

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

Mc KNIGHT

From Carver To Highwood

Road Acc't. No. _____

Date Filed 1-10-61

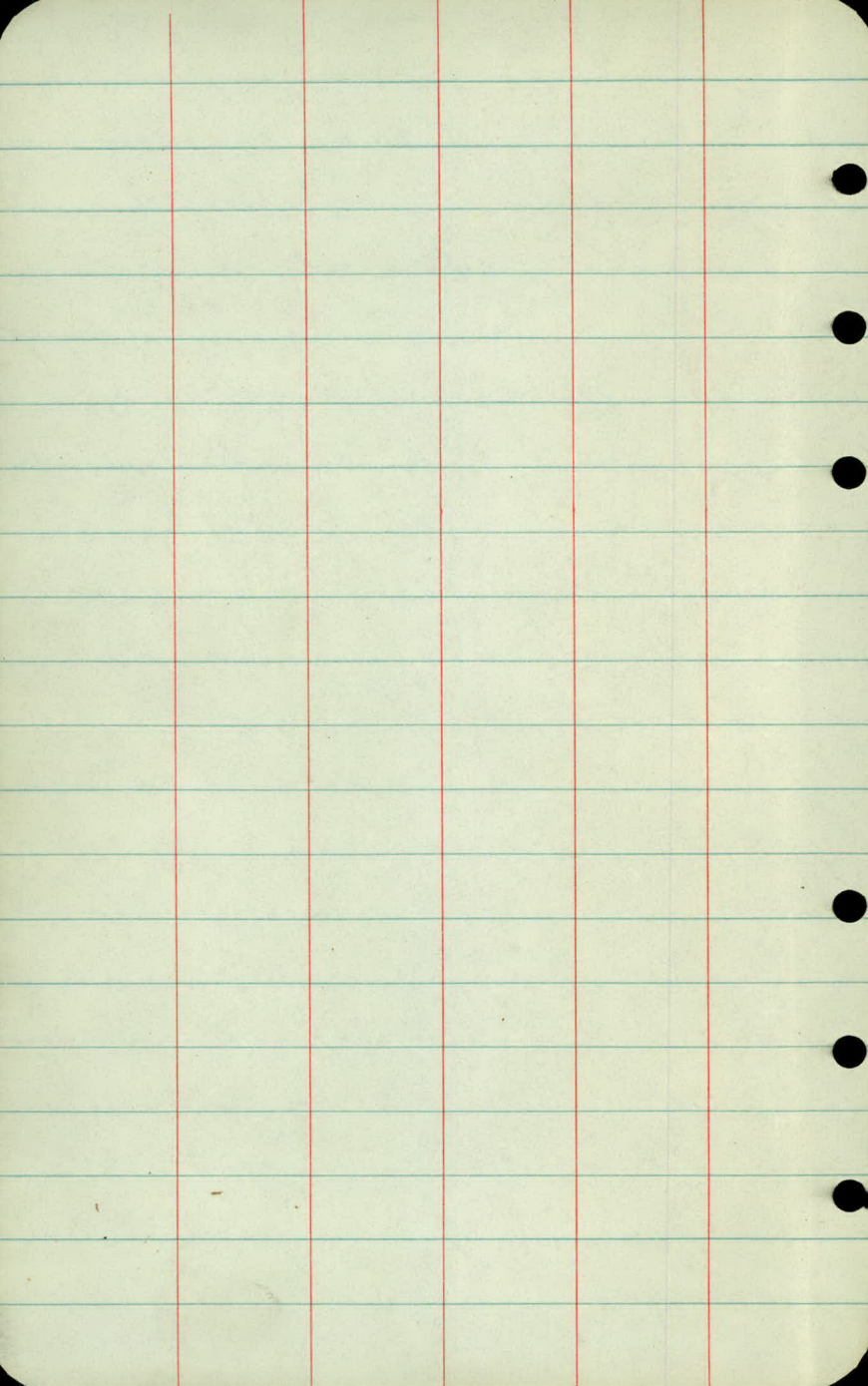
Dr 9
File Book 27

1
Mc KNIGHT

Carver Ave to Highwood

Plan Survey

Rec: 2/8/60



FK
RG
KP
LC
XJ
JS

Dec 11, 1959

2

Fog 36°

Alinément

Sta Point ΔL ΔR

26+08.97 P.O.T.

15+36.25 P.O.T.

13+00.86 P.I. $0^{\circ}05'30''$
 $0^{\circ}02'45''$

0+00 $\pm$ Carver Ave.

Jan 20, 1960

3

Disk
2" P. X

27.34

4" P.
Disk X

85.30

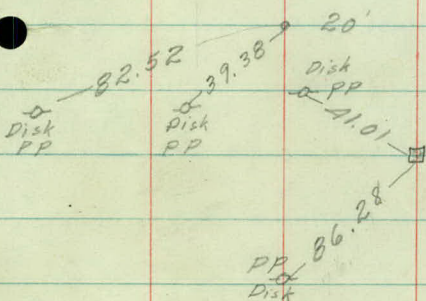


49.59

Disk
8

NW. Cor SA 1/4
SW 1/4

10" Sec 13-28-22
Mont



NW Cor Sec 24-28-22
Mont

Iron



32.2

32.2



34.1



Iron

28.48

PP

Boat Spike

Sta Point ΔL ΔR

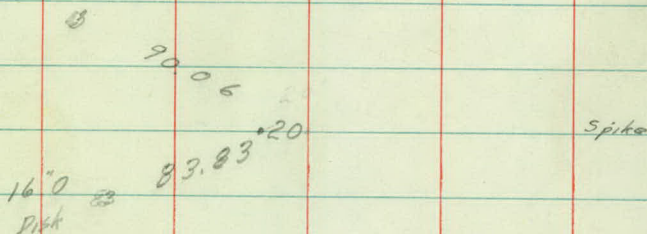
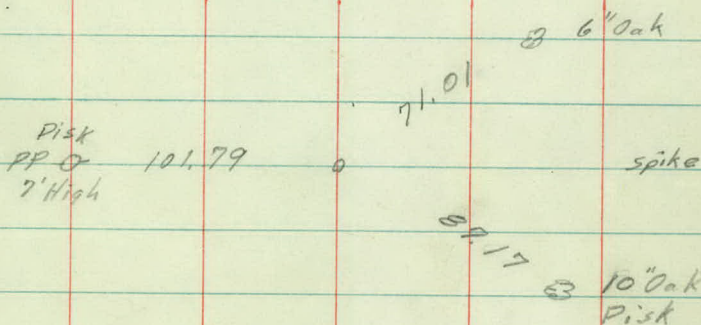
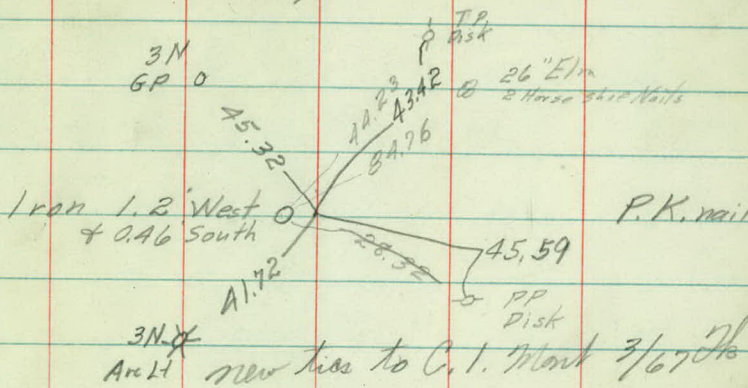
39+17.08 W $\frac{1}{4}$ Cor Sec 13 $\pm$ Highway

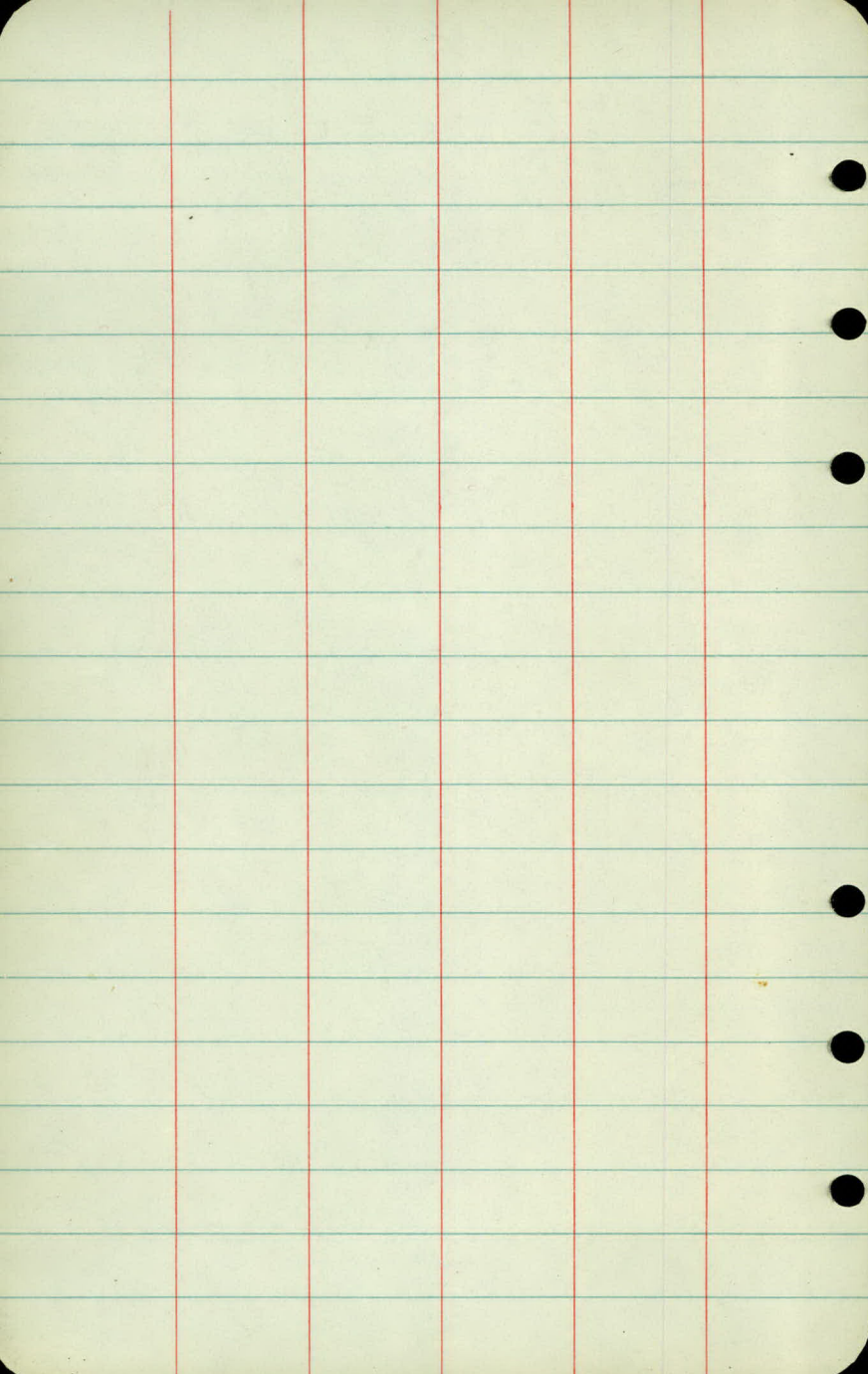
32+00 P.O.T.

29+23.47 20' @

Jan. 20, 1960

4





20 Jan 1960

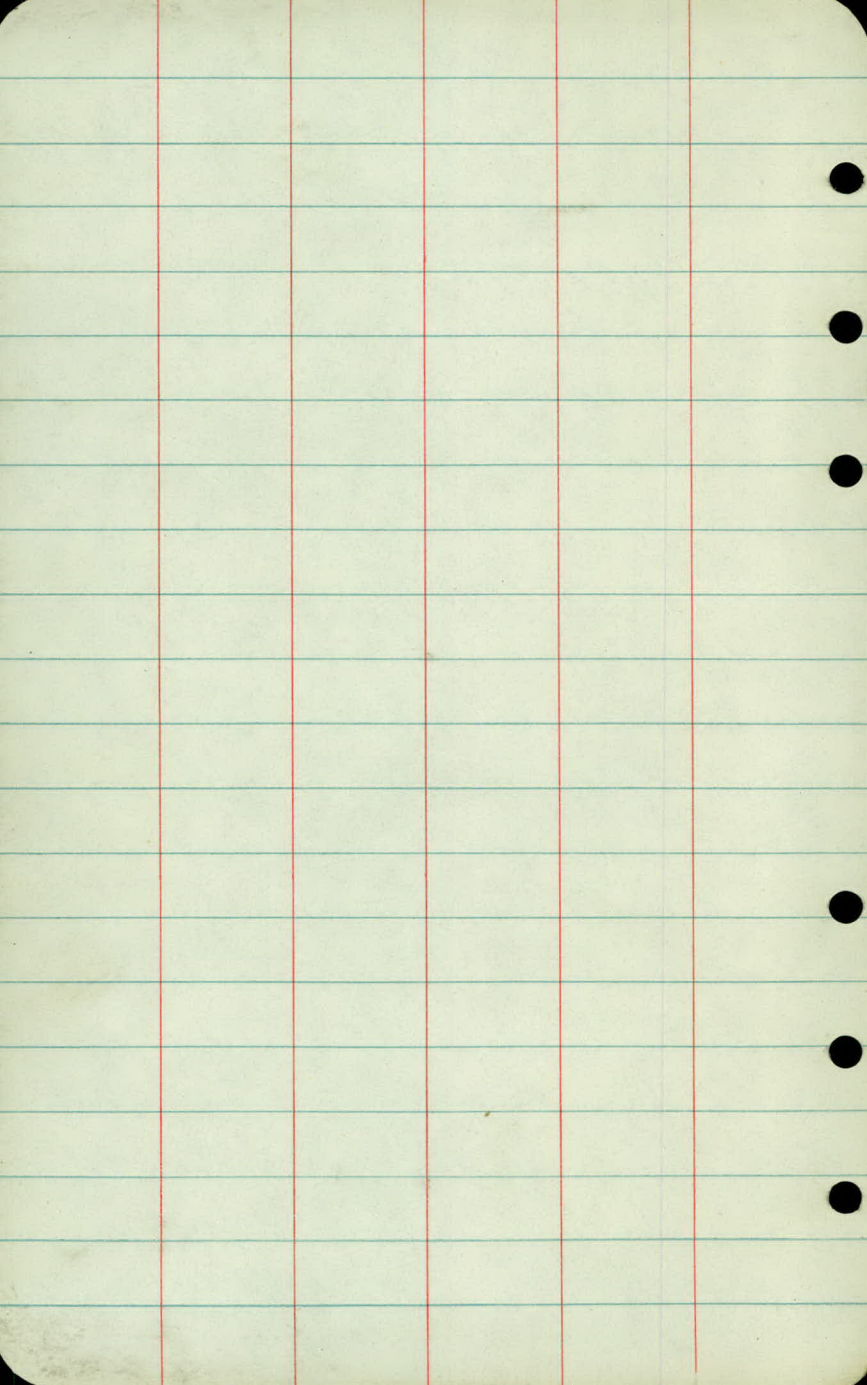
5

□ N.W. COR SEC 24-28-22
mont.

1300.86

• £ Carrer Ave

□ W 1/4 COR SEC 24-28-22



Topography

5	Lt	±	± Trail 21	Rt Road 42-54
+85	ER 71			+75 Road 25+35
+73	ER 71	+73 Road 30	+50 Road 15+±	13+22
4			Road 4+14	+23 PP 22
				+76 12" Cont 41
			Rt Ho Ent Rt	
			+30 PP 21	+52 ± to Ent 40
3			Road 4+14	+26 8" E 31
				+94 12" E 31
			+61 12" E 30	+90 PP 21
				+87 Cor. Cult. 35
				+11 10" E 21
			Road 0+11	
2				+88 End Rows Shrub 63 67 72
+80	12" B 66	+86 14" E 31		
	SE Co. Ho			
+55	8 1/2" E 31	+58 PP 19		
+55	6" E 31	+70 ± Ent 11		
+57	12" W 46	+41 10" E 65		
1		Road 38		
	+22 6" E 32			+35 Cor. Cult 35
				+62 8" E 29
+91	4" E 33			+84 8" E 29
	+59 6" E 34			+33 ER 7
+24	Sp 35	+40 ER 6	+25 PP 16	+32 14" E 57
0	+12 BR 28	+12 Edge BT ±	+12 BR 31	+39 14" E 57
		-11 Edge BT ±		Begin S Roads 63-68 872

FA
RG Same
JS
CW
JH

Jan 21, 1960
Jan 22, 1960 Rt

7

Marillac Ln

I-S-F



Cultivated

Nursery

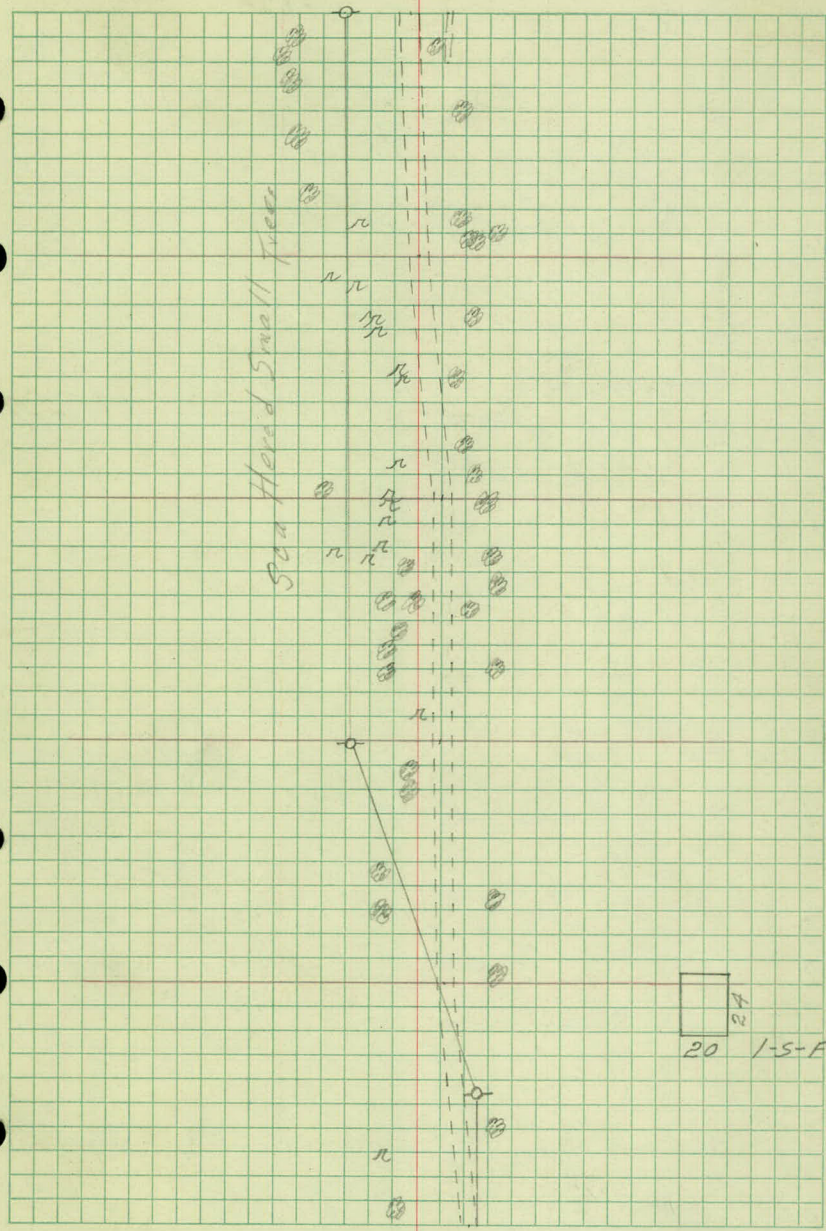
Carver Ave.

	LT	£	RT
10	+100 $\frac{PP}{31}$	Trail $\frac{4}{4}$	W. Out $\frac{12}{12}$
	+90 $\frac{5"BE}{33}$		+80 $\frac{Begin Washout}{12}$
+73 $\frac{6"BE}{53}$		+82 $\frac{4"BE}{57}$	+88 $\frac{4"Coll}{6}$
	+49 $\frac{6"BE}{51}$		+100 $\frac{14"BE}{19}$
+27 $\frac{Tr 4"BE}{46}$		+14 $\frac{STP}{25}$	+10 $\frac{6"BE}{32}$
9		Trail $\frac{£}{£}$	+16 $\frac{12"Phon}{18}$
+76 $\frac{STP}{20}$	+88 $\frac{STP}{27}$		+106 $\frac{8"BE}{25}$
+153 $\frac{STP}{8}$	+69 $\frac{STP}{18}$		+109 $\frac{STP}{23}$
	+49 $\frac{STP}{7}$		+74 $\frac{28"Coll}{23}$
+103 $\frac{4"BE}{40}$		+14 $\frac{STP}{9}$	+23 $\frac{6"BE}{20}$
8	+100 $\frac{STP}{11}$		+10 $\frac{6"BE}{24}$
+93 $\frac{STP}{13}$	+81 $\frac{STP}{16}$	+97 $\frac{STP}{13}$	+99 $\frac{8"BE}{28}$
+75 $\frac{STP}{20}$	+77 $\frac{STP}{25}$	+72 $\frac{6"BE}{6}$	+78 $\frac{6"BE}{31}$
+60 $\frac{6"BE}{13}$	+58 $\frac{8"BE}{£}$	+44 $\frac{4"BE}{8}$	+56 $\frac{6"BE}{22}$
+11 $\frac{STP}{£}$	+29 $\frac{8"BE}{12}$	+39 $\frac{6"BE}{12}$	+30 $\frac{6"E}{34}$
7			+100 $\frac{£ Trail}{10}$
	+99 $\frac{PP}{28}$		+36 $\frac{10"E}{33}$
+87 $\frac{Tr 6"BE}{1}$			
	+80 $\frac{14"O}{2}$		
+44 $\frac{8"BE}{14}$			+104 $\frac{10"E}{33}$
6	+29 $\frac{Tr 4"BE}{16}$		+100 $\frac{£ Trail}{11}$
			+79 $\frac{SW Cor Ho}{110.5}$
+29 $\frac{STP}{16}$			+54 $\frac{PP}{25}$
			+41 $\frac{8"E}{33}$
	+107 $\frac{Tr 14"BE}{8}$		
5			

Jan 22, 1960

Rt 8

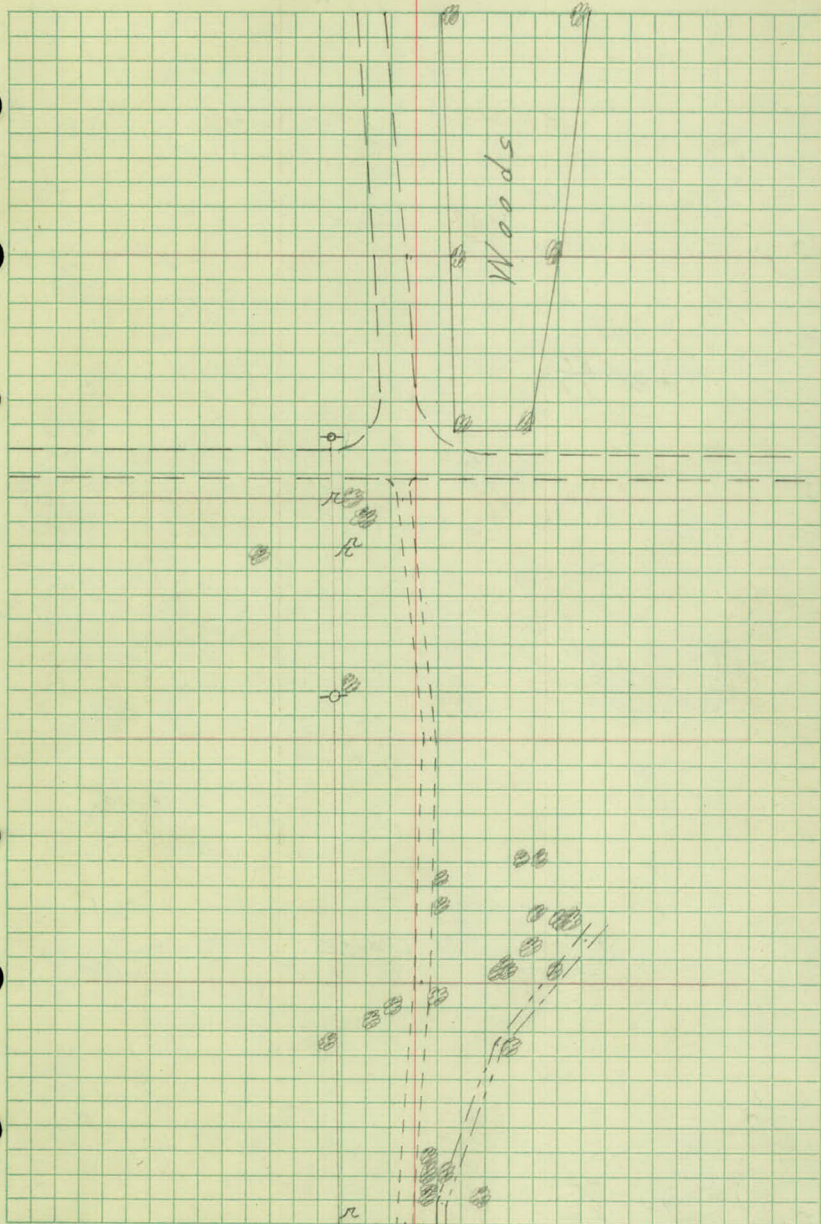
Sea Hored Small Trees



20 1-S-F

15	24	Road 24+13	Woods 12+92	RT
14		Road 17+4	Woods 15+61	
			+46 ER 2	+28 B. Wood 16-48
+44 ER 14				+18 BR 31
	+25 RP 34	+08 Edge Rb 2		
+20 BR 34		+00 Trail 5		
13	+00 16" C 26	+00 STP 24		
19A 6" C 20				
+79 STP 30	+94 8" C 18	+82 STP 27		
	+23 16" BE 28			
+77 6" C 66		+18 RP 33		
12		Trail 6		
		+44 10" C 12	+51 5-8" b 45	+51 2-6" o 51
		+28 2-8" o 6.1	+29 Tw 100 51	+32 6" C 12
		+07 6" o 28	+16 3-12" o 28	+18 2" Mat 7
		+28 8" o 65	+03 12" o 51	+04 3-6" Oak 25
		Trail 3		+05 12" b 38
11			+96 4" C 9	
		+74 12" C 40		+75 4" Wash out 35
	+90 18" C 9		+28 2-6" C 6	
+76 4" C 35		+85 10" C 18	+21 10" C 14	+09 W. Out 12
			+11 4" C 5	+22 4-4" C 6
10	+06 STP 27		+12 4" C 5	+12 3-6" o 27

9

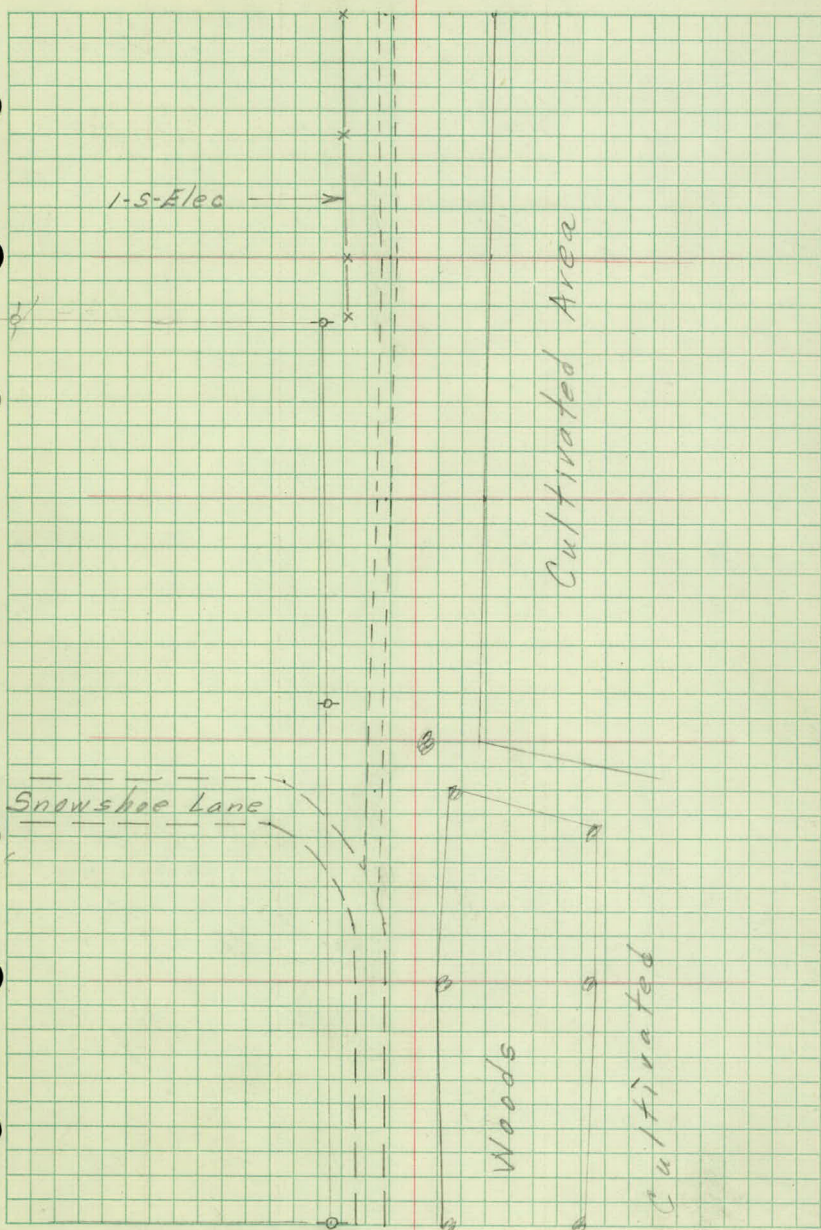


17

Jan 22, 1960

Rt

10



25

$$\begin{array}{r} \text{Lt Fe} \\ 43 \end{array} \quad \begin{array}{r} \text{Woods} \\ 7 \end{array}$$

£

Rt

24

$$\begin{array}{r} \text{Fe} \\ 44 \end{array} \quad \begin{array}{r} \text{Woods} \\ 5 \end{array}$$

$$+60 \quad \begin{array}{r} 10^{\text{th}} \text{E} \\ 62 \end{array}$$

23

$$\begin{array}{r} \text{Fe} \\ 43 \end{array} \quad \begin{array}{r} \text{Woods} \\ 3 \end{array}$$

$$+83 \quad \begin{array}{r} \text{Fe Cor} \\ 44 \end{array}$$

$$+70 \quad \begin{array}{r} \text{Fe Trail} \\ \text{Lt} \end{array}$$

$$+40 \quad \begin{array}{r} \text{Fe Trail} \\ 20 \end{array} \quad \begin{array}{r} \text{Lin Fe} \\ 135 \end{array} \quad \begin{array}{r} \\ 34 \end{array}$$

22

$$\begin{array}{r} \text{Woods} \\ 2 \end{array} \quad \begin{array}{r} \text{Fe} \\ 32 \end{array} \quad \begin{array}{r} \text{Fe Trail} \\ 15 \end{array}$$

$$+51 \quad \begin{array}{r} \text{B. Woods} \\ 2 \end{array}$$

$$+32 \quad \begin{array}{r} \text{End Cult} \\ 25 \end{array}$$

21

$$\begin{array}{r} \text{Fe} \\ 32 \end{array} \quad \begin{array}{r} \text{Fe Trail} \\ 14 \end{array} \quad \begin{array}{r} \text{Cult} \\ 26 \end{array}$$

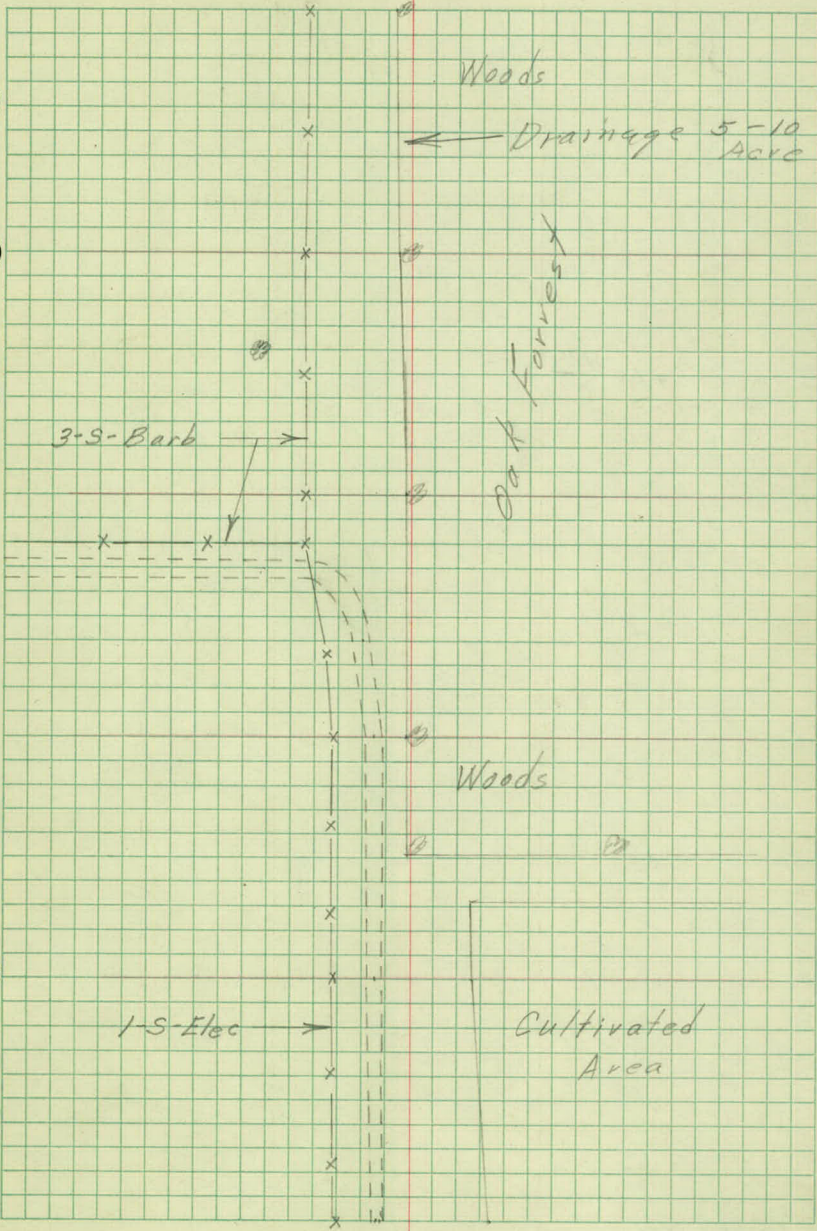
20

Lt

2 Jan 22, 1960

Bt

11



Lt

£

Rt.

30

+68 $\frac{10^0}{44}$ +94 $\frac{Cor. Nursery}{55}$ +96 $\frac{14^0}{38}$ +78 $\frac{6^0}{4}$

+42 $\frac{£ Ent}{101}$ +35 $\frac{£ Ent}{61}$ +45 $\frac{Woods}{18}$ +58 $\frac{Cor. Woods}{47}$

+27 $\frac{16^0}{105}$ +16 $\frac{£ Ent}{43}$ +75 $\frac{Cor. Woods}{15}$

+89 $\frac{6^0}{2}$ +20 $\frac{8^0}{80}$

+29 $\frac{£ Ent L Woods Cult}{59}$ 11 59 66

+94 $\frac{Woods}{20}$ +70 $\frac{Woods}{34}$ 28

+41 $\frac{Cor. Pine}{103}$ +91 $\frac{£ Ent}{86}$

+30 $\frac{Cor. Pines}{39}$

28 $\frac{Pines}{38}$ $\frac{Woods}{7}$ $\frac{Cult}{17}$ 24

+42 $\frac{Fe Cor}{16}$ +47 $\frac{R. T. L}{Folt}$

27 $\frac{Pines}{37}$ $\frac{Fe}{18}$ $\frac{Woods}{10}$ $\frac{Cult}{13}$ 20

+32 $\frac{Cor. Pines}{37}$

+36 $\frac{£ Fe}{22}$ +29 $\frac{Cor. Cult}{19}$

+036 +11 $\frac{13 Trees}{20-81}$ +16 $\frac{Woods}{11}$ +16 $\frac{Cor. Woods}{9}$

26 $\frac{Fe}{26}$ $\frac{Woods}{20}$

+79 $\frac{£ Woods}{6}$

+53 $\frac{8^0 Cult}{33}$ +68 $\frac{4 Cult}{30}$

+32 $\frac{Fe Cor}{43}$

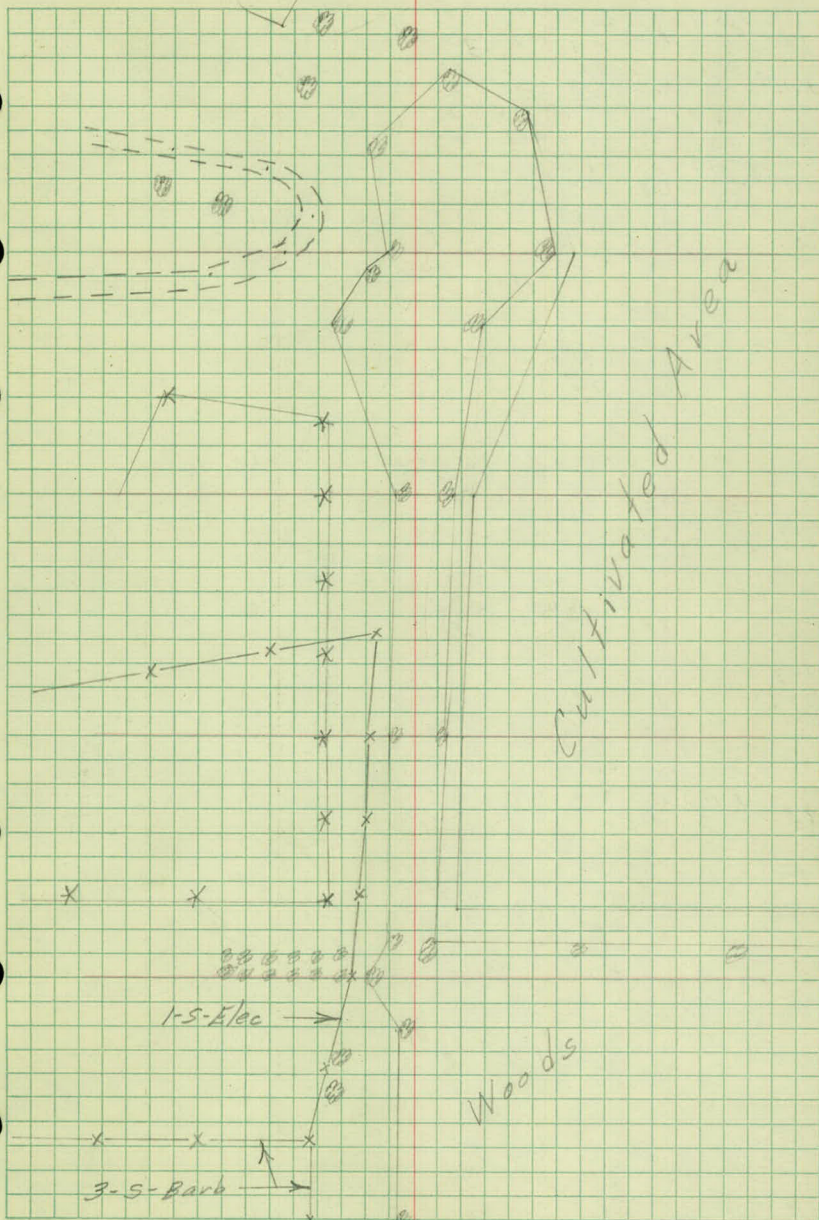
25

11

Jan 22, 1960

BT

12



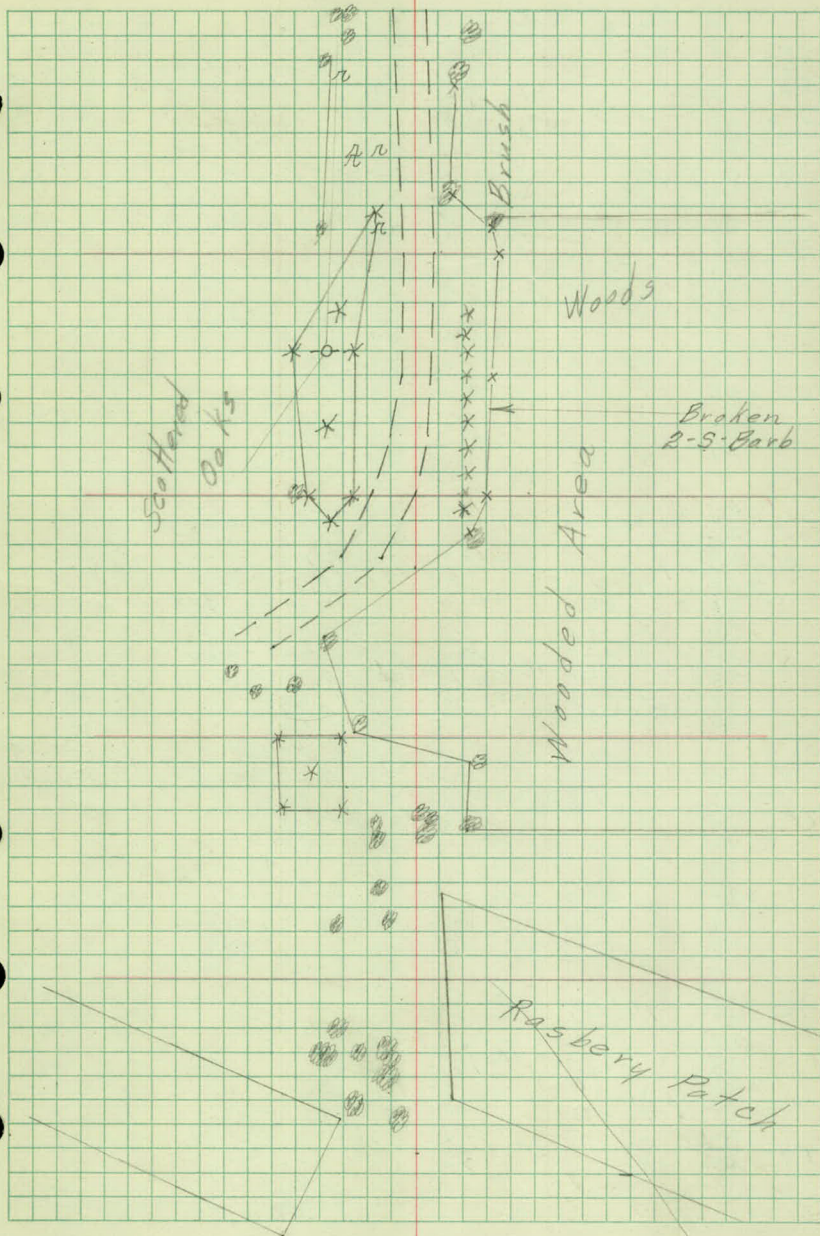
LT	Rd	RT
35	8 5	
+80 37	+90 24	+70 17
+42 26	+42 16	+76 18
+09 38	+36 29	+24 16
+99 8 0	+17 17	+12 31
34	+11 16	+15 28
	+50 5-7	+76 22
	+59 38	+25 10-5
+01 50	+60 24	
33	+44 26	+30 30
+89 35	+75 31	+85 23
+98 59	+48 67	+67 2
+20 14 0	+42 38	+27 77
+19 6 0	+02 25	+70 20
32	+100 30-57	
+64 7 0	+77 36-50	+61 22
	+57 16	+67 4
+38 8 0	+24 10 0	+90 24
31	+23 33	+69 6 0
+67 38	+69 8 0	+36 11
+67 6 0	+80 33	
	+59 12	
+47 26	+43 18 0	
30	+42 31	+28 90

Lt

± Jan 22, 1960

R1

13



LT

Z

RT

	+59 $\frac{ER}{15}$	+63 $\frac{ER}{9}$	+56 $\frac{TP}{20}$
	+29 $\frac{E.BT}{R+L}$	+58 $\frac{R.H.}{Fc}$	+55 $\frac{Fc}{T}$
+29 $\frac{BR}{51}$	+08 $\frac{Begin BT}{\#}$	+29 $\frac{B.R.}{42}$	
	+01 $\frac{12" CM \times Drain}{16 \frac{13}{14}}$		
39	+08 $\frac{ER}{28}$	+08 $\frac{ER}{21}$	
	+90 $\frac{BR}{9}$	+92 $\frac{2" P}{20}$	+97 $\frac{PP}{205}$
	+73 $\frac{Tw 10" C}{39}$	+91 $\frac{BR}{7}$	+89 $\frac{2" Pine}{18}$
+44 $\frac{14" O}{45}$		+36 $\frac{\# Ent}{19}$	+83 $\frac{2" Pine}{18}$
		+90 $\frac{Cor Culv}{24}$	
	+14 $\frac{14" O}{51}$	+87 $\frac{Ent}{27}$	+34 $\frac{Culv}{34}$
38	+63 $\frac{16" O}{32}$	+87 $\frac{14" O}{39}$	+70 $\frac{Cor Culv}{61}$
+39 $\frac{16" O}{48}$	+40 $\frac{16" O}{56}$	+42 $\frac{12" O}{35}$	+47 $\frac{5" E}{17}$
+28 $\frac{12" O}{53}$	+24 $\frac{18" O}{49}$	+32 $\frac{4" O}{35}$	+27 $\frac{6" E}{16}$
+10 $\frac{PP}{27}$	+74 $\frac{ERR}{15}$	+13 $\frac{18" O}{36}$	+01 $\frac{Cor Barn}{AA}$
37	+03 $\frac{8" O}{14}$	+03 $\frac{Road}{6-8}$	+00 $\frac{4" E}{44}$
+87 $\frac{8" O}{10}$	+97 $\frac{RTie}{Barn}$	+52 $\frac{10" Coll}{55}$	+81 $\frac{8" BE}{50}$
+97 $\frac{B.R. Prior}{20}$	+82 $\frac{6" O}{36}$	+72 $\frac{Fc Cor}{20}$	+62 $\frac{\# Ent}{10}$
+75 $\frac{4" O}{21}$		+62 $\frac{4" Coll}{19}$	+62 $\frac{2" E}{19}$
+02 $\frac{\# Ditch}{200}$	+31 $\frac{10" O}{74}$	+50 $\frac{RTie}{Fc}$	+46 $\frac{10" Coll}{82}$
36	+00 $\frac{EDitch}{158}$	+00 $\frac{Road}{8-7}$	+43 $\frac{4" Coll}{67}$
+91 $\frac{EDitch}{80}$	+93 $\frac{EDitch}{100}$	+97 $\frac{EDitch}{125}$	+89 $\frac{4" BE}{18}$
+75 $\frac{EDitch}{49}$	+87 $\frac{EDitch}{68}$	+64 $\frac{Culvert}{16}$	+46 $\frac{5" BE}{17}$
+67 $\frac{EDitch}{25}$	+74 $\frac{Cor N.}{80}$	+27 $\frac{4" BE}{15}$	+33 $\frac{4" BE}{14}$
+12 $\frac{RTie}{Misc$	+17 $\frac{Cor N.}{84}$	+06 $\frac{STP}{20}$	
35	+14 $\frac{STP}{24}$	+04 $\frac{3-6 BE}{28}$	+04 $\frac{STP}{17}$

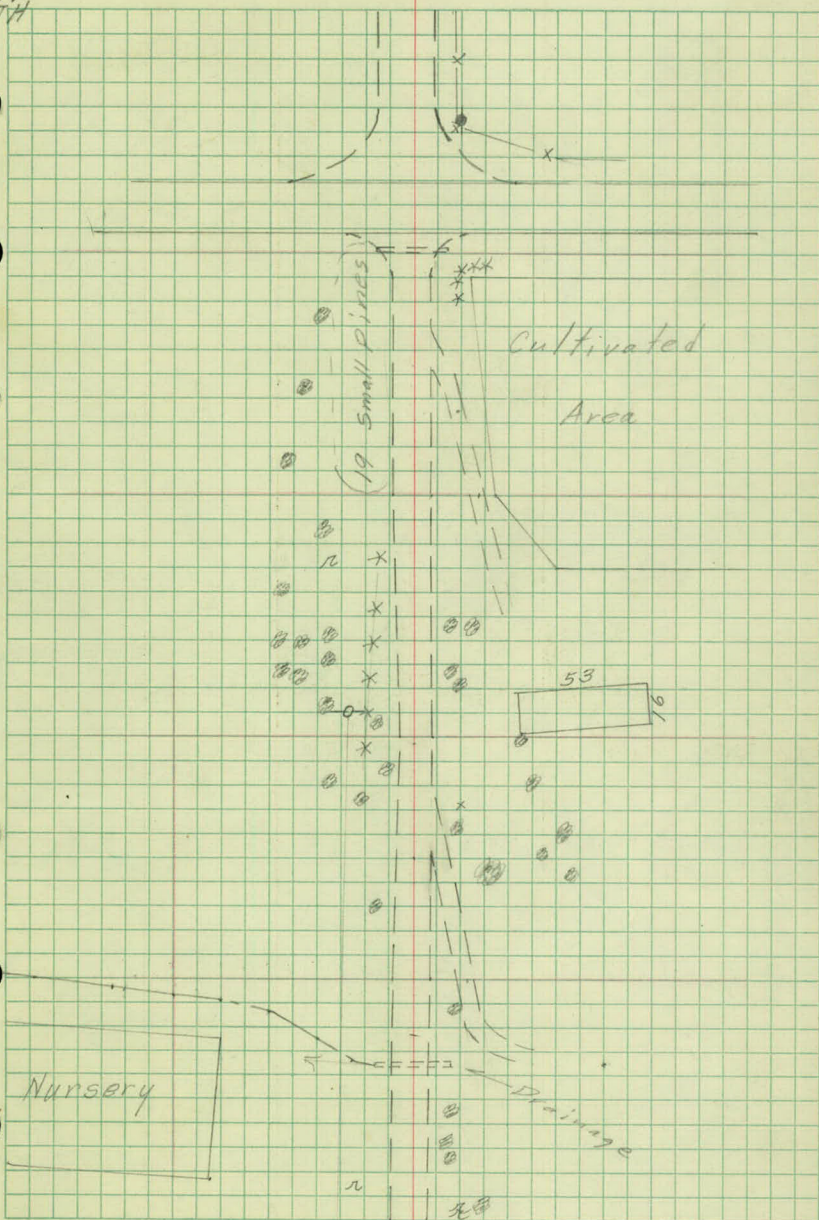
FK
RG
JS
CW
JH

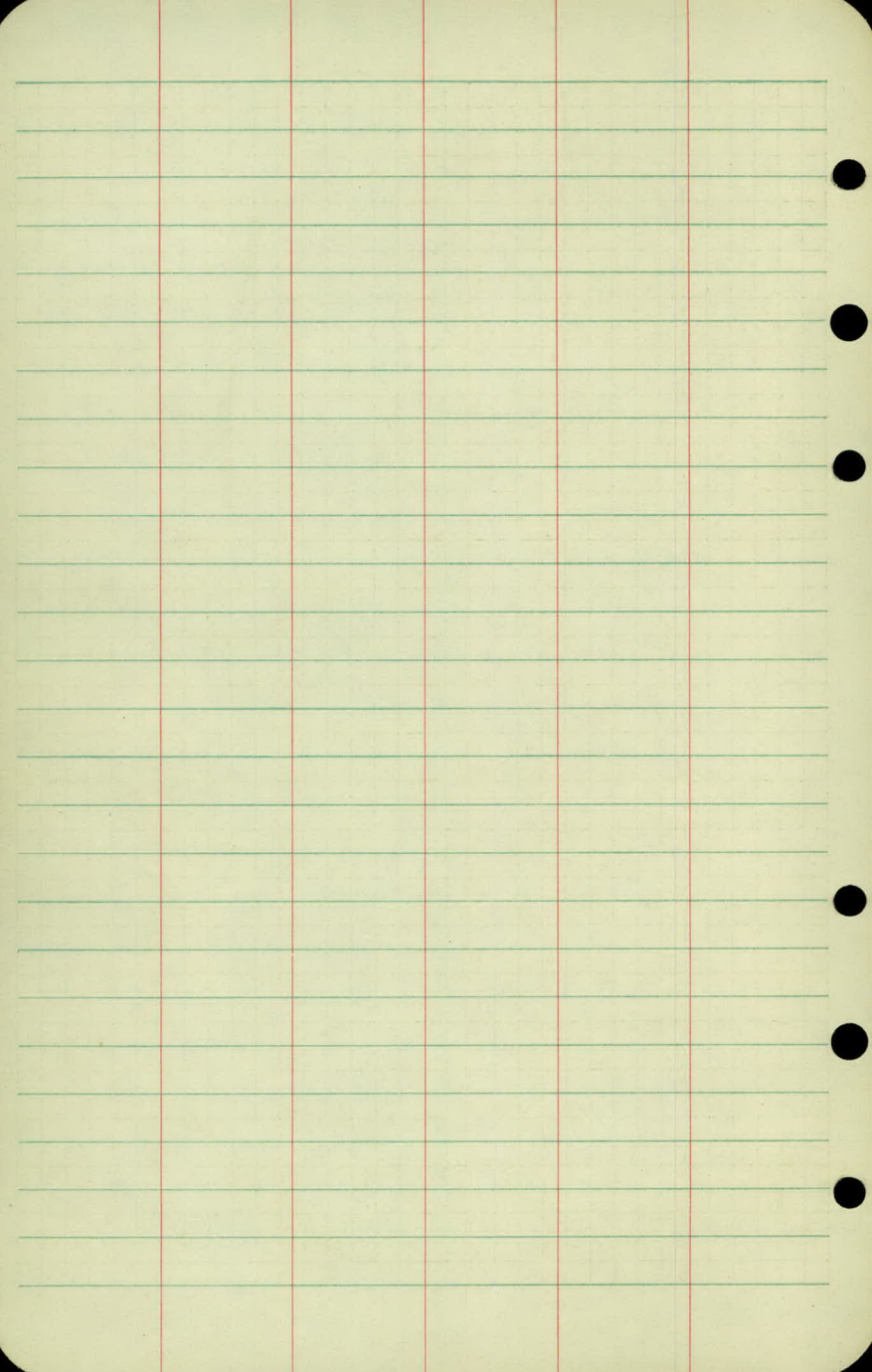
11

Jan. 25, 1960

Rt

14





McKnight Rd

Carver Ave to Highwood Ave

Bench Levels

12-15-59

L.C.

Checked by KP

10 FEB 1960

Sta	+	T	-	Elev	
B.M.	2.58	913.97			911.39 ✓
T.P.	0.13	901.04	13.06	900.91	
T.P.	1.77	889.58	13.23	887.81	
T.P.	5.82	885.91	9.49	880.09	
T.P.	0.66	877.85	8.72	877.19	
T.P.	0.23	866.70	11.38	866.47	
T.P.	7.35	862.46	11.59	855.11	
B.M.			3.95	858.51	✓
T.P.	8.61	862.85	8.22	854.24	
T.P.	13.71	876.32	0.24	862.61	
T.P.	8.47	884.41	0.38	875.94	
B.M.			4.97	879.44	
T.P.	13.56	897.81	0.16	884.25	
B.M.	13.32	910.65	0.48	897.33	
T.P.	13.24	923.83	0.06	910.59	
T.P.	8.36	931.43	0.76	923.07	
B.M.	13.63	943.15	1.91	929.52	
T.P.	0.65	940.48	3.32	939.83	
B.M.	0.34	929.47	11.35	929.13	✓

Lag screw in 36" Maple on Carver Ave E. of Deebach

Top N.W. lower stop Ho. # 2252 Carver Ave.

1st pole

spk. in p.p. Lt. sta 7400

2nd pole

spk in p.p. Lt. sta

3rd pole

spk in p.p. Lt sta

Last pole

spk. in p.p. 90' $\pm$ Lt sta 18+73

Sta + π — E/lev

T.P. 0.26 916.45 13.28 916.19

T.B.M. 0.67 904.32 12.80 903.65 (903.70)

T.P. 1.44 892.35 13.41 890.91 (890.96)

T.P. 0.29 879.49 13.15 879.20

T.P. 6.21 884.91 0.79 878.70

B.M. 2.75 882.16

B.M. 1.68 (883.23)

B.M. 11.55 (873.36)

BM 0.87 930.00

3.59 926.41

TBM 0.53 920.88 9.65 920.35

BM 4.66 912.15 13.39 907.49

T.B.M. 8.40 903.73 (903.75)

T.P. 1.47 880.67 879.20

TP 13.59 881.02 13.24 867.43

BM 7.75 873.27

SPK in 12" ^w Oak Lt sta ²⁶⁺⁰⁸ @ Fe line
N

Spike in PP Lt sta 32+09

Spk in gate post Lt sta

Spk in p.p. S.E. Cor McKnight + Highway

Top of Retaining wall N.E. Cor McKnight + 100

R.R. spk in 36" Cuth. N.W. Cor McKnight + Highway

Spike in PP 90' Lt sta 18+73

926.38

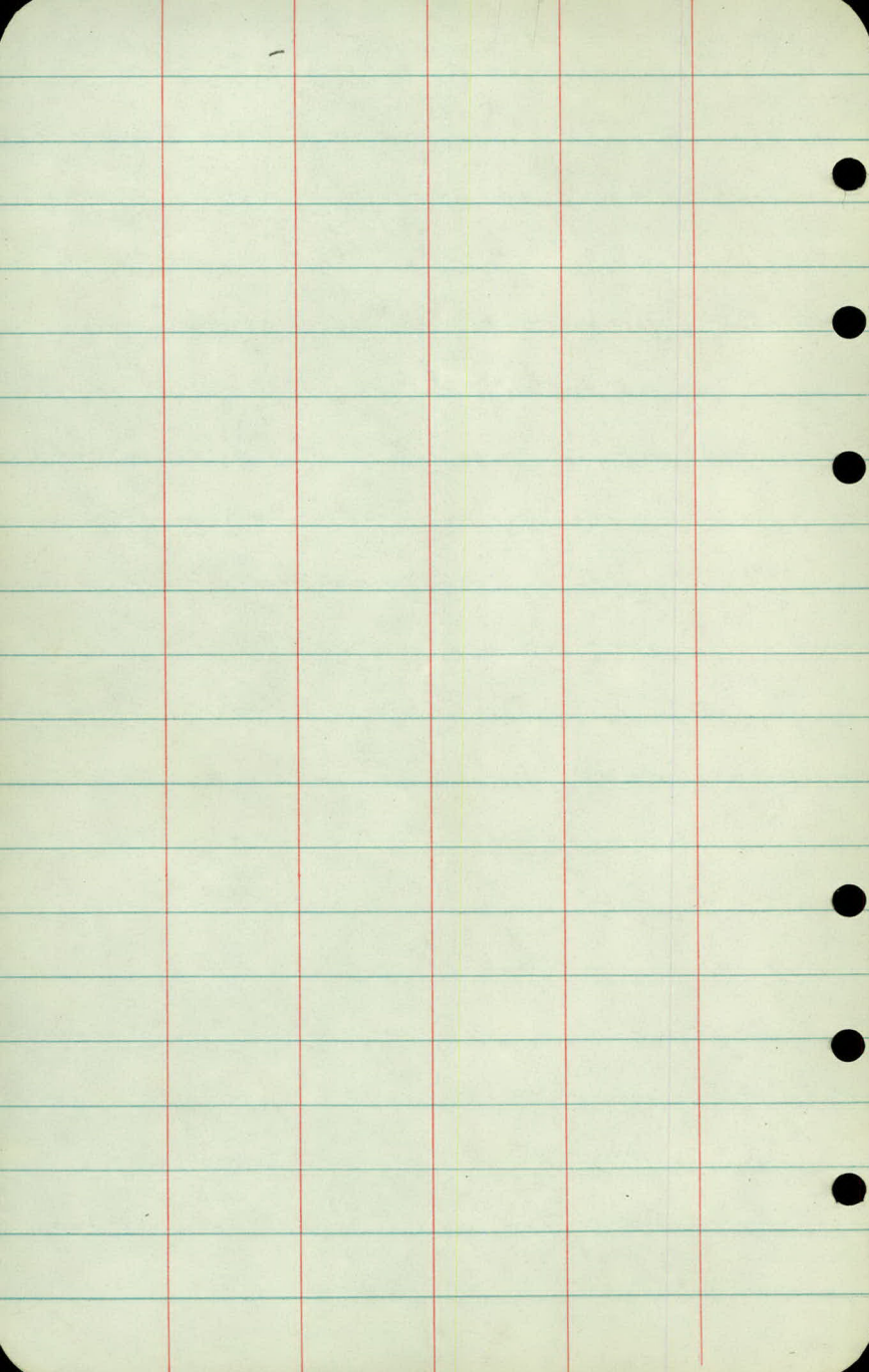
920.32 Boulder

907.05 6" Elm

Spike in 12" W Oak Lt sta 26+08 @ Fe line

Spike in Gate Post Lt

R.R. Spike in 36" Cuth. NW Cor McKnight + Highway



1

Bench Levels

Carver Ave

Deebach Rd. to McKnight Ave

2-8-60

RG
JS
JH

Sta	+	π	-	Elev	
BM	0.40	911.79			911.39
TP	1.75	900.02	13.52	898.27	
TP	0.40	886.76	13.66	886.36	
TP	4.27	878.69	12.34	874.42	
TP	0.93	866.28	13.34	865.35	
TP	7.16	861.98	11.46	854.82	
BM			3.47	858.51	858.51

~ Check Levels ~

BM	1.26	930.39		929.13	
TP	0.02	920.36	10.05	920.34	
TP	4.40	911.87	12.89	907.47	
TPM	0.30	904.03	8.14	903.73	903.80
TP	7.24	898.31	12.96	891.07	
BM	0.10	891.06	7.35	890.96	890.96
TP	0.22	879.57	11.71	879.35	
TP	12.29	883.09	8.77	870.80	
BM			9.71	873.38	873.38

Feb 8, 1960

Very Windy 40°

2

Lag Screw in 36" Maple on Carver Ave E. of Decker

Spike in PP NE Cor Carver + McKnight
Top NW Lower Step Ho # 2252 Carver

Spike in PP 90' Lt Sta 18+73

Boulder

Spike in 6" Elm 65' Lt Sta 23+50

Spike in W. Oak Lt. Sta 26+08 @ Fe Line

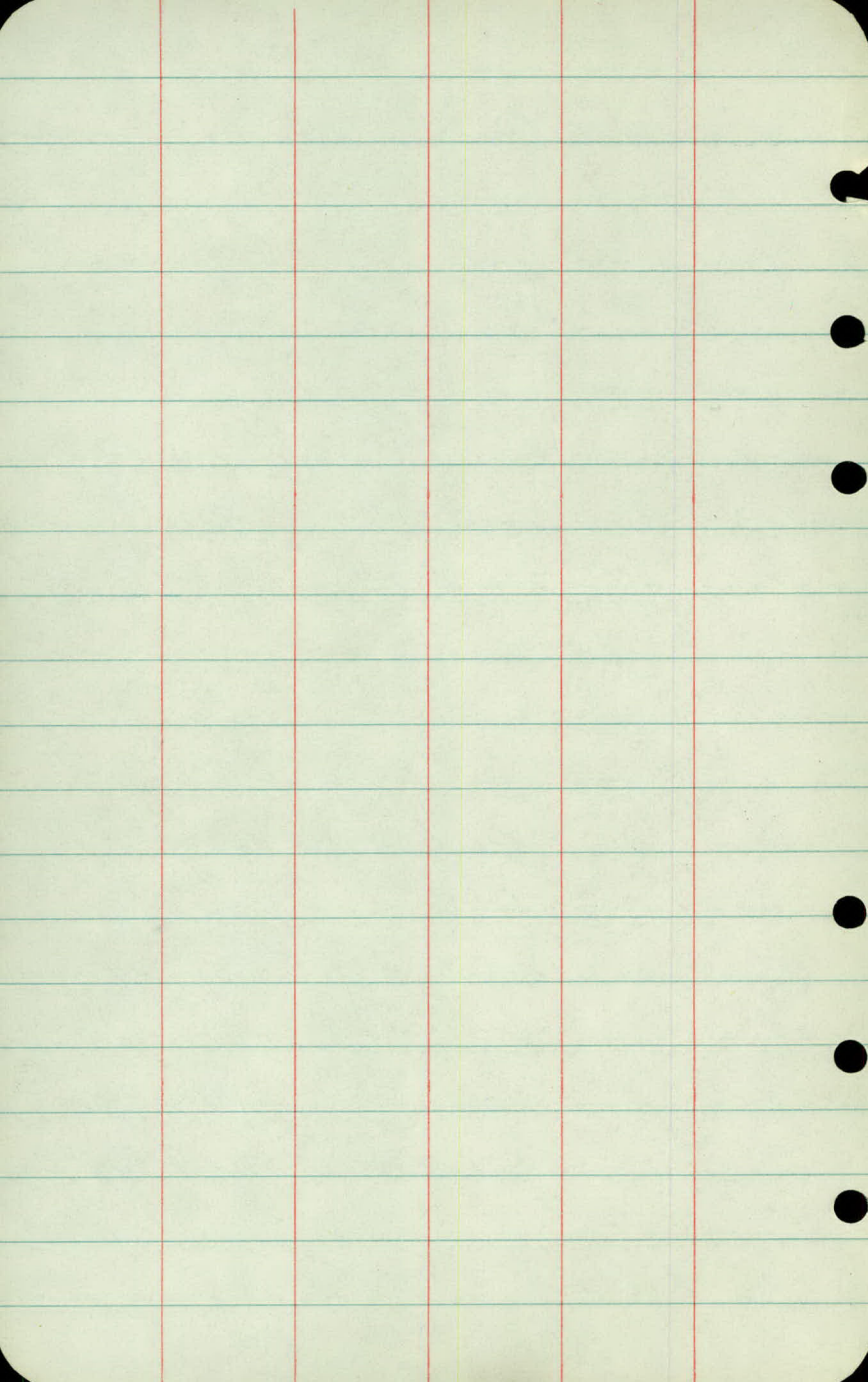
Boulder Sta 28+75 approx.

Spike in PP Lt. Sta 32+09

Spike in Gate Post Lt Sta ± 32+60

Rock

RR Spike in 36" Cottonwood NW Cor Highwood
E McKnight



X-Sections

Sta	+	π	-	Elev.
-----	---	-------	---	-------

BM	3.34	861.85		858.51
----	------	--------	--	--------

0+00

✓

+13

+24

+33

+50

FA
RQ
JS
CW
JH

Jan 25, 1960

19

N.W. Cor Lower Step H[#]2252 S.W. Cor Carver

51.3	51.4	52.2	53.4	54.5	55.2	56.1	56.3	56.7
10.6	10.5	9.7	8.5	7.4	6.7	5.8	5.6	5.2
105	100	75	32		25	65	75	100

58.7	57.4
3.2	4.5
175	129

52.0	52.6	53.4	54.2	54.7	54.7	55.5	55.9
9.9	9.3	8.5	7.7	7.2	7.2	6.4	6.0
75	53	20		18	26	57	75

52.8	53.4	52.7	53.6	53.5	54.2	54.3	54.0	54.1	54.3	54.3
9.1	8.5	9.2	8.3	8.4	7.7	7.6	7.9	7.8	7.6	7.6
75	64	59	36	13		13	22	41	59	75

52.8	54.1	53.5	52.9	53.9	54.2	54.4	54.7	54.2	54.2	54.5	54.7
9.1	7.8	8.4	9.0	8.0	7.7	7.5	7.2	7.7	7.7	7.4	7.2
75	61	39	23	8		7	14	20	34	58	75

53.3	54.0	54.3	53.6	55.1	54.8	55.0	55.2	55.5	55.5	55.0	55.3	55.6
8.6	7.9	7.6	8.3	6.8	7.1	6.9	6.7	6.4	6.4	6.9	6.6	6.4
75	55	43	25	8	6		64					

54.7	54.9	54.6	54.6	55.3	55.6
7.2	7.0	7.3	7.3	6.7	6.7
75	53	51	45	36	

Sta

+

π

-

Elev.

861.85

0+75

✓

1

✓

+ 50

✓

Jan. 25, 1960
RT 20

55.6	55.1	56.4	57.5	57.2	57.3	57.1	57.6	57.6	56.9	56.9
6.3	6.8	5.5	4.4	4.7	4.6	4.8	4.3	4.3	5.0	5.0
75	53	31	8	7		6	8	10	11	13

54.4	56.0	55.9	55.9	56.9	57.6	57.3
7.2	5.9	6.0	6.0	5.0	4.3	4.6
75	65	60	46	34	30	14

56.3	56.4	57.1	58.5	57.8	58.0	57.9	58.2	57.2	57.9	57.3
5.6	5.5	4.8	3.4	4.1	3.9	4.0	3.7	4.7	4.0	4.6
75	55	30	6	2		7	10	12	17	32

54.9	55.2	56.3	55.9	56.4
7.0	6.7	5.6	6.0	5.5
75	68	65	50	44

54.0	54.6	54.5	56.2	57.3	57.4	57.6	56.7	55.6	55.6	56.0
7.9	7.3	7.4	5.7	4.6	4.5	4.3	5.2	6.3	6.3	5.9
50	36	12	5			8	14	21	22	24

53.0	54.1	54.8	54.8	55.5	54.9	55.3
7.6	7.8	7.1	7.1	6.4	7.0	6.6
75	81	65	65	62	53	43

H0

Sta + π - Elev.

861.85

2

✓

+25

✓

+50

Jan 25, 1960

21

51.5	52.6	53.3	55.5	58.4	58.4	58.4	57.8	57.0	55.3	55.1
10.4	9.3	8.6	6.4	3.5	3.5	3.5	4.1	4.9	6.6	6.8
75	55	36	23	6		15	19	32	46	54

5+

56.0	56.1
5.9	5.8
75	66

51.7	53.2	55.5	58.4	58.3	58.0	58.1	58.3	57.6	56.2
10.2	8.7	6.4	3.5	3.6	3.9	3.8	3.6	4.3	5.7
56	37	20	7		2	12	17	30	37

51.1	50.8	56.5	55.6	53.5
10.8	11.1	5.4	6.3	6.4
68	75	75	58	48

50.2	51.1	52.2	54.3	56.4	56.7	56.3	56.4	56.8	56.1	53.4
11.7	10.8	9.7	7.6	5.5	5.2	5.6	5.5	5.1	5.8	6.5
65	51	33	17	4		3	14	28	35	50

50.2	57.0	56.3
11.7	4.9	5.6
75	75	64

Sta + π - Elev

861.85

2+75

✓

3

✓

+50

TP 496 862.03 4.78 859.07

L4

A

A1

51.2	52.2	52.9	53.9	54.5	55.1	55.2	54.6	55.2
10.7	9.7	9.0	8.0	7.4	6.8	6.7	7.3	6.7
40	29	13	4		3	15	21	34

51.2		51.1	50.9			56.4	55.8	55.0	55.2
19.7	10.8	11.0				5.5	6.1	6.9	6.7
56	67	75				75	62	48	41

51.2	51.6	52.2	52.5	53.3	54.1	54.2	54.4	53.9	54.6
10.7	10.3	9.7	9.4	8.6	7.8	7.7	7.5	8.0	7.3
61	43	26	12	3	3	9	15	19	37

50.8								56.0	55.4
11.1								5.9	6.5
75								75	60

52.3	52.3	52.5	53.0	53.6	54.0	54.3	54.5	54.0	54.5	55.0
9.6	9.6	9.4	8.9	8.3	7.9	7.6	7.4	7.9	7.4	6.9
66	54	38	17	6		3	16	24	49	65

51.9									
19.0									
75									

55.6
6.3
75

Sta + π - Elev.

862.03

3 + 75

+ 91

+ 91

4 ✓

4

+ 26

✓

Jan. 25, 1960

23

$\begin{array}{r} 52.2 \\ 9.8 \\ 75 \end{array}$
 $\begin{array}{r} 52.8 \\ 9.2 \\ 69 \end{array}$
 $\begin{array}{r} 53.1 \\ 8.9 \\ 56 \end{array}$
 $\begin{array}{r} 52.9 \\ 9.1 \\ 38 \end{array}$
 $\begin{array}{r} 53.3 \\ 8.7 \\ 8 \end{array}$
 $\begin{array}{r} 54.6 \\ 7.4 \\ 74 \end{array}$
 $\begin{array}{r} 54.7 \\ 7.3 \\ 3 \end{array}$
 $\begin{array}{r} 55.0 \\ 7.0 \\ 15 \end{array}$
 $\begin{array}{r} 54.6 \\ 7.4 \\ 29 \end{array}$
 $\begin{array}{r} 55.0 \\ 7.0 \\ 50 \end{array}$
 $\begin{array}{r} 56.1 \\ 5.9 \\ 75 \end{array}$

11

RT

$\begin{array}{r} 54.1 \\ 7.9 \\ 61 \end{array}$
 $\begin{array}{r} 53.5 \\ 8.5 \\ 49 \end{array}$
 $\begin{array}{r} 53.8 \\ 8.2 \\ 30 \end{array}$
 $\begin{array}{r} 54.6 \\ 7.4 \\ 17 \end{array}$
 $\begin{array}{r} 56.1 \\ 5.9 \\ 7 \end{array}$
 $\begin{array}{r} 53.7 \\ 6.3 \\ 6.3 \end{array}$
 $\begin{array}{r} 55.2 \\ 6.8 \\ 1 \end{array}$
 $\begin{array}{r} 55.3 \\ 6.7 \\ 14 \end{array}$
 $\begin{array}{r} 55.9 \\ 6.1 \\ 18 \end{array}$
 $\begin{array}{r} 55.1 \\ 6.9 \\ 35 \end{array}$

$\begin{array}{r} 54.4 \\ 7.6 \\ 75 \end{array}$

$\begin{array}{r} 56.6 \\ 5.4 \\ 75 \end{array}$
 $\begin{array}{r} 56.2 \\ 5.8 \\ 66 \end{array}$
 $\begin{array}{r} 55.3 \\ 6.7 \\ 46 \end{array}$

$\begin{array}{r} 55.5 \\ 6.5 \\ 44 \end{array}$
 $\begin{array}{r} 55.3 \\ 6.7 \\ 28 \end{array}$
 $\begin{array}{r} 54.4 \\ 7.6 \\ 20 \end{array}$
 $\begin{array}{r} 56.2 \\ 5.8 \\ 4 \end{array}$
 $\begin{array}{r} 55.9 \\ 6.1 \\ 13 \end{array}$
 $\begin{array}{r} 55.5 \\ 6.5 \\ 17 \end{array}$
 $\begin{array}{r} 56.3 \\ 5.7 \\ 26 \end{array}$
 $\begin{array}{r} 55.6 \\ 6.4 \\ 27 \end{array}$
 $\begin{array}{r} 55.9 \\ 6.1 \\ 27 \end{array}$

$\begin{array}{r} 55.2 \\ 6.8 \\ 58 \end{array}$
 $\begin{array}{r} 55.6 \\ 6.4 \\ 68 \end{array}$
 $\begin{array}{r} 55.3 \\ 6.7 \\ 75 \end{array}$
 $\begin{array}{r} 57.3 \\ 4.7 \\ 75 \end{array}$
 $\begin{array}{r} 56.6 \\ 5.4 \\ 65 \end{array}$

$\begin{array}{r} 55.9 \\ 6.1 \\ 49 \end{array}$
 $\begin{array}{r} 55.4 \\ 6.6 \\ 33 \end{array}$
 $\begin{array}{r} 55.0 \\ 7.0 \\ 20 \end{array}$
 $\begin{array}{r} 55.4 \\ 6.6 \\ 6 \end{array}$
 $\begin{array}{r} 56.4 \\ 5.6 \\ 7 \end{array}$
 $\begin{array}{r} 56.8 \\ 5.2 \\ 15 \end{array}$
 $\begin{array}{r} 56.2 \\ 5.8 \\ 18 \end{array}$
 $\begin{array}{r} 57.1 \\ 4.9 \\ 38 \end{array}$
 $\begin{array}{r} 57.6 \\ 4.4 \\ 37 \end{array}$
 $\begin{array}{r} 58.3 \\ 5.8 \\ 57 \end{array}$

$\begin{array}{r} 55.6 \\ 6.1 \\ 75 \end{array}$
 $\begin{array}{r} 55.6 \\ 6.1 \\ 75 \end{array}$
 $\begin{array}{r} 58.6 \\ 7.3 \\ 75 \end{array}$

Sta + π - Elev

862.03

4+40

+ 57 S. R. L. Marillac Lane

+ 76 E Marillac Lane

TP 12,39872.41 2.01 860.02

2

24

56.4	56.5	56.2	56.7	56.7	57.4	56.7	57.2	58.2	59.3
56	55	58	53	53	46	53	48	38	27
56	41	26	12		8	19	23	45	63

6.0	56.0							60.0	
75								2.0	
								75	

56.4	57.2	56.8	57.1	57.3	58.0	57.2	58.1	59.1	60.7
56	48	52	49	47	40	48	39	29	13
52	38	26	17		11	24	29	54	75

56.2	56.0								
58	6.0								
63	75								

57.0	57.4	57.8	58.2	58.4	58.5	59.2	58.7	59.2
50	46	42	38	36	35	28	33	28
60	46	30	17		19	25	34	43

56.7	56.2	55.4				61.0	60.4
53	58	66				10	1.6
75	100	125				75	68

Sta + π - Elev.

872.41

4+93

✓

5

✓

+13 N.P.L.

1

Jan 25, 1960

25

RT

1.

56.3	56.9	57.3	58.0	58.5	59.1	59.6	60.7	61.0
16.1	15.5	15.1	14.4	13.9	13.3	12.8	11.7	11.4
75	54	35	14		21	34	39	45

62.5	62.1	60.9
9.9	10.3	11.5
75	65	51

58.0	58.1	57.5	58.4	58.3	59.0	58.9	59.4	60.7
14.4	14.3	14.9	14.0	14.1	13.4	13.5	13.0	11.7
65	47	34	21		3	15	27	41

57.6	66.4	64.1	63.2	62.5	62.5	61.7
14.8	6.0	8.3	9.2	9.9	9.9	10.7
75	75	71	66	58	53	45

59.1	58.0	58.8	58.0	58.8	59.2	59.9	61.8	64.4
13.3	14.4	13.6	14.4	13.6	13.2	12.5	10.6	8.0
41	31	14	7		15	31	48	59

59.2	58.9	66.2
13.2	13.5	6.2
59	75	75

Sta + π - Elev.

872.41

5+40

✓

+ 78

✓

+ 88

Lt.

Jan 25, 1960

Rt.

26

61.6

59.8

60.2

60.0

60.0

60.7

61.6

62.7

10.8

12.6

12.2

12.4

12.4

11.7

10.8

9.7

40

24

13

15

34

52

59

61.7

61.8

61.9

66.7

65.9

10.7

10.6

10.5

5.7

6.5

56

70

75

75

68

66.3

66.2

65.5

63.6

63.7

62.2

61.5

61.9

62.2

63.1

6.1

6.2

6.9

8.8

8.7

10.2

10.9

10.5

10.2

9.3

57

41

31

16

5

11

14

28

43

66.3

65.0

63.0

64.6

65.6

64.8

6.1

7.4

7.4

7.8

6.8

7.6

75

75

72

62

55

50

67.4

67.0

64.6

64.3

63.0

62.3

62.4

63.3

64.1

5.0

5.4

7.8

8.1

9.4

10.1

10.0

9.1

8.3

45

33

16

7

10

20

36

40

67.2

66.9

70.5

68.6

68.0

67.3

5.2

5.5

1.9

3.8

4.4

5.1

59

75

40

75

52

46

110

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		872.41		
--	--	--------	--	--

6 +00				
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✓				
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+20				
-----	--	--	--	--

✓				
---	--	--	--	--

TP	12.79	879.60	5.60	866.81
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+40				
-----	--	--	--	--

Jan 25, 1960

27

68.4	68.4	65.7	65.5	64.5	63.3	63.1	63.4	64.9
4.0	4.0	6.7	6.9	7.9	9.1	9.3	9.0	7.5
46	32	15	7		7	19	32	41

68.0	67.6
4.4	4.8
62	75

69.0	68.6	67.5
3.4	3.8	4.9
75	66	47

70.4	70.8	68.3	68.0	66.7	66.9	65.6	65.9	64.8	65.0
2.0	1.6	4.1	4.4	5.7	5.5	6.8	6.5	7.6	7.4
45	31	17	8		3	6	15	28	39

70.0	69.9
2.4	3.0
59	75

69.4	68.8	68.2
3.0	3.6	4.2
75	65	47

71.4	72.2	72.4	70.9	70.6	70.0	69.7	68.1	69.0	67.5
8.2	7.4	7.2	8.7	9.0	9.6	9.9	10.9	10.6	12.1
53	37	24	15	5		3	6	15	27

70.5
9.1
75

70.0	69.1	67.2	66.9
9.6	10.5	12.4	12.7
75	59	53	43

Sta + π - Elev.

879.60

6+52

✓

+ 73

✓

F.B

BM 2.48 881.92 0.13 879.47 (879.44)

Jan 25, 1960

28

LT

4

BT

12.2	13.8	14.1	12.8	11.1	10.8	11.0	10.3	9.0
2.4	5.8	5.5	6.8	7.9	8.8	8.6	9.3	10.6
50	34	24	8		5	13	26	39

7.1								
8.5								
75								

14.0	16.0	16.8	16.6	15.9	15.9	14.4	14.1	10.1	10.8
5.6	3.6	2.8	3.0	3.7	3.7	5.2	5.5	8.9	8.8
40	24	17	9		3	6.5	18	23	36

12.1	12.4							
69	72							
62	75							

4.9	3.1	1.0	0.4	0.9	3.4	3.6	2.6	4.0	5.2
39	28	16	9		7	13	17	33	51

13.6	13.0							
6.0	6.6							
59	75							

Spike in PP. LT Sta 7+00

Sta

+

π

-

Elev.

881.92

7+00

✓

+ 30

✓

+55

✓

RG
JS
CW

Lt. Snow

Jan 26, 1960
Cold, Windy 5° 29
5th

Lt.

£

77.4	79.2	79.9	80.7	79.9	79.8	77.8	77.6	79.0	77.6
4.5	2.7	2.0	1.2	2.0	2.1	4.1	4.3	2.9	4.3
44	28	12	5		2	6	13	17	29

75.3	73.2
4.6	8.7
62	75

72.8	75.7
9.1	6.2
75	53

74.8	76.0	78.9	80.8	80.3	79.6	79.5	80.8	79.8
7.1	5.9	3.0	1.1	1.6	2.3	2.4	1.1	2.1
42	29	13		4	6	13	16	24

73.2	72.5
8.7	9.4
58	75

75.3	77.3	79.0
6.6	4.6	2.9
75	58	40

73.3	74.4	76.1	79.1	79.8	78.9	79.1	80.2	79.5
8.6	7.5	5.8	2.8	2.1	3.0	2.8	1.7	2.4
59	39	18		2	4	13	14	20

72.5
9.4
75

75.4	76.8	78.9
6.5	5.1	3.0
75	61	40

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		881.92		
--	--	--------	--	--

7+75				
------	--	--	--	--

✓				
---	--	--	--	--

8+00				
------	--	--	--	--

✓				
---	--	--	--	--

+10				
-----	--	--	--	--

✓				
---	--	--	--	--

TP	11.42	892.91	0.43	881.99
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Jan 26, 1960

130

LT.

RT.

14.9	16.1	17.3	19.0	18.9	14.3	10.5	14.6
7.0	5.8	4.6	2.9	3.0	2.6	1.4	2.3
28	15	3		5	11	14	21

✓

14.2	13.7	12.6
7.7	8.2	9.3
44	63	75

17.4	17.5	14.3
4.5	4.4	2.6
75	61	41

←

15.8	16.6	16.1	18.3	19.1	19.6	20.4	21.0	20.5
6.1	5.3	5.2	3.6	2.2	2.3	1.5	0.9	1.4
48	35	30	17		3	10	12	21

✓

15.5	15.1
6.4	6.2
65	75

19.8	19.4	19.8	20.4
2.1	2.5	2.1	1.5
75	67	56	39

←

18.1	17.6	19.0	20.3	20.1	20.8	21.1	20.8	20.4
3.8	4.3	2.9	1.6	1.8	1.1	0.8	1.1	1.5
24	20	14		3	7	16	34	57

17.4	16.9	16.6
4.5	5.0	5.3
36	54	75

20.4	20.0
1.5	1.9
75	90

Top Stamp

Sta	+	π	-	Elev
-----	---	-------	---	------

		892.91		
--	--	--------	--	--

8+47				
------	--	--	--	--

✓				
---	--	--	--	--

+75				
-----	--	--	--	--

✓				
---	--	--	--	--

9+00				
------	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

Jan 26, 1960

Rt

31

Lt.

L

80.9	81.5	81.9	82.6	82.3	82.1	82.6	83.0	82.9
12.6	11.4	11.0	10.3	10.6	10.8	10.3	9.9	10.0
21	13	4	2		3	9	12	18

81.9	81.1	79.7	78.8		82.9	82.8	82.1	82.1	83.8
11.0	11.8	13.2	14.1		10.0	10.1	10.8	10.2	9.1
24	39	55	75		75	61	47	39	23

85.8	82.0	84.8	83.5	83.8	84.6	84.9	85.6	85.4
7.1	10.9	8.1	9.4	9.1	8.3	8.0	7.3	7.5
27	20	14	11		8	13-16	17	35

84.8	82.8	82.4			85.8	85.6	85.2	84.5
8.1	10.1	10.5			7.1	7.3	7.7	8.4
41.7	62.4	75			75	69	54	50

86.7	85.4	87.5	86.4	86.5	86.7	87.8	86.1	88.9
6.2	7.5	5.9	6.5	6.4	6.2	5.1	6.8	4.0
17.21	10-14	6	4		4	8	11-13	17-19

85.2	84.6	84.3	87.9		86.6	87.6	86.8	87.0
7.7	3.3	3.6	5.0		6.3	5.3	6.1	5.9
26	35	50	66		42	37-40	35	25

		87.4			87.4	88.9		
		5.5			5.5	4.0		
		75			59	75		

Sta

+

 π

-

Elev

892.91

TP

13.28

900.53

5.66

887.25

Rock

9+13

✓

✓

+ 28

✓

✓

Jan 26, 1960

Lt.

E

Rt

32

89.7	88.1	90.4	88.9	88.4	88.0	89.6	87.2	89.7
10.8	12.4	10.1	11.6	12.1	12.5	10.9	13.3	10.8
17	12-13	8	4		3	7	10-15	18

87.4	92.5	93.3	92.4	87.3	88.5	88.4	89.2	88.6
13.1	8.0	7.2	8.1	13.2	12.0	12.1	11.3	11.9
24	35	46	64	42-45	39	31	28	22

91.6	88.5	88.9	90.0
8.9	12.0	11.6	10.5
75	47	63	75

94.9	93.6	92.8	90.7	89.7	89.4	90.8	88.3	91.4
5.6	6.9	7.7	9.8	10.8	11.1	9.7	12.2	9.1
42	26	8	4		3	6	9-12	16

93.8	92.5
6.7	8.0
57	75

89.4	90.2	91.2	91.0
11.1	10.3	9.3	9.5
44	41	30	25

90.2	91.2	93.7
10.3	9.3	6.8
48	60	75

Sta + π - Elev

900.53

9+46

✓

+75

✓

BM 13.63 910.96 3.20 897.33 (897.33)

10+00

✓

Jan 26, 1960
Jan 27, 1960

Lt.

2

Rt

94.0	94.2	91.9	92.0	91.6	93.1	99.7	94.1
6.5	6.3	8.6	8.5	8.9	7.4	10.8	5.8
22	9	6		2	5	11-16	20

94.8	96.5	95.6	93.9	98.2	96.3	94.6	94.2	94.5
5.7	4.0	4.9	6.6	2.3	4.2	5.9	6.3	6.0
31	49	61	75	75	55	52	45	33

95.3	95.6	96.5	94.9	94.3	95.5	96.1	90.8	97.0
5.2	4.9	4.0	5.6	6.2	5.0	4.4	9.7	3.5
40	23	9	2-6		2	6	13-16	22

94.4	93.1	903.5	900.5	98.9
6.1	7.4	18.0	-3.0	0.0
59	75	75	75	59

Spike in 2nd P.P.L. sta.

94.8	95.6	97.1	98.4	97.7	98.5	93.8	91.0	92.1
16.2	15.4	13.9	12.6	13.3	12.5	17.2	10.0	8.9
53	40	25	10		5	12	24	37

93.6	11.0	99.4	98.6	95.9
17.4	0.0	1.6	2.4	5.1
75	75	70	63	53

Sta

+

π

-

Elev

910.96

10+25

✓

+50

✓

+75

✓

TP

13.09

923.36

0.69

910.27

RG
KP
JS
JH

Lt.

±

Rt

Jan 27, 1960
100 - Cloudy

34

97.5	98.0	99.9	01.2	01.3	02.4	99.4	96.0	06.0
13.5	13.0	11.1	9.8	9.7	8.6	13.6	15.0	5.0
40	23	12	9		12	18	22-24	36

96.3	95.6					16.9	14.4	11.0	08.8
14.7	15.4					+5.9	+3.4	0.0	2.2
55	75					75	66	53	46

97.3	98.9	01.9	04.3	05.0	06.5	07.1	02.5	98.1	06.1
13.7	12.1	9.6	6.7	6.0	4.5	3.9	8.5	12.3	4.3
60	37	13	9		6	12	18	23-26	33

96.8						19.6	15.4	11.0
14.2						+8.6	+4.4	0.0
75						75	60	45

02.0	05.2	12.0	09.8	10.0	12.0	12.3	13.1	00.8
9.0	5.8	+1.0	1.2	1.0	+1.0	+1.3	+2.1	10.2
40	16	6	3		9	15	18	38-41

99.5	99.5					20.9	14.5	09.8
11.5	11.5					+9.9	+3.5	1.2
65	75					75	57	48

Spike in ground

Sta	+	π	-	Elev
-----	---	-------	---	------

		923.36		
--	--	--------	--	--

11+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+20				
-----	--	--	--	--

✓				
---	--	--	--	--

TP	10.09	931.89	1.56	921.80
----	-------	--------	------	--------

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

Jan 27, 1960

35

Lt.

E

Rt.

6.5	10.1	17.5	14.7	15.8	17.1	17.3	15.7	13.3
16.9	13.3	5.9	8.7	7.6	6.3	6.1	7.7	10.1
30	16	4		5	10	26	42	57

2.5

04.1

04.2

18.0

15.7

08.7

19.9

18.7

19.2

5.4

7.7

14.7

48

64

75

75

71

62-64

09.9

12.9

20.6

18.1

17.6

20.9

20.3

21.2

13.5

10.5

2.8

5.3

5.8

2.5

3.1

2.2

34

19

4

10

15

22

40

08.7

07.2

08.3

06.0

11.3

16.8

19.1

14.7

16.2

15.1

12.4

12.1

6.6

4.3

46

51

56

75

72-76

65

53

stamp

17.1

19.2

24.0

23.8

22.1

22.5

25.3

25.1

25.7

26.3

14.8

12.7

7.9

8.1

9.8

9.4

6.6

6.8

6.2

5.6

35

18

8

3

8

18

26

29

37

15.6

16.0

14.9

17.9

14.3

24.8

26.5

16.3

15.9

17.0

14.0

17.6

7.1

5.4

51

62

75

82

75-78

60

42

Sta	+	π	-	Elev
-----	---	-------	---	------

		931.89		
--	--	--------	--	--

+75				
-----	--	--	--	--

✓				
---	--	--	--	--

12+00				
-------	--	--	--	--

✓				
---	--	--	--	--

BM	6.77	936.29	2.36	929.53	929.52
----	------	--------	------	--------	--------

+20				
-----	--	--	--	--

✓				
---	--	--	--	--

Jan 27, 1960

Lt.			Rt			36		
2.2	2.0	2.6	2.2	2.9	2.0	2.1	2.8	2.6
8.7	5.9	5.3	7.7	7.0	4.9	4.8	4.1	13.3
18	12	7		13	18	37	54	71

2.6	2.2	2.1						5.3
10.3	10.7	11.8						16.6
40	63	76						82

2.3	2.1	2.4	2.4	2.5	2.7	2.7	3.0	3.9
5.6	4.8	3.5	3.5	6.2	5.2	3.2	1.0	0.0
46	23	17	8		14	19	27	49

2.5	2.4						1.9	3.9
6.9	7.4						15.0	1.0
69	75						88	63

Spike in PP Lt Sta 12+20 (3rd PP Lt ϕ)

2.5	2.7	2.0	2.2	2.3	2.1	2.8	3.0	3.9
7.8	6.6	6.3	7.1	10.0	9.2	8.5	3.3	3.4
37	22	16	10		7	14	28	47

2.0	2.6						3.0	3.3
9.3	10.7						5.8	5.0
60	75						76	70

Sta

+

π

-

Elev

936.29

+45

✓

+61

✓

13+00

+02

Van 27, 1960

Lt.

L

Rt.

37

29.5	31.0	31.8	28.7	28.6	28.9	31.1	33.6	32.2
6.8	5.3	4.5	7.6	2.7	7.4	5.2	2.7	4.1
50	28	23	6		11	19	28	51

27.9
8.4
75

29.7
6.6
75

30.6
5.7
68

31.4	32.1	30.9	29.3	29.2	29.4	30.0	32.8	32.9
4.9	4.2	5.4	7.0	7.1	6.9	6.3	3.5	3.4
42	27	16	7		6	14	25	58

30.9
5.4
60

29.6
6.7
75

30.3
6.0
75

31.1
5.2
63

33.7	33.6	33.6	33.6	32.4	32.3	32.1	32.0	32.3	32.3	32.3
2.6	2.7	2.7	2.7	3.9	4.0	4.2	4.3	4.0	4.0	4.0
15	61	38	24	20		18	33	49	69	75

33.1
3.2
75

33.1
3.2
62

33.0
3.3
38

32.6
3.7
21

32.4
3.9

32.1
4.2
19

32.0
4.3
37

31.6
4.7
55

31.7
4.6
75

Sta + π - Elev

936.29

13 + 13 $\pm$ Road

✓

+24

+25

✓

T.P. 11.27 947.34 0.22 936.07

B.M. 11.68 935.66

Jan 28, 1960

LT

2

RT

38

33.9	34.1	33.9	33.5	33.1	32.6	32.1	32.0	31.8	32.2
2.4	2.2	2.4	2.8	3.2	3.7	4.2	4.3	4.5	4.1
100	86	54	21		19	46	69	100	150

33.9
2.4
146

35.6
0.7
200

33.1
3.2
200

34.1	34.3	34.2	34.1	33.9	33.0	32.8	32.4	32.0
2.2	2.0	2.1	2.2	2.4	3.3	3.5	3.9	4.3
75	64	43	19		17	38	61	75

34.5	34.6	34.3	34.2	34.0	33.7	34.7	35.1	34.4
1.8	1.7	2.0	2.1	2.3	2.6	1.6	1.2	1.9
69	46	27	19		13	20	24	27

34.8
1.5
75

33.8	33.9	35.0	35.6	35.0	34.7
2.5	2.4	1.3	1.7	1.3	1.6
75	65	61	4.7	37	30

RR Spike in 4th PP 36' LT Sta 13+25

Sta

+

π

-

Elev

947.34

13+50

✓

+80.

✓

14+00

✓

Jan 27, 1960

Lt.				E		Rt.				39
35.8	36.0	35.9	35.9	36.2	36.4	37.6	36.8	36.6		
11.5	11.3	11.4	11.4	11.1	10.9	9.7	10.5	10.7		
53	40	24	13		10	14	18	33		

36.5
10.8
75

35.2 35.5 36.9 36.6
12.1 11.8 10.4 10.7
75 67 59 49

39.7	39.1	39.5	38.2	38.2	38.6	38.6	40.1	39.4	38.9	38.9
7.6	8.2	7.8	9.1	9.1	8.7	8.7	7.2	7.9	8.4	8.4
58	40	29	22	12		6	11	16	34	58

40.1
7.2
75

36.1 36.4
11.2 10.9
75 70

40.6	40.8	39.1	39.5	39.5	39.6	40.9	40.1	39.4	38.4
6.7	6.5	8.2	7.8	7.8	7.7	6.4	7.2	7.6	8.9
38	31	21	7		5	10	12	31	51

41.7
5.6
60

43.0
4.3
75

36.5 36.8 37.7
10.8 10.5 9.6
75 70 67

Sta

+

π

-

Elev

947.34

14+32

✓

+53

✓

+75

✓

Jan 27, 1960

Lt.

#

Rt

40

41.0	40.1	40.4	40.6	40.8	40.9	38.8	38.0	37.4	37.0
6.3	7.2	6.9	6.7	6.5	6.4	8.5	9.3	9.9	10.3
55	34	28	12		9	17	32	51	59

42.8
4.5
75

36.6
37.6
10.7 9.7
75 66

39.5	40.1	40.6	41.0	41.9	41.5	42.0	40.3	39.1
7.8	7.2	6.7	5.7	5.4	5.8	5.3	7.0	7.6
51	29	21	10		6	11	25	36

39.9
7.4
67

40.7
6.6
75

36.6
36.9
10.7 10.4
75 62

39.3	40.8	41.9	43.5	43.6	43.4	45.3	44.4	44.1	43.1
8.0	6.5	5.4	3.8	3.7	3.9	2.0	2.8	3.2	4.2
53	36	22	9		4	9	12	28	46

39.2
8.1
75

37.3
10.0 9.3 7.0
83 75 65

32
53
75

COLT.
2 FICK

Sta	+	π	-	Elev
TP		947.34	4.89	942.45
	8.35	950.80		

15+00

✓

+14

✓

+34

✓

JAN. 27, 1960

Lt.

L

Rt

41

Top STAKE 30' Lt. STA. 15+00

39.4	41.7	44.3	45.5	45.0	45.1	48.4	47.9	44.9
11.4	9.1	6.5	5.3	5.8	5.7	2.4	2.9	3.9
70	47	23	12		4	10	26	39

38.9

11.9
75

40.2	42.3	44.8
10.6	8.5	6.0
75	69	55

43.0	44.9	46.0	45.6	45.3	49.4	48.9	47.4	44.5
7.8	5.9	4.8	5.2	5.5	1.4	1.9	3.4	6.3
51	28	12		5	13	27	40	61

39.4

11.4
75

41.9

8.9
75

41.8	44.0	45.4	46.1	45.1	45.0	48.2	47.6	46.0
9.0	6.8	5.4	4.7	5.7	5.8	2.6	3.2	4.8
64	44	27	12		5	9	23	43

40.6

10.2
75

42.0	44.0
8.8	6.8
75	62

14
13
13

Sta + TP - Elev

950.80

15+73

✓

TP 111 945.33 6.58 944.22

16

+17

✓

42

38.1 38.2
12.4 12.6
75 71

SPIKE IN PP 25' LT STA 15+00 # 5946											
42.2	42.8	42.2	41.8	42.0	41.4	41.1	39.5	38.8	38.4	38.5	38.5
31	25	31	35	33	39	42	58	65	64	68	68
75	65	47	23	6		12	21	34	50	68	
41.3	42.0	41.5	41.2	41.2	40.7	40.6	39.5	39.7	39.4	39.4	39.5
40	33	38	41	41	46	47	58	56	59	59	59
75	57	45	26	8		3	11	27	45	45	45
									38.9	39.5	39.5
									64	58	58
									75	57	57

Sta + π - Elev

94533

16 + 28

✓

+ 50

✓

+ 20

✓

Jan 29, 1960

43

L+

A

R+

4.1	4.6	4.7	4.5	5.0	4.4	4.4	5.2	5.4	6.2
51	38	46	9		8	16	28	48	75

41.3

40.7

4.0

4.6

40.1	40.6	40.2	39.8	40.0	39.7	39.7	40.4	40.4	39.6
5.2	4.7	5.1	5.5	5.3	5.6	5.6	4.9	4.9	5.4
75	65	44	27	11		2	4	21	35

38.4

38.9

6.9

6.4

75

62

39.3	39.3	38.9	39.3	39.2	38.8	38.7	38.7	40.2	40.1	38.2
6.0	6.0	6.4	6.0	6.1	6.5	6.6	6.6	5.2	5.2	7.1
75	62	43	25	12		4	11	14	18	24

35.9

36.8

37.6

9.4 8.5 7.7

75 60 37

17 28 50 70 81

Sta + π - Elev

945.33

16+81

+94 ~~±~~ Snowshoe Lane (for Grade Check With City)

17

+13

+40

✓

+63

1
Mo Knight - Carver to Highway
X-Section

~~check KP~~

Sta + π - Elev

BM 11.35 940.48

(929.13)

17

16+94 $\pm$ Snow shoe Lane

✓

✓

✓

✓

FA
RG
JH

Lt

Feb 16, 1960
32° Snowing
RT

2

Spike in PP 90' Lt Sta

4.1

31.7	31.2	31.7	31.7	31.6	31.5	31.4	31.2	31.4
2.8	2.3	2.8	2.8	2.9	3.0	5.1	5.3	6.1
30	22	17	10		5	10	23	33

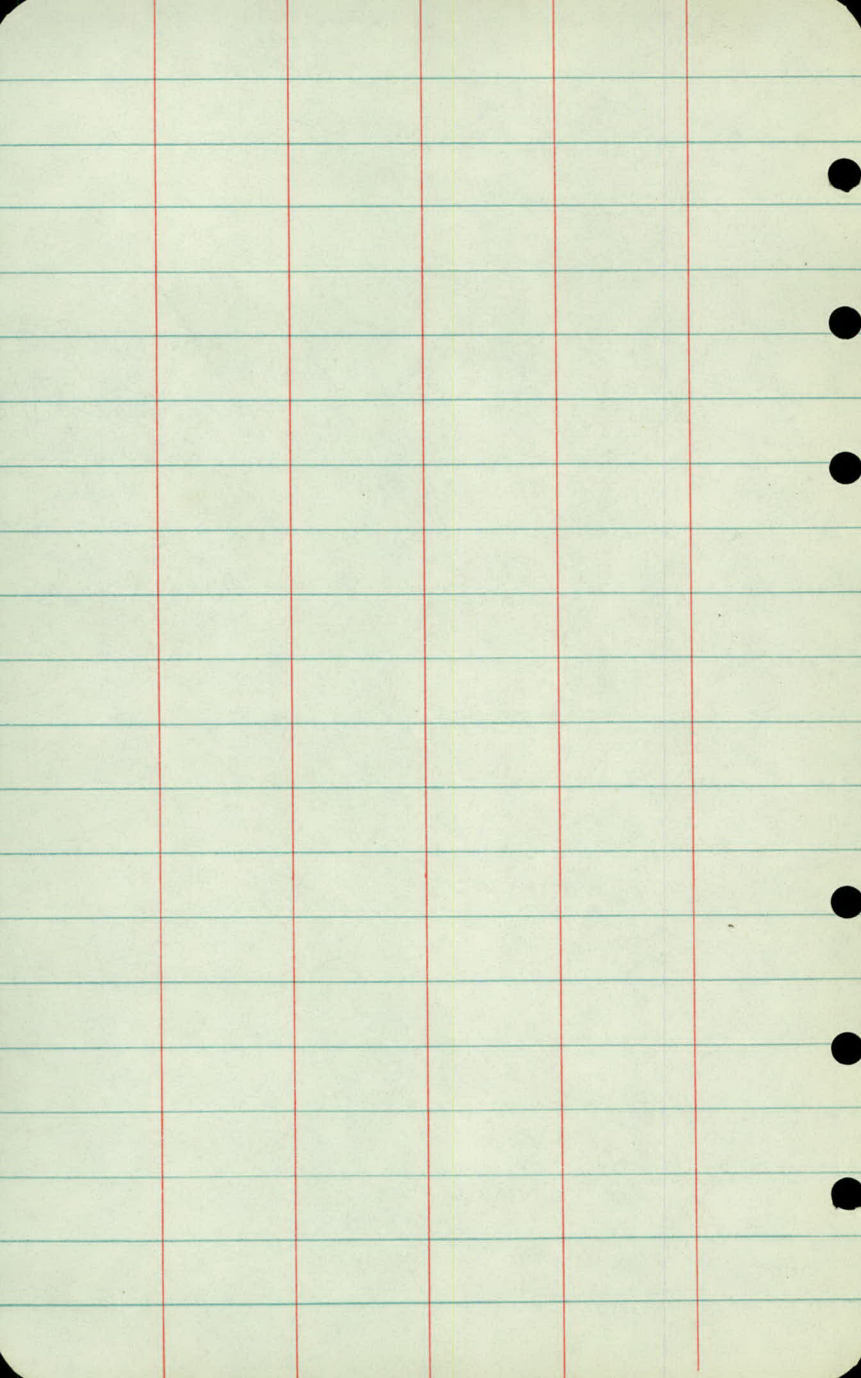
31.7	31.2	31.8	31.3		31.0	31.3	31.3
2.8	2.3	2.7	3.2		7.5	7.2	6.2
42	58	81	100		75	64	47

31.7	31.7	31.7	31.6
8.1	5.8	3.4	2.9
200	175	150	126

30.6	29.1	30.1
9.9	11.4	10.1
224	224	250

HO. 60' North

28.6	29.8
11.9	10.7
300	275



Jan 29, 1960

38.9	39.1	38.8	38.6	38.7	38.4	38.2	36.7	35.6	35.3	35.0
6.4	6.2	6.5	6.7	6.6	6.9	7.1	8.6	9.7	10.0	10.3
75	58	A2	27	15	A	12	30	51	75	

37.7	37.5	37.5	37.8	37.5	36.3	35.4	34.7	34.2	32.4	32.5
8.2	7.6	7.8	7.8	7.5	7.8	9.0	9.9	10.6	11.1	11.9
25	65	40	27	20	10	10	25	39	59	75

35.6	36.5	37.0	37.7	37.1	36.0	35.4	34.4	33.7	32.8	32.6
9.7	8.8	8.3	7.6	8.2	9.3	9.9	10.9	11.6	12.5	12.8
75	54	32	20	6		14	30	40	65	75

36.4	37.4	37.3	37.3	38.1	38.1	36.2	35.1	34.4	34.0
8.9	7.9	8.0	8.0	7.2	7.2	9.1	10.2	10.9	11.3
28	20	15	A	2		24	45	62	75

35.2	34.3
10.1	11.0
56	75

37.1	38.1	37.4	38.0	38.8	38.1	38.4	37.6	36.8	35.1
8.2	7.2	7.9	7.3	6.5	7.2	6.9	7.7	8.5	10.2
27	19	15	4	2		11	30	51	75

35.9	35.0	34.4
9.4	10.3	10.9
43	65	75

Sta + π - Elev

945.33

✓
17+81

✓
18

✓
TP 5.63 938.22 12.74 932.59

+28

✓
BM

9.09 938.22 9.09 929.13 (929.13)

Jan, 29, 1960

28

RT

LT

36.4	37.4	36.7	37.0	37.3	38.4	38.0	37.5	37.0	36.3	35.8
8.9	7.9	8.6	8.3	8.0	6.9	7.3	7.8	8.3	9.0	9.5
31	17	16	10	3		14	29	48	66	75

35.7	35.4	34.5
9.6	9.7	10.5
44	60	75

34.3	35.5	35.3	36.1	36.8	35.8	36.0	36.4	36.2	35.7
11.0	9.8	10.0	9.2	8.5	9.5	9.3	8.7	9.1	9.6
38	20	18	2		14	30	47	61	75

34.0	33.7
11.3	11.6
56	75

32.7	32.5	32.6	33.0	33.1	33.6	34.4	33.7	34.5	35.0
5.5	5.7	5.6	5.2	5.1	4.6	3.8	4.5	3.7	3.2
65	47	29	19	9		9	20	40	59

32.1
6.1
75

34.9
3.3
75

Spike in PP 90' LT Sta 18+73

Sta + π - Elev

938,22

18+64

✓

19

+38

✓

+62

63

4 Jan. 29, 1960

29

11

11

31.0	31.6	32.4	32.4	32.1	32.4	32.3	32.6	32.0
7.2	6.6	5.8	5.8	6.1	5.8	5.9	5.6	5.2
56	36	20	10		8	20	35	52

30.5

29.8

7.7
68

8.4
75

33.6

4.6
75

28.2	30.3	32.2	33.1	33.0	33.1	32.4	32.3	32.1	33.6
10.0	7.9	6.0	5.1	5.2	5.1	5.8	5.9	5.5	4.6
75	51	27	17	10		15	30	46	75

32.1	33.2	34.1	33.4	33.9	34.5	35.2	33.9	33.8	33.4	34.1
6.1	5.0	4.1	4.8	4.3	3.7	3.0	4.3	4.4	4.8	4.1
29	20	17	15	2		3	15	22	30	45

29.8

27.9

8.4
55

10.3
75

35.0

3.2
75

34.6

3.6
62

29.4	31.5	33.1	33.2	33.7	34.2	35.1	34.5	34.5	34.8	34.9
8.8	6.7	5.1	5.0	4.5	4.0	3.1	3.7	3.7	3.4	3.3
50	30	17	10	1		2	5	18	36	58

27.8

27.1

10.4
69

16.1
75

34.9

3.3
75

Sta + π - Elev.

938.22

20

✓

+39

+73

✓

21

TP 4.14 930.52 11.84 926.38

Jan. 29, 1960

30

RT

26.6	29.5	31.7	32.0	33.2	33.3	33.4	33.2	32.6	32.9
116	87	65	62	50	49	48	50	56	53
53	30	18	9		11	24	42	58	75

25.3

24.4

12.9
68

13.8
75

25.0

26.6

28.4

29.8

29.9

31.1

30.6

30.0

30.3

30.4

30.4

132	116	98	84	83	71	76	82	79	78	78
75	52	31	19	11		12	27	46	60	75

27.6

28.1

28.0

28.1

27.9

27.3

27.9

28.2

28.2

10.6	10.1	10.2	10.1	10.3	10.9	10.3	10.0	10.0
46	48	15	9		8	23	39	56

27.4

27.0

10.8
63

11.2
75

29.2

9.0
75

26.4

26.7

26.2

26.1

26.4

27.0

27.4

28.1

11.8

11.5

12.0

12.1

11.8

11.2

10.8

10.1

31

20

10

14

32

53

67

27.3

27.6

27.2

28.5

10.9
51

10.6
69

11.0
75

9.7
75

Sta + π - Elev.

930.52

21+32

+53

+79

Jan 28, 1960

31

RT



25.5	25.5	24.9	26.1	25.7	25.7	26.3	26.8	27.7
5.0	5.0	5.6	4.4	4.8	4.8	4.2	3.7	2.8
40	23	20	3		16	26	55	75

26.6	27.1	26.4
3.9	3.4	3.9
57	69	75

23.3	23.9	23.4	24.1	24.8	26.1	26.7	26.2	25.1
2.2	6.6	2.1	6.4	5.7	4.4	3.8	4.3	5.4
32	24	18	3		13	29	46	63

24.3	25.2	24.7
6.2	5.3	5.8
48	69	75

24.4
6.1
25

20.9	21.0	21.5	22.1	23.1	23.8	26.0	26.2	23.9	21.6	21.5
9.6	9.5	9.0	8.4	6.8	6.7	4.5	4.3	6.6	7.9	8.0
38	30	22	6	3		15	27	44	64	75

21.9	22.3
8.6	8.2
57	75

Sta + π - Elev
 930.52

22

✓

TP 12.75 933.07 10.20 920.32
 0.75
 12.00

+35

✓

+54

FA
RG
JS
JH

Jan. 22 1960
Feb. 1 1960
35° Clear Rt

32

Lt

18.9	19.9	20.9	22.5	22.6	22.4	22.4	23.1	23.9	24.4
11.6	11.1	9.6	8.0	7.9	8.1	8.1	7.4	6.6	6.1
30	26	7	3		14	34	49	61	75

18.6 18.6 19.0

→ 11.9 11.9 11.5
43 66 75
Top Boulder 10' Rt

18.2	17.8	18.5	19.4	18.8	18.5	19.8	22.1	25.6
14.9	15.3	14.6	13.7	14.3	14.6	13.3	11.0	7.5
23	18	7	3		2	13	30	48

16.5 16.5 16.1 16.2

→ 16.6 16.6 17.0 16.9
26 42 68 75

28.4 27.7
47 54
75 61

16.1 17.4 18.5 18.9 16.6 22.1 26.9 29.9 20.6

17.0	15.7	14.6	14.2	16.5	11.0	6.2	3.7	2.5
23	12	9	3		21	41	54	75

16.8 16.0 15.3 15.3

→ 16.3 17.1 17.8 17.8
29 39 65 75

Sta + π - Elev.

933.07

22+63

✓

+83

✓

23

✓

Feb 1, 1960

33

21

37

13.3	14.9	16.4	18.4	19.2	21.0	24.6	28.2	30.5
19.8	18.2	16.3	14.7	13.9	12.1	8.5	4.9	2.6
51	30	14	7		14	28	41	53

13.0	13.0							31.0
20.1	20.1							2.1
67	75							75

12.0	13.0	14.1	15.4	19.5	23.4	28.6	30.9	31.7
2.11	20.1	19.0	17.7	13.6	9.7	4.5	2.2	1.4
60	43	25	14		17	35	48	60

12.2								30.7
20.9								2.4
75								75

10.9	10.2	11.4	14.0	19.1	23.5	28.3	30.4	29.5
22.2	22.9	21.7	19.1	14.0	9.6	4.8	2.7	3.6
75	55	36	16		15	36	52	69

28.0
5.1
75

Sta	+	π	-	Elev
-----	---	-------	---	------

933.07

23+27

✓

+49

✓

TP	0.74	921.06	12.75	920.32	10 th Nail in 6"
TP	6.81	914.26	13.61	907.45	Elm

+67

✓

Feb 1, 1960

3/4

LT

RT

08.6	09.2	10.5	12.7	16.6	20.8	23.3	25.4	26.6
2.45	23.9	22.6	20.4	16.5	12.3	9.8	7.7	6.5
61	46	34	17		20	37	52	64

09.7
23.4
75

27.1
6.0
75

06.9	09.2	10.9	13.0	15.1	16.3	16.8	17.6	18.8
26.2	23.9	22.2	20.1	18.0	16.8	16.3	15.5	14.3
59	43	29.5	13		14	33	48	63

05.8
27.3
63

07.3
25.8
67

08.3
24.8
75

19.5
13.6
50

04.2	06.5	08.5	09.5	10.9	12.7	13.4	13.7	14.5	13.7
10.1	7.8	5.8	4.8	3.4	1.6	0.9	0.6	10.2	0.6
61	51	40	30	15		16	35	59	75

04.2
10.1
63

06.3
8.0
75

Sta + π - Elev.

914.26

24

+24

22

✓

59

TP 6.04 908.69 11.61 902.65

60

+42

+59

BM 8.80 916.25 1.24 907.45

+80

✓

Feb 1, 1960

35

14

84

0.4	0.6	0.4	0.3	0.3	0.1	0.1	0.2	0.9
12.9	12.7	11.9	10.0	8.0	7.2	7.2	7.1	7.4
75	59	43	20		16	33	51	75

0.2	0.3	0.5	0.9	0.8	0.7	0.3	0.8	0.2
14.1	14.0	13.8	13.4	12.5	11.6	11.0	10.5	10.1
54	41	30	17		23	44	66	75

00.0

14.3
75

99.3	99.6	99.9	99.6	99.8	00.4	0.1	0.2	0.2	0.2
9.4	9.1	8.8	9.1	8.9	8.3	7.6	6.6	5.5	4.5
75	61	42	32	17		18	37	57	75

99.1	99.3	99.6	99.9	00.0	00.1	0.5	0.2	0.3	0.5
9.6	9.4	9.1	8.8	8.7	8.0	7.2	5.8	4.4	2.8
75	63	50	37	20		20	40	54	75

Nail in 6" Elm Lt sta

0.5	0.7	0.3	0.7	0.3	0.8	0.6	0.2	0.8
13.8	13.6	13.2	13.6	13.0	12.5	11.7	11.1	9.5
42	31	16	5		12	27	38	58

0.1	0.5	0.3
14.2	14.8	15.0
55	70	75

08.3
8.0
75

Sfa + π - Elev

916.25

25+00

✓

+22

✓

T. B. M 11.38 915.13 12.53 903.72 903.72

+34

+58

+58
186

FK
RG
JH

Feb 1, 1960
Feb 2, 1960

36

Lt.

£

70368

04.5	05.9	06.1	07.3	08.0	09.2	10.0	10.5
11.8	10.4	10.2	9.0	8.3	7.1	6.3	5.8
38	20	7		15	30	43	56

04.0	03.3	02.4				11.9	11.1
12.3	13.0	13.9				4.4	5.2
51	65	75				75	64

09.0	10.2	10.2	11.0	11.7	11.7	12.0	11.2	11.1
7.3	6.1	6.1	5.3	4.6	4.6	4.3	5.1	5.2
43	29	21	11		11	21	36	50

07.5	05.9					10.9	10.9
8.8	10.4					5.4	5.4
61	75					75	65

26108

Spike in oak Lt. Sta @ FLine

05.1	07.1	09.8	10.4	11.1	11.5	11.1	10.1	09.4	09.9	10.0
10.0	8.0	5.3	4.7	4.0	3.6	4.0	5.0	5.7	5.2	5.1
75	61	42	25	8		9	30	47	67	75

07.6	08.3	08.6	08.6	08.6	08.1	06.8	06.3	06.2	07.2	07.4
75	6.8	6.5	6.5	6.5	7.0	8.3	9.8	8.9	7.9	7.7
46	37	24	11	2		18	36	52	67	75

06.1
03.4
02.0
01.7
01.5

Sta + π - Elev

915.13

25+86

26

✓

TBM 1.25 ^{904.95} ~~905.00~~ 11.38 903.75 (903.70)

+09 $\frac{1}{4}$ $\frac{1}{4}$ Line

+29

+46

2 Feb. 2, 1960

37

04.5	05.5	06.3	06.4	05.7	03.9	02.6	03.2	04.6	06.3
10.6	9.6	8.8	8.7	9.4	11.2	12.5	11.9	10.5	8.8
75	63	45	29	9		10	29	50	75

05.0	04.8	04.3	02.4	02.3	03.2	04.2	06.4
10.1	10.3	10.8	12.7	12.8	11.9	10.9	8.7
34	22	17		15	33	46	75

04.9	04.5	04.2
10.2	10.6	10.9
51	64	75

Spike in 12" W. oak Lt sta 26+08 @ Fedline

01.5	02.3	02.1	02.5	01.7	01.9	02.5	03.3	04.4	05.0	05.1
3.5	2.7	2.9	2.5	3.3	3.1	2.5	1.7	0.6	0.0	+0.4
75	53	33	19	8		17	35	50	66	75

99.5	99.6	00.0	00.4	00.6	00.7	00.8	00.1	01.0	02.6	04.0
5.5	5.4	5.0	4.6	4.4	4.3	4.2	4.9	4.0	2.4	1.0
75	56	41	21	9		6	12	26	50	75

98.0	98.4	99.0	98.8	98.7	98.5	98.3	99.0	00.3	01.8
7.0	6.6	6.0	6.2	6.3	6.5	6.7	6.0	4.7	3.2
75	54	36	21	11		15	35	58	75

Sta	+	+	-	Elev
-----	---	--------------	---	------

904.95
~~905.00~~

26+70

✓

TP	7.55	902.30	10.20	894.75
		902.35		894.80

+87

✓

27

✓

26 27 28 29

FK
RG
JS
JH

2

Feb 2, 1960
Feb 3, 1960

38

98.3	98.5	97.8	98.3	97.2	95.7	95.5	96.0	98.2
6.7	6.5	7.2	6.7	7.8	9.3	9.5	9.0	6.8
41	24	18	11		13	31	50	75

→ 98.1 97.2
6.9 7.8
51 100
Sta 22 2024

96.6	96.7	96.1	96.7	95.7	94.5	93.8	93.9	94.3	95.8
5.7	5.6	6.2	5.6	6.6	7.8	8.5	8.4	8.0	6.5
40	23	18	10		10	21	30	50	75

→ 96.4 96.5
5.9 5.8
67 75

95.6	95.1	94.6	94.5	95.0	94.1	93.9	93.0	93.9	94.9
6.7	7.2	7.7	7.8	7.3	8.2	8.9	9.3	8.4	7.4
49	30	20	15	11		11	33	57	75

→ 95.5 95.9
6.8 6.9
67 75

Sta

+

 π

-

Elev

902.30

~~902.35~~

27+28

✓

893.56

891.20

TP

2.36

~~893.61~~

11.10

~~891.25~~

+47

✓

+67

✓

Feb. 3, 1960

39

91.8

91.2

90.5

90.8

90.8

91.9

92.0

93.4

94.1

10.5

11.1

11.8

11.5

11.5

10.4

10.3

8.9

8.2

34

18

13

9

18

39

59

75

92.9

92.6

92.6

9.9

9.7

9.7

51

67

75

89.1

88.9

88.5

88.5

88.6

89.5

90.3

91.5

92.6

93.6

4.5

4.7

5.1

5.1

5.0

4.1

3.3

2.1

1.0

0.0

50

30

16

10

8

17

39

52

60

89.2

89.2

4.4

4.4

68

75

86.0

86.4

86.8

87.3

87.4

88.8

89.1

90.7

91.9

92.5

7.6

7.2

6.8

6.3

6.2

4.8

4.5

2.9

1.7

1.1

49

32

15

8

14

27

44

61

75

86.1

86.3

7.5

7.3

62

75

94.3

10.7

75

Sta + ~~x~~ - Elev.

893.56

~~893.61~~

27 + 82

28

+ 30

+ 51

+ 68

T.P. 10.11 901.18 2.49 891.07
~~901.23~~ ~~891.12~~

+ 84

Feb 3, 1960

40

82.2	84.2	84.0	84.6	85.6	85.8	86.5	87.6	88.2	89.6	90.8	91.6
24	26	20	20	28	7.1	6.0	5.6	4.0	2.8	2.0	
75	55	33	17	9		18	31	49	64	75	

82.2	83.2	83.5	84.2	84.6	85.0	86.1	86.4	87.0	89.1		
11.4	10.4	10.1	9.4	9.0	8.6	7.5	7.2	6.6	4.5		
75	56	45	27	11		17	37	56	75		

81.1	81.5	82.3	83.3	83.7	84.3	85.1	85.5	85.6	86.1	86.5	
12.5	12.1	11.3	10.3	9.9	9.3	8.5	8.1	8.0	7.5	7.1	
75	69	52	28	13		18	28	49	70	75	

82.7	83.2	84.2	85.4	86.1	86.4	86.5	87.0	86.7	86.3	85.7	
10.9	10.4	9.4	8.2	7.5	7.2	7.1	6.6	6.9	7.3	8.4	
75	65	49	27	11		15	24	35	55	75	

88.2	86.6	87.2	88.5	89.0	89.5	89.5	89.4	88.1	86.3	84.6	
5.4	7.0	6.4	5.1	4.6	4.1	4.1	4.2	5.5	7.3	9.0	
75	71	53	32	12		15	32	42	61	75	

91.1	92.3	92.6	93.2	93.6	93.7	93.1	91.4	89.6	88.0	86.2	
10.1	8.9	8.6	8.0	7.6	7.5	8.1	9.8	11.6	13.2	15.0	
75	62	47	32	16		11	27	40	50	58	

82.9
83.0
84.5
183 182 16.7
75 72 63

Sta + π - Elev.

901.18
~~901.23~~

29+00

✓

+07

✓

+20

✓

7
15
20

34
48
62

Feb 3, 1960

92.8	94.9	95.8	97.2	97.3	96.2	95.7	92.1	99.8	96.8
8.4	6.3	5.4	4.0	3.9	5.0	6.0	8.5	11.4	14.4
75	50	37	21	14		9	25	39	55

92.0	92.6	94.6
19.2	18.6	16.6
75	69	63

95.5	96.1	96.9	97.6	96.5	94.9	93.3	90.9	98.4
5.7	5.1	4.3	3.6	4.7	6.3	7.9	10.3	12.8
53	39	26	12		10	21	34	52

96.0	97.1	96.6
5.2	4.1	4.6
59	69	75

91.3	92.4	96.4
19.9	18.8	14.8
75	68	56

97.1	97.3	97.6	96.3	95.1	92.9	90.3	98.2	94.9
4.1	3.9	3.6	4.9	6.1	8.3	10.9	13.0	16.3
45	29	17	9		15	31	43	59

97.3	94.3	90.3	90.2
3.9	1.9	0.9	1.0
52	61	69	75

90.4	90.9
20.8	20.3
75	71

Sta

+

+

-

Elev.

901.18

~~901.23~~

29+34

✓

+48

✓

+62

Feb. 3, 1960

91.2	99.1	98.0	96.8	95.0	92.6	90.7	87.5	83.8
0.0	2.1	3.2	4.4	6.2	8.6	10.5	13.7	17.4
75	55	39	29	15		12	30	50

78.6	76.8	80.9
22.6	22.4	20.3
75	72	64

99.0	96.1	92.9	91.1	89.3	85.9	82.2	79.2
22.5	18.3	14.1	11.9	15.3	19.0	22.0	
61	41	22	10	21	39	53	

90.9
0.3
75

77.4	77.7
23.5	23.5
75	61

91.8	96.6	93.0	89.8	86.0	83.0	80.1	78.5
3.4	4.6	8.2	11.4	15.2	18.2	21.1	22.7
67	53	35	20	17	23	36	

98.4
2.8
75

77.0	76.8	77.3
24.2	24.4	23.9
75	65	51

Sta + π - Elev.

901.18

~~901.23~~

29+72

✓

+86

✓

888.37

888.25

TP

0.12

~~888.12~~

12.93

~~888.30~~

30

✓

Feb, 3, 1960

43

RT

90.7

88.0

85.6

83.7

79.9

78.9

77.0

10.5

13.2

15.6

17.5

21.3

22.4

24.2

40

25

12

14

27

45

93.3

96.0

76.9

76.6

7.9

5.2

24.3

24.6

57

75

75

61

87.7

84.8

81.9

80.2

78.4

76.9

76.7

13.5

16.4

19.3

21.0

22.8

24.3

24.5

49

32

14

12

30

51

90.2

91.9

77.0

11.0

9.3

24.2

64

75

75

84.6

82.2

80.3

79.3

78.2

76.9

76.8

77.0

77.4

3.8

6.2

8.1

9.1

10.2

11.5

11.6

11.4

11.0

65

48

29

14

14

36

59

75

86.2

2.2

75

Sta

+

π

-

Elev.

888.57

~~888.42~~

30 + 09

✓

+ 28

✓

+ 43

2 Feb 3, 1960

RT

44

83.3	80.8	79.0	77.4	76.8	76.6	76.9	77.1	77.7
5.1	7.6	9.4	11.0	11.6	11.8	11.5	11.3	10.7
66	49	31	15		14	35	51	75

84.2

4.2
75

78.1	78.2	77.5	76.9	76.3	77.1	77.0	77.6	78.0
9.7	10.2	10.9	11.5	12.1	11.3	11.4	10.8	10.4
72	54	34	14		11	29	52	75

79.4

9.0
25

78.7	78.1	77.5	78.2	78.3	78.3	77.8	77.9
9.7	10.3	10.9	10.2	10.1	10.1	10.6	10.5
75	53	36	19		9	23	39

79.0

9.4
75

78.3

10.1
51

Sta	+	π	-	Elev.
-----	---	-------	---	-------

888.37

~~888.42~~

30+66

✓

+ 82

✓

31

✓

TP

11.35 ~~895.75~~

895.70

4.02

884.35

~~884.40~~

Feb 3, 1960

45

51

11.
79.2
80.2

80.9

81.0

81.1

82.0

81.3

81.3

82.0

9.2 8.2 7.5 7.4 7.3 6.4 7.1 7.1 6.4
67 49 26 9 5 19 35 45

78.4

10.0
7.5

82.5

82.6

81.9

5.9 5.8 6.5
75 69 61

82.0

81.8

82.6

83.3

83.6

83.8

83.6

83.4

83.4

84.3

6.4 6.6 5.8 5.1 4.8 4.6 4.8 5.0 5.0 4.1
68 63 52 29 13 12 20 35 46

82.2

6.2
7.5

85.2

85.3

84.3

3.2 3.1 4.1
75 69 63

83.1

83.0

83.3

84.2

84.6

85.0

85.4

85.1

86.7

5.3 5.4 5.1 4.2 3.8 3.4 3.0 2.3 1.7
75 63 41 17 19 32 41 54

88.0

87.8

0.4 0.6
75 67

Sta + π - Elev.

895.70
~~895.75~~

31 + 24

✓

+ 38

✓

+ 54

✓

903.34

BM 12.38 ~~903.39~~ 472 891.03 ~~891.01~~ 890.96

54 66 77 86

Feb 3, 1960

46

83.6	84.3	84.5	84.7	85.9	86.9	88.8	89.9
12.1	11.4	11.2	11.0	9.8	8.8	6.9	5.8
47	26	9		9	26	49	64

83.2	83.2						90.6
12.5	12.5						5.1
61	75						75

83.4	84.3	85.5	85.8	86.3	86.9	88.3	88.9	91.1
12.3	11.4	10.2	9.9	9.4	8.8	7.4	6.8	4.6
53	39	25	11		14	34	44	56

83.2							83.6
12.5							2.1
75							75

83.7	85.7	88.1	89.3	90.8	91.6	92.2	93.8	95.0
12.0	10.0	7.6	6.4	4.9	4.1	3.5	1.9	0.7
53	40	24	12		10	27	49	60

83.7						97.7	95.7
12.6						+2.0	0.0
75						75	64

spike in PPL/st. 32 + 89

Sta + [↑] - Elev

903.34

~~903.39~~

31+66

✓

+77

✓

+86

✓

BM 13.04 904.00
~~904.05~~ 12.38 891.01 (890.96)

Feb 3, 1960

47

86.3	89.8	93.5	95.1	96.3	96.2	96.1	98.5
170	13.5	98	8.2	7.0	2.1	6.6	4.8
43	29	14		16	30	46	60

83.3	83.1						01.3
20.0	20.2						2.0
59	75						75

83.5	88.1	92.0	95.2	97.2	98.1	97.6	00.5	02.6
19.8	15.2	11.3	8.1	6.1	4.6	5.7	2.8	0.7
58	41	26	14		18	40	62	75

82.9							
20.4							
75							

83.6	87.4	92.0	95.8	98.0	99.0	98.3	99.9	02.0
19.7	15.9	11.3	7.5	5.3	4.3	5.0	3.4	0.9
60	28	27	15		20	37	55	69

48

83.0							03.9
20.3							1.0.6
75							75

Spike in PPLT Sta 32+09

Sta + π - Elev

904.00

~~904.15~~

32+00

✓

+09

+22

✓

+37

893.28

890.96

TP

2.32

~~893.28~~

1304

891.01

PH Feb 4 1960 48
 RG
 JS
 JH

90.5	93.2	95.3	96.6	97.3	97.7	97.5	98.3	99.8
13.5	10.8	8.7	7.4	6.7	6.3	6.5	5.7	3.2
55	45	27	12		15	27	39	61

89.5							93.6	92.6
14.5							0.4	1.4
75							7.5	70

99.3	90.1	92.5	94.1	94.6	95.5	96.3	97.2	99.2	92.7
14.7	13.9	11.5	9.9	9.4	8.5	7.7	6.8	4.8	1.3
75	54	38	23	8		15	38	51	75

85.3	87.0	90.5	92.0	92.1	93.5	95.6	98.8	99.5
18.7	17.0	13.5	12.0	11.9	10.5	8.4	5.2	4.5
58	42	24	13		15	29	49	67

85.9								90.2
18.1								3.8
75								75

81.0	82.7	85.6	87.7	88.8	90.5	94.8	96.0	97.1
23.0	21.3	18.4	16.3	15.2	13.5	9.2	8.0	6.9
55	39	23	10		17	37	51	60

80.2	81.1							98.3
23.8	22.9							5.7
57	75							75

Sta + Δ - Elev

893.28

~~893.23~~

32+47

✓

+57

✓

+69

888.17

~~888.22~~

13.52

879.76

~~879.81~~

TP

8.41

69

70

12

90

Feb 4, 1960

49

RT

79.3	80.4	82.1	85.1	86.6	87.3	86.9	87.7	89.5
140	129	112	8.2	6.7	6.0	6.4	56	38
41	39	30	12		9	10	17	20

79.9	80.5	80.4		93.1	92.7	92.5	91.7
13.4	12.8	12.9		0.2	0.6	0.8	1.6
56	72	75		75	56	40	34

79.3	78.3	79.2	82.2	84.1	85.3	84.8	85.6	86.8
140	150	141	11.1	9.2	8.0	8.5	7.7	6.5
44	28	26	11		10	11	18	20

79.6	78.9	78.5		89.4	88.9	89.0	98.1
137	144	148		3.9	4.4	4.3	4.6
59	67	75		75	68	55	38

78.1	77.8	76.9	78.7	80.7	81.9	81.9	83.6	84.8
15.2	15.5	16.4	14.6	12.6	11.4	11.4	9.7	8.5
40	28	13	8		9	13	19	20

79.2	78.7	78.8		85.4	85.3	85.4	85.4
14.1	14.6	14.5		7.9	8.0	7.9	7.9
42	55	100		75	68	48	33

Sta

+

π
888.17
~~888.22~~

-

Elev

32+78

✓

+ 82

✓

+ 90

✓

Feb 3, 1960

50

11

51

18.7

11.0

16.8

15.7

11.5

18.9

19.8

81.8

84.6

84.7

9.5

11.2

11.4

12.5

10.7

9.3

84

64

3.6

3.5

33

32

20

3

10

15

19

20

38

19.6

19.6

19.5

19.5

84.3

84.1

84.0

8.6

8.6

8.7

8.7

3.9

4.1

4.2

34

55

69

75

75

68

54

18.3

16.1

16.4

16.2

15.4

17.1

18.9

81.1

84.5

9.9

11.5

11.8

12.0

12.8

11.1

9.3

7.1

3.7

30

29

18

9

3

14

19

21

80.1

80.1

80.0

83.5

83.3

83.6

84.7

8.1

8.1

8.2

4.7

4.8

4.6

3.5

38

56

75

75

69

56

38

80.8

17.1

15.8

15.6

14.8

14.8

15.6

17.1

19.4

7.4

11.1

12.4

12.6

13.4

12.4

12.6

11.1

8.8

36

26

25

14

5

8

15

19

81.3

81.0

82.4

82.2

82.8

82.2

84.5

6.9

7.2

5.8

6.0

5.4

4.0

3.7

50

75

75

67

52

37

22

Sta + ^x - Elev

888.17

~~888.22~~

33

✓

TP ✓

8.88

888.13

~~888.18~~

4.92

879.25

~~879.30~~

+15

✓

✓

+40

Feb 4, 1960

LT

RT

51

81.6 78.3

74.6

74.4

74.2

73.3

74.2

77.0

80.6

6.6 9.9

13.6 13.8

14.0

14.9

14.0

11.2

7.6

25.5

37 26

20 9

7

15

21

25.5

25.5

25.5

82.6

82.3

82.4

80.6

80.7

81.0

82.5

83.6

5.6

5.9

5.8

7.6

2.5

2.2

5.7

4.6

4.3

6.1

7.5

7.5

6.9

5.1

3.9

27.5

Spika in Gate Post Lt 346 324 ?

79.2

76.9

74.0

72.5

72.4

72.7

71.4

71.1

8.9 11.2

14.1

15.6

15.7

15.4

16.7

16.4

23 21

17

15

3

13

16

16

80.6

84.0

83.9

83.8

79.6

81.8

77.9

73.0

7.5

4.1

4.2

4.3

8.5

6.3

10.2

15.1

31 45

5.9

7.5

4.1

2.6

2.5

1.7

78.3

77.9

77.9

9.8

10.2

10.3

5.6

6.9

7.5

82.1

77.4

71.6

70.0

70.1

70.2

68.8

70.4

72.8

6.0 10.7

16.5

18.1

18.0

17.9

19.3

17.7

15.3

33 24

14

12

7

16

19

25

69.1
19.0
18

Sta + π - Elev

888.13

~~888.18~~

33440

X

+55

✓

✓

+67

881.41

~~881.46~~

9.50

878.63

~~878.68~~

T.P.

2.78

Feb 4, 1960 52

14

85.5

26
75

86.3

18
54

85.1

30
44

77.0

11.1
29

75.9

12.2
34

72.6

4.5
48

82.4

5.7
63

80.0

7.2
75

79.7

8.4
27

72.4

15.7
15

68.4

19.7
9

68.4

19.7
9

68.4

19.7
9

67.5

20.6
16

68.1

20.0
18

83.4

4.7
35

85.1

3.0
52

85.7

2.4
60

85.6

2.5
75

74.1

14.0
30

72.6

15.5
29

70.5

17.6
25

69.3

18.8
20

73.1

15.0
35

81.1

2.0
48

68.8

19.3
69

67.9

20.2
75

75.1

13.0
20

69.2

18.7
11

67.1

21.0
8

67.3

20.8
10

67.0

21.1
16

66.4

21.7
20

68.3

19.6
22

68.3

19.8
22

80.1

8.0
27

82.5

5.6
34

83.0

5.1
48

83.9

4.2
61

84.1

4.0
75

67.5

20.6
52

70.2

17.9
34

73.0

15.1
28

70.5

17.6
25

65.5

22.6
68

63.9

24.2
75

Sta

+

881.41
~~881.46~~

-

Elev

33+84

✓

✓

34

✓

✓

Feb 4, 1960 53

24

R1

74.9	71.9	65.8	65.1	65.5	65.8	64.7	67.5
6.5	9.5	15.6	16.3	15.9	15.6	6.7	13.9
19	17	9	5		9	16	20

75.9	78.0	80.1	80.8	62.3	64.6	66.2	69.5
5.5	3.4	1.3	0.6	19.1	16.8	15.2	11.9
25	35	55	75	58	42	32	25

60.3	57.6	56.9
21.1	23.8	24.5
71	72	75

69.9	66.9	64.0	63.6	64.1	64.0	62.8	63.2	64.5
11.5	14.5	17.4	17.8	17.3	17.4	18.6	18.2	16.9
15	12	9	6		9	16	20	23

72.9	74.8	76.2	76.9	55.4	58.3	60.6	62.6
9.0	6.6	5.2	4.5	26.0	23.1	20.8	18.8
30	51	62	75	57	53	40	29

55.2	53.5
26.2	25.9
69	75

Sta	+	π	-	Elev
-----	---	-------	---	------

		881.41		
		881.46		

34+12				
-------	--	--	--	--

				X
--	--	--	--	---

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--	--	--	--	--

T.P.	0.39	868.12	13.68	867.83
		868.17		867.78

--	--	--	--	--

124				
20				
28				
104				

--	--	--	--	--

--	--	--	--	--

12				
----	--	--	--	--

27				
----	--	--	--	--

12				
----	--	--	--	--

70				
----	--	--	--	--

£ Feb. 4, 1960

54

LT

RT

66.7	64.9	62.1	62.4	62.9	62.9	61.6	60.0
14.7	16.5	18.7	19.0	18.5	18.5	19.8	21.4
26	14	11	7		10	19	30

68.9	70.2	72.2
12.5	11.2	9.2
39	52	64

52.8	53.6	53.7	52.9
28.6	27.8	27.7	24.5
68	62	47	40

73.4
8.0
75

51.3
20.1
75

Step

65.0	62.6	60.9	60.5	61.3	61.5	61.5	61.1	57.4	52.7
3.1	5.5	7.2	7.6	6.8	6.6	6.6	7.0	10.7	15.4
54	37	25	16	8		11	14	18	27

67.8
0.3
75

51.4	52.2	52.5
16.7	15.9	15.8
52	49	34

50.1	49.8
18.0	18.3
62	75

Sta + T - Elev.

868.12
~~968.11~~

34+42

54.77

+70

TP

3.20

857.77

~~857.82~~

13.55

854.57

~~854.62~~

35

TP

3.73

860.77

~~860.82~~

0.73

857.04

~~857.09~~

Feb 4, 1960

55

Lt

Rt

58.1	56.1	55.4	59.8	60.1	59.5	55.1	50.3	50.8
10.0	12.0	9.7	8.3	8.0	8.0	13.0	17.8	17.3
45	32	22	13		10	15	27	41

60.0	62.0
8.1	6.1
60	75

49.4	49.1	48.9
18.7	19.0	19.2
75	63	44

50.0	52.3	56.9	57.5	57.7	57.7	55.2	49.4	49.0
18.1	14.8	11.2	10.6	10.4	10.4	14.9	18.7	19.1
24	18	13	10		7	13	19	24

49.2	48.1	49.4	51.0	49.1	48.9	48.5	49.3
18.9	20.0	18.7	17.1	19.0	19.2	19.6	18.8
30	45	59	75	75	62	45	36

46.3	51.1	55.8	55.1	55.8	55.9	49.3	48.4	48.0	48.2
11.5	6.1	20	2.1	2.0	1.9	8.5	2.4	9.8	9.6
26	17	12			7	16	24	38	50

45.2	44.1	42.6	40.7	41.6	48.3	48.3
12.6	13.7	15.2	17.1	16.2	9.5	9.5
42	56	75	100	115	75	66

Rock Rt Sta 36 + 40

Sta + Δ - Elev.

860.77
~~860.82~~

35 + 35

✓

+ 58

✓

+ 65 Culvert Buried!

✓

72

+ 90

FK
RG
JS
JH

Feb 5, 1960 56
30° Cloudy

45.3	49.0	53.2	54.2	54.3	54.1	57.6	50.0	48.0
15.5	11.8	7.6	6.6	6.5	6.7	9.2	10.8	12.8
23	17	12	8		7	10	14	18

44.7	43.5	42.4	41.4	40.0	38.8	48.6	48.0	47.6	47.5
16.1	17.3	18.4	19.4	20.8	22.0	12.2	12.8	13.2	13.3
27	41	54	75	100	125	75	55	40	24

45.8	48.5	53.0	53.5	53.7	53.5	54.9	47.4	46.7
15.0	12.3	7.8	7.3	7.1	7.3	9.9	13.4	14.1
22	15	9	6		6	11	16	20

43.7	42.6	41.2	39.9	38.4	48.3	48.0	47.6	47.1
17.1	18.2	19.6	20.9	22.4	12.5	12.8	13.2	13.7
36	52	75	100	125	75	61	47	33

42.6	43.5	52.4	53.4	53.7	53.5	50.2	46.8	47.0
18.2	17.3	8.4	7.4	7.1	7.3	10.6	14.0	13.8
25	19	9.5	6		6	11	16	25

43.4	43.5	43.0	48.9	47.8	48.0	47.0
17.4	17.3	17.8	11.9	13.0	12.8	13.8
26	31	43	75	59	46	29

38.0	38.1	40.7	41.8
22.8	22.1	20.1	19.0
125	100	75	58

Sta

+

860.77
~~860.82~~

-

Elev.

35+72

✓

✓

+90

✓

X

Feb 5, 1960

57

21

21

46.9

49.3

52.8

53.5

53.8

53.6

49.9

47.3

47.0

13.9

11.5

8.0

7.3

7.0

7.2

10.9

13.5

13.8

18

14

10

5.5

7

12

17

23

43.0

41.6

43.1

42.9

49.4

48.2

47.7

48.5

17.8

19.2

17.7

18.4

11.4

12.6

13.1

12.3

29

34

39

53

75

61

53

38

38.0

39.1

40.6

41.2

22.8

21.7

20.2

19.6

125

100

75

65

44.6

49.2

53.5

54.0

54.2

54.0

48.9

49.1

49.0

16.2

11.6

7.3

6.8

6.6

6.8

1.9

11.7

11.8

24

15

9

5

8

15

23

32

42.6

42.1

40.7

40.4

40.1

40.3

40.6

18.2

18.7

20.1

10.4

10.7

10.5

12.2

38

51

61

71

67

52

39

Ditch

35.7

38.1

39.1

39.5

25.1

22.7

21.7

21.3

109

92

75

70

51.4

9.4

75

35.5

36.5

35.7

25.3

24.3

25.1

119

125

143

Sta

+

T

-

Elev

860.77
~~860.82~~

36

✓

+17

✓

+31

✓

X

31
49
58
67
77

E Feb 5, 1960

58

11

54

44.8	49.1	53.6	54.3	54.4	54.3	51.6	49.6
16.0	11.7	7.2	6.5	6.4	6.5	9.2	11.2
22	15	9	5		8	12	27

43.2	42.4	42.5	41.1	39.3	38.2	37.4	31.5	31.5	49.5
17.6	18.4	18.3	19.7	21.3	22.1	24	9.3	9.3	11.3
30	42	52	75	100	75	65	53		38

44.1	46.2	50.8	54.5	55.0	55.0	52.3	50.8	51.1	50.8
16.7	14.6	10.0	6.3	5.8	5.8	8.5	10.0	9.7	10.0
34	21	12	7		9	13	17	26	32

42.3	41.4	41.1	40.1	38.9	34.6	32.6	34.8	52.3
18.5	19.4	19.7	20.7	21.9	3.2	4.2	6.0	8.5
52	68	75	100	125	75	73	61	42

42.0	46.5	49.1	55.1	55.1	55.1	53.0	52.4	53.0	57.5
17.8	14.3	11.7	5.7	5.1	5.1	7.8	8.4	7.8	6.3
44	23	17	7		9	13	23	26	36

41.7	40.5	39.9	38.5		60.8	59.7	57.8
19.1	20.3	20.9	22.3		2.0	1.1	3.0
62	75	100	125		60	54	44

Sta + π - Elev

860.77
~~860.82~~

36+44

✓

+58

✓

+69

Feb 5, 1960

59

LT

RT

46.8	50.6	55.9	56.3	56.6	55.4	55.0	54.5	55.2
14.0	10.2	4.9	4.5	4.2	5.4	5.8	6.3	5.6
26	16	7		8	11	18	20	22

44.4	42.6	41.0	40.1	39.7	39.1	59.1
16.4	18.2	19.8	20.7	21.1	21.7	1.7
39	57	68	75	100	125	30

57.0	49.4	52.2	51.4	51.6	51.7	51.2	57.0	57.1	58.4
3.8	11.4	8.6	3.4	3.2	3.1	3.6	3.8	3.1	2.4
35	20	15	8		9	13	18	21	24

44.6	42.0	40.4	40.2	39.8	60.8
16.2	18.8	20.4	20.6	21.0	0.0
46	61	75	100	125	28

49.5	52.4	54.4	58.4	58.8	59.0	58.7	59.2	59.2
11.3	8.4	6.4	2.4	2.0	1.8	2.1	1.6	1.6
32	19	14	8		8	13	18	22

45.9	43.1	41.4	39.8	40.0	60.1
14.9	17.7	19.4	21.0	20.8	0.1
46	63	75	100	125	28

Sta	+	860.77 860.82	-	Elev
-----	---	-----------------------------	---	------

36+77

✓

TP	13.31	873.86	0.27	860.55
----	-------	-------------------	------	-------------------

TP	7.22	876.04	4.99	868.87
----	------	-------------------	------	-------------------

36+31

+ 44

+ 58

Feb 5, 1960 60

14

54

50.9	54.3	40.4	59.1	59.6	59.9	59.8	60.6
9.9	6.5	4.4	1.7	1.2	0.9	1.0	0.2
32	19	13	9		9	13	17

41.0	44.3	42.8	40.6	40.4
13.8	16.5	18.0	20.2	20.4
19	64	75	100	115

62.4	63.7
13.6	12.3
69	75

63.1	65.7	68.5	69.5	71.2
12.9	10.3	75	65	48
44	51	59	70	75

66.7	71.0	71.7	74.4
9.3	5.4	3.3	1.6
37	48	53	62

74.0	73.6	72.6	74.5
2.0	2.4	3.4	1.5
75	73	71	68

Sta

+

T

-

Elev.

876.04

~~876.09~~

36+69

✓

+ 77

37

12

TP

10.00

880.53

~~880.58~~

5.51

870.53

~~870.58~~

19 7 19 7

60 2 60 2

Feb 5, 1960

61

21

B1

64.8 68.1 70.0 74.5

11.2 7.7 6.0 1.5
35 39 43 50

74.2 74.0 72.1 71.5 71.7 74.5

1.8 2.0 3.3 3.5 4.3 1.5
75 72 69 62 57 53

62.2 66.1 71.4 73.0 74.4

13.8 9.9 4.6 3.0 1.6
29 41 55 68 75

60.5 62.5 63.1 62.2 62.5 62.3 61.9 62.3 64.2

15.5 13.5 12.9 13.8 13.5 13.7 14.1 13.7 11.8
17 14 9 6 8 11 13 16

58.2 54.3 50.5

17.8 21.7 25.5
24 38 55

73.5 69.6 68.5 67.1

2.5 6.4 7.5 8.9
40 32 26 23

42.4 42.5 46.8

33.6 33.5 29.2
110 100 75

13.8 72.4 13.0 72.4

2.2 3.6 3.0 3.6
44 51 56 60

13.2

2.8
2.5

Sta + ¹ - Elev

880.53

~~880.58~~

37+19

✓

✓

+37

✓

✓

TP

6.94

885.44

~~885.49~~

2.03

878.50

~~878.55~~

2 Feb 5, 1960 62

LT

RT

64.9	66.2	64.4	64.8	64.9	64.4	65.0
15.6	14.3	16.1	15.7	15.6	16.1	5.5
16	13	7		9	10	13

63.6	62.1	59.1	66.9	64.5	73.4	68.0
16.9	18.4	21.4	36	55	7.1	12.5
25	28	37	41	32	25	16

45.2	45.4	50.0	55.0	71.8	79.5	80.0
35.3	35.1	30.5	25.5	2.7	1.0	0.5
115	100	75	53	54	59	75

65.1	61.0	61.3	66.4	66.9	66.8	66.5	64.5	71.7
15.4	13.5	13.2	14.1	13.6	13.7	14.0	13.0	8.8
29	22	11	7		9	10.5	13	17

61.6	58.3	55.5	69.2	78.6	77.6	75.4
18.9	22.2	25.0	1.3	1.9	2.9	5.1
41	54	66	50	42	31	22

48.7	53.7	80.1	81.3
31.8	26.8	0.4	+0.8
100	75	55	75

Sta	+	T	-	Elev
		885.44		
		885.49		

37+60

✓

✓

+82

✓

✓

Lt

Feb 5, 1960

RT

63

10.3

10.4

9.2

9.7

9.9

9.7

9.7

11.3

15.1
18

15.0
11

16.2
8

15.7

15.5
8

15.7
10

15.7
12

14.1
14

11.0

9.8

6.7.2

14.4
22

15.6
25

18.2
35

8.4

19.1

17.2

14.3

8.0
41

6.3
31

8.2
21

11.1
18

59.3

60.8

64.2

28.1
75

24.6
60

21.2
46

81.3

82.4

83.4

4.1
54

3.0
66

2.0
75

69.9
15.5
28

12.8
12.6
15

12.4
13.0
11

11.4
14.0
8

12.0
13.4

12.3
13.1
8

11.8
13.6
11

12.9
12.5
13

15.0
10.4
16

67.1

63.5

61.2

18.3
42

21.9
58

24.2
67

82.6

81.5

80.6

79.6

2.8
55

3.9
41

4.8
38

5.8
25

59.3

26.1

84.1

1.3
75

Sta + π - Elev

885.44

~~885.49~~

38

✓

+14

✓

✓

29

53

70

Feb 5, 1960

64

14.9 14.5 13.3 13.3 13.9 13.9 13.3 13.3 13.9

10.5 10.9 12.1 12.1 11.5 11.5 12.1 12.1 11.5
15 12 11 9 8 9 10 11

11.9 10.8 10.9

13.5 16.6 20.5
24 38 56

10.9

24.5
75

81.1 81.8 83.1 84.8

4.3 3.6 1.7 0.6
32 36 62 75

14.4 15.1 15.4 14.3 15.1 14.8 14.5 15.9 14.3

11.0 9.7 10.0 11.1 10.3 10.6 10.9 9.5 6.1
17 14 11 10 7 8 13 16

12.2 10.2 10.1

13.2 15.2 19.3
27 35 56

82.6 81.6 14.1 18.1

2.8 3.8 6.3 6.7
50 31 26 19

61.1 62.4

24.3 23.0
75 71

84.0 84.9

1.4 0.5
66 75

Sta

+

T

-

Elev

885.44

~~885.49~~

38+29

✓

+53

✓

13.4
2.7
~~8.7~~

+75

✓

✓

3.3
7.6

Feb 5, 1960 65

11

11

73.3

75.6

76.4

75.6

76.3

76.3

77.4

78.1

80.7

81.7

12.1

9.8

9.0

9.8

9.1

9.1

8.0

7.3

4.7

3.7

27

16

13

10

9

3

20

22

26

70.9

68.0

64.4

62.8

85.4

83.9

82.3

14.5

17.4

21.0

22.6

0.0

1.5

3.1

38

52

67

75

75

63

45

74.2

76.7

77.6

76.9

77.8

77.5

80.6

81.6

82.8

11.2

8.7

7.8

8.5

7.6

7.9

4.8

3.8

2.6

30

16

13

10

11

15

23

43

72.0

68.3

65.0

64.2

85.4

84.7

13.4

17.1

20.4

21.2

0.0

0.7

40

57

71

75

75

64

73.2

76.5

77.2

78.3

78.4

78.8

78.8

81.2

82.1

83.3

12.2

9.9

8.2

7.1

7.4

6.6

6.6

4.2

3.3

2.1

41

27

19

13

11

12

16

23

43

69.0

64.2

85.8

85.0

16.4

21.2

10.4

0.4

59

75

75

63

Sta	+	π	-	Elev
		885.44		
		885.49		

38+97

✓

✓

BM	13.26	886.58		873.32	
		886.62	12.12	873.37	873.36

39 $\neq$ Ditch

✓

+09 Edge BT & Shoulder

Feb. 5, 1960

66

LT

RT

74.8

76.5

77.3

78.0

79.2

79.4

80.1

81.4

82.4

10.6

8.9

8.1

7.4

6.2

6.0

5.3

4.0

2.8

37

21

16

13

7

12

16

31

73.2

72.5

73.2

85.7

85.0

84.0

12.2

12.9

12.2

10.3

0.4

1.4

48

53

58

75

66

49

70.0

71.1

15.4

13.7

75

65

R.R. Spike in 36" Cell

74.2

75.5

76.4

77.9

79.1

79.6

80.0

80.8

80.7

12.4

11.1

9.9

8.7

7.5

7.0

6.6

7.6

9.9

5.9

46

31

FL 12" CM

14

10

13

FL 12" CM

24

15

13

73.6

74.0

73.1

72.2

85.0

85.2

82.1

13.0

12.6

12.5

14.4

1.6

3.4

4.5

53

58

69

75

75

56

39

72.5

74.0

75.9

77.7

79.2

80.5

82.4

84.3

85.8

14.1

12.6

10.7

8.9

2.4

6.1

4.2

2.3

0.8

75

57

36

15

15

38

60

75

Sta + π - Elev
886.58
886.62

39+17 $\pm$ Highwood

BM

3.36 883.26 883.25

2

67

71.5

72.9

74.1

77.3

79.24

80.5

82.7

84.7

85.8

15.1

13.7

12.5

9.3

7.34

6.1

3.9

1.9

0.8

97

75

59

22

14

38

62

75

69.1

68.1

91.5

90.1

88.1

17.5

18.5

+4.9

+3.5

+1.5

133

150

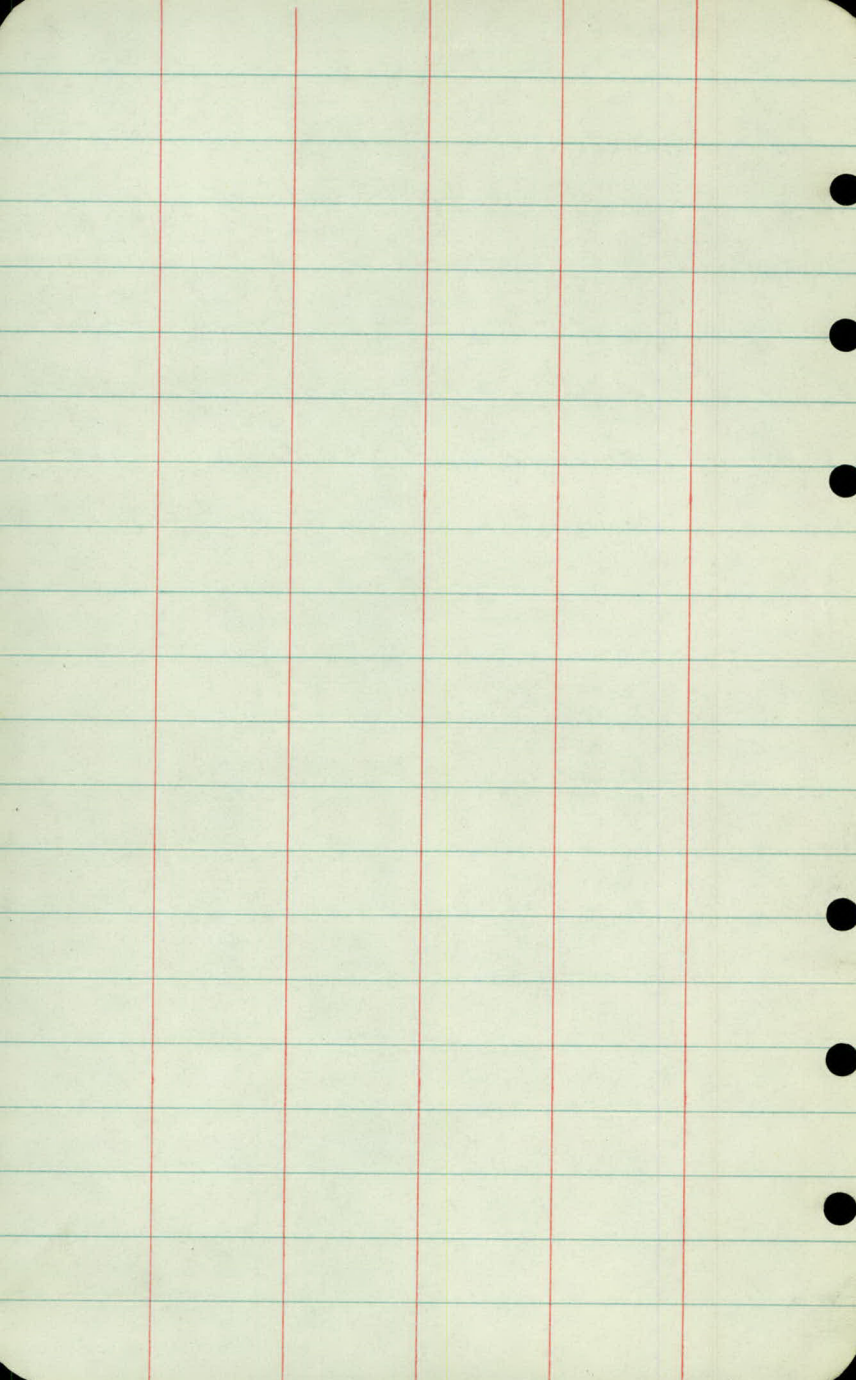
150

131

105

Top of Retaining Wall NE Cor McKnight +

Highwood



April 6, 1960

1

Mc Knight Carver to Highwood
X-Sections
on
Carver

Sta 35+68 Broken Timber
box Culvert
11.2 feet Below E of Road

reduced & checked by K P 4-11-60

Sta	+	π	-	Elev.
BM	2.32	860.83		858.51

0+00

54.4
6.4

50' West of McKnight

75' West

50' East of E of McKnight

75' East " " " "

JS
JL
JH

April 18, 1960

2

North

Top N.W. Cor Bottom Step H. McKnight & Carver SW Cor

McKnight & Carver

5 ⁰	5 ¹	5 ⁵	5 ⁷	5 ⁹
7.8	8.1	8.3	8.1	7.90
29	18	14	12	

5 ⁸	5 ¹
7.0	6.7
43	54

5 ¹	5 ¹	5 ⁸	5 ³	5 ⁰	5 ¹
7.7	8.1	8.0	8.5	8.8	8.7
50	34	25	17	14	

5 ⁶	5 ³	5 ⁹	5 ¹	5 ⁴	5 ⁶
6.2	6.5	6.9	6.7	5.4	5.2
48	35	26	21	12	

5 ⁵	5 ¹	5 ²	5 ⁰	5 ¹	5 ²
6.3	6.5	6.6	6.8	6.1	4.8
50	38	27	22	20	12

Sta	+	π	-	Elev.
BM	0.84	859.35		(858.51)

100' West of $\frac{1}{2}$ McKnight

125' West of $\frac{1}{2}$ McKnight

150' West of $\frac{1}{2}$ McKnight

50' W

6.42

52.93

✓ 52.9

FX
RG
JS
JL
JH

£

April 12, 1960

3

R/ or North
McKnight & Carver

Top N.W. Cor Bottom Step Ho SW. Cor

51.5	51.4	52.9	53.5	53.1
7.9	8.0	6.5	5.9	5.7
	14	18	41	50

50.8	50.7	53.4	53.8	54.8
8.6	8.7	6.0	5.6	4.6
	14.5	22	38	50

50.0	50.2	54.3	54.7	55.8
9.4	9.2	5.1	4.7	3.6
	14	34	41	50

Boxwood West

Sta	+	-	Elev
-----	---	---	------

BM	698	942.64	
----	-----	--------	--

			935.66
--	--	--	--------

0+40	Property Line		
------	---------------	--	--

✓			
---	--	--	--

+70			
-----	--	--	--

✓			
---	--	--	--

1			
---	--	--	--

+25			
-----	--	--	--

± April 12, 1960

4

14

81

RR Spike in 4th PP 3621 Sta 13125

25.0	30.0	32.4	33.7	32.8	33.4	33.7	34.8
176	12.6	10.2	8.9	9.8	9.2	8.9	7.8
75	47	19		7	11	21	35

40.5	38.5	36.5
2.1	4.1	6.1
100	78	58

26.2	28.5	31.1	33.4	32.9	33.4	34.1	35.6	37.8
16.4	14.1	11.5	9.2	9.7	9.2	8.5	7.0	4.8
74	50	26		9	13	26	49	67

41.7
0.9
93

24.9	27.8	29.6	31.4	33.2	33.9	37.8	40.6	41.5
17.7	14.8	13.0	11.2	9.4	8.7	4.8	2.0	1.1
65	38	17		10	27	56	73	80

23.9	26.2	28.4	32.0	33.1	34.0	34.9	38.0	41.6
18.7	16.4	14.2	10.6	9.5	8.6	7.7	4.6	1.0
67	41	16		11	29	32	55	74

Sta + π - Elev

942.64

1 + 50

2

+50

✓

3

6.2

+50

6.5

BM 3.08 938.74 6.98 935.66

Boxwood East

0 + 50

2 April 12, 1960

5

17

81

23.2	27.5	31.6	33.3	33.9	35.8	38.1	42.6
19.4	15.1	11.0	9.3	8.7	6.8	4.5	0.0
48	19		6	31	35	52	82

22.3	25.9	30.5	34.4	34.9	35.2	36.3	38.2	40.4
20.3	16.7	12.1	8.2	7.7	7.4	6.3	4.4	2.2
60	42	18		7	29	30	51	73

Real

24.9	28.5	31.8	33.1	34.6	36.6	36.0	36.6	37.4	38.4
17.7	14.1	10.8	9.5	8.0	6.0	4.6	6.0	5.2	4.2
56	36	16	4		12	13	28	29	34

Real

42.3	40.6
0.3	2.0
91	64

RR Spike in 1th PP 36 21 sta 131 25

37.5	36.4	34.8	32.8	31.6	31.7	31.5	31.6	32.4	32.7
1.2	2.3	3.9	5.9	7.1	7.0	7.2	7.1	6.3	6.0
69	46	22	21		5	16	36	51	70

38.4
0.3
100

32.8
59.4
88

Sta + π - Elev

938.74

1

✓

+50

2

✓

+50

2 April 12, 1960 6

34.0	33.3	33.0	31.7	31.8	32.2	31.7	30.6	29.3
4.7	5.4	5.7	7.0	6.4	6.5	7.0	8.1	9.4
57	40	21	18		5	12	15	38

30.9 31.6

7.8 7.1

60 91

Basement

26.2 27.3 27.5

12.5 11.4 11.2

95 84 65

34.2	33.7	33.4	31.9	32.0	32.0	31.6	28.9	27.6	26.7
2.5	0.0	5.3	6.8	6.7	6.7	7.1	9.8	11.1	12.0
15	60	52	31	16		9	17	35	60

30.6	31.6	33.4	33.1	33.1	32.5	30.8	28.7	27.5
8.1	7.1	5.3	5.6	5.6	6.2	7.9	10.0	11.2
74	46	18	8		11	23	46	67

27.7 27.7 27.1

11.0 11.0 11.6

100 95 80

31.6 32.1 33.7 33.7 33.7 33.7 34.2 33.4 31.2

7.1 6.6 5.0 5.0 5.2 5.0 4.5 5.3 7.5

52 39 19 7 13 14 25 45

30.6

8.1 50

Sta + π - Elev

938.74

3

34.6

+50

4.1

36.0

4

2.7

35.66

BM

3.08 935.66 (935.66)

April 12, 1960

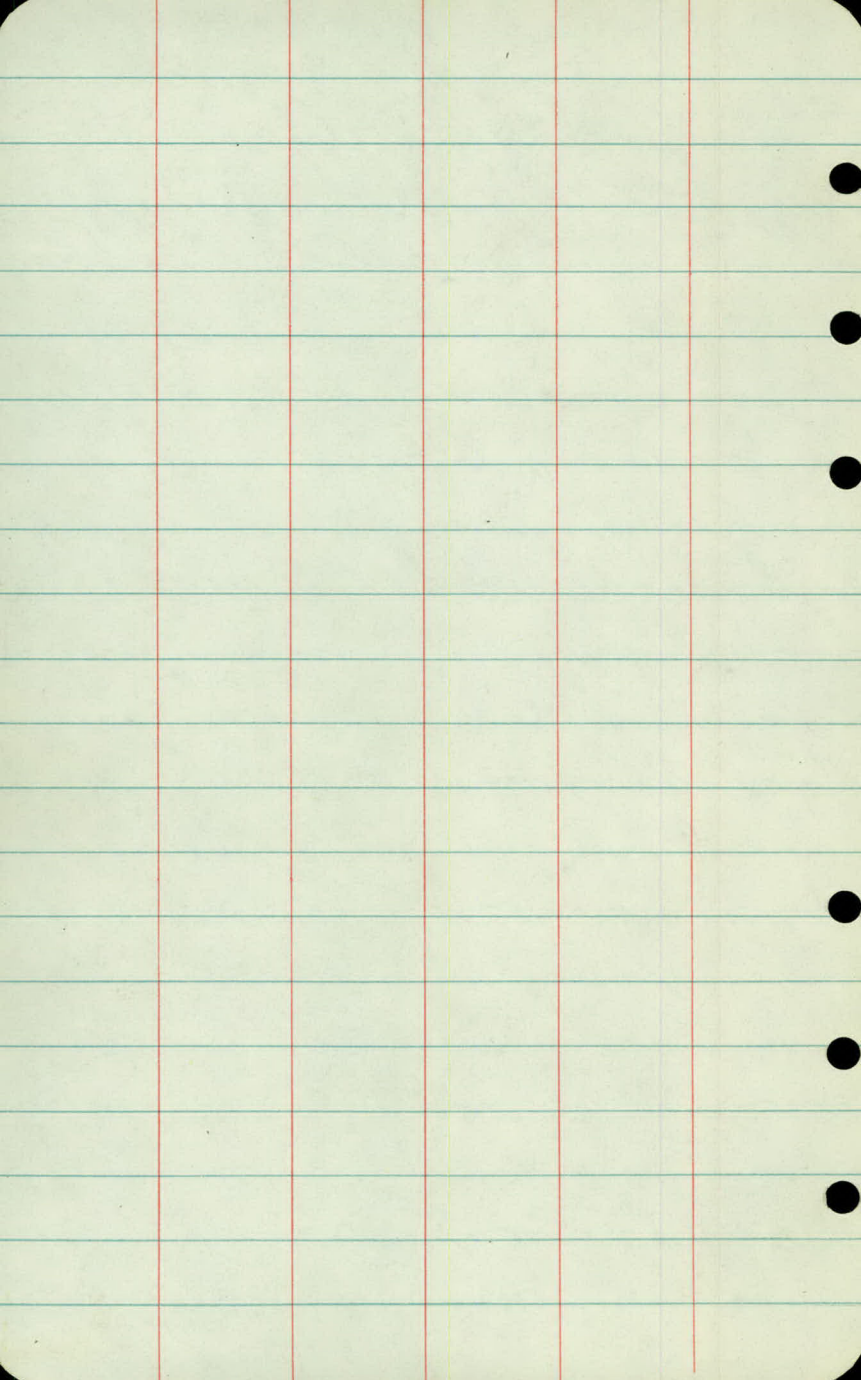
7

Lt

Rt

34.0	33.3	33.5	34.4	34.1	✓34.0	33.7	32.8	32.0	30.1
4.7	5.4	5.2	4.3	4.6	4.7	5.0	5.9	6.7	8.3
50	32	22	6		13	21	35	42	50

R.R. Spike in 4th AP 36' Lt Sta 13+25



FK
RG
JS
JL
WM

May 13, 1960
Clear 65°

1

Mo Knight

Carver to Highwood

House Locations

stadia

Object

Az. Stadia

at sta 32

to sta 39

0°00'

SE Cor Ho

279°03' 229'

NE Cor Ho

292°18' 197'

NW Cor Ho ①

229°00' 263'

SE Cor Ho ②

222°02' 261'

E trail

250°45' 303'

"

254°15' 257'

"

261°00' 223'

"

265°15' 187'

"

272°25' 146'

"

283°00' 111'

"

314°00' 75'

OBJECT

AZ.

STADIA

Legal description for drainage easement
on French property at Highwood and
Mc Knight Road.

Commencing at the East quarter corner
of Section 14, Township 28, Range 21,
Ramsey County, Minnesota; Thence West
along the east-west quarter line a ^{to the point of beginning of Easement} distance of 104.27 feet, ^{to the point of beginning of Easement} Thence Southwesterly
by an angle of $82^{\circ} 32'$ from said
east-west quarter line a distance of
350 feet and there terminating.

L.M.D.
D.S.
G.A.
DD.

26-NOV-79

CLOUDY 30°

MC KNIGHT RD.
AT HIGHWOOD

STA POINT Δ LT Δ RT

3+21.61 SPIKE

27.63

± 49.24

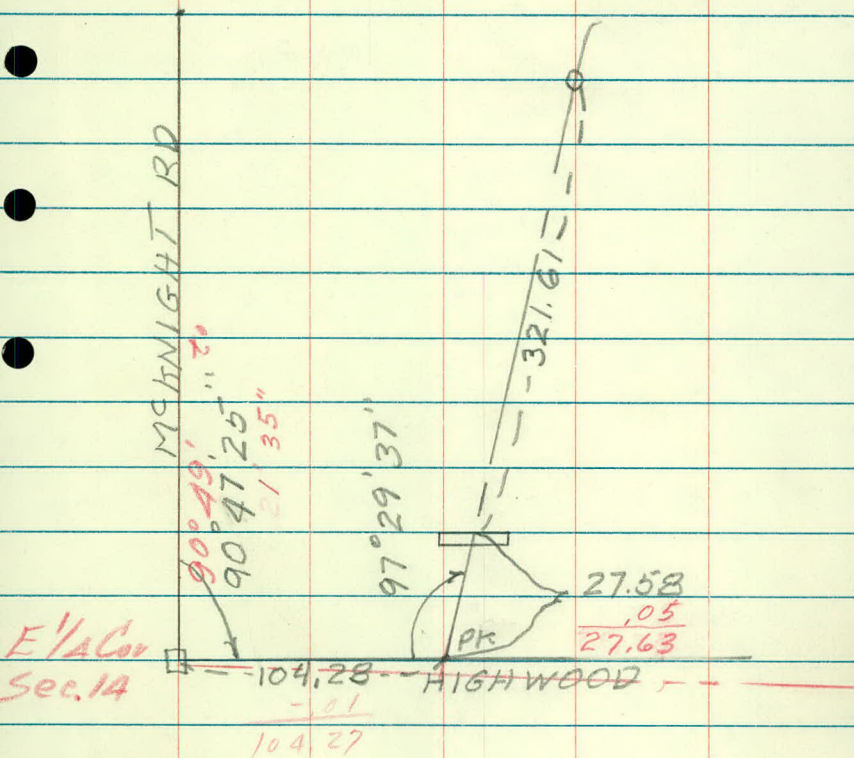
97° 29' 37'
1 35
97° 28'

0+00 PK

179 60
97 28
82° 32'

PK

26-NOV-74 2
CLOUDY 30°


$$\begin{array}{r} 321.61 \\ 27.63 \\ \hline 349.24 \end{array}$$