

Dr. 9 Bk. 17

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

LARPENTEUR AVE.

From Cleveland Ave. To Snelling Ave.

S.P. 62-630-01

Road Acc't. No. 30

Date Filed _____

Dr. 9
File Bk 17

LARPENTEUR

Cleveland to Snelling

59-30

Plan Survey

INDEX:

Alignment 2-5

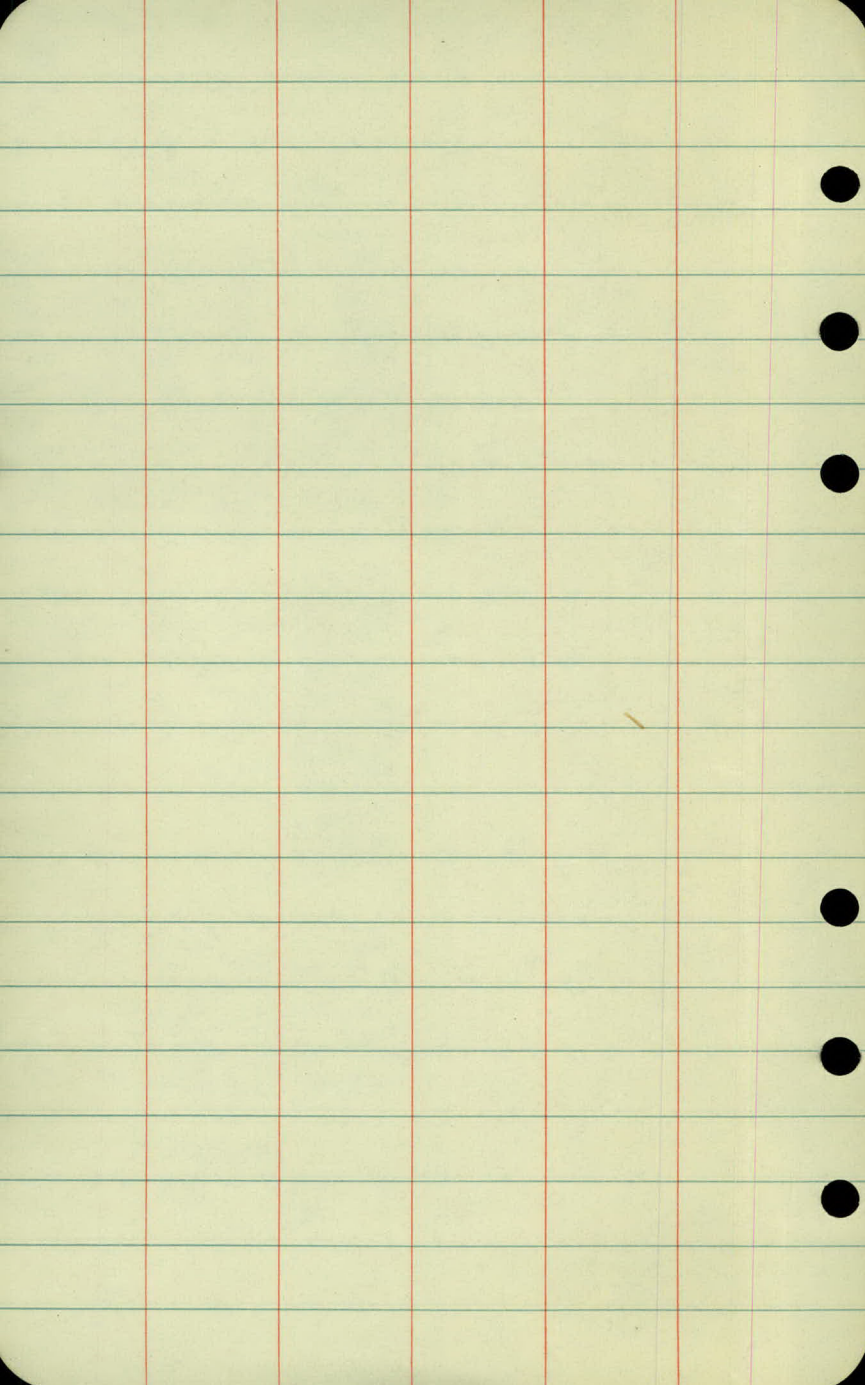
Topography 6-18

Bench Levels 19-20

X-Sections

Sta 96-104 21-34

50 - 34 -



FK
RG
KP
RR

Sept 23, 1958

2

Alignment

Sta Point $\Delta Lt.$ $\Delta Rt.$



52+81.83 P.I. $0^{\circ}09'$

Sept 23, 1958

3

Hand-drawn sketch map of a property corner. The map shows a corner of a lot with dimensions and bearings. A line runs from the top left towards the center, labeled '45.87' and '100''. Another line runs from the center towards the bottom left, labeled '68.32' and '73.2A'. A third line runs from the center towards the bottom right, labeled '146.78'. The corner is marked with a small square. The area is labeled 'TP O' and 'OPP'. The street 'Cleveland Ave' is labeled on the left, and 'R.R. No. 1' is labeled on the right. The word 'Mont.' is written at the bottom right.

Sta Point ΔL ΔR



79+07.91 P.I. $0^{\circ}07'$

FK
RG
KP
RR

Sept 24, 1958

4

Cor Fe Post x 55.37

E New Brighton Rd.

170.17
57.62
63.56

Iron

100.86
49.28
12" Ash
0 PP

Sta Point ΔL ΔR

105+33.71 P.I. $0^{\circ}17\frac{1}{2}'$

92+20.91 P.O.T.

FK
RG
RA

Sept 25, 1958

5

± Snelling Ave

Sign base □

71.00

46.46

68.94

o Hyd

69.55

o PP

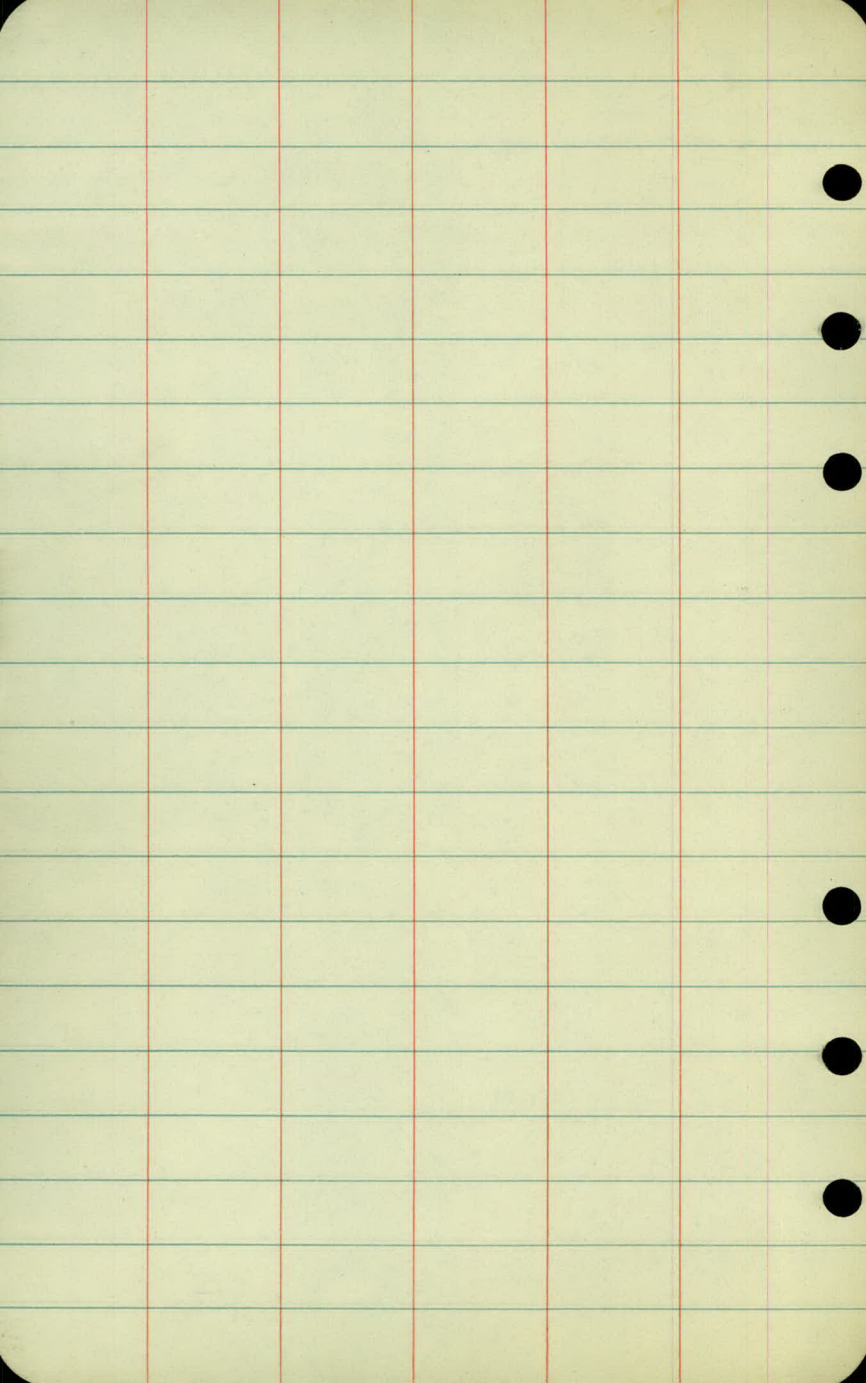
Mont

□ 35.55

x Fe Cor Mont

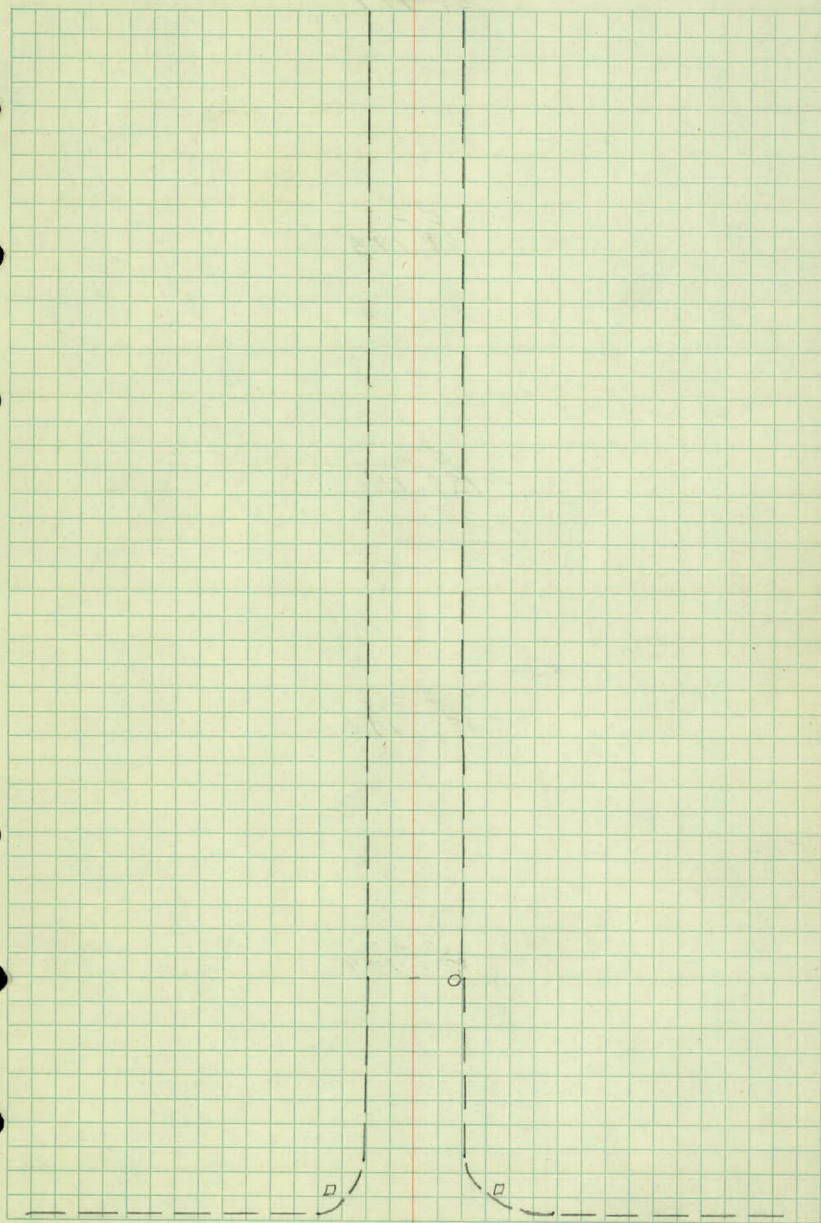
67.53

⊙ 10" E/m



Oct 8, 1958

8



63

$$\begin{array}{r} \text{BS} \\ 182 \quad 19.7 \end{array}$$

$$\begin{array}{r} \text{MH} \\ +35 \quad 29 \end{array}$$

62

$$\begin{array}{r} \text{BS} \\ 182 \quad 19.4 \end{array}$$

61

$$\begin{array}{r} \text{BS} \\ 186 \quad 18.7 \end{array}$$

60

+95 Ent

$$\begin{array}{r} \text{BS} \\ 188 \quad 19.0 \end{array}$$

59

$$\begin{array}{r} \text{BS} \\ 183 \quad 18.9 \end{array}$$

$$\begin{array}{r} \text{T-MH} \\ +58 \quad 17 \end{array}$$

58

$$\begin{array}{r} \text{BS} \\ 181 \quad 19.7 \end{array}$$

Oct 8, 1958

9

FL to Top = 10.30'

The diagram is drawn on a green grid. It features a vertical dashed line that runs from the top to the bottom of the page. To the left of this line, there are two horizontal dashed lines. The upper horizontal line is labeled 'FL to Top = 10.30' with a bracket underneath it. Below this, there is another horizontal dashed line. To the right of the vertical dashed line, there is a small circle near the bottom. The vertical dashed line has several small upward-pointing arrows along its length, particularly near the top.

68

$$+98 \frac{B^*P}{70}$$

$$\frac{B.S.}{19.7 \quad 19.7}$$

$$+77 \frac{T-MH}{17}$$

$$+60 \frac{E.Edge}{Ent}$$

67

$$19.1 \quad 19.3$$

$$+43 \frac{W.Edge}{Ent}$$

66

$$\frac{B.S.}{19.7 \quad 19.4}$$

$$+52 \frac{MH}{29.5}$$

65

$$\frac{B.S.}{19.7 \quad 19.9}$$

64

$$\frac{B.S.}{18.9 \quad 19.3}$$

63

$$+17 \frac{T-MH}{17}$$

$$\frac{B.S.}{18.2 \quad 19.7}$$

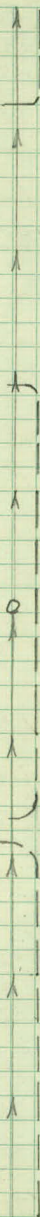
Oct 8, 1958

10

X

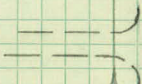
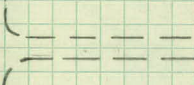
Parking

F.L. to Top = 10.60



o

o



73

$$\begin{array}{r} \cdot BS \\ 17.6 \quad 20.0 \end{array}$$

$$\begin{array}{r} \cdot B^{\circ}P \\ +64 \quad 52 \end{array}$$

$$+43 \cdot \text{Row P} \quad 55 \quad +54 \cdot B^{\circ}P \quad 53 \quad +59 \cdot 6^{\circ}P \quad 46$$

$$\begin{array}{r} \cdot T-MH \\ +36.5 \quad 17 \end{array}$$

$$+20 \cdot \text{End Hedge} \quad 50 \quad +36 \cdot \text{Row P} \quad 53 \quad +39 \cdot \text{Row P} \quad 52$$

72

$$\begin{array}{r} \cdot 6^{\circ}E/m \\ +13 \quad 52 \end{array}$$

$$\begin{array}{r} \cdot BS \\ 18.5 \quad N-18.8 \end{array}$$

$$\begin{array}{r} \cdot 7^{\circ}E \\ +80 \quad 52 \end{array}$$

$$\begin{array}{r} \cdot 7^{\circ}P \\ +26 \quad 53 \end{array}$$

$$+43 \cdot 8^{\circ}E \quad 52 \quad +21 \cdot 4^{\circ}Walk \quad 51$$

$$\begin{array}{r} \cdot B^{\circ}P \\ +16 \quad 53 \end{array}$$

71

$$\begin{array}{r} \cdot BS \\ 18.3 \quad +21 \quad 15^{\circ} \times 6^{\circ}CM \\ 29 \end{array}$$

$$\begin{array}{r} \cdot BS \\ 19.8 \end{array}$$

$$\begin{array}{r} \cdot 7^{\circ}E \\ +89 \quad 55 \end{array}$$

$$\begin{array}{r} \cdot BR \\ +79 \quad 37 \end{array} \quad +94 \cdot ER \quad 21.3$$

$$\begin{array}{r} \cdot MH \\ +63 \quad 27 \end{array}$$

$$\begin{array}{r} \cdot ER \\ +48 \quad 34 \end{array}$$

$$\begin{array}{r} \cdot BR \\ +38 \quad 19.6 \end{array}$$

$$\begin{array}{r} \cdot Arc Lt \\ +14 \quad 32 \end{array}$$

70

$$\begin{array}{r} \cdot B.S. \\ 17.0 \quad 19.7 \end{array}$$

$$\begin{array}{r} \cdot 3-6^{\circ}Pines \\ +98 \quad 66-89-101 \end{array}$$

$$\begin{array}{r} \cdot Ent \quad 12^{\circ} \times 35^{\circ}CM \\ +77 \quad 28 \end{array}$$

$$\begin{array}{r} \cdot 10^{\circ} Conc Ent \\ +77 \quad 53.5 \end{array}$$

$$\begin{array}{r} \cdot S.W. Cor Ho \\ +22 \quad 88 \end{array}$$

69

$$\begin{array}{r} \cdot BS \\ 17.8 \quad 18.8 \end{array}$$

$$\begin{array}{r} \cdot MH \\ +14 \quad 29 \end{array}$$

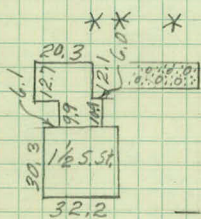
$$\begin{array}{r} \cdot BS \\ 19.7 \quad 19.7 \end{array}$$

68

Oct 8, 1958

11

N Fl to Top 12.20



FL to top = 11.30

78

$$\begin{array}{r} \text{BS} \\ 20.0 \quad 20.2 \end{array}$$

27

$$\begin{array}{r} \text{BS} \\ 19.6 \quad 19.4 \\ + 196.5 \quad 17 \end{array}$$

$$+ 69 \quad 10'' \text{A} \\ 34$$

$$+ 16 \quad \text{MH} \\ 29$$

76

$$\begin{array}{r} \text{BS} \\ 19.0 \quad 18.7 \end{array}$$

$$+ 89 \quad 4'' \text{P} \\ 42$$

25

$$\begin{array}{r} \text{BS} \\ 19.2 \quad 19.4 \end{array}$$

74

$$\begin{array}{r} \text{BS} \\ 17.3 \quad 20.0 \end{array}$$

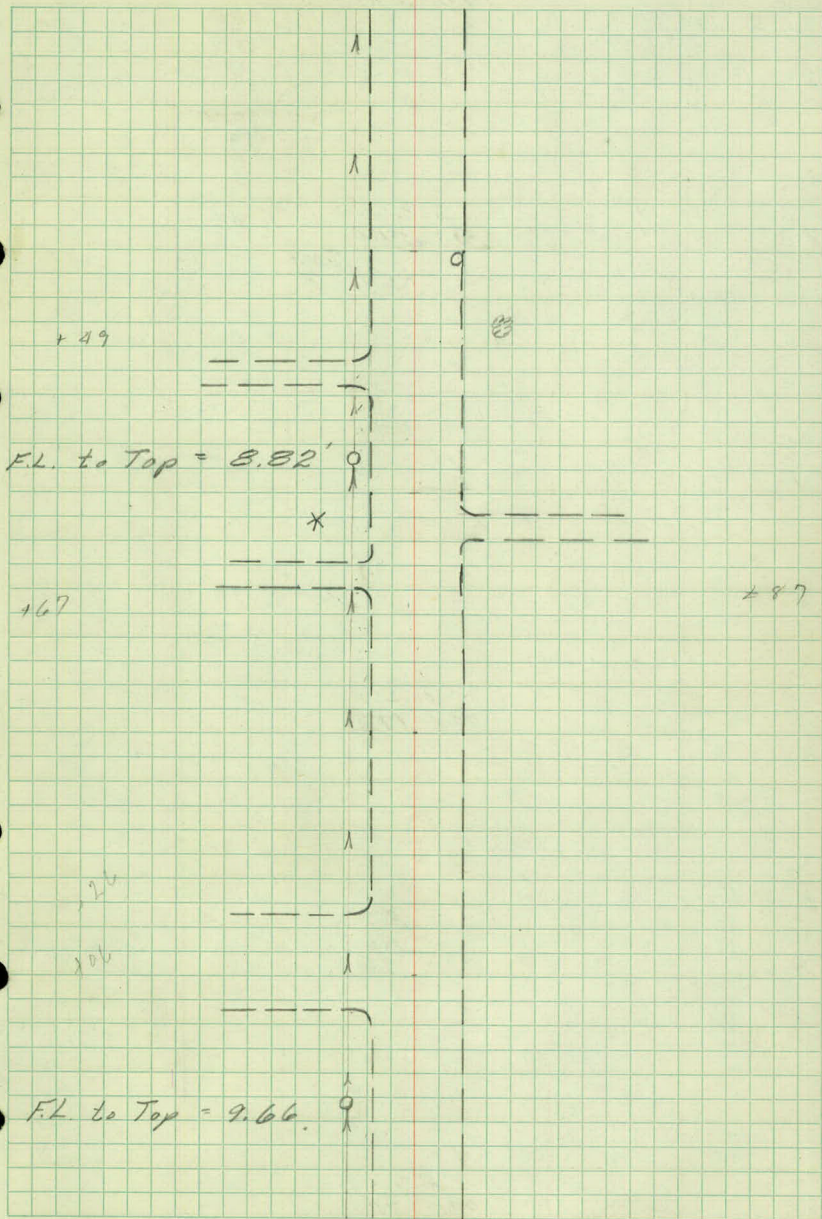
$$+ 47 \quad \text{MH} \\ 29$$

73

$$\begin{array}{r} \text{BS} \\ 17.6 \quad 20.0 \end{array}$$

Oct. 8, 1958

12



83

Lt

$$\begin{array}{r} \cdot \text{BS} \\ 19.0 \end{array} \quad \begin{array}{r} \cdot \text{BS} \\ 19.1 \end{array}$$

Rt

$$+49 \quad \begin{array}{r} \text{MH} \\ 2.5 \end{array}$$

82

$$\begin{array}{r} \cdot \text{BS} \\ 20.0 \end{array} \quad \begin{array}{r} \cdot \text{BS} \\ 20.0 \end{array} \quad \begin{array}{r} \cdot \text{T-MH} \\ +57 \end{array} \quad \begin{array}{r} \cdot \text{MH} \\ 18 \end{array}$$

81

$$\begin{array}{r} \cdot \text{BS} \\ 19.9 \end{array} \quad \begin{array}{r} \cdot \text{BS} \\ 20.7 \end{array} \quad \begin{array}{r} \cdot \text{3' Wall} \\ +23 \end{array} \quad \begin{array}{r} \cdot \text{3' Wall} \\ 32.5 \end{array} \quad \begin{array}{r} \cdot \text{Ent 15" x 20' CM} \\ +11 \end{array} \quad \begin{array}{r} \cdot \text{Ent 15" x 20' CM} \\ 28.5 \end{array} \quad \begin{array}{r} \cdot \text{NW. Cor. H.} \\ +100 \end{array} \quad \begin{array}{r} \cdot \text{NW. Cor. H.} \\ 105.6 \end{array}$$

80

$$\begin{array}{r} \cdot \text{BS} \\ 20.5 \end{array} \quad \begin{array}{r} \cdot \text{BS} \\ 19.2 \end{array}$$

$$+157 \quad \begin{array}{r} \cdot \text{ER} \\ 20.8 \end{array}$$

$$+30 \quad \begin{array}{r} \cdot \text{BR} \\ 45 \end{array}$$

79

$$+90 \quad \begin{array}{r} \cdot \text{ER} \\ 40.3 \end{array}$$

$$\begin{array}{r} \cdot \text{BS} \\ 19.7 \end{array}$$

$$+72 \quad \begin{array}{r} \cdot \text{BR} \\ 20.4 \end{array} \quad +86 \quad \begin{array}{r} \cdot \text{MH} \\ 27 \end{array}$$

78

$$\begin{array}{r} \cdot \text{E.Fe} \\ +75 \end{array} \quad \begin{array}{r} \cdot \text{E.Fe} \\ 33 \end{array} \quad \begin{array}{r} \cdot \text{BS} \\ 20.0 \end{array} \quad \begin{array}{r} \cdot \text{BS} \\ 20.2 \end{array}$$

$$+184 \quad \begin{array}{r} \cdot \text{MH} \\ 29 \end{array} \quad +160 \quad \begin{array}{r} \cdot \text{End} \\ \text{Cottivation} \end{array}$$

Oct. 9, 1958

13

Lt

Rt

+80

Top to FL = 9.50

+95

NS 30.3
EW 20

30.3

20

+21

Top to FL = 9.60

Top to FL = 9.75'

88

Lt

$$\begin{array}{r} \text{BS} \\ 19.6 \end{array} \begin{array}{r} \text{BS} \\ 19.7 \end{array}$$

Rt

87

$$\begin{array}{r} \text{BS} \\ 19.6 \end{array} \begin{array}{r} 20.4 \\ +76 \end{array} \begin{array}{r} 15'' \text{ Adj} \\ 40 \end{array}$$

$$\begin{array}{r} 8'' \text{ P} \\ +53 \\ \hline 49 \end{array}$$

86

$$\begin{array}{r} \text{BS} \\ 20-20.2 \\ \hline 3 \end{array} +04 \begin{array}{r} \text{MH} \\ 24.5 \end{array}$$

$$+44 \begin{array}{r} \text{Ent } 18'' \times 30' \text{ CM} \\ \hline 28 \end{array}$$

55

85

$$\begin{array}{r} \text{BS} \\ 20 \end{array} \begin{array}{r} 20 \end{array}$$

$$+49 \begin{array}{r} \text{NW. Cor Bldg} \\ \hline 97.5 \end{array}$$

84

$$\begin{array}{r} \text{BS} \\ 19.3 \end{array} \begin{array}{r} 19.3 \end{array}$$

83

$$\begin{array}{r} \text{BS} \\ 19.0 \end{array} \begin{array}{r} 19.1 \end{array}$$

$$+79 \begin{array}{r} 7'' \text{ P} \\ \hline 49 \end{array}$$

$$+97 \begin{array}{r} 8'' \text{ P} \\ \hline 71 \end{array}$$

$$+95 \begin{array}{r} 8'' \text{ P} \\ \hline 62 \end{array}$$

$$+76 \begin{array}{r} 6'' \text{ P} \\ \hline 41 \end{array}$$

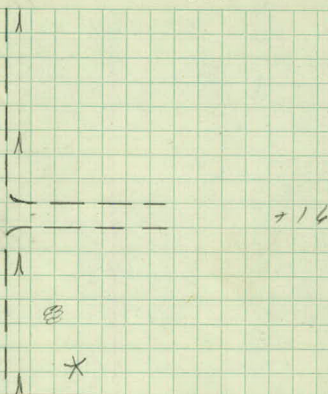
$$+76 \begin{array}{r} 6'' \text{ P} \\ \hline 55 \end{array}$$

Lt

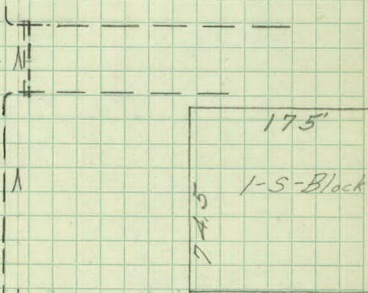
± Oct 9, 1958

Rt 14

15 5 14.8
55



o FL to Top = 10.10



93

$$\begin{array}{r} \text{BS} \\ 17.8 \quad 20.2 \end{array}$$

92

$$\begin{array}{r} \text{BS} \\ 19.7 \quad 20.9 \end{array}$$

91

$$\begin{array}{r} \text{BS} \\ 19.0 \quad 20.2 \end{array}$$

90

$$\begin{array}{r} \text{BS} \\ 18.7 \quad 20.5 \end{array}$$

$$\begin{array}{r} \text{Culv Headwall} \\ +75 \quad 23-35 \\ +77 \quad 23 \text{ Walk} \\ \quad 35 \end{array}$$

$$\begin{array}{r} +61 \quad 4 \text{ A} \\ \quad 50 \end{array}$$

$$\begin{array}{r} \text{MH} \\ +58 \quad 26 \end{array}$$

$$\begin{array}{r} \text{BS} \\ 19.8 \quad 20.3 \end{array}$$

$$\begin{array}{r} \text{Fetshrub} \quad 18 \text{ L. Pop} \\ +96 \quad 43 \quad +99 \quad 40 \end{array}$$

$$\begin{array}{r} +06 \quad 14 \text{ M} \\ \quad 60 \end{array}$$

$$\begin{array}{r} \text{Tripl'd BE} \\ +00 \quad 42 \end{array}$$

$$\begin{array}{r} \text{BS} \\ 19.6 \quad 19.7 \end{array}$$

88

Nov. 5, 1958

15

FA
HP
AB

^

^

^

^

^

^

^

o

o

FL. to Top = 10.30

^

^

o x

NO. 2

o x

SSU

Wood picket

^

#57

o

o

98

Lt

$$\begin{array}{r} \text{BS} \\ 26.5 \end{array} \begin{array}{r} 33.0 \end{array}$$

Rt

$$\begin{array}{r} \text{ER} \\ +60 \end{array} \begin{array}{r} 33.5 \end{array}$$

$$\begin{array}{r} \text{BR} \\ +45 \end{array} \begin{array}{r} 23.4 \end{array}$$

$$\begin{array}{r} \text{x-Fe} \\ +17 \end{array} \begin{array}{r} 34 \end{array}$$

$$\begin{array}{r} \text{Begin 15" x CM} \\ +53 \end{array} \begin{array}{r} \text{Ent } 29 \end{array}$$

97

$$\begin{array}{r} \text{BS} \\ 26.3 \end{array} \begin{array}{r} 22.0 \end{array}$$

$$\begin{array}{r} \text{BR} \\ +83 \end{array} \begin{array}{r} 38 \end{array}$$

$$\begin{array}{r} \text{ER} \\ +95 \end{array} \begin{array}{r} 22 \end{array}$$

$$\begin{array}{r} \text{MH} \\ +69 \end{array} \begin{array}{r} 25 \end{array}$$

$$\begin{array}{r} \text{MH} \\ +68 \end{array} \begin{array}{r} 38.5 \end{array}$$

$$\begin{array}{r} \text{MH} \\ +68 \end{array} \begin{array}{r} 27.5 \end{array}$$

$$\begin{array}{r} \text{Headwall} \\ +54 \end{array} \begin{array}{r} 22-39 \end{array}$$

$$\begin{array}{r} \text{Fry 30' LT} \\ +65 \end{array}$$

$$\begin{array}{r} \text{Ent 36" x 24" CM} \\ +43 \end{array} \begin{array}{r} 29 \end{array}$$

$$\begin{array}{r} \text{ER} \\ +50 \end{array} \begin{array}{r} 39 \end{array}$$

$$\begin{array}{r} \text{Fe Cor} \\ +28 \end{array} \begin{array}{r} 34 \end{array}$$

$$\begin{array}{r} \text{Headwall} \\ +21 \end{array} \begin{array}{r} 24-34 \end{array}$$

96

$$\begin{array}{r} \text{BR} \\ +38 \end{array} \begin{array}{r} 19.3 \end{array}$$

$$\begin{array}{r} \text{BS} \\ 19.0 \end{array} \begin{array}{r} 19.0 \end{array}$$

95

$$\begin{array}{r} \text{BS} \\ 18.9 \end{array} \begin{array}{r} 19.1 \end{array}$$

$$\begin{array}{r} \text{SW Cor H} \\ +35 \end{array} \begin{array}{r} 13.2 \end{array}$$

$$\begin{array}{r} \text{Rock Wall} \\ +13 \end{array} \begin{array}{r} 5.3 \end{array}$$

94

$$\begin{array}{r} \text{BS} \\ 19.2 \end{array} \begin{array}{r} 18.7 \end{array}$$

$$\begin{array}{r} \text{24" E} \\ +99 \end{array} \begin{array}{r} 51 \end{array}$$

$$\begin{array}{r} \text{MH} \\ +64 \end{array} \begin{array}{r} 29 \end{array}$$

$$\begin{array}{r} \text{SW Cor H} \\ +63 \end{array} \begin{array}{r} 13.2 \end{array}$$

$$\begin{array}{r} \text{24" E} \\ +62 \end{array} \begin{array}{r} 52 \end{array}$$

$$\begin{array}{r} \text{22" E} \\ +62 \end{array} \begin{array}{r} 67 \end{array}$$

93

$$\begin{array}{r} \text{BS} \\ 17.8 \end{array} \begin{array}{r} 20.2 \end{array}$$

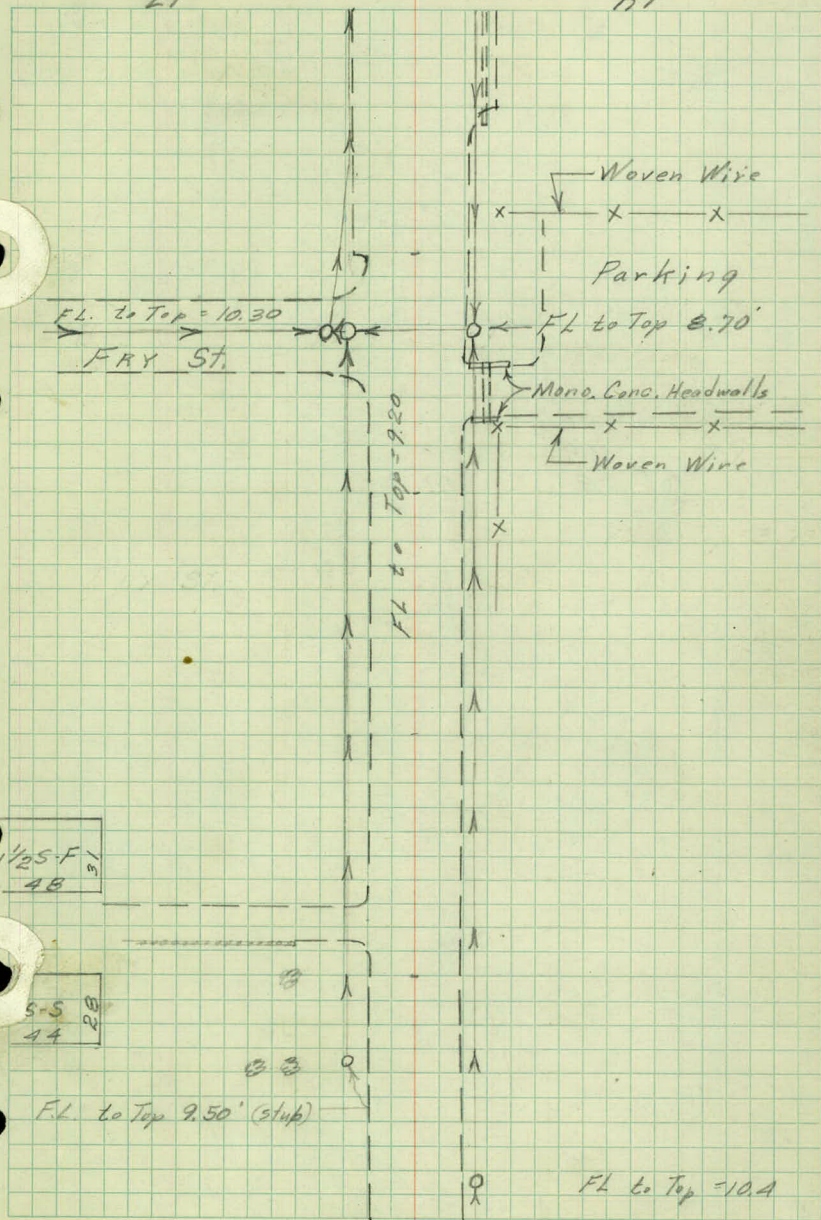
$$\begin{array}{r} \text{MH} \\ +15 \end{array} \begin{array}{r} 25 \end{array}$$

Nov 5, 1958

16

Lt

Rt



103

$$\begin{array}{r} \text{B.S.} \\ 40 \quad 22 \end{array}$$

$$+99 \frac{\text{Angle in Bldg.}}{77.5}$$

$$+56 \frac{\text{MH}}{39}$$

$$+94.5 \frac{28''\text{E}}{51}$$

$$+59 \frac{28''\text{E}}{50}$$

102

$$\begin{array}{r} \text{B.S.} \\ 37 \quad 22 \end{array}$$

$$+62 \frac{\text{ER}}{23}$$

$$+90 \frac{30''\text{E}}{50}$$

$$+53 \frac{\text{BR}}{29}$$

$$+72 \frac{25' \text{Walk (Mon)} }{28.5}$$

$$+19 \frac{\text{ER}}{29}$$

$$+56 \frac{20''\text{E}}{50}$$

$$+14 \frac{\text{BR}}{29}$$

$$\begin{array}{r} \text{B.S.} \\ 34.4 \quad 22 \end{array}$$

$$+19 \frac{30''\text{E}}{50}$$

$$+40 \frac{\text{PP}}{28}$$

$$+30 \frac{\text{Cor. BS.}}{33}$$

$$+85 \frac{18''\text{E}}{50}$$

$$+41 \frac{\text{ER}}{23}$$

$$+19 \frac{\text{Cor. BS.}}{46}$$

$$+30 \frac{\text{Cor. BS.}}{46}$$

$$+51 \frac{18''\text{E}}{50}$$

$$+63 \frac{\text{NW Cor. Bldg}}{78}$$

$$+19 \frac{\text{BR}}{45}$$

$$+12 \frac{\text{Cor Hedge}}{37}$$

$$+15 \frac{30''\text{E}}{50}$$

$$+28 \frac{\text{PP}}{28}$$

100

$$+05 \frac{\text{MH}}{39}$$

$$+08 \frac{\text{Cor. Curb}}{41}$$

$$+97 \frac{\text{E. RC}}{22}$$

$$+97 \frac{\text{Bay Walk}}{23-29}$$

$$+88 \frac{\text{Bay RC Cor. \& Cor}}{41}$$

$$+74 \frac{\text{Edge Cor. Ent}}{35}$$

$$+89 \frac{\text{ER}}{39}$$

$$+15 \frac{\text{Cor. Conc}}{41}$$

$$+16 \frac{\text{Cor. Conc}}{52.5}$$

$$+26 \frac{\text{Edge Cor. Ent}}{37}$$

$$+79 \frac{\text{BR}}{25}$$

$$+50 \frac{\text{Pump}}{57.5}$$

$$+11 \frac{\text{NW Cor. S. Sta.}}{94}$$

99

$$\begin{array}{r} \text{B.S.} \\ 26.5 \end{array}$$

$$+00 \frac{\text{Bay Rad. C.}}{22}$$

$$+03 \frac{\text{Sig.}}{26}$$

$$+10 \frac{\text{End RC}}{31}$$

$$+69 \frac{\text{Bay Curb}}{22}$$

$$+84 \frac{\text{Sig. Stub.}}{27}$$

$$+94 \frac{\text{Sig. Box}}{26}$$

$$+68 \frac{\text{Cor. Park Wood Guard}}{33}$$

$$+74 \frac{\text{PP}}{28}$$

$$+41 \frac{\text{NE Cor. Ent.}}{33}$$

$$+55 \frac{\text{Ent.}}{28}$$

$$+60 \frac{\text{MH}}{24}$$

$$+07 \frac{\text{NW Cor. Ent.}}{33}$$

$$+02 \frac{\text{NW Cor. Fire Sta.}}{77}$$

98

$$\begin{array}{r} \text{B.S.} \\ 26.5 \quad 33 \end{array}$$

Nov. 5, 1958

17

FL to Top 12.50'

Asph. Curb

64 L.F. of Portable Curb

144 L.F. of Portable Curb

Asph. Curb

FL. to Top = 10.35'

St. Marys Ave

Asph. Curb

F.U.G.T.A.
Bldg.

6' Mono.
Walk

F.U.G.T.A.
Service
station

Parking Area

FL. to Top = 7.70'

2 S Brick
Fire Barn

106

105

+90

CB

55

+97

ER

33

+77

BR

27

+11

SW Cor

Conc 366

50

+09

ER

22

104

+84

BCR

23

+26

SEC

Cor

Conc 366

50

+29

BR

22

+195

ERC

35

+82

BR

22

+78

PP

30

+56

MT

16

+10

Hedge

36.5

+81

Cr Hedge

36

+68

30"E

51

+83

ER

28

+77

BR

22.5

+89

± 8 Walk (Mond)

28.5

+53

ER

22.5

+163

30"E

50

+15

ER

30

+48

BR

28

+22

± 6 Walk (Mond)

28.5

+58

Sig. Pressure

2-11

+103

BR

23

BS

40

22

+102

PP

28

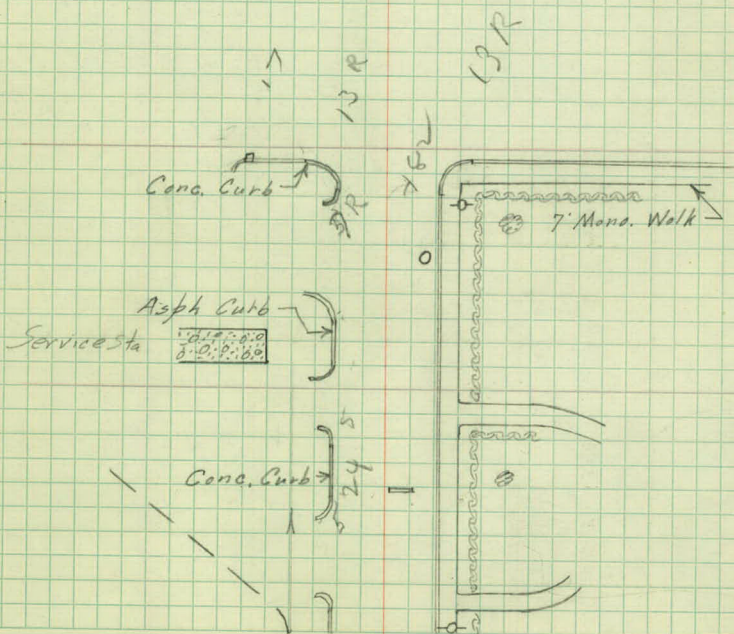
+81

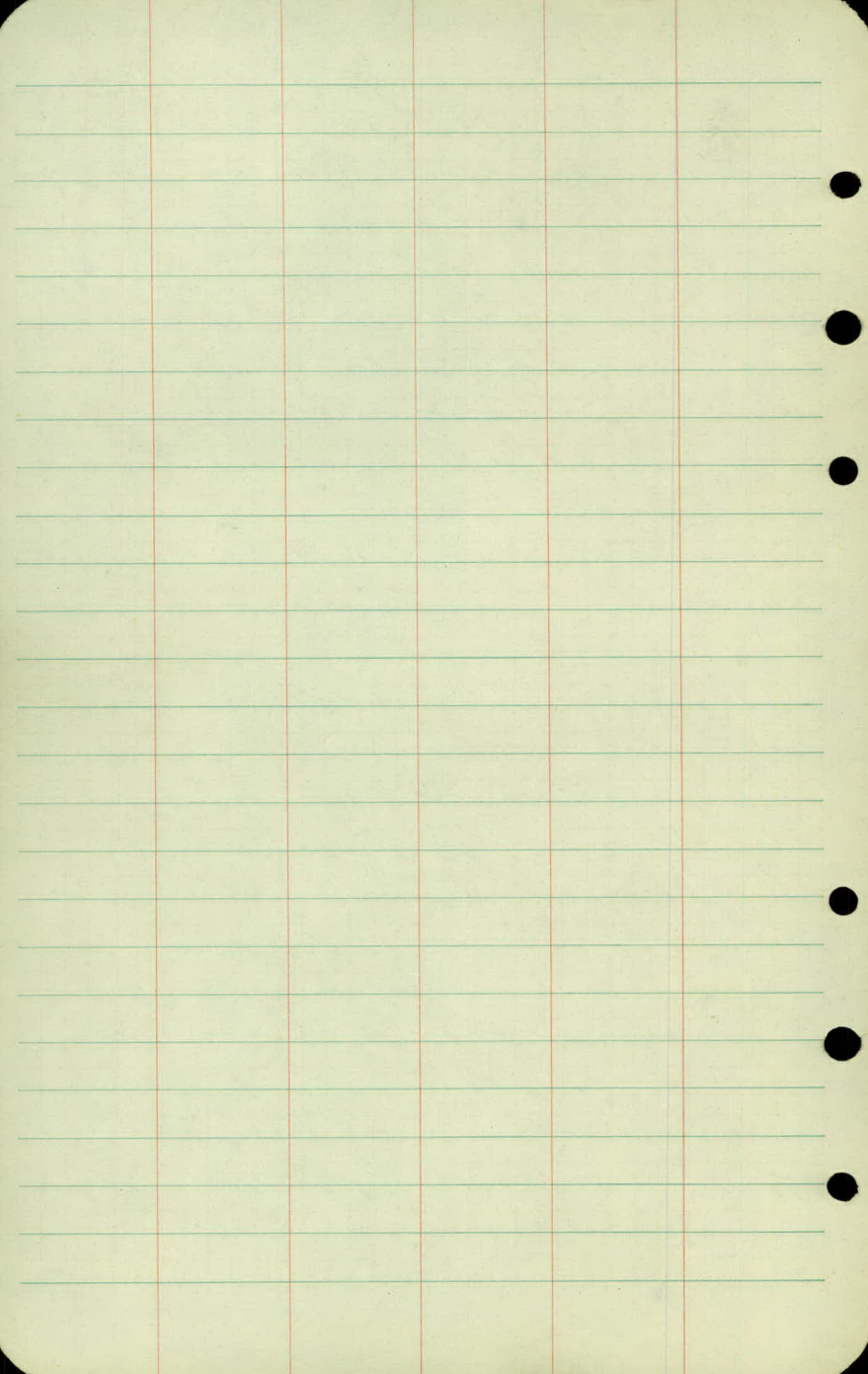
X-Hedge

37

+10

Plate





Jan 12, 1959

a

Re locate House Bt sta 46

Locate Sand Traps + Bldg.

Get Size of Box Culvert openings

Additional Topography

Sta

LH

L

PK

46

+01 NW. Cor Ho.
79.8

37

+91 Edge S. Trap
← 91 →+03 Edge S. Trap +58 Edge S. Trap
52 50

36

35 +80 Edge S. Trap
← 8734 +33 M.H.
17

2

30

29

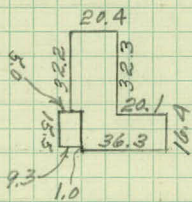
28 +86 S.W. Cor Bldg
153.2

Jan 12, 1959

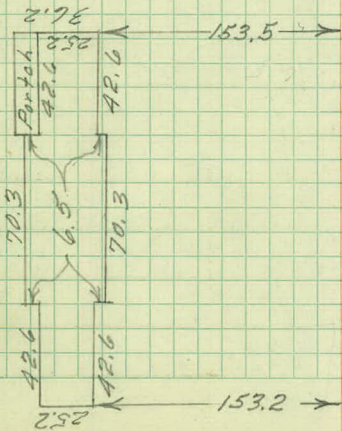
6

14

Pl



0



Sta

96+56 X- Drain

93+

81+37

59+52

52+09

Jan 12, 1959

C

M14

outlet 1.5' x 4.1'

in 4.0' x 1.8'

outlet 4.1' x 1.6'

in 4.0 x 1.0'

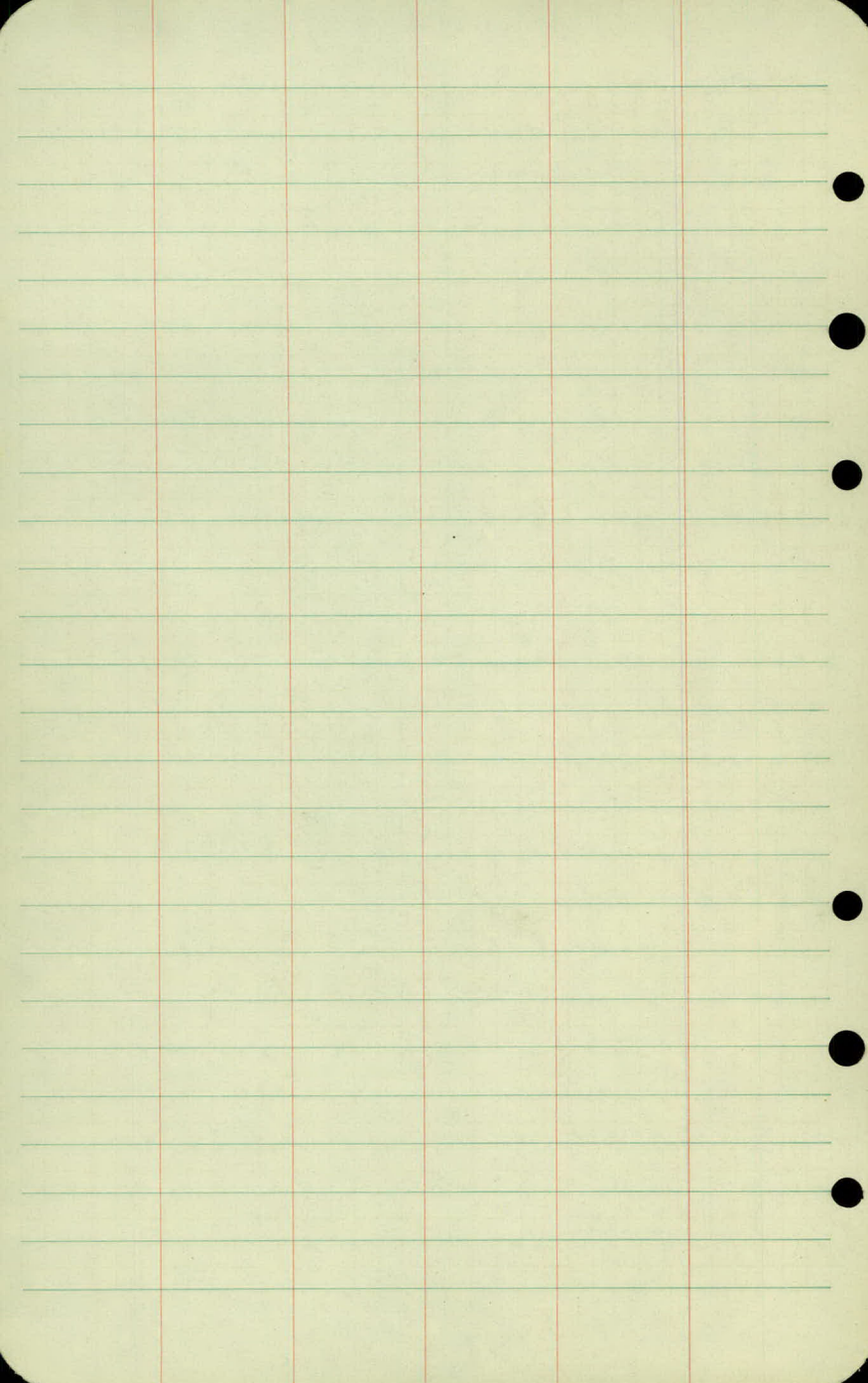
outlet 4.0 x 0.7'

in 4.0 x 2.1

outlet 4.1 x 1.9'

in 4.0 x 2.0

outlet 4.1 x 1.9'



FK
RG
JH

March 16, 1959

a

Signal Box

Locations

Larpentour & Cleveland

55

+63 Pull Box
21

54

+12 Sig. Cont. Box
49

53

+63 Pull Box
184

52

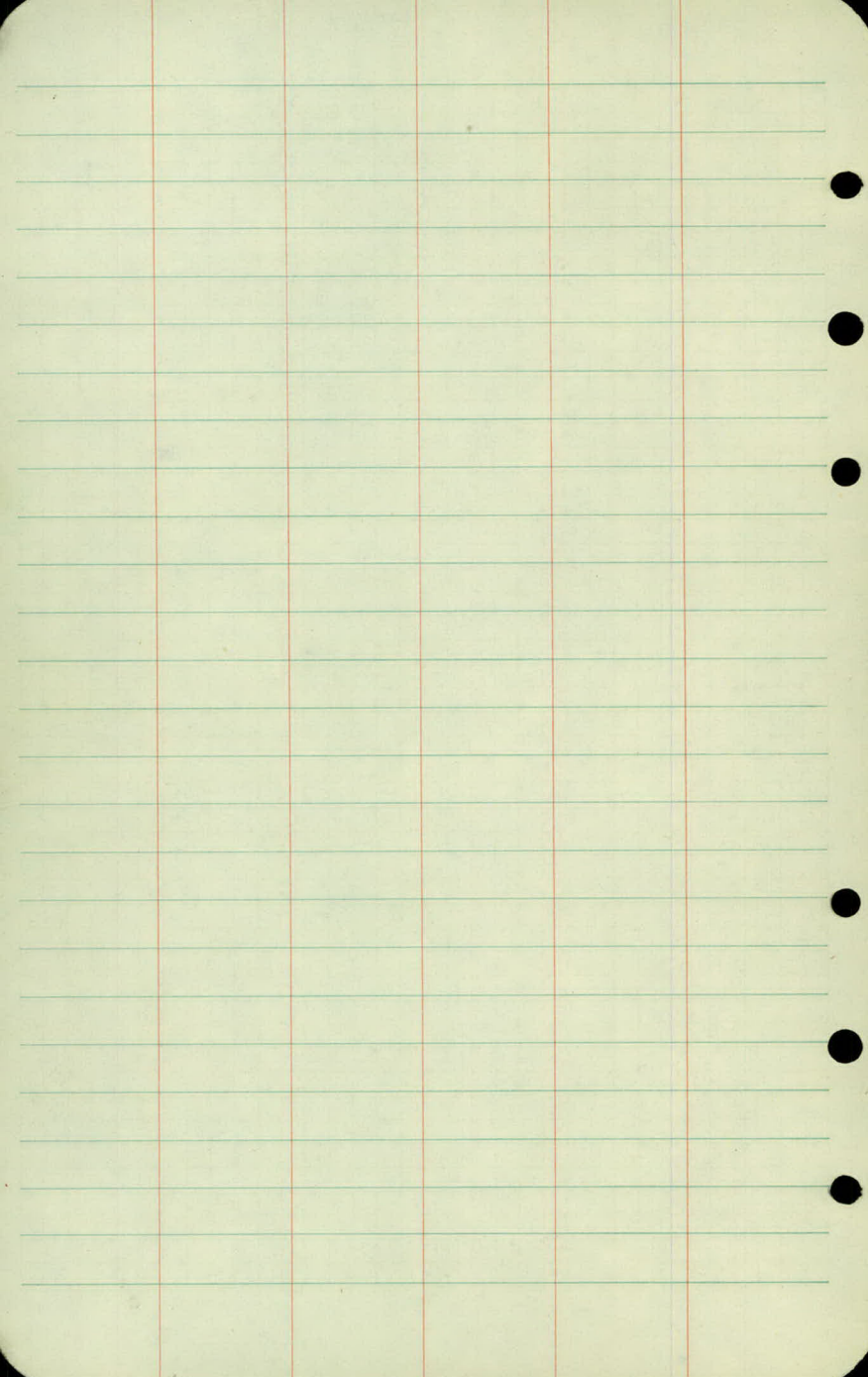
51

+00 Pull Box
21-23

March 16, 1959

6

?



LARPENTEUR

Cleveland to Snelling

Bench Levels

Sta	+	π	-	Elev
BM	1.85	982.31		(980.46)
BM			2.61	979.70 ^{979.69}
TP	2.64	979.21	5.74	976.57
BM	3.05		2.23	976.98
TP	4.292	979.98	3.52	975.69 ^{975.48}
BM	0.85	979.34	1.49	978.49
TP	1.95	974.86	6.43	972.91
BM	0.00	973.97	0.89	973.97
TP	3.52	968.84	8.65	965.32 ^{966.45}
BM			2.33	966.51
TP	3.20	965.68	6.36	962.48
BM	3.16	964.63	4.21	961.47 ^{959.10}
BM	2.83	961.92	5.54	959.09 ^{961.30}
BM			0.58	961.34
TP	4.71 ^s	960.11	6.52 ^s	955.40
BM			3.35	956.76 (956.73)
TP	4.59 ^s	961.92	2.78	957.33
BM			3.84 ^s	958.08 (958.05)
BM	2.58	961.67		959.09
BM			4.94	956.73

Top Mont Cleveland & Larpenteur

Top N.W. Cor Lower step School House

S.E. Cor. Walk 2061 W Larpenteur

E End Culvert

S.W. Cor Lower step Front of office Lt 6740

E. End Door Sill Ho[#] 1867 W. Larpenteur

Top N.W. Cor Top step Ho[#] 1750 W Larpenteur

Top Mont & Sta 92+21[±]

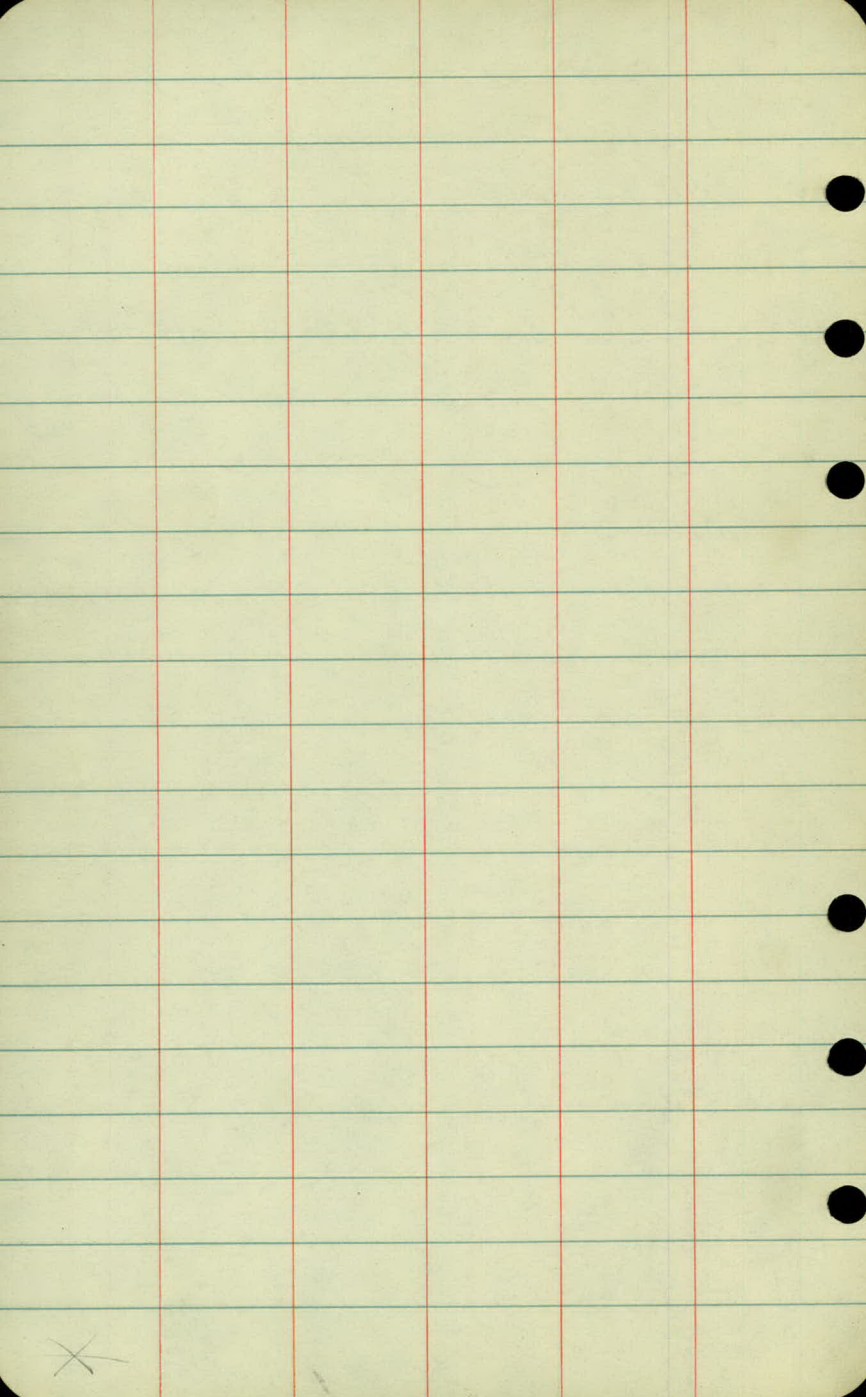
S.W. Cor Lower step Lt 93+70

Top N.W. Cor Lower step 1644 W. Larpenteur

Top Hyd Rt Sta 105+57

Top Mont & Sta 92+21

Top N.W. Cor Lower step 1644 W. Larpenteur



a

DIST.

VERT.
ANGLE

ROD
EQUIV.

ROD

DIFF.

ELEV

OBJECT

AZI

STADIA

N on E Larpenteur

910' West Montat Snelling

to Montat Snelling 90°00'

6E

156°36'

"

158°21'

"

161°40'

"

171°35'

"

179°42'

"

181°41'

"

181°47'

"

187°30'

"

193°19'

E South
end of box
culvert

132°25'

ditch

138°48'

"

110°40'

"

150°30'

"

163°10'

FK
RG
KP
AB

March 24
Clear Cool 32°

6

DIST.

VERT.
ANGLE

ROD
EQUIV.

ROD

DIFF.

ELEV

H. 1. = 960.9

415.3

955.6

4.4

956.5

548

11.9

49.0

583

12.2

48.7

607

12.3

48.6

638

14.0

46.9

712

15.7

45.2

870

18.2

42.7

1000

18.7

42.2

1100

20.5

40.4

1300

21.7

39.2

38

8.86

52.0

45

8.3

52.6

95

8.45

52.4

175

10.2

50.7

295

10.7

50.2

OBJECT

AZ.

STADIA

Nov. 21, 1958

C

Draw Location

59 +

stadia

$$HI = 981.99V$$

Object

AZ

Stadia

π at Sta 59+00

to Sta 69+00

90°00'

BM E. End Culvert

GE

189° 49

"

160°15' 52

"

140°15' 65

"

126°40' 84

"

118°40' 104

"

113°20' 126

"

126° 200

"

133°30' 170

"

142°20' 148

"

153°20' 131

"

170° 120

"

172°20' 170

"

156° 185

"

145°20' 208

"

136°50' 233

FK
AB
JH

Dist.	Vert. Angle	Rod Equiv.	Nov. 21, 1952		d Elev.
			Rod	Diff.	
			H.I. 532		76.69 (76.50) ✓
			6.30		(975.69) ✓
			7.6		74.4
			8.6		73.4 ✓
			9.1		72.9 ✓
			9.4		72.6 ✓
			9.1		72.9 ✓
			9.0		73.0 ✓
			10.3		71.7 ✓
			10.7		71.3 ✓
			10.4		71.6
			10.0		72.0 ✓
			9.2		72.8 ✓
			9.6		72.4 ✓
			9.6		72.4 ✓
			10.2		71.8 ✓
			10.8		71.2 ✓

$HI = 981.99$

Object

AZ

Stadia

G.E.

129° 20' 263

"

124° 35' 294

"

132° 20' 325

"

137° 30' 300

"

142° 25' 280

E OF DRAW

150° 25' 255

"

141° 10' 300

"

139° 40' 336

"

139° 55' 370

"

138° - 408

"

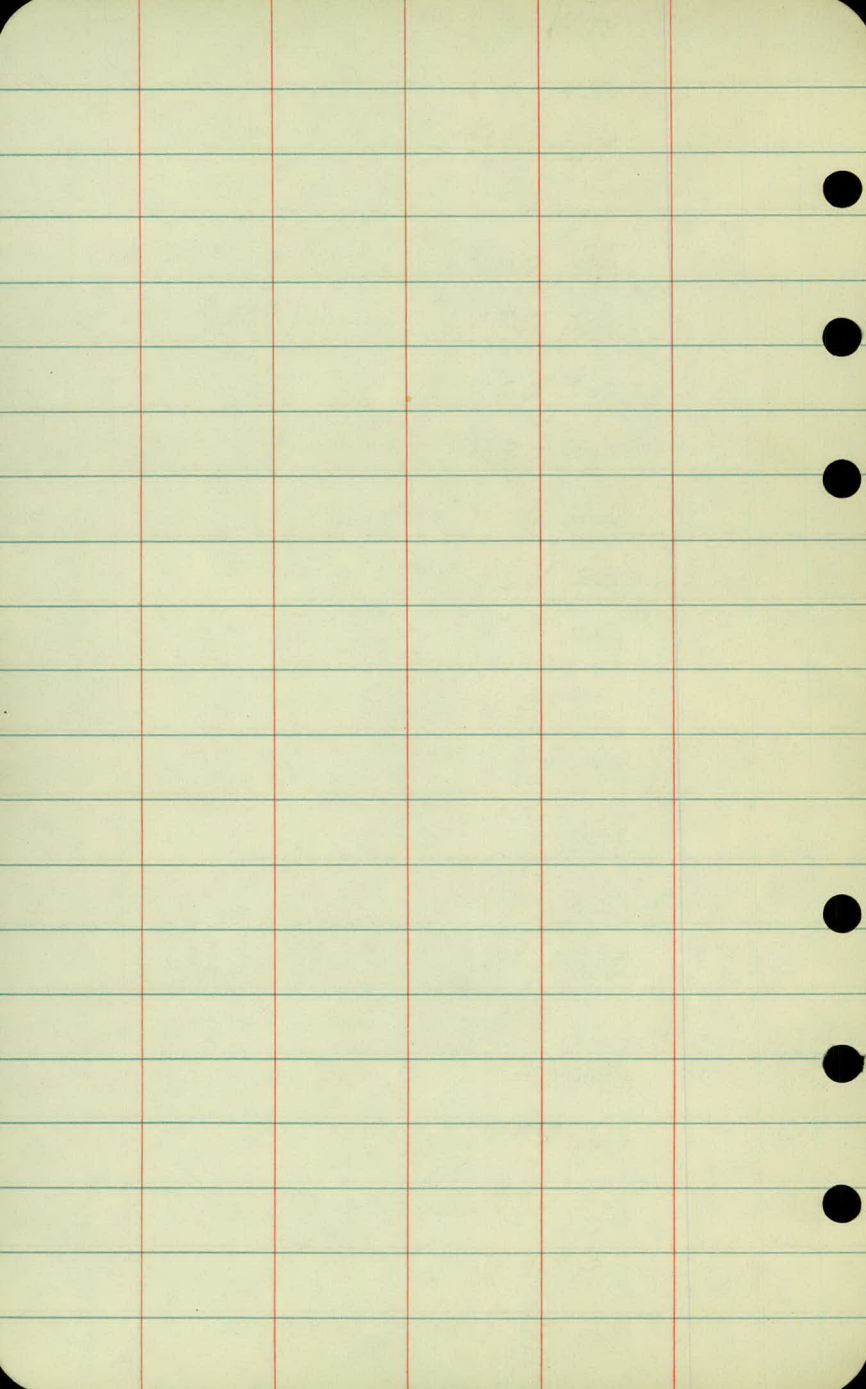
137° - 450

"

137° - 480

NOV. 21, 1958

Dist.	Vert. Angle	Rod Equiv.	Rod	Diff.	^e Elev.
			10.6		71.4 ✓
			10.2		71.8 ✓
			11.4		70.6 ✓
			11.3		70.7 ✓
			11.8		70.2 ✓
			10.8		71.2 ✓
			11.8		70.2 ✓
			12.4		69.6 ✓
			12.8		69.2 ✓
			13.4		68.6
			13.9		68.1
			13.6		68.4



Feb 16, 1959

a

Larpeur

59-30

M.H. Elev.

Sta	+	π	-	Elev.
BM	9.31	989.00		979.69
49+09			5.29	983.71
BM	3.30	981.79		978.49
67+77			5.71	976.08
67+00				67+00
77+00			5.05	76.74 976.74
BM	2.01	975.80		973.79
72+36.5			3.18	972.62
73+00			3.15	972.65 72.87
76+96.5			7.39	
77+00			7.07	68.94

49+09 MH Can be Lowered 3"±
 others Opened Can be Lowered 3.00'

46+59 8-6" E/ins 40' Rt

Feb 16, 1959

6

N.W. Cor Bottom Step School Ho

Top MH. 17' RT

S.W. Cor Bottom Step office Lt Sta 67+00

Top MH 17' RT

£

E. End Front Door Sitt Ho #1867

Top MH 17' RT

£

Top MH 17' RT

£

Gas Main Location

85+29 Gas Main x Road to 30' Lt

85+29 Gas Main on surface 30' Lt to sta

93+85 Gas Main goes underground 30' Lt

March 12, 1959

a

Additional Topography

Larpenteur 59-30

105

$\begin{array}{r} \text{Curb} \\ 185 \quad 106-118 + 83 \quad 52 \\ + 80 \quad \text{ERC} \\ 59 + 74 \quad \text{BRC} \\ 52 \\ + 68 \quad \text{P. Island} \\ 100-118 \end{array}$
 $\begin{array}{r} \text{P.I.S.} \\ 168 \quad 130-140 \\ + 85 \quad \text{Curb} \\ 130-140 \end{array}$
 $\begin{array}{r} \text{W Edge Conc} \\ + 56 \quad 104-143.5 \end{array}$

$+ 12.5 \quad \text{W. E. Parb ls } (12 \times 3)$
 $+ 13 \quad \text{W. E. Parb ls } (10 \times 3)$
 $+ 13 \quad \text{B.Curb} \quad + 25 \quad \text{EC} \quad + 27 \quad \text{Cn Conc}$
 $49.5 \quad 49.5 \quad 49.5-100$
 $+ 11 \quad \text{Cor Conc}$
 $49.5-100$
 $+ 12.5 \quad \text{Cor Blkg}$
 120

104

$\begin{array}{r} \text{B. Curb} \\ + 60 \quad 49.5 \end{array}$
 $\begin{array}{r} \text{E. Curb} \\ + 73 \quad 49.5 \end{array}$

103
102

$+ 34 \quad \text{Cn Blkg}$
 123

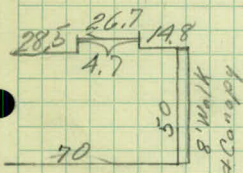
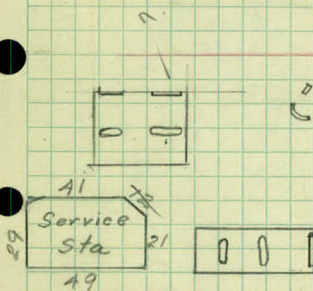
101

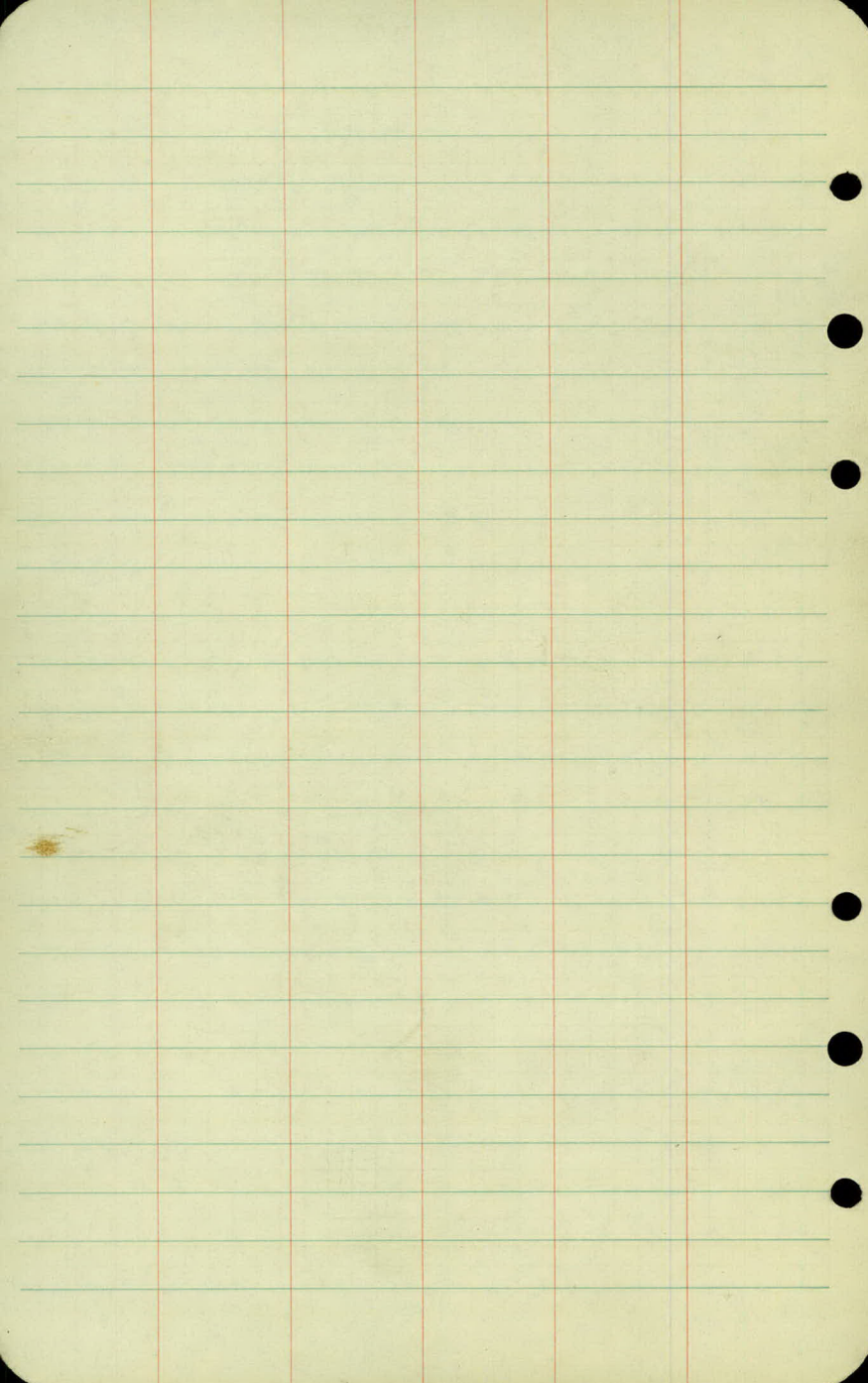
$+ 19 \quad \text{Alley}$
 $194-220$

$100 + 19 \quad \text{Ent} \quad 75-97 \quad + 19 \quad \text{End Curb} \quad 75$

$99 + 71 \quad \text{Traffic Signal}$
 27.4 Lt.

March 12, 1959 b





Sta + π - Elev.

BM 3.31 961.36

958.05

104+95 curb Rt

+87.4

(+83.7) sidewalk Rt (W. Edge 7' Conc. Walk) ^{W. J. B.}

+96 curb Lt

✓

105+23.71 Asph. at Edge of Conc

105

4.78 96.58

March 23, 1959
 Lt Rt ✓ 6

56.55	56.49	56.21	55.98	55.82
4.81	4.87	5.15	5.38	5.50
35	60	80	100	
Curb				

4.81	4.81	4.76	4.86	5.14	5.40
24	35	50	75	100	
Walk					

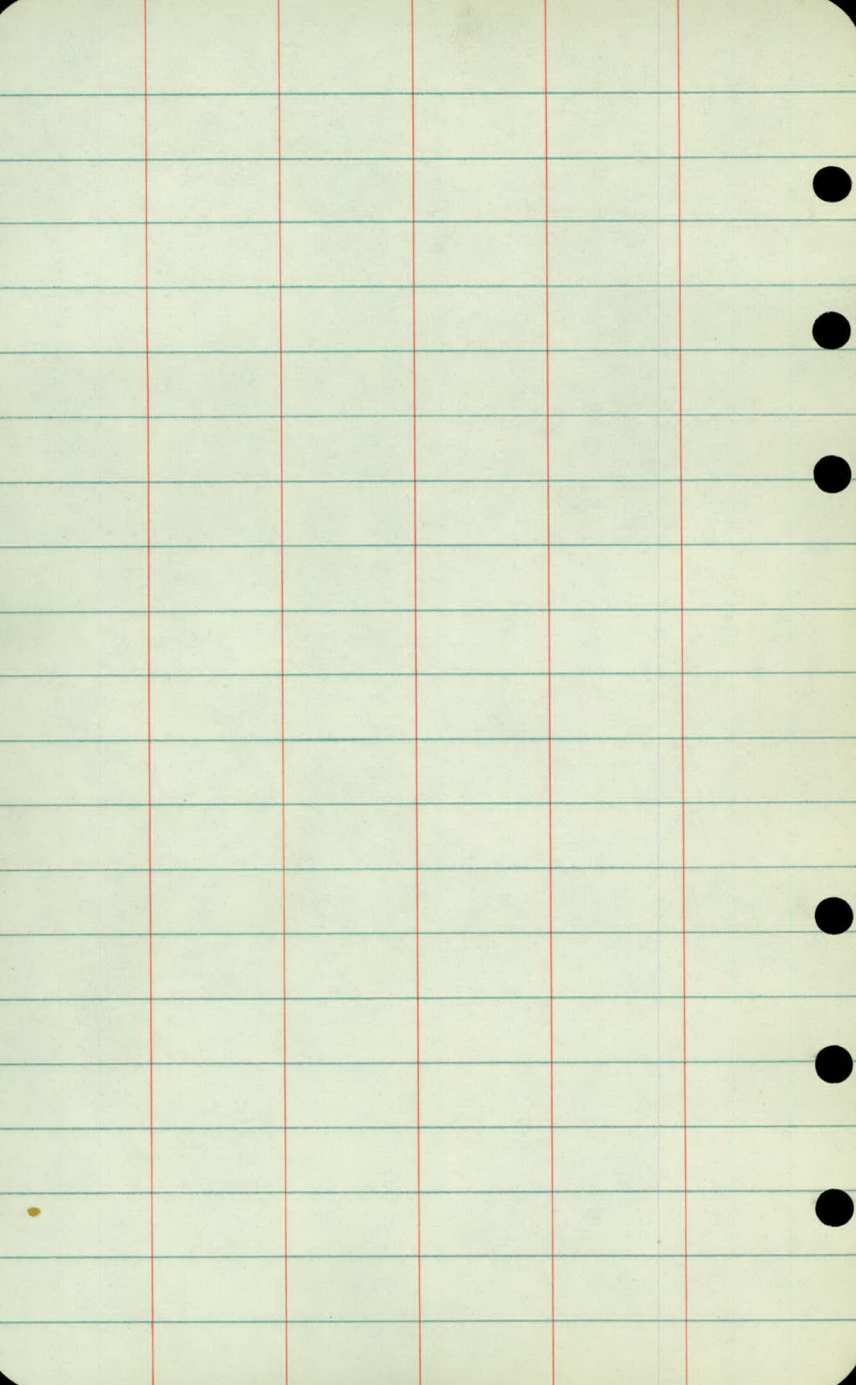
4.40	4.40	4.40	4.81
58	48	33	
Curb			

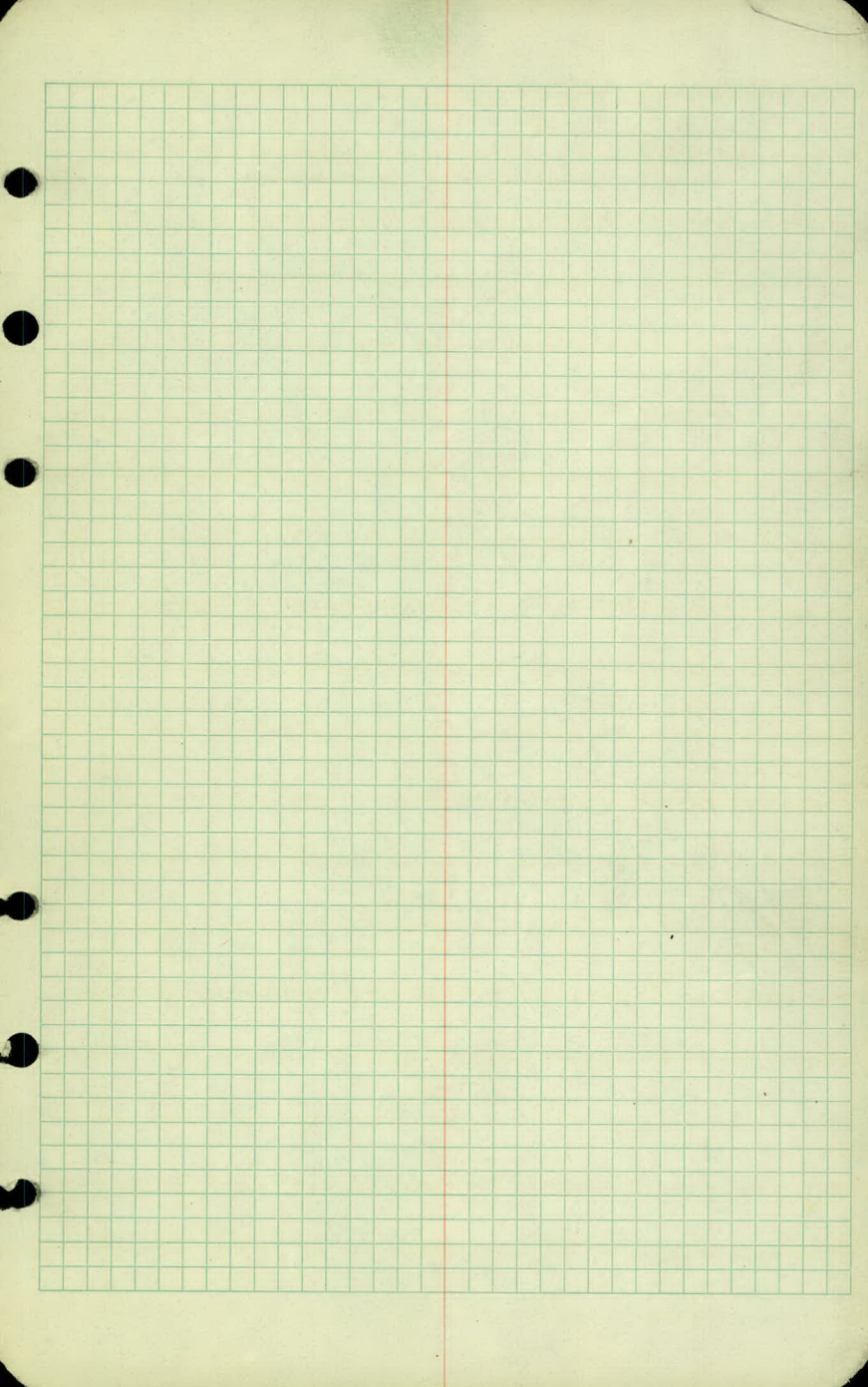
> Lt 4.42 4.42
 96 100
 Curb

56.41

4.75	4.95	5.38
30		30

£ check



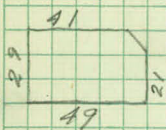


+87.4

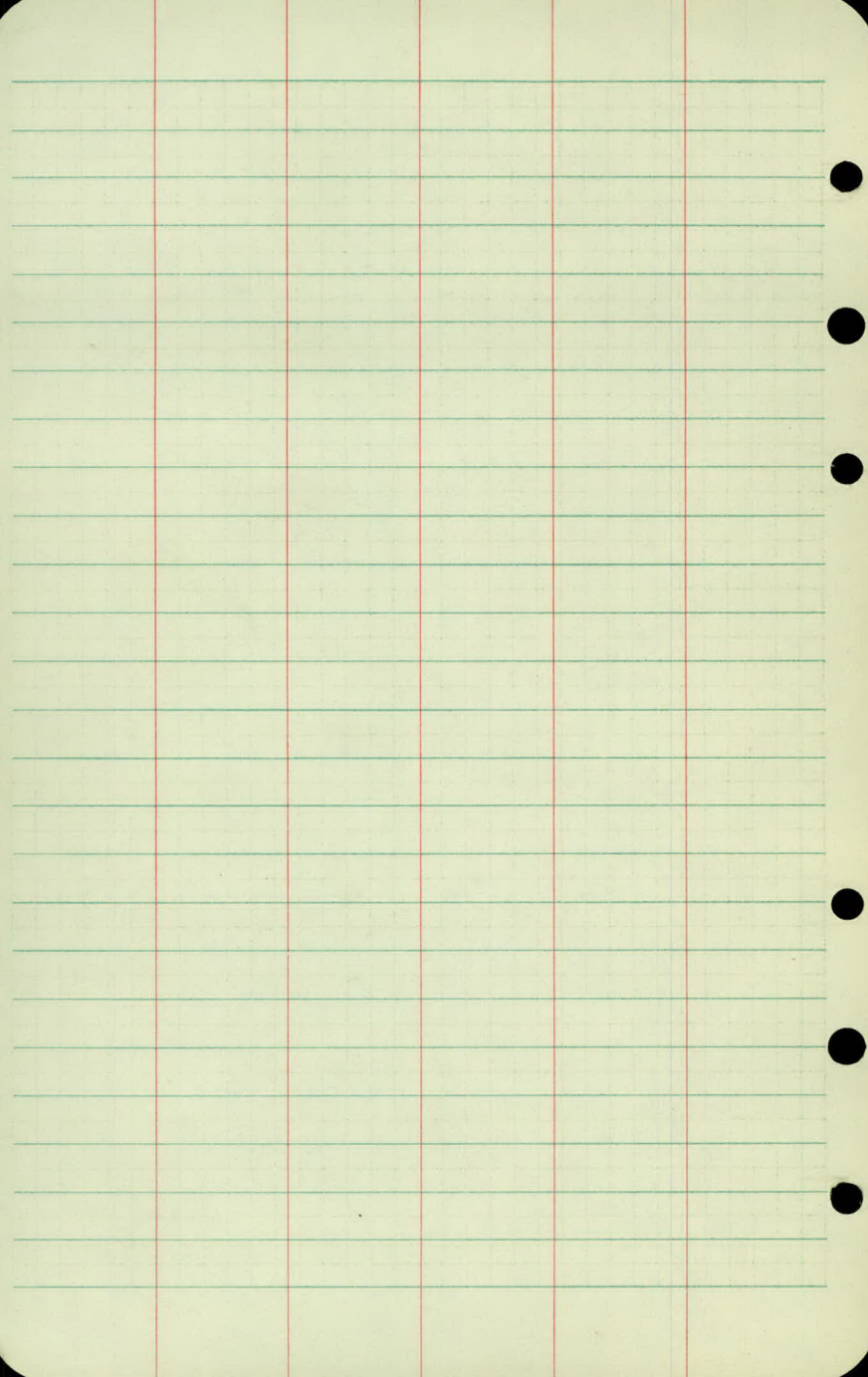
104+88 W. Edge of 7' Walk Rt

104+85 East Edge of Service Sta Signs + Curb

104+12.5 SW Cor Serv. Sta
119.9' Lt



119.9



March 18, 1959

a

Larpenteur

59-30

Parking Lot Disposal

AREA

Sta	+	π	-	Elev
BM	0.12	961.42		961.30
TP	4.61	957.55	8.48	952.94
0-97			9.6	947.95
0-83			9.1	948.45
0-63			9.2	948.35
0-45			9.1	948.45
0-21'			9.0	948.55
0-2'			8.7	948.85
0+01				

FK
RG
KP
JH

£

March 18, 1959

6

Rt

Top S.W. Cor Lower Step No #1687 Carpenter

163' Rt

193' Rt

212' Rt

221' Rt

224.5' Rt

231' Rt

51.5	51.2	51.5	51.8	51.2	51.6	51.4
6.1	6.4	6.1	5.8	6.4	6.0	6.2
	25	56	67	78	89	100

✓

49.1	49.4	49.6	50.1	50.1	50.7	51.3
8.5	8.2	8.0	7.5	7.5	6.9	6.3
217	211	200	186	168	150	120

Sta + π - Elev

957.55

0+01

0+50

✓

TP 6.41 957.36 6.60 950.95

1

✓

+50

FK
RG
HP
JH

£

March 18, 1959
March 19, 1959
RT

c

48.9	48.9	49.2	49.5	50.1	
8.7	8.7	8.4	8.1	7.5	✓
222	230	236	241	Fc	
				249.5	

50.8	50.8	50.6	50.5	50.3	50.1	49.8	49.6
68	68	70	71	73	75	78	80
25	30	50	75	100	125	150	

✓

49.6	49.5	49.1	49.1	49.3
8.0	8.1	8.5	8.5	8.3
250	243	225	200	175

Capped Pipe

50.7	50.5	50.4	50.2	49.9	49.6	49.5	49.4
67	69	70	72	75	78	79	80
19	48	75	100	123	150	172	

✓

49.7	49.7	49.3	49.1	49.3
7.7	7.7	8.1	8.3	8.1
250	245	241	222	200

50.7	50.5	50.3	50.2	50.0	49.8	49.5	49.4
67	69	71	72	74	76	79	80
28	54	81	100	123	146	176	

J

50.1	50.0	49.9	49.3
7.3	7.4	7.5	8.1
250	244	225	200

Sta + π - Elev

957.36

1+71

✓

2+15

✓

+20 Cor Garage 269' Rt

+23

✓

£

March 19, 1959

d

Rt

50.7	50.5	50.4	50.3	49.9	49.7	49.5	49.5
6.7	6.9	7.0	7.1	7.5	7.7	7.9	7.9
	28	49	81	100	119	140	154

✓

50.7	50.4	50.0	49.8	49.6
6.72	7.0	7.4	7.6	7.8
S.W. Cor. Conc Ent	231	218	200	182
250				

50.7	50.9	50.9	50.6	50.1	50.1	50.1	50.1
6.7	6.5	6.5	6.8	7.0	7.3	7.3	7.3
	8	23	41	69	95	100	124

✓

54.3	51.6	51.3	51.1	50.8	50.5	50.5	50.3
3.1	5.8	6.1	6.3	6.6	6.9	6.9	7.1
269	260	250	241	222	200	175	151

50.8	50.9	50.3	50.7	50.7	50.3	50.2	52.0
6.6	6.5	7.1	6.7	6.7	7.1	7.2	5.4
	21	36	41	53	76	94	

168 in STOCKPILE

✓

51.7	51.4	51.8	52.3	52.2	53.0	51.6	50.4	50.5	52.6
5.7	6.0	5.6	5.1	5.2	4.4	5.8	7.0	6.9	4.8
260	240	223	200	179	152	130	123	110	103

and STOCKPILE

54.0

3.4
268

W. side garage

Sta	+	↑	-	Elev.
-----	---	---	---	-------

		957.36		
--	--	--------	--	--

2+50				
------	--	--	--	--

r				
---	--	--	--	--

3				
---	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

MARCH 19, 1959

E

Rt

C.

50.7	51.2	51.2	50.8	51.2	51.1	51.0
6.7	6.2	6.2	6.6	6.2	6.3	6.4
	6	20	25	29	64	83

✓

	53.9	53.9	51.1	50.8	50.5	50.4
L.O.	3.5	3.5	6.3	6.6	6.9	7.0
	138	125	119	114	96	89

51.5	51.2	52.0	51.9	51.9	51.6	50.5	50.6
5.9	6.2	5.4	5.5	5.5	5.8	6.9	6.8
	2	6	26	48	81	87	96

✓

	54.3	54.4	51.9
L.O.	3.1	3.0	5.5
	131	106	100

51.7	51.7	52.7	52.6	52.8	52.7	52.5	50.9
5.7	5.7	4.7	4.8	4.6	4.7	4.9	6.5
	2	5	27	30	54	80	89

✓

	54.8	54.5	54.0	51.0
L.O.	2.6	2.9	3.4	6.4
	132	118	106	95

Sta + π - Elev

957.36

4

✓

+50

✓

TP 4.14 960.74 0.76 956.60

BM 1.04 956.70 956.73

£

March 19, 1959

f.

Rt

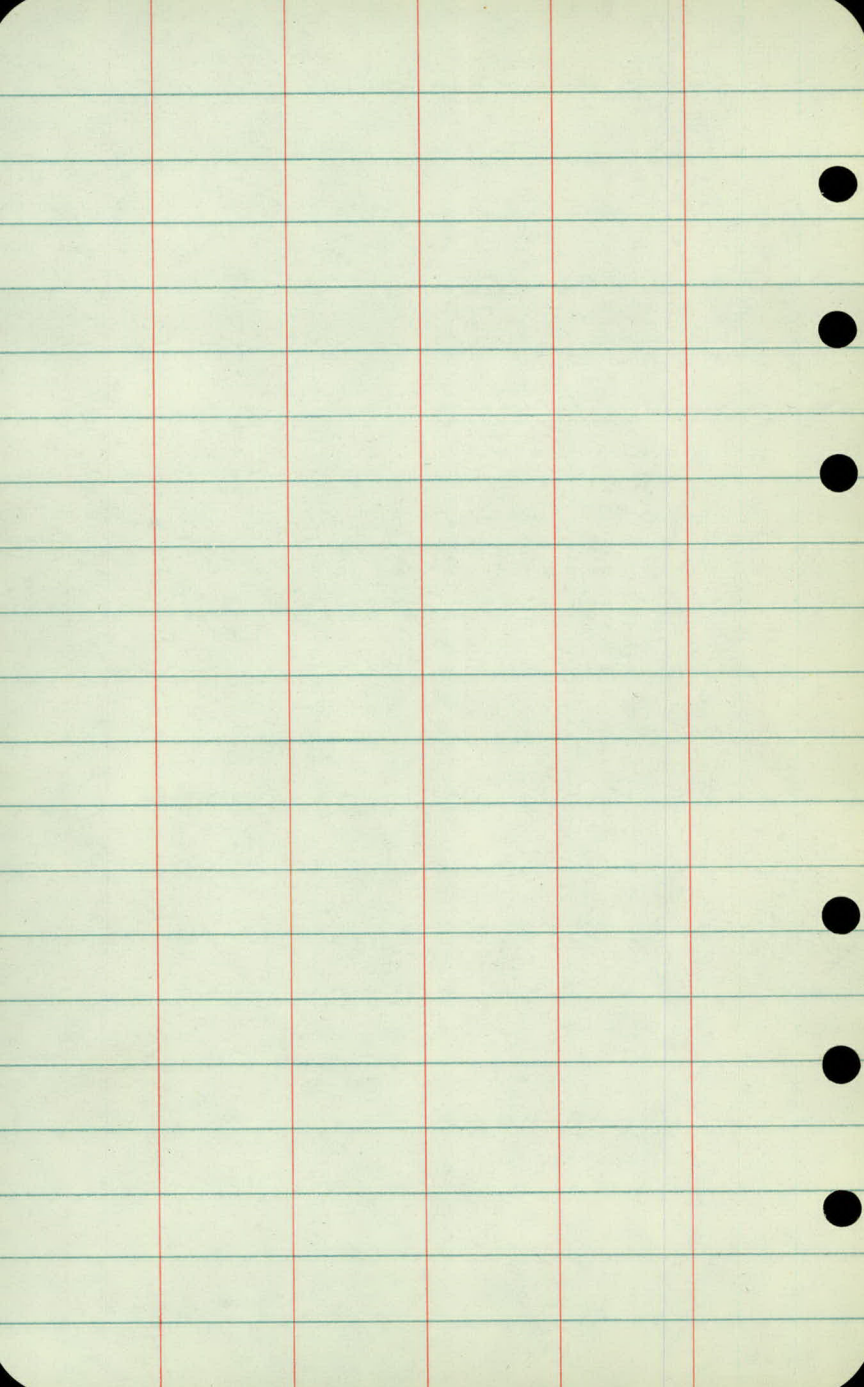
51.9	51.8	53.1	53.5	53.4	53.7	53.5	53.4
5.5	5.6	4.3	3.9	4.0	3.7	3.9	4.0
	2	4	16	25	39	51	80

	56.1	55.3	55.1	54.5	51.5	51.3
	1.30	2.1	2.3	2.9	5.9	6.1
Garage Apron	Bldg	137	115	107	98	86
	176					

52.6	54.2	54.4	54.6	54.4	52.3	52.3	52.3
4.8	3.2	3.0	2.8	3.0	5.1	5.1	5.1
	4	11	51	79	85	90	98

	55.3	55.0	54.6
L.O	2.1	2.4	2.8
	143	121	108

N.W. Cor Bottom step 1644 W Larpenteur



FK
KP
JH
HA

March 30, 1959 a

Low Spot Location

Crack at Cleveland

W	10'	E	10'	E
52.5		52.5		53'

Sta	+	π	-	Elev	
BM	3.60	954.55		950.95	Capped Iron
200' RT			4.9		
218' "			5.48		
220			5.58		
222			5.65 ✓	48.9	
223			5.60		
225			5.58		
227			5.64 ✓	48.9	
229			5.60		
231			5.65 ✓	48.9	
232			5.60		
233			5.55		
235			5.40		
237			5.36		

Take Your Pick

Larpenteur 59-30

Fence around school all Conc

Conc Corners only of U. of Minn. 2 + 2
+ Braces

Sta 59 to 60

1 in Conc south 1
2 in Conc North + 2 brace 2 2

Sta 66 +

2 Fe posts at Gate + Braces 2

Sta 71 + Post + Brace in Conc 1 1

Sta 75 + 90 2 Gate post in Conc 2 2
+ 2 Braces

Sta 77 + 50 Post + 2 Braces 1 2

Sta 79 + 50 2th Corner post + 2 braces 1 2

6

2 + 2

Sta 82+80 2 Gatepost & Braces

2 1

Sta 88+08 Post & Brace

Rt 1 2

Sta 92+ $\frac{1}{4}$ Post & 2 Braces

1 2

Sta 93+50 Post & 2 Braces

1 2

95 + ?

Post & 2 Braces

19 20

Post Braces

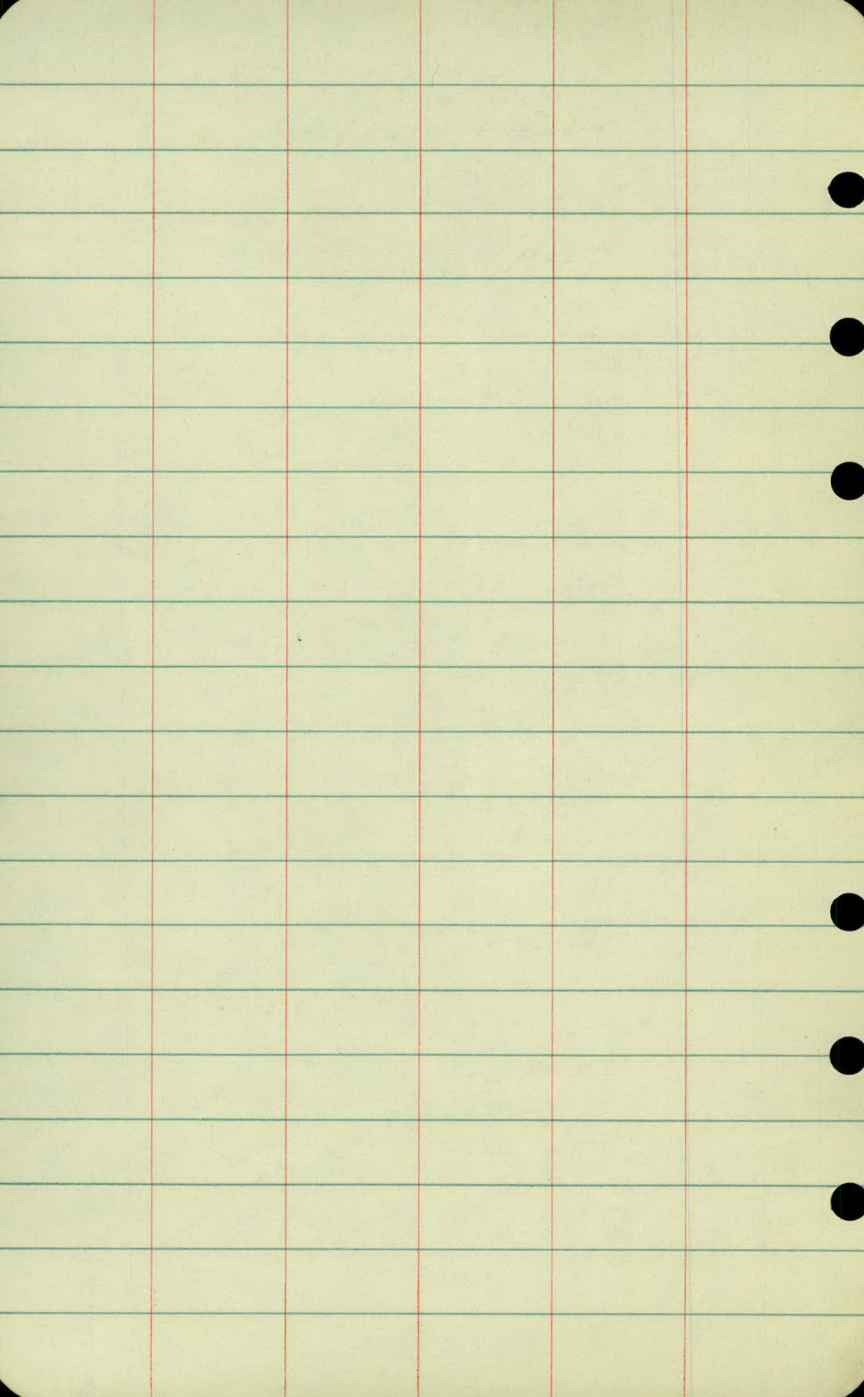
Sta 56+15 MH 33' Lt 3 $\frac{1}{2}$ " O.D.

Pipe

Pipe West + South

Sta 62+20 MH 30' Lt.

2 $\frac{5}{8}$ " OD In from North1 $\frac{7}{16}$ " OD out to East



March 25, 1959

a

One X-section of
Parking Area

Sta	+	π	-	Elev
-----	---	-------	---	------

BM	1.67	958.92		
----	------	--------	--	--

952.25

0+15

✓

4+00

7.1 5.1.8 £

£

March 25, 1959

6

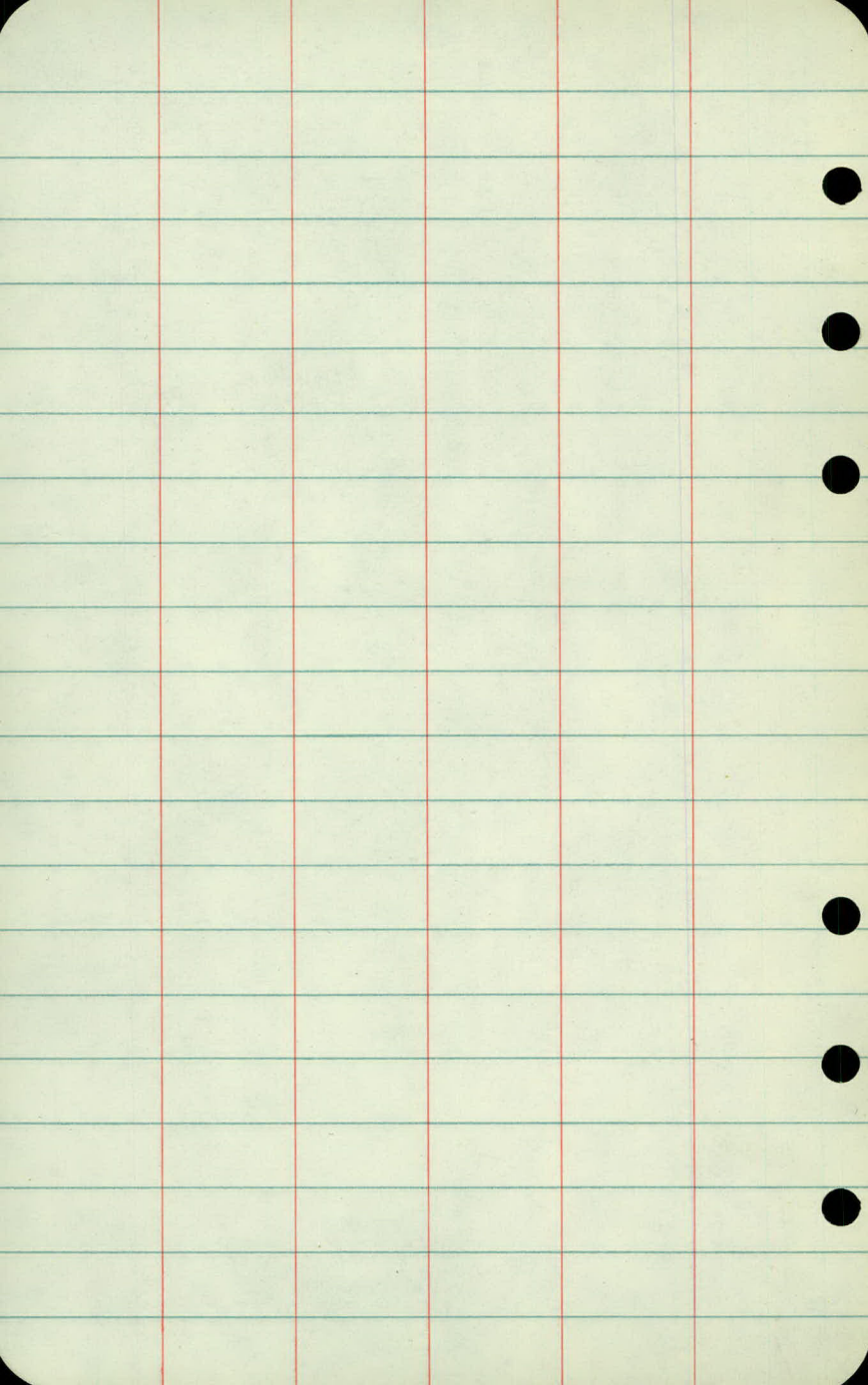
BT

51.2 51.1 51.0 51.4 51.6 51.8 51.9

7.7 7.8 7.9 7.5 7.3 7.5 8.0
11 27 50 67 92 100

49.4 49.3 48.6 46.9 49.4 49.8 50.1 50.7

9.5 9.6 10.1 10.0 9.5 9.1 8.8 8.2
250 243 231 219 200 184 157 129



X- Sections

Sta + π - Elev

BM 2.21 959.46

957.25

96

380

+28

✓

+30 Ent at Herdwall

✓

FK
AB
JH

Lt

Nov. 19, 1958

22

Rt

Top N.W. Cor ^{Top} Step 1644 W Carpenter

55.6 ✓
380

54.3

54.6

55.2

55.6

55.6

55.5

55.2

52.3

51.6

52.3

5.2 4.9 4.3 3.9 3.9 4.0 4.3 2.2 7.8 5.2
50 34 23 10 10 21 28 28.5 30

FL 36 CM

54.5

5.0
60

52.3

53.2

53.7

7.2 6.3 5.8
60 41 34

54.3

55.0

55.3

55.6

55.6

55.5

55.3

55.2

54.9

54.4

5.2 4.5 4.2 3.9 3.9 4.0 4.2 4.3 4.6 5.1
38 27 20 10 10 21 28 33 41

54.5

54.8

53.7

53.9

5.0 4.7
50 60

5.8
60

5.6
56

Sta + π - Elev

959.46

96+44 $\pm$ Ditch Left

✓

+49 Shoulder Left

+53 Ent Rt at Headwall

+54 Ditch at Headwall

Nov. 19, 1958

23

LT

RT

II

53.6

55.5

55.4

55.5

55.5

~~55.4~~

55.4

54.7

54.5

54.2

5.9 4.0 4.1 4.0 4.0 4.1 4.1 4.8 5.0 5.3
27 24 19 10 10 21 40 50 60

52.75

53.3

54.0

54.2

54.4

~~55.5~~

6.71 6.2 5.5 5.3 5.1
FL 31 33 50 60
15 CM
28

55.0

55.1

55.3

55.4

55.5

55.5

~~55.4~~

55.3

54.9

54.2

54.0

4.5 4.4 4.2 4.1 4.0 4.0 4.1 4.2 4.6 5.3 5.5
60 55 40 25 10 10 21 37 53 60

55.3

55.4

55.5

55.6

55.5

55.5

~~55.4~~

55.2

54.6

54.5

54.0

4.2 4.1 4.0 3.9 4.0 4.0 4.1 4.3 4.9 5.0 5.5
60 50 42 25 10 10 22 35 46 60

~~55.5~~

55.4

55.2

52.8

51.38

Duplicate 45361

4.0 4.1 4.3 6.7 8.08
10 21 26 FL 36 CM
28.5

~~55.5~~

54.0

54.2

54.5

52.3

5.5 5.3 5.0 7.2
60 54 43 38

Sta + π - Elev

959.46

96+68 $\pm$ Fry

✓

+83 E. Shoulder Fry

✓

+88

✓

✓

Nov 19, 1958

24

Lt

Rt

54.66

55.21

55.7

55.4

55.4

55.3

54.9

54.91

53.0

4.80

4.25

3.8

4.1

4.1

4.2

4.6

4.55

6.5

Top MH

Top MH

27

10

10

20

MH

34

38.5

27.5

2.5

55.6

55.6

55.5

55.8

56.3

54.4

54.6

54.5

52.4

3.9

3.9

4.0

3.7

3.3

5.1

4.9

5.0

7.1

50

60

100

150

200

60

30

45

41

55.3

55.4

55.5

55.4

55.4

55.2

54.8

54.3

52.7

4.2

4.1

4.0

4.1

4.1

4.3

4.7

5.2

6.8

52

39

24

10

10

20

26

33

55.3

54.6

54.5

52.4

4.2

4.9

5.0

7.1

60

60

46

40

53.3

55.4

55.2

55.3

55.4

55.2

54.7

54.0

52.5

6.2

4.1

4.3

4.2

4.1

4.3

4.8

5.5

7.0

28

26

22

10

10

21

27

34

53.06

53.3

54.4

54.9

54.6

54.6

52.5

6.40

6.2

5.1

4.6

4.9

4.9

7.0

28

29

30

45

60

49

43

FL 15"CM

54.4

54.7

5.1

4.8

60

53

Sta + π - Elev

959.46

97

✓

+10

✓

+15

Nov. 19, 1958

25

LT

RT

53.9	53.9	54.9	55.3	55.4	55.2	54.7	53.5	52.4	52.3
5.6	5.6	4.6	4.2	4.1	4.3	4.8	6.0	7.1	7.2
30	29	24	10		10	21	26	34	43

54.2		54.0	54.3	54.5		54.2		54.5	54.5
5.3	5.5	5.2	5.0			5.3	5.0	5.0	
34	47	64	70			70	62	49	

54.1	54.1	54.9	55.2	55.3	55.2	54.7	53.3	52.3	
5.4	5.4	4.6	4.3	4.2	4.3	4.8	6.2	7.2	
29	27	20	10		10	21	26	33	

54.5	54.2	54.3	54.5			54.0	54.2	54.3	52.2
5.0	5.3	5.2	5.0			5.5	5.3	5.2	7.3
30	43	58	70			70	63	51	44

54.4	54.0	55.0	55.2	55.3	55.1	54.7	53.2	52.2	
5.1	5.5	4.5	4.3	4.2	4.4	4.8	6.3	7.2	
28	27	18	10		10	21	25	33	

54.1	54.3	54.5				51.0	51.5	51.9	52.1
5.4	5.2	5.0				8.5	8.0	7.6	7.4
47	66	70				120	84	65	48

Sta + π - Elev

959.46

97 + 23

✓

+ 33

✓

+ 54

Nov 19, 1958

26

Lt

Rt

54.4	54.2	55.1	55.1	55.2	55.1	54.7	52.7	52.2
5.1	5.3	4.4	4.4	4.3	4.4	4.8	6.8	7.3
27	26	13	10		10	21	27	38

54.3	54.1	54.3				51.7	51.9
5.2	5.4	5.2				7.8	7.6
43	63	70				70	58

54.6	54.2	54.9	55.1	55.2	55.1	54.7	52.6	52.2
4.9	5.3	4.6	4.4	4.3	4.4	4.8	6.9	7.3
26	25	16	10		10	21	28	34

54.2	54.4	54.2	54.1		54.9	54.9	54.1	52.1
5.3	5.1	5.3	5.4		4.6	4.6	5.4	7.4
27	39	55	70		70	56	46	41

54.8	54.3	54.9	55.1	55.0	55.0	54.8	52.9	52.16
4.7	5.2	4.6	4.4	4.35	4.5	4.7	6.6	7.30
26	25	16	10		10	24	28	FL15°CN 27

54.4	54.2	54.1	54.5	55.3	55.2	54.8	52.8
5.1	5.3	5.4	5.0		4.2	4.3	4.7
27	43	60	70		70	65	46

Sta + π - Elev

959.46

57

97+57

✓

98

✓

+ 07

✓

TP 4.86 960.48 3.84 955.62

Nov. 19, 1958

27

LT

RT

54.8	54.3	54.9	55.0	55.1	55.0	54.9	54.9	55.3
4.7	5.2	4.6	4.5	4.4	4.5	4.6	4.6	4.2
26	25	15	10		10	28	45	66

54.5	54.2	54.1	54.3			55.3
5.0	5.3	5.4	5.2			4.2
27	43	62	70			70

55.0	54.5	54.9	55.1	55.2	55.1	55.5	55.9	56.0
4.5	5.0	4.6	4.4	4.3	4.4	4.0	3.6	3.5
25	24	15	10		10	32	50	70

54.5	54.8	54.2	54.2		
5.0	4.7	5.3	5.3		
26	38	50	70		

55.0	54.5	54.9	55.1	55.2	55.0	55.50	55.98	56.26
4.5	5.0	4.6	4.4	4.3	4.5	3.96	3.48	3.20
25	24	16	10		10	33	56	77
						Comp		Blodg.

54.5	54.9	54.1	54.1		
5.0	4.6	5.4	5.4		
26	37	51	70		

Sta + π - Elev

960.48

98+40

✓

+52

✓

+60

+67

Nov. 19, 1958

28

RT

55.2 54.6 54.9 55.0 55.2 55.1 55.0 55.62 55.90

5.3 5.9 5.6 5.5 5.3 5.4 5.5 4.86 4.58
26 24 17 10 10 20 34 53

Conc

54.9 55.2 54.7 54.7

5.6 5.3 5.8 5.8
27 37 52 70

56.30
4.18
Blg

54.8 55.0 55.4 54.7 55.0 55.2 55.1 55.0 55.0 55.63

5.7 5.5 5.1 5.8 5.5 5.3 5.4 5.5 5.5 7.85
45 27 25 24 10 10 20 GE FL 18" CM

28 29

55.0 55.3

5.5 5.2
62 70

55.7 55.5 55.5
4.8 5.0 5.0
20 60 36

55.26
5.42
Top MH
24

55.3 55.1 55.4 54.7 55.1 55.2 55.2 55.0 54.2 53.8

5.2 5.4 5.1 5.8 5.4 5.25 5.3 5.5 6.3 6.7
45 27 26 24 10 10 22 30 31

55.1 55.3

5.4 5.2
65 70

54.5 54.2 54.0
6.0 6.3 6.5
70 50 35

Sta + π - Elev

960.48

99

✓

TP 3.23 960.48 3.23 957.25

BM 4.02 960.75 3.75 956.73 (956.73)

+10

✓

+50

FK
RG
AB
JH

Nov 18, 1958
Dec. 2, 1958

29

LX

RT

55.1	55.7	54.8	55.2	55.4	55.3	54.9	55.3	55.4
54	5.1	5.7	5.3	5.1	5.2	5.6	5.2	5.1
26	25	24	10		10	22	22	27

55.5	55.5	55.4	55.6	55.5	54.58	54.28	54.13
50	5.0	5.1	4.9	✓	5.90	6.20	6.35
36	50	60	70		70	50	33
							BT

N.W. Cor Lower step 1644 W Larp

55.3	55.6	55.0	55.3	55.5	55.5	55.0	54.7	55.21
5.5	5.2	5.8	5.5	5.3	5.3	5.8	6.1	5.54
26	25	24	10		10	22	G	C

55.7	55.6	55.6	55.07	54.6	54.1	55.08	54.4
5.1	5.2	5.2	5.68	6.2	6.4	5.67	6.4
36	50	60	90	53	46	C	G

55.9	55.6	55.0	55.4	55.5	55.5	55.2	54.7	54.8
4.9	5.2	5.8	5.4	5.3	5.3	5.6	6.1	6.0
37	26	25	12		10	22	32	50

56.1	56.2	55.37	54.83
4.7	4.6	5.38	5.92
50	60	P. Island	57
		57	

Sta + π - Elev.

960.75

99+89

✓

100

✓

+05 Top MH 39' Lt.

5.37 955.38

+08?

+15

+19

Dec. 2, 1958

30

55.72	55.3	55.3	55.5	55.6	55.7	55.1	55.65
5.03	5.5	5.5	5.3	5.2	5.1	5.7	5.10
C	G	27	10		12	G	C
37						33	
55.4	54.87	55.8	56.22	55.20	55.0	55.48	55.0
5.4	5.88	50-4.53	5.55	5.55	5.8	5.27	5.8
G	C	G C		90	50	C	G
50		76	Apron			40	
55.6	55.5	55.2	55.5	55.7	55.3	55.68	55.83
5.2	5.3	5.6	5.3	5.14	5.1	5.5	5.07
50	39	25	14	54	12	G C	28.5
						22	Walk
56.3	57.1	57.9		55.27	55.1	55.2	55.65
4.5	3.7	2.9		5.48	5.7	5.6	5.10
100	150	200		90	72	41	C
				Apron			41
55.79	55.4	55.1	55.6	55.7	55.6	55.3	55.64
4.96	5.4	5.7	5.2	5.1	5.2	5.5	5.11
C	G	29	9		15	G	9
41						22	Walk
55.8	56.22				56.4	56.2	56.0
50	4.53				4.4	4.6	4.8
G	C				72	65	44
72							36

Sta + π - Elev

960.75

100+50

✓

101

✓

TP 4.80 961.63 3.92 956.83

+50

✓

2 Dec 2, 1958

31

Lt

R

55.8	55.8	55.5	55.6	55.7	55.7	55.3	55.73
5.0	4.88	5.3	5.2	5.05	5.1	5.5	5.02
32	C	22	10		10	G	C
	23					22	

56.0	55.5			57.1	56.6	56.3	55.84
4.8	4.3			37	4.2	4.5	4.91
48	72			78	82?	48	28.5
					62?		W/LK

56.0	56.11	55.7	55.8	55.9	55.8	55.5	55.82	55.96
4.8	4.64	5.1	5.0	4.87	5.0	5.3	4.93	4.79
33	23	22	12		10	G	C	28.5
	C					22		W/LK

56.4	57.0			57.4	57.2	57.1	56.9
4.4	3.8			3.4	3.6	3.7	3.9
48	72			77	72	57	41

56.9	56.4	56.2	56.7	55.8	55.9	55.4	55.96	56.05
4.7	5.2	5.4	5.9	5.8	5.7	6.2	5.67	5.58
A5	39	24	23	10	10	G	C	28.5
						22		W/LK

57.5				57.7	57.7	57.3	56.9
4.1				39	3.9	4.3	4.7
72				77	72	48	34

Sta + π - Elev

961.63

102

✓

+50

✓

957.01

+56 Top MH Lt. 39' Lt 4.62

103

Dec 2, 1958

32

LT

RT

56.3

56.31

56.0

55.8

55.9

55.8

55.6

56.11

56.15

5.3

5.32

5.6

5.8

5.70

5.8

6.0

5.52

5.48

34

23

22

11

10

G

C

28.5

C

22

Walk

57.1

57.4

58.0

58.0

57.8

57.4

4.5

4.2

3.6

3.6

3.8

4.2

50

72

72

64

52

34

56.7

56.35

55.8

55.9

56.0

56.1

55.7

56.11

56.19

4.9

5.28

5.8

5.7

5.6

5.5

5.6

5.52

5.44

36

C

22

10

10

C

22

28

23

Walk

57.1

57.4

58.1

57.8

57.6

57.4

4.5

4.2

3.5

3.8

4.0

4.2

47

72

72

62

49

34

56.5

56.53

56.1

56.0

56.1

56.1

55.8

56.27

56.38

5.1

5.10

5.5

5.6

5.46

5.5

5.8

5.36

5.25

36

C

23

12

10

G

C

28.5

23

G

22

Walk

57.1

57.3

57.8

57.5

57.4

4.5

4.3

3.8

3.9

4.2

59

72

77

50

34

Sta + π - Elev

961.63

103 + 50

✓

T.P. 4.20 962.09 3.74 957.89

104

✓

+ 10.8

57.40

4.69

57.31

+ 26.2

4.78

+ 50 in Ent 41

Dec 2, 1958

33

Lt

Rt

✱

56.7	56.37	55.9	56.2	56.4	56.3	55.9	56.37	56.60
4.9	5.26	5.7	5.4	5.2	5.3	5.7	5.26	5.03
37	C	G	10		11	G	C	28
	22.5					22		Walk
57.3	57.4				57.7	57.7	57.6	57.4
4.3	4.2				3.9	3.9	4.0	4.2
50	69				72	67	50	36

56.4	56.6	56.14	56.2	56.5	56.2	56.1	56.45	56.60
5.7	5.5	5.95	5.9	5.63	5.9	6.0	5.64	5.49
32	C	G	11		11	G	C	28.5
	22					22		Walk
56.6	57.4	57.5			57.6	57.5	57.4	57.3
5.5	4.7	4.6			4.5	4.6	4.7	4.8
40	50	72			72	64	50	34

SW Cor Conc slab

SE Cor Conc slab

57.0	56.7	56.2	56.4	56.6	56.4	56.0	56.49	56.65
5.1	5.4	5.9	5.7	5.5	5.7	6.1	5.60	5.49
50	38	23	10		10	G	C	28.5
						22		Walk
57.3	57.4				57.7	57.8	57.9	57.1
4.8	4.7				5.4	5.3	5.2	5.0
65	82				72	62	51	35

Sta + π - Elev

962.09

⁸⁵
104 + ~~35~~ W.P.L. Snelling
104 + 85 ^{2nd} π

✓

BM 4.03 958.06 (958.05)

BM 5.83 986.29 (980.46)

50+00

+50

Dec 2, 1958

34

Lt

Rt

56.76	56.3	56.6	56.6	56.4	56.1	56.26	56.64
5.33	5.8	5.5	5.5	5.7	6.0	5.53	5.45
<u>6</u>	<u>6</u>	11		12	<u>6</u>	<u>6</u>	30
22					23		Walt

57.2	57.2	57.1	56.8	56.7	56.32	56.6	56.6	56.7
4.9	4.9	5.0	5.3	5.4	5.77	5.5	5.5	5.4
35	53	58	61	72	70	62	50	43
					Walt			

Top Hyd Rt sta 105+57

Top Mont at Cleveland + Carpenter

81.9	81.9	83.5	83.6	83.72	83.6	83.2	82.0	81.9
44	44	28	2.7	2.57	2.7	3.1	4.3	4.4
29	25	20	10		10	20	27	30

84.1	84.5	84.1	84.4	81.6	82.1	82.1	82.9	83.0
2.2	1.7	2.2	1.9	4.7	4.2	4.2	3.4	3.3
33	40	58	70	70	55	42	38	34

84.1	81.3	81.3	82.9	83.2	83.3	83.1	82.8	81.3	81.4	82.0
22	50	50	34	3.1	3.0	3.2	3.5	5.0	4.9	3.3
32	27	25	21	11		11	21	27	31	33

84.2	84.0	84.0	84.0	81.5	81.8	81.9	83.1
2.1	2.3	2.3	2.3	4.8	4.5	4.4	3.2
34	42	54	70	70	57	43	38

Sta + π - Elev.

986.29

51

✓

+50

52

Dec 3, 1958

35

RT

80.9

11

80.9

82.5

82.6

82.8

80

82.6

82.1

80.9

81.0

82.6

54

54

38

37

3.51

3.7

4.2

5.4

5.3

3.2

30

26

21

10

12

21

30

32

35

83.2

83.2

83.1

83.1

80.9

81.1

81.6

3.1

3.1

3.2

3.2

5.4

5.2

4.7

35

42

57

70

70

53

45

80.3

80.3

82.1

82.0

82.4

81.9

81.6

80.3

80.3

6.0

6.0

4.2

4.3

4.15

4.4

4.7

6.0

6.0

29

27

20

10

12

22

27

31

82.5

82.3

82.4

82.5

80.3

80.7

81.4

81.9

3.8

4.0

3.9

3.8

6.0

5.6

4.9

4.4

35

44

58

70

70

56

41

34

79.4

81.6

81.6

81.5

81.5

81.5

81.5

80.4

79.6

6.9

4.7

4.7

4.8

4.66

4.8

4.8

5.9

6.7

27

20

17

10

11

21

26

28

79.5

81.5

81.9

81.6

79.3

80.0

80.8

81.1

79.5

6.8

4.8

4.4

4.7

7.0

6.3

5.5

5.2

6.8

29

32

35

44

70

58

43

34

32

81.7

81.7

4.6

4.6

59

Sta + π - Elev

64

986.29

52+42

✓

+52

✓

+58

2 Dec 3, 1958

36

LT

RT

79.5

80.6

80.8

81.0

81.3

81.1

80.8

80.6

79.5

79.3

6.8

5.7

5.5

5.3

5.0

5.2

5.5

5.7

6.8

7.0

28

24

19

11

11

21

26

28

30

79.5

81.1

81.3

80.9

81.1

79.2

80.0

80.4

80.8

6.8

5.2

5.0

5.4

5.2

7.1

6.3

5.9

5.5

30

35

42

61

70

70

54

43

34

81.0

80.7

80.4

80.6

80.8

81.1

81.0

80.7

80.6

80.8

5.3

5.6

5.9

5.7

5.5

5.2

5.3

5.6

5.7

5.5

44

30

27

19

12

10

22

32

42

80.7

80.9

79.6

80.1

5.6

5.4

6.7

6.2

58

70

70

56

80.1

80.3

80.5

80.8

81.1

80.9

80.6

80.3

80.2

79.1

6.2

6.0

5.8

5.5

5.2

5.4

5.7

6.0

6.1

7.2

49

32

19

11

12

21

33

41

43

80.0

80.0

78.7

79.0

6.3

6.3

7.6

7.3

61

70

70

63

Sta + π - Elev

+15
+29

986.29

52+60 Shoulder Cleveland So

+64 shoulder Cleveland No 980.70

+ Top MH

5.59

+81.83 $\neq$ Cleveland

53+00 Shoulder

+07 Ditch Line

+15 Property Line

TP

0.99 981.23

6.05 980.24

Dec 3, 1958

37

Lt

81

Duplicate + 60

81.0	80.8	80.5	80.1	79.9	79.6
5.3	5.5	5.8	6.2	6.4	6.7
	11	21	39	55	70

80.7	80.5	80.5	80.5	80.8	81.0
5.6	5.8	5.8	5.8	5.5	5.3
70	52	32	20	10	

Duplicate + 60

Top

81.6	81.3	81.0	80.9	80.7	80.7	80.5	80.29	80.81	79.20
4.7	5.0	5.3	5.4	5.6	5.6	5.8	6.00	6.28	7.09
150	100	50	42	19	11	10	21	50	100

80.8	80.8	80.6	80.4	79.5	80.3	80.4	80.3	80.1	79.9	79.7	79.4
5.5	5.5	5.7	5.9	6.8	6.0	5.9	6.0	6.2	6.4	6.7	6.9
70	65	51	34	20	10		10	22	38	56	70

79.9	80.1	79.6	80.0	80.1	80.1	80.2	80.2	80.1	80.0	79.5	79.9	78.5
6.4	6.2	6.7	6.3	6.2	6.2	6.1	6.1	6.2	6.3	6.8	7.4	7.8
70	52	36	35	23	11		10	20	37	38	55	70

79.9	79.1	79.6	79.7	79.9	80.1	80.0	79.8	79.6	79.3	78.6	78.6
6.4	7.2	6.7	6.6	6.4	6.2	6.3	6.5	6.7	7.0	7.7	7.7
36	31	27	22	11		10	23	32	43	58	70

79.8	79.8	79.8
6.5	6.5	6.5
4.8	6.2	7.0

Sta + π - Elev

981.23

53+29

✓

+50

✓

53+98 Top All H 17' RT

8.78
2.45

54

Dec. 3, 1958

38

L1

R1

78.0	78.0	79.6	79.7	79.9	79.7	79.6	78.3	78.2	78.7
32	32	16	15	13	15	16	29	30	25
31	27	22	10		10	22	29	31	34

79.0	79.0	78.6	78.7			78.4	78.4	78.2
22	22	26	25			28	28	30
34	46	59	70			70	60	39

77.3	77.2	77.7	79.4	79.4	79.6	79.4	79.1	77.6	77.5	77.7
39	40	35	18	18	16	18	21	36	37	35
31	29	25	21	10		10	22	27	30	34

78.0	78.6	78.2	78.3			77.6	77.4	77.2	77.2	77.2
32	26	30	29			36	38	40	40	
34	37	51	70			70	66	48	36	

77.2	76.7	77.2	78.7	78.9	79.0	78.8	78.5	76.8	76.8	76.5
40	45	40	25	23	22	24	27	44	44	47
34	32	24	21	9		10	22	29	34	39

77.6	77.7	77.8	78.2				76.5	76.6
36	35	34	30				47	46
35	44	51	70				70	50

Sta	+	π	-	Elev
-----	---	-------	---	------

		981.23		
--	--	--------	--	--

54+50				
-------	--	--	--	--

✓				
---	--	--	--	--

55				
----	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

Dec. 3, 1958

39

Lt

Rt

76.2	76.4	76.4	78.2	78.4	78.5	78.3	78.0	76.2	76.2	75.9
50	48	48	30	28	27	29	3.2	5.0	5.0	5.3
29	32	25	21	10		11	21	27	34	39

76.7	77.2	77.2	77.6	77.8			75.7	75.6	76.1	
45	40	4.0	36	34			5.5	5.6	5.1	
34	35	46	51	20			70	63	51	

76.0	75.8	76.1	77.7	78.0	78.10	77.8	77.6	75.6	75.8	75.4
52	54	5.1	3.5	3.2	3.12	3.4	3.6	5.6	5.4	5.8
32	28	25	21	10		11	21	29	33	39

76.4	76.7	76.7	77.1	77.2			75.3	75.4	75.4	
4.8	4.5	4.5	4.1	4.0			5.9	5.8	5.8	
34	35	45	63	70			70	66	50	

75.9	75.5	75.7	77.3	77.5	77.9	77.5	77.2	75.2	75.5	75.2
5.3	5.7	5.5	3.9	3.7	3.5	3.7	4.0	6.0	5.7	6.0
34	29	26	21	10		10	21	28	33	37

76.3	76.2	76.3	76.7				75.0	75.0	75.3	
4.9	5.0	4.9	4.5				6.2	6.2	5.9	
35	45	60	70				70	61	42	

Sta + π - Elev

981.23

56

✓

76.66

+ Top MH 33' 4.57

TP 3.37 980.03 4.57 976.66

+50

✓

57

FK
XP
JH

Dec. 3, 1958

Dec 22, 1958

40

LT

BT

75.7	75.6	75.7	77.3	77.3	77.4	77.2	77.1	75.1	75.5	75.2
55	56	55	39	39	3.81	40	41	61	5.7	6.0
34	29	26	20	10		10	20	28	33	36

76.1	75.9	76.2	76.3				74.6	74.6	75.1
51	53	50	49				66	66	61
35	47	61	70				70	67	51

75.5	75.5	76.9	77.1	77.2	77.3	77.1	76.8	76.7	76.2	75.2
45	45	3.1	29	28	2.7	2.9	3.2	3.3	3.8	4.8
32	26	21	18	10		10	18	21	23	27

75.8	75.9	75.8	76.1	76.2	76.3	76.2	76.3	76.6	75.3
42	41	42	39	38	3.7	5.8	5.7	5.2	5.4
33	36	48	50	63	70	70	53	41	39

75.9	75.6	76.8	77.0	77.1	77.2	77.0	76.7	76.6	75.1	75.0
47	44	32	30	29	2.80	3.0	3.3	3.4	4.9	5.0
29	25	21	18	10		10	16	21	26	33

75.8	75.9	76.0	76.2			76.1	76.2	76.8	76.8
42	41	40	3.8			5.9	5.8	5.2	5.2
33	44	52	70			70	66	48	36

Sta + π - Elev

980,03

57+50

58

+50

+56

76.52
3.51

Dec. 22, 1958 41

Lt

Rt

75.3	76.1	76.9	77.1	77.2	76.9	76.7	76.6	75.0	75.1
4.7	3.3	3.1	2.9	2.8	3.1	3.3	3.4	5.0	4.9
25	21	13	10		10	13	21	27	32

75.0	75.6	75.9	75.7	75.8	76.2	74.0	73.9	74.7	74.9	75.2
5.0	4.4	4.1	4.3	4.2	3.8	6.0	6.1	5.3	5.1	4.8
30	33	45	49	61	70	70	54	48	40	33

75.2	76.7	76.8	77.0	77.5	76.9	76.5	76.6	76.0	75.0
4.8	3.3	3.2	3.0	2.88	3.1	3.5	3.4	4.0	5.0
25	21	15	10		10	17	21	24	27

74.9	75.8	75.9	75.8	75.6	76.0	76.2	74.1	74.2	74.8	74.8	75.4	75.1
5.1	4.2	4.1	4.2	4.4	4.0	3.8	5.9	5.8	5.2	5.2	4.6	4.9
29	33	39	44	48	51	70	70	54	49	39	33	32

74.6	74.8	76.5	76.7	76.9	77.0	76.8	76.2	76.2	75.3
5.4	5.2	3.5	3.3	3.1	3.00	3.2	3.7	3.8	4.7
28	25	21	14	10		10	17	22	25

74.8	75.7	75.8	75.5	76.0	74.4	74.4	75.0	75.0	75.6	75.3
5.2	4.3	4.2	4.5	4.0	5.6	5.6	5.0	5.0	4.9	4.7
31	34	40	48	70	70	56	50	37	33	31

MH 17 RT

Sta	+	π	-	Elev
		980.03		

59

✓

+50

✓

60

TP	2.71	980.65	7.09	972.94
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Dec 22, 1958

42

Lt.

Rt.

74.5 76.2 76.4 76.6 76.8 ✓ 76.6 76.1 75.6 74.5
 55 38 36 34 3.22 3.4 39 44 55
 25 21 16 10 10 15 22 27

74.2 75.4 75.6 75.3 75.6 75.8 ✓ 73.9 74.1 74.0 73.8 74.2 74.6
 5.8 4.6 4.4 4.7 4.4 4.2 6.1 5.9 6.0 6.2 5.8 5.4
 31 34 40 48 55 70 70 60 47 41 38 33

76.5 74.2 74.3 76.1 76.2 76.4 ✓ 76.2 76.0 75.8 74.5 73.6
 4.5 5.6 5.7 3.9 3.8 3.6 3.8 4.0 4.2 5.5 6.4
 34 31 25 20 10 10 17 22 27 33

75.4 75.4 75.7 75.6 72.3 72.3 72.7 72.8 72.9
 4.6 4.6 4.3 4.4 ✓ 7.7 7.7 7.3 7.2 7.09
 42 52 68 70 70 56 53 38 Top 5.4
 35

73.7 75.7 76.1 76.2 76.3 ✓ 76.0 75.8 75.6 75.4 74.3
 6.3 4.3 3.9 3.8 3.7 4.0 4.2 4.4 4.6 5.7
 27 23 16 10 10 14 18 23 26

73.8 75.7 75.7 75.4 76.1 72.1 72.5 72.9 72.7 73.4 73.8
 6.2 4.3 4.3 4.1 3.9 7.7 7.5 7.1 7.3 6.6 6.2
 29 34 42 55 70 70 58 52 39 34 33

Top S.D. Rt Sta 59+50

Sta + π - Elev

980.65

60+50

✓

61

✓

+50

FK
RG
KP
JH

Dec 22, 1958

43

LT

£

BT

75.5 74.1 74.0 75.8 76.1 76.0 75.8 75.7 75.7 75.1
52 6.6 6.7 4.9 4.6 4.53 47 49 50 50 56
34 30 25 21 10 10 14 16 21 24

75.6 75.5 75.6 72.2 72.9 73.2 73.5 73.9 74.1 74.2
5.1 5.2 5.1 85 7.8 7.4 7.2 6.8 6.4 6.6 6.5
44 63 70 70 54 52 41 35 33 32 27

74.1 74.1 75.7 75.9 75.9 75.9 75.9 75.4 75.3 73.9 74.1
6.6 6.6 5.0 4.8 4.8 4.67 4.8 5.3 5.4 6.8 6.6
29 24 21 14 10 10 17 22 27 33

75.6 75.6 75.6 75.6 73.0 72.9 73.9 73.7 73.6
5.1 5.1 5.1 5.1 77 7.8 7.3 7.0 7.1
33 40 55 70 70 55 51 44 37

76.1 74.0 73.7 75.7 75.9 76.0 75.8 75.4 75.2 73.9 74.1
4.6 6.7 7.0 5.0 4.8 4.65 4.9 5.3 5.5 6.8 6.6
32 29 26 22 10 10 16 22 27 33

75.6 75.4 75.5 73.0 73.0 73.5 73.6 73.7
5.1 5.3 5.2 7.7 7.7 7.2 7.1 7.0
34 48 70 70 56 52 47 36

Sta + π - Elev

980.65

6.2

✓

+ 50

✓

6.3

75.71

+ 17

7.94

Dec. 22, 1958

44

Lt

£

Rt

73.9

73.9

75.8

75.9

76.0

75.9

75.5

75.5

74.0

74.0

6.8

6.8

4.9

4.8

4.6

4.8

5.2

5.2

6.7

6.7

31

26

21

10

10

16

21

28

30

75.5

75.8

75.7

75.6

75.7

75.1

75.7

75.8

74.0

74.1

74.4

52

4.9

5.0

5.1

5.0

7.6

7.4

7.0

6.9

6.7

34

40

43

63

70

70

63

51

41

39

36

33

74.7

72.9

74.9

75.8

76.0

76.1

76.2

75.9

75.7

75.7

74.3

74.4

60

58

4.9

4.7

4.6

4.4

4.8

5.0

5.0

6.4

32

25

20

17

10

10

15

21

27

33

75.1

75.2

75.2

75.2

75.2

73.5

73.6

73.9

73.8

74.1

74.4

56

55

5.5

5.5

7.2

7.1

6.8

6.9

6.6

34

38

52

70

70

65

53

49

38

35

74.8

75.4

75.7

76.0

76.1

76.2

76.0

75.7

75.8

75.4

74.2

5.9

5.3

5.0

4.7

4.6

4.4

4.7

5.0

4.9

5.3

6.5

24

21

19

15

10

10

15

20

23

28

74.5

74.9

74.9

74.9

74.9

73.6

73.6

73.9

73.9

74.4

74.1

6.2

5.8

5.8

5.8

5.8

5.8

7.1

7.1

6.8

6.8

6.3

6.6

28

32

38

53

70

70

57

55

37

33

32

Top M H R / 17'

Sta + π - Elev.

980.65

63+50

✓
TP 4.95 980.66 4.94 975.71

64

✓
96.99

+50

✓

2 Dec 22, 1958 45

LT

BT

75.1	75.1	75.9	76.2	76.3 ³²	76.1	75.8	75.6	74.1
5.6	5.6	4.8	4.5	4.33	4.0	4.9	5.1	6.6
31	26	21	10		10	15	21	27

74.8	74.9	75.1	75.1	73.3	73.7	73.8	74.3	74.1
5.9	5.8	5.6	5.6	7.4	7.0	6.9	6.4	6.6
34	44	58	70	70	51	40	33	32

75.6	75.6	75.5	76.1	76.2	76.4	76.4	76.3	76.0	76.0	74.3	74.2
5.1	5.1	5.2	4.6	4.5	4.3	4.23	4.4	4.7	4.7	6.4	6.5
50	35	27	20	17	10		10	16	22	28	32

75.7	77.5 ⁵²	73.8	73.8	74.0	73.9	74.4	74.5
5.0	3.14	6.9	6.9	6.7	6.8	6.3	6.2
70	House	70	65	50	38	35	33

76.7	76.5	76.5	76.7	76.7	76.6	76.3	74.5	74.6	75.3
4.0	4.2	4.2	4.0	4.0	3.94	4.1	4.4	6.2	6.1
60	53	31	20	10		10	20	28	31

76.6	74.5	74.5	74.6	74.5
4.1	6.2	6.2	6.1	6.2
70	70	59	49	39

Sta + π - Elev

980.66

64+65

✓

+84

✓

65

Dec 22, 1958

46

LT

2

RT

76.6	76.5	76.9	76.7	76.8	76.6	76.4	76.4	74.7	74.9
4.1	4.2	3.8	4.0	3.9	4.1	4.3	4.3	6.0	5.8
70	54	30	10		10	16	20	28	31

74.6	74.8	74.6	75.0	75.7
6.1	5.9	6.1	5.7	5.0
70	51	40	37	33

75.8	76.1	76.4	76.6	76.8	76.90	76.7	76.6	76.5	74.9
4.9	4.6	4.3	4.1	3.9	3.76	4.0	4.1	4.2	5.8
33	27	20	17	10		10	12	20	28

75.8	75.8
4.9	4.9
46	70

74.6	74.7	74.9	75.1	75.8	75.2
6.1	6.0	5.8	5.6	4.9	5.5
70	63	51	39	33	31

75.4	76.0	76.0	76.5	76.9	76.98	76.8	76.5	76.3	74.9	75.1
5.3	4.7	4.7	4.2	3.8	3.68	3.9	4.2	4.4	5.8	5.6
31	26	22	17	10		10	16	21	28	31

75.7	75.6	75.8
5.0	5.1	4.9
40	52	70

74.4	74.6	75.1	75.2	75.6	74.9
6.3	6.1	5.6	5.5	5.1	5.8
70	61	51	40	37	33

Sta + π - Elev.

980.66

65+50

✓

66

✓

T.P. 3.07 981.56 2.14 978.52 (978.49)

+ 31

FK
KP
JH

Lt

2 Dec 22, 1958
Dec 29, 1958

47

RT

75.3 75.3 76.5 76.9 77.0 77.1 77.0 76.7 76.7 75.0 75.1

54 54 42 38 37 35 37 40 40 5.7 5.6
36 27 20 17 10 10 16 21 28 31

75.2 75.3 75.5

55 54 5.2
42 50 70

74.5 74.8 75.0 75.2 75.5 75.7

6.2 5.9 5.7 5.5 5.2 5.0
70 53 40 36 34 33

75.1 75.0 76.4 76.9 77.1 77.1 77.0 76.7 75.0 75.0 75.9

5.6 5.7 4.3 3.8 3.6 3.5 3.7 4.0 5.7 5.7 4.8
33 28 20 16 10 10 22 27 30 33

75.3 75.3 75.4

54 54 5.3
38 58 70

74.0 74.4 74.5 75.4 75.5 76.0

6.7 6.3 6.2 5.3 5.2 4.7
70 61 51 44 39 36

Top S.W. Cor Lower Step front office Lt 67400

75.9 76.2 76.4 76.7 77.1 77.1 77.1 76.9 76.8 75.5 75.6

57 54 5.2 4.9 4.5 4.4 4.5 4.7 4.8 6.1 6.0
38 34 28 20 10 10 15 22 29 31

76.3

76.3

5.3 5.3
61 70

74.6 74.9 75.6 76.2 76.3

70 6.7 6.0 5.4 5.3
70 59 46 40 33

Sta + π - Elev

981.56

66+43

✓

BM 3.15 981.64 3.07 978.49

+70

✓

67

Dec 29, 1958

48

Lt

Rt

$\begin{matrix} 77.3 & 76.8 & 77.0 & 77.1 & 77.2 & 77.0 & 76.7 & 76.8 & 75.3 \\ 4.3 & 4.8 & 4.6 & 4.5 & 4.4 & 4.6 & 4.9 & 4.8 & 6.3 \\ 52 & 35 & 21 & 10 & & 10 & 18 & 22 & 27 \end{matrix}$

$\begin{matrix} 77.3 & 74.2 & 74.6 & 74.9 & 75.3 & 75.6 & 76.0 & 75.3 \\ 4.3 & 7.4 & 7.0 & 6.7 & 6.3 & 6.0 & 5.6 & 6.3 \\ 70 & 70 & 59 & 48 & 43 & 38 & 33 & 31 \end{matrix}$
 Top 5th Cor Lower Step office.

$\begin{matrix} 76.9 & 76.9 & 76.9 & 76.9 & 76.9 & 76.7 & 76.5 & 76.4 & 74.7 & 74.8 \\ 4.7 & 4.9 & 4.7 & 4.7 & 4.7 & 4.7 & 4.9 & 5.1 & 5.2 & 5.9 & 6.8 \\ 37 & 24 & 19 & 10 & & 10 & 15 & 22 & 28 & 31 \end{matrix}$

$\begin{matrix} 77.1 & 77.2 & 73.9 & 73.9 & 74.6 & 74.6 & 75.4 & 75.5 \\ 4.5 & 4.4 & 7.7 & 7.7 & 7.1 & 7.0 & 6.2 & 6.1 \\ 58 & 70 & 70 & 57 & 52 & 38 & 34 & 33 \end{matrix}$

$\begin{matrix} 77.5 & 77.1 & 77.0 & 76.9 & 76.7 & 76.7 & 76.5 & 76.3 & 76.2 & 74.5 & 74.6 \\ 4.1 & 4.5 & 4.6 & 4.7 & 4.9 & 4.9 & 5.1 & 5.3 & 5.4 & 7.1 & 7.0 \\ 70 & 57 & 38 & 18 & 10 & & 10 & 17 & 22 & 28 & 31 \end{matrix}$

$\begin{matrix} 74.0 & 74.0 & 74.4 & 74.4 & 75.0 & 75.1 \\ 76 & 76 & 72 & 72 & 66 & 65 \\ 70 & 61 & 52 & 39 & 34 & 33 \end{matrix}$

Sta + π - Elev
981.64

67 + 50

✓

+ 82

✓

+ 87

Dec 29, 1958

49

LT

RT

76.7	76.7	76.6	76.5	76.6	76.4	76.2	76.1	74.6	74.4
4.9	4.9	5.0	5.1	5.0	5.2	5.4	5.5	7.0	7.2
38	27	18	10		10	16	22	28	31

76.8	77.0
4.8	4.6
50	70

73.6	74.1	74.3	74.4	75.1
8.0	7.5	7.3	6.7	6.5
70	53	38	34	33

76.0	75.6	75.6	76.3	76.4	76.5	76.4	76.2	76.1	74.5	74.5
5.6	6.0	6.0	5.3	5.2	5.1	5.3	5.5	5.6	7.1	7.1
37	33	26	20	10		10	15	22	27	32

76.3	76.5	76.5
5.3	5.1	5.1
47	66	70

73.6	74.0	74.3	74.4	75.0
8.0	7.6	7.3	6.7	6.6
70	54	38	34	33

75.6	75.3	75.5	76.2	76.4	76.5
6.0	6.3	6.1	5.4	5.2	5.1
43	30	24	20	10	

Duplicate 182

75.7	75.9
5.9	5.7
56	70

Sta + π - Elev

981.64

67+23

✓

68

✓

+ 14

74.88
6.76

+50

TP 2.48 977.36 6.76 974.88

Dec 29 1958

50

11

11

75.4	76.1	76.2	76.4	76.5	76.3	76.2	75.5	74.6	74.3
6.2	5.5	5.4	5.2	5.1	5.3	5.4	6.1	7.0	7.3
24	20	17	10		10	20	24	27	30

75.0	75.6	76.4	76.7	76.7		73.6	74.0	74.4	74.8	75.0
6.6	6.0	5.2	4.9	4.9		8.0	7.6	7.2	6.8	6.6
29	34	37	51	70		70	33	37	34	33

75.0	75.0	76.1	76.4	76.4	76.2	76.1	75.8	74.6	74.3
6.6	6.6	5.5	5.2	5.2	5.4	5.5	5.8	7.0	7.3
30	25	19	10		10	16	22	26	28

76.5	76.7	76.8	76.8		73.8	74.0	74.4	75.0	75.1	74.5
5.1	4.9	4.8	4.8		7.8	7.6	7.2	6.6	6.5	7.1
36	51	63	70		70	54	37	34	33	31

Top MH Lt 29'

75.6	75.0	74.8	75.8	76.0	76.4	75.9	75.7	75.5	74.1	74.1
6.0	6.6	6.8	5.8	5.6	5.5	5.7	5.9	6.1	7.5	7.5
35	30	27	20	10		10	18	23	28	31

75.8	76.0	75.9			73.6	74.1	74.3	74.8	74.8
5.8	5.6	5.7			8.0	7.5	7.3	6.8	6.8
41	60	70			70	53	38	34	33

Top MH Lt 56 68+

Sta + π - Elev

977.36

69

✓

+50

✓

+23

✓

FK
KP
JH

LT

Dec 30, 1958

51

RT

74.1	75.0	75.7	75.7	75.8	75.5	75.4	75.5	73.6	73.6
3.3	2.4	1.7	1.7	1.6	1.9	2.0	1.9	3.9	3.8
29	26	21	10		10	16	22	27	30

75.5	75.7	76.0	76.1	73.6	73.9	74.0	74.7
1.9	1.7	1.4	1.3	3.8	3.5	3.4	2.7
36	54	70	HO	70	54	41	33

73.6	73.6	75.0	75.3	75.2	75.1	74.8	73.1	73.2
3.8	3.8	2.4	2.1	2.1	2.3	2.6	4.3	4.2
31	28	20	10		10	21	27	31

74.8	75.3	75.7	76.1	72.9	73.2	73.8	74.1
2.6	2.1	1.7	1.3	4.5	4.2	3.6	3.3
36	46	70	HO	70	47	35	3.3

75.6	75.1	74.8	75.1	75.0	74.8	74.7	73.0	72.9
1.75	2.3	2.6	2.3	2.3	2.6	2.7	4.4	4.5
63.53	36	22	10		10	20	27	30

Conc

75.8	72.8	72.9	73.0	73.7	73.9
1.55	4.6	4.5	4.4	3.7	3.5
70	70	54	43	35	33

Sta + π - Elev.

97736

70

✓

+09

✓

+36

✓

Dec. 30, 1958

52

Lt

Rt

75.2	74.9	74.5	74.8	74.76	74.5	74.3	72.7	72.9	73.1
2.2	2.5	2.9	2.6	2.6	2.9	3.1	4.7	4.5	4.0
57	43	22	10		10	21	27	31	33

75.1					72.4	72.7	72.6	73.2
→ 2.3					5.0	4.7	4.8	4.2
70					70	54	47	35

72.9	74.4	74.7	74.7	74.76	74.4	74.3	72.7	72.7	73.3
4.5	3.0	2.7	2.7	2.6	3.0	3.1	4.7	4.7	4.1
28	20	15	10		10	20	27	31	33

72.9	73.7	73.4	73.4		72.3	72.7	72.6	72.9
→ 4.5	3.7	4.0	4.0		5.1	4.7	4.8	4.5
33	38	55	70		70	54	45	35

73.1	72.4	74.0	74.4	74.46	74.2	74.0	74.0	72.4	72.1
4.3	5.0	3.4	3.0	2.9	3.2	3.4	3.4	5.0	5.0
35	31	21	10		10	17	22	27	31

73.2	73.3				72.0	72.3	72.4	72.9	73.1
→ 4.2	4.1				5.4	5.1	5.0	4.5	4.3
50	70				70	54	43	34	33

Sta + π - Elev.

977.36

70 + 42 $\pm$ Ditch Lt.

+ 50 Shoulder

+ 63 $\pm$ Tatum

Dec 30, 1958

53

LT

RT

72.0	73.4	74.0	74.4	74.36	74.4	74.2	73.9	73.9	73.2	72.3
54	40	34	30	30	32	3.5	35	42	5.1	
30	27	22	10		10	17	21	24	27	

72.0	72.2	72.1	72.0	72.2	72.3	72.8	72.9	72.4
54	5.2	5.3	54	52	51	46	45	50
47	66	70	70	54	43	35	33	31

73.7	73.8	74.0	74.2	74.4	74.36	74.4	74.1	73.8	73.9	72.7	72.2
37	36	34	32	30	30	3.3	36	3.5	47	5.2	
55	47	28	23	10	10	17	21	25	28		

72.0	72.2	72.3	72.7	72.9	72.3
5.4	52	51	47	45	51
70	54	41	34	33	31

74.2	74.08	74.3	74.3	74.36	74.0	73.7	73.8	72.1	72.3
3.2	228	3.1	3.1	3.1	3.4	27	36	5.3	5.1
51	27	19	10	10	17	21	27	31	

T_g MH

74.0	74.2	74.1	74.0	71.8	72.1	72.2	72.8	72.8
34	3.2	3.3	3.4	56	53	52	46	46
100	150	200	250	70	54	42	34	33

Sta + π - Elev

977.36

70+76 shoulder

✓

+82 $\pm$ Ditch Lt

✓

+88

2 Dec 30 1958 54

LT

RT

73.9	73.9	74.1	74.1	74.1	73.8	73.6	73.7	72.1	72.6
35	35	33	33	33	36	38	37	53	48
60	43	26	10		10	17	21	27	33

71.6	72.0	72.1	72.6	72.2
5.8	54	53	48	52
70	53	42	35	31

72.2	72.2	72.3	73.5	74.1	73.8	73.6	73.7	72.2	72.2
52	52	51	39	33	33	36	38	37	54
60	50	39	31	10		10	17	21	27

71.5	71.9	72.0	72.6	72.7
59	55	54	48	47
70	54	42	34	33

72.0	73.6	73.8	74.0	74.0	73.8	73.6	73.7	72.0	72.1
54	38	36	34	34	36	38	37	54	53
32	27	20	10		10	16	21	27	31

72.0	73.7	73.6	73.6	73.9	71.5	71.8	72.1	72.6
54	37	38	38	35	59	56	53	48
34	40	50	61	70	70	53	41	33

Sta	+	π	-	Elev
-----	---	-------	---	------

		977.36		
--	--	--------	--	--

71

✓

TP	2.21	975.72	3.85	973.51
----	------	--------	------	--------

+50

✓

72

Dec 30, 1958

55

Lt

E

Rt

$\begin{matrix} 73.6 & 72.2 & 73.7 & 73.9 & 73.9 & 73.7 & 73.6 & 72.0 & 72.1 & 72.5 \\ 38 & 52 & 37 & 3.5 & 3.4 & 3.7 & 3.9 & 5.4 & 5.3 & 4.9 \\ 38 & 31 & 22 & 10 & & 10 & 21 & 27 & 31 & 33 \end{matrix}$

$\begin{matrix} 73.5 & 74.1 & 74.4 & 74.8 & & 71.4 & 71.7 & 71.9 & 72.3 \\ \rightarrow 39 & 3.3 & 3.0 & 2.6 & 4 & 6.0 & 5.7 & 5.5 & 5.1 \\ 50 & 64 & 70 & 140 & & 70 & 57 & 39 & 36 \end{matrix}$

End Walk Lt stop Rt

$\begin{matrix} 72.7 & 71.8 & 71.9 & 73.4 & 73.6 & 73.7 & 73.6 & 73.2 & 71.6 & 71.7 & 72.2 \\ 3.0 & 3.9 & 3.8 & 2.3 & 2.1 & 2.0 & 2.2 & 2.5 & 4.1 & 4.0 & 3.5 \\ 38 & 32 & 28 & 21 & 10 & & 10 & 21 & 27 & 31 & 33 \end{matrix}$

$\begin{matrix} 73.3 & 73.0 & 72.9 & & & 71.5 & 71.8 & 71.7 \\ \rightarrow 2.4 & 2.7 & 2.8 & 4 & & 4.2 & 3.9 & 4.0 \\ 49 & 62 & 70 & & & 70 & 52 & 38 \end{matrix}$

$\begin{matrix} 72.3 & 71.4 & 72.8 & 73.3 & 73.4 & 73.4 & 73.2 & 73.0 & 71.3 & 71.4 & 71.9 \\ 3.4 & 4.3 & 2.9 & 2.4 & 2.3 & 2.3 & 2.5 & 2.7 & 4.4 & 4.3 & 3.8 \\ 38 & 29 & 24 & 20 & 10 & & 10 & 22 & 27 & 31 & 33 \end{matrix}$

$\begin{matrix} 72.9 & 72.5 & & & & 71.3 & 71.7 & 71.5 \\ \rightarrow 2.8 & 3.2 & 4 & & & 4.4 & 4.0 & 4.2 \\ 49 & 70 & & & & 70 & 52 & 39 \end{matrix}$

Sta	+ π	- Elev
-----	---------	--------

17	975.72
----	--------

 $72 + 58$

✓

 $+ 85 \pm$
$$n^{2^2^6}$$

3.47

73

✓

18.81

4.91

+ 48

450

Top MHH
29'

Dec 30, 1958

56

LT

RT

71.3	71.3	72.9	73.2	73.2	73.0	72.7	71.1	71.1	71.7
44	44	28	25	25	27	30	46	46	40
30	27	21	10		10	22	27	31	33

72.5	72.5	72.6	72.9
3.2	3.2	31	28
35	47	70	Ho

End walk 64 35

71.2	71.5	71.3
45	42	44
70	52	38

71.9	70.3	70.3	72.7	72.8	72.9	72.7	72.5	70.7	70.8	71.6
38	54	54	30	29	2.85	30	3.2	5.0	49	42
35	30	29	20	10		10	21	27	31	33

72.1	72.2
3.6	3.5
51	70

71.1	71.2	71.0
46	45	47
70	52	38

71.3	70.3	70.3	71.9	72.2	72.3	72.7	71.9	71.8	70.2	70.5
44	54	54	3.8	35	3.4	3.5	38	3.9	55	52
36	29	27	19	10		10	17	22	27	31

71.7	72.1	72.4
4.0	3.6	33
47	70	Ho

70.7	70.8	70.6	70.9
5.0	4.9	5.1	48
70	51	38	33

Sta + π - Elev.

975.72

73+84

✓

+88

74

✓

+33

Dec 30, 1958

57

Lt

Rt

69.8 71.1 71.5 71.7 71.8* 71.7 71.4 71.5 70.1 69.8
59 46 42 40 39 40 43 42 56 59
28 25 21 10 10 16 21 26 31

69.8 71.1 71.3 71.6 71.7 70.5 70.5 70.4 70.7
59 46 44 41 40 5.2 5.2 5.3 5.0
30 34 44 61 70 70 51 39 33

71.7 71.2 71.5 71.4 71.7 71.8*
40 4.5 4.2 4.3 4.0 39 duplicate +84 Rt
70 46 31 22 10

71.2 71.2 71.5 71.6 71.6* 71.5 71.3 71.3 69.7 69.8
4.5 4.5 4.2 4.1 4.1 4.2 4.4 4.4 6.0 5.9
48 32 20 10 10 17 21 27 31

71.3 71.3 70.2 70.3 70.2 70.6
4.4 4.4 5.5 5.4 5.5 5.1
65 70 70 51 38 33

71.0 70.8 70.5 70.8 70.9 71.2 71.3*
4.7 4.9 5.2 4.9 4.8 4.5 4.4 duplicate +38
58 46 30 20 10
70

Sta + π - Elev

975.72

24+38

✓

+50

✓

7.5

Dec 30, 1958

58

LT

ST

✓✓
11.2*

70.1	69.3	69.3	70.8	71.1	11.2*	71.0	70.9	70.5	69.2	68.8
56	64	64	49	46	4.5	4.7	4.8	5.2	6.5	6.9
32	30	28	23	10		10	20	23	27	30

70.3	70.5	70.8	71.1			69.9	70.0	69.9	70.2
54	52	49	46	✓		58	5.7	5.8	5.5
39	49	64	70			70	51	37	33

69.2	69.2	70.7	70.8	71.0	11.1*	70.9	70.7	69.0	69.0	70.0
6.5	6.5	5.0	4.9	4.7	4.6	4.8	5.0	6.7	6.7	5.7
30	28	23	20	10		10	21	27	30	33

69.9	70.1	70.3	70.7	71.8		69.9	70.0	69.8
5.8	5.61	5.4	5.0	3.9	✓	5.8	5.7	5.9
32	43	55	70	House		70.	51	37

Walt

68.5	68.5	70.0	70.2	70.5	4	70.7*	70.5	70.2	69.9	68.8	68.7
7.2	7.2	5.7	5.5	5.2	5.0	5.2	5.5	5.8	6.9	7.0	
31	28	23	20	10		10	17	22	26	30	

69.5	69.6	69.8		4		69.5	69.5	69.5	69.6
6.2	6.1	5.9				6.2	6.2	6.2	6.1
35	54	70				70	51	35	33

Sta + π - Elev

975.72

75+50

✓

BM 0.47 974.44 1.75 973.97 973.97

76

✓

+50

—

FX
RG
KP
JH

Dec 30, 1958
Jan. 6, 1959

59

LT

RT

67.8	67.8	69.7	69.9	70.0	70.1*	69.8	69.8	68.2	68.3	69.1
79	79	60	58	57	56	59	59	75	74	66
28	26	20	18	10		10	21	27	31	33

68.8	69.3	69.8	70.9		68.8	68.9	69.1
6.9	64	59	48	✓	6.9	6.8	6.6
32	42	70	40		70	51	35

F. End Door Sill Ho # 1867 W. Larpenteur

67.7	67.7	68.7	69.5	69.6	69.7	69.6	69.2	69.3	69.9	69.9
6.7	6.7	5.7	4.9	4.8	4.65	4.8	5.2	5.1	6.5	6.5
31	29	25	21	10		10	21	23	27	29

68.7	68.8	68.8	71.4	✓	68.1	68.3	68.8	68.9	68.8	68.7
5.7	5.6	5.6	3.0		6.3	6.1	5.6	5.5	5.6	5.7
35	57	70	40		70	58	45	39	33	32

67.4	67.5	69.1	69.3	69.3	69.3*	69.1	69.0	69.0	67.2	67.2
70	69	5.3	5.1	5.1	5.1	5.3	5.4	5.4	7.2	7.2
31	28	24	20	10		10	17	22	27	30

68.3	68.3		67.8	68.0	68.0	68.3	68.6	68.6
6.1	6.1		6.6	6.4	6.4	6.1	5.8	5.9
35	70		70	60	47	39	36	33

Sta + π - Elev

974.44

77

✓

+50

✓

TP 352 971.44 6.32 967.92

78

Jan. 6, 1959 60

LT

RT

67.5	68.6	68.8	68.8	68.9*	68.7	68.5	67.0	67.0
6.9	5.8	5.6	5.6	5.50	5.7	5.9	7.4	7.4
27	22	17	10		10	22	27	31

67.9	68.0	68.0		67.2	67.4	67.4	68.2	68.2
6.5	6.4	6.4	✓	6.9	6.7	6.7	6.2	6.2
33	58	70		70	62	46	37	33

66.8	67.9	68.2	68.3	68.3	68.4*	68.2	68.0	67.2	66.7
7.6	6.5	6.2	6.1	6.1	6.0	6.2	6.4	6.9	7.7
26	23	20	17	10		10	20	24	26

67.2	68.1	67.9	67.9	67.4	67.4	67.4	67.4	67.1
6.9	6.3	6.5	6.5	7.0	7.0	7.0	7.0	7.3
31	35	52	70	70	50	39	33	31

66.2	66.2	67.5	67.1	67.1	67.9*	67.0	67.3	66.5	66.5	66.7	66.5
5.2	5.2	3.9	3.7	3.7	3.5	3.8	4.1	4.9	4.9	4.7	4.6
29	27	22	20	10		10	22	25	26	28	33

67.7	67.6	67.5		66.9	66.8	66.8
3.7	3.8	3.9	✓	4.5	4.6	4.6
34	49	70		70	58	40

Sta + π - Elev

971.44

78+50

✓

+73

✓

+84 ± Ditch

+85

Jan 6, 1959

61

LT

RT

66.0 66.7 66.7 66.8 67.1 67.2* 66.8 66.6 65.4 65.6 65.9
54 67 47 46 43 42 46 48 60 58 55
31 26 20 15 10 10 23 27 30 32

66.9 66.9 67.1 67.1
4.5 4.4 4.3 4.3
32 46 64 70

66.2 66.2 66.3
5.2 5.2 5.1
70 47 35

66.2 66.5 66.4 66.8 66.8* 66.6 66.4 65.3 65.4 65.6
5.2 4.9 5.0 4.6 4.6 4.8 5.0 6.1 6.0 5.8
22 20 18 10 10 21 26 29 32

66.5 66.7 66.6 66.5 66.8
6.9 6.7 4.8 4.9 4.6
27 33 39 51 70

66.2 66.2 66.0
5.2 5.2 5.4
70 54 40

65.7 66.2 66.1 66.6 66.6* 66.4 66.2 64.9 64.9 65.6
5.7 5.2 5.3 4.8 4.8 5.0 5.2 6.5 6.5 5.8
34 27 19 10 10 21 25 28 33

65.5 65.4
6.1 6.0
30 35

66.1 65.9 65.6
5.3 5.5 5.8
70 55 39

65.98
5.96
28
TOMH

Sta + π - Elev

971.44

78+92 Shoulder Line

✓

79

+07.65⁺₋ $\neq$ Fairview

✓

+25

Jan 6, 1959

62

17

17

66.4	66.3	66.3	66.5	66.5*	66.4	66.2	64.5	65.0	65.6
5.0	5.1	5.1	4.9	4.9	5.0	5.2	6.9	6.4	5.8
60	41	25	10		10	22	25	30	33

66.1	65.8
5.3	5.6
70	50

66.48
4.96

66.7	66.7	66.5	66.2	66.4*	66.2	66.1	64.1	64.1
4.7	4.7	4.9	5.2	5.0	5.2	5.3	7.3	7.3
100	60	30	10		10	22	27	29

66.9	67.1
4.5	4.3
150	200

66.1	65.8	65.7
5.3	5.6	5.7
70	51	33

65.9	65.7	65.8	66.0	66.1*	66.0	65.9	64.2	64.2
5.5	5.7	5.6	5.4	5.3	5.4	5.5	7.2	7.2
60	44	26	10		10	24	28	30

66.1	66.1	65.8
5.3	5.3	5.6
70	52	34

Sta + π - Elev

971.44

79+34

✓

+42

✓

+50

Jan 6, 1959 63

11

11

64.4	65.0	65.4	65.9	65.9*	65.9	65.6	64.2	64.2
70	6.4	60	5.5	5.5	5.5	5.8	72	2.2
49	38	27	10		10	22	27	30

64.7
→ 6.7
60

66.2	66.0	65.8
5.2	5.4	5.6
49	45	34
40		

66.0	65.6	64.2	64.7	65.7	65.8*	65.7	65.4	64.0	64.0
5.4	5.8	72	6.7	5.7	5.6	5.7	6.0	7.4	7.4
60	44	35	29	10		10	23	27	30

66.2	65.7
5.2	5.7
49	35
40	

65.5	64.1	64.1	64.9	65.6	65.7*	65.5	65.5	63.9	63.9
5.9	7.3	7.3	6.5	5.8	5.7	5.9	5.9	7.5	7.5
36	31	30	24	10		10	22	27	30

65.8 65.7
→ 5.6 5.7
49 70

65.4	65.6
5.3	5.8
49	36
40	

Sta + π - Elev

971.44

80

✓

TP 3.29 968.37 6.36 965.08

+33

✓

+65

Jan 6, 1959

64

21

2

RT

64.8	64.9	65.1	65.1	64.9	64.8	64.5	63.1
6.6	6.5	6.3	6.2	6.5	6.6	6.9	8.3
22	18	10		10	17	22	27

63.2	63.2	64.5	64.4	64.4	64.4	64.5	64.4	64.1	63.1
8.2	8.2	6.9	7.0	7.0	7.0	6.9	7.0	7.3	8.3
26	29	34	39	53	70	70	53	34	29

Top 5 End Culvert

62.7	62.9	64.4	64.5	64.8	64.8	64.2	64.7	64.4	62.9	62.8
5.7	5.5	4.0	3.9	3.6	3.6	3.7	3.7	4.0	5.5	5.6
30	28	22	18	10		10	19	22	26	32

63.5	63.9	64.0	64.0	63.8		62.7	62.8	62.9
4.9	4.5	4.4	4.4	4.6		5.7	5.6	5.5
32	33	39	53	70		70	60	43

62.5	62.6	64.2	64.2	64.4	64.4	64.3	64.2	64.1	62.8	62.7
5.9	5.8	4.2	4.2	4.0	3.9	4.1	4.2	4.3	5.6	5.7
30	27	21	17	10		10	19	22	26	29

63.3	63.5	63.4	63.5	63.5		62.2	62.4	62.8
5.1	4.9	5.0	4.9	4.9		6.2	6.0	5.6
32	33	38	36	70		70	49	35

Sta	+	π	-	Elev
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Sta	+	π	-	Elev
80+94		968.37		

Sta	+	π	-	Elev
80+94		968.37		

Sta	+	π	-	Elev
80+94		968.37		

Sta	+	π	-	Elev
80+94		968.37		
81				

Sta	+	π	-	Elev
80+94		968.37		
81				

Sta	+	π	-	Elev
80+94		968.37		
81				
+23				

Jan 2, 1959

65

LT

RT

62.3	62.4	63.9	63.9	64.2	64.2	64.0	63.9	63.5	62.3	62.2
6.1	6.0	45	45	4.2	4.2	4.4	4.6	4.9	6.1	6.2
30	27	22	17	10		10	20	23	27	28

62.9	63.1	62.9	63.1	63.0	61.7	61.8	62.1	62.4
5.5	5.3	5.5	5.3	5.4	6.7	6.6	6.3	6.0
32	33	39	56	70	70	53	38	29

62.3	62.9	63.9	63.9	64.1	64.1	63.9	63.9	63.9	63.5
6.1	5.5	4.5	4.5	4.3	4.23	4.5	4.5	4.5	4.9
27	24	21	17	10		10	16	20	30

62.2	62.9	63.1	62.7	62.8	62.9	63.0	63.1	63.2
6.2	5.6	5.3	5.7	5.6	5.5	5.4	5.3	5.2
31	32	33	40	56	70	70	54	42

62.1	63.6	63.8	63.9	63.9	64.0	63.8	63.8	63.8	63.4	63.4
6.3	4.8	4.6	4.7	4.5	4.4	4.6	4.6	4.6	4.94	4.90
27	22	20	18	10		10	14	24	35	53

Walk

61.8	61.8	62.8	62.5	62.6	62.6	63.7	63.5
6.6	6.6	5.6	5.9	5.8	5.8	4.76	4.90
29	31	33	41	58	70	Walk	70

House Walk

Sta + π - Elev

968.37

81+30

✓

+50

✓

+56

6.329
5.08

82

± Jan. 7, 1959

66

LT

RT

61.7	63.7	63.6	63.8	63.9	63.9	63.8	63.9	61.9	61.8
6.7	4.7	4.8	4.6	4.5	4.5	4.6	4.5	6.5	6.6
29	22	20	10		10	19	23	28	29

61.6	62.8	62.5	62.5	62.5
6.8	5.6	5.9	5.9	5.9
31	33	46	59	70

63.1	63.1	63.2	62.4
5.3	5.3	5.2	6.0
70	54	39	31

61.9	63.3	63.6	63.6	63.8	63.9	63.5	63.5	63.3	61.8	61.6
6.5	5.1	4.8	4.8	4.6	4.6	4.9	4.9	5.1	6.6	6.8
29	24	22	17	10		10	15	22	25	29

61.7	62.3	62.4	62.3	62.3	62.4
6.7	6.1	6.0	6.1	6.1	6.0
31	32	33	41	57	70

Top MH 18' RT

61.3	61.4	61.7
7.1	7.0	6.7
70	47	34

62.1	62.9	63.3	63.4	63.6	63.6	63.2	63.1	63.1	62.5	61.3
6.3	5.5	5.1	5.0	4.8	4.8	5.2	5.3	5.3	5.9	7.1
28	24	22	17	10		10	21	23	25	27

62.0	62.4	62.4	62.4	62.5
6.4	6.0	6.0	6.0	5.9
32	33	38	60	70

61.0	61.0	61.7	61.1
2.4	2.4	6.7	2.3
70	55	35	30

Sta + π - Elev

968.37

82+50

✓

T.P.

+49 4.44 967.37 5.44 962.93

83+00

✓

+50

✓

FK
RG
KP

LT

Jan 7, 1959
Jan 8, 1959 RT 67

61.8 62.5 63.2 63.2 63.4 63.4 63.1 63.1 63.1 61.4 61.0
6.6 5.9 5.2 5.2 5.0 5.0 5.3 5.3 5.3 7.0 7.4
29 26 22 17 10 10 15 23 29 38

61.8 62.4 62.4 62.4 62.4 62.5
6.6 6.1 6.0 5.7 6.0 5.9
30 32 33 35 57 70
74 7.5
70 61

Top MH R!

61.4 61.4 63.0 63.2 63.5 63.6 63.4 62.9 61.3 60.9
6.0 6.0 4.4 4.2 3.9 3.83 4.0 4.5 6.1 6.5
30 28 23 17 10 10 21 26 38

61.9 62.4 62.3 62.1 62.5
5.5 5.0 5.1 5.3 4.9
32 34 36 50 70
60.9 61.0
6.5 6.4
70 53

61.5 62.8 62.8 63.1 63.3 63.2 62.7 62.3 61.2
5.9 4.6 4.6 4.3 4.06 4.2 4.7 5.1 6.2
31 22 17 10 10 19 22 26

62.0 62.3 62.4 62.0 62.3 62.4 61.4 61.3 61.1 61.2
5.4 5.1 5.0 5.4 5.1 5.0 6.0 6.1 6.2 6.2
33 34 36 44 59 70 70 55 42 31

Sta	+	π	-	Elev.
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		967.37		
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84+00				
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✓				
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+47				
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✓				
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+50				
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✓				
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Jan 8, 1959

68

LT

FT

61.0 62.5 62.6 63.0 63.1 63.0 62.8 62.4 60.3
 6.4 4.9 4.8 4.4 4.25 4.4 4.6 5.0 7.1
 28 22 17 10 10 16 22 27

61.0 61.8 62.1 61.7 61.6 62.4 62.2 62.0 62.1 61.9 60.5
 6.4 5.6 5.3 5.7 5.8 5.0 4.8 5.35 5.4 5.3 5.5 6.9
 30 33 34 40 47 51 70 75 70 48 35 31
 WALK

62.8 62.6 62.6 62.3 60.3 60.4
 Same as 84+50 LT. 4.58 4.8 4.8 5.1 7.1 7.0
 10 15 21 28 30

61.4 61.3 61.7 61.3
 6.0 6.1 5.7 6.1
 70 45 37 32

60.9 62.3 62.3 62.7 62.8 62.6 62.6 62.3 60.2 60.5
 6.5 5.1 5.1 4.7 4.6 4.8 4.8 5.1 7.2 6.9
 28 22 18 10 10 14 22 27 34

60.9 61.7 61.8 61.3 61.8 62.2 61.0 60.5
 6.5 5.7 5.6 6.1 5.6 5.2 6.4 6.9
 31 33 35 39 52 70 70 49

Sta + π - Elev

967.37

+56

✓

85+00

✓

+50

✓

TP

5.12

965.53

6.96

960.41

Jan 8, 1959

69

LT

RT

Same as 84+50 LT.

62.7	62.6	62.5	62.3	60.2	60.2
4.67	4.8	4.9	5.1	7.2	7.2
✓ 10	16	22	28	30	

62.2	61.7	61.1
5.2	5.7	6.3
70	51	34

60.2	60.2	61.8	61.9	62.3	62.4	62.1	62.1	61.8	60.0	60.0
7.2	7.2	5.6	5.5	5.1	5.02	5.3	5.3	5.6	7.4	7.4
31	27	22	17	10		10	15	24	27	29

61.2	61.4	60.9	61.3	61.3	63.5	62.7	62.0	61.4
6.2	6.0	6.5	6.1	6.1	3.79	4.7	5.4	6.0
34	36	41	50	70		70	51	40

Walk

60.0	61.3	61.4	61.9	61.9	61.6	61.5	61.1	60.7	59.6
7.4	6.1	6.0	5.5	5.47	5.8	5.9	6.3	6.7	7.8
27	22	18	10		10	14	20	26	30

60.0	60.7	61.1	60.7	60.9	62.2	61.5	60.9
7.4	6.7	6.3	6.7	6.5	5.2	5.9	6.5
31	34	36	45	70	90	49	33

E end Culvert entrance 85+50

Sta	+	π	-	Elev.
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		965.53		
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85+76				
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✓				
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+90				
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✓				
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86+00				
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✓				
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Jan 8, 1958

70

LT

RT

59.9	60.8	61.3	61.7	61.7	61.3	61.3	60.9	59.6	60.3
5.6	4.7	4.2	3.8	3.80	4.2	4.2	4.6	5.9	5.2
27	23	17	10		10	16	24	28	34

60.0	60.3	60.8	60.6	60.7	60.8	61.9	61.7	61.3
5.5	5.2	4.7	4.9	4.8	4.7	3.6	3.8	4.2
31	34	36	44	59	70	70	58	44

60.0	60.0	61.1	61.3	61.7	61.6	61.2	60.8	59.6	59.7
5.5	5.5	4.4	4.2	3.8	3.86	4.3	4.7	5.9	5.8
31	26	22	17	10		10	24	28	31

60.9	60.7	60.6	60.6	60.8	60.7	60.7	60.7	59.0
5.1	4.8	4.9	4.9	4.7		6.8	6.8	6.5
34	35	45	59	70		70	49	37

59.9	60.0	61.0	61.9	61.6	61.6	61.2	60.8	59.3	59.8
5.6	5.5	4.5	4.1	3.9	3.89	4.3	4.7	6.2	6.7
30	27	24	19	10		10	24	29	38

59.8	60.7	60.6	60.8	61.0	60.7	59.7	59.7
5.7	4.8	4.9	4.7	4.5		6.8	6.8
33	36	44	53	70		70	52

Sta + π - Elev

965.53

86+50

✓

+64

✓

+71

✓

Jan 8, 1958

71

✓

RT

✓

59.7	59.8	60.9	61.0	61.5	61.6	61.3	60.8	58.8	58.7
5.8	5.7	4.6	4.5	4.0	3.88	4.2	4.7	6.7	6.8
31	27	23	17	10		10	22	27	33

60.4	60.1	60.6	61.0	61.4
5.1	4.8	4.9	4.5	4.1
34	35	45	50	70

✓

58.7	58.7
6.8	6.8
70	47

✓

59.8	59.7	60.8	61.0	61.4	61.6	61.2	60.7	58.9	58.5	58.7
5.7	5.8	4.7	4.5	4.1	3.94	4.3	4.8	6.6	7.0	6.8
31	27	22	17	10		10	22	26	29	36

60.7	60.6	61.1	61.6
4.8	4.9	4.4	3.9
35	45	51	70

✓

58.5	58.5
7.0	7.0
70	54

✓

59.7	59.7	60.8	60.9	61.4	61.5	61.2	60.7	58.8	58.5	58.6
5.8	5.8	4.7	4.6	4.1	3.97	4.3	4.8	6.7	7.0	6.9
32	27	23	17	10		10	21	25	28	31

60.7	60.7	61.2	61.8
4.8	4.8	4.3	3.7
35	45	53	70

✓

60.2	59.7	59.5
5.3	5.8	6.0
70	54	34

Sta + π - Elev

965.53

87+00

✓

+50

✓

88+00

✓

Jan 8, 1958

72

LT

£

RT

59.6	60.6	60.8	61.4	61.4	61.1	60.8	58.2	58.2
5.9	4.9	4.7	4.1	4.09	4.4	4.7	7.3	7.3
27	23	16	10		10	23	28	30

59.5	60.7	61.1	60.9	61.4	62.1	60.8	60.2	59.9	59.6
6.0	4.8	4.4	4.6	4.1	3.4	5.13	5.3	5.6	5.9
30	33	35	44	51	70	House 70	46	33	

59.3	59.3	60.2	60.6	61.1	61.2	61.1	60.6	68.4	58.4	59.1
0.2	0.2	5.3	4.9	4.4	4.34	4.5	4.9	7.1	7.1	0.4
30	27	23	17	10		10	22	28	30	32

60.9	60.7	60.8	61.2	61.7		59.1	59.1
4.6	4.8	4.7	4.3	3.8		6.4	6.4
33	39	44	51	70		70	51

58.8	58.8	60.5	60.8	60.9	60.8	60.4	58.1	58.1	59.4
6.7	6.7	5.0	4.7	4.57	4.7	5.1	7.4	7.4	6.1
31	27	20	10		10	23	28	31	34

60.1	59.8	59.8	60.4	60.7		59.6	59.4
5.4	5.7	5.7	5.1	4.8		5.9	6.1
34	39	44	51	70		70	52

Sta	+	π	-	Elev
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		965.53		
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+50				
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✓				
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89+00				
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✓				
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+50				
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✓				
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TP	1.42	962.96	3.99	961.54 (961.47) [?]
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Jan 8, 1958

Lt.

~~L~~

~~Rt~~

73

58.6	60.3	60.3	60.6	60.7	60.5	60.1	57.8	57.8	59.8
6.9	5.2	5.2	4.9	4.83	5.0	5.4	7.7	7.7	5.7
27	22	17	10		10	23	29	31	34

58.6	59.1	59.0	58.9	59.4	59.6		59.4	59.4	59.4
6.9	6.4	6.5	6.6	6.1	5.9		6.1	6.1	6.1
32	34	39	45	51	70		House	70	57

58.7	58.0	57.8	59.8	60.3	60.5	60.3	59.8	57.3	57.3
6.8	7.5	7.7	5.7	5.2	5.01	5.2	5.7	8.2	8.2
35	31	27	21	10		10	23	29	31

58.5	58.5	58.8	59.9			58.7	58.6	58.9
7.0	7.0	6.7	6.6			6.8	6.9	6.6
39	45	52	70			70	55	35

57.7	57.6	59.6	59.9	60.2	60.0	59.8	59.7	57.2	57.3
7.8	7.9	5.9	5.6	5.30	5.5	5.7	5.8	8.3	8.2
32	27	21	12		10	16	24	28	31

58.4	58.4	58.4	58.7	58.7		61.1	58.3	58.3	58.3
7.1	7.1	7.1	6.8	6.8		4.38	7.2	7.2	7.2
35	39	46	51	70		House	70	58	33

NW Car Top Stop 1750 W. Larp. Ave

Sta	+	π	-	Elev
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		962.96		
--	--	--------	--	--

89+73				
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✓				
---	--	--	--	--

+79				
-----	--	--	--	--

✓				
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90+00				
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✓				
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Jan 8, 1958

Lt.

Rt.

74

57.6	57.6	59.5	60.0	60.1	60.0	59.9	59.6	56.9	56.9
5.4	5.4	3.5	3.0	2.85	3.0	3.1	3.4	6.1	6.1
31	27	22	10		10	19	24	28	31

58.6	58.5	58.4	58.7	58.6		58.5	58.6	58.3
4.4	4.5	4.6	4.3	4.4		4.5	4.4	4.7
35	39	46	50	70		70	50	34

58.6	57.9	59.4	59.9	60.1	60.0	59.9	59.4	59.2
5.4	5.1	3.6	3.1	2.88	3.0	3.1	3.6	3.84
31	26	22	10		10	20	33	45
								WALK

58.6	58.4	58.4	58.7	58.7		59.4	59.3
4.4	4.6	4.6	4.3	4.3		3.62	3.65
35	40	47	51	70		70	55
						WALK	WALK

59.9	59.3	59.4	59.9	60.0	59.9	60.0	59.5	59.3	59.4
5.1	3.7	3.6	3.1	2.98	3.1	3.0	3.5	3.7	3.6
27	22	18	10		10	22	33	55	70

57.8	58.5	58.5	58.4	58.8	58.7
5.2	4.5	4.5	4.6	4.2	4.3
31	34	40	47	52	70

Sta + π - Elev

962.96

+27

✓ Note: top of Wall leans to West

+50

✓

91+00

✓

Jan 8, 1958

Lt.

4

Rt

75

59.8 59.7 59.2 59.2 59.8 59.9 59.7 59.4 56.6 59.5 59.4

5.2 5.3 3.8 3.8 3.2 3.12 3.3 3.6 6.4 3.5 5.6

31 28 22 19 10 10 20 27 27 33

Wall

58.7 58.5 58.4 58.7 58.7 58.8 58.5 59.7 58.6 59.7

→ 4.3 4.5 4.6 4.3 4.3 3.2 5.5 3.3 5.4 3.3

35 39 45 50 70 70 70 50 50 33

Wall

Wall

Wall

59.9 59.8 59.2 59.2 59.8 59.8 59.6 59.2 56.6 56.9 56.6

5.1 5.2 3.8 3.8 3.2 3.19 3.4 3.8 6.4 6.1 6.4

31 27 21 18 10 10 21 27 31 48

58.7 58.4 58.4 58.7 58.7

→ 4.3 4.6 4.6 4.3 4.3

35 40 46 50 70

56.6

6.4

70

59.9 59.8 59.1 59.2 59.6 59.7 59.5 59.3 58.8 56.8 56.8

5.1 5.2 3.9 3.8 3.4 3.34 3.5 3.7 4.2 6.2 6.2

31 27 23 16 10 10 10 21 27 30

58.7 58.4 58.5 58.6 58.7

→ 4.3 4.6 4.5 4.4 4.3

35 39 47 56 70

56.5

56.9

6.5

6.1

70

50

Sta + π - Elev

962.96

+50

✓

92+00

✓

TP

3.64 962.73 3.82 959.14 959.09

+17

Jan 8, 1958
 & Jan 9, 1958
 RT

Lt.

76

57.8	57.7	59.1	59.4	59.50	59.3	58.7	56.8	56.8
5.2	5.3	3.9	3.6	3.49	3.7	4.3	6.2	6.2
31	28	23	10		10	23	28	30

58.6	58.3	58.3	58.6	58.7	56.7	57.2	57.2
4.4	4.7	4.7	4.4	4.3	6.3	5.8	5.8
35	39	46	56	70	70	55	34

57.7	57.7	58.8	59.0	59.4	59.3	59.2	58.6	56.9	56.9	57.8
5.3	5.3	4.2	4.0	3.6	3.56	3.8	4.4	6.1	6.1	5.2
30	27	23	16	10		10	22	26	28	33

58.6	58.1	58.2	58.6	58.7	59.0	59.6
4.4	4.9	4.8	4.4	4.3	6.0	5.4
35	39	45	49	70	70	53

Top Mant. sta 92+21 ±

57.5	58.5	58.8	58.9	59.2	59.3	59.0	58.7	58.2	56.5	56.5
5.2	4.2	3.9	3.8	3.5	3.4	3.7	4.0	4.5	6.2	6.2
27	24	20	15	10		10	19	22	27	29

57.5	58.1	58.5	58.0	58.4	58.5	57.2	57.7	57.7
5.2	4.6	4.2	4.7	4.3	4.2	5.5	5.0	5.0
29	33	35	38	50	70	70	47	31

Sta + π - Elev

962.73

92+24

✓

+50

✓

93

✓

+12

58.31
4.42

Jan. 9, 1958

75

LT

2

RT

57.5	57.5	58.5	58.9	59.2	59.2	59.1	58.7	58.2	56.5
42	5.2	4.2	3.8	3.5	3.45	3.6	4.0	4.5	6.2
30	28	23	15	10		10	19	23	26

58.2	58.5	58.0	58.4	58.5	58.5	58.5	58.9	59.0	58.7	56.5
4.5	4.2	4.7	4.3	4.2	4.2	4.2	3.8	3.7	4.0	6.2
33	35	38	49	63	70	70	52	38	35	32

57.7	57.5	58.7	58.9	59.0	59.2	59.0	58.7	56.6	56.6	58.9
5.0	5.2	4.0	3.8	3.7	3.5	3.7	4.0	6.1	6.1	3.8
31	28	23	14	10		10	23	27	31	33

58.3	58.5	58.1	58.4	58.5		57.8	58.2	58.5	58.9
4.4	4.2	4.6	4.3	4.2		4.9	4.6	4.2	3.8
33	35	38	49	70		70	52	38	35

57.2	57.2	58.5	58.6	58.7	58.8	58.5	58.6	57.5	56.3	56.3
5.5	5.5	4.2	4.1	4.0	3.9	4.2	4.1	5.2	6.4	6.4
30	28	22	14	10		10	24	27	29	32

58.2	58.4	57.8	58.2	58.3	58.5	57.3	57.8	58.3	58.7	58.5
4.5	4.3	4.9	4.5	4.4	4.2	5.4	4.9	4.4	4.0	4.2
33	35	37	47	61	70	70	51	36	35	33

Top MH 25.34

1.44
29

Sta + π - Elev.

962.73

93+50

✓

+54^t

57.66
5.07

94

✓

+11

Jan 8, 1959

76

LT

RT

57.6	57.3	58.3	58.2	58.3	58.2	58.2	58.0	55.3	55.3	58.3
51	54	44	45	44	45	47	74	74	44	
31	29	22	10		10	23	27	30	32	

58.3	58.4	57.1	57.1	58.7	56.1	57.0	57.3	58.0	57.8	58.4
44	43	40	40	40	60	57	54	47	49	43
33	35	47	60	70	70	62	49	40	37	35

Top MH 29.24

57.1	57.6	57.6	57.7	57.7	57.7	57.6	57.3	56.4	55.1	
56	51	48	50	50	49	6	51	54	43	76
29	25	22	20	10		10	20	24	26	

57.5	58.4	58.8	58.8	60.4	56.1	56.3	56.9	57.5	57.6	57.6	55.1
52	43	39	39	23	66	64	58	52	51	51	76
32	40	61	70	40	70	64	48	38	35	32	31

57.2	57.2	57.6	57.6	57.6	57.6	57.5	57.3	54.9	54.9	57.3
55	55	51	51	51	51	52	54	78	28	54
31	28	25	21	10		10	22	26	30	33

57.6	58.0	58.3	58.7	58.7	58.7	56.1	56.7	57.0	57.3	
51	47	44	40	40		66	60	57	54	
32	37	40	56	70		70	54	39	35	

Sta + π - Elev.

962.73

94+15

✓

+50

95

Jan 9, 1959 77

LT

RT

57.7	57.6	57.7	57.5	57.5	57.6	57.4	57.1	57.7	57.7	57.0
50	51	50	52	52	51	53	56	80	80	57
70	47	33	21	10		10	21	25	29	32

56.1	56.5	56.9	57.3	56.9
66	62	58	54	58
70	61	45	36	34

57.1	57.0	57.1	57.1	57.1	57.2	57.0	56.6	57.1	57.1	56.7
56	57	56	56	56	55	57	61	86	86	60
70	46	28	16	10		10	21	26	31	33

58.5

4.2
40

55.6	55.8	56.5
71	69	62
70	68	39

56.5	56.1	56.2	56.5	56.6	56.6	56.4	56.1	56.6	56.6
62	66	65	62	61	60	63	66	91	91
38	30	22	16	10		10	22	28	32

56.2	55.9	55.6	55.7		54.8	54.9	55.6	55.4
65	68	71	70		79	78	71	73
48	51	63	70		70	57	36	33

Sta + π - Elev.

962.73

95+50

✓

96

✓

B.M.

1.40 961.33 (961.34)

Jan. 9, 1959

LT

RT 78

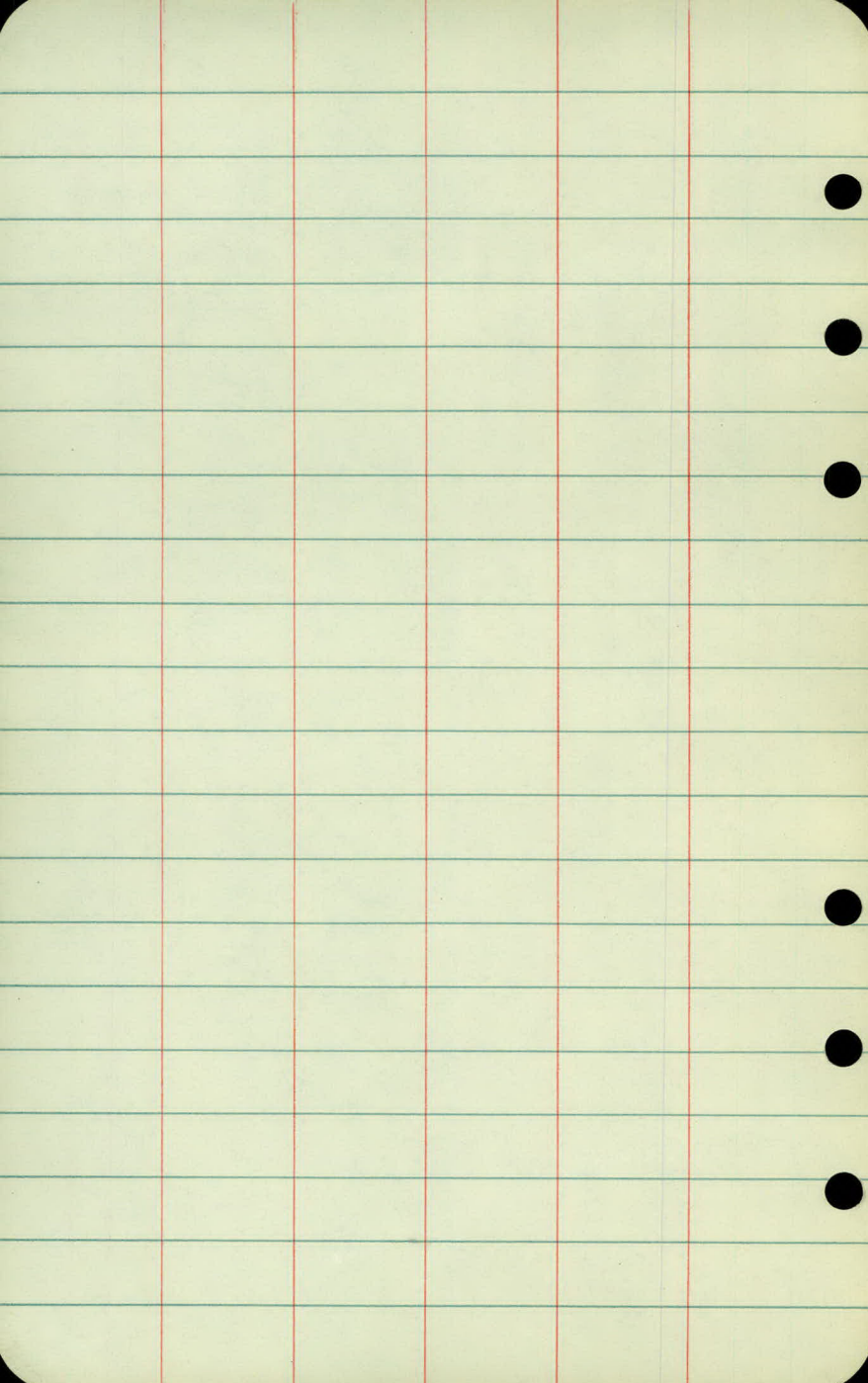
55.2	55.0	54.9	56.0	56.2	56.1	55.8	55.6	55.3	55.4	55.3
75	77	78	6.7	6.5	6.57	6.9	7.1	7.4	9.3	9.3
70	54	38	23	10		10	21	24	28	32

	55.5	55.9	54.4	54.9
✓	9.2	8.8	8.3	7.8
	70	51	35	34

54.6	54.5	54.5	55.6	55.7	55.7	55.6	55.2	54.4	52.9	52.1
8.1	8.2	8.2	7.1	7.0	6.97	7.1	7.5	8.3	9.8	9.8
70	55	39	24	10		10	21	24	27	33

✓	52.3	52.6	52.2	54.2
	10.4	10.1	9.5	8.5
	70	43	36	34

S.W. Cor Lower Step Ho LT sta 93+70



Fairview

Sta	+	π	-	Elev
BM	0.24	974.03 ²¹		973.79 ⁹⁷
TP	5.51	970.59	9.13	965.08 974.90

0+55

/

✓

+50

79+00

966.47
4.12 969.91

Jan 9, 1959

83

LT

RT

E. End Door Sill Ho #1867 W Larp

65.7	65.7	66.2	66.4	66.7	66.8	66.8	66.1	65.7	64.5
4.9	4.9	4.4	4.2	3.9	3.8	4.0	4.5	4.9	6.1
24	20	17	13	8		9	16	21	27

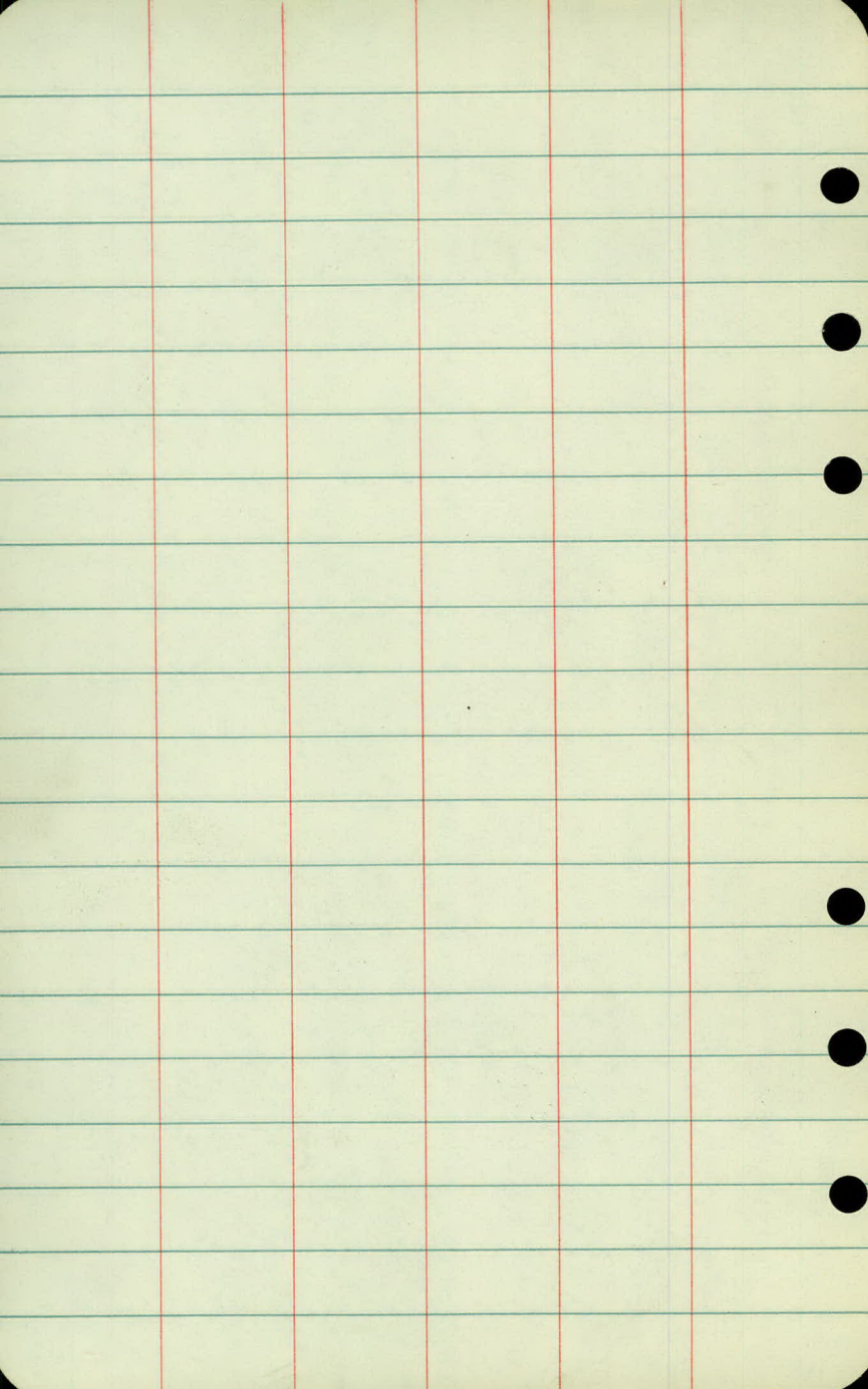
65.4	65.6	66.5	66.8	66.8	65.3	65.7	66.1	66.1	66.0	64.5
5.2	5.0	4.1	3.8	3.8	5.3	4.9	4.5	4.5	4.6	6.1
26	31	34	44	50	50	46	43	54	36	29

65.5	65.5	66.1	66.5	66.7	66.8	66.6	66.2	65.0	65.0	65.8
5.1	5.1	4.5	4.1	3.9	3.8	4.0	4.4	5.6	5.6	4.8
29	19	16	13	7		11	21	25	27	33

67.0	67.4	67.3			64.8	65.0	65.3	65.5
3.6	3.2	3.3			5.8	5.6	5.3	5.1
35	46	50			50	47	45	43.5

65.6	65.3	66.2	66.7	66.8	66.9	66.9	66.3	65.1	65.1	65.6
5.0	5.3	4.4	3.9	3.8	3.7	3.7	4.3	5.5	5.5	5.0
29	22	17	10	5		8	20	24	26	31

67.2	67.6	67.6			64.9	65.1	65.4	65.5	65.4
3.4	3.0	3.0			5.7	5.5	5.2	5.1	5.2
34	45	50			50	48	45	43.5	39



X-Street

X-sections

Tatum St

Sta + π - Elev

BM 3.27 977.24 973.97

BM 3.42 978.60 2.06 975.18

70+61.91 $\neq$ Totum

0+27

14.05
4.55

+55

✓

1

80

RF

Top MH £

					7A.7
	73.9	73.A	73.A	X	3,90k
>	51	52	52		34
	25	38	50		Wick

Sta + π - Elev

978.60

⁵⁰
1 + ~~00~~ ? +

✓

BM

0.11 978.49 (978.49)

Jan 9, 1959

81

Lt

St

X

RT

72.6	72.6	73.6	73.8	74.1	74.1	74.0	73.9	72.8	72.8	74.2
6.0	6.0	5.0	4.8	4.5	4.5	4.6	4.7	5.8	5.8	4.9
22	18	15	13	7		7	14	18	22	25

73.7	73.5	73.4	73.4
------	------	------	------

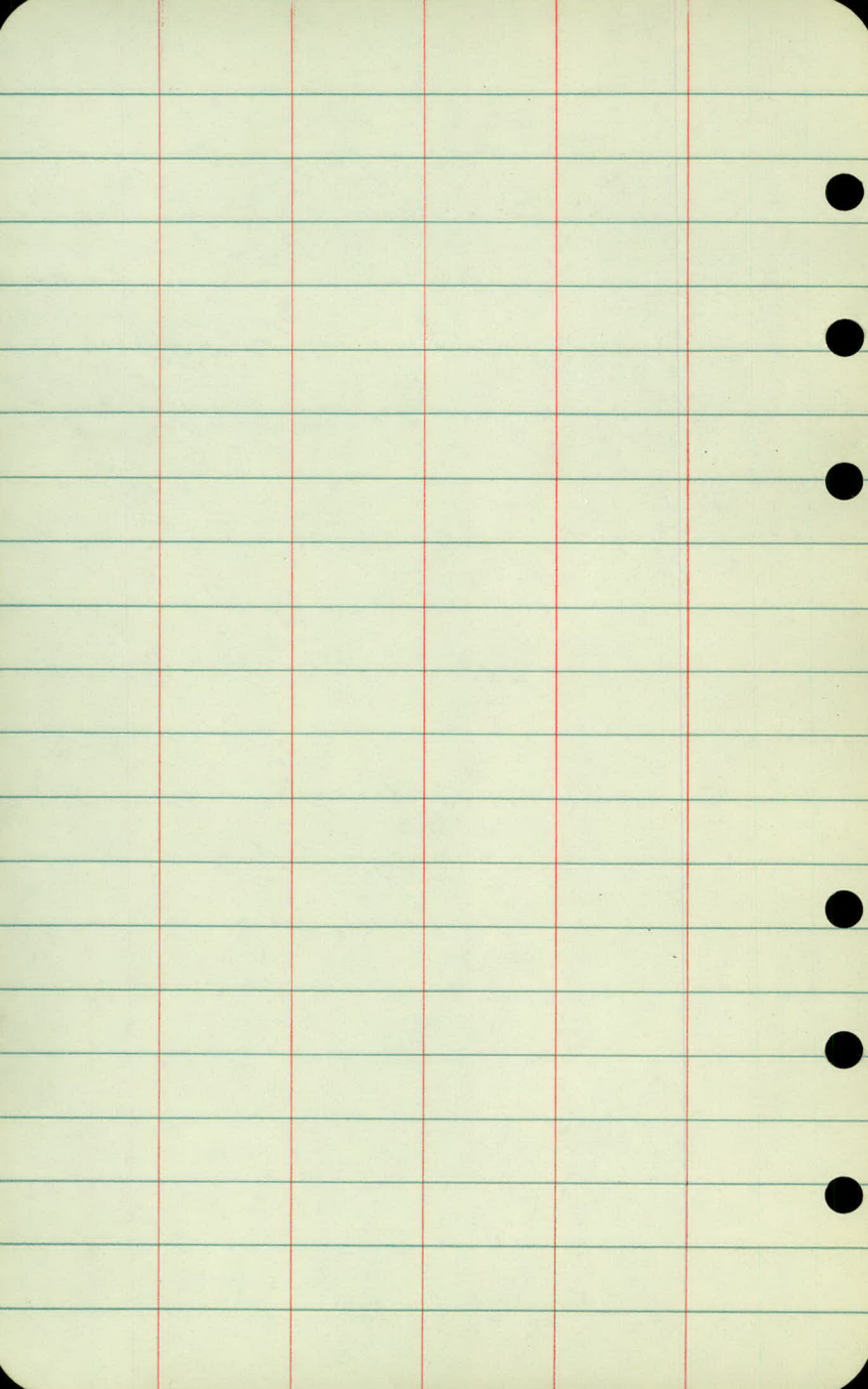
X

74.7	74.4
------	------

4.9	5.1	5.2	5.2
25	33	44	50

3.86	4.2
48	39

S.W. Cor Lower Step front office Lt. Sta 67+00



Fry Street

Sta 96 + 69.7 = ± Fry

Sta + π - Elev

BM 3.84 960.57

956.73

0 + 55

✓

/

✓

+ 50

Sta 96+00

4.83 955.74

Jan 7, 1959

85

Top N.W. Cor Lower step 1694 Warp on terrace

54.6	54.7	55.4	55.6	55.7	55.6	55.4	55.3	55.4	55.4	55.4
60	59	52	50	49	50	52	53	52	52	54
30	24	17	12	5		5	10	11	12	15

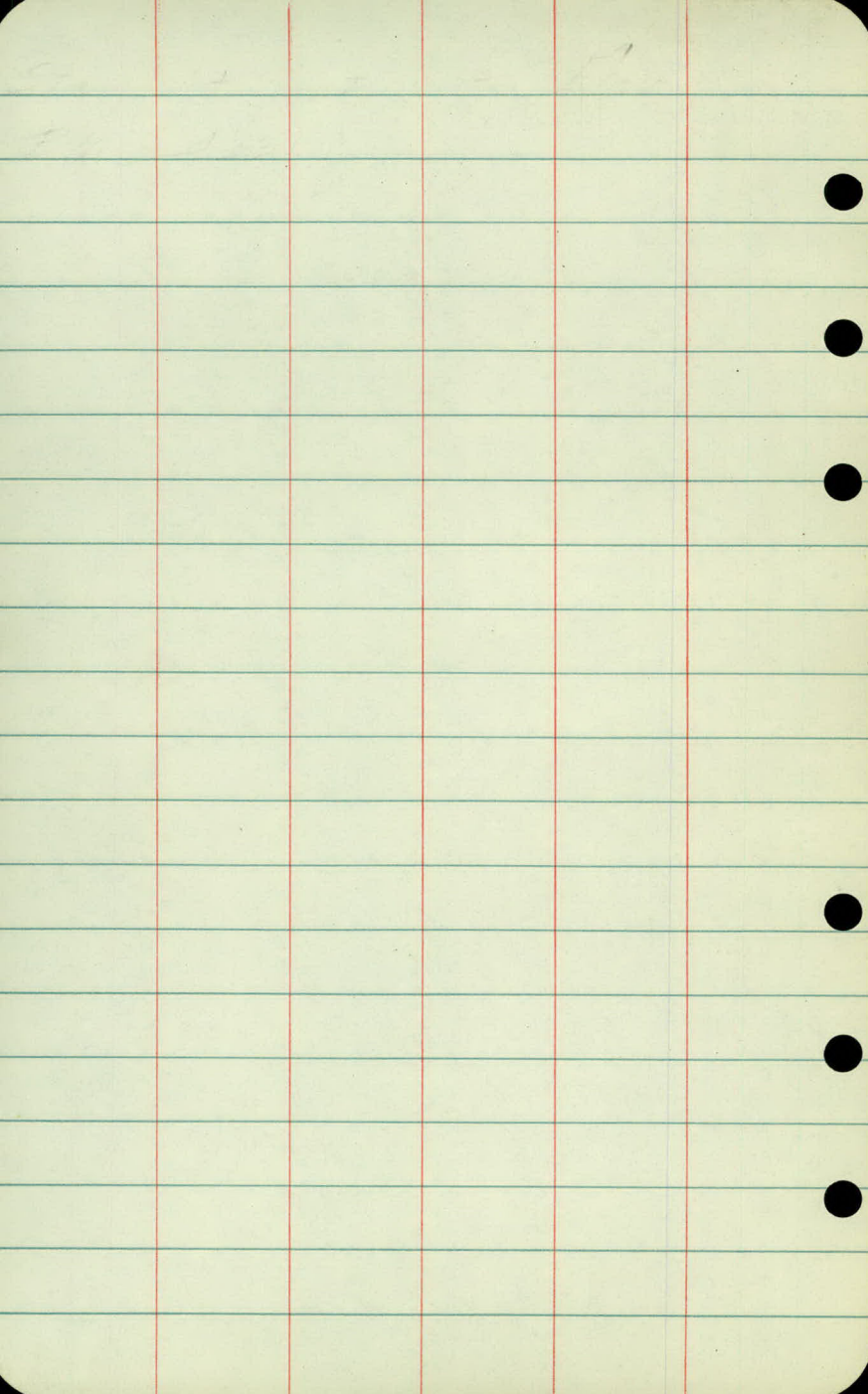
54.5	54.6	54.4		54.4	54.4	54.5	54.6	54.7
6.1	6.0	6.2	✓	6.2	6.2	6.1	6.0	5.9
35	39	50		50	40	29	24	20

54.8	54.9	55.3	55.4	55.5	55.5	55.4	55.3	55.5	55.6
58	57	53	52	51	51	52	53	51	51
28	24	21	18	11		5	9	11	13

55.1	54.7	54.7		54.3	55.0	55.3	55.2
5.5	5.9	5.9	✓	6.3	5.6	5.3	5.4
31	43	50		50	40	30	21

55.1	55.0	55.4	55.5	55.9	55.8	55.7	55.8	55.2	55.2	54.8
55	56	52	51	47	48	49	48	54	54	58
29	23	21	19	12		8	9	18	30	42

55.3	55.2	55.2		54.6
5.3	5.4	5.4	✓	6.0
31	43	50		50



Jan 9, 1957

86

St. Marys Ave

$\pm = \text{Sta } 99 + 95.4$

Sta + π - Elev

BM 4.33 961.06

956.73

0+55

✓

/

✓

+50

Sta 100+00

5.45 955.61

Jan 9, 1959

87

LT

AT

Top N.W. Cor Lower Step 1644 W. Larp.

56.1	55.8	56.1	55.A	55.7	55.7	55.6	56.0	55.9	55.9	56.0
50	53	50	57	5A	5A	55	51	52	52	51
27	16	15.5	15	8		15	15	16	31	38

56.1	56.2
50	49
40	50

56.1
50
50

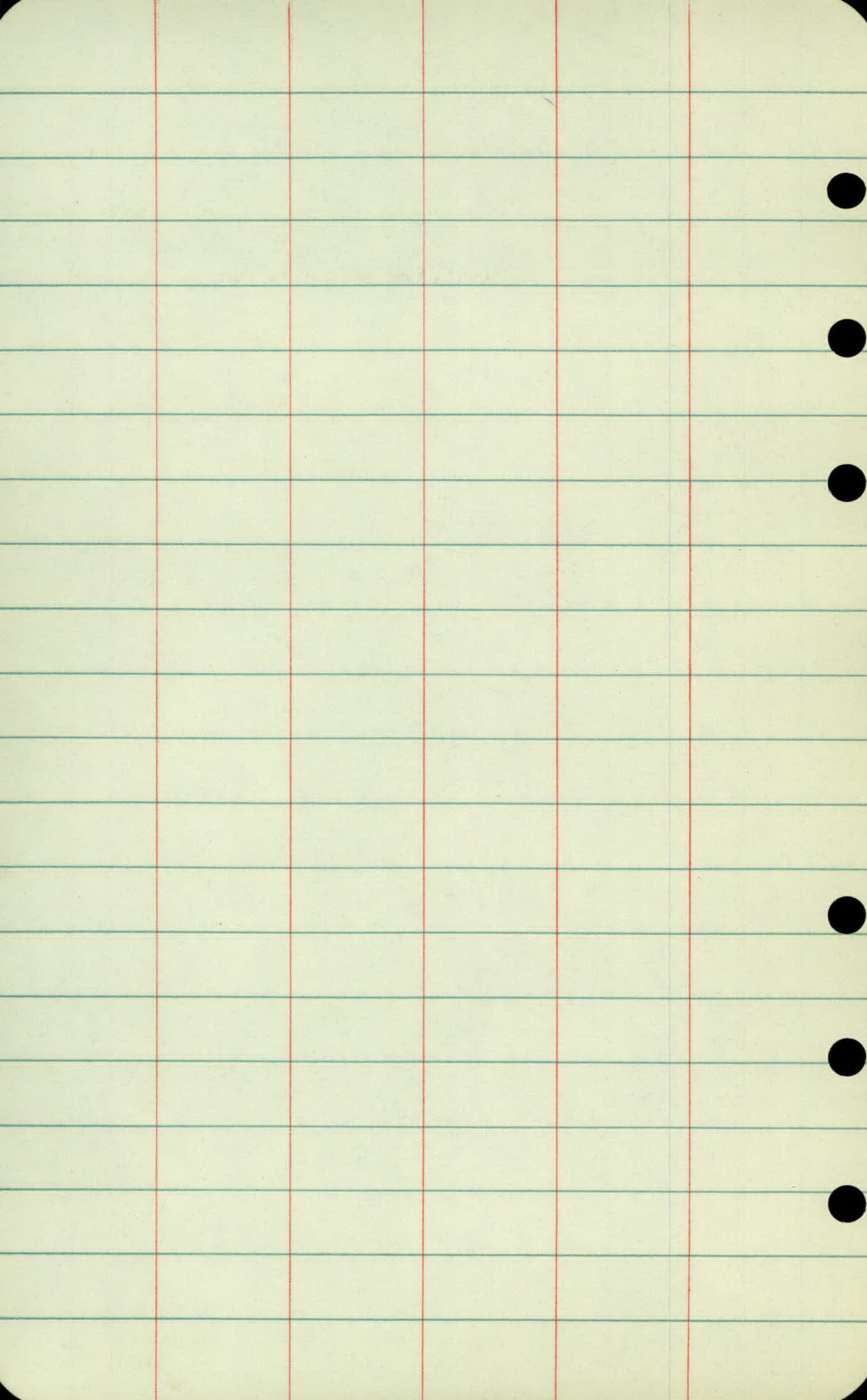
56.8	56.6	56.5	56.3	56.3	56.A	56.0	56.A	56.7	56.9	57.1
4.3	4.5	4.6	4.8	4.8	4.7	5.1	4.7	4.4	4.2	4.0
31	28	16	15	9		15	16	26	40	50

56.8	56.7
4.3	4.4
40	50

57.6	57.2	57.2	56.9	57.1	57.2	57.0	56.7	57.3	57.2	56.9
3.5	3.9	3.9	4.2	4.0	3.9	4.1	4.4	3.8	3.9	4.2
31	28	16	14	7		7	13	15	26	33

57.7	57.5
3.4	3.6
43	50

57.1	57.1
40	40
50	44



FX
RG
KP
JH

Jan. 12, 1959 88

Cleveland Ave.

Sta	+	π	-	Elev.
BM	5.78	98548		(979.70)

0+00 S. Line of School Prop.

✓

+50

✓

/

89

15.9 17.8 17.9 18.4 17.8 17.9 18.0 ✓ 17.9 17.7 18.3 17.8 17.7 15.6

76.4 76.5 76.4

75.6 75.5 75.7

99	100	9.8
50	34	27

77.1 76.4 76.4 78.0 78.1 78.2 78.1 77.8 76.1 76.2 76.0

8.4	9.1	9.1	7.5	7.4	7.3	7.4	7.7	9.4	9.3	9.5
28	24	22	19	12		12	20	23	26	34

$\gamma \gamma^3$
 $\gamma \gamma^2$

→ 8.2	8.3
31	50

75.9
9.6
50

7.9 7.4 7.4 7.4 7.4 7.4 7.3 7.3 7.9 7.2

76	8.1	8.1	7.1	7.1	7.05	7.15	7.2	8.6	8.3
27	25	23	20	12		12	20	23	26

27.9
 27.8

7.6	7.7
31	50

76.7 76.9

8.8 8.6
50 34

Sta + π - Elev

985.48

1+50

✓

2

✓

+09.5

✓

2+64.5 £ Larpeur

Jan 12, 1955

90

LT

RT

78.1	78.1	79.0	78.9	79.0	78.9	78.8	78.5	78.8	78.8
24	24	6.5	6.6	6.5	6.6	6.7	7.0	7.7	7.7
25	22	21	12		12	17	20	21	23

79.1	79.7	78.9
6.4	6.3	6.6
28	31	50

79.7	79.9	78.3
7.8	7.6	7.2
50	34	25

78.9	78.9	79.7	79.7	79.8	79.7	79.5	78.7	78.7
6.6	6.6	5.8	5.8	5.73	5.8	6.0	6.8	6.8
25	23	22	12		12	20	22	23

79.7	79.9	79.6
5.8	5.6	5.9
27	31	50

78.8	79.0	78.9
6.7	6.5	6.6
50	34	26

78.9	78.9	79.9	79.9	79.9	79.8	79.6	79.0	78.9
6.6	6.6	5.6	5.6	5.55	5.7	5.9	6.5	6.6
25	23	21	12		12	20	22	30

80.3	80.2	79.9
5.2	5.3	5.6
27	31	50

79.0	78.7
4.5	4.8
50	34

Sta + X - Elev

985.48

3+19.5

✓

+50

✓

4

Jan 12, 1959 91

LT

80.1	80.1	80.6	81.0	81.0	81.0	80.7	80.4	80.1
5.4	5.4	4.9	4.5	4.5	4.5	4.8	5.1	5.4
25	23	17	8		10	17	22	25

81.0	81.1
4.5	4.4
31	50

79.2	79.2	79.7
6.3	6.3	5.8
50	35	32

80.3	80.2	80.8	81.1	81.2	81.1	80.9	80.3	80.0
5.2	5.3	4.7	4.4	4.3	4.4	4.6	5.2	5.5
27	23	19	7		10	18	24	33

80.9	81.5	81.3	81.5
4.6	4.0	4.2	4.0
31	34	35	56

79.4	79.4
6.1	6.1
50	36

81.3	80.3	80.3	80.9	81.4	81.6	81.3	81.0	80.6	80.2
4.2	5.2	5.2	4.6	4.1	3.9	4.2	4.5	4.9	5.3
31	27	23	20	11		7	18	20	24

81.4
4.1
50

79.5	79.6	80.2	80.1
6.0	5.9	5.3	5.4
50	35	31	29

Sta + π - E/ev.

985.48

4+50

✓

Sta 54+00 Long

19'
6.38 979.10

Lt.

£

Jan. 12, 1959

Rt

92

80.3 80.2 80.9 81.4 81.7 81.4 81.1 80.2 80.3 80.0

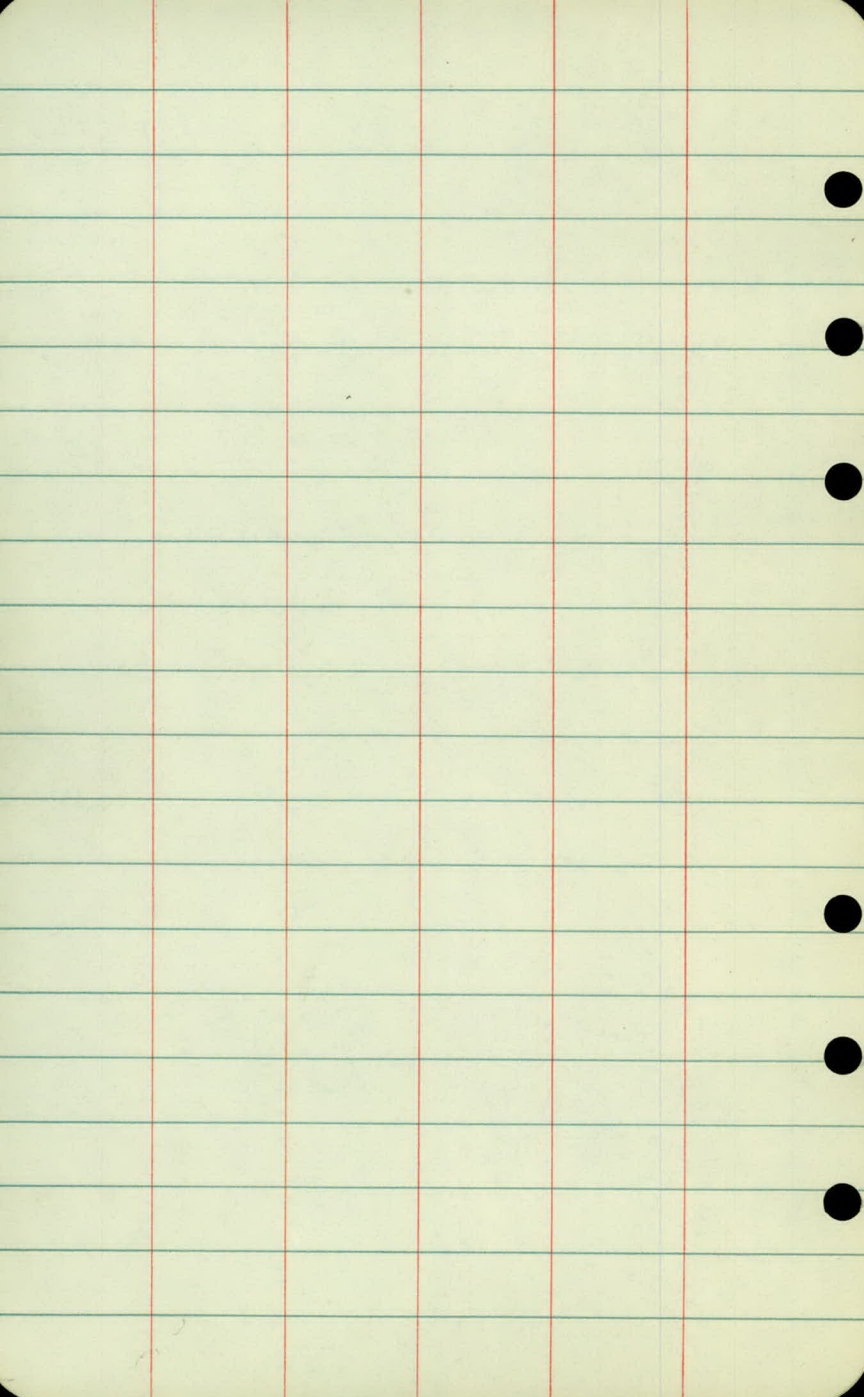
52 53 46 41 38 41 44 53 52 55
26 22 18 11 12 17 22 26 32

80.9 81.0 80.6 80.8

4.6 4.5 4.9 4.7
29 31 34 50

79.4 79.5

6.1 6.02
50 35



X-Section
of
Sanitary Sewer M.H. Elev.

Sta	+	π	-	Elev
BM	6.35	986.04		979.69

52+30

BM	6.35	979.69	979.69
----	------	--------	--------

93+54 M.H. L+

R6

JH

JH

Lt.

L

Rt

6

Feb 6, 1959

Corner Cleveland & Larp.

Top NW Cor Bottom Step of School SW

79.2	79.7	80.9	81.1	81.33	81.2	81.0	80.8	80.0
------	------	------	------	-------	------	------	------	------

6.8	6.3	5.1	4.9	4.71	4.8	5.0	5.2	6.0
-----	-----	-----	-----	------	-----	-----	-----	-----

26	24	21	10		10	17	22	27
----	----	----	----	--	----	----	----	----

79.2	80.4	81.3	81.2		80.1	80.7	79.1	79.1
------	------	------	------	--	------	------	------	------

6.8	5.6	4.7	4.8		5.9	5.3	6.9	6.9
-----	-----	-----	-----	--	-----	-----	-----	-----

28	31	34	43		44	34	31	30
----	----	----	----	--	----	----	----	----

81.4

81.4

79.6

79.2

4.6

4.6

6.4

6.8

114

67

71

83

44

34

Top N.W. Cor Bottom Step of School on

SW Cor. Cleveland & Larp. Aves.

Sta	+	π	-	Elev
BM	2.93	981.41		(978.48)

62+35			5.80	975.61
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65+52			6.38	975.03
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66+00			4.39	977.02 $\neq$
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BM	1.12	975.03		973.91
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76+16			6.54	68.49
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78+86			9.13	65.90
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76+00			5.30	69.8 $\neq$
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BM	3.95			961.54 47
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86+04			4.63	
-------	--	--	------	--

89+58			5.96	
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88+00				60.9 $\neq$
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Feb 13, 1959

C.

Top S.W. Cor. Lower Step Front of office
Lt. Sta 67+00

Top MH 29' Lt.

Top MH 29.5' Lt.

E. End Front door Sill Ho # 1867 W Larp.

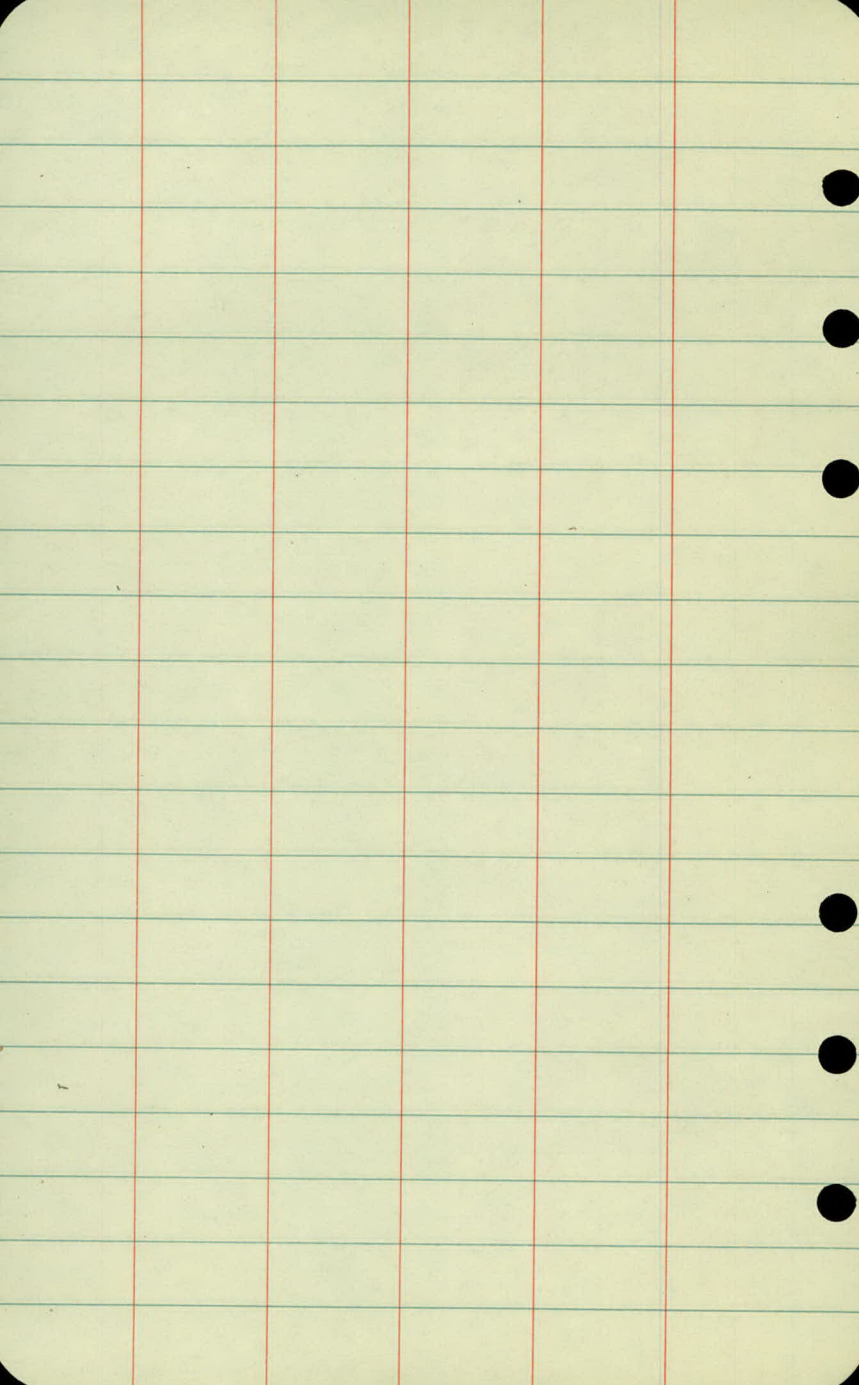
Top MH 27' Lt

Top MH 27' Lt

N.W. Cor Top Step Ho # 1750

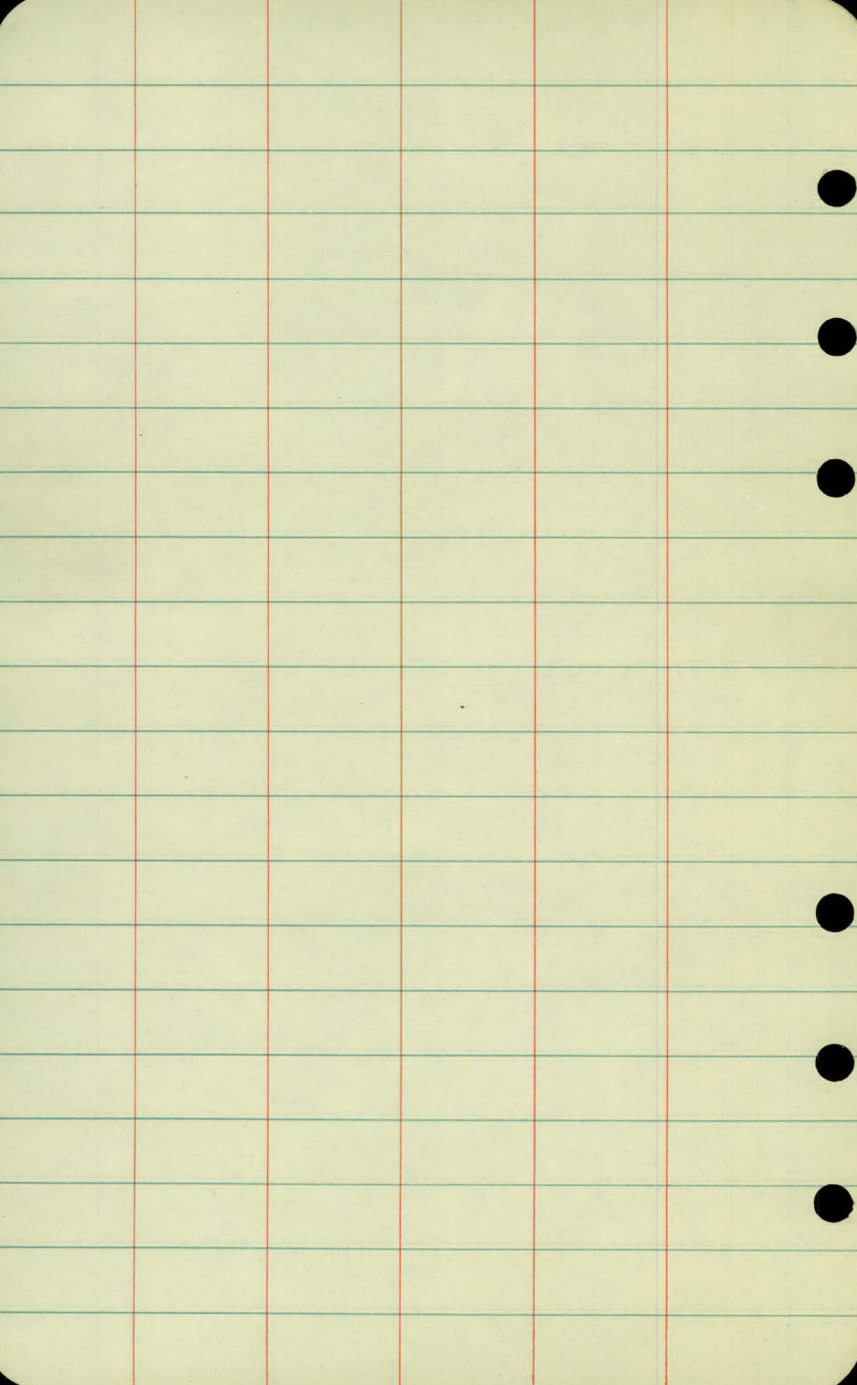
Top MH 24.5' Rt

Top MH 26' Rt.



Feb 16, 1959

c



FK
RL
RR
DF
OP

July 9, 1959

1

Larpentau

59-30

Water Main Location

Sta

62+19.97

Elbow Water Main
32.71' Lt

July 8, 1957

2

