

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

LEXINGTON AVE.

From C2 To D

Road Acc't. No. _____

Date Filed 1-6-60

File Dr. 9 Bk 22

Lexington

"C 2" to "D"

New Curve Data

Sta Point ΔL ΔRt

2. 3.

+43.83 PT

5 New Data

+50 $\Delta = 31^\circ 49'$

4 $D = 6^\circ \text{ Arc}$ $\Delta = 31^\circ 51 \frac{3}{4}'$

+50 $T = 272.17$ $D = 6^\circ \text{ Arc}$

3 $L = 530.28$ $T = 272.58$

+85.38 P1 $R = 954.93$ $L = 531.04$

+0.34

+85.72 New P.I. $R = 954.93$

+50 $01.8' / 5'$

2 $1^\circ 30' / 50' = 30'$

+50 $100' = 99.95'$

1

+50

+13.55 P.C.

FA
JL
WM
RL

June 27, 1960

1

127 16
95 27
31 49
105 38 30
31 47
31 47 30
31 49 00

50.14
19.80

Punch hole
End Culv. "

.34

PP 0

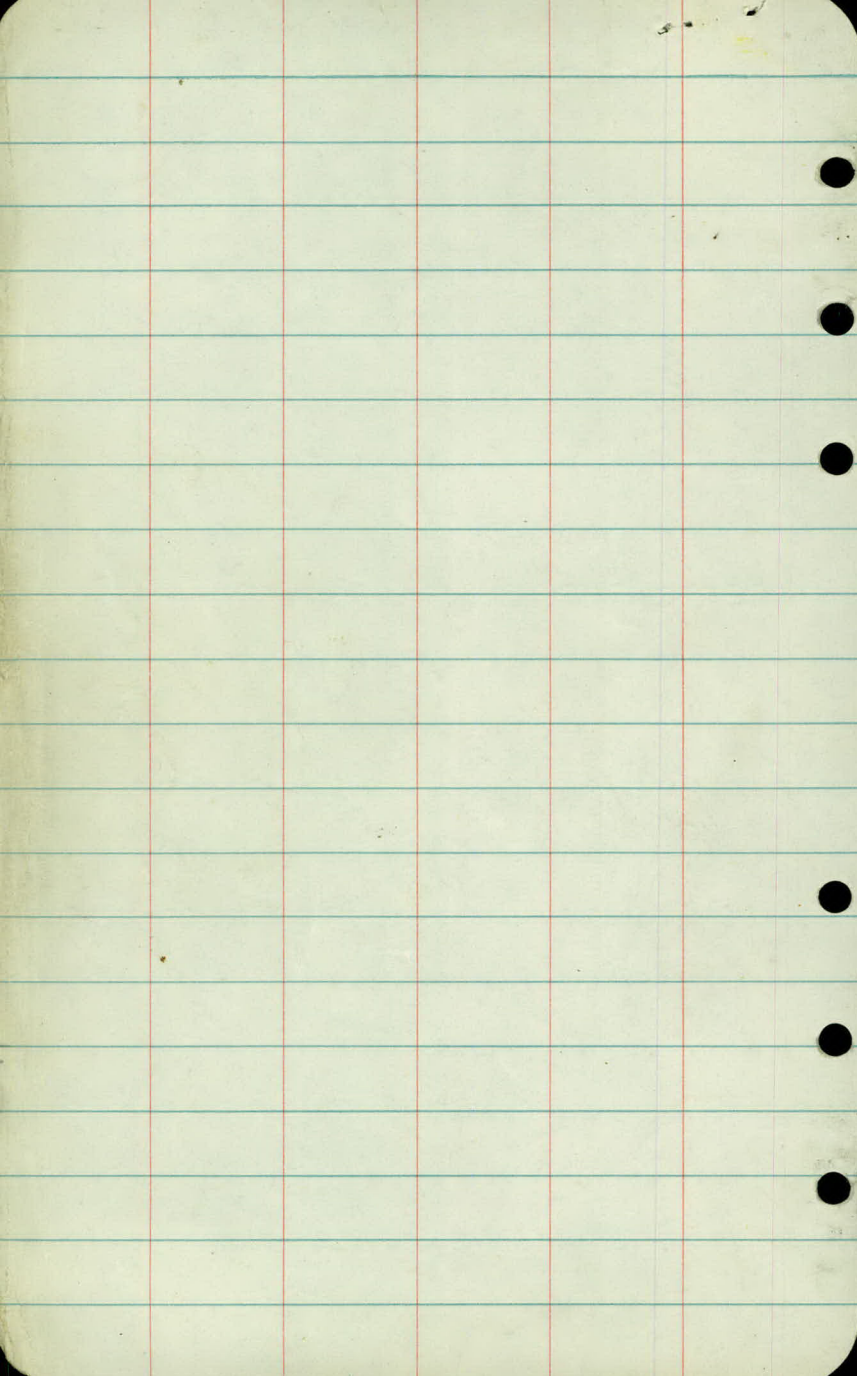
85.24

58.36

Punch hole
End Culverts

60.66

PK Nail



PLAN

Survey

LEXINGTON AVE.

Josephine Rd to Brecken Ave.

Brecken Ave

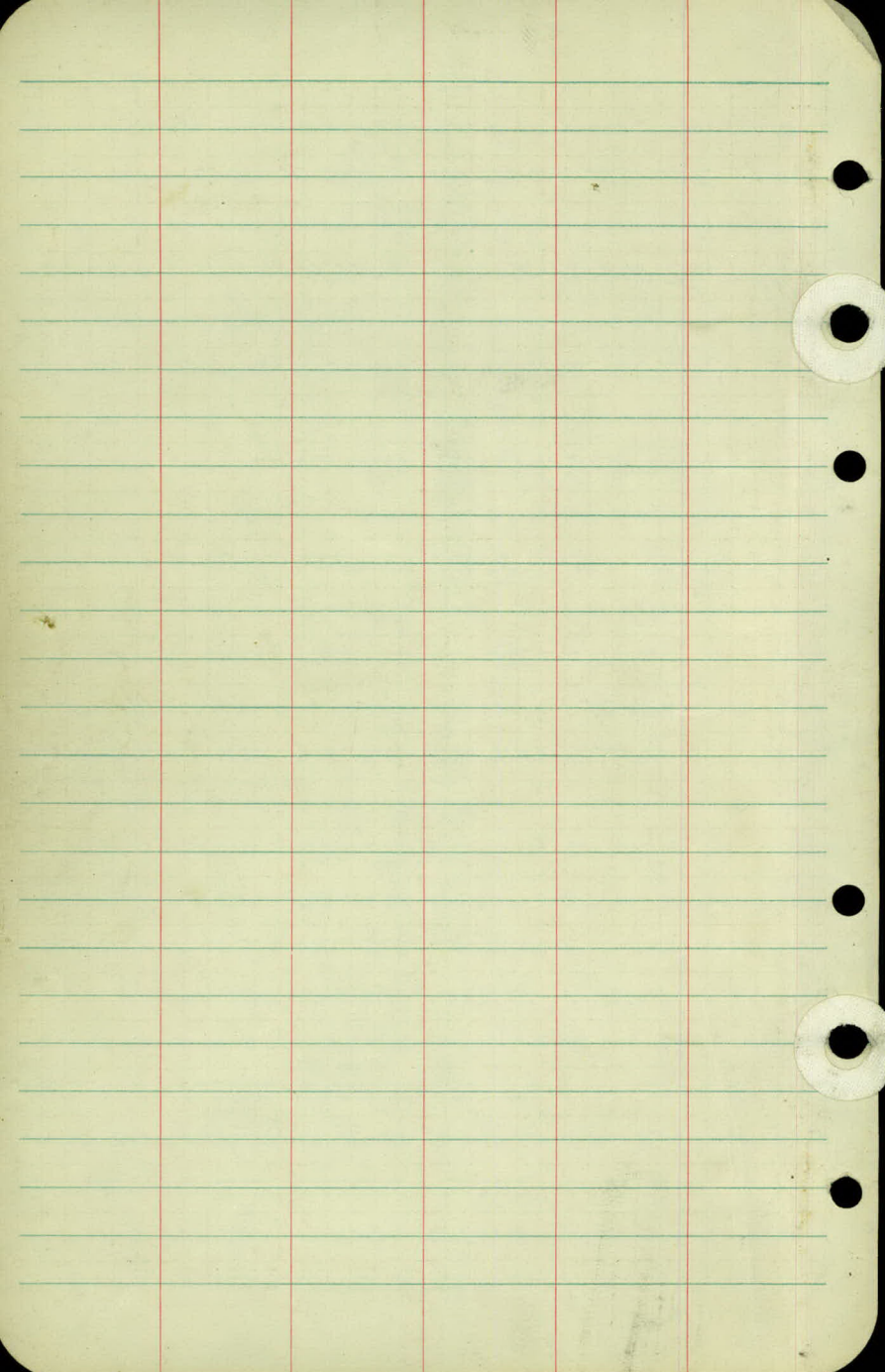
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Alignment 2-4

Josephine Rd

ECG 3/16/60

Co Rd C 2



INDEX

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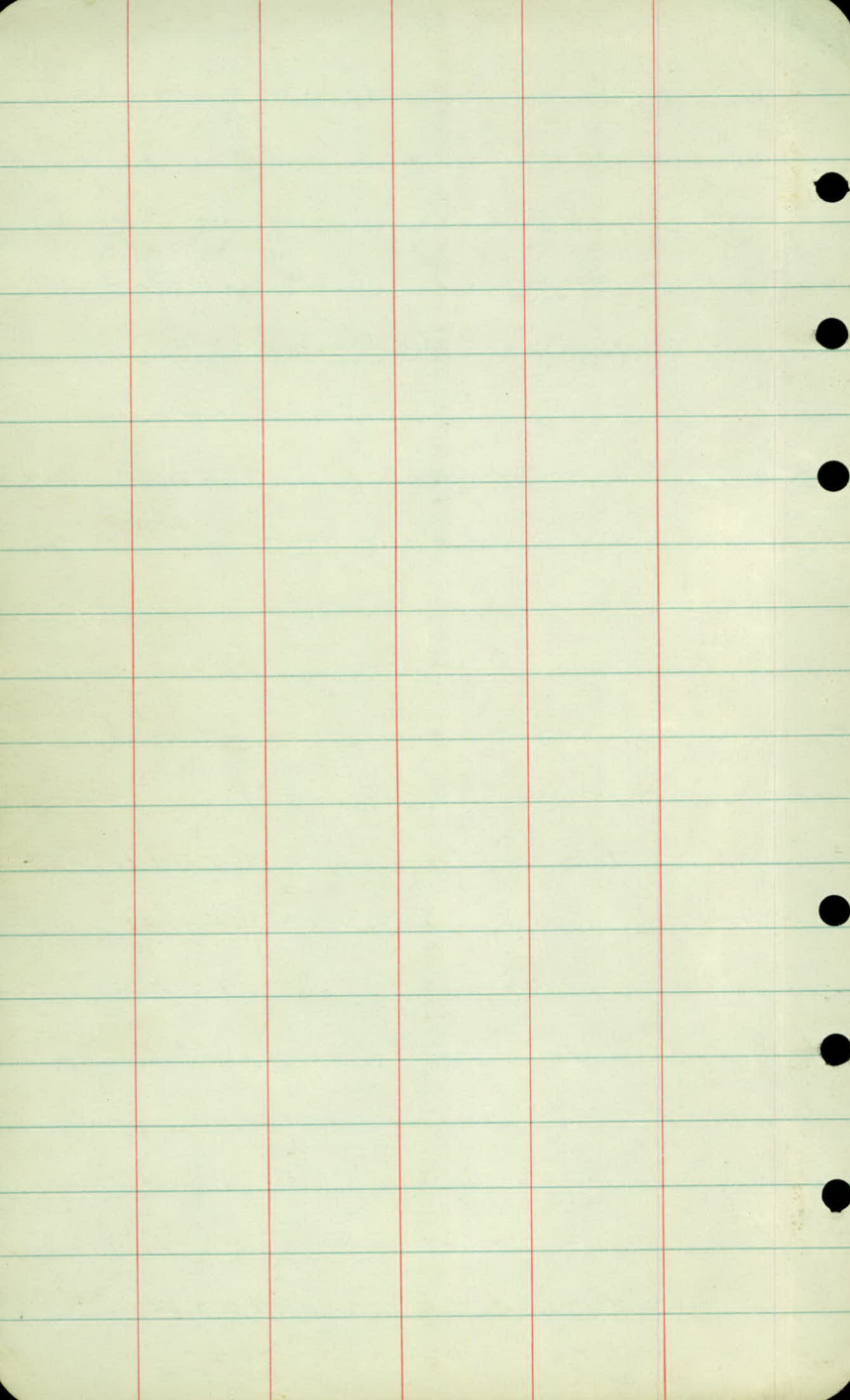
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FK
RG
JS
JH

Feb. 18, 1960 52
Cloudy Cold 4°

Alinement

Void

Sta Point ΔLt ΔRt

7+14.44 P.O.T.

3+99.93 PT $14^{\circ}59'48''$

+50 $12^{\circ}30'$ $\Delta = 29^{\circ}59'37\frac{1}{2}''$

3 $10^{\circ}-$ $D = 10^{\circ}$

2+53.49 P.I. $29^{\circ}59'37\frac{1}{2}''$ $T = 153.49$

+50 $7^{\circ}30'$ $L = 299.93$

2 $5^{\circ}-$ $R = 572.96$

+50 $2^{\circ}30'$

1 PC $0^{\circ}00'$

0+00

Feb 18, 1960

63

1/4 1/4 Line

153.75

135.75

Iron

408.03

3 nails

543.78

561.78

96°56'15"

PP
Disk 0

109.36

46.85

20" O B
Disk

Punch
hole

section line

Sta	Point	ΔL	ΔR
-----	-------	------------	------------

15+88.33	P.O.T.		
----------	--------	--	--

+66.63	P.T.		
--------	------	--	--

+50			
-----	--	--	--

15			
----	--	--	--

14+50.13	P.I.		
----------	------	--	--

+50			
-----	--	--	--

14			
----	--	--	--

+50			
-----	--	--	--

13+30.21	P.C.		
----------	------	--	--

		$11^{\circ}49'15''$	
--	--	---------------------	--

		$10^{\circ}59.4'$	$\Delta = 23^{\circ}38\frac{1}{2}'$
--	--	-------------------	-------------------------------------

		$8^{\circ}29.4'$	$D = 10'$
--	--	------------------	-----------

		$T = 119.92$	
--	--	--------------	--

		$5^{\circ}59.4'$	$L = 236.42$
--	--	------------------	--------------

		$3^{\circ}29.4'$	$R = 572.96$
--	--	------------------	--------------

		$59.4'$	
--	--	---------	--

		$0^{\circ}00'$	
--	--	----------------	--

FK
RG
JS
JH

Feb. 18, 1960
Feb 23, 1960

7
4

N Property Line Brenner Ave

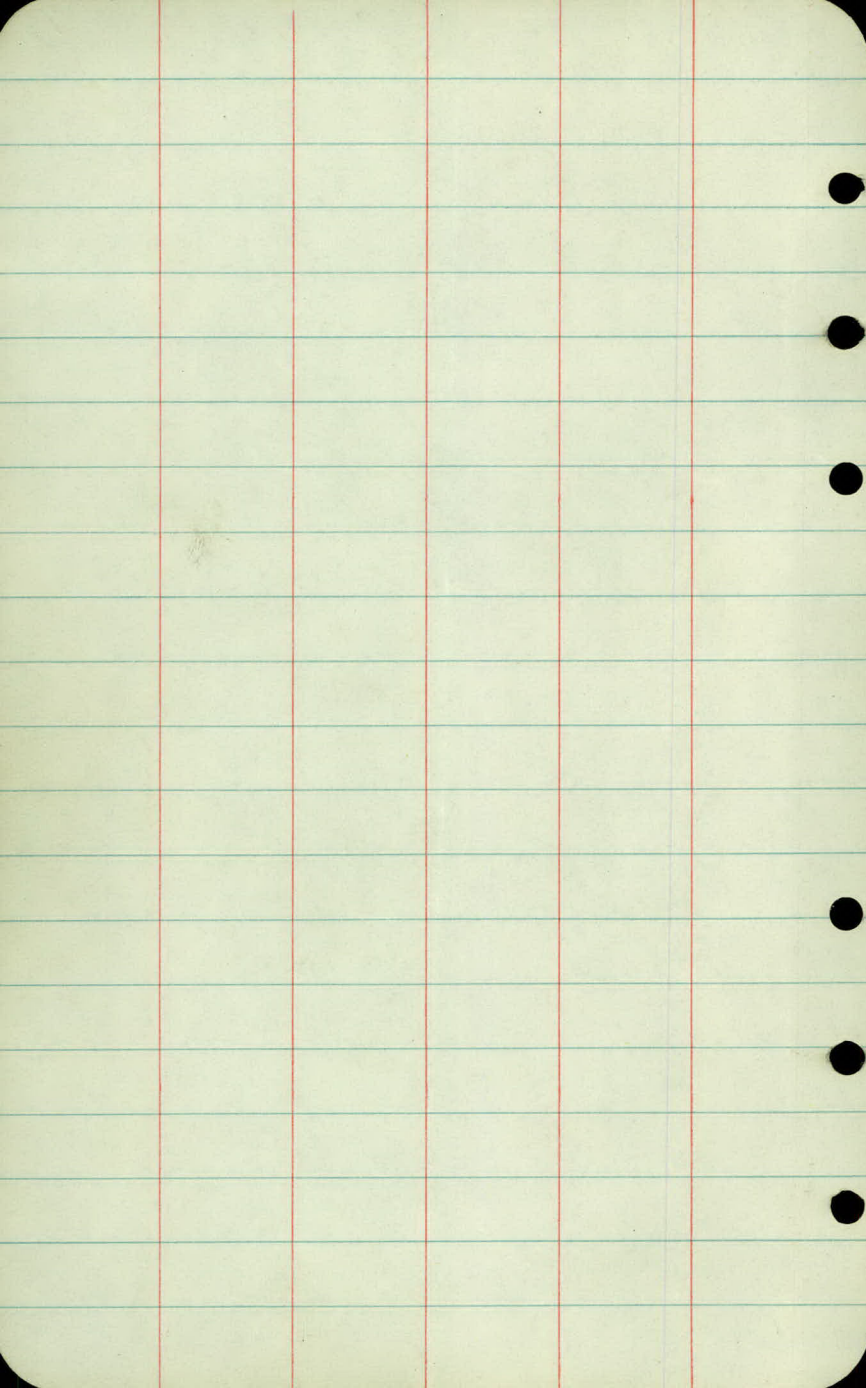
P.K. Nail

PP O
Disk

A 5.15

27.26

OPP
Disk



June 27, 1960 8,

New Curve

Sta Point ΔL ΔR

$$\Delta = 31^{\circ} 49'$$

$$D = 6^{\circ} \text{ Arc}$$

$$T =$$

$$L =$$

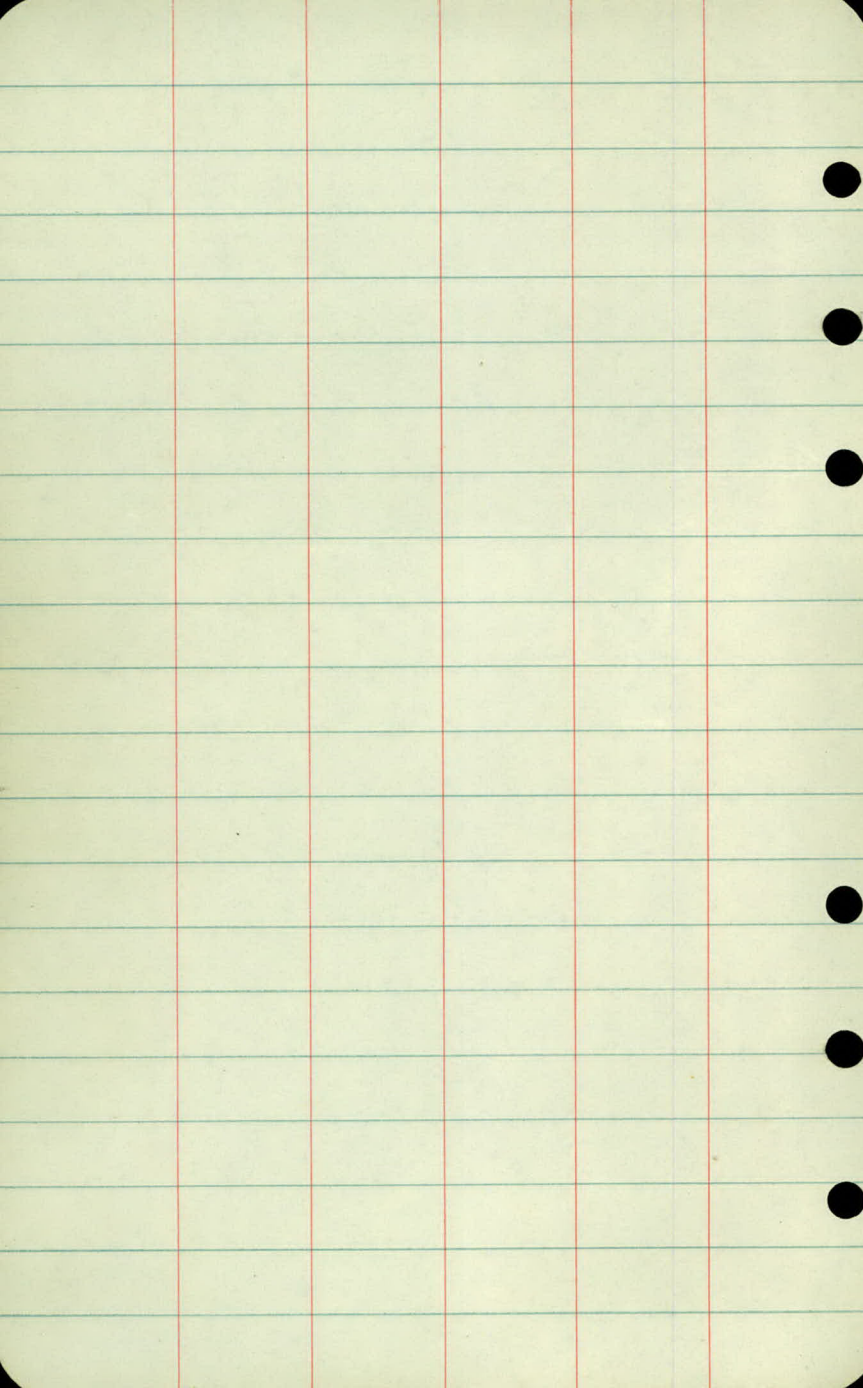
$$2+85.72 \quad P.I.$$

$$R = 954.93$$

June 27, 1960

92

P.K. Nail



New Alignment

$$\frac{A + B}{C + D} = \frac{A}{C} + \frac{B}{D}$$

Sta	Point	ΔL	ΔR
+78.88	P.T.		$10^{\circ} 54'$
+50			$10^{\circ} 19.2'$
17			$9^{\circ} 19.2'$ $X = 21^{\circ} 47\frac{1}{2}'$
+50			$8^{\circ} 19.2'$
16			$7^{\circ} 19.2'$ $D = 4^{\circ} \text{Arc}$
+50			$6^{\circ} 19.2'$
15+09.82	P.I.		$T = 275.73$
15			$5^{\circ} 19.2' = 544.79$
+50			$4^{\circ} 19.2'$
14			$3^{\circ} 19.2' R = 1,432.40$
+50			$2^{\circ} 19.2'$
13			$1^{\circ} 19.2'$ $1.2' / ft$
+50			$0^{\circ} 19.2'$ $1.0' / 50' = 50'$
12+34.09	P.C.		$0^{\circ} 00'$ 99.98

7+14.44	P.O.T.		
+43.84	P.T.		$15^{\circ} 56'$
5			$14^{\circ} 37'$
+50			$13^{\circ} 07'$
4			$11^{\circ} 37'$ $\Delta = 31^{\circ} 51\frac{3}{4}'$
+50			$10^{\circ} 07'$
3			$8^{\circ} 37'$ $D = 6^{\circ} \text{Arc}$
2+85.38	P.I.		$T = 272.58$
+50			$7^{\circ} 07'$
2			$5^{\circ} 37'$ $L = 531.04$
+50			$4^{\circ} 07'$
1			$2^{\circ} 37'$ $R = 954.93^{\checkmark}$
+50			$1^{\circ} 07'$
0+12.80	P.C.		$0^{\circ} 00'$ $01.8' / ft$
			$1^{\circ} 30' / 50' = 50.00$
			$100' = 99.95$

FA
RG
FS
JL
WM

April 21, 1960

21

157+14.75 Lex Ave

line

17+30.21 old pc

20.00

spike

$\frac{1}{4}$ $\frac{1}{4}$ Line

85.36
4781
25.57

A+00 (old)

10.21

E Josephine Rd

A+00 19.12

49.81

old

Lex Ave P.O. ST. 2+35.57 =
Josephine Rd Sta 22+06.07

2+15.2 on E of Lex

Sta

~~old~~ Line

9+00

7+14.44 P.O.T. old & New

+43.84 PT 6.0'

5 6.0'

+50 4.0'

4 0.5'

+50 5.6'

3 9.0

+50 10.6

2 10.4

+50 8.5

1 4.0

+50 0.4

0+12.8 PC 0.0

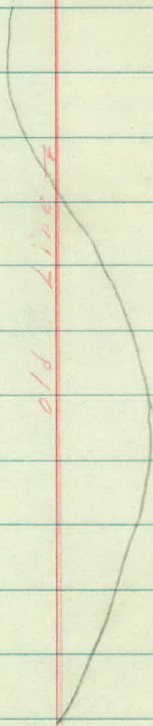
0+00

FK
JS
W/M

April 22, 1960

3
12

New Line to Lake
173



LT ⁴ old Line Rt

+78.88 PT 0.0

+50 0.3

17 2.1

+50 5.8

16 12.3

+50 20.2

15 25.2

+50 28.0

14 28.0

+50 25.2

13 20.6

+50 18.0

12+34.09 PC 17.5

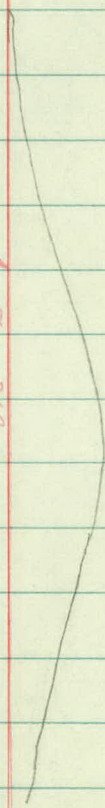
12+00

April 22, 1960

73

35
11.5

old line



New Line to Lake
167'

House Locations
obj Az Stadia

π AT P.I.

Sta 2+85.38

To Sta. 10+00 0°00' New Line

S. E. Cor. 322°20' 245'

N. E. Cor. 328°14' 286'

π AT P.I. Sta 15+09.82

To Sta 17+78.88

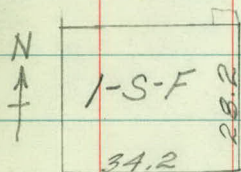
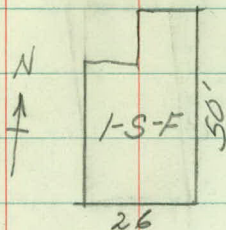
→ 0°00'

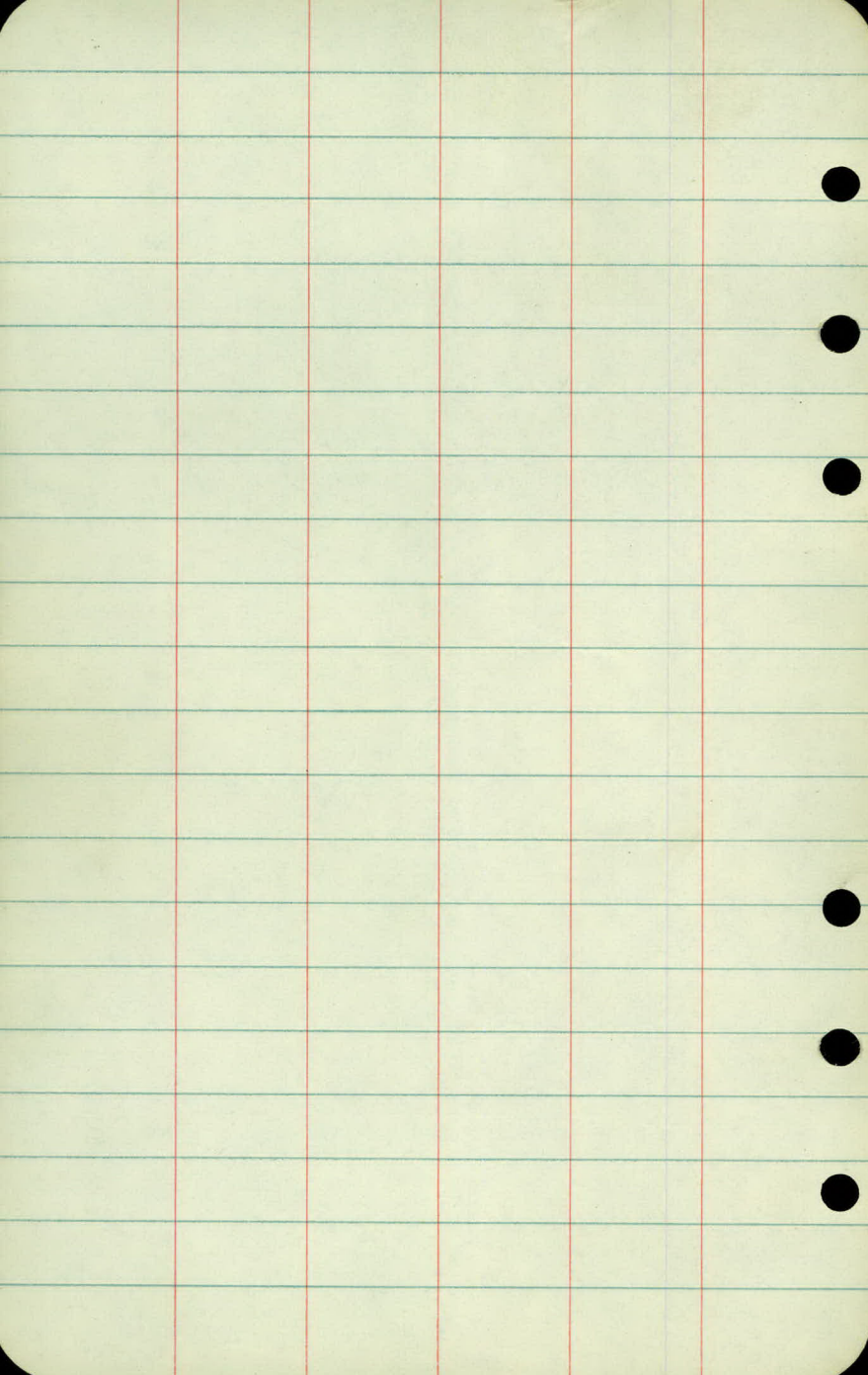
S. E. Cor. Ho. 226°05' 116'

N. E. Cor. Ho. 239°54' 118'

April 22, 1960

5
14





October 14, 1959 18,

Josephine Park

Stadia

OBJECT

AZ.

STADIA

N 40803' W of the East

hi 4.5

1/4 1/4 Cor of NE 1/4 Sec 3-29-23

to said 1/4 1/4 Cor 270°00'

E Lexington

270°00'

edge swamp

151°00' 11

" "

345°15' 10

" "

344°50' 21

" "

341°30' 32

" "

003°40' 54

" "

14°45' 74

" "

24°35' 98

" "

23°30' 131

" "

30°00' 163

" "

24°50' 186

" "

17°10' 175

250°45' 10

275°40' 24

KP
RJ
JH DIST.

VERT.
ANGLE

ROD
EQUIV.

October 13, 1959
Overcast 40°
ROD DIFF.

192
ELEV.

1.85

5.3

5.2

5.3

4.9

OBJECT

AZ.

STADIA

π at point 641.1' W
of said $\frac{1}{4}$ $\frac{1}{4}$ corner

n150

to said $\frac{1}{4}$ $\frac{1}{4}$ cor

90°00'

£ Lexington

90°00'

edge of swamp

85°30' 201 ✓

" " "

70°00' 180 ✓

" " "

63°00' 180 ✓

" " "

54°20' 186 ✓

" " "

46°00' 193 ✓

" " "

39°30' 189 ✓

" " "

30°00' 181 ✓

" " "

29°10' 193 ✓

" " "

23°50' 193 ✓

" " "

24°00' 170 ✓

" " "

15°40' 174 ✓

" " "

16°50' 212 ✓

13°12' 212 ✓

13°50' 176 ✓

Oct. 14, 1959

203.

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

3.8

7.4

7.3

7.4

7.3

7.4

7.4

7.4

7.5

7.2

7.3

7.4

7.4

7.3

7.2

OBJECT

AZ.

STADIA

~~at point 41.1' W
of said 1/4 1/4 cor.~~

h 15.0

Edge of swamp 41°30' 220 ✓

" " 42°10' 246 ✓

" " 42°40' 266 ✓

" " 42°35' 255 ✓

Top of Knoll 58°10' 218

Oct. 14, 1959

213

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

7.5

7.6

7.3

7.8

+2°54' +11.0

5.0

+6.0

13.5 above
Swamp

2 18
5.05
10 90
90 90 0
91.00 90

OBJECT

AZ.

STADIA

To ~~at~~ Lexington on
N. Line Brenner Ave.
to ~~at~~ Lexington N. 000°00'

N.W. Cor Barn 89°16' 98

S.W. Cor. Barn 111°13½' 106

N.E. Cor. House 131°12' 134

N.W. Cor House (proper) 140°00' 116

N.W. Cor Store 171°13' 197

SW Cor Store 171°56' 217

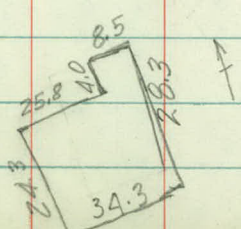
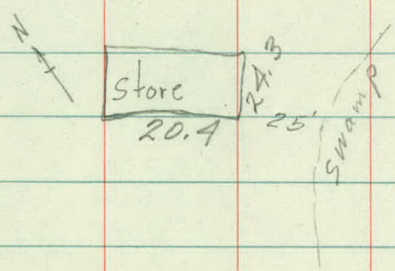
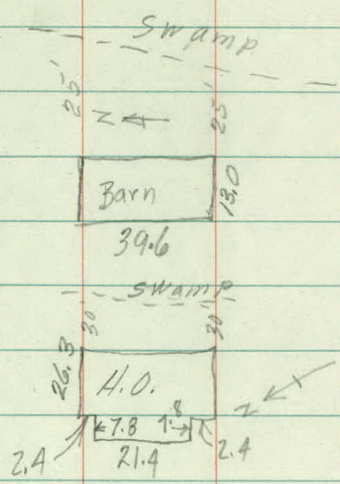
this bldg. is parallel to Lex. Ave.

S.E. Cor. Ho. 208°00' 179'

NE. Cor Ho
proper 216°55' 171

14 October, 1957 224.

DIST.	Y. PT. + ANGLE	PROD ELEV.	PROD	DIFF.	ELEV.
-------	-------------------	---------------	------	-------	-------



object

AZ

stadia

π on $\frac{1}{2}$ Lexington Ave

on N. LINE Brenner Ave

S.E. Cor.
Shed

219°50' 138

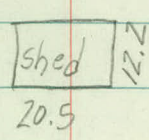
N.E. Cor
shed

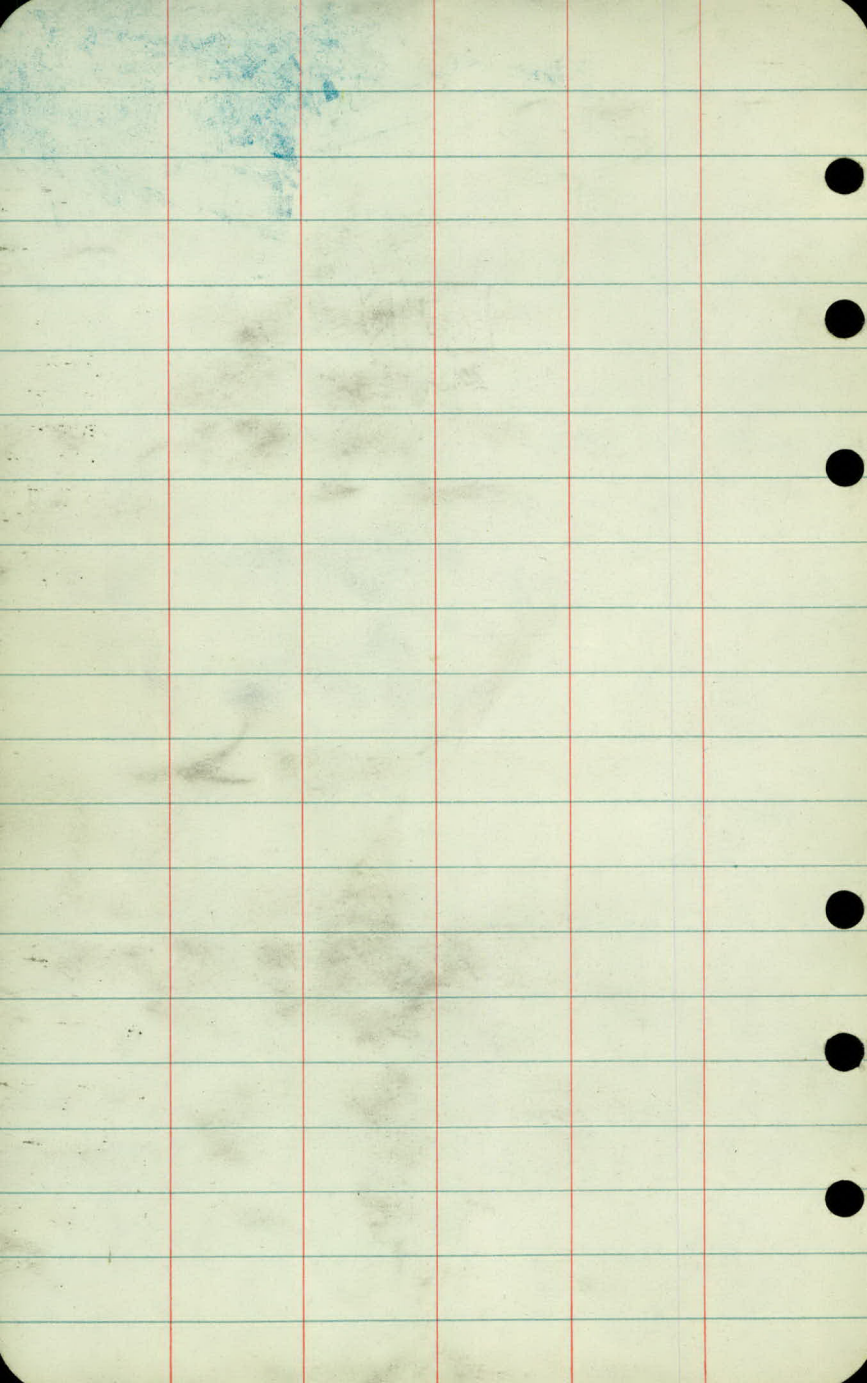
225°17' 134

14 Oct. 1959

235.

dist vert ang. rod elev rod diff elev





FK.
RG
JH

Dec. 16, 1958

243

Topography

7

+21 Edge Water
£

7

+95 Fe +91.49 Iron +92 Fe Cor
£ £ 29.5
+90 Culvert
61
+62.5 £ Lexington
£

6

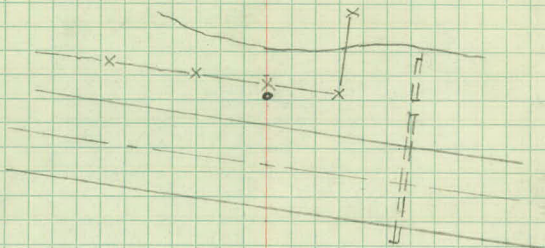
4.

+08.03 Iron
£

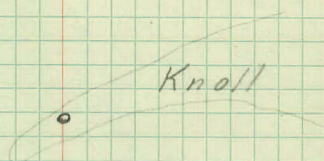
2

0+00 E.N.E. $\frac{1}{4}$ $\frac{1}{4}$ Cor Sec. 3 Rose

Dec 16, 1958 25 A



Swamp

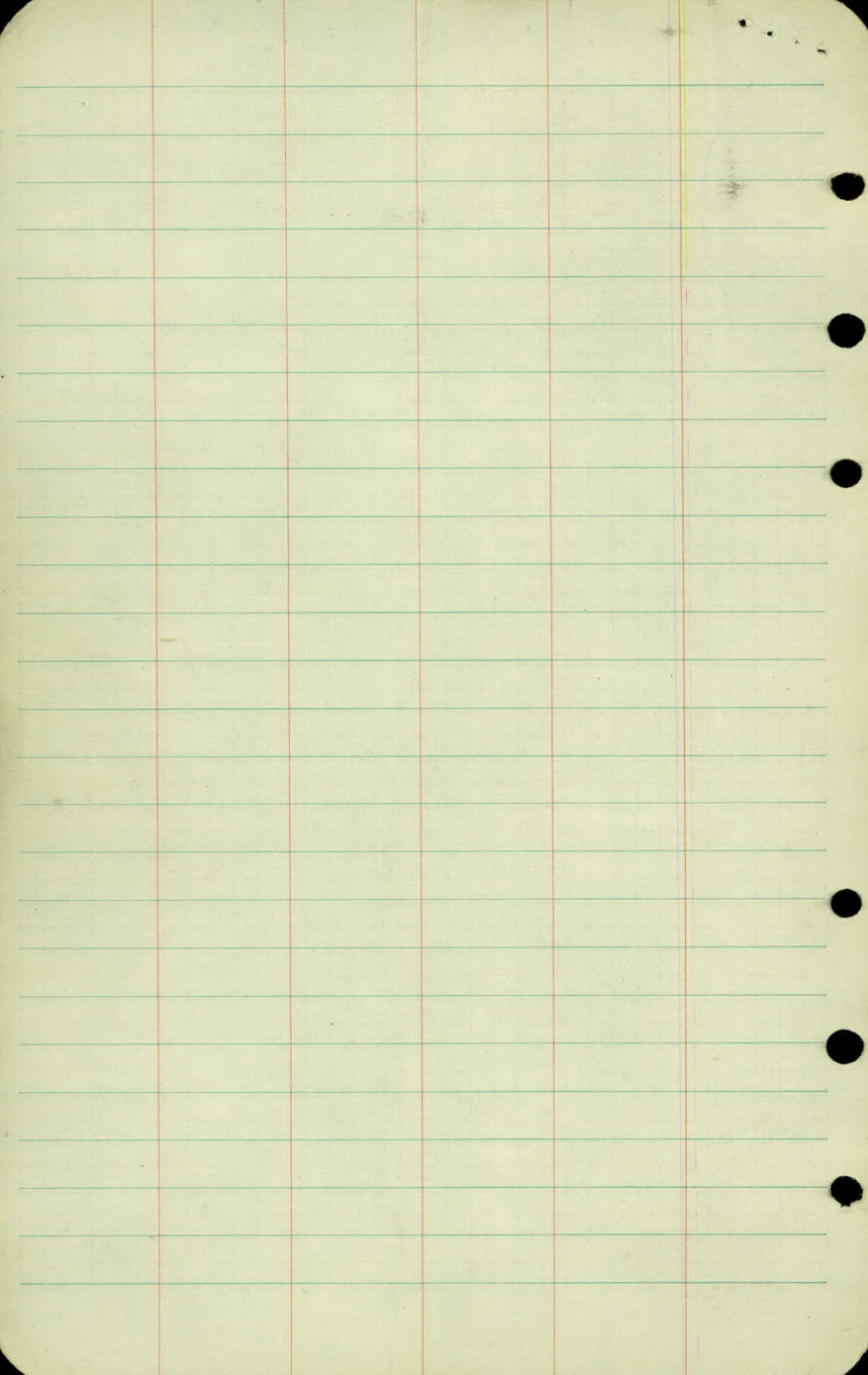


Knoll

Lake

Swamp

1/2" Pipe



Feb 13, 1958

26

Lake Josephine
Stadium
East End

4 pages

Obj Az. Stadia

on Sec Line

908' W. of NE Cor

Sec 3 Rose Twp.

to N.E. Cor Sec 3 90°00'

shoreline

87°36' 372' ✓

98°21' 381' ✓

105°57' 430' ✓

119°54' 451' ✓

135°15' 477' -

149°20' 558' -

158°24' 708' ✓

160°21' 758' ✓

Rt. of Sta 2+00

160°45' 900' ✓

SW Cor House

156°46' 820' ✓

SW Cor House

148°55' 675' ✓

NW Cor House

147°06' 658' ✓

NE Cor House

144°55'

NW Cor House

156°26'

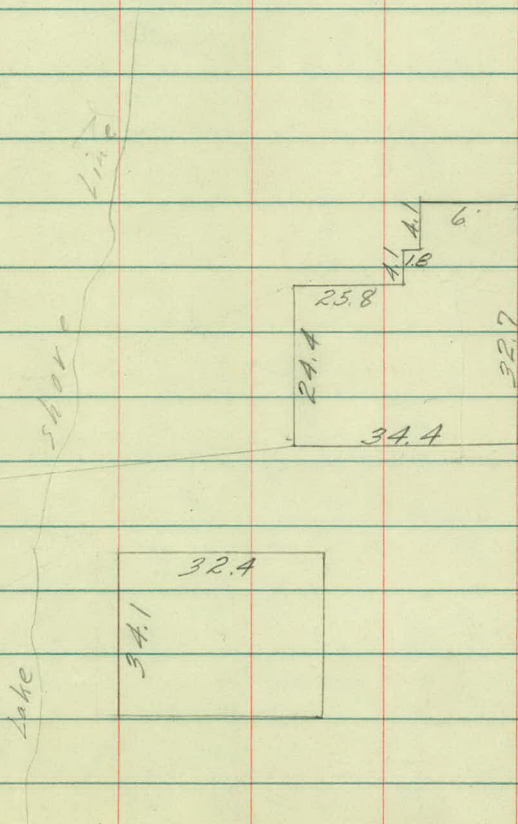
FK
RG
K
AB
RJ
PR

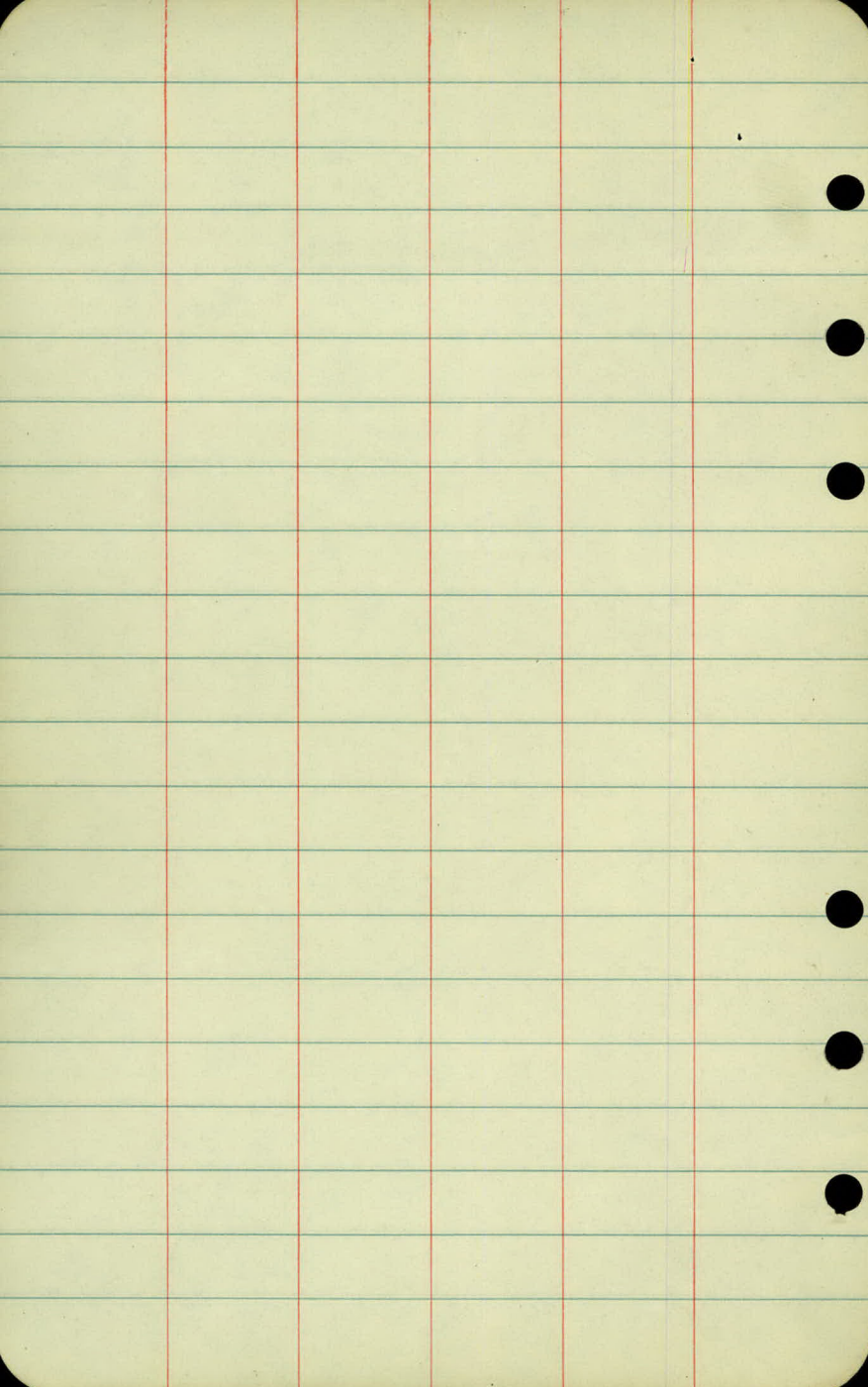
Vert A

Feb 13, 1958

Rod

27.2
Elev





TOPOGRAPHY

4 $\frac{Road}{92-63}$ $\frac{SWP}{41}$ $\frac{R1}{196}$ $\frac{4^{13}L}{44}$

$+92$ $\frac{PP}{43}$

$+50$ $\frac{Road}{71-42}$ $\frac{SWP}{20}$

3 $\frac{Road}{17-20}$ $\frac{SWP}{2}$

$+50$ $\frac{R. tie N}{Side Jos.}$

$+50$ $\frac{Road}{33-45}$

$+50$ $\frac{ER}{69}$

$+50$ $\frac{SWP}{7}$

$+54$ $\frac{Arch}{1}$

$+107$ $\frac{R. tie}{S.S. Jos.}$

$+12$ $\frac{R. tie}{sign}$

2 $+100$ $\frac{End Fe}{46}$

$+100$ $\frac{BR}{22}$

$\frac{Road}{22-6}$ $\frac{SWP}{19}$

$+99$ $\frac{SWC Cox Sign}{26}$ $6X6$

$\frac{Fe}{41}$

$+50$ $\frac{Road}{16-12}$ $\frac{SWP}{20}$

1 $+100$ $\frac{Bay Broken Fe}{50}$

$\frac{Road}{14-14}$ $\frac{SWP}{39}$

0 $\frac{Road}{14-14}$ $\frac{SWP}{37}$

Feb 23, 1960 296

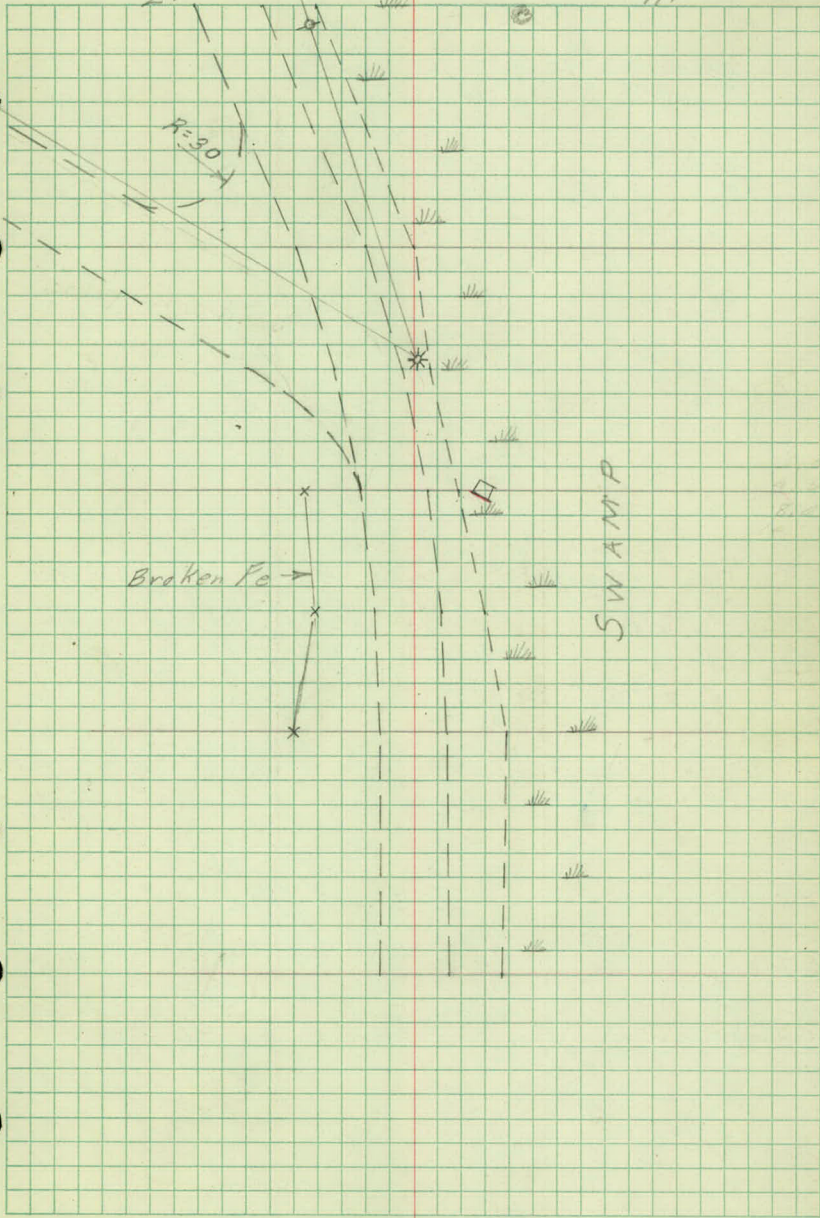
Lt

Rt

R=90

Broken Pe →

SWAMP



Lt

E

Rt

9

SWP
76SWP
64

+68

Begin Lowland & Woods
(Swamp at Higher Level)

8

± Road
100SWP
64SWP
62+80 PP
72E.A. 36" SOP
76+50 SWP
65+50 B. ILL
PIPESWP
64+67 SWP
82+40 SWP
115

7

+38 PP
71

6

± Road
100SWP
59

5

± Road
100SWP
59+94 PP
70

6-5" M

+64 45

+64 8" BE
17+59 4" BE
25+50 ± Road
91+34 Quad 4" BE
27+50 8" BE
14+44 4" BE
PR

4

+29 TW 6" BE
23

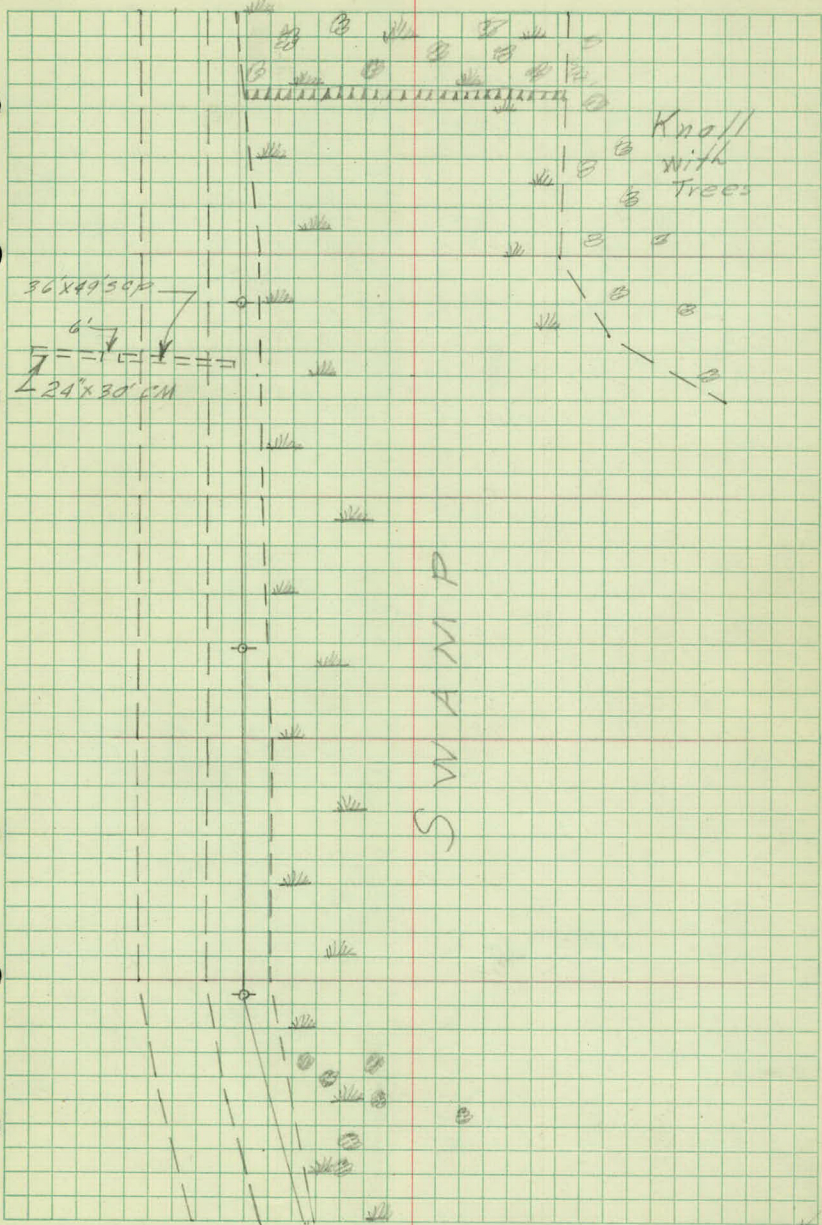
Lt

L

Feb. 23, 1960

Rt

307



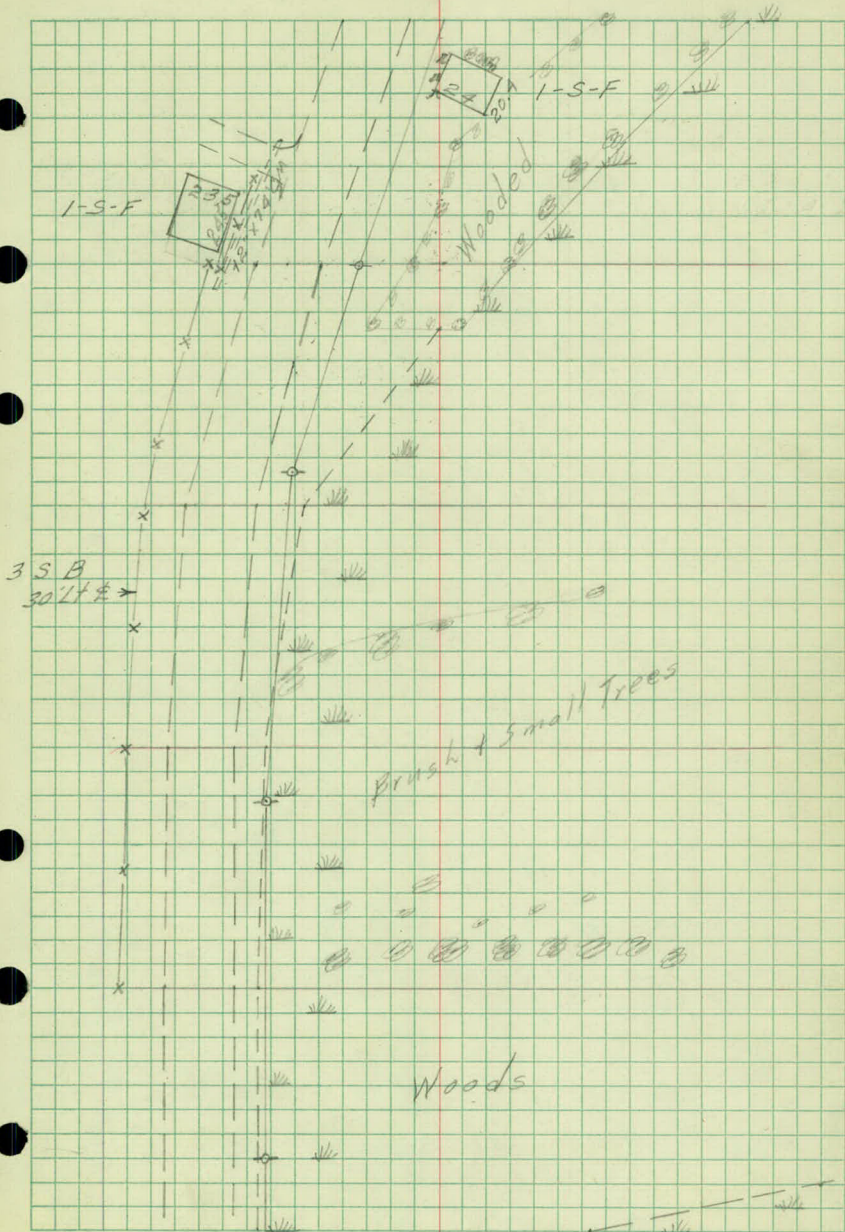
14	27 Road 40-12			Rt Woods 68 +84 SWP 1	SWP 125	
+45	Ent Lt	+74	SWP 1	+70.5 Bldg \$	Rtie Bldg 6-63 +93 12-25	
+35	E.Fe 76	+51	NECult 65	+71 SWP 2	+50 SWP 80	+50 Woods 5-120" BE
100	Rtie Wd Lt	+29	NECortb 83	+25 Woods \$	+63 13	
13	100 Fe Cor 96	Woods 12	4 Road 63	Woods 30	+61.5	SE Cor Bldg 20
+99	Fe Cor 90	+99	PP 33	+98 Fe Cor 90		
+89	SE Cult 94		+50 Road 60	+73 SWP \$		
+75	Begin Woods 29-10					
		+14	PP 61			
12	4 Road 89		SWP 56			
		+55	End Trees + Brush			
11	4 Road 99		SWP 72			
	+78	PP 72				
		+20	End Woods Begin Trees + Brush			
10	4 Road 100		SWP 75			
	+30	PP 72		+20	SWP T60	
9			SWP 76			

Lt

Feb 23, 1960

Rt

318



Sta

Lt

L

Rt

+50 ^{Swp}
40

17

Fe Road
33 14 14

Woods Beyond
50'

+44 Ent
Lt

+70 12" BF
33

+35 6" M
47

+19 24" M
53

16

Fe Road
32 14 14

+11 3-14" 2
40

Woods Swp
60 133

+95 PP 27 +87 Ent 12" x 12" CM
22

+99 PP
27

+50 Road
14.5 13.5

+98 6" CM H
37

+68 22" D
35

+79 RTie
Fe

+50 Swp
156

+59 6" D
34

+59 Fe Cor
35

+28 E 10" Hedge
30

15

Road
18-10

+01 12" W
30

Woods Swp
110 150

+97 28" W
71

+98 28" W
56

+99 28" W
43

+89 18" W
28

+97 8" PE
30

+50 Swp
135

+52 12" E
25

+50 18" E
35

+59 SWC N 16
68

+70 Top Cone Steps
44

+71 RTie
H. Rt

+43 10" W
22

+42 12" E
22

+42 16" M
44

+68 B. Cone Steps
32

+50 Road
26-2

+39 PP
12

+25 E 10" Hedge
19

+50 Woods
106

14

+19 PP
43

+14 +12 Ent
Rt

Lt

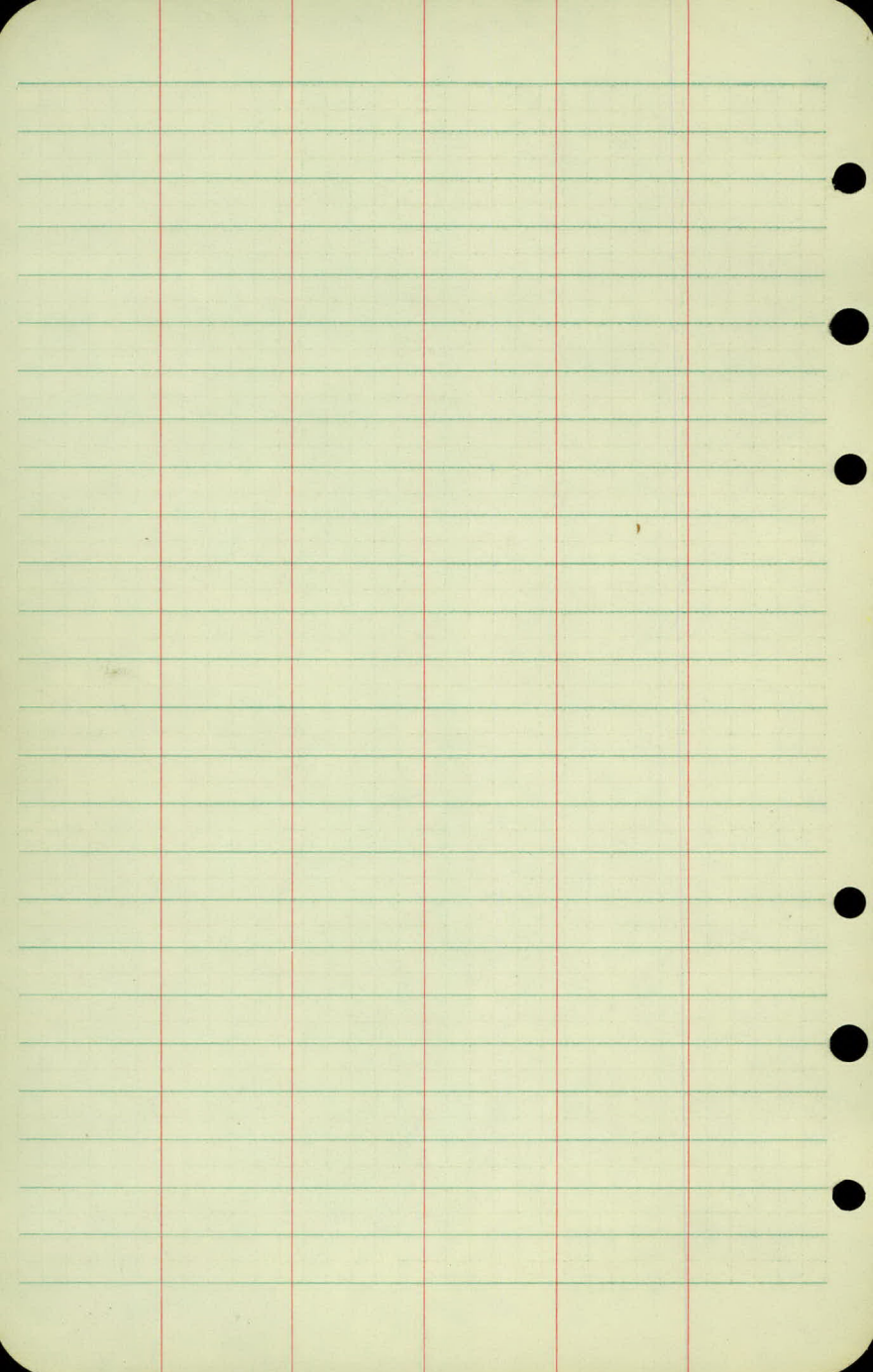
+

Feb 24, 1960

329

R1





Lexington & Josephine

+05 N End 12" CM
79

3

Possible Intersection E. End ^{15" CM} ~~12" CM~~ Submerged
+50 56 +54 2

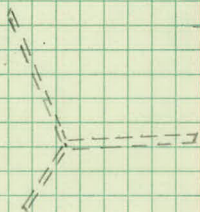
129 SE 18" CM
72.5

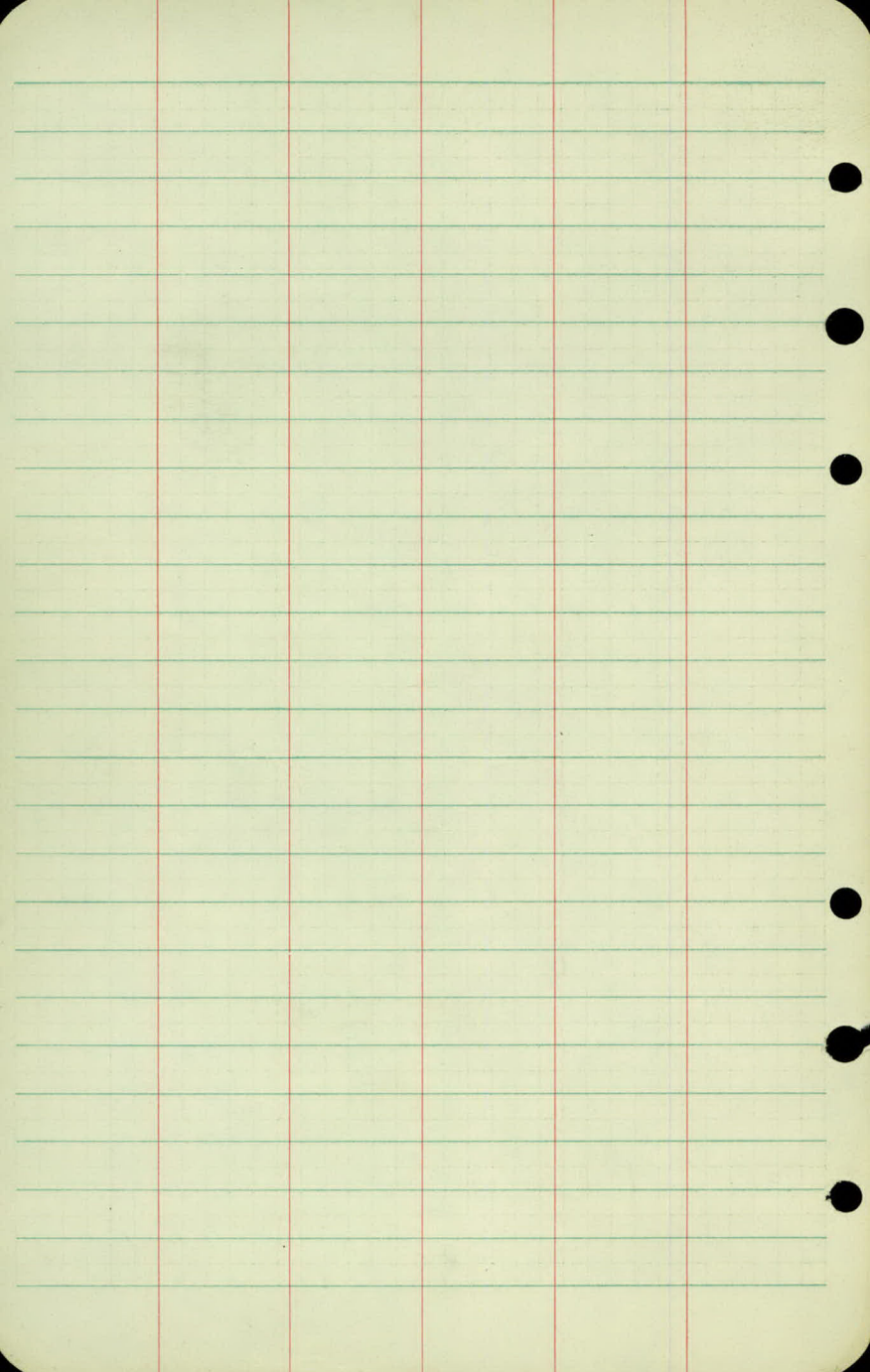
2

1

FR
RG
JL
WM
JH

June 15, 1960 34₂





Feb 23, 1960

35
10

Bench Levels

Sta	+	-	Elev	
BM	2.76	890.49		(887.73)
W.S.	10.35	893.83	7.01	883.48
BM			5.35	
BM	5.72	893.83	5.72	888.11 (888.10)
TP	9.43	895.82	7.44	886.39
BM	6.75	900.48	2.09	893.73 (893.72)
BM	13.75	911.30	2.93	897.55 (897.54)
TP	12.73	923.75	0.28	911.02
TP	7.50	930.45	0.80	922.95
BM		27.2	3.2	
BM	3.05	900.60		897.55
BM	2.67	896.40	6.87	893.73 A
TP	8.30	894.67	10.03	886.37
BM	5.37	893.45	6.59	888.08 (888.10)
BM			5.02	888.43 (888.44)

Feb 23, 1960

36
11

RR Spike in 30" Oak at Pump Outlet of Josephine

Lake Josephine

(old) Spike in PP NE Cor Josephine + Lexington⁺

(New) Spike in PP NW Cor " + "

Top W. E. 36" SCP Culvert

Spike in Guy Pole

Spike in 8" B. E. Fe. Post Stump at Ent Lt 16+80^x

PK Nail

Nail in Arc Lt Pole SE. Cor D + Lexington

(Missing)

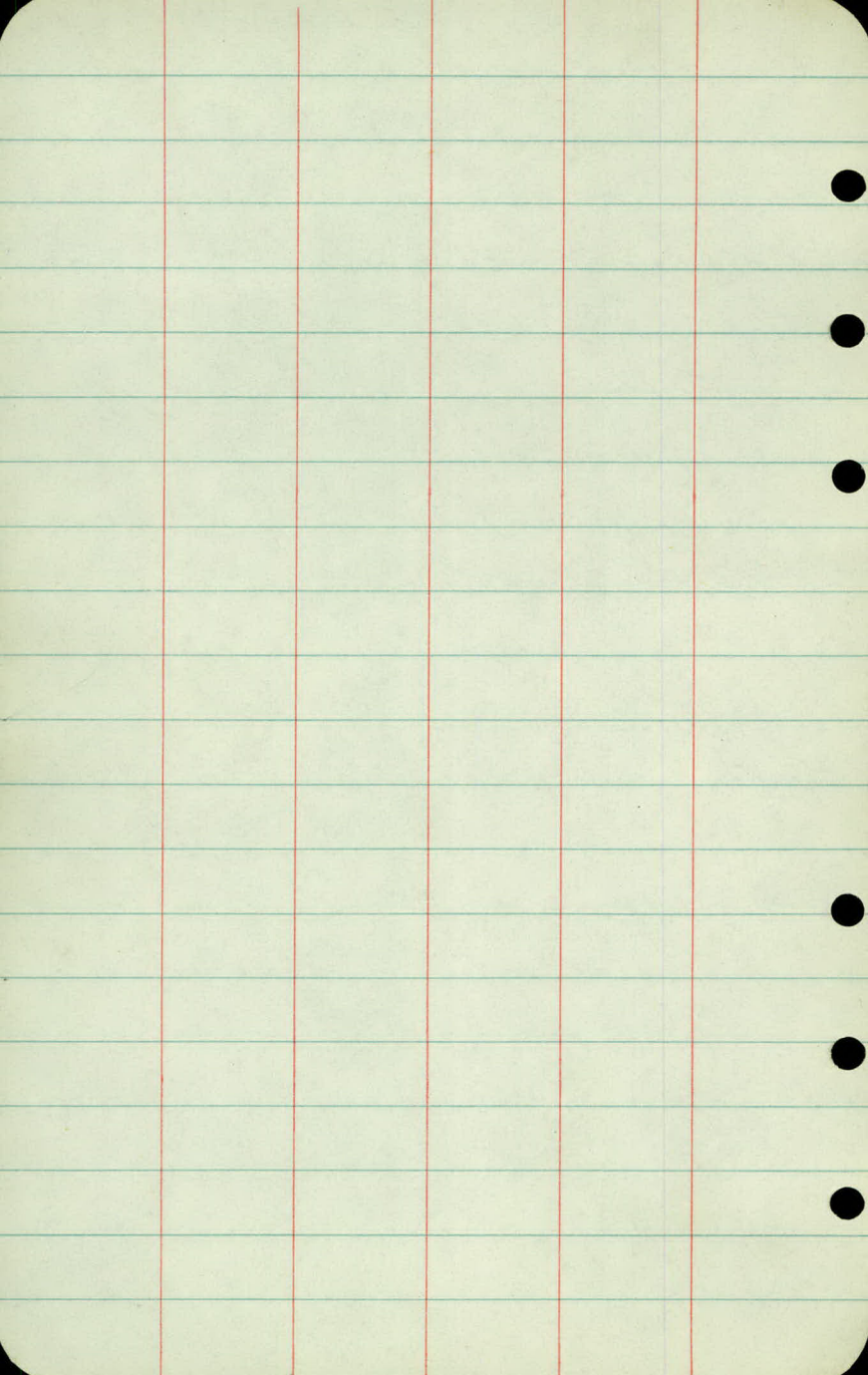
Spike in 8" B. E. Fe. Post Stump at Ent Lt 16+80

Spike in Guy Pole

Top W. E. 36" SCP Culvert

Spike in PP NW. Cor Josephine + Lexington

Nail in PP NW. " " "



FK
RG
JS

March 3, 1960
Clear 11°

37/12

X-Sections

Sta	+	x	-	Elev.
BM	5.51	893.61		888.10

0+00

✓

+50

✓

/

✓

March 3, 1960 38/13

LT

RT

Spike in PP NW Cor Josephine + Lexington

87.6	87.6	89.2	89.1	89.29	89.0	88.7	88.0	86.4
6.0	6.0	4.4	4.5	4.31	4.6	4.9	5.6	7.2
28	25	20	13		10	18	22	26

83.6
0.0
36

83.7
84.1
84.9
9.9 9.5 8.7
75 63 45

87.4	87.4	89.0	89.1	89.4	89.0	88.9	86.1	85.7
6.2	6.2	4.6	4.5	4.2	4.6	4.7	7.5	7.9
28	25	19	13		11	18	30	35

83.6
0.0
37

84.1
84.9
9.5 8.7
75 52

87.5	87.0	89.1	89.1	89.31	88.9	88.9	88.4	85.8
6.1	6.6	4.5	4.5	4.30	4.7	4.7	5.2	7.8
26	23	17	12		13	17	22	29

83.6
0.0
31

84.2
84.7
85.0
9.4 8.9 8.6
75 65 50

Sta + π - Elev

893.61

1 + 50

✓

+ 66

✓

2

✓

March 3, 1960 37 14

LT

86.1	86.1	89.0	89.1	89.3	88.9	88.7	87.8	85.5
7.5	7.5	4.6	4.5	4.3	4.7	4.9	5.8	8.1
29	26	19	15		10	16	20	25

87.9	89.4	93.6		84.1	84.3	84.7	85.2
5.7	4.2	0.0		9.5	9.3	8.9	8.4
35	40	52		75	62	42	26

86.1	88.9	89.0	89.3	89.2	88.9	88.5	83.0	84.7
7.5	4.7	4.6	4.3	4.4	4.7	5.1	8.6	8.9
27	21	16	5		8	15	24	36

85.8	86.4	86.6	87.6	90.3		84.2	84.3
7.8	7.2	7.0	6.0	3.3		9.4	9.3
32	33	39	50	75		75	58

85.7	88.2	88.7	89.0	88.7	88.3	88.0	87.0	84.6
7.9	5.4	4.9	4.6	4.9	5.3	5.6	6.6	9.0
33	27	22	9		6	10	14	20

85.3	85.4	85.6		84.0	84.3	84.4	84.7
8.3	8.2	8.0		9.6	9.3	9.2	8.9
50	64	75		75	54	41	26

Sta + π - Elev.

893.61

2+25

✓

TP 6.91 891.72 8.80 884.81

+50

✓

3

✓

March 3, 1960 40,5

RI

87.5	87.6	88.6	88.7	88.1	88.1	86.4	84.3	84.2	84.4
6.1	6.0	5.0	4.9	5.5	5.5	7.2	9.3	9.4	9.2
50	38	26	15		5	10	16	34	41

84.8	85.2						84.3	84.1
8.8	8.4						9.3	9.5
65	75						75	70

87.8	88.5	88.5	88.1	87.8	85.1	84.6	84.1	84.1
3.9	3.2	3.2	3.6	3.9	4.6	7.1	7.6	7.6
53	33	21	9			32	53	75

87.5
4.2
75

88.5	88.0	87.6	85.6	84.7	84.4	84.5	84.8	84.4
3.2	3.7	4.1	6.1	7.0	7.3	7.2	6.9	7.3
36	25	13	6		7	21	36	58

88.7	87.9
3.0	3.8
51	75

84.1
7.6
75

Sta	+	π	-	Elev.
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Sta	+	π	-	Elev.
-----	---	---	---	-------

891.72

Sta	+	π	-	Elev.
-----	---	---	---	-------

3+50

✓

A

✓

+20

✓

✓

March 3, 1968 41/16

Lt

81

41/16

88.0	87.7	85.4	84.7	84.8	84.7	84.6	84.5	84.1
3.7	4.0	6.3	7.0	6.9	7.0	7.1	7.2	7.6
43	35	24	14	18	41	61	75	

88.7	89.7	86.6	86.5
3.0	2.0	5.1	5.2
57	76	84	90

87.7	86.3	85.7	85.5	85.5	85.5	83.6	86.1	85.9
4.0	5.4	6.0	6.2	6.2	6.2	6.1	5.6	5.8
57	47	33	14	18	30	42	52	

88.5	89.6	90.2	88.8	90.7		84.8	85.3
3.2	2.1	1.5	2.9	1.0		6.9	6.4
75	93	103	110	123		75	70

86.1	85.7	85.7	86.1	86.6	84.4	86.8	86.7	86.3
5.6	6.0	6.0	5.6	5.1	5.3	4.9	5.0	5.4
48	38	21	16	15	37	51	58	

87.8	87.9	88.8	89.6
3.9	3.8	2.9	2.1
61	70	84	97

85.3
6.2
75

90.2	89.4	89.1	90.3
1.5	2.3	2.6	1.4
120	116	112	106

Sta + π - Elev.

891.72

4+68

✓

✓

5

TP 2.29 889.42 4.59 887.13

March 3, 1960 427

RT

86.8	86.6	86.4	86.5	86.4	86.2	85.9	85.7	85.2
4.9	5.1	5.3	5.2	5.3	5.5	5.8	6.0	6.5
64	52	30	13	12	30	47	75	

88.2	88.8	90.0	89.3
3.5	2.9	1.7	2.4
73	93	111	114

91.5	89.3
0.2	2.4
123	117

88.4	85.5	84.8	84.8	84.7	84.7	84.7	84.7	84.6
3.3	6.2	6.9	6.9	7.0	7.0	7.0	7.0	7.1
77	61	38	17	16	36	56	75	

88.3	89.1	89.3
3.4	2.6	2.4
85	98	109

90.5	89.2	89.0	89.5
1.2	2.5	2.7	2.2
127	123	119	116

Sta	+	π	-	Elev
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		889.42		
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5+50				
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✓				
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✓				
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6				
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✓				
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✓				
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March 3, 1960 43 18

LT

RT

88.4	84.4	84.3	84.1	84.2	84.1	84.2	84.1	84.1
1.0	5.0	5.1	5.3	5.2	5.3	5.2	5.3	5.3
78	60	38	15	25	49	68	75	

88.8	88.6	89.1	89.3
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0.6	0.8	0.3	0.1
84	86	100	114

89.2	87.8	87.8	89.1
0.2	1.6	1.6	0.3
131	127	122	118

88.4	84.0	83.9	83.9	83.9	83.9	83.9	84.0	83.1
1.0	5.4	5.5	5.5	5.5	5.5	5.5	5.4	5.7
78	60	40	18	25	44	59	75	

88.7	89.3	89.0	89.0
0.7	0.1	0.4	0.4
87	100	114	117

88.3	87.4	87.4
1.1	2.0	2.0
131	127	123

Sta	+	π	-	Elev
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Sta	+	π	-	Elev
		889.42		

Sta	+	π	-	Elev
6+50				

Sta	+	π	-	Elev
✓				

Sta	+	π	-	Elev
✓				

Sta	+	π	-	Elev
7				

Sta	+	π	-	Elev
✓				

Sta	+	π	-	Elev
✓				

March 3, 1968 44/19

RT

88.5	21	84.2	83.8	83.8	83.7	83.7	83.7	83.3
09	5.2	5.6	5.6	5.7	5.7	5.7	6.1	
79	65	46	28		23	51	75	



88.8	89.3	88.7	88.3
0.6	0.1	0.7	1.1
86	100	113	119

87.4	86.6	87.0
2.0	2.8	2.9
133	130	122

88.1	83.9	83.7	83.6	83.6	83.6	83.9	83.7	83.7
1.3	5.5	5.7	5.8	5.8	5.8	5.5	5.7	5.7
78	63	42	18	23	49	67	75	



88.5	89.1	88.5	88.1
0.9	0.3	0.9	1.3
86	100	113	120

86.9	87.1
2.5	2.3
133	123

Sta	+	π	-	Elev
-----	---	-------	---	------

		889.42		
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7+50				
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✓				
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✓				
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TP	4.48	890.65	3.25	886.17
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8				
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✓				
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✓				
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March 3, 1960 45 20

88.1	83.9	83.0	83.9	83.6	83.6	83.6	83.8	84.3	84.4
1.3	5.5	5.7	5.8	5.8	5.8	5.6	5.1	5.0	
80	66	41	18		22	46	69	75	

88.3	88.9	88.5
1.1	0.5	0.9
87	100	115

86.6	86.6	88.0
2.8	2.8	1.4
129	123	119

83.57	83.51
5.85	5.91
FL 30" SCP	FL 30" SCP
88.2	83.7
2.5	2.0
79	18

88.6	89.0	88.4	88.0	87.3
2.1	1.7	2.3	2.7	3.4
88	100	115	120	123

87.0
3.7
131

£ March 3, 1960 46 21

81

85.6

84.8

84.8

84.9

84.1

84.4

85.4

87.2

90.4

5.1

5.9

5.9

5.8

6.6

6.3

5.3

3.5

0.3

69

61

44

20

23

43

60

70

88.2

88.7

88.9

88.5

2.5

2.0

1.8

2.2

80

87

100

114

87.4

87.6

88.5

3.3

3.1

2.2

129

121

119

85.0

85.8

85.2

85.0

84.3

84.7

85.7

86.5

88.4

5.7

4.9

5.5

5.7

4.4

6.0

5.0

4.2

2.3

44

32

18

14

16

28

44

62

85.3

86.3

88.3

88.7

5.4

4.4

2.4

2.0

66

73

81

87

86.8

87.6

88.5

88.6

89.0

3.9

3.1

2.2

2.1

1.7

13/122

118

115

100

90.1

0.0

72

Sta	+	π	-	Elev
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		890.65		
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8+75				
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✓				
---	--	--	--	--

✓				
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9				
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March 3, 1960 41 22

84.

85.4	85.5	86.3	86.5	86.2	85.9	85.6	85.1	87.1
5.3	5.2	4.4	4.2	4.5	4.8	5.1	5.0	3.6
67	51	35	19		13	29	43	62

86.0	88.3	88.7	89.0		89.1	88.3
4.7	2.4	2.0	1.7		1.0	2.4
72	80	87	100		75	72

86.8	87.8	88.5	88.6
3.9	2.9	2.2	2.1
130	122	118	115

86.3	86.9	86.3	85.9	85.8	85.8	85.9	85.4	86.0
4.4	3.8	4.4	4.8	4.9	4.9	4.8	5.3	4.7
77	66	44	22		16	37	40	62

88.4	88.8	89.1	88.7
2.3	1.9	1.6	2.0
81	88	100	115

87.1
3.6
75

87.1	87.8	88.6
3.6	2.9	2.1
130	121	118

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		898.65		
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9+50				
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✓				
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✓				
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TP	8.28	895.49	3.44	887.21
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10				
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✓				
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✓				
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FX
JS
JH

21

March 3, 1960 48
March 7, 1960 23

88.2	86.2	85.1	85.6	85.4	85.8	85.1	84.8	85.0
25	45	50	5.1	5.3	4.9	5.0	5.9	5.7
81	77	48	22		20	39	44	64

89.1	89.5	89.3
------	------	------

1.6	1.2	1.4
87	100	114

87.0	87.4	89.1
------	------	------

3.7	3.3	1.6
130	126	118

Nail in PP

88.1	86.8	86.5	85.9	85.9	85.7	85.8	85.4	84.6	84.7
74	8.7	9.0	9.6	9.6	9.8	9.7	10.1	10.9	10.8
75	65	54	42	21	22	45	49	66	

89.3	89.3	89.9	89.6
------	------	------	------

6.2	6.2	5.6	5.9
83	88	100	115

84.8
10.7
75

88.0	88.1	89.3
------	------	------

7.5	7.4	6.2
130	124	119

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		895.49		
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10+24				
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✓				
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✓				
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+30				
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✓				
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✓				
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March 7, 1960 49
Rt. 24

Lt.

87.8	87.1	86.2	85.9	85.6	85.5	85.3	84.7
7.7	8.4	9.3	9.6	9.9	10.0	10.2	10.8
75	71	51	23		25	46	52

89.3	89.8	90.3	90.2		84.8
6.2	5.7	5.3	5.3		10.7
78	89	100	113		75

88.3	89.9
7.2	5.6
130	119

88.9	85.9	85.1	84.9	84.7	84.6	84.7	84.6	84.8
6.6	9.6	10.4	10.6	10.8	10.9	10.8	10.9	10.7
78	71	43	22		24	48	66	75

89.9	90.4	90.3
5.6	5.1	5.2
88	100	114

88.3	90.1
7.2	5.4
130	119

Sta

+

π

-

Elev

895.49

10 + 65

✓

✓

11

✓

✓

± March 7, 1960

50
25

Lt.

Rt

85.5

84.9

84.9

84.6

84.7

84.7

84.7

10.0

10.6

10.6

10.9

10.8

10.8

10.8

61

36

16

24

42

61

87.0

90.0

90.1

90.8

84.8

8.5

5.5

5.4

4.7

10.7

73

81

87

100

75

89.3

90.8

90.9

6.2

4.7

4.6

130

118

113

90.4

86.1

84.8

84.7

84.7

84.7

84.6

84.6

5.1

9.4

10.7

10.8

10.8

10.8

10.9

10.9

82

70

43

18

24

50

75

90.5

91.3

91.9

5.0

4.2

3.6

86

100

114

89.9

90.4

91.8

5.6

5.1

3.7

128

121

118

Sta	+	π	-	Elev.
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		895.49		
--	--	--------	--	--

11+50				
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✓				
---	--	--	--	--

✓				
---	--	--	--	--

12				
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✓				
---	--	--	--	--

✓				
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March 7, 1960 51 26

Lt.

Rt.

85.8	85.2	84.9	84.8	84.6	84.6	84.1
9.7	10.3	10.6	10.7	10.9	10.9	10.8
67	46	22		21	42	63
89.9	91.0	91.0	91.9			84.6
5.6	4.5	4.5	3.4			10.9
75	81	85	100			75

89.9	90.7	92.7	92.6
5.6	4.8	2.8	2.9
127	122	116	112

91.9	86.8	86.0	85.3	84.9	84.9	84.7	84.8
3.6	8.7	9.5	10.2	10.6	10.6	10.8	10.7
74	64	59	27		20	42	62

91.8	92.5	93.1	93.8				84.1
3.7	3.0	2.4	1.7				10.8
79	91	100	109				75

93.3	91.9
2.2	3.6
120	115

Sta	+	π	-	Elev.
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		895.49		
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12+35				
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✓				
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✓				
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+72				
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✓				
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✓				
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BM				
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5.70	899.43	1.70		
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			893.79	
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			893.77	
--	--	--	--------	--

				893.73
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March 7, 1960 52 27

BT

90.3	88.3	86.1	85.6	85.3	85.2	85.1	84.9
5.2	7.2	9.4	9.9	10.2	10.3	10.4	10.6
58	42	32	17		23	49	69

90.1	92.4	92.3	93.6
5.4	3.1	3.2	2.5
62	68	72	86

84.8
10.7
75

93.8	92.5	94.2	93.9
1.7	3.0	1.3	1.6
115	110	104	100

93.3	91.9	89.7	86.1	85.8	85.4	85.2	85.2	85.1
2.2	3.6	5.8	9.4	9.7	10.1	10.3	10.3	10.4
41	27	14	3		21	42	63	75

91.4	91.5	93.1	93.0
4.1	4.0	2.4	2.5
48	50	54	58

94.6	92.5	92.5	94.4	94.4	93.7
2.9	3.0	3.0	1.1	1.1	1.8
97	95	91	87	72	

101 spike in Gay Pole

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		899.43		
--	--	--------	--	--

13+00				
-------	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

+25				
-----	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

TP	5.21	900.36	4.28	895.15
----	------	--------	------	--------

FK
RG
JS
JH

March 8, 1960 53 28

Lt

Rt

92.6	94.4	94.2	93.2	90.5	88.1	85.7	85.6	85.4
6.8	5.0	5.2	6.2	8.9	11.3	13.7	13.8	14.0
38	34	27	16		14	26	45	66

92.6	93.3	93.3	93.5	94.0
6.8	6.1	6.1	5.9	5.4
40	44	50	64.5	79.5

85.4
14.0
75

95.0
4.4
90

94.1	93.7	93.7	94.5	94.0	93.4	89.9	86.1	85.6
5.3	5.7	5.7	4.9	5.4	6.0	9.5	13.3	13.8
55	41	36	24	5	4	22	43	66

94.5	95.1	95.7
4.9	4.3	3.7
69	76	80

85.6
13.8
75

94.6	94.3	94.0	94.2	94.3	93.9	92.6	89.1	87.2
4.8	5.1	5.4	5.2	5.1	5.5	6.8	10.3	12.2
58	45	31	20	5	26	35	47	67

94.8	95.2
4.6	4.2
65	78

86.1
13.3
75

Sta + π - Elev.

900.36

14

✓

+21

✓

+33

✓

March 8, 1960 54 29

95.0	95.0	94.8	94.7	94.9	95.5	95.1	94.5	94.1	93.3
5.4	5.4	5.6	5.7	5.5	5.9	5.3	5.9	6.3	7.1
44	40	27	14		11	27	45	55	68

94.3	94.3	94.4	00.4					92.8
6.1	6.1	1.0	0.0					7.6
47	49	58	69					75

95.3	94.9	94.9	94.8	95.0	95.4	95.7	94.5	94.1
5.1	5.5	5.5	5.6	5.7	5.0	4.7	5.9	6.3
40	34	22	9		12	30	51	68

94.8	94.8	00.4						95.4
5.6	5.6	0.0						5.0
43	45.5	54						75

95.5	95.0	95.0	94.9	95.0	95.4	97.5	96.8	95.7
4.9	5.4	5.4	5.5	5.4	5.0	2.9	3.6	4.7
36	30	18	6		10	16	31	49

95.1	95.1	96.5	00.4			95.6	94.1	94.3
5.3	5.3	3.9	0.0			4.8	6.3	6.1
38	40	43	49			75	72	62

Sta + π - Elev.

900.36

14+50

✓

+ 75

✓

TP 3.03 901.51 1.88 898.48

15

✓

March 8, 1960

55
30

94.9	95.6	95.0	95.1	95.0	95.1	97.7	97.2	97.0
5.5	4.8	5.4	5.3	5.4	5.3	2.7	3.2	3.4
33	30	24	13		15	19	30	45

94.9	00.4
5.5	0.0
35	43

94.2	94.2	97.8
6.2	6.2	2.6
75	70	61

95.0	95.5	95.4	95.4	95.3	95.2	95.4	97.2	97.4
5.4	4.9	5.0	5.0	5.1	5.2	5.0	3.2	3.0
28	26	22	9		2	17	22	40

95.0	96.7	00.4
5.4	3.7	0.0
32	34.5	40

98.1	97.8
2.3	2.6
63	55

95.1	95.1	95.6	95.5	95.5	95.5	95.4	94.6	94.6	96.9
6.4	6.4	5.9	6.0	6.0	6.0	6.1	6.9	6.9	4.6
26	24	21	17	5		14	17	20	27

96.9	01.5
4.6	0.0
30	36

98.1	97.9	97.3
3.4	3.6	4.2
75	63	45

Sta + π - Elev

901.51

15+50

,

✓

16

✓

+50

✓

March 8, 1960 56

14

RT 31

95.6

95.6

96.0

95.8

95.7

95.7

95.6

94.4

94.4

96.4

5.9

5.9

5.5

5.7

5.8

5.8

5.9

7.1

7.1

5.1

25

22

19

14

11

8

22

25

32

01.5-

0.0

33

95.0

95.3

95.7

6.5

6.2

5.8

75

68

51

95.3

95.3

96.3

96.2

96.4

96.2

96.2

94.6

94.6

6.2

6.2

5.2

5.3

5.1

5.3

5.3

6.9

6.9

23

20

17

13

13

19

22

25

99.9

00.0

00.4

95.0

95.7

97.4

96.7

16

1.5

1.1

65

5.8

4.1

4.8

29

37

56

75

59

39

30

97.0

97.7

97.6

97.1

97.2

96.9

96.7

95.7

95.7

4.5

3.8

3.9

4.4

4.3

4.6

4.8

5.8

5.8

41

31

21

13

13

21

23

26

96.3

96.4

93.7

94.0

94.7

96.4

96.7

5.2

5.1

2.8

7.5

6.8

5.1

4.8

60

75

75

62

39

33

30

Sta + π - Elev

901.51

17

✓

+50

18

BM

3.97 897.54 (897.54)

March 8, 1960 5732

2+

Rt

91.8	97.8	97.9	97.7	98.0	97.8	97.5	96.5	93.7
9.7	3.7	3.6	3.8	3.5	3.7	4.0	5.0	7.8
29	16	15	13		12	20	24	28

✓

91.8	91.1
9.7	10.4
34	50

89.0	90.1	91.8
12.5	11.4	9.7
75	62	45

99.1
24
99.6
0.9

Spike in 8" BE Fe Post stump Lt Sta 16+80

X-Sections - to Ground
Sta + x - Elev

7+50

8+00

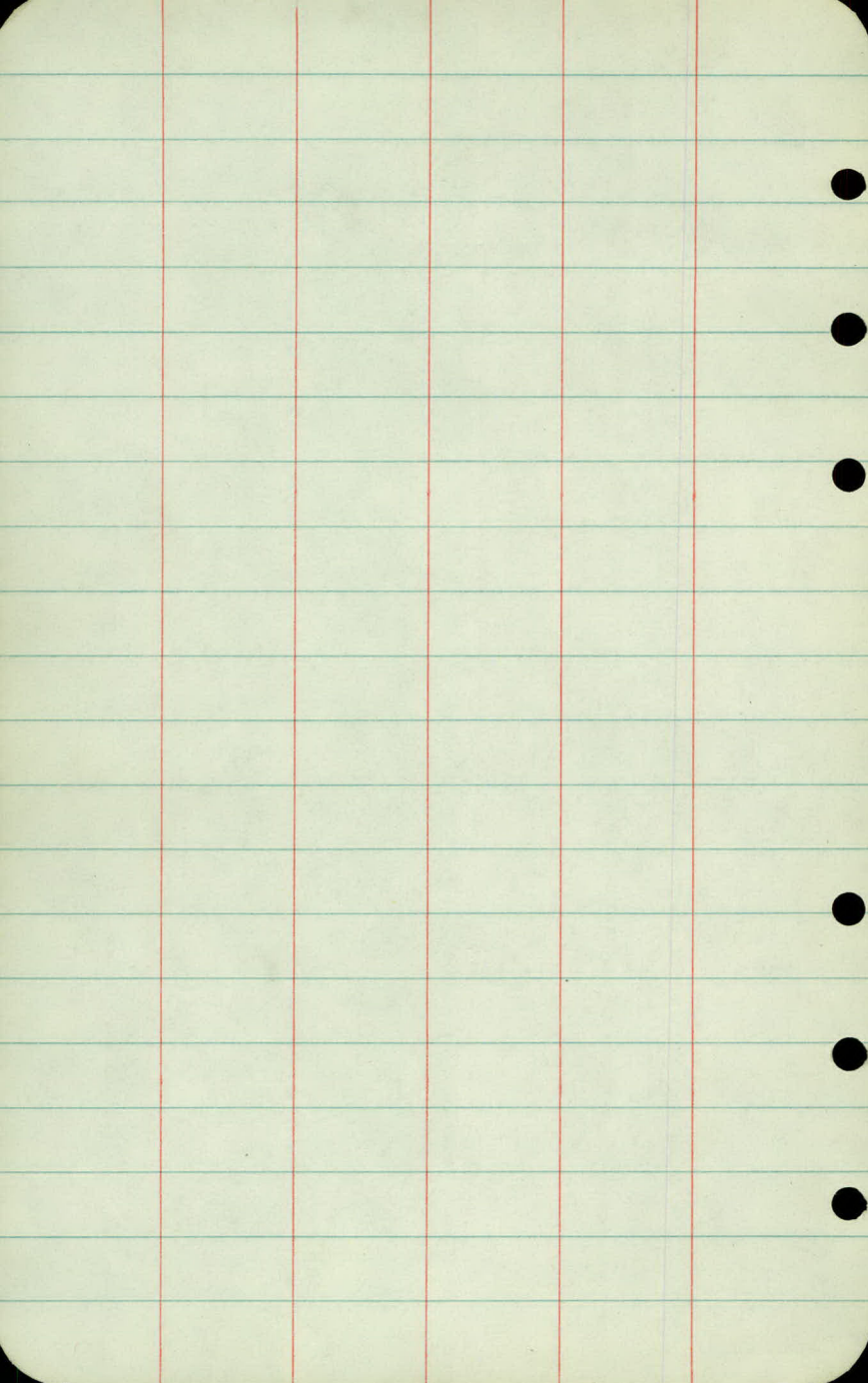
March 8, 1960 5833
RT

21

829

0.0	-07	-0.7	-0.9	0.0
66	41	19	2	6

0.0	-03	0.0
10	2	10



Soundings

+

Borings

Equipment

20 lb hammer

9" Auger

2" Auger

Borings taken

March 16, 17, 18 & 21, 1966

RG

GP George Patch

LT Louis Tima

RB Robt. Bigelbach

Sta 1490 30' Bl

Feet	Blows	Material
0-1		Anger Soundings Peat Fibers Muck
1-2		
2-3		
3-4		
4-5		
5-6		
6-7		
7-8		
8-9		
9-10		
10-11	13	
11-12	6	Equipment:
12-13	16	2" Earth Anger.
13-14	25	20
14-15	17	
15-16	12	
16-17	15	
17-18	30+	

March 8, 1960

60
35

Sta

1490

60' R/L

Feet	Feet	Blows	Blows	Material
19-20	0-1	one more push		Auger Soundings
20-21	1-2			
21-22	2-3			
22-23	3-4			
23-24	4-5	8		Fibrous Peat
24-25	5-6	7		
25-26	6-7	9		
26-27	7-8	21		
27-28	8-9	35		Muck
	9-10			
	10-11			
	11-12			
	12-13			
	13-14			
Equipment: 9" Peat Auger				
	15-16			
	16-17			
	17-18			
	18-19			

Sta 2450 30' Rt

Feet	Feet	Blows	Blows	Material
19-20	0-1	5		
20-21	1-2	18		
21-22	2-3	17		
22-23	3-4	17		
23-24	4-5	18		
24-25	5-6	25		
25-26	6-7	31		
	7-8			
	8-9			
	9-10			
	10-11			
	11-12			
	12-13			
	13-14			
	14-15			
	15-16			
	16-17			
	17-18			
	18-19			

Auger Soundings

Fibrous Peat

one Man Pushed

Equipment:
9" Peat Auger

FX
RG
JS Sta 2+50
JH

March 9, 1960
60' Rt

61
36

Feet	Feet	Blows	Blows	Material
19-20	0-1	one		
20-21	1-2	man		
21-22	2-3	Push		
22-23	3-4	7		
23-24	4-5	19		
24-25	5-6	27		
25-26	6-7	27	Push	
26-27	7-8	27		
27-28	8-9	30		
	9-10			
	10-11			
	11-12		one man	
	12-13			
	13-14			
	14-15			
	15-16			
	16-17			
	17-18			
	18-19			

Auger Soundings
Fibers
Material
Silt

Equipment 2" Earth Auger

Sta 3+00

£

Feet

Blows

Material

0-1

1-2

2-3

3-4

4-5

5-6

6-7

7-8

8-9

9-10

10-11

3

11-12

1

Equipment:

12-13

3

9" Peat Auger

13-14

6

20" hammer

14-15

9

15-16

15

16-17

25

17-18

36

↑
Auger Soundings

Fibers Peat

Muck

Silt

+ Sand

March 9, 1960 6237

Sta 3+00 30' Rt

Feet	Feet	Blows	Blows	Material
------	------	-------	-------	----------

0-1

1-2

2-3

18-19 3-4 12

19-20 4-5 18

20-21 5-6 22

21-22 6-7 20

22-23 7-8 30+

8-9

9-10

10-11 2

11-12 1

12-13 1

13-14 2

14-15 6

15-16 5

16-17 12

17-18 18

Auger Soundings

Fiberus Peat

Silt
+
Sand

Equipment:

9" Peat Auger

STADIA

AZ.

OBJECT

Sta 3+00 60' Rt

Feet

Blows

Material

18-19	0-1	2
19-20	1-2	11
20-21	2-3	20
21-22	3-4	18
22-23	4-5	25
23-24	5-6	35+

6-7

7-8

8-9

9-10

10-11

11-12

12-13

13-14

14-15

15-16

16-17

17-18

SOUNDINGS

Auger

Fiberus Peat

silt & Peat

silt & Sand

Man Push

Equipment:

9" Peat Auger

ELEV.

DIFF.

ROD

DOWN

ANGLE

DIST.

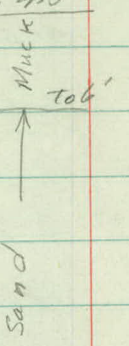
March 9, 1960 6338

Sta 3+50 \$ Elev = 884.8

Feet	Blows	Material
0-1	0	Fibrous Peat
1-2	0	
2-3	1	
3-4	3	Peat & Loam
4-5	4	
5-6	8	Blue Sandy Clay
6-7	6	
7-8	20	Sand
8-9	18	
9-10	9	
10-11	6	
11-12	16	
12-13	14	
13-14	7	
14-15	12	
15-16	30+	

Equipment: 20" Hammer
9" Foot Auger

Sta	3+50	30' Rt	Elev = 885.0
Feet		Blows	Material
0-1			↑
1-2			
2-3			
3-4		Pushed	Fibrous Peat
4-5			To 4.5'
5-6			Muck
6-7		15	↑
7-8		6	
8-9		20	Sand
9-10		21	
10-11		22	
11-12		32	



DIST. VERT. HORIZ. ROD DIFF. ELEV.

PK
RG
JS
JL
JH

March 10, 1960 6439

Sta 3450 60' Rt

Feet	Blows	Material
0-1		
1-2		
2-3		
3-4		
4-5	3	
5-6	12	
6-7	12	
7-8	9	
8-9	14	
9-10	25	
10-11	30 +	

0-1

1-2

2-3

3-4

4-5

5-6

6-7

7-8

8-9

9-10

10-11

Blows

3

12

12

9

14

25

30 +

Material

Fibrous
Peat

Peaty
Loam

Sandy Blue
Clay

STADIA

AZ.

OBJECT

Sta 3450 21' Lt ✓

Feet Blows Material

0-1

1-2

2-3

Pushed

Fibrous Peat
to 4.5'

3-4

12

4-5

3

Peaty Loam 9.
to 5.5'

5-6

12



6-7

9

Blue Clay

7-8

15



8-9

37

ELEV.

DIFF.

ROD

ROD

VERT
MALL

DIST.

March 10, 1960

65 40

Sta 4+00 £

Feet		Blows	Material
0-1			Peat
1-2			
2-3			
3-4			
4-5		17	
5-6	✓	18	
6-7		16	
7-8		21	
8-9		15	
9-10		19	
10-11		23	
11-12		16	
12-13		30+	

Auger Soundings

Clay

Sta 4+00 30' Lt

Feet

Blows

Material

0-1

1-2

2-3

3-4

4-5

5-6

6-7

7-8

8-9

without
coupling

Pushed

35+

✓

0

10

9

20

30+

Fibrous
Peat

To 3.5'

Clay

ELEV.

DIFF.

ROD

ROD
EQU.VERT.
ANGL.

DIST.

FR
RG
JS
JL

March 11, 1960

6641

Sta 4+00 30' R+

Feet Blows Material

0-1

1-2

2-3

3-4

4-5

5-6

6-7

13

30+

Peat

To 3.5'

clay

Sand

✓

Sta 4+00 60' Rt

Feet	Blows	Material
------	-------	----------

0-1		Peat
-----	--	------

1-2		
-----	--	--

2-3		
-----	--	--

3-4		
-----	--	--

4-5	6	
-----	---	--

5-6	30+	
-----	-----	--

6-7		
-----	--	--

Peat

Sand & Gravel

Blue Clay



March 11, 1960 67
42

Sta 4+50

60' RT

Feet

Blows

Material

0-1

1-2

2-3

3-4

30+

Silty
Sand

Gravel

Clay

Sta 4+50 30' Bl

Feet Blows Material

0-1

1-2

2-3

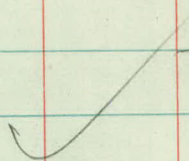
3-4

4-5

30

Silty Sand

Clay



Sta 4+50

March 11, 1960 6843

Feet

Blows

0-1

1-2

2-3

3-4

4-5

5-6

6-7

7-8

8-9

4

11

25

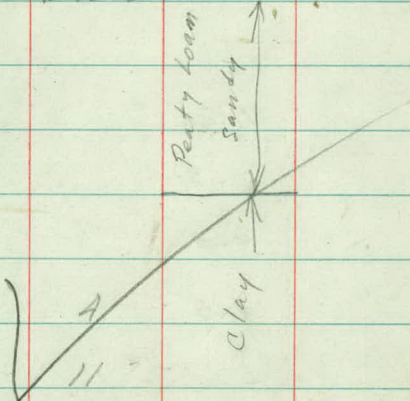
25

27

Peaty loam

Sandy

Clay



Sta 4+50 30 Lt

Feet

Blows Material

0-1

water table 1'

0-1' Pent
Small amt of
gravel

1-2

silt loam

2-3

3-4

silty
Clay (Black)

4.5'

4-5

5-6

4

6-7

11

7-8

15

8-9

15

9-10

31

Blue
Clay

Sta 5+00 March 11, 1960 69.44
60.1t

Feet	Blows	Material
0-1		Sand & Peat
1-2		
2-3		Silty Clay
3-4		
4-5	6	
5-6	6	Sand (Blue)
6-7	5	
7-8	1	Blue Clay
8-9	12	
9-10	21	
10-11	26	
11-12	32	

3' water
table

Sta 5+00 30'lt

Feet Blows Material

0-1

1-2

2-3

3-4

4-5

5-6

6-7

7-8

8-9

9-10

10-11

5

7

12

22

29

Sand
& Peat

Silty
Loam

Silt

Blue clay

T. 6.5'

Sta 5400 ±

March 15, 1968 70
Snowing 45

Feet

Blows

Material

0-1

1-2

2-3

3-4

4-5

5-6

6-7

7-8

8-9

52

5

10

21

31

Sand & Bat

Pasty Loam

Sandy Blue Clay

Blue Clay

Sta 5400 30' Rt

Feet

Blows Material

0-1

1-2

2-3

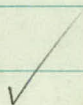
3-4

4-5

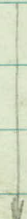
5-6

6-7

7-8



Sand & Peat



3.5

Sandy Blue Clay

4.5

2

11

23

30

Blue Clay

Sta 5400 60' Rt March 15, 1960 7146

Feet

Blows Material

0-1

1-2

2-3

3-4

4-5

5-6

6-7

1

4

13

34

Peat & Sand

Sandy Blue Clay

Sta 5+50 60' RT

Feet

Blows Material

0-1

Peat

1-2

✓

Sand & Peat

2-3

3-4

Silt Loam

4-5

2

5-6

1

6-7

4

7-8

4

8-9

10

8.3'

9-10

14

10-11

18

11-12

14

Blue Clay

12-13

21

13-14

33

March 11, 1960 727

Sta 5+50 30 R.R.

Feet	Blows	Materials
------	-------	-----------

0-1		Peat
-----	--	------

1-2		Sand
-----	--	------

2-3		Peaty Loam
-----	--	------------

3-4	✓	Silt Loam
-----	---	-----------

4-5		
-----	--	--

5-6		
-----	--	--

6-7	14	6.75'
-----	----	-------

7-8	26	Blue Clay
-----	----	-----------

8-9	32	
-----	----	--

Sta 5+50 £

Feet	Blows	Material
0-1		Peat
1-2		Sand
2-3		Silt
3-4		
4-5		<u>Total 5'</u>
5-6	9	
6-7	30	Blue clay

March 11, 1960 73
48

Sta 5+50 30' Lt

Feet	Blows	Material
0-1		Peat
1-2		"
2-3		Peaty loam
3-4		Silt-Sand
4-5		Blue Sand
5-6	8	Blue Sandy Clay
6-7	12	Blue Clay
7-8	10	
8-9	12	
9-10	24	
10-11	30+	

Sta 5+50 66' Lt

Feet	Blows	Material
0-1		Peaty Loam
1-2		Sand
2-3	✓	Silty Sand (Black)
3-4		"
4-5	0	Blue Sand
5-6	1	"
6-7	5	Blue Sandy Clay
7-8	11	Blue Clay
8-9	11	
9-10	24	
10-11	34	

March 11, 1960 74
49

Sta 6+00 60' Lt

Feet	Blows	Material
0-1		Sand
1-2		" water
2-3		silty Sand (Black)
3-4	✓ 2	"
4-5	4	"
5-6	4	" ✓
6-7	14	"
7-8	3	Muck
8-9	10	<u>To 8.5'</u> Blue Sand
9-10	15	↓
10-11	18	
11-12	13	
12-13	17	
13-14	30	

Sta 6+00 30' Lt

Feet

Blows Material

0-1

Peat

1-2

Sand

2-3

Silty Sand

3-4

"

4-5

1

"

5-6

0

"

6-7

4

Blue Sandy Clay

7-8

11

Blue Clay

8-9

14

9-10

22

10-11

21

11-12

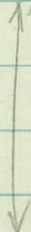
18

12-13

21

13-14

30+



Sta

6+00

±

March 11, 1960

75
50

Feet

Blows

Material

0-1

Sand

1-2

Sand

Water

2-3

Black Silt Sand

3-4

"

4-5

3

"

5-6

10

To 5.5'

Black Clay

6-7

16

↓

7-8

18

8-9

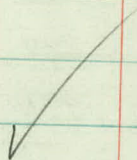
20

9-10

17

10-11.

29



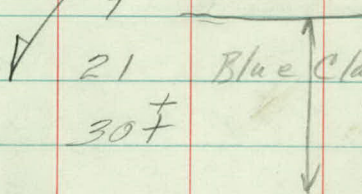
Sta 6+00 30' Rt

Feet	Blows	Material
0-1		Sand
1-2		"
2-3		"
3-4		"
4-5	6	Black Silty Sand
5-6	5	<u>To 5.5'</u> Blue clay
6-7	7	✓
7-8	16	
8-9	18	
9-10	21	
10-11	30	

March 15, 1960 76
60

Sta 6+00 60' Rt

Feet	Blows	Material
0-1		Sand
1-2		"
2-3		Black Silty Sand
3-4	1	"
4-5	2	"
5-6	6	Sandy Peat Lign
6-7	9	
7-8	21	Blue Clay
8-9	30 ⁺	
9-10		



Sta 6+50 60' Rt

Feet	Blows	Material
0-1		Peat + Sand
1-2		Silty Sand
2-3		"
3-4	1	"
4-5	2	Sandy Clay
5-6	3	Blue Clay
6-7	14	✓
7-8	26	
8-9	30+	

March 11, 1960

71
61

Sta 6+50

30' Rt

Feet

Blows

Material

0-1

Sand

1-2

Sand & Water

2-3

Silty Sand

3-4

"

4-5

4

"

5-6

8

"

6-7

5

Sandy Clay To 6.5'

7-8

12

Blue Clay

8-9

34

Sta 6+50 ±

Feet

Blows Material

0-1

Sand

1-2

"

Water 81.7

2-3

"

3-4

"

4-5

6

"

5-6

6

Black Sand

6-7

2

Muck

7-8

0

"

8-9

10

Blue Clay (Pure)

9-10

12

10-11

15

11-12

17

12-13

30+

Sta 6+50

30' Lt

78
62

Feet	Blows	Material
0-1		Sand
1-2		Sand Water
2-3		"
3-4		"
4-5		"
5-6	9	"
6-7	8	"
7-8	10	
8-9	3	
9-10	12	
10-11	9	
11-12	20	
12-13	24	
13-14	14	
14-15	21	
15-16	22	
16-17	30+	

Sta 6+50 60' L

Feet	Blows	Material
0-1		Sand
1-2		" water
2-3		"
3-4		"
4-5	11	"
5-6	24	"
6-7	20	
7-8	21	
8-9	18	
9-10	18	
10-11	15	
11-12	14	
12-13	30+	

Sta 7+00 60' Lt

Feet	Blows	Material
0-1		Sand
1-2		" Water
2-3		"
3-4		"
4-5	4	sandy Peat Loam
5-6	0	"
6-7	2	"
7-8	4	"
8-9	3	"
9-10	12	Sand
10-11	13	
11-12	13	
12-13	8	
13-14	7	
14-15	6	
15-16	21	
16-17	30	
17-18		

Pushed sounding rod to 13' during Borings

Sta 7+00 30' Lt

Feet	Blows	Material
0-1		Sand
1-2		" water
2-3		"
3-4		"
4-5		Peat & Silty peat
5-6	2	"
6-7	9	"
7-8	5	Sandy peat Loam
8-9	6	"
9-10	9	"
10-11	14	"
11-12	18	Sand
12-13	22	
13-14	23	
14-15	30+	

push
Rod
10-11.5'

11.5'

March 11, 1960

80
64

Sta 7+00 ±

Feet Blows Material

0-1

Sand

1-2

"

= 81.6
water

2-3

"

3-4

Sandy peat

4-5

peat

5-6

"

6-7

1

"

7-8

7

sandy peat

8-9

13

sand

9-10

27

Blue clay

10-11

20

11-12

23

12-13

21

13-14

21

14-15

30

Sta 7+00 30' Rt

Feet	Blows	Material
0-1		Sand
1-2		" water
2-3		"
3-4		peat
4-5	1	"
5-6	9	sandy loam
6-7	7	"
7-8	7	"
8-9	13	Blue sandy clay
9-10	17	
10-11	22	
11-12	22	
12-13	25	
14-15	35	

March 14, 1960 81
Cool -80 + 25° 65

R6
CW
LT
RB

Sta 7+00 60' RT

Feet Blows Material

0-1 Sand
1-2 " water

2-3 "

3-4 "

4-5 "

5-6 Blue Sandy Clay

6-7 "

7-8 20

8-9 34

9-10

Sta 7+50 60' RT

Feet

Blows Material

0-1

Sand

1-2

"

2-3

" water

3-4

Blue Sandy Clay

4-5

30

Blue gravelly Clay

5'-5 $\frac{1}{2}$

27

"

March 19, 1960 82
66

Sta 7+50 30' RT

Feet Blows

Material

0-1

Sand & gravel

1-2

Sand

2-3

" water

3-4

Blue Sand

4-5

Push

" To

5-6

Push

" Blue Sandy clay

6-7

18

Brown Sandy clay

7-8

31

Brown Clay

8-9

38+

Sta 7+50 ±

Feet Blows Material

0-1

Peat

1-2

Sandy peat

2-3

"

3-4

✓ "

4-5

Push

peaty loam

5-6

Push

Blue sandy clay

6-7

Push

"

7-8

Push

"

8-9

19

To 8.5
Brown clay

9-10

27

10-11

24

11-12

37

March 14, 1960 83

67

Sta 7+50 30' Lt

Feet Blows Material

0-1

peaty loam

1-2

" water

2-3

"

3-4

"

4-5

" ✓

5-6

"

6-7

"

7-8

"

8-9

"

9-10

Push

"

10-11

11

clay

11-12

20

12-13

31

Sta 7+50 60' RT

Feet Blows Material

0-1

Peaty loam

1-2

" water

2-3

"

3-4

"

4-5

"

5-6

"

6-7

"

7-8

8-9

"

9-10

"

10-11

"

11-12

"

12-13

"

13-14

9

Blue Sandy Clay

14-15

12

15-16

9

16-17

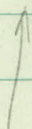
30

17-18

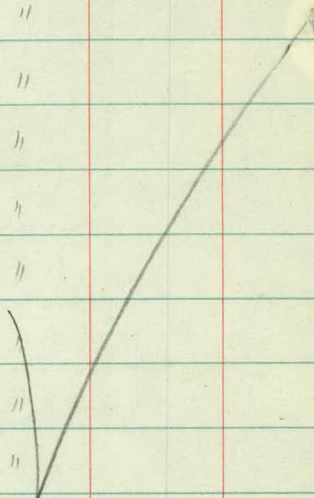
14

18-19

35



Push



March 14, 1960 84
68

Sta 8+00 60' LT

Feet	Blows	Material
0-4		Sand & water
4-10	Push	peat
10-11	10	silt
11-12	9	sandy silt
12-13	12	to 12.5' Blue clay
13-14	26	
14-15	12	
15-16	9	
16-17	19	
17-18	21	
19-20	15	
20-21	21	
21-22	18	
22-23	27	
23-24	34	

Sta 8+00 30' Lt

Feet

Blows Material

0-4

Sandy peat

4-7

Push

peaty loam

7-8

6

Sandy peat loam

8-9

1

Muck

9-10

13

Blue clay

10-11

20

11-11½'

30

March 14, 1960 85

69

Sta 8400 £

Feet	Blows	Material
0-4		peaty loam
4-5	Push	"
5-6	2	"
6-7	1	Blue clay
7-8	4	"
8-9	22	"
9-10	34	

Sta 8+00 30' RT

Feet

Blows Material

0-4

Sand & gravel 0-2

4-5

Push

2-5' peaty loam

5-6

15

Brown sandy clay

6-7

36

"

7-8

8-9

9-10

March 14, 1960 86

70

Sta 8+00 60' RT

Feet

Blows

Material

0-3

3-4

4-5

22

30+ Refusal

Sand & gravel
" clay

Sta 8+50 40' Rt

Feet	Blows	Material
0-3.5	6	Sand & gravel (Brown)
3.5-4	6	Silty sand
4-4.5	30	Sandy clay



March 14, 1960 87

71

Sta 8+50 20'12+

Feet

Blows

0-3

Sand & silty sand

3-5

Push

" "

5-6

30+

Brown & Blue Mottled
clay

6-7

✓

Sta 8+50

£

Feet

Blows

0-4

0-1 Sand

1-4 peaty loam

4-5

Push

"

5-6

22

sandy gravelly

Blue clay

6-9

14

7-8

8

8-9

27

9-10

30

March 14, 196088

72

Sta 8+50 30' Lt

Feet	Blows	Material
0-3		Sand
3-7	Push	3-5 peaty loam 5-7 peat
7-8	5	peaty loam
8-9	6	"
9-10	25	Blue Clay
10-11	30	
11-12		
12-13		

Sta 8 + 50

60' LT

Feet

Blows

Material

0-4

Sand
Peat (Fibrous)

4-8

Push

Peat (Fibrous)

8-9

5

To 8.5'

9-10

8

Peaty loam
9.5'
Sandy Blue clay

10-11

14

Blue Clay

11-12

24

12-13

30 +

March 14, 1968

89

13

Sta 9+0.0 60' LT

Feet	Blows	Material
0-3.5		Sand
3.5-4	8	"
4-5	8	"
5-6	2	Fibrous peat
6-7	4	" "
7-8	7	" 7.5' "
8-9	18	Sandy peat
9-10	10	sand
10-11	10	
11-12	16	
12-13	17	2" Auger to 12.5'
13-14	16	
14-15	16	
15-16	30 +	
16-17		

Sta 9+00 30' Lt

Feet	Blows	Material
0-4		0-1 Clay 1-4 Sand
4-5	16	Sand Water
5-6	2	peat
6-7		"
7-8		"
8-9	8	Sand
9-10	7	"
10-11	10	Blue Clay
11-12	28	
12-13	36	

March 14, 1960 90
74

Sta 9+00 ±

Feet	Blows	Material
0-4		Clay to Sandy clay
4-6	Push	Peat
6-7	5	Peat 6.5' Blue Sand
7-8	✓ 8	Sand
8-9	19	Brown Sandy Clay
9-10	27	
10-11	30+	
11-12		
12-13		

Sta 9+00 25' RT

Feet	Blows	Material
0-4		0-2 Clay 2-4 Peat
4-5	18	To 4.5 Sand Blue Clay
5-6	3	Sand
6-7	30+	Clay
7-8		
8-9		
9-10		
10-11		

March 14, 1969

75

Sta 9+00 50' RT

Feet	Blows	Material
------	-------	----------

0-3

Clay

3-4

6

Brown Clay

4-5

30

Blue, Clay

Stal 9+50 65' RT

Feet	Blows	Material
0-4		0-2 Peat 2-4 Fibrous peat
4-5	13	sand
5-6	7	sandy peat
6-7	15	clay
7-8	26	✓
8-9	30	

March 14, 1960 92

Sta 9+50 40' RT

76

Feet	Blows	Material
0-3		0-1 clay 1- peat
3-5	Push	Peat
5-6	3	sandy peat
6-7	1	Peat loam
7-8	3	Sand ^{to 7.75'}
8-9	23	Blue Clay
9-10	22	
10-11	22	
11-12	30	

Sta 9450 ~~4~~

Not Bored

March 14, 1960 ⁰⁹³
77

Sta 9+50

30' Lt

Feet	Blows	Material
0-4		Clay
4-10	Push	Fibrous peat
10-11	9	silt
11-12	6	"
12-13	5	" 2" Auger push to 13'
13-14	2	Silty clay
14-15	10	" To 15'
15-16	11	Blue Clay
16-17	14	
17-18	24	
18-19	21	
19-20	30+	

Sta 9+50 60' Lt

Feet	Blows	Material
0-3		0-2 Clay peat
3-4	Push	Fibrous peat
4-5	3	"
5-6		"
6-7		"
7-8		"
8-9		"
9-10	Push	"
10-11		"
11-12		"
12-13		Fibrous peat
13-14	4	sand
14-15	8	silty clay
15-16	9	
16-17	11	
17-18	14	to 17.5' Blue Clay
18-19	9	"
19-20	8	"
20-21	6	"

2" Auger borings

Sta 9+50 60' Lt (cont) 94

Feet Blows 78

21-22

✓ 13 Blue Clay

22-23

✓ 38+ "

Sta 10+00 50' Lt

Feet	Blows	Material	
0-3		Sandy clay (Brown)	
3-4	2	"	
4-5	4	" to 5'	
5-6	3	Fibrous peat	
6-7	3	"	
7-8	4	"	
8-9	5	"	
9-10	10	" clay (Trace)	
10-11	8	peaty loam	
11-12	8	"	
12-13	9	sand	2" Auger
13-14	8	13' trace of brown clay	
14-15	9	Brown clay	
15-16	10	"	
16-17	9	mottled clay to 17'	
17-18	16	gray clay	
18-19	25	"	
19-20	23		
20-21	31		

March 14, 1960 95

Sta 10+00

30' Lt

79

Feet	Blows	Material
0-3		Clay
0-12	Push	Fibrous peat to 10' peaty loam to 12'
12-13	13	Blue-gray Clay
13-14	13	"
14-15	12	"
15-16	10	"
16-17	14	"
17-18	12	"
18-19	9	
19-20	20	
20-21	16	
21-22	30+ refusal	

Mottled clay Red & gray

Sta 10+00 &

Feet	Blows	Material
------	-------	----------

0-3

Clay

3-10

Push

Fibrous Pent to 10'

10-11

8

silt

11-12

9

"

12-13

8

Silty Clay

13-14

30

sand (coarse sand)

14-15

32

15-16

16-17

March 14, 1960 96

Sta 10+00 30' Rt

80

Feet	Blows	Material
0-3		0-3 clay
3-10	Push	Fibrous peat
10-11	9	Blue clay
11-12	5	"
12-13	13	"
13-14	19	
14-15	30+	
15-16		
16-17		

Sta 10+00 60' Rt

Feet Blows Material

0-3

Fibrous peat

3' water

3-11

Push

to 9'

11-12

5

9' to 11' Blue clay

Blue clay

12-13

9

11

13-14

15

14-15

32+

15-16

16-17



381.7

March 14, 1960 97
81

Sta 10+00 100' Rt

Feet Blows Material

0-3

Fibrous peat (water at 3')

3-9

Push

peat + mucky peat

9-10

12

Blue clay

10-11

22

11

11-12

35+

12-13

13-14

Sta 10+50 100' R+

Feet	Blows	Material
0-3		Fibrous peat + water
3-10	Push	Fibrous peat + muck
10-11	9	Blue clay
11-12	16	
12-13	24	
13-14	30+	✓
14-15		

March 14, 1960

98

82

Sta 10+50 60'RT

Feet Blows Material

0-3 Peat water at 3'

3-10 Push Fibrous peat

10-11 9 Blue Clay

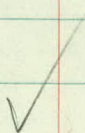
11-12 10 "

12-13 11 "

13-14 14

14-15 24

15-16 33



Sta 10+50 30' RT

Feet	Blows	Material
------	-------	----------

0-3		Peat
-----	--	------

3-10	Push	Fibrous Peat & water
------	------	----------------------

10-11	6	Blue Clay
-------	---	-----------

11-12	12	
-------	----	--

12-13	14	
-------	----	--

13-14	27	
-------	----	--

14-15	25	
-------	----	--



15-16	30+	
-------	-----	--

16-17		
-------	--	--

March 15, 1960 99
Cool 10°

RG 10 + 50 £

83

CW
LT
RB

Feet Blows Material

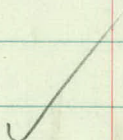
0-3 Peat

3-13 Push Fibrous peat + water - 81.7

13-14 9 Silt to 13.5'
Blue clay

14-15 40 +

15-16



Sta 10+50 25' LT

Feet	Blows	Material
------	-------	----------

0-3		Peat
-----	--	------

3-10	Push	Fibrous peat + water
------	------	----------------------

10-11	8	To 10.5'
-------	---	----------

		10.5'
		Blue clay

11-12	11	"
-------	----	---

12-13	24	"
-------	----	---

13-14	32	
-------	----	--

14-15		
-------	--	--

15-16		✓
-------	--	---

March 15, 1960 100

Sta 10+50 60' Lt

84

Feet	Blows	Material
------	-------	----------

0-3		Peat
-----	--	------

3-9		
-----	--	--

	Push	
--	------	--

		Peat
		Fibrous peat to 8'
		<u>Blue clay</u>

9-10		
------	--	--

	8	
--	---	--

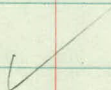
		"
--	--	---

10-11		
-------	--	--

	25*	
--	-----	--

11-12		
-------	--	--

	30+	
--	-----	--



Sta 11+00 60' LT

Feet	Blows	Material
------	-------	----------

0-3		Peat
-----	--	------

to 4.5'

3-7	Push	4.5' to 7' sandy loam
-----	------	-----------------------

7-8	17	Blue Clay
-----	----	-----------

8-9	31+	
-----	-----	--

9-10		
------	--	--

March 15, 1969
101
85

Sta 11+00 30' Lt

Feet	Blows	Material
0-3		Peat
3-7	Push	Fibrous Peat to 6' 6-7' Muck
7-8	6	Blue sandy clay
8-9	4	"
9-10	15	Blue clay
10-11	23	
11-12	30+	

Sta 11+00 ±

Feet Blows Material

0-3

Peat & water

817

3-10

Push

Fibrous peat to

10.5'

10-11

5

sandy loam

11-12

5

sandy loam

12-13

4

"

13-14

5

"

14-15

7

"

15-16

10

Blue clay

16-17

23

17-18

20

18-19

21

19-20

22

20-21

35+

March 15, 1960 102
86

Sta 11+00 30' RT

Feet Blows Material

0-3

Peat

water = 84.6

3-14.5 Push

Silty clay ^{10.5'}

14.5-15 8

Blue clay

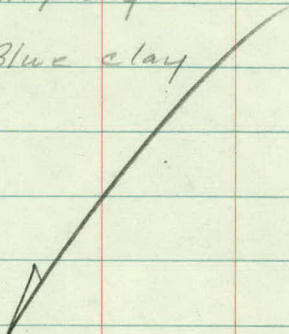
15-16 7

16-17 11

17-18 11

18-19 20

19-20 30



Sta 11+00 60' Rt

Feet	Blows	Material
------	-------	----------

0-3		
-----	--	--

		Peat
--	--	------

3-14		
------	--	--

	Push	
--	------	--

		Fibrous peat <u>To 9'</u> 9'-13' silt
--	--	--

14-15		
-------	--	--

	15	
--	----	--

		13' Blue clay
--	--	---------------

		"
--	--	---

15-16		
-------	--	--

	14	
--	----	--

		"
--	--	---

16-17		
-------	--	--

	17	
--	----	--



17-18		
-------	--	--

	23	
--	----	--

18-19		
-------	--	--

	30+	
--	-----	--

19-20		
-------	--	--

March 15, 1960

103

87

Sta 11+00 100' RT

Feet	Blows	Material
------	-------	----------

0-3

0-3 Peat water

Fibrous peat to 8'

3-11

Push

8'-10 Silt

10' Blue clay

11-12

7

"

12-13

10

"

13-14

3

11

14-15

16

15-16

22

16-17

30+



Sta 11+50 100' RT

Feet	Blows	Materials
------	-------	-----------

0-3		Peat
-----	--	------

		Fibrous peat to 7.5'
--	--	----------------------

3-10		
------	--	--

	Push	
--	------	--

		7.5' silt
--	--	-----------

10-11		
-------	--	--

	13	
--	----	--

		Blue clay
--	--	-----------

11-12		
-------	--	--

	11	
--	----	--

12-13		
-------	--	--

	10	
--	----	--

13-14		
-------	--	--

	7	
--	---	--

14-15		
-------	--	--

	10	
--	----	--

15-16		
-------	--	--

	25	
--	----	--

16-16.5		
---------	--	--

	23	
--	----	--

		Refusal
--	--	---------

March 15, 1960

104

88

Sta 11+50 60' RT

Feet Blows Material

0-3

Peat
Fibrous Peat to 8.5'

3-14 Push

8.5' silt to 13'

14-15 10

13'-Blue Clay

15-16 27

"

16-17 14

17-18 18

18-19 31+

19-20

Sta 11+50 30' RT

Feet	Blows	Material
------	-------	----------

0-3		Peat
-----	--	------

3-14	Push	Fibrous peat to 8'
------	------	--------------------

		8' silt to 14'
--	--	----------------

14-15	11	Blue Clay
-------	----	-----------

15-16	24	
-------	----	--

16-17	30	
-------	----	--

17-18	1	
-------	---	--

18-19		
-------	--	--

19-20		
-------	--	--



March 15, 1960 105

Stall 11450 L

89

Feet Blows Material

0-3

Peat water

3-9

Push

Fibrous peat to 6.5' then
layer of sandy silt
to 8.5' 8.5' to 9.0' silt

9-10

11

9' Blue sand

10-11

4

silt

11-12

3

"

12-13

4

"

13-14

5

"

14-15

6

"

15-16

12

Blue clay

16-17

25

17-18

31

18-19

19-20

Sta 11+50 30' Lt

Feet	Blows	Material
0-3		Peat water
3-5		Fibrous peat
5'-6.5'	Push	Silt
6.5'		Silty sand or
11-12	5	Sandy loam to 8.5'
8.5' to 13'		sandy Blue clay
12-13	6	
13-14	12	Blue clay
14-15	22	
15-16	20	
16-17	30	
17-18		

March 15, 1960 106
90

Sta 11+50 60' LT

Feet	Blows	Material
------	-------	----------

0-3		Peat to 5'
-----	--	------------

		5' to 5.5' sand
--	--	-----------------

3-5.5	Push	
-------	------	--

		5.5' Blue Clay
--	--	----------------

5.5-6	6	
-------	---	--

		Blue Clay
--	--	-----------

6-7	26	
-----	----	--

7-8	30	
-----	----	--

Sta 12+00 50' Lt

Feet	Blows	Material
------	-------	----------

0-3

Peat

3-4

Push

Sand

4-5

22

Brown Clay

5-6

35+

6-7



7-8

March 15, 1960 107
91

Sta 12+00 25' LT

Feet	Blows	Material
------	-------	----------

0-3		Peat
-----	--	------

3-4	Push	Peat
-----	------	------

4-5	5	Loam
-----	---	------

5-6	4	Blue clay
-----	---	-----------

6-7	10	Blue Clay
-----	----	-----------

7-8	23	
-----	----	--

8-9	30+	
-----	-----	--

Sta 12+00 ±

Feet	Blows	Material
------	-------	----------

0-3

Peat

3-7

Push

Peaty Loam

7-8

6

Loam

8-9

14

Blue Clay

9-10

20

10-11

24

11-12

30

12-13

7

March 15, 1960 108

Sta 12+00 30' RT

92

Feet Blows Material

0-3 Peat

3-9 Push Fibrous peat to 7'
7'-9' sandy loam

9-10 3 Loam

10-11 2 "

11-12 1 "

12-13 7 " 12.5'
Blue clay

13-14 ✓ Blue clay

14-15 23

15-16 21

16-17 20

17-18 21

18-19 30+

Sta. 12+00 60' RT

Feet	Blows	Material
------	-------	----------

0-3		Peat
-----	--	------

3-13		Fibrous Peat to 8'
------	--	--------------------

	Push	8-13' silt
--	------	------------

13-14		Blue Clay
-------	--	-----------

	22	
--	----	--

14-15		
-------	--	--

	30	
--	----	--

15-15.5		
---------	--	--

	23	
--	----	--

March 15, 1960 109

Sta 12400 100' RT

93

Feet	Blows	Material
0-3		Peat
3-13	Push	3'-Fibrous Peat to 9' 9'-13' Silt
13-14	19	Blue Clay
14-15	16	
15-16	14	
16-17	17	
17-18	16	
18-19	30	

Sta 72736 60' RT

Feet Blows Material

0-3

Peat

3-12

Push

3' Fibrous Peat to 7'
7' Peaty Loam to 8'
8' Sandy Loam to 10.5'
10.5 to 12' Blue Clay

12-13

21

13-14

19

14-15

20

15-16

27

16-17

30

March 15, 1960 110

Sta 12+36 30' RT

94

Feet Blows Material

0-3

Peat

3-8

Push

3' Fibrous Peat to 5'

5' Sand to 6.5'

6.5' to 8.5' Sandy clay (Blue gray)

8-9

9

8.5' to 9' Blue clay

9-10

20

Blue clay

10-11

22

11-12

24

12-13

25

13-14

14
30

Sta 12+36 £

Feet	Blows	Material
0-3		Peat
3-4	Push	3-5' Peaty Loom 5-6' sandy clay
6-7	9	6' Blue Clay
7-8	32+	7.5' Brown clay
8-9		
9-10		

March 15, 1960 III

Sta 12+36 20' Lt

95

Feet	Blows	Material
0-3		Peat
3-4	Push	Peat to 3.5'
4-5	9	3.5 to 4.5'
5-6	25	Sandy Clay
6-7	32+	4.5'-6'
7-8		Blue Brown Clay (Mottled)

0-3

Peat

3-4

Push

Peat to 3.5'

4-5

9

3.5 to 4.5'

Sandy Clay

5-6

25

4.5'-6'

Blue Brown Clay (Mottled)

6-7

32+

7-8

12+72 £

Feet	Blows	Material
0-3		Peat to 3.75'
3-4	8	Brown clay to 4'
4-5	30+	Brown clay
5-6		

March 15, 1960

112

12+72

30' RT

96

Feet	Blows	Material
------	-------	----------

0-3

Peat

3-5.5

Push

3-4.5' Sandy silt

4.5-5.5' Sandy clay (gray)

5.5-6

10

Brown Clay

6-7

30 +

Brown Clay

7-8

8-9

9-10

Sta 12+72 60' RT

Feet	Blows	Material
0-3		Peat to 4'
3-6	Push	4'-6' Fibrous Peat
6-7	6	Sandy Blue Clay
7-8	2	silt
8-9	18	^{Sandy} Blue Clay
9-10	14	
10-11	15	
11-12	31	
12-13		
13-14		

March 15, 1960

113

Sta 12+72 100' RT

97

Feet	Blows	Material
0-3		0-4' Peat
3-10	Push	4'-7.5' Fibrous Peat 7.5'-9' sandy
10-11	X6	9'-11' Blue clay
11-12	25	Blue clay
12-13	30+	
13-14		
14-15		

Sta 13+00 35' RT

Feet	Blow	Material
0-3		feet to 4'
3-6	Push	
6-7	16	Blue clay
7-8	17	
8-9	3X	
9-10		

March 15, 1960 114
98

Sta 13+00 60' RT

Feet Blows

Material

0-3

Peat

3-4 Push

Peat

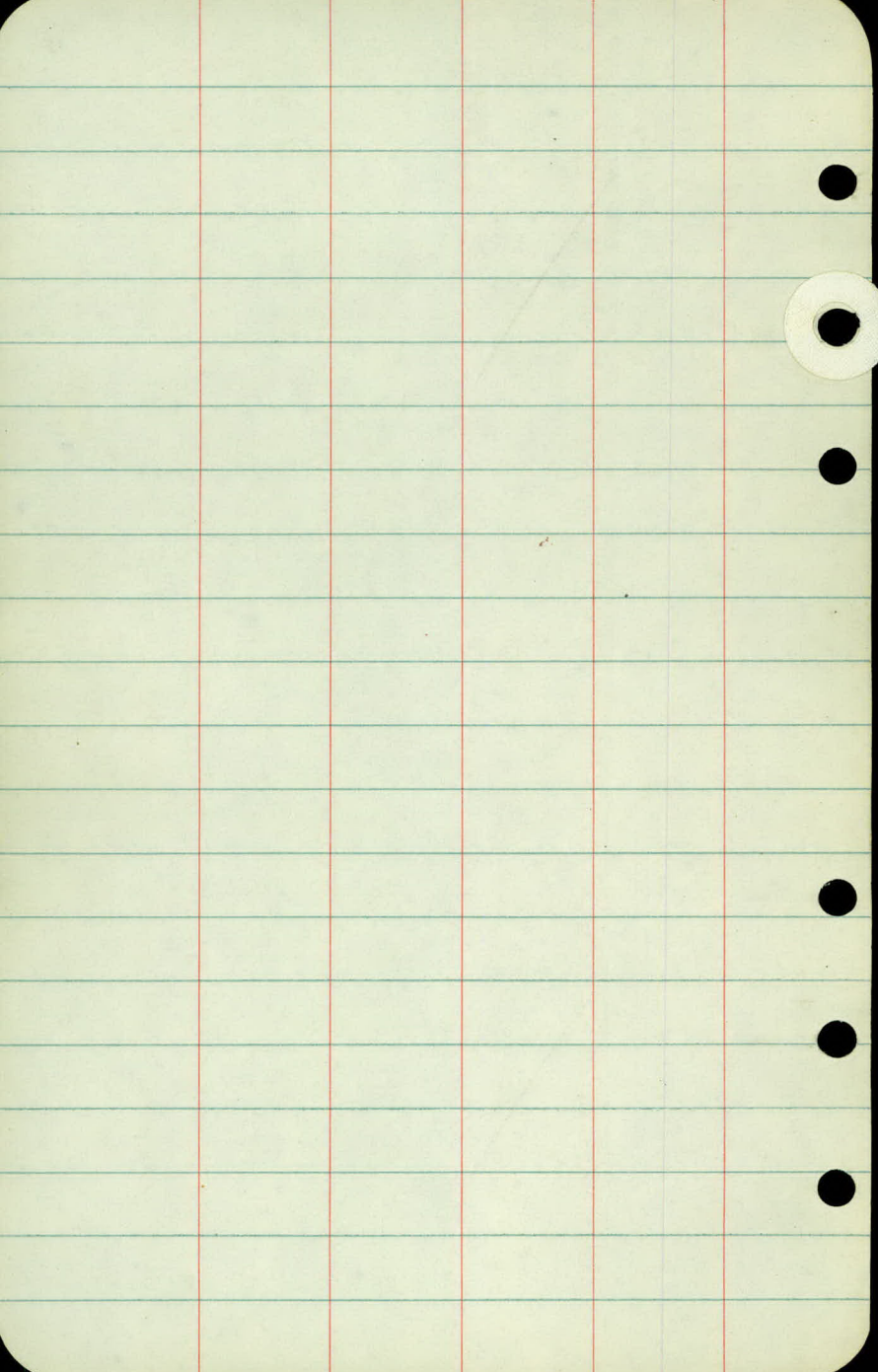
4-5 11

sandy Blue Clay

5-6 244 refusal Blue Clay 5.5'

6-7

7-8



RG
RR
RH
MN

Sept 6, 1960
Hot

Sounding & Soil Borings
Sta 2+00; 2+50; 3+00
all 80' Rt &

Sta 2+00 80' RT &

Depth	Blows	Material
0-1	↑	Peat water to top
1-2		Fibrous peat (orange)
2-3		" " "
3-4		" " "
4-5		" " "
5-6		" " "
6-7		" " Very Dark Brown
7-8		" " "
8-9		Muck very wet
9-10		"
10-11		"
11-12		"
12-13		<u>" To 12' 5"</u> Black Muck w/silt
13-14		"
14-15		"
15-16	Push	Sil (silt loam) Black
16-17	↓	Si (silt) Black w/VF sand
17-18	15	Si " " "
18-19	20+	Blue Clay till w/flecks of Brown

Sept 6, 1960

Sta 2+50 80 RT

Depth	Blows	Material
0-1	↑	Peat Water to top
1-2		Fibrous Peat (orange)
2-3		" " "
3-4		" " "
4-5		" " "
5-6		" " "
6-7		" " Very dark Brown
7-8		" " "
8-9		" " "
9-10		to 9.5' " "
10-11		silty peat (Blackish/Very Wet
11-12		"
12-13		"
13-14	Push	silt Loam
14-15		" "
15-16		silt (silty clay / loam) w/ F sand
16-17		"
17-18		"
18-19	↓	" w/ (white sand grains) Till

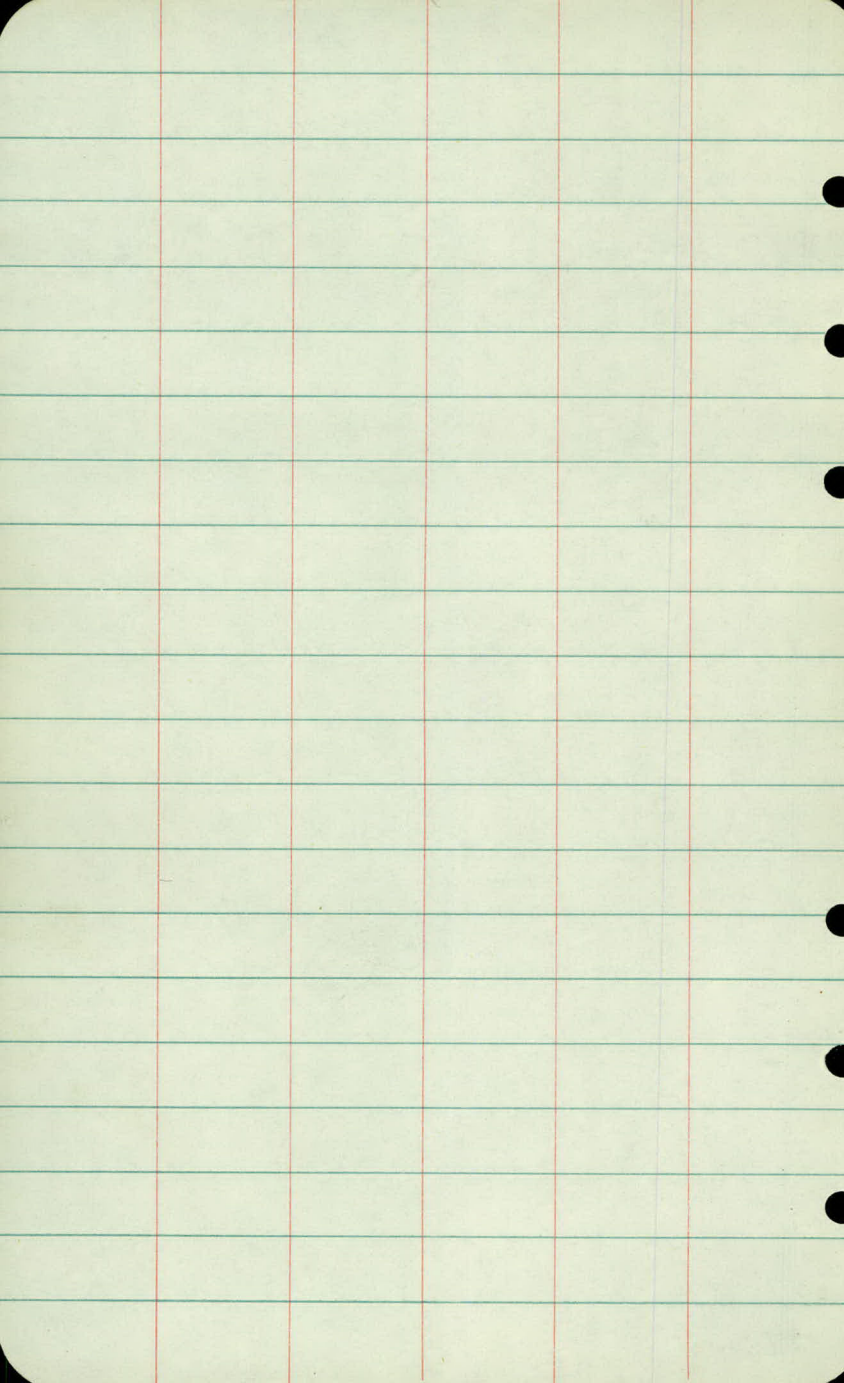
2+50 (cont)

- 19-20 Push SiCl w/white sand grains) wet
- 20-21 Push " " " wet
- 21-22 20 + Blue clay to 21.5'
Brown silt loam (dry) with fine
quartz crystals + organic
matter

Sept 6, 1960

Sta 3+00 80' RT

Depth	Blows	Material
0-1	↑	Peat
1-2		"
2-3		Fibrous Peat (Orange)
3-4	Push	"
4-5		"
5-6	↓	Fibrous peat very wet (Brown)
6-7		Muck (semi liquid peat)
7-8		to 7.5' Blue Sand till w/ some gravel
8-9		"
9-10	↓	"
10-11	12	Blue sandy Clay Till
11-12	10	"
12-13	12	"
13-14	23	"
14-15		
15-16		
16-17		
17-18		
18-19		



PL - Peaty Loam
 S = sand C = clay
 8:00 AM - 4:30

March 11, 1960 115
 99

Sta	LT		RT	
3+50	S 20'		P 30'	P 60'
4+00	S 30'	P S	P 30'	P 60'
4+50	S 30'	P S	P 30'	P 60'
5+00	60'S 30'P	P S	30'P	60'P
5+50	60'S 30'P	P S	30'S	60'S
6+00	60'S 30'S	S S	30'S	60'S New Blade
6+50	60'S 30'S	S S	30'S	60'S
7+00	60'S 30'S	S S	30'S	60'S
7+50	60'S 30'PL Peaty Loam	S S	30'S	60'S 4C
8+00	60'S 30'PL	PL 1-3' New Blade S+G 3'	30'PL	60'S 12HM
8+50	S 60'	S 1-4 S 1-3 PL 3'	PL-S 20'	60'S 12:30 Lunch 1-4 S+G C 4'
9+00	SC 0-2 60'S L 2-3 S-3'-C	C 0-2' 30'PL 2'- C	C 0-3' 25'	C 2'- 50'
9+50	C 60'	C 30'	C 40'	PL 65'
10+00	C 50'	C 0-4' P 1-4' S 30'	C 0-4' 30'	P 60'
1+50	P 60'	P 25' 3'-FP	P 30'	P 60'
11+00	P 60'	P 30'	P 30'	P 60'
11+50	3:00 P 60'	P 30'	P 30'	P 60'
12+00	50' SC 2-4'	P 25'	P 30'	P 60'

Sta	LT	RT
12+36	L 0-2 C2 → 20'	P 30' 60'
12+72	C1 →	P 30' 60' 100'
13+00		P 35' 60'

100 holes

Lake Josephine Park
Borings & Soundings
sta 0+00 to 1+90

RG

JL

JH

3 pages

Sta 0+00 30' Rt

Depth	Blows	Material	
0-1		Peat	6" Frost Post hole digger
1-2		Brown Sand	
2-3	19	" Sand	2" Auger
3-4	25+	" Sand	

Sta 0+00 60' Rt.

Depth	Blows	Material	Frost to 24"
0-1		Peat w/ sand	Post hole digger
1-2		Sandy Peat w/ fine gravel	
2-3		Peat	2" Auger
3-4	Push	"	↓
4-5	2	"	
5-6	7	Gray sand	
6-7	11	"	
7-8	8	"	
8-9	18	Blue Sandy Clay	
9-9.5'	20		

R6
JL
JH

April 22, 1960
Warm, Windy

117
2

Sta 0+50 35' Rt No Frost

Depth	Blows	Material	
0-1		Peat	
1-2		Brown Sand	Post Hole digger
2-3	11	" "	to 3'
3-4	16	" "	2" Auger
4-4 1/2	20	" "	"

Sta 0+50 70' Rt. Frost to 3'

Depth	Blows	Material	
0-0.5		Peat	
0.5-1		Brown Sand	
1-2		"	
2-3		"	Post hole digger
3-4	1	Fibrous Peat	2" Auger
4-5	1	"	
5-6	3	To 5.75' Sand (Gray)	
6-7	6	Gray Sand	
7-8	11	Blue Sandy Clay	
8-9	22 +	"	

Sta 1+00 27' Rt No Frost

Depth	Blows	Material	
0-1		Peat	
1-2		Brown Sand	
2-3		" "	Post hole digger
3-4	6	" "	2" Auger
4-4.5	21+	" "	"
4.5-6'		Sand	"

Sta 1+00 75' Rt. 24" Frost

Depth	Blows	Material
0-0.5		Peat
0.5-1		Sand & Peat
1-1.5		"
1.5-2		Sandy Peat
2-3		Peat
3-4		"
4-5		"
5-6		"
6-7		"
7-8	Push	"

R6
JL
JH

April 22, 1960

178
3

Sta 1+00 75' RT (cont)

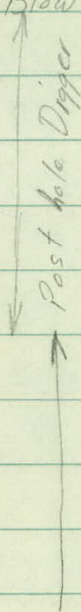
Depth	Blows	Material	
8-9	9	Brown Sand	2" Auger
9-9.5	21+	Sand	"
9.5-10		Sand	"

Sta 1+50 20' RT 12" Frost

Depth	Blows	Material
0-1		Peat
1-2		Fibrous Peat
2-3		Brown Sand
3-3.5		" "
3.5-4		Fibrous Peat
4-5	4	Gray Sand
5-6	3	Gray Sand
6-7	21+	Blue Clay

Post Hole Digger

Sta 1+50 70' RT

Depth	Blows	Material
0-1	 Post hole Digger	Peat
1-2		Fibrous Peat
2-3		" "
3-4		" "
4-5		" "
5-6	 Push	" "
6-7		Muck
7-8		"
8-9		"
9-10		"
10-11	 Push	Gray Sand
11-12		Gray Sand
12-13	15	Blue Clay
13-14	26	

Lexington Ave.

Co Rd "C2" to Co Rd. "D"

Sta + π - Elev.

PC 4.37 93.46

0+00

4.37 89.29

0-100'

4.46 89.20

0-200

4.34 89.32

BM 9.32 906.84

892.54

17+50

7.52 99.34

+78.9 PT

6.70 900.16

18

6.01 00.85

+50

4.21 02.65

19

2.29 4.57

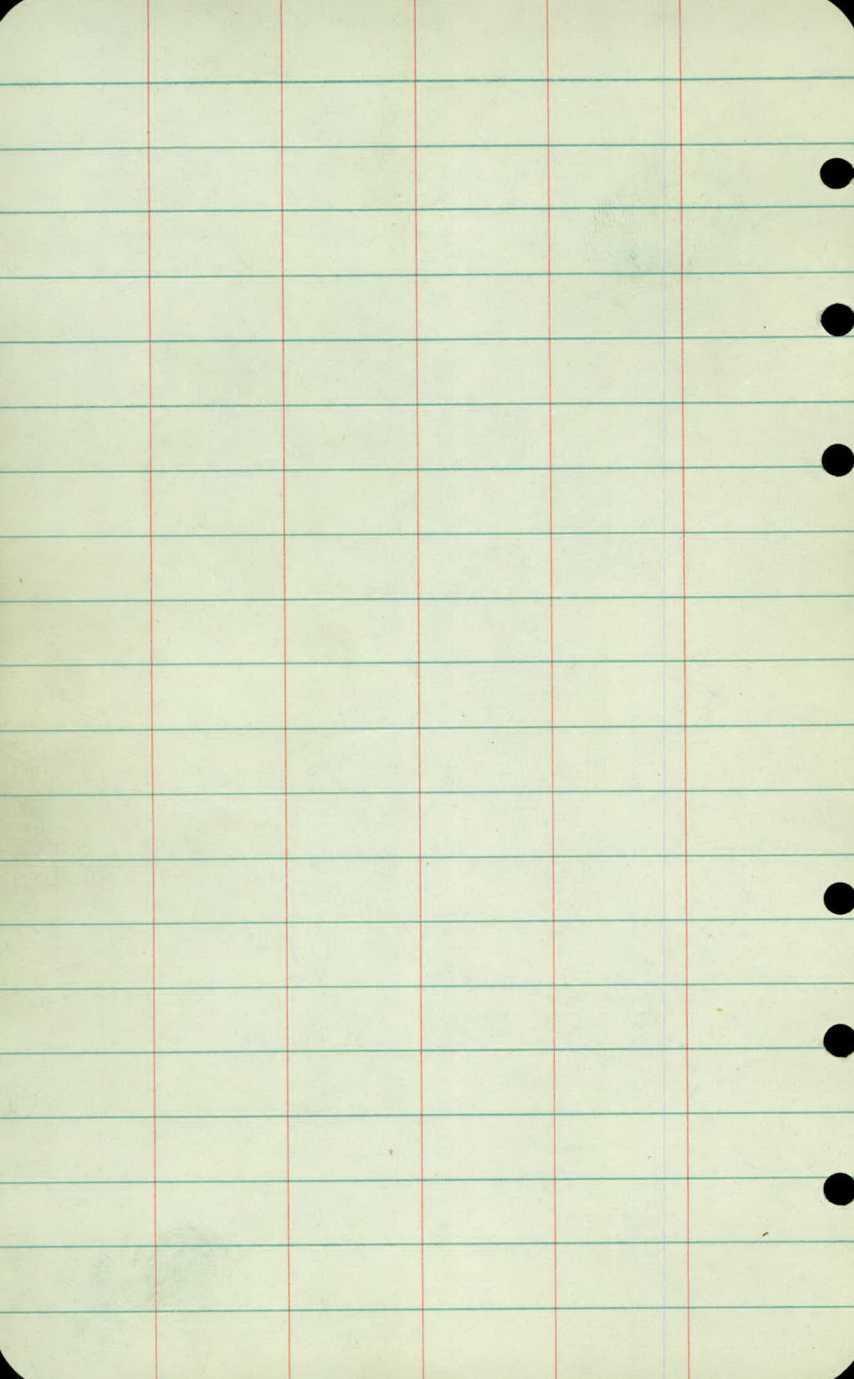
FR
RG
JL
WM
JH

June 16, 1960

120₂

Rain 55°

Spike in stump Fe Post Lt Sta 16+50



FR
JL
WM
JH

June 17, 1960
June 21, 1960

121 3

Boat Spike at Depot Night Club

0.27' West of Sec Line

0+00 = P1 0°03' left.

676.36
66°52' 25.99
Lexington Ave.

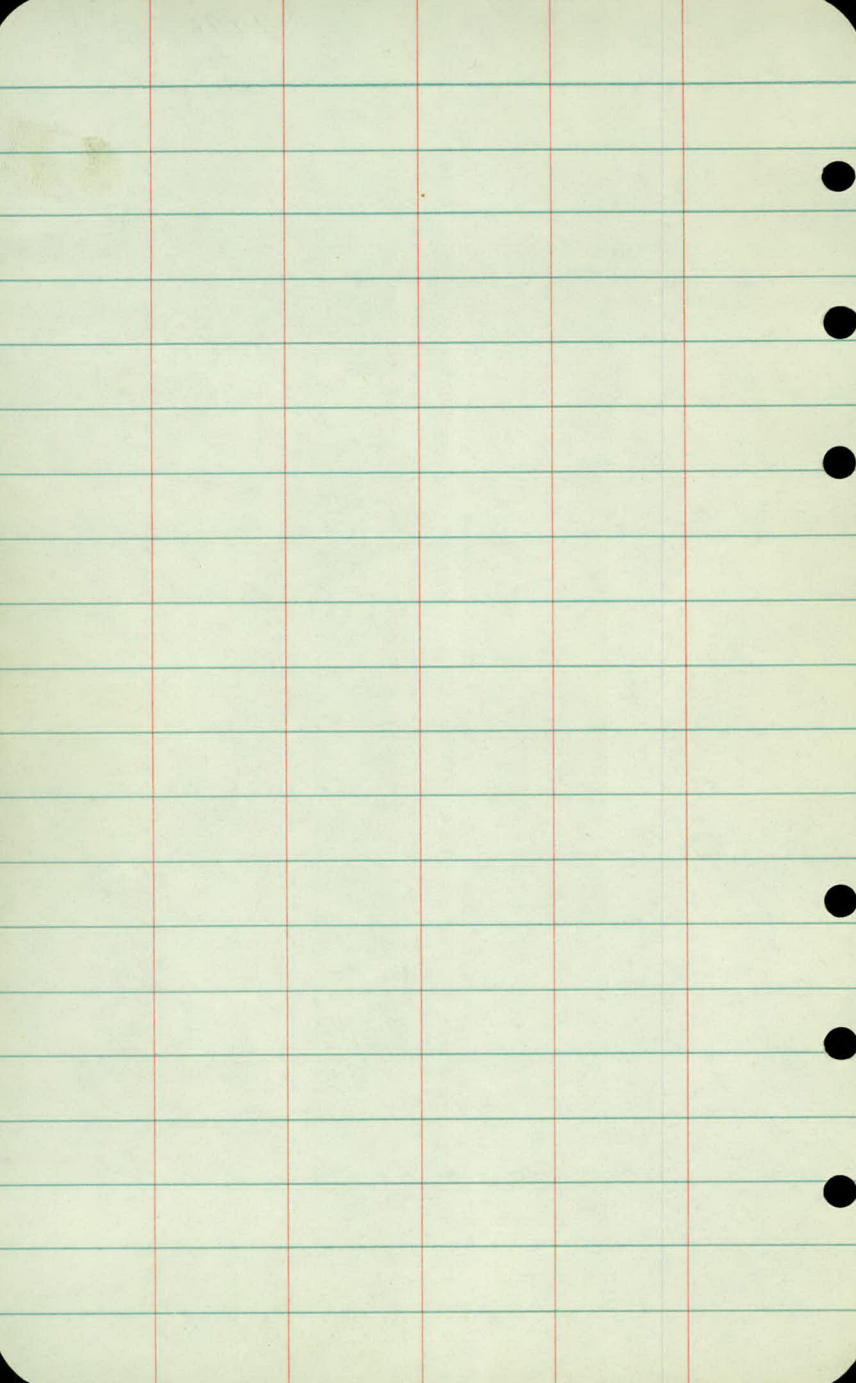
89°08'

272.01

Co Rd "C2"

91°22' Map

91°33'
LPD 1028.11
3/4



June 21, 1960

122
4

Additional x-Sections

Sta + π 17+50
 18 +50
 19 Elev

0+00 £ 392 893.21

889.29

0-50'

0-100'

W.S.

8.81

BM 9.13 906.67

892.54

17+50

99.34

1 v

18

1 v

FK
JL
WM
JH
RL

West Lt

June 21, 1960 123 5
Ft East

92.1	91.0	91.9	91.3	88.7	89.0	89.2	88.9	88.4	85.0	84.6	84.0
0.5	2.2	5.3	5.9	4.5	4.2	4.0	4.3	4.8	8.2	8.6	9.2
37	35	30	25	20	13	X	13	19	27	39	50

92.8	89.1	87.6	87.8	89.0	89.0	89.2	88.8	87.9	85.0	84.2	82.7
0.4	4.1	5.6	5.4	4.2	4.2	4.0	4.4	5.3	8.2	9.0	10.5
36	32	27	23	19	12	X	14	21	28	38	50

Water Surface

Spike in Stump Fe Post 11 Sta 16+50

89.0	93.5	95.9	98.6	99.3	99.4	99.2	97.9	91.9	88.1
17.7	13.2	10.8	8.1	7.4	7.32	7.5	8.8	14.8	18.6
34	27	23	18	15		13	21	31	38

88.0	87.7		87.3
18.7	19.0		19.4
42	50		50

96.2	99.9	99.8	99.6	99.9	99.7	99.8	99.8	99.2
10.5	6.8	5.9	6.1	5.8	6.0	5.9	7.9	13.5
25	20	18	14		13	18	23	32

93.9	91.2	89.7		88.5	88.4
12.8	15.5	17.0		18.2	18.3
30	38	50		50	40

STA.

+

π

-

ELV.

906.67

18+50

✓

19+00

✓

✓

June 21, 1960

124 6

Lt

2

Rt

00.0	02.1	02.7	02.4	02.7	02.3	02.5	01.8	04.5
6.7	4.6	4.0	4.3	4.0	4.4	4.2	4.9	7.2
26	20	17	13		13	17	21	26

07.3	05.5	03.8	05.3	04.8	06.3
9.4	11.2	12.9	13.4	11.9	10.4
31	37	50	50	39	33

00.2	03.3	04.5	04.3	04.6	04.4	04.4	04.2	02.3
6.5	3.4	2.2	2.4	2.1	2.3	2.3	2.5	4.4
28	21	17	13		13	17	19	23

07.2	05.4	03.5	02.8	08.9	09.3	07.3	07.5	00.4
9.5	11.3	13.2	13.9	7.8	7.4	9.4	9.2	6.3
33	37	47	50	41	36	34	32	27

06.7
10.0
50

Sta	+	π	-	Elev.
BM	3.18	891.28		888.10

FL, N.E 12" CM	5.69
----------------	------

FL 15" CM	8.73
-----------	------

$$\begin{array}{r} 2.26 \\ 1.23 \\ \hline 1.03 \end{array}$$

FL 18" CM	8.26
-----------	------

June 22, 1960, 1257

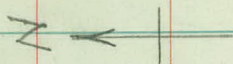
FK
JL
WM
JH
RL

Spike in PP N.W. Cor Josephine & Lexington

N.W. Cor Lexington & Josephine Rd

2' Lt Sta 2+54

72.5' Lt Sta 2+24



Section Line

iron

662.61

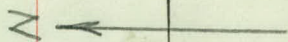
83°07'

Lexington Ave.

Lex. Ave Sta. 146+09.90

1/4 1/4 Line

June 22, 1960 126 8



Section Line 7

Boat Spike

294.45

old iron

44.6

spike
(for R/W Acquisition)

16.17

Boat Spike

34.63

Brenner Ave.

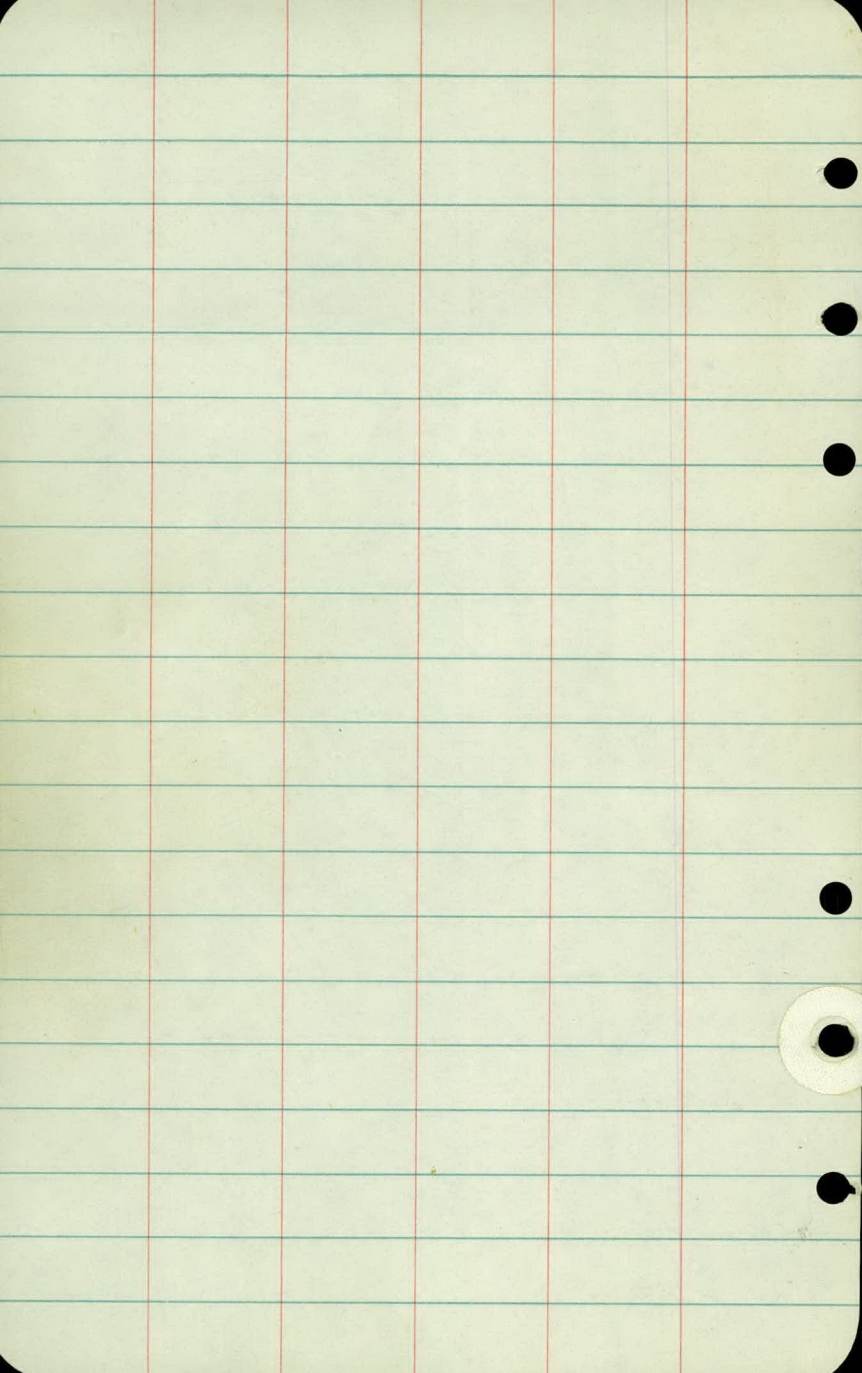
38.83

old iron

155+4.22

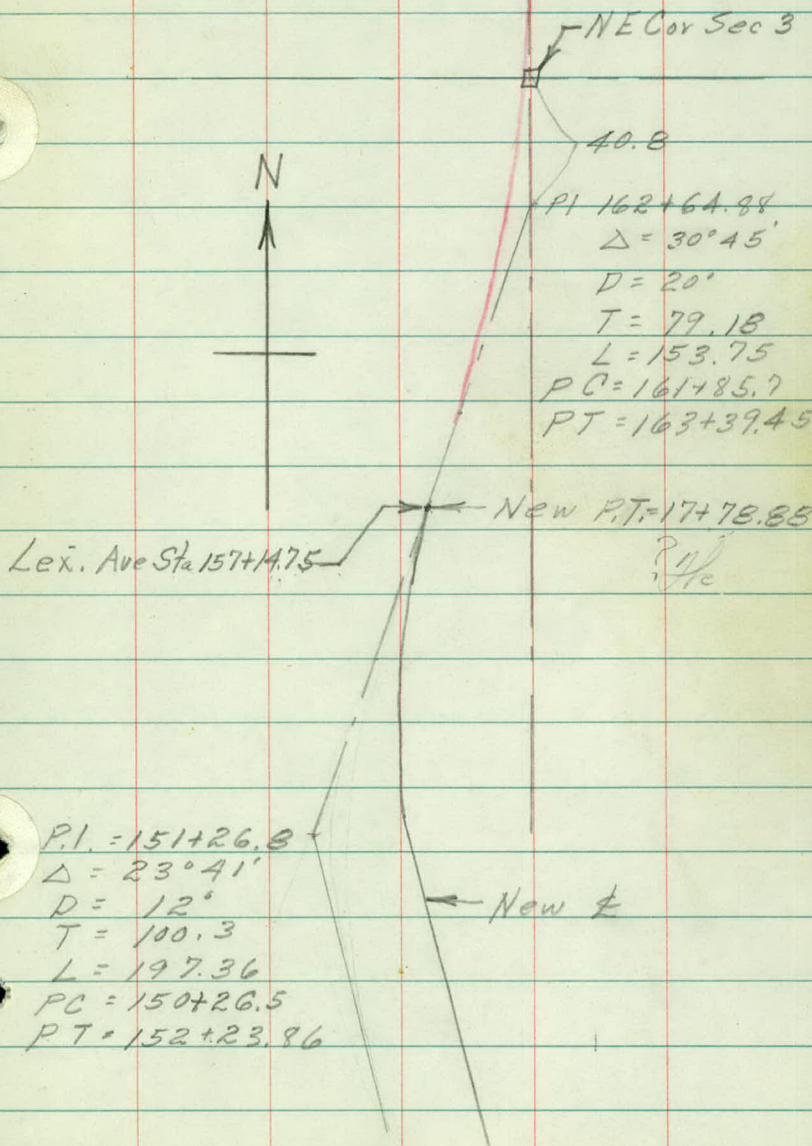
Lexington

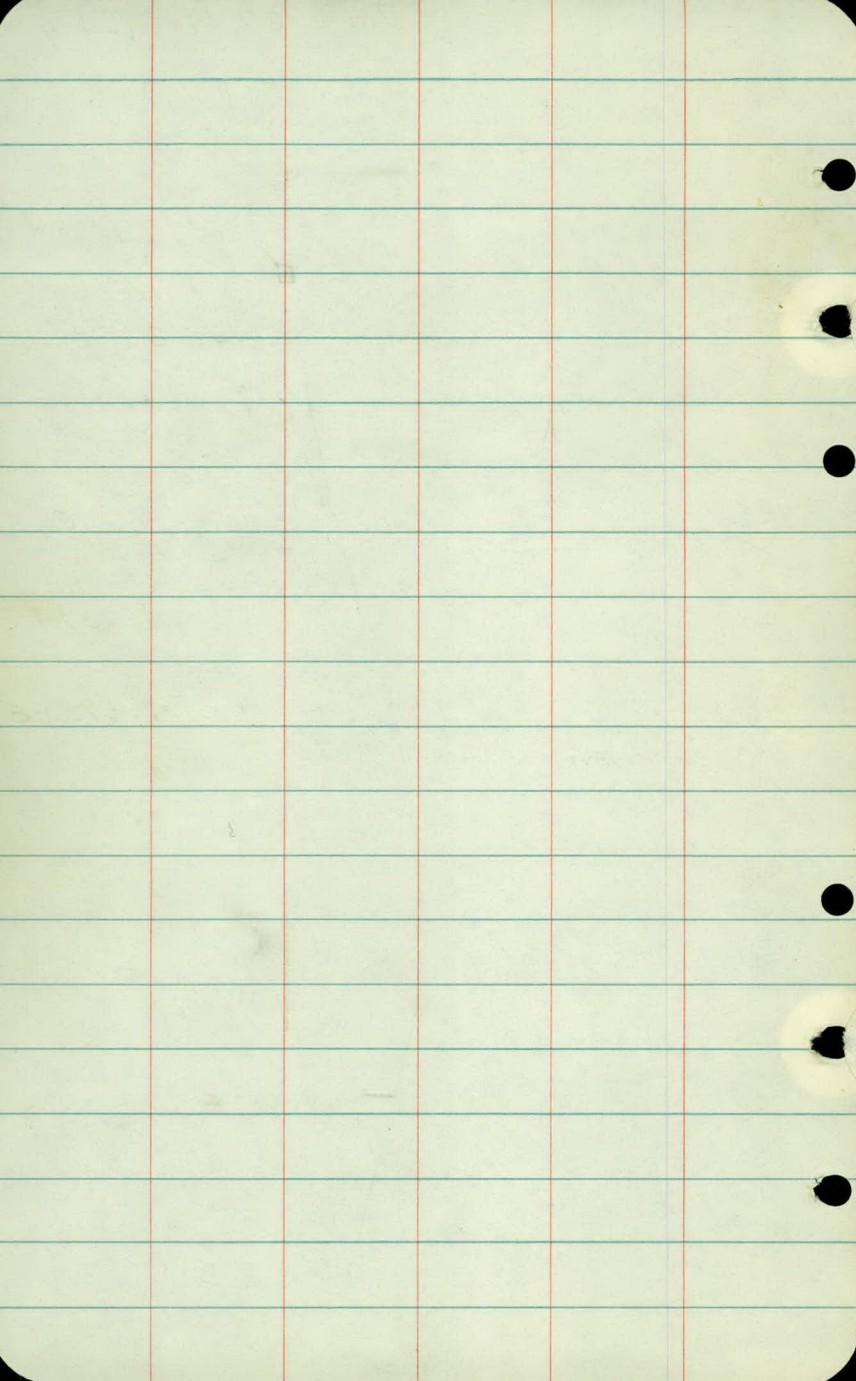
44.6
16.17
34.63
95.40



June 27, 1960, 127 9

FK
JL
WM
RL





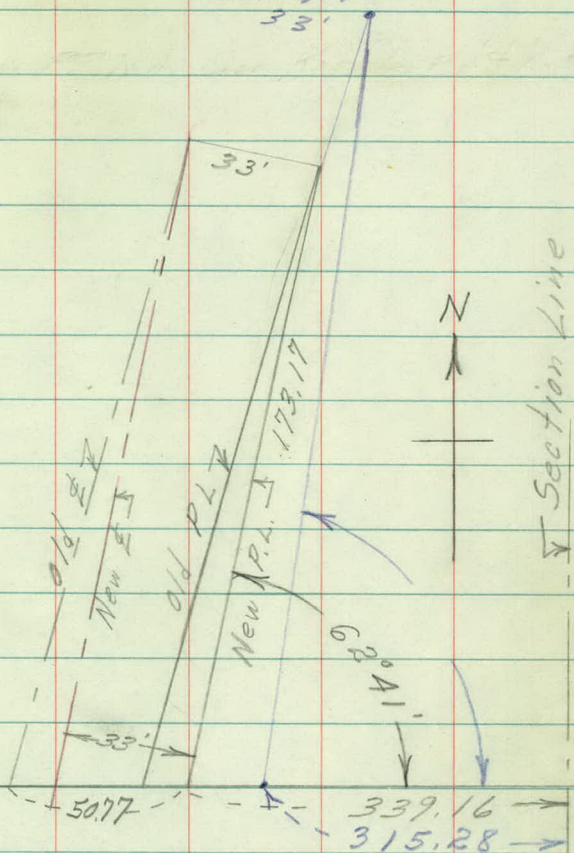
Lexington Ave

Property Acquisition
Description

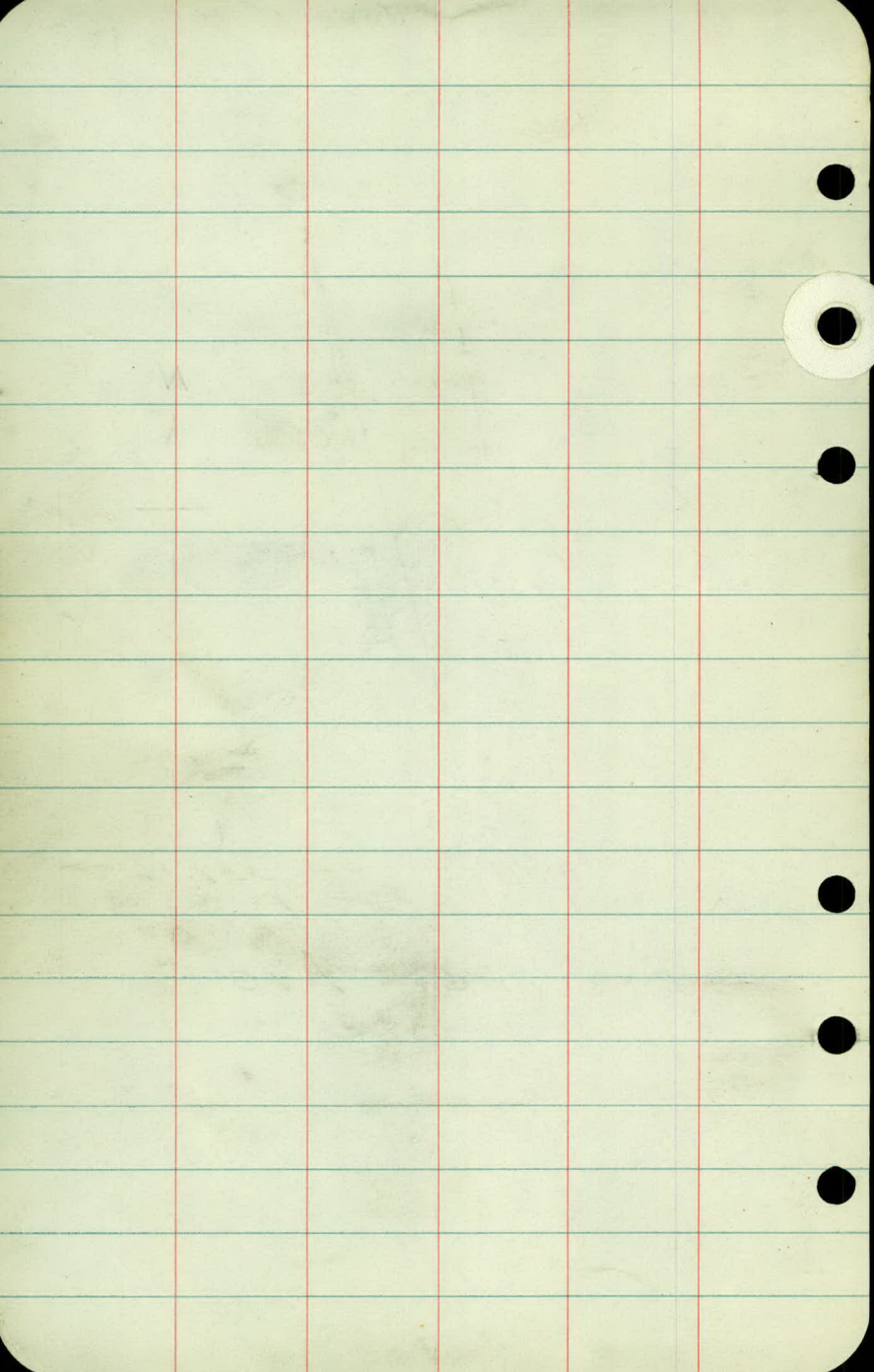
Sta Point
P.T.

17+78.88 P.T.

33



Brenner Ave.



SURVEY OF
East Line Section 3 Rose
and
So. Line Gov. Lot 3
in proposed
JOSEPHINE PARK.

4 pages

Dec. 12-18-58

K.A.

Sta Point

28+58.66

1557.97R

25+16.13 ~~P.O.T.~~ 0.27 W. of Sec Line

13+21.01 P.O.T. $\frac{1}{4}$ $\frac{1}{4}$ Cor.

13+00

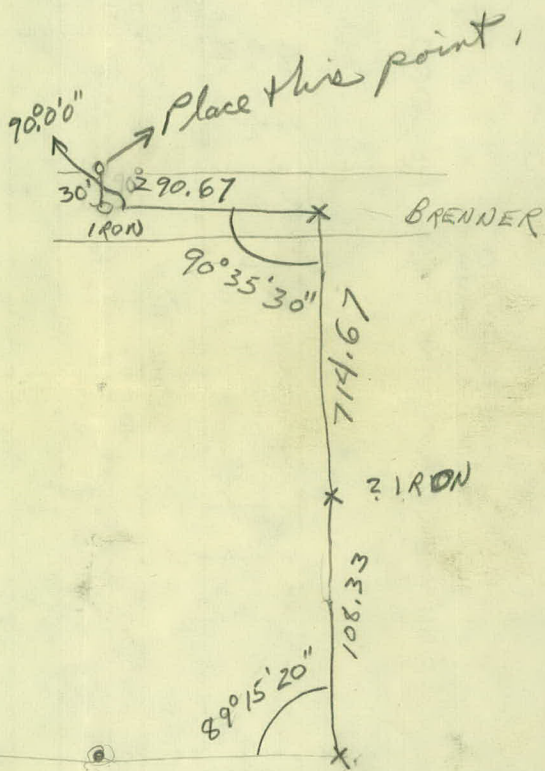
2859.25

13 21.01 M

13 21.25 R

0+00

↑
N



X CZ MON

DAILY ENGINEERING TIME RECORD

FUND.

DEPT.

DATE _____

NAME

EMPLOYEE NO.

P O R T

CLASSIFICATION

	DATE	DESCRIPTION	AMOUNT
1	1900	...	...
2	1900	...	...
3	1900	...	...
4	1900	...	...
5	1900	...	...
6	1900	...	...
7	1900	...	...
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17	1900	...	...
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29	1900	...	...
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36	1900	...	...
37	1900	...	...
38	1900	...	...
39	1900	...	...
40	1900	...	...
41	1900	...	...
42	1900	...	...
43	1900	...	...
44	1900	...	...
45	1900	...	...
46	1900	...	...
47	1900	...	...
48	1900	...	...
49	1900	...	...
50	1900	...	...
51	1900	...	...
52	1900	...	...
53	1900	...	...
54	1900	...	...
55	1900	...	...
56	1900	...	...
57	1900	...	...
58	1900	...	...
59	1900	...	...
60	1900	...	...
61	1900	...	...
62	1900	...	...
63	1900	...	...
64	1900	...	...
65	1900	...	...
66	1900	...	...
67	1900	...	...
68	1900	...	...
69	1900	...	...
70	1900	...	...
71	1900	...	...
72	1900	...	...
73	1900	...	...
74	1900	...	...
75	1900	...	...
76	1900	...	...
77	1900	...	...
78	1900	...	...
79	1900	...	...
80	1900	...	...
81	1900	...	...
82	1900	...	...
83	1900	...	...
84	1900	...	...
85	1900	...	...
86	1900	...	...
87	1900	...	...
88	1900	...	...
89	1900	...	...
90	1900	...	...
91	1900	...	...
92	1900	...	...
93	1900	...	...
94	1900	...	...
95	1900	...	...
96	1900	...	...
97	1900	...	...
98	1900	...	...
99	1900	...	...
100	1900	...	...

MAINT.

CONST.

STARTING TIME	STOPPING TIME	REMARKS
11:00	11:15	11:00
11:15	11:30	11:15
11:30	11:45	11:30
11:45	12:00	11:45
12:00	12:15	12:00
12:15	12:30	12:15
12:30	12:45	12:30
12:45	13:00	12:45
13:00	13:15	13:00
13:15	13:30	13:15
13:30	13:45	13:30
13:45	14:00	13:45
14:00	14:15	14:00
14:15	14:30	14:15
14:30	14:45	14:30
14:45	15:00	14:45
15:00	15:15	15:00
15:15	15:30	15:15
15:30	15:45	15:30
15:45	16:00	15:45
16:00	16:15	16:00
16:15	16:30	16:15
16:30	16:45	16:30
16:45	17:00	16:45
17:00	17:15	17:00
17:15	17:30	17:15
17:30	17:45	17:30
17:45	18:00	17:45
18:00	18:15	18:00
18:15	18:30	18:15
18:30	18:45	18:30
18:45	19:00	18:45
19:00	19:15	19:00
19:15	19:30	19:15
19:30	19:45	19:30
19:45	20:00	19:45
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20:15	20:30	20:15
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22:30	22:45	22:30
22:45	23:00	22:45
23:00	23:15	23:00
23:15	23:30	23:15
23:30	23:45	23:30
23:45	24:00	23:45

ENDING TIME

DIS-TRIBU-TION

[illegible]

CHECKED _____ SUPERVISOR

TOTAL

131 2

6th
C. W.

Handwritten diagram showing a line with a dimension of 10" and an angle of 29° 08'.

W¹⁴ Car. Sec. 2

$$\begin{array}{r} 132 + 3868 \\ 131 + 5668 \\ \hline 2140219 \end{array}$$

$$\begin{array}{r} 549.56 \\ 300 \\ \hline 2102.19 \\ 29451.75 \end{array}$$

$$\begin{array}{r} 2859 \\ 342 \\ \hline 2517 \end{array} \quad \begin{array}{r} 176.60 \\ 166.06 \\ \hline 342.66 \end{array}$$

$$\begin{array}{r} 25 + 16.55 \\ 342.66 \\ \hline 2859.21 \\ + 98 \\ \hline 2859.23 \end{array} \quad \begin{array}{r} 38 \\ 3\frac{1}{2} \\ 12 \\ 14 \\ 84 \\ 98 \end{array}$$

$$\begin{array}{r} 2516.13 \\ 13 \\ \hline 121613 \\ 39 \\ \hline 1215.52 \\ 13 \\ \hline 15 \end{array} \quad \begin{array}{r} 34 \\ 39 \end{array}$$

$$\begin{array}{r} 156 \\ 156 \\ 156 \\ 156 \\ 156 \end{array}$$

Feb 13, 1958 1323

Sta

L

Rt.

8+28

X-Fe 63' to Shore Line

8+00

67' to Shore Line

7+00

72' to Shore Line

6+00

63' to Shore line

5+05

N.E. Cor. Shed 38.5' Rt Parallel to Lex.

5+00

60' Shore line

4+00

54' Shore line

3+00

62' shore line

2+29

N.E.

N.W. Cor. Cottage - parallel to Lex.

2+00

108'
Shore Line

0+00

L Lexington & S.P.L. Brenner

Feb 13, 1958 1334
81

38.5

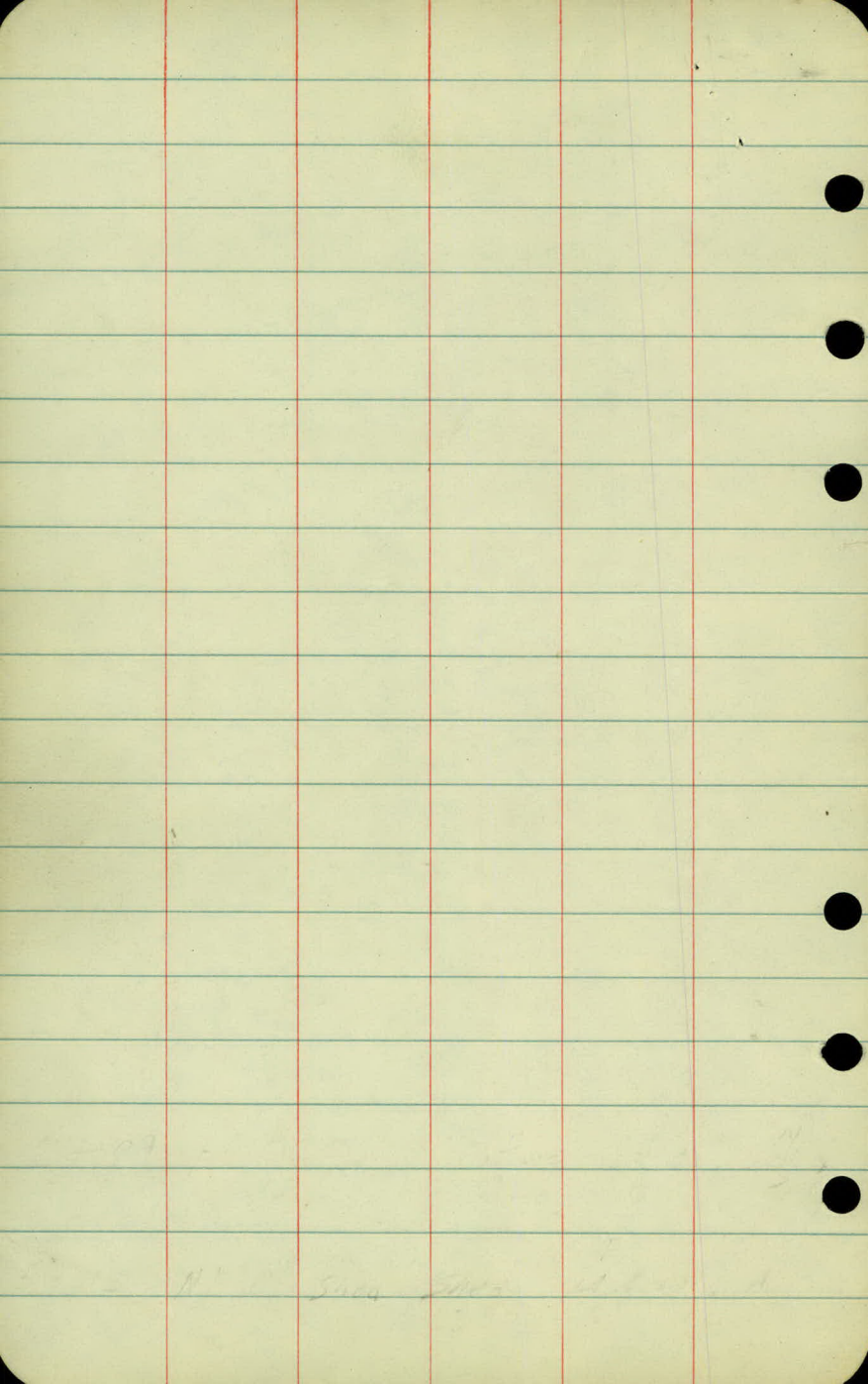
14.4

16.4

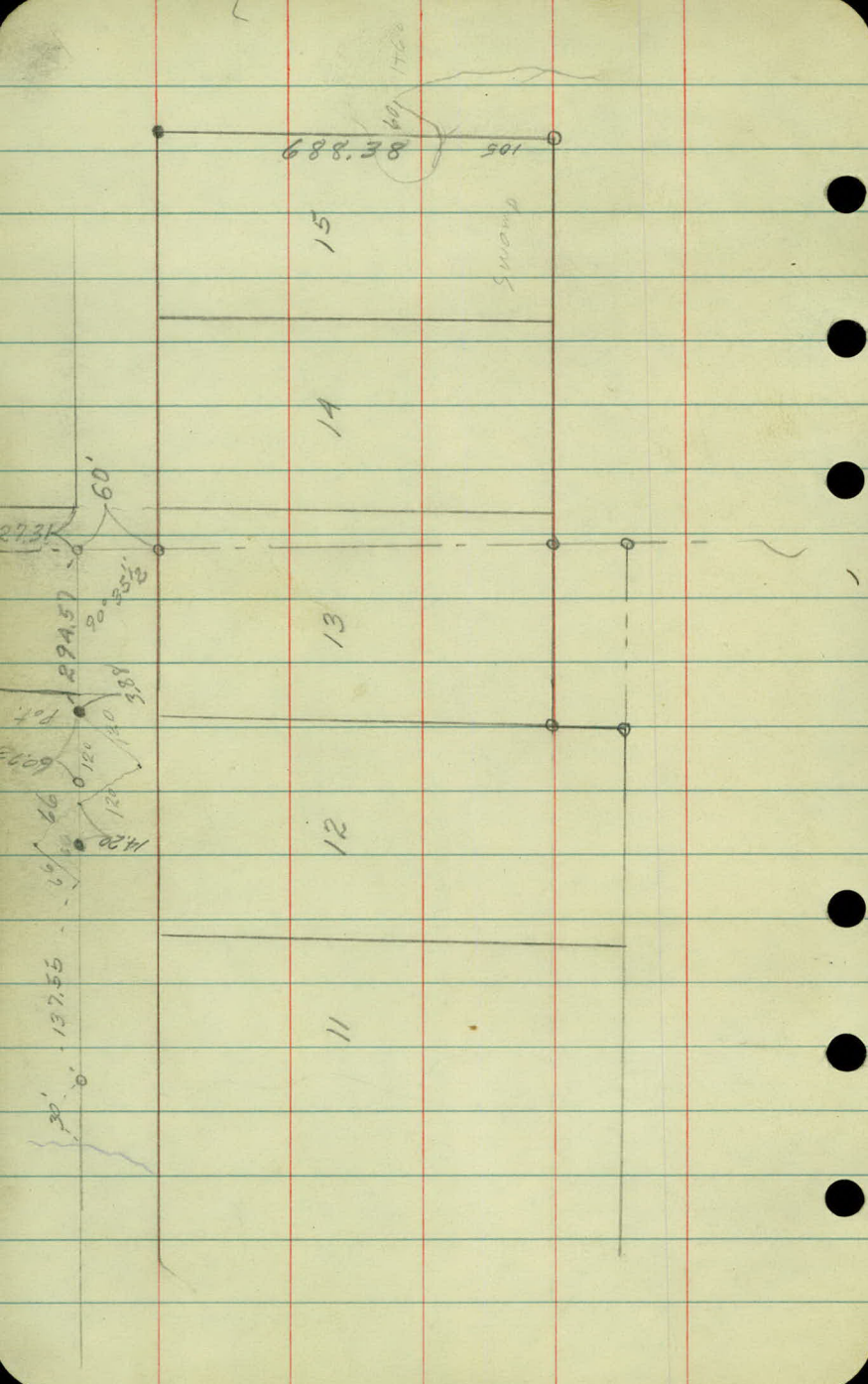
28.5

23.4

24.4



Josephine Park



April 14, 1959 135 2

89°38' Cal

2632.61

7 6 5 4 3 2 1

90°09'

2858.66

2861

13 14 15

30

2917.59

31

32

223.20

89°40'

2627.20

89°14'10"
89°24'30"
90°35'38"

27.23

89°24'10"

13

1

684.67

2860.02 Along Lot Line

108.36

292.10

318

89°15'

25.90

30

292.30

108.33

25.70

90°54'

120
57.28
71.72

60° 42' 30" 75.50

59.44

80° 09'

89° 08' 10" 2858.66

91° 32'

88° 35'

2910.59

2627.20

91° 32'
90° 16'

1° 16'
76

28
19
57

91° 32'
38'
90° 54'

179 60
89 44
90 16

5.41 x
2859 21.74
541

2174
8696
57 10870
117.61.34

2.50 x
1321 2174

132104
10832
68467
60

2174.00
2.5

10870
6348

74350

1321x = 7435

487 = 487

23.20
487
28.07

1321 7435
5284
11510
10868

2420
9247
14730

2859 4.113
11761.34
11436

3253
2859
3944
2859
10850

23.20
411
27.31

91 37
90 16
148
181.75
91 30

108.03
292.30
115.73

136
91 383
60 549'14'
189 54 194
549 9 18
3 14
100 12
541 3859 5410 1
718 6 3

2.50 x
1320 1428
1320 x =

1428
2.5
7140
2856
3570.0

19
4176
4
36
8944
19
98025
91003

2.70
1320 3370.00
2640
9300
9240
6000

29 17.39
5925
283834 9054

87 40
88 44
116 76'

23.20
270
25.90

89 44
91 32
0 76

89 14
90 09
88 35
91 32 30

2320
4085
27.23

5.46
+7'

358 120
360

0266
2859 7600 ft

13 20 01
108 33
14.28 34 x .02 = 38'
4 84 67
21 13 01
90 92 30
56 30
35 40

90 92
38
90 54

38
276

$$\begin{array}{r}
 2917.59 \\
 2858.66 \\
 \hline
 4 \overline{) 158.93} \quad 14.73 \\
 \underline{4} \\
 18 \\
 \underline{16} \\
 28 \\
 \underline{28} \\
 13 \\
 \underline{12}
 \end{array}$$

$$\begin{array}{r}
 2632.61 \\
 2627.20 \\
 \hline
 5.41 \\
 2.70
 \end{array}$$

$$\begin{array}{r}
 14.73 = 4 \\
 \hline
 2629.91 = 661.9 \\
 318
 \end{array}$$

$$X = 3.71$$

$$\begin{array}{r}
 25.90 \\
 636 \\
 \hline
 661.9
 \end{array}$$

$$\begin{array}{r}
 684.67 \\
 3.71 \\
 \hline
 688.38 \\
 652.43 \\
 \hline
 (36)
 \end{array}$$

$$\begin{array}{r}
 36 \\
 636
 \end{array}$$

$$5.66 / 100$$

$$6 / 100$$

$$1.8 \overline{) 360}$$

$$\begin{array}{r}
 10.03 / 100 \\
 1.8 / 100
 \end{array}$$

Josephine Park

Soundings

2 pages

Platted

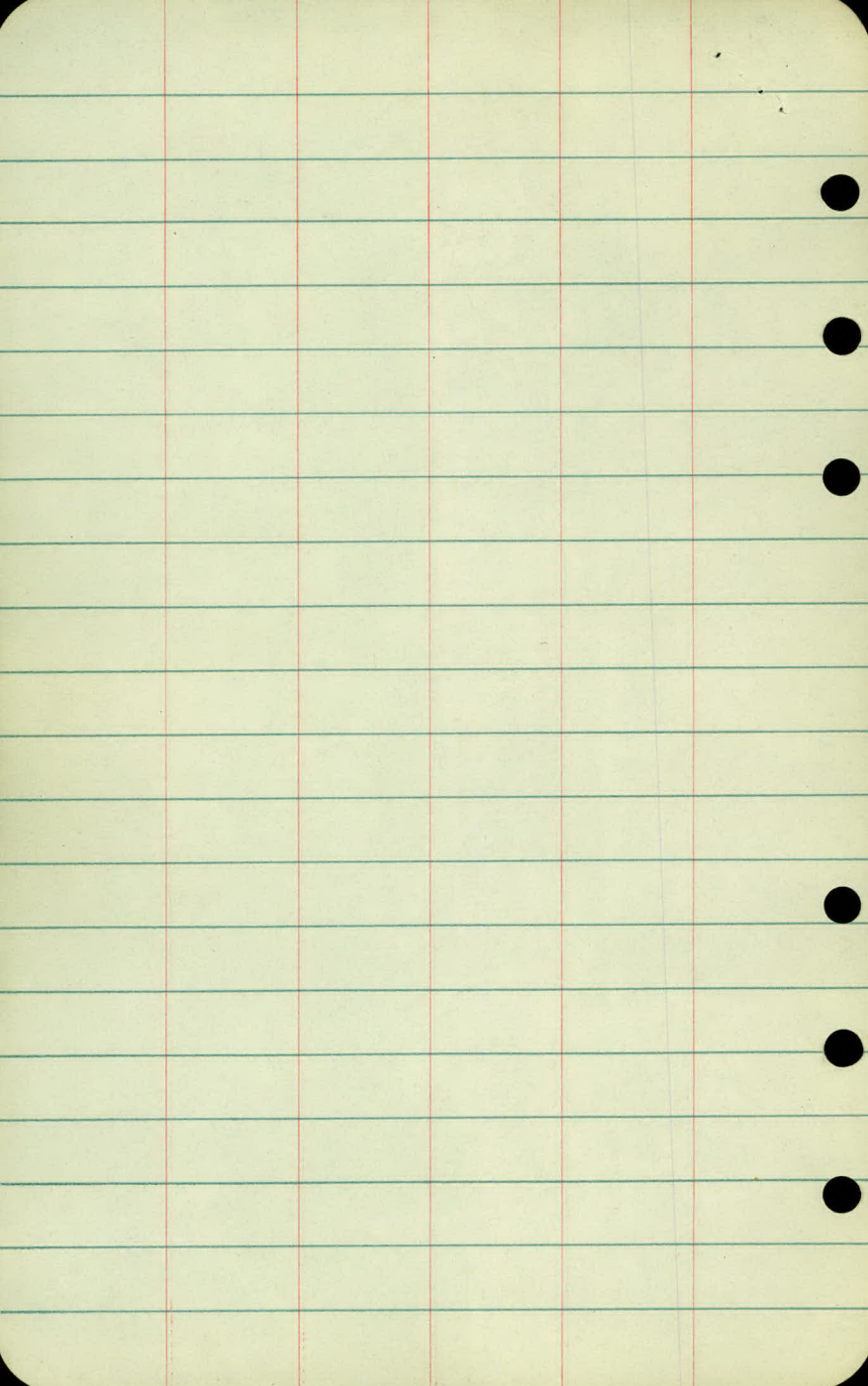
Lat Sta 51+234 S.H.
to NW Cor Sec 2 = 0°00'

	Az.	Stadia	Depth
JH #1	193°25'	458'	24'
#2	196°25'	550'	16'
#3	195°10'	650'	10'
#4	198°20'	750'	6'
#5	206°50'	765'	8'
#6	208°20'	880'	10'
#7	209° -	1000'	14'
#8	204° -	970'	8'
#9	198°20'	960'	7'
#10	192°40'	880'	18'

FK
LC
RG
KP
CW

Dec 3, 1957

138 2



LEXINGTON AVE

Josephine Rd to Co Rd/D

SOUNDINGS

JUNE 13, 1958

TEST	KP RR RM	FEET			
HOLE #					
1	22				
2	15				
3	5				
4	8				
5	4				
6	10				
7	7				
8	18	near bath house			
9	8				
10	8				
11	24				
12	14				
13	8				
14	6				
15	6				
16	6				
17	4				
18	16				
19	6				

2' Vegetation - Loose Peat

3' Clay + 5' Fibrous peat

1' Vegetation 3' Fibrous peat

2' Vegetation 2' Fibrous peat

1' Vegetation 4' Fibrous peat

2' Vegetation 3' Fibrous Peat

AZ

At Lexington + Josephine Rd
to Josephine Rd 285°20'

1 79°15' 75'

2 18°10' 100'

3 4°25' 159'

4 4°05' 324'

5 2°30' 385'

6 359°20' 4.42

7 357°20' 595

8 ✓

9 ✓

10 ✓

11 96°55' 133'

12 63°10' 154'

13 46°35' 194'

14 17°40' 294

15 13°20' 354

16 7°00' 4.35

17 5°15' 528

Δ Pt A 341°52' 406

to low south 149°40'

June 18, 1954 1413

442

17' 140F $\pm$ 60K.

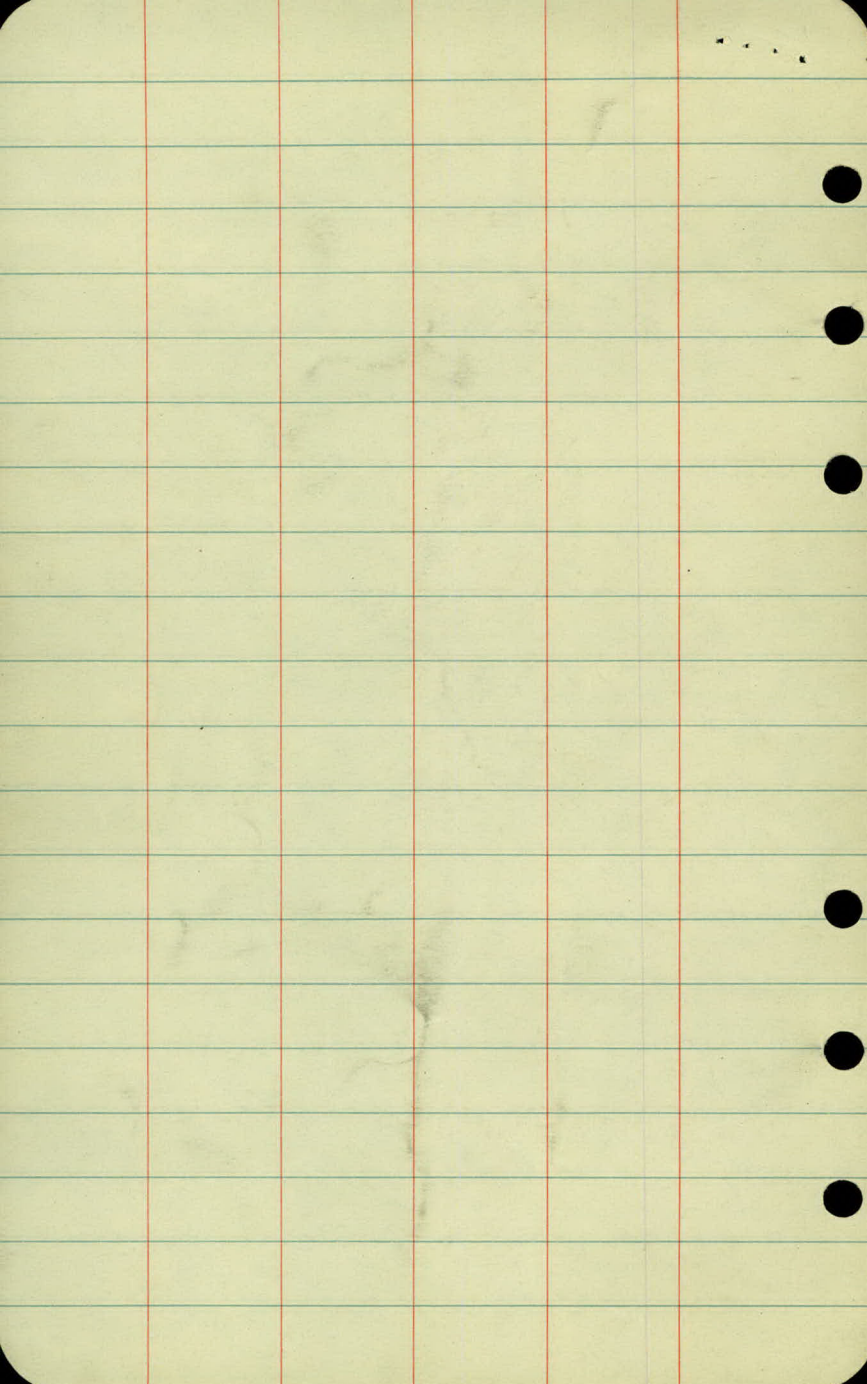
Nat Δ Pt A
 to $\pm$ Lex & Josephine 161°52' 406'
 Δ Pt B 359°25' 389'
 29

Nat Δ Pt B
 to Δ Pt A 179°25' 389'
 to Δ Pt C 11°57' 157'
 # 8 Hob 105°55' 87'

Nat Δ Pt C
 to Δ Pt B 191°57' 157'
 to Δ Pt A 183°01' 543'

9 137°40' 81'
 18 90°04' 100'
 10 69°50' 103'
 19 53°15' 183'
 $\pm$ Lexington 274°30' 17'
 " " 184°35' 218'

June 17, 1958 / 42 7



Josephine Park

Shore Traverse

§

House Location

Sta. Point ΔL ΔR

Lat Pt G from Pt F to Pt H = $84^{\circ}10'$

Lat Pt H to Pt I $0^{\circ}00'-00''$ HI = 4.7

NW Cor Ho Lt $68^{\circ}23\frac{1}{2}'$ 150' 1.0 Rod
+ $0^{\circ}40'$

SW Cor Ho Lt $64^{\circ}40'$ 122' 1.0 Rod
+ $0^{\circ}30'$

SE Cor Ho Lt $51^{\circ}10'$ 134' 1.0 Rod
- $0^{\circ}15'$

Lat F def. L from Pt E to Pt H = $19^{\circ}51\frac{1}{2}'$

7+23.33 Pt G

5+05.78 Pt F $12^{\circ}11'$

4+38.33 Pt E $10^{\circ}09'$

3+42.56 Pt. D $8^{\circ}00'30''$

2+14.29 Pt. C $15^{\circ}39\frac{1}{2}'$

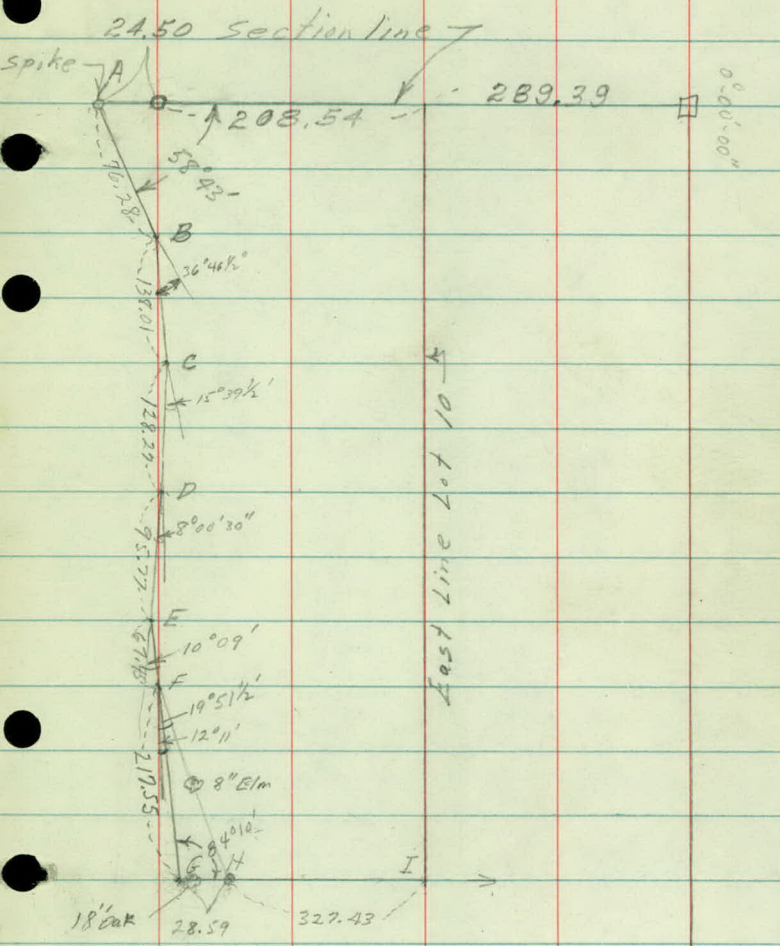
0+76.28 Pt. B $36^{\circ}46\frac{1}{2}'$

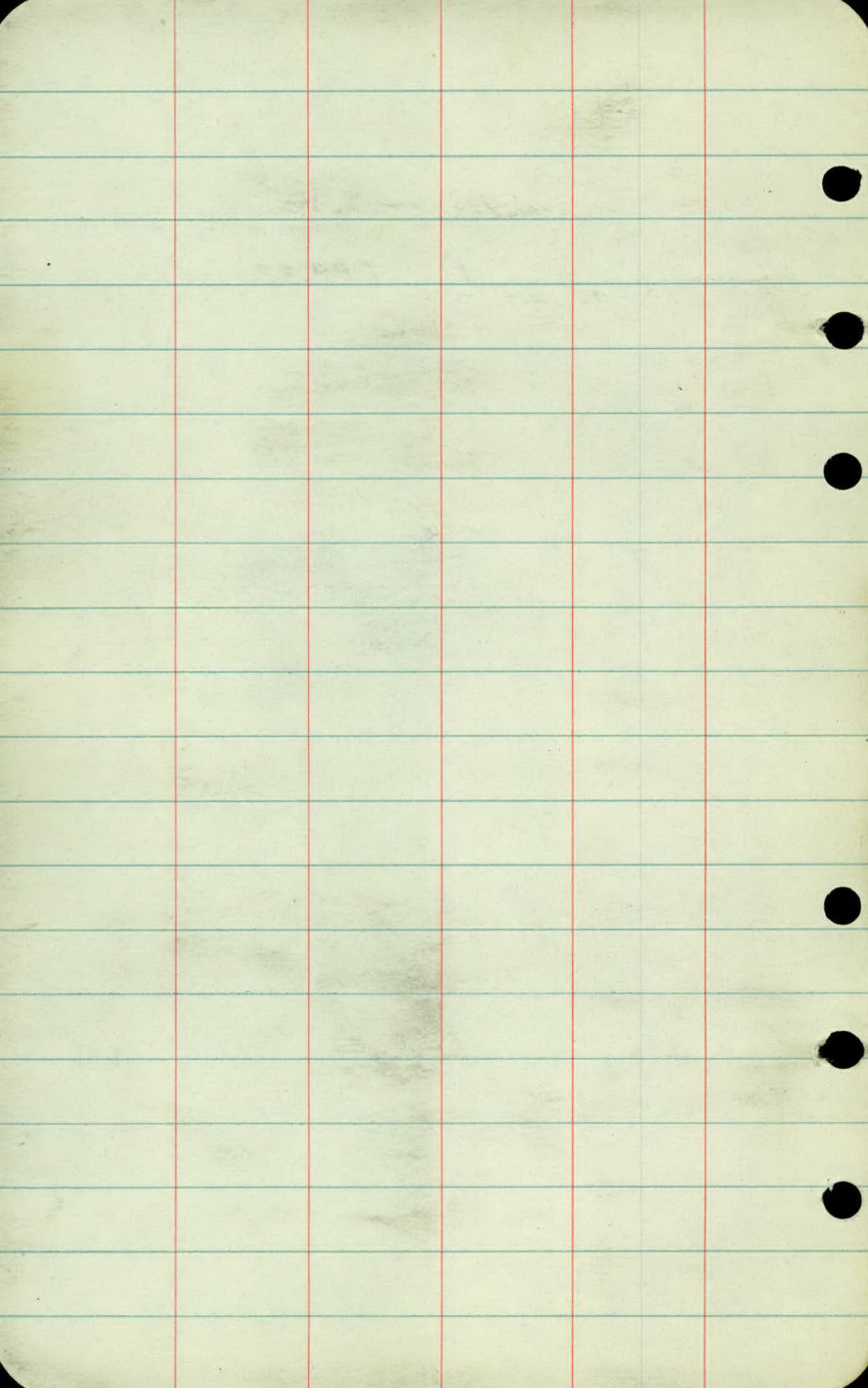
0+00 Pt. A
Spike $58^{\circ}43'$ E. to S.

FK
RG
JS
JL
WM

1714.60
121.17
284.3

April 28, 1960 144 2
Drizzle 45°





Sept. 2, 1960
145 1

New Profile

Sta	+	π	-	Elev
BM	4.09	901.63		(897.54)
			6.8	948 94.9
14			7.3	94.3
+21			6.0	95.6
+33			5.0	96.6
+50			4.2	97.4
+75			4.3	97.3
15			4.8	96.8
+50			2.4	94.2
16			5.3	96.3
+50			4.5	97.1

FX
JL
WM
HG

Sept. 2, 1960 146 2

Spike in 8" Bass Wood Fe Post Stamp Lt Sta 16+80

11.2' Rt of old 14

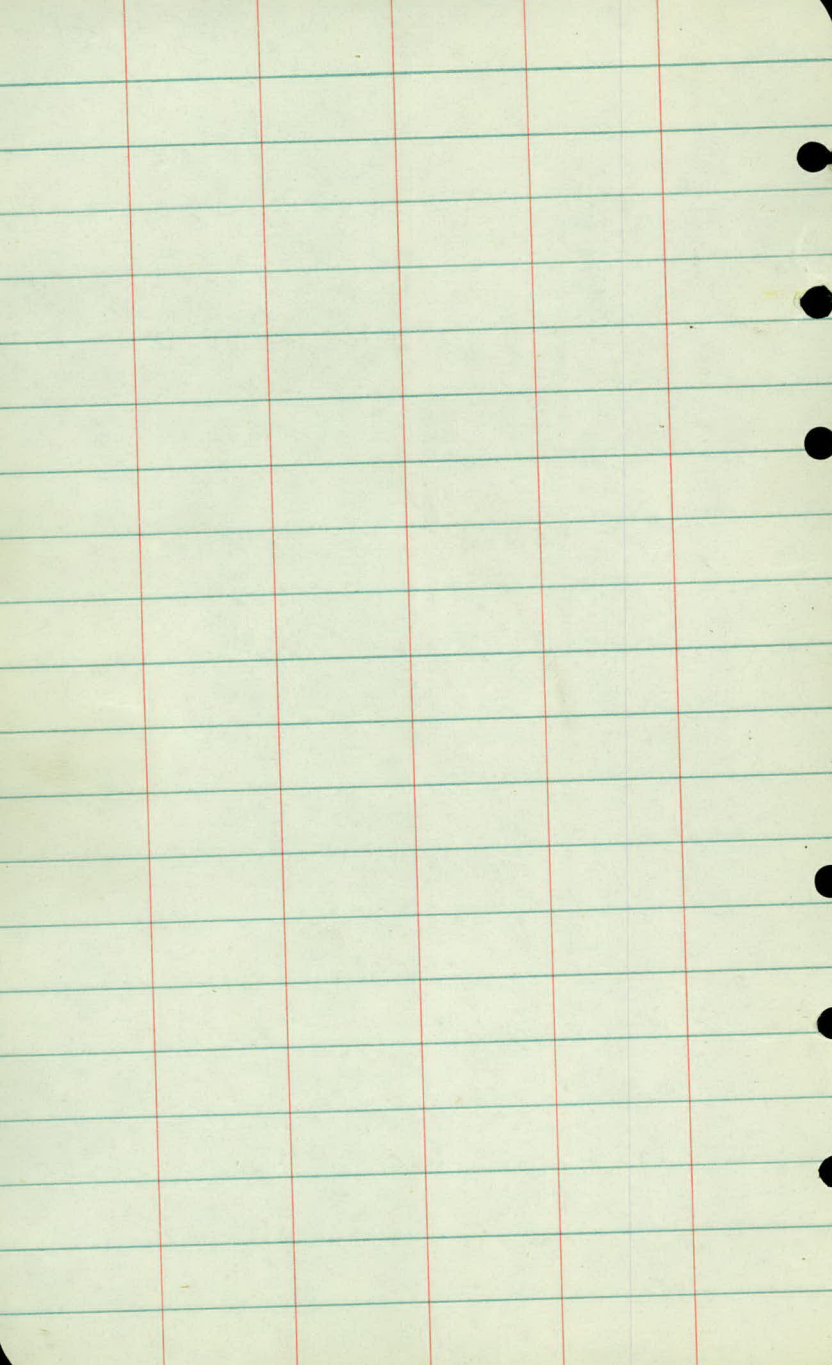
Sta	+	π	-	Elev
		901.63		
17			3.5	98.1
+50			2.3	99.3
18			0.7	00.9
TP	8.05	908.99	0.69	900.94
+17.03			7.5	01.5
+50			6.2	02.8
19			4.3	04.7
+50			2.2	06.8
20			0.0	09.0
BM			11.46	897.53 (897.54)

Lt

Sept 2, 1960 1473
Bt

P.T.

Spike in 8" Bass Wood Fe Post Stp 11 Sta 16+80



Josephine Park

Stadia

at N.E. Cor.

Rec/ 9/1/60

OBJECT	AZ.	STADIA	
X AT NE corner Lot[#] 15 915.18			
To SE corner Lot [#] 15	180°00'		
"			
Blvd.	271°00'	50'	✓
"	271°00'	100'	✓
"	269°30'	155'	✓
center of wters. ^{churchill} Brenner	285°40'	165'	✓
G.E.	259°00'	172'	✓
"	256°20'	157'	✓
"	254°10'	139'	✓
"	245°30'	104'	✓
"	258°45'	60'	✓
"	250°40'	40'	✓
"	262°30'	90'	✓
"	257°10'	213'	✓
Edge swamp	239°40'	290'	✓
"	231°15'	280'	✓
"	221°00'	254'	✓
G.E.	203°40'	172'	✓
L Brenner at NE Cor Lot 15	0°00'	33'	

FK
JL
WM
HG
DIST.

VERT.
ANGLE

ROD
EQUIV.

Sept 1, 1960
ROD

DIFF.

149 2
ELEV.

			4.15	iron	
			Ground Elev. 5.4		909.8
			7.6		907.6
			9.2		906.0
			11.2		904.0
			11.5		903.7
-3° 19'	-9.9	12.0	-21.9		893.3
-3° 19'	-9.1	11.9	-21.0		894.2
-3° 17'	-7.9	11.0	-18.9		896.3
-3° 17'	-5.9	11.6	-17.5		897.7
-3° 17'	-3.4	12.0	-15.4		899.8
LR		12.4			902.8
LR		13.3			901.9
-3° 27'	-12.8	12.0	-24.8		890.4
-3° 27'	-17.4	11.1	-28.5		886.7
-3° 44'	-18.2	12.0	-30.2		885.0
-3° 44'	-16.5	13.8	-30.3		884.9
-2° 30'	-7.5	13.0	-20.5		894.7
		6.2			909.0

OBJECT	AZ.	STADIA
X AT NE Corner Lot #15 To SE Corner Lot #15	180° 00'	
G. E.	201° 40'	115'
"	180° 00'	67'
"	"	117'
"	"	158'
"	"	215'
"	"	266'
"	"	304'
Edge of swamp	200' S	130' W
"	300' S	58' W
"	400' S	27' W
Edge of swamp crosses E. Line of Lot 15	482' S 525 SW 20' L	
BM 4.98	893.08	888.10
		888.99
		897.54
FL	9.89	883.19
FL	9.53	883.55
FL	9.39	883.69
FL	9.38	883.70

DIST. VERT. ROD Sept 1, 1960 150 3
ANGLE EQUIV. ROD DIFF. ELEV.

HI 4.15

-2° 00' - 4.0 13.0 - 17.0 898.2

LR 7.3 907.9

" 9.2 906.0

" 6.7 908.5

" 7.6 907.6

" 8.7 906.5

" 11.6 903.6

939
25

G.E. 15 9.2 above swamp

Spike in PP NW Cor Josephine & Lex

Nail. " "

Spike in 8" ^(Bass Wood) B&W Fe Post Stp 21 Sta 16+8

East End 30" SCP

West End 30" SCP

East End 24" CM

West End 24" CM

OBJECT			AZ.	STADIA
BM	12.13	909.67		(897.54)
TP	13.55	922.76	0.46	909.21
TP	6.32	928.69	0.39	922.37
TP	1.48	920.51	9.66	919.03
TP	1.48	911.96	10.03	910.48
BM	0.93	911.96	0.93	911.03
TP	12.31	922.79	1.48	910.48
TP	9.39	929.55	2.63	920.16
TP	0.43	918.09	11.89	917.66
TP	0.76	905.52	13.33	904.76
BM			8.05	897.47 (897.54)

100' West of the W. Line of Churchill

Swamp is 75' Feet south of SL Brenner

Swamp Crosses South Line of

Brenner Ave 185' West of the

West Line of Churchill

DIST.

VERT.
ANGLEROD
EQUIV.

ROD

DIFF.

ELEV.

Sep 15/1960 151.4

Spike in 8" BW Fe Post stump Lt Sta 16+80

stake

Iron NE Cor Lot 15

stake

Spike in 8" Bass Wood Fe Post stump Lt Sta 16+80

OBJECT

AZ.

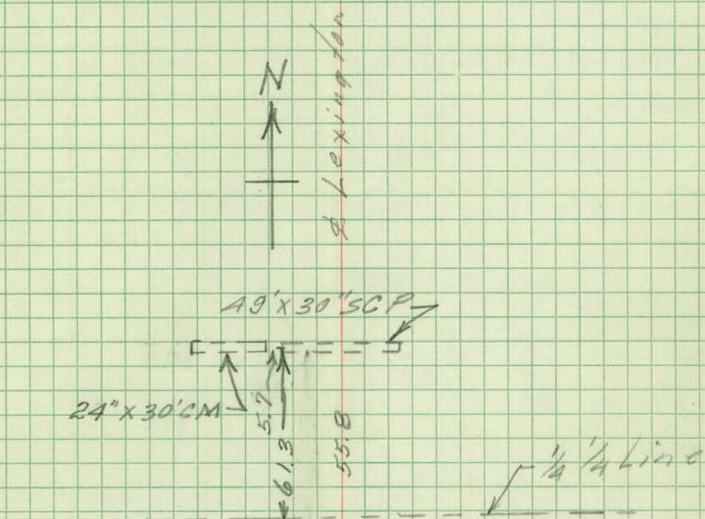
STADIA

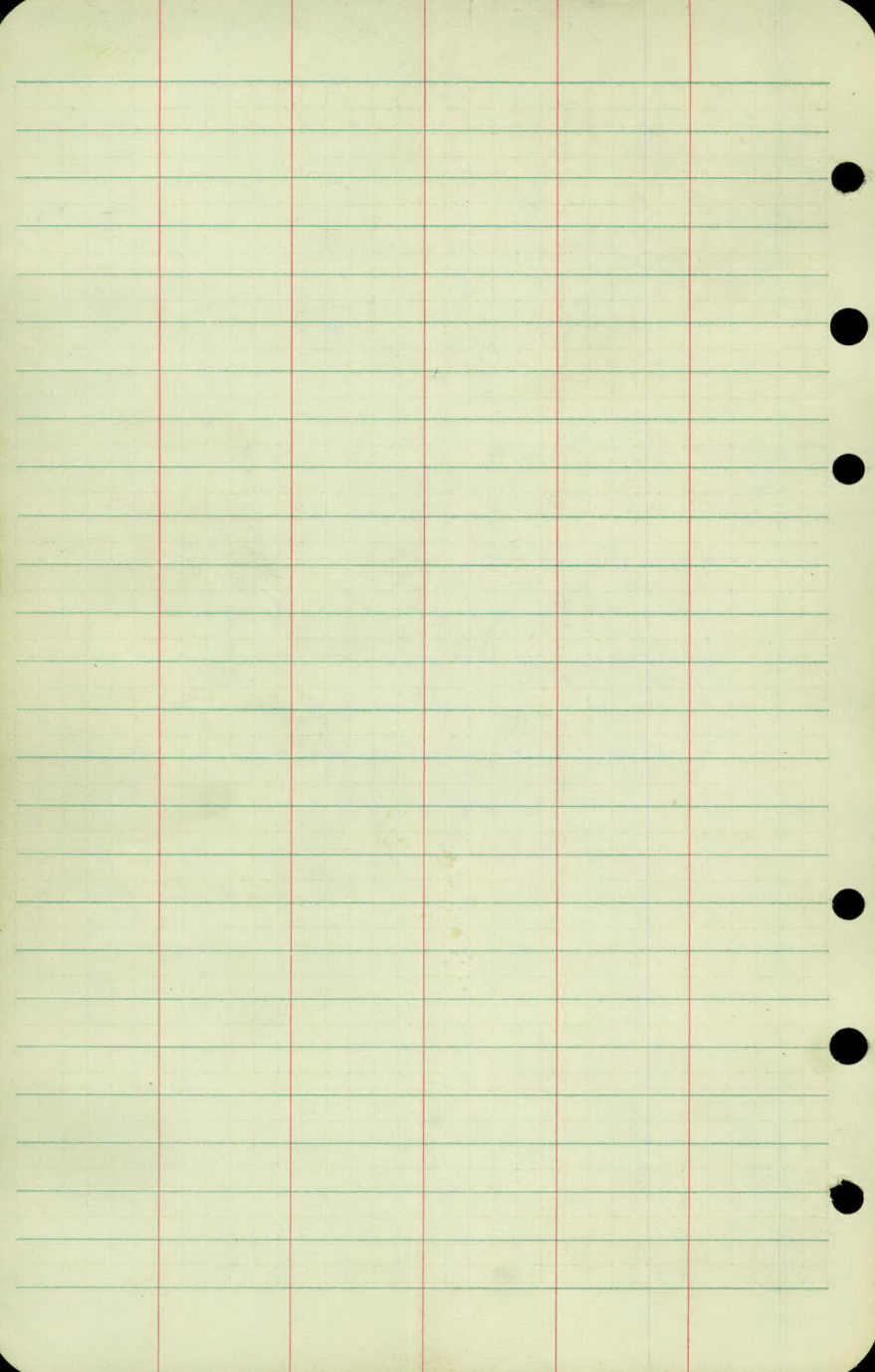
Sept 1, 1960 152 5



49' E. End 30' SCP

Sept 1, 1960 1536





PK
JL
WM
HG

Sept. 7, 1960 (154)

Swamp Locations

Edge Swamp 100' E of S.E.
Cor Lot 15

Edge Swamp 160' N & 60' East
of SE Cor Lot 15

S Edge of Delta with Trees 10.5'
N of SE Cor Lot 15

N. Edge of Delta with trees 522'
South of NE Cor Lot 15
Delta = 60' Diameter

Edge Swamp 136' East of Section
Line Along N Line Brenner
Edge Swamp 187' N of N. Line
Brenner Ave along section line

Elev. Top MH $\pm$ Brenner & Churchill
= 903.33

FL inv. E. = 895.77

FL inv N = 895.82

Profile

Existing Lexington

Sta	+	π	-	Elev
BM	6.55	894.65		(888.10)
0+00			5.7	89.0
+50			5.9	88.8
1			5.9	88.8
1			10.9	83.8 83.6
+50			5.7	89.0
+90	Ent Rt			
2			5.7	89.0
			+4.6	99.3
TP	9.63	898.58	5.70	888.95
+50			9.3	89.3
3			8.8	89.8

FK
JL
WM
HG

Sept. 9, 1960 1562

Spike in PP NW. Cor Josephine & Lex.
& Lexington at $\frac{1}{4}$ $\frac{1}{4}$ Line

Swamp Right

Top Knoll Rt

636

27

663

Sta	+	π	-	Elev
-----	---	-------	---	------

		898.58	90.5	
--	--	--------	------	--

3+50			8.1	
------	--	--	-----	--

			91.3	
--	--	--	------	--

4			2.3	
---	--	--	-----	--

			91.9	
--	--	--	------	--

+50			6.7	
-----	--	--	-----	--

			84.4	
--	--	--	------	--

			84.4	
--	--	--	------	--

+75			14.2	84.4
-----	--	--	------	------

			92.5	
--	--	--	------	--

			92.5	
--	--	--	------	--

5			6.1	
---	--	--	-----	--

			93.3	
--	--	--	------	--

			93.3	
--	--	--	------	--

+50			5.3	
-----	--	--	-----	--

			93.8	
--	--	--	------	--

			93.8	
--	--	--	------	--

6			4.8	
---	--	--	-----	--

			94.3	
--	--	--	------	--

			94.3	
--	--	--	------	--

+50			1.3	
-----	--	--	-----	--

			94.6	
--	--	--	------	--

			94.6	
--	--	--	------	--

7			4.0	
---	--	--	-----	--

			94.9	
--	--	--	------	--

			94.9	
--	--	--	------	--

+50			3.7	
-----	--	--	-----	--

			3.7	
--	--	--	-----	--

Sept 2, 1960 157 3

Swamp Rt

$$\begin{array}{r} 1321 \\ 89.15 \\ \hline 1410.15 \end{array}$$

Sta	+ K	-	Elev.
-----	--------	---	-------

	898.58		
--	--------	--	--

		95.1	
--	--	------	--

		3.2	
--	--	-----	--

		95.6	
--	--	------	--

		3.0	
--	--	-----	--

+50			
-----	--	--	--

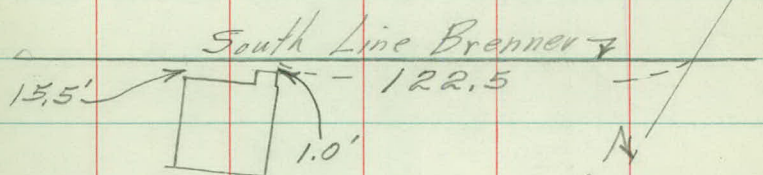
TP	5.22	900.99	2.81	895.77
----	------	--------	------	--------

BM				
----	--	--	--	--

			3.43	897.56
--	--	--	------	--------

				897.54
--	--	--	--	--------

House Relocation

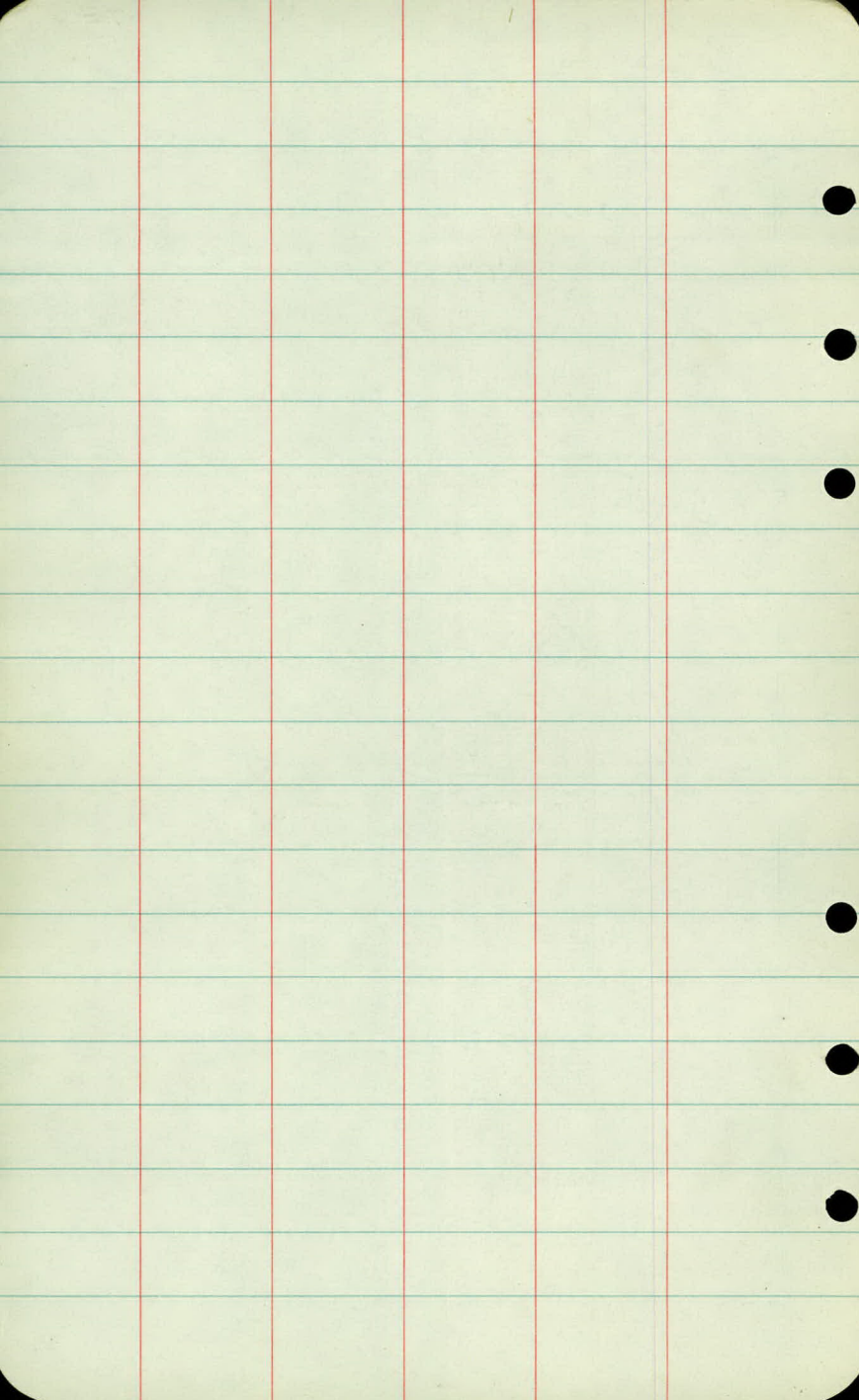


Eves over R/W

Lexington Ave

Sept 9, 1960 1584

Spike in Bass Wood Fe Post Stump Gtsta 16780



Josephine Park

Stadia

Locations of SOILS EXPLORATION
COMPANY test Holes

Angle at NE cor Lot 15

Used $90^{\circ}09'$

OBJECT

AZ. STADIA

π on S. Line Brenner

165.3' West of NE Cor Lot 15

to NE Cor Lot 15 $0^{\circ}00'$

Test Hole #				
14	127°50'	154'	153	
" "	9 17	85°00'	231'	229
" "	13	92°55'	269'	✓
" "	10	71°35'	440'	✓
" "	11	87°25'	419'	✓
" "	12	80°50'	550'	✓

π on N Line Brenner Ave

+ Section Line

to S. Line Brenner + Section Line 180°

Test Hole #17	182°-	98'
" " 16	130°16'	208'
" " 15	128°20'	454'

EX
JL
WM
HG

DIST.

VERT.
ANGLE

ROD
EQUIV.

ROD

DIFF.

160
ELEV. 2

Sept 12, 1960

5°

5°

—

—

—

—

OBJECT

AZ.

STADIA

π at P.I. Sta 2437

to Sta 0400

180°00'

2. S.W.

(N.W.) Car Ho

351°2½' 303'

S.E. " "

355°3½' 289'

N.E. " "

0°01' 328'

Driveway

1°42' 349'

"

4°5' 361'

"

6°10' 367'

"

7°50' 367'

"

8°45' 381'

"

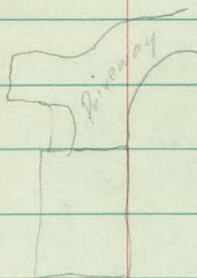
5°57' 379'

"

3°3' 374'

"

0°50' 384'



Sept. 16, 1960

161

Additional x-sections

Sta + π - Elev

BM 5.62 893.72

888.10

0+00

4.41 889.3

0-150'

0-200'

0-200

✓

FA
RG
JL
WM
RR

W
Lt

Sept 16, 1960
F
Rt

162

Spike in PP N.W. Cor Josephine & Lex.

93.2	90.0	88.1	87.9	89.1	89.1	89.3	88.8	88.4	85.1	84.5	84.5
0.4	3.7	5.0	5.8	4.6	4.6	4.4	4.9	5.3	8.6	9.2	9.2
37	32	27	23	18	12		13	20	30	35	44

4.4

✓

4.4

84.5
9.2
50

93.4	91.5	89.0	88.1	89.1	89.1	89.3	88.8	88.3	85.2	84.8
0.3	2.2	4.7	5.6	4.6	4.6	4.4	4.9	5.4	8.5	8.9
35	32	28	23	19	13		13	21	33	39

✓

84.3
9.4
50

897.59

Sta + π - Elev.

BM 4.64 892.74

888.19

A

✓

✓

+50

FK
WM
RR

LT

Sept. 19, 1960
Revised line

163

BT

Spike in PP NW Cor. Josephine & Lex.

85.3.	85.2.	85.4.	85.6.	85.8.	86.4.	86.7.	86.0.
7.4	7.5	7.3	7.1	6.9	6.3	6.0	6.7
57	47	31	11		14	21	47

85.7.	87.4.	87.8.	89.2.	84.2.	84.5.	85.4.
7.0	5.3	4.9	3.5	8.5	8.2	7.3
62	72	82	100	78	73	59
BT						

89.1.	88.1.	90.1.	89.6.
3.6	4.6	2.6	3.1
130	121	115	102
BT			

86.1.	85.6.	86.0.	86.2.	86.1.	86.1.	86.1.	85.5.
6.6	7.1	6.7	6.4	6.6	6.6	6.6	7.2
68	56	20	10		20	46	57

86.8.	87.8.	87.8.	89.7.
5.9	4.9	4.9	3.0
81	87	95	122
BT			

85.2.
75
75

91.9.	89.6.	89.9.
0.8	3.1	2.8
146	137	130

Sta + π - Elev.

BM 6.29 900.03

893.74

13+63.17

✓

14+00

✓

14+16

✓

FK
JL
WM
RR

Sept 20, 1960 164

LT

RT

Spike in Q. Polk.

94.2	93.2	92.9	91.8	91.8	85.6	85.7
5.8	6.8	7.1	8.2	10.2	14.4	14.6
30	14	9		11	29	42
94.9						95.0
5.1						15.0
38						59

94.8	94.9	94.2	93.6	93.6	91.7	81.8
5.2	5.1	5.8	6.4	6.4	8.3	12.2
46	28	12		19	36	56
95.0	94.7	94.1			95.2	95.6
5.0	5.3	5.3			14.8	14.4
62	73	79			78	71

91.2	96.1	96.2	95.1	93.9	92.0	96.1	93.7
2.8	3.3	3.8	4.3	8.1	6.0	3.9	6.3
48	36	28	16		9	18	41

95.2	94.8	94.8	94.8		95.2	90.3
4.7	5.2	5.2	5.2		14.8	9.7
52	61	67	80		80	56

STA

+

π

-

ELV.

900.03

14+27

✓

✓

T.P. 6.06 901.85 4.24 895.79

14+50

✓

+66

✓

Sept 20, 1960

165

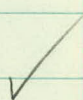
Lt		E		Rt			
97.1	96.6	96.7	97.1	94.0	94.2	96.9	
2.9	3.4	3.3	2.9	6.0	5.8	3.1	
26	15	5		5	12	17	
97.2	97.3	94.8	94.9	88.4	92.2	96.1	96.6
2.7	2.7	5.2	5.1	11.6	7.7	3.6	3.4
37	46	51	63	74	61	47	30

94.9
5.1
81

E of Lexington

94.8	97.1	91.6	91.6	98.2	98.0	
7.1	4.8	4.3	4.3	3.7	3.9	House
44	39	33	15		2	

95.1	95.2	95.3	95.2	
6.8	6.7	6.6	6.7	
50	57	69	86	



95.1	95.2	96.8	97.2	97.1	97.1	98.2	97.0	94.9	91.6
6.5	6.7	5.1	4.7	4.2	4.2	3.7	4.9	7.0	10.3
64	44	33	29	13		17	37	53	76



95.2
6.6
77

STA + π - ELEV.

901.85

15+00

✓

✓

+50

✓

16+00

✓

Sept. 20, 1960

165

Lt Q Rt
 94.5 94.5 96.8 96.9 96.8 96.8 96.4 93.9
 7.4 7.4 5.1 5.0 5.1 5.1 5.5 8.0
 33 29 25 13 18 34 53

95.5 95.5 95.6 95.5 91.5 91.6
 6.4 6.4 6.3 6.4 10.4 10.3
 36 42 55 69 75 67

94.8 95.8
 7.1 6.1
 78 73

95.8 95.8 93.7 93.7 96.0 95.5 95.1 94.7 94.5 93.5
 6.1 6.1 8.2 8.2 5.9 6.4 6.8 7.2 7.4 8.4
 29 23 19 16 9 19 39 59 69_{SS}

96.0 95.9 96.1 95.9 902.9
 5.9 6.0 5.8 6.0 11.0
 41 54 59 66 75

96.1 96.5 96.1 95.0 95.0 96.1 95.2 95.2 95.6

5.2 5.4 5.5 6.9 6.9 5.8 6.6 6.6 6.3
 30 6 10.1 7 7.3 5 24 44 59
 96.5 96.5 95.1 95.1 99.1 99.6 90.2
 5.4 5.4 6.2 6.2 2.4 2.3 11.7
 43 47 50 53 60 75 75

S+A + π - ELV.

T.P. 3.62 901.16 4.30 897.55 (897.54)

16+50

✓

17+00

✓

17+50

✓

T.P. 5.60 906.56 0.20 900.96

Sept. 20, 1960 166

Lt.

Q

Rt

BM	91.1	91.1	91.1	91.1	91.1	91.1	91.1	91.1
3.8	3.9	3.6	3.8	4.1	4.6	7.8	9.0	
37	32	21	7		4	10	25	

94.1	94.3	94.2	96.1	98.1	98.1	98.1	98.1	98.1
6.5	6.9	7.0	14.9	12.5	10.8	10.2		
46	59	75	75	60	46	38		

95.8	98.0	98.2	98.6	98.1	98.1	98.1	98.1	98.1
5.4	3.2	3.0	2.6	2.9	2.7	4.3	11.0	13.0
36	31	26	13		6	11	21	42

90.8	90.0	99.5	99.1	95.2	95.6	96.5
10.4	11.2	11.7	11.5	16.0	15.6	14.7
44	55	70	75	77	69	60

91.9	99.6	99.5	99.8	99.8	99.7	99.6	91.0	91.9
3.3	1.6	1.7	1.4	1.4	1.5	1.6	4.2	13.3
27	23	20	7		7	12	19	33

92.6	98.2	91.1	96.8	95.5	96.0	96.1	96.6
9.6	12.9	14.1	14.4	15.7	15.2	14.8	14.6
36	43	58	75	75	70	56	40

Q Lexington

STA	+	∇	-	ELV.
-----	---	----------	---	------

		906.56		
--	--	--------	--	--

18+00				
-------	--	--	--	--

✓				
---	--	--	--	--

18+50				
-------	--	--	--	--

✓				
---	--	--	--	--

19+00				
-------	--	--	--	--

✓				
---	--	--	--	--

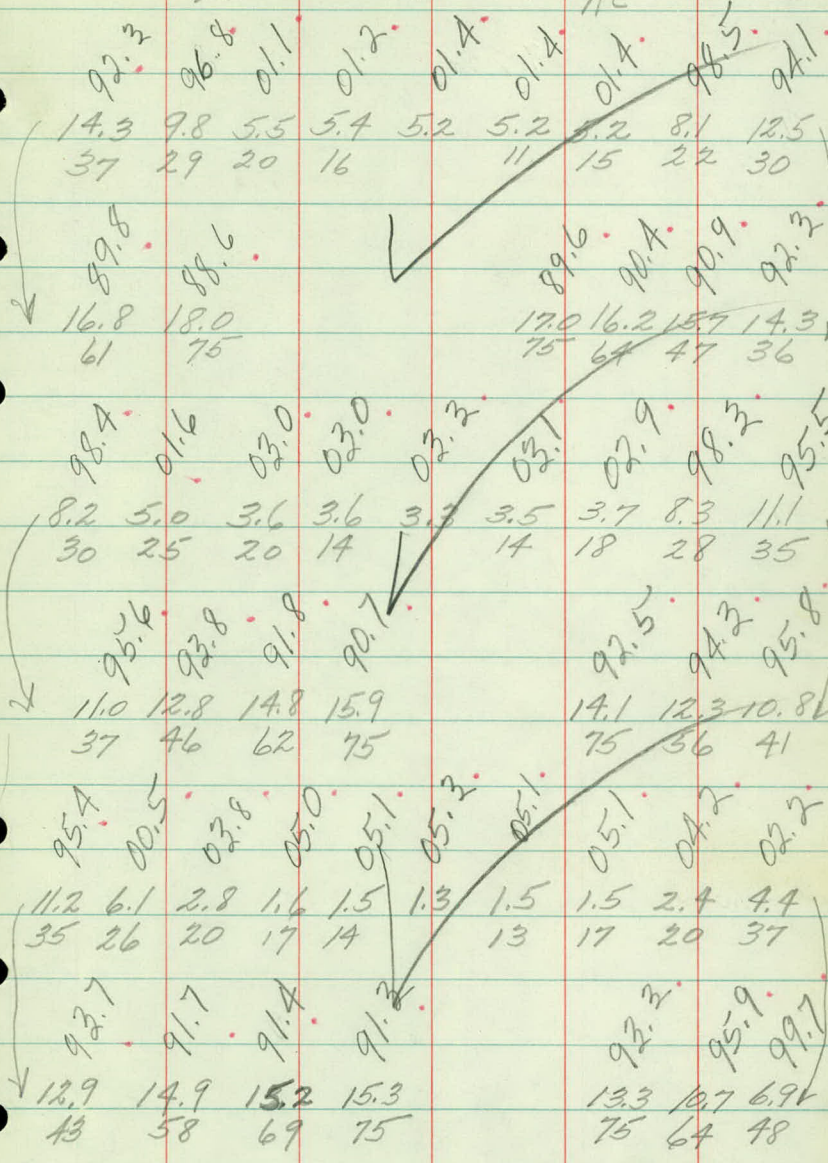
T.P.	12.67	917.93	1.30	905.26
------	-------	--------	------	--------

Sept. 20, 1960 167

Lt

♀

Rt



♀ STA. 19+00

STA	+	π	-	ELV.
-----	---	-------	---	------

		917.93		
--	--	--------	--	--

19+50				
-------	--	--	--	--

✓				
---	--	--	--	--

20+00				
-------	--	--	--	--

✓				
---	--	--	--	--

20+50				
-------	--	--	--	--

21+00				
-------	--	--	--	--

21+50				
-------	--	--	--	--

+

X

-

ELV.

917.93

22+00

B.M.

0.22 917.71

T.P.

1.91

907.18

12.66

905.27

B.M.

9.64 897.54

897.54

Sept 20, 1960 169

Lt

£

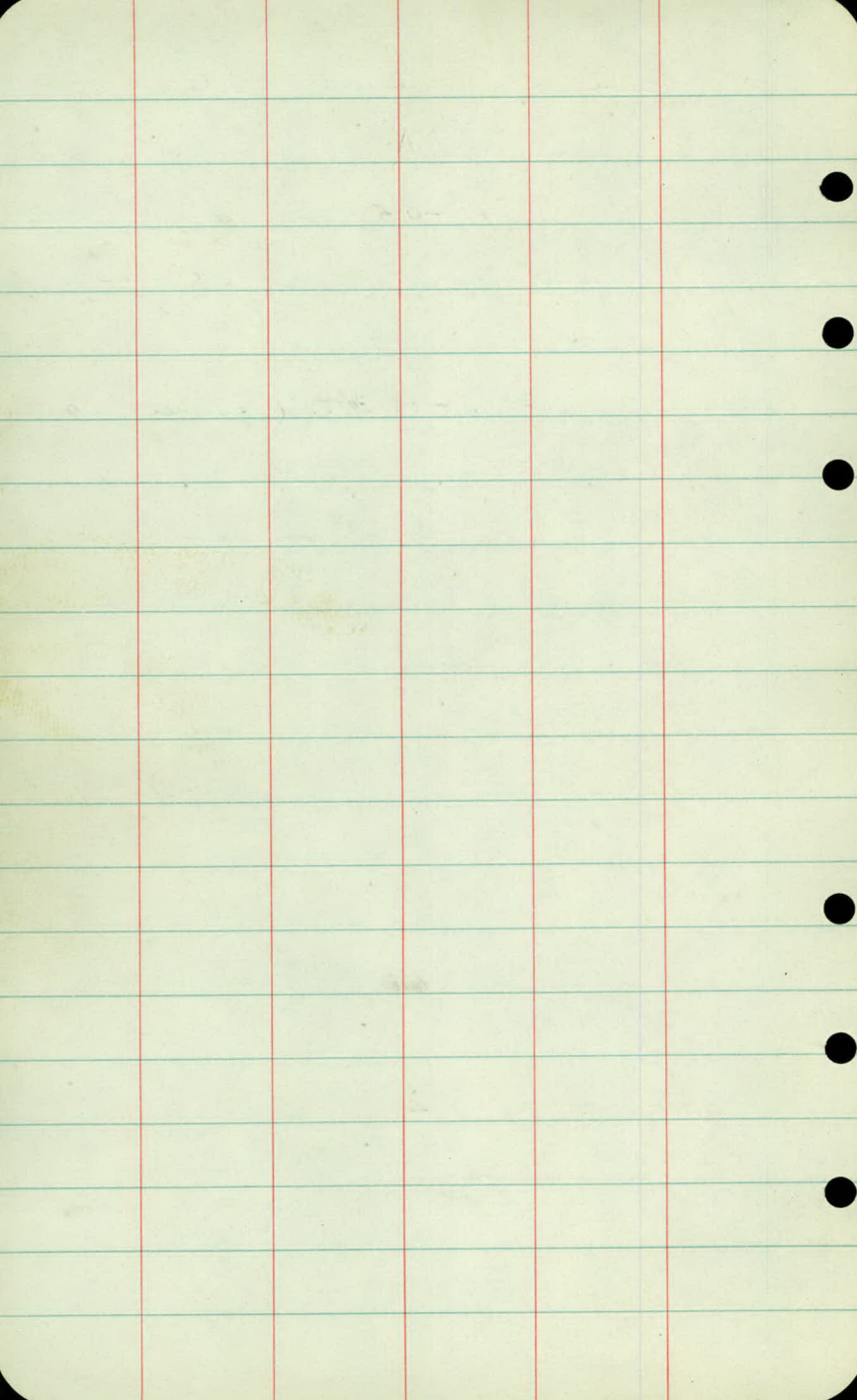
Rt

18.4
17.1
+0.5

SOUTH END SERVICE STATION CULVERT S TOP

£ STATION 19+00

Fence Post STA 16+80 30/2 (OLD LOCATION)



FX
JL
WM
RR

Sept. 21, 1960

120

Borrow Pit

Lexington Ave - CR to D

2+40.61

1+00

0+51.40

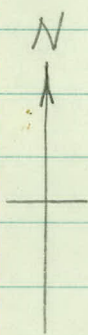
--- 43.60 ---

Iron

Boat Spike

E Brenner

1+68.44



0+00

75

13+63.17
PC

Sta + π - Elev.

BM 11.49 905.23 • 593.74

13+63.17

0+00

✓

✓

13+88

+25

✓

✓

TP 11.80 907.09 • 9.94 895.29 •

Sept 26, 1960

121

Lt

Rt

Spike in GP Lt sta 13t

94.6 94.4 94.2 94.4 94.9

10.6 10.8 11.0 10.8 10.3

46 28 13 59 ←

94.7 93.3 93.3 96.2

10.5 11.9 11.9 9.0

49 51 55 60

96.4 90.2 95.2 96.6 95.9

18.8 15.0 10.0 8.6 9.3

23 112 97 83 72

94.1 93.9 94.8 94.6 94.6 94.5

11.1 11.3 10.4 10.6 10.6 10.7

38 35 31 13 4.7 = 75' Lt

98.7 97.3 98.8 97.0

6.5 5.9 6.4 8.2

48 58 72 75

98.0 97.4

7.2 7.8

85 82

Sta + π - Elev

907.09 *

13+88
0+25

14+13
+50

✓

✓

✓

TP 3.25 908.34 * 2.00 905.09 *

14+38
+75

Sept 21, 1960 172

LT

RT

94.7 91.2 93.6 95.3
224 159 135 118
135 117 110 103

94.5 95.0 94.8 94.9 94.8
12.6 12.1 12.3 12.2 12.3
23 20 15 9.1 = 75

94.8 91.4 92.4 91.0
12.3 5.7 4.7 6.1
26 37 52 75

94.5 97.0 99.3 98.5 98.4
12.6 10.1 78 8.6 8.7
117 108 87 85 78

87.8 84.0
19.3 23.1
132 146
Step SE Cor H₀

92.4 95.0 94.9 95.3 94.9 95.0
59 133 134 130 134 133
26 11 8 5 14 = 75

Sta

+

π

-

$\angle$

14+38
0+75

908.34

✓

✓

14+63
1+00

✓

✓

FK
JL
WM

Sept. 22, 1960

173

11

RI

01.9 01.0 01.0 02.6 03.2

6.4 7.3 7.3 5.7 5.1

84 81 75 72 51

00.8 00.6 00.9 01.5 05.3

7.5 7.7 8.4 10.8 13.0

88 94 100 116 122

05.3 06.1

23.0 22.2

147 140

03.4 04.3 03.7 01.8 06.9 04.9 00.9 05.1 05.2

4.9 4.0 4.6 6.5 11.4 13.4 13.4 13.2 13.1

62 59 36 9 6 8 14 19

03.5 04.3 03.5 02.1 02.7

4.8 4.0 4.8 6.2 5.6

70 72 95 98 100

06.8 08.1 05.1 01.5 03.1

21.5 20.2 13.2 6.8 5.2

151 145 195 122 106

Sta + π - ELV.

908.34

15+01.67

1+38.5

S Line of Brenner

✓

✓

15+31.67

1+68.5

E of Brenner

✓

✓

T.P. 3.20 907.54 4.00 904.34

Sept 22, 1960

124

LT

2

RT

04.4

04.4

04.5

03.6

02.5

01.9

04.8

04.9

3.9
70

3.9
64

3.8
48

4.7
25

5.8

6.4
15

13.5
26

~~13.7~~
~~27~~

13.4
29=75

04.8

04.3

03.8

01.8

3.5
95

4.0
112

4.5
130

6.5
137

06.6

07.8

05.5

21.7
164

20.5
160

12.8
178

03.8

03.6

03.9

04.1

04.0

03.4

03.1

02.5

08.8

4.5
81

4.7
65

4.4
39

4.2
20

4.3

4.9
15

5.2
27

5.8
32

9.5
37.5=75

02.8

02.1

09.9

05.1

5.5
110

6.2
135

8.4
147

12.6
154

07.4

08.3

20.9
171

20.0
165

Top of 1st L 1+50

N Property Line = Base Line
Brenner

Sta.	+	Δ	-	ELV.
------	---	---	---	------

907.54

0+53 = 75' Lt on N Property Line

0+60

0+80

1+00

1+38

1+72

2+00

Sept 23, 1960

125

Lt

Q

Rt

02.5 02.6 02.7
5.0 4.9 4.8 ✓
=18 10
25' Lt

03.5 03.7 04.1 04.1 ✓
4.0 3.8 3.4 3.4
30 25 12

04.1 04.4 04.8 04.5 ✓
3.4 3.1 2.7 3.0
30 22 10

03.9 03.7 02.3 02.1 ✓
3.6 3.8 5.2 5.4
30 22 11

03.3 02.9 01.7 00.4 ✓
4.2 4.6 5.8 7.1
30 23 14

01.7 01.8 00.5 00.0 ✓
5.8 5.7 7.0 8.5
30 20 11

5+9. + $\wedge$ - ELV,

907.54 .

2+25

T.P. 5.97 905.03 . 8.48 899.06 .

2+40

2+50

2+69.6

T.P. 3.68 903.86 . 4.85 900.18 .

B.M. 6.29 897.57 . 897.54

Sept. 22, 1960

176

Lt

Q

Rt

02.6	01.5	00.2
4.9	6.0	7.3
30	18	



01.6	01.3	00.7	00.8
3.4	3.7	4.3	5.2
30	25	14	



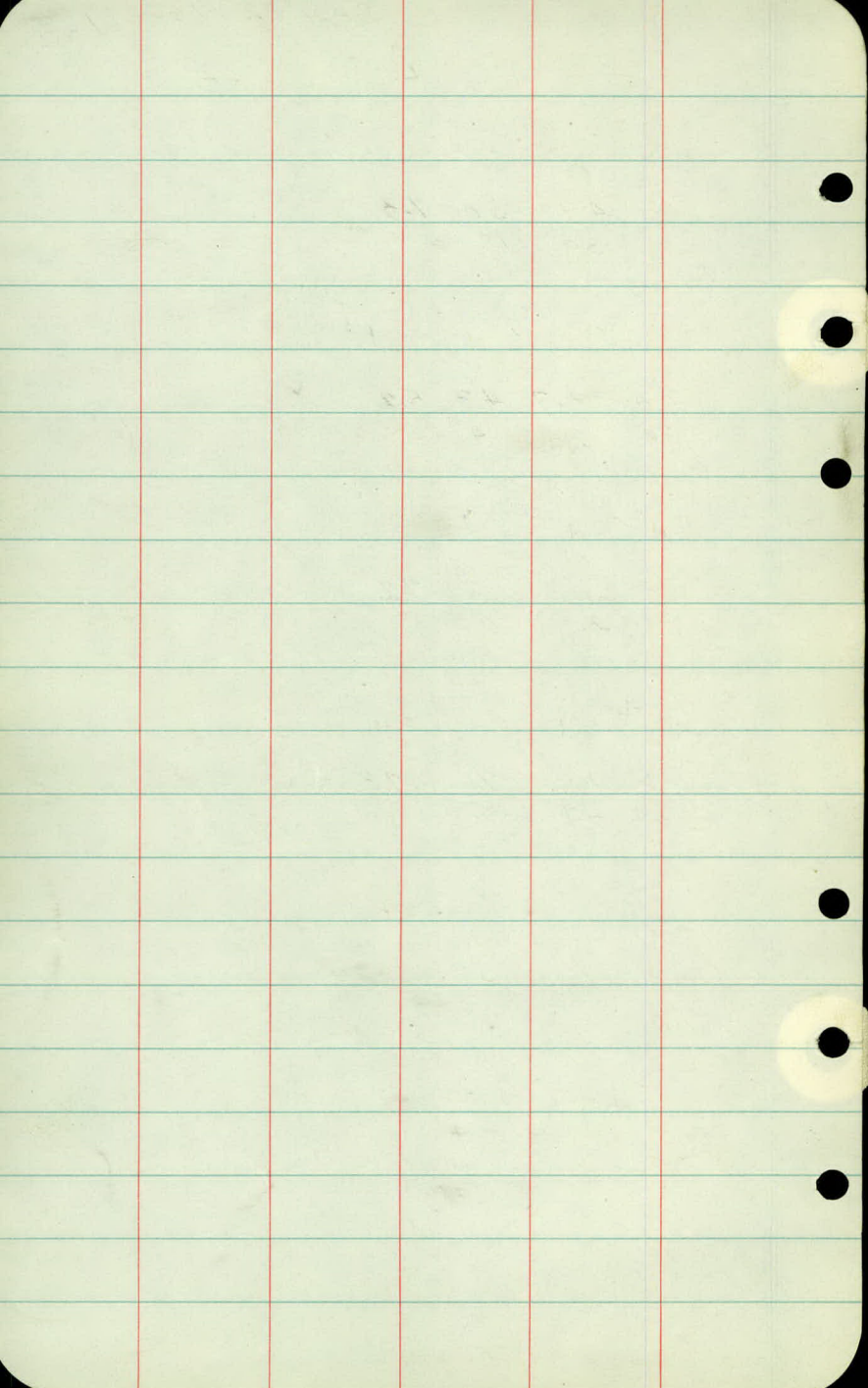
09.2	08.7	08.8	07.8
5.8	6.3	6.2	7.2
30	20	10	



87.4	88.2	88.0	87.7
17.6	16.8	17.0	17.3
30	24	12	



Fence Post Stamp



FX
JL
WM

Sept 27, 1960 177
a

Lexington Ave

Additional X-sections

Sta + π - Elev

BM 5.29 893.39

888.10

4+6 P.T.

5+50 $\pm$ Ent Lt

✓

✓

✓

BM 5.00 898.74

893.74

13+00

FK
JL
WM

Lt

L

Sept. 27, 1960 178
6

Rt

Spike in PPNW Cor Josephine & Lex

85.3
8.1

83.9	84.0	83.9	83.9	83.9	84.0	84.0	83.8
9.5	9.4	9.5	9.5	9.5	9.4	9.4	9.6
67	28	29	12		20	40	70

84.1	84.5	87.7	88.5	88.6
9.3	8.9	5.7	4.9	4.8
81	88	100	104	114

ERoad

88.7	89.0	89.1	89.1
4.7	4.4	4.3	4.3
177	153	139	127
		ER	ER

88.6
4.8
199

Spike in Guide Pole Lt 5th 12±

93.3	90.6	86.1	85.0	84.8	84.8	84.8	84.6	84.7
5.4	8.1	12.6	13.7	13.9	13.9	13.9	14.1	14.1
75	63	40	17		17	35	53	75

Sta + π - ELV.

898.74

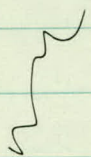
13+25

✓

14+50

✓

14



Sept 24, 1960

179^c

Lt

L

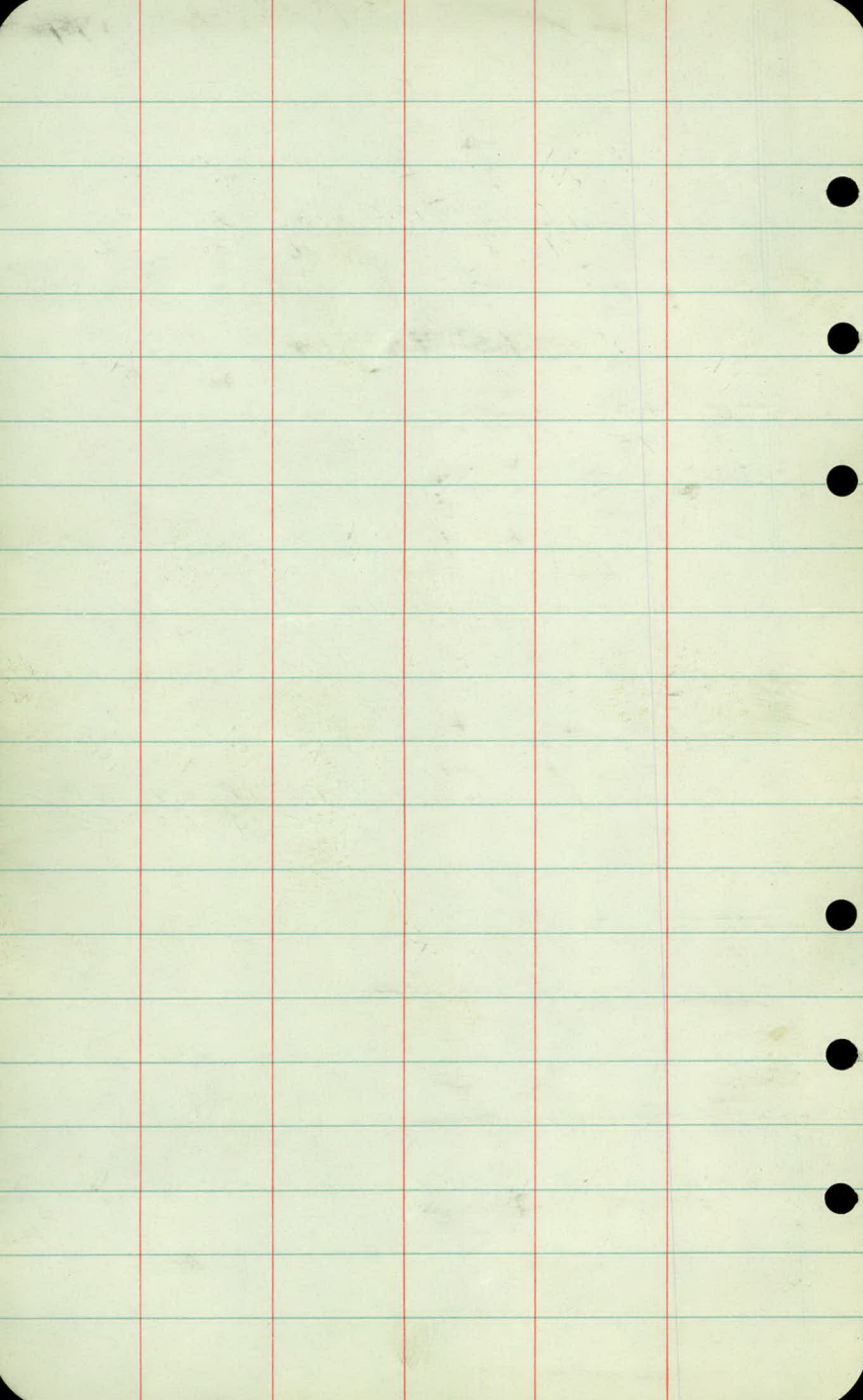
Rt

92.1	89.2	87.1	85.8	85.2	85.1	85.2	85.0
6.6	9.5	11.6	12.9	13.5	13.6	13.5	13.7
52	37	21	8		16	30	52
94.1	94.2						
4.6	4.5						
58	75						
							84.8
							13.9
							75

97.6	93.7	93.7	97.0
1.1	5.0	5.0	1.7
8	9	34	38

89.7	90.9	93.0	96.3
9.0	7.8	5.7	2.4
75	69	63	52

93.5
5.2



Josephine Rd.

Ent

Alinement &
X-sections

Sta Point ΔL ΔR

~~22+28.75~~ P.O.C. Δ Lexington

~~+62.35~~ P.T. $13^{\circ}22.5'$

~~+50~~ $11^{\circ}28'$

$\Delta = 26^{\circ}45'$ ✓

~~+25~~ $7^{\circ}35.5'$

$D = 31^{\circ}$ Arc ✓

~~21+20~~ P.I.

$T = 43.94$ ✓

~~21~~ $3^{\circ}43'$

$L = 86.29$ ✓

~~20+76.06~~ P.C. $0^{\circ}00'$

$R = 184.82$ ✓

18990

~~18+86.16~~ ? POT

18+86.77

FA
JL
WM

Oct. 3, 1960
Clear 60°

181

Beat Spike

189.90

52.18

52.63

Spike

sta	+	π	-	Elev.
BM	4.33	892.43		888.10
		992.43		988.10

20+76

21+00

+25

Oct 3, 1960

182

Lt

Rt

Spike in RR N.W. Co. Josephine A. & Mex. 1.0

Spike in RR	N.W. Co.	Josephine A.	Mex. 1.0
81.9	81.9	81.5	81.0
4.5	4.7	4.9	5.4
28	24	11	41

81.0 86.6

5.4 5.8

31 50

87.6

4.8

50

81.9	81.5	81.9	81.7	81.5	81.1	86.0
4.5	4.9	4.5	4.7	4.9	5.3	6.4
27	23	12		12	25	29

86.8 86.4

5.6 6.0

31 50

86.4 86.4

5.6 6.0

50 40

86.3	81.1	81.6	88.0	81.9	81.5	81.1	81.0	85.3
6.1	4.7	4.8	4.4	4.5	4.9	5.3	5.4	7.1
41	34	25	12		16	25	33	37

86.1

6.3

50

85.1

7.3

50

Sta

+

Σ

-

Elev.

892.43

992.43

21+50

✓

+78

✓

20+50

20+00

19+50

Oct 3, 1960

183

Lt

Q

Rt

88.7	88.6	88.5	88.3	87.7	87.1	87.0
3.7	3.8	3.9	4.1	4.7	5.3	5.4
50	43	17		17	32	40

84.1	84.3
8.3	8.1
50	45

87.6	88.0	88.3	88.4	88.4	88.2	87.7	87.1
4.8	4.4	4.1	4.0	4.0	4.2	4.7	5.3
50	33	11		23	38	50	58

87.4	86.0	85.2
5.0	6.4	7.2
66	85	100

84.8
7.6
70

88.0
4.4
88.4
4.0
88.8
3.6

Sta.

+

π 892.43 -

ELV.

992.43

19+00

4.33

888.10

888.10

988.10

988.10

Oct 3, 1960 184

Lt

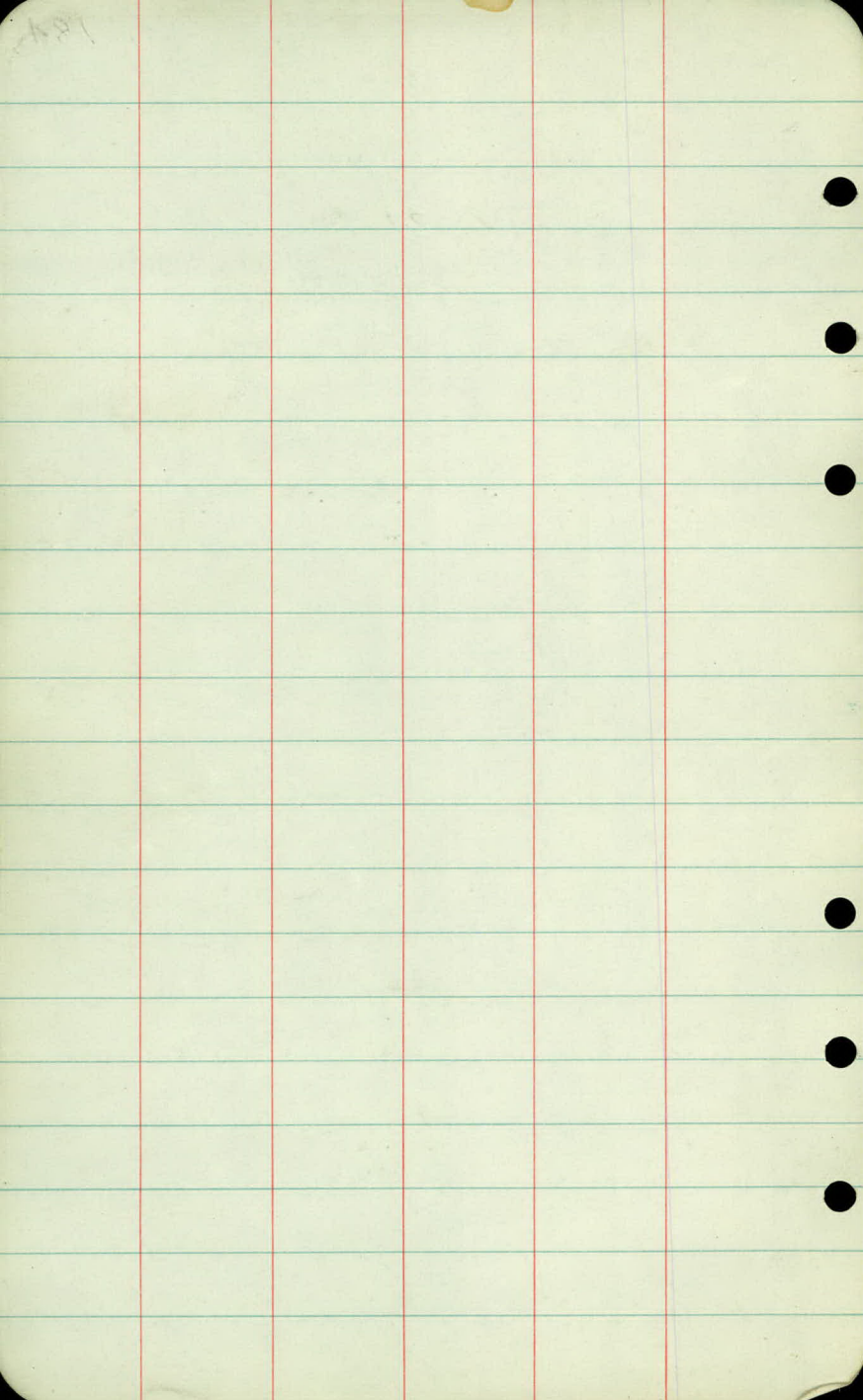
Q

Rt

89.3

3.1

Spike in p.p. Sas. & hex.



7 OCTOBER 1960

KP

185

KJ

Lexington Ave
Josephine Park
(swamp soundings)

3 PAGES

plotted KP

10/10/60

Sta LT

≠

RT

13+00

30'

0



1

2

3

4

5

6

7

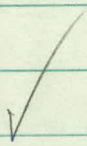
8

15

10

14

push



STA.

LT.

±

RT.

186

13+00

60'

0

1 0

2 0

3 3

✓ 4 5

5 6

6 8

7 11

8 14

Sta

LT

±

PT

13+25

0

1 5

2 7

3 16

4 60

5

30'

0

1 1

2 3

3 7

4 9

5 11

6 22

Sta

LT

±

RT

187

13+25 30'

60'

0

1

2

✓ 3

4 9

5 21

↑
push
↓

0

1 0

2 0

3 0

✓ 4 0

5 4

6 7

7 12

8 30

Sta

LT

#

RT

13+63

60'

0	
1	0
2	9
3	8
4	25
5	

312
300
12

298
280
18

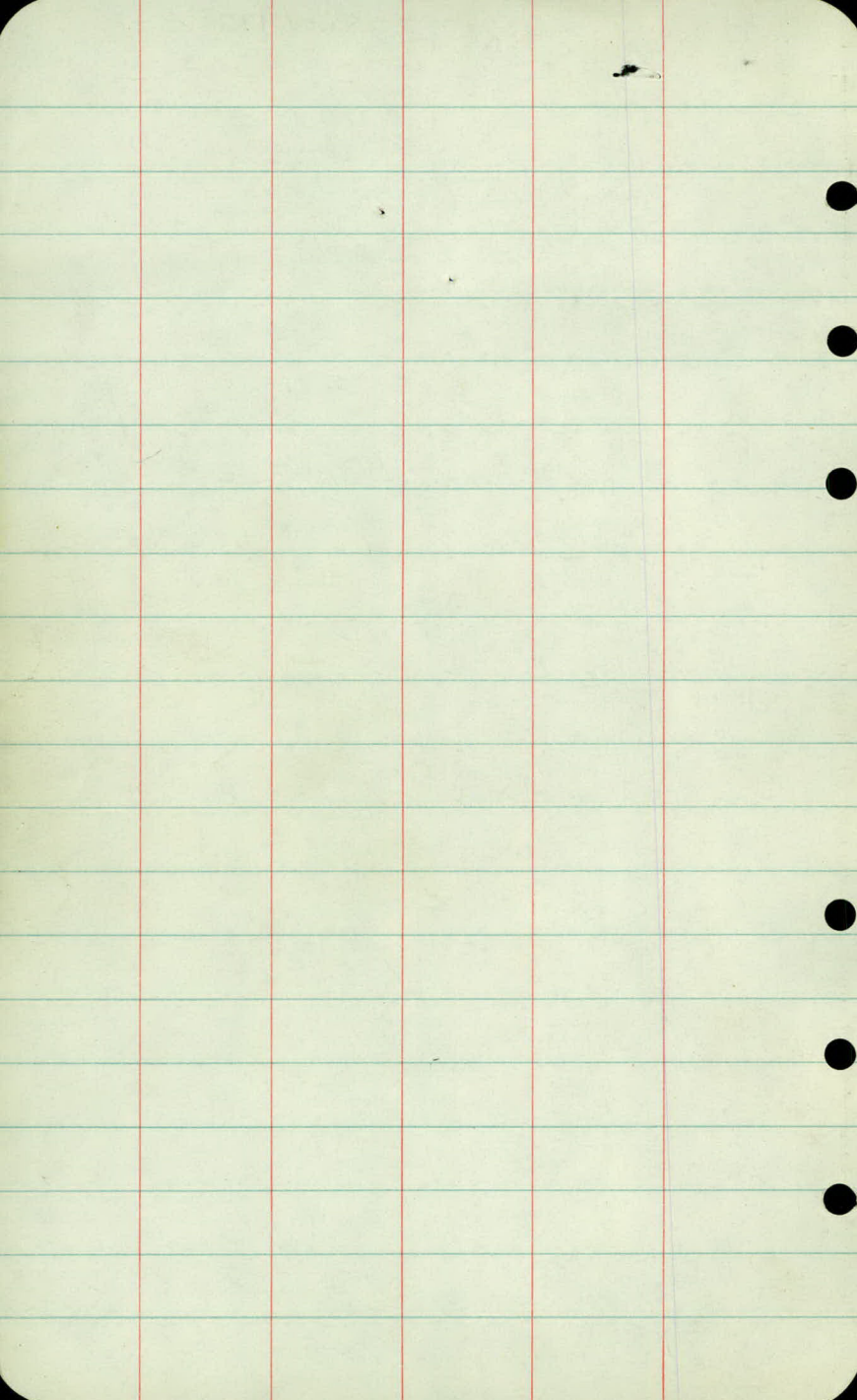
18 Nov. 1960

188

K.P.
JH
JL
FS
WM

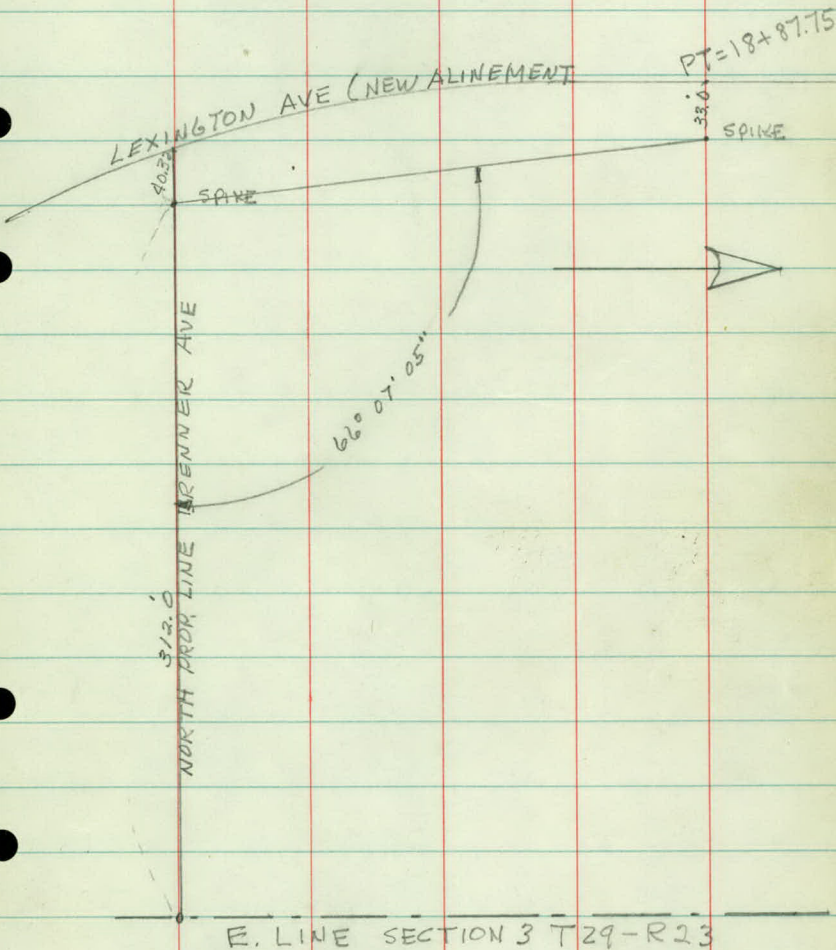
LEXINGTON AVE

60-TH10

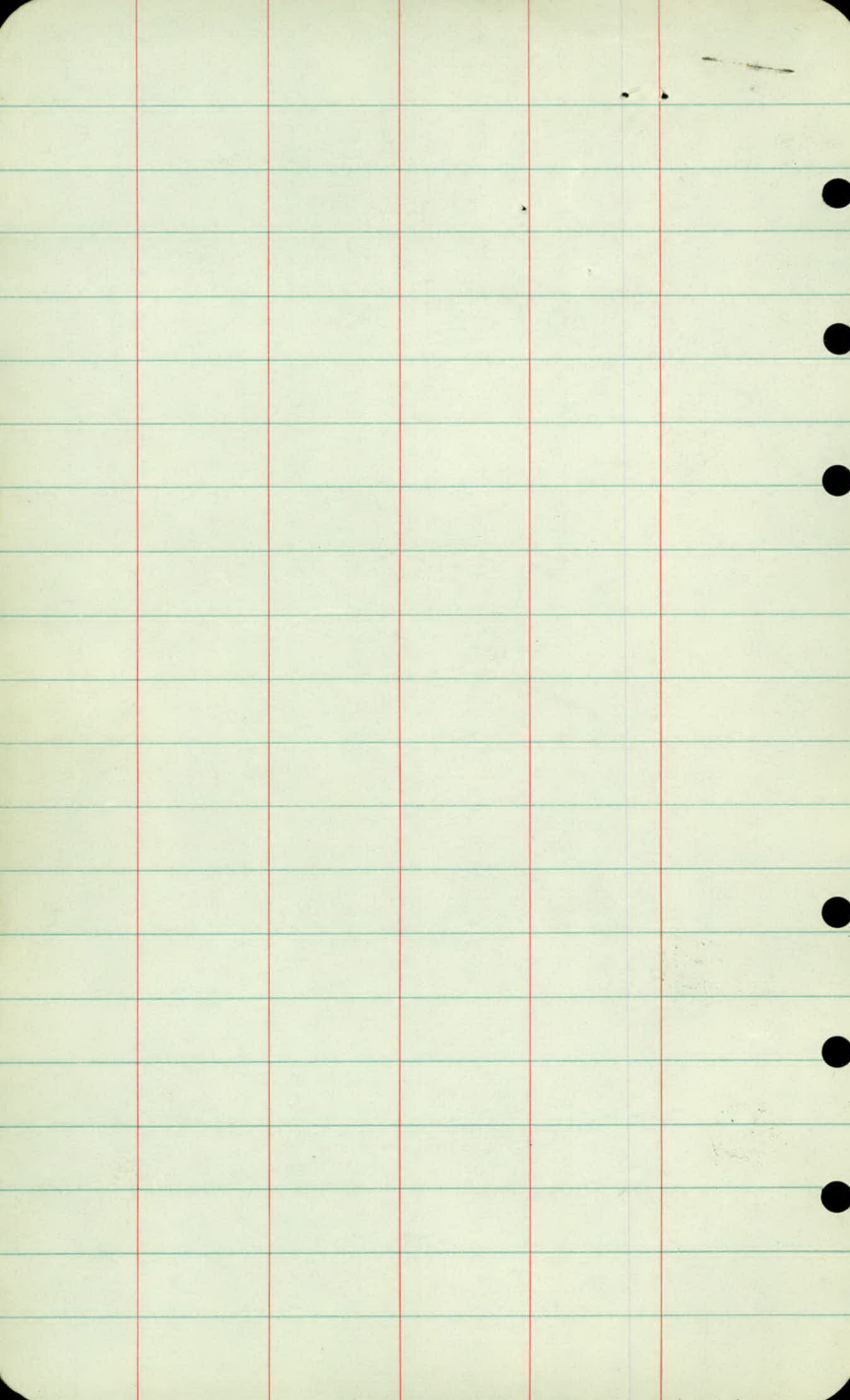


18 Nov. 1960

189



NOT TO SCALE.



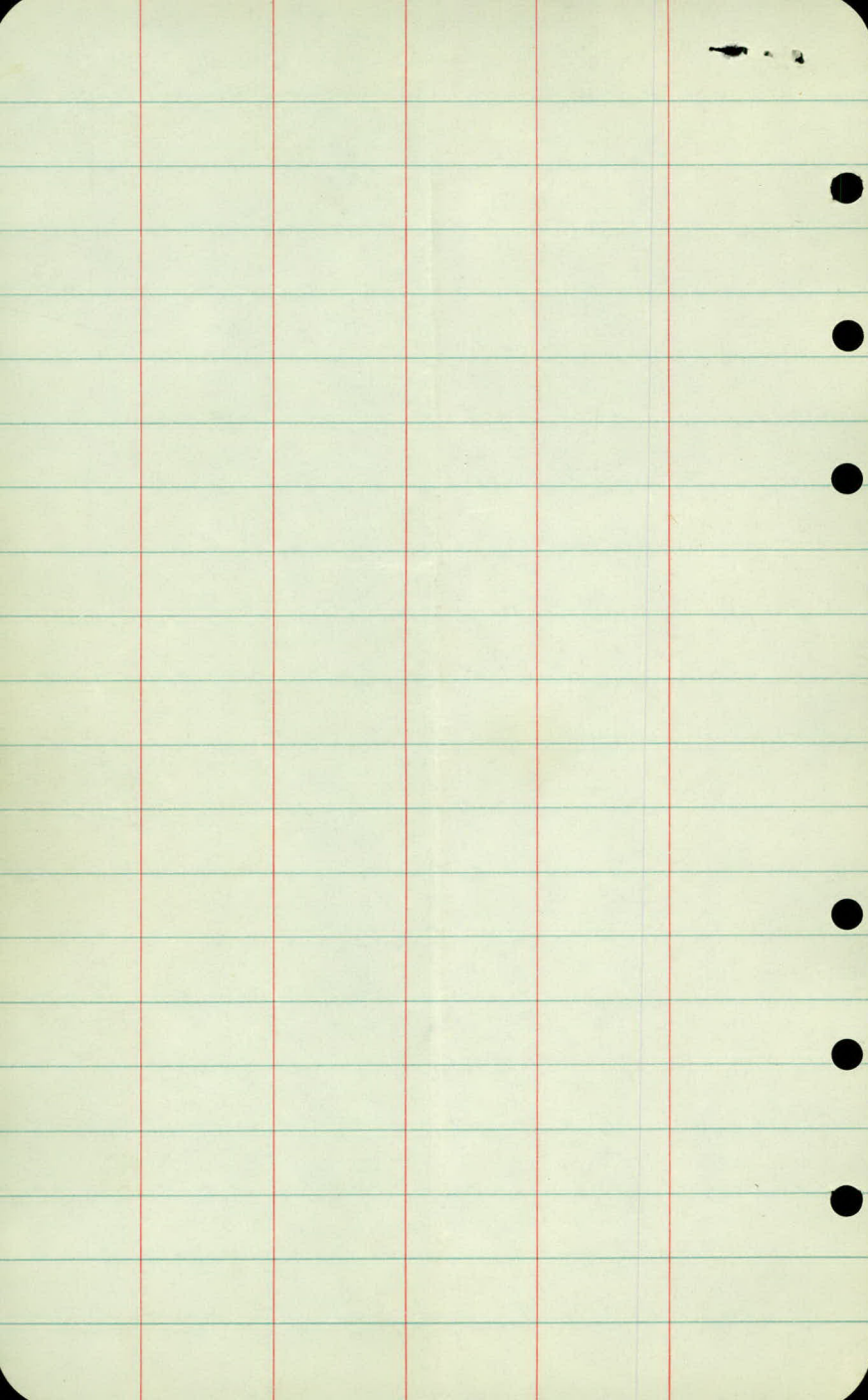
1
192

Lexington Ave.

At

Bremmer Ave.

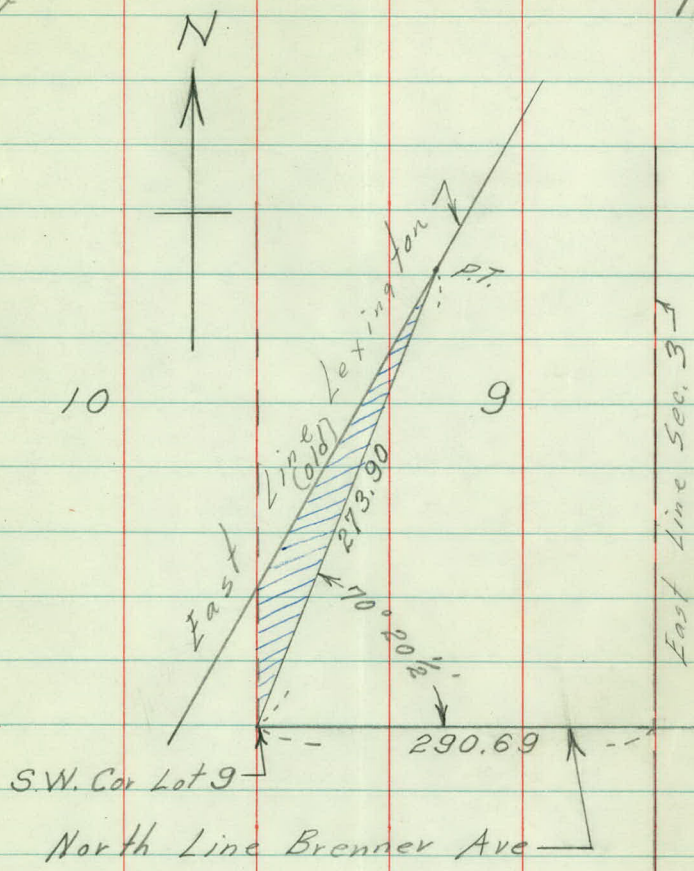
New R/W Line

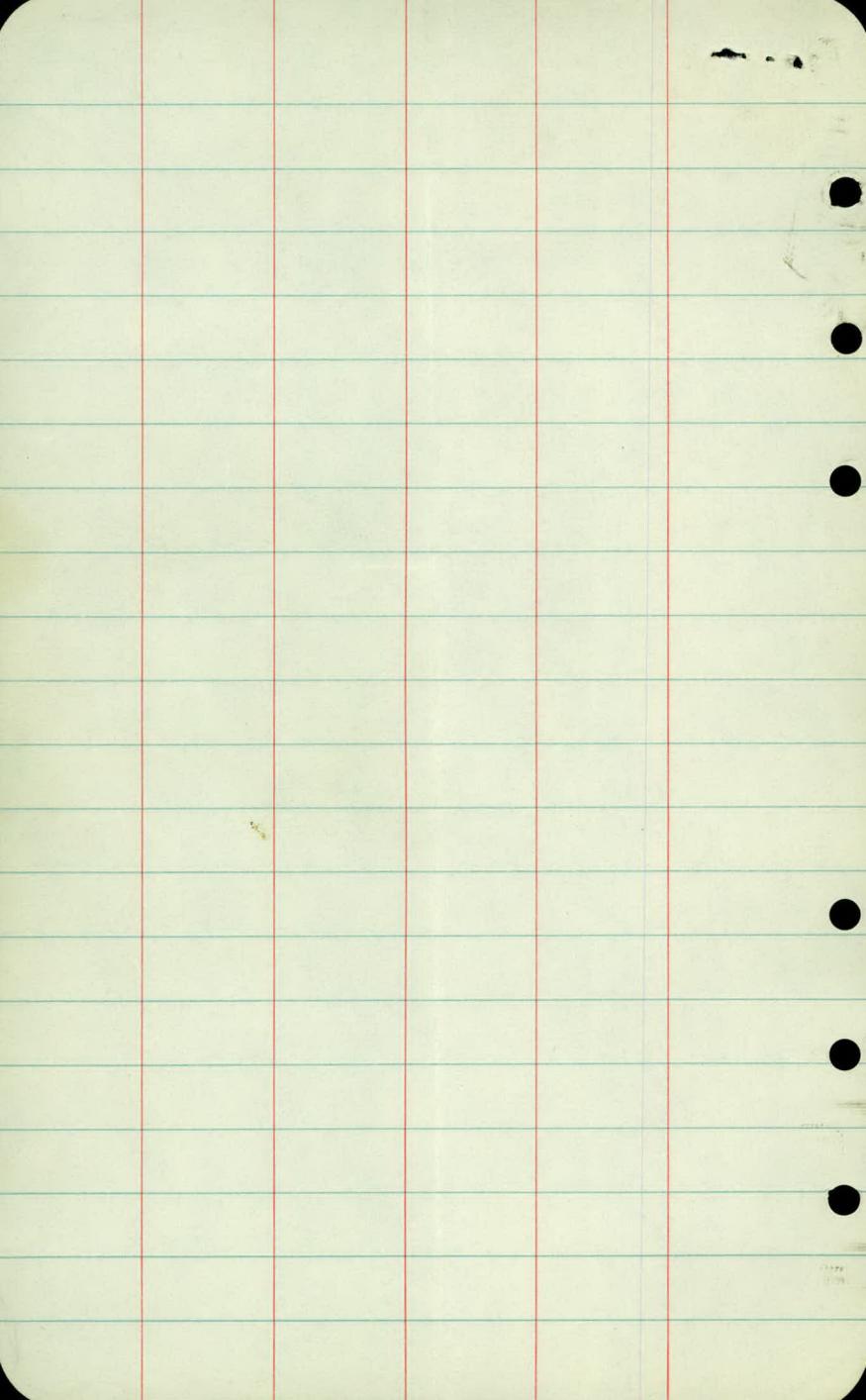


FK
WM
BZ
DF

August 15, 1961

2
191





Co. Proj. 60-T.H.10

Josephine Borrow Pit

Bench Levels

Borrow Pit

12 PAGES

Lexington Ave

Sta	+	Σ	-	Elev
BM _{#1}	5.54	893.64		888.10
TP ₁	3.91	893.82	3.73	889.91
TP ₂	5.35	893.94	5.23	888.59
TP ₃	7.04	899.96	1.02	892.92
TP ₄	12.75	912.13	0.58	899.38
TP ₅	13.39	924.57	0.95	911.18
BM _{#2}			7.62	916.95
TP ₆	2.81	927.31	0.07	924.50
BM ₃			4.71	922.60
	50.79		16.29	888.1
	16.29			34.50
	34.50			
BM ₃	47.7	927.37		922.60
TP ₆	0.21	924.71	2.87	924.50
BM ₂			7.76	916.95
TP ₅	1.21	912.41	13.51	911.20
			7.74	904.67
TP ₄	10.46	899.86	13.01	899.40
TP ₂	5.43	894.04	11.25	888.61
TP ₁	3.88	893.82	4.10	889.94
	76.75			
	66.77		5.68	888.14
				888.10

RG
IL
WM
JH

Dec 5, 1960

2

Spike in PP NW cor Josephine & Lexington

Nail in Hub

Top of stake

Spike in ground

top of stake

Top of Stake

Spike in PP by Pink House (1st P.P.)

Top of Fence Post. by 3rd PP

Spike in 5th P.P. (Transformer on Pole)

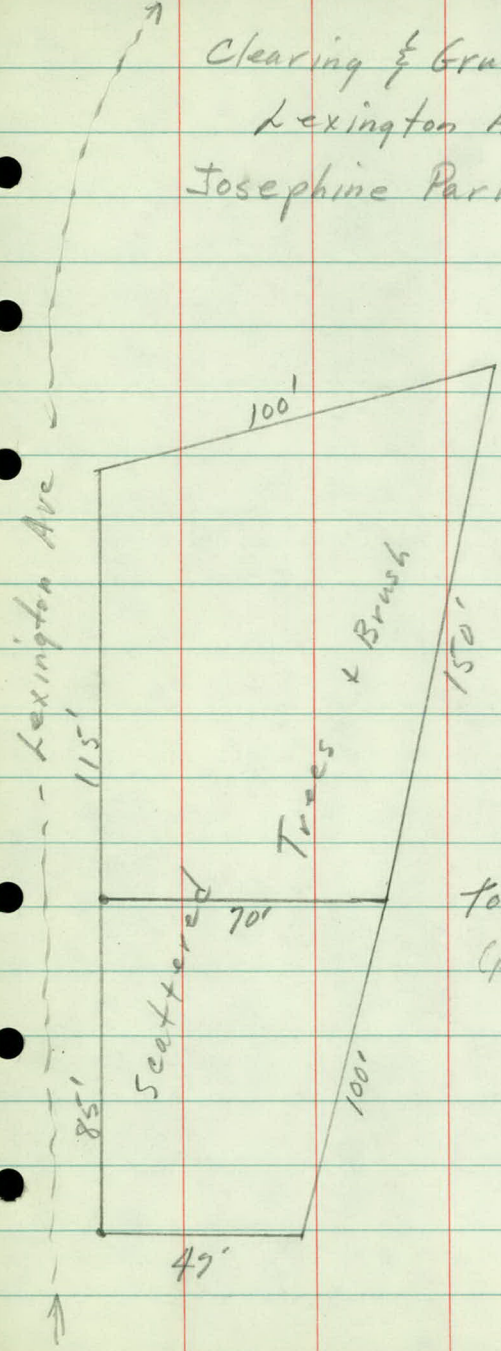
SOUTH Rim mt on service Road

426430.1 yds



1-20-60

Clearing & Grubbing Lexington Ave Josephine Park



Total = .355 Acre
(planimetered)

GrT Nat. Ground about

Sta 8+00 to 8+45

90' $\pm$ R+6 150' $\pm$ R+

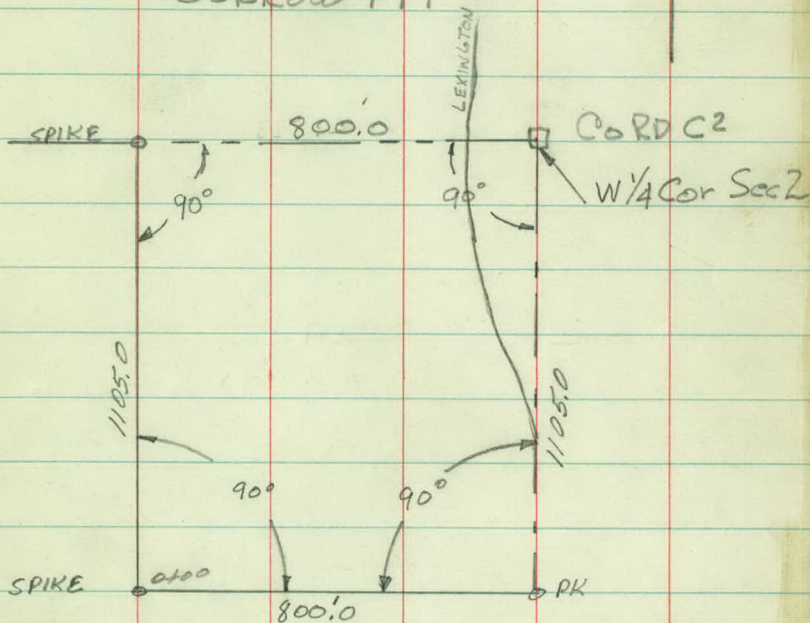
K.P.
J.S.
F.S.
L.B.
R.B.

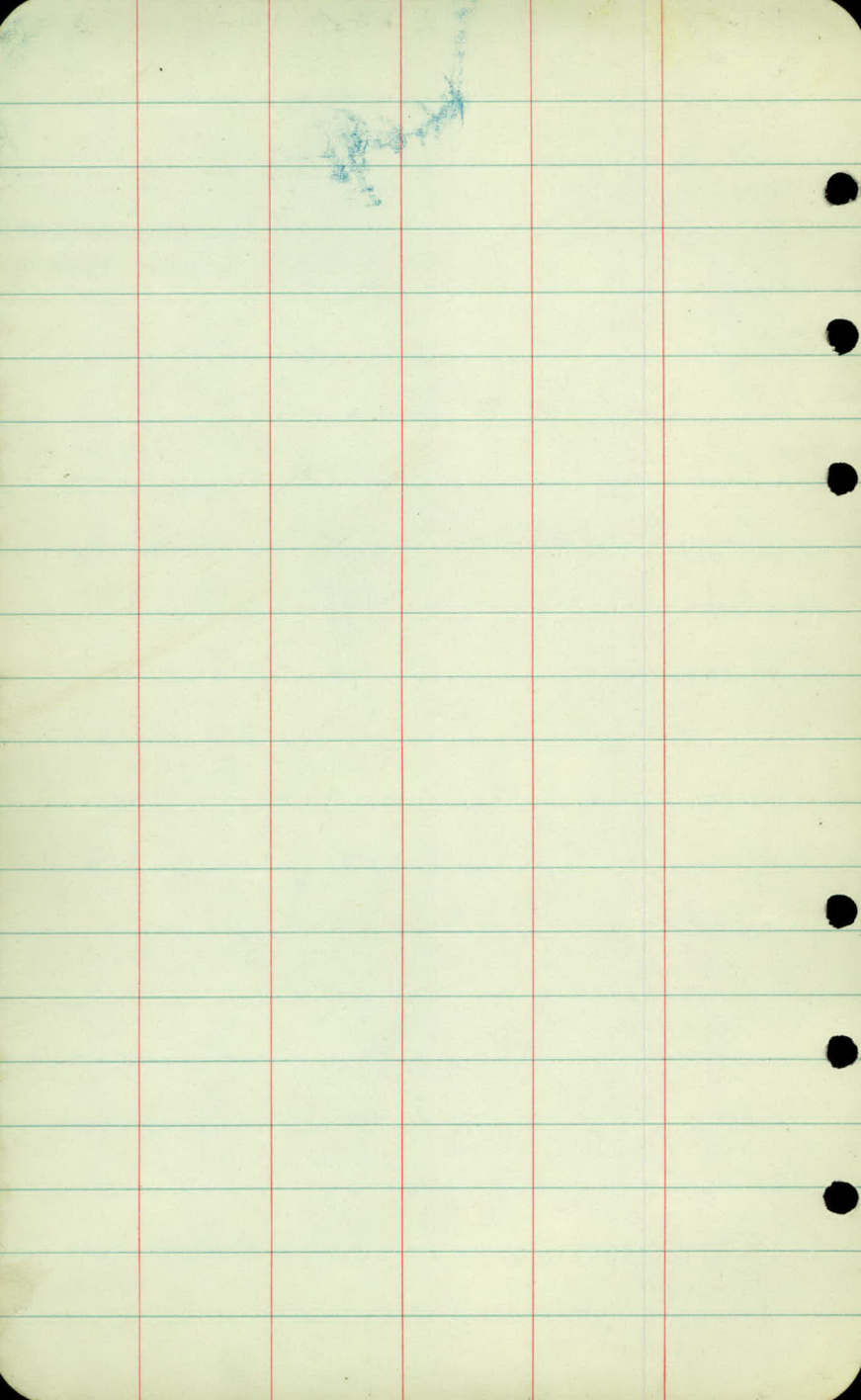
5 DEC. 1960
35° CLOUDY

2

LEXINGTON AVE

BORROW PIT





K.P. PG
US JL
FS WM
RB JH
LB

6 DEC. 1960
Cold 17°

3.

LEXINGTON AVE
BORROW PIT
X-sections

pages 3-23

STA	+	π	-	ELEV
-----	---	-------	---	------

BM	8.79	925.74		
----	------	--------	--	--

916.95

8+00

✓

✓

+45

✓

LT

Z

RT

SPIKE IN P.P. (1st) by Pink Ho.

20.5	22.3	25.1	24.4	25.1	25.3	23.9	20.2
5.2	3.4	0.6	1.3	0.6	0.4	1.9	5.5
35	20	9		17	27	42	71
Fe.							

11.1	12.4	15.3	17.4
14.6	13.3	10.4	8.3
159	138	119	100

11.5	14.1
14.2	11.6
170	200

19.7	19.9	22.0	21.9	23.2	22.9	22.4	22.3	21.9	18.7	16.0
6.0	5.8	3.7	3.8	2.5	2.8	3.3	3.4	3.8	7.0	9.7
37	24	20	15	6		14	26	34	54	76
Fe										

02.7	03.9	06.9	09.2	11
23.0	21.8	18.8	16.5	14.0
169	158	137	120	100

02.5	02.8
23.2	22.9
185	200

Sta

+

π

—

ELEV

925.74

8480

r

r

9400

✓

+53

Lt Lt Pt

19.6	18.7	19.6	18.8	19.7	15.8	16.6	17.2	13.5
6.1	7.0	6.1	6.9	6.0	9.9	9.4	8.5	12.2
36	26	21	12		19	37	56	78
Fe								

03.0	06.1	05.7	07.3	11.4
22.7	20.6	20.0	18.4	14.3
146	126	108	100	91

00.8	09.9	00.0
24.9	25.8	25.7
164	184	200

19.4	18.3	11.7	08.8	08.0	07.2	07.3	07.9	07.6
6.3	7.4	14.0	16.9	17.7	18.5	18.4	17.8	18.1
37	27	21	10		27	47	66	100
Fe								

99.1	99.5	01.6	01.1	05.9
24.6	26.2	24.1	21.6	19.8
200	172	149	130	112

18.8	18.4	17.1	13.1	08.8	00.9	05.2	06.2	06.3
6.9	7.3	8.6	12.6	16.9	18.9	20.5	19.2	19.4
38	32	28	14		9	23	38	66

Sta

+

π

-

ELEV.

925.74

9+53

✓

9+70

✓

✓

10+00

Lt

2

Rt

06.1 5.8 04.0
19.4 19.9 21.7
89 100 118

27.7 27.6 28.2 0.6
28.0 28.1 27.5 25.1
200 195 169 139

18.4 16.7 13.0 9.8 7.4 0.5 0.7 0.9
7.3 9.0 12.7 16.9 18.3 25.2 25.0 24.8
35 26 13 15 31 48 62

3.8 5.7 6.2 4.5 4.1
21.9 200 19.5 21.2 21.6
114 100 89 85 76

01.2 99.3 97.9 96.9
24.5 26.4 27.8 28.8
130 140 170 200

16.1 14.0 13.3 9.7 7.9 5.1 0.9 0.8
9.6 9.7 12.4 16.6 17.8 20.6 24.8 23.9
37 28 17 7 12 21 48

Sta	+	π	-	Elev
-----	---	-------	---	------

		925.74		
--	--	--------	--	--

10+00				
-------	--	--	--	--

✓				
---	--	--	--	--

428				
-----	--	--	--	--

39				
----	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

+39				
-----	--	--	--	--

Lt \$ RT

03.7 05.3 02.3
 22.0 20.4 23.4
 87 100 112

06.0 05.5 07.0 00.4
 29.7 30.2 28.7 25.3
 200 169 144 132

15.9 16.9 12.1 09.7 07.6 02.4 01.9 02.2 10.0
 9.8 9.8 13.6 16.0 18.1 23.3 23.8 23.5 20.7
 34 26 10 13 22 43 65 73

06.0 02.1 01.9 05.9 05.5
 29.7 23.6 23.8 19.8 20.2
 129 128 116 100 87

04.8 05.6 05.2
 30.9 30.1 30.5
 164 189 200

15.9 15.7 16.1 12.7 10.1 07.9 07.3 07.2 06.4
 9.8 10.0 10.6 13.0 15.6 17.8 18.4 18.5 19.3
 35 28 23 12 16 35 60 79

Sta	+	π	-	ELEV.
-----	---	-------	---	-------

		925.74		
--	--	--------	--	--

10+39				
-------	--	--	--	--

✓				
---	--	--	--	--

+56				
-----	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

+75				
-----	--	--	--	--

6 DEC. 1960

8

27

E

Rt

5.5 5.0 1.5
 0 0 0
 20.2 29.7 24.2
 100 119 127

94.6 95.4 94.9 94.6 96.0
 31.1 30.3 30.8 31.1 29.9
 200 190 176 159 151

15.6 14.2 13.3 12.5 11.2 9.2 7.3 4.7
 10.1 11.5 12.4 13.2 14.5 16.5 18.4 21.0
 34 21 13 25 51 73 100

94.5 94.2 96.3 99.2 93.8
 31.2 31.5 29.4 26.5 21.9
 188 175 152 138 126

93.7
 32.0
 200

14.5 13.8 12.6 11.9 10.8 9.3 6.4 3.7
 11.2 11.9 13.1 13.8 14.9 16.4 17.3 22.2
 34 24 13 23 46 74 100

S/a

+

π

-

ELEV.

925.74

10+75

✓

+95

✓

11+05

MH 111.0 RT $\pm$

✓

2+

±

6 DEC. 1960

Rt

9

07.3	09.1	04.6	03.9
23.4	26.6	31.1	31.8
122	140	163	186

03.1
32.6
200

17.8	11.8	10.5	10.2	08.7	06.9	05.1	04.5
12.9	13.9	15.2	15.5	17.0	18.8	20.6	21.2
43	24	5		18	50	85	100

03.1 03.7 05.1 08.5 02.8
32.6 32.0 30.6 29.2 22.9
200 189 162 141 118

12.7	12.0	11.4	09.5	07.2	05.5	05.3
13.0	13.7	14.3	16.2	18.5	20.2	20.4
35	13		28	59	84	100

07.1 05.1 08.7 07.7 04.4
33.6 32.6 27.0 25.0 21.3
200 170 148 136 117

Sta

+

π

-

925.74

8+45

✓

✓

Lt

E

RT

10.

02.8

01.1

05.0

05.4

22.9

21.6

20.7

20.3

200

218

224

254

06.9

05.2

05.2

05.4

05.7

06.0

19.8

20.5

20.5

20.3

20.0

19.7

395

388

360

325

300

271

05.6

05.1

05.3

05.7

20.1

20.6

20.4

20.4

400

428

450

456

09.1

01.6

03.4

26.6

24.1

22.3

500

473

465

Sta

+

K

-

ELEV

925.74

8+00

✓

Tp

11.61

936.10

1.25

924.49

5+00

✓

L+

E

R+

11.

14.2	16.7	16.8	18.6	20.0
11.5	9.0	8.9	7.1	5.7
200	227	253	280	300

9.3	10.9	12.6	10.5	11.4	18.9
16.4	14.8	13.1	7.2	8.3	6.8
450	428	400	373	339	326

07.4	6.2
18.3	20.5
475	500

Top Fe Post (Steel)

21.6	21.6	21.9	26.1	27.8	27.7	25.4
14.5	14.5	14.2	10.0	8.3	8.4	10.7
27		18	40	70	100	125
Fe						

19.6	19.5	23.1	25.4
16.5	16.6	13.0	10.7
240	200	170	148

21.0	23.0	21.7	25.4
15.1	13.1	9.0	10.9
268	300	346	385

2.0
12.1
400

Sta	+	Δ	-	ELEV
-----	---	----------	---	------

		936.10		
--	--	--------	--	--

5+00				
------	--	--	--	--

+50				
-----	--	--	--	--

Lt

L

Rt

12

~~23.4~~
~~12.7~~
~~452~~

~~19.7~~
~~16.4~~
~~500~~

~~22.0~~
~~14.1~~
~~29~~
~~66~~

~~22.8~~
~~13.3~~
~~21~~

~~21.4~~
~~9.7~~
~~21~~

~~29.8~~
~~6.3~~
~~29~~

~~31.9~~
~~4.2~~
~~66~~

~~31.5~~
~~4.6~~
~~100~~

~~19.0~~
~~17.1~~
~~226~~

~~21.8~~
~~14.3~~
~~200~~

~~23.6~~
~~12.5~~
~~181~~

~~27.8~~
~~8.3~~
~~142~~

~~18.5~~
~~17.6~~
~~270~~

~~20.4~~
~~15.7~~
~~300~~

~~3~~
~~12.8~~
~~330~~

~~16.6~~
~~9.5~~
~~359~~

~~18.3~~
~~17.8~~
~~500~~

~~24.0~~
~~12.1~~
~~444~~

~~26.4~~
~~9.8~~
~~400~~

~~27.9~~
~~8.2~~
~~379~~

Sta	+	π	-	ELEV.
-----	---	-------	---	-------

		936.10		
--	--	--------	--	--

6+00				
------	--	--	--	--

v				
---	--	--	--	--

7+00				
------	--	--	--	--

v				
---	--	--	--	--

TP	0.31	924.83	11.58	924.52
----	------	--------	-------	--------

			7.86	916.97	916.95
--	--	--	------	--------	--------

LT ~~4~~

RT

13

21.9	24.2	31.6	33.9	31.3	28.6	27.9	26.3
14.2	11.9	4.5	2.2	4.8	7.5	8.2	9.8
31		29	48	100	148	173	200
FC							

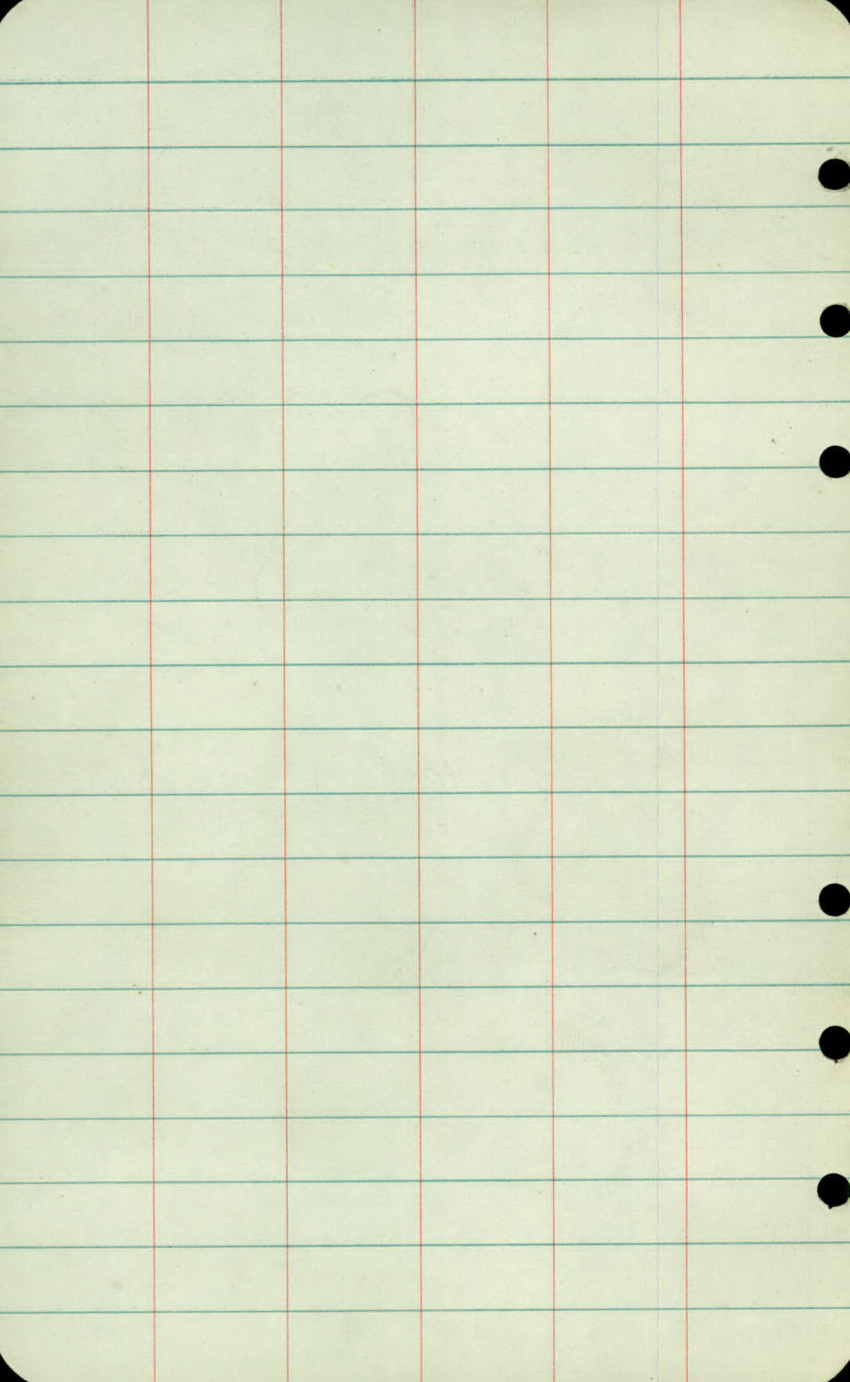
18.0	24.3	28.5	29.9	24.6	20.1	19.0	21.9
18.1	11.8	7.6	6.2	11.5	16.0	17.1	14.3
500	451	400	374	340	300	264	222

✓ 11.1	✓ 11.1	✓ 5.3	✓ 26.4	✓ 9.4	✓ 30.1	✓ 30.0	✓ 9.5	✓ 27.6	✓ 24.2	✓ 22.1
15.0	12.0	10.8	7.7	6.7	6.0	6.1	6.6	8.5	11.9	14.0
34	20		21	24	56	100	138	166	200	227

✓ 20.4	✓ 2.4	✓ 18.8	✓ 21.1	✓ 5.4	✓ 2.7	✓ 2.8	✓ 2.2	✓ 21.0
15.7	8.7	7.3	9.0	10.7	12.4	13.3	13.9	15.1
450	400	382	353	329	300	284	265	250

TOP ROCK

NAIL IN 1ST PP BY PINK Ho.



RG
JK
WM
JH

Dec 7, 1960

14

Josephine Borrow Pit

Additional X-Sections $\frac{1}{2}$

Extension X-Sections

Sta	+	A	-	Elev
TBM	11.05	935.55		924.50
4+50				
✓				
✓				
✓				
5+25				
✓				

RG
JL
WM
JH

Dec 7, 1960
cloudy, 22°

1.3

wooden
Top of Fence Post by 3rd R.P.

22.0	21.5	20.5	19.6	19.1	17.0	16.8	18.4
13.6	14.1	15.1	16.0	16.5	18.6	18.8	17.2
26	15		27	60	100	150	200
Fe							

29.5	27.5	24.3	21.7	20.2
6.1	8.1	11.3	13.9	15.4
321	300	283	260	235

29.0	27.5	26.8	26.6	26.4	26.9
6.6	8.1	8.8	9.0	9.2	8.7
337	365	388	400	431	456

23.9	25.4	26.5
11.7	10.2	9.1
500	483	470

21.6	22.5	22.5	22.4	21.3	20.5	21.6	21.6
14.0	13.3	14.1	13.2	8.3	5.1	4.0	4.0
27	14		10	33	69	90	100
Fe							

18.8	20.5	23.1	27.9	30.7
16.8	15.1	12.5	8.2	4.9
221	200	175	148	120

Sta

+

 π

-

Elev

935.55

5+25

✓

5+75

✓

✓

✓

L+

E

P+

16

20.4	21.9	24.6	26.2	26.1
15.2	14.2	11.9	9.3	9.5
261	300	324	345	378

17.9	20.7	22.8	23.8	24.6
12.7	14.9	12.8	11.8	11.0
500	478	456	427	400

22.1	22.8	23.9	25.2	27.9	31.5	31.9	32.7	31.3
13.5	12.8	12.2	10.4	8.2	4.1	2.7	2.9	4.3
30	16		5	20	29	49	78	100
FC								

19.9	24.8	26.0	27.0	28.8
15.7	10.8	9.6	8.6	6.8
241	200	185	161	127

18.3	20.0	21.7	26.9
17.3	15.6	13.9	8.7
283	300	329	356

3.8	5.5	28.7	29.8	29.9
11.8	10.1	6.9	5.8	5.7
450	425	400	395	379

Sta.

+

π

-

ELV.

935.55

5+75

6+25

✓

✓

✓

✓

Dec 7, 1960

Lt

L

Rt

17

21.3

17.9

14.5

17.7

474

500

22.0

22.1

23.3

23.4

28.8

27.4

24.0

31.7

13.6

12.5

12.3

10.2

6.8

3.2

2.6

3.9

32

23

11

16

24

49

70

Fe.

27.4

29.7

30.0

31.6

8.2

5.9

5.6

4.0

200

164

136

100

22.4

20.1

22.3

✓

13.2

15.5

13.3

240

267

300

26.1

28.1

28.6

26.4

9.5

7.5

7.0

9.2

443

400

362

333

19.9

16.9

✓

15.7

18.7

479

500

Sta	+	π	-	Elev
-----	---	-------	---	------

		935.55		
--	--	--------	--	--

6+50				
------	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

6+75				
------	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

Dec 1, 1960

18

Rt

21.6	23.6	23.7	25.6	28.7	32.8	32.0	31.2	31.8	30.8	29.2	27.5
14.0	12.0	11.9	10.0	5.9	2.8	3.6	4.4	3.8	4.8	6.4	8.1
32	21	11		17	20	44	67	100	140	177	200
fc											

27.5	28.5	28.7	27.6	24.5	21.7	22.0	24.7
8.1	7.1	6.9	8.0	11.3	13.9	13.6	11.9
429	400	376	343	300	271	254	232

22.4	16.4
13.2	19.2
466	500

21.4	23.0	24.2	24.3	25.3	27.3	31.7	31.2	30.8
14.2	12.6	11.4	11.3	10.1	8.3	3.9	4.4	4.8
39	25	21	8		11	21	51	87
fe								

25.2	27.0	28.1	31.0	31.6
12.4	8.6	7.5	4.6	4.0
238	200	187	146	100

22.4	24.6	24.8	26.8	28.8
13.2	11.0	10.8	8.8	6.8
266	294	300	340	373

16.9	21.5	24.1	28.4
18.7	14.1	9.5	7.2
500	441	434	400

Sta

+

π

-

Elev

935.55

7+25

✓

✓

✓

7+50

✓

✓

Dec 7, 1960

LT

Q

RT

19

21.3	25.0	25.6	28.0	28.1	29.3	29.9	28.1	26.5	25.1
14.3	10.6	10.0	7.6	7.5	6.3	6.7	7.5	9.1	10.5
Fe 17			18	50	57	86	100	125	142

25.6	26.7	22.9	18.7	20.2	22.5
10.0	9.9	12.7	15.9	15.4	13.1
300	295	288	245	200	171

25.1	25.5	26.4	25.5	23.1
10.5	10.1	9.2	10.1	13.5
329	358	381	400	424

15.6	18.6
20.0	17.0
497	452

21.1	22.8	25.1	25.3	29.0	27.2	26.4	24.5	21.4	17.3	17.1
14.5	12.8	10.5	10.3	6.6	8.4	9.2	11.1	14.2	18.3	18.5
34	25	15		23	45	73	100	126	166	200

22.1	22.9	23.7	25.6	21.8	19.2
13.5	12.7	11.9	10.0	13.8	16.4
386	361	335	300	267	238

21.3	17.8	14.2	10.7
14.3	17.8	21.4	24.9
400	429	467	500

Sta

+

 π

-

Elev

935.55

2+75

✓

✓

TBM

11.06

924.49

TBM

13.05

917.72

904.67

4+50

MH

9.89

5+00

5+25

Sta

+

Δ

-

Elev

912.72

5+50

5+75

6+00

✓

6+25

6+50

Sta

+

π

-

ELV.

917.72

6+75

✓

7+00

7+25

✓

7+50

At

12.4.	07.5.	04.5.	03.4.	01.7.	00.9.	98.9.	98.4.	97.6.	97.7.
5.3	10.2	13.2	14.9	16.0	16.8	18.8	19.3	20.1	20.0
525	557	582	584	600	613	630	649	656	661

Ditch

00.6.

00.1.

17.1 17.6 ✓

677 671

Lex

11.1.	06.6.	04.9.	03.4.	00.8.	00.0.	98.1.	96.4.	96.5.	99.1.	99.6.
6.6	11.1	12.8	14.3	16.9	17.7	19.6	21.3	21.2	18.6	18.1
524	548	560	564	590	600	624	645	651	661	668

Ditch

Lex

12.9.	10.0.	06.4.	04.6.	02.5.	00.0.	97.9.	96.7.	95.7.	95.7.
4.8	7.7	11.3	13.1	15.2	17.7	19.8	21.0	22.0	22.0
500	525	542	544	558	581	600	619	636	642

Ditch

98.6

98.0

19.1 19.7 ✓

658 651

Lex

07.7.	06.8.	04.6.	01.0.	96.8.	95.7.	94.8.	94.8.	97.2.	97.7.
8.0	10.9	13.1	16.7	20.9	22.0	22.9	22.9	20.5	20.0
500	523	526	557	586	600	626	634	642	649

Ditch

Lex

Sta

+

π

-

Elev

917.72

7+75

8+00

8+45

TBM

13.05

904.67

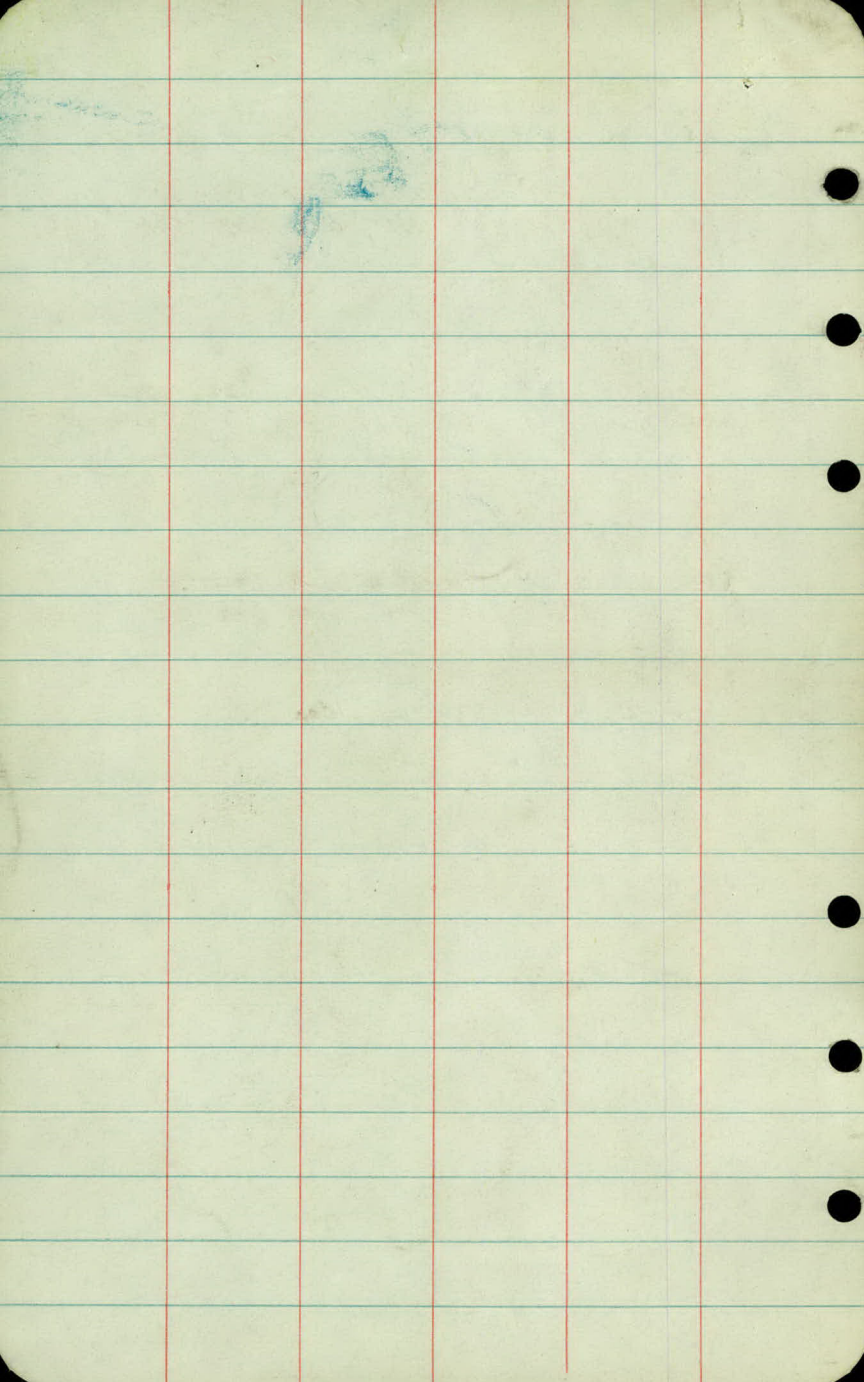
Dec 17, 1960

RL

23

96.2	94.9	91.9	98.3	95.0	94.7	94.7	97.0	97.6	
11.5	12.8	15.8	19.4	22.7	23.0	23.0	20.7	20.1	
517	518	541	569	600	620	631	640	646	
					Ditch			Lex	
94.7	94.2	93.2	91.2	96.0	94.2	94.2	96.8	97.3	
13.0	13.5	14.5	16.5	21.7	23.5	23.5	20.9	20.4	
504	505	514	538	577	600	625	636	642	Lex
98.0	96.4	92.4	92.3	92.3	95.0	95.6			
18.9	21.3	25.3	25.4	25.4	22.7	22.1			
511	533	571	600	606	616	622			

South rim MH on service Road



JAN 11, 1961

STRIPPING FINALS

Lexington Ave.

Borrow Pit

8+00 To 5+00

50' RT. TO 200' RT.

Plotted
1/19/61

R76

CREW

RG

JL

WM

LB

Sta	+	-	Elev
BM	9.19	913.86	904.67
TP	13.66	924.00	3.52 910.34
8+00			
7+75			
7+50			
TP	11.87	933.68	2.19 921.81
7+25			
7+00			
6+75			

Jan 11, 1961

200' RT

So. rim MH on service Rd.

rock

18.4	14.8	10.7	9.6	9.4	11.5	12.9
5.6	9.2	13.3	14.4	14.8	12.5	10.1
88	89	106	127	147	153	200
NG					NG	

22.9	18.6	15.0	11.5	10.9	14.9	16.3
4.1	5.5	9.0	12.5	13.1	9.6	7.7
66	80	87	118	141	145	200
NG					NG	

26.6	17.3	16.4	14.7	19.7	17.0
+ 2.6	6.7	7.6	9.3	4.3	7.0
64	76	109	137	143	200
NG				NG	

rock

30.1	19.3	18.5	16.4	25.2	20.9
3.6	14.4	15.2	12.3	9.5	12.8
65	76	100	131	138	200
NG				NG	

30.0	22.4	21.0	19.1	29.6	23.9
3.7	11.3	12.7	14.6	4.1	9.8
67	70	100	124	133	200
NG				NG	

30.8	24.3	22.1	20.7	27.4	30.1	26.3
2.9	9.4	11.6	13.0	6.3	3.6	7.4
68	73	100	122	125	129	200
NG					NG	

Sta	+	π	-	Elev
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		933.68		
--	--	--------	--	--

6+50				
------	--	--	--	--

T.P.	10.67	933.63	10.72	922.96
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6+25				
------	--	--	--	--

6+00				
------	--	--	--	--

5+75				
------	--	--	--	--

5+50				
------	--	--	--	--

5+25				
------	--	--	--	--

RG
JL
WM
LB

2

Jan 11, 1961
Jan 12, 1961
200' RT

31.3	25.6	24.6	22.3	31.1	27.6
2.3	8.1	9.1	11.4	2.6	6.1
69	75	100	116	130	200
NG				NG	

Top wooden Fe. post by 2nd Telephone Pole So of Pink Ho.

31.6	25.4	23.9	22.8	30.4	27.4
2.0	8.2	9.7	10.8	3.2	6.2
70	74	100	119	127	200
NG				NG	

33.0	29.8	25.9	24.4	22.4	29.9	26.2
0.6	3.8	7.7	9.2	11.2	3.7	7.4
64	69	75	100	120	126	200
NG					NG	

32.8	26.2	24.1	23.5	29.1	27.4
0.8	7.4	9.5	10.1	4.5	9.2
59	70	100	113	123	200
NG				NG	

31.3	25.4	24.1	23.7	29.7	27.9
2.3	8.2	9.5	9.9	3.9	11.8
58	67	100	115	120	200
NG				NG	

29.7	27.4	26.6	25.5	25.3	30.8	20.4
3.9	6.2	7.0	8.1	8.3	2.8	13.2
59	62	78	100	111	118	200
NG					NG	

Sta + π - Elev

933.63

5+00

TP 2.50 927.65 8.48 925.15

BM 5.10 922.55 922.60

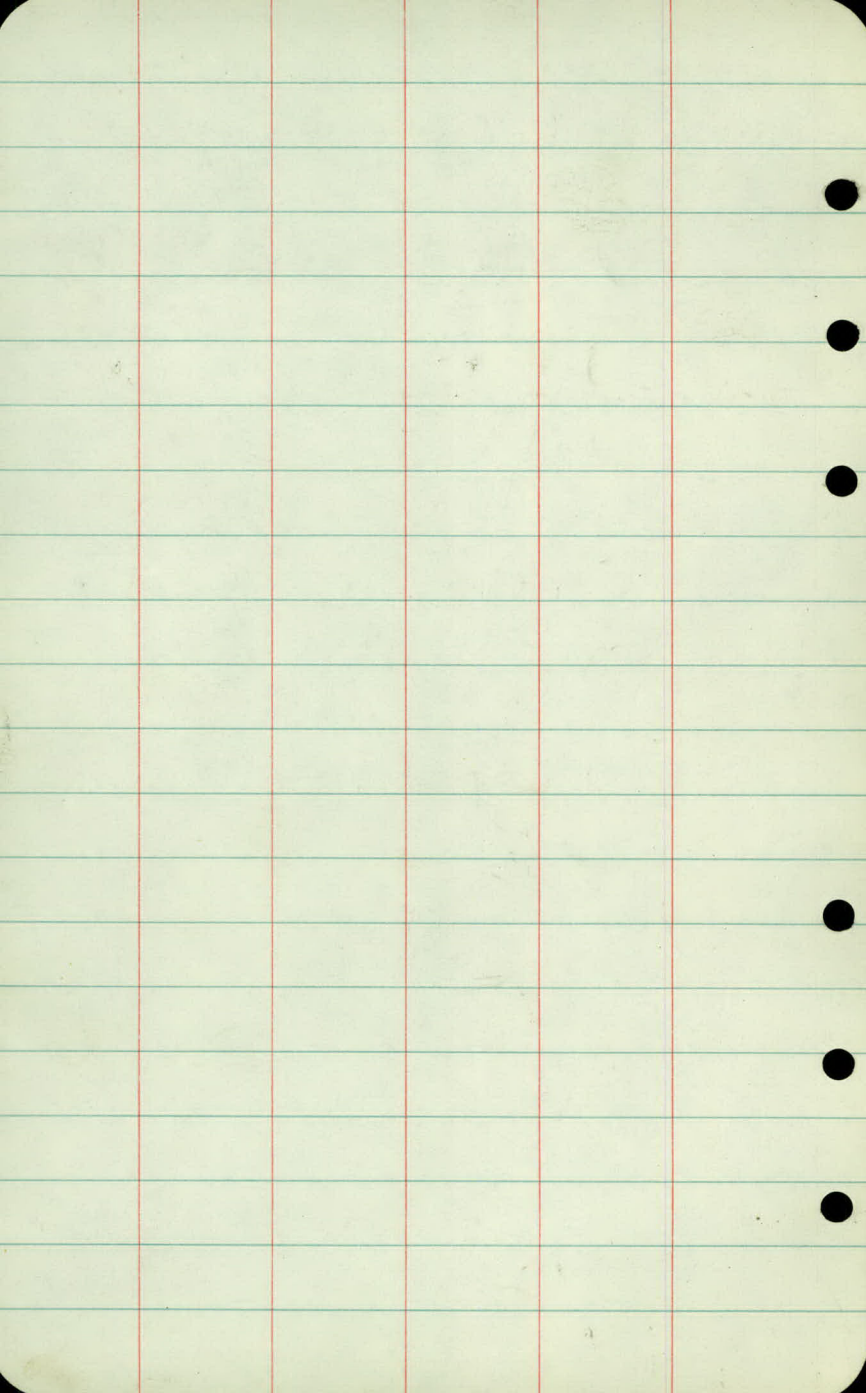
Jan 12, 1961

2

26.9 26.1 25.7 26.1 25.4 19.2
 6.5 7.5 7.9 7.5 8.2 14.4
 54 81 100 108 125 200
 NG NG

rock

Spika in Transformer pole (5th pole from Pink Ho.)



RG
JS
FS
WM

Jan 20, 1961
8° Cold, Cloudy

1

Lexington Ave Borrow Pit

stripping X-Sections

6+25 to 7+50 200' Rt to 118' Rt

Plotted 1/20/61

R76

Sta	+	π	-	Elev
BM	8.85	931.45		922.60

6+25

6+50

6+75

7+00

7+25

7+50

BM

8.85 922.60

Jan 20, 1960

F

200' RT

2

Spike in 5th P.Pole

		30.1	28.6	28.5	27.1
	1.4	1.9	3.0	4.4	
✓	128	156	176	200	
	NG	NG	NG	NG	
✓	21.2	18.9	19.4	20.4	21.6
	10.3	12.6	13.1	11.1	3.9
	118	141	160	188	200
					NG
	19.0	20.6	18.7	18.4	26.9
✓	12.5	10.9	12.8	13.1	4.6
	122	140	173	189	200
					NG
✓	19.5	19.3	17.5	17.3	24.4
	12.0	12.2	14.0	14.2	7.1
	125	151	181	193	200
					NG
✓	16.2	16.2	16.3	15.3	20.3
	17.3	15.3	15.2	16.2	11.2
	138	161	173	193	200
					NG
✓	15.1	16.8	16.6	17.2	
	16.4	14.7	14.9	14.3	
	138	157	180	200	
					NG

Spike in 5th P.Pole

Sta	+	π	-	Elev
BM	7.23	929.83		922.60

5+75

6+00

6-00

6+25

7.23 922.60

BM	7.31	929.91		922.60
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5+75

5+50

RG
JS
FS
WM

Feb 3, 1961 3
Clear, Fair 200' RT

Spike in 5th PP

✓ 23.5	26.8	24.5	20.8	21.6	25.0	23.3
6.3	3.0	5.3	9.0	8.2	4.8	6.5
115	118	140	155	171	180	200

✓ 16.9	19.0	19.1	17.4	18.1	25.4	25.1
12.9	10.8	10.7	12.4	11.7	4.4	4.7
112	125	145	163	181	189	200

✓ 18.7	18.7	18.6	18.9	26.7	26.8
11.1	11.1	11.2	10.9	3.1	3.0
117	145	168	186	193	200

RG; JS; JL; WM; FS

Feb 8, 1961
90° Clear

Spike in 5th PP

✓ 11.4	19.4	19.2	18.3	18.6	23.8	24.2	23.2
18.5	10.5	10.7	11.6	11.3	6.1	5.7	6.7
108	113	143	161	178	179	182	200

✓ 10.8	19.8	19.6	18.6	18.5	22.5	22.7
19.1	10.1	10.3	11.3	11.4	7.4	7.2
100	109	131	153	177	180	200

Sta

+

x

-

ELV

929.91

5+25

5+50

5+75

Final x-sections Granular
Material Removed

7+50

7+75

7+25

✓

7+00

Feb 8, 1961
200 Ac 4

12.3 19.1 19.4 19.0 18.5 21.4 22.8 23.1
17.6 10.8 10.5 10.9 11.4 2.5 7.1 6.8
98 104 130 153 176 178 184 200

24.3 24.3 21.3 21.3 19.9 19.0 19.0 21.2 19.5
5.6 5.6 8.6 8.6 10.0 10.9 10.9 8.7 10.4
70 79 85 100 127 150 166 178 200

0.82 0.82 0.84 0.86 10.8 17.1 16.7 16.4 17.7
21.7 21.7 21.5 21.3 19.1 12.8 13.2 13.5 12.2
76 100 120 140 150 157 163 175 200

02.9 00.8 03.2 08.2 09.9 14.6 15.7 21.0
24.0 29.1 26.1 21.7 20.0 15.3 14.2 8.9
157 169 178 179 184 180 195 200

0.1 0.16 0.87 0.93
20.8 20.3 21.2 22.6
151 124 100 77

10.6 10.3 11.3 03.9 09.0 09.23 02.4 11.8 17.6 24.4
19.3 19.6 18.6 26.0 38.9 37.6 27.5 18.1 12.3 5.5
79 100 136 140 160 168 184 189 192 200

Sta

+

π

-

Elev

929.91

6+75

✓

6+50

✓

6+25

T.P.

7.31

922.60

Feb 8, 1961

200 RE 5

11.0	00.4	888.5	886.7	04.7	08.9	18.9	26.8
18.9	29.5	41.4	33.2	25.2	21.0	11.0	3.1
121	132	145	172	183	188	192	200

11.0	11.4
18.9	8.5
100	83

00.1	886.6	889.2	895.9	00.9	20.7	27.9	27.6
29.8	43.3	40.7	34.0	29.0	9.2	2.0	2.3
128	150	160	169	179	187	194	200

12.3	11.6	11.3
17.6	18.3	18.6
113	100	85

893.2	886.9	896.0	03.7	18.7	19.6	26.8	26.9
36.7	43.0	34.9	26.2	11.2	10.3	3.1	3.0
140	158	172	181	183	190	195	200

11.6	11.0	11.3
18.4	18.9	18.6
117	100	85

Spike in 5th P.P.

Sta	+	π	-	Elev
BM	3.39	925.99		922.60

6+00

5+75

5+50

5+25

5+00

I.P.

3.40

922.59

922.60

Rt

Feb 14, 1961

6

200' At

Spike in 5th PP

11.4	11.2	11.2	898.0	897.0	897.0	0.16	2.0
14.6	14.8	14.8	28.0	39.0	39.0	24.4	+1.0
85	100	113	142	150	155	175	200

11.4	11.2	11.1	897.6	896.5	896.1	24.4	2.3
14.6	14.8	14.9	38.4	39.5	19.9	1.6	17
87	100	108	146	156	178	187	200

13.0	11.9	0.3	899.0	898.3	0.8	22.8	2.8
13.0	14.1	22.7	37.0	37.7	24.2	3.2	3.2
79	110	120	142	156	185	189	200

11.5	11.2	12.4	06.4	03.2	5.7	22.9	2.0
14.5	13.8	13.6	19.6	22.8	20.3	3.1	3.0
80	100	113	127	154	182	187	200

11.8	11.3	17.0	16.5	18.1	22.4	22.3
9.2	8.7	9.0	9.5	7.9	3.6	3.7
77	100	125	150	176	183	200

Spike in 5th PP

Gravel-Sand Excavation

Sta	+	π	-	Elev
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BM	8.10	912.77		904.67
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8+00

7+75

7+50

7+25

✓

7+00

9.12.77

Feb 16, 1961

Windy 30°

24

£

So. rim MH on Service Rd

09.8	09.5	09.8
3.0	3.3	3.0
150	125	100

09.5	09.3	06.2	894.3	893.7	99.0
3.3	3.5	6.6	18.5	19.1	13.8
150	138	124	113	104	97

08.7	09.0	894.4	86.2	95.6	900.5	11.5
4.1	3.8	18.4	26.6	17.2	12.3	1.3
150	135	124	113	100	85	70

08.7	08.5	900.7	90.4	91.8	99.0	03.3
4.6	4.3	12.1	22.4	21.2	13.8	9.5
150	135	130	108	103	90	95

10.3
2.5
70

07.5	08.3	01.1	889.0	93.3	899.9	08.9
5.3	4.5	11.7	23.8	19.5	12.9	2.9
150	134	128	110	100	91	69

STA	+	Δ	-	ELEV.
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		912.77		
--	--	--------	--	--

TP1	804	918.90	2.91	909.86
-----	-----	--------	------	--------

5+25

+50

+75

6+00

+25

+50

16 Feb 1961

RT

8

$\begin{array}{r} 08.4 \\ 9.5 \\ 165 \end{array} \begin{array}{r} 11.1 \\ 7.8 \\ 125 \end{array} \begin{array}{r} 10.9 \\ 8.0 \\ 200 \end{array} \begin{array}{r} 209 \\ NG \end{array}$

$\begin{array}{r} 08.8 \\ 10.1 \\ 173 \end{array} \begin{array}{r} 10.6 \\ 8.3 \\ 184 \end{array} \begin{array}{r} 11.1 \\ 7.8 \\ 200 \end{array} \begin{array}{r} 11.7 \\ 7.2 \\ 211 \end{array} \begin{array}{r} 214 \\ NG \end{array}$

$\begin{array}{r} 07.3 \\ 11.6 \\ 176 \end{array} \begin{array}{r} 11.6 \\ 7.3 \\ 183 \end{array} \begin{array}{r} 13.5 \\ 6.4 \\ 200 \end{array} \begin{array}{r} 13.1 \\ 5.8 \\ 215 \end{array} \begin{array}{r} 10.6 \\ 217 \\ NG \end{array}$

$\begin{array}{r} 05.0 \\ 13.9 \\ 180 \end{array} \begin{array}{r} 11.8 \\ 7.1 \\ 186 \end{array} \begin{array}{r} 13.7 \\ 5.2 \\ 200 \end{array} \begin{array}{r} 14.3 \\ 4.6 \\ 218 \end{array} \begin{array}{r} 18.5 \\ 222 \\ NG \end{array}$

$\begin{array}{r} 06.0 \\ 12.9 \\ 184 \end{array} \begin{array}{r} 13.9 \\ 5.0 \\ 189 \end{array} \begin{array}{r} 16.8 \\ 2.1 \\ 222 \end{array} \begin{array}{r} 19.2 \\ 224 \\ NG \end{array}$

$\begin{array}{r} 06.7 \\ 12.2 \\ 186 \end{array} \begin{array}{r} 14.1 \\ 4.8 \\ 189 \end{array} \begin{array}{r} 15.3 \\ 3.6 \\ 224 \end{array} \begin{array}{r} 18.0 \\ 226 \\ NG \end{array}$

Sta	+	Δ	-	ELEV
-----	---	---	---	------

		918.90		
--	--	--------	--	--

6+75				
------	--	--	--	--

7+00				
------	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

8+00				
------	--	--	--	--

BM				
----	--	--	--	--

		1.94		
--	--	------	--	--

		916.96		
--	--	--------	--	--

		916.95		
--	--	--------	--	--

16 Feb. 1961

9

Rt

08.3	14.3	15.0	15.5	
10.6	4.6	3.9	3.4	+8
188	193	200	230	232 NG

08.1	13.5	13.5	14.4	14.4	
10.8	5.4	5.4	4.5	4.5	+75
190	194	200	216	233	235 NG

08.0	13.6	14.6	15.2	
10.9	5.3	4.3	3.7	+4.3
194	197	215	234	238 NG

10.5	12.9	11.5	11.1	
8.4	6.0	7.4	7.8	+82
195	200	223	235	240 NG

09.7	11.3	11.2	11.1	
9.2	7.6	7.7	7.8	+8.0
174	186	200	235	245 NG

09.8	10.7	13.2	14.3	
9.1	8.2	5.7	4.6	+2.5
170	188	210	241	244 NG

Spike in first PP (pink Ho)

Sta	+	π	-	ELV.
	9.69	914.36	914.36	904.67
6+75				
6+50				
6+25				
6+00				
BM		9.69	904.67	904.67

Feb 17, 1961

10

FINALS

PL

MH ON SERVICE Rd

	897.9	897.7	90.6	89.6	07.3	06.4
13.8	23.7	23.8	13.8	7.1	8.0	
85	98	103	120	125	150	

	897.9	91.8	91.8	00.6	06.7	05.8
16.5	22.6	22.6	13.8	9.3	8.6	
85	100	105	119	125	150	

	897.4	89.3	89.4	96.4	23.0	5.0
17.0	25.1	25.0	18.0	11.4	9.4	
85	100	105	119	123	150	

	897.4	89.6	89.2	00.1	04.1	04.9
17.0	24.8	25.2	14.3	10.3	9.5	
85	99	105	118	125	150	

MH ON Service Rd

Sta	+	π	-	Elev
-----	---	-------	---	------

BM	6.15	910.82		904.67
----	------	--------	--	--------

5+75

5+50

T. P.	8.79	915.45	4.16	906.66
-------	------	--------	------	--------

5+25

	6.31	920.30	1.46	913.99
--	------	--------	------	--------

STYIPIDIZY

6+75

7+00

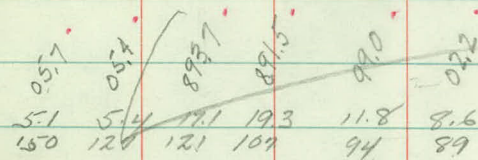
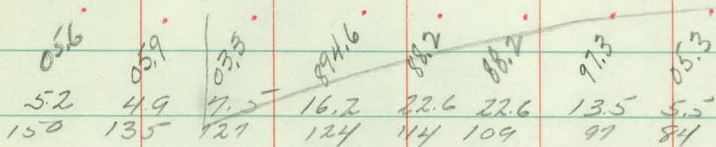
R6
J5
J5
J5
WH

E

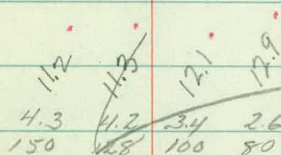
Rt

Feb 21, 1961 11
30° Clear

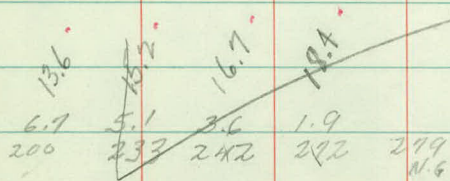
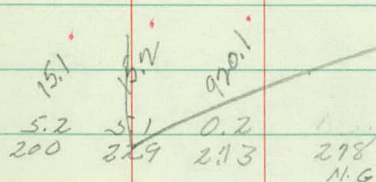
MH on Service Road



Frozen dirt 5+35 - 135' Rt



Frozen dirt 6+06 - 200' Rt



Sta + π - ELEV

920.30

7+25

+50

+75

B.M.

3.32 916.98

916.95

Feb 21, 1961

12

E

 RG
 JS
 W/M
 JK
 FS

14.0	14.7	15.8	18.5	
6.3	5.6	4.5	1.8	
200	230	233	272	279 NG

12.3	13.6	18.6	
8.0	6.7	1.7	
200	232	278	285 NG

11.4	12.7	18.6	
8.9	7.6	1.7	
200	227	248	285 NG

Spike in First P.P. Pink House

Sta	+	π	-	Elev
BM	7.95	912.62		904.67

6+50

✓

6+75.

7+00

+25

+50

KP
RG
JS
WM
FS

Feb 27, 1961

Rt.

Rim MH on Service Road

07.2	06.9	899.6	893.6	888.8	890.0
5.4	5.7	13.9	19.0	23.8	22.6
175	179	180	191	200	208

15.4	894.0
+2.8	18.6
224	214

88.1	07.9	898.2	889.8	888.0	890.0	896.8
4.5	4.7	14.4	23.2	28.6	22.6	15.8
175	180	185	200	205	215	227

88.2	08.2	02.7	892.2	884.6	889.4	894.6	16.7
4.4	4.4	9.9	20.4	28.0	23.2	18.0	14.1
175	183	185	200	215	224	236	244

88.1	08.2	06.5	03.6	899.1	890.6	890.1	896.4	899.7
4.5	4.4	6.1	9.0	13.5	22.0	22.5	16.2	12.9
175	182	190	196	198	214	221	231	233

88.7	09.6	898.6	897.4	900.5	88.7	15.7
3.9	3.0	14.0	15.2	12.1	3.9	18.3
175	196	216	226	253	264	278

116

STA

+

π

-

ELEV.

912.62

7+75

8+00

✓

BM

7.96

904.66

904.67

27 FEB 1961

21

RT

✓

09.4		10.5	05.6	05.2	04.9	08.3	19.2
3.2	2.1	7.0	7.4	7.7	4.3	+10.6	
175	199	217	228	253	268	280	

✓

09.3	09.9	13.8	14.9	12.6	13.4
3.3	2.7	+1.2	+2.3	0.0	+0.8
175	186	200	204	209	227
		NG			

	17.0	15.1	14.6
	+4.4	+2.5	+2.0
287	279	269	248
NG			

TOP MH ON SERVICE ROAD

STA	+	π	-	ELEV.
	8.09	912.76		904.67

5+50

5+75

6+00

6+25

✓

BM

8.09

904.67

904.67

KP
US
UL
FS

2 MARCH 1961

±

RT

TOP MH ON SERVICE LANE

06.2	09.5	11.0	11.1	
6.6	9.3	11.8	11.1	+8.0
150	175	200	209	211

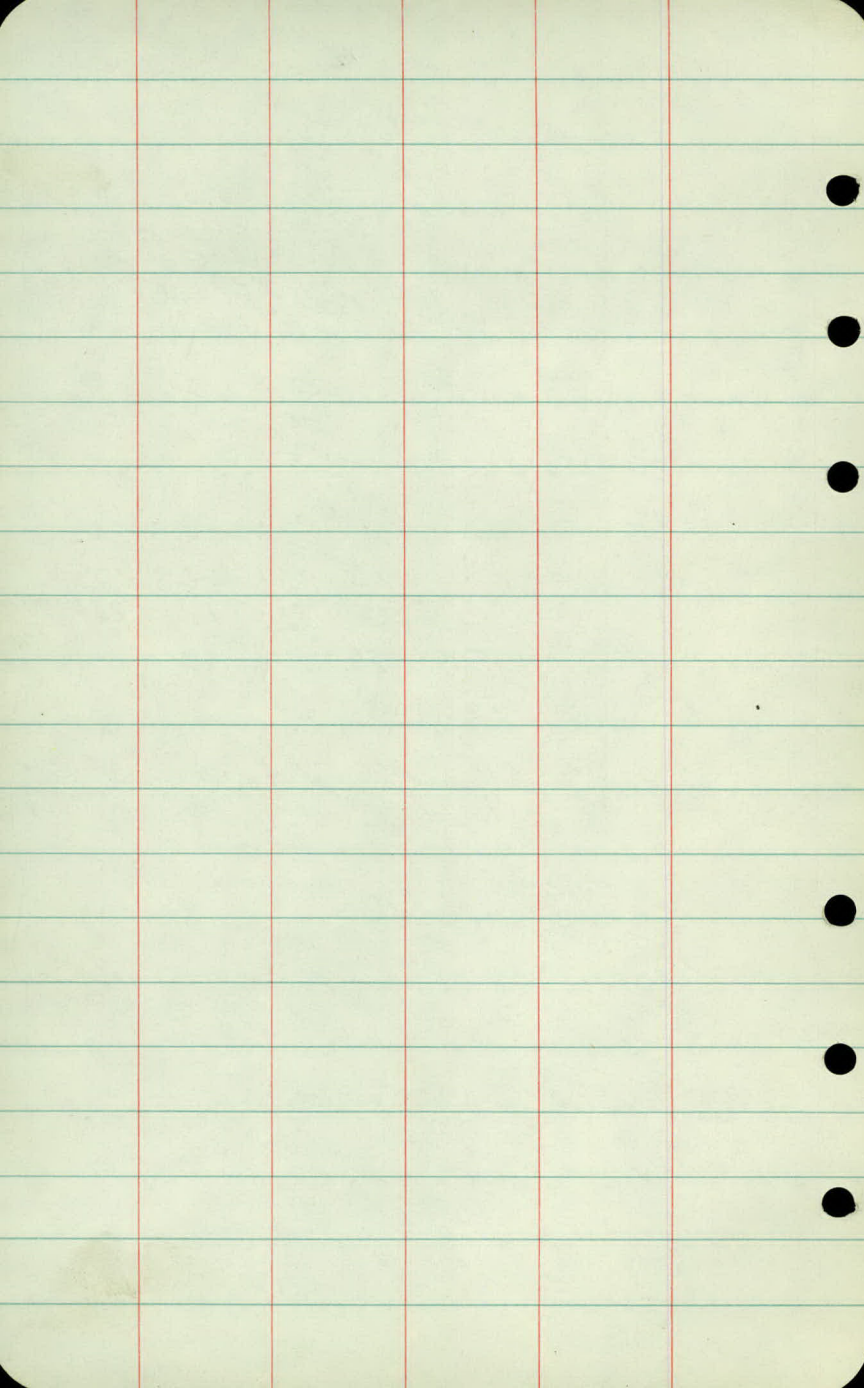
05.3	06.1	08.9	09.9	09.9	09.5
7.5	6.7	13.9	20.0	19.9	15.3
150	165	179	191	197	205

05.4	06.0	05.5	06.1	08.0	05.8
7.4	6.8	17.3	26.1	24.8	17.0
150	164	173	188	199	207

05.8	06.1	08.5	09.4	07.2	09.2
7.0	6.7	14.3	20.4	25.6	13.6
150	171	178	187	195	211

225
STR

TOP MH ON SERVICE LANE.



JS
SL
WM
FS

8 MARCH 1961

STRIPPING

Lexington Borrow Pit

5+25 to 7+75

Sta	+	$\times$	-	ELV
	4.64	927.24		922.60

5+25

5+50

5+75

6+00

6+25

6+50

2

26

2

Spike in 5th

	22.2	23.3	24.1	23.1	23.1	23.0
NG	3.0	3.9	3.1	4.1	4.1	4.2
10	17	29	36	56	72	



	22.6	22.8	23.3	22.5
--	------	------	------	------

NG	NG	4.6	4.4	3.9	4.7
	23	29	48	64	71



	22.1	22.1	21.0	20.7
--	------	------	------	------

NG	NG	4.5	5.1	6.2	6.5
	15	23	44	62	75



	21.3	21.0	20.3
--	------	------	------

NG	NG	5.9	6.2	6.9
	21	27	53	77



	23.2	20.7	19.7	19.5
--	------	------	------	------

NG	NG	4.0	6.5	7.5	7.7
	19	27	32	56	73



	22.5	20.0	19.8	19.6	16.8
--	------	------	------	------	------

NG	NG	4.7	7.2	7.4	9.6	10.4
	13	23	32	51	71	85



Sta

+

X

-

ELL

927.24

6+75

7+00

7+25

7+50

7+75

4.63

922.61

6+00

2

✓ NG. NG 3.8 7.6 10.7 8.9 8.6 8.8 13.6
16 25 35 40 43 59 72 89

23.4 19.6 16.5 18.3 18.6 16.4 13.6

✓ NG. NG 7.9 8.4 8.7 10.5 14.7
17 24 45 58 71 76

19.3 18.8 16.5 16.1 12.5

✓ NG. NG 5.1 7.4 8.6 9.4 12.9 15.7
17 24 31 48 67 78 80

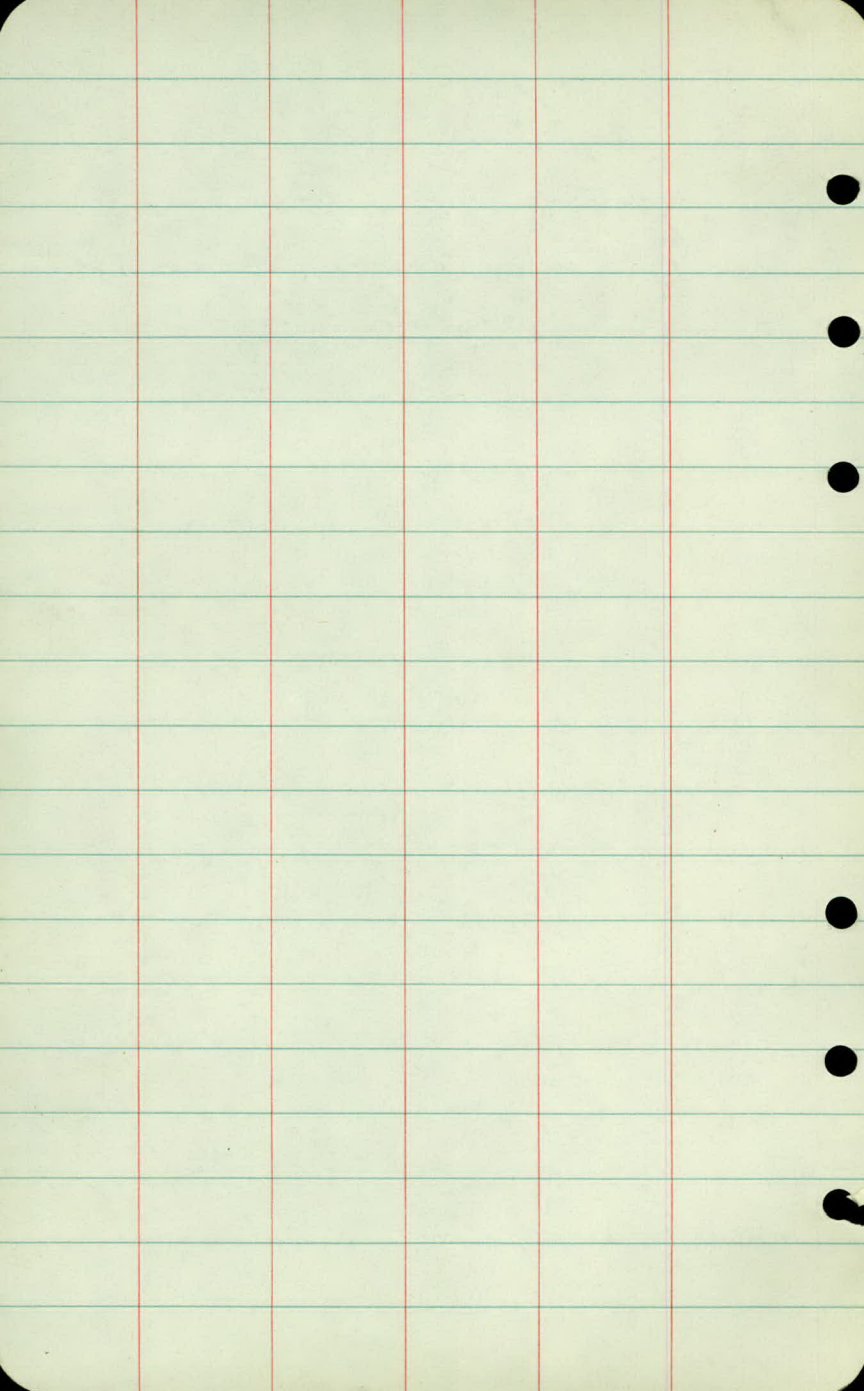
22.1 19.8 18.4 17.6 14.3 11.5

✓ NG. NG 4.8 6.7 9.2 15.6
17 24 29 64 84

22.4 20.5 18.0 11.6

✓ NG. NG 5.9 8.9 9.5 14.7
26 31 47 64 86

21.3 18.3 17.1 12.5



6 MAY 1961

LEXINGTON AVE
BORROW PIT

STA 6+75 - 8+00 6/8/61

" 7+00 - 6+25 6/9/61

STA	+	π	-	ELEV
BM	4.16	921.11		916.95

6+75

7

+25

+50

+75

8

TP	4.24	912.29	13.06	908.05
----	------	--------	-------	--------

6 MAY 1961

F

RT

SPIKE IN PP (PINK HOUSE)

19.8	20.0	19.7	18.3	14.9	09.9	07.8
1.3	1.1	1.4	2.8	6.2	11.2	13.3
30	44	60	70	75	88	125

09.2	10.9	10.1	07.7
11.9	10.2	11.0	13.4
70	75	98	125

10.8	08.4
10.3	12.7
82	125

10.4	08.7
10.7	12.4
83	125

19.8	12.8	15.7	10.1	09.7
NG 1.3	8.3	5.4	11.0	11.4
25 32	67	73	90	125

STA	+	π	-	ELEV
-----	---	-------	---	------

STA	+	π	-	ELEV
		912.29		

STA	+	π	-	ELEV
7+00				

STA	+	π	-	ELEV
+25				

STA	+	π	-	ELEV
+50				

STA	+	π	-	ELEV
+75				

907.8 ✓

4.49

907.80

907.80

JUNE 1961

✓

RT

10.0	06.9	05.1
2.3	5.4	7.2
35	45	64

✓

12.3	898.3	97.9
0.0	14.0	14.4
35	50	52

✓

	12.3	98.3	98.4
16	0.0	14.0	13.9
15	20	50	71

Ground at Sta 6+75 125' RT

STA	+	π	-	ELEV
BM	6.89	911.56		904.67

7+25

7+00

6+75

TP	4.81	909.56	6.81	904.75
----	------	--------	------	--------

7+25

7+00

6+75

			4.81	904.75	904.75
--	--	--	------	--------	--------

KP
FS
RB
ERDOR.

£

8 MAY 1961

R+

MH ON SERVICE DRIVE

✓ 10.6

✓ 1.0
80

09.2

✓ 2.4
✓ 100

✓ 10.2

✓ 1.4
82

09.3

✓ 2.3
100

✓ 11.0

✓ 0.6
80

09.2

✓ 2.4
100

TOP LATH

7

NG
25

✓ 899.1

12.5
63

896.7

✓ 116
17

12.9
45

895.4

14.2
54

7

NG
38

902.6

7.0
45

TOP LATH

STA	+	π	-	ELEV
BM	9.52	914.19		904.67

7+00

6+75

6+50

TP	2.25	907.05	9.39	904.80
----	------	--------	------	--------

7+00

6+75

6+50

2.25	904.80	904.80
------	--------	--------

KP
FS
RB

£

9 JUNE 1961

Rt

TOP MIT ON SERVICE DRIVE

✓	10.2 4.0 83	09.5 4.7 100
---	-------------------	--------------------

✓	09.8 4.4 80	09.7 4.5 100
---	-------------------	--------------------

?	✓	09.6 4.6 80	09.2 5.0 100
NG 38			

TOP LATH

✓	03.8 3.3 34	09.2 10.9 47	09.7 10.4 59
---	-------------------	--------------------	--------------------

✓	02.1 10.0 47	06.7 10.4 59
---	--------------------	--------------------

✓	04.9 2.2 50	02.2 4.9 65
---	-------------------	-------------------

LATH

STA	+	π	-	ELEV.
BM	9.37		914.04	904.67

6+75

6+50

6+25

TP	1.55	906.35	9.24	904.80
----	------	--------	------	--------

6+75

6+50

6+25

			1.55	904.80	904.80
--	--	--	------	--------	--------

15 JUNE 1961

E

RT

TOP MA ON SERVICE DRIVE

NG
10

09.4

4.6
79

09.7

4.3
100NG
18.13

10.1

3.9
82

09.2

4.8
100NG
22

10.9

3.1
82

09.2

4.8
100

TOP LATH

04.2

2.2
42

09.8

8.6
53

09.7

8.7
59

09.0

7.4
34

06.9

9.5
48

08.3

8.1
62

05.8

0.6
24

05.8

0.6
40

03.4

3.0
63

LATH

STA	+	π	-	ELEV.
BM	9.60	914.27		904.67

6+50

6+25

6+00

5+75

TP	1.01	905.82	9.46	904.81	904.80
----	------	--------	------	--------	--------

6+50

6+25

KP
FS
RS
00

E

RT

16 JUNE 1961

TOP MH ON SERVICE DRIVE

N6
8

10.4
3.9
85
09.4
4.9
100

N6
12

11.3
3.0
85
09.4
4.9
100

N6
19

10.8
3.5
77
09.2
5.1
100

N6
41

13.1
1.2
79
09.5
4.8
100

TOP STAKE

899.4
8.4
49

899.2
6.6
36

899.6
8.2
59

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		905.82		
--	--	--------	--	--

6+00				
------	--	--	--	--

BM				
----	--	--	--	--

		101		
--	--	-----	--	--

			904.81	
--	--	--	--------	--

				904.80
--	--	--	--	--------

16 JUNE 1961

RT

~~903.3~~

0.1

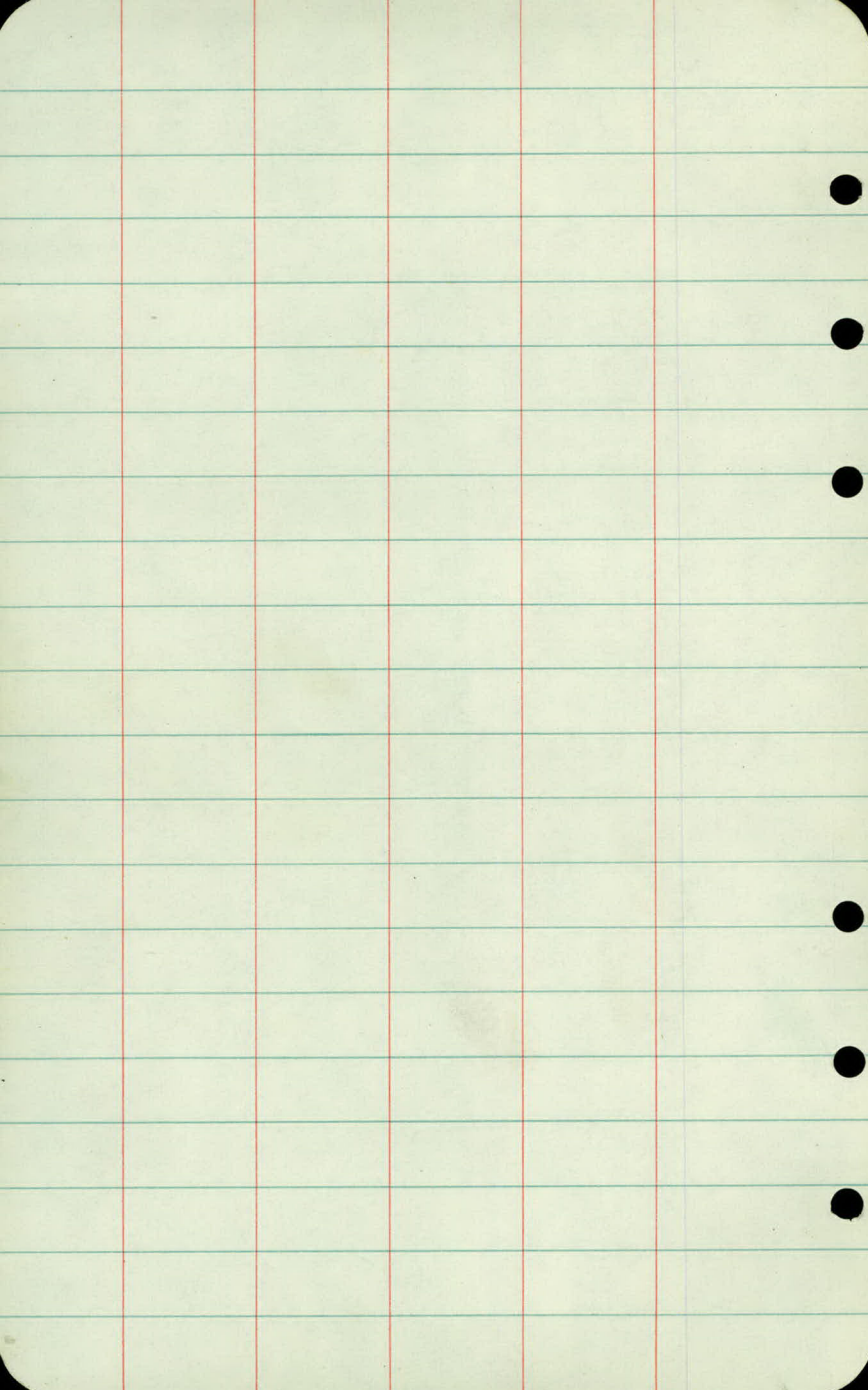
2.5

4.7

38

58

TOP STAKE



29 JUNE 1961

KP
FS
RB
JD

Lexington Ave
Borrow Pit

STA	+	π	-	ELEV.
BM	9.46	914.13		904.67
TP	4.90	912.83	6.20	907.93

6+25

6+00

5+75

5+50

5+25 = N/G

TP	3.89	904.77	11.95	900.88
----	------	--------	-------	--------

29 JUNE 1961

£

R+

TOP MH ON SERVICE DRIVE

TOP ROCK

NG
11

10.0

09.3

✓ 2.8 3.5
86 100

NG
20

09.5

09.5

✓ 3.3 3.3
88 100

NG
41

10.3

09.7

✓ 2.5 3.1
86 100

NG
61

12.8

11.9

✓ 0.0 0.9
83 100

ROCK

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		904.77		
--	--	--------	--	--

6+25				
------	--	--	--	--

6+00				
------	--	--	--	--

5+75				
------	--	--	--	--

5+50				
------	--	--	--	--

TP		3.89	900.88	
----	--	------	--------	--

29 JUNE 1961

~~E~~

~~R~~

898.2

95.1

6.6

9.7

42

59

94.5

93.9

10.3

10.9

54

70

904.8

03.5

0.0

1.3

54

70

ROCK

Sta	+	Δ	-	Elev.
-----	---	---	---	-------

B.M.	8.87	916.54		907.67
------	------	--------	--	--------

6+00

6+25

6+50

6+75

7+00

7+12

T.P.	2.23	906.23	12.54	904.00
------	------	--------	-------	--------

\$

Rt.

Top MH. on Service Drive

	12.5	12.3
✓	4.0	4.2
	88	100

	12.1	12.3
✓	4.4	4.2
	96	100

	11.7	12.2
✓	4.8	3.9
	93	100

	12.8	12.5
✓	3.7	4.0
	94	100

	12.7	12.7
✓	3.8	3.8
	93	100

	13.1	12.9	12.4
	3.4	3.6	4.1
	47	77	100

Rock

STA

+

Δ

-

ELV.

906.23

6+00

6+25

6+50

6+75

7+00

T.P.

2.21

904.02

904.00

E

June 30, 1961
Rt

NG.

900.1	889.7	86.2
6.1	16.5	0.0
43	60	83

NG.

01.4	893.4	890.2	01.4
4.8	128	16.0	4.8
42	53	66	84

NG.

98.7	89.0	02.7
7.5	17.2	3.5
52	66	85

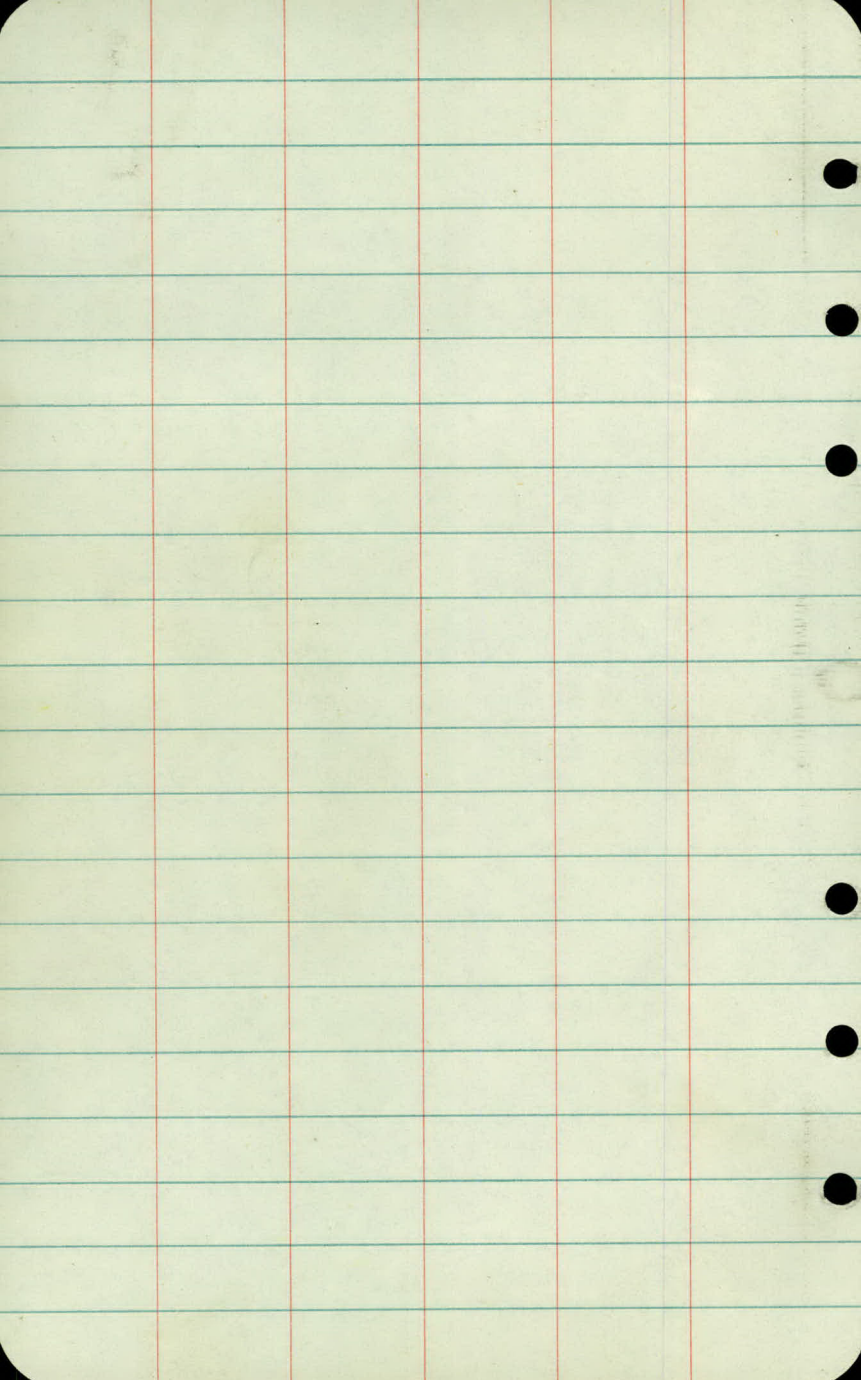
NG.

98.1	93.5	92.2	05.4
8.1	12.7	13.0	0.8
59	65	73	86

NG.

04.0	04.8	02.8	04.2
2.2	1.4	3.4	2.0
57	68	75	85

Rock



Josephine Park

West line old TH #10
84.67

• 16+00 ±

○ N Line Brenner Ave
72.46 • 15+50 ±

9
2
8
0

• 15+00 ±

Lake Josephine

