

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PARTIAL PLAN Survey

Co. Road "C"

From S.T.H. #61 To E. Co. LINE

Road Acc't. No. _____

Date Filed 2-16-61

Dr. 9
File BK. 30

Co Rd "C"

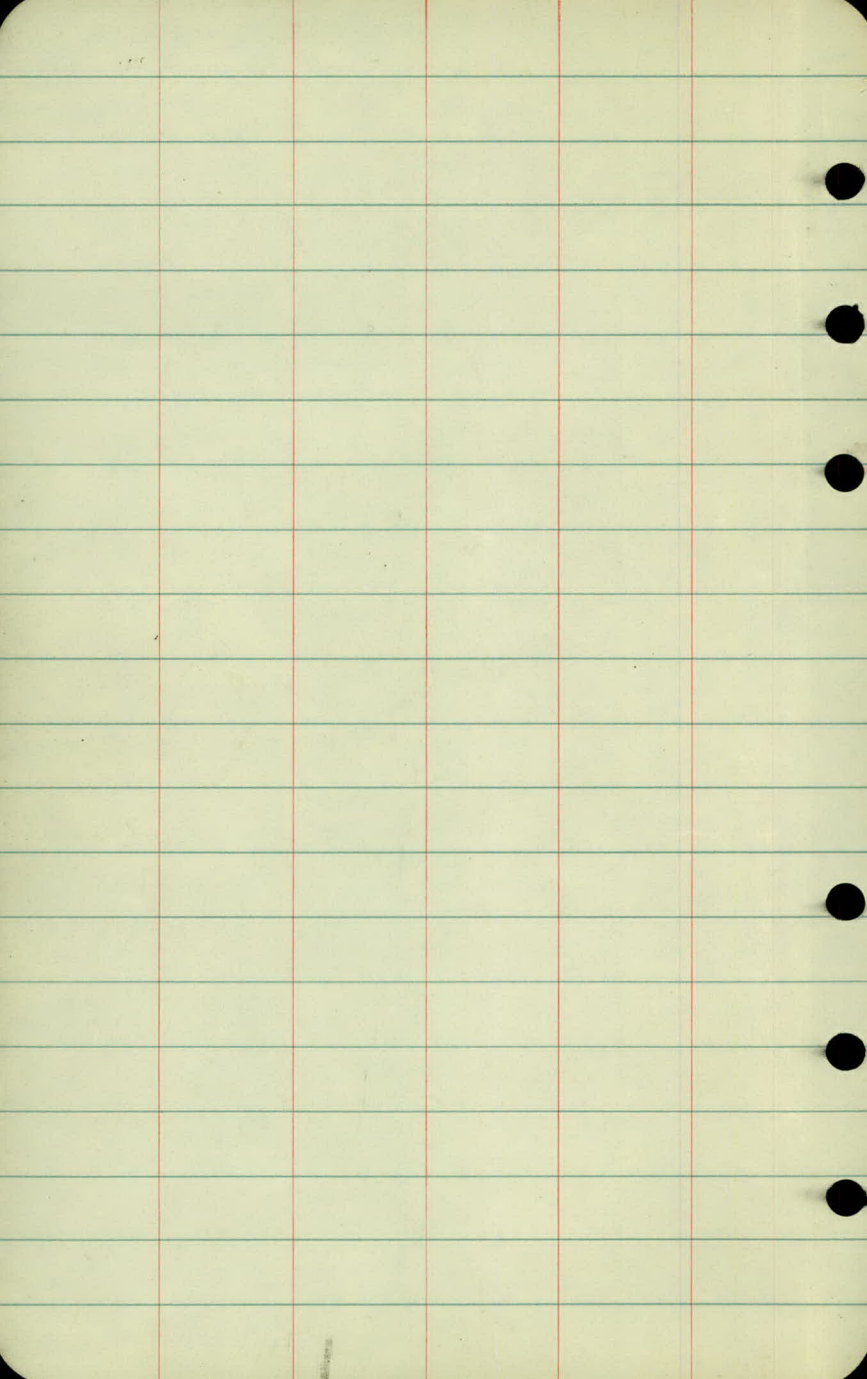
S.T.H. #61 to E. Co. Line

PLAN SURVEY

EAST CO. LINE Rd.

S.T.H.

#61



FK
RG
KP

Feb 25, 1957

2

Alignment

Sta Point Δ Lt. Δ Rt.

52+40.06 P.I.

0°46' English

38+29.08 P.O.T.

37+96.85 P.O.T.

37+64.38 P.O.T.

~~Hywel~~

Given
25+81.34 P.I. 0°09'

PK
RG HC
KP RC

Feb 25, 1957

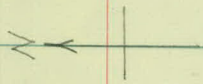
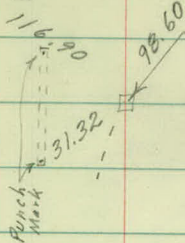
3

N.W.
Cor Fo

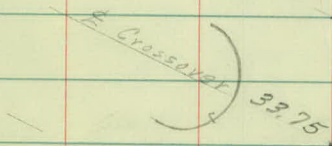
NW Cor
Fo

S.E. Cor Sec 4-30-22

Mont.



Reefing Nail



A No. 10 Round Lane
PK Nail

26.53

R. Nail

2658.72 M
To Book

A. So. Bound Lane

Mont
Tipped
Not-Used

Sta Point ΔL ΔR

78+70.68 P.I. $0^{\circ}22\frac{1}{4}'$

70+50.40 P.O.T.

66+61.60 Pot $\neq$ Track

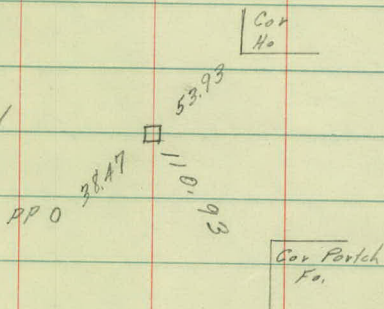
63+37.46 P.O.T.

FX HC M
 RG HC M
 KP RCHC
 WH M RG

March 1, 1957
 Cool Windy 27°

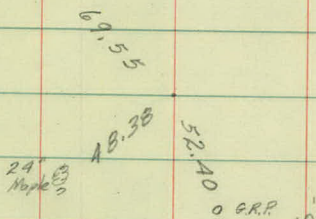
4

Hazelwood

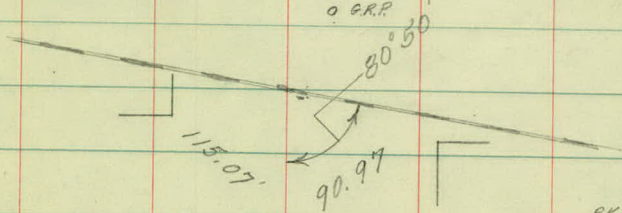


Mont Disturb
 Use Spike

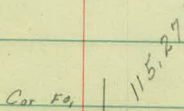
PPO O PP



P.K. Nail



P.K. Nail



Sta	Point	ΔL	ΔR
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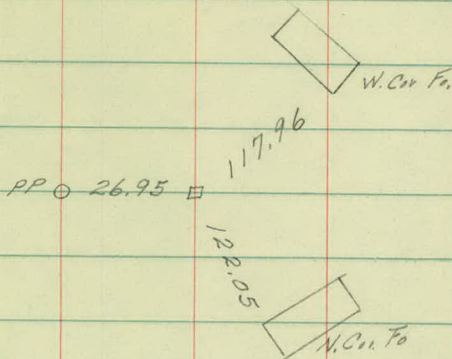
104+96.69	P.I.	$0^{\circ} 30\frac{1}{2}'$	
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35+72.68	P.O.T		
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FK
RG
KP
WH

March 4, 1957

5



Mont



PP ○ 30.26

P.K. Nail

117.26

PP ○

Sta	Point	ΔL	ΔR
-----	-------	------------	------------

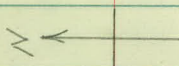
131+29.45	P.I.	$0^{\circ}10\frac{1}{4}$	
-----------	------	--------------------------	--

121+25.5	P.O.T		
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March 4, 1957

6

12" BE @ 40.20 36.01 0 PP
± Ariel St. □ 35.87 0 TP



± White Bear Ave.

Sta	Point	ΔL	ΔR
-----	-------	------------	------------

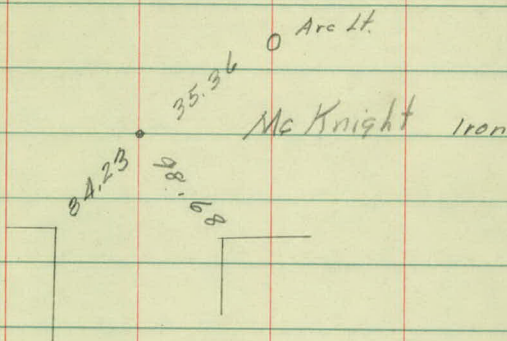
157+54.74	P.I.	0° 41'	
-----------	------	--------	--

146+95.29	P.O.T.		
-----------	--------	--	--

March 5 1957

7

E 4th St N.W.



N

27.27 OPP

50.50 @ 12"0

Roofing Nail

Sta	Point	Δ Lt	Δ Rt
-----	-------	------	------

189+00			
--------	--	--	--

183+66.44	P.I.		
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		$0^{\circ}00\frac{3}{4}'$	
--	--	---------------------------	--

FK
RG
KP

£ March 5, 1957

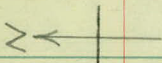
8

Margaret St.

A
D.A. 6.60

PK Nait

64.92



Hyd 8 39.40

38.68



♀ Bellaire

Mont.

46.22

Conc. □
Fe. Con.

Sta Point ΔL ΔR

209+76.67

204+00 P.O.T.

^{1.00}
203+60.99 P.O.T.

197+18.64 P.O.T.

$$2611.4 = \frac{1}{2} \text{ min}$$

$$33 \left[\begin{array}{c} 503.45 \\ 22 \times 25 \end{array} \right] 66 \left[\begin{array}{c} 17.45 \\ 602 \end{array} \right] 576.7 33 \left[\begin{array}{c} 550 \end{array} \right] 33$$

$$669.45$$

$$683.45$$

$$642.7$$

$$616 = 2611.6$$

$$33 \left[\begin{array}{c} 26.73 \quad 26.73 \\ 22 \times 25 \end{array} \right] 66 \left[\begin{array}{c} 33.72 + 33.72 \\ 22 \times 25 \end{array} \right] 66 \left[\begin{array}{c} 25 \times 23 \\ +.45 \\ 185 \end{array} \right] 66 \left[\begin{array}{c} 25 \times 22 \end{array} \right] 33$$

550

$$209 \quad 76.66$$

$$183 + 66.44$$

$$26 \quad 10.22$$

1.38 short

$$\begin{array}{r} 1.38 \quad \times \\ 2611.6 \quad 616 \end{array}$$

$$2611.6 \times =$$

$$1.38$$

$$616$$

$$828$$

$$138$$

$$828$$

$$852.08$$

$$209 \quad 76.67$$

$$616$$

$$203 + 60.67$$

$$33$$

$$203 + 61.00$$

$$616$$

$$642.7$$

$$1258.7$$

$$1258.7$$

$$1.38$$

$$100696$$

$$37761$$

$$12587$$

$$\begin{array}{r} 1.38 \quad \times \\ 2611.6 \quad 1258.7 \end{array}$$

$$2611.6 \times =$$

$$1737.006$$

$$2611.6 \quad 1737.006$$

$$156672$$

$$2097667$$

$$170286$$

$$1258.7$$

$$182812$$

$$19717.97$$

$$13$$

$$67$$

$$19718.64$$

$$\begin{array}{r} 2611.6 \quad 133 \\ 852.08 \\ 78348 \\ 68600 \end{array}$$

£ March 5, 1957

9

£ E. Co Line

Brass Plug



~

21.91

73.33

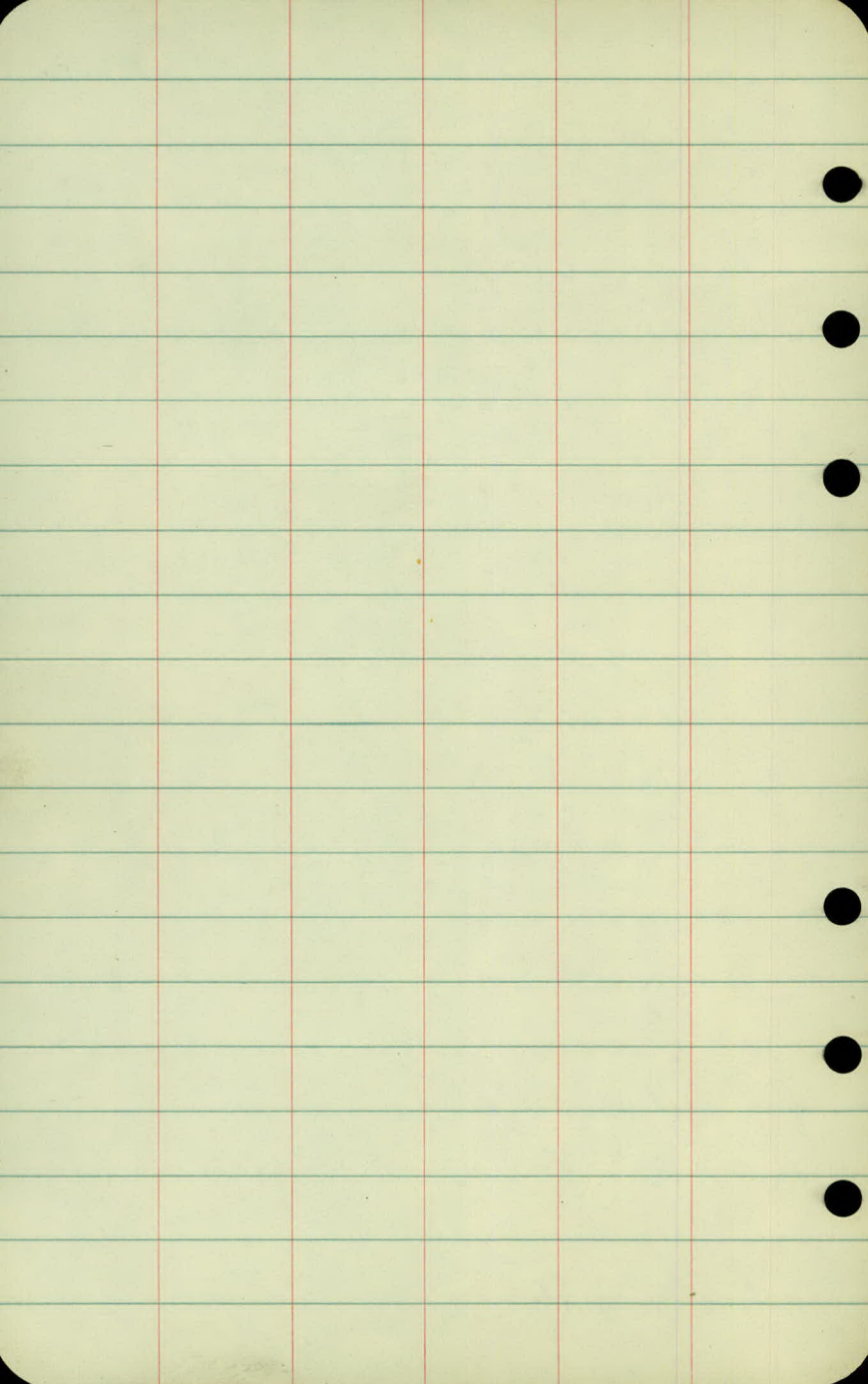
63.05

No. 304

P.K. Nail

£ N. Henry St.

£ Charles St.



Topography

42

14 10 ✓

6-4"

Lombardys ✓

+57 $\frac{\text{begin Fence}}{32}$ ✓+60 $\frac{\text{ENT } 20'}{13}$ ✓+97 $\frac{\text{Begin } 15 \times 25 \frac{1}{2} \text{ CM CULVERT}}{24}$ ✓+51 $\frac{\text{PP}}{28}$ ✓+35 $\frac{\text{ENT}}{18}$ ✓+60 $\frac{15 \times 32 \text{ CM}}{24}$ ✓+12 $\frac{\text{SW } 6'}{20}$ ✓+27 $\frac{\text{NE Cor. Church}}{85}$ ✓

41

11 13 ✓

+94 $\frac{\text{Iron pole}}{63.5}$ ✓+71 $\frac{\text{E. Cor. Sch.}}{54}$ ✓Steps to Ent $\frac{\text{Flagstone}}{24-32}$ ✓+31 $\frac{\text{Steps (5')}}{21}$ ✓+63 $\frac{\text{SW } 4'}{19}$ ✓+59 $\frac{\text{begin } 12 \times 19 \text{ CM}}{23}$ ✓

40

13 12 ✓ +13 $\frac{\text{N.W. Cor. Church}}{72}$ ✓+92 $\frac{\text{Con. School}}{53.5}$ ✓+84 $\frac{\text{PP}}{28}$ ✓+55 $\frac{\text{END Wall}}{34}$ ✓+93 $\frac{\text{SP}}{28}$ ✓+70 $\frac{\text{House}}{110}$ ✓+90 $\frac{\text{Flag pole}}{45}$ ✓+88 $\frac{\text{Steps}}{20}$ ✓+41 $\frac{\text{SW } 5'}{54}$ ✓+92 $\frac{\text{begin } 15 \times 19 \text{ CM}}{23}$ ✓+137 $\frac{\text{Wall}}{51}$ ✓+137 $\frac{\text{Wall}}{63}$ ✓+28.5 $\frac{\text{CB}}{40}$ ✓+55 $\frac{\text{CB=Surface Drain}}{47}$ ✓+44 $\frac{\text{Wall}}{74}$ ✓+20 $\frac{\text{House}}{120}$ ✓+28.5 $\frac{\text{ENT (19')}}{15}$ ✓

39

12 14 ✓ +100 $\frac{\text{CB}}{32}$ ✓+75 $\frac{\text{CB}}{91}$ ✓

17 +75 25

+43 $\frac{\text{CB}}{50}$ ✓

60 +45 50

+29 $\frac{\text{PP}}{57}$ ✓

+29.08 POT E N.B. Lane

38

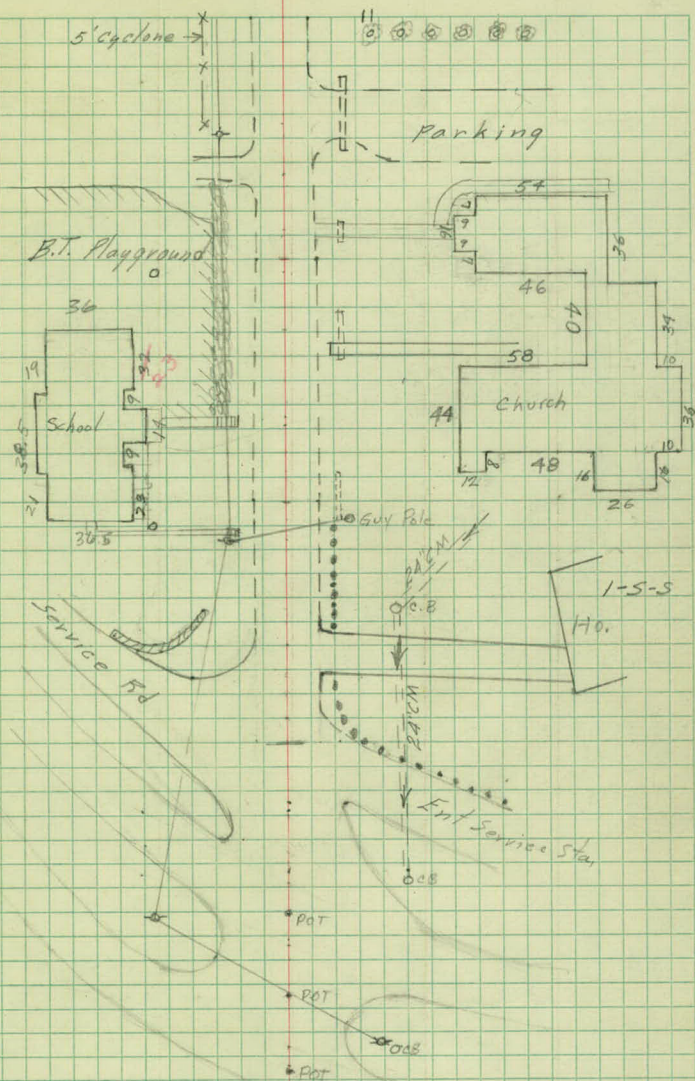
+96.85 POT E X-over

+82 $\frac{\text{PP}}{39}$ ✓+82 $\frac{\text{CB}}{44}$ ✓

+64.38 POT E S.B. Lane

37

11



47

+64 Spired Cor 30 +18 SW Cor Ho 112 +48 SW Ho 15 7
 +44 PP 29 +43 25" BE 51 +38 SE Cor Ho 78 +81 17" Maple 34
 +31 drive 18 +23 End Hedge 30 +21 7" BE 35
 +05 11" BE 35 +04 SW Cor Ho 61

46

+74 21" M 36 +76 BEGIN HEDGE 30 +61 SE Cor Ho 60 16 8
 +91 7" BE 87 +39 SW Cor ho 60
 +79 27" M 59 +91 7" BE 35 +21 DRIVE 24
 +74 15" M 81 +39 21" BE 50 +08 hedge 30-97
 +74 20" M 103 +31 SE Cor GAR 107 +08 PP 28
 +11 SW Cor GAR 107 +05 SE Cor GAR 97

45

+84 3" P 47 +99 DRIVE 24 +77 SE Cor ho 59
 +84 4" SPR 58 +86 SW Cor bn 97 +55 SW Cor ho 59 +50 END 15" X CM 20" 32
 +84 3" P 68 +43 5" SPR 25 +41 10" E 41 +46 PP 28
 +84 3" P 80 +16 8" E 40 +40 DRIVE 19

44

+68 End L.H. 31 +70 21" TW ELM 98 15 9
 +15 Seg. Lilac H. 31 +70 14" ELM 90 +69 Orig Fence 31 +50 DRIVE 12" X 20" CM 21 22
 +14 3" P 44 +14 11" Jun 35 +14 15" ELM 76
 +14 4" P 58 +12 PP 28 +15 PP 27

43

+92 SE Cor ho 61 +80 4" BL SE 54 +80 12" BE 48 +9 10" BE 97
 +78 4" BL SP 54 +80 1" E Cor ho 107
 +68 SW Cor House 60
 +64 DRIVE 22 +57 END FENCE 33 +14 DRIVE 18 +7 NW Cor ho 108
 +4 Begin Stone WALL 52 +22 END 15" X 25" CM 24

42

14

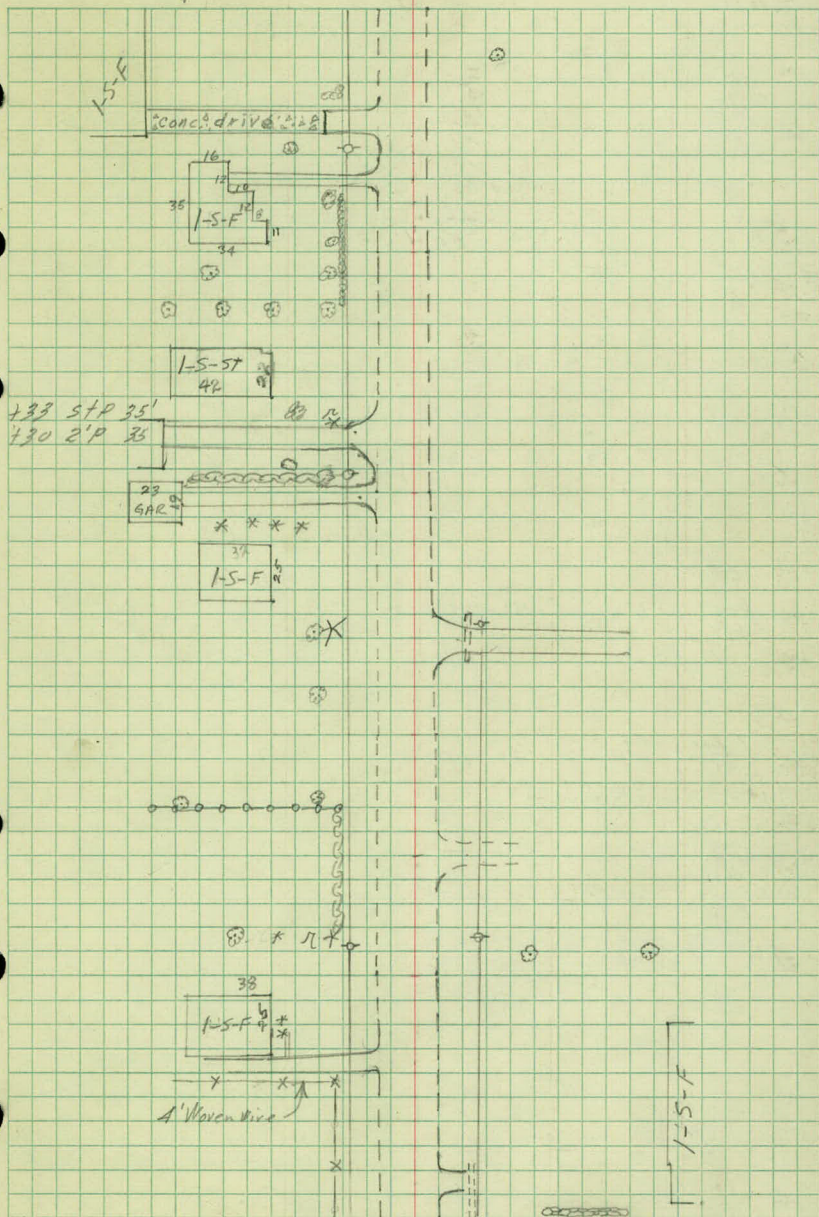
10

52

24

RG Mar 12
 KP Cloudy 45°
 AB Windy

12



52

10 11

+95 $\frac{ELM}{RT}$ +93 $\frac{9" CW}{68}$

+60 $\frac{14" CW}{46}$

+29 $\frac{5" ELM}{43}$ +29 $\frac{DRIVE}{20}$

51

+10 $\frac{20" CW}{100}$

+20 $\frac{20" CW}{49}$ 12 11

+04 $\frac{NE Cor Ho}{111}$

+73 $\frac{8" ELM}{78}$ +93 $\frac{9" ELM}{82}$

+62 $\frac{5" Ash}{60}$ +94 $\frac{6" Cottonwood}{55}$

+82 $\frac{NW Cor Ho}{111}$

+53 $\frac{PP}{28}$

+44 $\frac{SE Cor Ho}{81}$

+57 $\frac{PP}{33}$

+30 $\frac{4 steps}{30}$

+20 $\frac{SW Cor Ho}{81}$

50

+22 $\frac{19" Elm}{73}$

+07 $\frac{8" Elm}{56}$ 13 10

+91 $\frac{6" Poplar}{44}$

+75 $\frac{Fe Cor}{40}$

+51 $\frac{W.W.Fc}{32}$

+77 $\frac{8" Elm}{50}$

+51 $\frac{Conc Wall}{29}$

+41 $\frac{Conc. Ent}{29}$

+35 $\frac{SW Cor Ho}{52}$

+37 $\frac{End Fence}{28}$

49

+15 $\frac{PP}{28}$ +13 $\frac{Willow}{43}$

+02 $\frac{SW (2.0")}{23}$ 13 10

+52 $\frac{2" Pine}{39}$

+91 $\frac{SE Cor ho}{68}$

+91 $\frac{12" willow}{43}$

+79 $\frac{FENCE}{27}$

+68 $\frac{DRIVE}{25}$

+60 $\frac{Fence}{29 \frac{1}{2} 51 \frac{1}{2}}$

+16 $\frac{SW Cor ho}{86}$

+47 $\frac{91" ELM}{57}$

+57 $\frac{SE Cor ho}{90}$

+12 $\frac{9" ELM}{87}$

+22 $\frac{6" ELM}{60}$

+53 $\frac{Box 12' X 24' CM}{24}$

+05 $\frac{PP}{28}$

+05 $\frac{FENCE}{28-43}$

+67 $\frac{15" ELM}{38}$ 15 9

48

+98 $\frac{SE Cor ho}{87}$

+76 $\frac{SW Cor ho}{96}$

+58 $\frac{12" Oak}{61}$

+38 $\frac{STP}{38}$

+15 $\frac{15' X 24' F. edge ELM}{25}$

+59 $\frac{9" Ch Elm}{43}$

+71 $\frac{SE Cor Ho}{98}$

+66 $\frac{drive}{27}$

+19 $\frac{SW Cor Ho}{98}$

+15 $\frac{5" Spr}{61}$

+15 $\frac{PP}{28}$

47

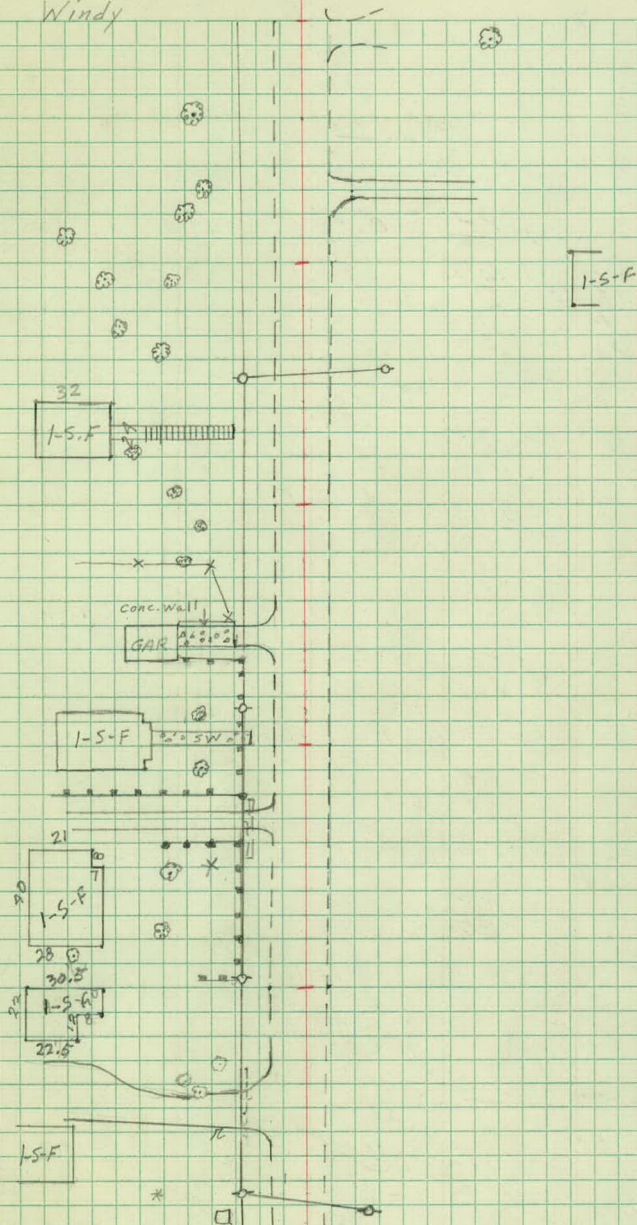
+00 $\frac{SE Cor Ho}{106}$

+06 $\frac{6' X 7' DISTCRB}{31}$ 15 7

+09 $\frac{PP}{26}$

+21 $\frac{drive}{21}$

RG Mar 13
 KP Cloudy 45°
 AB Windy



1-S-F

57

BT
12-9 ✓+65 Cor Hedge
33 ✓+59 $\frac{6"PI}{39}$ ✓ +60 $\frac{18"BE}{54}$ RTic Hedge +62+32 $\frac{SW Cor Ho}{6.5}$ ✓ +36 $\frac{12" B.S. Pine}{39}$ ✓+15 $\frac{Ent}{2+}$ ✓ +28 $\frac{Cor Hedge}{33-56}$ ✓56 +01 $\frac{PP}{28}$ ✓ +01 $\frac{Cor Hedge}{35}$ ✓ BT
12-9 ✓+47 $\frac{6"E}{42}$ ✓ +71 $\frac{10"A}{61}$ ✓ +78 $\frac{8"PI}{35}$ ✓+29 $\frac{8"M}{59}$ ✓ +32 $\frac{Lilac}{51}$ ✓ +57 $\frac{18"BE}{39}$ ✓+06 $\frac{12"M}{5.5}$ ✓ +29 $\frac{12"M}{41}$ ✓ +19 $\frac{Ent}{21}$ ✓+37 $\frac{6"E}{39}$ ✓ +04 $\frac{12"M}{36}$ ✓ +37 $\frac{Spired Cor Hedge}{35}$ ✓55 +44 $\frac{10"A}{33}$ ✓ +46 $\frac{5"E BT}{41}$ ✓ 12-9 ✓+97 $\frac{NE Cor Ho}{127}$ ✓+42 $\frac{PP}{28}$ ✓BT
11-11 ✓

54

+43 $\frac{N. End Culvert Buried}{42}$ ✓+43 $\frac{S.E. CMCulvert}{More than 24'}$ +36 $\frac{PP}{27}$ ✓

53

12-11 ✓

+50 $\frac{BR}{39}$ +76 $\frac{ER}{11}$ ✓+67 $\frac{PP}{41}$ ✓+72 $\frac{Bcg 15"X 20"CM}{23}$ ✓+98 $\frac{SW Cor. Garage}{37.7}$ ✓+32 $\frac{ER}{41}$ ✓+93 $\frac{NW Cor Ho}{83}$ ✓+21 $\frac{BEGIN 21X40' CM}{24}$ ✓+12 $\frac{PP}{28}$ ✓+05 $\frac{10" BE}{100}$ ✓+07 $\frac{BR}{10}$ ✓+05 $\frac{12" CW}{42}$ ✓

52

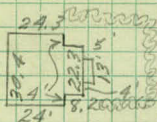
+05 $\frac{9" BE}{83}$ ✓+05 $\frac{12" CW}{64}$ ✓

RG MARCH 13
 KP CLOUDY 45°
 AB WINDY

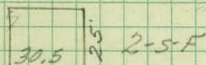
March 29, 1957
 FX Cloudy Cool
 RG 35°
 KP 37

14

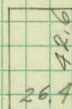
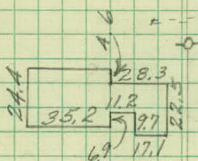
1-S-F



✓ +95 10" A 50
 ✓ +90 18" B 39'



1-S-F



62

$$\frac{BT}{11 \ 11} \checkmark$$
 $+43 \frac{PP}{28} \checkmark$
 $+64 \frac{6"A}{47} \checkmark +91 \frac{8"M}{61} \checkmark$
 $+29 \frac{12"BE}{56} \checkmark$
 $+44 \frac{SW Cor Ho}{85} \checkmark$
 $+05 \frac{SW Cor Ho}{74} \checkmark$
 $+09 \frac{R.Tie}{Ho 17} \checkmark$
 $61 +07 \frac{6"A}{55} \checkmark$
 $\frac{BT}{12 \ 11} \checkmark$
 $+38 \frac{4"M}{62} \checkmark$
 $+57 \frac{10"BE}{43} \checkmark$
 $+80 \frac{8"E}{50} \checkmark +58 \frac{7"CE}{65} \checkmark$
 $+83 \frac{6"CE}{66} \checkmark$
 $+20 \frac{2 Ent}{39} \checkmark$
 $+06 \frac{R.Tie}{Ent} \checkmark$
 $+33 \frac{12"CE}{50'} \checkmark$

60

 $\frac{BT}{12 \ 10} \checkmark$
 $+97 \frac{PP}{27.5} \checkmark$
 $+95 \frac{NE Cor Ho}{91} \checkmark$
 $+40 \frac{4"BE}{28} \checkmark$
 $+56 \frac{ER}{32} \checkmark$
 $+75 \frac{BR}{34} \checkmark$
 $+34 \frac{BR}{10} \checkmark +36 \frac{End Perry P.}{32} \checkmark$

59

 $\frac{BT}{12 \ 10} \checkmark$
 $+81 \frac{6"BE}{38} \checkmark$
 $+57 \frac{6"BE}{44} \checkmark$
 $+68 \frac{PP}{27.5} \checkmark$
 $+15 \frac{Tw 6"BE}{46} \checkmark$
 $+16 \frac{PP}{24} \checkmark$

58

 $\frac{BT}{13 \ 10} \checkmark$
 $+97 \frac{Cor Barry Patel}{30}$
 $+91 \frac{Ent 15" \times 28" CM}{20} \checkmark$
 $+36 \frac{PP}{27.5} \checkmark$

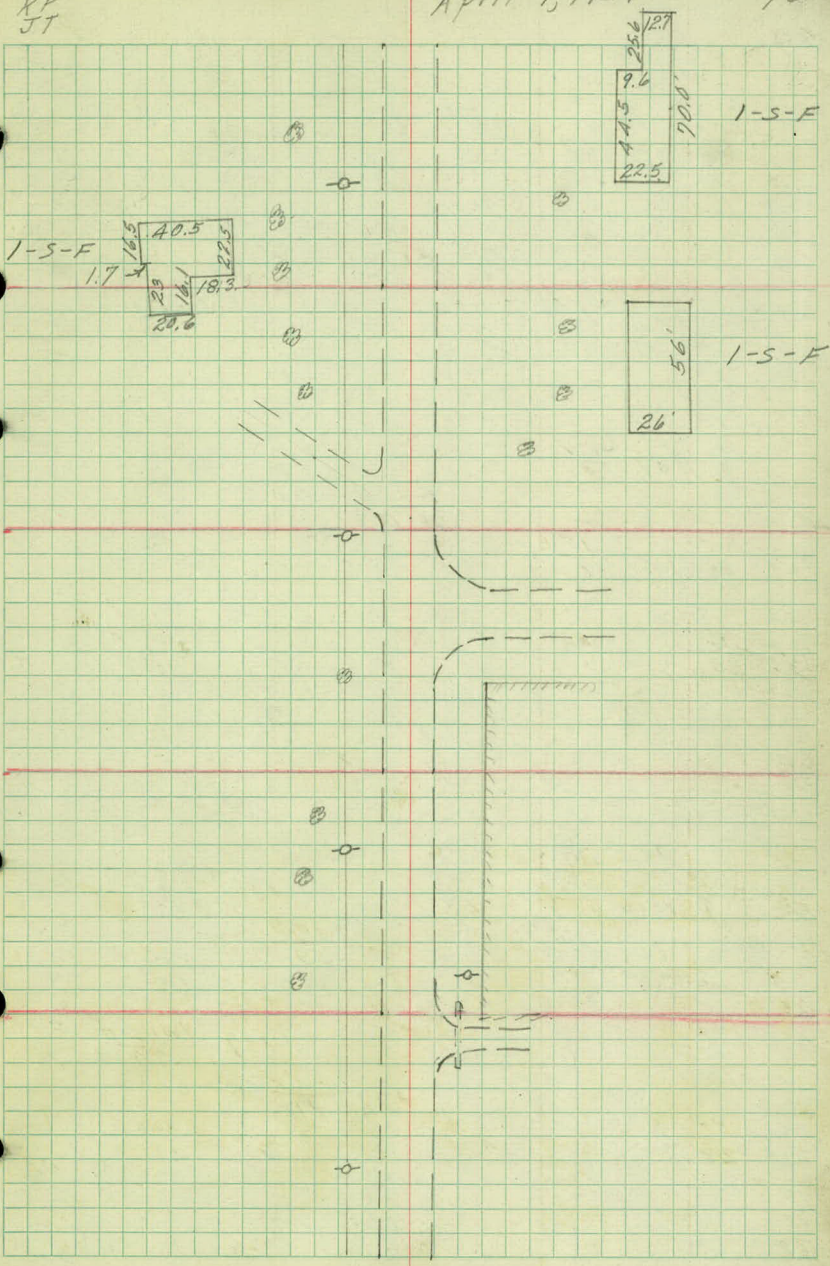
57

 $\frac{BT}{12 \ 9} \checkmark$

FR
RG
XP
JT

March 29, 1957
April 1, 1957

15



67

+61.60 $\frac{\text{Tracks}}{\text{E}}$

RTic
105 Fe Lt

107 NW Cor Bridge
13 ✓

114 TP 25 ✓

102 E Fe 13

+15 Fe 100

~~108 RTic Fe Lt~~

103 SW Cor Bridge 12' ✓

66

+106 E Fe 12

GR BT 6H 11 9.5 10 ✓ 13 ✓

PP 198 28 ✓

196 GP 23.5 ✓

+94 Fe 100

107 $\frac{4''A}{48}$ ✓

GRP 12 ✓ BT 9.5-10.5 ✓

GRP 12.5 ✓

65

+82 $\frac{26''P}{6.2}$ ✓ +83 $\frac{40''P}{41}$ ✓

197 $\frac{6A}{75}$ ✓

+85 BGRP 12 ✓

+53 $\frac{8''E}{51}$ ✓ +76 $\frac{12''A}{74}$ ✓

+36 $\frac{5''P}{51}$ ✓ +51 $\frac{SW Cor Ht}{96}$ ✓

146 RTic Holt ✓

+39 GP 21.5 ✓

+17 $\frac{14''E}{50}$ ✓ +18 $\frac{12''E}{66}$ ✓

+30 B.G.R. 11 ✓

64

+105 PP 29 ✓

+107 $\frac{E 15 CM BT}{26}$ ✓ 9-12 ✓

+60 $\frac{14''Ct}{5.4}$ ✓ +52 $\frac{BR}{9}$ ✓

+82 ER 42 ✓

+53 $\frac{3''Sp}{48}$ ✓ +42 $\frac{6''Spmer}{49}$ ✓

+60 $\frac{3''Sp}{64}$ ✓

+20 $\frac{SW Cor Ht}{92}$ ✓

+70 $\frac{WE 15 CM}{26}$ ✓

+28 $\frac{10 C.E.}{65}$ ✓

+63 Cor Ent 97 ✓

+98 $\frac{BR}{38}$ ✓ +16 $\frac{Ent 12 \times 16 CM}{22}$ ✓

+56 $\frac{Brk Wall}{53}$ ✓

+93 $\frac{Ent 12 \times 26 CM}{20}$ ✓

63

BT 9.5-12 ✓

+56 PP 22.5 ✓

189 NW Cor Ht 84 ✓ E 38.5 N 36.5

+97 $\frac{6''CE}{41}$ ✓

+68 $\frac{12 \times 26 CM Ent}{21}$ ✓

+83 PP 28 ✓

+40 PP 32 ✓

+51 $\frac{6''CE}{42}$ ✓

62

BT 11 11 ✓

+26 $\frac{Ent 12 \times 26 CM}{21}$ ✓

16

80° 50'

Wood Board Fe

A strand Barb

2-S-F 50.5

15" x 36" CM

2-5-F

E 26.8
N 24.5

 $1\frac{1}{2}-5-A$

1-5-5

$$72 \quad \frac{BT}{12.10} \checkmark$$

$$+63 \frac{8"BE}{51"} +64 \frac{70}{60} +64 \frac{106.77}{73} \checkmark$$

$$+59 \frac{24"Co}{33"} +60 \frac{B.5' Lib. Hdr.}{32} \checkmark$$

$$+41 \frac{28"Co}{38"} +50 \frac{Ent}{21} +41 \frac{20"Co}{54} \checkmark$$

$$+08 \frac{STP}{33} +15 \frac{PP}{28} + \checkmark \quad +12 \frac{PP}{25} \checkmark$$

$$71 \quad +00 \frac{STP}{33} \checkmark \quad \frac{BT}{11-10} \checkmark$$

$$+82 \frac{28"Co}{43} \checkmark$$

$$+72 \frac{End Hedge}{42} +66 \frac{20" M}{43} \checkmark$$

$$+20 \frac{Beg Hanger's Hdr.}{42} +39 \frac{SW Corb.}{100} \checkmark$$

$$+27 \frac{24" M}{43} +13 \frac{Ent}{44} \checkmark +08 \frac{RTic Ent}{21} \checkmark$$

$$20 \quad +00 \frac{Beg Lib. Hdr.}{40-53} \checkmark \quad \frac{BT}{10.9} \checkmark \quad +01 \frac{EGR}{12} \checkmark$$

$$+71.5 \frac{MH}{3.3}$$

$$+85 \frac{STP}{42} \checkmark +92 \frac{12" M}{42} +98 \frac{STP}{26} \checkmark$$

$$+87 \frac{EGR}{H.5} +52 \frac{6" O}{28} +90 \frac{STP}{32} \checkmark$$

$$+29 \frac{PP}{27.5} \checkmark +38 \frac{Tw 4" O}{28} \checkmark$$

$$69 \quad +00 \frac{Ron Willow}{55} \checkmark \quad \frac{GR}{12} \frac{BT}{10-10} \checkmark \quad \frac{GR}{12} \checkmark$$

$$+64 \frac{BGR}{12} +54 \frac{Ent}{21} \checkmark$$

$$+44 \frac{EEGR}{12} +26 \frac{12" O}{42} \checkmark$$

$$68 \quad \frac{GR}{12} \checkmark \quad \frac{BT}{10} \checkmark \quad \frac{GR}{10} \checkmark \quad 12.5 \checkmark$$

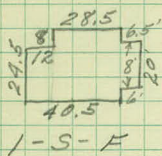
$$+64 \frac{18" Co}{45} +67 \frac{12" Co}{45} \checkmark$$

$$+44 \frac{PP}{26} \checkmark +15 \frac{BGR}{13} \checkmark +16 \frac{Beg G.R.}{F3} \checkmark$$

$$67 \quad +15 \frac{NE Cor Bridge}{13} \checkmark +10 \frac{SE Cor Bridge}{12} \checkmark$$

April, 1957

17.1.



27

 $\frac{BT}{12-10} \checkmark$ 198 $\frac{\text{Extr Wide Ent}}{RT} \checkmark$ 180 $\frac{PP}{28} \checkmark$ +67 $\frac{E, Fe}{32} \checkmark$ +69 $\frac{\text{Lot 82 Lilac}}{30-36} \checkmark$ +18 $\frac{NW, C. Shed}{50} \checkmark$

26

 $\frac{BT}{12-10} \checkmark$ +12 to +24 $\frac{Fe}{32} \checkmark$ Brush 30-35 $\checkmark$ +70 $\frac{MH}{1}$ +20 $\frac{stP}{67} \checkmark$ +18 $\frac{PP}{28} \checkmark$ +19 $\frac{R. Bush}{40-61} \checkmark$ +62 $\frac{NW, C. Barn}{94} \checkmark$ 75 +08 $\frac{D^*P}{42} \checkmark$ $\frac{BT}{12-9} \checkmark$ +32 $\frac{Fe Cor}{32} \checkmark$ +30 $\frac{20^*W}{45} \checkmark$ +93 $\frac{8^*CE}{43} \checkmark$ +67 $\frac{8^*P}{42} \checkmark$ +59 $\frac{J. W. Cor Ho}{81.5} \checkmark$ +62 $\frac{P. Shrub}{44} \checkmark$ +66 $\frac{Juniper}{37} \checkmark$ +46 $\frac{Ent}{11} \checkmark$

24

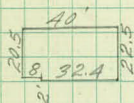
 $\frac{BT}{12-9} \checkmark$ +62 $\frac{Rose Ba}{27} \checkmark$ +66 $\frac{PP}{28} \checkmark$ +50 $\frac{Ent}{14} \checkmark$ +59 $\frac{8^*BE}{52} \checkmark$ +40 $\frac{18^*P_2}{43} \checkmark$ +59 $\frac{15A}{73} \checkmark$ +14 $\frac{24^*M}{43} \checkmark$ +27 $\frac{8^*A}{43} \checkmark$ 73 +08 $\frac{SM, Cor Ho}{89} \checkmark$ $\frac{BT}{12-9} \checkmark$ +84 $\frac{10^*M}{43} \checkmark$ +97 $\frac{21^*BT}{43} \checkmark$ +80 $\frac{End Hedge}{37} \checkmark$ +68 $\frac{MH}{2}$ +42 $\frac{TW 6^*H}{33} \checkmark$ +52 $\frac{12^*BE}{40} \checkmark$ +73 $\frac{Ent}{RT} \checkmark$ +17 $\frac{3^*P_2}{52} \checkmark$ +38 $\frac{PP}{27.0} \checkmark$ +29 $\frac{TW 8^*D}{26} \checkmark$ 72 +06 $\frac{24^*D}{37} \checkmark$ $\frac{BT}{12-10} \checkmark$

FK
RG
KP
JT

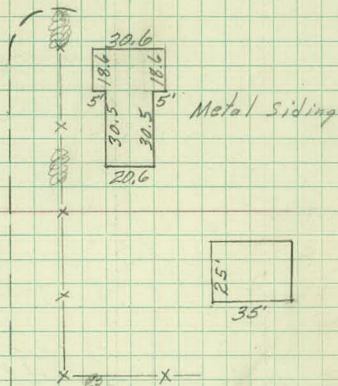
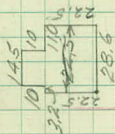
April 2, 1957

18

1-S-S



2-2-F



$$82 \quad 100 \frac{FeCor}{35} \checkmark \quad \frac{BT}{1011} \checkmark$$

$$+59 \frac{PP}{27} \checkmark \quad +69 \frac{37E}{62} \checkmark$$

$$+35 \frac{End x Fe}{34} \checkmark$$

$$81 \quad \frac{BT}{1011} \checkmark$$

$$+97 \frac{Ent}{17} \checkmark$$

$$+88 \frac{FeCor}{29}$$

$$+85 \frac{RHe Fe}{21} \checkmark$$

$$+49 \frac{Tw12BE}{36} \checkmark$$

$$+A2 \frac{SWCorHo}{40} \checkmark$$

$$+84 \frac{10M}{43} \checkmark$$

$$+41 \frac{6BE}{32} \checkmark$$

$$+18 \frac{CorFe}{30} \checkmark$$

$$+28 \frac{8CA}{54}$$

$$+28 \frac{26BE}{57}$$

$$+30 \frac{NWCorHo}{33} \checkmark$$

$$80 \quad 100 \frac{PP}{27} \checkmark$$

$$\frac{BT}{1111} \checkmark$$

$$+82 \frac{Ent}{RT} \checkmark$$

$$+54 \frac{36CH}{52} \checkmark$$

$$+17 \frac{Tw12BE}{30} \checkmark$$

$$+04 \frac{5BE}{32} \checkmark$$

$$+10 \frac{NWCorHo}{38} \checkmark$$

$$79 \quad +12 \frac{ER}{12} \checkmark$$

$$\frac{BT}{1111} \checkmark$$

$$+13 \frac{ER}{10} \checkmark$$

$$+71 \frac{MH}{0.5}$$

$$+80 \frac{BR}{48} \checkmark$$

$$+A4 \frac{ArchLt.}{28} \checkmark$$

$$+61 \frac{ER}{19} \checkmark$$

$$+61 \frac{ER}{51} \checkmark$$

$$+80 \frac{BR}{47} \checkmark$$

$$+31 \frac{BR}{12.5} \checkmark$$

$$+24 \frac{BR}{10} \checkmark$$

$$+A2 \frac{End Lilac Hedge}{32} \checkmark$$

$$78 \quad \frac{BT}{1210} \checkmark$$

$$+02 \frac{8E}{33} \checkmark$$

$$+A1 \frac{240}{57} \checkmark$$

$$+61 \frac{12P}{34} \checkmark$$

$$+42 \frac{12BE}{34} \checkmark$$

$$+45 \frac{18BE}{43} \checkmark$$

$$+49 \frac{NWCorHo}{49} \checkmark$$

$$\frac{BT}{1210} \checkmark$$

$$+22 \frac{PP}{31} \checkmark$$

$$+23 \frac{Tw14BE}{45} \checkmark$$

$$+23 \frac{Lilac}{63} \checkmark$$

$$77 \quad \frac{BT}{1210} \checkmark$$

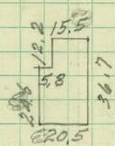
April 2, 1957

19

2-S-S

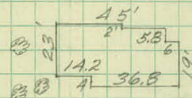


6" Abandon Foundation



1 1/2 - S - F

~~~~~



2-2-F

BT  
12 9

87

+71  $\frac{Sig}{59}$  → +67  $\frac{Sig}{43}$

+195  $\frac{STP}{37}$  +183  $\frac{NW Cor Ho}{140}$   
+188  $\frac{STP}{38}$  +167  $\frac{CE 4"}{39}$  +185  $\frac{6"E}{76}$   
+57 Ent 12" X 24 CM  
20  
+22  $\frac{NW Cor Ho}{75}$

BT  
12-10.5 ↓

86

+91  $\frac{PP}{29}$

+163  $\frac{2'Hedges}{38}$

+145  $\frac{10"A}{64}$  ↓

BT  
12 10 ↓

+16  $\frac{NE Cor Ho}{87.5}$  ↓

+86  $\frac{RSH}{63}$  ↓

+65  $\frac{PP}{28}$  ↓

+82  $\frac{ER}{10}$  ↓

+73  $\frac{10"P}{71}$  ↓

+71  $\frac{8"P}{69}$  ↓

+65  $\frac{PP}{41}$

+78  $\frac{P. Sh}{60}$  *Pre-shrub*

+13  $\frac{5"E}{29}$  ↓

+58  $\frac{BR}{42}$  ↓

+70  $\frac{P. Sh}{64}$  ↓

+100  $\frac{ER}{43}$  ↓

BT  
11 11 ↓

+108  $\frac{BR}{70}$  ↓

+102  $\frac{5"E}{29}$  ↓

+95  $\frac{6"E}{31}$  ↓

84

+16  $\frac{SW Cor Ho}{77}$  ↓

83

+15  $\frac{PP}{27}$  ↓

BT  
11 11 ↓

+89  $\frac{Ent}{Lt}$  ↓

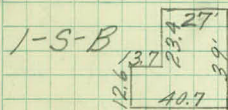
+141  $\frac{SW Cor Ho}{74.5}$  +55  $\frac{Ch 12'Silo}{57}$  ↓

82

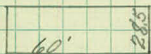
+48  $\frac{E. Fe}{32}$  ↓

BT  
10 11 ↓

26.6 20  
30



24.5  
GO



92

$$\frac{BT}{11 \ 10}$$

$$\frac{Woods}{34}$$

$$+97 \frac{Ent \ 1}{21}$$

$$+59 \frac{PP}{29}$$

$$+25 \frac{Cor Woods}{35}$$

$$+15 \frac{Sign}{45} \text{ to } +18 \frac{Sign}{38}$$

91

$$\frac{BT}{11 \ 10}$$

$$+93 \frac{15" \times 62' \times D \ CM}{32.5 - 29.5}$$

$$+28 \frac{PP}{29}$$

$$\frac{BT}{11 \ 10}$$

90

$$+88 \frac{Sign}{34}$$

$$+83 \frac{Sign}{46}$$

$$+76 \frac{Sign}{54}$$

89

$$\frac{BT}{11 \ 10}$$

$$+96 \frac{PP}{29}$$

$$+39 \frac{Ent \ 12" \times 29' \ CM}{20}$$

$$+35 \frac{7" \ 8' \ 8"}{38}$$

88

$$\frac{BT}{12 \ 9}$$

$$+71 \frac{Sign}{39} \rightarrow +78 \frac{Sign}{45}$$

$$+29 \frac{14" \ E}{82}$$

$$+18 \frac{Row \ 6" \ Willows}{43 - @ \ 8'}$$

$$+15 \frac{PP}{29}$$

$$+14 \frac{PP}{29.5}$$

$$\frac{BT}{12 \ 9}$$

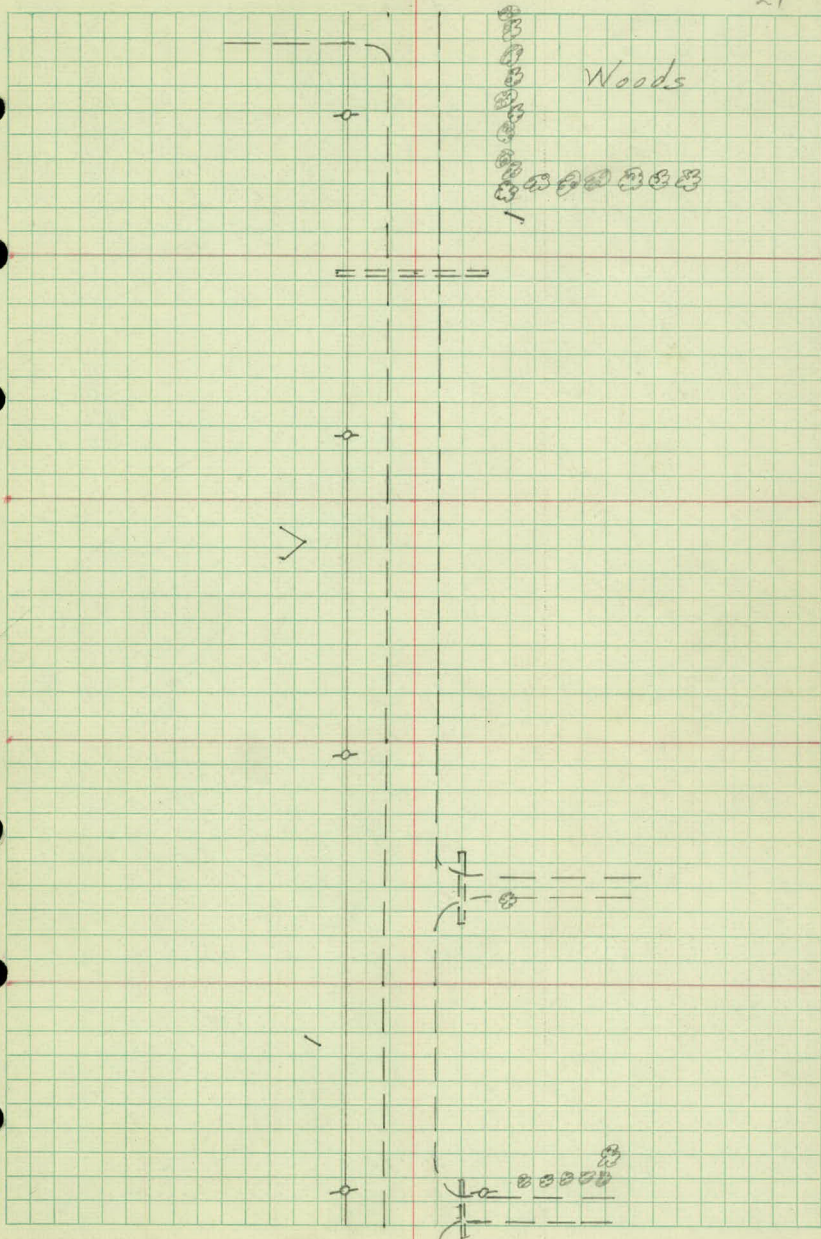
$$+07 \frac{Ent \ 12" \times 24' \ CM}{20}$$

87



April 2, 1957

21



27

31 9.33  
6.9  
19.5

BT  
12 9

96

+68 Ent 15'x20'CM  
23  
+81 36" M  
37  
+52 Tn 20' M  
37 +33 NW Cor Ho  
116  
BT  
11 9.5 +21 Tn 18' M  
38

95

+52 Arc Lt  
28

+63 18'x49'CM  
28-21

+31 ER  
36 +48 BR  
42 +72 ER  
08  
BT  
11 9 +10 BR  
9 +11 8" M  
46  
+77 2 1/2 ac  
38 +88 2 1/2 ac  
38 +88 56  
8" E  
+69 34 +66 10' M  
55 +82 35  
28.3  
+46 NW Cor Ho  
76 +52 6" E  
34 +61 34  
14" E  
+25 X-Hedge  
34 +41 6" E  
14  
BT  
11 10 +05 10' E  
35 +23 8" E  
35  
+56 Steps 2' 10'x6'CM  
22.5 +64 6" P  
42 56  
+38 35 +50 8" P  
13" E  
+35 NW Cor Ho  
66 +35 5" E  
35 +86 6" E  
35  
+05 5' Cor  
35 +06 PP  
29 +15 10' BE  
58

94

+22 PP  
28

+105 10' E  
35 +23 35  
6" P  
+56 Steps 2' 10'x6'CM  
22.5 +64 56  
42 56  
+38 35 +50 8" P  
13" E  
+35 NW Cor Ho  
66 +35 5" E  
35 +86 6" E  
35  
+05 5' Cor  
35 +06 PP  
29 +15 10' BE  
58

93

BT  
10-10 +00 29 Wall  
55

+91 PP  
29

+82 Ent  
33 +96 Arc  
34  
+94 4' Brick Slope Protection  
33 Co Ho  
+69 R Tie Ent  
BT +95 E 15'x32.5' CM  
29  
+68 Cor Woods  
51

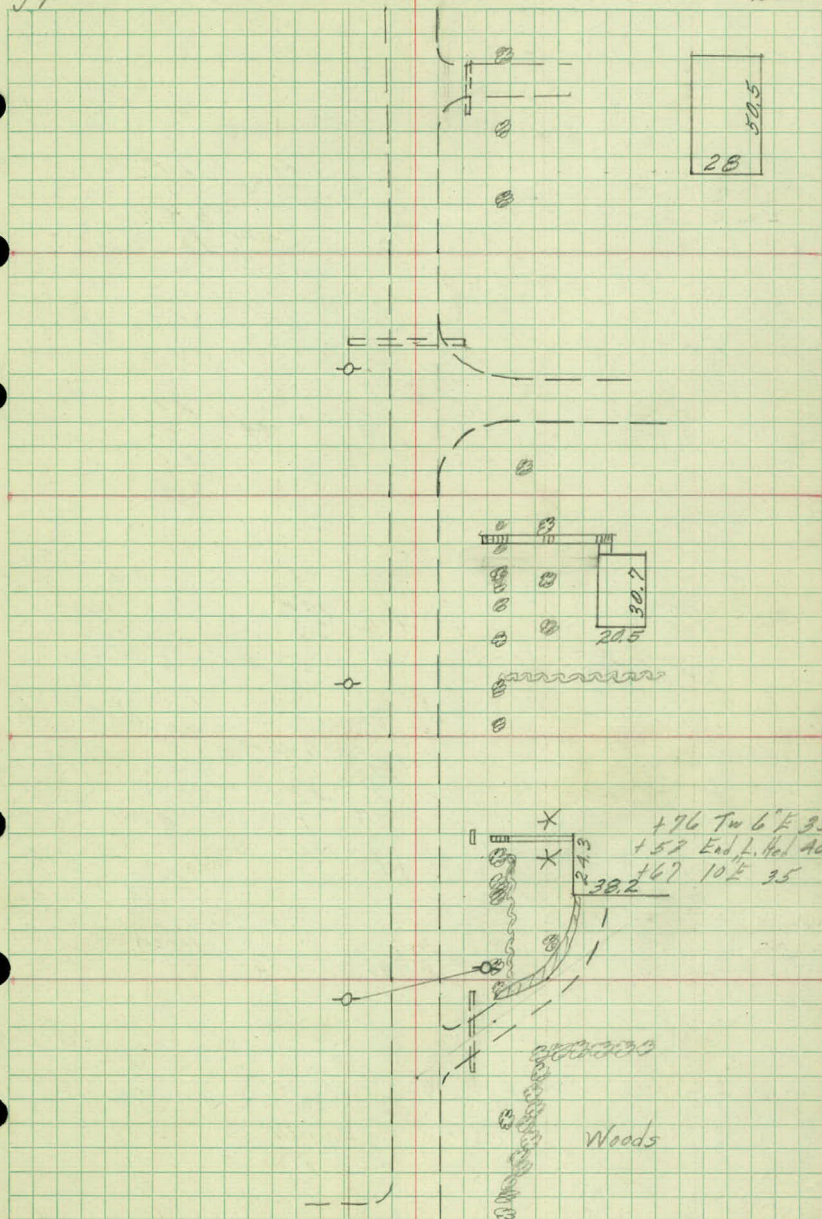
92

+43 12' CM  
37

FK  
RG  
KP  
JT

April 8, 1957  
Clear Cool 25°

22





102

BT  
11 11+84  $\frac{PP}{28}$ +73  $\frac{8''M}{35}$ 

101

$$\begin{array}{r} +39 \frac{BR}{35} \\ BT \\ 11 \ 10 \end{array} \quad \begin{array}{r} +59 \frac{ER}{10} \\ +109 \frac{BR}{70} \end{array} \quad +123 \frac{ER}{35}$$
+38  $\frac{SW \text{ Cor Ho}}{78}$ +80  $\frac{20''M}{37}$ 

100

+25  $\frac{PP}{28}$ +48  $\frac{20''M}{37}$ +105  $\frac{ER}{11.5}$ BT  
10+117  $\frac{Tw 10''M}{37}$ +81  $\frac{BR}{41}$ +86  $\frac{Tw 12''M}{38}$ +47  $\frac{PP}{28}$ +55  $\frac{ER}{49}$  +56  $\frac{14''M}{38}$ +41  $\frac{BR}{11}$ 

99

BT  
11 10+25  $\frac{15''M}{38}$ +40  $\frac{Ent}{41}$ +90  $\frac{R, T, \text{ Cor Ho}}{41}$ +84  $\frac{N.W. \text{ Cor Ho}}{117}$ +97  $\frac{24''M}{38}$ +75  $\frac{SW \text{ Cor Ho}}{23}$ +72  $\frac{Cospeel}{55}$ +89  $\frac{Cospeel}{66}$ +28  $\frac{PP}{28}$ 

98

BT  
115 9+34  $\frac{30''M}{38}$ +29  $\frac{Ent}{Lt.}$ +44  $\frac{24''M}{38}$ +74  $\frac{30''M}{38}$ 

+

+13  $\frac{24''M}{37}$ +106  $\frac{NW \text{ Cor Ho}}{116}$ 

97

+11  $\frac{PP}{28}$ 

12 9

+103  $\frac{Ent}{23} \times 20' \text{ CM}$



April 8, 1957

23

30.4 N  
41.6 E

30.4  
41.6

42.5 N  
28.5 E

28.5  
42.5

30.4  
48.2

24.3  
46.6

107  $\frac{BT}{10 \ 12}$   
 $\frac{12 \times 24 \text{ EN}}{23}$   
 +75  $\frac{\text{Plank Wall}}{48 \text{ P}}$  +81  $\frac{SW \text{ Cor H}_0}{81}$   
 169  $\frac{6 \text{ E}}{44}$  159  $\frac{PP}{28}$  132  $\frac{SW \text{ Cor H}_0}{81}$   
 163  $\frac{\text{Sign}}{44 \text{ to } 69 \text{ B1}}$   
 162  $\frac{PP}{65}$   
 106  $\frac{Row L.P.}{43}$   
 $\frac{BT}{10 \ 11}$   $\frac{N \text{ Cor H}_0}{101 \ 74}$   
 105  $\frac{ER}{11 \ 11}$  +124  $\frac{ER}{11}$  +104  $\frac{BR}{40}$  +102  $\frac{R \text{ Tie}}{40 \ 84}$   
 +96  $\frac{PP}{26}$   
 104  $\frac{BT}{11 \ 11}$  +157  $\frac{BR}{11}$  +182  $\frac{ER}{39}$  +102  $\frac{3" \text{ Pine}}{58}$   
 +199  $\frac{N \text{ Cor H}_0}{73.5}$   
 +142  $\frac{\text{Arc Lt}}{28}$  +126  $\frac{R \text{ Tie H}_0}{RT}$  +164  $\frac{\text{Ent}}{RT}$   
 +143  $\frac{14" \text{ M}}{35}$   
 106  $\frac{8' \text{ Conc Ent}}{34}$  +125  $\frac{\text{Sign}}{42 \text{ to } 130 \ 35}$   
 103  $\frac{\text{Ent } 12" \times 20 \text{ CM}}{103 \ 23}$   $\frac{BT}{11 \ 11}$  +15  $\frac{PP}{64}$   
 197  $\frac{SW \text{ Cor H}_0}{74}$   
 102  $\frac{R \text{ Tie H}_0}{RT}$  +129  $\frac{RT}{RT}$  +139  $\frac{14" \text{ M}}{37}$   
 +10  $\frac{N \text{ Cor H}_0}{77}$

April 8, 1957  
April 15, 1957

2A

1-S-F

36.5  
24.4

0000000

1-S-S

44.5  
24.3

1-S-B

24.2  
44.3

1-S-F

64.5  
23.6

1-S-B

24.7  
45.4



113

112

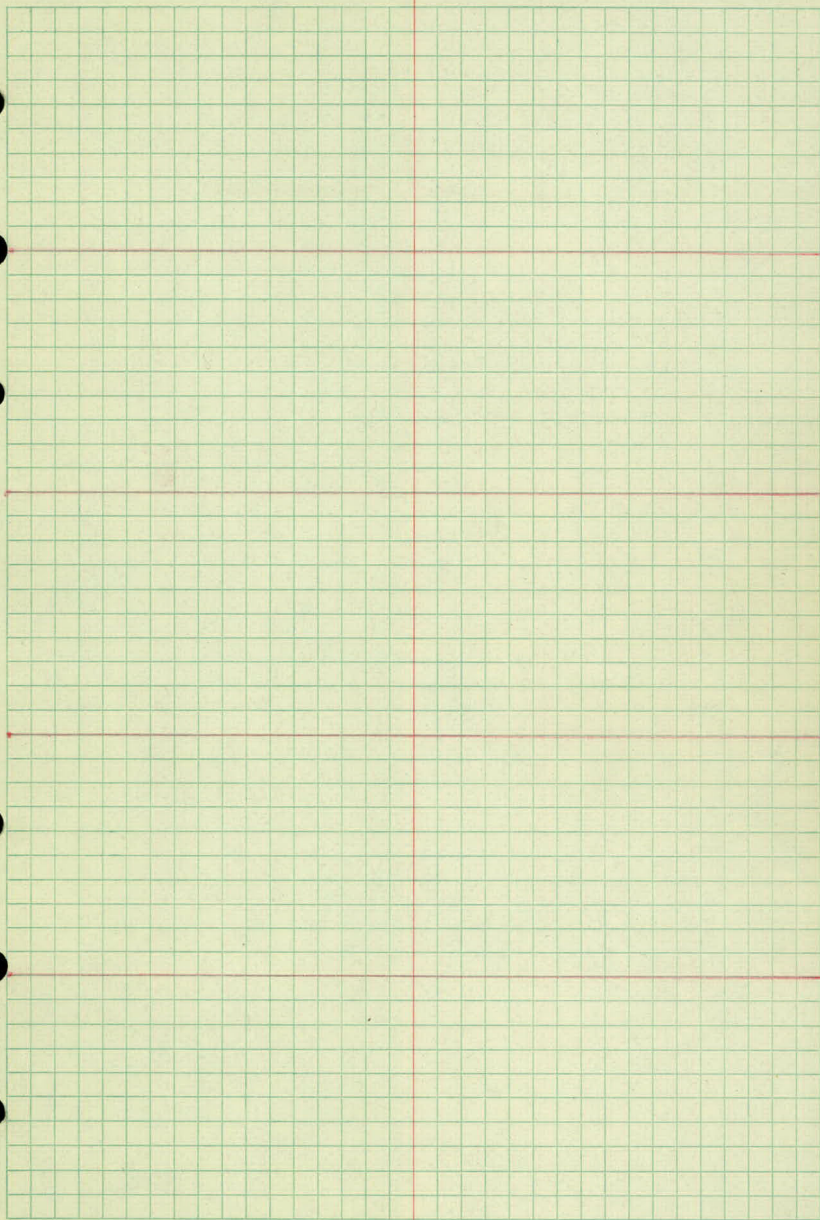
111

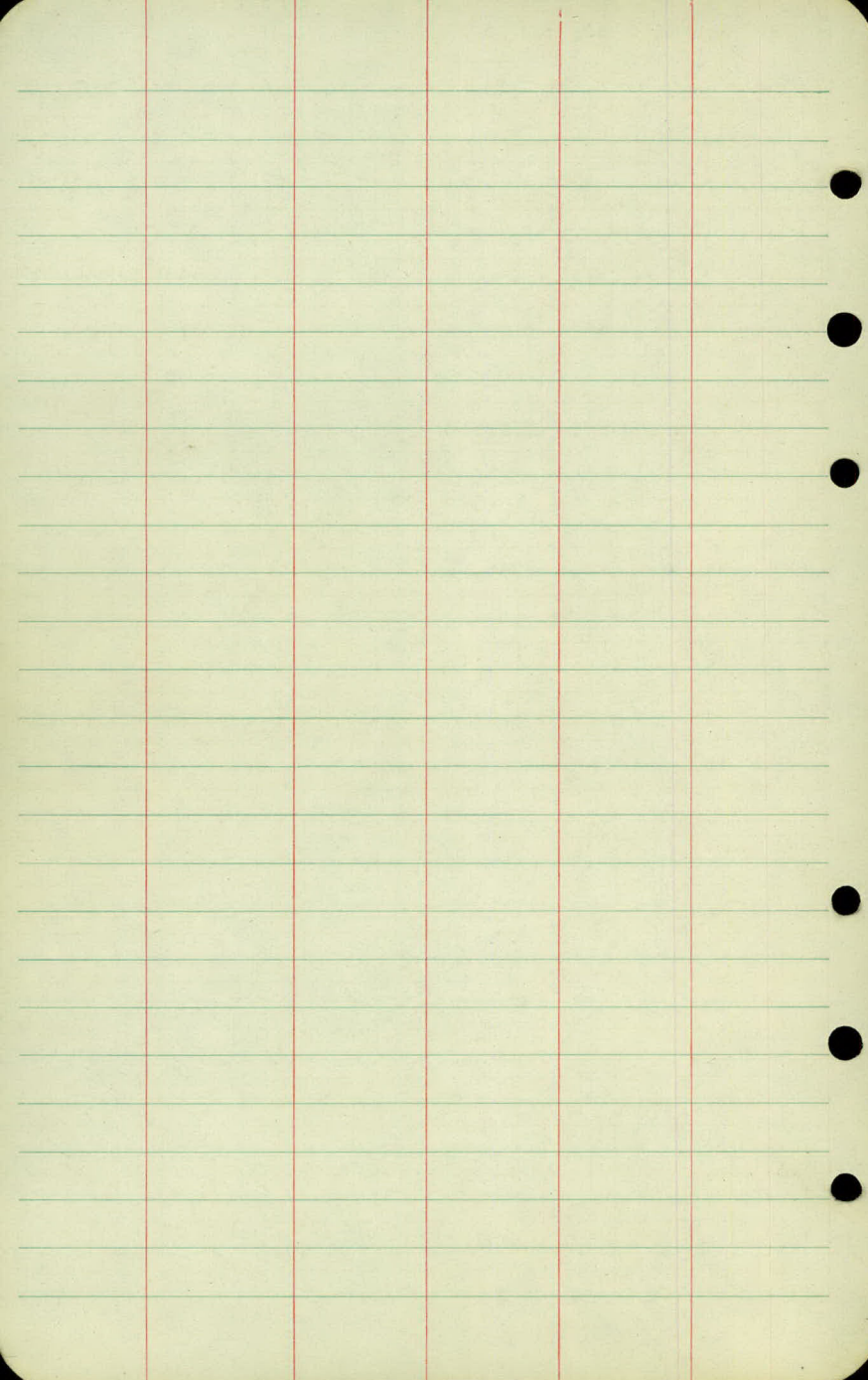
110

109

108







PK W N  
RG T N  
KP T T  
WH T T

Feb 26, 1957  
Cold Windy 10°

a

Bench Levels

| Sta              | +      | $\pi$   | -      | Elev.   |
|------------------|--------|---------|--------|---------|
| BM               | 0.72   | 931.270 |        | 930.55  |
| TP1              | 3.24   | 925.215 | 9.295  | 921.975 |
| BM <sub>1</sub>  |        |         | 7.145  | 918.070 |
| TP2              | 6.353  | 918.468 | 13.100 | 912.115 |
| TP3              | 11.364 | 929.138 | 0.694  | 917.774 |
| TP4              | 10.632 | 937.038 | 2.732  | 926.406 |
| TP <sub>5</sub>  | 3.038  | 939.905 | 0.171  | 936.867 |
| BM <sub>2</sub>  |        |         | 0.656  | 939.249 |
| TP <sub>6</sub>  | 0.698  | 927.539 | 13.064 | 926.841 |
| BM <sub>3</sub>  |        |         | 9.723  | 917.816 |
| TP <sub>7</sub>  | 3.929  | 918.224 | 13.244 | 914.295 |
| TP <sub>8</sub>  | 1.719  | 910.887 | 9.056  | 909.168 |
| TP <sub>9</sub>  | 13.751 | 924.038 | 0.600  | 910.287 |
| BM <sub>4</sub>  |        |         | 0.062  | 923.976 |
| TP <sub>10</sub> | 0.143  | 923.058 | 1.123  | 922.915 |
| TP <sub>11</sub> | 8.730  | 927.316 | 4.472  | 918.586 |
| BM <sub>5</sub>  |        |         | 1.685  | 925.631 |
| TP <sub>12</sub> | 1.814  | 924.835 | 4.295  | 923.021 |
| TP <sub>13</sub> | 10.514 | 932.043 | 3.306  | 921.529 |
| BM <sub>5</sub>  |        |         | 0.626  | 931.417 |

Figures  
checked  
X



Feb 26, 1957

b

U.S. G.S. BM C-31 N.E. Cor White Bear Ave & Co Rd "C"

NAIL IN POWER POLE # 1097

EAST END OF FRONT DOOR SILL HOUSE # 1861.

EAST END OF CULVERT N.E. CORNER BRIEF ST. + "C"

TOP OF GUARD RAIL POST

Nail in PP at Southlawn Drive

E. End Front Door Sill Ho # 1763 E Co Rd "C"

Top W. End Water table Ho. # 2647 Gem St.

Gas pipe elbow at Ho # 2647 Gem St.

Nail in PP

W. End Front Door sill Ho # 1616 E Co. Rd. "C"

Nail in PP # 198

Nail in PP 100' E & 30' N of Hazelwood  $\frac{1}{2}$  Co. Rd C.

Top NW. Cor Lower step Ho # 1534 E Co Rd "C"

Nail in Power Transformer Pole

Top G.R. Post Easternmost on N. Side Co Rd "C"

Top W. Edge T iron Reflector post N.E. Cor Bridge 

Sta +  $\pi$  - Elev.

932.043

TP<sub>14</sub> 0.506 923.617 8.932 923.111

BM<sub>6</sub> 1.106 918.033 6.690 916.927

TP<sub>15</sub> 0.178 908.848 9.363 908.670

BM<sub>7</sub> 4.190 899.687 13.351 895.497 \*

TP<sub>16</sub> 1.702 898.834 2.555 897.132

TP<sub>17</sub> 5.702 896.353 8.183 890.651

TP<sub>18</sub> 3.620 894.788 5.185 891.168

TP<sub>19</sub> 5.462 895.057 5.193 889.595

BM 4.69 890.367 (890.37) 003

BM<sub>8</sub> 3.067 891.990

BM 5.322 935.872 (930.55)

TP<sub>1</sub> 4.127 934.344 5.655 930.217

BM<sub>1</sub> 9.168 934.663 8.849 925.495 (925.495)

BM 5.551 929.112 (929.11)

TP<sub>2</sub> 8.625 942.363 0.925 933.738 (933.738)

TP<sub>3</sub> 11.878 951.766 2.475 939.888 ✓

TP<sub>4</sub> 12.980 964.402 0.344 951.422 ✓

BM 8.432 965.990 6.844 957.558 (957.558) ✓

FK <sup>H</sup>  
RG <sup>1</sup> <sup>X</sup>  
KP <sup>X</sup>  
WH <sup>P</sup>

Feb 26, 1957  
Feb 27, 1957  
Cold 13° Windy

C

Nail in End G.R. Post.

Top S. End 2 1/2" Nail Box Post #1386 E.C. Rd "C"

Nail in Transformer P.P.

|   |     |
|---|-----|
| 3 | WSP |
| 3 | 535 |
| 5 | 1   |
|   | 4   |

Spike in Arc Lt. Post <sup>#330</sup> By H. #1337 E.C. Rd "C"

Nail in Transformer P.P.

Top E. End Double Ent Culvert #1255-57 E.C. Rd "C"

Nail in P.P. #349

N. Side of Metal Doorsill of W. Door School Host STH #61

Spike in Switch Power Pole <sup>#618</sup> at School Alley Ent 4 "C"

U.S.G.S. BM C-31 N.E. Cor White Bear Ave & Co. Rd "C"

Top iron Rt by 1st TP Rt

Top S. End 12" X-drain - 200 W. of Ariel St.

Top Manht at Ariel & Co. Rd "C"

Nail in PP

Nail in PP at Ent to #701 W 17th Ave.

Top Hyd By Sta 149±



- 001

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

965.990

|    |       |         |       |         |         |
|----|-------|---------|-------|---------|---------|
| BM | 3.876 | 969.386 | 0.480 | 965.510 | 965.510 |
|----|-------|---------|-------|---------|---------|

|    |       |         |       |         |         |
|----|-------|---------|-------|---------|---------|
| BM | 4.578 | 969.904 | 4.060 | 965.326 | 965.332 |
|----|-------|---------|-------|---------|---------|

|    |       |         |       |         |         |
|----|-------|---------|-------|---------|---------|
| BM | 2.136 | 968.551 | 3.489 | 966.415 | 966.421 |
|----|-------|---------|-------|---------|---------|

|    |       |         |       |         |         |
|----|-------|---------|-------|---------|---------|
| BM | 3.232 | 969.262 | 2.521 | 966.030 | 966.036 |
|----|-------|---------|-------|---------|---------|

|    |       |         |       |         |         |
|----|-------|---------|-------|---------|---------|
| BM | 3.220 | 971.077 | 1.405 | 967.857 | 967.851 |
|----|-------|---------|-------|---------|---------|

|    |       |         |       |         |        |
|----|-------|---------|-------|---------|--------|
| BM | 5.787 | 976.682 | 0.182 | 970.895 | 970.89 |
|----|-------|---------|-------|---------|--------|

|                 |        |         |       |         |  |
|-----------------|--------|---------|-------|---------|--|
| TP <sub>5</sub> | 12.545 | 988.309 | 0.918 | 975.764 |  |
|-----------------|--------|---------|-------|---------|--|

|                 |        |          |       |         |  |
|-----------------|--------|----------|-------|---------|--|
| TP <sub>6</sub> | 13.584 | 1001.258 | 0.635 | 987.674 |  |
|-----------------|--------|----------|-------|---------|--|

|                 |       |          |       |         |  |
|-----------------|-------|----------|-------|---------|--|
| TP <sub>7</sub> | 7.980 | 1005.567 | 3.671 | 997.587 |  |
|-----------------|-------|----------|-------|---------|--|

|                 |       |          |       |          |          |
|-----------------|-------|----------|-------|----------|----------|
| BM <sub>2</sub> | 0.250 | 1004.700 | 1.117 | 1004.450 | 1004.450 |
|-----------------|-------|----------|-------|----------|----------|

|                 |       |          |       |         |  |
|-----------------|-------|----------|-------|---------|--|
| TP <sub>8</sub> | 4.453 | 1002.507 | 6.646 | 998.054 |  |
|-----------------|-------|----------|-------|---------|--|

|                 |  |  |       |          |          |
|-----------------|--|--|-------|----------|----------|
| BM <sub>3</sub> |  |  | 2.185 | 1000.322 | 1000.322 |
|-----------------|--|--|-------|----------|----------|

|                   |       |         |        |         |  |
|-------------------|-------|---------|--------|---------|--|
| T.P. <sub>9</sub> | 3.958 | 993.119 | 13.346 | 989.161 |  |
|-------------------|-------|---------|--------|---------|--|

|                    |       |         |       |         |  |
|--------------------|-------|---------|-------|---------|--|
| T.P. <sub>10</sub> | 6.691 | 997.841 | 1.969 | 991.150 |  |
|--------------------|-------|---------|-------|---------|--|

|                 |  |  |       |         |         |
|-----------------|--|--|-------|---------|---------|
| BM <sub>4</sub> |  |  | 3.072 | 994.769 | 994.769 |
|-----------------|--|--|-------|---------|---------|

|                  |       |          |       |         |  |
|------------------|-------|----------|-------|---------|--|
| TP <sub>11</sub> | 3.295 | 1000.811 | 0.325 | 997.516 |  |
|------------------|-------|----------|-------|---------|--|

|                 |       |          |       |         |         |
|-----------------|-------|----------|-------|---------|---------|
| BM <sub>5</sub> | 0.656 | 1000.462 | 1.005 | 999.306 | 999.795 |
|-----------------|-------|----------|-------|---------|---------|

|                  |       |         |       |         |  |
|------------------|-------|---------|-------|---------|--|
| TP <sub>12</sub> | 4.143 | 994.655 | 9.950 | 990.512 |  |
|------------------|-------|---------|-------|---------|--|

|                 |  |  |       |         |         |
|-----------------|--|--|-------|---------|---------|
| BM <sub>6</sub> |  |  | 1.955 | 992.700 | 992.689 |
|-----------------|--|--|-------|---------|---------|



Feb 27, 1957

d

Top Hyd 1<sup>st</sup> Sta 148+30<sup>±</sup>

Top Hyd Front Ho # 435 W 17<sup>th</sup> Ave

Top Hyd B<sub>y</sub> Ho # 345 W 17<sup>th</sup> Ave #2295 C

Top Hyd N.W. Cor Delaware + Co Rd "C"

Top Hyd Across from Ho # 232 W 17<sup>th</sup> Ave.

Top Hyd S.E. Cor. 2<sup>nd</sup> St + 17<sup>th</sup> Ave = C

Cor step

Top Hyd N.E. Cor Bellaire + Co Rd "C"

Top Hyd N.E. Cor Margaret + Co Rd "C"

NW Cor 1<sup>st</sup> Step Store

Top Hyd NW Cor Charles + Co Rd "C"

S.W. Cor E. Portch Ent Well

Top Hyd N.E. Cor Henry St + Co Rd "C"

Top Water Shut off No Side

Top Hyd N.W. Cor. Co. Rd. "C"  $\frac{1}{2}$  E. Co. Line

| Sta                | +     | $\pi$    | -      | Elev.    |                      |
|--------------------|-------|----------|--------|----------|----------------------|
| BM <sub>6</sub>    | 1.990 | 994.690  |        | 992.700  |                      |
| TP                 | 7.648 | 1000.474 | 1.864  | 992.826  |                      |
| BM <sub>5</sub>    | 0.571 | 1000.377 | 0.668  | 999.806  |                      |
| TP                 | 3.659 | 997.418  | 6.618  | 993.759  |                      |
| BM <sub>4</sub>    |       |          | 2.638  | 994.780  |                      |
| BM <sub>5</sub>    | 1.007 | 1000.813 |        | 999.806  |                      |
| TP <sub>11</sub>   |       |          | 3.291  | 997.522  | + .006               |
| TP                 | 3.802 | 997.562  | 7.053  | 993.760  |                      |
| BM <sub>4</sub>    |       |          | 2.782  | 994.780  | .011                 |
| T.P. <sub>10</sub> | 2.220 | 993.376  | 6.406  | 991.156  | + .006               |
| T.P.               | 9.980 | 1000.455 | 2.901  | 990.475  |                      |
| BM <sub>3</sub>    | 2.635 | 1002.965 | 0.125  | 1000.330 | + .008<br>300        |
| TP                 | 5.249 | 1005.584 | 2.630  | 1000.335 | .014<br>+ .022       |
| BM <sub>2</sub>    |       |          | 1.112  | 1004.472 | 1004.450             |
| T.P.               | 1.888 | 997.242  | 10.230 | 995.354  |                      |
| T.P. <sub>13</sub> | 2.590 | 987.908  | 11.924 | 985.318  |                      |
| BM                 |       |          | 10.448 | 977.460  | + .036<br>800<br>764 |
| TP <sub>5</sub>    | 1.269 | 977.069  | 12.108 | 975.800  |                      |
| TP                 | 1.538 | 974.298  | 4.309  | 972.760  | + .022<br>716        |
| BM                 | 0.257 | 971.173  | 3.382  | 970.916  | 970.895<br>21        |

FR  
RG  
KP  
WH

Feb 28, 1951  
Cool Clear 29°

e

Top Hyd N.W. Cor Co Rd "C" & E. Co. Line

Manhole

Top Hyd. N.E. Cor. Henry St.  $\frac{1}{2}$  Co Rd "C"

Manhole

Top Hyd NW Cor Charles  $\frac{1}{2}$  Co Rd "C"

Top Hyd N.E. Cor Henry St & Co Rd "C"

M.H.

Top Hyd N.W. Cor Charles & Co Rd "C"

Fe. P

Top Hyd N.E. Cor Margaret & Co Rd "C"

Top Hyd N.E. Cor Bellaire & Co Rd "C"

N.W. Cor Lower step

Spike in PP S.E. Cor 1<sup>st</sup> St & Co Rd "C"

Nail in Tree Root

Top Hyd S.E. Cor 2<sup>nd</sup> St & Co Rd "C"

Sta +  $\pi$  - E/ev

971.173

BM 1.355 969.239 3.289 967.884 ✓

BM 2.672 968.741 3.170 966.069 ✓

BM 2.870 969.321 2.290 966.451

TP 3.085 969.328 3.078 966.243

BM 3.695 969.060 3.963 965.365

TP 5.129 968.999 5.190 963.870 } .016

BM 0.836 966.369 3.466 965.533

BM 0.090 957.669 8.790 957.579

TP 1.349 948.695 10.323 947.346

TP<sub>3</sub> 0.449 940.355 8.789 939.906

TP<sub>2</sub> 2.435 936.191 6.599 933.756

BM 7.065 929.126

TP 3.555 933.575 6.171 930.020

BM, 8.070 925.505 ✓

TP 5.498 934.905 4.168 929.407 009

TP, 5.765 935.983 4.687 930.218 ✓

BM 5.436 930.547



Feb 28, 1957

f

Top Hyd across from Ho #232 W 17<sup>th</sup> Ave

Top Hyd N W Cor Delaware & Co Rd "C"

Top Hyd By Ho #345 W 17<sup>th</sup> Ave

Top Hyd Front of Ho #435 W 17<sup>th</sup> Ave

Nail in PP

Top Hyd Lt. Sta 148+50±

Top Hyd By Sta 144±

Top E. End Ent Culvert Ho #634 W 17<sup>th</sup> Ave

Nail in PP at Ent to #701 W 17<sup>th</sup> Ave.

Top Mont at Ariel & Co Rd "C"

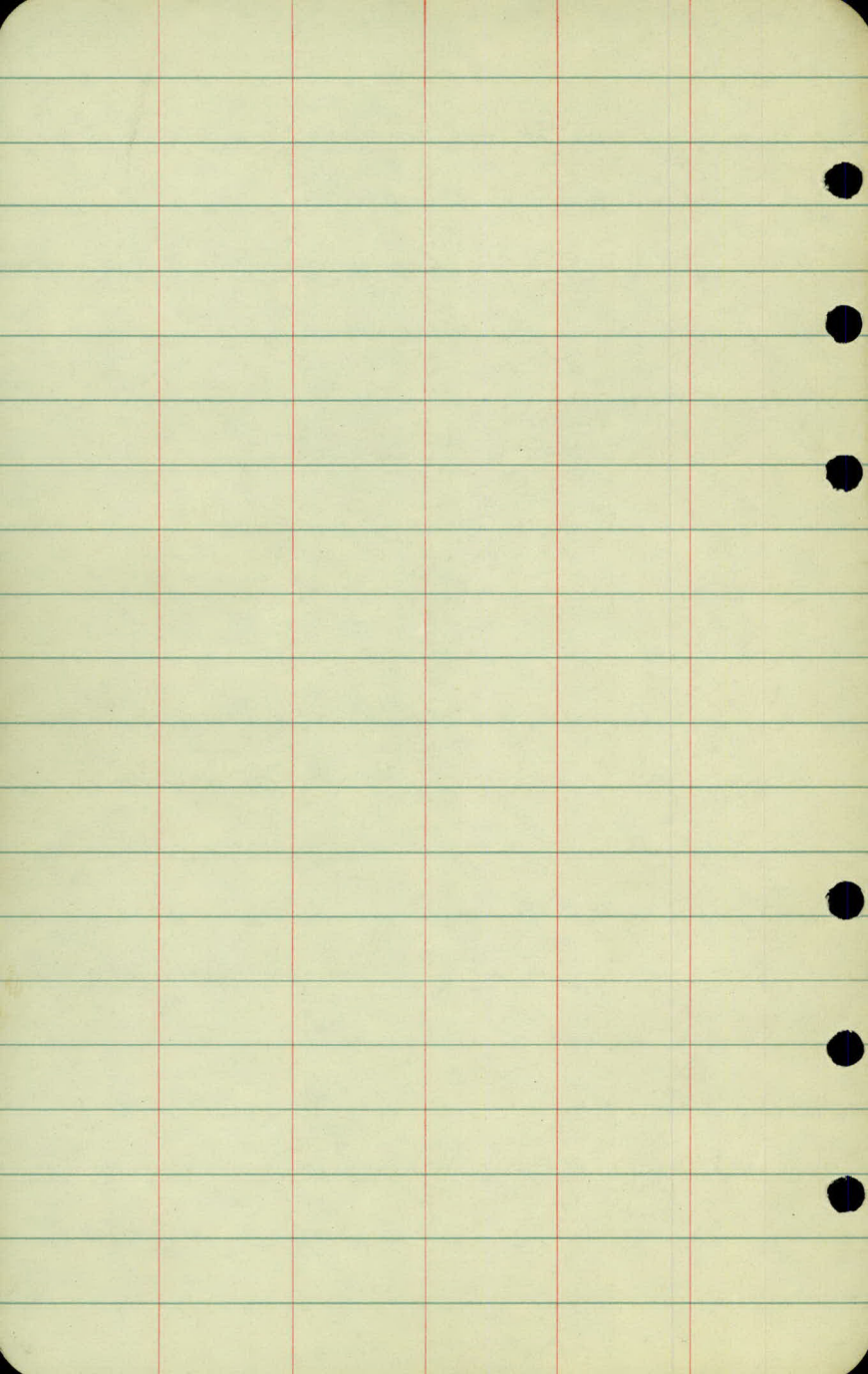
Spike in Arc Lt. Pole S.E. Cor Ariel & Co Rd "C"

Top S End 18" CN X Drain 200' W of Ariel St

Spike in Tree

iron

V.S. GS BM-C31 NE Cor White Bear Ave & Co Rd "C"



1  
Profile

C. R. C.

STH #61 to English

6 pages

| Sta   | +    | $\pi$  | -    | Elev   |
|-------|------|--------|------|--------|
| BM    | 2.99 | 894.98 |      | 891.99 |
| 38+29 |      |        | 7.07 | 87.91  |
| +50   |      |        | 7.5  | 87.5   |
| 39    |      |        | 8.3  | 86.7   |
| +50   |      |        | 7.8  | 87.2   |
| 40    |      |        | 7.1  | 87.9   |
| +50   |      |        | 6.4  | 88.6   |
| 41    |      |        | 5.7  | 89.3   |
| +50   |      |        | 5.3  | 89.7   |
| 42    |      |        | 5.0  | 90.0   |
| +50   |      |        | 4.7  | 90.3   |
| 43    |      |        | 4.4  | 90.6   |
| +50   |      |        | 4.2  | 90.8   |
| 44    |      |        | 4.3  | 90.7   |
| +50   |      |        | 4.2  | 90.8   |
| 45    |      |        | 4.1  | 90.9   |
| +50   |      |        | 3.8  | 91.2   |
| 46    |      |        | 3.5  | 91.5   |
| T.P.  | 7.24 | 898.63 | 3.59 | 891.39 |



FK  
RG  
JS  
JH

Jan 2, 1960  
Clear 35°

2

Spike in Switch PP# 618 at School Alley Ekt 80

£ North Bound Lane

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

898.63

|       |  |  |     |      |
|-------|--|--|-----|------|
| 46+50 |  |  | 6.9 | 91.7 |
|-------|--|--|-----|------|

|    |  |  |     |      |
|----|--|--|-----|------|
| 47 |  |  | 6.7 | 91.9 |
|----|--|--|-----|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 6.5 | 92.1 |
|-----|--|--|-----|------|

|    |  |  |     |      |
|----|--|--|-----|------|
| 48 |  |  | 6.3 | 92.3 |
|----|--|--|-----|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 6.1 | 92.5 |
|-----|--|--|-----|------|

|    |  |  |     |      |
|----|--|--|-----|------|
| 49 |  |  | 5.5 | 93.1 |
|----|--|--|-----|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 4.9 | 93.7 |
|-----|--|--|-----|------|

|    |  |  |     |      |
|----|--|--|-----|------|
| 50 |  |  | 4.4 | 94.2 |
|----|--|--|-----|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 4.0 | 94.6 |
|-----|--|--|-----|------|

|    |  |  |     |      |
|----|--|--|-----|------|
| 51 |  |  | 3.8 | 94.8 |
|----|--|--|-----|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 3.6 | 95.0 |
|-----|--|--|-----|------|

|    |  |  |     |      |
|----|--|--|-----|------|
| 52 |  |  | 3.5 | 95.1 |
|----|--|--|-----|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +40 |  |  | 3.5 | 95.1 |
|-----|--|--|-----|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 3.5 | 95.1 |
|-----|--|--|-----|------|

|      |      |        |      |        |
|------|------|--------|------|--------|
| T.P. | 4.27 | 899.33 | 3.57 | 895.06 |
|------|------|--------|------|--------|

|       |  |  |  |  |
|-------|--|--|--|--|
| 53+43 |  |  |  |  |
|-------|--|--|--|--|

|    |  |  |      |               |
|----|--|--|------|---------------|
| 53 |  |  | 4.51 | 94.82 (94.79) |
|----|--|--|------|---------------|

Jan 7, 1960

3

Lt

£

Rt

£ English

88.6

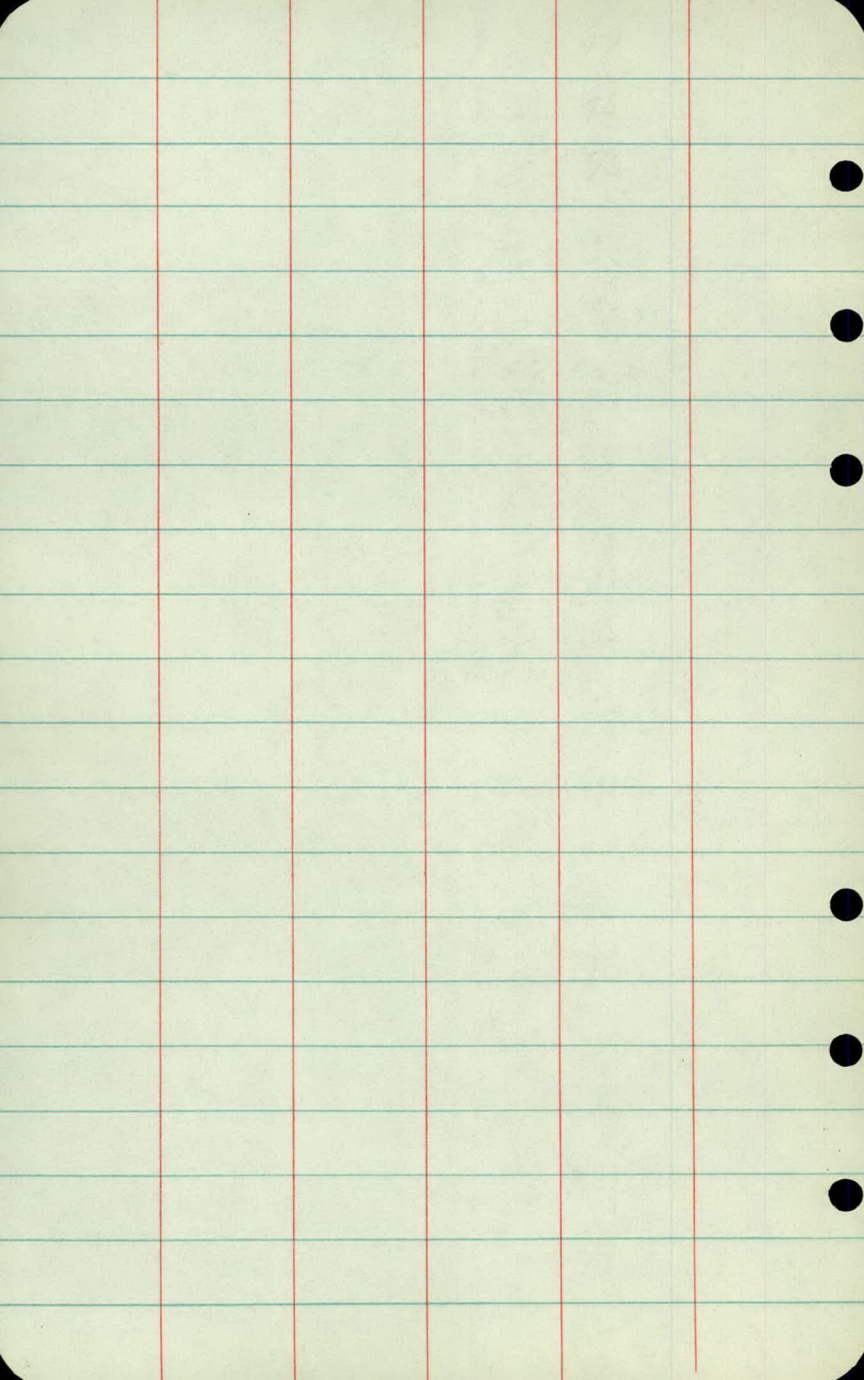
87.40

94.6

88.28 91.4

10.7 11.93 4.7  
Ground Top CM X Drain  
41 41.1

11.05 7.9  
24 24  
Top CM Ground  
X Drain





Dec. 21, 1959

1

X-Sections

Co Rd "C"

English to Hazelwood

42 pages

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

|    |      |        |  |  |
|----|------|--------|--|--|
| BM | 4.23 | 899.73 |  |  |
|----|------|--------|--|--|

|  |  |  |  |        |
|--|--|--|--|--------|
|  |  |  |  | 895.50 |
|--|--|--|--|--------|

|    |  |  |  |  |
|----|--|--|--|--|
| 53 |  |  |  |  |
|----|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +24 |  |  |  |  |
|-----|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +32 |  |  |  |  |
|-----|--|--|--|--|

FX  
RG  
KP  
KJ  
JS  
JH  
Spike

Dec. 21, 1959 2  
RT

14

in Arc H. Pole #330 by Ho #1337 E.C. RBC

|      |      |      |       |      |      |      |      |      |
|------|------|------|-------|------|------|------|------|------|
| 93.1 | 92.6 | 94.6 | 94.79 | 94.6 | 94.4 | 94.1 | 94.4 | 92.4 |
| 6.6  | 7.1  | 5.1  | 4.94  | 5.1  | 5.3  | 5.6  | 5.3  | 7.3  |
| 36   | 22   | 11   |       | 10   | 11   | 16   | 17   | 21   |
| Ho.  |      |      |       |      |      |      |      |      |

|      |      |      |      |
|------|------|------|------|
| 97.7 | 96.7 | 95.5 | 92.4 |
| 20   | 30   | 4.2  | 7.3  |
| 75   | 58   | 35   | 25   |
| Ho   |      |      |      |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 93.0 | 91.8 | 93.9 | 94.3 | 94.4 | 94.7 | 94.3 | 93.9 | 91.4 | 91.8 | 95.6 |
| 6.7  | 7.9  | 5.8  | 5.4  | 5.3  | 5.0  | 5.4  | 5.8  | 8.3  | 7.9  | 4.1  |
| 34   | 25   | 17   | 12   | 10   |      | 11   | 17   | 23   | 27   | 37   |

|      |      |      |
|------|------|------|
| 93.1 | 97.5 | 96.8 |
| 46   | 22   | 29   |
| 61   | 75   | 60   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 88.5 | 89.1 | 93.9 | 94.4 | 94.7 | 94.5 | 94.0 | 91.3 | 91.7 | 95.7 |
| 11.2 | 10.6 | 5.8  | 5.3  | 5.0  | 5.2  | 5.7  | 8.4  | 8.0  | 4.0  |
| 48   | 30   | 17   | 11   |      | 11   | 16   | 23   | 27   | 38   |

|      |      |      |      |
|------|------|------|------|
| 88.9 | 89.0 | 97.4 | 96.8 |
| 10.8 | 10.7 | 2.3  | 2.9  |
| 70   | 75   | 75   | 60   |

Sta

+

$\pi$

-

Elev.

899.73

53+65

✓

54

✓

+50

✓



Dec. 21, 1959

3

14

Rt

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 87.8 | 89.7 | 93.7 | 94.1 | 94.6 | 94.4 | 93.7 | 91.3 | 91.3 | 96.3 |
| 11.9 | 10.0 | 6.0  | 5.6  | 5.1  | 5.3  | 6.0  | 8.4  | 8.4  | 8.4  |
| 34   | 285  | 16   | 12   | 11   | 17   | 23   | 30   | 30   | 39   |

|      |      |      |      |  |  |  |      |      |  |
|------|------|------|------|--|--|--|------|------|--|
| 88.2 | 88.5 | 88.2 | 88.3 |  |  |  | 92.1 | 96.7 |  |
| 11.5 | 11.2 | 11.5 | 11.4 |  |  |  | 2.6  | 3.0  |  |
| 37   | 37   | 65   | 75   |  |  |  | 75   | 58   |  |

|      |      |      |      |       |      |      |      |      |  |
|------|------|------|------|-------|------|------|------|------|--|
| 89.3 | 92.1 | 93.7 | 94.1 | 94.63 | 94.4 | 94.0 | 91.3 | 91.4 |  |
| 10.4 | 7.6  | 6.0  | 5.6  | 5.10  | 5.3  | 5.7  | 8.4  | 8.3  |  |
| 32   | 23   | 17   | 12   | 10    | 16   | 24   | 31   |      |  |

|      |      |      |  |  |  |      |      |      |  |
|------|------|------|--|--|--|------|------|------|--|
| 87.7 | 87.6 | 87.4 |  |  |  | 98.2 | 97.5 | 97.1 |  |
| 12.0 | 12.1 | 12.3 |  |  |  | 1.5  | 2.2  | 2.6  |  |
| 37   | 52   | 75   |  |  |  | 75   | 62   | 39   |  |

|      |      |      |      |      |      |      |      |      |  |
|------|------|------|------|------|------|------|------|------|--|
| 88.8 | 88.8 | 93.8 | 94.5 | 94.8 | 94.7 | 94.5 | 92.7 | 92.7 |  |
| 10.9 | 10.9 | 5.9  | 5.2  | 4.9  | 5.0  | 5.2  | 7.0  | 7.0  |  |
| 38   | 35   | 18   | 12   | 10   | 17   | 24   | 30   |      |  |

|      |      |      |  |  |  |      |      |      |  |
|------|------|------|--|--|--|------|------|------|--|
| 89.1 | 89.0 | 89.1 |  |  |  | 99.7 | 98.7 | 97.9 |  |
| 10.6 | 10.7 | 10.6 |  |  |  | 0.0  | 1.0  | 1.8  |  |
| 40   | 56   | 75   |  |  |  | 75   | 55   | 37   |  |

Sta +  $\pi$  - Elev

899.73

55

✓

+24

✓

+34

Dec. 21, 1959 4

LT

RT

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 92.1 | 91.6 | 94.5 | 94.9 | 95.2 | 95.1 | 94.8 | 94.0 | 94.4 |
| 7.6  | 8.1  | 5.2  | 4.8  | 4.52 | 4.6  | 4.9  | 5.7  | 5.3  |
| 57   | 36   | 18   | 12   | ✓ 19 | 16   | 20   | 25   |      |

92.0  
7.7  
75

99.5  
0.2  
75

99.2  
0.5  
58

98.3  
96.3  
1.4  
37

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 92.8 | 93.3 | 94.6 | 95.0 | 95.4 | 95.3 | 95.3 | 94.5 | 94.3 |
| 6.9  | 6.4  | 5.1  | 4.7  | 4.3  | 4.4  | 4.4  | 5.2  | 5.4  |
| 53   | 33   | 16   | 12   |      | 9    | 16   | 20   | 26   |

92.7  
7.0  
75

99.6  
0.1  
75

99.2  
0.5  
55

98.3  
96.3  
1.4  
36

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 93.1 | 93.0 | 94.4 | 95.1 | 95.5 | 95.4 | 95.3 | 94.1 | 93.3 |
| 6.6  | 6.7  | 5.3  | 4.6  | 4.2  | 4.3  | 4.4  | 5.6  | 6.4  |
| 54   | 34   | 20   | 13   |      | 8    | 16   | 27   | 46   |

92.9  
6.8  
75

95.2  
4.5  
75

93.7  
6.0  
61

Sta +  $\pi$  - Elev.

899.73

55+66

✓

56

✓

BM 8.74 904.24 4.23 895.50 (895.50)

+29

✓

+64



RG  
KP  
KJ  
JS  
JH

Dec. 21, 1959  
Dec 23, 1959  
26° snow HT

5

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 92.3 | 92.9 | 94.9 | 95.5 | 95.9 | 95.9 | 95.8 | 94.7 | 94.9 |
| 7.4  | 6.8  | 4.8  | 4.2  | 3.8  | 3.8  | 3.9  | 5.0  | 4.8  |
| 50   | 33   | 19   | 13   |      | 8    | 19   | 29   | 51   |

91.5  
91.7

8.2  
75

96.8  
2.9  
75

|      |      |              |      |       |              |      |      |      |
|------|------|--------------|------|-------|--------------|------|------|------|
| 92.7 | 93.5 | 95.4<br>94.4 | 96.1 | 96.61 | 96.4<br>96.4 | 96.7 | 96.2 | 97.1 |
| 7.0  | 6.2  | 4.3          | 3.6  | 3.12  | 3.1          | 3.0  | 3.5  | 2.6  |
| 50   | 36   | 21           | 13   |       | 8            | 18   | 22   | 48   |

92.0

7.7  
75

98.5  
1.2  
75

Spike in Arc Lt Pole #330 by Ho #1337 EC. P. C. X

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 94.0 | 94.4 | 96.5 | 96.4 | 94.3 | 94.3 | 94.4 | 96.4 | 96.4 | 96.4 |
| 10.2 | 9.4  | 7.7  | 7.4  | 6.9  | 6.9  | 6.8  | 7.4  | 7.4  | 5.9  |
| 33   | 25   | 19   | 13   |      | 8    | 16   | 18   | 25   | 31   |

92.4

11.8  
57

92.5

11.7  
67

99.5

1.7  
75

94.2

5.0  
58

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

| Sta | + | $\pi$  | - | Elev |
|-----|---|--------|---|------|
|     |   | 904.24 |   |      |

| Sta   | + | $\pi$  | - | Elev |
|-------|---|--------|---|------|
| 56+64 |   | 904.24 |   |      |

| Sta   | + | $\pi$  | - | Elev |
|-------|---|--------|---|------|
| 56+64 |   | 904.24 |   |      |
| ✓     |   |        |   |      |

| Sta   | + | $\pi$  | - | Elev |
|-------|---|--------|---|------|
| 56+64 |   | 904.24 |   |      |
| ✓     |   |        |   |      |
| +67   |   |        |   |      |

| Sta   | + | $\pi$  | - | Elev |
|-------|---|--------|---|------|
| 56+64 |   | 904.24 |   |      |
| ✓     |   |        |   |      |
| +67   |   |        |   |      |
| ✓     |   |        |   |      |

| Sta   | + | $\pi$  | - | Elev |
|-------|---|--------|---|------|
| 56+64 |   | 904.24 |   |      |
| ✓     |   |        |   |      |
| +67   |   |        |   |      |
| ✓     |   |        |   |      |
| 57    |   |        |   |      |

| Sta   | + | $\pi$  | - | Elev |
|-------|---|--------|---|------|
| 56+64 |   | 904.24 |   |      |
| ✓     |   |        |   |      |
| +67   |   |        |   |      |
| ✓     |   |        |   |      |
| 57    |   |        |   |      |
| ✓     |   |        |   |      |

Dec. 23, 1959 6

LT

RT

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 94.1 | 95.4 | 94.6 | 97.9 | 94.3 | 94.3 | 98.0 | 94.6 | 97.6 | 90.1 |
| 9.5  | 8.8  | 6.6  | 6.3  | 5.9  | 5.9  | 6.2  | 6.6  | 6.6  | 3.8  |
| 38   | 26   | 19   | 14   |      | 8    | 16   | 18   | 23   | 32   |

|      |      |
|------|------|
| 93.6 | 92.4 |
| 10.6 | 11.8 |
| 55   | 75   |

|     |     |
|-----|-----|
| 0.4 | 0.0 |
| 2.8 | 3.2 |
| 75  | 56  |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 95.0 | 99.1 | 99.8 | 98.1 | 98.4 | 98.4 | 98.0 | 94.1 | 94.1 | 90.5 |
| 8.7  | 7.1  | 6.4  | 6.1  | 5.8  | 5.8  | 6.2  | 6.5  | 6.5  | 3.7  |
| 26   | 22   | 18   | 13   |      | 8    | 16   | 18   | 24   | 33   |

|      |      |      |      |
|------|------|------|------|
| 95.4 | 95.3 | 94.1 | 92.9 |
| 8.8  | 8.9  | 10.1 | 11.3 |
| 34   | 44   | 59   | 75   |

|     |     |
|-----|-----|
| 0.4 | 0.7 |
| 2.8 | 3.5 |
| 75  | 52  |

|      |      |      |      |       |      |      |      |      |
|------|------|------|------|-------|------|------|------|------|
| 96.4 | 96.9 | 98.1 | 99.0 | 99.12 | 99.4 | 99.0 | 99.0 | 91.4 |
| 7.8  | 7.3  | 5.5  | 5.2  | 4.82  | 4.8  | 5.2  | 5.2  | 2.8  |
| 31   | 26   | 19   | 13   |       | 9    | 16   | 22   | 31   |

|      |      |      |
|------|------|------|
| 95.1 | 94.3 | 93.7 |
| 8.5  | 9.9  | 10.5 |
| 47   | 66   | 75   |

|     |     |
|-----|-----|
| 0.2 | 0.4 |
| 1.4 | 1.8 |
| 75  | 60  |

| Sta | + | $\pi$ | - | Elev. |
|-----|---|-------|---|-------|
|-----|---|-------|---|-------|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 904.24 |  |  |
|--|--|--------|--|--|

|       |  |  |  |  |
|-------|--|--|--|--|
| 57+50 |  |  |  |  |
|-------|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

|    |  |  |  |  |
|----|--|--|--|--|
| 58 |  |  |  |  |
|----|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

|    |      |        |      |        |
|----|------|--------|------|--------|
| TP | 6.66 | 908.05 | 2.85 | 901.39 |
|----|------|--------|------|--------|

|     |  |  |  |  |
|-----|--|--|--|--|
| +30 |  |  |  |  |
|-----|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|



Dec. 23, 1959

7

RT

| 99.1 | 99.2 | 99.9 | 00.3 | 00.6 | 00.8 | 00.6 | 00.2 | 0.7 |
|------|------|------|------|------|------|------|------|-----|
| 6.5  | 6.0  | 4.3  | 3.9  | 2.6  | 3.4  | 3.6  | 4.0  | 2.5 |
| 34   | 27   | 21   | 12   | 3.6  | 8    | 19   | 21   | 29  |

| 96.2 | 95.0 | 94.1 |
|------|------|------|
| 8.0  | 9.2  | 10.1 |
| 51   | 65   | 75   |

| 03.3 | 02.4 |
|------|------|
| 0.9  | 1.8  |
| 75   | 50   |

| 96.1 | 98.2 | 01.1 | 01.5 | 01.9 | 01.9 | 02.1 | 00.9 | 00.9 |
|------|------|------|------|------|------|------|------|------|
| 8.1  | 6.0  | 3.1  | 2.7  | 2.30 | 2.3  | 2.1  | 3.3  | 3.3  |
| 38   | 27   | 20   | 12   |      | 8    | 18   | 19   | 21   |

| 93.4 | 92.0 |
|------|------|
| 10.8 | 12.2 |
| 62   | 75   |

| 04.1 | 02.9 | 02.1 |
|------|------|------|
| 0.1  | 1.3  | 2.1  |
| 75   | 54   | 24   |

| 94.4 | 91.0 | 01.9 | 02.3 | 02.8 | 02.4 | 02.7 | 01.9 | 01.9 |
|------|------|------|------|------|------|------|------|------|
| 13.7 | 10.6 | 6.2  | 5.8  | 5.3  | 5.3  | 5.4  | 6.2  | 6.2  |
| 48   | 33   | 20   | 12   |      | 9    | 16   | 18   | 21   |

| 92.2 | 91.6 |
|------|------|
| 15.9 | 16.5 |
| 72   | 75   |

| 04.6 | 03.4 | 03.2 |
|------|------|------|
| 3.5  | 4.7  | 4.9  |
| 75   | 49   | 26   |

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 908.05 |  |  |
|--|--|--------|--|--|

|       |  |  |  |  |
|-------|--|--|--|--|
| 58+70 |  |  |  |  |
|-------|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

|    |  |  |  |  |
|----|--|--|--|--|
| 59 |  |  |  |  |
|----|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

|    |      |        |      |        |
|----|------|--------|------|--------|
| TP | 5.65 | 911.58 | 2.12 | 905.93 |
|----|------|--------|------|--------|

|     |  |  |  |  |
|-----|--|--|--|--|
| +38 |  |  |  |  |
|-----|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

Dec. 23, 1959

8

LT

RT

95.1

94.0

03.0

03.5

04.0

03.9

03.1

03.0

03.0

03.4

05.4

13.0 9.1 5.1 4.6 4.1 4.2 4.4 5.1 5.1 2.7  
54 32 20 12 9 16 18 21 28

91.9

16.4  
75

05.1

3.0  
75

04.8

3.3  
57

98.9

02.3

04.1

04.6

04.9

05.0

04.7

04.1

04.1

9.2 5.8 4.0 3.5 3.14 3.1 3.4 4.0 4.0  
40 27 21 12 9 16 18 22

95.9

12.2  
55

93.0

15.1  
75

06.4

1.7  
75

06.5

1.6  
54

06.8

1.3  
30

04.6

3.5  
25

04.6

3.5  
23

96.1

00.1

05.9

06.0

966.1

06.1

05.9

05.3

06.4

06.5

14.9 11.5 5.7 5.6 5.5 5.5 5.7 6.3 5.2 5.1  
61 43 21 11 9 15 20 25 27

94.0

17.6  
75

08.5

3.1  
75

08.3

3.3  
68

08.2

3.4  
47

08.6

3.0  
31

Sta +  $\pi$  - Elev.

911.58

59+43

✓

2.

+51 Burm

✓

+52 Gutter

+67  $\neq$  Clarence st.

TP

A.36

913.81

2.13

909.45



Dec 23, 1959 10

Lt

Rt

| 01.0 | 01.0 | 06.6 | 01.0 | 01.3 | 01.4 | 01.3 | 06.9 | 01.4 | 01.9 | 01.3 |
|------|------|------|------|------|------|------|------|------|------|------|
| 6.8  | 6.8  | 7.3  | 6.8  | 6.5  | 6.4  | 6.5  | 6.9  | 6.4  | 5.9  | 5.5  |
| 28   | 21   | 17   | 15   | 10   | 11   | 19   | 34   | 59   | 75   |      |

04.3

04.3

→ 9.5 14.5  
42 75

Duplicate + 81 Lt

| 01.5 | 01.4 | 06.8 | 01.2 | 01.9 | 01.8 |
|------|------|------|------|------|------|
| 6.3  | 6.4  | 7.0  | 6.6  | 5.9  | 5.0  |
| 10   | 21   | 26   | 48   | 66   |      |

09.0  
4.8  
75

| 01.8 | 01.4 | 01.9 | 01.9 | 04.03 | 08.0 | 01.7 | 06.6 | 06.4 | 10.2 |
|------|------|------|------|-------|------|------|------|------|------|
| 6.0  | 6.4  | 6.1  | 5.9  | 5.78  | 5.8  | 6.1  | 7.2  | 7.0  | 3.6  |
| 26   | 20   | 13   | 10   |       | 10   | 16   | 19   | 22   | 35   |

→ 01.8 04.4 02.0  
6.0 9.4 11.8  
41 59 75

11.1 11.2 10.7  
2.7 2.6 3.1  
75 65 45

Sta +  $\pi$  - Elev

913.81

60 + 18

✓

TP 9.79 919.24 4.36 909.45

+38

✓

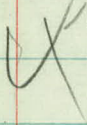
+62

✓

Lt

Rt

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 01.6 | 06.1 | 05.9 | 06.1 | 06.3 | 06.3 | 05.4 | 05.6 | 04.6 | 04.2 |
| 10.0 | 5.5  | 5.7  | 5.5  | 5.3  | 5.3  | 5.7  | 6.0  | 4.0  | 4.4  |
| 40   | 20   | 18   | 12   |      | 10   | 17   | 21   | 27   | 30   |



98.4  
13.2  
54

94.3  
17.3  
75

08.2  
3.4  
75

04.9  
5.7  
53

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 98.3 | 03.6 | 06.4 | 06.1 | 06.3 | 06.5 | 06.5 | 06.1 | 06.3 | 06.4 | 04.2 |
| 13.3 | 8.0  | 5.2  | 5.5  | 5.3  | 5.1  | 5.1  | 5.5  | 5.3  | 4.8  | 4.4  |
| 57   | 35   | 21   | 19   | 12   |      | 10   | 19   | 22   | 23   | 40   |



94.9  
16.7  
75

08.2  
3.4  
75

04.9  
5.7  
63

2

Duplicate 152 Lt

|      |      |      |      |      |      |
|------|------|------|------|------|------|
| 06.6 | 06.5 | 06.2 | 06.8 | 04.5 | 08.0 |
| 5.0  | 5.1  | 5.4  | 4.8  | 4.1  | 3.6  |
| 10   | 19   | 36   | 55   | 75   |      |



|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 03.4 | 06.0 | 06.7 | 06.8 | 06.4 | 07.0 | 07.1 | 07.6 | 08.2 | 06.5 | 08.9 |
| 8.2  | 5.6  | 4.9  | 4.8  | 4.8  | 4.6  | 4.5  | 4.0  | 3.4  | 3.1  | 2.7  |
| 39   | 29   | 21   | 15   | 12   | 14   | 37   | 60   | 75   | 100  |      |

00.6  
11.0  
56

94.0  
14.6  
75

09.5  
2.1  
200

09.3  
2.3  
150

Sta +  $\pi$  - Elev

913.81

59 + 81

✓

+ 82

✓

60



Dec 23, 1959 11

11

RT

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 03.5 | 04.0 | 04.9 | 08.3 | 08.6 | 08.1 | 08.5 | 09.1 | 09.1 | 11.1 |
| 8.3  | 4.8  | 5.9  | 5.5  | 5.2  | 5.1  | 5.3  | 6.7  | 6.7  | 2.7  |
| 70   | 49   | 32   | 12   |      | 10   | 15   | 19   | 21   | 36   |

✓

04.9  
8.9  
75

12.8  
1.0  
75

12.5  
1.3  
64

12.1  
1.7  
47

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 09.2 | 08.8 | 08.3 | 08.9 | 09.1 | 09.2 | 08.9 | 08.1 | 08.1 | 12.1 |
| 10.0 | 10.4 | 10.9 | 10.3 | 10.1 | 10.0 | 10.3 | 11.1 | 11.1 | 7.1  |
| 42   | 29   | 20   | 11   |      | 10   | 15   | 20   | 22   | 38   |

✓

09.1  
10.1  
61

09.4  
9.8  
75

14.6  
4.6  
75

13.8  
5.4  
56

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 12.6 | 11.8 | 09.1 | 08.9 | 09.6 | 09.8 | 09.8 | 09.1 | 08.9 | 13.9 |
| 6.6  | 7.4  | 9.5  | 10.3 | 9.6  | 9.4  | 9.4  | 9.5  | 10.3 | 5.3  |
| 47   | 38   | 27   | 18   | 11   |      | 10   | 15   | 23   | 45   |

✓

11.8  
7.4  
63

10.7  
8.5  
75

15.5  
3.7  
75

15.0  
4.2  
59

Sta +  $\pi$  - Elev

919.24

61

✓

TP 6.22 923.40 2.06 917.18

+50

✓

62

✓

± Dec 23, 1959

12

LT

RT

|      |      |      |      |       |      |      |      |      |      |
|------|------|------|------|-------|------|------|------|------|------|
| 15.4 | 11.3 | 10.2 | 10.1 | 10.90 | 10.9 | 10.6 | 10.0 | 10.0 | 10.9 |
| 3.4  | 7.9  | 9.0  | 8.5  | 8.34  | 8.3  | 8.6  | 9.2  | 9.2  | 8.3  |
| 50   | 29   | 20   | 10   |       | 11   | 16   | 18   | 27   | 24   |

2.

15.2  
4.0  
75

15.1 15.1 15.6 14.4  
3.5 3.5 3.6 4.4  
140 75 59 46  
82

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 14.5 | 16.1 | 13.7 | 11.5 | 12.1 | 12.2 | 12.0 | 11.6 | 10.8 | 10.8 | 14.9 |
| 4.9  | 6.7  | 9.7  | 11.9 | 11.3 | 11.2 | 11.4 | 11.8 | 12.6 | 12.6 | 8.5  |
| 66   | 43   | 33   | 19   | 10   |      | 11   | 16   | 20   | 21   | 37   |

14.9  
4.5  
75

17.5 17.6 17.2  
5.2 5.8 6.2  
85 75 57  
40

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 14.1 | 16.5 | 12.9 | 13.4 | 13.4 | 13.2 | 12.4 | 12.1 | 12.1 |
| 4.3  | 6.9  | 10.5 | 10.0 | 10.0 | 10.2 | 10.6 | 11.3 | 11.3 |
| 46   | 35   | 21   | 10   |      | 11   | 16   | 20   | 23   |

20.0 20.4  
3.4 3.0  
63 75

16.7 16.5 15.9 14.9  
6.7 6.9 7.5 8.7  
75 67 49 34

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

923.40

62+18

✓

+52

✓

+72



2 Dec. 23, 1959

13

LT

RT

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 14.3 | 13.1 | 13.0 | 13.6 | 13.9 | 13.6 | 13.4 | 11.9 | 11.4 | 13.1 |
| 5.1  | 10.3 | 9.9  | 9.6  | 9.5  | 9.8  | 10.0 | 11.5 | 11.5 | 9.9  |
| 40   | 22   | 18   | 12   |      | 12   | 17   | 20   | 22   | 25   |

|      |      |
|------|------|
| 18.1 | 19.7 |
| 4.7  | 3.7  |
| 55   | 75   |

|      |      |      |
|------|------|------|
| 13.4 | 13.5 | 13.6 |
| 10.0 | 9.9  | 9.8  |
| 75   | 59   | 42   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 16.6 | 14.3 | 14.0 | 14.4 | 14.6 | 14.8 | 14.5 | 14.5 | 13.1 | 14.6 |
| 6.8  | 9.1  | 9.4  | 9.0  | 8.8  | 8.6  | 8.9  | 8.9  | 10.3 | 8.8  |
| 35   | 27   | 19   | 17   | 11   |      | 13   | 16   | 21   | 29   |

|      |      |
|------|------|
| 16.7 | 19.7 |
| 6.7  | 5.7  |
| 53   | 75   |

|      |      |
|------|------|
| 14.4 | 14.3 |
| 9.0  | 9.1  |
| 75   | 52   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 15.9 | 14.1 | 15.1 | 15.2 | 15.3 | 15.1 | 13.6 | 14.9 | 14.7 | 14.6 |
| 7.5  | 8.7  | 8.3  | 8.2  | 8.1  | 8.3  | 9.8  | 8.5  | 8.7  | 8.8  |
| 38   | 20   | 16   | 9    |      | 15   | 22   | 25   | 42   | 59   |

|      |      |
|------|------|
| 16.2 | 16.8 |
| 7.2  | 6.6  |
| 54   | 75   |

|      |
|------|
| 14.3 |
| 9.1  |
| 75   |

Sta +  $\pi$  - Elev.

923.40

62+84

✓

63

✓

+27

✓

Dec 23, 1959

14

LT

BT

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 15.5 | 14.9 | 15.4 | 15.5 | 16.6 | 15.3 | 15.4 | 14.1 | 14.8 |
| 7.9  | 8.5  | 8.0  | 7.9  | 7.8  | 7.9  | 8.0  | 9.3  | 8.6  |
| 28   | 20   | 17   | 9    |      | 13   | 16   | 21   | 25   |

|      |      |      |  |      |      |      |
|------|------|------|--|------|------|------|
| 15.1 | 15.1 | 16.1 |  | 16.3 | 16.3 | 16.0 |
| 7.9  | 7.7  | 7.3  |  | 6.9  | 7.1  | 7.4  |
| 47   | 63   | 75   |  | 75   | 61   | 42   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 16.0 | 15.2 | 15.2 | 15.1 | 15.9 | 16.1 | 15.9 | 15.9 | 14.8 | 14.4 | 15.1 |
| 7.4  | 8.2  | 8.2  | 7.7  | 7.5  | 7.30 | 7.5  | 7.5  | 8.6  | 8.6  | 7.7  |
| 32   | 27   | 21   | 18   | 9    |      | 13   | 16   | 20   | 22   | 27   |

|      |      |  |  |      |      |      |      |
|------|------|--|--|------|------|------|------|
| 15.1 | 16.9 |  |  | 15.1 | 14.5 | 14.1 | 16.9 |
| 7.7  | 6.5  |  |  | 5.9  | 5.9  | 6.3  | 6.5  |
| 49   | 75   |  |  | 40   | 75   | 61   | 49   |
|      |      |  |  | 84   |      |      |      |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 18.0 | 15.8 | 15.4 | 16.5 | 17.0 | 17.1 | 16.8 | 16.9 | 15.7 | 15.7 | 16.9 |
| 5.4  | 7.6  | 8.0  | 6.9  | 6.4  | 6.3  | 6.6  | 6.7  | 7.7  | 7.7  | 6.5  |
| 44   | 35   | 24   | 18   | 9    |      | 13   | 16   | 20   | 22   | 28   |

|      |      |      |  |      |      |      |
|------|------|------|--|------|------|------|
| 18.8 | 19.8 | 21.0 |  | 18.4 | 18.3 | 14.9 |
| 4.6  | 3.6  | 2.4  |  | 5.0  | 5.1  | 5.5  |
| 61   | 75   | 140  |  | 75   | 62   | 47   |
|      |      | 92   |  |      |      |      |

Sta + X - Elev.

923<sup>40</sup>

63+57

✓

+ 25

✓

+ 88 ⊥ Elm St.

✓



Dec 23, 1959

15

14

15

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 16.6 | 16.5 | 19.1 | 19.1 | 18.0 | 18.2 | 18.1 | 19.4 | 19.9 | 16.9 |
| 6.8  | 6.9  | 5.7  | 6.0  | 5.4  | 5.2  | 5.3  | 5.6  | 6.5  | 6.5  |
| 32   | 22   | 19   | 15   | 9    |      | 11   | 18   | 20   | 22   |

|      |      |      |
|------|------|------|
| 18.1 | 19.2 | 20.0 |
| 5.3  | 4.2  | 3.4  |
| 38   | 57   | 75   |

|      |      |      |      |
|------|------|------|------|
| 20.9 | 19.8 | 19.1 | 18.0 |
| 2.7  | 3.6  | 4.3  | 5.4  |
| 75   | 52   | 34   | 25   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 18.9 | 18.3 | 18.6 | 18.1 | 18.8 | 18.9 | 18.1 | 19.2 | 19.2 | 18.6 |
| 4.5  | 5.1  | 4.8  | 4.7  | 4.6  | 4.7  | 4.7  | 6.2  | 6.2  | 4.8  |
| 42   | 35   | 20   | 7    |      | 11   | 17   | 18   | 20   | 27   |

|      |      |
|------|------|
| 19.4 | 19.9 |
| 4.0  | 3.5  |
| 58   | 75   |

|                 |      |      |      |
|-----------------|------|------|------|
| 21.36           | 20.9 | 20.4 | 19.9 |
| <del>21.0</del> | 2.7  | 3.0  | 3.7  |
| G. Apron        | 75   | 61   | 43   |
| 96              |      |      |      |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 20.3 | 19.6 | 19.1 | 19.5 | 19.3 | 19.3 | 19.0 | 19.1 | 19.1 | 19.1 | 19.3 |
| 3.1  | 3.8  | 4.3  | 3.9  | 4.1  | 4.1  | 4.4  | 4.3  | 5.3  | 5.3  | 4.1  |
| 85   | 55   | 41   | 21   | 8    |      | 13   | 16   | 19   | 23   | 29   |

|      |      |      |      |
|------|------|------|------|
| 20.8 | 21.7 | 22.3 | 22.8 |
| 2.6  | 1.7  | 1.1  | 0.6  |
| 100  | 140  | 170  | 200  |

|      |      |      |
|------|------|------|
| 21.3 | 21.1 | 20.6 |
| 2.1  | 2.3  | 2.8  |
| 75   | 65   | 49   |

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 923.40 |  |  |
|--|--|--------|--|--|

|    |  |  |  |  |
|----|--|--|--|--|
| 64 |  |  |  |  |
|----|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +14 |  |  |  |  |
|-----|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +39 |  |  |  |  |
|-----|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

£ Dec 23, 1959 16

21

54

19.4 19.2 19.2 19.1 19.78 14.5 19.2 18.2 18.3  
4.0 4.2 4.2 3.7 3.62 3.9 4.2 4.9 4.9  
50 30 15 9 11 17 19 24

20.1  
3.3  
75

✓

21.3 21.4 21.4 20.9 19.5  
2.1 2.0 2.0 2.5 3.9  
40 75 64 48 30  
84

18.0 18.0 19.1 19.5 20.2 20.4 20.1 20.1 19.8 19.4 19.4  
5.4 5.4 3.7 3.9 3.2 3.0 3.3 3.3 3.6 4.0 4.0  
31 26 17 14 9 9 12 17 19 23

19.6 19.9 20.6  
3.8 3.5 2.8  
38 57 75

✓

21.5 21.4 20.6 19.8  
1.9 2.0 2.8 3.6  
75 58 37 26

19.3 19.3 19.8 21.3 21.3 21.4 21.1 20.9 20.3 20.1 20.9  
5.1 5.1 3.6 2.1 2.1 2.0 2.3 2.6 3.1 3.3 2.5  
30 27 20 12 8 12 17 20 24 41

20.4 21.1 21.2  
3.0 2.3 2.2  
36 57 75

✓

19.8 21.0  
3.6 2.4  
75 59

Sta +  $\pi$  - Elev

923.40

64+57

✓

+ 75

✓

TP

7.16

929.55

1.01

922.39

65

✓



FX  
RG  
JS  
JH

Dec 23, 1957 17  
Jan 11, 1960  
Overcast 20° 97% Humidity Windy

LT

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 18.9 | 18.9 | 22.0 | 22.0 | 22.1 | 21.9 | 21.4 | 20.8 | 20.9 | 19.5 |
| 45   | 45   | 14   | 14   | 1.3  | 1.5  | 2.0  | 2.6  | 2.5  | 3.9  |
| 30   | 27   | 12   | 8    |      | 11   | 17   | 24   | 32   | 45   |

|      |      |      |      |  |      |      |
|------|------|------|------|--|------|------|
| 20.1 | 21.4 | 21.9 | 22.4 |  | 19.4 | 18.6 |
| 2.7  | 2.0  | 1.7  | 1.0  |  | 6.0  | 4.8  |
| 35   | 56   | 75   | 88   |  | 75   | 59   |
|      |      |      | HO   |  |      |      |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 19.4 | 19.4 | 21.1 | 22.6 | 22.1 | 22.9 | 22.9 | 22.3 | 19.2 | 19.6 | 15.1 |
| 4.0  | 4.0  | 2.3  | 0.8  | 0.7  | 0.5  | 0.7  | 1.1  | 3.9  | 5.8  | 7.7  |
| 30   | 27   | 21   | 13   | 9    |      | 11   | 15   | 28   | 42   | 62   |

|      |      |      |  |      |
|------|------|------|--|------|
| 21.1 | 21.8 | 22.2 |  | 14.4 |
| 2.3  | 1.6  | 1.2  |  | 9.0  |
| 34   | 50   | 75   |  | 75   |

High Point E. Edge stump LT 5 to 64 + 60

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 20.2 | 20.2 | 21.1 | 23.8 | 23.8 | 23.8 | 23.6 | 23.7 | 19.7 | 15.6 |
| 9.3  | 9.3  | 7.9  | 5.8  | 5.8  | 5.75 | 6.0  | 5.9  | 9.9  | 14.0 |
| 31   | 29   | 22   | 12   | 8    |      | 9    | 12   | 28   | 48   |

|      |      |      |      |
|------|------|------|------|
| 22.2 | 22.5 | 22.0 | 23.4 |
| 7.4  | 7.1  | 6.6  | 6.2  |
| 36   | 62   | 88   | 100  |

| Sta | + | $\pi$ | - | Elev. |
|-----|---|-------|---|-------|
|-----|---|-------|---|-------|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 929.55 |  |  |
|--|--|--------|--|--|

|       |  |  |  |  |
|-------|--|--|--|--|
| 65+30 |  |  |  |  |
|-------|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +55 |  |  |  |  |
|-----|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +75 |  |  |  |  |
|-----|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

Jan. 11, 1960

18

LT

RT

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 21.7 | 23.7 | 25.2 | 25.1 | 25.1 | 24.8 | 25.0 | 20.7 | 16.5 |
| 79   | 59   | 44   | 4.5  | 4.5  | 4.8  | 4.6  | 8.9  | 13.1 |
| 28   | 20   | 12   | 9    |      | 9    | 12   | 27   | 42   |

|      |      |      |      |      |      |
|------|------|------|------|------|------|
| 21.1 | 21.1 | 22.6 | 22.1 | 24.4 | 24.1 |
| 85   | 85   | 70   | 65   | 52   | 49   |
| 32   | 33   | 37   | 63   | 88   | 100  |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 22.1 | 23.2 | 25.5 | 26.2 | 26.2 | 26.2 | 25.9 | 25.9 | 21.1 | 16.1 | 15.9 |
| 75   | 64   | 41   | 3.3  | 3.9  | 3.4  | 3.7  | 3.7  | 8.5  | 13.5 | 13.8 |
| 28   | 24   | 17   | 12   | 8    |      | 9    | 13   | 29   | 51   | 56   |

|      |      |      |      |      |      |
|------|------|------|------|------|------|
| 21.7 | 21.7 | 22.3 | 23.0 | 23.9 | 24.8 |
| 79   | 79   | 73   | 66   | 57   | 48   |
| 31   | 32   | 37   | 64   | 85   | 100  |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 25.6 | 26.2 | 21.3 | 27.1 | 21.1 | 26.8 | 26.8 | 22.2 | 17.9 | 15.6 |
| 4.0  | 3.3  | 2.3  | 2.5  | 2.5  | 2.8  | 2.8  | 7.4  | 11.7 | 14.0 |
| 19   | 15   | 12   | 9    |      | 9    | 13   | 26   | 44   | 52   |

|      |      |      |      |      |      |
|------|------|------|------|------|------|
| 23.1 | 21.7 | 21.4 | 22.0 | 23.0 | 24.4 |
| 65   | 79   | 82   | 76   | 66   | 52   |
| 27   | 33   | 43   | 61   | 80   | 100  |

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 929.55 |  |  |
|--|--|--------|--|--|

|       |  |  |  |  |
|-------|--|--|--|--|
| 65+93 |  |  |  |  |
|-------|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

|    |  |  |  |  |
|----|--|--|--|--|
| 66 |  |  |  |  |
|----|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +07 |  |  |  |  |
|-----|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

|    |      |        |       |        |
|----|------|--------|-------|--------|
| TP | 2.33 | 918.84 | 13.04 | 916.51 |
|----|------|--------|-------|--------|



Jan 11, 1960

19

Lt

Rt

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 24.2 | 26.6 | 27.7 | 27.8 | 28.0 | 27.9 | 28.0 | 27.1 | 23.7 |
| 54   | 30   | 1.9  | 1.8  | 1.6  | 1.7  | 1.6  | 2.5  | 5.9  |
| 24   | 17   | 13   | 9    |      | 9    | 12   | 15   | 25   |

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| 21.0 | 21.4 | 21.7 | 22.0 | 24.7 | 15.2 | 17.6 | 21.1 |
| 8.6  | 8.2  | 7.9  | 6.6  | 4.9  | 14.4 | 12.0 | 8.5  |
| 34   | 39   | 57   | 80   | 100  | 56   | 48   | 34   |

|      |                 |      |      |      |      |      |      |      |      |
|------|-----------------|------|------|------|------|------|------|------|------|
| 23.6 | <del>26.4</del> | 28.1 | 28.1 | 28.3 | 28.2 | 28.0 | 29.6 | 20.4 | 16.8 |
| 60   | 3.2             | 1.5  | 1.5  | 1.27 | 1.4  | 1.6  | 5.1  | 9.2  | 12.8 |
| 23   | 17              | 12   | 9    |      | 10   | 12   | 19   | 29   | 42   |

|      |      |      |      |      |      |
|------|------|------|------|------|------|
| 21.1 | 20.8 | 21.2 | 21.6 | 22.6 | 24.8 |
| 8.5  | 8.8  | 8.4  | 8.0  | 7.0  | 4.8  |
| 31   | 33   | 37   | 53   | 75   | 100  |

|      |      |      |      |      |      |      |       |      |
|------|------|------|------|------|------|------|-------|------|
| 20.4 | 24.8 | 21.9 | 28.4 | 28.4 | 28.7 | 28.8 | 29.03 | 22.8 |
| 9.2  | 4.8  | 1.7  | 1.2  | 1.2  | 0.9  | 0.8  | 0.52  | 6.8  |
| 28   | 15   | 13   | 12   | 10   |      | 11   | 12    | 13   |

Curb

|      |      |      |      |      |
|------|------|------|------|------|
| 19.0 | 20.0 | 21.2 | 22.6 | 24.8 |
| 10.6 | 9.6  | 8.4  | 7.0  | 4.8  |
| 35   | 42   | 51   | 72   | 100  |

Top Fc Post Rt

Sta +  $\pi$  - Elev.

19A

918.84

65

+30

+55

+75

+93

66

Lt

Jan 11, 1960 20  
8+

✓

|      |      |      |      |
|------|------|------|------|
| 14.1 | 12.5 | 10.8 | 09.7 |
| 4.1  | 6.3  | 8.0  | 9.1  |
| 56   | 74   | 88   | 100  |

✓

|      |      |      |      |
|------|------|------|------|
| 14.5 | 11.7 | 09.8 | 08.8 |
| 4.3  | 7.1  | 9.0  | 10.0 |
| 56   | 74   | 90   | 100  |

✓

|      |      |      |
|------|------|------|
| 13.1 | 10.4 | 08.6 |
| 5.7  | 8.4  | 10.2 |
| 69   | 85   | 100  |

✓

|      |      |                 |
|------|------|-----------------|
| 12.0 | 10.5 | <del>08.3</del> |
| 6.8  | 8.3  | 10.5            |
| 73   | 82   | 100             |

✓

|      |      |      |
|------|------|------|
| 12.6 | 10.1 | 08.2 |
| 6.2  | 8.1  | 10.5 |
| 69   | 84   | 100  |

✓

|      |      |      |      |      |
|------|------|------|------|------|
| 13.3 | 11.4 | 08.8 | 08.1 | 04.5 |
| 5.5  | 7.4  | 10.0 | 12.7 | 14.3 |
| 52   | 62   | 77   | 91   | 100  |

Sta

+

A

-

Elev

918.84

66+07

✓

TP

7.66 921.11 5.39 913.45

+07

+13

✓

✓

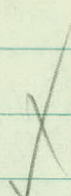


Jan 13, 1960

21

LT

RT



|      |      |      |      |
|------|------|------|------|
| 18.2 | 14.1 | 10.1 | 09.0 |
| 0.6  | 4.7  | 8.1  | 11.8 |
| 23   | 38   | 51   | 65   |

|      |      |
|------|------|
| 02.6 | 04.3 |
| 16.2 | 14.5 |
| 100  | 84   |

|      |      |      |
|------|------|------|
| 18.5 | 18.1 | 19.2 |
| 2.6  | 3.0  | 1.8  |
| 7    |      | 8    |

Under Bridge

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 18.2 | 20.2 | 19.5 | 17.1 | 16.1 | 17.6 | 18.2 | 18.3 | 17.2 | 15.2 |
| 2.8  | 0.9  | 1.6  | 4.0  | 4.4  | 3.5  | 2.9  | 2.8  | 3.9  | 5.8  |
| 21   | 17   | 13   | 8    |      | 7    | 12   | 17   | 21   | 26   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 16.8 | 15.1 | 16.2 | 17.4 | 02.1 | 02.6 | 05.2 | 08.0 | 11.2 | 12.2 |
| 4.3  | 6.0  | 4.8  | 3.7  | 17.4 | 17.5 | 15.8 | 13.1 | 9.8  | 7.8  |
| 25   | 31   | 35   | 39   | 100  | 94   | 78   | 64   | 52   | 42   |

|      |      |      |
|------|------|------|
| 21.0 | 19.9 | 19.0 |
| 0.1  | 1.2  | 2.1  |
| 57   | 50   | 44   |

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 921.11 |  |  |
|--|--|--------|--|--|

|       |  |  |  |  |
|-------|--|--|--|--|
| 66+20 |  |  |  |  |
|-------|--|--|--|--|

✓

|     |  |  |  |  |
|-----|--|--|--|--|
| +26 |  |  |  |  |
|-----|--|--|--|--|

✓

|    |  |  |  |  |
|----|--|--|--|--|
| FM |  |  |  |  |
|----|--|--|--|--|

|      |        |       |        |
|------|--------|-------|--------|
| 0.58 | 911.26 | 10.43 | 910.68 |
|------|--------|-------|--------|

|     |  |  |  |  |
|-----|--|--|--|--|
| +26 |  |  |  |  |
|-----|--|--|--|--|

Jan 16, 1960

22

LT

BT

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 12.9 | 11.5 | 14.1 | 14.1 | 12.9 | 13.5 | 14.4 | 15.0 | 14.2 | 14.5 |
| 22   | 26   | 6.4  | 7.0  | 8.2  | 7.6  | 6.7  | 6.1  | 6.8  | 6.6  |
| 35   | 29   | 18   | 10   | 3    |      | 6    | 9    | 12   | 17   |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 16.2 | 18.6 | 19.8 | 21.0 | 20.7 | 07.4 | 09.1 | 11.5 | 12.0 |
| 4.8  | 25   | 1.3  | 0.1  | 0.9  | 13.7 | 12.0 | 9.6  | 8.1  |
| 42   | 50   | 54   | 64   | 69   | 62   | 51   | 38   | 24   |

|      |      |      |      |
|------|------|------|------|
| 09.4 | 09.2 | 10.6 | 10.5 |
| 11.7 | 11.8 | 10.5 | 10.6 |
| 30   | 26   | 20   | 12   |

|      |      |      |      |
|------|------|------|------|
| 11.9 | 12.7 | 14.8 | 15.8 |
| 9.2  | 7.4  | 6.3  | 5.3  |
| 37   | 44   | 52   | 59   |

N.E. Cal old footing E side Tracks

|      |      |      |      |      |      |
|------|------|------|------|------|------|
| 10.8 | 10.5 | 09.7 | 09.9 | 08.5 | 06.6 |
| 0.5  | 0.8  | 1.6  | 1.4  | 2.8  | 4.7  |
| 7    | 14   | 19   | 27   | 39   |      |

|      |      |      |      |      |
|------|------|------|------|------|
| 00.2 | 09.9 | 00.5 | 02.3 | 04.6 |
| 11.1 | 11.4 | 10.8 | 9.0  | 6.7  |
| 100  | 93   | 82   | 66   | 49   |

Sta                    +                     $\pi$                     -                    Elev

911.26

66+33

✓

+41

r

✓

TP                    0.91                    906.97                    5.20                    906.06

+46

✓



Jan 15/1960 23

17

81

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 06.3 | 06.5 | 08.0 | 07.6 | 07.4 | 06.5 | 05.5 | 01.2 | 00.6 |
| 5.0  | 4.8  | 3.3  | 3.7  | 3.9  | 4.8  | 5.8  | 10.1 | 10.7 |
| 29   | 27   | 20   | 10   |      | 13   | 23   | 37   | 51   |

|      |      |      |      |
|------|------|------|------|
| 08.2 | 08.8 | 10.0 | 11.2 |
| 3.0  | 2.5  | 1.3  | 0.1  |
| 33   | 43   | 50   | 55   |

|      |      |      |      |
|------|------|------|------|
| 01.6 | 01.5 | 01.8 | 01.5 |
| 9.7  | 9.8  | 9.5  | 9.8  |
| 100  | 90   | 74   | 58   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 04.4 | 04.0 | 06.0 | 05.5 | 06.4 | 04.3 | 04.0 | 02.5 | 02.2 | 01.9 | 01.6 |
| 6.9  | 7.3  | 5.3  | 5.8  | 4.9  | 7.00 | 7.3  | 8.8  | 9.1  | 9.4  | 9.7  |
| 33   | 27   | 20   | 11   | 6.5  |      | 4    | 13   | 26   | 49   | 75   |

|      |      |      |
|------|------|------|
| 02.9 | 04.8 | 06.5 |
| 2.4  | 6.5  | 4.8  |
| 43   | 50   | 62   |

|      |      |      |
|------|------|------|
| 02.3 | 02.4 | 01.8 |
| 9.0  | 8.9  | 9.5  |
| 100  | 98   | 88   |

Top South Rail/Rock

Ballast

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 01.3 | 01.7 | 02.9 | 02.9 | 02.9 | 02.2 | 01.8 | 01.7 | 02.4 | 02.5 |
| 5.7  | 5.3  | 4.1  | 4.1  | 4.1  | 4.8  | 5.2  | 5.3  | 4.6  | 4.5  |
| 29   | 21   | 16   | 11   |      | 16   | 36   | 49   | 65   | 86   |

Ballast

|      |      |      |
|------|------|------|
| 01.9 | 02.0 | 04.2 |
| 5.1  | 5.0  | 2.8  |
| 40   | 51   | 63   |

|      |       |
|------|-------|
| 02.4 | 02.88 |
| 4.6  | 4.09  |
| 100  | 79    |

Rail

Sta +  $\pi$  - Elev.

906.97

66+54

BM 6.76 912.82 0.91 906.06

+62

✓

+69

169

26

78 84

EX  
RG  
JS  
CW

LT

Jan 11, 1960  
Jan 13, 1960  
Overcast 35° RT

24

|      |      |      |      |      |      |       |      |       |
|------|------|------|------|------|------|-------|------|-------|
| 02.4 | 02.6 | 02.1 | 02.0 | 01.9 | 02.8 | 03.06 | 02.4 | 02.95 |
| 4.6  | 4.4  | 4.9  | 5.0  | 5.1  | 4.2  | 3.91  | 4.6  | 4.02  |
| 53   | 38   | 20   | 10   |      | 17   | 32    | 61   | 64    |

Ballast Rail Rail

01.3 01.6 01.9

01.3 01.5 02.4

5.7 5.4 5.1  
70 83 100

5.7 5.5 4.6  
100 92 79

Top South Rail/Rail

Ballast

02.6 02.6 02.2 02.1 02.22 02.7

02.6 01.5 01.2 01.5

|      |      |      |      |      |    |      |      |      |      |      |
|------|------|------|------|------|----|------|------|------|------|------|
| 10.2 | 10.2 | 10.6 | 10.7 | 9.5  | 9  | 10.1 | 10.2 | 11.3 | 11.5 | 11.3 |
| 100  | 97   | 77   | 55   | Rail | 17 | 27   | 43   | 55   | 68   |      |

Ballast

01.0 00.9

11.8 11.9  
100 84

02.0 02.37 02.8 02.7 01.9 01.8 02.1 01.2 00.7

|     |      |      |      |      |      |      |      |      |
|-----|------|------|------|------|------|------|------|------|
| 9.8 | 9.45 | 10.0 | 10.1 | 10.9 | 11.0 | 10.7 | 11.6 | 12.1 |
| 77  | Rail | 61   | 50   | 14   | 10   | 19   | 36   | 58   |

Ballast

02.1 02.3

01.4 01.2 01.5

10.7 10.5  
94 100

11.4 11.5 11.3  
100 89 71

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

| Sta   | + | $\pi$  | - | Elev |
|-------|---|--------|---|------|
| 66+76 |   | 912.82 |   |      |

| Sta   | + | $\pi$  | - | Elev |
|-------|---|--------|---|------|
| 66+76 |   | 912.82 |   |      |

| Sta   | + | $\pi$  | - | Elev |
|-------|---|--------|---|------|
| 66+76 |   | 912.82 |   |      |
|       |   |        |   |      |

| Sta   | + | $\pi$  | - | Elev |
|-------|---|--------|---|------|
| 66+76 |   | 912.82 |   |      |
|       |   |        |   |      |
| +78   |   |        |   |      |

| Sta   | + | $\pi$  | - | Elev |
|-------|---|--------|---|------|
| 66+76 |   | 912.82 |   |      |
|       |   |        |   |      |
| +78   |   |        |   |      |
|       |   |        |   |      |

| Sta   | + | $\pi$  | - | Elev |
|-------|---|--------|---|------|
| 66+76 |   | 912.82 |   |      |
|       |   |        |   |      |
| +78   |   |        |   |      |
|       |   |        |   |      |
| +84   |   |        |   |      |

| Sta   | + | $\pi$  | - | Elev |
|-------|---|--------|---|------|
| 66+76 |   | 912.82 |   |      |
|       |   |        |   |      |
| +78   |   |        |   |      |
|       |   |        |   |      |
| +84   |   |        |   |      |
|       |   |        |   |      |



2 Jan 13, 1960

25

Lt

81

02.8 01.9 01.9 02.6 03.1 06.6 04.5 03.8 05.0 05.0

10.0 10.9 10.9 10.2 9.7 6.2 8.3 9.0 7.8 7.8  
57 41 31 5 7 14 32 50 57

02.42 02.0 03.49 02.0

02.0 02.1 02.5 02.5 02.7

9.39 9.8 9.33 9.8 9.8 9.7 10.3 9.3 9.1  
68 88 97 100 100 80 75 69 61  
Rail Rail

01.8 02.5 04.7 06.1 06.0 06.2 07.0 05.2 05.2 06.4 05.9

11.0 10.3 8.1 6.1 6.8 6.6 5.8 7.6 7.6 6.4 6.9  
46 31 16 9 4 8 17 26 43 56

01.9 02.9 02.45 02.0 02.0 02.9 02.2 04.0 02.6

10.9 9.9 9.37 9.8 9.8 8.9 9.5 8.8 9.2  
57 68 78 93 100 100 83 69 66  
Rail

02.3 04.7 07.4 07.9 07.8 07.7 08.6 09.8 07.4 04.9

10.5 8.1 5.4 4.9 5.0 5.1 4.2 3.0 5.4 7.9  
53 35 18 5 7 15 38 51 62

02.7 02.1 02.0 02.1

05.1 05.2 05.3

10.1 10.7 10.8 9.7 7.7 7.6 7.5  
64 74 91 100 100 89 69

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 912.82 |  |  |
|--|--|--------|--|--|

|       |  |  |  |  |
|-------|--|--|--|--|
| 66+91 |  |  |  |  |
|-------|--|--|--|--|

✓

|    |      |        |      |        |
|----|------|--------|------|--------|
| BM | 7.98 | 918.66 | 2.14 | 910.68 |
|----|------|--------|------|--------|

|    |  |  |  |  |
|----|--|--|--|--|
| 67 |  |  |  |  |
|----|--|--|--|--|

✓

|     |  |  |  |  |
|-----|--|--|--|--|
| +05 |  |  |  |  |
|-----|--|--|--|--|

|     |
|-----|
| 5.1 |
| 1.2 |
| 3.2 |

✓

Jan 13, 1960

LT

RT 26

05.2 07.2 08.6 10.0 p.6 12.3 11.8 10.8 07.1

76 56 42 28 22 0.5 10 20 51  
52 34 24 10 14 27 37 51

02.2 01.5 01.9

04.9 05.1 05.9

9.6 11.3 10.9  
62 83 100

29 27 69  
100 88 68

N.W. cor old footing

07.5 09.2 12.0 15.2 14.6 13.8 14.0 16.1 17.4 15.2

11.2 9.5 6.7 3.5 4.1 4.9 4.7 2.6 1.3 3.4  
47 35 28 18 12 7 11 19 29

04.9 03.2 03.6

05.4 06.0 06.1 04.8 12.0 12.2

13.8 15.4 15.1  
56 70 100

13.3 12.7 12.0 8.9 6.7 5.5  
100 80 63 46 37 34

12.4 15.9 18.9 16.8 15.3 17.6 19.6 16.9 12.4 08.0

6.3 2.8 10.2 1.9 3.4 11 10.9 1.8 6.3 10.7  
32 25 16 10 9 19 29 38 51

09.1 05.4 03.8 02.5

05.1 06.1 06.6

9.0 13.3 14.9 15.2  
45 57 64 100

13.0 12.6 12.1  
100 88 69

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 918.66 |  |  |
|--|--|--------|--|--|

|        |  |  |  |  |
|--------|--|--|--|--|
| 67 +10 |  |  |  |  |
|--------|--|--|--|--|

✓

|    |       |        |      |        |
|----|-------|--------|------|--------|
| TP | 11.76 | 929.86 | 0.56 | 918.10 |
|----|-------|--------|------|--------|

|     |  |  |  |  |
|-----|--|--|--|--|
| +10 |  |  |  |  |
|-----|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +15 |  |  |  |  |
|-----|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +20 |  |  |  |  |
|-----|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +40 |  |  |  |  |
|-----|--|--|--|--|



Jan. 13, 1960

27

14

54

|      |      |      |      |      |      |
|------|------|------|------|------|------|
| 18.2 | 17.5 | 16.0 | 16.9 | 18.7 | 13.9 |
| 0.5  | 1.2  | 2.7  | 1.8  | 0.0  | 4.8  |
| 11   | 7    |      | 7    | 11   | 37   |

|      |      |      |      |      |
|------|------|------|------|------|
| 05.4 | 06.0 | 06.9 | 06.6 | 08.1 |
| 13.3 | 12.7 | 11.8 | 12.1 | 10.6 |
| 100  | 88   | 67   | 62   | 51   |

spike

|      |      |      |      |
|------|------|------|------|
| 16.0 | 19.4 | 21.0 | 21.4 |
| 13.9 | 10.5 | 8.9  | 8.5  |
| 29   | 23   | 19   | 13   |

|      |      |      |      |
|------|------|------|------|
| 25.9 | 22.5 | 19.8 | 16.9 |
| 4.0  | 7.4  | 10.1 | 13.5 |
| 13   | 19   | 28   | 33   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 17.2 | 20.2 | 22.2 | 28.0 | 28.3 | 27.9 | 27.1 | 24.9 | 21.8 | 17.8 |
| 12.7 | 9.7  | 6.6  | 1.9  | 1.6  | 2.0  | 2.2  | 5.0  | 8.1  | 12.1 |
| 30   | 25   | 19   | 12   |      | 11   | 12   | 17   | 25   | 32   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 18.2 | 21.4 | 25.0 | 28.1 | 28.0 | 28.0 | 27.6 | 27.5 | 26.1 | 21.4 | 17.4 |
| 11.7 | 8.5  | 4.9  | 1.8  | 1.9  | 1.9  | 2.3  | 2.4  | 3.8  | 8.5  | 12.5 |
| 29   | 24   | 17   | 13   | 11   |      | 11   | 13   | 15   | 26   | 34   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 15.8 | 18.4 | 24.1 | 27.1 | 26.8 | 27.0 | 26.5 | 26.2 | 22.6 | 19.1 | 16.1 |
| 14.1 | 11.5 | 5.8  | 2.8  | 3.1  | 2.9  | 3.4  | 3.6  | 7.3  | 10.2 | 13.2 |
| 33   | 29   | 18   | 12   | 10   |      | 10   | 13   | 22   | 28   | 34   |

| Sta                  | +    | $\pi$  | -    | Elev.  |
|----------------------|------|--------|------|--------|
| 67                   |      | 929.86 |      |        |
| 67+55                |      |        |      |        |
|                      | +75  |        |      |        |
| 68                   |      |        |      |        |
| 10<br>20<br>30<br>40 | +10  |        |      |        |
|                      | +20  |        |      |        |
| ✓                    |      |        |      |        |
| TP                   | 0.70 | 929.56 | 7.20 | 922.66 |

Jan 13, 1960 28

LT

RT

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 18.3 | 22.0 | 25.3 | 26.3 | 26.0 | 26.2 | 25.9 | 25.9 | 22.1 | 17.5 |
| 11.6 | 7.9  | 4.6  | 3.6  | 3.9  | 3.7  | 4.0  | 4.0  | 7.8  | 12.4 |
| 27   | 20   | 15   | 12   | 10   |      | 10   | 12   | 22   | 32   |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 17.1 | 21.2 | 25.4 | 25.2 | 25.4 | 25.2 | 25.3 | 23.0 | 17.0 |
| 12.8 | 8.7  | 4.5  | 4.7  | 4.5  | 4.7  | 4.6  | 6.9  | 12.9 |
| 29   | 22   | 12   | 10   |      | 10   | 12   | 19   | 33   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 16.0 | 17.9 | 22.1 | 24.5 | 24.3 | 24.5 | 24.3 | 24.4 | 20.8 | 16.1 |
| 13.9 | 12.0 | 7.8  | 5.4  | 5.6  | 5.4  | 5.6  | 5.5  | 9.1  | 13.8 |
| 33   | 29   | 21   | 12   | 10   |      | 10   | 13   | 23   | 33   |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 16.4 | 22.1 | 24.0 | 24.1 | 24.1 | 23.9 | 24.1 | 21.2 | 17.1 |
| 13.5 | 7.8  | 5.9  | 5.8  | 5.8  | 6.0  | 5.8  | 8.6  | 12.8 |
| 32   | 19   | 12   | 10   |      | 10   | 12   | 21   | 32   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 16.1 | 17.9 | 22.0 | 23.8 | 23.7 | 23.8 | 23.7 | 23.8 | 20.5 | 16.0 |
| 13.2 | 12.0 | 7.9  | 6.1  | 6.2  | 6.1  | 6.2  | 6.1  | 9.4  | 13.9 |
| 33   | 29   | 19   | 12   | 9    |      | 10   | 12   | 23   | 35   |

|      |      |      |      |
|------|------|------|------|
| 16.9 | 16.8 | 15.2 | 13.1 |
| 13.0 | 13.1 | 14.6 | 16.2 |
| 36   | 52   | 64   | 75   |

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 923.36 |  |  |
|--|--|--------|--|--|

|       |  |  |  |  |
|-------|--|--|--|--|
| 68+50 |  |  |  |  |
|-------|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +80 |  |  |  |  |
|-----|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

|    |  |  |  |  |
|----|--|--|--|--|
| 69 |  |  |  |  |
|----|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|



Jan 13, 1960

29

LT

RT

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 19.5 | 21.9 | 22.7 | 22.6 | 22.8 | 22.6 | 22.6 | 20.1 | 16.2 |
| 3.9  | 1.5  | 0.7  | 0.8  | 0.6  | 0.8  | 0.8  | 3.3  | 2.2  |
| 25   | 18   | 12   | 9    |      | 9    | 12   | 21   | 34   |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 16.2 | 17.7 | 17.8 | 17.9 | 05.9 | 06.2 | 07.4 | 08.6 | 12.1 |
| 51   | 57   | 56   | 55   | 17.5 | 17.2 | 16.0 | 14.8 | 14.7 |
| 30   | 42   | 67   | 75   | 100  | 92   | 71   | 61   | 44   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 17.2 | 19.6 | 21.8 | 21.7 | 21.6 | 21.6 | 21.6 | 18.7 | 15.6 | 12.8 |
| 6.2  | 3.8  | 1.6  | 1.7  | 1.8  | 1.8  | 1.8  | 4.7  | 2.8  | 10.6 |
| 29   | 20   | 12   | 10   | 10   | 12   | 24   | 35   | 44   |      |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 17.2 | 19.0 | 19.0 | 18.4 | 18.3 | 18.1 | 18.7 | 06.9 | 08.0 | 10.1 |
| 6.2  | 4.4  | 4.4  | 5.0  | 5.1  | 4.7  | 4.7  | 16.5 | 15.4 | 13.3 |
| 32   | 35   | 37   | 38   | 43   | 49   | 75   | 100  | 78   | 58   |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 17.1 | 17.1 | 18.9 | 21.2 | 20.9 | 21.1 | 20.9 | 21.0 | 18.4 | 15.6 |
| 6.3  | 6.3  | 4.5  | 2.2  | 2.5  | 2.3  | 2.5  | 2.4  | 5.0  | 2.8  |
| 29   | 27   | 20   | 12   | 10   |      | 10   | 12   | 24   | 34   |

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| 19.2 | 19.6 | 19.2 | 09.1 | 09.1 | 12.2 | 12.5 | 12.9 |
| 4.1  | 3.8  | 4.2  | 14.3 | 12.7 | 11.2 | 9.9  | 9.5  |
| 34   | 58   | 75   | 75   | 69   | 52   | 44   | 40   |

Sta +  $\pi$  - Elev.

923.36

69+28

✓

+60

✓

TP<sub>13</sub>

1.79 921.57 (921.53)

BM

2.65 913.33

910.68

67+15

+20

Jan 13, 1960 30

LT

RT

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 17.1 | 17.1 | 18.4 | 20.4 | 20.2 | 20.3 | 20.2 | 20.3 | 18.0 | 15.2 |
| 6.3  | 6.3  | 5.0  | 3.0  | 3.1  | 3.1  | 3.2  | 3.1  | 5.4  | 8.2  |
| 27   | 25   | 20   | 12   | 10   |      | 10   | 12   | 21   | 32   |

|      |      |      |      |  |  |  |  |      |      |
|------|------|------|------|--|--|--|--|------|------|
| 18.9 | 19.2 | 18.8 | 18.0 |  |  |  |  | 12.5 | 13.1 |
| 4.5  | 4.2  | 4.6  | 5.4  |  |  |  |  | 10.9 | 10.3 |
| 31   | 33   | 52   | 75   |  |  |  |  | 75   | 50   |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 16.0 | 17.7 | 20.0 | 20.0 | 19.1 | 19.7 | 19.9 | 16.8 | 15.0 |
| 7.4  | 5.7  | 3.4  | 3.4  | 3.7  | 3.7  | 3.5  | 6.6  | 8.4  |
| 24   | 19   | 12   | 10   |      | 10   | 2    | 24   | 39   |

|      |      |      |      |  |  |  |  |      |      |
|------|------|------|------|--|--|--|--|------|------|
| 15.9 | 17.7 | 17.1 | 17.0 |  |  |  |  | 15.3 | 15.1 |
| 7.5  | 5.7  | 6.3  | 6.4  |  |  |  |  | 8.1  | 8.3  |
| 26   | 30   | 54   | 75   |  |  |  |  | 75   | 55   |

Top Eastern most G.R. Post N. Side Co. Rd "C"

Top NW Cor old footing E Side Tracks

LT

RT

|      |     |      |      |      |      |
|------|-----|------|------|------|------|
| 10.7 | 9.1 | 10.0 | 06.4 | 06.1 | 05.5 |
| 2.6  | 5.2 | 6.3  | 6.9  | 7.2  | 7.8  |
| 41   | 48  | 54   | 67   | 80   | 100  |

|      |      |      |      |      |      |
|------|------|------|------|------|------|
| 11.1 | 08.0 | 06.8 | 06.2 | 06.0 | 05.3 |
| 2.2  | 5.3  | 6.5  | 7.1  | 7.3  | 8.0  |
| 41   | 47.5 | 55   | 69   | 83   | 100  |

Sta +  $\pi$  - Elev

913.33

67+40

+55

+75

68

+10

+20

BM

6.31

916.99

2.66

910.67

910.68

76

0.57

05.9



£

Jan 13, 1960

31

RT

✓ 12.0. 08.2. 06.5. 05.9. 04.8.  
1.3 5.1 6.8 7.4 8.5  
40 50 67 82 100

✓ 12.9. 12.2. 10.5. 07.6. 06.6. 05.7. 04.6.  
0.4 1.1 2.8 5.7 6.7 7.6 8.7  
40 44 54 62 67 84 100

✓ 13.3. 12.3. 11.6. 09.6. 06.4. 05.8. 04.5.  
0.0 1.0 1.7 5.7 6.9 7.5 8.8  
41 45 52 63 70 83 100

✓ 13.3. 12.4. 09.8. 07.4. 06.4. 05.7. 05.0.  
0.0 0.9 3.5 5.9 6.9 7.6 8.3  
43 47 56 63 70 82 100

✓ 12.6. 09.5. 07.4. 06.2. 05.9. 05.1.  
0.7 3.8 5.9 7.0 7.4 8.2  
44 54 63 69 83 100

✓ 12.7. 09.5. 07.5. 06.5. 05.7. 05.2.  
0.6 3.8 5.8 6.8 7.6 8.1  
45 54 63 69 85 100

Top N.W. Cor old footing E. Side Tracks

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 916.99 |  |  |
|--|--|--------|--|--|

|       |  |  |  |  |
|-------|--|--|--|--|
| 67+10 |  |  |  |  |
|-------|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +15 |  |  |  |  |
|-----|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +20 |  |  |  |  |
|-----|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +40 |  |  |  |  |
|-----|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +55 |  |  |  |  |
|-----|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +75 |  |  |  |  |
|-----|--|--|--|--|

FK  
RG  
JS  
CW  
JH

Jan. 14, 1960  
Cloudy 30°

32

14  
03.2 03.3 04.5 08.2 10.9 14.5  
13.8 13.7 12.5 8.8 6.1 2.5  
100 35 61 50 43 31

03.2 03.5 04.8 06.8 11.5 16.2 ✓  
13.8 13.5 12.2 10.2 5.5 0.7  
100 78 60 52 42 28

03.2 03.2 04.6 06.6 11.2 15.6 ✓  
13.7 13.7 12.4 10.4 5.8 1.4  
100 76 61 51 40 31

03.5 03.5 04.1 06.4 11.0 ✓  
13.5 13.5 12.9 10.6 6.0  
100 79 61 47 38

03.8 03.9 05.1 07.3 12.0 ✓  
13.2 13.1 11.9 9.7 5.0  
100 76 57 43 34

04.2 05.2 06.1 08.0 12.2 ✓  
12.7 11.7 10.3 9.0 3.7  
100 75 57 45 33

Sta +  $\pi$  - Elev

916.99

68

+10

BM

10.93 906.06 906.06

T P<sub>13</sub> 2.05 923.58

921.53

69+71.5

4.15

Top MH  
3.3' Rt

70

✓

+50



Jan 14, 1960

33

Lt

♂

|      |      |      |      |      |
|------|------|------|------|------|
| 06.1 | 07.2 | 09.0 | 11.5 | 13.6 |
| 10.9 | 9.8  | 8.0  | 5.5  | 3.4  |
| 100  | 83   | 64   | 47   | 39   |

✓

|      |      |      |      |      |
|------|------|------|------|------|
| 08.4 | 09.3 | 09.9 | 12.4 | 15.0 |
| 8.6  | 7.7  | 7.1  | 4.6  | 2.0  |
| 100  | 81   | 63   | 46   | 35   |

✓

Top South Rail Rock Post

Lt

♂

♂

Top Easternmost G.R. Post N. Side of C"

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 16.0 | 16.2 | 17.6 | 19.4 | 19.3 | 19.0 | 19.3 | 18.3 | 16.7 | 15.8 |
| 7.6  | 7.4  | 6.0  | 4.2  | 4.3  | 4.6  | 4.3  | 5.3  | 6.9  | 7.8  |
| 47   | 33   | 20   | 12   | 10   |      | 10   | 15   | 25   | 44   |

✓

|      |      |
|------|------|
| 15.9 | 16.0 |
| 7.7  | 7.6  |
| 69   | 75   |

|      |      |
|------|------|
| 17.0 | 16.6 |
| 6.6  | 7.0  |
| 75   | 63   |

|      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
| 15.7 | 15.5 | 16.2 | 17.8 | 18.1 | 18.4 | 18.3 | 17.9 | 16.5 | 15.8 | 15.9 |
| 7.9  | 8.1  | 7.3  | 5.8  | 5.5  | 5.2  | 5.3  | 5.7  | 7.1  | 7.8  | 7.7  |
| 55   | 35   | 26   | 14   | 10   |      | 10   | 15   | 25   | 37   | 62   |

|      |      |
|------|------|
| 16.0 | 16.2 |
| 7.6  | 7.4  |
| 75   | 70   |
|      | 91   |

|      |
|------|
| 16.0 |
| 7.6  |
| 75   |

Sta

+

$\pi$

-

Elev

923.58

71

✓

+35

✓

+58

72

Jan. 14, 1960

34

BT

15.3 15.3 17.5 17.7 18.0 17.9 16.7 15.9 16.0 16.0

83 83 6.1 5.9 5.6 5.7 6.9 7.7 7.6 7.6  
29 26 15 10 13 23 41 59 75

15.9 15.8 15.4

7.7 7.8 8.2  
33 53 75

16.1 15.8 15.8 17.6 18.1 18.1 18.2 17.3 16.6 16.1

7.5 7.8 7.8 6.0 5.5 5.5 5.3 6.3 7.0 7.5  
54 33 27 20 10 12 19 34 56

15.7 16.0

7.9 7.6  
75 62

16.2

7.4  
75

17.7 17.6 17.7 17.9 18.0 18.2 18.2 17.4 16.9 16.1 16.6

5.9 6.0 5.9 5.7 5.6 5.4 5.3 6.2 6.7 7.5 7.1  
75 61 36 20 10 13 20 38 57 75

18.0 17.2 17.2 18.2 18.2 18.5 18.4 17.8 17.4 17.3 17.9

5.6 6.4 6.4 5.4 5.4 5.1 5.2 5.8 6.2 6.3 5.7  
28 24 23 16 10 12 21 43 60 75

18.9 18.8 18.9

4.7 4.8 5.2  
31 50 75

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 923.58 |  |  |
|--|--|--------|--|--|

|        |  |  |  |  |
|--------|--|--|--|--|
| 72 +50 |  |  |  |  |
|--------|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +68 |  |  |  |  |
|-----|--|--|--|--|

|  |  |  |      |  |
|--|--|--|------|--|
|  |  |  | 4.31 |  |
|--|--|--|------|--|

|    |  |  |  |  |
|----|--|--|--|--|
| 73 |  |  |  |  |
|----|--|--|--|--|

|   |  |  |  |  |
|---|--|--|--|--|
| ✓ |  |  |  |  |
|---|--|--|--|--|

|     |  |  |  |  |
|-----|--|--|--|--|
| +50 |  |  |  |  |
|-----|--|--|--|--|

|    |  |  |  |  |
|----|--|--|--|--|
| 74 |  |  |  |  |
|----|--|--|--|--|

|                    |  |  |  |  |
|--------------------|--|--|--|--|
| T.P. <sub>12</sub> |  |  |  |  |
|--------------------|--|--|--|--|

|      |  |  |  |  |
|------|--|--|--|--|
| 3.87 |  |  |  |  |
|------|--|--|--|--|

|        |  |  |  |  |
|--------|--|--|--|--|
| 926.89 |  |  |  |  |
|--------|--|--|--|--|

|      |  |  |  |  |
|------|--|--|--|--|
| 0.57 |  |  |  |  |
|------|--|--|--|--|

|        |  |  |  |  |
|--------|--|--|--|--|
| 923.01 |  |  |  |  |
|--------|--|--|--|--|

|        |  |  |  |  |
|--------|--|--|--|--|
| 923.02 |  |  |  |  |
|--------|--|--|--|--|



Jan 14, 1960

35

LT

RT

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 18.8 | 18.5 | 18.8 | 18.9 | 19.0 | 18.9 | 18.6 | 19.1 | 19.6 |
| 4.8  | 5.1  | 4.8  | 4.7  | 4.6  | 4.7  | 5.0  | 4.5  | 4.0  |
| 28   | 21   | 17   | 10   |      | 12   | 23   | 42   | 57   |

19.2 19.2 18.7

4.4 4.4 4.9  
31 48 75

20.2

3.4  
75

Top NH 2' RT

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 19.1 | 19.1 | 19.2 | 19.1 | 19.3 | 19.3 | 19.3 | 19.7 | 20.2 | 20.6 |
| 4.5  | 4.5  | 4.4  | 4.5  | 4.3  | 4.3  | 4.3  | 3.9  | 3.4  | 3.0  |
| 42   | 25   | 19   | 10   |      | 13   | 19   | 41   | 61   | 75   |

19.0 19.0 19.3

4.6 4.6 4.3  
65 75 40  
84

19.4 19.5 19.6 20.0 19.9 19.7 20.1 20.4 20.5 20.8 20.8

|     |     |     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 4.2 | 4.1 | 4.0 | 3.6 | 3.7 | 3.9 | 3.5 | 3.2 | 3.1 | 2.8 | 2.8 |
| 75  | 62  | 51  | 21  | 10  |     | 14  | 22  | 40  | 59  | 75  |

22.2 22.0 21.3 20.8 20.6 20.9 20.9 21.4 21.4 21.6 21.7

|     |     |     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 1.4 | 1.6 | 2.3 | 2.8 | 3.0 | 2.7 | 2.7 | 2.2 | 2.2 | 2.0 | 1.9 |
| 51  | 35  | 28  | 21  | 10  |     | 13  | 22  | 40  | 61  | 75  |

22.1

1.5  
75

Sta

+

$\pi$

-

Elev

926.89

74+30

✓

+60

✓

7.5

✓

Jan 14, 1960

36

14

51

22.4 21.7 21.2 21.2 21.2 21.3 21.3 21.8 22.1 21.8 21.7  
 45 52 57 57 57 56 56 51 48 51 52  
 41 29 22 19 10 11 18 28 45 64

22.4 22.4

45 45  
 59 75

22.0

49  
 75

23.5 23.2 21.5 21.6 21.5 21.5 21.7 22.1 22.6 22.4 22.8  
 34 37 54 53 54 54 52 48 43 45 41  
 50 32 25 18 10 14 18 25 44 61

23.7 23.5

32 34  
 75 110  
 81

23.2

37  
 75

23.7 21.7 21.9 21.9 22.0 21.9 22.2 23.1 23.8 24.2  
 32 52 50 50 49 50 47 38 31 26  
 31 25 19 10 11 20 37 54 75

23.6 22.4

33 35  
 51 75

Sta

+

$\pi$

-

Elev

926.89

75+50

✓

+70

4.20

76

✓

+50

✓



Jan. 14, 1960

37

LT

RT

21.8 21.8 22.0 22.4 22.5 22.3 22.3 22.3 22.4 24.0

5.1 5.1 4.9 4.5 4.4 4.6 4.6 3.6 3.5 2.9  
25 23 22 10 12 18 34 48 62

22.5 22.4 21.9

24.4

3.4 3.5 5.0  
31 49 75

2.5  
75

Top MH 1' RT

22.4 22.2 22.2 22.4 22.4 22.6 22.6 22.5 22.6 22.8

3.5 4.6 4.6 4.5 4.5 4.3 4.3 4.4 3.3 3.1  
32 25 23 20 10 13 20 31 52

22.1 22.9 22.2

24.9

3.8 4.0 4.7  
54 66 75

2.0  
75

22.2 22.3 22.4 22.4 22.6 22.5 22.5 22.7 24.2

4.6 4.6 4.5 4.5 4.3 4.4 4.4 3.2 2.7  
24 22 20 10 12 20 30 45

24.2 24.3 24.1 23.6

24.4 24.4

2.7 2.6 2.8 3.3  
35 55 65 75

2.5 2.5  
75 59

Sta +  $\pi$  - Elev

926.89

77

✓

+50

22.4

4.5

22.1

78

4.8

21.7

+50

5.2

22.0

+71

4.90

TP<sub>12</sub>

3.87

923.02

923.02

Jan 14, 1960

38

LT

BT

22.4.

22.4.

22.5.

22.5.

22.7.

22.8.

22.9.

23.1.

24.1.

24.0.

45  
25

45  
22

44  
19

44  
10

4.2

4.1  
12

4.0  
22

3.8  
31

2.8  
53

2.9  
66

24.0.

24.1.

24.2.

23.8.

2.9  
34

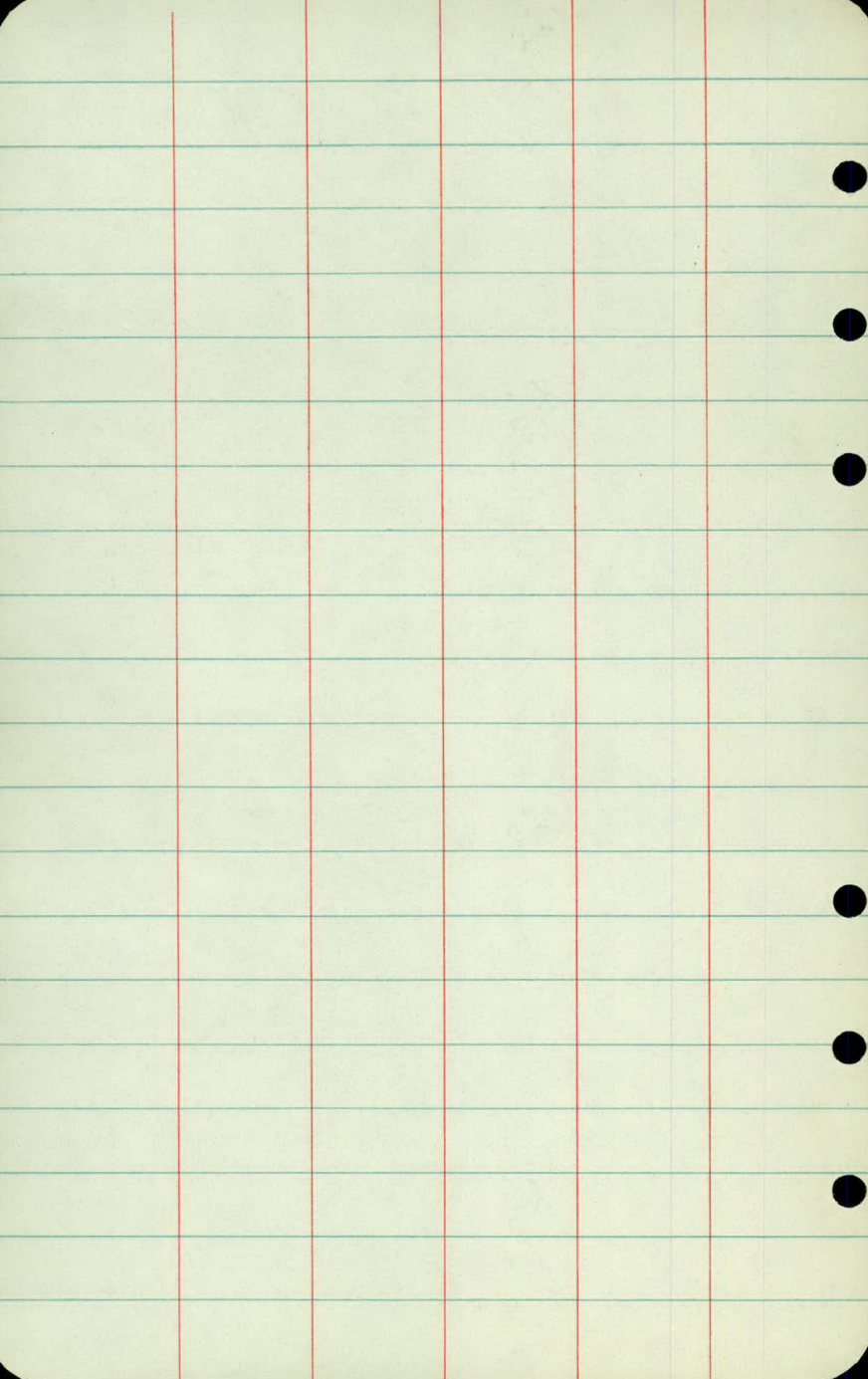
2.8  
53

2.7  
75

3.1  
75

Top MH & Hazelwood

Nail in Power Transformer Pole





Dec 26, 1959

39

Bridge Elev.

footing & Bents

9

| Sta             | +     | $\pi$  | -     | Elev.  |
|-----------------|-------|--------|-------|--------|
| BM              | 0.23  | 931.65 |       | 931.42 |
| TP              | 0.36  | 919.49 | 12.52 | 919.13 |
| BM              | 0.57  | 911.26 | 8.80  | 910.69 |
| Footing<br>a    |       |        | 10.80 | 901.46 |
| Rail            |       |        | 8.09  |        |
| Rail            |       |        | 8.04  | 903.22 |
| Footing<br>b    |       |        | 5.16  |        |
| Footing<br>c    |       |        | 2.17  |        |
| T.P.            | 11.17 | 918.70 | 3.73  | 907.53 |
| A. Footing<br>d |       |        | 5.10  | 913    |
| Footing<br>e    |       |        | 18.74 | 899.96 |
| A. Footing<br>f |       |        | 4.85  | 913    |
| TP              | 13.37 | 931.50 | 0.57  | 918.13 |
| BM              |       |        | 0.07  | 931.43 |
| BM              | 2.76  | 913.45 |       | 910.69 |
| Footing<br>g    |       |        | 13.50 | 899.95 |
| Footing<br>h    |       |        | 12.92 | 901.53 |
| Footing<br>i    |       |        |       |        |

N

E

Dec 21, 1959

40

S

Top W. Edge T Post N.E. Cor Bridge Sta 67+15

N.W. Cor old bridge Abutment E side of Track

E. Abutment  
f

Bent 1

W. Rail E

i

b

Bent 2

E Rail E

g

e

Bent 3

N ←

h

a

Bent 4

c

Bent 5

d

Bent 6

W. Abutment

Top W. Edge T Post N.E. Cor Bridge Sta 67+15

N.W. Cor old bridge Abutment E. side

| Sta               | +    | $\pi$  | -      | Elev   |
|-------------------|------|--------|--------|--------|
|                   |      | 913.45 |        |        |
| NE Cor            |      |        | -12.12 | 925.57 |
| NE Cor            |      |        | -12.60 | 926.05 |
| SE Cor            |      |        | -12.70 | 926.15 |
| SE Cor            |      |        | -12.10 | 925.55 |
| Top footing<br>in |      |        | 7.50   |        |
| NE Cor            |      |        | -12.39 |        |
| SW Cor            |      |        | -12.41 |        |
| NE Cor            |      |        | -12.81 |        |
| SE Cor            |      |        | -12.69 |        |
| TP                | 8.23 | 918.92 | 2.76   | 910.69 |
| NE Cor            |      |        | -6.69  |        |
| SE Cor            |      |        | -6.71  |        |
| SW Cor            |      |        | -6.16  |        |
| NW Cor            |      |        | -6.14  |        |
| NW Cor            |      |        | -7.73  |        |
| SW Cor            |      |        | -7.68  |        |
| Top Bent 1        |      |        | -6.43  |        |
| W Rail            |      |        | -15.80 |        |
| E Rail            |      |        | 15.78  |        |



FK  
RG  
KP  
KJ  
JH  
JS

Dec. 22, 1959  
Snowing 27°

41

Top Bent A

Top Bent 3

Top Bent 3

Top Bent A

Top Bent 2

Top Bent 2

Top Bent 5

" " 5

Top Bent 6

" " 6

Top Bent 3

" " 3

Top Bent 4

" " A

20' Rt

20' Rt

| Sta | + | $\pi$  | - | Elev. |
|-----|---|--------|---|-------|
|     |   | 918.92 |   |       |

|         |  |  |       |  |
|---------|--|--|-------|--|
| W. Rail |  |  | 15.68 |  |
|---------|--|--|-------|--|

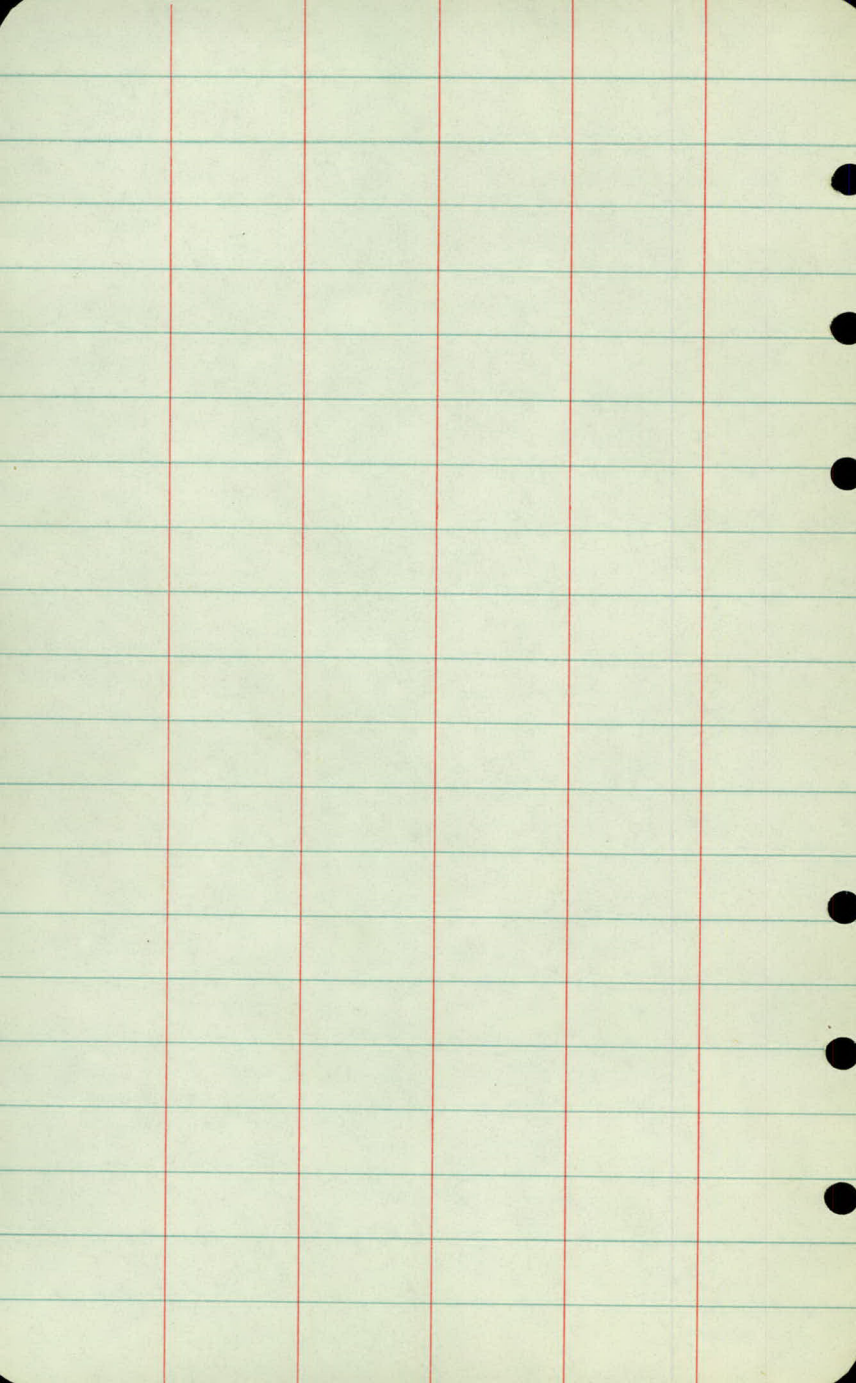
|         |  |  |       |  |
|---------|--|--|-------|--|
| E. Rail |  |  | 15.65 |  |
|---------|--|--|-------|--|

|           |  |  |       |        |
|-----------|--|--|-------|--------|
| E Rail 12 |  |  | 15.69 | 903.23 |
|-----------|--|--|-------|--------|

Dec. 22, 1959 42

20' Lt.

20' Lt.





1  
Co Rd C at  
N.P. Bridge

Profile

Englis to Hazelwood

| Sta | +    | $\pi$  | - | Elev   |
|-----|------|--------|---|--------|
| BM  | 5.38 | 900.88 |   | 895.50 |

|       |  |  |     |      |
|-------|--|--|-----|------|
| 52+40 |  |  | 5.8 | 95.1 |
|-------|--|--|-----|------|

|    |  |  |     |      |
|----|--|--|-----|------|
| 53 |  |  | 6.1 | 94.8 |
|----|--|--|-----|------|

|    |  |  |     |      |
|----|--|--|-----|------|
| 54 |  |  | 6.3 | 94.6 |
|----|--|--|-----|------|

|    |  |  |     |      |
|----|--|--|-----|------|
| 55 |  |  | 5.7 | 95.2 |
|----|--|--|-----|------|

|    |  |  |     |      |
|----|--|--|-----|------|
| 56 |  |  | 4.4 | 96.5 |
|----|--|--|-----|------|

|    |  |  |     |      |
|----|--|--|-----|------|
| 57 |  |  | 1.6 | 99.3 |
|----|--|--|-----|------|

|    |       |        |      |        |
|----|-------|--------|------|--------|
| TP | 11.44 | 910.69 | 1.63 | 899.25 |
|----|-------|--------|------|--------|

|    |  |  |     |      |
|----|--|--|-----|------|
| 58 |  |  | 8.8 | 01.8 |
|----|--|--|-----|------|

|    |  |  |     |      |
|----|--|--|-----|------|
| 59 |  |  | 5.8 | 04.8 |
|----|--|--|-----|------|

|    |  |  |     |      |
|----|--|--|-----|------|
| 60 |  |  | 2.7 | 08.0 |
|----|--|--|-----|------|

|    |      |        |      |        |
|----|------|--------|------|--------|
| TP | 9.96 | 918.63 | 1.97 | 908.72 |
|----|------|--------|------|--------|

908.67

FX  
RG  
KP

Oct 28, 1958

2

Spike in Arc Lt Post #330 by Ho #1337EG.R/C

English

| Sta | +     | $\pi$  | -    | Elev   |
|-----|-------|--------|------|--------|
|     |       | 918.63 |      |        |
| 61  |       |        | 7.8  | 10.8   |
| 62  |       |        | 5.3  | 13.3   |
| +50 |       |        | 4.0  | 14.6   |
| 63  |       |        | 2.6  | 16.0   |
| +50 |       |        | 0.8  | 17.8   |
| TP  | 13.26 | 930.70 | 1.19 | 917.44 |
| 64  |       |        | 11.0 | 19.7   |
| +50 |       |        | 8.9  | 21.8   |
| 65  |       |        | 6.9  | 23.8   |
| +50 |       |        | 4.8  | 25.9   |



FK  
RG  
HP

Oct 28, 1958

3

| Sta   | +    | $\pi$  | -    |        |
|-------|------|--------|------|--------|
|       |      | 930.70 |      |        |
| 66+00 |      |        | 2.5  | 28.2   |
| +25   |      |        | 1.4  | 29.3   |
| +50   |      |        | 0.9  | 29.8   |
| +75   |      |        | 1.1  | 29.6   |
| 67    |      |        | 1.8  | 28.9   |
| +25   |      |        | —    |        |
| +50   |      |        | 4.4  | 26.3   |
| TP    | 0.16 | 924.71 | 6.15 | 924.55 |
| 68    |      |        | 0.4  | 24.3   |

FK  
RG  
KP

October 28, 1958

A

| Sta | + | $\pi$  | - | Elev |
|-----|---|--------|---|------|
|     |   | 924.71 |   |      |

|       |  |  |     |      |
|-------|--|--|-----|------|
| 68+50 |  |  | 2.2 | 22.5 |
|-------|--|--|-----|------|

|    |  |  |     |      |
|----|--|--|-----|------|
| 69 |  |  | 3.8 | 20.9 |
|----|--|--|-----|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 5.0 | 19.7 |
|-----|--|--|-----|------|

|    |  |  |     |      |
|----|--|--|-----|------|
| 70 |  |  | 5.9 | 18.8 |
|----|--|--|-----|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 6.3 | 18.4 |
|-----|--|--|-----|------|

|    |  |  |     |      |
|----|--|--|-----|------|
| 71 |  |  | 6.4 | 18.3 |
|----|--|--|-----|------|

|    |  |  |     |      |
|----|--|--|-----|------|
| 72 |  |  | 5.9 | 18.8 |
|----|--|--|-----|------|

|    |  |  |     |      |
|----|--|--|-----|------|
| 73 |  |  | 5.1 | 19.6 |
|----|--|--|-----|------|



October 28, 1958

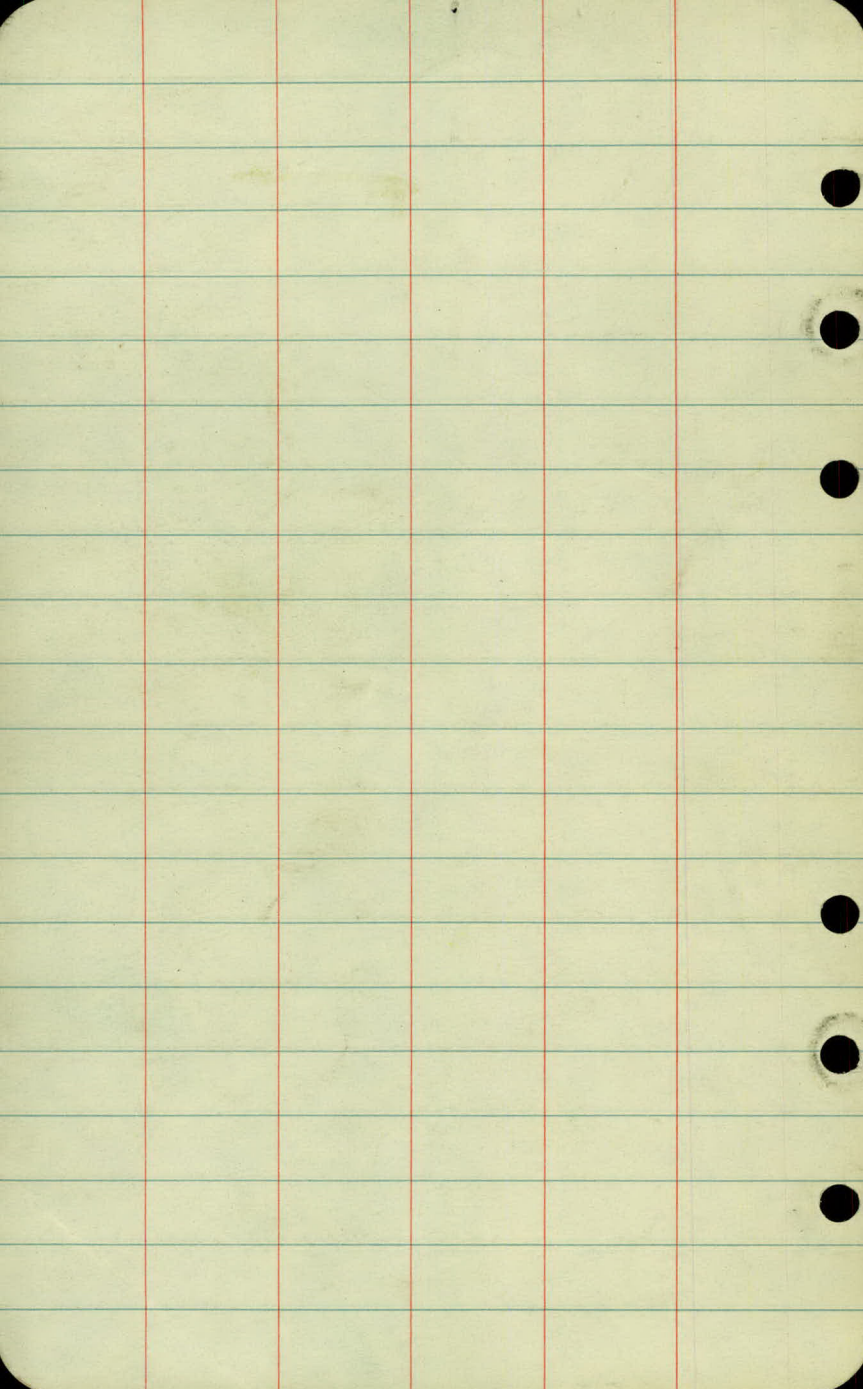
5

| Sf <sub>g</sub> | + | $\pi$  | -    | Elev    |
|-----------------|---|--------|------|---------|
|                 |   | 924.71 |      |         |
| 74              |   |        | 3.7  | 21.0    |
| 75              |   |        | 2.6  | 22.1    |
| BM              |   |        | 3.19 | 921.52  |
|                 |   |        |      | 921.529 |

Oct. 28, 1958

6

Top G.R. Post Easternmost Post N. Side





Sept 28, 1960

4

Profile

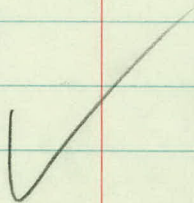
Bridge # 7279

Co. Rd. "C"

East of T. H. 61

Rec. 9/29/60

Plotted  
L. D. G.



| Sta | +    | $\pi$  | - | Elev   |
|-----|------|--------|---|--------|
| BM  | 9.60 | 931.99 |   | 922.39 |

|    |  |  |      |       |   |
|----|--|--|------|-------|---|
| 65 |  |  | 8.20 | 23.79 | - |
|----|--|--|------|-------|---|

|       |  |  |      |       |   |
|-------|--|--|------|-------|---|
| 66+05 |  |  | 3.95 | 28.04 | - |
|-------|--|--|------|-------|---|

|     |  |  |      |       |   |
|-----|--|--|------|-------|---|
| +15 |  |  | 3.72 | 28.27 | - |
|-----|--|--|------|-------|---|

|     |  |  |      |       |   |
|-----|--|--|------|-------|---|
| +24 |  |  | 3.34 | 28.65 | - |
|-----|--|--|------|-------|---|

|     |  |  |      |       |   |
|-----|--|--|------|-------|---|
| +33 |  |  | 3.18 | 28.81 | - |
|-----|--|--|------|-------|---|

|    |      |        |      |        |  |
|----|------|--------|------|--------|--|
| TP | 4.54 | 933.68 | 2.85 | 929.14 |  |
|----|------|--------|------|--------|--|

|     |  |  |      |       |   |
|-----|--|--|------|-------|---|
| +43 |  |  | 4.63 | 29.05 | - |
|-----|--|--|------|-------|---|

|     |  |  |      |       |   |
|-----|--|--|------|-------|---|
| +54 |  |  | 4.73 | 28.95 | - |
|-----|--|--|------|-------|---|

|     |  |  |      |       |   |
|-----|--|--|------|-------|---|
| +62 |  |  | 4.84 | 28.84 | - |
|-----|--|--|------|-------|---|

|     |  |  |      |       |   |
|-----|--|--|------|-------|---|
| +70 |  |  | 5.06 | 28.62 | - |
|-----|--|--|------|-------|---|

FK  
JL  
WM

~~Sept.~~ Sept. 28, 1960

5

stamp

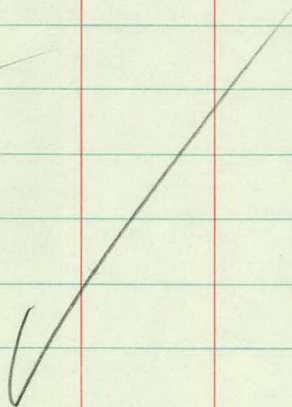
£

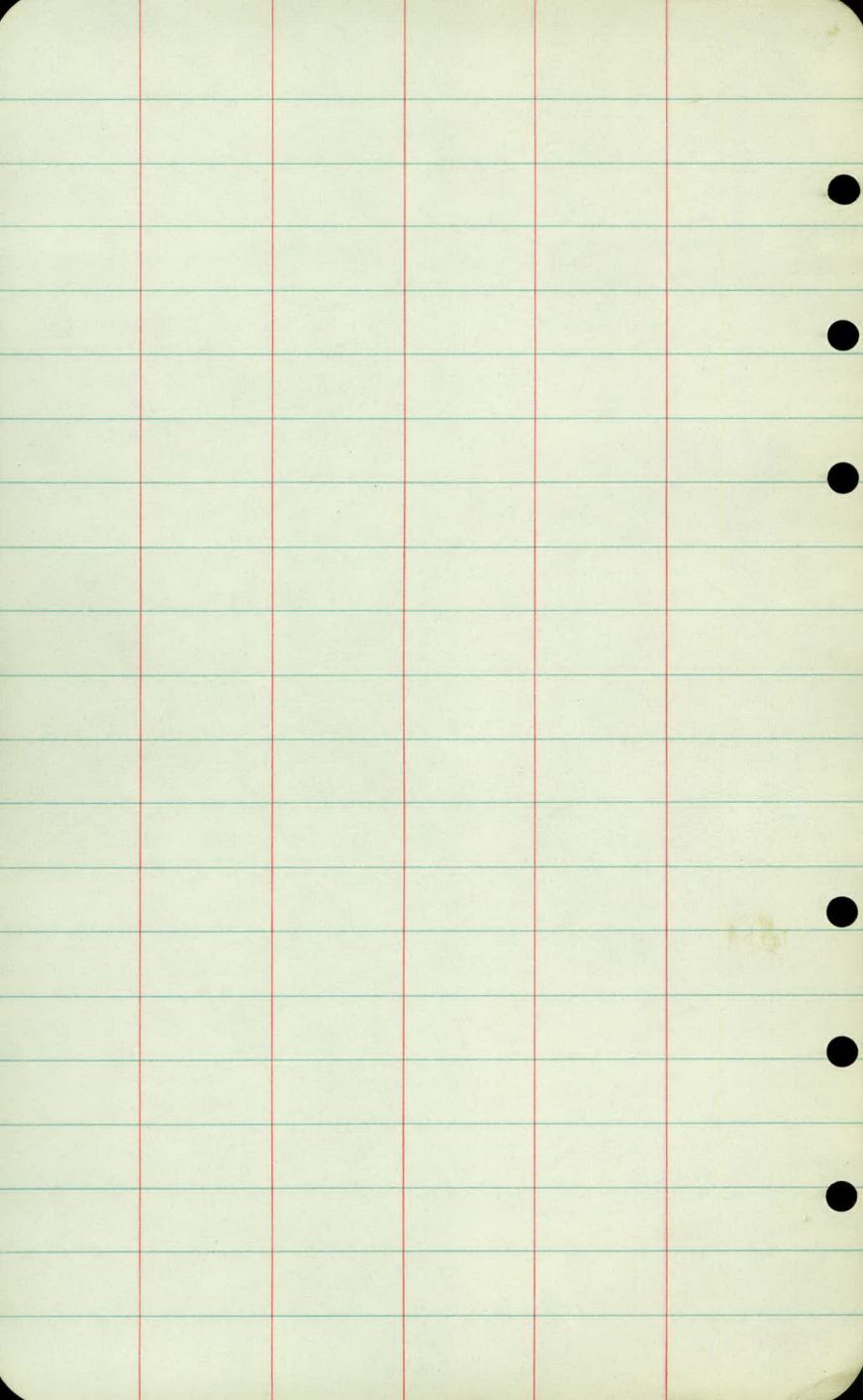
| Sta   | + | $\pi$  | -     | Elev   |   |
|-------|---|--------|-------|--------|---|
|       |   | 933.68 |       |        |   |
| 66+77 |   |        | 5.15  | 28.53  | - |
| +85   |   |        | 5.23  | 28.45  | - |
| +94   |   |        | 5.30  | 28.38  | - |
| 67    |   |        | 5.52  | 28.16  | - |
| +11   |   |        | 5.84  | 27.84  | - |
| stake |   |        | 10.92 | 922.76 |   |



Sept 28, 1960

9 22.76  
908.50  
14.26  
C 14.27

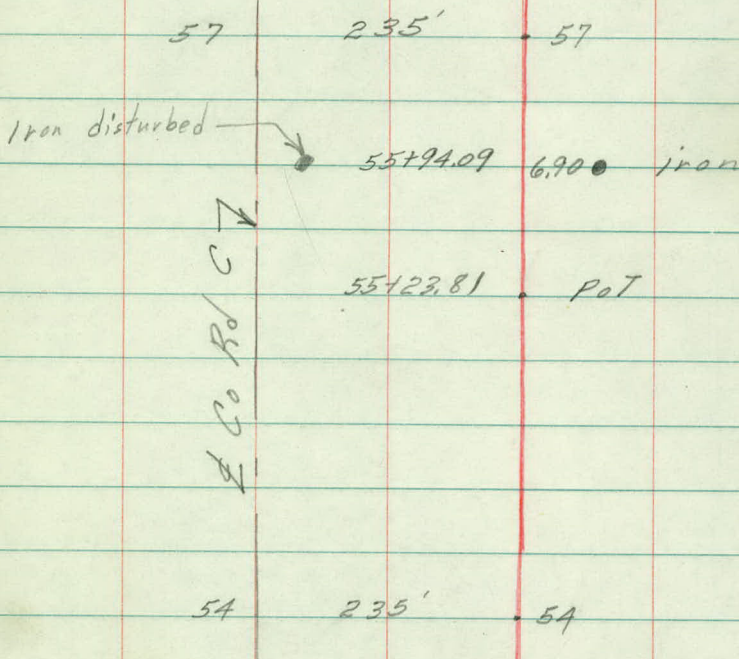




Co Rd "C" Bridge # 7279

Borrow Pit

x-sections



CMD.KP 10/18/60

Rec. 10/17/60 11 pages  
reduced 10/18/60 KP

Sta +  $\pi$  - Elev.

BM 9.54 905.04

895.50

52+50

✓

TP 9.40 911.36 9.08 901.96

+75

✓

53

✓



FA  
JL  
WM

Oct. 14, 1960  
Fog 58

2

Spike in Archt. Pole #330 by Ho #1337 E.C.R.D.C.

|      |      |      |      |        |      |      |      |
|------|------|------|------|--------|------|------|------|
| 99.8 | 99.1 | 00.6 | 00.5 | ✓ 00.2 | 99.8 | 98.8 | 95.2 |
| 5.2  | 5.3  | 4.4  | 4.5  | 4.8    | 5.2  | 6.2  | 9.8  |
| 55   | 48   | 36   | 15   |        | 13   | 22   | 35   |

99.1  
5.3  
6.5

91.9      92.8  
13.1      12.2  
75      52  
Fe

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 02.0 | 01.3 | 01.5 | 01.1 | 00.7 | 00.4 | 97.5 |
| 9.4  | 10.1 | 9.9  | 10.3 | 10.7 | 11.0 | 13.9 |
| 39   | 32   | 14   | ✓    | 13   | 24   | 31   |

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| 03.1 | 98.4 | 98.5 | 94.5 | 97.0 | 96.8 | 95.5 | 94.3 |
| 7.7  | 13.0 | 12.9 | 16.9 | 14.4 | 14.6 | 15.9 | 17.1 |
| 46   | 55   | 78   | 75   | 71   | 66   | 61   | 47   |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 99.1 | 98.4 | 02.2 | 02.0 | 01.6 | 01.1 | 01.3 | 00.4 | 99.1 |
| 133  | 130  | 9.2  | 9.4  | 9.8  | 10.3 | 10.1 | 11.0 | 11.7 |
| 49   | 34   | 24   | 14   | ✓    | 13   | 37   | 42   | 45   |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 97.9 | 98.1 | 98.8 | 00.6 | 00.1 | 00.7 | 00.5 |
| 13.5 | 13.3 | 12.6 | 10.8 | 11.3 | 10.7 | 10.9 |
| 65   | 85   | 75   | 72   | 64   | 58   | 47   |
|      |      | Fe   |      |      |      |      |

Sta +  $\pi$  - Elev.

911.36

53+25

✓

+50

✓

+75

✓

Oct. 14, 1960 3

L1

RT

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 98.2 | 98.2 | 97.8 | 01.3 | 02.7 | 02.7 | 02.8 | 02.6 | 02.9 |
| 132  | 132  | 136  | 10.1 | 87   | 8.7  | 8.6  | 8.8  | 8.6  |
| 44   | 26   | 8    | 1    | ✓ 18 | 36   | 52   | 67   |      |

98.3 98.3

03.9 04.9 03.3

→ 13.1 13.1  
60 83

7.5 6.5 8.1  
76 72 69

98.4 98.8 99.0 99.3 99.6 02.2 04.5 04.9 04.9

130 126 124 12.1 11.8 9.2 6.9 6.5 6.6  
30 21 10 ✓ 3 9 14 30 39

98.8 98.7 98.2 06.9 07.2 04.9 05.2 05.0 04.3

→ 12.6 12.7 132 154.2 6.5 6.2 6.4 7.1  
48 65 84 } 82 76 73 56 44 41

98.4 98.9 99.3 00.1 01.5 01.9 01.8 02.3 06.6

130 125 12.1 11.3 99 9.5 9.6 9.1 4.8  
70 50 33 14 ✓ 8 16 20 31

98.3

09.6 10.1 01.2 06.5 06.4 06.4

→ 13.1  
80 } 1.8 1.3 4.2 4.9 5.0 5.0  
88 80 77 71 61 46

Sta +  $\Delta$  - Elev

911.36

54

✓

✓

TP 6.59 915.33 2.62 908.74

+25

✓

+50



Oct. 14, 1960 4

LT

BT

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 07.1 | 08.0 | 05.9 | 08.1 | 08.6 | 08.6 | 05.1 | 08.1 | 08.2 |
| 3.7  | 3.4  | 5.5  | 3.3  | 2.8  | 2.8  | 6.3  | 2.7  | 3.2  |
| 23   | 17   | 13   | 10   |      | 6    | 12   | 17   | 30   |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 05.5 | 01.9 | 00.2 | 08.8 | 08.3 | 01.8 | 08.2 |
| 5.9  | 9.5  | 11.2 | 12.6 | 3.1  | 3.6  | 3.2  |
| 28   | 38   | 48   | 71   | 75   | 67   | 48   |

|      |      |      |      |      |
|------|------|------|------|------|
| 08.8 | 08.7 | 09.2 | 10.9 | 13.1 |
| 12.6 | 12.7 | 2.2  | 0.5  | 12.3 |
| 100  | 86   | 78   | 80   | 83   |

Tack in stake 54+100

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 00.1 | 08.4 | 08.8 | 09.0 | 09.4 | 08.9 | 09.1 | 10.4 | 10.6 |
| 15.2 | 6.9  | 6.5  | 6.3  | 5.9  | 6.4  | 6.2  | 4.9  | 4.7  |
| 62   | 50   | 42   | 19   | 9    | 18   | 25   | 39   |      |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 09.2 | 08.7 | 16.5 | 14.8 | 13.7 | 11.5 | 10.6 |
| 16.1 | 16.6 | 11.2 | 0.5  | 1.6  | 3.8  | 4.7  |
| 67   | 94   | 83   | 81   | 80   | 76   | 59   |

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| 08.8 | 10.0 | 09.9 | 10.2 | 09.9 | 09.9 | 12.8 | 13.5 |
| 6.5  | 5.3  | 5.4  | 5.1  | 5.4  | 5.4  | 2.5  | 1.8  |
| 43   | 28   | 16   |      | 14   | 26   | 36   | 60   |

Sta +  $\pi$  - Elev

915.33

54+50

TP 4.97 915.95 4.35 910.98

+75

✓

55

✓

TP 13.68 928.52 1.11 914.84

54+75

Oct 14, 1960 5  
RT

99.3 99.7 04.8 14.3 14.9 19.9  
16.0 15.6 10.5 ✓ 1.0 0.4 + 4.6  
100 67 48 69 20 75  
54+50 stake

05.0 09.0 10.3 10.5 10.8 10.4 12.0 15.8  
11.0 7.0 5.7 5.5 5.2 5.6 4.0 0.2  
61 58 54 29 ✓ 17 38 46

00.3 99.2 99.4  
15.7 16.8 16.6  
65 70 91

01.5 01.0 11.4 12.0 14.4 14.4  
14.5 9.0 4.6 4.0 ✓ 1.6 1.6  
66 50 36 18 8

99.8 99.7  
14.2 16.3  
88 100

15.9 16.5 21.1 21.4  
12.6 ✓ 12.0 7.4 7.1 7.2  
48 59 67 86 89

Sta +  $\pi$  - Elev

928.52

55

✓

✓

TP 5.17 930.31 3.38 925.14

+20

✓

+35



47

± Oct. 14, 1960

RT

6

|      |      |      |      |
|------|------|------|------|
| 15.8 | 16.8 | 18.2 | 19.8 |
| 12.7 | 11.7 | 10.3 | 8.7  |
| 11   | 14   | 23   | 31   |

|      |      |      |      |
|------|------|------|------|
| 21.4 | 21.4 | 21.1 | 19.6 |
| 71   | 74   | 74   | 8.9  |
| 70   | 61   | 48   | 45   |

|      |      |      |      |
|------|------|------|------|
| 21.8 | 22.3 | 23.9 | 22.9 |
| 6.7  | 6.2  | 4.6  | 5.6  |
| 77   | 82   | 85   | 100  |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 16.1 | 19.8 | 24.2 | 25.9 | 27.5 | 27.1 | 25.8 | 24.1 | 23.1 |
| 14.2 | 10.5 | 6.1  | 4.4  | 2.8  | 3.2  | 4.5  | 6.2  | 7.2  |
| 53   | 51   | 32   | 16   |      | 13   | 27   | 46   | 67   |

|      |      |
|------|------|
| 22.3 | 22.6 |
| 8.0  | 7.7  |
| 100  | 86   |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 17.1 | 17.9 | 22.5 | 25.3 | 26.6 | 26.4 | 24.8 | 22.7 | 22.1 |
| 13.2 | 12.4 | 7.8  | 5.0  | 3.7  | 3.9  | 5.5  | 7.6  | 8.2  |
| 65   | 55   | 35   | 18   |      | 12   | 28   | 51   | 67   |

|        |
|--------|
| 15.9   |
| → 14.4 |
| 69     |

|      |      |
|------|------|
| 21.0 | 20.9 |
| 9.3  | 9.4  |
| 100  | 88   |

Sta +  $\pi$  - Elev.

930.31

55+50

✓

TP 3.83 923.29 10.85 919.46

+ 75

10.3

913.0

✓

56

Oct. 14, 1960 7

LT

BT

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 12.9 | 11.1 | 21.0 | 23.7 | 24.5 | 24.2 | 22.6 | 21.2 | 20.2 |
| 174  | 132  | 93   | 66   | 58   | 61   | 77   | 91   | 101  |
| 68   | 49   | 31   | 15   | 15   | 15   | 32   | 48   | 67   |

|      |      |
|------|------|
| 19.1 | 19.2 |
| 11.2 | 11.1 |
| 100  | 88   |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 10.5 | 13.8 | 16.4 | 19.4 | 20.8 | 20.5 | 19.5 | 18.3 | 17.9 |
| 12.8 | 9.5  | 6.9  | 3.9  | 2.5  | 2.8  | 3.8  | 5.0  | 5.4  |
| 72   | 53   | 36   | 17   | 17   | 17   | 34   | 52   | 69   |

09.5  
→ 13.8  
77

|      |      |
|------|------|
| 16.9 | 17.2 |
| 6.4  | 6.1  |
| 100  | 88   |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 09.5 | 12.6 | 15.5 | 17.8 | 19.2 | 19.3 | 18.1 | 16.9 | 16.2 |
| 138  | 10.7 | 7.8  | 5.5  | 4.1  | 4.0  | 5.2  | 6.4  | 7.1  |
| 74   | 52   | 31   | 15   | 19   | 19   | 43   | 64   | 83   |

15.8  
7.5  
100

Sta

+

$\pi$

-

Elev.

923.29

56 + 25

✓

+ 50

✓

+ 75

✓



Oct 14, 1960 8

11  
 09.4 10.9 14.0 17.6 19.9 20.1 19.2 16.8 16.8  
 137 124 93 57 34 32 41 45 65  
 66 57 36 16 22 39 44 64

15.0 16.3  
 8.3 7.0  
 100 81

09.3 11.9 14.6 17.4 20.2 20.5 18.9 19.8 18.2  
 14.0 11.4 8.7 5.9 3.1 2.8 4.4 3.5 5.1  
 61 46 31 17 6 11 15 21

15.0 15.9 16.7 18.8 20.4 18.2  
 8.3 7.4 6.6 4.5 2.9 5.1  
 100 81 65 46 27 24

11.6 12.5 16.0 18.7 17.9 17.7 19.0 19.6 18.7  
 117 108 73 46 54 56 43 37 46  
 44 38 18 3 5 13 17 28

09.7  
 13.6  
 53

13.3 14.1 16.5 18.1  
 10.0 9.2 6.8 5.2  
 100 81 58 43

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

|    |  |        |  |  |
|----|--|--------|--|--|
| 57 |  | 923.29 |  |  |
|----|--|--------|--|--|

|  |  |       |  |  |
|--|--|-------|--|--|
|  |  | 93.50 |  |  |
|--|--|-------|--|--|

|  |  |       |  |  |
|--|--|-------|--|--|
|  |  | 27.79 |  |  |
|--|--|-------|--|--|

|  |  |       |  |  |
|--|--|-------|--|--|
|  |  | 13.21 |  |  |
|--|--|-------|--|--|

✓

|    |      |        |       |        |
|----|------|--------|-------|--------|
| TP | 1.01 | 911.09 | 13.21 | 910.08 |
|----|------|--------|-------|--------|

55+35

✓

+20

✓

Oct. 14, 1960 9  
BT

11  
09.6 12.2 15.8 18.4 18.3 17.5 17.5 16.3  
13.7 11.1 7.5 4.9 5.0 5.8 5.8 7.0  
53 37 18 13 35 41 46

✓ 10.9 12.5 13.8  
12.4 10.8 9.5  
100 86 69

00.5 04.0 06.5 09.8  
10.6 7.1 4.6 1.3  
130 114 103 87

98.3 96.7  
12.8 14.4  
141 151

00.0 01.4 05.8 09.4  
11.1 9.7 5.3 1.7  
138 117 102 98

99.4  
11.7  
153

Sta +  $\pi$  - Elev.

911.09

55+50

+75

56

BM 13.42 908.92 15.54 895.55 (895.50)

+25

61 +50

71 +75

87



FK  
JL  
WM

Oct 14, 1960  
Lt Oct 17, 1960 10

|      |      |      |      |      |
|------|------|------|------|------|
| 91.5 | 99.1 | 02.1 | 05.0 | 08.4 |
| 13.6 | 12.0 | 9.0  | 6.1  | 2.7  |
| 14.8 | 137  | 123  | 108  | 89   |

|      |      |      |      |      |      |
|------|------|------|------|------|------|
| 96.7 | 98.1 | 99.7 | 02.5 | 05.9 | 08.3 |
| 14.4 | 130  | 11.4 | 8.6  | 5.2  | 2.8  |
| 172  | 150  | 134  | 116  | 97   | 86   |

|      |      |      |      |      |      |
|------|------|------|------|------|------|
| 98.2 | 99.0 | 01.6 | 02.3 | 04.6 | 07.6 |
| 12.9 | 12.1 | 9.5  | 8.8  | 6.5  | 3.5  |
| 180  | 155  | 136  | 120  | 101  | 87   |

Spike in Arc Lt P<sub>2</sub> 330 B<sub>2</sub> H<sub>2</sub> 1337 ECRd C

|      |      |      |      |      |
|------|------|------|------|------|
| 99.9 | 00.0 | 01.6 | 04.1 | 06.2 |
| 9.0  | 8.9  | 7.3  | 4.8  | 2.7  |
| 170  | 152  | 126  | 100  | 87   |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 01.0 | 01.1 | 02.3 | 03.7 | 05.8 | 06.0 | 08.1 |
| 7.9  | 7.8  | 6.6  | 5.2  | 3.1  | 2.9  | 0.8  |
| 160  | 147  | 120  | 97   | 83   | 77   | 56   |

|      |      |      |      |
|------|------|------|------|
| 01.9 | 02.8 | 04.5 | 07.2 |
| 7.0  | 6.1  | 4.4  | 1.7  |
| 150  | 125  | 90   | 67   |

Sta      +       $\pi$       -      Elev.

908.92

57      section  $\rightarrow$  9.6

11.

Oct 17, 1960

11

03.0

✓ 03.4

04.7

06.8

5.9

5.5

4.2

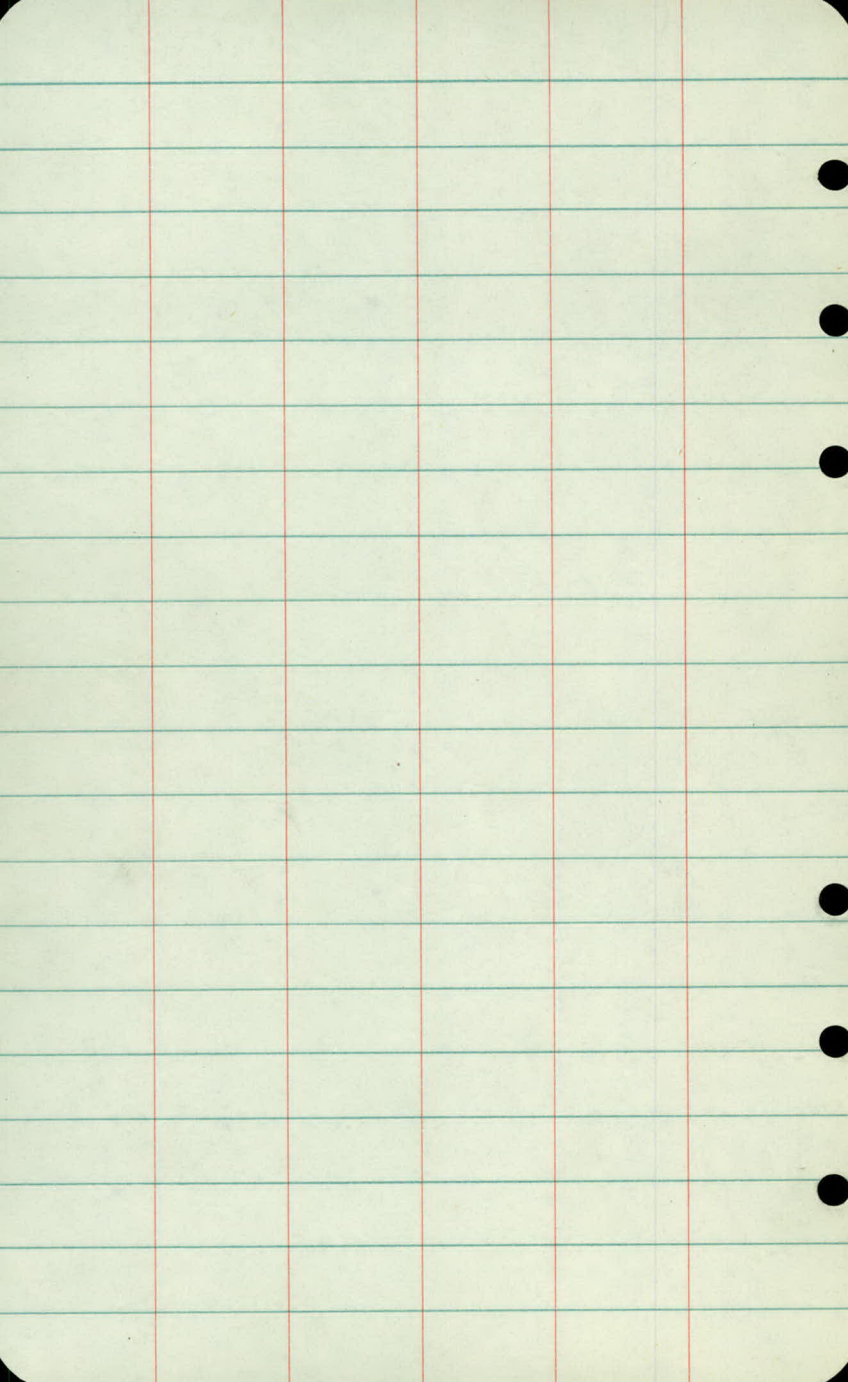
2.1

150

126

98

72





Co. Rd. "C" Borrow Pit

Additional X-Sections

3 pages

| Sta | +    | $\pi$  | -    | Elev   |
|-----|------|--------|------|--------|
| BM  | 8.50 | 904.00 |      | 895.50 |
| TP  | 8.42 | 910.41 | 2.03 | 901.97 |

53+75

54+00

+20

✓

+33

✓

R6  
JL  
WIN  
B3

April 11, 1961

Lt.

E

R+

2

Spike in Power Pole #330 by Ho<sup>u</sup> 1337 E.C., R.L.C.

|      |      |      |      |     |          |
|------|------|------|------|-----|----------|
| 11.8 | 11.6 | 11.1 | 10.3 | 8.9 | NG on Rt |
| 70   | 50   | 33   | 14   |     |          |

|      |      |      |     |     |     |     |     |     |
|------|------|------|-----|-----|-----|-----|-----|-----|
| 11.6 | 10.7 | 10.4 | 9.9 | 5.4 | 2.4 | 4.7 | 1.4 | 1.2 |
| 75   | 50   | 28   | 8   |     | 5   | 12  | 20  | 34  |

|     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 9.9 | 9.1 | 9.7 | 8.6 | 5.1 | 0.8 | 0.9 | 1.1 | 0.5 |
| 60  | 42  | 33  | 18  | 12  | 2   |     | 8   | 25  |
|     |     |     |     |     |     |     | NG  | NG  |

|      |      |
|------|------|
| 10.8 | 11.6 |
| 63   | 75   |

|      |     |     |     |     |     |     |
|------|-----|-----|-----|-----|-----|-----|
| 10.7 | 8.6 | 5.3 | 2.0 | 1.0 | 0.9 | 1.0 |
| 67   | 59  | 51  | 45  | 30  | 15  |     |
|      |     |     | NG  | NG  | NG  |     |

|      |
|------|
| 11.2 |
| 25   |

| sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

|    |  |        |  |  |
|----|--|--------|--|--|
| TP |  | 910.41 |  |  |
|----|--|--------|--|--|

|    |      |        |       |        |
|----|------|--------|-------|--------|
| TP | 2.81 | 901.58 | 11.64 | 898.77 |
|----|------|--------|-------|--------|

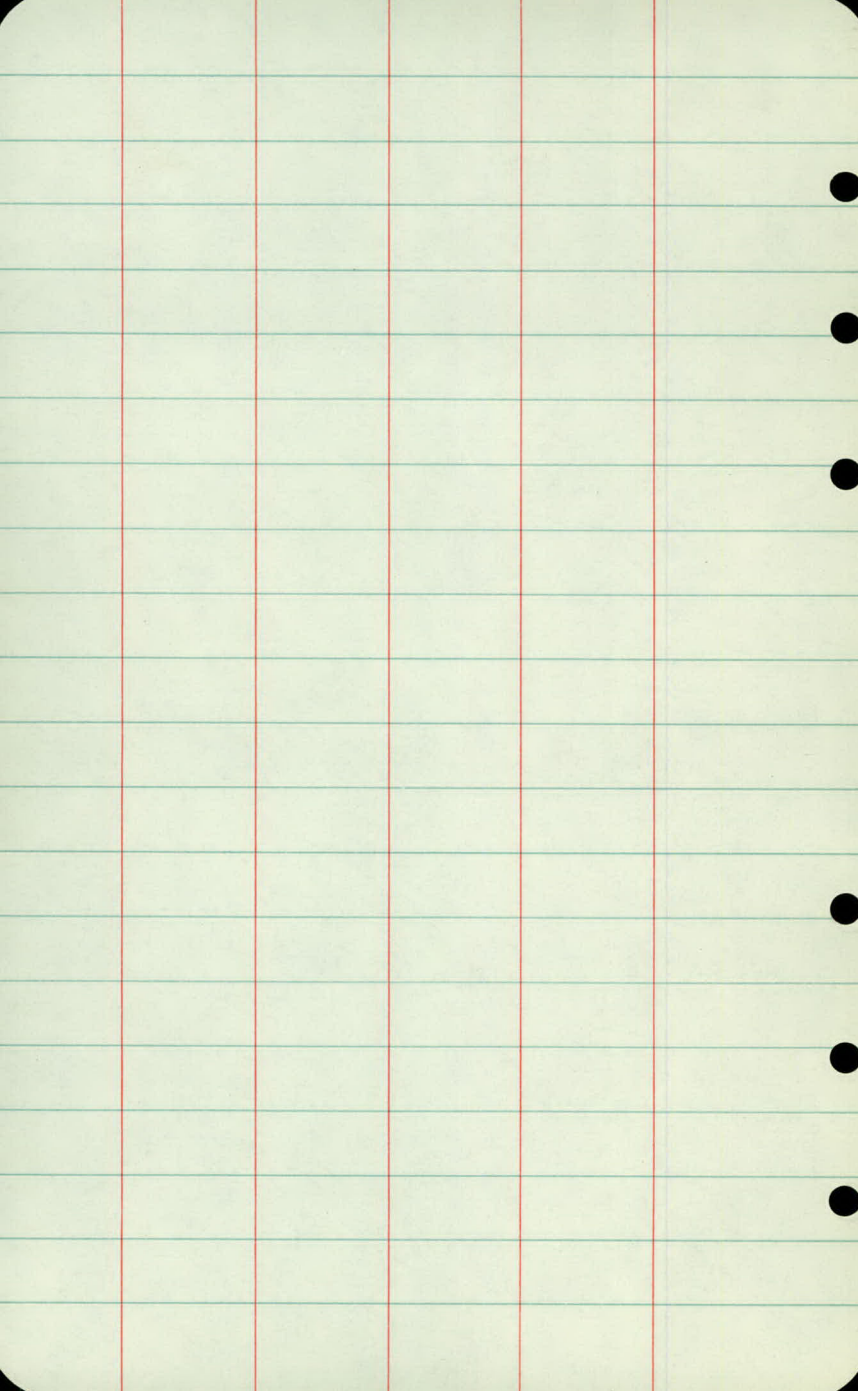
|    |  |  |      |          |
|----|--|--|------|----------|
| BM |  |  | 6.06 | 895.52   |
|    |  |  |      | (895.50) |



April 17, 1961

3

Spike in PPT#330 by HD#1337 E. Co. Rd C



Co Rd "C"

White Bear Ave to Bellaire

Profile  
&  
Benches

Drainage seems to Extend to 2 blocks south  
and indefinite to North

16 pages

RCG 11/8/56

plotted 11/56

| Sta | +     | $\pi$  | -    | Elev            |
|-----|-------|--------|------|-----------------|
| BM  | 5.12  | 935.67 |      | (930.55)        |
| T.P | 3.15  | 933.26 | 5.56 | 930.11          |
| TP  | 8.24  | 937.31 | 4.19 | 929.07 (929.05) |
| TP  | 11.72 | 948.62 | 0.41 | 936.90          |
| TP  | 12.93 | 960.97 | 0.58 | 948.04          |
| BM  |       |        | 3.37 | 957.60          |

145 3.04 57.9

+50 1.8 59.2

146 0.56 960.41

T.P. 7.99 968.40 0.56 960.41

+50 6.8 61.6



FK 4  
RG X  
KP Rd 2A

± Nov. 7, 1956 2  
Cold Windy 36° R<sub>L</sub>  
30 MPH

U.S.G.S. BM-C31-NE Cor Co Rd "C" +

White Bear Ave

Top Mont N  $\frac{1}{4}$  Cor Sec 11-T29-R22

Top Hyd NE Cor

Sta 144 ±  
+ Co Rd C

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 968.40 |  |  |
|--|--|--------|--|--|

|     |  |  |      |      |
|-----|--|--|------|------|
| 147 |  |  | 6.13 | 62.3 |
|-----|--|--|------|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 5.6 | 62.8 |
|-----|--|--|-----|------|

|     |  |  |      |      |
|-----|--|--|------|------|
| 148 |  |  | 4.94 | 63.5 |
|-----|--|--|------|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 4.5 | 63.9 |
|-----|--|--|-----|------|

|    |  |  |      |        |
|----|--|--|------|--------|
| BM |  |  | 2.83 | 965.57 |
|----|--|--|------|--------|

|     |  |  |      |      |
|-----|--|--|------|------|
| 149 |  |  | 4.34 | 64.1 |
|-----|--|--|------|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 4.4 | 64.0 |
|-----|--|--|-----|------|

Nov. 1956

3

Lt

B+

Top Hyd Lt Sta 148+50±

| Sta | + | x | - | Elev |
|-----|---|---|---|------|
|-----|---|---|---|------|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 968.40 |  |  |
|--|--|--------|--|--|

|     |  |  |      |      |
|-----|--|--|------|------|
| 150 |  |  | 4.55 | 63.8 |
|-----|--|--|------|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 4.6 | 63.8 |
|-----|--|--|-----|------|

|     |  |  |      |      |
|-----|--|--|------|------|
| 151 |  |  | 4.52 | 63.8 |
|-----|--|--|------|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 4.4 | 64.0 |
|-----|--|--|-----|------|

|     |  |  |      |      |
|-----|--|--|------|------|
| 152 |  |  | 4.41 | 64.0 |
|-----|--|--|------|------|

|    |      |        |      |        |
|----|------|--------|------|--------|
| TP | 5.09 | 969.08 | 4.41 | 963.99 |
|----|------|--------|------|--------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 5.1 | 64.0 |
|-----|--|--|-----|------|



£ Nov 7, 1956

Lt

Rt

4

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

969.08

|     |  |  |      |      |
|-----|--|--|------|------|
| 153 |  |  | 4.96 | 64.1 |
|-----|--|--|------|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 4.8 | 64.3 |
|-----|--|--|-----|------|

|     |  |  |      |      |
|-----|--|--|------|------|
| 154 |  |  | 4.71 | 64.4 |
|-----|--|--|------|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 4.7 | 64.4 |
|-----|--|--|-----|------|

|     |  |  |      |      |
|-----|--|--|------|------|
| 155 |  |  | 4.73 | 64.4 |
|-----|--|--|------|------|

|    |      |        |      |        |
|----|------|--------|------|--------|
| BM | 3.72 | 969.13 | 3.67 | 965.41 |
|----|------|--------|------|--------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 4.8 | 64.3 |
|-----|--|--|-----|------|

2 Nov. 7, 1956

5

Lt

Rt

Top Hyd Lt Sta 155<sup>±</sup>

Sta +  $\pi$  - Elev

969.13

156 4.83 64.3

+50 4.9 64.2

157 4.58 64.5

+50 4.4 64.7

+ 59.6  $\pm$  4<sup>th</sup> st N.W. 4.37 64.7  
64.8

158 4.34 64.8



Nov. 7, 1956

1+

RT

6

|       |      |      |      |      |
|-------|------|------|------|------|
| 67.25 | 66.1 | 65.5 | 65.1 | 64.8 |
| 1.85  | 3.0  | 3.6  | 4.0  | 4.3  |
| 250   | 200  | 150  | 100  | 50   |
| MH    |      |      |      |      |

4.37

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 969.13 |  |  |
|--|--|--------|--|--|

|        |  |  |     |      |
|--------|--|--|-----|------|
| 158+50 |  |  | 4.5 | 64.6 |
|--------|--|--|-----|------|

|     |  |  |      |      |
|-----|--|--|------|------|
| 159 |  |  | 4.73 | 64.4 |
|-----|--|--|------|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 5.0 | 64.1 |
|-----|--|--|-----|------|

|     |  |  |      |      |
|-----|--|--|------|------|
| 160 |  |  | 5.35 | 63.7 |
|-----|--|--|------|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 5.4 | 63.7 |
|-----|--|--|-----|------|

|    |     |        |      |        |
|----|-----|--------|------|--------|
| BM | 168 | 968.17 | 2.64 | 966.49 |
|----|-----|--------|------|--------|

|     |  |  |      |      |
|-----|--|--|------|------|
| 161 |  |  | 4.54 | 63.7 |
|-----|--|--|------|------|

£ Nov. 21956

LT

RT

7

Top Hyd Lt. Sta  $160 \pm 80^{\pm}$  B<sub>4</sub> H<sub>0</sub> #345 C.R.J.C

| Sta    | +    | $\pi$    | -    | Elev   |   |
|--------|------|----------|------|--------|---|
|        |      | 968.17   |      |        |   |
| 161+50 |      |          | 4.7  | 63.5   |   |
| 162    |      |          | 4.64 | 63.6   |   |
| +50    |      |          | 4.6  | 63.6   |   |
| 163    |      |          | 4.52 | 63.7   |   |
| +50    |      |          | 4.4  | 63.8   |   |
| +85    | ±    | Delaware | 4.29 | 63.9   |   |
| 164    |      |          | 4.32 | 63.9   |   |
| BM     | 2.38 | 968.47   | 2.08 | 966.09 | ✓ |



Nov 7, 1956

8

17

RT

|      |      |      |      |      |
|------|------|------|------|------|
| 61.9 | 62.4 | 63.3 | 63.3 | 63.3 |
| 6.3  | 5.8  | 4.89 | 4.9  | 4.9  |
| 250  | 200  | 150  | 100  | 50   |

970.2  
Elev 3rd St +  
15th Ave N.W.

Top Hyd N.W. Cor. Delaware & Co Rd "C"

| Sta | + | $\pi$  | - | Elev |
|-----|---|--------|---|------|
|     |   | 968.47 |   |      |

|        |  |  |     |      |
|--------|--|--|-----|------|
| 164+50 |  |  | 4.5 | 64.0 |
|--------|--|--|-----|------|

|     |  |  |      |      |
|-----|--|--|------|------|
| 165 |  |  | 4.50 | 64.0 |
|-----|--|--|------|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 4.4 | 64.1 |
|-----|--|--|-----|------|

|     |  |  |      |      |
|-----|--|--|------|------|
| 166 |  |  | 4.25 | 64.2 |
|-----|--|--|------|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 4.0 | 64.5 |
|-----|--|--|-----|------|

|     |  |  |      |      |
|-----|--|--|------|------|
| 167 |  |  | 3.90 | 64.6 |
|-----|--|--|------|------|

£ Nov. 2, 1956

9

11

RT

| Sta | + | x | - | Elev |
|-----|---|---|---|------|
|-----|---|---|---|------|

|  |  |        |  |  |
|--|--|--------|--|--|
|  |  | 968.47 |  |  |
|--|--|--------|--|--|

|        |  |  |     |      |
|--------|--|--|-----|------|
| 167+50 |  |  | 3.6 | 64.9 |
|--------|--|--|-----|------|

|    |      |        |      |        |
|----|------|--------|------|--------|
| BM | 2.99 | 970.90 | 0.56 | 967.91 |
|----|------|--------|------|--------|

|     |  |  |      |      |
|-----|--|--|------|------|
| 168 |  |  | 5.81 | 65.1 |
|-----|--|--|------|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 5.5 | 65.4 |
|-----|--|--|-----|------|

|     |  |  |      |      |
|-----|--|--|------|------|
| 169 |  |  | 5.01 | 65.9 |
|-----|--|--|------|------|

|     |  |  |     |      |
|-----|--|--|-----|------|
| +50 |  |  | 4.4 | 66.5 |
|-----|--|--|-----|------|

|     |  |  |      |      |
|-----|--|--|------|------|
| 170 |  |  | 3.83 | 67.1 |
|-----|--|--|------|------|



£ Nov 7, 1956

10

Lt

Bl

Top Hyd Lt of £ By HO<sup>#</sup> 232 Co Bl "C"

| Sta | + | $\pi$  | - | Elev |
|-----|---|--------|---|------|
|     |   | 970.90 |   |      |

|        |  |     |  |      |
|--------|--|-----|--|------|
| 170+50 |  | 3.6 |  | 67.3 |
|--------|--|-----|--|------|

|    |      |        |      |        |
|----|------|--------|------|--------|
| BM | 3.73 | 974.66 | +0.3 | 970.93 |
|----|------|--------|------|--------|

|     |  |      |  |      |
|-----|--|------|--|------|
| 171 |  | 7.06 |  | 67.6 |
|-----|--|------|--|------|

|     |  |     |  |      |
|-----|--|-----|--|------|
| +50 |  | 6.7 |  | 68.0 |
|-----|--|-----|--|------|

|     |  |      |  |      |
|-----|--|------|--|------|
| 172 |  | 6.34 |  | 68.4 |
|-----|--|------|--|------|

|     |  |     |  |      |
|-----|--|-----|--|------|
| +50 |  | 5.7 |  | 69.0 |
|-----|--|-----|--|------|

|     |  |      |  |      |
|-----|--|------|--|------|
| 173 |  | 4.94 |  | 69.8 |
|-----|--|------|--|------|

E Nov 3, 1956

11

11

11

Top Hyd NE Cor 2<sup>nd</sup> St & Co Rd "C"

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

974.66

173+50

4.3 70.4

174

3.93 70.8

+ 50

3.7 71.0

175

3.34 71.4

+ 50

2.75

|      |      |        |      |        |
|------|------|--------|------|--------|
| T.P. | 7.79 | 981.02 | 1.43 | 973.23 |
|------|------|--------|------|--------|

|      |      |        |      |        |
|------|------|--------|------|--------|
| B.M. | 3.25 | 982.99 | 1.28 | 979.74 |
|------|------|--------|------|--------|

|      |      |        |      |        |
|------|------|--------|------|--------|
| B.M. | 1.40 | 983.57 | 0.82 | 982.17 |
|------|------|--------|------|--------|

|      |      |        |      |        |
|------|------|--------|------|--------|
| B.M. | 0.77 | 981.63 | 2.71 | 980.86 |
|------|------|--------|------|--------|

|      |      |        |      |        |
|------|------|--------|------|--------|
| B.M. | 0.70 | 980.44 | 1.89 | 979.74 |
|------|------|--------|------|--------|



£ Nov 7, 1956

12

Lt

Rt

Top Hyd NE Cor 16<sup>th</sup> Ave NW & 1<sup>st</sup> St NW.

Top Hyd NE Cor. 15<sup>th</sup> Ave NW & 1<sup>st</sup> St. NW

Top Hyd NE Cor 14<sup>th</sup> Ave NW & 1<sup>st</sup> St NW

Top Hyd NE Cor 13<sup>th</sup> Ave NW & 1<sup>st</sup> St NW

| Sta  | +    | $\pi$  | -     | Elev.           |
|------|------|--------|-------|-----------------|
|      |      | 980.44 |       |                 |
| BM   | 0.33 | 977.13 | 3.64  | 976.80          |
| BM   | 6.96 | 975.34 | 8.75  | 968.38          |
| TP   | 2.72 | 972.88 | 5.185 | 970.16          |
| BM   | 0.18 | 968.17 | 4.89  | 967.99 (965.20) |
| TP   | 3.21 | 961.10 | 10.28 | 957.89          |
| TP   | 4.99 | 962.97 | 3.12  | 957.98          |
| BM   |      |        | 0.95  | 962.02 (961.71) |
| TP   | 1.37 | 974.60 |       | 973.23          |
| BM   | 0.10 | 971.03 | 3.67  | 970.93          |
| BM   |      |        | 3.13  | 967.90          |
| BM   | 3.71 | 969.79 | 4.95  | 966.08          |
| BM   |      |        | 3.32  | 966.47          |
| BM   | 3.89 | 969.25 | 4.43  | 965.36          |
| BM   | 0.67 | 966.22 | 3.70  | 965.55          |
| BM   | 0.27 | 957.86 | 8.63  | 957.59          |
| T.P. | 0.43 | 944.75 | 13.54 | 944.32          |
| T.P. | 2.14 | 936.88 | 10.01 | 934.74          |
| BM   |      |        | 7.83  | 929.05 (929.05) |

FK  
RG  
KP

Nov 7, 1956

13

Nov. 8, 1956

Cold Windy 30°  
18MPH.

Top Hyd NE Cor 12<sup>th</sup> Ave NW + 1<sup>st</sup> St NW

Top Hyd SE Cor Castle Ave + 1<sup>st</sup> St NW

Top Hyd 22<sup>nd</sup> Rt Sta 14+32 1<sup>st</sup> St No. St. Paul

Across from Ho # 891

Top Hyd NE Cor 7<sup>th</sup> St + 1<sup>st</sup> St No St. Paul

Top Hyd SE Cor 2<sup>nd</sup> St + Co Rd "C"

Top Hyd Lt of E By Ho # 232 Co Rd "C"

Top Hyd N.W. Cor Delaware + Co Rd "C"

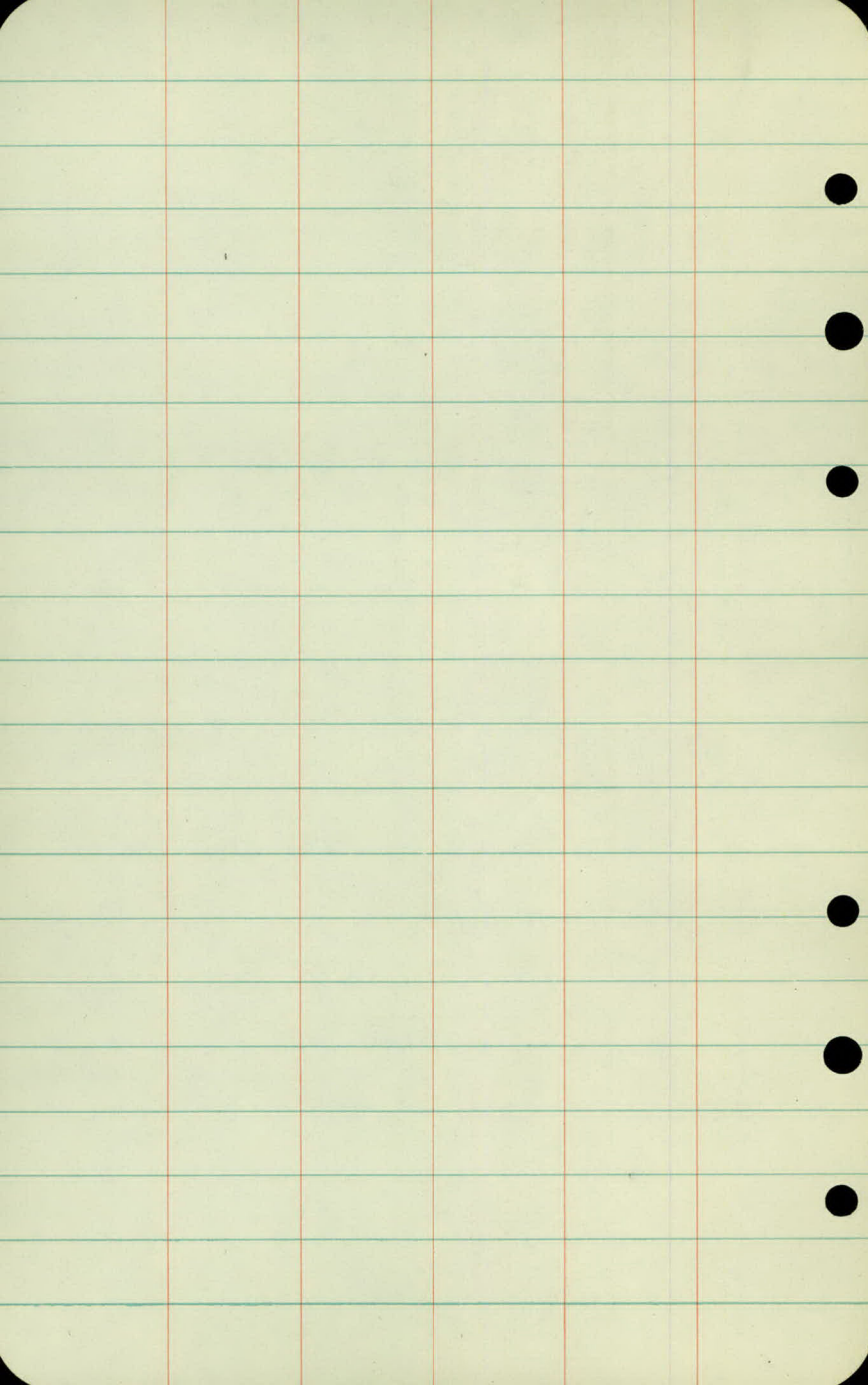
Top Hyd Lt Sta 160+80<sup>±</sup> By Ho # 345 Co Rd "C"

Top Hyd Lt Sta 155<sup>±</sup>

Top Hyd Lt. Sta 148+50<sup>±</sup>

Top Hyd NE Cor + Co Rd "C" Sta 144<sup>±</sup>

Top Mont N  $\frac{1}{4}$  Cor Sec 11-29-22





Nov 7, 1956

1A

4<sup>th</sup> St

South from Co Rd "C"

| Sta | +    | $\pi$  | - | Elev   |
|-----|------|--------|---|--------|
| BM  | 3.72 | 969.13 |   | 965.41 |

0 + 50

1

+ 50

2

+ 50

3

+ 50

4

+ 50

2 Nov 7, 1956

15

Top Hyd Lt Sta 155<sup>+</sup>

64.1  
5.0

64.1  
5.0

64.1  
5.0

63.9  
5.2

63.7  
5.4

63.7  
5.4

63.8  
5.5

63.8  
5.5

63.8  
5.5

Sta

969.13

5

+50

6

+50

7

+50

BM

2.64 966.49



63.6

5.5

63.5

5.6

63.2

5.9

63.1

6.0

M H

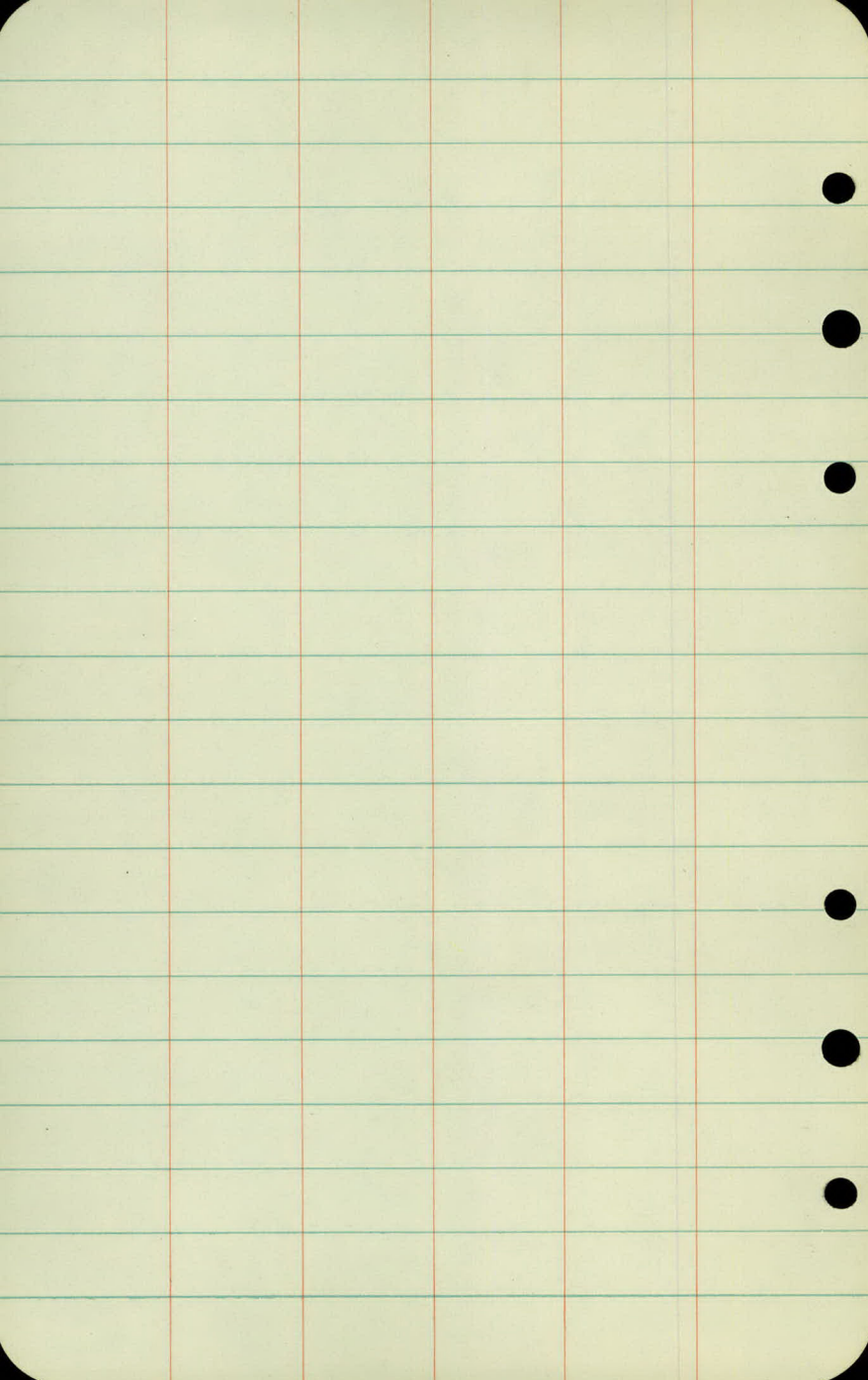
60.3

8.8

57.8

11.3

Top Hyd Lt By Ho # 345 Co Rd "C"



2"

0

V

V

16 1/2

0

V

0"

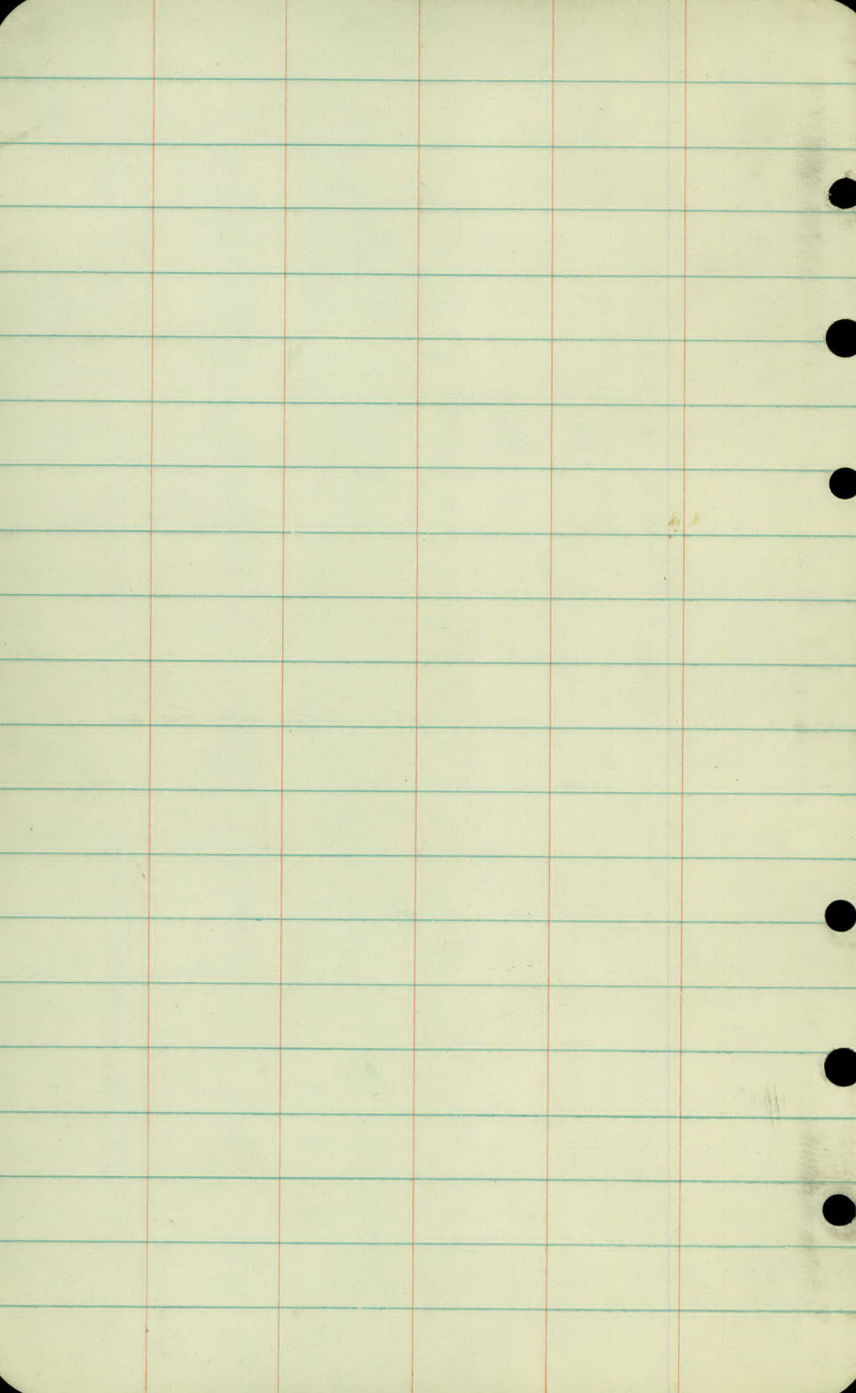
V

V

0

V

15 1/2





FK  $\pi$   
DSchacht  $\dagger$

May 5, 1975  
Clear 68°  
Best day so far this year <sup>1</sup>

Co. Rd. "C"

Southlawn to Van Dyke

# Lenker Type Rod

Sta

BM

913.10

BM

918.02 (918.07)

BM

913.95

TP

909.24

Top N. End Pipe

901.88

N. Edge Service Rd

903.8

9.12 892.76

901.88

10' N of Pipe

0.9 893.7

40' N of Pipe

0.3 893.0

Inv N. End of pipe

4.03 896.79

TP

6.83 902.41

909.24

8.50 896.34

2.43 904.84

3.39 899.73

3.00 899.3

2.9 899.2

3.2 899.5

BM

7.50 897.34

904.84

1.29 905.30

9.25 906.59

FK  
DS

May 5, 1975

2

Spike in P.P. NE Corner Van Dyke & C

E. End Front door sill Ho # 1861 "C"

Top Hyd N. W. Corner Van Dyke & C

60' North

Top S. End of Pipe

Inv S. End Culvert

Ditch 5' South

" 30' "

" 55' "

Door sill House S. Side E of Ditch

Lenker Type Rod  
+

905.80

BM 8.69 913.99

BM 7.84 913.14 (913.10)

MH 7.79 913.09

Top Pipe 901.88

894.2 903.2 C 9.0

904.2 C 10.0

TP 7.20 900.76 907.96

899.00  
1.76 4.08 904.84

899.00 2.19 2.95

1

1.24 2.00 C 3.00

2.24 C 4.00

BM 5.82 906.58 (906.59)

V. 2.1/8



Top Hyd N.W. Cor Van Dyke

Spike in P.P. NE Corner Van Dyke & C

Top MH at Pipe

West side

East side

Stake

Top S. End Conc door sill Ho E. of Ditch

