

Book # 82 - Dr # 8

LAKE JOHANNA
LAKE VALENTINE WATERWAY

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed **9-22-30**

File No.

1-31-30

Locations of Shore line
on
No. End Lake Johanna
and
So. End Lake Valentine.

+50

3

+50

2

+50

1

+50

0+00

+50

1

1

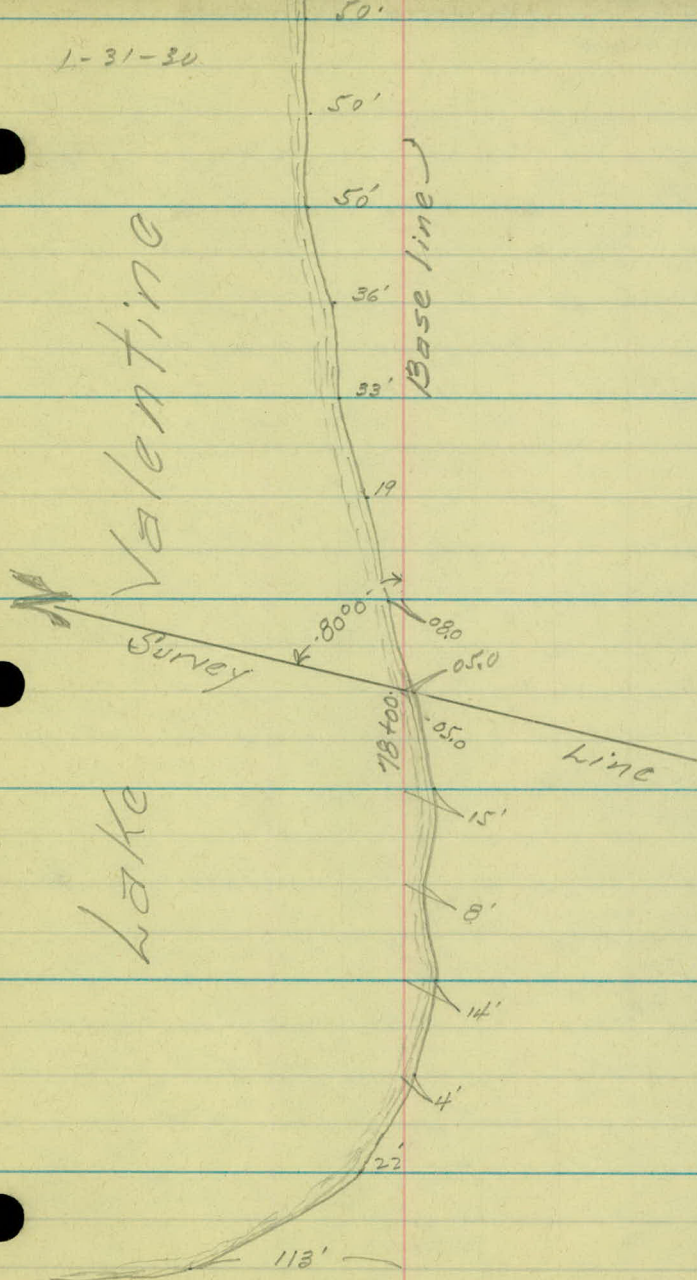
+50

2

+50

3

1-31-30



+50

3

+50

2

+50

1

+50

0+00

+50

1

+50

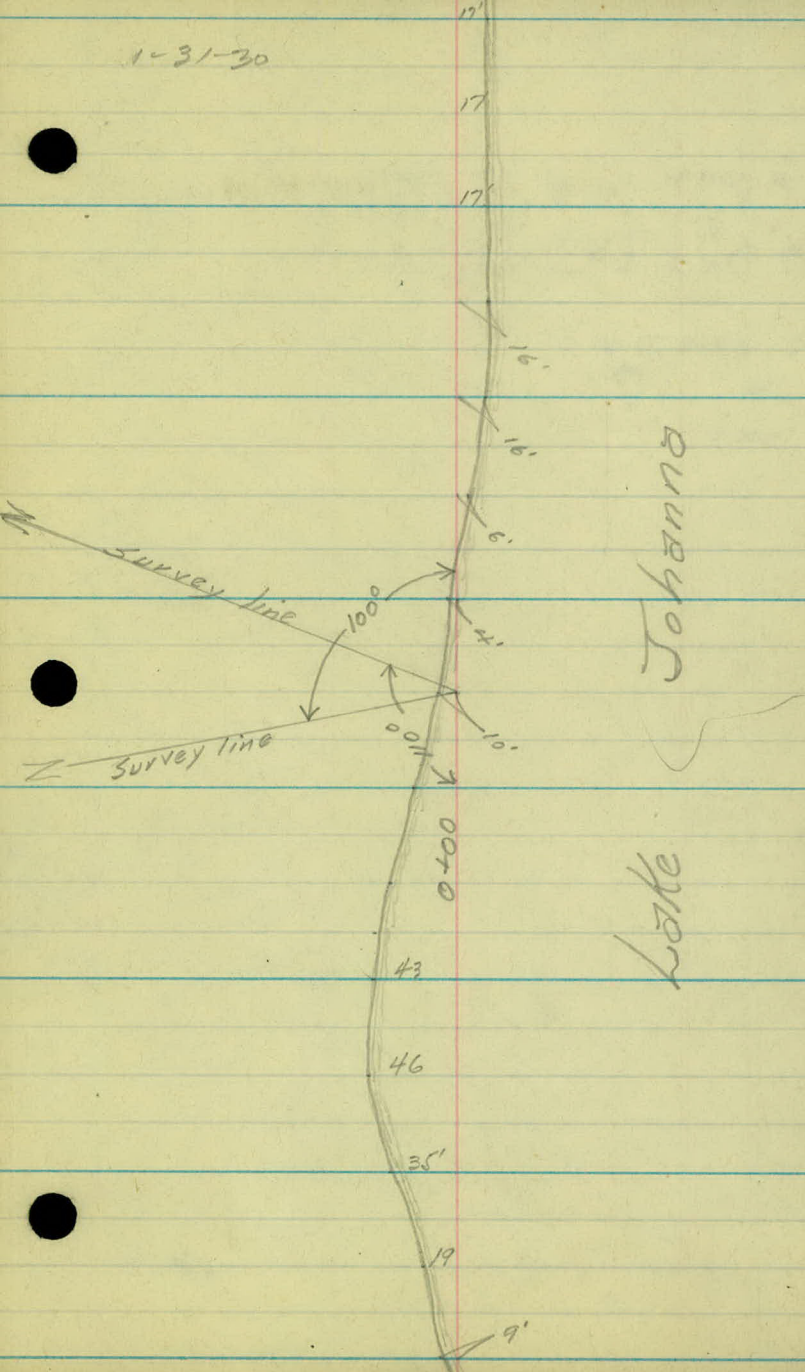
2

+50

3

+50

1-31-30



1-31-30

{ $\angle$ of Bridges = $17+05.0$
} Δ To Tracks = $89^{\circ}17'$ from
Fwd. Tan.

Clear + Cold.

1-20-30

A Weber

Beaton

Skogland

Bell

Location

Transit

Survey

Lake Johanna To Lake Valentine.

Sta. Point Δ Lt. Δ R.

9+06.64
9+07.0 # 4 16° 14'

139.54
7+67.1
7+67.4 # 3 52° 30'

177.63
5+89.47
5+89.7 # 2 15° 30'

198.83
3+90.64
3+90.8 # 1 53° 30'

283.68
1+06.96
1+07.0 P.O.T.

0+00 # 0

1-20-30 Clear and Cold.

Spike

Spike

Spike

Spike

24" Hard Map

6.15

10" Oak side ties.

6.22

R.R. spike

£ Johanna Blvd.

Water Gauge.

No. End Lake Johanna.

Sta. Point Δ Lt R/L Δ

19+19.84
19+20.6 #10 $80^{\circ}52'$

164.34

17+51.50 ✓
17+56.2 #9 $42^{\circ}00'$

17+05.4988 ✓
17+06.2 P.O.T.

16+23.80
16+24.45 #8 $29^{\circ}14'$

167.18 ✓
14+56.62
14+57.2 #7 $25^{\circ}05'$

222.51 ✓
12+34.11
12+34.6 #6 $45^{\circ}40'$

188.13 ✓
11+97.31 Int. of So. line Sec 28-30-23.

10+45.98
10+46.4 #5 $33^{\circ}30'$

139.24 ✓

1-20-30 Clear + Cold.

Spike

Spike

Under Seoline trestle.

Spike

Spike

Spike

So. $\frac{1}{4}$ cor. Sec. 28-30-23

Spike

1-23-30

29°55'

Spike

Sta. Number Δ Lt Δ Rt.

35+85.37 #16 50°00'

323.18 ✓

32+62.19 #15 41°50'

283.95 ✓

29+78.24 #14 55°00'

141.13

28+37.11 ✓
~~28+38.25~~ ✓ #13 54°30'

26+181.52 ✓
26+155.59
~~26+56.65~~ #12 55°00'

363.80 ✓
22+91.77
~~22+92.2~~ #11 25°00'

371.95 ✓

Clear & Cold. 1-20-30

o = spike

spike

spike

spike

spike

spike

spike

Sta.

$\Delta L.$ $\Delta R.$

47+95.31 #22

56°34'

100.72

46+94.59 #21

53°12'

Draw To Valentine.

143.39

45+51.2 #20

33°36'

43+42.90 Int. of E and W $\frac{1}{4}$ line Sec. 28-30-23

43+02.16 #19

80°54'

401.16

39+01.0 #18

22°56'

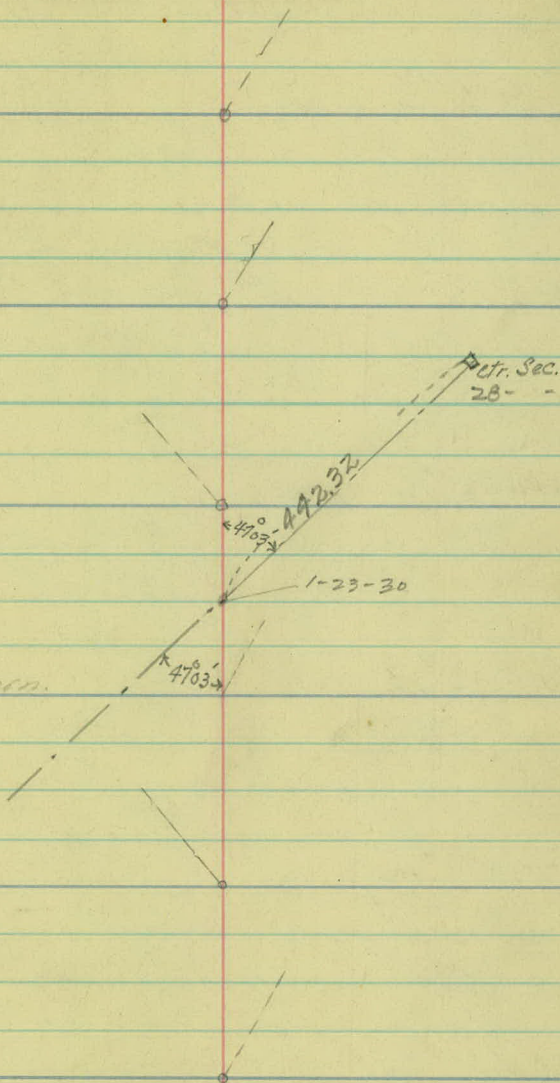
167.0

37+34.0 #17

45°22'

148.63

1-21-30 Cold + Clear



Sta.

ΔL ΔR

$65 + 27.94 \# 28$

$56^{\circ} 48'$

138.17

$63 + 81.77 \# 27$

$12^{\circ} 54'$

277.85 ✓

$61 + 11.92 \# 26$

$66^{\circ} 44'$

217.04 ✓

$58 + 94.88 \# 25$

$9^{\circ} 40'$

308.68 ✓

$55 + 86.2 \# 24$

$23^{\circ} 14'$

500.7 ✓

$50 + 85.5 \# 23$

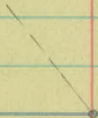
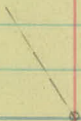
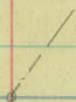
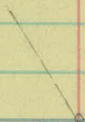
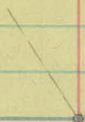
$40^{\circ} 10'$

290.19

Cold + Clear

1-21-30

o = spike.



Sta.

ΔL $\Delta Rt.$

77+95.0 Edge of Ice So. Shore Lake Valentine.

74+42.32 Int. E + W $\frac{1}{4}$ line Sec. 28-30-23

74+08.70 So. Edge of Pav. Anoka Cutoff.

74+08.60 P.O.T.

73+31.0 #30 44° 10'

468.1

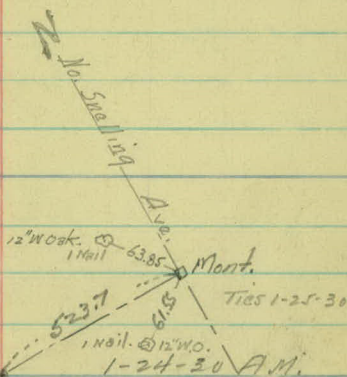
68+62.70 #29 7° 26'

334.96

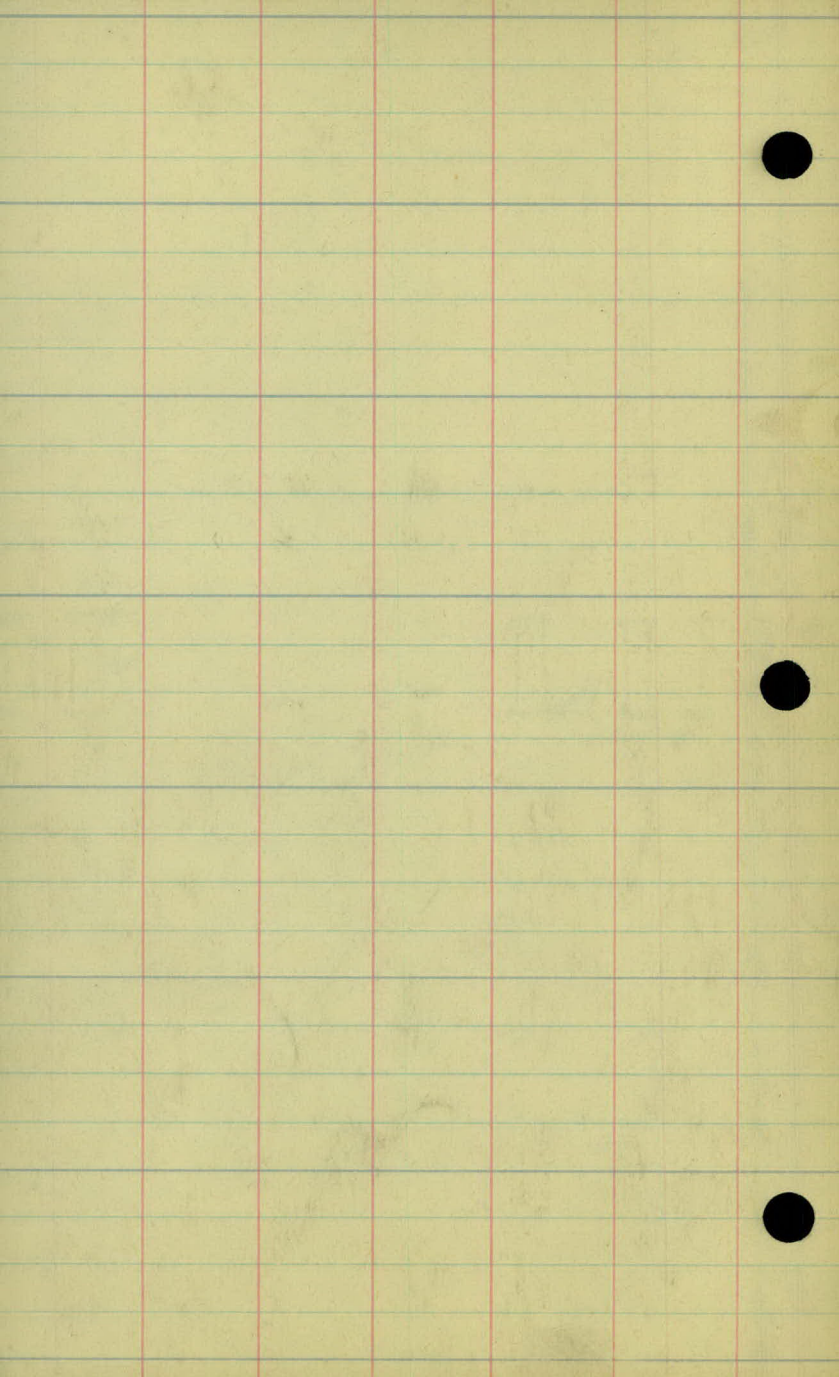
1-22-30

Clear & Cold.

E. $\frac{1}{4}$ cor. Sec. 28.



spike at Edge of Pave.



* Weber
Beaton
Stooglan
Bell.

Cross Section.

Sta. 0+00 To Sta. 77+95

Jan. 1930

Lake Johanna To

Lake Valentine.

Sta. + H.I. - Elev

888.78

0.69 889.47 ✓ 10.74 78.73 ✓

3.64 882.37

0+00 = Water Gauge No. End Lake Johanna.

+ 10 Shore line

+ 50

+ 68 Toe of Slope.

T.R. 10.73 889.46 ✓ 3.64 878.73 ✓

+ 72

+ 86 Toe of Shoulder.

+ 94 Top of Shoulder.

1+07. ± Road (Johanna Blvd.)

+ 21 Top of Shoulder.

+ 25 Toe of Shoulder.

+ 52

Lt.

E

R4

Cold + Snow 1-24-30 P.M.

spike in 20" Oak St. cor Refractory No. End Lake
Johanna.

$$\begin{array}{r} 7.7 \\ 50 \\ \hline 74.7 \end{array} \quad \begin{array}{r} 7.8 \\ 25 \\ \hline 74.6 \end{array} \quad \begin{array}{r} 7.8 \\ 25 \\ \hline 74.6 \end{array} \quad \begin{array}{r} 7.8 \\ 25 \\ \hline 74.6 \end{array} \quad \begin{array}{r} 7.5 \\ 50 \\ \hline 74.9 \end{array}$$

$$\begin{array}{r} 7.3 \\ 50 \\ \hline 75.1 \end{array} \quad \begin{array}{r} 7.6 \\ 25 \\ \hline 74.8 \end{array} \quad \begin{array}{r} 7.5 \\ 25 \\ \hline 74.9 \end{array} \quad \begin{array}{r} 7.4 \\ 25 \\ \hline 75.0 \end{array} \quad \begin{array}{r} 7.1 \\ 50 \\ \hline 75.1 \end{array}$$

$$\begin{array}{r} 5.9 \\ 50 \\ \hline 76.5 \end{array} \quad \begin{array}{r} 5.9 \\ 25 \\ \hline 76.5 \end{array} \quad \begin{array}{r} 5.9 \\ 25 \\ \hline 76.5 \end{array} \quad \begin{array}{r} 5.8 \\ 25 \\ \hline 76.6 \end{array} \quad \begin{array}{r} 5.5 \\ 50 \\ \hline 76.9 \end{array}$$

$$\begin{array}{r} 3.8 \\ 50 \\ \hline 85.7 \end{array} \quad \begin{array}{r} 4.5 \\ 35 \\ \hline 85.0 \end{array} \quad \begin{array}{r} 4.5 \\ 17 \\ \hline 85.0 \end{array} \quad \begin{array}{r} 4.5 \\ 25 \\ \hline 85.0 \end{array} \quad \begin{array}{r} 4.0 \\ 25 \\ \hline 85.5 \end{array} \quad \begin{array}{r} 1.0 \\ 35 \\ \hline 88.5 \end{array} \quad \begin{array}{r} 0.5 \\ 50 \\ \hline 89.0 \end{array}$$

$$\begin{array}{r} 9.4 \\ 50 \\ \hline 80.1 \end{array} \quad \begin{array}{r} 10.2 \\ 34 \\ \hline 79.3 \end{array} \quad \begin{array}{r} 11.0 \\ 14 \\ \hline 78.5 \end{array} \quad \begin{array}{r} 8.5 \\ 7 \\ \hline 81.0 \end{array} \quad \begin{array}{r} 8.4 \\ 4 \\ \hline 81.1 \end{array} \quad \begin{array}{r} 8.8 \\ 10 \\ \hline 80.7 \end{array} \quad \begin{array}{r} 9.8 \\ 22 \\ \hline 79.7 \end{array} \quad \begin{array}{r} 8.0 \\ 50 \\ \hline 81.5 \end{array} \quad \begin{array}{r} 7.4 \\ 50 \\ \hline 82.1 \end{array}$$

$$\begin{array}{r} 8.0 \\ 50 \\ \hline 81.5 \end{array} \quad \begin{array}{r} 7.6 \\ 33 \\ \hline 81.9 \end{array} \quad \begin{array}{r} 7.6 \\ 17 \\ \hline 81.9 \end{array} \quad \begin{array}{r} 7.6 \\ 20 \\ \hline 81.9 \end{array} \quad \begin{array}{r} 6.4 \\ 20 \\ \hline 83.1 \end{array} \quad \begin{array}{r} 3.7 \\ 37 \\ \hline 85.8 \end{array} \quad \begin{array}{r} 3.3 \\ 50 \\ \hline 86.3 \end{array}$$

$$\begin{array}{r} 7.4 \\ 50 \\ \hline 82.1 \end{array} \quad \begin{array}{r} 7.0 \\ 25 \\ \hline 82.5 \end{array} \quad \begin{array}{r} 5.2 \\ 7 \\ \hline 84.3 \end{array} \quad \begin{array}{r} 4.4 \\ 25 \\ \hline 85.1 \end{array} \quad \begin{array}{r} 3.4 \\ 27 \\ \hline 86.1 \end{array} \quad \begin{array}{r} 2.6 \\ 50 \\ \hline 86.9 \end{array}$$

$$\begin{array}{r} 4.6 \\ 50 \\ \hline 84.9 \end{array} \quad \begin{array}{r} 4.1 \\ 25 \\ \hline 85.4 \end{array} \quad \begin{array}{r} 3.6 \\ 25 \\ \hline 85.9 \end{array} \quad \begin{array}{r} 3.2 \\ 25 \\ \hline 86.3 \end{array} \quad \begin{array}{r} 2.9 \\ 50 \\ \hline 86.6 \end{array}$$

$$\begin{array}{r} 4.6 \\ 50 \\ \hline 84.9 \end{array} \quad \begin{array}{r} 4.3 \\ 24 \\ \hline 85.7 \end{array} \quad \begin{array}{r} 4.2 \\ 19 \\ \hline 85.3 \end{array} \quad \begin{array}{r} 4.8 \\ 19 \\ \hline 84.7 \end{array} \quad \begin{array}{r} 4.2 \\ 38 \\ \hline 85.3 \end{array} \quad \begin{array}{r} 4.0 \\ 50 \\ \hline 85.5 \end{array}$$

$$\begin{array}{r} 4.8 \\ 50 \\ \hline 84.7 \end{array} \quad \begin{array}{r} 4.7 \\ 33 \\ \hline 84.8 \end{array} \quad \begin{array}{r} 4.8 \\ 14 \\ \hline 84.7 \end{array} \quad \begin{array}{r} 5.6 \\ 21 \\ \hline 85.9 \end{array} \quad \begin{array}{r} 5.1 \\ 21 \\ \hline 85.5 \end{array} \quad \begin{array}{r} 4.0 \\ 50 \\ \hline 85.5 \end{array}$$

$$\begin{array}{r} 7.2 \\ 50 \\ \hline 82.3 \end{array} \quad \begin{array}{r} 7.2 \\ 38 \\ \hline 82.3 \end{array} \quad \begin{array}{r} 7.1 \\ 15 \\ \hline 82.4 \end{array} \quad \begin{array}{r} 7.6 \\ 21 \\ \hline 81.9 \end{array} \quad \begin{array}{r} 7.0 \\ 21 \\ \hline 82.5 \end{array} \quad \begin{array}{r} 6.3 \\ 31 \\ \hline 83.7 \end{array} \quad \begin{array}{r} 4.7 \\ 42 \\ \hline 84.8 \end{array} \quad \begin{array}{r} 4.5 \\ 50 \\ \hline 85.0 \end{array}$$

889.46

Elev.

1 + 80

2

+ 50

T.P.

2.79 883.18 ✓ 9.07 880.39 ✓

3

+ 33 So. Side of Ditch

+ 42 E Ditch

+ 49 No. Side of Ditch

+ 56

3.49 883.88 ✓ 2.79 880.39 ✓

+ 90 $\Delta 1$

4

+ 50 = Note = All elev. on Rt of E from
Sta. 4+50 to Sta. 18+50 (inc) were taken
with Hand level.

5

+ 50

23.4 880.28 ✓ 5.94 877.94 ✓

1-24-30 Lt

Cold-Snow.

9.4	9.0	10.0	9.8	9.0	7.2	2.5
<u>50</u>	<u>31</u>	<u>18</u>	<u>11</u>	<u>25</u>	<u>50</u>	
80.1	80.5	77.5	79.7	80.5	82.3	87.0

10.2	10.7	9.7	8.0	5.8	2.7	
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<u>50</u>	<u>21</u>	<u>18</u>	<u>33</u>	<u>50</u>		
79.3	78.8	79.8	81.5	83.7	86.8	

11.8	11.8	11.5	10.2	8.6	6.2	
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<u>50</u>	<u>26</u>	<u>21</u>	<u>35</u>	<u>50</u>		
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77.7	77.7	78.0	79.3	80.9	83.3	
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6.8	7.0	7.0	6.6	5.6	4.8	
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<u>50</u>	<u>25</u>	<u>22</u>	<u>45</u>	<u>50</u>		
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76.4	76.2	76.2	76.6	77.6	78.4	
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7.7	7.2	6.6	7.0	7.0	8.0	8.0	6.6
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<u>50</u>	<u>25</u>	<u>21</u>	<u>32</u>	<u>38</u>	<u>45</u>	<u>50</u>	
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75.5	76.0	76.6	76.2	76.2	75.2	75.2	76.6
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10.0	10.0	10.0	10.0	9.7	9.0	8.2	
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<u>50</u>	<u>42</u>	<u>21</u>	<u>20</u>	<u>40</u>	<u>50</u>		
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73.2	73.2	73.2	73.2	73.5	74.2	75.0	
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8.0	8.0	7.0	7.0	7.5	8.0	7.6	
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<u>50</u>	<u>28</u>	<u>13</u>	<u>11</u>	<u>18</u>	<u>50</u>		
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75.2	75.2	76.2	76.2	75.7	75.2	76.6	
------	------	------	------	------	------	------	--

8.6	8.2	7.2	6.8	6.4	5.4	5.4	7.4
-----	-----	-----	-----	-----	-----	-----	-----

<u>50</u>	<u>31</u>	<u>17</u>	<u>14</u>	<u>30</u>	<u>46</u>	<u>50</u>	
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75.3	75.7	76.7	77.1	77.5	78.5	78.5	76.5
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1-25-30

Very Cold

-20

9.2	9.0	8.5	8.0	6.5	5.9	5.7	3.5	3.1	3.1
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<u>100</u>	<u>75</u>	<u>50</u>	<u>36</u>	<u>9</u>	<u>10</u>	<u>27</u>	<u>45</u>	<u>50</u>	
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74.7	74.9	75.4	75.9	77.4	78.0	78.8	80.4	80.8	80.8
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Ditch

9.0	8.8	10.5	10.5	9.0	9.0	7.8	5.8	4.7	3.5	2.0
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<u>100</u>	<u>77</u>	<u>72</u>	<u>65</u>	<u>61</u>	<u>50</u>	<u>25</u>	<u>15</u>	<u>25</u>	<u>50</u>	
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74.9	75.1	75.4	75.4	74.9	74.4	76.1	78.1	79.2	80.4	81.9
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Ditch

9.5	9.5	11.4	11.2	9.4	9.2	9.0	7.8	6.6	+0.7	+3.4	+7.0
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<u>110</u>	<u>103</u>	<u>100</u>	<u>98</u>	<u>95</u>	<u>50</u>	<u>42</u>	<u>12</u>	<u>6</u>	<u>25</u>	<u>50</u>	
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74.4	74.4	75.5	72.7	74.5	74.7	74.9	76.1	77.3	78.0	80.7	84.3
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9.4	9.8	9.5	10.0	9.1	7.2	+5.4	+9.3				
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<u>100</u>	<u>82</u>	<u>68</u>	<u>50</u>	<u>22</u>	<u>31</u>	<u>50</u>					
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70.1	72.1	74.4	72.4	74.8	76.7	82.1	86.0				
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10.6	10.0	9.6	9.5	9.0	7.5	+3.0	+5.4	+12.0			
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<u>100</u>	<u>75</u>	<u>50</u>	<u>29</u>	<u>14</u>	<u>18</u>	<u>28</u>	<u>50</u>				
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75.3	73.9	74.3	74.4	74.9	76.4	79.4	81.8	88.4			
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spike in 16" W.O. 3' Rt. Sta. 5+15

880.28

6

+50

7

+50

8

T.P.

3.97 878.29 ✓ 6.00 874.28 ✓ 874.32

+50

9

+50

10

+50

11

+50

12

T.P.

4.85 879.17 ✓ 3.97 874.32 ✓

1-27-30 AM. Lt $\neq$ R4

Snowing

7.0	6.7	6.2	6.4	5.2	3.6	+3.0	+5.4	+15.5
<u>100</u>	<u>70</u>	<u>50</u>	<u>40</u>	<u>76</u>	<u>15</u>	<u>21</u>	<u>50</u>	
73.3	72.6	74.1	73.9	75.1	76.7	79.7	82.1	92.2

7.2	7.2	6.6	6.8	6.1	5.4	3.7	+2.8	+5.4	+18.0
<u>100</u>	<u>77</u>	<u>65</u>	<u>50</u>	<u>32</u>	<u>18</u>	<u>14</u>	<u>22</u>	<u>50</u>	
72.1	72.1	72.7	73.5	74.2	74.9	76.6	79.4	82.0	94.6

7.2	7.2	8.5	8.5	7.2	7.2	7.3	6.6	5.3	3.6	+1.2	+5.4	+16.4
<u>100</u>	<u>103</u>	<u>100</u>	<u>95</u>	<u>92</u>	<u>70</u>	<u>50</u>	<u>38</u>	<u>15</u>	<u>17</u>	<u>22</u>	<u>50</u>	
73.1	73.1	71.8	73.1	73.1	73.0	73.7	75.0	76.7	77.9	82.1	93.1	

7.0	7.5	8.7	8.8	7.5	7.7	7.0	6.0	3.5	+2.9	+5.4	+11.2
<u>100</u>	<u>82</u>	<u>80</u>	<u>77</u>	<u>75</u>	<u>50</u>	<u>29</u>	<u>76</u>	<u>20</u>	<u>30</u>	<u>50</u>	
73.3	72.8	71.5	71.5	72.8	72.6	73.2	74.3	76.8	78.7	82.2	88.0

8.0	8.2	9.2	9.0	8.0	8.2	7.4	6.8	5.6	3.7	+2.0	+5.4	+11.6
<u>100</u>	<u>96</u>	<u>84</u>	<u>82</u>	<u>80</u>	<u>68</u>	<u>50</u>	<u>34</u>	<u>15</u>	<u>28</u>	<u>50</u>		
71.3	71.1	71.5	71.5	72.3	72.1	72.1	74.5	74.7	76.6	78.6	82.0	86.7

6.5	6.9	6.2	5.7	4.6	3.7	1.8	2.0	+5.4	+17.0
<u>100</u>	<u>88</u>	<u>69</u>	<u>50</u>	<u>34</u>	<u>18</u>	<u>11</u>	<u>20</u>	<u>50</u>	
71.8	71.4	71.1	72.6	72.7	74.6	76.5	78.5	81.9	93.5

7.0	6.5	5.8	5.3	3.6	2.2	0.2	+5.4	+10.8	+16.2	+23.3
<u>100</u>	<u>75</u>	<u>50</u>	<u>41</u>	<u>24</u>	<u>9</u>	<u>7</u>	<u>20</u>	<u>37</u>	<u>50</u>	
71.3	71.8	72.5	73.0	74.7	76.1	78.1	83.5	88.9	94.3	96.4

6.8	6.6	6.2	5.3	3.8	1.4	+1.8	+5.4	+12.4	+17.8	+22.8
<u>100</u>	<u>72</u>	<u>50</u>	<u>33</u>	<u>21</u>	<u>8</u>	<u>17</u>	<u>30</u>	<u>40</u>	<u>50</u>	
71.5	71.7	72.1	73.0	74.5	76.9	78.7	82.3	89.3	94.7	99.7

6.8	6.7	5.8	5.0	4.0	1.0	+1.6	+5.4	+12.5	+17.9	+22.5
<u>100</u>	<u>75</u>	<u>50</u>	<u>34</u>	<u>22</u>	<u>7</u>	<u>17</u>	<u>31</u>	<u>41</u>	<u>50</u>	
71.5	71.6	72.7	73.2	74.2	77.3	78.9	82.7	89.8	95.2	99.8

6.8	6.5	5.8	5.2	3.8	+0.2	+5.4	+12.5	+17.9	+20.9
<u>100</u>	<u>75</u>	<u>50</u>	<u>40</u>	<u>26</u>	<u>15</u>	<u>30</u>	<u>43</u>	<u>50</u>	
71.5	71.8	72.7	73.1	74.5	78.5	83.9	91.0	96.4	99.4

7.0	6.8	6.0	5.4	4.4	1.8	+2.0	+5.4	+13.6
<u>100</u>	<u>70</u>	<u>50</u>	<u>33</u>	<u>16</u>	<u>12</u>	<u>25</u>	<u>50</u>	
71.3	71.5	72.3	72.9	73.9	76.5	78.5	81.9	90.1

7.1	7.0	6.0	5.6	4.8	2.1	+2.4	+5.4	+12.0	+15.4
<u>100</u>	<u>73</u>	<u>50</u>	<u>39</u>	<u>24</u>	<u>12</u>	<u>19</u>	<u>36</u>	<u>50</u>	
71.2	71.3	71.3	72.7	73.5	76.2	78.5	81.6	88.2	91.6

6.0	6.6	8.0	7.8	6.6	6.0	5.0	3.6	1.4	+2.4	+5.4	12.5	17.9
<u>110</u>	<u>100</u>	<u>96</u>	<u>93</u>	<u>92</u>	<u>70</u>	<u>50</u>	<u>24</u>	<u>11</u>	<u>19</u>	<u>43</u>	<u>60</u>	

72.3	71.7	70.3	70.5	72.3	73.3	74.7	76.9	79.3	82.3	89.4	94.8
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12

879.17

+34⁶ Δ Pt.

(Back Tan)

+50

13

+50

T.P. 5.73 878.77 ✓ 6.13 873.04 ✓

14

+57 Δ Pt.

(Back Tan)

+57 Δ Pt.

(Fwd. Tan)

15

+50

16

+24 Δ Pt.

(Back Tan)

+24 Δ Pt.

(Fwd. Tan)

T.P. 8.70 881.75 ✓ 5.72 873.05 ✓

+50 Toe at So. side of Fill Pt.

Smearing Lt £ Rt = all plus readings

71.6 72.1 73.1
 76 71 78 87 87 77 70 65 5.8 4.5 33 + 2.4 + 5.4 + 12.4 + 15.2
 100 81 85 84 81 79 71 50 36 15 14 24 50 60
 70.5 71.5 72.2 72.7 73.4 74.7 75.9 78.3 81.3 88.3 91.1

75 80 88 88 75 75 6.6 5.8 5.2 4.4 2.8 + 5.4 + 10.0 + 12.4 + 17.8
 70 85 84 82 81 70 50 34 20 13 17 31 43 64
 71.7 71.2 70.4 70.4 71.7 71.7 72.6 73.4 74.0 74.8 76.4 81.8 86.4 88.8 94.2

7.4 7.7 6.8 6.2 5.4 3.1 + 5.4 + 12.5 + 17.9 + 21.9
 100 75 50 33 18 14 30 45 60
 71.8 71.5 72.1 73.0 73.8 76.1 81.5 88.6 94.0 98.0

8.2 7.8 6.8 6.2 5.0 3.0 + 5.4 + 5.4 + 12.5 + 17.9
 100 75 50 33 16 11 15 32 50
 71.0 71.4 72.4 73.0 74.2 76.2 79.6 81.6 88.7 94.1

7.2 7.0 6.5 5.8 4.8 1.9 + 5.4 + 5.4 + 12.5 + 16.9
 100 70 50 35 16 9 14 22 36 50
 71.6 71.8 72.3 73.0 74.0 76.9 80.1 82.3 85.3 89.4 93.6

7.3 7.5 6.7 5.8 3.0 + 5.0 + 5.4 + 12.5 + 17.5
 100 72 50 23 11 16 33 50
 71.5 71.3 72.1 73.0 75.8 78.8 81.2 88.3 93.3

7.2 7.0 6.5 6.0 5.2 3.0 + 3.0 + 5.4 + 12.5 + 14.7
 100 72 50 34 16 14 21 40 50
 71.6 71.8 72.3 72.8 73.6 75.8 78.8 81.2 88.3 90.2

7.8 7.0 7.0 6.4 5.9 + 2.9 + 4.0 + 12.5 + 17.9
 100 75 50 23 29 37 58 82
 71.0 71.8 71.8 71.4 72.9 75.8 76.9 85.4 90.8

9.4 8.7 7.2 7.2 6.8 6.5 6.2 + 0.6 + 3.2 + 5.4 + 12.5
 100 76 50 42 38 22 25 58 72 97
 69.6 70.1 71.6 71.6 72.0 72.3 73.6 75.8 78.0 85.1

9.5 9.4 8.7 7.4 6.6 + 1.6 + 2.9 + 5.4 + 7.0 + 12.5
 100 75 50 22 37 50 81 93 120 113
 69.2 69.4 70.1 71.4 72.2 73.8 75.1 77.6 79.2 84.7

Edge Ice. → 9.6 9.5 9.2 8.2 7.5 7.7 + 2.2 + 5.4 + 12.4 + 17.9 + 25.0 + 33.4
 88 72 50 37 15 31 44 65 79 96 115
 69.2 69.3 69.6 70.6 71.3 71.7 73.3 76.5 82.5 89.0 96.1 904.5

" → 9.5 9.4 8.2 7.4 7.4 7.7 + 1.6 + 4.5 + 12.5
 70 47 37 39 15 35 85 108
 69.3 69.4 70.6 71.4 71.4 71.1 72.7 75.6 83.6

12.5 12.4 11.6 9.8 10.4 10.4 10.8 4.4 5.4 7.4 9.5
 Ice. 60 44 38 29 22 12 26 33 53 93
 69.3 69.4 70.2 71.0 71.0 71.1 74.2 75.8 76.8 78.8 80.9

881.75

16+80 So. shoulder of R.R. Fill on Rt.

17 E of Fill under Trestle. on Rt.

+25 No. Shoulder of R.R. Fill on Rt.

+56 $\Delta F4$ Toe at No. side of Fill. Rt.

18

+50

T.P. 9.49 887.26 ~~1398~~ 877.77 ✓

19

+20 $\Delta F4$

(Back Tan.)

+20 $\Delta F4$

(Fwd Tan.)

20

+50

21

+50

Top = 1000

Ice + 12.5 11.0 92 72 62 + 12.5 + 19.6 + 23.5 + 24.4
66 50 18 5 19 31 50 51
 69.3 70.8 70.6 74.6 75.6 88.1 95.2 99.1 head trail 100.0

Ice + 12.5 105 88 76 + 12.5 + 19.6 + 20.6 + 20.6 + 24.6
65 50 28 — 22 37 41 55 55
 69.3 71.3 73.0 74.8 91.7 98.8 99.8 99.8 103.8

Ice + 12.5 113 97 76 40 + 12.5 + 17.9 + 20.7 + 22.5
65 50 28 13 — 24 32 40 59
 69.3 70.5 72.1 74.8 77.8 90.2 95.7 98.5 100.3

(Back Ten.) Ice. 12.5 120 115 105 92 + 2.0 + 5.4 + 9.6 + 12.5
73 50 41 22 — 19 38 88 103
 69.3 69.8 70.3 71.3 72.6 74.6 78.0 82.2 85.1

112 102 96 90 82 + 2.4 + 5.4 + 6.7 + 12.5 31.4 31.4
100 70 50 26 — 27 43 50 64 109 135
 70.6 71.6 72.2 72.8 73.6 76.0 79.0 80.3 81.1 90.0 95.0

91 88 85 82 76 60 + 1.4 + 5.4 + 9.8
100 75 50 30 11 12 30 71
 72.7 73.0 73.3 73.6 74.8 75.8 77.2 81.2 85.6

Wye level

125 118 105 94 86 90 72
50 39 20 — 21 40 50
 70.8 71.5 72.8 77.9 78.7 78.9 80.1

100 92 90 90 90
50 24 — 21 50
 77.3 78.1 78.3 78.3 78.3

90 8.0 7.2
— 26 50
 78.3 79.3 80.1

145 140 138 128 9.9 7.4 4.2
100 75 46 27 — 20 50
 72.8 73.3 73.5 74.5 77.5 79.9 82.1

156 148 142 140 128 9.9 3.4 2.0
100 75 50 34 18 — 34 50
 71.7 72.5 73.1 73.3 74.5 77.4 83.9 85.3

163 152 147 140 135 10.0 2.8 2.5
100 75 50 33 17 — 35 50
 71.0 72.1 72.6 72.3 73.6 77.3 81.5 80.8

162 154 145 133 125 10.3 4.7 4.5
100 75 50 18 8 — 29 50
 71.1 71.9 72.8 74.0 74.8 77.0 82.6 82.8

X Sections on R.L. from Sta. 1400 to Sta. 22 + 50 (incl) were taken with Wye level

887.26

22

+50

3.25 880.20 ✓ 10.31

876.95 ✓

+91.79 Δ 124

(Back Tan.)

23 { - Note - Readings on Rt. from Sta.
22 + 91.79 to Sta. 50+00 were taken with -
- Hand level }

+50

24

+50

25

+50

26

+50 Δ Pt.

(Back Tan.)

+56 " "

(Fwd. Tan.)

27

1-28-30

Lt

£

Tt.

164	155	146	138	102	47	43	45	55
<u>100</u>	<u>75</u>	<u>41</u>	<u>16</u>		<u>28</u>	<u>41</u>	<u>50</u>	<u>70</u>
70.9	71.8	71.7	71.5	72.1	82.6	83.0	82.8	81.8

160	154	147	132	101	63	47	42	34
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71.3	<u>100</u>	<u>75</u>	<u>34</u>	<u>20</u>	17.2	81.3	<u>41</u>	<u>50</u>	<u>70</u>
Top spike	71.9	54.5	53.2	51.7	77.7				

Hand Level.

90	86	77	64	3.2	+5.4	+7.7
<u>100</u>	<u>80</u>	<u>50</u>	<u>27</u>		<u>42</u>	<u>65</u>
71.2	71.6	72.5	73.8	77.0	82.4	84.7

90	80	73	68	52	3.0	+5.4	+6.2	Fence
<u>100</u>	<u>75</u>	<u>50</u>	<u>39</u>	<u>20</u>		<u>40</u>	<u>67</u>	
71.2	71.2	72.9	73.4	75.0	77.2	82.6	83.4	

88	78	60	47	2.8	+5.4	+7.4	+8.4	Fence
<u>100</u>	<u>77</u>	<u>50</u>	<u>27</u>		<u>40</u>	<u>60</u>	<u>75</u>	
71.4	72.4	74.1	75.5	77.4	82.8	84.8	85.8	

88	77	70	67	4.0	+5.4	+9.4
<u>100</u>	<u>79</u>	<u>50</u>	<u>33</u>		<u>33</u>	<u>59</u>
71.4	72.5	73.2	73.5	76.2	82.1	86.1

92	87	82	76	66	4.1	+5.4	+12.5
<u>100</u>	<u>75</u>	<u>50</u>	<u>35</u>	<u>14</u>		<u>24</u>	<u>50</u>
71.0	71.5	72.0	72.6	73.6	76.1	81.5	88.6

92	90	85	80	66	4.2	+5.4	+16.4
<u>100</u>	<u>75</u>	<u>50</u>	<u>36</u>	<u>18</u>		<u>19</u>	<u>50</u>
71.0	71.2	71.7	72.2	73.6	76.0	81.4	92.4

90	88	87	74	3.3	+5.4	+12.5	+14.5
<u>100</u>	<u>75</u>	<u>50</u>	<u>30</u>		<u>17</u>	<u>41</u>	<u>50</u>
71.2	71.2	71.5	72.8	76.9	82.3	89.4	91.4

Ditch

90	110	110	90	85	80	65	3.0	+5.4	+8.4	+10.7
<u>104</u>	<u>102</u>	<u>100</u>	<u>98</u>	<u>75</u>	<u>50</u>	<u>27</u>		<u>17</u>	<u>31</u>	<u>50</u>
71.2	69.2	69.2	71.2	71.7	72.2	73.7	77.2	82.6	85.6	87.9

92	92	108	108	85	84	77	62	4.2	+4.2	+5.4	+7.4
<u>100</u>	<u>78</u>	<u>95</u>	<u>92</u>	<u>87</u>	<u>75</u>	<u>50</u>	<u>26</u>		<u>50</u>	<u>61</u>	<u>75</u>
71.0	71.0	69.0	69.0	71.7	71.8	72.5	74.0	76.0	80.2	81.4	83.4

86	75	66	53	1.8	+3.4	+5.4	+11.4
<u>100</u>	<u>75</u>	<u>50</u>	<u>25</u>		<u>35</u>	<u>45</u>	<u>79</u>
71.6	72.7	73.6	74.9	78.4	81.8	83.8	89.8

86	80	62	46	3.0	+2.6	+5.4	+12.5
<u>100</u>	<u>78</u>	<u>50</u>	<u>27</u>		<u>25</u>	<u>40</u>	<u>78</u>
71.6	71.2	71.0	75.6	77.2	79.8	82.6	89.7

880.20

+50

T.P. 5.43 881.38 ✓ 4.25 875.95 ✓

28

+37⁰ Δ Pt

(Back Tan.)

29

+78 Δ Pt.

(Back Tan.)

+78 Δ "

(Fwd. Tan.)

30

+50

+77

T.P. 9.50 885.56 ✓ 5.32 876.06 ✓

31

+39

Top Hump

(Back Tan.)

32

+62 Δ Pt.

(Back Tan.)

1-28-30

Lt

L

Rt.

9.0 7.8 6.2 4.6 1.1 +5.4 +12.5
 71.2 100 71.175 50 38 79.1 37 79
 Top of Stake 24.2 27.0

10.3 9.4 8.1 6.0 2.2 +5.4 +11.6
 100 77 50 31 34 75
 71.1 71.0 73.3 75.1 79.2 84.6 90.8

10.2 9.5 8.0 5.5 2.6 +5.4 +11.4
 100 80 50 29 30.4.2 65-90.6
 71.4 71.9 73.2 75.9 78.8 +1.4 +5.4 +9.4 (Furd Tan.)

10.7 10.2 9.5 8.6 6.6 +3.7 +5.4 +9.4
 100 78 50 23 35 44 70
 70.7 71.2 70.7 72.8 74.8 78.5 79.2 81.8

11.0 11.0 10.0 9.4 8.4 +5.4 +7.8
 100 77 50 29 49 75
 70.4 70.4 71.4 72.0 73.0 98.4 80.8

9.5 9.4 9.1 8.9 8.4 +3.2 +5.0
 100 75 50 29 42 67
 71.9 72.0 72.2 72.5 73.0 76.2 76.0

8.0 8.4 8.0 7.7 6.6 +3.0 +4.4 +7.6
 100 77 50 26 36 50 75
 72.4 73.0 73.4 73.7 74.8 77.8 79.2 82.4

4.1 4.5 5.0 4.4 3.7 1.8 +3.2 +6.0
 100 76 50 25 37 50 75
 77.3 76.9 76.4 77.0 77.7 79.5 82.1 83.0

0.4 1.0 2.5 3.2 2.3 +0.6 +2.4 +4.7
 100 78 50 25 28 50 75
 81.0 80.4 78.9 78.2 79.1 79.7 81.5 83.8

2.4 3.0 4.2 4.8 4.3 +1.4 +2.9 +3.5
 100 75 50 25 28 50 75
 83.2 82.6 81.4 80.8 80.3 82.7 83.2 84.8

0.8 2.0 2.8 3.3 2.4 0.7 +2.0 +3.4 +3.4
 100 75 50 40 21 30 75
 84.8 83.6 82.8 82.3 83.2 84.9 86.9 88.3 88.3

7.5 8.5 9.3 9.2 8.8 6.7 +5.4 +11.0
 100 76 50 32 14 22 45
 78.1 77.1 76.3 76.4 76.8 78.9 84.3 89.9

12.5 12.4 11.8 10.7 8.5 +2.4 +4.1 +5.4 +12.5
 100 77 50 29 11 27 31 52
 73.1 73.2 73.8 74.9 77.1 79.5 81.2 82.5 89.6

885.56

+62 ΔP_4

(Fwd. Tan.)

33

+50

34

+50

35

+50

+85 ΔP_4

(Back Tan.)

+85 " "

(Fwd. Tan.)

36+50

37

+34

(Back Tan.)

+34

(Fwd. Tan.)

T.P.

5.60

880.72

✓ 10.44

875.12

✓

1-28-30

Lt

L

Rt

7.7	9.7	11.7	10.7	8.5	+2.0	+3.8	+5.4	+12.5
<u>100</u>	<u>77</u>	<u>50</u>	<u>26</u>	<u>8</u>		<u>30</u>	<u>37</u>	<u>60</u>
72.9	75.9	73.9	74.9	77.1	79.1	76.9	77.5	89.6

9.2	10.7	12.1	12.1	11.7	9.0	+1.4	+2.6	+4.0	+12.5
<u>100</u>	<u>80</u>	<u>64</u>	<u>50</u>	<u>35</u>	<u>11</u>	<u>17</u>	<u>40</u>	<u>72</u>	
76.4	74.9	73.5	73.5	73.9	76.6	79.0	79.2	81.0	89.1

12.5	12.5	12.7	11.5	8.8	+2.4	+4.1	+4.7	+12.5
<u>100</u>	<u>81</u>	<u>50</u>	<u>25</u>	<u>18</u>		<u>24</u>	<u>32</u>	<u>67</u>
73.1	73.1	72.9	74.1	76.8	79.2	80.9	81.5	89.3

14.0	13.3	12.5	11.1	7.4	+3.9	+4.7	+8.4	+10.0	12.5
<u>100</u>	<u>75</u>	<u>50</u>	<u>27</u>	<u>15</u>	<u>26</u>	<u>31</u>	<u>41</u>	<u>50</u>	
71.6	72.3	73.1	74.5	78.2	82.1	82.9	81.3	88.2	90.7

15.0	14.4	13.5	12.5	9.1	+5.4	+8.6	+15.2	+16.2	+17.8
<u>100</u>	<u>75</u>	<u>50</u>	<u>31</u>	<u>18</u>	<u>31</u>	<u>40</u>	<u>44</u>	<u>50</u>	
70.6	71.2	72.1	73.1	76.5	81.9	85.1	91.7	92.7	94.3

15.4	15.0	14.2	12.5	9.5	2.4	+5.4	+10.0	+14.9	+17.5
<u>100</u>	<u>75</u>	<u>50</u>	<u>27</u>	<u>15</u>	<u>25</u>	<u>42</u>	<u>47</u>	<u>60</u>	
70.2	70.6	71.4	73.1	76.1	78.5	81.5	86.1	91.0	93.6

15.0	14.5	13.8	12.0	9.1	+4.9	+12.5	+12.6		
<u>100</u>	<u>75</u>	<u>50</u>	<u>22</u>	<u>23</u>	<u>41</u>	<u>50</u>			
70.6	71.1	71.8	73.6	76.5	81.4	87.0	89.1		

14.0	13.0	11.8	10.6	7.2	+5.4	+12.5	+15.9		
<u>100</u>	<u>75</u>	<u>50</u>	<u>35</u>	<u>20</u>	<u>39</u>	<u>51</u>			
71.6	72.6	73.8	75.0	78.4	83.8	90.9	94.3		

14.7	14.2	12.8	10.6	7.2	+5.4	+12.5	+16.9		
<u>100</u>	<u>75</u>	<u>50</u>	<u>28</u>	<u>18</u>	<u>40</u>	<u>58</u>			
70.9	71.4	72.8	75.0	78.4	83.8	90.9	95.3		

15.4	14.8	13.2	11.2	7.6	+5.4	+12.5	+16.9		
<u>100</u>	<u>80</u>	<u>50</u>	<u>25</u>	<u>18</u>	<u>40</u>	<u>57</u>			
70.2	70.8	72.2	74.2	78.0	77.4	84.5	94.9		

15.2	14.8	13.8	12.2	8.7	+5.4	+12.5	+17.5		
<u>100</u>	<u>75</u>	<u>50</u>	<u>25</u>	<u>19</u>	<u>38</u>	<u>52</u>			
70.4	70.2	71.8	72.4	76.9	82.3	89.4	94.4		

15.2	15.2	14.5	14.0	10.7	+5.4	+12.5	+16.3		
<u>100</u>	<u>80</u>	<u>50</u>	<u>23</u>	<u>29</u>	<u>51</u>	<u>61</u>			
70.9	70.7	71.7	71.6	74.9	80.3	87.4	91.2		

14.7	15.2	14.6	13.8	12.8	10.7	+5.4	+12.5	+16.2	
<u>100</u>	<u>75</u>	<u>50</u>	<u>46</u>	<u>16</u>	<u>26</u>	<u>47</u>	<u>59</u>		

Top of spike Sta. 37 + 34.00 74.9 80.3 87.4 91.1

70.9 70.4 71.0 71.8 72.8 74.9

880.72

38

+50

39+01 ΔPt.

(Back Tan. only)

+50

40

11

+50

41

+50

42

+50

43+02.16 ΔPt

(Back Tan.)

" " " " "

(Fwd. Tan.)

T.P. 8.04 883.05 ✓ 5.71 \$75.01 ✓

+50

E + W 1/4 line Sec 26.

1-29-30

ht

L

Rt

$$\begin{array}{r} 100 \\ 100 \\ 70.7 \end{array} \quad \begin{array}{r} 100 \\ 75 \\ 70.7 \end{array} \quad \begin{array}{r} 90 \\ 50 \\ 71.7 \end{array} \quad \begin{array}{r} 74 \\ 25 \\ 73.3 \end{array} \quad \begin{array}{r} 4.5+5.4 \\ 76.1 \\ 81.6 \end{array} \quad \begin{array}{r} +12.5 \\ 37 \\ 88.7 \end{array} \quad \begin{array}{r} +17.9 \\ 52 \\ 94.1 \end{array}$$

$$\begin{array}{r} 101 \\ 100 \\ 70.6 \end{array} \quad \begin{array}{r} 99 \\ 70 \\ 71.8 \end{array} \quad \begin{array}{r} 90 \\ 50 \\ 71.7 \end{array} \quad \begin{array}{r} 65 \\ 20 \\ 71.2 \end{array} \quad \begin{array}{r} 3.5+5.4 \\ 77.2 \\ 82.6 \end{array} \quad \begin{array}{r} +12.5 \\ 17 \\ 89.7 \end{array} \quad \begin{array}{r} +17.9 \\ 50 \\ 93.1 \end{array}$$

$$\begin{array}{r} 100 \\ 100 \\ 70.7 \end{array} \quad \begin{array}{r} 9.5 \\ 78 \\ 71.2 \end{array} \quad \begin{array}{r} 8.3 \\ 50 \\ 72.4 \end{array} \quad \begin{array}{r} 7.8 \\ 41 \\ 72.9 \end{array} \quad \begin{array}{r} 5.5 \\ 21 \\ 75.2 \end{array} \quad \begin{array}{r} 1.8+5.4 \\ 78.9 \\ 84.3 \end{array} \quad \begin{array}{r} +12.5 \\ 30 \\ 91.4 \end{array} \quad \begin{array}{r} +17.9 \\ 48 \\ 96.8 \end{array}$$

$$\begin{array}{r} 103 \\ 100 \\ 70.4 \end{array} \quad \begin{array}{r} 95 \\ 75 \\ 71.2 \end{array} \quad \begin{array}{r} 85 \\ 50 \\ 72.2 \end{array} \quad \begin{array}{r} 72 \\ 30 \\ 73.5 \end{array} \quad \begin{array}{r} 3.2+5.4 \\ 77.5 \\ 82.9 \end{array} \quad \begin{array}{r} +12.5 \\ 18 \\ 90.0 \end{array} \quad \begin{array}{r} +17.9 \\ 42 \\ 95.4 \end{array} \quad \begin{array}{r} +20.2 \\ 52 \\ 97.7 \end{array}$$

$$\begin{array}{r} 106 \\ 100 \\ 70.1 \end{array} \quad \begin{array}{r} 92 \\ 75 \\ 71.5 \end{array} \quad \begin{array}{r} 86 \\ 50 \\ 72.1 \end{array} \quad \begin{array}{r} 70 \\ 25 \\ 73.7 \end{array} \quad \begin{array}{r} 3.8+5.4 \\ 76.9 \\ 82.3 \end{array} \quad \begin{array}{r} +12.5 \\ 18 \\ 89.4 \end{array} \quad \begin{array}{r} +17.9 \\ 48 \\ 94.8 \end{array}$$

$$\begin{array}{r} 108 \\ 100 \\ 69.9 \end{array} \quad \begin{array}{r} 95 \\ 75 \\ 71.2 \end{array} \quad \begin{array}{r} 86 \\ 50 \\ 72.1 \end{array} \quad \begin{array}{r} 72 \\ 25 \\ 73.5 \end{array} \quad \begin{array}{r} 3.7+5.4 \\ 77.0 \\ 82.4 \end{array} \quad \begin{array}{r} +12.5 \\ 17 \\ 89.5 \end{array} \quad \begin{array}{r} +17.9 \\ 47 \\ 94.9 \end{array}$$

$$\begin{array}{r} 101.5 \\ 100 \\ 70.2 \end{array} \quad \begin{array}{r} 92 \\ 79 \\ 71.5 \end{array} \quad \begin{array}{r} 86 \\ 50 \\ 72.1 \end{array} \quad \begin{array}{r} 70 \\ 25 \\ 73.7 \end{array} \quad \begin{array}{r} 4.0+5.4 \\ 76.7 \\ 82.1 \end{array} \quad \begin{array}{r} +12.5 \\ 17 \\ 89.2 \end{array} \quad \begin{array}{r} +17.9 \\ 43 \\ 94.6 \end{array} \quad \begin{array}{r} +20.3 \\ 56 \\ 97.0 \end{array}$$

$$\begin{array}{r} 107 \\ 100 \\ 70.0 \end{array} \quad \begin{array}{r} 9.6 \\ 76 \\ 71.1 \end{array} \quad \begin{array}{r} 8.7 \\ 50 \\ 72.0 \end{array} \quad \begin{array}{r} 82 \\ 36 \\ 72.5 \end{array} \quad \begin{array}{r} 6.5 \\ 22 \\ 74.2 \end{array} \quad \begin{array}{r} 3.2+5.4 \\ 77.5 \\ 82.9 \end{array} \quad \begin{array}{r} +12.5 \\ 34 \\ 85.0 \end{array} \quad \begin{array}{r} +17.9 \\ 45 \\ 95.4 \end{array} \quad \begin{array}{r} +23.1 \\ 60 \\ 900.6 \end{array}$$

$$\begin{array}{r} 102 \\ 100 \\ 70.5 \end{array} \quad \begin{array}{r} 84 \\ 50 \\ 72.5 \end{array} \quad \begin{array}{r} 4.0+5.4 \\ 76.7 \\ 82.1 \end{array} \quad \begin{array}{r} +12.5 \\ 22 \\ 89.2 \end{array} \quad \begin{array}{r} +17.9 \\ 43 \\ 94.6 \end{array}$$

$$\begin{array}{r} 102 \\ 100 \\ 70.5 \end{array} \quad \begin{array}{r} 82 \\ 50 \\ 72.5 \end{array} \quad \begin{array}{r} 4.4+4.0 \\ 76.3 \\ 80.3 \end{array} \quad \begin{array}{r} +5.4 \\ 26 \\ 81.7 \end{array} \quad \begin{array}{r} +9.6 \\ 30 \\ 85.9 \end{array} \quad \begin{array}{r} +11.6 \\ 50 \\ 87.9 \end{array}$$

$$\begin{array}{r} 100 \\ 100 \\ 70.7 \end{array} \quad \begin{array}{r} 8.5 \\ 50 \\ 72.2 \end{array} \quad \begin{array}{r} 5.8 \\ 72.4 \end{array}$$

$$\begin{array}{r} 108 \\ 100 \\ 70.7 \end{array} \quad \begin{array}{r} 80 \\ 50 \\ 72.2 \end{array} \quad \begin{array}{r} 5.8 \\ 72.4 \end{array}$$

Top Spike 54.2, 43 + 02.16 70.9

$$\begin{array}{r} 127 \\ 100 \\ 70.4 \end{array} \quad \begin{array}{r} 106 \\ 50 \\ 64.5 \end{array} \quad \begin{array}{r} 8.8 \\ 36 \\ 73 \end{array} \quad \begin{array}{r} 5.5+5.4 \\ 77.6 \\ 83.0 \end{array} \quad \begin{array}{r} 80 \\ 36 \\ 85.6 \end{array} \quad \begin{array}{r} 11.2 \\ 50 \\ 88.8 \end{array}$$

883.05

44

+50

45

+51.2 Δ Ft.

(Back Turn)

46

+50

+9.4 Δ Ft.

(Back Turn)

+9.4 Δ Ft.

(Fwd Turn)

47+25

Δ Ft in Ditch

B.M.

1.21

882.41

1.92

881.13

881.20

+50

+60

Elev of Bottom of Ditch on Δ = 871.6

+80

48

48+50

{ Hand level used on Lt and Rt.
From Sta. 47+50 To 50+00 (inc) }

1-30-30 L R.

12.2 10.2 5.8 +5.4 +10.0 +12.5 +14.7
100 50 24 41 51 63
 70.9 72.9 77.3 82.7 87.3 89.8 92.0

11.6 9.2 6.0 +5.4 +12.0
100 50 23 50
 71.5 73.9 77.1 82.5 89.1

9.7 9.0 5.2 +5.4 +10.2
100 50 23 50
 73.4 74.1 77.9 83.3 88.1

8.5 8.5 6.8 4.4 +5.4 +12.5
100 50 20 20 50
 74.6 74.6 76.3 78.7 84.1 91.2

8.3 8.3 8.3 6.2 +2.0 +5.4 +12.5 +17.9
100 50 32 15 26 46 59
 74.8 75.8 74.8 76.9 78.9 82.3 89.4 94.8

Ditch

104 80.4 134 134 97 8.1 8.0 6.7 5.7 +1.7 +5.4 +11.8 +16.2
100 75 72 68 64 58 50 15 15 31 50 70
 72.7 72.7 69.7 69.7 73.4 75.0 75.1 76.1 77.1 79.1 82.8 89.2 95.6

Ditch

90 75 10.2 11.7 11.7 10.2 7.2 6.1
100 85 72 50 40 38 14
 74.1 75.6 77.9 76.4 76.4 77.9 75.9 77.0

Ditch

4.7 6.0 6.8 4.6 12.2 12.2 9.2 6.1
84 64 50 21 19 17 14
 78.4 77.1 76.2 73.5 70.9 70.9 77.9 77.0

Ditch

30 30 75 80 11.5 11.5 8.2 5.8 +5.4 +9.7 +12.5
93 89.7 75.6 75.1 32 71.6 74.8 77.3 18 38 58
 spike 10 24 83.4 70.1 +5.4 47 +2 82.7 87.2 89.8

Ditch

+60 +5.0 +0.7 0.0 -3.6 -1.8 6.7 +2.0 +5.4 +9.8 +12.5
58 47 37 21.0 13.0 9.0 75.0 14.3 24.1 45.5 53.4
 88.4 87.4 83.1 10.8 49.4 +5.4 +3.8 44.7 +5.4 82.7 87.2 89.8
 60 42 33 14. 24 86 64
 +8.0 +5.4 +1.0 6.6 +0.4 -1.6 -3.8 -1.2
54 24 8 21 41 47 52
 90.4 87.8 83.1 75.8

Ditch

+90 +20 1.6 -4.6 -5.0 -6.0 9.0 -5.0 +3.9
46 12 8 21 30 35 41 80
 91.4 90.4 90.8 76.2 75.8 74.2 71.8 75.8 84.7

+12.9 +12.5 +10.2 +5.4 4.8 -0.8 -3.6 -5.2 -3.0 +10 +14
52 30 16 7 12 26 30 34 50 62
 90.3 94.9 97.6 87.8 77.6 76.8 74.0 72.1 71.6 78.6 83.0

882.41

49

+50

50

T.P.

7.56

886.59

✓ 3.38

879.03

✓

+50

Δ 7.56 Lt

51

+50

52

+50

53

+50

54

+50

T.P.

6.24

884.45

✓ 8.38

878.21

✓

55

{ Wye level used at Lt from
Sta. 50+50 to 54
incl. }

1-30-30

Lt

E

Rt

+23.9 +17.4 42.5 +5.4 +1.2 6.2 +0.4 -1.6 -3.6 -1.0 +1.4 +1.5
57 33 25 16 10 7 20 25 29 37 65
 906.3 99.8 94.9 87.8 83.6 76.7 76.6 74.6 72.6 75.2 77.6 88.7

+17.1 +16.3 12.5 +4.4 +3.0 5.7 -0.4 -4.0 -4.0 +0.9 +2.9 -1.0
60 53 37 21 10 21 27 33 36 50 68
 99.5 98.7 94.9 86.8 85.4 76.7 76.3 72.7 72.7 77.6 79.6 86.7

+12.5 +11.0 +5.4 +3.6 4.2 -1.8 -2.6 -5.6 -5.6 -3.6 -3.6 -0.5
84.9 93.4 98.8 39 27 78.2 7 23 26 30 32 50 76
 F.P. 300 No. 04. Sec 26. Mont 86.0 76.4 75.6 72.6 72.6 74.6 76.1 77.7

14 38 65 85 9.8 11.4 10.4 13.7 10.4 90.85
50 37 19 8 36 54 64 68 80 100
 85.7 82.8 80.1 78.1 76.8 75.7 76.7 72.9 76.7 77.6 78.1

38 50 6.4 9.3 10.7 11.8 13.5 14.0 12.9 12.5
50 40 21 25 50 91 75 100 110
 87.8 81.6 80.7 77.3 76.9 74.8 73.1 73.6 73.7 72.1

31 4.9 8.5 12.1 12.7 Ditch 130 ft.
50 21 50 100
 83.5 81.7 78.1 74.5 73.9

33 5.1 6.6 7.6 8.9 10.5 11.9 12.8
50 42 22 13 25 50 100
 82.3 81.5 80.0 79.0 77.7 76.1 74.7 73.8

2.5 5.3 6.7 8.8 10.6 11.6 12.7
50 38 23 25 50 100
 84.1 81.3 79.9 77.8 76.0 75.0 73.9

2.5 5.9 7.0 8.6 10.3 11.6 12.6
50 36 18 25 50 100
 84.1 80.7 79.6 78.0 76.3 75.0 74.0

5.2 6.3 7.7 9.2 10.4 11.6 12.9
50 40 19 25 50 100
 81.4 81.3 78.9 77.5 76.7 75.0 73.7

5.5 7.4 8.0 9.7 11.0 11.6 13.0
50 31 19 25 50 100
 81.1 79.7 78.6 76.9 75.6 75.0 73.6

5.5 7.1 8.1 9.6 11.0 11.7 13.2
50 32 18 25 50 100
 81.1 79.5 78.5 76.6 75.6 74.9 73.4

Top Stake

38 5.6 7.5 8.8 9.6 10.7 11.5
50 24 25 50 75 100

80.7 78.9 77.0 75.7 75.4 73.8 73.0

E 190 Swamp

884.45

+50

56

+50

57

+50

58

50

59

+50

60

+50

61

61 + 11.92

Fred Tan

1-30-30

L1

L2

L3

<u>3.9</u>	<u>5.8</u>	<u>7.3</u>	<u>8.4</u>	<u>9.2</u>	<u>11.3</u>
50	25	25	25	50	100
80.6	78.7	77.7	76.1	75.3	72.2

<u>3.2</u>	<u>5.5</u>	<u>7.1</u>	<u>8.5</u>	<u>9.3</u>	<u>11.2</u>
50	22	25	25	50	100
81.3	79.0	77.6	76.0	75.2	73.3

<u>4.0</u>	<u>6.0</u>	<u>7.4</u>	<u>8.5</u>	<u>8.9</u>	<u>11.4</u>
50	25	25	25	50	100
80.5	78.5	77.1	76.0	75.6	73.1

<u>3.7</u>	<u>5.4</u>	<u>6.7</u>	<u>8.2</u>	<u>9.2</u>	<u>11.0</u>
50	25	25	25	50	100
80.8	79.1	77.8	76.3	75.3	73.5

<u>2.9</u>	<u>4.1</u>	<u>5.0</u>	<u>7.0</u>	<u>8.0</u>	<u>9.2</u>	<u>10.6</u>
50	38	25	25	25	50	100
81.6	80.5	79.5	77.5	76.5	75.3	73.9

<u>3.7</u>	<u>5.6</u>	<u>7.3</u>	<u>8.5</u>	<u>9.5</u>	<u>9.7</u>	<u>10.6</u>
50	25	25	25	50	75	100
80.9	78.9	77.7	76.0	75.1	74.8	73.9

<u>3.7</u>	<u>5.0</u>	<u>6.6</u>	<u>7.5</u>	<u>8.8</u>	<u>9.7</u>	<u>10.4</u>
74	50	25	25	25	50	100
80.8	79.5	77.9	77.0	75.7	74.8	74.1

<u>2.9</u>	<u>4.8</u>	<u>6.3</u>	<u>7.4</u>	<u>8.8</u>	<u>9.8</u>	<u>10.4</u>
74	50	25	25	25	50	100
81.6	79.7	78.7	77.1	75.7	74.7	74.1

<u>2.7</u>	<u>4.2</u>	<u>6.6</u>	<u>7.5</u>	<u>9.0</u>	<u>10.0</u>	<u>10.4</u>
62	50	25	25	25	50	100
81.8	80.3	77.9	77.0	75.5	73.5	74.1

<u>2.5</u>	<u>4.4</u>	<u>5.9</u>	<u>7.6</u>	<u>9.0</u>	<u>10.1</u>	<u>10.0</u>
62	50	25	25	25	50	100
81.0	80.1	78.6	76.9	75.5	74.4	73.5

<u>3.2</u>	<u>4.3</u>	<u>6.3</u>	<u>7.7</u>	<u>8.9</u>	<u>9.8</u>	<u>10.0</u>
62	50	25	25	25	50	100
81.3	80.2	78.7	76.8	75.6	74.7	73.5

<u>3.7</u>	<u>4.5</u>	<u>5.9</u>	<u>7.6</u>	<u>8.6</u>	<u>9.3</u>	<u>9.7</u>
62	50	25	25	25	50	100
80.8	80.0	78.6	76.9	75.4	75.2	74.8

<u>5.8</u>	<u>6.1</u>	<u>7.0</u>	<u>7.5</u>
65	50	25	25
78.7	78.4	77.5	77.0

884.45

+50

62

+50

63

+50

64

+50

65

T.P.

+50

8.30

885.47

7.28

877.17

66

+50

67

+60

on £

1-30-30

Lt

L

Rt.

61	6.5	8.0	8.6	9.5	9.6	9.8
<u>62</u>	<u>50</u>	<u>25</u>		<u>25</u>	<u>50</u>	<u>100</u>
78.4	78.0	74.6	75.9	78.0	74.9	74.7

49	5.9	7.9	9.0	9.6	9.9
<u>50</u>	<u>25</u>		<u>25</u>	<u>50</u>	<u>100</u>
79.6	78.6	76.6	75.6	74.9	74.6

4.0	5.4	6.9	8.5	9.7	9.9
<u>50</u>	<u>15</u>		<u>25</u>	<u>50</u>	<u>100</u>
80.5	79.1	77.6	76.0	74.8	74.6

3.7	5.4	7.1	8.4	9.3	9.5
<u>50</u>	<u>17</u>		<u>25</u>	<u>50</u>	<u>100</u>
80.8	79.1	77.4	76.1	75.2	75.0

3.2	4.0	5.1	7.2	8.3	9.2	8.5
<u>62</u>	<u>50</u>	<u>25</u>		<u>25</u>	<u>50</u>	<u>100</u>
81.3	80.5	79.4	77.3	76.2	75.3	76.0

2.9	4.8	5.8	7.4	7.9	8.2	7.7
<u>75</u>	<u>50</u>	<u>25</u>		<u>25</u>	<u>50</u>	<u>100</u>
81.6	79.7	78.7	77.1	76.6	76.4	76.8

4.4	5.7	6.1	6.8	7.7	8.5	9.0	9.3
<u>75</u>	<u>50</u>	<u>29</u>		<u>25</u>	<u>50</u>	<u>75</u>	<u>75</u>
84.1	78.8	78.4	77.7	76.8	76.0	75.5	75.2

62	70	72	76	80	9.2	9.7
<u>75</u>	<u>50</u>	<u>20</u>		<u>25</u>	<u>50</u>	<u>100</u>
78.2	75.5	75.0	74.9	74.9	75.3	75.8

Top of spike

54.5 63+89

1-31-30

7.2	8.0	8.8	9.6	10.2	10.5	12.0	9.6	9.7
<u>75</u>	<u>50</u>	<u>25</u>		<u>25</u>	<u>50</u>	<u>52</u>	<u>58</u>	<u>100</u>
78.3	77.5	76.7	75.9	75.3	74.8	73.5	75.9	75.8

Ditch

6.6	8.2	8.8	9.2	9.3	9.8	11.4	11.4	9.2	9.2
<u>75</u>	<u>50</u>	<u>25</u>		<u>25</u>	<u>37</u>	<u>38</u>	<u>41</u>	<u>45</u>	<u>100</u>
78.9	77.3	76.7	76.0	76.2	75.7	74.1	74.1	76.3	76.3

Ditch

5.4	7.2	8.2	8.5	8.5	10.7	10.7	9.0	8.2	8.0
<u>75</u>	<u>50</u>	<u>25</u>		<u>21</u>	<u>25</u>	<u>28</u>	<u>33</u>	<u>50</u>	<u>100</u>
80.1	78.3	77.3	77.0	77.0	74.8	74.8	76.5	77.3	77.5

Ditch

4.6	6.0	7.2	7.0	7.1	10.1	11.1	11.1	7.7	8.1	7.0
<u>75</u>	<u>50</u>	<u>25</u>		<u>3</u>	<u>8</u>	<u>11</u>	<u>13</u>	<u>18</u>	<u>50</u>	<u>100</u>
80.9	79.5	78.2	78.5	78.4	78.4	74.4	74.4	77.8	77.4	78.5

7.1

78.4

885.47

+18

Bottom Ditch on L

"

+46

"

+50

68

+23

+63 $\Delta P +$

(Back Ten)

69

+50

70

+50

T.F

702

884.82

✓ 7.67

877.80

✓

71

+50

72

1-31-30

Snowing

11.1

74.4

11.0

74.5

Ditch											
32	56	66	66	9.0	11.0	11.0	7.0	6.1	7.5	6.1	
75	50	34	8		4	6	10	76	50	100	
82.5	79.9	78.9	78.9	76.5	74.5	74.5	78.5	79.4	78.0	74.4	
Ditch											
40	46	4.7	6.2	6.7	10.5	10.5	7.4	5.2	5.3		
75	50	25		14	21	23	27	40	100		
81.5	80.9	80.8	79.3	78.8	75.0	75.0	78.1	80.2	80.2		
Ditch											
4.0	5.4	7.2	8.2	8.4	7.7	10.5	10.5	8.1	6.8	4.2	4.7
75	59	45	25		18	22	24	26	50	62	100
81.5	80.1	78.3	77.3	77.1	77.8	75.2	76.3	77.0	78.7	81.3	80.8
Ditch											
33	4.0	6.5	8.2	8.7	10.1	10.1	8.7	8.0	5.0		
75	50	25		23	26	28	31	50	100		
82.2	81.5	79.0	77.3	76.8	75.4	75.4	76.8	77.5	80.5		
Ditch											
3.5	5.4	6.8	8.0	8.7	10.2	10.2	9.5	8.0			
75	50	25		31	36	38	40	100			
82.0	80.1	78.7	77.5	76.8	75.3	75.3	76.0	77.5			
Ditch											
5.4	6.6	7.0	7.7	8.7	8.8	10.0	10.5	9.1	9.2		
75	50	25		25	44	46	49	50	100		
80.1	78.9	78.5	77.8	76.8	76.7	75.5	75.1	76.4	76.3		
Ditch											
7.5	8.0	8.3	8.8	9.0	9.2	9.2	10.2	10.2	9.4	9.4	
75	50	25		25	50	53	55	58	60	100	
78.0	77.5	77.2	76.7	76.5	76.3	76.3	76.3	76.3	76.1	76.1	
Ditch											
7.7	8.8	9.2	9.2	9.0	9.0	10.7	10.7	9.6	9.7		
77.8	75	50	25	50	63	66	68	70	100		
Top Stake	74.0	74.0	74.7	76.3	76.3	76.7	76.7	74.8	74.8	75.9	75.8
Ditch											
6.5	8.1	8.6	8.4	8.8	8.6	10.0	10.0	9.0	9.2		
75	50	25		50	73	75	77	80	100		
78.3	76.7	76.2	76.4	76.0	76.2	74.8	74.6	75.8	75.6		
Ditch											
5.7	7.2	8.3	8.6	8.6	8.6	9.8	9.8	9.0	8.7		
75	50	25		50	85	87	89	92	100		
79.1	77.6	76.5	76.2	76.2	76.2	75.0	75.0	75.8	76.1		
Ditch											
4.2	6.0	4.0	8.3	8.6	8.1	9.8	9.8	8.6	8.6		
75	50	25		50	95	96	97	102	110		
80.6	78.8	77.8	76.5	76.2	76.7	75.0	75.0	76.2	76.2		

884.82

+50

73

+31

$\Delta P4$

(Back Ton)

+76

Toe Slope.

5.39

879.43

✓

+81

+90

Toe Shoulder

8.28

887.71

✓

5.39

879.43

✓

74 + 03.0

Top Shoulder.

+08.8

So Edge pave

+22.3

$\neq$ Pave.

+35.8

No. Edge Pave.

+42

Top Shoulder

+53

Toe Shoulder

+62

Top Ditch Rt.

1-21-30

R/

$$\begin{array}{r} 3.8 \\ \hline 75 \\ 80.0 \end{array} \quad \begin{array}{r} 5.3 \\ \hline 50 \\ 79.5 \end{array} \quad \begin{array}{r} 6.8 \\ \hline 25 \\ 76.0 \end{array} \quad \begin{array}{r} 8.0 \\ \hline 50 \\ 76.8 \end{array} \quad \begin{array}{r} 8.7 \\ \hline 50 \\ 76.1 \end{array} \quad \begin{array}{r} 8.4 \\ \hline 100 \\ 76.4 \end{array}$$

$$\begin{array}{r} 4.4 \\ \hline 75 \\ 80.4 \end{array} \quad \begin{array}{r} 5.4 \\ \hline 50 \\ 79.5 \end{array} \quad \begin{array}{r} 6.8 \\ \hline 25 \\ 76.0 \end{array} \quad \begin{array}{r} 8.3 \\ \hline 50 \\ 76.5 \end{array} \quad \begin{array}{r} 8.5 \\ \hline 50 \\ 76.3 \end{array} \quad \begin{array}{r} 8.7 \\ \hline 100 \\ 76.1 \end{array}$$

$$\begin{array}{r} 4.4 \\ \hline 75 \\ 80.4 \end{array} \quad \begin{array}{r} 6.2 \\ \hline 50 \\ 78.6 \end{array} \quad \begin{array}{r} 7.4 \\ \hline 25 \\ 77.4 \end{array} \quad \begin{array}{r} 8.5 \\ \hline 50 \\ 76.3 \end{array} \quad \begin{array}{r} 8.5 \\ \hline 100 \\ 76.3 \end{array}$$

$$\begin{array}{r} 5.0 \\ \hline 50 \\ 79.8 \end{array} \quad \begin{array}{r} 6.2 \\ \hline 25 \\ 78.6 \end{array} \quad \begin{array}{r} 8.5 \\ \hline 50 \\ 76.3 \end{array} \quad \begin{array}{r} 8.5 \\ \hline 50 \\ 76.3 \end{array}$$

$$\begin{array}{r} 4.4 \\ \hline 50 \\ 80.4 \end{array} \quad \begin{array}{r} 5.8 \\ \hline 25 \\ 79.0 \end{array} \quad \text{Culvert} \quad \begin{array}{r} 5.8 \\ \hline 50 \\ 79.0 \end{array}$$

$$\begin{array}{r} 3.8 \\ \hline 50 \\ 79.0 \end{array} \quad \begin{array}{r} 4.2 \\ \hline 25 \\ 80.6 \end{array} \quad \begin{array}{r} 5.6 \\ \hline 50 \\ 79.2 \end{array} \quad \begin{array}{r} 5.3 \\ \hline 50 \\ 79.5 \end{array}$$

Top Culvert Sta 73+00

$$\begin{array}{r} 1.3 \\ \hline 100 \\ 86.4 \end{array} \quad \begin{array}{r} 1.3 \\ \hline 50 \\ 86.4 \end{array} \quad \begin{array}{r} 1.9 \\ \hline 50 \\ 85.8 \end{array} \quad \begin{array}{r} 2.7 \\ \hline 50 \\ 85.0 \end{array} \quad \begin{array}{r} 2.9 \\ \hline 100 \\ 80.8 \end{array}$$

$$\begin{array}{r} 1.55 \\ \hline 50 \\ 86.16 \end{array} \quad \begin{array}{r} 1.97 \\ \hline 50 \\ 85.74 \end{array} \quad \begin{array}{r} 2.7 \\ \hline 50 \\ 85.0 \end{array}$$

$$\begin{array}{r} 2.55 \\ \hline 50 \\ 85.16 \end{array} \quad \begin{array}{r} 2.6 \\ \hline 50 \\ 85.1 \end{array} \quad \begin{array}{r} 3.07 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 3.47 \\ \hline 50 \\ 84.24 \end{array} \quad \begin{array}{r} 3.15 \\ \hline 50 \\ 84.52 \end{array} \quad \begin{array}{r} 3.2 \\ \hline 50 \\ 84.5 \end{array}$$

$$\begin{array}{r} 3.5 \\ \hline 100 \\ 84.5 \end{array} \quad \begin{array}{r} 3.4 \\ \hline 50 \\ 84.3 \end{array} \quad \begin{array}{r} 3.0 \\ \hline 50 \\ 84.7 \end{array} \quad \begin{array}{r} 3.0 \\ \hline 50 \\ 84.7 \end{array} \quad \begin{array}{r} 2.6 \\ \hline 100 \\ 85.1 \end{array}$$

$$\begin{array}{r} 5.2 \\ \hline 100 \\ 82.5 \end{array} \quad \begin{array}{r} 6.4 \\ \hline 50 \\ 81.3 \end{array} \quad \begin{array}{r} 6.8 \\ \hline 50 \\ 80.9 \end{array} \quad \begin{array}{r} 8.0 \\ \hline 25 \\ 81.2 \end{array} \quad \begin{array}{r} 6.5 \\ \hline 50 \\ 81.2 \end{array} \quad \begin{array}{r} 6.5 \\ \hline 50 \\ 81.2 \end{array} \quad \begin{array}{r} 5.8 \\ \hline 100 \\ 81.9 \end{array}$$

$$\begin{array}{r} 7.2 \\ \hline 100 \\ 80.5 \end{array} \quad \begin{array}{r} 7.2 \\ \hline 50 \\ 80.5 \end{array} \quad \begin{array}{r} 8.0 \\ \hline 25 \\ 79.7 \end{array} \quad \begin{array}{r} 7.5 \\ \hline 50 \\ 80.2 \end{array} \quad \begin{array}{r} 6.7 \\ \hline 100 \\ 81.0 \end{array}$$

887.71

+68

Bottom Ditch on Pt.

+71

Top Ditch on Pt.

7.28 886.71

✓ 6.28

879.43 ✓

75

+50

76

+02.0

+50

77

+50

+95

Shore Valentine

(876.10)

7.28

879.43 ✓

1-31-30 Lt £ Rt.

<u>7.6</u>	<u>7.4</u>	<u>6.2</u>	<u>7.2</u>	<u>7.8</u>	11.0	<u>11.2</u>	<u>11.2</u>
<u>100</u>	<u>75</u>	<u>50</u>	<u>30</u>	<u>5</u>		<u>50</u>	<u>100</u>
80.1	80.3	81.5	80.5	79.9	76.7	76.5	76.5

<u>7.0</u>	<u>5.0</u>	<u>7.7</u>	<u>7.0</u>	<u>10.7</u>	11.0	<u>10.8</u>	<u>8.0</u>	<u>8.7</u>	<u>8.7</u>
<u>100</u>	<u>60</u>	<u>25</u>	<u>6</u>	<u>2</u>		<u>4</u>	<u>7</u>	<u>50</u>	<u>100</u>

Top Culvert + 80.0 80.7 77.0 76.7 76.9 77.7 79.0 79.0

80.7 82.7

<u>5.2</u>	<u>6.4</u>	<u>5.7</u>	<u>9.4</u>	<u>9.4</u>	<u>6.0</u>	<u>7.4</u>	<u>8.6</u>
<u>50</u>	<u>19</u>	<u>4</u>		<u>6</u>	<u>10</u>	<u>20</u>	<u>50</u>
81.5	80.3	81.0	77.3	77.3	80.7	79.3	78.1

<u>6.0</u>	<u>6.0</u>	<u>7.3</u>	<u>9.6</u>	<u>9.6</u>	<u>7.0</u>	<u>6.7</u>	<u>8.2</u>	<u>7.8</u>
<u>50</u>	<u>7</u>	<u>3</u>		<u>7</u>	<u>9</u>	<u>14</u>	<u>23</u>	<u>50</u>
80.7	80.7	79.4	77.1	77.1	79.7	80.0	78.5	78.9

<u>9.0</u>	<u>8.0</u>	<u>10.2</u>	<u>10.2</u>	<u>8.2</u>	<u>8.0</u>	<u>5.5</u>
<u>50</u>	<u>8</u>	<u>6</u>		<u>1</u>	<u>14</u>	<u>50</u>
77.7	78.7	76.5	76.5	78.5	78.7	81.2

<u>9.0</u>	<u>8.2</u>	<u>10.2</u>	<u>10.2</u>	<u>8.4</u>	<u>8.0</u>	<u>5.0</u>
<u>50</u>	<u>9</u>	<u>6</u>		<u>15</u>	<u>50</u>	
77.7	78.5	76.5	76.5	78.3	78.7	81.7

← Ditch →

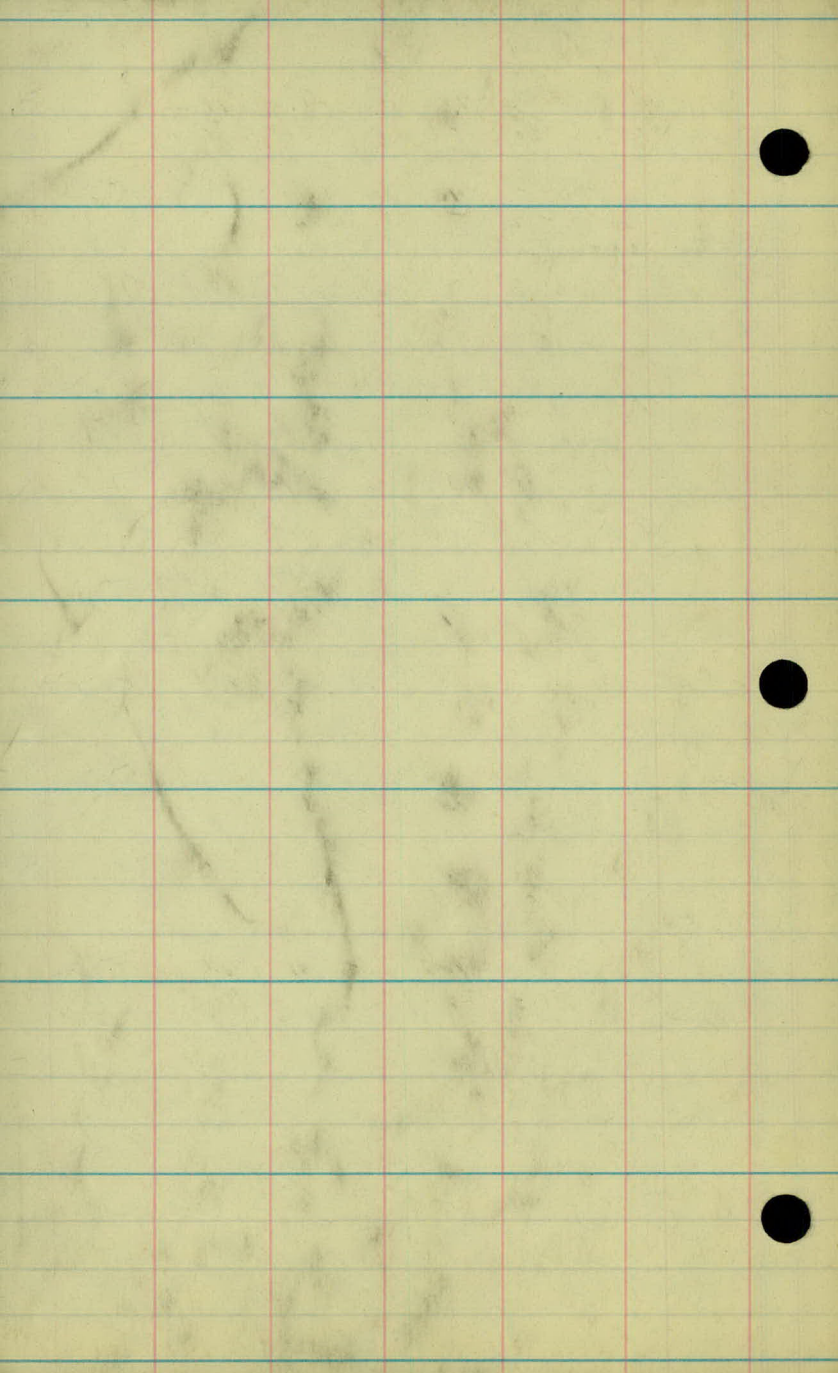
<u>9.8</u>	<u>9.2</u>	<u>10.0</u>	<u>10.0</u>	<u>9.4</u>	<u>9.2</u>	<u>8.2</u>	<u>6.4</u>
<u>50</u>	<u>24</u>	<u>20</u>	<u>18</u>	<u>15</u>		<u>25</u>	<u>50</u>
76.9	77.5	76.7	76.7	77.3	77.5	78.5	80.3

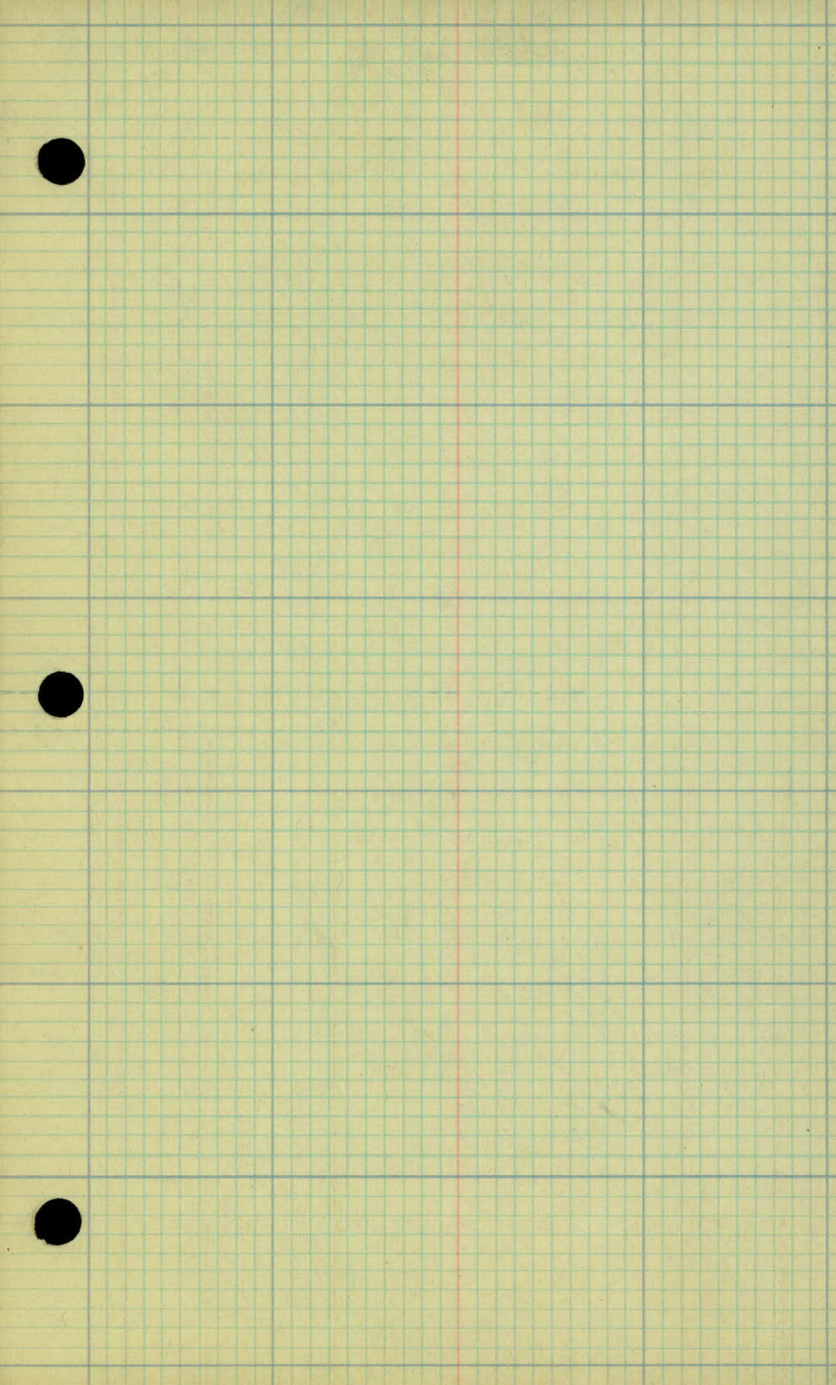
<u>10.4</u>	<u>10.2</u>	<u>9.8</u>	<u>9.4</u>	<u>8.6</u>
<u>50</u>	<u>25</u>		<u>25</u>	<u>50</u>
76.3	76.5	76.9	77.3	78.1

<u>10.8</u>	<u>10.8</u>	<u>10.5</u>	<u>10.5</u>	<u>10.5</u>
<u>50</u>	<u>25</u>		<u>25</u>	<u>50</u>
75.9	75.9	76.2	76.2	76.2

<u>10.6</u>	<u>10.5</u>	<u>10.5</u>	<u>10.5</u>	<u>10.6</u>
<u>50</u>	<u>25</u>		<u>25</u>	<u>50</u>
76.1	76.2	76.2	76.2	76.1

Culvert.





1

5

4

3

2

1

0 + 0 0

Hay Meadow on ht. 55

+60 = Int. of Edge of Woods

Hay Meadow

Hilly Woods

+ 55 = Beg. Woods 50'

 $+41 = \text{£ Ditch}$

-50'

+ 50 = Edge Trees

+ 41 = 12" Twin B.O. 4'

 $+32 = 10'' \text{ W.O. } 8''$ $+28^{\circ} 8' \text{BO. } 20'$

+18 = Twin B, 10" - 20"

$$+ 97 = 10'' \text{ W.O. } 21'$$

485 = 15" Oak 7"

23 = 12" W.O. 16'

$+70 = 10'' \text{ B.O. } 10'$
 $+62 = 12'' \text{ B.O. } 9'$

$$+60 = 10'' \text{ W.O. } 9'$$

7.55 1.00 3.00 1.00

+ 51 = 10" Ash 4'

$\angle 45 = 8'' \text{ N.O. } 25'$

$$\angle 36 = 4^\circ \text{ W.O. } 10'$$
 $+32 = 10^{\circ} \text{ W.O. } 9^{\circ}$ $+ 32 = 10^{\circ} \text{B.O. } 17'$
$$400 = 5 \cdot W.O.24'$$
$$+ 87 = 1002k \quad 15'$$

+ 82 = 10" Oak 15'

+69 = 20 OK 14
14 - 1" 0.4 0.1

+ 66 = 6" Oct 9'

+ 65 = 10' Oak 14'

$$\begin{aligned} + 44 &= 8 \text{ Oz} \times 10' \\ + 34 &= 5'' \text{ Asht } 10' \end{aligned}$$

+ 34 = 5" Ash 10"

432 Group 3-6 Ash J

 $+85 = 6'' \text{ OK}$ 5'
$$+74 = 10'' - 6'' - 4'' - 3'' \text{ Ash} = 2,7' - 14'' - 14'' - 8''$$
$$+72 = 10 + 6 \quad H_{SH} = 24 - 20$$

+69 = 12" C.W. 5'

+55 = End Light Brush

+ 83 = Twin^{10"} Ash 19'

+ 76 = 4" tree 25'

$$+70 = 4'' \text{ free } 19'$$

+ 20 = Licht Brust

+20 = 219m 2103
+10 = Shore line

- Water Gauge.

Lake Johanna

12

11

10

9

8

7

6

+34 = Int. of Woods

+00 Edge of Woods 10'

+70 = Int. of Edge of Woods

Hay Meadow

+00 = Int. of Woods

Hay Meadow

Edge of Wood 15'

Edge of Woods 20'

Hay Meadow

+87 = E. Power line
+55 = Edge of
Power line
Clearing

Hay Meadows

Edge of woods on line.

Hilly Woods

19

18

17

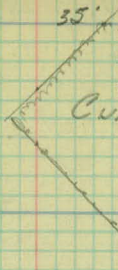
16

15

14

13

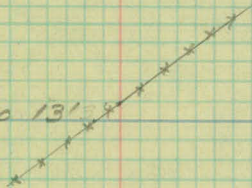
Hay Meadow



+66 = Int. of Cult Field
Cultivated Field.

+80 = 30" Bur Oak
17'

+10 = Int. F.
+00 = R/W. Fence 13'

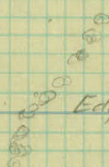


+05.0 = $\pm$ R.R. Trestles.
(Note on page following.)

Meadow

+50 = End Woods 55'

Edge of Woods 15'



+59 = Int. of Woods (A.P.)

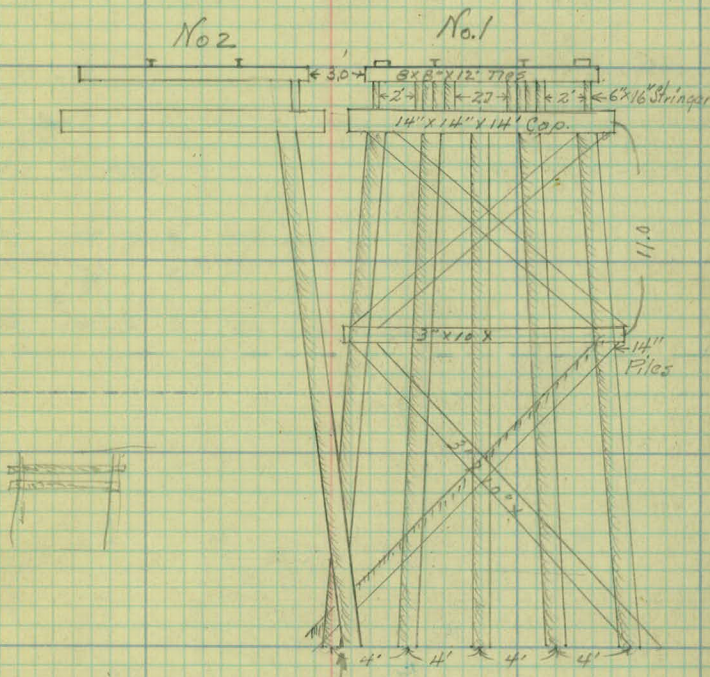
Hay

+50 = Edge of woods 5'

+00 = Edge of Woods 5' 0 0 0

2-1-30

3" X 10" Sway Braces.



± Brigs = 174050

26

25

24

23

22

21

20

Hay Meadow

57'

Fence line
N+3 1/4 Sec 28

+52 Cluster of 12-6° Wills 32'
+35 Cluster of 10-5° Wills 29'

+27 Fence Int.
No. +50 1/4 Sec 28

29'

Hay

33

32

31

30

29

28

27

Fence 28'

Cult.
Fields

the Fence 5'
N+S. $\frac{1}{4}$ line

Fence of N+S. $\frac{1}{4}$ 45'
line

Hay
Meadow

40

39

38

37

36

35

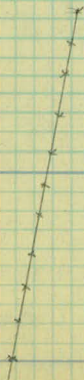
34

Hay Meadow

Hay Meadow.

+85 F - 62'
11.5 1/4 Lne

Cultivated



47

46

45

44

43

42

41

Hay Meadow

+59 = 8" H.O. 2'
+45 = Group of 6-8" Oaks 17'

+02.6 Δ Pt Fence 53' Lt End Ten.
E. W. 1/4 line

Hay Field

Hay Meadow

+90 = Cluster 4. 18" 32'
Pop

+59-15" B.O. 3'
+53 Int F.
E + W. 1/4 line.

Hay Field

50

49

2

1

$0+00 = 47+40 \quad \Delta 42^{\circ} \text{ Rt.} = \text{Base line.}$

-1

+68 F. line 12'
+55 F. cor. 4
+41 F. cor. 43

+97 F. Cor. on 4
+84 F. Cor. 23'

+80 2 Ditch 7.5'
Δ Ft.

Hay Field

Wooded Pasture

Base line

Tree line = 30'

Tree line = 30'

+100 = Beg. Wooded Hill 28'

+50 = Tree line 32'

+05.0 = Beg. Corner Tree. 37'

+23 Ditch 16'

-90 Int Rd.

-15 2 Rd.

Cultivated

Hay Field

+42 = Int Ditch

Hay

+34 D. Tol 43'
+26 = 2 Rd.

+93 = Cr. Bridge
Belvert.
31'
2-18'x18' Vix.
1-18'x18' C.I.

+16 = 15' W.O. 4'
+00 = Ditch 7' 64'

Ditch

17'

57

56

55

54

53

52

51

Woods

+100 F = 14'

+34 Δ Pt Fence 27'

+101 F = 24'

+100-15" B.O. 24'

Woods

+48-8" Oak 23'

+22-Twin 8" Oak 23'
Fence 23'

+95-2-12" B.O. 23'

+73-15" B.O. 23'

Fence line 23'

Hay Meadow

64

63

62

61

60

59

58

No. of Fence.

+ 00 F. 34'

Wooded Pasture

+ 00 F. = 49'

+ 00 F. = 36'

Hay

Hay Meadow.

71

70

69

68

67

66

65

72 - 400

100

Ditch

+00 Ditch 31'

+63 Ditch 27'

+00 Ditch 21'

+42 Int of Ditch Δ

+00 Ditch 12'

Field

Hay

+00 Ditch 40'

Hay

+00 Ditch 54'

77

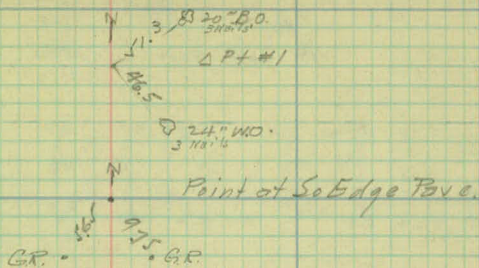
76

75

74

73

72



100 End Fence 30'



100 F = 9'

722 F Cor. 6'

+ B₀ = So. End of Culvert
= L of 2 - 36" x 86' - P₂

