

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN

Survey

LARPENTEUR AVE.

From SNELLING To FERNWOOD

Road Acc't. No. _____

Date Filed 1-6-61

File Dr 9 Bk 24

1
LARPENTEUR

SNELLING to FERNWOOD

PLAN SURVEY

INDEX:

Alignment 2-5

Topography 6-14.

~~BM~~ ~~946.49~~

251.50 lost a section

~~BM~~ ~~912.80~~

~~BM~~ ~~911.84~~

FK
RG
CW

Nov. 13, 1957
Drizzle 48°

2

Alignment

Nov. 13, 1957

£

3

Arc
Light



Hyd

46.46

68.9A

S.W. Cor. Sec 15-29-23



71.00

63.55

PP

Sign Base



Sta	Point	ΔL	ΔR
-----	-------	------------	------------

26 + 61.89 P.I. $1^{\circ}04'$

± Nov. 13, 1951

4

20" E/m



N.W. Cor
cleaners

66.57

129.89

± Hamline



S¹/₄ Cor 15-29-23

49.21

± Hyd

161.22

N.W. Cor
Falcon
Station
Walk

Sta Point Δ Lt Δ Rt

38+48.20 P.I.

£ Nov. 13, 1957

5

N.W. Cor

Ho.

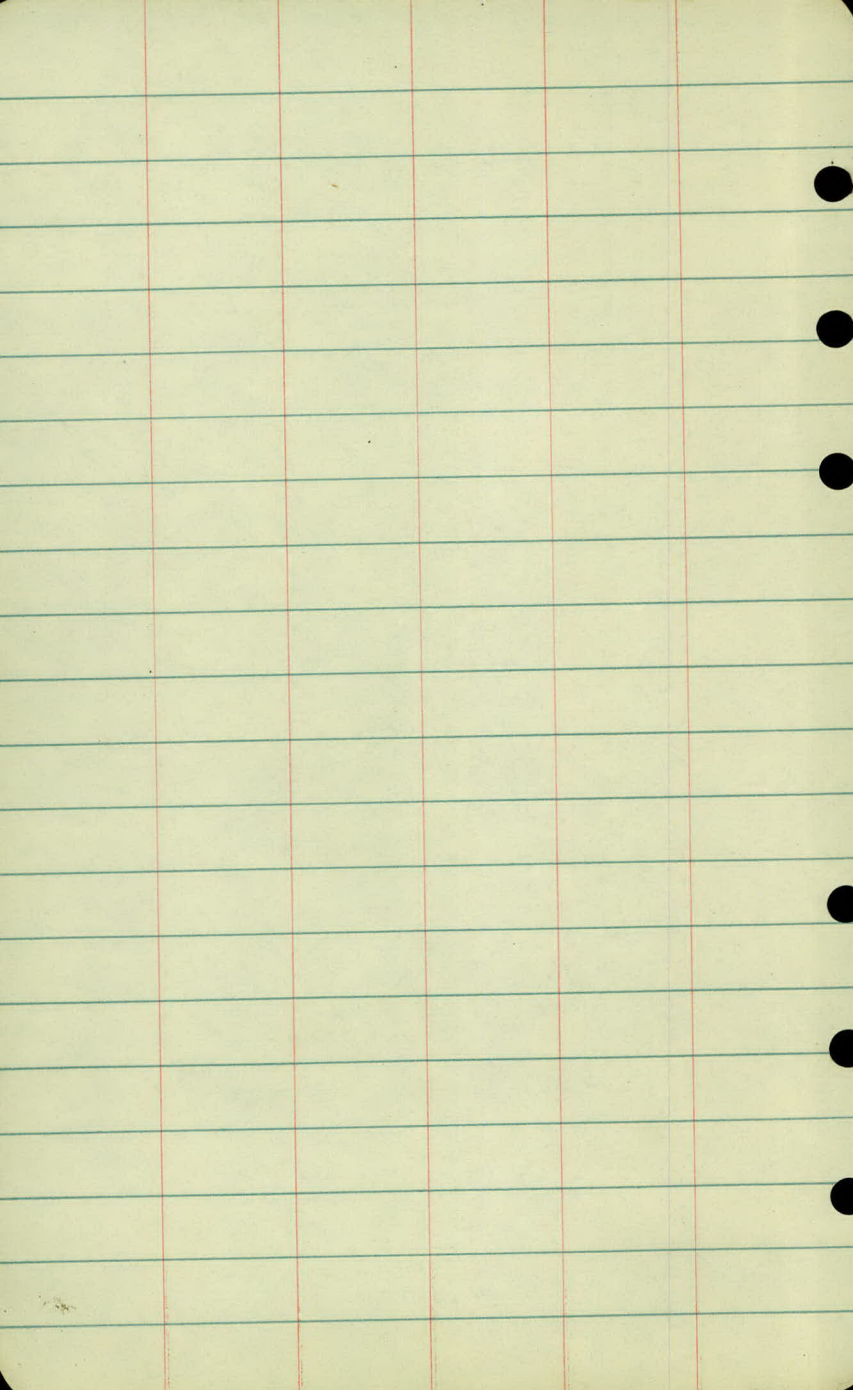
S.W. Cor
Station

109.06

73.68

102.93

Drive in
S.E. Cor



TOPOGRAPHY

±

5

+99 $\frac{BEnt}{2'R}$

+96 $\frac{MH}{41}$

+24 $\frac{Stub Pole}{35}$

4

+03 $\frac{Arc Lt}{33}$

+01 $\frac{Arc Lt}{35}$

+80 $\frac{CB}{31.5}$

3

+46 $\frac{CB}{31.5}$

+08 $\frac{MH}{41.5}$

+10 to +41 $\frac{Ent}{3' Rad}$

+04 $\frac{EGR Post}{40}$

+54 $\frac{MH}{28}$

+51 $\frac{Sig Pressure Plate}{3'-13}$

+36 $\frac{Ch 2R}{32}$ +07 $\frac{Ch 2R}{32}$

2

+58 $\frac{PP}{38}$ 62 50

+28 $\frac{MH}{78}$

+42 $\frac{ER}{10}$

+10 $\frac{RC}{24}$

1

+90 $\frac{BR}{60'}$

+68 $\frac{W. Edge}{NB Lane}$

+42 $\frac{Curb}{24}$

+12 $\frac{E. Edge}{SB Lane}$

0

+79 $\frac{End Ent}{3'R}$ ok

+59 $\frac{PP}{33}$

+03 $\frac{GP}{32}$

+74 $\frac{W.E. Ent}{50}$

+55 $\frac{End Conc}{10-30}$

+40 $\frac{Edge Conc}{35'}$

+50 $\frac{BRC}{35}$

+100 $\frac{BRC}{34}$

+82 $\frac{BGR Post}{40}$

+59 $\frac{Ch 3'R}{33}$

+23 $\frac{BEnt}{50}$

+60 $\frac{Cor Conc}{Station}$

+63 $\frac{Edge Conc}{30}$

+59 $\frac{PP}{33}$

+50 $\frac{Ent}{54 to 77}$

+71 $\frac{Rfic Edge}{Ent}$

+29 $\frac{3' Ent Rad}{33}$

+99 $\frac{End Ent}{50}$

+92 $\frac{End Ent}{30}$

+55 $\frac{ERC}{30}$

+52 $\frac{Signal}{29}$

+68 $\frac{E.R.C.}{50}$

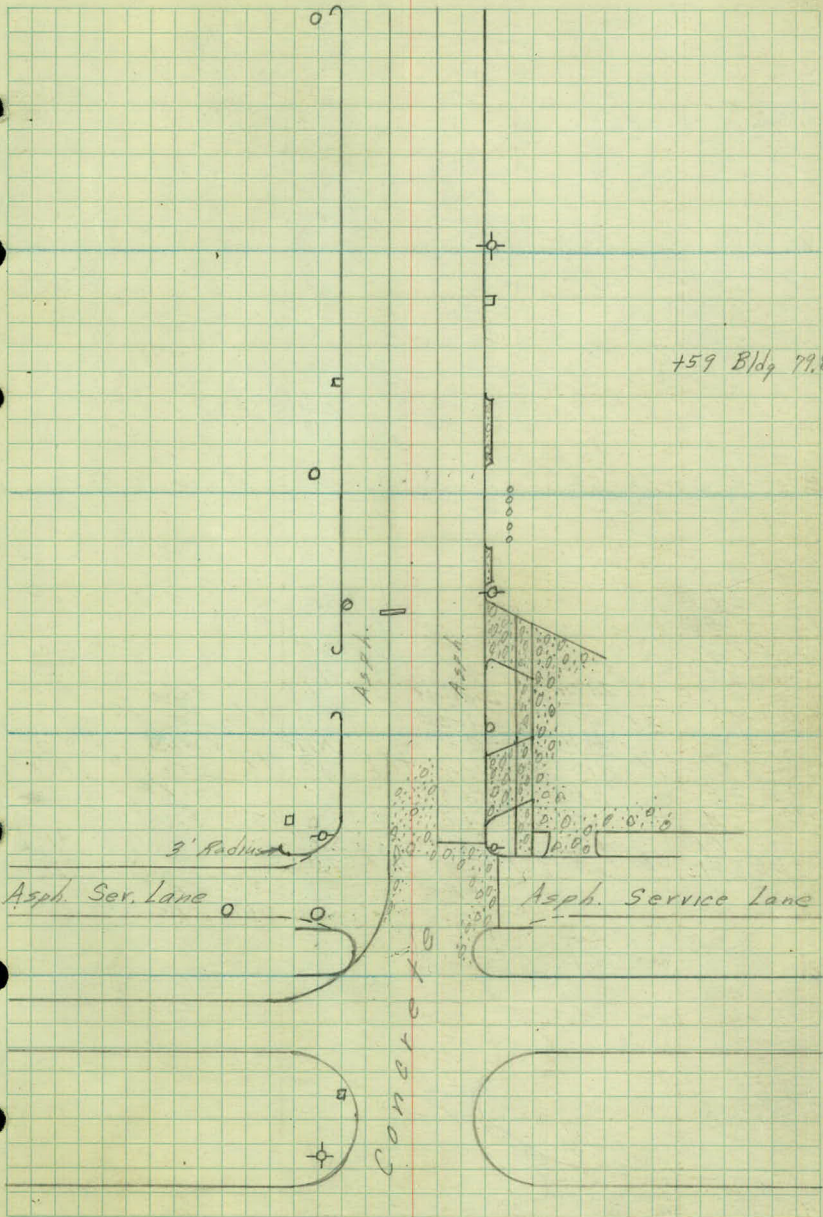
+12 $\frac{E. Edge}{SB Lane}$

+26 $\frac{Arc Lt}{38}$

+12 $\frac{BRC}{50}$

Nov 15, 1957

7



RT

+92.5 $\frac{26}{44}$ Walk		+76 $\frac{12 \times 8 \text{ Vt Walk}}{27.5}$	+176 $\frac{26 \text{ Walk}}{49.5}$
+37 $\frac{16 \text{ E}}{51}$	+62 $\frac{W50}{47}$	+72 $\frac{18 \text{ E}}{51}$	+34 $\frac{PP}{32}$
9	+105 $\frac{14 \text{ E}}{51}$	+112 $\frac{4 \text{ Walk}}{30}$	+25 $\frac{\text{Walk } 15 \times 15.5 \text{ Vt}}{27.5}$
+176 $\frac{W50}{45}$	+87 $\frac{\text{Cor Hedge}}{49}$	+90 $\frac{W50}{46}$	+26 $\frac{26 \text{ Walk}}{49.5}$
+63 $\frac{25 \text{ Walk}}{49}$		+67 $\frac{16 \text{ E}}{51}$	
+75 $\frac{W50}{45}$	+41 $\frac{\text{Cor 2 Hedge}}{49}$	+63 $\frac{MH}{18}$	+74 $\frac{6 \text{ E}}{56}$
+39 $\frac{\text{End Walk}}{44-50}$		+28 $\frac{16 \text{ E}}{51.5}$	+55 $\frac{\text{Walk } 12 \times 7.5 \text{ Vt}}{27}$
8	+107.5 $\frac{26 \text{ W}}{50}$	+16 $\frac{B.T.}{13}$	+25 $\frac{6 \text{ E}}{56}$
+89 $\frac{12 \text{ E}}{51}$			+154 $\frac{26 \text{ W}}{50}$
			+93 $\frac{PP}{32.5}$
+58 $\frac{24 \text{ Vt}}{50}$	+36 $\frac{8 \text{ Ash}}{51}$	+30 $\frac{E.R.}{19}$	+78 $\frac{6 \text{ E}}{56}$
+106 $\frac{P.Cor}{50}$		+15 $\frac{Hyd}{41}$	+48 $\frac{\text{Walk } 12 \times 9 \text{ Vt}}{28}$
7	+100 $\frac{E, \text{End } 21 \text{ CM}}{35}$	+100 $\frac{\text{Box Walk}}{44-50}$	+25 $\frac{MH}{41.5}$
+91 $\frac{BR}{50}$	+176 $\frac{MH}{40}$	+60 $\frac{CB}{104}$	+101 $\frac{P.Cor}{50}$
+43 $\frac{E.R.}{54}$	+43 $\frac{BR}{30}$	+58 $\frac{P.O. Rad}{42}$	+25 $\frac{6 \text{ E}}{57}$
+25 $\frac{CB}{31.5}$	+95 $\frac{\text{Cor Conc}}{50}$	+37 $\frac{\text{Open MH}}{34-38}$	+197 $\frac{B. Walk}{43.5}$
			+54 $\frac{Ch. 2R}{32}$
			+53 $\frac{\text{Arc Lt}}{32}$
			+15 $\frac{CB}{31.5}$
6	+100 $\frac{E.R.}{30}$		
	+93 $\frac{BR}{34}$		
	+54 $\frac{\text{Cor Conc}}{50}$		
+64 $\frac{B. Ent}{2 \text{ R}}$		+28 $\frac{E. Ent}{2 \text{ R}}$	
	+26 $\frac{SD}{28}$		
5		+22 $\frac{PP}{34}$	

Nov. 15, 1957

8

BT
13/13

BT
30/27

6' Mono Walk

6' Mono Walk

4' Mono Walk

Asph.

18" CM
→

ARONA AV.

Elec. Cable

E Asph.

Asph.

Asph.

Asph.

Asph.

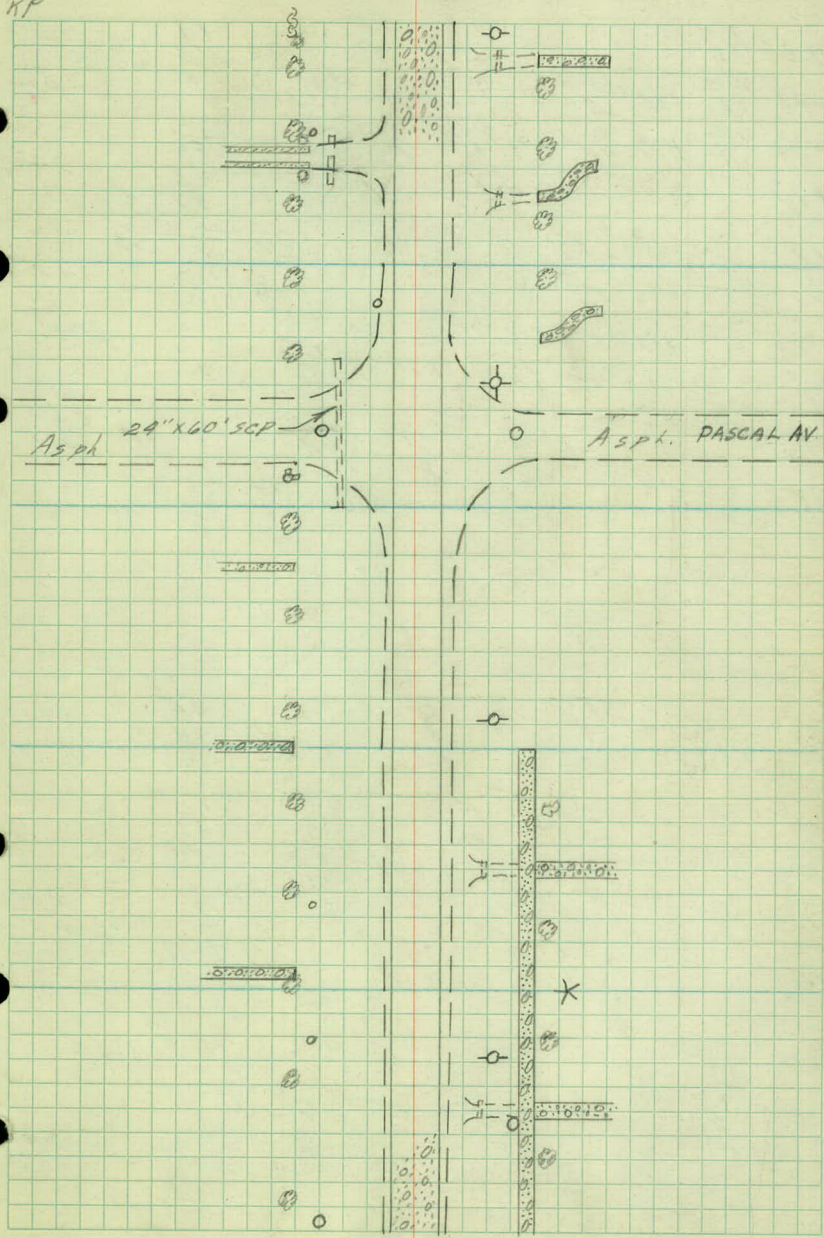
Asph.

15	B. Hedge	BT	15.15			
+95	53			+96	PP	
+155	10"E 52	+82	12"E 52	+93	Andy S.	
+154	W.S.O. 15	+38	Spiral 49	+50	Spiral 49	
+44	Ent 15"X20"SCP		2.2 Ribbons	+28	4' Walk	
14	+24	8"E 52		+19	52	
+95	12"E 52			+95	18"E 53	
+63	6"E 52	+72	ER 17	+70	ER 13	
+31	M.H. 40	+45	BR 53	+60	ER 24"SCP	
+00	W.E 24"SCP		33.5 Hyd	+12	52	
13	+18	ER 51		+20	ER 50	
+80	BR 13			+19	22	
	+94	24"E 51				
	+155	22"E 51		+69	ER 75	
12	+16	18"E 51		+12	PP 32	
	+99	4' Walk 52		+98	End Walk	
+78	14"E 51			+40	14"E 51	
+16	W.S.O. 44			+50	Walk 12"X5.5V.1	
				+107.5	46' Walk 50	
11	+01	22"E 51		+100	6"P 63	
				+78	W.S.O. 43.5	
				+79	6"E 55	
+62	14"E 51			+50	Walk 12"X6.5'V.1	
				+45.5	M.H. 41.5	
10	+04	M.H. 40		+13	14"E 51	
				+31	8"E 55.5	

FR
LC
RG
KP

Dec 11, 1957
Dec 12, 1957

9



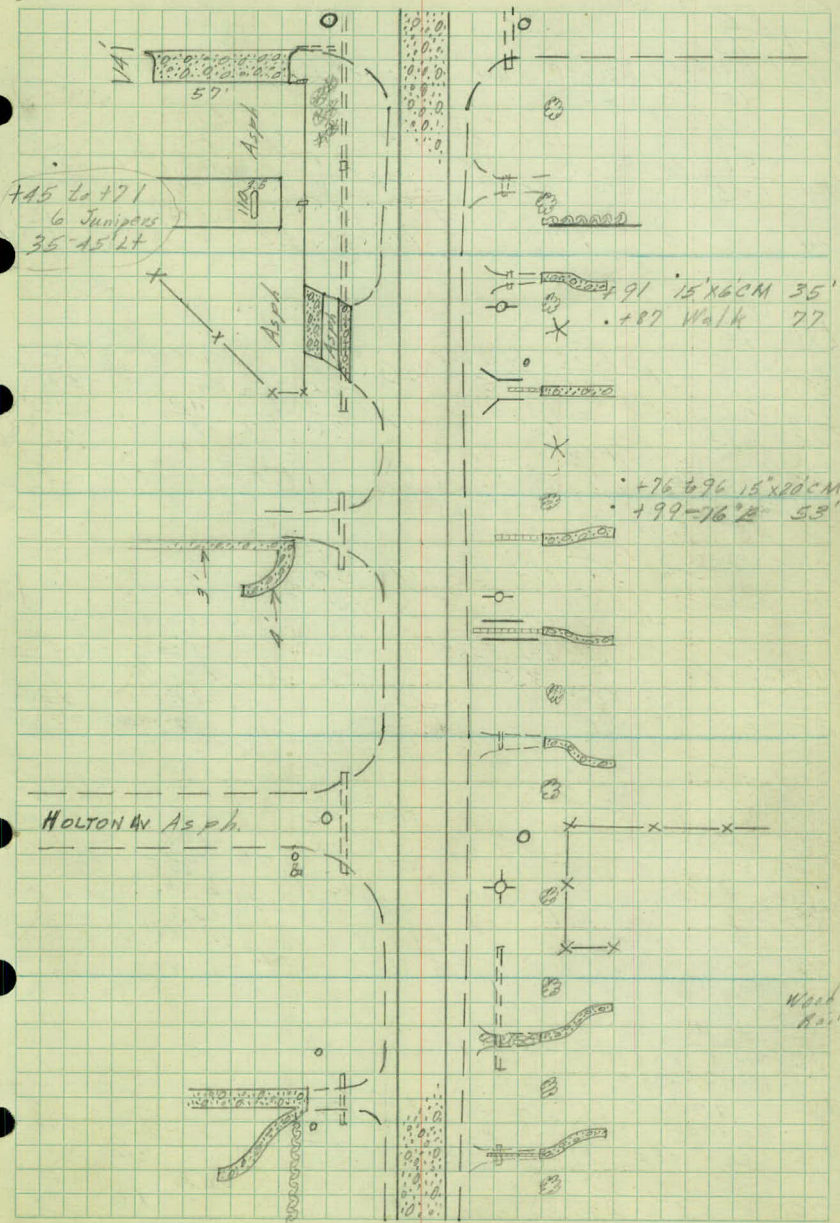
£

[illegible]

FX
RG
KP
CW

Dec 12, 1957
Fly Cloudy 8°

10



61 Long

BT.

25 PP 15 20

174 31.5 129 30.5 180 Rep Ent

165 15" 18" X 21" SCP Spirea 178 S.E. 18" SCP 185 Flg. Lamp 2

126 48 159 45 174 PP 173 10" E

114 50 18" X 21" SCP 132 2-WSO 162 15" X 5' SCP 4' Walk

24 106 5" P 11 Rtie BT 4' Walk 15" X 5' SCP Hex Tile

191 WSO 42

139 58 151 49 18" X 21" SCP 153 4' Walk 15" X 6' SCP 18" Tile

113 91.5 119 56 129 4" P 117 PP 124 MH 133 2-WSO

23 100 57 108 36 14 16 109 50 35 32-50

177 52 87 Ent 18" X 21" SCP

39 62 168 54 174 62 178 8" CE

29 49 134 53 144 53 153 51 36 23-51

48 + 123 49 130 E.E. 18" SCP 118 4-3" B 133 2-WSO 149 20" E

22 113 52 14 16 104 4' Walk 15" X 8' SCP 35 Vit

166 PP 32

150 W.E. 15" CM 35 171 Conc Ent 121 12" CE 128 2-WSO

21 N.E. 12" CM 55.5

165 31-40 176 5.21 185 6" X 5' Vit 47-52

159 31-40 162 51 18" X 6' SCP 16" E

126 34.5 132 52 132 Hyd 118 12" E 134 5" B 142 WSO

20 108 40 136 15 109 45 113 32 116 35

Dec 13, 1957

11

RG
KP
CW

+65 Hip Rap Ent
Shoulders

+14 Rip Rap Ent
Shoulders

[illegible]
$$\begin{array}{r} 15'' \times 18'' \\ \times 80' 50'' \\ \hline \end{array}$$

0.00000

30

19.4 255

175 B Curb (Asph)
19

125 End S. Wall
28-24

180 PP
31

125 W.E. 24 CM
21

126 BT
23-18

29

BT Road & Gutt

Curb
24.5

195 S. Wall
23-28

175 Cor Wall
37

169 Box B.T. Curb
24

148 Ent
26

28

stone
33-23

BT
23 23

121 PP
30

102 Ent
31

102 ER
23

125 Box Stone Wall & Gutter
24-31

125 BT
22-26

27 125 E.E. 24 CM
25

BT
22 17

edge Curb
32

175 BR
50

193 Sig + 3 GR
28

192 Sig + 3 GR
32

144 E.R.
32

120 BR
45

180 Arc Lt
30

145 ER
55

126 Sig + 3 GR
36

133 Hyd
40

136 MH
45

123 W.E. 24 CM
36

128 Sig + 4 BR
30.5

120 Fls. Lamp
45

111 BR
22

119 Sig Box
39

26 113 BR
15

BT
15 23

106 PP
49

108 E. GRP
49

177 PP
32

188 W. End Punt Is
70

151 End
Ent

161 Sig
49-53

171 B.G.R.
49

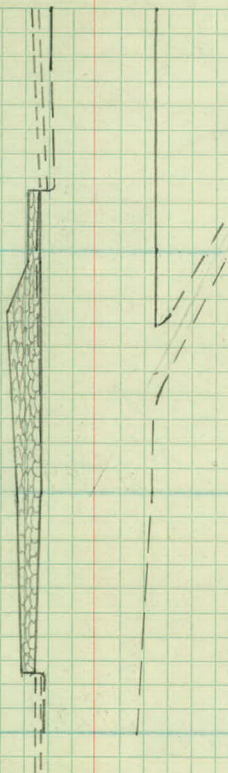
25

BT
15 20

153 W.E. Punt Is
70

Dec 13, 1957

12



10

35

$$\begin{array}{r} \text{Curb} \\ 33 \end{array} \quad 32$$

34

$$\begin{array}{r} \text{Curb} \\ 33.5 \end{array} \quad 30.4$$

$$+21 \quad \begin{array}{r} \text{PP} \\ 36 \end{array}$$

33

$$\begin{array}{r} \text{Curb} \\ 31 \end{array} \quad 29$$

$$+75 \quad \begin{array}{r} \text{PP} \\ 34 \end{array}$$

$$+28 \quad \begin{array}{r} \text{MH} \\ 34 \end{array}$$

$$+15 \quad \begin{array}{r} \text{MH} \\ 32.5 \end{array}$$

32

$$\begin{array}{r} \text{Curb} \\ 27 \end{array} \quad 27.6$$

31

$$\begin{array}{r} \text{Curb} \\ 23.5 \end{array} \quad 27$$

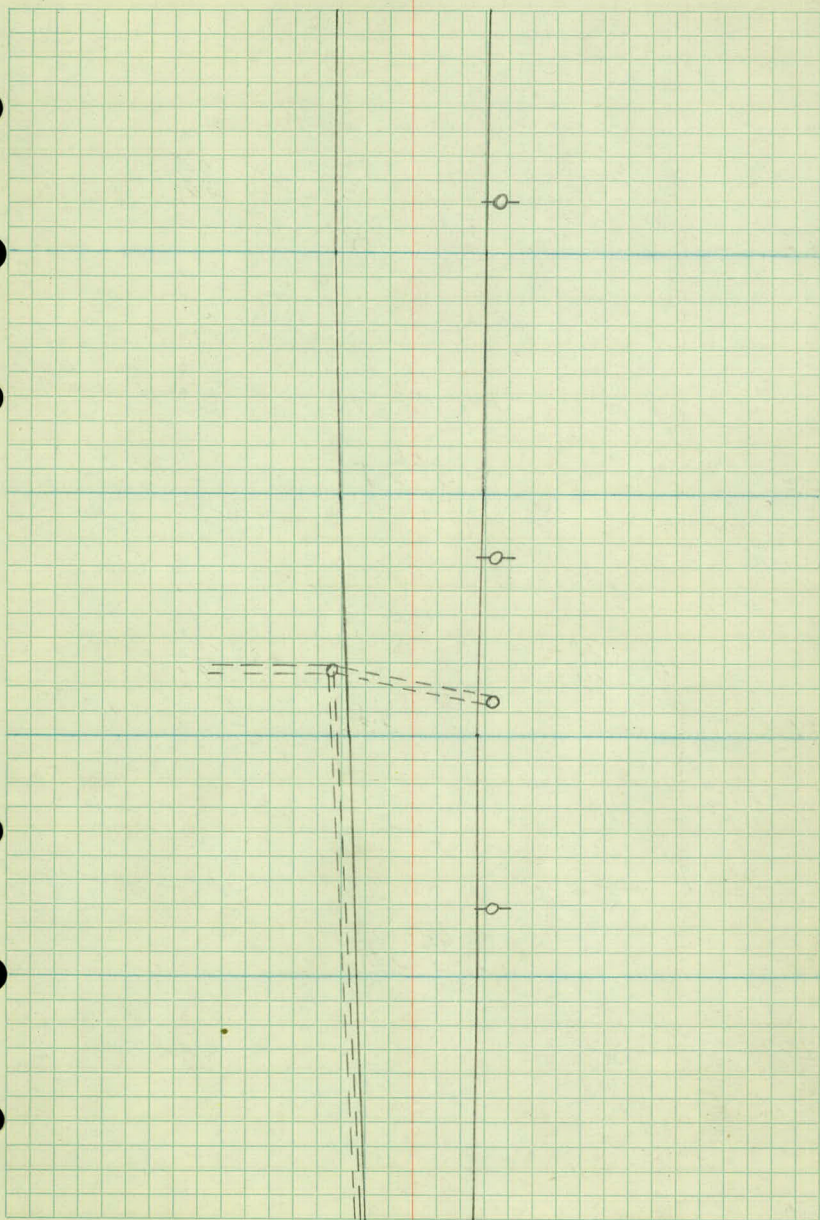
$$+29 \quad \begin{array}{r} \text{PP} \\ 33 \end{array}$$

30

$$\begin{array}{r} \text{Curb} \\ 19.4 \end{array} \quad 25.5$$

Dec 13, 1957

13



40

$$+30 \frac{MH}{34}$$

$$+27 \frac{18"E}{39}$$

39

$$\frac{Curb}{35}$$

$$+97 \frac{Cor Conc}{44.8}$$

$$+76 \frac{Cor Conc}{AA.7}$$

$$+82 \frac{W.E.R. 13.}{60.5}$$

$$+71 \frac{End Ent}{35}$$

$$+63 \frac{PP}{40}$$

$$+72 \frac{18"E}{39}$$

$$+20 \frac{\$25 Ent}{Asph}$$

$$+39 \frac{By Ent}{35}$$

$$+38 \frac{\$ Alley}{Asph}$$

38

$$\frac{Curb}{34.5} \quad 34.5$$

$$+60 \frac{MH}{SA}$$

$$+68 \frac{CB}{37}$$

$$+69 \frac{CB}{37}$$

$$+52 \frac{4" Walk}{Asph}$$

$$\frac{Conc steps}{44.5}$$

$$+62 \frac{MH}{39}$$

$$+1A \frac{18"E}{44}$$

$$+52 \frac{4" Walk}{Asph}$$

$$+62 \frac{MH}{39}$$

$$+28 \frac{PP}{39}$$

$$+12 \frac{\$30 Ent}{Asph}$$

$$+18 \frac{16 E}{44}$$

37

$$\frac{Curb}{32.5}$$

$$+78 \frac{Ent}{Asph}$$

$$+24 \frac{4" Walk}{Asph} \quad \frac{Conc steps}{33-53}$$

36

$$\frac{Curb}{33.5} \quad 32.5$$

$$+82 \frac{\$ Ent}{Asph}$$

$$+77 \frac{PP}{37}$$

35

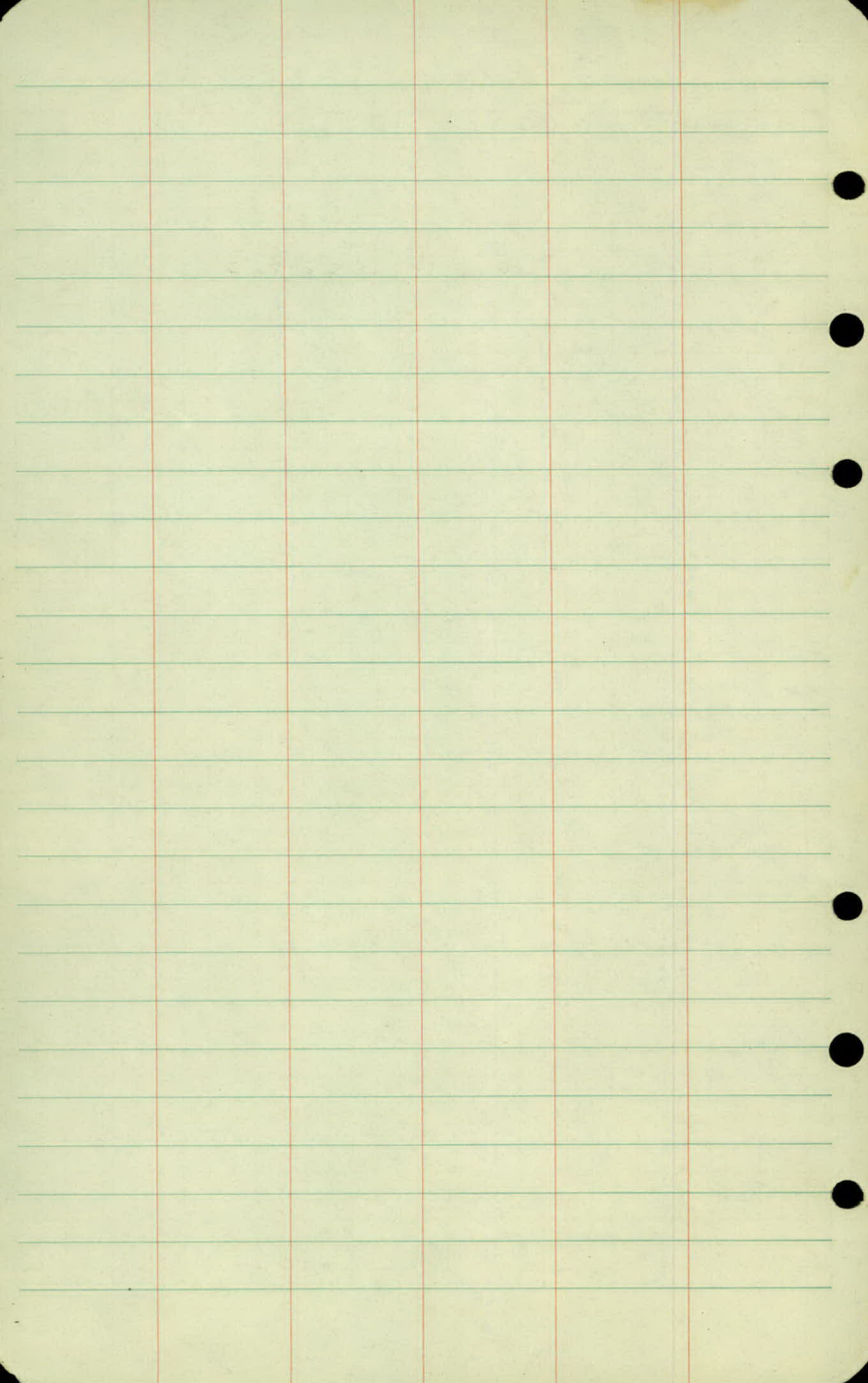
$$+09 \frac{MH}{34}$$

Dec 13, 1957

14



15. 13 x 3.5



Bench Levels

Sta	+	π	-	Elev.
BM	0.67	958.72		(958.05)
BM			2.52	956.20 (956.44)
BM	2.26	956.75	4.23	954.49 (955.03)
BM			2.94	953.81
BM	2.65	955.45	3.95	952.80 (952.85)
BM	1.03	953.62	2.86	952.59
BM	1.95	950.82	4.75	948.87
BM			4.08	946.74 (947.62)
BM	7.63	952.47	5.98	944.84 (944.98)
BM			2.61	949.86 (949.97)
BM				912.91
BM				913.01
BM				914.95
BM				914.88
BM				(932.18)

Elevations
Voids
Use page 11

Top Hyd Snelling & Larpenteur

Top Mont Snelling & Larpenteur

Top Hyd N.E. Cor Arona & Larpenteur

Top Hyd N.W. Cor Pascal & Larpenteur

Top S.E. Cor Lower Step Ho #1463 W. Larp. Ave

Top Hyd N.W. Cor Halton & Larpenteur

Top Hyd N.E. Cor Albert & Larpenteur

Top Hyd SW. Cor Hamline & Larpenteur

Top Mont at Hamline & Larpenteur

Top Lower Step Stucco Ho #1707 Hamline Ave

Top SW. Cor Conc Ent Slab #1255 W Larpenteur

Top Hyd Fernwood & Larpenteur

Top Hyd S.E. Cor Dunlap & Larpenteur

Sta	+	π	-	Elev	Corrected Elevations
BM	4.32	951.06		946.74	946.74
BM	4.79	953.66	2.19	948.87	948.87
BM	2.72	955.31	1.07	952.59	952.59
BM	2.31	956.12	1.50	953.81	953.81
BM	4.28	958.77	1.63	954.49	954.49
BM	3.57	959.77	2.57	956.20	956.20
BM			1.73	958.04	958.05
BM	1.60	948.34		946.74	946.74
TPV			79.5	940.35 ³⁴	.43
TP	0.47	935.22	13.59	934.75	
TP	0.24	923.84	11.62	923.60	
BM	2.22	915.09	10.97	912.87	912.86
BM	8.43	923.28	0.24	914.85	914.84
TP	9.35	932.20	0.43	922.85	
BM			0.00	932.20	932.18

Nov. 13, 1957

17

Top Hyd S.W. Cor Hamline & Larpenteur

Top Hyd NE Cor Albert & Larpenteur

Top Hyd N.W. Cor Holton & Larpenteur

Top Hyd N.W. Cor Pascal & Larpenteur

Top Hyd NE Cor Arona & Larpenteur

Top Mont at Snelling & Larpenteur

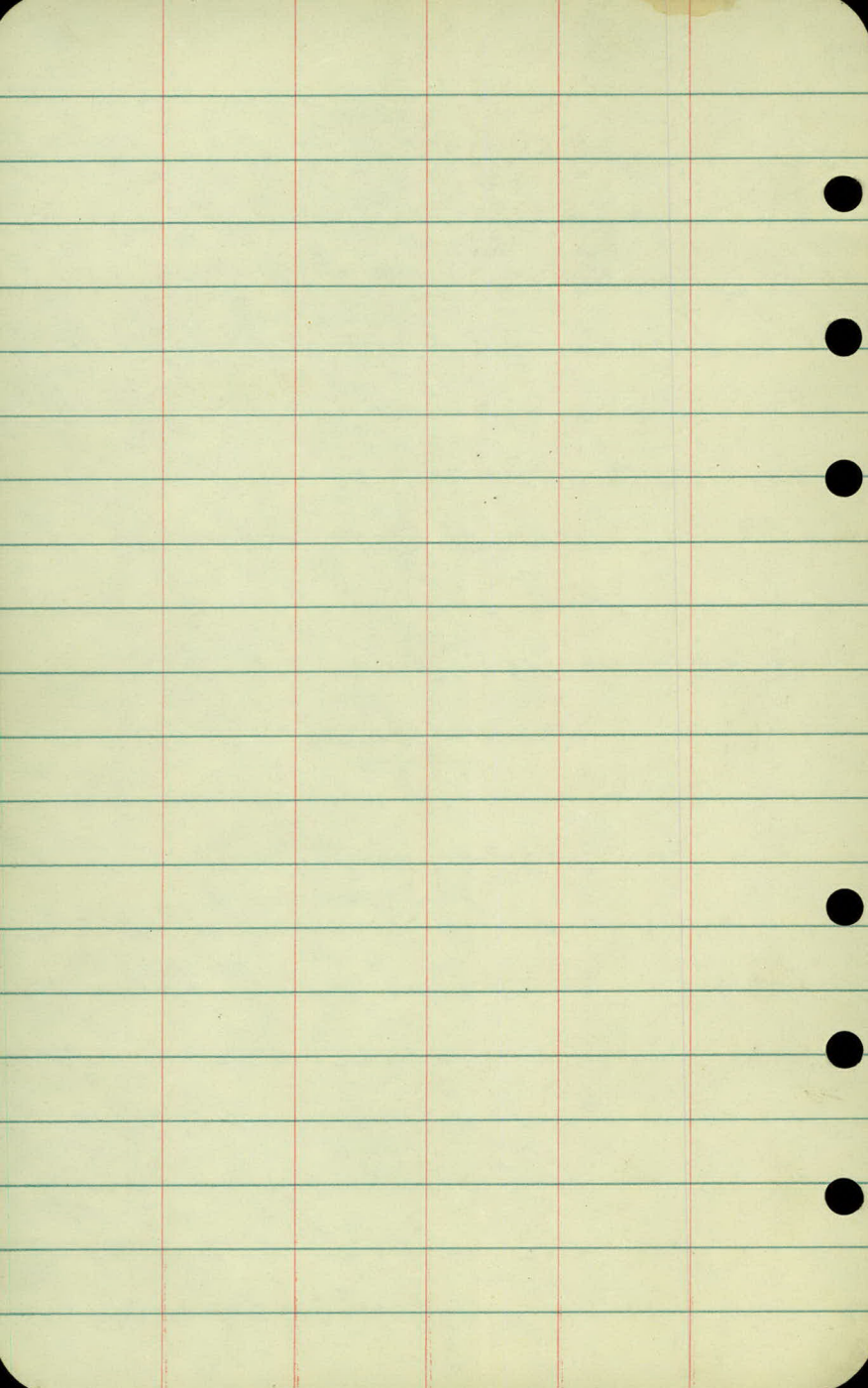
Top Hyd Snelling & Larpenteur

Top Hyd S.W. Cor Hamline & Larpenteur

S.W. Cor Conc Ent Slab[#] 1255 W, Larpenteur

Top Hyd S.W. Cor Fernwood & Larpenteur

Top Hyd SE cor. Dunlap & Larpenteur



10-9-57

X-SECTIONS

Larp. Ave - Fernwood
~~to Snelling Ave~~

Snelling Ave to Fernwood

+ T -

BM

1.93

956.42

954.49

6+00

+47

+58

+76

& Arona Ave

+92

+94

2.2
RG
KP
CW

1000 1400
Cloudy 30°

19

Lt.

4

14

top hyd NE Cor Larpenteur & Arona

52.70	52.31	51.50	51.0	51.2	51.52	51.3	50.8	51.40	51.8	52.0	✓
3.72	4.11	4.92	5.4	5.2	4.90	5.1	5.6	5.02	4.6	4.4	
70	50	30	30	21		20	31	31	45	66	
Conc.	Conc.	Top	Top					Top			
		Curve	Curve					Curve			

52.38	52.25	51.9	51.57	51.4	51.4	51.4	51.3	50.7	51.26	51.0	51.1	50.8	✓
4.04	4.17	4.5	4.85	5.0	5.0	5.0	5.1	5.7	5.16	5.4	5.3	5.6	
70	59	48	30	30	20		23	31	31	45	50	65	
Conc.	Conc.								Top				
									Curve				

51.3	51.2	51.68	51.4	51.4	51.4	51.3	50.9	50.7	50.5	✓
5.1	5.2	4.74	5.0	5.0	5.0	5.1	5.5	5.7	5.9	
70	59	42	42	20		20	32	50	65	
		Top	Top							
		Curve	Curve							

51.1	51.3	40.10	51.35	51.3	51.4	51.1	51.0	50.8	50.7	50.4	✓
5.3	5.1	16.32	5.07	5.1	5.0	5.3	5.4	5.6	5.7	6.0	
100	50	39	40	20		24	45	63	74	104	
		L.L.	Top								
			N.H.								

51.5	51.6	51.0	51.0	51.0	51.2	51.4	51.0	50.7	50.6	50.5	✓
4.9	4.8	5.4	5.4	5.4	5.2	5.0	5.4	5.7	5.8	5.9	
51	45	36	32	20			20	39	57	67	
60								50.7	51.0	50.9	
								5.7	5.4	5.5	✓
								33	44	58	

Sta + π - Elev

956.42

6+99

51.64
4.78
60
51.61
4.81
50.5

7+00

+01

+26

M. H.

+50

8+00

Lt

\$

17

61.50	50.9	51.0	50.7	51.1	51.4	51.0	50.7	51.23	51.28
492	55	54	57	53	50	54	57	519	514
44.5	41	36	31	20		20	31	44	50
S.W.								S.W.	S.W.

51.4
5.0

51.48
50.48
499
44
50
494
med

50.9	51.0	50.7	51.1	51.4	51.0	50.7	51.26	51.37
499	55	54	57	53	50	54	57	516
44	40	35	33	20	20	28	44	50
							S.W.	S.W.

51.67
4.75
41.5
Top M.H.

42.52
13.90
41.5
F.L.

51.91	51.73	50.6	51.2	51.4	51.3	51.6	49.7	50.9	51.92
451	469	58	52	50	51	48	6.7	5.5	450
49	43	33	18		13	20	28	32	44
S.W.	SW.								S.W.

52.00	51.79	50.7	51.2	51.4	51.2	51.3	49.6	51.2	51.94
442	463	57	52	50	52	51	6.8	5.2	448
50	46	33	20		11	22	27	36	44
S.W.	S.W.								S.W.

5/1 + π - Elev

956.42

8 + 38

End S.W. Lt. Side

+ 63

5.19
5.23 - N.S.P. M.H.
18' Rt

T.P.

4.83

956.09

5.16

951.26

9 + 00

+ 12

+ 50

+ 92

21

21

21

21

52.5	51.86	50.7	50.9	51.3	51.3	51.2	51.2	50.1	51.5	61.92	52.07
4.37	4.56	5.7	5.5	5.1	5.1	5.2	5.2	6.3	4.9	4.50	4.35
49	43	32	24	12		10	23	28	38	44	50
	S.W.									S.W.	S.W.

52.1	51.93	51.4	50.7	51.2	51.3	51.2	51.1	49.8	51.3	51.90	52.04
4.3	4.49	5.0	5.7	5.2	5.1	5.2	5.3	6.6	5.1	4.52	4.38
55	48.5	47	30	15		11	23	28	35	44	50
	S.W.									S.W.	S.W.

Ch. S.W. @ H. #1499

52.0	51.8	51.0	50.7	51.0	51.2	51.3	51.2	51.2	49.7	50.8	51.73	51.86
4.1	4.3	5.1	5.4	5.1	4.9	4.8	4.9	4.9	6.4	5.3	4.36	4.23
60	50	47	32	23	13		11	22	28	34	44	50
											S.W.	S.W.

51.26
483
50
S.W.

51.3	51.1	50.9	50.6	50.9	51.2	51.3	51.0	49.6	51.0	51.73	51.98
4.8	5.0	5.2	5.5	5.2	4.9	4.8	5.1	6.5	5.1	4.36	4.11
60	48	40	28	22	12		22	28	37	44	50
										S.W.	S.W.

51.34
4.75
49
S.W.

51.08
50.1
43
S.W.

Sta

+

π

-

Elev

956.09

10 + 00

+03

M. H.

+50

11

+07

+50

24

五

RT

22

[illegible]

5.01	3.92
5.08	16.88
40	40
Top M.H.	F.L.

$\frac{51.7}{4.4}$	$\frac{51.2}{4.9}$	$\frac{50.8}{5.3}$	$\frac{50.5}{5.6}$	$\frac{51.1}{5.0}$	$\frac{51.2}{4.9}$	$\frac{51.2}{4.9}$	$\frac{49.3}{6.8}$	$\frac{51.3}{4.8}$	$\frac{51.78}{4.31}$	$\frac{51.89}{4.20}$
60	47	38	24	21	13	23	29	36	44 S.W.	50 S.W.

[illegible]

5/12
4.97
50
S.W.

[illegible]

sta	+	$\bar{A}$	-	Elev
-----	---	-----------	---	------

956.09

11+97		End s.w.		
-------	--	----------	--	--

12+00

+04

+50

B.M.	0.85	954.66	2.25	953.84	953.81
------	------	--------	------	--------	--------

+77

+88

24

4

23

51.5	50.7	50.4	50.8	51.0	51.0	50.8	51.1	48.9	50.2	51.0
46	54	5.7	5.3	5.1	5.1	5.3	5.0	7.2	5.9	5.1
49	42	34	23	12		14	27	28	35	40
4.39										
52.5										
sw.	51.70									
					51.0		51.6		51.71	
						45		438		51.68
						54		50		
								sw		sw

52.0	51.5	50.7	50.5	50.9	51.0	51.0	50.7	48.8	49.9	50.2	50.0	49.8	50.3
4.1	4.6	5.4	5.6	5.2	5.1	5.1	5.4	7.3	6.2	5.9	6.1	6.3	5.8
60	49	40	30	21	11		21	27	35	42	47	53	60

51.1	50.6	50.4	51.0	50.9	50.9	50.5	50.0	48.9	48.7	49.4	49.6	49.4
5.0	5.5	5.7	5.1	5.2	5.2	5.6	6.1	7.2	7.4	6.7	6.5	6.7
60	43	27	21	11		21	25	28	32	40	50	62

Top Hyd. N. W. Cor. Pascag Ave

51.2	50.9	50.8	50.4	50.6	50.8	50.9	50.9	50.6	50.5	50.2	48.9	48.9	49.3	49.5	49.5
37.6	39	4.3	4.1	3.9	3.8	3.8	4.1	4.2	4.5	5.8	5.8	5.4	5.2	5.2	5.2
52	49	37	32	23	12		15	22	24	30	33	37	45	60	60
sw.															

51.2	50.9	50.4	50.2	50.7	50.8	50.9	50.5	50.4	49.2	49.8	49.4
3.5	3.8	4.3	4.5	4.0	3.9	3.8	4.2	4.3	5.5	4.9	5.3
59	49	44	35	25	12		15	25	31	49	60

Sta + π - Elev

954.66

13+00

+ 13

+ 16

+ 30

± Pascal Ave

+ 46

+ 48

Lt.

E

Rt

24

50.9	50.8	50.2	50.0	50.6	50.7	50.9	50.7	50.5	50.8	50.4	50.5	50.7
38	39	45	47	41	40	38	40	42	39	43	42	40
58	49	45	34	29	12		16	28	32	36	53	60

50.9	50.5	50.5	50.7	50.8	50.9	50.8	50.4	50.6	50.9
38	42	42	40	39	38	39	43	41	38
61	54	45	32	14		19	34	42	59

50.6	50.4	50.7	50.8	50.9	50.7	50.5	50.5	50.6
4.1	4.3	4.0	3.9	3.8	4.0	4.2	4.2	4.1
60	46	31	13		24	38	52	60

51.2	51.1	51.0	50.78	50.8	50.9	50.9	50.8	50.8	50.7	50.9	51.0	51.2
35	36	37	388	39	38	38	39	39	395	38	37	35
100	75	50	41	25	11		13	25	41	50	75	100
			M.H.						M.H.			

50.7	50.7	50.6	50.9	50.8	50.8	50.7	50.6	50.7	50.7
4.0	4.0	4.1	3.8	3.9	3.9	4.0	4.1	4.0	4.0
60	56	38	20	15		14	30	47	58

51.1	51.0	50.5	50.7	50.7	50.8	50.6	50.6	50.8	50.8	50.8
36	37	42	40	40	39	41	41	39	39	39
66	59	50	29	16		10	23	38	54	60

sta

+

↑

-

Elev

954.66

13 + 62

+ 70

14 + 00

+ 28

+ 42

+ 47

+ 50

} Ribbon Ent. 2' wide Conc.

10-9-57 25

Lt	#	Pt.
50.9	38	50.9
50.1	46	50.6
48.9	58	50.6
50.1	46	49.6
50.6	4.1	50.5
50.8	3.9	50.8
50.9	3.8	50.9
50.6	4.1	
50.6	4.1	
49.6	51	
50.5	4.2	
50.8	3.9	
50.9	3.8	

50.9
3.8
60

50.83
3.83
52
S.W.

50.9	38	50.9
50.6	41	50.7
49.3	5.4	50.7
49.2	5.5	49.7
49.4	5.3	49.5
50.5	4.2	50.5
50.6	4.1	50.9
50.8	3.9	
50.7	4.0	
50.7	4.0	
49.7	5.0	
49.5	5.2	
50.5	4.2	
50.9	3.8	

60 47 37 33 29 24 13 12 21 26 33 54 60

50.81
3.85
49.5
S.W.

50.50
4.16
46

50.46
4.21
46

50.9	38	50.9
50.3	4.4	50.8
48.9	5.8	50.8
49.4	5.3	50.7
50.4	4.3	49.2
50.6	4.1	49.0
50.8	3.9	50.9
50.8	3.9	51.8
50.7	4.0	
49.2	5.5	
49.0	5.7	
50.9	3.8	
51.8	2.9	

60 45 33 27 21 12 14 22 27 32 48 60

Sta

+

π

-

Elev

954.66

14 + 83

15 + 00

+ 27

+ 50

[?]
+ 26.76

16 + 00

16 + 00

+ 07

Lt.

#

10-9-57

Pt.

26
33

52.02

2.64

49.5

S.W.



51.1	50.6	49.0	48.9	50.2	50.6	50.7	50.7	50.6	49.1	49.1	50.9	51.1	52.5
3.6	4.1	5.7	5.8	4.5	4.1	4.0	4.0	4.1	5.6	5.6	3.8	2.6	2.2
62	48	37	27	22	11		14	23	28	30	41	53	60

51.96

2.70

50

S.W.

51.2	50.9	50.4	48.7	48.7	50.5	50.5	50.6	50.6	50.4	49.6	49.9	51.4	52.6
3.5	3.8	4.3	6.0	6.0	4.2	4.2	4.1	4.1	4.3	5.1	4.8	3.3	2.1
60	48	38	31	28	21	12		17	25	30	35	42	60

50.86

3.80
49 Ent

50.4

4.3

52.32

2.39

50

S.W.



49.9	48.6	48.4	48.4	49.9	50.2	50.3	50.4	50.3	50.7	51.3	52.3	52.8
4.8	6.1	6.3	6.3	4.8	4.5	4.4	4.3	4.4	4.0	3.4	2.4	1.9
47	40	36	26	20	11		21	26	35	43	49	60

50.4

4.3

60



Sta + π - Elev

954.66

16 + 15

B.M. 0.37 952.96 2.07 952.59 952.59

+36

+48

+50

+67 $\pm$ Holton Ave

T.P. 1.38 953.97 0.37 952.59 952.59

+81 shoulder Holton Lt

FK
RG
KP
CW

11
X
7
16

LT

LT

10-9-57
Dec 13, 1957

RT

27
34

✓

50.4	49.9	48.4	48.1	49.8	50.3	50.3	50.3	50.2	48.9	48.4	50.4	52.0	52.3
43	48	63	66	49	44	44	44	45	58	63	43	27	24
65	45	37	26	20	15		14	22	27	33	43	54	60

Top Hyd. N.W. Cor. Holton Ave

49.9	49.7	48.6	48.1	48.3	49.7	50.0	50.2	50.1	50.0	48.0	48.2	51.1	51.5	52.4
31	33	44	49	47	33	30	28	29	30	50	48	19	15	06
60	44	39	34	29	24	13		16	22	28	32	38	54	60

49.0	49.0	49.3	49.8	50.0	50.1	50.1	50.0	47.8	48.2	50.5	51.4	52.1
40	40	37	32	30	29	29	30	52	48	25	16	09
62	51	40	24	12		19	21	29	33	46	53	60

49.3	49.5	49.7	50.0	50.1	50.1	47.9	47.9	47.2	50.5	51.5	51.9
3.7	3.5	3.3	3.0	2.9	2.9	5.1	5.1	3.8	2.5	1.5	1.1
62	45	29	12		20	27	30	38	47	53	60

49.4	49.5	49.6	49.7	50.1	49.8	49.9	49.9	48.0	48.0	49.3	51.1	51.9
36	35	34	32.5	2.9	3.2	3.1	3.1	5.0	5.0	3.7	1.9	1.1
100	75	55	40	26	12		20	28	30	41	47	60

M.H.

Top Hyd. N.W. Cor. Holton Ave.

49.2	49.4	49.5	49.3	49.7	49.8	49.7	49.7	47.6	47.6	49.8	51.1
48	46	45	47	43	42	43	43	64	64	42	29
60	52	34	28	10		10	21	28	31	43	48

51.8
2.2
60

Sta + π - Elev.

953.97

16+86 $\pm$ Ditch Lt

✓

+95 Back slope

✓

+97

17

Dec. 13, 1957

Lt

F

RT

28
35

49.5	47.6	47.6	49.6	49.6	49.7	49.6	49.2	49.2	47.9	48.3	48.4
45	64	64	44	44	4.3	44	48	48	61	57	56
41	30	27	21	10		10	20	30	33	41	54

51.1	51.8
29	2.2
49	60

48.4
5.6
60

✓

47.9	47.8	47.8	48.7	49.1	49.5	49.6	49.6	49.6	47.8	47.8	49.5
61	62	62	53	49	45	4.4	4.4	45	62	62	45
36	32	28	25	21	10		10	22	31	34	40

49.4	49.5
46	45
49	60

51.7	51.2
2.3	28
60	51

✓

51.16
2.81
50
Walk

✓

49.6	49.5	47.8	47.6	49.0	49.5	49.6	49.5	49.4	47.6	49.4	51.1
44	45	62	64	50	45	44	45	46	64	46	29
60	49	34	26	22	10		10	22	33	42	50

51.5
2.5
60

✓

Sta.

+

π

-

Elev

953.97

17+4A

+50

✓

+64

✓

+68

Dec 13, 1957

14

2

14

24
36

50.53
3.44
Walk
50

47.0	47.4	48.1	48.6	48.9	49.0	49.0	49.0	47.4	47.2	47.1
7.0	6.6	5.9	5.4	5.1	5.0	5.0	5.0	6.6	6.8	6.9
32	27	22	20	10		10	23	27	31	36

47.0	47.9	49.0	49.2		50.8	50.4	49.8	49.1
7.0	6.1	5.0	4.8		3.2	3.6	4.2	4.9
35	40	49	60		60	51	47	40

47.8	48.1	48.6	48.7	48.8	48.9	48.8	48.8	47.2	47.0	47.8
6.2	5.9	5.4	5.3	5.2	5.1	5.2	5.2	6.8	7.0	6.2
31	28	23	18	10		10	22	27	34	39

46.7	46.7	47.7	49.1	49.17		50.5	50.1
7.3	7.3	6.3	4.9	4.80		3.5	3.9
34	35	38	49	60		60	51

Walk

49.2	48.6	48.7	48.9	48.7	48.7	48.9	48.8	48.8	47.0	47.1	50.2	50.7
4.8	5.4	5.3	5.1	5.3	5.3	5.1	5.2	5.2	7.0	6.9	3.8	3.3
48	40	32	24	19	10		10	22	27	35	50	60

49.0
49.0
4.88
3.6
Walk

49.2
4.8
60

✓

Sta

+

K

-

E/ou

953.97

17+78

+80

✓

+94

✓

18

TP

A.79

952.05

671

947.26

Dec 13, 1957

38

39

Lt

F

Rt

48.8

1.99

Walk

54

48.9

48.8

48.8

48.6

48.6

48.7

48.7

48.7

48.8

49.4

49.8

5.1 5.2 5.2 5.4 5.4 5.3 5.3 5.3 5.2 4.6 4.2
 54 40 25 18 10 10 20 28 40 46

48.9

5.1
60

51.0

30 363
 60 51
 Walk

48.8

48.8

48.5

48.4

48.5

48.6

48.5

48.4

48.4

48.4

48.9

5.2 5.2 5.5 5.6 5.5 5.4 5.5 5.6 5.6 5.6 5.1
 45 33 27 21 10 10 20 25 28 40

48.6

5.4
53

48.7

5.3
60

50.8

32 3.7
 60 53

47.8

48.7

48.3

48.3

48.4

48.5

48.5

48.4

46.9

46.8

49.1

6.2 5.3 5.7 5.7 5.6 5.5 5.5 5.6 7.1 7.2 4.9
 30 25 22 17 10 10 22 26 36 47

46.3

47.8

48.0

48.2

47.9

50.7

50.1

2.7 6.2 6.0 5.8 6.1
 34 40 46 50 60
 33 3.9
 60 53

Sta.

+

π

-

Elev.

952.05

18+29

✓

+33

✓

+43

+50

Dec 13, 1957

31
38

Lt.

≡

Rt

45.7	47.3	47.8	47.8	48.1	48.2	48.1	48.0	46.5	46.5	49.2
------	------	------	------	------	------	------	------	------	------	------

64	48	4.3	4.3	4.0	3.9	4.0	4.1	5.6	5.6	2.9
33	26	22	18	10		10	22	27	36	49

45.9	46.6	47.3	47.3							49.8
------	------	------	------	--	--	--	--	--	--	------

62	5.5	4.8	4.8							23
37	43	49	60							60

47.6	47.0	47.1	47.5	47.7	48.1	48.2	48.1	48.0	46.6	46.4	49.1
------	------	------	------	------	------	------	------	------	------	------	------

45	5.1	5.0	4.6	4.4	4.0	3.9	4.0	4.1	5.5	5.7	3.0
49	44	30	25	19	10		10	23	27	34	48

47.5

4.6
60

49.9

2.2
60

49.21

2.84
49
Walk

47.0	47.1	47.4	47.5	47.9	48.0	47.9	47.7	46.3	46.3	47.6
------	------	------	------	------	------	------	------	------	------	------

5.1	5.0	4.7	4.6	4.2	4.1	4.2	4.4	5.8	5.8	4.5
60	42	31	25	10		10	23	28	33	38

Asph

49.7

48.8

2.4
60
3.3
48

Sta + π - Elev

952.05

18 + 88

19

+ 21

+ 50

BM 3.14 952.01 3.15 948.90 (948.87)

2 Dec 13, 1957

39

47

PT

47.85
47.4
4.20
49
Walk

47.3	47.1	47.1	47.2	47.5	47.6	47.3	47.4	45.9	45.7
4.8	5.0	5.0	4.9	4.6	4.5	4.6	4.7	6.2	6.4
60	49	30	22	10		10	21	26	32

47.1	47.1	46.6
3.0	5.0	5.5
60	47	40

47.57

4.48

Cone

At. Base Pumps Island

70

47.44

4.61

Edge Conc.

60

46.5	46.5	46.7	46.8	47.1	47.2	47.1	47.0	45.3	45.3	46.4	46.9
5.6	5.6	5.4	5.3	5.0	4.9	5.0	5.1	6.8	6.8	5.7	5.2
29	26	22	17	10		10	23	28	41	52	60

46.8

46.7

46.8

5.3

5.4

5.3

35

30

60

Top Hyd. N.E. Cor Albert & Larpenteur

sta + π - Elev

952.01

19+66 Property Line

✓

+ 73

✓

+ 81 Gutter Line

+ 97

BM 1.58 950.45 3.14 948.87 (948.87)

± Dec 13, 1957

40

27

31

46.18	46.2	46.5	46.3	46.8	46.9	47.0	46.9	46.5	46.5	44.7	44.7
58.3	58	55	57	52	51	50	51	55	55	73	73
60	43	33	26	15	10		10	19	22	28	37

Conc

46.6	45.8	45.0
5.4	6.2	7.0
60	47	38

45.9	46.3	46.3	46.7	46.9	47.0	46.9	46.2	45.4	44.8	45.2
6.1	5.7	5.7	5.3	5.1	5.0	5.1	5.8	6.6	7.2	6.8
56	38	30	17	10		10	24	29	34	41

45.69	45.64	46.3	46.0
6.32	6.37	5.7	6.0
56.5	60	60	51

Conc

45.5	45.6	45.9	46.3	46.9	47.0	46.8	46.4	46.1	45.9	45.7	45.6
6.5	6.4	6.1	5.7	5.1	5.1	5.0	5.6	5.9	6.1	6.3	6.5
60	53	43	36	15	10	10	30	39	47	51	60

45.93
6.08
MH
AO

46.35
5.66
MH
AO

Top Hyd N.E. Cor Albert & Carpenter

Sta + π - Elev

950.45

20

+13

+22

✓

+30

FX
RG
CW

Dec. 16, 1957
Clear 24°

41

14

RT

46.0	46.1	46.3	46.6	46.9	47.0	46.8	46.9	46.6	46.4	46.2
4.5	4.4	4.2	3.9	3.6	3.5	3.7	3.6	3.9	4.1	4.3
60	45	31	19	10		10	13	27	41	60

45.1	45.9	46.5	46.3	46.8	46.9	46.8	46.1	46.2	45.7	45.7
5.4	4.6	4.0	4.2	3.7	3.6	3.7	4.4	4.3	4.8	4.8
60	49	35	28	10		10	28	39	54	60

46.2	46.6	46.4	46.7	46.8	46.9	46.7	46.6	46.3	45.1	44.7
4.3	3.9	4.1	3.8	3.7	3.6	3.8	3.9	4.2	5.4	5.8
40	29	22	13	10		10	13	21	28	36

45.9		46.2	45.9	44.9
4.6		4.3	4.6	5.6
60		60	48	42

45.8	46.4	46.5	46.7	46.7	46.8	46.6	46.6	46.3	46.2	44.9
4.7	4.1	4.0	3.8	3.8	3.7	3.9	3.9	4.2	4.3	5.6
30	25	22	13	10		10	13	20	22	26

45.0	44.5	44.3	44.7	45.0	46.3	46.1	45.1	44.7	44.8
5.5	6.0	6.2	5.8	5.0	4.2	4.4	5.4	5.8	5.7
34	35	37	38	42	60	55	48	41	35

46.0	45.8
4.5	4.7
60	45

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		950.45		
--	--	--------	--	--

20+50				
-------	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

+62				
-----	--	--	--	--

+85				
-----	--	--	--	--

21				
----	--	--	--	--

✓				
---	--	--	--	--

+05				
-----	--	--	--	--

Dec 16, 1957 42
RT

LT

45.5	46.3	46.3	46.7	46.8	46.5	46.5	46.4	46.1	44.9
50	4.2	4.2	3.8	3.7	40	40	41	4.4	5.6
27	23	20	10		10	14	21	23	28

44.7	44.3	44.3	44.6	45.7	46.7	44.9	44.7	44.6
------	------	------	------	------	------	------	------	------

58	6.2	6.2	5.9	4.8	3.8	5.6	5.8	5.9
35	36	37	38	43	60	48	44	36

46.3	46.2
42	43
60	53

45.15

46.12
A.33
Walk
51

5.30
FL. 6.14
47

44.4	45.7	46.7	46.5	46.5	46.6	46.3	46.4	46.3	44.8	44.1
6.1	4.8	4.3	4.0	4.0	3.9	4.2	4.1	4.2	5.7	6.4
34	24	20	13	10		10	13	21	27	35

44.5	46.1	45.1	45.0
6.0	4.4	5.4	5.5
44	51	58	60

46.9	44.8	44.2
3.6	5.7	6.3
60	48	42

44.94
4.02
53
Walk

Sta + π - Elev

250.45

21+47

✓

+52

✓

22

+06

Dec 16, 1957

43

45.1 46.1 46.5 46.4 46.5 46.3 46.3 46.2 44.2

5.4 4.4 4.0 4.1 4.0 4.2 4.2 4.3 6.3
29 21 12 10 10 13 21 27

44.3 45.1 46.5 46.7 46.5 46.1 44.7 44.1

6.2 5.4 4.0 3.8 4.0 4.4 5.8 6.4
36 44 49 60 60 54 48 35

45.9 45.9 46.1 46.4 46.4 46.5 46.3 46.3 46.2 46.9

4.6 4.6 4.4 4.1 4.1 4.0 4.2 4.2 4.3 3.6
36 26 21 13 10 10 13 21 27

46.4 46.6 46.5 46.5 46.1 44.7 44.1

4.1 3.9 4.4 4.0 4.4 5.8 6.4
49 60 Walk 60 54 48 35
51

46.7 46.7 46.3 46.5 46.3 46.4 46.2 46.2 46.1 45.9 44.2

3.8 3.8 4.2 4.0 4.2 4.1 4.3 4.3 4.4 4.6 6.3
35 25 21 12 10 10 14 21 24 28

46.7 46.6 46.2 45.7 44.7 44.4 44.0

3.8 3.9 4.3 4.8 5.8 6.1 6.5
45 60 60 52 47 42 35

18.5
1.58
Walk
50

Sta + π - Elev

950.45

22+26

✓

+31

✓

+50

✓

+54

TP 2.59 948.97 4.07 946.38

2 Dec 16, 1957

44

RT

46.6

46.5

46.5

46.3

46.4

46.1

46.2

46.1

44.3

3.9

4.0

4.0

4.2

4.1

4.4

4.3

4.4

6.2

34

22

13

10

10

14

21

27

46.7

46.6

46.5

44.5

44.1

3.8

3.9

4.0

6.0

6.4

48

60

60

46

34

44.4

46.1

46.3

46.4

46.2

46.3

46.1

46.2

46.1

44.2

44.0

6.1

4.4

4.2

4.1

4.3

4.2

4.4

4.3

4.4

6.3

6.5

31

24

21

13

10

10

13

21

28

36

44.0

45.7

46.3

46.4

44.6

6.5

4.8

4.2

4.1

5.9

37

47

60

30

47

43.7

44.2

46.1

46.3

46.2

46.3

46.0

46.1

46.1

44.4

44.2

6.8

6.3

4.4

4.2

4.3

4.2

4.5

4.4

4.4

6.1

6.3

35

29

21

14

10

10

14

21

28

35

44.1

45.5

46.2

46.5

46.5

45.9

44.7

6.4

5.0

4.3

4.0

4.0

4.6

5.8

40

47

50

60

60

52

44

Eliza
4.52
51
Walk

Sta + π - Elev.

948.97

23

✓

+ 11

+ 50

✓

+ 54

2 Dec 16, 1957 45

17

RT

44.6

46.0

46.1

46.1

46.1

45.9

46.0

46.0

46.2

45.9

4.4 3.0 2.9 2.9 2.9 3.1 3.0 3.0 2.8 3.1
29 22 14 10 10 14 20 24 27

44.0

44.2

45.5

46.0

46.4

46.2

44.8

44.0

44.1

✓

→ 5.0 4.8 3.5 3.0 2.6 2.8 4.2 5.0 4.9
34 37 43 49 60 60 45 38 33

46.20

2.77
51
walk

44.2

44.5

45.9

46.1

46.0

46.2

46.0

46.0

45.9

44.2

44.0

4.8 4.5 3.1 2.9 3.0 2.8 3.0 3.0 3.1 4.8 5.0
33 27 22 14 10 10 14 22 28 37

43.8

44.8

45.5

46.5

46.26

46.6

46.2

45.2

✓

→ 5.2 4.2 3.5 2.5 2.71 2.4 2.8 3.8
36 43 48 60 50 60 53 48

Ent.
Canc.

46.00

2.97
51
Walk

Sta + π - Elev.

948.97

24

✓

+06

+13

+50

✓

+61

Dec 16, 1957 46

Lt

Rt

44.1 45.7 45.9 45.8 46.0 45.7 45.7 45.4 43.9

4.9 3.3 3.1 3.2 3.0 3.3 3.3 3.6 5.1
27 21 13 10 10 15 23 30

43.9 43.5 45.1 45.9 46.3 46.5 46.4 44.9 43.8

5.1 5.5 3.9 3.1 2.7 2.5 2.6 4.1 5.2
33 36 43 50 60 60 57 46 35

46.00
2.97
50

46.25
2.72
53
Walk

Asph on Ribbon

44.5 45.9 45.8 45.7 45.7 45.5 45.4 45.1 44.0 43.9

4.5 3.1 3.2 3.3 3.3 3.5 3.6 3.9 5.0 5.1
27 20 13 10 10 14 24 28 32

43.5 44.8 45.5 45.9 44.8 44.1

5.5 4.2 3.5 3.1 4.2 4.9
36 47 60 60 48 42

44.95

45.20

A.02
Conc Rib
44

3.77
Walk
51

Sta + π - Elev.

948.97

25

✓

+50

✓

Note: Station Attendant said there are only
Asph. Ent Now as the grade has not been
definitely been set. Pumps could possibly
be lowered

TP	2.13	950.07	1.03	947.94	94
BM			3.28	946.79	(946.74)

Dec. 16, 1957 47

Rt.

44.2

45.4

45.5

45.6

45.62

45.4

45.2

45.0

44.4

4.8 3.6 3.5 3.4 3.35 3.6 3.8 4.0 4.6
27 21 15 10 10 16 21 31

43.8

43.4

44.0

44.5

44.5

45.2

44.8

44.6

5.2 5.6 5.0 4.5 4.5 3.8 4.2 4.4
32 37 46 50 60 60 50 39

43.4

44.0

45.3

45.5

45.4

45.5

45.2

45.1

44.7

44.6

5.6 5.0 3.7 3.5 3.6 3.5 3.8 3.9 4.3 4.4
36 26 21 14 10 10 16 26 37

43.4

44.3

44.3

46.2

45.7

45.5

45.3

5.6 4.7 4.7
44 51 60

2.8 3.3 3.5 3.7
101 71.5 60 48
Walk Aglat Pump

Top Hyd S.W. Cor Hamline & Largentoun

Sta	+ π	- Elev
1	2	3
4	5	6
7	8	9
10	11	12
13	14	15
16	17	18
19	20	21
22	23	24
25	26	27
28	29	30
31	32	33
34	35	36
37	38	39
40	41	42
43	44	45
46	47	48
49	50	51
52	53	54
55	56	57
58	59	60
61	62	63
64	65	66
67	68	69
70	71	72
73	74	75
76	77	78
79	80	81
82	83	84
85	86	87
88	89	90
91	92	93
94	95	96
97	98	99
100	101	102
103	104	105
106	107	108
109	110	111
112	113	114
115	116	117
118	119	120
121	122	123
124	125	126
127	128	129
130	131	132
133	134	135
136	137	138
139	140	141
142	143	144
145	146	147
148	149	150
151	152	153
154	155	156
157	158	159
160	161	162
163	164	165
166	167	168
169	170	171
172	173	174
175	176	177
178	179	180
181	182	183
184	185	186
187	188	189
190	191	192
193	194	195
196	197	198
199	200	201
202	203	204
205	206	207
208	209	210
211	212	213
214	215	216
217	218	219
220	221	222
223	224	225
226	227	228
229	230	231
232	233	234
235	236	237
238	239	240
241	242	243
244	245	246
247	248	249
250	251	252
253	254	255
256	257	258
259	260	261
262	263	264
265	266	267
268	269	270
271	272	273
274	275	276
277	278	279
280	281	282
283	284	285
286	287	288
289	290	291
292	293	294
295	296	297
298	299	300
301	302	303
304	305	306
307	308	309
310	311	312
313	314	315
316	317	318
319	320	321
322	323	324
325	326	327
328	329	330
331	332	333
334	335	336
337	338	339
340	341	342
343	344	345
346	347	348
349	350	351
352	353	354
355	356	357
358	359	360
361	362	363
364	365	366
36		

+

π

—

Flex

Lt

£

St

48

~~Top Hyd SW. Cor Carpenter & Hamline~~

~~2255 W Larp~~

~~Top Hyd SW. Cor Fernwood~~

Sta	+	X	-	Elev
BM	3.60	950.34		946.74

26+00

✓

+23

✓

+25

FX
 RG
 KP
 GW

Dec 19, 1957
 Overcast 320 81 49

S.W. Cor Hamline & Carpenter Hy

44.1	43.3	43.3	45.1	45.2	45.3	44.8	44.7	45.0	45.0	45.1
62	70	70	5.2	5.1	5.0	5.5	5.6	5.3	5.3	5.2
44	40	30	24	14		20	28	30	49	62
	44.5									
		44.6								
	58	5.7								
	52	60								

at base pump
Island

42.4	42.4	45.0	44.8	45.0	45.1	45.0	44.7	44.9	44.8	44.9
7.9	7.9	5.3	5.5	5.3	5.2	5.3	5.6	5.4	5.5	5.9
37	34	28	25	10		14	25	33	40	60
	44.3									
		44.7								
	6.0	5.6	5.5							
	38	55	60							

45.2	44.7	44.9	45.1	45.0	45.1	45.0	44.6	44.9	44.7	44.8
5.1	5.6	5.4	5.2	5.3	5.2	5.3	5.7	5.4	5.4	5.5
31	28	24	15	10		13	26	33	40	60
	45.2									
		44.6								
	5.1	5.7	5.6	5.5						
	37	39	53	60						

Sta + π - Elev

950.34

26+46 Gutter Line

+62 $\neq$ Hamline

✓

✓

+78 Gutter Line

Dec. 19, 1957
RT

50

11

45.2	45.1	45.0	45.0	45.1	44.7	44.5	44.5	44.6
5.1	5.2	5.3	5.3	5.2	5.6	5.8	5.8	5.7
64	47	30	14		19	40	34	69

45.8	45.4	45.1	44.9	45.0	44.8	44.8	44.8	45.0
4.5	4.9	5.2	5.4	5.3	5.5	5.5	5.5	5.3
100	75	50	25		11	32	43	67

46.2	46.7	47.3	47.7	45.3	45.3	45.1	45.1	45.1
4.1	3.6	3.0	2.6	5.0	5.0	5.2	5.2	5.2
125	150	200	225	175	150	125	100	82

48.5	48.3	48.0	45.4	45.2	44.9	44.5
1.8	2.0	2.3	4.9	5.1	5.4	5.8
300	275	250	200	225	250	275

45.0	44.7	44.5	44.6	44.6	44.4	44.3	44.6	44.6
5.3	5.6	5.8	5.7	5.7	5.9	6.0	5.7	5.7
90	57	40	16		16	26	33	50

60

44.8
5.5
66

Sta + π - Elev.

950.34

26+94 E. Prop. Line Hamline

✓

✓

✓

27

Dec 19, 1957

51

LH

RT

44.9	44.6	44.0	43.9	44.1	43.9	43.8	44.8	45.2
5.4	5.7	6.3	6.4	6.2	6.4	6.5	5.5	5.1
53	36	25	20		15	18	23	37

45.5
4.8
70

45.2
45.1
45.0
44.8
45.1
5.1 5.2 5.3 5.5 5.2
85 65 50 43 42

45.4
45.76
45.9
46.1
4.9 4.58 4.4 4.2
97 99 115 133
Walk

46.1
46.1
46.2
46.2
4.2 4.2 4.1 4.1
200 190 165 154

44.1	43.7	43.8	43.7	43.8	43.6	44.4	44.7	44.5
6.2	6.6	6.5	6.6	6.5	6.7	5.9	5.6	5.8
27	25	21	19		17	22	29	31

44.9
45.3
45.4
45.7
5.4 5.0 4.9 4.6
38 49 59 69

45.3
45.2
45.0
5.0 5.1 5.3
67 59 47

Laop Ave
Snelling To Fernwood

Sta + π - Elev

950.34

27+22

✓

+27

✓

+50

21

RT

44.1	43.3	42.4	42.5	42.8	42.8	43.3	43.4	44.5	45.1
6.2	7.0	7.9	7.8	7.5	7.5	7.0	6.9	5.8	5.2
27	23	21	18		18	22	26	37	48

45.4	46.6	46.6	46.6					45.3	
4.9	3.7	3.7	3.7					5.0	
31	38	52	60					58	
								Bldg	

45.9	40.6	40.6	41.9	42.2	42.6	42.5	43.0	43.8	44.7	45.2
4.4	9.7	9.7	8.4	8.1	7.7	7.8	7.3	6.5	5.6	5.1
31	26	23	22	18		17	21	32	43	50

46.9	46.9
3.4	3.4
46	65



40.0	40.0	40.8	41.2	41.4	41.4	41.8	42.5	42.9
10.3	10.3	9.5	9.1	8.9	8.9	8.5	7.8	7.4
25	23	21	14		19	21	34	42



46.9	47.3
3.4	3.0
33	38
	Bldg
	L.O.

45.7	45.2	44.9
4.6	5.1	5.4
64	52	49
Bldg		

Sta	+	π	-	Elev
		950.34		

28

✓

TP	13.50	953.89	9.95	940.39
----	-------	--------	------	--------

+20

+50

+68

TP	0.58	940.97	13.56	940.39
----	------	--------	-------	--------

Dec 18 1957

53

Lt

Rt

37.5	37.5	38.2	38.2	38.9	38.6	38.1	38.7	42.8
12.8	12.8	12.1	12.1	11.4	11.7	12.2	11.6	7.5
23	22	21	18		17	24	33	40

48.5

49.4

45.8

45.3

45.1

44.8

1.8

0.9

4.5

5.0

5.2

5.5

38

51

75

62

58

49

40

Nail in PP Rt sta 28+10

49.7

48.9

42.1

44.8

45.2

45.9

45.9

4.2

5.0

11.8

9.1

8.7

8.0

8.0

50

40

35

46

50

62

75

49.4

49.2

49.1

48.9

4.5

4.7

4.8

5.0

96

70

50

40

Garage

49.8

49.6

49.8

49.7

46.6

41.4

4.3

4.1

4.2

7.3

88

70

50

42

40

49.9

4.0

100

Sta	+	π	-	Elev
-----	---	-------	---	------

Sta	+	π	-	Elev
-----	---	-------	---	------

940.97

Sta	+	π	-	Elev
-----	---	-------	---	------

28+20

Sta	+	π	-	Elev
-----	---	-------	---	------

+50

Sta	+	π	-	Elev
-----	---	-------	---	------

✓

Sta	+	π	-	Elev
-----	---	-------	---	------

+68

Sta	+	π	-	Elev
-----	---	-------	---	------

✓

Sta	+	π	-	Elev
-----	---	-------	---	------

+93

Sta + Δ - Elev

940.97

29

✓

TP 1.52 935.36 7.13 933.84

+26 in Ditch

✓

+26.5 Top Culvert

+50

Dec 19, 1957

55

Lt

Rt

33.3	33.5	34.0	34.2	34.1	33.9	33.8	34.3	34.1	33.5
7.7	7.5	7.0	6.8	6.9	7.1	7.2	6.7	6.9	7.5
23	20	17	11		16	23	24	24.5	35

Curb

34.9	33.8	33.5	32.6	28.7		31.2	31.0	33.4	X
6.1	7.2	7.5	8.4	12.3		9.8	10.0	7.6	
25	35	42	47	55		62	52	46	

Top W. 1 24" CM Lt St. 29 + 26

33.9	31.9	31.9	33.5	33.4	33.2	33.0	32.9	33.4	33.0
1.5	3.5	3.5	1.9	2.0	2.2	2.4	2.5	2.0	2.4
24	21.5	20.5	20	12		15	24	24	27

Guth Curb

32.9	32.4	27.8	24.2			30.6	31.1	32.6	X
2.5	3.0	2.6	1.2			4.8	4.3	2.8	
36	47	57	62			60	52	49	

33.6	34.0	33.7	33.4
1.8	1.4	1.7	2.0
27	23	20	12

32.3	33.0	32.6	32.5	32.4	32.2	31.9	32.4	32.1
3.1	2.4	2.8	2.9	3.0	3.2	3.5	3.0	3.3
26	21	17	11		12	G	C	27

24

31.5	31.3	24.8	23.5	29.6	30.1	31.8	31.9
3.9	4.1	10.6	11.9	5.8	5.3	3.6	2.5
36	47	58	60	60	52	49	39

Sta + x - Elev

935.36

872

30

926.64

✓

+50

✓

TP 2.27 928.91 8.72 926.64

2.27

928.91

31

✓

Dec 19, 1956

54

14

14

30.2	30.8	30.5	30.5	30.5	30.2	30.1	30.6	30.3
5.2	4.6	4.9	4.9	4.9	5.2	5.3	4.8	5.1
25	C	G	10		17	6	C	26

29.9

29.7

22.6

27.8

28.0

29.7

30.2

5.5

5.7

12.8

7.6

7.4

5.7

5.2

37

47

60

60

52

49

37

28.2

28.7

28.3

28.6

28.6

28.3

28.1

28.6

28.3

7.2

6.7

7.1

6.8

6.8

7.1

7.3

6.8

7.1

24

C

G

10

6

12

G

C

30

21

26

28.1

28.2

21.2

25.0

25.5

27.6

27.9

7.3

7.2

14.2

10.4

9.9

7.8

7.5

34

48

60

60

54

51

40

Sta

26.5

26.9

26.5

26.6

26.6

26.5

26.2

26.7

26.1

24

20

24

23

23

24

27

22

28

30

C

G

10

13

G

29

35

23

28

26.4

26.3

18.9

22.7

22.8

25.5

25.8

25

26

10.0

6.2

6.1

3.4

3.1

40

46

60

60

57

52

46

Sta + π - Elev.

928.91

31+50

✓

32

✓

415

+28

Dec 13, 1957

57

Lt

Rt

24.9	24.9	24.5	24.6	24.6	24.1	24.5	24.0	23.6
40	40	44	43	43	48	44	49	53
28	C	G	20		G	C	30	44
	24				27			

24.3	24.2	18.5	18.5			21.0	21.3	23.4
46	47	10.4	10.4			7.9	7.6	5.5
36	47	57	60			60	55	52

22.4	22.9	22.4	22.6	22.6	22.0	22.0	22.3	22.0
65	60	65	6.3	6.3	6.9	6.9	6.6	6.9
32	C	G	20		24	G	C	29
	26					27		

22.1	21.8	14.6			18.0	18.2	20.8	21.6
6.8	7.1	14.3			10.9	10.7	8.1	7.3
43	49	60			60	54	51	39

17.47

11.44
S. D Ring
339

20.47

842
33.9

Grote MH

Sta + π - Elev.

928.91

10.42

32+50

918.49

✓

TP 2.02 920.51 10.42 918.49

33

✓

+50

✓

2 Dec 19, 1957

58

LT

RT

20.2	20.6	20.2	20.7	20.7	20.1	20.0	20.3	19.9
8.7	8.3	8.7	8.2	8.2	8.8	8.9	8.6	9.0
29	C	G	17		20	G	C	29
	28					28		

19.8	19.6	18.3		15.5	16.0	18.7	19.5
21	93	15.6		13.9	12.9	10.2	9.4
42	50	60		60	56	50	40

18.1	18.4	17.9	18.3	18.5	18.1	18.0	18.4	17.9
24	21	2.6	2.2	2.0	2.4	2.5	2.1	2.6
33	C	G	20		20	G	C	32
	30					29		

17.9	17.5	10.9		15.2	15.7	16.8	18.4
2.6	3.0	9.6		5.3	4.8	3.7	2.1
42	48	60		60	56	51	43

15.7	16.2	15.7	16.0	16.2	15.9	15.8	16.2	15.9
4.8	4.3	4.8	4.5	4.3	4.6	4.7	4.3	4.6
42	C	G	20	3.3	3.6	G	C	31
	33				20	29		

15.4	07.5		14.6	14.2	15.3	15.5
5.1	13.00		5.9	6.3	5.2	5.0
48	60		60	58	50	45

Sta + π - Elev.

920.51

34

✓

TP 3.29 914.22 9.58 910.93

+50

✓

35

✓

+10

Dec 18 1957

59

11.

RT.

13.7	14.0	13.5	13.9	14.2	13.8	13.6	14.0	13.6
6.8	6.5	7.0	6.6	6.3	6.7	6.9	6.5	6.9
39	C	G	20		20	G	C	33
	22					29		

13.5	6.5					12.4	13.0	13.3
7.0	14.0					8.1	2.5	2.2
48	60					60	53	47

11.9	12.3	11.8	12.2	12.4	12.0	11.8	12.3	11.8
2.3	1.9	2.4	2.0	1.8	2.2	2.4	1.9	2.4
37	C	G	20		20	G	C	35
	32					30		

11.4	3.4					12.3	11.9	11.8
2.8	10.8					1.9	2.3	2.4
49	60					60	56	47

10.8	10.3	10.7	10.9	10.9	10.6	10.4	10.8	10.5
3.4	3.9	3.5	3.3	3.3	3.6	3.8	3.4	3.7
C	G	25	20		20	G	C	42
33						31		

10.5	10.1	8.4	8.2	7.6		12.1	11.6	10.7
3.7	4.1	5.8	6.0	6.6		2.1	2.6	3.5
39	49	54	59	60		60	58	53

09.50
4.72
For MH Gate
33.9

Sta + π - Elev

914.22

35+50

✓

36

✓

+50

Dec 19, 1957

60

LT

RT

09.7	10.0	09.5	09.7	09.7	09.3	09.1	09.5	09.5
4.5	4.2	4.7	4.5	4.5	4.9	5.1	4.7	4.7
39	C	G	20		20	G	C	41
	32					31		

09.7	10.2				11.3	11.6	10.7	09.8
4.5	4.0				2.9	2.6	3.3	4.4
50	60				60	58	55	53

08.9	09.0	08.5	08.7	08.6	08.3	08.0	08.5	08.6
5.3	5.2	5.7	5.5	5.6	5.9	6.2	5.7	5.6
36	G	G	20		20	G	C	42
	33					32		

09.0	09.0	10.8				11.8	11.2	08.8
5.2	5.2	3.4				2.4	3.0	5.4
48	55	60				60	56	53

08.4	08.4	07.9	08.0	07.9	07.7	07.4	07.7	07.4	08.1
5.8	5.8	6.3	6.2	6.3	6.5	6.8	6.3	6.8	4.1
39	C	G	20		20	G	C	41	51
	33					32			

08.5	11.1	11.7				11.4	09.8	08.4
5.7	3.1	2.5				2.8	4.4	5.8
48	56	60				60	56	53

Sta + π - Elev.

914.22

6.84

907.38

37

✓

TP 5.93 913.31 6.84 907.38

5.93

913.31

+50

✓

+62

+68

± Dec 19, 1957 61

LT

RT

0 9.4	0 7.6	0 7.4	0 7.4	0 7.6	0 7.2	0 6.9	0 7.4	0 7.5
4.8	6.6	6.8	6.8	6.6	7.0	7.3	6.8	6.7
60	47	39	20		20	G	C	37

0 8.8	0 8.2	0 7.0	0 7.8
5.4	6.0	7.2	6.4
60	57	50	42

0 7.0	0 7.3	0 6.9	0 7.4	0 7.5	0 7.1	0 6.8	0 7.1	0 7.6
6.3	6.0	6.4	5.9	5.8	6.2	6.5	6.2	5.7
44	C	G	20		20	G	C	42
	34					33		

12.6
0.7
60

0 4.2	0 4.6	0 5.5
9.1	8.7	7.8
60	53	47

0 6.24
7.07
Top MH Grate
33.9

0 6.20
7.11
Top MH Grate
33.9 5.2 decm

0 6.59
36'
Top "H" CB

Ice

Sta	+	X	-	Elev
-----	---	---	---	------

Sta	+	X	-	Elev
		913.31		

Sta	+	X	-	Elev
38				

Sta	+	X	-	Elev
✓				

Sta	+	X	-	Elev
+50				

Sta	+	X	-	Elev
✓				

Sta	+	X	-	Elev
39				

Dec. 19, 1957 62

BT

11

08.2

51

C

37

07.9

5.4

44

07.7

5.6

G

11.4

1.9

56

07.7

5.6

32

11.7

1.4

60

07.8

5.5

20

08.0

5.3

07.5

5.8

20

07.1

6.2

G

35

07.6

5.7

C

06.1

2.2

60

07.2

6.1

40

06.2

7.1

51

08.3

5.0

46

08.2

5.1

40

08.3

5.0

33

08.4

4.9

20

08.5

4.8

20

08.1

5.2

20

07.7

5.6

35

07.6

5.7

38

07.2

6.1

47

08.7

4.6

60

07.0

6.3

60

07.0

6.3

57

09.5

3.8

60

09.3

4.0

47

08.9

4.4

32

09.1

4.2

20

09.2

4.1

20

09.1

4.2

20

08.7

4.6

G

09.2

4.1

C

35

08.8

4.5

36

14.8

11.5

57

14.6

11.3

49

12.8

0.5

45

44

08.8

4.5

44

Sta + π - Elev

913.31
3.30

39+34

+30

TP 5.97 915.98 3.30 910.01

BM 1.08 1.08 914.90 914.89

BM

Dec 19, 1957 63

14

15

09.8	09.2	09.5	09.6	09.7	09.5	09.2	09.7
3.5	4.1	3.8	3.7	3.6	3.8	4.1	3.6
C	G	26	14		20	G	C
3.5						3.5	

✓

09.8	09.9		15.3	14.4	12.5	09.6	09.8
3.5	3.4		+2.0	+1.1	0.8	3.7	3.5
52	60		56	48	44	44	39

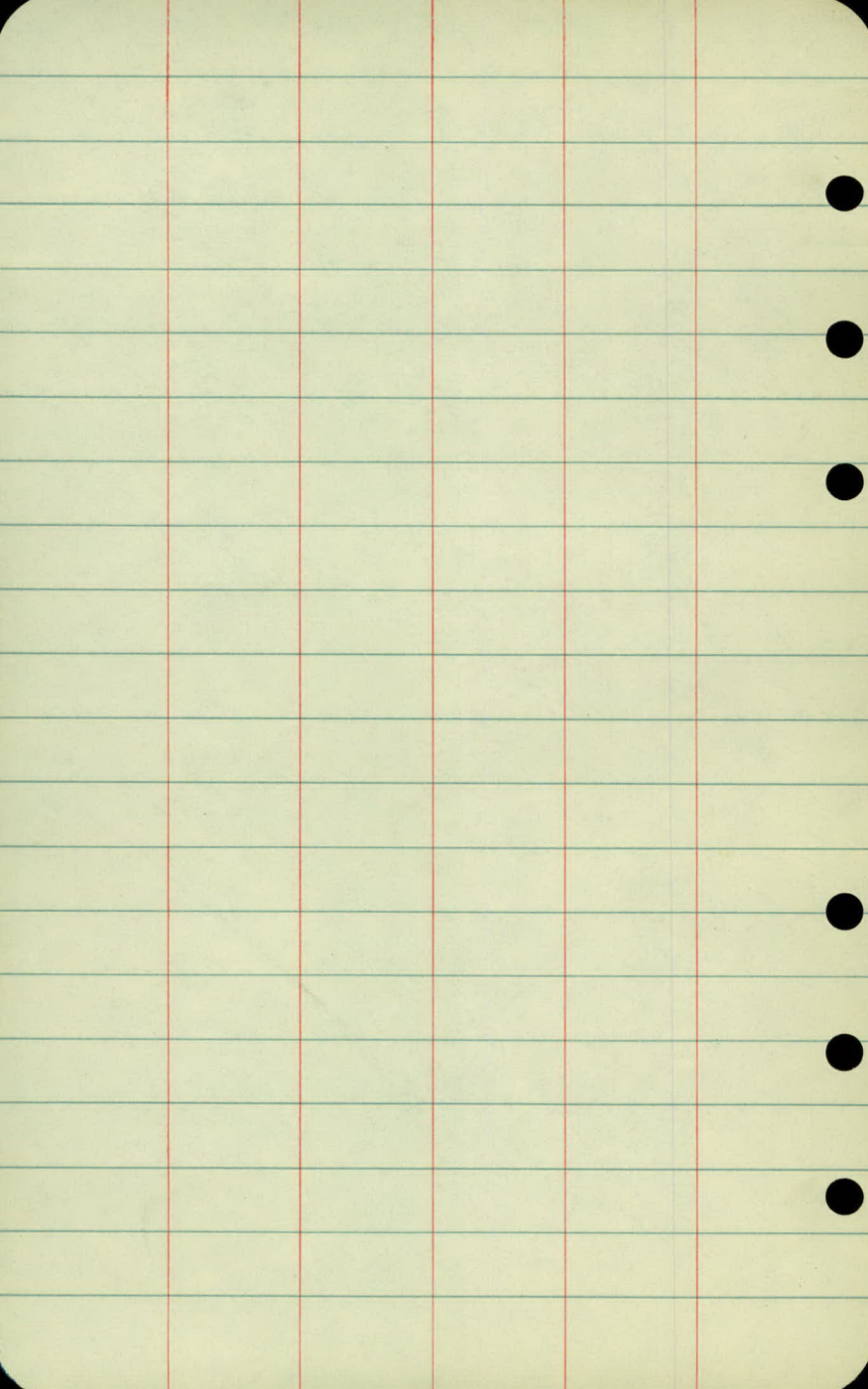
09.24

4.09

Top HHRing
33.9

Top Hyd SW Cor Fernwood & Larp

Plotted
L.D. 7.1



AK
RG
KP
CW

Dec 20, 1957

6A

Sta	+	π	-	Elev.
BM	1.33	959.38		958.05

0+00

+50

+79 $\pm$ N. Bound Lane

1

+13 $\pm$ Island

✓

Dec 20, 1957

65

It

RT

Top Hyd So. side Larpentour at Snelling

56.5

2.9

✓

56.0

3.4

✓

56.6

2.8

100

56.3

3.1

50

55.8

3.6

55.3

4.1

50

54.7

4.7

100

✓

56.2

3.2

60

55.9

3.5

45

55.7

3.7

32

55.5

3.9

55.3

4.1

28

55.2

4.2

58

55.2

4.2

60

✓

56.0

3.4

35

55.9

3.5

26

55.4

4.0

23

55.4

4.0

19

55.3

4.1

55.1

4.3

27

55.9

3.5

30

55.7

3.7

46

55.4

4.0

60

55.6

3.8

49

55.0

4.4

60

✓

Sta + π - Elev

959.38

+20 Service Lane Gutter Line

✓

+26

+37

+50 Gutter Line

✓

+60 Property Line

Dec 29, 1957 66

14

54.9	54.9	55.3	55.2	55.2	55.1	55.0	54.9	54.7
4.5	4.5	4.1	4.2	4.2	4.3	4.4	4.5	4.0
54	40	24	15		15	30	37	53

54.9
4.5
60

54.12

54.6
4.8
60

4.46
100 MH 41

55.0	55.0	54.9	54.9	54.7	54.9	54.8	54.5	54.2
4.4	4.5	4.5	4.7	4.5	4.6	4.9	5.2	
75	50	39	22	15	25	50	75	

54.6
4.8
60

54.71	54.4	54.6	54.4	54.6	54.5	54.4	54.2	54.63
4.67	5.0	4.8	5.0	4.8	4.9	5.0	5.2	4.75
C	G	20	15		19	28	G	C

4.5

54.74

54.5

54.6

54.2

54.73

54.4

54.54	54.2	54.3	54.4	54.5	54.5	54.1	54.52	55.00
4.84	5.2	5.1	5.0	4.9	4.9	5.3	4.86	4.38
C	G	17	10		20	G	C	50

30

54.5

54.7

54.3

54.89

4.49

60

200C

54.5

4.9

37

4.7

48

5.1

62

54.89

4.49

60

200C

Sta + π - Elev.

959.38

2

✓

+50

✓

+53

Possible MH

28' Rt
29' Lt

3

✓

+10

T.P.

5.70

958.91

6.17

953.21

Dec 20, 1957

67

14

RT

54.10

5.28

0

30

53.7

5.7

6

20

53.9

5.5

20

54.0

5.4

10

54.1

5.3

54.0

5.4

10

53.7

5.7

6

30

54.06

5.32

50

4.79

50

Conc

54.69

1.69

60

Conc

53.9

5.5

42

54.0

5.4

60

53.46

5.92

C

30

53.1

6.3

G

53.3

6.1

20

53.4

6.0

10

53.5

5.9

53.3

6.1

10

53.1

6.3

G

30

53.96

5.42

Walk

50

53.9

5.5

60

53.7

5.7

38

53.9

5.5

54

54.0

5.4

60

52.99

6.39

C

30

52.6

6.8

G

52.8

6.6

20

52.9

6.5

10

53.0

6.4

52.9

6.5

10

52.8

6.6

20

52.6

6.8

30

52.96

6.42

C

53.3

6.1

41

53.6

5.8

49

53.72

5.6

60

Walk

53.2

6.2

60

53.3

6.1

50

Top MH 41

Sta	+	π	-	Elev
-----	---	-------	---	------

		958.91		
--	--	--------	--	--

3+50				
------	--	--	--	--

✓				
---	--	--	--	--

4				
---	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

+96				
-----	--	--	--	--

Dec. 20, 1957 68

14 51

52.67	52.2	52.5	52.5	52.6	52.4	52.1	52.55
6.24	6.7	6.4	6.4	6.3	6.5	6.8	6.36
C	G	20	10		10	G	C
30						30	
53.2	53.5	53.66		52.65	52.5	52.5	52.5
5.7	5.4	5.25		6.26	6.4	6.4	6.4
43	50	60		71	60	50	44
		Walk		Walk			

52.41	51.9	52.2	52.2	52.3	52.2	52.1	52.0	52.38
6.50	7.0	6.7	6.7	6.6	6.7	6.8	6.9	6.53
C	G	20	10		10	20	G	C
30						30		
53.57	53.77				52.60	52.6	52.5	
5.34	5.14				6.31	6.3	6.4	
51	60				73	50	46	
Walk	Walk				Walk			

52.16	51.7	51.9	51.9	52.0	51.9	51.9	51.6	52.07
6.75	7.2	7.0	7.0	6.9	7.0	7.0	7.3	6.84
C	G	20	10		10	20	G	C
30							30	
53.0	53.82					52.51	52.6	52.3
5.9	5.09					6.40	6.3	6.6
42	60					71	56	42
	Walk					Walk		
	52.34							

6.57
Top M.H. 41 10.15 deep

Sta + Δ - Elev

958.91

5

✓

+ 50

✓

+ 46

BM

4.41 954.50 (954.49)

Dec 20, 1957

69

Lt.

Rt

51.88

7.03

C

30

52.4

6.5

44

51.4

7.5

G

52.7

6.2

60

51.6

7.3

20

51.7

7.2

10

51.8

7.1

51.7

7.2

10

51.8

7.1

20

51.3

7.6

G

52.58

6.35

71

Walk

51.83

7.08

C

52.4

6.5

51

51.65

7.26

C

30

52.4

6.5

49

51.1

7.8

G

52.96

5.95

59

51.5

7.4

20

51.5

7.4

10

51.6

7.3

51.5

7.4

10

51.5

7.4

20

51.1

7.8

G

52.34

6.57

71

Walk

51.55

7.36

C

52.0

6.9

49

51.75

7.16

MH

35

Tip Hyd at Arona

Sta + π - Elev

BM 2.60 951.47 948.87

19+97 $\pm$ Albert St

23+

23+

22+00 $\pm$ 5.15 946.32 946.35

2 Dec 20, 1957

70

21

81

Top Hyd NE Co. Albert St

45.7	45.7	45.7	45.6	46.1	46.92	46.3	45.9	45.8	45.7
5.8	5.8	5.8	5.9	5.4	4.55	5.2	5.6	5.7	5.8
250	200	150	100	50		50	100	150	200

44.92

6.55

Top MH

41'

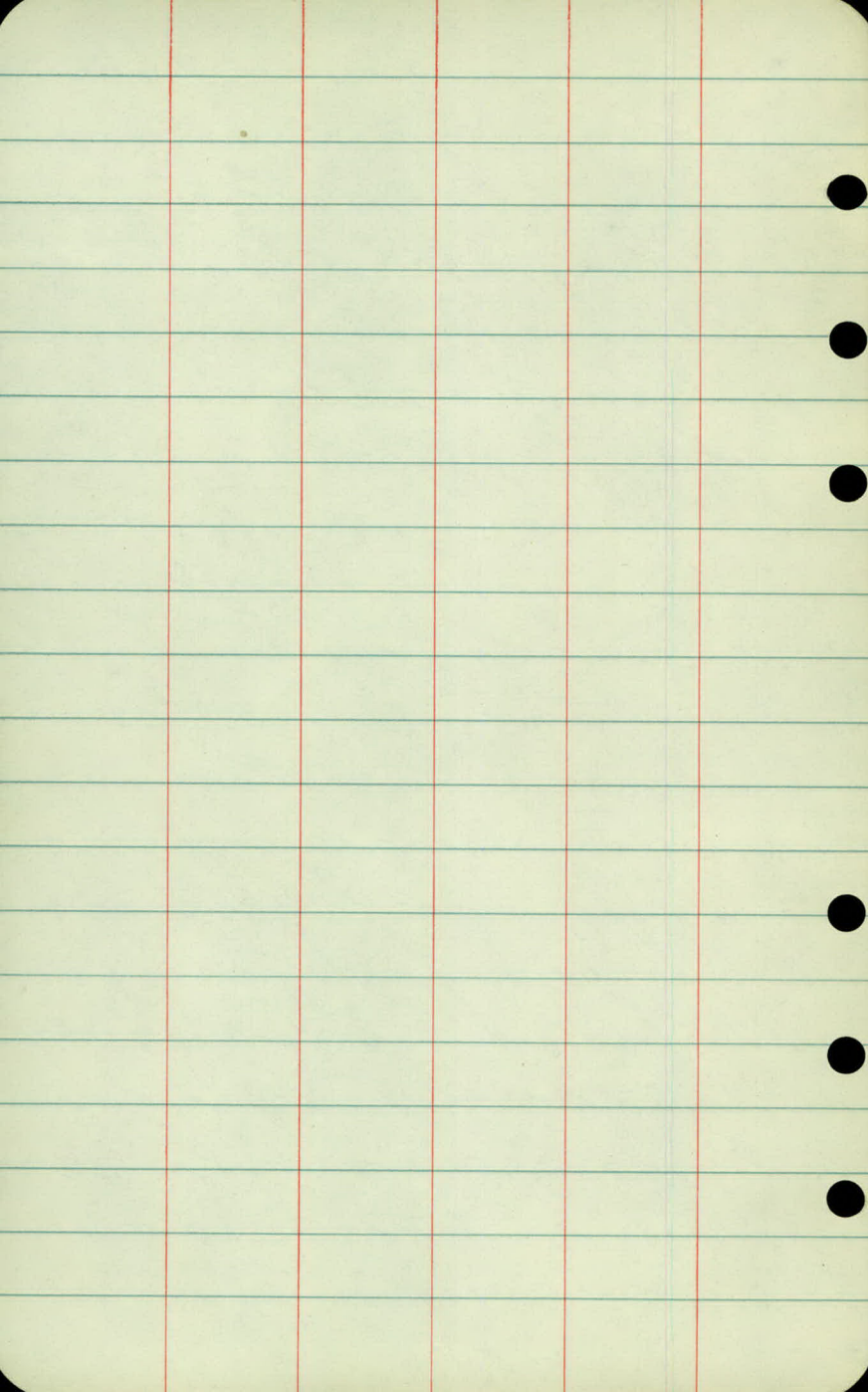
44.70

6.77

Top MH

41'

✓ plotted
L.D. J.



FX
RG
CW
RJ

January 24, 1958
Overcast Raw 24° a

Locations at Snelling

5

$$491 \frac{MH}{24}$$

4

3

2

$$153 \frac{MH}{24'}$$

1

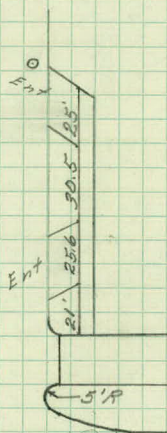
$$\begin{array}{rcl}
 +51 & \frac{Curb}{35 \rightarrow} & \\
 +20 & \frac{E.R.C.}{34} & +20 \frac{Cur Conc}{35.1} \\
 +10 & \frac{R.C.C}{31} & +13 \frac{Curb}{29.3} \\
 +00 & \frac{Curb}{65+80} & +07.5 \frac{Curb}{35}
 \end{array}$$

0

Jan 24, 1958

6

0

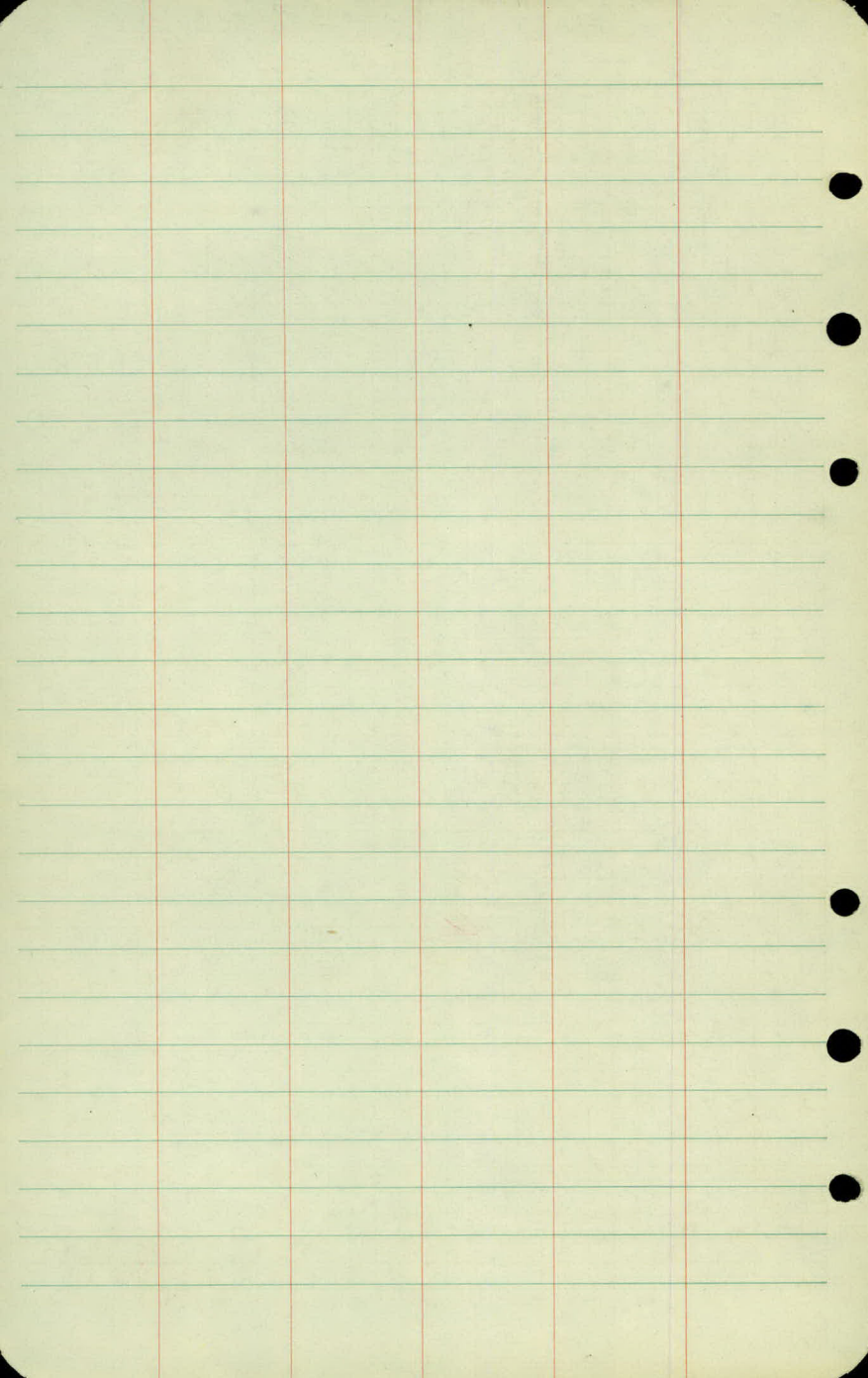


25 Ent

30.5

Ent 25.6

21



Jan 24, 1958

C

x-sections

Sta	+	π	-	Elev.
BM	1.80	959.85		958.05

1+01

Arena North

BM	2.71	957.20		954.49
----	------	--------	--	--------

0+50

+75

1+04

7+00	El Arpentier	5.72	951.48
------	--------------	------	--------

Jan 24, 1938

d

lt.

rt

Top Hyd Snelling & Larpenteur

55.73	55.71	55.50	55.31	55.26
4.12	4.14	4.35	4.54	4.59
30	26		26	35

Top Hyd NE

52.14	51.90	51.4	51.4	51.38	51.0	51.6	51.59	51.66
50.6	5.30	5.8	5.8	5.82	6.2	5.6	5.61	5.54
30	C	G	16		16	19	25	30
	21.5						Walk	

52.44	52.3	51.2	51.26	51.0	51.7	51.69	51.79
4.76	4.9	6.0	5.94	6.2	5.5	5.51	5.41
30.6	25	16		17	20	25	30
Conc						Walk	

52.5	51.55	50.9	51.19	51.0	52.0	51.83	51.94
4.7	5.65	6.3	6.01	6.2	5.2	5.37	5.26
30	16	15.5		16	20	25	30
	TopCB					Walk	

Hamline Ave 50

Sta + - Elev.

BM 3.20 949.94

(946.24)

0+50 Hamline S.

0+99 Hamline S.

0+50 Hamline N

1

+50

45.3

26+38 MH ~~45.287~~

5.24

44.70

26+38 MH 40.5' Lt

5.12

44.82

27+00 61' arched

6.07

43.87

Jan 24, 1958

e

LT

RT

Top Hyd SW Cor Hamline & Carpenter

45.14	44.82	44.6	44.88	44.4	44.6	44.7	45.0
4.80	5.12	5.3	5.06	5.5	5.3	5.2	4.9
50	30	16		17	27	38	50
conc							

45.3	45.1	44.7	44.8	45.12	44.8	45.4	45.66	45.81
4.6	4.8	5.2	5.1	4.82	5.1	4.5	4.28	4.13
50	37	20	11		17	26	29	35
mark								

44.6	44.6	44.8	45.0	45.1	44.6	44.7	45.0	45.8
5.3	5.3	5.1	4.9	4.8	5.3	5.2	4.9	4.1
50	44	28	20		14	23	36	50

45.1	45.4	45.4	45.79	45.2	45.0	46.0	46.5
4.8	4.5	4.5	4.15	4.7	4.9	3.9	3.4
50	30	21		16	27	32	50

45.7	45.8	46.1	46.70	46.2	45.4	46.1	46.5
4.2	4.1	3.8	3.24	3.7	4.5	3.8	3.4
50	35	18		13	28	31	50

MH 16. A' Deep Inv in from W & N
Inv out South

MH 15.8' Deep Same

Sta + π - Elev

BM 0.21 913.07

(912.86)

✓
38+28.95

✓
+38.95 E. Alley

✓
+48.95

✓
38+00 E. Larp 5.12 907.95

Jan 24, 1958

\$

f

Lt.

1255

Rt.

S.W. Co. Conc Ent slab 1550 W Carpenter

08.4	08.0	08.2	08.25	07.7	07.4	07.7	07.0
4.7	5.1	4.9	4.82	5.4	5.7	5.4	6.1
50	35	23		25	34	35	4.6

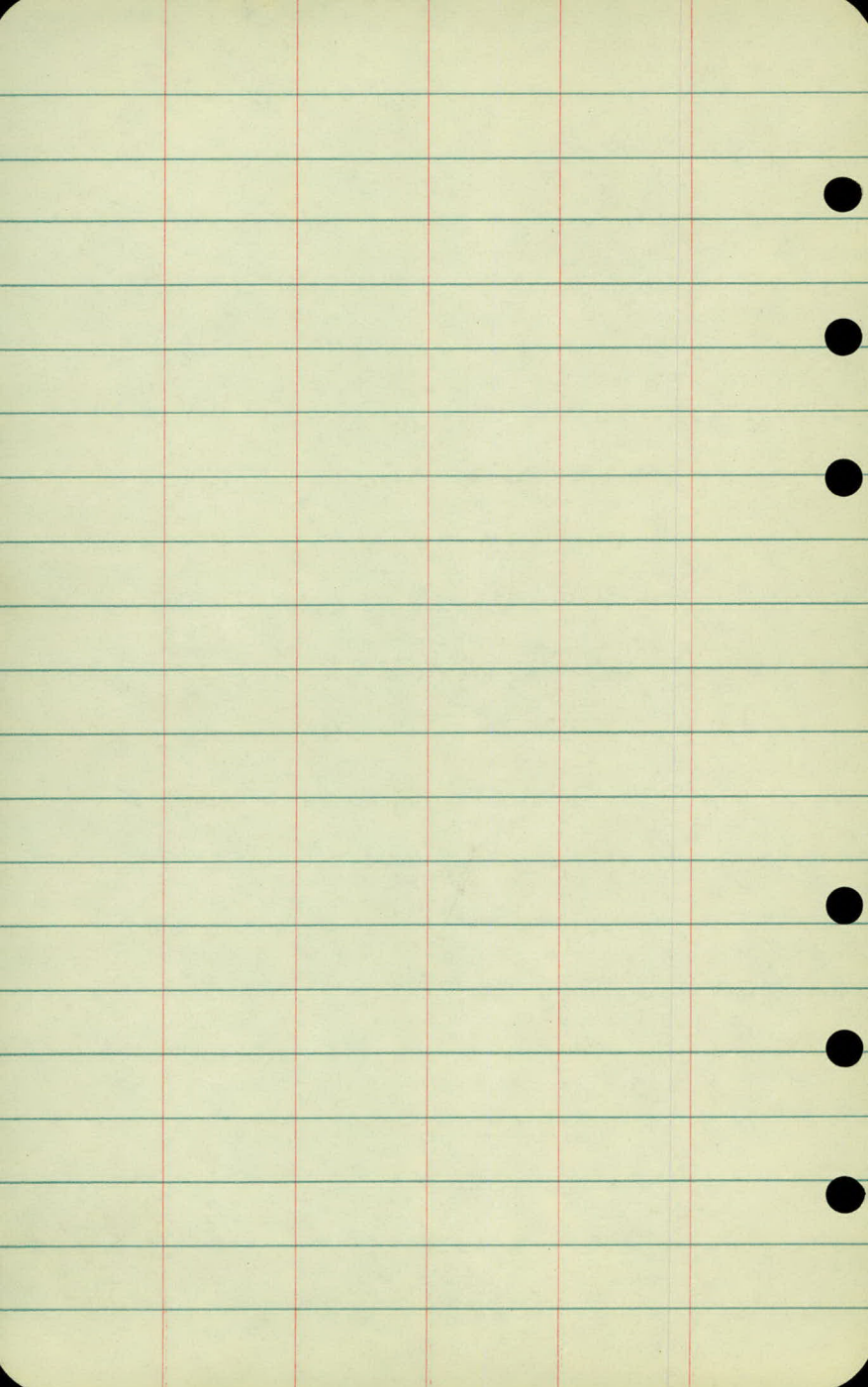
08.0	07.6	07.3	06.9	06.7
5.1	5.5	5.8	6.2	6.4
100	90	80	68	50

08.4	08.3	08.1	08.3	08.37	07.8	07.5	07.7	06.9	06.8
4.7	4.8	5.0	4.8	4.70	5.3	5.6	5.4	6.2	6.3
50	43	36	22		24	34	35	47	50

07.5	07.3	06.9	06.8
5.6	5.8	6.2	6.3
100	92	78	65

08.4	08.2	08.3	08.4	08.46	07.8	07.6	07.8	07.3
4.7	4.9	4.8	4.7	4.61	5.3	5.5	5.3	5.8
50	43	34	22		26	35	36	44

07.8	07.3	07.2	07.0	07.0
5.3	5.8	5.9	6.1	6.1
100	85	74	62	50



FK
RG
CW
RJ

Jan 27, 1958
Snowing 24°

i

Sta + π - Elev.

BM 0.60 91346 (912.86)

32

+28

+50

33

+50

34

Jan 27, 1958

J

Lt

£

1255

S.W. Cor Conc. Ent Slab 1550 W. Larpentour

08.1	09.5	11.4	13.4	13.5
5.4	4.0	2.1	0.1	0.0
100	86	73	65	60

✓

02.5	02.7	04.0	04.2	05.80
11.0	10.8	9.5	9.3	7.66
100	98	83	75	74

Fe

F.L. 30' SCP

02.7	03.0	05.1
10.8	10.5	8.4
82.5	75.5	71

Fe

03.3	03.5	05.3
10.2	10.0	8.2
77.7	81	77.7

Fe

03.0	03.3	05.4
10.5	10.2	8.1
75	69	64

Fe

02.8	03.2	05.4
10.7	10.3	8.1
71	64.5	61

Fe

75

71

Sta + K - Elev.

913.46

34+50

+87

35

2.58 10.88

BM 0.31 905.85 7.92 905.54

32+50

82.5

33

98

FX
RG
CW
PR

Lt

Jan 27 1958
Jan 28, 1958
Snowing 23°

k

03.1	03.4	05.2
10.4	10.1	8.3
67	61	57



02.1	02.3	02.2	02.9	05.2
11.4	11.2	11.3	10.6	8.3
100	86	72	63	57

683
38
630

07.1	08.5	08.6	10.0
6.4	5.0	4.9	3.5
70	60	54.5	58.5

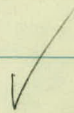


S. End 3' Horizontal Brace S.E. Cor 6' Cyclone Fe

00.5	00.6	01.3	02.1	02.8
5.4	5.3	4.6	3.8	3.1
133	127	112	85	82.5



78.2	99.1	00.4	02.0	02.5
7.7	6.8	5.5	3.9	3.4
123	112	102	83	78



97.8	94.1
8.1	11.8
145	150

Sta + A - Elev

905.85

33+25 ✓

77
41

✓

33+50

13.8
56
194

75
62

✓

13.7
2.4

33+75

73

Jan 28, 1958

l

2+

90.0	91.5	95.5	91.8	92.5
15.9	14.4	10.4	4.1	3.4
118	103	94	83	77

88.4

17.5

147

86.5

90.0

92.4

95.8

90.8

92.6

19.4	15.9	13.5	10.1	5.1	3.3
137	118	98	88	81	75

86.4

20.5

151

88.8

90.9

95.9

90.9

92.3

17.1	15.0	10.0	5.0	3.6
104	84	90	78	73

Sta + H.I. - Elev
905.85

33+75

73

34+00

71

✓

+50

67

✓

+66

5.59
4.48
10.07

Jan 28, 1958

m

Lt

E

Rt

96.2	96.2	92.9	88.5
9.7	9.7	13.0	17.4
148	133	129	118

96.8	95.9	96.9	01.3	02.6
9.1	10.0	9.0	4.6	3.3
104	94	82	76	71

✓

98.8	96.8	96.7	97.6	98.9
7.1	9.1	9.2	8.3	7.0
114	121	140	151	171

96.4	97.0	99.3	99.1	01.6	02.6
9.5	8.9	6.6	6.8	4.3	3.3
107	93	85	77	73	67

✓

96.8	97.9	98.9	01.1	01.9
9.1	8.0	7.0	4.8	4.0
117	123	133	142	147

97.4	95.78	97.1	01.4	02.8
8.5	10.07	8.8	4.5	3.1
87	80	80	72	66

(FL Apron)

Sta + X - Elev

905.85

34+66

66

BM 9.01 914.55 0.31 905.54

TP 0.13 903.83 10.85 903.70

29+50

30

+50

31

?

✓

TP 13.36 915.74 1.45 902.38

BM

2.84

912.90

912.86

Jan 28, 1958
~~2~~

m

Lt.

01.5	29.9	99.1
4.4	6.0	6.8
116	108	97

91.3	92.0	92.8	94.0	95.1	98.4
12.5	11.8	11.0	9.8	8.7	5.4
150	137	121	111	105	100

✓

90.6	90.7	91.1	91.7	93.0	96.7
13.2	13.1	12.7	12.1	10.8	7.1
150	128	113	109	105	100

89.8	91.0	91.5	92.1	93.5	96.1
14.0	12.8	12.3	11.7	10.3	7.7
150	131	118	108	105	100

92.7	94.7	96.2	97.1	98.9	102.4
11.1	9.1	7.6	6.7	4.9	1.4
130	117	106	100	92	86

90.7	89.7
13.1	14.1
150	165

S.W. Cor. Conc Ent Stoop 1255 W Carpenter

Sta

+

π

-

26

FX
RC
CW
RJ

Jan. 30, 1958
Clear 170

0

All Test Holes Approx. 3' BT of $\frac{1}{2}$

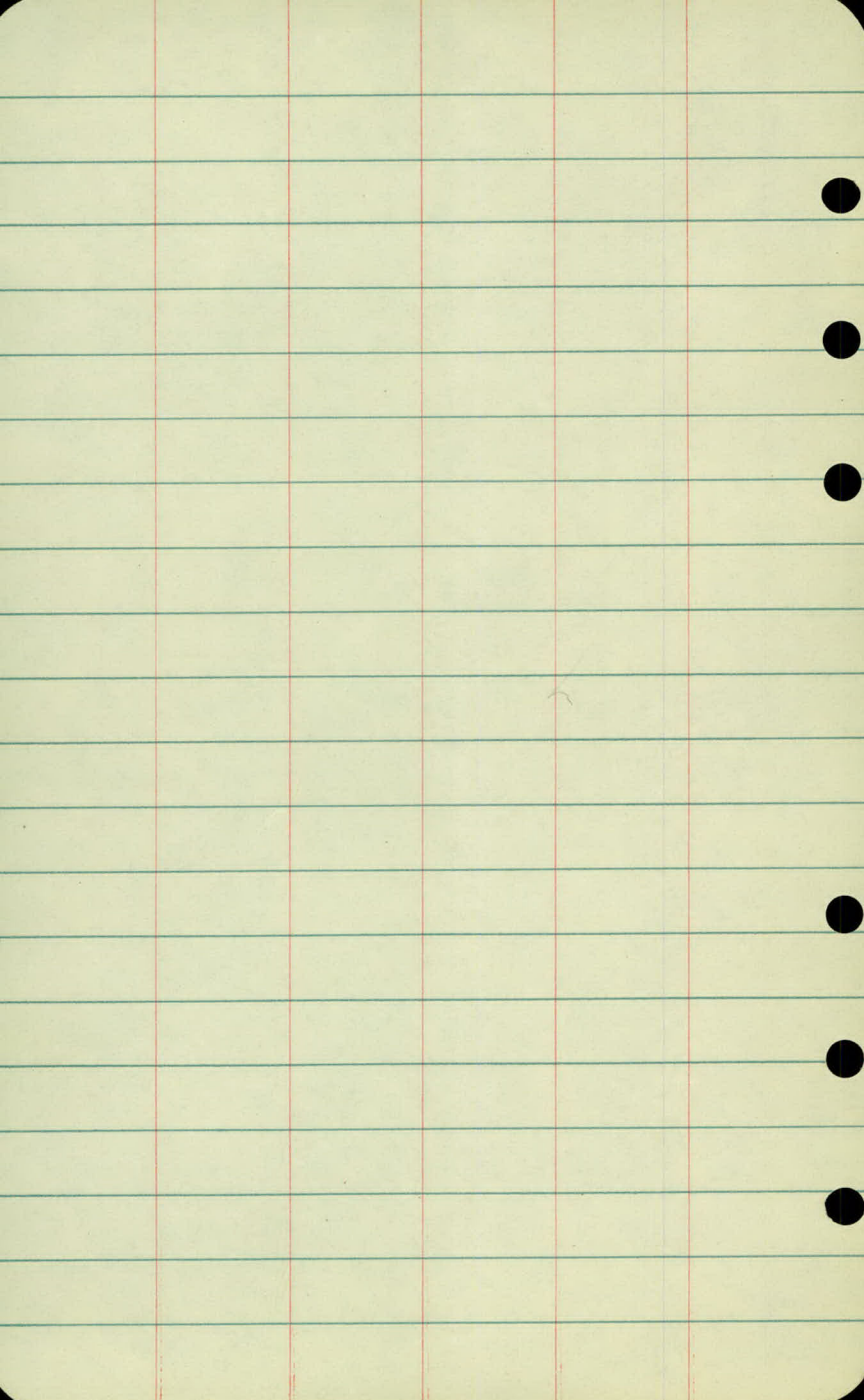
Sta 30+02 BT $2\frac{1}{2}$ " Thick

Sta 32+50 BT 3" Thick

Sta 35+00 BT 3" Thick

Sta 37+30 BT 5" Thick

Sta 39+00 BT $3\frac{1}{2}$ " Thick



Larpenfeu Mile 3

Sta	+	π	-	Elev
-----	---	-------	---	------

0+53	± 2'	Asph Patch	25.5' Rt	
------	------	------------	----------	--

1+00	Cor 2'	Asph Patch	25.5' Rt	
------	--------	------------	----------	--

1+00	± 2'	Asph Patch	±	
------	------	------------	---	--

1+00	End 2' Patch	31.5' Lt		
------	--------------	----------	--	--

BM	0.69	958.74		958.05
----	------	--------	--	--------

2+54		5.81	52.93	
	Inv. 12.5' deep		<u>-12.5</u>	
			40.43	

3+06		5.45		
------	--	------	--	--

	M.H. 10.15' deep		41.22	Inv.
4+90		7.37	51.37	

4+94		6.37		
------	--	------	--	--

BM		4.25	954.47	954.47
----	--	------	--------	--------

FX
HP
CW

Jan 10, 1957

6

End Patch Burned

Top Hyd snelling & Larpenteur

Top MH 28' Lt

MH 40' Lt

MH 27' Lt

MH 41' Lt

BM Top Hyd From a

Sta	+	π	-	Elev
-----	---	-------	---	------

BM	3.48	952.35		948.87
----	------	--------	--	--------

19+15

19+00

0+50

Albert st. No.

1+00

" " "

0+50

Albert st. So.

1+00

" " "

FX
KP
CW
LC

Lt.

Jan 13, 1958
Fog 29°

Rt.

C

N.E. Cor Albert & Lamp Ave

47.57	47.45	47.1	47.0	46.9	47.2	47.4	47.5	47.3	47.2	46.7	45.4	46.2	46.4	47.4
4.78	4.90	5.3	5.4	5.5	5.2	5.0	4.9	5.1	5.2	6.7	7.0	6.2	6.0	5.0
90	60	49	36	26	19	10		10	21	26	30	40	47	55
conc.														
(4.30 70 island)									4.3-4.05 Ho.		4.5 70		4.6 60	
											47.9		47.8	

47.59

4.76 chh.

46.7	46.4	46.1	45.8	46.1	46.2	46.0	45.8	46.1	45.9	46.0
5.7	6.0	6.3	6.6	6.3	6.2	6.4	6.6	6.3	6.5	6.4
45	29	16	15	8		11	16	17	28	45

46.8	46.21	46.01	45.2	45.7	45.4	45.1	45.4	45.6	46.2	46.6
5.6	6.14	6.34	7.2	6.7	7.0	7.3	7.0	6.8	6.2	5.8
46	31	25	17		11	16	20	30	34	41-Ho
conc.		conc.								

45.7	45.8	45.9	45.8	46.2	46.3	46.1	45.6	46.0	46.1	46.2	46.3
6.7	6.6	6.5	6.6	6.2	6.1	6.3	6.8	6.4	6.3	6.2	6.1
50	31	18	15	12		13	15	19	31	42	50

46.6	46.0	45.6	45.8	45.9	45.6	45.9	46.7	47.2
5.8	6.4	6.8	6.6	6.5	6.8	6.5	5.7	5.2
33	17	16	11		16	17	29	37

Sta	+	π	-	Elev
B. M.	1.94	954.53		952.59

0+50		Halton Ave		
------	--	------------	--	--

1+00		"	"	
------	--	---	---	--

17+00				
-------	--	--	--	--

1-13-58

D

Lt.

£

Rt.

Top Hyd N.W. Cor. Holton + Larp Ave

49.9	49.8	49.5	49.6	48.7	49.4	49.5	49.5	49.1	48.5	48.3	48.4	47.4
4.6	4.7	5.0	5.5	5.8	5.1	5.0	5.0	5.4	6.0	6.2	6.1	5.1
47	34	27	24	20	18		10	14	16	18	21	28
										49.2	49.2	✓
										5.3	5.3	
										5.0	4.2	
50.8	50.4	49.5	49.4	49.1	49.3	49.4	48.7	48.3	48.6	49.4	48.5	49.5
3.7	4.1	5.0	5.1	5.4	5.2	5.1	5.8	6.2	5.9	5.1	5.0	5.0
50	42	32	23	20	19		14	19	24	30	42	50

49.51

502 ctk.

Sta	+	Δ	-	Elev
B. M.	1.18	954.99		953.81

14 + 10

B. M.	1.41	955.22		953.81
-------	------	--------	--	--------

0 + 50 Pascal Ave No.

1 + 00 " " "

0 + 50 Pascal Ave So.

1 + 00 " " "

13 + 00

Lt.

£

1-13-58

E

RT

Top Hyd. N.W. Cor. Pascal + Larp Ave

50.4	50.84	50.9	51.0	51.1	51.0
4.6	4.5	4.1	4.0	3.9	4.0
50	60	73	88	101	110
			51.3	51.3	
			3.7	3.7	
			146	131	

Top Hyd N.W. Cor Pascal + Larp.

50.8	50.7	50.8	50.4	50.4	50.9	50.5	50.9	50.7	50.6
4.4	4.5	4.4	4.8	4.8	4.3	4.7	4.3	4.5	4.6
50	35	23	18	13		17	20	33	50

51.3	51.1	51.1	50.7	51.1	50.9	51.1	51.2	51.6
3.9	4.1	4.1	4.5	4.1	4.3	4.1	4.0	3.6
33	24	16	14		15	17	32	46

50.5	50.6	50.9	50.9	50.7	50.8	50.4	50.6	50.8	50.9	50.0	49.4
4.7	4.6	4.3	4.3	4.5	4.4	4.8	4.6	4.4	4.3	5.2	5.8
50	37	28	19	14		11	15	16	24	36	50

51.5	51.3	50.9	51.1	51.2	50.9	50.8	51.0	51.0	50.2	49.7	49.4
3.7	3.9	4.3	4.1	4.0	4.3	4.4	4.2	4.2	5.0	5.5	5.8
31	17	14	8		11	12	16	28	35	46	50

Ho.

4.35chk.

Sta	+	π	-	Elev
-----	---	-------	---	------

B M	2.72	956.53		953.81
-----	------	--------	--	--------

9+50

10+00

9+93

B.M.			2.04	954.49	954.49
------	--	--	------	--------	--------

1-13-58

F

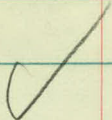
LT

E

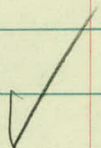
RI

Top Hyd. N.W. Cor Pascal + Larp.

52.1	52.1	51.7	51.3
4.4	4.4	4.8	5.2
81	76	64	50
Ho.			



52.2 ²⁴	52.1	51.7	51.4
43.1	4.4	4.8	5.1
86.5	80	64	50
conc. walk			



51.80
4.73
70
conc. walk

Top Hyd. N.E. Cor. Aroma + Larp.

Sta	+	π	-	Elev
BM	3.32	950.06		(946.74)

23+24	^{Top} MHLT	5.34	44.72
-------	---------------------	------	-------

23+13	^{Top} MHLT	5.11	44.95
-------	---------------------	------	-------

21+00	±	4.09	✓ 46.0 946.0
-------	---	------	--------------

BM	2.28	956.09		(953.81)
----	------	--------	--	----------

10+45	MHL RT	4.44	951.65
-------	--------	------	--------

10	±	4.84	✓ 51.25 51.2
----	---	------	--------------

26+38	M.H. 45.3'
-------	------------

16+59	M.H. 40.5' RT
-------	---------------

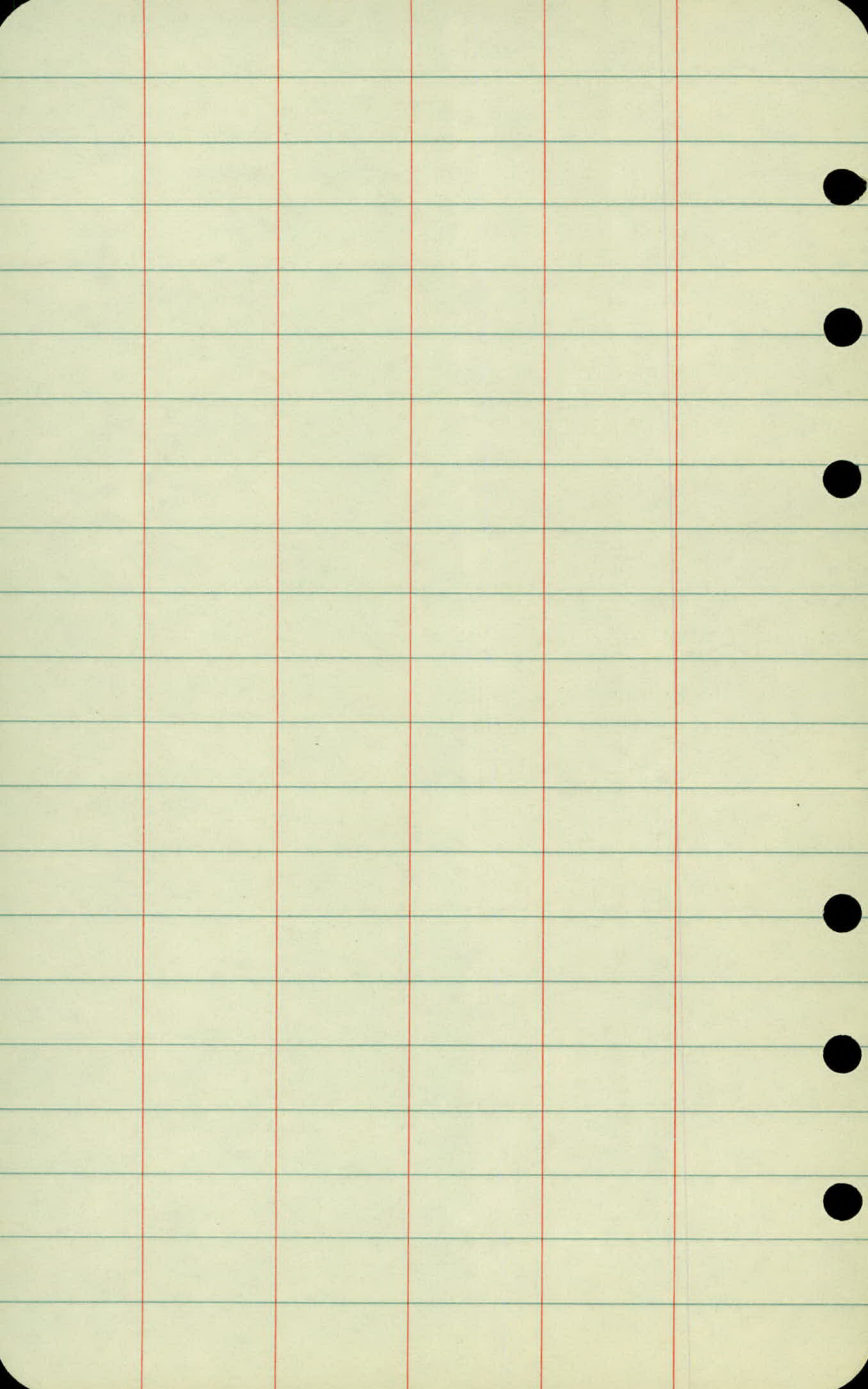
Elev Pond 3-10-58	(893.36)
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FR
RG
KP
CW
AB
RJ

March 10, 1958
Fair 25°

Top Hyd SW Cor Hamline & Larp

Top Hyd NW Cor Pascal & Larpenteur



Manholes & Catch Basins
Larp Ave

Sta 37+61 Lt. + RT.

Sta 37+69 Lt. + Rt.

Sta	+	x	-	Elev
BM	2.35	915.21		912.86
MH				
37+61			9.06	906.15

CB				
37+69			8.57	Lt
			8.52	Rt
	FL	9.14	Lt	street Elev
	FL	9.10	Rt	" "
	FL	11.18		invert Lt
	FL	10.86		invert Rt

Top Step 1255 Larp

MH 35' LT

MH 34' RT

Top Elev 906.15

906.15

Top of Grate to
Flow Line Lt.
6.4'

Top Grate to
FLine RT
5.4'

Top of Grate to
F.L. Connecting 12"
SCP to Lt. CB = 2.65'

Top of Grate to FL
Connecting 12" SCP to
RT C.B. = 2.28'

CB 36' LT

CB 35' RT

Top of CB 906.64 ✓

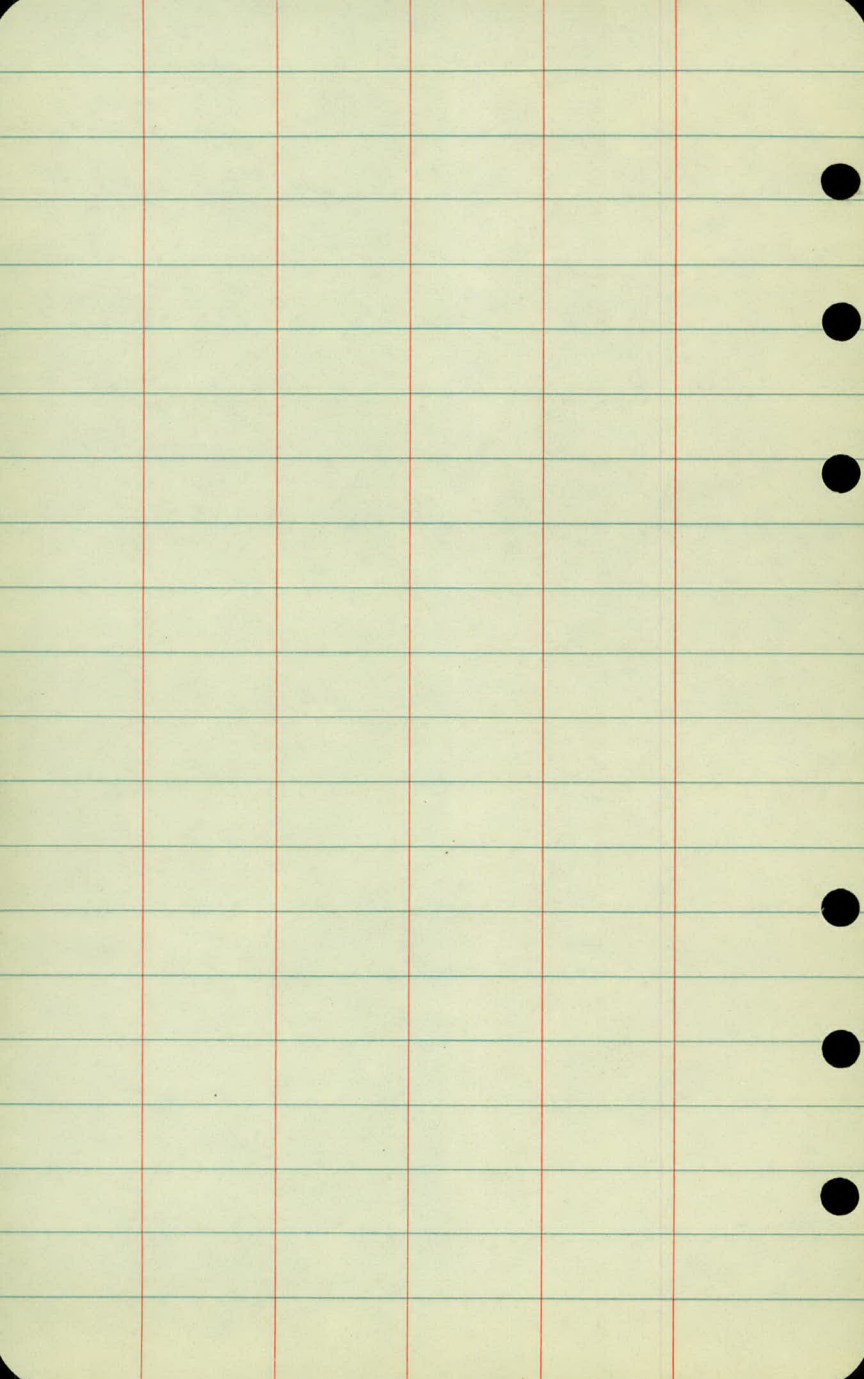
Top of CB 906.69 ✓

Flow line 906.07 street

906.11 FL street

904.03 invert Elev Lt

904.35 " " RT



FX
KP
CW

W
T
P

Dec 26, 1957

d

Larpenteur

Mile 3

Side Walk Elev.

2 pages

Sta + π - Elev

BM 1.86 956.35 954.49

6+32

7+01

7+13 Lowest Point to Be Effected

7+00 $\pm$ 4.93 951.42

Pannels of Walk Rt From Arena

in 6 Pannels 3-3-2

4 Dec 26, 1957

6

Lt

Rt

Tap Hyd NE Cor Larpenteur & Arona

52.25

51.98

4.10

4.37

71.5

120

Cor Walk

50.04

50.73

51.35

6.31
150

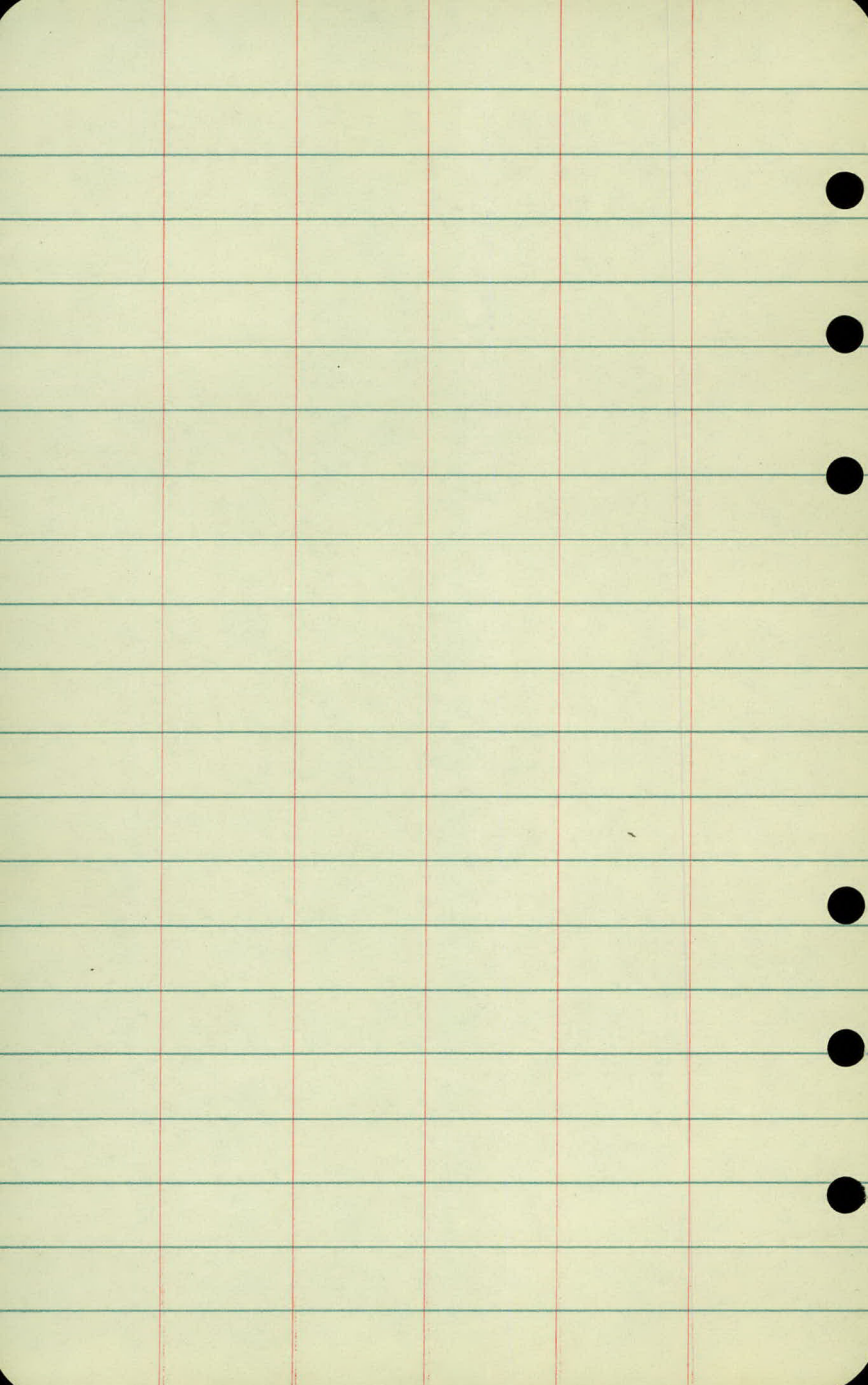
5.62
100

5.0
50

51.18

5.17

3.5
Walk at Cor Garage



Jan 24, 1958

9

Drainage Area Fence Location

37

36

+435 $\frac{R. Tie}{Fe}$

35

+85.10 $\frac{Fe. Cor.}{64.57}$

+84.7 $\frac{Fe. Cor.}{94.6}$

34

33

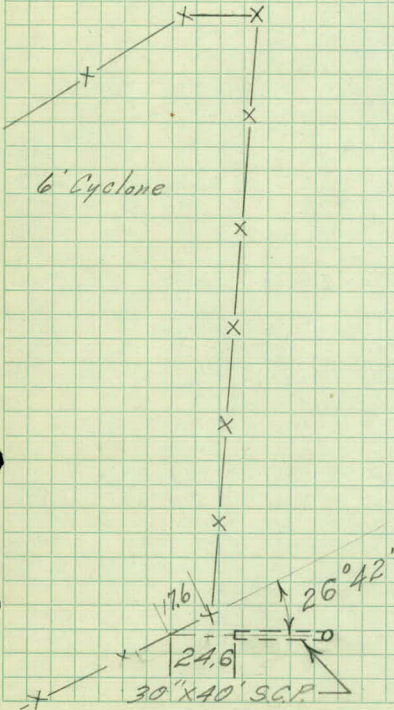
+36.9 $\frac{Fe. Cor.}{83.49}$

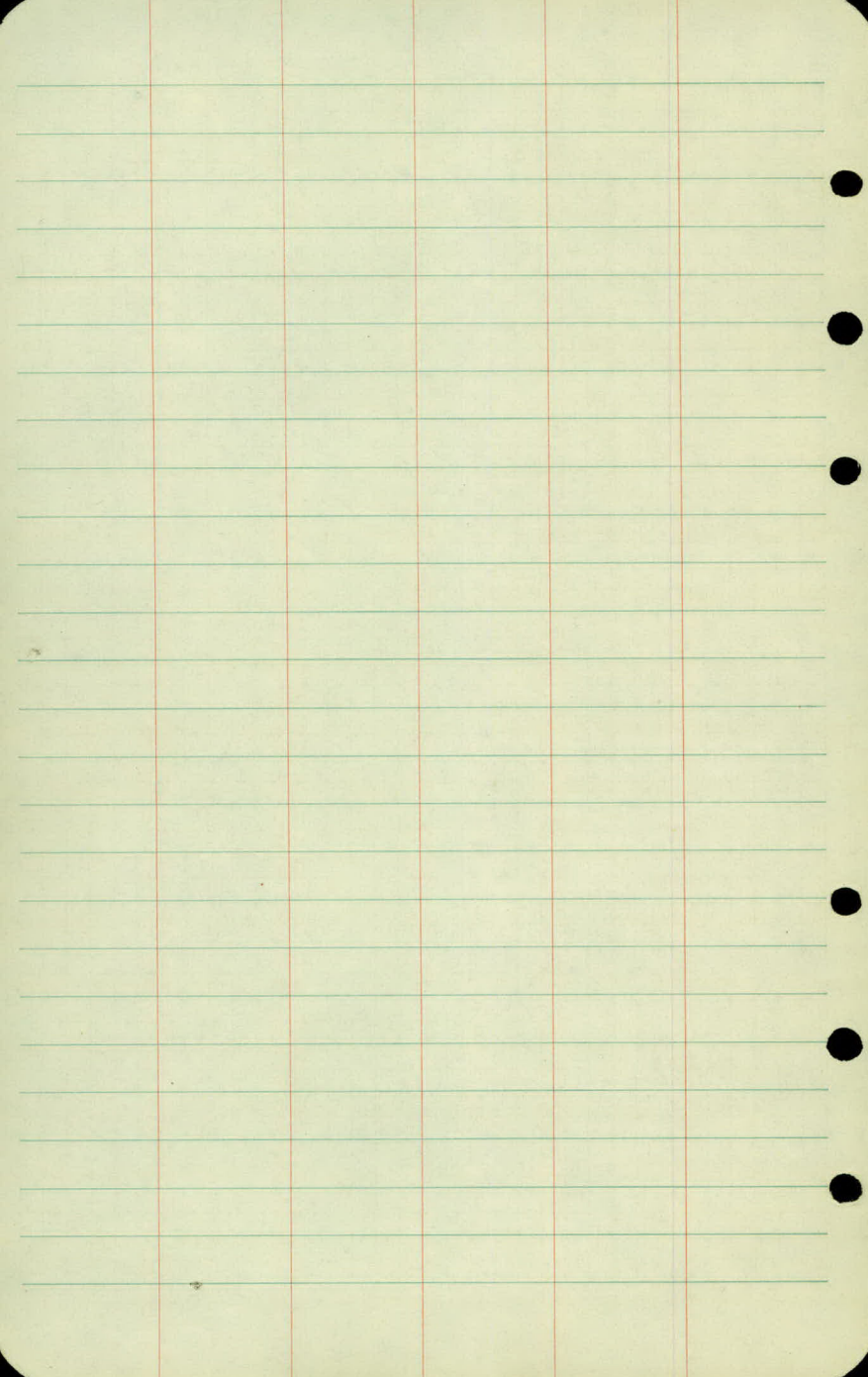
+28.8 $\frac{End 30" Rpe}{74}$

32 +100.4 $\frac{Fe Post}{155.3}$ P.I. 10' Beyond

Jan 24, 1958

1





FK
RG
CW.

Nov. 14, 1957

18

LARPEUR Mile 3

Profile Elevations

Pascal to Hamline

Sta	+	π	-	Elev
BM	1.77	955.58		(953.81)

13			4.78	50.8
----	--	--	------	------

+71			4.8	50.8
-----	--	--	-----	------

14			4.82	50.76
----	--	--	------	-------

+28			4.82	50.76
-----	--	--	------	-------

+43			5.12	50.46
-----	--	--	------	-------

+47			5.15	50.43
-----	--	--	------	-------

+84			3.59	51.99
-----	--	--	------	-------

15			4.90	50.68
----	--	--	------	-------

+27			3.71	51.87
-----	--	--	------	-------

Nov. 14, 1957

19

Top Hyd NW Cor Pascal & Laipenteur

±

Walk 53' Rt

±

Walk 50' Rt

Drive Ribbon 46' Lt

Drive Ribbon 46' Lt

Walk 50' Rt

±

Walk 50' Rt

Sta + π - Elev

955.58

15 + 51 4.70 50.88

+ 74 3.33 52.25

16 5.26 50.32

+ 97 4.48 51.10

17 6.12 49.46

BM 0.54 953.13 2.98 952.60 952.59

17 3.66 49.47

+ 44 2.66 50.47

+ 87 4.24 48.89

+ 80 2.90 50.23

FK
RG
CW

Nov 14, 1957
Nov 15, 1957

20

£ 8.7' Conc Ent 49' Lt

Walk 50' Rt

£

Walk 50' Rt Ho⁺ 1426

£

Top Hyd Holton & Larp

£

Walk 50' Rt

Walk 53' Lt Ho Red 40

Walk 51' Rt

Holton

Sta + π - Elev

953.13

18 4.73 48.40

+40 4.02 49.11

+50 6.37 46.76

+89 5.35 47.78

19 5.65 47.48

+06 5.80 47.33

+27 5.78 47.35

20 6.22 46.91

BM 2.19 951.06 4.24 948.89 (948.87)

+⁶²~~82~~ 4.92 46.14

21 4.52 46.54

Nov 15, 1957

21

£

Walk 49' Rt

Service station Ent 50' Lt

Walk 50' Rt

£

SW. Cor

Conc Ent of Service station 59' Lt

SE Cor Conc Ent

£

Top Hyd NE. Cor Albert & Lorp

Walk 52' Lt

£

Plotted

Sta + π - Elev

951.06

21+06 4.69 46.37

+52 5.10 45.96

+70 4.50 46.56

22 4.73 46.33

+05 5.24 45.82

+18 4.54 46.52

+23 4.55 46.51

+53 5.14 45.92

23 4.97 46.09

+10 4.95 46.11

Nov 13, 1957

22

Walk 54' Rt

Walk 51' Rt

End Conc (77' Lt) Ent

Walk 50' Rt

Conc Ent Ribbon 48' Lt

Conc Ent Ribbon 48' Lt

Walk 50' Rt

±

Walk

Plotted

Sta + π - Elev
 951.06

23 + 50 4.93 46.13

+ 54 5.16 45.90

24 5.18 45.88

+ 04 4.92 46.14

+ 11 5.14 45.92

+ 61 5.96 45.10

+ 62 6.23 44.83 ✓

+ 67 6.31 44.75 ✓

25 5.50 45.56 ✓

25 6.15 44.91 ✓

Nov. 15, 1957

23

Conc Ent 50' Lt

Walk 51' Rt

±

Walk 53' Rt

Conc Ent 50' Lt (Asph over Tile)

Walk 50' Rt

Conc Ribbon 44' Lt

Conc Ribbon 44' Lt

±

55' Rt in Service Station Ent

Plotted:

Sta	+	π	-	Elev	
		951.06			
+58 25+50			4.91	46.15	✓
+96 +88			5.00	46.06	✓
26			5.80	45.26	✓
BM			4.329	46.74	(46.74)

Nov 15, 1957

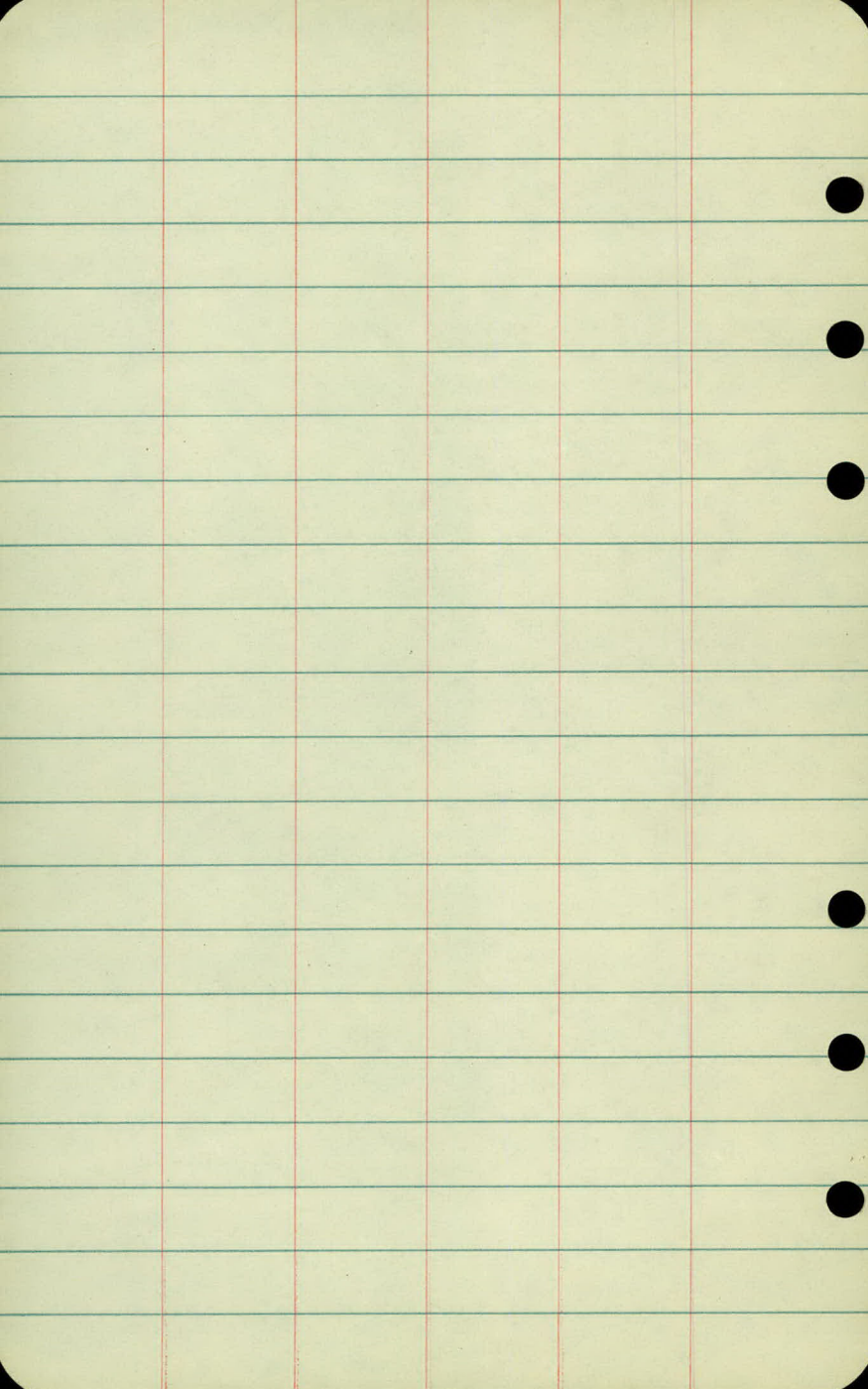
24

Pump Island 70' Rt

Pump Island 70' Rt

£

Top Hyd SW. Cor Hamline & LaPointe



X-Sections

Hamline S. of Larp.

Hamline ~~£~~ Larp = 0 + 00

Sta	+	π	-	Elev
BM	2.99	949.73		946.74

0+98

1+11

✓

+13

✓

RG
KP
AL

Lt

£

Rt

1

March 18, 1958

Top Hyd SW cor Hamline & Larp

3.9	4.10	4.9	4.7	4.60
46	30	20	8	
	SW			

45.90	45.84			
3.83	3.89	4.7	4.8	4.57
36	30	22	13	
SW	SW			

3.7	3.3
50	68

4.0	4.5	4.8	4.57
26	22	13	

45.83	45.92	
3.88	3.81	3.4
30	36	43
SW	SW	

Sta	+	π	-	Elev
-----	---	-------	---	------

		949.73		
--	--	--------	--	--

1+13				
------	--	--	--	--

1+30				
------	--	--	--	--

BM				
----	--	--	--	--

	4.87	944.86	944.98	
--	------	--------	--------	--

Lt.

E

March 18, 1958

RT

2

3.2	3.1
59	68

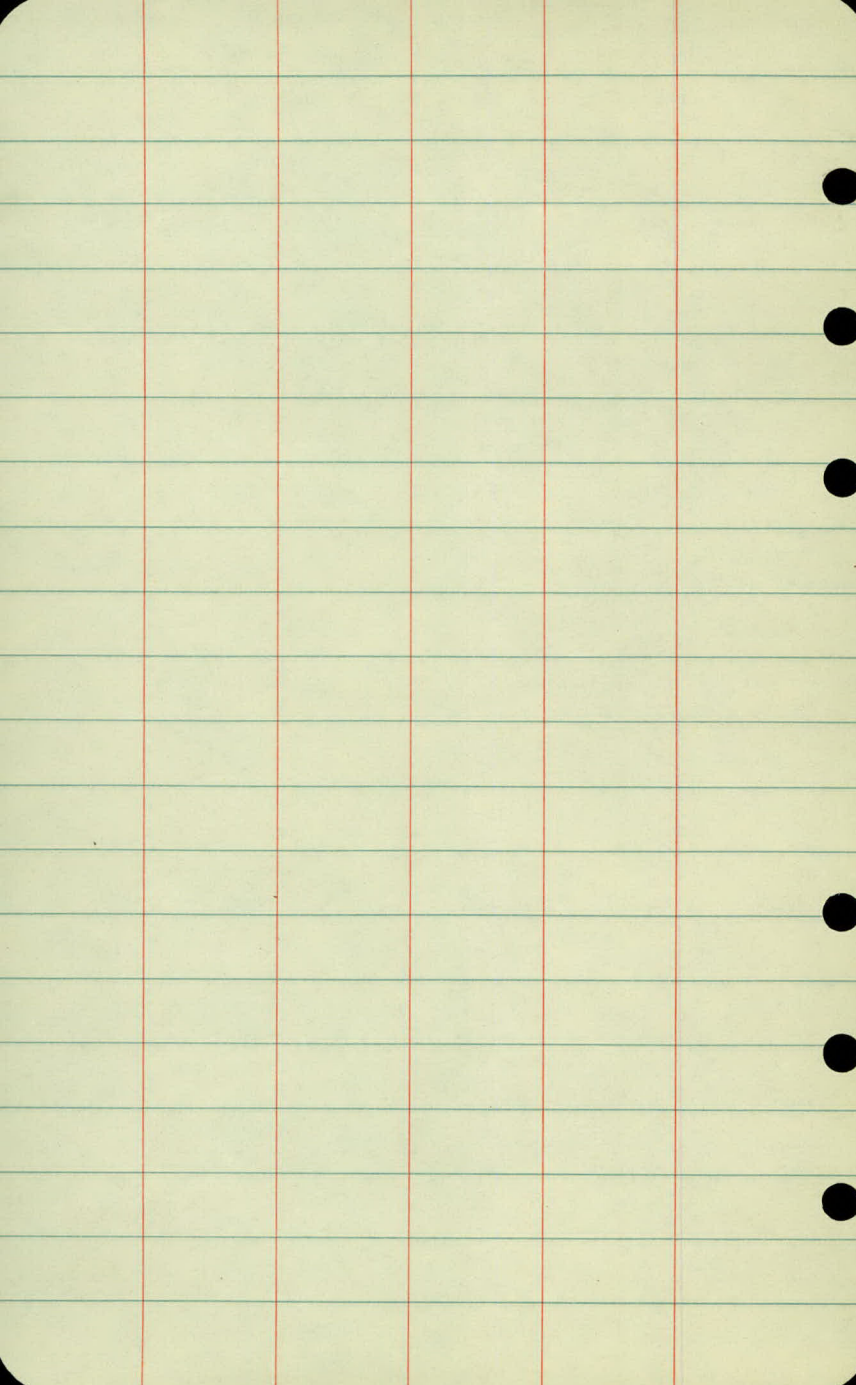
45.95

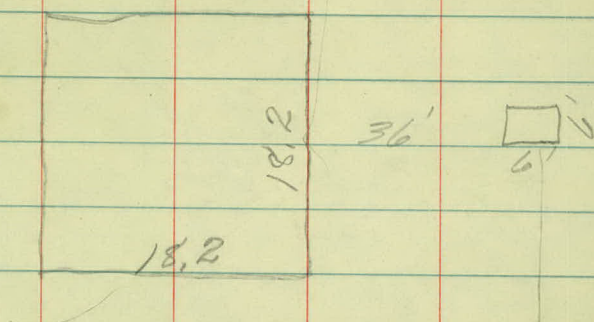
3.78	3.9	4.3	4.7	4.56
30	26	22	16	
SW				

46.13

3.60	3.11
36	56
SW	SW @
	Bldg

Monument Hamline & Larp



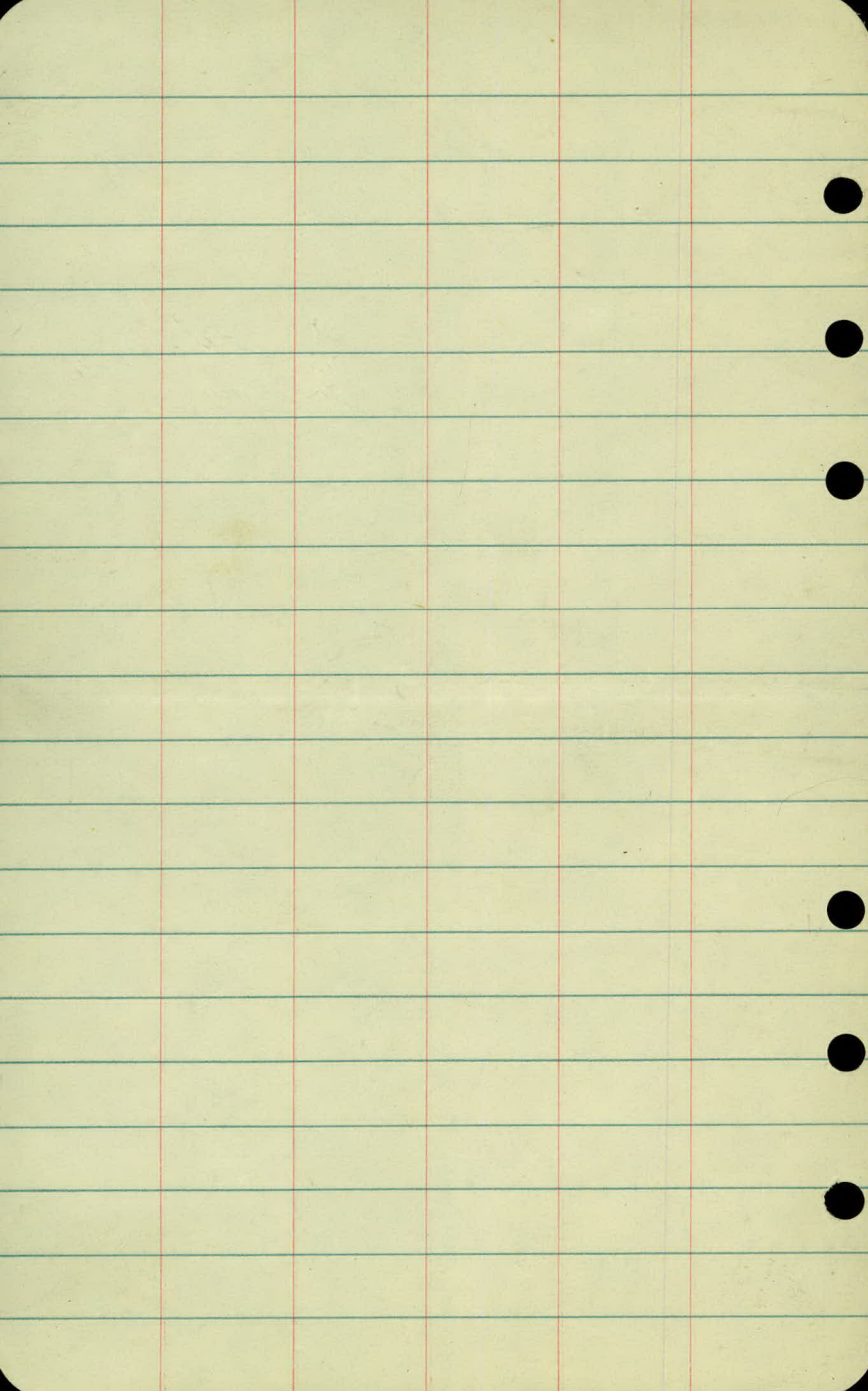


N
↑

18'

85'

House



Area

Hand-drawn map of a service station area on graph paper. The station is a rectangle with dimensions 52' by 43.7'. To the left is a car with dimensions 37.5' by 35.7'. To the right is a truck with dimensions 42.5' by 31.4'. A highway line runs vertically on the right side.

parking

N

106.5

74

Drive

* 720
6 Cyclone

691 P.P. Transformers

parking

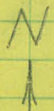
Pack King

Area

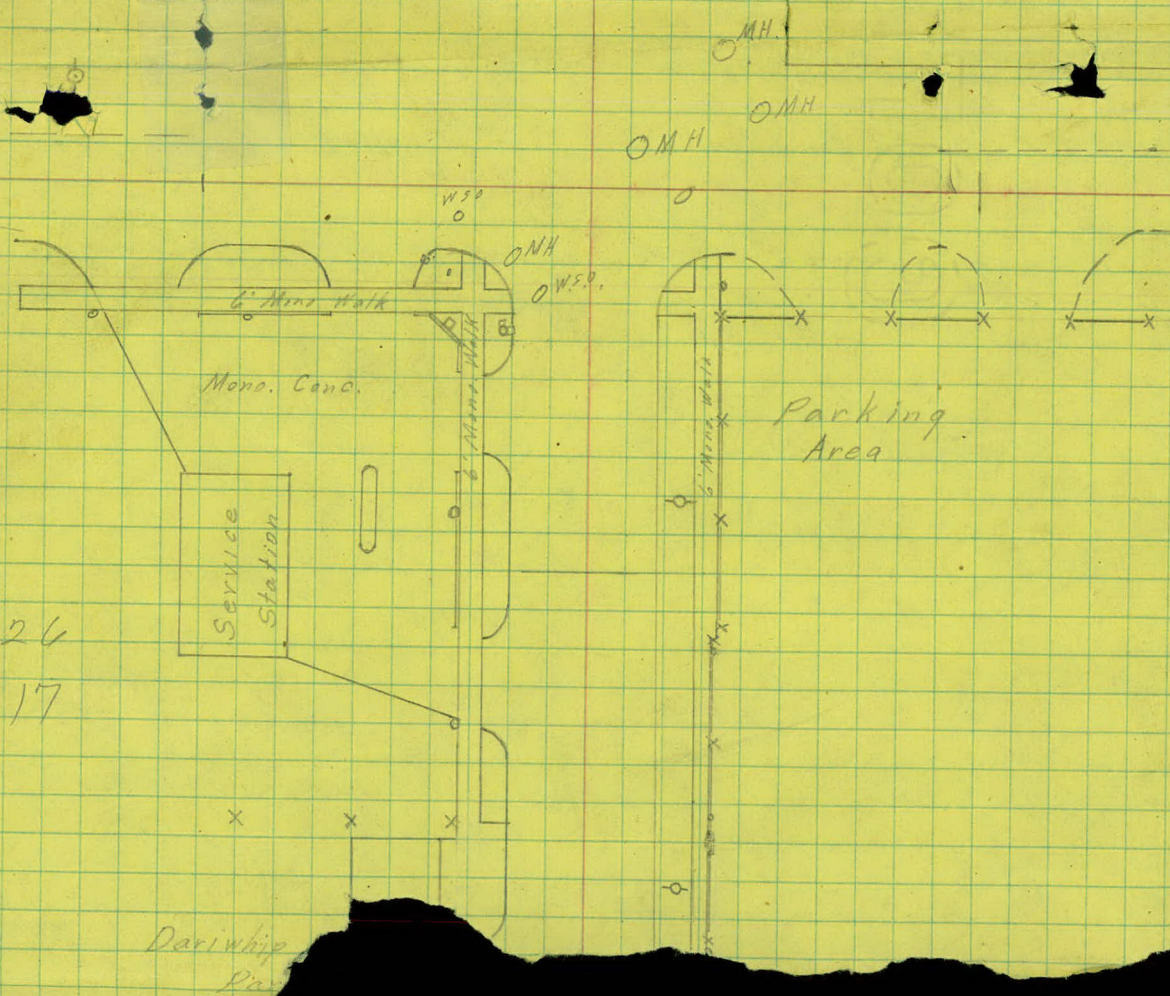
Math.

90'

14 06
 28 W
 28 NS



+34 MH 21
 +18 MH 28
 0405 MH 15



Y
 H.S.D. 26
 MH 17

Deriwhip
 Pa

FK
RG
KP
RJ
AB
PR

Feb 14, 1958

1

Larpenteur Mile 3

Sta	+	π	-	Elev
BM	1.99	914.85		912.86

37+71			10.08	04.77
-------	--	--	-------	-------

37+63			8.71	06.14
-------	--	--	------	-------

Snelling Ave Location
 from E. P. L. Snelling
 0+00 $\pm$ Larpenteur

	Service Lane	N. B Lane
1+00	10 + 35	60 + 94
2+00	15 + 36	65 + 98
4+00	10 + 37	75 + 107
6+45	10 + 40	95 + 128

Feb 14, 1958

2

SV. Car Conc Ent slab 1255W Luper fence

FL. 12'x10'CM. 52' Rt

Top great Ring Rt 34'

S. Bound Lane

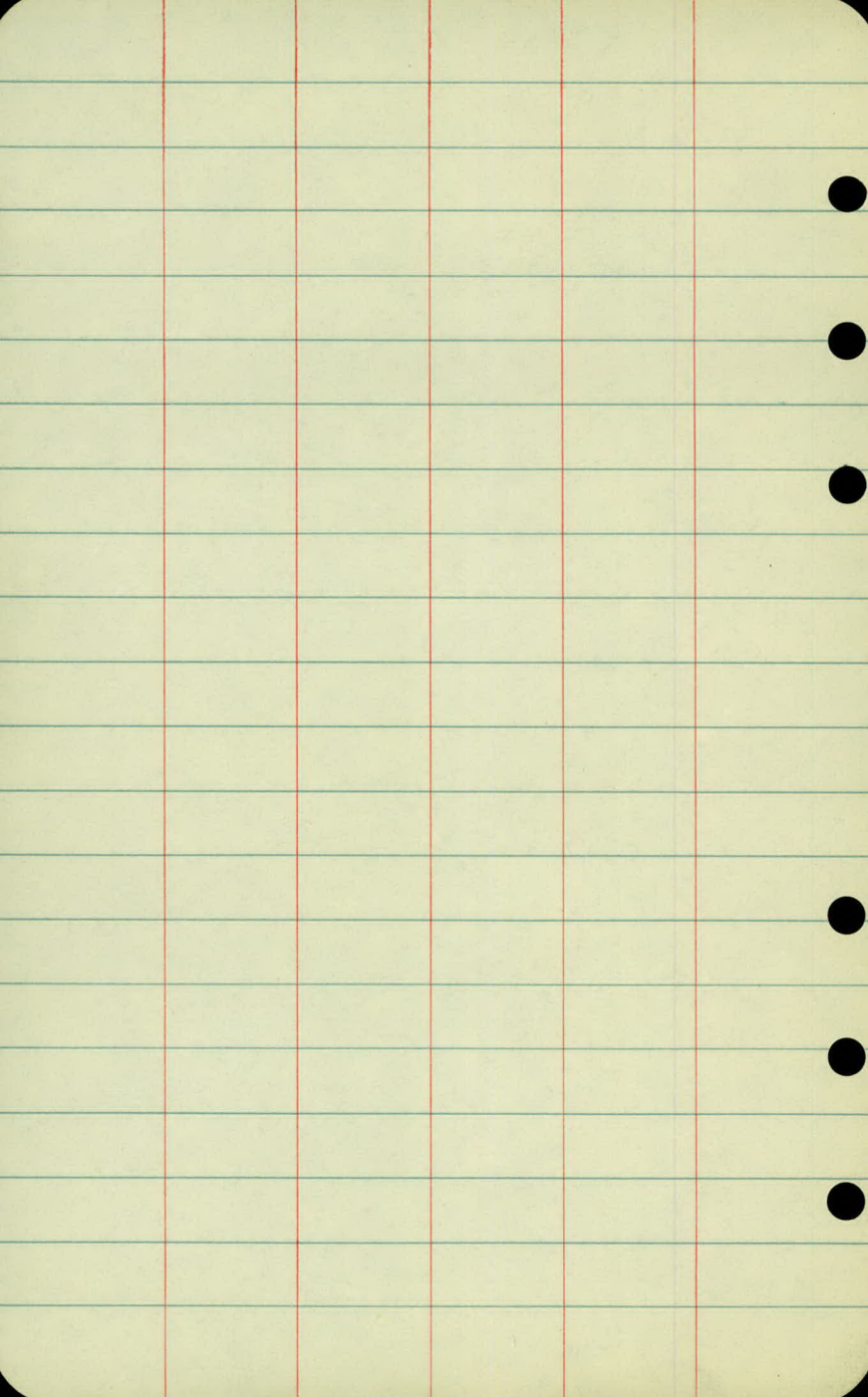
148.5 4/73'

148 + 173

146 + 173

151 + 175

N Carb Line of Idaho



Feb 14, 1958

3

Topography

5

$$\begin{array}{r}
 +99 \frac{26 \text{ M}}{38} \\
 \text{End Ent} \\
 +80 \frac{25}{25}
 \end{array}$$

$$\begin{array}{r}
 +87 \frac{BR}{22}
 \end{array}$$

4

3

2

$$\begin{array}{r}
 \text{BEAT} \\
 +95 \frac{22}{22}
 \end{array}$$

1

$$\begin{array}{r}
 \text{End Ent} \\
 +14 \frac{20}{20} \\
 \text{ERC} \\
 +56 \frac{23}{23}
 \end{array}$$

$$\begin{array}{r}
 \text{PP} \\
 +60 \frac{32}{32}
 \end{array}$$

$$\begin{array}{r}
 \text{Gas Vent} \\
 +48 \frac{34}{34}
 \end{array}$$

$$\begin{array}{r}
 \text{Curb} \\
 +39 \frac{34}{34} \rightarrow
 \end{array}$$

$$\begin{array}{r}
 \text{B. Ent} \\
 +56 \frac{23}{23}
 \end{array}$$

$$\begin{array}{r}
 \text{MH} \\
 +27 \frac{43}{43}
 \end{array}$$

0

+

$$\begin{array}{r}
 \text{Sig} \\
 +12 \frac{34}{34}
 \end{array}$$

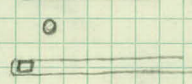
$$\begin{array}{r}
 \text{E. 1/64} \\
 +12 \frac{32}{32}
 \end{array}$$

29
33
42

4

4

RT



10

9

8

$$\begin{array}{r}
 +157 \frac{36^M}{40} \\
 +34 \frac{36^M}{39}
 \end{array}$$

7

$$+77 \frac{33^M}{39}$$

$$+56 \frac{30^M}{39}$$

6

$$+18 \frac{26^M}{40}$$

$$+98 \frac{30^M}{39}$$

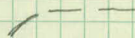
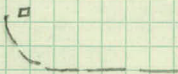
$$+64 \frac{51^M}{20}$$

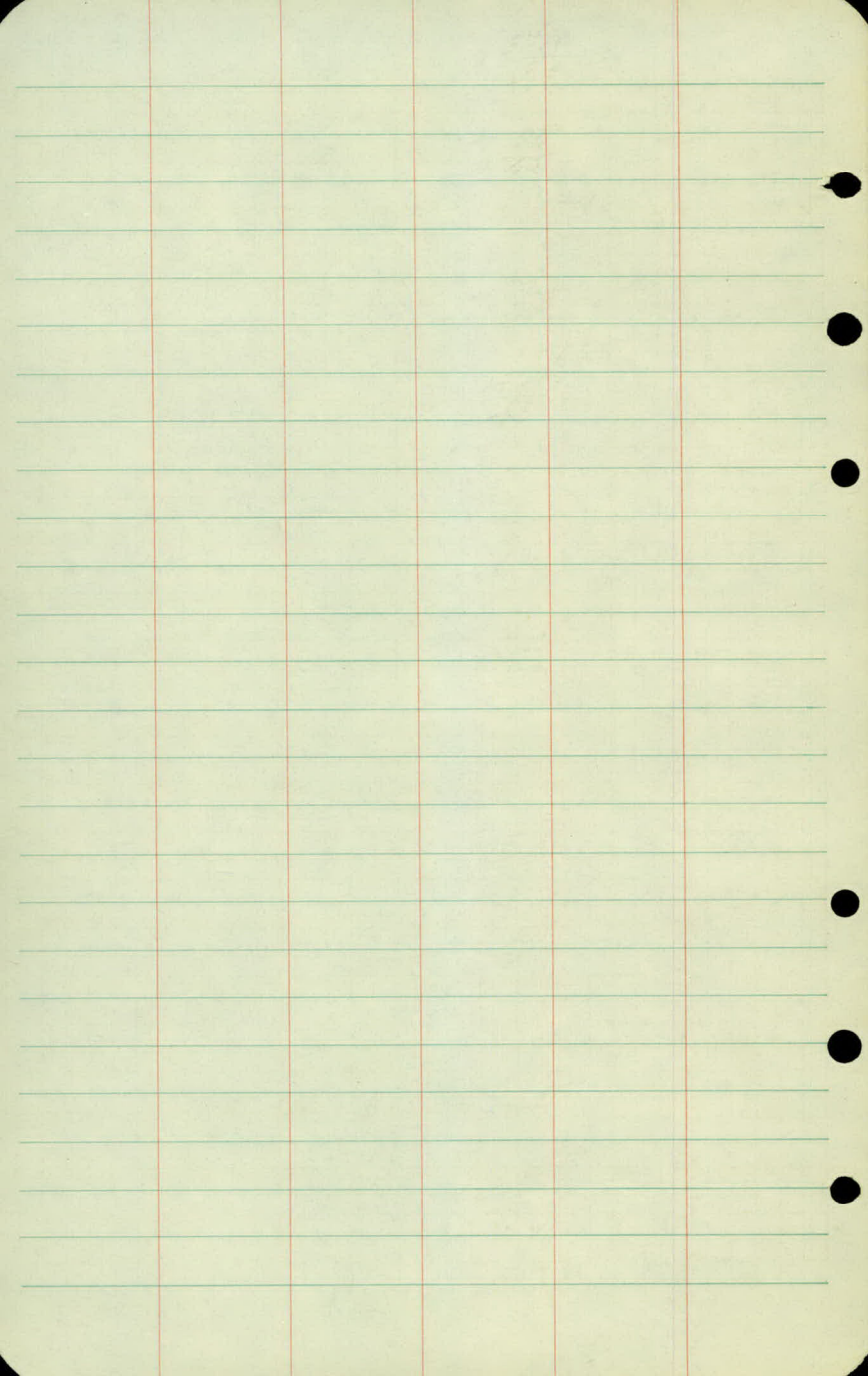
$$+58 \frac{ER}{20}$$

5

$$+16 \frac{ER}{45}$$

$$+40 \frac{ER}{39}$$





Mile 2
Profile

Sta + π - Elev

BM 3.27 988.32

985.05

0+00 = ~~4~~ Larp. 16' of Monument.

+50

1+00

+50

2+00

RG
RJ
AB

Feb 14, 1958

£

7

Top Hyd Larpenteur + Snelling

83.47

4.85

83.67

4.65

34

83.57

4.75

83.52

4.80

34

83.49

4.83

83.52

4.80 conc

34

83.43

4.89

83.92

4.4

34

83.28

5.04

83.37

4.95

34

Sta	+	π	-	Elev
-----	---	-------	---	------

		988.32		
--	--	--------	--	--

2+50				
------	--	--	--	--

3+00				
------	--	--	--	--

3+50				
------	--	--	--	--

4+00				
------	--	--	--	--

4+50				
------	--	--	--	--

RG
RJ
AB

Feb 14, 1958

£

Rt

8

83.09

83.42

5.23

4.9

34

82.95

83.12

5.37

5.2

34

82.88

83.22

5.44

5.1

34

82.90

83.12

5.42

5.2

34

82.74

82.72

5.58

5.6

34

Sta	+	π	-	Elev
		988.32		

5+00

T.P	2.59	986.67	4.24	984.08
-----	------	--------	------	--------

5+50

6+00

+50

7+00

RG
RJ
AB

Feb 14, 1958

L

RT

9

82.64

5.68

82.42

5.9

34

Base of Signal 29' RT Sta 5+50

82.60

4.07

83.07

3.6

34

82.45

4.22

82.57

4.1

34

82.20

4.47

82.47

4.2

34

82.18

4.49

81.57

5.1

34

Sta	+	T	-	Elev
-----	---	---	---	------

		986.67		
--	--	--------	--	--

7+50				
------	--	--	--	--

8+00				
------	--	--	--	--

BM		3.37		983.30
----	--	------	--	--------

8+50				
------	--	--	--	--

9+00				
------	--	--	--	--

9+50				
------	--	--	--	--

Feb 14, 1958

RG
RJ
AB

Lt

Lt

Rt

10

N. Edge of 4.00
Conc. Apron 34

82.11
4.56

81.47
5.2
34

82.27
4.40

81.37
5.3
34

Conc. at Base of Center Brick Partition Fire Dept
Bldg 77.5' S of Sta 7+50

82.45
4.22

82.60
4.07
34

82.67
4.00

81.77
4.9
34

82.96
3.71

82.07
4.6
34

Sta	+	Σ	-	Elev
-----	---	----------	---	------

		986.67		
--	--	--------	--	--

T.P	4.19	988.27	2.59	984.08
-----	------	--------	------	--------

B.M.			3.22	985.05
------	--	--	------	--------

				985.05
--	--	--	--	--------

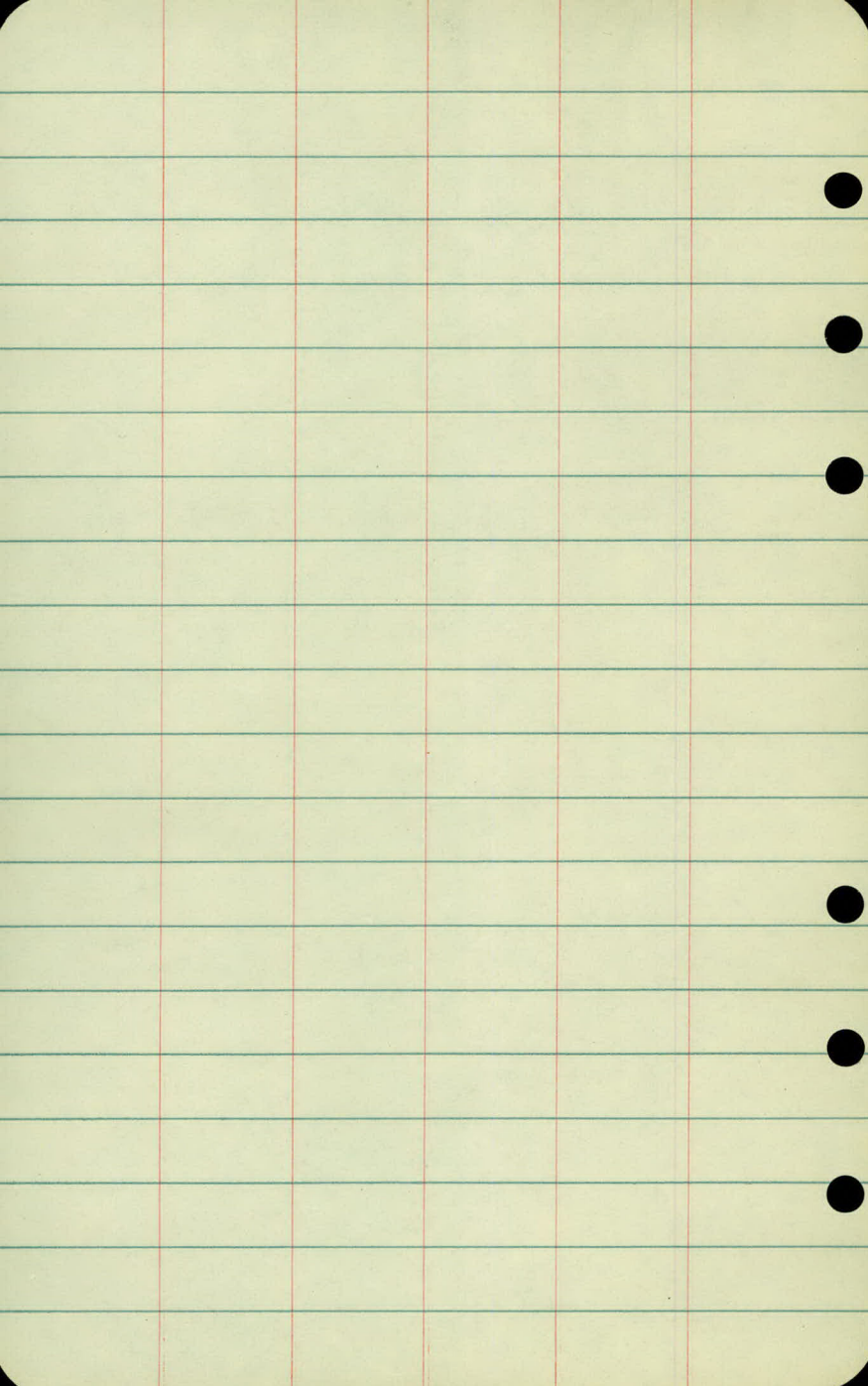
RG
RJ
AB

Feb 14, 1958

11

Signal Base 29' N. Sta 7+50

Top Hyd Snelling & Larp.



Feb 19, 1958

a

Larpentour & Snelling
Signal Locations

platted
2/19/58

1

$$+13 \frac{519}{32}$$

$$+51 \frac{519}{29}$$

$$+44 \frac{519 \text{ Box}}{38} +44 \frac{PP}{32}$$

0 +00

$$+33 \frac{519}{30}$$

$$-15 \frac{\text{End Island (4')}}{66}$$

$$-12 \frac{519}{34}$$

$$-39 \frac{B.R.C}{33}$$

$$-52 \frac{E.R}{20}$$

FK
KP
AB

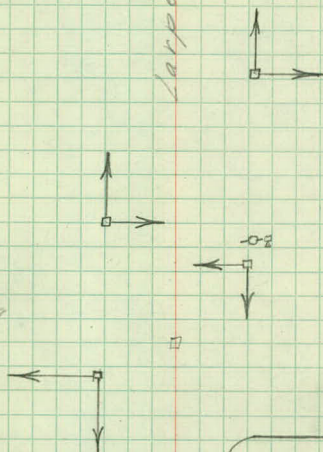
Feb 19, 1958

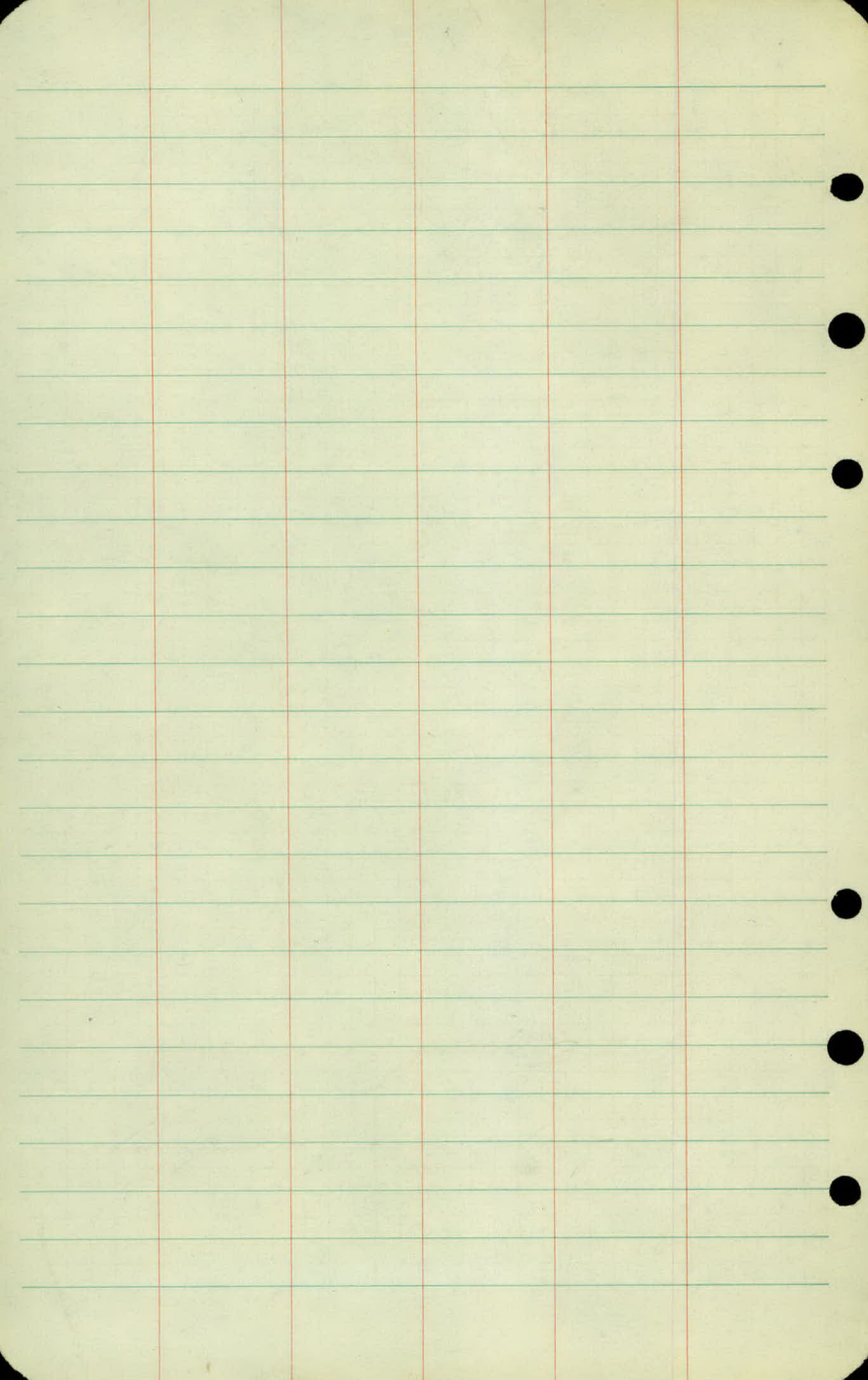
6.

Carpenter Mile 3

Snelling

Ave





X-Sections of
Huron St. - from Idaho to Larp.

Rec 3-18-58

3:00 P.M.

J.B.

Sta	+	π	-	Elev
-----	---	-------	---	------

BM				939.07
---------------	--	--	--	--------

0+00				
------	--	--	--	--

+16				
-----	--	--	--	--

+31				
-----	--	--	--	--

+40				
-----	--	--	--	--

✓				
---	--	--	--	--

RG
KP
AB

Lt.

E

Rt.

2

March 17, 1958

~~Top Hyd. SW Cor Huron + Idaho~~

-1	-2	-1	5.8	0	+1.2	+3
50	32	12		12	29	51

-4	-4	-1	0	5.8	0	+1	+1	+3
47	29	23	10		8	19	41	60

-2	-2	0	5.4	-1	0	+2
53	29	14		12	31	48

-3.3	-4	0	5.0	+2	-1.5	-2.9
25	18	14		15	21	34

+3.9
42

-2.6
46

Sta	+	π	-	Elev
B.M.	9.61	948.68		939.07
1+00			8.50	940.18
MH			12.65	936.03
1+50			6.34	942.34
2+00			4.5	944.18
2+30			4.4	944.28
2+40			5.2	943.48
TP	1.82	937.92	12.58	936.10

March 17, 1958

LT.

E

Rt.

3

Top View of Hump Island

41.2 10	41.2 24	40.1 20	40.2 14	5.3	41.9 10	41.5 20	41.5 35
-1.5	-1.5	0	0	-1.3	-1.3	-1.3	-1.8

Grate ring to invert (Flow line) 12.51'

42.8 50	42.5 30	42.2 14	✓	42.2 10	42.8 15	43.2 38
-1.5	-1.2	+1.1	✓	+1.1	-1.5	-1.9

43.6 28	43.7 10	✓	44.4 11	44.7 28	44.4 45
+1.6	+1.5	✓	-1.2	-1.5	-1.4

44.6 27	45.2 16	46.3 6	✓	46.9 12	47.0 26	46.3 49
-0.5	-0.9	-1.0	✓	-1.6	-0.9	-2.0

46.5 49	46.5 28	46.5 12	✓	47.0 11	47.1 22	47.5 53
+2.0	-1.0	-1.0	✓	+2.5	+6.4	-11.0
						5.5

Sta	+	π .	-	Elev
TP	0.64	937.92 924.85	13.71	924.21
2+80			1.1	923.75 ⁹

✓

3+00			8.0	916.85 ^{to}
------	--	--	-----	----------------------

✓

3+34			10.8	914.05
------	--	--	------	--------

Lx.

E

Rt.

4

$$\begin{array}{r} 30.2 \\ \times 2 \\ \hline -6.5 \\ 23 \end{array}$$

$$\begin{array}{r} 29.2 \\ \times 2 \\ \hline -5.5 \\ 21 \end{array}$$

$$\begin{array}{r} 27.0 \\ \times 2 \\ \hline -4.0 \\ 17 \end{array}$$

$$\begin{array}{r} 70 \\ \times 2 \\ \hline \end{array}$$

$$\begin{array}{r} 17.0 \\ \times 2 \\ \hline +6.8 \\ 7 \end{array}$$

$$\begin{array}{r} 14.2 \\ \times 2 \\ \hline +8.4 \\ 17 \end{array}$$

$$\begin{array}{r} 19.1 \\ \times 2 \\ \hline +10.7 \\ 22 \end{array}$$

$$\begin{array}{r} 34.1 \\ \times 2 \\ \hline +11.0 \\ 40 \end{array}$$

$$\begin{array}{r} 10.3 \\ \times 2 \\ \hline +16.5 \\ 53 \end{array}$$

$$\begin{array}{r} 9.62 \\ \times 2 \\ \hline +14.2 \\ 33 \end{array}$$

$$\begin{array}{r} 24.9 \\ \times 2 \\ \hline -8.1 \\ 24 \end{array}$$

$$\begin{array}{r} 22.8 \\ \times 2 \\ \hline -6.0 \\ 19 \end{array}$$

$$\begin{array}{r} 20.0 \\ \times 2 \\ \hline -3.2 \\ 10 \end{array}$$

$$\begin{array}{r} 86 \\ \times 2 \\ \hline \end{array}$$

$$\begin{array}{r} 14.9 \\ \times 2 \\ \hline +1.9 \\ 9 \end{array}$$

$$\begin{array}{r} 13.8 \\ \times 2 \\ \hline +3.0 \\ 26 \end{array}$$

$$\begin{array}{r} 12.4 \\ \times 2 \\ \hline +4.1 \\ 33 \end{array}$$

$$\begin{array}{r} 40.0 \text{ Elev} \\ \times 2 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 10.5 \\ \times 2 \\ \hline +6.3 \\ 53 \end{array}$$

$$\begin{array}{r} 11.1 \\ \times 2 \\ \hline +5.7 \\ 39 \end{array}$$

$$\begin{array}{r} 21.8 \\ \times 2 \\ \hline -7.8 \\ 30 \end{array}$$

$$\begin{array}{r} 15.8 \\ \times 2 \\ \hline -1.8 \\ 21 \end{array}$$

$$\begin{array}{r} 13.5 \\ \times 2 \\ \hline +0.5 \\ 6 \end{array}$$

$$\begin{array}{r} 93 \\ \times 2 \\ \hline \end{array}$$

$$\begin{array}{r} 14.8 \\ \times 2 \\ \hline -0.8 \\ 13 \end{array}$$

$$\begin{array}{r} 14.3 \\ \times 2 \\ \hline -0.3 \\ 32 \end{array}$$

$$\begin{array}{r} 14.2 \\ \times 2 \\ \hline -0.8 \\ 44 \end{array}$$

$$\begin{array}{r} 38.5 \text{ Elev} \\ \times 2 \\ \hline 55 \end{array}$$

Sta + π - Elev

924.85

3+34

3+51

8.7

ⁿ
916.15

✓

3+74

8.3

ⁿ
916.55

✓

Lt.

L

March 17, 1958

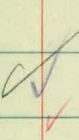
Rt.

5


 $\begin{array}{r} 13.3 \\ 13.8 \\ \hline \end{array}$
 $+0.7$
51

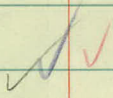
 $\begin{array}{r} 20.0 \\ 12.0 \\ \hline \end{array}$
-3.8
29

 $\begin{array}{r} 18.0 \\ 10.0 \\ \hline \end{array}$
-2.2
19

 $\begin{array}{r} 17.6 \\ 10.0 \\ \hline \end{array}$
-1.4
9

 $\begin{array}{r} 15.6 \\ 10.0 \\ \hline \end{array}$
+0.6
13

 $\begin{array}{r} 15.8 \\ 10.0 \\ \hline \end{array}$
+0.8
20

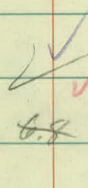
 $\begin{array}{r} 15.6 \\ 10.0 \\ \hline \end{array}$
+0.6
36

 $\begin{array}{r} 22.6 \\ 29.0 \\ \hline \end{array}$
-6.4
35

 $\begin{array}{r} 17.4 \\ 10.0 \\ \hline \end{array}$
+1.8
52

 $\begin{array}{r} 15.8 \\ 10.0 \\ \hline \end{array}$
+0.4
44

 $\begin{array}{r} 14.3 \\ 12.0 \\ \hline \end{array}$
+2.2
30

 $\begin{array}{r} 17.0 \\ 14.0 \\ \hline \end{array}$
+2.6
20

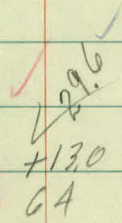
 $\begin{array}{r} 16.3 \\ 16.0 \\ \hline \end{array}$
+0.2
10

 $\begin{array}{r} 15.4 \\ 14.0 \\ \hline \end{array}$
+1.2
11

 $\begin{array}{r} 14.9 \\ 13.0 \\ \hline \end{array}$
+1.7
28

 $\begin{array}{r} 15.8 \\ 15.0 \\ \hline \end{array}$
+0.8
39

 $\begin{array}{r} 16.3 \\ 16.0 \\ \hline \end{array}$
+0.2
37

 $\begin{array}{r} 18.1 \\ 19.0 \\ \hline \end{array}$
-1.6
44

 $\begin{array}{r} 21.6 \\ 26.0 \\ \hline \end{array}$
-5.1
51

 $\begin{array}{r} 29.6 \\ 17.0 \\ \hline \end{array}$
+12.0
64

 $\begin{array}{r} 3.0 \\ 27.0 \\ \hline \end{array}$
+26.5
90

 $\begin{array}{r} 14.4 \\ 12.0 \\ \hline \end{array}$
+2.2
53

Sta	+	π	-	Elev
-----	---	-------	---	------

		924.85		
--	--	--------	--	--

+83				
-----	--	--	--	--

			10.8	
--	--	--	------	--

				914.05
--	--	--	--	--------

✓

4+00				
------	--	--	--	--

			10.3	
--	--	--	------	--

				914.55
--	--	--	--	--------

✓

+26				
-----	--	--	--	--

			11.6	
--	--	--	------	--

				913.25
--	--	--	--	--------

March 17, 1958

4

4

27

6

$$\begin{array}{r} 14.1 \\ \times 1.1 \\ \hline 0 \\ 24 \end{array}$$

$$\begin{array}{r} 15.2 \\ \times 1.0 \\ \hline -1.1 \\ 15 \end{array}$$

$$\begin{array}{r} 15.7 \\ \times 1.0 \\ \hline -1.6 \\ 10 \end{array}$$

$$\begin{array}{r} 12.7 \\ \times 1.1 \\ \hline 7.3 \end{array}$$

$$\begin{array}{r} 12.7 \\ \times 1.1 \\ \hline +1.4 \\ 10 \end{array}$$

$$\begin{array}{r} 12.8 \\ \times 1.1 \\ \hline +1.3 \\ 21 \end{array}$$

$$\begin{array}{r} 14.7 \\ \times 1.1 \\ \hline -0.6 \\ 37 \end{array}$$

$$\begin{array}{r} 15.6 \\ \times 1.1 \\ \hline -1.5 \\ 42 \end{array}$$

$$\begin{array}{r} 19.7 \\ \times 1.1 \\ \hline -5.6 \\ 55 \end{array}$$

$$\begin{array}{r} 21.4 \\ \times 1.1 \\ \hline -7.3 \\ 57 \end{array}$$

$$\begin{array}{r} 15.7 \\ \times 1.1 \\ \hline -1.6 \\ 64 \end{array}$$

$$\begin{array}{r} 15.7 \\ \times 1.1 \\ \hline -1.1 \\ 55 \end{array}$$

$$\begin{array}{r} 15.7 \\ \times 1.1 \\ \hline -1.1 \\ 55 \end{array}$$

$$\begin{array}{r} 14.8 \\ \times 1.1 \\ \hline -0.2 \\ 41 \end{array}$$

$$\begin{array}{r} 14.0 \\ \times 1.1 \\ \hline +0.6 \\ 25 \end{array}$$

$$\begin{array}{r} 14.2 \\ \times 1.1 \\ \hline +0.4 \\ 10 \end{array}$$

$$\begin{array}{r} 15.2 \\ \times 1.1 \\ \hline 5.7 \end{array}$$

$$\begin{array}{r} 15.2 \\ \times 1.1 \\ \hline -0.6 \\ 11 \end{array}$$

$$\begin{array}{r} 14.8 \\ \times 1.1 \\ \hline -0.2 \\ 31 \end{array}$$

$$\begin{array}{r} 15.0 \\ \times 1.1 \\ \hline -0.4 \\ 97 \end{array}$$

$$\begin{array}{r} 19.8 \\ \times 1.1 \\ \hline -5.2 \\ 56 \end{array}$$

$$\begin{array}{r} 15.7 \\ \times 1.1 \\ \hline -0.8 \\ 59 \end{array}$$

$$\begin{array}{r} 15.7 \\ \times 1.1 \\ \hline -0.8 \\ 59 \end{array}$$

$$\begin{array}{r} 20.7 \\ \times 1.1 \\ \hline -7.4 \\ 56 \end{array}$$

$$\begin{array}{r} 18.1 \\ \times 1.1 \\ \hline -4.8 \\ 42 \end{array}$$

$$\begin{array}{r} 14.0 \\ \times 1.1 \\ \hline -0.7 \\ 24 \end{array}$$

$$\begin{array}{r} 13.1 \\ \times 1.1 \\ \hline +0.2 \\ 10 \end{array}$$

$$\begin{array}{r} 12.9 \\ \times 1.1 \\ \hline 8.4 \end{array}$$

$$\begin{array}{r} 12.9 \\ \times 1.1 \\ \hline +0.4 \\ 13 \end{array}$$

$$\begin{array}{r} 13.8 \\ \times 1.1 \\ \hline -0.5 \\ 30 \end{array}$$

$$\begin{array}{r} 13.8 \\ \times 1.1 \\ \hline -0.5 \\ 54 \end{array}$$

$$\begin{array}{r} 10.9 \\ \times 1.1 \\ \hline +2.4 \\ 63 \end{array}$$

Sta	+	π	-	Elev
		924.85		
4+36			5.3	919.55 924.55

TP	10.24	932.64	2.45	922.40
----	-------	--------	------	--------

+44			8.1	924.54
-----	--	--	-----	--------

✓

+54			3.6	929.04
-----	--	--	-----	--------

✓

RG
KP
AB

March 18, 1958

RT.

7

18.1 -1.5 52	19.2 0	24.5 -5.0 25	21.4 -1.8 13	6.2	+2.0 11	+5.5 29	+5.7 53	+8.3 65
+28.5 100								

20.9 -6.4 53	29.6 -5.1 3.2	29.1 -2.6 14	7.4	+1.1 13	+3.6 30	+6.6 52	+9.6 68
-------------------------------	--------------------------------	-------------------------------	-----	------------	------------	------------	------------

27.5 -3.0 63	29.9 -5.4 68
-------------------------------	-------------------------------

31.2 -2.2 62	30.4 -1.4 40	28.7 +0.3 18	5.0	+0.7 7	+0.7 17	+3.1 34	+6.4 54
-------------------------------	-------------------------------	-------------------------------	-----	-----------	------------	------------	------------

30.4 -1.4 64

Sta	+	Δ	-	Elev
-----	---	----------	---	------

		932.64		
--	--	--------	--	--

4+76				
------	--	--	--	--

		932.64	3.6	929.04
--	--	-------------------	-----	--------

✓

TD				
----	--	--	--	--

		2.25		930.39
--	--	------	--	--------

Flat Rt & Lt over 60'

March 18, 1958

\$

RT

8

LT

$\begin{array}{r} 31.4 \\ - 26.6 \\ \hline \end{array}$	$\begin{array}{r} 30.5 \\ - 27.5 \\ \hline \end{array}$	$\begin{array}{r} 29.5 \\ - 28.5 \\ \hline \end{array}$	$\begin{array}{r} 28.7 \\ - 28.3 \\ \hline \end{array}$	$\begin{array}{r} 27.5 \\ - 30.5 \\ \hline \end{array}$	$\begin{array}{r} 27.0 \\ - 5.0 \\ \hline \end{array}$
-2.4	-1.5	-0.5	5.8	+0.3	+2.0
63	47	23		14	56

$\begin{array}{r} 34.8 \\ - 23.8 \\ \hline \end{array}$

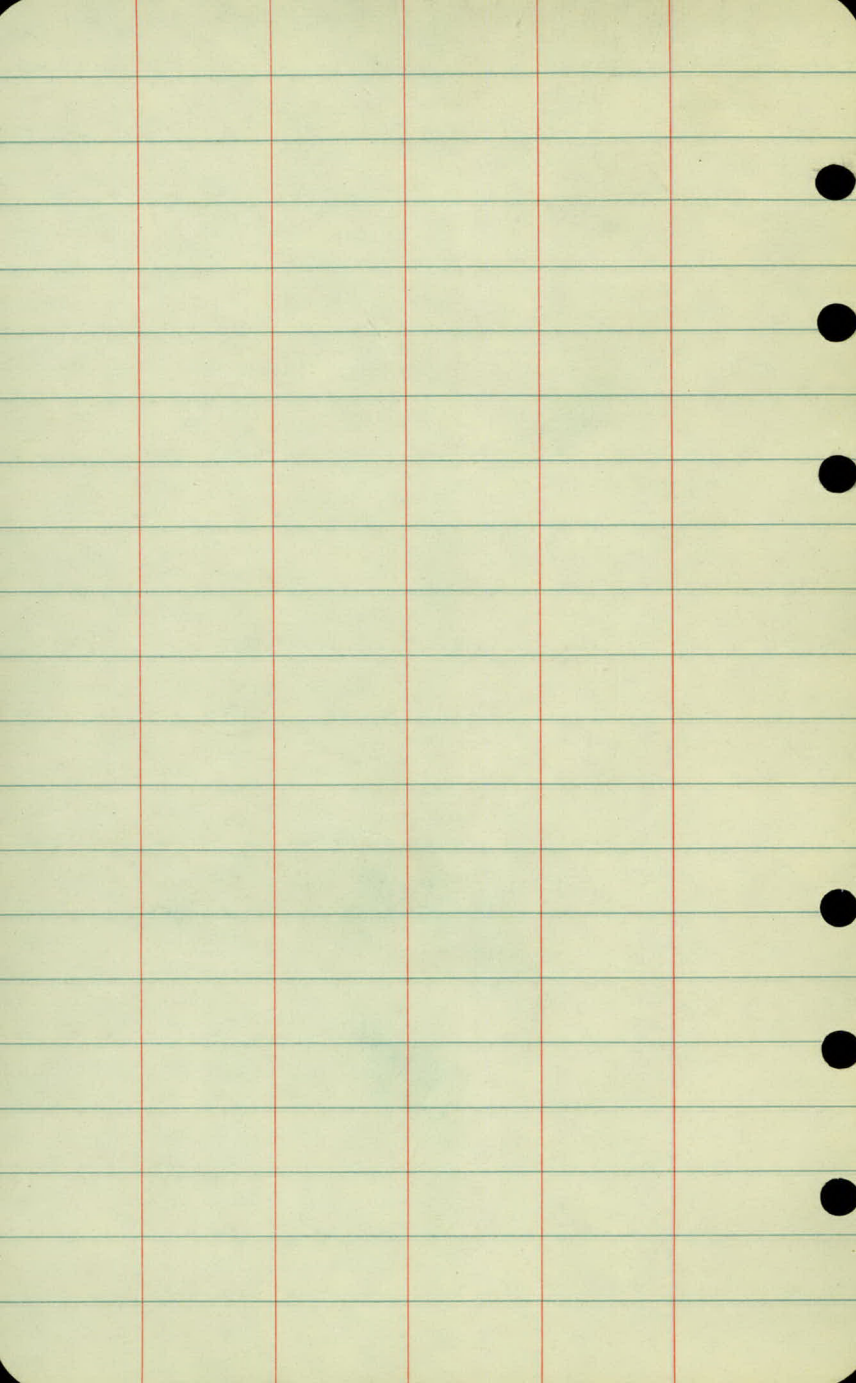
-5.2
68

48.0 Elev
81

$\begin{array}{r} 24.1 \\ - 33.9 \\ \hline \end{array}$

+4.9
64

Sta 30+00 mile #3 Laporte Ave



FK
RG
KP
GW
AB
RJ

March 5, 1958
Fair Overcast 32°

1

HURON ST.

IDAHO to LARPENTEUR

A pages

5

Tw 16" CW
+13 $\frac{22}{}$

STP
+14 $\frac{33}{}$

4
+108 $\frac{16" CW}{35}$

End Coll. W.
+155 $\frac{40-50}{}$

STP
+89 $\frac{51}{6}$

STP
+61 $\frac{2}{}$

STP
+60 $\frac{2}{}$

STP
+24 $\frac{21}{}$

STP
+21 $\frac{7}{}$

20" CW
+11 $\frac{26}{}$

16" CW
+18 $\frac{5}{}$

16" CW
+21 $\frac{4}{}$

3
+60 Begin Coll. Woods
 $\frac{25-50}{}$

7" BE
+50 $\frac{7}{}$

8" BE
+41 $\frac{1}{}$

E. Fe
+36 $\frac{31}{}$

2

X-Fe
+90 $\frac{31}{}$

Trip 6" M
+78 $\frac{34}{}$

W. Car shed
+63 $\frac{28}{}$

R Tie
+81 $\frac{shed}{}$

PP
+58 $\frac{22}{}$

Fe Car
+49 $\frac{31}{}$

Trip 8" M
+31 $\frac{31}{}$

20" M
+56 $\frac{34}{}$

1

SE Car Garage
+22 $\frac{51}{}$

E. Ent
+09 $\frac{R+}{}$

SE Car Ho
+60 $\frac{27}{}$

SW Car Ho
+67 $\frac{37}{}$

18" BE
+91 $\frac{29}{}$

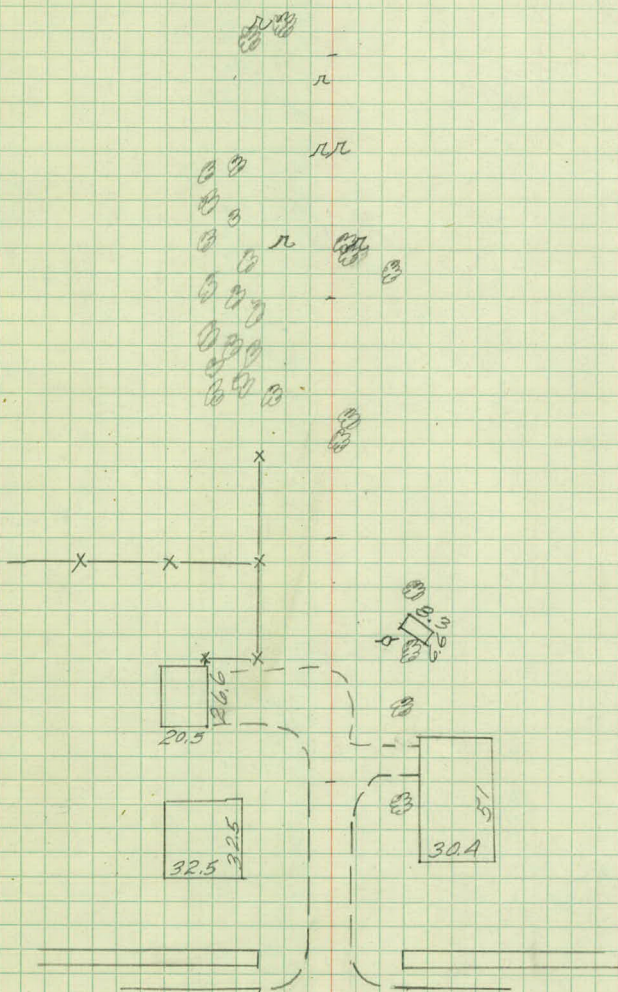
Walk
+30 $\frac{31}{}$

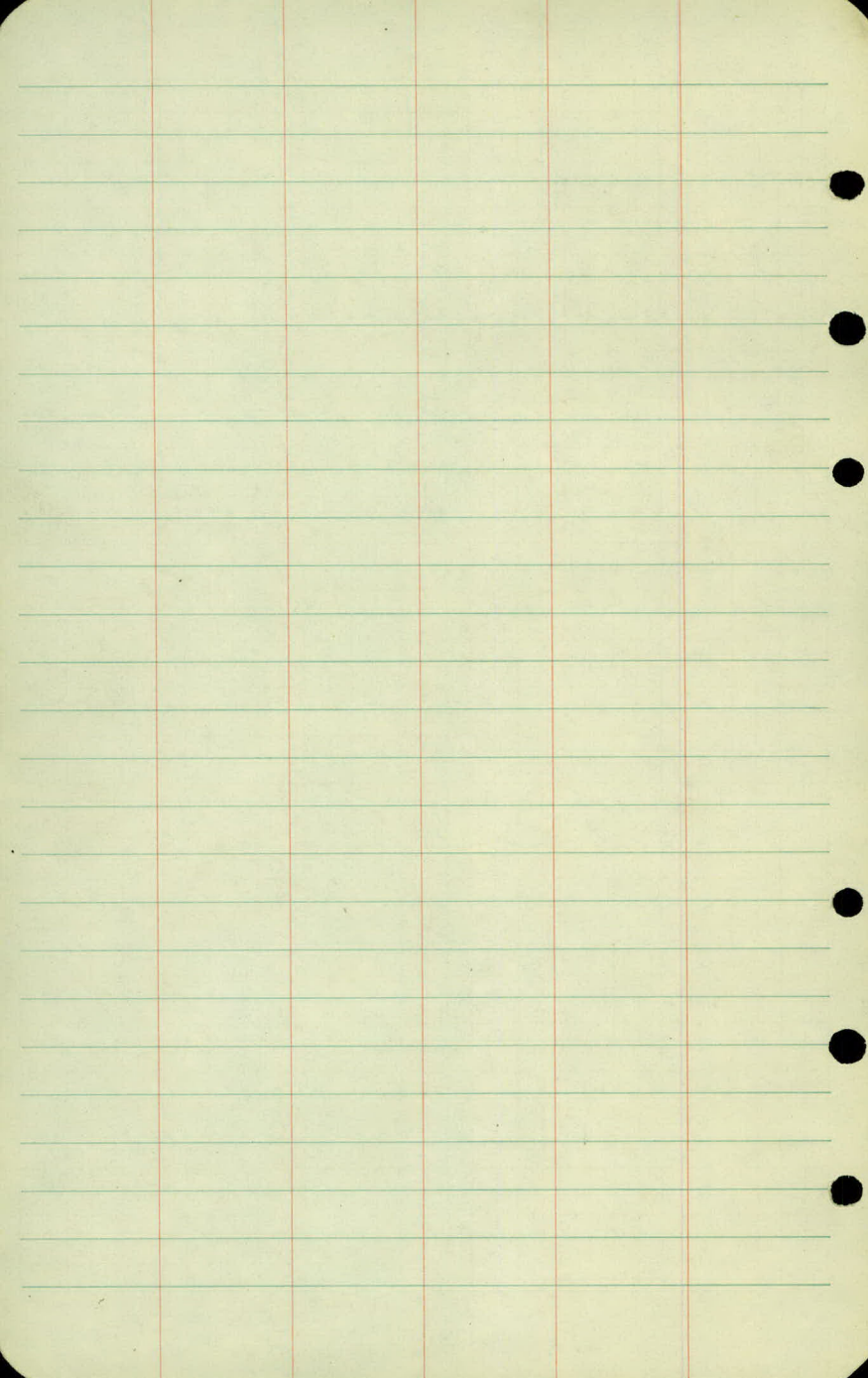
Walk
+30 $\frac{30}{}$

0

March 5, 1958

2





March 5, 1958

3

Building Elev.

sta	+	T	-	Elev.
		254.63		694.10
BM	9.66	948.73		244.97 739.07
MH			12.69	241.94
				936.04
				47.03
			7.60	417.13
				48.69
			5.94	42.79
				242.93
			11.7	37.03
				248.67
			5.96	42.77
				250.03
2+00			4.6	44.13

March 5, 1958

4

Top Hyd SW cor Huron & Idaho

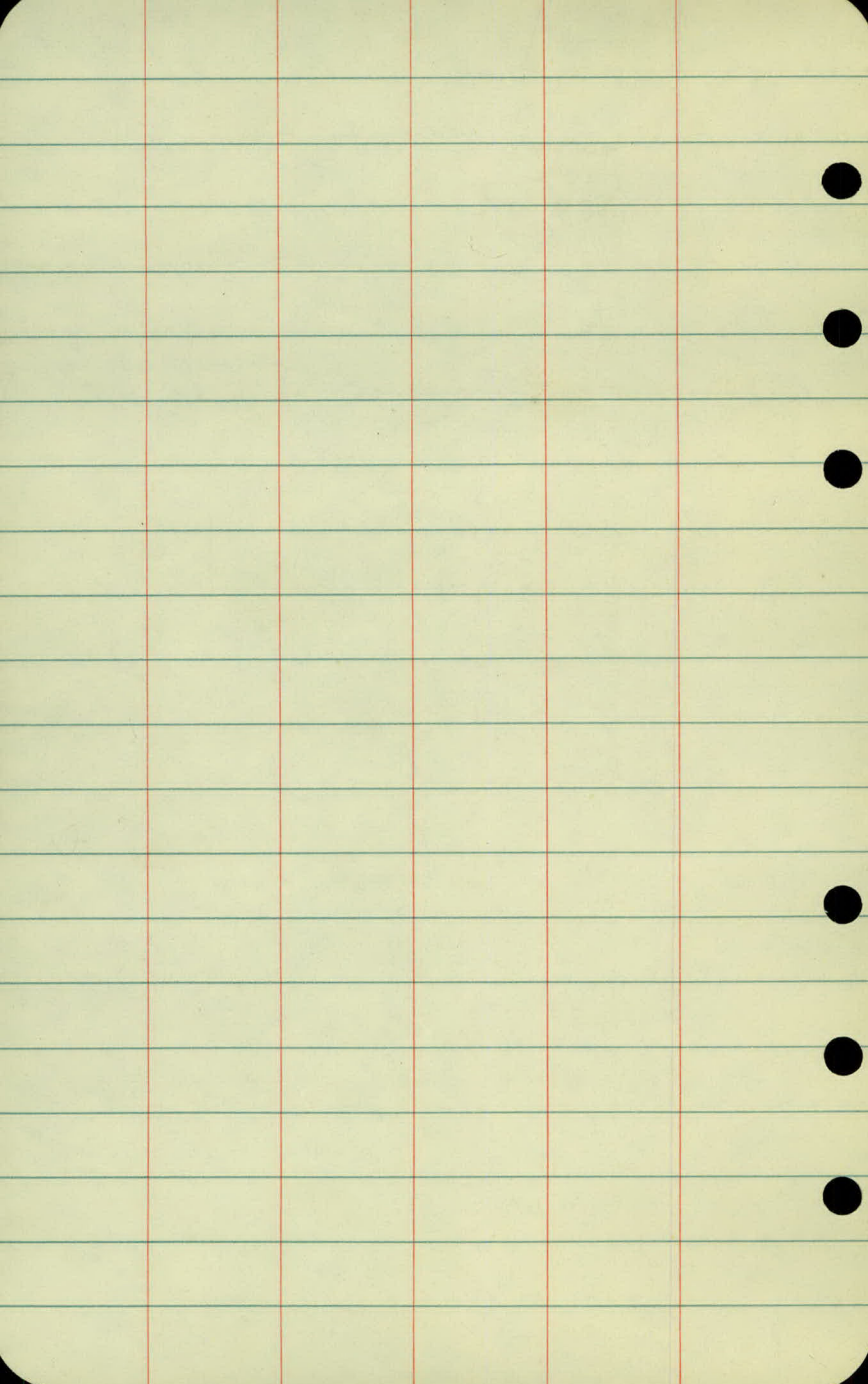
& Huron & Idaho

S.W. at steps E side house 1311 Idaho

Ground Elev at Steps W side house NE corner

Ground Elev at Basement Garage for above houses
Huron & Idaho

Floor Elev Garage 1311 Idaho



FK
RG
AB

April 9, 1958

1

Bench Transfers



CARPENTERS AVE

Construction Bench Marks

Sta	+	-	Elev
BM	1.29	959.34	958.05
to BM		4.27	955.07
2+00		5.24	954.10
BM	1.72	956.21	954.49
BM		3.29	952.92
8+00		4.83	
BM	1.71	955.52	953.81
BM		2.72	952.80
13+00		4.73	
BM	2.33	954.82	952.49
BM		3.49	951.33
16+00		4.61	
BM	1.91	950.78	948.87
BM		3.34	947.44
24+00		4.24	

April 9, 1958

2

Top Hyd at Snelling & Larpenteur

Top E End Pump Island S.E. Cor

£

Top Hyd N.E. Cor Arona & Larpenteur.

N.E. Cor Conc. Ent. Slab 1510 W Larpenteur

£

Top Hyd N.W. Cor Pascal & Larpenteur

Top S.E. Cor Lower Step Ho # 1463 W Larp.

£

Top Hyd N.W. Cor Holton & Larpenteur

Top S.E. Cor Lower Step Ho # 1433 W Larp

£

Top Hyd N.E. Cor Albert & Larpenteur

Top N.E. Cor Lower Step Ho # 1396 W Larp

£

Sta	+	π	-	Elev
-----	---	-------	---	------

BM	3.49	950.23		
----	------	--------	--	--

				946.74
--	--	--	--	--------

BM			3.65	946.58
----	--	--	------	--------

25+00			4.69	945.54
-------	--	--	------	--------

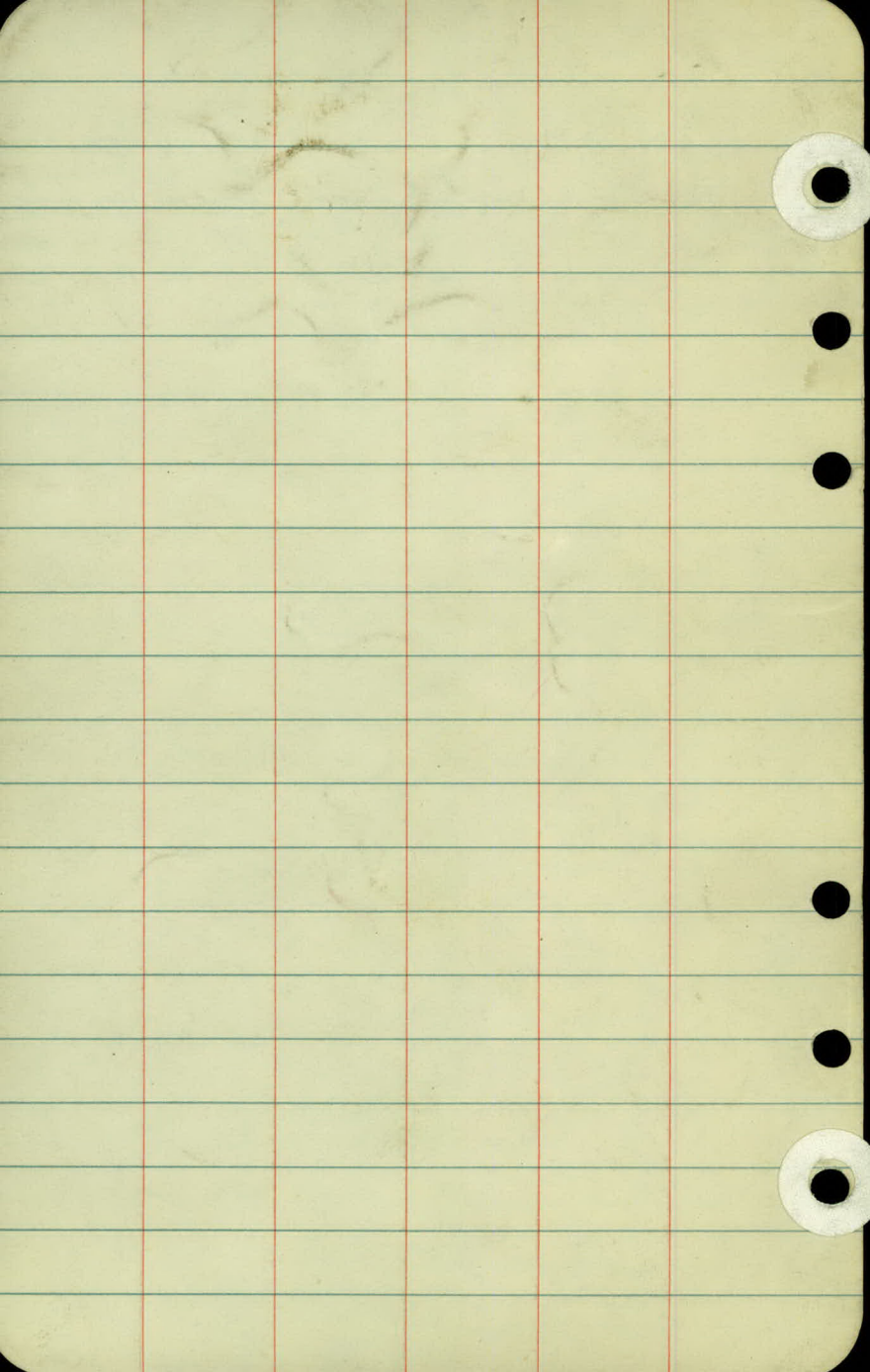
April 9, 1958

3

Top Hyd S.W. Cor Hamline & Larp

Top S.E. Cor Lower step Ho #1357 W. Larp

£



KP

RL

AUGUST 13, 1958

1

FINALS

LARPEUR AVE
FERNWOOD - ARONA
CURB

30

3 9 + 36
29 / 9 8
3 8
9 4.2 / 8
4 3
6

8
93 90.4
7.6
8 8

KP
RL

SOUTH SIDE AUGUST 13, 1954

2.

ARONA

31' R
CURB

591'

23.9'
R CURB

PASCAL

26.2' R
CURB

596'

23.4'
RC

ALBERT

25.4'
RC

537.5'

30'
RC

HAWKLINE

32'
RC

155'

20'
RC

HURON

21'
RC

582.8'

10.6'
RC

FERNWOOD

TOTAL

2760.3

33.0
844.6
144

29.0
38.0

42.2
586.2

65.1
83.0

10.6
74.0

40.2
74.6

127.0
28.0

943.0

72.2
66.2
2960.9

43
1982
2572
4512

114.2
74.6
88

133.6
65.1
2189

844.6
138.4

10912
144

33
253210160

KD AUGUST 13, 1958

NORTH SIDE

3

RL

ARONA

← 30'
PC

58.5

TOTAL 2459.7

← 25'

PASCAL

← 26.5

2680.95

3103.8

218.8

5784.75

HOLTON

← 22.8

← 25.8

188.7

ALBERT

← 24.2

← 26.2

451.5

HAMLIN

← 30'

← 30'

1015.7

FERNWOOD

