

Book # 92-Dr. # 8

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

X-Section Survey

U. FARM GRAVEL PIT

: _____ To _____

Road Acc't. No. _____

ate Filed 1935

File 8

8/8/35

Original
X Sections
U Farm Gravel Pit

Platted
Aug. 27, 1935

Sta	+	π	-	Elev.
B.M.	170	201.70		Assumed 200.00

0-35				Commonwealth St. 200.2
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0-23				Shoulder 200.00
------	--	--	--	-----------------

0-17				Toe Slope 97.6
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0				Nb. Fence 97.6
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+25				98.0
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+50				97.8
-----	--	--	--	------

+75				96.6
-----	--	--	--	------

+00				96.9
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Top Post E of No. Ent. to P.1

1.5

1.7

4.1

Fcc										Fcc				Sh	
5.2	5.1	5.0	4.6	4.0	3.6	3.5		4.2	4.6	4.3	4.3	4.5	4.2	2.5	
127	115	94-76	71	45	28	9	4.1	18	24	36	39	65	80	97	
										4.8	3.9	2.6	2.4		
										146	119	109	100		

Fcc														Sh+Fcc	
5.9	4.5	3.2	3.4	3.9	3.4	2.8		3.9	4.5	5.1	4.7	4.2	Sh	4.6	
122	114	108	83	69	46	15	3.7	14	23	45	79	87-94		113	
6.9														5.9	5.6
133														155	137

Fcc														Sh	
3.7	4.2	4.7	2.0	2.6	3.2	3.6	3.2	3.9	4.0	4.8	5.8	5.7	5.1	4.8	5.2
115	104	93	76	62	42	19	8		5	12	34	38	77	85	107
2.5	2.1											6.6	6.5	5.7	Fcc
125	142											155	139	113	

Fcc														Sh	
2.0	2.3	2.6	4.2	1.8	2.3	3.0	2.8	4.4	5.1	5.9	6.4	6.8	6.2	5.2	5.9
115	100	88	76	64	45	35	20	12		14	33	56	69	84	111
1.5	2.1														7.3
128	149														144

Fcc														Sh	
2.5	1.5	1.5	3.0	1.9	2.9	4.0	4.5	4.8	4.9	6.1	7.1	7.2	6.8	5.6	6.1
141	114	110	71	42	25	17	11		4	10	27	58	75	85	106
												8.0	7.8	7.5	6.7
												147	140	126	110

Sta	+	π	-	Elev
		201.70		
1 + 25				96.8
	+50			97.1
0	9.79	205.85	5.64	196.06
3				97.8
	+25			98.8
	+50			99.5
	+75			200.8
0	9.40	212.49	2.76	203.09
4				033

Reverse Lt to Rt This Section

A

$\frac{Fec}{47.0}$	$\frac{Sh}{6.0}$	$\frac{Sh2}{5.9}$	$\frac{6.9}{7.4}$	$\frac{7.1}{6.6}$	$\frac{6.6}{4.7}$	$\frac{4.7}{8}$	4.9	$\frac{4.7}{6}$	$\frac{4.0}{21}$	$\frac{2.6}{39}$	$\frac{2.3}{46}$	$\frac{2.8}{58}$	$\frac{1.7}{71}$	$\frac{1.2}{92}$
$\frac{7.7}{116}$	$\frac{7.6}{126}$										$\frac{1.0}{142}$	$\frac{1.5}{132}$	$\frac{1.32}{114}$	$\frac{1.4}{100}$

$\frac{Fec}{0.5}$	$\frac{0.4}{97}$	$\frac{0.8}{83}$	$\frac{1.2}{74}$	$\frac{1.3}{66}$	$\frac{2.1}{38}$	$\frac{3.5}{25}$	$\frac{4.3}{10}$	4.6	$\frac{4.7}{8}$	$\frac{5.0}{11}$	$\frac{4.9}{16}$	$\frac{7.1}{29}$	$\frac{7.2}{45}$	$\frac{7.4}{69}$	$\frac{Sh}{6.3}$
$\frac{0.8}{136}$	$\frac{0.9}{148}$											$\frac{7.8}{124}$	$\frac{7.5}{117}$	$\frac{Fec}{7.12}$	$\frac{Sh}{6.2}$

$\frac{4.0}{141}$	$\frac{Fec}{4.7}$	$\frac{5.6}{100}$	$\frac{7.7}{67}$	$\frac{8.6}{34}$	8.1	$\frac{6.7}{58}$	$\frac{6.1}{83}$	$\frac{6.3}{95}$	$\frac{6.3}{100}$	$\frac{Fec}{6.5}$	$\frac{7.0}{103}$	$\frac{7.0}{123}$	$\frac{6.9}{142}$
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$\frac{Fec}{3.5}$	$\frac{3.2}{115}$	$\frac{3.4}{100}$	$\frac{4.6}{75}$	$\frac{6.6}{42}$	$\frac{7.0}{25}$	7.1	$\frac{6.3}{29}$	$\frac{5.2}{55}$	$\frac{Fec}{5.1}$	$\frac{5.4}{101}$	$\frac{4.8}{111}$	$\frac{2.4}{120}$	$\frac{2.4}{133}$
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$\frac{Fec}{3.2}$	$\frac{2.5}{116}$	$\frac{2.6}{100}$	$\frac{3.4}{82}$	$\frac{5.3}{50}$	$\frac{6.0}{27}$	$\frac{6.6}{14}$	6.4	$\frac{5.8}{16}$	$\frac{3.5}{47}$	$\frac{2.5}{72}$	$\frac{Fec}{2.02}$	$\frac{2.2}{100}$	$\frac{2.2}{129}$
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$\frac{3.8}{144}$	$\frac{Fec}{2.9}$	$\frac{2.8}{100}$	$\frac{3.7}{74}$	$\frac{4.7}{42}$	$\frac{5.5}{29}$	5.1	$\frac{5.0}{7}$	$\frac{4.1}{11}$	$\frac{3.4}{20}$	$\frac{2.7}{43}$	$\frac{1.8}{84}$	$\frac{1.4}{93}$	$\frac{Fec}{1.0}$
											$\frac{2.0}{145}$	$\frac{1.3}{115}$	

$\frac{Fec}{11.2}$	$\frac{10.0}{113}$	$\frac{9.9}{100}$	$\frac{9.8}{48}$	$\frac{9.3}{29}$	$\frac{9.3}{25}$	9.2	$\frac{9.7}{13}$	$\frac{9.2}{20}$	$\frac{9.0}{54}$	$\frac{8.1}{77}$	$\frac{7.1}{97}$	$\frac{Fec}{10.0}$	$\frac{8.0}{123}$
												$\frac{9.1}{148}$	

Sta	+	π	-	Elev.
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212.49

4+25

03.3

+50

06.4

+75

06.8

5+00

07.7

+25

07.8

+50

208.0

①

4.10

212.81

4.38

208.11

+75

07.6

Sta + π - Elev.

212.81

6+00

07.2

+25

06.0

+50

04.7

○

8.60

204.21

BM

1.88

201.88

200.00

1+75

97.2

2+00

97.0

+25

95.9

+50

95.9

Feeby

5.4	5.1	4.5	3.8	3.7	5.0	5.6	7.9	11.7	12.4	13.2	15.7
149	115	100	81	58	13		31	84	93	100	126

Fee

5.5	5.1	4.2	5.3	6.8	8.5	12.1	12.8	13.8	15.8
152	111	100	74	35	32	84	91	100	122

Fee

5.6	5.8	5.9	5.5	6.3	8.1	9.0	12.8	13.9	16.3
136	105	100	71	46		25	90	100	135

Top Stake Sta. 7100

Top Post @ NW Cor Pit

Fee

1.6	1.8	1.9	1.5	1.4	2.2	2.0	2.7	4.7	5.1	5.6	6.2	6.0	5.5	6.3	5.7
126	116	100	89	64	51	30	16	18	28	35	50	63	76	84	

0.6

143												7.2	6.5	5.8
												156	115	100

Fee

3.6	4.1	3.8	3.5	3.3	3.5	4.2	4.9	4.5	4.7	5.1	4.1	3.7	4.1	4.3	5.1
115	100	92	71	50	33	24	14	6	11	26	47	64	74	79	97

2.9

123	143														
-----	-----	--	--	--	--	--	--	--	--	--	--	--	--	--	--

12

4.3	5.5	6.6	6.9	6.1	5.7
254	246	210	155	120	106

Fee

2.9	5.0	6.4	5.7	5.4	5.2	5.3	6.0	6.0	5.3	4.6	3.1	2.2	2.8	3.4
145	114	97	92	79	49	25	10		14	20	39	55	80	99

1.2

5.3	6.8	7.3	6.2	4.8	3.9
300	240	200	186	149	119

Fee

5.5	6.4	5.9	6.0	7.0	7.3	6.6	6.7	6.0	5.6	4.7	3.4	2.5	2.0	3.4	3.9
100	86	79	56	47	35	27	10		5	20	36	54	73	105	122

4.2

114	140														
-----	-----	--	--	--	--	--	--	--	--	--	--	--	--	--	--

1.2

5.3	6.8	7.3	6.2	4.8	3.9
300	240	200	186	149	119

Sta	+	π	-	Elev
		201.88		

2+75

96.9

B.M.

3.49

207.70

204.21

6+75

03.4

7+00

03.1

+25

02.6

+50

01.7

+75

00.1

Sta.	+	π	-	Elev.
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207.70

8+00

98.5

+25

97.6

+50

96.9

+70

S. Fence of P.t. 96.3

B.M.

10.79 196.91

$\frac{5.9}{136}$ $\frac{6.5}{100}$ $\frac{6.4}{89}$ $\frac{6.6}{56}$ $\frac{7.3}{31}$ $\frac{8.0}{18}$ $\frac{9.2}{5}$ $\frac{9.8}{17}$ $\frac{9.5}{42}$ $\frac{8.9}{58}$ $\frac{6.8}{85}$ $\frac{5.9}{100}$ $\frac{5.1}{129}$

$\frac{7.5}{137}$ $\frac{8.5}{100}$ $\frac{8.3}{85}$ $\frac{8.2}{58}$ $\frac{9.0}{34}$ $\frac{9.9}{15}$ 10.1 $\frac{10.3}{17}$ $\frac{9.6}{36}$ $\frac{8.6}{55}$ $\frac{7.0}{85}$ $\frac{6.1}{100}$ $\frac{5.1}{131}$

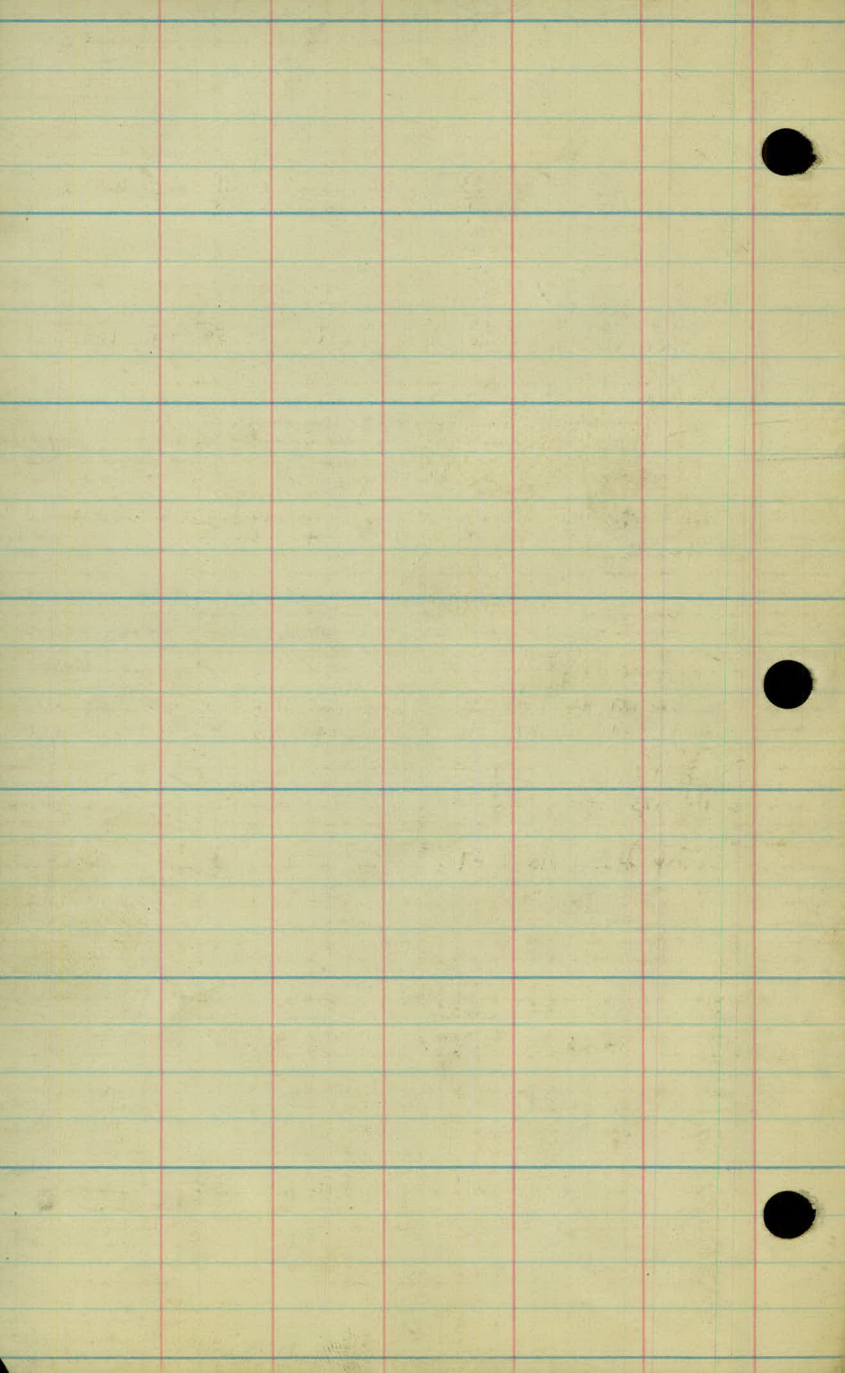
$\frac{8.7}{132}$ $\frac{9.4}{100}$ $\frac{9.6}{83}$ $\frac{9.6}{68}$ $\frac{9.8}{39}$ $\frac{10.4}{19}$ 10.8 $\frac{10.8}{14}$ $\frac{10.0}{36}$ $\frac{8.9}{54}$ $\frac{7.3}{85}$ $\frac{6.8}{100}$ $\frac{5.9}{127}$

$\frac{10.4}{110}$ $\frac{10.7}{86}$ $\frac{11.0}{54}$ $\frac{10.4}{36}$ $\frac{11.0}{29}$ $\frac{11.0}{19}$ $\frac{11.2}{5}$ 11.4 $\frac{11.0}{29}$ $\frac{10.2}{43}$ $\frac{9.4}{60}$ $\frac{8.3}{86}$ $\frac{7.5}{100}$ $\frac{7.3}{137}$

$\frac{10.3}{110}$ $\frac{9.7}{123}$ $\frac{9.2}{145}$

Top Hub Sta 8+70

Mont.



8/16/35

Portell

-X-Sections

"U" Farm Gravel Pit

•(Stripping)

Sta	+	π	-	Elev
B.M.	3.02	203.02		200.00

2+25				95.8
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2+41		00	Cut	
------	--	----	-----	--

2+50				95.3
------	--	--	--	------

+75				94.6
-----	--	--	--	------

3				94.4
---	--	--	--	------

+25				93.0
-----	--	--	--	------

0	11.47	206.83	7.66	195.36
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+50				92.6
-----	--	--	--	------

+75				95.1
-----	--	--	--	------

Top Post @ N.W. Ent to Pit

7.2

$\frac{8.1}{23}$ N.G. $\frac{7.8}{18}$ $\frac{9.5}{13}$ Top Gravel $\frac{8.4}{5}$ $\frac{8.0}{3}$ 7.1
 7.7 $\frac{7.8}{11}$ $\frac{8.0}{14}$ N.G. $\frac{5.6}{26}$ $\frac{4.6}{36}$

7.2 $\frac{7.0}{20}$ $\frac{8.9}{17}$ $\frac{9.0}{11}$ $\frac{8.6}{5}$ $\frac{8.7}{3}$ 6.1
 8.4 $\frac{8.1}{2-14}$ $\frac{8.0}{18}$ $\frac{7.4}{22}$ N.G. $\frac{5.4}{28}$ $\frac{4.8}{40}$

N.G. $\frac{5.8}{45}$ $\frac{5.7}{34}$ $\frac{9.8}{16}$ $\frac{10.1}{22}$ $\frac{10.0}{14}$ $\frac{9.7}{10}$ $\frac{8.7}{8-4}$ 5.2
 8.6 $\frac{8.2}{4}$ $\frac{7.9}{11}$ $\frac{8.2}{18}$ N.G. $\frac{4.6}{30}$ $\frac{4.2}{44}$

N.G. $\frac{3.7}{44}$ $\frac{3.9}{39}$ $\frac{10.6}{29}$ $\frac{10.4}{16}$ $\frac{8.1}{11}$ $\frac{7.5}{8}$ $\frac{9.8}{4}$ 4.2
 10.0 $\frac{9.9}{5}$ $\frac{8.0}{9-21}$ $\frac{7.7}{22}$ 60 Cut = + 22 $\frac{3.8}{27}$ $\frac{6.2}{30}$ $\frac{5.8}{33}$ $\frac{5.7}{38}$ $\frac{3.1}{42}$
 N.G. $\frac{1.9}{49}$ $\frac{2.1}{95}$

N.G. $\frac{6.3}{49}$ $\frac{6.7}{40}$ $\frac{11.7}{32}$ $\frac{11.6}{26}$ $\frac{12.0}{14}$ $\frac{11.2}{9}$ $\frac{11.4}{5}$ 7.3
 14.2 $\frac{14.3}{3}$ $\frac{12.3}{8}$ $\frac{11.9}{19}$ $\frac{8.5}{26}$ $\frac{8.2}{42}$ Top Gravel $\frac{9.1}{49}$ $\frac{4.6}{95}$
 N.G. $\frac{2.9}{49}$

Nat. Gr $\frac{5.2}{58}$ $\frac{5.8}{50}$ $\frac{5.9}{39}$ $\frac{11.1}{31-11}$ $\frac{11.3}{4}$ 6.0
 11.7 $\frac{11.4}{5}$ $\frac{10.9}{11}$ $\frac{10.5}{16}$ $\frac{7.9}{29}$ $\frac{8.7}{45}$ $\frac{8.9}{72-90}$ $\frac{4.5}{95}$
 3.5
 101

Sta	+	π	-	Elev.
		206.83		

3+87		See	Lt.	96.7
------	--	-----	-----	------

4				99.1
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+25				200.1
-----	--	--	--	-------

+50				01.6
-----	--	--	--	------

+59				02.1
-----	--	--	--	------

+68		00	Cut	
-----	--	----	-----	--

①	8.03	210.21	4.65	202.18
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BM			6.02	204.19	204.21
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00 Cut = +75

NG 4.3 7.5 1A 5.3 10.6 10.1
 4.4 114 109-58 54 38 29 4 10.1
 119

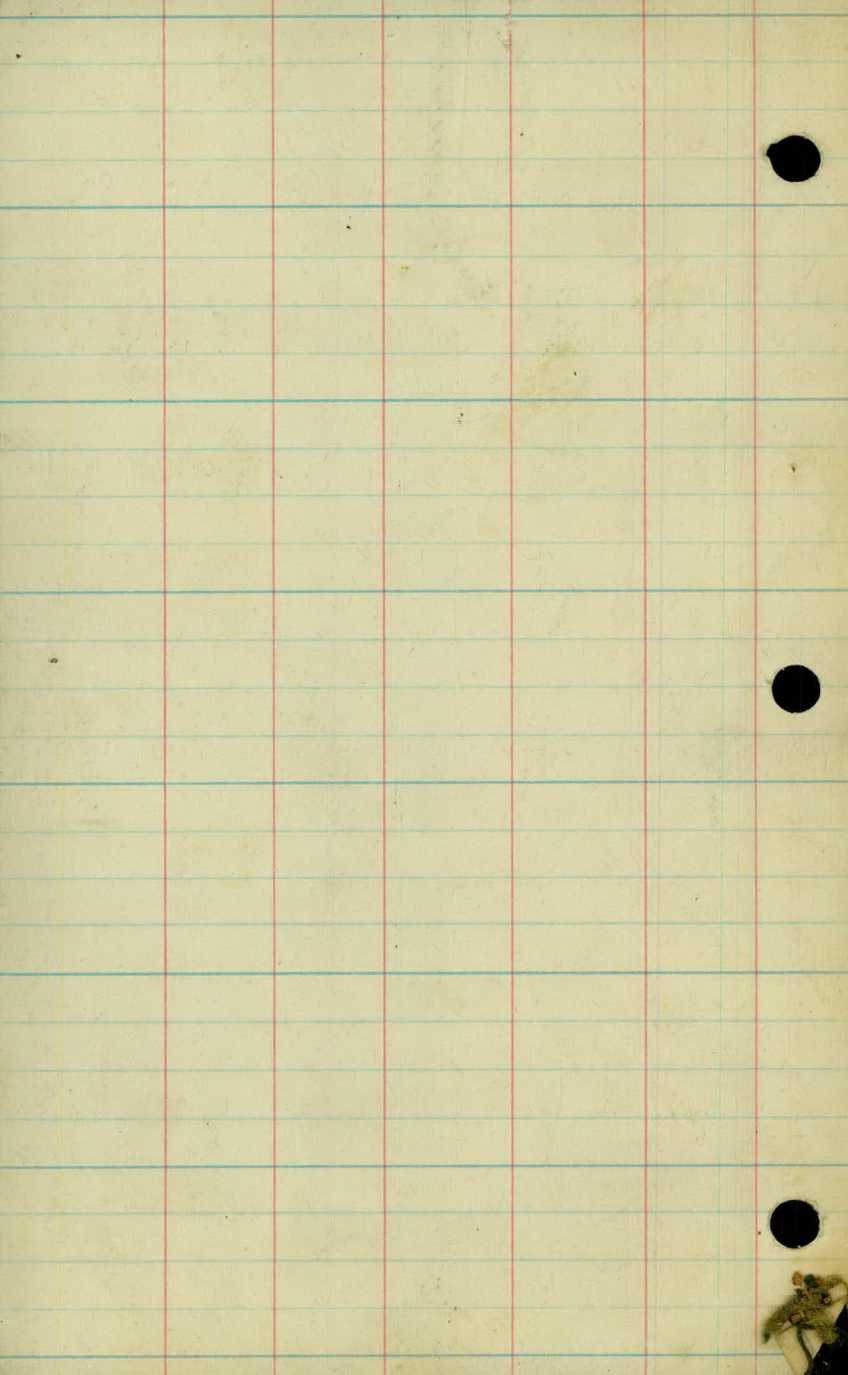
NG 4.5 4.4 7.1 Top gravel 7.0 4.1 NG 4.4 9.4 9.6 7.8 3.5 7.9 1.6 5.9 5.4 5.5 1.5 NG 1.5
 118 113 109 58 54 36 30 17 3 7.7 5 36 69 77 92 99 103

NG 3.6 3.5 6.6 6.5 6.4 2.5 3.0 6.0 6.5 3.5 6.4 5.6 5.2 1.4 NG 1.7
 119 114 109 100 54 48 33 18 6 6.7 19 61 92 99 104

3.2 5.5 5.6 5.8 5.5 5.1 5.2 0.4 5.2 4.1 4.4 2.8 4.0 6.1 5.6 NG 2.0
 119 114 108 100 85 63 40 30-9 13 22 25 70 82 92 97
 2.1 102

NG 2.9 3.0 5.5 5.3 5.4 5.0 4.4 4.7 4.0 3.1 3.6 4.7 6.2 4.9 NG 2.2 2.5
 118 113 108 100 83 56 24 14 27 59 68 78 91 97 100

Top Stake Sta. 7+00



9/23/35

Portell

X- Sections
U Farm Gravel Pit

Pla Heel 9/23/35-

Sta

+

X

-

BM.

3.48

203.48 ✓

200.00 ✓

2+00

97.0 ✓

+25

95.8 ✓

+50

95.0 ✓

+75

93.9 ✓

3

92.4 ✓

+25

91.4 ✓

①

10.90

202.26 ✓

12.12

91.36 ✓

Top fee post @ NW. Cor. of Pit.

6.5

$\frac{6.9}{25}$ $\frac{7.9}{15}$ 7.7 $\frac{6.8}{13}$ $\frac{5.5}{30}$

$\frac{8.3}{27}$ $\frac{8.0}{17}$ $\frac{9.0}{14}$ $\frac{7.6}{8.5}$ $\frac{8.3}{16}$ $\frac{6.1}{26}$ $\frac{5.2}{36}$

$\frac{7.5}{35}$ $\frac{7.4}{24}$ $\frac{9.4}{16}$ $\frac{6.6}{9.6}$ $\frac{8.4}{6}$ $\frac{8.6}{18}$ $\frac{5.6}{28}$ $\frac{5.2}{40}$

45. $\frac{6.3}{34}$ $\frac{11.2}{23}$ $\frac{5.7}{11.1}$ $\frac{8.4}{8-19}$ $\frac{5.0}{29}$ $\frac{4.7}{43}$

$\frac{3.3}{54}$ $\frac{4.3}{38}$ $\frac{12.0}{26}$ $\frac{4.7}{12.1}$ $\frac{8.7}{6}$ $\frac{8.5}{26}$ $\frac{4.8}{27}$ $\frac{3.1}{53-59}$ $\frac{7.2}{67}$ $\frac{7.0}{77}$ $\frac{1.8}{84}$
 $\frac{2.4}{100}$ 88

Sta

+

π

-

202.26 ✓

3+50

92.2 ✓

~~+63~~

95.1 ✓

+75

94.4 ✓

4

89.1 ✓

+25

200.5 ✓

0

7.71

207.47 ✓

2.50

199.76 ✓

~~+39~~

200.9 ✓

+50

201.6 ✓

$$\begin{array}{r} 1.8 \\ 50 \end{array} \begin{array}{r} 2.3 \\ 40 \end{array} \begin{array}{r} 7.0 \\ 38 \end{array} \begin{array}{r} 8.6 \\ 30 \end{array} \begin{array}{r} 10.6 \\ 28 \end{array} \begin{array}{r} 10.9 \\ 15 \end{array} \begin{array}{r} 2.8 \\ 19.1 \end{array} \begin{array}{r} 7.8 \\ 8 \end{array} \begin{array}{r} 6.1 \\ 21 \end{array} \begin{array}{r} 13.0 \\ 36 \end{array} \begin{array}{r} 12.1 \\ 60 \end{array} \begin{array}{r} 10.8 \\ 78 \end{array} \begin{array}{r} 0.0 \\ 96 \end{array}$$

$$\begin{array}{r} 0.8 \\ 59 \end{array} \begin{array}{r} 1.8 \\ 32 \end{array} \begin{array}{r} 6.7 \\ 32 \end{array} \begin{array}{r} 7.0 \\ 16 \end{array} \begin{array}{r} 8.0 \\ 13 \end{array} 7.2 \begin{array}{r} 5.7 \\ 23 \end{array} \begin{array}{r} 13.3 \\ 50 \end{array} \begin{array}{r} 12.5 \\ 80 \end{array} \begin{array}{r} 5.6 \\ 91 \end{array} \times$$

$$\begin{array}{r} 0.3 \\ 70 \end{array} \begin{array}{r} 1.1 \\ 48 \end{array} \begin{array}{r} 6.8 \\ 39 \end{array} \begin{array}{r} 6.6 \\ 15 \end{array} 7.9 \begin{array}{r} 7.8 \\ 6 \end{array} \begin{array}{r} 11.9 \\ 38 \end{array} \begin{array}{r} 13.1 \\ 57 \end{array} \begin{array}{r} 12.4 \\ 80 \end{array} \times$$

$$\begin{array}{r} 0.3 \\ 111 \end{array} \begin{array}{r} 3.2 \\ 106 \end{array} \begin{array}{r} 2.7 \\ 61 \end{array} \begin{array}{r} 5.7 \\ 48 \end{array} \begin{array}{r} 4.5 \\ 12 \end{array} 13.2 \begin{array}{r} 13.6 \\ 58 \end{array} \begin{array}{r} 16.3 \\ 67 \end{array} \times$$

$$\begin{array}{r} 10.6 \\ 109 \end{array} \begin{array}{r} 2.1 \\ 106 \end{array} \begin{array}{r} 1.9 \\ 71 \end{array} \begin{array}{r} 3.4 \\ 44 \end{array} 1.8 \begin{array}{r} 1.9 \\ 8 \end{array} \begin{array}{r} 11.2 \\ 25 \end{array} \begin{array}{r} 7.2 \\ 55 \end{array} \begin{array}{r} 4.4 \\ 74 \end{array} \begin{array}{r} 1.1 \\ 75 \end{array} \times$$

$$\begin{array}{r} 4.2 \\ 116 \end{array} \begin{array}{r} 4.1 \\ 112 \end{array} \begin{array}{r} 7.2 \\ 107 \end{array} \begin{array}{r} 7.0 \\ 79 \end{array} \begin{array}{r} 8.1 \\ 46 \end{array} 6.6 \begin{array}{r} 6.3 \\ 24 \end{array} \begin{array}{r} 5.9 \\ 67 \end{array} \begin{array}{r} 6.3 \\ 91 \end{array} \begin{array}{r} 1.9 \\ 97 \end{array} \begin{array}{r} 2.2 \\ 100 \end{array}$$

$$\begin{array}{r} 3.9 \\ 115 \end{array} \begin{array}{r} 3.8 \\ 111 \end{array} \begin{array}{r} 6.5 \\ 105 \end{array} \begin{array}{r} 5.7 \\ 70 \end{array} \begin{array}{r} 6.7 \\ 33 \end{array} 5.9 \begin{array}{r} 4.8 \\ 22 \end{array} \begin{array}{r} 5.0 \\ 73 \end{array} \begin{array}{r} 6.7 \\ 81 \end{array} \begin{array}{r} 6.2 \\ 92 \end{array} \begin{array}{r} 2.3 \\ 96 \end{array} \begin{array}{r} 2.6 \\ 100 \end{array}$$

Sta + π -

207.47

4+59

02.5 ✓

+68

00 Cut

207.47

4+25

200.5
Section Extensions Rth

~~3+65~~

95.1

3+75

94.4

4

89.1

+25

200.5

⊙

934

210.82 ✓

599

201.48 ✓

6.63

204.19 ✓

204.21 ✓

$$\begin{array}{cccccccccccc} 3.6 & 3.7 & 6.0 & 6.0 & 6.5 & 6.1 & & & & & & \\ \hline 114 & 110 & 105 & 87 & 49 & 15 & 5.0 & 4.7 & 3.5 & 4.0 & 6.6 & 5.8 & 2.6 \\ & & & & & & & \hline & & & & & & & 14 & 45 & 65 & 76 & 91 & 96 \\ & & & & & & & & & & & & \hline & & & & & & & & & & & & 2.8 \\ & & & & & & & & & & & & \hline & & & & & & & & & & & & 100 \end{array}$$

(-4.2)

$$\begin{array}{ccc} 5.7 & 1.4 & 2.1 \\ \hline 92 & 98 & 100 \end{array}$$

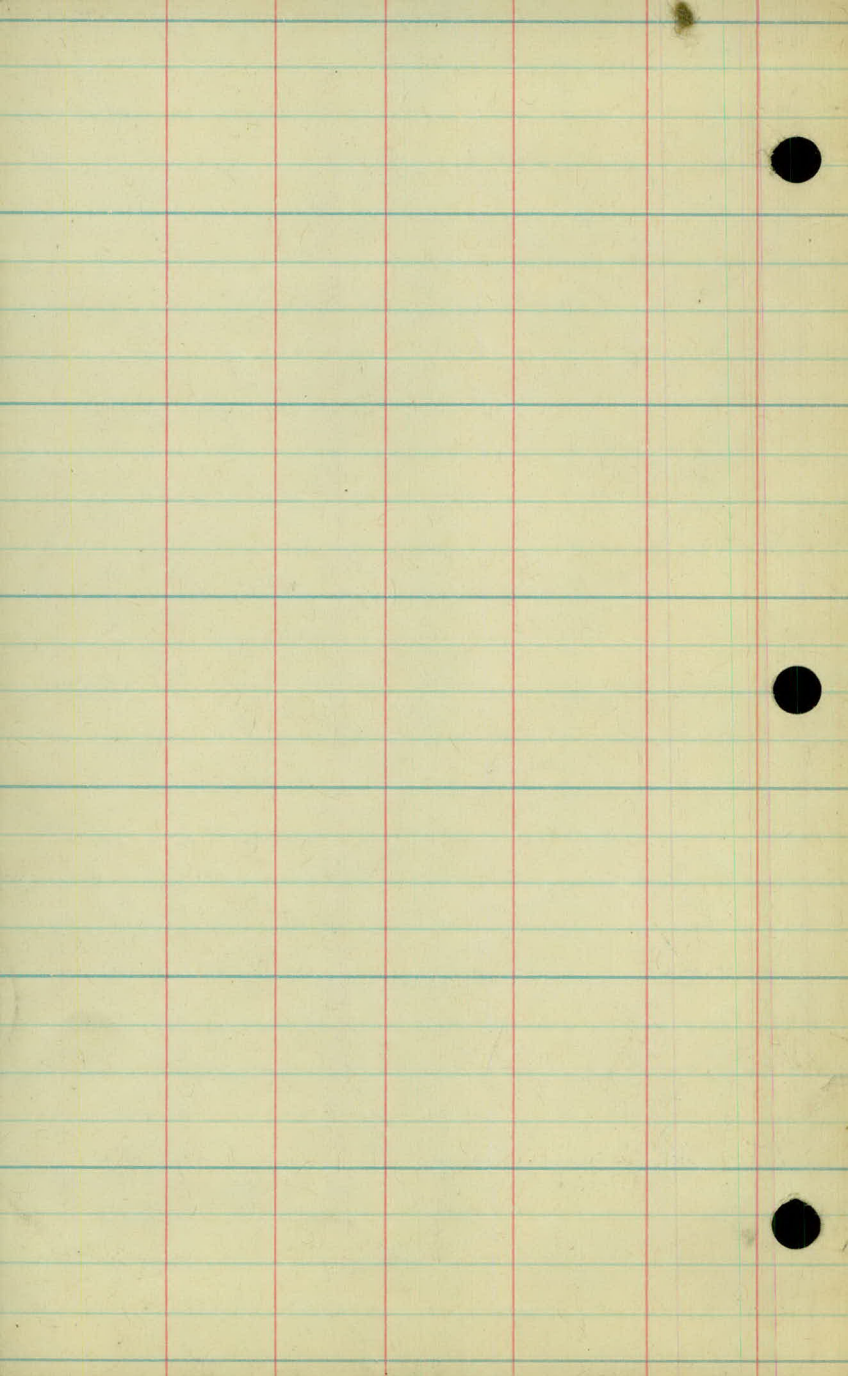
$$\begin{array}{cc} 3.0 & 3.3 \\ \hline 100 & 102 \end{array}$$

$$\begin{array}{ccc} (6.7) & 3.5 & 2.5 & 2.7 \\ \hline & 95 & 99 & 100 \end{array}$$

$$\begin{array}{ccc} (4.2) & 6.7 & 2.2 \\ \hline & 88 & 98-101 \end{array}$$

$$\begin{array}{ccc} 5.7 & 1.4 & 2.1 \\ \hline 92 & 98 & 100 \end{array}$$

Top Stk Sta 7+00



1-3
11/25/35

Portell

X-Sections
"U" Farm Gravel Pit

Platt
Jan. 21, 1936
m.l.

Sta + π -

BM 10.26 210.26 200.00

4+50 01.6

+75 02.9

+97 04.1

5 05.8

+10 05.8

+16

+25

74

Top Post @ NW Ent to Rt.

$$120 - \frac{6.1}{114} \frac{7.9}{108} \frac{9.8}{100} \frac{10.1}{64} \frac{9.6}{25} 8.6 \frac{7.6}{27-58} \frac{8.7}{92} \frac{5.2}{97-100}$$

$$\frac{6.6}{122} \frac{6.7}{115} \frac{8.8}{109} \frac{8.0}{75} \frac{10.4}{67} \frac{7.8}{14} 7.3 \frac{6.5}{14} \frac{7.1}{44} \frac{10.2}{91} \frac{6.6}{97} \frac{6.5}{100}$$

$$\frac{6.5}{121} \frac{8.1}{115} \frac{6.4}{38} \frac{7.6}{36} 6.2 \frac{7.9}{34} \frac{9.3}{69} \frac{10.0}{93} \frac{6.8}{96} \frac{7.4}{100}$$

$$\frac{8.2}{121} \frac{7.7}{93} \frac{7.6}{70} \frac{5.4}{41} 2.6 \frac{6.6}{62} \frac{10.6}{91} \frac{7.7}{95} \frac{7.8}{100}$$

$$\frac{6.3}{135} \frac{7.2}{133} \frac{4.9}{120} \frac{3.4}{98} \frac{3.0}{80} \frac{6.4}{67} \frac{4.6}{37} 4.5 \frac{5.2}{27} \frac{7.0}{64} \frac{8.3}{69} \frac{9.4}{82} \frac{10.1}{92} \frac{7.6}{96} \frac{8.5}{100}$$

$$\frac{6.1}{140} \frac{7.5}{136} \frac{4.8}{119} \frac{3.3}{100} \frac{2.7}{78} \frac{2.3}{30} 2.4 \frac{3.4}{26} \frac{6.0}{34} \frac{7.0}{65} \frac{9.3}{81} \frac{9.2}{111} \frac{7.6}{90}$$

$$\frac{8.2}{100}$$

Same as Orig Sec Lt.

$$2.6 \frac{3.4}{25} \frac{5.7}{31} \frac{7.4}{66} \frac{8.9}{70} \frac{9.7}{82} \frac{11.2}{91} \frac{8.2}{97} \frac{8.1}{100}$$

Sta

+

π

-

210.26

5+48

5+60

00 Stripping

603

20423

20421

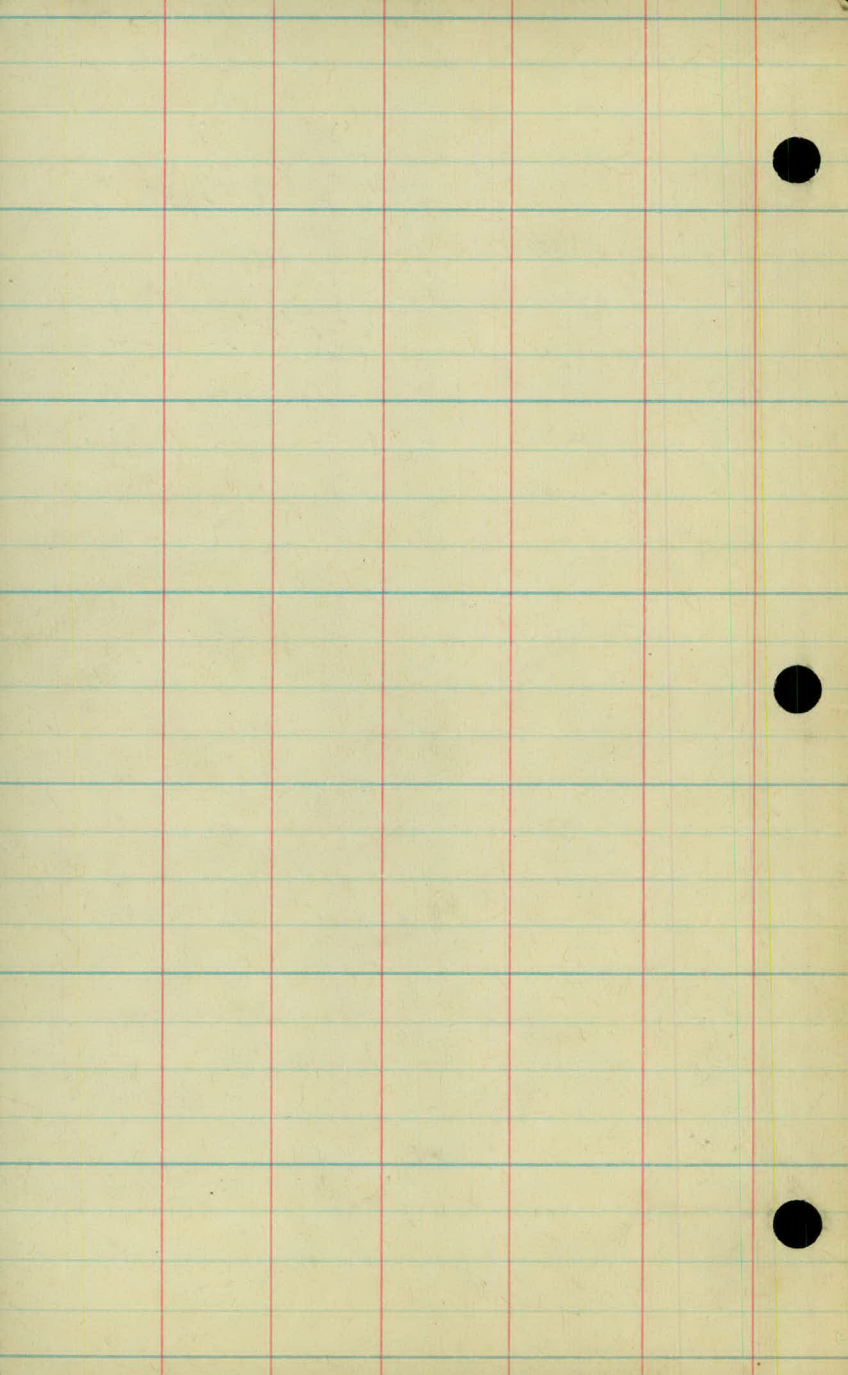
Same as Orig Sec Lt.

$$\begin{array}{r}
 2.4 \\
 2.4 \quad \frac{3.7}{22} \quad \frac{5.1}{25} \quad \frac{8.4}{64} \quad \frac{9.8}{68} \quad \frac{11.4}{90} \quad \frac{9.1}{94} \\
 \hline
 9.5 \\
 100
 \end{array}$$

Same as Orig Sec Lt.

$$\begin{array}{r}
 2.6 \quad \frac{4.5}{29} \quad \frac{7.6}{68} \quad \frac{9.5}{94} \\
 \hline
 \end{array}$$

Top Stake Sta 7+00



1-4

1/14/36

Portell

X-Sections

U Farm Gravel Pit

Sta	+	π	-
-----	---	---	---

B.M.	9.04	209.04	200.00
------	------	--------	--------

3+00

3+25

+50

0	9.09	209.09	9.04	200.00
---	------	--------	------	--------

+75

4

+75

+50

+75

Top Post @ N.W. Ent to P.t

00
Section on Rt.

$$\frac{5.6}{100} \quad \frac{9.6}{36}$$

$$\frac{10.2}{10.2}$$

$$\frac{10.1}{29}$$

$$\frac{8.0}{60.67-75}$$

$$\frac{12.1}{75}$$

$$\frac{1.6}{81}$$

$$\frac{7.3}{82}$$

$$\frac{7.7}{110}$$

$$\frac{5.6}{100} \quad \frac{8.5}{37}$$

$$9.5$$

$$\frac{7.3}{93} \quad \frac{5.3}{97}$$

$$\frac{6.1}{100} \quad \frac{7.6}{49}$$

$$8.3$$

$$\frac{4.3}{77} \quad \frac{4.0}{100}$$

$$\frac{9.1}{100} \quad \frac{8.8}{87} \quad \frac{10.3}{51}$$

$$5.8$$

$$\frac{8.8}{98} \quad \frac{3.2}{100} \quad \frac{3.9}{110}$$

$$\frac{8.8}{100} \quad \frac{8.0}{73} \quad \frac{10.2}{42}$$

$$5.8$$

$$\frac{3.1}{100} \quad \frac{3.8}{110}$$

$$\frac{7.6}{100} \quad \frac{8.6}{43}$$

$$2.7$$

$$\frac{4.2}{96} \quad \frac{4.1}{100} \quad \frac{5.0}{110}$$

$$\frac{6.6}{100} \quad \frac{6.5}{80} \quad \frac{7.9}{69} \quad \frac{7.8}{49}$$

$$2.7$$

$$\frac{8.3}{87} \quad \frac{5.8}{91} \quad \frac{5.5}{95} \quad \frac{5.6}{100} \quad \frac{5.6}{110}$$

Sta

+

π

-

209.09

5

+25

Q

105

117.36

12.78

196.31

3+25

3+50

3+75

4

+25

+50

+75

$$\begin{array}{r} 3.1 \\ 100 \end{array} \quad \begin{array}{r} 2.6 \\ 91 \end{array} \quad \begin{array}{r} 2.0 \\ 78 \end{array} \quad \begin{array}{r} 5.7 \\ 66 \end{array} \quad \begin{array}{r} 6.2 \\ 43-34 \end{array}$$

1.4

(Top Grave)

$$\begin{array}{r} 8.7 \\ 70-87 \end{array} \quad \begin{array}{r} 7.6 \\ 93 \end{array} \quad \begin{array}{r} 6.6 \\ 95 \end{array} \quad \begin{array}{r} 7.3 \\ 100 \end{array} \quad \begin{array}{r} 7.3 \\ 110 \end{array}$$

00 Section 44

1.3

$$\begin{array}{r} N6.7 \\ 1.3 \\ 6 \end{array}$$

N6.7

$$\begin{array}{r} 1.6 \\ 11 \end{array} \quad \begin{array}{r} 5.5 \\ 19 \end{array} \quad \begin{array}{r} 9.6 \\ 88 \end{array} \quad \begin{array}{r} 7.6 \\ 93 \end{array} \quad \begin{array}{r} 8.0 \\ 100 \end{array} \quad \begin{array}{r} 8.6 \\ 110 \end{array}$$

$$\begin{array}{r} 5.1 \\ 27 \end{array} \quad \begin{array}{r} 5.8 \\ 1 \end{array} \quad \begin{array}{r} +1.4 \\ 5.6 \\ 6 \end{array} \quad \begin{array}{r} 2.2 \\ 6 \end{array}$$

$$\begin{array}{r} 6.1 \\ 27 \end{array} \quad \begin{array}{r} 7.3 \\ 1 \end{array} \quad \begin{array}{r} +2.1 \\ 7.0 \\ 6 \end{array} \quad \begin{array}{r} 3.3 \\ 24 \end{array} \quad \begin{array}{r} 2.2 \\ 24 \end{array} \quad \begin{array}{r} 6.2 \\ 33 \end{array} \quad \begin{array}{r} 5.2 \\ 77 \end{array}$$

$$\begin{array}{r} 8.7 \\ 29 \end{array} \quad \begin{array}{r} 8.9 \\ 7 \end{array} \quad \begin{array}{r} +3.4 \\ 8.0 \\ 14 \end{array} \quad \begin{array}{r} 5.7 \\ 14 \end{array}$$

$$\begin{array}{r} 9.9 \\ 41 \end{array} \quad \begin{array}{r} 9.0 \\ 29 \end{array} \quad \begin{array}{r} 9.7 \\ 5 \end{array} \quad \begin{array}{r} +5.9 \\ 8.4 \\ 7 \end{array} \quad \begin{array}{r} 6.3 \\ 7 \end{array}$$

$$\begin{array}{r} 8.8 \\ 30 \end{array} \quad \begin{array}{r} 8.9 \\ 20 \end{array} \quad \begin{array}{r} 8.4 \\ 3 \end{array} \quad \begin{array}{r} +5.9 \\ 7.3 \\ 3 \end{array} \quad \begin{array}{r} 6.6 \\ 3 \end{array}$$

$$\begin{array}{r} 12.0 \\ 35-25 \end{array} \quad \begin{array}{r} +9.0 \\ 11.9 \\ 7 \end{array} \quad \begin{array}{r} 10.6 \\ 7 \end{array}$$

$$\begin{array}{r} 6.3 \\ 44 \end{array} \quad \begin{array}{r} 10.8 \\ 36 \end{array} \quad \begin{array}{r} 11.6 \\ 3 \end{array} \quad \begin{array}{r} +9.4 \\ 10.7 \\ 8 \end{array} \quad \begin{array}{r} 10.9 \\ 8 \end{array}$$

Sta

+

X

-

19736

5

0

9.17

200.22

6.31

191.05

3+75

4

+25

+50

+75

5+00

BM

0.21

200.01

200.00

$$\begin{array}{r} 1.2 \\ 33. \end{array} \quad \begin{array}{r} 8.6 \\ 11. \end{array} \times 10.3 \quad \begin{array}{r} 8.9 \\ 10. \end{array}$$

$$+0.6 \quad \begin{array}{r} 9.5 \\ 29 \end{array} \quad \begin{array}{r} 11.6 \\ 46 \end{array} \quad \begin{array}{r} 11.0 \\ 71-79 \end{array}$$

$$+3.1 \quad \begin{array}{r} 9.0 \\ 22 \end{array} \quad \begin{array}{r} 10.0 \\ 26 \end{array} \quad \begin{array}{r} 12.8 \\ 27-40 \end{array} \quad \begin{array}{r} 7.3 \\ 49 \end{array} \quad \begin{array}{r} 12.8 \\ 58 \end{array} \quad \begin{array}{r} 13.2 \\ 75 \end{array}$$

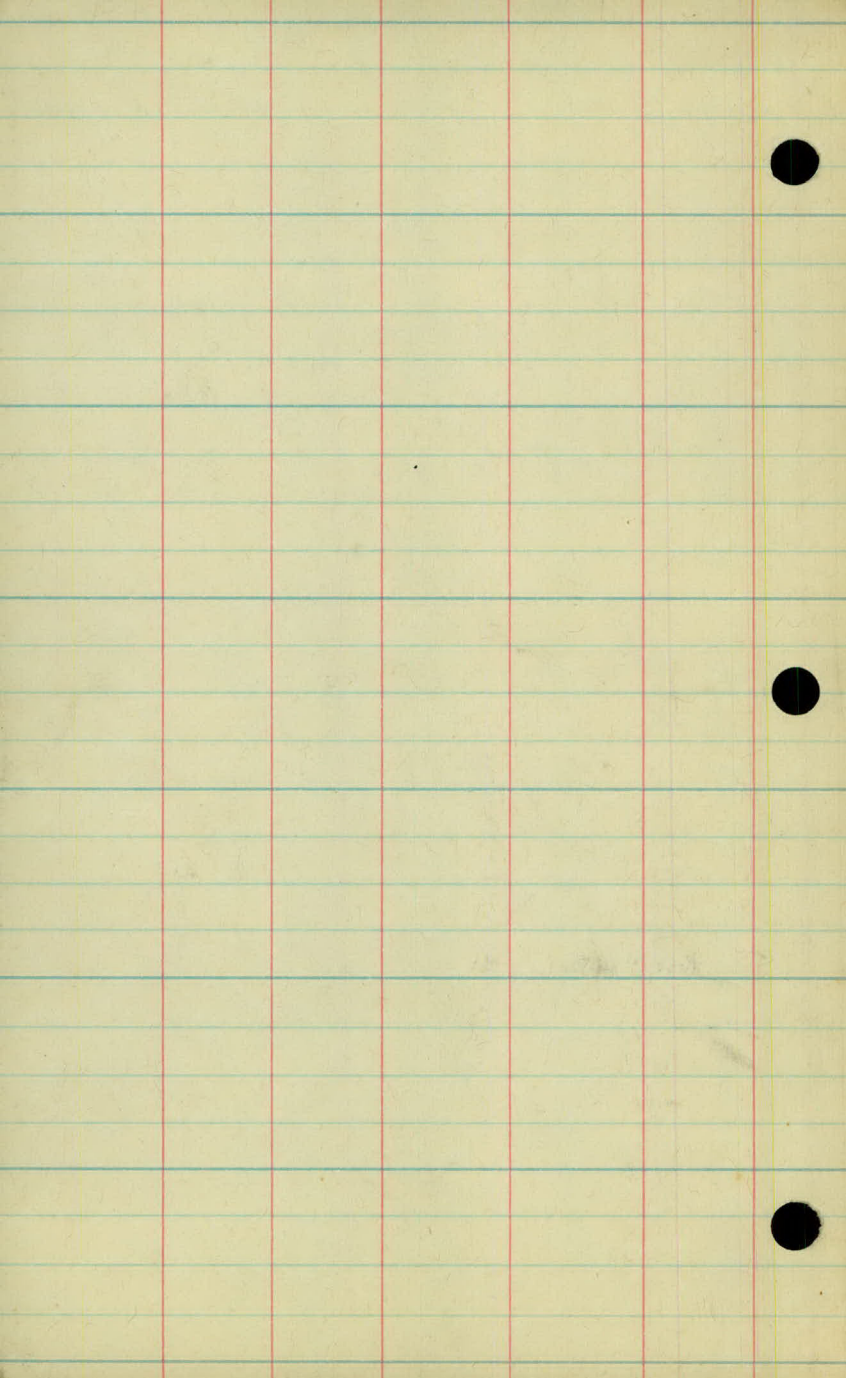
$$+3.1 \quad \begin{array}{r} 8.2 \\ 21 \end{array} \quad \begin{array}{r} 13.5 \\ 23 \end{array} \quad \begin{array}{r} 13.8 \\ 45 \end{array} \quad \begin{array}{r} 5.5 \\ 51 \end{array} \quad \begin{array}{r} 13.0 \\ 63 \end{array} \quad \begin{array}{r} 12.7 \\ 79 \end{array}$$

$$+6.2 \quad \begin{array}{r} 13.7 \\ 19 \end{array} \quad \begin{array}{r} 13.6 \\ 69 \end{array}$$

$$+6.6 \quad \begin{array}{r} 13.5 \\ 22 \end{array} \quad \begin{array}{r} 13.4 \\ 45 \end{array} \quad \begin{array}{r} 12.8 \\ 62 \end{array} \quad \begin{array}{r} 12.0 \\ 75 \end{array}$$

$$+7.5 \quad \begin{array}{r} 12.8 \\ 18 \end{array} \quad \begin{array}{r} 10.9 \\ 30 \end{array} \quad \begin{array}{r} 4.5 \\ 65 \end{array}$$

Top Post NW Ent to Pit



Mar 18, 1936

H.T. Purte II

U Farm Gravel Pit

X-Sections

Platt
March 19, 1936

Sta	+	π	-
BM.	3.06	203.06 ✓	200.00

		2.91	200.15 ✓
○	2.82	192.88 ✓	190.06 ✓

4+00			89.6
------	--	--	------

+25			89.9
-----	--	--	------

4+50			87.6
------	--	--	------

+75			86.3
-----	--	--	------

5+00			85.6
------	--	--	------

+25			86.5
-----	--	--	------

Top post NW Ent. to Pit

Cor. office Steps

$\times 10.4$

$\frac{4.5}{44}$	$\frac{5.5}{36}$	$\frac{5.0}{5}$	$\frac{3.3}{33}$	$\frac{1.8}{6}$	$\frac{1.9}{23}$	$\frac{5.4}{29}$	$\frac{6.0}{73}$
------------------	------------------	-----------------	------------------	-----------------	------------------	------------------	------------------

$\times 10.4$

$\frac{5.2}{59}$	$\frac{6.6}{38}$	$\frac{6.0}{9}$	$\frac{3.0}{30}$	$\frac{1.3}{21}$	$\frac{6.2}{26}$	$\frac{5.8}{74}$
------------------	------------------	-----------------	------------------	------------------	------------------	------------------

$\times 13.5$

$\frac{4.4}{68}$	$\frac{8.2}{57-12}$	$\frac{6.6}{10}$	$\frac{5.3}{53}$	$\frac{5.6}{6}$	$\frac{7.0}{20}$	$\frac{6.2}{73}$
------------------	---------------------	------------------	------------------	-----------------	------------------	------------------

$\times 13.9$

$\frac{6.8}{70}$	$\frac{8.8}{60}$	$\frac{8.6}{24}$	$\frac{6.2}{16}$	$\frac{6.6}{66}$	$\frac{6.4}{67}$
------------------	------------------	------------------	------------------	------------------	------------------

$\times 14.8$

$\frac{2.4}{47}$	$\frac{37}{18}$	$\frac{7.3}{73}$	$\frac{6.3}{15}$	$\frac{6.5}{63}$
------------------	-----------------	------------------	------------------	------------------

$\times 14.9$

$\frac{6.4}{64}$	$\frac{6.7}{41}$
------------------	------------------

Sta

+

π

✓

-

192.85

✓

9.61

209.76

200.15

4+00

4 +25

4 +50

4 +75

5 +00

5 +25

+50

= 00 cut

B.M.

9.75

200.01 ✓

200.00

Cor. Office Steps

$$\frac{9.5}{77} \quad \frac{11.1}{57}$$

$$\frac{4.4}{99}$$

$$\frac{9.0}{80} \quad \frac{8.8}{78}$$

$$\frac{6.5}{78}$$

$$\frac{4.2}{99}$$

$$88 - \frac{8.2}{78}$$

$$3.4$$

$$\frac{4.7}{95}$$

$$\frac{7.1}{79} \quad \frac{8.6}{78}$$

$$3.0$$

$$\frac{7.2}{85}$$

$$\frac{6.0}{76}$$

$$\frac{3.2}{89} \quad \frac{2.6}{78} \quad \frac{6.8}{65} \quad \frac{7.0}{54}$$

$$2.1$$

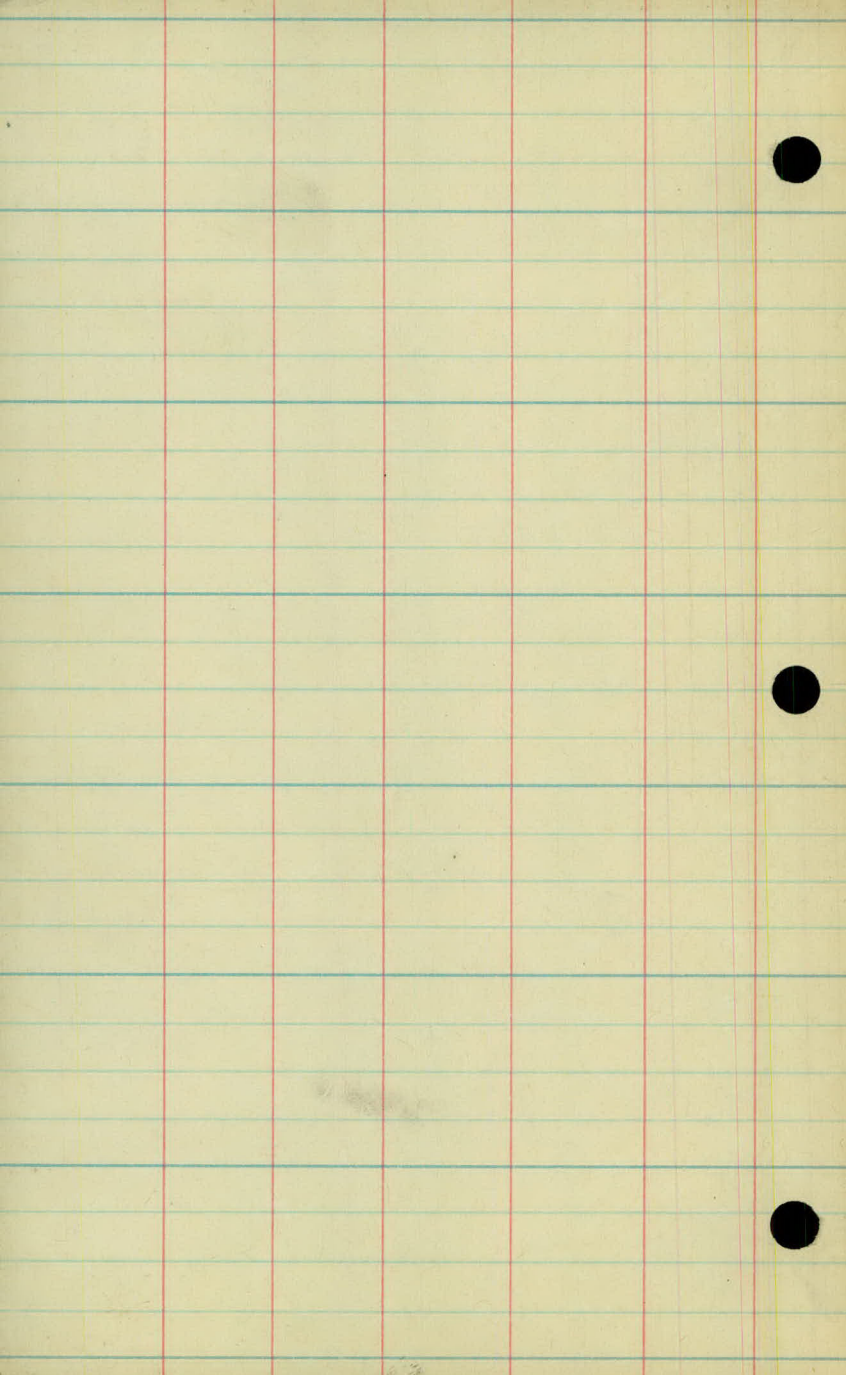
$$\frac{8.7}{80} \quad \frac{7.3}{95}$$

$$\frac{1.5}{59} \quad \frac{1.6}{26}$$

$$2.10$$

$$\frac{8.6}{72} \quad \frac{8.3}{94}$$

Top Post NW End to Pit



1-4
5/12/36
Portall

X- Sections

U Farm Gravel Pit

Sta	+	∞	-
BM	9.49	209.49 ✓	200.00

0		13.13	196.36 ✓
---	--	-------	----------

BM		2.30	207.19 ✓
----	--	------	----------

4+25

4+50

4+75

4+85

5

5+25

5+50

5+75

4+25

Top Post @ NW Ent. to Rt

Top rock on walk to office

Set on NW Cor Top Conc. water Trough

6.2

$\frac{4.1}{102}$ $\frac{4.3}{110}$

3.1

$\frac{4.3}{99}$ $\frac{5.4}{110}$

2.7

$\frac{5.6}{98}$ $\frac{6.1}{110}$

$\frac{6.4}{115}$ $\frac{6.6}{110}$

Topward
 $\frac{2.5}{84}$ $\frac{7.1}{92}$ $\frac{5.8}{77}$ $\frac{6.9}{110}$

$\frac{7.6}{115-109}$

1.8

$\frac{7.6}{82}$ $\frac{9.4}{91}$ $\frac{6.7}{96}$ $\frac{7.9}{110}$

$\frac{5.6}{115}$ $\frac{5.4}{107}$

1.5

Top
 $\frac{8.5}{76}$ $\frac{10.4}{90}$ $\frac{7.6}{95}$ $\frac{9.2}{110}$

$\frac{3.3}{115}$ $\frac{2.6}{86}$

1.5

$\frac{7.9}{60}$ $\frac{12.3}{75}$ $\frac{12.6}{86}$ $\frac{8.9}{94}$ $\frac{10.1}{110}$

$\frac{1.0}{115}$ $\frac{2.7}{109}$ $\frac{3.4}{89}$ $\frac{1.3}{67}$

1.9

$\frac{6.2}{28}$ $\frac{7.1}{63}$ $\frac{12.0}{95}$ $\frac{7.6}{100}$ $\frac{10.3}{110}$

Top
 $\frac{6.2}{115}$ $\frac{6.3}{113}$ $\frac{9.2}{109}$ $\frac{8.6}{83}$

6.2

Sta + π -
269.49

4+50

4+75

5+80

6

6+25

6+50

6+67

6+75

End Stripping

0

0.05

196.41

18.13

196.36

4+25

4+50

4+75

$$\frac{5.8}{115-113} \quad \frac{T.G.2}{84.2} \quad 107-102$$

(3.1)

$$\frac{5.7}{119} \quad \frac{6.0}{110}$$

(2.7)

$$\frac{0.9}{115} \quad \frac{1.4}{93} \quad \frac{3.5}{88} \quad \frac{1.8}{52} \quad \frac{3.0}{27} \quad 4.2 \quad \frac{7.0}{57} \quad \frac{11.9}{94} \quad \frac{9.1}{101} \quad \frac{10.5}{110}$$

$$\frac{0.4}{82} \quad \frac{0.2}{68} \quad \frac{2.0}{61} \quad \frac{2.7}{43} \quad \frac{4.2}{25} \quad T.G. (2.3) \quad 4.9 \quad \frac{6.6}{16} \quad \frac{8.1}{58} \quad \frac{11.2}{97} \quad \frac{10.4}{106} \quad \frac{11.0}{110}$$

$$\frac{0.8}{70} \quad \frac{1.3}{53} \quad \frac{4.2}{45} \quad T.G. (3.5) \quad 5.7 \quad \frac{7.7}{42} \quad \frac{11.5}{100} \quad \frac{10.3}{105} \quad \frac{11.3}{110}$$

$$\frac{2.5}{57} \quad \frac{1.8}{47} \quad \frac{5.3}{39} \quad T.G. (4.8) \quad 7.4 \quad \frac{8.6}{32} \quad \frac{10.1}{66} \quad \frac{8.5}{73} \quad \frac{9.8}{91}$$

$$\frac{2.7}{68} \quad \frac{3.7}{44} \quad \frac{6.1}{36} \quad \frac{7.7}{17} \quad 8.2 \quad \frac{9.5}{31} \quad \frac{7.9}{42} \quad \frac{9.1}{64}$$

$$\frac{9.2}{58} \quad \frac{11.5}{50} \quad \frac{10.6}{39} \quad \frac{9.8}{8} \quad \frac{7.8}{5} \quad T.G. (16.9) \quad 6.6 \quad \frac{5.7}{20} \quad \frac{10.2}{26} \quad \frac{9.4}{75}$$

$$\frac{12.1}{66-56} \quad \frac{11.7}{13} \quad \frac{9.5}{7} \quad T.G. (10.0) \quad 9.1 \quad \frac{9.2}{17} \quad \frac{10.4}{23} \quad \frac{10.2}{72}$$

$$\frac{13.4}{87} \quad \frac{13.2}{64} \quad \frac{12.3}{58} \quad \frac{11.9}{23} \quad \frac{10.0}{19} \quad T.G. (10.4) \quad 10.3 \quad \frac{9.7}{35} \quad \frac{9.4}{67}$$

Sta + π ✓ -
196.41

4+85

5

5+25

5+50

0

7.50 203.86 ✓ 0.05 196.36 ✓

B.M.

3.86 200.00 ✓ 200.00

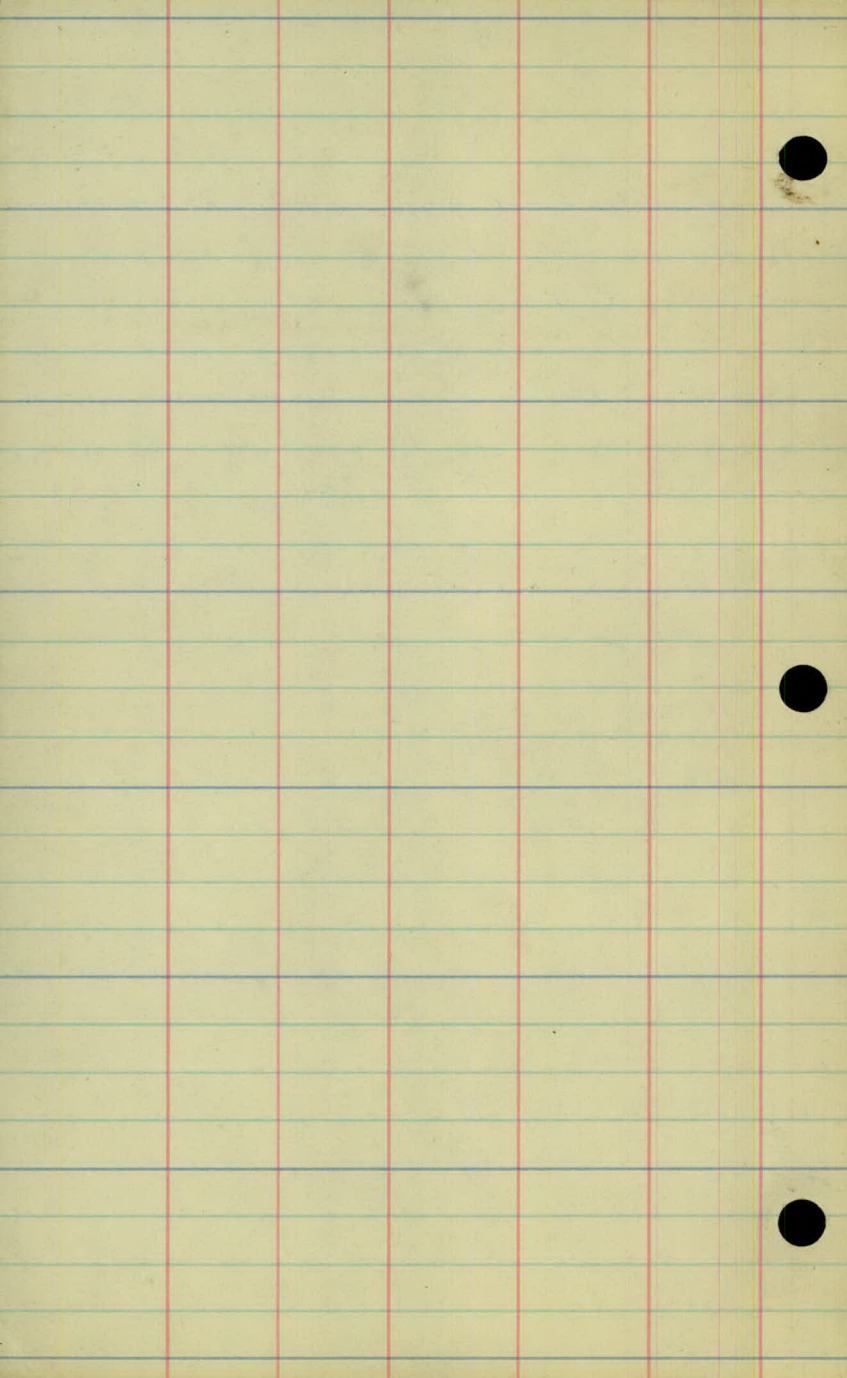
$$\begin{array}{r} 13.3 \quad 12.5 \quad 12.2 \quad 10.0 \quad 9.9 \quad 9.2 \quad 9.8 \quad 9.6 \\ \hline 90 \quad 58 \quad 24 \quad 21 \quad 10 \quad 38 \quad 65 \end{array}$$

$$\begin{array}{r} 13.1 \quad 12.9 \quad 12.5 \quad 10.7 \quad 10.2 \quad 9.9 \quad 9.5 \\ \hline 94 \quad 65 \quad 29 \quad 26 \quad 32 \quad 60 \end{array}$$

$$\begin{array}{r} 13.3 \quad 13.0 \quad 12.9 \quad 10.5 \quad 10.4 \quad 10.0 \quad 9.1 \quad 9.8 \\ \hline 86 \quad 64 \quad 34 \quad 32 \quad 12 \quad 11 \quad 52 \end{array}$$

$$\begin{array}{r} 10.6 \quad 10.0 \quad 10.2 \\ \hline 40 \quad 24 \end{array}$$

Top Post @ NW Ent. to Pt



7/29/36

Portell

X-Sections

U Farm Gravel Pit

Platted Aug 4, 1936
A.P.C.

Sta + π -

B.M. 1.80 208.99 ✓ 207.19

5

+25

+50

+75

6

+25

+50

+75

7

7	+25				01.6
7 +	30 = 00				
0	0.37	197.43	11.93	197.06	
0	4.87	191.36	10.94	186.49	

NW. Cor Top Conc Water Trough

$$\begin{array}{r} 5.1 \\ 140 \end{array} \quad \begin{array}{r} 6.9 \\ 135 \end{array} \quad \begin{array}{r} 7.1 \\ 110 \end{array}$$

(1.3) -

$$\begin{array}{r} T6 \\ 8.0 \\ 83 \end{array} \quad \begin{array}{r} T6 \\ 8.8 \\ 92 \end{array} \quad \begin{array}{r} 5.9 \\ 97 \end{array} \quad \begin{array}{r} 7.0 \\ 105 \end{array} \quad \begin{array}{r} 7.4 \\ 110 \end{array}$$

$$\begin{array}{r} 4.5 \\ 140 \end{array} \quad \begin{array}{r} 4.7 \\ 124 \end{array}$$

(1.2) -

$$\begin{array}{r} T6 \\ 8.2 \\ 76 \end{array} \quad \begin{array}{r} T6 \\ 9.7 \\ 90 \end{array} \quad \begin{array}{r} 7.7 \\ 96 \end{array} \quad \begin{array}{r} 8.7 \\ 110 \end{array}$$

$$\begin{array}{r} 2.3 \\ 140 \end{array} \quad \begin{array}{r} 2.1 \\ 131 \end{array}$$

(1.0) -

$$\begin{array}{r} T6 \\ 10.7 \\ 65 \end{array} \quad \begin{array}{r} 11.4 \\ 87 \end{array} \quad \begin{array}{r} 8.7 \\ 96 \end{array} \quad \begin{array}{r} 9.4 \\ 110 \end{array}$$

$$\begin{array}{r} 1.2 \\ 140 \end{array} \quad \begin{array}{r} 0.9 \\ 127 \end{array}$$

(1.4) -

$$\begin{array}{r} T6 \\ 8.6 \\ 62 \end{array} \quad \begin{array}{r} 11.4 \\ 95 \end{array} \quad \begin{array}{r} 9.2 \\ 100 \end{array} \quad \begin{array}{r} 9.9 \\ 110 \end{array}$$

$$\begin{array}{r} 1.4 \\ 140 \end{array} \quad \begin{array}{r} 0.8 \\ 129 \end{array} \quad \begin{array}{r} 3.2 \\ 125-118 \end{array}$$

(1.8) -

$$\begin{array}{r} T6 \\ 8.0 \\ 55 \end{array} \quad \begin{array}{r} 10.5 \\ 94 \end{array} \quad \begin{array}{r} 9.9 \\ 104 \end{array} \quad \begin{array}{r} 10.2 \\ 110 \end{array}$$

$$\begin{array}{r} 1.3 \\ 140 \end{array} \quad \begin{array}{r} 1.5 \\ 134 \end{array} \quad \begin{array}{r} 4.3 \\ 129 \end{array} \quad \begin{array}{r} 3.8 \\ 96 \end{array}$$

(3.0) -

$$\begin{array}{r} 8.0 \\ 53 \end{array} \quad \begin{array}{r} 11.7 \\ 99 \end{array} \quad \begin{array}{r} 10.5 \\ 105 \end{array} \quad \begin{array}{r} 11.0 \\ 110 \end{array}$$

$$\begin{array}{r} 1.6 \\ 140 \end{array} \quad \begin{array}{r} 1.6 \\ 127 \end{array} \quad \begin{array}{r} 5.1 \\ 121 \end{array} \quad \begin{array}{r} 3.8 \\ 100 \end{array} \quad \begin{array}{r} 2.1 \\ 69 \end{array}$$

(4.3) -

$$\begin{array}{r} 8.6 \\ 48 \end{array} \quad \begin{array}{r} 10.8 \\ 89 \end{array} \quad \begin{array}{r} 10.1 \\ 98 \end{array} \quad \begin{array}{r} 11.2 \\ 110 \end{array}$$

$$\begin{array}{r} 1.9 \\ 140 \end{array} \quad \begin{array}{r} 2.0 \\ 132 \end{array} \quad \begin{array}{r} 5.9 \\ 124 \end{array} \quad \begin{array}{r} 4.7 \\ 100 \end{array} \quad \begin{array}{r} 4.9 \\ 57 \end{array}$$

(5.6) -

$$\begin{array}{r} T6 \\ 9.2 \\ 33 \end{array} \quad \begin{array}{r} 11.2 \\ 87 \end{array} \quad \begin{array}{r} 10.1 \\ 91 \end{array} \quad \begin{array}{r} 11.5 \\ 110 \end{array}$$

$$\begin{array}{r} 2.5 \\ 140 \end{array} \quad \begin{array}{r} 5.7 \\ 135 \end{array} \quad \begin{array}{r} 4.9 \\ 130 \end{array} \quad \begin{array}{r} 6.2 \\ 60 \end{array} \quad \begin{array}{r} 37 \end{array}$$

(5.9) -
8.1

$$\begin{array}{r} 12.6 \\ 77 \end{array} \quad \begin{array}{r} 10.7 \\ 86 \end{array} \quad \begin{array}{r} 11.2 \\ 110 \end{array}$$

(6.4) -

$$\begin{array}{r} 3.3 \\ 140 \end{array} \quad \begin{array}{r} 3.9 \\ 120 \end{array} \quad \begin{array}{r} 5.0 \\ 97 \end{array} \quad \begin{array}{r} 5.6 \\ 73 \end{array} \quad \begin{array}{r} 6.6 \\ 20 \end{array} \quad \begin{array}{r} 7.4 \\ 11 \end{array} \quad \begin{array}{r} 6.9 \\ 33 \end{array} \quad \begin{array}{r} 10.0 \\ 62 \end{array}$$

Sta	+	π	-
		191.36	

5			84.9
---	--	--	------

5	+25		86.4
---	-----	--	------

	+50		
--	-----	--	--

	+75		
--	-----	--	--

6			
---	--	--	--

	+25		
--	-----	--	--

	+50		
--	-----	--	--

6	+75		
---	-----	--	--

0	12.28	198.77	4.87	186.49
---	-------	--------	------	--------

0	49.2	203.50	0.19	198.58
---	------	--------	------	--------

BM			3.52	199.98	200.00
----	--	--	------	--------	--------

$$\begin{array}{r} 8.2 \\ 84 \end{array} \quad \begin{array}{r} 7.9 \\ 2 \end{array} \quad \begin{array}{r} 65 \\ 3 \end{array} \quad \begin{array}{r} 5.4 \\ 3 \end{array} \quad \begin{array}{r} 4.8 \\ 63 \end{array}$$

$$\begin{array}{r} 8.3 \\ 84 \end{array} \quad \begin{array}{r} 7.7 \\ 71 \end{array} \quad \begin{array}{r} 8.0 \\ 18 \end{array} \quad \begin{array}{r} 5.1 \\ 9 \end{array} \quad \begin{array}{r} 5.0 \\ 50 \end{array} \quad \begin{array}{r} 4.5 \\ 57 \end{array}$$

$$\begin{array}{r} 7.8 \\ 102 \end{array} \quad \begin{array}{r} 7.5 \\ 44 \end{array} \quad 32 - \begin{array}{r} 5.4 \\ 14 \end{array} \quad \begin{array}{r} 4.1 \\ 20 \end{array} \quad \begin{array}{r} 5.9 \\ 10 \end{array} \quad \begin{array}{r} 6.2 \\ 40 \end{array} \quad \begin{array}{r} 6.4 \\ 46 \end{array}$$

$$\begin{array}{r} 8.0 \\ 90 \end{array} \quad \begin{array}{r} 8.1 \\ 43 \end{array}$$

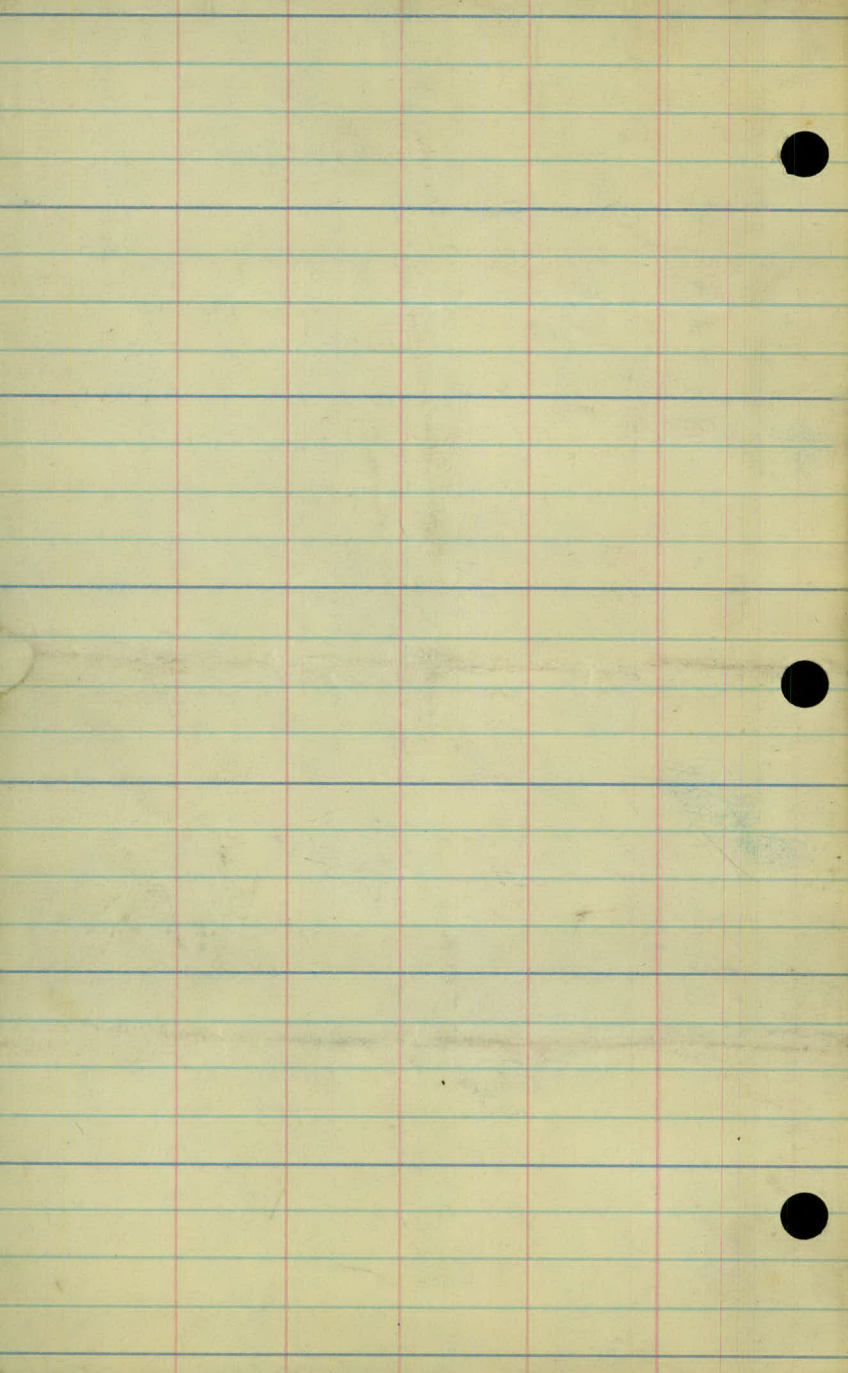
$$\begin{array}{r} 8.0 \\ 85 \end{array} \quad \begin{array}{r} 7.7 \\ 35 \end{array} \quad \begin{array}{r} 8.3 \\ 35 \end{array}$$

$$\begin{array}{r} 8.3 \\ 45 \end{array} \quad \begin{array}{r} 7.7 \\ 36 \end{array} \quad \begin{array}{r} 8.5 \\ 36 \end{array}$$

$$\begin{array}{r} 8.2 \\ 43 \end{array} \quad \begin{array}{r} 8.4 \\ 27 \end{array} \quad \begin{array}{r} 8.4 \\ 27 \end{array}$$

$$\begin{array}{r} 8.2 \\ 31 \end{array} \quad \begin{array}{r} 8.1 \\ 5 \end{array} \quad \begin{array}{r} 8.1 \\ 5 \end{array}$$

Tap Post NW Cor Pit



9/11/36

H.T. Portell

X- Sections

V Farm Gravel Pit

Plotted
Sept 16/1936
H.T. Portell

B.M.

7.74

207.74

200.00

5 + 75

6

+25

+50

+75

7

+25

0

4.90

199.67

12.97

194.77

0

4.93

190.89

13.71

185.96

5 + 75

Top Post NW Cor P.t

$$\frac{40.5}{128}$$

$$\frac{40}{136}$$

0.5

$$\frac{13}{143}$$

1.7

$$\frac{0.4}{140-131}$$

3.0

$$\frac{0.7}{140-132}$$

$$\frac{4.2}{125-119}$$

4.3

$$\frac{1.4}{140-136}$$

$$\frac{2.5}{124}$$

$$\frac{3.9}{81}$$

4.6

$$\begin{array}{r} \text{NG} \\ 2.2 \\ \hline 140 \end{array} \quad \begin{array}{r} 2.4 \\ \hline 77 \end{array} \quad \begin{array}{r} \text{T.G.} \\ 3.9 \\ \hline 86 \end{array}$$

5.0

$$\begin{array}{r} 7.3 \\ \hline 95 \end{array} \quad \begin{array}{r} 7.1 \\ \hline 47 \end{array} \quad \begin{array}{r} 5.2 \\ \hline 40 \end{array} \quad \begin{array}{r} 4.8 \\ \hline 27 \end{array} \quad \begin{array}{r} 7.5 \\ \hline 20 \end{array} \quad 7.6$$

190.89

6

+25

+50

+75

7+00

0

12.69

202.88

0.70

190.19

285

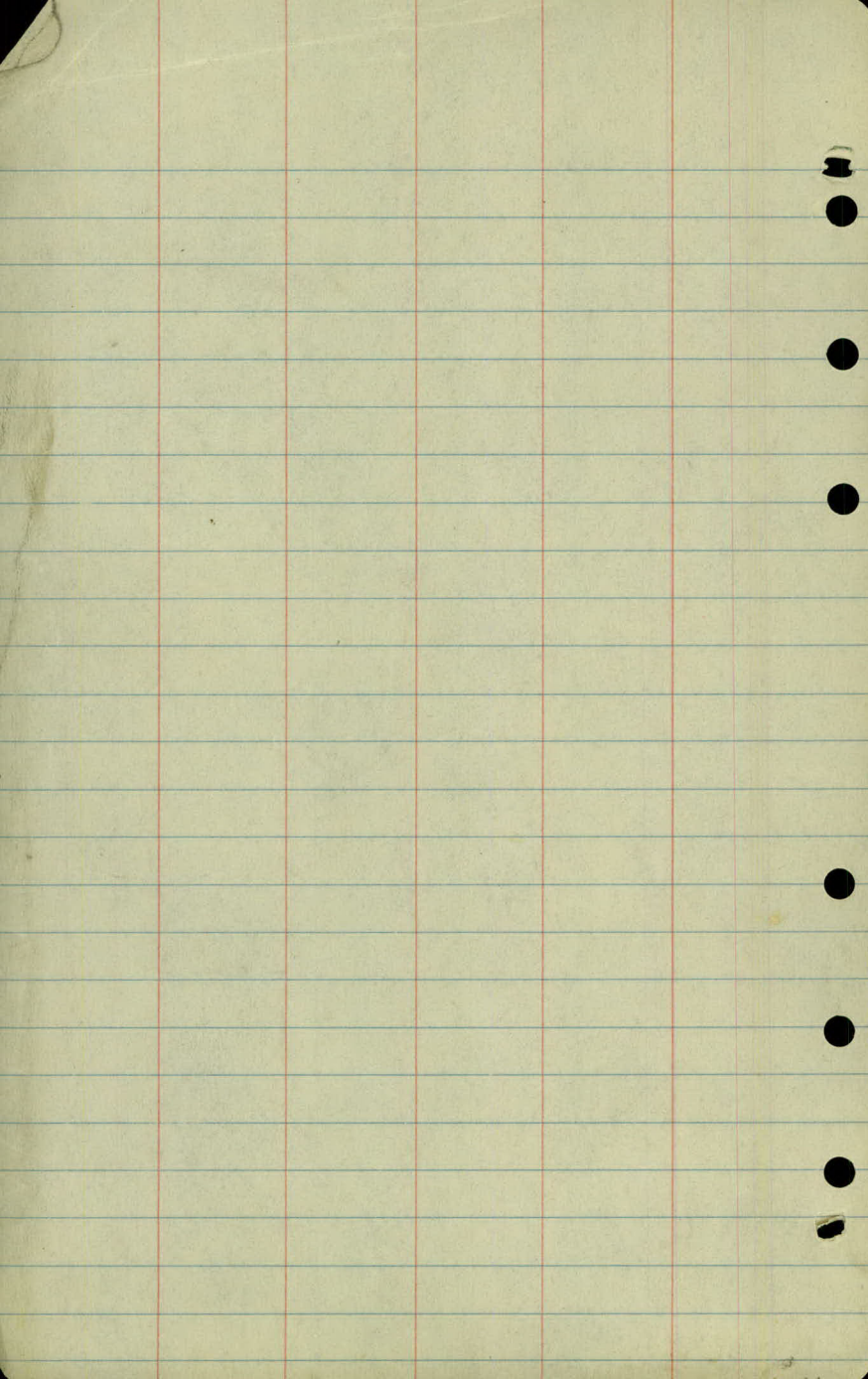
$$\frac{8.0}{103} \quad \frac{7.1}{53} \quad \frac{5.0}{45} \quad \frac{5.1}{35} \quad \frac{6.8}{30} \quad 7.1 \quad (16.9)$$

$$\frac{8.1}{111} \quad \frac{7.7}{60} \quad 7.1 \quad (15.1)$$

$$\frac{7.7}{103} \quad \frac{7.9}{63} \quad \frac{7.0}{54} \quad \frac{7.0}{24} \quad \frac{7.8}{13} \quad 2.8 \quad (13.8)$$

$$\frac{8.0}{58} \quad 7.6 \quad (12.5)$$

$$\begin{array}{r} +20. \\ 86 \\ \hline \end{array} \quad \begin{array}{r} +121 \\ \times \end{array} \quad (12.2)$$



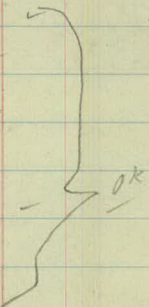
University Farm Gravel Pit

X-sections $\frac{12}{28}$
 $\frac{36}{36}$

{ Artell
Bratager
Wilks
Gottfried
Goldberg

T.G. = Top of Gravel as Stripped
N.G. = Natural Ground.

Sta.	+	X	-	Elev.
B.M.		✓		200.00
	7.60	207.60		✓
T.P.#1	12.80	207.60	(12.80)	(194.80) ✓
T.P.#2		✓	2.08	204.52
	1.96	206.48		✓
B.M.	7.49	206.48	7.49	198.99
T.P.#3		✓	11.64	194.84 ✓
	4.17	199.01		✓
T.P.#1			4.21	194.80 ✓
T.P.#3	0.40	195.74		194.84



3+50 X

3+75 X

4+00 X

4+25 X

4+50 X

4+75 X

5+00 X

Base
Line.
Z

Rt

Top of Post N.W. Cor. of Pit.

Nail in Fence Post.

Spike in 14" Oak

All readings to Rt. of Base Line.

$\frac{00}{47}$ $\frac{3.1}{62}$ $\frac{2.3}{76}$

+4.3

X

$\frac{6.4}{47}$ $\frac{6.0}{76}$

+5.6

X

$\frac{7.0}{76}$ $\frac{7.0}{66}$ $\frac{1.5}{76}$

$\frac{1.5}{85}$ $\frac{1.5}{90}$

$\frac{7.0}{285}$

+6.1

+8.1

$\frac{8.4}{79}$ $\frac{8.4}{67}$ $\frac{2.0}{76}$

$\frac{2.1}{71}$ $\frac{10.3}{185}$

$\frac{12.7}{215}$

$\frac{9.2}{280}$

$\frac{9.2}{325}$

+11.2

$\frac{8.4}{77}$ $\frac{8.4}{67}$ $\frac{2.1}{76}$

$\frac{0.8}{85}$ $\frac{3.0}{115}$

$\frac{5.9}{145}$

$\frac{2.8}{185}$

+11.6

$\frac{11.0}{76}$ $\frac{10.8}{50}$ $\frac{3.1}{75}$

$\frac{3.4}{85}$ $\frac{3.5}{100}$

$\frac{8.1}{175}$

$\frac{6.7}{185}$

$\frac{5.9}{170}$ $\frac{3.0}{180}$

+12.5

$\frac{11.0}{76}$ $\frac{11.0}{58}$ $\frac{7.0}{70}$ $\frac{9.2}{85}$

$\frac{10.3}{100}$ $\frac{11.6}{175}$

$\frac{12.0}{165}$

Sta. + K - Elev.

5+25 X 195.24

5+50 X

5+75 X

6+00 X

6+25 X

6+50 X

6+75 X

T.P. 0.40 194.84

9.40 204.24

3+50 X

3+75 X

4+00 X

4+25 X

4+50 X

Base
line.

Rt.

+12.6 $\frac{9.7}{00}$ $\frac{8.5}{46}$ $\frac{6.9}{68}$ $\frac{10.3}{72}$ $\frac{11.6}{85}$ $\frac{7.7}{78}$ $\frac{13.8}{105}$ $\frac{12.1}{148}$

+12.8 $\frac{8.7}{00}$ $\frac{10.6}{45}$ $\frac{5.9}{55}$ $\frac{12.1}{66}$ $\frac{10.5}{85}$ $\frac{11.7}{95}$ $\frac{6.7}{103}$ $\frac{12.8}{118}$ $\frac{13.6}{145}$ $\frac{11.1}{150}$ $\frac{6.0}{167}$

+12.4 $\frac{11.8}{2}$ $\frac{10.7}{38}$ $\frac{8.0}{46}$ $\frac{11.7}{56}$ $\frac{12.4}{85}$ $\frac{9.5}{92}$ $\frac{11.9}{98}$ $\frac{3.7}{112}$ $\frac{5.8}{121}$

+12.0 $\frac{11.4}{00}$ $\frac{11.4}{33}$ $\frac{8.3}{44}$ $\frac{11.0}{50}$ $\frac{11.6}{85}$ $\frac{12.0}{100}$

+10.8 $\frac{11.5}{00}$ $\frac{11.8}{30}$ $\frac{10.3}{36}$ $\frac{10.7}{85}$ $\frac{9.0}{95}$

+9.5 $\frac{12.0}{00}$ $\frac{11.8}{18}$ $\frac{10.7}{20}$ $\frac{10.7}{25}$ $\frac{11.8}{30}$ $\frac{11.7}{71}$ $\frac{10.7}{85}$

+8.2 $\frac{12.0}{2}$ $\frac{5.9}{17}$ $\frac{5.7}{23}$ $\frac{12.7}{40}$ $\frac{12.7}{71}$ $\frac{8.0}{85}$

76
N.G. N.G. N.G. T.G. ¹¹ T.G. N.G. 3140:00 stripping
 $\frac{00}{97}$ $\frac{4}{285}$ $\frac{26}{335}$ $\frac{56}{351}$ $\frac{3.8}{375}$ $\frac{00}{385}$

74
T.G. T.G. N.G. ³⁴ T.G. N.G. T.G. T.G. T.G. N.G.
 $\frac{1.7}{57}$ $\frac{3.7}{118}$ $\frac{00}{134}$ $\frac{2.3}{185}$ $\frac{3.3}{275}$ $\frac{8.5}{285}$ $\frac{6.6}{338}$ $\frac{4.2}{385}$ $\frac{0.9}{396}$

78 ^{reading}
T.G. T.G. N.G. N.G. ⁹ T.G. T.G. N.G. N.G.
 $\frac{4.0}{100}$ $\frac{4.6}{176}$ $\frac{0.5}{185}$ $\frac{1.9}{225}$ $\frac{2.2}{300}$ $\frac{7.7}{392}$ $\frac{2.5}{402}$ $\frac{2.4}{470}$

525
0.9
T.G. T.G. T.G. T.G. T.G. T.G. N.G. N.G.
 $\frac{3.6}{101}$ $\frac{3.0}{127}$ $\frac{11.7}{331}$ $\frac{8.7}{368}$ $\frac{7.5}{396}$ $\frac{17.0}{400}$ $\frac{4.2}{410}$ $\frac{4.4}{426}$

181
+2.2
T.G. T.G. T.G. T.G. T.G. T.G. N.G. N.G.
 $\frac{5.4}{230}$ $\frac{6.1}{250}$ $\frac{9.7}{285}$ $\frac{11.9}{321}$ $\frac{9.1}{385}$ $\frac{8.8}{405}$ $\frac{5.8}{413}$ $\frac{6.3}{430}$

Sta. + X - Elev.

204.24

4+75 X

5 X

5+25 X

5+50 X

5+75 X

6 X

6+25 X

6+50 X

6+75 X

7+05

B.M.

5.26

198.98

T.P.#1

194.80

12.77 207.57

B.M.

7.56

200.01

Base
Line

RT.

180 +2.6

T.G.	T.G.	T.G.	T.G.	T.G.	T.G.	N.G.	N.G.
6.0	6.3	9.7	11.1	11.6	10.0	24.	7.4
185	222	255	285	315	322	385	400

165 +3.5

T.G.	T.G.	T.G.	T.G.	T.G.	T.G.	N.G.	N.G.
9.9	9.0	11.1	12.7	12.0	10.9	6.0	6.2
175	195	213	237	285	322	349	385

148 +3.6

T.G.	T.G.	T.G.	T.G.	T.G.	N.G.	N.G.	N.G.	N.G.	N.G.
11.0	12.0	12.7	13.5	13.2	8.8	8.7	7.6	8.9	8.5
165	174	185	225	268	280	285	326	365	385

5+40 = 00 Exc. on Rt.

127 +3.8

T.G.	N.G.	N.G.	N.G.	N.G.	N.G.	N.G.	N.G.	N.G.	N.G.
10.4	5.6	8.7	12.8	12.5	11.7	10.4	12.0	14.3	14.7
170	178	215	225	260	285	313	325	355	385

+3.4

T.G.	T.G.	N.G. here out	N.G.	N.G.	N.G.	N.G.	N.G.	N.G.	N.G.	N.G.
5.7	10.1	6.4	8.7	10.7	14.2	14.0	12.9	13.5	12.1	8.5
155	170	175	198	213	221	255	285	347	357	302

+3.0

T.G.	T.G.	N.G. here out	N.G.	N.G.	N.G.	N.G.	N.G.	N.G.	N.G.
8.1	8.5	6.9	8.2	8.6	8.7	8.2	7.4	7.3	5.8
114	127	131	160	185	219	255	285	335	347

+1.8

N.G.	N.G.
6.1	7.5
110	133

+0.5

T.G.	T.G.	N.G.
7.6	7.6	6.2
100	105	108

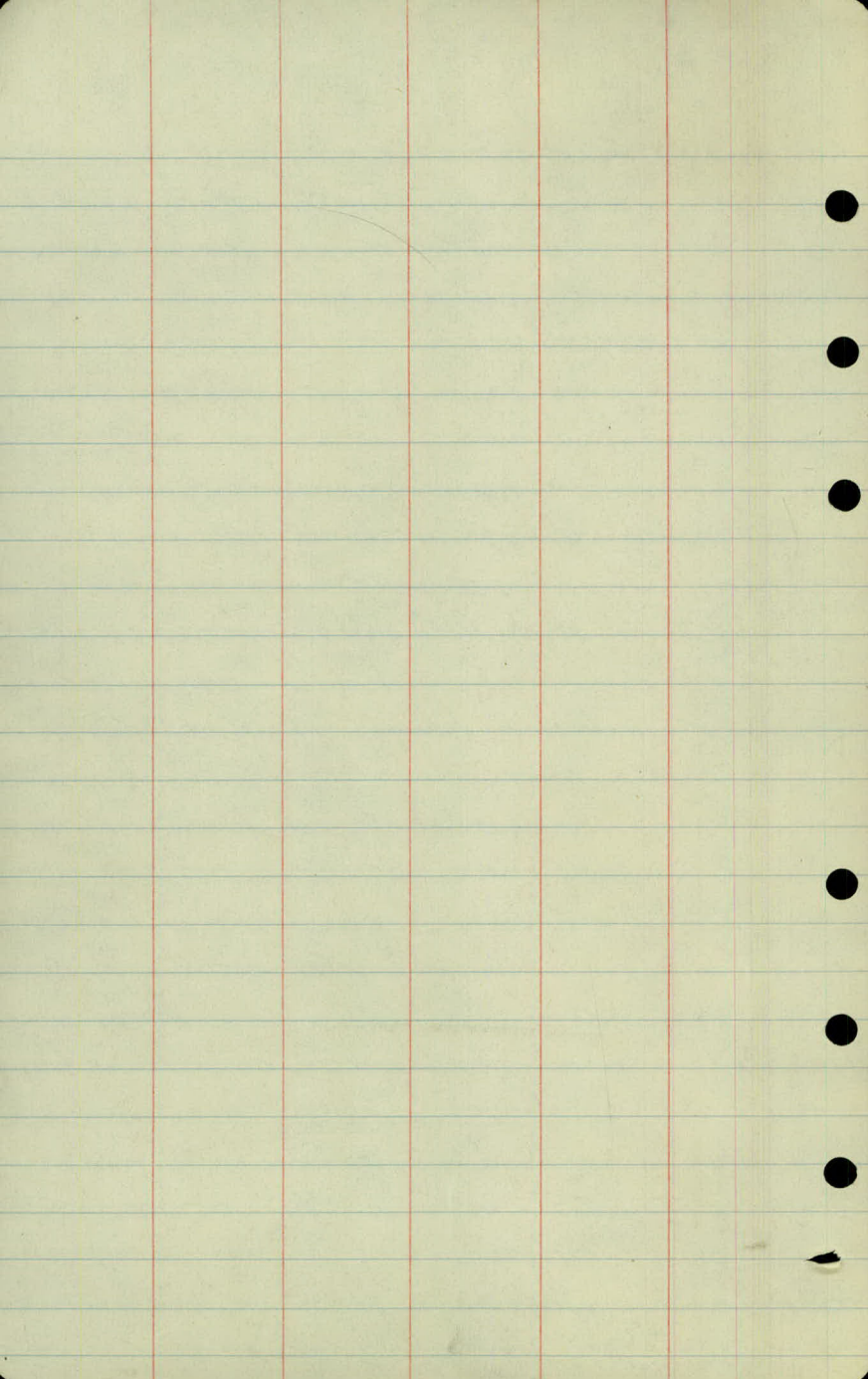
0.8

T.G.	T.G.	N.G.
8.2	8.2	6.7
90	99	103

00 Exc.

198.99

[200.00] Top of Post N.W. Cor. of Pt.

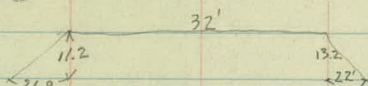


12 3
9 8
2 0

Stock Pile #1 Road Gravel

00 = 00

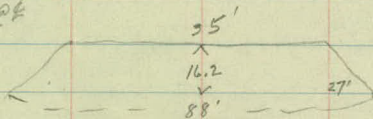
0+86



1

1+12

4' higher @ 1/2



2

1+33

and

1+48

9.8+0+86

70'

125'

22.0'

3

1+72

00

Stock Pile #2 Road Gravel

0+60

33

10.3

62

4

+1.9 to 0+60

0+76

51.0'

12.2

76'

52'

5

1+74

24.0

120

6

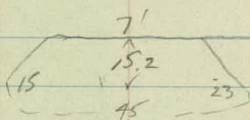
2+07

00

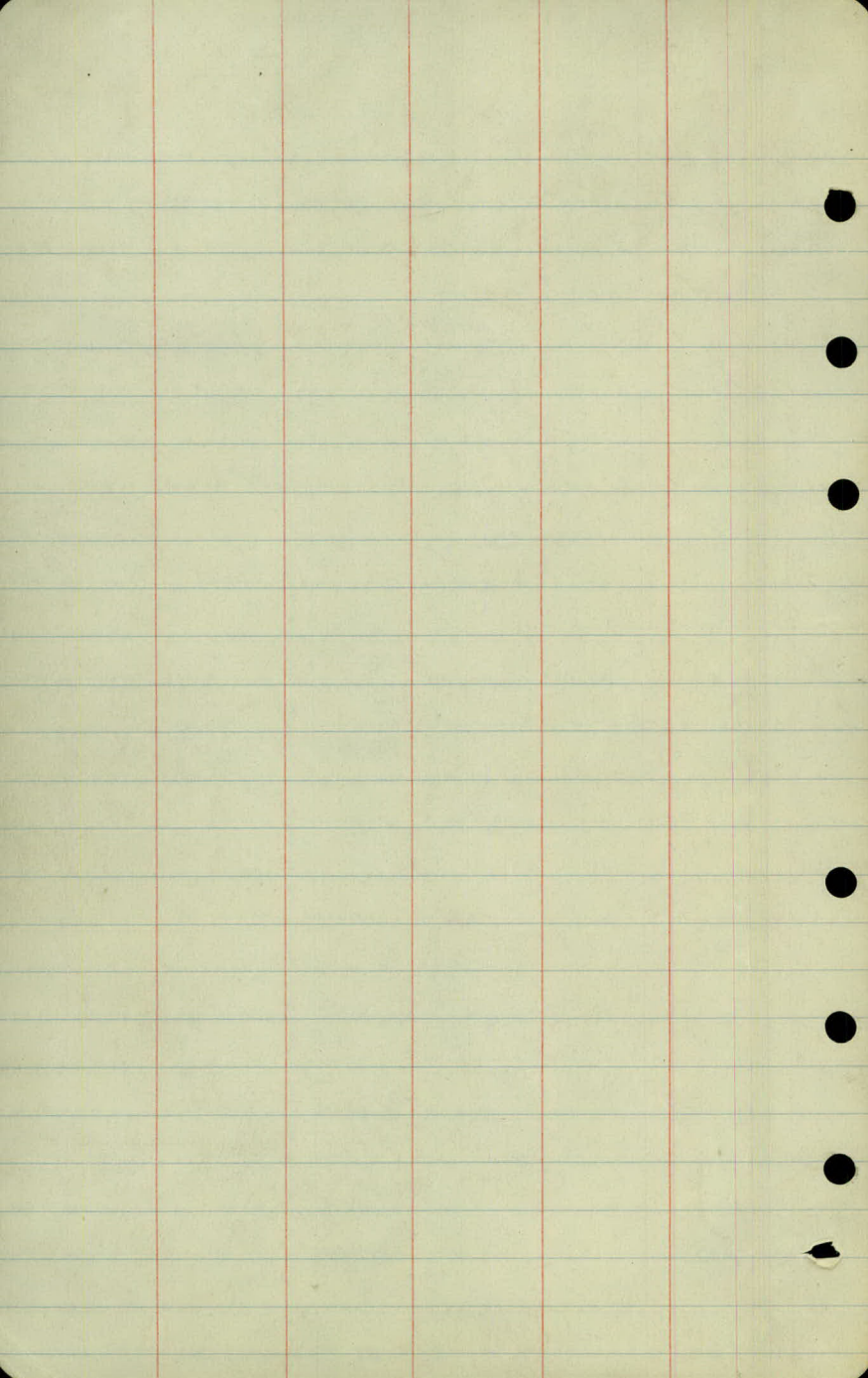
Sheet Pile #3 (3/4" Box K)

0+48

0+71 = 00



7



1
L-Farm Gravel Pit
X-Sections

3/29/27

Distance
Right
Base
Line.

+ π - Elev.

B.M. 4.65 203.64 198.99

125'

150'

175'

200'

225'

250'

275'

Spike in 14" Oct.

N.G.	T.G.	T.G.	T.G.						
+0.3	16	3.7	3.8	14.7	13.8	12.8	15.8	16.0	20.0
3+69	3+81	4+00	4+11	4+34	4+38	4+48	4+56	4+76	4+81

16.0	18.0	21.3	21.5	7.6	7.6	N.G.
4+90	5+00	5+18	5+59	5+80	6+00	6+01

N.G.	T.G.	T.G.							
+1.0	6.5	5.0	17.1	15.9	15.8	18.5	17.9	18.3	18.1
3+34	3+53	3+98	4+20	4+25	4+44	4+54	4+70	4+82	5+05

21.0	14.4	5.5	9.5	6.8
5+46	5+68	5+75	5+86	5+91

N.G.	T.G.	T.G.						
+0.8	8.3	6.0	19.1	19.1	13.0	9.3	11.2	5.6
3+33	3+37	3+84	4+07	4+60	4+77	5+00	5+24	5+44

N.G.	T.G.	T.G.							
00	8.5	7.7	19.0	19.1	18.2	4.8	9.1	12.6	7.9
3+24	3+26	3+74	3+95	4+27	4+58	4+76	5+00	5+30	5+47

N.G.	T.G.	T.G.							
+0.3	9.0	8.2	20.0	21.5	19.6	19.6	6.3	10.5	12.8
3+17	3+15	3+51	3+80	4+00	4+40	4+61	4+74	5+00	5+40

N.G.	T.G.	T.G.							
3.9	8.4	9.7	18.8	20.7	20.8	20.0	9.1	11.8	9.8
3+00	3+09	3+65	3+80	4+00	4+21	4+63	4+76	5+00	5+44

N.G.	T.G.	T.G.							
+4.5	8.7	9.1	21.0	19.7	19.5	18.0	18.0	11.8	11.6
2+91	2+95	3+73	3+89	4+00	4+41	4+67	4+80	5+00	5+20

Dist
Right
Base
Line

+

x

-

Elev.

300'

203.64

375'

350'

375'

400'

410' 200

B.M.

4.65

198.99

N.G.	T.G.	T.G.	T.G.	T.G.	T.G.	T.G.	T.G.	T.G.	T.G.
<u>3.6</u>	<u>8.9</u>	<u>9.7</u>	<u>9.2</u>	<u>7.2</u>	<u>10.2</u>	<u>10.7</u>	<u>7.1</u>	<u>7.1</u>	<u>20.5</u>
2+73	2+83	2+00	2+40	2+73	3+77	3+81	3+89	4+00	4+18

N.G.	T.G.	T.G.	T.G.	N.G.
<u>18.5</u>	<u>10.3</u>	<u>10.7</u>	<u>11.0</u>	<u>7.6</u>
4+56	4+69	5+00	5+10	5+16

N.G.	T.G.	T.G.	T.G.	T.G.	T.G.	T.G.	T.G.	T.G.	T.G.	N.G.
<u>4.0</u>	<u>7.2</u>	<u>7.1</u>	<u>7.6</u>	<u>8.6</u>	<u>16.6</u>	<u>16.6</u>	<u>10.9</u>	<u>10.9</u>	<u>10.0</u>	<u>5.7</u>
2+78	3+00	3+46	4+00	4+09	4+21	4+27	4+34	4+61	5+00	5+06

N.G.	N.G.	N.G.	T.G.	T.G.	T.G.	T.G.	T.G.	N.G.
<u>3.1</u>	<u>5.4</u>	<u>6.0</u>	<u>6.1</u>	<u>7.2</u>	<u>9.5</u>	<u>10.4</u>	<u>10.5</u>	<u>5.4</u>
2+84	2+87	3+00	3+50	4+00	4+25	4+50	4+88	5+00

N.G.	T.G.	T.G.	T.G.	T.G.	T.G.	N.G.
<u>00</u>	<u>3.5</u>	<u>4.5</u>	<u>7.2</u>	<u>7.7</u>	<u>9.5</u>	<u>5.4</u>
3+35	3+48	3+77	4+00	4+36	4+81	4+89

N.G.	T.G.	T.G.	N.G.
<u>1.3</u>	<u>6.0</u>	<u>8.5</u>	<u>6.0</u>
3+91	4+15	4+55	4+61

Spike in 14" Oak

Stock Piles.

#1 Sand

0+00

0+26

0+57₁₅

0+75

#1 - $\frac{3}{4}$ " Rock

0+00

0+34

0+61

0+91

#1 Road Gravel.

This stock pile has not been
touched since previous measurement.

Lt.

4

RT

4

00

$$-\frac{4.9}{17}$$

$$\frac{00}{8}$$

$$\frac{00}{13}$$

$$-\frac{6.6}{26}$$

$$-\frac{14.0}{26}$$

$$\frac{00}{9}$$

$$\frac{00}{6}$$

$$-\frac{14.0}{20}$$

00

00

$$-\frac{7.5}{15}$$

$$\frac{00}{5}$$

$$\frac{00}{5}$$

$$-\frac{10.5}{23}$$

$$-\frac{14.0}{24}$$

$$\frac{00}{4}$$

$$\frac{00}{4}$$

$$-\frac{12.0}{27}$$

00

Stock Piles.

#2 Road Gravel.

0+00

0+50

0+73

0+88

1+15

1+41

1+57

1+70

2+03

L+

Q

R+

5

00

$$-\frac{10.0}{39}$$

$$\frac{00}{20}$$

$$\frac{00}{16} - \frac{8.5}{30}$$

$$-\frac{13.8}{51}$$

$$+\frac{0.5}{26}$$

00

$$\frac{00}{6}$$

$$+\frac{3.6}{25}$$

$$-\frac{11.0}{45}$$

$$-\frac{16.8}{65}$$

$$+\frac{2.8}{30}$$

$$+\frac{1.0}{18}$$

00

$$+\frac{2.0}{23}$$

$$-\frac{13.0}{45}$$

$$-\frac{16.6}{34}$$

$$+\frac{1.0}{14}$$

00

$$+\frac{1.0}{18}$$

$$-\frac{16.6}{43}$$

$$-\frac{18.6}{34}$$

$$\frac{00}{10}$$

00

$$+\frac{1.5}{14}$$

$$-\frac{18.2}{44}$$

$$-\frac{21.1}{46}$$

$$\frac{00}{9}$$

00

$$+\frac{0.8}{9}$$

$$-\frac{19.8}{41}$$

$$-\frac{25.0}{74}$$

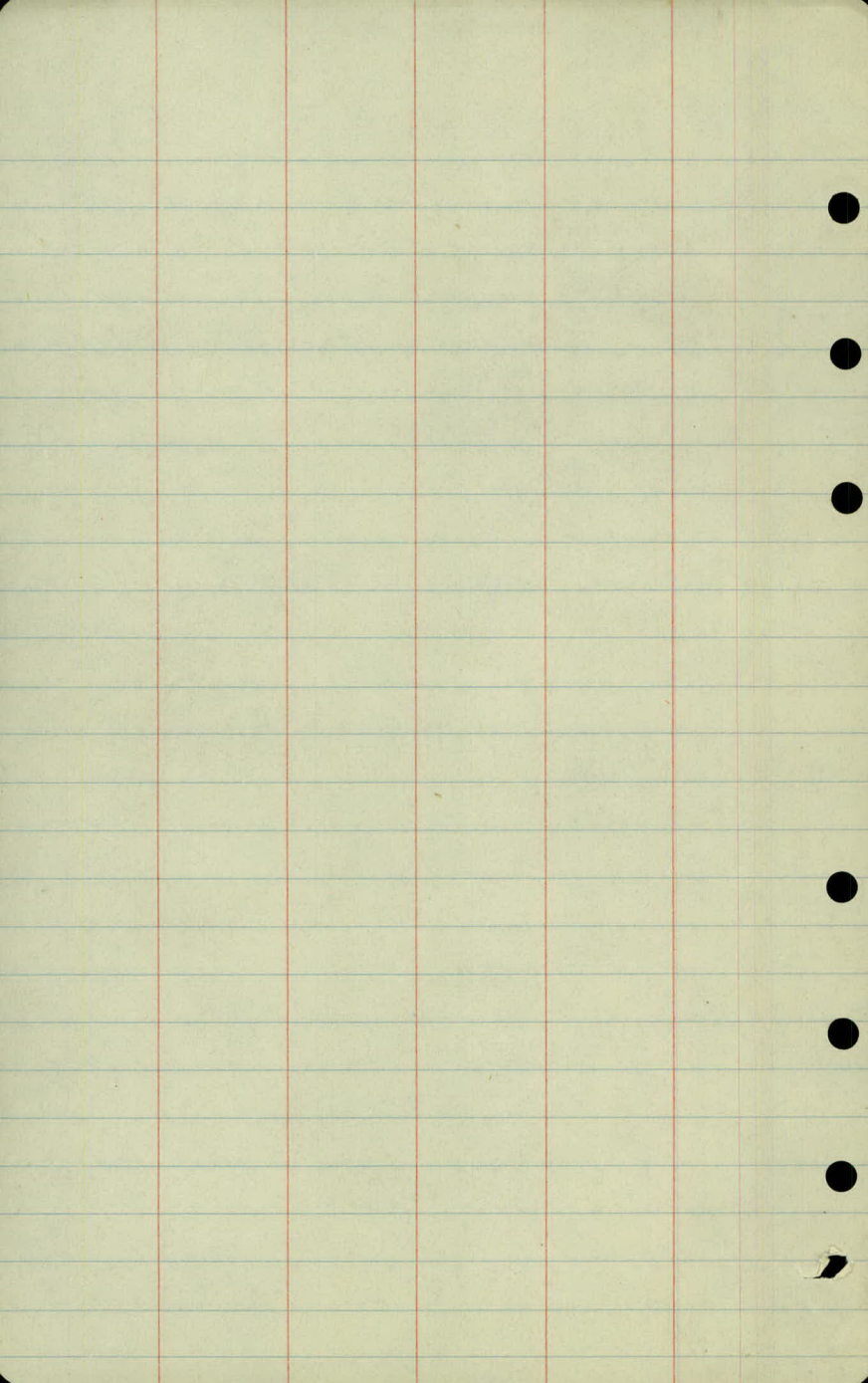
$$\frac{00}{19}$$

00

$$\frac{00}{10}$$

$$-\frac{21.0}{40}$$

00



1
Stock Piles

U-Farm Gravel Pit.

Fair Grounds.

9/21/37

K.A.

Crushed Rock Pile.

0+00

+25

+44

+70

Gravel Pile #1

0+00

+25

+38

+49

00

$$\frac{0.0}{17}$$

$$\frac{+4.8}{4'}$$

$$\frac{+8.0}{4}$$

$$\frac{0.0}{18}$$

$$\frac{0.0}{19}$$

$$\frac{+4.8}{4}$$

$$\frac{+13.0}{4}$$

$$\frac{0.0}{18}$$

00

00

$$\frac{0.0}{21}$$

$$\frac{+9.5}{7}$$

$$\frac{+6.0}{11}$$

$$\frac{0.0}{23}$$

$$\frac{0.0}{28'}$$

$$\frac{+5.7}{12}$$

$$\frac{+7.3}{9}$$

$$\frac{0.0}{22}$$

00

Gravel Pile #2

0+00

+25

+50

+75

1+05

+35

+53

+86

00

$$\frac{00}{23}$$

$$\frac{+4.0}{16}$$

$$\frac{+43}{9}$$

$$\frac{00}{16}$$

$$\frac{00}{36}$$

$$\frac{+7.4}{25}$$

$$\frac{+70}{40}$$

$$\frac{00}{19} 49$$

$$\frac{00}{50}$$

$$\frac{+10.6}{31}$$

$$+10.1$$

$$\frac{00}{18}$$

$$\frac{00}{51}$$

$$\frac{+13.2}{33}$$

$$\frac{+15.5}{31}$$

$$\frac{00}{31}$$

$$\frac{00}{52}$$

$$\frac{+17.2}{25'}$$

$$\frac{+21.5}{42}$$

$$\frac{00}{74'}$$

$$\frac{00}{53}$$

$$\frac{+18.5}{21}$$

$$\frac{+21.5}{42}$$

$$\frac{00}{74}$$

00

Gravel Pile #3

0 + 00

+50

+65

1 + 00

+50

+72

+82

$$\frac{0.0}{41}$$

$$\frac{+100}{26}$$

$$\frac{+83}{19}$$

$$\frac{0.0}{29}$$

00

$$\frac{0.0}{17}$$

$$\frac{+70}{39.0}$$

$$\frac{-00}{43}$$

$$\frac{0.0}{31}$$

$$\frac{+55}{4.4}$$

$$\frac{0.0}{50}$$

$$\frac{0.0}{28}$$

$$\frac{+70}{42}$$

$$\frac{0.0}{53}$$

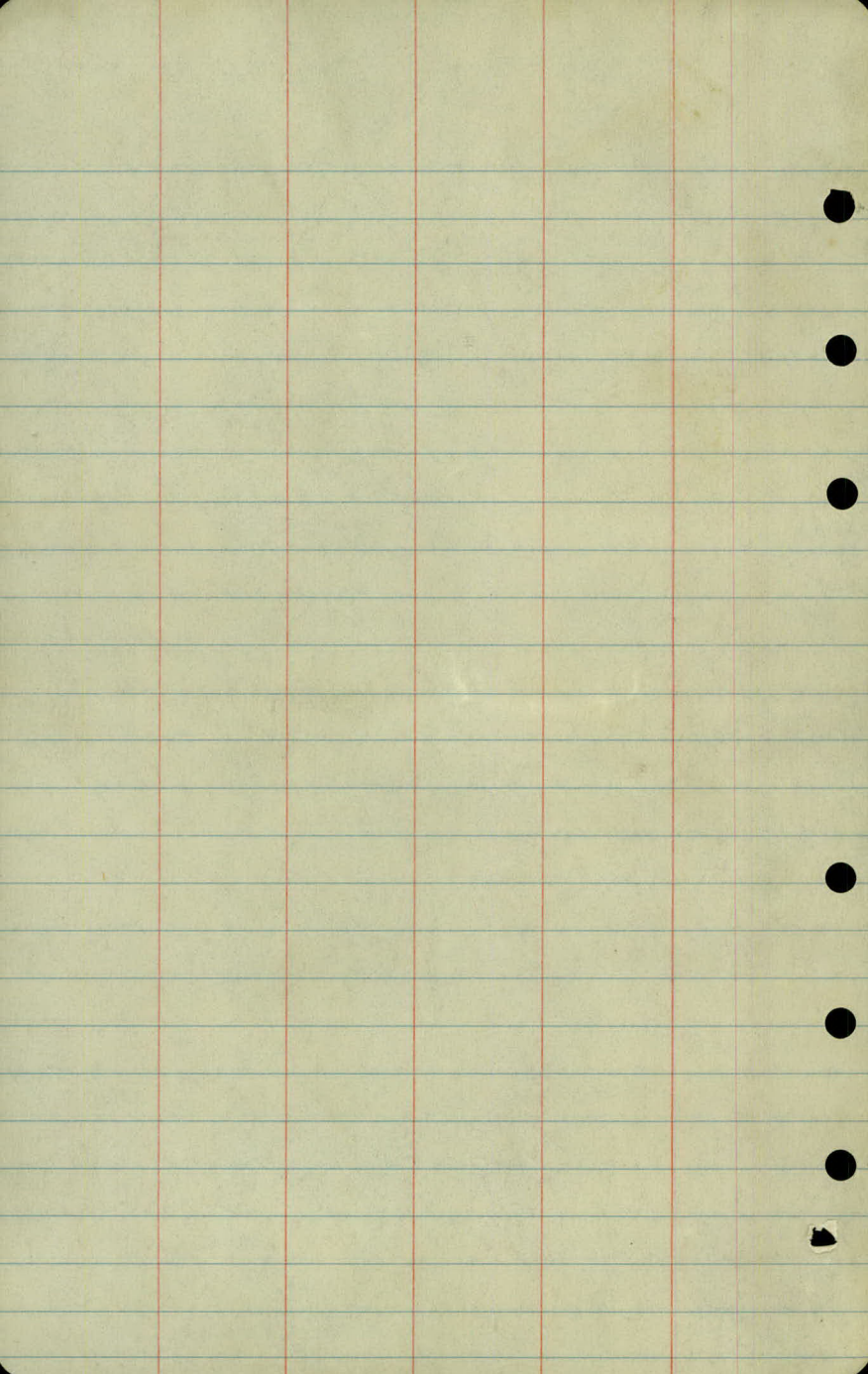
$$\frac{0.0}{8}$$

$$\frac{+96}{}$$

$$\frac{+70}{43}$$

$$\frac{0.0}{55}$$

00



Gravel Pit

Stock Pile

X. 9.

Nov. 22, 1927

0400

+33

+98

1 +13

+32

00

-126
23.0

00

-193
31

-221
30.0

00

-197
32.0

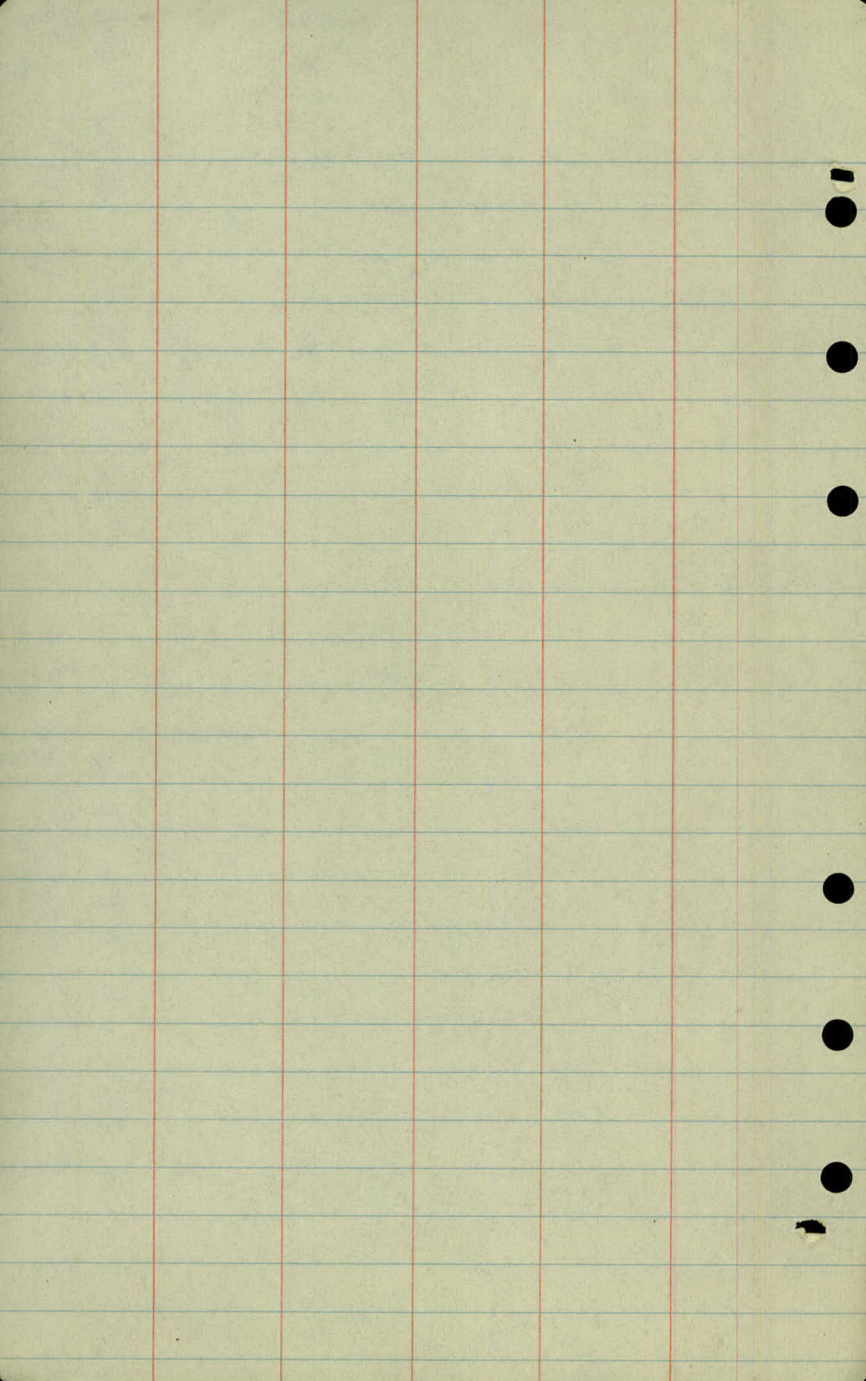
-140
44.0

-103
22.0

00

-12.3
30.0

00



FINAL X SECTIONS

UGRAVEL PIT

Plotted 2-16-38
ma B.

Sta	+	A	-	Elev.
B.M.	5.80	2.0580		200.00
0+00				98.1
+25				98.1
+50				97.8
+75				96.8
1				97.0

+25				97.2
+50				97.1

T.P. # ①	7.74	2.0710	6.44	199.36
+75				97.6

2				98.3
+25				97.4

T.P.	7.74	2.0712	7.74	199.36
+50				95.9

2/3/38

K.H.
L.B.H.
L.C.
M.d.G.

Lt.

E

Rt

Top Fe. Post E. of No. Ent. to Pit.

7.8

N.G.	77	76	98	69	59	40	9.8	N.G.
38		50	81	94	150	200	250	270

8.0

N.G.	80	76	94	70	54	37	N.G.
40		27	78	100	150	200	275

9.2

N.G.	90	103	103	71	40	N.G.
31		34	68	76	200	300

8.9

N.G.	88	107	109	72	40	40	20	N.G.
25		75	76	89	130	200	250	300

9.0

N.G.	86	85	104	107	80	51	44	09	N.G.
30		10	28	64	80	146	200	300	330

8.7

N.G.	46	76	77	87	84	127	110	53	85	99	59	53	33	27
135	68	50	34		10	34	50	60	80	95	115	136	172	233
												27	N.G.	
												280	305	

9.9

N.G.	73	68	91	85	95	96	108	96	96	111	97	73	68	44	40
135	124	80	67	25		7	33	43	66	76	111	118	137	163	228
													40	N.G.	
													264	290	

10.1

N.G.	91	101	88	95	74	75	43	46	43	N.G.
140	118	63		60	116	137	145	200	297	305

11.2

N.G.	107	103	107	97	75	77	89	78	38	32	43	18
139	110	71	82		60	88	100	140	150	184	220	236
											17	22
											261	300
												305

11.2

N.G.	107	106	112	105	87	78	83	45	37	N.G.
137	100	81		76	32	66	132	150	200	225

540

+

4

—

Elev.

207.12

2

+ 75

194.4

3

93.2

+2.5

750

+75

A

425

450

475

5

Lt.

E

Rt.

$$+70 = C.O.O$$

10.2

N.G.	95	107	107	126	127	128	91	76	86	N.G.	N.G.	116	N.G.
116	96	69	22	17		16	26	96	190	141	294	310	323

-9.3

N.G.	139	139	142	N.G.	N.G.	122	128	92	N.G.
32	24		14	28	24	269	300	353	353

-8.3

N.G.	121	125	87	N.G.
208	292	290	308	316

-7.6

N.G.	108	1200	128	121	87	74	N.G.
150	160	200	250	300	350	375	387

-6.8

N.G.	N.G.	8.8	105	(5cc)	106	9.0
100	125	137	204	(10cc)	300	350
				3		

7.7	N.G.
380	392

7.0	6.7	(5cc)	106	116	105	N.G.
101	137	(10cc)	300	350	387	391
		3				

3.1

13.2	105	103	N.G.
337	376	373	307

0.7

138	138	118	N.G.
310	350	398	411

-0.5

90	90	122	132	141	138	125	N.G.
180	200	250	305	325	253	313	378

+0.6

123	155	140	132	N.G.
178	235	300	332	347

Sta	+	π	-	Elev.
		207.12		

5 +25

I.P.	0.20	199.56		199.36
------	------	--------	--	--------

3 +25 191.5

+50 89.9

+75 89.1

A 87.9

+25 86.6

I.P.	4.71	195.68	8.59	190.97
------	------	--------	------	--------

+50 84.8

+75 83.8

4 +25

9 +00

8 +75

Lt.

E

Rt.

$$+0.7 \quad \frac{142}{166} \quad \frac{158}{200} \quad \frac{160}{262} \quad \frac{N.G.}{281}$$

from T.R. #1

+0.8

$$\frac{N.G.}{39} \quad \frac{78}{28} \quad \frac{81}{10} \quad \frac{84}{27} \quad \frac{N.G.}{57} \quad \frac{N.G.}{67} \quad \frac{25}{76} \quad \frac{28}{87} \quad \frac{N.G.}{87} \quad \checkmark$$

-0.1

$$\frac{N.G.}{46} \quad \frac{91}{33} \quad \frac{97}{7} \quad \frac{97}{19} \quad \frac{41}{36} \quad \frac{52}{75} \quad \frac{71}{78} \quad \frac{9.2}{100} \quad \frac{N.G.}{100} \quad \checkmark$$

+1.2

$$\frac{N.G.}{53} \quad \frac{104}{34} \quad \frac{105}{33} \quad \frac{103}{74} \quad \frac{108}{74} \quad \checkmark$$

3.7

$$\frac{N.G.}{83} \quad \frac{0.4}{76} \quad \frac{0.4}{62} \quad \frac{113}{78} \quad \frac{117}{25} \quad \frac{113}{66} \quad \frac{111}{77} \quad \frac{63}{92} \quad \frac{53}{92} \quad \checkmark$$

3.7

$$\frac{N.G.}{85} \quad \frac{135}{57} \quad \frac{130}{57} \quad \frac{120}{82} \quad \frac{60}{100} \quad \frac{60}{130} \quad \frac{5.2}{130} \quad \checkmark$$

T.R. #2

16.7

$$\frac{N.G.}{111} \quad \frac{116}{74} \quad \frac{109}{50} \quad \frac{10.4}{33} \quad \frac{83}{77} \quad \frac{96}{82} \quad \frac{0.8}{100} \quad \frac{0.8}{120} \quad \frac{15}{143} \quad \frac{9.9}{200} \quad \frac{110}{271} \quad \frac{12.8}{293} \quad \frac{12.2}{293} \quad \checkmark$$

11.1

$$\frac{N.G.}{115} \quad \frac{116}{89} \quad \frac{115}{45} \quad \frac{99}{110} \quad \frac{9.9}{32} \quad \frac{10.9}{60} \quad \frac{11.9}{75} \quad \frac{40}{93} \quad \frac{30}{107} \quad \frac{42}{82} \quad \frac{20}{162} \quad \frac{13.5}{162} \quad \checkmark$$

7.6

$$\frac{8.7}{142} \quad \frac{100}{170} \quad \frac{75}{200} \quad \frac{12.9}{250} \quad \frac{130}{300} \quad \frac{10.2}{322} \quad \checkmark$$

7.6

$$\frac{11.1}{189} \quad \frac{106}{212} \quad \frac{135}{235} \quad \frac{13.5}{276} \quad \checkmark$$

5.1

$$\frac{106}{233} \quad \checkmark$$

Sta.	+	π	-	Elev.
		195.68		
5	+00			184.1
	+25			86.4
	+50			87.1
	+75			83.5
6				83.7
	+25			83.8
	+50			83.2
	+75			85.1
7				84.6
	+25			84.9
	+50			84.3
T.P.	3.24	189.84 ✓	9.08	186.60 ✓

Lt.

E

Rt.

+12.0

N.G.	118	118	116	116	66	58	113	13.2
<u>111</u>	<u>85</u>	<u>50</u>	<u>37</u>	<u>69</u>	<u>83</u>	<u>110</u>	<u>109</u>	

+11.9

N.G.	120	118	93	89	82	104	101	136	134
<u>124</u>	<u>94</u>	<u>19</u>	<u>21</u>	<u>77</u>	<u>83</u>	<u>100</u>	<u>110</u>	<u>149</u>	

+12.2

N.G.	113	120	110	86	100	99	113	110	129	135	14	100	N.G.
<u>135</u>	<u>99</u>	<u>45</u>	<u>38</u>	<u>35</u>	<u>70</u>	<u>79</u>	<u>105</u>	<u>111</u>	<u>134</u>	<u>142</u>	<u>131</u>	<u>177</u>	

+11.9

N.G.	120	121	97	118	122	113	101	104	113	107	52	10	N.G.
<u>135</u>	<u>94</u>	<u>50</u>	<u>31</u>	<u>15</u>	<u>32</u>	<u>37</u>	<u>57</u>	<u>63</u>	<u>109</u>	<u>114</u>	<u>174</u>	<u>177</u>	

+11.6

N.G.	121	120	88	98	112	120	123	110	107	119	102	N.G.
<u>143</u>	<u>102</u>	<u>54</u>	<u>45</u>	<u>34</u>	<u>28</u>	<u>36</u>	<u>34</u>	<u>56</u>	<u>63</u>	<u>104</u>	<u>119</u>	

+10.3

N.G.	121	120	119	124	108	112	98	N.G.
<u>146</u>	<u>112</u>	<u>50</u>	<u>23</u>	<u>33</u>	<u>57</u>	<u>76</u>	<u>108</u>	

+9.0

N.G.	94	120	120	125	124	106	109	100	N.G.
<u>138</u>	<u>100</u>	<u>85</u>	<u>50</u>	<u>74</u>	<u>26</u>	<u>56</u>	<u>81</u>	<u>104</u>	

+7.7

N.G.	116	123	106	106	102	N.G.
<u>134</u>	<u>98</u>	<u>76</u>	<u>38</u>	<u>85</u>	<u>99</u>	

+7.4

N.G.	100	114	111	112	104	N.G.
<u>143</u>	<u>107</u>	<u>46</u>	<u>97</u>	<u>83</u>	<u>100</u>	

+6.9

N.G.	103	112	113	108	116	103
<u>160</u>	<u>127</u>	<u>100</u>	<u>54</u>	<u>29</u>	<u>67</u>	

+6.8

N.G.	106	112	114	114	114	106
<u>166</u>	<u>148</u>	<u>100</u>	<u>43</u>	<u>35</u>	<u>62</u>	

189.84

7 + 75

184.6

8 + 00

T.P. 10.14 189.68 0.30 189.59

7 + 25

+50

+75

8 + 00

96.2

+25

95.6

+50

95.2

T.P. 5.23 202.83 2.08 197.60

B.M. 3.81 199.02 198.99

10.3

N.G.	38	53	66	64	52	54
162	48	122	100	50	36	

+ 8.7

N.G.	48	62	61
158	143	100	69

+ 02.9

26	N.G.
81	110

+ 2.0

28	N.G.
74	110

+ 0.4

38	N.G.
59	100

- 1.2

30	35	50	37	N.G.
14	22	57	100	

- 2.1

N.G.	41	19	22	41	43	16	N.G.
165	100	87	93		20	66	100

- 2.8

N.G.	35	27	44	50	13	N.G.
170	100	60	23	63	100	

Spt in 14" Oak

