

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

Koehler Road

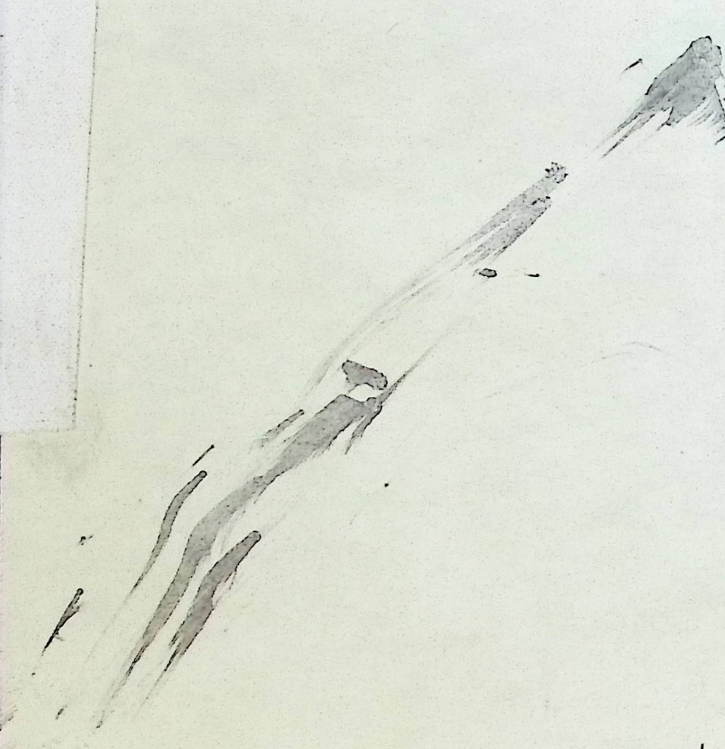
From Edgerton To Centerville

Road Acc't. No. _____

Date Filed 1-6-61

File Dr. 9 Bk. 23

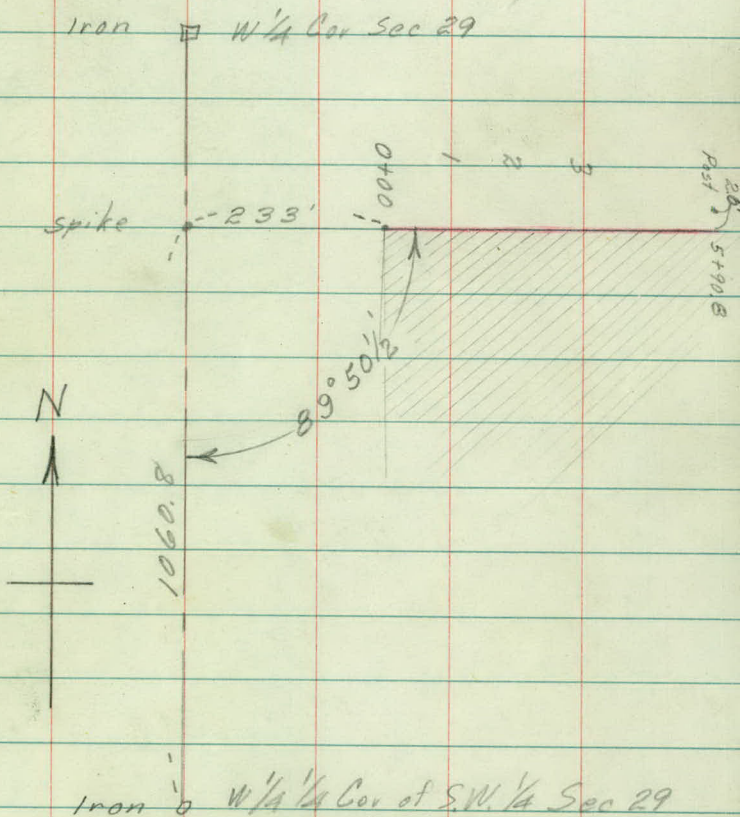
Drainage at Centerville



Kochler Road

Borrow Pit

at 3790 McMenamy



Sta	+	π	-	Elev.
BM	5.13	912.40		907.27
TP	12.92	924.61	0.71	911.69
TP	10.57	934.15	1.03	923.58
BM			1.16	932.99
T.P.	5.10	938.98	0.27	933.88
T.P.	0.81	931.14	8.65	930.33
T.P.	2.51	923.17	10.48	920.66
BM			2.34	920.83' 920.88'

FR
JL
WM
JH

June 2, 1960 2
Overcast 58° Sprinkle

Spike in PP N.W. Cor Kochler Bldg
McMenemy

P.P. Stp.

Spike in P.P. by #3822 McMenemy

± Road

± Road

Rock

(Settled) Top of S. End of Upper Step Platform
Next to the E. Side of Road 900' N. / W. 1/4 Cor
Sec 29

Sta	+	π	-	Elev.
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BM	9.39	942.38		932.99
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0+00	in Garden			
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✓

+50

✓

1

✓

4

June 3, 1960

3

RT

Spike in PP by #3822 MoMenomy

7.4	9.5	10.9	12.9	14.3	13.6
35.0	32.9	31.5	29.5	28.1	28.8
17	40	69	81	95	

148	147	143	137
162	150	124	100
Garden			

8.4	10.0	10.5	11.2	11.9	11.4
34.0	32.4	31.9	31.2	30.5	31.0
29	46	68	78	90	

13.2	12.4	12.0	11.2
158	140	122	100
Garden			

5.6	6.6	7.8	8.9	9.4	10.3	11.6
36.8	35.8	34.6	33.5	33.0	32.1	30.8
25	60	84	100	120	140	

12.8	160
Garden	

Sta	+	π	-	Elev
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		942.38		
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1+33				
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+64				
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+50				
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June 3, 1960

4

RT

39.4	38.8	38.1	36.3	34.3	32.8	30.9	28.4
3.0	3.6	4.3	6.1	7.9	9.6	11.5	14.0
17	47	72	100	119	138	161	

Garden

39.7	38.9	38.6	36.7	34.4	32.3	29.6
2.7	3.5	3.8	5.7	8.0	10.1	12.8
24	44	71	100	119	136	

25.6	27.7	29.1
16.8	14.7	13.3
193	160	150

38.3	38.4	38.0	36.5	35.5	33.8	30.8
4.1	4.0	4.4	5.9	6.9	8.6	11.6
27	50	79	100	123	149	

25.5	26.1	28.6
16.9	16.3	13.8
200	193	169

35.6	35.9	36.9	37.1	36.1	35.7	34.7	33.6
6.8	6.5	5.5	5.3	6.3	6.7	7.7	8.8
13	27	58	82	100	124	150	

28.3	29.7	31.4
14.1	12.7	11.0
217	200	182

Sta	+	π	-	Elev.
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TP	7.12	939.13	10.37	932.01
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+82				
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June 3, 1960 - 5
RT

12.1	11.0	8.6	7.3	7.1	7.2	7.3	7.5
30.3	31.4	33.8	35.1	35.3	35.2	35.1	34.9
16	42	69	88	100	115	137	

13.3	12.3	10.7	10.6	10.3	8.8
29.1	30.1	31.7	31.8	32.1	33.6
241	231	216	200	188	163

12.1	11.6	11.5	9.8	8.9	8.5	7.9
27.0	27.5	27.6	29.3	30.2	30.6	31.2
5	21	46	69	88	100	

13.6	11.7	10.0	8.3	7.9	8.1
25.5	27.4	29.1	30.8	31.2	31.0
218	200	187	165	141	121

13.5	13.0	11.3	10.7	10.0	11.3
25.6	26.1	27.8	28.4	28.1	27.8
16	44	68	87	100	

17.2	14.1	12.2	11.7
21.9	25.0	26.9	27.4
200	175	156	129

Sta	+	X	-	Elev
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BM				
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	6.21	932.92	932.99	
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June 3, 1960

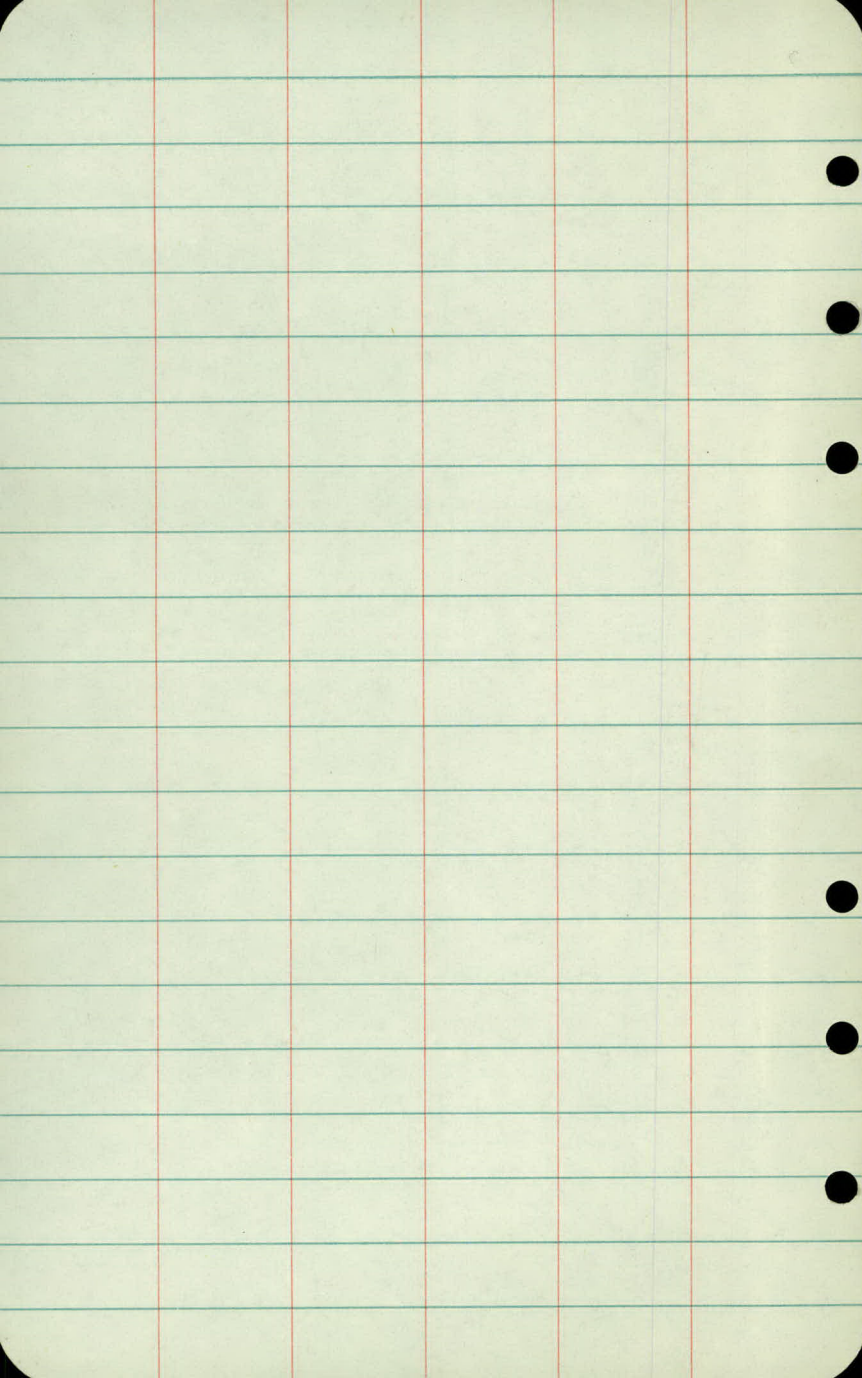
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RT

24.6	25.4	26.6	27.0	26.1	25.7
14.5	13.7	12.5	12.1	13.0	13.4
	19	47	79	100	119
		21.0	23.2	25.3	25.4
		18.1	15.9	13.8	13.7
		200	180	157	138

Spike in PP by #3822 McMenemy

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2228400
2230200
2232000
2233800
2235600
2237400
2239200
2241000
2242800
2244600
2246400
2248200
2250000
2251800
2253600
2255400
2257200
2259000
2260800
2262600
2264400
2266200
2268000
2269800
2271600
2273400
2275200
2277000
2278800
2280600
2282400
2284200
2286000
2287800
2289600
2291400
2293200
2295000
2296800
2298600
2300400
2302200
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2309400
2311200
2313000
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2325600
2327400
2329200
2331000
2332800
2334600
2336400
2338200
2340000
2341800
2343600
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2347200
2349000
2350800
2352600
2354400
2356200
2358000
2359800
2361600
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2365200
2367000
2368800
2370600
2372400
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2390400
2392200
2394000
2395800
2397600
2399400
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2403000
2404800
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2410200
2412000
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2424600
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2428200
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2435400
2437200
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2458800
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2462400
2464200
2466000
2467800
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2487600
2489

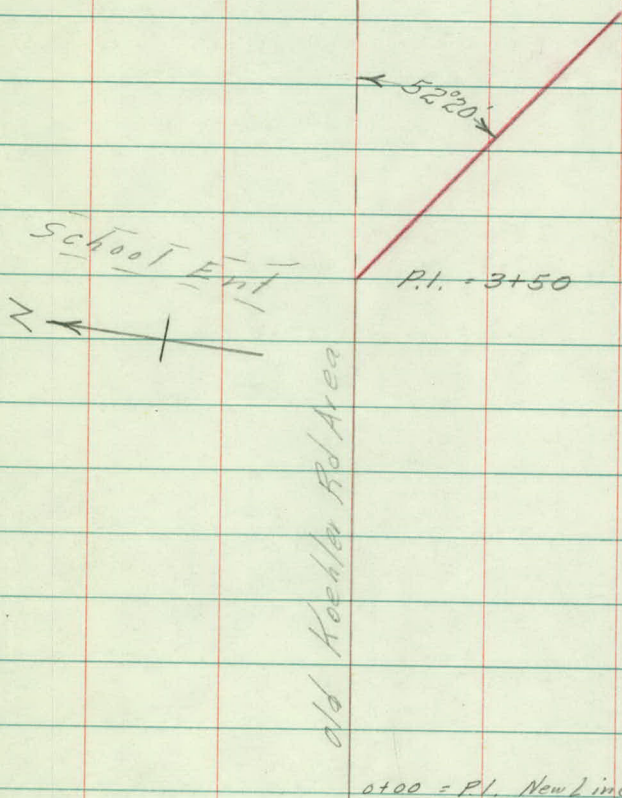


June 3, 1960

7

Koehler Road

old Road Excavation



Sta + π - Elev.

BM 908 925.68

916.62

4+00

✓

+50

✓

5

✓

June 3, 1960

8

11

BT

Frame of Steel Cover plate of Dry Well SW of School

15.9	17.2	17.6	17.7	16.9	15.7	14.9	12.2
9.8	8.5	8.1	8.0	8.8	10.0	10.8	13.5
31	26	20	14	BT	13	18	25

16.3	17.2	17.0	15.0
9.4	8.5	50	34
37	50		

18.0	18.2	18.9	18.7	18.3	17.7	17.5	16.6	14.3
7.7	7.5	6.8	7.0	7.4	8.0	8.2	9.1	11.4
30	25	20	11	BT	8	11	15	20

19.1	19.7	19.9	20.2	11.6	11.7	13.1
6.6	6.0	5.8	5.5	14.1	14.0	12.6
34	42	48	50	50	48	29

20.9	20.0	20.9	21.3	21.1	20.9	20.4	20.7	17.6
4.8	5.7	4.8	4.4	4.6	4.8	5.3	5.0	8.1
28	21	17	9	BT	9	14	17	24

20.9	21.3	17.2	17.5	18.2	17.3
4.8	4.4	8.5	8.2	7.5	8.4
39	50	50	37	29	27

Sta + π - Elev.

925.68

5+25

✓

+37 Along Concrete Edge of Centerville

BM

1.98 923.70 (923.69)

June 3, 1960

9

LT

RT

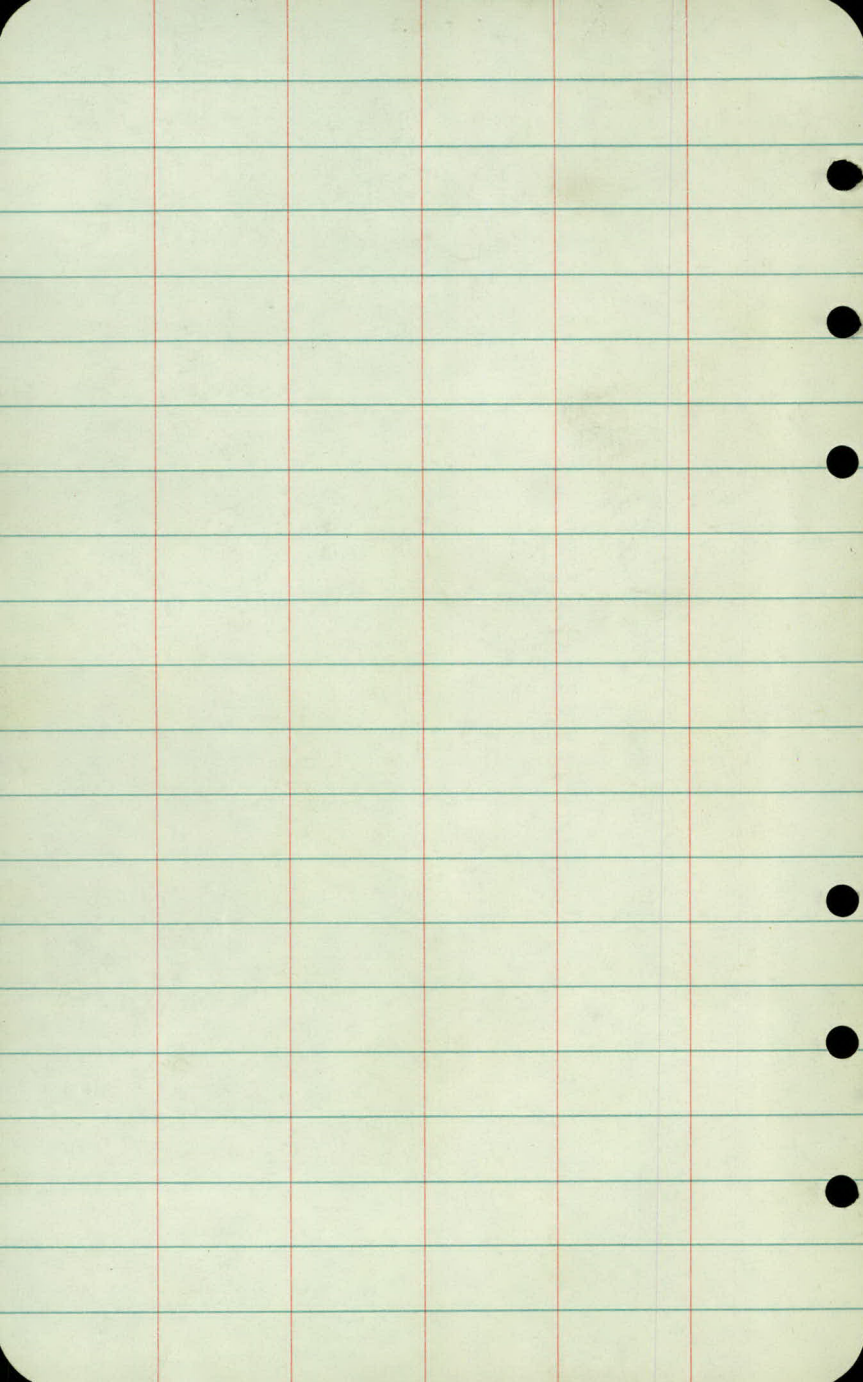
25.0	24.7	24.2	24.0	23.3	22.6	22.7	20.0	17.6
0.7	1.0	1.5	1.7	2.4	3.1	3.0	5.7	8.1
50	38	25	14	16	18	27	34	

BT

19.4	19.8
6.3	5.9
50	42

24.8	24.6	24.4	24.2	24.0	23.9	23.7
0.9	1.1	1.3	1.5	1.7	1.8	2.0
50	38	17		17	34	50

RR Spike in PP NEC, E & Centerville



Kochler Rd.
(at Centerville Rd.)

Profile Grade

Sta. P.G.

11+00 917.6

+16 17.4

+50 16.9

12+00 15.9

+13 15.6

+36 15.0

+50 14.7

+77 14.0

13+00 13.4

+42 12.8

+68 12.8

14+00 13.2

+50 15.0

+80 16.5

15+00 17.5

+50 19.9

16+00 21.7

+37 22.5

+62 22.8

+70 22.8

Sta P.G.

16+78 26.9

+93.91 23.0

Kochler Rd.

Profile Grade

1
KOEHLER ROAD

at

Centerville Road

PLAN SURVEY

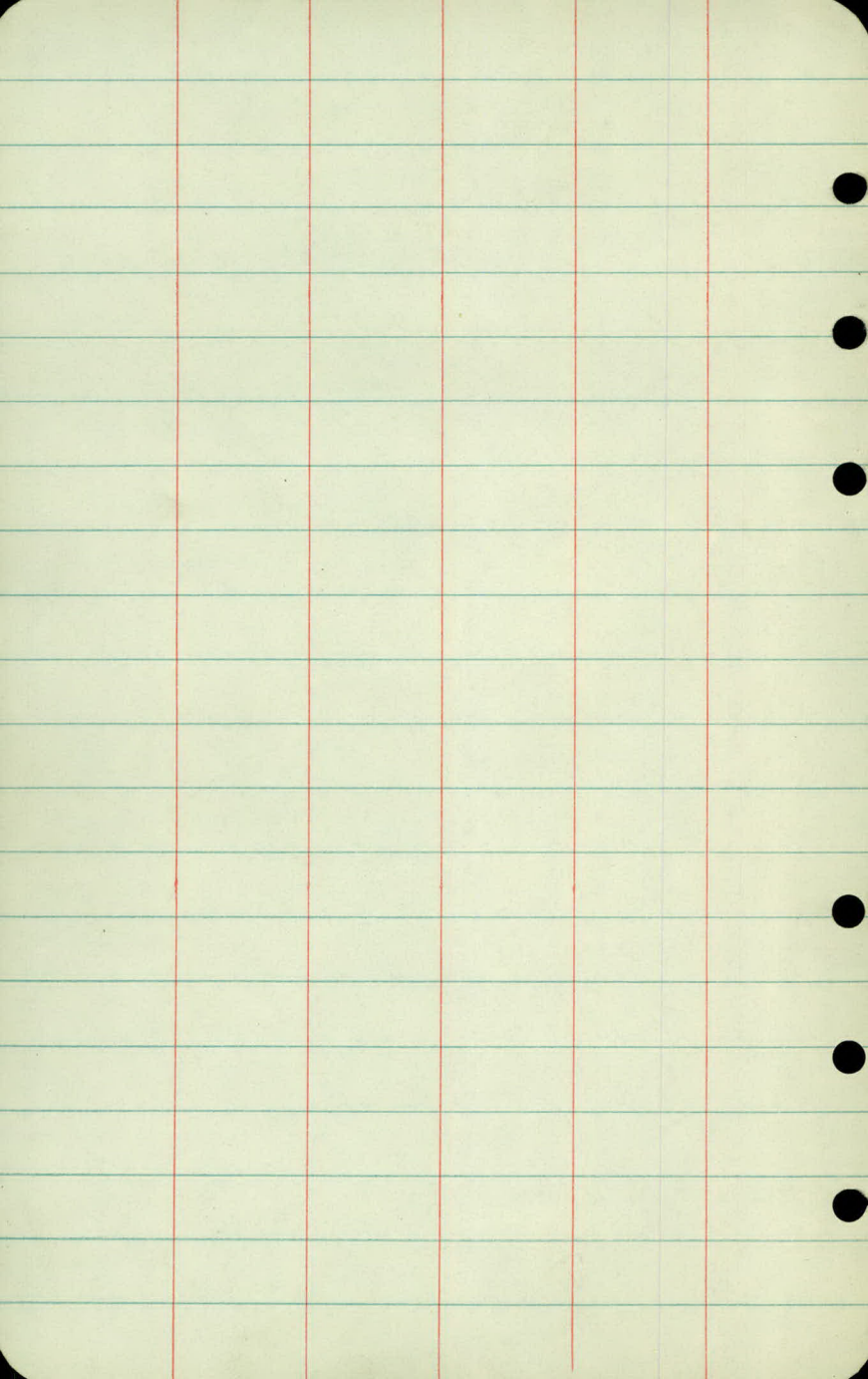
Alignment 2-3

Topography 4-6

Bench Levels 7-8

X-Sections 9-18

PCC 1/12/60



FX
RG
JS
CW
JH

January 15, 1960
Cold Clear 10° Windy

2

Alinement

~~X~~ "1" Line

Sta Point Δ Lt Δ Rt

16+93.97 P.I. $\pm$ Centerville Rd

+42.94 P.T.

$17^{\circ}00'45''$

13

$13^{\circ}47'12'' \Delta = 34^{\circ}01'30''$

+50

$10^{\circ}02'12'' D = 15^{\circ}$

12+32.90 P.I. = ^{Sta 2+32.90} P.I. of Line "B" T = 116.79

2

$6^{\circ}17'12'' L = 226.83$

+50

$2^{\circ}32'12'' R = 381.97$

11 +16.11 PC

$0^{\circ}00'$

Jan. 15, 1960

3

163.36 M.
42.1/100
N.T.B.
F.K.

nail

$93^{\circ} 25\frac{1}{2}'$

N

P.P. Ground Wire

Borrow P.P. Base Line
 $\Delta = 101.9$
 $11^{\circ} 16\frac{1}{2}'$

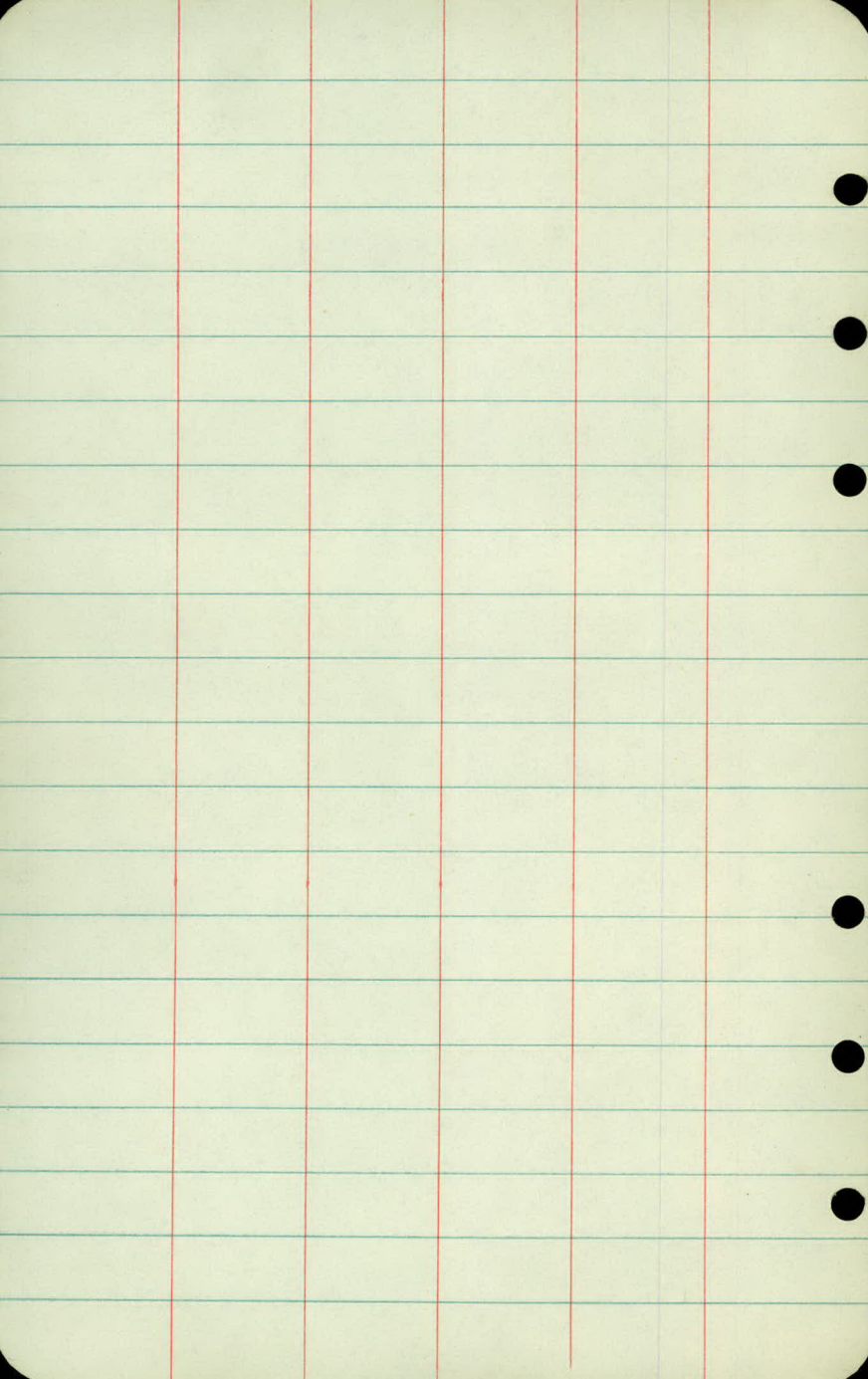
Boat Spike

120.86

158.22

Cor. Fo

Cor Stucco Ho

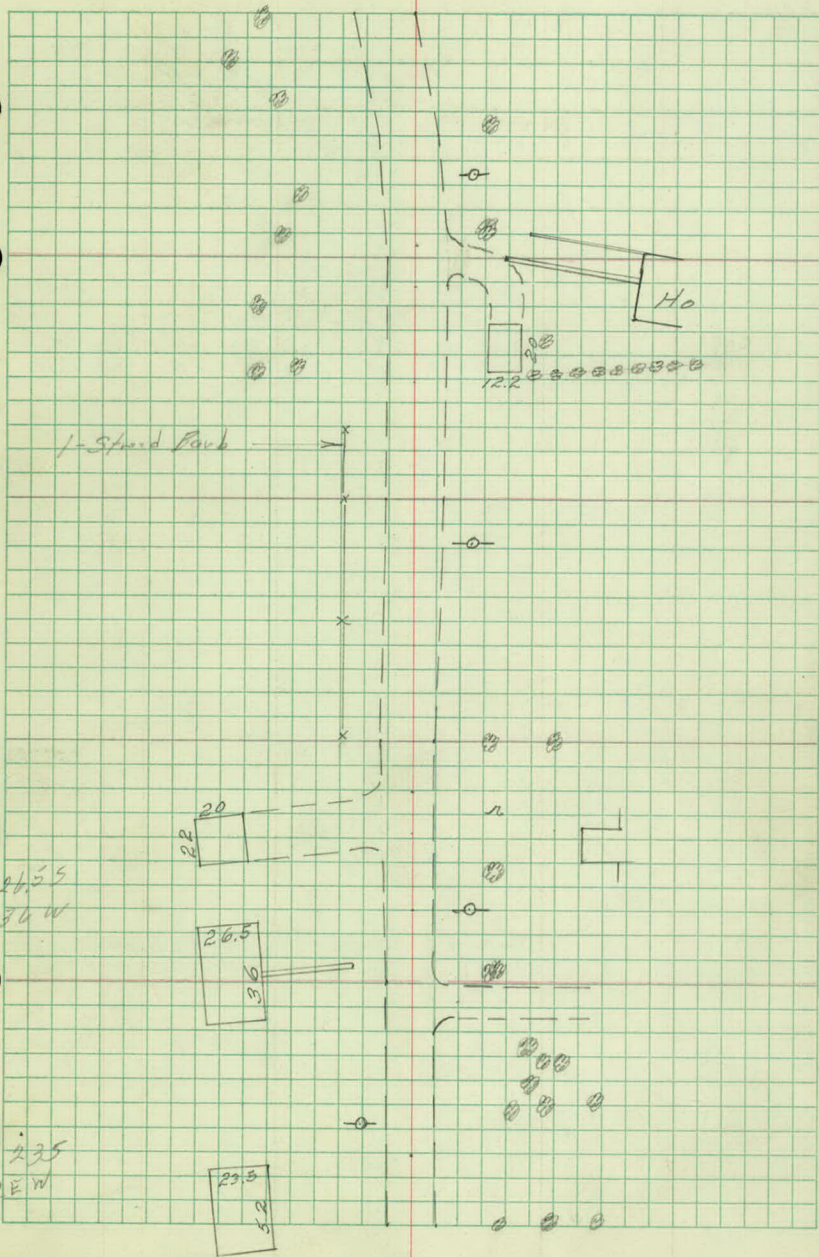


Topography

[illegible]

Jan 15, 1960

5



+19 57 ^{24" BSP}

17

+15 ^{24" SCP}
49

+84 ^{Edge Cone}
±

+66 ^{PP}
61

+58 ^{PP}
82

+48 ^{End Scattered Trees}
10' Lt to 85' Rt

16

+77 ^{Begin Small}
^{Scattered Trees}
12' Lt to 90' Rt

15

+84 ^{Edge Lowland}
±

14

+100 ^{Lowland}
62

+26 ^{43" Cott.}
31

+43 ^{Lowland}
±

+22 ^{24" E.H.}
36

13

+100 ^{BT}
59

+100 ^{Lowland}
50

+80 ^{PP}
30

+50 ^{BT}
50 to 25' Lt

+32 ^{± Ent}
78

+51 ^{Ent}
52

+32 ^{Trip BEM}
60

12

Jan 15, 1960

6

Centerville

Road

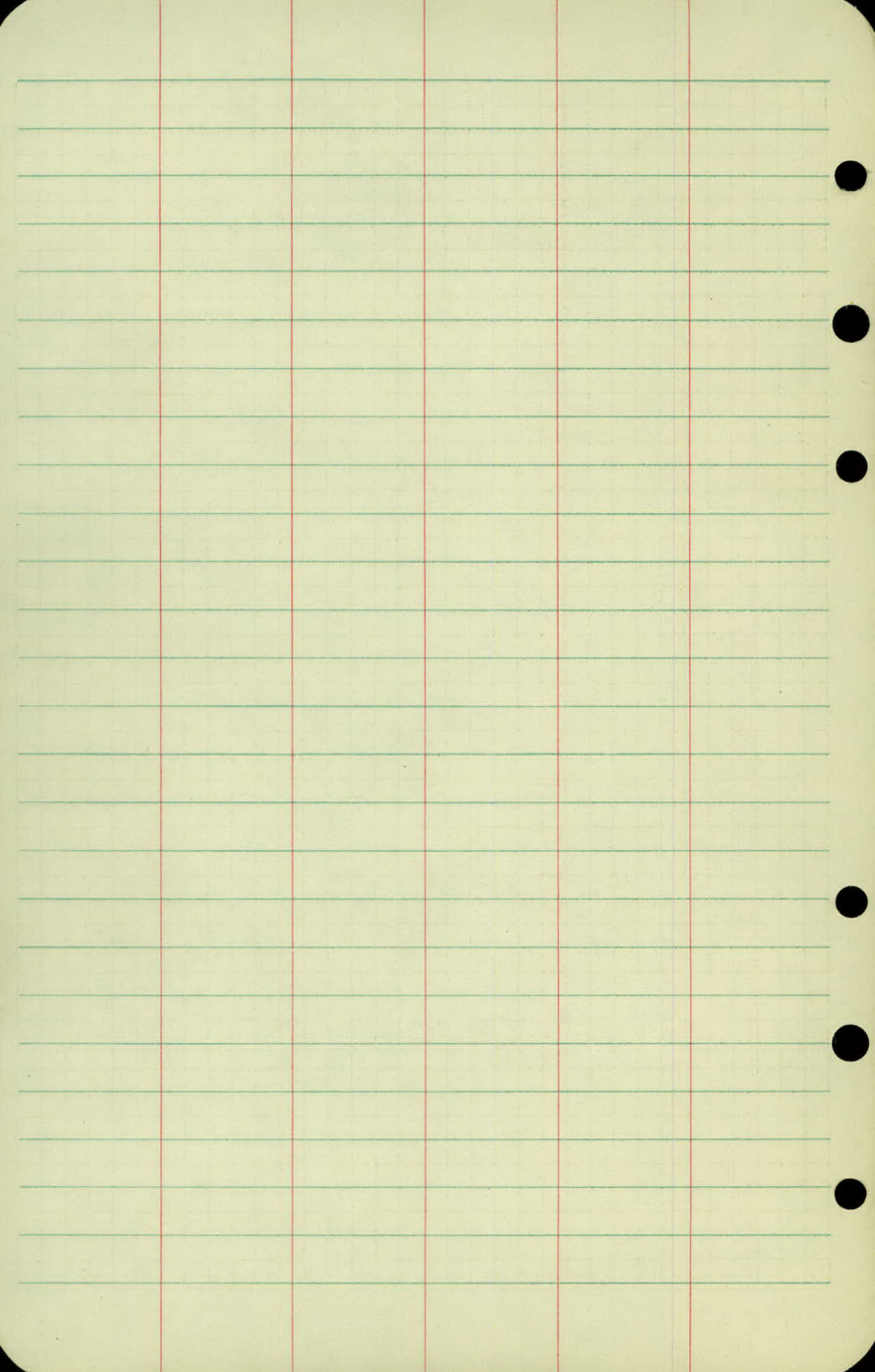
5 5 5 5
4 3 3
2 2 2 2
1 1 1 1

Lowland

5
4

1

5



Bench Levels

checked by KP

10 FEB 1960

Sta	+	π	-	Elev.
BM	5.36	927.69		922.33
TP	5.38	928.37	4.70	922.99
BM			4.68	923.69
BM			6.95	921.62 921.52
TP	3.61	920.21	11.77	916.60
TP	5.26	922.87	2.60	917.61
BM			5.18	917.69
TP	3.24	919.93	6.18	916.69
TP	5.41	917.09	8.25	911.68
BM			0.15	916.94 916.93

Iron Plug N.E. Cor Sec 32-30-22

E Co. Rd "E" $\frac{1}{2}$ Centerville Rd.

RR Spike in PP NE Cor Co. Rd. "E" $\frac{1}{2}$ Centerville Rd

Nail in PP NW Cor Koehler Rd $\frac{1}{2}$ Centerville Rd.

N.W. Cor.

Frame of steel cover plate of Dry Well 200' SW
of school

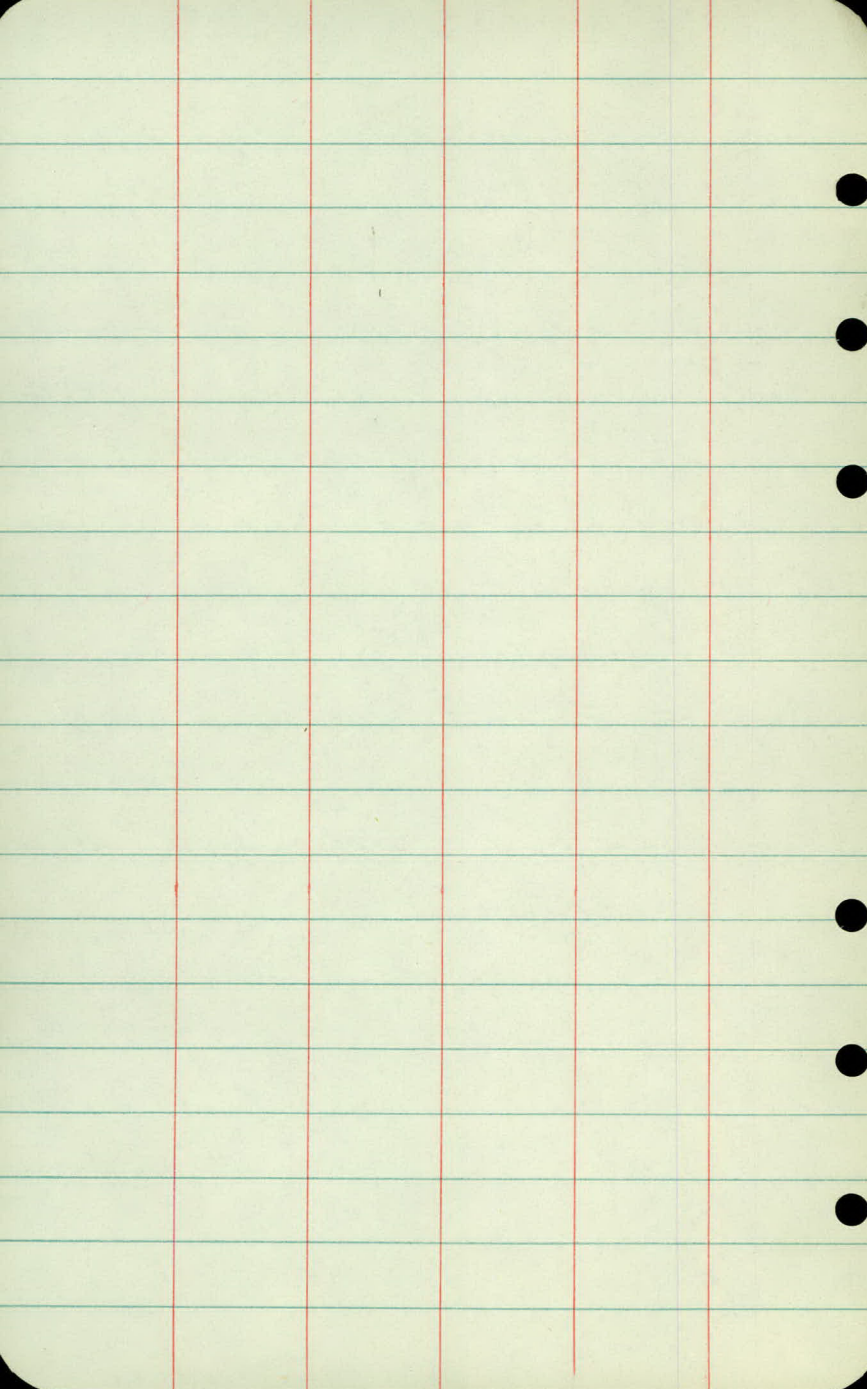
Sta 1400 Koehler Rd.

Top SW Cor. Lower Step ^{Ho. #} 677 Koehler Rd

Pt. on pavement.

Top Fe post

Spike in PP NW Cor Koehler Rd & Edgerton



x-sections

reduced & checked by KP

10 FEB 1960

Sta	+	π	-	Elev
BM	5.32	923.01		(917.69)

8+00

+13

+50

+87

TP	7.04	927.29	2.76	920.25
----	------	--------	------	--------

AK
KG
JS
JH
CW

Jan 18, 1960
Overcast Snowing 20° 10

Top S.W. Cor Lower step Hoth 677 Kessler Rd

17.5	17.2	17.5	17.1	17.5	17.6	17.8	17.8	18.5	19.1	19.9
5.5	5.8	5.5	5.9	5.5	5.25	5.2	5.2	4.5	3.9	3.6
40	49	31	17	11		7	15	31	51	75

17.6	17.3	17.3	17.2	17.6	17.9	17.9	18.0	18.8	20.8	20.8
5.4	5.7	5.7	5.8	5.4	5.1	5.1	5.0	4.2	2.2	2.2
40	50	35	17	11		7	12	19	33	41

20.8	20.7
2.2	2.3
75	64

17.4	17.5	17.2	17.9	18.1	18.0	18.1	19.3	21.4	21.9
5.6	5.5	5.8	5.1	4.9	5.0	4.9	3.7	1.6	1.1
55	34	18	10		8	12	20	27	35

21.2	21.6
1.8	1.4
71	54

17.7	17.9	17.9	17.6	18.1	18.2	18.2	18.3	20.1	21.7	22.0
5.3	5.1	5.1	5.4	4.9	4.8	4.8	4.7	2.9	1.3	1.0
55	38	27	19	7		7	11	18	28	37

17.4	21.7	21.8
5.6	1.2	1.2
75	59	

Sta + π - Elev

927.29

9+00

✓

+50

✓

10

4 Jan 18, 1960

11

Lt

Rt

17.9	18.1	17.8	18.0	18.3	18.3	18.7	21.2	24.4	23.4
9.4	9.2	9.5	9.3	9.0	9.0	8.6	6.1	2.9	3.9
49	30	19	13		8	14	22	29	41

17.9	17.6						23.3	23.2
9.4	9.7						4.0	4.1
65	75						75	52

18.7	18.3	18.0	18.2	18.4	18.3	18.7	21.1	25.7	24.9
8.6	9.0	9.3	9.1	8.8	9.0	8.6	6.2	1.6	2.9
45	29	18	9		8	15	23	31	44

19.0	18.8						24.4	24.5
8.3	8.5						2.9	2.8
63	75						75	64

18.7	18.3	18.0	18.2	18.3	18.2	18.1	18.8	21.0	24.1
8.6	9.0	9.3	9.1	9.0	9.1	9.2	8.5	6.3	3.2
41	28	18	11		7	12	24	29	35

19.2	18.4						23.4	23.4
8.1	8.9						3.9	3.9
61	75						75	64

Sta	+	π	-	Elev
-----	---	-------	---	------

		927.29		
--	--	--------	--	--

10 + 25				
---------	--	--	--	--

✓				
---	--	--	--	--

+ 34				
------	--	--	--	--

✓				
---	--	--	--	--

+ 48				
------	--	--	--	--

Jan 18, 1960 12

19.1	18.4	18.0	18.1	18.2	18.0	18.0	18.8	20.4	23.4
8.2	8.9	9.3	9.2	9.1	9.3	9.3	8.5	6.9	3.9
47	28	18	10		9	13	23	27	33

19.0	19.5	22.1	22.4
8.3	7.8	5.2	4.9
64	75	25	53

21.9	19.8	17.9	18.1	18.2	18.0	18.3	19.4	20.8	23.2
5.4	7.5	9.4	9.2	9.1	9.3	9.1	7.9	6.5	4.1
33	27	17	9		10	17	25	28	34

25.2	25.6	25.5	25.1	21.3	21.9
2.1	1.7	1.8	2.2	6.0	5.4
41	55	66	75	75	56

21.7	19.4	18.4	17.8	17.9	18.1	18.0	17.9	19.5	18.8	19.0
5.6	7.9	8.9	9.5	9.4	9.2	9.3	9.4	7.8	8.5	8.3
34	26	21	13	9		10	16	25	30	43

24.5	24.8	24.6	24.2	20.7	21.9
2.8	2.5	2.7	2.1	6.6	5.4
39	54	66	75	75	51

Sta + π - Elev

927.29

10 + 76

✓

11

✓

TP 2.28 917.91 11.66 915.63

+16

✓

Jan. 18, 1960

13

LT

RT

21.3	20.9	18.3	17.5	17.5	17.9	17.8	17.6	17.5	17.8
6.0	6.4	9.0	9.8	9.8	9.4	9.5	9.7	9.8	9.5
53	37	27	17	10		11	18	27	38

21.6 21.0

19.1 19.7 20.1 18.6

5.7 6.3
66 75

8.2 7.6 7.2 8.7
75 64 49 46

16.9	16.7	16.9	17.2	17.6	17.7	17.5	17.1	17.40
10.4	10.6	10.4	10.1	9.7	9.6	9.8	10.2	9.89
37	24	18	10		9	7	30	Conc 38

17.2 17.7 17.6

17.3 17.3 17.4

10.1 9.6 9.7
53 67 75
P.L. East Spike

10.0 10.0 9.9
93 75 46
140

14.7 15.0 16.2 17.0 17.4 17.5 17.4 17.3 16.4

3.2	2.9	1.7	0.9	0.5	0.4	0.5	0.6	1.5
49	31	18	11		8	18	27	33

15.4 16.2

14.5 15.2 16.0

2.5 1.7
60 75

3.4 2.7 1.7
75 58 46

sta + π - Elev

917.91

11 + 50

✓

12

✓

+13

✓

Jan 18, 1960

14

1	2	3	4	5	6	7	8	9	10
2.7	2.9	5.5	6.5	17.0	17.0	16.6	15.8	14.7	13.6
5.2	5.0	2.4	1.4	0.9	0.9	1.3	2.1	3.2	4.3
40	30	21	14		7	19	25	41	63

13.0	13.1				13.2
→ 4.9	4.8				4.7
59	75				75

11.7	11.9	15.7	16.2	15.9	15.8	15.0	12.9	12.1
6.2	6.0	2.2	1.7	2.0	2.1	2.9	5.0	5.8
60	13	26	13		2	7	13	23

$\begin{matrix} 12.0 \\ \rightarrow 5.9 \\ 75 \end{matrix}$

11.6	15.4	16.0	15.7	15.4	11.6	10.3	09.2	07.8
6.3	2.5	1.9	2.2	2.5	6.3	7.6	8.7	10.1
49	33	20	7		11	24	53	75

$\frac{11.3}{66}$	$\frac{11.5}{75}$
-------------------	-------------------

Sta + π - Elev

917.91

12+36

✓

+50

✓

+77

✓

2 Jan 18, 1960

15

$\begin{matrix} 15.2 & 15.8 & 15.3 & 13.3 & 11.4 & 10.2 & 08.7 & 07.5 & 07.0 \\ 27 & 21 & 26 & 46 & 6.5 & 7.7 & 9.2 & 10.4 & 10.9 \\ 45 & 30 & 12 & 6 & 15 & 40 & 34 & 61 \end{matrix}$

$\begin{matrix} 12.9 & 12.5 & 11.1 \\ 5.0 & 5.4 & 6.8 \\ 62 & 72 & 80 \end{matrix}$

$\begin{matrix} 05.2 & 05.7 \\ 12.7 & 12.2 \\ 75 & 66 \end{matrix}$

$\begin{matrix} 15.2 & 15.6 & 15.2 & 15.0 & 11.2 & 10.5 & 09.5 & 07.2 & 06.7 & 06.2 \\ 27 & 23 & 27 & 29 & 6.7 & 7.4 & 8.4 & 10.7 & 11.2 & 11.7 \\ 53 & 40 & 26 & 20 & 9 & 18 & 44 & 49 & 55 \end{matrix}$

$\begin{matrix} 14.2 & 10.9 \\ 3.7 & 7.0 \\ 63 & 75 \end{matrix}$

$\begin{matrix} 04.6 & 04.9 \\ 13.3 & 13.0 \\ 75 & 66 \end{matrix}$

$\begin{matrix} 15.5 & 14.9 & 10.2 & 08.8 & 07.9 & 06.9 & 06.4 & 05.0 & 04.1 \\ 24 & 30 & 7.7 & 9.1 & 10.0 & 11.0 & 11.5 & 12.9 & 13.8 \\ 51 & 33 & 20 & 12 & 19 & 27 & 42 & 60 \end{matrix}$

$\begin{matrix} 15.1 & 12.5 \\ 2.8 & 5.4 \\ 65 & 75 \end{matrix}$

$\begin{matrix} 03.3 \\ 14.6 \\ 75 \end{matrix}$

Sta + X - Elev

917.91

13

TP 5.44 913.67 9.68 908.23

13

+42

+68

14

+50

Jan 18, 1960 Rt 16

15.3 15.4 14.5 10.6 09.7 08.2 05.8
 2.6 2.5 3.4 7.3 8.2 9.7 12.1
 75 70 51 38 19 18
 Sta 13 spike &

03.8 03.1 01.7 01.9
 9.9 10.6 12.0 11.8
 33 50 68 75

09.8 08.3 06.8 04.5 02.1 01.4 01.3 01.2
 3.9 5.4 6.9 9.2 11.6 12.3 12.4 12.5
 75 59 38 19 21 47 75

06.8 06.2 04.8 03.0 01.9 01.4 01.1 01.1 01.1 01.2
 6.9 7.5 8.9 10.7 11.8 12.3 12.6 12.6 12.6 12.5
 75 65 53 35 18 20 44 58 75

03.7 02.6 02.2 01.9 02.0 01.9 01.4 01.4 01.4
 10.0 11.1 11.5 11.8 11.7 11.8 12.3 12.3 12.3
 75 62 48 32 16 27 52 75

03.1 02.7 02.5 02.4 02.0 01.3 02.1 02.1 02.2
 10.6 11.0 11.2 11.3 11.7 11.4 11.6 11.6 11.5
 75 58 42 24 21 46 64 75

Sta + Δ - Elev

913.67

14+80

15

+50

TP 11.89 925.00 0.56 913.11

16

+37

25

23

41

+62 Top Back slope

Jan 15 1960 17
BT

05.0	04.6	04.1	03.9	03.5	03.2	03.3	02.8	02.5	02.5
8.7	9.1	9.6	9.8	10.2	10.5	10.4	10.9	11.2	11.2
75	68	55	35	17		21	48	68	75

05.6	05.1	05.3	05.0	04.6	04.4	04.3	03.7	03.1	03.5
29	8.0	8.4	8.7	9.1	9.3	9.4	10.0	10.6	10.2
75	67	52	32	14		24	49	59	75

08.6	08.7	08.9	09.0	09.1	09.0	09.3	09.4	09.2	09.4
5.1	5.0	4.8	4.7	4.6	4.7	4.4	4.3	4.5	4.3
75	64	49	32	13		22	39	61	75

14.3	14.2	14.0	13.9	14.4	14.1	14.2	14.3	13.8
10.7	10.8	11.0	11.1	10.6	10.9	10.8	10.7	11.2
75	53	36	16		23	45	63	75

19.7	19.7	19.6	19.1	19.1	18.9	18.4	18.0	17.4	17.2
5.3	5.3	5.4	5.9	5.9	6.1	6.6	7.0	7.6	7.8
75	64	51	30	16		22	43	60	75

20.7	21.1	21.1	21.2	21.3	21.2	21.3	21.0	21.3
4.3	3.9	3.9	3.8	3.7	3.8	3.7	4.0	3.7
75	51	32	12		21	45	64	75

Sta + π - Elev

925.00

16+70 $\pm$ Ditch

✓

78
+75

17.20

2.80

+78 Shoulder

493.97 $\pm$ Centerville Rd

17+19

6.23 918.27

BM

1.30 923.70 (923.69)

1

Jan 18, 1960

14	15	16	17	18	19	20	21	22
17.9	18.9	18.6	18.9	18.8	18.9	19.2	18.9	18.6
21	6.1	6.4	6.1	6.2	6.1	5.8	6.1	6.4
52	45	32	15		19	40	60	25

14	15
18.0	17.9
7.0	7.1
67	75

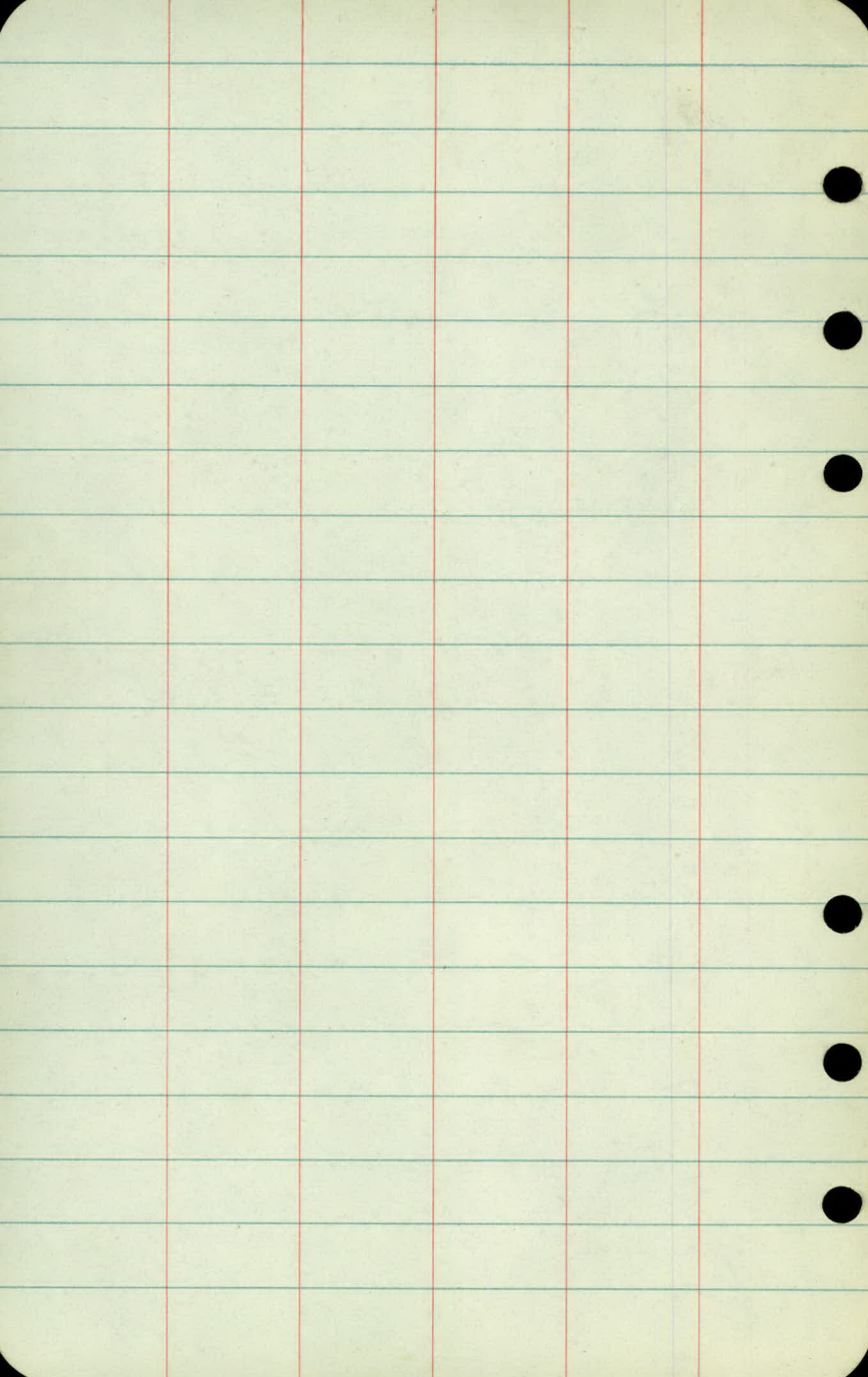
EL 24 SCP 49' LT

16	17	18	19	20	21	22	23	24
23.2	23.0	22.8	22.9	22.8	22.7	22.5	22.4	22.4
1.8	2.0	2.2	2.1	2.2	2.3	2.5	2.6	2.6
75	60	40	20		24	47	68	75

16	17	18	19	20	21	22	23	24
23.4	23.3	23.2	23.1	23.0	22.9	22.8	22.7	22.5
1.6	1.7	1.8	1.9	2.0	2.1	2.2	2.3	2.5
100	75	50	25		25	50	75	100

EE 24" SCP 57' LT

RR Spike in PP NE Cor Cor'd E' Centerville



CA
RG
JS
JL
JH

March 29, 1960
cloudy 500

19

Borrow Pit

x-sections

Sta + π - Elev.

BM 3.53 920.13

916.60

0+00

✓
1543

✓

+50

1

+50

2

March 29, 1960

20

N.W. Cor

Lt

Rt

200' S.W. of School

Frame of Steel Cover plate of Dry Well

12.2	14.8	15.4	15.9	15.63	15.0	11.8	9.8
79	53	47	42	45	51	83	103
33	26	20	9		8	16	32

→ 9.0
46

10.4	11.4	14.6	15.5	15.2	14.9	10.8	9.5
9.7	8.7	5.5	4.6	4.9	5.2	9.3	10.6
49	37	26	11		8	18	33

11.3	13.5	14.1	15.3	14.9	13.9	10.7	9.2
8.8	6.6	6.0	4.8	5.2	6.2	9.4	10.9
47	35	29	11		8	17	32

10.7	11.1	14.5	15.2	14.4	13.7	10.8	8.6
9.4	9.0	5.6	4.9	5.7	6.4	9.3	11.5
53	39	28	14		4	12	29

14.1	14.9	15.1	14.5	13.7	13.3	11.2	8.6
6.0	5.2	5.0	5.6	6.4	6.8	8.9	11.5
32	29	15	4		4	9	29

Sta + π - Elev.

920.13

2+00

+50

3

+50

+73 W. Edge Ent

A

Culvert Possible Sta 2+80

March 29, 1960 21

11

RT

11.6 12.0 11.3
8.5 8.1 8.8
61 46 40

✓

12.0 12.1 14.2 15.1 15.2 14.3 13.4 9.9 7.9
8.1 8.0 5.9 5.0 4.9 5.8 6.7 10.2 12.2 ✓
58 39 33 26 12 5 15 33

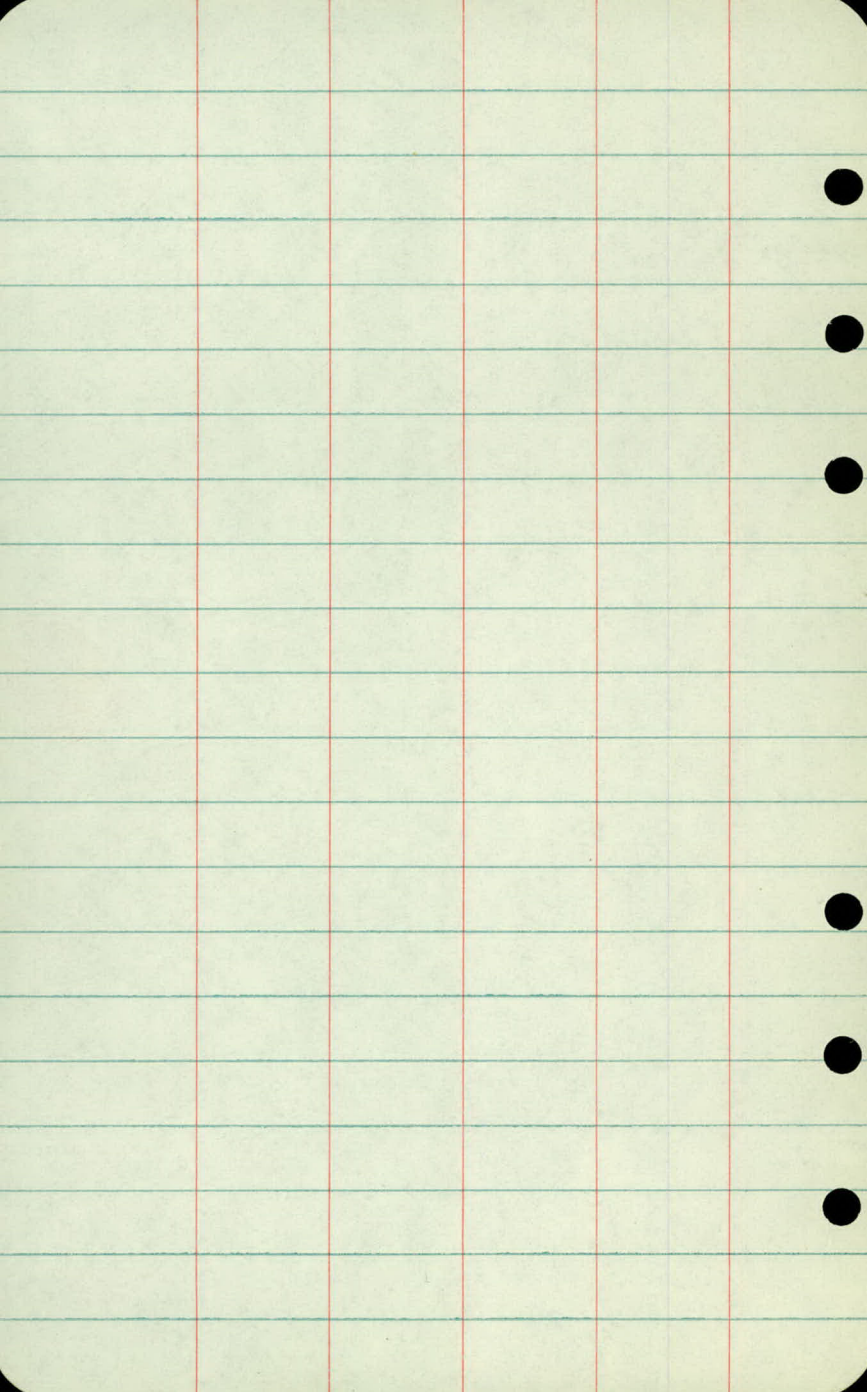
12.5 12.3 15.5 16.0 15.2 14.4 10.3 7.5
7.6 7.8 4.6 4.1 4.9 5.7 9.8 12.6 ✓
49 30 23 15 10 21 44

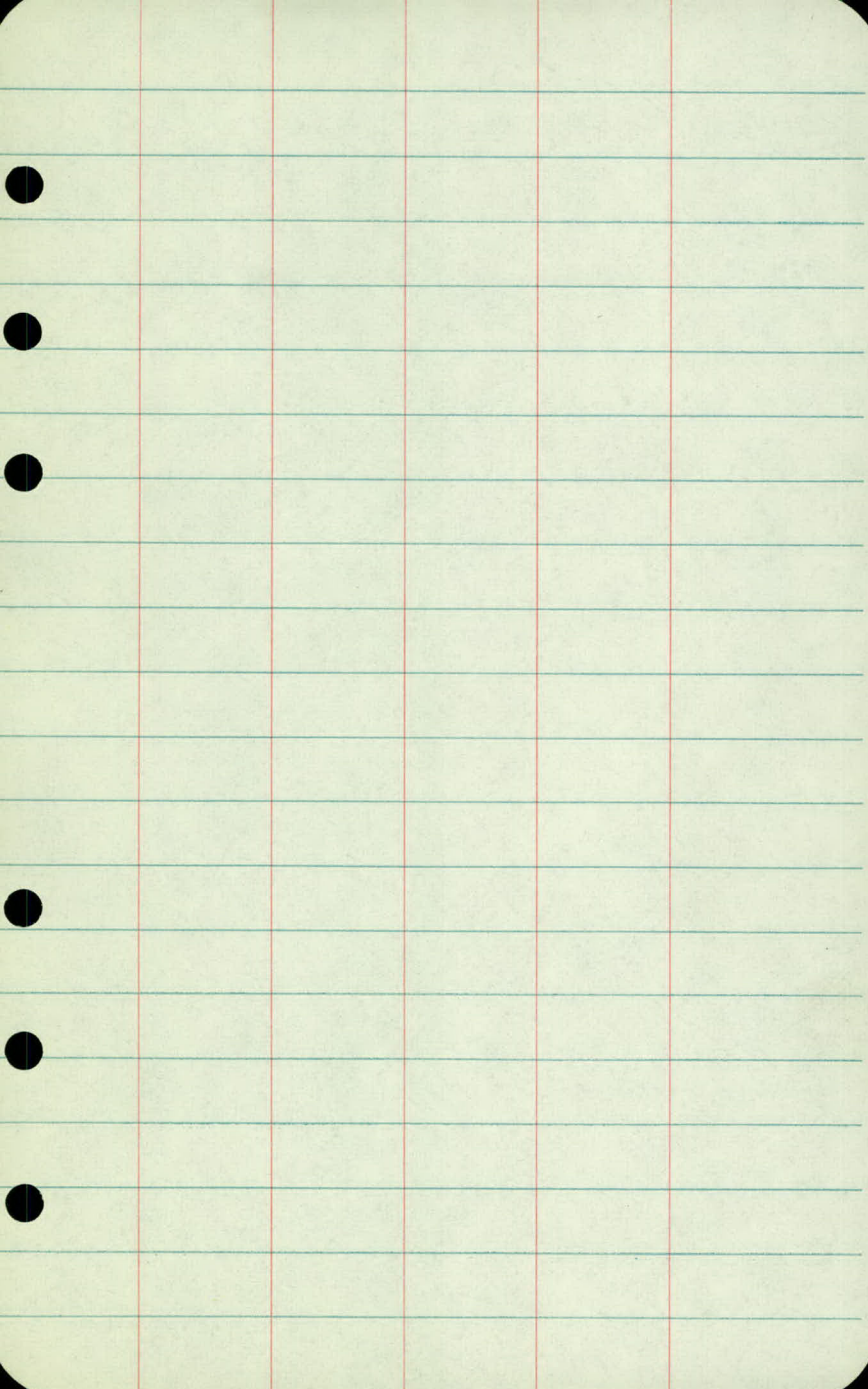
13.5 14.3 15.7 16.4 16.7 16.0 14.9 11.4 9.3
6.6 5.8 4.4 3.7 3.4 4.1 5.2 8.7 10.8
45 20 12 4 19 31 43 63

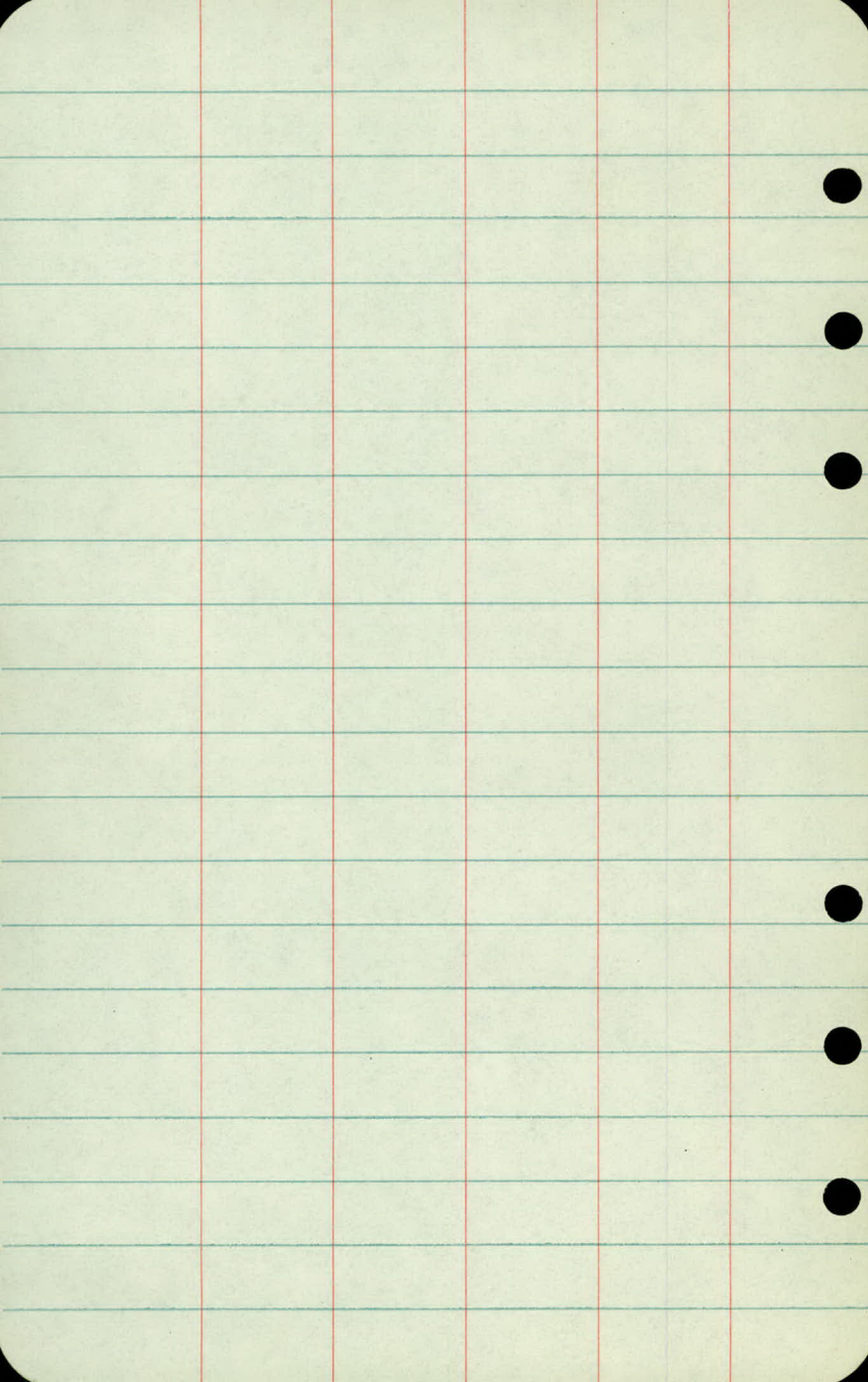
14.8 15.1 16.9 16.9 14.2 16.4 15.3 11.4 10.3
5.3 5.0 3.2 3.2 2.9 3.7 4.8 8.7 9.8
36 12 7 18 32 44 64 87

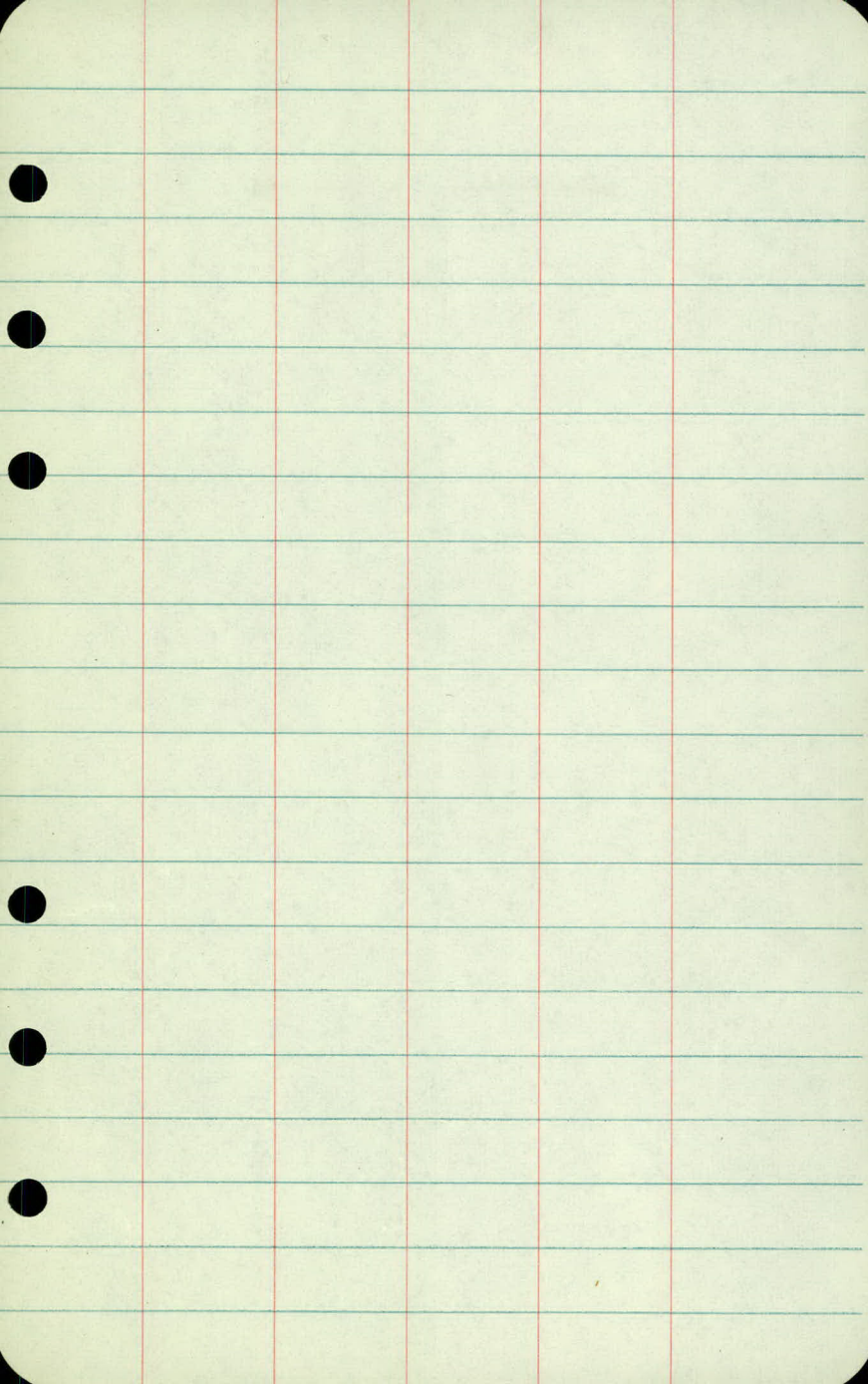
18.39

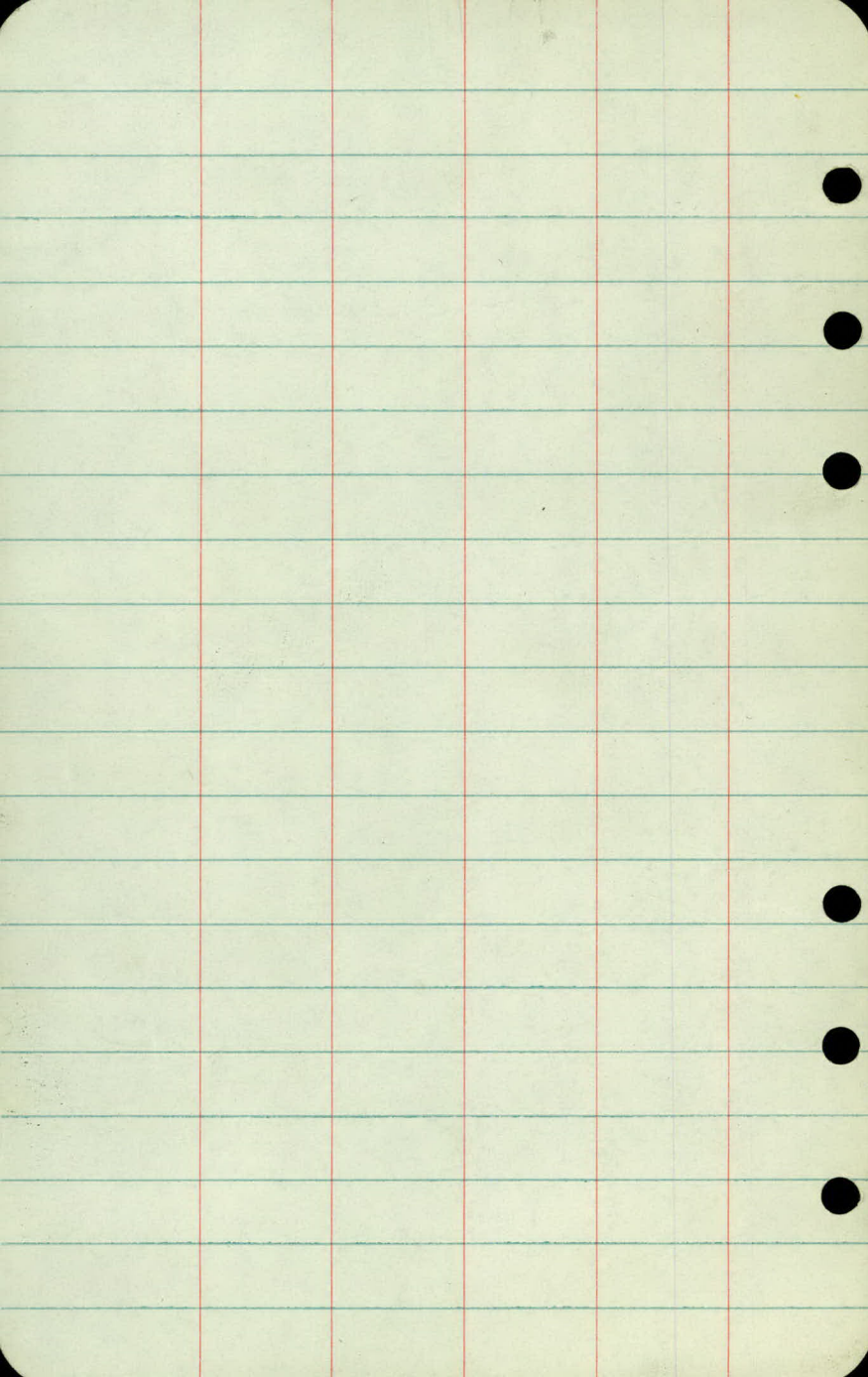
1.74











K.P.
J.S.
FLORANU, SULLIVAN
R.B.
L.B.

7 NOV. 1960
clear, cold, 23°
windy 1.

Koehler Road

OLD. Road EXCAVATION

FINAL X-SECTION

Sta	+	π	-	ELEV.
BM	1.04	917.64		916.60
0+00				
✓				
+50				
✓				
1+00				
✓				
TP	3.62	917.02 917.33	3.93	913.71 913.40

7 NOV. 1960

2.

LT

≠

RT

Cover plate of Dry Well 200' SW School

12.5	12.3	13.3	14.1	14.9	13.8	11.0	67.3
5.1	5.3	4.3	1.5	2.7	3.8	6.6	10.3
75	44	25		20	36	46	62

048

12.8
75

10.6	11.8	11.4	11.8	11.9	12.0	14.7	13.9	12.6
NG								
7.0	5.8	6.2	5.8	5.7	5.6	2.9	3.7	5.1
48	34	24	15		12	27	47	70

11.2
6.4
75

12.0	11.6	11.3	09.7	10.1	09.7	08.1
NG						
5.6	6.0	6.3	7.9	7.5	8.4	9.5
46	36	17		13	28	45

13.1
5.4

10.4

4.5 72
72 59

Spike in PP 8.0 RT 2400

Sta

+

π

-

ELEV

917.02
917.33

1+50

✓

2+00

1

2+50

3+00

3+50

7 NOV. 1960

3

LT

E

RT

108

NG

11.7 10.6 09.7 08.7 06.1 04.5

6.2	5.8	6.4	7.3	8.3	10.9	12.5
45	30	13		18	37	51

03.7 03.7

13.8 13.8
75 70

11.7

NG

11.7 11.1 10.0 09.6 08.4 06.9 04.7

5.8	5.3	5.9	7.0	7.4	8.6	10.1	12.8
42	37	29	14	✓ 17	37	57	

12.3

NG

11.8 10.8 10.7 9.3 07.9 06.8 05.2

4.7	5.2	6.2	6.8	7.7	9.1	10.7	11.8
49	41	29	14	✓ 18	35	46	

12.0

NG

11.5 10.7 09.9 08.5 08.4 08.0 07.1

5.0	5.5	6.3	7.1	8.5	8.6	9.0	9.9
40	27	14	✓ 18	31	39	50	

13.5

NG

14.0 13.4 13.0 13.7 11.9 10.4 09.9

3.1	3.0	3.6	4.0	3.8	5.1	6.6	7.1
31	22	12	✓ 16	30	47	61	

+

K

-

4+00

$$\begin{array}{r} 917.02 \\ 917.93 \end{array}$$

BM 8.66 ~~925.61~~ ^{0.38} 0.38 916.64 ⁶⁴ 916.60

~~.21~~
~~925.26~~ 11.87 ~~913.74~~
 913.39

BM 8.67 925.27 916.60

11.87 913.40

BM 1.54 923.73 923.69

4+00

+50

5

+25 No change

BM 1.54 923.73 923.69

L+

7 NOV. 1960

RT

4.

16.4	11.0	09.9	10.3
0.4	6.0	7.1	6.7
	<u>14</u>	<u>29</u>	<u>45</u>

Top Dry Well

SPike in pp 8.0 RT Sta 2+00

TOP DRY WELL

SPike in pp. 8.0 RT STA 2+00

SPike in pp. N.E. Cor Cord E. Cent. Rd.

17.1
old rd.

8.3

2

18.5
old rd

✓ 6.8
3.0

21.3
old rd

✓ 4.0

17.0

8.3

21.2

4.1

13.5

11.8

18.8

6.5

12.8

12.5

± ditch 18.0

7.3

12.4

NG

12.9

41

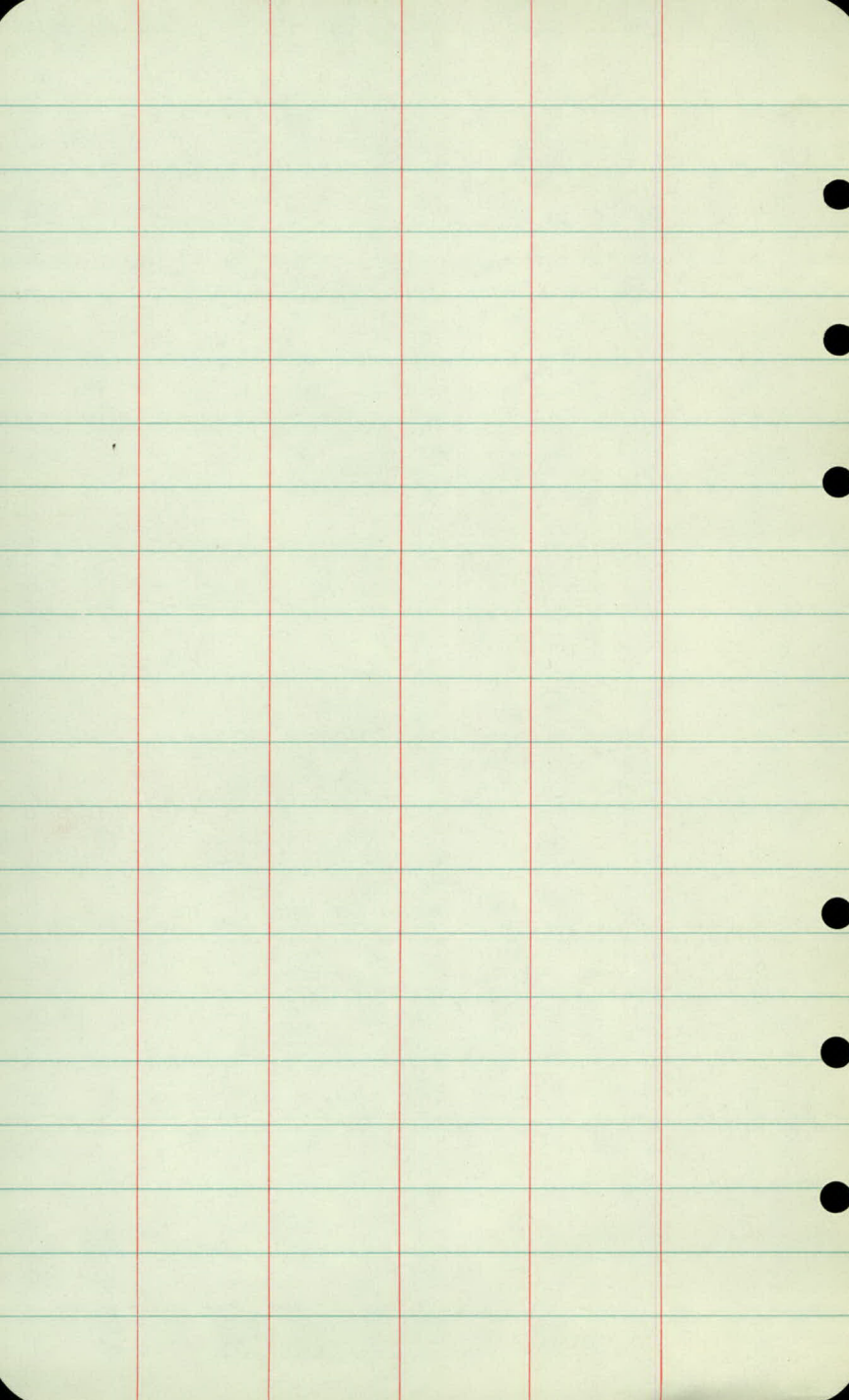
18.5

NG

6.8

41

SPike in P.P. N.E. Cor E. Cent Rd.



KP
US
JH
RB
LB.

3 NOV. 1960
Sunny, Cool 30°

1.

Koehler Road
Borrow P.T (Final x-sections)
at 3790 McMenemy

5 pages.

Sta	+	π	-	ELEV.
BM	9.12	942.11		932.99

0+00

+50

✓

1+00

✓

+33

#

2.

RT.

SPIKE IN P.P. BY #3822 McMenamy.

NO CHANGE

33.8	31.9	31.4	30.7	30.6	30.7	30.3
8.3	10.2	10.7	11.4	11.5	11.4	11.8
	21	46	73	92	100	112

✓

30.0

NG

12.1

124

36.6	33.4	30.9	31.2	31.2	31.0	31.0
5.5	8.7	11.2	10.9	10.9	11.1	11.1
	13	26	45	71	95	100

✓

30.1

NG

30.4

30.6

12.0

11.7

11.5

144

136

122

39.3	34.8	30.7	31.0	31.2	31.0	30.5	30.4	29.5
2.8	7.3	11.4	11.1	10.9	11.1	11.2	11.7	12.6
	15	29	50	71	92	121	134	147

✓

29.0

NG

13.1

153

Sta

+

π

-

ELEV.

942.11

1764

✓

2+00

✓

+50

✓

4

3.

RT

39.6	36.7	33.1	30.4	30.9	31.0	30.8	30.9	31.7
2.5	5.4	9.0	11.5	11.2	11.1	11.3	11.2	11.4
10	21	30	48	70	92	100	123	

✓

28.9 29.8

NG

13.2 12.3

153 141

38.4	35.7	37.9	30.9	30.3	30.5	30.6	30.7
3.9	6.4	9.2	11.2	11.8	11.6	11.6	11.4
12	21	28	34	54	74	96	

✓

25.4 26.8 28.4 29.9 30.5

NG

16.7 15.3 13.9 12.2 11.5

200 183 169 147 123

35.4	32.9	30.7	29.9	30.1	29.9	29.9	29.9
6.9	9.2	11.4	12.2	12.0	12.2	12.2	12.2
18	27	37	64	86	100	123	

✓

26.8 29.1 29.4 29.4

15.5 13.3 13.0 12.9 12.7

235 213 200 188 159

Sta	+	π	-	ELEV.
-----	---	-------	---	-------

		942.11		
--	--	--------	--	--

3+00				
------	--	--	--	--

✓				
---	--	--	--	--

TP	2.16	932.53	11.74	930.37
----	------	--------	-------	--------

3+50				
------	--	--	--	--

✓				
---	--	--	--	--

+82				
-----	--	--	--	--

✓				
---	--	--	--	--

3 NOV 1960

4.

RT

301	295	299	298	296	295	290
12.0	12.6	12.2	12.3	12.5	12.6	13.1
	22	46	68	93	100	128

✓

26.8	28.4	28.1	28.9	28.9
------	------	------	------	------

15.3	13.7	13.4	13.2	13.2
254	227	200	183	155

TOP ROCK 20' RT STA 3+03

27.1	28.1	28.9	29.7	28.6	28.5	28.4	28.0
5.4	4.4	3.6	3.3	3.9	4.0	4.1	4.5
	32	54	69	100	131	157	185

✓

24.5	23.5	25.3	26.9
------	------	------	------

7.9	8.9	7.2	5.6
255	236	219	200

26.1	26.3	27.8	28.4	28.2	27.9	27.9	27.9
6.4	6.2	4.7	4.1	4.3	4.6	4.6	4.6
	20	40	66	91	100	128	153

✓

21.7	22.2	24.7	27.6
------	------	------	------

10.8	10.3	7.8	4.9
210	200	183	168

Sfa	+	π	-	ELEV.
		932.53		

4+00

✓

+26 Toe slope

✓

12.14 939.63 5.04 927.49

BM 6.62 933.01 932.99

3 Nov. 1960

5.

≠

RT

25.1	25.4	26.3	27.3	27.3	27.3	27.7	26.5
7.4	7.1	6.2	5.2	5.2	5.2	5.3	6.0
	21	46	66	90	100	127	148

✓

20.7	21.3	23.4
NG		
11.8	10.2	8.9
191	180	166

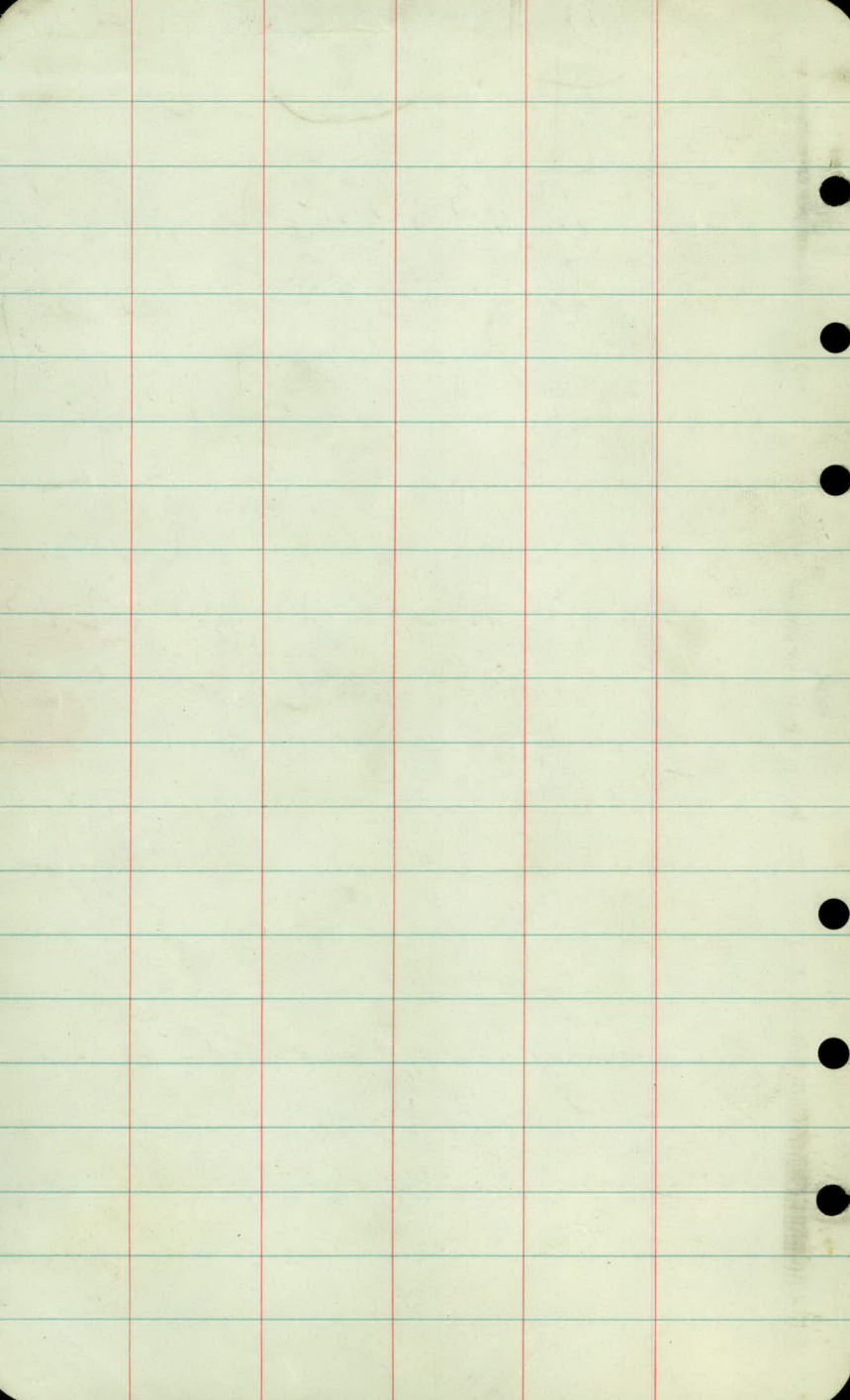
23.9	23.9	23.9	24.9	24.8	21.3	20.7	20.3
8.6	8.6	8.6	9.6	10.7	11.2	11.8	12.2
	21	43	59	82	100	129	156

19.4 ✓

13.3
179

E. Corner Fireplace Bldg. behind
10#3814 McMenemy.

Spike in P.P. by 3822 McMenemy



Kohler Road

Drainage

from Co Rd E at

Centerville Road

4+30.05

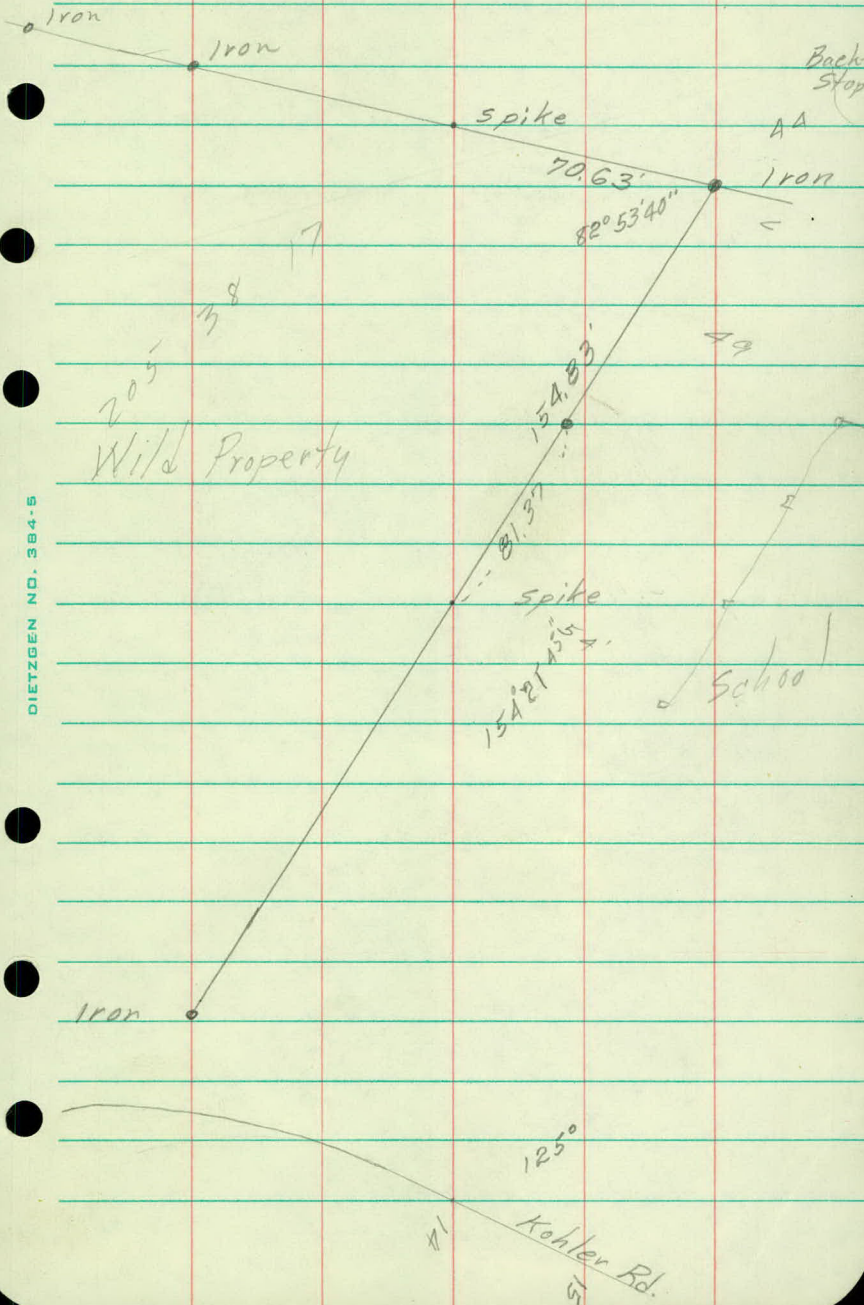
2+68.10 P.O.T.

0+00 = Sta 1A Kohler Road

FK
RJ
EY

Oct. 14, 1976

2



88 45 40

44 22 50

88 45 40

86 37 21

173 74 27

86 37 27

132.86

63.00

69.86

14100.00

2.80

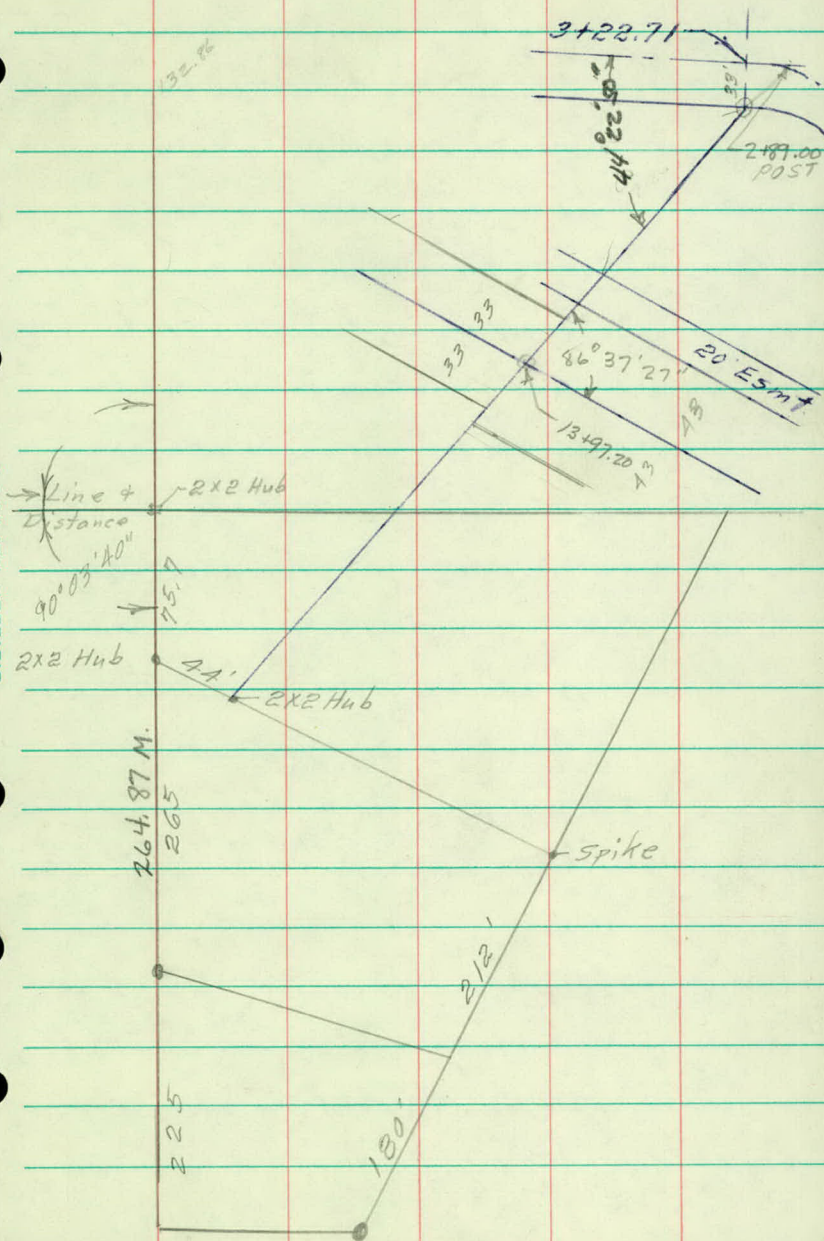
1397.20

5

5

5

5



$$936 \overline{) 7051} \begin{array}{r} 66000 \\ 6552 \end{array}$$

$$4.18 \quad .0048$$

$$\begin{array}{r} 4800 \\ 4680 \\ \hline 1200 \end{array}$$

$$.0044 \quad 378$$

$$2.89 \quad 3.19$$

$$101.79$$

$$200$$

$$301.79$$

$$300.32$$

$$1.47$$

$$1.5427$$

$$69$$

$$1.74$$

$$179 \ 59 \ 60$$

$$90 \ 18 \ 30$$

$$89 \ 41 \ 30$$

$$1.35$$

$$15 \ 54$$

$$32 \ 57$$

$$57$$

$$78$$

$$24 \ 90$$

$$17 \ 90$$

$$8.01$$

$$89 \ 97$$

$$98 \ 37$$

$$88 \ 41$$

$$56'$$

$$2$$

$$1.68/100'$$

$$19 \ 1/100$$

$$57$$

J.A.
D.S.
BL
BW

68.19 IRON
54.20 SPIKE
4

A
N

4.62' IRON

9+60.63

3.42' IRON

9+85.63

2.86' IRON

6+64.33

6.27'

3+63.00

IRON

X
Fe
Post

301.79 M

SPIKE

3+54.11

Kohler

Rd

2+94.91

SPIKE

5.06'

3.34'

IRON

2+80.85

89° 37' 30" P
90° 37' 30" M

2x2 Hub

0+00

Random Line

95 52 10
191 44 20
10

95 52 10
3 3
288 36 30
287 36 20

90 24 52
2 - 180 49 45
1 - 90 24 50
3-63.00
48.37
411.37

90 25 18
180 50 36
180 49 50
46
23
90 24 55

180 50

90 23 78
90 24 55
23

270 73 90
180 49 50
90 24 40
90 27 15
3 271 74 30

270 73 90
180
90 23 56

J.A.
D.S.
B.L
B.W
F.K.

10-22-76

5

A
N

Placed.
SPIKE

Core Lots
3, 4, & 7

IRON • 0.50'

9+60.63

IRON

10.00' - IRON

7+85.63

0.04'
IRON

LEANING
OVER

Approx location
IRON • 0.92--

Wild

Property

IRON • 5.66'

6+64.33

HO #

GAR

S.E. COR

71.73

IRON P.O.T

4+11.36

IRON • 4.62'

3+63.00

1.38' SPIKE

3+54.11

95° 52' 15"

Kohler

PK STA 7+33.55

Rd.
PI
6+14.35

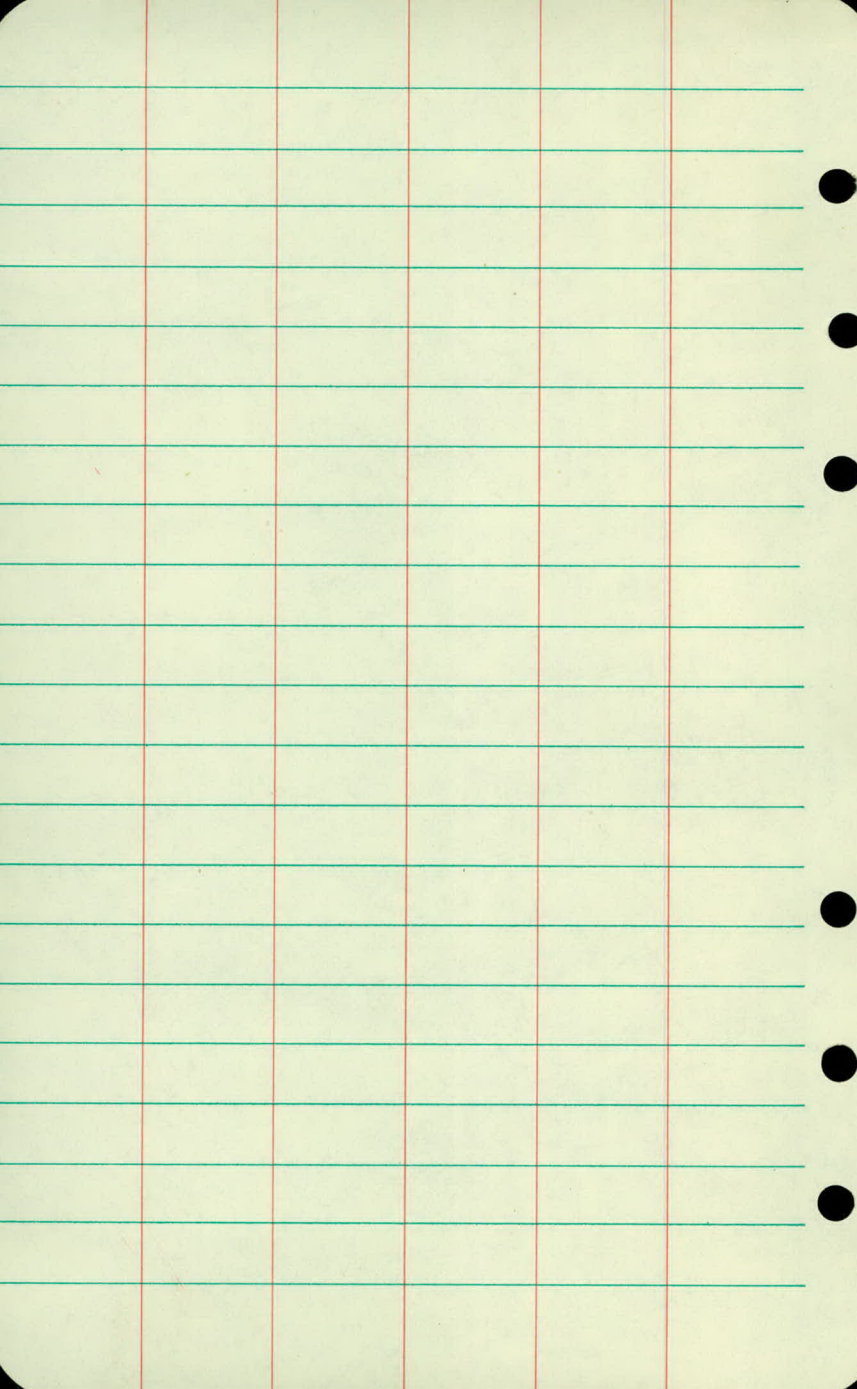
4.50' IRON

2+80.85

90° 24' 52"

2x2 Hub

0+00



J.A.
D.S.
B.L.
B.W

10-22-76
CLR 400

6

A
N

30.15

40

44

PK

Kohler Rd

PK @ Kohler
& Centerville

DIETZGEN NO. 384-5

