

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

Mc KNIGHT ROAD

From LOWER AFTON To U.S. #12

Road Acc't. No. _____

Date Filed 2-16-61

Dr. 9
File BK 31

SELECT GRANULAR MATERIAL
PROSPECT

RAMSEY COUNTY - AREA JOB 91-910

STA 41+00 - 47+00 LT & RT

3-2-60

E. GIBBEN
D. ALLEN
R. MAHER

SELECT GRAN MAT'L

41+00 125' LT Φ
0.0-3.0 SL BR
S-1 { 3.0-15.0 LS BR

42+00 125' LT Φ
0.0-1.0 SL DK BR
No 1.0-3.7 SL-CL BR
SAMPLE 2.7-15.0 LS BR

43+00 125' LT Φ
0.0-2.0 SL-CL BR
S-1 { 2.0-15.0 LS BR

44+00 125' LT Φ
No 0.0-2.2 SL DK BR
SAMPLE 2.2-15.0 LS BR

45+00 125' LT Φ
0.0-1.3 SL DK BR
1.3-3.0 SL-CL BR
S-1 { 3.0-15.0 LS BR

46+00 125' LT Φ
No 0.0-2.0 SL DK BR
SAMPLE 2.0-15.0 LS BR

SELECT GRAIN MAT'L

47+00 125' LT Φ

0.0-2.2 SL

DK BR

S-1 { 2.2-9.0 LS

BR

9.0-10.0 SL

GR

45+00 100' RT Φ

0.0-1.2 SL

DK BR

1.2-2.0 SL

BR

S-1 { 2.0-15.0 LS

BR

45+00 100' RT Φ

NO

0.0-1.7 SL

DK BR

SAMPLE 1.7-15.0 LS

BR

44+00 100' RT Φ

0.0-2.0 SL

DK BR

S-1 { 2.0-15.0 LS

BR

43+00 100' RT Φ

NO

0.0-1.0 SL

DK BR

SAMPLE 1.0-2.3 SL

BR

2.3-15.0 LS

BR

AREA 56B 51-510
RAMSEY CO.

SELECT GRAN. MAT'L

42+00 - 100' RT E

NO	0-17 SL	DK BR
SAMPLE	17-42 LS	BR
	42-70 SL	BR
	70-100 CL	BR

SELECT GRANULAR MATERIAL

PROSPECT

RAMSEY COUNTY - AREA 56-91-910

STA. 56+00 - 63+00 125' LT. E

3-2-60

E. CRIPPEN
D. ALLEN
R. MAHER

SELECT GRAN MAT'L

56+00 125' LT S
0.0-2.8 SL DR BR
S-1 { 2.8-10.0 LS BR

57+00 125' LT S
No. 0.0-9.0 SL-CL DR BR-DR
SAMPLE 9.0-15.0 LS BR

58+00 125' LT S
0.0-1.0 SL-CL DR BR
1.0-2.0 SL-CL BR
S-1 { 2.0-15.0 LS BR

59+00 125' LT S
No. 0.0-2.2 SL-CL DR BR
SAMPLE 2.2-15.0 LS BR

60+00 125' LT S
0.0-1.0 SL-CL DR BR
1.0-3.0 SL-CL BR
S-1 { 3.0-15.0 LS BR

SELECT SPAN MAT'L

4400 125' LT E
No 0.0-27 SL-CL BR
SAMPLE 29-15.0 LS BR

62400 125' LT E
No 0.0-1.5 SL DK BR
1.5-4.0 SL-CL BR
4.0-6.0 LS BR
S-1 6.0-8.0 LS-SL BR
8.0-15.0 LS BR

63400 125' LT E
No 0.0-1.5 SL-CL DK BR
SAMPLE 1.5-8.0 SL-CL BR
8.0-5.0 CL BR

L. S. Morrison, County Engineer

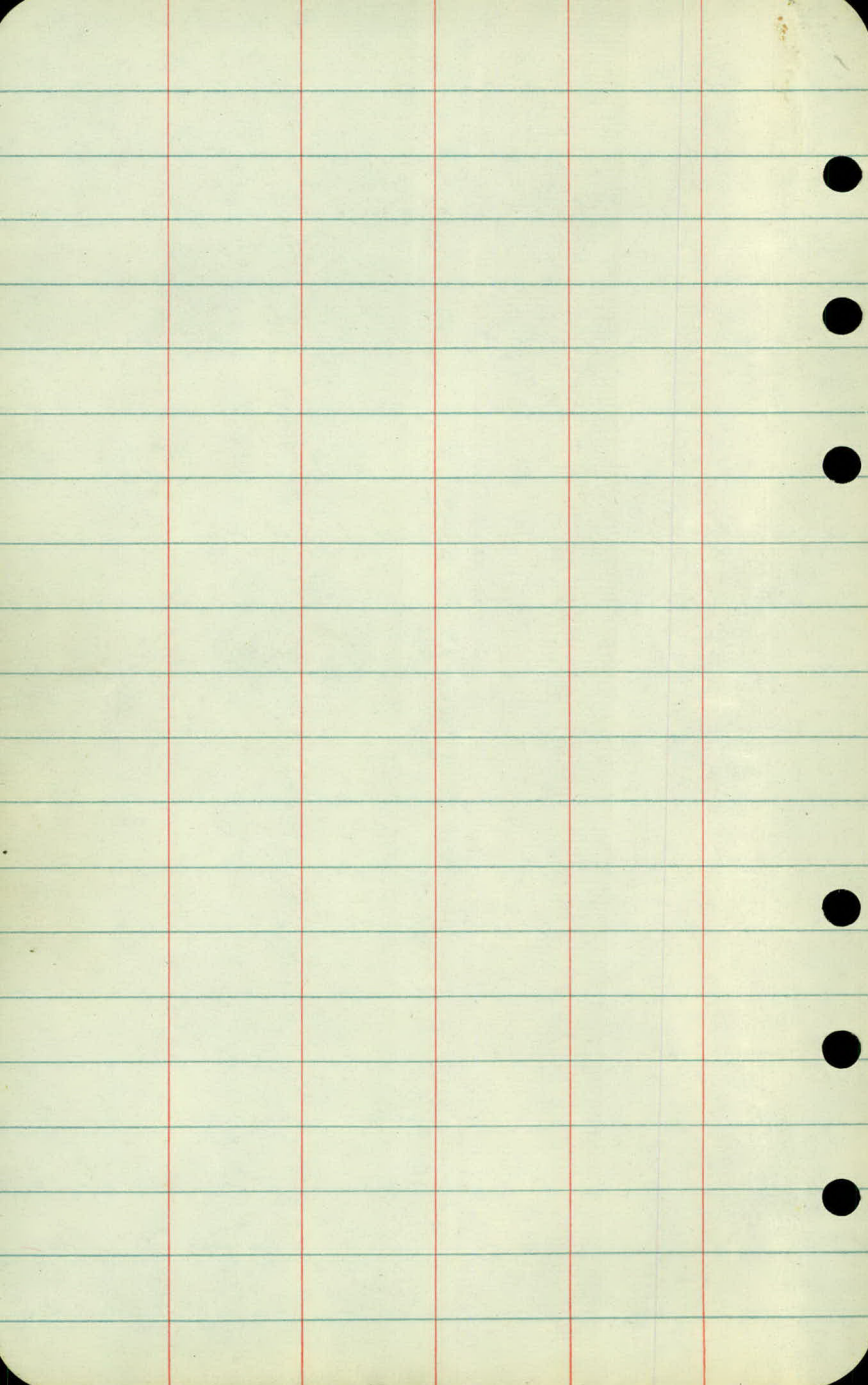
Count House

St Paul 2, Minn

1
Mc Knight Road

Plan Survey

Lower Aston to U.S. #12



FR
RG
KP
KJ
JH

Nov. 23, 1959
Overcast 28°

2

Alinement

Sta Point ΔL ΔR

52+54.32 P.O.T. Mont. 0.30' West

39+42.05 P.I. $0^{\circ}03\frac{1}{2}'$

31+00 Page 5
26+26.83 P.O.T. Ties Page 5
21+00 P.O.T.

16+83.96 Iron 0.10' West

13+11.60 P.I.

0+00 $\pm$ Lower Afton Rd

FR
RG
KP
JH.

November 24, 1959 3
Overcast 24°
Windy Rt

Lt

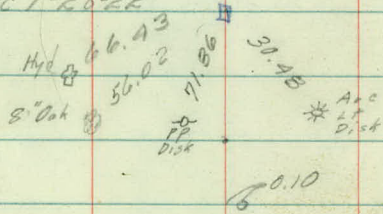
West 0.30



Mont

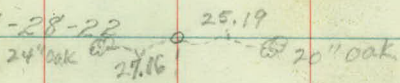
W 1/4 Cor Sec 1-28-22

RR Spike
Mont. in ditch

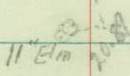


Spike
Iron

S.W. Cor Sec 1-28-22

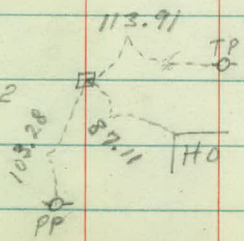


Iron



W 1/4 Cor of
NW 1/4 Sec 12-28-22

Mont



Sta Point ΔL ΔR

13+27.29 P.O.T. $\neq$ W.B.L. U.S. #12

72+70.96 P.O.T. $\neq$ E.B.L. U.S. #12

67+07.29 P.I.

$0^{\circ}22\frac{1}{4}'$

FK
RG.
KJ
JH.

November 25, 1959
Cloudy 10°

A

Canway

Brass Plug

Gas Control
Box Post

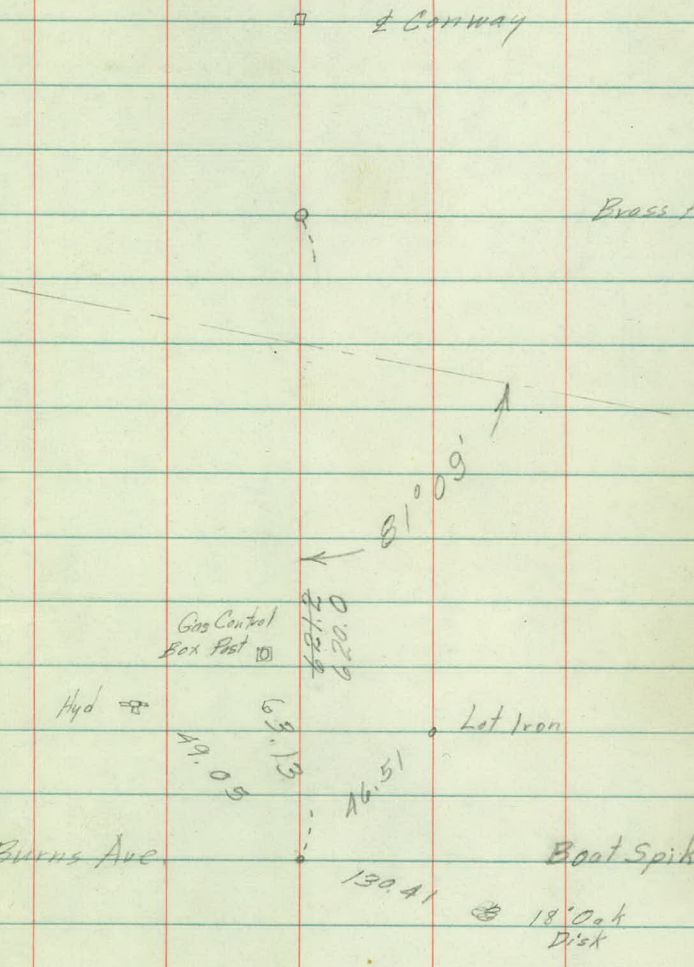
Hyd

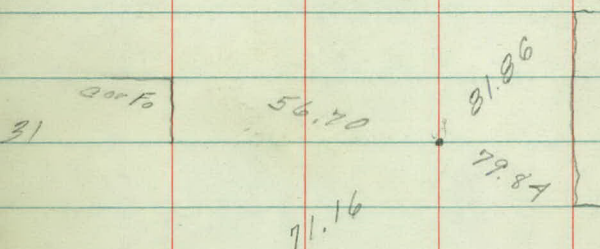
Let Iron

Burns Ave

Boat Spike

18' Oak
Disk





Hyd

(23)

Brick
House

(31)

July 23 1964

FK

TL

GB/ank

75.50

62.61

55.13

26+26.83 P&T 1/4 1/4 Cor

Garage

Apron

64.94

(25)

McKnight Rd.

TOPOGRAPHY

Lower Afton Rd. to Highway #12

12-15-59

L.S.

5 Woods 0.0

FC
E

+80-ΔFC
62
+70 Brush
20-62
+50 Brush
20-62
+03-24" Elm
63
+03-8" Elm
65

4 +50-8" oak Woods 8
36
+50-18" oak
19
+18 SE Cor Shed
9
+75 Bag Woods
10 Lt
+44-12" oak
24
+11-18" oak
15
+34-6" oak
29
+03-30" oak
28
+61-12" oak
E
+00-18 Elm ditch
35
41
+66-18" oak
24

3 +82-24" oak
17
+35- Bag Brush 0-60
+30-2-8" Elm
25
+35-36" Elm
19
+14 SE Cor Shed
35
+29-12" oak
21
+29-24" B.E.
36

2 +95 SE Cor Shed
36
+87-24" B.E.
12
+34-6" apple
8
+24-6" B.E.
43
+30-8" Elm
15
+52-8" Elm
0
+57 SE Cor Shed
36
+57-6" Elm
7
+57-4" Elm
3

+37-5 SE Cor Shed
11
+10-8" * Tree * 8"
53
+21 SE Cor Ho.
35
+12" Elm
70
+75-6" Elm
25
+25-12" Elm
65
+50-4" Elm
50
+40-4" Elm
21
+28-12" Elm
35
+28-6" Elm
29
+36-2
2
+14 E.B.T.
E
+57 Bag Brush
2

0 +67-18" O
28
+64-2" *
56
+62-2" *
42
+60-2" *
60
+14 E.B.T.
E
+57 Bag Brush
2

FC.
0.0

FC.
0.0

FC
2

+11-Δ FC.
2

+150 ditch
58

3-wire

+90 F. Brush
10'

+68-2-6"E/m/s

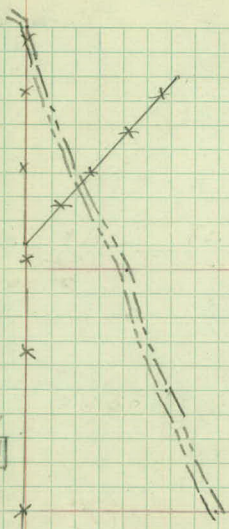
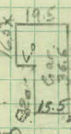
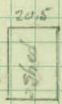
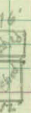
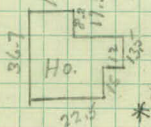
+45-8"E/m/s +45-6"E/m/s

+78-6"E/m/s

+27 End Row pop tree
2' 11 trees

+20-End of * Trees
2' (10)

+93 beg Row 4" * Trees
2'



10

$$\begin{array}{r} FC \\ 3' \end{array}$$

$$\begin{array}{r} \checkmark \text{Brush } 10' \\ \underline{60'} \end{array}$$

$$\begin{array}{r} \checkmark \\ + 50 \text{ bag. small pine trees} \\ 1' \text{ to } 4' \text{ high } \underline{60-75'} \end{array}$$

9

woods

$$\begin{array}{r} FC \\ 3' \end{array}$$

$$\begin{array}{r} \checkmark \\ + 90 \text{ bag Brush} \\ \underline{45} \end{array}$$

8

woods

$$\begin{array}{r} FC \\ 4' \end{array}$$

$$\begin{array}{r} \checkmark \\ + 20 - 8" \text{ Apple tree} \\ \underline{10'} \end{array}$$

7

$$\begin{array}{r} FC \\ 3' \end{array}$$

$$\begin{array}{r} \checkmark \text{End of Brush} \\ \underline{30'} \end{array}$$

$$\begin{array}{r} \checkmark \\ + 87 - 24" \text{ B.E.} \\ \underline{58} \end{array}$$

$$\begin{array}{r} \checkmark \\ + 32 - 10" \text{ Elm} + 62 - 6" \text{ Elm} \\ \underline{42} \quad \underline{38} \end{array}$$

$$\begin{array}{r} \checkmark \\ + 23 - 6" \text{ Elm} \\ \underline{50} \end{array}$$

6

$$\begin{array}{r} \checkmark \\ + 92 - 8" \text{ Birch} \\ \underline{22'} \end{array}$$

$$\begin{array}{r} \checkmark \\ + 79 \Delta \text{ in } FC. \\ \underline{4} \end{array}$$

$$\begin{array}{r} \checkmark \\ + 50 \text{ woods} \end{array}$$

$$\begin{array}{r} \checkmark \\ + 25 \text{ ditch.} \\ \underline{50'} \end{array}$$

$$\begin{array}{r} \checkmark \\ + 50 \text{ Brush} - \\ \underline{60'} \end{array}$$

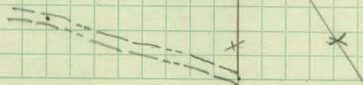
5

$$\begin{array}{r} \checkmark \\ + 80' \\ + 00 \text{ ditch } \times \text{ E} \end{array}$$

9 Trees
* *

(11 + 40 = End of *)
See Next page

11



15

$$+ 63 - \frac{10'' \text{ Pop.}}{44}$$

$$+ 29 - \frac{6'' \text{ Pop.}}{50}$$

$$+ 21 - \frac{2-6'' \text{ willows}}{50}$$

14

$$+ 42 - \frac{2-8'' \text{ Pops.}}{36}$$

$$+ 59 - \frac{10'' \text{ Pop.}}{11} + 74 - \frac{6'' \text{ Elm}}{39}$$

$$+ 50 - \frac{8'' \text{ P.K.}}{6} + 54 - \frac{12'' \text{ Pop.}}{10}$$

$$+ 20 \text{ End of woods} + 50 - \frac{12'' \text{ Pop.}}{12}$$

$$+ 13 \times \text{Fc (Ends)}$$

$$\frac{3 \text{ wire}}$$

13

$$+ 50 \text{ Creek} \Delta = \text{East}$$

12

woods

Fc
3

wood

$$+ 90 \text{ Creek Xs } \&$$

$$+ 40 - \text{End of Pine Tree}$$

$$65-75$$

$$+ 10 \text{ woods}$$

11

woods

Fc.
3

$$21 \text{ pine Trees}$$

$$62-77$$

$$+ 81 - \frac{10'' \text{ Elm}}{16}$$

$$+ 74 - \frac{12'' \text{ Elm}}{21}$$

$$+ 35 - \frac{15'' \text{ Elm}}{20}$$

10

woods

Cult.
12'

Cult.
75'

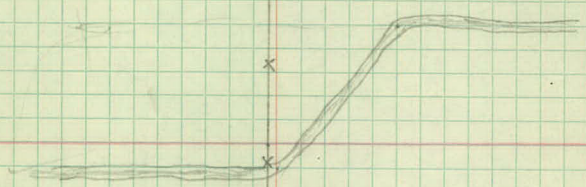
Cult.
20'

Cult.
56'

+ 30-Cult.
30'

Cult.
76'

X X X X X X X



woods

14 Trees

33 Trees

* *

20

19

18

17

16

✓
+55 End Trees
✓
+50 Trees
82'
28-81
+10- beg Trees
56'
14 Trees

15

cult.

cult.

cult.

cult.

cult.

cult.



25

$$\begin{array}{r}
 + \checkmark 39 - 18'' \text{oak} \\
 \quad \quad \quad \underline{72} \\
 + \checkmark 33 - 18'' \text{oak} \\
 \quad \quad \quad \underline{72} \\
 + \checkmark 23 - 18'' \text{oak} \\
 \quad \quad \quad \underline{23}
 \end{array}$$

24

$$\begin{array}{r}
 + \checkmark 99 \text{ Fc Cor } 3 \text{ wire} \\
 \quad \quad \quad \underline{41}
 \end{array}$$

$$\begin{array}{r}
 + \checkmark 44 \text{ Fc Cor } 3 \text{ wire} \\
 \quad \quad \quad \underline{4} \\
 + 40 \text{ End Cult.}
 \end{array}$$

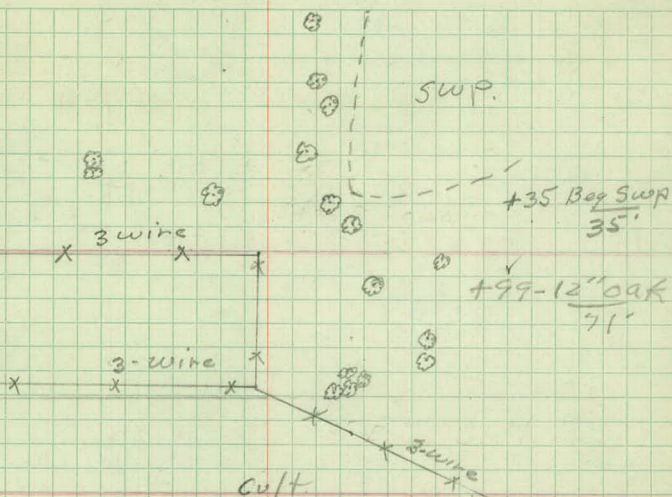
23

$$\begin{array}{r}
 + \checkmark 71 - 8'' \text{oak} + \checkmark 97 - 15'' \text{oak} \\
 \quad \quad \quad \underline{20} \quad \quad \quad \underline{19} \\
 + \checkmark 42 - 12'' \text{oak} + \checkmark 61 - 12'' \text{oak} \\
 \quad \quad \quad \underline{17} \quad \quad \quad \underline{24} \\
 + \checkmark 12 - 12'' \text{oak} + \checkmark 20 - 12'' \text{oak} \\
 \quad \quad \quad \underline{35} \quad \quad \quad \underline{24} \\
 + \checkmark 65 - 12'' \text{oak} + \checkmark 87 - 15'' \text{oak} \\
 \quad \quad \quad \underline{67} \quad \quad \quad \underline{43} \\
 + \checkmark 47 - 12'' \text{oak} + \checkmark 65 - 12'' \text{oak} \\
 \quad \quad \quad \underline{32} \quad \quad \quad \underline{67} \\
 + \checkmark 42 - 12'' \text{oak} + \checkmark 44 - 12'' \text{oak} \\
 \quad \quad \quad \underline{29} \quad \quad \quad \underline{46} \\
 + \checkmark 25 \text{ Fc } 3 \text{ wire} \quad \quad \quad \underline{34} \\
 \quad \quad \quad \underline{34} \\
 + 20 \text{ End Cult.} \quad \quad \quad \underline{\text{Fc}} \\
 \quad \quad \quad \underline{90}
 \end{array}$$

22

21

20



30

✓
+ 90 - Sw. cor. corn crib
73

29

✓
+ 42 - Sw. cor. corn crib
73
✓
+ 54 - PP.
108
✓
+ 42 - 6' B. P.C.
42
✓
+ 18 X F.C. 6' Board + 18 - Sw. cor. shed
29

28

✓
+ 24 - Sw. cor. corn crib
24
✓
+ 24 - Sw. cor. corn crib
24

+55 Hyd
51
+55 W.S.O.
29

27

✓
+ 70 - Sw. cor. corn crib
30
✓
+ 50 Sw. cor. corn crib
29

26

✓
+ 80 - 15" oak
81
✓
+ 57 - 24" oak
50
✓
+ 41 - 15" oak
9
✓
+ 10 - 24" oak
51
✓
+ 62 - Sw. cor. corn crib
5

25

✓
+ 70 - Sw. cor. corn crib
30
✓
+ 50 Sw. cor. corn crib
29
✓
+ 24 - Sw. cor. corn crib
24

110.0

6.5' 16.5' crib

5.1' 12.5'

10.0'

3

Board Fc. 6' Hi.

5.1' 12.5'

Board Fc. 6' Hi.

4

swp.

35

Cult. 8' 8' Cult. - 10'

$$+85 \frac{PP}{67}$$

34

12 8' 8'

$$+35 \frac{MH}{38}$$

33

Cult. 8' 8' Cult. 10'

+33 by Cult. - 15'

+13 - 4" Pine
39'

32 -

Rd. - 18

$$+99 \times 6" \text{ Pine } + 24 \times \frac{5}{74} \text{ SW Cult.}$$

+36 126.6

$$+48 - 4" \text{ Pine } + 83 \frac{SW \text{ Cor. G. Ho}}{82.6}$$

$$+36 - 74" \text{ Oak } + 37 - 12" \text{ BE}$$

$$+23 - 24" \text{ BE } + 29 - 24" \text{ BE}$$

31 -

$$+78 - \frac{PP}{76} + 85 - \frac{SW \text{ Cor. Gar.}}{78}$$

$$+71 - \frac{N.W. \text{ Cor. Shed}}{77} + 69 \text{ Gas pump}$$

$$+35 - \frac{\text{Round cor. crib } 20' \text{ dia}}{79} + 42 - \frac{PP}{75}$$
+90 $\frac{SW \text{ Cor. Ho}}{54}$ +54 $\frac{Hyd}{54}$ +51 $\frac{\text{Gutter}}{49}$ +60 $\frac{S.E. \text{ Walk}}{48}$

30

+20 $\frac{\text{Gutter}}{39}$ +02 $\frac{SW \text{ Cor. Corn crib}}{74}$

o

cult.

cult.

o

cult.

cult.

Green House

186

90.2

office

310P

1-S-F

40

20.3

24.2

Gar.

41.3

Gas
Pump

72.5

Metal
Shed

36.5

20'

Round
Crib

6.5 Crib

16.6

41 24.4

5' Walk

40 +80-stp
 .33 +43-M.H.
 +55 Edge BT 5.5 +80-Beg cult. R+Lt

+33E Rad. +33 Edge BT. +33 E Rad
 50 +08 Hyd 30
 +08 MH 38 +14 P.P.
 41 3 WSD 72
 108 38 +05-End cult.

39 +102 S.E. Walk 14' 2'
 50 +92 MH 38 +95-beg. Rad.

+50-Cult 50
 +47 SE Cor H. 58 +44-Trees End.
 28

38 cult. 13' 3" cult. Trees
 100 6-43

+36-Trees 10'

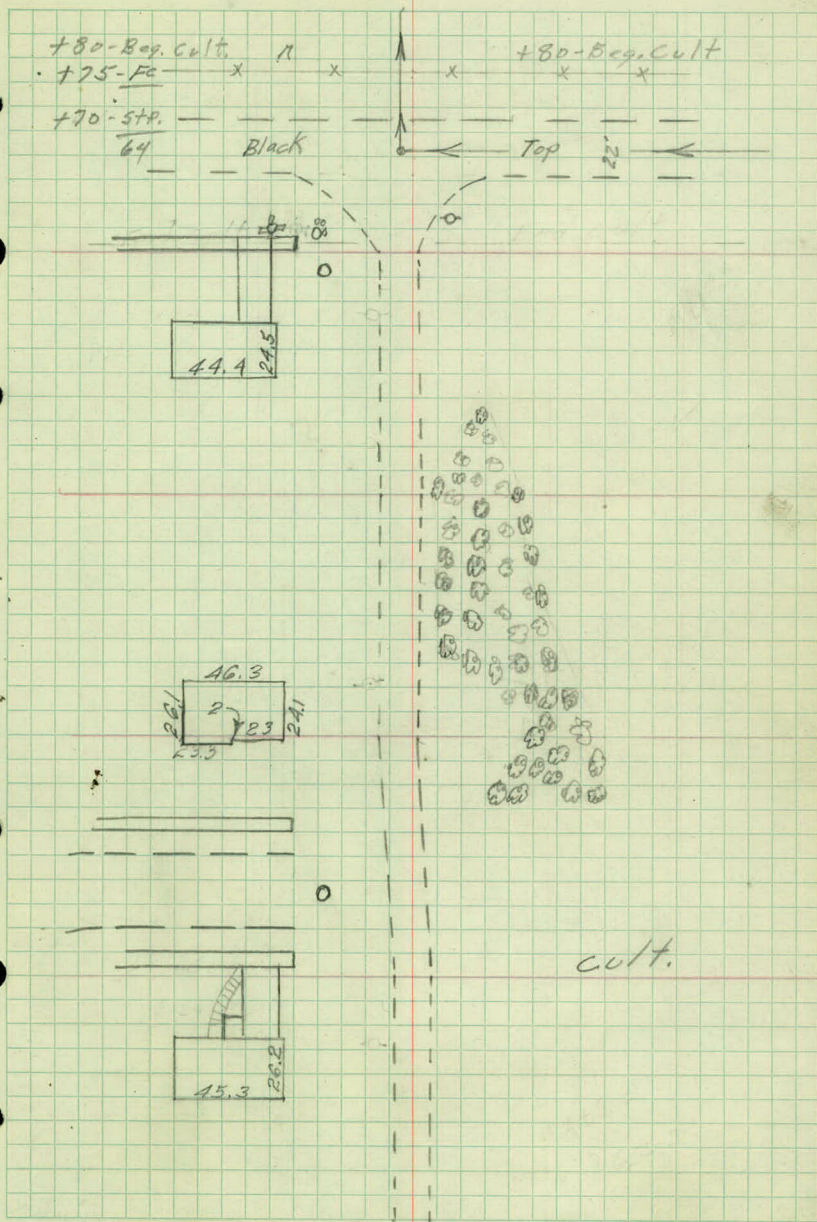
37 14' 2' Trees
 +97 SE Cor H. 55 50-80

+136 MH 38
 +61 SE Walk 50.5
 +20 Gutter 50 +51 Gutter 50 +77-Beg Trees 34-79

36 +05 5' Walk 50 8' 8' cult. -10'

+49 SE Cor H. 54

35



45

Cult.

44

43

+ 48 - $\frac{MH}{6}$

42

41

40

Cult.

cult.

cult.



cult.

cult.

50

cult.

cult.

$$+21 \frac{\text{Fe Cor}}{76}$$

49

$$+55 \text{ - ditch } \frac{62}{62}$$

+35 ditch x 4

48

$$+08 \frac{\text{Fe Angle}}{87}$$

ditch 3' Bottom
 $\frac{33}{33}$

$$+90 \frac{\text{Fe Cor}}{100}$$

$$+82 \text{ - M.H. } \frac{6}{6}$$

+50 - ditch 3' Bottom
 $\frac{74}{74}$

47

ditch 3' Bottom
 $\frac{110}{110}$

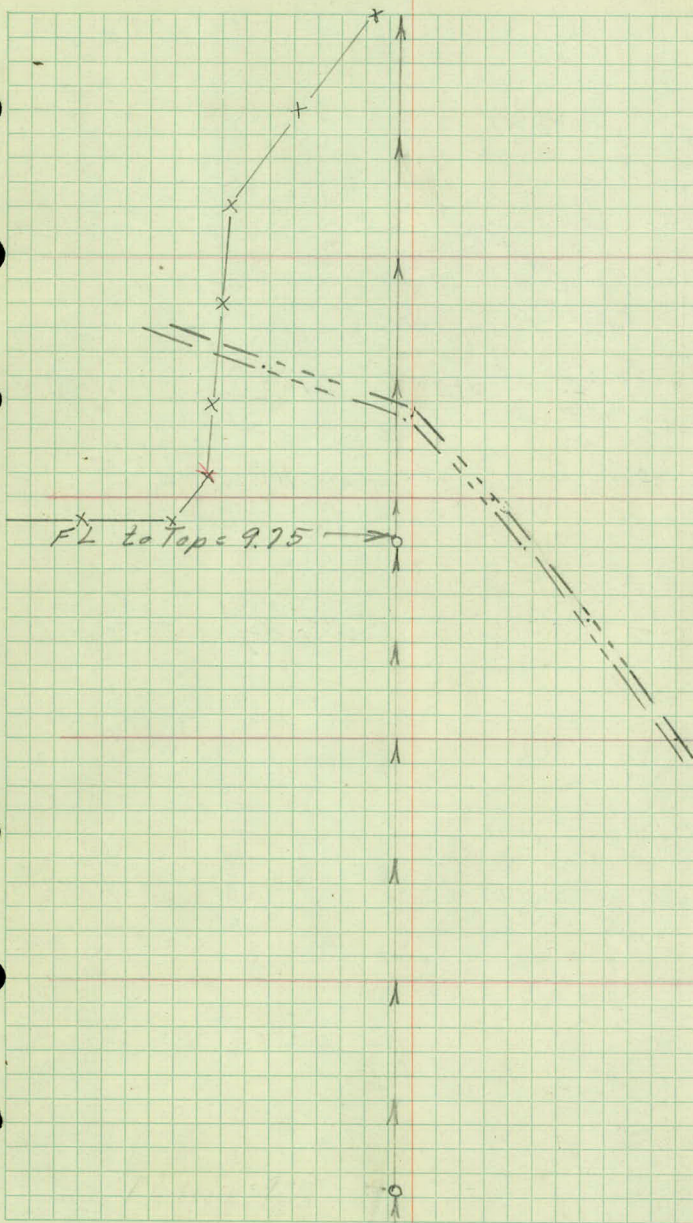
46

$$+14 \text{ - M.H. } \frac{6}{6}$$

45

cult.

cult.



55

Pasture

54

$\downarrow$ + 40 - Creek $\frac{42}{\downarrow}$
 $\downarrow$ + 26 - Twin Linden $\frac{36}{\downarrow}$
 $\downarrow$ + 18 - 12" oak $\frac{21}{\downarrow}$ + 24 - 12" oak $\frac{57}{\downarrow}$
 $\downarrow$ + 08 - 15" oak $\frac{56}{\downarrow}$
 $\downarrow$ + 71 - Creek X 5 $\frac{4}{\downarrow}$
 $\downarrow$ + 70 - Creek $\frac{50}{\downarrow}$
 $\downarrow$ + 22 - 12" oak $\frac{24}{\downarrow}$ + 27 - 12" Birch $\frac{28}{\downarrow}$
 $\downarrow$ + 11 - 8" oak $\frac{24}{\downarrow}$ + 18 - 6" Birch $\frac{39}{\downarrow}$
 $\downarrow$ + 05 - 12" Linden $\frac{62}{\downarrow}$

53

$\downarrow$ + 99 - 12" oak $\frac{41}{\downarrow}$
 $\downarrow$ + 94 - 12" oak $\frac{22}{\downarrow}$ + 97 - 18" oak $\frac{21}{\downarrow}$
 $\downarrow$ + 86 - 15" oak $\frac{76}{\downarrow}$ + 92 - 18" oak $\frac{44}{\downarrow}$
 $\downarrow$ + 82 - 15" oak $\frac{68}{\downarrow}$
 $\downarrow$ + 95 - 6" Birch $\frac{72}{\downarrow}$
 $\downarrow$ + 84 - 12" oak $\frac{57}{\downarrow}$ + 93 - 18" oak $\frac{40}{\downarrow}$
 $\downarrow$ + 20 End cult. beg. pasture

52

$\downarrow$ + 67 - M.H. $\frac{6}{\downarrow}$

51

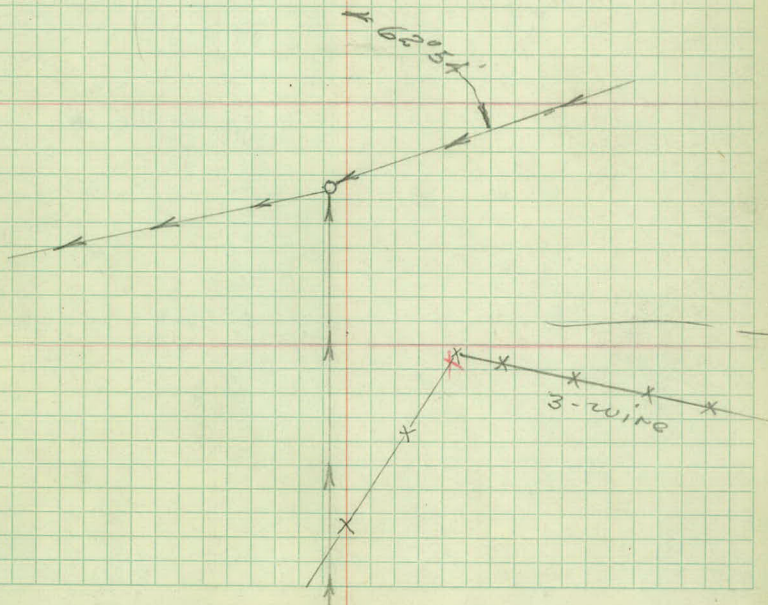
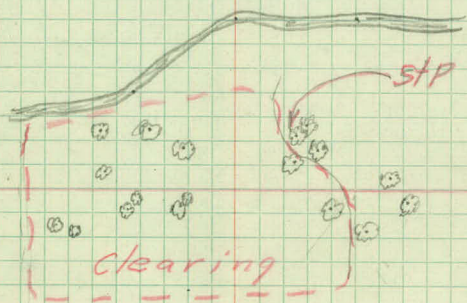
$\downarrow$ + 05 - R. Tie to FC.

$\downarrow$ + 97 - beg. FC. $\frac{48}{\downarrow}$ - 3 wire

$\downarrow$ + 24 $\frac{Fe}{\downarrow}$

50

pasture



60

$$\begin{array}{r}
 \text{Cult.} \quad \checkmark \quad \text{FC.} \\
 +99 \frac{10''w}{18} \quad 20 \quad \frac{13}{19} \quad \checkmark \\
 +77 \frac{2-15''w}{14-17} \quad +89 \frac{12''w}{9} \\
 +73 \frac{18''w}{19} \quad +64 \frac{15''w}{15} \\
 +54 \text{ FC. Ger} \quad \frac{16}{16} \quad +54 \text{ FC. XS} \\
 \end{array}$$

+50 End Cult. Rt

59

Cult

58

cult.

57

Cult.

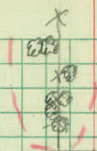
56 +90 bag. Cult. +81 Rd. XS & 10' wide

End pasture +70 FC. X 4

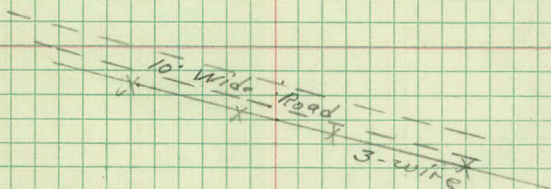
$$\begin{array}{r}
 +85 \text{ FC.} \\
 \hline
 58
 \end{array}$$

$$\begin{array}{r}
 +60 \text{ FC. 3 wire} \\
 \hline
 79
 \end{array}$$

55



3 wire
No Fence 2/14/62 R76



65

Low Land
120

Low Land
100

+50 End of Brush
LT + RT

beg. Low Land

64

+65 Cor Brush
8

End Trees
25'

+60 FC Cor
8

+55 End Cult
20

+50 Trees + Brush
10

63

Cult Brush
15' 8

Brush Trees
66'

+50 Trees
66

62

Cult
15' FC
5 9

Brush - Trees
98

+50 Brush
5

61

Cult. FC
15 10

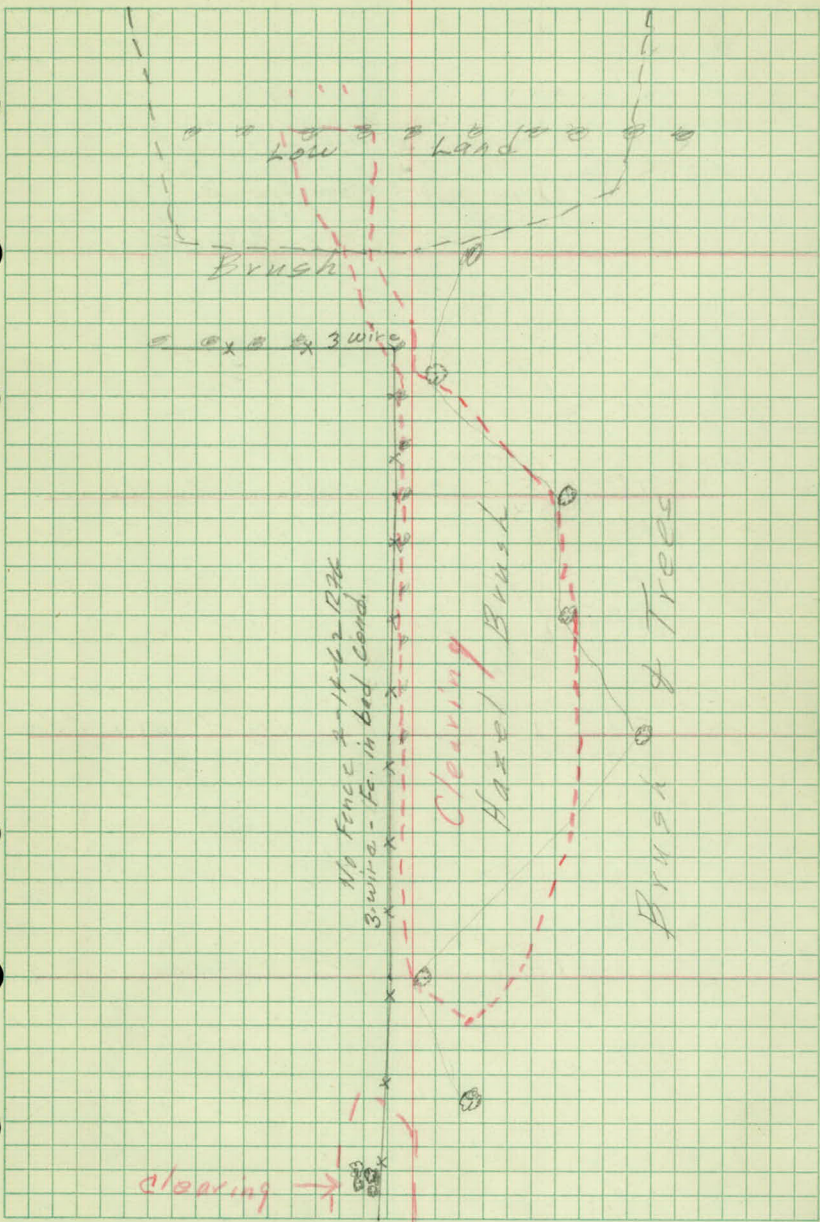
woods + brush
5'

+15 - 4 - 15" W.
14

+50 woods + brush
25'

60

FC
13'



70

+ 98 - spillway B.T.
10 - 50 7' wide+ 44 - 24' 0"
45+ 14 - 12' 0"
70'+ 38 - 8' 0"
43+ 44 - 24' 0"
66+ 36 - 18' 0"
37+ 40 - 24' 0"
71'12" B.E.
35Brush
23'+ 49 - 15' 0"
43+ 16 - 15' 0" + 23 - 15' 0"
39 38

68

+ 70 - Cas. shot off
20'+ 67 - M.H.
22+ 41 - N.S.P.M.H.
19'+ 27 Hyd.
44'+ 57 Bag. Brush
24'

+ 23 - B.T. 20

67

+ 91 - Bag. spillway
14+ 75 - E spillway B.T.
14' 3' B.T.

Fc. 79' B.T. 10 - 20'

+ 85 in Fc.
25

+ 61 Fc. X3

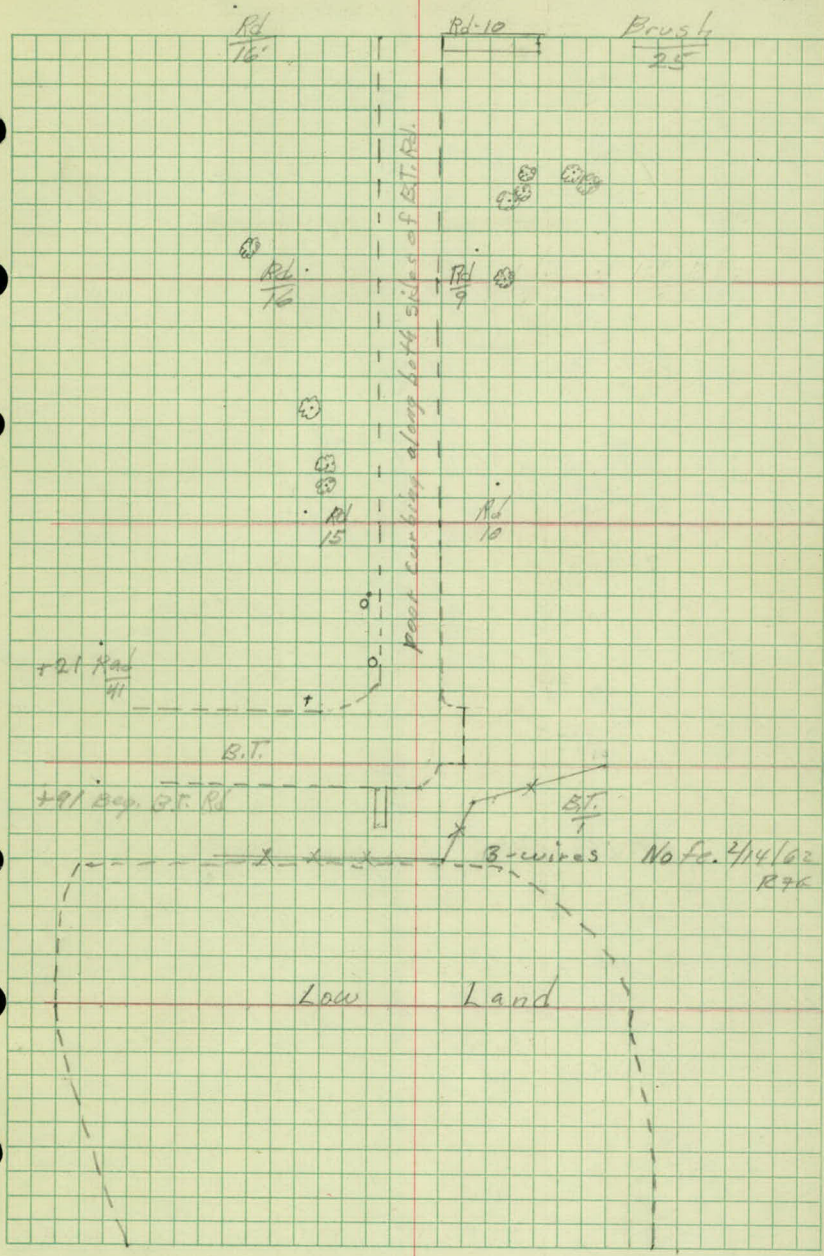
A in Fc.
11'+ 60 Low Land
140+ 60 Low Land
40

66

Low Land
150Low Land
90

65

Low Land
120Low Land
100



127.29 ± W.B.L.
±

73

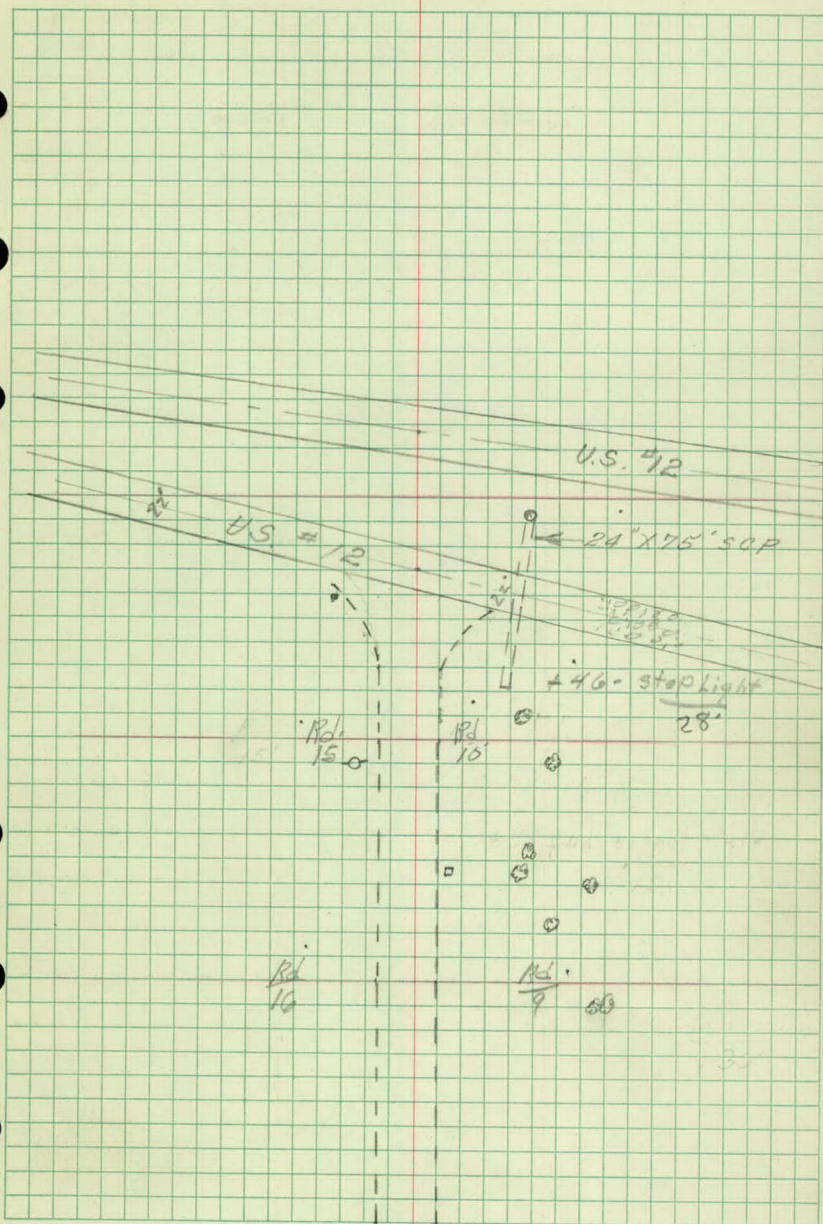
+65 End Rad	+55 End Rad	+92 ⁵⁰ 48.5'
35	31	
+170.96 ± EBL	+30 bag Rad	
±	10	
+60 Gas shut off	+22.5 End 24" Conc Culv.	
32	38	
+30 Bag Rad	+11- 15" E 1st	
16	46	

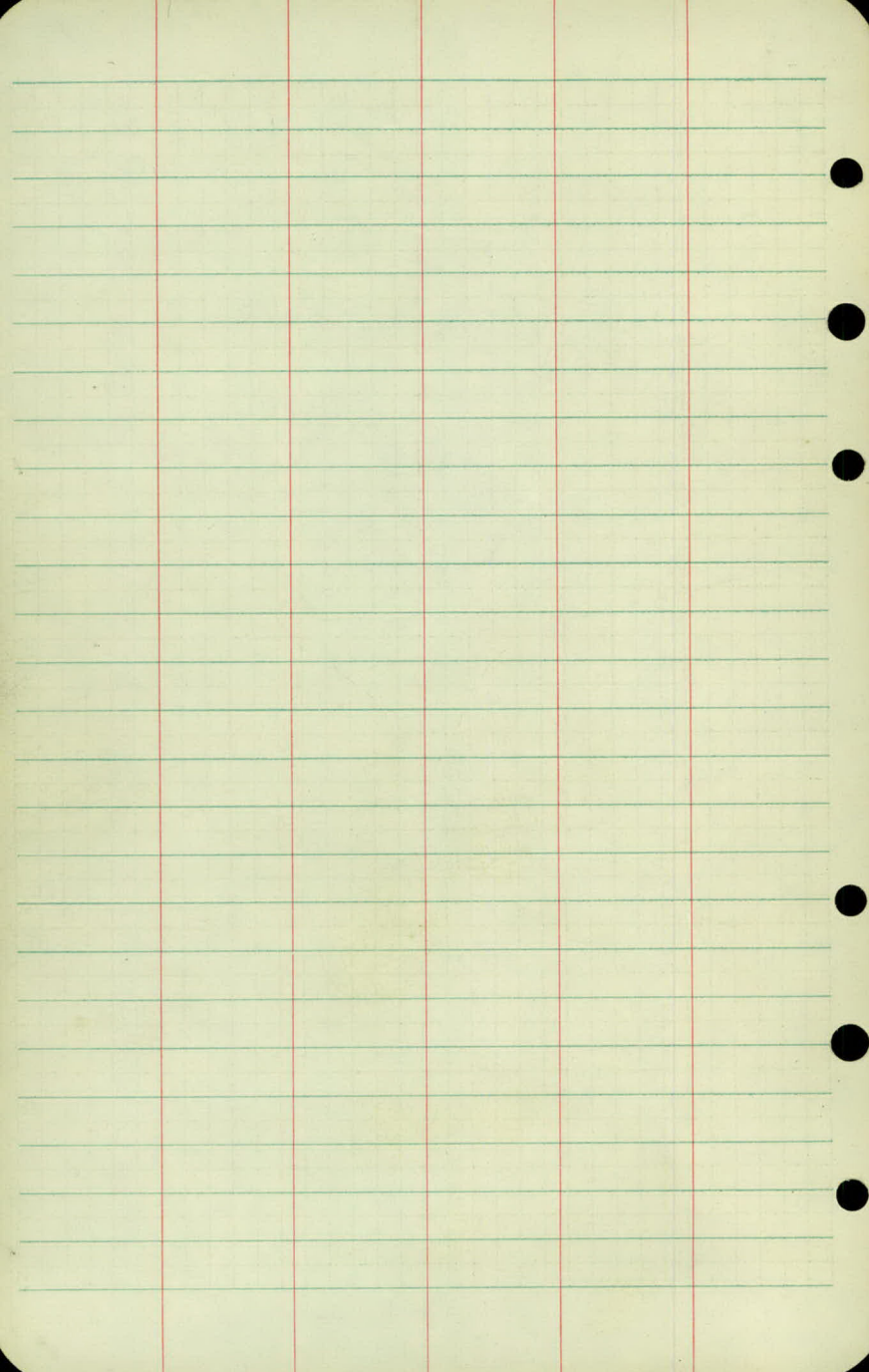
72

+90 p.p.	2'x2' Pull Box
26	12.5' - 14.5'
	+91-30"0
	56
	+45 signal plat
	END
	+47-8"0
	46
	+55-12"0
	49
	+24-12"0
	57
	+40-15" P40
	73
	+93-2-8"0
	71'
	+90 E. Brush
	30

71

70





10 NOVEMBER 1959 21.
CLOUDY + 40°

KP
UH
KJ

MCKNIGHT ROAD
LOWER AFTON RD to STH#12
BENCH LEVELS

STA	+	π	-	ELEV.
-----	---	-------	---	-------

BM	0.12	972.12		972.40 972.00
----	------	--------	--	------------------

	0.89	960.33	12.68	959.44
--	------	--------	-------	--------

	0.07	947.08	13.32	947.01
--	------	--------	-------	--------

	0.90	935.28	12.70	934.38
--	------	--------	-------	--------

	0.10	923.18	12.20	923.08
--	------	--------	-------	--------

	1.02	910.82	13.38	909.80
--	------	--------	-------	--------

			8.28	902.54
--	--	--	------	--------

			6.69	904.13
--	--	--	------	--------

	12.89	923.08	0.63	910.19
--	-------	--------	------	--------

	12.56	935.34	0.30	922.78
--	-------	--------	------	--------

	6.72	941.78	0.28	935.06
--	------	--------	------	--------

			2.31	939.47
--	--	--	------	--------

	8.88	937.84	12.82	928.96
--	------	--------	-------	--------

	13.27	949.59	1.52	936.32
--	-------	--------	------	--------

			1.27	948.32
--	--	--	------	--------

Lt

±

10 NOV. 1959 22.

Rt

TOP N.W. COR. LOWER STEP HO# 366 MCKNIGHT

SPIKE IN 18" OAK ³⁷²~~318~~ S. AND 12' WEST OF
MONT. N.W. COR SEC 12-28-22

(iron)
TOP MONT. N.W. COR SEC 12-T28-R22

SPIKE IN 16" OAK 40' RT. INSIDE PASTURE
FENCE. APPROX. 1100' N. OF MONT. (iron)

SPIKE IN P.P. 300' N. OF FARM HOUSE AND
ABOUT 100' W. OF SECTION LINE.

Sta	+	Δ	-	Elev
B.M.	1.22	949.54		948.32
T.P.	0.54	937.07	13.01	936.53
T.P.	0.12	924.31	12.88	924.19
B.M.	4.04	917.69	10.66	913.65
T.P.	1.65	908.06	11.28	906.41
T.B.M.	5.34	907.83	5.57	902.49
T.P.	9.28	916.54	0.57	907.26
T.P.	13.59	928.32	1.81	914.73
T.P.	6.39	934.26	0.45	927.87
B.M.			4.68	929.58
T.P.	10.16	938.43	5.99	928.27
B.M.	9.24	944.75	2.92	935.51
T.P.	12.77	956.98	0.54	944.21
T.P.	12.96	969.52	0.42	956.56
T.P.	5.02	974.30	0.24	969.28
			5.37	968.93 969.37 (Hiway)

LC
JS

11-24-59

23

Spk. in p.p. 11' W. of sta 34+25

Spk. in 24" Elm 130' E. of 39+75

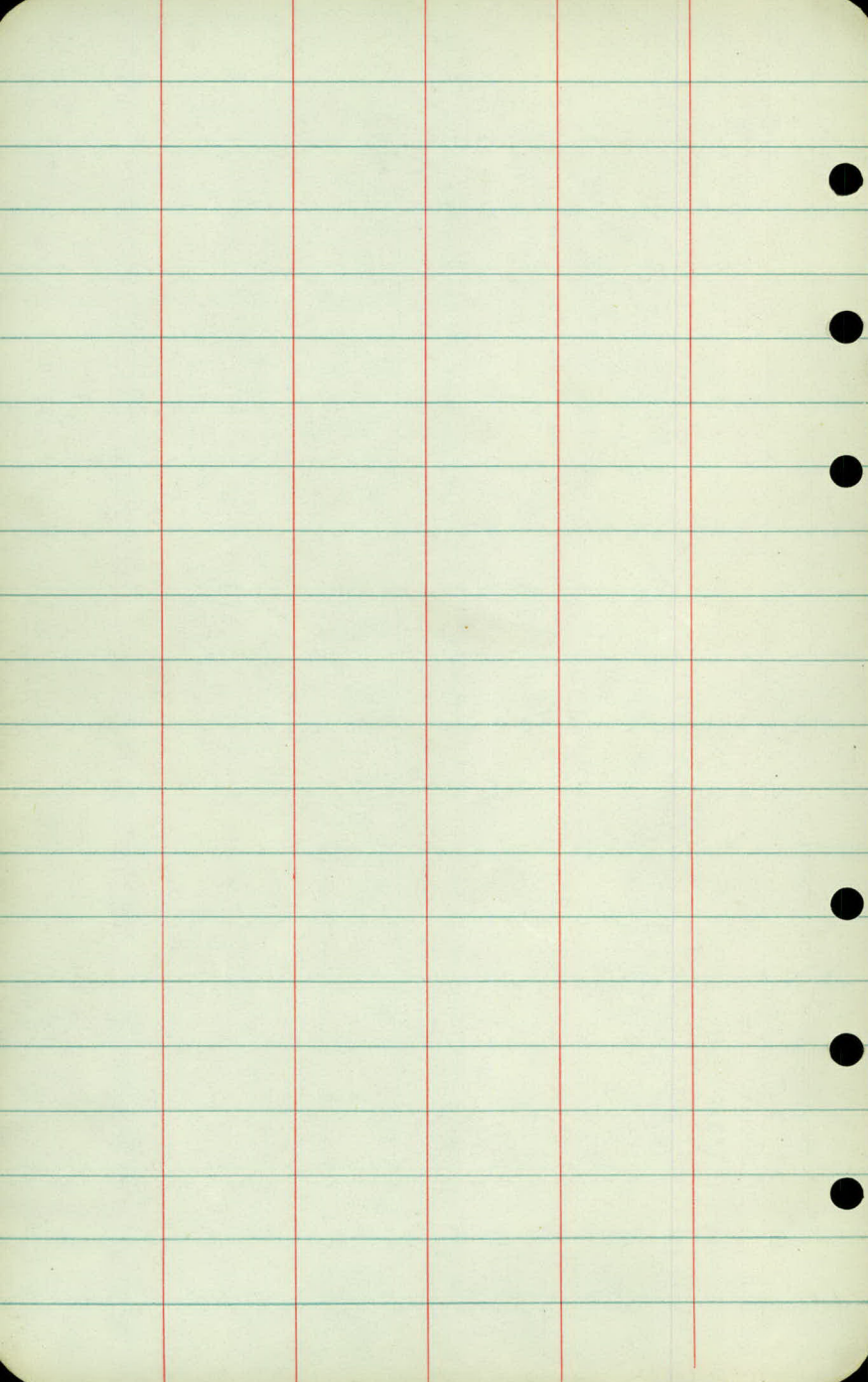
Top Mont. 52+50 ±

Spk. in 18" W. oak. 90' Rt. Sta 62+80

Top Hyd. N. W. Cor. McKnight + Burns

11-25-59

Top Brass plug Hiney #12 + McKnight Rd



X-Sections

Sta	+	π	-	Elev.
BM	0.89	972.89		972.40 <u>972.00</u>
		973.29		

0-145			0.0	73.3
-------	--	--	-----	------

0-100			2.5	70.8
-------	--	--	-----	------

0-50			4.6	68.7
------	--	--	-----	------

0+00				
------	--	--	--	--

+18	Shoulder			
-----	----------	--	--	--

+21	Ditch Line			
-----	------------	--	--	--

FK
RG
JH

± November 27, 1959
P.C. 23°

25

lt

ft

Top N.W. Cor Lower step No #366 McKnight

66.5	66.7	66.9	67.2	67.2	67.0	66.9	67.2	67.1
6.8	6.6	6.4	6.1	6.1	6.3	6.4	6.1	6.2
100	75	50	25		25	50	75	100

66.2	66.2	66.8	66.7	66.9	66.6	66.2	66.3	66.2
7.1	7.1	6.5	6.6	6.4	6.7	7.1	7.0	7.1
100	77	50	26		28	53	72	100

65.1	66.7	66.8	65.9	65.8	66.7	66.4	66.2	66.1
6.6	6.5	6.4	6.5	6.6	6.6	6.9	7.1	7.2
59	42	39	32		15	36	62	76

65.5	65.3
7.8	8.0
80	100

65.3
8.0
100

Sta + π - Elev

973.29
972.89

0+30

✓

+52

✓

T.P. 3.81 966.67 10.43 962.86
962.46

+75

✓

Nov. 22/1959

26

7.7	7.4	6.6	7.0	6.9	7.7	7.9	8.0	8.8	8.5
58	55	31	17		15	39	74	84	100

7.8	7.8
80	100

64.1	64.4	64.6	65.3	65.8	64.8	64.5	63.9	63.7	63.1
9.2	8.9	8.7	8.0	7.5	8.5	8.8	9.4	9.6	10.2
75	50	36	30	15		4	6	27	49

64.2	9.1
	100

62.9	62.7	62.7	63.4
10.4	10.6	10.6	9.9
100	97	84	68

63.7	63.8	63.8	63.8	64.3	63.7	63.3	62.6	62.4
3.0	2.9	2.9	2.9	2.4	3.0	2.4	4.1	4.3
79	57	39	23		9	29	38	62

63.7	3.0
	100

62.6	61.8	62.2
4.1	4.9	4.5
100	95	83

Sta + π - Elev

966.67

966.27

1+00

✓

+33

✓

TP

1.29

962.11

961.71

5.85

960.82

960.42

+79

✓

£ Nov. 27, 1959 27

11

81

62.3	62.03	62.7	62.8	63.1	63.0	62.9	62.5	61.3	60.9
4.4	4.4	4.0	3.9	3.6	3.7	3.8	4.2	5.4	5.8
67	41	28	9		7	28	38	52	71

62.6
4.1
100

62.5
4.2
100

61.3
5.4
90

61.32	61.0	60.7	61.3	61.5	61.7	61.4	60.8	57.3
5.35	5.7	6.0	5.4	5.2	5.0	5.3	5.9	9.4
40	57	31	11		7	22	35	63
69								

62.1
4.6
100

60.6
6.1
90

59.5
7.2
77

59.7	60.5	59.4	58.2	57.7	57.4	56.1	54.6	54.5
2.4	1.6	2.7	3.9	4.4	4.7	6.0	7.5	7.6
45	40	27	100		5	22	41	58

58.6
3.5
70

58.6
3.5
87

58.5
3.6
100

59.8
2.3
100

57.9
4.2
78

Sta + π - Elev

962.11

961.71

1 + 80

2

T.P.

7.81

956.84

956.44

1308

949.03

948.63

+30

Nov. 27, 1959

Rt 28

21

5.7 56.4
43 34 27 13 58.1
5.9 56.2
2.1 60.2
4.0 57.6
4.5

Duplicate + 79 Rt

57.9
4.2
50
58.5
3.6
74
58.4
3.7
100

57.2
4.9
23
57.9
4.2
20
58.2
3.9
12
56.8
5.3
9
55.6
6.5
5
54.8
7.3
5
51.8
10.3
23
51.8
10.3
36
52.6
9.5
53

56.8
5.3
36
56.9
5.2
56
57.1
5.0
87
57.2
4.9
100
56.6
5.5
100
55.5
6.6
76

54.8
2.0
55
54.6
2.2
46
55.3
1.5
31
55.4
1.4
20
53.9
2.9
19
50.9
5.9
31
48.7
8.1
53
48.5
8.3
68
49.6
7.8
81
50.6
6.2
81

55.5
1.3
78
55.5
1.3
86
56.0
0.8
100
50.6
6.2
100

Sta	+	π	-	Elev
-----	---	-------	---	------

956.84

956.44

2+73

✓

✓

3

✓

✓

TP

1.11

950.14

949.74

7.81

949.03

948.63

Nov 27, 1959

29

14

84

52.2

4.6
32

52.3

4.5
21

52.0

4.8
7

51.2

5.6
9

50.4

6.4
22

48.3

8.5
46

44.2

12.6
56

43.3

13.5
56

52.3

4.5
49

52.6

4.2
67

53.4

3.4
83

53.8

3.0
100

42.4

14.4
78

44.4

12.4
76

44.1

12.7
67

43.3

13.5
63

41.0

15.8
88

42.2

14.6
91

45.8

11.0
93

47.1

9.7
100

49.8

2.0
62

49.6

2.2
48

50.1

6.7
34

49.3

7.5
14

49.0

7.8
10

48.6

8.2
10

45.9

10.9
27

42.8

14.0
42

50.4

6.4
80

51.1

5.7
100

45.2

11.6
86

38.5

18.3
75

39.2

17.6
59

41.4

15.4
56

45.9

10.9
92

46.4

10.4
100

Sta	+	π	-	Elev.
-----	---	-------	---	-------

950.14

949.74

3+45

✓

TP

8.90

947.00

946.60

12.04

938.10

937.70

1.50

942.4

3+68

✓

+ 85

939.71

939.31

10.37

936.63

936.23

TP

3.08

FK
RG
KP
JH

LT

± November 27, 1959 30
November 30, 1959
Overcast 25° RT

46.5	47.4	47.5	46.5	46.1	45.5	43.7	41.4	36.6
3.6	2.7	2.6	3.6	4.0	4.6	6.4	8.7	13.5
51	46	31	10		9	22	35	54

45.9	46.3	46.4		44.1	43.5	42.4	39.6	34.9
4.2	3.8	3.7		6.0	6.6	7.7	10.5	15.2
64	79	100		100	87	73	60	57

44.4	46.4	46.0	45.1	44.1	42.0	39.5	36.0	35.4
2.6	0.6	1.0	1.9	2.9	5.0	7.5	11.9	11.6
54	41	29	12		12	32	48	59

43.5	43.6	43.4		45.0	42.2	39.5	34.7	34.1
3.5	3.4	3.6		2.0	4.8	7.5	12.9	12.9
66	84	100		100	76	68	64	62

42.9	43.5	44.2	42.4	41.2	37.6	36.0	33.2	33.8
4.1	3.5	2.8	4.6	5.8	9.4	11.0	13.8	13.2
54	45	33	12		23	40	46	60

41.3	41.2	40.5		43.6	42.6	41.3	37.7	
5.7	5.8	6.5		3.4	5.0	5.7	9.3	
67	83	100		100	80	72	65	

Sta + π - Elev

939.71
~~946.60~~

4+00

✓

+16

✓

+31

✓

Sta + π - Elev.

939.71

939.31

4+56

✓

✓

+85

✓

TP

0.08

934.29

933.89

5.50

934.21

933.81

5+02

November 30, 1959 32

11

R1

29.3	21.1	20.6	21.4	24.2	26.8	30.8	31.1
10.4	18.6	19.1	18.3	15.5	12.9	8.9	8.6
26	14	9		8	12	16	19
30.7	30.5	30.1	29.3	34.7	33.1	31.3	28.8
9.0	9.2	9.6	10.4	5.0	6.6	8.4	10.9
36	52	72	86	58	40	30	27

28.8	36.3	36.6	38.0
10.9	3.4	3.1	1.7
100	70	81	100

26.6	19.1	18.6	23.0	28.6	29.7	22.7	22.6	30.0
13.1	20.6	21.1	16.7	11.1	10.0	17.0	17.1	9.7
49	29	22	11		6	7	11	19

25.8	25.0	24.7	35.7	34.9	33.7	32.2
13.9	14.7	15.0	4.0	4.8	6.0	7.5
65	85	100	100	81	62	44

Cor Fe Post R1 Sta 4+85

15.9	16.6	17.6	18.6	19.6	20.5	24.7	27.2	29.6
18.4	17.7	16.7	15.7	14.7	13.8	9.6	7.1	4.7
54	39	18	8		5	14	18	20

Sta + π - Elev

934.29

933.89

5+02

+07

✓

+15

+50

+72

Nov. 30, 1959

33

2+

RT

15.8	19.2	20.1	18.7	20.0	25.0	27.2	29.5	29.4	30.4
18.5	15.1	14.2	15.6	14.3	9.3	7.1	4.8	4.9	3.9
5.5	42	24.	8	13	17	18	37	47	
15.4	14.8	14.8	14.8	14.8	14.8	14.8	14.8	14.8	14.8
18.9	19.5	19.5	19.5	19.5	19.5	19.5	19.5	19.5	19.5
76	100	100	100	100	100	100	100	100	100
21.5	23.8	24.2	25.6	27.0	28.2	29.0	29.1	29.2	29.7
12.8	10.5	10.1	8.7	7.3	6.1	5.3	5.2	5.1	4.6
100	79	64	46	24	8	17	41	53	75
22.7	24.1	24.5	25.2	26.0	26.8	26.6	27.0	27.8	27.9
11.6	10.2	9.8	9.1	8.3	7.5	7.7	7.3	6.5	6.4
100	73	54	38	19	5	19	41	65	81
22.9	23.9	24.1	24.2	24.8	25.0	24.6	23.3	23.2	24.6
11.4	10.4	10.2	10.1	9.5	9.3	9.7	11.0	11.1	9.7
100	70	49	22	12	15	17	23	26	33
27.3	25.8	25.3	25.3	25.3	25.3	25.3	25.3	25.3	25.3
7.0	8.5	9.0	9.0	9.0	9.0	9.0	9.0	9.0	9.0
100	74	52	52	52	52	52	52	52	52

Sta + ~~+~~ - Elev

934.29

933.89

5+88

✓

6

✓

924.50

920.90

3.60

924.10

13.39

920.50

+ 17

✓

166

Nov. 30, 1959 34

14

54

11.1	11.2	10.6	10.4	10.6	13.0	12.8
46	29	10		7	16	22

23.2	23.1	23.7	23.9	23.7	21.3	21.5
------	------	------	------	------	------	------

11.1	11.6	11.8
66	83	100

8.6	9.6	9.9	10.2	10.9
100	73	50	35	25

11.7	10.9	11.7	11.5	13.4	14.3	14.2	11.5	11.0
56	35	18	5		3	18	25	30

11.9	12.7
76	100

9.1	10.3	10.8
100	74	54

4.1	3.6	3.5	3.1	2.8	4.4	5.1	5.2	3.3	3.0	3.2
68	52	36	15	7		2	18	24	29	44

4.7	5.2
84	100

1.2	2.2	2.8	5.7	5.8
100	71	58	51	49

Sta + ~~T~~ - Elev

924.50

924.10

6+46

✓

920.93

911.89

TP

9.04

920.53

12.61

911.49

+ 83

✓

7

✓

Nov. 30, 1959 35

21

21

15.7	17.0	17.0	17.9	16.5	17.0	17.9	17.0	16.3	16.6
8.8	7.5	7.5	6.6	8.0	7.5	6.6	7.5	8.2	7.9
41	26	15	6		20	35	45	47	54

15.7	14.5	12.7
8.8	10.0	11.8
58	74	100

21.7	20.5	19.4
2.8	4.0	5.1
100	75	60

07.7	09.2	10.4	11.4	11.7	12.7	12.8	12.6	13.2	14.9
13.2	11.7	10.5	9.5	9.0	8.2	8.1	8.3	7.7	6.0
64	35	20	7		10	20	28	35	46

07.1	06.0
13.8	14.9
75	100

20.6	19.1	17.8	14.7	14.6
0.3	1.8	3.1	6.2	6.3
100	88	77	65	52

05.8	07.1	08.7	09.7	10.5	11.6	11.5	12.7	16.3
15.1	13.8	12.2	11.2	10.4	9.3	9.4	8.2	4.6
63	38	19	8		18	26	39	61

03.9	03.4
17.0	17.5
82	100

20.3	18.6
0.6	2.3
100	85

Sta + ~~7~~ - Elev

920.93

920.53

7+24

✓

916.08

915.88

TP 0.20 915.68 5.05 915.48

10.9

+55

✓

8

+35

FX
RG
KP
JH

Nov. 30, 1959 96
Dec 1, 1959
Overcast 320 BT

11

03.0	04.4	05.8	07.8	09.7	10.4	11.1	12.2	15.1	16.9
17.9	16.5	15.1	13.1	11.2	10.5	9.8	8.7	5.8	4.0
82	62	38	14		18	29	43	59	76

02.7
→ 18.2

20.7 ✓
0.2
100

Nail in 4" Elm, 55' 81 sta 7+25

02.2	03.2	06.8	07.7	09.1	09.8	11.4	15.3
13.9	12.9	9.3	8.4	7.0	6.3	4.7	0.8
80	60	24	12		18	31	58

00.8
→ 15.3
100

98.7	00.2	01.2	03.0	06.5	07.3	08.1	09.7	12.3	15.4
17.4	15.9	14.9	13.1	9.6	8.8	8.0	6.4	3.8	0.7
100	72	53	31	8		13	19	37	53

00.2	01.9	03.7	05.6	07.0	08.0	09.2	11.6	15.3
15.9	14.2	12.4	10.5	9.1	8.1	6.9	4.5	0.8
46	28	16	7		13	18	36	54

99.0
→ 17.1
65

97.5
18.6
83

96.4
19.7
100

✓

✓

Sta + π - Elev

716.08

915.68

8+61

10.9

✓

9

✓

P.M

902.54

+50

✓

2 Dec 1, 1959

37

11

51

100.1	01.6	05.0	06.0	06.4	07.2	08.9	11.1	15.3
16.0	14.5	11.1	10.1	9.7	8.9	7.2	5.0	0.8
39	24	7		1	11	17	33	52

98.6	97.5	96.6	95.5	95.3
17.5	18.6	19.5	20.6	20.8
57	71	78	94	100

✓

96.5	98.8	00.0	03.3	05.6	06.9	09.1	10.6	15.9
19.6	17.3	16.1	12.8	10.5	9.2	7.0	5.5	0.2
66	46	33	15		12	20	30	52

95.3	94.1
20.8	22.0
83	100

✓

96.5	98.2	00.3	03.4	04.2	05.1	07.5	09.3	12.6
19.6	17.9	15.8	12.7	11.9	11.0	8.6	6.8	3.5
48	38	21	8		4	17	22	35

94.8	95.1
21.3	21.0
71	100

16.1
0.0
42

✓

Sta	+	π	-	Elev
-----	---	-------	---	------

		916.48		
		915.68		

10

✓

TP(Pawn)

6.94

908.74

909.14

908.77

929.48

915.89

TP(up) 13.60

929.08

0.19

915.49

915.48

7+55

8

+35

+61

Dec. 6, 1959

38

11

19+

96.9

99.8

02.8

03.9

08.1

11.7

16.0

19.2

16.3

13.3

12.2

10.0

4.4

0.1

48

27

10

10

30

41

96.3

96.7

97.1

✓

19.8

19.4

19.0

66

85

100

Nail in 16" oak 21 5/4 8+80

16.9

18.6

21.8

12.6

10.9

2.7

✓

66

80

100

17.2

18.5

20.7

23.9

✓

12.3

11.0

8.8

5.6

57

20

83

100

16.9

18.7

21.1

24.8

✓

12.6

10.8

8.4

4.7

58

69

81

100

17.4

20.8

26.0

12.1

8.7

3.5

✓

58

75

100

Sta + ^Δ - Elev

929.48

929.08

9+00

+50

10

TP

6.07

931.93

931.53

3.62

925.86

925.46

13.60

17.93

~~15.11~~

15.41

902.92

902.52

(902.54)

+50

✓

11

Lt

Dec. 1, 1959
Snowing

39

Rt

11.7	8.2	5.2
55	72	82

✓

8.9	6.3	3.7	+1.0
54	67	78	100

✓

7.6	5.2	2.3	+1.9
56	68	80	100

✓

Spike in 18" oak 273'S + 12" W
of Iron Mount

28.1	26.5	22.2	19.1
	10	24	36

2.1	8.6	11.5	14.7
100	74	59	49

✓

18.4	22.7	18.4	12.0	8.6
28.4	25	40	62	77

✓

F.K.
OK

2.8
100

✓

Sta	+	π	-	Elev
-----	---	-------	---	------

931.93
931.53

11+35
13.6

✓

+60

✓

		919.00		918.58
TP	0.42	918.60	13.35	918.18
		909.82		907.55
TP	2.27	909.42	11.45	907.15

10+50

✓

Dec 1, 1959

40

LT

RT

03.2	05.2	07.6	15.3
28.7	26.7	24.3	16.6
	13	25	60

25.7	21.7	17.3
6.2	10.2	14.6
100	83	69

02.7	05.9	08.2	10.9
29.2	26.0	23.7	21.0
	19	35	54

22.1	18.4	15.1
9.8	13.5	16.8
100	88	73

Nail in 12" Ely Root

98.6	00.1	02.4	02.8	03.8
11.2	9.7	7.4	7.0	6.0
47	25	12	7	

97.6	98.3	97.8
12.2	11.5	12.0
66	86	100

Sta + π - Elev

909.82

909.42

11+00

✓

+ 35

✓

12.77

907.94

907.53

7 P 10.39 907.54 2.27 907.15

12.4

+ 60

✓

Dec 1, 1959

41

Lt

Rt

99.0	99.1	00.0	01.4
10.8	10.7	98	84
85	62	44	18



99.2
→ 10.6
100

99.3	00.0	00.6	02.1
10.5	9.8	92	7.7
65	48	25	11



99.6	96.5	93.4
10.2	13.3	16.4
76	95	100

97.0	98.7	00.0	00.8	02.0
10.9	9.0	7.9	7.1	5.9
46	34	21	16	6

97.0	96.3	93.3	93.3
10.9	11.6	14.6	14.6
62	76	82	86



95.5	96.2
12.4	11.7
100	89

Sta + π - Elev

907.94
902.54

11+78

12.4

✓

+90

✓

✓

12

Dec. 1, 1959

42

BT

11

94.1	95.9	97.1	97.7	98.6	01.1	04.5	06.8	09.8
138	120	108	102	93	68	34	11	+1.9
61	59	40	27		13	23	35	57

93.8	97.8	00.7				19.3	13.7	✓
14.1	10.1	7.2				+11.4	+5.8	✓
69	75	100				100	75	

94.5	95.7	97.1	95.6	95.7	96.1	98.9	00.2	02.1
134	122	108	123	122	118	90	77	58
132	27	19	8		6	9	17	20

94.5	96.4	00.1	01.0	17.0	14.2	10.9	07.8	05.6
134	115	78	69	+9.1	+6.3	+30	9.1	2.3
37	60	67	72	100	87	71	52	38

01.6	01.0
6.3	6.9
100	90

01.4	00.6	96.1	95.9	96.3	96.1	96.4	97.4	99.6
65	73	118	120	116	118	115	105	83
49	31	28	14		9	14	15	21

Sta + π - Elev

907.94
907.54

12

+06

✓

+25

✓

918.18

904.57

T.P. 13.65 917.78 3.37 904.17 (904.13)

Lt

Dec. 1, 1959 43
RT

5.9	6.3	7.8	8.6	10.4	9.9	7.4	11.2	9.0
57	36	21	5		11	13	18	21
02.5	02.7			13.6	12.0	10.0	06.6	02.8
5.4	5.2			+5.7	+4.1	+2.1	1.3	5.1
77	100			100	87	75	55	41
04.9	03.3	02.9	01.1	00.6	00.5	00.0	97.2	97.3
3.0	4.6	5.0	6.8	7.3	7.4	7.9	10.7	10.6
69	47	28	14		12	21	25	30
05.5	06.2			09.5	08.6	06.1	00.1	00.6
2.4	1.7			+1.6	+0.7	1.8	7.8	7.3
88	100			100	86	63	45	39
02.0	01.6	00.1	99.3	97.5	98.0	00.5	96.7	98.9
5.5	5.9	4.5	0.9	+3.0	+6.8			
100	71	38	53	76	100			
02.4	02.0	03.4	07.0	10.9	14.7			

iron mont.

Sta	+	π	-	Elev
-----	---	-------	---	------

Sta	+	π	-	Elev
-----	---	-------	---	------

918.18
917.78

Sta	+	π	-	Elev
12+44				

Sta	+	π	-	Elev
1				

Sta	+	π	-	Elev
✓				

Sta	+	π	-	Elev
2				

Sta	+	π	-	Elev
✓				

Sta	+	π	-	Elev
+56				

Sta	+	π	-	Elev
✓				

Sta	+	π	-	Elev
+75				

Dec. 1, 1954

Lt.

F

Rt.

44

05.1

13.1

41

06.5

11.7

60

04.5

13.7

23

07.7

10.5

82

02.2

16.0

16

08.3

9.9

100

02.3

15.9

15

02.9

15.3

69

02.0

16.2

15

00.9

17.3

57

99.4

18.8

23

99.7

18.5

46

00.9

17.3

28

97.5

20.7

42

99.7

18.5

34

97.5

20.7

39

03.7

14.5

84

99.0

19.2

96

99.0

19.2

100

07.4

10.8

43

05.7

12.5

28

06.0

12.2

18

03.2

15.0

9

03.3

14.9

7

03.2

15.0

7

01.3

16.9

11

01.2

17.0

17

02.7

15.5

22

08.7

9.5

60

09.6

8.6

73

10.7

7.5

100

01.3

16.9

100

00.7

17.5

92

98.8

19.4

85

98.6

19.6

66

98.3

19.9

46

01.4

16.8

38

13.4

4.8

80

11.6

6.6

60

08.9

9.3

39

08.3

9.9

17

05.8

12.4

4

02.8

15.4

4

02.7

15.5

12

05.3

12.9

15

04.9

13.3

29

cont. next page

Sta + $\bar{T}$ - Elev

918.18
917.78

12+75

✓

BM 10.74 915.27 914.87 13.65 904.53 904.13

TP 12.18 926.37 925.97 1.08 914.19 913.79

11.1

13+00

✓

+12

FX
RC
KP
XJ
JS
JH

Lt.

Dec 1, 1959
Dec 2, 1959 45
Fair 220 Rt.

15.4
2.8
100

03.1
15.1
60
03.4
14.8
81
01.6
16.6
54
04.0
14.2
100
02.0
16.2
46
04.1
14.1
42
9.5
10.1
✓

Iron Mont

14.7
11.7
46
12.1
14.3
30
09.5
16.9
12
08.8
17.6
2
05.3
21.1
22.8
1
03.6
22.8
5
03.6
18.0
11
07.1
19.3
26

17.3
9.1
66
18.9
7.5
87
19.3
7.1
100
07.5
18.9
100
07.3
19.1
82
06.8
19.6
67
06.6
19.8
61
07.2
19.2
50
06.1
20.3
37
✓

18.4
8.0
52
16.3
10.1
39
12.6
13.8
24
09.7
16.7
5
04.6
21.8
5
03.8
22.6
11
09.8
16.6
27
09.1
17.3
27
08.5
17.9
33

20.8
5.6
72
22.9
2.5
100
09.9
16.5
100
07.1
17.3
75
08.9
17.5
49
✓

Sta + π - Elev

926.37
925.97

13+29

11.1

+60

+60

14.

25
46
72

Dec. 2, 1959

46

LT

RT

18.2	14.7	13.4	12.2	08.6	04.1	04.1	11.5	11.8
8.2	11.7	13.0	14.2	17.8	22.3	22.3	14.9	14.6
54	34	18	5		7	10	16	36

21.7	23.7				12.9	12.3	12.2	
4.7	2.7				13.5	14.1	14.2	
77	100				100	25	56	

26.6	23.4	19.3	15.6	14.6	12.4	12.2	06.1	05.4	06.2
04	3.0	7.1	10.8	11.8	14.0	14.2	20.3	21.0	20.2
100	77	55	33	22		1	9	18	23

16.8	16.3	15.0	13.8	12.1	
9.6	10.1	11.4	12.6	14.3	
100	86	68	49	31	

24.9	21.1	17.7	15.9	14.5	13.5	12.4	10.0	07.9
1.5	5.3	8.7	10.5	11.9	12.9	14.0	16.4	18.5
72	51	30	11		12	25	32	37

26.4	29.3				20.8	19.4	16.9	14.8	07.3
0.0	2.9				5.6	7.0	9.5	11.6	19.1
81	100				100	84	65	51	42

Sta	+	Σ	-	Elev
		926.37		
		925.97		

14+25

✓

TP	10.02	936.04	0.35	926.02	925.62	Transit
----	-------	--------	------	--------	--------	---------

+46

✓

+72

9.7

Dec. 2, 1959

47

30.4 26.4 24.3 21.0 17.4 16.1 15.1 14.3 13.6 9.5
 100 100 21 54 90 103 113 121 128 16.9
 100 74 62 40 15 11 27 35 45

19.7 18.1 16.6 14.4
 6.5 8.3 98 12.0
 100 80 71 51

25.7 22.8 18.4 18.8 18.0 16.6 15.9 15.0 9.9
 10.3 13.2 176 172 180 194 20.1 21.0 26.7
 6.7 45 24 13 8 20 32 44

28.1 30.3 19.9 18.3 16.6 14.6 10.2
 7.9 5.7 16.1 17.7 19.4 21.4 25.8
 84 100 100 85 71 55 49

25.0 22.2 20.6 20.2 19.0 17.6 16.2 15.1 13.0
 11.0 138 154 158 17.0 18.4 19.8 20.9 23.0
 60 43 22 10 11 20 46 51

28.0 30.7 19.7 18.2 16.0 10.5
 8.0 5.3 16.3 17.8 20.0 25.5
 80 100 100 85 69 59

Sta + π - Elev

936.04
935.64

15+00

9.7

✓

+50

✓

16

Dec. 2, 1959

48

1+

8+

110	135	146	149	156	173	189	195	241
60	39	17	10		12	34	53	61
25.0	22.5	21.4	21.1	20.4	18.7	17.1	16.5	11.9

94	59				120	127	192	238
75	100				100	88	77	69
26.6	30.1				19.0	18.3	16.8	12.2

78	126	121	124	139	161	172	189	221
67	43	23	10		18	39	69	78
28.2	23.4	23.7	23.6	22.1	19.9	18.8	17.1	13.9

46	24					183	197
88	100					100	84
31.4	33.6					17.7	16.3

28	53	77	83	102	124	142	157	165
64	42	20	11		16	34	55	75
33.2	30.7	28.3	27.7	25.8	23.6	21.8	20.3	19.5

0.0	1.0							
87	100							
36.0	37.0							

12.5
100
18.5

Sta	+	T	-	Elev
		936.04		
		935.64		

16+40

✓				935.83	
	1.88	925.91	0.21	935.49	
TP	11.55	937.31	0.21	935.76	level
		937.71			

+75

17

+30

Dec 2, 1959

81 49

36.6	35.1	34.2	32.0	30.9	29.8	28.6	26.3	24.6	22.5
10.6	0.9	1.8	4.0	5.1	6.2	7.4	9.7	11.4	12.5
73	49	38	12	5		10	25	49	72

37.2
+1.2
100

20.5
15.5
100

35.6	35.9	35.2	34.1	33.7	32.6	30.5	28.1	25.2	23.6	21.9
2.1	1.8	2.5	3.6	4.0	5.1	7.2	9.6	12.5	14.1	15.8
100	69	46	27	8		20	43	66	82	100

34.2	34.4	34.7	34.6	33.7	33.4	32.7	30.5	28.6	26.4	24.7	22.5
3.5	3.3	3.0	3.1	4.0	4.3	5.0	7.2	9.1	11.3	13.0	15.2
100	86	69	57	29	8		22	40	62	79	

33.0	32.8	32.3	31.6	31.5	31.0	28.7	26.7	24.5	22.6
4.7	4.9	5.4	6.1	6.2	6.7	9.0	11.0	13.2	15.1
77	56	44	22	6		22	45	71	100

33.2
4.5
100

Sta + π - Elev.

937.71
937.31

17+70

18

✓

+30

✓

+60

Dec. 2, 1959

49

11

RT

32.2	31.7	30.9	29.6	28.7	28.1	27.1	26.0	24.0	22.4	22.1
55	60	68	81	90	96	106	117	137	153	150
100	84	68	40	15		7	20	49	74	100

32.0	30.8	29.2	28.2	27.8	27.0	25.9	24.9	23.8	22.6	
5.7	6.9	8.5	9.5	9.9	10.7	11.8	12.8	13.9	15.1	
94	78	54	28	9		8	20	41	62	

32.6										
5.1							14.2	14.3	15.0	
100							100	89	79	

29.7	28.4	27.7	27.6	26.7	25.0	24.3	23.6	23.2		
8.0	9.3	10.0	10.1	11.0	12.7	13.4	14.1	14.5		
62	41	21	6		6	22	39	58		

31.6	33.5									
6.1	4.2						13.1	14.3		
83	100						100	74		

30.7	29.5	28.3	27.6	27.6	27.1	25.6	24.7	23.7	23.3	
7.0	8.2	9.4	10.1	10.1	10.6	12.1	13.0	14.0	14.4	
65	50	32	18	7		11	30	52	66	

Sta

+

π

-

Elev

937.71

937.31

18+60

19

18

28

62

✓

+18

✓

+38

2 Dec 2.1959

50

LT

RT

34.7
30
100

32.6
51
84

24.3
13.4
82

24.8
12.9
100

33.1
46
66

32.0
57
52

31.2
6.5
42

29.6
8.1
23

29.0
8.7
8

28.8
8.9
8

27.6
10.1
7

26.2
11.5
16

25.2
12.5
31

24.1
13.6
43

34.7
30
85

36.0
1.7
100

27.0
10.7
100

25.9
11.8
85

25.4
12.3
70

24.7
13.0
54

33.8
3.9
64

31.7
6.0
45

30.3
7.4
28

29.2
8.5
9

27.9
9.8
16

26.4
11.3
16

25.6
12.1
28

24.6
13.1
38

25.1
12.6
52

35.2
2.5
82

36.9
0.8
100

28.9
8.8
100

27.4
10.3
85

26.2
11.5
70

34.3
3.4
79

31.8
5.9
57

29.6
8.1
34

28.3
9.4
12

27.9
9.8
11

26.7
11.0
11

25.7
12.0
21

24.9
12.8
31

25.7
12.0
48

36.9
0.8
100

30.8
6.9
100

28.0
9.7
75

Sta + π - Elev

937.71

937.31

19+62

✓

20

✓

+25

Dec. 2, 1959

51

LT

RT

31.6	29.4	28.2	28.0	27.8	27.0	25.8	25.4	26.1
6.1	8.3	9.5	9.7	9.9	10.7	11.9	12.3	11.6
75	50	27	9		8	17	28	38

34.8

2.9
100

31.3

6.4 8.3 10.6
100 82 59

29.7

8.0
67

29.1

8.6
45

28.5

9.2
22

28.2

9.5
6

27.9

9.8
7

27.1

10.6
20

26.7

11.0
42

26.4

11.3
65

27.1

10.6
65

30.0

7.7
85

31.0

6.7
100

27.0

8.7
100

27.9

9.8
82

31.3

6.4
65

30.7

7.0
42

30.0

7.7
17

29.6

8.1
6

29.4

8.3
7

28.7

9.0
21

27.7

10.0
37

27.5

10.2
56

27.3

10.4
56

31.7

6.0
88

32.0

5.7
100

28.1

9.6
100

27.7

10.0
77

Sta + π - Elev

937.71

937.31

20+50

✓

946.07

932.58

TP 13.49 945.67 5.13 932.18

+75

✓

946.10

939.84

BM 6.23 945.70 6.23 939.44 939.42

21

✓

2+00

57±

Dec. 2, 1959

52

LT

ST

35.1	34.3	33.3	32.1	32.3	31.4	29.7	28.8	28.1
26	34	44	56	54	63	80	89	96
68	43	25	6		6	17	37	52

34.8	34.5						28.1	28.1
29	32						96	96
86	100						100	73

39.3	38.5	37.3	36.4	35.7	34.2	32.8	31.6	30.3
68	76	88	97	104	119	133	145	158
63	46	24	13		7	13	26	42

39.1	38.6					29.1	29.2	29.4
70	75					170	168	167
79	100					100	80	63

Spike in 16" dot 23+60R+±

43.5	42.9	41.6	40.2	38.9	37.3	36.2	34.8	32.8
26	32	45	59	72	88	99	113	133
61	50	33	18		8	18	28	49

43.6	42.9					30.7	31.8
25	32					154	143
82	100					100	70

Sta	+	π	-	Elev.
-----	---	-------	---	-------

946.10
945.70

21+24

✓

+46

✓

+70

✓

Dec. 2, 1959 53

L+

R+

45.7	44.6	43.1	41.2	40.2	38.9	37.4	35.4	33.9
0.4	1.5	3.0	4.9	5.9	7.2	8.7	10.7	12.2
72	54	34	15	9	19	35	54	46
45.2								
0.9								
100								

43.9	43.7	42.5	41.0	40.0	38.1	35.9	34.3	32.9
2.2	2.4	3.6	5.1	6.1	8.0	10.2	11.8	13.2
82	60	35	18	9	22	45	67	
44.0								
2.1								
100								

41.4	41.1	40.4	39.7	38.7	37.2	35.0	33.7	32.5
4.7	5.0	5.7	6.4	7.4	8.9	11.1	12.4	13.6
83	59	34	13	9	22	42	61	
42.0								
4.1								
100								

Sta	+	π	-	Elev
		946.10		
		945.70		

22+00

✓

+35

✓

+75

		941.12		939.87
BM	1.25	940.72	6.23	939.47

Dec. 2, 1959 54

11

Rt

7.1	7.8	8.3	8.7	9.3	9.4	11.0	12.4	13.3
88	63	39	16	9.3	9.4	11.0	12.4	13.3
39.0	38.3	37.8	37.4	36.8	36.7	35.1	33.7	32.8

39.4
6.7
100

31.7
14.4
100

31.9
14.2
84

32.1
14.0
68

90	97	10.9	11.4	11.8	12.3	13.2	13.6
82	60	39	16	11.8	12.3	13.2	13.6
37.1	36.4	35.2	34.7	34.3	33.8	32.9	32.5

37.7
8.4
100

33.1
13.0
100

32.7
13.4
83

32.5
13.6
66

10.8	11.9	12.3	12.2	12.5	12.4	11.5
60	41	20	12.2	12.5	12.4	11.5
35.3	34.2	33.8	33.9	33.6	33.7	34.6

36.3
9.8
71

37.3
8.8
100

38.0
8.1
100

36.1
10.0
75

Spike in 16" oak Rt Sta 23+60±

Sta + π - Elev

741.12

940.72

23

✓

+ 25

✓

+ 41

Dec. 2, 1959

55

14

RT

37.5

35.9

34.4

34.0

33.7

34.4

34.5

35.2

37.4

3.6

5.2

6.7

7.1

7.4

6.7

6.6

5.9

3.7

68

48

30

12

10

22

37

54

38.5

38.3

41.0

40.7

40.1

2.6

2.8

0.1

0.4

1.0

84

100

100

87

74

37.8

36.0

35.4

35.1

35.8

35.7

36.7

37.8

38.7

3.3

5.1

5.7

6.0

5.3

5.4

4.4

3.3

2.4

51

28

8

5

8

22

31

57

39.6

40.1

39.9

37.9

38.6

38.8

1.5

1.0

1.2

3.2

2.5

2.3

73

95

100

100

91

78

38.5

37.5

37.1

37.8

37.6

37.2

38.6

39.2

38.9

2.6

3.6

4.0

3.3

3.5

3.7

2.5

1.9

2.2

54

33

11

4

8

18

31

46

39.5

39.9

39.8

34.6

35.7

37.0

1.6

1.2

1.3

6.5

5.4

4.1

77

96

100

100

87

70

Sta

+

π

-

Elev

941.12

940.72

23+57

✓

+75

✓

24

✓

Dec. 2, 1959 56

14

54

39.0	38.3	38.7	38.6	38.1	37.6	38.9	39.0	38.5
2.1	2.8	2.4	2.5	3.0	3.5	2.2	2.1	2.6
28	11	10	3	8	13	23	26	36

39.2	38.6	38.3	31.5	32.7	34.1	35.9	37.1
1.9	2.5	2.8	9.6	8.4	7.0	5.2	4.0
50	73	100	100	87	76	60	50

39.4	39.6	38.7	38.4	36.7	35.7	36.9	36.3	35.1
1.7	1.5	2.4	2.7	4.4	5.4	4.2	4.8	6.0
43	32	10	6	7	14	27	41	

37.0	35.2	35.5	30.1	30.4	31.4	33.6
9.1	5.9	5.6	11.0	10.7	9.7	7.5
69	96	100	100	89	74	57

38.0	38.9	37.5	35.6	33.5	32.6	31.7	30.1	28.5
3.1	1.2	3.6	5.5	7.6	8.5	9.4	11.0	12.6
58	37	18	5	9	20	28	46	

35.5	33.1	28.0	26.4	26.8
5.6	8.0	13.1	14.7	14.3
75	100	100	80	64

Sta	+	π	-	Elev
		941.12		
		940.72		

24+15

✓

+43

+43

TP

6.38

936.38

10.73

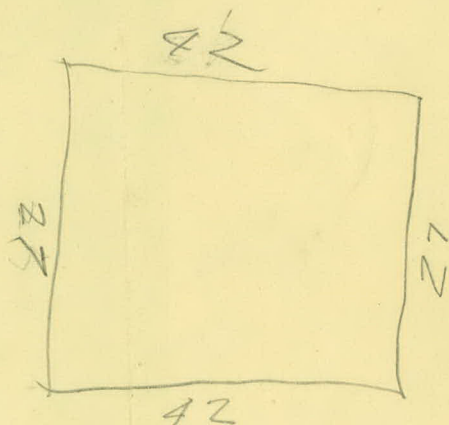
929.99

930.00

936.78

930.39

515



17416-04T 23

9.73 FL TOT

4 ADS

9" CASTING



9" CASTING

13.65 FL

4 ADS

Dec. 2, 1959

57

36.4	39.2	39.0	35.0	32.9	31.0	29.4	27.6	25.9
4.7	1.9	2.1	4.1	8.2	10.1	11.7	13.5	15.2
67	41	33	9	8	8	19	29	36
8.5	31.6	9.5				15.3	16.1	16.1
87	100					100	75	59

36.6	35.4	33.3	31.8	31.4	30.4	29.7	26.8	25.5
4.5	5.7	7.8	9.3	9.7	10.7	11.4	14.3	15.6
42	22	7	2	4	4	16	24	33
5.6	33.4	32.1	31.5			23.4	23.5	24.0
59	73	88	100			100	75	52

Sta + π - Elev

936.78
936.38

24+78

✓

25

✓

+16

✓

Dec. 2, 1959 58

16
39
25
25

BT

32.2	32.1	33.0	31.2	29.5	28.7	28.7	26.1	24.5
4.6	3.7	3.8	5.6	7.3	8.1	8.1	10.7	12.3
55	41	25	5		3	18	30	45
53.2	31.7	32.9	33.6			23.4	23.3	23.6
5.6	5.1	3.9	3.2			134	135	13.2
62	68	89	100			100	82	60

32.5	30.6	32.2	31.7	30.0	27.7	27.4	27.4	26.0	24.3
4.3	6.2	4.6	5.1	6.8	9.1	9.4	9.4	10.8	12.5
41	35	31	23	5		9	23	36	54

32.5	30.5	35.4						23.5	23.5
4.3	3.3	1.4						13.3	13.3
62	80	100						100	73

32.5	30.9	28.7	29.6	29.3	26.9	26.6	27.0	26.3	24.4
4.3	5.9	8.1	7.2	7.5	9.9	10.2	9.8	10.5	12.4
39	23	17	13	9		13	20	32	53

33.6	34.3	36.5	36.2				23.5	23.5	
3.3	2.5	1.3	0.6				13.3	13.3	
55	72	89	100				100	76	

Sta + π - Elev

936.78
936.38

25 + 39

+ 62

26

936.31

~~935.91~~

~~933.91~~

935.91

926.21

~~925.81~~

~~923.81~~

10.57

~~12.57~~

T.P.

10.10

~~924.81~~

Dec. 2, 1959

59

14

B1

33.1	31.1	28.0	27.1	26.6	26.3	24.7	24.1	23.6
3.7	5.7	7.8	9.7	10.2	10.5	12.1	12.7	13.2
58	38	22	10		19	31	45	67

135.0	35.8	35.7				23.2	23.2	23.6
1.8	1.0	1.1				13.6	13.6	13.6
77	94	100				100	85	85

28.3	25.5	24.9	24.5	25.3	26.0	26.0	24.3	23.7
8.5	11.3	11.9	12.3	11.5	10.8	10.8	12.5	13.1
59	41	30	10		4	19	28	42

30.0	31.5	31.9				23.2	23.2	23.5
6.8	5.3	4.9				13.6	13.6	13.3
76	91	100				100	83	62

23.6	23.6	23.5	24.2	26.2	25.9	23.6	23.4
13.2	13.2	13.3	12.6	10.6	10.9	13.2	13.4
67	43	17		9	20	31	54

23.9	24.2				23.3	23.2	23.2
12.9	12.6				13.5	13.6	13.6
86	100				100	77	77

Sta	+	π	-	Elev
-----	---	-------	---	------

		933.91		
		935.91		
		936.31		

26+50				
-------	--	--	--	--

✓				
---	--	--	--	--

+80				
-----	--	--	--	--

✓				
---	--	--	--	--

27				
----	--	--	--	--

Dec. 2, 1959

60

14

RT

23.6	23.6	23.6	23.7	23.7	25.9	26.1	24.2	23.5
12.7	12.7	12.7	12.6	12.6	10.4	10.2	12.1	12.8
100	73	51	23		14	23	33	57

23.6	23.5
12.7	12.8
100	78

23.6	23.6	23.7	23.7	24.2	25.9	26.4	25.0	24.5
12.7	12.7	12.6	12.6	12.1	10.4	9.9	11.3	11.8
100	74	45	17		13	27	37	53

24.1	24.2
12.2	12.1
100	78

23.6	23.6	23.7	24.1	25.3	26.0	26.3	26.0	25.7
12.7	12.7	12.6	12.2	11.0	10.3	10.0	10.3	10.6
100	59	30	10		11	29	44	62

25.2	25.4	25.7
11.1	10.9	10.6
100	95	79

sta

+

π

-

E/ev

~~933.91~~

~~935.91~~

936.31

27+35

✓

+63

✓

+81

± Dec. 2, 1959

61

Lt

Rt

23.6	23.5-	23.6	24.3	25.6	26.4	26.8	26.3	26.7	26.9
12.7	12.8	12.7	12.0	10.7	9.9	9.5	10.0	9.6	9.4
80	68	36	14		5	16	21	27	42

→ 23.6
12.7
100

26.3
10.0
100

26.5-
9.8
89

26.9
9.4
70

27.3
9.0
55

24.0	24.7	25.8	27.3	27.7	27.9	27.6	27.8	27.7
12.3	11.6	10.5	9.0	8.6	8.4	8.7	8.5	8.6
87	65	39	20		13	26	43	61

→ 24.0
12.3
100

27.6
10.9
100

27.8
10.2
86

27.7
9.3
72

26.6	27.2	28.2	28.3	28.9	29.0	28.1	28.7	28.0
9.7	9.1	8.1	8.0	7.4	7.3	8.2	7.6	8.3
78	49	27	14		6	23	37	50

→ 26.6
9.7
100

28.1
11.0
100

28.7
10.0
82

28.0
9.0
69

Sta	+	π	-	Elev.
		933.71		
		935.91		
		936.31		

28

✓

+17

✓

+42

Dec. 2, 1959 62

LT

RT

30.0	30.8	29.2	29.6	30.3	30.3	29.4	28.8	29.7
6.3	5.5	7.1	6.7	6.0	6.0	6.9	7.5	6.6
38	23	12	7	11	26	30	37	

29.4	28.1	28.2
6.9	8.2	8.1
57	83	100

26.5	28.0	29.2
98	73	71
100	74	55

31.9	33.3	32.6	30.5	31.2	31.2	31.3	30.8	30.6	31.4
44	30	37	5.8	5.1	5.1	5.0	5.5	5.7	4.9
47	26	22	12	7		9	25	43	65

30.6	30.1	29.9
5.7	6.2	6.4
67	86	100

28.8	30.8
75	55
100	79

33.9	34.8	35.3	32.9	32.5	32.7	32.7	33.1	34.1
2.4	1.5	1.0	3.4	3.8	3.6	3.6	3.2	2.2
71	44	22	11		12	24	39	55

33.9	34.1
2.4	2.2
90	100

32.4	33.7	34.7
3.9	2.6	1.6
100	88	72

Sta + π - Elev

~~933.91~~
~~935.91~~
 936.31

28+72

✓

TP 6.37 ~~940.28~~
~~942.28~~ 0.00 ~~933.91~~
 942.68 935.91
 936.31

29

✓

TP 6.79 ~~945.87~~
~~947.87~~ 1.20 ~~941.48~~
 948.27 939.08
 941.08

+50

Dec 2, 1959
Rt

63

L1

1.2	1.4	1.1	2.5	2.0	2.7	2.6	0.9	0.0
66	37	19	10		16	34	52	60

1.1 35.2
88

1.0 35.3
100

0.2 36.1
100

10.9 37.2
77

7.0	7.1	7.5	8.1	8.5	8.6	8.4	7.9	4.7
8.3	55	33	16		8	27	47	72

6.8 35.9
100

4.5 38.2
100

4.2 38.5
81

11.7	11.8	11.8	12.0	12.1	12.5	12.0	12.0	9.7
71	52	26	11		12	20	36	55

11.7 36.6
89

11.3 37.0
100

6.4 41.9
100

7.1 41.2
79

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		945.87		
		947.87		
		948.27		

30

✓

+22

✓

+62

TP

5.85

	²⁸
949.50	
951.28	
951.68	

2.44

945.83
945.93
943.43
945.45

Dec 2, 1959 64

14

RT

38.3	37.5	37.5	38.6	38.5	39.5	42.8	43.9	44.6
10.0	8.8	8.8	9.7	9.8	8.8	5.5	4.4	3.7
58	37	18	6		18	38	50	68

37.7	37.3
10.6	11.0
81	100

45.9	45.5
2.4	2.8
100	81

40.0	41.0	40.3	40.6	42.2	43.1	44.5	44.5	44.7
8.3	7.3	8.0	7.7	6.1	5.2	3.8	3.8	3.6
46	26	18	7		8	27	36	48

39.3	39.0	39.6
9.0	9.3	8.7
67	85	100

47.1	46.8	46.5
1.2	1.5	1.8
100	86	69

44.1	44.6	43.4	45.3	45.5	46.2	46.7	47.2	48.0
4.2	3.7	4.9	3.0	2.8	2.1	1.6	1.1	0.3
50	40	22	8		17	36	55	74

Bldg

43.9	42.0	41.8	44.2	44.2
4.4	6.3	6.5	4.1	4.1
64	77	91	97	100

SE Cor Bldg Ent slab

Sta + π - Elev.

~~949.28~~
~~28~~
~~951.36~~
951.68

31

+14

+32

✓

+64

✓

PK
RG
JH

Dec. 3, 1959
Clear 32°

65

17

81

48.1	47.5	45.9	46.1	46.4	47.2	47.8	48.2	48.1	48.23
3.6	4.2	5.8	5.6	5.3	4.5	3.9	3.5	3.6	3.45
38	35	23	12		22	42	65	78	Fl.
HO								Bldg	

48.3	48.2	47.5	46.6	47.0	47.3	47.9	48.3	48.2
3.4	3.5	4.2	5.1	4.7	4.4	3.8	3.4	3.5
39	23	17	15		20	47	69	78
HO								Bldg

48.2	47.9	47.1	47.2	47.3	47.4	48.7	48.6	48.4
3.5	3.8	4.6	4.5	4.4	4.3	3.0	3.1	3.3
23	16	14	8		5	10	24	45

48.4	48.6	48.0	48.2	48.5	48.1	47.8
3.3	3.1	3.7	3.5	3.2	3.6	3.9
40	HO	100	93	74	67	49

48.3	48.1	47.9	47.7	48.0	48.5	48.3	47.9	48.2
3.4	3.6	3.8	4.0	3.7	3.2	3.4	3.8	3.5
74	51	28	14		5	17	34	56

48.2
3.5
100

48.4	48.4
33	3.3
100	78

Sta

+

π_{28}

-

Elev.

~~949.28~~

~~951.28~~

951.68

32

✓

+50

33

Dec. 3, 1959

66

24

RT

47.0	47.0	46.8	47.6	48.0	48.1	47.7	47.8	47.8
4.7	4.7	4.9	4.1	3.7	3.6	4.0	3.9	3.9
44	26	17	9		5	20	23	40

47.2	47.3	47.4
4.5	4.4	4.3
63	86	100

48.3	48.8	47.8
3.4	2.9	3.9
100	81	63

47.0	46.8	46.8	47.4	47.7	47.7	47.9	47.7	47.1	47.1
4.7	4.9	4.9	4.3	4.0	4.0	3.8	4.0	4.6	4.6
29	24	15	7		9	11	16	20	34

47.0	46.9	47.0
4.7	4.8	4.7
52	77	100

47.8	47.7	47.4
3.9	4.0	4.3
100	74	50

47.3	47.2	47.7	47.2	47.4	47.8	47.7	48.0	47.3	47.7
4.2	4.5	4.0	4.5	4.3	3.9	4.0	3.7	4.4	4.0
32	15	11	9	8		10	12	27	46

47.5	47.4	47.3
4.2	4.3	4.4
57	83	100

48.1	47.9
3.6	3.8
100	70

Sta + π - E/ev

951.68
~~951.28~~

33+50

✓

34

✓

BM 1.11 949.84 ~~949.43~~ 2.95 948.73 948.33 (948.32)

+ 21

± Dec. 3, 1959

67

Lt.

Rt.

48.0	48.3	47.5	48.0	48.3	48.1	48.8	47.5	47.8
3.7	3.4	4.2	3.7	3.4	3.6	2.9	4.2	3.9
15	10	9	6		9	12	25	46

47.8	47.7	47.6	47.6		47.8	47.7
3.9	4.0	4.1	4.1		3.9	4.0
35	60	82	100		100	71

48.4	48.2	47.2	47.6	47.7	47.5	48.3	48.3	47.5	47.4
3.3	3.5	4.5	4.1	4.0	4.2	3.4	3.4	4.2	4.3
14	10	9	5		9	11	15	24	31

47.9	47.8	47.9	48.0	48.1	47.8		46.6	47.0
3.8	3.9	3.8	3.7	3.6	3.9		5.1	4.7
15	31	54	72	86	100		100	65

Spike in PP 11/11 sta 34+25

47.6	47.6	47.9	46.7	47.1	46.8	47.9	47.3	47.4
2.2	2.2	1.9	3.1	2.7	3.0	1.9	2.5	2.4
38	15	11	9		9	12	18	42

47.8	47.8	47.6		46.3	46.8
2.0	2.0	2.2		3.5	3.0
64	83	100		100	74

Sta + π - Elev.

949.83
~~949.43~~

34+55

✓

35

✓

1354
0.29
13.25

+30

✓

Dec 3, 1959

68

Lt.

Rt

46.5	46.8	45.1	45.7	45.8	45.4	46.3	46.4	45.8	45.6
3.3	3.0	4.7	4.1	4.0	4.4	3.5	3.4	4.0	4.2
21	11	9	5		9	10	15	23	42

46.8	47.5	47.5	47.6					43.6	44.5
3.0	2.3	2.3	2.2					6.2	5.3
43	67	91	100					100	66

45.3	44.6	43.6	42.1	42.8	42.1	43.0	42.8	41.1
4.5	5.2	6.2	7.7	7.0	7.7	6.8	7.0	8.7
45	25	11	7		10	11	15	30

46.4	47.1	47.8			37.5		38.3	39.2
3.4	2.7	2.0			12.3		11.5	10.6
64	83	100			100		79	54

41.6	40.6	39.5	40.0	40.1	39.5	40.2	38.9	36.9
8.3	9.2	10.3	9.8	9.6	10.3	9.6	10.9	12.9
28	11	9	6		10	11	19	37

43.7	45.3	46.4	47.1				33.8	34.8
6.1	4.5	3.4	2.7				16.0	15.0
48	69	84	100				100	62

Sta + π - Elev.

83
~~949.43~~

35+69

13.25

✓

36

✓

+30

940.51

936.29

T.P.

4.22

940.11

13.54

935.89

Dec. 3, 1959

69

LT

RT

40.0	38.2	37.2	35.8	36.2	35.4	36.2	35.6
9.8	11.6	12.6	14.0	13.6	14.4	13.6	14.2
42	23	11	9		10	11	15

42.3	44.5	45.7	28.1	28.8	30.4	33.2	34.8
7.5	5.3	4.1	21.7	21.0	19.4	16.6	15.0
63	83	100	100	73	50	27	18

36.2	34.4	33.1	33.1	32.4	32.8	32.3	29.9
13.6	15.4	16.7	16.6	17.4	17.0	17.5	19.9
28	13	10		10	11	13	19

38.6	41.3	43.2	22.1	23.1	24.5	27.2
11.0	8.5	6.6	27.7	26.7	25.3	22.6
52	81	100	100	84	61	34

33.8	32.4	31.7	30.3	30.1	29.6	30.0	29.5	25.7
16.0	17.4	18.1	19.5	19.6	20.2	19.8	20.3	24.1
32	21	15	11		8	10	12	20

35.0	37.4	41.1	18.2	19.8	21.2	23.4
14.8	12.4	8.7	31.6	30.0	28.6	26.4
54	75	100	100	82	60	35

Sta	+	π	-	Elev
		940.51		
		940.11		

36+52

13.24
 1.70
 12.5

✓

+73

✓

TP	9.43	936.00	13.54	926.57
----	------	--------	-------	--------

13.51
 2.51
 10.0

37

✓

± Dec. 3, 1959

70

Lt

Rt

32.9	30.8	28.1	28.3	28.3	27.7	28.2	27.5	22.9
76	97	11.4	12.2	12.2	12.8	12.3	13.0	17.6
54	30	14	11		5	8	10	20

5.0	1.7				15.8		19.5	21.0
77	100				24.7	22.3	21.0	19.5
					100	70	49	30

30.4	28.8	26.8	25.8	25.7	25.4	25.9	23.6	22.3
10.1	11.7	13.7	14.7	14.8	15.1	14.6	16.9	18.2
48	25	13	11		6	8	15	26

33.2	34.7	36.8		14.5	16.0	17.6	19.3
7.3	5.8	3.7		26.0	24.5	22.9	21.2
68	83	100		100	79	61	46

spite in RR Lt 37120

28.6	26.7	25.8	24.7	24.8	24.0	23.6	22.0	19.1
78	9.7	10.6	11.7	11.6	12.4	12.8	14.4	17.3
51	28	15	11		5	11	27	51

4.8	1.9				13.9	15.4	17.4
77	100				22.5	21.0	19.0
					100	86	68

12.08 inv
 13.60 outlet
 - E/ev.

Sta + T
 936.40
 936.00

37+23

✓

+65

✓

38

✓

		923.58		922.92
TP	0.66	923.18	13.48	922.52
		923.58		914.04
BM	9.54	923.19	9.54	913.64
				(913.65)

Dec 3, 1959

71

Lt

Rt

26.1	25.2	24.4	23.4	23.4	23.0	21.0	20.0
103	112	120	130	130	134	134	164
43	29	16	11		6	14	26
	27.2	28.3	29.9	32.4		15.1	16.9
→ 9.2	8.1	6.5	4.0			213	195
55	68	80	100			100	72
							45
							18.0

23.3	22.5	22.0	21.6	21.3	21.0	21.2	18.5	16.8
13.1	13.9	14.4	14.8	15.1	15.4	15.2	17.9	19.6
56	40	26	14		4	6	20	42
	24.9	25.9	27.1			13.8	14.8	15.9
→ 11.5	10.5	9.3				22.6	21.6	20.5
74	87	100				100	79	59

20.5	20.0	19.9	20.1	19.7	19.4	19.9	17.2	16.0
15.9	16.4	16.5	16.3	16.7	17.0	16.5	19.2	20.4
48	27	14	6		3	4	19	44
	21.7	22.6	23.9			12.1	13.3	14.6
→ 14.7	13.8	12.5				24.3	23.1	21.8
66	82	100				100	82	63

Spike in 24" Elm 130' E of Sta 39+75

Sta	+ π	- Elev.
1	10.00	10.00
2	10.00	10.00
3	10.00	10.00
4	10.00	10.00
5	10.00	10.00
6	10.00	10.00
7	10.00	10.00
8	10.00	10.00
9	10.00	10.00
10	10.00	10.00
11	10.00	10.00
12	10.00	10.00
13	10.00	10.00
14	10.00	10.00
15	10.00	10.00
16	10.00	10.00
17	10.00	10.00
18	10.00	10.00
19	10.00	10.00
20	10.00	10.00
21	10.00	10.00
22	10.00	10.00
23	10.00	10.00
24	10.00	10.00
25	10.00	10.00
26	10.00	10.00
27	10.00	10.00
28	10.00	10.00
29	10.00	10.00
30	10.00	10.00
31	10.00	10.00
32	10.00	10.00
33	10.00	10.00
34	10.00	10.00
35	10.00	10.00
36	10.00	10.00
37	10.00	10.00
38	10.00	10.00
39	10.00	10.00
40	10.00	10.00
41	10.00	10.00
42	10.00	10.00
43	10.00	10.00
44	10.00	10.00
45	10.00	10.00
46	10.00	10.00
47	10.00	10.00
48	10.00	10.00
49	10.00	10.00
50	10.00	10.00
51	10.00	10.00
52	10.00	10.00
53	10.00	10.00
54	10.00	10.00
55	10.00	10.00
56	10.00	10.00
57	10.00	10.00
58	10.00	10.00
59	10.00	10.00
60	10.00	10.00
61	10.00	10.00
62	10.00	10.00
63	10.00	10.00
64	10.00	10.00
65	10.00	10.00
66	10.00	10.00
67	10.00	10.00
68	10.00	10.00
69	10.00	10.00
70	10.00	10.00
71	10.00	10.00
72	10.00	10.00
73	10.00	10.00
74	10.00	10.00
75	10.00	10.00
76	10.00	10.00
77	10.00	10.00
78	10.00	10.00
79	10.00	10.00
80	10.00	10.00
81	10.00	10.00
82	10.00	10.00
83	10.00	10.00
84	10.00	10.00
85	10.00	10.00
86	10.00	10.00
87	10.00	10.00
88	10.00	10.00
89	10.00	10.00
90	10.00	10.00
91	10.00	10.00
92	10.00	10.00
93	10.00	10.00
94	10.00	10.00
95	10.00	10.00
96	10.00	10.00
97	10.00	10.00
98	10.00	10.00
99	10.00	10.00
100	10.00	10.00

923.59
923.19

 $38 + 32$

✓

+ 65

✓

39

✓

32
65

± Dec. 3, 1959 72

RT

14

19.3	18.6	18.4	18.7	18.5	18.2	18.6	16.2	14.5
4.3	5.0	5.2	4.9	5.1	5.4	5.0	2.4	2.1
46	26	14	6		3	4	10	25

20.2	21.5	22.4			10.8	12.0	12.8	13.6
3.4	2.1	1.2			12.8	11.6	10.8	10.0
63	83	100			100	76	55	40

18.0	17.4	17.5	17.6	17.5	17.3	15.0	13.0	12.2
5.6	6.2	6.1	6.0	6.1	6.3	8.6	10.6	11.4
53	35	14	6		5	18	39	60

18.8	19.5	20.1				10.1	10.7	
4.8	4.1	3.5				13.5	12.9	
72	88	100				100	81	

16.9	16.8	16.5	16.7	16.2	16.1	14.5	12.6	11.5
6.7	6.8	7.1	6.9	7.4	7.5	9.1	11.0	12.1
54	36	19	9		4	13	31	54

17.2	17.6	18.1			08.7	09.3	10.1	10.8
6.4	6.0	5.5			14.9	14.3	13.5	12.8
71	88	100			100	98	79	73

Sta	+	Δ	-	Elev
		923.58		
		923.19		

39+12

✓

+20

12.93

✓

		918.53		917.05	914.05
BM	A.48	918.13	9.54	913.65	(913.65)

+30 Shoulder

+42 $\pm$ Upper Aslon

12 20 3 42 59 72 2 Dec. 3, 1959 73

14

81

70	76	74	71	7.5	8.0	8.0	10.5	11.4
60	41	24	9		6	10	27	50

17.2
6.4
81

17.8
5.8
100

15.5 13.6 12.9 12.3
100 94 87 70

8.2	8.5	8.4	7.5	7.4	7.6	8.2	8.1	8.9	10.1
80	65	44	33	11		10	13	17	31

15.8
7.8
91

16.1
7.5
100

15.4 15.83 13.0 12.6 11.8 10.9
100 96 90 85 70 51
FL 30" 50" P

1.2	20	24	26	2.7	2.8	3.3	3.9	3.8	4.0
100	79	62	42	20		23	51	84	100

13	20	24	2.7	3.00	3.1	3.2	3.3	3.4	3.4
100	74	53	30	MH		24	43	75	100

18.5
0.0
148

20.2
+1.7
200

12.08 Top to Inv. E.
13.60 Top to F.L. N.

15.4
3.1
200

15.4
3.1
150

Sta + π - Elev.

918.53
918.13

39+59

+72

✓

+82

✓

40

Dec 3, 1959

73

Lt

Rt

16.5	15.9	15.4	15.2	15.1	14.9	14.4	14.6	14.5	14.5
202	263	1	33	34	3.6	4.1	3.9	4.0	4.0
100	77	56	35	14		25	50	75	100

12.3	13.7	14.1	12.9	13.1	12.0	12.0	10.9	10.9
6.2	4.8	4.4	5.6	5.4	6.5	6.5	7.6	7.6
49	29	16	4		15	34	41	57

12.4	13.0	13.7	12.9	13.1	12.0	12.0	10.9	10.9
6.1	5.5	4.8	5.6	5.4	6.5	6.5	7.6	7.6
71	86	100			15	34	41	57

FL30"SCP

12.0	12.3	12.8	12.7	12.4	10.8	10.1	09.8	09.5
6.5	6.2	5.7	5.8	6.1	7.7	8.4	8.7	9.0
68	39	24	8		14	31	49	62

12.9	14.0							
5.6	4.5							
80	100							

12.7	12.1	11.8	12.0	11.6	10.7	09.8	09.5	08.9	08.8	09.2
5.8	6.4	6.7	6.5	6.9	7.8	8.7	9.0	9.6	9.7	9.3
100	77	53	31	16		10	23	45	65	84

9.7
100

Sta + Δ - Elev

918.53

~~918.13~~

40 + 50

✓

+ 8.7

✓

41

✓

Dec. 3, 1959 74
BT

LT

13.7	13.5	12.9	12.3	11.8	11.3	10.6	10.1	9.5	9.1
4.8	5.0	5.6	6.2	6.7	7.2	7.9	8.4	9.0	9.4
67	48	29	13		16	30	47	68	87

14.2	14.3
4.3	4.2
89	100

8.8
9.7
100

15.1	14.4	14.1	13.7	13.3	13.0	12.7	12.3	11.7
3.4	4.1	4.4	4.8	5.2	5.5	5.8	6.2	6.8
72	53	35	17		10	23	39	56

15.6
2.9
100

10.1	11.1
8.4	7.4
100	74

14.7	14.1	13.9	13.8	13.4	13.1	12.6	12.3	12.0
3.8	4.4	4.6	4.7	5.1	5.4	5.9	6.2	6.5
75	58	41	18		10	23	39	56

15.2
3.3
100

10.3	11.3
8.2	7.2
100	78

Sta + π - Elev.

918.53
918.13

41+50

✓

42

✓

+48

5.69 12.84

+50

✓

Dec 3, 1959

75

LT

RT

5.6	5.2	5.0	5.0	4.9	4.6	4.9	5.5	6.5
82	62	39	16		12	29	52	79

12.9
12.5
10.0
100

13.3
13.5
13.5
10.8
7.7
100

7.1	6.3	5.9	5.3	4.9	4.9	5.0	5.0	6.0
78	62	40	18		13	31	54	80

11.4
12.2
12.6
13.2
13.6
13.5
13.5
12.5

10.5
8.0
100

Top MH 4' LT FL to Top = 13.9

8.4	7.7	7.0	6.3	5.5	5.5	5.4	5.4	5.5
84	71	49	28		11	23	44	62

10.1
10.8
11.5
12.2
13.0
13.0
13.1
13.1
13.0

9.3
9.2
100

11.0
12.3
7.5
6.2
100
83

Sta + Δ - Elev

914.53
918.13

43

✓

513.55

912.84

TP 8.75 913.19 5.69 912.44

+30

✓

+61

44

Dec 3, 1959

76

Lt

Rt

10.3				12.2	11.8		11.7			10.8
8.2	7.4	7.1	6.7	6.3	6.7	6.8	7.4	7.7		
77	59	37	16		13	29	54	71		

09.3

9.2

09.0

9.5

100

SEdge MH 62151042+48

11.3	11.5	11.9	11.8	11.8	12.0	11.6	11.3	10.5	09.9	09.0
2.3	2.1	1.7	1.8	1.8	1.6	2.0	2.3	3.1	3.7	4.6
66	51	30	12		11	20	36	52	69	85

10.7

2.9

85

10.0

3.6

100

08.3

10.3

100

08.0	08.7	09.3	09.9	10.2	10.5	09.7	09.1	07.7	07.1	06.5
5.6	4.9	4.3	3.7	3.4	3.1	3.9	4.5	5.9	6.5	7.1
100	80	56	37	18		12	27	55	74	100

07.8

5.8

100

08.7

4.9

60

08.8

4.8

38

08.6

5.0

18

09.4

4.2

7

09.0

4.6

12

08.1

5.5

28

07.3

6.3

50

06.4

7.2

73

06.1

7.5

100

05.9

7.7

100

549

+

π .

-

Elev

713.59

9/3.19

44 +50

45

415

+50

+75

46

Lt.

£

Rt

77

09.5	09.8	09.4	08.6	08.0	07.6	06.9	06.2	06.2	06.3	06.6	✓
4.1	3.8	4.2	5.0	5.6	6.0	6.7	7.4	7.4	7.3	7.0	
100	83	68	43	19		15	31	49	72	100	

10.1	09.8	08.9	08.0	07.3	07.1	06.5	06.9	07.5	08.0	✓
3.5	3.8	4.7	5.6	6.3	6.5	7.1	6.7	6.1	5.6	
100	82	61	37	13		22	45	69	100	

06.25
7.34 M. H. FL to Top = 13.2 feet
6

08.6	07.4	06.6	06.5	07.3	06.9	06.6	07.0	07.3	07.6	✓
5.0	6.2	7.0	7.1	6.3	6.7	7.0	6.6	6.2	6.0	
100	77	55	28	10		16	37	68	100	

07.5	06.5	06.4	06.6	07.4	07.2	06.4	06.9	07.2	07.0	07.0	✓
6.1	7.1	7.2	7.0	6.2	6.4	7.2	6.7	6.4	6.6	6.6	
100	68	46	22	6		15	39	68	82	100	

06.7	06.2	06.2	06.4	07.1	06.8	06.1	06.3	06.1	05.6	05.1	✓
6.9	7.4	7.4	7.2	6.5	6.8	7.5	7.3	7.5	8.0	8.5	
100	70	49	27	8		15	48	62	81	100	

54

+

K

-

Elev.

913.59

913.19

46450

905.38

904.62

t.p.

0.76

904.98

8.97

904.22

+75

47

+50

+88

+91

F

9.1	8.4	8.4	8.8	7.8	8.2	9.1	10.5	11.8	12.8	13.4
100	69	45	23	10		16	41	64	85	100
04.5	05.0	05.2	04.8	05.8	05.4	04.5	03.1	01.8	00.8	00.2

1.5	0.8	0.8	0.8	1.5	0.7	1.0	1.6	3.6	5.4	6.4	7.0
100	80	62	40	22	5		14	34	58	77	100
03.9	04.6	04.6	04.6	03.9	04.7	04.4	03.8	01.8	00.0	99.0	98.4

2.2	2.0	2.0	2.1	2.6	2.3	2.5	3.7	5.2	6.7	8.5	9.7
100	84	67	44	22	8		13	34	58	82	100
03.2	03.4	03.4	03.3	02.8	03.1	02.9	01.7	00.2	98.7	96.9	95.7

5.9	5.7	5.6	5.9	6.2	5.6	6.0	7.2	8.0	9.8	13.9	9.8	7.8	7.4
100	85	67	44	22	6		19	44	62	69	77	85	100
99.5	99.7	99.8	99.5	99.2	99.8	99.4	98.2	97.4	95.6	91.5	96.6	97.6	98.0

ditch

6.9	6.8	6.6	7.0	7.5	8.1	8.4	8.1	8.6	14.5	14.7	10.6	8.6	7.5	6.3
100	85	71	52	29	12	6		18	40	47	55	63	82	100
98.5	98.6	98.8	98.5	97.9	97.3	96.94	97.3	96.8	94.9	90.7	94.8	96.8	97.9	99.1

M H 91 + 82

M. H.

9.2	9.1	9.3	8.7	8.6	8.8	9.3	10.6	14.3	8.9	8.2	6.3
100	73	50	24	7		17	31	37	56	73	100
96.2	96.3	96.1	96.7	96.8	96.6	96.1	94.8	91.1	96.5	97.7	99.1

sta

+

π

-

Elev

905.38
904.98

48+00

+22

+34

+45

+75

49

95.3	95.6	95.4	95.8	96.2	96.1	94.5	91.7	96.3	97.4	99.3
10.1	9.8	10.0	9.6	9.2	9.3	10.9	13.7	9.1	8.0	6.1
100	79	60	32	7		22	32	53	74	100

93.6	93.7	94.7	95.4	94.4	91.3	91.5	95.6	96.2	96.7	99.4
11.8	11.7	10.7	10.0	11.0	14.1	13.8	9.8	9.2	8.7	6.0
100	79	44	12	8	13	19	32	42	64	100

93.3	93.5	94.2	94.8	94.1	92.3	91.4	91.5	95.4	96.1	96.8	99.2
12.1	11.9	11.2	10.6	11.3	13.1	14.0	13.9	10.0	9.3	8.6	6.2
100	84	57	28	18	8		6	22	36	64	100

93.1	93.1	92.8	90.8	90.7	92.2	96.0	95.7	96.1	96.2	97.0	98.8
12.1	12.1	12.6	14.6	14.7	13.2	9.4	9.7	9.3	9.2	8.4	6.6
100	61	44	33	22	14	6	15	40	40	68	100

93.0	93.4	94.1	94.8	96.1	97.4	97.0	97.5	98.2	99.1
12.4	12.0	11.3	10.6	9.3	8.0	8.4	7.9	7.2	6.3
100	78	60	39	12		13	40	68	100

93.0	93.4	94.9	95.3	96.8	98.3	98.6	99.5	100.6	101.4
12.4	12.0	10.5	10.1	8.6	7.1	6.8	5.9	4.8	4.0
100	81	76	40	14		12	36	67	100

sta

+

T.

-

E/co

905.51
904.98

49+40

911.75

903.04

T.P.

8.71

911.35

2.34

902.64

+80

50

+50

✓

51

Dec. 4, 1959

80

LC
RG
JS
KJ
JH
TX
✓

£

RT

93.7	94.6	97.3	97.2	97.8	00.8	02.8	02.7	03.3	04.5	05.4
11.7	10.8	8.1	8.2	7.6	4.6	2.6	2.7	2.1	0.9	0.0
100	90	78	49	28	12		12	35	60	100

✓

96.3	97.9	99.9	01.1	02.9	05.8	06.5	07.6	07.7	09.3	10.6	10.7
15.4	13.8	11.8	10.6	8.8	5.9	5.2	4.1	4.0	2.4	1.1	1.0
100	85	57	32	16		10	26	39	64	86	100

✓

97.3	99.1	00.7	01.9	03.6	06.4	06.7	07.5	08.7	09.4	10.7	11.1
14.4	12.6	11.0	9.8	8.1	6.3	5.0	4.2	3.0	2.3	1.0	0.6
100	81	62	37	17	3		9	22	45	72	100

✓

02.5	03.1	03.8	05.0	06.2	06.9	07.4	07.9	08.2	09.0
9.2	8.6	7.9	6.7	5.5	4.8	4.3	3.8	3.5	2.7
60	43	20	10		10	21	44	62	84

00.0	98.0
11.7	13.7
78	100

09.7
2.0
100

✓

97.2	98.7	00.3	02.0	03.5	03.9	04.4	05.3	05.7	06.1
14.5	13.0	11.2	9.7	8.2	7.8	7.3	6.4	6.0	5.6
100	72	49	22		10	32	55	77	100

✓

Sta + TP - Elev.

911.75
911.35

51 + 14

+ 50

+ 66

02.60
9.15

52

915.78

902.87 902.89

TP 12.89 915.38 8.88 902.47 (902.49)

0.13
+ 15

✓

+ 62

12 62 7

Dec. 4, 1959

81

Lt

R1

96.7	98.5	00.2	01.7	02.9	03.7	04.1	05.0	06.1
15.0	13.2	11.5	10.0	8.8	8.0	7.6	6.7	5.6
100	74	46	19		15	37	66	100

✓

96.0	96.8	98.4	00.7	02.9	04.0	04.4	06.2	07.0	08.0
15.7	14.9	13.3	11.0	8.8	7.7	7.3	5.5	4.7	3.7
100	74	49	26		16	33	56	80	100

TMP NH 6.24 FL to Top = 17.7' INV to Top 12.9

✓

96.0	96.2	96.7	00.7	03.5	05.4	06.9	08.1	09.3	10.8
15.7	15.5	15.0	11.7	8.2	6.3	4.8	3.6	2.4	0.9
100	74	50	23		18	37	57	79	100

Top Mont Sta 52+54.32

✓

96.4	96.6	97.1	99.0	03.4	05.0	06.4	07.2	08.5
19.4	19.2	18.7	16.8	12.4	10.8	9.4	8.6	7.3
82	64	45	25		11	24	39	58

→ 96.4
19.4
100

12.1
3.7
100 82

✓

96.9	97.5	00.9	01.5	02.7	04.6	07.0	11.0	15.8
18.9	18.3	14.9	14.3	13.1	11.2	8.8	4.8	0.0
53	32	11	4		6	28	47	57

→ 96.8
19.0
75 100

19.5
+3.7
100 87

✓

Sta	+	π	-	Elev
		915.78		
		915.38		

52+72

✓

53+00

✓

+12

BM	0.13	902.62	12.89	902.49	902.49
TP	5.58	900.84	7.36	895.26	

+12

Dec 4, 1939

92

Lt.

F

Rt

97.4	99.5	01.1	01.5	02.9	05.1	08.8	14.2	15.8
18.4	16.3	14.7	14.3	12.9	10.7	7.0	1.6	0.0
39	20	12	4		7	32	60	70

97.0	97.0	96.7				15.6	16.6	17.4
18.8	18.8	19.1				0.2	+0.8	+1.6
62	83	100				100	89	80

97.1	97.6	99.1	00.8	02.7	05.0	08.5	02.0	98.5
18.7	18.2	16.7	15.0	13.1	10.8	7.3	13.8	17.3
57	37	27	11		13	34	49	66

96.8	94.5	94.5				98.1	98.6
19.0	21.3	21.3				17.7	17.2
71	88	100				100	82

01.8	02.8	04.1	01.8
14.0	13.0	11.7	14.0
8	21	28	

Top Mont Sta 52 + 54.32

94.4	95.8	97.0	97.4	99.9	98.5	95.6	94.8	96.6	97.0
6.8	5.4	4.2	3.8	1.3	2.7	5.6	6.4	4.6	4.2
100	72	55	34	16	38	49	74	90	100

Sta	+	π .	-	Elev
-----	---	---------	---	------

901.24

900.84

53+22

✓

+38

✓

+50

✓

27 98 500 1 11

Dec. 4, 1959

83

11

81

96.0	96.4	96.5	98.6	00.7	03.2	99.6	96.3	95.6	91.0
52	48	47	26	0.5	+2.0	16	49	56	102
62	51	32	17			18	27	30	39

94.5	94.1	93.4	88.5
67	71	78	12.7
78	95	100	Creek
			125

95.4	94.1	92.1	90.6
58	71	91	10.6
100	78	66	53

89.0	88.9	94.2	95.5	97.2	97.8	97.1	91.2	90.9	91.5
122	123	70	57	4.0	34	41	10.0	10.3	97
75	48.5	48	13		8	17	28	39	50

93.0	93.4	91.9	88.6	95.5	93.8	90.8	91.2	95.7
82	78	93	126	57	74	104	10.0	55
77	88	100	120	100	83	79	72	59

88.9	93.0	94.3	94.9	95.0	92.1	93.6	94.3	95.6
123	82	69	63	62	91	76	69	56
41	37	31	5	6	20	31	49	66

89.6	90.9	89.7	88.2
116	103	115	130
45	61	76	100

95.4	95.4	91.9	91.3
58	58	93	99
100	98	90	74

Sta	+	π	-	Elev
-----	---	-------	---	------

Sta	+	π	-	Elev
		901.24		
		900.84		

Sta	+	π	-	Elev
53+60				

Sta	+	π	-	Elev
53+60				
✓				

Sta	+	π	-	Elev
53+60				
✓				
+ 70				

Sta	+	π	-	Elev
53+60				
✓				
+ 70				
✓				

Sta	+	π	-	Elev
53+60				
✓				
+ 70				
✓				
+ 82				

Sta	+	π	-	Elev
53+60				
✓				
+ 70				
✓				
+ 82				
✓				

82 91

Dec. 4, 1959

84

Lt

Rt

91.7	89.4	89.2	91.6	92.0	90.9	91.2	93.1	95.1
95	118	120	96	92	103	100	81	61
48	36	32	19		7	29	42	60

93.7	94.3						95.2	95.9
75	69						60	53
76	100						100	75

94.5	93.8	88.7	89.0	88.8	89.1	89.3	89.3	93.2
67	74	125	122	124	121	119	119	80
35	26	17	8		8	25	43	58

93.6	94.7	94.1	94.4				95.3	95.4
76	65	71	68				59	58
49	63	70	100				100	74

95.0	94.7	94.8	94.1	94.5	94.2	91.0	91.2	93.3
62	65	64	71	67	70	102	100	79
58	46	23	12		8	20	29	35

94.2	94.2		94.8	92.4	90.4	89.5	90.0
70	70		64	88	108	117	112
85	100		100	77	61	52	48

Sta	+	π .	-	Elev
		901.24		
		900.84		

53+91

✓

54

+50

55

		910.96		897.19
TP	13.77	910.56	4.05	896.79

+30

Dec 4, 1959

84

L+

B+

94.3	94.6	94.9	95.2	96.2	95.2	94.2	89.5	89.8
6.9	6.6	6.3	6.0	5.0	6.0	7.0	11.7	11.4
100	79	48	18		27	57	70	73

✓

91.7	93.4
9.5	9.8
100	88

94.1	94.4	95.2	94.8	95.3	95.6	95.4	96.4	96.5	96.4
7.1	6.8	6.0	6.4	5.9	5.6	5.8	4.8	4.7	4.8
100	80	55	39	19		22	55	85	100

✓

94.7	94.9	95.4	95.2	95.4	95.7	96.2	96.4	97.0	98.0
6.5	6.3	5.8	6.0	5.8	5.5	5.0	4.8	4.2	3.2
100	77	57	43	22		20	45	70	100

✓

95.5	95.6	95.9	95.7	96.2	96.5	97.3	97.9	99.7
5.7	5.6	5.3	5.5	5.0	4.7	3.9	3.3	1.5
100	81	54	24		19	45	70	100

✓

97.2	97.3	97.0	96.6	97.0	97.8	98.7	99.2	99.1	93.0
13.8	13.7	14.0	14.4	14.0	13.2	12.3	10.8	10.9	8.0
100	82	56	28		20	42	70	82	100

✓

Sta + T. = Elev

910.96
910.56

55+55

✓

+65

✓

TP 7.32 911.81 911.41 6.47 904.09
904.49

+75

✓

♀ Dec. 4, 1959
 Dec 8, 1959

85

47

9 B+

10.9	11.4	11.3	11.6	12.0	12.0	10.8	9.4	8.3
76	49	26	16		16	36	49	61
100.1	99.6	99.7	99.4	99.0	99.0	100.2	101.6	102.7

9.8	9.7	10.1	10.6	10.8	10.5	8.2	8.4	8.6
87	72	52	24		9	23	42	74
01.2	01.3	00.9	00.4	00.2	00.5	02.8	02.6	02.4

$\rightarrow 9.5$
 $\frac{100}{100}$

$\rightarrow 7.8$
 $\frac{100}{100}$

Spike in Fe Post.

86	8.8	03.0	70	9.6	02.2
100	8.2	03.6	54	9.0	02.8
			38	9.0	02.8
			23	8.7	03.1
			9	8.3	03.5
				8.8	03.0
			18	9.0	02.8
			46	9.2	02.6
			66	9.2	02.6
			84	9.2	02.6
100	8.5	03.3			

Sta	+	π	-	Elev
		911.81		
		911.41		

55+82

✓

+90

✓

TP		53 12.04916.43	7.32	49 904.09
----	--	-------------------	------	--------------

56

RG
KJ
JH

Dec 8, 1959

Dec. 9

RT

86

1+

#

03.6

8.2
50

7.9
72

04.6
7.2
72

04.3
7.5
86

04.0

7.8
40

04.1
7.7
100

04.1
7.7
68

04.4
7.4
100

03.5

8.3
34

03.7
8.1
4.1

04.0

12.5
37

04.8
11.7
100

03.3

8.5
19

03.4
8.4
16

03.5

13.0
16

02.1

8.7

02.0
8.8

03.1

13.4

02.8

9.0
16

02.8
9.0
18

02.7

13.8
16

02.6

9.2
35

02.4
9.4
43

02.2

14.3
32

02.5

9.3
57

02.5
9.3
65

02.3

14.2
52

02.4

9.4
77

03.1
8.7
91

02.7

13.8
78

03.8
12.7
100

03.5
8.3
100

03.9
7.9
100

Nail in fe. Post 50' Lt Sta 55+70 (approx)

sto + π - E/ev

⁵³
916.13

56 + 35

✓

+ 75

✓

57

✓

FK
KP
JHDec 9, 1959
Clear Cool 25°

87

RT

06.6	05.2	05.3	04.9	04.4	03.5	02.7	02.6
99	11.3	11.2	11.6	12.1	13.0	13.8	13.9
42	27	20	12		15	34	55

06.9	07.0	07.2
96	95	93
60	80	100

04.6	02.9
11.9	13.6
100	76

09.8	09.5	08.2	08.0	07.1	05.9	04.5	03.5
67	70	83	85	94	10.6	12.0	13.0
55	34	23	11		14	35	53

09.7	10.1	10.4
68	64	61
71	87	100

05.2	04.1	03.3
11.3	12.4	13.2
100	87	70

10.8	09.6	09.4	09.3	08.6	07.1	05.7	04.5	03.1
57	69	71	72	79	94	10.8	12.0	11.4
31	20	15	8		15	32	46	66

11.2	11.5	11.9	12.7
53	50	46	38
51	70	88	100

05.4	04.2
11.1	12.3
100	78

Sta + π - Elev
⁵³
 916.73

57+50

✓

TP 9.15 ⁸³ 920.73 4.85 ⁶⁸ 911.28

58

✓

+ 50

✓

Dec. 9, 1959

88

12.5	11.9	10.9	10.8	10.3	9.5	7.8	7.0	6.0
40	46	56	57	62	70	87	95	105
42	24	16	8		8	28	45	64

13.7	14.9	16.0
2.8	4.6	0.5
65	85	100

0.62	0.5.6
10.3	10.9
100	83

14.4	12.9	12.3	11.6	11.0	10.8	10.3	9.4	8.8
64	79	85	92	92	100	105	114	120
56	32	18	7		15	30	50	66

15.7	16.1	17.1	18.3
5.1	4.7	3.7	2.5
73	80	85	100

0.7.8	0.8.0
130	12.8
100	84

15.6	14.2	13.1	12.7	12.3	12.1	11.9	11.8	11.6	10.7
5.2	6.6	7.7	8.1	8.5	8.7	8.9	9.0	9.2	10.1
62	41	19	9		20	41	60	77	100

17.2	17.8	19.8
3.6	3.0	1.0
77	81	100

✓

Sta + π - Elev

⁸³
920.43

59

✓

+50

✓

60

✓

Dec. 9, 1959

89

Rt

14.2	13.1	11.8	11.3	10.7	10.7	10.1	11.9	12.8
6.6	7.7	9.0	9.5	10.1	10.1	10.7	8.9	8.0
73	57	32	16		20	44	66	84

16.0	17.4
4.8	3.4
83	100

12.7
8.1
100

14.8	12.9	12.0	10.9	10.8	10.7	10.0	09.7	10.4
6.0	7.9	8.8	9.9	10.0	10.1	10.8	11.1	10.4
82	55	34	13		15	32	54	78

15.4	16.1
5.4	4.7
93	100

11.6
9.2
100

13.2	12.8	11.9	12.0	10.7	09.8	09.3	08.9	08.6	08.3
7.6	8.0	8.9	8.8	10.1	11.0	11.5	11.9	12.2	12.5
46	27	24	22	13		16	33	56	77

13.7	14.9	17.1
7.1	5.9	3.7
66	82	100

08.3
12.5
100

Sta + $\bar{A}$ - Elev

⁸³
920.43

60 + 32

✓

+ 68

✓

61

✓

TP 13.67 933.30 932.90 1.20 919.23 ⁶³

Dec. 9, 1959

90

RT

14.4

13.6

12.3

11.4

10.8

09.6

08.6

08.2

6.4 7.2 8.5 9.4 10.0 11.2 12.2 12.6
 46 26 12 10 12 31 53

15.1

16.5

19.2

07.8

07.9

5.7 4.3 1.6 13.0 12.9
 6.7 8.4 100 100 76

15.3

14.3

12.9

11.5

10.2

09.4

08.9

09.4

5.5 6.5 7.9 9.3 10.6 11.4 11.9 11.4
 45 22 12 9 14 36 59

16.4

18.0

18.6

20.3

09.8

09.4

4.4 2.8 2.2 0.5 11.0 11.4
 6.5 7.9 8.8 100 100 85

18.1

17.1

16.5

16.5

16.0

14.9

13.4

13.1

12.5

13.2

2.7 3.7 4.3 4.3 4.8 5.9 7.4 7.7 8.3 2.6
 6.8 4.5 2.4 1.1 9 32 39 50 6.5

20.8

23.0

13.5

13.7

0.0 2.2 7.3 7.1
 8.7 100 100 84

Sta + π - Elev

~~932.12~~

~~932.90~~

933.30

61 + 35

+ 50

+ 69

Dec, 9, 1959

91

11

4

8

21.0

21.2

22.0

21.5

20.9

20.2

19.2

18.9

18.2

12.3

12.1

11.3

11.8

12.4

13.1

14.1

14.4

15.1

35

25

13

7

18

31

45

55

22.1

23.2

25.4

18.0

18.3

✓

11.2

10.1

7.9

15.3

15.0

✓

54

71

100

100

78

25.1

24.6

23.8

24.7

25.3

25.1

24.9

24.8

24.5

24.5

8.2

8.7

9.5

8.6

8.0

8.2

8.4

8.5

8.8

8.8

75

49

35

24

11

10

26

43

62

✓

26.6

6.7

100

24.3

90

24.6

8.7

83

26.5

25.6

26.1

26.7

27.0

26.4

26.4

26.3

26.4

6.8

7.7

7.2

6.6

6.3

6.9

6.9

7.0

6.9

56

35

24

10

3

18

35

58

26.8

28.3

25.8

26.3

6.5

5.0

75

70

75

100

100

75

✓

Sta + π - Elev.

~~932.90~~
933.30

61+90

✓

62

✓

TP 5.36 ^{.81} 936.71 1.85 ^{.45} 931.05

+35

✓

BM

6.80 936.78 6.80 930.01 929.98
936.38 929.61 929.58
94.53 728.83 9.25

35 5072

Dec 9, 1959

92

LT		RT	
28.0	27.2	27.6	27.6
5.3	6.1	5.7	5.7
54	35	25	11
28.5	29.8		
4.8	3.5		
74	100		
28.7	28.0	28.3	28.2
4.6	5.3	5.0	5.1
58	37	23	10
27.4	26.8		
5.9	6.5		
59	9		
26.5	26.7		
6.8	6.6		
28	47		
25.8	26.0		
7.5	7.3		
100	84		
30.4	30.7	31.4	31.1
6.4	6.1	5.4	5.7
44	24	11	8
30.9	31.0	31.7	
5.9	5.8	5.1	
67	84	100	
28.2	28.5	29.1	
8.6	8.3	7.7	
100	84	70	

SPIKE IN 18" W. OAK 90' RT STA 62+80

Sta + π - Elev

78
936.38

62+50

✓

+73

✓

63+00

✓

Dec

93

Lt

H

Pt

31.5	31.0	31.5	32.2	31.7	32.0	31.6	31.5	31.4	30.5
5.3	5.7	5.3	4.6	5.1	4.8	5.2	5.3	5.4	6.3
68	44	24	11	8		10	31	48	67
5.0	4.6						7.8	6.7	
87	100						100	82	

31.3	30.9	31.9	31.8	32.3	31.5	31.3	31.0	30.3
5.5	5.9	4.9	5.0	4.5	5.3	5.5	5.8	6.5
62	38	17	7		7	21	43	63

31.5	31.8					32.1		
5.3	5.0					4.7		
85	100					100		

29.6	29.6	29.4	30.6	30.2	29.9	29.5	28.6	27.8	27.2
7.2	7.2	7.4	6.2	6.6	6.9	7.3	8.2	9.0	9.6
76	53	30	13	7		14	33	43	60

29.8
7.0
100

25.0
11.8
100

26.5
10.3
78

30.58 78

Sta + π - Elev.

.78
936.38

63+30

✓

+58

✓

Tp 2.22 929.^{.87}47 9.13 927.^{.165}25

+78

✓

Dec. 8, 1959

94

Lt

Rt

27.9	27.7	27.9	28.2	27.5	27.1	26.2	25.5	24.3
8.9	9.1	8.9	8.6	9.3	9.7	10.6	11.3	12.5
72	50	25	6		13	28	43	58

28.5
8.3
100

22.6
14.2
100

23.4
13.4
76

27.9	27.5	26.6	25.2	24.7	23.7	23.2	22.0	21.4
8.9	9.3	10.2	11.6	12.1	13.1	13.6	14.8	15.4
75	43	19	8		17	20	43	90

28.3
8.5
100

21.3
15.5
100

nail in fence post 8' Lt sta 63+58

26.7	26.0	25.7	24.9	24.1	23.6	23.3	22.9	22.2	21.7	20.4
3.2	3.9	4.2	5.0	5.8	6.3	6.6	7.0	7.7	8.2	9.5
85	70	55	34	9		13	31	51	74	83

27.2
2.7
100

20.0
9.9
100

sta + π - Elev.
^{.87}
 929.47

63+91

✓

TP 8.33 ^{.98} 935.58 2.22 ^{.65} 927.25

64

✓

+50

✓

BM 0.06 935.98 0.06 ^{.92} 935.52 935.91
 935.51

FX
RG
HP
JH

Dec 9, 1959
Dec 10, 1959 95

1+

R1

25.6	24.8	24.2	23.6	23.4	22.9	22.1	21.5	20.7
43	51	57	63	65	70	78	84	92
75	53	33	13		16	32	59	81

26.8

3.1
100

20.2
9.7
100

Nail in Fe Post 8' 1" Sta 63+58

24.6	24.0	23.8	23.2	22.6	21.8	21.2
11.4	12.0	12.2	12.8	13.4	14.2	14.8
51	32	16		19	42	62

25.0

11.0
70

26.6

9.4
100

20.0
16.0
100

20.9
15.1
84

25.9	25.7	25.5	25.0	24.7	24.7	24.4	23.2	23.9
10.1	10.3	10.5	11.0	11.3	11.3	11.6	12.8	12.1
61	48	37	23		14	26	30	38

26.1

9.9
82

26.7

9.3
100

22.8

13.2
100

22.6

13.4
90

21.1

14.9
78

22.8

13.2
63

23.0

13.0
49

Top Hyd Burns & Mc Knight

Sta + π - Elev

..97
935.57

65

✓

+50

✓

+77

✓

Dec. 10, 1959 96
Clear Cool 23°
RT

LT

28.4	27.0	26.3	26.2	25.5	25.7	25.6	25.4	23.5
7.6	9.0	9.7	9.8	10.5	10.3	10.4	10.6	12.5
100	69	38	19		16	32	53	60

25.2	24.6	25.0
10.8	11.4	11.0
100	76	66

28.7	28.4	28.0	27.3	27.3	27.1	27.0	27.0	26.7
7.3	7.6	8.0	8.7	8.7	8.9	9.0	9.0	9.3
81	63	43	17		14	29	51	65

29.1
6.9
100

27.1
8.9
100

26.7
9.3
84

29.4	29.4	29.2	29.4	28.9	28.1	27.7	27.5	27.4
6.6	6.6	6.8	6.6	7.1	7.9	8.3	8.5	8.6
83	63	44	33	14	19	36	57	73

29.2
6.8
100

28.6
7.4
100

27.7
8.3
89

Sta + π - Elev

935.⁹⁷57

66

✓

+34

✓

+59

✓

Dec. 10, 1959

97

LT

RT

29.8	29.8	29.8	29.5	29.5	29.1	28.3	27.8	28.4
6.2	6.2	6.2	6.5	6.5	6.9	7.7	8.2	7.6
85	65	41	18		13	31	49	74

29.6
6.4
100

29.6
6.4
100

30.0	30.5	30.4	29.9	29.7	28.9	28.6	28.4	29.0	29.7
6.0	5.5	5.6	6.1	6.3	7.1	7.4	7.6	7.0	6.3
88	70	59	37	18		21	44	68	85

29.8
6.2
100

30.3
5.7
100

30.0	30.1	29.9	29.3	28.7	28.5	28.6	29.2	29.7
6.0	5.9	6.1	6.7	7.3	7.5	7.4	6.8	6.3
91	71	46	18		20	44	73	87

30.0
6.0
100

30.4
5.6
100

Sta	+	T	-	Elev
-----	---	---	---	------

		97 935.57		
--	--	--------------	--	--

66+71				
-------	--	--	--	--

✓				
---	--	--	--	--

+79				
-----	--	--	--	--

✓				
---	--	--	--	--

67+91	Burn			
-------	------	--	--	--

✓				
---	--	--	--	--

FX
RG
HP
LG
JH
JS

Dec. 10, 1959

98

LT

2

RT

30.2	30.0			29.0	28.6	28.6	29.3	29.7
5.8	6.0			7.0	7.4	7.4	6.7	6.3
88	100			18	45	71	90	

32.1	32.5	30.6	31.3	32.5	32.8	32.5	30.2	28.7	28.7	28.8
3.9	3.5	5.4	4.7	3.5	3.2	3.5	5.8	7.3	7.3	7.2
35	18	14	10	5		9	16	20	42	68

32.3	32.7	33.1	33.3				30.6	29.7
37	33	2.9	2.7				5.4	6.3
48	74	89	100				100	87

32.7	32.6	31.4	32.5	32.3	31.9	31.6	29.4	28.9
3.3	2.4	4.6	3.5	3.7	4.1	4.4	6.6	7.1
34	20	16	8		13	20	31	44

32.7	32.7	33.2				30.3	29.6	29.0
3.3	3.3	2.8				5.7	6.4	2.0
61	83	100				100	82	65

Sta + π - Elev

^{.97}
~~935.57~~

66+93 Gutter

67

3.9

32.07

+07.29 $\pm$ Burns

✓

+22 Gutter

✓

Dec. 10, 1959 99

17

17

37	4.0	4.4	3.8	4.0	4.1	4.4	5.0	7.1	7.1
52	29	15	9		10	21	29	39	44
32.3	32.0	31.6	32.2	32.0	31.9	31.6	31.0	28.9	28.9

32.5
3.5
29

32.7
3.3
100

30.3
5.7
100

29.6
6.4
82

29.0
7.0
65

30	33	3.7	4.2	3.8	3.8	4.2	4.7	5.7	6.0
78	45	24	17	12		12	25	47	62
33.0	32.7	32.3	31.8	32.2	32.2	31.8	31.3	30.3	30.0

33.2
2.8
100

33.7
2.3
150

31.4
4.6
100

30.1
5.9
76

3.3	3.4	4.0	3.7	3.8	3.9	4.7	5.5	5.3
59	30	20	10		22	27	52	72
32.7	32.6	31.0	32.3	32.2	32.1	31.3	30.5	30.7

33.0
3.0
87

33.0
3.0
100

31.9
4.1
100

31.1
4.9
88

Sta + π - Elev

^{.97}
935.57

67+24

✓

+ 40.27 Property Line

✓

+ 41

2.59 33.38

+ 48

✓

^{.94}
947.86

BM

11.95

947.46

0.03

^{.94}

935.54

(935.51)

Dec. 10, 1959 100

LT

RT

32.6	32.3	32.0	32.3	32.2	31.9	31.2	30.4	30.8
3.4	3.7	4.0	3.7	3.8	4.1	4.8	5.6	5.2
25	23	20	11		23	28	54	72

33.0	32.7	33.1	32.9
3.0	3.3	2.9	3.1
36	57	91	100

31.8	31.4
4.2	4.6
100	91

33.2	33.4	33.2	33.0	33.0	32.9	33.0	32.1	31.2
2.8	2.6	2.8	3.0	3.0	3.1	3.0	3.9	4.8
53	36	15	14		9	14	27	31

33.2	33.1
2.8	2.9
79	100

33.1	32.1	31.5	30.9	31.0
2.9	3.9	4.5	5.1	5.0
100	81	67	58	49

ctr 3' MH 18' LT

33.6	34.0	33.9	33.5	33.5	33.3	33.5	32.2	31.9	32.8
2.4	2.0	2.1	2.5	2.5	2.7	2.5	3.8	4.1	3.2
46	30	16	15		10	25	37	58	77

33.0	32.5	31.0	31.0
3.0	3.5	5.0	5.0
57	70	82	100

34.1
1.9
100

Top Hyd N.H. Cor Burns & Mc Knight

Sta + π - Elev

⁻⁸⁶
947.46

67+60

✓

+68

12.46 35.40

+75

✓

68

✓

4 Dec. 10, 1959

101

Lt

RI

33.6	34.6	34.7	34.3	34.4	34.0	34.3	33.8	33.2
14.3	13.3	13.2	13.6	13.5	13.9	13.6	14.1	14.7
42	33	155	15		10	10.5	17	26
32.1	31.3	32.1	32.1		35.8	34.6	33.6	33.1
15.8	16.6	15.8	15.8		12.1	13.3	14.3	14.8
55	72	87	100		100	89	66	44
CH. MH	18.21							
34.8	35.9	35.9	35.4	35.7	35.3	35.6	35.0	
13.1	12.0	12.0	12.5	12.2	12.6	12.3	12.9	
37	28	17	15		10	11	23	
33.6	33.6	34.1			37.2	35.9	35.1	34.8
14.3	14.3	13.8			10.7	12.0	12.8	13.1
53	78	100			100	75	53	35
36.7	38.1	38.1	37.7	38.2	37.6	37.9	37.0	36.4
11.2	9.8	9.8	10.2	9.7	10.3	10.0	10.9	11.5
40	25	18	10		10	11	21	38
36.5	36.9	37.0	37.0		38.0	37.5	37.1	36.6
11.4	11.0	10.9	10.9		9.9	10.4	10.8	11.3
58	73	85	100		100	87	70	54

Sta + π - Elev

^{.86}
947.46

68+24

✓

+51

✓

+72

✓

Dec. 10, 1959 102

14

15

38.8	38.6	39.9	39.8	39.5	40.0	39.5	39.7	39.1	38.3	37.1
91	93	80	81	84	79	84	82	88	96	108
59	48	30	17	16		9	10	18	22	34

38.1	38.3	39.5	39.4		38.4	37.7	37.4		37.2	
98	96	84	85		95	102	105		107	
67	81	88	100		100	87	70		53	

40.3	40.3	42.4	42.4	41.8	42.2	41.9	42.2	41.4	41.5	
76	76	55	55	61	57	60	57	65	64	
50	38	30	18	16		9	10	14	19	

40.4	40.1		38.1	37.8	37.2	37.2	37.5	38.2		
75	78		98	101	107	107	104	97		
75	100		100	93	73	60	38	26		

40.6	44.0	44.2	43.7	44.0	43.8	44.0	43.4	38.9	38.1	
73	39	37	42	39	41	39	45	90	98	
42	33	17	16		9	10	18	27	36	

40.6	40.0	39.3		37.2	36.8	37.1	37.5	37.6		
73	79	86		107	111	108	104	103		
56	71	100		100	81	67	51	38		

Sta + π - Elev

^{.86}
947.46

69

✓

✓

TP 12.55 ^{959.05} 958.65 1.36 [^] 946.10 ^{.150}

+28

✓

+67

Dec 10, 1959 103

46.4 46.8 46.0 46.4 46.4 45.9 46.3 45.9 45.4 40.3
 1.5 1.1 1.9 1.5 1.5 2.0 1.6 2.0 2.5 7.6
 33 18 16 8 9 10 13 19 29

41.0 40.1 39.1 38.8 36.4 36.6 37.5 38.4 ✓
 6.9 7.8 8.8 9.1 11.5 11.3 10.4 9.5
 45 53 68 78 100 79 63 45

35.8 12.1 10.1
 100 90

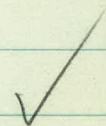
stone 6 11 sta 69

48.8 49.1 48.5 48.8 48.8 48.3 48.5 48.1 46.4
 10.3 10.0 10.6 10.3 10.3 10.8 10.6 11.0 12.7
 32 17 16 8 8 9 19 22

48.1 46.1
 11.0 13.0
 36 39

51.8 52.2 52.3 51.8 52.1 52.0 51.5 51.8 51.0 47.1
 7.3 6.9 6.8 7.3 7.0 7.1 7.6 7.3 8.1 12.0
 35 27 17 15 7 9 9.5 19 25

48.7
 10.4
 40



Sta	+	π .	-	Elev
		959.05		
		958.65		

70

✓

+29

972.08

TP

13.15

971.68

0.12

958.93
958.53

+67

71

+26

+48 Pull Box 15' R/L 5.56

104

✓

✓

✓

64.3	61.8
7.8	10.3
35	40

Sta + π - Elev

972.08
~~971.68~~

71+53

✓

178

72

✓

+17

BM 6.32 $\cdot 165$ 975.25 2.73 $\cdot 969.35$ 968.95 (968.93)

Dec 10, 1959

105

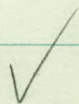
2+

RT

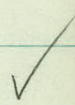
67.2	67.8	67.9	67.7	68.1	68.2	67.9	68.1	67.4	64.6
49	43	42	44	40	39	42	40	47	7.5
32	29	16	15	8	9	10	17	20	

66.8
5.3
36

63.6
8.5
41



66.7	69.6	70.0	70.1	69.9	70.0	69.8	70.0	69.0	65.8
54	2.5	2.1	2.0	2.2	2.1	2.3	2.1	3.1	6.3
38	34	25	16	15	9	10	20	25	



70.6	70.9	70.3	70.6	70.7	70.3	70.4	69.6	59.9
1.5	1.2	1.8	1.5	1.4	1.8	1.7	2.5	12.2
28	18	14	8	9	10	20	35	

70.3
8
34

66.7
5.4
39

63.4
8.7
100

61.9
10.2
82

61.7
10.4
61

59.9
12.2
52

58.7
13.4
39



66.7	70.1	70.5	69.9
54	20	16	22
39	33	16	15

70.5
1.6
8

70.5
1.6
9

70.4
1.7
11

70.7
1.4
18

70.5
1.6
32

62.2
9.9
36

61.1
11.0
36



Brass Plug ± VBL US #12 McKnight

100 79 59 45 12.5 38

Sta + π - Elev

c .65
975.25

72+29

✓

+41

✓

+52

✓

Dec. 10, 1959

106

BT

14

66.1	70.3	70.3	69.9	70.5	70.5	70.7	67.0	68.5	71.0
96	54	54	58	52	52	50	87	22	47
39	32	18	16	10	25	33	47	71	

63.6	57.7	57.26
12.1	18.0	
42	54	

73.5	73.3
22.4	24
100	97

63.4	69.8	69.6	69.7	70.4	70.6	71.1	71.8	72.9	74.0
12.3	5.9	6.1	6.0	5.3	5.1	46	39	2.8	1.7
43	32	19	13	15	26	38	53	79	

60.7
15.0
64

75.0
0.7
100

60.3	64.4	68.0	69.2	70.3	71.0	72.0	72.58	72.65
15.4	11.3	7.7	6.5	5.4	4.7	3.7	30.7	3.00
100	71	42	20	18	38	54	60	

conc

74.69	74.05
0.96	1.60
100	87

conc

Sta + π - Elev

⁶⁵
~~975.25~~

72+59.5

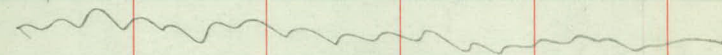
✓

+70.7 on ϕ of F.B.L. US#12

✓

BM

969.33
6.32 968.93 (968.93)



TP 3.30 ^{1.80}
~~949.50~~ 946.50
946.10

69+28

+67

Dec. 10, 1959

107

67.7	68.0	68.5	69.0	69.98	70.26	71.54	72.99	74.60
8.0	7.7	7.2	6.7	5.67	5.39	4.11	2.66	1.05
57	47	37	26		10	36	67	100
Concrete								

67.0	65.0	63.7						
8.7	10.7	12.0						
72	90	100						

65.15	65.46	66.54	67.62	68.61	69.75	71.13	72.20	73.44
10.50	10.19	9.11	8.13	7.04	5.90	4.52	3.45	2.21
100	94	69	48	25		29	51	77
All concrete								

74.58
1.07

Brass Plug & WBL VS #12 + Mo Knight

stone 6' 11" Sta 69

38.5	36.8	36.0	34.8
11.3	13.0	13.8	15.0
37	59	75	100
35.7	33.8	34.1	33.9
14.1	16.0	15.7	15.9
44	57	78	100

Sta	+	π	-	Elev
-----	---	-------	---	------

949.80
~~949.40~~

70 + 00

+ 29

+ 67

71

+ 26

B. M.

13.89

91
935.51

935.51

~~TP~~

~~946.10~~

Dec. 10, 1959

108

R

R+

37.0	34.9	34.7	35.2	
12.8	14.9	15.1	14.6	✓
45	53	70	100	✓
38.2	37.2	37.4	36.8	✓
11.6	12.6	12.4	13.0	12.7
48	54	66	88	100
41.4	39.9	40.0	40.1	✓
8.4	9.9	9.8	9.7	✓
49	70	80	100	
44.0	43.2	41.1	42.2	✓
5.8	6.6	8.7	7.6	
48	63	83	100	
45.8	45.0	45.9	45.6	✓
4.0	4.8	3.9	4.2	3.0
47	53	69	86	100

Top Hyd. N.W. Cor Burns

stone 6' 2" sta 69

Sta	+	π	-	Elev.
BM	3.08	^{.41} 972.01		^{963.35} 968.93
TP1	0.32	^{.67} 963.27	9.06	962.95

7/453

+78

TP	9.96	^{973.31} 972.91	0.32	^{963.35} 962.95
BM			3.97	^{969.34} 968.94
				968.93

RG
KP
JS

Rt

Dec 11, 1959

109

Brass Plug $\pm$ W.B.L. US#12 & McKnight

top cfr. culvert sta 72+17 38' Rt

54.2	49.5	50.7	50.5	51.7	53.2	52.9
9.5	14.2	13.0	13.2	12.0	10.5	10.8
32	39	42	52	66	83	100

59.7	55.7	56.4	57.9	57.9
4.0	8.0	7.3	5.8	5.8
33	39	61	86	100

top culvert

brass plug US#12 WBL & McKnight

Sta	+	π	-	Elev
BM	6.89	942. ^{.80} 40		935.51

TP

69+28

+67

70

+29

+67

TP	13.81	952. ^{.35} 95	4.26	938. ^{.54} 14
----	-------	------------------------	------	------------------------

71

R6
JH
FK

Lt.

Dec 10, 1959 110
2

Top Hyd N/W Cor McKnight $\frac{1}{2}$ Burns Ave

33.6	34.3	34.5	35.3	37.6	41.4
9.2	8.5	8.3	7.5	5.2	1.4
100	90	79	71	55	46

✓

31.3	31.8	32.2	33.7	38.1
11.5	11.0	10.6	9.1	4.7
100	82	73	66	56

✓

30.3	30.5	32.5	34.5	38.5
12.5	12.3	10.3	8.3	4.3
100	86	75	68	61

✓

30.4	30.7	33.4	36.9	40.9
12.4	12.1	9.4	5.9	1.9
100	90	80	68	62

✓

31.9	33.4	35.9	41.0
10.9	9.4	6.9	1.8
100	86	76	67

✓

38.4	38.5	39.9	45.1
14.0	13.9	12.5	7.3
100	88	74	63

✓

Sta	+	π	-	Elev
		952.35		
		951.95		

71+26

+53

+78

72

		962.06		949.53
TP	13.03	961.66	3.32	948.63

+17

+29

Dec. 10, 1959 111

1A
39.8
12.6
100
82
40.1
12.3
82
43.7
8.7
70
48.9
3.5
61

✓

41.0
11.4
100
41.3
11.1
83
43.4
9.0
75
45.8
6.6
67
49.8
2.6
60

✓

43.6
8.8
100
44.7
7.7
86
45.6
6.8
74
48.5
3.9
64
50.7
1.2
60

✓

47.2
5.2
100
48.7
3.7
79
50.6
1.8
65
51.7
0.7
63
52.4
0.0
61
Rock

✓

50.0
12.1
100
51.5
10.6
80
54.2
2.9
61
56.8
5.3
54
61.0
1.1
48

✓

54.6
10.5
100
53.9
8.2
71
57.3
4.8
55
60.7
1.4
48

✓

Sta + π - Elev.

962.06
961.66

72+41

TP 11.76 ^{.46} 972.06 1.36 ^{.70} 960.30

BM 3.11 969.35 968.95 868.93

Dec 10, 1959 112

54.5

7.6

100

47

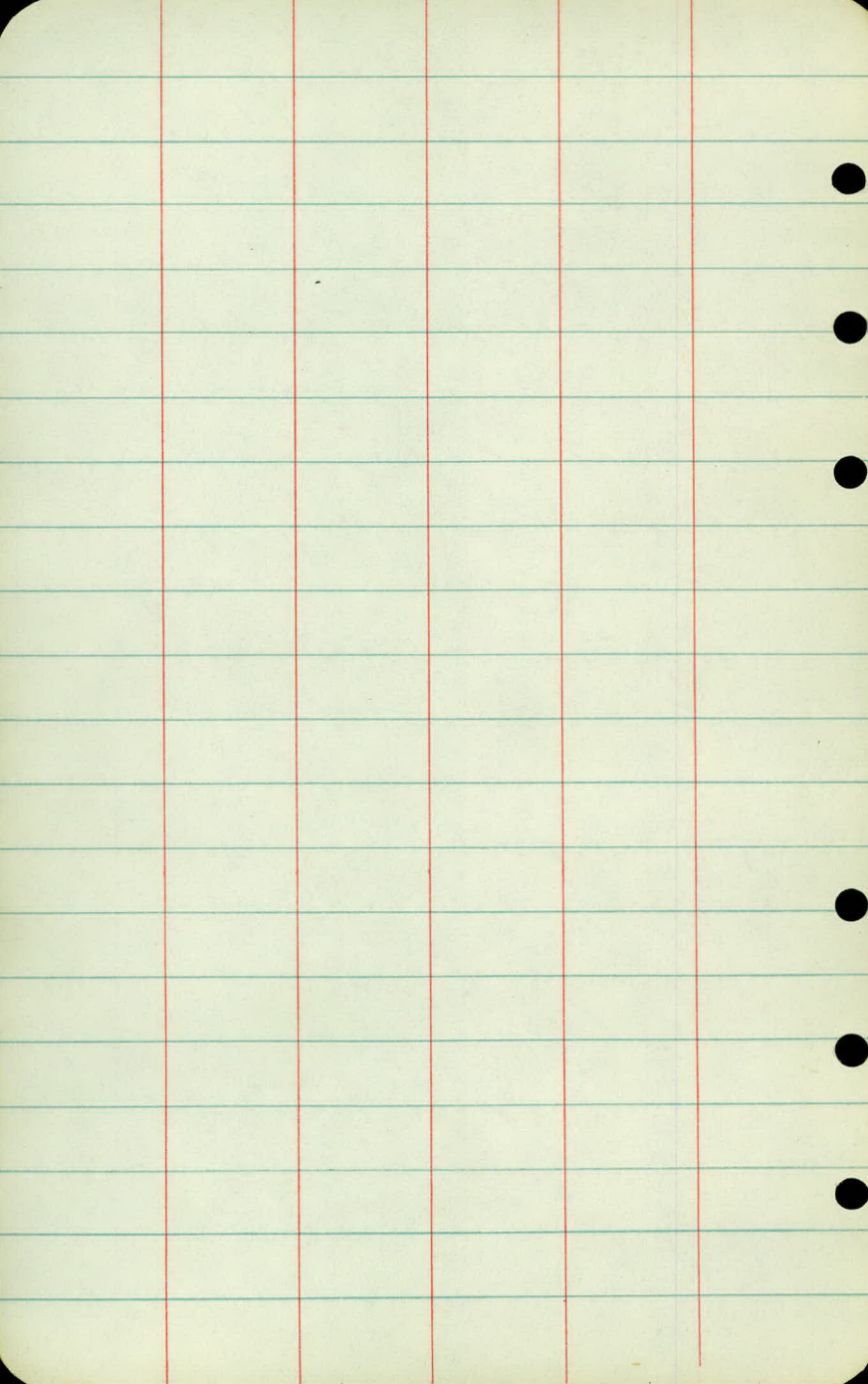
57.0

5.1

82



Brass Plug & W. BL US #12 & No Knight



FK
RG
JS
JL
JH

March 31, 1960
Overcast 26°

113

Burns Ave

x-sections

30

NPL

spike

W.P.L.
Suburban Ave

N

0+00



± Mo Knight

Rec. 3/31/60

Sta	+	π	-	Elev
BM	5.59	941.10		935.51

0+50

✓

1

✓

+50

March 31, 1960

114

LT

RT

Top Hyd NW. Cor Burns & McKnight

29.4	31.8	32.2	31.9	32.3	32.3	32.5	32.7	32.0
11.7	9.3	8.9	9.3	8.8	8.8	8.6	8.9	8.4
36	29	16	15	14	15	17	31	50

29.4	29.6	29.8
11.7	11.5	11.3
48	68	75

29.7	32.6	32.8	32.3	32.8	32.7	32.9	32.9	31.0	31.7
11.4	8.5	8.3	8.8	8.3	8.4	8.2	8.2	10.1	9.4
37	29	16	15	15	16	31	38	50	

29.6	29.3
11.5	11.8
56	75

29.9	33.5	33.5	33.0	33.3	33.1	35.0	36.2
11.2	7.6	7.6	8.1	7.8	8.0	6.1	4.9
37	29	16	15	15	31	50	

29.6	29.2
11.5	11.9
57	75

Sta + π - Elev

941.10

2 + 00

✓

+ 50

✓

+ 69

3

TP 13.29 953.11 1.28 939.82

March 31, 1960

115

Lt

RT

34.2	34.4	33.7	34.0	33.9	35.3	36.5
6.9	6.7	7.4	7.1	7.2	5.8	4.6
29	16	15		15	30	50

30.6	30.2	30.1
10.5	10.9	11.0
38	53	75

32.9	35.5	36.1	34.9	35.2	35.0	35.6	36.4	37.4
8.2	5.6	5.0	6.2	5.9	6.1	5.5	4.7	3.7
36	29	35	15		14	16	35	50

32.8	35.6
8.3	5.5
56	75

35.9	35.9	35.6	35.6	35.9	35.7	36.7	37.5
5.2	5.2	4.5	5.5	5.2	5.4	4.4	3.6
50	32	16	14		14	25	50

37.4	37.3	37.6	37.0	37.3	37.0	38.6	38.8	40.7
3.7	3.8	3.5	4.1	3.8	4.1	3.5	2.3	0.4
50	38	16	14		14	35	44	49

Sta	+	π	-	Elev.
-----	---	-------	---	-------

953.11

3+50

✓

4+00

✓

+50

5

TP	7.48	957.99	2.60	950.51
----	------	--------	------	--------

BM	2.35	957.99	2.35	955.64
----	------	--------	------	--------

TP	0.27	946.05	12.21	945.78
----	------	--------	-------	--------

BM			10.54	935.51
----	--	--	-------	--------

(935.51)

± March 31, 1960

1+

Rt

116

44.1	40.0	39.8	39.4	39.8	39.4	39.6	40.5	42.1
9.0	13.1	13.3	13.7	13.3	13.7	13.5	12.6	11.0
33	25				15	16	29	48

44.5	43.9	46.6		42.3
8.6	9.2	6.5		10.8
41	48	75		56

49.5	43.8	43.1	42.7	43.3	42.9	43.5	43.6	42.4
3.6	9.3	10.0	10.4	9.8	10.2	9.6	9.5	10.7
39	29	16	14		14	16	31	50

49.9
32
50

46.5
6.6

49.4
3.7

Top Hyd N.W. Cor Suburban & Burns

Top Hyd N.W. Cor Burns & McKnight

Sta + π - Elev.

+

不

—

Lev.

BM 3.18 905.67 902.49

5.50 900.2

54 10.41 95.26 94.44
9526
.8

TP 1.58 904.08 903.31
409
.78

53 3.30 02.37 02.3

+12 4.27 01.2

+22 5.40 900.27 99.56
7

12.89
9526
9448
95.48
78

Begin Spotting
x-sect 14+72

Spot to 75-80'

1
Check Fleus.
Sta 24 to 34
McKnight Rd

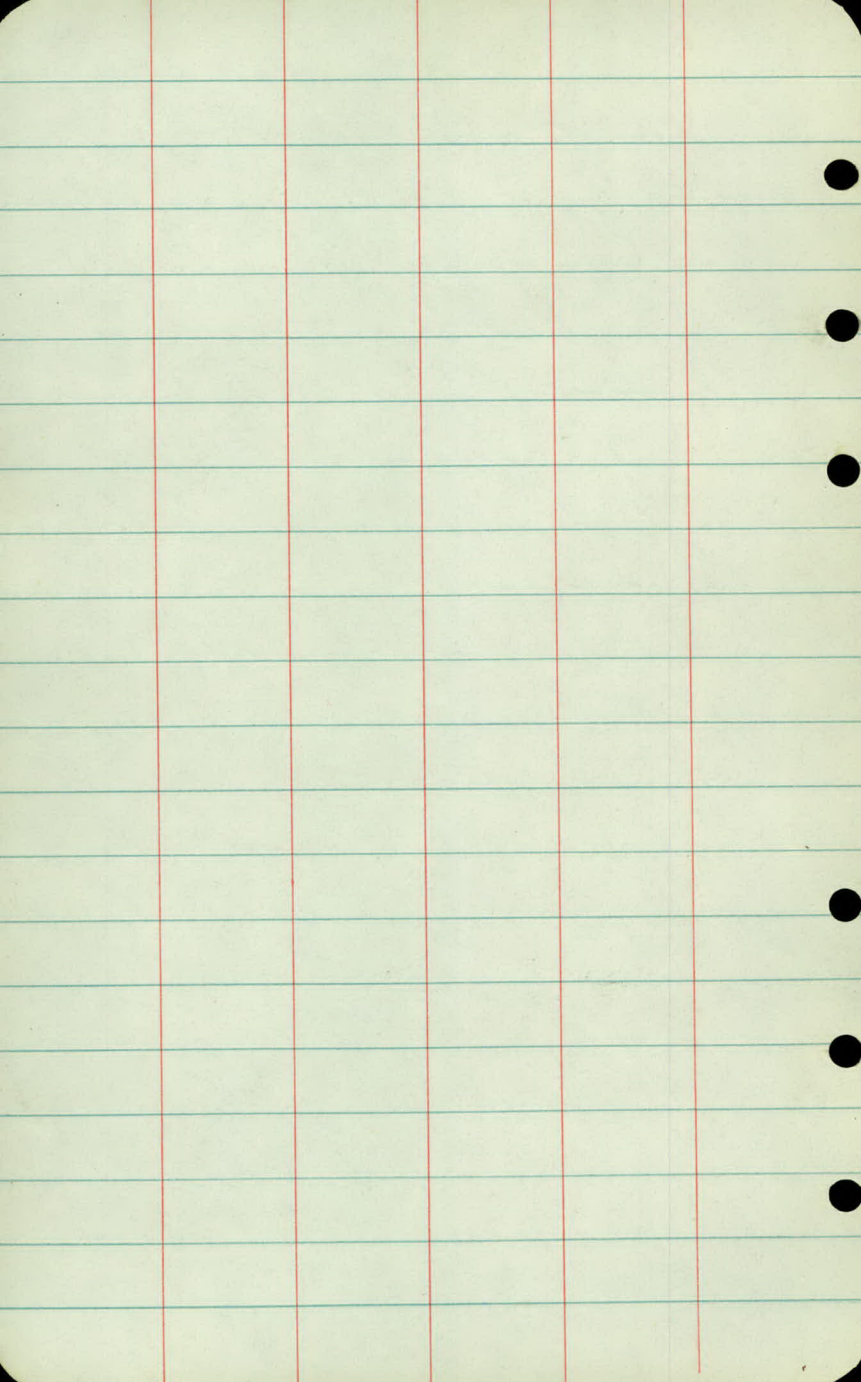
A. Clark
checked O.K.
12-10-59

✓ Goldie

Sta	+	Σ	-	Elev
B.M.	0.77	940.64		939.87
24+00			7.1	33.5
25			13.0	27.6
T.P.	0.56	930.92	10.28	930.36
26			6.8	24.1
27			5.7	25.2
T.P.	9.97	940.70	0.19	930.73
28			10.4	30.3
29			6.5	34.2
T.P.	12.59	950.10	3.19	937.51
30			11.6	38.5
31			3.8	46.3
32			2.1	48.0
33			2.4	47.7
34			2.4	47.7
B.M.			1.38	948.72

2
spk. in 15" oak Rt. sta. 23+60±

spk. in pp. Lt sta 34+25

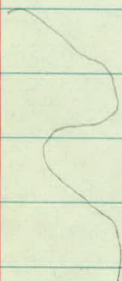


1

Battle Creek Line

for

New Channel



1+00

→ N

0+00 = ~~E~~ McKnight
← Sta 53+91

Sta	+	x	-	Elev
BM	0.44	903.33		(902.89)
T.P.	3.62	898.23	8.72	894.61

1 +00

+25

+50

✓

+62

✓

FK
JL
WM
JH

July 25, 1960
Clear 80°

2

Lt.

RT

Top Mont Sta 52 + 54.32

886	90.0	938	943	941	942	945	946
2.6	8.2	4.4	3.9	4.1	4.0	3.7	3.7
44	41	36	23		15	32	50

Stream

89.5	89.9	94.3	93.9	93.9	94.1	94.2	
9.7	8.3	3.9	4.3	4.3	4.1	4.0	3.7
53	51	45	22		20	36	50

93.5	93.8	92.4	93.4	93.6	93.6	94.9	95.0
4.7	4.9	5.8	4.8	4.6	4.6	3.3	3.2
50	23	15	11		17	46	50

Stream

	93.5	92.0	89.0	88.4
→	4.7	6.2	9.2	9.8
	82	91	100	107

90.2	91.3	91.6	92.9	93.4	93.7	94.3	95.0
8.0	6.9	6.6	5.3	4.8	4.5	3.9	3.2
51	39	26	14		15	32	50

← Drainage

Stream

89.8	91.8	91.2	87.8
→	8.4	6.4	7.0
	60	68	74

Sta + π - Elev.

898.23

1+75

✓

2

✓

✓

+50

✓

July 25, 1960

3

927
927

927

931

930

937

937

940

947

55 50 51 47 45 45 36 35
55 41 27 13 15 33 50

891

87.6

9.1
71

10.6
73

Stream

935

938

939

937

936

937

940

943

4.7 4.4 4.3 4.5 4.6 4.5 4.2 3.9
69 58 34 14 18 41 50

884

884

9.8
78

10.8
80

930

930

930

934

936

5.2 5.2 5.2 4.8 4.6
84 63 45 13

930

929

926

923

5.2 5.3 5.6 5.9
100 123 151 159

88.2

88.2

11.8

10.0

167

164

Stream

Sta + π - Elev.

898.23

2+90

✓

55

2.1

896.1

✓
(96.2)

July 25, 1960

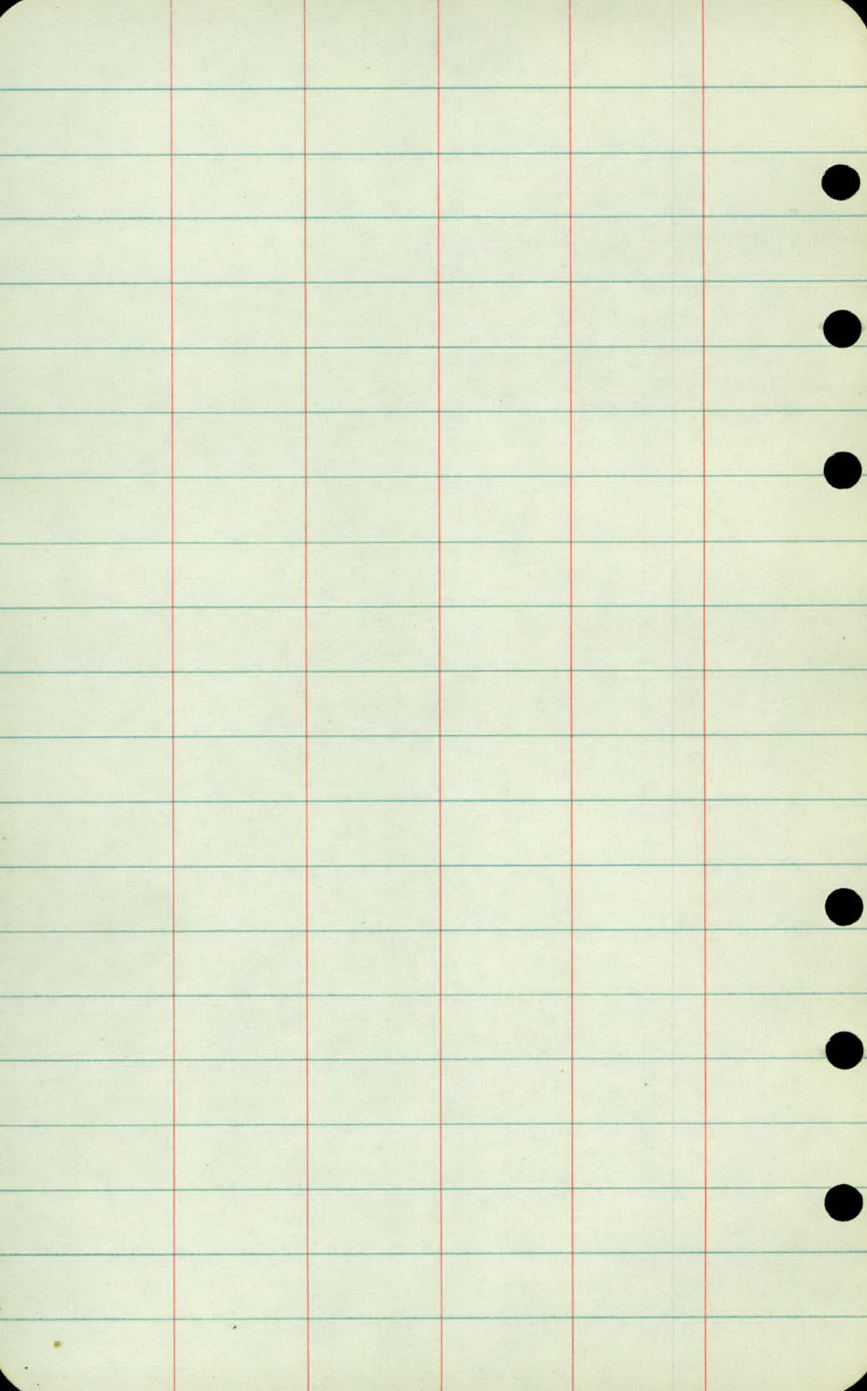
21

~~2~~ 4

5.4 5.8 5.9 5.6 4.9 4.0 2.9
140 100 89 67 44 19

→ 5.4 6.8 9.8 11.8
166 188 197 202

~~2~~



1
Ditch Locations

stadia

OBJECT

HI = 909.8

AZ.

STADIA

X at sta 54+00

to sta 59+00

0°00'

Battle Creek

176°10'

"

"

221°10'

"

"

217°20'

"

"

225°20'

"

"

242°10'

"

"

239°20'

"

"

226°40'

"

"

227°20'

"

"

236°10'

"

"

246°50'

"

"

236°30'

"

"

226°50'

"

"

235°30'

"

"

235°30'

232°40'

FX
JS
D12
JH

INVERT.
ANGLE

HEAD
EQUIV.

March 17, 1960
Clear Cool 30°
ROD
DIEF.

ELEV. 2

H1 = 5.2
900.8

895.6

29

11.8

89.0

45

12.2

88.6

61

12.1

88.7

94

12.6

88.2

110

12.6

88.2

153

13.3

87.5

158

12.8

88.0

180

13.0

87.8

194

13.6

87.2

206

13.6

87.2

232

13.8

87.0

285

14.1

86.7

315

14.4

86.4

380

14.8

86.0

475

15.6

85.2

H.I. 900.8

OBJECT

AZ.

STADIA

E Battle Creek

" " 119°10'

" " 75°40'

" " 96°20'

" " 88°00'

" " 89°40'

W Battle Creek At Bridge 83°35'

At Sta 49+00

to Sta 40+00 180°00'

E Ditch 180°00'

" " 253°45'

" " 269°30'

" " 265°00'

" " 270°40'

" " 273°00'

" " 275°50'

" At Culvert W. End 276°20'
Over Sewer

March 19 1960

Clear And Cool 30°

3

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
51'			11.3		89.5
86'			11.0		89.8
129			10.8		90.0
161			10.8		90.0
189			10.6		90.2
274			8.9		91.9
			41.5.25		98.3
				903.5	
65'			11.8		91.7
98			13.0		90.5
165			14.1		89.4
218			14.2		89.3
288			14.5		89.0
358			15.3		88.2
402			15.8		87.7
440			17.3		86.2

OBJECT

AZ.

STADIA

At Culvert E. END

④ Ditch over Sewer $279^{\circ}10'$ " " $158^{\circ}00'$ " " $151^{\circ}25'$ " " $145^{\circ}30'$ " " $136^{\circ}00'$ " " $127^{\circ}20'$ " " $123^{\circ}00'$

March 17, 1960 4

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

463			14.7		85.8
120			11.9		91.6
226			11.6		91.9
253			10.2		93.3
285			9.4		93.8
327			9.2		94.3
415			8.4		95.1

OBJECT

AZ.

STADIA

Check Elev. of Culvert at
Lake & Types of Culvert
Stadia of High ground at
N.E. Cor. of Property
Elev of NE Cor.

22 AUG 1960 ①

J.H. K clear - Hot

H.G. 1

D.E. 1

F.S. □

Final for Berm Sect.
X-sections

McKnight RD

Upper Afton to Burns

reduced: 29 August 1960 K.P.

② STA	+	Δ	-	ELEV
BM	5.92	919.97		914.05
BM				935.91
39+72				
+82				
40+00				
+50				
+87				
41+00				
+50				
42+00				
50				

LT

E

22 Aug 60

RT

(3)

SPIKE in 24" ELM 130' RT STA 39+75

TOP HYD N.W. COR BURNS AND McKnight

12.1	16.1	15.8	12.1
7.9	3.9	4.2	6.6
62.7	46.3	23	17.7
top	top	top	top
12.9	16.1	15.6	12.6
7.1	3.9	4.4	7.4
58.1	46	24	17
11.9	15.9	15.3	11.6
8.1	8.1	27	8.4
58.1	47	24	16.1
12.1	15.1	15.1	12.1
6.3	4.6	4.9	7.3
53	47	22	18.1
14.1	15.1	14.9	12.1
5.6	4.6	5.1	6.3
51.5	47	24	19
14.0	15.1	14.8	12.1
6.0	4.9	5.2	6.3
52	48	22	20
13.3	14.2	14.2	12.5
6.7	5.8	5.8	6.5
53	48	25	20
12.1	13.4	13.5	13.1
7.6	6.6	6.5	6.9
52	48.6	24	21

Sta ④ + A - El,

42+50 919.97

TP 7.99 911.98

1.42 913.40

43

+30

+61

44+00

+50

45+00

+50

+75

$\begin{matrix} 11.4 & 12.6 & 7.6 & 2.3 & \text{E} \\ 104 & 104 & 104 & 104 & \\ 8.6 & 7.4 & 7.5 & 7.7 & \\ 52 & 49 & 25 & 21.6 & \checkmark \end{matrix}$

R +

(5)
 22 Aug 60

$\begin{matrix} 11.1 & 11.9 & 11.1 & 11.7 & \checkmark \\ 2.3 & 1.5 & 1.7 & 1.7 & \\ 52.8 & 48 & 25 & 22 & \end{matrix}$

$\begin{matrix} 11.2 & 11.4 & 11.4 & 11.8 & \\ 22 & 2.0 & 2.0 & 1.6 & \checkmark \\ 52 & 48 & 25.6 & 20 & \end{matrix}$

$\begin{matrix} 9.2 & 10.1 & 10.8 & 9.8 & \\ 4.2 & 2.7 & 2.6 & 3.6 & \checkmark \\ 54 & 48 & 26 & 18 & \end{matrix}$

$\begin{matrix} 1 & 10.0 & 10.2 & 08.4 & \\ 09.1 & 3.4 & 3.2 & 5.0 & \checkmark \\ 52.3 & 48 & 26.5 & 18 & \end{matrix}$

$\begin{matrix} 08.9 & 09.3 & 09.0 & 07.9 & \\ 4.5 & 4.1 & 4.4 & 5.5 & \checkmark \\ 50.2 & 47 & 26.9 & 20.5 & \end{matrix}$

$\begin{matrix} 08.5 & 08.4 & 08.4 & 07.5 & \\ 4.9 & 5.0 & 5.0 & 5.9 & \checkmark \\ 49.7 & 48 & 27 & 23 & \end{matrix}$

$\begin{matrix} 06.6 & 07.6 & 07.4 & 06.5 & \\ 6.8 & 5.8 & 6.0 & 6.9 & \checkmark \\ 52 & 49 & 28 & 22 & \end{matrix}$

$\begin{matrix} 06.3 & 07.3 & 07.0 & 06.5 & \\ 71 & 6.1 & 6.4 & 6.9 & \checkmark \\ 53 & 48 & 27.6 & 22 & \end{matrix}$

⑥

+

*

-

46+00

913,40

+50

+75

47+00

TP

1.77

905.86

9.31

904.09

+50

+88

+91

48+00

+22

+34

22 Aug 60

06.0	06.7	06.9	06.2
74	41.7	6.5	7.2
52	49	27.4	22

05.0	05.1	06.0	04.8
8.4	7.7	2.4	86
53	48	28	21.7

04.5	05.6	05.6	03.9
8.9	7.8	7.8	9.5
54	49	29	22.4

03.3	5.5	5.5	9.5
10.1	7.9	82	11.1
56	47	29	19.2

04.6	04.8	04.7	04.6
6.3	1.1	1.7	4.1
66	47	26	12

06.4	04.3	03.9	06.6
9.5	1.6	2.0	9.3
66.4	47	29	7.2

05.9	04.2	03.9	06.0
10.0	1.7	2.0	9.9
66.4	47	27	7.7

05.3	04.2	03.7	05.9
10.6	1.7	2.2	10.0
68.	47	28	6.6

03.5	04.0	03.3	05.3
12.4	1.9	2.6	10.6
73	48	29.4	3.4

04.3	04.2	03.5	
11.6	1.7	2.4	
71	47	25.9	

91.4
14.1
5.0

8

+

A

-

48+45

905.86

+75

49+00

+40

+80

50+00

T.P

1.15

903.71

3.30

902.56

+50

51+00

+14

+50

Lt
 94.5 04.0 03.3
 11.4 1.9 2.6
 70 47 26
 92.1 03.6 03.0 99.0
 13.2 2.3 2.9 6.9
 74.3 48.4 25.4 12.6
 95.1 03.1 02.9 00.7
 10.8 2.8 3.0 5.2
 66.4 49.4 25.7 14.4
 97.8 03.0 02.9 02.5
 8.1 2.9 3.0 3.4
 60 49.5 27 25
 99.1 02.9 02.8
 6.2 3.0 3.1
 58.7 47 27
 01.7 02.8 02.8
 4.7 3.1 3.1
 53 47 26.4
 02.8 02.4 02.4 02.9
 09 1.3 1.3 0.8
 52 47 26.5 24.6
 00.2 02.1 01.7 01.9
 3.5 1.6 2.0 1.8
 54 49 27 23.4
 99.4 02.1 01.4
 4.3 1.6 2.3
 56 49 24.6
 97.7 01.8 01.5
 6.0 1.9 2.2
 58.7 50 25.5

Lt
 96.2 95.8
 9.7 10.1 ✓
 4.6
 98.9 97.0
 7.0 8.6 ✓
 13.8
 00.4 98.1
 5.5 7.2 ✓
 15.8 19.6
 02.1 03.2
 3.2 2.7 ✓
 27.8
 02.3 02.1 08.1
 3.6 2.8 (+2.2) ✓
 25.6 42.7
 02.1 03.0
 3.2 2.9 ? ✓
 28.6
 02.3 01.9
 1.4 1.8 ✓
 26.6
 02.0 01.7
 1.7 2.0 ✓
 26
 02.1 02.0 ✓
 1.6 1.7
 2.8
 02.1 01.5
 1.6 2.2 ✓
 2.8

Rt
 22 Aug 60

(10)

+

5

-

52

903,71

52+15

+62

+72

53

+12

+22

+38

+50

+60

96.5	01.4	01.2	00.5	01.4	01.0	22 Aug 66		
7.2	2.3	2.5	3.2	2.3	2.7	✓		
62	51	26	21.6		2.9			
96.5	01.4	01.2	00.5	01.3	00.8	✓		
7.2	2.3	2.5	3.2	2.8	2.9			
62	51	28	23.5		28.6			
96.6	00.8	00.6	00.5	00.2	00.6	✓		
7.1	2.9	3.1	3.2	3.5	3.2			
62.3	51.6	26.3	21.7		28			
96.9	00.8	00.6	00.6	00.2	00.6	✓		
6.8	2.9	3.1	3.1	3.5	3.1			
60.5	51	25	20.5		27.6			
97.0	00.1	99.9	00.0	99.8	00.6	✓		
6.2	3.6	3.8	3.7	3.9	3.1			
63	51	23	17.7		24			
96.5	00.3	99.3		99.9	00.1	92.9	95.3	
7.2	3.4	4.4		3.8	3.0	0.8	8.4	✓
60	46.2	205			21.4	31.6	52.5	
95.4	00.1	99.0	00.0			01.1	91.1	✓
7.9	3.6	4.7	3.7			2.6	12.6	
61	44	18.2				18	36.2	
94.9	98.3	97.7	98.4	99.6	98.2	91.4		✓
8.8	5.4	6.0	4.9	4.1	5.5	12.3		
36	30	12.2	13.4		16	37		
94.3	97.1	97.3	96.5	96.1	96.6	93.3		✓
9.4	6.6	6.4	7.2	7.6	7.1	10.4		
37	31	21	2.4		18.2	?		
98.2	96.3	96.8	98.4	92.3				
15.5	7.4	6.9	15.3	11.4				
41	32	22	13					

12

+

A

-

TP

903.71

1.16

902.55

10.64 913.19

50+00

+50

51+00

+14

+50

52+00

+15

+62

+72

53+00

TBM rim Mt of Larryhoe Drive 10.64

902.55

LT

RT

13
22 44 60

6

<u>3.8</u>	09.4 ✓
<u>45</u>	
<u>5.2</u>	08.0 ✓
<u>42</u>	
<u>87</u>	04.5 ✓
<u>37.3</u>	
<u>8.9</u>	04.3 ✓
<u>37.5</u>	
<u>8.3</u>	04.9 ✓
<u>37.2</u>	01.3 ✓
<u>5.9</u>	
<u>43.2</u>	07.6 ✓
<u>5.6</u>	
<u>46.0</u>	12.6 ✓
<u>0.6</u>	
<u>54</u>	12.8 ✓
<u>0.4</u>	
<u>54.2</u>	07.3 ✓
<u>5.9</u>	
<u>76</u>	

14

+

A

-

0.76

903.31

+BM

902.55

53+70

+82

+91

54+00

+50

55+00

+30

+55

+65

LT

E

RT

15
23 4/6

TBM-Rim Mt @ McKnight & Larry Ho Drive

3.5' ~~16'~~ Fill = 2.08 cy.
[CULV]

9.9-6.4

60" CMP with 16x3.5 fill over

92.8	98.5	96.1	94.8	94.3
9.5	9.8	8.6	8.5	9.0
52	36	25	18.6	

94.5	99.4	99.3	96.2	94.9
8.8	3.9	9.0	7.1	8.4
64	38	26	18	2.5

94.7	00.8	00.4	96.7	95.9	95.1
8.6	2.5	2.9	6.6	7.4	8.2
61	41	26	8.2	5.9	

95.2	01.4	01.4	98.1	98.5	95.6
8.1	1.9	1.9	5.2	8.8	7.7
61	46	25	18	8	

95.8	01.8	01.4	00.6	00.3	96.0
7.5	1.5	1.9	2.7	3.0	7.3
62	29	27	23	11	

96.8	02.3	01.9	01.2	00.1	96.7
6.5	1.0	1.4	2.1	2.6	6.6
60	48	27	22	13	30

99.7	00.0	00.0	01.0	01.0	99.0
3.6	0.3	0.8	1.7	2.3	4.3
58	48	40	23	14	10

01.4	03.0	02.4	02.0	01.8	0.1
1.8	0.3	0.5	1.3	1.5	3.2
57	46	27	22	14	8

(16)

+

π

—

55+75

903,31

3.88

899.43

TP

12.80

912.23

+82

+90

56+00

+35

+75

57+00

+50

3.10

909.13

872

TP

8.70

917.83

58+00

+50

$\begin{array}{r} \cdot 2 \\ 0 \end{array}$
 $\begin{array}{r} \cdot 2 \\ 0 \end{array}$
 $\begin{array}{r} \cdot 2 \\ 0 \end{array}$
 $\begin{array}{r} \cdot 0 \\ 0 \end{array}$

17
23 Aug 60

old read not disturbed

$\begin{array}{r} \cdot 9 \\ 0 \end{array}$	$\begin{array}{r} \cdot 4 \\ 0 \end{array}$	$\begin{array}{r} \cdot 6 \\ 0 \end{array}$	$\begin{array}{r} \cdot 6 \\ 0 \end{array}$	$\begin{array}{r} \cdot 9 \\ 0 \end{array}$	✓
83	87	8.6	9.6	9.3	
52	46	27	16		
$\begin{array}{r} \cdot 4 \\ 0 \end{array}$	$\begin{array}{r} \cdot 1 \\ 0 \end{array}$		$\begin{array}{r} \cdot 2 \\ 0 \end{array}$	$\begin{array}{r} \cdot 3 \\ 0 \end{array}$	✓
7.8	8.1		9.0	9.9	
52	47			19	
$\begin{array}{r} \cdot 3 \\ 0 \end{array}$	$\begin{array}{r} \cdot 1 \\ 0 \end{array}$		$\begin{array}{r} \cdot 1 \\ 0 \end{array}$	$\begin{array}{r} \cdot 1 \\ 0 \end{array}$	✓
4.9	7.1		8.1	9.1	
56	4.7			20	
$\begin{array}{r} \cdot 6 \\ 0 \end{array}$	$\begin{array}{r} \cdot 2 \\ 0 \end{array}$		$\begin{array}{r} \cdot 4 \\ 0 \end{array}$	$\begin{array}{r} \cdot 9 \\ 0 \end{array}$	✓
2.6	6.0		6.4	7.3	
57	47			23	
$\begin{array}{r} \cdot 2 \\ 0 \end{array}$	$\begin{array}{r} \cdot 3 \\ 0 \end{array}$		$\begin{array}{r} \cdot 6 \\ 0 \end{array}$	$\begin{array}{r} \cdot 6 \\ 0 \end{array}$	✓
11.2	07.3		06.6	05.6	
1.0	4.9		5.6	6.6	
60	48			28.5	
$\begin{array}{r} \cdot 4 \\ 0 \end{array}$	$\begin{array}{r} \cdot 2 \\ 0 \end{array}$		$\begin{array}{r} \cdot 2 \\ 0 \end{array}$	$\begin{array}{r} \cdot 3 \\ 0 \end{array}$	✓
12.4	08.2		08.2	07.3	
41.4	4.0		4.0	4.9	
62	48.5			31	
$\begin{array}{r} \cdot 7 \\ 0 \end{array}$	$\begin{array}{r} \cdot 6 \\ 0 \end{array}$		$\begin{array}{r} \cdot 4 \\ 0 \end{array}$	$\begin{array}{r} \cdot 8 \\ 0 \end{array}$	✓
14.7	09.6		09.4	09.8	
31	8.2		8.2	8.0	
60.4	50			29	
$\begin{array}{r} \cdot 2 \\ 0 \end{array}$	$\begin{array}{r} \cdot 5 \\ 0 \end{array}$		$\begin{array}{r} \cdot 2 \\ 0 \end{array}$	$\begin{array}{r} \cdot 8 \\ 0 \end{array}$	✓
15.2	10.5		10.2	10.8	
2.6	7.3		7.6	7.0	
59	48.5			28.6	
				5.9	
				32.8	

18

+

-

59+00

917.83

+50

60+00

+32

+68

TP

2.34

915.49

61+00

13.41

928.90

+35

+50

+69

+90

$$\begin{array}{r} 12.6 \\ 52 \\ \hline 52.5 \end{array} \quad \begin{array}{r} 12.3 \\ 51.5 \\ \hline 48.6 \end{array}$$

$$\begin{array}{r} 4.7 \\ 7.1 \\ \hline 10.7 \end{array}$$

$$\begin{array}{r} 10.5 \\ 7.3 \\ \hline 26.4 \end{array}$$

19
2344960

$$\begin{array}{r} 12.8 \\ 5.0 \\ \hline 51.5 \end{array} \quad \begin{array}{r} 13.4 \\ 8.4 \\ \hline 47.4 \end{array} \quad \begin{array}{r} 12.8 \\ 5.0 \\ \hline 27 \end{array} \quad \begin{array}{r} 11.3 \\ 6.5 \\ \hline 22 \end{array}$$

$$\begin{array}{r} 10.7 \\ 7.1 \\ \hline \end{array}$$

$$\begin{array}{r} 13.7 \\ 4.6 \\ \hline 53 \end{array} \quad \begin{array}{r} 14.8 \\ 3.0 \\ \hline 47 \end{array} \quad \begin{array}{r} 14.3 \\ 3.5 \\ \hline 26.7 \end{array} \quad \begin{array}{r} 12.2 \\ 5.6 \\ \hline 22 \end{array}$$

$$\begin{array}{r} 9.8 \\ 8.0 \\ \hline \end{array}$$

$$\begin{array}{r} 14.4 \\ 3.4 \\ \hline 53 \end{array} \quad \begin{array}{r} 15.9 \\ 1.9 \\ \hline 48 \end{array} \quad \begin{array}{r} 15.0 \\ 2.8 \\ \hline 26.6 \end{array} \quad \begin{array}{r} 13.0 \\ 4.8 \\ \hline 21 \end{array}$$

$$\begin{array}{r} 11.0 \\ 6.8 \\ \hline \end{array}$$

$$\begin{array}{r} 15.8 \\ 2.2 \\ \hline 54 \end{array} \quad \begin{array}{r} 16.8 \\ 1.0 \\ \hline 48 \end{array} \quad \begin{array}{r} 16.7 \\ 1.6 \\ \hline 27 \end{array} \quad \begin{array}{r} 15.6 \\ 2.2 \\ \hline 22 \end{array}$$

$$\begin{array}{r} 13.8 \\ 8.0 \\ \hline \end{array}$$

$$\begin{array}{r} 13.4 \\ 4.4 \\ \hline 8 \end{array} \quad \begin{array}{r} 9.4 \\ 19.5 \\ \hline \end{array}$$

$$\begin{array}{r} 17.3 \\ 11.6 \\ \hline 60 \end{array} \quad \begin{array}{r} 17.4 \\ 11.3 \\ \hline 45.6 \end{array}$$

$$\begin{array}{r} 16.7 \\ 12.2 \\ \hline \end{array}$$

$$\begin{array}{r} 16.2 \\ 12.7 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 12.8 \\ 16.1 \\ \hline 46.6 \end{array}$$

$$\begin{array}{r} 23.1 \\ 5.8 \\ \hline 62 \end{array} \quad \begin{array}{r} 18.7 \\ 10.2 \\ \hline 47.5 \end{array}$$

$$\begin{array}{r} 18.3 \\ 10.6 \\ \hline 22.5 \end{array}$$

$$\begin{array}{r} 17.8 \\ 14.1 \\ \hline \end{array}$$

$$\begin{array}{r} 17.6 \\ 11.3 \\ \hline 24 \end{array}$$

$$\begin{array}{r} 20.3 \\ 8.6 \\ \hline 51.6 \end{array}$$

$$\begin{array}{r} 20.0 \\ 8.9 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 25.1 \\ 3.8 \\ \hline 63 \end{array} \quad \begin{array}{r} 18.8 \\ 10.1 \\ \hline 47 \end{array}$$

$$\begin{array}{r} 18.4 \\ 10.5 \\ \hline 28 \end{array}$$

$$\begin{array}{r} 18.7 \\ 19.2 \\ \hline 39 \end{array}$$

$$\begin{array}{r} 22.6 \\ 6.3 \\ \hline 53 \end{array}$$

$$\begin{array}{r} 22.3 \\ 4.6 \\ \hline 63 \end{array} \quad \begin{array}{r} 24.3 \\ 4.6 \\ \hline 63 \end{array}$$

$$\begin{array}{r} 26.3 \\ 2.6 \\ \hline 63.9 \end{array} \quad \begin{array}{r} 19.8 \\ 9.3 \\ \hline 47 \end{array}$$

$$\begin{array}{r} 19.1 \\ 9.8 \\ \hline 29 \end{array}$$

$$\begin{array}{r} 19.5 \\ 9.4 \\ \hline 23 \end{array}$$

$$\begin{array}{r} 24.8 \\ 4.1 \\ \hline 56 \end{array}$$

$$\begin{array}{r} 24.3 \\ 4.6 \\ \hline 63 \end{array} \quad \begin{array}{r} 26.4 \\ 2.5 \\ \hline 63 \end{array}$$

$$\begin{array}{r} 28.2 \\ 0.7 \\ \hline 66.5 \end{array} \quad \begin{array}{r} 20.2 \\ 8.7 \\ \hline 47 \end{array}$$

$$\begin{array}{r} 19.9 \\ 9.0 \\ \hline 29 \end{array}$$

$$\begin{array}{r} 20.0 \\ 8.9 \\ \hline 29 \end{array}$$

$$\begin{array}{r} 26.0 \\ 2.9 \\ \hline 46.5 \end{array}$$

$$\begin{array}{r} 25.0 \\ 3.9 \\ \hline 59 \end{array}$$

$$\begin{array}{r} 26.0 \\ 2.9 \\ \hline 64 \end{array}$$

(20)

62+00

928.90

+35

+50

+73

63+00

5.57 923.33

TP 8.46 931.79

+30

+58

+78

+91

64+00

0.66
29.4 20.5

(+0.5) 8.4
67.0 46
31.0 21.5

(+2.1) 7.4
68.5 46
31.1 21.8

(+2.2) 7.1
68.4 47
31.0 22.5

(+2.1) 6.4
65.5 46
29.4 23.9

(+0.5) 5.2
62 48.0
27.5 24.8

4.3 7.0
59 48
27.5 25.2

4.3 6.8
57 49
27.5 25.0

28.8 26.6
5.0 5.2
73 53

25.0 25.0
6.8 5.8
62 49

✓ 8.6 20.3
20.4 26.3

21.3 20.7
7.6 8.2
21.6 21.2

7.3 7.3
28.1 29
22.1 21.7

✓ 6.8 7.2
22.9 22.8
6.0 6.1

24.2 24.0
7.6 7.8
24.8 23.4

24.5 24.1
6.8 7.2
25.0 24.1

25.4 24.0
6.4 7.8
25.7 22.8

25.7 23.4
6.1 8.4
25.7 22.4

26.0 22.1
5.8 8.7
26.0 22.4

20.4 26.3
8.5 2.6
28 40

20.7 26.6
8.2 2.3
28 43

21.2 26.6
7.7 2.3
29 42

21.7 26.7
7.2 2.2
27 40

22.8 27.1
6.1 1.8
28 37

23.4 25.7
8.4 6.1
28 36

24.1 24.1
7.2 7.2
27 34

24.0 22.8
7.8 9.0
29 35.6

22.4 22.4
9.4 9.4
20 20

(21) 2.7
25.0 26.2
25.0 26.2

26.1 29.1
2.8 40.8
58 67

25.8 30.6
3.1 4.7
56 66

26.0 29.9
2.9 4.0
54 64

26.2 27.4
2.7 1.5
54 59

24.8 24.8
7.0 7.0
51 51

23.7 23.7
8.1 8.1
53 53

22.8 22.8
9.0 9.0
35.6 35.6

22.4 22.4
9.4 9.4
20 20

22.4 22.4
9.4 9.4
20 20

(22)

+

π

-

4+50

931.79

5+00

+50

+77

1.98 929.81

T.P

6.37 936.18

66+00

+34

+59

+71

+79

+91

0.33 935.85

BM
935.91

26.0 28.0 27.1 26.8 28.2 24.8
518 38 4.7 50 3.4 7.0 7.1
57 53 51 24 21.6 15.3

26.9 28.5 28.0 26.1 25.2
4.9 3.3 3.8 5.7 6.6
56.5 63.5 24 17.5

27.9 29.8 29.5 27.1 26.8
3.9 2.0 2.3 4.7 5.0
55 50 22.5 18

29.2 30.6 29.9 28.8 28.6
2.6 1.2 1.2 3.0 3.2
51 48 22 20

29.5 31.3 30.9 29.4 29.3
6.7 4.9 5.3 6.8 6.9
54 49 24 20

30.1 31.9 31.3 29.6
6.1 4.3 4.9 6.6
56 51 25 20

29.8 32.3 31.7 29.3
6.4 3.9 4.5 6.9
58 50 26 20.5

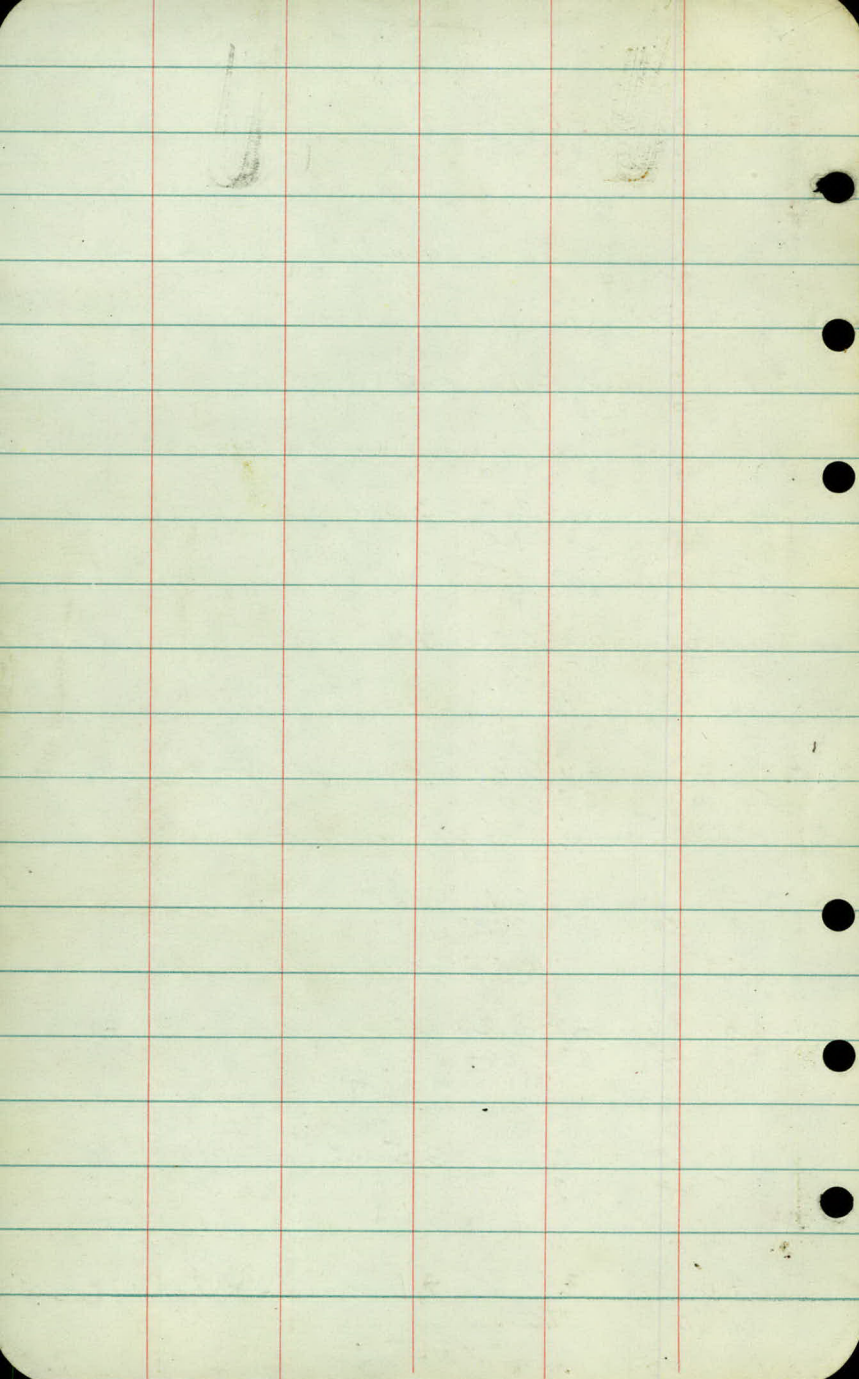
29.7 32.6 31.8 30.0
6.5 3.6 4.4 6.2
65 48 23 20

32.4 32.4 32.3 32.7
3.8 3.8 3.9 3.5
65 48 23

32.2 32.4 32.1
4.0 3.8 4.1
59.6 37.6

Five Hyd Burns & McKnight

only grade



FK
RG
AP
RO
DIST.

VERT.
ANGLE

ROD
EQUIV.

ROD

DIFF.

ELEV.

Dec 11, 1959

McKnight - Lower Aftm to VS[#]12

Sta 11 $\pm$ = 0.2' Lower than 10 $\pm$

Sta 11 $\pm$ = 0.2' Lower than 10+50 $\pm$

Sta 11 $\pm$ = 0.4' Higher than 11+35 $\pm$

Sta 11 $\pm$ = 0.5' Higher than 11+50 $\pm$

$$\begin{array}{r}
 19 + 30.92 \text{ New} \\
 19 + 27.08 \text{ old} \\
 \hline
 3.84
 \end{array}$$

$$\begin{array}{r}
 23 + 06.57 \\
 3.84 \\
 \hline
 2.73
 \end{array}$$

$$\begin{array}{r}
 6.57 \\
 1.5 \\
 \hline
 328.5 \\
 657.5 \\
 918.5 \\
 1826 \\
 1.5 \\
 \hline
 9130
 \end{array}$$

$$\begin{array}{r}
 50 \\
 2030' / 100' \\
 150' / 100' \quad 1.5' / 84
 \end{array}$$

$$\begin{array}{r}
 9130 \\
 1826 \\
 \hline
 27390 \\
 9855 \\
 \hline
 37245
 \end{array}$$

FK
WM
RB

Dec. 5, 1961

9

Elevations

Note: Add 0.40'
to all Elevations
as Bench Elevations
Were Not Changed.

use elev's in red figure

Sta	+	π	-	Elev.	914.05
BM	9.47	923.12			913.65
39+08			6.54	916.58	916.98
39+08			4.38	918.74	919.14
39+07			6.56	916.56	916.96
39+02			6.45	916.67	917.07
38+92			5.98	917.14	917.54
T.P.	11.99	934.27	0.84	922.28	922.68
37+11			9.88	924.39	924.79
36+66			8.86	925.41	925.81
36+61			8.96	925.31	925.71
36+36			8.51	925.76	926.16
36+10			6.75	927.52	927.92
36+05			6.62	927.65	928.05
TP	13.56	947.61	0.22	934.05	934.45
33+35			6.98	940.63	941.03
30+54			2.79	944.82	945.22
30+65			5.45	942.16	942.56
30+60			5.54	942.07	942.47
31+00			1.87	946.14 945.74	46.38

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6

Spike in 24" Elm 130' E of 39+73

Top MH 41' Lt

Top Hyd 58' Lt

NE Cor Walk 50' Lt

SE Cor Walk 50' Lt

Top MH 38' Lt

/

± Basement Garage

NE Cor Walk 50' Lt

SE Cor Walk 50' Lt

MH 38' Lt West Rim

NE Cor Walk 50' Lt

SE Cor Walk 50' Lt

MH 38' Lt

Top Hyd Lt 54'

NE cor Walk 48' Lt

SE cor Walk 48' Lt

2

Sta	+	π	-	Elev	
BM	7.29	952.11		944.82	945.22
					948.63
31+00			4.20	947.91	948.23
					939.40
T.P	0.15	939.15	13.11	939.00	925.82
					914.05
TP	0.07	925.49	13.73	925.42	
		13.45			
BM		11.84	11.82	913.67	913.65

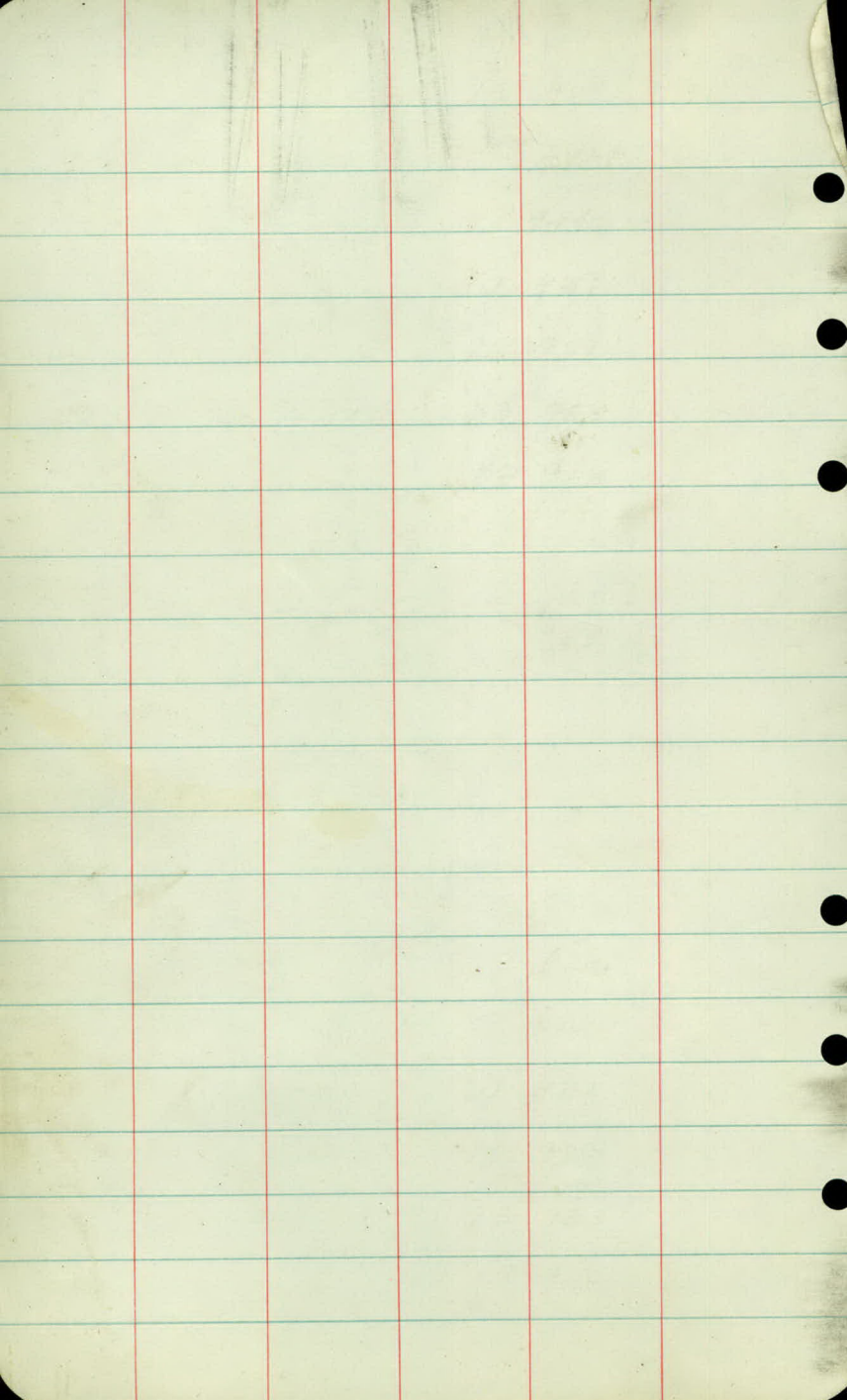
Dec. 5, 1961

C

Top Hyd 54' Lt Sta 30+54

Floor Garage Rt

Spike in 24" Elm 130' E. of 39+75



S $\frac{1}{2}$ of SW $\frac{1}{4}$
NE $\frac{1}{4}$ of SW $\frac{1}{4}$ except
E 286.81' of N 243'

S $\frac{1}{2}$ of NW $\frac{1}{4}$ of SE $\frac{1}{4}$
of NW $\frac{1}{4}$ of SE $\frac{1}{4}$
N $\frac{1}{2}$ lying West of a line
660' East of NW Corner of
SE $\frac{1}{4}$ at 90° to N Line