15+96.82 New P.I.

Sta Point ΔL ΔR Description

+27.31 PT $7^{\circ} 19.375'$

7 $6^{\circ} 55'$

+50 $6^{\circ} 10'$

6 $5^{\circ} 25'$

+50 $4^{\circ} 40' \Delta = 14^{\circ} 38\frac{3}{4}'$

5 $3^{\circ} 55' D = 3^{\circ}$

+84.58 P.I. $T = 245.46'$

+50 $3^{\circ} 10' L = 488.46$ ¹⁹

4 $2^{\circ} 25' R = 1910.08$

+50 $1^{\circ} 40'$

3 $0^{\circ} 55'$

+50 $0^{\circ} 10'$
 $0^{\circ} .098'$

+39.12 P.C. $0^{\circ} 00'$

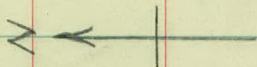
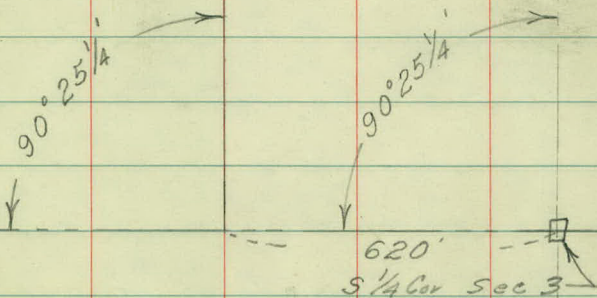
0+100 $\neq$ Hamline

May 7, 1958

3

Boat Spike

10/10
see 40



3

Sta Point ΔL ΔR

26+79.12 $\pm$ Lexington Ave

25+21.12 P.O.T. S.E. Cor. School Property

+88.07 P.T. $7^{\circ}19'37.5''$

+50 $6^{\circ}45''$

19 $6^{\circ}00''$

+50 $5^{\circ}15''$

18 $4^{\circ}30''$

$\Delta = 14^{\circ}38\frac{3}{4}''$

+50 $3^{\circ}45''$

$D = 3^{\circ}$

~~15+96.82~~

New P.I.

17+45.34 P.I.

$T = 245.46$

17 $3^{\circ}00''$

$L = 488.19$

+50 $2^{\circ}15''$

$R = 1910.08$

16 $1^{\circ}30''$

+50 $0^{\circ}45''$

15 $0^{\circ}00''$

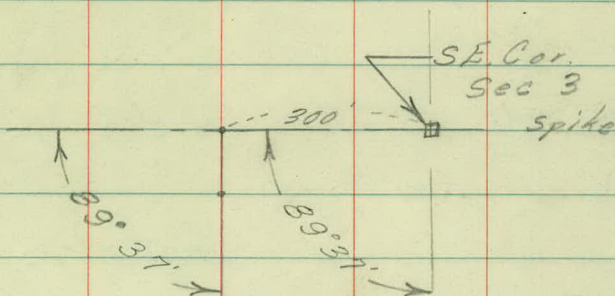
14+99.88 P.C. $0^{\circ}00''$

D.

G

FK
RG
KP
AB

May 7, 1958
May 12, 1958



S.W. Cor. School Property → 163.96

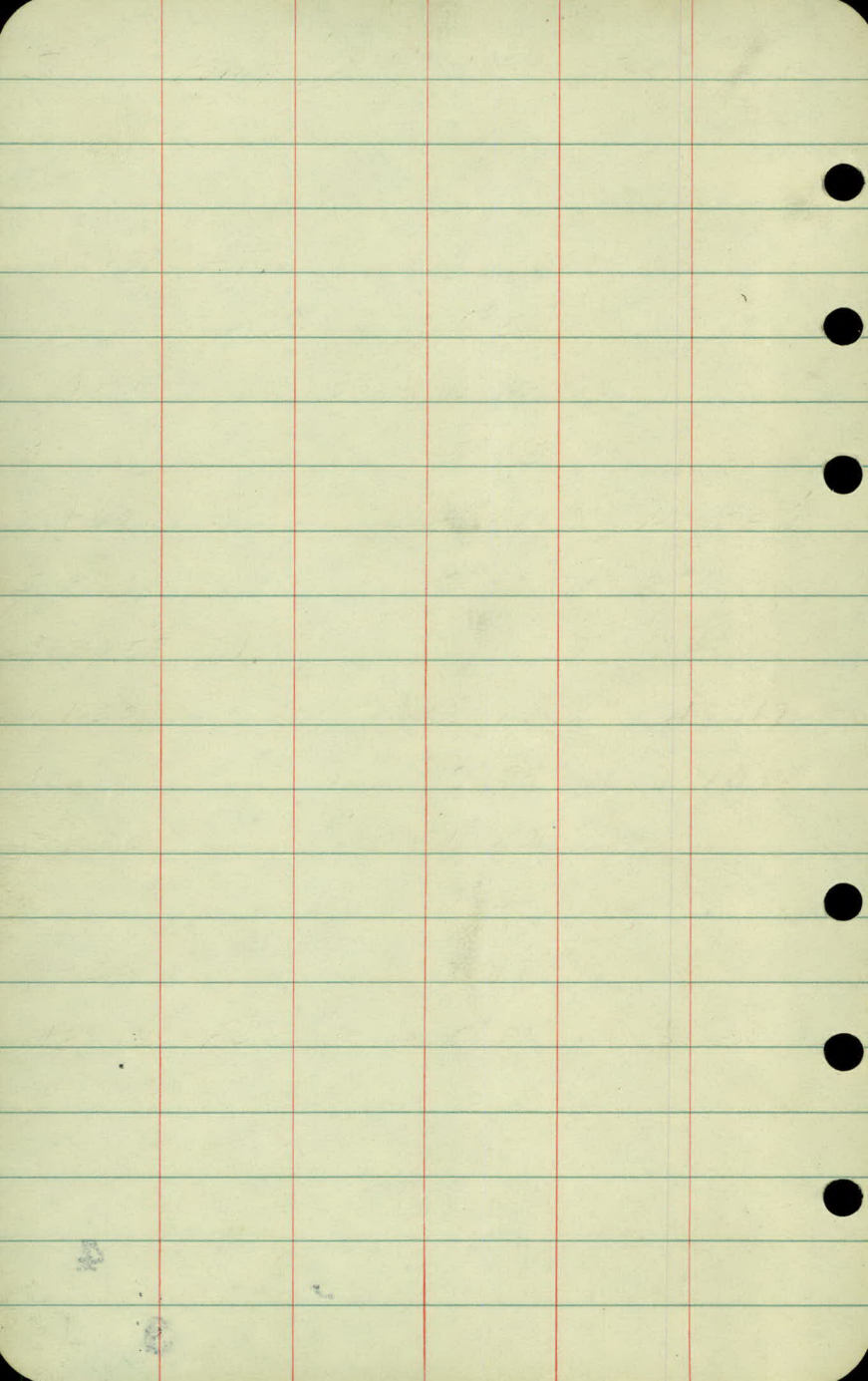
Cor Conc Ents/ab

87.43

18" Oak Disk

178.61

Void



July 26, 1958

21
a

-47 E

B Line
Alignment

Sta Point A RT 26 AUG 1959

KP

+38.51 P.T.	7°20'	
7	6°45'	
+50	6°00'	Δ 14°41'
6	5°15'	D 3°
+50	4°30'	T 246.09
5	3°45'	L 489.44
+50	3°00'	R 1910.08
4	2°15'	
+50	1°30'	
3	0°45'	
2+49.07 PC	0+00	
0+00	£ Hamline	

FK
RL
RR
RM

July 21, 1958

25
6

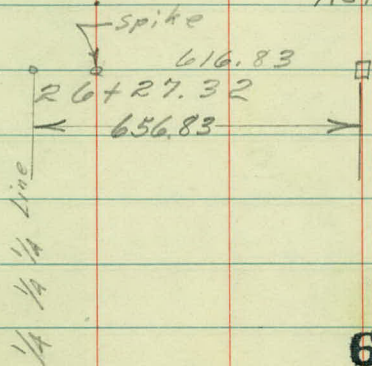
Boat Spike

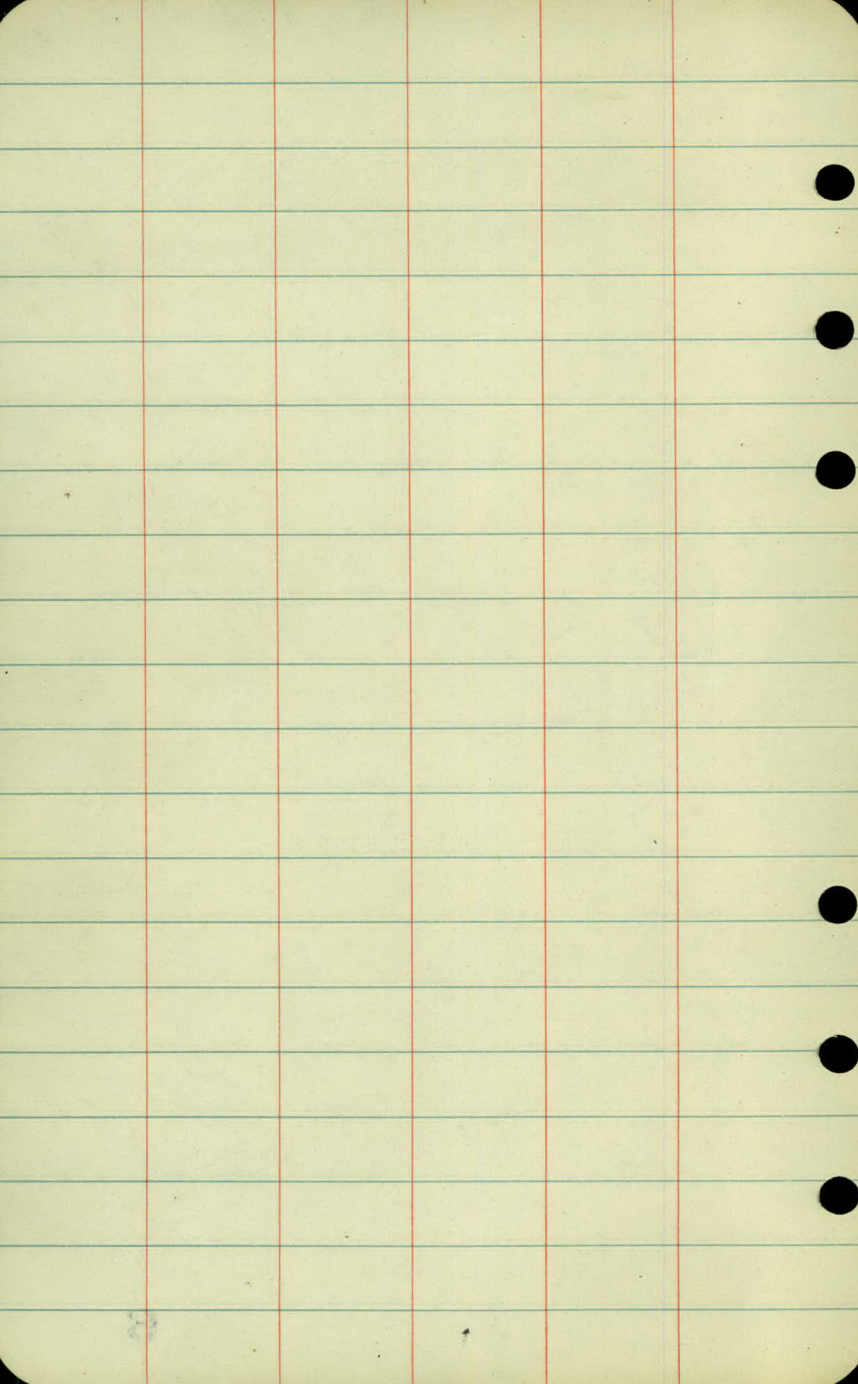
4+95.16

Boat Spike

Moved 0+00 3.17' South

P.C. Boat Spike





FK
RL
RR
RM

July 17, 1956

~~34~~
6

"B" Line
Alignment

Sta Point Δ LT DRT

26+74.80 $\pm$ Lexington

⁰²
~~130.49~~ PT 7° 19.35'

18 6° 51.9'

+50 6° 06.9'

17 5° 21.9'

+50 4° 36.9'

$\Delta = 14^{\circ} 38^{\frac{3}{4}}'$

16 3° 51.9'

D = 3°

^{87.29}
15 ~~127.76~~ P.I.

T = 245.46

+50 3° 06.9'

L = 488.19

15 2° 21.9'

R = 1910.08

+50 1° 36.9'

14 0° 51.9'

+50 0° 06.9'

13+42.30 0° 00'

⁷⁷
41.83

FX
RL
RR
RM

July 18, 1938

35
3/1

Boat Spike

340'

Spike in Root
24"0

S.E. Cor
Sec 3

2 < 1

Ties OK

94' 57

10"0
Dist

71.68

2x2 Hub

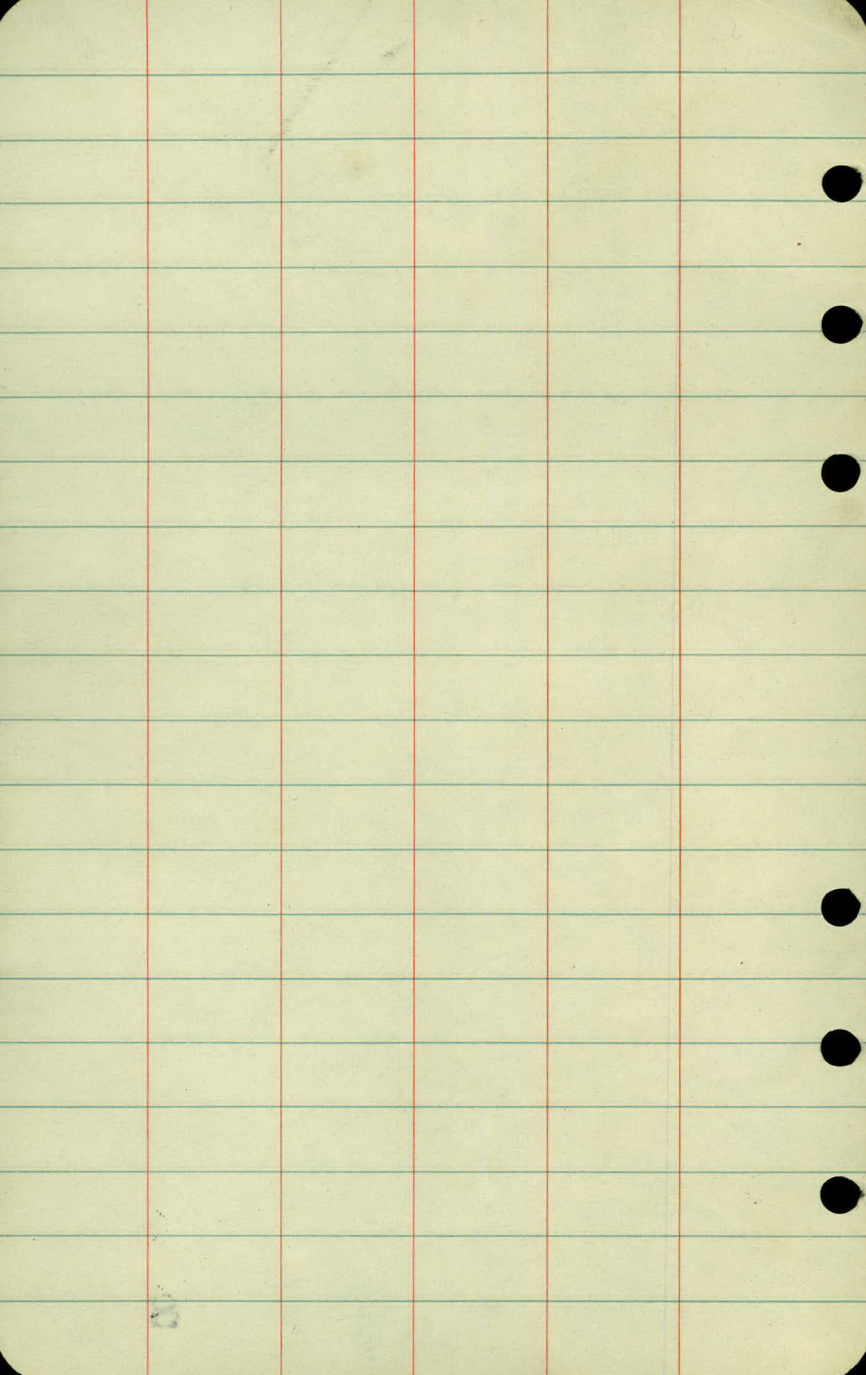
54.80 15"0
98.31 Dist

87.40

18"0
Dist

22"0
Dist

2x2 Hub



May 12, 1958

5

Topography

Co. Rd. I

5

Lt

£

Rt

4

+42 Edge Swamp
£

3

2

1

0+17 Toe of Slope

0+13 Shoulder

0+7 Edge BT

0

W. 8

FK
RG
KP
AB

May 12, 1958

6

Lt.

~~E~~

Rt



Swamp



Swamp

Hamline

Ave.

	Lt.	£	Rt.
10	$+100 \frac{\text{SWP}}{16}$		$+100 \frac{\text{SWP}}{100}$
	$+50 \frac{\text{SWP}}{35}$		$+50 \frac{\text{SWP}}{130}$
9	$+100 \frac{\text{SWP}}{23}$		$+100 \frac{\text{SWP}}{102}$
	$+100 \frac{\text{SWP}}{30}$		$+100 \frac{\text{SWP}}{43}$
	$+50 \frac{\text{SWP}}{41}$		
	$+27 \frac{\text{SWP}}{59}$		$+27 \frac{\text{SWP}}{26}$
7	$+100 \frac{\text{SWP}}{79}$		$+100 \frac{\text{SWP}}{24}$
	$+50 \frac{\text{SWP}}{120}$		$+50 \frac{\text{SWP}}{33}$
6			$+100 \frac{\text{SWP}}{53}$
			$+50 \frac{\text{SWP}}{74}$
			$+25 \frac{\text{Beg SWP}}{156}$
5			

platted

May 12, 1958

Lt

E

Rt 7

Swamp

Swamp

15

Lt

£

Rt

14

+38 15 Strand Elec Fe
£ N-S

13

12

+17 R. Tie Ditch
Rt

+08 Angle in Ditch
24

11

+02 1' Pitch
£

+50 SWP
30

+30 SWP
£

10

Lt

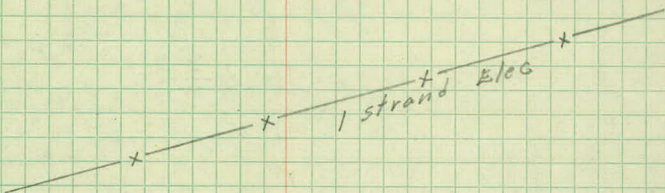
£

May 12, 1958

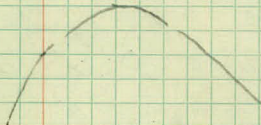
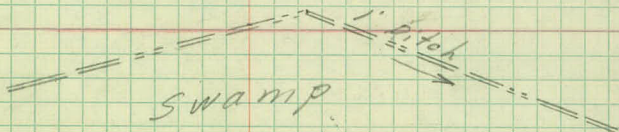
Rt

8

Swamp



Swamp



20

Lt.

£

Rt

$$+31 \frac{28''0}{14}$$

$$+31 \frac{Tw 4'' BE}{23}$$

$$+24 \frac{8'' BE}{32} +27 \frac{5'' p}{35} +31 \frac{10'' BE}{32}$$

+25 End Cultivated
Area Lt

$$+22 \frac{30''0}{1}$$

19

$$+17 \frac{6'' BE}{17}$$

$$+21 \frac{Tw 4'' BE}{27}$$

$$+98 \frac{4'' Cedar}{35}$$

$$+49 \frac{16''0}{19}$$

$$+75 \frac{10''0}{24}$$

$$+22 \frac{Broken 3 Barb Fe}{£ N-S} +26 \frac{Run Cedars 10A ant}{1-70}$$

$$+14 \frac{22''0}{7}$$

$$+44$$

$$+81 \frac{30''0}{22}$$

$$+67 \frac{26''0}{37}$$

$$+69 \frac{30''0}{25}$$

$$+35 \frac{24''0}{36}$$

$$+59 \frac{24''0}{16}$$

$$+48 \frac{14''0}{21}$$

$$+19 \frac{14''0}{21}$$

$$+44 \frac{20''0}{£}$$

$$+26 \frac{30''0}{24}$$

$$+12 \frac{14''0}{2}$$

$$+88 \frac{Tw in 18''0}{3}$$

17

$$+97 \frac{20'' WO}{12}$$

$$+87 \frac{18'' W}{43}$$

$$+38 \frac{Trip 16'' W}{14}$$

$$+25 \frac{Edge Swamp}{£ N-S}$$

$$+105 \frac{1 Strand Elec Fr}{£ N-S}$$

16

$$+63 \frac{£ 2' Ditch}{£ N-S}$$

15

81

May 12, 1958

9

Lt

E

Rt

Hay field

Cultivated

Area

3 strand Barb
Broken down

fast

2' Ditch

Swamp

25

Lt

£

Rt

24

23

22

21

100 to +75 Low Area

20

May 12, 1958

10

Lt

Rt

Field

Hay

Low Area

Lt

~~£~~

Bt.

27

+03 Shoulder
~~£~~

+94 Edge B.T.
~~£~~

+70 Edge B.T.
~~£~~

+52 P.P.
77

+60 Shoulder
~~£~~

+52 P.P.
51

26

25

May 12, 1958

11

Lt

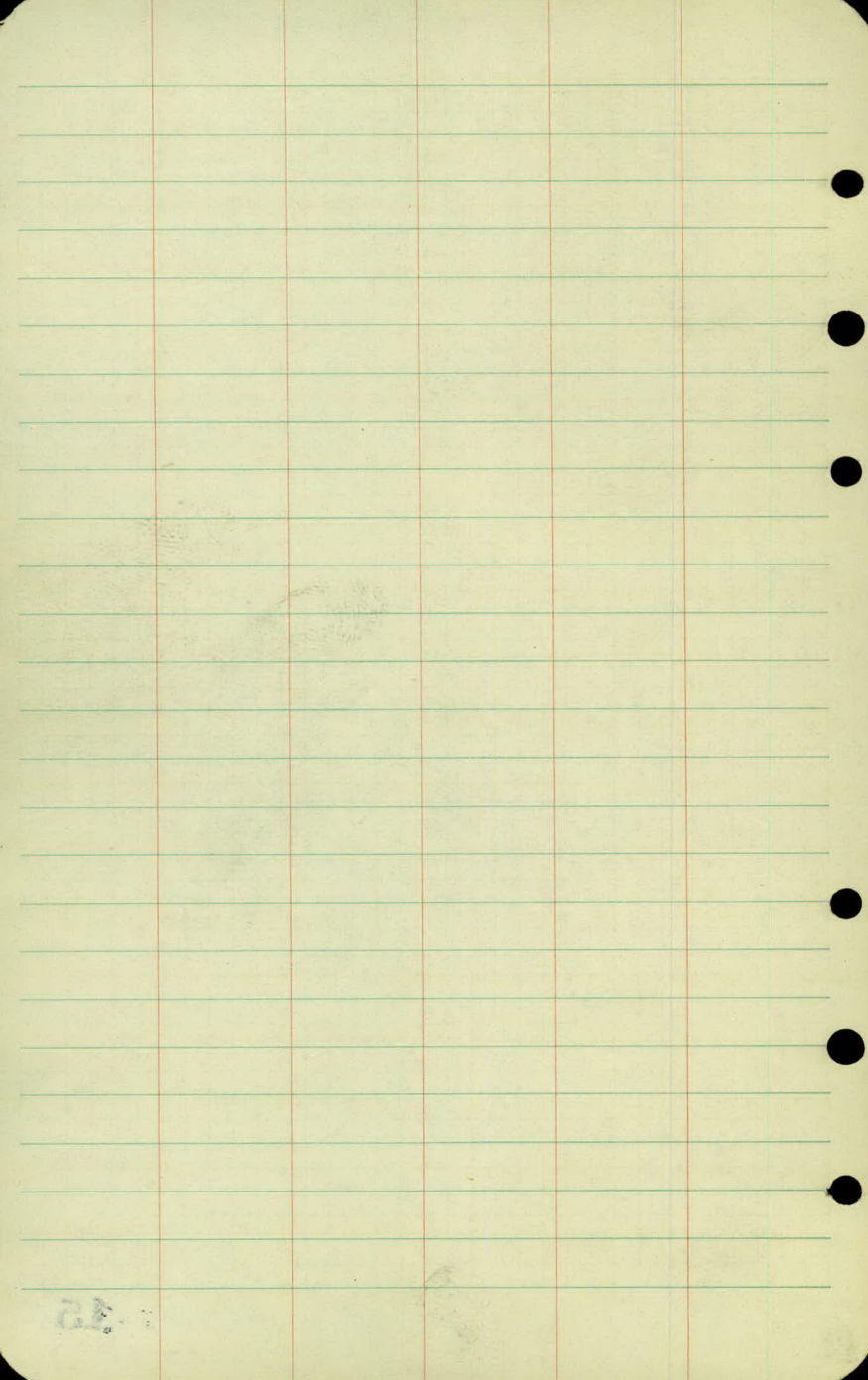
Rt

Lexington

Ave.



Hay Field



FK
RG
KP
AB

May 12, 1958

12

X-sections

Sta	+	π	-	Elev
-----	---	-------	---	------

BM	0.35	892.94		(892.59)
----	------	--------	--	----------

T.P.	7.12	893.22	6.84	886.10
------	------	--------	------	--------

0+00 $\neq$ Hamline

+07 Edge B.T.

+13 Shoulder

+17 Toe of Slope

+50

May 12, 1958
\$

13

Lt

Rt

Top of Brick N.W. Cor of Brick + Conc MH 200' Rt

Sta 211+50

Top E. End 30" C.M. Culvert 380' Net Mont

90.6	90.1	90.0	89.7	89.4	88.9	88.7
2.6	3.1	3.2	3.50	3.8	4.3	4.5
150	100	50		50	100	150

89.7	89.6	89.4	89.2	88.8	
3.5	3.6	3.8	4.0	4.4	✓
50	29		23	50	

88.8	88.8	88.7	88.5	88.4	88.4	88.3
4.4	4.4	4.5	4.7	4.8	4.8	4.9
50	33	18		13	27	50

87.7	87.3	87.1	87.0	87.4	87.7	87.3	87.4	87.8	87.1
5.5	5.9	6.1	6.2	5.8	5.5	5.9	5.8	5.4	6.1
50	33	22	9	7		13	26	36	50

87.7	87.3	87.7	87.6	87.1	86.6	
5.5	5.9	5.5	5.6	6.1	6.6	✓
50	31	14		21	50	

87.1	86.9	86.5	86.2	86.2	86.3	86.2
6.1	6.3	6.7	7.0	7.0	6.9	7.0
50	37	19		14	29	50

Sta + π - Elev

893.22

1 + 50

2

+ 50

3

TP 13.72 901.68 5.26 887.96

+ 46

+ 62

TP 7.55 902.71 6.52 895.16

May 12, 1958 14

Lt

Rt

87.8	87.6	87.5	87.4	87.2	87.2	86.8	86.6
5.4	5.6	5.7	5.8	6.0	6.0	6.4	6.6
50	34	22	8		16	33	50

87.8	87.8	87.3	87.0	87.2	86.7	
5.4	5.4	5.9	6.2	6.0	6.5	
50	40	16		24	50	

87.3	87.4	87.3	86.9	87.0	87.1	
5.9	5.8	5.9	6.3	6.2	6.1	
50	38	17		26	50	

87.7	87.6	87.7	87.6	87.7	87.9	87.9
5.5	5.6	5.5	5.6	5.5	5.3	5.3
50	38	14		16	35	50

Hub PC.

88.9	88.9	88.8	89.0	89.2	89.2	89.5	89.7
12.8	12.8	12.9	12.7	12.5	12.5	12.2	12.0
50	28	11		13	21	39	50

91.4	91.7	91.5	91.2	91.3	91.1	91.1
10.3	10.0	10.2	10.5	10.4	10.6	10.6
50	34	15		13	34	50

o/b stake #321+00

Sta + π - Elev

902.71

3+62

4

✓

✓

+25

✓

52

FX
RG
KP
AB

May 13, 1958
Windy P. Cloudy 55° 15

93.5	93.0	92.3	91.9	91.1	91.6	91.3	91.3
92	97	104	108	116	111	114	114
100	90	75	51		55	80	100

97.0	96.6	96.5	95.7	95.5	95.4	95.2	95.0
5.7	6.1	6.2	7.0	7.2	7.3	7.5	7.7
73	55	38	19		17	25	39

98.1	98.3	98.8	98.1	95.9	95.5	95.4	95.1	95.1
4.6	3.4	1.9	0.6	6.8	7.2	7.3	7.6	7.6
90	100	116	132	100	96	80	67	53

02.7
0.0
140

98.9	98.4	98.6	98.1	97.6	97.3	97.0	97.3	97.5
3.8	4.3	4.1	4.6	5.1	5.4	5.7	5.4	5.2
69	48	28	12		24	44	67	83

99.6	99.4	99.7	99.4	97.8	97.8	98.1	98.1
3.1	2.3	1.0	0.3	4.9	4.9	4.6	4.6
87	100	116	136	150	144	125	100

02.7
0.0
149

Sta + π - Elev.

902.71

4+50

✓

✓

5

✓

✓

52

May 13, 1958 16

99.0	98.7	99.1	97.9	97.6	97.2	96.6	96.2	96.1
3.7	4.0	3.6	4.8	5.1	5.5	6.1	6.5	6.6
51	30	16	5		21	43	63	74

99.4	90.0	90.4	90.7		96.1	96.4	96.1	96.3
3.3	2.7	2.3	2.0		6.6	6.3	6.6	6.4
69	83	100	112		155	139	122	100

02.7	02.1
0.0	0.6
134	127

99.6	98.4	97.6	97.6	97.6	96.6	95.8	96.4	94.8
3.1	4.3	5.1	5.1	5.1	6.1	6.9	7.3	7.9
70	48	28	11		17	34	53	71

99.9	90.4	90.9	90.4	92.7	93.0	93.5	94.2	94.3
2.8	2.3	1.8	2.3	10.0	9.7	9.2	8.5	8.4
84	100	122	141	157	144	123	100	93

99.6
3.1
158

Sta + π - Elev

902.71

5+50

✓

5+68 Page ¹⁹40

6

✓

✓

TP 2.86 896.85 8.72 893.99

+50

05

May 13, 1958

17

LT

RT

98.4	97.3	96.7	96.6	96.0	95.2	94.1	92.5	90.6
43	54	60	61	67	75	86	102	121
79	58	40	18		17	36	52	66

98.5	99.0	97.7	96.1
42	37	50	66
100	116	137	155

88.9	89.5
13.8	13.2
93	80

96.3	95.6	95.1	94.4	93.2	91.7	90.6	89.5	88.9
64	71	76	83	95	110	121	132	138
51	35	24	13		21	36	43	54

97.6	97.9	97.9	97.3
5.1	4.8	4.8	5.4
69	76	86	100

91.1	93.8	94.9	96.3
116	89	78	64
158	148	122	113

Hub Sta 6100

93.9	94.0	93.3	93.0	92.0	90.5	89.4	88.3
30	29	36	39	49	64	75	86
84	59	36	13		17	35	50

92.6
4.3
100

21

Sta + π - Elev

896.85

7 +00

✓

+50

8

+50

9

TP

4.23 892.62

May 13, 1958 18

14

15

92.6	92.2	92.8	91.8	91.4	90.3	88.7	88.6
4.3	3.7	4.1	5.1	5.5	6.6	8.2	8.3
61	40	18	9		17	40	50

✓

91.3
5.6
77

91.1	91.9	92.6	92.7	92.1	91.0	89.6	88.8	88.6
5.8	5.0	4.3	4.2	4.8	5.9	7.3	8.1	8.3
50	35	20	10		8	26	43	50

✓

89.6	90.7	92.0	92.3		91.9	90.3	88.9
7.3	6.2	4.9	4.6		5.0	6.6	8.0
50	32	14			13	31	50

✓

89.4	90.4	91.4	92.4		92.4	91.0	89.6
7.5	6.5	5.5	4.5		4.5	5.9	7.3
50	31	13			16	33	50

✓

89.0	90.4	91.3	92.1		92.8	91.7	91.1
7.9	6.5	5.6	4.8		4.1	5.2	5.8
29	24	10			14	34	50

22

89.4
7.5
42

89.4
7.5
50

91.8

Sta	+	π	-	Elev
-----	---	-------	---	------

T.P	6.40	900.39		893.99
-----	------	--------	--	--------

5+68

✓

✓

5+50

$\pm$

4.4

95.99

T.P.

4.72

897.34

892.62

~~892.62~~

9+50

10+00

FX
RG
AB

May 13, 1958
May 14, 1958
BT

19

14

Hub 6+00

97.1	97.3	96.9	96.3	95.5	94.7	93.7	91.8	90.7
3.3	3.1	3.5	4.1	4.9	5.7	6.7	8.6	9.7
64	44	25	9		14	22	39	50

98.1	98.3	97.3
2.3	2.1	3.1
87	100	110

94.9	95.9	97.4
5.5	4.5	3.0
156	144	126

Hub 9+00

89.1	89.5	91.0	91.5	92.2	92.5	91.6	91.6	91.1
8.2	7.8	6.3	5.8	5.1	4.8	5.7	5.7	6.2
50	36	28	16	8		22	40	50

89.1	89.1	88.8	90.3	90.5	91.0	91.6	91.2	90.4
8.2	8.2	7.5	7.0	6.8	6.3	5.7	6.1	6.9
50	41	30	15		14	26	41	50

Sta + 141 - Elev

897.34

10+50

11+00

+50

12+00

+50

May 14, 1958

Lt			Lt			Rt			20
88.9	88.2	89.3	89.0	88.9	89.1	88.9			
8.4	8.1	8.0	8.3	8.4	8.2	8.4		✓	
50	33	16		22	35	50			

88.4	88.2	88.1	86.9	88.2	88.2	88.5	87.0	88.0	88.2
8.9	9.1	9.2	10.4	9.1	9.1	8.8	10.3	9.3	9.1
50	30	11	5	16	37	42	47	50	
			to ditch				to ditch		

87.9	87.8	87.9	87.8	87.9	87.8	87.6
9.4	9.5	9.4	9.5	9.4	9.5	9.7
50	35	15		13	30	50

87.6	87.7	87.4	87.2	87.2	87.2	87.0
9.7	9.6	9.9	10.1	10.1	10.1	10.3
50	35	16		15	32	50

87.5	87.0	87.2	86.9	86.9	86.7	86.9
9.8	10.3	10.1	10.4	10.4	10.6	10.4
50	34	15		19	36	50

Sta	+	HI	-	Elev
-----	---	----	---	------

		897.34		
--	--	--------	--	--

13+00				
-------	--	--	--	--

+50				
-----	--	--	--	--

14+00				
-------	--	--	--	--

T.P.	10.94	898.42	9.86	887.48
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14+50				
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15+00				
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2 x 20

May 14, 1958

Lt.		Lt.		Rt.		21
87.1	87.1	86.9	86.7	86.5	86.7	86.7
10.2	10.2	10.4	10.6	10.8	10.6	10.6
50	34	15		18	36	50

87.0	86.9	86.6	86.4	86.5	86.7
10.3	10.4	10.7	10.9	10.8	10.6
50	30	10	15	38	50

86.8	86.8	86.7	86.6	86.3	86.2	86.4
10.5	10.5	10.6	10.7	11.0	11.1	10.9
50	28	15		17	35	50

86.7	86.7	86.5	86.5	86.4	86.3	86.3
11.7	11.7	11.9	11.9	12.0	12.1	12.1
50	33	15		20	35	50

86.7	86.7	86.7	86.5	86.5	86.5	86.4
11.7	11.7	11.7	11.9	11.9	11.9	12.0
50	32	17		16	35	50

Sta	+	HI	-	Elev
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		898.42		
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15+50				
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✓				
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15+64				
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			12.3	
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				86.12
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16+00				
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+50				
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17+00				
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22

May 14, 1958

Lt.

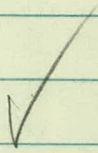
Lt.

Pt

22

86.1	86.9	86.9	86.7	86.6	86.5	86.5
12.3	11.5	11.5	11.7	11.8	11.9	11.9
£2 1/4 ch	24	19	16	32	50	
39						

87.2	87.1
11.2	11.3
44	50



£ 2" ditch

87.7	87.4	87.6	87.4	87.5	87.5	86.9
10.7	11.0	10.8	11.0	10.9	10.9	11.5
50	33	19		19	39	50

90.1	90.2	90.2	89.9	89.9	89.9	89.8
8.3	8.2	8.2	8.5	8.5	8.5	8.6
50	33	18		15	34	50

93.2	93.1	93.6	93.5	93.7	93.3	93.6
5.2	5.3	4.8	4.9	4.7	5.1	4.8
50	31	15		19	38	50

Sta + HI - Elev

898.42

17+50

✓

T.P. 11.43 908.89 0.96 897.46

17+50

18+00

✓

May 14, 1958

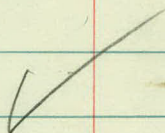
Lt		Rt.		23	
98.3	97.9	97.9	97.8	97.7	97.4
0.1	0.5	0.5	0.6	0.7	1.0
52	41	18		17	36
					59
					85



96.9
1.5
100

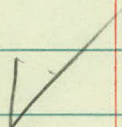
Boat Spike (P.I) Sta 17+48.3

98.8	99.9	01.1
10.1	9.0	7.8
63	85	100



01.1	01.3	01.8	02.3	02.7	03.0	02.7	02.6
7.8	7.6	7.1	6.6	6.2	5.9	6.2	6.3
55	41	20		19	39	62	83

02.3	03.2
6.6	5.7
79	100



02.2
6.7
100

Sta	+	HI	-	Elev
-----	---	----	---	------

		908.89		
--	--	--------	--	--

18+25				
-------	--	--	--	--

✓				
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+50				
-----	--	--	--	--

✓				
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+75				
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T. P.	3.37	907.27	4.99	903.90
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May 14, 1958

Lt.

2

Rt

24

02.5	02.6	03.8	04.6	04.7	04.9	04.3
6.4	6.3	5.1	4.3	4.2	4.0	4.6
60	37	19		16	40	63

03.3	04.3
5.6	4.6
82	100

✓

03.2	03.8
5.7	5.1
100	86

03.2	03.4	03.9	05.3	06.3	06.6	06.4
5.7	5.5	5.0	3.6	2.6	2.3	2.5
60	37	20		18	36	58

03.8	04.3
5.1	4.6
79	100

✓

05.8	06.1
3.1	2.8
100	80

05.2
3.7

28

spike SW cor school Property

Sta + π - Elev

907.27

18+75

✓

19+00

✓

19+27.25 beginning of school property

✓

88

RG
KP
AB

LH

2

May 15, 1938

Rt

25

03.7	03.5	04.0	05.2	05.7	06.3	07.2	07.2
3.6	3.8	3.3	2.1	1.6	1.0	0.1	0.1
66	36	10		3	22	56	62

04.0
3.3
100

✓

03.2	03.0	03.1	04.1	05.2	06.2	07.0	07.3
4.1	4.3	4.2	3.2	2.1	1.1	0.3	0.0
55	33	8		16	36	54	67

03.4
3.9
81

03.5
3.8
100

✓

02.8	02.4	02.6	03.5	03.6	04.6	05.8	06.7	06.2
4.5	4.9	4.7	3.8	3.7	2.7	1.5	0.6	1.1
53	25	9	4		24	48	75	100

03.1
4.2
84

03.0
4.3
100

02.8
4.5
130

06.4
0.9
195

06.0
1.3
179

05.4
1.9
153

05.7
1.6
123

02.3
5.0
150

06.6
1.3
200

29

Sta	+	T	-	Elev
-----	---	---	---	------

		907.27		
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19+50				
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✓				
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TD	5.19	906.26	6.20	901.07
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20+00				
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✓				
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MAY 15, 1958

26

4

4

PT

01.9	01.8	01.9	02.0	02.3	03.8	04.9	06.2
5.4	5.5	5.4	5.3	5.0	3.5	2.4	1.1
88	50	12		11	31	58	86

01.8	01.8	01.7	06.4	05.5	05.5	06.0
5.5	5.5	5.6	0.9	1.8	1.8	1.3
100	132	150	181	156	126	100

106.3
1.0
200

✓

sta 20

02.8
10

01.1	00.9	00.9	00.8	00.7	01.0	01.2	02.1	03.5
5.2	5.4	5.4	5.5	5.6	5.3	5.1	4.2	2.8
100	81	51	23		14	28	56	84

01.5
4.8
131

01.6
4.7
162

03.3
3.0
151

04.0
2.3
143

03.9
2.4
123

04.0
2.3
100

03.5
2.8
156

04.5
1.8
160

04.2
2.1
188

04.4
1.9
200

✓

30

Sta	+	π	-	Elev
-----	---	-------	---	------

		906.26		
--	--	--------	--	--

20+27				
-------	--	--	--	--

✓				
---	--	--	--	--

20+50				
-------	--	--	--	--

✓				
---	--	--	--	--

21+00				
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✓				
---	--	--	--	--

4

May 15. 1958 RT 27
 00.7 00.4 00.3 00.8 01.2 01.3
 5.6 5.9 6.0 5.1 5.0
 22 55 85 100

✓ 03.3 02.6 02.1 02.2
 3.0 3.7 4.2 4.1
 200 173 142 121

01.4 01.2 01.0 00.7 00.5 00.8 00.6 00.6 00.6
 4.9 5.1 5.3 5.6 5.8 5.5 5.7 5.7 5.7
 100 87 60 32 28 55 100 127

01.7 02.0 01.8 01.3 00.8 01.5
 4.6 4.3 4.5 5.0 5.5 4.8
 126 156 200 191 167 159

02.2 01.8 01.7 01.6 01.5 01.8 01.3 00.9 00.5
 4.1 4.5 4.6 4.7 4.8 4.5 5.0 5.4 5.8
 100 72 42 22 51 44 65 100

02.6 02.7 02.0 00.9 00.9 00.2
 3.7 3.6 6.3 5.4 6.4 6.1
 130 150 176 171 144 120

6.1 5.3 5.7
 188 197 200

Sta	+	π	-	Elev
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		906.26		
--	--	--------	--	--

21+50				
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✓				
---	--	--	--	--

21+65				
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✓				
---	--	--	--	--

22+00				
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✓				
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TP	5.94	911.13	1.07	905.19
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May 15, 1958

H

F

Rt

28

2.7	3.0	3.3	3.6	3.5	3.5	3.8	4.1	4.5
100	77	42	27		18	43	70	100

2.4	2.3				4.5	5.1	5.3	4.8
125	150				200	187	157	128

1.6	1.9	2.2	2.3	2.3	2.5	2.4	2.8	2.9
100	88	57	26		25	59	91	100

1.6	1.7				3.9	3.8	3.4	3.2
126	150				200	183	156	125

1.5	1.3	1.6	1.5	1.5	1.5	1.3	1.3	1.6
97	75	50	26		25	56	79	100

1.1	1.1				2.8	1.8	1.8	1.6
124	150				200	177	150	123

sta 22

32

Sta

+

π

-

Elev

911.13

22+50

✓

23+00

✓

23+50

✓

MAY 15, 1958

29

4

4

Pl

05.9	05.9	05.7	05.8	05.5	05.4	05.5	05.5	05.4
5.2	5.2	5.4	5.3	5.6	5.7	5.6	5.6	5.7
100	76	50	24		25	51	74	100

05.8	05.6
5.3	5.5
124	150

X

03.2	03.2	04.9	05.1
7.9	7.5	6.2	6.0
200	175	148	124

06.1	06.1	05.9	06.3	06.8	06.5	06.3	06.1	06.1
5.0	5.0	5.2	4.8	4.3	4.6	4.8	5.0	5.0
100	78	50	27		31	52	75	100

05.7	06.2
5.4	4.9
125	150

X

03.4	05.1	05.6	05.5
7.7	6.0	5.5	5.6
200	173	150	125

05.1	05.1	05.5	05.8	06.4	06.5	06.5	06.2	06.0
6.0	6.0	5.6	5.3	4.7	4.6	4.6	4.9	5.1
115	93	56	25		16	44	71	100

05.6
5.5
150

X

04.4	04.6	05.2	05.5
6.7	6.5	5.9	5.6
196	175	153	126

03.7
7.4
200

33

Sta	+	π	-	Elev
-----	---	-------	---	------

		911.13		
--	--	--------	--	--

24+00				
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✓				
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✓				
---	--	--	--	--

24+50				
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✓				
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TP	4.92	906.70	9.35	901.78
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LT

RT

RT

05.0	05.0	05.2	05.4	05.7	06.2	06.3	06.1
6.1	6.1	5.9	5.7	5.4	4.9	4.8	5.0
100	63	27		27	55	76	100

05.4	05.9		04.7	04.9	05.0	05.4
5.7	5.2		6.4	6.2	6.1	5.7
125	150		186	174	151	123

03.1
8.0
200

04.7	04.5	03.5	03.1	03.2	03.7	04.1	04.4	04.6
6.4	6.6	7.6	8.0	7.9	7.4	7.0	6.7	6.5
100	87	53	26		27	62	90	100

05.1	06.1		02.3	03.3	03.9	04.3
6.0	5.0		8.8	7.8	7.2	6.8
125	150		200	183	157	126

Sta + T - Elev

906.70

25+00

✓

25+21.12 end of school property

✓

25+50

✓

DE

MAY 15, 1958

31

LT

LT

RT

04.0	02.8	01.7	01.1	01.1	01.4	01.7	02.2	02.8
2.7	3.9	5.0	5.6	5.6	5.3	5.0	4.5	3.9
100	75	51	27		30	58	79	100

05.0	06.3				01.7	02.3	02.4	02.6
1.7	0.4				5.0	4.4	4.3	4.1
125	150				200	173	148	123

03.3	01.9	00.6	00.1	900.0	00.0	00.3	01.0	01.4
3.4	4.8	6.1	6.6	6.7	6.7	6.4	5.7	5.3
100	75	50	26		25	52	76	100

04.9	06.0				00.8	01.4	01.4	01.6
1.8	0.7				5.9	5.3	5.3	5.1
125	150				200	172	149	123

01.8	00.2	98.6	97.7	97.5	97.7	98.5	98.8	99.1
4.9	6.5	8.1	9.0	9.2	9.0	8.2	7.9	7.6
100	74	51	25		23	48	75	100

03.5	04.8				99.6	99.7	99.6	99.3
3.2	1.9				7.1	7.0	7.1	7.4
125	150				200	174	150	125

Sta + π - Elev

906.70

26+00

✓

26+46 Top Backslope

✓

TP 3.93 897.^{.78}88 12.85 893.^{.85}95

26+54 E ditch

✓

23

4

4

PT

98.6	94.9	93.9	94.1	94.5-	95.7	96.6	97.1
8.1	11.8	12.8	12.6	12.2	11.0	10.1	9.6
76	46	23		24	48	74	100

00.0	01.7	08.3	99.7	97.4	97.4	97.1	96.8
6.7	5.0	3.4	7.0	9.3	9.3	9.6	9.9
100	125	150	154	200	178	154	127

98.1	96.1	93.5-	96.1 10.6 165 93.2	93.1	93.5-	93.5-	93.6	94.2
8.6	10.6	13.2	13.5	13.6	13.2	13.2	13.1	12.5
82	64	38	23		24	47	76	100

98.8	95.1	95.0	95.4	96.0	95.9	95.7	95.3
7.9	11.6	11.7	11.3	10.7	10.8	11.0	11.4
92	100	138	150	200	180	156	125

spike at Lexington sta 26+79.12

94.0	93.6	92.9	91.7	91.5-	91.4	91.1	91.2	91.0
3.8	4.2	4.9	6.1	6.3	6.4	6.7	6.6	6.8
100	80	54	23		16	43	71	100

94.6	95.1			91.4	91.6	91.2	90.9	90.9
3.2	2.7			6.4	6.2	6.6	6.9	6.9
130	150			210	188	152	137	120

Sta + π - Elev

^{.78}
897.88

26+62 edge of shoulder

v

26+70 edge of blacktop

26+79.12 $\pm$ Lexington

26+78.65

BM

5.37

892.41

892.51

892.23

MAY 15, 1958

4

4

RT

33

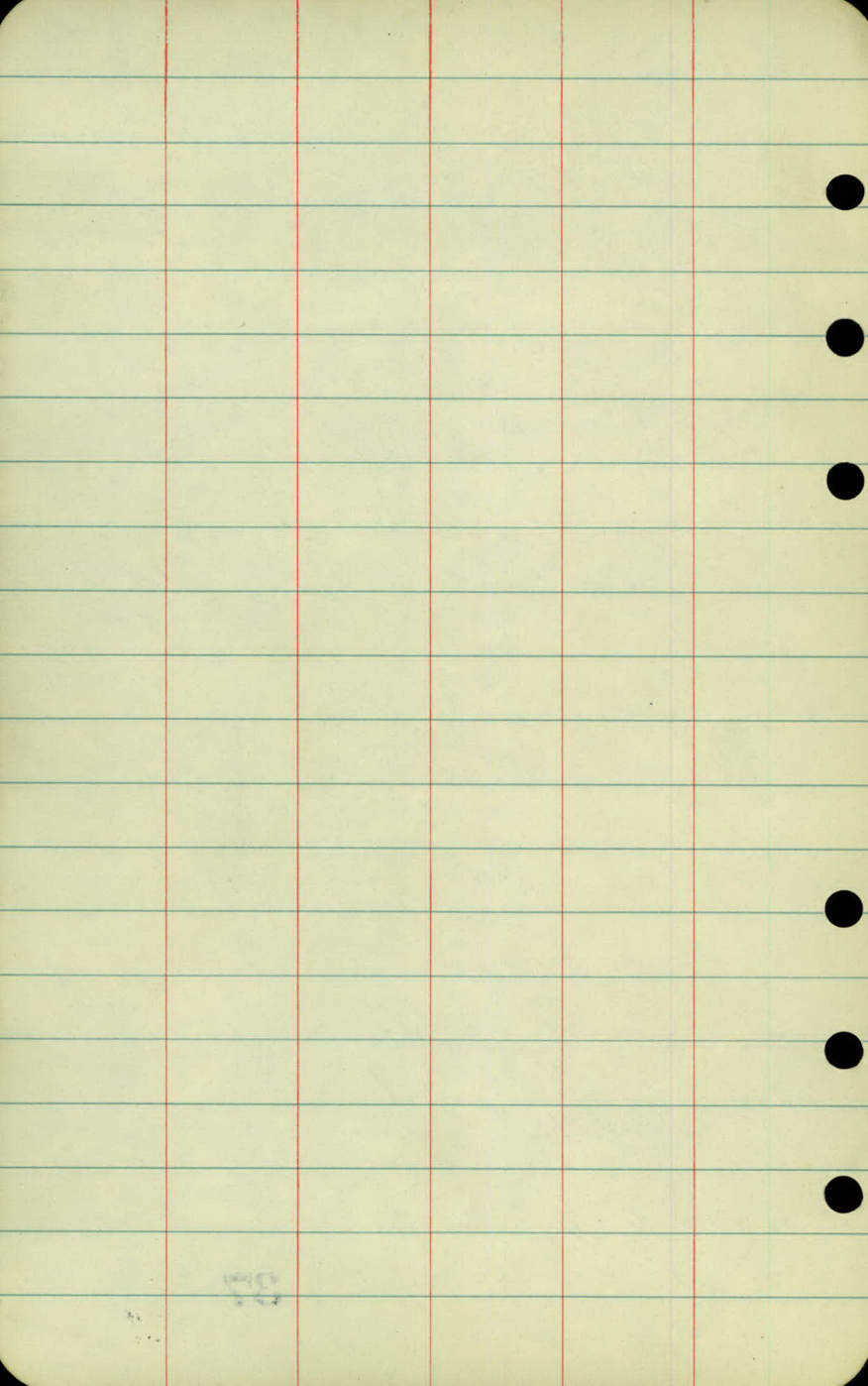
94.7	94.2	93.7	93.4	92.9	92.8	92.7	92.6
3.1	3.6	4.1	4.4	4.9	5.0	5.1	5.2
82	51	23		26	53	78	100

94.9	95.2	95.3		92.8	92.6	92.7	92.7
2.9	2.6	2.5		5.0	5.2	5.1	5.1
100	125	150		200	175	150	125

96.7	96.1	95.2	94.4	93.7	93.2	92.9	92.7	93.1	93.1
1.1	1.7	2.6	3.4	4.1	4.6	4.9	5.1	4.7	4.7
200	150	100	50		40	75	100	150	200

96.9	96.3	95.5	94.6	93.9	93.3	93.0	93.4	93.3
0.9	1.5	2.3	3.2	3.9	4.5	4.8	4.4	4.5
200	150	100	50		50	100	150	200

Spike in PP SW cor Lexe Co R/I



JA
RR
SR
RM
JM

August 13, 1958

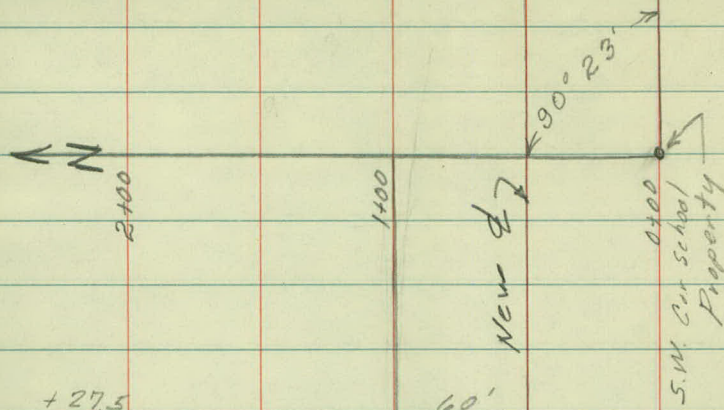
1

Co Rd I

Hamline to Lexington

x-section Extensions

Original Borrow Pit A



+ 27.5

60'

19

59.85

+ 75

59.70

+ 50

59.55

18+30. ? PT

+ 25

59.4

18

59.0

+ 50

57.2

17

54.1

August 13, 1958 2

Sta	+	π	-	Elev
20+00	7.93	908.63		900.7
22+00	3.83	908.63		904.8
$\pm$ Lev				893.9

Borrow Pit X-Sections

1+00

✓

1+50

✓

Lt

August 13, 1958

3

04.2	04.1	04.5	04.5	03.8	03.2
44	45	41	41	48	54
100	90	66	48	25	

02.6	00.9	98.3	95.6	94.3	
6.0	7.7	10.3	13.0	14.3	55
120	140	170	190	200	

04.3	04.9	04.4	03.8	03.4	03.0	02.6
4.3	3.7	4.2	4.8	5.2	5.6	6.0
120	100	80	60	40	20	

03.3	01.4	99.2	95.9	93.7	
5.3	7.2	9.4	12.7	14.9	
140	160	180	200	2.15	

Sta + π - Elev

908.63

2+00

✓

+50

✓

3

OP

August 13, 1958

4

14

4

5.1	5.9	6.0	6.6	6.9	7.3
100	80	60	40	20	

03.5

02.7

02.6

02.0

01.7

01.3

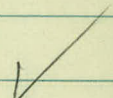
03.8

03.6

01.5

98.3

94.4



4.8	5.0	7.1	10.3	14.2	5.5
125	150	175	200	225	

01.5

01.9

01.7

01.9

01.4

00.9

00.8

7.1	6.7	6.9	6.7	7.2	7.7	7.8
125	100	80	60	40	20	

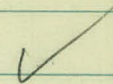
00.9

00.7

98.9

95.6

94.2



7.7	7.9	9.7	13.0	14.4	
150	175	200	225	250	

98.2

99.3

99.5

99.7

99.6

00.8

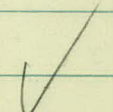
10.4	9.3	9.1	8.9	9.0	7.8
125	100	75	50	25	

97.0

96.0

95.4

94.4



11.6	12.6	13.2	14.2	
150	175	200	225	

Sta	+	x	-	Elev
-----	---	---	---	------

		908.63		
--	--	--------	--	--

3+50				
------	--	--	--	--

✓				
---	--	--	--	--

4				
---	--	--	--	--

+50				
-----	--	--	--	--

5				
---	--	--	--	--

April 13, 1958

5

4

14

95.0

96.5

97.6

97.9

98.0

99.3

13.6
125

12.1
100

11.0
75

10.7
50

10.6
25

9.3

93.6
15.0
150

✓

94.1

95.1

96.1

97.7

99.4

14.5
100

13.5
75

12.5
50

10.9
25

9.2

✓

93.7

95.2

97.9

14.9
50

13.4
25

10.7

✓

93.8
148

Sta	+	π	-	X-Section Extensions from Elev Old Line
		908.63		
19+27.5				
+50				
20				
+27				
+50				
21				
+50				
+65				
22				
TP	A.56	910.06	3.13	905.50
SD				

August 13, 1958

6

Lt

200 7.3 01.3
175 6.8 01.8

200 7.7 00.9

175 7.3 01.3

200 7.0 01.6

175 6.8 01.8

200 6.4 02.2

175 6.7 01.9

200 6.0 02.6

175 6.3 02.3

200 5.4 03.2

175 5.7 02.9

200 4.8 03.8

175 4.6 04.0

200 4.0 04.6

175 3.8 04.8

200 3.8 04.8

175 3.7 04.9

Sta + π - Elev

910.06

22+50

23

+50

24

+50

25

+21.12

ϕ Lev

16.2 893.86 893.90

August 13, 1958

7

44

07.1
3.0
200

07.4
2.7
200

07.5
2.6
200

08.4
1.7
200

08.4
1.7
200

06.1
4.0
200
06.8
3.3
175

06.8
3.3
175

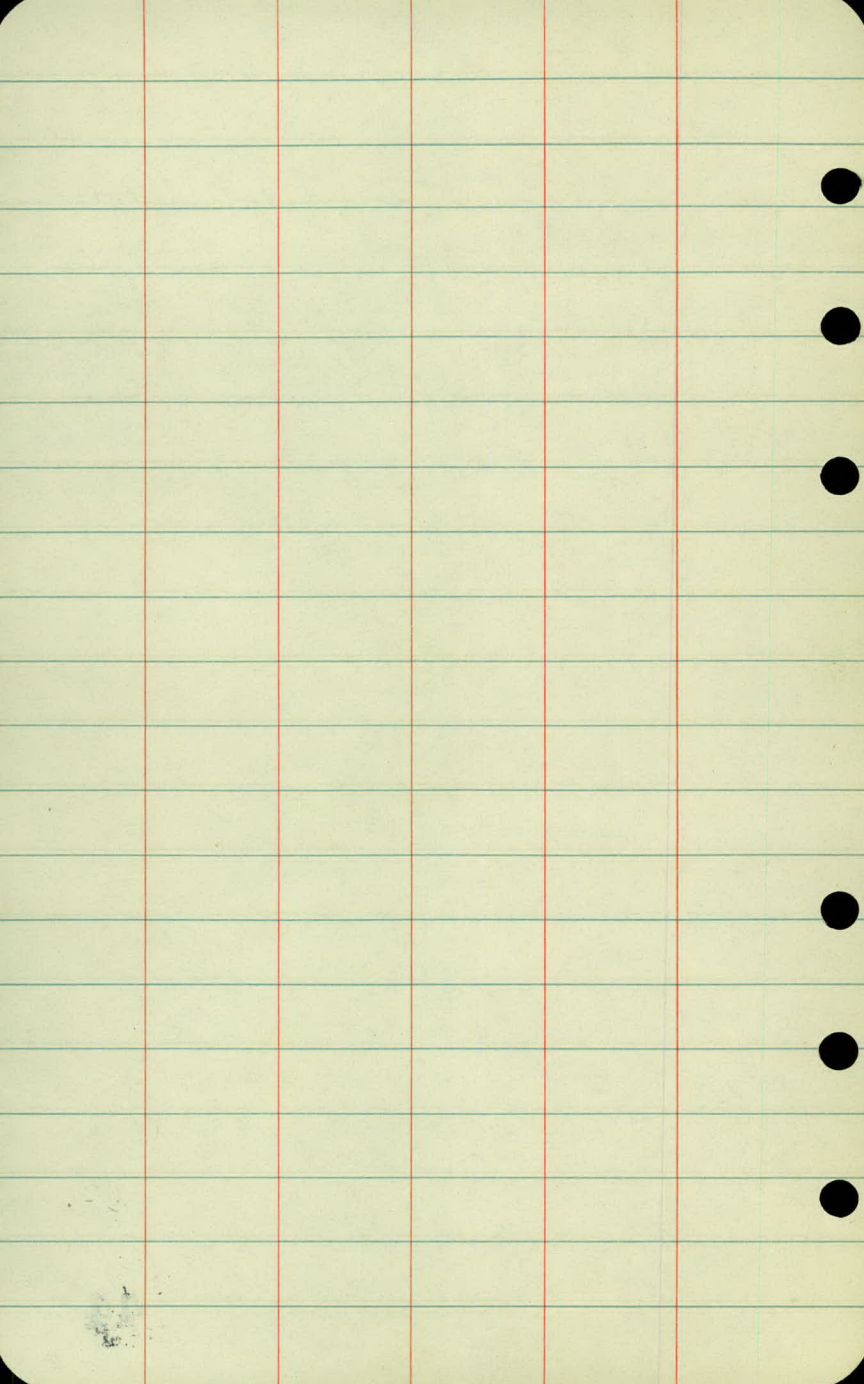
07.4
2.7
300
07.8
2.3
175

06.0
4.1 ✓
175

06.6
3.5 ✓
175

07.1
3.0 ✓
175

07.5
2.6 ✓
175



Swamp Locations

Co. Rd "I" Hamlin To Lex

Object	Az.	Dist
⊙ at Sta 0+00		
to P.L. Sta 4+85	90°00'	485'

Swamp at Shoulder	9°20'	109
-------------------	-------	-----

Swamp	41°35'	112
-------	--------	-----

"	60°40'	168
---	--------	-----

"	66°50'	235
---	--------	-----

"	56°50'	252
---	--------	-----

"	47°30'	217
---	--------	-----

"	29°40'	190
---	--------	-----

"	21°40'	245'
---	--------	------

"	24°50'	320
---	--------	-----

"	33°15'	350
---	--------	-----

"	43°05'	342
---	--------	-----

"	52°05'	314
---	--------	-----

"	64°45'	278
---	--------	-----

"	74°30'	280
---	--------	-----

"	75°55'	330
---	--------	-----

"	85°20'	344
---	--------	-----

plattner

OBJECT

May 6, 1958

AZ DIST

35

Swamp

94°30' 340

"

103°20' 324

"

113°25' 325

"

121°30' 360

"

129°00' 410

"

133°45' 455

"

136°40' 510

"

139°10' 560

"

138°50' 620

Swamp at
water dept R/W

143°25' 685

platted.

Obj	Az	Stadia	
at Sta 7+27.31 P.T.			
to PI Sta 4+85	284°38 $\frac{1}{2}$ '		
Edge of Swamp	248°20'	212'	
"	238°50'	247'	
"	229°00'	285'	
"	222°05'	326'	
"	216°55'	370'	
"	213°00'	422'	
"	208°40'	466'	
"	204°20'	500'	
"	198°45'	514'	
£4' ditch	201°30'	528'	Flowing East to West
"	205°20'	540'	
"	208°45'	586'	
"	211°45'	580'	
to Sta 8+00			
Edge of Swamp	31°07'	62'	
"	353°40'	85'	
"	342°15'	135'	
"	334°20'	184'	

FK Vert Rod May 16, 1958 36
 RG Dist Angle Equiv. Rod Diff. Elev
 AB

11.7

11.6

12.0

11.8

X section & Elev. = 892.3
 L.C.

3.88

?
 892.84

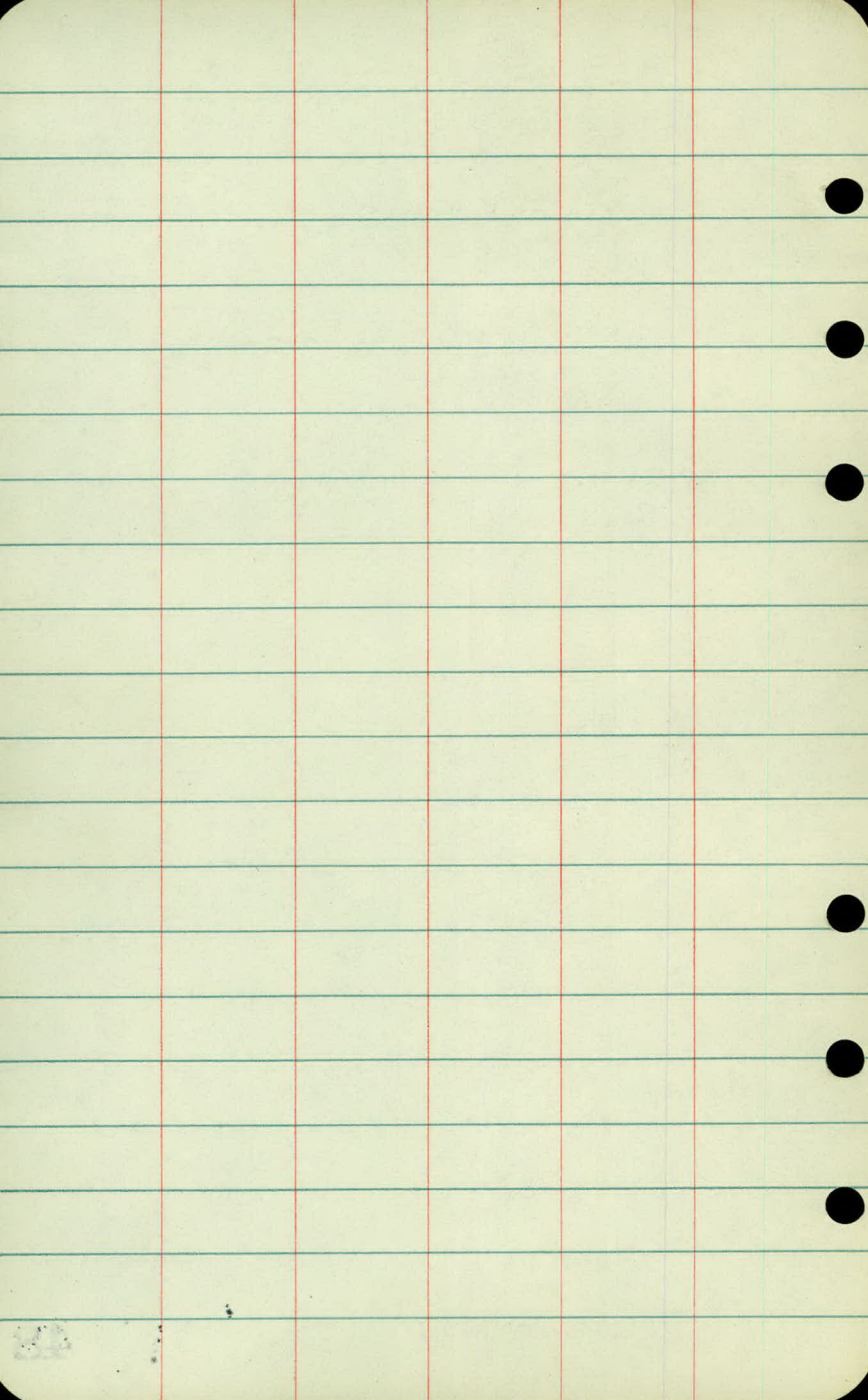
Obj	A2	Stadia
Edge of Swamp	328°20'	237'
"	324°15'	289'
"	324°15'	348'
"	325°00'	402'
"	327°50'	460'
"	325°00'	518'
"	325°55'	583'
"	328°00'	630'
"	333°07'	657'
"	337°25'	669'
"	342°35'	660'

FK
RG
AB

Vert.
Angle
Equiv
Rod
Ditt
Elev

May 16, 1958 37

Platted



May 12, 1958

38

Building Locations

Stadia

Object Az Stadia

At P.T. Sta 19+88.07

to Sta 26 90° 00'

S.E. Cor 4' x 4' ^{Cob} Shed 245° 55' 110 ..

N.E. Cor Garage 241° 40' 123 ..
15.5 x 12.3

S.E. Cor Garage 235° 20' 132 ..

N.W. Cor Shed 228° 20' 131 ..
30' x 8.4'

N.E. Cor Shed 217° 05' 112 ..

N.W. Cor House 193° — 166 ..

N.E. Cor House } 25' 184° 15' 163 ..

S.E. Cor House } 45.5 184° — 209 ..

NE Cor Pump Ho } N 8.2 S E 6.3 W 207° 25' 182 ..

NE Cor Toilet } N 4' S E 5' W 204° 30' 220 ..

At P.I. Sta 17+45.34 Same as 17+48.3 (Profile)

To Sta 26+00 Az 90°-00'

NW Cor Granery 137° 30' 130' 16' E + W

SW Cor Granery 140° 05' 150' 12' N + S

NE Cor Granery 132° 15' 148'

NW Cor. Corn Crib 130° 45' 150' 7' E + W
16' N + S

Vert Rod May 12, 1958 39
 Dist Angle Equiv. Rod Diff Elev

H.I. 5.1

+1° 01' +1.9 1.0 +0.9

+2° 50' +6.1 5.0 +1.1

+2° 38' +6.1 5.0 +1.1

+1° 15' +2.9 2.0 +0.9

+0° 46' +1.5 1.0 +0.5

— 0.5

— 0.92

+1° — +3.6 4.0 -0.4

+1° 04' +3.4 2.0 +1.4

+0° 33' +2.1 3.0 -0.9

H.I. = 5.2

+1° 35' +3.6 2.0 +1.6

+1° 35' +4.1 2.4 +1.7

+1° 48' +4.6 2.0 +2.6

+3° 00' +7.8 5.0 +2.8

Object	Az	Stadia	
NE Cor Corn Crib	128°15'	153'	32.5' N + S 24.5' E + W
NE Cor Barn	147°02'	155'	
NE Cor. Machine Shed	140°10'	233'	32.5' E + W 14' N + S

Vert Rod

May 12, 1958

May 12, 1958

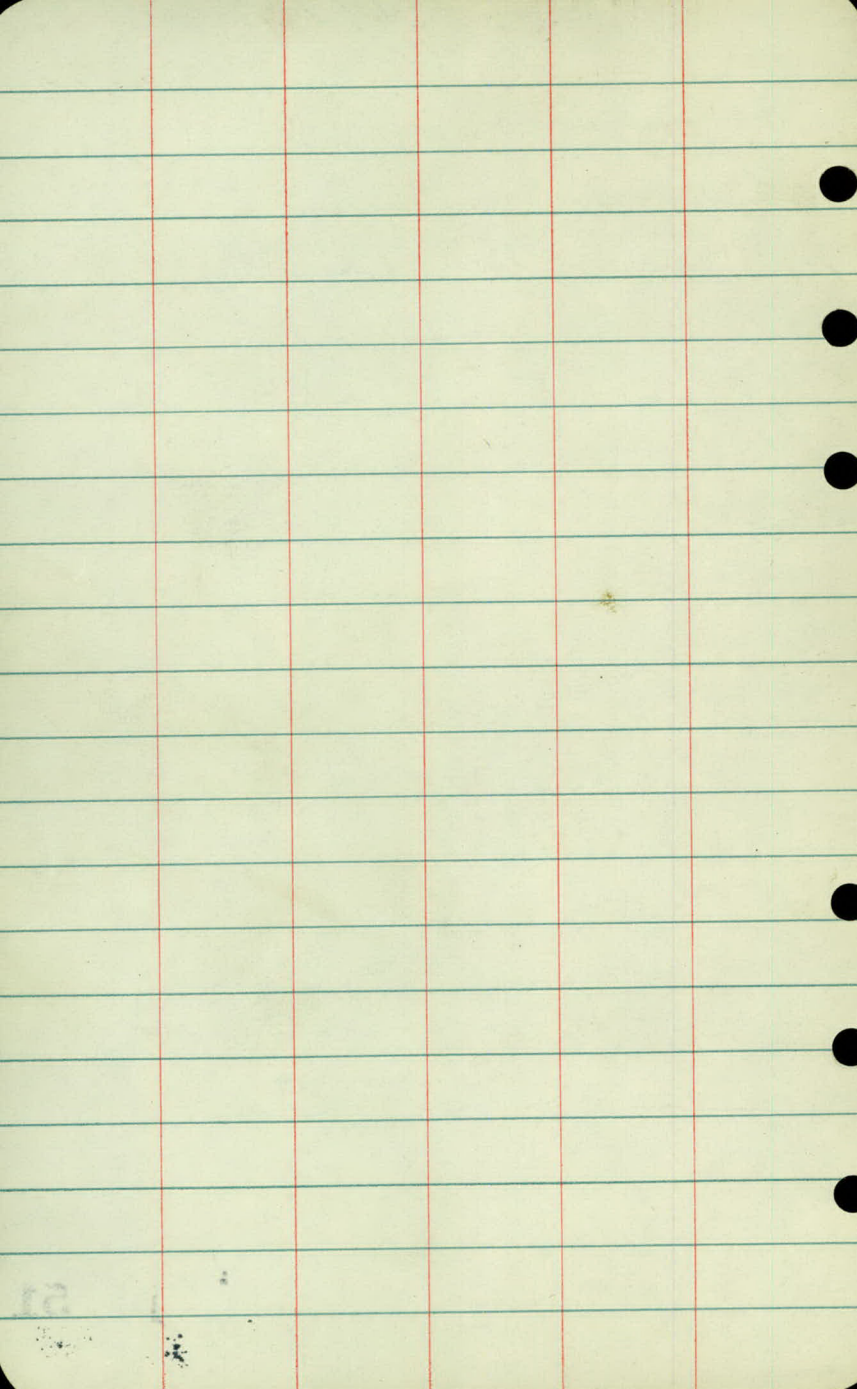
Dist	Angle	Equiv	Rod	Diff	Elev 40
------	-------	-------	-----	------	---------

+3°00'	+8.0	4.6'	+3.4		
--------	------	------	------	--	--

—

0.1

+2°00'	+8.1	6.0	+2.1		
--------	------	-----	------	--	--



May 16, 1958
Fair 65°

41

Soundings

Equipment: $\frac{1}{2}$ " Push Rod
Post Hole digger
2" Earth Auger
6" Post Hole Auger

Note: Post Hole Digger used 0-3'

Sta 0+21 Φ Elev 887.7

Feet

Push
Rod

Material

0-1

1-2

2-3

3-3.7

3.7-4

4-5

Auger Soundings

Peat

Sand

May 16, 1958

42

Sta 0+20

35' Rt Elev 887.8

Feet

Push
Rod

Material

0-1

1-2

2-3

3-4

4-5

5-6

Auger Soundings

Peat

Fibrous
Peat

Peat

sand

Sta 0+20

35' Lt Elev 887.4

Feet

Push
Rod

Material

0-1

1-2

2-3

3-4

4-5

5-6

Auger Soundings

Peat

Fibrous
Peat

Sand

clay

May 16, 1958

43

Sta 0+50

£

887.6

Feet

Push
Rod

Material

0-1

1-2

2-3

3-4

4-5

5-6

6-6.5



Auger Soundings

Peat
Sand

Sta 0+50

35' Bl Elev. 887.0

Feet

Push
Rod

Material

0-1

1-2

2-3

3-4

4-5

5-6

6-6.5

6.5-7

6

7-8

8-9

9-10

Auger Soundings

Peat

Peat Sand

Sand

Y

May 16, 1958

44

Sta 0+50

35' Lt Elev 887.5

Feet

Push
Rod

Material

0-1

1-1½

1½-2½

2½-3½

3½-4

4-5

5-6

Auger Soundings

peat

Fiberus

peat

sand

clay

Sta 1+00 Elev. 886.2

Feet Push Rod Material

0-1

1-2

2-2.5

2.5-3

3-4

4-5



Auger Soundings

Peat
Sand

May 16, 1958

45

Sta 1400 35' RT Elev 886.2

Feet

Push
Rod

Material

0-1

1-2

2-3

3-4

4-5

5-6

6-7

Auger Soundings

Peat

Sand

Sta 1+00 35' Lt Elev 886.9

Feet

Push
Rod

Material

0-1

1-1½

1½-2

2-3

3-4

4-5

5-6

↑
Soundings
↓
Peat
↓
Sand
↓
Gravel
↓
Auger

May 16, 1958 46

Sta 1150

35' RT Elev 886.6

Feet

Push
Rod

Material

0-1

1-2

2-3

3-4

4-5

5-6

Auger Soundings

Peat

Sand

Sta 1+50 ± Elev. 887.2

Feet

Push
Rod

Material

0-1

1-2

2-3

3-4

4-5

5-6

Auger Soundings

Peat

sand

clay

May 16, 1958 47

Sta 1+50 35' Lt Elev 887.6

Feet Push Rod Material

0-1

1-2

2-2½

2½-3

3-4

4-5

Anger Soundings

Peat

Sand

clay

Sta 2+00 ± Elev. 887.0
Feet Push Rod Material

0-1

1-2

2-3

3-4

4-5

5-6

Auger Soundings

peat

sand

clay

FK
RG
KP
AB

May 19, 1958

48

Sta 2+00 35' Lt Elev

Feet	Push Rod	Material
0-1		
1-2		
2-2½		
2½-3		
3-4		
4-4½		
4½-5		
5-6		

Auger Soundings

Peat

sand

clay

sand

Sta 2+00 35' Rt. Elev.

Feet Push Rod Material

0-1

1-2

2-3

3-4

4-5

5-6

6-6 $\frac{1}{2}$

6 $\frac{1}{2}$ -7

Auger Soundings

peat

clay

sand

May 19, 1958

49

Sta 2+50 ±

Elev.

Feet

Push
Rod

Material

0-1

Peat

1-2

Fibers

Peat

2-3

3-4

4-5

5-6

6-7

7-8

8-9

9-10

10-11

11-12

12-13

Soundings

Auger

Peat

Clay

Sta	2+50	35' Lt	Elev
	Feet	Push Rod	Material
0-1			
1-2			
2-3			
3-4			
4-5			
5-6			
6-7			
7-8			
8-9			
9-10			
10-11			
11-12			
12-13			
13-14			

Auger Soundings

Peat

clay

May 19, 1958

50

Sta 2+50

35' Rt Elev

Feet

Push
Rod

Material

0-1

1-2

2-3

3-4

4-5

5-6

6-7

7-8

8-9

9-10

10-11

Auger Soundings

Peat

Clay

Sta 3+00 ±

Elev.

Push

Rod

Material

Feet

0-1

1-2

2-3

3-4

4-5

5-6

6-7

7-8

8-9

Auger Soundings

Peat

Clay

Y

May 19, 1958

51

Sta 3400 35' Rt - Elev

Feet

Push
Rod

Material

0-1

1-2

2-3

3-4

4-5

5-6

6-7

Auger Soundings

Top soil

Fibers

Peat

Sand
with
Peat
in
it

clay

Sta 3+00 35' Lt Elev.

Feet

Push
Rod

Material

0-1

1-2

2-3

3-4

4-5

5-6

6-7

7-8

Auger Soundings

Peat

Sand
&
Peat

Sand

Y

May 19, 1958

52

Sta 3+50 ±

Elev.

Feet

Push
Rod

Material

0-1

↓

↓ Topsoil

1-2

↓ sand

Sta 6400 35' Rt Elev

Feet

Push
Rod Material

0-1

Topsoil

1-2



sand

2-3

May 19, 1958

53

Sta 6+50

35' Rt Elev.

Feet

Push
Rod

Material

0-1

Topsoil

1-2

2-3

sand

3-4

Sta 7+00 35' Rt Elev

Feet Push Rod Material

0-1

Topsoil

1-2

2-3

Y

Y sand

May 19, 1957

54

Sta 7+50 35' Rt Elev.

Feet

Push
Rod

Material

0-1

Topsoil

1-2

↓

↓

2-3

Sand

Sta 8+00 35' Rt Elev

Feet	Push Rod	Material
------	----------	----------

0-1		
-----	--	--

1-2		
-----	--	--

2-3		
-----	--	--

Topsoil

Sand

May 19, 1958

55

Sta 8+00 35' Lt. Elev.

Feet

Push
Rod

Material

0-1

Topsoil

1-2

↓

↓

2-3

↓

Sand

Sta 8+50 35' Lt. Elev.

Feet	Push Rod	Material
------	-------------	----------

0-1		Topsoil
-----	--	---------

1-2	Y	
-----	---	--

2-3		sand
-----	--	------

May 19, 1958

56

Sta 9+00 35' Lt. Elev.

Feet

Push

Rod

Material

0-1

Topsoil

1-2

2-3

sand

Sta 10+00 35' Lt Elev

Feet	Push Rod	Material
0-1	↓	Peat
1-2	↓	↑
2-3		sand

May 19, 1958

57

Sta 10+50 ±

Elev

Feet

Push
Rod

Material

0-1

Peat

1-2

Y

Sand

2-3

Sta 10+50 35' Lt Elev

Feet

Push
Rod

Material

0-1

Peat

1-2

Sand

2-3

Y

May 19, 1958

58

Sta 10+50 35' Rt Elev.

Feet Push Rod Material

0-1

Topsoil

1-2

↓

2-3

↑
Sand

Sta 11+00 ± Elev

Feet

Push
Rod

Material

0-1

Peat

1-2

Fibervus

Peat

2-3

Peat

3-4

Sand

4-5

↑ Auger Soundings ↑

May 19, 1958

59

Sta 11+00 35' Rt Elev

Feet

Push
Rod

Material

0-1

1-2

2-3

3-4

4-5

Auger Soundings

Frozen
PeatFibrous
Peat

Sand

Sta 11+00 35' Lt. Elev.

Feet

Push
Rod

Material

0-1

1-2

2-3

3-4

4-5

5-6

Frozen
Peat

Fibrous
Peat

Peat

Sand

Auger Soundings

May 19, 1958

60

Sta 11+50 ±

Elev
Push
Rod

Feet

Material

0-1

Frozen
Peat

1-2

Fibrous
Peat

2-3

Fibrous
Peat

3-4

Peat

4-5

Peat

5-6

Sand

6-7

7-8

Auger Soundings

↓

↓

Sta 11750 35' Rt Elev

Feet

Push
Rod

Material

0-1

1-2

2-3

3-4

4-5

5-6

6-7

7-8

8-9

9-10

↑
Auger Soundings
No Fibers
Frozen
Peat
Peat

Y

May 19, 1958

61

Sta 11+50 35' Lt Elev.

Feet

Push
Rod

Material

0-1

1-2

2-3

3-4

4-5

5-6

↑
Auger Soundings
↓

Peat

Peat
Fibers
Peat

Peat



Sta 12+00 ±

Elev

Push

Rod

Material

Feet

0-1

1-2

2-3

3-4

4-5

5-6

6-7

16'

Y

Peat

Fibers

Peat

Peat

May 19, 1958

62

Sta 12+00 35' Rt

Elev

Push
Rod

Material

Feet

0-1

1-2

2-3

3-4

4-5

5-6

6-7

Auger Soundings
No Fibrous Root

Peat

18'

Sta 13+00 $\frac{1}{2}$

Flav

Push Rod

Material

0-1

1-2

2-3

3-4

4-5

5-6

No Fibers Peat
Peat

23

May 19, 1958

63

Sta 13+00 35' Lt Elev.

Feet Push Rod Material

0-1

1-2

2-3

3-4

4-5

5-6

6-7

Auger Soundings
No Fibrous Plant
Plant

26'

Y

Sta 14100 ±

Elev
Push
Rod

Feet

Material

0-1

1-2

2-3

3-4

4-5

5-6

6-7

Fibrous
Peat

Auger Soundings

Peat

16

Y

May 19, 1958

64

Sta 15+00 ±

Elev.

Push

Rod

Material

Feet

0-1

1-2

2-3

3-4

4-5

5-6

6-7

7-8

No Fibrous Peat

Peat

25'

Y

Sta 15+50 ± Elev

Feet

Push
Rod

Material

0-1

1-2

2-3

3-4

4-5

5-6

↑
Auger Soundings
↓

No Fibrous Peat
Peat

22

Y

FX
RG
KP
AB

May 20, 1958

65

Sta 16100 ± Elev.

Feet

Push
Rod

Material

0-1

1-2

2-3

3-4

4-5

Y

Anger Soundings

Peat

Sand

Peat

Sand

Sta- 15 + 75

±

Elev

Feet

Push
Rod

Material

0-1

1-2

2-3

3-4

4-5

5-6

Auger Soundings

peat

sand

peat

sand

13'

Y

May 20, 1958

66

Sta 15+75 35' Rt Elev

Feet Push Rod Material

0-1

1-2

2-3

3-4

4-5

5-6

6-7

12'

Anger Soundings
Peat
Sand
Sand & Peat
Sand

Sta 15+75 35' LT Elev.

Feet

Push
Rod

Material

0-1

1-2

2-3

3-4

4-5

5-6

Auger Soundings

Peat
sand

13'



May 20, 1958

67

Sta 12+00 35' Lt

Elev

Feet

Push
Rod

Material

0-1

1-2

2-3

3-4

4-5

5-6

Auger Soundings

Peat

Fibers

Peat

Peat

13'

Y

Sta 16+00 35' Lt Elev

Feet

Push
Rod

Material

0-1

Topsoil

1-2

Sand

2-3

3-4

↓

May 20, 1958

68

Sta 16+00 35' BT

Elev

Push
Rod

Material

Feet

0-1

Topsoil

1-2

2-3

sand

3-4

Y

Push Sta	Rod	Swamp Depth	
	35' Lt	2	35' Rt
12+25	17'	21	22'
12+50	24'	26	20 P
13+00	26'	23	16' P
+50	26'	19 Rock	18 P
14	17'	16	17' P
+50	20'	21 Rock	30' P
15	26'	25	30' P
+50	16'	22	20' P

May 20, 1958

69

17-54.34
1 57.52
15796.82

50.87
45.00
61.65
157.52

UB

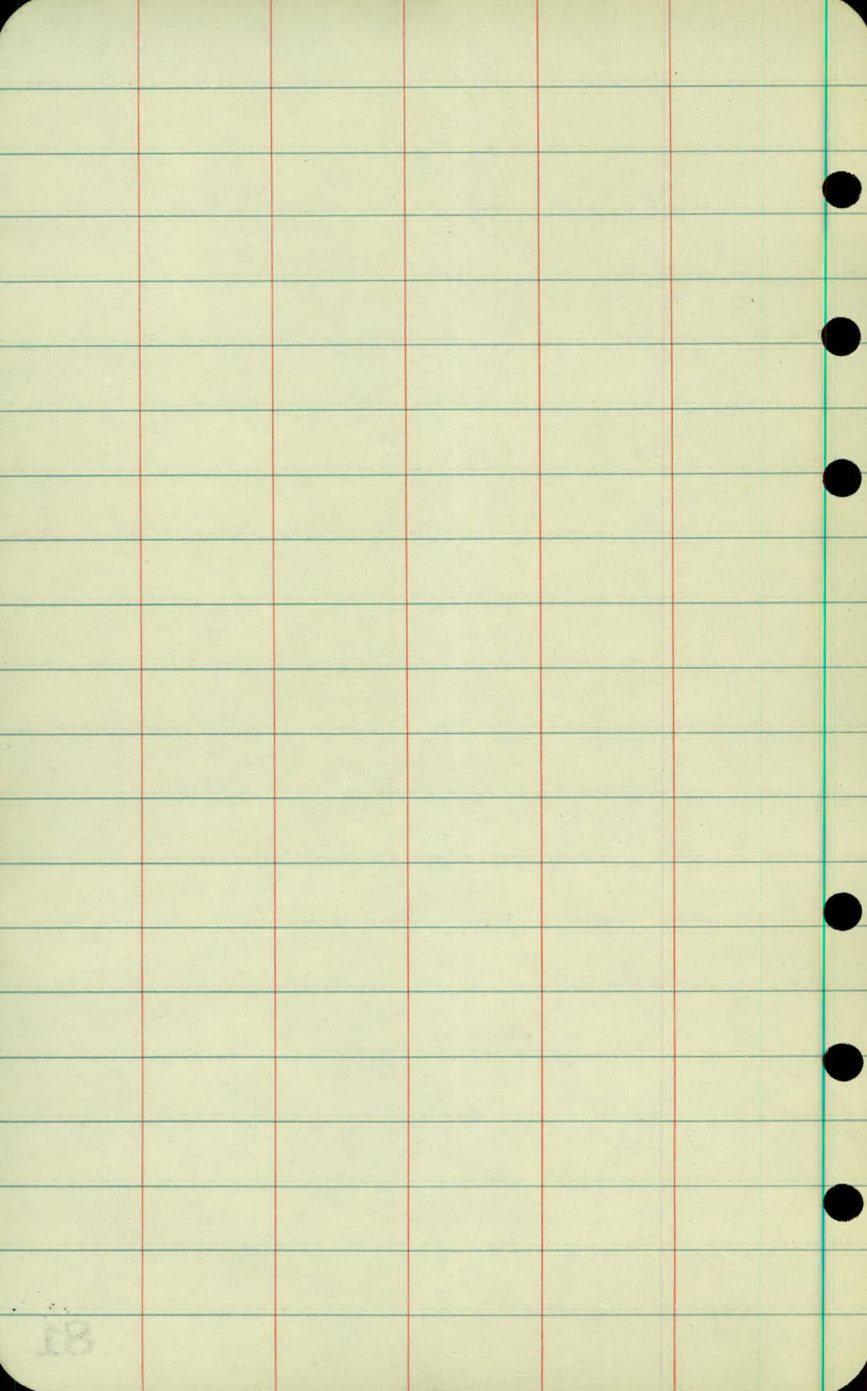
AUGUST 12, 1958 1

KP
RL

CO. RD. "I"

LEXINGTON - HAMLINE

SOUNDINGS



Sta.

50' LT.

25' LT

25' RT

50' RT.

Kt.

Kt.

12+50

23'

20'

13+00

24

*

x

16

13+50?

22

x

x

15

14+00

14

16

14+50?

20

x

x
24+

15+00?

18

x

x

x

x
20

15+50

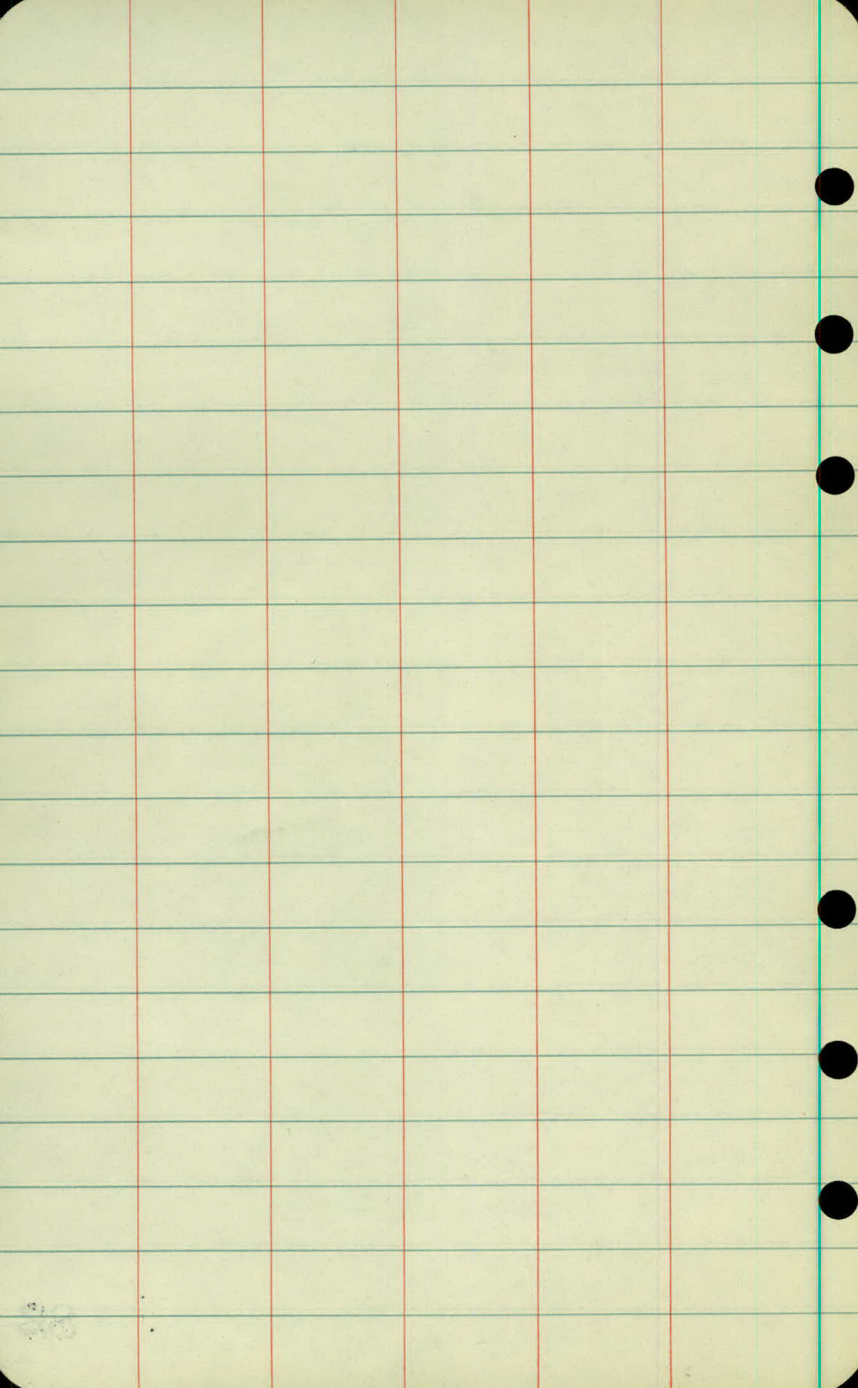
13'

+

x

x

x
24+



July 18, 1958

~~86~~
38

"B" Line Additional
Topography

May Have Been Located on Original Line

$$+66 \frac{32''0}{8}$$

$$+33 \frac{26''0}{10'}$$

17

$$+84 \frac{26''W}{19}$$

16

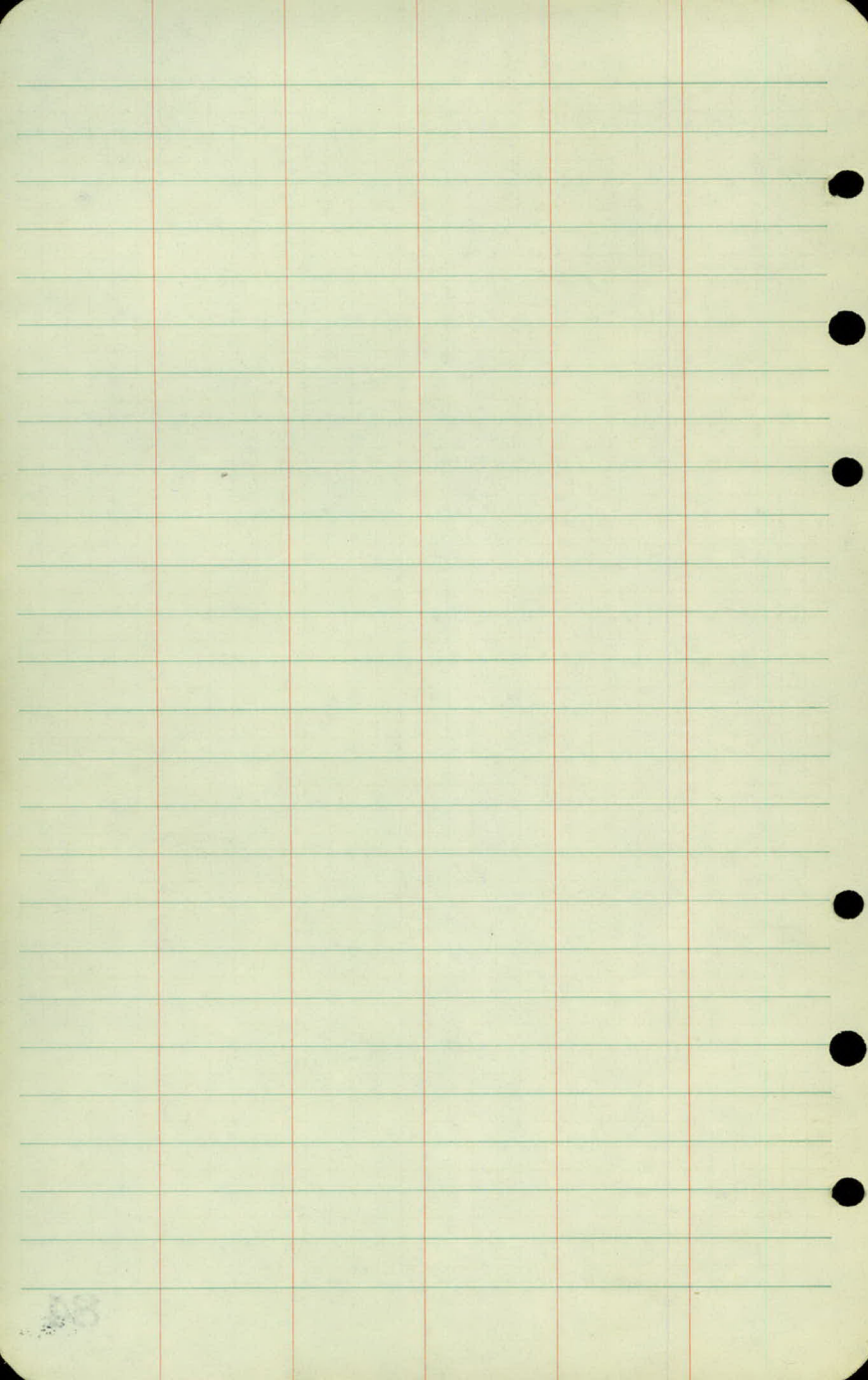
July 18, 1958

37
37

23

23

23



July 18, 1958

~~38~~
40

"B" Line

x-sections

Sta	+	π	-	Elev
-----	---	-------	---	------

BM	1.09	904.99		903.90
----	------	--------	--	--------

No Change to Sta 16+00

T.P.	2.35	896.32	11.02	893.97
------	------	--------	-------	--------

16

+50

17

TP	9.49	903.50	2.31	894.01
----	------	--------	------	--------

+50

18

T.P.	8.27	910.45	1.32	902.18
------	------	--------	------	--------

± July 18, 1958

39

21

41

41

Spike S.W. Cor School Property

8.4	8.6	8.8	8.8	8.7	6.6	8.5	8.3	8.5
50	41	28	15		15	28	41	50

6.3	6.2	6.1	5.9	6.0	6.2	6.3	6.2	6.4
50	42	29	14		15	30	40	50

2.5	2.9	3.1	3.1	2.9	2.7	2.7	2.6	2.7
50	41	26	13		12	25	39	50

4.9	5.4	5.4	5.9	5.7	5.5	5.6	5.3	5.4
50	40	27	10		14	28	41	50

1.1	1.4	1.9	1.4	1.8	1.3	0.9	0.5	0.4
50	47	34	17		14	27	40	50

18 stake

Sta + π - Elev

910.45

18+25

+50

+75

19

BM 1.89 905.79 6.55 903.90 (903.90)

+50

20

Lt

 July 18, 1958 40
 RT 42

72	74	79	79	75	69	61	56	52
50	42	27	16		13	28	41	50

64	69	70	72	70	67	61	46	44
50	40	27	15		12	25	40	50

62	64	67	70	71	70	68	52	46
50	44	29	15		10	20	39	50

69	71	72	74	75	77	75	64	56
50	42	34	19		15	30	38	50

Spike S.W. Cox school Property

39	39	40	40	40	40	40	37	36
50	45	31	15		11	26	42	50

46	47	48	49	48	51	53	52	49
50	47	32	15		15	33	42	50

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		905.79		
--	--	--------	--	--

20+50				
-------	--	--	--	--

T.P.				
------	--	--	--	--

	4.72	901.07	901.07	
--	------	--------	--------	--

July 18, 1958

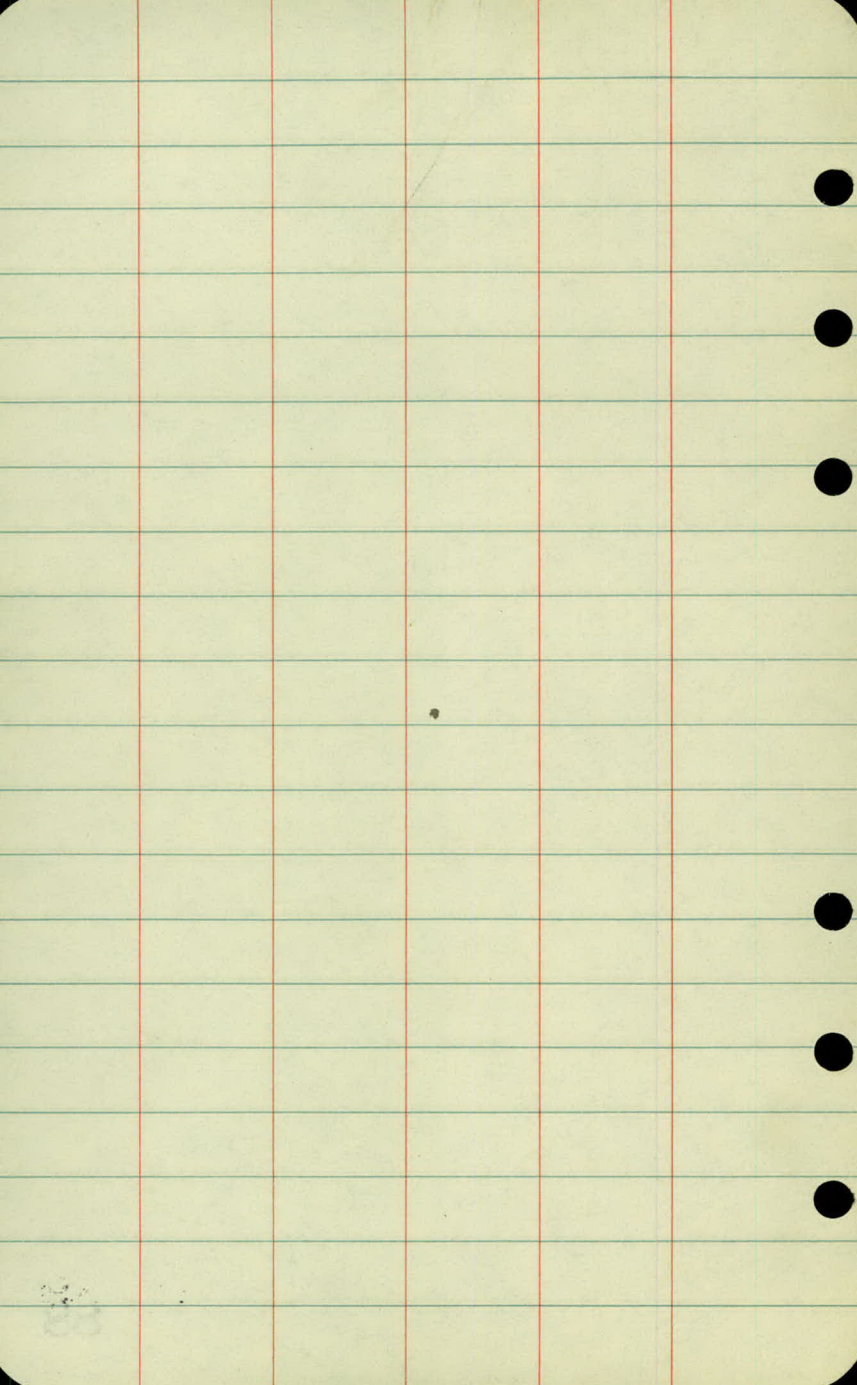
Lt

Rt

41
43

4.5	4.6	4.6	5.1	5.0	5.1	5.1	5.3	5.1
50	42	31	17		17	30	41	50

sto 20100 original



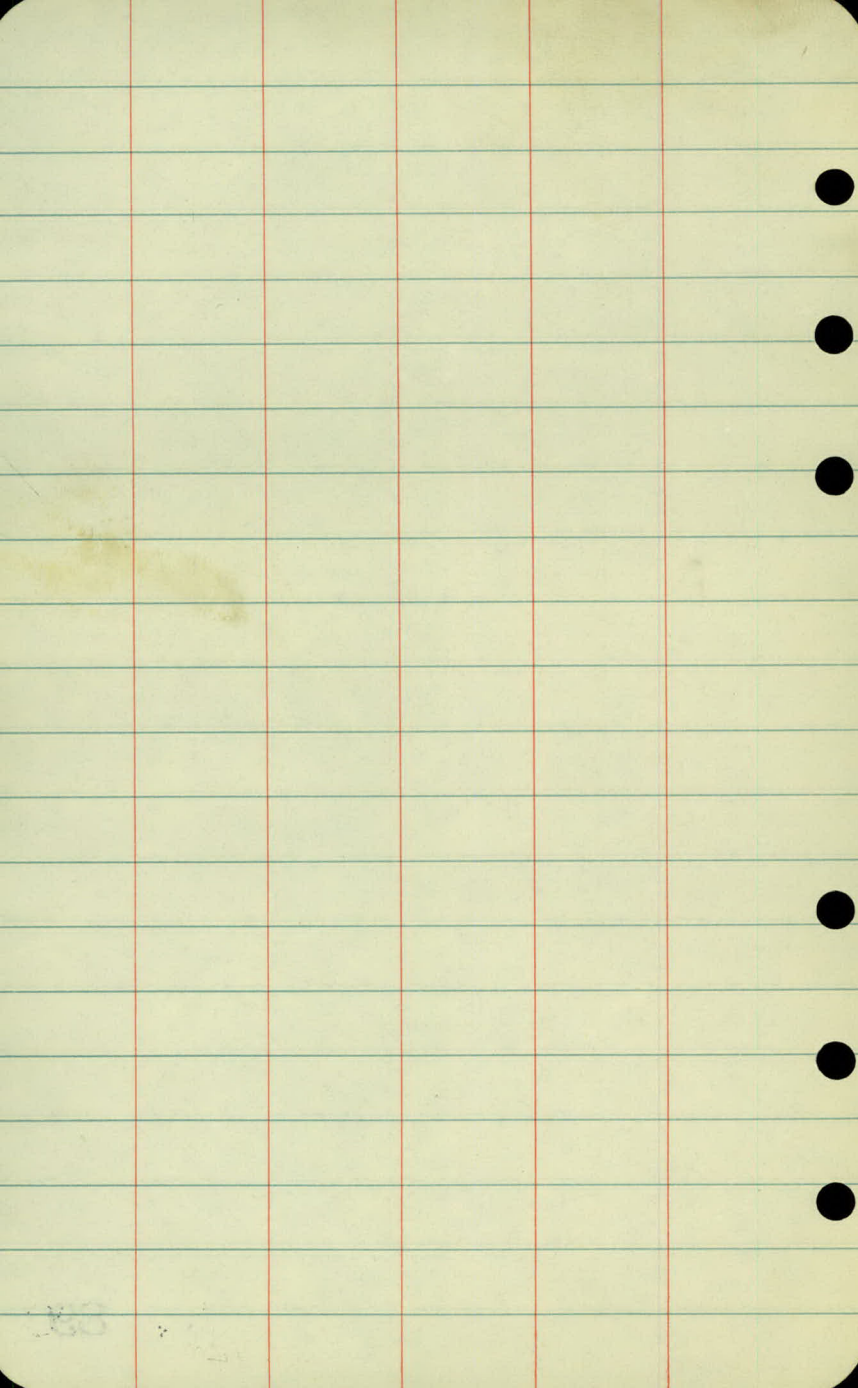
AUGUST 14, 1958

1

KP
RL
RS
SR

COUNTY RD. "I"
LEXINGTON - HAMLINE

SOUNDINGS



KP
RL
RS
SR

Lt

AUGUST 14, 1958

~~E~~

Rt

2.

25'

25'

12+50 24

13+00 24

13+50 16

14+50

25

15+00

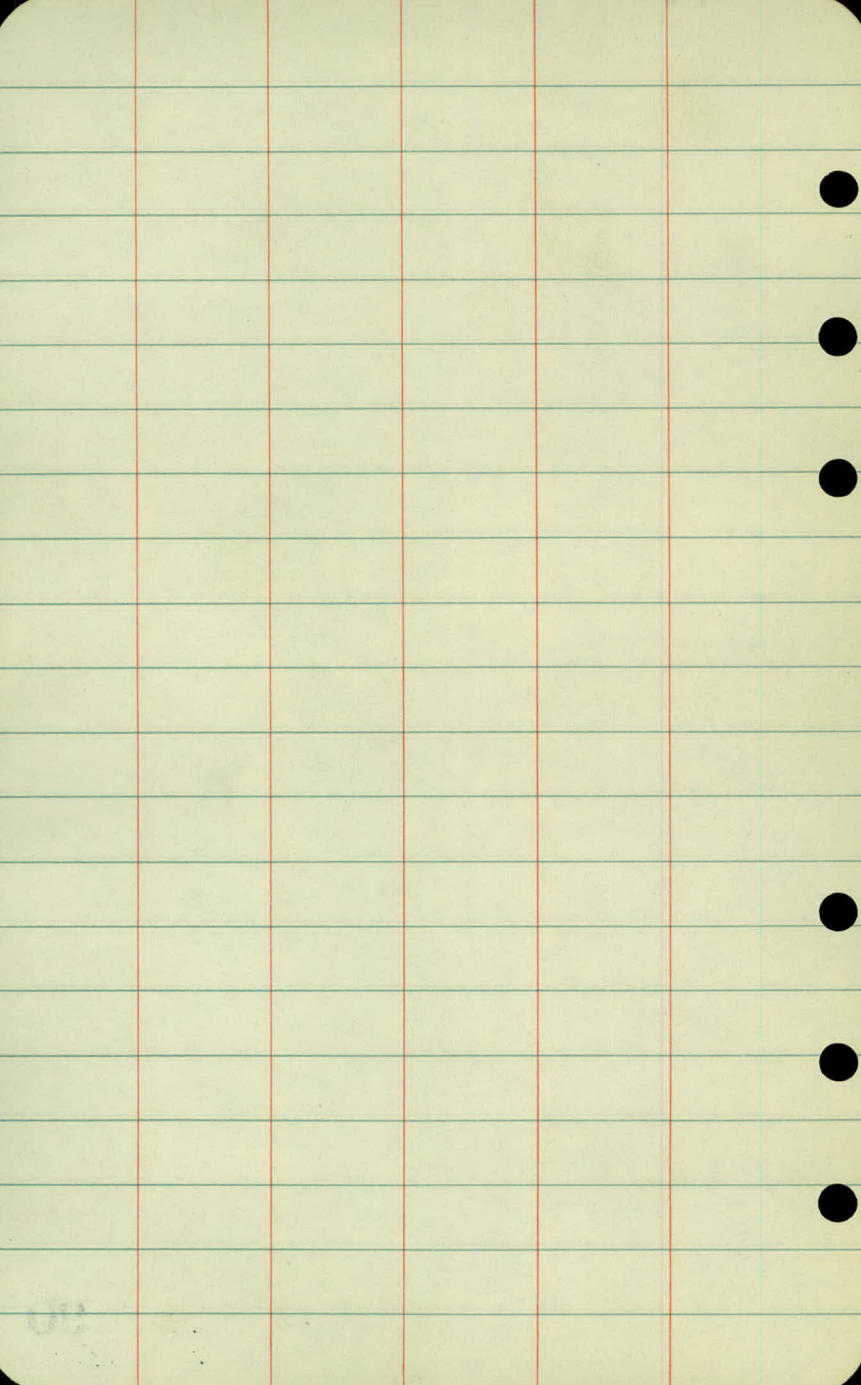
24

25

15+50

19

20



August 14, 1958

Co Rd I

Hamline to Lexington

X-section Extensions

Sta	+	X	-	Elev
0+00	13.35	903.11		889.76

4+00

✓

✓

+25

2 August 14, 1935 2
Lt Rt

Hamline

7.7 7.3 6.2 6.1 6.4
75 100 125 150

10.4 10.1 9.0 8.2
250 225 200 175

→ 11.6 12.3
275 300

5.6 5.0 4.8 5.2
75 100 120 145

6.7 6.8 6.5 6.1
222 200 183 168

→ 7.3 7.6 7.9 9.1
245 268 285 300

Sta + π - Elev.

903.11

A+50

✓

✓

✓

5

J.P

9.11

00912

310

900.21

2 August 14, 1958 3
RT

7.5 6.6 6.4 6.9
75 100 125 150

7.5 7.8 7.8 7.3
241 220 200 176

→ 7.5 7.4 8.5 9.4
263 280 300 319

12.2 11.0
350 340

5.4 8.2 8.9 9.6
75 100 125

10.0 10.2 10.5 10.4
212 200 175 150

93

→ 8.9 9.1 9.5 9.3
230 253 275 300

Sta + π - Elev

909.12

4

✓

✓

+25

LT

\$
Aug. 14, 1958 4

4.0 4.5 5.8 8.1 10.5
186 173 150 125 100

→ 3.1 2.5 4.0 6.4
200 225 242 254

13.3 12.2 10.1
300 289 2.76

2.7 4.7 6.1 7.0 8.9
185 166 148 125 100

→ 2.5 3.4 5.4 9.5
200 219 235 260

14.8 13.4
300 285

Sta + π - Elev

909.12

4+50

✓

5

✓

+50

13.00 89612

August 14, 1958

5

Lt

L

3.7 4.0 6.0 8.0 8.3
183 165 140 118 100

→ 4.4 6.0 10.3 14.0
200 213 233 260

10.3 8.7 7.7 2.9 8.6
180 163 145 121 100

→ 13.1
200

14.2 12.4 11.0 10.5 13.00
160 141 125 100

August 13, 1958

ft

3

ft

5.1
F3.5
34.0

3.0
F2.0

13.5
F12.0
68.0

4.3
F2.2
28.8

3.0
F1.4

14.4
12.3
69.2

4.4
F1.7
26.8

2.8
F0.1

12.2
F9.5
58.0

3.9
F0.6
22.4

2.8
F0.0

4.8
F1.5
26.0

4.5
C9.3
31.9

2.9
C0.5

5.3
C1.0
3.8
34.0

5.14
C0.2
31.6

4.34
C1.0

3.0
C2.3
37.9

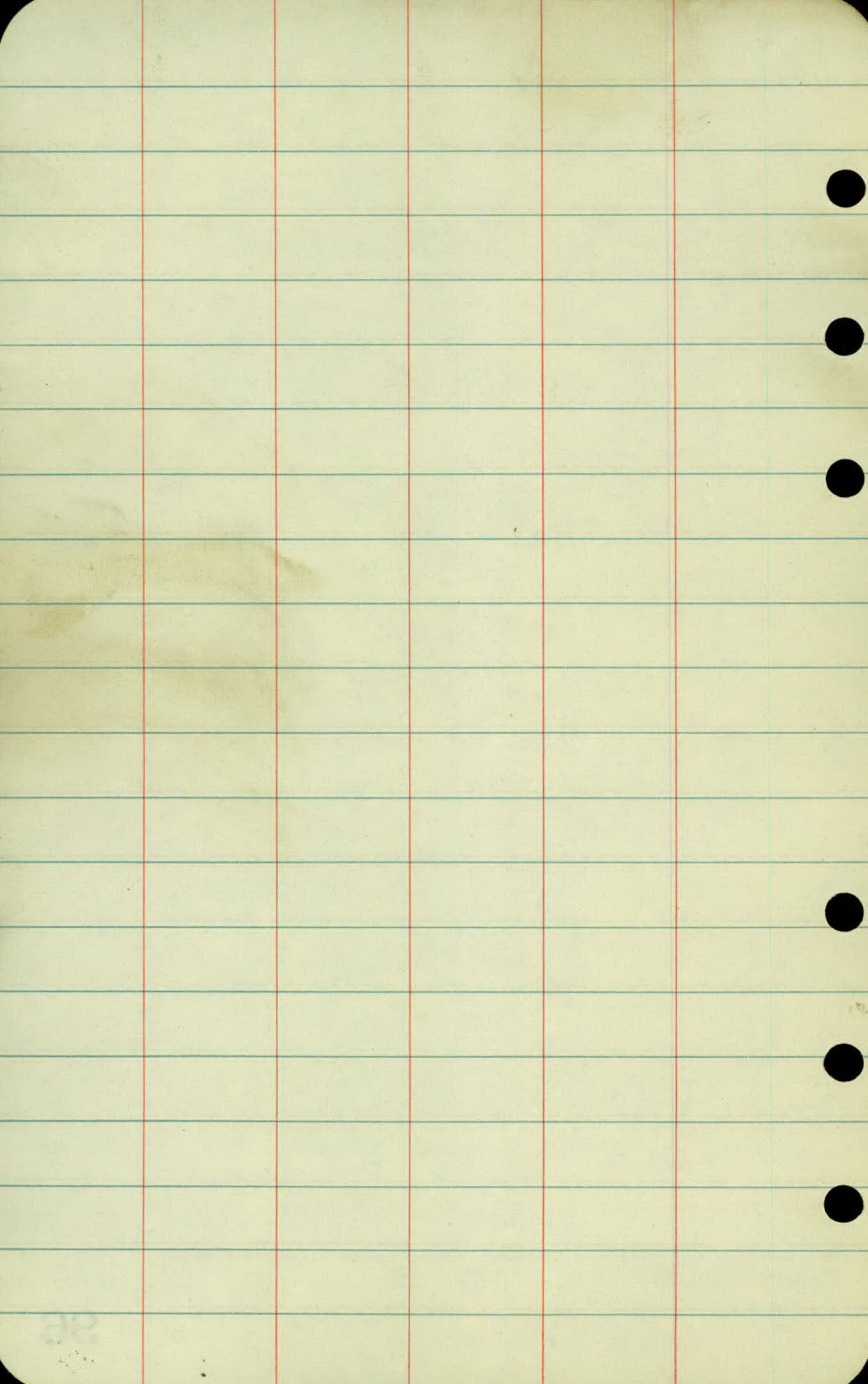
KP
RL
RS
SR

AUGUST 19, 1958

1.

CO. RD. I

LEXINGTON - HAMLINE



KP
 RL
 RS
 SR

Lt

AUGUST 14, 1958
 AUGUST 15, 1958

E Rt 2.

50 25 25 50

13+00

22

19

13+50

18

19

14+50

22

23

15+00 22

24

27

29

29

15+50

18

20

20

24

Sta 12+50 £

Feet

Material

0-1

some fiber peat

1-2

2-3

3-4

4-5

5-6

peat

FK
RR
SR
RM
JM

August 15, 1958

Sta 13+50

£

Feet

Material

0-1

1-2

2-3

3-4

4-5

5-6

No. Fibrous Peat
Peat

Sta 14+50 E

Feet

Materials

0-1

Topsoil &

1-2

Small fibers

2-3

3-4

4-5

5-6

Peat

Co Rd I

X-sect dist. to Borrow Pit

Rec. 12/16/58

Sta

Dist to sta 4430 of B.P.

6+50

~~3+00~~

18.2

+46

+62

98.7

55.7

4

71.2

53.2

+25

51.3

+50

49.2

5

43.4

+50

36.1

+68

33.0

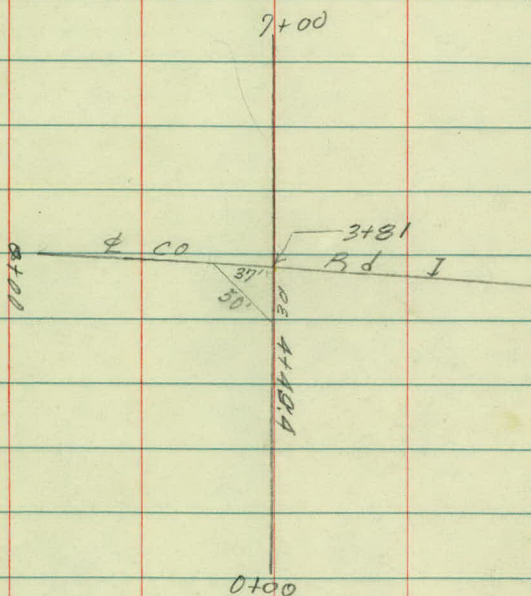
6

27.4

Co Rd I 58-03

Borrow Pit

X-sections



Sta + π - Elev

BM 7.88 900.47

892.59

0+00

91.4

✓

+50

92.8

✓

1

94.8

✓

FX
RG
KP
AB

Nov. 3, 1958

2

LT

RT

Top of Brick NW Cor of Brick & Conc MH

89.2	89.8	90.5	90.8	91.4	91.6	91.2	89.5	88.2
11.3	10.7	10.0	9.7	9.1	8.9	9.3	11.0	12.3
54	38	30	20		16	23	39	59

88.5
12.0
72

87.7
12.8
73

90.1	90.6	91.1	91.9	93.2	92.8	93.0	91.9	89.7	88.7
10.4	9.9	9.4	8.6	7.3	7.7	7.5	8.6	10.8	11.8
63	59	38	24	11		18	27	43	54

89.0
11.5
88

88.9
12.1
100

89.7	95.2	95.4	94.6	94.8	94.7	93.4	92.5	90.7
8.8	5.3	5.1	5.9	5.7	5.8	7.1	8.0	9.8
48	26	15	7		5	22	30	42

91.0
9.5
56

90.7
9.8
75

89.0
11.5
100

88.4
12.1
67

88.8
11.7
58

90.2
10.3
48

Sta + π - Elev

900.47

1+50

95.4

✓

2

95.6

✓

+50

96.5

Nov. 3, 1958 3

11

BT

94.4	96.0	96.3	95.3	95.4	94.9	93.9	90.5	88.9
6.1	4.5	4.2	5.2	5.1	5.6	6.6	10.0	11.6
45	35	25	11		10	22	42	55

90.9	91.0	89.4	89.5	88.4		88.7
96	9.5	11.1	11.0	12.1	✓	11.8
63	86	97	100	115		63

91.0	96.3	96.5	95.0	95.7	95.6	94.7	93.4	91.1	90.5	89.7
9.5	4.2	4.0	5.5	4.8	4.9	5.8	7.1	9.4	10.0	10.8
71	39	23	16	12		10	22	38	45	62

90.9	89.5	89.5	88.1		88.6
9.6	10.6	11.0	12.4	✓	11.9
95	99	112	132		63

96.1	98.0	98.0	96.3	96.5	95.7	94.3	92.8	91.4	90.3
4.4	2.5	2.5	4.2	4.0	4.8	6.2	7.7	9.1	10.2
58	45	28	16		10	22	39	47	65

93.0	91.1	90.9	89.8	88.7		88.3	88.6	89.2
2.5	9.4	9.6	10.7	11.8	✓	12.2	11.9	11.3
75	83	97	100	120		92	79	71

Sta + π - Elev.

900.47

3

96.4

✓

✓

3+81

+30

95.7

✓

✓

3+81

± C. Rd I 58-03

TP

5.20

903.61

2.06

898.41

Nov. 3, 1958

Lt

#

Rt

4

297.7	297.1	295.9	295.8	296.4	296.4	296.0	295.0	293.5	292.3
2.8	3.4	4.6	4.7	4.1	4.1	4.5	5.5	7.0	8.2
25	17	8	4		10	23	42	59	75

297.4	296.3	295.3	293.7	291.8	289.9	290.1	291.9
3.1	4.2	5.2	6.8	8.7	10.6	10.4	8.9
38	52	58	71	79	120	95	89

289.5	291.1
11.0	9.4
101	93

✓

295.4	292.0	292.1	296.6	295.7	296.2	296.2	295.6	294.5
5.1	3.5	3.4	3.9	4.8	4.3	4.3	4.9	6.0
52	37	22	8		6	25	43	63

292.3	291.5	290.1	289.8	293.0	294.1	294.2	294.0
8.2	9.0	10.4	10.7	7.5	6.4	6.3	6.5
74	88	96	100	111	107	100	83

288.6	289.4	291.9	291.1	290.5
11.9	11.1	8.6	9.4	10.0
136	118	126	146	165

✓

Sta + π - Elev

903.61

4+30

✓

✓

✓

+50

Nov. 3, 1958

5

Rt

Lt

92.3	93.9	97.2	98.7	99.3	99.0	98.3	97.2	98.8
11.3	9.7	6.4	4.9	4.3	4.6	5.3	4.4	4.8
73	64	39	18		11	27	36	66

91.5	89.7
12.1	13.9
87	97

98.0	97.5	97.9	98.1
5.6	6.1	5.7	5.5
156	126	100	93

96.9	95.5	95.0	94.6
6.7	8.1	8.6	9.0
161	178	195	200

90.0	92.0	93.2
13.6	11.6	10.4
253	240	219

89.7	92.9	95.8	98.3	99.1	99.5	99.6	99.1	99.9	98.9	98.0
139	107	78	5.9	4.5	4.1	4.0	4.5	3.7	4.7	5.6
100	77	50	30	12		24	29	60	100	132

93.1	93.4	94.0	95.3	97.4
10.5	10.2	9.6	8.3	6.2
208	200	196	179	165

92.5	88.4
11.1	15.2
222	238

Sta + π - Elev

903.61

5

✓

TP 9.50 909.48 3.63 899.98

+50

✓

6

Nov. 3, 1958 6

27

By

6

10.1	11.5	12.7	13.1	9.7	8.8	7.2	5.2
86	100	114	185	171	150	125	100
93.5	92.1	90.9	90.5	93.9	94.8	96.4	98.4
71	54	36	2.2	16	16	3.2	
65	59	41	19	8	23	48	75
96.5	98.2	100.0	101.7	101.4	101.1	102.0	102.0

9.1	6.3	5.0	5.8	4.4	4.2	5.3	6.7	10.1
88	72	50	22	16	30	44	64	
00.4	03.2	04.5	03.7	05.1	05.3	04.2	02.8	99.4

→ 10.8	13.0	16.0	17.8	17.8	15.3	12.1
100	110	130	154	110	100	78
98.7	96.5	93.5	91.7	91.7	94.2	97.4

0.9	2.8	2.8	3.0	4.5	7.2	10.7	13.4	15.6
85	63	42	21		17	33	48	64
08.6.	06.7.	06.7.	06.5.	05.0.	02.3.	98.8.	96.1.	93.9.

0.09.3.	03.0.	99.2.	19.7.
0.2	6.5	10.3	17.8
97	124	139	72

18.0	16.2	13.2	105
192	176	154	
91.5	93.3	96.3	

Sta + π - Elev

909.48

6+25

✓

✓

+50

60.4

Nov. 3, 1958

7

14

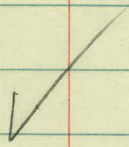
RT

07.5	06.7	06.2	04.5	01.1	98.6	96.2	93.9
20	28	33	50	84	109	133	156
85	66	46	26		16	28	38

07.9	07.8	04.6	00.8
1.6	1.7	4.9	8.7
92	100	122	139

95.8	96.6
13.7	12.9
169	163

Row Pine

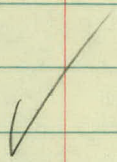


05.3	04.1	02.1	99.9	97.1	95.7
42	54	74	96	124	138
81	65	48	27		15

05.6	05.2	05.3	03.5
3.9	4.3	4.2	6.0
92	100	113	130

95.4	97.4	01.0
14.1	12.1	8.5
182	168	148

Row Pine



Sta + π - Elev

909.48

7+00

✓

4+50

11.5 98.0 ✓

5+50

13.34 96.14 96.0

Nov. 3, 1958

8

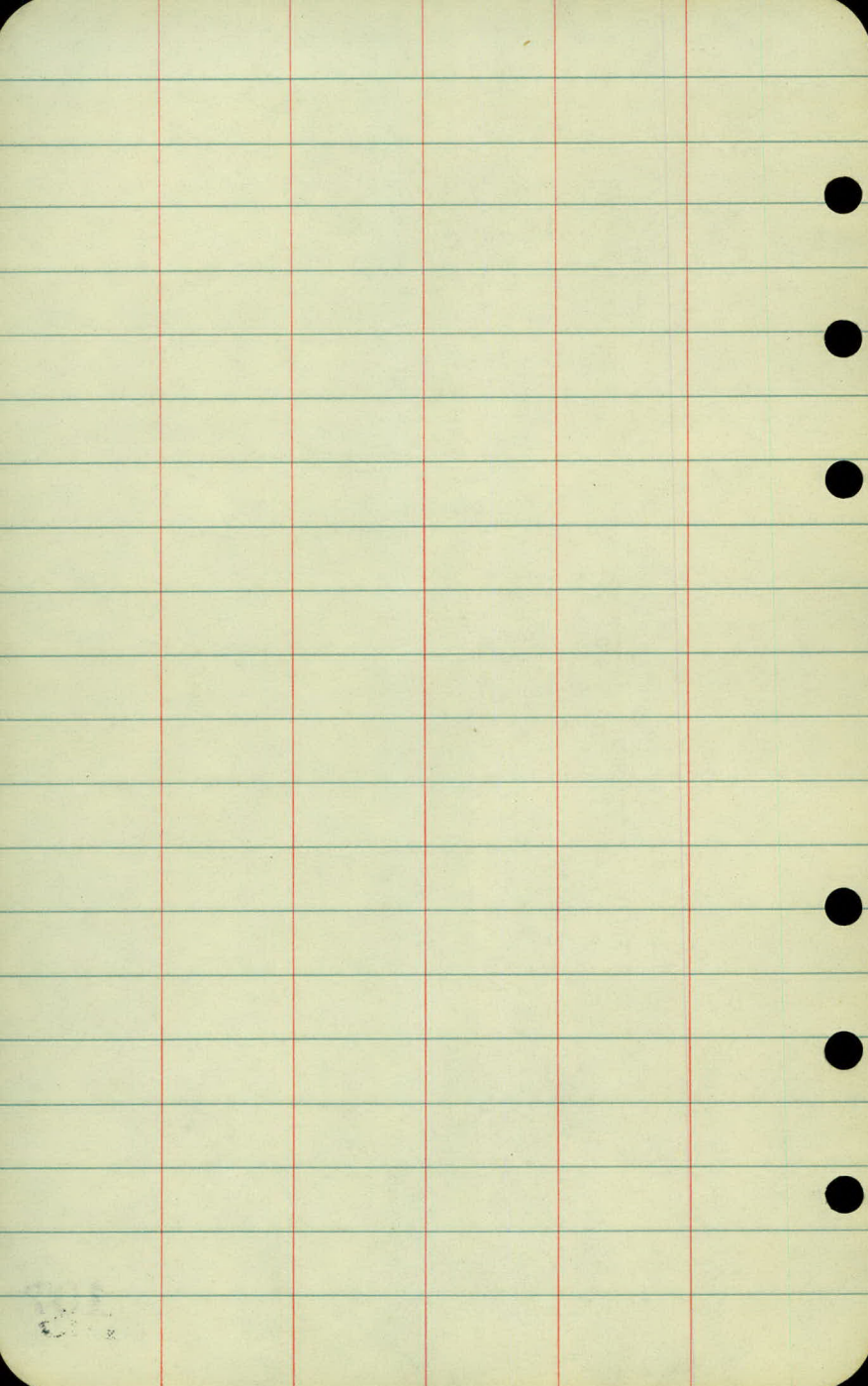
4

4

03.2	03.1	02.4	01.0	97.8	95.1	94.3	93.6
6.3	6.4	7.1	8.5	11.7	14.4	15.2	15.9
127	108	100	92	69	46	25	

03.1	01.1	98.5	96.1
6.4	8.4	11.0	13.4
148	166	184	200

✓



Borrow Pit

X-Sections (Continuations)

Co Rd "I" $\frac{1}{2}$ Hamline

4 pages

Sta	+	π	-	Elev
BM	12.83	905.42		892.59

6+50 on the flat

7+00

✓

7+50

✓

8+00

LC
RG
KP LT
JS

May 13, 1959
Very Windy 50°
Hamline & Co Rd "I"

Top of Brick NW Cor Manhole 200' Rt Mont

94.1	96.2	95.9	96.2	96.0	95.4	94.8
11.3	9.2	9.5	9.2	9.4	10.0	10.6
200	176	135	100	77	25	

98.9	90.9	90.2	99.2	98.3	95.1	92.2
6.5	4.5	5.2	6.2	7.1	10.3	13.2
179	147	123	100	82	50	

96.6	93.4
8.8	12.0
200	220

90.8	92.0	91.6	98.1	97.2	93.8	90.0
4.6	3.4	3.8	7.3	8.2	11.6	15.4
187	152	131	100	90	45	

99.3	96.2	93.7
6.1	9.1	11.7
260	233	279

91.6	99.9	98.1	96.0	94.2	90.6	87.8
3.8	5.5	7.3	9.4	11.2	14.8	15.6
192	166	127	100	72	41	

Sta	+	π	-	Elev
-----	---	-------	---	------

		905.42		
--	--	--------	--	--

8+00				
------	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

9+00				
------	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

May 13, 1959

3

L.T.

4

01.5	00.5	08.6	07.7
3.9	4.9	6.8	7.7
200	248	280	300

01.3	01.4	01.8	06.1	03.6	00.5	09.9
4.1	4.0	3.6	9.3	11.8	14.9	15.5
237	200	152	100	66	47	

00.0	06.9	04.9	01.4
5.4	8.5	10.5	14.0
274	300	342	361

LaMetty's
cut

04.3	00.8	07.3	03.4	00.4	09.8
1.1	4.6	8.1	12.0	15.0	15.6
176	133	100	56	33	

03.2	02.3	02.0	08.6
2.2	3.1	3.4	6.8
200	244	291	300
			CUT

03.7	01.8	07.7	05.6	03.7	03.3
1.7	3.6	7.7	9.8	12.2	12.1
156	133	100	65	22	

Sta + π - Elev

905.42

9 + 50

BM

9.71 895.71

T.P. 1.77 895.57 11.62 893.80

BM

7.42 888.15 (888.15)

BM

2.93 892.64 (892.59)

May 13, 1959

Lt

4

4

05.3	04.6	04.3	03.9	03.4	03.2
0.1	0.8	1.1	1.5	2.0	12.2
188	200	249	300	318	335
					Cut

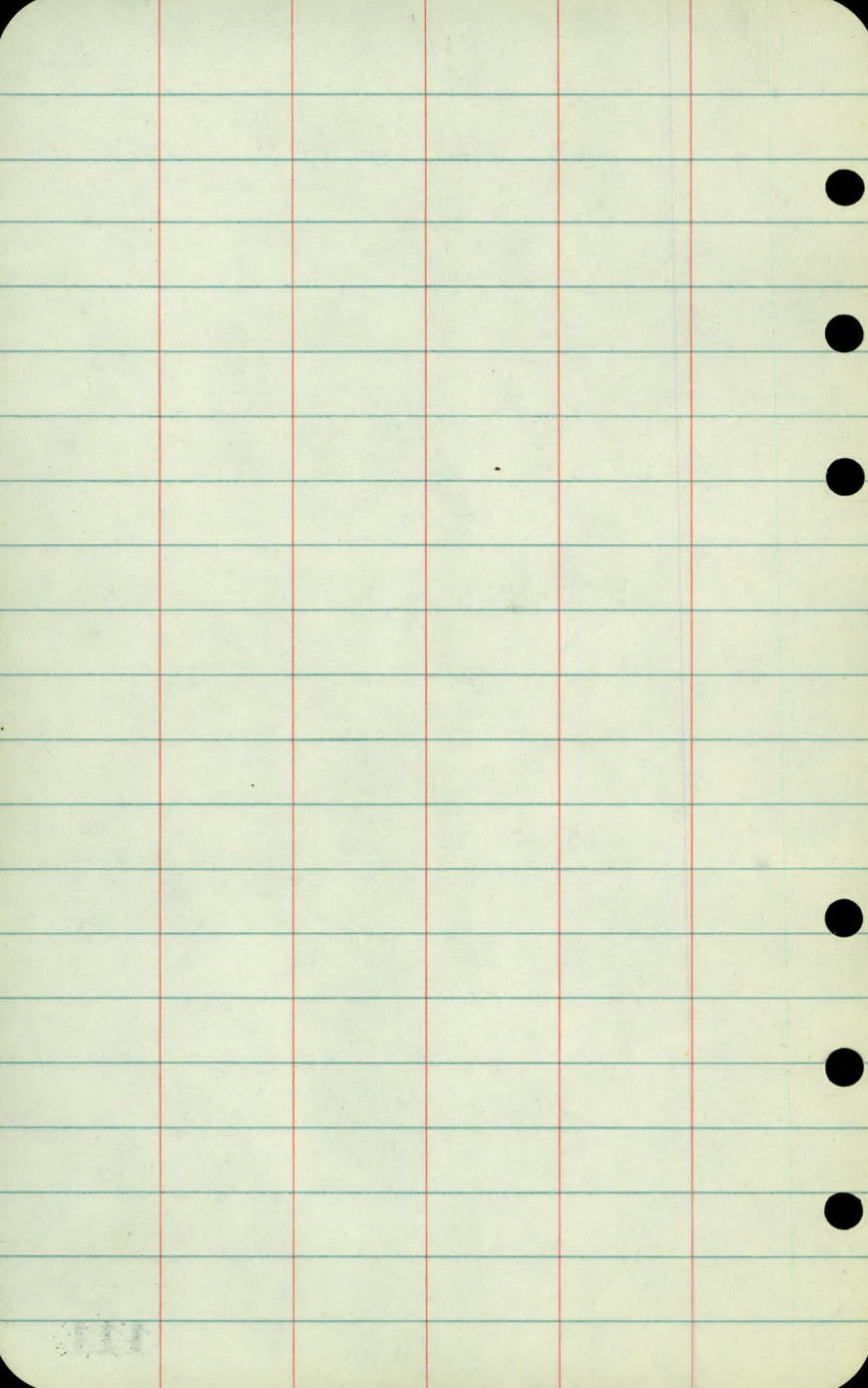
SE Cor Base Flicks Fence (Plant)

488 1/2
100

Top Snow fence post

Top Mont Hamline & Co Rd "I"

Top Brick NW Cor Manhole 200' RT Mont
Hamline & Co Rd "I"



May 25, 1959

1

Co Rd I

Borrow Pit X-Sections

(Final)

Sta + π - Elev.

B/M 6.84 90255

895.71

6+00

✓

✓

+25

FK
RG
KP

May 25, 1959

2

£

Base of SE. Cor Fe. Post Flick's Ind. Plant

q5.7	q6.0	q5.8	q5.8	q5.5	q5.2	q5.0	q0.5
6.9	6.6	6.8	6.8	7.1	7.4	7.6	12.1
81	61	40	13		26	42	84

q5.3	q5.1	q5.2
7.3	7.5	7.4
100	120	135

89.8
12.8
100

q3.6	q4.5	q5.2
9.0	8.1	7.4
188	176	156

q5.9	q5.9	q5.9	q5.0	q5.3	q5.2	q4.4	q5.5	q0.7
6.7	6.7	6.7	7.6	7.3	7.4	8.2	9.1	11.9
77	55	36	22		10	28	46	67

q5.5	q5.5	q5.5	q5.5
7.1	7.1	7.1	7.1
100	121	142	165

q0.2
124
82

88.6	q2.7	q4.5
14.0	9.9	8.1
215	200	190

Sta	+	π	-	Elev
-----	---	-------	---	------

		902.55		
--	--	--------	--	--

6+50				
------	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

7				
---	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

May 25, 1959 3
RT

LT

q6.0

q5.2

q5.2

q4.8

q4.1

q3.8

q4.8

q0.3

6.6 7.4 7.4 7.8 8.5 8.8 10.8 12.3
69 46 22 5 21 40 60

q6.1

q6.1

q6.3

q5.8

6.5 6.5 6.3 6.8
100 123 147 172

q6.6

q9.3

q3.9

14.0 11.3 8.7
225 214 200

q6.6

q6.0

q5.1

q4.0

q2.3

6.0 6.6 7.5 8.6 10.3
90 71 49 21

q6.6

q7.0

q7.3

q6.8

6.0 5.6 5.3 5.8
100 121 145 170

q3.0

q3.3

q5.9

q6.3

9.6 9.3 6.7 6.3
235 226 200 193

q2.0

10.6

247

Sta	+	π	-	Elev
-----	---	-------	---	------

		902.55		
--	--	--------	--	--

7+50				
------	--	--	--	--

✓				
---	--	--	--	--

+75				
-----	--	--	--	--

✓				
---	--	--	--	--

8				
---	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

May 25, 1959

Lt

£

4

96.4	96.2	95.5	94.6	94.0	91.2	90.1
6.2	6.4	7.1	8.0	8.6	11.4	12.5
100	88	70	53	38	21	

97.0	97.0	97.5	97.1	98.0	97.6	✓
5.6	5.6	5.1	4.9	4.6	5.0	N.G
136	152	77	200	226	245	263
		177				

96.8	96.2	95.8	94.7	92.5	91.0
5.8	6.4	6.8	7.9	10.1	11.6
122	100	78	67	51	35

96.6	97.8	99.2	99.2	99.8	98.6	98.1
6.0	4.8	3.4	3.4	2.8	4.0	4.5
148	170	200	218	236	258	N.G
						275

98.6	97.3	96.0	93.9	91.0	89.9	89.8
4.0	5.3	6.6	8.7	11.6	12.7	12.8
122	100	89	67	45	23	

99.3	99.7	00.8	01.4	00.5	00.6	✓
3.3	2.9	1.8	1.2	2.1	2.0	
138	159	178	196	208	219	

00.8	00.6
1.8	2.0
251	233

115

Sta + π - Elev
902.55

8+25

✓

8+45 End of Exc. if any

BM

6.84 895.71

May 25, 1959

5

Lt

00.9

00.1

97.2

95.3

94.6

93.6

1.8

2.5

5.4

7.3

8.0

9.0

134

120

100

90

79

71

01.5

01.5

01.6

00.7

00.6

99.9

1.1

1.1

1.0

1.9

2.0

2.7

~~2.9~~

153

171

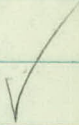
199

208

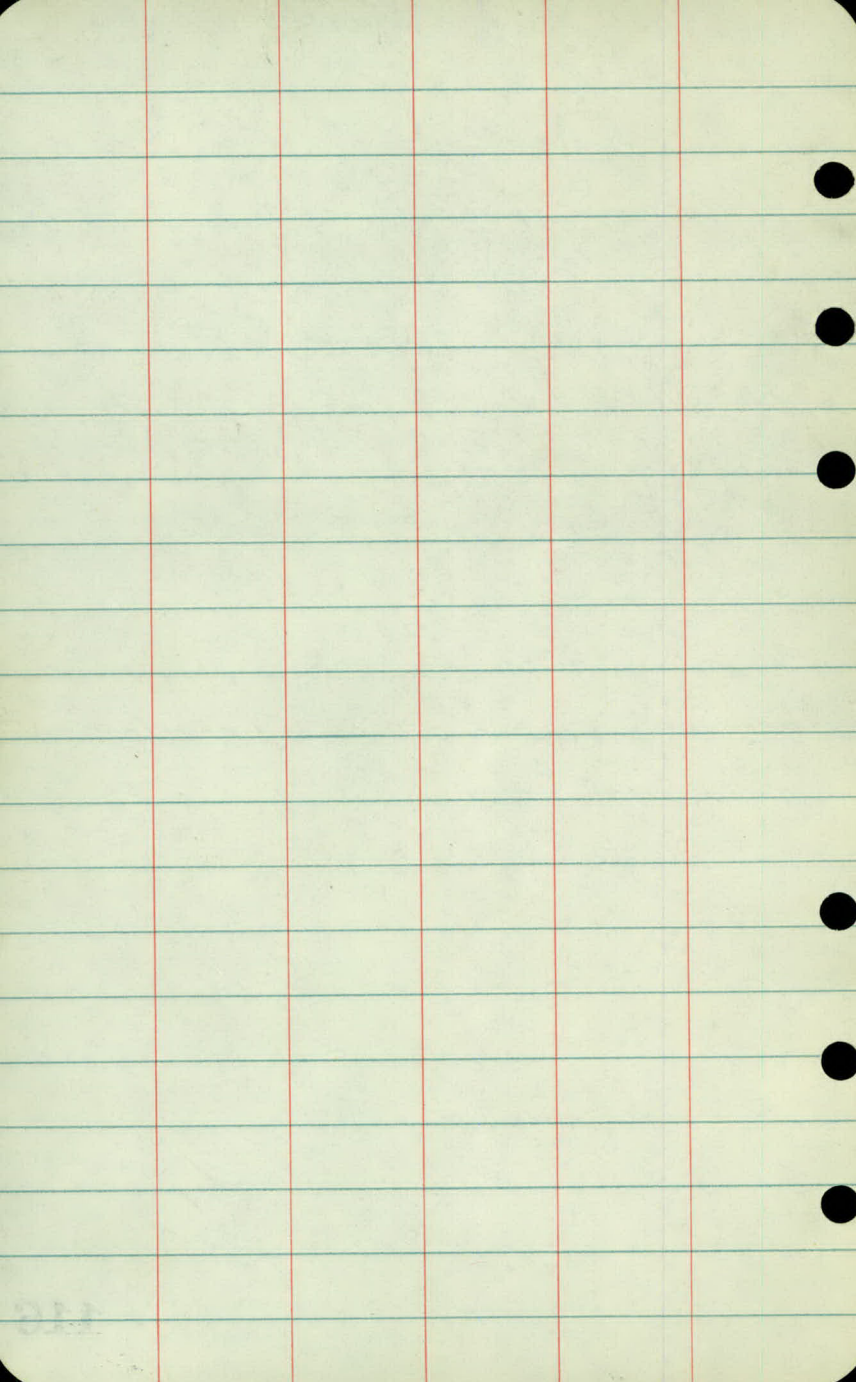
221

290

~~262~~



Base of SE, Cov Fe. Post Flick's Ind. Plant.



FK
RL
RR
DF

July 2, 1959

1

C. Rd I 58.03

Final X-Sections

Sta + π - Elev

BM 10.64 902.86

892.22

19+27.25

✓

+50

✓

20

July 2, 1959

2

2

Spike in 20" oak 100 ft Sta 16+80

00.4 98.7 98.4 97.9 97.7 95.8 95.7

25 42 45 5.0 52 7.1 7.2
119 98 81 63 50 38 24

01.9

1.0 ✓
123
NG

99.4 98.6 98.0 97.5 97.5 96.3 96.0

3.5 4.3 4.9 5.4 5.4 6.6 6.9
107 96 80 61 48 40 24

00.4

01.9

2.5 1.0 ✓
117 124

98.2

98.0

98.0

97.8

97.0

96.4

4.7 4.9 4.9 5.1 5.9 6.5
100 84 63 50 41 24

01.9

1.0 ✓
117

Sta + π - Elev

902.86

20+27

+50

21

+50

+65

TP 9.98 911.50 • 1.34 901.52 •

22

801

July 2, 1959

3

Lt

✓ 01.8 00.6 98.7 98.6 98.4 97.7 96.7
 1.1 2.3 4.2 4.3 4.5 5.2 6.2
 120 110 100 74 59 44 24
 NG

✓ 02.0 99.1 99.1 98.8 98.2 97.3 97.1
 0.9 3.8 3.8 4.1 4.7 5.6 5.8
 114 102 76 63 45 38 24
 NG

✓ 99.5 99.4 98.9 97.9 97.4
 NG 3.4 3.5 4.0 5.0 5.5
 115 95 75 51 38 24

✓ 01.4 00.3 00.2 99.8 98.0
 NG 1.5 2.6 2.7 3.1 4.9
 123 98 82 66 50 24

✓ 01.5 00.7 00.7 00.4 98.7 98.1
 NG 1.4 2.2 2.2 2.5 4.2 4.8
 129 97 80 61 48 38 24

01.3 01.2 00.9 00.9 99.2 98.5
 10.2 10.3 10.6 10.6 123 130
 92 70 61 49 40 24

02.2 04.1 05.0
 9.3 7.4 5.5
 107 123 137

Sta + π - Elev

911.50

22+50

✓

23

✓

+50

1

0.00

July 2, 1959

Lt

E 4

✓ 01.7 01.6 01.3 01.1 99.5 98.9
9.8 9.9 10.2 10.4 12.0 12.6
93 82 70 53 40 24

02.6 04.3 05.0
→ 8.9 7.2 6.5
107 121 138

✓ 02.8 01.9 01.5 01.3 99.5 99.0
8.7 9.6 10.0 10.2 12.0 12.5
109 91 65 51 40 24

04.5 04.8
→ 7.0 6.7
137 150

✓ 02.3 01.4 01.1 00.8 99.2 98.6
9.2 10.1 10.4 10.7 12.3 12.9
101 84 68 52 40 24

03.1 04.4 04.9
→ 8.4 7.1 6.6
119 138 150

Sta + π - Elev

911.50 .

24

✓

+50

✓

25

✓

TP 0.51 905.19 . 6.82 904.68 .

July 2, 1959 £ 5

Lt

✓ 00.6 00.1 00.8 00.1 00.8 00.1
10.9 11.4 11.7 12.4 12.7 13.4
91 73 53 48 39 24

01.8 03.5 04.6 05.4
→ 9.7 8.0 6.9 6.1
111 132 150 164

✓ 00.5 00.9 00.0 00.8 00.0 00.3
11.0 11.6 12.5 12.7 13.5 14.2
113 95 71 52 40 24

01.3 02.8 03.5 03.8
→ 10.2 8.7 8.0 7.7
126 141 150 165

✓ 00.4 00.1 00.4 00.6 00.8 00.5
11.1 12.4 13.1 13.9 14.7 15.0
129 107 90 69 48 24

00.8
→ 10.7
147

Sta + π - Elev

905.19

25+21.12

+50

$\neq$ Lex

874.46 ✓

10.73 ~~994.46~~ (94.4)

July 2, 1959

£

6

Lt

✓

04.8

02.4

00.5

98.1

96.9

96.3

96.2

116 0.4

2.8

4.7

7.1

8.3

8.9

9.0

124 113

102

92

79

63

35

24

✓

04.1

02.1

97.5

96.1

95.9

95.7

1.1

3.1

7.7

9.1

9.3

9.5

102

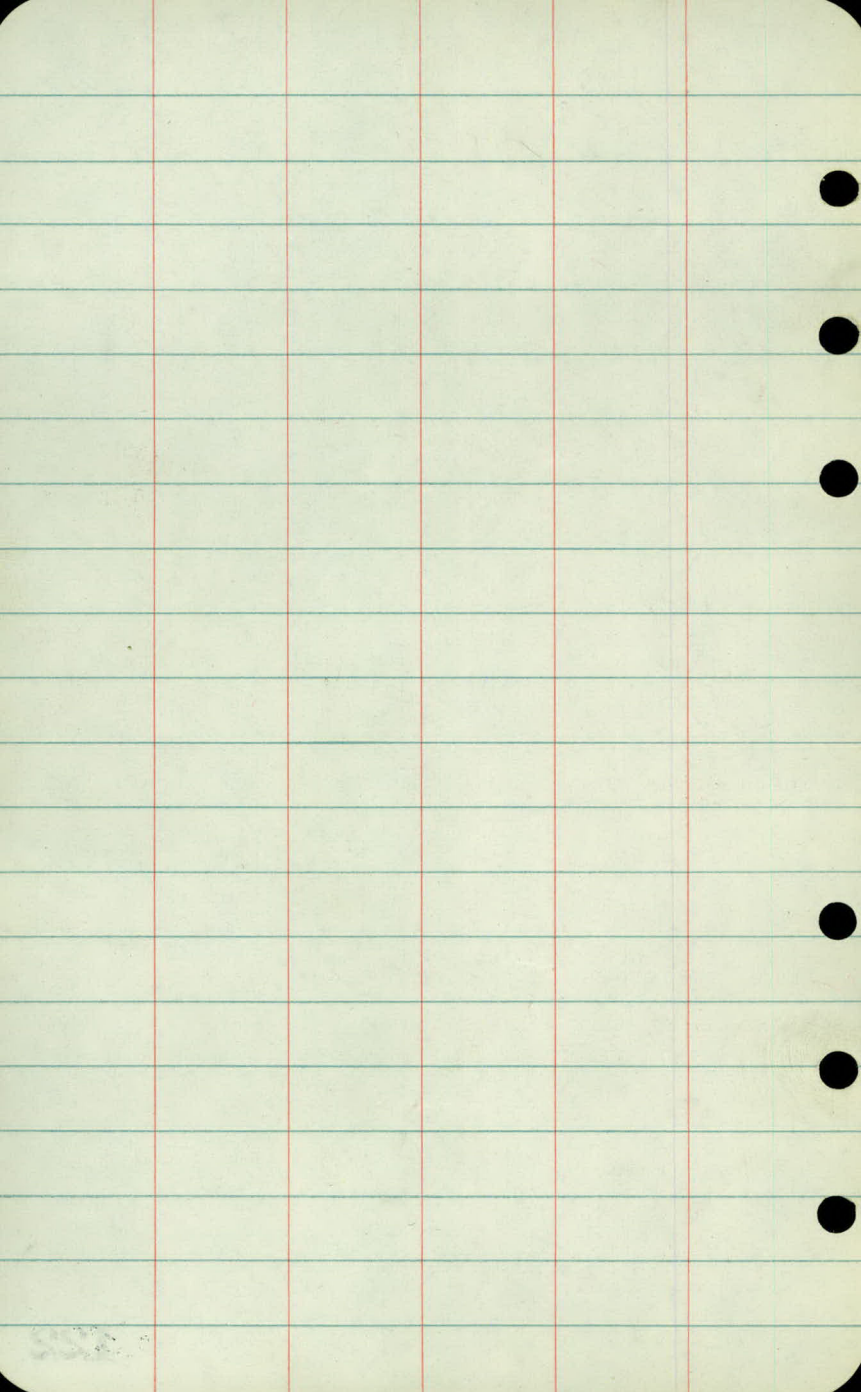
97

75

61

42

24



FK
RL
RR
OP
DF

June 30, 1959

1

Co Rd I 58-03

Profile

5 pages

Rec. 6/30/59 K.A.

Sta + π - Elev

BM 7.61 899.83

892.22

17

+50

18

+50

19

+50

USE

June 30, 1959 2

Lt

RT

Spike in 20" out 100' RT Sta 16+80

93.3
6.5

93.3
6.5

93.2
6.6

94.1
5.7

94.2
5.6

94.2
5.6

94.6
5.2

94.8
5.0

94.8
5.0

95.3
4.5

95.4
4.4

94.3
4.5

95.7
4.1

96.0
3.8

95.6
4.2

96.2
3.6

96.6
3.2

96.3
3.5

Sta + π - Elev

899.83.

20

+50

21

TP 4.31903.79 2.35897.48

+50

22

+50

June 30, 1959

3

LT

RT

96.9
2.9

97.0
2.8

96.9
2.9

97.6
2.2

97.5
2.3

97.3
2.5

98.1
1.7

97.7
2.1

98.0
1.8

98.3
5.5

98.3
5.5

98.4
5.4

98.8
5.0

98.7
5.1

98.7
5.1

99.0
4.8

99.0
4.8

99.1
4.7

Sta + π - Elev

90379.

23

+50

24

+50

25

+50

June 30, 1959 A

11

BT

99.3

99.1

99.3

4.5

4.7

4.5

98.9

98.9

99.1

4.9

4.9

4.7

98.6

98.5

98.4

5.2

5.3

5.9

98.0

97.6

97.9

5.8

6.2

5.9

96.8

96.6

96.9

7.0

7.2

6.9

95.5

95.6

95.9

8.3

8.2

7.9

Sta + π - Elev

903.79

26

+50

26+74. $\neq$ Lev

9.38 894.41 (94.4)

swampy purp. Swamp
Lake Phaler
Upper Afton

June 30, 1959

5

LT

BT

95.0

95.1

94.5

8.8

8.7

9.3

94.7

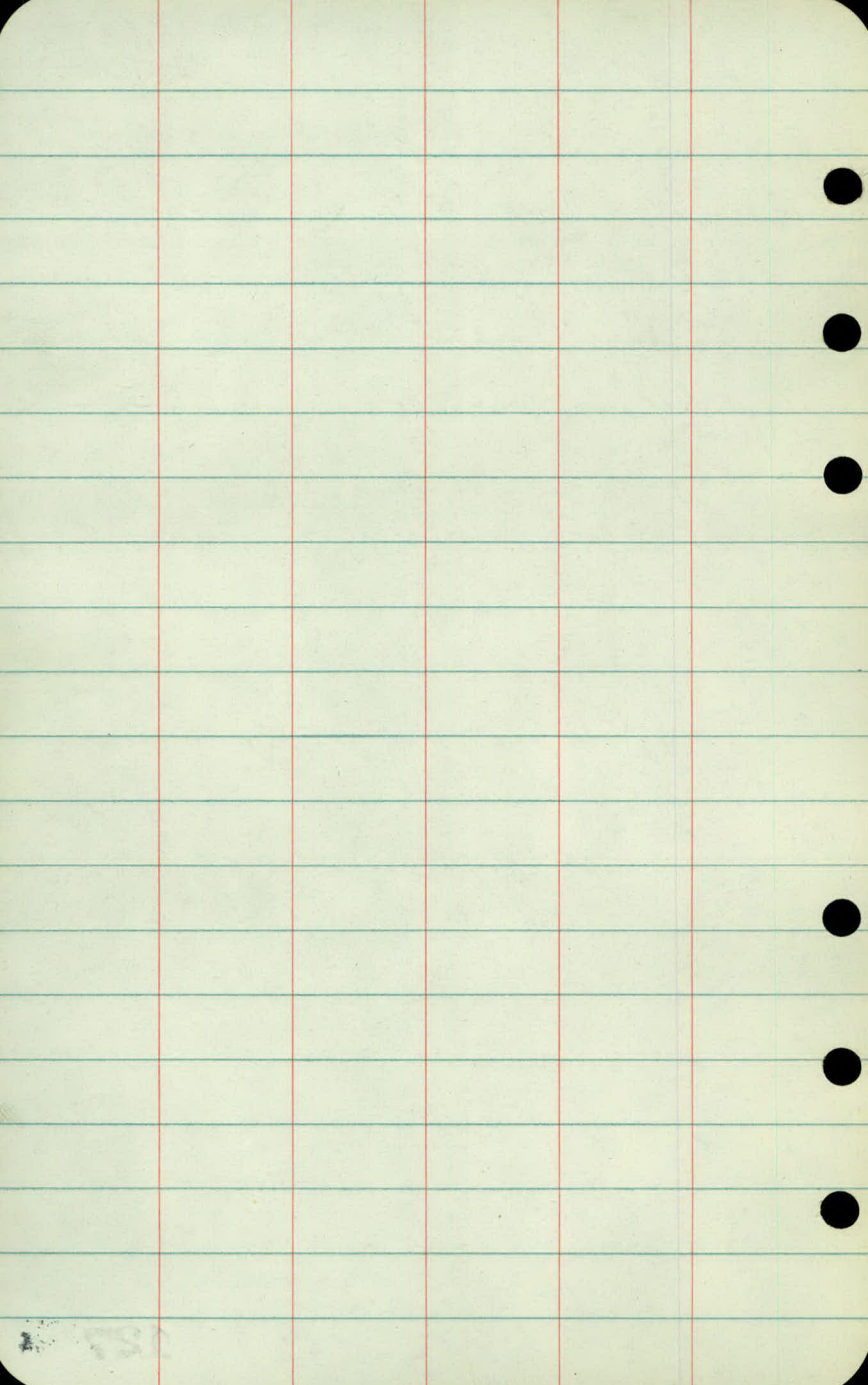
94.9

94.3

9.1

9.4

9.5



Co Rd I 58-03

Overload x-sections

4 pages

Rec. 6/29/59 K.H.

Sta + π - Elev

BM 9.40 901.62

892.22

9+50

10

+50

11

+50

12

FK
RL
RR
OP
DF

June 24, 1959

2

LT

RT

Spike in 24" Out 100' RT Sta 16+80

90.0	90.5	91.9	92.9	92.1	90.1
11.6	11.1	9.7	8.7	9.5	11.5
32	24	19	✓	19	30

89.4	91.7	92.8	93.5	93.5	93.2	92.8	91.9	90.0
12.2	9.9	8.8	8.1	8.1	8.4	8.8	9.7	11.6
33	18	16	8	✓	12	15	19	33

88.4	91.3	93.1	94.0	94.3	94.3	93.4	88.6
13.2	10.3	8.5	7.6	7.3	7.3	8.2	13.0
31	21	16	12	✓	7	16	31

88.3	95.3	95.2	94.6	88.1
13.3	6.3	6.4	7.0	13.5
27	15	✓	18	27

99.5	95.7	96.3	96.4	96.4	95.5	87.8
12.1	5.9	5.3	5.2	5.2	6.1	13.8
29	17	6	✓	7	17	28

99.9	95.6	96.4	96.8	96.5	96.3	88.1
11.7	6.0	5.2	4.8	5.1	5.3	13.5
27	16	8	✓	9	17	26

Sta + π - Elev

901.62.

12+50

13

+50

14

TP 4.75 901.45 4.92 896.70.

+50

15+20

June 24, 1957

3

Lt

Rt

91.0	95.6	96.2	96.3	96.3	95.6	88.3
10.6	6.0	5.4	5.3	5.3	6.0	13.3
20	15	6	✓	8	19	29

89.6	92.3	92.4	95.5	96.3	96.4	95.8	95.1	88.4
120	93	92	6.1	5.3	5.2	5.8	6.5	13.2
30	26	23	17	6	✓	10	22	30

88.7	94.3	93.9	95.8	96.6	96.5	96.0	95.8	88.0
129	83	7.7	5.8	5.0	5.1	5.6	5.8	13.6
33	27	21	18	6	✓	9	21	32

88.8	94.9	95.3	96.9	96.8	96.8	96.1	96.3	88.2
128	7.2	6.3	5.2	4.8	4.8	5.5	5.3	13.4
33	26	20	18	9	✓	10	19	32

87.6	94.2	94.4	97.4	97.1	96.4	96.5	89.3
13.9	7.3	7.1	4.1	4.4	5.1	5.0	12.2
34	23	22	18	✓	10	18	31

87.8	96.8	96.7	96.3	87.8
13.8	47	4.8	5.2	13.8
27.	16	✓	16	28

Sta + π - Elev.

901.95

15+50

TP 4.14 900.60 4.99 896.46

16

+50

BM

8.34 892.26 892.22

June 24, 1959

4

LT

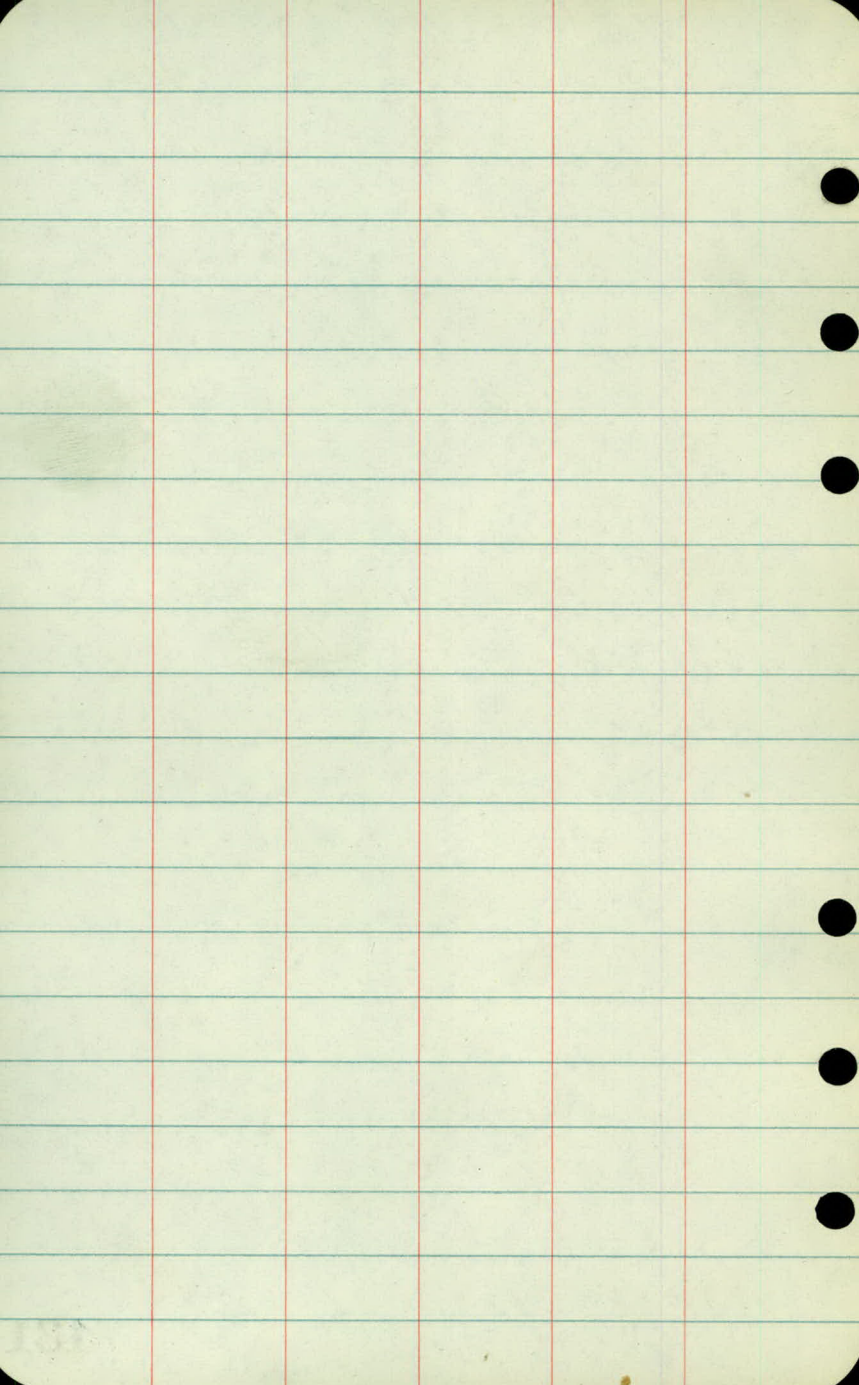
RT

89.2	95.5	95.8	95.5	88.1
11.4	5.1	4.8	5.1	12.5
28	19	✓	15	27

90.3	95.6	95.3	94.4	90.6
10.3	5.0	5.3	6.2	10.0
31	21	✓	22	31

91.5	93.1	93.5	93.5	92.8	90.3
9.1	7.5	7.1	7.1	7.8	10.3
23	14	17	28	40	

Spike in 20" cat 100' RT sta 16+80



1
Co Rd I 58-03

Soundings
Boreon Pit A

Sta 2+00 90' Lt

Feet Material

0-4 sand

4-7 clay

Sta 3+00 95' Lt

Feet Material

0-3½ sand

3½- clay

FK
KP
AB

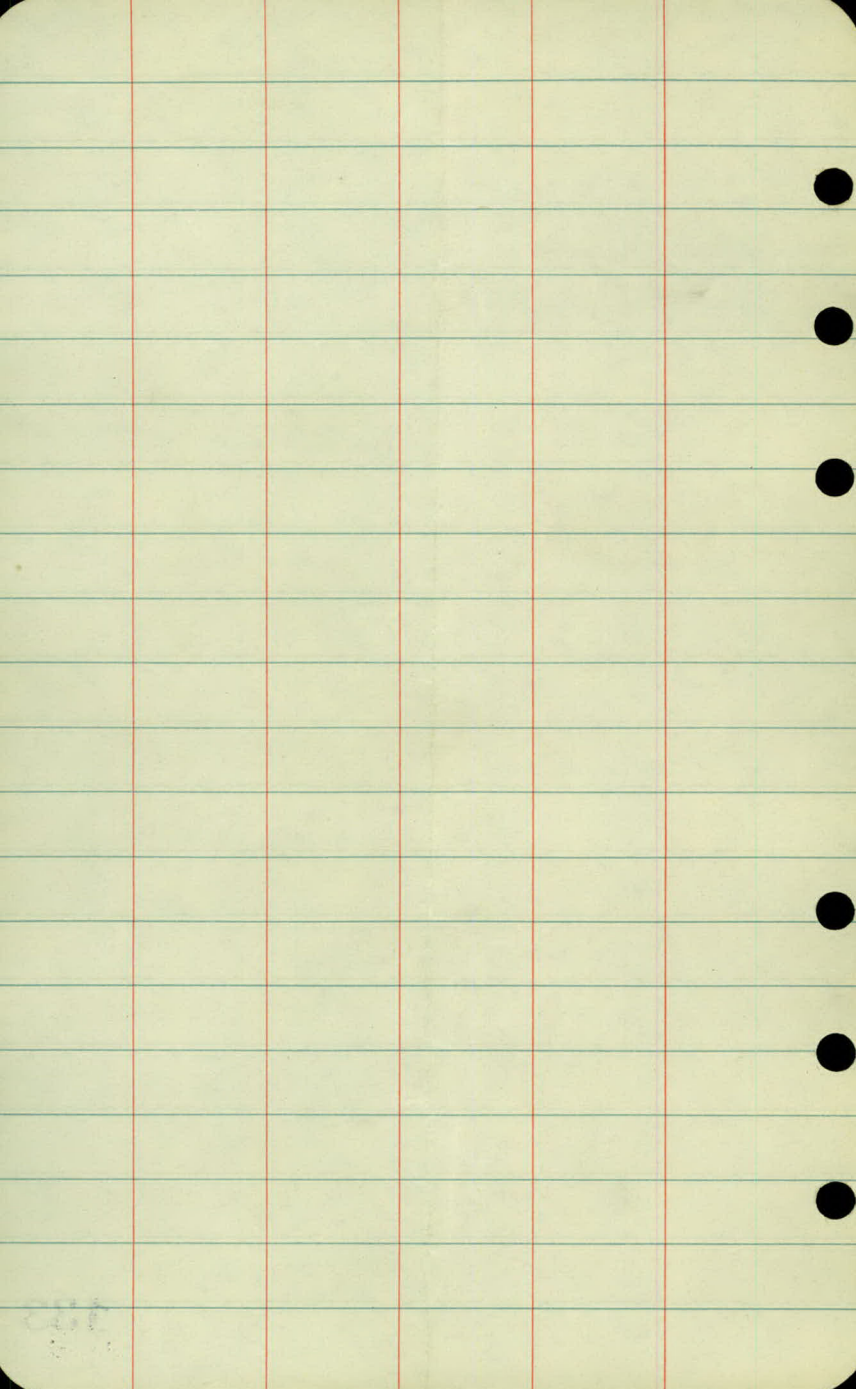
Oct 31, 1958
Clear 50°

2

3 + 75

Clay at Surface

50' Lt



FK
RL
RR
KO

Sept 16, 1959

1

Borrow Pit

FINAL X-SECTIONS

Sta + π - Elev

BM 8.83 901.42

(892.59)

0+00

10.1 891.3

0+50 No change

1

+50

2

+50

Sept 16, 1959

2

17

RT

91.8	93.5	94.7	94.5	93.8	92.7	91.0
9.6	7.9	6.7	6.9	7.6	8.7	10.4
47	38	26		16	27	40

✓

94.7	95.8	95.4	95.2	95.0	94.2	93.1	92.0
6.7	5.6	6.0	6.2	6.4	7.2	8.3	9.4
42	30	17		9	17	27	35

✓

94.6	96.2	95.7	94.9	94.3	93.8	91.2
6.8	5.2	5.7	6.5	7.1	7.6	10.2
46	33	18		13	24	37.5

✓

96.9	97.2	95.8	95.8	96.4	95.8	94.6	93.9	92.1
4.5	4.2	5.6	5.6	5.0	5.6	6.8	7.5	9.3
53	44	35	28	20		15	26	42

✓

Sta + Δ - Elev

901.42

3

✓

+30

✓

TP 5.76 898.66 8.52 892.90

+30

✓

✓

FX
AL
RR
KJ

Sept. 16, 1959
Sept 17, 1959 RT 3

11

97.2	96.9	96.8	96.3	96.1	95.2	94.8	94.4	93.6
4.2	4.5	4.6	5.1	5.3	6.2	6.6	7.0	7.8
31	25	18	8		19	29	40	55

95.7	95.8	96.5	96.7	95.2
5.7	5.6	4.9	4.7	6.2
38	46	50	54	60

96.0	95.9	95.8	95.8	95.4	95.4	94.9	94.7	94.4	93.9
5.4	5.5	5.6	5.6	6.0	6.0	6.5	6.7	7.0	7.5
46	35	24	17	8		9	21	30	48

95.3	94.3	92.9	91.4
6.1	7.1	8.5	10.0
54	56	71	80

Boat Spike P.L. 11-95.16

92.8	93.2
8.6	8.2
74	61

92.6	92.6	93.6	93.9	94.1	94.3	94.5	94.6	94.5
6.1	6.1	5.1	4.8	4.6	4.4	4.2	4.1	4.2
75	68	47	19		12	24	39	54

90.9	90.4	89.9
7.8	8.3	8.8
95	102	111

93.6	93.6	94.0	94.0	94.3
5.1	5.1	4.7	4.7	4.4
150	138	118	95	70

136

93.8	93.8	93.8	93.5	93.4
4.9	4.9	4.9	5.2	5.3
171	189	200	216	225

Sta + π - Elev.

898.66

A+30

A+50

/

✓

/

1

5

35.1

Sept 17, 1959

4

11

11

RT

92.3 91.2 90.0
6.4 7.5 8.7
243 260 273



93.4 94.3 94.1 94.1 94.3 94.1 94.6 94.8 94.8
5.3 4.4 4.6 4.6 4.4 4.6 4.1 3.9 3.9
74 58 34 12 17 35 55 75

91.7 90.4 89.6
7.0 8.3 9.1
97 107 123



93.7 94.3 94.4 94.5
5.0 4.4 4.3 4.2
150 128 116 97

93.5 93.5 92.1 90.7
5.2 5.2 6.6 8.0
177 192 225 241

89.9
8.8
255

93.9 95.2 95.3 95.5 95.5 95.3 95.6 95.1 95.1
4.8 3.5 3.4 3.2 3.2 3.4 3.1 3.6 3.6
98 75 48 22 25 49 75 101



Sta	+	π	-	Elev
-----	---	-------	---	------

		898.66		
--	--	--------	--	--

5+00				
------	--	--	--	--

+50				
-----	--	--	--	--

Co Rd I 58-03

0+00				
------	--	--	--	--

		8.95		
--	--	------	--	--

			89.71	89.7 ✓
--	--	--	-------	--------

+07				
-----	--	--	--	--

+13				
-----	--	--	--	--

Sept 17, 1959

5

LT

RT

✓

90.3
8.4
138
95.6
31
71
95.5
32
47
95.7
30
24
93.2
5.5
114

94.5
4.2
125
93.9
4.8
150
92.7
6.0
172
91.6
7.1
186
90.1
8.6
195
89.5
9.2
200

94.6
4.1
113
94.7
4.5
138
93.0
5.7
150
92.9
7.8
171
89.5
9.2
183

95.8
2.9
27
96.0
2.7
50
95.2
3.5
75
93.3
5.4
99
90.4
8.3
133
91.3
7.4
120

✓

89.7
9.0
51
ESB
89.7
9.0
40
EBS
89.5
9.2
31
BS
89.5
9.2
20
89.4
9.3
20
89.3
9.4
21
88.8
9.9
39
BS
88.7
10.0
56
BS
88.2
10.5
68
✓

89.6
9.1
63
89.5
9.2
40
89.5
9.2
31
89.5
9.2
20
89.4
9.3
20
89.3
9.4
21
88.8
9.9
39
BS
88.7
10.0
56
BS
88.2
10.5
68
✓

Sta + π - Elev

898.66

0 + 17

+40.5

+50

1

+50

✓

Sept. 17, 1959

6

11

BT

89.4	89.5	89.5	89.6	89.4	89.3	89.0	88.6	88.3
9.3	9.2	9.2	9.1	9.3	9.4	9.7	10.1	10.4
52	37	26	18	19	31	41	50	✓
SB	BS				BS	BS		

87.36
11.30
FL 24" CM
30'

86.66
12.0
FL 24" CM
30

87.7	87.9	87.5	87.7	90.0	89.7	89.5	87.4	87.1	✓
11.0	10.8	9.2	9.0	8.7	9.0	9.2	11.3	11.6	
50	32	19	13	BS	14	22	33	50	
					BS				

88.4	88.4	88.7	90.2	90.2	90.7	90.4	89.9 90.9	87.9	87.6	88.0	✓
10.3	10.3	10.0	8.5	8.5	8.0	8.3	7.8 7.8	10.8	11.1	10.7	
50	36	28	19	14		12	19	28	40	50	

89.6	89.0	89.1	90.4	90.7	91.2	90.8	90.4	88.9	88.3	88.2	
9.7	9.7	9.6	8.3	8.0	7.5	7.9	8.3	9.8	10.4	10.5	
50	37	28	20	13		12	18	23	32	36	

✓
88.8
9.9
50

Sta + π - Elev.

898.64

2

+50

3

+46

✓

+62

Sept. 17, 1959

7

89.8	89.4	89.4	90.8	91.0	91.4	91.2	90.9	88.7	88.4	89.2
89.9	9.3	9.3	7.9	7.7	7.3	7.5	7.8	9.8	10.3	9.5
50	38	27	19	13		12	18	26	39	50
88.9	89.1	89.6	91.0	91.2	91.8	91.5	91.2	88.7	87.9	88.9
9.8	9.6	9.1	7.7	7.5	6.9	7.2	7.5	10.0	10.8	9.8
50	35	26	18	14		12	18	28	40	50
89.3	89.4	89.6	91.6	91.9	92.2	91.9	91.5	89.5	89.2	89.1
9.4	9.3	9.1	7.1	6.8	6.5	6.8	7.2	9.2	9.5	9.6
50	38	28	19	13		12	18	28	36	50
90.7	90.3	92.0	92.3	92.7	92.3	91.9	90.4	90.3	90.7	
8.5	8.4	6.7	6.4	6.0	6.4	6.8	8.3	8.4	8.0	
33	28	18	13		12	18	27	32	36	
90.4	90.2						90.6		90.7	
8.3	8.5						8.1	8.0		
40	50						50	43		
90.7	90.5	92.1	92.4	92.8	92.4	92.0	90.6	90.6	91.4	
8.0	8.2	6.6	6.3	5.9	6.3	6.7	8.1	8.1	7.3	
33	27	18	13		12	18	27	33	41	
91.4	92.2	92.5							91.3	
7.3	6.5	6.2							7.4	
40	47	50							50	

Sta + π - Elev

898.66

4+00

✓

+ 25

✓

+50

✓

T.P. 4.01 896.91 5.75 892.91 (892.90)

Sept. 12, 1959

8

14

RA

91.0	91.1	92.3	92.6	93.0	92.7	92.3	91.1	91.5
77	76	64	61	57	60	64	76	72
33	26	18	13		12	17	28	34

92.3	93.4	94.0		96.3	95.0	93.3
64	53	47	✓	24	37	54
40	46	52		68	53	44

91.7	91.1	91.4	92.4	92.8	93.1	92.8	92.3	91.2	91.2	92.9
70	76	73	63	59	56	59	64	75	75	58
37	31	26	18	13		12	18	26	33	40

92.7	94.0							96.0	95.0
60	47							27	37
43	50							56	50

90.9	91.4	92.6	92.9	93.2	93.0	92.5	91.3	91.1	92.2
78	73	61	58	55	57	62	74	76	65
32	26	18	13		12	18	28	32	38

91.9	93.4	94.3					95.8	94.2
68	53	44					29	45
38	46	50					54	47

P.T.

Sta	+	π	-	Elev
-----	---	-------	---	------

		896.91		
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5+00				
------	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

+68				
-----	--	--	--	--

121

Sept. 13 1959

9

11

RT

91.1	91.5	92.9	93.3	93.5	93.2	92.9	91.7	91.7
5.8	5.4	4.0	3.6	3.4	3.7	4.0	5.2	5.2
31	27	18	13		12	17	26	33

91.6	93.6	94.4	94.5			94.8	94.5	93.1
5.3	3.3	2.5	2.4			2.1	2.4	3.8
36	44	53	67			51	48	41

91.6	91.9	93.2	93.5	93.8	93.5	93.2	91.9	91.5
5.3	5.0	3.7	3.4	3.1	3.4	3.7	5.0	5.4
31	26	19	14		12	17	25	31

92.1	93.5	93.7	94.1			92.5	92.8
4.8	3.4	3.2	2.8			4.4	4.1
37	45	56	67			51	41

91.7	91.8	93.2	93.5	93.9	93.6	93.3	91.9	91.5
5.2	5.1	3.7	3.4	3.0	3.3	3.6	5.0	5.4
32	28	19	14		12	17	25	31

91.8	93.4	93.6	93.8	93.9		91.6	92.1
5.1	3.5	3.3	3.1	3.0		5.3	4.8
35	44	56	65	68		54	44

Sta + π - Elev.

896.91

6 + 100

✓

+ 50

✓

7

✓

201

Sept. 17, 1959

10

Lt

St

5.1	4.8	3.5	3.3	2.9	3.3	3.6	5.0	5.6
31	27	19	14		12	17	27	35

4.6	3.7	3.4	3.4				6.1	5.7
39	42	65	75				52	45

5.0	4.7	3.6	3.2	3.0	3.3	3.6	5.1	6.1
33	29	18	15		12	18	27	37

3.8	3.3	3.2	4.5				6.5	
45	56	71	102				50	

5.6	5.2	3.8	3.4	3.1	3.3	3.7	5.3	6.8
33	27	18	13		12	17	28	39

4.4	3.8	5.6	6.4				2.0	
41	51	75	87				51	

Sta + π - Elev

896.91

7+50

✓

TP 1.87 895.30 3.48 893.43

8

✓

+50

✓

LET

Sept. 17, 1959 11

LT

RT

90.9	91.3	92.9	93.3	93.5	93.4	93.0	91.4	89.9
6.0	5.6	4.0	3.6	3.4	3.5	3.9	5.5	7.0
32	26	18	12		12	17	26	37
91.7	90.4							89.8
5.2	6.5							7.1
44	60							52
8+00								

90.5	90.8	92.7	93.1	93.4	93.2	92.8	91.0	89.9	89.5
4.8	4.5	2.6	2.2	1.9	2.1	2.5	4.3	5.4	5.8
31	27	18	13		12	17	27	36	50

90.4	90.1	89.9							
4.9	5.2	5.4							
35	44	50							

90.3	90.9	91.6	91.9	93.3	93.0	92.7	90.7	90.1	
5.0	4.4	3.7	3.4	2.0	2.3	2.6	4.6	5.2	
30	26	18	13		12	17	28	33	

89.7	89.8								
5.6	5.5								
39	50								
89.5	89.9								
5.8	5.4								
50	44								

Sta + Δ - Elev

895.30

9+00

+50

10

T.P. 3.25 896.24 2.31 892.99

2 Sept. 17, 1959 12

LT

RI

90.1	90.8	92.3	92.7	93.1	92.8	92.5	90.7	90.2	90.8
5.2	4.5	3.0	2.6	2.2	2.5	2.8	4.6	5.1	4.5
37	27	18	13		12	17	27	33	43

90.0
5.3
46

89.4
5.9
50

✓

91.3
4.0
50

89.4	90.2	90.9	92.1	92.6	93.0	92.7	92.3	91.3	90.8
5.9	5.1	4.4	3.2	2.7	2.3	2.6	3.0	4.0	4.5
50	39	28	18	13		11	17	25	30

✓

91.2
4.1
50

91.0
4.3
37

90.7	91.2	92.1	92.4	93.0	92.7	92.2	91.0	90.9
4.6	4.1	3.2	2.9	2.3	2.6	3.1	4.3	4.4
35	27	18	13		12	17	27	37

90.2
5.1
45

89.9
5.4
52

✓

90.6
4.7
50

Sta 10 E

✓

Sta + π - Elev

896.24

10 + 50

+ 88 x-Drain

11

✓

+ 50

12

FK
RL
RR
KJ

Sept. 18, 1959

13

LT

RT

90.0	90.5	91.2	92.0	92.4	92.9	92.6	92.1	90.8	90.3	90.5
62	57	50	42	38	33	36	41	54	59	51
50	40	27	18	12	✓ 3	13	18	26	34	50

87.69
8.55
29
FL 24" CM

92.8
34

87.02
9.22
31
FL 24" CM

90.1	90.2	92.0	92.4	92.79	92.5	92.1	90.9	90.4
61	60	42	38	345	37	41	53	58
37	27	18	13		12	18	27	34

89.8
64
50

89.2
70
50

90.1	90.4	91.0	92.1	92.4	92.7	92.4	92.1	91.1	90.7	90.6
61	58	52	41	38	35	38	41	51	55	56
50	✓ 40	27	17	12		13	18	27	37	50

90.1	90.7	91.3	92.1	92.5	92.8	92.5	92.1	90.9	90.3	90.6
61	55	49	41	37	34	37	41	53	59	56
50	40	27	18	13		12	17	26	40	50

Sta + π - Elev

896.24

12 + 50

13

+ 50

14

+ 50

15 + 00 X Drain

Sept. 18, 1958

14

11

81

90.3	90.5	91.1	92.1	92.5	92.8	92.5	92.0	90.7	89.9	89.6
5.9	5.7	5.1	4.1	3.7	3.4	3.7	4.2	5.5	6.3	6.6
50	40	27	18	13		12	17	30	41	50

90.7	90.9	91.1	92.0	92.5	92.7	92.5	92.1	90.7	89.7	89.6
5.5	5.3	5.1	4.2	3.7	3	3.7	4.1	5.5	6.5	6.6
50	42	29	18	14		11	18	33	48	50

90.4	90.1	90.9	92.0	92.3	92.8	92.5	92.1	91.1	90.3	89.9
5.8	6.1	5.3	4.2	3.9	3.4	3.7	4.1	5.1	5.9	6.3
50	45	31	19	14		11	17	30	45	50

90.5	90.4	91.0	92.1	92.4	92.8	92.6	92.1	91.1	90.6	89.5
5.7	5.8	5.2	4.1	3.8	3.4	3.6	4.1	5.1	5.6	6.7
50	40	29	19	15		11	18	29	38	50

90.0	90.6	91.1	92.2	92.4	92.7	92.5	92.0	91.1	90.5	90.3	89.8
6.2	5.6	5.1	4.0	3.8	3.5	3.7	4.2	5.1	5.7	5.9	6.4
50	37	27	18	14		11	18	21	31	41	50

86.01

10.23

FL 2A "CM

41'

85.85

10.39

FL 2A "CM

40'

Sta	+	π	-	Elev
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		896.24		
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15+00				
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+20				
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+50				
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TP	6.54	898.93	3.85	892.39
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16+00	6.54	898.93		
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K.S.

✓

+50				
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✓

Sept 18, 1959

15

11

RT

88.2	89.5	90.7	92.1	92.4	92.8	92.4	92.2	90.8	90.4	88.9
80	67	55	41	38	34	38	40	54	58	73
40	36	27	18	14		13	18	26	35	39

90.3	89.9	90.6	92.0	92.3	92.8	92.6	91.9	90.8	89.5	89.1
59	63	56	42	39	34	36	43	54	67	71
50	35	30	18	14		13	19	27	43	50

91.1	90.7	92.0	92.4	92.8	92.5	92.1	90.3	89.5
51	55	42	58	34	37	41	59	67
50	31	18	13		14	19	39	50

91.6	91.3	91.8	92.1	92.2	92.7	92.5	92.0	90.6	90.7	90.7
73	26	71	68	67	62	64	69	83	82	82
36	28	23	19	17		16	19	33	39	50

92.5	92.0	91.9	92.6	92.7	92.4	91.5	91.9	91.8	91.6
64	69	70	63	62	65	74	70	71	73
34	27	23	20		21	24	29	39	50

Sta.	+	T	-	Elev
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		898.93		
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17100				
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✓				
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+50				
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✓				
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✓				
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TP	8.02	902.89	4.06	894.87
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18				
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September 18, 1939

4.

101

Rt.

16

93.3	93.2	92.7	93.0	93.1	93.0	92.9	93.4	93.4
5.6	5.7	6.2	5.9	5.8	5.9	6.0	5.5	5.5
27	21.5	21	11		12	21	22	29
93.5	94.2	95.1	95.1			93.5	93.8	93.2
5.4	4.7	3.8	38	✓		5.4	5.1	5.7
36	41.5	48.5	50			50	41	37

93.6	93.8	93.2	93.5	93.7	93.7	93.2	93.8	93.7	93.8
5.3	5.1	5.7	5.4	5.2	5.2	5.7	5.1	5.2	5.1
25	21.5	21	11		9	21.5	22	29	36
97.9	97.5	97.5	97.7	98.3	98.2	97.9	96.2	94.2	
5.0	3.4	1.4	1.2	0.6	0.7	1.0	2.7	4.7	
36	44	52	69	50	49	46	42	38	

98.3

0.6

100

277

1.2

75

P.T. Boot Spike

^{95.3}	^{94.4}	^{94.4}	^{94.3}	^{93.8}	^{94.1}	^{94.3}	^{94.2}	^{93.9}	^{94.4}	^{94.5}	^{94.6}
76	85	85	86	91	88	86	87	90	85	84	83
43	37	25	22	21.5	12		9	22	22.5	31	37

^{98.2}	^{98.4}	^{98.6}	^{98.9}				^{98.6}	^{99.5}	^{95.9}
→ 47	45	43	40		✓		0.3	3.4	70
54	67	75	100			X	56	49	40

Sta.

+

π

-

Elev.

902.89

18+25

✓

+50

✓

+75

✓

300

September 18, 1959.

17

H.

Rt.

95.1	94.8	94.5	94.0	94.3	94.6	94.5	94.2	94.7	94.8	94.7
28	8.1	8.4	8.9	8.6	8.3	8.4	8.7	8.2	8.1	8.2
40	28	22.5	22	12		10	21.5	22	26	34

a c

95.9	97.9	98.3	98.5	98.8	98.9	✓ 02.9	00.5	97.9	96.3	95.2
7.0	5.0	4.6	4.4	4.1	4.0	0.0	2.4	5.5	6.6	7.7
45	52	55	66	76	100	56	50	43	40	38

95.5	95.0	94.9	94.3	94.7	94.9	94.9	94.5	95.0	95.1	95.1
7.4	7.9	8.0	8.6	8.2	8.0	8.0	8.4	7.9	7.8	7.8
42	33	22.5	22	9		8	22.5	23	31	35

98.5	98.7	98.9	99.1		✓ 02.8	01.8	97.6	95.9
4.4	4.2	4.0	3.8		0.1	1.1	5.3	7.0
54	63	73	100		58	56	45	40

95.8	95.3	95.1	94.6	94.8	95.1	95.0	94.8	95.3	95.4	96.7
7.1	7.6	7.8	8.3	8.1	7.8	7.9	8.1	7.6	7.5	6.2
42	36	22	21.5	13		14	22.5	23	37	43

97.7	98.1	98.6	98.9	99.0		✓ 01.0	98.6
5.2	4.8	4.3	4.0	3.9		1.9	4.3
50	33	61	75	100		55	49

Sta.

+

X

-

Elev.

902.89

19

✓

✓

+27.25

✓

✓

T.P

11.95

908.20

6.64

896.25

Sept 18, 1959

18

LT.

RT.

95.4	95.4	94.8	95.1	95.3	95.3	95.0	95.7	95.5
75	75	8.1	78	76	76	7.9	7.2	7.4
32	22.5	22	13		10	22.5	23	31

95.6	95.9	98.0	98.5
7.3	7.0	4.9	4.4
38	41	51	59

92.9	90.2	96.3	95.6
0.0	2.7	4.6	7.3
61	55	42	38

99.0	98.8	98.6
3.9	4.1	4.3
100	75	65

✓

96.0	95.8	95.3	95.3	95.6	95.6	95.4	95.3	95.7	95.8	96.1
6.9	7.1	2.6	7.6	7.3	7.3	7.5	7.6	7.2	7.1	6.8
38	25.5	25	23	9	10	21.5	22	31	40	

Right Side

Left Side

96.4	97.0	97.6	98.2
6.5	5.9	5.3	4.7
45	52	59	65

97.7	97.7	97.1
5.2	5.2	5.8
54	50	48

✓

99.2	98.9	98.6
3.7	4.0	4.3
75	73	69

Ent Curb Rt 19+45

✓

19142

Sta + A - Elev

908+20

18+00

+25

+50

+75

19

TP 11.59 907.84 11.95 896.25

19+39 ± Ent RT

0475 of Enti

FX
BR
JH

Sept 21, 1959 19
Fog 69° RH

11

3.2	3.2
0	0
5.0	5.0
57	68

✓

05.2	05.2
3.0	3.0
62	69

✓

06.6	06.8
1.6	1.4
67	73

✓

06.8	08.0
1.4	1.2
68	74

✓

04.8	06.4	07.5
3.4	1.8	0.7
66	73	81

✓

03.4	01.1	99.4	99.0	99.1	99.1	99.5	04.4	06.4
4.4	6.7	8.4	8.8	8.7	8.7	8.3	3.4	1.4
26	19	12	7		7	13	24	33
NG								NG

✓

Sfa + π - Elev

907.84

1 + 00

+25

+50

+75 End of Ent Cut

19 + 50

Sept. 26, 1959 20

05.2	02.6	01.5	01.4	01.3	02.5	06.4	06.7
2.6	5.2	6.3	6.4	6.5	5.3	1.4	1.1
19	12	7		7	12	21	23
NG							NG

06.0	03.7	03.6	03.5	03.6	05.2	07.1
1.8	4.1	4.2	4.3	4.2	2.6	0.7
18	9	7		7	11	17
NG						NG

05.6	05.0	05.0	05.1	05.3	06.2
2.0	2.8	2.8	2.7	2.5	1.6
16	10	7		7	10
NG					NG

95.9	95.4	95.6	95.84	95.8	95.5	96.1	96.1
119	124	122	120	120	123	117	117
21.5	21	14		11	23	24	37

95.9	96.0
12.1	11.8
26	37

99.5	98.8	97.1
8.3	9.0	10.7
75	67	54

Sta	+	π	-	Elev
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		907.84		
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19+79				
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✓				
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20				
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✓				
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+27				
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✓				
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Sept. 26, 1959 21

96.3 95.8 95.9 96.2 96.1 95.8 96.4

11.5 12.0 11.9 11.6 11.7 12.0 11.4
22 21.5 11 10 22 22.5

96.1 96.5 02.3 01.8 97.7 96.6 96.3

11.7 11.3 5.5 6.0 10.1 11.2 11.5
29 38 68 62 46 41 31

96.6 96.1 96.2 96.3 96.2 96.0 96.5 96.6

11.2 11.7 11.6 11.5 11.6 11.8 11.3 11.2
22 21.5 10 12 22 22.5 32

96.9 96.7 01.2 01.0 97.9 96.7

11.4 11.1 6.6 6.8 9.9 11.1
25 38 66 58 46 39

97.0 96.5 96.5 96.6 96.4 96.2 96.5 97.0

10.8 11.3 11.3 11.2 11.4 11.6 11.0 10.8
22 21.5 11 14 21.5 22 32

97.0 01.0 01.1 97.1

10.8 6.8 6.7 10.7
35 64 56 38

Sta + π - Elev

907.84

20+50

✓

21

✓

+50

201

Sept 21, 1959

22

LT

84

97.2

96.7

96.8

97.0

96.7

96.7

97.2

97.3

10.6
22.5

11.1
22

11.0
10

10.8

11.1
14

11.1
21.5

10.6
22

10.5
32

97.4

10.4
35

90.9

6.9
60

91.0

6.8
55

99.4

8.4
48

97.5

10.3
39

97.9

9.9
41
in Ent

97.0

10.8
21

97.3

10.5
10

97.5

10.3

97.4

10.4
10

97.3

10.5
21.5

97.9

9.9
22

97.9

9.9
31

92.1

5.7
72

91.8

6.0
58

98.2

9.6
39

98.5

9.3
38

98.3

9.5
22

97.8

10.0
21.5

98.0

9.8
10

98.0

9.8

98.0

9.8
12

97.8

10.0
21.5

98.1

9.4
22

98.5

9.3
37

93.1

9.7
74

93.3

9.5
57

Sta + π - Elev

907.84

21+65

✓

22

✓

+50

008

Sept. 21, 1959

23

LT

BT

98.6	98.4	97.9	98.2	98.2	98.1	97.9	98.4	98.6
9.2	9.4	9.9	9.6	9.6	9.7	9.9	9.4	9.2
38	22	21.5	11		10	22	22.5	38

✓

98.1	98.9
8.7	8.9
73	59

99.0	98.6	98.1	98.4	98.5	98.4	98.1	98.6	98.9
8.8	9.2	9.7	9.4	9.3	9.4	9.7	9.2	8.9
37	22	21.5	11		11	22	22.5	38

✓

95.0	95.2
2.8	2.6
75	64

99.3	98.8	98.3	98.6	98.7	98.6	98.5	99.1	99.3
8.5	9.0	9.5	9.2	9.1	9.2	9.3	8.7	8.5
36	22	21.5	9		11	22	22.5	38

✓

95.7	95.7
2.1	2.1
75	67

Sta + π - Elev

907.84

23

✓

+50

✓

24

✓

TP 6.58 904.85 9.57 898.27

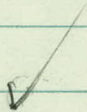
2 Sept 21, 1959

24

LT

RT

99.4	98.9	98.4	98.7	98.7	98.7	98.5	99.1	99.3
8.4	8.9	9.4	9.1	9.1	9.1	9.3	8.7	8.5
38	22	21.5	9		12	21.5	22.5	38



06.6
1.2
75

06.8
1.0
71

99.2	98.7	98.2	98.4	98.4	98.4	98.3	98.8	99.1
8.6	9.1	9.6	9.4	9.4	9.4	9.5	9.0	8.7
38	22	21	9		10	21.5	22	37



06.8
1.0
79

06.7
1.1
73

98.7	98.3	97.7	98.0	98.0	97.9	97.6	98.2	98.4
9.1	9.5	10.1	9.8	9.8	9.9	10.2	9.6	9.4
37	22.5	22	10		11	21.5	22	37



06.0
1.8
75

05.9
1.9
69

Sept 21, 1959 25

97.9	97.3	97.0	97.2	97.3	97.1	96.8	RT	97.4	97.7
6.9	7.3	7.8	7.6	7.5	7.7	8.0		7.4	7.1
38	22.5	22	11		11	21.5		22	38

04.0	03.9	01.5
18	0.9	3.3
73	65	53

97.1	96.3	96.6	96.6	96.3	96.0	96.5	97.0
7.7	8.5	8.2	8.2	8.5	8.8	8.3	7.8
48	21	9		11	21.5	22	37
In Ent							

01.3	00.9
3.5	3.9
65	54

96.7	95.9	96.3	96.3	96.0	95.6	96.2	96.8	00.3
8.1	8.9	8.5	8.5	8.8	9.2	8.6	8.0	4.5
39	21.5	9		10	21.5	22	38	53

00.0
4.8
65

Sta + π - E/cv

904.85

25+50

✓

26

✓

+46

+54

128

2 Sept 21, 1959 26

96.7	95.8	95.3	95.7	95.7	95.6	95.2	95.7	96.0
8.1	9.0	9.5	9.1	9.1	9.2	9.6	9.1	8.8
40	22.5	22	11		10	22	22.5	36

97.5	97.6	96.3
7.3	7.2	8.5
59	50	40

95.2	94.7	94.9	94.9	94.6	94.3	94.8	94.7
9.6	10.1	9.9	9.9	10.2	10.5	10.0	10.1
22.5	22	10		11	22	22.5	37

95.8	96.0	94.3
9.0	8.8	10.5
39	62	51

94.7	94.9	94.4	94.0	93.7	93.2	93.9	93.4
10.1	9.9	10.4	10.8	11.1	11.6	10.9	11.4
50	40	23		15	27	30	50

94.9	94.8	94.4	94.3	94.1	93.7	93.3	93.1	93.0
9.9	10.0	10.4	10.5	10.7	11.1	11.5	11.7	11.8
50	45	28	14		17	31	44	50

Sta + x - Elev

904.85

26+62

+70

+78.65

10.4

94.45

cal. ✓

94.48

BM

12.28

892.57

92.41

892.23

TP

2.64

898.89

8.67

896.18

896.25

19

3.59

95.30

95.29

4.26

94.73

BM

6.60

898.82

6.60

892.29

892.22

TP

7.05

903.30

2.64

896.28

896.25

T.P.

2.46

900.76

5.00

898.30

5.95

97.35

97.35

4.12

96.64

96.65

± Lev

6.20

894.56

BM 40' Rt

6.83

893.93

8.18

892.58

Sept 21, 1959 27

✓ 95.1	94.9	94.6	94.4	94.2	93.9	93.5	93.4
9.7	9.9	10.2	10.4	10.6	10.9	11.3	11.4
50	43	27	14		15	36	50

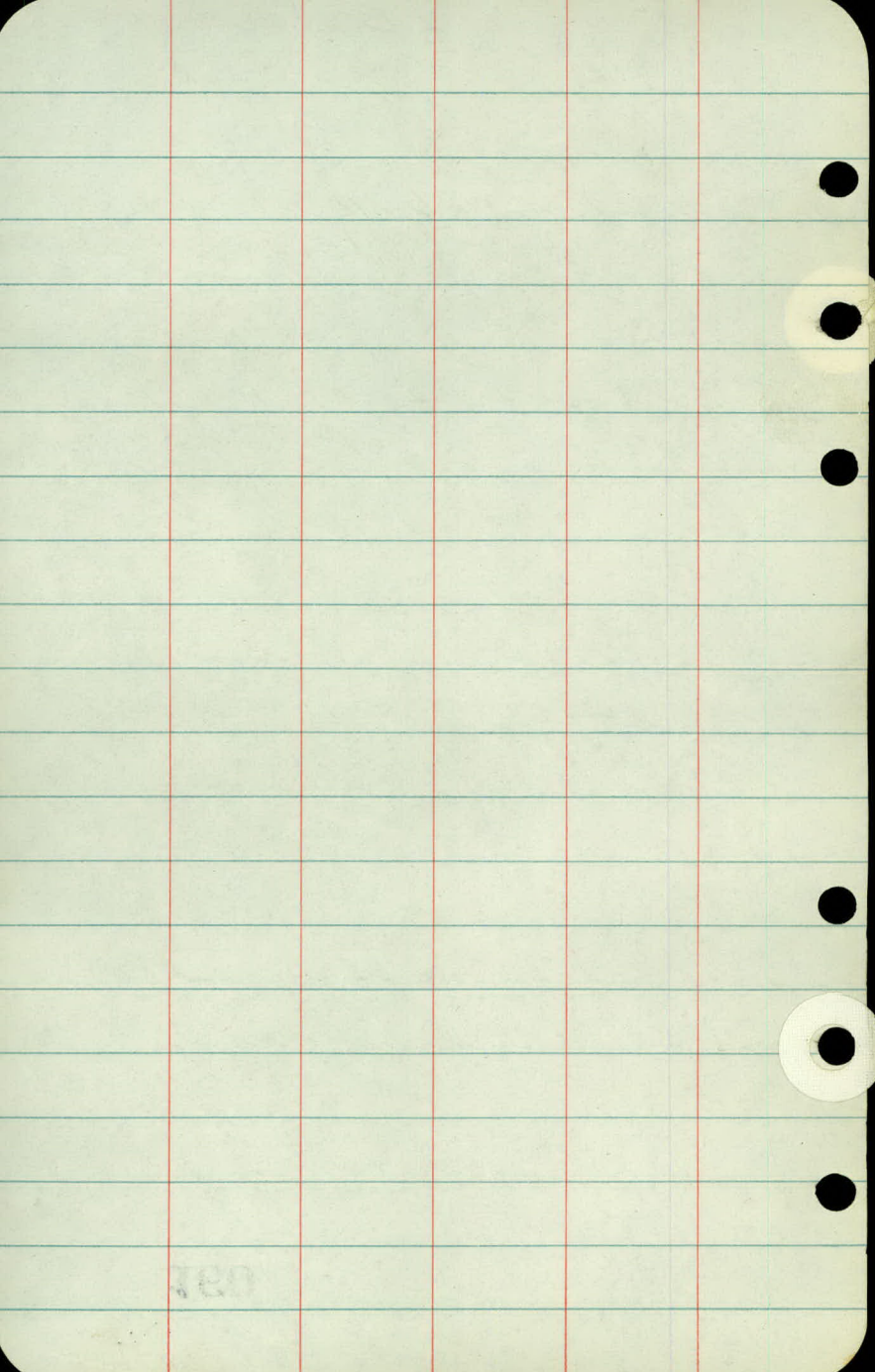
✓ 95.1	94.8	94.5	94.4	94.1	93.7	93.5
9.7	10.0	10.3	10.4	10.7	11.1	11.3
50	30	15		16	39	50

Spike in PP S.W. Cor Lex & Co Rd I
Ent Curb Rt 19+45

Spike in 24" oak 100' Rt Sta 16+80
Ent Curb Rt 19+45

160 → 09T

Spike in PP S.W. Cor Lex & Co Rd I



Final Topography

Co. Rd "I"

Hamline Ave. to Lexington Ave.

6 Pages

5+00

Lt.

±

Rt.

13.4 BT 12.1

17.9 B 17.3

+50

13.4 BT 12.1

17.5 B 17.4

13.2 BT 12.2

17.5 B 17.4

4+00

+50

13.2 BT 12.8

17.1 B 17.4

3+00

13.7 BT 12.6

18.3 B 17.5

2+00

13.3 BT 12.6

18.5 B 18.0

1+00

14.3 BT 12.9

18.2 B 17.7

End Radius

447 12

+ 47

End Radius

15

IMP
24" x 60' CM

+50

+39 30 Lt.

12.4 BT 17.7

12.7 B 17.1

B. Rad

+06 53

B. Rad

+06 80

+07 51 - 56

0+00 ± Hamline

+06 = Edge of B-S.

Note: {

BT = Black Top

B = Lift or Base

RG
JH

Lt.

±

Sept 15, 1959
Cool, & Windy
Rt.

z ——— n

Hamline Ave

Lt.

Z

Rt.

10+00

12.8 BT 12.6
18.2 B 17.5

9+00

12.7 BT 12.7
18.0 B 17.6

8+00

13.2 BT 12.1
18.0 B 17.3

7+00

12.8 BT 12.6
17.6 B 18.0

+50

13.2 BT 12.6
17.9 B 17.8

6+00

13.8 BT 11.9
18.4 B 16.9

+50

13.7 BT 12.3
18.3 B 17.0

5+00

13.4 BT 12.1
17.9 B 17.3

R6
JH

Sept 15, 1959
Cool, Windy
Rt,

2

Lt,

4

N
|
S

Lt.

Z

Rt.

15+00

14.7 BT 13.2
18.1 B 18.4

150

14.5 BT 12.0
18.1 B 18.2

14+00

15.3 BT 11.5
19.0 B 17.7

13+00

14.1 BT 12.3
18.5 B 18.2

12+00

12.8 BT 12.4
18.2 B 17.6

11+00

12.7 BT 12.8
17.9 B 17.5

+88.5

10P
24" X 60' CM
29

10+00

12.8 BT 12.6
18.2 B 17.5

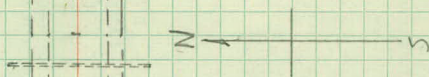
KG
IH

Sept 15, 1959
Cool, Windy
Rt.

3

Lt.

L



20+00

Lt.

21.5 22.0

Rt.

	Begin Rad	End Rad
+45	31.7	+54 23.2
+38 Ent (12')		
	Begin Rad	End Rad
+19	22.2	+32 31.3

19+00

21.4 22.1

18+00

21.5 22.0

+50
20.9 21.5

17+00

	21.0, 21.5	
	Begin Curb	Begin Curb
+73	20.8	+75 21.0
	+50	
	20.3 BT 21.2	
	21.2 B 23.3	

16+00

16.4 BT 17.2
18.9 B 19.5

+50
14.0 BT 14.3
17.6 B 18.6

15+00

14.7 BT 13.2
18.1 B 18.4

R6
JH

Lt.

4

Sept 15, 1959
Cool, Windy
Rt.

4



25+00

Lt.

21.8 21.9

Rt.

End Rad

+89

49.0

Begin Rad

+82

22.0

End Curb

+82

22.0

24+00

21.8 21.8

23+00

21.8 21.8

22+00

21.7 22.0

End Rad

+21

22.1

Begin Rad

+08

47

21+00

21.7 21.9

+98 Ent

End Rad

+82

36

Begin Rad

+76

21.6

End of Curb

+76

21.6

20+00

21.5 22.0

RG
JH

Sept 15, 1959
Cool, Windy
RT

5

LT,

4

1

2

3

2

3

Lt.

±

Rt.

27+00	+73.5 = Lexington	
End Bit. +64	Edge Blacktop	+64 End Bit.
+64	45	End Rad
+64	52	+50
+35	21.8	27.2 BT 30.5
	Begin Rad	+64
		End Rad
		60
		Begin Rad
		21.8
	+35	End Curb
	21.8	21.8
26+00	21.8 21.8	

+25	Begin Curb	End Rad
	21.8	21.8
+19	Begin Rad	RT+27
	37.5	

25+00 21.8 21.9

RG
JH

Lt.

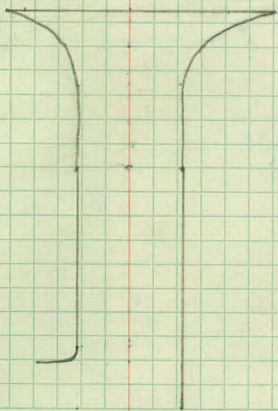
2

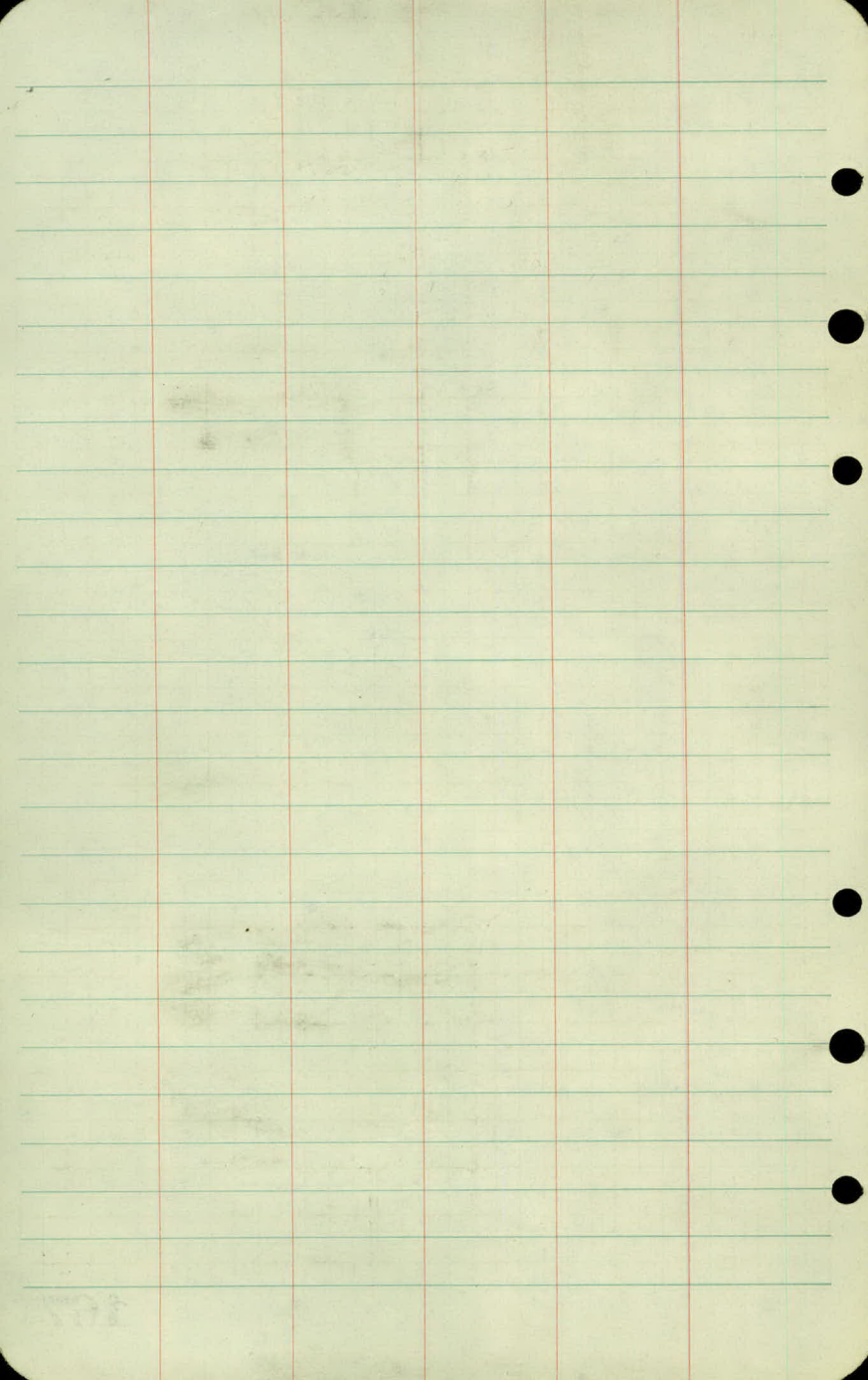
Sept 15, 1959
Cool, Windy
Rt.

6



Lexington Ave





October 28, 1959

1

Co Rd I 58-03

Curb Length

Culvert Location

20+76

End Curb

16+75

Begin curb

Begin Curb

14+98

24" X 81' CM X-Drain

41 - 40

+0.7

BT
38

SB
53

+12

BT
31

SB
45

+0.7

BT
46

SB
53

+12

BT
39

SB
46

FK
HP
KJ

October 28, 1959

2

40	1
36	3
11	2
26	2.2
69	6.6
183	4.8 =

Total Curb

+50	BT	SB
	13	18

+40	BT	SB
	13	18

+30	BT	SB
	16	25

+20	BT	SB
	23	36

112 LF

363 LF to Ent

401 LF to Ent

696.6 LF Curb
Including Radius

268.2 LF to Ent
Including Radius

163' 13.4'

Ent Slab =
16.3' x 13.4'

+50	BT	SB
	15	17

+40	BT	SB
	17	21

+30	BT	SB
	21	25

+20	BT	SB
	28	36

Hamline

169

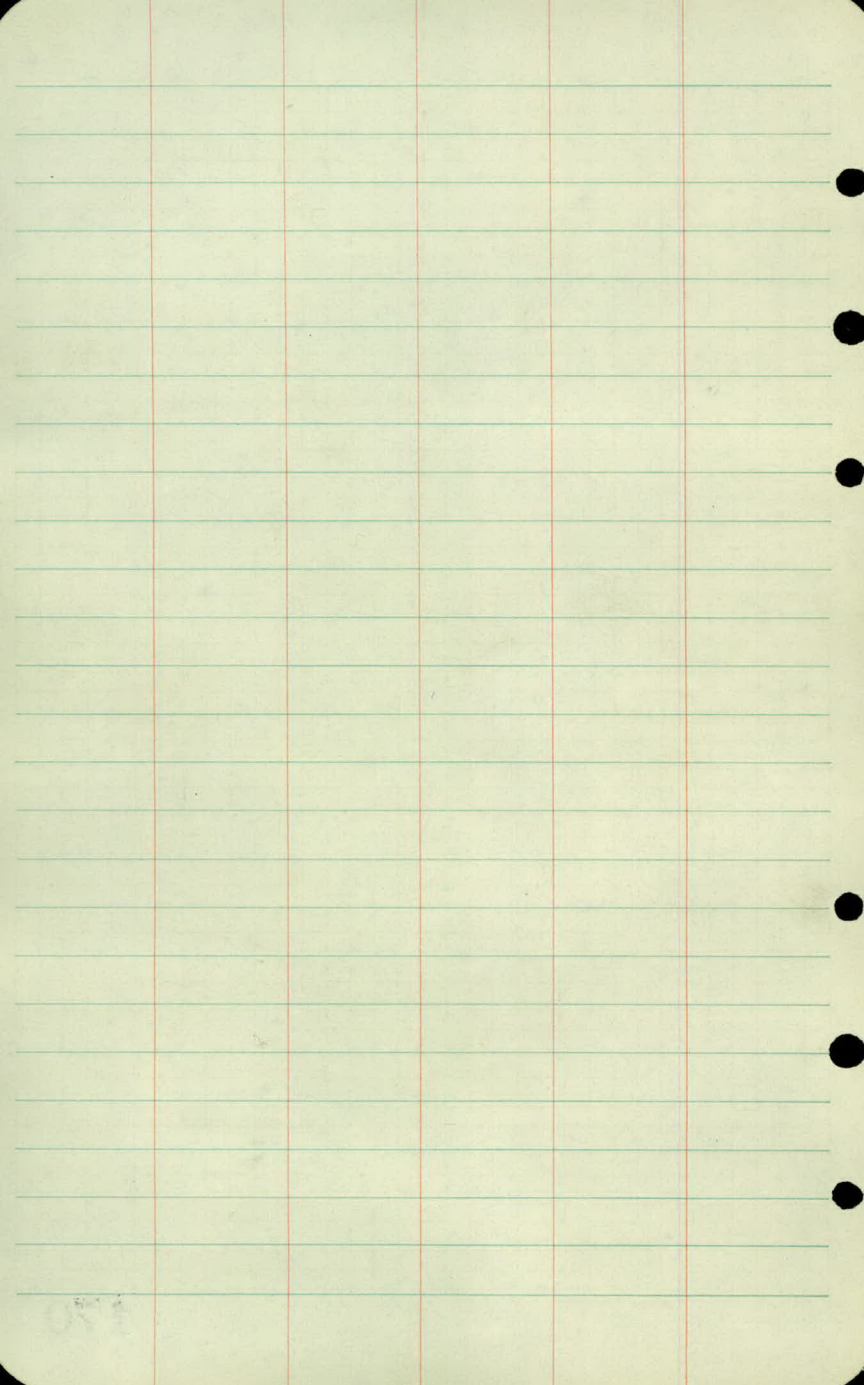
4

$\begin{array}{r} +71 \quad \overline{BT} \quad \overline{SB} \\ 44 \quad 51 \\ +67 \quad \overline{BT} \quad \overline{SB} \\ 39 \quad 49 \end{array}$	$\begin{array}{r} +71 \quad \overline{BT} \quad \overline{SB} \\ 48 \quad 35 \\ +67 \quad \overline{BT} \quad \overline{SB} \\ 43 \quad 48 \end{array}$
$\begin{array}{r} 155 \quad \overline{BT} \quad \overline{SB} \\ 25 \quad 28 \end{array} \quad +67 \quad \overline{BT} \quad \overline{SB} \quad 36$	$\begin{array}{r} 155 \quad \overline{BT} \quad \overline{SB} \\ 28 \quad 31 \end{array} \quad +67 \quad \overline{BT} \quad \overline{SB} \quad 40$
$\begin{array}{r} 26 \quad +45 \quad \overline{BT+SB} \\ 23 \end{array}$	$\begin{array}{r} +45 \quad \overline{BT} \quad \overline{SB} \\ 24 \quad 25 \end{array}$

October 28, 1959

3

Lexington



Nov. 2, 1959

1

Seeding Area

5

Seeding
45 - 18 18 - 48

Seeding
+50 48-18 19-50

A

Seeding
49 - 18 18 - 54

Seeding
+50 45-17 19-42

3

Seeding
43 - 19 18 - 45

2

Seeding
42 - 19 18 - 46

1

Seeding
38 - 18 18 47

Seeding
+60 35-17-20-40

Seeding
+40 35-21

+18 Cor.S
133

+18 Cor.S
90

+40 Seeding
25-37

+20 Seeding
50-90

0 +107 Cor.S
64 133

+07 Cor.S
90

FK
RG
KP
KJ

Nov. 2, 1959

2

27

30

50 X 28

50 X 31

30

31

50 X 31

50 X 33

31

36

50 X 29

50 X 29

27

23

50 X 25

50 X 25

24

27

Seeded Area

Seeded Area

100 X 24

100 X 27

23

28

100 X 21

100 X 29

20

29

40 X 19

40 X 25

18

20

20 X 17

20 X 16

14

12

10 X 80

10

seeding
43-18 18-40

9

seeding
38-18 18-40

8

seeding
31-18 18-36

seeding
+150 35-18 18-43

7

seeding
43-18 18-42

seeding
+150 45-19 18-46

6

seeding
48-19 18-42

seeding
+150 45-19 18-45

5

Nov 2, 1959

5

25

22

100 X 22

100 X 22

20

22

100 X 17

100 X 20

13

18

50 X 15

X

50 X 22

17

25

50 X 21

7

50 X 24

X

25

24

50 X 26

50 X 23

26

22

50 X 27

50 X 23

29

24

50 X 26

50 X 24

50 X 26

50 X 24

26

27

50 X 27

50 X 28

27

30

173

Seeded Area

Seeded Area

15

Seeding
35-18 18-35

14

Seeding
45-18 18-45

Seeding
+50 45-19 18-42

13

Seeding
45 19 18-42

Seeding
+50 45-18 18-43

12

Seeding
45-19 19-42

11

Seeding
40-19 18-40

10

Nov 2. 1959

4

17

17

100 x 22

100 x 22

27

27

50 x 26

50 x 26

26

24

50 x 26

50 x 24

26

24

50 x 26

50 x 24

27

25

50 x 26

50 x 24

26

23

Seeded Area

Seeded Area

100 x 24

100 x 22

21

22

100 x 23

100 x 22

25

22

26

Seeding
40-23 23-56

Ent Cut Area
seeded
R+

19

+21 Seeding
50-22
Seeding
← 22 23-57

+150 Seeding
← 22 23-56

18

Seeding
← 22 23-51

+150 Seeding
← 22 22-47

17

Seeding
100 ← 22 22-49

+150 Seeding
100 ← 22 23-50

16

Seeding
100 ← 20 20-57

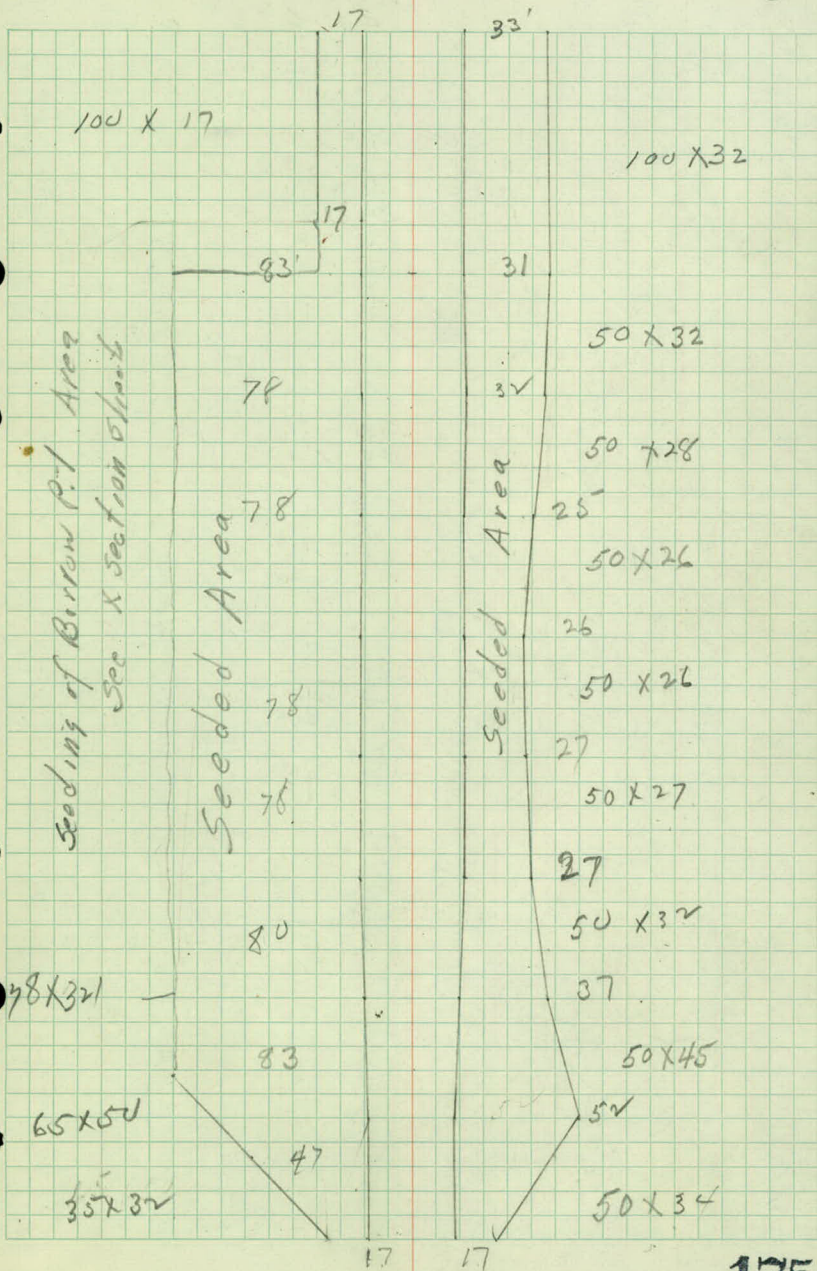
+56 Seeding
90 ← 18 18-70

+35 Seeding
66 18

15

Nov 2, 1959

5



25

Seeding
23-60

24

Seeding
23-72

23

Seeding
23-69

22

Seeding
23-65

21

Seeding
23-55

+80 End Seeding
90-23

20

Nov 2, 1959

6

37

$$100 \times 43 =$$

49

$$100 \times 48$$

46

$$100 \times 44$$

42

$$100 \times 39$$

37

$$100 \times 35 =$$

33

No Sampling

Seeded Area

17

$$100 \times 17$$

17

176

+62 End seeding
50 - 75
+50 seeding
35 - 78

+35 Cor seeding
23 - 60

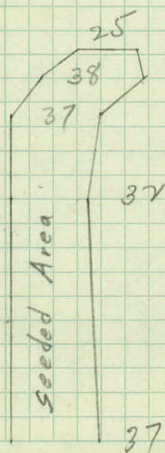
seeding
23 - 55

26

25

Nov. 2, 1959

7



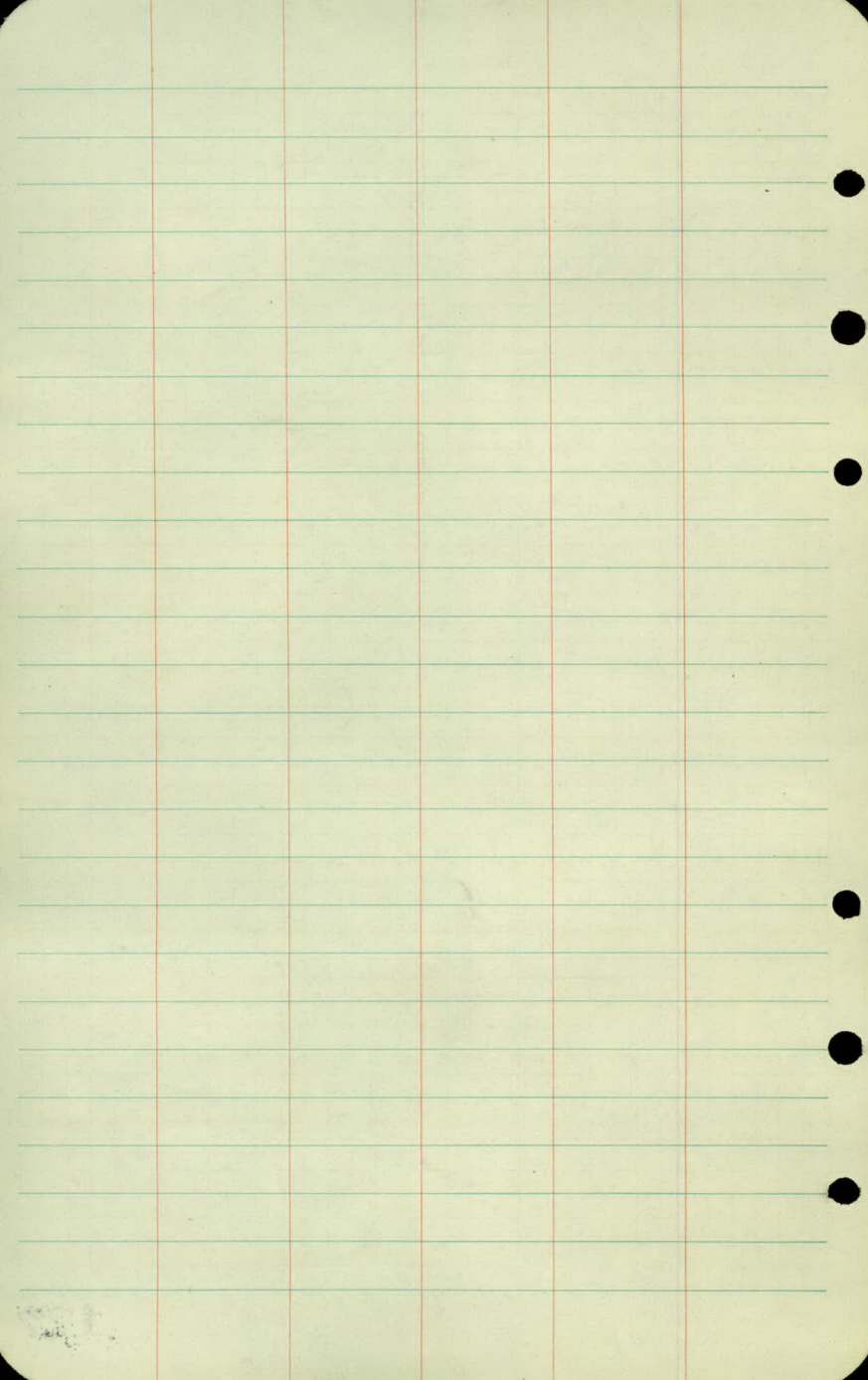
$$12 \times 32 =$$

$$15 \times 37.5 =$$

$$35 \times 35 =$$

$$100 \times 34$$

177



1
Co Rd I

58-03

Sewer drainage stakes

Sta	PG	PGB	-	Elev.
BM	8.03	900.25		892.22
20+50	97.0	3.25		
21	97.5	2.75		
+50	98.1	2.15		
	94.95	5.30		
TP	4.27	902.42	2.10	898.15
22	98.6	3.82		
	94.7	2.72		
+50	99.0	3.42		
	94.45	7.97		
23	99.0	3.42		
	94.2	8.22		

TA
RR
DF
JH

± August 4, 1959

2

Lt

Rt

Spike in 20" Oak 100' Rt Sta 16+80

Gr
24

Gr
24

C. 3.15 Gr
FL 24

C. 3.90 Gr
FL 24

C 4.55 Gr
FL

C 4.80 Gr
FL

Sta	PG	PGR	-	Elev
		902.42		

23+50	98.7	3.72		
	93.95	8.47		

24	98.1	4.32		
	93.7	8.72		

+50	97.3	5.12		
	93.15	9.27		

25	96.5	5.92		
	92.60	9.82		

+50	95.7	6.72		
	92.05	10.37		

26	95.5	6.92		
	91.7			
	91.40	11.02		

+50	91.0	11.42		
	FL 907	11.72		

± August 4, 1959

3

LT

RT

C 4.75 Gr
FL 24

C 4.40 Gr
FL 24

C 4.15 Gr
FL 24

C 3.90 Gr
FL

C 3.65 Gr
FL

C 4.10 Gr
C 4.05

11.32
C 4.0 FL
11.32

Dist from $\frac{1}{4}$ Cr. to Align
on South Shore and
Back to the P.I.

From Alignment to MC^{#5}

FK
LC
KP
KJ
JH

November 12, 1959
Overcast 16°

1

Borrow Pit "A"

Final Re X-sections

(40)

Sta + N - Elev.

BM 11.59 903.81 892.22

200

1

✓

+50

✓

2

191

Nov 12, 1959

2

Lt

E

Rt

Spike in 20" Oak 100' Rt Sta 16180

98.1	98.2	98.3	98.4	98.5	98.6
5.7	5.6	5.5	5.4	5.4	5.6
131	100	79	52	26	

96.8	96.7	95.8
6.0	7.1	8.0
158	185	200

98.3	98.7	98.8	98.7	98.7	98.7	99.3	99.7
5.5	5.1	5.0	5.1	5.1	5.1	4.5	4.1
150	124	100	86	62	35		7

97.5	96.3	95.6	95.0
6.3	7.5	8.2	8.8
174	200	224	240

98.5	98.6	98.5	98.3	98.1	99.1	01.5
5.3	5.2	5.3	5.5	5.7	4.7	2.3
100	87	61	33	9		14

98.1	97.8	97.5	96.5	96.0
5.7	6.0	6.3	7.3	7.8
123	149	173	200	218

95.4
8.4
237

182

Sta + π - Elev

903.81.

2+50

✓

✓

3

✓

+ 50.

November 12, 1959

2

17

E

97.5	97.6	97.8	97.9	97.5'	98.0	01.5'
6.3	6.2	6.0	5.9	6.3	5.8	2.3
100	81	56	33	13		14

97.1	96.1	95.9	95.8	95.8
6.7	7.4	7.9	8.0	8.0
125	145	167	189	200

94.8	95.0	95.7
9.0	8.8	8.1
250	243	220

95.8	96.1	96.7	97.4	97.1	97.4	98.1	01.3
8.0	7.6	7.1	6.4	6.7	6.4	5.7	2.5
122	100	75	52	29	7		12

95.2	94.7	94.8	94.8	98.3
8.6	9.1	9.0	9.0	5.5
143	166	184	200	

95.2	95.7	96.3	96.8	96.6	96.9	97.8	01.3
8.6	8.1	7.5	7.0	7.2	6.9	6.0	2.5
118	100	78	56	35	9		14

94.5	94.2
------	------

9.3	9.6
137	150

183

Sta + * - Elev

903.81

4

✓

+50

19400

8.6

95.2

✓

+65

End Cut

Nov. 12, 1959
£

3

Lt.

94.5 95.0 95.7 95.7 96.7 97.6 01.3

9.3 8.8 8.1 8.1 7.1 6.2 2.5
96 72 49 31 11 18

94.1 93.3

9.7 10.5
107 122

93.8 94.5 95.3 95.5 97.4 01.3
10.0 9.3 8.5 8.3 6.4 2.5
50 33 22 12 31

184

