

Book #67-Dr. #8

SURVEY OF
McCARRON'S BEACH

JAN. 1926

FILE 10

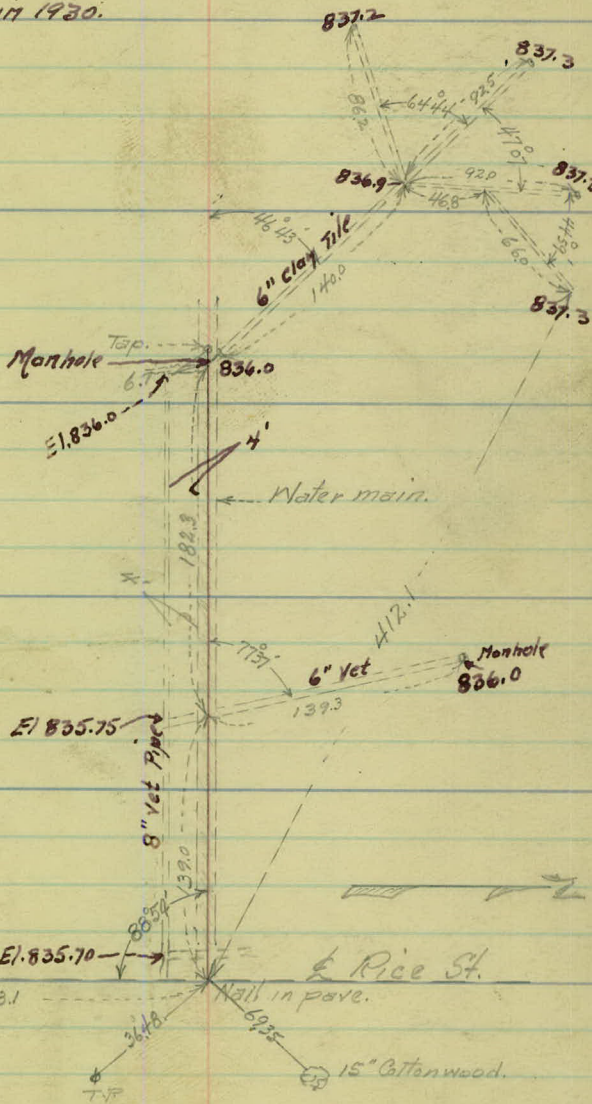
Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed 4-24-26

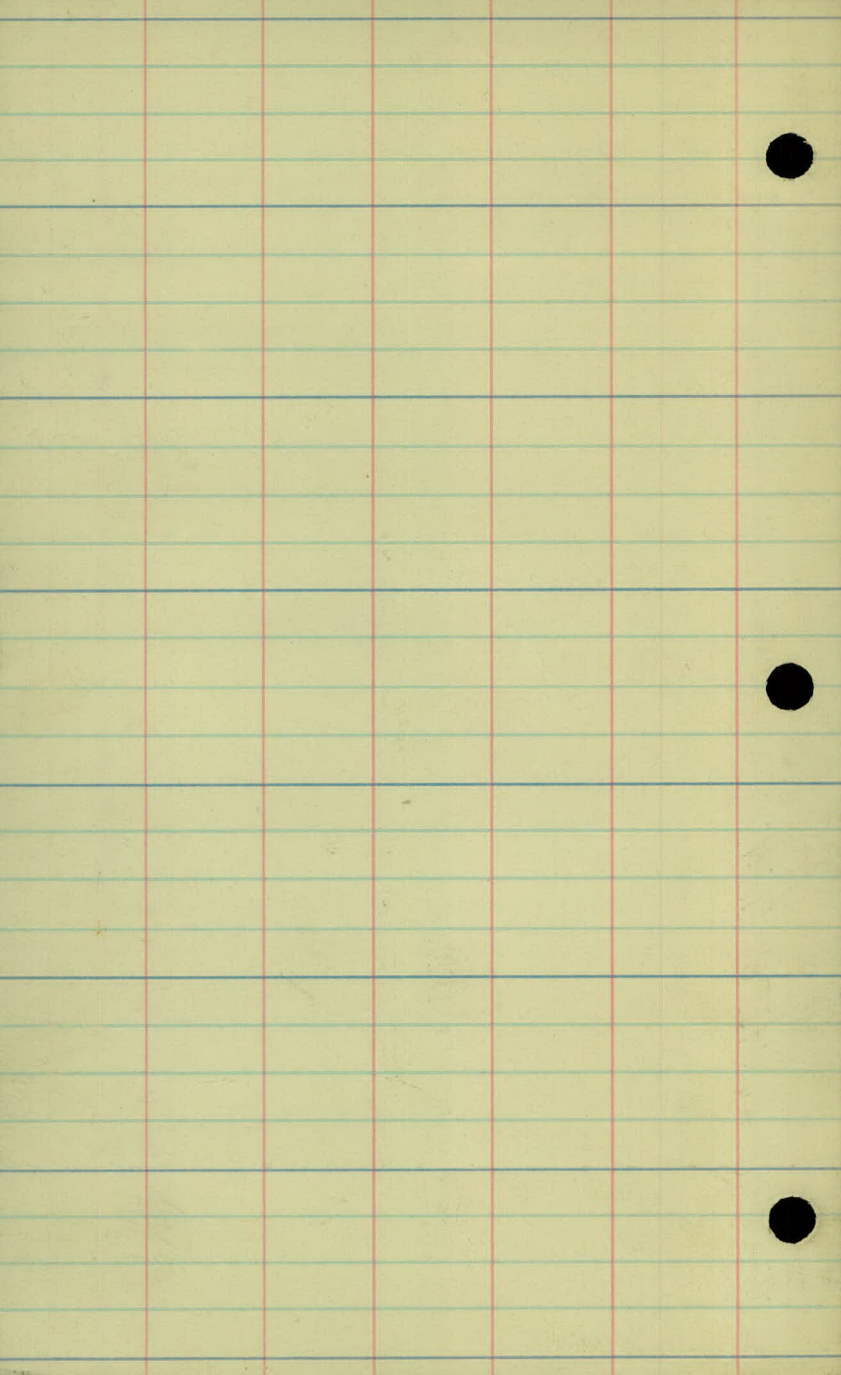
File No. "10"

Location of drain tile M^c Carron's
5-9-31 Beach.

Installed May-1931 in addition to Corrugated
pipe put in in 1930.



City Limits Co. D. "A"



-1930

2



Elevations on Back of this Sheet as of 1930

2 Pic St & Carpentier Ave.

Elw - See Other Side

	Elev. 1930	Elev 1931
± Rice Over Culv	842.69	842.69
Bottom Culv under Rice	834.40	834.40
W.S. " " "	836.08	Fluctuates.
Sta 0+29 Invert Tile	835.48	835.48
Sta 0+56 " "	835.58	835.58
Sta 1+68.8	836.20	835.3 settles
Sta 2+68	836.50	835.0 "
Sta 4+36.6	836.83	835.8
Sta 5+60	836.93	836.7
Sta 6+28 End.	836.99	836.2
Top of pipe at Spicket	838.88	839.00

8" Corrugated - Perforated Pipe @ 67¢
per foot 1930.

284 @ 67¢ = 189.28

McCarrons Beach. Survey.

Jan. 4th - 1926

Austin }
Skoglund } Party
Fritz }
Jankoski }

Station	+	H.I.	—	Elev.
B.M.	1.36	845.56		844.20
T.P.	5.03	843.92	6.67	838.89
T.P.	5.07	843.92	5.07	838.85
T.P.	7.74	846.66	5.00	838.92
T.P.	7.29	844.53	9.42	837.24

12-30-25

Spike in Stump. Near old. Ice. House. location

S.W. Cor. McCarrons Lake.

Sta. 0+00 to Sta.

height.

844.53

Elev.

0+00	1.69	842.84
+17	2.5	42.0
+30	8.4	36.1
+42	8.3	36.2
+50	7.8	36.7
1+00	8.5	36.0
+50	8.5	36.0
2+00	8.6	35.9
+50	8.5	36.0
3+00	8.6	35.9
+50	8.5	36.0
4+00	8.7	35.8
+50	8.6	35.9
5+00	8.4	36.1
+50	6.5	38.0
6+00	5.3	39.2
+22	4.0	40.5
+50	3.5	41.0
+66	3.5	41.0
+77	4.2	40.3
+91	5.3	39.2
+92	5.3	39.2

$\frac{1}{2}$ Wagener St.

$\frac{1}{2}$ Rice St. Pav.

Top. Ice Edge Lake.

Sta 0+54

844.53

Elev

Left

0+00	1.61	842.92
+18	2.7	41.8
+27	7.8	36.7
+50	8.6	35.9
1+00	8.5	36.0
+50	9.7	35.8
2+00	8.5	36.0
+50	8.4	36.1
3+00	8.4	36.1
+50	8.2	36.3
4+00	8.2	36.3
+50	8.0	36.5
5+00	7.6	36.9
+50	5.6	38.9
+72	4.0	40.5
6+00	3.3	41.2
+36	4.2	40.3
+40	4.7	39.8
+42	5.2	39.3

4 Rice St. Top. Por.

Ice Bay

" "

" "

Edge Lake Top Ice

Sta. 1+08

height.

844.53

Elev.

0 + 00

1.41 843.12

+ 20

2.3 42.2

+ 27

6.1 38.4

+ 40

6.1 38.4

+ 45

5.3 39.2

+ 50

5.3 39.2

+ 75

6.1 38.4

1 + 00

7.2 37.3

+ 25

8.5 36.0

+ 50

8.6 35.9

2 + 00

8.6 35.9

+ 50

8.6 35.9

3 + 00

8.1 36.4

+ 50

8.2 36.3

4 + 00

7.6 36.9

+ 50

7.0 37.5

5 + 00

6.7 37.8

+ 25

5.7 38.8

+ 50

3.2 41.3

+ 75

2.3 41.2

+ 97

4.3 40.2

6 + 00

5.2 39.3

T.P.

7.49

844.73

7.29

937.24

1/2 Rice St. Pavement.

Ice Bog. hand.

vv vv vv

vv vv vv

vv vv vv

Edge. lake

Sta 1+62

844.73

Elev.

best.					
0 + 00	1.58	843.15			
+ 20	1.8	42.9			
+ 26	3.9	40.8			
+ 40	4.6	40.1			
+ 45	3.4	41.3			
+ 50	3.0	41.7			
1 + 00	3.8	40.9			
+ 50	6.3	38.4			
2 + 00	7.1	37.6			
+ 50	7.8	37.4			
3 + 00	7.7	37.0			
+ 50	9.0	36.7			
4 + 00	7.3	37.4			
+ 50	6.2	38.5			
+ 86	5.4	39.3			
5 + 00	4.2	40.5			
+ 25	2.4	42.3			
+ 42	2.6	42.1			
+ 50	3.6	41.1			
+ 63	5.4	39.3			
+ 81	5.8	38.9			
T.P.	8.23	849.04	3.92	840.81	

Rice St Pav.

Edge hole Top Ice.

Sta. - 2+16

849.04

Elev

Left

0+00	5.65	843.39
+25	6.4	42.6
+30	7.4	41.6
+36	5.1	43.9
+50	6.0	43.0
1+00	6.7	42.3
+50	7.3	41.7
2+00	8.0	41.0
+50	8.6	40.4
3+00	9.2	39.8
+50	10.2	38.8
4+00	10.5	38.5
+50	9.7	39.3
+81	8.8	40.2
+98	7.2	41.8
5+00	7.1	41.9
+08	7.7	41.3
+23	8.9	40.1
+50	10.2	38.8

162
20
16

4 Rice St Pav.

Ice + Edge Lake

Sta. - 2 + 70

849.04

Elev.

Hgt.

0 + 00

5.35

843.69

+ 27

5.8

43.2

+ 38

6.8

42.2

+ 40

5.7

43.3

+ 50

6.0

43.0

1 + 00

5.8

43.2

+ 50

6.8

42.7

2 + 00

6.4

42.6

+ 50

6.8

42.2

3 + 00

8.0

41.0

+ 50

9.6

40.4

4 + 00

9.1

39.9

+ 21

9.5

39.5

+ 33

7.7

41.3

+ 50

7.5

41.5

+ 60

7.4

41.6

+ 76

7.6

41.4

+ 91

9.0

40.0

+ 94

9.5

39.5

5 + 15

10.2

38.8

T.P.

3.62

Rice St. Pav.

Edge Lake. Top. Ice

Sta. - 2 + 24

Left

849.04

Elev.

0 + 00	5.05	843.99
+ 27	5.8	43.2
+ 30	6.5	42.5
+ 36	6.5	42.5
+ 39	4.6	44.4
+ 50	4.9	44.2
1 + 00	4.8	44.2
+ 50	4.8	44.2
2 + 00	5.2	43.6
+ 50	5.7	43.3
3 + 00	6.7	42.3
+ 50	7.8	41.2
+ 75	8.0	41.0
+ 81	7.3	41.7
4 + 00	7.4	41.6
+ 30	7.7	41.3
+ 50	7.7	41.3
+ 62	8.4	40.6
+ 66	9.4	39.6
+ 81	10.1	38.9

4 Rice St. Pav.

Edge Lake Top of Ice.

Sta. 3+78

849.04

Elev.

0 + 00	5.00	844.04
+ 21	5.5	43.5
+ 27	6.1	42.9
+ 36	4.4	44.6
+ 50	4.6	44.4
1 + 00	4.5	44.5
+ 50	4.3	44.7
+ 75	6.0	43.0
2 + 00	6.2	42.8
+ 25	7.0	42.0
+ 50	5.0	44.0
3 + 00	6.6	42.4
+ 50	6.2	40.8
4 + 00	7.5	41.5
+ 32	8.0	41.0
+ 24	5.0	44.0
+ 50	7.7	39.3
+ 66	7.9	39.1

$\frac{1}{2}$ Rec. St. Pav.

Edge Lake Top. of Ice

Sta. - 4 + 32

Left

849.04

Elev.

0 + 00	5.00	844.04
+ 24	5.7	43.3
+ 36	7.7	41.3
+ 50	8.0	41.0
1 + 00	6.0	43.0
+ 25	4.2	44.8
+ 50	4.5	44.5
2 + 00	4.9	44.1
+ 25	4.8	44.2
+ 50	6.7	42.3
3 + 00	8.3	40.7
+ 25	9.5	39.5
+ 50	9.3	39.7
+ 80	8.0	41.0
4 + 00	7.7	41.3
+ 22	8.2	40.8
+ 26	9.5	39.5
+ 42	9.7	39.3

Rice St. Pav.

Edge. Lake. Top. of Ice

Sta. - 4 + 86

849.04

Elev.

0 + 00	5.30	843.74
+ 24	6.0	43.0
+ 35	11.1	37.9
+ 38	10.5	38.5
+ 50	10.2	38.8
1 + 00	10.0	39.0
+ 50	9.7	40.3
2 + 00	9.4	40.6
+ 50	9.9	40.1
3 + 00	9.6	39.4
+ 50	9.2	39.8
+ 72	8.2	40.8
+ 84	7.8	41.2
4 + 00	8.7	40.3
+ 07	8.7	40.3
+ 12	9.5	39.5
+ 32	9.8	39.2

£ Rice. St. Pav.

Edge. Lake. Top. of Ice.

Sta - 5+40

849.04

Left

Elev.

0 +00

5.55 848.49

+25

6.9 42.1

+35

11.2 37.8

+38

10.6 38.4

+50

11.0 38.0

1 +00

10.7 38.3

+50

10.5 38.5

2 +00

10.5 38.5

+50

10.5 38.5

3 +00

10.0 39.0

+50

9.6 39.4

+64

8.5 40.5

+81

7.8 41.2

4 +00

8.5 40.5

+10

8.8 40.2

+12

9.5 39.5

+41

9.8 39.2

38.5
20
18.5

1/2 Rice. St. Pav.

Edge Lake Top Ice

Sta - 5+94

Elev.

849.04

Elev.

0 + 00

5.65

843.39

+ 22

6.4

42.6

+ 31

10.8

38.2

+ 50

11.0

38.0

1 + 00

11.1

37.9

+ 50

11.0

38.0

2 + 00

10.2

38.8

+ 50

10.0

39.0

3 + 00

9.6

39.4

+ 44

9.3

39.7

+ 50

8.2

40.6

+ 71

8.2

40.8

+ 74

8.7

40.3

4 + 00

7.9

41.1

+ 50

8.7

40.3

+ 60

9.4

39.6

5 + 00

10.2

39.8

Rice St. Pav.

Sta. 6 + 57.86

Left

849.04

Elev.

0 + 00

5.45

843.59

+ 20

6.5

42.5

+ 30

11.5

37.5

+ 34

11.6

37.4

+ 40

11.0

38.0

+ 50

11.0

38.0

1 + 00

11.0

38.0

+ 50

11.3

37.7

2 + 00

10.9

38.1

+ 50

10.5

38.5

3 + 00

9.5

39.5

+ 26

9.0

40.0

+ 41

7.2

41.8

+ 50

7.2

41.8

+ 75

7.5

41.5

4 + 00

9.0

41.0

+ 25

6.6

42.2

+ 50

6.0

43.0

+ 65

5.7

43.3

5 + 00

6.8

42.2

+ 50

7.5

41.5

T.P.

4.08

848.77

4.35

844.69

B.M.

4.53

844.24

(844.30)

$\frac{1}{2}$ Center St.

12-30-25

$\frac{1}{2}$ Rice St. Pav.

Spike in Ele. Pole. on W. side of Rice St.
Directly East of McCarrons lake.

844.20

5.4
2.9
8.3

848.77 H.I.

4.09
844.68
2.02

846.70 H.I.

7.74

838.96

4.95

843.91

4.96

838.95

1.93

840.88

4.95

835.93

6.48

842.41

1.17

843.58

48.15

9.6
38.55

48.15

10.6
37.55

48.15

10.6
37.55

48.15

11.35
36.80

48.15

48.15

10.7
37.45

5494

4439

125

48.15

11.0
36.75

8.8

2.6

11.2

B.M. 844.30

3.85

848.15

10.7
1.3
12.0

5400

4400

+50 26.4 Timber. Brg. 16' x 20'

3400

461 (12" $\oplus$ 22' R4

2+00

+ 76 (10" E) 31' R4.

1400

Intake: 837.55

Ditch 837.5

Inv. 836.8

4 Rice St. 0100

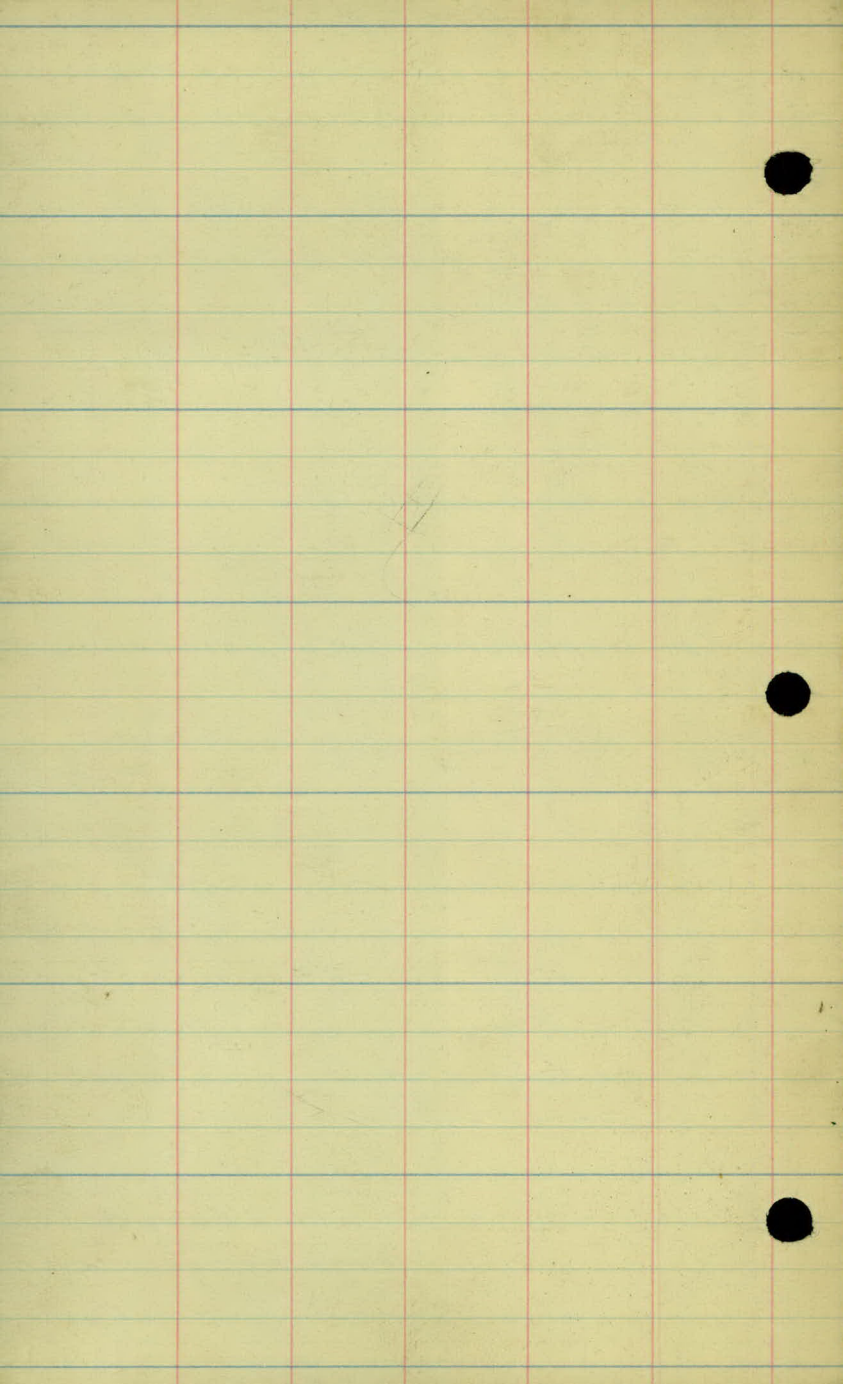
30" x 20" C.M.P.

5.758.744

Low hand

Low Land.
See P.R.B.

5494



McCarrons Beach

- (3+78-273) - 24" Oak 13' ht. ✓
- (5+40-398) - 8" Willow 7' ht. ✓
- (4+86-385) - { Willow Clump } 2' ht. ✓
6-12" Trees
- (4+32-397) - { Willow Clump } 8' ht. ✓
3-12" Trees
- (2+70-469) - { Willow Clump } 10' ht. ✓
4-8" Trees
- (2+16-500) - { Willow Clump } 14' ht. ✓
2-12" Trees
- (2+16-506) - (10" Willow) 2' ht. ✓
- (1+62-578) - { Willow Clump } 35' ht. ✓
4-8" Trees
- (1+62-530) - (6" Willow) 20' ht. ✓

(4+86-391) - (12" Willow) 5' ht. ✓

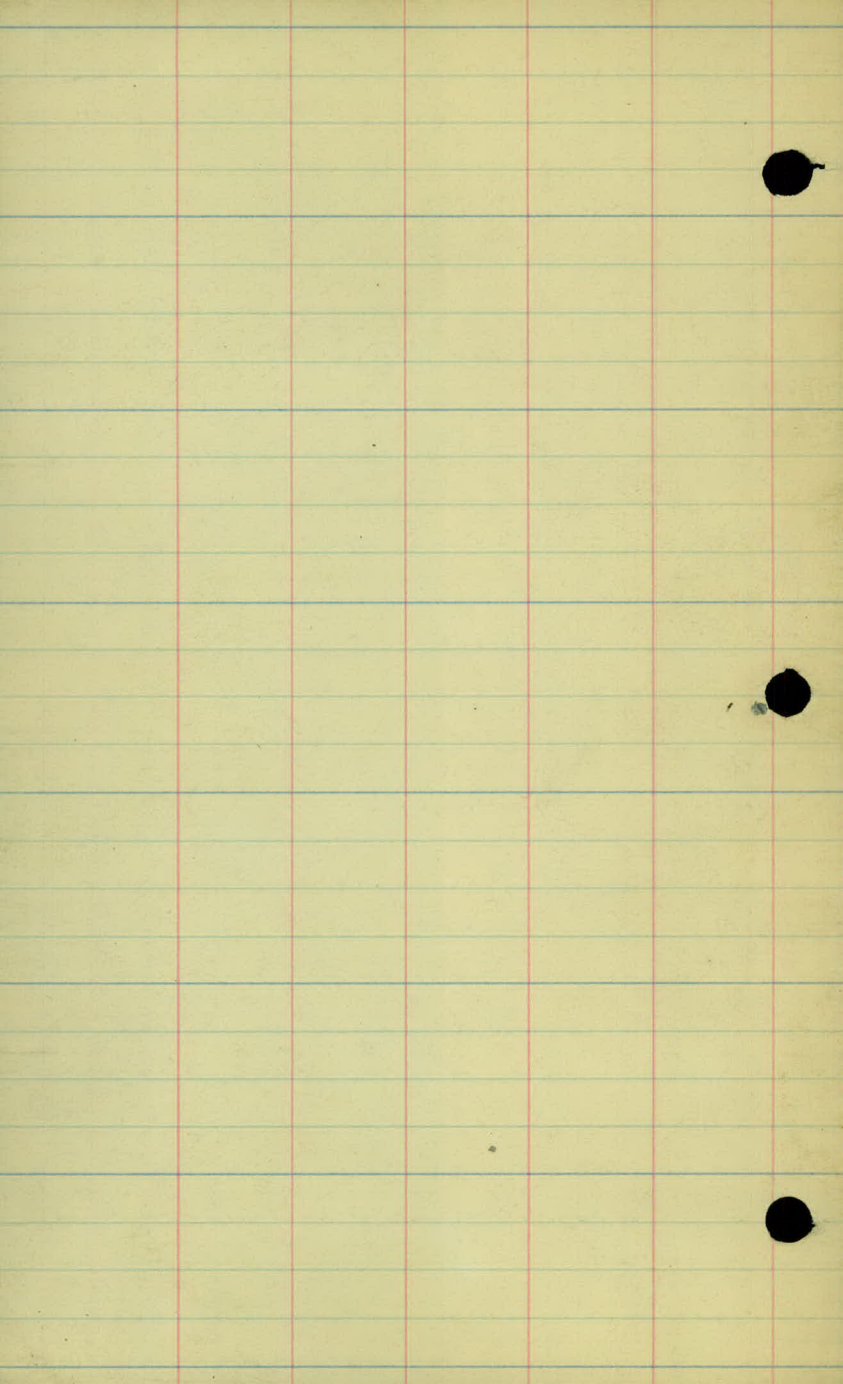
(2+16-513) - (10" Willow) 10' ht. ✓

(1+62-550) - (6" Willow) 6' ht. ✓

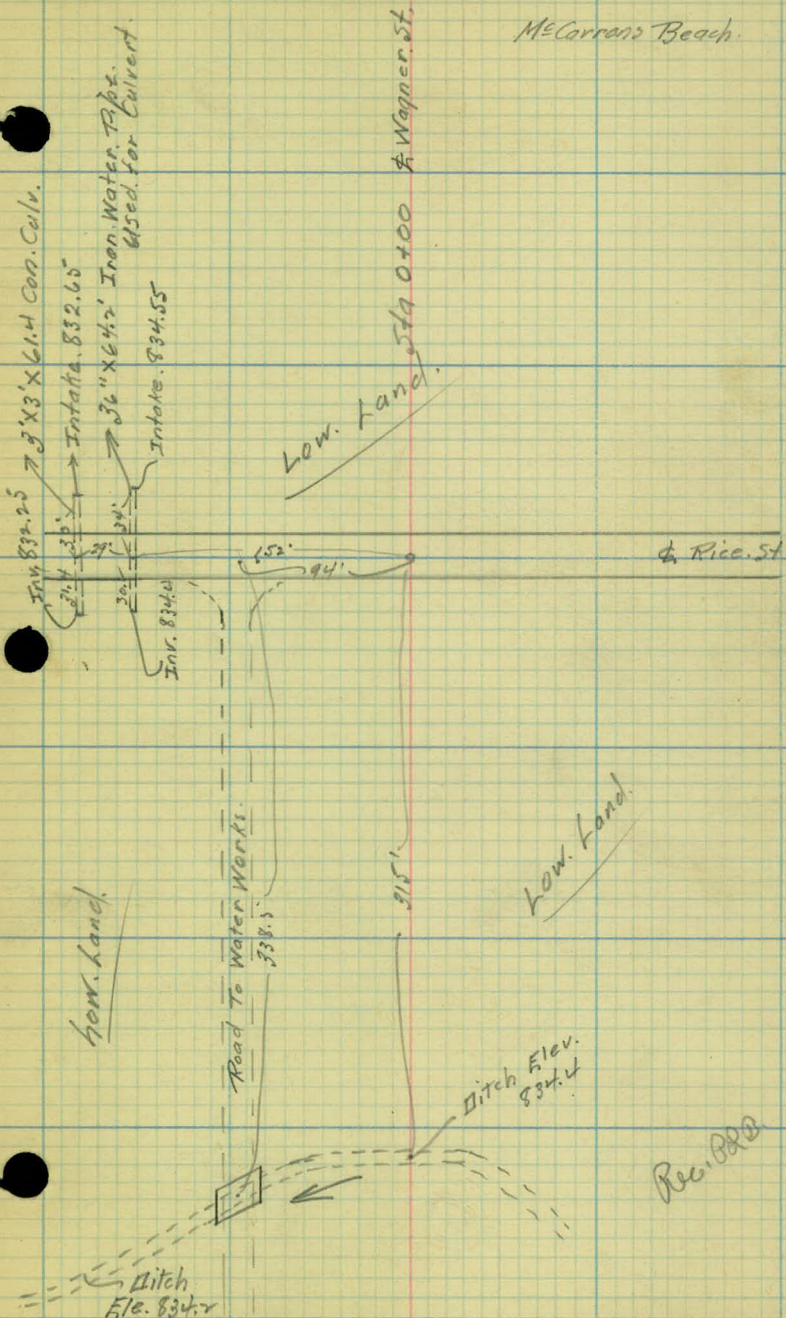
(1+62-555) - (8" Willow) 14' ht. ✓

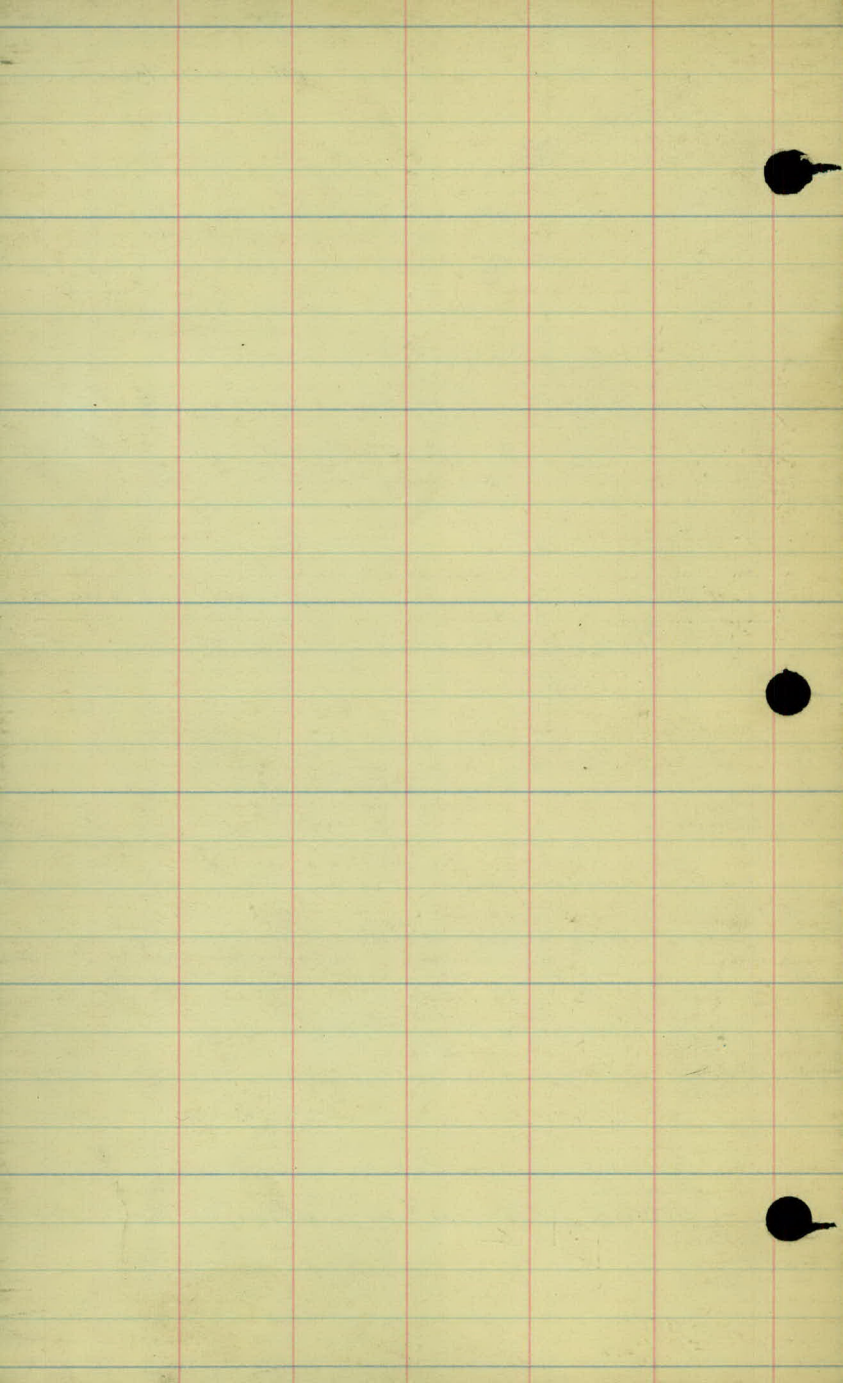
(1+62-560) - (10" Willow) 23' ht. ✓

see P.R.B.



McCarrans Beach.





McCarrons Beach - Soundings

Elev. 836.4 ✓

Elev. 42.8

Sta.
 $\frac{1+08}{300'}$

Sta.
 $\frac{3+78}{200'}$

26' Wet. Veg. Bog.

8' Firm Sand.

Pushed
2" Iron pipe
Down 26' 4"
Ind. of firm
Bottom.

7' Wet Sand.
Thin layers
of Shale.

15' Ind. of
Quick sand.

Moved 1" Pipe
Down 20'

Elev. 810.4

1+08
300' Left
No 4

No 2

Elev. 42.3

Elev. 38.5

Sta. 5+24
 $\frac{5+24}{300}$

Sta.
 $\frac{5+40}{200'}$

6' Firm Sand.

5' Dry. Peat.
2' Sandy Peat.
4" Layer Shale.

Moved 1" Pipe Down 14'

16'-7' Firm Wet Sand

39'-10' Wet Sand.

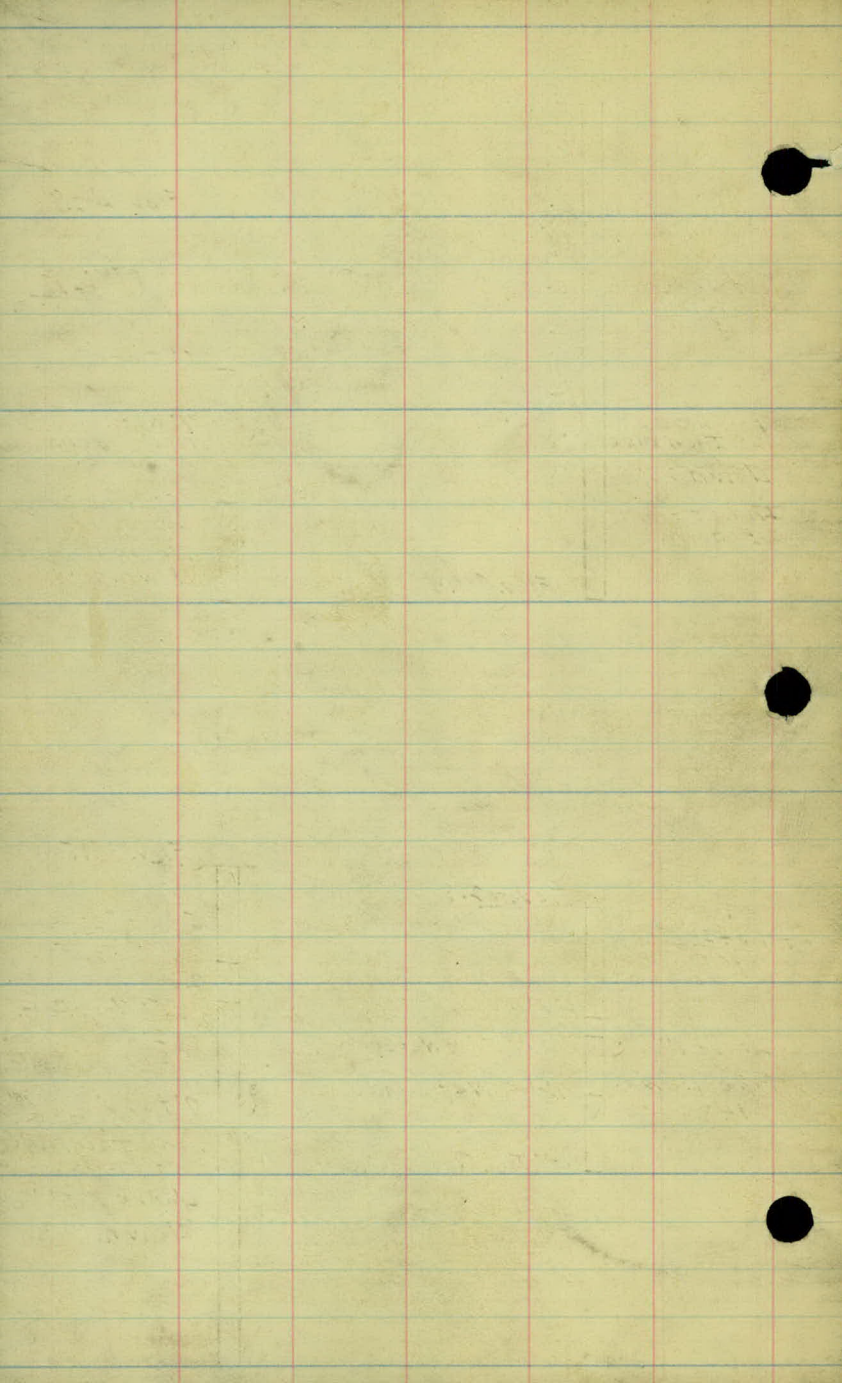
14' Ind. Quick sand

7' to 26'
Sandy Peat.
and thin layers
of Shale.

Moved 1" Pipe
Down 26'

No 3

No 1



Location of Borrow Pit
at McCarrons Blvd. S. & Rice St.

Crane

McIntyre

Berthoume

Frank.

Sta.

Point

Lt.

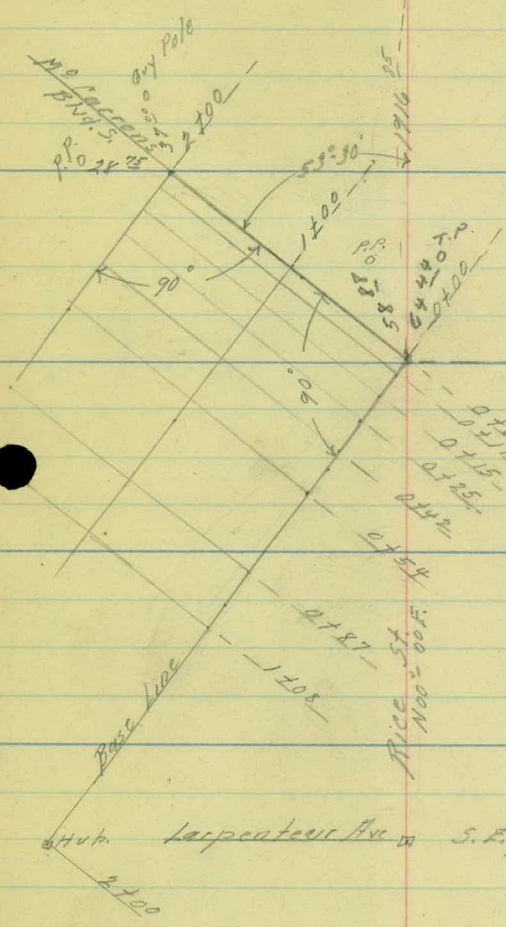
Rt.

7+15¹⁵ P.I. 53°-30

0+00

3/23/24

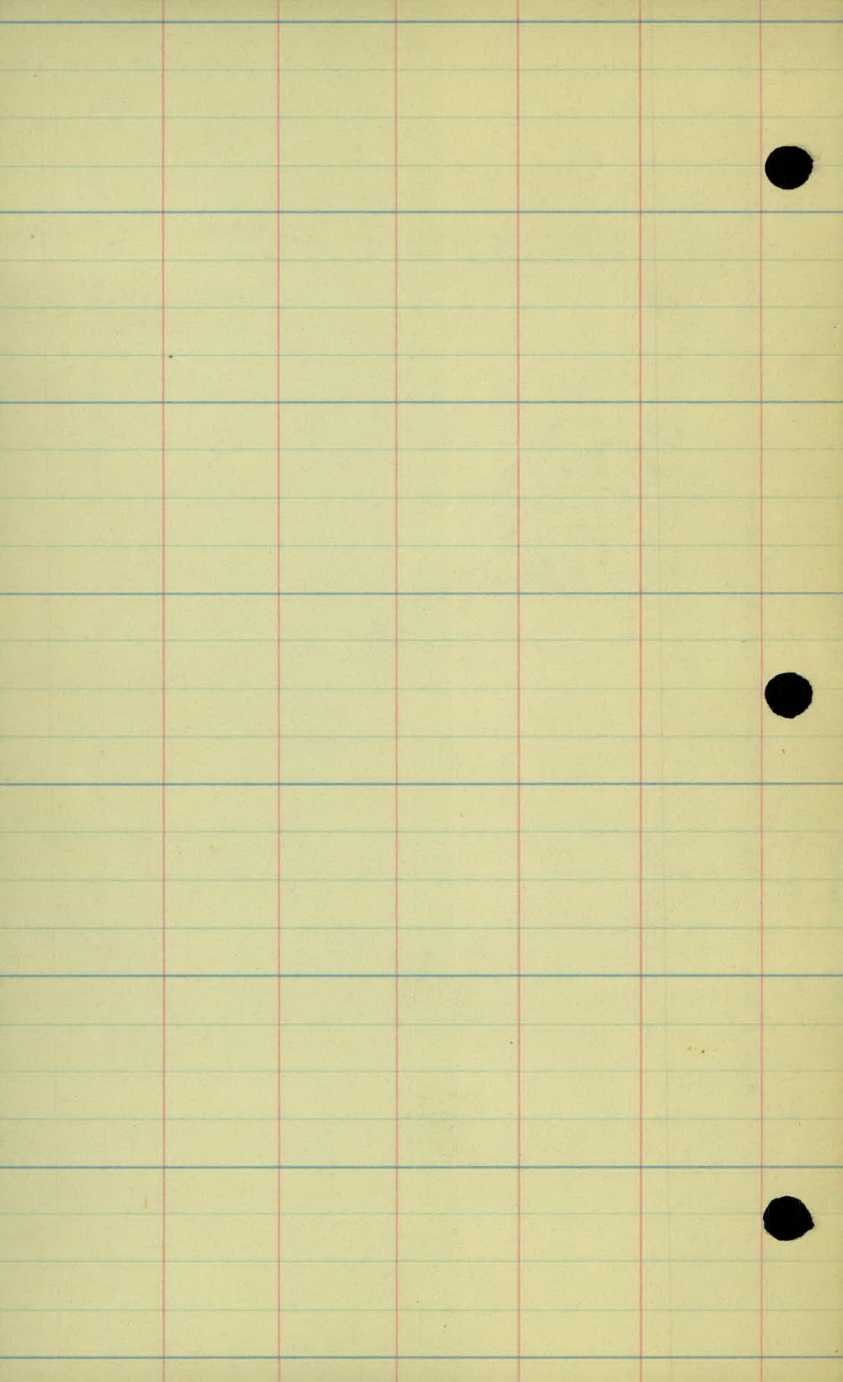
1/4 Cor. E. line Sec. 13



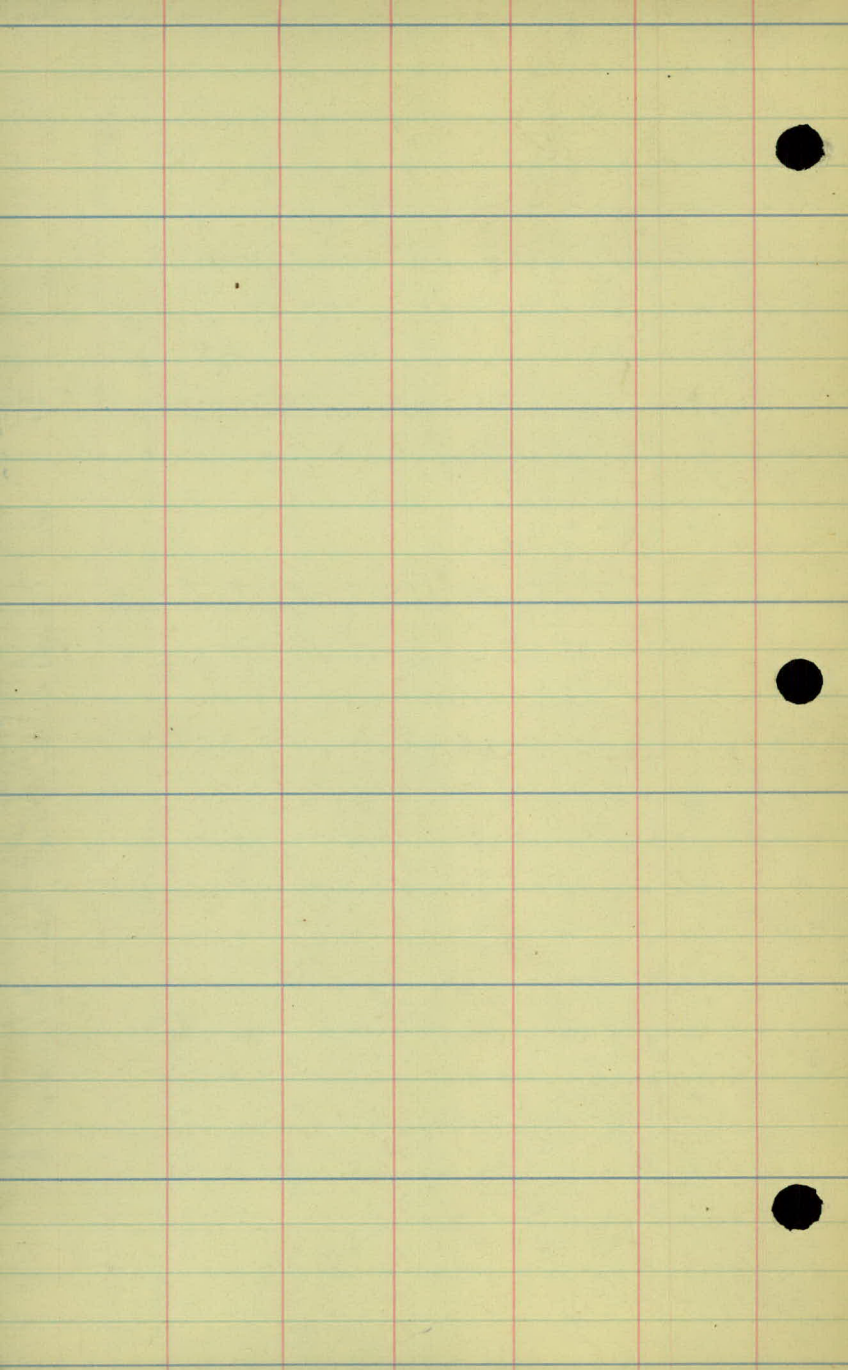
7+15¹⁵ = 0+00 McCarrens Bl

Larpenetier Ave

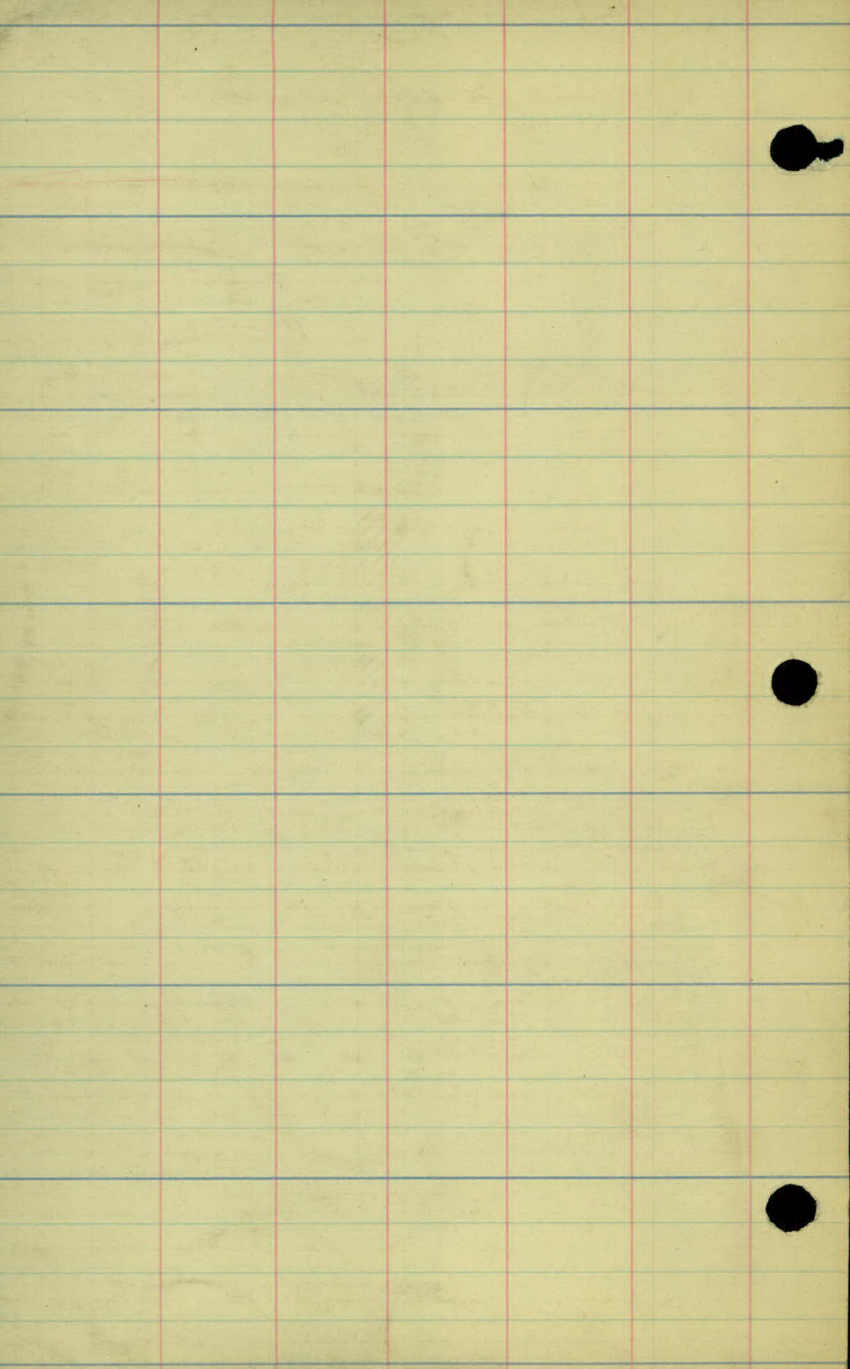
S. E. Cor. Sec. 13
Stone Mt.



Art. Topog. 017
Barrow Pit at McCarrons Bldg's
& Rice St.



6700



Proj. #26-02.

Original X sections
on Ditch N. Side of M^r. Carron's
Beach.

Sta.	+ H.I.	- Elev.
B.M.	3.52 846.52	843.00
T.P.	5.33 845.68	6.17 840.35
0+33		

0+35

1+00

1+50

2+00

2+50

3+00

3+29

3+45

3+44 Edge of Bridge

3+50

3+64

3+65 Edge of Bridge

4+00

B.M. 2.68 843.00

$$\frac{8.1}{10} \quad 8.1 \quad \frac{8.1}{10}$$

$$\frac{7.1}{10} \quad 7.1 \quad \frac{7.1}{10}$$

$$\frac{7.4}{10} \quad 7.4 \quad \frac{7.4}{10}$$

$$\frac{7.4}{10} \quad 7.4 \quad \frac{7.4}{10}$$

$$\frac{7.5}{10} \quad 7.5 \quad \frac{7.5}{10}$$

$$\frac{7.1}{10} \quad 7.1 \quad \frac{7.1}{10}$$

$$\frac{7.4}{8} \quad \frac{7.4}{4} \quad \frac{6.0}{3} \quad 6.3 \quad \frac{6.1}{4} \quad \frac{6.5}{10}$$

$$\frac{5.6}{10} \quad \frac{5.4}{8} \quad \frac{7.2}{5} \quad \frac{7.2}{3} \quad 5.4 \quad \frac{5.7}{10}$$

$$\frac{4.4}{10} \quad \frac{4.5}{4} \quad \frac{7.2}{3} \quad 7.2 \quad \frac{5.7}{2} \quad \frac{4.4}{5} \quad \frac{4.3}{10}$$

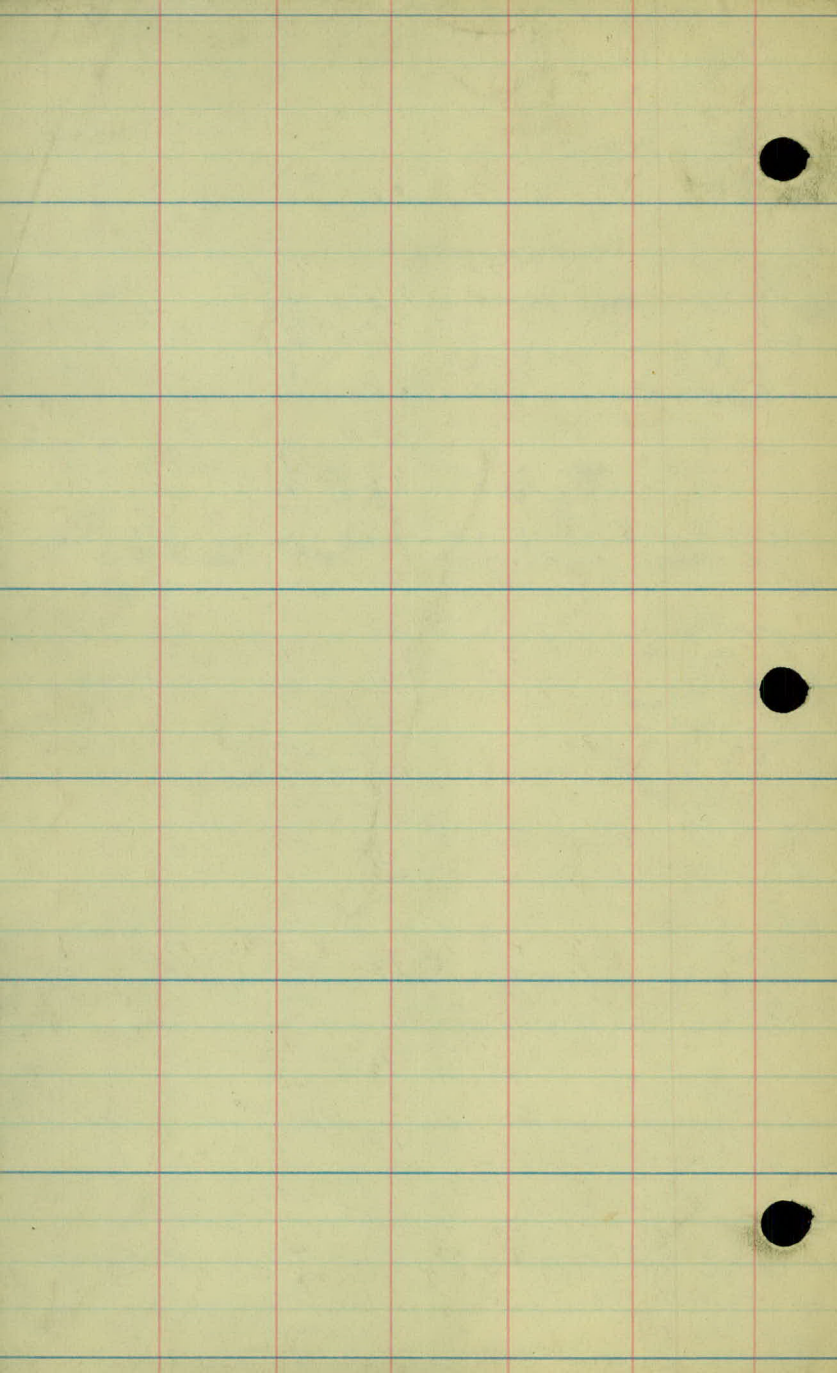
$$\frac{4.9}{10} \quad 5.2 \quad \frac{4.3}{10}$$

$$\frac{5.0}{10} \quad 4.9 \quad \frac{4.6}{10}$$

$$\frac{5.0}{10} \quad 4.9 \quad \frac{5.4}{10}$$

$$\frac{5.5}{10} \quad \frac{5.7}{4} \quad \frac{7.0}{2} \quad 7.0 \quad \frac{7.0}{1} \quad \frac{5.7}{4} \quad \frac{5.5}{10}$$

$$\frac{5.5}{10} \quad \frac{5.6}{3} \quad \frac{6.7}{1} \quad 6.9 \quad \frac{6.9}{1} \quad \frac{5.6}{3} \quad \frac{5.9}{10}$$



Proj. # 26-02.

McCarron's Beach.

Final x Sections from Sta.
0+00 to Sta. 6+22.

Sta.	+	H.I.	-	Red.	Elev.
B.M.	4.10	847.10		843.00	
0+03					

0+00

0+54

1+08

1+62

2+16

T.P.	5.04	848.09	4.05	843.05
------	------	--------	------	--------

2+70

3+24

3+78

4+32

T.P.	3.23	846.41	4.91	843.18
------	------	--------	------	--------

4+70

3+24

3+78

6/8/26

N.

Top of Water

Left.

(7.1)

8.2 6.6 5.5 6.1 6.4 7.0 8.0 7.8 9.4
700 677 665 662 641 631 600 590 550

2 Rice St 00

8.2 6.6 6.5 5.5 6.1 5.8 5.0 7.8 9.4
700 676 664 662 658 641 600 590 550

(7.1)

8.2 7.8 6.4 6.0 5.3 4.8 11.4 9.9 9.9
660 643 630 600 550 534 519 500 475

(7.1)

8.2 7.5 6.6 6.3 6.0 4.9 7.9 10.3 8.1 8.5 4.4 4.3 4.1
614 600 588 550 500 462 448 400 100 30 33 12 0.0

(7.1)

5.4 6.2 6.4 7.6 8.2
450 500 550 563 581 ✓

5.2 5.2 10.5 10.4 10.3 9.9 10.3 5.1 4.6 4.1 4.3 4.7 6.5 6.5 4.0 4.1 4.1
400 384 374 350 300 200 193 169 150 100 50 34 31 29 25 12 00

(7.1)

8.2 7.6 5.7 6.5 6.0 5.8 5.3 4.6 4.4 4.3 4.3 4.3 4.2 4.3 6.1 6.0 4.1 4.0 3.9
547 528 507 506 450 400 350 300 250 200 150 100 50 34 30 27 23 12 00

(7.1)

4.7 4.9 5.0 5.1 5.0 4.8 6.6 6.6 4.9 4.7 4.5
350 300 150 100 50 35 30 27 24 12 00

(8.1)

Bath 4.9 5.0 5.0 5.0 5.0 4.8 6.2 6.2 4.7 4.6 4.3
House 459 400 150 100 50 33 29 26 23 12 00

(8.1)

4.9 5.1 4.9 5.0 5.1 5.0 4.9 6.3 6.4 4.9 4.35 4.15
260 237 200 150 100 50 34 30 26 23 12 00

(8.1)

5.0 5.2 5.0 5.1 5.0 5.0 6.5 6.6 4.5 4.3 4.2
150 200 150 100 50 44 30 27 23 12 00

(8.1)

7.5 6.9 5.5 5.5 5.2 4.5 3.3
508 475 476 450 400 350 300

(6.4)

7.5 7.0 5.7 5.1 4.4 4.7 13.4
478 458 450 400 350 313 House.

(6.4)

7.5 6.7 5.6 5.3 4.5 4.1 3.4 3.6
463 434 434 400 350 323 309 300

(6.4)

Sta	+	H.I.	-	Red.	Elev.
		846.41			

4+32

3.93	847.08	3.24	845.15
------	--------	------	--------

4+86

5+40

5+94

6+15

6+22

B.M.

4.05	843.03	843.00
------	--------	--------

2/8/36

Loft.

7.5 7.0 5.8 5.6 4.8 4.7 4.4
440 428 418 400 350 318 300

(6.4)

8.2 6.2 6.2 5.5 4.7 4.3 4.4 4.6 4.4 4.5 4.3 6.3 4.2 3.65 3.5
424 396 350 294 288 250 200 150 100 50 35 27 23 12 00

(7.1)

8.2 6.5 6.1 5.3 4.7 4.6 4.6 4.5 4.6 4.4 6.3 6.7 4.7 3.9 3.7
425 400 350 300 250 200 150 100 50 35 30 27 24 12 00

(7.1)

8.2 6.6 6.2 6.0 4.9 4.7 4.9 5.1 5.1 4.7 4.0 3.9
484 459 400 350 300 250 200 150 100 50 12 00

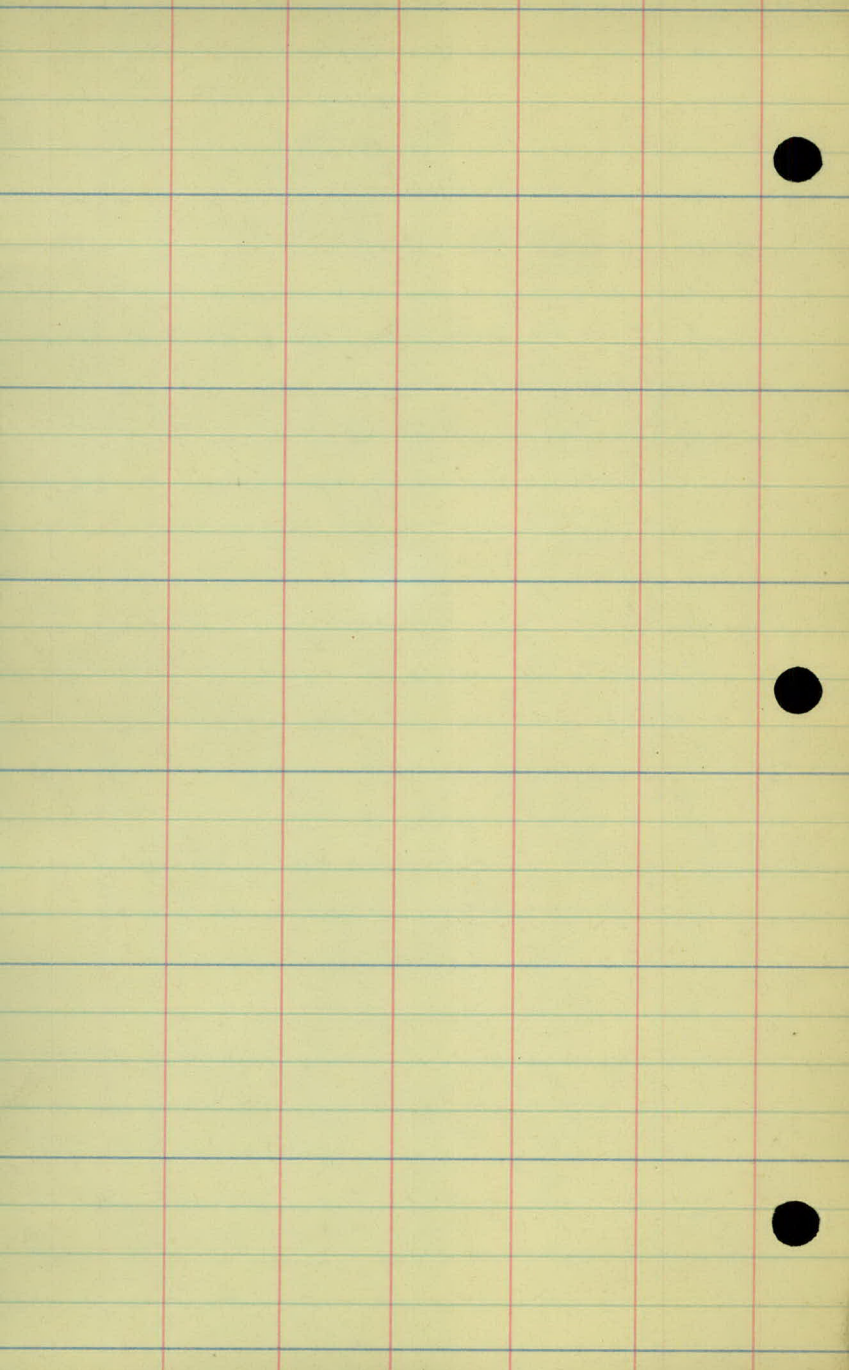
(7.1)

8.2 6.8 6.3 6.1 5.8 5.0 4.6 4.9 5.2 5.0 5.0 4.6 4.1 4.0
522 500 450 400 350 300 250 200 150 100 50 30 12 00

(7.1)

8.2 6.8 6.3 6.7 6.4 7.6 8.2 9.2 9.6 9.6 9.4 9.4 4.1 4.0
522 500 450 400 350 300 250 200 150 50 50 30 12 00

(7.1)



Proj. # 26-02.

M^r. Carrons Beach.

Final x sections of Barrow.

Pit at M^r. Carrons Blvd. South
and Rice St.

Sta.	+ H.I.	-	Red.	Elev.
B.M.	5.40	895.01	889.41	
0+00			5.10	
0+11			4.92	
0+15			4.90	
0+25			5.0	
0+42			5.8	
0+54			6.6	
0+87			6.4	
1+08			6.7	
1+38			5.9	
1+54			5.7	
1+70			2.3	
T.P.	11.62	903.39	3.24	891.77
1+82			9.3	
2+00			9.1	

6/7/20

Right.

(5.1)

$$\begin{array}{r} 5.1 \\ 0.0 \end{array} \quad \begin{array}{r} 5.28 \\ 15. \end{array} \quad \begin{array}{r} 0.9 \\ 52 \end{array} \quad \begin{array}{r} 9.2 \\ 100 \end{array} \quad \begin{array}{r} 104 \\ 164 \end{array} \quad \begin{array}{r} 10.9 \\ 200 \end{array}$$

$$\begin{array}{r} 4.9 \\ 0.0 \end{array} \quad \begin{array}{r} 4.97 \\ 7 \end{array} \quad \begin{array}{r} 6.4 \\ 31 \end{array} \quad \begin{array}{r} 8.3 \\ 69 \end{array} \quad \begin{array}{r} 9.3 \\ 100 \end{array} \quad \begin{array}{r} 10.5 \\ 151 \end{array} \quad \begin{array}{r} 11.3 \\ 200 \end{array}$$

(5.0)

$$\begin{array}{r} 4.9 \\ 0.0 \end{array} \quad \begin{array}{r} 4.90 \\ 4 \end{array} \quad \begin{array}{r} 6.3 \\ 15 \end{array} \quad \begin{array}{r} 7.5 \\ 62 \end{array} \quad \begin{array}{r} 9.3 \\ 68 \end{array} \quad \begin{array}{r} 10.1 \\ 90 \end{array} \quad \begin{array}{r} 8.9 \\ 93 \end{array} \quad \begin{array}{r} 9.5 \\ 110 \end{array} \quad \begin{array}{r} 11.9 \\ 117 \end{array} \quad \begin{array}{r} 13.3 \\ 161 \end{array} \quad \begin{array}{r} 13.9 \\ 200 \end{array}$$

(5.0)

$$\begin{array}{r} 5.0 \\ 0.0 \end{array} \quad \begin{array}{r} 5.6 \\ 17 \end{array} \quad \begin{array}{r} 6.6 \\ 24 \end{array} \quad \begin{array}{r} 7.6 \\ 64 \end{array} \quad \begin{array}{r} 8.3 \\ 93 \end{array} \quad \begin{array}{r} 8.9 \\ 112 \end{array} \quad \begin{array}{r} 10.7 \\ 121 \end{array} \quad \begin{array}{r} 11.5 \\ 134 \end{array} \quad \begin{array}{r} 13.2 \\ 150 \end{array} \quad \begin{array}{r} 13.9 \\ 200 \end{array}$$

(5.2)

$$\begin{array}{r} 5.8 \\ 0.0 \end{array} \quad \begin{array}{r} 6.0 \\ 14 \end{array} \quad \begin{array}{r} 6.5 \\ 29 \end{array} \quad \begin{array}{r} 6.9 \\ 54 \end{array} \quad \begin{array}{r} 7.4 \\ 100 \end{array} \quad \begin{array}{r} 7.2 \\ 133 \end{array} \quad \begin{array}{r} 8.5 \\ 150 \end{array} \quad \begin{array}{r} 12.4 \\ 182 \end{array} \quad \begin{array}{r} 12.7 \\ 200 \end{array}$$

(6.0)

$$\begin{array}{r} 6.0 \\ -8 \end{array} \quad \begin{array}{r} 6.6 \\ 0.0 \end{array} \quad \begin{array}{r} 6.6 \\ 43 \end{array} \quad \begin{array}{r} 7.1 \\ 100 \end{array} \quad \begin{array}{r} 7.4 \\ 138 \end{array} \quad \begin{array}{r} 8.6 \\ 172 \end{array} \quad \begin{array}{r} 10.7 \\ 190 \end{array} \quad \begin{array}{r} 11.6 \\ 200 \end{array}$$

(6.9)

$$\begin{array}{r} 6.9 \\ -14 \end{array} \quad \begin{array}{r} 6.4 \\ 0.0 \end{array} \quad \begin{array}{r} 6.1 \\ 29 \end{array} \quad \begin{array}{r} 6.2 \\ 58 \end{array} \quad \begin{array}{r} 7.1 \\ 100 \end{array} \quad \begin{array}{r} 7.2 \\ 122 \end{array} \quad \begin{array}{r} 6.7 \\ 128 \end{array} \quad \begin{array}{r} 7.1 \\ 144 \end{array} \quad \begin{array}{r} 8.2 \\ 158 \end{array} \quad \begin{array}{r} 8.9 \\ 194 \end{array} \quad \begin{array}{r} 10.0 \\ 200 \end{array}$$

(7.3)

$$\begin{array}{r} 7.2 \\ -21 \end{array} \quad \begin{array}{r} 6.5 \\ 13 \end{array} \quad \begin{array}{r} 6.7 \\ 0.0 \end{array} \quad \begin{array}{r} 6.0 \\ 10 \end{array} \quad \begin{array}{r} 5.5 \\ 38 \end{array} \quad \begin{array}{r} 6.8 \\ 100 \end{array} \quad \begin{array}{r} 6.5 \\ 127 \end{array} \quad \begin{array}{r} 7.9 \\ 140 \end{array} \quad \begin{array}{r} 8.4 \\ 200 \end{array} \quad \begin{array}{r} 7.9 \\ 204 \end{array}$$

(7.4)

$$\begin{array}{r} 7.1 \\ -11 \end{array} \quad \begin{array}{r} 5.6 \\ -5 \end{array} \quad \begin{array}{r} 5.9 \\ 0.0 \end{array} \quad \begin{array}{r} 5.6 \\ 13 \end{array} \quad \begin{array}{r} 4.6 \\ 22 \end{array} \quad \begin{array}{r} 4.4 \\ 37 \end{array} \quad \begin{array}{r} 5.9 \\ 100 \end{array} \quad \begin{array}{r} 6.6 \\ 144 \end{array} \quad \begin{array}{r} 7.5 \\ 200 \end{array} \quad \begin{array}{r} 7.6 \\ 213 \end{array} \quad \begin{array}{r} 5.4 \\ 221 \end{array}$$

(5.1)

$$\begin{array}{r} 5.5 \\ -9 \end{array} \quad \begin{array}{r} 5.8 \\ -5 \end{array} \quad \begin{array}{r} 5.7 \\ 0.0 \end{array} \quad \begin{array}{r} 5.6 \\ 7 \end{array} \quad \begin{array}{r} 3.4 \\ 25 \end{array} \quad \begin{array}{r} 4.9 \\ 63 \end{array} \quad \begin{array}{r} 5.5 \\ 100 \end{array} \quad \begin{array}{r} 6.0 \\ 125 \end{array} \quad \begin{array}{r} 6.0 \\ 158 \end{array} \quad \begin{array}{r} 6.8 \\ 200 \end{array} \quad \begin{array}{r} 7.3 \\ 214 \end{array} \quad \begin{array}{r} 3.9 \\ 219 \end{array}$$

(3.4)

$$\begin{array}{r} 2.3 \\ 0.0 \end{array} \quad \begin{array}{r} 0.0 \\ 7 \end{array} \quad \begin{array}{r} 0.8 \\ 24 \end{array} \quad \begin{array}{r} 1.5 \\ 39 \end{array} \quad \begin{array}{r} 4.6 \\ 51 \end{array} \quad \begin{array}{r} 5.4 \\ 78 \end{array} \quad \begin{array}{r} 5.4 \\ 100 \end{array} \quad \begin{array}{r} 5.8 \\ 147 \end{array} \quad \begin{array}{r} 5.8 \\ 192 \end{array} \quad \begin{array}{r} 6.2 \\ 204 \end{array} \quad \begin{array}{r} 0.3 \\ 211 \end{array}$$

(1.8)

Approve H.I

$$\begin{array}{r} 9.3 \\ 0.0 \end{array} \quad \begin{array}{r} 3.7 \\ 12 \end{array} \quad \begin{array}{r} 7.1 \\ 37 \end{array} \quad \begin{array}{r} 8.4 \\ 45 \end{array} \quad \begin{array}{r} 13.2 \\ 62 \end{array} \quad \begin{array}{r} 13.9 \\ 100 \end{array} \quad \begin{array}{r} 13.3 \\ 150 \end{array} \quad \begin{array}{r} 13.6 \\ 184 \end{array} \quad \begin{array}{r} 10.6 \\ 200 \end{array} \quad \begin{array}{r} 9.5 \\ 202 \end{array} \quad \begin{array}{r} 3.6 \\ 204 \end{array} \quad \begin{array}{r} 6.0 \\ 210 \end{array}$$

(9.0)

$$\begin{array}{r} 7.1 \\ 0.0 \end{array} \quad \begin{array}{r} 1.1 \\ 24 \end{array}$$

(7.1)

Sta.	+	H.I.	-	Red.	Elev.
		903.39			

2+07				6.3	
------	--	--	--	-----	--

2+13				5.2	
------	--	--	--	-----	--

2+23				3.9	
------	--	--	--	-----	--

T.P.	11.17	913.35	1.21	902.18	
------	-------	--------	------	--------	--

2+00					
------	--	--	--	--	--

2+07					
------	--	--	--	--	--

2+13					
------	--	--	--	--	--

2+23					
------	--	--	--	--	--

T.P.	0.77	902.95	11.17	902.18	
------	------	--------	-------	--------	--

T.P.	2.12	893.29	11.76	891.17	
------	------	--------	-------	--------	--

B.M.			3.89	887.40	889.41
------	--	--	------	--------	--------

Right.

$$\begin{array}{r} 6.3 \\ 00 \\ \hline 1.1 \\ 26 \end{array}$$

$$\begin{array}{r} 5.2 \\ 00 \\ \hline 0.5 \\ 24 \end{array}$$

$$\begin{array}{r} 3.9 \\ 00 \\ \hline 0.0 \\ 23 \end{array}$$

(17.1)

6.1	4.7	20.5	23.0	22.8	23.3	16.9	14.8	11.9	6.5	9.8
30	75	79	89	100	137	144	167	197	198	200

(5.8)

6.3	4.8	4.8	17.0	20.3	20.0	12.0	10.3	10.2	1.8	5.7
59	75	84	88	100	131	148	157	192	193	200

Above H.I.

(5.2)

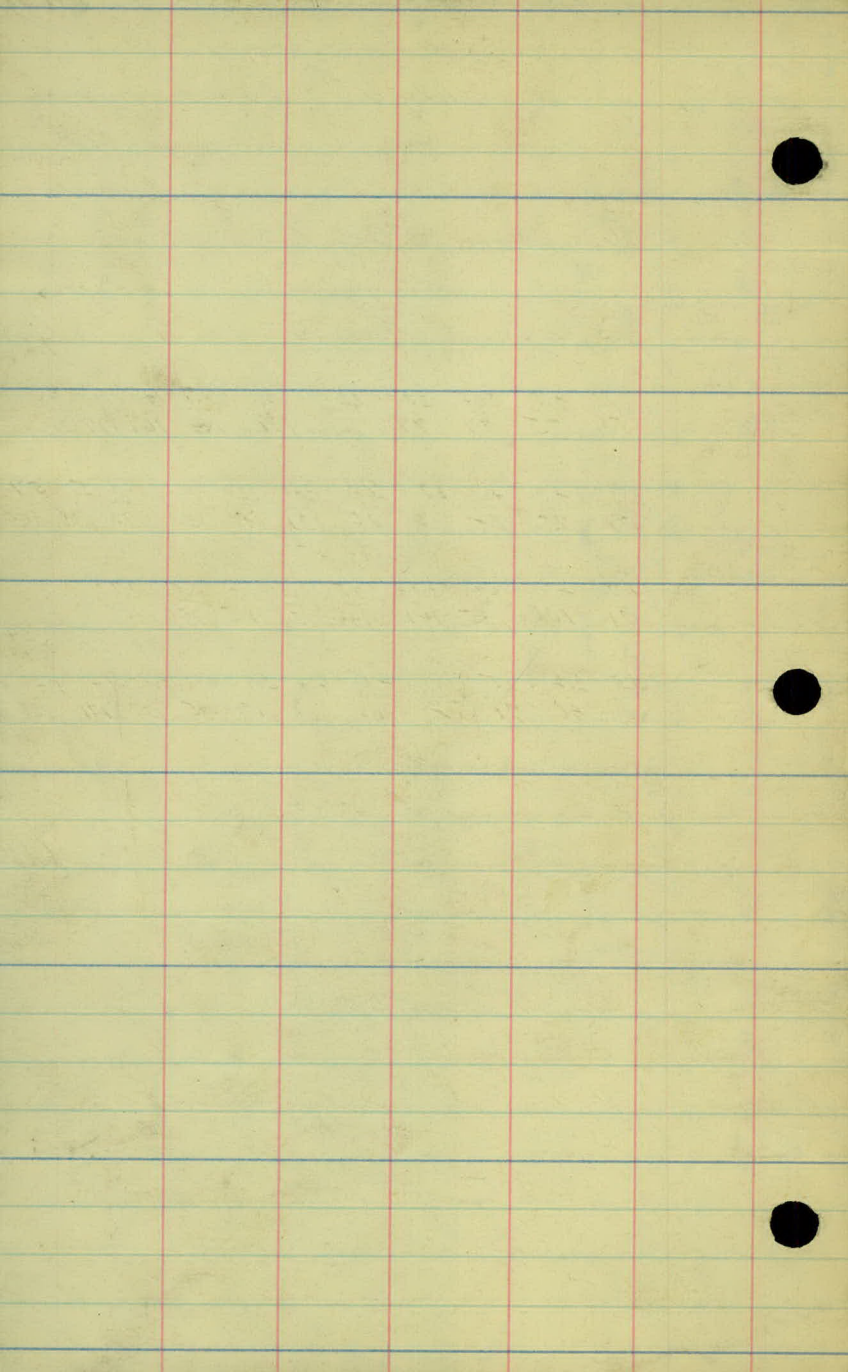
4.9	4.9	0.0	+1.4	9.5	6.2	6.4	0.0	4.7
71	100	135	141	144	154	185	186	200

Above H.I. 2.4

(4.5)

4.5	2.2	1.5	1.8	4.1	4.4	3.4	0.0	+4.5	+4.8	+4.0
48	60	71	82	100	108	119	135	158	171	180

same as original



Proj. #26-02,
Final x sections of
Sand Cut at McCarrons Beach.

Sta.	+	H.I.	-	Elev.
B.M.	3.55	846.55		843.00
0+00				

0+03

0+54

1+08

1+62

2+03

2+14

2+55

2+70

2+92

3+24

3+78

3+80

5/1/24

Left.

Same as Original X 500.

N.

7.3 5.6 5.7 4.5 7.7 8.1
685 658 645 600 585 575

(6.6)

7.3 6.1 5.4 5.2 4.7 4.5 9.3 9.0
642 630 600 583 550 527 517 500

6.6

7.3 6.1 6.0 5.1 4.7 9.1 9.5
600 585 550 500 454 445 400

(6.6)

7.3 6.0 5.5 5.1 4.5 4.4 4.7 9.9 9.9
542 550 500 450 430 400 383 371 350

(6.6)

7.3 6.0 6.1 5.4 5.3 4.7 7.5 7.2 7.4 6.4 5.4 4.8 4.5 4.5 4.5 5.1 3.6 3.4
534 521 500 450 414 331 321 272 250 200 150 100 75 50 34 30 20 00

(6.6)

7.3 6.7 5.9 5.4 4.8 4.6 4.2 7.1 6.5 5.8 5.1 5.1 8.0 6.9 4.1 4.3 3.8 3.3
527 518 500 450 400 350 319 308 250 200 150 135 100 55 48 33 23 00

6.6

7.3 5.9 5.3 4.5 4.0 5.8 5.0 7.5 7.1 6.0 7.4 7.3 3.6 3.1
506 485 410 350 312 304 254 245 200 182 100 43 34 00

6.6

7.3 5.7 5.6 4.8 4.0 5.8 4.7 7.4 6.8 7.2 7.1 7.4 3.8 3.0
474 472 400 350 312 306 258 252 200 150 100 43 40 00

6.6

7.3 6.4 5.5 5.7 4.7 4.3 5.1 4.4 7.0 6.9 6.7 6.4 7.0 3.6 2.9
478 471 450 400 350 310 303 267 263 217 150 50 40 28 00

(6.6)

7.3 6.4 5.8 5.6 5.0 4.5 5.8 6.4 6.5 5.5 6.6 3.2 2.9
467 463 450 400 350 310 307 254 150 63 40 25 00

(6.6)

7.3 5.9 5.4 4.6 4.8 5.4 6.2 5.4 5.0 5.3 5.5 3.2 2.6
457 441 400 350 300 250 200 150 100 50 34 21 00

6.6

6.0 5.4 5.4
215 165 150

579. + H.I. - Elev.

846.55

3785

3799

4713

4718

3.27 846.30 3.52 843.03.

4732

4763

4786

5740

5794

6715

6718

B.M.

3.28 843.02 843.00

5/1/26.

N

<u>5.9</u>	<u>6.1</u>	<u>8.6</u>	<u>7.8</u>	<u>5.2</u>	<u>5.1</u>
214	212	207	174	165	150

6.6

<u>5.8</u>	<u>5.9</u>	<u>8.2</u>	<u>8.7</u>	<u>6.0</u>
224	220	209	174	150

6.6

<u>5.2</u>	<u>5.0</u>	<u>8.0</u>	<u>7.4</u>	<u>5.4</u>	<u>5.6</u>
224	218	205	170	144	150

6.6

<u>5.0</u>	<u>5.1</u>	<u>5.1</u>	<u>5.3</u>
224	207	165	150

<u>7.3</u>	<u>5.9</u>	<u>5.5</u>	<u>4.7</u>	<u>4.1</u>	<u>5.4</u>	<u>4.3</u>	<u>5.5</u>	<u>5.6</u>	<u>5.4</u>	<u>4.7</u>	<u>5.4</u>	<u>3.0</u>	<u>2.4</u>
428	420	400	350	287	284	250	200	150	118	89	38	22	00

(6.3)

<u>7.3</u>	<u>6.0</u>	<u>4.8</u>	<u>4.0</u>	<u>6.1</u>	<u>5.8</u>	<u>4.4</u>	<u>5.1</u>	<u>5.4</u>	<u>6.9</u>	<u>7.7</u>	<u>8.7</u>	<u>8.7</u>	<u>3.3</u>	<u>2.6</u>
419	414	350	284	283	250	200	150	120	75	40	38	35	25	00

6.3

<u>7.3</u>	<u>5.7</u>	<u>5.4</u>	<u>3.8</u>	<u>6.7</u>	<u>6.4</u>
414	403	350	284	281	250

6.3

<u>7.3</u>	<u>6.2</u>	<u>5.4</u>	<u>4.7</u>	<u>4.0</u>	<u>7.4</u>	<u>7.8</u>
414	410	350	315	285	283	250

6.3

<u>7.3</u>	<u>6.2</u>	<u>5.4</u>	<u>5.0</u>	<u>4.5</u>	<u>4.1</u>	<u>7.2</u>	<u>7.6</u>
423	450	414	350	310	284	283	250

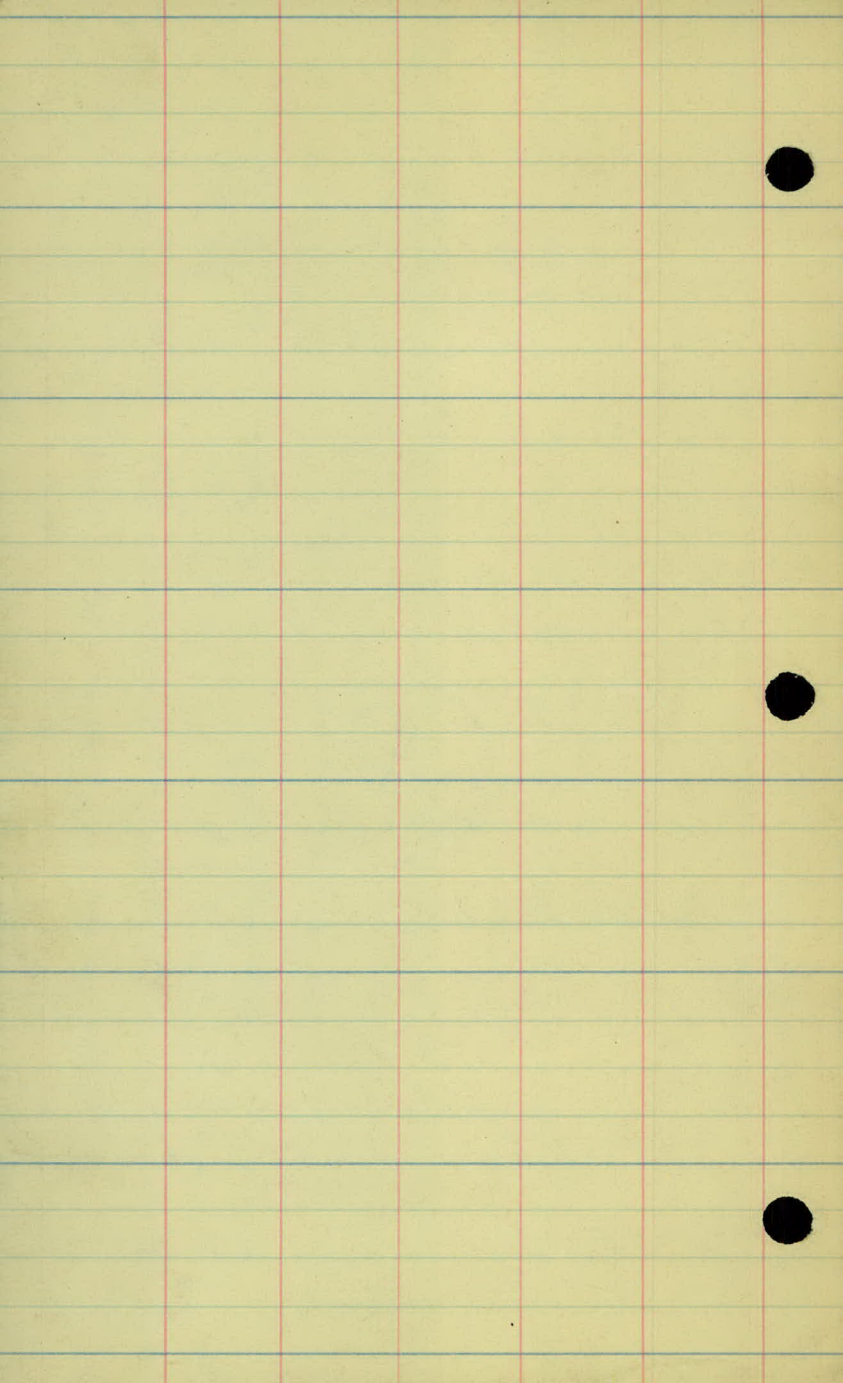
6.3

<u>7.3</u>	<u>6.0</u>	<u>4.7</u>	<u>5.7</u>	<u>5.2</u>	<u>5.0</u>	<u>4.3</u>	<u>7.0</u>	<u>8.3</u>
515	500	475	450	400	350	284	281	250

6.3

<u>7.3</u>	<u>6.0</u>	<u>5.8</u>	<u>5.7</u>	<u>6.1</u>	<u>5.6</u>	<u>6.8</u>	<u>7.1</u>
577	500	475	450	400	350	284	250

6.3



Proj. # 26-02

Bench Marks at H^o Carrons Beach.

Sta.	f	H.I.	-	Elev.
B.M.	3.48	847.68		844.20
T.P.	6.70	846.02	8.36	839.32 =
B.M.			3.02	843.00

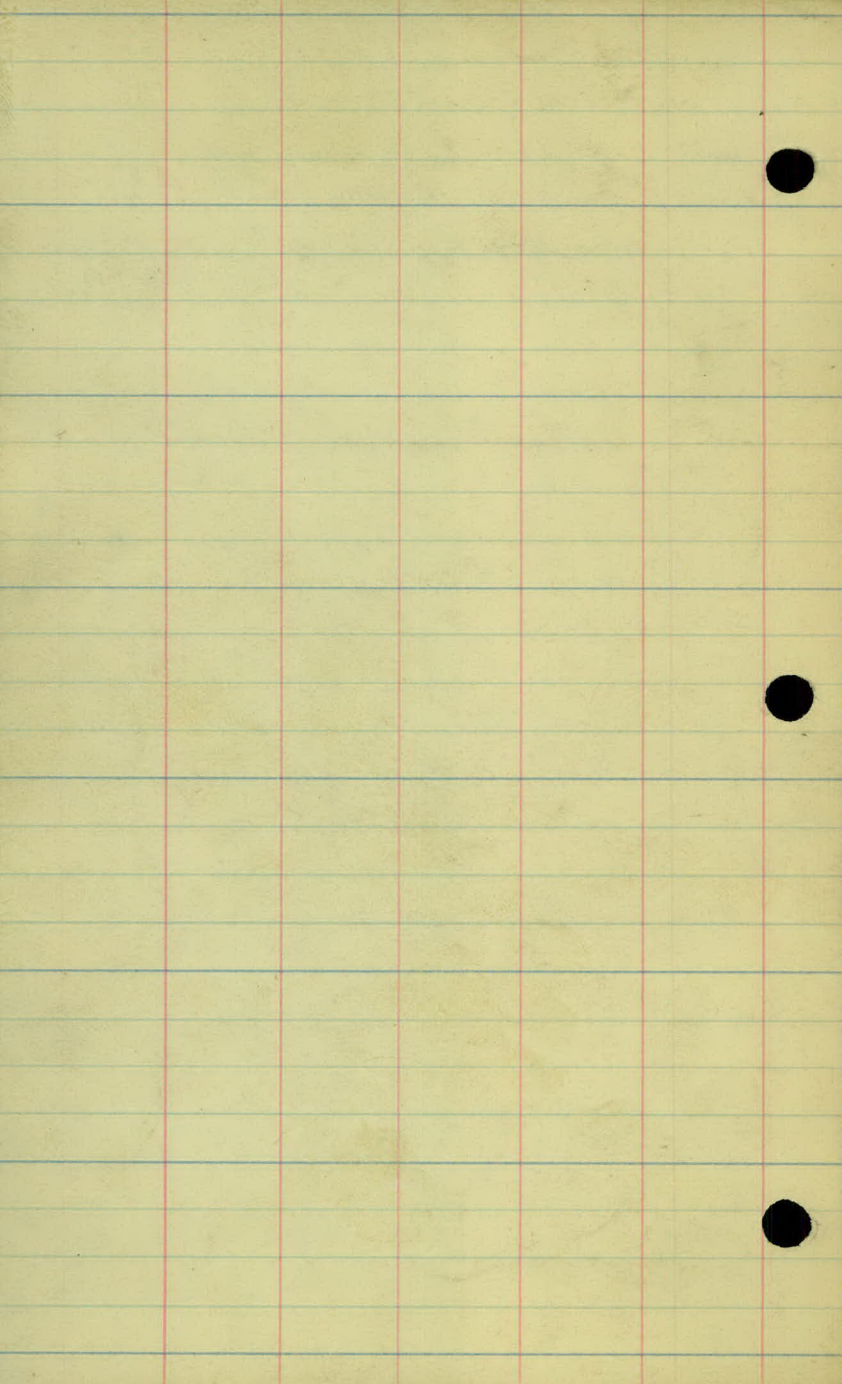
4/20/26

Lalle. Imp. on stump by old Ice Schute,

Water Elev. 4/20/24

Spr. in Twin Willow. 20' from Shore Line 10' N.

of Rice Sta. 2+70 Set. 4/20/26.



Proj. # 26-02.

X sections on Borrow Pit.
at McCarrons Blvd. S. & Rice St.

Sta.	+	H.I.	-	Elev.
B.M.	2.67	886.97		884.30
T.P.	9.24	894.68	1.55	885.42 ✓
B.M.			5.27	889.41 ✓
0+00	Mc Carrons Blvd. S.		4.76	889.92 ✓
0+11			4.73	889.95
0+15			4.45	890.03
0+25			4.9	889.8
0+42			5.7	889.0
0+54			6.6	888.1
0+87			7.0	887.7
1+08			7.1	887.6
1+38			4.8	889.9
1+54			3.1	891.6
T.P.	11.43	905.71	0.40	894.28 ✓
2+00			9.4	896.3
0+42				

Spr N. P.P. Lt. Sta 16+12 On Proj. # 26-02

RT.

Spr N. in P.P. 34 Rt. Sta. 0+50

4.76 $\frac{4.75}{15}$ $\frac{6.7}{50}$ $\frac{8.9}{100}$ $\frac{10.5}{200}$

4.7 $\frac{7.1}{50}$ $\frac{9.2}{100}$ $\frac{10.9}{200}$

4.7 $\frac{6.3}{34}$ $\frac{8.1}{50}$ $\frac{10.7}{100}$ $\frac{12.4}{150}$ $\frac{13.2}{200}$

4.9 $\frac{5.4}{14}$ $\frac{6.9}{17}$ $\frac{10.5}{100}$ $\frac{12.7}{150}$ $\frac{13.7}{200}$

5.7 $\frac{6.8}{4}$ $\frac{7.2}{14}$ $\frac{8.0}{41}$

6.6 $\frac{7.0}{9}$ $\frac{5.6}{17}$ $\frac{8.0}{45}$

7.0 $\frac{6.4}{9}$ $\frac{2.7}{15}$ $\frac{0.0}{34}$

7.1 $\frac{4.5}{14}$ $\frac{0.0}{13}$

4.8 $\frac{2.7}{12}$ $\frac{0.0}{20}$

3.1 $\frac{0.0}{14}$

9.4 $\frac{2.4}{30}$

16.7 $\frac{7.6}{41}$ $\frac{6.8}{80}$ $\frac{10.5}{100}$

Base line

Sta. + H. I. - Elev

905.71

0754

0787

1708

1738

1754

T.P. 12.44 717.85 0.30 905.41

0787

1708

1738

1754

2700

T.P. 1.05 906.87 12.03 905.82

0742

0754

0787

17.6	$\frac{7.7}{50}$	$\frac{4.8}{65}$	$\frac{3.0}{83}$	$\frac{4.4}{100}$					
18.0	$\frac{2.4}{63}$	$\frac{0.2}{75}$							
18.1	$\frac{5.3}{41}$	$\frac{0.0}{73}$							
15.8	$\frac{1.4}{50}$	$\frac{0.0}{55}$							
14.1	$\frac{3.6}{36}$	$\frac{0.0}{48}$							
30.2	$\frac{9.7}{100}$	$\frac{12.1}{121}$							
30.3	$\frac{9.7}{83}$	$\frac{7.3}{100}$	$\frac{7.3}{110}$	$\frac{8.0}{114}$	$\frac{12.4}{136}$				
28.0	$\frac{5.1}{82}$	$\frac{2.8}{93}$	$\frac{2.5}{100}$	$\frac{2.8}{120}$	$\frac{6.5}{138}$	$\frac{10.1}{150}$			
26.3	$\frac{5.7}{73}$	$\frac{3.6}{84}$	$\frac{2.1}{100}$	$\frac{1.5}{122}$	$\frac{2.4}{132}$	$\frac{4.7}{145}$	$\frac{10.0}{165}$		
21.6	$\frac{10.4}{54}$	$\frac{9.3}{74}$	$\frac{8.4}{100}$	$\frac{5.8}{125}$	$\frac{1.7}{150}$	$\frac{1.5}{164}$	$\frac{3.2}{176}$	$\frac{6.3}{186}$	$\frac{12.2}{200}$
17.9	$\frac{13.7}{114}$								
18.8	$\frac{9.7}{123}$	$\frac{11.9}{134}$							
19.2	$\frac{4.2}{137}$	$\frac{8.4}{150}$							

Sta. + H.I. - Elev.
906.87

1+08

1+38

1+54

2+00

T.P. 0.15 894.94 12.08 894.79

0+42

0+54

0+87

1+08

1+38

1+54

B.M. 1.52 890.74 5.52 887.42 887.41

B.M. 6.43 884.31 884.30

Rt.

$$19.3 \quad \frac{6.0}{150} \quad \frac{11.9}{168}$$

$$17.0 \quad \frac{5.3}{171} \quad \frac{10.5}{187}$$

$$15.3 \quad \frac{4.4}{182} \quad \frac{11.9}{200}$$

$$10.6 \quad \frac{7.3}{217} \quad \frac{10.5}{227} \quad \frac{14.5}{250}$$

$$5.9 \quad \frac{10.7}{160} \quad \frac{12.2}{171} \quad \frac{12.7}{200}$$

$$6.8 \quad \frac{9.6}{175} \quad \frac{11.5}{200}$$

$$7.2 \quad \frac{2.9}{167} \quad \frac{2.3}{183} \quad \frac{7.9}{200} \quad \frac{11.7}{215}$$

$$7.3 \quad \frac{7.4}{200} \quad \frac{9.1}{215}$$

$$5.0 \quad \frac{2.8}{200} \quad \frac{4.8}{211} \quad \frac{5.6}{225}$$

$$3.3 \quad \frac{2.8}{211} \quad \frac{4.4}{225}$$

SpK in P.P. 34 Mt. Sta.

SpK in P.P. 24 Sta 16 + 12 On Proj. # 26-62

