

Book #50 - Dr. #8

MAINT. SURVEY
COUNTY ROAD "E"

From Rice Str.
To Lexington Ave.
RD. $\frac{1}{2}$ N^o 6

4-24-24

"13"

SURVEY COUNTY ROAD E.

BETWEEN SEC'S 30 & 31

T 30 - 23.

COUNTY
COUNTY

AVE

490.0 12" let
wood

COUNTY

ROAD E

1110 E.P.

4870 E.P.

PP 10" 80
5029

50.5

Cob. Pier

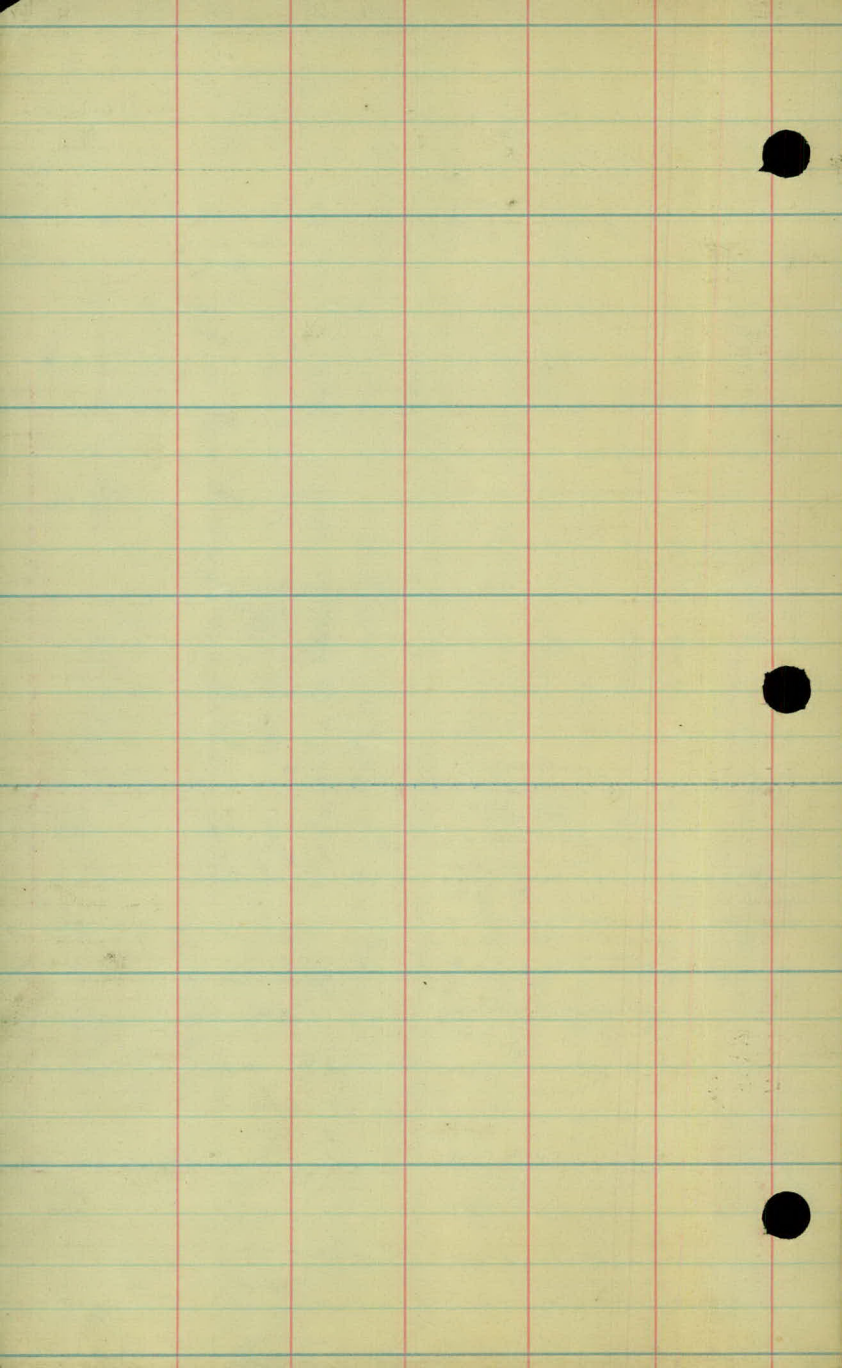
5380 E.P.

ANOKA
RAMSEY

2627
FAIRCHILD

2627.41

2



COUNTY ROAD "E"

BETWEEN SECTIONS 29 & 32
T 30 - R 23

T.P.
443.30
2
433.00 T.P.

CLEVELAND AVE.

COUNTY ROAD "E"

E.P.

32.80

47.64

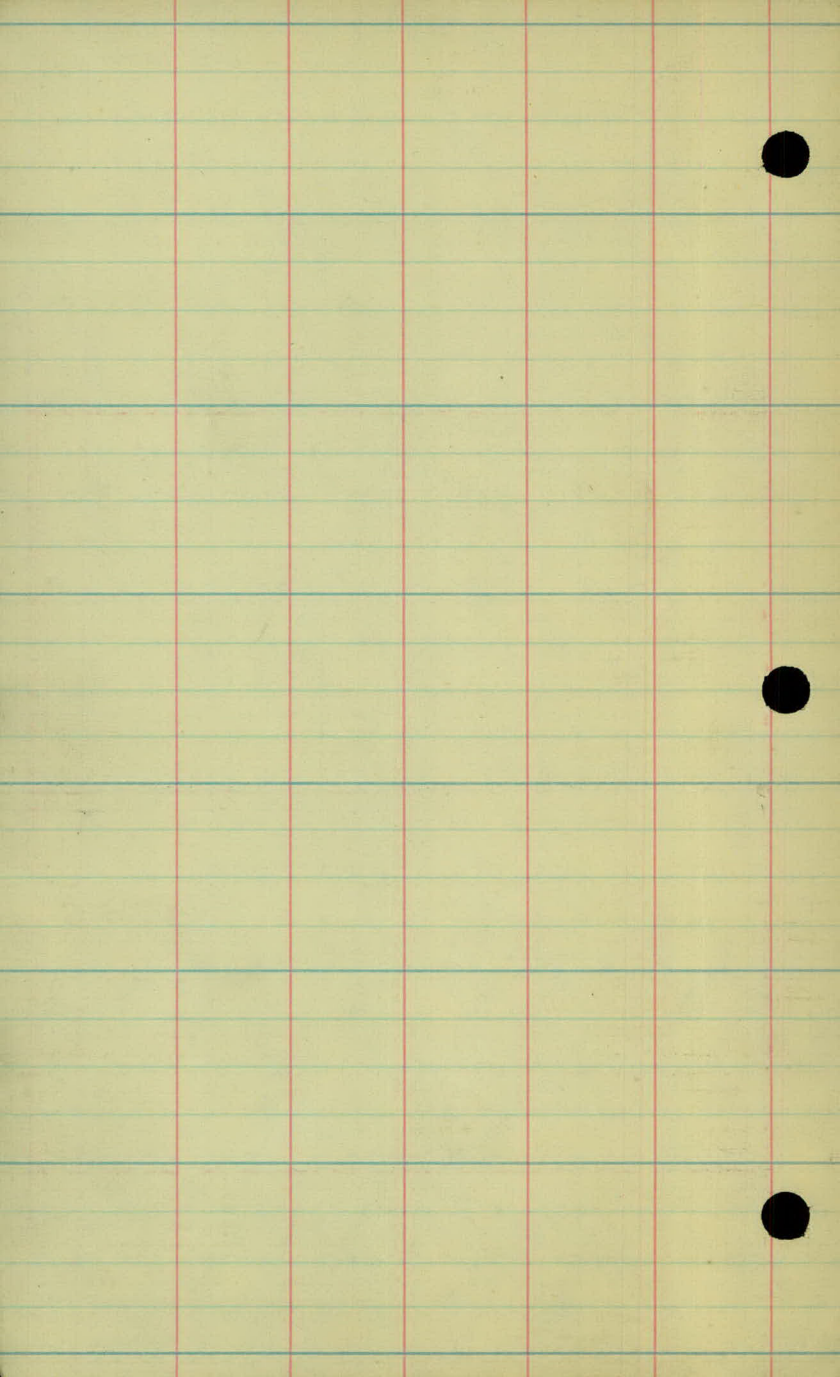
G.P.

38.24

T.P.

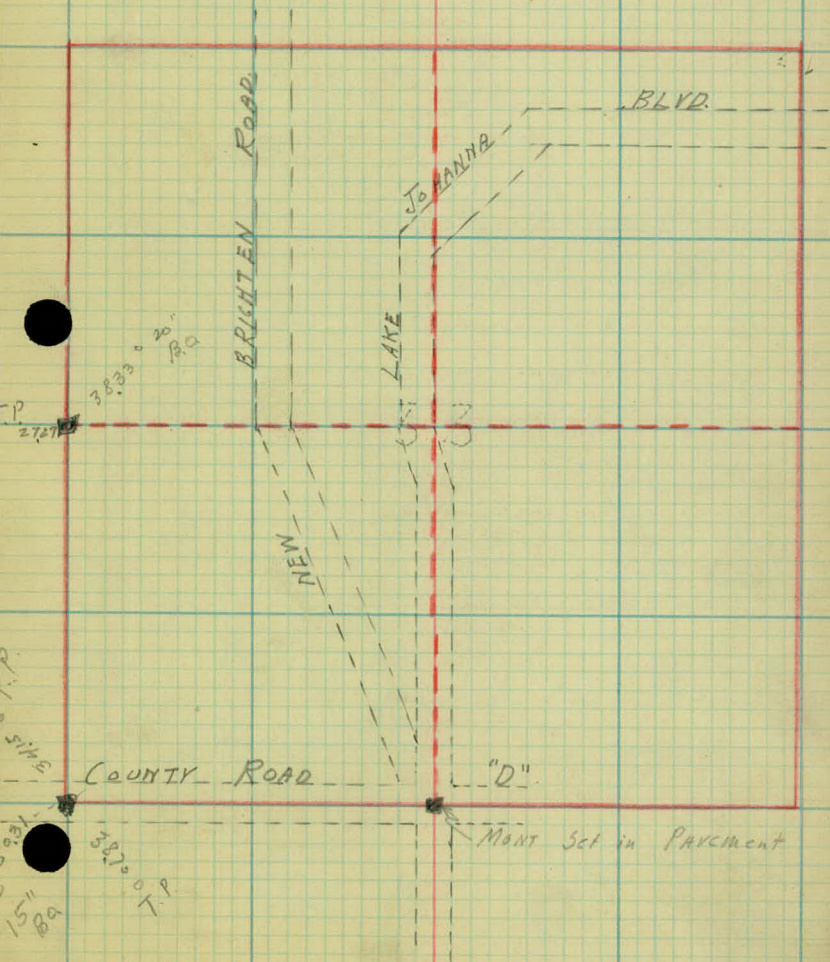
CLEVELAND AVE.

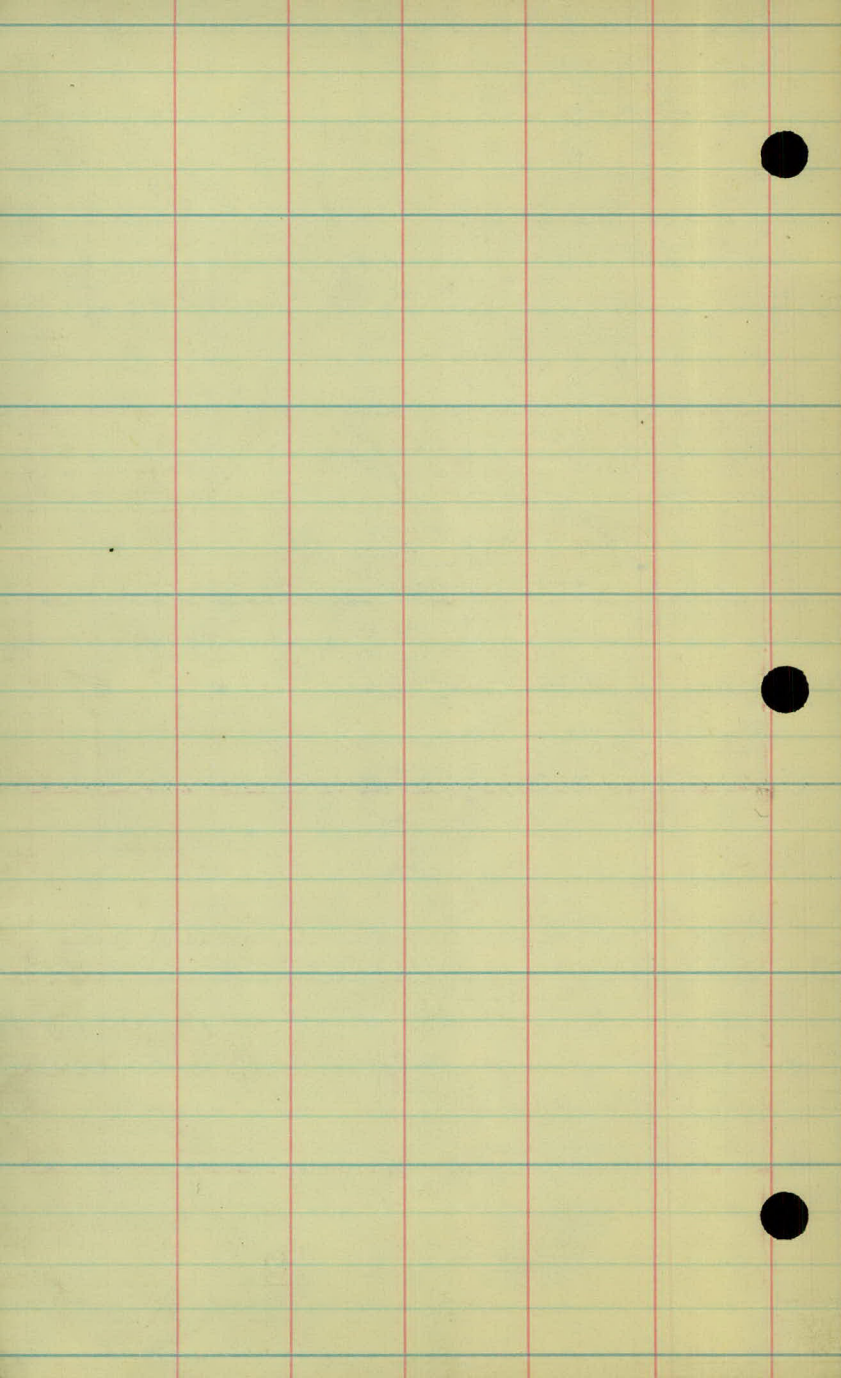
3 2



COUNTY ROAD E.

SECTION 33-30-23.

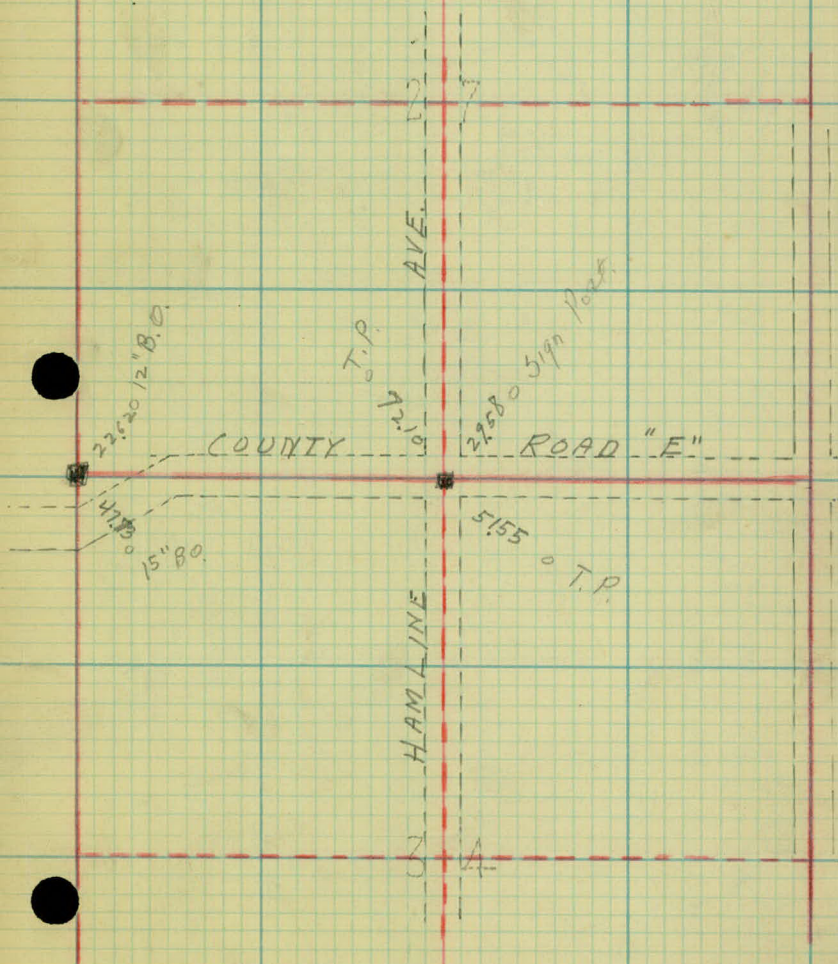


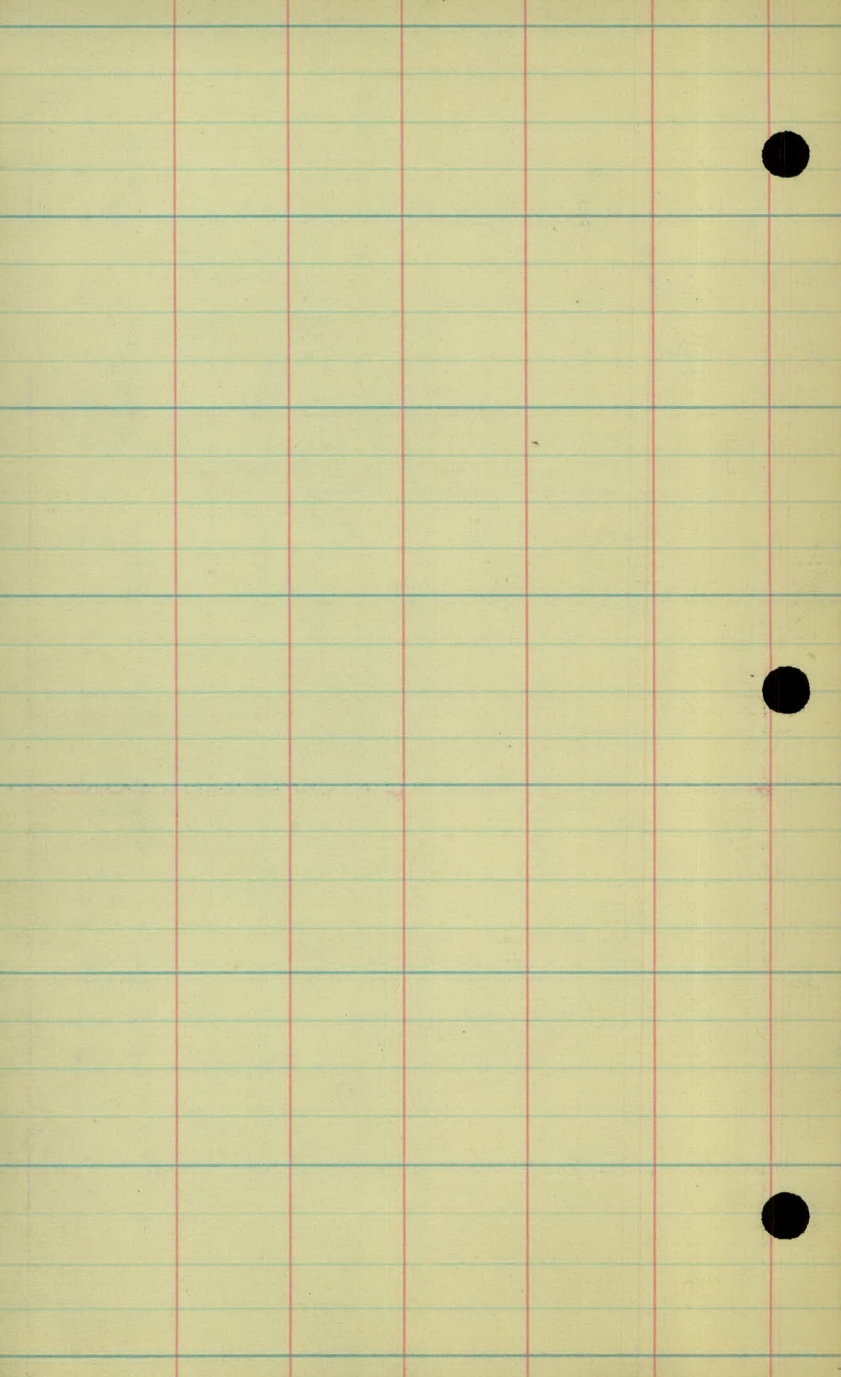


4
COUNTY ROAD "E"

BETWEEN SEC'S 27 & 34

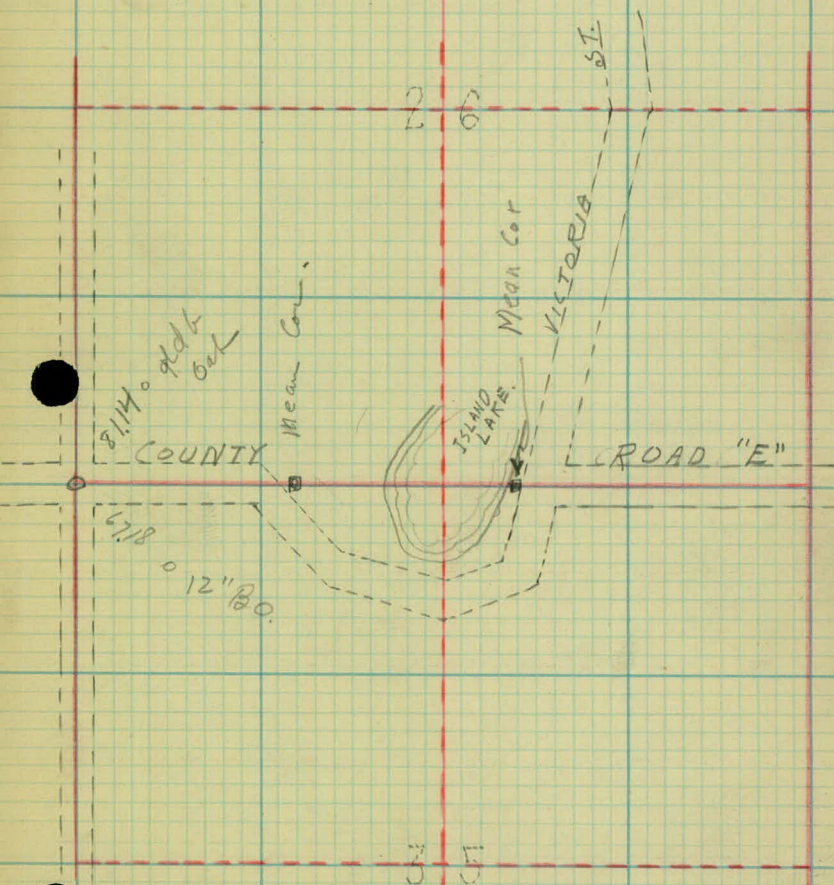
T. 30 - R. 23.

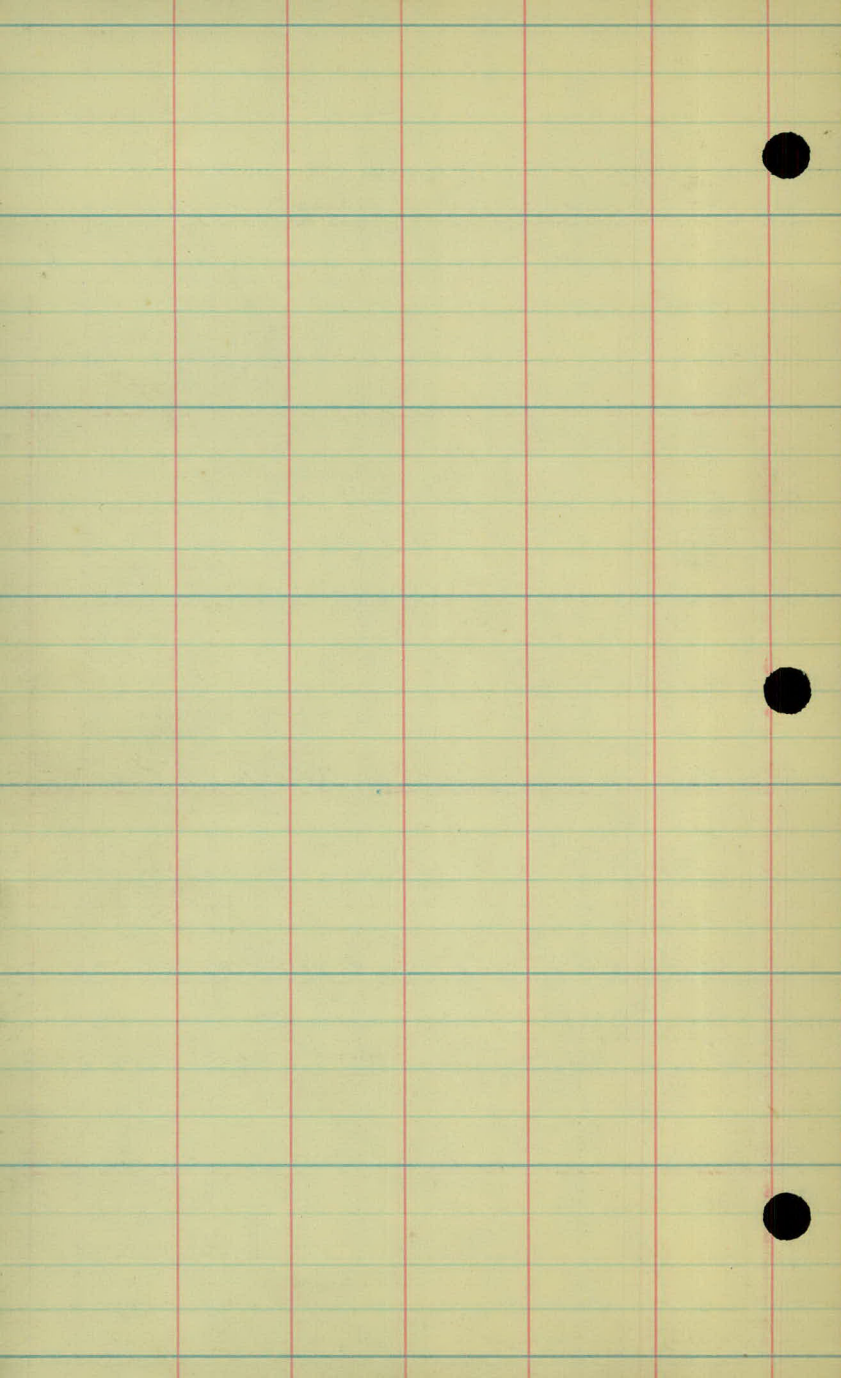




COUNTY ROAD "E"

BETWEEN Sec's 26 & 35.

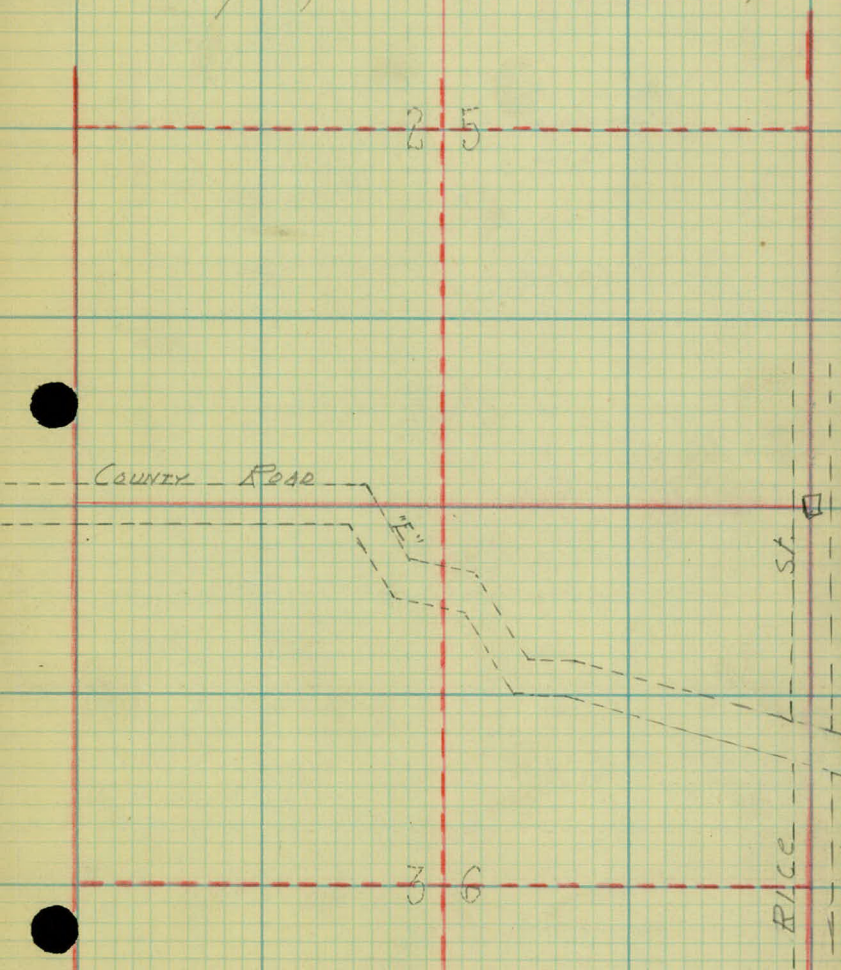


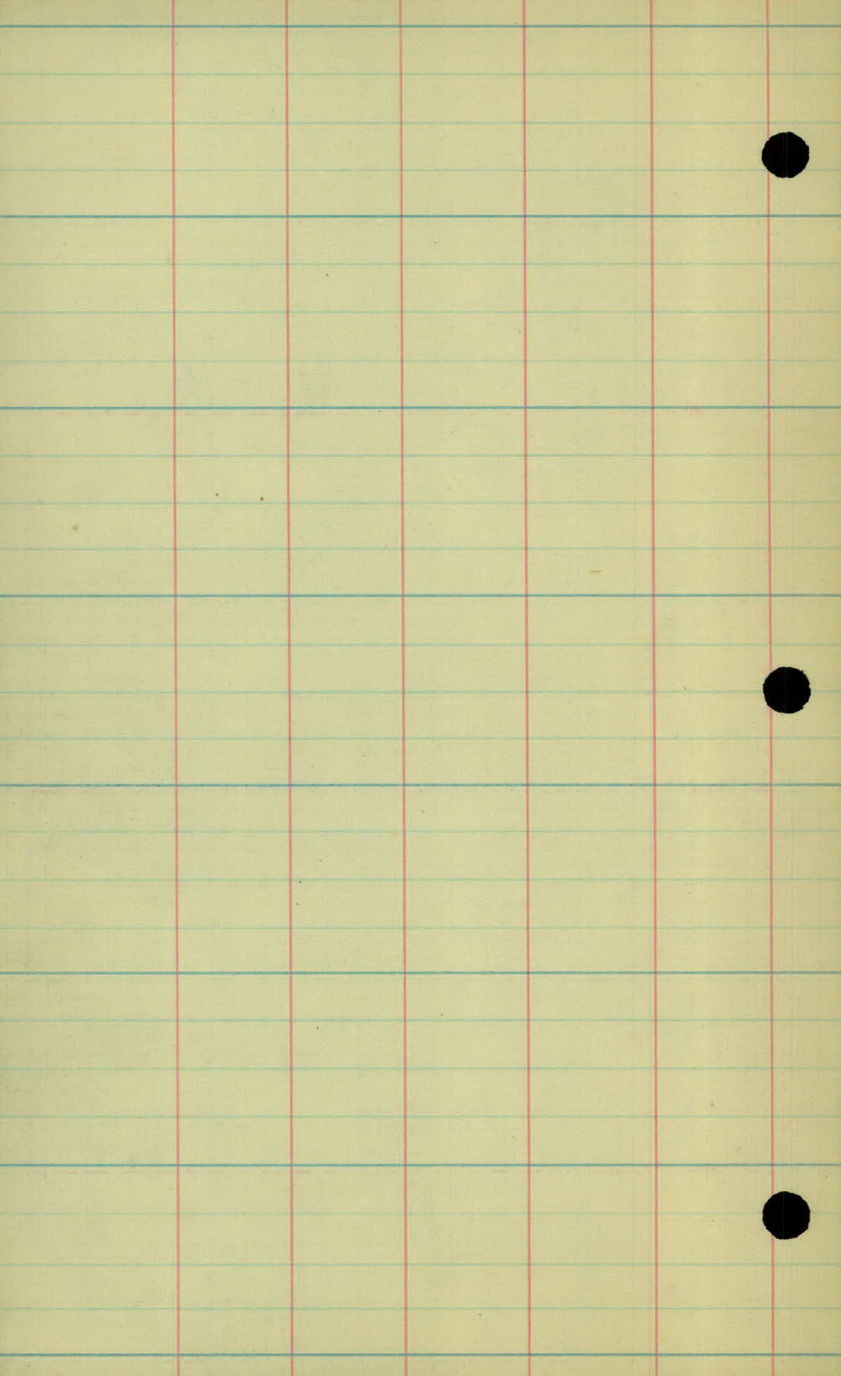


6
COUNTY ROAD "E"

BETWEEN SEC 3 25 & 36
T 30 R 23

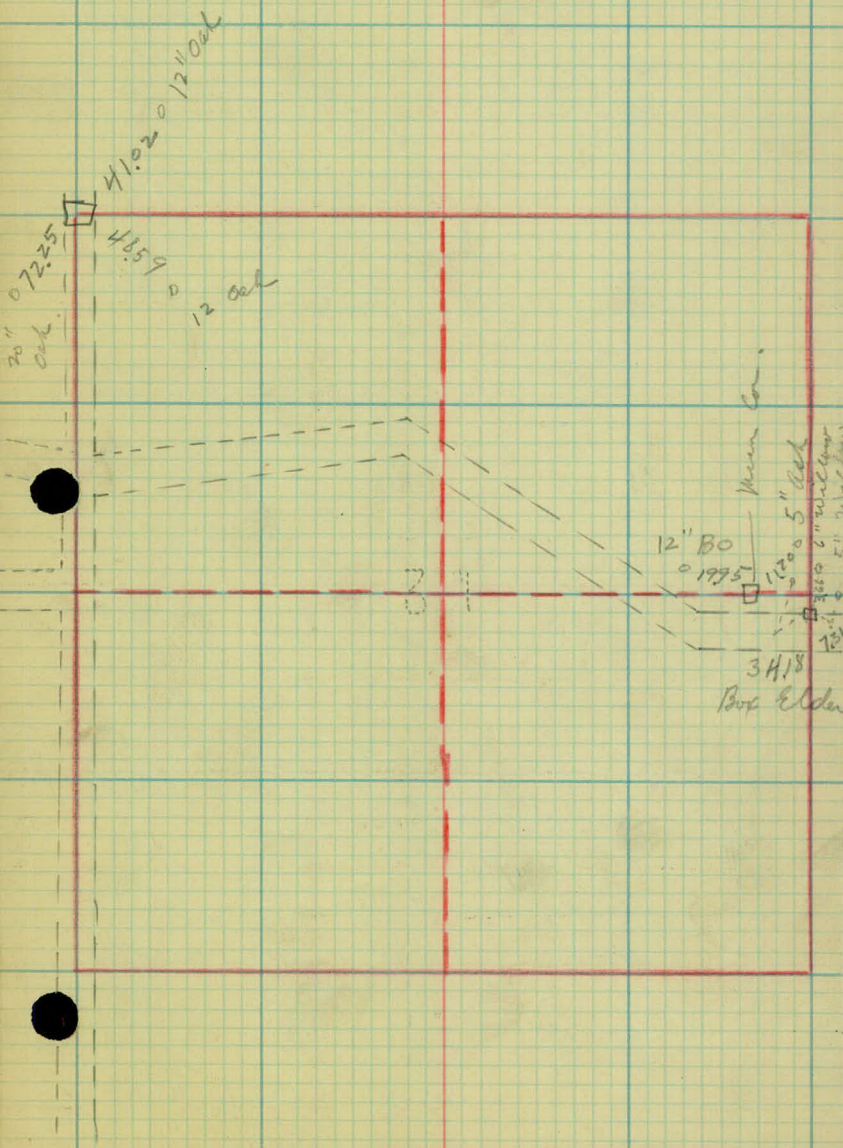
Survey by Austin Rice to Lexington

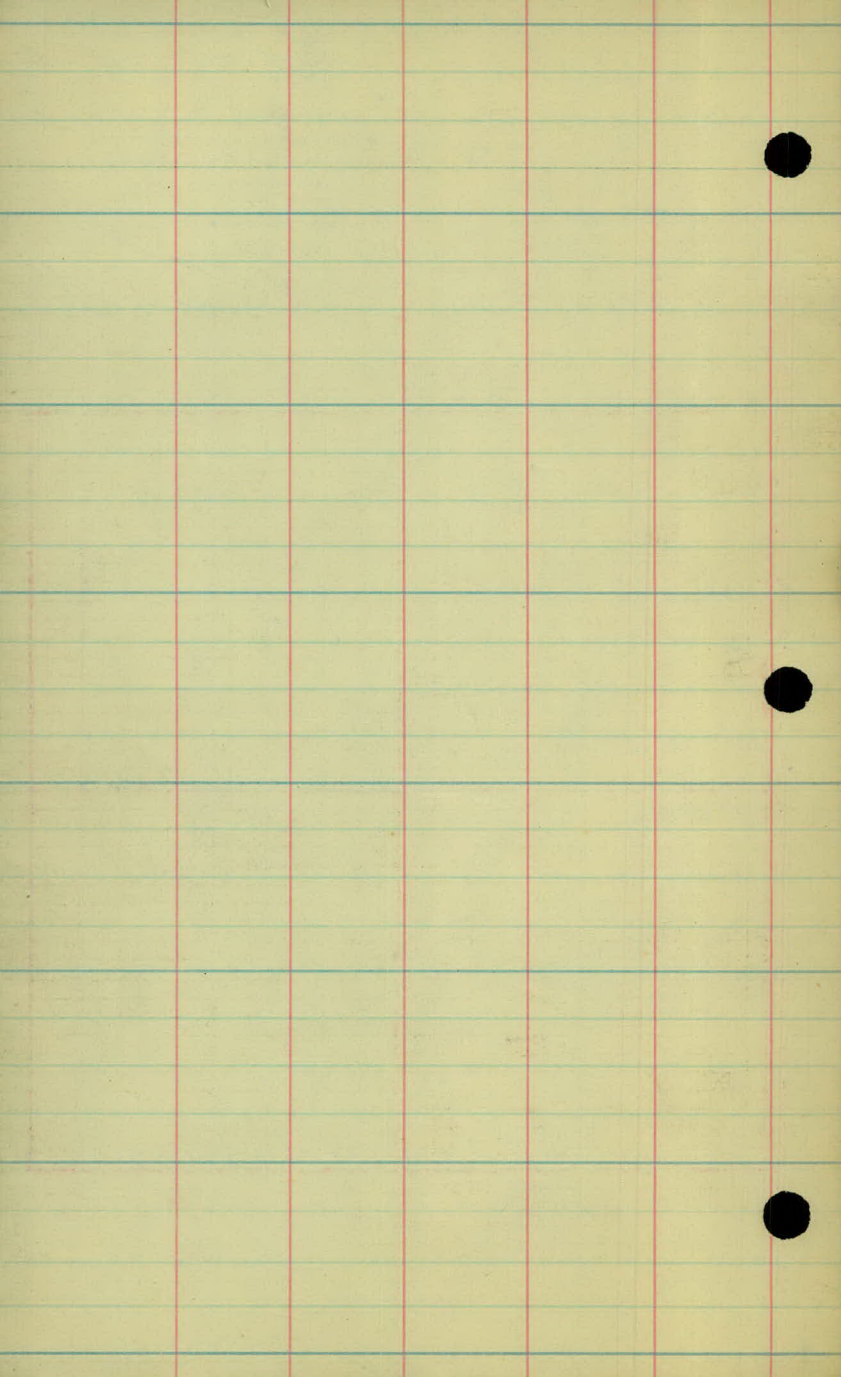




COUNTY ROAD "E"

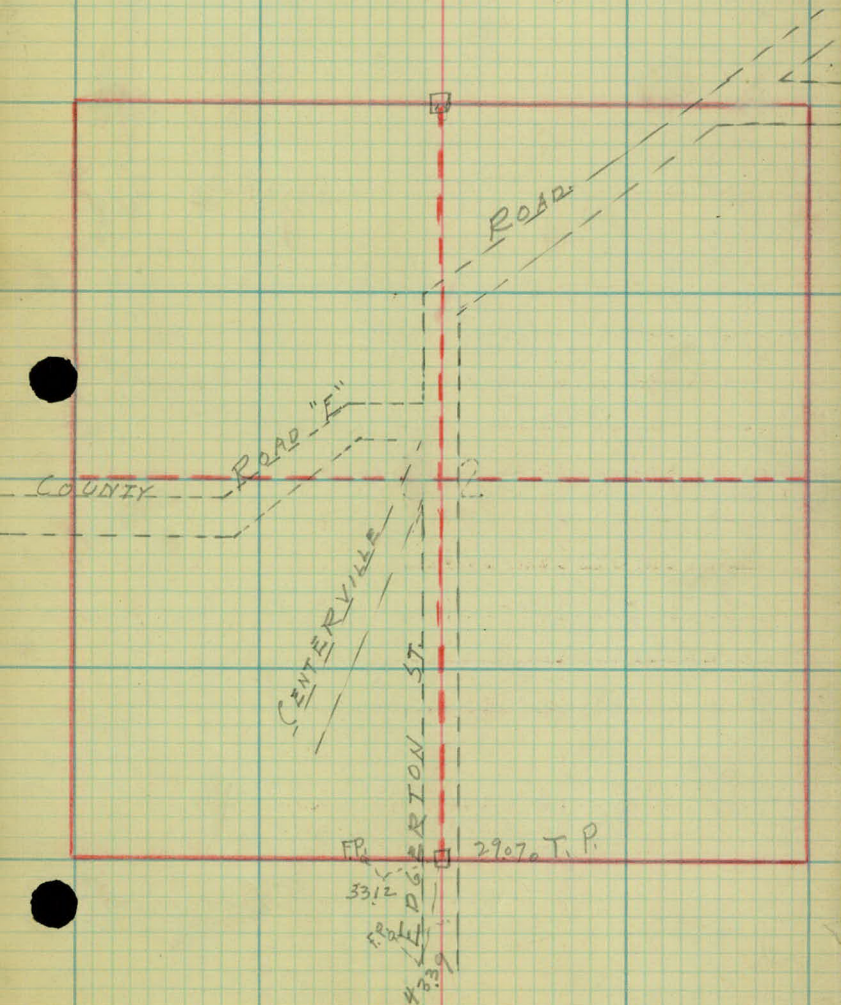
SECTION 31- 30-22

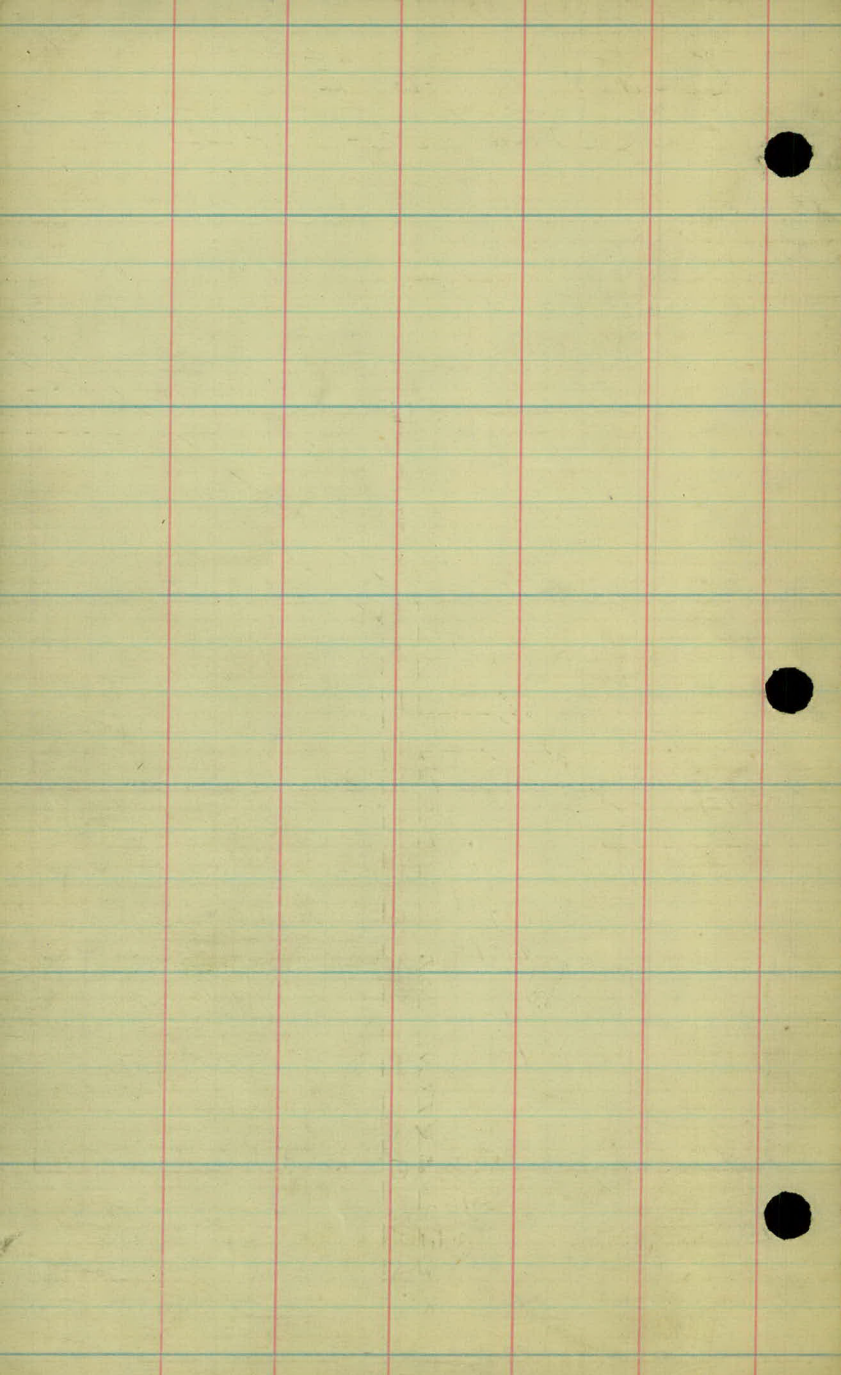




COUNTY ROAD "E"

SECTION 32-30-22





Road #6

Co. Rd. "F" Rice to Lexington.
Transit Notes

Sta 0+00 to 114+78.8

R. H. Austin }
D. N. Skooglan } Party.
W. Maloney }
M. Galvin }

Wm. L. Sweeney
only a part of the
notes

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed 4/24/24

File No. "13"

Ang. ht. Ang. Rt.

6 + 55.0 P.T.

5.88° 20' W.

5 + 49.6 P.I.

6° 20'

4 + 43.9 P.C.

5.82° 00' W.

3 + 56.1 P.T.

2 + 58.4 P.I. 28° 00'

1 + 56.1 P.C.

N. 70° 00' W.

0 + 00 = E Rice St Pavement.

Rd #6

Sta - Def.

4+43.9 - 0°00'

5+00 - 0°50'

6+00 - 2°20'

6+55 - 3°10'



3° Curve TR.

 $\Delta = 60.20'$

Rad = 1910.1

Tang = 105.7

P.C. = 4+43.9

Length = 211.1

P.T. = 6+55

Sta - Def

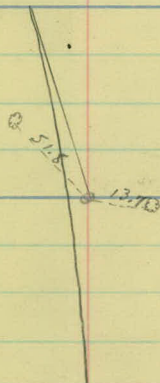
1+56' - 0°00'

2+00 - 3°04'

+50 - 6°34'

3+00 - 10°04'

+56' - 14°00'



14° Curve Lt.

 $\Delta = 28.00'$

Rad = 410.3

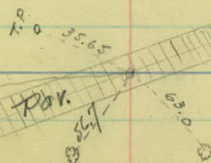
Tang = 102.3

B.C. = 1+56'

Length = 200.0

P.T. = 3+56'

← -- 70°00' →



Mont

E 1/4 Sec. 36

Rice St. Par.

North

Anght. Ang. Rt.

5.86°02'W.

12+61.6 P.T.

12+03.0 P.I. 36°58'

11+38.4 P.C.

N.57°00'W.

9+71.8 P.T.

8+88.4 P.I.

34°40'

7+98.5 P.C.

5.88°20'W.

Sta. - Def

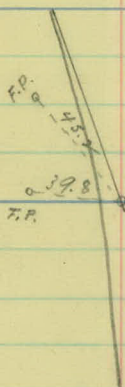
11+38.4 - 0°00'

+ 50 - 10°44'

12+00 - 9°14'

+ 50 - 16°44'

+ 61.6 - 18°29'



30° Curve Lt.

 $\Delta = 36°58'$

Rad = 193.18

Tang = 64.6

P.C. = 11+38.4

Length = 123.2

P.T. = 12+61.6

Sta. - Def

7+98.5 - 0°00'

8+00 - 0°09'

+ 50 - 5°09'

9+00 - 10°09'

+ 50 - 15°09'

+ 71.8 - 17°20'



20° Curve e. RT.

 $\Delta = 34°40'$

Rad = 287.94

Tang = 89.9

B.C. = 7+98.5

Length = 173.3

P.T. = 9+71.8

2
Anght. Ang. Rt.

26+45.1 P.T.

Void

23+73.4 P.I. $89^{\circ}36'$

18+98.4 P.C.

N. $7^{\circ}38'$ W.

14+10.1 P.T.

13+60.6 P.I.

$86^{\circ}20'$

12+78.9 P.C.

S. $86^{\circ}02'$ W.

Rd. #6

~~Sta. - Def.~~
~~18+98.4 - 0°00'~~
~~19+00 - 0°06'~~
~~+50 - 3°06'~~
~~20+00 - 6°06'~~
~~+50 - 9°06'~~
~~21+00 - 12°06'~~
~~+50 - 15°06'~~
~~22+00 - 18°06'~~
~~+50 - 21°06'~~
~~23+00 - 24°06'~~
~~+50 - 27°06'~~
~~24+00 - 30°06'~~
~~+50 - 33°06'~~
~~25+00 - 36°06'~~
~~+50 - 39°06'~~
~~26+00 - 42°06'~~
~~+45' - 44°48'~~

~~Void.~~

12° Curve Left.

$\Delta = 89°36'$

Rad. = 47834

Tang = 475.0

P.C. = 18+98.4

Length = 746.7

P.T. = 26+45.1

70° Curve Rt.

$\Delta = 86°20'$

Rad = 87.17 ✓

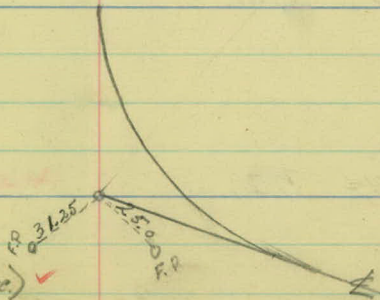
Tang 81.76 ✓

P.C. = 12+78.9 ✓

Length = 131.2 (Act. Arc.) ✓

P.T. = 14+10.1 ✓

Rad. Hub. Set.



^E
Anght. Ang. Rt.

Equation $27+38 = 27+24$ (Long Station)

$27+38^{\circ}$ P.T.

S. $82^{\circ}46'$ W.

$26+59.0$ P.I. $6^{\circ}20'$

$25+79.7$ P.C.C.

S. $89^{\circ}06'$ W.

$24+34.2$ P.I. $35^{\circ}45'$

$22+77.6$ P.C.C.

N. $55^{\circ}09'$ W.

$21+51.2$ P.I. $41^{\circ}11'$

$20+13.0$ P.C.C.

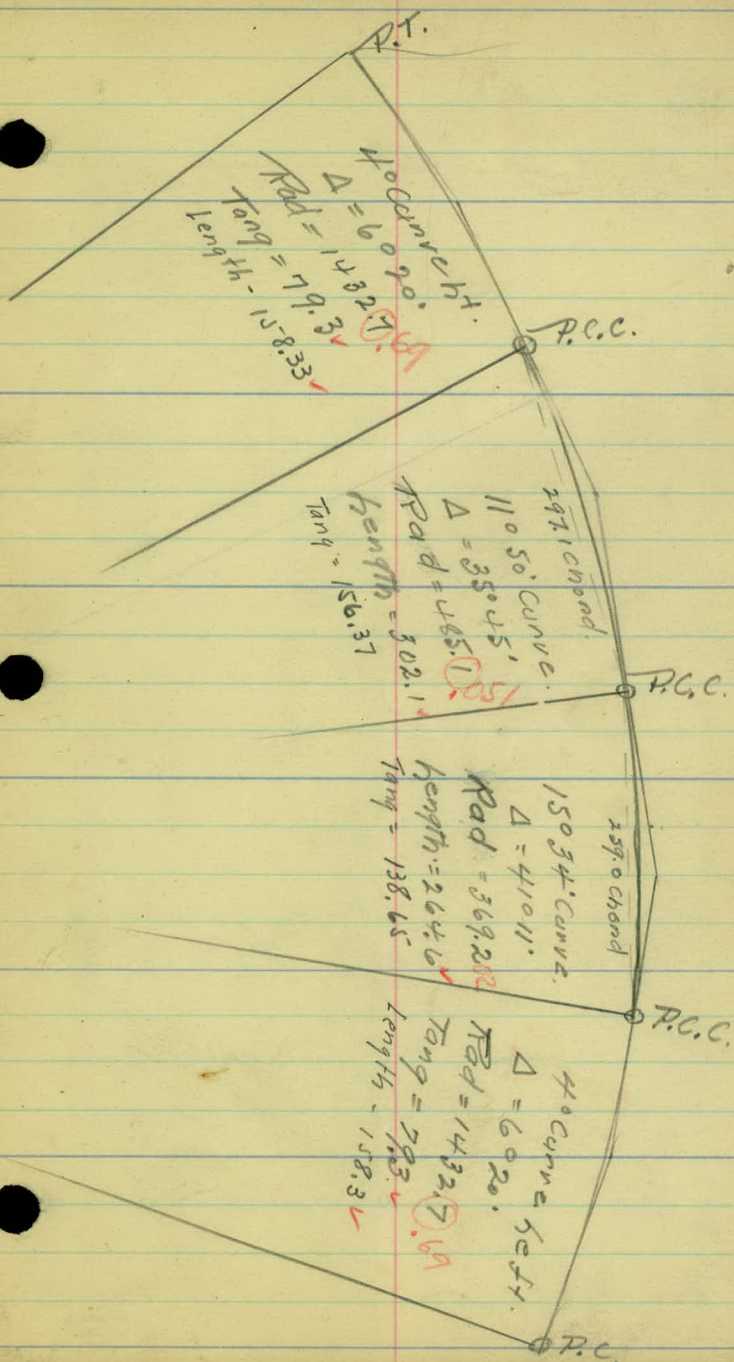
N. $13^{\circ}58'$ W.

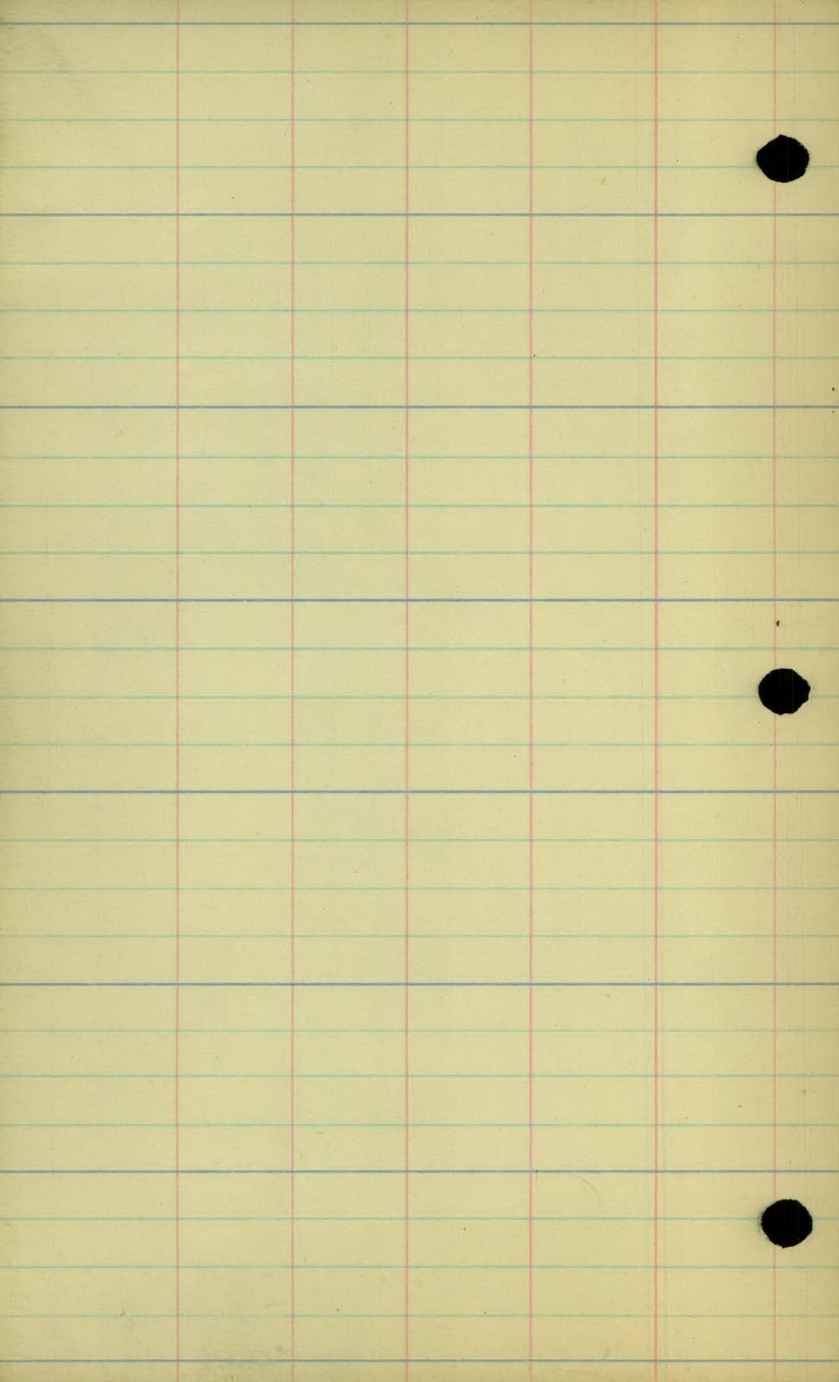
$19+34$ P.I. $6^{\circ}20'$

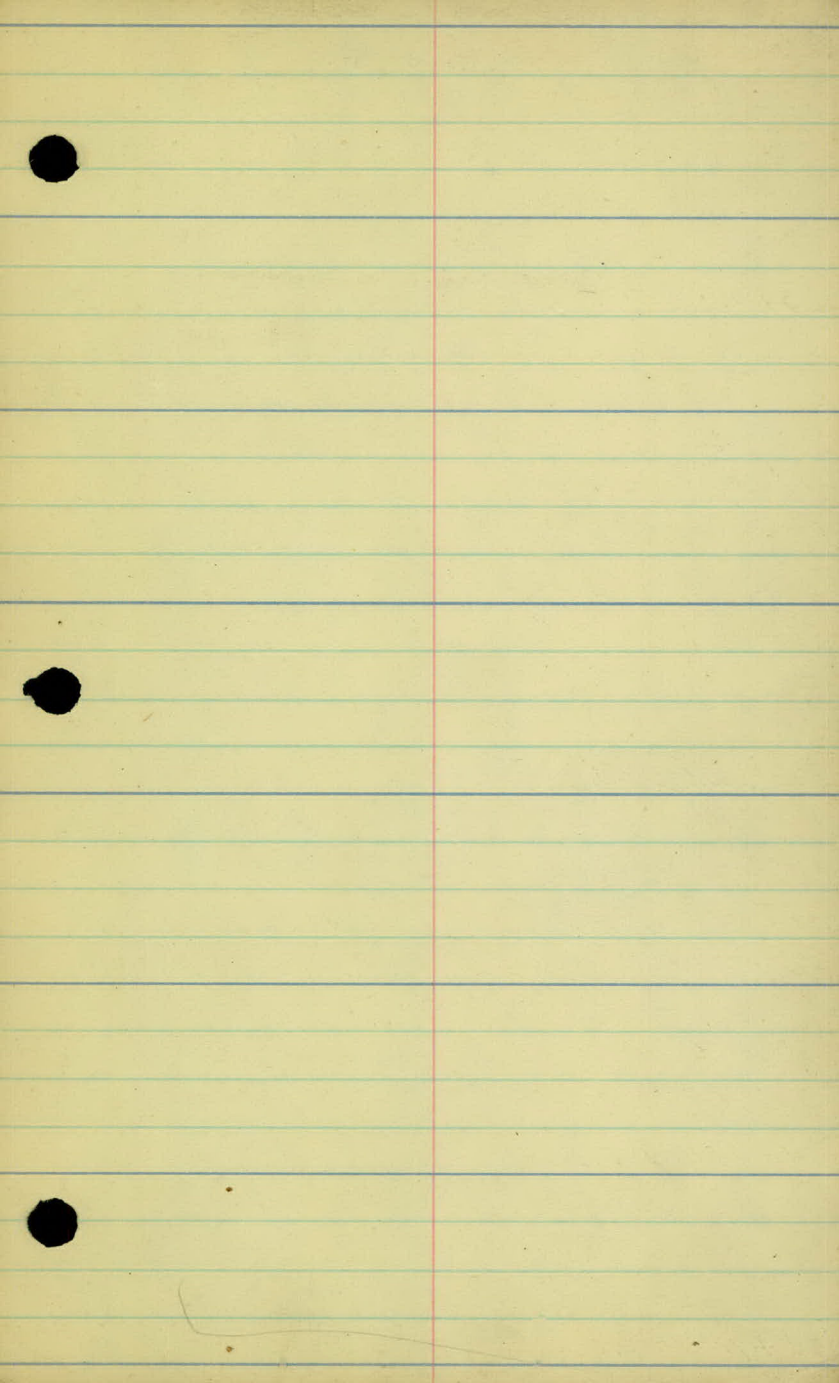
$18+54.7$ P.C.

N. $7^{\circ}38'$ W.

8936







Ang. ht. Ang. Rt.

34+19.7 ✓ P.T.

N. 89° 49' W.

33+06.2 P.I. 16° 00'

31+91.1 ✓ P.C.

N. 73° 49' W.

31+68.9 ✓ P.T.

31+32.6 P.I. 71° 25'

30+83.7 ✓ P.C.

30+56.6 ✓ P.T.

N. 2° 24' W.

29+99.9 P.I.

94° 50'

28+91.1 ✓ P.C.

S. 82° 46' W.

S. 1/4 Cor □
Sec. 25-30-23

340.0 - -

MC. Grass Lake

Sta. - Def

31+91.1 - 0000

32+00 - 0019

33+00 - 3049

34+00 - 7019

34+19.7 - 8000



7° Curve Lt.

$\Delta = 16^{\circ}00'$

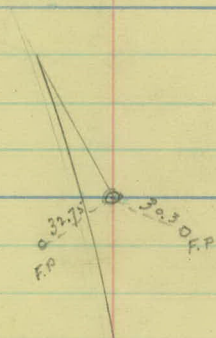
Rad = 819.02 ✓

Tang = 115.1 ✓

P.C. = 31+91.1 ✓

Length = 228.6 ✓

P.T. = 34+19.7 ✓



94° Curve Lt.

$\Delta = 71^{\circ}25'$

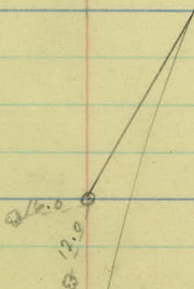
Rad = 68.37 ✓

Tang = 49.1 ✓

P.C. = 30+83.7 ✓

Length = 852 ✓ Actual Arc.

P.T. = 34+68.9 ✓



600° Curve Rt.

$\Delta = 94^{\circ}50'$

Rad = 100.0 ✓

Tang = 108.813 ✓

P.C. = 28+91.1 ✓

Length = 165.5 ✓ Actual Arc.

P.T. = 30+56.6 ✓

E
Ang. Lt. Ang. Rt.

5.87°09'W.

42 + 55.9 ✓ P.T.

41 + 55.5 P.I. 6°02'

40 + 54.8 ✓ P.C.

38 + 96.4 P.O.T

N. 86°49'W.

37 + 55.1 ✓ P.T.

36 + 05.2 P.I

3°00'

34 + 55.1 ✓ P.C

N. 89°49'W.

4-16 24

2

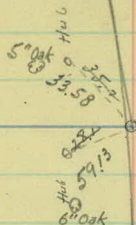
Sta - Det

40+54.8 - 0° 00'

41+00 - 0° 41'

42+00 - 2° 11'

42+55.9 - 3° 01'



3° Curve left

$\Delta = 6° 02'$

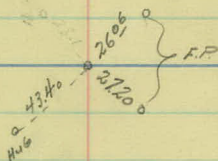
Rad = 1910.1 ✓

Tang = 100.7 ✓

P.C. = 40+54.8 ✓

Length = 201.1 ✓

P.T. = 42+55.9 ✓



Sta - Det

34+55' - 0° 00'

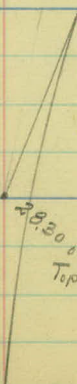
35+00 - 0° 13 1/2'

36+00 - 0° 43 1/2'

37+00 - 1° 13 1/2'

+55' - 1° 30' 31.07

31.07



1° Curve Rt.

$\Delta = 3° 00'$

Rad = 5729.65 ✓

Tang = 150.1 ✓

P.C. = 34+55' ✓

Tip F.R. Length = 300.0 ✓

P.T. = 37+55' ✓

Ang Lt. Ang Rt.

589°59'W.

53+94.2[✓] P.T.

52+95.8 P.I.

1°58'

51+97.5[✓] P.C.

5.88°01'W.

50+56.0 P.I.

1°17'

5.89°18'W.

47+40.8[✓] P.T.

46+33.3 P.I.

2°09'

45+25.8[✓] P.C.

5.87°09'W.

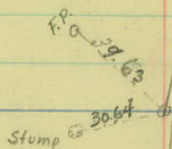
Sta. - Def

51+97.5 - 0°00'

52+00 - 0°01'

53+00 - 0°31'

+94.2 - 0°59'



1° Curve Rt.

 $\Delta = 1°58'$

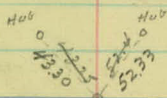
Rad = 5729.65 ✓

Tang = 98.3 ✓

P.C. = 51+97.5 ✓

Length = 196.7 ✓

P.T. = 53+94.2 ✓



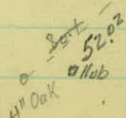
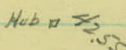
Sta. - Def

45+28.8 - 0°00'

46+00 - 0°22'

47+00 - 0°52'

+40.8 - 1°04 1/2'



1° Curve Rt.

 $\Delta = 2°09'$

Rad = 5729.65 ✓

Tang = 107.5 ✓

P.C. = 45+28.8 ✓

Length = 218.0 ✓

P.T. = 47+40.8 ✓

Ang ht. Ang Rt.

N. 86° 53' W.

61 + 28.5 P.T.

59 + 80.3 P.I.

5° 56'

58 + 31.8 P.C.

S. 87° 11' W.

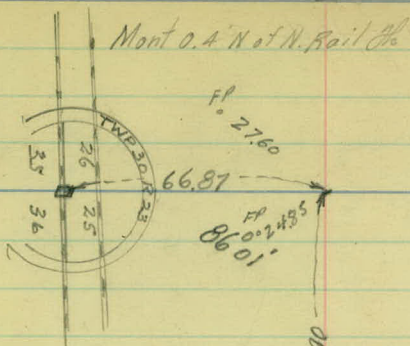
57 + 57.0 P.T.

56 + 87.0 P.I. 2° 48'

56 + 17.0 P.C.

S. 89° 59' W.

4-16 24



Sta. - Det

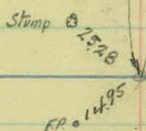
58+31.8 - 0°00'

59+00 - 0°41'

60+00 - 1°041'

61+00 - 2°41'

+28.5 - 2°58'



2° Curve Rt.

$\Delta = 5°56'$

Rad = 2864.9 ✓

Tang = 148.5 ✓

P.C. = 58+31.8 ✓

Length = 296.7 ✓

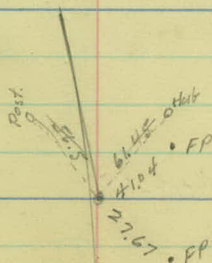
P.T. = 61+28.5 ✓

Sta. - Det

56+17.0 - 0°00'

57+00 - 0°50'

57+57 - 1°24'



2° Curve ht.

$\Delta = 2°48'$

Rad = 2864.9 ✓

Tang = 70.01 ✓

P.C. = 56+17.0 ✓

Length = 140.0 ✓

P.T. = 57+57 ✓

Flight. Ang. Rt.

N. 88° 03' W.

67 + 56.9 ✓ P.T.

66 + 74.4 P.I.

3° 18'

65 + 91.9 ✓ P.C.

5.88° 39' W.

65 + 49.3 ✓ P.T.

64 + 74.9 P.I. 4° 28'

64 + 00.4 ✓ P.C.

N. 86° 53' W.

Sta. - Def.

65+91.9 - 0°00'

66+00 - 0°05'

67+00 - 1°05'

67+56.9 - 1°39'

F.P. 28.70

F.P. 22.98

2° Curve Rt.

 $\Delta = 3°18'$

Rad = 2864.93 ✓

Tang = 52.53 ✓

P.C. = 65+91.9 ✓

Length = 165.0 ✓

P.T. = 67+56.9 ✓

Sta. - Def.

64+00.4 - 0°00'

65+00 - 1°30'

+49.3 - 2°14'

F.P. 31.66

F.P. 34.92

3° Curve Lt.

 $\Delta = 4°28'$

Rad = 1910.1 ✓

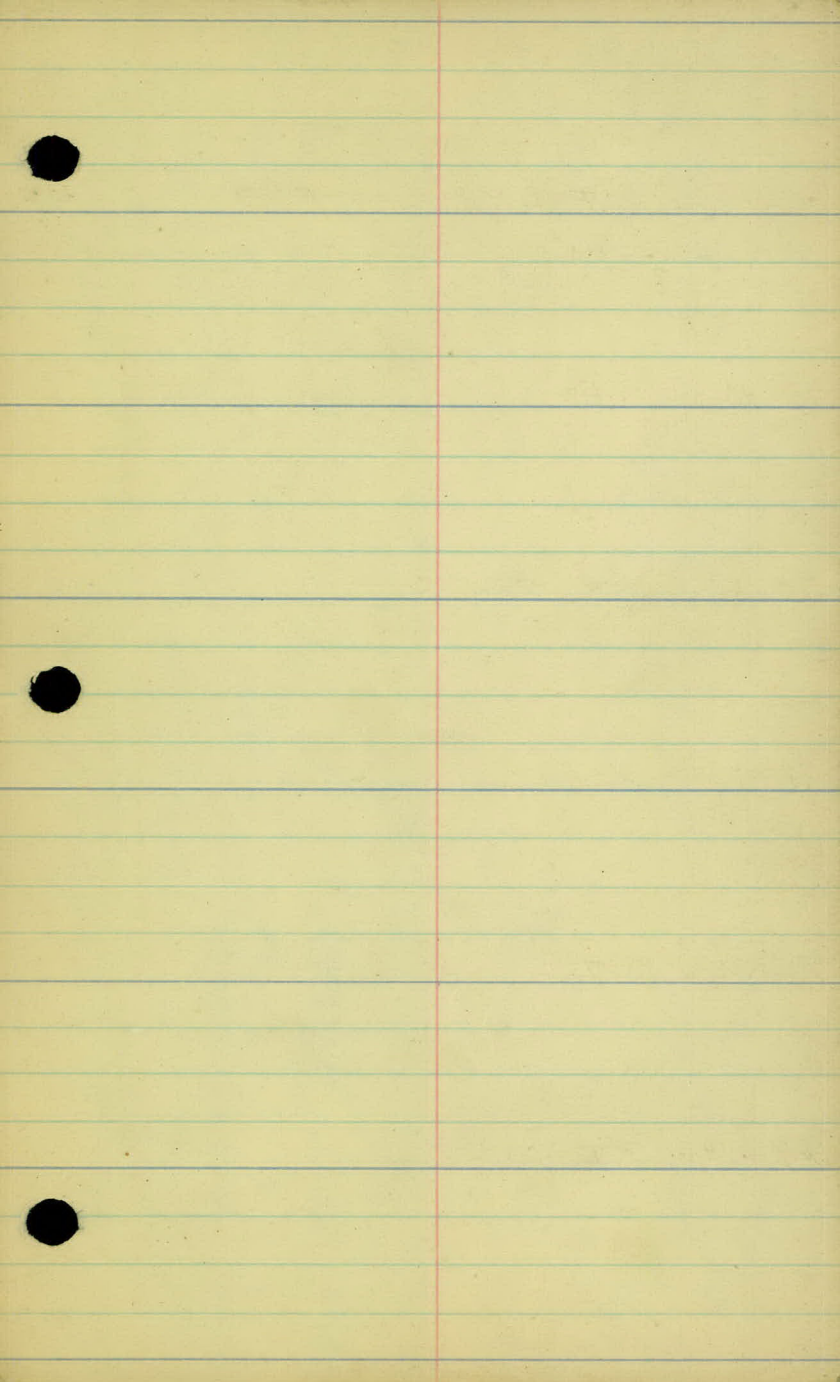
Tang = 74.5 ✓

P.C. = 64+00.4 ✓

Length = 148.9 ✓

P.T. = 65+49.3 ✓

69+74.2 P.I.



⁴
Anght. Ang R.

78+46.0 P.O.T. E.R.R.

78+32.2 E.R.R.

5.17°20'W.

78+16.8[✓] P.T.

✓77+80.3 P.I. 73°03'

77+29.67 P.C.

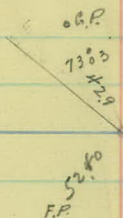
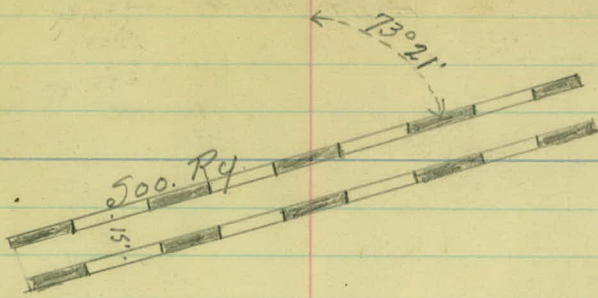
N.89°37'W.

70+52.6[✓] P.T.

69+74.2 P.I. 1°34'

68+95.9[✓] P.C.

N.88°03'W.



94° Curve ht.

$$\Delta = 73^{\circ} 03'$$

$$\text{Rad} = 68.37 \checkmark$$

$$\text{Tang} = 50.63 \checkmark$$

$$\text{P.C.} = 77 + 29.67 \checkmark$$

$$\text{length} = 87.16 \text{ Arc.} \checkmark$$

$$\text{P.T.} = 78 + 16.83 \checkmark$$

Rad. Hub set.

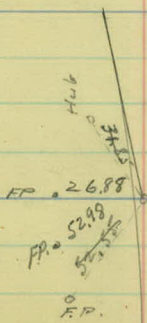
Sta - Def

$$68 + 95.9 - 0000'$$

$$69 + 00 - 0001'$$

$$70 + 00 - 0031$$

$$+ 52.6 - 0047'$$



1° Curve ht.

$$\Delta = 10^{\circ} 34'$$

$$\text{Rad.} = 5729.6 \checkmark$$

$$\text{Tang} = 78.3 \checkmark$$

$$\text{P.C.} = 66 + 95.9 \checkmark$$

$$\text{Length} = 156.7 \checkmark$$

$$\text{P.T.} = 70 + 52.6 \checkmark$$

~~4~~
Anght. Ang. Rt.

5.88° 51' W.

85 + 316 ✓ P.T.

83 + 65 P.I. 3° 20'

81 + 983 ✓ P.C.

N. 87° 49' W.

79 + 490 ✓ P.T.

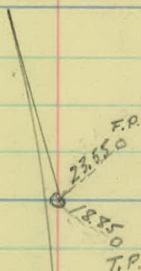
79 + 178 P.I.

74° 51'

78 + 736 ✓ P.C.

5.17° 20' W.

Sta - Def
 71+983 - 0000'
 82+00 - 0000 1/2'
 83+00 - 0030 1/2'
 84+00 - 1000 1/2'
 85+00 - 1°30 1/2'
 +31.6 - 1040'



1° Curve Left
 $\Delta = 3^\circ 20'$
 Rad = 5729.6 ✓
 Tang = 166.7 ✓
 P.C. = 81+98.3 ✓
 length 333.3 ✓
 P.T. = 85+31.6 ✓



120° Curve R.H.
 $\Delta = 74^\circ 51'$
 Rad = 57.73 ✓
 Tang = 44.17 ✓
 P.C. = 78+73.6 ✓
 length = 75.4 Act. Arc. ✓
 D.T. = 79+49° ✓
 Rad. Hub. Set

Height Ang. Rt.

N. 77° 34' W.

89 + 86.2 ✓ P. T.

88 + 89.9 P. I.

29° 38'

87 + 88.6 ✓ P. C.

S. 72° 48' W.

87 + 43.8 ✓ P. T.

86 + 44.3 P. I. 16° 03'

85 + 43.2 ✓ P. C.

S. 88° 51' W.

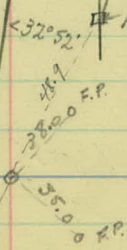
177
182
177

Sta. - Def.
 87+88.6 - 0°00'
 88+00 - 0°51' ^{5th}
 +50 - 4°36' ^{192.5}
 89+00 - 8°21' ^{8.35}
 +50 - 12°06' ^{5th}
 +86.2 - 14°49'

15° Curve. Rt.
 $\Delta = 29°38'$
 Rad = 383.1
 Tang = 101.3 ✓
 B.L. = 87+88.6 ✓
 length = 197.6 ✓
 P.T. = 89+86.2 ✓



Sta. - Def
 85+43.2 - 0°00'
 86+00 - 2°16 1/2'
 +50 - 4°16 1/2'
 87+00 - 6°16 1/2'
 +43.8 - 8°01 1/2'



M.C. 8° Curve Lt.
 $\Delta = 16°03'$
 Rad = 716.8 ✓
 Tang = 101.1 ✓
 P.C. = 85+43.2 ✓
 length 200.6 ✓
 P.T. = 87+43.8 ✓

~~E~~
Anght. Ang. Rt.

N. 88° 06' W.

94 + 88.9 ✓ P.T.

94 + 20.6 P.I. 2° 44'

93 + 52.2 ✓ P.C.

N. 85° 22' W.

92 + 93.4 ✓ P.T.

91 + 63.6 P.I. 7° 48'

90 + 33.4 ✓ P.C.

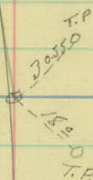
N. 77° 34' W.

Sta - Def

93+52.2 - 0°00'

94+00 - 0°29'

94+88.9 - 1°22'



2° Curve ht.

$\Delta = 2^\circ 44'$

Rad = 2864.93 ✓

Tang = 68.4 ✓

P.C. = 93+52.2 ✓

Length = 136.7 ✓

P.T. = 94+88.9 ✓

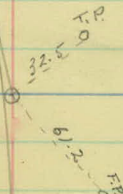
Sta. - Def

90+33.4 - 0°00'

91+00 - 1°00'

92+00 - 2°30'

+93.4 - 3°54'



3° Curve ht.

$\Delta = 7^\circ 08'$

Rad = 1910.08 ✓

Tang = 130.2 ✓

P.C. = 90+33.4 ✓

Length = 260.0 ✓

P.T. = 92+93.4 ✓

4
Anght. Ang. R.

114+78.8 Mont. & Lexington Ave.

S. 88° 15' W.

110+55.0 P.I. 0° 54'

S. 89° 09' W.

104+54.3 P.I. 0° 18'

S. 89° 27' W.

97+89.5[✓] P.T.

96+67.0 P.I. 2° 27'

95+44.5[✓] P.C.

N. 88° 06' W.

Lexington.

Mont.
N.W. Cor Sec. 35

Mont.
E 1/4 Sec. 27

88°56'

20.5
26.8

10"
34.95

51.75

Sta. - Def.

95+44.5 - 0°00'

96+00 - 0°10 1/2'

97+00 - 0°46 1/2'

+89.5 - 1°13 1/2'

1° Curve ht.

$\Delta = 2°27'$

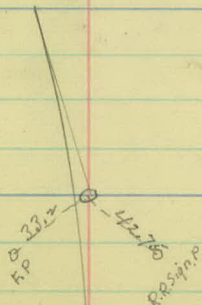
Rad. = 5729.65

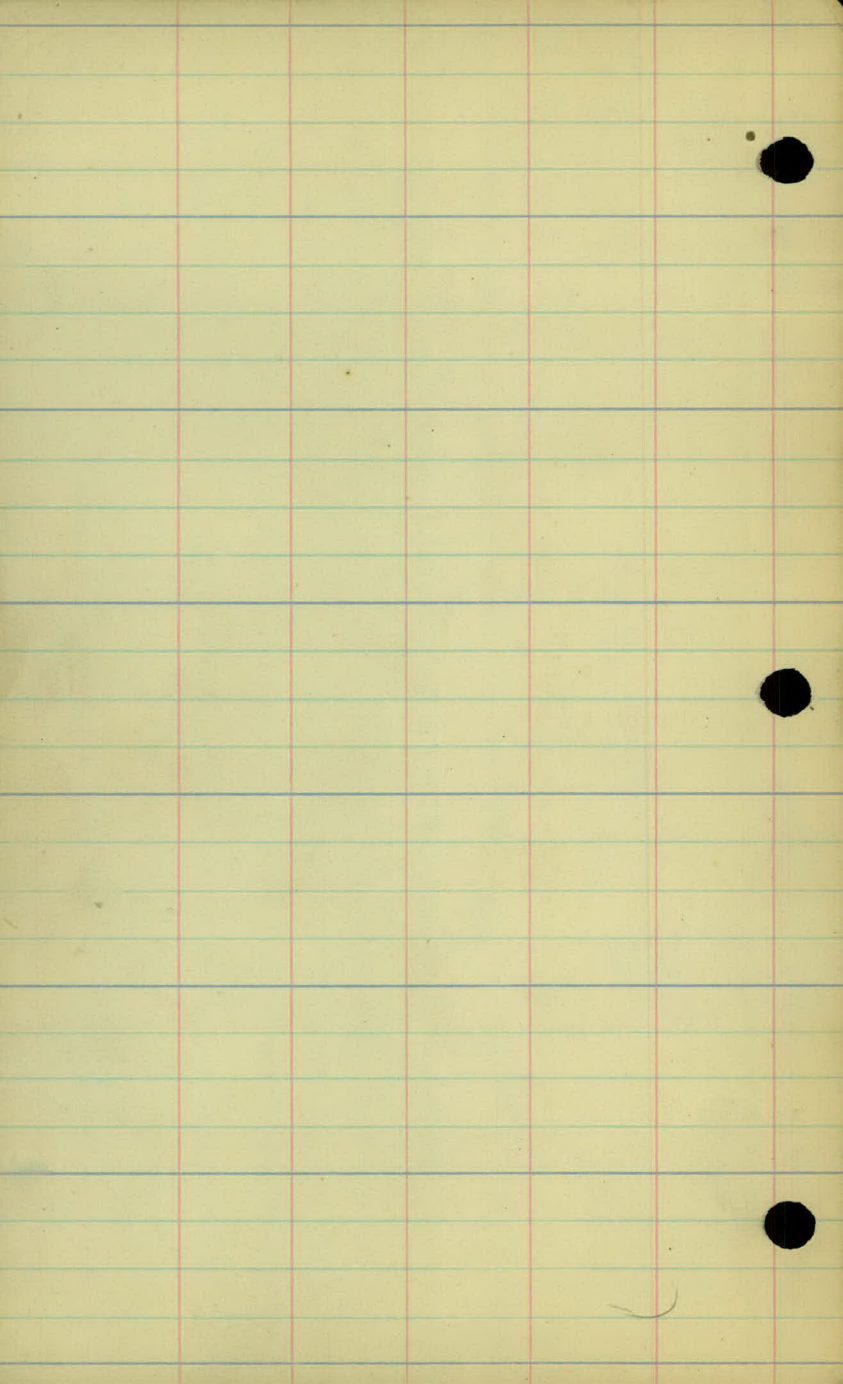
Tang. = 122.5

P.C. = 95+44.5

Length = 245.0

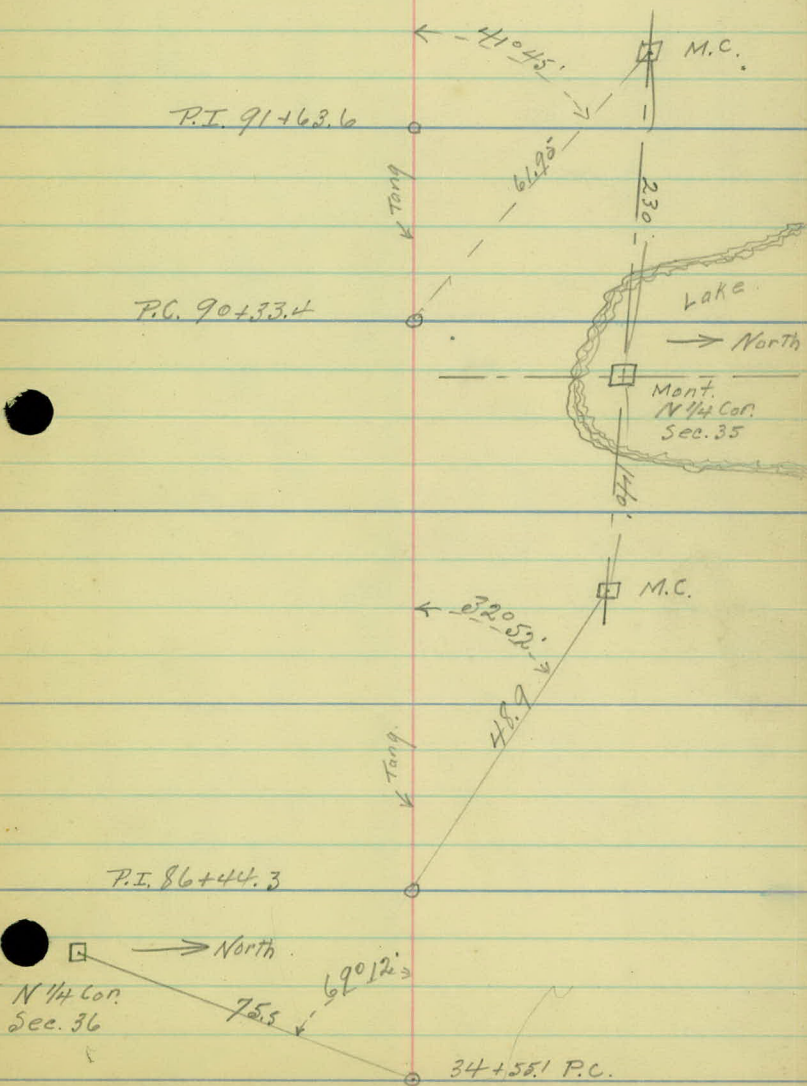
P.T. = 97+89.5

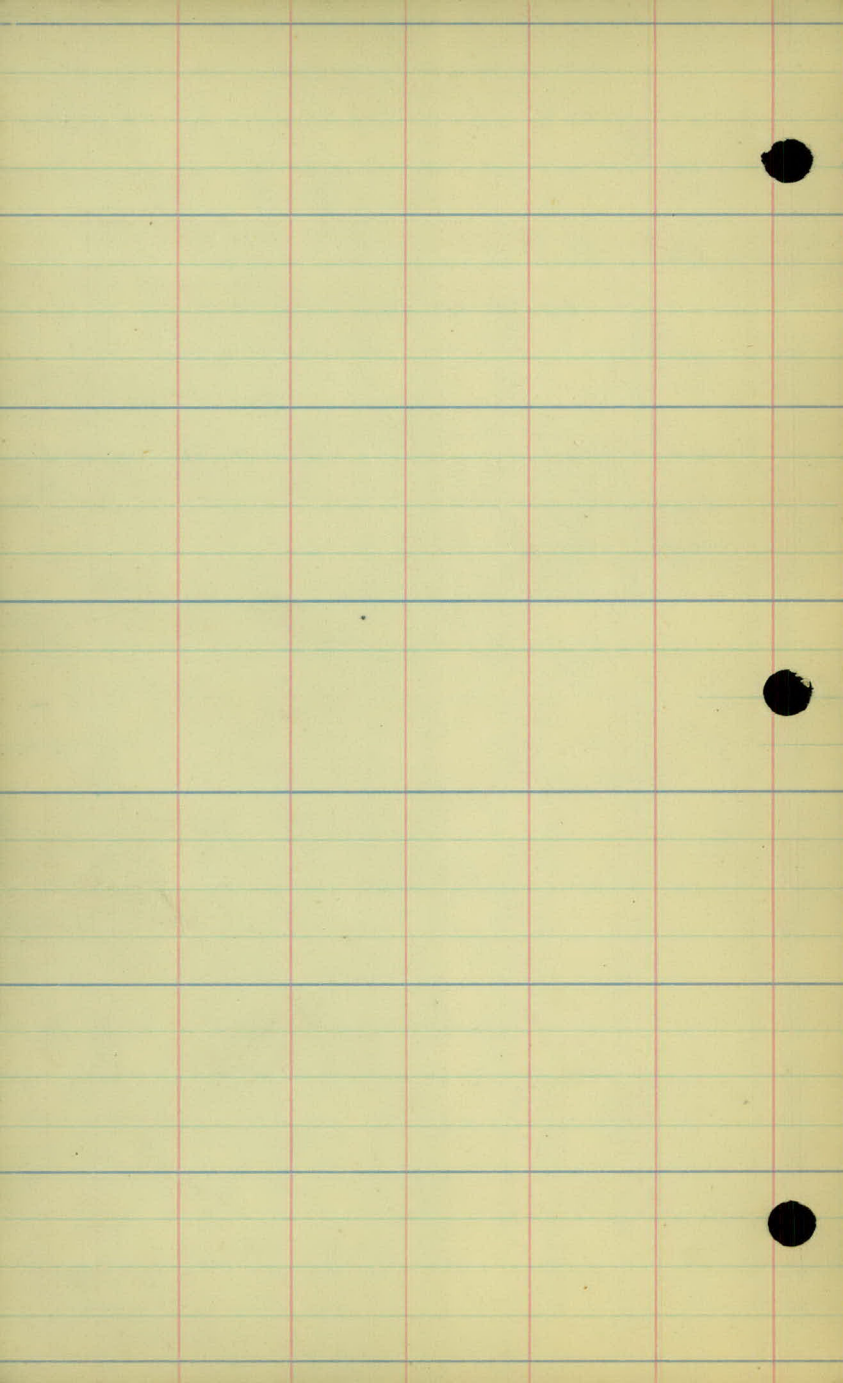


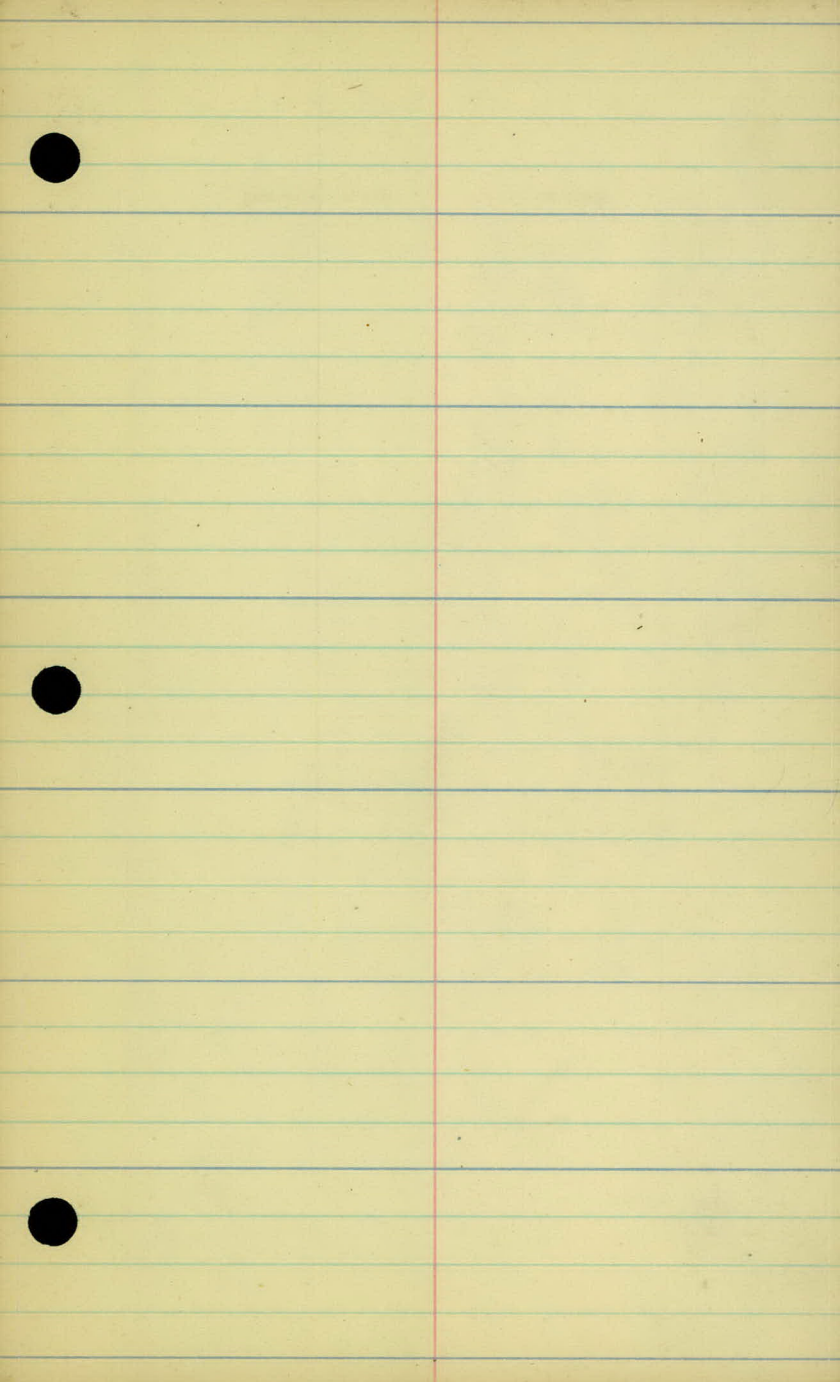


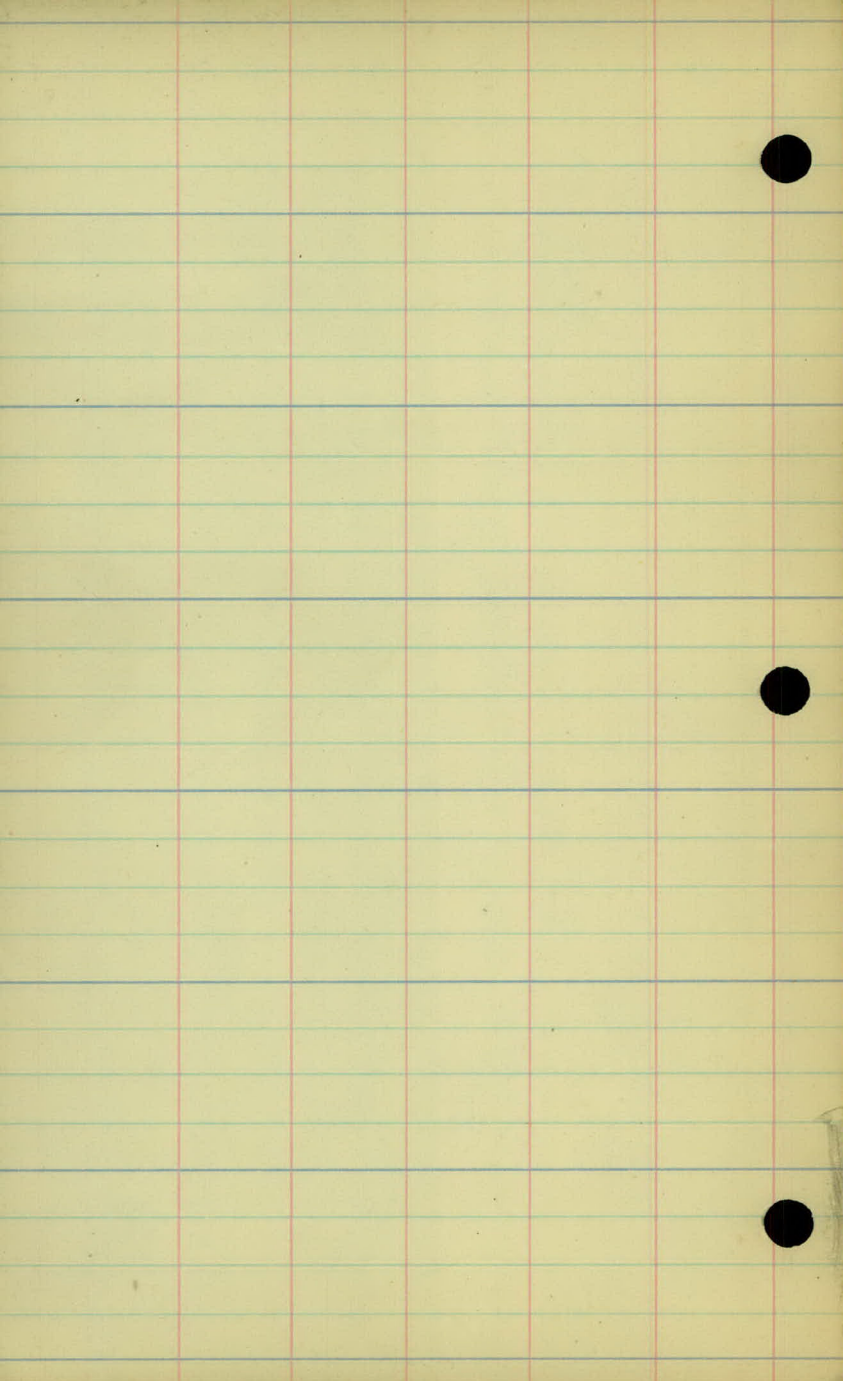
Section Ties.

#6









Rd #6

7+00

6+00

5+00

4+00

3+00

2+00

1+00

0+00

Pasture

Timber

Timber

Reed

Reed

48'

51'

58'

71'

80'

71'

38'

17'

185'

439

425'

15 T. P. 31' 4

27.
26

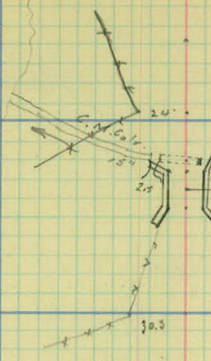
105

12+00

Little
Owasso

432 T.P. 30 R

13+00



12+00

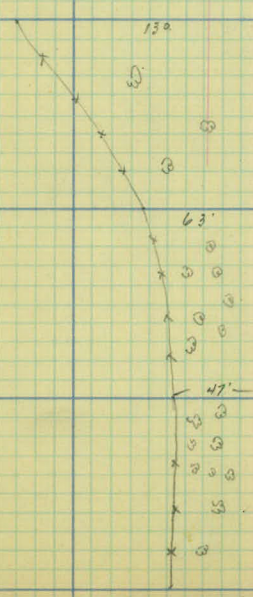
11+00

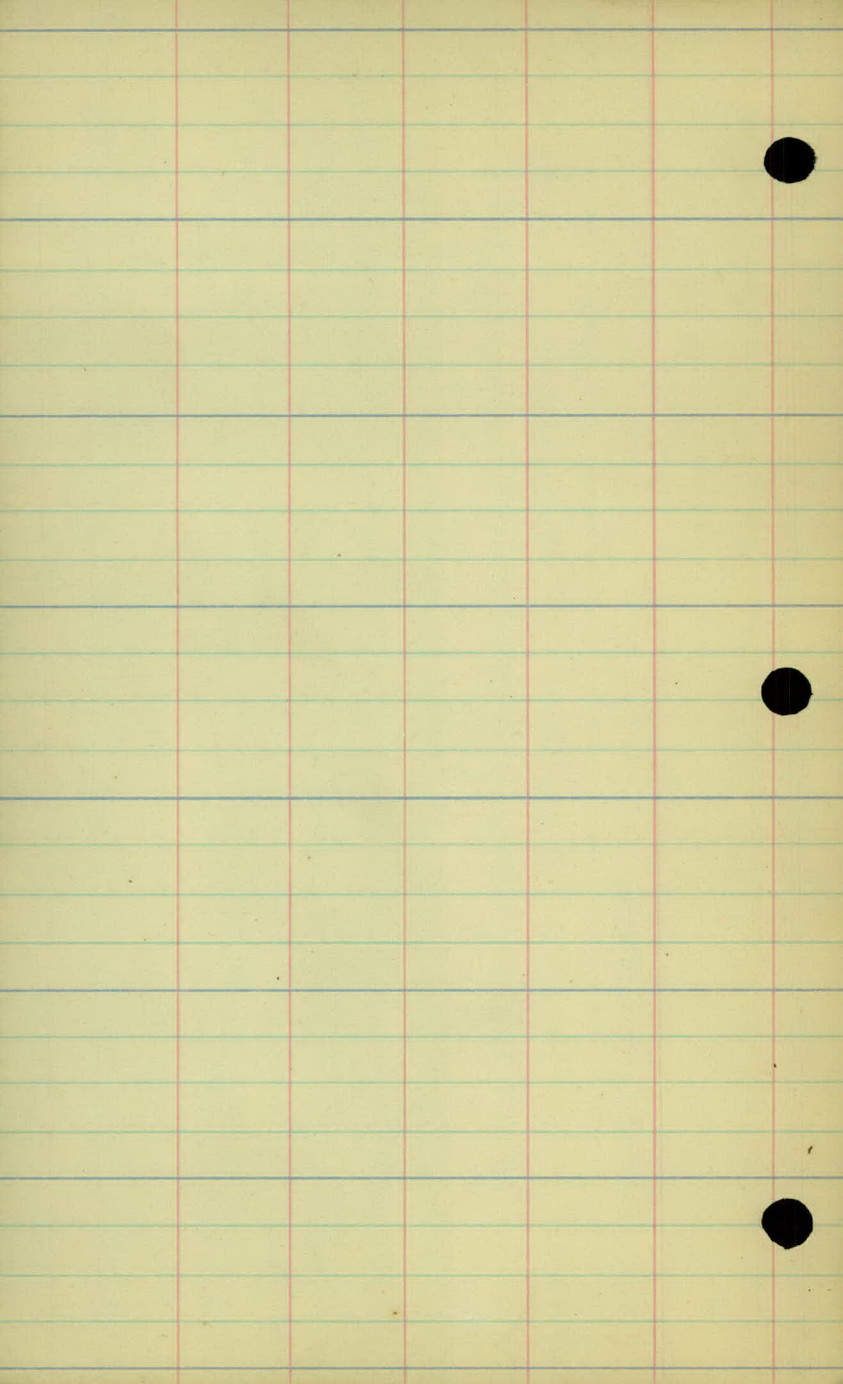
10+00

9+00

8+00

7+00





21+00

21'

20+00

100 T.P. 87'

21

109

19+00

100 T.P. 69'

21'

105

18+00

31

55

100 T.P. 59' R

500. Ry.

17+00

41'

59

190 T.P. 47' R

16+00

42'

51

181 T.P. 49' R

15+00

39

50

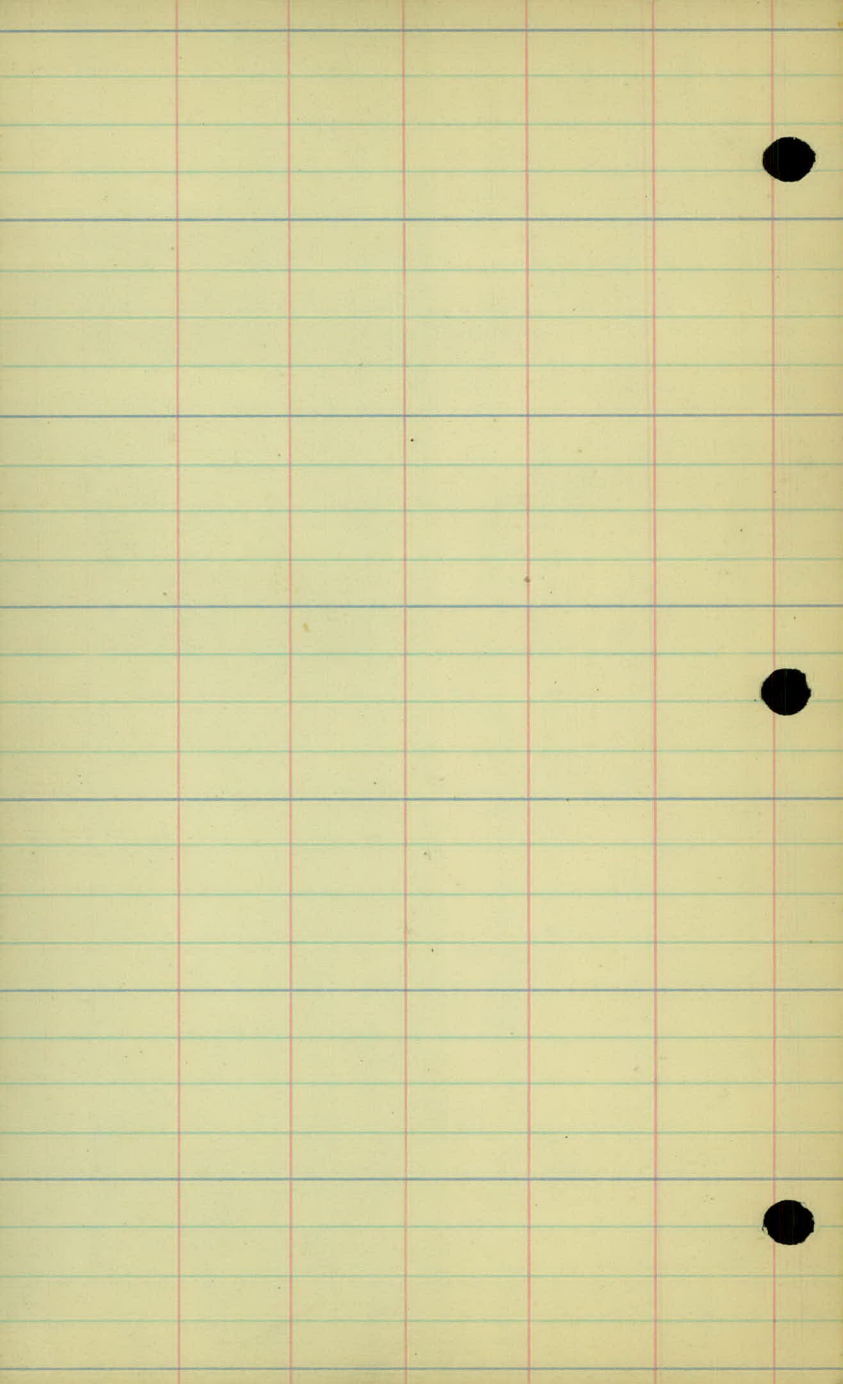
171 T.P. 50' R

21'

125 Bcg. Fence

14+00

Cultivated



26+00

27+00

26+00

25+00

24+00

23+00

22+00

21+00

117

400 Rad Fence

90

41.5'

36'

29'

102 Drive

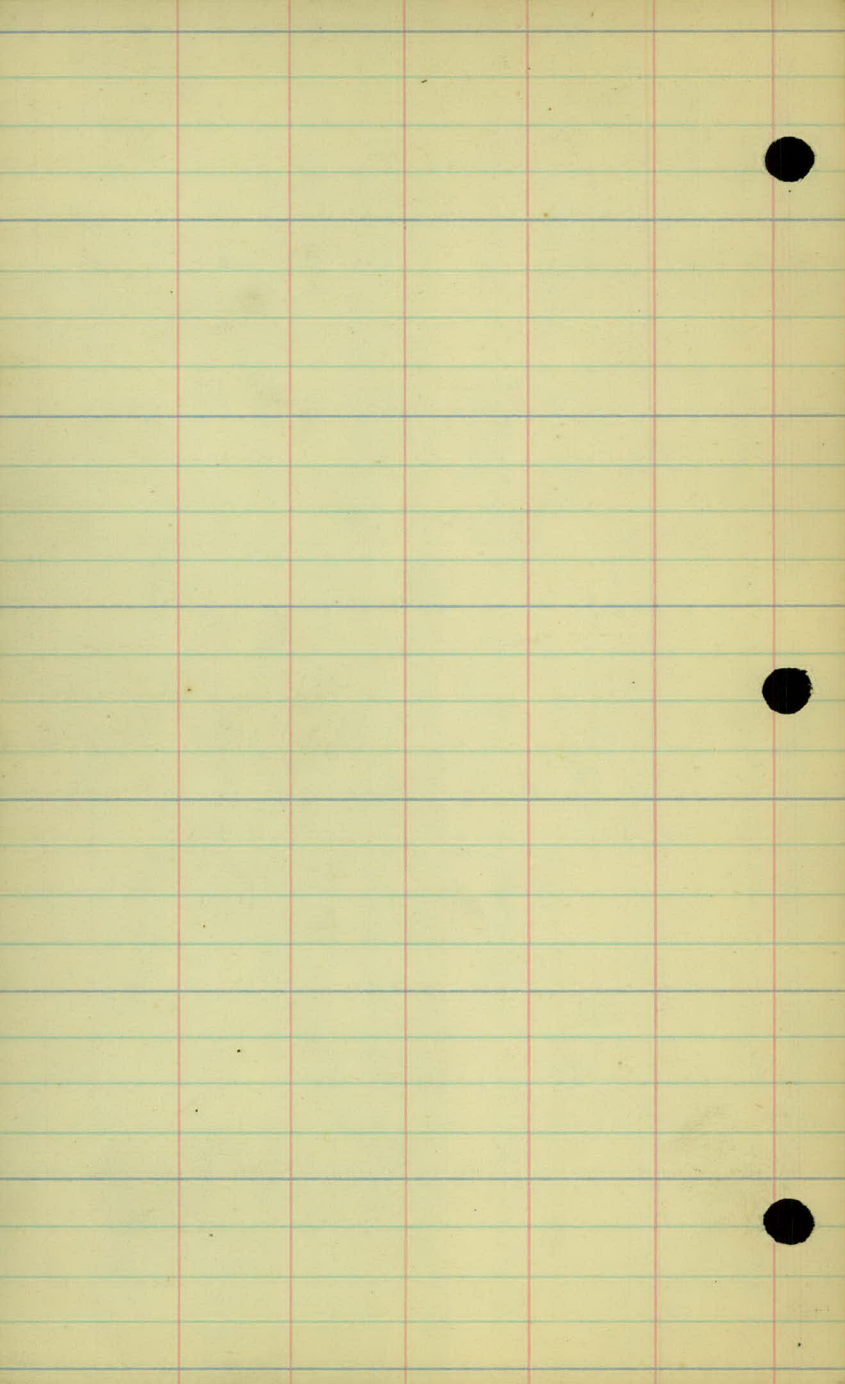
28'

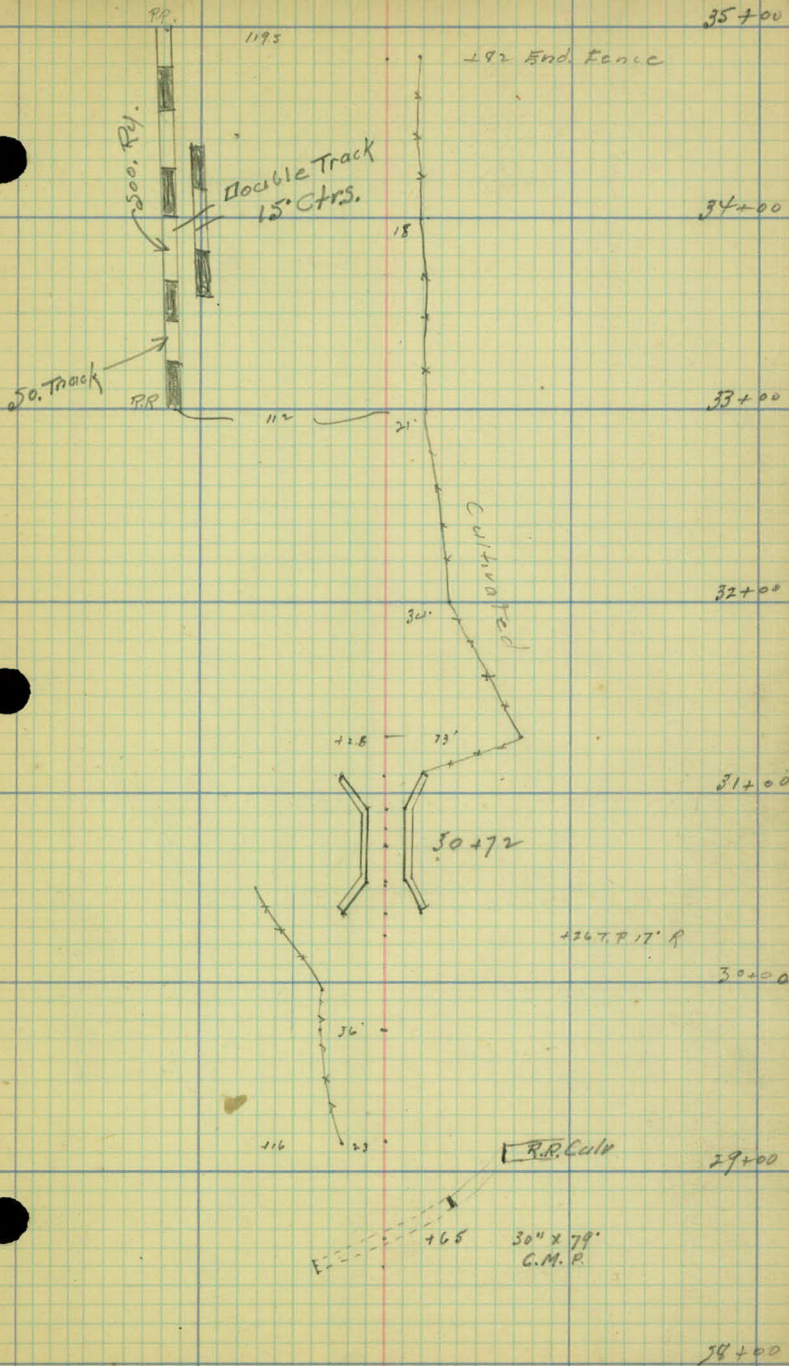
22'

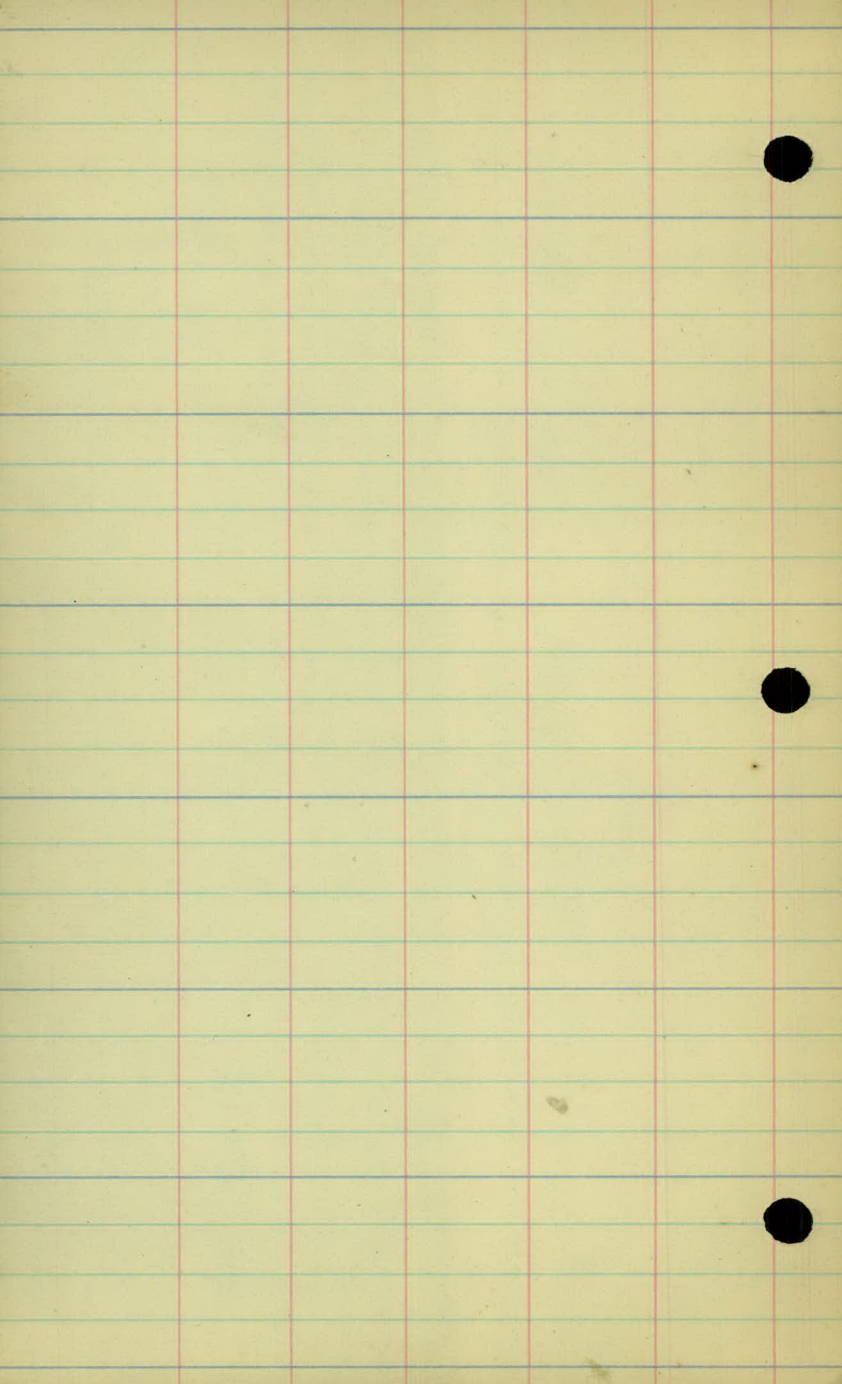
101

500. TR

Meadow Land







472+00

41+00

+87 Drive

40+00

78.0

132'

39+00

15' ctrs

38+00

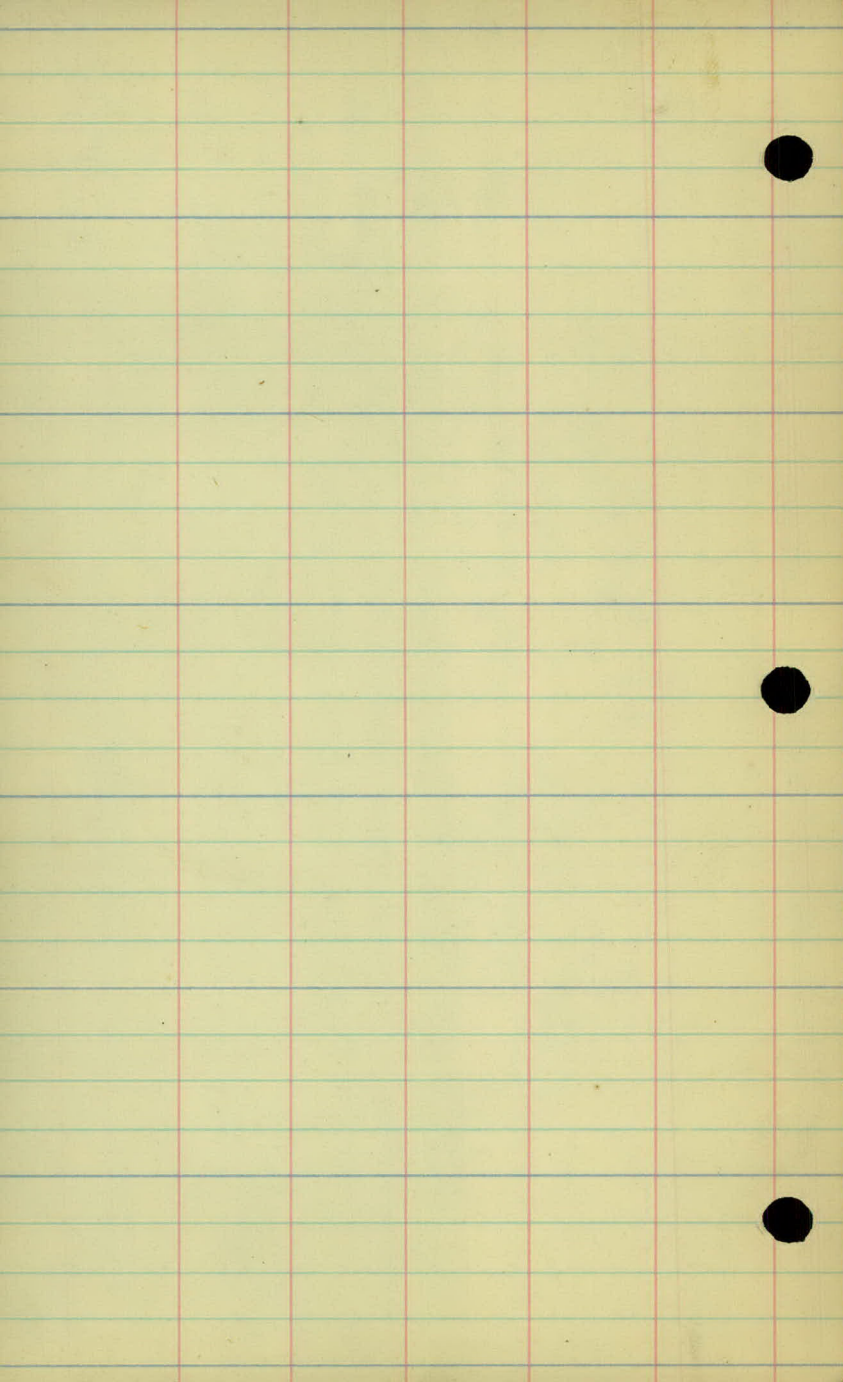
Cultivated

37+00

36+00

119.5

35+00



49+00

48+00

47+00

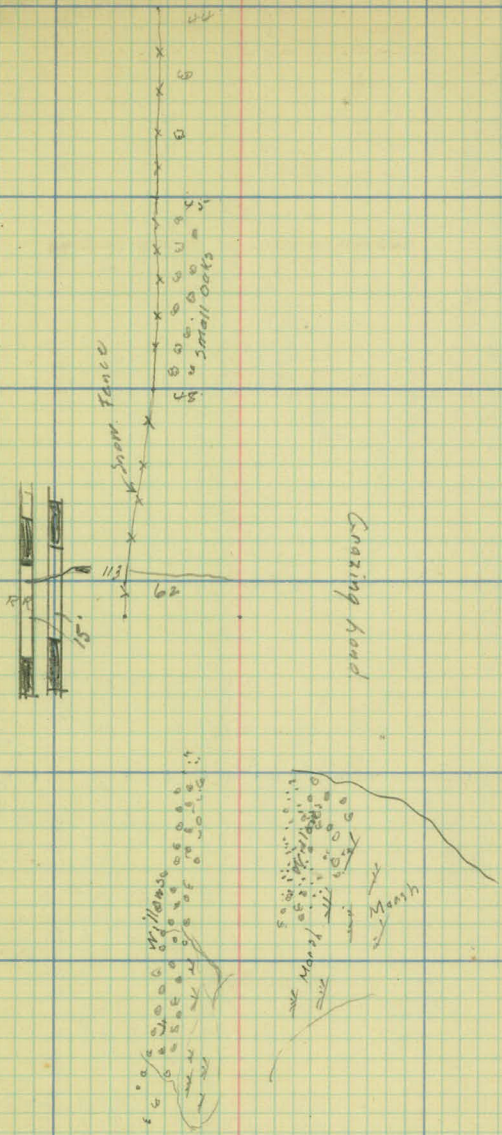
46+00

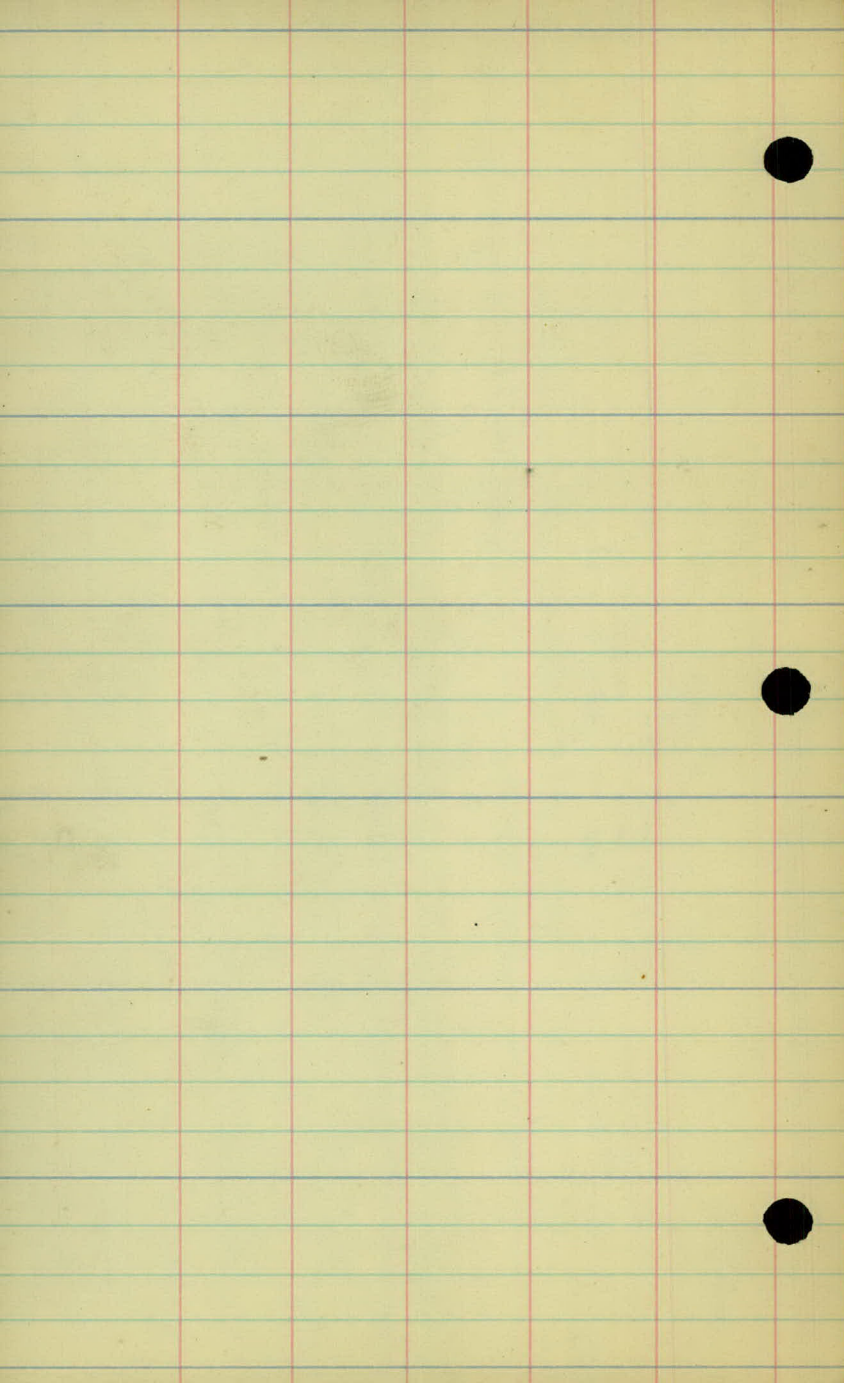
45+00

44+00

43+00

42+00





56+00

55+00

54+00

53+00

52+00

51+00

50+00

49+00

+50 Tacc 20' H.

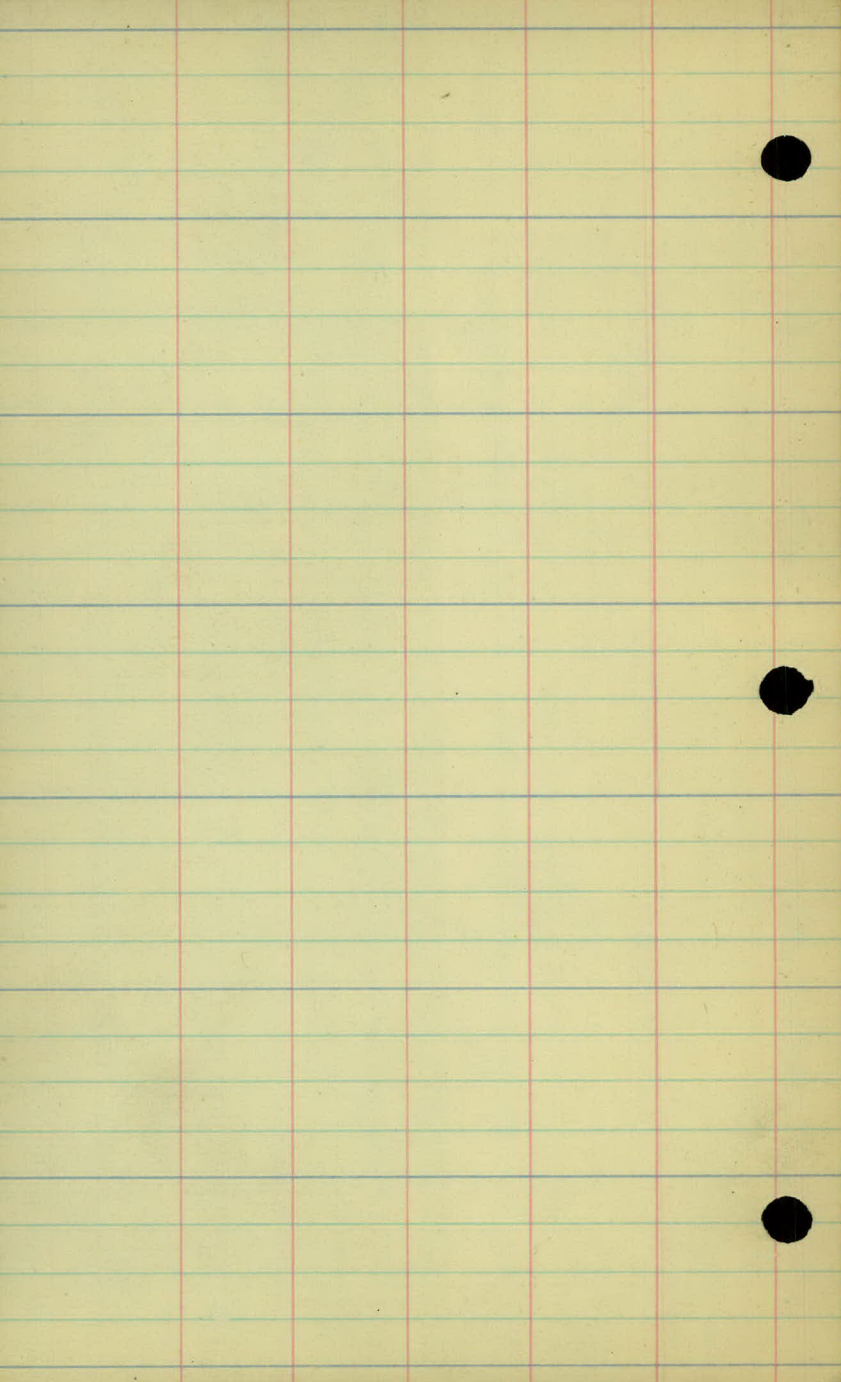
+63 Top Fence

R.R.

150 ft

Snow Fence

Grazing land.



63+00

62+00

61+00

60+00

59+00

58+00

57+00

56+00

76

23

23

17

7

21

25

28

R.R.

73

Cultivated

15' End Fence

Onchard

40 KE

30' Berry, Bushes

Ornate

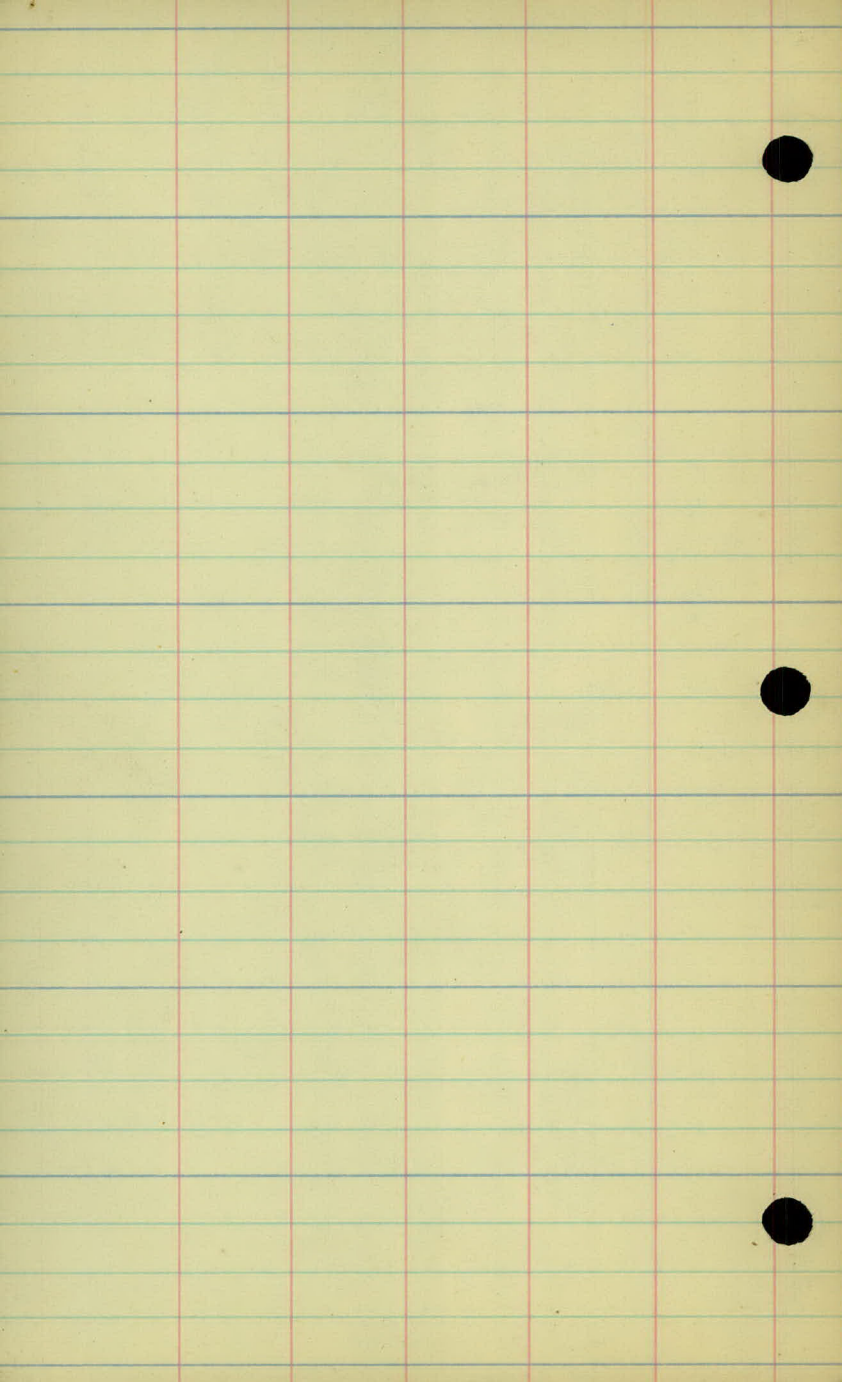
185

Tom pond

15' chgs

4" Drain

102 Tree 25' L



70+00

69+00

68+00

67+00

66+00

65+00

64+00

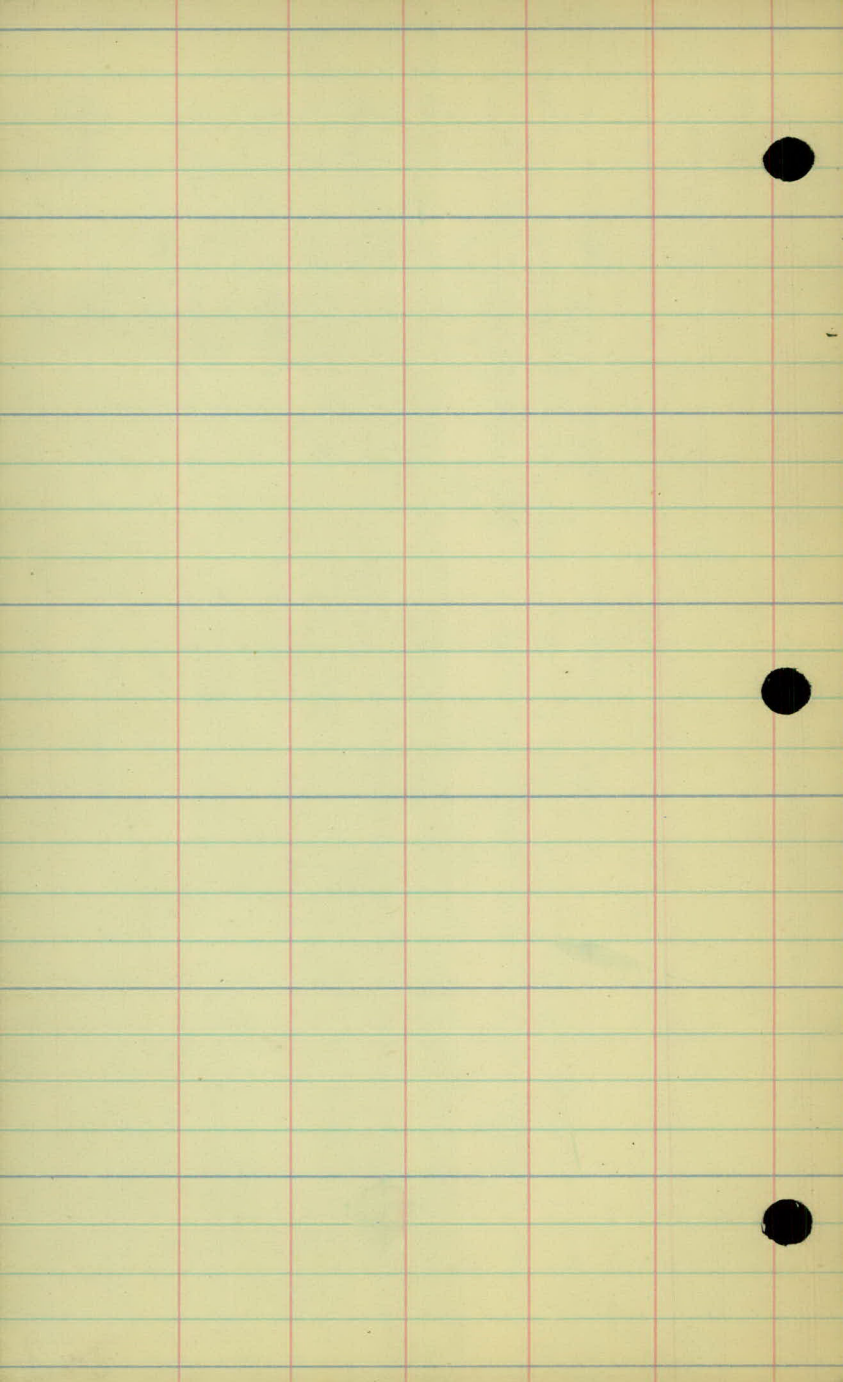
63+00

26
23'
22
20'
21'
23'
23'
22



200. Rd

Cultivated



H.

Rt.

77+00

Snow Fence

21'
21'
22'
24'
35'
25'
26'
26'
26'

76+00

+76 R.R. Xing Sign. 14' Rt.

Cultivated

75+00

+65 Beg. Snow Fence

+34 R.R. Xing Sign. 11' R.

74+00

73+00

R.R. 81.5

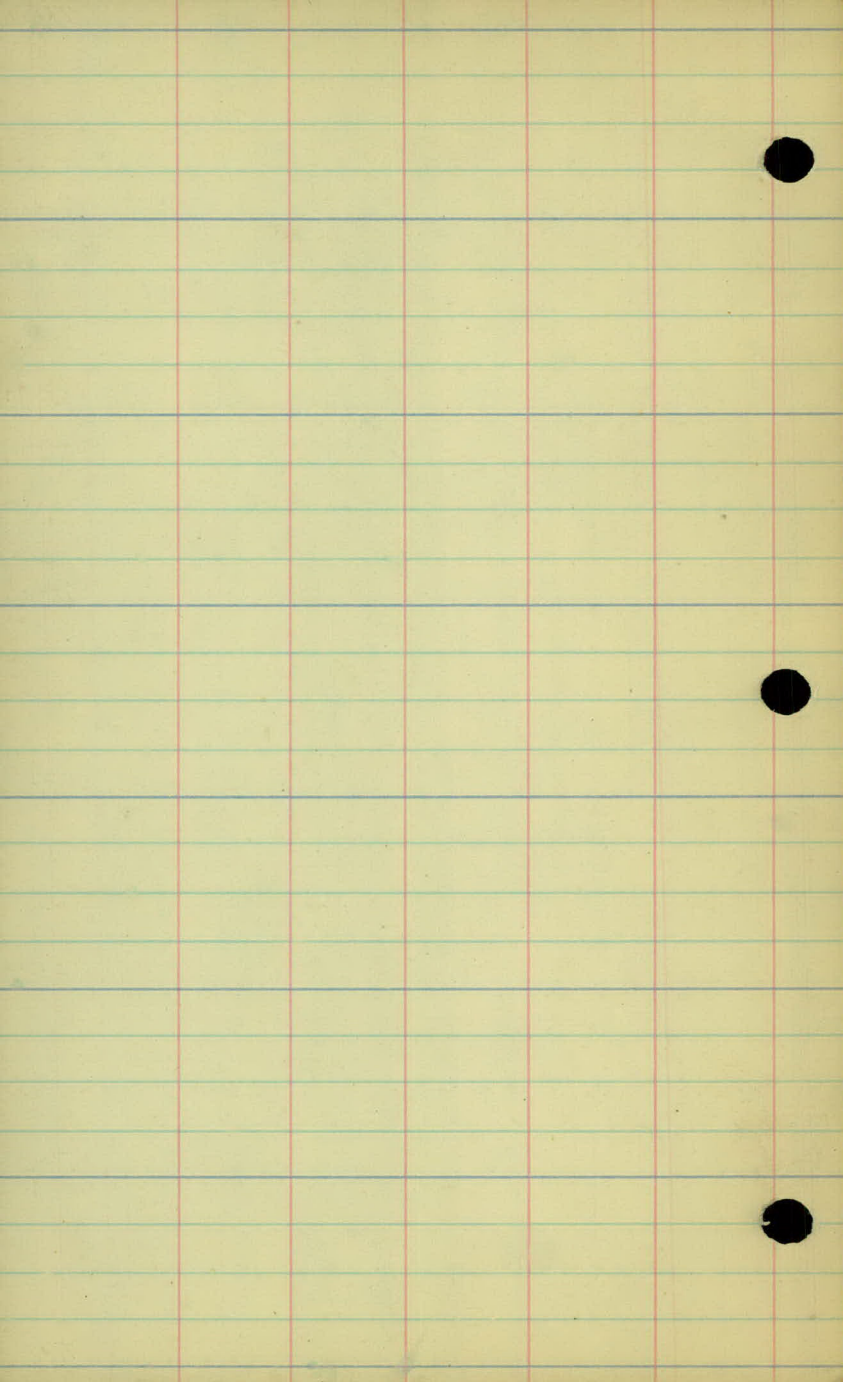
72+00

Cultivated

+46 End. Snow Fence

71+00

70+00



84+00

+00 T.P. 16' h

21

+53 T.P. 18' R

83+00

+80 T.P. 16' h

21

+24 T.P. 19' R

82+00

+52 T.P. 16' h

22

+12 T.P. 22' R

81+00

+02 R.R. Xing Sig. 12' h

25

+34 T.P. 15' h

25

+96 T.P. 35' R

80+00

+40 Tree 19' h

+37 T.P. 13' h

24.5

+27 T.P. 18' R

79+00

+87 T.P. 33' h

+98 T.P. 26' h

+11.3

12

F. Cor

+60 Danger Sig. 18' h

F. Cor

500' R₄

68'

39'

52'

Fen. Co + 08 G. P. 21' R
+03 S. R. 16' R

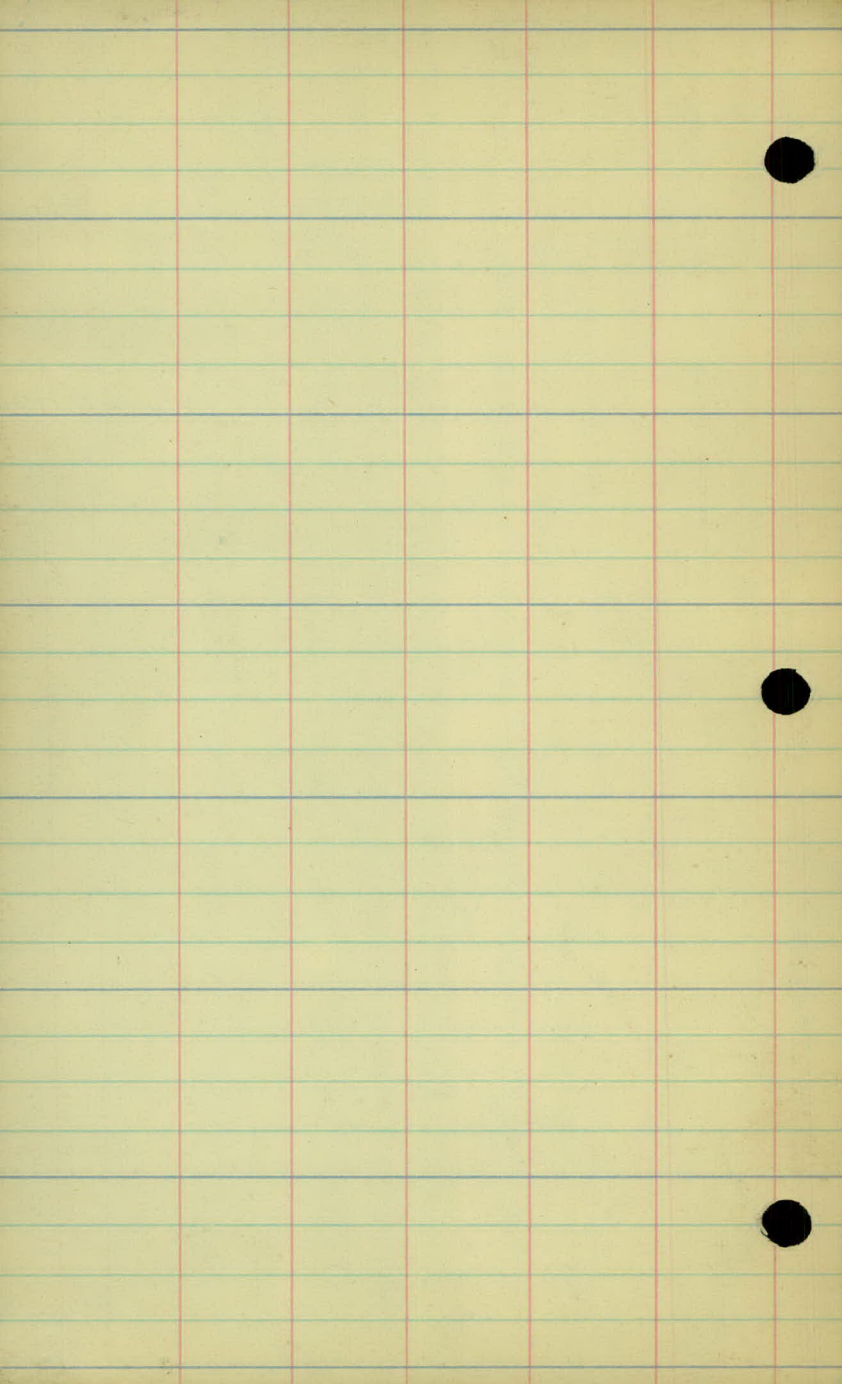
78+00

+88 T.P. 24' R

+87 T.P. 17' h

+65 Sign. P. 20' h

77+00



82'

+02 T.P. 57' P 91+00

+54 T.P. 25' R

90+00

Stump hard

40' 1/2

89+00

88+00

Meadow hard

+32 T.P. 16' R

87+00

+95 T.P. 42' R

46'

+10

15' C.M.

24" Con. Pipe under R.P.

86+00

29

+56 T.P. 24' R

+69 T.P. 15' L

+432 @

60.5

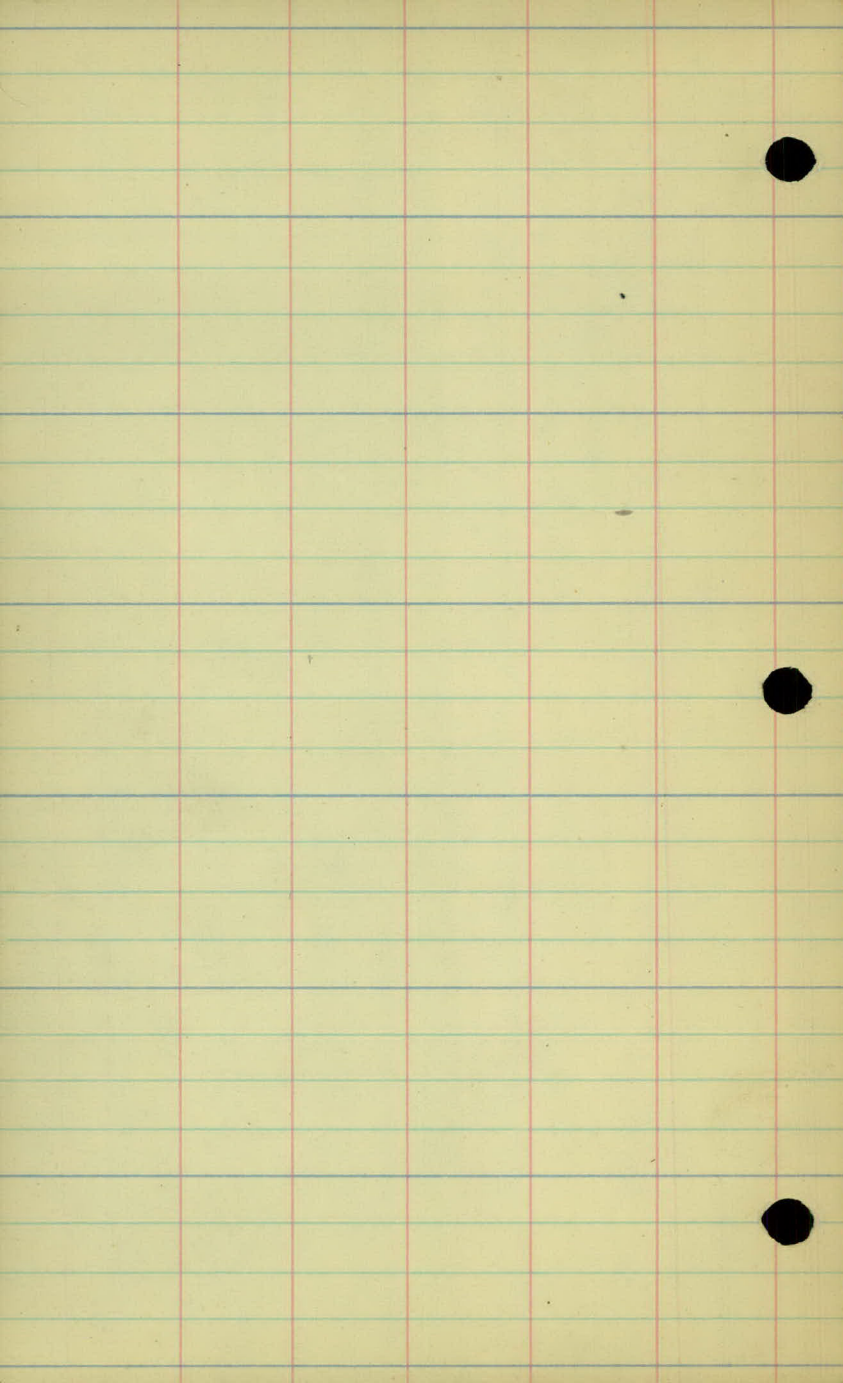
Meadow hard

85+00

23'

+73 T.P. 18' R

84+00



96+00

23'

55'

+88 T.P. 24' R

+64 T.P. 13' R

Timber

23'

51'

+10 T.P. 22' R

+33 T.P. 11' R

97+00

24'

29'

+57 T.P. 23' R

+15 T.P. 11' R

96+00

Timber

25'

25'

+00 T.P. 15' R

+07 T.P. 15' R

95+00

24'

31'

+26 T.P. 32' R

+65 T.P. 18' R

93+00

Timber

24'

37'

+14 T.P. 42'

+89 T.P. 25' R

92+00

26'

44'

Stamp
head.

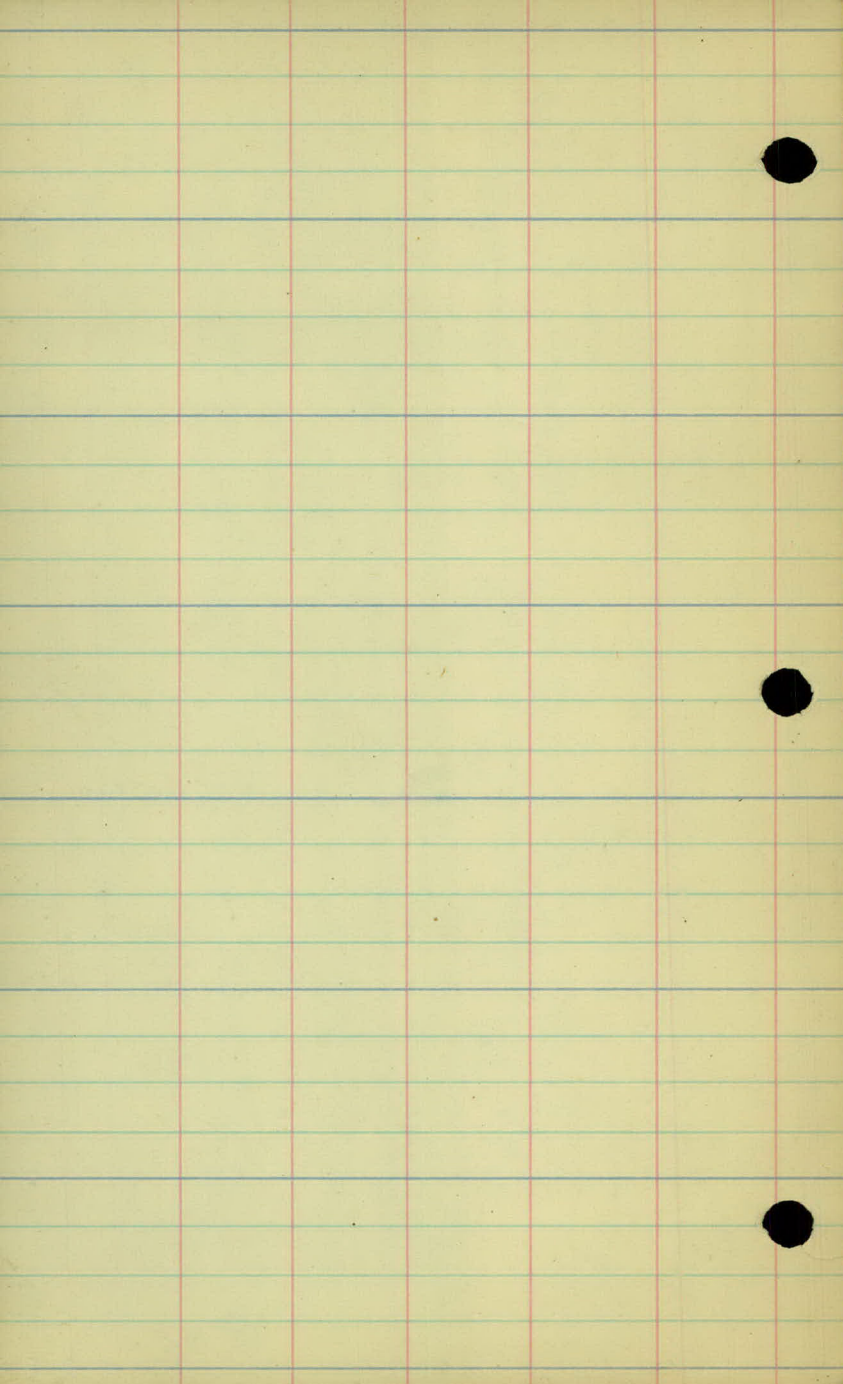
+50

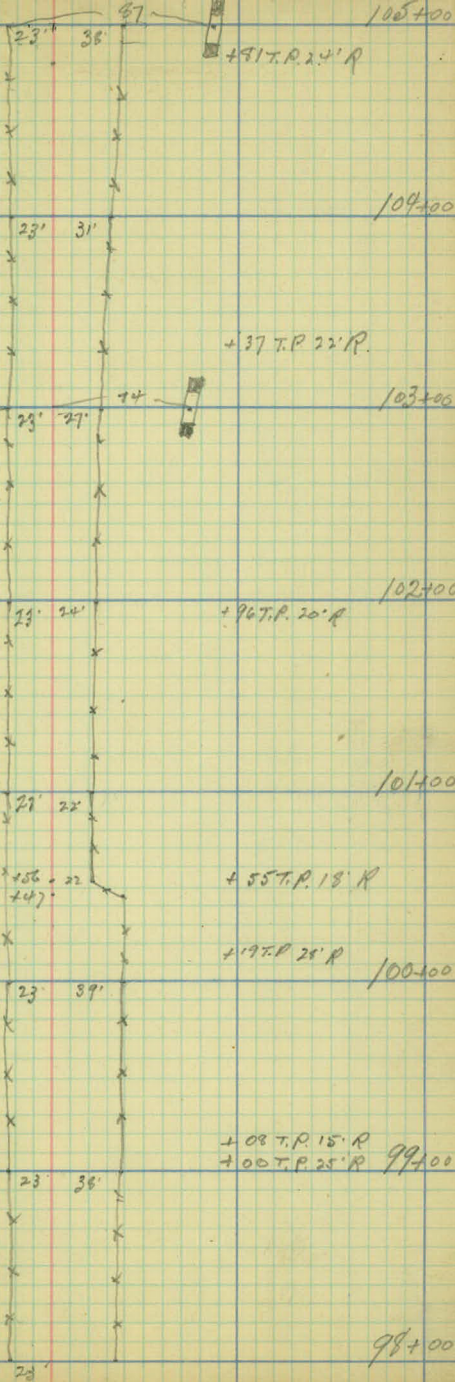
+57

53'

58'

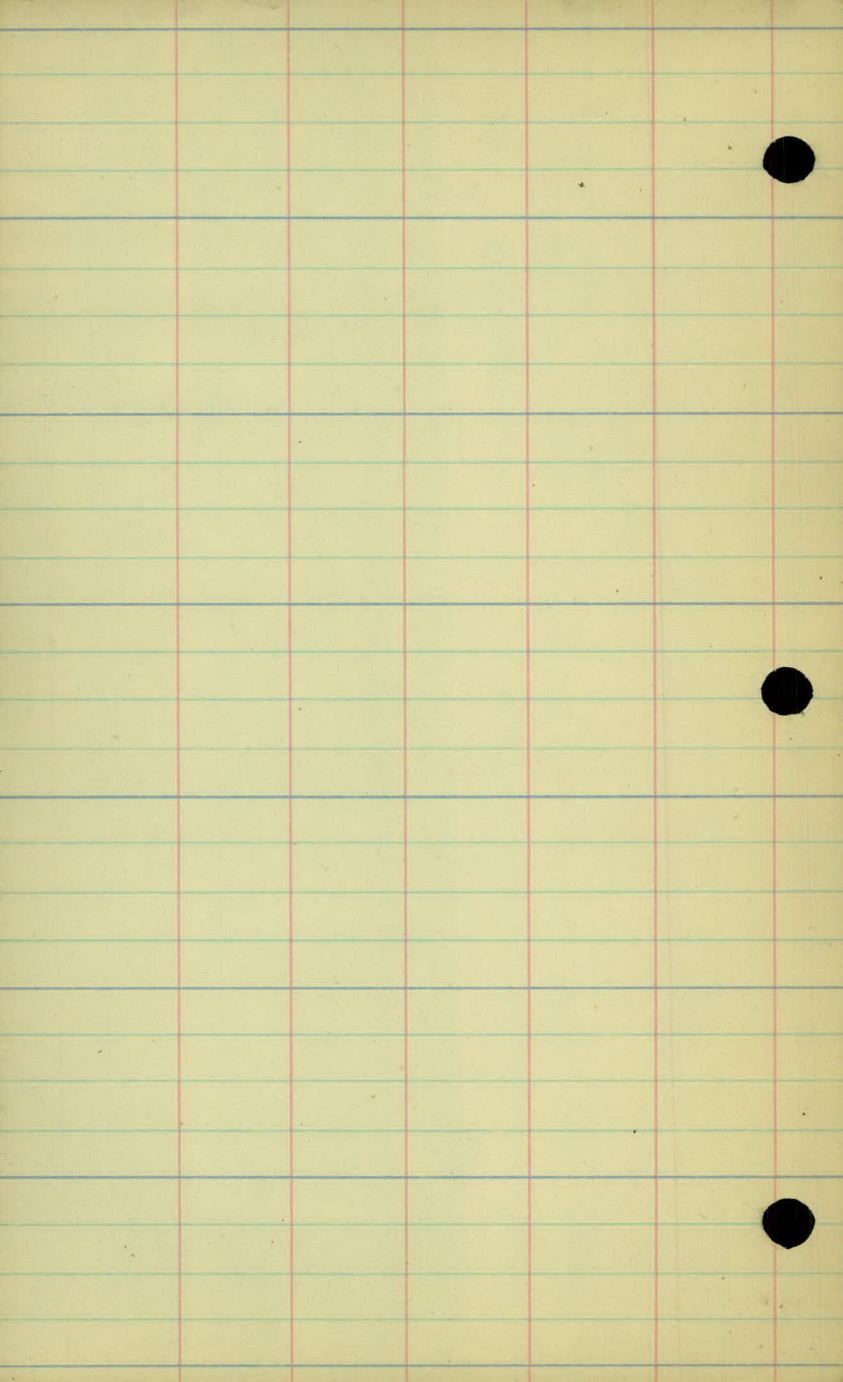
91+00





Timber

Timber



112+00

+37 T.P. 17' R

111+00

+09 T.P. 16'

110+00

+65 T.P. 15' R

109+00

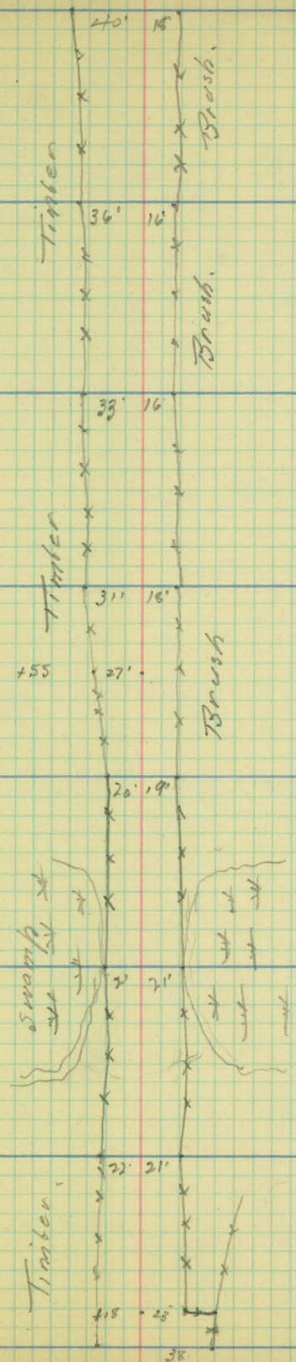
+67 T.P. + Fence 19' R

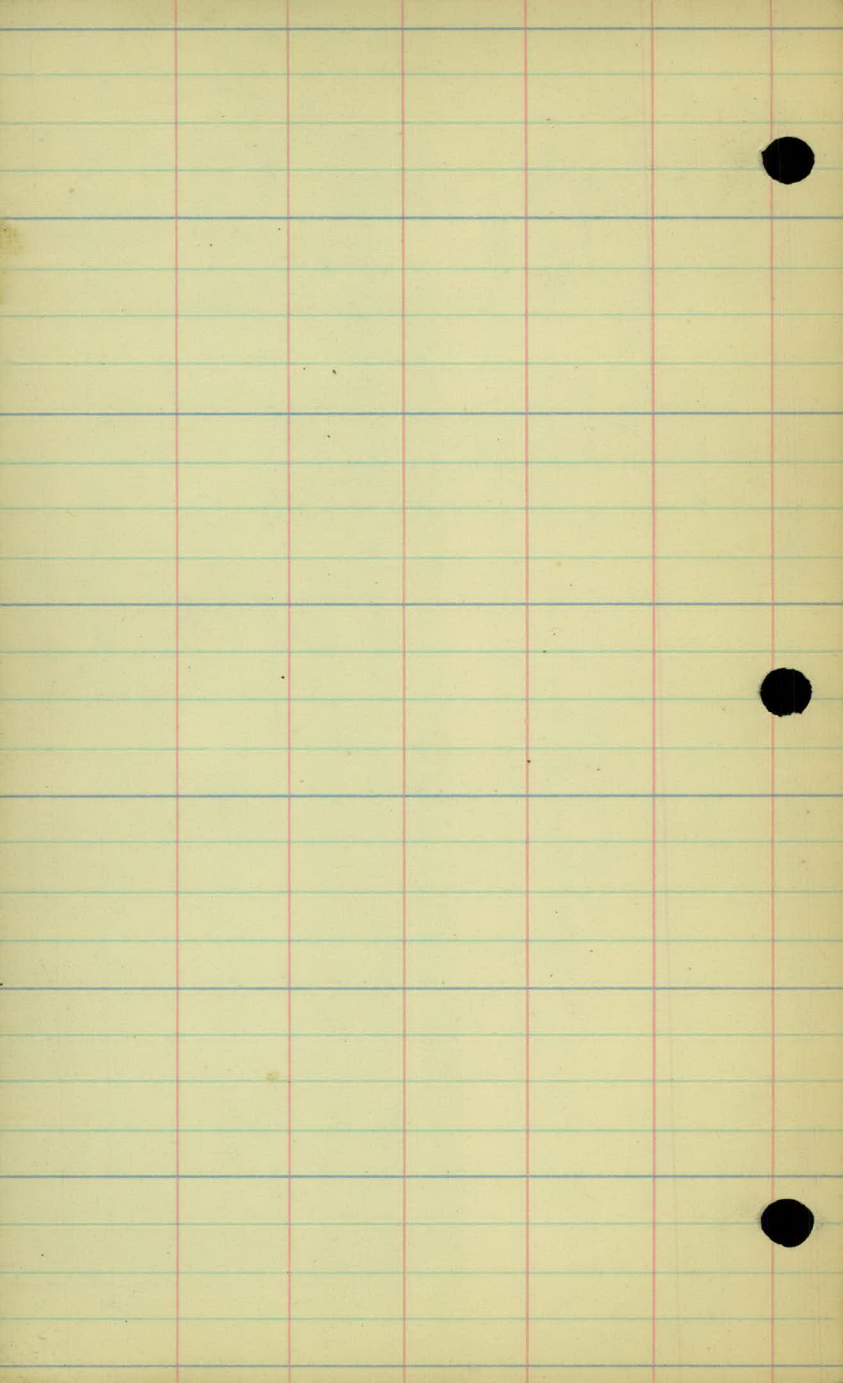
107+00

+20 T.N. 22' R

106+00

105+00





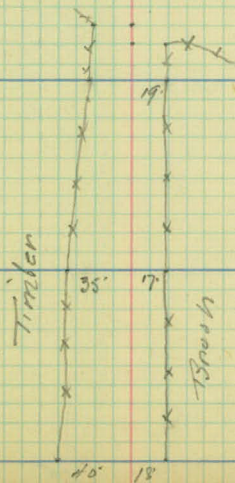
+78.8

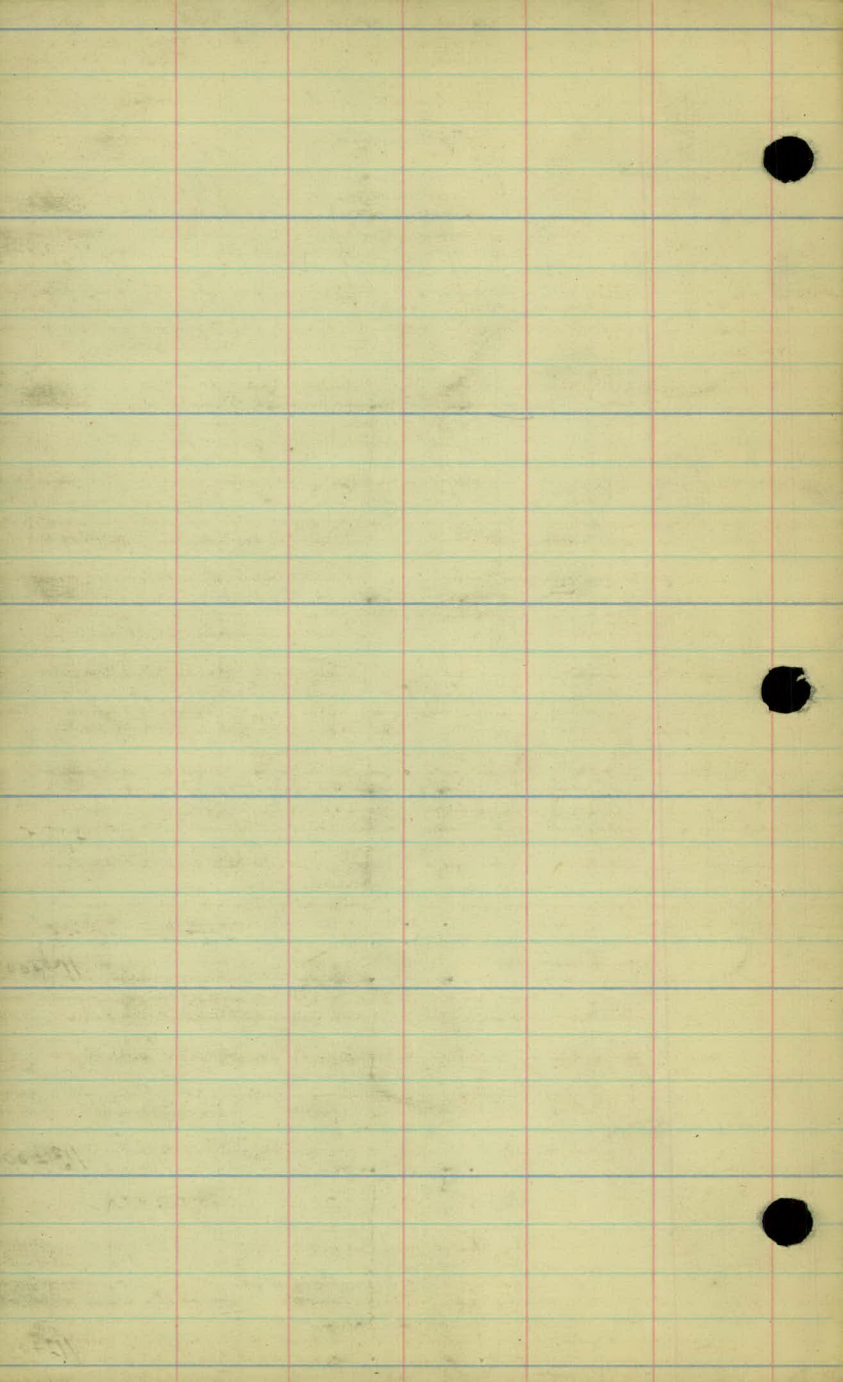
+21 T.P. + Fence 15' R
114+00

113+00

+83 T.P. 17' R

112+00





Road #6

Co. Rd "E." Rice to Lexington
Level Notes

Sta. 0+00 to

Austin	} Party
Skoglan	
Maloney	
Galvin	

April

Station	+	H.I	-	Rod.	Elev.
B.M.	4.53	238.77			234.24
0 + 00				4.5	34.3.
+ 24				4.4	34.4.
+ 36				4.7	34.1.
1 + 00				4.8	34.0.
2 + 00				5.0	33.8.
+ 50				5.0	33.8.
3 + 00				5.4	33.4.
+ 50				6.0	32.8.
T.P.	4.05	236.28	6.54	232.23	
4 + 00				3.8	32.5.
5 + 00				4.5	31.8.
6 + 00				4.2	31.9.
7 + 00				4.8	31.5.
8 + 00				5.4	30.9.
+ 50				5.5	30.8.
9 + 00				5.4	30.9.
+ 50				6.3	30.0.
T.P.	2.11	231.64	6.75	229.53	
10 + 00				8.7	27.9.
11 + 00				8.8	22.8.
+ 50				11.9	19.7.
T.P.	0.54	220.06	12.12	219.52	
12 + 00				4.0	16.1.
+ 50				7.3	12.8.
+ 65.6				8.0	12.1.
+ 65.6				298	222.02

Spike in 30" Cottonwood 40' R7 Sta 1462 { Ricc. St.
Nerv. par.

Bottom I. Berms.

Station	+	H.I.	-	Red	Elev.
		220.06			
12+79				8.2	211.9
+90				7.7	12.4
13+45				4.7	15.4
T.P.	9.33	225.92	3.47	216.59	
B.M.				8.25	217.67
14+00				7.7	18.2
15+00				5.2	20.7
16+00				2.7	23.2
17+00				0.5	25.4
T.P.	5.36	230.58	0.70	225.22	
18+00				3.9	26.7
+50				3.4	27.2
19+00				3.2	27.4
+50				3.4	27.0
20+00				4.8	25.8
+50				6.5	24.1
21+00				8.6	22.0
+50				10.6	20.0
22+00				13.0	17.6
T.P.	0.35	217.94	12.99	217.59	
+50				2.6	15.3
23+00				5.7	12.8
+50				7.4	10.5
24+00				9.6	208.3
+50				11.5	206.4
T.P.	0.35	207.06	11.23	206.71	

Spike in T.P. 25' R. sta 13+30

217.94
- 0.37
<u>217.57</u>
10.94
<u>228.51</u>
1.93
<u>226.58</u>
4.30
<u>230.88</u>
0.73
<u>230.15</u>
5.12
<u>235.27</u>
4.51
<u>230.76</u>
7.13
<u>237.91</u>
4.57
<u>233.34</u>
5.57
<u>238.91</u>
4.72
<u>234.19</u>

Nail in stp. 15 Rt. 24+65

Station	+	H.I. ✓	—	Red.	Elev.
		207.06			
25 + 00				2.9	204.2
+ 50				5.0	202.1
26 + 00				6.9	200.2
27 + 00				8.9	198.2
Eggs {27+38=27+24) (ong. Sta 114)					
+ 50				9.2	197.9
28 + 00				8.7 ✓	198.4
T.P.	9.77	208.12 ✓	8.71	198.35	✓
B.M.				7.38	200.74
29 + 00				8.9	199.2
+ 738				6.5	201.6
30 + 38.0				3.4	204.7
+ 54				2.5	205.6
+ 91				1.1 ✓	207.0
T.P.	10.00	217.14 ✓	0.98	207.14	
31 + 00				10.0	207.1
+ 15				9.5	207.6
+ 26.3				9.2	207.9
32 + 00				7.7	209.4
+ 50				6.9	210.2
33 + 00				5.7	211.4
+ 50				4.3	212.8
34 + 00				3.5	213.6
+ 50				3.3	213.8
35 + 00				2.9	214.2
36 + 00				1.5	215.6

Spike is 24" Oak 75' ht Sta 29 + 30

Station + H.I. - Red. Elev.

217.14 ✓

37+00

0.0 ✓ 217.1

T.P. 7.46 224.25 0.35 216.79

+50

5.9 18.4

38+00

4.7 19.6

+50

4.1 20.2

39+00

2.7 20.6

+50

4.1 20.2

40+00

4.8 19.5

+50

5.9 18.4

41+00

7.7 16.6

42+00

9.4 14.9

+50

9.5 14.8

43+00

9.0 ✓ 15.3

T.P. 11.33 226.30 9.28 214.97 ✓

+50

10.5 15.8

44+00

8.7 17.6

45+00

5.0 21.3

+50

2.5 23.8

46+00

0.2 ✓ 26.1

T.P. 2.94 228.97 0.32 225.98 ✓

B.M. 2.94 230.16 1.76 227.22 227.22

+50

2.0 28.2

47+00

0.1 ✓ 30.1

T.P. 11.86 241.65 0.37 229.79

48+00

8.1 33.6

+50

6.1 35.6

Spike in 8" Birch 60' H. Sta. 45+55

Station	+	H.I.	-	Pod.	Elev.
		241.65			
49+00				4.5	237.2
+50				3.2	38.5
50+00				2.7	39.0
+40				1.6	40.1
51+00				1.8	39.9
+50				2.0	39.7
52+00				1.9	39.8
T.P.	9.66	249.37	1.94	239.71	
53+00				8.8	40.6
54+00				6.2	43.2
+50				5.2	44.2
55+00				3.9	45.5
56+00				1.6	47.8
+40				0.8	48.6
T.P.	10.28	257.88	1.77	247.60	
+70				8.4	49.5
57+00				7.6	50.3
+50				7.0	50.9
58+00				6.4	51.5
B.M.				2.91	254.97
+40				5.7	52.2
59+00				5.1	52.8
+40				4.6	53.3
60+00				3.9	54.0
+50				3.1	54.8
61+00				2.5	55.4

spike in Stamp. 40. Rt. Sta 58+00

Station	+	H.I.	—	Rod.	Elev.
		257.88			
62+00				0.7	257.2
T.P.	10.98	267.85	1.01	256.87	
+50				9.5	58.4.
63+00				8.2	59.7.
+60				6.2	61.7.
64+00				4.8	63.1.
65+00				2.6	65.3.
+50				1.8	66.1.
66+00				1.8	66.1.
67+00				2.8	65.1.
T.P.			2.21	265.64	

267.85

12.15

255.70

2.12

257.82

10.22

247.60

0.56

248.16

8.67

239.49

1.80

241.09

11.32

229.77

1.06

230.83

12.73

218.10

4.88

222.98

4.97

218.01

0.92

218.93

11.21

207.72

0.94

208.66

7.98

200.68

10.37

190.31

8.78

181.53

8.78

172.75

0.42

173.17

208.66

10.37

198.29

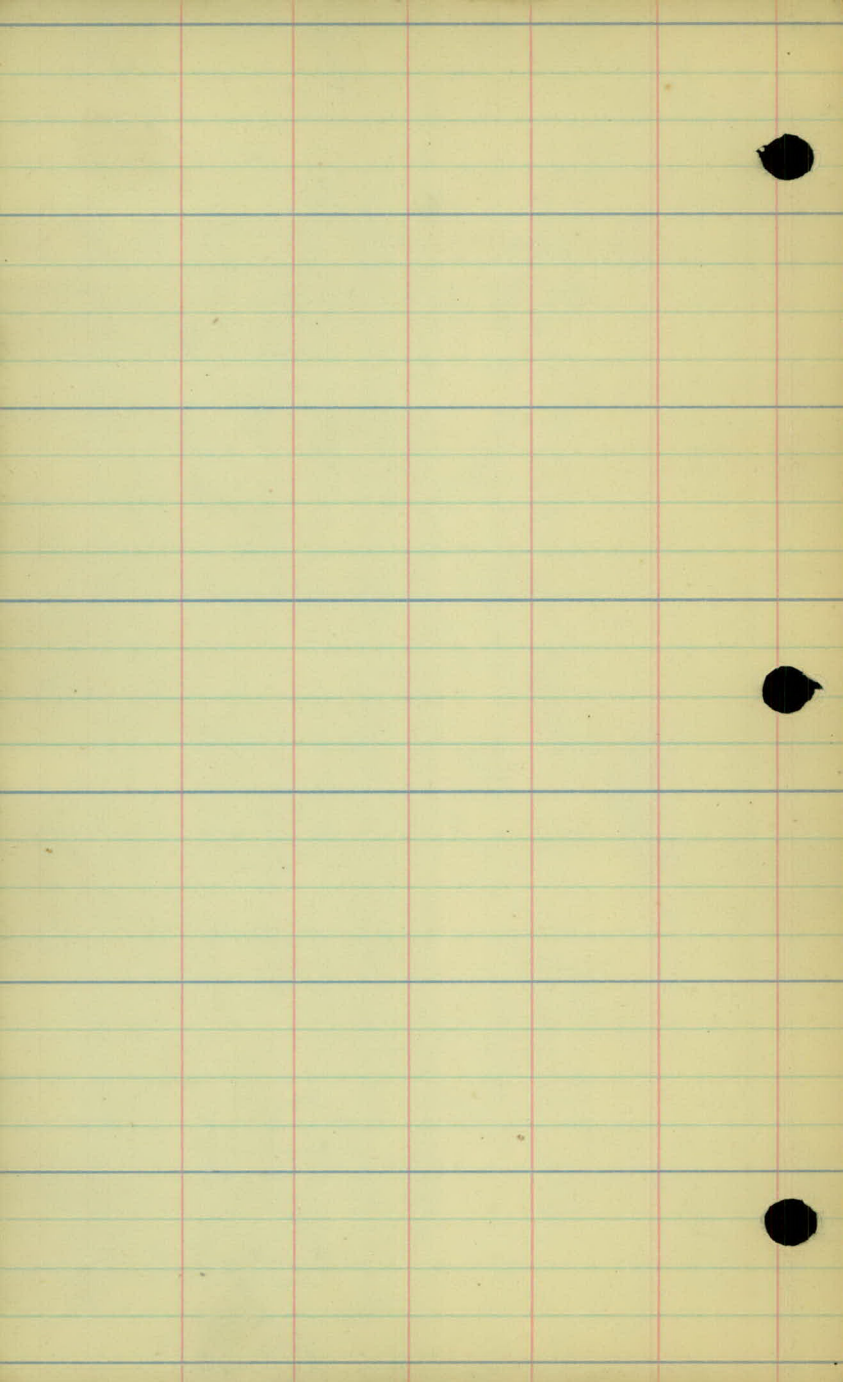
8.78

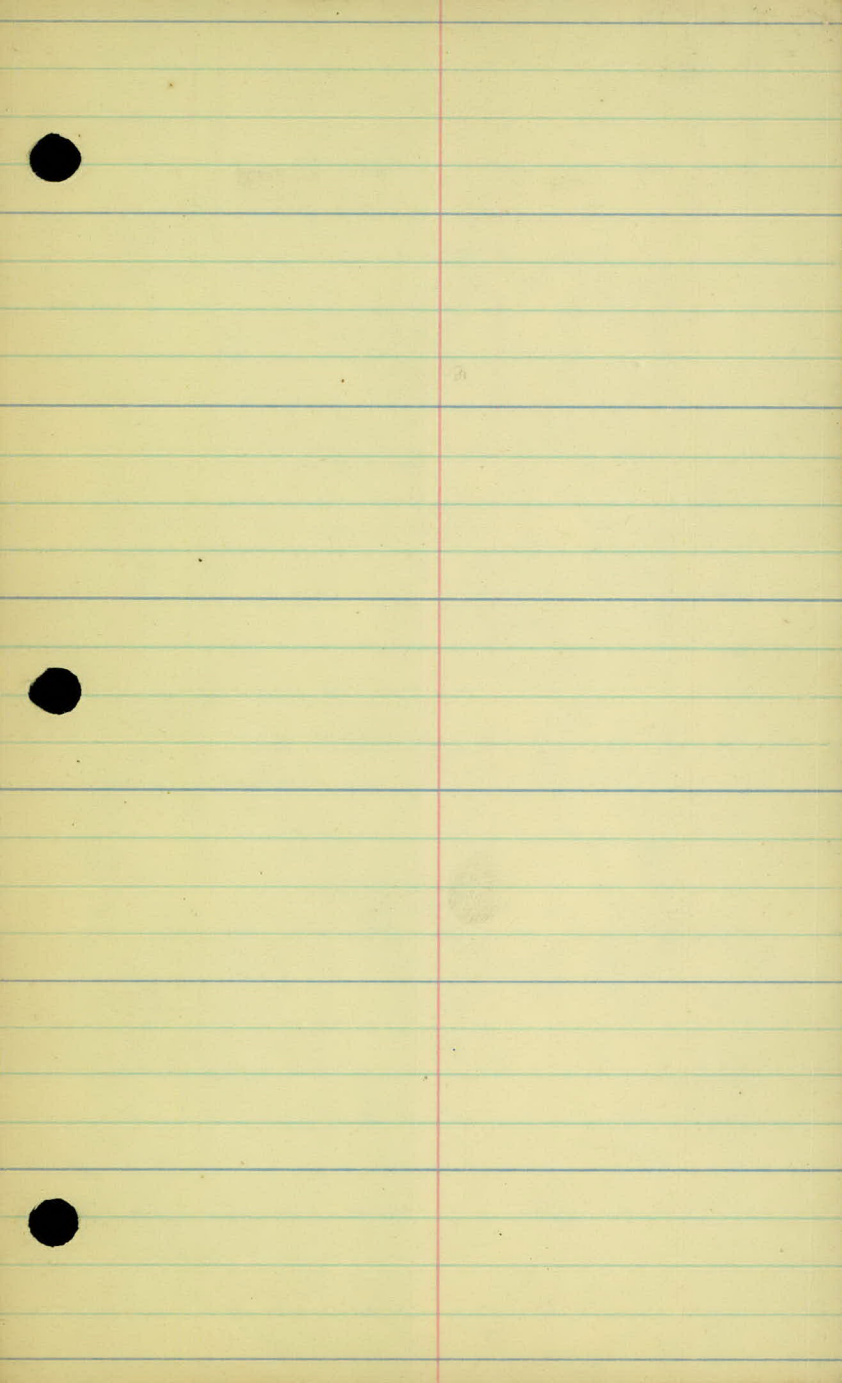
207.07

0.42

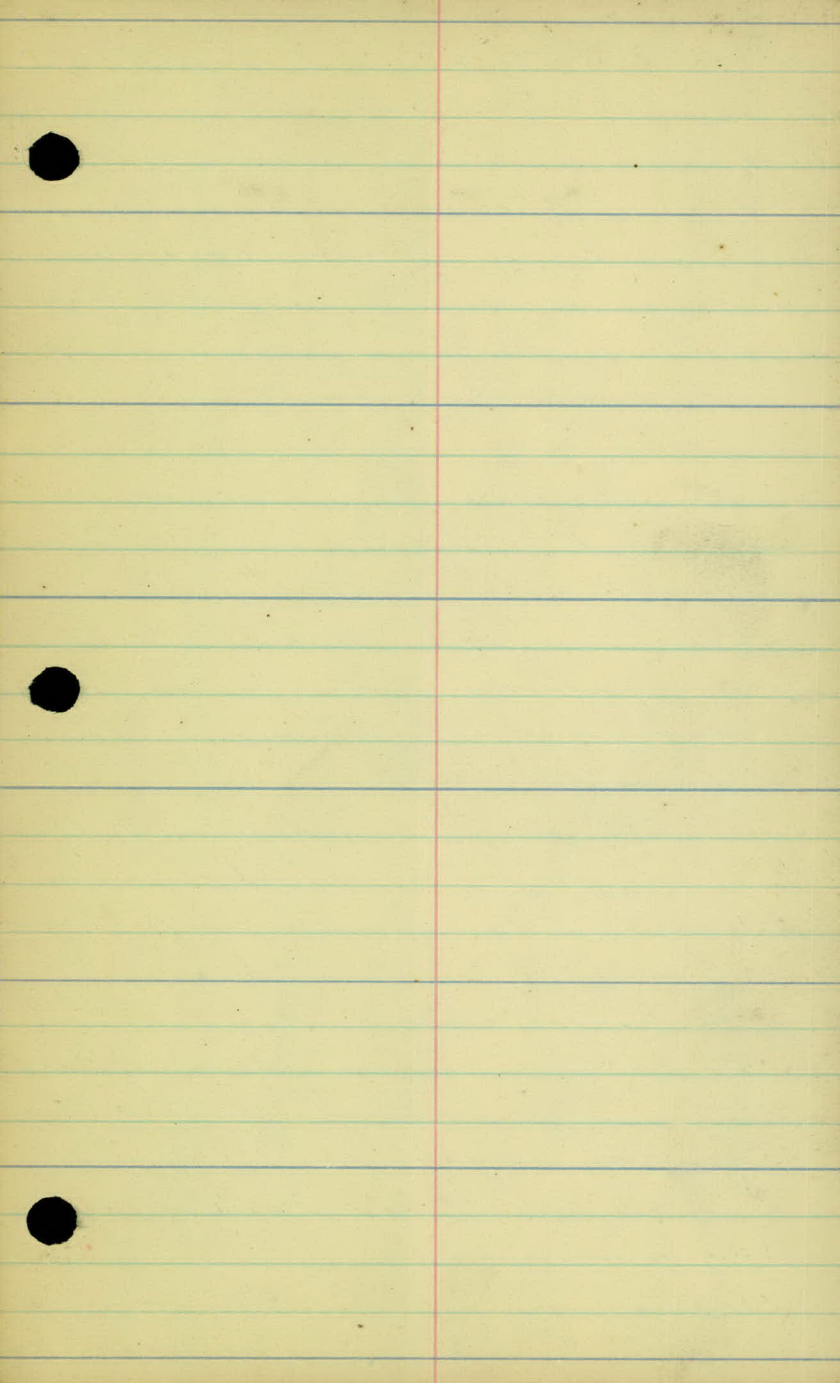
206.65

Nail in F.P. 20' left. Sto. 67-100





	+	H.I.	-	Flev	
T.P.	2.15	267.79		265.64	
68+00				3.90	263.9.
+50				5.0	62.8.
69+00				5.5	62.3.
+80				5.6	62.2.
70+00				5.8	62.0.
+35				6.2	61.6.
71+00				7.2	60.6.
T.P.	3.54	264.01	7.32	260.47	
+50				4.2	59.8.
72+00				4.6	59.4.



Station	+	H.F.	-	Rod.	Elev.
		264.01			

72 + 30				4.6	259.4
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+ 75				4.6	59.4
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73 + 00				4.8	59.2
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+ 50				5.2	58.8
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74 + 00				5.6	58.4
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+ 25				5.6	58.4
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75 + 00				5.8	58.2
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+ 50				5.8	58.2
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76 + 00				6.4	57.6
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T.P.	7.48	264.80	6.49	257.32	
------	------	--------	------	--------	--

+ 50				7.1	57.7
------	--	--	--	-----	------

77 + 00				6.7	57.1
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+ 30				6.2	58.6
------	--	--	--	-----	------

+ 42				6.0	58.8
------	--	--	--	-----	------

+ 45				6.0	58.8
------	--	--	--	-----	------

+ 73				5.9	58.9
------	--	--	--	-----	------

78 + 05				6.1	58.7
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+ 20				6.2	58.6
------	--	--	--	-----	------

+ 29.9	Top. Root			6.15	58.65
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+ 34.9	vv vv			6.14	58.66
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+ 45.5	vv vv			6.16	58.64
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+ 50.6	vv vv			6.18	58.62
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B.M.	1.13	263.80	2.13	262.67	262.67
------	------	--------	------	--------	--------

+ 56.0				5.0	58.8
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+ 73.6				4.9	58.9
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Sp. in T.P. 33' ht. Sta. 78+87.0

Station	+	H.I	-	Rod	Elev.
		263.80			

79	+ 11.3			4.2	259.6
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	+ 50.			4.3	59.5
--	-------	--	--	-----	------

80	+ 00			4.7	59.1
----	------	--	--	-----	------

	+ 50			4.8	59.0
--	------	--	--	-----	------

81	+ 00			5.3	58.5
----	------	--	--	-----	------

	+ 50			6.0	57.8
--	------	--	--	-----	------

82	+ 00			6.6	57.2
----	------	--	--	-----	------

	+ 20			6.8	57.0
--	------	--	--	-----	------

83	+ 00			8.2	55.6
----	------	--	--	-----	------

T.P.	4.75	260.23	8.32	255.48	
------	------	--------	------	--------	--

84	+ 00			5.0	55.2
----	------	--	--	-----	------

	+ 50			5.1	55.1
--	------	--	--	-----	------

85	+ 00			4.9	55.3
----	------	--	--	-----	------

	+ 30			4.8	55.4
--	------	--	--	-----	------

86	+ 00			4.7	55.5
----	------	--	--	-----	------

	+ 50			4.7	55.5
--	------	--	--	-----	------

87	+ 00			4.5	55.7
----	------	--	--	-----	------

	+ 60			4.0	56.2
--	------	--	--	-----	------

88	+ 00			3.5	56.7
----	------	--	--	-----	------

	+ 50			2.5	57.7
--	------	--	--	-----	------

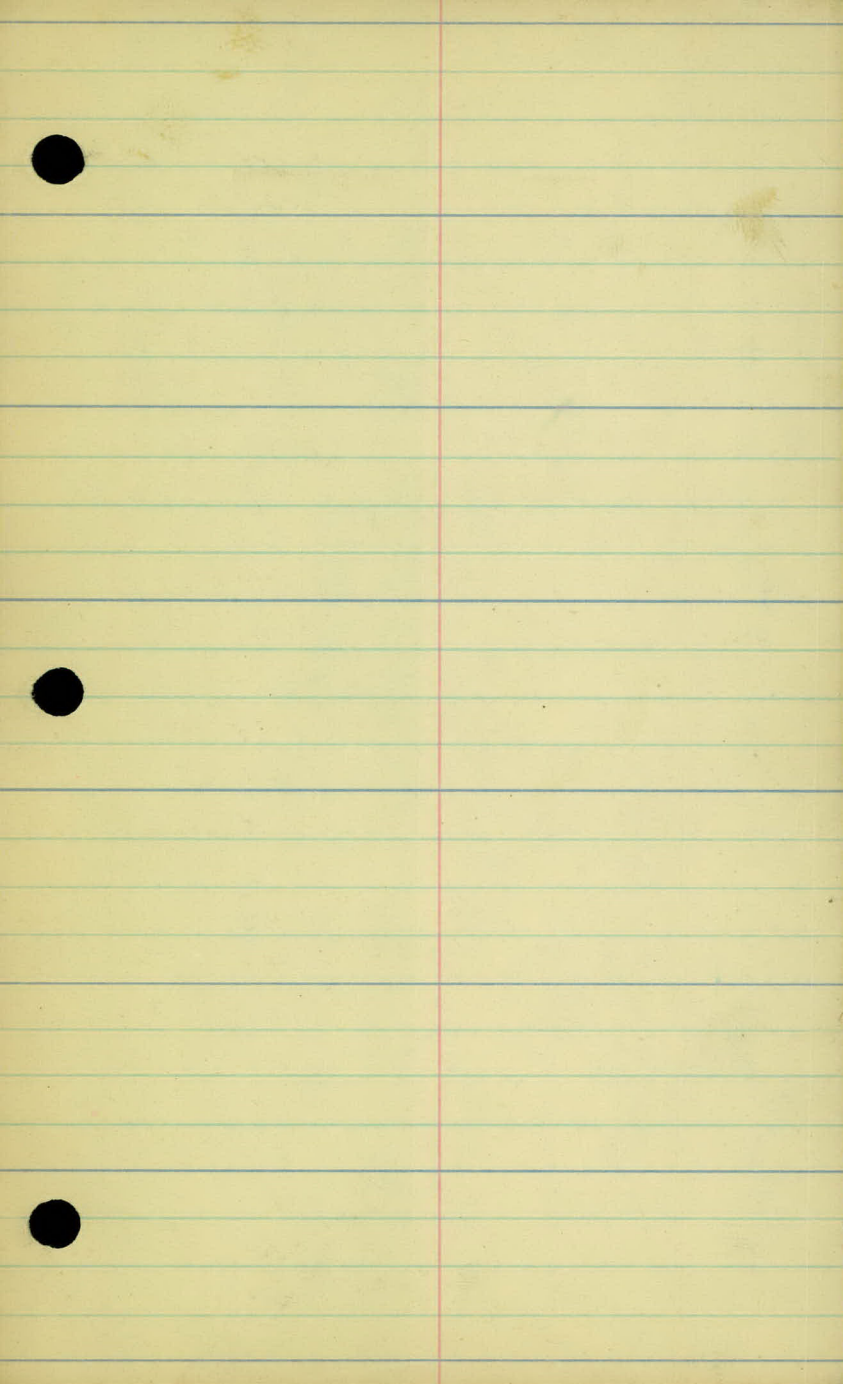
89	+ 00			1.3	58.9
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T.P.	9.82	268.02	2.03	258.20	
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	+ 50			8.0	60.0
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90	+ 00			7.1	60.9
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	+ 30			6.7	61.3
--	------	--	--	-----	------



Station	+	H.I.	-	Red.	Elev.
		268.02			
90 + 55				6.0	262.0
91 + 00				5.1	62.9.
+ 60				4.2	63.8.
92 + 00				3.3	64.7.
93 + 00				1.8	66.2.
+ 25				1.7	66.3.
94 + 00				1.3	66.7.
+ 60				1.5	66.5.
T.P.	0.95	267.54	1.43	266.59	
95 + 00				1.7	64.8.
+ 50				3.0	64.5.
96 + 00				4.3	63.2.
+ 50				5.5	62.0.
B.M.				6.80	260.74
97 + 00				6.5	61.0.
+ 50				7.5	60.0.
98 + 00				8.2	59.3.
+ 50				8.8	58.7.
99 + 00				9.1	58.4.
T.P.	2.03	260.27	9.30	258.24	
+ 40				1.8	58.5.
100 + 00				2.3	58.0.
101 + 00				3.8	56.5.
102 + 00				5.1	55.2.
103 + 00				6.3	54.0.

Sp in 6" OOK 50' left Sta 96+12

Station + H.I. - Rod Elev.

260.27

103 +50 6.9 253.4

104 +00 7.3 53.0

+50 7.6 52.7

105 +00 8.6 51.7

T.P. 4.07 255.15 9.19 251.08

+50 4.60 50.6

106 +00 5.5 49.7

107 +00 6.8 48.4

+50 6.3 48.9

108 +00 5.2 50.0

B.M. 5.30 249.85

+35 4.4 50.8

109 +00 3.1 52.1

+50 2.0 53.2

110 +00 1.1 54.1

+60 0.3 54.9

T.P. 4.57 258.68 1.04 254.11

111 +00 3.5 55.2

+50 3.4 55.3

112 +00 3.5 55.2

+50 3.4 55.3

113 +00 3.9 54.8

+50 4.3 54.4

114 +00 5.2 53.5

+50 6.0 52.7

B.M. 4.95 253.73 253.73

Sp in 16" Oak. 40' heft. Sta. 108 + 35

306.15	Lexington
253.73	Co. Road "E"
52.42	Equation

✓ Some Used for Lexington Ave Data. }
Sp in 18" Oak. N.E. Cor. Lexington + Co. Rd. "E" }

α. heads

B.M. 253.73

+ 4.95

258.68

- 3.50

255.18
1.40

256.58

5.50

251.08

9.23

260.31

20.08

258.23

9.65

267.88

20.02

265.86

3.08

268.94

12.76

256.18

3.97

260.15

4.95

255.20

8.82

264.02

6.00

258.02

4.97

262.99

2.60

260.39

6.26

266.65

1.04

265.61

56.58

6.71

49.87

67.86

7.15

60.73

64.02

62.67

1.35

65.64

Road #6

Co. Rd. "F" Rice to Lexington.

X-Section Notes.

Sta. 0+00 to.

Austin
Skoglund
Maloney
Galvin

} Party.

Station

Elev.

0 + 00

34.3

+ 24

34.4

+ 36

34.1

1 + 00

34.0

2 + 00

33.8

+ 50

33.8

3 + 00

33.4

4 + 00

32.5

5 + 00

31.8

6 + 00

31.9

7 + 00

31.5

8 + 00

30.9

9 + 00

30.9

+ 50

30.0

10 + 00

27.9

11 + 00

22.8

+ 50

19.7

12 + 00

16.1

+ 41 End. wing walls

13.5

+ 65 $\pm$ Viaduct

12.1

+ 90 End. wing walls

12.4

13 + 00

15.4

14 + 00

18.2

15 + 00

20.7

+ 50

22.0

16 + 00

23.2

H.

±

Rt.

				0.0	
				33.0	
			-1.2	-0.9	-0.5
			33.0	24.0	16.0
-0.4	-1.0	0.0	-0.7	-0.4	
33.0	25.0	16.0	12.0	8.0	
-0.6	-0.6	-0.8	-1.1	-0.7	-0.4
33.0	24.0	16.0	14.0	12.0	8.0
	-0.8	-1.0	-0.8	-0.6	
	33.0	22.0	14.0	9.6	
-1.1	-0.7	-0.3	-1.1	-0.5	
33.0	25.0	17.0	14.0	8.0	
-0.7	-0.8	-0.1	-1.3	-0.5	
33.0	24.0	16.0	13.0	9.0	
-1.0	-0.8	-0.4	-0.6	-0.1	
33.0	26.0	14.0	10.0	5.0	
-0.5	-0.6	-0.5	-0.2	-0.0	
33.0	24.0	16.0	11.0	7.0	
-0.2	-0.5	-1.3	-1.5	-0.5	-0.2
33.0	21.0	17.0	16.0	12.0	8.0
-0.3	-0.4	-0.4	-1.4	-1.1	-0.4
33.0	27.0	18.0	16.0	13.0	7.0
-0.6	-0.8	-0.8	-1.1	-0.5	-0.3
33.0	23.0	18.0	15.0	12.0	8.0
	0.0	-0.2	-0.5	-0.3	0.0
	33.0	26.0	17.0	14.0	7.0
+2.8	+2.8	+2.0	-1.1	-0.4	-0.1
33.0	25.0	18.0	15.0	13.0	7.0
+4.6	+4.1	-1.1	-0.8	-0.3	
33.0	20.0	14.0	12.0	7.0	
	+4.0	+4.1	-1.4	-0.7	-0.4
	33.0	21.0	14.0	12.0	7.0
+3.0	+2.9	-1.5	-0.6	-0.3	
33.0	24.0	17.0	17.0	11.0	
+3.0	+2.9	+1.9	-1.1	-1.2	-0.2
33.0	22.0	21.0	18.0	16.0	13.0
	+5.3	+5.0	Wing	+3.0	-0.2
	33.0	23.0	17.0	13.0	11.0
			-0.5	-0.2	
			7.0	7.0	
+3.4	Wing				
33.0	24.0	16.0	-0.5	-0.2	
	+3.5	+1.7	+2.0	0.0	+0.1
	33.0	27.0	21.0	19.0	11.0
	+4.2	+4.5	+1.4	-0.3	-0.2
	33.0	17.0	15.0	12.0	7.0
+4.6	+4.5	+4.9	+0.2	-0.5	-0.2
33.0	28.0	22.0	15.0	11.0	8.0
	+4.0	+3.7	+1.7	-0.8	-0.5
	33.0	21.0	19.0	13.0	8.0
+2.2	+2.8	-1.3	-0.3	-0.1	
33.0	22.0	15.0	13.0	7.0	

				+0.2	
				33.0	
			-0.2	-0.3	-1.5
			11.0	16.0	17.0
			33.0		
-0.2	-1.1	-0.4	-0.2		
11.0	15.0	17.0	33.0		
-0.5	-0.7	-1.1	-0.7	-0.6	
7.0	14.0	12.0	16.0	33.0	
-0.3	-0.9	-1.0	-0.5	-0.4	
7.0	12.0	22.0	25.0	33.0	
-0.3	-0.6	-1.3	-1.0	+0.2	0.0
7.0	12.0	15.0	17.0	22.0	33.0
-0.4	-0.5	-1.2	-1.2	0.0	0.0
8.0	12.0	15.0	18.0	21.0	33.0
-0.3	-0.7	-1.1	-1.2	-1.2	
7.0	12.0	14.0	22.0	33.0	
-0.5	-0.9	-1.6	-1.0	-1.0	-1.1
7.0	11.0	12.0	15.0	22.0	33.0
-0.4	-0.7	-1.5	-0.8	-0.8	-0.8
7.0	11.0	14.0	16.0	24.0	33.0
-0.4	-0.5	-1.1	-0.5	-0.4	-0.5
7.0	11.0	14.0	17.0	24.0	33.0
-0.3	-0.8	-0.7	-0.3	-0.1	
7.0	12.0	15.0	23.0	33.0	
-0.3	-1.0	-1.4	-0.2	0.0	0.0
8.0	12.0	15.0	18.0	28.0	33.0
-0.3	-0.6	-1.0	+1.7	+1.5	
8.0	11.0	13.0	18.0	33.0	
-0.4	-1.0	+4.6	+4.5	+3.0	
8.0	14.0	20.0	25.0	33.0	
-0.2	-0.5	-0.8	+2.0	+5.0	+8.5
7.0	11.0	18.0	17.0	21.0	23.0
-0.3	-0.4	-1.0	+2.5	+4.0	+5.0
7.0	12.0	19.0	20.0	25.0	27.0
-0.2	-0.7	-1.0	+1.9	+4.0	+3.5
9.0	15.0	18.0	24.0	27.0	33.0
-0.3	-0.8	+1.2	Edgewing	+2.0	+4.2
10.0	12.0	17.0	20.0	25.0	33.0
-0.2	-0.4	-0.9			
7.0	9.0	10.0			
-0.5	-0.6	+4.2	Wing	+5.0	+6.9
7.0	11.0	16.0	17.0	24.0	33.0
-0.7	-1.2	-1.1	+4.4	+1.5	+0.8
10.0	12.0	16.0	17.0	26.0	33.0
-0.5	-1.2	+1.8	+4.0	+4.0	
7.0	17.0	18.0	27.0	33.0	
-0.5	-0.5	-0.7	+1.9	+2.6	+3.5
7.0	10.0	12.0	15.0	26.0	27.0
-0.2	-0.5	-0.4	+0.7	+2.4	+0.5
5.0	12.0	18.0	22.0	27.0	33.0
-0.4	-0.6	-0.9	+2.0	+0.9	
7.0	11.0	14.0	28.0	33.0	

Station	Elev.
16 + 42.	224.1
17 + 00	225.4
18 + 00	26.7
19 + 00	27.4
20 + 00	25.8
21 + 00	22.0
22 + 00	17.6
23 + 00	12.8
24 + 00	208.3
+ 75	205.3
25 + 00	204.2
26 + 00	200.2
27 + 00	98.2
27 + 50	97.9
$\left. \begin{array}{l} 27 + 50 \\ 28 + 00 \end{array} \right\} = 64' (27 + 38 = 27 + 24)$	
28 + 00	98.4
+ 65	98.9
29 + 00	99.2
+ 75	201.7
30 + 00	202.8
+ 33 End Wing Wall	204.3
+ 40 " " "	204.7
+ 71.6 $\frac{1}{2}$ Viaduct	205.9
31 + 03. End Wing	207.2
+ 15 " "	207.6
+ 69	208.7

15

2

14

$\frac{+1.3}{33.0}$	$\frac{+2.0}{20.0}$	$\frac{-1.2}{15.0}$	$\frac{-0.7}{12.0}$	$\frac{-0.6}{10.0}$	$\frac{0.5}{8.0}$	$\frac{-0.5}{14.0}$	$\frac{+1.3}{24.0}$	$\frac{+4.0}{31.0}$	$\frac{+4.0}{32.0}$
$\frac{+1.7}{33.0}$	$\frac{+2.0}{19.0}$	$\frac{-0.1}{15.0}$	$\frac{-0.8}{12.0}$	$\frac{-0.3}{6.0}$	$\frac{-0.6}{12.0}$	$\frac{-0.9}{14.0}$	$\frac{+2.1}{20.0}$	$\frac{+2.0}{33.0}$	
$\frac{2.7}{33.0}$	$\frac{+2.0}{28.0}$	$\frac{+1.2}{17.0}$	$\frac{-0.8}{13.0}$	$\frac{-0.2}{10.0}$	$\frac{-0.2}{7.0}$	$\frac{-0.8}{12.0}$	$\frac{-1.0}{16.0}$	$\frac{+3.0}{23.0}$	$\frac{+3.0}{33.0}$
$\frac{+2.0}{33.0}$	$\frac{+1.5}{20.0}$	$\frac{-1.1}{14.0}$	$\frac{-0.7}{12.0}$	$\frac{-0.1}{6.0}$	$\frac{-0.5}{7.0}$	$\frac{-0.8}{12.0}$	$\frac{-0.9}{16.0}$	$\frac{+1.7}{19.0}$	$\frac{+2.2}{33.0}$
$\frac{+0.5}{33.0}$	$\frac{+1.3}{24.0}$	$\frac{+1.3}{17.0}$	$\frac{-1.1}{13.0}$	$\frac{-0.4}{6.0}$	$\frac{-0.2}{7.0}$	$\frac{-0.3}{12.0}$	$\frac{-0.6}{13.0}$	$\frac{+2.0}{17.0}$	$\frac{+3.2}{33.0}$
$\frac{+2.8}{33.0}$	$\frac{+2.8}{24.0}$	$\frac{-0.8}{18.0}$	$\frac{-0.5}{12.0}$	$\frac{+0.3}{5.0}$	$\frac{-0.3}{5.0}$	$\frac{-0.2}{8.0}$	$\frac{-0.6}{10.0}$	$\frac{+2.0}{16.0}$	$\frac{+4.0}{19.0}$
$\frac{+4.0}{33.0}$	$\frac{+4.5}{24.0}$	$\frac{+3.2}{23.0}$	$\frac{0.0}{19.0}$	$\frac{-0.7}{14.0}$	$\frac{+0.2}{5.0}$	$\frac{-0.4}{7.0}$	$\frac{-0.6}{9.0}$	$\frac{0.0}{12.0}$	$\frac{+5.6}{20.0}$
$\frac{+1.5}{33.0}$	$\frac{+2.5}{28.0}$	$\frac{+2.3}{19.0}$	$\frac{-0.2}{13.0}$	$\frac{-0.6}{9.0}$	$\frac{+0.2}{5.0}$	$\frac{-0.3}{12.0}$	$\frac{-0.6}{15.0}$	$\frac{+1.4}{21.0}$	$\frac{+4.7}{26.0}$
$\frac{+1.7}{33.0}$	$\frac{+1.7}{21.0}$	$\frac{-1.3}{21.0}$	$\frac{-0.3}{11.0}$	$\frac{-0.4}{5.0}$	$\frac{-0.5}{5.0}$	$\frac{0.0}{14.0}$	$\frac{+0.1}{19.0}$	$\frac{+0.1}{23.0}$	$\frac{+2.2}{26.0}$
$\frac{-3.7}{33.0}$	$\frac{-3.7}{25.0}$	$\frac{-2.5}{16.0}$	$\frac{-0.7}{11.0}$	$\frac{-0.5}{6.0}$	$\frac{-0.1}{6.0}$	$\frac{-0.6}{13.0}$	$\frac{-0.9}{20.0}$	$\frac{-0.7}{29.0}$	$\frac{-0.7}{33.0}$
$\frac{-5.5}{33.0}$	$\frac{-4.7}{24.0}$	$\frac{-3.4}{17.0}$	$\frac{-0.9}{12.0}$	$\frac{-0.3}{6.0}$	$\frac{-0.2}{6.0}$	$\frac{-0.5}{12.0}$	$\frac{-2.0}{15.0}$	$\frac{-2.1}{23.0}$	$\frac{-2.2}{33.0}$
$\frac{-7.8}{33.0}$	$\frac{-6.0}{21.0}$	$\frac{-2.3}{14.0}$	$\frac{-0.7}{11.0}$	$\frac{-0.4}{6.0}$	$\frac{-0.3}{7.0}$	$\frac{-0.6}{11.0}$	$\frac{-4.5}{18.0}$	$\frac{-5.0}{20.0}$	$\frac{-6.0}{33.0}$
$\frac{-6.5}{33.0}$	$\frac{-5.5}{22.0}$	$\frac{-3.5}{16.0}$	$\frac{-1.0}{11.0}$	$\frac{-0.5}{6.0}$	$\frac{-0.3}{6.0}$	$\frac{-0.5}{11.0}$	$\frac{-4.8}{17.0}$	$\frac{-5.0}{33.0}$	
$\frac{-6.0}{33.0}$	$\frac{-6.0}{28.0}$	$\frac{-4.7}{18.0}$	$\frac{-3.2}{14.0}$	$\frac{-0.9}{11.0}$	$\frac{-0.2}{7.0}$	$\frac{-0.5}{11.0}$	$\frac{-2.4}{15.0}$	$\frac{-3.2}{23.0}$	$\frac{-2.8}{33.0}$
$\frac{-7.0}{33.0}$	$\frac{-5.6}{21.0}$	$\frac{-2.7}{15.0}$	$\frac{-1.0}{11.0}$		$\frac{-0.1}{5.0}$	$\frac{-0.4}{12.0}$	$\frac{-2.6}{16.0}$	$\frac{-3.5}{22.0}$	$\frac{-3.5}{33.0}$
$\frac{-6.7}{33.0}$	$\frac{-7.0}{24.0}$	$\frac{-5.7}{18.0}$	$\frac{-0.9}{11.0}$	$\frac{-0.4}{7.0}$	$\frac{-0.2}{7.0}$	$\frac{-0.9}{12.0}$	$\frac{-5.5}{19.0}$	$\frac{-6.5}{33.0}$	
$\frac{-5.0}{33.0}$	$\frac{-5.0}{22.0}$	$\frac{-2.8}{18.0}$	$\frac{-0.9}{13.0}$	$\frac{-0.2}{7.0}$	$\frac{-0.1}{7.0}$	$\frac{-0.6}{17.0}$	$\frac{-3.1}{21.0}$	$\frac{-5.0}{25.0}$	$\frac{-7.5}{33.0}$
$\frac{+2.5}{33.0}$	$\frac{-1.5}{30.0}$	$\frac{+1.5}{28.0}$	$\frac{+0.8}{25.0}$	$\frac{+0.5}{19.0}$	$\frac{-0.3}{5.0}$	$\frac{-0.7}{11.0}$	$\frac{-1.0}{18.0}$	$\frac{-4.0}{23.0}$	$\frac{-4.8}{33.0}$
$\frac{-0.8}{33.0}$	$\frac{-2.0}{30.0}$	$\frac{-0.1}{25.0}$	$\frac{-0.1}{18.0}$	$\frac{+0.1}{5.0}$	$\frac{-0.4}{7.0}$	$\frac{-0.7}{17.0}$	$\frac{-1.9}{18.0}$	$\frac{-1.5}{20.0}$	$\frac{+0.2}{22.0}$
$\frac{+6.5}{33.0}$	$\frac{+7.0}{27.0}$	$\frac{+4.6}{21.0}$	$\frac{-0.9}{15.0}$	$\frac{-0.9}{13.0}$	$\frac{-0.2}{8.0}$	$\frac{-0.5}{14.0}$	$\frac{+3.8}{20.0}$	$\frac{+5.0}{22.0}$	$\frac{+9.2}{33.0}$
$\frac{+9.0}{33.0}$	$\frac{+6.5}{27.0}$	$\frac{+5.0}{22.0}$	$\frac{+1.5}{18.0}$	$\frac{-1.0}{14.0}$	$\frac{-0.2}{8.0}$	$\frac{-0.5}{13.0}$	$\frac{+0.7}{16.0}$	wing	
Wall					$\frac{-0.1}{6.0}$	$\frac{-0.4}{10.0}$	Wall		
Wing					$\frac{-0.1}{6.0}$	$\frac{-0.3}{10.0}$	$\frac{-0.8}{13.0}$	$\frac{+0.7}{18.0}$	$\frac{+1.9}{22.0}$
$\frac{+7.0}{33.0}$	$\frac{+5.0}{28.0}$	$\frac{+2.5}{24.0}$	$\frac{+1.8}{20.0}$	$\frac{-0.9}{15.0}$	$\frac{0.0}{7.0}$	$\frac{0.0}{14.0}$	$\frac{-0.5}{22.0}$	$\frac{+1.0}{33.0}$	
$\frac{-0.7}{33.0}$	$\frac{-0.7}{28.0}$	$\frac{0.0}{19.0}$	$\frac{-0.2}{11.0}$		$\frac{-0.1}{6.0}$	$\frac{-0.2}{12.0}$	$\frac{-0.3}{23.0}$	$\frac{0.0}{33.0}$	

Station

Elev.

32 + 00

209.4

+ 75

210.8

33 + 00

211.4

+ 45

212.7

34 + 00

213.6

+ 50

213.8

35 + 00

214.2

+ 50

214.9

36 + 00

215.6

37 + 00

217.1

+ 65

218.7

38 + 00

219.6

+ 30

219.9

+ 70

220.3

39 + 00

220.6

40 + 00

219.5

+ 50

218.4

41 + 00

216.6

+ 50

215.8

42 + 00

214.9

+ 50

214.8

43 + 00

215.3

44 + 00

217.6

45 + 00

221.3

+ 50

223.8

46 + 00

226.1

64.

F

R4.

-0.3 10.2 0.0
33.0 26.0 18.0

+1.2 41.0 -0.5 -0.3 -0.1 0.0
33.0 27.0 26.0 22.0 15.0 7.0

+3.5 43.0 -0.7 -0.7 0.0 -0.3
33.0 24.0 21.0 19.0 15.0 8.0

+6.2 45.7 -0.3 -1.0 -0.4 -0.3
33.0 25.0 21.0 18.0 17.0 7.0

+4.6 43.7 -0.4 -0.7 -0.3 -0.3
33.0 25.0 23.0 20.0 18.0 7.0

+3.5 42.8 -0.9 -0.9 -0.2 -0.8
33.0 23.0 21.0 18.0 16.0 10.0

-0.2 -0.5 -2.0 -2.0 -0.3 -0.3
33.0 22.0 20.0 17.0 14.0 8.0

-8.5 -7.0 -2.0 -0.3
33.0 21.0 14.0 11.0

-6.7 33.0 -5.5 -2.5 -0.2
25.0 20.0 15.0 11.0

-1.2 -8.7 -0.9 -0.2
33.0 18.0 16.0 7.0

+5.0 44.2 -1.0 -1.2 -0.5 0.0
33.0 24.0 19.0 16.0 15.0 8.0

+0.5 -0.3 -1.0 -1.0 -0.4 -0.3
33.0 22.0 19.0 17.0 15.0 8.0

-1.0 0.0 10.1 -0.9 -0.9 -0.2 -0.3
33.0 29.0 18.0 17.0 15.0 14.0 8.0

+0.8 0.0 0.0 -0.5 -0.5 -0.3 -0.3
33.0 29.0 22.0 15.0 17.0 14.0 13.0 7.0

-1.8 43.0 43.5 10.1 -0.8 -0.2 0.0
33.0 27.0 19.0 17.0 15.0 12.0 7.0

-4.5 41.5 41.7 -1.2 -1.4 -0.5 -0.5
33.0 24.0 20.0 18.0 15.0 13.0 7.0

-7.0 41.5 41.0 41.5 -1.7 -0.7 -0.4
33.0 29.0 25.0 20.0 18.0 14.0 8.0

-7.2 -4.0 -2.5 -0.4 -0.3
33.0 27.0 17.0 13.0 8.0

-6.0 -3.0 -3.4 -2.5 -0.7 -0.4
33.0 29.0 21.0 16.0 12.0 8.0

-0.5 41.8 41.8 -0.8 -1.0 -0.5 -0.5
33.0 30.0 19.0 17.0 15.0 13.0 7.0

-2.5 -1.0 -0.8 -1.4 -1.4 -0.6 -0.4
33.0 31.0 18.0 17.0 14.0 11.0 8.0

-8.0 -7.0 -4.9 -0.6 -0.3
33.0 24.0 17.0 10.0 6.0

-8.7 -7.6 -5.0 -2.3 -0.7 -0.4
33.0 25.0 21.0 17.0 13.0 9.0

-7.7 -7.0 -5.0 -1.1 -0.3
33.0 23.0 18.0 13.0 10.0

-2.0 -2.5 -1.3 -0.2 -0.2
33.0 24.0 18.0 15.0 10.0

+8.8 46.4 45.8 -1.3 -1.1 -0.4 -0.3
39.0 37.0 35.0 25.0 23.0 21.0 7.0

-0.3 0.0 -0.1 -0.5
7.0 17.0 26.0 33.0

-0.3 -0.3 -0.5 -2.1
8.0 12.0 16.0 33.0

-0.2 -0.7 -1.4 -0.8 -1.3
7.0 16.0 20.0 23.0 33.0

-0.2 -0.5 -0.9 -0.1 0.0
8.0 14.0 16.0 24.0 33.0

-0.3 -0.8 -1.6 -1.6
7.0 14.0 17.0 33.0

-0.2 -0.5 -1.3 -0.5 -0.5
7.0 14.0 16.0 21.0 33.0

-0.3 -0.6 -1.5 -2.0 -2.0
8.0 13.0 16.0 25.0 33.0

-0.1 -0.4 -4.1 -5.5 -6.0
7.0 12.0 17.0 23.0 33.0

+0.1 -0.3 -6.9 -8.2 -9.3
3.0 12.0 19.0 26.0 33.0

-0.6 -2.0 -3.8 -5.0 -5.6
10.0 13.0 16.0 25.0 33.0

-0.2 -0.9 -2.1 -2.1 -1.1 -0.5 -0.6
8.0 13.0 16.0 20.0 21.0 27.0 33.0

-0.5 -1.9 -1.5 -1.7 -0.7 10.2 42.5
6.0 15.0 16.0 19.0 20.0 24.0 33.0

-0.5 -0.5 -1.4 -0.5 43.0
8.0 12.0 16.0 24.0 33.0

-0.4 -0.7 -1.4 -1.4 -0.5 41.0 42.2
7.0 12.0 15.0 18.0 19.0 24.0 33.0

-0.4 -0.7 -1.4 -1.4 41.6 42.2 41.5
7.0 13.0 14.0 17.0 21.0 26.0 33.0

-0.2 -0.4 -1.0 -0.9 42.0 42.5 42.0
8.0 13.0 15.0 17.0 22.0 26.0 33.0

-0.4 -0.4 -1.2 42.0 42.9 42.5
7.0 12.0 15.0 19.0 25.0 33.0

-0.4 -0.5 -2.0 -2.7
8.0 12.0 17.0 33.0

-0.3 -0.9 -2.4 3.1 -2.9
8.0 13.0 17.0 27.0 33.0

-0.3 -0.9 -1.2 -1.2
8.0 14.0 20.0 33.0

-0.4 -0.6 -1.2 -1.2 -1.5
7.0 13.0 16.0 25.0 33.0

-0.2 -0.6 3.1 -4.9 -4.9
7.0 12.0 17.0 37.0 33.0

-0.4 -0.5 -5.0 9.8 -10.8
7.0 11.0 18.0 24.0 33.0

-0.2 -0.6 3.1 -5.0 -10.0 -10.2
7.0 12.0 13.0 17.0 27.0 33.0

-0.2 -0.5 -0.9 -0.6 -2.5
8.0 13.0 16.0 25.0 33.0

-0.2 -0.5 -1.2 49.2 47.0 47.0
7.0 13.0 16.0 20.0 21.0 33.0

Station

Elev.

46 + 50

228.2

47 + 00

30.1

48 + 00

33.6

49 + 00

37.2

50 + 80

38.8

50 + 56

40.0

51 + 00

39.9

+ 50

39.7

52 + 00

39.8

+ 50

40.2

53 + 00

40.6

54 + 00

43.2

+ 60

44.6

55 + 00

45.5

56 + 00

47.8

57 + 00

50.3

58 + 00

51.5

+ 50

52.3

59 + 00

52.8

+ 40

53.3

60 + 00

54.0

61 + 00

55.4

+ 30

55.9

62 + 00

57.2

+ 50

58.4

$$0+50 = 95.4$$

$$17+20 = \underline{93.3}$$

$$\begin{array}{r} .00.0647 \\ 17 \overline{) 1.1000} \\ \underline{102} \end{array}$$

$$\begin{array}{r} 80 \\ 68 \\ \hline 120 \\ 119 \\ \hline \end{array}$$

$$\begin{array}{r} .0647 \\ 5 \\ \hline .3225 \end{array}$$

$$0+50 = 95.4$$

$$24+56 = \underline{93.7}$$

$$1.7$$

$$\begin{array}{r} 2400 \\ .05 \\ \hline 12000 \end{array}$$

$$\begin{array}{r} 24 \\ .08 \\ \hline 1.92 \end{array}$$

$$\begin{array}{r} 92.7 \\ \hline 95.6 \end{array}$$

$$\begin{array}{r} 1.7 \\ \hline 93.9 \end{array}$$

$$\begin{array}{r} 24 \\ .06 \\ \hline 1.44 \end{array}$$

$$\begin{array}{r} 93.7 \\ \hline 95.14 \end{array}$$

10.5

10.1
9.7

24 X 42

100.28

3.36

96.92

5.30

102.22

4.80

97.42 -

95.0

1.7

93.3

6.2

2 + 50 = 4.5

44.

4

R1.

+12.0	+19.0	+5.0	+3.2	+1.7	-1.6	-1.6	-0.5	-0.4	-0.3	-0.5	-0.9	+0.7	+5.0	+10.0	+12.3
42.0	38.0	33.0	32.0	27.0	22.0	19.0	18.0	10.0	9.0	14.0	17.0	19.0	23.0	31.0	36.0
+7.6	+4.3	+5.0	+3.0	-0.7	-0.5	-0.2			-0.4	-0.5	-1.2	-1.2	+1.5	+5.0	+6.2
33.0	28.0	25.0	22.0	19.0	15.0	9.0			8.0	16.0	17.0	19.0	22.0	28.0	33.0
+17.0	+6.5	+5.0	+2.6	-1.0	-0.7	-0.1			-0.3	-1.2	-1.7	-1.6	-4.5	+1.0	
33.0	24.0	25.0	23.0	20.0	16.0	9.0			8.0	15.0	16.0	17.0	25.0	33.0	
+3.2	+3.2	-1.6	-1.4	-0.6	-0.4				-0.5	-0.9	-1.6	+1.0	+4.7	+4.7	
33.0	21.0	17.0	14.0	13.0	9.0				10.0	16.0	19.0	23.0	27.0	33.0	
+2.7	+1.6	-1.0	-1.0	-0.3	-0.3				-0.4	-0.8	-1.5	-1.5	+3.3	+3.0	
33.0	20.0	17.0	15.0	13.0	8.0				10.0	15.0	17.0	20.0	25.0	33.0	
+7.6	+5.0	+0.4	-0.3	-1.3	-0.5				-0.4	-1.1	-1.4	-0.8	+5.0	+4.5	
35.0	33.0	26.0	19.0	16.0	10.0				9.0	15.0	17.0	19.0	25.0	33.0	
+2.8	+2.1	+1.5	-1.0	-0.6	-0.3				-0.2	-0.9	-1.5	+1.4	+1.0		
33.0	24.0	18.0	16.0	13.0	9.0				8.0	12.0	15.0	21.0	33.0		
0.0	+0.2	+0.5	-1.1	-0.6	-0.3				-0.3	-0.6	-1.2	-0.7	-0.6		
33.0	23.0	16.0	15.0	12.0	8.0				6.0	11.0	14.0	17.0	33.0		
+0.4	+1.2	+0.8	-0.4	-1.2	-0.6	-0.3			-0.4	-0.6	-1.9	-1.9			
33.0	30.0	20.0	14.0	15.0	11.0	7.0			6.0	13.0	19.0	33.0			
+0.3	+0.3	+0.2	-1.0	-0.4	-0.4	-0.4			-0.2	-0.5	-2.0	-2.2			
33.0	28.0	19.0	14.0	10.0	8.0				8.0	14.0	18.0	33.0			
+0.6	+1.3	+0.5	-0.4	-0.4	-0.2				-0.3	-0.5	-1.7	-2.4	-2.4		
33.0	29.0	16.0	15.0	13.0	8.0				6.0	13.0	16.0	22.0	33.0		
+2.2	+2.2	+1.0	-0.6	-0.6	-0.4	-0.2			-0.3	-0.6	-1.6	-1.6	-2.3		
33.0	24.0	17.0	15.0	13.0	12.0	8.0			8.0	19.0	15.0	20.0	33.0		
+4.5	+3.5	+1.3	+0.6	-0.8	-0.9	-0.1	-0.1		-0.3	-0.6	-1.1	-1.1	+1.2	+0.5	
33.0	30.0	23.0	17.0	16.0	14.0	12.0	8.0		8.0	11.0	18.0	15.0	15.0	33.0	
+7.0	+5.0	+2.5	0.0	-1.0	-0.3	-0.1			-0.3	-1.0	-1.4	-1.5	-1.0	-0.5	
33.0	30.0	24.0	17.0	16.0	13.0	9.0			7.0	12.0	13.0	16.0	22.0	33.0	
+7.3	+8.1	+8.3	+5.0	-0.7	-0.3	-0.1			-0.2	-0.3	-1.0	+0.4	+1.1	+0.6	
33.0	29.0	24.0	20.0	15.0	12.0	8.0			8.0	13.0	16.0	17.0	25.0	33.0	
+7.8	+6.6	+9.5	+5.0	+0.7	-0.5	-0.4	-0.4		-0.2	-0.5	-1.0	-0.3	+2.8	+4.2	+5.0
33.0	27.0	23.0	19.0	16.0	14.0	11.0	9.0		8.0	14.0	16.0	18.0	21.0	26.0	33.0
+1.0	+2.5	+2.5	-1.1	-1.1	-0.8				-0.1	-0.2	-0.7	+1.8	+2.3	+2.5	
33.0	22.0	18.0	14.0	12.0	11.0				7.0	12.0	17.0	19.0	23.0	33.0	
-4.3	-2.0	-0.9							-0.2	-0.6	-1.0	+0.8	+1.1		
33.0	20.0	14.0	9.0						7.0	12.0	15.0	22.0	33.0		
-6.0	-3.0	-1.6	-0.5	-0.2					-0.2	-0.8	0.0				
33.0	29.0	18.0	14.0	8.0					8.0	17.0	33.0				
-5.6	-0.6	-0.4	-0.8	-0.9	-0.4				-0.2	-0.7	-2.5	-3.3	-4.5		
33.0	27.0	18.0	16.0	13.0	10.0				7.0	12.0	15.0	22.0	33.0		
-7.4	-1.4	+0.5	-0.8	-0.3	-0.2				-0.6	-2.7	-6.5	-8.5			
33.0	26.0	17.0	13.0	11.0	7.0				11.0	14.0	21.0	27.0			
-7.0	-1.0	-0.5	0.0	-1.4	-0.8	-0.3			-0.1	-0.8	-3.3	-4.3			
33.0	26.0	20.0	15.0	13.0	11.0	7.0			7.0	14.0	20.0	33.0			
-6.0	+0.7	+2.5	+2.3	0.0	-1.4	-0.7			-0.1	-0.6	-0.9	-3.0	-3.3		
33.0	29.0	23.0	20.0	14.0	12.0	10.0			8.0	13.0	18.0	24.0	33.0		
0.0	+4.0	+3.0	0.0	+0.3	-0.9	-0.5			0.0	-0.7	-1.5	-4.0	-6.5	-6.5	
33.0	29.0	23.0	17.0	14.0	12.0	10.0			7.0	12.0	18.0	23.0	29.0	33.0	
0.0	+1.0	-0.3	-1.0	-0.6	-0.5	-0.2			-0.3	-1.0	-4.8	-8.3	-8.3		
33.0	28.0	23.0	21.0	14.0	11.0	8.0			8.0	14.0	19.0	25.0	33.0		

Station

63 + 00

+ 75

64 + 00

65 + 00

Elev.

259.7.

62.3.

63.1.

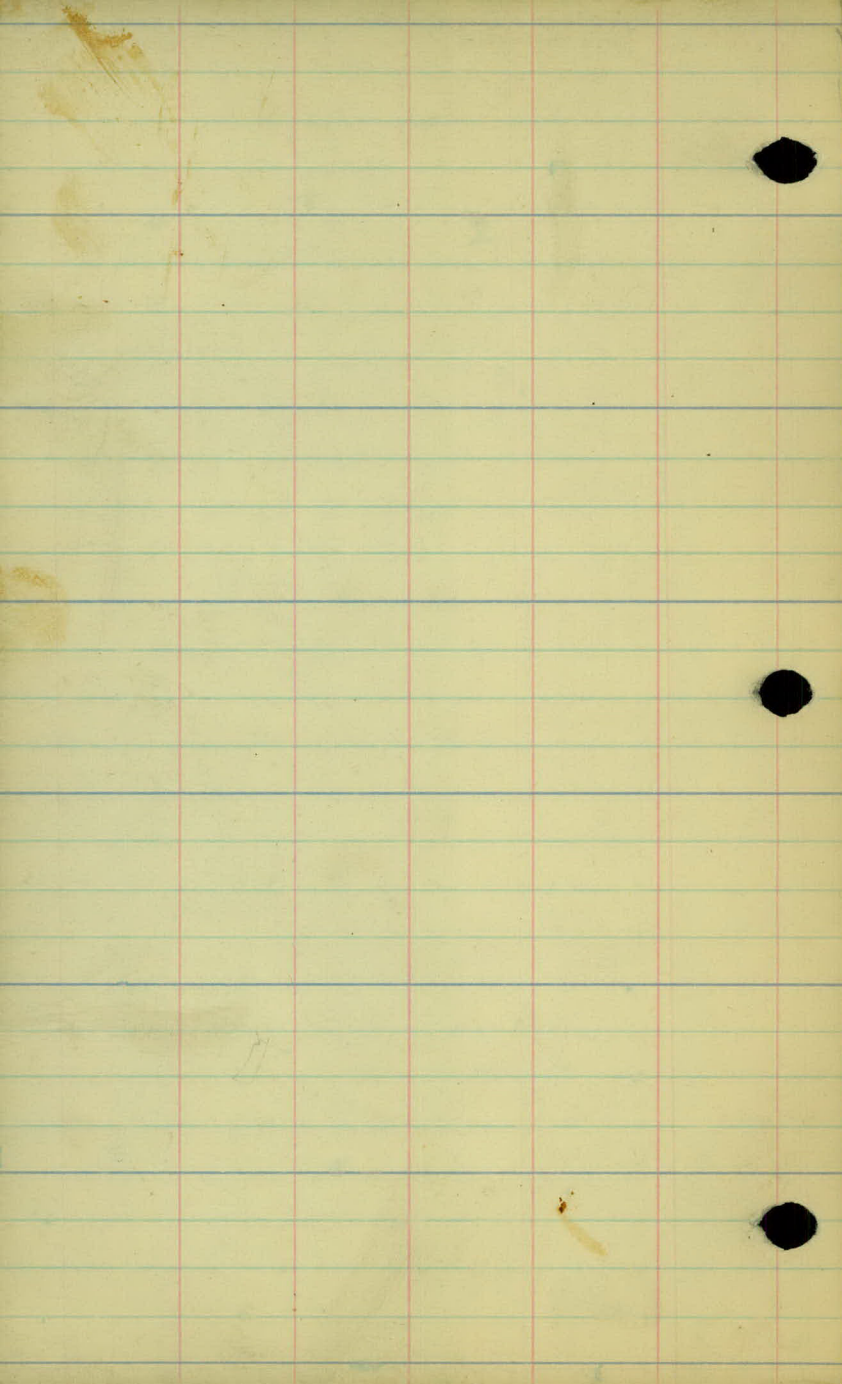
65.3.

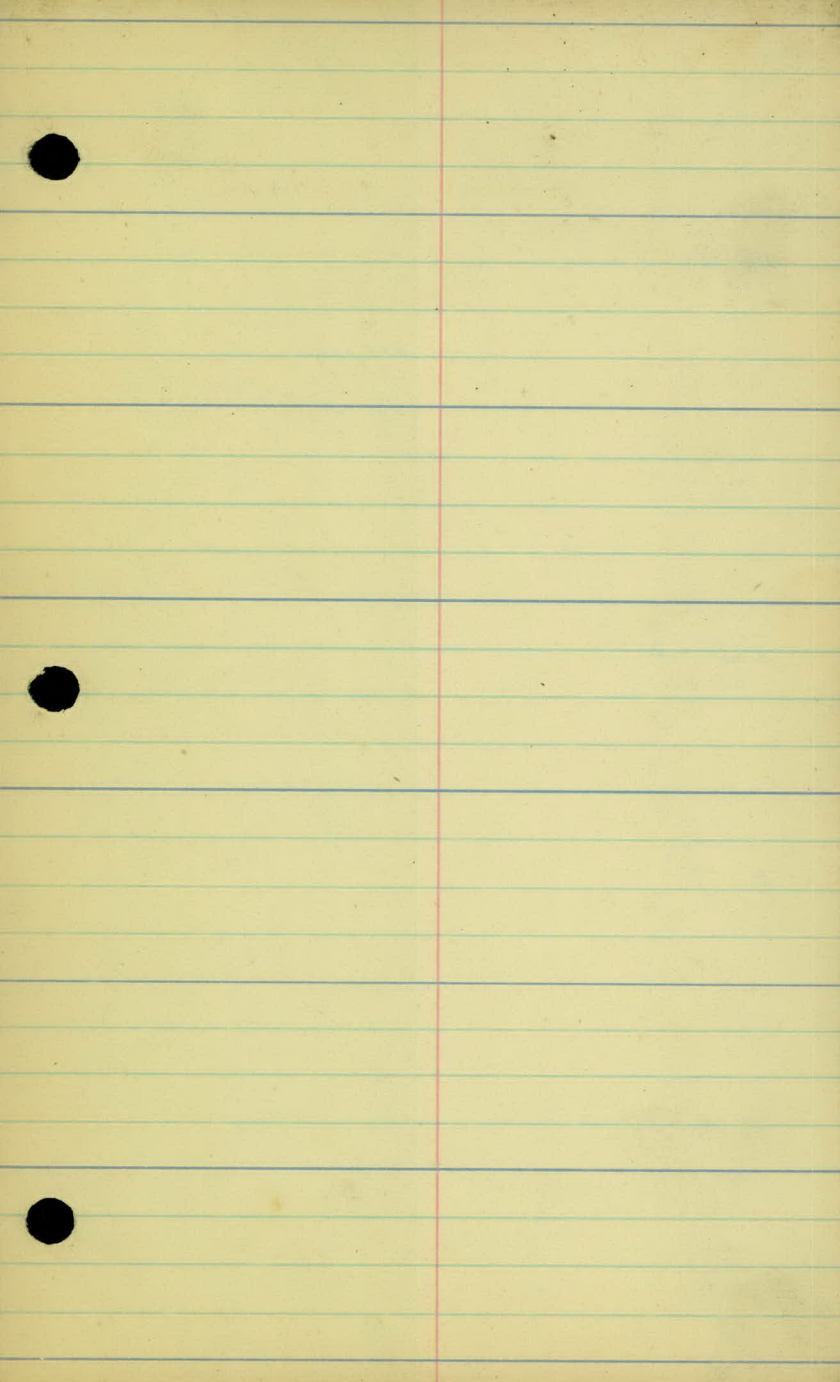
47.

七

不

[illegible]





Station

Elev.

65 + 35

65.6

66 + 00

266.1

67 + 00

65.1

+ 25

64.8

68 + 00

63.9.

+ 40

63.0.

69 + 00

62.3.

+ 80

62.2.

70 + 00

62.0.

+ 35

61.6.

+ 90

60.9.

71 + 00

60.6.

+ 50

59.8.

$$\begin{array}{r|rrrrrr} +2.8 & +5.0 & +6.6 & +6.0 & +4.0 & -0.8 & -1.0 & -0.3 & -0.3 \\ 33.0 & 30.0 & 28.0 & 24.0 & 19.0 & 15.0 & 13.0 & 12.0 & 7.0 \end{array} \quad \begin{array}{r|rrrrrr} -0.3 & -1.0 & -1.7 & -3.4 & -5.3 \\ 7.0 & 13.0 & 19.0 & 21.0 & 33.0 \end{array}$$

$$\begin{array}{r|rrrrrr} +1.6 & +3.8 & +4.8 & +3.9 & +3.3 & -0.8 & -0.8 & -0.3 \\ 33.0 & 31.0 & 27.0 & 22.0 & 19.0 & 15.0 & 13.0 & 12.0 \end{array} \quad \begin{array}{r|rrrrrr} -0.3 & -0.8 & -1.5 & -3.1 & -4.5 & -6.0 \\ 8.0 & 12.0 & 15.0 & 20.0 & 21.0 & 33.0 \end{array}$$

$$\begin{array}{r|rrrrrr} -0.9 & -0.1 & -0.1 & -0.1 & -1.1 & -1.0 & -0.4 & -0.2 \\ 33.0 & 26.0 & 21.0 & 17.0 & 16.0 & 13.0 & 12.0 & 7.0 \end{array} \quad \begin{array}{r|rrrrrr} -0.5 & -1.1 & -5.0 & -8.1 & -8.5 \\ 9.0 & 12.0 & 17.0 & 22.0 & 33.0 \end{array}$$

$$\begin{array}{r|rrrrrr} -5.0 & -3.0 & -1.0 & -1.0 & -1.2 & -0.3 & -0.2 \\ 33.0 & 31.0 & 21.0 & 15.0 & 13.0 & 12.0 & 9.0 \end{array} \quad \begin{array}{r|rrrrrr} -0.6 & -1.0 & -5.0 & -8.6 & -9.1 \\ 6.0 & 12.0 & 16.0 & 22.0 & 33.0 \end{array}$$

$$\begin{array}{r|rrrrrr} +2.9 & +2.9 & +2.1 & +1.4 & 0.0 & -1.3 & -0.6 & -0.4 \\ 33.0 & 30.0 & 24.0 & 23.0 & 17.0 & 15.0 & 12.0 & 9.0 \end{array} \quad \begin{array}{r|rrrrrr} -0.3 & -0.7 & -2.0 & -3.5 & -5.6 & -5.1 \\ 8.0 & 12.0 & 15.0 & 20.0 & 26.0 & 33.0 \end{array}$$

$$\begin{array}{r|rrrrrr} -1.0 & -1.1 & -1.5 & -0.5 & -0.3 \\ 33.0 & 29.0 & 16.0 & 14.0 & 10.0 \end{array} \quad \begin{array}{r|rrrrrr} -0.3 & -0.7 & -1.8 & -3.5 & -2.7 & -1.5 \\ 7.0 & 12.0 & 17.0 & 20.0 & 26.0 & 33.0 \end{array}$$

$$\begin{array}{r|rrrrrr} 0.0 & -1.0 & -1.5 & -1.5 & -0.7 & -0.5 \\ 33.0 & 24.0 & 20.0 & 15.0 & 13.0 & 8.0 \end{array} \quad \begin{array}{r|rrrrrr} -0.3 & -0.9 & -2.9 & -3.0 & -2.4 \\ 7.0 & 12.0 & 17.0 & 25.0 & 33.0 \end{array}$$

$$\begin{array}{r|rrrrrr} +6.5 & +8.5 & +7.9 & +5.0 & -0.3 & -0.7 & -0.3 & -0.1 \\ 33.0 & 26.0 & 22.0 & 20.0 & 16.0 & 14.0 & 13.0 & 9.0 \end{array} \quad \begin{array}{r|rrrrrr} -0.4 & -0.8 & -2.5 & -3.0 & -3.0 \\ 7.0 & 11.0 & 16.0 & 21.0 & 33.0 \end{array}$$

$$\begin{array}{r|rrrrrr} +5.0 & +6.5 & +6.8 & +5.0 & -0.5 & -0.7 & -0.4 & -0.3 \\ 33.0 & 27.0 & 23.0 & 21.0 & 16.0 & 14.0 & 12.0 & 8.0 \end{array} \quad \begin{array}{r|rrrrrr} -0.3 & -0.8 & -2.2 & -3.0 & -3.2 \\ 8.0 & 12.0 & 17.0 & 25.0 & 33.0 \end{array}$$

$$\begin{array}{r|rrrrrr} +5.0 & +7.3 & +6.8 & +5.0 & -0.7 & -0.6 & -0.3 \\ 33.0 & 27.0 & 24.0 & 21.0 & 17.0 & 14.0 & 8.0 \end{array} \quad \begin{array}{r|rrrrrr} -0.3 & -1.0 & -2.2 & -2.5 & -2.5 \\ 8.0 & 13.0 & 16.0 & 21.0 & 33.0 \end{array}$$

$$\begin{array}{r|rrrrrr} +0.5 & +1.5 & +2.0 & -0.7 & -1.0 & -0.5 & -0.3 \\ 33.0 & 27.0 & 20.0 & 17.0 & 15.0 & 13.0 & 8.0 \end{array} \quad \begin{array}{r|rrrrrr} -0.3 & -0.8 & -2.0 & -2.2 & -1.4 \\ 8.0 & 12.0 & 15.0 & 20.0 & 33.0 \end{array}$$

$$\begin{array}{r|rrrrrr} +2.7 & +2.5 & +2.1 & +0.7 & -0.5 & -1.0 & -0.5 & -0.8 \\ 33.0 & 27.0 & 22.0 & 18.0 & 17.0 & 16.0 & 13.0 & 8.0 \end{array} \quad \begin{array}{r|rrrrrr} -0.3 & -0.7 & -1.8 & -1.4 & 0.0 \\ 7.0 & 12.0 & 16.0 & 22.0 & 33.0 \end{array}$$

$$\begin{array}{r|rrrrrr} -1.3 & -0.7 & 1.0 & -0.7 & -0.4 \\ 33.0 & 22.0 & 17.0 & 13.0 & 10.0 \end{array} \quad \begin{array}{r|rrrrrr} -0.3 & -0.8 & -2.1 & -1.8 & -0.2 \\ 8.0 & 12.0 & 15.0 & 23.0 & 33.0 \end{array}$$

Station

Elev.

72+00

59.4.

+30

59.4.

+75

59.4.

73+00

59.2.

+50

58.8.

74+00

58.4.

+25

58.4.

75+00

58.2.

76+00

57.6.

77+00

58.1.

+30

58.6.

+45

58.8.

+73

58.9.

五十一

4

A4

$\frac{-0.4}{33.0}$	$\frac{-0.7}{26.0}$	$\frac{-0.2}{20.0}$	$\frac{-0.8}{17.0}$	$\frac{-0.4}{13.0}$	$\frac{0.0}{8.0}$	$\frac{-0.4}{8.0}$	$\frac{-0.7}{12.0}$	$\frac{-2.0}{15.0}$	$\frac{-2.8}{20.0}$	$\frac{-5.6}{33.0}$
---------------------	---------------------	---------------------	---------------------	---------------------	-------------------	--------------------	---------------------	---------------------	---------------------	---------------------

0.0	3.0	11.0	-0.3	-0.7	0.0	0.0	-0.4	-1.0	-2.0	-3.5	-3.0	-2.8
53.0	26.0	19.0	17.0	15.0	12.0	8.0	8.0	14.0	18.0	22.0	28.0	33.0

0.0	+0.2	+1.2	-0.7	-0.9	-0.4	0.0	-0.5	-0.7	-2.1	-3.1	-2.5	+2.5	+1.9
330	260	190	160	140	130	90	90	140	70	190	230	300	330

$+0.6$	$+0.8$	-0.8	-0.5	0.0	-0.2	-0.2	-0.5	-1.5	-3.0	-2.5	$+1.8$	$+2.1$
33.0	19.0	17.0	15.0	13.0	8.0	9.0	14.0	16.0	18.0	21.0	29.0	33.0

10.6	11.2	-0.9	-0.9	-0.3	-0.1	0.0	-0.6	-1.5	-3.5	-1.2	0.0	0.0
33.0	20.0	18.0	15.0	12.0	7.0	7.0	13.0	15.0	18.0	20.0	23.0	33.0

<u>+2.0</u>	<u>+2.2</u>	<u>-0.6</u>	<u>-0.8</u>	<u>-0.1</u>	<u>-0.1</u>	<u>-0.4</u>	<u>-0.8</u>	<u>-1.7</u>	<u>-3.6</u>	<u>-1.7</u>	<u>-1.8</u>	<u>-1.5</u>
33.0	21.0	17.0	15.0	14.0	8.0	7.0	12.0	15.0	18.0	20.0	26.0	33.0

41.0	41.0	40.8	41.0	41.0	40.1	40.1	40.4	40.8	42.7	43.8	43.6	43.0
33.0	25.0	20.0	18.0	16.0	14.0	8.0	7.0	12.0	16.0	17.0	25.0	33.0

$\frac{-1.9}{93.0}$	$\frac{-2.1}{24.0}$	$\frac{-3.5}{23.0}$	$\frac{-3.2}{20.0}$	$\frac{-2.0}{17.0}$	$\frac{-0.9}{15.0}$	$\frac{-0.4}{8.0}$	$\frac{-0.4}{6.0}$	$\frac{-0.7}{12.0}$	$\frac{-2.2}{15.0}$	$\frac{-4.5}{21.0}$	$\frac{-4.7}{33.0}$
---------------------	---------------------	---------------------	---------------------	---------------------	---------------------	--------------------	--------------------	---------------------	---------------------	---------------------	---------------------

-2.0	-2.7	-4.1	-4.1	-1.7	-0.7	-0.4	0.0	-0.3	-1.2	-3.1	-4.7	-4.5
33.0	24.0	22.0	16.0	16.0	13.0	7.0	8.0	13.0	16.0	19.0	24.0	33.0

$\frac{-1.5}{33.0}$	$\frac{-1.5}{28.0}$	$\frac{-2.3}{24.0}$	$\frac{-3.0}{19.0}$	$\frac{-1.6}{16.0}$	$\frac{-0.5}{12.0}$	$\frac{-0.2}{9.0}$	$\frac{-0.1}{10.0}$	$\frac{-0.3}{15.0}$	$\frac{-1.0}{22.0}$	$\frac{0.0}{33.0}$
---------------------	---------------------	---------------------	---------------------	---------------------	---------------------	--------------------	---------------------	---------------------	---------------------	--------------------

$\frac{-1.0}{33.0}$	$\frac{-1.0}{25.0}$	$\frac{-0.7}{20.0}$	$\frac{-1.7}{17.0}$	$\frac{-0.7}{14.0}$	$\frac{-0.3}{8.0}$	$\frac{0.0}{9.0}$	$\frac{0.0}{16.0}$	$\frac{-0.2}{19.0}$	$\frac{+3.1}{23.0}$	$\frac{+4.0}{33.0}$
---------------------	---------------------	---------------------	---------------------	---------------------	--------------------	-------------------	--------------------	---------------------	---------------------	---------------------

$\frac{-0.7}{33.0}$	$\frac{0.0}{20.0}$	$\frac{-1.7}{17.0}$	$\frac{-0.5}{12.0}$	$\frac{+0.4}{9.0}$	$\frac{+0.4}{18.0}$	$\frac{0.0}{29.0}$	$\frac{+1.1}{38.0}$
---------------------	--------------------	---------------------	---------------------	--------------------	---------------------	--------------------	---------------------

♀ Victoria

+0.3	+0.2	-1.4	-0.7	-0.2	+0.4	+1.0	+1.4
33.0	22.0	17.0	14.0	9.0	8.0	17.0	33.0

Station

Elev.

78 + 0.5

58.7.

+ 2.5

58.6.

+ 5.6

58.8.

+ 7.1

58.9.

+ 9.8

59.4.

79 + 11.0

59.6.

+ 50.0

59.5.

80 + 0.0

59.1.

81 + 0.0

58.5.

+ 5.0

57.8.

82 + 0.0

57.2.

+ 2.0

57.0.

83 + 0.0

55.6.

H.

E

R4

$$\begin{array}{r} -2.0 \quad -3.0 \quad -1.7 \quad +0.5 \quad -0.6 \quad -0.3 \\ 33.0 \quad 30.0 \quad 26.0 \quad 17.0 \quad 14.0 \quad 9.0 \end{array}$$

$$\begin{array}{r} 0.0 \quad -0.5 \quad -0.1 \quad +2.0 \quad +2.2 \quad +2.4 \\ 8.0 \quad 12.0 \quad 14.0 \quad 19.0 \quad 26.0 \quad 33.0 \end{array}$$

LRR

$$\begin{array}{r} -0.4 \quad -0.5 \quad 0.0 \\ 33.0 \quad 19.0 \quad 8.0 \end{array}$$

$$\begin{array}{r} +0.2 \quad -0.1 \quad -1.0 \quad +0.5 \quad +1.7 \\ 10.0 \quad 16.0 \quad 20.0 \quad 22.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} +3.0 \quad +2.0 \quad +1.5 \quad -0.5 \quad -0.5 \quad 0.0 \\ 33.0 \quad 23.0 \quad 16.0 \quad 14.0 \quad 12.0 \quad 11.0 \end{array}$$

$$\begin{array}{r} -0.1 \quad -0.5 \quad -0.4 \quad -0.4 \\ 8.0 \quad 11.0 \quad 23.0 \quad 33.0 \end{array}$$

LRR

$$\begin{array}{r} +2.6 \quad +1.5 \quad -0.3 \quad -0.5 \quad 0.0 \\ 33.0 \quad 18.0 \quad 16.0 \quad 14.0 \quad 12.0 \end{array}$$

$$\begin{array}{r} 0.0 \quad -0.7 \quad +0.5 \quad +2.0 \quad +1.5 \quad +1.0 \\ 7.0 \quad 12.0 \quad 15.0 \quad 19.0 \quad 26.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} +1.8 \quad +2.0 \quad +0.2 \quad -0.2 \quad 0.0 \quad +0.2 \\ 33.0 \quad 29.0 \quad 26.0 \quad 24.0 \quad 20.0 \quad 9.0 \end{array}$$

$$\begin{array}{r} -0.2 \quad -0.7 \quad +1.3 \quad +1.3 \quad +1.0 \\ 9.0 \quad 13.0 \quad 18.0 \quad 24.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} +0.6 \quad +0.6 \quad 0.0 \\ 33.0 \quad 23.0 \quad 11.0 \end{array}$$

$$\begin{array}{r} -0.2 \quad -0.9 \quad +1.2 \quad +1.5 \quad +1.0 \\ 6.0 \quad 12.0 \quad 15.0 \quad 24.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} +1.6 \quad +2.3 \quad 0.0 \quad -0.9 \quad -0.4 \quad -0.2 \\ 33.0 \quad 17.0 \quad 15.0 \quad 13.0 \quad 10.0 \quad 6.0 \end{array}$$

$$\begin{array}{r} -0.3 \quad -0.6 \quad -0.9 \quad -0.7 \quad +1.3 \quad +1.5 \quad +1.2 \\ 8.0 \quad 14.0 \quad 15.0 \quad 17.0 \quad 19.0 \quad 26.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} +2.5 \quad +2.3 \quad 0.0 \quad -1.2 \quad -1.0 \quad -0.3 \quad -0.1 \\ 33.0 \quad 25.0 \quad 16.0 \quad 15.0 \quad 13.0 \quad 11.0 \quad 7.0 \end{array}$$

$$\begin{array}{r} -0.3 \quad -0.5 \quad -1.0 \quad -0.8 \quad +1.0 \quad +1.5 \quad +1.5 \\ 10.0 \quad 14.0 \quad 15.0 \quad 17.0 \quad 19.0 \quad 25.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} +1.0 \quad +1.5 \quad -1.7 \quad -1.2 \quad -0.5 \quad -0.4 \\ 33.0 \quad 20.0 \quad 16.0 \quad 13.0 \quad 12.0 \quad 7.0 \end{array}$$

$$\begin{array}{r} -0.2 \quad -0.7 \quad -1.1 \quad +2.3 \quad +2.5 \quad +2.5 \\ 8.0 \quad 12.0 \quad 15.0 \quad 19.0 \quad 26.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} +0.9 \quad +0.3 \quad -1.0 \quad -1.5 \quad -0.5 \quad -0.3 \\ 33.0 \quad 20.0 \quad 17.0 \quad 14.0 \quad 11.0 \quad 8.0 \end{array}$$

$$\begin{array}{r} -0.4 \quad -0.6 \quad -1.2 \quad -1.1 \quad +3.0 \quad +3.0 \\ 8.0 \quad 11.0 \quad 13.0 \quad 15.0 \quad 19.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} -2.5 \quad 0.0 \quad -1.0 \quad -1.8 \quad -1.8 \quad -0.6 \quad -0.3 \\ 33.0 \quad 27.0 \quad 18.0 \quad 17.0 \quad 15.0 \quad 13.0 \quad 9.0 \end{array}$$

$$\begin{array}{r} -0.3 \quad -0.7 \quad -1.3 \quad -1.3 \quad +0.3 \quad +0.9 \quad +1.6 \\ 6.0 \quad 11.0 \quad 13.0 \quad 15.0 \quad 17.0 \quad 22.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} -3.8 \quad -2.2 \quad -1.8 \quad -0.6 \quad -0.3 \\ 33.0 \quad 21.0 \quad 15.0 \quad 12.0 \quad 8.0 \end{array}$$

$$\begin{array}{r} -0.4 \quad -0.5 \quad -1.4 \quad -1.4 \quad -0.1 \quad +0.1 \quad +1.7 \quad +2.8 \\ 8.0 \quad 11.0 \quad 13.0 \quad 15.0 \quad 17.0 \quad 22.0 \quad 25.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} -4.5 \quad -4.0 \quad -3.1 \quad -0.8 \quad -0.1 \\ 33.0 \quad 26.0 \quad 20.0 \quad 17.0 \quad 6.0 \end{array}$$

$$\begin{array}{r} -0.3 \quad -0.5 \quad -1.1 \quad -0.7 \quad +0.2 \quad +1.1 \\ 8.0 \quad 13.0 \quad 15.0 \quad 20.0 \quad 27.0 \quad 33.0 \end{array}$$

Station

Elev.

84 + 00

55.2

+ 60

55.1

85 + 00

55.3

+ 30

55.4

86 + 00

55.5

+ 50

55.5

87 + 00

55.7

+ 60

56.2

88 + 00

56.7

+ 50

57.7

89 + 00

58.9

+ 50

60.0

90 + 00

60.9

51.

E

R1.

$$\begin{array}{r} -4.0 \quad -3.4 \quad -2.5 \quad -0.6 \quad -0.3 \\ 33.0 \quad 25.0 \quad 21.0 \quad 15.0 \quad 7.0 \end{array} \quad \begin{array}{r} -0.2 \quad -0.5 \quad -1.5 \quad -0.3 \quad 0.0 \quad -0.8 \\ 8.0 \quad 13.0 \quad 16.0 \quad 18.0 \quad 23.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} -2.0 \quad -1.6 \quad -0.7 \quad -0.3 \\ 33.0 \quad 22.0 \quad 17.0 \quad 7.0 \end{array} \quad \begin{array}{r} -0.4 \quad -0.8 \quad -0.7 \quad -0.6 \quad -0.9 \quad -2.0 \\ 8.0 \quad 12.0 \quad 15.0 \quad 18.0 \quad 22.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} +2.0 \quad +1.2 \quad -1.3 \quad -1.3 \quad -0.6 \quad -0.3 \\ 33.0 \quad 21.0 \quad 19.0 \quad 17.0 \quad 15.0 \quad 9.0 \end{array} \quad \begin{array}{r} -0.3 \quad -1.5 \quad -2.5 \quad -3.0 \quad -3.0 \\ 10.0 \quad 20.0 \quad 22.0 \quad 31.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} +4.0 \quad +3.5 \quad -0.9 \quad -0.9 \quad -0.3 \quad -0.2 \\ 33.0 \quad 23.0 \quad 20.0 \quad 17.0 \quad 15.0 \quad 8.0 \end{array} \quad \begin{array}{r} -0.4 \quad -0.9 \quad -1.5 \quad -1.5 \quad -3.0 \quad -2.5 \\ 9.0 \quad 16.0 \quad 18.0 \quad 22.0 \quad 30.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} +0.7 \quad -0.5 \quad -1.6 \quad -1.7 \quad -0.7 \quad -0.2 \\ 33.0 \quad 22.0 \quad 21.0 \quad 18.0 \quad 16.0 \quad 8.0 \end{array} \quad \begin{array}{r} -0.2 \quad -1.1 \quad -2.2 \quad -3.1 \quad -2.0 \\ 9.0 \quad 14.0 \quad 18.0 \quad 27.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} +0.0 \quad +0.6 \quad -1.5 \quad -1.5 \quad -0.7 \quad -0.3 \\ 33.0 \quad 23.0 \quad 21.0 \quad 18.0 \quad 16.0 \quad 9.0 \end{array} \quad \begin{array}{r} 0.0 \quad -1.4 \quad -3.3 \quad -3.7 \\ 12.0 \quad 19.0 \quad 22.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} +1.0 \quad +0.8 \quad -1.0 \quad -1.0 \quad 0.5 \quad -0.2 \\ 33.0 \quad 24.0 \quad 22.0 \quad 18.0 \quad 14.0 \quad 9.0 \end{array} \quad \begin{array}{r} 0.0 \quad -0.4 \quad -0.9 \quad -0.8 \quad -3.5 \\ 7.0 \quad 18.0 \quad 21.0 \quad 27.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} +6.3 \quad +5.5 \quad +0.3 \quad -1.0 \quad +0.2 \quad 0.0 \\ 33.0 \quad 24.0 \quad 21.0 \quad 18.0 \quad 16.0 \quad 8.0 \end{array} \quad \begin{array}{r} -0.4 \quad -1.0 \quad -2.0 \quad -4.6 \quad -5.2 \\ 10.0 \quad 19.0 \quad 23.0 \quad 29.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} +5.0 \quad +4.5 \quad +4.0 \quad +0.2 \quad -1.0 \quad 0.0 \quad 0.0 \\ 33.0 \quad 28.0 \quad 24.0 \quad 22.0 \quad 20.0 \quad 18.0 \quad 10.0 \end{array} \quad \begin{array}{r} -0.4 \quad -1.3 \quad -3.0 \quad -5.3 \quad -6.0 \\ 8.0 \quad 18.0 \quad 21.0 \quad 25.0 \quad 29.0 \end{array} \left\{ \begin{array}{l} \text{Edge hole} \end{array} \right.$$

$$\begin{array}{r} +2.3 \quad -0.8 \quad -1.2 \quad 0.0 \quad 0.0 \\ 33.0 \quad 23.0 \quad 20.0 \quad 17.0 \quad 10.0 \end{array} \quad \begin{array}{r} -0.6 \quad -1.7 \quad -3.5 \quad -6.5 \quad -7.4 \\ 9.0 \quad 16.0 \quad 19.0 \quad 25.0 \quad 30.0 \end{array} \left\{ \begin{array}{l} \text{Edge hole} \end{array} \right.$$

$$\begin{array}{r} +3.7 \quad -0.5 \quad -2.0 \quad -2.0 \quad -0.8 \quad 0.0 \\ 33.0 \quad 20.0 \quad 17.0 \quad 15.0 \quad 14.0 \quad 7.0 \end{array} \quad \begin{array}{r} -0.4 \quad -0.9 \quad -3.2 \quad -7.5 \quad -9.0 \\ 9.0 \quad 16.0 \quad 19.0 \quad 26.0 \quad 33.0 \end{array} \left\{ \begin{array}{l} \text{Edge hole} \end{array} \right.$$

$$\begin{array}{r} +4.0 \quad -0.3 \quad -1.5 \quad -1.7 \quad -0.7 \quad -0.3 \\ 33.0 \quad 16.0 \quad 14.0 \quad 12.0 \quad 10.0 \quad 7.0 \end{array} \quad \begin{array}{r} -0.1 \quad -0.3 \quad -1.5 \quad -8.5 \quad -9.0 \\ 9.0 \quad 14.0 \quad 17.0 \quad 27.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} +1.0 \quad -0.1 \quad -1.5 \quad -1.5 \quad -0.8 \quad 0.0 \\ 33.0 \quad 19.0 \quad 17.0 \quad 14.0 \quad 12.0 \quad 8.0 \end{array} \quad \begin{array}{r} -0.2 \quad -0.6 \quad -3.0 \quad -9.0 \quad -10.0 \\ 7.0 \quad 13.0 \quad 17.0 \quad 28.0 \quad 33.0 \end{array}$$

Station

Elev.

90+30

261.3.

90+55

62.0.

91+00

62.9.

+60

63.8.

92+00

64.7.

93+00

66.2.

+25

66.3.

94+00

66.7.

+60

66.5.

95+00

65.8.

+50

64.5.

96+00

63.2.

97+00

61.0.

57

4

174.

$$\begin{array}{ccccccc} -\frac{2.0}{33} & -\frac{1.5}{14} & -\frac{0.7}{12} & -\frac{0.1}{07} & -\frac{0.2}{07} & -\frac{0.4}{12} & -\frac{1.9}{15} & -\frac{8.0}{24} & -\frac{9.5}{33} \end{array}$$

$$\begin{array}{ccccccc} -\frac{0.0}{33} & -\frac{0.5}{23} & -\frac{1.0}{15} & -\frac{0.6}{11} & -\frac{0.3}{07} & -\frac{0.4}{11} & -\frac{1.3}{16} & -\frac{3.0}{17} & -\frac{5.9}{25} & -\frac{9.0}{33} \end{array}$$

$$\begin{array}{ccccccc} +\frac{6.2}{33.0} & +\frac{6.2}{22.0} & +\frac{1.6}{16.0} & -\frac{1.1}{14.0} & -\frac{1.1}{12.0} & -\frac{0.4}{10.0} & -\frac{0.2}{08} & -\frac{0.5}{18} & -\frac{1.0}{33} \end{array}$$

$$\begin{array}{ccccccc} +\frac{7.7}{33.0} & +\frac{7.7}{24.0} & +\frac{2.6}{17.0} & -\frac{0.6}{15.0} & -\frac{0.6}{12.0} & \frac{0.0}{11.0} & \frac{0.0}{8.0} & -\frac{0.2}{8.0} & -\frac{0.7}{16.0} & -\frac{0.9}{22.0} & -\frac{1.8}{26.0} & +\frac{12.5}{30.0} & +\frac{12.5}{33.0} \end{array}$$

$$\begin{array}{ccccccc} +\frac{6.0}{33.0} & +\frac{6.5}{24.0} & +\frac{1.3}{17.0} & -\frac{0.8}{15.0} & -\frac{1.0}{13.0} & -\frac{0.2}{12.0} & -\frac{0.1}{8.0} & -\frac{0.5}{9.0} & -\frac{0.6}{17.0} & -\frac{1.1}{19.0} & \frac{0.0}{21.0} & +\frac{13.0}{24.0} & +\frac{12.3}{31.0} & +\frac{0.0}{33.0} \end{array}$$

$$\begin{array}{ccccccc} +\frac{0.6}{33.0} & +\frac{2.0}{23.0} & +\frac{1.5}{17.0} & -\frac{1.0}{15.0} & -\frac{1.0}{13.0} & -\frac{0.5}{12.0} & -\frac{0.2}{7.0} & -\frac{0.5}{12.0} & -\frac{1.2}{13.0} & -\frac{1.2}{15.0} & -\frac{0.2}{17.0} & -\frac{1.5}{27.0} & -\frac{3.8}{33.0} \end{array}$$

$$\begin{array}{ccccccc} +\frac{0.2}{33.0} & +\frac{0.7}{26.0} & +\frac{1.2}{19.0} & -\frac{0.7}{15.0} & -\frac{1.0}{14.0} & -\frac{0.5}{12.0} & -\frac{0.1}{7.0} & -\frac{0.4}{8.0} & -\frac{0.8}{12.0} & -\frac{1.6}{15.0} & -\frac{1.0}{17.0} & -\frac{1.8}{23.0} & -\frac{3.0}{33.0} \end{array}$$

$$\begin{array}{ccccccc} +\frac{1.1}{33.0} & +\frac{1.8}{26.0} & +\frac{1.6}{20.0} & +\frac{0.2}{17.0} & -\frac{1.2}{16.0} & -\frac{1.2}{14.0} & -\frac{0.5}{12.0} & -\frac{0.2}{9.0} & -\frac{0.6}{15.0} & +\frac{1.0}{16.0} & +\frac{0.7}{20.0} & -\frac{0.7}{25.0} & -\frac{2.0}{33.0} \end{array}$$

$$\begin{array}{ccccccc} +\frac{4.0}{33.0} & +\frac{4.5}{26.0} & +\frac{5.6}{22.0} & +\frac{1.7}{16.0} & -\frac{1.2}{13.0} & -\frac{0.6}{10.0} & -\frac{0.5}{9.0} & -\frac{0.6}{12.0} & -\frac{1.0}{15.0} & +\frac{1.5}{18.0} & +\frac{14.3}{20.0} & +\frac{12.7}{27.0} & +\frac{3.0}{33.0} \end{array}$$

$$\begin{array}{ccccccc} +\frac{3.0}{33.0} & +\frac{3.7}{20.0} & -\frac{0.4}{15.0} & -\frac{1.5}{13.0} & -\frac{0.6}{10.0} & -\frac{0.3}{8.0} & -\frac{0.4}{12.0} & -\frac{0.9}{13.0} & -\frac{1.0}{15.0} & +\frac{1.8}{18.0} & +\frac{13.9}{21.0} & +\frac{4.5}{29.0} & +\frac{4.5}{33.0} \end{array}$$

$$\begin{array}{ccccccc} +\frac{2.0}{33.0} & +\frac{2.8}{25.0} & +\frac{2.8}{18.0} & +\frac{0.5}{15.0} & -\frac{1.5}{13.0} & -\frac{0.7}{10.0} & -\frac{0.3}{7.0} & -\frac{0.3}{17.0} & -\frac{0.5}{13.0} & -\frac{1.2}{15.0} & -\frac{1.2}{17.0} & +\frac{12.2}{21.0} & +\frac{1.2}{26.0} & +\frac{12.1}{33.0} \end{array}$$

$$\begin{array}{ccccccc} -\frac{1.5}{33.0} & -\frac{1.1}{23.0} & -\frac{1.5}{18.0} & -\frac{1.9}{17.0} & -\frac{0.7}{12.0} & -\frac{0.2}{7.0} & -\frac{0.4}{7.0} & -\frac{0.8}{14.0} & -\frac{1.8}{17.0} & -\frac{2.3}{25.0} & -\frac{3.4}{33.0} \end{array}$$

$$\begin{array}{ccccccc} -\frac{7.8}{33.0} & -\frac{6.3}{19.0} & -\frac{3.1}{14.0} & -\frac{0.9}{11.0} & -\frac{0.3}{6.0} & -\frac{0.4}{7.0} & -\frac{0.6}{11.0} & -\frac{3.1}{15.0} & -\frac{6.6}{22.0} & -\frac{7.7}{33.0} \end{array}$$

Station

Elev.

98 + 00

259.3.

+ 50

58.7.

99 + 00

58.4.

+ 40

58.5.

100 + 00

58.0.

101 + 00

56.5.

102 + 00

55.2.

103 + 00

54.0.

+ 50

53.4.

104 + 00

53.0.

+ 50

52.7.

105 + 00

51.7.

106 + 00

49.7.

$$\begin{array}{r} -8.1 \quad -5.6 \quad -2.6 \quad -0.8 \quad -0.6 \\ 33.0 \quad 17.0 \quad 14.0 \quad 11.0 \quad 8.0 \end{array}$$

$$\begin{array}{r} -0.3 \quad -0.9 \quad -3.5 \quad -4.0 \quad -2.5 \\ 7.0 \quad 11.0 \quad 15.0 \quad 21.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} -5.3 \quad -4.5 \quad -3.9 \quad -2.4 \quad -0.9 \quad -0.4 \\ 33.0 \quad 28.0 \quad 18.0 \quad 13.0 \quad 11.0 \quad 7.0 \end{array}$$

$$\begin{array}{r} -0.3 \quad -0.8 \quad -3.0 \quad -4.9 \quad -4.0 \quad -0.6 \\ 7.0 \quad 13.0 \quad 17.0 \quad 24.0 \quad 27.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} -1.5 \quad -1.0 \quad -2.9 \quad -3.7 \quad -0.9 \quad -0.4 \\ 33.0 \quad 25.0 \quad 22.0 \quad 19.0 \quad 12.0 \quad 8.0 \end{array}$$

$$\begin{array}{r} -0.4 \quad -0.7 \quad -2.2 \quad -3.5 \quad +0.5 \quad +0.5 \\ 9.0 \quad 13.0 \quad 15.0 \quad 20.0 \quad 25.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} 0.0 \quad +0.3 \quad -2.6 \quad -2.4 \quad -0.9 \quad -0.3 \\ 33.0 \quad 29.0 \quad 22.0 \quad 17.0 \quad 13.0 \quad 7.0 \end{array}$$

$$\begin{array}{r} -0.3 \quad -0.9 \quad -3.4 \quad -1.9 \quad +0.9 \quad +1.0 \\ 7.0 \quad 13.0 \quad 19.0 \quad 24.0 \quad 29.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} -1.0 \quad -0.3 \quad -1.2 \quad -0.7 \quad -0.3 \\ 33.0 \quad 19.0 \quad 15.0 \quad 13.0 \quad 8.0 \end{array}$$

$$\begin{array}{r} -0.5 \quad -0.9 \quad -1.7 \quad -1.8 \quad +1.1 \quad +1.0 \\ 9.0 \quad 12.0 \quad 14.0 \quad 18.0 \quad 22.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} -2.2 \quad -0.9 \quad -0.4 \quad -1.0 \quad -0.3 \\ 33.0 \quad 22.0 \quad 16.0 \quad 14.0 \quad 8.0 \end{array}$$

$$\begin{array}{r} -0.3 \quad -0.9 \quad -0.5 \quad +0.7 \quad +1.4 \\ 8.0 \quad 12.0 \quad 17.0 \quad 18.6 \quad 33.0 \end{array}$$

$$\begin{array}{r} -2.6 \quad -2.5 \quad -2.0 \quad -1.2 \quad -0.4 \\ 33.0 \quad 22.0 \quad 16.0 \quad 14.0 \quad 9.0 \end{array}$$

$$\begin{array}{r} -0.3 \quad -0.7 \quad -1.5 \quad -0.2 \quad +0.1 \quad +0.6 \\ 6.0 \quad 13.0 \quad 16.0 \quad 20.0 \quad 24.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} -3.3 \quad -2.8 \quad -1.6 \quad -0.8 \quad -0.3 \\ 33.0 \quad 25.0 \quad 16.0 \quad 14.0 \quad 8.0 \end{array}$$

$$\begin{array}{r} -0.4 \quad -0.8 \quad -1.7 \quad -1.8 \quad -1.1 \quad -1.0 \\ 7.0 \quad 11.0 \quad 14.0 \quad 19.0 \quad 21.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} -3.1 \quad -2.4 \quad -0.9 \quad -0.5 \\ 33.0 \quad 17.0 \quad 11.0 \quad 8.0 \end{array}$$

$$\begin{array}{r} -0.3 \quad -1.0 \quad -1.5 \quad -0.6 \quad -0.6 \\ 8.0 \quad 15.0 \quad 17.0 \quad 26.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} -0.8 \quad -0.3 \quad 0.0 \quad 7.2 \quad -0.6 \quad -0.4 \\ 33.0 \quad 22.0 \quad 18.0 \quad 15.0 \quad 12.0 \quad 8.0 \end{array}$$

$$\begin{array}{r} -0.6 \quad -1.8 \quad -2.1 \quad -2.0 \quad +0.6 \quad +0.6 \\ 8.0 \quad 15.0 \quad 21.0 \quad 26.0 \quad 30.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} 0.0 \quad +1.2 \quad +1.6 \quad -1.2 \quad -0.4 \\ 33.0 \quad 23.0 \quad 17.0 \quad 14.0 \quad 8.0 \end{array}$$

$$\begin{array}{r} -0.4 \quad -0.5 \quad -1.7 \quad 0.0 \quad +2.4 \quad +2.6 \\ 8.0 \quad 12.0 \quad 18.0 \quad 28.0 \quad 32.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} +0.5 \quad +1.4 \quad -1.2 \quad -0.7 \quad -0.5 \\ 33.0 \quad 19.0 \quad 16.0 \quad 13.0 \quad 9.0 \end{array}$$

$$\begin{array}{r} -0.3 \quad -1.0 \quad -2.1 \quad -1.7 \quad -0.3 \quad +0.8 \\ 7.0 \quad 12.0 \quad 18.0 \quad 22.0 \quad 29.0 \quad 33.0 \end{array}$$

$$\begin{array}{r} -3.6 \quad -3.5 \quad -3.3 \quad -1.5 \quad -0.6 \\ 33.0 \quad 23.0 \quad 17.0 \quad 14.0 \quad 11.0 \end{array}$$

$$\begin{array}{r} -0.5 \quad -1.0 \quad -2.8 \quad -2.8 \quad -2.5 \\ 8.0 \quad 12.0 \quad 15.0 \quad 20.0 \quad 33.0 \end{array}$$

Station

Elev

107 + 00

248.4 .

+ 50

48.9 .

108 + 00

50.0 .

+ 35

50.8 .

109 + 00

52.1 .

110 + 00

54.1 .

+ 60

54.9 .

111 + 00

55.2 .

+ 50

55.3 .

112 + 00

55.2 .

+ 50

55.3 .

113 + 00

54.8 .

+ 50

54.4 .

$$\text{Mansh} \left\{ \begin{array}{cccc} -6.0 & -3.3 & -1.1 & -0.6 \\ 23.0 & 16.0 & 12.0 & 7.0 \end{array} \right. \quad \begin{array}{cccc} -0.3 & -0.8 & -3.1 & -5.7 \\ 7.0 & 11.0 & 14.0 & 20.0 \end{array} \left\{ \text{Mansh} \right.$$

$$\begin{array}{ccccc} -7.0 & -6.6 & -3.3 & -1.2 & -0.4 \\ 33.0 & 25.0 & 16.0 & 13.0 & 7.0 \end{array} \quad \begin{array}{ccccc} -0.4 & -0.8 & -2.6 & -4.7 & -5.5 \\ 8.0 & 12.0 & 16.0 & 19.0 & 33.0 \end{array}$$

$$\begin{array}{ccccc} -4.0 & -3.6 & -2.2 & -1.0 & -0.4 \\ 33.0 & 24.0 & 18.0 & 13.0 & 7.0 \end{array} \quad \begin{array}{ccccc} -0.5 & -0.8 & -2.2 & -1.2 & -1.2 \\ 8.0 & 12.0 & 16.0 & 20.0 & 33.0 \end{array}$$

$$\begin{array}{ccccc} -1.5 & +0.3 & -1.1 & -0.4 & \\ 33.0 & 18.0 & 14.0 & 8.0 & \end{array} \quad \begin{array}{ccccc} -0.4 & -0.7 & -1.4 & -0.7 & +0.9 & +1.0 \\ 7.0 & 11.0 & 14.0 & 16.0 & 22.0 & 33.0 \end{array}$$

$$\begin{array}{ccccc} +1.0 & +2.6 & +0.8 & -0.7 & -0.4 \\ 33.0 & 19.0 & 16.0 & 14.0 & 7.0 \end{array} \quad \begin{array}{ccccc} -0.3 & -0.8 & -1.6 & +0.7 & +3.2 & +3.5 \\ 7.0 & 12.0 & 15.0 & 20.0 & 23.0 & 33.0 \end{array}$$

$$\begin{array}{ccccc} +1.0 & +2.7 & +2.4 & +0.2 & -0.9 & -0.4 \\ 33.0 & 23.0 & 17.0 & 15.0 & 12.0 & 8.0 \end{array} \quad \begin{array}{ccccc} -0.5 & -0.8 & -1.4 & +0.1 & +2.4 & +5.0 \\ 8.0 & 13.0 & 15.0 & 18.0 & 21.0 & 33.0 \end{array}$$

$$\begin{array}{ccccc} +1.5 & +1.5 & +1.0 & -0.5 & -0.4 \\ 33.0 & 21.0 & 15.0 & 12.0 & 8.0 \end{array} \quad \begin{array}{ccccc} -0.5 & -0.8 & -1.1 & 0.0 & +2.2 & +1.5 \\ 7.0 & 11.0 & 14.0 & 16.0 & 19.0 & 33.0 \end{array}$$

$$\begin{array}{ccccc} +5.1 & +1.5 & +1.2 & +1.2 & -0.8 & -0.2 \\ 33.0 & 25.0 & 20.0 & 14.0 & 12.0 & 7.0 \end{array} \quad \begin{array}{ccccc} -0.4 & -0.6 & -1.0 & +0.2 & -0.5 & -1.7 \\ 8.0 & 12.0 & 15.0 & 17.0 & 23.0 & 33.0 \end{array}$$

$$\begin{array}{ccccc} +2.4 & +1.6 & +0.2 & -0.8 & -0.3 \\ 33.0 & 22.0 & 18.0 & 13.0 & 8.0 \end{array} \quad \begin{array}{ccccc} -0.4 & -0.9 & -2.6 & -5.2 & \\ 7.0 & 12.0 & 15.0 & 33.0 & \end{array}$$

$$\begin{array}{ccccc} +0.4 & -1.0 & -1.6 & -1.7 & -0.8 & -0.3 \\ 33.0 & 21.0 & 18.0 & 14.0 & 12.0 & 8.0 \end{array} \quad \begin{array}{ccccc} -0.5 & -1.2 & -3.3 & -5.5 & -7.0 \\ 7.0 & 13.0 & 15.0 & 20.0 & 33.0 \end{array}$$

$$\begin{array}{ccccc} 0.0 & -1.4 & -1.9 & -0.9 & -0.2 \\ 33.0 & 24.0 & 17.0 & 13.0 & 8.0 \end{array} \quad \begin{array}{ccccc} -0.4 & -1.0 & -1.9 & -2.8 & -3.0 \\ 7.0 & 13.0 & 17.0 & 21.0 & 33.0 \end{array}$$

$$\begin{array}{ccccc} +5.0 & -0.4 & -1.4 & -0.7 & -0.3 \\ 33.0 & 26.0 & 17.0 & 13.0 & 8.0 \end{array} \quad \begin{array}{ccccc} -0.6 & -1.0 & -1.7 & -0.9 & +0.7 & -0.9 \\ 8.0 & 12.0 & 15.0 & 18.0 & 20.0 & 33.0 \end{array}$$

$$\begin{array}{ccccc} +6.2 & +0.9 & -0.2 & -1.0 & -0.3 \\ 33.0 & 24.0 & 19.0 & 17.0 & 7.0 \end{array} \quad \begin{array}{ccccc} -0.3 & -0.9 & +0.2 & +2.0 & +3.5 & +2.0 \\ 7.0 & 13.0 & 15.0 & 20.0 & 23.0 & 33.0 \end{array}$$

Station
114+00

Elev.
253.5.

+25

53.1.

+50

52.7.

+78.8

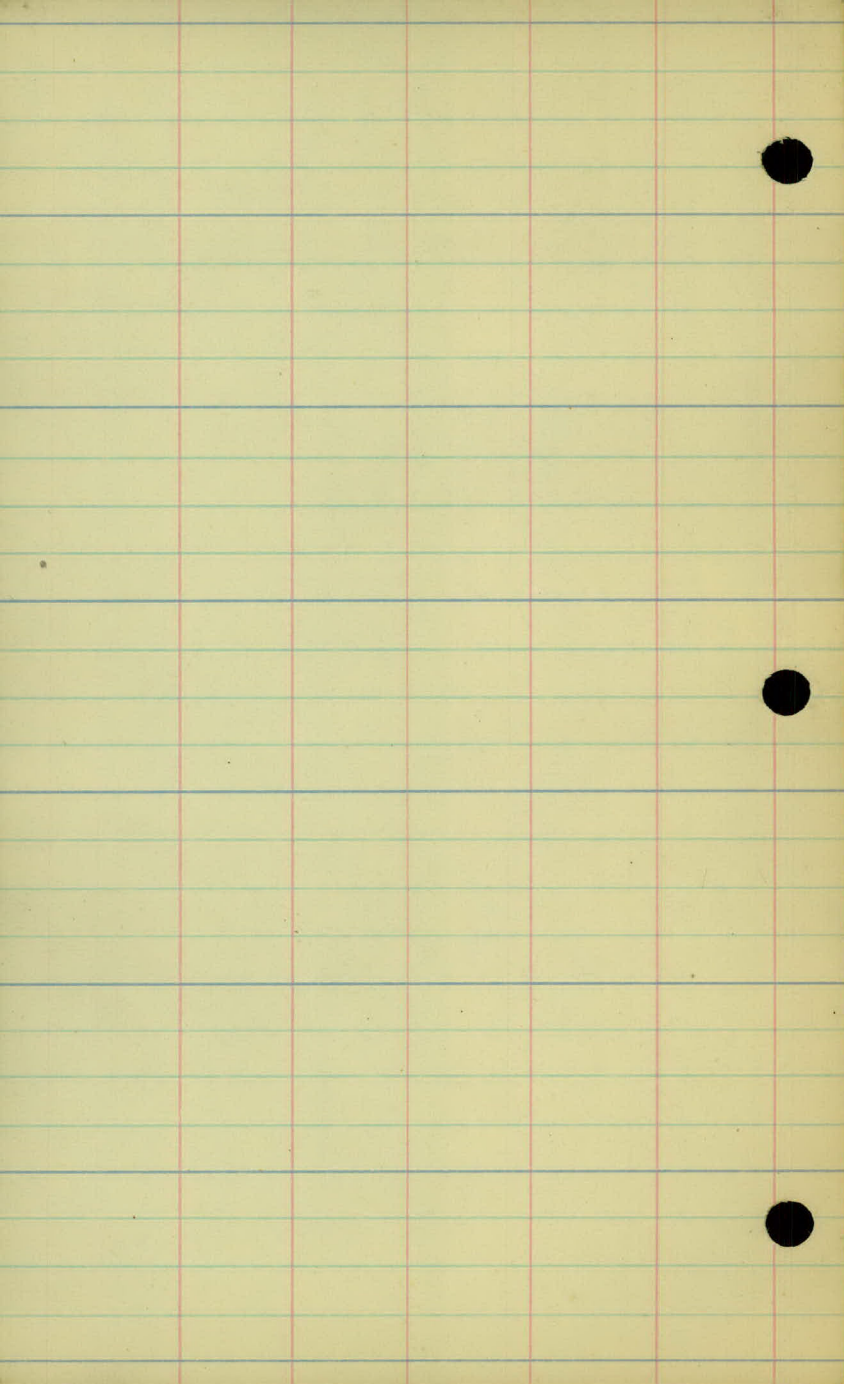
52.6

$$\begin{array}{cccccc} +2.1 & +2.0 & 0.0 & -0.9 & -0.6 & -0.3 \\ \hline 33.0 & 21.0 & 18.0 & 14.0 & 12.0 & 8.0 \end{array} \quad \begin{array}{cccccc} -0.4 & -0.9 & -1.5 & +0.4 & +0.3 & +0.0 \\ \hline 9.0 & 13.0 & 14.0 & 18.0 & 25.0 & 33.0 \end{array}$$

$$\begin{array}{cccccc} +1.6 & +1.5 & -1.6 & -1.6 & -0.5 & -0.1 \\ \hline 33.0 & 19.0 & 15.0 & 13.0 & 12.0 & 8.0 \end{array} \quad \begin{array}{cccccc} -0.5 & -1.2 & -1.5 & +0.2 & -0.6 & \\ \hline 8.0 & 17.0 & 19.0 & 21.0 & 33.0 & \end{array}$$

$$\begin{array}{cccc} -0.5 & -1.1 & 0.0 & 0.0 \\ \hline 33.0 & 28.0 & 20.0 & 9.0 \end{array} \quad \begin{array}{ccc} -0.2 & -0.7 & -1.3 \\ \hline 9.0 & 16.0 & 33.0 \end{array}$$

$$\begin{array}{ccc} +1.0 & -1.6 & +0.6 \\ \hline 33.0 & 24.0 & 11.0 \end{array} \quad \begin{array}{ccc} 0.0 & -0.4 & -0.5 \\ \hline 11.0 & 21.0 & 33.0 \end{array}$$



Co. Rd. "F" Road #6

Drainage Notes

Station

43+40 - 18" x 49.5 C.M.P.

Ext. 23.5 Rt. - 26.0 Ht.

Int. Elev. = 205.43

Inv. $vv = 205.23 - \frac{204.4}{15.0}$
Drains Rt.

28+65.0 - 30" x 79 C.M.P.

Ext. 41.0 Rt. - 38' Ht.

Int. Elev. = 190.42 (End. Settled).

Inv. $vv = 191.18 - \frac{190.7}{15.0}$
Drains Rt.

12+80 - 12" x 23 C.M.P.

Ext. 8' Rt. - 15' Ht.

Int. = 210.5

Inv. = 209.77

Drains 6 ft.

0+22 - 15" x 46 C.M.P.

Ext 18' Rt. - 28' 6 ft.

Intake - 232.15

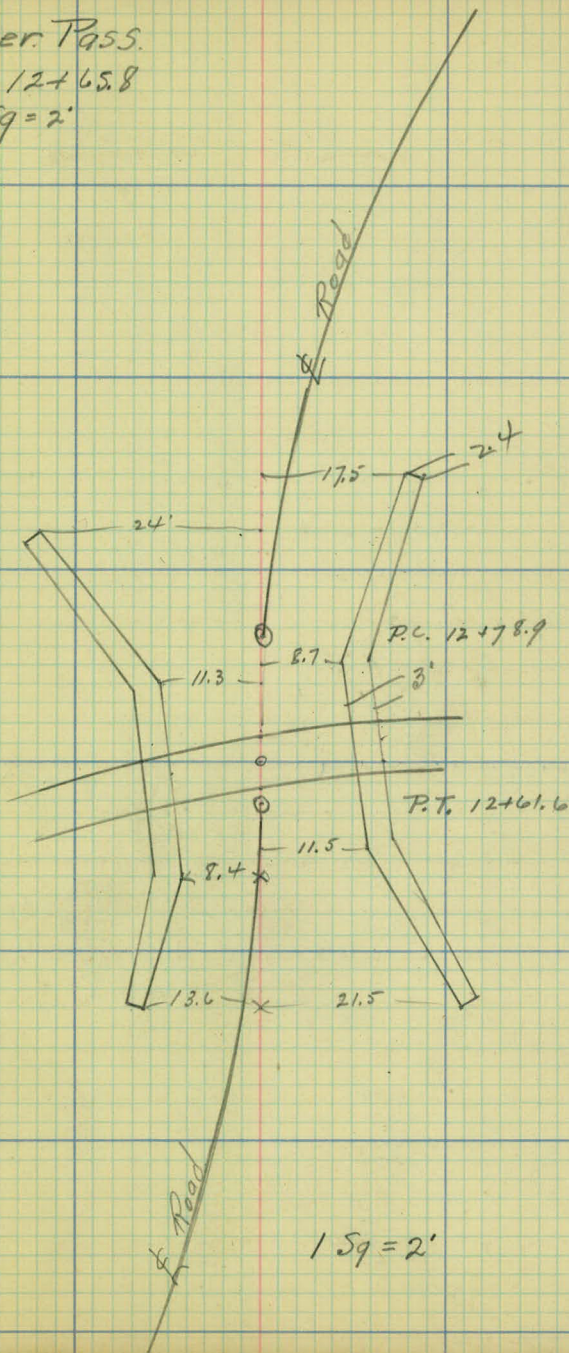
Invert - 232.11

Drains Rt.

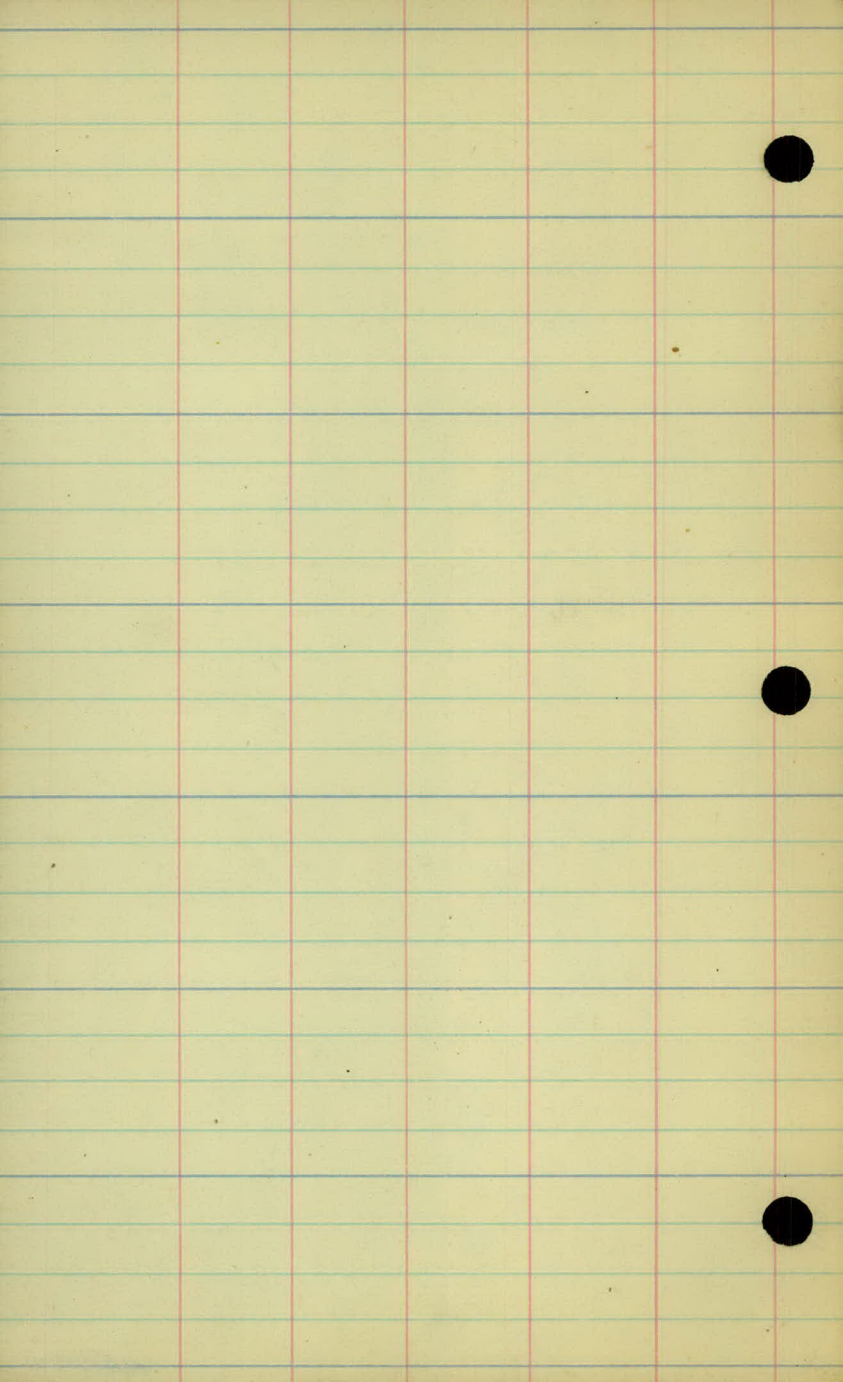
Under Pass.

Sta 12+65.8

1 Sq = 2'



1 Sq = 2'



TWIN CITY CONCRETE PIPE CO.
AN AFFILIATE OF
ELK RIVER CONCRETE PRODUCTS CO.

PLANT: TUXEDO 1-2615

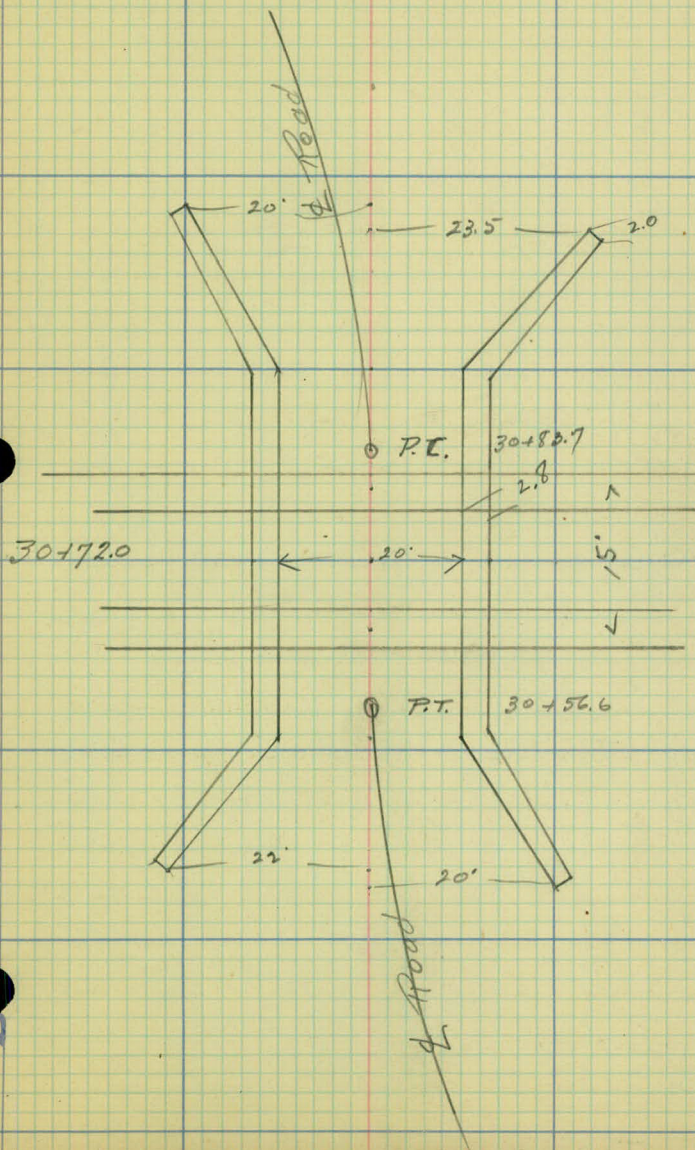
HARRY T. CALLINAN

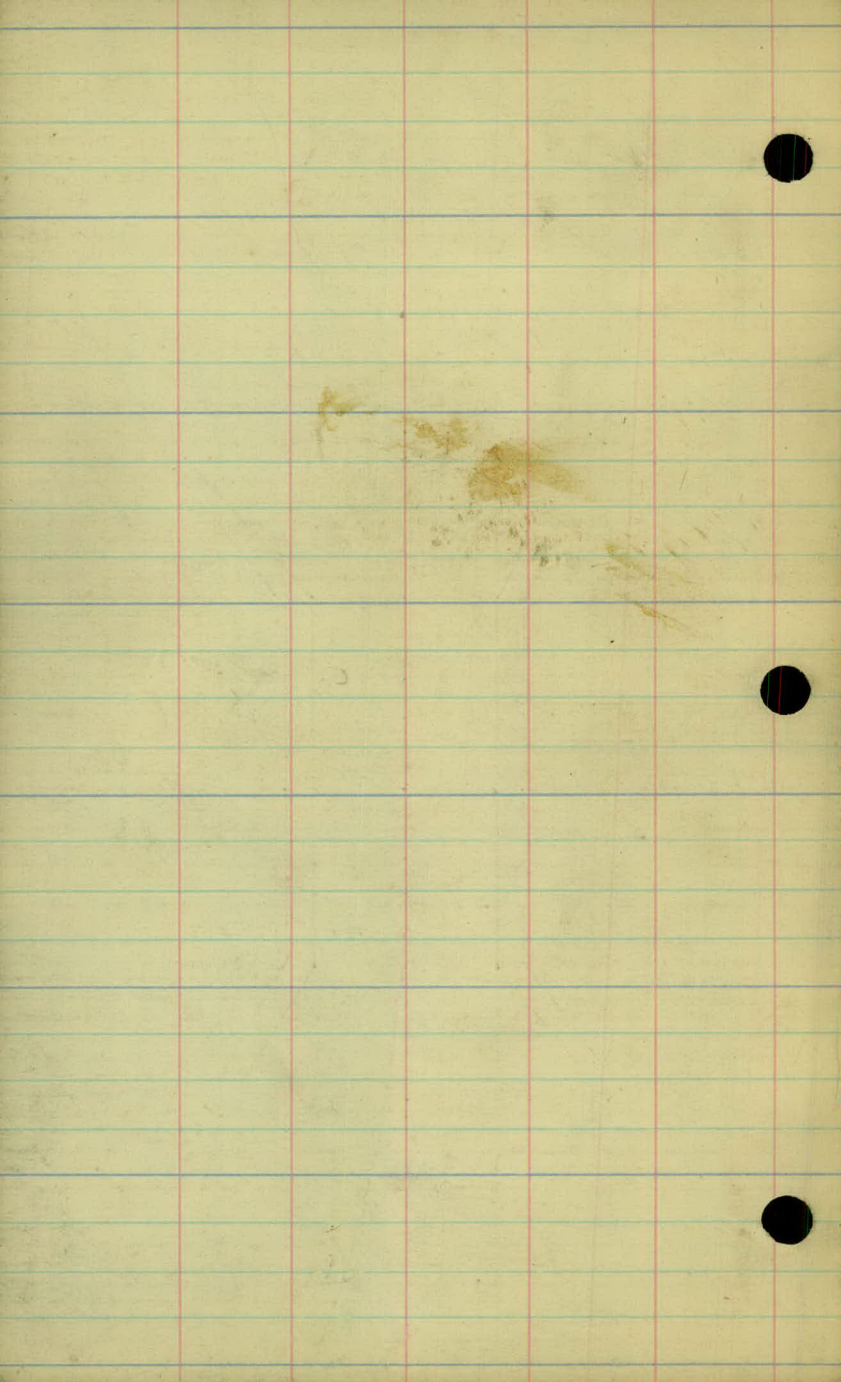
Res. Hopkins, Minn.
West 8-1459

Office: 650 Builders Exchange
Federal 6-2679

12 + 65
30 + 72

Under. Pass
Sta 30+72
15g = 2'





Maint. Survey
Road #6

Turned in
5-5-24

PJH

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed 5-5-24

File No.

Station	Elev	Invent	Outlet	R	L
76+55	⁷⁶⁺⁰⁰ 257.6	52.45	51.91	28'	23'
78+19	⁷⁸⁺²⁸ 258.6	55.68	55.62	21.5'	13'
86+10	⁸⁶⁺⁰⁰ 255.5	53.24	51.60	19'	17.5'
97+47	⁹⁸⁺⁰⁰ 259.30	52.98	50.41	23'	23'
107+06	¹⁰⁷⁺⁰⁰ 248.40	42.39	41.81	17'	23'

18" Corr Pipe Drains Left

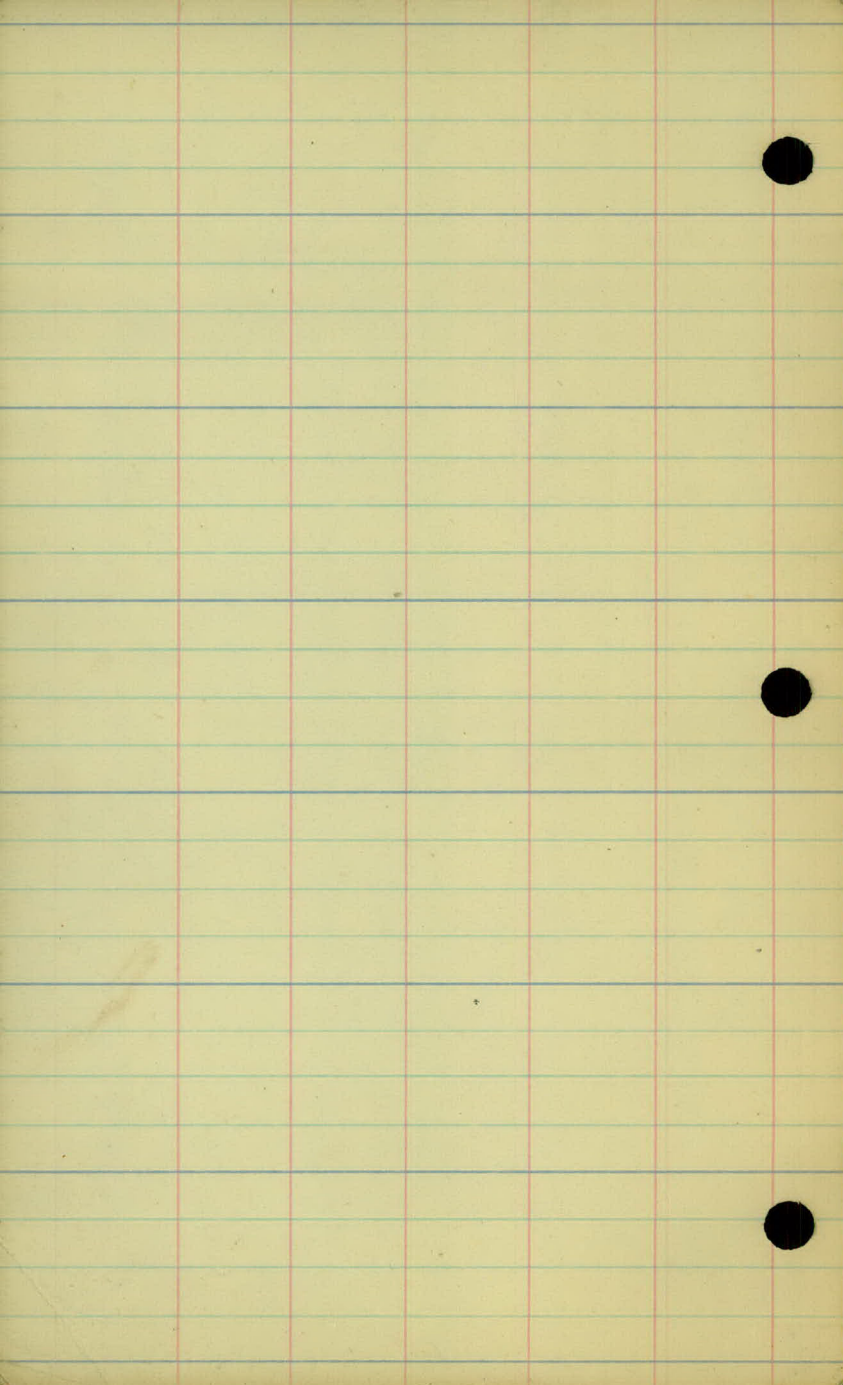
18" Corr Pipe Drains Left

15' Corr Pipe Drains Right

12" Corr Pipe on Ends 4' Each End - The rest is 10" Vet pipe
Drains Left

10" Corr pipe on Left side 8" Vet pipe on right
Drains Left

Note: Can not tell how much of each kind
of pipe



0

1,1

			Grade	Rod	Ground
0+00	5.85	105.85	100.00	100.0	100.0
+50			99.70 ✓	6.3	99.6
1+00			99.40 ✓	6.0	99.9
+50			99.1 ✓	5.3	100.6
2+00			98.8 ✓	5.6	100.3
+50			98.5 ✓	6.5	99.4
3+00			98.2 ✓	7.3	98.6
+50			97.9 ✓	7.3	98.6
4+00			97.6 ✓	8.0	97.9
4+24 Int				7.9	98.0
Inv.				8.3	

$$\begin{array}{r}
 100.0 \\
 97.5 \\
 \hline
 4+24 \quad 2.5000 \quad 60.59 \\
 2120 \\
 \hline
 3800 \\
 3816
 \end{array}$$

$$\begin{array}{r}
 105.9 \\
 98.5 \\
 \hline
 7.1
 \end{array}$$

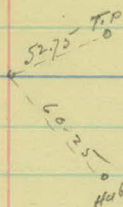
$$\begin{array}{r}
 105.9 \\
 99.7 \\
 \hline
 6.2
 \end{array}$$

$$\begin{array}{r}
 105.9 \\
 97.6 \\
 \hline
 8.3
 \end{array}$$

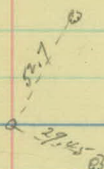
$$\begin{array}{r}
 105.9 \\
 99.4 \\
 \hline
 6.5
 \end{array}$$

$$\begin{array}{r}
 105.9 \\
 97.5 \\
 \hline
 8.4
 \end{array}$$

P.I. 26 + 59.0



P.C.C. 22 + 77.6



P.I. 19 + 54.0

