

Book #60-Dr #8

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey

DITCH # 16

From WATER DEP. R.W. To W. SH. L. GERVAIS

Road Acc't. No.

Date Filed.

File. 8

Purke Wm.
Skoog
Ball
Goldberg

Profile Levels Ditch #16
Sta. 0+00 to Sta. 48+00
(Water Dept R/W)

Sta	+	π	-	Elev
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B.M.	3.80	203.80		200.00 Assumed
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0	0.28	191.15	12.93	190.87
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0	0.24	178.28	13.11	178.04
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B.M.	5.64	183.36	10.39	167.89 = 177.72 ^{Not Part Datum mg}
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0+00	Weir @ Rear School			73.6
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1				73.4
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2				73.7
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3				73.7
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4				74.1
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0	7.63	184.11	6.88	176.48
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5				74.4
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6				75.0
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183.36
 688
 176.48

RR. SpKin TP @ W/W R/W and Little Canada

Crest Weir @ rear Little Canada School

9.8

10.0

9.7

9.7

9.3

$\frac{1.7}{20}$ $\frac{1.7}{14}$ $\frac{3.4}{11}$ $\frac{5.4}{7}$ $\frac{8.6}{2}$ $\frac{9.6}{2}$ 9.7 $\frac{9.6}{2}$ $\frac{8.6}{2}$ $\frac{6.6}{6}$ $\frac{3.6}{13-20}$

9.1

Sta	+	π	-		Elev
		184.11			
7					74.9
8					75.0
①	7.69	184.81	6.99	177.12	
9					75.1
9 +21		Outlet 42" Conc. Pipe			75.31
①	3.58	186.51	1.88	182.93	
10		Top Ground over Pipe			83.2
11		Top Ground over Pipe			83.9
+81		Inlet 42" Conc. Pipe			75.48
①	4.70	185.02	6.19	180.32	
12					75.9
13					75.6
14					75.6

Lt

$$\begin{array}{r} 184.81 \\ 1.88 \\ \hline 2.93 \end{array}$$

Rt

9.2

9.1

$$\begin{array}{r} 9.7 \\ 2 \end{array} \quad 9.7 \quad \begin{array}{r} 9.7 \\ 2 \end{array} \quad \begin{array}{r} 2.0 \\ 11 \end{array} \quad \begin{array}{r} 2.6 \\ 20 \end{array}$$

$$\begin{array}{r} 0.7 \\ 20-11 \end{array} \quad 9.50 \text{ Flow Line}$$

3.3

2.6

11.03 Flow Line

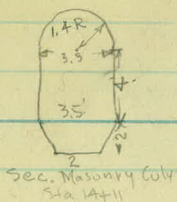
Top Center Head Wall Sta 11+81

9.1

9.4

$$\begin{array}{r} 3.0 \\ 20-9 \end{array} \quad \begin{array}{r} 9.4 \\ 2 \end{array} \quad 9.4 \quad \begin{array}{r} 9.4 \\ 2 \end{array} \quad \begin{array}{r} 6.4 \\ 3 \end{array} \quad \begin{array}{r} 3.2 \\ 9-20 \end{array}$$

Sta	+	π	-	Elev
		185.02		
14+11		Outlet Masonry Arch		75.62
①	12.47	196.22	1.27	183.75
14+15		Outlet Masonry Arch		
B.M.			8.35	187.87
②	3.86	186.96	13.12	183.10
14+65		Inlet Masonry Culv		75.79
15				75.7
16				75.8
+21		Outlet 36" Tile Pipe		76.11
17		Top Ground over Pipe		80.3
18		" " " "		80.8
+82		Inlet 36" Tile Pipe		76.21
19				76.2



9.40 Flow Line

S.W. Cor. Headwall Sta. 14+65

11.17 Flow Line

$$\frac{3.7}{20-16} \quad \frac{10.1}{3} \quad \frac{11.2}{2} \quad 11.3 \quad \frac{11.5}{3} \quad \frac{10.0}{4} \quad \frac{9.2}{7} \quad \frac{5.0}{12-20}$$

11.2

10.85

6.7

6.2

10.75 Flow Line

10.8

Sta	+	x	-	Elev
		186.96		
①	5.97	185.46	7.47	179.49
20				76.7
+45		Outlet 36" Tile Pipe		76.44
21 +03		Inlet 36" Tile Pipe		76.58
22				76.8
23				77.5
24				77.9
②	7.59	185.35	7.70	177.76
25				77.6
+82.7		Outlet 36" Tile Pipe		76.93
26		Top Ground Over Pipe		81.7
27		" " " "		80.9
+76		Inl. 36" Tile Pipe		77.00

$$\frac{0.8}{20-15} \quad \frac{8.0}{5} \quad \frac{8.0}{3} \quad \frac{9.0}{2} \quad 8.8 \quad \frac{8.7}{2} \quad \frac{8.0}{2} \quad \frac{7.5}{5} \quad \frac{0.5}{16-20}$$

9.02 F.L.

8.88 F.L.

8.7

8.0

7.6

Note Washout @ Sta 25+25
filled Ditch being dug out
by E.R.A.

5.5
2.8

$$\begin{array}{ccccccccccc} \text{Over H.L.} & & & & & & & & & & \text{Over H.L.} \\ +2.0 & 4.5 & 5.0 & 7.7 & 7.8 & 7.8 & 5.1 & 3.8 & +1.7 & & \\ \hline 14 & 7 & 4 & 2 & & 2 & 4 & 8 & 13 & 20 & \end{array}$$

8.42 F.L.

3.7

4.5

8.35 F.L.

Sta	+	π	-		Elev
		185.35			
28					77.6
29					76.9
①	3.80	183.69	5.46	179.89	
30					77.4
31					77.5
32					78.0
33					77.7
34					78.5
35					78.7
36					78.2
②	10.40	189.58	4.51	179.18	
37					77.3

8.4

8.5

$$\begin{array}{cccccccccc}
 +3.0 & 00 & 4.0 & 6.0 & 6.3 & 6.3 & 4.0 & 00 & +1.0 \\
 20 - 15 & 10 & 3 & 2 & 2 & 2 & 3 & 8 & 15
 \end{array}$$

6.2

5.7

6.0

5.2

$$\begin{array}{cccccccccc}
 +1.0 & 00 & 5.0 & 5.0 & 5.0 & 4.0 & 1.0 & +3.0 & +4.0 \\
 15 & 9 & 2 & 2 & 2 & 6 & 11 & 17 & 25
 \end{array}$$

5.5

12.3

Sta	+	π	-	Elev.
		189.58		
38				77.8
39				77.7
40				77.9
41				77.3
42				77.3
+58.5	Outlet 42" Conc. Pipe			78.50
43	Top Ground over Pipe			83.0
44	"	"	" "	84.3
+21	Inlet 42" Conc. Pipe			79.33
B.M.		4.63	184.95	184.95
45				78.4
46				79.0

4.63

11.8

11.9

$$\frac{4.2}{25-20} \quad \frac{6.2}{12} \quad \frac{10.2}{5-3} \quad \frac{11.7}{2} \quad 11.7 \quad \frac{11.7}{2} \quad \frac{5.8}{11-20}$$

12.3

12.3

11.08 F.L.

3.6

5.3

10.25 F.L.

Top Cor. Wing Wall Sta 44+21

$$\frac{4.6}{20-12} \quad \frac{11.1}{4} \quad 11.2 \quad \frac{11.1}{3} \quad \frac{7.4}{10-15}$$

10.6

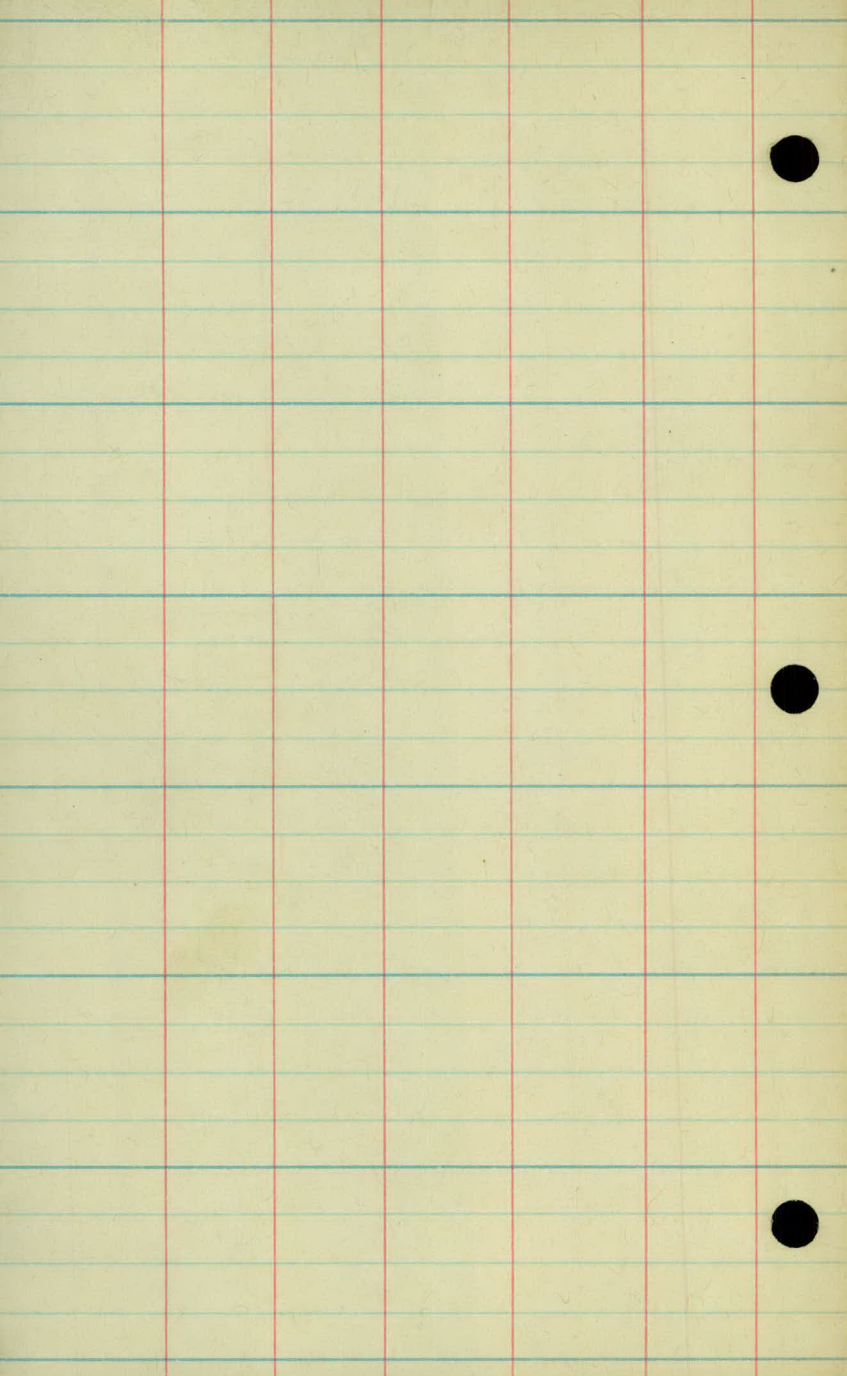
Sta	+	π	-	Elev
		189.58		

47				79.2
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48				79.4
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10.4

10.2



X-Sections

Ditch #16 - South End
from

E. Water Dept. R.W to W. Shore Lake Genvais
Sta 0+00 to Sta 30+25

Sta.	+	Δ	-	Elev.
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B.M.	280	180.52		177.72
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0+00				73.6
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+30				73.3
-----	--	--	--	------

+62				73.5
-----	--	--	--	------

1				73.7
---	--	--	--	------

①	3.29	179.35	446	176.06
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+75	Beg New School Fill Rt			
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2				73.7
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+33	Fce Crosses			
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+50				74.0
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3				73.9
---	--	--	--	------

+30	ctr. Fill Wash			73.8
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Crest Weir So. Sta. 0+00

$$\frac{4.2}{15} \quad \frac{3.8}{6} \quad \frac{7.0}{3} \quad 6.9 \quad \frac{7.2}{4} \quad \frac{4.8}{5} \quad \frac{3.4}{8} \quad \frac{4.0}{9}$$

Curb Apron
Apron of Weir
WS 67/35 = 6.55

$$\frac{4.3}{15} \quad \frac{3.4}{8} \quad \frac{6.2}{3} \quad \frac{6.2-7.1}{2} \quad 7.2 \quad \frac{6.5}{4} \quad \frac{4.0}{7} \quad \frac{3.7}{15}$$

$$\frac{5.1}{15} \quad \frac{4.6}{7} \quad \frac{6.5}{2} \quad 7.0 \quad \frac{6.9}{2} \quad \frac{5.0}{4} \quad \frac{4.0}{15}$$

$$\frac{3.8}{12} \quad \frac{Fcc}{8} \quad \frac{5.0}{7} \quad \frac{5.6}{3} \quad \frac{6.6}{2} \quad 6.8 \quad \frac{6.6}{2} \quad \frac{5.5}{4} \quad \frac{3.8}{15}$$

$$\frac{4.4}{15} \quad \frac{Fcc}{8} \quad \frac{4.4}{3} \quad \frac{5.1}{3} \quad 5.7 \quad \frac{5.1}{3} \quad \frac{4.7}{4} \quad \frac{2.2}{9} \quad \frac{T.S.}{15}$$

$$\frac{3.5}{15} \quad \frac{3.3}{7} \quad \frac{4.1}{2} \quad \frac{5.4}{1} \quad 5.4 \quad \frac{5.4}{2} \quad \frac{5.0}{3} \quad \frac{4.2}{9} \quad \frac{3.5}{16} \quad \frac{T.S.}{30}$$

$$\frac{3.4}{15} \quad \frac{2.8}{9} \quad \frac{4.6}{4} \quad \frac{5.0}{1} \quad \frac{5.5}{1} \quad 5.5 \quad \frac{5.1}{1} \quad \frac{5.0}{5} \quad \frac{4.3}{6} \quad \frac{Fcc}{16} \quad \frac{T.S.}{41}$$

$$\frac{3.0}{16} \quad \frac{1.6}{8} \quad \frac{4.6}{1} \quad 5.6 \quad \frac{4.8}{1-4} \quad \frac{2.7}{5} \quad \frac{1.3}{15} \quad \frac{T.S.}{34}$$

Sta.	+	Δ	-	Elev.
		179.35		
3+60				73.7
4				73.6
	+17	Fence Crosses		
①	6.65	180.99	5.01	174.34
				73.4
5				
6				72.7
	+15	End School Fill Rt		
7				72.4
①	10.97	183.46	8.50	172.49
BM			7.70	175.76
8				72.0
①	5.88	178.67	106.7	172.79
9				71.9
	+30	Fce Crosses		

$$\frac{2.4}{15} \quad \frac{4.0}{5} \quad \frac{5.4}{1} \quad 5.7 \quad \frac{5.0}{2.5} \quad \frac{2.7}{9} \quad \frac{1.4}{20} \quad \text{T.S.}$$

$$\frac{3.1}{15} \quad \frac{4.8}{7} \quad \frac{5.8}{2} \quad 5.8 \quad \frac{5.4}{3} \quad \frac{4.2}{5} \quad \frac{\text{Fcc}}{11} \quad \frac{\text{T.S.}}{3.1} \quad \frac{1.5}{15}$$

$\frac{\text{Fcc}}{5} \quad \frac{\text{Fcc}}{10}$

$$\frac{5.4}{15} \quad \frac{\text{Fcc}}{9} \quad \frac{6.4}{4} \quad \frac{7.6}{3} \quad 7.6 \quad \frac{7.6}{3} \quad \frac{6.0}{4} \quad \frac{4.0}{15} \quad \frac{1.5}{32}$$

$$\frac{6.7}{15} \quad \frac{\text{Fcc}}{7} \quad \frac{7.0}{3} \quad \frac{8.3}{2} \quad 8.3 \quad \frac{8.3}{2} \quad \frac{7.3}{3} \quad \frac{6.8}{15} \quad \frac{\text{T.S.}}{5.5} \quad \frac{5.5}{26}$$

$$\frac{7.4}{15} \quad \frac{\text{Fcc}}{14} \quad \frac{6.6}{3} \quad \frac{8.6}{2} \quad 8.6 \quad \frac{8.6}{2} \quad \frac{6.6}{3} \quad \frac{6.6}{15}$$

SpKin 30" Cot. Wood. 4' Rt. Sta. 7+75

$$\frac{3.8}{20} \quad \frac{\text{Fcc}}{10} \quad \frac{6.7}{10} \quad \frac{11.4}{2} \quad 11.5 \quad \frac{11.4}{2} \quad \frac{10.0}{5} \quad \frac{9.5}{15}$$

$$\frac{4.2}{15} \quad \frac{\text{Fcc}}{12} \quad \frac{5.2}{4} \quad \frac{6.7}{2} \quad 6.8 \quad \frac{6.7}{2} \quad \frac{5.0}{5} \quad \frac{6.0}{8} \quad \frac{5.8}{15}$$

$$\frac{\text{Fcc}}{15}$$

$$\frac{\text{Fcc}}{20}$$

Sta	+	π	-	Elev
		178.67		

10				71.4
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11				71.0
----	--	--	--	------

12				70.7
----	--	--	--	------

	+	Ctr FE Bridge		
①	4.02	175.61	7.08	171.59

13				69.8
----	--	--	--	------

14				69.1
----	--	--	--	------

	+75			68.5
--	-----	--	--	------

5	+90	Old Centerville Rd R/L	68.4	
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15				68.4
----	--	--	--	------

	+10			68.3
--	-----	--	--	------

16				68.2
----	--	--	--	------

$$\frac{5.0}{17} \frac{5.8}{4} \frac{7.1}{2} 7.3 \frac{7.0}{3} \frac{6.5}{4} \frac{6.0}{20} \text{ Fee}$$

$$\frac{6.5}{20} \frac{6.8}{4} \frac{7.1}{3} 7.7 \frac{7.7}{3} \frac{6.5}{4} \frac{6.2}{19} \text{ Fee}$$

$$\frac{3.6}{14} \frac{5.6}{5} \frac{8.0}{2} 8.0 \frac{7.8}{3} \frac{6.6}{4} \frac{5.6}{13} \frac{3.4}{18} \text{ Fee}$$

$$\frac{4.5}{15} \frac{4.2}{6} \frac{5.1}{2} 5.8 \frac{5.8}{1} \frac{4.6}{3} \frac{4.0}{5} \frac{3.6}{15}$$

$$\frac{5.2}{15} \frac{4.7}{5} \frac{6.0}{2} 6.5 \frac{5.8}{3} \frac{4.9}{5} \frac{5.0}{15}$$

$$\frac{5.5}{15} \frac{5.6}{3} \frac{7.1}{2} 7.1 \frac{7.1}{2} \frac{5.2}{4} \frac{4.5}{8} \frac{6.8}{15}$$

$$15 - \frac{0.0}{10} \frac{6.8}{2} 7.2 \frac{7.0}{2} \frac{5.8}{5} + \frac{0.5}{13}$$

$$\frac{2.5}{9} \frac{7.2}{1} 7.2 \frac{6.8}{3} \frac{1.2}{10-15}$$

$$\frac{5.6}{15} \frac{5.6}{5} \frac{7.2}{2} 7.3 \frac{7.3}{2} \frac{5.5}{5} \frac{4.2}{10} \frac{3.5}{15}$$

$$\frac{6.4}{15} \frac{6.0}{5} \frac{7.4}{2} 7.4 \frac{7.4}{2} \frac{6.2}{5} \frac{6.2}{15}$$

Sta	+	π	-	Elev
		175.61		

17				67.8
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①	2.55	172.57	5.59	170.02
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18				67.6
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19				67.4
----	--	--	--	------

20				67.3
----	--	--	--	------

21				66.8
----	--	--	--	------

+09	Fce			
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+15				66.4
-----	--	--	--	------

①			5.67	166.90
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BM			1.30	171.27
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B.M.	Topo + Rock in V. Elev. Cul.	166.90		
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380	170.70	166.90		
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21+70	Flow line Masonry Culv.	66.1		
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22+00				66.0
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$$\frac{6.1}{15} \quad \frac{5.8}{5} \quad \frac{7.8}{2} \quad 7.8 \quad \frac{7.8}{2} \quad \frac{5.8}{5} \quad \frac{6.2}{15}$$

$$\frac{4.7}{15} \quad \frac{3.7}{5} \quad \frac{5.0}{2} \quad 5.0 \quad \frac{4.8}{3} \quad \frac{3.8}{5} \quad \frac{3.6}{16}$$

$$\frac{4.2}{15} \quad \frac{3.6}{6} \quad \frac{5.1}{2} \quad 5.2 \quad \frac{5.1}{2} \quad \frac{3.8}{5} \quad \frac{3.6}{15}$$

$$\frac{4.2}{15} \quad \frac{4.1}{5} \quad \frac{5.2}{2} \quad 5.3 \quad \frac{5.2}{2} \quad \frac{4.4}{4} \quad \frac{4.0}{15}$$

$$\frac{4.2}{15} \quad \frac{4.1}{5} \quad \frac{5.6}{2} \quad 5.8 \quad \frac{5.6}{2} \quad \frac{4.0}{4} \quad \frac{2.2}{15}$$

Edgerton St

Inl. 15 x 4.7' Masonry Culv 6.2 ^{Flow Line Inlet} Thru Edgerton St. 53' long

Rock @ Inl Culv 21+15

SpKin "H" Pole 12' Rt. Sta. 21+00

46

$$\frac{3.0}{15} \quad \frac{2.4}{4} \quad \frac{4.7}{1} \quad 4.7 \quad \frac{4.7}{1} \quad \frac{2.7}{3} \quad \frac{2.4}{15}$$

+ H.1 - EIV
170⁷⁰

23+00 65.6 65.6

24+00 65.0

~~25+00~~ 64.9

26+00 25+00 64.9

27+00 26+00 64.8

T.P. 77' 174⁶¹ 43' 166.39

26+11 INV. 60" Corr. Culv 30' long 64.5

26+41 outlet of Culv. 64.5

27+00 65.4

27+60 65.3

28+00 65.2

29+00 64.8

29+45 64.5

$$\frac{2.7}{15} \quad \frac{3.2}{3} \quad \frac{5.1}{1} \quad 5.1 \quad \frac{5.1}{1} \quad \frac{2.8}{4} \quad \frac{2.8}{15}$$

$$\begin{array}{r} 16690 \\ 1771 \\ \hline 174.61 \end{array}$$

$$\frac{35}{15} \quad \frac{35}{4} \quad \frac{57}{2} \quad 57 \quad \frac{57}{2} \quad \frac{34}{4} \quad \frac{35}{15}$$

$$\frac{32}{15} \quad \frac{35}{5} \quad 58 \quad \frac{58}{2} \quad \frac{38}{5} \quad \frac{40}{15}$$

$$\frac{34}{15} \quad \frac{47}{5} \quad \frac{57}{4} \quad 59 \quad \frac{58}{3} \quad \frac{47}{5} \quad \frac{47}{15}$$

$$10^1$$

$$10^1$$

$$\frac{76}{15} \quad \frac{80}{8} \quad \frac{92}{6} \quad 92 \quad \frac{92}{3} \quad \frac{75}{6} \quad \frac{75}{15}$$

$$\frac{75}{15} \quad \frac{82}{6} \quad \frac{93}{3} \quad 93 \quad \frac{94}{4} \quad \frac{74}{8} \quad \frac{65}{15}$$

$$\frac{82}{15} \quad \frac{82}{7} \quad \frac{95}{4} \quad 94 \quad \frac{94}{4} \quad \frac{80}{7} \quad \frac{75}{15}$$

$$\frac{84}{15} \quad \frac{84}{10} \quad \frac{95}{7} \quad 98 \quad \frac{97}{5} \quad \frac{80}{8} \quad \frac{80}{15}$$

$$\frac{91}{20} \quad \frac{85}{10} \quad \frac{98}{6} \quad 101 \quad \frac{91}{7} \quad \frac{91}{12} \quad \frac{84}{25}$$

+ H.I - EIV
1746'

30+00

64.1

Top of Water 1645' Lake Gervais

30+25

End Dt. #16 ^{64.0} So. End.

B.M. E. 184.95 Top. S.W. Cor. Wing Wall. Sta. 44

$$\begin{array}{r} 80 \\ 20 \end{array} \quad \begin{array}{r} 75 \\ 9 \end{array} \quad \begin{array}{r} 98 \\ 4 \end{array} \quad 105 \quad \begin{array}{r} 105 \\ 3 \end{array} \quad \begin{array}{r} 83 \\ 11 \end{array} \quad \begin{array}{r} 52 \\ 15 \end{array}$$

10¹⁰

Lake Gervais

$$\begin{array}{r} 114 \\ 15 \end{array}$$

116

$$\begin{array}{r} 112 \\ 15 \end{array}$$

	+	H.1	-	EIV.	Stroog Bell	June 13-35
B.M	392	18887		18495	goloberg	
48+00					79.4	4806' No of Weir @ New Canada School
48+33					79.72	INV. TWIN 30" X 20' CORR
48+53					79.57	Flow line of Culv.
49+00					79.2	
T.P.	616	18681	822	18065		
50+00					78.3	Approx W.W. R/W
51+00					78.2	
52+00					78.6	
53+00					78.0	
53+70					77.6	int of ditch
54+00					77.7	
55+00					78.1	
56+00					78.8	

Top of S.W. Wing Wall Sta. 44+00

$\frac{47}{15}$ $\frac{50}{11}$ $\frac{87}{5}$ $\frac{94}{4}$ 95 $\frac{93}{3}$ $\frac{85}{3}$ $\frac{33}{13}$ $\frac{33}{20}$

915

930

$\frac{46}{20}$ $\frac{62}{9}$ $\frac{88}{5}$ $\frac{88}{3}$ $\frac{26}{2}$ 97 $\frac{97}{3}$ $\frac{91}{4}$ $\frac{86}{6}$ $\frac{40}{15}$ $\frac{40}{20}$

$\frac{53}{15}$ $\frac{54}{9}$ $\frac{82}{5}$ 85 $\frac{83}{5}$ $\frac{44}{12}$ $\frac{42}{20}$

$\frac{41}{15}$ $\frac{52}{9}$ $\frac{76}{5}$ $\frac{84}{3}$ 86 $\frac{82}{3}$ $\frac{77}{6}$ $\frac{48}{10}$ $\frac{48}{15}$

$\frac{48}{13}$ $\frac{56}{6}$ $\frac{79}{3}$ 82 $\frac{80}{4}$ $\frac{72}{7}$ $\frac{47}{11}$ $\frac{41}{17}$

$\frac{60}{15}$ $\frac{57}{10}$ $\frac{85}{5}$ 88 $\frac{83}{6}$ $\frac{48}{12}$ $\frac{44}{20}$

$\frac{92}{25}$ 92 $\frac{88}{8}$ $\frac{58}{13}$ $\frac{58}{20}$

E of ditch

$\frac{57}{15}$ $\frac{57}{9}$ $\frac{64}{7}$ $\frac{82}{4}$ 91 $\frac{81}{8}$ $\frac{68}{8}$ $\frac{55}{15}$ $\frac{58}{20}$

$\frac{60}{15}$ $\frac{60}{8}$ $\frac{82}{5}$ 87 $\frac{82}{4}$ $\frac{72}{6}$ $\frac{55}{9}$ $\frac{45}{16}$

$\frac{5.5}{16}$ $\frac{5.2}{10}$ $\frac{7.6}{3}$ 8.0 $\frac{7.3}{5}$ $\frac{4.6}{10}$ $\frac{4.3}{16}$

186.91

0 9.41 190.49 5.73 181.08

57 78.4

58 77.7

59 78.5

60 78.5

61 77.7

62 77.9

+84 F.L. 48" x 20 L.M. Field Xing 177.41
177.31

63 + 04 77.3

0 4.37 185.84 9.02 181.47

186.81
573
181.08

$$\begin{array}{r} 8.3 \\ 15 \overline{) 8} \end{array} \quad \begin{array}{r} 11.4 \\ 2 \end{array} \quad 12.1 \quad \begin{array}{r} 11.3 \\ 2 \end{array} \quad \begin{array}{r} 8.1 \\ 10 \end{array} \quad \begin{array}{r} 7.5 \\ 15 \end{array}$$

$$\begin{array}{r} 9.7 \\ 15 \overline{) 8} \end{array} \quad \begin{array}{r} 12.1 \\ 3 \end{array} \quad 12.8 \quad \begin{array}{r} 12.6 \\ 3 \end{array} \quad \begin{array}{r} 8.3 \\ 13 \end{array} \quad \begin{array}{r} 7.5 \\ 20 \end{array}$$

$$\begin{array}{r} 8.0 \\ 15 \overline{) 8} \end{array} \quad \begin{array}{r} 11.6 \\ 2 \end{array} \quad 12.0 \quad \begin{array}{r} 11.1 \\ 3 \end{array} \quad \begin{array}{r} 7.5 \\ 12 \end{array} \quad \begin{array}{r} 6.1 \\ 20 \end{array}$$

$$\begin{array}{r} 7.4 \\ 15 \overline{) 10} \end{array} \quad \begin{array}{r} 11.4 \\ 3 \end{array} \quad 12.0 \quad \begin{array}{r} 11.1 \\ 3 \end{array} \quad \begin{array}{r} 7.0 \\ 10 \end{array} \quad \begin{array}{r} 5.9 \\ 20 \end{array}$$

$$\begin{array}{r} 9.6 \\ 15 \overline{) 10} \end{array} \quad \begin{array}{r} 12.2 \\ 3 \end{array} \quad 12.8 \quad \begin{array}{r} 12.4 \\ 3 \end{array} \quad \begin{array}{r} 9.4 \\ 10 \overline{) 15} \end{array}$$

$$\begin{array}{r} 9.5 \\ 15 \end{array} \quad \begin{array}{r} 10.5 \\ 8 \end{array} \quad \begin{array}{r} 12.3 \\ 5 \end{array} \quad 12.6 \quad \begin{array}{r} 12.3 \\ 6 \end{array} \quad \begin{array}{r} 10.3 \\ 10 \end{array} \quad \begin{array}{r} 10.2 \\ 15 \end{array}$$

13.08
1318

$$\begin{array}{r} 10.4 \\ 15 \end{array} \quad \begin{array}{r} 10.8 \\ 8 \end{array} \quad \begin{array}{r} 12.4 \\ 4 \end{array} \quad 13.2 \quad \begin{array}{r} 12.8 \\ 2 \end{array} \quad \begin{array}{r} 10.9 \\ 3 \end{array} \quad \begin{array}{r} 10.0 \\ 10 \overline{) 15} \end{array}$$

Sta	+	π	-	1
		185.84		

64				77.3
----	--	--	--	------

65				77.7
----	--	--	--	------

66				77.8
----	--	--	--	------

0	5.78	186.57	5.05	180.79
---	------	--------	------	--------

67				78.0
----	--	--	--	------

	5.78	186.57	5.05	180.79
--	------	--------	------	--------

68				78.2
----	--	--	--	------

+59	48" X 14 CM	Field Xing		77.77 77.77
-----	-------------	------------	--	----------------

68 +91	Lateral Dt. Lt			78.4
--------	----------------	--	--	------

68 +91	36" X 42' CM	Road		78.37 78.67
--------	--------------	------	--	----------------

70				78.3
----	--	--	--	------

71				78.5
----	--	--	--	------

72				78.7
----	--	--	--	------

$$\frac{5.4}{15} \frac{6.1}{6} \frac{8.5}{4} \quad 8.5 \quad \frac{8.5}{5} \quad \frac{6.5}{6} \quad \frac{5.0}{10-15}$$

$$\frac{4.9}{15} \frac{5.6}{7} \frac{7.7}{4} \quad 8.1 \quad \frac{7.7}{5} \quad \frac{6.5}{7} \quad \frac{5.5}{15}$$

$$\frac{3.9}{15} \frac{4.8}{10} \frac{7.5}{4} \quad 8.0 \quad \frac{7.6}{3} \quad \frac{4.8}{6} \quad \frac{4.3}{15}$$

$$\frac{5.3}{15-10} \frac{6.1}{6} \frac{8.0}{3} \quad 8.6 \quad \frac{7.9}{4} \quad \frac{5.1}{10} \quad \frac{4.7}{15}$$

$$\frac{5.2}{15} \frac{5.9}{8} \frac{7.9}{4} \quad 8.4 \quad \frac{7.8}{3} \quad \frac{5.0}{8-15}$$

8.80.0ut

8.80.1inl

$$\frac{5.2}{20} \frac{5.4}{9} \frac{8.0}{4} \quad 8.2 \quad \frac{8.4}{3} \quad \frac{6.4}{7} \quad \frac{4.6}{15}$$

8.20.0ut

7.90.1inl

$$\frac{5.3}{15-10} \frac{8.3}{4} \quad 8.3 \quad \frac{8.0}{4} \quad \frac{5.1}{10} \quad \frac{5.4}{20}$$

8.1

$$\frac{4.9}{15-11} \frac{7.7}{4} \quad 7.7 \quad \frac{7.6}{4} \quad \frac{5.2}{10} \quad \frac{5.4}{15}$$

Sta	+	π	-	Elev.
		186.57		

73				79.2
----	--	--	--	------

0	4.10	186.59	4.08	182.49
---	------	--------	------	--------

74				79.5
----	--	--	--	------

75				80.0
----	--	--	--	------

76				80.2
----	--	--	--	------

77				78.5
----	--	--	--	------

78				78.1
----	--	--	--	------

79				78.4
----	--	--	--	------

0	7.78	190.06	4.31	182.28
---	------	--------	------	--------

80				78.0
----	--	--	--	------

81				78.3
----	--	--	--	------

82				78.6
----	--	--	--	------

83				78.2
----	--	--	--	------

$$15 - \frac{4.9}{10} \quad \frac{7.0}{7} \quad 7.4 \quad \frac{7.0}{4} \quad \frac{5.0}{10} \quad \frac{5.6}{15}$$

$$\frac{5.4}{15} \quad \frac{5.0}{10} \quad \frac{6.6}{7} \quad 7.1 \quad \frac{6.6}{5} \quad \frac{5.1}{8} \quad \frac{5.8}{15}$$

$$\frac{5.0}{15} \quad \frac{4.9}{9} \quad \frac{6.7}{7} \quad 6.6 \quad \frac{6.2}{7} \quad \frac{5.0}{10-15}$$

$$\frac{4.4}{15} \quad \frac{4.6}{9} \quad \frac{6.0}{5} \quad 6.4 \quad \frac{6.1}{6} \quad \frac{5.0}{10-15}$$

$$\frac{4.8}{15} \quad \frac{5.2}{7} \quad \frac{8.1}{4} \quad 8.1 \quad \frac{8.1}{4} \quad \frac{4.6}{9-13}$$

$$\frac{4.8}{15} \quad \frac{5.4}{8} \quad \frac{7.8}{5} \quad 8.5 \quad \frac{7.6}{4} \quad \frac{5.2}{8} \quad \frac{4.4}{15}$$

$$\frac{4.8}{15-8} \quad \frac{6.7}{5} \quad 8.2 \quad \frac{7.7}{4} \quad \frac{4.7}{8} \quad \frac{4.1}{15}$$

$$\frac{7.1}{15-8} \quad \frac{11.1}{4} \quad 12.1 \quad \frac{11.6}{4} \quad \frac{7.9}{10} \quad \frac{7.0}{15}$$

$$\frac{9.8}{15} \quad \frac{9.6}{7} \quad \frac{11.2}{5} \quad 11.8 \quad \frac{11.4}{7} \quad \frac{8.2}{12-20}$$

$$\frac{9.7}{15} \quad \frac{10.1}{10} \quad \frac{11.6}{8} \quad 11.5 \quad \frac{11.1}{8} \quad \frac{9.9}{10-15}$$

$$\frac{9.7}{15} \quad \frac{9.6}{10} \quad \frac{11.7}{5} \quad 11.9 \quad \frac{11.7}{5} \quad \frac{10.9}{9} \quad \frac{9.3}{12-15}$$

Sta	+	Σ	-		Elev
		190.06			
84					78.2
85					79.5
86					78.7
87	5.73	186.49	9.30	180.76	78.7
88					77.5
89					77.4
90					78.1
91					79.6
92					79.6
93	5.46	190.75	12.0	185.29	
+60	4.5'	190.75	12.0	185.29	
					78.85
					RR. Pipe
					78.57
B.M.			6.92	183.83	
					89.35

$$\frac{9.3}{15} \quad \frac{10.4}{8} \quad \frac{11.6}{5} \quad 11.9 \quad \frac{11.6}{5} \quad \frac{9.9}{10-15}$$

$$\frac{4.8}{20} \quad \frac{5.7}{10} \quad \frac{10.0}{5} \quad 10.6 \quad \frac{9.7}{5} \quad \frac{6.8}{9} \quad \frac{6.6}{17}$$

$$\frac{8.2}{17} \quad \frac{8.2}{11} \quad \frac{10.5}{8} \quad 11.4 \quad \frac{10.5}{6} \quad \frac{8.4}{11-15}$$

$$\frac{5.1}{15} \quad \frac{8.2}{7} \quad \frac{7.8}{5} \quad 7.8 \quad \frac{7.8}{4} \quad \frac{7.0}{5} \quad \frac{5.6}{12-15}$$

7.1 W.S. = 79.4

$$\frac{7.6}{30} \quad \frac{8.3}{9} \quad 9.0 \quad \frac{9.0}{4} \quad \frac{7.9}{9} \quad \frac{7.1}{21}$$

$$\frac{8.5}{25} \quad \frac{8.3}{4} \quad \frac{8.9}{2} \quad 9.1 \quad \frac{8.8}{3} \quad \frac{7.1}{10} \quad \frac{7.7}{20}$$

$$\frac{7.4}{20} \quad \frac{6.9}{8} \quad \frac{8.3}{3} \quad 8.4 \quad \frac{8.4}{3} \quad \frac{6.1}{11} \quad \frac{6.6}{18}$$

$$\frac{6.2}{15} \quad \frac{5.1}{10} \quad \frac{7.0}{4} \quad 6.9 \quad \frac{6.9}{4} \quad \frac{5.7}{6} \quad \frac{5.6}{15}$$

$$\frac{8.9}{15} \quad \frac{6.6}{10} \quad \frac{6.6}{4} \quad 6.9 \quad \frac{6.7}{3} \quad \frac{4.7}{10} \quad \frac{4.5}{15}$$

92+26 RRR/W

Out: 11.9 FL
In: 12.18

Top No End RR Cul. Sta 93+00
1.4 B/R

190.75

93

78.55

+06

Top Over flow

80.7

+50

77.9

94

76.8

+32

W/s. Twin lake

76.71

92+50 E RRTM

13-21 281

$$\frac{9.9}{10} \quad \frac{10.3}{4} \quad 12.2 \quad \frac{10.6}{4} \quad \frac{9.6}{10-15}$$

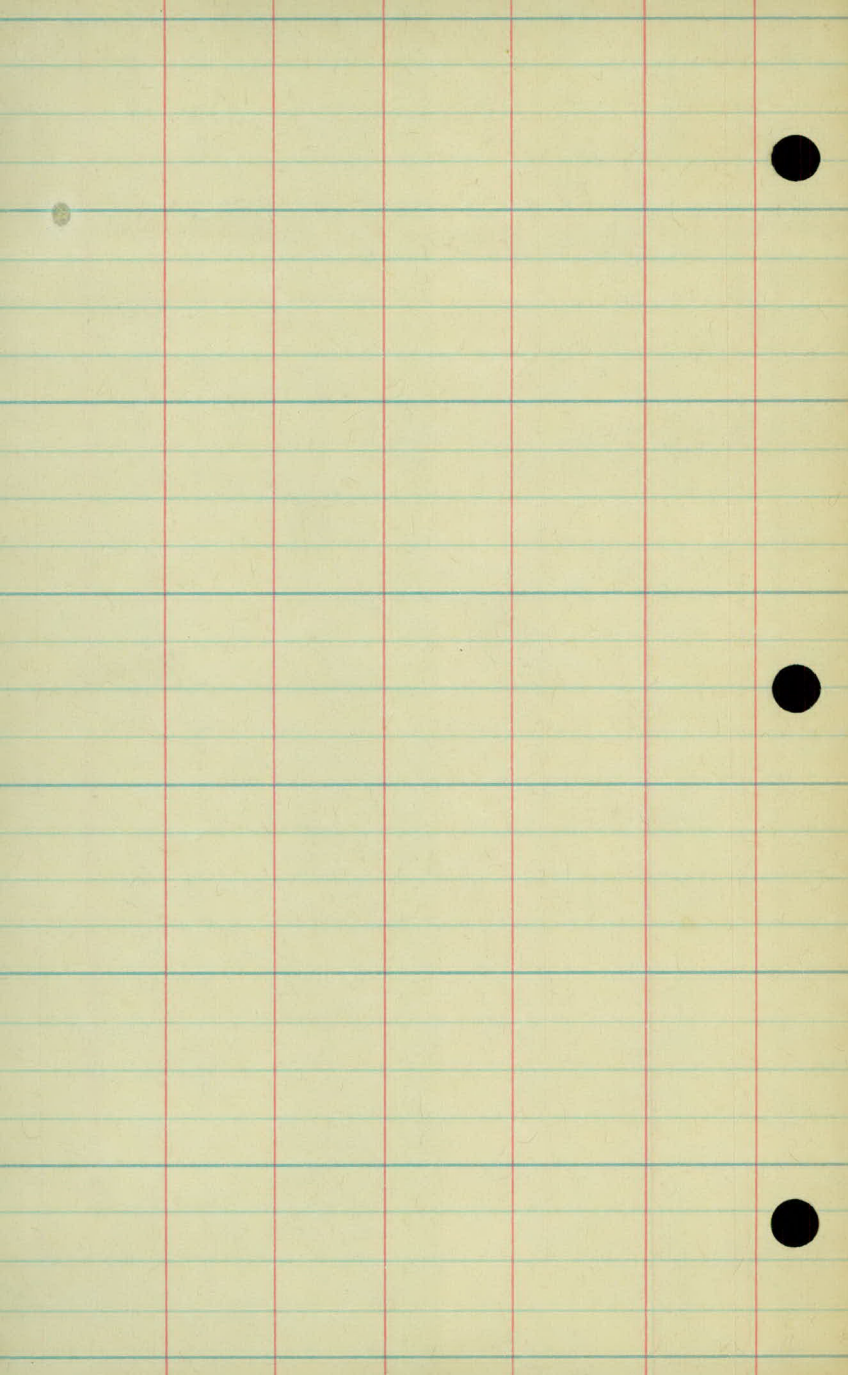
10.0 15' x 25' long 2' high
Top Wall

11.6 Bottom overflow

L.O. 12.9 L.O.

L.O. 14.0 L.O.

14.04 6/13/35



Lateral Dt Lt Sta 68+91

Sta	+	π	-	Elev
-----	---	-------	---	------

BM	949	186.86	-	177.37
----	-----	--------	---	--------

0+00	Dt. Intersection			77.37
------	------------------	--	--	-------

1				77.5
---	--	--	--	------

2				77.3
---	--	--	--	------

3				77.3
---	--	--	--	------

4				77.1
---	--	--	--	------

5				77.3
---	--	--	--	------

6				77.5
---	--	--	--	------

7				77.8
---	--	--	--	------

8	490	185.43	6.33	180.53
---	-----	--------	------	--------

8				76.3
---	--	--	--	------

Outlet Fl. 36" x 42' C.M. Sta 68+91 (Main Ditch)

9.49

9.4

9.6

9.6

9.8

9.6

9.4

9.1

9.1

8.1 W.S. = 77.3

Sta

+

 π

-

Elev

185.43

9

76.7

10

76.9

11

77.1

12

77.0

13

76.9

14

77.0

+30

End Ditch

77.0

+38

RR R/W

79.9

 $\frac{1}{2}$ Trk NP RR

84.80

8.7

8.5

8.3

8.4

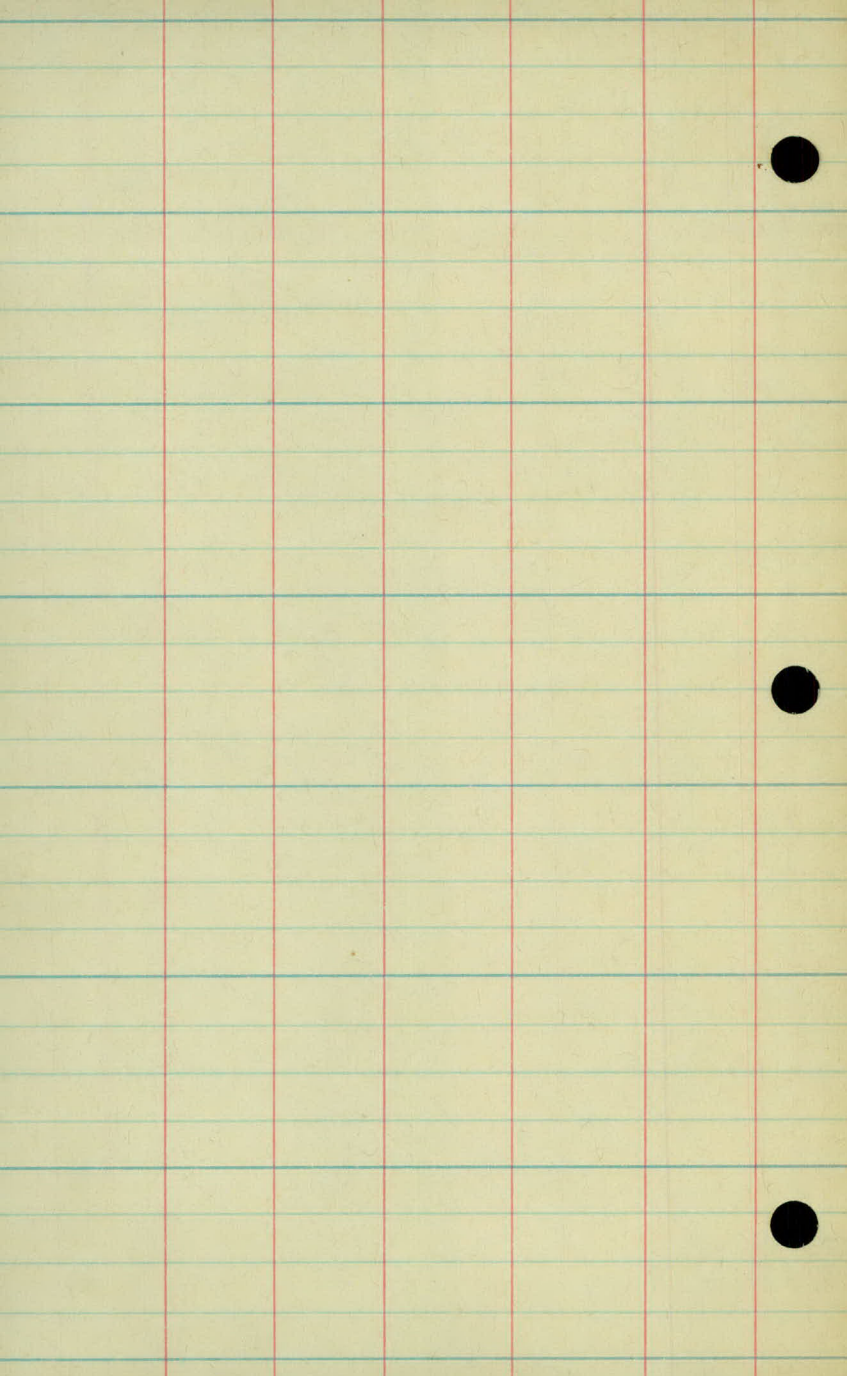
8.5

8.4

8.4

4.5

0.63



Lateral Ditch Lt Sta 53+70
on Sec Line N+S.

Sta	+	π	-
B.M.	86	186.20	177.60

53+70 Bottom ditch = 0+00

1+0			77.6
-----	--	--	------

2+0			77.6
-----	--	--	------

3+0			77.6
-----	--	--	------

4+0			77.2
-----	--	--	------

5+0			77.2
-----	--	--	------

6+0			77.1
-----	--	--	------

7+0			77.2
-----	--	--	------

8+0			77.1
-----	--	--	------

9+0			77.0
T.P.	4.50	185.10	5 ⁶⁰ 180.60

10			76.6
----	--	--	------

11			77.1
----	--	--	------

± Dt. @ Sta 53+70

86

86

86

86

90 $\frac{7.15}{\text{Top Water}} = 79.05$

90

91

90

91

92

85

8.0

Sta	+	-	Elev
		185.10	
12			76.8
13			77.1
14			76.7
15			76.9
+88	Sec line + Cor $\frac{1}{2}$ M. E of Rec St.		
16			76.9
17			76.9
18			77.9
+03	± N.P. Trestle		
+36	No. RR. R/W End Ditch		79.1
B.M.		3.55	181.55

8.3

8.0

12' wide Ditch

8.4

8.2

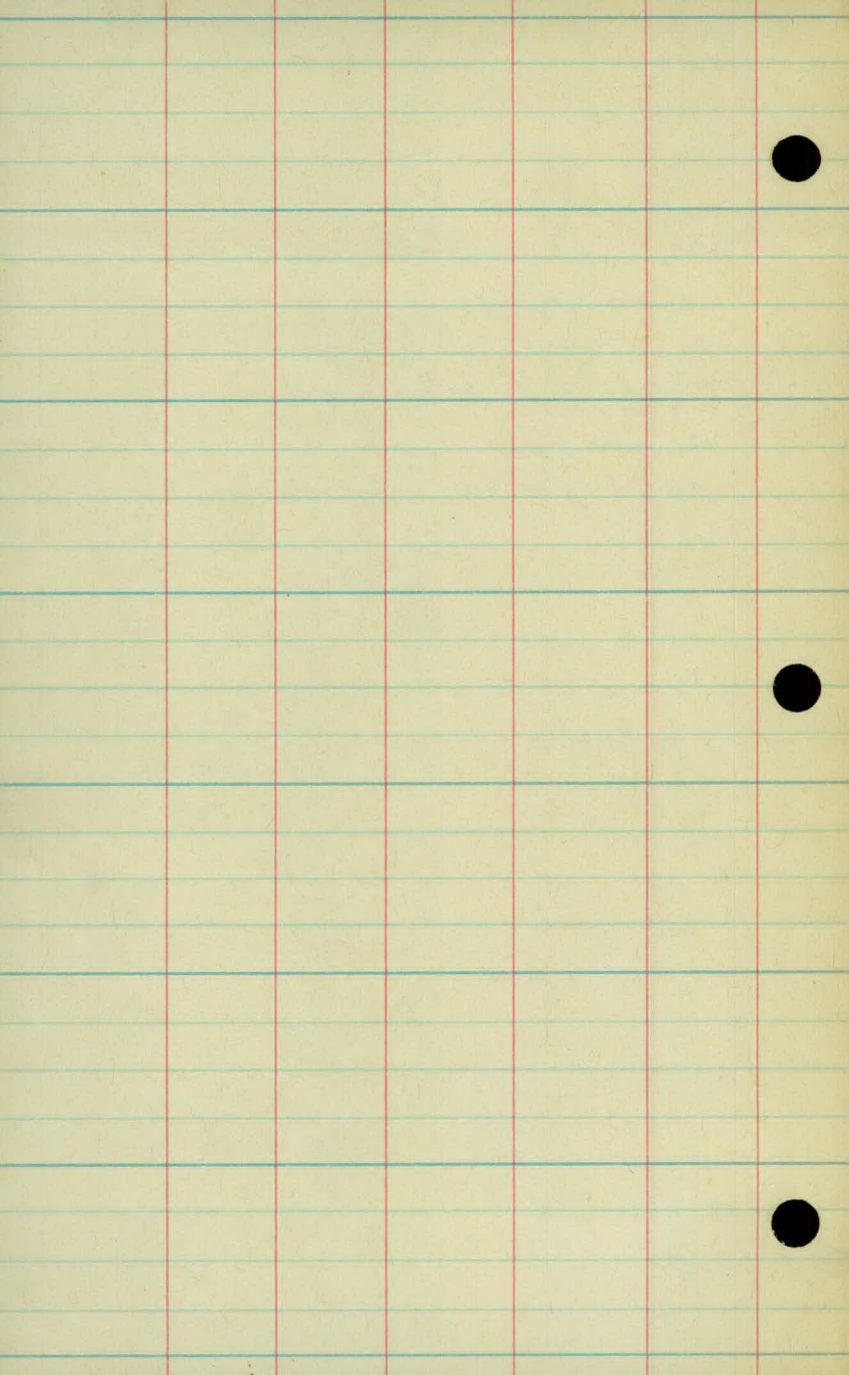
8.2

8.2

7.2

6.0

So. Cor Dump Plank @ E E Trestle



Sta

£

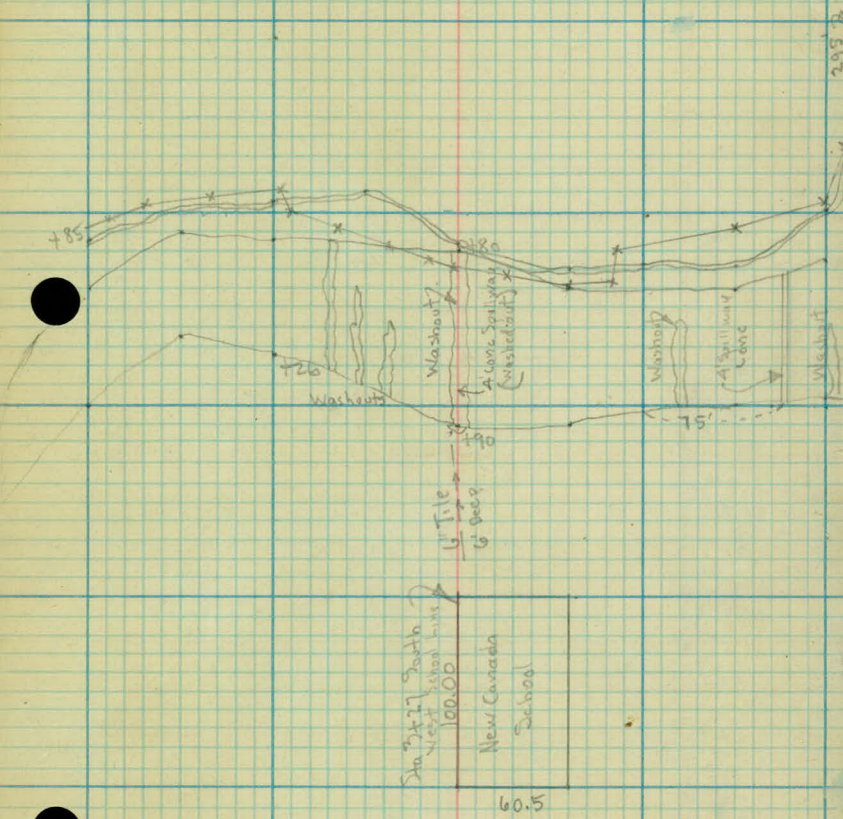
200 Lt 150 Lt 100 Lt 60 Rt 150 Rt 200 Rt

295 Rt.

	+90	+86				+90
+60			+60	+60	+75	
	+35	+26				
+00				+00	+04	+15
			+90			

0+00

Note - Washouts about
 3 deep 6/12/35
 6 deep 6/17/35



To Rice St.
Little Canada Rd
To Edgartown →
Not to Scale

