

Dr. 9 Bk. 11

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

Plan Survey

Mc Menemy
From Co Rd "F" To Co Rd "G"

Road Acc't. No. _____

Date Filed 2-6-59

File Dr. 9 Bk 11

1
Mc MENEMY St

Co. Rd "F" to Co. Rd "G"

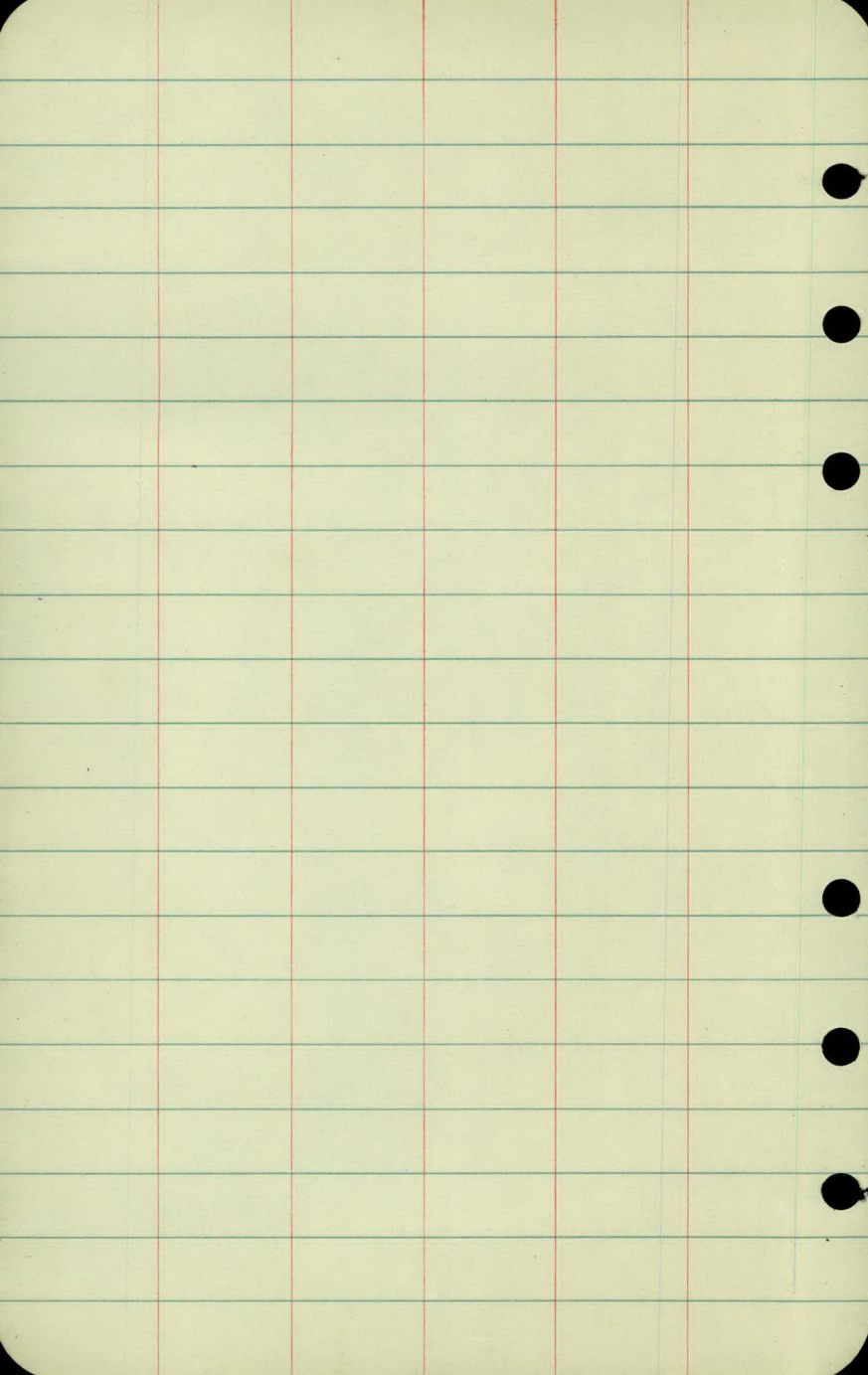
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Alignment 1-5
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Rec

4/18/57

1:45 PM



April 5, 1957

2

Alignment

Sta Point Δ L Δ R

24+62.63 $\pm$ Track

(13+35.76)

13+36.33 P.O.T.

0+00 $\pm$ Co Rd F. West

April 3, 1957

±

3

58.40 Rt. Beg-1' Curve
Spike

51° 21'

1x2

26.3

Best Spike

P.P. in Yard

Transformer
Pole on Co Rd F

TP 0 65.69

32.22 0 PP

Mount.

82° 09'

Arc Lt 0

Sta Point ΔL ΔR

29+00 P.O.T.

(26+25.82)

26+26.00 P.I.

$0^{\circ}48'$

FA
RG
KP
JT

April 8, 1957
± Cool Clear 25°

4

East Spike

disk
18" 0

95.82

E 1/4 Cor Sec 19-30-22 →

Monit.

34.39

62.07

disk
24" 0

disk
PP

Sta Point ΔL ΔR

(52+57.54)

52+58.67 $\pm$ Co Rd "G"

5

5

Disk
24"0

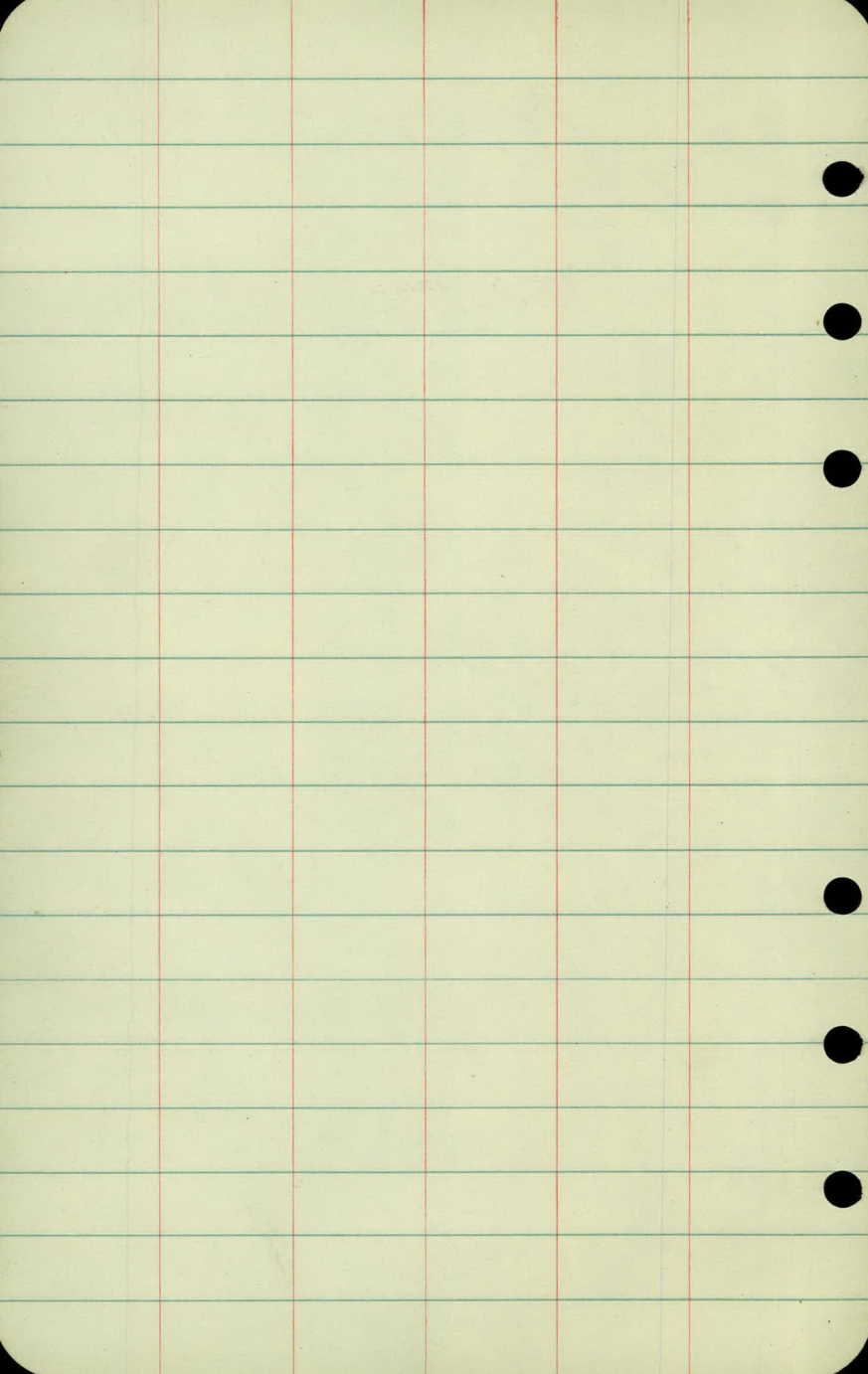
51.38



Bolt

95.00

Disk
30"0



April 9, 1957

6

Topography

4 Pothole ~~Brush~~ Road ~~Brush~~
 $\frac{+12}{15}$ $\frac{17}{7}$ $\frac{3}{14}$ $\frac{20}{32}$

+55 ~~B. Brush~~ +74 ~~B. Pothole~~
 $\frac{8-17}{}$ $\frac{28}{}$
 $\frac{+14}{27}$ $\frac{121}{13}$

3 Road ~~Brush~~ 105 ~~stp-22~~
 $\frac{5}{12}$ $\frac{24}{35}$ $\frac{193}{31}$ $\frac{143}{33}$ $\frac{189}{RT}$ $\frac{131}{34}$

2 Road ~~Brush~~
 $\frac{8}{11}$ $\frac{23}{31}$
 $\frac{+98}{30}$ $\frac{178}{29}$

1 Road ~~Brush~~
 $\frac{9}{10}$ $\frac{20}{33}$
 $\frac{+39}{23}$

+30 $\frac{TP}{58}$ +57 $\frac{ER}{8}$ +17 ~~Brush~~ +26 ~~stp-23~~ +18 ~~stp-23~~
0 +104 $\frac{BR}{55}$ +21 $\frac{POR}{24}$ +106 $\frac{Ent}{RT}$

-06 $\frac{Edge BT}{50}$ -03 $\frac{ER}{9}$ -04 $\frac{PP}{32}$
-50 $\frac{Fe}{50}$ -30 $\frac{ER}{50}$ -22 $\frac{Edge BT}{}$ -58 $\frac{ER}{50}$ -29 $\frac{BR}{34}$
-79 $\frac{Arc. Lt.}{23}$ -62 $\frac{Line Fe}{29}$ -59 $\frac{POR}{23}$ -71 $\frac{POR}{22}$ -83 $\frac{TP}{40}$
-98 $\frac{BR}{11}$ -28 $\frac{Fe}{28}$ -11 $\frac{BT}{8}$ -96 $\frac{BR}{8}$

9

Brush
33 10Road
6 12~~Pothole~~
~~18 50~~+93 $\frac{PP}{34}$ +86 $\frac{E. Brush}{30}$

+54 Pothole-62

+63 $\frac{P.Hole}{25}$ 8 Pothole-61 $\frac{Brush}{37}$ ~~14~~Road
4 12Brush
21 33+88 $\frac{P. Brush}{28}$ +96-51p-30

139-51p-19

+30-51p-21

+24 $\frac{P. Brush}{15}$ ~~22~~+164 $\frac{51p}{30}$
+50 $\frac{51p}{26}$ ✓Road
4 13+91 $\frac{E. Brush}{32}$ +89 $\frac{51p}{30}$

+64-51p-32

+26 $\frac{51p}{30}$

6

Road
4 15Brush
25 37+96 $\frac{PP}{32}$ +79-51p-31+55 $\frac{E. Pothole}{40-80}$

+87-51p-50

+30 $\frac{E. Brush}{14}$ +36 $\frac{51p}{34}$ +50-51p-36+25 $\frac{Pothole}{15}$

+33-51p-34

5

Pothole
12 17 8Road
3 15Brush
20 29+68 $\frac{51p}{14}$ +54 $\frac{51p}{13}$

4

Road
3 14

April 9, 1957

£

8

Lowland

Pothole

14

$$\begin{array}{r} \text{Road.} \\ 10 \ 8 \end{array}$$

$$\begin{array}{r} \text{R. Tie Ent} \\ 180 \ \text{LT} \end{array}$$

13

$$\begin{array}{r} \text{Road.} \\ 7 \ 9 \end{array}$$

12

$$\begin{array}{r} \text{E. Brush} \\ 100 \ 17-27 \end{array}$$

$$\begin{array}{r} \text{Road.} \\ 7 \ 9 \end{array}$$

$$\begin{array}{r} \text{Ent} \\ 183 \ \text{RT} \end{array}$$

$$\begin{array}{r} \text{PP} \\ 196 \ 34 \end{array}$$

$$\begin{array}{r} \text{12" A} \\ 170 \ \text{BR} \end{array}$$

$$\begin{array}{r} \text{12" A} \\ 111 \ \text{BX} \end{array}$$

$$\begin{array}{r} \text{1" Plum} \\ 110 \ \text{BX} \end{array}$$

11

$$\begin{array}{r} \text{Brush} \\ 33 \ 17 \end{array}$$

$$\begin{array}{r} \text{Road} \\ 7 \ 10 \end{array}$$

$$\begin{array}{r} \text{Ent} \\ 196 \ \text{RT} \end{array}$$

169-stp-30'

$$\begin{array}{r} \text{E. Fe} \\ 147 \ 29 \end{array}$$

$$\begin{array}{r} \text{E. Brush} \\ 184 \ 27-23 \end{array}$$

+28-stp-29'

+17-stp-26'

10

$$\begin{array}{r} \text{Brush} \\ 32-12 \end{array}$$

$$\begin{array}{r} \text{Road} \\ 6 \ 11 \end{array}$$

$$\begin{array}{r} \text{Brush} \ \text{Fe} \\ 117-30 \ 30 \end{array}$$

$$\begin{array}{r} \text{12" X? Vite} \\ 141 \ 18 \end{array}$$

$$\begin{array}{r} \text{E. Pathole} \\ 183 \ 53-60 \end{array}$$

$$\begin{array}{r} \text{Ent 12" X 20cm} \\ 125 \ 30-26-21 \end{array}$$

$$\begin{array}{r} \text{E. Fe} \\ 180 \ 29 \end{array}$$

$$\begin{array}{r} \text{42" Cott. stp.} \\ 143 \ 17 \end{array}$$

$$\begin{array}{r} \text{B. Brush} \\ 132 \ 19-30 \end{array}$$

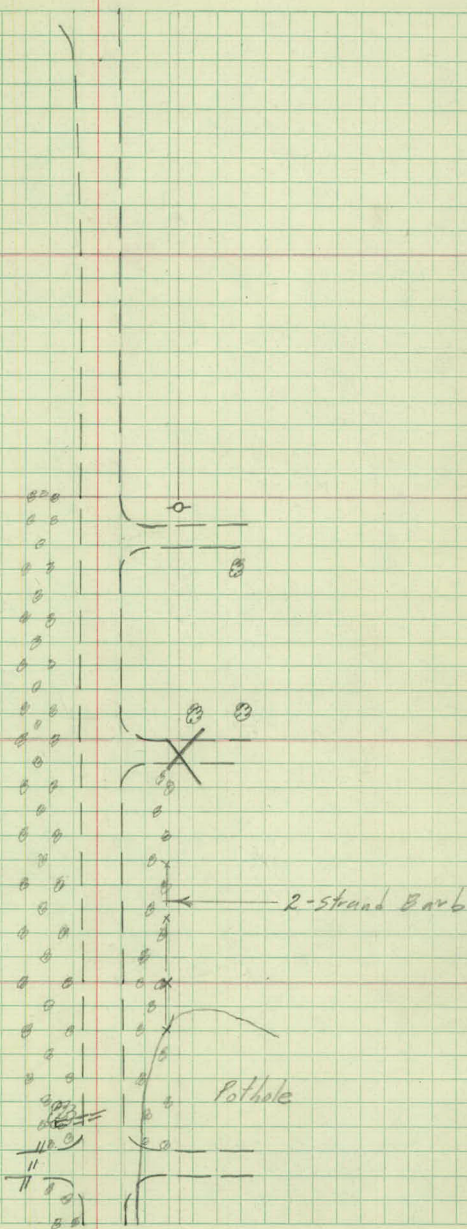
9

$$\begin{array}{r} \text{Road} \\ 6 \ 12 \end{array}$$

$$\begin{array}{r} \text{Ent} \\ 124 \ \text{RT} \end{array}$$

April 9, 1957

9



19

$$\begin{array}{r} \text{Brush} \\ 26 \end{array} \begin{array}{r} \text{X} \\ 13 \end{array}$$

$$\begin{array}{r} \text{Road} \\ 6 \end{array} \begin{array}{r} 12 \end{array}$$

$$\begin{array}{r} \text{Brush} \\ 16 \end{array} \begin{array}{r} \text{X} \\ 38 \end{array}$$

$$+27 \begin{array}{r} \text{stp} \\ 24 \end{array}$$

$$+35 \begin{array}{r} \text{PP} \\ 38 \end{array}$$

18

$$\begin{array}{r} \text{Brush} \\ 27 \end{array} \begin{array}{r} \text{X} \\ 15 \end{array}$$

$$\begin{array}{r} \text{Road} \\ 8 \end{array} \begin{array}{r} 11 \end{array}$$

+21-End Brush-21-35

$$\begin{array}{r} \text{Brush} \\ 17 \end{array} \begin{array}{r} \text{X} \\ 46 \end{array}$$

179-stp-21'

$$+62 \text{ - Beg. Brush} \\ 22-30'$$

17

$$\begin{array}{r} \text{Brush} \\ 28 \end{array} \begin{array}{r} \text{X} \\ 16 \end{array}$$

$$\begin{array}{r} \text{Road} \\ 9 \end{array} \begin{array}{r} 8 \end{array}$$

$$\begin{array}{r} \text{Brush} \\ 19 \end{array} \begin{array}{r} \text{X} \\ 42 \end{array}$$

$$+23 \begin{array}{r} \text{A"O stp.} \\ 20 \end{array}$$

+64-stp-28'

16

$$\begin{array}{r} \text{Brush} \\ 30 \end{array} \begin{array}{r} \text{X} \\ 17 \end{array}$$

$$\begin{array}{r} \text{Road} \\ 9 \end{array} \begin{array}{r} 6 \end{array}$$

$$\begin{array}{r} \text{Brush} \\ 15 \end{array} \begin{array}{r} \text{X} \\ 23 \end{array}$$

$$+74 \text{ Beg Fe} \\ 33$$

$$+36 \begin{array}{r} \text{PP} \\ 35 \end{array}$$

$$+56 \begin{array}{r} \text{B. Brush} \\ 19 \end{array} \begin{array}{r} \text{X} \\ 32 \end{array}$$

$$+28 \begin{array}{r} \text{B. Brush} \\ 16 \end{array}$$

15

$$\begin{array}{r} \text{Road} \\ 11 \end{array} \begin{array}{r} 4 \end{array}$$

$$+30 \begin{array}{r} \text{Ent} \\ 38 \end{array}$$

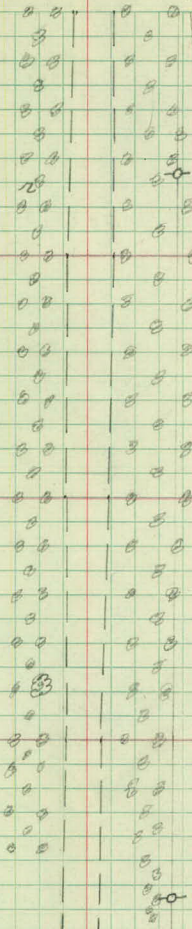
14

$$\begin{array}{r} 10 \end{array} \begin{array}{r} 8 \end{array}$$

April 9, 1957

£

10



~~Lowland~~

11

24

$$\begin{array}{r} \text{Road} \\ 87 \end{array}$$

$$+93 \quad \frac{\text{Rtic Ent}}{\text{Rt}}$$

$$+88 \quad \frac{\text{TP}}{43}$$

$$+71 \quad \frac{\text{end Fe}}{37}$$

$$+33 \quad \frac{\text{Beg Fe}}{37}$$

$$+39 \quad \frac{\text{PP}}{36}$$

23

$$\begin{array}{r} \text{Road} \\ 88 \end{array}$$

22

$$\begin{array}{r} \text{Road} \\ 710 \end{array}$$

$$+80 \quad \frac{\text{IRON}}{33}$$

$$+180 \quad \frac{\text{end Fe}}{37}$$

$$+18 \quad \frac{\text{PP}}{36}$$

$$+05 \quad \frac{\text{Ent}}{\text{Rt}}$$

21

$$\begin{array}{r} \text{Road} \\ 610 \end{array}$$

$$+97 \quad \frac{\text{L. Brush}}{1720}$$

$$+43 \quad \frac{\text{Beg Fe}}{30}$$

$$+37 \quad \frac{\text{End Brush}}{1829}$$

20

$$23- \quad \frac{\text{Brush}}{3}$$

$$\begin{array}{r} \text{Road} \\ 610 \end{array}$$

$$\frac{\text{Brush}}{1629}$$

19

$$\begin{array}{r} \text{Road} \\ 612 \end{array}$$

$$02 \quad \frac{\text{end Fe}}{33}$$

11

29

	195	$\frac{STP}{12}$	199	$\frac{STP}{15}$
+54	14	STP	174	STP
+16	11	STP	150	$\frac{STP}{12}$
+12	$\frac{STP}{12}$	+12	$\frac{STP}{10}$	114

28	$\frac{Fe}{29}$	$\frac{Road}{59}$	$\frac{Fe}{33}$
----	-----------------	-------------------	-----------------

+13 ~~E. Bush~~ 17-22

27 ~~22-14~~ $\frac{Fe}{25}$ $\frac{Road}{6-10}$ $\frac{Fe}{33}$

+95 $\frac{STP}{14}$

+75 $\frac{STP}{16}$

+160 ~~E. Bush~~ 16-23

+132 $\frac{PP}{37}$

26

	$\frac{Fe}{25}$	$\frac{Road}{710}$	$\frac{Fe}{33}$
--	-----------------	--------------------	-----------------

+14 $\frac{Fe Cor}{27}$ +36 $\frac{R.Tie Fe}{17}$ +57 $\frac{Fe Cor}{38}$

+103 $\frac{RR Xing Sign}{14}$

+134 $\frac{R.Tie Fe}{11}$

25

	+100	$\frac{\Phi Ent}{28}$	$\frac{Road}{94}$
--	------	-----------------------	-------------------

+71 $\frac{E. Planks}{5}$

+58 $\frac{E. Planks}{15}$

+40 $\frac{PP}{37}$

+80 $\frac{R.Tie Ent}{17}$

+134 $\frac{TP}{13}$

+24

	+127	$\frac{RR Xing Sign}{7}$	+20	$\frac{\Phi Ent}{29}$
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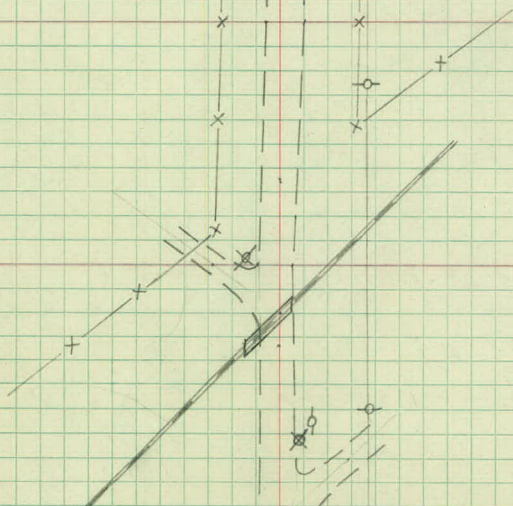
April 10, 1957

12

A-Strand B. →

42"

56' W. W. Fe



34

$\frac{Fe}{30}$	$\frac{Brush}{30}$	$\frac{Road}{10}$	$\frac{Fe}{31}$
	19	6	

+139 $\frac{x-Fe}{30}$

+117 $\frac{R.T. \times Fe}{Rt}$

~~110~~ ~~$\frac{STP}{40}$~~

33

$\frac{Fe}{28}$	$\frac{Brush}{30}$	$\frac{Road}{9-6}$	$\frac{Fe}{31}$
	18		

+199 $\frac{STP}{21}$

+130 $\frac{PP}{35}$

+190 $\frac{STP}{18}$

32

$\frac{Fe}{29}$	$\frac{Brush}{29}$	$\frac{Road}{7-7}$	$\frac{Fe}{31}$
	18		

~~113~~ ~~$\frac{STP}{20-28}$~~

31

$\frac{Fe}{27}$	$\frac{Road}{6-9}$	$\frac{Fe}{31}$
-----------------	--------------------	-----------------

30

$\frac{Fe}{28}$	$\frac{Road}{5-9}$	$\frac{Fe}{33}$
-----------------	--------------------	-----------------

+11

~~20~~ $\frac{STP}{15}$

+26 $\frac{PP}{37}$

+106 $\frac{STP}{16}$

29

$\frac{Fe}{28}$	$\frac{Road}{4-9}$	$\frac{Fe}{33}$
-----------------	--------------------	-----------------

April 10, 1957

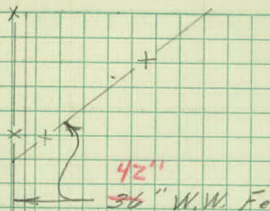
£

13

Scattered Woods

2-1/2 x 1/2

Cultivated



39

$$\frac{\text{SwP}}{35}$$

$$\frac{\text{Fc}}{28}$$

$$\frac{\text{Road}}{88}$$

$$\frac{\text{Fc}}{32}$$

$$+127 \frac{\text{PP}}{32}$$

38

$$\frac{\text{SwP}}{25}$$

$$\frac{\text{Fc}}{28}$$

$$\frac{\text{Road}}{99}$$

$$\frac{\text{Fc}}{32}$$

$$+97 \frac{\text{Possible X-Drain}}{\text{Buried}}$$

37

$$\frac{\text{SwP}}{25}$$

$$\frac{\text{Fc}}{28}$$

$$\frac{\text{Road}}{89}$$

$$\frac{\text{Fc}}{32}$$

36

$$\frac{\text{SwP}}{30}$$

$$\frac{\text{Fc}}{28}$$

$$\frac{\text{Road}}{89}$$

$$\frac{\text{Fc}}{33}$$

+53

~~Exp Brush~~

$$+31 \frac{\text{PP}}{33}$$

+25 B. Swamp

85

35

$$\frac{\text{Fc}}{28}$$
~~Brush~~

$$\frac{\text{Road}}{87}$$

$$\frac{\text{Fc}}{32}$$

+96

STP

$$+80 \text{ STP}$$

22

+11 STP

25

+10 STP

21

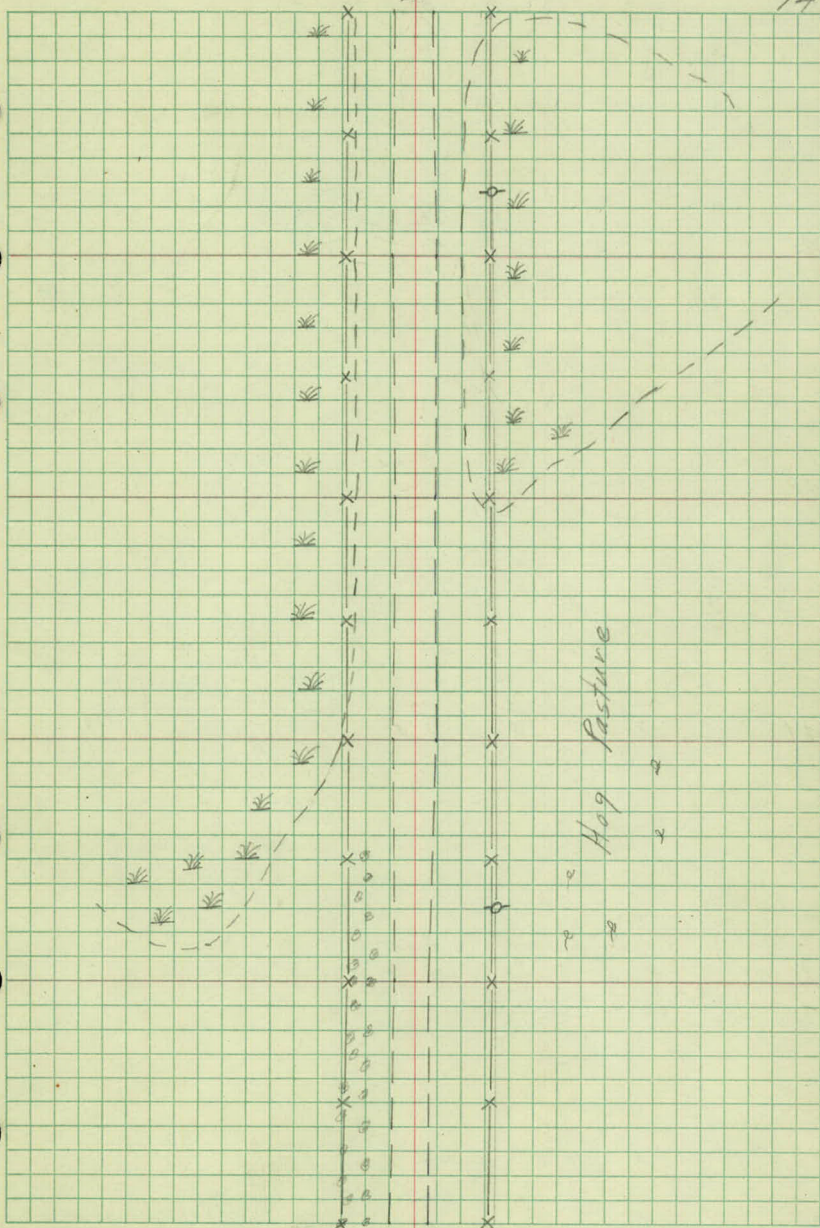
34

$$\frac{\text{Road}}{186}$$

April 11, 1957

14

£



44 $\begin{array}{r} \text{Fc} \\ 34 \end{array}$ $\begin{array}{r} \text{Brush} \\ 34 \end{array}$ $\begin{array}{r} \text{Road} \\ 142 \end{array}$ $\begin{array}{r} \text{Fc} \\ 33 \end{array}$
 $+98 \frac{\text{StP}}{24}$

$+80 \frac{\text{StP}}{25}$ $+76 \frac{\text{StP}}{25}$

43 $\begin{array}{r} \text{Fc} \\ 33 \end{array}$ $\begin{array}{r} \text{Brush} \\ 24 \end{array}$ $\begin{array}{r} \text{Road} \\ 132 \end{array}$ $\begin{array}{r} \text{Fc} \\ 32 \end{array}$

$+89 \frac{\text{A.E.}}{20}$

$+05 \frac{\text{X-Fc}}{31}$

42 $\begin{array}{r} \text{Fc} \\ 33 \end{array}$ $\begin{array}{r} \text{Brush} \\ 27 \end{array}$ $\begin{array}{r} \text{Road} \\ 132 \end{array}$ $\begin{array}{r} \text{Fc} \\ 31 \end{array}$

$+29 \frac{\text{StP}}{21}$ $+95 \frac{\text{StP}}{27}$ $+25 \frac{\text{PD}}{32}$
 $+05 \frac{240}{53}$

41 $\begin{array}{r} \text{Brush} \\ 27 \end{array}$ $\begin{array}{r} \text{Fc} \\ 32 \end{array}$ $\begin{array}{r} \text{Road} \\ 114 \end{array}$ $\begin{array}{r} \text{Fc} \\ 32 \end{array}$

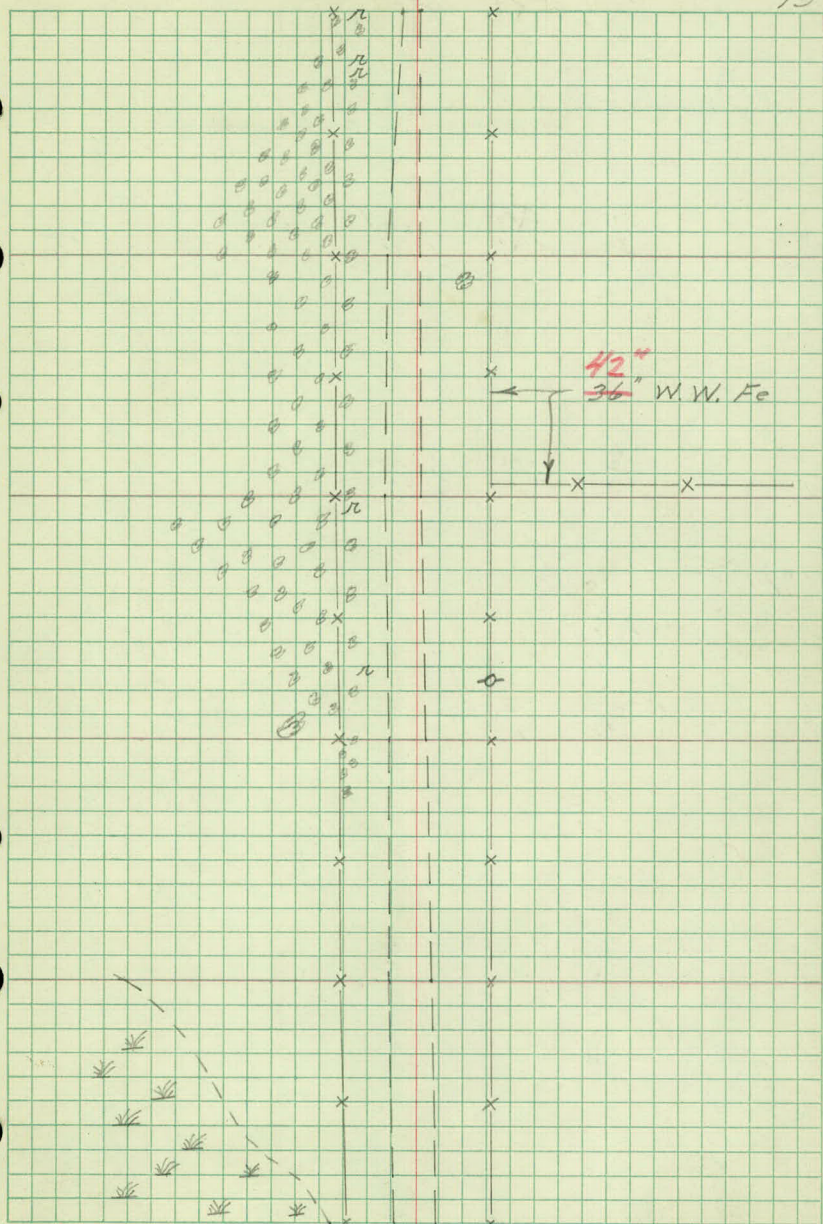
$+77 \frac{\text{Brush}}{29}$

40 $\begin{array}{r} \text{StP} \\ 120 \end{array}$ $\begin{array}{r} \text{Fc} \\ 31 \end{array}$ $\begin{array}{r} \text{Road} \\ 117 \end{array}$ $\begin{array}{r} \text{Fc} \\ 32 \end{array}$

39 $\begin{array}{r} \text{StP} \\ 33 \end{array}$ 28 98 32

April 15, 1957

15



49 Pothole Fc Brush Road Fc
 38 35 31 21 9 5 38

+38 B. Pothole
 60

48 Fc Brush Road Fc
 33 40 19 10 1 36

+32 Stp
 25

+27 PP
 30

47 Brush Fc Road Fc
 41 23 34 12 - 2 36

+99 Ent
 17

+77 Stp +39 Stp
 26 35

+50 X-Fc
 36

+37 Stp
 25

+25 B. Fc
 35

+31 Stp
 26

+23 Stp
 27

46 Brush Fc Road
 38 29 34 15 - 1

+59 S.W. Cor Ho
 70

+40 Stp
 31

+42 Ent
 RT

45 Fc Road
 34 13 0

+90 B. Brush
 45 31

+12 B. Brush +2 Stp
 29 23

+84 Fc Cor
 33

+24 Stp
 22

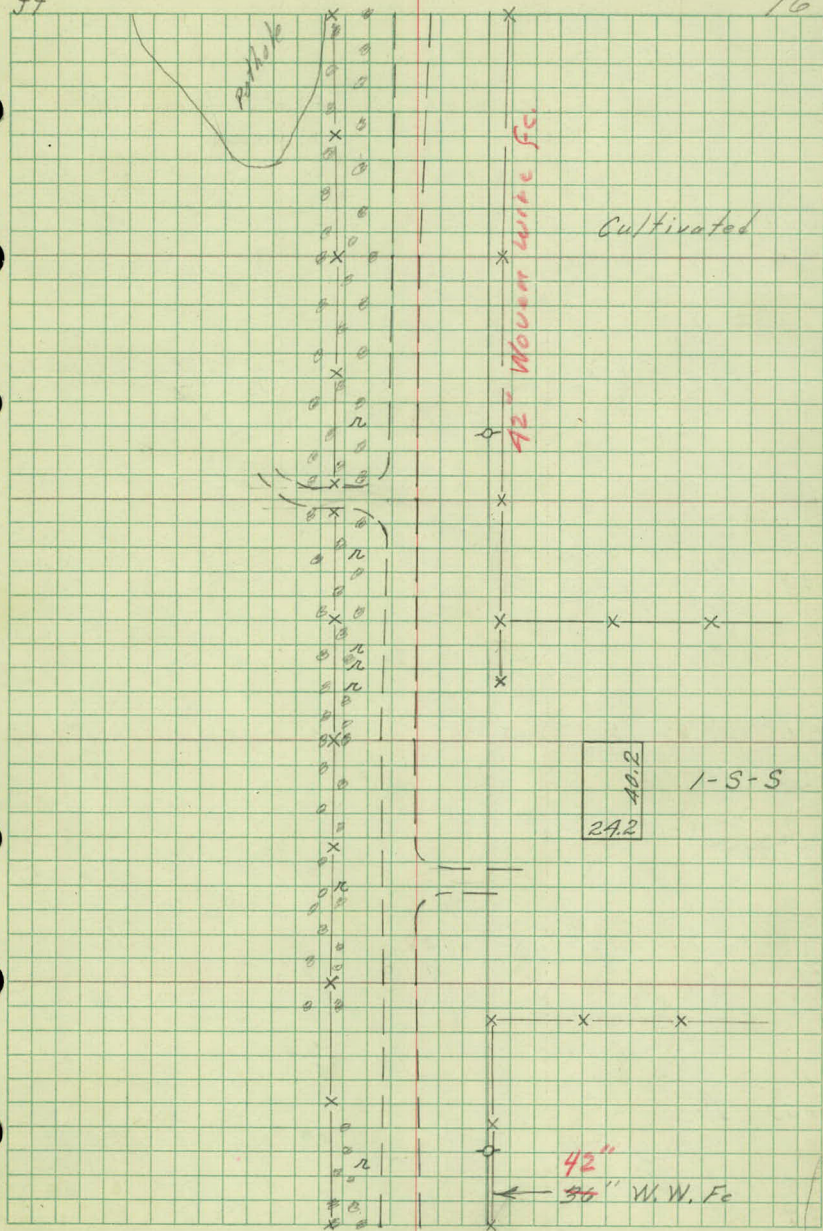
+31 PP
 31

44 Fc Brush Road Fc
 34 34 23 14 2 33

FK
RG
KP
JT

April 12, 1957
Cool Clear Bright 20°

16



£

+44 $\frac{ER}{50}$

+68 $\frac{Edge Pave}{£}$

+44 $\frac{ER}{44}$

+44 $\frac{Beg Pave}{£}$

+09 $\frac{BR}{6}$

+17 $\frac{BR}{12}$

+06 ~~$\frac{Car Brush}{8}$~~

$\frac{Road}{6.8}$

52

+81 $\frac{R. Tie}{Fe Lt}$

+68 $\frac{16''}{38}$

+23 $\frac{STP}{18}$

+84 $\frac{Fe Cor}{35}$

+82 $\frac{Fe Cor}{33}$

+08 $\frac{24''}{49}$

+11 $\frac{STP}{26}$

+02 $\frac{24''}{44}$

51

$\frac{Fe}{35}$ ~~$\frac{Brush}{35}$~~

$\frac{Road}{8}$ $\frac{Fe}{6}$

$\frac{Fe}{34}$

+73 $\frac{24''}{48}$

+74 $\frac{STP}{19}$

+53 $\frac{28''}{50}$

+17 $\frac{STP}{23}$

+49 $\frac{PP}{28}$

+06 $\frac{22''}{38}$

50

$\frac{Fe}{34}$

~~$\frac{Brush}{35-20}$~~

$\frac{Road}{9}$ $\frac{Fe}{7}$

$\frac{Fe}{37}$

+01 $\frac{STP}{21}$

+94 $\frac{20''}{48}$

+88 $\frac{E. Pothole}{100}$

+97 $\frac{STP}{21}$

+97 ~~$\frac{Wood}{18}$~~

+83 $\frac{16''}{44}$

+92 $\frac{STP}{21}$

+99 $\frac{STP}{16}$

+53 $\frac{18''}{40}$

+79 $\frac{Tr. 16''}{52}$

+52 $\frac{STP}{22}$

+13 $\frac{STP}{17}$

+39 $\frac{STP}{22}$

+29 $\frac{STP}{20}$

+40 $\frac{STP}{20}$

49

$\frac{Pothole}{38}$ $\frac{Fe}{35}$

~~$\frac{Brush}{35-21}$~~

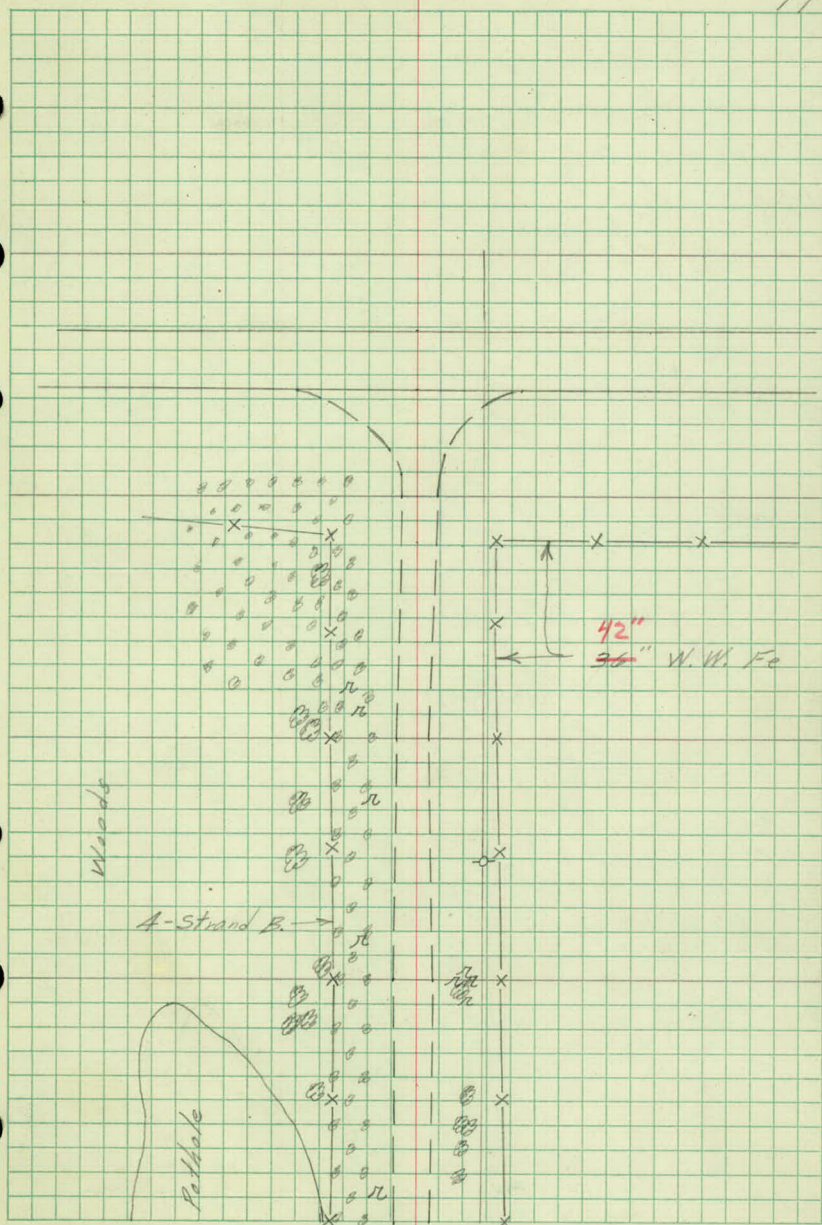
$\frac{Road}{9.5}$ $\frac{Fe}{38}$

+19 $\frac{STP}{19}$

+73 ~~$\frac{2'' Col}{20}$~~

April 12, 1957

17



Ent Culvert Lt Sta 9+25

X-Drain Sta 37+97

April 13, 1957

18

Bench Levels

Note: 1.0' Error on
T.P. 3

Sta	+	π	-	Elev.
BM	6.11	938.74 ⁵		932.635
T.P. ₁	0.38	931.30 ⁵	7.82	930.92 ⁵
BM	4.49	925.72 ⁵	10.07	921.23 ⁵ 921.23
BM			2.64	923.08 ⁵ 923.08
T.P. ₂	0.38 ⁵	918.24 ⁵	7.86 ⁵	917.86
T.P. ₃	<u>1.61</u> ⁵	906.51 ⁵⁰	13.35	904.89 ⁵
BM.			2.77	903.74 ⁷³ 904.74
T.P.	0.97 ⁵	895.53 ⁵⁵	11.95	894.56 ⁵⁵ 895.56
T.P.	8.10 ⁵	901.24 ²²	2.40	893.13 ¹²⁵
T.P.	11.01	911.67 ⁶⁵	0.58	900.66 ⁶⁴
BM	10.98 ⁵	918.76 ⁷⁴	3.89	907.78 ⁷⁶ 908.78
T.P.	0.12	914.34 ³²	4.54	914.22 ²⁰⁵
BM	4.63	913.61 ⁵⁹	5.36	908.98 ⁹⁶ 909.98
T.P.	12.31	925.38 ³⁶	0.54	913.09 ⁶⁵
T.P.	12.60	937.38 ³⁶	0.60	924.78 ⁷⁶
T.P.	1.16 ⁵	937.45 ⁴²	1.10	936.28 ²⁶
B.M.			5.19	932.26 ²³ 932.26
T.P.	2.52	927.22 ¹⁹	12.75	924.70 ⁶⁷
T.P.	9.75	933.08 ⁰⁵	3.89	923.33 ³⁰ 927.07 ^{or}
BM	2.81 ⁵	928.88	7.01	926.07 ⁰⁴ 927.07

FK
RG
KP
JT

April 11, 1951
Cold 18° Windy

19

U.S.G.S. N-5 1107' W. + 22' N. of McMenemy & "G"

~~Top Bolt~~ ^{gone} in West of McMenemy & Co. Rd "G"

Spike in PP SE. Cor. McMenemy & "G"

Spike in PP Rt Sta 41+25

Rock

Spike in 30" ^{oak} ~~out~~ 120' Lt Sta 30+80

Sta 23+88 43' Lt.

Spike in TP SW Cor. of McMenemy & 500 RR

11+96

Spike in Transformer Pole Sta. ~~24+18~~ 36' Rt.

Spike in Arc Lt. Pole SW. Cor. Co Rd F & McMenemy

Sta	+	π H.I.	-	Elev
		928.88		
T.P.	3.67	922.78 ⁵	9.77	919.11 ⁵
B.M			3.21	919.57 ⁵ (920.58)
BM	4.23	936.86		(932.635)
T.P.	0.44	930.65	6.65	930.21
BM	4.16	925.39 ³⁸	9.43	921.22 ⁵
TP	2.87	920.73 ⁷²	7.53	917.86 ⁸⁵ (917.86)
TP	0.71	908.68 ⁶⁷	12.76	907.97 ⁹⁶
BM			3.94	904.74 ⁷³
TP			13.12	895.56 ⁵⁵

April 11, 1957

20

Top S.W. Cor. Bottom Step 400' S + 150' E of
McMenemy St + Co. Rd. F.

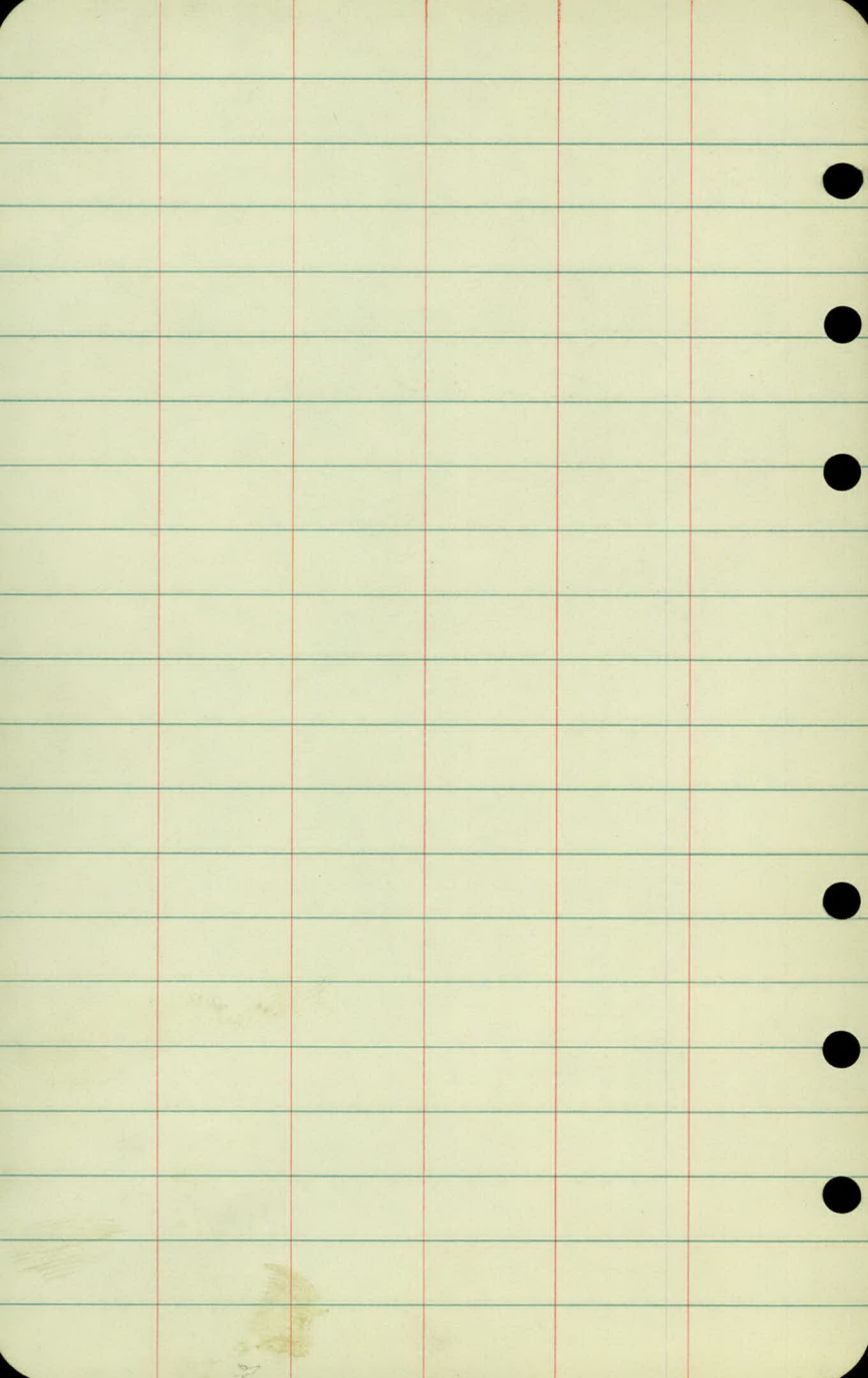
U.S. G.S. N-5 1107' W + 22' N. of McMenemy + G

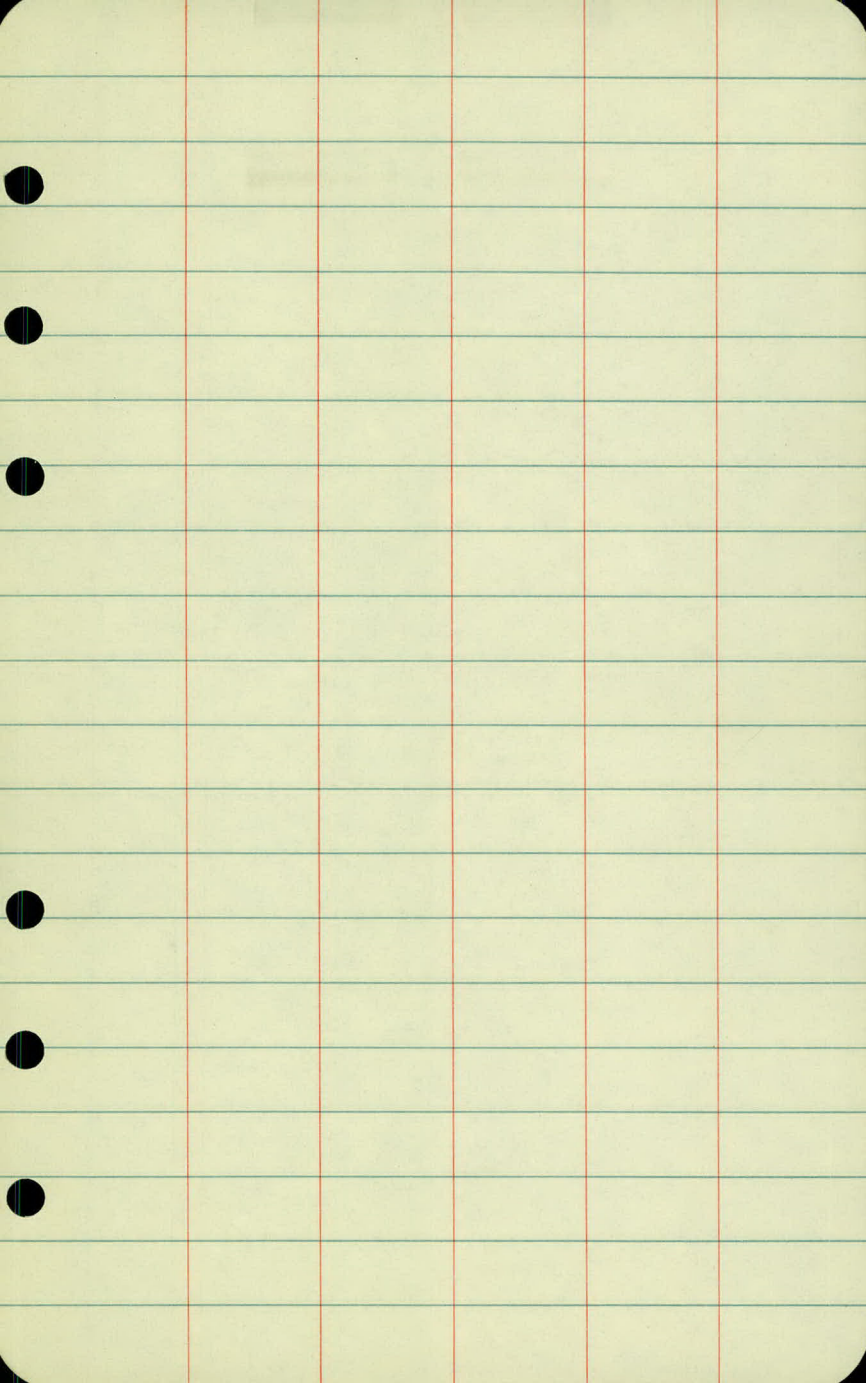
~~gone~~

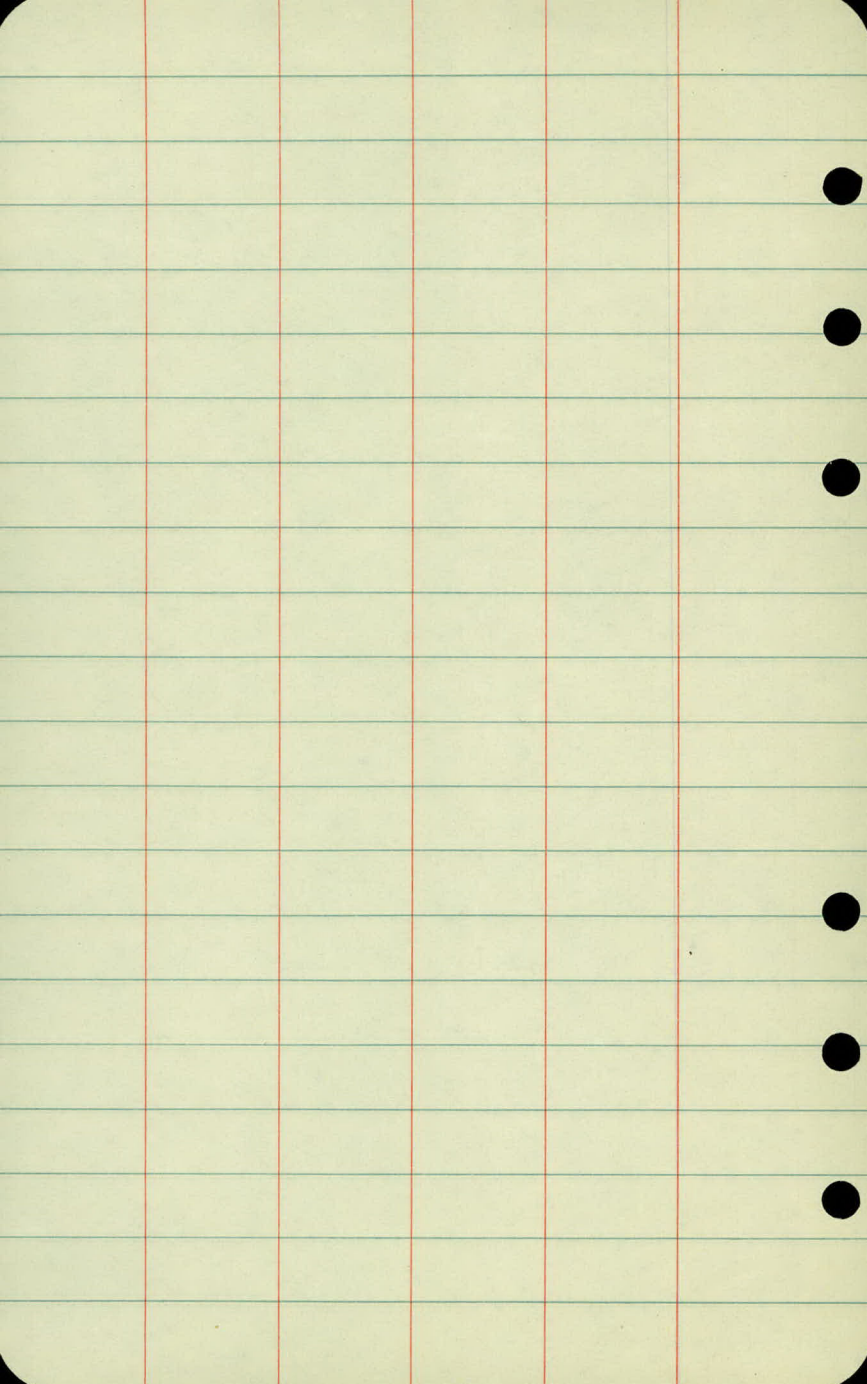
~~Top Belt in Mont E McMenemy + Co Rd 'G'~~

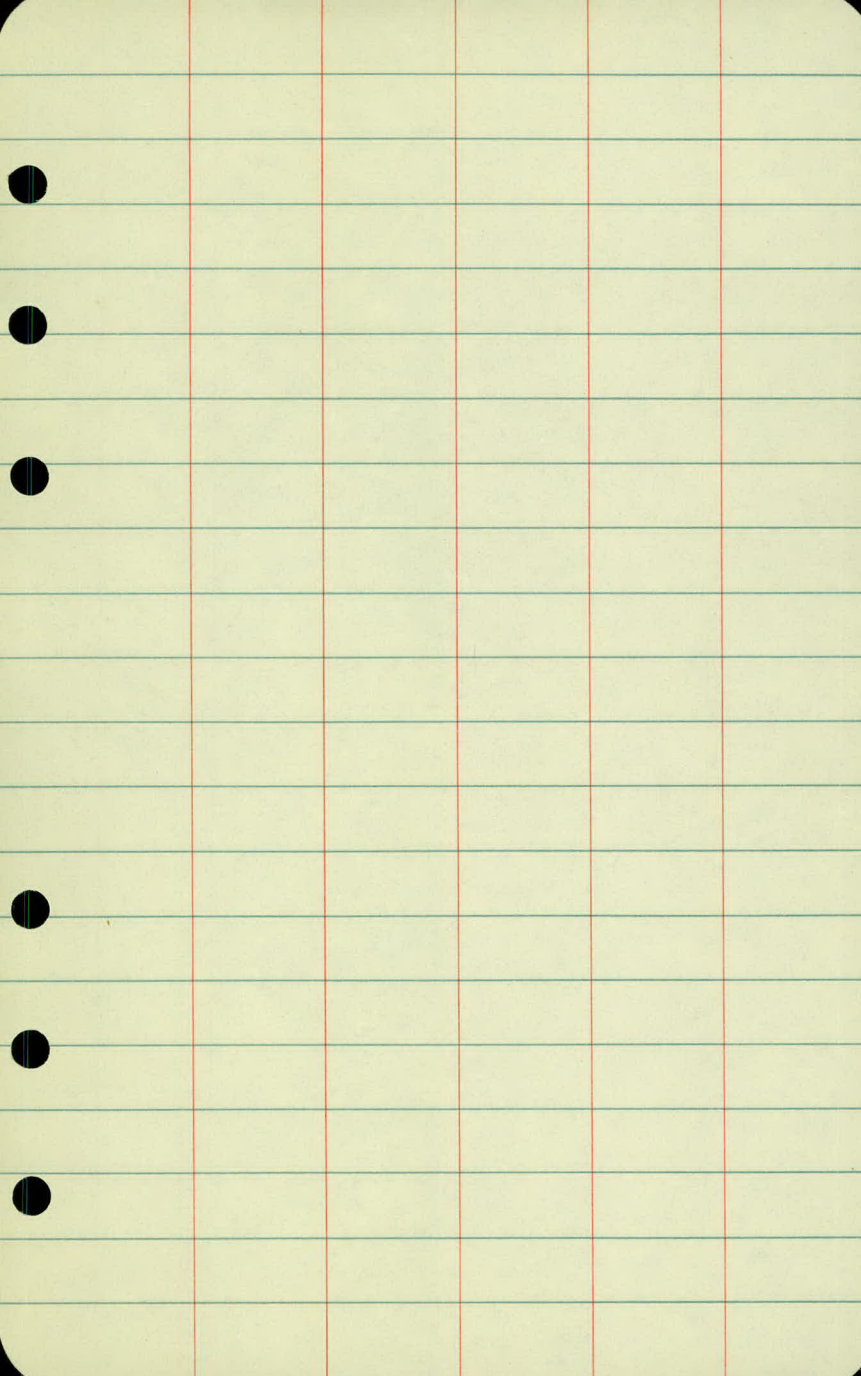
Spike in PP Rt Sta 91+25

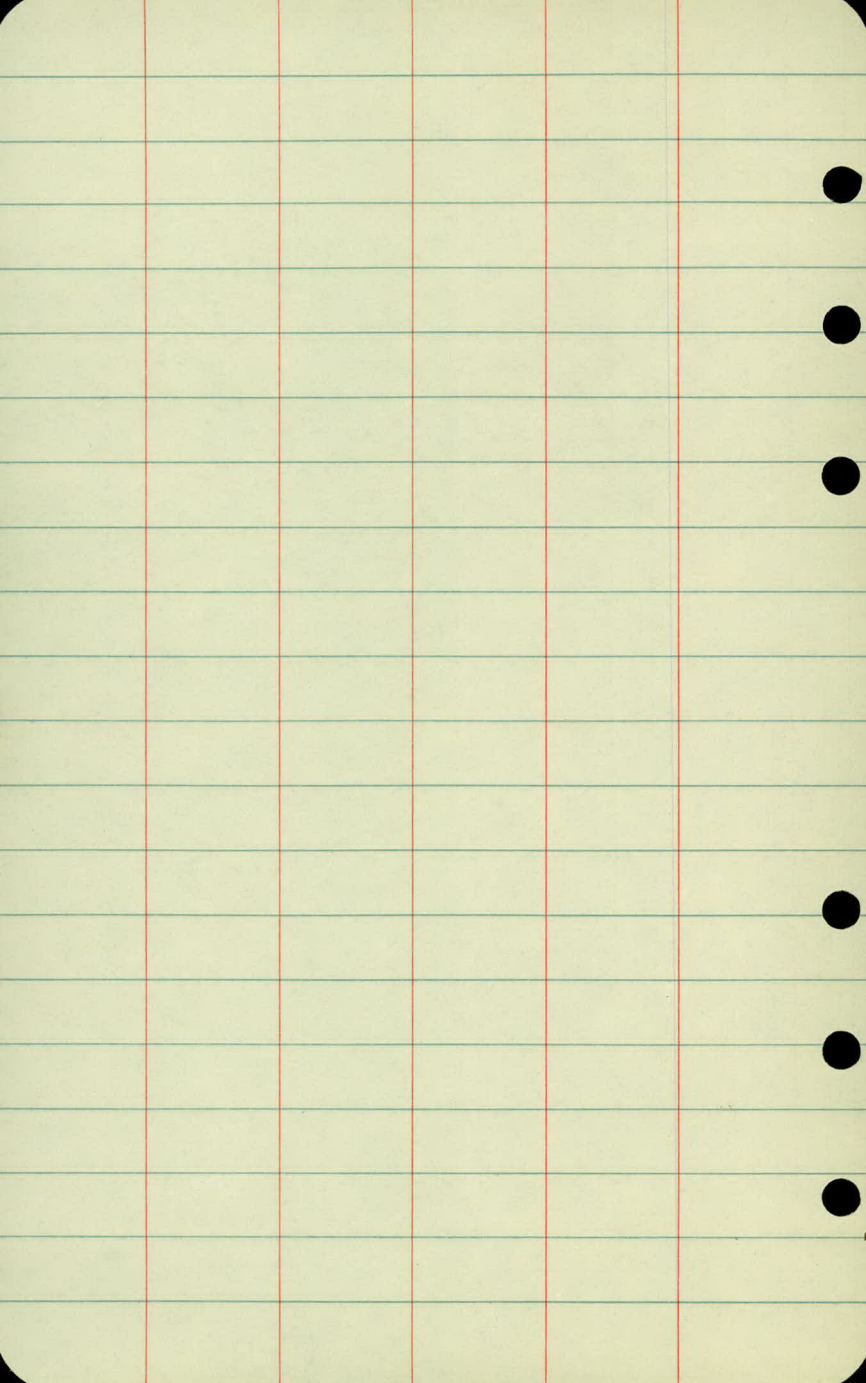
Rock











April 12, 1957

21

x-Sections

Sta + π - Elev

BM 11.02 938.08^{1.}

927.06

-150

13.5

24.6

-100

11.3

26.8

-70

9.8

28.3

-40

8.4

29.7

-34 $\pm$ Co R/F

✓

-27 Edge Pavc. Rt

April 12, 1957

22

Spike in Arc Lt. Pole S.W. Cor Co Rd "F" of Mc Menamy

36.2	35.1	33.7	31.8	30.4	29.1	27.7	26.9	26.1
1.9	3.0	4.4	6.3	7.7	9.0	10.9	11.2	12.0
100	75	50	21		22	44	62	87

37.3	38.1		23.8	24.7	25.7
0.8	0.0		14.3	13.4	12.4
135	163		200	150	99

30.8	30.0	28.0	27.0	26.3
7.3	8.1	10.1	11.1	11.8
	13	36	53	73

Sta + π - Elev

938.08

0-10

✓

0+00

+26

✓

TP 13.53 945.16 6.45 931.63

+40

April 12, 1937

34.3	33.6	32.5	31.4	31.0	30.3	30.1	29.5	28.1
3.6	4.5	5.6	6.7	7.1	7.8	7.7	8.6	10.0
50	35	15		8	14	15	25	34

26.6	28.0
11.5	10.1
50	40

34.4	34.0	32.8	31.8	31.1	31.0	30.9	30.1	30.1
3.7	4.1	5.3	6.3	7.0	6.5	5.2	4.0	3.0
50	39	15		12	19	25	36	50

33.7	33.5	33.2	33.4	32.9	32.3	32.2	31.9	31.3	30.8
4.4	4.6	4.9	4.7	5.2	5.8	5.9	2.2	1.8	1.3
65	50	32	13		10	19	23	27	33

36.6	36.5	36.2
1.5	1.6	1.9
50	37	35

Ment

42.1	34.0	33.3	33.3	33.1	32.4	32.7	32.5
3.1	11.2	11.9	11.9	12.1	12.8	12.5	12.7
39	32	25	13		14	15	18

Sta	+	π	-	Elev
-----	---	-------	---	------

		945.16		
--	--	--------	--	--

+40				
-----	--	--	--	--

✓				
---	--	--	--	--

+75				
-----	--	--	--	--

✓				
---	--	--	--	--

1+00				
------	--	--	--	--

✓				
---	--	--	--	--

Lt.			✓	Rt	24
42.8	42.8	42.5		36.3	37.1
2.4	2.4	2.7		8.9	8.1
54	75	100		83	64
				37.3	37.5
				7.9	7.2
				45	33
				10.1	10.1
				24	24

34.8
10.4
100

39.2	33.3	32.9	33.1	33.3	33.1	32.8	33.2	36.8
6.0	11.9	12.3	12.1	11.9	12.1	12.4	12.0	8.4
28	20	14	8	8	8	16	19	27

44.3	44.0	43.7	43.5	42.5	35.4	37.2	39.4	40.2
0.9	1.2	1.5	1.7	2.7	9.8	8.0	5.8	5.0
35	37	52	64	100	100	73	50	35

33.2	33.0	32.7	33.1	33.2	33.0	32.7	33.3	36.8
12.0	12.2	12.5	12.1	12.0	12.2	12.5	11.9	8.4
20	15	14	6		8	16	20	27

38.3	44.9	44.4	44.0	37.2	37.7	38.0	39.8	40.6
6.9	0.3	0.8	1.2	8.0	7.5	7.2	5.4	4.6
24	36	39	53	100	75	67	49	36

Sta	+	π	-	Elev
-----	---	-------	---	------

		945.16		
--	--	--------	--	--

1+00				
------	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

2+00				
------	--	--	--	--

Lt.

E

Rt.

25

42.0
3.2
100

42.2
3.0
96

42.9
2.3
71

✓

37.7
7.5
27

32.1
13.1
19

32.1
13.1
14

32.3
12.9
6

32.5
12.7
10

32.4
12.8
10

32.1
13.1
17

32.7
12.5
18

33.7
11.5
21

✓

41.9
3.3
34

41.5
3.7
39

40.9
4.3
61

41.3
3.9
81

39.6
5.6
87

38.8
6.4
69

39.2
6.0
46

38.7
6.5
34

34.0
11.2
24

✓

40.8
4.4
100

39.8
5.4
100

29.9
15.3
17

30.7
14.5
14

30.4
14.8
13

30.9
14.3
7

31.0
14.2
10

30.9
14.3
8

30.3
14.9
18

31.2
14.0
19

✓

29.9
15.3
19

35.6
9.6
26

40.4
4.8
35

40.1
5.1
47

37.8
7.4
71

37.0
8.2
49

36.3
8.9
37

33.5
11.7
27

32.2
13.0
24

✓

Sta	+	π	-	Elev
-----	---	-------	---	------

		945.16		
--	--	--------	--	--

2+00				
------	--	--	--	--

T.P.	8.89	941.82	12.23	932.93
------	------	--------	-------	--------

+33				
-----	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

Lt

Rt

Rt.

26

39.1	39.7	39.8	39.5	40.0
6.1	5.5	5.4	5.7	5.2
100	83	65	99	100

Rock

29.1	29.8	29.8	29.8	30.1	29.9	29.2	30.2	30.6
12.7	12.0	12.0	12.0	11.7	11.9	12.6	11.6	11.2
21	13	12	7		8	18	20	23

37.1	36.9	36.5	36.3	35.7	35.2	35.0	31.8	31.9
4.7	4.9	5.3	5.5	6.1	6.6	6.8	10.0	9.9
32	46	64	82	53	42	35	30	25

36.4	36.0	37.0	38.5	39.3
5.4	5.8	4.8	3.3	2.5
100	93	71	89	100

28.6	29.3	28.8	29.2	29.5	29.4	28.6	29.5	30.8
13.2	12.5	13.0	12.6	12.3	12.4	13.2	12.3	11.0
21	13	12	6		9	19	20	25

31.3	34.5	33.4	32.7	39.5	37.5	34.7	32.6	31.0
10.5	7.3	8.4	9.1	2.3	4.3	7.1	9.2	10.8
26	33	56	80	93	73	53	35	31

Sta	+	π	-	Elev
-----	---	-------	---	------

		941.82		
--	--	--------	--	--

T.P.	4.25	933.77	12.30	929.52
------	------	--------	-------	--------

3+00		933.77		
------	--	--------	--	--

✓

✓

+50

✓

Lt

E

Rt

27

Rock

26.2	26.9	26.5	27.0	27.2	27.2	26.5	26.5	27.3	28.1
9.6	6.9	7.3	6.8	6.6	6.6	7.3	7.3	6.5	5.7
16	11	10	4		11	17	19	21	31

26.2	25.2	25.2	25.0
7.6	8.6	8.6	8.8
23	27	42	57

33.8	32.0	28.9	27.7	28.1
0.0	1.8	4.9	6.1	5.7
66	58	44	35	34

26.4	25.3	24.3
7.4	8.5	9.5
80	70	65

20.6	20.5	20.8	24.4	25.1	25.2	25.1	22.9	22.4
13.2	13.3	13.0	9.4	8.7	8.6	8.7	10.9	11.4
56	38	20	9		11	21	26	38

20.5
13.3
85

30.8	28.2	23.5
3.0	5.6	10.3
80	73	55

Sta + π - Elev

933.77

4+00

✓

+50

✓

T.P.

9.45 924.32

B.M.

6.70 927.07 (927.06)

T.P.

8.76 933.08

924.32

5

FA
RG
KP
JT

Lt

April 15, 1957
Cloudy 38° Rt

28

19.3	23.5	23.8	23.9	24.0	20.5	21.1
14.5	10.3	10.0	9.9	9.8	13.3	12.7
12	7		13	21	28	43
pond						

28.4	25.0	22.1
5.4	8.8	11.7
85	73	59

19.2	22.7	23.1	23.2	23.0	20.3	20.4
14.6	11.1	10.7	10.6	10.8	13.5	13.4
15	8		12	20	25	42
pond						

28.7	24.3	20.8
5.1	9.5	13.0
80	66	50

Rock Sta 5+21 21' Rt.

Spike in Aicht. Pole SW Cor. Co. Rd F 1/2 McMenemy

Rock

17.8	19.2	20.1	23.1	23.2	23.4	23.3	20.5	20.4
15.3	13.9	13.0	10.0	9.9	9.7	9.8	12.6	12.7
19	WS 14	11	7		9	20	27	31

28.1	22.4
5.0	10.7
63	40

Sta	+	π	-	Elev
-----	---	-------	---	------

		933.08		
--	--	--------	--	--

5+50				
------	--	--	--	--

✓				
---	--	--	--	--

+75				
-----	--	--	--	--

✓				
---	--	--	--	--

TP	2.32	932.97	2.43	930.65
----	------	--------	------	--------

6				
---	--	--	--	--

April 15, 1957
April 16, 1957

PG
AP
JT

Lt

Rt.

29

19.1	20.8	23.1	24.4	23.9	24.2	24.3	24.7	24.3	24.5
14.0	12.3	10.0	8.7	9.2	8.9	8.9	8.8	8.4	8.8
32	23	16	9	6	13	20	21	25	30

17.9
15.2
40

✓

33.0
0.1
71
30.2
2.9
46
30.1
3.0
38

24.4	24.6	25.2	25.4	24.8	24.9	24.8	25.7	25.6	24.8
8.7	8.5	7.9	7.7	8.3	8.2	8.3	7.4	7.5	1.3
21	17	14	10	8	10	21	22	27	38

22.3
10.8
3.5
21.1
12.0
5.5
20.4
12.7
7.0
Not in PP

✓

32.9
0.2
61
31.7
1.4
45

24.8	26.0	25.6	26.1	25.4	25.5	25.6	25.4	26.1	27.1	32.2
8.2	7.0	7.4	6.9	7.6	7.5	7.4	7.6	6.9	5.9	0.8
41	30	17	10	7	9	20	21	28	36	

22.9
10.1
5.6

✓

33.0
0.0
66
32.4
0.6
53

Sta	+	$\bar{A}$	-	Elev
-----	---	-----------	---	------

		932.97		
--	--	--------	--	--

6+50				
------	--	--	--	--

✓				
---	--	--	--	--

7				
---	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

T.P.				
------	--	--	--	--

11.65				
-------	--	--	--	--

933.79				
--------	--	--	--	--

10.83				
-------	--	--	--	--

922.14				
--------	--	--	--	--

April 16, 1957

LT.	R	RT	30
27.6 54 26	26.5 65 21	26.8 62 10	26.1 69 7
27.6 54 34	25.9 71 45	23.3 9.7 59	26.2 6.8 9
24.6 8.4 29	26.2 6.8 25	24.4 6.6 14	26.1 6.8 11
22.2 10.8 42	25.3 7.7 9	25.8 7.2 11	25.7 7.3 11
24.6 10.6 25	24.5 8.5 11	24.5 8.5 11	24.2 8.8 19
25.2 7.8 18	24.9 8.1 10	24.5 8.5 11	25.5 7.5 20
21.0 12.0 32	18.0 15.0 37	15.1 12.9 50	33.0 0.0 56
24.5 65 21	26.8 62 10	26.1 69 7	26.2 6.8 9
27.6 54 34	25.9 71 45	23.3 9.7 59	26.1 6.8 9
24.6 8.4 29	26.2 6.8 25	24.4 6.6 14	26.1 6.8 11
22.2 10.8 42	25.3 7.7 9	25.8 7.2 11	25.7 7.3 11
24.6 10.6 25	24.5 8.5 11	24.5 8.5 11	24.2 8.8 19
25.2 7.8 18	24.9 8.1 10	24.5 8.5 11	25.5 7.5 20
21.0 12.0 32	18.0 15.0 37	15.1 12.9 50	33.0 0.0 56

Sta	+	π	-	Elev
-----	---	-------	---	------

		933.79		
--	--	--------	--	--

8700				
------	--	--	--	--

✓				
---	--	--	--	--

+40				
-----	--	--	--	--

✓				
---	--	--	--	--

+70				
-----	--	--	--	--

April 16, 1957

LT.

E

Rt.

31

10.7	10.4	10.9	10.6	10.6	10.8	9.7	9.2
14	9	7	.	9	17	19	25

12.2
1.5
18

30.6
3.2
63

29.9
3.9
48

29.5
4.3
33

12.4	12.1	11.5	11.5	11.7	11.3	11.5	11.6	12.2	12.2
14	11	10	8	7		11	21	23	25

26.5
7.3
53

25.8
8.0
34

25.1
8.7
30

14.0	13.0	12.0	11.8	12.1	11.8	12.0	12.2	12.9	12.9
14	11	9	8	7		14	20	24	26

23.8
10.0
59

22.9
10.9
47

22.4
11.4
34

Sta + π - Elev

933.79

9400

✓

+40

✓

+68

April 16, 1959

Lt.

F

Rt.

32

21.2

21.5

21.3

21.6

21.6

21.1

20.2

12.6

12.3

12.5

12.2

12.2

12.7

13.6

10

9

7

10

19

22

19.8

14.0

14

21.8

12.0

66

21.0

12.8

47

20.8

13.0

35

20.3

13.5

31

18.6

15.2

16

21.6

12.2

13

21.6

12.2

10

21.5

12.3

9

22.0

11.8

9

22.0

11.8

9

21.3

12.5

19

20.8

13.0

21

W.S

20.1

13.7

25

19.8

14.0

50

20.1

13.7

32

21.3

12.5

19

22.5

11.3

14

22.6

11.2

10

22.4

11.4

9

22.8

11.0

9

22.7

11.1

9

22.7

11.1

14

23.0

10.8

15

22.8

11.0

21

20.7

13.1

24

19.8

14.0

29

18.7

15.1

36

17.8

16.0

53

20.4

13.4

50

20.8

13.0

32

22.1

11.7

22

Sta + Δ - Elev

933.79

10+00

✓

+ 40

✓

TP 5.67 937.17 2.29 931.50

+ 85

April 16, 1957

11.

RT 33

10.3	9.6	9.8	10.1	9.7	10.1	9.6	9.4	10.5
24	16	10	9	24.1	14	15	20	24

10.6	9.5	10.0	10.2	12.0	12.0	11.8	11.2
29	33	38	54	60	50	40	30

6.2	5.8	7.6	8.2	4.9	8.3	7.3	6.0	6.0	4.7
29	17	14	12	7.9	14	17	22	25	27

4.3	4.6
35	52

Iron RT

8.0	7.1	6.2	4.9
55	45	32	30

6.2	8.2	8.8	9.4	9.9	9.3	9.9	5.4	5.2	9.5	9.5
23	19	15	14	11		14	21	24	27	32

7.2	7.2	2.6	2.6	2.8	3.1
25	28	33	36	49	56

6.7	6.3
60	18

Sta + π - Elev

937.17

11

✓

+27

✓

+54

✓

April 16, 1937

L1

R1

34

61	7.5	8.0	8.6	9.1	8.6	9.2	7.9	4.9	3.7	4.4
22	20	16	12	11		13	18	22	27	40

6.7	6.7	1.6	2.2	3.0			4.7	4.6		
25	27	34	48	60			54	45		

6.5	5.9	6.9	7.1	7.8	7.5	8.0	6.9	4.9	4.2	4.5
23	20	17	12	11		13	14	21	29	39

6.7	4.3	4.7	5.6							
28	31	34	58							

6.4	6.4	5.0	4.7	6.8	6.5	7.0	6.0	5.1	6.0	5.9
39	27	19	15	11		12	14	18	29	40

56 30.8

55 31.1

Sta + X - Elev

937.17

11 782

✓

12

✓

TP 9.62 945.75 1.04 936.13

12.50 933.25 (933.26)

+ 32

65

April 16, 1957

14

14

35

55	46	43	51	58	54	58	52	57	60	66
32	25	14	12	11	12	20	34	45	56	
31.7	32.6	32.9	32.1	31.4	31.8	31.4	32.0	31.5	31.2	30.6

5.5
43
31.7

5.0
55
32.2



341	340	342	327	321	325	321	336	317	305	301
37	27	16	12	11	14	19	32	42	55	
3.1	3.2	3.0	4.5	5.1	4.7	5.1	3.6	5.5	6.7	7.1

2.3
56
349



75	98	104	126	121	125	114	107	107	124
29	25	18	12		14	15	17	26	33
38.3	36.0	35.4	33.2	33.7	33.3	34.4	35.1	35.1	33.4

6.2
43
39.6

5.6
57
40.2



14.6
53
31.2

12.0
38
32.8

Sta + π - Elev

945.75

12 + 6.5

✓

13

✓

+35

✓

April 16, 1957

14

51

37

9.2	10.5	11.4	10.9	10.8	11.2	10.5	11.1	11.5
19	15	13	7		14	17	32	41

8.6	6.0	4.2	2.8	2.6	2.5			
25	28	40	54	65	78			52

4.8	6.9	7.5	9.3	10.1	9.5	10.1	9.9	10.7	11.6	12.6
29	24	19	14	13		13	21	29	33	44

2.7	1.9	2.3								
48	61	79								54

2.5	3.8	6.8	8.2	9.0	8.6	9.1	8.6	9.2	9.7	12.9
44	30	24	16	14		11	20	32	42	50

2.6	3.4
58	72

Sta + X. - Elev

945.75

13+60

✓

14

✓

+50

15

TP

11.78 92397

April 16, 1957

14

Rt 38

30 2.5 42.3

23 7.1 38.7

16 8.0 37.8

14 8.5 37.3

8.2 37.6

12 8.5 37.3

27 7.6 38.2

38 7.1 38.7

51 7.5 38.3

47 2.7 43.1

62 3.8 42.0

77 5.2 40.6

✓

45 4.7 41.1

30 4.3 41.5

23 7.4 38.4

18 7.7 38.1

13 8.5 37.3

8.1 37.7

11 8.4 37.4

31 8.0 37.8

47 7.6 38.2

60 7.1 38.7

59 5.8 40.0

77 7.8 38.0

✓

56 6.3 39.5

42 5.5 40.3

30 5.1 40.7

23 8.1 37.7

16 8.9 36.9

15 9.5 36.3

9.1 36.7

11 9.8 36.0

12 9.1 36.7

24 7.9 37.9

40 7.6 38.2

58 6.8 39.0

50 4.4 41.4

31 5.7 40.1

25 9.3 36.5

16 10.5 35.3

15 11.4 34.4

11.0 34.8

10 11.5 34.3

11 11.0 34.8

16 9.9 35.9

23 9.9 35.9

34 9.6 36.2

45 4.0 41.2

65 4.7 41.1

79 5.4 40.4

✓

58 9.0 45.8

55 2.5 43.3

Sta	+	π	-	Elev
TP	0.01	922.15		922.14

7+50

8

✓

+40

+70

✓

April 16, 1951

Lt

RT

39

T.P. Page 30

09.6	11.5	14.2
12.6	10.7	8.0
84	67	52

✓

07.2	08.8	10.9	13.2	16.0
15.0	13.4	11.3	9.0	6.2
63	49	38	33	27

✓

→ 06.4
15.8
73
W.S.

06.5	08.8	11.3	15.3
15.7	13.4	10.9	6.9
62	46	31	23

✓

09.4	11.4	13.1	18.1
12.8	10.8	9.1	4.1
51	40	28	19

✓

→ 07.0
15.2
67
W.S.

06.4
15.8
89
W.S.

✓

Sta + π - Elev

922.15

9+00

+40

32
90

TP 10.39 944.36 933.97

15+32

✓

+70
+70

TP 1.10 932.29 1322 931.14

April 16, 1957

40

Lt

Rt

08.5
13.7
72

12.2
10.0
51

13.4
8.8
39

14.7
7.5
26

✓

15.4
6.8
42

17.4
4.8
30

18.1
4.1
19

16.6
3.5
F.L. 12
18

✓

13.1
9.1
62

12.0
10.2
83

Rock Lt Sta 13+40 Page 38

37.6
6.8
31

33.7
10.2
25

33.7
10.7
15

33.0
11.4
14

33.4
11.0
10

32.9
11.5
10

33.4
11.0
11

34.8
9.6
20

40.4
4.0
25

40.2
4.2
36

✓

38.3
6.1
46

39.0
5.4
63

✓

40.6
3.8
50

34.3
10.1
31

31.8
12.6
25

32.0
12.4
15

31.4
13.0
13

31.7
12.7
10

31.2
13.2
10

33.3
11.1
12

33.4
11.0
21

34.6
9.8
29

34.2
10.2
36

✓

34.2
10.2
41

35.2
9.2
59

✓

35.4
9.0
50

Sta + π - Elev

932.24

16 + 00

✓

+ 33

✓

+ 66

2 April 16, 1957

11

RT

41

1.9	1.7	1.7	2.3	2.0	2.6	1.8	2.2	3.1
28	24	50	14	10	12	17	21	
30.3	30.5	30.5	29.9	30.2	29.6	30.4	30.0	29.1

15

1.5	1.3	0.8				1.9	2.9	2.4
32	48	59				52	36	30
30.7	30.9	31.4				30.3	29.3	29.8

3.9	3.1	3.3	3.8	3.4	4.0	3.7	6.5	6.9
25	19	14	13		11	15	23	28
28.3	29.1	28.9	28.4	28.8	28.2	28.5	25.7	25.3

3.8	3.4	2.8					7.1	6.9
27	46	62					50	32
28.4	28.8	29.4					25.1	25.3

4.9	5.8	4.6	4.7	5.3	4.8	5.5	5.2	8.4	9.7
30	26	19	14	13		10	16	24	36
27.3	26.4	27.6	27.5	26.9	27.4	26.7	27.0	23.8	22.5

4.3	4.1								
47	58								
27.9	28.1								21.5

54

Sta + π - E/ev.

932.24

17+00

✓

+50

✓

T.P. 1.44 923.29 10.39 921.85

18

✓

4 April 16, 1957

42

14

BT

71	61	60	68	63	71	67	71	80
22	18	14	13		13	15	18	20
25.1	26.1	26.2	25.4	25.9	25.1	25.5	25.1	24.2

71	63	54	53		12.2	10.8	9.6
25	29	47	58		57	38	27
25.1	25.9	26.8	26.9		20.0	21.4	22.6

9.4	8.3	8.2	9.1	8.8	8.2	8.8	10.9	11.9	12.6	13.6
26	18	15	13	9		17	23	33	48	58
22.8	23.9	24.0	23.1	23.4	24.0	23.4	21.3	20.3	19.6	18.6

8.9	8.9	8.1	
28	40	56	
23.3	23.3	24.1	

20	13	15	23	15	21	18	18	38
21	17	13	12		15	16	18	28
21.3	22.0	21.8	21.0	21.8	21.2	21.5	21.5	19.5

1.7	2.4	2.8	2.5		9.8	7.6	6.5	5.5
25	30	41	57		55	41	38	33
21.6	20.9	20.5	20.8		13.5	15.7	16.8	17.8

Sta + π - Elev

923.29

18+22

✓

+70

✓

19+00

✓

April 16, 1957

43

Lt

Bt

20.0	20.9	20.7	20.1	20.8	20.1	20.4	18.5	17.6
3.3	2.4	2.6	3.2	2.5	3.2	2.9	4.8	5.7
24	16	13	12		15	17	27	31

18.8	18.3	18.8				11.4	13.1	
4.5	5.0	4.5				11.9	10.2	
28	37	57				58	47	

✓

16.0	18.3	18.3	17.8	18.4	18.5	17.6	17.9	17.5
7.3	5.0	5.0	5.5	4.9	4.8	5.7	5.4	5.8
23	15	12	11		6	15	16	19

✓

14.4	13.7	12.9	12.5		09.5	10.6	11.8	13.2
8.9	9.6	10.4	10.8		13.8	12.7	11.5	10.1
27	35	46	57		55	46	35	27

✓

12.9	16.8	16.9	16.6	17.1	16.6	16.9	16.5	13.1
10.4	6.5	6.4	6.7	6.2	6.7	6.4	6.8	10.2
25	14	11	10		11	15	18	26

✓

11.3	10.4				09.6	09.8	11.1	
12.0	12.9				13.7	13.5	12.2	
39	56				59	46	34	

✓

Sta + π - Elev

923.29

T.P. 3.04 917.46 8.87 914.42

19+50

✓

20+00

✓

+25

✓

April 16, 1957

LT

4

Rt

44

11.4	14.6	14.9	14.6	15.0	14.6	14.9	14.4	11.4
6.1	2.9	2.6	2.9	2.5	2.9	2.6	3.1	6.1
25	12	11	9		13	14	17	25
10.1	08.6	07.7			09.4	09.0	10.0	
7.4	8.9	9.8			8.1	8.5	7.5	
33	44	56			58	38	32	

10.3	12.9	13.1	12.7	13.2	12.9	13.3	12.5	08.8
7.2	4.6	4.4	4.8	4.3	4.6	4.2	5.0	8.7
17	12	10	9		15	16	19	33
08.6	08.0	07.6	07.0			10.5	09.7	
8.9	9.5	9.9	10.5			7.0	7.8	
23	32	45	57			57	44	

10.3	11.9	12.5	12.0	12.4	12.2	12.7	10.2	09.3
7.2	5.6	5.0	5.5	5.1	5.3	4.8	7.3	8.2
15	12	10	9		14	15	26	32
08.7	08.1	08.1	07.6			11.3	10.0	
8.8	9.4	9.4	9.9			6.2	7.5	
20	29	42	57			53	39	

Sta + π - Elev

917.46

20+55

✓

21+00

T.P. 3.24 913.93 6.77 910.69

+38

✓

April 16, 1957

Lt.

#

Rt

45

08.7	10.8	11.4	11.2	11.7	11.4	11.7	11.2	10.0
8.8	6.7	6.1	6.3	5.8	6.1	5.8	6.3	7.5
16	12	10	9		14	15	17	32

07.2	06.4	06.0	05.8		12.4	11.7	11.0
10.3	11.1	11.5	11.7	✓	5.1	5.8	6.5
22	32	42	56		58	45	40

05.7	09.3	10.4	10.1	10.7	10.3	10.5	11.2	11.3	11.2
11.8	8.2	7.1	7.4	6.8	7.2	7.0	6.3	6.2	6.3
20	13	10	9		15	22	33	44	59

04.2	03.1	02.1
13.3	14.4	15.4
30	42	56

07.2	09.3	09.7	09.3	09.9	09.7	09.6	09.9	09.8
6.7	4.6	4.2	4.6	4.0	4.2	4.3	4.0	4.1
19	13	10	9		9	15	17	18

05.2	03.7	02.3	01.4		08.3	08.5	08.7
8.7	10.2	11.6	12.5	✓	5.6	5.4	5.2
23	34	44	57		60	45	36

Sta	+	π	-	Elev
-----	---	-------	---	------

		913.93		
--	--	--------	--	--

21+73				
-------	--	--	--	--

✓				
---	--	--	--	--

22+00				
-------	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

+41				
-----	--	--	--	--

✓				
---	--	--	--	--

April 16, 1957

Lt

E

Rt

46

06.7
7.2
20

08.7
5.2
14

09.3
4.6
11

09.0
4.9
10

09.5
4.4
14

08.9
5.0
14

09.1
4.8
16

05.7
8.2
32

05.1
8.8
35

05.5
8.4
28

04.2
9.7
39

02.1
11.8
56

✓

03.4
10.5
56

03.4
10.5
46

07.9
6.0
18

08.9
5.0
14

09.2
4.7
12

09.0
4.9
11

09.3
4.6
15

08.7
5.2
15

05.2
8.7
33

04.9
9.0
39

05.9
8.0
46

07.0
6.9
20

06.2
7.7
24

04.8
9.1
32

03.2
10.7
43

✓

08.5
5.4
53

13.2
54

✓

04.3
9.6
36

06.6
7.3
22

09.3
4.6
16

09.5
4.4
13

09.2
4.7
12

09.7
4.2
13

09.0
4.9
13

09.6
4.3
16

09.4
4.5
19

08.7
5.2
24

06.1
7.8
31

02.0
11.9
46

09.3
14.6
55

✓

09.9
4.0
50

09.0
4.9
39

06.2
7.7
33

Sta + π - Elev

913.93

22+60

✓

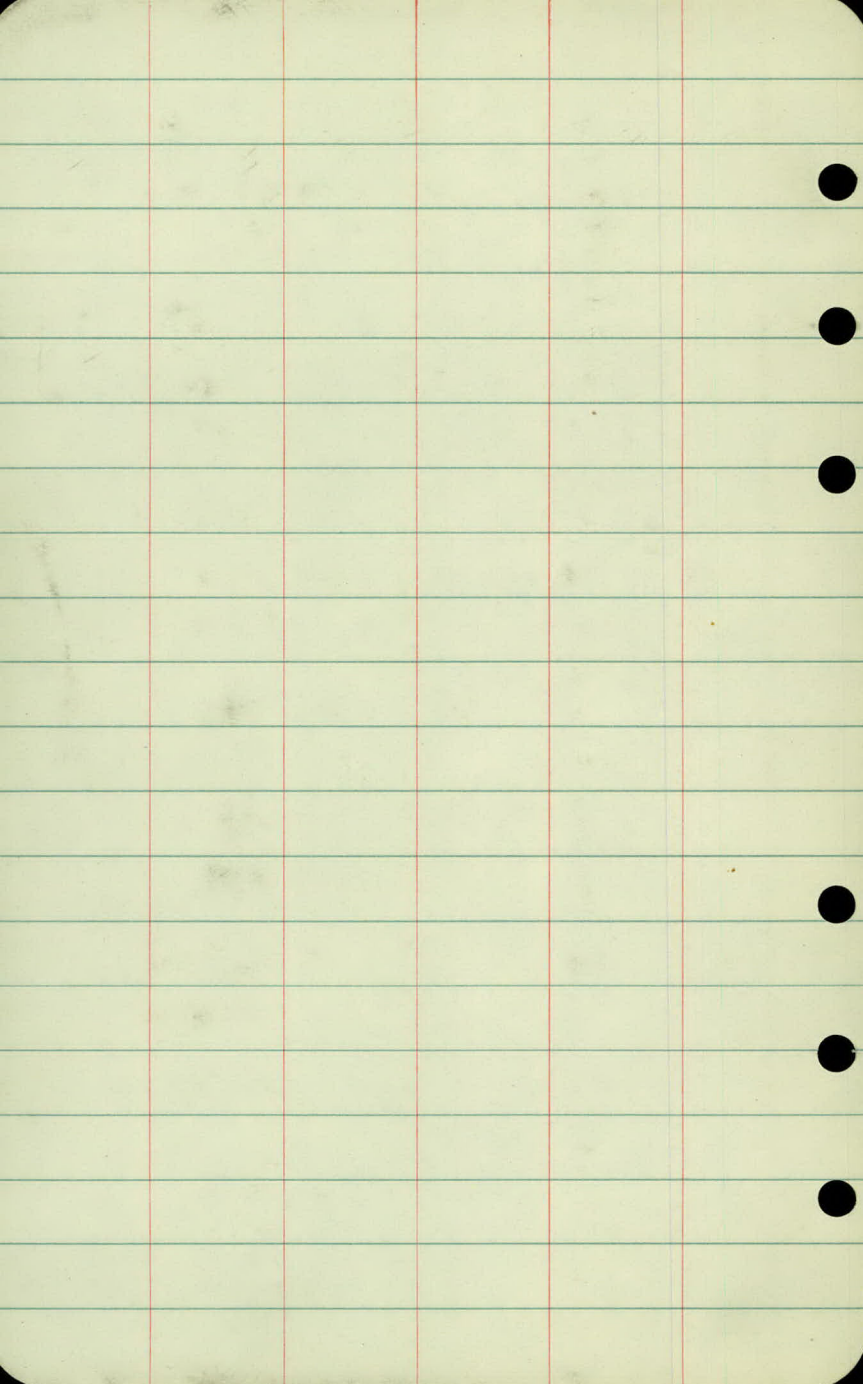
B.M.

3.95 909.98 (909.98)

April 16, 1957

Lt.					Rt.				
07.1	09.8	09.9	09.4	09.9	09.3	10.1	10.5	10.1	47
6.8	4.1	4.0	4.5	4.0	4.6	3.8	3.4	3.8	
24	16	13	11	12	16	21	34		
05.2	02.9	00.8				10.7	10.6		
8.7	11.0	13.1				3.2	3.3		
33	42	50				53	43		

Spike in T.P. SW Cor. Sooline Tracks ¹/₂ McMenomy



24+67.63 = $\pm$ Tracks

Sta + π - Elev

BM 3.96 913.94 (909.98)

23+00

✓

+30

✓

✓

+68

FX
KP
JT

April 30, 1957

LT

RT 49

Spike in T.P. SW. Cor McMenemy & So. RR

09.4	11.0	10.4	09.5	09.9	9.7	10.8	10.1	10.1
4.5	2.9	3.5	4.4	4.0	4.2	3.1	3.8	3.8
24	17	14	11		12	14	26	38

07.2 13.9
→ 6.7 10.0
36 50

P. 09.9 09.5
4.0 4.4
50 45

11.3	10.1	09.7	09.0	09.6	09.3	09.6	09.7	10.2
2.6	3.8	4.2	4.9	4.3	4.6	4.3	4.2	3.7
36	29	18	12		11	13	18	23

09.6 08.2
→ 4.3 5.7
44 50

P. 09.5 11.5 10.1 09.9
4.4 2.4 3.8 4.0
50 45 40 30

09.9	09.1	08.9	08.2	08.8	08.5	08.8	08.9	09.1
4.0	4.8	5.0	5.7	5.1	5.4	5.1	5.0	4.8
37	27	17	13		11	24	40	43

09.9
→ 4.0
50

P. 06.9
7.0
50

Sta + π - Elev

913.94

24

✓

+42

✓

+64.5

+70.7

BM

3.96 909.98

April 30, 1957

RT 50

14

08.3	08.0	08.2	08.4	08.4	08.6	07.7
5.6	5.9	5.7	5.5	5.5	5.3	6.2
24	14	10		9	28	38

08.4	08.6	08.3		06.3	07.9	07.8
5.5	5.3	5.6		7.6	6.0	6.1
35	47	50		50	42	40

08.0	08.4	08.5	08.2	08.4	08.3	08.2	08.7	09.2
5.9	5.5	5.4	5.7	5.5	5.6	5.7	5.2	4.7
23	22	15	12	P	7	24	42	50

07.8	08.0	08.56	08.48
6.1	5.9	5.38	5.46
26	30	36	48
		S. Rail	N. Rail

08.89
5.05
S Rail

08.92
5.02
N Rail

Spike in T.P. S.W. Cor. McMonery & Sae R.R.

Sta + π - E/ey

BM 3.40 913.38

909.98

+75

✓

25+00

✓

+27

Lt

E

May 16, 1957

Rt

51

Spike in T.P. S.W. Cor. McMenamy + Soo RR

08.8	08.5	08.6	08.5	08.97 NTR
4.6	4.9	4.8	4.9	4.41
27	12		4	5.3

07.9	08.3	10.0	13.4
5.5	5.1	3.4	0.0
34	39	45	50

P.

09.3	08.6	08.1	08.2	07.9	07.5	07.4	08.1
4.1	4.8	5.3	5.2	5.5	5.9	6.0	5.3
24	13	11		7	15	21	24

10.0	12.2	13.4
3.4	1.2	0.0
36	42	50

P.

09.23 NTR	08.5
4.15	4.9
36.2	33

11.7	08.3	08.1	07.8	08.0	07.7	08.1	07.4	06.9
1.7	5.1	5.3	5.6	5.4	5.7	5.3	6.0	6.5
27	19	13	11		9	22	27	37

12.0	12.1
1.4	0.7
32	50

P.

08.5	08.4
4.9	5.0
50	47

Stg

+

π

-

E/ev

913.38

+60

✓

+77

✓

26+00

Lt.

May 16, 1957

Rt.

52

09.1	09.2	08.5	07.6	07.9	07.7	07.5	07.4	07.5	07.4
4.3	4.2	4.9	5.8	5.5	5.7	5.9	6.0	5.9	6.0
34	25	14	11		10	19	32	42	50

10.5

2.9
50

P.

08.4	08.8	08.7	07.6	08.1	07.7	06.9	06.7	07.1	07.0
5.0	4.6	4.7	5.8	5.3	5.7	6.5	6.7	6.3	6.4
26	19	14	10		11	22	31	43	50

09.3

10.4

4.1
393.0
50

P.

07.7	06.7	07.5	07.9	08.3	07.7	07.1	06.3	06.1	06.7
5.7	6.7	5.9	5.5	5.1	5.7	6.3	7.1	7.3	6.7
136	26	20	10		13	18	24	33	50

09.0

4.4
50

P.

Sta + π - Elev.

913.38

+26

✓

+70

✓

27+00

✓

Lt

May 16, 1951

Rt

53

06.0	05.4	08.4	08.5	08.7	07.9	06.7	06.1	05.9	06.3
7.4	8.0	5.0	4.9	4.7	5.5	6.7	7.3	7.5	7.1
35	26	16	10		14	20	27	34	50

7.9
0
5.5
50

P.

06.5	04.9	05.4	09.4	09.9	09.5	09.2	07.9	07.1
6.9	8.5	8.0	4.0	3.5	3.9	4.2	5.5	6.3
38	23	19	12		11	19	21	26

08.3
5.1
50

07.4
6.0
50

07.0
6.4
35

07.3	08.3	10.1	10.7	11.0	10.8	10.3	09.3	08.7
6.1	5.1	2.7	2.7	2.4	2.6	3.1	4.1	4.7
24	16	12	8		10	18	21	29

07.0
6.4
28

07.3
6.1
35

09.4
4.0
50

P.

08.8
4.6
50

08.8
4.6
35

Stg + T - E/ev

913.38

+29

✓

TP 13.69 926.53 0.54 912.84

+64

✓

Lt

MAY 16, 1951

Rt

54

09.5	09.9	12.0	11.9	12.3	11.9	11.7	10.4	10.6
3.9	3.5	1.4	1.5	1.1	1.5	1.7	3.0	2.8
21	17	13	8		11	18	26	33

09.9	10.4	13.0
3.5	3.0	0.4
27	36	50

10.7	10.5
2.7	2.9
50	44

15.6	14.6	14.1	13.6	13.9	13.5	14.3	13.5
10.9	11.9	12.4	12.9	12.6	13.0	12.2	13.0
27	21	10	8		13	15	22

16.9	19.2
9.6	7.3
37	50

14.1	13.5	13.3
12.4	13.0	13.2
50	40	32

Sta + T - Elev

926.53

28+00

✓

* + 25

✓

* + 50

✓

Lt

E

May 16, 1957

Rt

55

17.8	16.8	16.5	15.6	15.8	15.5	17.2	18.0	18.9
8.7	9.7	10.0	10.9	10.7	11.0	9.3	8.5	7.6
20	16	10	8		13	15	23	27

21.1	23.0	24.5	26.3	P.	20.3	20.1	19.2
5.4	3.5	2.0	0.2		6.2	6.4	7.3
26	29	36	50		50	44	33

21.5	19.0	17.8	17.0	17.1	18.8	19.2	20.1	22.5	23.5
5.0	7.5	8.7	9.5	9.4	9.7	7.3	6.4	4.0	3.0
22	18	10	8		12	16	22	27	33

25.3	P.	25.4	25.3	24.3
1.2		1.1	1.2	2.2
27		63	50	39

24.0	20.1	19.1	18.1	18.3	18.0	20.5	21.8	23.3
2.5	6.4	7.4	8.4	8.2	8.5	6.0	4.7	3.2
23	15	10	8		12	14	19	25

26.3	P.	26.5	25.5	24.2
0.2		0.0	1.0	2.3
26		50	40	33

Sta

+

↑

-

Elev

926.53

* +75

✓

*
29+00

✓

* +27

Lt

E

Rt

56

MAY 16, 1957

23.3	19.5	19.5	18.9	19.1	18.9	20.8	23.0	25.1
3.2	7.0	7.0	7.6	7.4	7.6	5.7	3.5	1.4
21	13	10	8		13	15	23	30

25.6
0.9
26

P.

25.5
1.0
36

20.4	19.6	19.5	19.1	19.4	19.5	20.5	21.7	24.1	25.7
6.1	6.9	7.0	7.4	7.1	7.0	6.0	4.8	2.4	0.8
19	16	10	9		13	14	20	27	32

23.4 23.7 23.7
3.1 2.8 2.8
24 28 38

P.

26.3
0.2
36

17.0	19.5	18.9	19.3	18.9	19.2	19.2	20.3	21.5	23.3	24.6
9.5	7.0	7.6	7.2	7.6	7.3	7.3	6.2	5.0	3.2	1.9
27	17	13	10	9		13	15	19	23	29

17.0 18.2
8.7 8.3
34 50

P.

26.1
0.4
33

Stg + π - E/er.

926.53

* +60

✓

* +80

✓

30 + 00

Lt

E

May 16, 1957

Rt

57

19.3	17.7	18.4	18.5	17.8	18.3	18.0	20.2	21.1	23.4
7.2	8.8	8.1	8.0	8.7	8.2	8.5	6.3	5.4	3.1
18	13	11	9	8		12	14	19	25

18.8	17.5	16.9	15.2						24.5
7.7	9.0	9.6	11.3						2.0
23	30	35	50						33

16.9	17.9	17.2	17.9	17.9	16.9	17.5	17.0	18.8	19.9	19.9	20.8
9.6	8.6	9.3	8.6	8.6	9.6	9.0	9.5	7.7	6.6	6.6	5.7
28	21	16	13	11	9		13	15	17	20	22

15.8	14.3										
10.7	12.2										
37	50										

14.8	15.5	16.3	16.7	15.9	16.5	16.4	16.0	17.2	17.6
11.7	11.0	10.2	9.8	10.6	10.0	10.1	10.5	9.3	8.9
27	21	17	10	8		7	13	15	19

14.3	13.5	12.7							
12.2	13.0	13.8							
30	41	50							

Stg + π - Elev

926.53

TP1 10.00 916.53

TP2 6.24 931.28 1.49 925.04

28+00

+25

+50

+75

✓

FK
KP
JT

Lt

May 16, 1957
May 21, 1957
Rt

58

Station 30+00

nail in fence post rt. sta 28+55

²⁸
3.1
65

P.

²²
2.1
59

³
8.0
70

30.7	29.7	29.1	27.0	26.0	26.2
0.6	1.4	2.2	4.3	5.3	5.1
71	58	46	30	67	81

30.8	30.6	30.4	30.8	28.3	26.8	28.1	29.6
0.5	0.7	0.9	1.5	3.0	4.5	3.2	1.7
73	64	53	37	30	53	67	81

27.1	26.5	28.7	29.0	27.8	25.9	26.6	28.4	29.9	30.0
4.2	4.8	2.6	2.3	3.5	5.4	4.7	2.9	1.4	1.3
76	65	47	35	30	39	44	55	67	80

P.

28.9
2.4
93

Sta + π - Elev

931.28

29

✓

+27

+60

+80

T.P. 1.61 920.62 12.27 919.01

T.P. 1

4.09 916.53 (916.53)

30+28

T.P. 2.79 916.46 29.5 912.67

2 May 26, 1951 59

Lt

Rt

22.0	22.3	25.7	26.0	26.5	27.7	29.1	29.9
9.3	9.0	7.6	7.3	4.8	3.6	2.2	1.4
70	53	49	45	38	50	62	73

P.

27.4	28.7
3.9	2.6
100	86

P.

27.1	28.6	30.0	29.0	27.1
4.2	2.7	1.3	2.3	4.2
38	52	67	82	93

P.

25.1	26.9	28.2	27.4	25.3
6.2	4.4	3.1	3.9	6.0
38	51	62	75	90

P.

25.6	26.0	26.2	24.9
5.7	5.3	5.1	6.4
46	60	66	81

10.8	11.4	12.1	14.3	14.9	14.8	14.7	14.0	14.9
9.8	9.2	8.5	6.3	5.7	5.8	5.9	6.6	5.7
28	20	15	11		10	16	20	32

10.4	09.9	09.1
10.2	10.7	11.5
31	45	56

P.

18.4	15.9
2.2	4.7
62	44

Sta + π - Elev 908.78

916.46

30+50

✓

+75

✓

31

BM 4.62 913.40 7.68 908.78 (908.78)

2 May 21/1957

60

Lt

At

07.5	08.1	09.0	13.2	13.8	13.9	13.6	12.4	12.3
90	84	75	3.3	2.7	2.6	2.9	4.1	4.2
27	24	17	9		6	16	21	31

P.

07.6	07.3	07.1				13.4	12.7
8.9	92	94				3.1	3.8
32	40	50				50	43

05.6	06.7	07.8	12.0	12.5	12.6	12.3	11.5	10.9
10.9	9.8	8.7	4.5	4.0	3.9	4.2	5.0	5.6
27	18	16	10		6	15	19	26

P.

05.0	05.1	05.3		12.2	11.8	11.0	10.9
11.5	11.4	11.2		4.3	4.7	5.5	5.6
31	45	50		50	43	33	31

03.8	04.6	05.7	10.9	11.3	11.3	10.9	10.1	09.8
12.7	12.0	10.8	5.6	5.2	5.2	5.6	6.4	6.7
36	27	18	10		7	15	18	22

P.

03.8				11.3	10.3	10.0
12.7				5.2	6.2	6.5
50				50	38	31

slope in 30" out 120' Lt sta 30+80

Sta + π - Elev

913.40

31+37

✓

+ 72

✓

32

14

May 23, 1951
Clear Cool 45°

RT

61

09.0	09.6	09.2	09.6	09.4	09.9	09.4	08.8
44	38	42	38	40	35	40	46
13	11	10		13	14	17	19

P.

07.0	05.8	04.7	04.0
64	81	87	94
17	29	33	50

10.9	09.7	09.0
2.7	3.7	4.4
50	40	30

07.0	07.4	08.4	07.8	07.8	07.3	08.4	08.9	09.3	10.1
64	60	50	56	56	61	50	45	41	33
28	23	12	10		12	14	30	35	50

P.

06.8	06.9
66	65
38	50

07.9	07.1	07.0	06.4	06.5	06.0	07.5	08.6	09.6	10.4
55	63	64	70	69	74	59	48	38	30
18	16	12	11		12	13	30	42	50

P.

08.0	08.2	09.3
54	52	41
28	37	50

Sta

+

π

-

Elev.

913.40

32+26

✓

+ 57

✓

33+00

✓

Lt

Z

NH₄ 23.1 15.1
Clear Cool 45° 62
Rt

07.9	06.4	06.2	05.2	05.2	04.9	06.8	08.0	08.6
5.5	7.0	7.2	8.2	8.2	8.5	6.6	5.4	4.8
18	16	13	11		11.5	12.5	24	34

P.

08.2	10.1			10.0
5.2	3.3			3.4
30	50			50

06.0	04.4	03.5	03.9	04.0	03.6	06.0	07.7	08.3	09.3
7.4	9.0	9.9	9.5	9.4	9.8	7.4	5.7	5.1	4.1
19	17	13	11		11	11.7	24	37	50

P.

06.9	09.6
6.5	3.8
31	50

04.9	02.7	02.7	02.0	02.2	01.7	04.7	06.5	07.3
8.5	10.7	10.7	11.4	11.2	11.7	8.7	6.9	6.1
26	20	14	13		11	12.7	27	37

P.

04.9	07.1
8.5	6.3
33	50

08.1
5.3
50

Sta	+	π	-	Elev
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		913.40		
--	--	--------	--	--

TP	6.71	907.30	12.81	900.59
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33+27

✓

+ 60

✓

34+00

✓

Lt

E

May 23, 1957
Clear Cool 45°
Rt

63

04.8	02.0	01.8	00.8	01.1	00.6	02.1	04.1	05.1
2.5	5.3	5.5	6.5	6.2	6.7	4.9	3.2	2.2
26	20	14	12		10.7	11.9	14.6	26

04.8	05.1	06.3
2.5	1.9	1.0
32	42	50

01.2	05.7
0.1	1.6
50	37

01.1	00.7	99.6	99.7	99.7	99.6	01.1	02.9	03.8
6.2	6.6	7.7	7.6	7.6	7.7	5.9	4.4	3.5
20	15	12	6		10.2	11.3	15	26

03.6	04.3	04.5	05.4	05.8
3.7	3.0	2.8	1.9	1.5
24	27	32	42	50

05.5	04.1
1.8	3.2
50	37

00.3	98.8	99.1	98.3	98.4	98.3	00.0	00.6	01.1
7.0	8.5	8.2	9.0	8.9	9.0	7.3	6.7	6.2
24	20	14	12		9.5	12.5	23	39

00.1	01.7
7.2	5.6
33	50

03.1	02.3
4.2	5.0
50	42

Sta

+

π

-

Elev

907.30

34+50

✓

TP

3.52

899.92

10.90

896.40

35+00

✓

+50

Lt.

 $\frac{1}{2}$ clear Cool 50°
Rt.

64

96.9	97.0	97.3	96.9	97.0	97.0	97.6	98.1	98.3
10.4	10.3	10.0	10.4	10.3	10.3	9.7	9.2	9.0
32	23	13	11		11	12	19	30

P.

96.9
→ 10.4
50

99.4 98.5
7.9 8.8
50 39

95.1	96.2	96.2	95.7	96.0	95.5	96.1	96.3	96.3
4.8	3.7	3.7	4.2	3.9	4.4	3.8	3.6	3.6
17	14	12	11		13	14	26	40

P.

94.5 93.6 93.3
→ 5.4 6.3 6.6
30 42 50

97.3
2.6
50

91.0	92.4	94.3	94.4	95.1	94.2	94.5	94.2	94.2
8.9	7.5	5.6	5.5	4.8	5.7	5.4	5.7	5.7
28	18	15	13		13	17	29	38

P.

90.9 90.4
→ 9.0 9.5
34 50

94.3
5.6
50

Sta

+

π

-

Elev

899.92

36+00

✓

+ 50

✓

37+00

✓

Lt

May 23, 1951
Clear Cool 60°

E

Rt

65

89.8	90.9	93.1	93.3	93.9	93.5	93.0	92.7	92.1
10.1	9.0	6.8	6.6	6.0	6.4	6.9	7.2	7.8
23	18	15	11		10	16	31	33

89.2 89.5
10.7 10.4
30 50

P.

92.1
7.8
50

89.0	89.6	91.8	92.4	92.8	92.5	91.5	90.4	89.8	89.4
10.9	10.3	8.1	7.5	7.1	7.4	8.4	9.5	10.1	10.5
27	18	16	10		10	19	29	33	50

P.

88.9
11.0
50

88.5	89.0	91.2	91.4	91.9	91.3	90.6	89.1	88.7
11.4	10.9	8.7	8.5	8.0	8.6	9.3	10.8	11.2
30	19	16	11		12	20	25	33

P.

88.5
11.4
50

88.9
11.0
50

Sta

+

π

-

Elev

899.92

37+50

✓

TP 7.39 898.58 8.73 891.19

+97

ditch line

38+00

+50

✓

Lt

May 23 1957
Cool, Cloudy 55°
Rt

66

88.1	88.2	90.2	90.7	91.1	90.9	90.6	88.5	88.6
11.8	11.7	9.7	9.2	8.8	9.0	9.3	11.4	11.3
28	19	16	11		9	14	18	22

88.4

 11.5
50

88.6

88.4

 11.3 11.5
50 33

87.7	88.0 ditch elev
10.9	10.6
30	22

87.8	ditch elev
10.8	
18	

88.1	88.1	88.7	89.0	90.5	90.9	91.2	90.8	90.4	88.5	88.5	87.9
10.5	10.5	9.9	9.6	8.1	7.7	7.4	7.8	8.2	10.1	10.1	10.7
50	30	27	17	15	11	9	9	13	16	30	33

88.7	89.1	90.8	91.4	91.8	91.5	91.1	88.8	88.6
9.9	9.5	7.8	7.2	6.8	7.1	7.5	9.8	10.0
30	20	18	12		10	15	18	26

 88.6
10.0
50

 88.4 88.2
10.2 10.4
50 32

Sta

+

π

-

Elev

898.58

39+00

✓

+50

✓

40+00

✓

Lt

11/49 23, 1751
Cool to cloudy 600
Rt

67

89.7	90.9	92.1	92.3	92.9	92.4	92.1	89.6	89.6
8.9	7.7	6.5	6.3	5.7	6.2	6.5	9.0	9.0
30	21	18	12		10	17	21	31

P.

88.9 88.9
→ 9.7 9.7
35 50

88.9
9.7 ←
50

90.4	92.0	92.8	93.4	93.9	93.5	92.9	92.8	93.8
8.2	6.6	5.8	5.2	4.7	5.1	5.7	5.8	4.8
30	26	20	13		10	12	19	22

P.

90.5 90.0
→ 8.1 8.6
38 50

90.1 90.5 91.3
8.5 8.1 7.3 ←
50 33 28

95.0	94.8	94.3	94.7	95.1	94.8	94.5	94.5	95.3
3.6	3.8	4.3	3.9	3.5	3.8	4.1	4.1	3.3
26	19	17	13		8	10.5	13	22

95.7 93.4 92.5 93.0
→ 2.9 5.2 6.1 5.6
29 32 36 44

P.

93.8 94.0 96.2
4.8 4.6 2.4 ←
50 34 27

92.9
5.7
50 ←

Sta	+	Δ	-	Elev
-----	---	----------	---	------

		898.58		
--	--	--------	--	--

40+50				
-------	--	--	--	--

✓				
---	--	--	--	--

TP	13.38	910.66	1.30	897.28
----	-------	--------	------	--------

41+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+34				
-----	--	--	--	--

✓				
---	--	--	--	--

BM				
----	--	--	--	--

	5.92	904.74	(904.74)	
--	------	--------	----------	--

Lt

E

May 23, 1958
cool cloudy 60°

68

Rt

96.5	96.0	96.1	96.4	96.4	96.1	96.1	97.1	96.8
2.1	2.6	2.5	2.2	2.2	2.5	2.5	1.5	1.8
29	26	15	8		6	14	24	25

93.7	93.5	93.4
4.9	5.1	5.2
33	41	50

96.3	95.9
2.3	2.7
50	33

98.6	98.0	97.8	98.0	98.2	98.0	98.7	98.9	99.9
12.1	12.7	12.9	12.7	12.5	12.7	12.0	11.8	10.8
24	22	14	10		9	12	21	29

98.6	96.2	94.1
12.1	14.5	16.6
26	32	50

91.2	90.1	99.1
9.5	10.6	11.6
50	38	32

99.1	99.9	99.1	99.1	99.3	99.3	90.9	92.6	94.2
11.0	10.8	11.6	11.6	11.4	11.4	9.8	8.1	6.5
26	20	17	13		9.5	10.5	20	31

98.7	98.4	97.8
12.0	12.3	12.9
34	40	50

91.9	96.4	95.3
2.8	4.3	5.4
62	50	41

Spike in pp right sta 41+25

Sta + π - Elev

910.66

41+50

✓

* +75

✓

BM 10.38 915.12 5.92 904.74 904.74

+75

42+00

Lt

May 23, 1957
Cool, partly cloudy 60° 69
Rt

01.7	00.6	00.2	99.7	00.0	00.0	01.4	03.1	06.0
9.0	10.1	10.5	11.0	10.7	10.7	9.3	7.6	4.7
27	23	19	14		9	10	19	30

00.7	00.2	99.8
10.0	10.5	10.9
34	42	50

10.7	10.1	09.0	07.5
0.0	0.6	1.7	3.2
61	57	50	40

02.0	01.0	00.7	01.0	01.0	01.1	02.9	05.3	08.5	09.7
8.7	9.7	10.0	9.7	9.7	9.6	7.8	5.4	2.2	1.0
23	18	14	8		9	10.5	20	31	35

03.9	03.6	02.9	01.8
6.8	7.1	7.8	8.9
28	33	41	50

Spike in P.P. right sta 41+25

12.1	13.7	14.6
3.0	1.4	0.5
47	55	58

02.9	02.6	01.8	02.1	02.1	02.2	04.4	07.9	10.6
12.2	12.5	13.3	13.0	13.0	12.9	10.7	7.2	4.5
23	20	15	8		9	12	23	32

05.1	04.3	02.6
10.0	10.8	12.5
27	36	50

14.7
0.4
48

Sta

+

Δ

-

Elev

915.12

*
42+28

✓

*
+65

✓

*
43+00

✓

Lt

f

Midy 25, 1957
Cool, Partly Cloudy 60° 70°
Rt

04.4	04.5	03.1	03.7	03.5	03.3	06.3	08.7	12.2	13.2
10.7	10.6	12.0	11.4	11.6	11.8	8.8	6.4	2.9	1.9
24	21	17	6		10	12	20	31	35

06.0	05.1	03.3
9.1	10.0	11.8
27	35	50

15.1
0.0
42

05.8	04.8	04.8	05.6	05.5	05.1	07.8	09.3	12.4	14.4
9.3	10.3	10.3	9.5	9.6	10.0	7.3	5.8	2.7	0.7
20	19	17	7		10	12	15	31	38

06.2	08.2	07.2	05.8	04.8
8.9	6.9	7.9	9.3	10.3
23	28	35	44	50

09.1	08.1	06.6	06.6	07.6	07.5	07.1	09.9	12.1	14.8
6.0	7.0	8.5	8.5	7.5	7.6	8.0	5.2	3.0	0.3
28	22	20	18	7		10	11	17	25

08.2	06.5	04.6
6.9	8.6	10.5
33	41	50

Sta + Δ - Elev

915.12

*
43 + 35

✓

*
+ 70

✓

*
44 + 00

✓

TP 13.16 926.16 2.12 ^{913.00}
~~923.00~~

Lt

L

Cool, partly cloudy, 60°

Rt

71

10.3	09.0	09.1	09.8	09.5	09.1	13.1	14.2
4.8	6.1	6.1	5.3	5.6	6.0	2.0	0.9
22	20	18	11		8.5	11.4	16

08.6	07.1	03.9
6.5	8.0	11.2
30	35	50

12.0	10.9	10.9	11.6	11.6	10.9	14.2
3.1	4.2	4.2	3.5	3.5	4.2	0.9
22	20	18	11		9	10.5

08.3	07.1	04.0
6.8	8.0	11.1
33	37	50

13.2	12.6	12.6	13.2	13.1	12.7	14.8
1.9	2.5	2.5	1.9	2.0	2.4	0.3
22	19	17	9		9	10

09.3	05.0
5.8	10.1
34	

Sta

+

π

-

Elev

926.16

41+75

42+00

42+28

42+65

43+00

43+35

43+55

43+70

Lt

E

Rt

May 23, 1957
cool, partly cloudy 60° 72

P. 16.6 19.2
9.6 7.0
70 85

P. 16.8 20.1 23.4
9.4 6.1 2.8
57 72 87

P. 16.5 20.3 24.1 25.8
9.7 5.9 2.1 0.4
47 65 86 93

P. 17.7 21.9 23.7 24.6
8.5 4.3 2.5 1.6
51 74 83 89

P. 16.4 18.5 22.6 24.0 25.7
9.8 7.7 3.6 2.2 0.5
31 34 63 75 82

P. 17.4 21.0 23.6 24.7 25.6
8.8 5.2 2.6 1.5 0.6
30 45 61 73 78

washout right 15' wide on top 4' on bottom
39' in length. 9' right to 48' right

14.2 15.3 16.2 17.7 18.1
12.0 10.9 10.0 8.5 8.1
11.5 17 26 32 35

P.

26.0 24.1 21.8
0.2 2.1 4.4
91 71 50

Sta

+

π

-

Elev

926.16

44+00

✓

+33

✓

+69

✓

Lt

 cloudy - windy 65° 73
 Rt

 16.1 18.8 18.5 19.2 22.1
 10.1 7.4 7.7 7.0 4.1
 15 30 33 38 47

 26.0 24.3 23.8
 0.2 1.9 2.4
 83 69 63

 14.8 14.8 13.9 14.5 14.5 14.3 16.9 17.7 20.5 20.5
 11.4 11.4 12.3 11.7 11.7 11.9 9.3 8.5 5.7 5.7
 25 22 18 9 9 10 14 31 33

 12.6 11.4 08.4
 13.7 14.8 17.8
 35 38 50

 25.7 24.0 21.9
 0.5 2.2 4.3
 80 61 42

 17.3 16.1 15.6 15.1 15.8 15.7 15.6 18.0 18.9 19.8 21.4
 8.9 10.1 10.6 11.1 10.4 10.5 10.7 8.2 7.3 6.4 4.8
 31 27 22 19 9 7.5 9 13 23 32

 16.3 14.4
 9.9 11.8
 37 50

 25.1 24.0 22.8
 1.1 2.2 3.4
 75 60 48

Sta + π - Elev

926.16

45+00

✓

+24

✓

+55

✓

TP

8.72 927.06

7.82

~~918.34~~
~~928.34~~

Lt.

£

24.4 23.1 19.3
Cloudy Windy 65° 74
Pt.

17.1	16.6	16.0	16.8	16.7	16.4	18.3	19.9	21.6	23.1
9.1	9.6	10.2	9.4	9.5	9.8	7.9	6.3	4.6	3.1
26	21	19	8		7	8	19	33	50

20.5 20.2 19.8 19.2
5.7 6.0 6.4 7.2
31 36 43 50

P.

18.4	17.5	17.2	16.8	17.5	17.3	17.4	17.8	19.2	20.5	21.3
7.8	8.7	9.0	9.4	8.7	8.9	8.8	8.4	7.0	5.7	4.9
27	24	21	20	9		4	6	15	31	45

21.5 21.5 20.8
4.7 4.7 5.4
30 36 50

P.

21.3
4.9
50

21.8	21.8	18.4	17.7	18.1	18.1	18.0	18.7	20.1	22.0	22.7
4.4	4.4	7.8	8.5	8.1	8.1	8.2	7.5	6.1	4.2	3.5
42	31	24	20	9		4	6	19	40	50

21.7
5.0
50

P.

23.5 walk
2.70
63

Sta + π - Elev

927.06

46+00

✓

+35

✓

+74

✓

Lt

~~Lt~~
 July 23, 1957
 Cloudy & Windy 65° 75°
 Rt

19.0	18.5	18.2	18.4	18.3	18.2	18.7	20.0	21.7	22.6
8.1	8.6	8.9	8.7	8.8	8.9	8.4	7.1	5.4	4.5
27	20	18	8		4.5	5.0	19	37	50

21.8	21.6	21.6
5.3	5.5	5.5
34	46	50

 23.03
 New Corho.
 4.03
 70

19.9	17.9	17.6	17.9	18.0	17.8	18.5	20.4	21.4
7.2	9.2	9.5	9.2	9.1	9.3	8.6	6.7	5.7
26	19	17	8		5	6	15	30

20.8	20.8
6.3	6.3
36	50

23.5	22.3
3.6	4.8
50	36

17.7	16.5	16.8	17.4	17.4	17.4	18.0	20.5	21.2	22.8
9.4	10.6	10.3	9.7	9.7	9.7	9.1	6.6	5.9	4.3
34	22	17	6		5	5.5	13	20	34

19.0
8.1
50

24.7	23.7
2.4	3.4
50	44

Sta + π - Elev

927.06

*
47+00

✓

*
+50

✓

*
48+00

✓

BM

5.82 921.24

921.23

Lt

E

May 25, 1975
Partly cloudy

Rt

76

16.4	15.8	16.7	17.2	17.2	17.2	18.2	21.5	22.3	24.1
10.7	11.3	10.4	9.9	9.9	9.9	8.9	5.6	4.8	3.0
41	28	19	9		5	7	16	20	35

17.6
9.5
50

26.7
0.4
51

14.4	14.6	16.6	17.0	17.1	17.2	17.8	18.8	23.6	24.8
12.7	12.5	10.5	10.1	10.0	9.9	9.3	8.3	3.5	2.3
36	26	18	8		5	7	11	19	29

15.9
11.2
58

26.3
0.8
36

12.3	15.2	16.6	17.2	17.3	17.4	18.3	23.4	24.4	25.2
14.8	11.9	10.5	9.9	9.8	9.7	8.8	3.7	2.7	1.9
37	18	16	6		7	8	19	24	32

11.8
15.3
50

26.3
0.8
35.5

25.7
1.4
34

Top bolt in Mont E Co. Rd "G" E McMenamy

Sta	+	Δ	-	Elev
BM	1.80	924.88		923.08
* 48+50				
✓				
* + 70				
✓				
* 49+00				
✓				

Lt

L

May 24, 1957
clear 65°
RT

77

Spike in P.P. S.E. Cor. Co Rd 16 E. McHenry

10.8	11.2	14.1	17.2	18.3	18.1	19.0	23.7	24.6
14.1	13.7	10.8	7.7	6.6	6.8	5.9	1.2	0.3
46	34	18	13		9	9.5	18	21

09.6
→ 15.3
50

P.

09.4	11.2	15.5	17.8	18.7	18.6	19.9	20.6	20.9	22.4
15.5	13.7	9.4	7.1	6.2	6.3	5.0	4.3	4.0	2.5
46	32	15	12		10	11.5	14	16.5	20.5

09.2
→ 15.7
50

P.

24.7
0.2
23

10.8	13.5	16.6	18.7	19.6	19.4	21.1	21.7	24.9
14.1	11.4	8.3	6.2	5.3	5.5	3.8	3.2	0.0
34	22	14	12		11	13	16	20.5

09.4
→ 15.5
50

P.

Sta + π - Elev

924.88

*
49+28

✓

*
+60

✓

*
50+00

✓

BM 2.12 925.20 1.80 923.08 (923.08)

Lt

E

May 24, 1957
clear 65°
RT

78

12.5	17.3	19.5	20.3	20.1	21.4	22.2	24.9
12.4	7.6	5.4	4.6	7.8	3.5	2.7	0.0
34	16	14		10	11	15.5	19.5

P.

10.0
14.9
50

15.2	18.8	20.3	20.8	20.5	21.5	21.9	24.9
9.7	6.1	4.6	4.1	4.4	3.4	3.0	0.0
34	16	14		11	11.5	20	22.5

P.

13.0
11.9
50

17.5	19.5	20.6	20.1	20.6	20.2	21.1	21.7	23.9
7.4	5.4	4.3	4.8	4.3	4.7	3.8	3.2	1.0
34	17	15	12		11.5	12	20	21.5

P.

15.1
9.8
50

24.9 24.4
0.0 0.5
36 26

Spike in P.P. S.E. Cor Corl 6 & McMenemy

Sta	+	π	-	Elev
-----	---	-------	---	------

		925.20		
--	--	--------	--	--

50+35				
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✓				
---	--	--	--	--

+70				
-----	--	--	--	--

✓				
---	--	--	--	--

51+00				
-------	--	--	--	--

✓				
---	--	--	--	--

Lt

E

 May 24, 1951
 Clear 65°
 Pt

79

18.2	19.5	20.2	19.3	19.8	19.5	20.0	20.2	21.4
7.0	5.7	5.0	5.9	5.4	5.7	5.2	5.0	3.8
33	16.5	15	13		12	12.5	17	23

P.

16.7
 8.5
 50

22.1 22.0
 3.1 3.2
 50 35

17.9	18.4	19.1	18.6	19.2	18.8	19.4	19.3	19.2
7.3	6.8	6.1	6.6	6.0	6.4	5.8	5.9	6.0
28	16	14	12		12	12.5	23	35

P.

18.1 17.6
 7.1 7.6
 34 50

19.1
 6.1
 50

16.9	17.8	19.0	18.4	18.9	18.5	19.2	18.7	18.2
8.3	7.4	6.2	6.8	6.3	6.7	6.0	6.5	7.0
26	16	14	11		12	12.5	22	33

P.

16.4 15.0
 8.8 10.2
 35 50

18.1
 7.1
 50

Sta	+	π	-	Elev
-----	---	-------	---	------

		925.20		
--	--	--------	--	--

51+31				
-------	--	--	--	--

✓				
---	--	--	--	--

+ 58				
------	--	--	--	--

✓				
---	--	--	--	--

+ 83				
------	--	--	--	--

✓				
---	--	--	--	--

Lt

May 24, 1957
Clear 65° Rt

80

13.9	16.6	18.4	18.1	18.7	18.3	18.8	18.0	17.6
11.3	8.6	6.8	7.1	6.5	6.9	6.4	7.2	7.6
34	18	15	12		12	12.5	22	33

13.0
12.2
42

12.1
13.1
50

17.1
8.1
50

11.8	13.4	17.9	18.9	18.3	17.8	17.0	16.4
13.4	11.3	7.3	6.5	6.9	7.4	8.2	8.8
34	20	13		12	16	22	32

11.3
13.9
50

16.1
9.1
50

14.9	14.7	16.2	18.2	18.8	18.5	16.9	16.0	15.9
10.3	10.5	9.0	7.0	6.4	6.7	8.3	9.2	9.3
35	25	16	11		13	19	33	50

15.8
9.4
50

Sta + π - Elev

925.20

52+00

✓

↓

+15

✓

↓

+24

✓

Lt

Z

May 24, 1957
clear 68°
Rt

81

17.7	17.7	18.4	18.5	19.2	18.8	17.6	16.7	16.1
7.5	7.5	6.8	6.7	6.0	6.4	7.6	8.5	9.1
32	19	17	11		12	18	34	50

19.2
6.0
50

19.0	19.4	19.1	19.8	19.2	17.9	17.2	16.7
6.2	5.8	6.1	5.4	6.0	7.3	8.0	8.5
32	12	10		14	19	35	50

21.0
4.2
50

19.3	19.7	20.0	20.2	19.4	18.6	17.9	17.8
5.9	5.5	5.2	5.0	5.8	6.6	7.3	7.4
25	15	10		17	21	42	50

19.9
5.3
36

20.5
4.7
50

Sta + π - Elev

✓

925.20

52 +35 Shoulder line

✓

+45 Edge of pavement

✓

+57 $\pm$ C.O.Rd "6"

+58.8 Mont

BM

3.96 921.24

921.23

May 24, 1957
Clear 68°

Lt

£

Rt

82

21.0	20.9	21.0	20.9	20.5	19.9	19.8	19.7
4.2	4.3	4.2	4.3	4.7	5.3	5.4	5.5
38	27	10		13	28	44	50

21.4
3.8
50

P.

21.1	21.7	21.2	20.8	20.4
3.1	3.5	4.0	4.4	4.8
50	25		25	50

P.

23.0	22.1	21.7	21.3	20.8	20.5	19.8
2.2	3.1	3.5	3.9	4.4	4.7	5.4
100	50	25		25	50	100

P.

Mont £ Co Rd. 6, & McMenemy

Sta + π - Elev

BM 13.57 936.65

923.08

47+00

+50

48+00

+50

+70

49+00

Spike in PP

Lt.

June 2 Pt

83

P. 26.4 31.2 34.5
10.3 5.5 2.2
52 71 87

P. 28.4 32.7 35.9
8.3 4.0 0.8
53 67 80

P. 27.3 29.9 34.1 35.7
9.4 6.8 2.6 1.0
43 55 71 82

P. 25.7 26.8 28.6 30.7 33.3 34.3
11.0 9.9 8.1 6.0 3.4 2.4
27 36 49 59 72 81

P. 26.4 27.1 29.0 31.4 33.5 34.7
10.3 9.6 7.7 5.3 3.2 2.0
28 35 48 60 72 85

P. 27.2 28.7 30.1 33.5 34.8 34.9
9.5 8.0 6.6 3.2 1.9 1.8
26 36 47 66 75 86

Sta + π - Elev

936.65

49+28

+60

50+00

BM

13.56 923.09 923.08

The End

June 3, 1957

84

BT

P	27.4	29.2	30.6	31.7	34.3	34.1
	9.3	7.5	6.1	4.0	2.4	2.6
	26	37	47	60	75	86

P	27.7	28.6	30.0	31.0	31.3	31.1
	9.0	8.1	6.7	5.7	5.4	5.6
	27	36	50	65	80	91

P	25.6	26.3	26.9
	11.1	10.4	9.8
	44	62	78

Spike in PPSE Cor. G & McMenamy

Sta	i	π	-	Elev
TP	6.21	937.71		931.50

11			9.2	28.5	28.6
----	--	--	-----	------	------

12			5.3	32.4	32.5
----	--	--	-----	------	------

10+83 O.K.

11

✓

+27

✓

FK
KP
AB

April 29, 1958

85

iron Rt Page 33

29.6	28.9	28.1	28.4	28.5	28.3	27.7	28.3	28.4
8.1	8.8	9.6	9.3	9.2	9.4	10.0	9.4	9.3
20	14	12	6		6	14	16	22
30.9	30.6	35.6	34.7			29.3	29.1	
6.8	7.1	2.1	3.0			8.4	8.6	
22	27	33	50			50	41	
31.2	30.2	30.0	29.3	29.6	29.3	28.9	29.4	29.8
6.5	7.5	7.7	8.4	8.1	8.4	8.8	8.3	7.9
21	18	13	11		7	15	25	50
30.4	33.2	32.3						
7.3	4.5	5.4						
27	37	50						

Sta	+	π	-	Elev.
-----	---	-------	---	-------

11 +54				
--------	--	--	--	--

✓				
---	--	--	--	--

+82	O.K.	No Change		
-----	------	-----------	--	--

April 29, 1958

RT

86

41

30.4

31.6

32.4

30.4

30.6

30.2

30.2

29.8

29.8

73

6.1

5.3

73

7.1

7.5

7.5

7.9

7.9

29

22

15

11

12

15

20

9.5

31.0

30.7

30.0

→ 6.7

2.0

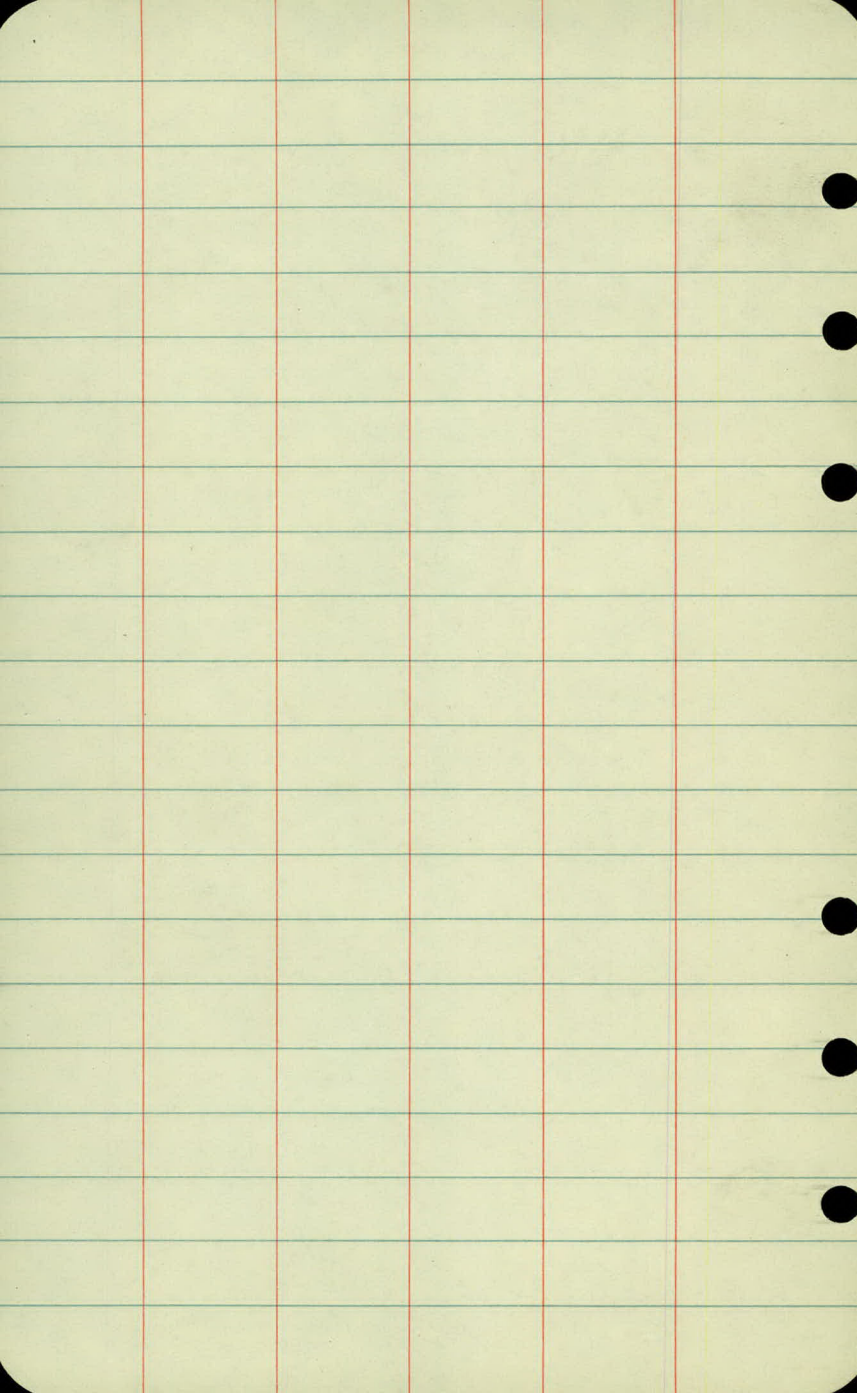
7.7

32

50

50

✓



FK
RG
KP
AB

May 20, 1958

87

X-Section Extensions

Sta	+	π	-	Elev.
-----	---	-------	---	-------

BM	13.23	923.21		
----	-------	--------	--	--

				(909.98)
--	--	--	--	----------

24+00				
-------	--	--	--	--

+42				
-----	--	--	--	--

+68				
-----	--	--	--	--

✓				
---	--	--	--	--

+75				
-----	--	--	--	--

✓				
---	--	--	--	--

May 20, 1958

88

Lt

Spike in T.P. SW. Cor McMenemy & Soo RR

07.5	12.0	06.6	07.5
15.7	11.2	16.6	15.7
151	130	110	90

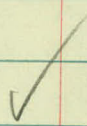


13.2	23.7	25.2	20.7	08.1
5.5	10.0	+0.5	+2.0	2.5
151	129	115	93	54

✓ 93
140

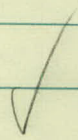
17.7	23.7	27.2	24.2	24.2	08.5
5.5	+0.5	+4.0	+1.0	+1.0	14.7
185	158	119	100	75	44

08.2
15.0
207



27.7	23.2	21.1	19.7	22.8	08.4
+4.5	0.0	2.1	3.5	0.4	14.8
113	107	103	77	70	39

23.7	18.7	13.2	5.5
+0.5	4.5	10.0	
148	180	201	



Sta + π - Elev

923.21

25+00

✓

+27

✓

+60

24+676 ±

14.43 908.8 (908.9)

May 20, 1958

89

27.2	23.2	14.5	13.3	10.2
+4.0	0.0	8.7	9.9	13.0
131	120	100	55	36

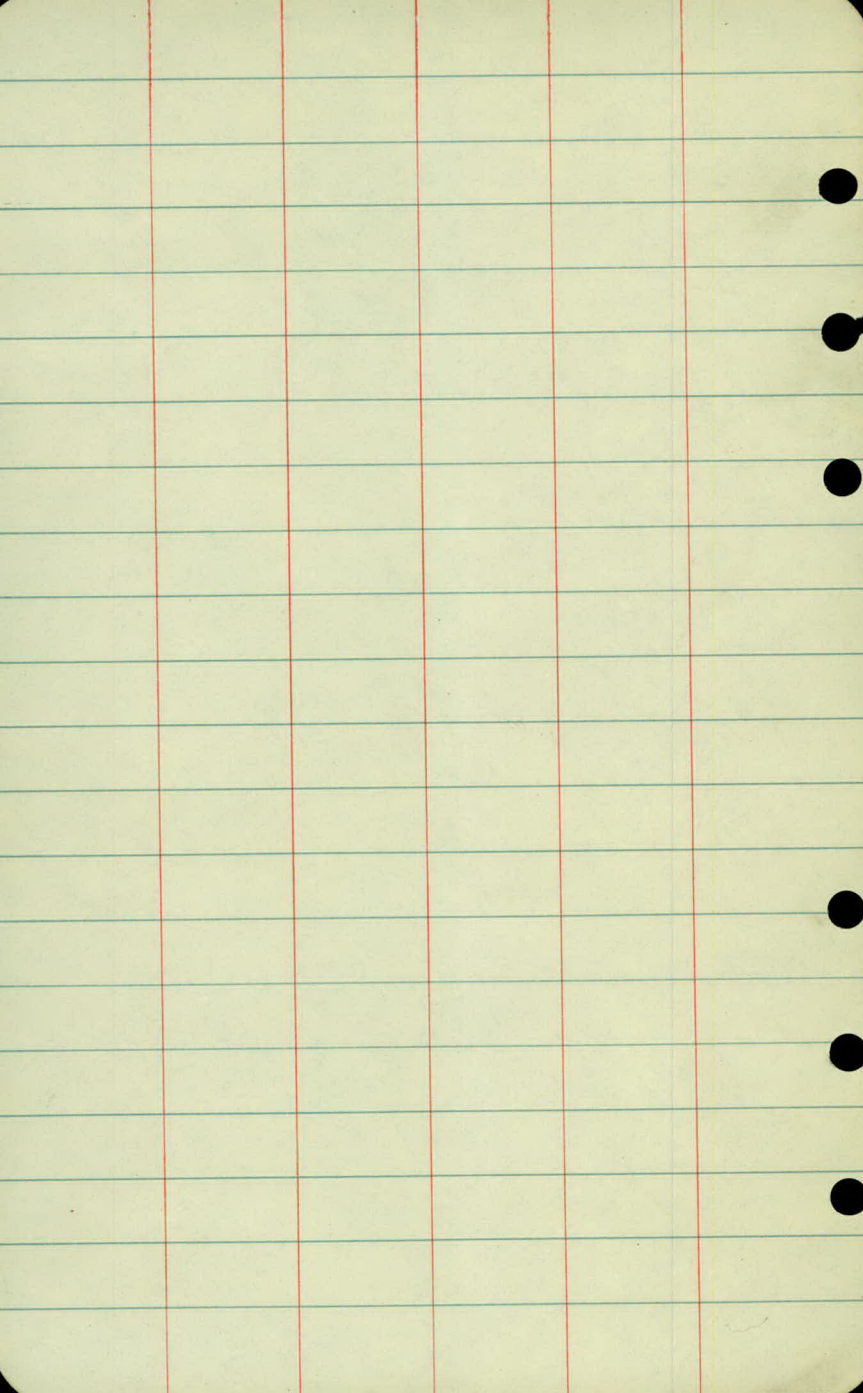
26.2	22.2	
+3.0	1.0	5.5
182	195	

29.2	27.5	23.2	15.6	13.9	13.9
+6.0	+4.3	0.0	7.6	9.3	9.3
149	140	135	127	100	77

9.5

28.7	23.2	13.2
+5.5	0.0	10.0
180	212	243

31.2	31.2	23.2	16.0	12.3
+8.0	+8.0	0.0	7.2	10.9
279	179	141	118	77



check levels

Sta	+	π	-	Elev
B.M	2.09	923.32		921.23

	0.22	910.55	12.99	910.33
--	------	--------	-------	--------

B.M	5.59	910.55	5.59	904.96
-----	------	--------	------	--------

	1.23	898.59	13.59	896.96
--	------	--------	-------	--------

	11.74	910.18	0.15	898.44
--	-------	--------	------	--------

	1.40	921.50	0.08	910.10
--	------	--------	------	--------

	5.65	915.83	11.32	910.18
--	------	--------	-------	--------

	12.61	928.33	0.11	915.72
--	-------	--------	------	--------

	12.62	940.85	0.14	928.19
--	-------	--------	------	--------

	3.20	931.21	12.84	928.01
--	------	--------	-------	--------

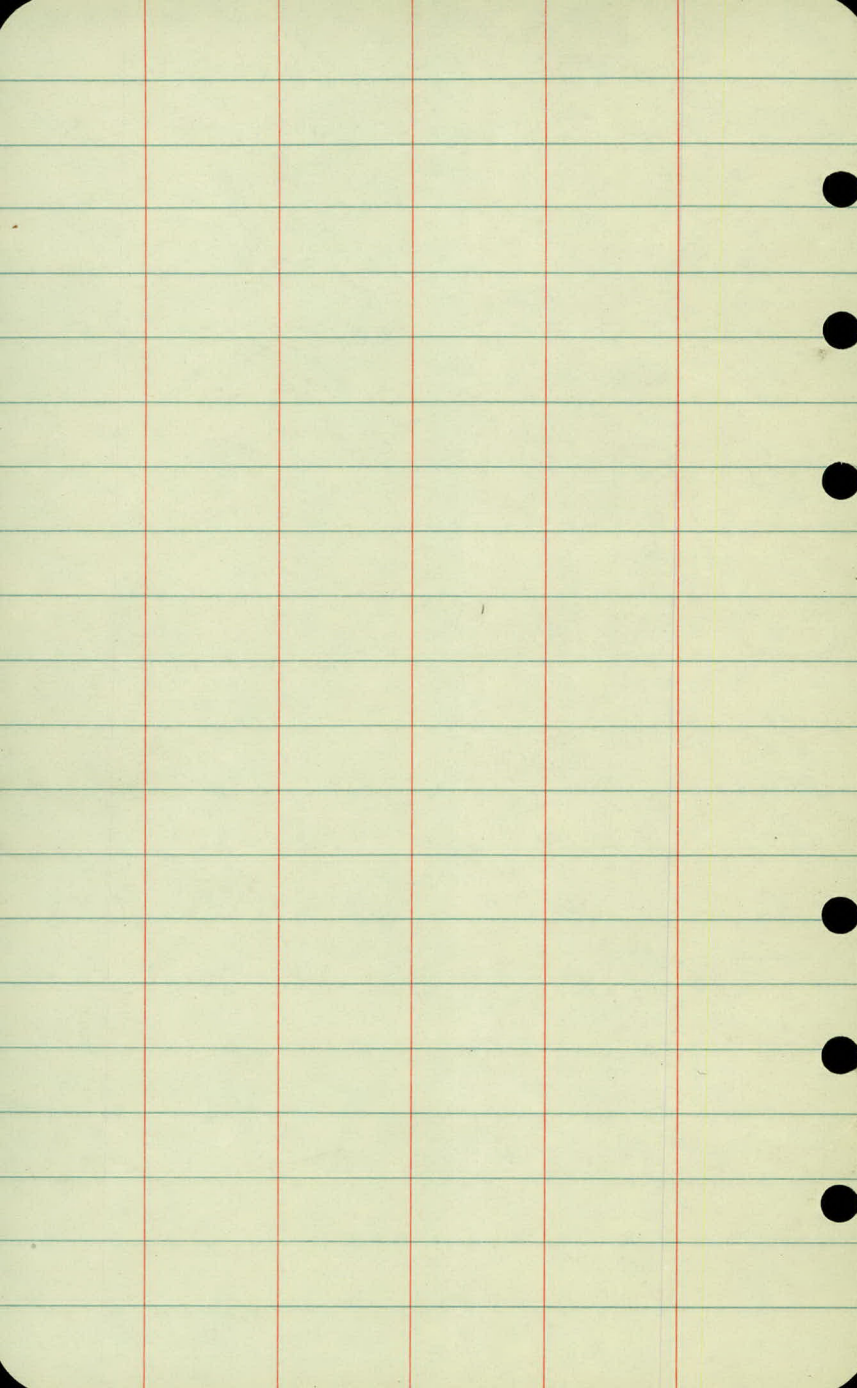
	7.77	938.26	0.72	930.49
--	------	--------	------	--------

			10.98	927.28
--	--	--	-------	--------

Mon

Top Bolt & McMonemy & GRIG

Spt in PP Rt Sta 41+2



$$\begin{array}{r} 921.23 \\ 209 \\ \hline \end{array}$$

$$\begin{array}{r} 923.32 \\ 1299 \\ \hline \end{array}$$

$$\begin{array}{r} 910.33 \\ 22 \\ \hline \end{array}$$

$$\begin{array}{r} 910.55 \\ 1359 \\ \hline \end{array}$$

$$\begin{array}{r} 896.96 \\ 163 \\ \hline \end{array}$$

$$\begin{array}{r} 858.59 \\ 15 \\ \hline \end{array}$$

$$\begin{array}{r} 858.44 \\ 1174 \\ \hline \end{array}$$

$$\begin{array}{r} 810.18 \\ 05 \\ \hline \end{array}$$

$$\begin{array}{r} 910.10 \\ 1140 \\ \hline \end{array}$$

$$\begin{array}{r} 931.50 \\ 1132 \\ \hline \end{array}$$

$$\begin{array}{r} 910.18 \\ 560 \\ \hline \end{array}$$

$$\begin{array}{r} 910.83 \\ 11 \\ \hline \end{array}$$

$$\begin{array}{r} 915.72 \\ 1261 \\ \hline \end{array}$$

$$\begin{array}{r} 928.33 \\ 819 \\ \hline \end{array}$$

$$\begin{array}{r} 92819 \\ 1266 \\ \hline \end{array}$$

$$\begin{array}{r} 740.85 \\ 1284 \\ \hline \end{array}$$

$$\begin{array}{r} 72801 \\ 320 \\ \hline \end{array}$$

$$\begin{array}{r} 931.21 \\ -22 \\ \hline \end{array}$$

$$\begin{array}{r} 930.49 \\ 227 \\ \hline \end{array}$$

$$\begin{array}{r} 938.24 \\ 1098 \\ \hline \end{array}$$

$$\begin{array}{r} 92728 \\ \hline \end{array}$$

921.23

185

923.08

1279

910.09

22

910031

91018

24

91031

559

90986

90472

810

82

91282

410

90872

FK
RG
AB
JH

Nov 25, 1958

1

Man Monemey

P. P Locations

1 page

0+00 PP 32 ✓ not moved

2+94 PP 32.5 ✓

5+92 PP 48' Rt moved

8+93 PP 34 ✓ not moved

11+95 PP 35 ✓ " "

15+35 PP 55' Rt moved

18+33 PP 36 ✓ not moved

21+20 PP 36.5 ✓ " "

23+33 PP 36 ✓ " "

24+36 PP 36.5 ✓ " "

25+75 PP 38 ✓ " "

27+30 PP 50 moved

29+29 PP 69 "

32+31 PP 56 "

35+27 PP 53 "

38+29 PP 48 "

41+27 PP 33 ✓ not moved

44+33 PP 48 moved

47+29 PP 43 "

50+33 PP 29 ✓ not moved?

X sections

McMenamy & RR tracks
McMenamy

5 pages

A

Sta + Δ - Elev

4.60 ~~4.66~~
913.52

908.92

0+00

200' west of ~~McMenamin~~ ^{McMenamy}
on center of tracks

0+63

✓

0+87

✓

2

McMenamy

$$\begin{array}{r} 10.4 \\ 3.1 \\ \hline 34 \end{array} \quad \begin{array}{r} 03.9 \\ 9.6 \\ \hline 26 \end{array}$$

Sta	+	T	-	Elev
-----	---	---	---	------

		4.60		
		913.52		

1+00				
------	--	--	--	--

✓				
---	--	--	--	--

1+10				
------	--	--	--	--

✓				
---	--	--	--	--

		4.60	908.92	
--	--	------	--------	--

RG
KD
AB

LT

APRIL 23 1958
Cool 45°
E

RT

3

3.7	6.2	6.2	6.0	5.9	6.0	6.3	7.8	7.4
21	14	9	5		5	9	15	23

1.6	0.0	12.0
24	26	49

3.7	6.2
39	32

6.2	6.2	6.4	5.9	5.8	5.9	6.3	6.0	6.1
15	10	8	5		5	8	9	16

0.9	13.5
24	50

1.3	5.4
40	27

north rail on E ~~McMenemie~~
McMenemy

Sta	+	π	-	Elev
	4.56	913.48 4.56		90892

1+37

✓

1+88

✓

2+00 = E 170° 17200 way st

2+10

✓

R6
KP
AB

Lt

APRIL 24, 1958
Cool 40°
Rt 4

north rail on E McMenomnie

13.0	07.9	07.5	07.8	07.9	07.9	07.5	08.1	08.1
0.5	5.6	6.0	5.7	5.6	5.6	6.0	5.4	5.4
29	17	8	5		5	7	9	26

13.5-
0.0
30
+ 11.1
50

08.3
5.2
42

12.6	09.1	08.8	08.9	08.8
0.9	4.4	4.7	4.6	4.7
43	37	16	5	

13.5-
0.0
44
+ 0.8
4.6

08.5	08.3	08.1	08.3	08.3
5.0	5.2	5.4	5.2	5.2
5	5	8	10	23

08.6
4.9
41

Sta + π - Elev

~~4.56~~
913.48

2+40

✓

2+55

✓

4.56 908.92

BM

3.50 909.98 909.98

RG
KP
AB

Lt

APR 12 24 1958
± COOL 40°

Rt

5

✓ 08.7	08.4	08.0	08.1	09.9
4.8	5.1	5.5	5.4	3.6
	5	8	12	17

✓ 09.5	09.6	10.4
4.0	3.9	3.1
38	30	25

07.3	08.0	07.8	08.4	08.8	08.5	07.9	09.9	10.0
6.2	5.5	5.7	5.1	4.7	5.0	5.6	3.6	3.5
12	9	8	5		6	10	16	21

08.0	07.3	08.0	10.1	11.0	09.5	10.7
5.5	6.2	5.5	3.4	2.5	4.0	2.8
16	26	47	42	36	31	25

McMenemy

north rail on McMenemy
spike in PP SW Cor McMenemy
and 500 line tracks

