

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN

Survey

LARPENTEUR AVE.

From McMenemy To Edgerton

Road Acc't. No. _____

Date Filed 2-7-61

Dr. 9
File Bk. 28

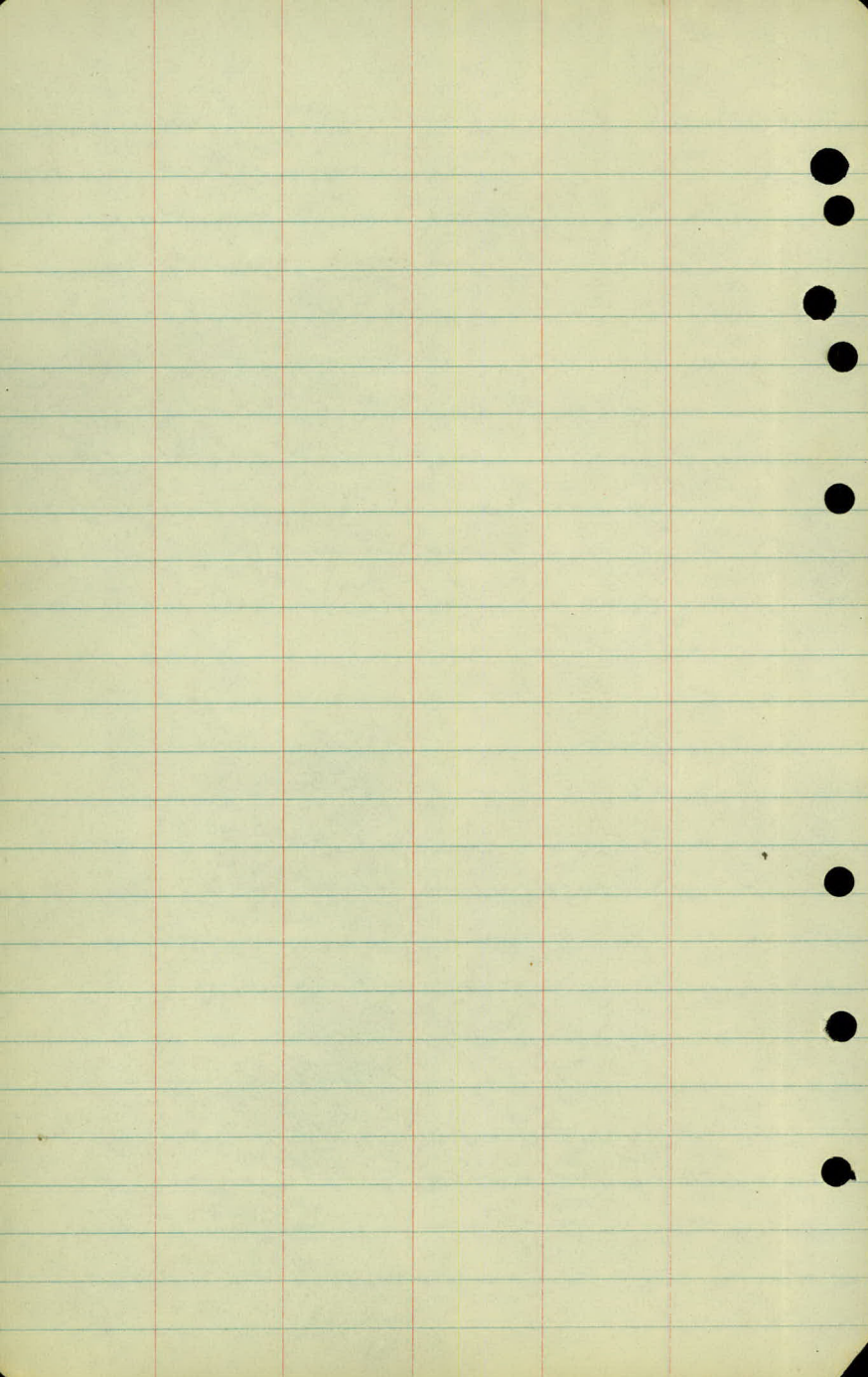
1
Larpenteur

McMenamy to Edgerton

Profile

11 pages

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	Blank
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17 August 1953

FK
AM
LO
MMo

2

Alignment

Sta Point ΔL ΔR .

26+12.40 $\pm$ Edgerton

15+50.5 P.O.T = 0+00 Desoto St (1936 survey)

13+06.20 P.O.T.

9+86.23 P.O.T.

0+00 $\pm$ Mc Menemy

E

E

Mont.

24" Oak

B

24" B.F.

B 33.01

21.66

East Spike

36" Oak

B

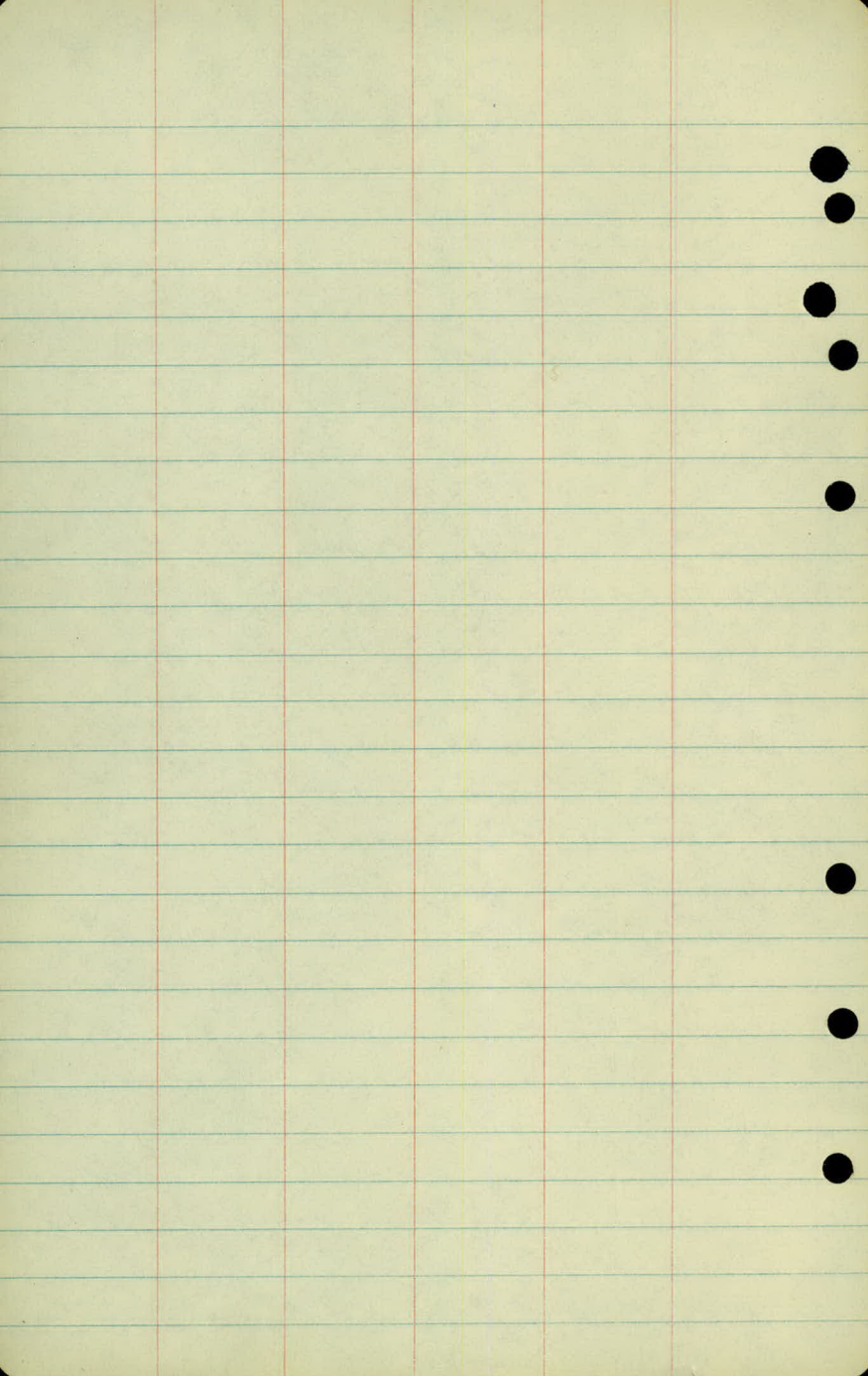
103.91

East Spike

12" Cott. B 2.3

E

Mont.



A

Profile

Sta + π - Elev

BM 5.27863.16

857.89

0+00 E McMenamy 858.6

+13

58.1

+50

4.4

58.8

+75

59.3

1

59.8

+43

+50

56.7

2

54.7

Lt.

Ht. 5

50'

2

30'

Top N.E. Cor. Bottom Step Ho 1625 McMenamy

1.5	2.7	4.6	6.5	8.1
100	50		50	100

2.0	5.1	6.9
50		50

3.5	4.4	3.6
-----	-----	-----

63.3			60.1
+0.1	3.1	3.9	3.1
75			3.3
Ho			Ho

62.7			
9.5	3.8	3.4	3.3
80			
Proposed Garage Floor			

59.7
3.5
Garage Floor
40

6.0	6.5	3.8
		50

50	8.5	3.8
----	-----	-----

Sta + π - Elev

863.16

53.8

2+50

55.9

3

57.0

+50

TP 13.53 874.64 2.05 861.11

58.2

4

59.3

+50

63.8

5

70.7

+50

TP 12.12 886.22 0.54 874.10

+50

21 Sept 1933

FM
AM
LC

Lt

50'

L

Rt 6

50'

3.4

9.4

5.4

1.7

7.3

11.0

0.5

6.2

9.7

11.4

16.4

22.0

9.9

15.3

21.8

5.8

10.8

16.0

3.9

11.9

Spike at sta 6+00

9.6
50

15.4
32

Sta	+	x	-	Elev
		886.22		

6				74.0
---	--	--	--	------

	+50			82.6
--	-----	--	--	------

	TP	12.83	898.77	0.28	885.94
--	----	-------	--------	------	--------

	+70			88.8
--	-----	--	--	------

7				93.1
---	--	--	--	------

	+50			898.5
--	-----	--	--	-------

8				
---	--	--	--	--

	+50			
--	-----	--	--	--

	TP	12.10	910.19	0.66	898.09
--	----	-------	--------	------	--------

8				904.2
---	--	--	--	-------

Lt

L

Rt

55	8.6	12.2	13.7	18.2
50	40		33	50

1.8	2.8	3.6	7.3	12.4
50	33		32	50

12.1	13.4	10.0		19.0
50	6			50

8.5	10.0	5.7		13.0
50	8			50

3.2	3.8	4.5	0.3	8.7
50	35	10		50

1.3	2.2	1.8	2.4
50	7	20	50

293.2

5.6
50

6.0

Sta + X - Elev

910.19

900.5

8450

BM 215 910.13 2.15 908.04 (907.9)

9

04.5

+50

04.2

10

899.5

BM 5.95 913.93 2.15 907.98

9

+50

10

TP 0.91 901.57 13.27 900.66

+50

887.6

Lt

L

Rt

7.2	7.8	11.4	11.6	9.7	3.6
50	37	20	5		10

4 in 15" Oak 50' Rt Sta 9+10

5.0	5.8	14.0	10.2	5.6		5.4
50	34	21	6			50

5.0	4.6	12.4	12.1	5.9
50	34	20	9	

14.1	13.0	12.4	16.9	10.6
50	3	23	8	

3.3	3.2
16	17

3.7	4.4
8	56

11.5	11.0	10.0
5	22	50

14.0	13.0	7.1
	16	50

Sta + K - Elev

901.57

TP 0.04 888.20 13.41 888.16

10+50

11 876.0

TP 1.07 877.05 12.22 875.98

+30

71.3

+45

62.0

+60

66.5

12 63.9

TP 1.18 865.03 13.20 863.85

12 (63.9)

+50

58.5

T.P. 4.85 863.29 6.59 858.44

Lt

L

Rt

9

7.6 5.5 2.5 2.7
50 36 23 7

13.7 13.1 10.6 11.0 12.2 13.3 12.8 8.1
50 29 18 6 6 31 50

0.4 4.4 3.4 3.7 5.8 8.0
50 35 24 11 50

15.1

✓
13.4 2.8 7.8 8.2 10.6 16.7 16.7 14.2 15.0
50 36 27 10 12 19 22 50

863.85

1.0 5.6 14.2 10.7 13.2
50 35 22 15

- (1.1)

9.8
50

✓

3.4 6.1 8.3 3.8 6.5 12.9 13.7
50 35 27 14 11 50 ✓

Sta + X - Elev
863.29

13 52.6

+50 53.3

14 56.4

+27 61.8

TP 11.14 87399 0.44 862.85

+50 64.5

+75 65.3

15 65.9

VOID

See pages 55 to 62

Lt

2

St.

9.6 10.6 4.3 10.7 11.7 13.8 ✓
50 30 16 2 50

12.0 11.2 5.0 10.0 12.9 13.7 ✓
50 32 14 5 50

8.6 9.2 3.7 3.6 6.9 9.2 9.2 ✓
50 32 19 6 7

1.5

6.8 7.9 9.9 9.5 9.8 8.3 7.49 ✓
50 34 26 40 50 57
Top West Rail

+2.0 0.5 7.9 8.7 8.6 8.0 7.23 7.32
50 35 22 25 28 35 42
W. Rail E. Rail

8.0 ✓
50

+6.8 2.2 8.0 8.1 6.99 7.03 7.9 8.2 6.0 ✓
50 28 14 11.5 18 26 45 50
W. Rail E. Rail

Sta + X - Elev

873.99

15+11

67.15

+14.45 $\neq$ Tracks

66.7

+17.7

67.19

BM

5.92 868.07 (868.15)

Lt

£

Rt

11

67.13

6.84

Top West
Rail

✓

7.3

✓

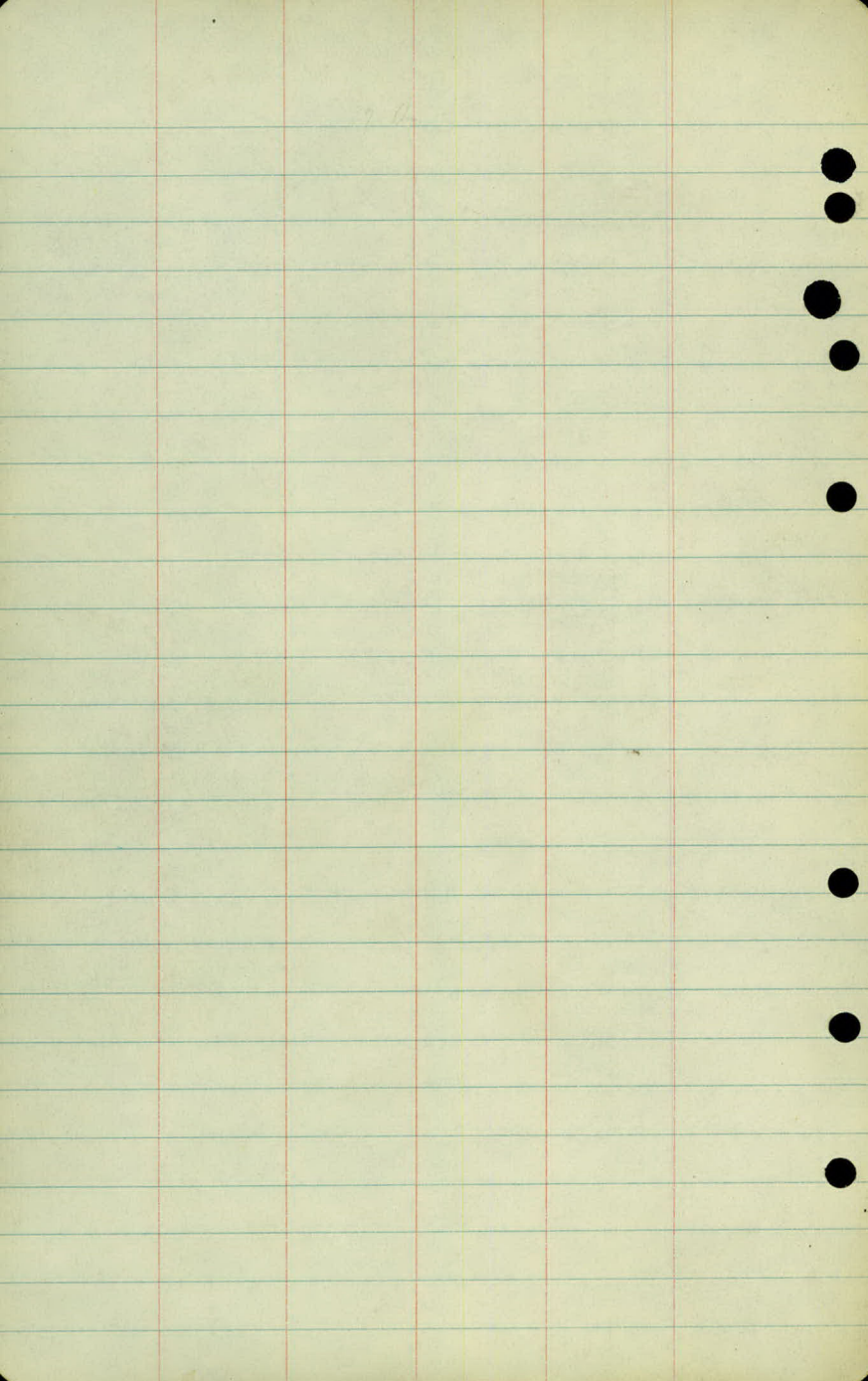
69.19

6.80

Top East
Rail

✓

N.W. Cor. S.W. Conc Footing cfr. Pier



X-Sections

in

Pages A-H

8.5

Sta + x - Elev

BM 5.27 863.16 857.89

58.8

0+50

4.4

+61 House

+63 House

59.8

3.4

+31

56.7

+50

6.5

54.7

8.5

2

53.8

+50

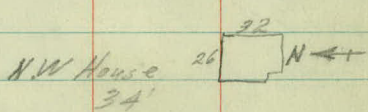
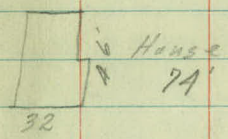
9.4

600 + 1153.
FK
AM.
LO
MMO

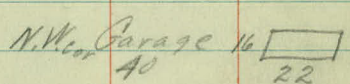
13
B

LT ♀ RT

Top NE Cor R.H. Step H. 1675 Mo Memory								
60.2	59.2	58.7	58.4	58.5	59.7	58.9	58.1	
+1.4	+0.9	-0.1	-0.4	-0.3	+0.9	+0.7	+0.7	✓
45	33	14	3		9	27	50	



59.6	58.3	57.4	57.4	57.6	60.5	59.4	60.0	60.0	✓
-0.2	-1.5	-2.4	-2.4	-2.2	+0.7	-0.4	+0.2	+0.2	
50	41	23	12	9	5	13	29	50	



57.4	56.9	56.4	56.4	55.2	55.2	60.2	59.9	53.7	53.7	✓
+0.7	+0.2	-0.3	-0.3	-1.5	-1.5	+3.5	+3.2	+3.0	+3.0	
50	38	22	9	5	2	5	20	40	50	

58.2	57.9	56.4	55.8	54.7	53.7	59.7	59.7	59.7	59.7	✓
+3.5	+3.2	+1.7	+1.1	+0.0	+1.0	+5.0	+5.0	+5.0	+5.0	
50	38	23	9	6	3	10	28		50	

59.5	57.6	57.0	54.2	52.8	52.6	58.3	56.7		✓
+5.7	+3.8	+3.2	+0.4	-1.0	-1.2	+4.5			
50	22	8	2	17	31	50			

Sta + π - Elev

863.16

55.9

7.3

+50

57.0

6.2

+72 $\angle$ St. Left 5.5 57.7

TP 13.53 87464 2.05 861.11

16.4 58.2

59.3

+50

15.3

63.8

10.8

70.7

+50

3.9

11

2

RT

60.9

54.8

53.3

52.7

150	140	124	0.0	-11	-26	-32	X
50	30	7	2	20	32	50	

63.0

62.0

60.7

60.3

58.3

55.7

54.6

53.6

160	150	13.7	13.3	11.3	-1.3	2.4	3.4	X
50	37	18	8	4	12	34	50	

63.4

61.8

61.0

58.2

+5.7	+4.1	+3.3	+0.5
50	25	8	3

64.7

64.6

66.5

+7.0

+8.8

75

100

63.4

62.5

61.1

59.2

152	143	12.9	1.0	-1.8	-2.0	-1.1	X
50	34	10	5	8	24	50	

64.7

64.3

63.3

61.9

57.9

56.4

55.2

53.8

+5.4	+5.0	+4.0	+2.6	-1.4	-3.3	1.4	X
50	37	18	6	6	25	50	

69.3

66.5

66.5

66.1

64.6

62.7

60.5

59.5

15.5	12.7	2.7	2.3	10.8	-1.1	-3.3	-4.3	X
50	33	25	7	3	8	26	50	

75.8

70.8

70.7

70.8

68.9

66.5

62.6

+5.1	+0.1	0.0	+0.1	-1.8	-4.2	-8.1	X
45	33	27	6	7	25	50	

+76.8

+6.1

+10.1

50

75

Sta + A - Elev

874.64

TP 12.12 886.22 0.54 874.10
6 12.2^{14.0}

82.6

+50

3.6

TP 12.83 898.79 0.28 885.94

88.8

+70

10.0

93.1

7

5.7

4.0

D¹⁵

Lt

L

Rt

76.0	75.4	74.4	73.0	72.1	67.3
+2.0	+1.4	+0.4	-1.0	-1.9	6.7
21	6	3	21	33	50

✓

77.7	79.7	82.7
+3.7	+5.7	8.7
40	44	75

X

83.8	82.3	82.1	82.7	81.1	79.6	78.6	75.5
+1.2	-0.3	-0.5	+0.1	-1.5	-3.0	-4.0	-7.1
41	30	9	7	11	21	31	38

+

83.6	84.5
+1.0	+1.9
50	75

74.3	73.1
-11.3	-9.5
73	49

+

85.6	84.8	85.1	85.6	87.1	84.1	80.6	76.6
-3.2	-4.0	-3.7	-3.2	-1.7	-4.7	-8.2	-12.2
33	14	8	4	16	32	47	60

X

87.0	87.6
-1.8	-1.2
50	75

90.3	88.9	89.1	93.5	91.3	89.4	83.9	80.0
-2.8	-4.2	-4.0	+0.4	-1.8	-3.7	-9.2	13.1
44	26	10	4	21	38	60	75

91.5	91.5
-1.6	-1.6
59	75

X

Sta + x - Elev

898.77

98.5

7+50

0.3

898.5

55

1.2

+81

TP

12.10

910.19

0.68

898.09

02.0

+81

2 St. Left

8.2

902.0

04.2

8

6.0

00.5

+50

9.7

907.98

BM

2.15

910.13

2.15

908.04

907.89

7.5

E 16

Lt

L

RH

93.9	94.1	93.6	98.3	95.0	91.6	83.7
-46	-4.4	-4.9	-0.2	-3.5	-6.9	-14.8
42	26	11	2	25	45	7.3

96.4	97.5	99.3
-2.1	-1.0	+0.8
56	75	100

X

98.5	97.1	96.3	95.7	91.7	92.0	91.8	96.8	92.0	85.0
-3.5	-4.9	-5.7	-6.3	-4.3	0.0	-0.2	-5.2	-10.0	-17.0
75	50	25	12	6	2	11	22	42	64
99.5	99.3	99.8							
-2.5	-1.7	-2.2							
100	150	200							

X

99.1	97.6	96.7	97.1	93.7	97.7	92.7	86.7
-5.1	-6.6	-7.5	-7.1	-0.5	-6.5	11.5	-17.5
76	55	23	7	11	23	41	60

X

99.7
-4.5
100

93.0	92.0	98.5	99.0	96.5	99.3	93.0	87.0
+2.5	+1.5	-2.0	-1.5	+6.0	-1.2	-2.5	-13.5
63	36	19	3	8	25	49	7.6

94.0
+3.5
100

X

Spt in 15" Oct 50' RH Sta 9+10

Sta	+	π	-	Elev
9		910.13	04.5 5.6	

BM	4.00	911.98	2.15	907.98	907.98
----	------	--------	------	--------	--------

+50

04.3

10

99.6

+50

87.2

TP	1.51	900.04	13.45	898.53
----	------	--------	-------	--------

+50

87.2

TP	0.42	887.54	12.92	887.12
----	------	--------	-------	--------

F¹⁷

4

RT

0.0	+ 1.0
60	100
4.5	5.5

93.5	✓ 98.2
-11.0	-6.3
100	78

18	14.5	14.5	13.6	7.7	1.8	14	2.6	5.3	10.5
20	11	9	9	9	30	52	73	100	
97.5	97.5	98.4	94.3	10.2	10.6	9.4	06.7	01.5	

0.56	1.50	0.313	97.5
6.4	6.9	8.7	14.5
33	50	69	100

18.143	18.2	19.4	18.1	12.4	9.7	8.4	7.3
97.7	93.8	92.6	93.6	99.6	92.3	93.6	94.7
33	23	18	9		4	18	11

15.4	18.6	23.1
50	75	100
76.6	93.4	88.9

0.3	0.36	0.47
7	8.4	7.3
18	41	
0.3	0.17	✓ 0.2
10.7	10.3	8.3
100	94	66

- 24.8

19.6	17.4	17.5	20.6
32	55	77	100

57.2	88.6	88.0	89.2	
12.8	11.4	12.0	10.8	4
6	10	20		

Sta + π - Elev
10+50 887.54 (87.2)

11 75.9

+30

(71.1)

+45

(61.6)

+60

(66.4)

12

(63.8)

TP 0.74 874.78 13.50 87404

$\frac{85.0}{25} \frac{2.1}{17} \frac{84.4}{12} \frac{86.9}{3}$
 $\frac{85.4}{17} \frac{84.4}{12} \frac{86.9}{3}$

- (0.3)

RA

$\frac{81.1}{47} \frac{78.9}{80} \frac{78.7}{100}$
 $\frac{81.1}{47} \frac{78.9}{80} \frac{78.7}{100}$

X

$\frac{79.6}{100} \frac{78.3}{80} \frac{76.6}{67} \frac{73.5}{49} \frac{73.4}{41} \frac{75.9}{116} \frac{74.9}{12.6} \frac{75.8}{117} \frac{76.6}{10.9}$
 $\frac{79.6}{100} \frac{78.3}{80} \frac{76.6}{67} \frac{73.5}{49} \frac{73.4}{41} \frac{75.9}{116} \frac{74.9}{12.6} \frac{75.8}{117} \frac{76.6}{10.9}$

$\frac{77.0}{10.5} \frac{77.1}{10.4}$
 $\frac{77.0}{10.5} \frac{77.1}{10.4}$

$\frac{79.3}{82} \frac{81.7}{5.8} \frac{83.8}{3.7} \frac{81.7}{5.8}$
 $\frac{79.3}{82} \frac{81.7}{5.8} \frac{83.8}{3.7} \frac{81.7}{5.8}$

$\frac{81.2}{3.3} \frac{84.7}{2.8} \frac{80.3}{7.2} \frac{74.4}{13.1} \frac{72.9}{14.6}$
 $\frac{81.2}{3.3} \frac{84.7}{2.8} \frac{80.3}{7.2} \frac{74.4}{13.1} \frac{72.9}{14.6}$

- (16.4)

X

$\frac{82.0}{10.5} \frac{85.5}{2.0}$
 $\frac{82.0}{10.5} \frac{85.5}{2.0}$

- (25.9)

X

$\frac{89.7}{12.2} \frac{88.3}{10.8} \frac{83.9}{9.6}$
 $\frac{89.7}{12.2} \frac{88.3}{10.8} \frac{83.9}{9.6}$

- (21.1)

X

$\frac{87.2}{0.3} \frac{83.2}{4.3}$
 $\frac{87.2}{0.3} \frac{83.2}{4.3}$

- (23.7)

X

Sta	+	π	-	Elev
		874.78		
11+30				71.1

+45	Washout			61.6
-----	---------	--	--	------

+60				66.4
-----	--	--	--	------

12	2 checks per notes			63.8
----	--------------------	--	--	------

19

L+			2		RT		
71.0	68.9	73.3	87.1	71.0	70.5	69.2	68.3
3.8	5.9	1.5	3.7	3.8	4.3	5.6	6.5
28	18	11		8	18	30	54

X	61.3	65.7
	13.5	9.1
	100	76

73.7	70.7	70.2	68.1	61.6	63.2	65.6	65.6	64.0	61.6
1.1	4.1	4.6	6.7	13.2	11.6	9.2	9.2	10.8	13.2
35	28	17	10		15	17	36	55	75

→ 1. 73.7
42

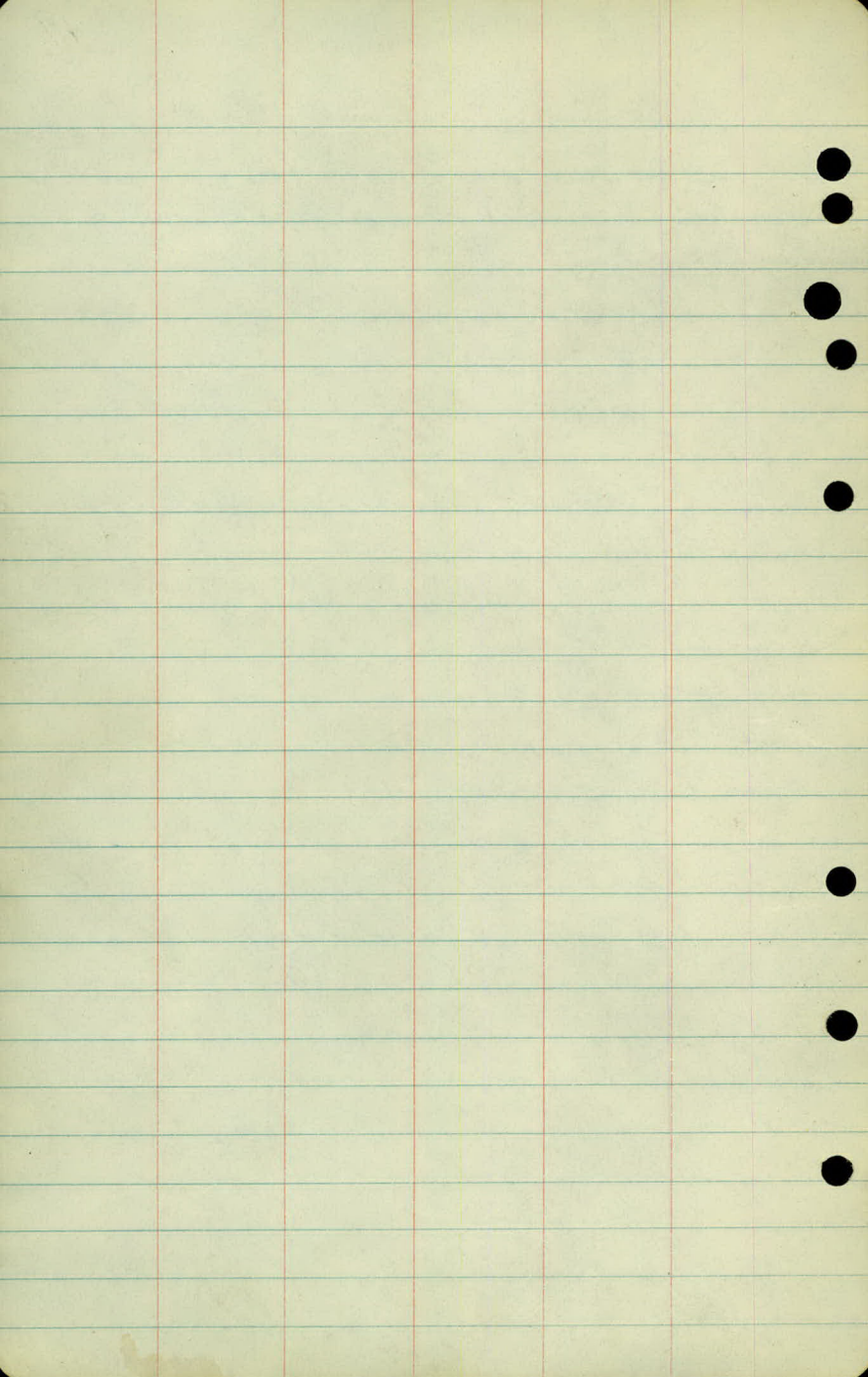
→ 61.6
13.2
6

74.8	73.9	68.0	69.6	68.5	66.4
0.0	0.9	6.8	5.2	6.3	8.4
40	35	24	18	8	

X

86.3	78	59.7	56.4
14.0	15.1	18.4	
	15	32	

✓



120
1915
A.M.
L.C.
M.M.

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

STADIA

LARPEUR - AVE

East of McMenemy st.

at sta 8+00

OBJECT

AZ.

STADIA

$\bar{A}$ at Sta. 8+00 H.I. = 4.95

$0^{\circ}00' = \text{North}$

To Sta. 0+00 $270^{\circ}00'$ = Mont. & Mc W. enemy St.

\$ Rd.

$354^{\circ}20'$

" "

$356^{\circ}30'$

" "

$356^{\circ}50'$

" "

$354^{\circ}20'$

" "

$349^{\circ}45'$

" "

$343^{\circ}20'$

Dist

\$ Rd. to House

$271^{\circ}30'$ 208

" "

$261^{\circ}15'$ 175

" "

$258^{\circ}30'$ 170

" "

$241^{\circ}20'$ 149

" "

$227^{\circ}-$ 136

" "

$209^{\circ}50'$ 124

" "

$189^{\circ}20'$ 115

S. W. Cor. Ho.

$164^{\circ}30'$ 168

N. W. Cor. Ho

$159^{\circ}50'$ 157

N. E. Cor. Ho

$149^{\circ}10'$ 216

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	-------------	------------	-----	-------	-------

H.I. = 909.2

904.2

stadia

200			9.3		99.9
285			13.7		95.5
365			15.4		93.8
423			14.1		95.1
472			13.2		96.0
496			12.1		97.1
223	-15°	55.8	9.0	66.8	842.4
188	-15°	47.0	12.2	59.2	30.0
182	-15°	45.5	13.2	58.7	50.5
160	-15°	40.0	17.8	57.8	51.4
154	-20°	49.5	14.1	63.6	45.6
140	-20°	46.0	16.5	61.5	47.7
130	-20°	41.8	15.5	67.3	41.9
190	-20°	61.1	5.9	67.0	42.2
178	-20°	57.2	6.7	63.9	45.3
232	-15°	58.0	2.7	60.7	48.5

OBJECT

AZ.

STADIA

950.22

Lake

943.00

10/10/53

~~House Locations~~

Topography

4
 +84 Edge Rd
 24
 +64 End R
 67
 +177 R.Tic Gar
 Ent

Road
 33-13

+155 PP
 54

+122 Beg. R.
 34

Road
 33-12

3

+174 S.C. Gar
 67'

+35.5 R.Tic
 Ho
 +30 R.Tic Gar

2

Road
 32-11

+183 PP
 22

1
 +100 2 10' Conc Ent Road
 47 32-10
Road
 +65 31-11
 +63 2 Ent
 2

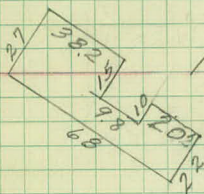
+25 T.P. +26 End R. +29 End R +25 Arch Lt
 73 33 5 25
 0 +09 E. Rad +09 Edge ET +09 E. Rad
 42 4 21

-12 Edge ET
 4

Platted

Nov 9, 1955

23



9

Path
16

 $+22 \frac{PP}{50}$
 $+106 \frac{14''0}{65}$
Path
24

 3
 166 W. Edge E. Edge
 ST 17 + 95 ST

 $+150 \frac{16''0}{5}$
 $+150 \frac{14''0}{38}$

7

Trail
28-17

 $+74 \frac{PP}{53} +74 \frac{Ent}{85}$
 $+130 \frac{24''0}{5}$

6

Trail
25-13

 $+84 \frac{Ent}{2}$

5

Road
31-11

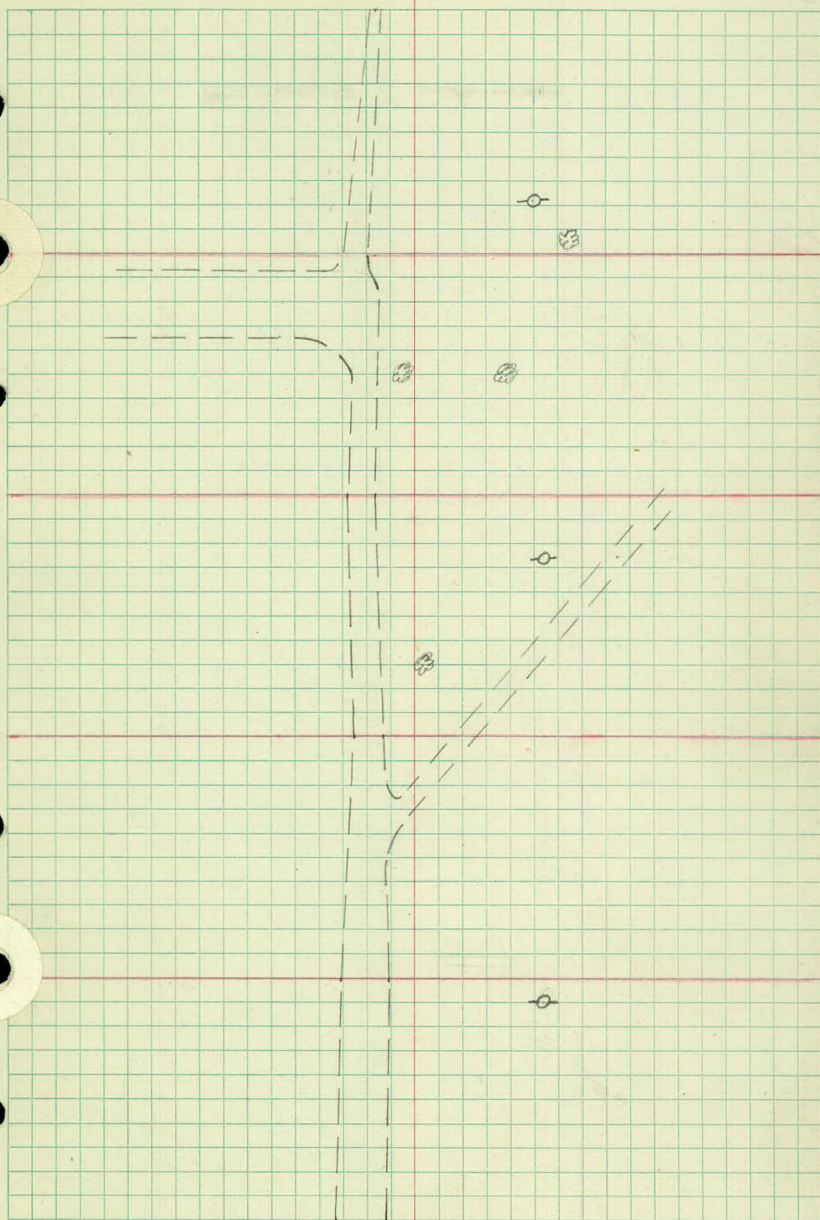
 $+90 \frac{PP}{53}$

4

Plotted

Nov 9, 1955

24



2

14

$$+90 \frac{4'' \text{ El.}}{40}$$

13

$$+00 \frac{N \text{ End } 15' \text{ SCP}}{32}$$

$$+02 \frac{SE 15' \times 34' \text{ SCP}}{2}$$

$$+41 \frac{26''}{49}$$

$$+87 \frac{28'' \text{ BE}}{27}$$

$$+07 \frac{26''}{35}$$

$$+16 \frac{14''}{52}$$

12

$$+88 \frac{240}{60}$$

$$+74 \frac{18''}{45}$$

$$+70 \frac{16''}{42}$$

$$+06 \frac{12'' \text{ W.}}{27}$$

$$+64 \frac{18''}{79}$$

11

$$+99 \frac{30''}{35}$$

10

Path
13

$$+84 \frac{12''}{2}$$

$$+59 \frac{12'' \text{ BE}}{6}$$

$$+33 \frac{14'' \text{ C. of}}{30}$$

$$+09 \frac{14''}{49}$$

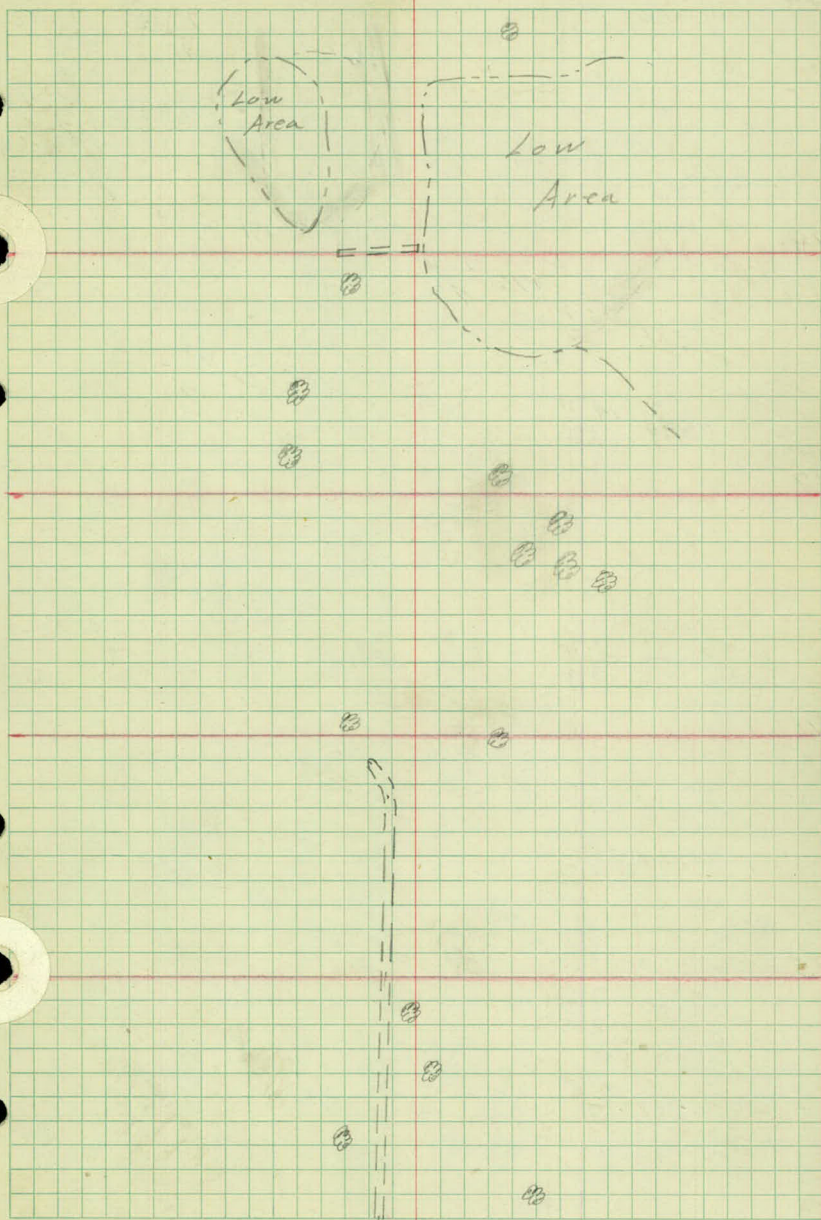
9

Path
16

Platted

Nov 9, 1955

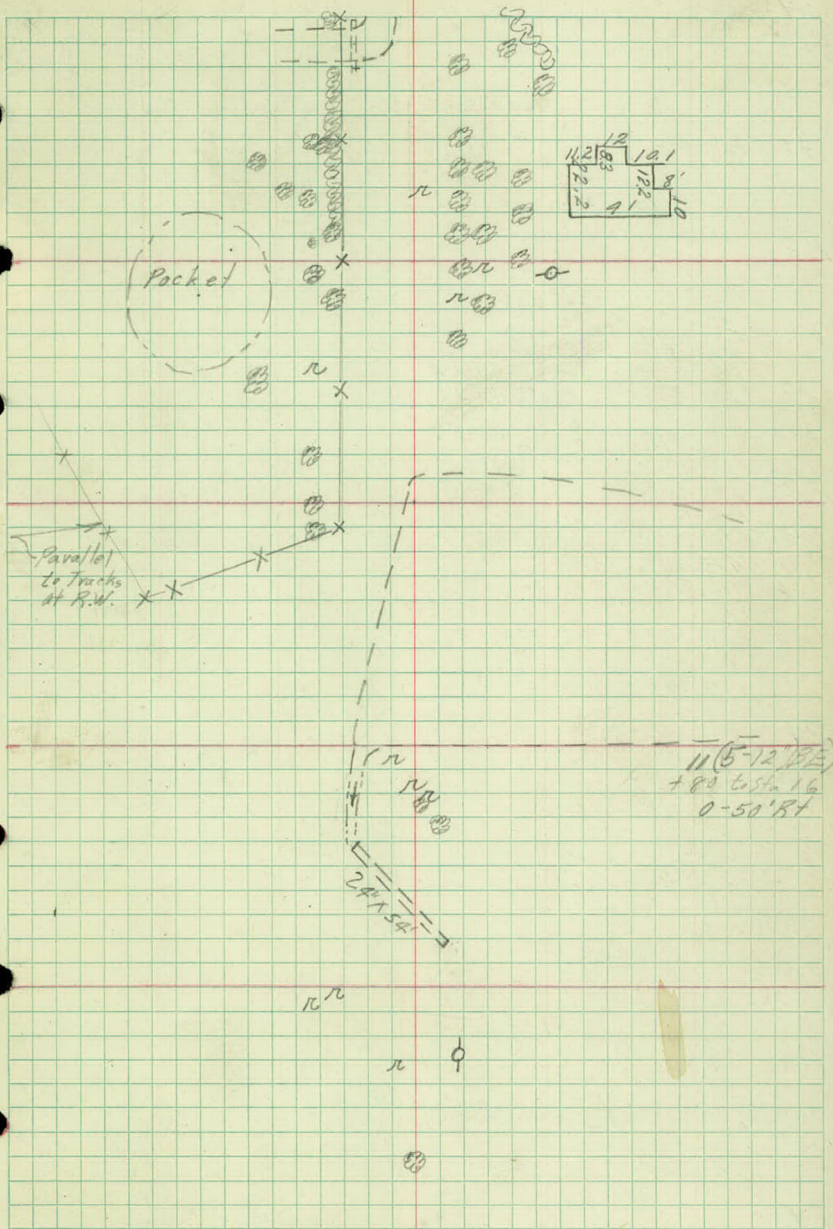
25



	Fe 30	Road 20-7				
19						
+88	25	Elm.	+80	14"A	+88	12"BE
+48	12"E		+38	12"A	+52	14"A
+41	10A		+28	12"E	+34	12"A
+10	32		+25	18	+18	66
18			+01	14"A	+11	10"A
+85	90		+96	12"W	+97	18
+81	26"O		+81	14"A	+82	17
+150	24"W		+56	14"W	+68	17
+20	14"W		+10	12"E		
17			+100	R.Tic Fe		
+98	12"W		+90	Fe Cor		
+188	10"W					
16						
+64			+83	1	+79	10
+59	24		+67	10	+76	3
15			+92	14	+96	36
+68	9		+28	14"BE		
14						

Nov 2, 1955

26



24

Road
23-9

+89 PP
28.6

+17 End R.
24

23

+32 Road
Cesspool Cleanout ✓
42.6

+69 PP +77 Beg St. +95 B. Red
29.5 30 52

+50 Stp +103 S.W.C.Ho +164 12"E +20.71 Iron
33 60 33 0.20

+108 12"E +118 3' Walk +129 14"W
34 28 34

22

Road
24-8.5

+163 2" Flys Walk +68 8"A +175 12" X 20' X Drain
30 41 26.6

+136 14"E +146 Stp +157 20"E ✓
36 43 36

+123 PP +133 N.W.C. Bar +132 By Litch H
31 49 30

+121 GP +105 \$ 25' Ent
1 11

21

Road
10

+146 PP +122 Stp
31 2

20

+102 S.W.C. Cont Road
111 25-12

+85 SE 15" X 8" CM +95 6"E
10 35

+80 NE 15" X 8" CM +68 Ent 12" X 16" CM
27 27.5

+155 On Hedge +158 Fe Cor +171 Ent Lt
32 30.5 2

+04 18"W +128 PP +20 16"E +123 Ent/Lt on Hedge
54 32 10 13

+19 +100 S.W.C. Ho +104 R. Ho +124 \$ Ent +102 16"W
74 26

Nov. 10, 1955

27

+92 Enb. Kedge 29
 +89 14 E 34 15"
 +86 8 A 46

27 25

Change	12	32
	22	22

+22 Edge Conc

+101 End R
17

26

+99 $\frac{E. Rad}{38}$

+94 $\frac{Hxd}{36}$

+90 $\frac{PP}{34}$

+84 $\frac{Beg R}{21}$

+83 $\frac{Beg R}{A}$

+90 $\frac{Archt}{20}$

+92 $\frac{TP}{23}$

+78 $\frac{Tw. L2' Blk}{48}$

+108 $\frac{PP}{27}$

+79 $\frac{STP}{19}$

+83 $\frac{\pm 6' Walk}{30}$

+77 $\frac{Trips}{A3}$

25

Road
23-9

Face 4x4 Conc Water Shutoff ✓

+30 32.9

+39 $\frac{PP}{28}$

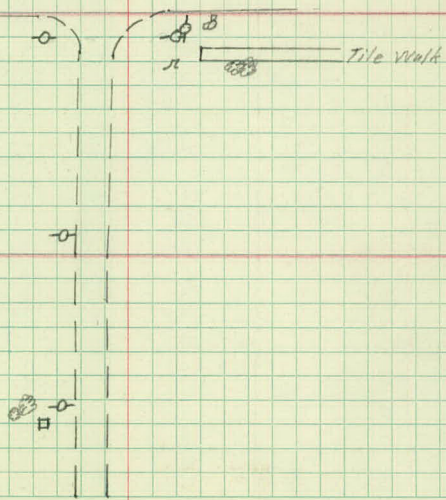
+37 $\frac{6'E}{43}$

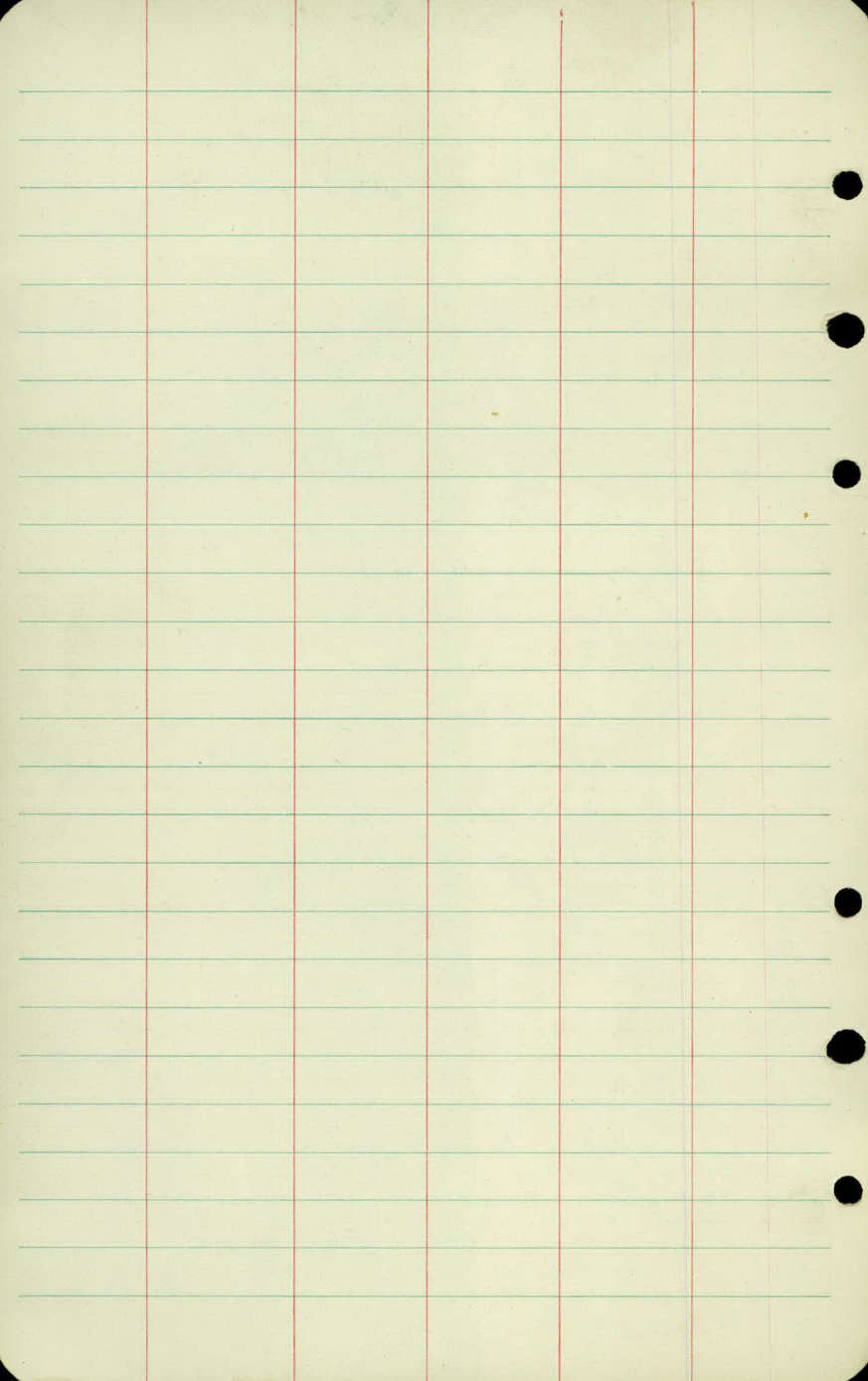
+36 $\frac{Lilac}{18}$

24

Nov 10, 1955

28





Nov 4, 1955

29

House Locations

Stadia

HI = 906.4

Object	Az	Stadia
--------	----	--------

At P.Q.T. Sta 9+86.23

to Mont Larp & Edgerton 90°00'

Sta 10

Sta 9

S Cor Ho	47°45'	527
----------	--------	-----

W " "	44°53'	525
-------	--------	-----

E Ent	56°20'	362	Ent Lt
-------	--------	-----	--------

E Desoto St	59°40'	585'
-------------	--------	------

E " "	69°25'	558'
-------	--------	------

SE Cor Ho	61°29'	700
-----------	--------	-----

SW " "	60°40'	680
--------	--------	-----

New?

SW Cor Ho	118°54'	820
-----------	---------	-----

NW Cor Ho	117°24'	808
-----------	---------	-----

E Desoto St Sol Bridge	105°30'	625
------------------------	---------	-----

E " "	120°30'	755
-------	---------	-----

E " "	122°50'	805
-------	---------	-----

Nov 4 1955 30

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

H.I. =

6.9

1.9

899.5
899.6
904.4

2-S-B

SW = 26'

SE = 21'

+1' 40'

40

585
92
677

2-S-F

E 24 W

N 32 S

6.0

6.0

2-S-S

E 27 W

N 24 S

0.8

1.4

10.9

3.0

OBJECT

AZ.

STADIA

At sta 6

to 0400

270°-

Sta 5

270°-

E Ent

270°- 17

" "

146°20' 50

" "

139°45' 106

" "

133°25' 157

" "

128°15' 206

" "

124°40' 273

At sta 9200

To 00° 270°00

To sta

N.E. Cor 140.

132°15' 297

N.W. Cor.

135°19' 232

Corr.
Dist.

Vert. Angle

Nov. 22, 1955

31

Rod.

H.I. = 879.2

H.I. 5.2

874.0

15.8

63.4

6.1

73.1

6.3

72.9

8.1

71.1

9.3

69.9

9.7

69.5

+ 1°28'

+7.0

16.0

-9.0

70.2

H.I. = 98.7

11-25-55

893.1

H.I. = 5.6

-3°31'

-18.1

2.0

-20.1

78.7

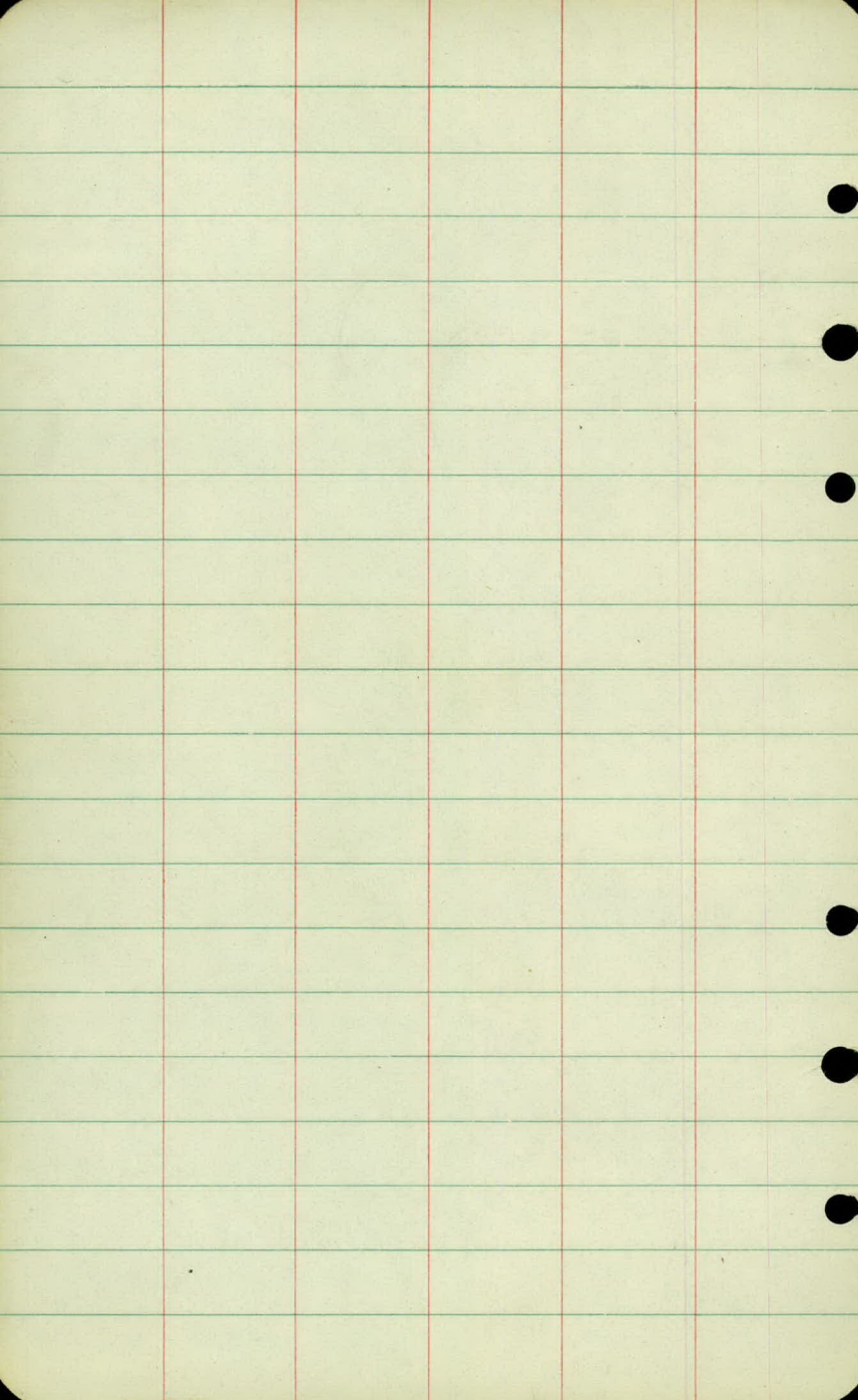
-4°07'

-16.6

10.0

126.6

72.1



A.M.
L.C.
W.I.

11/25

34

AD. X SECTIONS

LARPEUR - AVE - McMENNEY - To EDCERTON

STA	+	π	-	ELEV
-----	---	-------	---	------

B.M.	7.13	865.02		857.89
------	------	--------	--	--------

1 + 00

2 + 18

2 + 45

2 + 75

B.M.	7.13	857.89		
------	------	--------	--	--

LT

2

PT

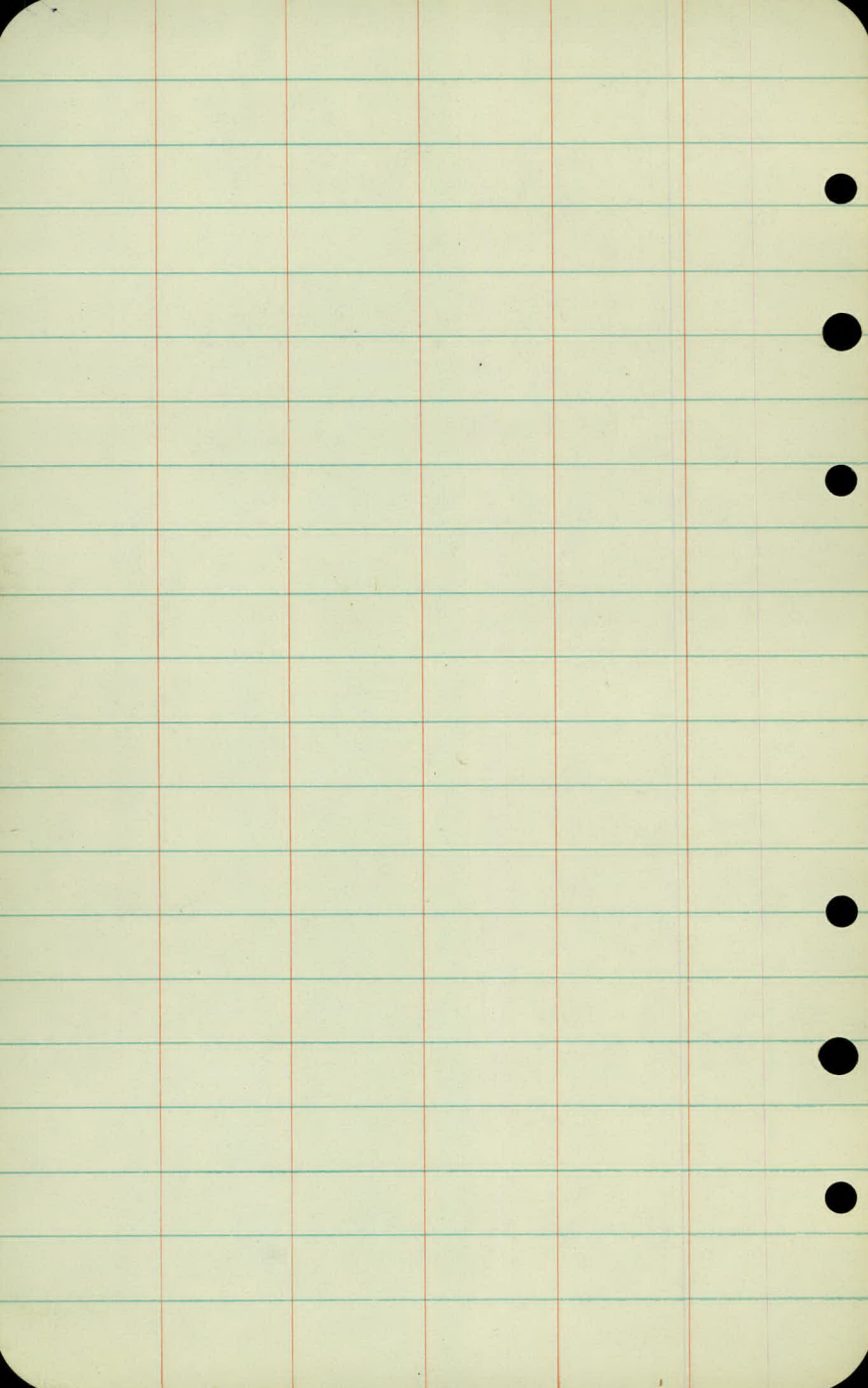
35

N.E. COR. BOT. STEP HO. ¹⁴ 1675 McMEVEMY

59.28	62.9	62.75					
ENT. 40	6A						
5.74 21	2.27	56.0	55.0	54.6	54.8	58.6	59.4
5.59.2	5.51.7	8.56.4	10.0	10.4	10.2	6.4	5.6
5.52.6	5.51.7	8.6 9.0	6		4	11	24
60 43.33	24	15 9					50
60.4							
4.6							
28.6							

64.8	64.0	59.8	58.4	58.6	57.7	57.6	55.0	54.7	53.4	52.5	51.9	51.6
0.2	1.0	5.2	6.6	4.7	2.7	4.1	10.0	10.3	11.6	12.5	13.1	13.4
68	59	41	33	23	14	8	3		15	35	57	78

N.E.-COR BOT-STEP HO² 1675 McMENEMY



Larperneur
Mc Menemy to Edgerton

X-Sections
sta 12 to Edgerton

pages I-T

Sta	+	π	-	Elev.
BM	0.12	868.27		868.15

TP	10.26	874.27	4.26	864.01
----	-------	--------	------	--------

11 + 60

12 254

12

TP	2.72	863.35	13.49	860.63
----	------	--------	-------	--------

12

+ 50

FR
AM
WJ

Nov 7, 1955

357

LT

RT

N.W. Cor. SW. Conc Footing Ctr. Rev

66.6	61.2	60.6	62.8	62.2
7.7	13.1	13.7	11.5	12.1
	10	20	22	45

58.4	58.9	60.6
15.9	15.4	13.7
100	96	73

62.8	66.1	66.0	64.0	61.0
11.5	8.2	8.3	10.3	13.3
20	16	8		10

62.8	69.9	70.5	71.4	73.1
11.5	4.4	3.8	2.9	1.2
24	32	34	41	48

60.4	58.2	55.4	54.4	51.4
30	5.2	8.0	9.0	12.0
12	28	41	66	100

57.6	56.8	61.3	61.0	56.6	54.2	51.2	51.4	50.4	49.6
5.8	6.6	2.1	2.4	6.8	9.2	12.2	12.0	13.0	13.8
31	28	18	11		4	16	40	78	100

Sta. + π - Elev.

863.35

12+50

13

+02

+02

+50

FK
AM
LC
WT

£ Nov. 8, 1955

38

14

RT

65.5
121 0.9 3.3
100 63 45



51.11 52.2 59.0 58.9 52.6 51.6 50.8 49.7 49.2 49.2
12.24 11.2 4.4 4.5 10.8 11.8 12.6 13.7 14.2 14.2
FL15"SCP 32 20 13 2 25 41 72 100
32

53.6 54.0 59.2
→ 9.8 9.4 1.2
48 76 100



49.34
14.01
FL15"SCP
3

51.4 52.2 58.4 58.3 53.4 50.4 49.7 50.3
12.0 11.2 50. 51 10.0 13.0 13.7 13.1
56 31 19 11 5 21 55

52.4 54.3
→ 11.0 9.1
80 100

50.3 50.7
13.1 12.7
100 81



Sta + π - Elev

863.35

14

✓

TP 7.80 870.71 0.44 862.91

+ 50

✓

15

✓

+17

P

Nov 8, 1955

39

14

RT

55.7	54.9	59.6	59.9	56.3	54.3	54.8	54.0	56.6	62.1
77	85	38	35	71	91	86	94	68	13
56	32	21	7		7	25	47	75	97

54.2 56.7
9.2 6.7
80 100

✓

64.2	63.3	63.6	63.5	64.5	64.8	64.3	65.7	66.55
6.5	74	71	72	6.2	5.9	6.4	5.0	4.16
60	35	28	11		10	42	51	61
								Rail

✓

66.5 67.1
4.2 3.6
80 100

68.8	65.9	65.9	66.2	67.08	67.01	66.3
1.9	4.8	4.8	4.5	3.63	3.70	4.4
22	12		4	11	19	26
				Rail	Rail	

70.2 66.1 65.5
0.5 4.6 5.2
55 48 34

65.28

5.43

FL 24" SC P

Sta + π - Elev

870.71

15+25

BM 12.48 880.63 2.56 868.15

+ 62

+ 67

✓

16

Nov 8, 1955

400

47

BT

70.7	67.2	67.41	67.37	66.9	68.4	69.7
0.0	3.5	3.20	3.34	3.8	2.3	1.0
25	22	13	6		7	18

Rev.

N.W. Cor S.W. Conc Footing Ch Pier

66.02
1461
25
FL 24" SCP

66.8	66.6	70.1	70.7	79.0
13.8	14.0	10.5	9.9	1.6
29	25	20	13	

	68.0	67.83	67.89	67.4	72.0	75.2	80.1
→ 12.6	12.80	12.74	13.2	86	54	0.5	
34	41.5	48.5	58	67	73	84	
	Bail						

75.0	70.2	70.4	71.9	72.1	71.5	71.0	70.6	70.4
56	10.4	10.2	8.7	8.5	9.1	9.6	10.0	10.2
35	24	10	5		34	52	77	100

75.2	72.1	66.7	67.9	68.40	68.44	67.7	67.0
5.4	8.5	13.9	12.7	12.23	12.19	12.9	13.6
48	55	67	70	74.5	80.5	88	89
						71.7	
						89	
						100	

Sta	+	π	-	Elev.
		880.63		

16+50

17

+50

TP	13.65	889.91	4.37	876.26
----	-------	--------	------	--------

18

+50

TP	8.05	894.95	3.01	886.90
----	------	--------	------	--------

2 Nov. 8, 1955

41N

Lt.

Rt.

79.6	75.4	72.0	71.5	70.8	70.3	70.3	70.5	70.6
1.0	5.2	8.6	9.1	9.8	10.3	10.3	10.1	10.0
75	58	33	13		18	31	60	80

76.2 73.5
4.4 7.1
88 100

70.7 ✓
9.9
100

78.1	76.7	75.8	73.9	73.4	71.7	71.1	70.9	71.2	71.9	74.0
2.5	3.9	4.8	6.7	7.2	8.9	9.5	9.7	9.4	8.7	6.6
100	73	52	30	12		19	30	57	80	100

76.7	78.1	77.8	76.0	75.9	77.2	78.4	79.1	80.6	82.8
3.9	2.5	2.8	4.6	4.7	3.4	2.2	1.5	0.0	+2.2
85	55	34	28	9		17	34	50	75

Back

76.2	77.8	78.6	78.2	82.3	83.1	84.9	87.7	89.5
13.7	12.1	11.3	11.7	7.6	6.8	5.0	2.2	0.4
68	49	30	9		10	14	30	42

82.3	82.0	80.6	81.0	86.6	87.7	89.4
7.6	7.9	9.3	8.9	3.3	2.2	0.5
53	30	28	9		3	20

Sta + π - Elev.

894.95

18+50

19

✓

+50

✓

20

Nov 8, 1955

42

14

BT

91.5	93.7	97.7
35	13	12.7
33	50	40

86.0	86.5	86.6	86.1	86.0	87.8	88.9	90.2	90.2	89.6
90	85	84	89	90	72	61	48	48	54
23	21	8	7	3		2	14	34	50

83.8	83.8	86.3	92.9	92.9	93.9
11.2	11.2	8.7	2.1	2.1	1.1
26	27	30	44	50	40

87.6	86.1	86.1	87.6	88.2	88.1	88.0	87.2	87.3
74	89	89	74	68	69	70	78	77
30	28	27	23	9		10	29	50

94.3	95.0
0.7	0.0
43	50

87.3	88.0	87.8	86.3	86.4	86.8	86.9	87.1
77	70	72	8.7	8.6	8.2	8.1	7.9
28	25	11	6		17	40	50

87.9	94.0	94.5
7.1	1.0	0.5
32	46	50

Sta + π - Elev

894.95

20+50

✓
+81

✓
TP 4.01 894.22 4.74 890.21

21

Nov. 8, 1955 43 P

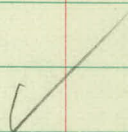
Lt

54

87.8	88.1	87.7	86.2	86.5	87.3	88.5	90.2
72	6.9	7.3	8.8	8.5	7.7	6.5	4.8
29	17	8	A		18	36	50

→ 94.3
0.7
43

94.6
0.4
50



88.4	88.2	86.8	86.8	88.0	88.7	88.9	89.9	90.7
6.6	6.8	8.2	8.2	7.0	6.3	6.1	5.1	4.3
18	8	4	3		5	23	39	50

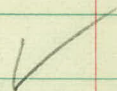
→ 88.5
6.5
28

89.4
5.6
33

94.5
0.5
44

94.2
0.8
50

Nail in PP Lt 51a 21 +



88.5	88.2	86.9	86.9	87.8	88.3	88.7	89.3
5.7	6.0	7.3	7.3	6.4	5.9	5.5	4.9
18	8	4	2		5	29	50



→ 88.7
5.5
29

89.4
4.8
50

Sta	+	π	-	Elev
-----	---	-------	---	------

		894.22		
--	--	--------	--	--

21+50				
-------	--	--	--	--

✓				
---	--	--	--	--

22				
----	--	--	--	--

✓				
---	--	--	--	--

+19				
-----	--	--	--	--

+50				
-----	--	--	--	--

FX
AM
LC
WJ

Lt

Nov. 9, 1955

L

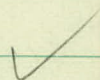
RT

494

88.4	88.6	88.4	87.1	87.1	87.7	88.2	88.5
5.8	5.6	5.8	7.1	6.5	6.5	6.0	5.7
25	16	7	4		7	25	50

88.4	88.7
5.8	5.5
30	49

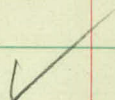
Garage



88.5	88.8	88.6	87.6	87.6	87.8	88.3	89.3
5.7	5.4	5.6	6.6	6.6	6.4	5.9	4.9
24	15	7	4		8	29	50

89.0	89.5	89.6
5.2	4.7	4.6
33	50	60

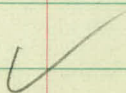
House



89.34	89.10
4.88	5.12
31	27.5
3' Walk	Landing

88.9	89.3	89.1	87.5	87.6	87.7	87.9	89.2
5.3	4.9	5.1	6.7	6.6	6.5	6.3	5.0
23	14	6	2		8	30	50

88.6	89.2	89.9
5.6	5.0	4.3
25	29	50



Sta + π - Elev

894.22

23 Aprox $\pm$ Jessie st

+ 25

+ 65

Nov. 9, 1955

45

11

84

88.9	89.0	89.5	89.3	87.7	87.8	88.6	89.7	91.0	92.1
53	52	47	49	65	64	56	45	32	21
50	30	16	6	2		5	19	39	50

✓

89.7	89.9	89.8	
4.5	4.3	4.4	Down 4%
100	130	150	

88.8	89.4	89.2	86.9	86.7	87.6	88.8	91.6
54	48	50	7.3	7.3	66	54	26
26	15	8	3		9	27	50

83.9	83.2
10.3	11.0
36	50

✓

89.5	89.5	89.1	87.6	87.0	87.7	88.8	90.2
47	47	51	66	7.2	65	54	40
23	15	8	3		15	35	50

84.3	83.2	83.0
9.9	11.0	11.2
32	37	50

✓

Sta + π - Elev

894.22

24

+50

TP 7.58 898.08 3.72 890.50

25

4
7
9

+50

+75

+82

2 Nov. 9, 1955

46

11

11

82.9	84.2	86.4	89.4	89.8	89.3	87.4	87.1	87.2	87.7	89.1
113	100	78	48	44	49	68	71	70	6.5	5.1
50	41	32	25	16	7	3		7	23	50

87.6	88.9	90.1	90.3	90.1	87.9	87.7	87.8	88.1	88.9
53	41	39	4.1	6.3	6.5	6.4	6.1	5.3	
42	25	16	8	3		8	24	50	

90.3	90.7	90.8	90.6	89.0	88.7	89.5	90.2
7.8	7.4	7.3	7.5	9.1	9.4	8.6	7.9
50	25	16	7	4		23	50

90.7	91.2	91.5	91.5	91.4	94.8	94.8	95.9
7.4	6.9	6.6	6.6	6.7	3.3	3.3	2.2
50	25	14	4		7	25	50

90.6	91.6	92.1	91.8	92.0	94.4	95.6	96.0	97.2
7.5	6.5	6.0	6.3	6.1	3.7	2.5	2.1	0.9
50	25	13	6	1		3	20	50

90.6	91.9	92.4	92.2	92.1	92.1	93.1	93.3	94.0	94.6
7.5	6.2	5.7	5.9	6.0	6.0	5.0	4.8	4.1	3.5
50	23	13	4		1	2	10	30	50

Sta + X - Elev

898.08

26

+ 12.40

BM

146 896.62 (896.59)

2

Nov. 9, 1955

47

Lt

RT

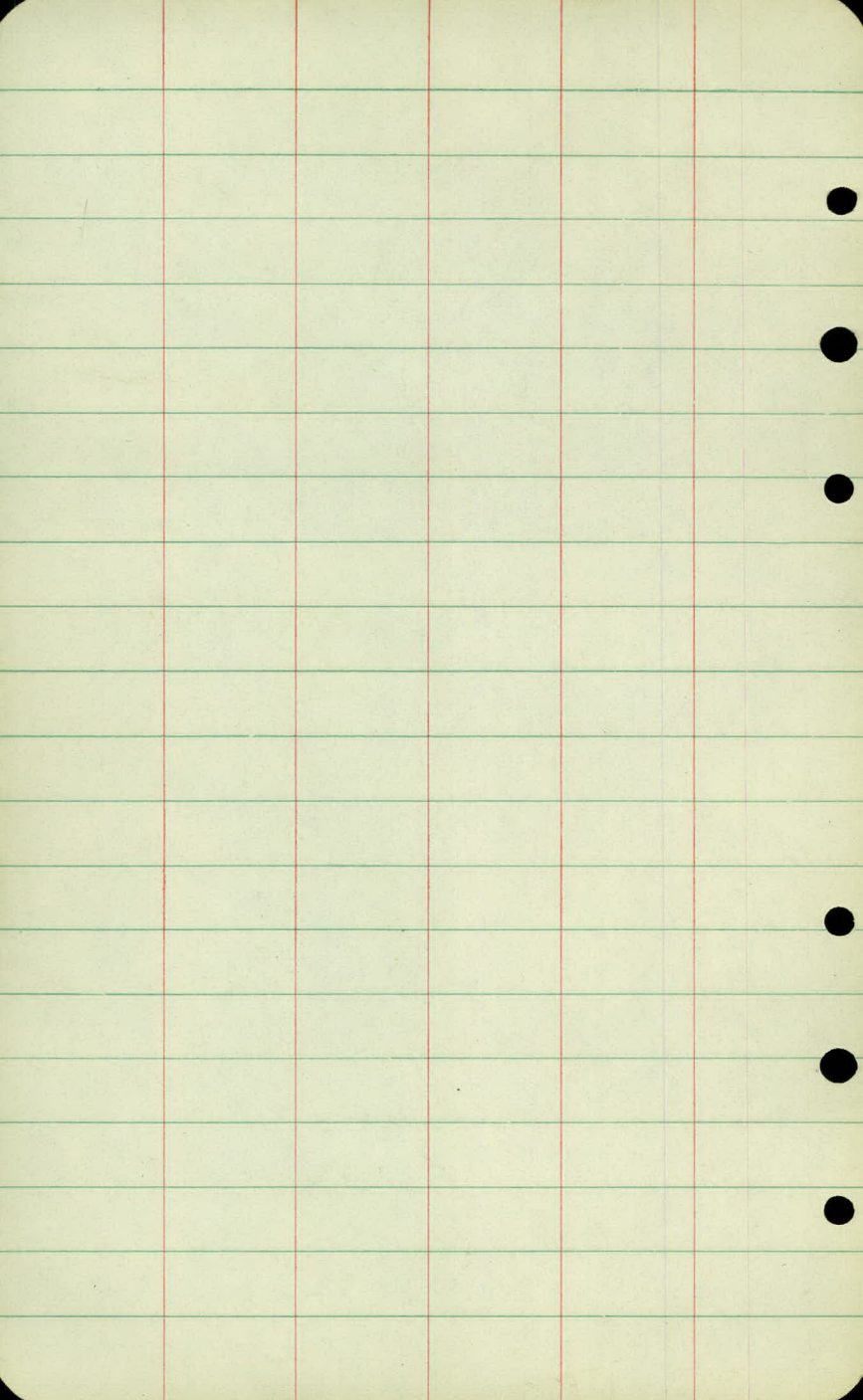
91.2	91.9	92.6	92.8	93.2	93.7
6.9	6.2	5.5	5.3	4.9	4.4
50	30	12		25	50

✓

91.5	92.3	93.1	93.5	94.2	94.6
6.6	5.8	5.0	4.6	3.9	3.5
50	25		25	50	100

✓

Top Hyd S.W. Cor Edgerton & Larpenfour



FK
AM
LC
WJ

Nov. 10, 1955

48

Additional x-sections

Sta	+	π	-	Elev.
BM	192	870.07		868.15

14+15

✓ sta. 14+15 to 16 inc.

VOID

+29 { see pages 55 to 62 }
for new x sections

+90

2 Nov 10, 1955

492

Lt.

Rt.

Top N.W. Cor Footing

57.6	56.7	59.8	60.8	58.1	56.3	58.0	61.1	63.5	63.9
12.5	13.4	10.3	9.3	12.0	13.8	12.1	9.0	6.6	6.2
50	31	19	6		8	18	27	45	50

57.1	59.3
13.0	10.8
70	100

66.25	65.7	62.8	63.3
3.82	4.4	7.3	6.8
92	88	67	60

Rail

59.9	59.3	62.0	61.6	60.5	59.5	59.8	63.0	64.5
10.2	10.8	8.1	8.5	9.6	10.6	10.3	7.1	5.6
50	31	20	14		2	13	20	35

61.9	62.7
8.2	7.4
75	100

66.43	65.9	63.7
3.64	4.2	6.4
74	72	50

Rail

71.8	69.9	65.9	65.5	65.6	66.4	66.91	66.85
11.7	0.2	4.2	4.6	4.5	3.7	3.6	3.22
30	25	10		10	19	24	33

Rail Rail

66.3	64.3	64.3	66.6
7.8	5.8	5.8	3.5
60	50	45	38

Sta + π - Elev.

870.07

15+06

+42

BM 11.90 880.05 1.92 868.15

14+90

15+06

+25

& Nov 10, 1955 503

Lt

RT

70.1	66.4	66.8	67.13	67.09	66.7	65.6
0.0	3.7	3.3	2.94	2.98	3.4	4.5
24	15		6	13	20	27

69.9	66.0
0.2	4.1
48	37

67.59	67.59	67.1	67.9
248	248	3.0	2.2
26.8	20.7	17	10

67.6
2.5
34

Top NW Cor. West Pier Footing

80.0	76.1	79.0	78.2
0.1	4.0	1.1	1.9
38	73	78	100

75.7	77.5	79.4	77.6	77.4
4.4	2.6	0.7	2.5	2.7
32	53	58	73	100

76.6	78.0	78.6	79.1
3.5	2.1	1.5	1.0
40	58	75	100

Sta + π - Elev

880.05

15+42

890.97 1.26 878.79

T.P. 12.18 891.97 ~~0.26~~ ~~879.79~~

BM 3.11 891.28 2.80 888.17

14+90

15

+06

FK
AM
JB

LH

E

Nov. 10, 1955
Nov. 14, 1955
54

54

71.9
8.2

80.1
0.0
12

✓

Boat Spike NE Wing Bridge abutment

78.9 80.4 82.6 82.4
12.4 10.9 8.7 8.9
73 67 55 48

78.3 80.0 84.6 84.9
13.0 11.3 6.7 6.4
79 83 94 100

✓

83.0 82.9 81.7 79.3
8.3 8.4 9.6 12.0
68 55 48 40

✓

81.8 80.8 82.1 82.5 83.9 85.5
9.5 10.5 9.2 8.8 7.4 5.8
73 75 80 87 95 100

84.5 84.1 83.3 82.3 79.8
6.8 7.2 8.0 9.0 11.5
71 66 58 54 40

✓

85.1 84.7 87.0
6.2 6.6 4.3
79 89 100

Sta + π - Elev

891.28

15+25

✓

+42

+67

TP 5.64 890.59 6.33 884.95

+67

TP 4.84 882.60 12.83 877.76

Lt

Rt

85.9 82.5 77.8 74.2
54 8.8 13.5 12.1
68 59 49 35

86.6 88.5 89.1
4.7 2.8 2.2
75 83 100

89.0 88.1 82.7 79.6
23 3.2 8.6 11.7
90 81 78 71

89.1
2.2
100

83.1 73.9
8.2 12.4
100 90

82.9 85.1 86.2 85.0
8.4 6.2 5.1 6.3
.24 34 48 62

82.8 84.1
8.5 7.2
100 81

85.0 86.4 86.4 85.7 84.9
5.6 4.2 4.2 4.9 5.7
14 19 28 44 57

82.6 83.4
8.0 7.2
100 80

Sta	+	Δ	-	Elev
-----	---	----------	---	------

		882.60		
--	--	--------	--	--

15+90				
-------	--	--	--	--

✓

16+25				
-------	--	--	--	--

TP	13.76	892.29	1.07	878.53
----	-------	--------	------	--------

18+70				
-------	--	--	--	--

2 Nov, 14, 1955 53/6

Lt

Bx

70.0	69.7	70.6	73.1	73.6	74.6	74.1	73.9	75.4
12.6	12.9	12.0	9.5	9.0	8.0	8.5	8.7	7.2
23	17	10		20	34	54	73	100

73.3	73.1	71.7	66.1	67.3	
9.3	9.5	10.9	16.5	15.3	8.1
30	43	52	60	63	68

74.2	71.8	71.0	70.6	70.5	70.1	70.5	70.4
8.4	10.8	11.6	12.0	12.1	12.5	12.1	12.2
35	27	19		19	41	63	90

77.9	78.4	74.9	71.8	67.3	67.9	
4.7	4.2	7.7	10.8	15.3	14.7	12.0
49	61	74	85	93	100	100

Cor Fe Post

81.4	82.8	83.3	83.1	87.7	88.7	89.7	92.3
10.9	9.5	9.0	9.2	4.6	3.6	2.6	0.0
24	22	16	7		2	18	40

81.4	83.9	85.3	86.4
10.9	8.4	7.0	5.9
27	30	41	52

Sta + π - Elev

892.29

18+79

+96 ✓

+96

TP 4.93 893.09 4.13 888.16

20+92

TP

2.83 890.26 890.21

2 Nov 14, 1955

54

Lt

Rt

86.0	85.5	84.3	85.3	87.8	89.0	89.4	90.5	91.9	92.2
6.3	6.8	8.0	7.0	4.5	3.3	2.9	1.8	0.4	0.1
20	8	6	4		2	11	23	39	43

✓

85.8	86.4	86.8
6.5	5.9	5.5
30	36	52

86.6	86.5	86.4	85.8	85.8	87.9	89.2	89.9	90.5	91.2	91.8
5.7	5.8	5.9	6.5	6.5	4.4	3.1	2.4	1.8	1.1	0.5
41	29	8	6	3		3	12	31	38	50

✓

87.8	88.8	89.1
4.5	3.5	3.2
68	100	107

♀ Garage

88.5	88.1	87.0	87.0	87.8	88.1	89.0	88.6	89.1	90.3
4.6	5.0	6.1	6.1	5.3	5.0	4.1	4.5	4.0	2.8
18	6	5	3	1		4	11	30	50

✓

88.7	89.8	91.3
4.4	3.3	1.8
30	56	67

Nail in PP Lt Sta 21⁺

Check Bench

Sta	+	π	-	Elev
-----	---	-------	---	------

BM	11.66	879.81		868.15
----	-------	--------	--	--------

			1.02	878.79
--	--	--	------	--------

Nov 29, 1955

55

NEW X-SECTIONS

X-sections

Re-X sections

Use these sections
instead of originals

Sta	+	π	-	Elev.
-----	---	-------	---	-------

BM	1.84	869.99		868.15
----	------	--------	--	--------

14+15

✓

+29

14.

81.

Top NW. Cor. W. Pier footing

60.2	61.0	61.0	60.8	58.0	56.6	57.5	60.2	61.3
98	90	90	92	12.0	13.4	12.5	98	87
24	20	14	7		12	18	28	37

57.0		65.7	66.19	65.7	65.2	64.4	62.1	62.7
13.0		4.3	3.80	4.3	4.8	5.6	7.9	7.3
31		100	97	95	90	84	69	42

Rail

57.2		58.0	57.7	60.3
12.8	12.0	12.3	9.7	
42	59	74	100	

59.3	61.8	61.9	62.0	60.6	59.6	59.0	59.5	60.8
10.7	8.2	8.1	8.0	9.4	10.4	11.0	10.5	9.2
32	23	15	5		3	7	15	22

66.36	66.36	65.8	64.6	64.4	63.4	64.0	64.5	63.3
36.9	36.3	4.2	5.4	5.6	6.6	6.0	5.5	6.7
90	83.5	80	73	66	59	50	36	29

Rail

65.9	65.3
4.1	4.7
94	100

✓

Sta + π - Elev

869.99

14+29

+90

✓

15

✓

+06

Lt

Rt

64.4
5.6
100

63.3
6.7
79

61.2
8.8
62

59.4
10.6
41



70.0
0.0
25

67.3
2.7
17

66.0
4.0
11

65.6
4.4
8

65.6
4.4
13

66.3
3.7
19

66.5
3.5
21

66.99
3.00
Rail

69.5
0.5
60

65.9
4.1
50

65.5
4.5
39

66.4
3.6
37

66.94
3.05
28
Rail

68.5
1.5
22

66.1
3.9
13

65.8
4.2
6

65.8
4.2
1

65.9
4.1
6

66.8
3.2
6

67.11
2.88
11
Rail

67.06
2.93
18
Rail

69.5
0.5
49

65.9
4.1
40

65.6
4.4
29

66.4
3.6
26

69.6
0.4
22

66.2
3.8
14

65.9
4.1
8

66.4
3.6
2

66.8
3.2
5
Rail

67.17
2.82
12
Rail

67.14
2.85
18
Rail

66.7
3.3
18

65.8
4.2
23

69.3
0.7
41

66.7
3.3
36

66.1
3.9
32

Sta + x - Elev

86999

15+25

✓

+42

TP 1248 882.47 0.00 869.99

+90

15

Nov 30, 1955

58

Lt

Rt

67.45

66.94

~~67.40~~

67.37

67.0

67.1

67.5

69.6

69.2

69.9

254

305

~~259~~

3.0

2.9

2.5

0.4

0.8

0.1

14

11

7

3

2

2

13

17

28

Rail

Rail

66.9

67.1

✓

3.1

2.9

17

23

67.63

67.2

67.3

68.0

69.1

236

28

27

20

0.9

24

20

18

12

6

Rail

67.1

67.67

67.3

67.4

✓

2.9

2.32

2.7

2.6

26

31

34

38

Nail

Rail

78.7

80.1

80.6

78.2

70.9

75.9

77.9

77.9

77.2

77.0

76.8

38

24

1.9

43

11.6

66

4.6

4.6

5.3

5.5

5.7

62

54

45

38

28

68

72

74

78

92

100

80.0

72.8

77.9

78.9

77.0

76.7

76.5

2.5

2.7

1.6

3.6

5.5

5.8

6.0

41

30

61

65

70

87

100

✓

Sta + x - Elev

882.47

15+06

+25

15+42

14+90

TP 12.06 894.23 0.30 882.17 3.75

15

Nov 30, 1953 59

Lt

Rt

81.5
1.0 30
48 39 29

77.5
5.0 4.1 4.1 5.2 6.0
53 57 60 64 70

76.5
6.0
100 78

81.0
1.5 4.0 7.5 9.6
61 54 43 33
Abt

75.2
7.3 6.2 6.3 6.1 6.1 5.9
37 46 57 66 86 100

82.5
0.0
78
Abt

74.5
8.0 9.6 11.5
58 50

72.4
10.1
4

80.8
1.7 0.3
19 23

83.7
+1.2
100

81.8
0.7 5.8 5.8
88 77 73

✓

81.2
13.0 12.4 10.5 10.7
69 64 54 51

✓

79.3

14.9
73

79.6

14.6
79

81.8

12.4
87

84.8

9.4
96

84.9

9.3
100

Sta + Δ - Elev

894.23

15+06

✓

+25

+42

✓

BM

6.04 888.19

BM

12.47 880.62

868.15

+67

2 Nov 30, 1955 60

RT

LT

80.9	82.8	83.5	82.7
13.3	11.4	10.7	11.5
75	70	64	52

82.4	82.0	83.4	85.5	86.0
11.8	12.2	10.8	8.7	8.2
77	84	91	96	100

89.2	89.0	88.3	86.7	83.5
5.0	5.2	5.9	7.5	10.7
100	81	77	69	63

87.8	87.4	85.7	84.6	83.4	83.9	81.8	80.9
6.4	6.8	8.5	9.6	10.8	10.3	12.4	13.3
100	90	83	79	29	41	60	78

81.7
12.5
100

B. Spike N.E. Wing of Bridge

Top NW Cor W. Pier footing

67.8	67.8	69.0	70.8	77.3	78.9
12.8	12.8	11.6	9.8	3.3	1.7
23	23	21	12	4	
10.3	10.3	10.4	10.2		
25	29	21			

Sta + π - Elev

880.62

15+67

✓

+90

✓

+90

Nov 30, 1955

64

R1

11

68.00	67.7	67.6	66.6
12.62	12.9	13.0	14.0
50	46	42	39
Rail			

67.5	68.08	67.8	67.6	67.8	71.4	73.6	80.4
13.1	12.54	12.8	13.0	12.8	9.2	7.0	0.2
53	57	61	63	69	77	86	97

70.0	69.4	70.2	72.6	73.5	73.4	73.3	72.7	72.6
10.6	11.2	10.4	8.0	7.1	7.2	7.3	7.9	8.0
24	19	11	3		12	26	42	62

74.6	74.6	72.2	72.1	71.7		73.1
6.0	6.0	8.4	8.5	8.9	End Lowland	7.5
32	34	37	43	52	175'	100

68.42	67.9	67.7	66.6
12.20	12.7	12.9	14.0
73	69	64	61

21' 0.66

67.9	68.48	68.1	67.1	68.2	71.5
12.7	12.14	12.5	13.5	12.4	9.1
77	80	85	90	92	100

Sta + π - Elev

880.62

16

TP 12.95 892.28 129 879.33

15+67

✓

BM

4.12 888.16 (888.16)

Nov 30, 1955

62

LH

RT

70.4	70.5	71.9	72.2	71.9	71.9	71.9	71.9	72.2
10.2	10.1	8.7	8.4	8.7	8.7	8.7	8.7	8.4
17	10	6		12	32	55	77	100

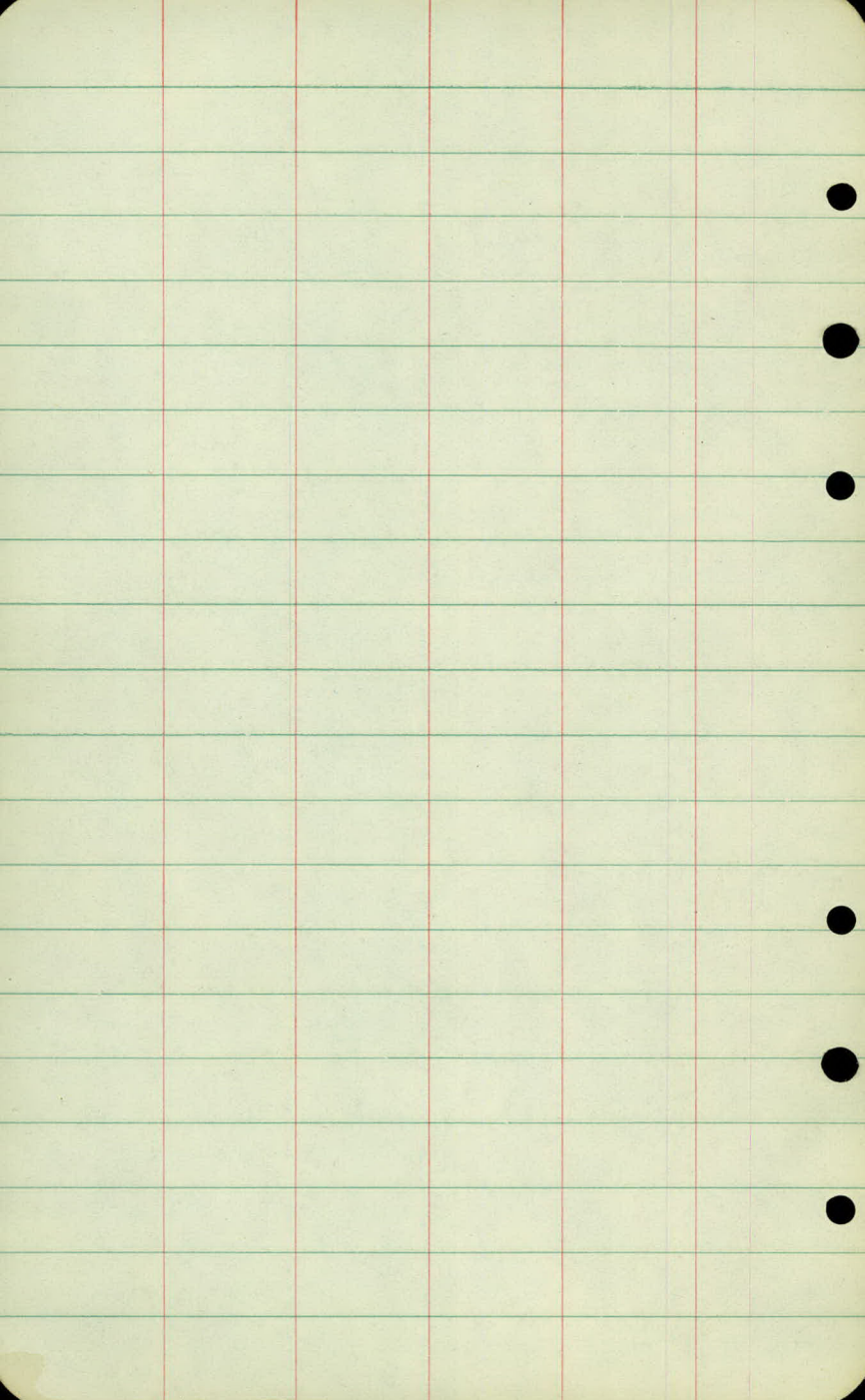
70.8	72.3	75.9	76.9	76.3	71.9	71.8	66.9	67.9
9.8	8.3	4.7	3.7	4.3	8.7	8.8	13.7	12.7
24	28	35	45	51	60	62	73	75

68.6	68.3	68.67	68.1	68.61	68.1
12.6	12.3	11.95	12.5	12.01	12.5
100	96	90	87	83	79

82.1	84.6	85.0	86.6
10.2	7.7	7.3	5.7
4	10	17	19

82.5	83.9	85.4	86.7	87.2
9.8	8.4	6.9	5.6	5.1
100	72	51	34	23

B. Spike in NE Wing of Bridge



LARPELLEUR

McMenemy to Edgerton

additional x-sections

2 pages

Sta + π - Elev

BM 1.42 869.57 868.15

14+50

TP 10.70 879.79 0.48 869.09

14+50

TP 11.33 890.12 1.00 878.79

BM 1.96 888.16 888.16

FX
AM
LC
WJ

Dec 6, 1955 62B

Top W. Conc Pier Footing West Pier

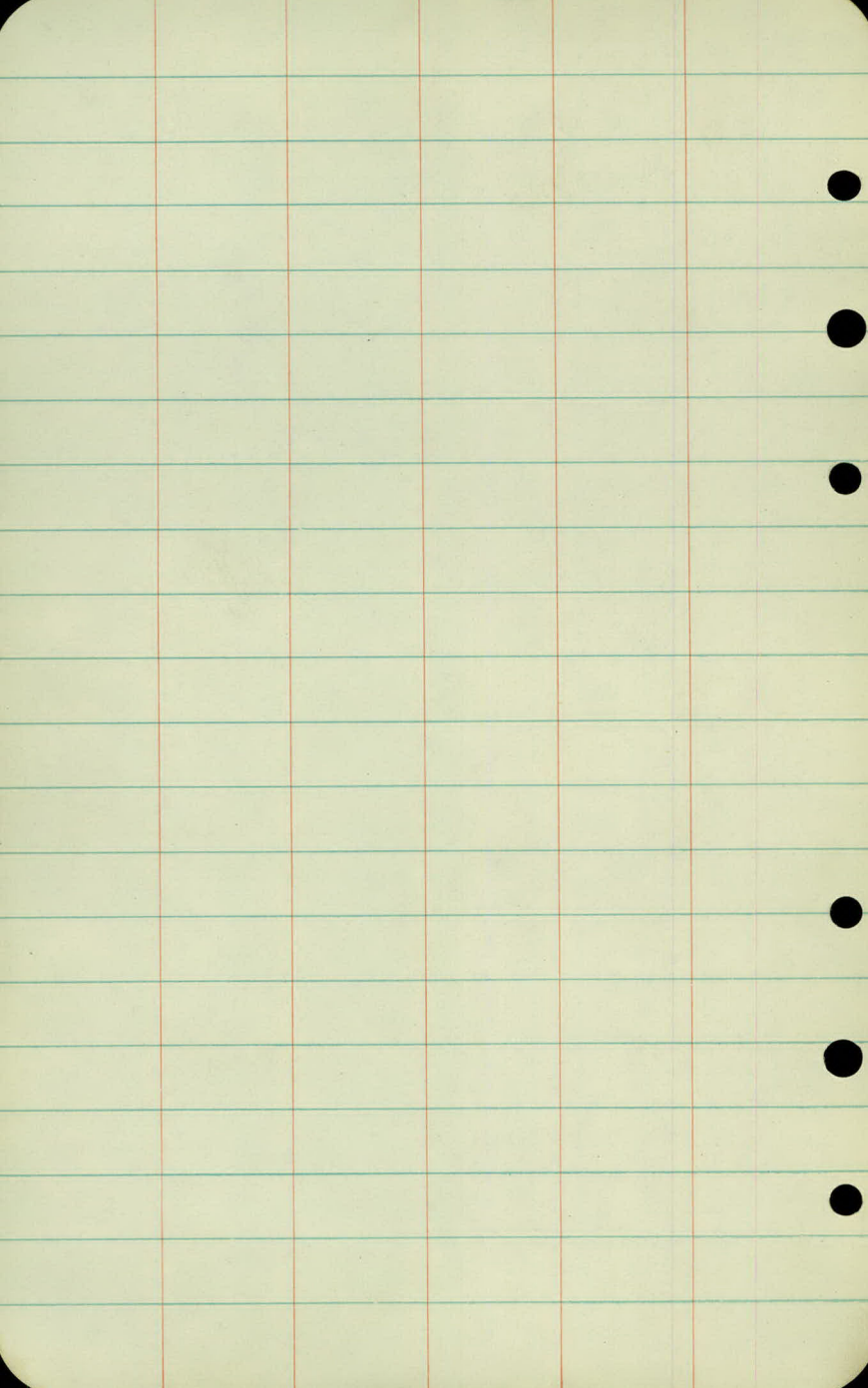
65.2	65.0	64.0	63.7	63.8	64.6	65.0	64.7	64.2	64.6
44	46	56	59	58	50	46	49	54	50
42	31	25	14	5		8	25	38	47

67.9	65.7	64.7	65.0	65.7	66.1	66.49	66.54	66.0	65.7
0.7	3.9	4.9	46	39	3.5	308	303	36	3.9
100	93	85	81	77	73	69	62	59	55
						Rail	Rail		

66.8	66.0	66.1	68.8
2.8	3.6	3.5	0.8
52	56	60	68

71.9	70.0
79	98
100	86

B. Spike NE Wing of Bridge



12-1-55

63

LARPENTEUR

Mc Menemy to Edgerton

x-street x-sections

Edgemont
+
Arkwright

7 pages

Edgemont St.

Sta + π - Elev.

BM 6.96 864.85 857.89

0+00 Section Line Sta 3423 [?] 59.2

TP 11.46 874.89 1.42 863.43

Sta 5 11.15 863.74 63.8

0+50

✓

1

✓

Rx

6.7

619	624	620	626	634	633
130	125	129	123	115	116
38	42	50	67	78	50
		Driveway			

669
8.0
65
H.

67.6	66.9
7.3	8.0
50	37

Sta	+	π	-	Elev
-----	---	-------	---	------

		874.89		
--	--	--------	--	--

1+41				
------	--	--	--	--

✓				
---	--	--	--	--

+59				
-----	--	--	--	--

2				
---	--	--	--	--

Dec. 1, 1955 65

LT

RT

67.5	68.4	68.9	69.5	69.4	69.6	69.5	68.9	69.3
7.4	6.5	6.0	5.4	5.5	5.3	5.4	6.0	5.6
50	32	19	8		5	11	12	14

73.1	70.8	69.4	67.9	67.9	69.7
1.8	4.1	5.5	7.0	7.0	6.2
50	37	29	27	26	25

69.8	69.9	70.4	70.2	70.8	70.9	70.8	70.4	70.2	69.4	69.4
5.1	5.0	4.0	4.7	4.1	4.0	4.1	4.5	4.7	5.5	5.5
50	36	19	16	10		10	14	24	26	27.5

76.9	74.9	73.1	71.3
+20	0.0	1.8	3.6
50	42	36	30

73.7	73.8	73.2	73.6	74.0	73.7	73.3	72.5	72.5
1.2	1.1	1.7	1.3	0.9	1.2	1.6	2.4	2.4
28	19	16	13		6	13	17	18

73.3	72.9	81.9	78.9	74.9	73.9	73.3
1.6	2.0	+70	+40	0.0	1.0	1.6
32	50	50	40	30	27	20

Ark right St.

Sta	+	x	-	Elev.
BM	0.04	908.02		907.98
Sta 8			4.0	904.0

0+00 Sec Line Sta 7+80.6 018

House Between streets ^{No} 2.0

+ P 5.87 906.59 7.30 900.72

0 + 50

✓

1

Lt.

Rt.

RR Spike in Oak Rt sta 9+10±

6.2

East Iron

956	946	954	957	972	972	981	993	02.2
11.0	12.0	11.2	9.9	9.4	9.4	8.5	7.3	4.4
32	28	26	13		15	34	46	62
949	917	874				03.7	03.2	
11.7	14.9	19.2				2.9	3.4	
43	66	100				100	83	
986	99.3	986	992	995	996	991	99.4	99.8
8.0	7.3	8.0	7.4	7.1	7.0	7.5	7.2	6.8
47	25	15	3		6	16	32	38
959	92.8	90.2					048	038
10.7	13.8	16.4					1.8	2.8
67	82	100					100	68

Sta + π - Elev

906.59

+50

✓

2

✓

TP 2.5289998 9.13 89746

+50

2 Dec. 1, 1955

67

2+

R4

00.4	00.4	00.0	00.3	00.6	00.6	00.3	00.2	00.8
6.2	6.2	6.6	6.3	6.0	6.0	6.3	6.4	5.8
48	24	14	7		6	10	29	38

99.6	95.2	95.2		99.4	93.4	93.6	92.3
7.0	10.0	11.4		8.2	3.2	3.0	4.3
73	90	100		100	83	68	50

99.7	99.3	98.9	99.3	99.6	99.6	98.7	99.1	99.0
6.9	7.3	7.7	7.3	7.0	7.0	7.9	7.5	7.6
48	27	12	8		9	16	17	31

00.4	99.9	99.1		91.0	95.3	99.7
6.2	6.7	7.5		5.5	15.6	11.3
72	93	100		73	60	44

97.1	96.8	96.2	96.8	97.1	97.1	96.5	96.9	93.0
2.9	3.2	3.8	3.2	2.9	2.9	3.5	3.1	7.0
45	20	14	7		3	14	32	45

98.0	98.7	99.1		83.7	86.5	90.4
2.0	1.3	0.9		16.3	13.5	9.6
69	91	100		100	72	53

sta + π - Elev

899.98

3

✓

+58.83

4

944

+50

953

+50

5

962

Dec 1, 1955 68

Lt

Rt

93.3	94.2	94.6	94.3	94.5	94.1	94.0	92.9	90.1
6.7	5.8	5.4	5.7	5.5	5.9	6.0	7.2	9.9
42	32	22	8		14	28	35	47

92.8	91.4	91.4	80.8	84.5	85.8
7.2	8.6	8.6	15.2	15.5	14.2
57	78	100	100	82	65

89.9	91.1	94.2	93.6	93.6	93.4	93.0	91.5	89.5
10.1	8.9	5.8	6.4	6.4	6.6	7.0	8.5	11.5
48	41	30	15		14	26	34	44

87.4	87.2	85.8	86.2
11.6	12.8	14.2	13.8
67	94	75	56

5.6

4.7

3.8

Sta + π - Elev

899.98

5+50

96.8

6

97.5

TP 6.00 905.61 0.37 899.61

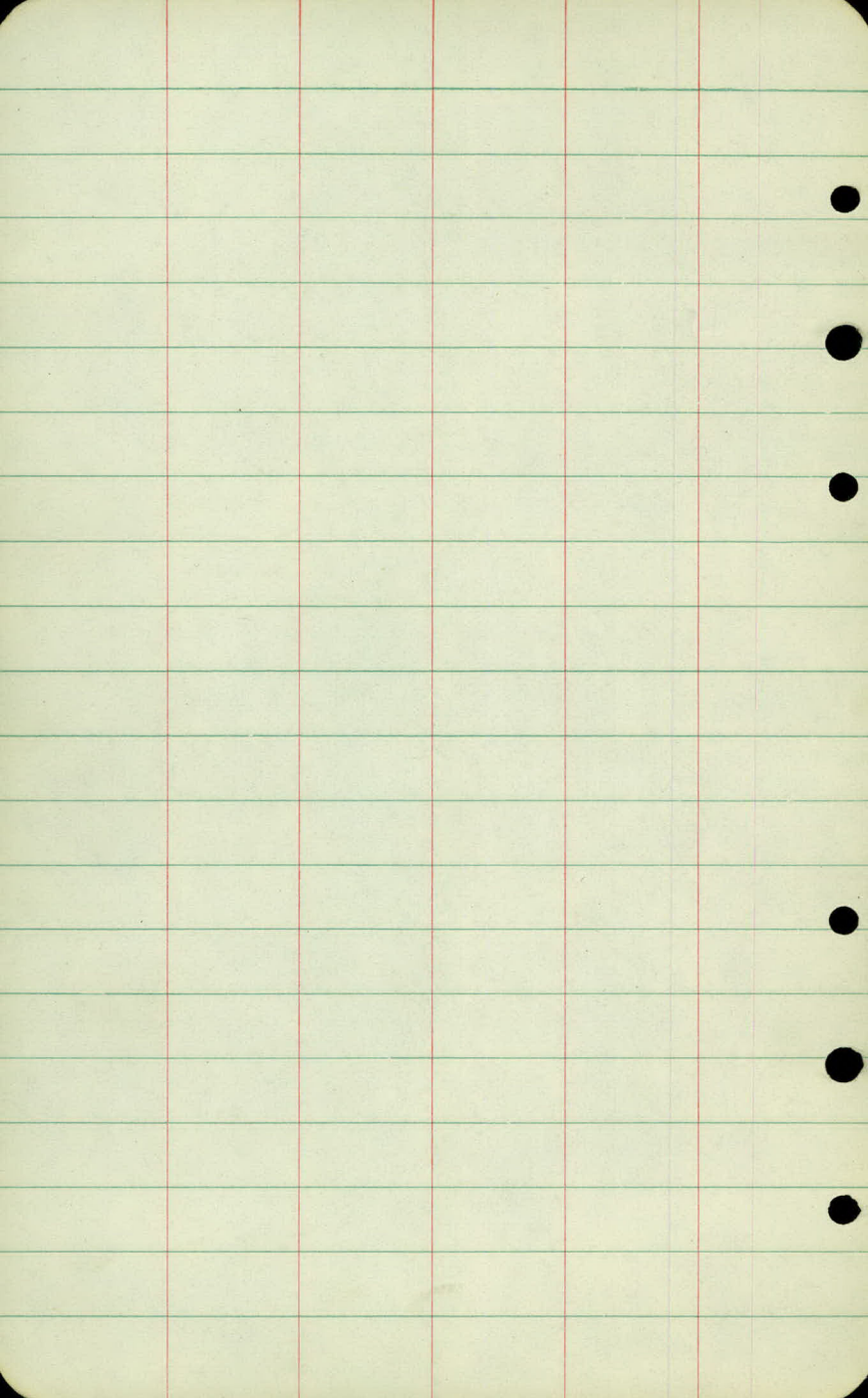
Sta 8 Sec. 1 inc 1.55 904.06

Dec 1, 1955 69

3.2

2.5

sta 2



FK
LC
WJ

Dec. 15, 1955

70

X-Section Extensions

Sta	+	π	-	Elev
BM	5.73	863.62		857.89
BM			2.89	860.73

3+72

TP	13.63	874.67	2.58	861.04
----	-------	--------	------	--------

"	10.43	884.01	1.09	873.58
---	-------	--------	------	--------

BM	13.44	894.78	2.67	881.34 (881.22)
----	-------	--------	------	-----------------

5+50

6

TP	11.57	905.59	0.76	894.02
----	-------	--------	------	--------

Dec. 15, 1955 71

Lt

Rt

Top NE Cor Bottom Step H. #1675 McMenamy

Top Hyd SW Cor Larpentour + McMenamy

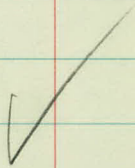
58.1	56.8	56.8	53.1
5.5	6.8	6.8	10.5
	8	33	60

Spike in 18" Oak 1' Rt sta 6+28^t

87.5	86.4	84.7	82.1
7.3	8.4	10.1	12.7
129	111	100	85
88.3	89.4	90.6	92.9
6.5	5.4	4.2	1.9
147	165	189	200

92.1	90.6	88.9	86.8	85.1
2.7	4.2	5.9	8.0	9.7
175	148	127	100	85

93.4
14
200



Sta + π - Elev

905.59

6

+50

✓

+70

✓

7

Dec 15, 1955
Clear 50°F Windy R+

72

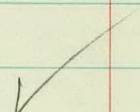
14

99.8	97.7	96.4	94.3
5.8	7.9	9.2	11.3
250	235	221	210

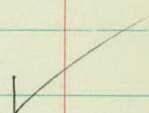


93.6	92.4	90.0	86.6	85.0
12.0	13.2	15.6	19.0	20.6
163	145	126	100	85

95.1	96.6	98.6	90.2	90.9
10.5	9.0	7.0	5.4	4.7
184	200	219	234	250



95.2	93.4	91.3	88.9	88.0
10.4	12.2	14.3	16.7	17.6
166	145	125	100	85



96.7	97.9	99.4	99.6	99.8
8.9	7.7	6.2	6.0	5.8
185	200	217	233	250

99.9	98.7	95.5	92.8	91.5
5.7	6.9	10.1	12.8	14.1
177	160	130	100	85



100.2	100.2	99.6	98.8	
5.4	5.4	6.0	6.8	
100	221	237	250	

Sta + π - Elev.

905.59

8+50

✓

9

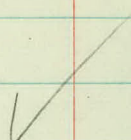
✓

740 900.68 12.31 893.28

+50

L+

97.3	01.4	03.1	04.0	04.0
8.3	4.2	2.5	1.6	1.6
186	172	164	139	115
93.0	89.7	88.3	87.4	
12.6	15.9	17.3	18.2	
200	215	237	250	



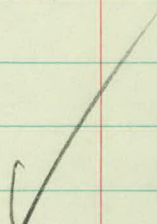
89.0	94.6	99.1	02.6	05.2
16.6	11.1	6.5	3.0	0.4
170	153	139	126	112



12.7

85.9
19.7
180

82.0	81.5	83.9	88.3	93.5
18.7	19.2	16.8	12.4	7.2
200	172	155	136	117



83.4
17.3
225

84.4
16.3
250

Sta + π - Elev

900.68

9

TP 2.59 895.87 740 893.28

10

✓

+50

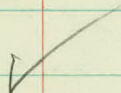
11

+30

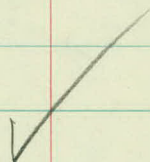
FK
LC
WT

Dec 15, 1955
Dec 16, 1955 74

83.9	82.7	83.5	84.3
16.8	18.0	17.2	16.4
250	225	200	191

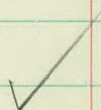


81.5	80.4	80.3	81.5	84.7
14.4	15.5	15.6	14.4	11.2
200	165	143	129	111



83.2	85.7
12.7	10.2
220	250

85.2	83.3	80.7	80.0	79.3
10.7	12.6	15.2	15.9	16.6
215	200	170	146	123



86.3	85.3	82.8	81.2	79.6
9.6	10.6	13.1	14.7	16.3
215	200	168	138	118



88.0	87.3	85.5	83.9	83.0	83.3
7.9	8.6	10.4	12.0	12.9	12.6
215	200	176	154	134	115

Sta + π - Elev

895.87

11+45

12

TP 13.35 908.34 0.88 894.99

BM 0.24 908.10 907.98
+1.12

BM 6.61 887.95 881.34 (881.22)

6+70

7

+50

TP 13.22 892.86 8.31 879.64

Dec 16, 1955

75

89.1	86.5	84.7	85.1	86.3
6.8	9.4	11.2	10.8	9.6
200	179	152	141	119

92.2	91.2	88.9
3.7	4.7	2.0
150	128	116

Spike in 15" Oak 30' Rt Sta 9+10

Spike in 18" Oak 1' Rt Sta 6+28

73.8	72.2	71.5	70.9
14.2	15.8	16.5	17.1
64	70	80	93
Ent			

77.3	73.7	70.8
10.7	14.3	17.2
80	90	93
Edge Ent		

80.2	77.4	74.8	73.4
7.8	10.6	13.2	14.6
85	94	100	105

70.2
17.8
112
Edge Ent

Sta	+	π	-	Elev
-----	---	-------	---	------

		892.86		
--	--	--------	--	--

7+81				
------	--	--	--	--

8				
---	--	--	--	--

+50				
-----	--	--	--	--

9				
---	--	--	--	--

9				
---	--	--	--	--

BM				
----	--	--	--	--

		12.21		880.65
--	--	-------	--	--------

TP				
----	--	--	--	--

	13.02	902.73	3.15	889.71
--	-------	--------	------	--------

+50				
-----	--	--	--	--

				876
--	--	--	--	-----

				21
--	--	--	--	----

FK
LC
WJ

4

Dec 16, 1955
Dec 20, 1955

B+

76

Lt

81.2	76.7	75.1	73.9
11.7	16.2	17.8	18.0
75	91	97	100

✓

80.9	76.8	74.0	71.9
12.0	16.1	18.9	21.0
75	90	100	115

✓

85.1	83.0	81.4	76.7	71.0
2.8	9.9	11.5	16.2	21.9
90	100	108	119	137

✓

91.2	88.9	84.5	80.8	76.1
1.7	4.0	8.4	12.1	16.8
115	128	135	145	156

✓

Top East Cor. Basement Ho

Top of iron with Elbow

97.5	92.8	88.4	80.7
5.2	9.9	14.3	22.0
124	146	160	181

✓

Sta + π - Elev

902.73

10

83.2

19.5

+50

18

84.7

TP 8.26 909.70 1.29 901.44

BM 1.59 908.11 (907.98)
+13

2

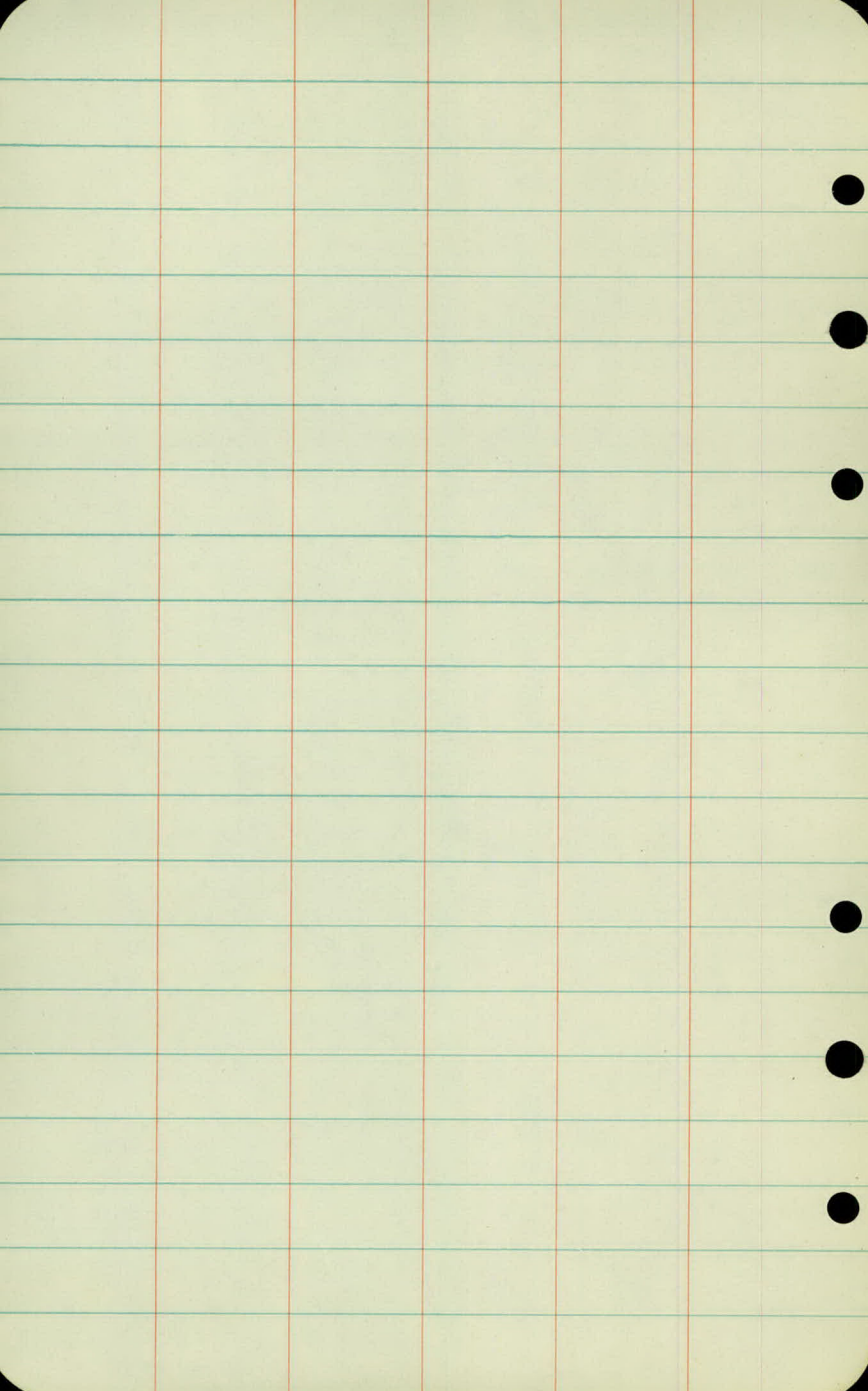
Dec 20, 1935

77

99.9	98.6	92.8	86.7	82.9
1.8	4.1	9.9	16.0	19.8
134	151	178	200	212

92.4	89.5	85.2	79.7
10.3	13.2	17.5	23.0
124	148	175	200

Spike in 15" Oak 50' Rt Sta 9+10



LARPEUR

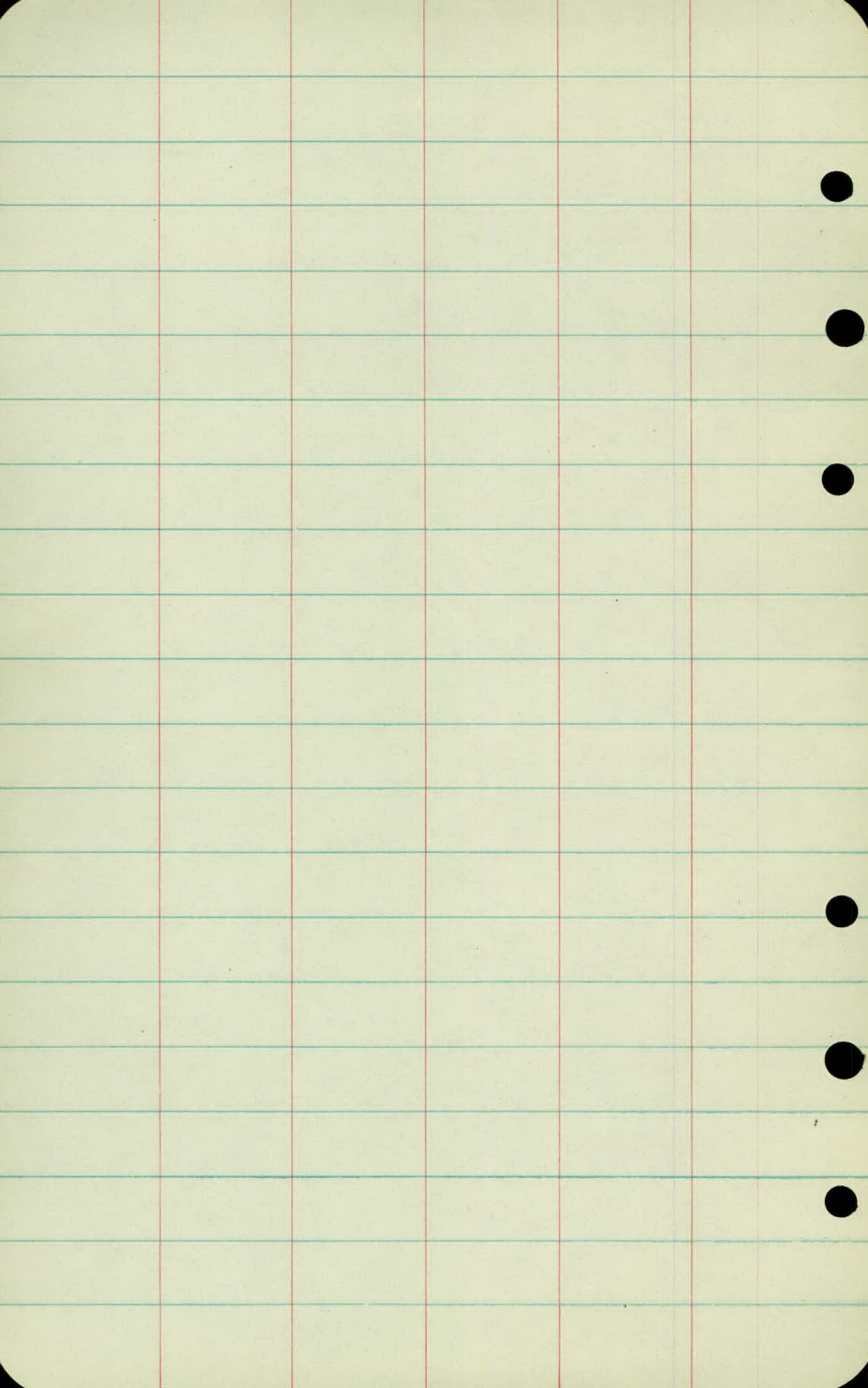
McMenemy to Edgerton

Desota Street Survey

Lt. sta 14+30

Rt sta 16+10

Wrong End of Chain



FK
LC

Dec. 28, 1955

79
2

Alignment North

Lt. of sta. 14+30

Sta	Point	ΔL	ΔR
-----	-------	------------	------------

+36.22 =		$16^{\circ} 07\frac{1}{4}'$	
----------	--	-----------------------------	--

3		$13^{\circ} 13.4'$	$\Delta = 32^{\circ} 14\frac{1}{2}'$
---	--	--------------------	--------------------------------------

+50		$9^{\circ} 13.4'$	$D = 16^{\circ}$
-----	--	-------------------	------------------

2+38.55	P.I.	$32^{\circ} 14\frac{1}{2}'$	$T = 103.84$
---------	------	-----------------------------	--------------

2		$5^{\circ} 13.4'$	$L = 201.51$
---	--	-------------------	--------------

+50		$1^{\circ} 13.4'$	$R = 359.265$
-----	--	-------------------	---------------

1+34.71	PC	$0^{\circ} 00'$	
---------	----	-----------------	--

0+55	P.I.	$23^{\circ} 07'$	
------	------	------------------	--

0+00 Section line Sta 14+30
 14+30 Larp. Avc =

Dec 28, 1955

80
3

Beat Spike

Spike

90°00' →

Spike

Sta Point ΔL ΔR

~~4+19.12 / P.I. - 1936 SURVEY~~
~~4+22.65 = P.I.~~
~~= old 4+19.12~~

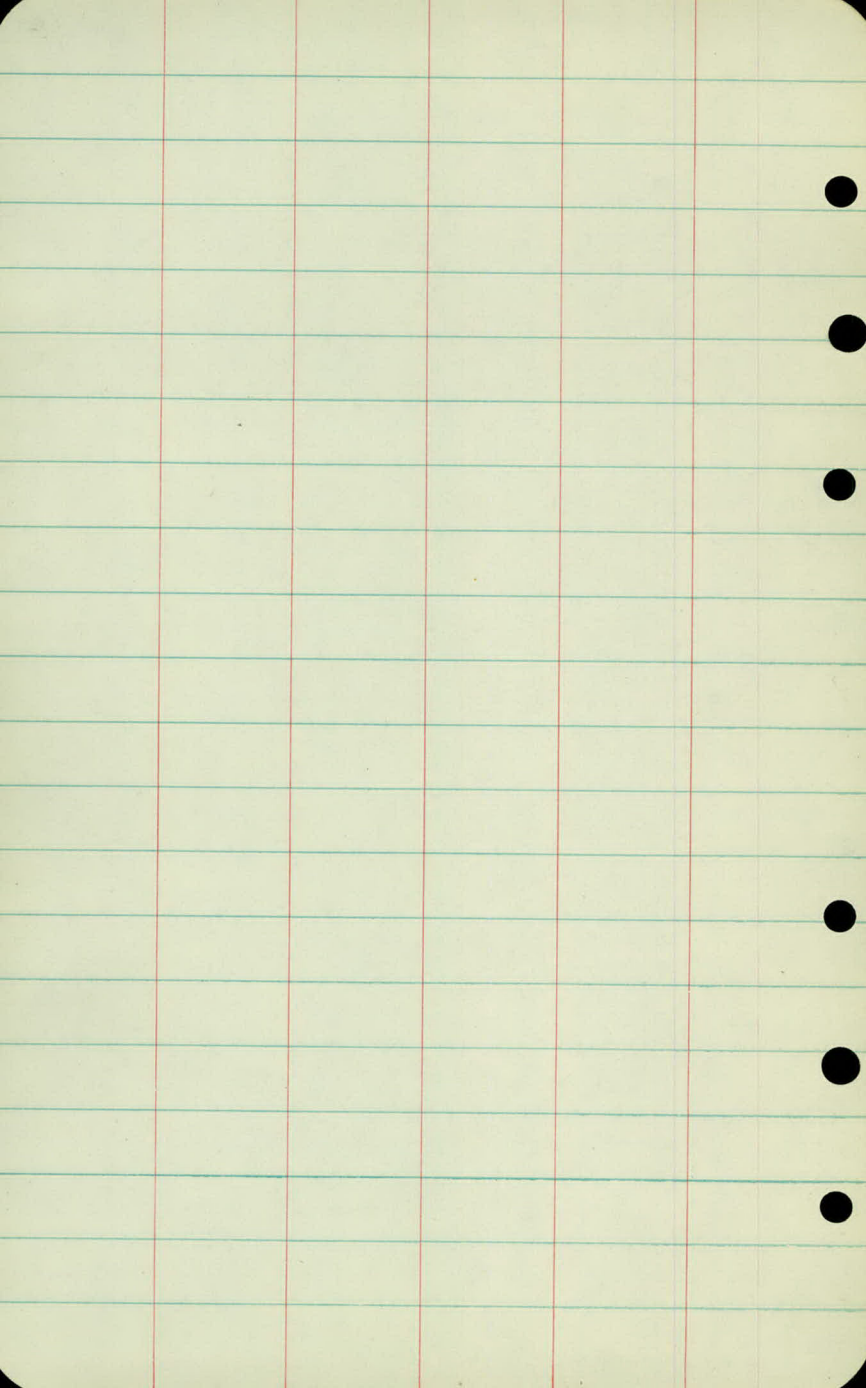
Note: Same bearing as when
checked original line (1934)

FK
LG
AB
W

£ Jan 3, 1956

81#

Boat Spike



Jan 3, 1956

82⁵/₅

Alignment south

Rt sta. 16+10

Sta	Point	ΔH	ΔR
-----	-------	------------	------------

+95.01			
+94.99	P.T.	$16^{\circ}02'15''$	

+75		$13^{\circ}32.3'$	$\Delta = 32^{\circ}04\frac{1}{2}'$
-----	--	-------------------	-------------------------------------

+50		$10^{\circ}24.8'$	$D = 25^{\circ}$
-----	--	-------------------	------------------

+33.1	P.I.	$32^{\circ}04\frac{1}{2}'$	$T = 66.39$ ✓
-------	------	----------------------------	---------------

+25		$7^{\circ}17.3'$	$L = 128.30$ ✓
-----	--	------------------	----------------

+1	P.I.	$4^{\circ}09.8'$	$R = 231.01$
----	------	------------------	--------------

+75		$1^{\circ}02.3'$	
-----	--	------------------	--

+66.69	P.C.	$0^{\circ}00'$	
--------	------	----------------	--

0+41	P.I.	$41^{\circ}20'$	
------	------	-----------------	--

0+00 Section Line Sta 16+10

Jan 3, 1956

83
6

spike

spike

90° 00' →

spike

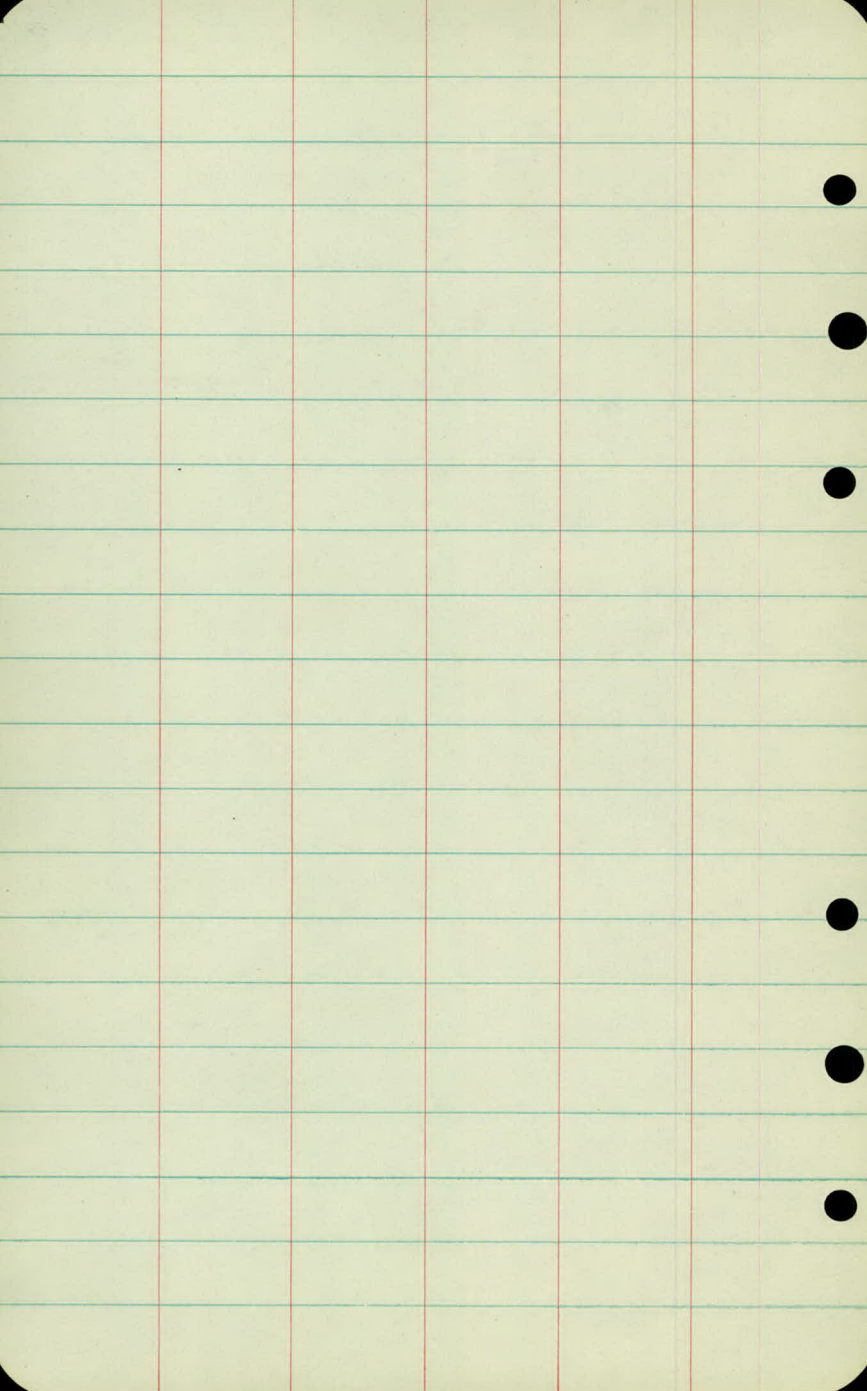
Sta Point Δ Lt Δ Rt

2 + 25.84 P.O.T.

£ Jan 3, 1955

847

spike



DESOTA ST.

X-Sections

North of Larp Ave.

Lt. Sta. 14100

888.16

Sta	+	π	-	Elev
BM	1.12	869.27		868.15

0+55 Parallel to Sec. Line

1

+34.71 PC

TP 11.93 880.56 0.64 868.63

0+55

1+ 17

+34.71

FX
LC
AB
CW

Jan 5, 1956

86
7

14

RT

W. Cor. Conc. footing Ch. Pire Desoto St. Bridge

51.4	51.6	52.5	54.1	57.8	61.3	65.0	68.6
17.9	17.7	16.8	15.2	11.5	8.0	4.3	0.7
100	78	53	40	17		14	27

60.3	58.6	59.1	61.8	66.1
9.0	10.7	10.2	7.5	3.2
100	74	55	33	16

70.6	69.3	68.4	68.0	67.3
11.3	0.0	0.9	1.3	2.0
100	92	80	68	52

72.6	78.6	80.2
7.0	2.0	0.4
46	58	62

71.0	74.9	77.3	78.8	78.6
9.6	5.7	3.2	1.8	2.0
18	31	37	42	

67.8	69.8	71.4	74.5	77.6	80.1
12.8	10.8	9.2	6.1	3.2	0.5
49	35	24	15		12

Sta + π - Elev

880.56

1+50

T.P. 12.69 892.26 0.99 879.57

0+55

62

1

42

12

+34.71

Jan 5, 1956

87
#

11

B1

72.0

73.7

74.4

76.5

79.6

80

6.9

6.2

4.1

1.0

53

40

29

16

73.2

74.1

76.2

74

6.5

4.4

67

82

100

82.7

83.2

82.5

81.7

79.0

9.6

9.1

9.8

10.6

12.3

69

76

24

30

98

86

92

Bridge

77.7

80.2

83.4

86.3

14.6

12.1

8.4

6.0

50

60

67

77

84.0

82.7

81.1

3.3

3.6

5.7

90

84

83

Abutment on Wing

84.0

85.9

86.7

87.3

84.0

8.3

6.4

5.6

5.0

3.3

27

38

48

56

65

89.3

3.0

23

81

Sta + π - Elev

892.26

1+50

2

BM 11.70 899.86 4.08 888.18 (888.16)

2

+50

T.P 10.69 908.99 1.56 898.30

3

Jan 5, 1936 88 #

14

81

83.9 87.4 88.2 89.0 89.6 89.6
8.4 4.9 4.1 3.3 2.7 2.7
17 33 43 50 54 62
E.R.

84.7 84.5 83.9 83.9 85.6 89.1 90.2 91.0 91.0 91.1
6.4 7.4 7.8 8.4 8.4 6.7 3.2 1.7 1.3 1.3 1.2
87 72 57 41 25 11 20 30 39

Boat spike in N.E. Wing of Bridge

90.8 92.6 92.6
9.1 7.3 7.3
43 49 57

94.0 93.7 95.1 96.9 95.5 93.8 93.9 93.7 95.3
5.9 6.2 4.8 3.0 4.4 6.1 6.0 6.2 4.6
5.4 3.9 2.2 8 7 14 20 24

95.1 96.3 98.3 98.8 99.3 100.9 99.9
4.8 3.6 1.6 1.1 0.6 1.0 0.0
67 79 100 50 45 38 33
2+50 & 1'stale

100.6 100.1 99.1 97.6 96.8 96.6 96.5 98.6
8.4 8.9 9.9 11.4 12.2 12.4 12.5 10.4
23 12 9 6 6 12 16

01.7 02.8 04.8 07.2 00.5 00.0 98.7
7.3 6.2 4.2 1.8 8.5 9.0 10.3
35 47 63 78 50 30 18

Sta + A - Elev.

908.99

3+36.22

+50

4

+50

T.P. 1.26 899.55 10.70 898.29

BM 4.85 893.01⁰⁰ 11.40 888.15¹⁶

TP 1.09 888.16¹⁹ 5.94 887.07¹⁰

SO. OF LARE AVE. South
Desoto

0+41

Jan 5, 1956

89
12

21

RT

044	038	032	984	98.2	981	987	989	990
46	5.2	5.8	11.6	10.8	10.9	10.3	10.1	11.0
40	35	20	10		10	14	20	40

98.6
104

99.3
9.7

99.5
95

Boat Spike in NE Wing of Bridge

Where from?

709	705	70.4	70.1	71.4	72.2	73.3	85.8	86.1
17.3	17.7	17.8	18.1	16.8	16.0	14.9	2.4	2.1
75	52	36	20		14	21	42	49

771	76.2	81.6	86.5	86.3	84.7	84.8
11.1	12.0	6.6	1.7	1.9	3.5	3.4
96	86	75	65	61	58	51

Sta + π - Elev

888.¹⁹16

0+75

✓

1

+07

✓

+50

2 Jan. 5, 1956

90
13

11

81

71.1	70.5	70.4	70.7	72.9	84.0	84.4	83.2	83.4
171	127	178	175	15.3	4.2	3.8	5.0	4.8
69	56	40	23		22	28	30	38

71.1
17.1
75

76.7
115
75

76.3
119
65

80.3
79
55

84.7
3.5
46

85.1
31
42

80.4
7.8

73.0	73.5	74.6	82.5	82.9	82.4	82.7	83.4
15.2	19.7	13.6	5.7	5.3	5.8	5.7	4.8
31	21	13		8	12	21	22

71.5
16.7
42

70.6
17.6
55

71.1
17.1
68

71.1
17.1
75

76.4
11.8
52

77.8
10.4
40

80.8
7.4
35

83.9
4.1
28

75.8	77.4	80.7	81.8	81.4	81.3	81.0	77.6
12.4	10.8	7.5	6.4	6.8	6.9	7.2	10.6
31	20	8		3	13	21	27

74.3
13.9
43

73.0
15.2
60

76.7
11.5
50

77.2
11.0
34

Sta + π - Elev

888.^{.19}/₁₆

1+95

✓

2

+25.84 P.O.T.

+30

+50

24

24

76.8	78.3	89.0	81.5	82.0	81.6	80.9	79.0	78.1
11.4	9.9	8.2	6.7	6.2	6.6	7.3	9.2	10.1
32	23	16	8		11	16	21	31

76.1	75.0	74.7		77.3		77.6
12.1	13.2	13.5		10.9		10.6
45	56	60		50		41

72.0
6.2

80.1	82.0	81.7	82.2	82.5	82.3	81.4	79.7	78.6	78.4
8.1	6.2	6.5	6.0	5.7	5.9	7.1	8.5	9.6	9.8
19	12	9	6		9	13	22	44	50

78.2	77.2
10.0	11.0
27	50

82.9
3

Sta + π - Elev

888.16¹⁹

3

+50

TP 7.24 894.30 1.10 887.06⁰⁹

BM 6.17 888.13 (888.16)

Jan 5, 1955

92
~~75~~

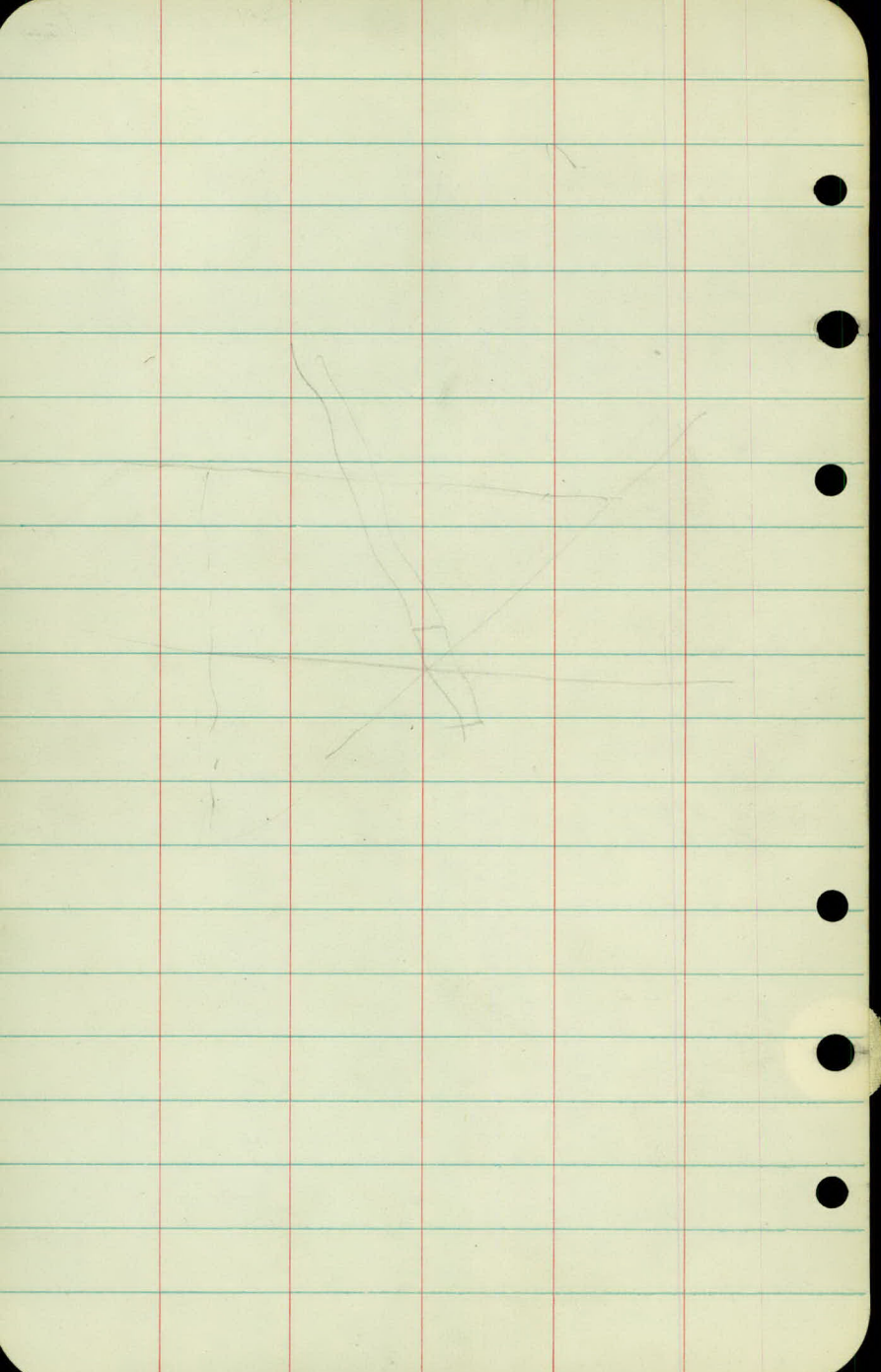
Lt

Rt

88.7
8
3.5

87.6
8
0.6

Brat Spike in NE Wing of Bridge



Profile

70' South of Sec Line

5 pages

Sta	+	π	-	Elev
BM	18.20	886.35		868.15

14+49.5

+54

+62

+70

76.5

85

FK
LC
AB
CW

Jan 12, 1956 94 2

W. Cor. Conc. footing Ch. Pier Desota St. Bridge

66.65

19.7

Rail

70'

65.75

20.6

64.95

21.4

65.25

21.1

67.35

19.0

70.85

15.5

Sta	+	π	-	Elev
-----	---	-------	---	------

		886.35		
--	--	--------	--	--

14+88				
-------	--	--	--	--

+92				
-----	--	--	--	--

15				
----	--	--	--	--

+08				
-----	--	--	--	--

+21				
-----	--	--	--	--

+30				
-----	--	--	--	--

Jan 12, 1956

95
9

70' RT

75.95

10.4

70'

78.05

8.3

77.65

8.7

76.45

9.9

76.55

9.8

76.95

9.4

Sta + x - Elev

886.35

15135

+46

+52

+54

+61

+64

Jan 12, 1956

96A

78.65

2.7

84.25

2.1

84.15

2.2

82.85

3.5

82.65

3.7

83.95

2.4

Sta	+	π	=	Elev
		886.35		

15 + 71

+ 82

+ 87

16

+ 15

+ 35

1 + ⁵94.99 L Desoto St South

Jan 12, 1936 97
5

20' Rt

83.95

2.4

75.05

11.3

72.95

13.4

71.85

14.5

70.45

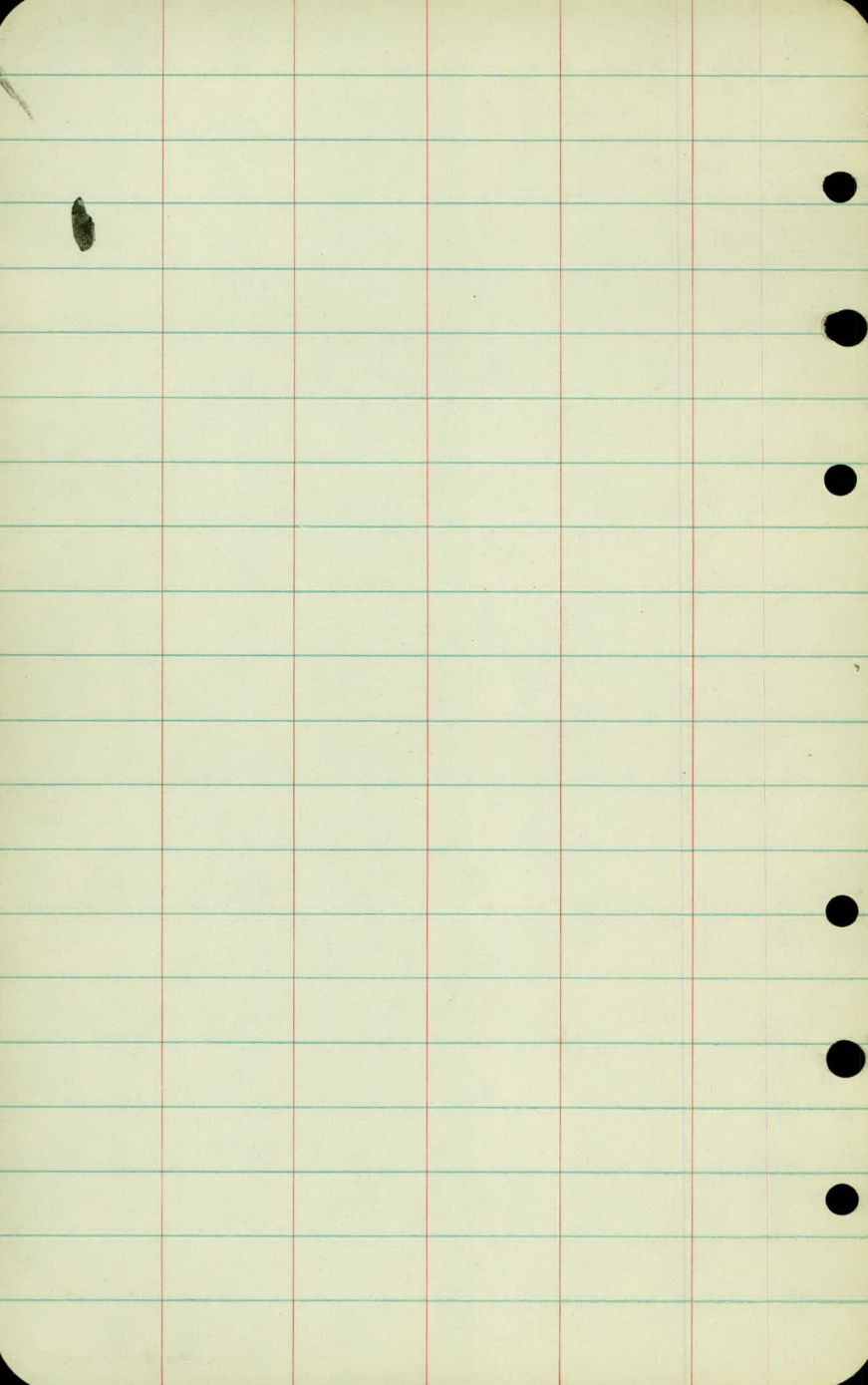
15.9

70.35

16.0

81.95

4.4



¢ Profile

also Profile 70'R+¢Lt.

Sta	+	π	-	Elev
B.M.	5.50	863.39		857.89

0+00

+09

+20

+34

+61

1

+10

+36

+70

2

+50

2-13-50

GB
AM
MB
K.R.

70' Lt

2

105

70' Rt

Top Bottom Step, NE Cor, 1675 McMenamy

61.5	58.6	56.2
1.9	4.8	7.2
	58.5	
	4.9	
	58.5	
	4.9	
	58.6	
	4.8	
	60.1	
	3.3	
55.9	60.9	59.6
7.5	2.5	3.8
	61.0	
	2.4	
	55.4	
	8.0	
	53.4	
	10.0	
	53.6	
	9.8	
56.8	53.6	
4.6		
17	9.8	

Sta	+	π	-	Elev
		863.39		

2+50

+90

3

+50

4

+30

+62

TP	13.27	876.05 [✓]	0.61	862.78 [✓]
----	-------	---------------------	------	---------------------

5

+50

6

TP	12.86	888.38 [✓]	0.53	875.52 [✓]
----	-------	---------------------	------	---------------------

6+10.1

+33

106

70' Lt

2

Rt 70'

59.3

4.1

51.5

11.9

58.7

58.2

55.7

4.7

5.2

7.7

12

57.2

6.2

60.6

58.3

2.8

5.1

63.4

8

58.8

0.0

4.6

10.5

59.1

4.3

58.3

17.8

66.3

9.8

13.0

81.7

10

63.1

69.9

75.6

6.2

15.1

61.0

66.6

9.5

83.2

75.3

5.2

13.1

83.8

80.5

4.6

7.9

19.7

68.7

Sta	+	π	-	Elev
-----	---	-------	---	------

888.38

6+70

7

TP	12.60	900.90	0.08	888.30
----	-------	--------	------	--------

7+00

+30

+48.80 P.O.T.

+75

8+00

TP	13.54	911.98	2.46	898.44
----	-------	--------	------	--------

BM			4.00	907.98
----	--	--	------	--------

8+00

+50

9

70' LT old road cut 2

86.6 88.8 82.2

1.8 10.4 6.2

87.3 82.2

1.1 6.2

16

90.7 92.8

10.2 8.1

96.5

4.4

93.9 94.9 98.4

13.0 6.0 2.5

18

97.1

3.8

18

84.4

16.5

83.4

17.5

Top boat Spt. @ P.Q.T. sta. 7+13.80

Spt in 15' oak, 50' Rt @ Sta 9+10

11.0 98.9 04.1

1.0 13.1 7.9

18

19.1 00.3

11.7

18

13.7 99.5 04.4

11.0 21.5 01.0

11.0

Sta	+	π	-	Elev
		911.98 [✓]		

9+50

0

T.P.	0.99	899.66 [✓]	13.31	898.67 [✓]
------	------	---------------------	-------	---------------------

+50

11

+66

T.P.	0.30	886.78 [✓]	13.18	886.48 [✓]
------	------	---------------------	-------	---------------------

11

+30

T.P.	0.75	874.27 [✓]	13.26	873.52 [✓]
------	------	---------------------	-------	---------------------

+50

+66

12

+50

2-17-50

G.B. M.B.

A.M. BS. 70'

70' 108

Lt

C

Rt

03.6	97.6	04.3	07.7
8.4	14.4	7.7	4.3
05.7	18	93.3	03.0
16.3	18.7	13.7	2.0
	18		
80.1	83.9	87.4	96.5
19.6	15.8	12.3	3.2
	18		
			84.9
			14.8

86.8		
12.9		
77.4	75.3	76.2
9.4	11.5	10.6
	9	
		71.8
		15.0

Profile
old Road Grade

		62.2
		12.1
		7.1
		67.2
		64.5
		57.0
64.1		
10.2	61.5	
10.2	128	17.3
	13	

Sta	+	π	-	Elev
-----	---	-------	---	------

874.27 ✓

T.P.	8.32	869.18 ✓	13.41	860.86 ✓
------	------	----------	-------	----------

12

13

+50

+80

14

+36

+50

15

BM

1.03

868.15 ✓

T.P.	12.89	880.12 ✓	1.95	867.23
------	-------	----------	------	--------

Lt

C

Rt

51.3

12.9

49.6

19.6

52.1

17.10

52.4

14.8

54.5

14.7

56.6

12.6

56.8

12.4

20.622

64.7

4.5

Top WR

284 3.4

60 70

68.7

0.5

62.85

+13.67

70

66.5

2.7

15

66.0

3.2

67.29

1.89 W Rail

67.33

185-ER.

65.7

3.5

45

17.85

+18.67

70

NW cor, SW Long Footing - Ctr. Pier

Note: Elev. Top of Planking = 891.85

25' N. of C Larp. along W edge of Bridge

Sta	+	π	-	Elev
-----	---	-------	---	------

		880.12 [✓]		
--	--	---------------------	--	--

15+50				
-------	--	--	--	--

+63				
-----	--	--	--	--

+71				
-----	--	--	--	--

16				
----	--	--	--	--

+50				
-----	--	--	--	--

17				
----	--	--	--	--

+50				
-----	--	--	--	--

18				
----	--	--	--	--

IP	13.57	893.14 [✓]	0.55	879.57 [✓]
----	-------	---------------------	------	---------------------

18				
----	--	--	--	--

+25				
-----	--	--	--	--

		House		
--	--	-------	--	--

+56				
-----	--	--	--	--

19				
----	--	--	--	--

		House		
--	--	-------	--	--

Lt

Q

Rt

		74.5	
	5.6		↑
		78.5	
	1.6		Under Bridge
		81.1	
	+1.0		↓
68.52		72.7	
top ERail			
11.0	12.1	7.4	72.4
	70		2.7
78.2		71.7	70
1.9		8.4	73.1
70			8.0
		72.7	
	7.4		73.4
		77.2	
77.5		2.9	6.7
2.6			80.7
70			+0.6
3.8	76.3		
70			
	79.6	82.3	
	13.5	10.8	96.9
	18		+2.8
			70
			40
			3.8
			89.3
			67
		87.6	
	5.5		
			40
			3.5
			89.3
			67
95.1			
Ho			91.7
	86.6		
+2.0	4.5	87.9	
75	16	5.2	1.4
			70

Sta	+	π	-	Elev
		893.14 [✓]		

+50

20

+50

21

T.P.	5.70	896.03 [✓]	2.81	890.33 [✓]
------	------	---------------------	------	---------------------

+37

+50

22

+50

+86

¢ Jessie St.

23

97.4

+4.3
70

88.4

4.7

88.5

4.6
70

86.6

6.5

95.0

+1.9
70

88.2

4.9
18

86.5

6.6

92.6

0.50

89.5

3.6

88.7

4.4
18

88.2

4.9

91.1

2.0

$$\begin{array}{r} \text{cor Gov.} \\ 6.9 \\ \hline 52 \end{array}$$

89.1

87.7

8.3

89.2

6.8

88.9

7.1
18

88.2

2.8

89.9

6.1

87.8

8.2

90.2

5.8

90.0

6.0
100

89.3

6.7
50

89.6

6.4
17

87.9

8.1

6.4 89.6

17

7.7 88.3

94.3

1.7
70

Sta

+

π

-

Elev

896.03[✓]

23+50

24

+50

25

T.P. 4.56 897.01[✓] 3.58 892.45[✓]

+43

+75

+87

26

+12.40

Profile Edgerton

+50

27

L+

E

R+

83.0

89.5

86.9

94.7

13.0

4.5

9.1

1.3

70

16

20

82.4

89.8

87.3

91.6

13.6

6.2

8.7

4.4

17

90.4

87.6

90.8

5.6

8.4

5.2

9.1

16

98.7

92.7

16.9

5.1

7.3

3.3

9.5

16

90.9

95.5

12.5

5.5

6.1

1.5

82.6

15

94.5

97.9

14.4

2.5

+ 0.9

92.6

0.9

4.4

92.9

9.1

93.0

94.24

96.1

86.4

88.1

89.64

91.36

10.60

8.90

7.37

5.65

4.03

2.77

0.95

200

150

100

50

93.4

50

100

5.65

3.6

94.8

2.2

Sta	+	π	-	Elev
-----	---	-------	---	------

		897.01		
--	--	--------	--	--

27+50				
-------	--	--	--	--

BM				
----	--	--	--	--

	0.45	896.56		
--	------	--------	--	--

			896.59	
--	--	--	--------	--

Lt

Z

Rt

96.3

0.7

Top Hyd, S.W. cor. Larpenteur & Edgerton

Sta

+

万

capitulum

Elev.

Larpenleur Ave

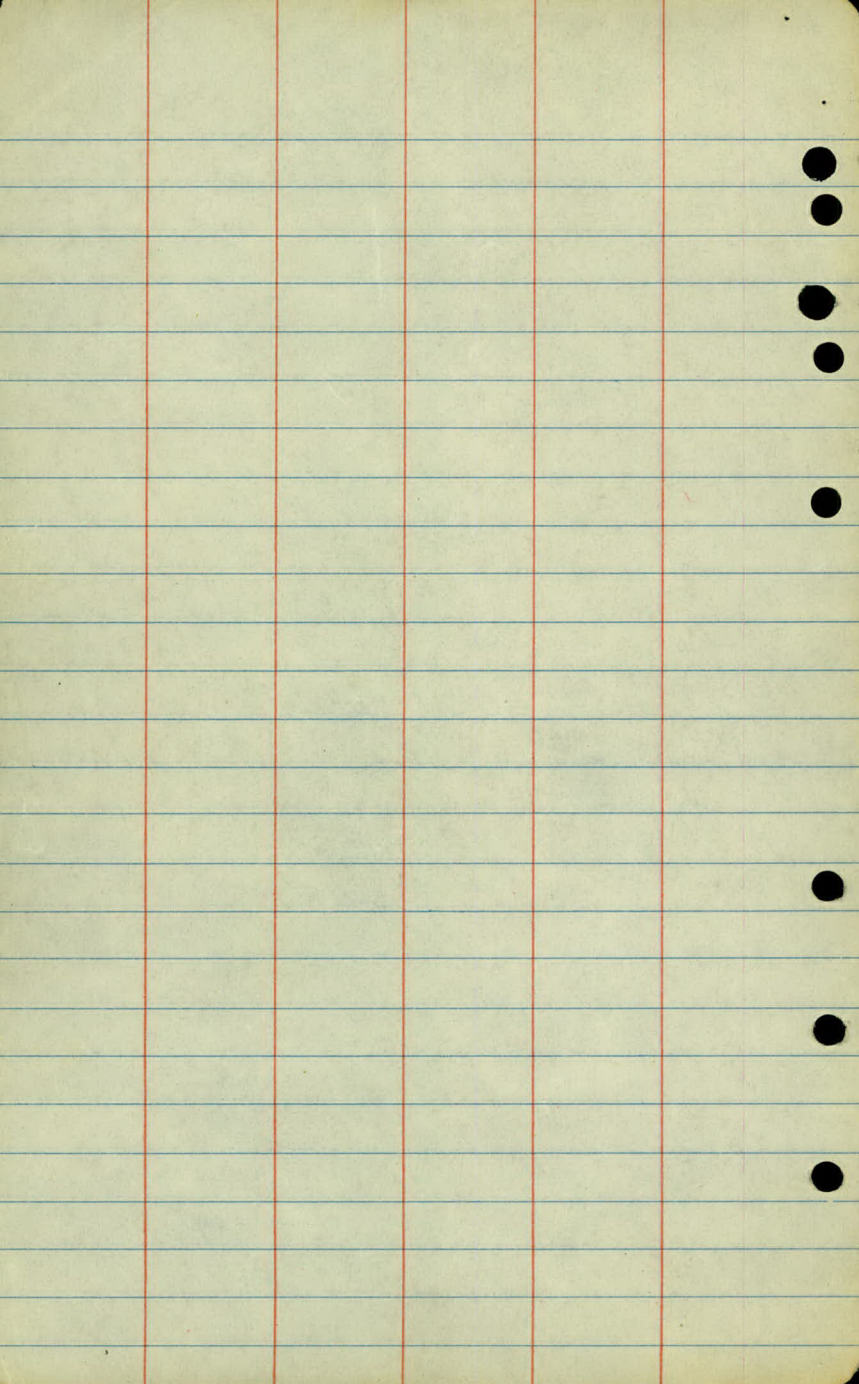
McMenamy St. to Edgerton St

Alignment & Profile

INDEX	PAGE	
Alignment	1 to 3	
X sections	3 to 19	
"	34 - 62	
Topography	20 - 33A	
Edgewart St. Xsec.	63 - 65	Feb - 1950
Arkwright St.	66 - 69	GB
De Soto St. Line? change	78 - 92	AM MB K.R.

W. Brown
Aug 66 85

REC.
2-17-50
K.A.



Alignment

Sta Pt. Alt. A Rt.

1514.90 P.O.T. ϕ Soo Line track.

13+06.20 P.O.T.

9+86.23 P.O.T.

7+48.80 P.O.T.

5+00 P.O.T.

0+00 P.I. ϕ McMenamy

2-10-50

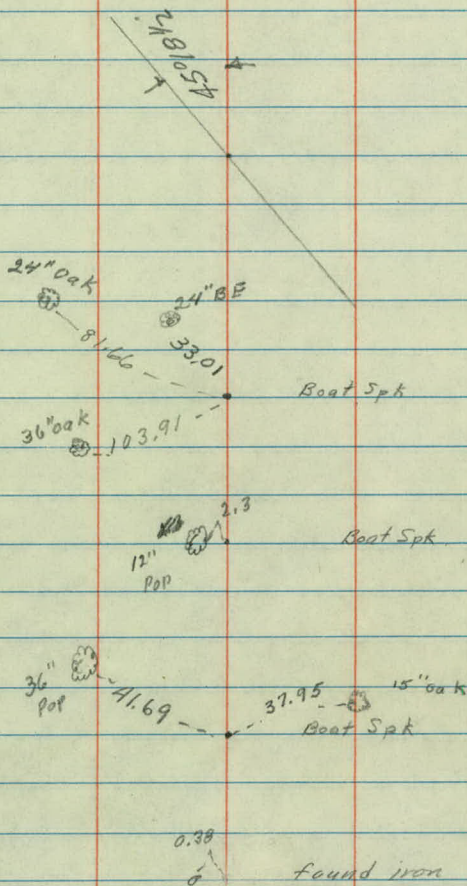
GB.

AM.

MB.

BC.

2



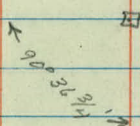
$89^\circ 34 \frac{1}{4}' \rightarrow$

$\swarrow$ SW cor sec 17

W 1/4 cor sec 17

26+12⁴⁰ PI ♀ Edgerton

1560.31 POT ♀ Bridge



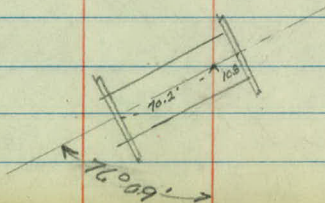
Stadia Road Location

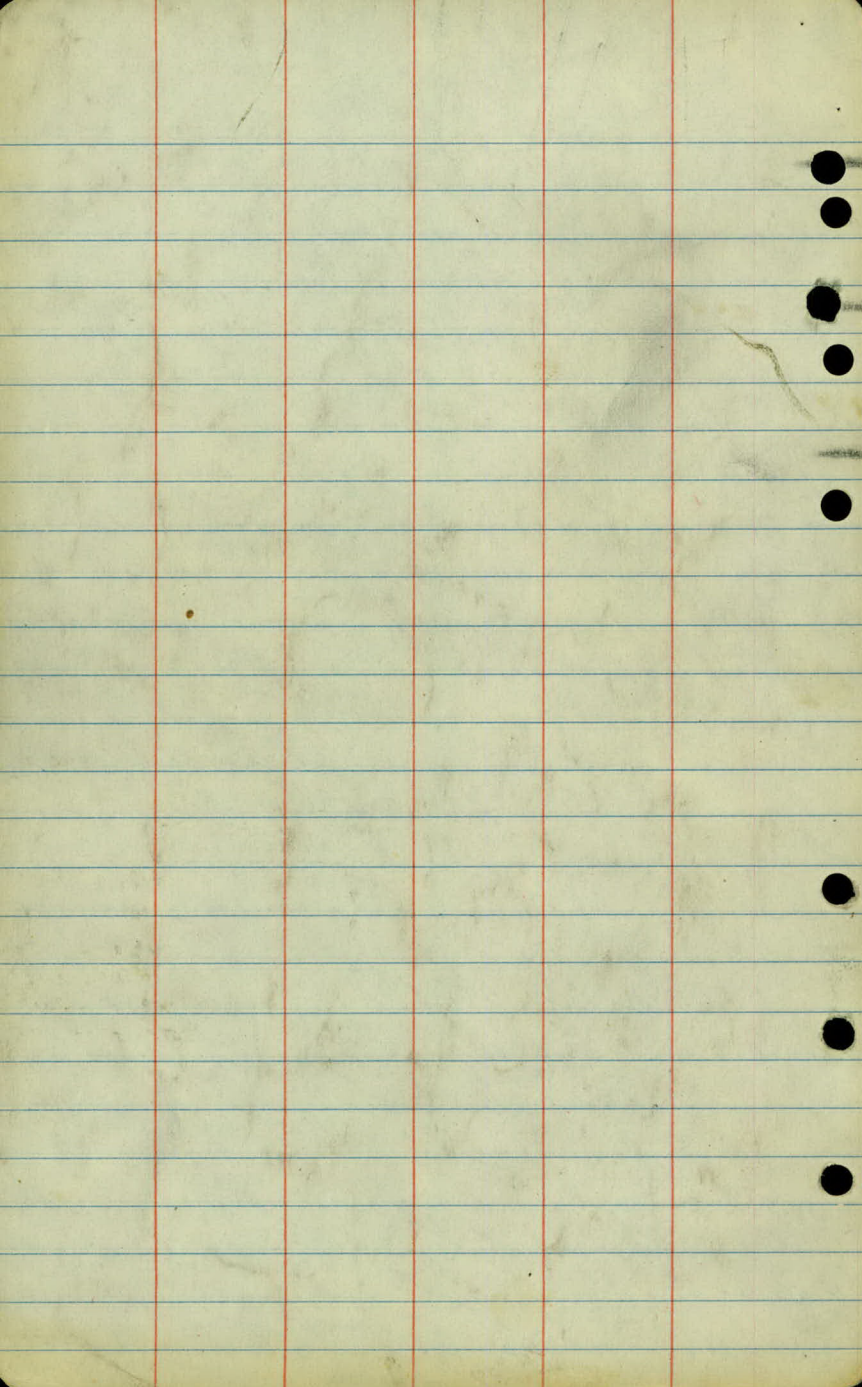
Az Dist

Then See Line @ Bridge

To POT Sta. 9+86.32 - 90°00'

∅ Rd	162°00' - 92'
"	167°40' - 186'
"	169°00' - 287'
"	354°20' - 65'
"	040°40' - 142'
"	40°50' - 208'
"	356°45' - 305'



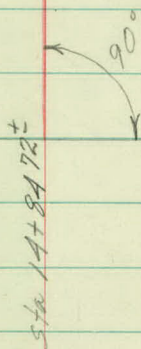


FK
JM
RG

May 18, 1956
Fair Windy

Larpenteur Ave., McMenamy St. to
De Soto St.

RR Lot 1 Borrow Pit



Sta + π - Elev

BM 12.99 881.14

868.15

0+00

0+27.5 No Rail

+58

May 18, 1956

14

RT

2

Top W. Cor. Center Pier Bridge

65.5

15.6

✓

68.5

65.6

66.2

66.92

12.6
39

15.5
20

14.9
16

14.22
N. Rail

W-R/W
3'

76.9

80.1

84.0

4.2
49

1.0
54

12.9
61

87.0

86.4

+5.9
65

+5.3
61

Shoulder

77.0

73.5

69.7

66.2

65.1

65.1

66.1

4.1
18

7.6
16

11.4
9

14.9

16.0
9.3
W-R/W

16.0
16

15.0
20

78.1

76.2

81.0

85.7

3.0
26

4.9
39

0.1
52

+4.6
62

Shoulder

66.52
146.2
27
S-Rail

✓

Sta + π - Elev

881.14

0+80

✓

1

✓

✓

+30

May 18, 1956

14

RT

76.3
4.8
41

76.3
4.8
26

76.6
4.5
10

78.0
3.1

74.5
6.6
10

70.6
10.5
13.0
W-R/W

66.3
14.8
26

77.5
3.6
48

80.9
0.2
54

84.4
+3.3
61

shoulder

66.26
14.88
47

S-Rail

64.9
16.2
37

✓

77.4
3.7
47

76.3
4.8
41

76.4
4.7
29

76.5
4.6
11

77.4
3.7

77.5
3.6
10

77.2
1.9
14.5
W-R/W

80.0
1.1
18

75.0
6.1
30

80.4
0.7
52

82.5
+1.4
55

64.7
16.4
50

65.9
15.2
42

71.8
9.3
31

65.7
15.4
59

66.1
15.0
66

S-Rail

✓

80.6
-0.5
46

77.5
3.6
37

76.9
4.2
24

76.9
4.2
12

76.8
4.3

77.4
3.7
26

77.0
4.1
18.0
W-R/W

79.4
1.7
35

78.7
2.4
41

✓

81.2
+0.1
50

shoulder

Sta + π - Elev
881.14

+30

✓

TP 10.41 883.87 7.68 873.46

+65

✓

2

May 18, 1954

14

RF

4

74.8	70.1	63.9	63.9
6.3	11.0	17.2	17.7
51	62	75	82

65.64
15.50
96
39

81.0	79.1	77.6	77.2	76.6	77.3	80.3	78.2
2.9	4.8	6.3	6.7	7.3	6.6	3.6	5.7
41	35	14		13.1	33	42	51

Shoulder W-RW

66.8	69.2	72.6	74.8
17.1	14.7	11.3	9.1
82	71	65	59

80.3	78.1	77.4	77.3	76.5	77.7	81.2	77.6
3.6	5.8	6.5	6.6	7.4	6.2	2.7	6.3
31	22	5.7		23	36	46	63

W-R/W

81.9	82.1	67.3	71.9	72.9
2.0	1.8	16.6	12.0	11.0
37	44	89	79	71

Shoulder

Sta + π - Elev

883.87

2135

+70

+86.3 S.P.L. Ref 1

5
32
32

TP 2.25 870.47

1245

870.42

May 18, 1956

82.8	80.6	78.5	77.4	76.1	75.7	78.2	76.6
1.1	3.3	5.4	6.5	7.8	8.2	5.7	7.3
42	25.6	12		18	38	47	68

82.8						67.1	71.1
1.1						16.8	12.8
46						95	84

Shoulder

84.2	83.4	81.5	79.6	78.5	76.7	74.5	71.9
+0.3	0.5	2.4	4.3	5.4	7.2	9.4	12.0
52	39	25	11		15	38	66

67.9	69.6
16.0	14.3
100	82

83.4	81.8	79.7	78.2	77.4	77.3	75.8	74.9	74.0
0.5	2.1	4.2	5.7	6.5	6.6	8.1	9.0	9.9
52.2	43	30	15		14	30	50	74

85.0							
+1.1							
59							

Shoulder

74.9	75.2	73.5
9.0	8.7	10.4
100	91	84

73.3	67.6
10.6	16.3
118	141

870.47

1+65

2

✓

+ 35

✓

+ 70

May 18, 1956

14

RT

63.3	62.6	63.5	65.26
7.2	7.9	7.0	5.21
100	111	127	133

S Rail

62.1	58.6	58.6	61.4
8.4	11.9	11.9	9.1
100	109	124	134

64.37	62.8	61.6
610	7.7	8.9
164	156	145

S Rail

65.2	59.7	58.4	57.1
5.3	10.8	12.1	13.4
100	117	143	182

63.92	62.1
6.55	8.4
200	191

S Rail

65.2	61.7	58.6	56.6
5.3	8.8	11.9	13.9
118	135	146	172

61.5	56.2	55.6
9.0	14.3	14.9
221	203	195

Sta + π - Elev

870.47

2+70

2+86.3

✓

✓

BM

2.30

868.17

868.15

May 18, 1956

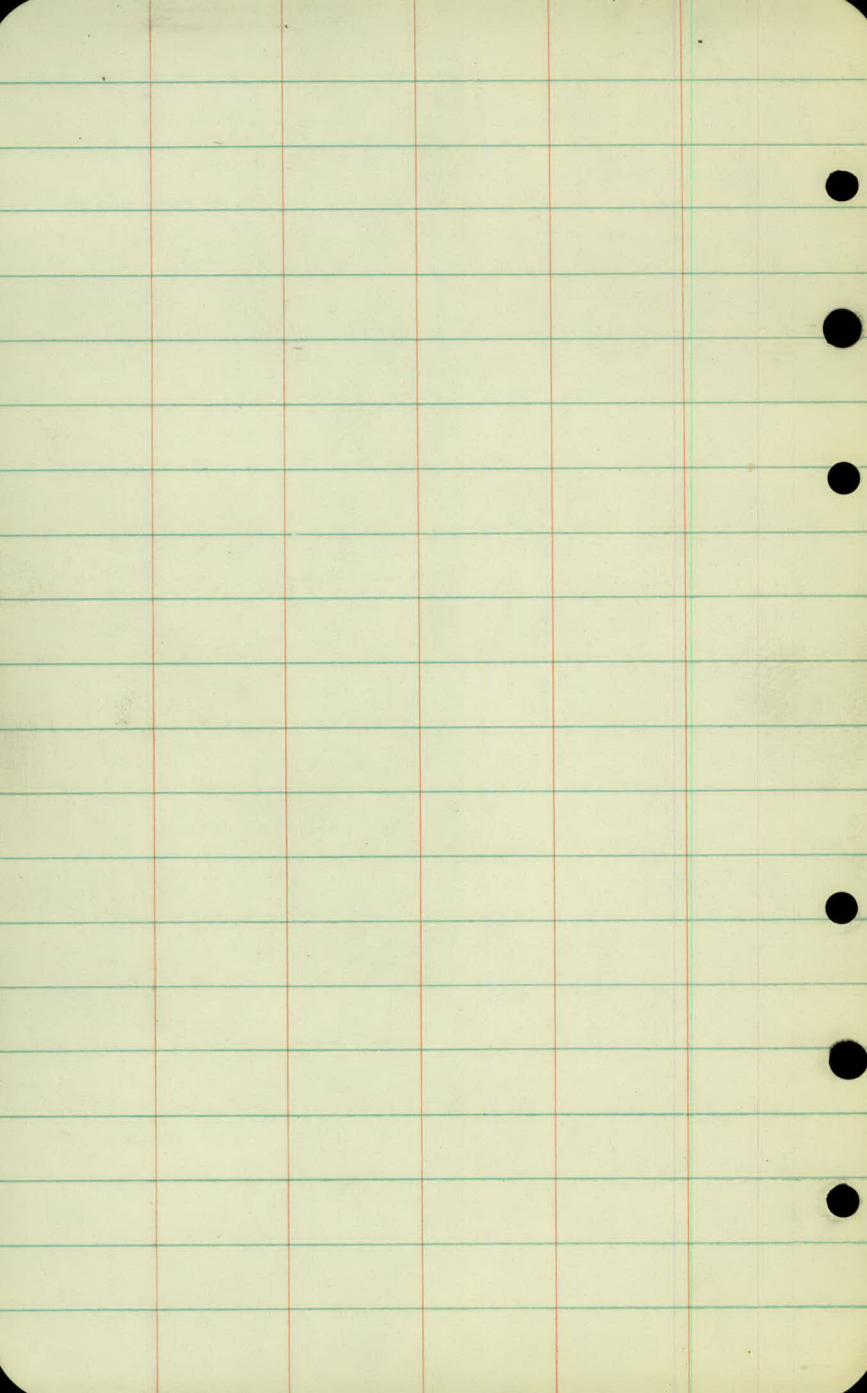
1st

RT

7

62.6	63.51	
7.9	6.96	
231	234	✓
	5-Rail	
63.51	59.2	56.0
7.0	11.3	14.5
154	165	177
61.5	55.5	55.6
9.0	15.0	14.9
237	220	200
62.8	63.30	
7.7	7.17	✓
243	247	

Top W. Cor Footing Center Pier Bridge



1
Larpenleur
McMenemy to Edgerton

X-sections

not used - 9-16-59

R.C.

Sta + π - Elev

BM 4.28 865.01

(860.73)

0+00

+18

+38

+50

/

✓

FX
KP
JH
HA

£ March 31, 1959

2

LT

RT

Top Hyd SW Cor Carpenter & McMenemy

61.0	60.0	59.5	59.1	58.1	57.4
4.0	5.0	5.5	5.9	6.9	7.6
50	25	10	✓	25	50

61.0	60.1	59.8	59.3	58.8	57.7	57.1	56.4
4.0	4.3	5.2	5.7	6.2	7.3	7.9	8.6
50	42	19	17	✓	21	34	50

61.2	60.0	60.1	59.7	59.3	59.2	58.9	58.3	58.0	57.3	57.3	57.0
3.8	5.0	4.9	5.3	5.7	5.8	6.1	6.7	7.0	5.7	5.7	6.0
039	32	21	17	11	✓	9	14	17	25	50	

61.5	60.0	60.0	59.7	59.7	59.2	58.9	58.1	57.2	57.2	57.5	57.5
3.5	5.0	5.0	5.3	5.8	5.8	6.1	6.9	5.8	5.8	5.5	5.5
50	39	29	21	17	11	✓	15	18	25	37	50

59.8	59.4	59.2	59.3	59.2	58.7	58.5	58.0	57.2	60.0
5.2	5.6	5.8	5.7	5.8	6.3	6.5	6.0	5.8	5.0
40	29	17	11		10	15	17	28	31

59.9	61.0
5.14	4.02
41	50
Ent	

60.0	60.0
5.0	5.0
50	45

Sta	+	π	-	Elev
-----	---	-------	---	------

Sta	+	π	-	Elev
		865.01		

Sta	+	π	-	Elev
1+50				

Sta	+	π	-	Elev
✓				

Sta	+	π	-	Elev
2				

Sta	+	π	-	Elev
+50				

Sta	+	π	-	Elev
3				

Sta	+	π	-	Elev
✓				

2 March 31, 1959

3

LT

RA

58.6	60.0	59.7	59.4	60.6	59.6	59.2	58.9	59.2	59.6	59.5
6.4	5.0	5.3	5.6	5.4	5.4	5.8	6.1	5.8	5.4	5.5
40	35	19	16	11		9	15	24	35	50

58.6	59.3	59.3
6.4	5.7	5.7
41	45	50

✓

61.6	60.3	60.2	59.6	59.8	59.9	59.6	59.2	60.0	59.7	59.5
3.4	4.7	4.8	5.4	5.2	5.1	5.4	5.8	5.0	5.3	5.5
50	36	21	17	10		10	16	22	32	50

✓

63.9	60.8	60.4	59.9	60.1	60.2	59.9	59.6	60.3	60.5	59.2
1.1	4.2	4.6	5.1	4.9	4.8	5.1	5.4	4.7	4.5	5.8
50	37	22	16	10		10	17	21	35	50

✓

60.0	60.9	60.4	60.5	60.6	60.4	60.2	60.1	59.7
4.95	4.1	4.6	4.5	4.4	4.6	4.8	4.9	5.27
28	23	16	9		11	16	25	CB
CB								28

61.5	63.0	63.6
3.5	2.0	1.4
33	44	50

✓

56.3	60.2	61.3	61.4
8.7	4.8	3.7	3.6
50	42	38	31

Sta	+	π	-	Elev
		865.01		

3+43

✓

+58

✓

+89

✓

TP	8.46	870.94	2.53	862.48
----	------	--------	------	--------

Lt

March 31, 1959 4

Rt

62.6	61.8	60.9	60.9	61.1	60.9	60.4	61.3	61.7
24	32	41	41	39	41	46	37	33
37	26	17	8		7	17	23	33

 63.4

→ 1.6
50

✓

56.5	61.5
8.5	3.5
50	39

62.3	61.7	61.3	61.1	61.2	61.1	60.7	61.6	61.8
2.70	3.3	3.7	3.9	3.8	3.9	4.3	3.5	3.2
C	G	20	11		8	18	22	31
29								

62.3	62.8	62.9	63.4		59.6	61.8
27	2.20	2.1	1.60		54	3.2
G	C	G	C		50	40
40		50				

62.9	62.5	62.0	61.7	61.6	61.5	61.3	61.7	60.7
2.10	2.5	3.0	3.3	3.4	3.5	3.7	3.3	4.3
G	G	24	15		9	14	23	35
33								

62.8	63.3	63.3	63.8		60.1
22	1.70	1.7	1.21		49
G	C	G	C		50
40		50			

Sta + π - Elev

870.94

4

✓

+50

✓

5

March 31, 1959

5

LT

RT

63.2	62.8	62.0	61.9	61.9	61.8	61.5	62.0	61.5
78	82	90	91	91	92	95	90	95
37	25	15	10		9	15	23	32

63.9

✓

60.1

71
50

10.9
50

63.7	63.2	62.7	62.8	62.9	62.7	62.5	63.0	63.4
73	78	83	82	81	83	85	80	76
39	28	15	8		10	14	23	33

✓

61.8

62.9

65.2
5.8
45

65.5
5.5
50

9.2
50

8.1
46

64.7	64.4	63.9	63.9	64.0	63.9	63.5	64.2	64.6
63	66	71	71	70	71	75	68	64
35	25	15	8		10	15	20	30

✓

65.3

69.7

59.5

64.6

5.7
41

1.3
50

11.5
50

6.4
40

Sta + K - Elev.

870.94

5+50

✓

BM 8.03 876.78 2.19 868.75

6

✓

+50

✓

FK
HP
JH

March 31, 1959
April 1, 1959
RT 6

LT

66.2	65.8	65.0	65.4	66.4	65.2	64.9	65.6	65.9
4.8	5.2	6.0	5.6	5.6	5.8	6.1	5.4	5.1
28	19	11	9		9	14	23	34

66.6	66.9	69.8		64.3	65.6
4.4	4.1	1.2		6.7	5.4
36	42	50		50	41

Spike in PP LT sta 5 + 70

67.4	67.0	66.7	66.8	66.9	66.8	66.4	66.9	67.2
9.4	9.8	10.1	10.0	9.9	10.0	10.4	9.9	9.6
29	18	16	8		6	14	19	39

68.8	71.4			67.3
8.0	5.4			9.5
44	50			50

67.6	69.5	68.8	68.2	68.4	68.5	68.2	67.8	68.6	68.8
3.2	7.3	8.0	8.6	8.4	8.3	8.6	9.0	8.2	8.0
50	39	24	15	9		9	15	18	36

68.5
8.3
50

Sta + π - Elev.

876.78

6+89

7

✓

+48

+50

✓

4 April 1, 1959

7

Lt.

Rt.

69.2

762

Ch. CB

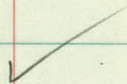
16

70.4	69.8	69.8	70.1	70.3	70.0	69.5	69.5	70.5
6.4	7.0	7.0	6.7	6.5	6.8	7.3	7.3	6.3
22	15	14	8		12	14	16	19

72.0

76.3

→ 4.8 0.5
39 50



70.2

70.5

6.6 6.3
50 38

71.1

5.70

Ch. G.B.

16

72.8	72.2	71.4	71.9	72.0	71.8	71.5	71.5	72.0
4.0	4.6	5.4	4.9	4.8	5.0	5.3	5.3	4.8
38	21	17	11		10	12	16	19

72.5

→ 3.3
50



71.8

72.5

5.0 4.3
50 36

Sta	+	π	-	Elev
		876.78		

7+67	Carb Line			
------	-----------	--	--	--

✓

+97	Carb Line			
-----	-----------	--	--	--

✓

TP	13.35	887.08	3.05	873.73
----	-------	--------	------	--------

8			13.3	
---	--	--	------	--

+12				
-----	--	--	--	--

+12				
-----	--	--	--	--

April 1, 1959

8

LT

RT

72.9	72.5	72.3	72.6	72.6	72.3	72.2	72.9	73.1
3.9	4.3	4.5	4.2	4.2	4.5	4.6	3.9	3.7
G	20	15	9		9	16	19	36
42								

73.4	73.2	73.6		72.5
3.40	3.6	3.15		4.3
C	G	C		50
42		50		

73.8	73.4	73.3	73.6	73.6	73.6	73.2	73.2	73.7
2.97	3.4	3.5	3.2	3.2	3.2	3.6	3.2	3.1
C	G	14	8		8	16	26	44
36								

73.7	74.2		73.6
3.1	2.59		32
G	C		50
Carb	50		

74.1	73.7	74.2	74.2	74.0	73.4	74.1
13.0	13.4	12.9	12.9	13.1	13.7	13.0
19	15	5		8	16	17

74.1	74.4		74.7	74.7
13.0	12.7		12.4	12.4
39	50		50	35

Sta + π - Elev

887.08

8+50

✓

9

✓

+50

± April 6, 1959

9

11

BT

75.7

75.3

75.6

75.7

75.4

75.0

75.8

11.4

11.8

11.5

11.4

11.7

12.1

11.3

18

16

8

6

15

18

76.0

77.0

81.1

✓

77.9

76.0

11.1

10.1

6.0

9.2

11.1

29

38

50

50

28

78.4

77.5

77.2

77.4

77.6

77.3

77.1

77.8

8.7

9.6

9.9

9.7

9.5

9.8

10.0

9.3

37

17

15

8

8

16

18

82.9

✓

80.0

78.6

77.7

4.2

50

7.1

8.5

9.4

50

41

27

79.8

79.3

79.0

79.1

79.3

79.0

78.6

79.3

79.9

7.3

7.8

8.1

8.0

7.8

8.1

8.5

7.8

7.2

27

17

16

8

9

16

18

40

80.5

81.0

84.3

81.9

6.6

6.1

2.8

5.2

37

40

50

✓

50

Sta + π - Elev

887.08

10

✓

+50

✓

11

✓

TP 11.19 895.89 2.38 884.70

April 1, 1959 10

Lt

Rt

82.0	81.4	80.6	81.0	81.2	80.9	80.5	81.1	81.9
5.1	5.7	6.5	6.1	5.9	6.2	6.6	6.0	5.2
28	17	16	8		8	17	18	40

82.4 85.4
 → 4.7 1.7
 37 50



83.7
 3.4
 50

83.7	83.1	82.4	82.7	83.0	82.9	82.3	83.1	83.5
3.4	4.0	4.7	4.4	4.1	4.2	4.8	4.0	3.6
30	17	15	7		7	17	19	38

83.6
 → 3.5
 50



85.4
 1.7
 50

85.5	84.7	84.1	84.5	84.7	84.5	84.2	85.0	85.3
1.6	2.4	3.0	2.6	2.4	2.6	2.9	2.1	1.8
35	18	16	7		9	16	17	35

85.1 84.6
 → 2.0 2.5
 46 50



83.7 85.5
 3.4 1.6
 50 43

Sta + π - Elev

895.89

11+50

✓

12

✓

+50

Lt

April 1, 1959

BH

11

86.8

85.9

86.3

86.4

86.2

85.8

86.8

9.1
1710.0
159.6
7

9.5

9.7
810.1
169.1
17

87.1

85.8

83.2

✓

88.7

86.9

87.3

→ 8.8
3210.1
3612.7
50

SS

13.2
419.0
348.6
29

88.9

88.6

87.7

88.0

88.2

88.0

87.3

88.3

89.3

→ 7.0
287.3
188.2
157.9
8

7.7

7.9
78.6
167.6
186.6
29

84.5

83.5

✓

84.2

89.0

→ 11.4
4612.4
50

SS

11.7
436.9
35

90.7

90.0

89.2

89.5

89.7

89.6

88.9

89.9

90.5

→ 5.2
295.9
176.7
156.4
8

6.2

6.3
77.0
166.0
185.4
26

88.7

84.1

85.7

90.6

→ 7.2
3411.8
50

✓

SS

10.7
455.3
36

Sta + π - Elev

895.89

13

✓

+50

✓

TP 5.14 897.94 3.09 892.80

+75

✓

2 April 1, 1939 12

LT

RT

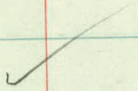
92.0	91.5	90.4	90.6	90.7	90.4	89.9	90.7	91.2
3.9	4.4	5.5	5.3	5.2	5.5	6.0	5.2	4.7
30	18	15	9		10	17	19	35

86.4

85.9

→ 9.5
38

10.0
44



93.0	92.4	91.4	91.5	91.7	91.6	91.2	91.9	92.2
2.9	3.5	4.5	4.4	4.2	4.3	4.7	4.0	3.7
25	19	16	9		8	17	19	34

93.0

88.5

82.2

91.1

→ 2.9
33

7.4
40

8.7
42

4.8
37



93.9	93.6	92.0	92.2	92.4	92.1	91.7	92.4	92.6
4.0	4.3	5.9	5.7	5.5	5.8	6.2	5.5	5.3
42	25	18	11		7	16	18	35

90.4

87.7

→ 7.5
47

10.2
43



sta	+	π	-	Elev
-----	---	-------	---	------

897.94

14

BM	4.40	898.72	3.62	894.32	894.34
----	------	--------	------	--------	--------

16+00

+20

+50

✓

17

TP	2.41	895.82	5.31	893.41
----	------	--------	------	--------

4 April 1, 1959 13

21

RT

94.1	94.2	92.2	92.9	92.8	92.6	93.0	93.2	88.3
38	3.7	5.7	5.0	5.1	5.3	4.9	4.7	9.6
50	40	29	13	✓ 13	21	32	42	
BM Plate on Bridge #7231								

93.0	93.1	94.2	93.9	93.3	99.4
5.7	5.6	4.5	4.8	5.4	9.3
5	5	21	29	36	
Abutment					

85.2	90.5	93.4	94.3	94.5	93.7	93.4	88.5
135	8.2	5.3	4.4	4.2	5.0	5.3	10.2
45	29	19	7	✓	20	33	40

94.3	94.0	94.0	93.7	93.2	92.5	92.9	92.6
4.4	4.7	4.7	5.0	5.5	6.2	5.8	6.1
29	24	14		14	24	26	33

94.2	89.0		88.3
→ 4.5	9.7		10.4
38	47		39

89.9	92.5	92.6	91.9	92.1	92.5	92.4	92.0	92.7	92.6	88.0
8.8	6.2	6.1	6.8	6.6	6.2	6.3	6.7	6.0	6.1	10.7
37	27	23	15		10	24	26	32	40	

Sta + π - Elev

895.82

17+55

✓

18

✓

+50

✓

4 April 1959 14

LT

BT

91.2

90.3

90.9

91.1

91.1

91.0

91.5

91.2

4.6

5.5

4.9

4.7

4.7

4.8

4.3

4.6

24

22

11

10

22

23

30

91.2

85.4

✓

85.3

4.6

10.4

10.5

33

41

38

90.3

90.8

89.5

89.8

89.9

89.7

89.5

90.3

90.0

5.5

5.0

6.3

6.0

5.9

6.1

6.3

5.5

5.8

33

24

20

12

8

15

18

22

88.0

7.8

37

✓

91.5

89.5

87.5

4.3

6.3

8.3

50

40

28

89.3

89.7

89.5

88.5

88.9

88.8

88.7

88.5

89.3

90.8

93.5

6.5

6.1

6.3

7.3

6.9

7.0

7.1

7.3

6.5

5.0

2.3

33

31

23

20

12

9

14

18

27

50

89.0

85.0

✓

6.8

10.8

45

50

Sta + π - Elev

895.82

19

✓

+50

✓

+98 ^{L4} Top C.B. Cover 31.5 8.45

20

✓

TP 6.24 893.57 8.49 887.33

± April 1, 1959 15

LT

RI

88.5	88.5	87.8	88.2	88.3	88.0	87.7	88.4	89.7
7.3	7.3	8.0	7.6	7.5	7.8	8.1	7.4	6.1
34	26	20	11		8	15	20	34

89.4

→ 6.4
40

✓

89.8

90.3

6.0 5.5
50 47

88.3	88.3	87.5	87.6	88.0	87.5	87.3	87.6	87.9
7.5	7.5	8.3	8.2	7.8	8.3	8.5	8.2	7.9
30	24	20	12		9	17	23	30

89.0

89.1

→ 6.8 6.7
39 50

✓

87.5

87.4

8.3 8.4
50 47

87.2	86.6	87.0	87.3	87.4	87.1	86.9	86.9	86.7	87.4
8.6	7.2	8.8	8.5	8.4	8.7	8.9	8.9	9.1	8.4
31	30	19	10		9	16	24	29	Top

Ch. Covg.
31.5

88.3

90.8

→ 7.5 5.0
40 50

✓

87.2

87.4

8.6 8.4
50 40

Sta + π - Elev

893.57

20+50

✓

21

✓

+50

22

April 1, 1959

16

LT

RT

88.4	88.1	87.8	87.3	87.4	87.2	87.0	87.5	87.8
5.2	5.5	5.8	6.3	6.2	6.4	6.6	6.1	5.8
38	27	19	17		11	16	19	31

82.3
→ 1.3
50

✓

89.9 89.4 88.2
3.7 4.2 5.4
50 45 42

89.2	88.5	87.6	87.6	87.3	87.2	88.0	88.2
4.4	5.1	6.0	6.0	6.3	6.4	5.6	5.4
50	24	15		10	15	18	39

✓

89.5 88.9
4.1 4.7
50 41

88.9	88.9	88.6	88.0	87.8	87.4	88.2	88.5	89.1
4.7	4.7	5.0	5.6	5.8	6.2	5.4	5.1	4.5
48	28	18	16		15	19	28	50

✓

89.6	89.0	88.6	87.9	88.1	87.9	88.5	88.9	89.2	90.0
4.0	4.6	5.0	5.7	5.5	5.7	5.1	4.7	4.4	3.6
50	32	17	16		16	19	32	44	50

✓

Sta + π - Elev

893.57

22+50

T.P. 6.99 896.16 4.40 889.17

+73

✓

23

+13

✓

FK
KP
HA
JH

LT

2 April 1959 17
April 2, 1959
BT

89.9 89.4 88.7 88.2 88.4 88.6 88.2 88.6 89.1
3.7 4.2 4.9 5.4 5.2 5.0 5.4 5.0 4.5 Under
50 33 17 15 7 15 18 32 Const
S.E. Cor Walk Landing ✓

88.9 88.8 88.4 88.6 88.8 88.6 88.3 89.1 89.4
7.3 7.4 7.8 7.6 7.4 7.6 7.9 7.1 6.8
29 20 16 8 8 15 20 25
89.2 89.3 89.9 89.9
7.0 6.9 4.3 5.3
40 50 50 35

89.0 89.1 88.8 88.5 89.0 89.0 88.8 88.5 89.3 89.5 89.1
7.2 7.1 7.4 7.7 7.2 7.2 7.4 7.7 6.9 5.7 4.1
50 37 29 17 9 8 14 21 34 50

89.6 89.2 88.7 88.9 89.1 88.9 88.7 89.5 89.5
6.6 7.0 7.5 7.3 7.1 7.3 7.5 6.7 5.7
21 18 15 8 8 14 21 32
89.4 89.4 89.8 89.8
6.8 6.8 10.4 4.4
32 42 50 50

Sta + π - Elev

896.16

23+50

✓

24

✓

+50

TP 3.09 897.34 1.91 894.25

FK
KP
JH
HA

April 2, 1959 18
April 3, 1959
RT

LT

89.8	89.6	89.0	89.2	89.3	89.2	89.2	89.9	90.6
6.4	6.6	7.2	7.0	6.9	7.0	7.0	6.3	5.6
29	16	15	8		8	14	18	32

89.8
→ 6.4
42

85.3
10.9
50



91.8
4.4
50

90.7	90.1	89.5	89.7	89.9	89.8	89.7	90.2	91.4
5.5	5.8	6.7	6.5	6.3	6.4	6.5	6.0	4.8
22	17	14	7		7	15	18	40

90.5
→ 5.7
35

90.2
6.0
43

86.8
9.4
50



91.8
4.4
50

91.8	91.6	90.3	90.1	90.5	90.1	90.2	90.8	91.7
4.4	4.6	5.9	5.8	5.7	5.8	6.0	5.4	4.5
25	19	14	9		7	14	20	32



91.5
→ 4.7
34

90.8
5.4
43

89.6
6.6
50

90.7
3.5
50

Sta + π - Elev

897.34

25+00

✓

+50

✓

+81 W. P. L. Edgerton

✓

April 3, 1959
 Overcast Windy 39° 19
 ft.

LT

92.3	91.7	90.9	91.1	91.2	91.1	90.8	92.1	92.3
5.0	5.6	6.4	6.2	6.1	6.2	6.5	5.2	5.0
21	17	14	7		8	15	20	29

92.4	91.9	92.2
4.9	5.4	5.1
32	39	50

95.1	94.4	92.7
2.2	2.9	4.6
50	42	34

92.7	92.7	91.5	91.6	91.9	91.9	91.7	92.8	93.2
4.6	4.6	5.8	5.7	5.4	5.4	5.6	4.5	4.1
31	21	15	8		8	16	21	32

92.6	92.4
4.7	4.9
40	50

92.8	94.8
0.5	2.5
50	40

92.8	92.0	92.1	92.3	92.4	92.4	92.3	93.0	93.3
4.5	5.3	5.2	5.0	4.9	4.9	5.0	4.3	4.0
33	22	17	9		7	14	19	26

92.3	91.2
5.0	6.1
40	50

94.5	94.2	93.7
2.78	3.09	3.6
50	40	34
Walk		

Sta + π - Elev

897.34

26

+02.4 Edge

+ $\pm$ Edgerton 4.16

BM 0.66 896.68 (896.59)

BM 2.70 897.04 (894.34)

T.P. 0.93 894.37 3.60 893.44

T.P. 4.76 892.14 6.99 887.38

T.P. 6.39 895.60 2.93 889.21

T.P. 2.54 896.82 1.32 894.28

0.10 896.72

April 3, 1959

20

LT

RT

61	91.2	91.2	91.4	92.1	92.6	92.9	92.9	93.0	93.3	93.5
6.1	5.9	5.2	4.7	4.4	4.4	4.3	4.0	3.8		
50	41	34	24	13		9	21	36	50	

✓

91.3	91.8	92.4	92.7	93.0	93.1	93.3	93.5	93.8
6.0	5.5	4.9	4.6	4.3	4.2	4.0	3.8	3.5
50	36	21	9		12	25	38	50

✓

Top Hyd S.W. Cor Larp + Edgerton
BM Plate on Bridge #7231

