

Book # 38 - Dr - 8

MAINT. SURVEY
ST CO. LINE ROAD

From White Bear Blvd.

To North St. Paul

RD. % N^o 22 4

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed

File No. "13"

East County Line Road

Road Acct No. 22

Alignment Notes

Sta 78+14.5 to 133+67.2

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed _____

File No. "13"

Rd # 22

Sta Point Lt Δ Rt Calc

98+11.4 POT

91+32.2 POT

51°13'E ✓

80+96.5 PI 0°56' Section Corner

80+86.3 $\frac{1}{2}$ hinge of car trk.

78+14.5 EC Beginning of Road Hect No 20

78+14.5 EC End of Rd Hect No 24

50°17'E ✓

②
FMC 3-4-24
Rd Rect Ho 22

8" Cotton wood



45.35

8" Cotton wood



49.55

30° = hub R.P.

30° = hub R.P.

1° 56'

89° 29'

P.I. Sect. Cor

Sec line



N

M.C. □

Sta Point Lt Δ Rt Calc.

133+67² End Road acct. No. 22 Sec. Cor.

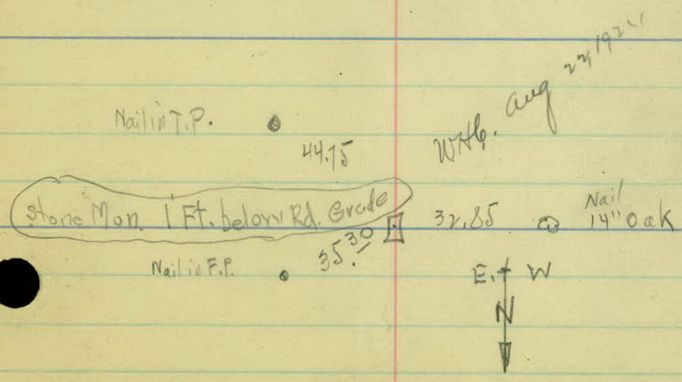
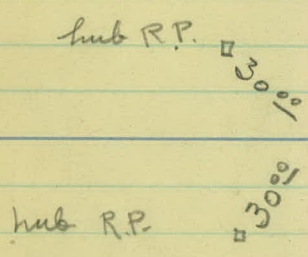
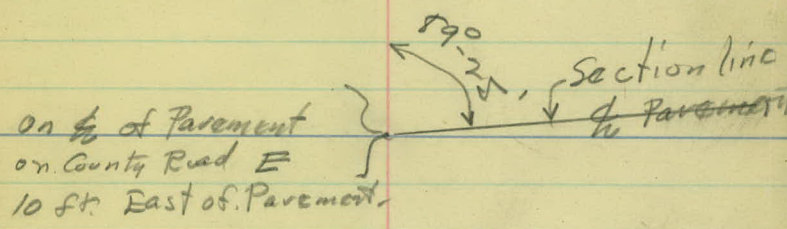
118+80⁶ POT

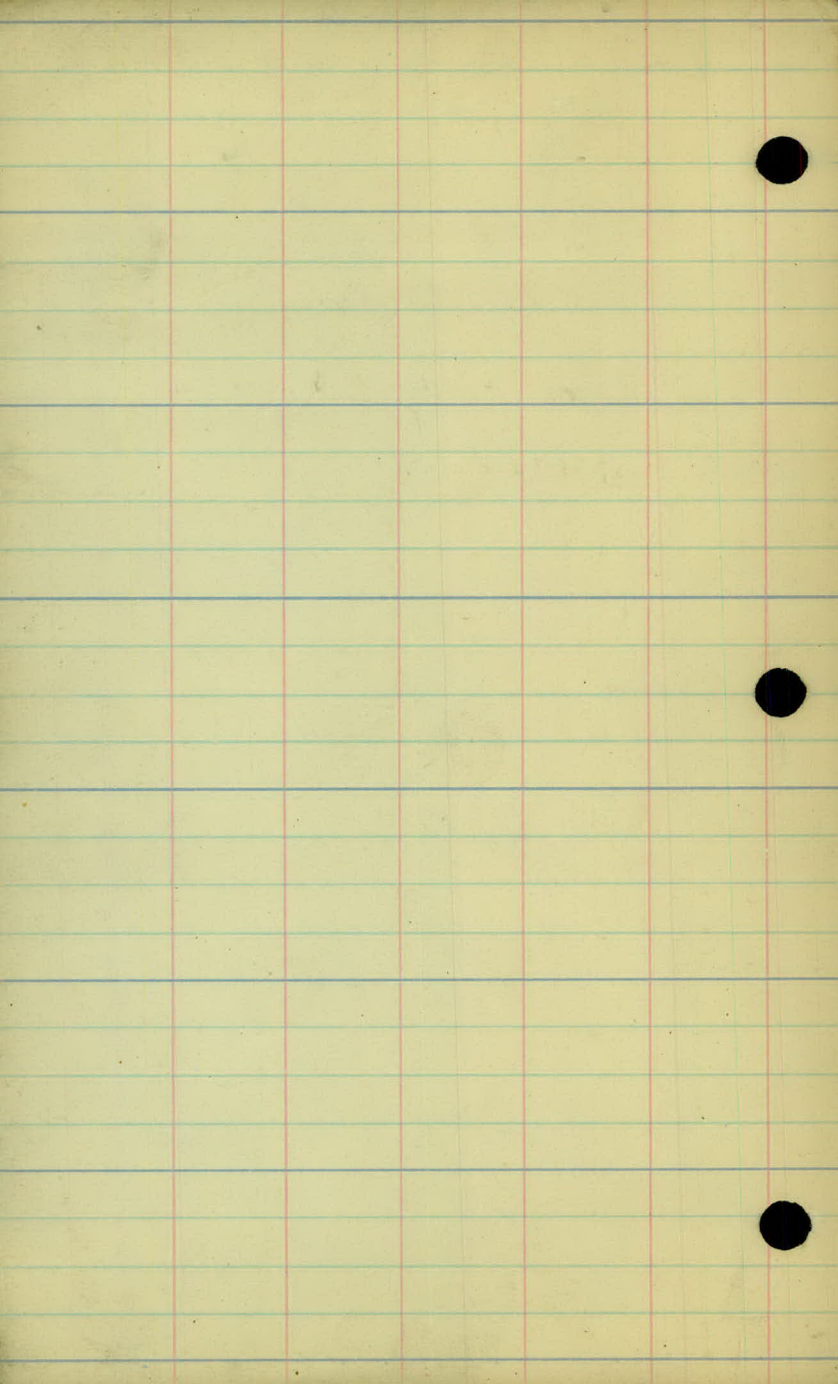
50°30'E ✓

107+32⁸ PI

0-43' $\frac{1}{4}$ Cor.

EMC. 3-5-24
Rd. Sect. Ho. 22





East County Line Road
Road Acct No 22
Levels
Sta 78+50 to 133+67.2

Sta + HI - FI

B.M.	876	250.67✓		240.86	240.91
79			0.3	250.4✓	
T.P.	13.01	262.32✓	1.44		249.23✓
80			3.5	258.7✓	
T.P.	12.90	274.54✓	0.60		261.64✓
80+84			8.32	266.2	266.22✓✓
80+96.5			8.03	266.57✓	
92			4.2	270.3✓	
83			0.2	274.3✓	
T.P.	11.61	285.19✓	0.96		273.158✓
84			6.9	278.3✓	
85			2.8	282.4✓	
T.P.	11.47	296.22✓	0.44		284.75✓
86			9.9	286.3✓	
87			6.8	289.4✓	
88			3.5	292.7✓	
T.P.	10.46	305.64✓	1.04	?	295.18✓
89			9.3	296.3✓	
90			6.6	299.0✓	
B.M.			2.10		303.54✓
91			4.8	300.8✓	
92✓			4.1	301.5✓	
93			4.4	301.2✓	
94			4.0	301.6✓	
T.P.	5.74	306.19✓	4.79		300.85✓

(5)
F.M.C. 3-4-24
Road Acct No. 22

RR spike in T.P. ~~Rd~~ Sta 77+55

No. rail of Elec line
over hole in mount. sec. cor. B.M.

89+90 T.P. 25 ft Lt RR spike

Sta	+	HI	-	EL
		306.59 ✓		
95			4.7	301.9 ✓
96			4.8	301.8 ✓
97			4.6	302.0 ✓
98			4.7	301.9 ✓
99			4.4	302.2 ✓
100			4.5	302.1 ✓
BM	2.6 ✓	306.04 ✓	3.17	303.42 ✓
101			4.3	301.7 ✓
102 ✓			5.0	301.0 ✓
103			6.2	299.8 ✓
104			7.7	298.3 ✓
T.P.	3.04	300.89 ✓	8.19	297.85 ✓
105			3.2	297.4 ✓
106			4.1	296.8 ✓
107			5.6	295.3 ✓
Bm	4.35	297.82 ✓	7.42	293.47 ✓
108			3.7	294.1 ✓
109			4.9	292.9 ✓
110 ⁺⁵⁰			4.9 ^{5.3}	292.9 ✓
111			2.5	295.3 ✓
T.P.	11.7 ✓	308.43 ✓	1.11	296.71 ✓
112 ✓			10.6	297.8 ✓
113			6.9	301.5 ✓
114			2.9	305.5 ✓
T.P.	11.09	318.66 ✓	0.86	307.57 ✓
115			8.9	309.8 ✓

FMK. 3-4-24
Ed. Sect. No 22

99+45 T.P. 30ft Lt R.P. spike

107+65 R.P. spike in T.P. 30ft Lt.

318.66

116			5.1	313.6 ✓
117			0.8	317.9 ✓
T.P.	9.61	327.71 ✓	0.56	318.10 ✓
118			6.2	321.5 ✓
118 + 50			4.9	322.8 ✓
119			4.4	323.3 ✓
120			4.6	323.1 ✓
121			5.7	322.0 ✓
121 + 50			6.8	320.9 ✓
122			8.1	319.6 ✓
123			10.3	317.4 ✓
T.P.	2.90	319.45 ✓	11.16	316.55 ✓
B.M.			3.95	315.50 ✓
124			4.0	315.5 ✓
125			6.3	313.2 ✓
126			8.2	311.3 ✓
127			10.3	309.2 ✓
T.P.	2.91	312.33 ✓	10.03	309.42 ✓
128			4.7	307.6 ✓
129			4.8	307.5 ✓
130			4.5	307.78
131			4.4	307.9 ✓
132 ✓			3.8	308.5 ✓
T.P.	5.49	312.81 ✓	5.01	307.32 ✓
133			4.4	308.4
767.5			4.1	308.7

(7)
F.MC 3-J-24
Rd. Acct. No 22

sta 123 + 27-30 ft Lt 8" oak

BM

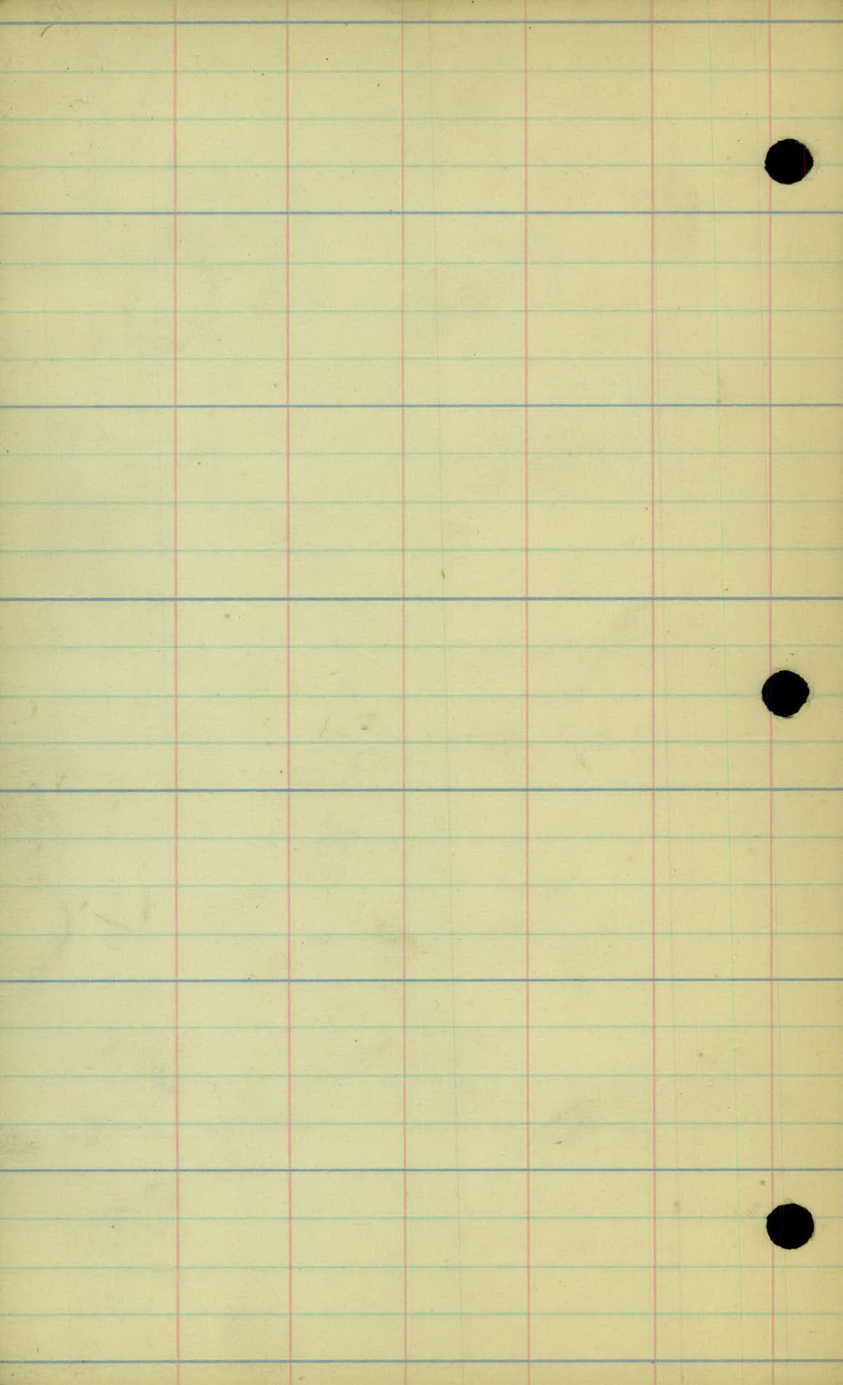
312.81

8.18

304.63 v 304.76

(8)
FMC 3-5-24
Rd. Sect No 22

top of Cor F.P. Rt of E Co. Rd. So. of Co Rd E.



East County line Road

Road Acct. No 22

Art. Topog.

Sta 78 to 133 + 67 =

84

83

82

81

80

79

78

FMC - 3-4-24
Rd. Acct No 22

R13Y

+90 Damage sign 15
+78 ^{PR} 25 F/32
pipe line 420
R10

R10

Hedge / 26

10 10

(TP
 +43 P.P 25
 +12 FC 28
 +19 King sign 12
 +06 waiting 26
 +62 P.P 23 FC 33
 +12 sign 19
 +52 TP 25
 +62 R 10

R. 0

+73 pole 26 F3 ✓
+24 Fc 3 ✓
+21 TP 2 22

Birchwood
+92 PP 39
+85 FC 3m
+75 TP 1 FC 33

Street. 28.

+16 steps 16
 +41 sign 25-35
 +28 plop corner 33
 +30 Road sign 18

160TP37
+54 Xinc 19
+50 R10

+13 pillars 32
pillars 32 R 10

scattered trees

ridge 32

+83 sign 13
+39 line 20

90

89

88

87

86

85

84

FMC 3-4-24
RD Hect 110 22

(11)

R 12

R 11

+91 PP
+100 FC

+100 pipe 33

+100 FC
R 110

+95 pole (dead) 26

+67 pole 25

R 110

+68 pole 25

R 110

hedge 31

+29 TP 25
R 110

+26 TP 25

+97 hedge 31
+80 TP 24

+82 cone steps 26

+69 stick

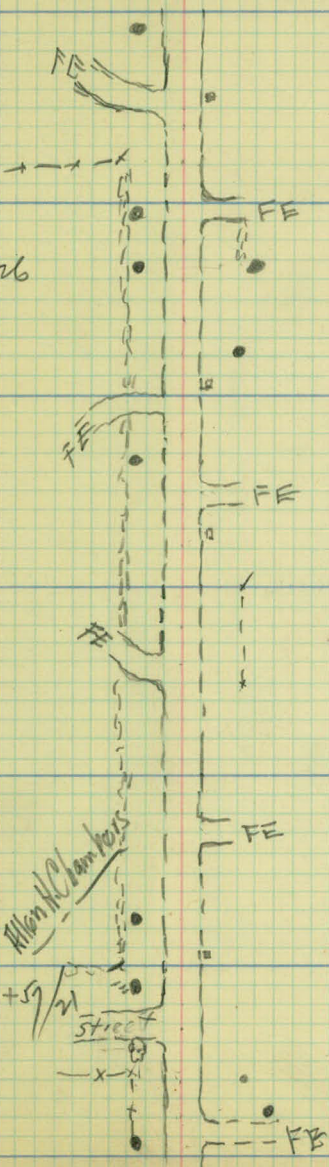
End of water line

+53 tree 24

+44 FC 26

+38 Ranger sign

+07 TP 28



+55 TP 24 12

R 110

pole line Xing +68

+66 proper 23

+22 TP 30

+05 mby 1

R 11

+29 mby 13

R 110 F 32

F 32

R 11

+79 mby 13

+08 mby 12
tree

R 11

+40 mby 22

+44 power line Xing

pole 43

96

95

94

93

92

91

90

F.M.C. 3-4-24
 Rd. Sect. No 22

(12)

K/11
 +97 huc FC 33
 +10 huc 31
 +62 huc 31
 +36 TP
 +11 huc
 R/12

R/12 F/29

+21 huc
 +62 huc 22
 +44 huc 22
 +41 FC 30
 +93 TP 30
 +99 FC 30

R/12 F/29

+71 huc 11

Street

lane

R/11

R/12

+77 TP 54

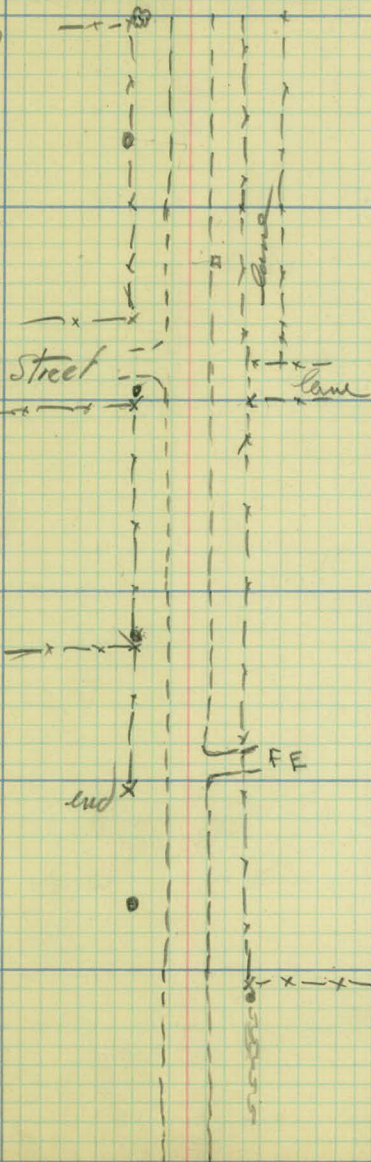
R/10
 +96 FC 31

R/11

+36 TP 30
 R/11

R/10

+91 FC 33
 +96 prof cor.



102✓

101

100

99

98

97

96

F.M.C. 3-4-24
Ed. Heet. No 22

R/14

+91 TR 35 F/36

R11 F30

R/11

und
FE

R/12

+91 FC 37

+63 TP 35

+37 hu 36

+06 hu 36

R 12

+71 hu 15

R12 F/30

+8 hu 35

+59 hu 36

+44 TP 35

+36 hu 33

+16 hu 32

R11 F30

R/11

+91 hu 33

+41 hu 33

+4 TP 33

R 12

R12 F30

+25 hu 33

+45 hu 33

+14 hu 33

R 11

R11 F30

+82 hu 33

+74 TP 33

+53 hu 33

+27 hu 33

108

107

106

105

104

103

102

FMC 3-4-24
Rd. Sect No 22

F/17 R/12

R/12

+55 TP 33
+21 FC/24
R/12

+39 ~~tree~~ 31
+33 FC/33 tree
R/12 F33

+31 TP 33 F34
R/12

+46 ~~tree~~ 29 F33
+44 ~~tree~~ 28
R/12

R/11

R/11

+86 TP 33 F34

R/12

R/12 F31

+84 ~~tree~~ 31

+36 TP 33 F34
R/12

R/12

+35 ~~TP~~ 33

X-X

FE

FE

FE

114

113

112

111

110

109

108

FMC 3-5-24
Rd. Sect. No 22

(15)

R/12 ✓

R/12

R/10

R/10

R/11

+90 tons

+36 tons 27
15/12 ✓

+21 tons 12

R/12 ✓

R/11

R/12 ✓
+90 tons 21

+53 tons 24

Waste dump
Waste dump

FR

III



+20 steps 21

R/12 ✓

+34 FR 33

+40 FC 24

+32 tons 21

+28 tons 24

+23 tons 22

+23 tons 19

F/10 R/11

+46 tons 19

+63 tons 19

F/12 R/12 ✓

+94 FR 33

1120

119

118

117

116

115

114

FMC 3-5-24
Ed. Fleet No 22

R/12

R/12

R/12

R/12

R/12

R/12

R/12

R/12

R/12

R/12

R/12

R/12

Main side borrow

Main side borrow

waste dump

waste dump

FE

126

128

124

123

122✓

121

120

FMC 3-S-24
R.D. Sect No 22

(17)

R/10

+98 trees 24

+11 trees 26

F/b R/10

R/10 ✓

+35 trees 29
+31 trees 31

R

R/10 ✓

+63 trees 23

+29 trees 21

+15 trees 24

+10 trees 24

R/10 trees 21 R/

BM →

FE

+33 trees 27

R/10

+70 trees 27

R/10 ✓

{ +77 trees 21
7 trees
+34 trees 25

R/10 ✓

R/10 ✓

R/10 ✓

+17 trees 25

R/10 ✓

+27 trees 30

+44 trees 33

+10 trees 34

132 ✓

131

130

129

128

127

126

FMC 3-5-24
TRD Foot 14022

R/12

R/12

R/12

R/12 tuz

R/11

R/12
+94 tuz 31

+35 PC 19
+31 tuz 20
tuz 20 Fuz R/12
+90 tuz 21
+71 tuz 21
+60 tuz 21
+51 tuz 21
+15 tuz 21
R/12

+72 tuz 38

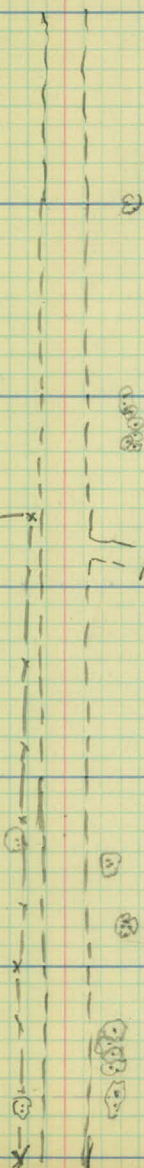
R/12

+65 tuz 24
+32 tuz 24
+19 tuz 24
+16 tuz 24
Fuz R/12

R/12

+26 Swallow 35
+19 Swallow 33
R/12

+26 tuz 25
+68 tuz 29
+48 tuz 25
+21 tuz 21 Fuz



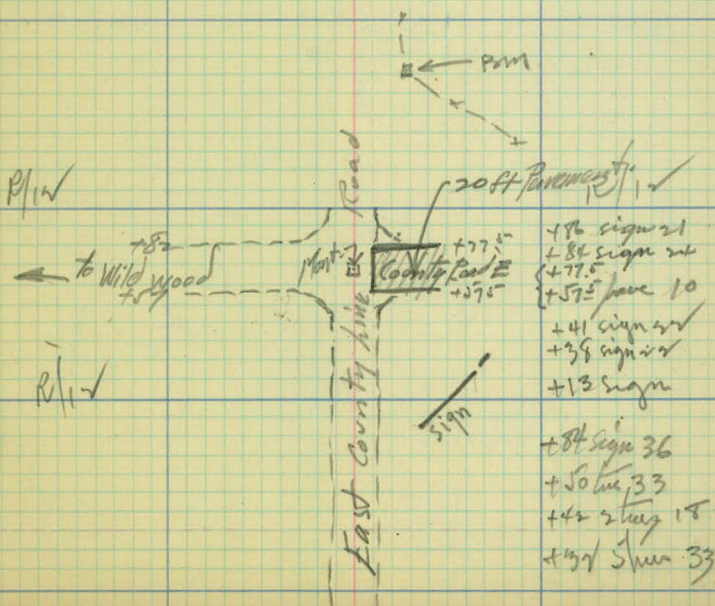
134

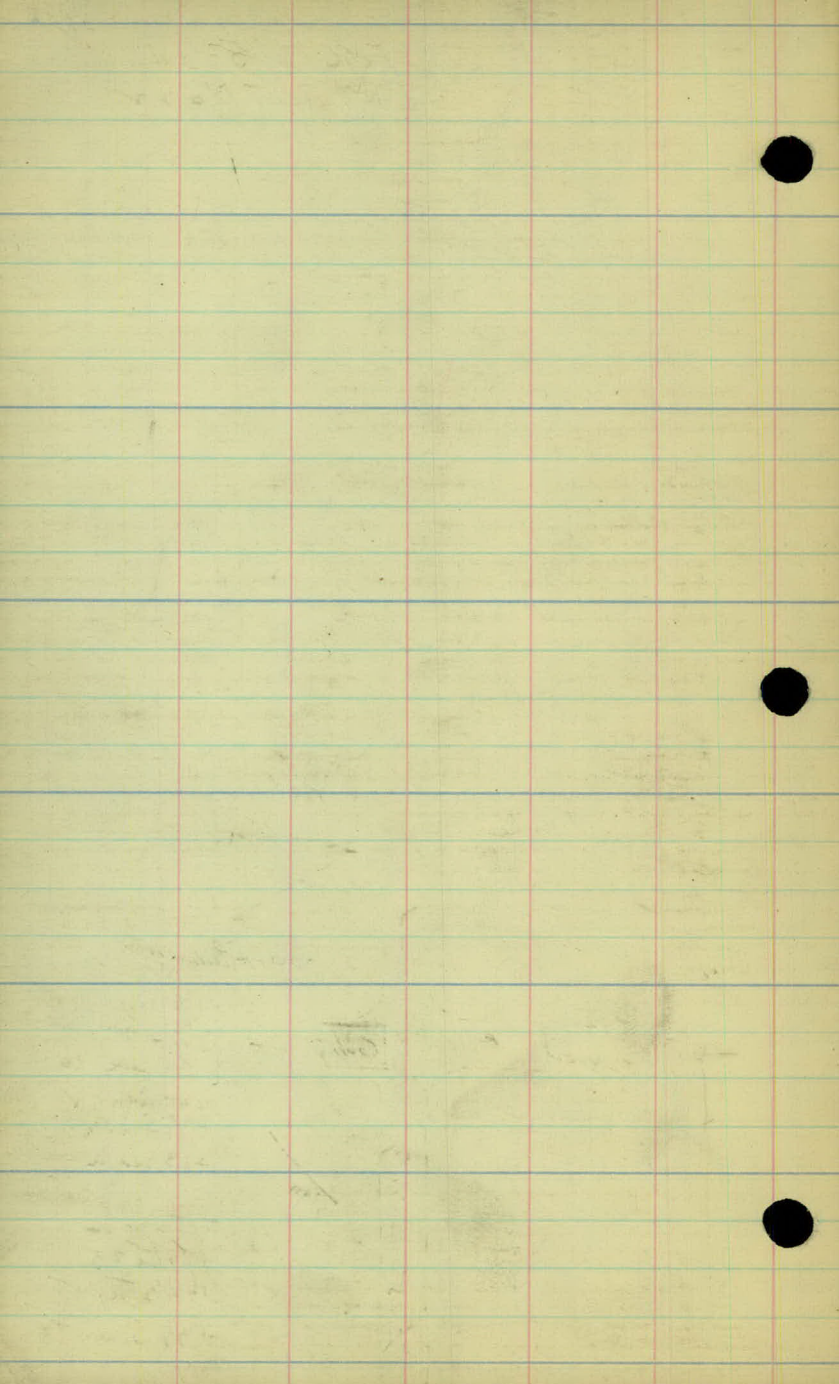
133

132

FMC 3-5-24
RD Acct No 22

(19)





East County Mine Road
Road Acct. No 22 ✓

X Sections

Sta 78+50 to ~~133~~ + 67.2

Sta.
78+50

Elev
247.7

79

250.4 ✓

79+50

54.6

80

58.7 ✓

29

80+50

61.6 ✓

80+70

62.8 ✓

81+15

65.4

81+25

66.0

81+30

66.3

82

70.3 ✓

83

74.3 ✓

83+50

76.3

84

78.3 ✓

84+55

80.6

Sta.	Elev
84+64	80.9
84+75	81.4
84+80	81.6
85	82.4 ✓
85+50	84.4
86	86.3 ✓
86+50	87.9
87	89.4 ✓
87+50	91.1
88	92.7 ✓
88+50	94.5
89	96.3 ✓
89+50	97.7
90	99.0 ✓

FMG	3-6-24	Rd Rect	110.2	L+	X Sect.	R+	(22)
				+1.2 33	-0.6 -1.4 -1.4 +0.7 +1.8 9 12 14 17 33		
				+1.0 33	-0.4 -1.4 -1.4 -1.0 +1.0 9 11 13 15 33		
				+3.4 +2.4 -1.3 -1.3 +0.1 33 27 18 14 14	-0.4 -1.4 -1.4 -1.0 +1.0 9 11 13 15 33		
				+4.8 -1.4 +3.0 -1.1 -1.1 -0.3 33 30 24 16 13 10	-0.3 -1.0 -1.0 -0.6 0.0 11 13 15 17 33		
				+4.8 +4.8 -1.0 -1.0 -0.2 33 28 15 12 9	-0.6 -1.0 +1.0 +0.4 12 16 20 33		
				+2.6 +2.6 +1.0 -1.4 -1.4 -0.2 33 29 21 15 13 10	-0.4 -1.4 -1.4 +1.0 +1.6 11 14 17 20 33		
				+3.4 +2.0 -1.2 -1.2 +0.1 33 25 16 13 10	-0.6 -0.6 +0.4 -1.4 13 16 18 33		
				+0.4 -1.2 -0.2 33 15 9	-0.3 -1.1 -1.3 +0.5 +0.6 0.0 11 13 16 19 28 33		
				-1.6 -1.6 -1.3 -0.4 33 29 14 11	0.0 -0.6 -0.6 +0.3 -2.0 11 13 15 18 33		
				-1.3 -1.3 +0.1 33 30 9	-0.4 -1.0 -1.6 -2.6 11 13 27 33		
				-0.6 -0.6 -1.3 -0.1 33 29 12 8	-0.2 -1.9 -2.0 -3.0 11 14 27 32		
				+0.4 0.0 -1.4 -1.4 -0.5 33 21 14 12 9	0.0 -0.6 -0.8 11 25 33		
				+2.8 +2.0 0.0 33 29 10	-0.2 -0.6 -0.6 0.0 -0.2 10 13 15 20 33		
				+1.0 +6.1 -6.9 -1.2 -0.9 33 28 17 14 12	-0.2 -1.0 -1.0 +2.1 11 12 16 31		

Sta.
90+50

Elev.

299.9

91

300.8

✓

91+50

301.2

92

01.5

✓

92+50

01.3

93

01.2

✓

93+50

01.4

94

01.6

✓

94+50

01.8

95

01.9

✓

95+50

01.8

96

01.8

✓

96+50

01.9

97

02.0

✓

Lt.

Xsect.

Rt.

+9.5	-0.4	-1.0	-1.0	-0.5	-1.0	-0.3	+1.4	+7.5
31	18	13	12	12	14	18	28	33

+9.2	+0.8	-0.5	-0.9	-0.8	0.0	+8.2	+8.7
32	22	16	12	12	17	29	33

FMC
3-6-24
Rt. Rect. No. 2

+13.5	+0.2	-0.8	-0.3	+0.2	+7.1	+7.1
41	23	16	14	16	26	33

+6.0	+0.5	-0.6	-0.4	-0.8	+0.9	+0.4
35	27	17	12	18	23	31

-0.5	-0.4	-0.8	-0.8	-0.4	-0.5	-1.1	-2.2	-5.4
33	18	17	14	11	13	19	24	31

-0.4	-0.8	-0.4	-0.3	-1.2	-2.2	-7.0
33	13	10	13	14	23	31

-0.7	-1.0	-0.5	-0.6	-1.7	-1.7	-1.2	-1.2
33	14	11	10	13	21	29	33

-2.0	-1.0	-1.0	-1.4	-0.7	-0.4	-0.8	-0.8	+3.1	+4.3
33	29	19	15	11	10	12	14	24	31

0.0	0.0	-1.2	-1.2	-0.4	-0.3	-0.6	-0.4	+3.8	+4.2
33	18	16	13	10	12	14	18	27	31

+4.3	+0.9	-0.7	-0.7	-0.5	-0.6	-0.9	-0.9	0.0	+2.2	+2.3
33	20	16	14	12	11	13	15	18	29	33

0.0	-0.8	-1.4	-0.5	-0.9	-1.0	0.0
33	17	15	11	12	14	30

+1.4	0.0	-0.3	-0.3	-0.7	-0.6	-0.3	0.0	-1.5
32	12	9	9	12	15	16	24	32

0.0	+0.7	-0.2	-0.6	-0.2	-0.4	+1.0	+1.2
33	31	12	10	10	15	18	30

-0.8	-1.0	-0.4	-0.6	-0.4	+0.9	+2.3
33	14	18	12	16	19	29

Sta	Elev
97+50	01.9
98	01.9 ✓
98+50	02.1
99	02.2 ✓
99+50	02.2
100	02.1 ✓
100+50	01.9
101	01.7 ✓
101+50	01.3
102 ✓	01.0 ✓
102+50	00.4
103	99.8 ✓
103+50	99.1
104	98.3 ✓

Lt. X Sect. 1st

-1.8 -1.3 -0.5 -0.2 -0.6 -10.4 +3.0
32 14 10 10 16 18 33

-1.2 -0.7 -0.2 -0.3 -0.4 +0.3 -0.6 -10.4
32 14 11 12 12 16 22 33

-1.7 -1.5 -0.7 -0.3 -0.8 -1.6 -0.8
33 15 12 11 17 26 31

00 -1.2 -0.3 -0.5 -1.0 -2.4 -1.0 -0.6
33 17 11 13 14 23 28 33

+0.4 00 -0.2 -0.4 -0.4 +0.3 00 +1.0
33 17 11 11 15 16 22 28

-4.0 -0.8 -1.8 -1.8 -1.3 -0.7 -0.3 -0.7 00 00
33 26 19 15 13 10 11 15 18 33

-2.5 +0.7 -0.6 -1.2 -0.7 -0.3 -0.8 -0.6 +1.8 +3.4 +3.2
34 28 21 14 11 13 15 19 22 30 33

+2.8 +3.0 +0.4 -0.4 -0.4 -0.3 -0.8 +1.0 +4.6 +4.8 +4.3
33 26 16 15 10 13 15 19 23 30 33

+6.2 +2.2 +0.3 -0.5 -0.7 -0.8 +0.2 +4.4 +3.8
35 22 15 11 13 15 18 24 33

+3.4 +2.3 -0.4 -0.5 -1.5 +0.6 +4.8 +6.1
34 25 15 12 13 18 25 33

+1.4 +1.2 -0.5 -0.7 -0.4 -1.0 +5.0 +7.7 +7.7
33 24 17 12 12 15 24 28 33

+4.5 +5.0 +0.8 -0.3 -0.4 -0.2 +8.9 +9.0
34 25 18 13 13 16 29 33

+0.6 +1.7 -0.7 -1.0 -0.5 -0.6 -1.2 -1.0 +3.2 +3.8
33 21 17 14 11 12 16 19 28 31

-4.0 -4.0 -1.6 -1.0 -0.1 -0.4 -1.2 -1.8 -8.0
33 30 24 15 12 10 16 26 33

FMC
3-6-2K
Pd. Hect 11022

Sta

Elev.

104 + 50

97.9

105

97.4

✓

106

96.8

✓

106 + 50

96.0

107

95.3

✓

108

94.1

✓

108 + 70

93.3

109

92.9

✓

109 + 65

92.9

110

92.9

✓

110 + 50

94.1

111

95.3

✓

111 + 50

96.6

112

97.8

✓

LA Xsect. RA

(25)

-4.3 -4.2 -1.7 -1.0 -0.4
33 26 21 14 12
+0.8 -2.0 -1.8 -0.5
33 18 15 10

-0.3 -10.1 -10.9
10 29 33
-0.4 -6.0 -6.7 -8.8 -10.5
11 21 25 29 34

+6.3 +6.2 +1.3 -0.3 -0.3 00
33 25 18 14 12 11

-0.7 -1.8 -3.5 -7.0
11 14 23 32

+5.0 +5.0 -0.4 -0.2
33 25 16 12

-0.3 -0.8 -0.4 -3.4 -4.2
10 15 16 32 32

+2.5 +1.8 -0.4 -0.3
33 24 18 12

-0.2 -0.4 -0.5 -2.4
10 13 16 32

-1.8 -1.8 -1.2 -0.3
33 20 15 12

-0.4 -2.2 -3.7 -4.6
10 16 24 32

-1.4 -0.6 -0.2
33 14 12

-0.4 -3.4 -5.0 -5.5
11 19 26 34

-2.2 -1.2 -0.3
33 14 11

-0.7 -3.1 -4.8 -5.0
12 18 26 33

-5.0 -4.8 -3.8 -0.4
31 24 18 10

-0.4 -2.5 -5.0 -6.0
12 18 28 32

-3.8 -3.4 -1.2 -0.6
33 25 14 10

-0.6 -2.2 -4.3 -5.0
11 18 25 33

+2.4 +2.8 -1.8 -1.8 -0.6
33 24 17 15 11

-0.6 -1.4 -1.7 -1.3 -1.7
12 16 26 27 33

+5.5 +4.5 -0.6 -1.0 -0.7
33 25 16 12 11

-0.3 -0.7 -0.4 -0.6
12 20 22 33

+2.0 +1.3 -0.8 -0.7 -0.3
34 20 18 13 10

-0.6 -1.6 -1.2 -1.2 +0.4 -1.2
12 16 19 25 28 33

-2.2 -2.2 -1.1 -0.3
33 19 11 10

-0.7 -2.0 -3.2 -3.2 -2.4 -3.3
12 17 23 25 28 36

Sta

Elev.

112 + 50

99.6

~~112 + 50~~

113

301.5 ✓

114

05.5 ✓

115

09.8 ✓

115 + 50

12.2

+24 +24
33 31

116

13.6 ✓

117

17.9 ✓

118

21.5 ✓

119

23.3 ✓

120

23.1

Sta 120 + 51

Iron pipe 22 ft. 2 ft.

121

22.0

121 + 50

20.9 ✓

122

19.6 ✓

122 + 50

18.5

~~Sta~~

Elev

123

17.4 ✓

123+50

16.4

124

15.3 ✓

125

13.2 ✓

126

11.3 ✓

127

09.2 ✓

127+70

08.1

128

07.6 ✓

128+50

07.5

129

07.5 ✓

129+50

07.7

130

07.8 ✓

131

07.9 ✓

Lt X Sect. Rr

27

-1.4 -1.4 -0.4
33 27 10

-0.8 -1.7 -2.4
12 16 33

+2.6
33

+1.0 +1.0 -1.0 -1.0 -0.4
33 19 14 12 10

-0.6 -0.6 +0.8 +0.6 +2.0
13 18 21 24 28

+4.0 +4.0 0.0 -1.0 -1.0 -0.6
33 22 18 14 12 11

-0.3 -3.0 +3.4 +5.4 +6.0
11 16 22 28 33

+6.5 +6.5 +1.2 -0.5
33 26 15 13

-1.5 -1.0 +6.4 +6.4
13 18 24 33

+0.5 0.0 -1.0 -1.4 -1.4 -0.4
33 21 17 16 13 10

-0.7 -1.7 -2.2 -0.8
13 16 21 30

-8.0 -7.0 -0.5
33 25 11

-0.4 -4.0 -5.0
12 22 33

-8.4 -7.0 -0.1
33 26 11

-0.5 -2.6 -7.0 -7.4
12 19 28 33

-7.7 -7.7 -0.7
33 26 12

-0.5 -2.2 -6.0 -6.2
12 18 24 33

-8.0 -6.5 -0.8
33 22 12

-0.6 -2.2 -3.5 -1.5 -1.5
12 17 21 27 33

-5.4 -6.5 -0.7
33 22 12

-0.6 -1.5 -1.5 0.0
12 13 24 33

-7.0 -6.0 -5.0 -0.5
33 26 19 10

-0.6 -1.0 -0.5 +1.0 +2.4
12 14 18 23 35

+1.5 +3.4 0.0 -0.6
34 21 16 10

-0.6 -0.2 +7.0
12 18 30

+12.4

36 +0.8 -0.5 -0.6
22 18 12

-0.6 -1.0 -1.0 +13.0
12 16 20 38

Sta.

Elev.

131+60

08.3

132

08.5 ✓

132+50

08.4

133

08.4 ✓

133+10

08.4

133+50

08.6

133+67 ~~5~~

~~5~~ 08.7 ✓

Lt

X sect.

Rt.

(28)

+ 12.6

35

-0.4

19

-0.6

13

-0.6

12

-0.7

16

-0.7

18

+14.6

39

+6.4

33

+7.4

28

-0.7

16

-1.1

11

-0.3

10

-1.5

20

+11.2

35

+0.8

35

+1.7

18

-0.8

14

-0.2

10

-1.0

17

+1.0

26

+6.0

35

-3.5

34

-2.6

23

-0.8

13

-0.3

12

-0.8

28

+0.8

34

-3.5

34

-2.6

23

-0.8

13

-0.3

12

-0.8

28

-1.2

36

-4.0

45

-1.3

21

-0.5

15

20

14

-0.5

28

-2.5

39

-1.5

33

-0.3

34

on pavement.

Sta.

LATITUDE & DEPARTURE CHART

Proj. Road #24 From White Bear & Lake Phalen Rd. - To East Co. Line Rd. -

STA.	DIST.	Deflection		COURSE	Latitude		Departure		TOTALS	
		L.	R.		+ N	- S	+ E	- W	Latitude	Departure
0+00										
	81.3 ✓			S 13° 01' E.	79.21 ✓	18.31 ✓				
0+81.3		25° 20'							-79.21 ✓	18.31 ✓
	350.1 ✓			S 38° 21' E	274.56 ✓	217.22 ✓				
4+28.7		51° 24'							-353.77 ✓	235.53 ✓
	1548.3 ✓			S 89° 45' E	6.75 ✓	1548.28 ✓				
19+62.0		42° 50'							-360.52 ✓	7783.81 ✓
	474.6 ✓			S 46° 55' E.	324.18 ✓	346.62 ✓				
24+25		57° 33'							-684.70 ✓	2130.43 ✓
	581.8 ✓			N 75° 32' E	145.35 ✓	563.35 ✓				
29+71.9		53° 36'							-539.35 ✓	2693.78 ✓
	1857.1 ✓			N 81° 08' E	286.25 ✓	1834.9 ✓				
48+28.8		37° 00'							-253.1 ✓	4528.68 ✓
	501.7 ✓			S 61° 52' E	236.57 ✓	442.42 ✓				
53+21.3		20° 45'							-489.67 ✓	4974.10 ✓
	859.7 ✓			S 82° 37' E.	110.48 ✓	852.57 ✓				
61+78.0		56° 40'							-600.15 ✓	5823.67 ✓
	522.26 ✓			S 25° 57' E	469.64 ✓	228.55 ✓				
66+78.4		29° 20'							-1069.79 ✓	6052.22 ✓
	413.0 ✓			S 55° 17' E.	235.21 ✓	339.47 ✓				
70+82.9		24° 40'							-1305.00 ✓	6391.69 ✓
	329.6 ✓			S 30° 37' E	283.65 ✓	167.86 ✓				
74+08.4		41° 00'							-1588.65 ✓	6559.55 ✓
	365.7 ✓			S 71° 37' E	115.33 ✓	347.04 ✓				
77+61.7		71° 26'							-1703.98 ✓	6906.59 ✓
	71.9 ✓			S 00° 11' E.	71.9 ✓	0.23 ✓				
78+08.85									-1775.88 ✓	6906.82 ✓

Comp. { M.W. C.
C.A. O.
✓ N.D.C.

Sta. 133+67 $\pm$ to 257+02 $\frac{6}{6}$

E County Line Road

Mar. & Apr. 1924

F. M. Conner

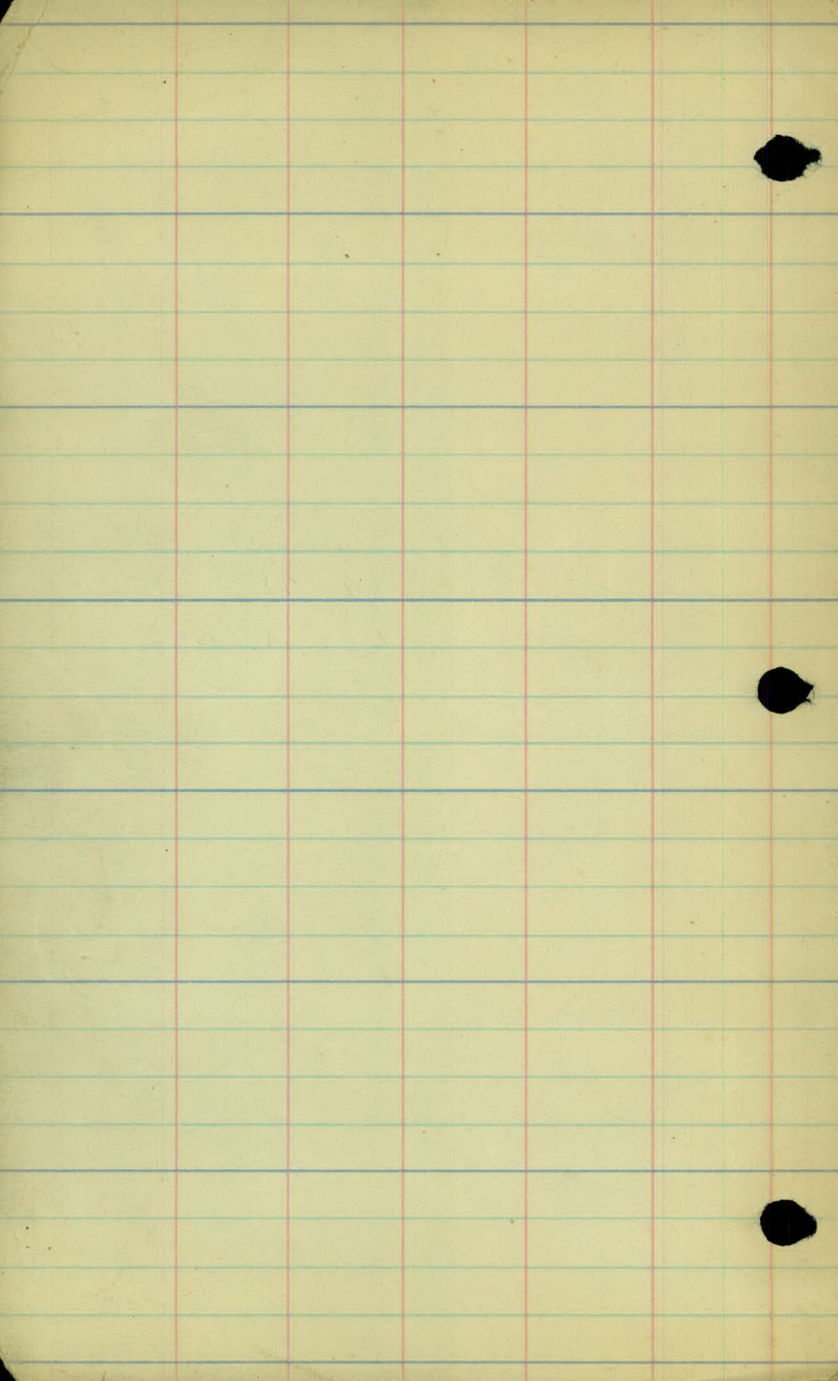
H. H. Wilshusen

Joe Mahoney

E. J. Keogh.

⁴
INDEX

± Align.	Page	(2)	to	(6)
Art. Topog.	✓	(7)	✓	(28)
± Levels	✓	(29)	✓	(42)
X Sect.	✓	(43)	✓	(65)



Align Notes
E. Co. Line & Road.

Sta Point Lt Δ Rt Cule

~~210+56.6 P.T. = 210+58.0~~

~~5.41°42'E.~~

~~+57.3 PT~~

~~20-30~~

~~+50~~

~~19-27 1/4~~

~~PI = 209+89.0~~

~~+25~~

~~15-52 1/4~~

~~$\Delta = 41^{\circ}00'$~~

210+00

12-17 1/2

~~$D = 28-39'$ Lt~~

+75

8-42 1/2

~~$T = 74.8$~~ 75.5

+50

5-07 3/4

~~$L = 143.1$~~

+25

1-33

~~$R = 200$~~ 202.1

~~209+18.5 P.C.~~

~~209+14.2 P.C.~~

209+89 (M.C.) PI 41-00

197+00 POT

5.0°42'E.

44.35
186+43.4 P.I. 0°01'

5.0°41'E.

160+05.8 ^{PI} Mont

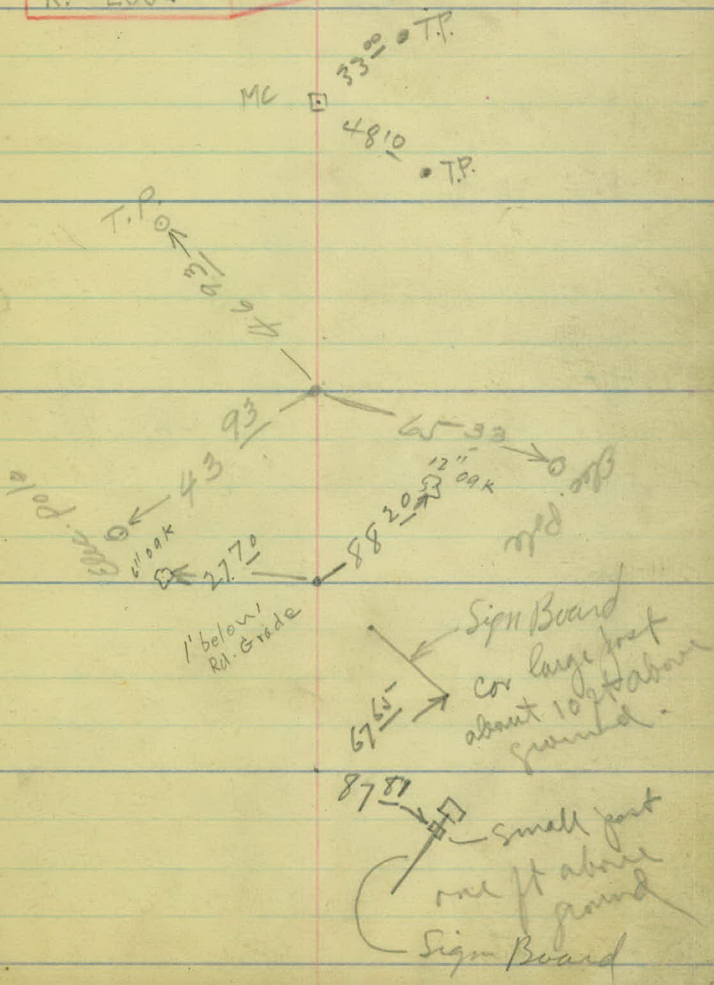
0°02'

5.0°43'E.

133+67.2 PI 0°13'

5.0°36'E.

11.8+ POT

$R_s = 200\Omega$ 

S/A Point L+ Δ R+ Calc

5.2°48'W

214+73.3✓

22-00

~~215+45.3✓ P.T.~~

~~+25~~

~~215~~

~~+75~~

~~+50~~

~~214 +25~~

~~213+99.4✓ P.C.~~

~~211+56.7~~

11-00✓

9-27 1/4 PI=214+73.3

7-34 $\Delta=22-00$

5-41 D=15°05' R+.

3-49 T=73.9✓

1-55 3/4 L=145.9✓

00 R=380°381°

519°12'E.

22-30

~~212+27.9✓ PT~~

~~212~~

~~+75~~

~~+50~~

~~+25~~

~~211~~

~~210+83.4✓ P.C.~~

11-15✓ PI=211+56.7

9-03 1/2 $\Delta=22-30$ R+.

7-06 3/4 D=15°34'

5-10 T=73.3✓

3-13 1/4 L=144.5✓

1-17 1/2 R=368°369.2

00

5.41°42'E.

(4)

214+73.3 PI $68^{\circ}20'$ O.T.P.

7600  Bath house

P.I. 214+73.3

Δ . $22^{\circ}-00'$

D. $15^{\circ}07'-R.$

T. 73.9'

L. 145.0'

R. 380.0'

P.C. 213+99.4

P.T. 215+44.4 = 215+45.3

Correct Curve Datum

211+56.7 PI $91^{\circ}10'$ O.T.P. $\rightarrow 10''$ oak.

$75^{\circ}40'$

O.T.P. Correct Curve Datum

P.I. 211+56.7

Δ . $22^{\circ}30'$

D. $15^{\circ}37'-R.$

T. 73.2'

L. 143.6'

R. 368.0'

P.C. 210+83.5

P.T. 212+27.1 = 212+27.8

Sta Point Lt Δ Rt Calc

50°41'E.

220+302 PI 36-59

221+216 P.T. = 221+227 ✓

~~+227³ PT 18-29 1/2~~

221 16-21 1/2 PI = 220+302

+75 13-58 1/2 $\Delta = 36-59'$

+50 11-29 1/2 $D = 19-25' Lt$

+25 9-03 1/2 $T = 198.7$ 99.1

220 6-37 1/2 $L = 190.4$ 190.5

+75 4-11 1/2 $R = 295.0$ 296.5

+50 1-45 1/2

219+319 P.C. 00

536°18'W

217+054 PI

33-30

218+132 PT

16-45 ✓

218+022 P.T. =

15-44

218

+75 13-51 PI = 217+054

+50 11-58 $\Delta = 33-30$

+25 10-05 $D = 16-45 Rt$

217 8-12 $T = 114.37$ 103.3

+75 6-19 $L = 224.17$ 200.0

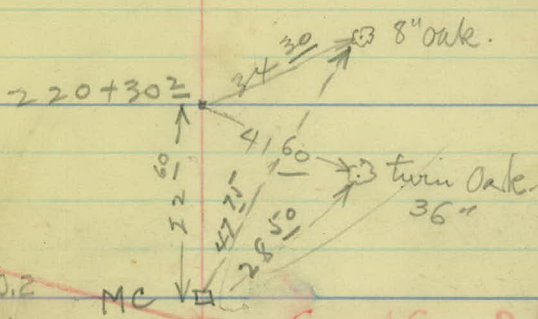
+50 4-26 $R = 380.0$ 343.3

+25 2-33

216 0-41

216+022 P.C. 00

52°48'W.



P.I. 220+30.2
 Δ . $36^{\circ}59'$
 D . $-19^{\circ}31' L$.
 T . $-98.7'$
 L . $-187.2'$
 R . $-295.0'$

MC

P.C. 219+31.5
 $P.T. 221+18.7 = 221+22.3$

Correct Curve Datum

+6.00 15" oak

P.I. 217+05.4

88 90

P.I. 217+05.4
 Δ . $33^{\circ}30'$
 D . $15^{\circ}07' R$.
 T . $114.4'$
 L . $219.1'$
 R . $380.0'$

P.C. 215+91.0
 $P.T. 218+10.1 = 218+13.2$

Correct Curve Datum

Sta Point Lt. Δ Pt. Calc

{ 137+91⁴ End of Proj 23-54
{ 257+02⁶ End = PT of Pavement.

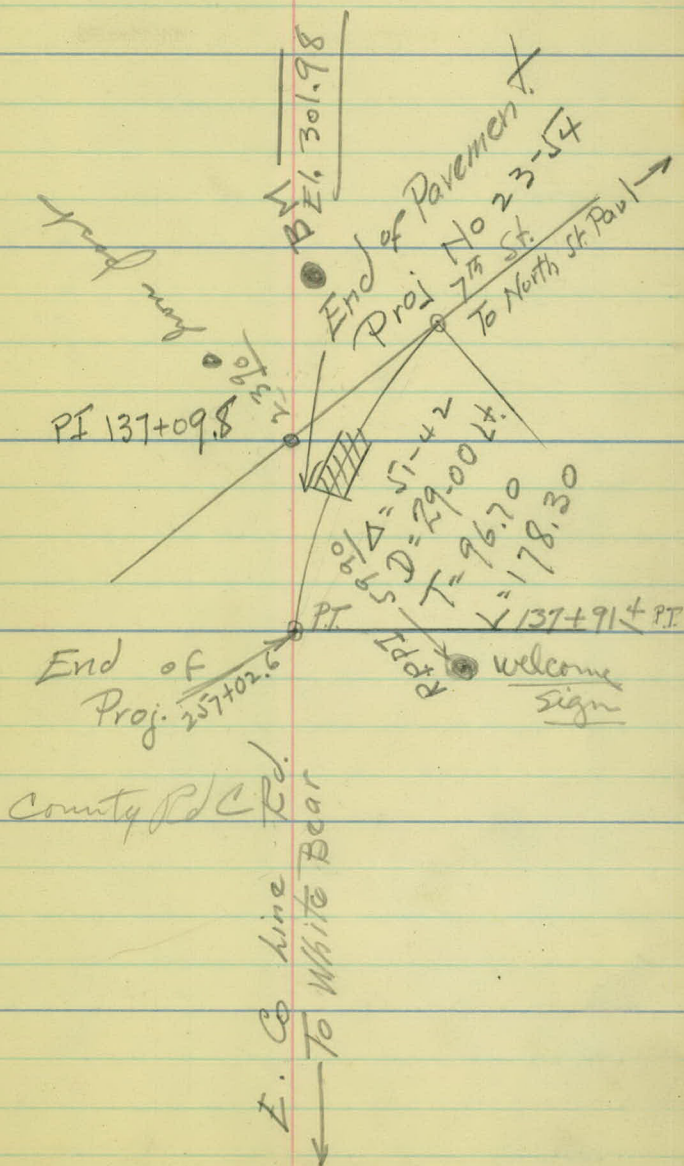
247+06³ $\frac{1}{2}$ Svc Line 50°48'E.

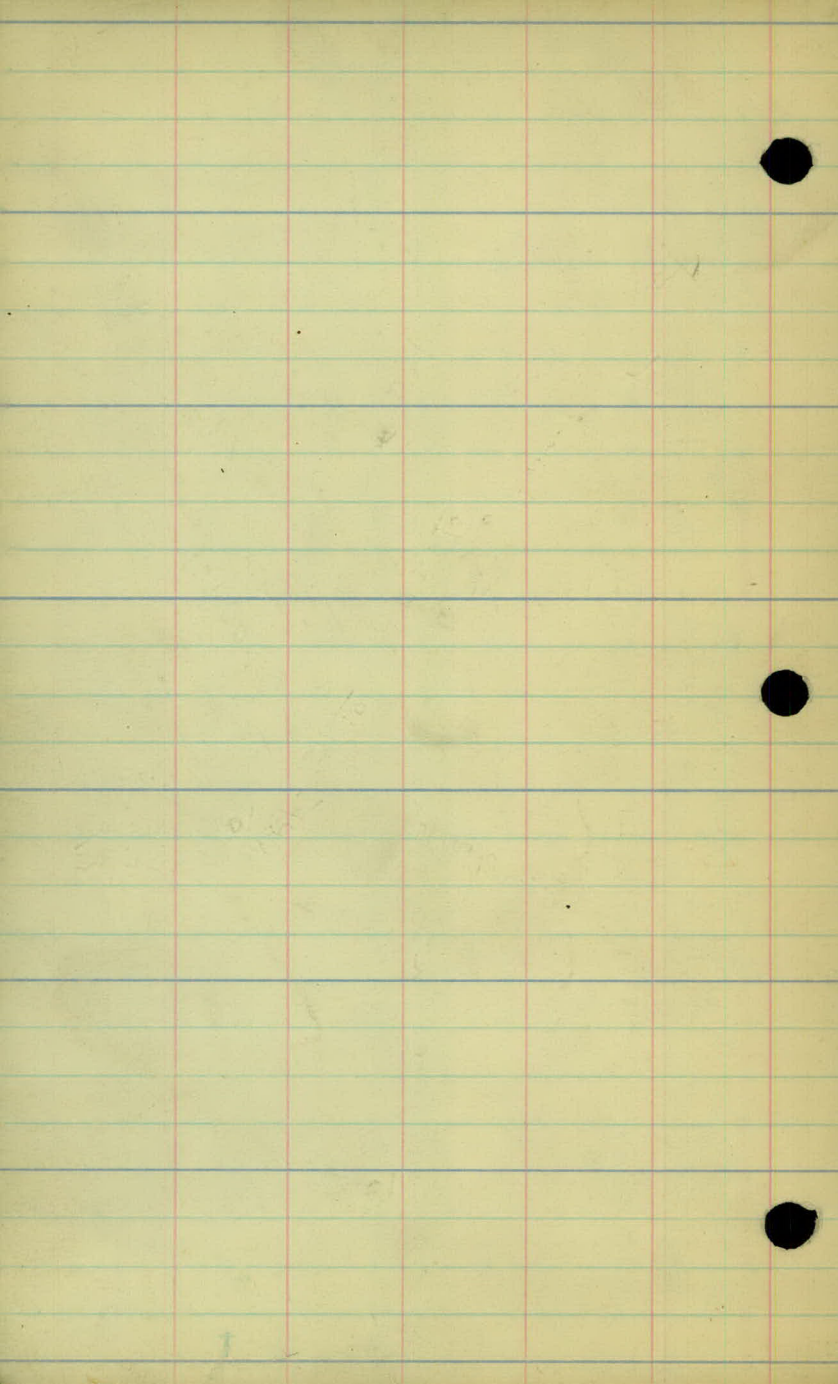
240+60⁶⁵ 0-07'

236+95⁵ $\frac{1}{2}$ st car tracks

50°41'E.

⑥





①

$$PI = 209 + 89.0$$

$$\Delta = 41 - 00 \text{ Lt.}$$

$$T = 74.78$$

$$D = 28 - 39$$

$$L = 143.11$$

$$R = 200$$

$$\text{tang} = 26.12$$

mc #6

$$\begin{array}{r} 74.78 \\ 26.12 \\ \hline 73.29 \\ 174.19 \end{array}$$

$$\begin{array}{r} 210 + 83.4 \text{ PC} \\ 73.3 \\ \hline 211 + 56.7 \text{ PT} \end{array}$$

$$\begin{array}{r} 209 + 89.0 \\ 74.8 \\ \hline 209 + 14.2 \text{ PC} \\ 1 + 43.1 \end{array}$$

$$\begin{array}{r} 210 + 57.3 \text{ PT} \\ 26.1 \\ \hline 210 + 83.4 \text{ PC} \\ 1 + 44.5 \end{array}$$

$$\begin{array}{r} 212 + 27.9 \text{ PT} \\ 1 + 71.5 \\ \hline 213 + 99.4 \text{ PC} \\ 1 + 45.9 \end{array}$$

$$\begin{array}{r} 215 + 45.3 \text{ PT} \\ 57.8 \\ \hline 216 + 03.1 \text{ PC} \\ 1 + 97.0 \end{array}$$

$$\begin{array}{r} 218 + 00.1 \text{ PT} \\ 1 + 31.4 \\ \hline 219 + 31.5 \text{ PC} \end{array}$$

②

$$PI = 211 + 56.7$$

$$\Delta = 27 - 30 \text{ Rt.}$$

$$T = 73.29$$

$$D = 15 - 34$$

$$L = 144.51$$

$$R = 368.0$$

$$\text{tang} = 17.11$$

$$\begin{array}{r} 73.29 \\ 171.47 \\ \hline 73.86 \\ 318.62 \end{array}$$

$$216 + 03.1$$

$$\begin{array}{r} 213 + 99.4 \\ 73.9 \\ \hline 214 + 73.3 \text{ PT} \end{array}$$

$$214 + 73.3 \text{ PT}$$

$$\begin{array}{r} 73.86 \\ 57.84 \\ \hline 102.30 \\ 234.00 \end{array}$$

$$\begin{array}{r} 216 + 03.1 \\ 1 + 02.3 \\ \hline 217 + 05.4 \text{ PT} \end{array}$$

$$217 + 05.4 \text{ PT}$$

③

$$PI = 214 + 13.3$$

$$\Delta = 22 - 38 \text{ Rt.}$$

$$T = 73.86$$

$$D = 15 - 05$$

$$L = 145.91$$

$$R = 380.0$$

$$\text{tang} = 57.84$$

$$PI = 211 + 05.7$$

$$\Delta = 33 - 00 \text{ Rt.}$$

$$T = 102.30$$

$$D = 16 - 45$$

$$L = 196.97$$

$$R = 342.0$$

$$\begin{array}{r} 102.3 \\ 131.4 \\ \hline 98.7 \\ 332.4 \end{array}$$

$$\text{tang} = 131.39$$

④

GRAVEL PIT DAILY REPORT

NAME OF PIT _____

DATE _____ 192 _____

HELP RECORD

FOREMAN _____	HOURS @ _____	\$ _____
ENGINEER _____	" @ _____	\$ _____
TEAMS _____	" @ _____	\$ _____
LABORERS _____	" @ _____	\$ _____
		TOTAL \$ _____

SUPPLIES

RECEIVED		USED
GAS _____	GALS.	_____ GALS.
OIL _____	QTS.	_____ QTS.
GREASE _____	LBS.	_____ LBS.

REPAIRS

(ENTER REPAIR PARTS IN DETAIL AND NOTE HRS. DELAY IN MAKING REPAIRS)

MATERIAL HAULED FROM PIT

TRUCK NO.	GRAVEL										SAND									
	NUMBER OF LOADS										NUMBER OF LOADS									
1																				
2																				
3																				
4																				
5																				
6																				
7																				
8																				
9																				
10																				
11																				
12																				
13																				
14																				
15																				
16																				
GRAND TOTAL																				

AVERAGE SIZE OF LOAD _____ CU. YDS.

TOTAL GRAVEL REMOVED _____ CU. YDS.

" SAND " " " "

WEATHER _____

FOREMAN _____

(5)

$$PI = 520,430.2$$

$$\Delta = 36-59.47$$

$$T = 98.66$$

$$D = 19-25$$

$$L = 190.41$$

$$R = 295.0$$

mc no 5

1/18

DPT

$$\begin{array}{r} 219+31.5 \\ 98.7 \\ \hline 220+30.2 \end{array}$$

$$\begin{array}{r} Lt \\ \hline 41-00 \\ 36-59 \\ \hline 77-59 \end{array}$$

$$\begin{array}{r} Rt \\ \hline 22-30 \\ 22-00 \\ 33-34 \\ \hline 77-64 \\ 77-59 \\ \hline \end{array}$$

$$0-05 Rt$$

$$0-05 Rt$$

GRAVEL PIT DAILY REPORT

NAME OF PIT _____

DATE _____ 192

HELP RECORD

FOREMAN	_____	HOURS	@	_____	\$	_____
ENGINEER	_____	"	@	_____	\$	_____
TEAMS	_____	"	@	_____	\$	_____
LABORERS	_____	"	@	_____	\$	_____
					TOTAL \$	_____

SUPPLIES

RECEIVED		USED	
GAS	_____ GALS.	_____	_____ GALS.
OIL	_____ QTS.	_____	_____ QTS.
GREASE	_____ LBS.	_____	_____ LBS.

REPAIRS

(ENTER REPAIR PARTS IN DETAIL AND NOTE HRS. DELAY IN MAKING REPAIRS)

MATERIAL HAULED FROM PIT

GRAVEL										SAND												
TRUCK NO.	NUMBER OF LOADS										TOTAL LOADS	NUMBER OF LOADS										TOTAL LOADS
1																						
2																						
3																						
4																						
5																						
6																						
7																						
8																						
9																						
10																						
11																						
12																						
13																						
14																						
15																						
16																						
GRAND TOTAL																						

AVERAGE SIZE OF LOAD _____ CU. YDS.

TOTAL GRAVEL REMOVED _____ CU. YDS.

" SAND " " "

WEATHER _____

FOREMAN _____

Artificial Topog.
E. Co. line Road.

138

137

136

135

134

(8)

R/12

R/12 F/18

R/13

R/14 F/18

+ 86 trees/24
+ 56 trees
+ 48 trees
+ 24 trees

R/12

R/12 F/19

Cultivated

Cultivated

E. Co. line Road

FE

FE

Top of
Co. Post B.M.

+ 91 FC/21

R/10

R/10

← To Wild Wood

Co. Ed. E Par.

+ 90 Iron Sign/21
+ 84 Iron Sign/25
+ 77 - Par. 10
+ 55 v/10

144

143

142

141

140

139

138

9

R/v 7/24

R/12

+63 true/30
+38 true/30
R/V #30

1e/12

+98 km/30
+63 km/30
R/V F/29

$$+68 \text{ FC}/24$$

$$R/1 \checkmark \quad F/2 \checkmark$$

$\frac{1}{2} / 12 \quad \frac{1}{2} / 23$

12/12 F/22

+34 FC/23
P/13

R/12 F/19

p/14

R/13 F/19

R/12

$$R/1 \sim F/8$$

Cultivated

Cultivated

Cultivated

Cultivated

F. O. Line Road.

 $f \in$

F.E.

150

149

148

147

146

145

144

R/12
+98 Pillar 25

+10 Pillar 55
R/12

+92 pillar 32

R/12

R/12

+53 tree 25
R/12

R/12

R/12

R/12

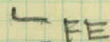
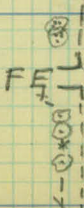
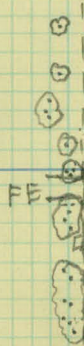
Cultivated

Cultivated

+92 tree 23
+50 tree 25
+36 tree 30
+30 tree 30
+14 tree 20
+98 tree 25
+803 tree 20
+702 tree 20
+60 Mbf 15
+46.2 tree
+30.2 tree
+20.2 tree 20
+13 tree 18
R/12

Buildings

+903 tree 21
+87.3 tree 21
+56 F/35
+44 tree
+37 tree 24
+20 tree 24
R/12 F/12



R/12

R/12

R/12

156

155

154

153

152

151

150

R-12

911. bx. +34/13
911. bx. +32/15
FC
+11. Pillar - 32
R-12 F/33
+50 Pillar - 32
+57 Pillar 47
+47 + Pillar 47
+30. Pillar - 47

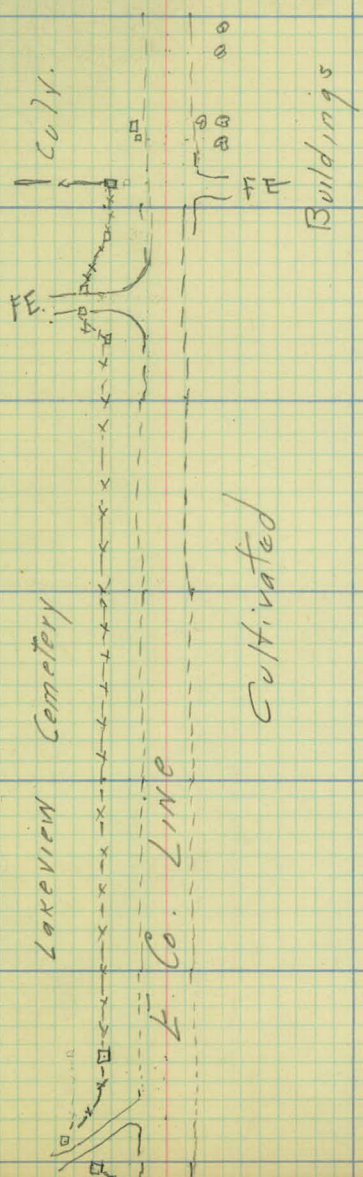
R-12

FL-33-R-12

R-12
FL-33

R-12

+52 Pillar 51
+10. Pillar 55



R-12
+98. tree 27
+72. tree 27
+45³ tree - 21. 30
+32. tree 30

R-10

R-10

R-12

R-12

R-12

162

161

160

159

158

157

156

R-12 7/30

7/23 R-12

R-10 7/27

7/28 R-12

+49 trees / 20
+09 - F.C. 24
R-12

+42 - EC / 32
7/33 R-12

R-12

R-12 - F / 29

R-10

158 trees 28
R-10

+60 End Branch / 15

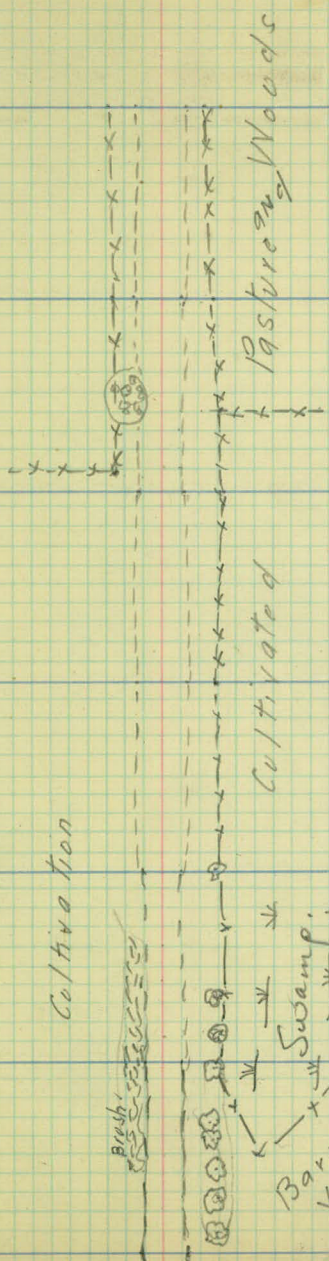
R-10

+36 trees
+15 trees 28
R-10

+51 - Branch / 18

R-12

+97 trees - 28
+77 trees 28
+51 trees 28
+40 trees 28
+26 trees 28
R-12



168

167

166

165

164

163

162

R/12

F/31 R/12

+91 turf F/24

R/12

Colvated

+92 FC/24

+66 Machine shed/31

+53 Machine shed/28

+40 Mgr 12/15 shed.

+37 tur 19

+18 tur 18

+18 barn 49

+95 barn 49

Barn

FE

+59 FC/33

R/12

R/10

+92 FC/33

+92 - 5 tur/33

+61 tur/33

R/14

R/10

+64 tur/33

Buildings

R/10 F/30

F/36 R/10

Pond

R/10 F/24

+59 turf 20

Woods of Pasture

Woods of Pasture

174

173

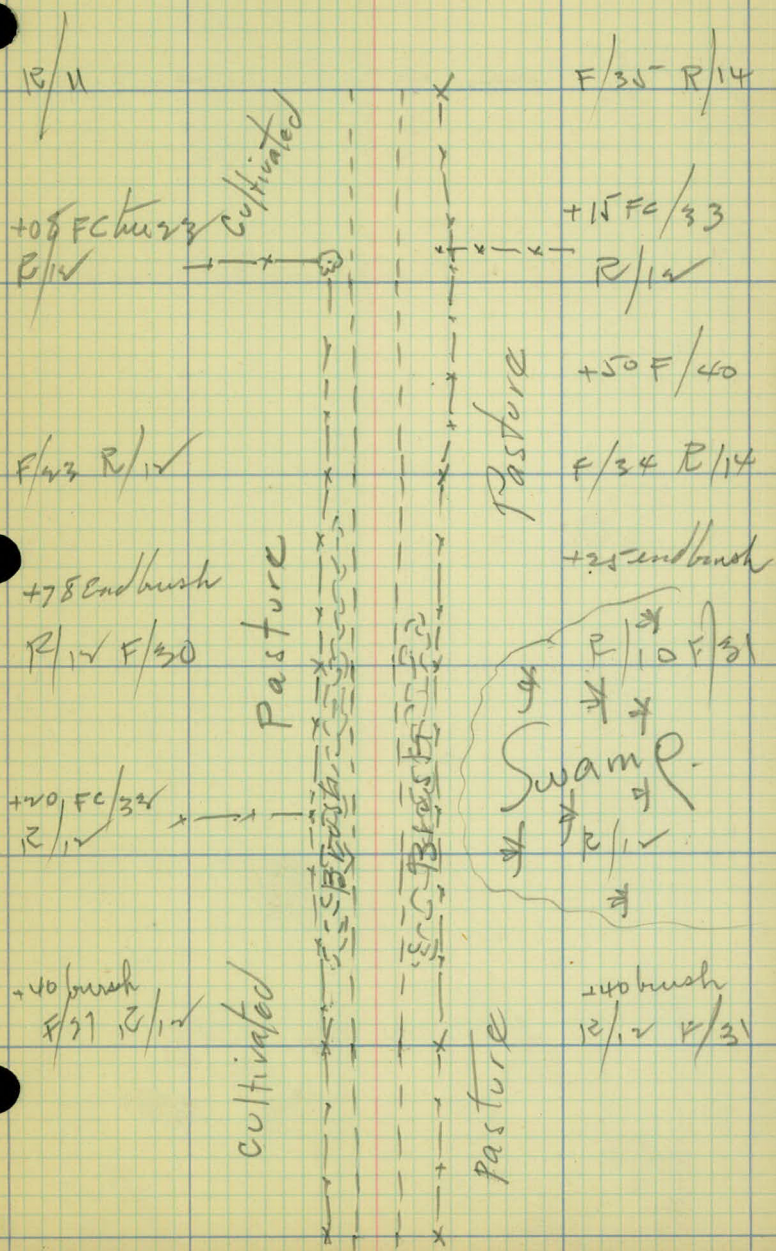
172

171

170

169

168



180

179

178

177

176

175

174

R-10

7/21 R/12

R/11

cultivated

R/11 7/21

R/12

Ref.

cultivated

R/12 7/33

+60.7 c. 21m²

R/12

E. Co. Line

R/12 7/31

R/12

Woods and Pasture

7/37 R/10

R/12

cultivated

R/12. 7/37

R/11

46.4m/31

F/21

186

185

184

183

182

181

180

+90' " " House 75 R/12
 +50' 20' New 33' House
 +23' 31' New
 +8' 20' tree
 R/12 185x100-F.E.
 +16' New
 +80' New

7/27 R/12

7/25 R/12

R/11

7/21 R/12

R/11

7/21 R/11

+30

R/12

7/21 R/12

R/12

7/22 R/12

R/10

7/21 R/12

Garden and Orchard

Cultivated

Cultivated

192

191

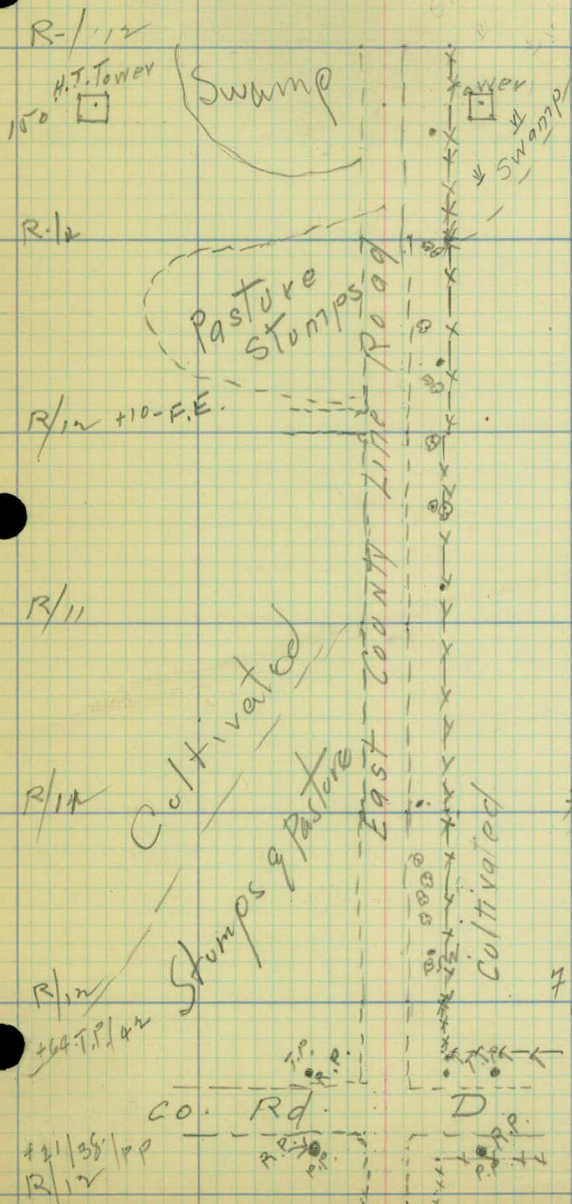
190

189

188

187

186



7/33 R-1/10
 +73/H. T. Tower
 +55/T.P./28
 7/33 R-1/12
 +95-2 trees - 25
 +55-trees - 20
 +34-T.P./30
 +26-2 trees 25
 7/33 R-1/12
 +95-trees 25
 +60-2 trees 25
 +18/T.P./31
 7/33 R-1/11
 +05/T.P./29
 7/33 R-1/11
 +26-T.P./28
 7/31 R-1/12
 +68/70/33
 +64-trees 26
 +61-2 trees 25
 +16/70 T.P.
 7/27 R-1/2

198

197

196

195

194

193

192

R/10

R/15

+80 T.P. / 28

R/10

Swamp

brush

Cultivated

R/17 F/33

R/12

+49 T.P. / 29

Swamp

R/12 F/33

+22 T.P. - 29

R-13

7/33 R-12

R-12

Cultivated

Cultivated

7/33 R-12
+96 T.P. - 29

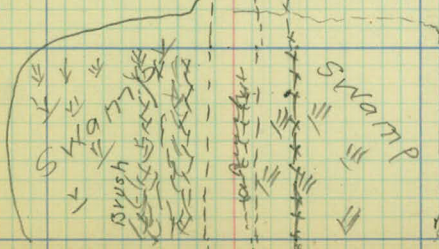
R-12

R-12

+76 T.P. / 28

R-12

7/33 R-10



204

203

✓ 04

201

✓ 00

199

198

R/11 F/27

R/13 F/33

R/10 F/30

Cultivated

Woods

+31 tur 22
R/15 F/36
+95 TP/32
+47 FC/36
+24-3 tur 22
+03 tur 25
E/16

G/10 F/30

FE

Swamp

R/11 F/32

+88 FC/33
+66 T.P. 30

R/15 F/33

+36 FC/24

R/10

Cultivated

Cultivated

+35 TP/28
R/15 F/33

R/10

+06 TP. 29 F/33
R/15

R/10 Swamp

+49 FC/31

R/15 F/33

210

209

208

207

206

205

204

R/13 F/20

R/11 F/17

+52 FC/16

R/10 F/15

R/10 F/20

F/22 R/12

R/14 F/24

R/14 F/24

Swamp

Cultivated

0 danger sign

or R.P.

R/15

+85 MC/15

+93 danger sign 20

+45 T.P. 31

R/14 F/33

+71 TP/27

+36 km 50

R/15 F/34

+70 TP/28

+5 MB/20

R/16 F/23

+80 TP. 29

R/15 F/34

+16 TP. 30

R/13 F/34

+17 TP 30

R/13 F/33

brush

Woods

216

215

214

213

212

211

210

R/1

R/13

R/14

R/12

Cultivated

+86 tree 21
+68 T.P. 34
+44 tree 22
+16-24 tree

R/13
+77 Cor. B. 60
+38 Cor. Bath no. 61
+37 21
+56 tree 22
+19 tree 21
+13 tree 23

R/12

R/12 L/100

+31 mby 14

R/15

FE

R/15

R/15

Pasture

+98 tree 30

+44 tree 32
+08 tree 23 P/12

+88 FC 22

R/15 P/23

Pasture

FE

+94 tree 21
+70 tree
+66 tree 17

+25 T.P. 61 L/80
R/11

+44 T.P. 44

Swamp

R.P.

+10 T.P. 29 L/80

222✓

221

220

219

218

217

216

RR

R/10

F/25 R/25

+14 TP 46
R/12

+02 TP 18
R/12

R/12

end of F 152 1/5
+37 mlt F 17
R/11 F 15

+51 culu 19
+44 F 20 end.
R 12

Orchard.

Orchard

Cultivated

FE LI BM

FE

FE

MC

Summer homes

R/11 F 23

+83 Danger Supn 1/5

+05 MC 34
R/15 F 37

+80 F 46

+5 TP 22

R/12
+90 culu 30
+85 culu 28

+69 culu 3

+61 culu 20

+46 culu 20

R/12

+99 culu 20

+92 culu 20

culu +39-15

+36 culu 15

+30 culu 16

R 11

+58 culu 15

+41 TP 52

+15-3 culu 20

+04 culu 21

12" from
pipe
culu.

FE

Silver

226

227

226

225

224

223

222

23

R/10

+68 Mbx 10
+25 TP 17

R/10

Swamp

R/15

+82 FC/34
+25 FC/33

R/15

+66 FC 23

+91 F 26 R/10

+87 ha 18

+59 cor made 19

+55 trees

+36 Mbx 10

+25 Mbx 9

+10 ha 18

R/10

+05 Mbx 11 TP 100

FE

Concrete wall.

FE

FE

R/15 F/33

+68 F/33
+68 ha 32

F/22 F/34

R/10

+85 TP 20

R/10

+52 TP 24

R/10

Orchard

R/22 F/33

R/22 F/34

R/20 F/25

234

233

232

231

230

229

228

240

239

238

237

236

235

234

(25)

R/15

R/12 Tree 18

+72 tree 17
+52 tree 18
+28 tree 17
R/11 +06 tree 17

+44 cube 16

R/13

+98 Sign 11 R.
+64 TP 16
+60 tree 36
+27 tree 36
+18 tree 30

+65 TP 26
+50 tree 22
+17 tree 23

R/12

+88-5 tree 30
+79 tree 31
+65 tree 29
+56-2 tree 29
+37 Xing 12
+22 TP 15

R/11 +12 tree 30

+83 tree 24
+35 cor. ho. 35

R/11

+62 TP 14
+40 tree 30
R/14

+70 tree 24
+58 tree 24
+51 Xing sign 14

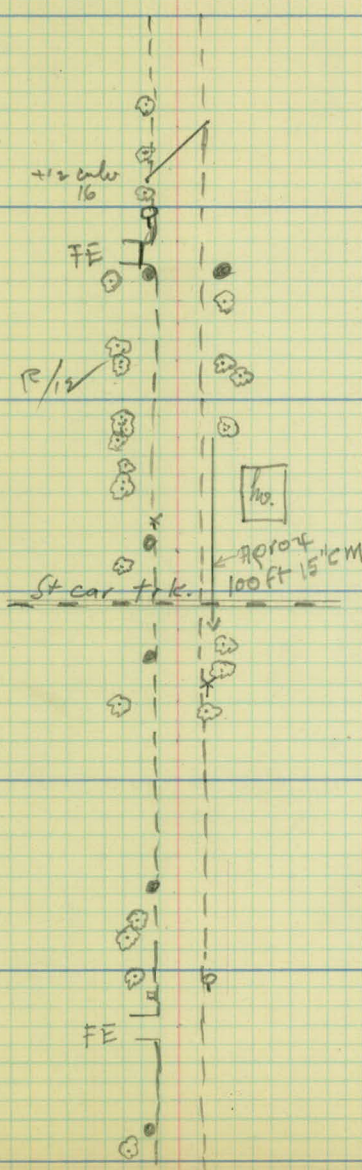
+35 tree 24
R/13

+42 TP 13
+24 tree 21
+17 tree 29
R/14

R/14

+95 tree 21
+87 tree 14
+30 tree 24
+26 tree 24
+17 TP 13
+05 tree 26

+93 dengue sign 14



246

245

244

243

242

241

240

(26)

R/12

R/12

+08 tree 31
R/15
+93 tree 20
+73 tree 32
+66 tree 29
+52 tree 25
+35 tree 28
+07 TP 20
R/15

+75 tree 20
+22 tree 29
+09 RR sign 14
R/13

+93 tree 30
+07 mbr 16
R/13

+28 tree 30
R/17
+75 TP 20

street

+07 sign 12

culv.

R/15

+83 FC 27
+75 tree 21
+63 tree 29 R/12
+58 tree 26
+46 tree 22
+28-3 trees 22
+75 "
+18 tree 21
+10-3 trees 22
+58 tree 26 R/12
+58 FC again 26
+64 tree 33
+44 tree 24
+38 hyl. 33
+25 TP 26
+16 str sign 15

+28 TP 22
R/17
+77 TP 24
+77 tree 35
+19 sign 16 RR
+06 mbr TP 17
+05 tree 21

Co Rd

C

IBM

252

251

250

249

248

247

246

(R7)

R/11

R/13 F23

+45 TP 23

R/13

R/13 F/22

R/14

+98 TP 22
+74 Iron post 13

R/13 F22

+78 mbl 15
+75 mbl 15

R/13

R/13 F/20

+66 mbl 20
+60 mbl 20

F0/38 F/12

2/12 F/39

R/14

+83 F43

+71 F36

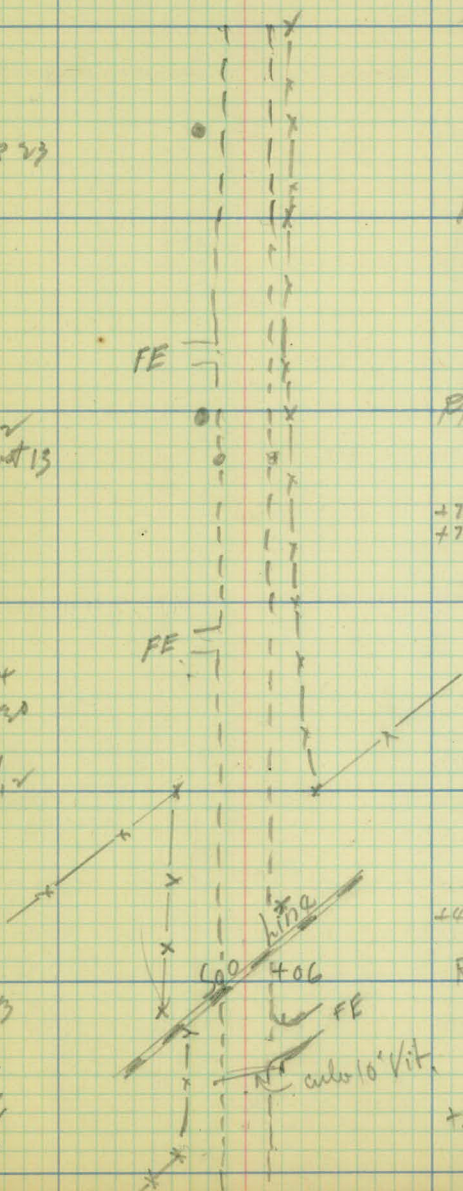
+25 TP 26

+07 F035

+42 Xing Sign 20

R/12

+55 mbl 15



256

257

258

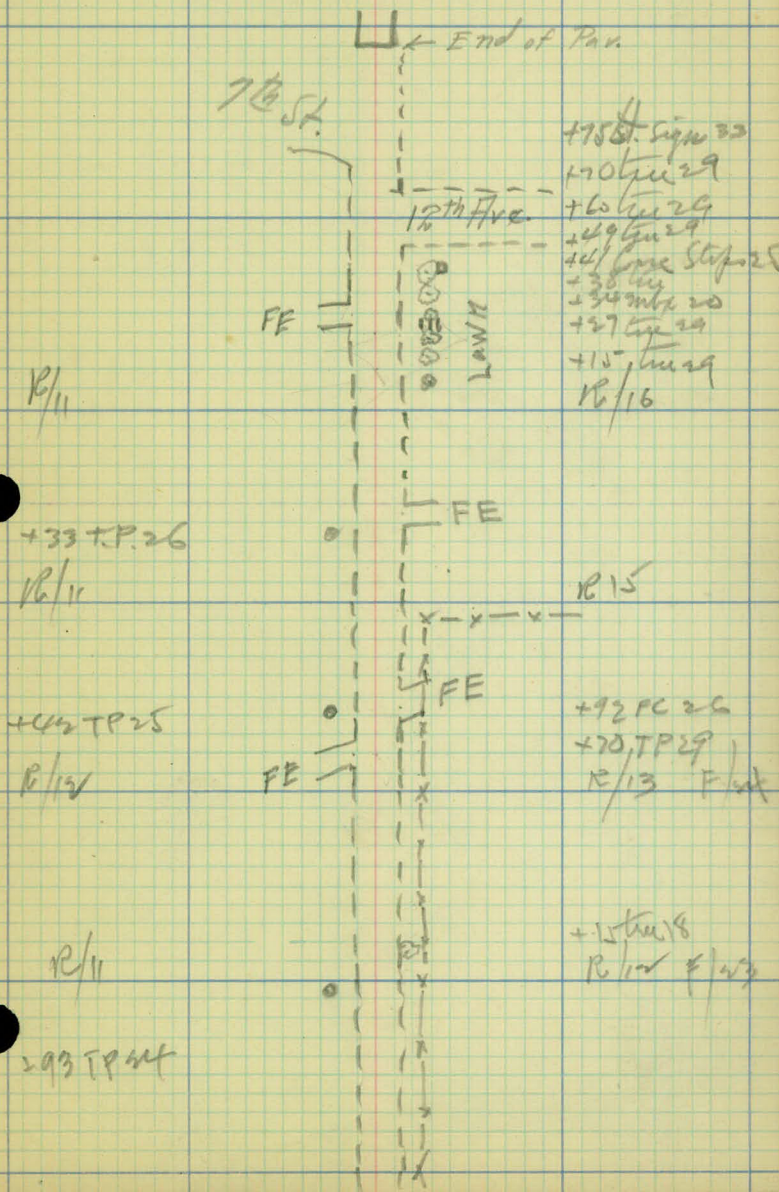
259

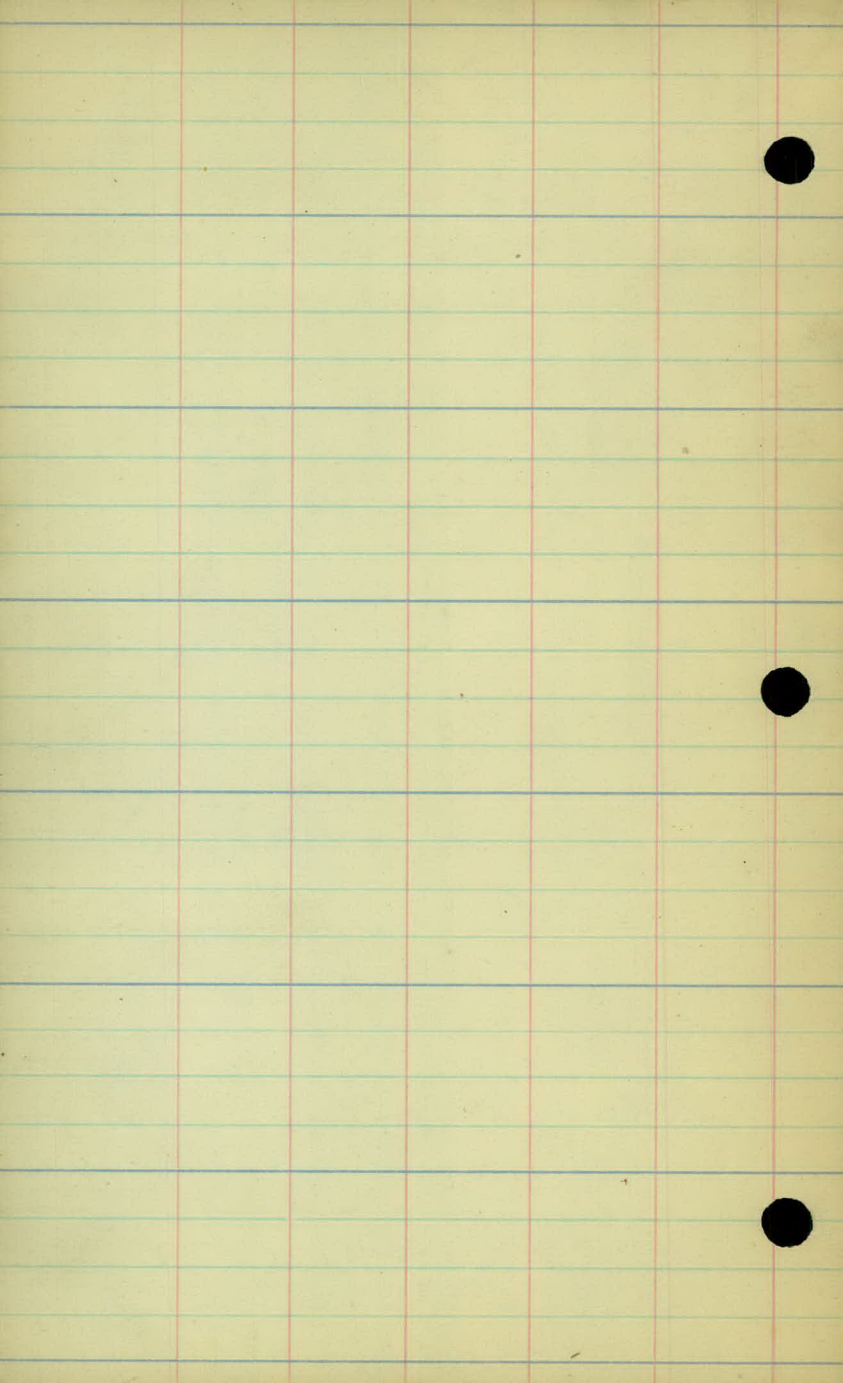
260

261

262

(28)





to levels

E. Co. Line Road.

BM	8.57	313.33 ✓		304.76 ✓
134			4.8	08.5 ✓
+50			5.0	08.3 ✓
135			4.8	08.5 ✓
+50			4.1	09.2 ✓
136			3.3	09.0 10.0
+50			2.2	11.1 ✓
137			0.7	12.6 ✓
T.P.	11.25	323.76 ✓	0.82	312.5 ✓
+50			9.4	14.4 ✓
138			7.9	15.9 ✓
+50			6.2	17.6 ✓
139			4.6	19.2 ✓
+50			2.7	21.1 ✓
140			0.7	23.1 ✓
T.P.	10.88	333.83 ✓	0.81	322.95 ✓
+50			8.8	25.0 ✓
141			6.4	27.4 ✓
+50			4.0	29.8 ✓
142			1.2	32.6 ✓
T.P.	10.69	342.67 ✓	1.85	331.98 ✓
+50			7.2	35.5 ✓
143			4.7	38.0 ✓
T.P.	10.20	349.35 ✓	3.5	339.15 ✓
+50			8.7	40.6 40.7
144			6.0	43.4 ✓
+50			3.8	45.5 45.6

Sta 134 + 90.20 ft Rt top of ltr. F.P.

Sta 133 + 67.5

			<u>tops</u>	<u>m</u>
100 ft RR	07.6	5.7		3/3
50 " "	08.2	5.1		3/3
00 " "		4.9		3/3
50 " Lt	05.5	7.8		3/3
100 " "	02.6	10.7		3/3

1333
 82
 12.51
 11.25
 23.76

349.35

Sta.	+	HI	-	
T.P.	11.33	359.06 ✓	1.62	347.73 ✓
145			11.0	48.1 ✓
+50			8.6	50.5 ✓
146			6.2	52.9 ✓
B.M.			6.94	52.12 ✓
+50			4.4	54.7 ✓
147			2.6	56.4 56.5
T.P.	12.20	368.68 ✓	2.58	356.48 ✓
+50			10.3	58.4 ✓
148			9.2	59.5 ✓
+50			8.1	60.6 ✓
149			7.5	61.2 ✓
+50			7.0	61.7 ✓
150			6.3	62.4 ✓
+50			5.5	63.2 ✓
151			4.7	64.0 ✓
+50			4.0	64.7 ✓
152 ✓			3.9	64.8 ✓
T.P.	2.80	367.47 ✓	4.01	364.67 ✓
+50			3.8	63.7 ✓
153 ✓			5.4	62.1 ✓
+50			6.9	60.6 ✓
154			9.1	58.4 ✓
+50			10.6	57.9 56.9
155			12.0	55.5 ✓
T.P.	0.76	356.24 ✓	11.99	355.48 ✓
+50			2.1	54.1 ✓

R.C. Spike in 12" oak 30 ft Lt Sta 146+00

$$\begin{array}{r} 59.06 \\ 69 \\ \hline 57.17 \end{array}$$

156		356.24 ✓	3.8	52.4 ✓
+50			5.6	50.6 ✓
157			6.7	49.5 ✓
+50			7.6	48.6 ✓
158			8.3	47.9 ✓
+50			9.5	46.7 ✓
159			10.5	45.7 ✓
+50			11.8	44.4 ✓
T.P.	1.94	346.75 ✓	11.43	344.81 ✓
160			3.3	43.4 43.5
+50			4.7	43.0 42.1
BM			4.92 ✓	41.83 ✓
161			5.6	41.2
+50			6.4	40.4
162 ✓			7.3	39.45
+50			8.2 ✓	38.6
163 ✓			8.7	38.0
+50			8.9	37.8
164			8.6	38.2
T.P. 160	3.47	341.62 ✓	8.60	338.15 ✓
+50			3.4	38.2 ✓
165			3.6	38.0 ✓
+50			3.9	37.7 ✓
166			3.9	37.7 ✓
+50			4.3	37.3 ✓
167			4.7	36.9 ✓
+50			5.0	36.6 ✓

160 + 75 - 30 ft Rt. 12" oak R.P. spike

168		341.62 ✓	5.2	36.4 ✓
+50			5.3	36.3 ✓
169			5.7	35.9 ✓
+50			5.9	35.7 ✓
170			6.3	35.3 ✓
+50			6.6	35.0 ✓
171			6.7	34.9 ✓
T.P.	6.00	341.17 ✓	6.45	335.17 ✓
+50			5.8	35.4 ✓
172			5.6	35.6 ✓
+50			5.6	35.6 ✓
173			5.3	35.8 ✓
+50			5.4	35.8 ✓
174			5.2	36.0 ✓
+50			5.0	36.2 ✓
175			4.9	36.3 ✓
+50			4.9	36.3 ✓
176			4.8	36.4 ✓
+50			4.9	36.3 ✓
177			5.2	36.0 ✓
+50			5.3	35.9 ✓
178			5.3	35.9 ✓
T.P.	8.86	344.31 ✓	5.69	335.48 ✓
+50			8.3	36.0 ✓
179			8.1	36.2 ✓
+50			7.6	36.7 ✓
180			6.9	37.4 ✓

180 + 50	344.34 ✓	6.0	38.3 ✓
181		5.4	38.9 ✓
+ 50		4.4	39.9 ✓
182 ✓		4.2	40.1 ✓
+ 50		3.9	40.4 ✓
183 ✓		3.5	40.8 ✓
+ 50		3.4	40.9 ✓
184		3.4	40.9 ✓
+ 50		3.0	41.3 ✓
TP 4.44	345.98 ✓	2.90	341.44 ✓
185		4.4	41.5 ✓
+ 50		4.3	41.6 ✓
186		4.5	41.4 ✓
BM 5.01	345.59 ✓	5.30	340.58 ✓
+ 434		4.2	41.4 ✓
{ 50 Ret. su Cor. ✓		3.7	41.9 ✓
		3.5	42.1 ✓
		5.1	40.5 ✓
		2.4	38.2 ✓
187		5.9	39.7 ✓
+ 50		6.7	38.9 ✓
188		8.4	37.2 ✓
+ 50		9.6	36.0 ✓
189		10.9	34.7 ✓
TP 1.20	335.79 ✓	11.00	334.59 ✓
+ 50		2.9	32.9 ✓
190		4.8	31.0 ✓

BM 187+30-309⁺ Rt. R.R. spike TP.

190 + 50		335.79 ✓	6.5	29.3 ✓
191			8.0	27.8 ✓
+ 50			10.0	25.8 ✓
192 ✓			✓ 12.0	23.8 ✓
T.P.	1.25	325.47 ✓	11.87	323.92 ✓
+ 50			3.0	22.2 ✓
193			3.4	21.8 ✓
+ 50			3.9	21.3 ✓
194			4.5	20.7 ✓
+ 50			5.0	20.2 ✓
195			5.6	19.6 ✓
+ 50			6.1	19.1 ✓
196			6.5	18.7 ✓
+ 50			6.9	18.3 ✓
197			7.6	17.6 ✓
+ 50			✓ 8.5	16.7 ✓
BM	3.98	318.43 ✓	10.72	314.45 ✓
198			2.6	15.8 ✓
+ 50			2.5	15.9 ✓
199			2.5	15.9 ✓
+ 50			2.5	15.9 ✓
200			2.9	15.5 ✓
+ 50			3.5	14.9 ✓
201			4.0	14.4 ✓
+ 50			4.3	14.1 ✓
202 ✓			4.6	13.8 ✓
+ 50			5.1	13.3 ✓

147 + 80 30 Rt. RPSyk. in T.P.

203		318.43 [✓]	5.5	12.9 [✓]
+50			6.0	12.4 [✓]
204			7.0	11.4 [✓]
+50			7.9	10.5 [✓]
205			9.4 [✓]	09.0 [✓]
T.P.	2.53	311.56 [✓]	9.40	309.03 [✓]
+50			3.6	08.0 [✓]
206			4.9	06.7 [✓]
+50			6.1	05.5 [✓]
207			7.4	04.2 [✓]
+50			9.2	02.4 [✓]
208			10.8	00.8 [✓]
+50			12.0 [✓]	99.6 [✓]
T.P.	3.43	303.13 [✓]	11.86	299.70 [✓]
209			4.4	98.7 [✓]
	P.C.		4.7	98.4 [✓]
209+25			4.7	98.4 [✓]
+50			5.2	97.9 [✓]
+75			4.9	98.2 [✓]
210			4.5 [✓]	98.6 [✓]
B.M.			8.3 [✓]	294.81 [✓]
+25			4.3	98.8 [✓]
+50			4.3	98.8 [✓]
	P.T.		4.3	98.8 [✓]
+83.4	P.C.		4.2 [✓]	98.9 [✓]
211			4.2	98.9 [✓]
+25			4.2	98.9 [✓]

210+50 Rt ^{RR} 5 pk. 30 2d Rt.

211	50	303.13	4.1	99.0	✓
	+75		4.1	99.0	✓
	212		4.0	99.1	✓
	P.T.		4.1	99.0	✓
	+50		4.2	98.9	✓
	213		4.1	99.0	✓
	+50		4.1	99.0	✓
	P.C.		4.2	98.9	✓
	+25		4.1	99.0	✓
	+50		4.0	99.1	✓
	+75		3.8	99.3	✓
	215		3.6	99.5	✓
	+25		3.7	99.4	✓
	T.P.	8.35 307.83	3.65	299.48	✓
	P.T.		8.3	99.5	✓
	P.C.		8.0	99.8	✓
	216		7.9	99.9	✓
	+25		7.8	300.0	✓
	+50		7.7	00.1	✓
	+75		7.4	00.4	✓
	217		6.6	01.2	✓
	+25		5.5	02.3	✓
	+50		4.9	02.9	✓
	+75		3.8	04.0	✓
	218		3.0	04.8	✓
	P.T.		2.5	05.3	✓
	+50		1.3	06.5	✓

307.83 ✓

T.P.

10.4 ✓ 317.83 ✓

0.42

307.41 ✓

219

9.5

08.3 ✓

P.C.

8.4

09.4 ✓

+50

8.0

09.8 ✓

+75

7.2

10.6 ✓

220

6.3

11.5 ✓

B.M.

3.25

314.58 ✓

B.M.

6.51

311.32 ✓

+25

5.3

12.5 ✓

+50

4.5

13.3 ✓

+75

4.1

13.7 ✓

221

3.6

14.2 ✓

221 + 223 PT

3.3

14.5 ✓

B.M.

7.40

318.72 ✓

311.32 ✓

+50

3.8

14.9 ✓

222

3.9

14.8 ✓

+50

4.4

14.3 ✓

223

3.2

13.5 ✓

+50

6.4

12.3 ✓

224

8.0

10.7 ✓

+50

9.6

09.1 ✓

225

11.2

07.5 ✓

T.P.

0.40

307.66 ✓

11.46

307.26 ✓

+50

1.7

06.0 ✓

226

3.0

04.7 ✓

+50

4.5

03.2 ✓

240
50
29,000

381

#1008.14 Bm #22 ✓ L.I. B.M. differ - 693.56
35 ft Rt Sta 220 *Rsfk 36 twin lake.

220
2440
60
28600

227		307.66 ✓	5.7	02.0 ✓
+50			6.6	01.1 ✓
228			7.3	00.4 ✓
+50			7.6	00.1 ✓
229			7.7	00.0 ✓
+50			8.1	99.6 ✓
230			8.0	99.7 ✓
+50			8.0	99.7 ✓
231			8.0	99.7 ✓
T.P.	5.80	305.34 ✓	8.12	297.54 ✓
+50			5.5	99.8 ✓
232 ✓			5.1	00.2 ✓
+50			5.0	00.3 ✓
233			5.0	00.3 ✓
+31			4.9	00.4 ✓
{ 50 ft Rt.			5.7	99.6 ✓
	100 ✓ ✓		5.7	99.6 ✓
	50 ft Lt.		6.1	99.2 ✓
	100 ✓ ✓		6.3	99.0 ✓
+50			4.9	00.4 ✓
234			4.7	00.6 ✓
+50			4.5	00.8 ✓
235			4.4	00.9 ✓
+50			4.3	01.0 ✓
236			4.1	01.2 ✓
+50			4.3	01.0 ✓
+92			4.3	301.0 ✓

(39)

sheet 4

North Rail

236+99	305.34 ✓	4.6	300.88 ✓
237		4.4	00.9 ✓
+50		5.3	300.0 ✓
238		5.6	99.7 ✓
+50		6.3	99.0 ✓
239		7.1	98.2 ✓
+50		7.4	97.9 ✓
240		7.5	97.8 ✓
T.P. 5.14	302.54 ✓	7.94	297.40 ✓
Bm		4.86	297.68 ✓
+60		4.4	98.1 ✓
{ 50 ft Lt.		5.8	96.7 ✓
		6.4	96.1 ✓
		4.8	97.7 ✓
		3.6	98.9 ✓
241		4.6	97.9 ✓
+50		4.8	97.7 ✓
242		4.5	98.0 ✓
+50		4.5	98.0 ✓
243		4.4	98.1 ✓
+50		4.3	98.2 ✓
244		4.0	98.5 ✓
+50		3.4	99.1 ✓
245		3.1	99.4 ✓
T.P. 6.77	305.67 ✓	3.64	298.90 ✓
+50		5.7	300.0 ✓
246		5.6	300.1 ✓

Smith Rail

991.17 BM #23

(40)

693.56

297.61

302.54

4.56

297.68

240+25 Rt. 30 ft. T.P. LIBM #23 991.17
Co. Rd C:

246+50	305.67 [✓]	5.2	300.5 [✓]
247+02		4.88	300.79 [✓]
247+07		4.88	300.79
+50		4.8	300.9 [✓]
248		4.8	00.9 [✓]
+50		4.8	00.9 [✓]
249		4.8	00.9 [✓]
+50		4.7	01.0 [✓]
250		4.5	01.2 [✓]
+50		4.7	01.0 [✓]
251		5.0	00.7 [✓]
+50		5.1	00.6 [✓]
252 [✓]		5.3	00.4 [✓]
+50		5.5	00.2 [✓]

T.P. 8.68	308.39 [✓]	5.96	299.71 [✓]
253		7.8	00.6 [✓]
+50		7.3	01.1 [✓]
254		6.5	01.9 [✓]
+50		5.7	02.7 [✓]
255		5.1	03.3 [✓]
+50		4.5	03.8 [✓] 03.9
256		4.4	04.0 [✓]
+50		4.3	04.1 [✓]
257		4.5	03.9 [✓]
257+02.6 P.T.		4.5	03.9 [✓]
+90 End of Row.		5.04	303.35 [✓]

North Rail

On Pavement

308.39 ✓

Bm

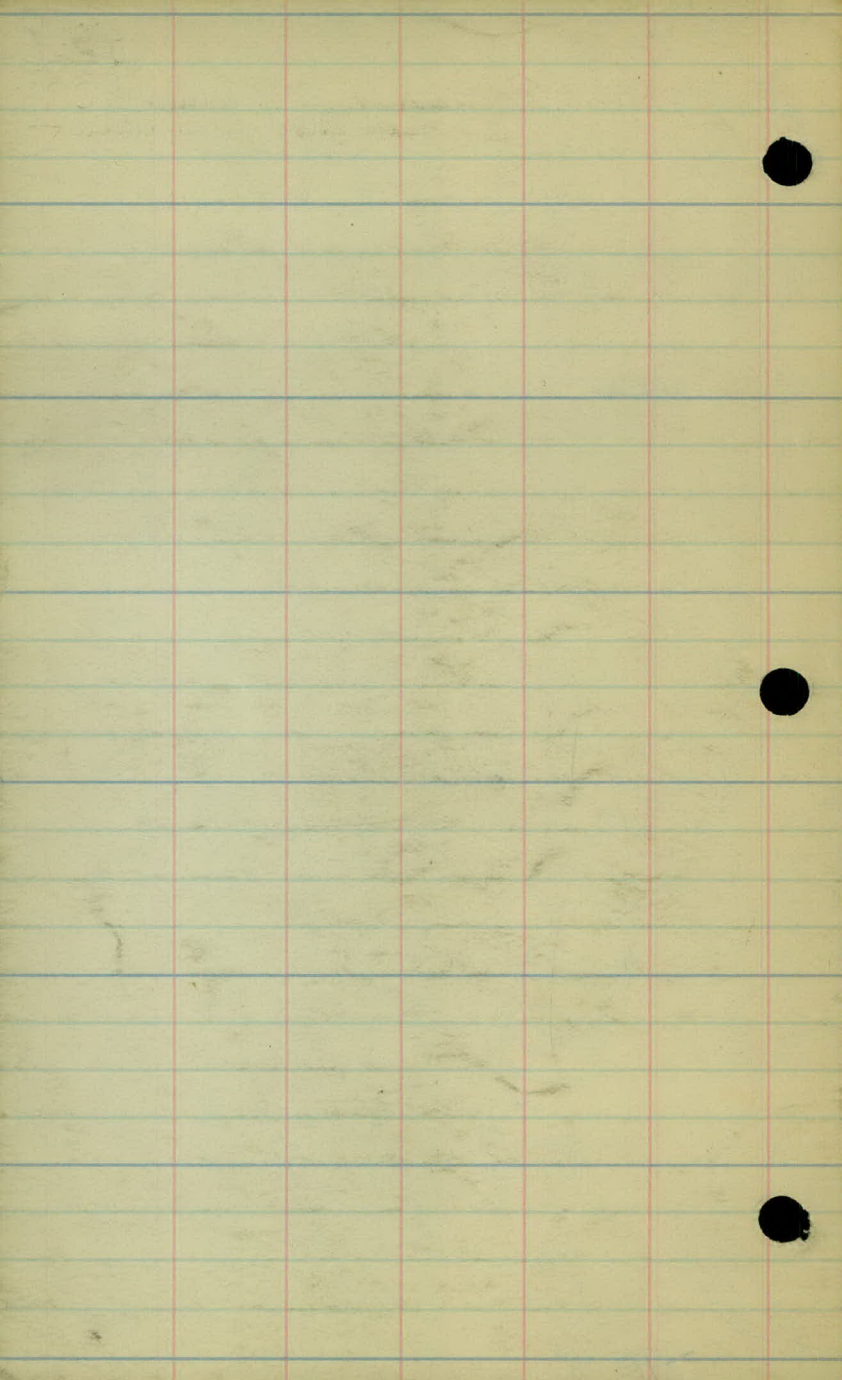
6.36

302.03 ✓

301.98

(42)

B.M. El. 301.98 Marked on P.P. behind G.R. ^{50.}
near end of pavement.



Road # 22

X- Sections
E. Co. Mine Road.

Sta.	surf El.
133 + 75	308.6
134	308.5 ✓
+50	308.3 ✓
135	308.5 ✓
+50	309.2 ✓
136	309.0 ✓ 310.0
+50	311.1 ✓
137	312.6 ✓
+50	314.4 ✓
138	315.9 ✓
+50	317.6 ✓
139	319.2 ✓
+50	321.1 ✓
140	323.1 ✓

Lt.

E

Rt.

(44)

Section same as 153+675

$$\begin{array}{ccc} -7.1 & -1.4 & -1.5 \\ 32 & 19 & 16 \end{array}$$

$$\begin{array}{ccc} -0.4 & -0.5 & -8.0 -8.5 \\ 9.0 & 16 & 31 \quad 33 \end{array}$$

$$\begin{array}{ccc} -9.8 & -5.9 & -1.0 \\ 33 & 25 & 12 \end{array}$$

$$\begin{array}{ccc} -0.7 & -9.0 & -10.0 \\ 11 & 26 & 33 \end{array}$$

$$\begin{array}{ccc} -8.5 & -7.6 & -1.0 \\ 33 & 25 & 13 \end{array}$$

$$\begin{array}{ccc} -0.6 & -0.3 & -8.2 -8.5 -10.0 \\ 8.0 & 10 & 20 \quad 26 \quad 33 \end{array}$$

$$\begin{array}{ccc} -1.1 & -1.1 & -4.6 -4.6 -0.8 \\ 33 & 30 & 24 \quad 17 \quad 12 \end{array}$$

$$\begin{array}{ccc} -0.7 & -0.4 & -3.3 -8.5 -10 -13 \\ 9.0 & 11 & 19.0 \quad 24 \quad 29 \quad 34 \end{array}$$

$$\begin{array}{ccc} -2.3 & -1.6 & -2.5 -2.5 -0.7 \\ 33 & 27 & 24 \quad 14 \quad 11 \end{array}$$

$$\begin{array}{ccc} -0.7 & -0.2 & -2.5 -2.5 +6.7 10.0 \\ 10 & 12 & 17 \quad 23 \quad 32 \quad 33 \end{array}$$

$$\begin{array}{ccc} -6.1 & -5.1 & -3.6 -0.1 \\ 33 & 27 & 16 \quad 12 \end{array}$$

$$\begin{array}{ccc} -0.6 & -1.4 & -1.6 +1.5 +1.5 \\ 12 & 16 & 26 \quad 32 \quad 33 \end{array}$$

$$\begin{array}{ccc} +0.5 +0.5 -1.1 -1.1 -0.5 \\ -1.6 34 & 26 & 22 \quad 19 \quad 15 \quad 11 \end{array}$$

$$\begin{array}{ccc} -0.4 & 0.0 & -2.3 -2.3 10.0 \\ 11 & 12 & 22 \quad 24 \quad 33 \end{array}$$

$$\begin{array}{ccc} -1.0 & +0.2 & 0.0 -1.7 -1.0 \\ 33 & 25 & 20 \quad 18 \quad 12 \end{array}$$

$$\begin{array}{ccc} -0.7 & -2.5 & -2.5 +3.0 +2.8 \\ 11 & 16 & 22 \quad 29 \quad 33 \end{array}$$

$$\begin{array}{ccc} -4.5 & -2.5 & -0.7 \\ 33 & 15 & 11 \end{array}$$

$$\begin{array}{ccc} -0.5 & -0.2 & 0.0 \\ 10 & 18 & 33 \end{array}$$

$$\begin{array}{ccc} -6.2 & -4.5 & -0.7 \\ 33 & 18 & 11 \end{array}$$

$$\begin{array}{ccc} -0.7 & -1.5 & -1.2 \\ 11 & 19 & 33 \end{array}$$

$$\begin{array}{ccc} -1.4 -0.6 & -1.2 & -2.2 -2.2 -0.8 \\ 33 & 28 & 20 \quad 15 \quad 14 \quad 11 \end{array}$$

$$\begin{array}{ccc} -0.7 & -0.2 & -1.5 -2.1 -1.6 \\ 10 & 13 & 15 \quad 20 \quad 33 \end{array}$$

$$\begin{array}{ccc} +0.3 +1.0 +0.3 & -3.3 & -3.3 -0.8 \\ 33 & 28 & 25 \quad 21 \quad 16 \quad 11 \end{array}$$

$$\begin{array}{ccc} -0.5 & -0.2 & -1.6 -4.0 \\ 10 & 12 & 15 \quad 33 \end{array}$$

$$\begin{array}{ccc} -5.3 & -4.8 & -3.7 -0.6 \\ 33 & 28 & 16 \quad 11 \end{array}$$

$$\begin{array}{ccc} -0.9 & -5.0 & -6.5 \\ 11 & 20 & 33 \end{array}$$

140
+50

Surf
E11
325.0 ✓

141

327.4 ✓

+50

329.8 ✓

142

332.6 ✓

+50

335.5 ✓

143

338.0 ✓

+50

340.6 340.7

144

343.4 ✓

+50

345.6

145

348.1 ✓

+50

350.5 ✓

146

352.9 ✓

+50

354.7 ✓

Lt.

E

Rt

(45)

$$\begin{array}{ccc} -10.0 & -9.0 & -0.8 \\ \underline{33} & \underline{23} & \underline{12} \end{array}$$

$$\begin{array}{ccc} -0.6 & -8.5 & -8.8 \\ \underline{12} & \underline{23} & \underline{33} \end{array}$$

$$\begin{array}{ccc} -10.0 & -9.2 & -0.7 \\ \underline{33} & \underline{24} & \underline{12} \end{array}$$

$$\begin{array}{ccc} -0.5 & -0.6 & -7.6 & -8.2 \\ \underline{11} & \underline{13} & \underline{24} & \underline{33} \end{array}$$

$$\begin{array}{ccc} -6.3 & -4.8 & -0.7 \\ \underline{33} & \underline{17} & \underline{11} \end{array}$$

$$\begin{array}{ccc} -0.2 & -5.5 & -5.5 \\ \underline{13} & \underline{22} & \underline{33} \end{array}$$

$$\begin{array}{ccc} +4.0 & +4.0 & +2.8 & -0.5 & -0.7 \\ \underline{33} & \underline{30} & \underline{22} & \underline{18} & \underline{12} \end{array}$$

$$\begin{array}{ccc} -0.7 & -1.4 & -0.5 & -0.2 \\ \underline{10} & \underline{13} & \underline{23} & \underline{33} \end{array}$$

$$\begin{array}{ccc} +6.3 & +6.3 & +5.3 & -0.4 & -0.4 \\ \underline{33} & \underline{29} & \underline{25} & \underline{17} & \underline{10} \end{array}$$

$$\begin{array}{ccc} -0.8 & -1.0 & +5.0 & +2.5 \\ \underline{11} & \underline{16} & \underline{23} & \underline{33} \end{array}$$

$$\begin{array}{ccc} +8.2 & +8.2 & +7.0 & -0.3 & 0.0 \\ \underline{33} & \underline{30} & \underline{24} & \underline{15} & \underline{12} \end{array}$$

$$\begin{array}{ccc} -0.4 & -0.5 & -1.0 & +7.5 & +4.5 \\ \underline{10} & \underline{14} & \underline{17} & \underline{27} & \underline{33} \end{array}$$

$$\begin{array}{ccc} +7.7 & +7.7 & +7.0 & -0.5 & 0.0 \\ \underline{33} & \underline{31} & \underline{27} & \underline{17} & \underline{12} \end{array}$$

$$\begin{array}{ccc} -0.4 & -1.3 & -1.3 & +8.0 & +6.7 \\ \underline{10} & \underline{13} & \underline{17} & \underline{26} & \underline{33} \end{array}$$

$$\begin{array}{ccc} +3.9 & +4.9 & +4.5 & +4.5 & -1.1 \\ \underline{33} & \underline{26} & \underline{24} & \underline{21} & \underline{15} \end{array}$$

$$\begin{array}{ccc} -0.9 & -0.8 & -1.5 & +4.0 & +2.7 \\ \underline{10} & \underline{13} & \underline{19} & \underline{23} & \underline{33} \end{array}$$

$$\begin{array}{ccc} +2.8 & +2.8 & +2.0 & +1.4 & -0.6 \\ \underline{33} & \underline{26} & \underline{24} & \underline{18} & \underline{15} \end{array}$$

$$\begin{array}{ccc} -1.1 & +2.3 & +1.5 \\ \underline{15} & \underline{20} & \underline{33} \end{array}$$

$$\begin{array}{ccc} +2.5 & +1.6 & 0.0 & -0.8 & -0.7 \\ \underline{33} & \underline{30} & \underline{25} & \underline{17} & \underline{12} \end{array}$$

$$\begin{array}{ccc} -0.5 & -1.0 & +1.2 & +1.2 \\ \underline{12} & \underline{18} & \underline{23} & \underline{33} \end{array}$$

$$\begin{array}{ccc} +0.5 & -0.8 & -0.7 \\ \underline{33} & \underline{27} & \underline{10} \end{array}$$

$$\begin{array}{ccc} -0.2 & -1.4 & -1.4 & +7.6 & +7.2 \\ \underline{13} & \underline{16} & \underline{19} & \underline{27} & \underline{33} \end{array}$$

$$\begin{array}{ccc} -1.2 & -1.5 & 0.0 & -1.0 \\ \underline{33} & \underline{30} & \underline{19} & \underline{17} \end{array}$$

$$\begin{array}{ccc} -0.4 & +0.1 & -0.7 & -0.7 & +10.0 \\ \underline{15} & \underline{16} & \underline{18} & \underline{20} & \underline{33} \end{array}$$

$$\begin{array}{ccc} 0.0 & +1.5 & -0.5 & -0.6 \\ \underline{33} & \underline{21} & \underline{17} & \underline{13} \end{array}$$

$$\begin{array}{ccc} -0.5 & -0.3 & +1.2 & +1.2 \\ \underline{12} & \underline{20} & \underline{29} & \underline{29} \end{array}$$

33

147	357.5
+50	358.4 ✓
148	359.5 ✓
+50	360.6 ✓
149	361.2 ✓
+50	361.7 ✓
150	362.4 ✓
+50	363.2 ✓
151	364.0 ✓
+50	364.7 ✓
152	364.8 ✓
+50	363.7 ✓

Lt.

£

Rt

(46)

$$\begin{array}{r} 0.0 \\ 33 \end{array} \quad \begin{array}{r} +1.9 \\ 21 \end{array} \quad \begin{array}{r} -0.9 \\ 16 \end{array}$$

$$\begin{array}{r} -0.7 \\ 14 \end{array} \quad \begin{array}{r} 0.0 \\ 19 \end{array} \quad \begin{array}{r} +5.2 \\ 30 \end{array} \quad \begin{array}{r} +8.2 \\ 33 \end{array}$$

$$\begin{array}{r} +0.4 \\ 33 \end{array} \quad \begin{array}{r} +2.0 \\ 24 \end{array} \quad \begin{array}{r} -1.4 \\ 18 \end{array} \quad \begin{array}{r} -1.1 \\ 16 \end{array}$$

$$\begin{array}{r} -0.4 \\ 15 \end{array} \quad \begin{array}{r} -1.0 \\ 16 \end{array} \quad \begin{array}{r} -1.0 \\ 18 \end{array} \quad \begin{array}{r} +6.0 \\ 26 \end{array} \quad \begin{array}{r} +5.3 \\ 33 \end{array}$$

$$\begin{array}{r} -2.5 \\ 33 \end{array} \quad \begin{array}{r} -1.8 \\ 18 \end{array} \quad \begin{array}{r} -0.4 \\ 14 \end{array}$$

$$\begin{array}{r} -0.3 \\ 10 \end{array} \quad \begin{array}{r} 0.0 \\ 18 \end{array} \quad \begin{array}{r} +2.6 \\ 23 \end{array} \quad \begin{array}{r} +3.0 \\ 33 \end{array}$$

$$\begin{array}{r} -6.5 \\ 33 \end{array} \quad \begin{array}{r} -5.3 \\ 22 \end{array} \quad \begin{array}{r} -0.8 \\ 12 \end{array}$$

$$\begin{array}{r} -0.7 \\ 16 \end{array} \quad \begin{array}{r} +2.3 \\ 22 \end{array} \quad \begin{array}{r} +3.2 \\ 33 \end{array}$$

$$\begin{array}{r} -6.5 \\ 33 \end{array} \quad \begin{array}{r} -6.0 \\ 13 \end{array} \quad \begin{array}{r} -1.1 \\ 14 \end{array}$$

$$\begin{array}{r} -0.5 \\ 10 \end{array} \quad \begin{array}{r} -1.0 \\ 13 \end{array} \quad \begin{array}{r} -0.7 \\ 16 \end{array} \quad \begin{array}{r} +3.0 \\ 21 \end{array} \quad \begin{array}{r} +3.5 \\ 33 \end{array}$$

$$\begin{array}{r} -0.3 \\ 33 \end{array} \quad \begin{array}{r} -0.7 \\ 14 \end{array}$$

$$\begin{array}{r} -0.4 \\ 11 \end{array} \quad \begin{array}{r} -0.7 \\ 15 \end{array} \quad \begin{array}{r} +3.2 \\ 21 \end{array} \quad \begin{array}{r} +3.0 \\ 33 \end{array}$$

$$\begin{array}{r} +0.5 \\ 33 \end{array} \quad \begin{array}{r} +0.1 \\ 12 \end{array}$$

$$\begin{array}{r} -0.7 \\ 17 \end{array} \quad \begin{array}{r} +2.6 \\ 19 \end{array} \quad \begin{array}{r} +2.3 \\ 33 \end{array}$$

$$\begin{array}{r} +1.2 \\ 33 \end{array} \quad \begin{array}{r} 0.0 \\ 23 \end{array} \quad \begin{array}{r} -0.5 \\ 11 \end{array}$$

$$\begin{array}{r} -0.5 \\ 14 \end{array} \quad \begin{array}{r} +1.1 \\ 18 \end{array} \quad \begin{array}{r} +0.6 \\ 20 \end{array} \quad \begin{array}{r} +0.6 \\ 33 \end{array}$$

$$\begin{array}{r} +2.6 \\ 33 \end{array} \quad \begin{array}{r} +0.5 \\ 27 \end{array} \quad \begin{array}{r} -0.4 \\ 13 \end{array}$$

$$\begin{array}{r} -0.8 \\ 14 \end{array} \quad \begin{array}{r} +1.5 \\ 18 \end{array} \quad \begin{array}{r} +1.5 \\ 19 \end{array} \quad \begin{array}{r} +0.8 \\ 20 \end{array} \quad \begin{array}{r} +0.3 \\ 33 \end{array}$$

$$\begin{array}{r} +3.0 \\ 33 \end{array} \quad \begin{array}{r} +0.6 \\ 26 \end{array}$$

$$\begin{array}{r} -0.6 \\ 10 \end{array} \quad \begin{array}{r} -0.7 \\ 14 \end{array} \quad \begin{array}{r} +3.2 \\ 20 \end{array} \quad \begin{array}{r} +2.0 \\ 22 \end{array} \quad \begin{array}{r} +2.0 \\ 33 \end{array}$$

$$\begin{array}{r} +2.0 \\ 33 \end{array} \quad \begin{array}{r} +0.3 \\ 27 \end{array}$$

$$\begin{array}{r} -0.7 \\ 14 \end{array} \quad \begin{array}{r} -0.2 \\ 15 \end{array} \quad \begin{array}{r} -0.2 \\ 17 \end{array} \quad \begin{array}{r} +5.5 \\ 23 \end{array} \quad \begin{array}{r} +5.5 \\ 33 \end{array}$$

$$\begin{array}{r} +2.1 \\ 33 \end{array} \quad \begin{array}{r} +0.4 \\ 27 \end{array}$$

$$\begin{array}{r} -0.5 \\ 12 \end{array} \quad \begin{array}{r} -0.3 \\ 13 \end{array} \quad \begin{array}{r} -0.3 \\ 17 \end{array} \quad \begin{array}{r} +1.3 \\ 27 \end{array} \quad \begin{array}{r} +1.3 \\ 33 \end{array}$$

153

362.1 ✓

+50

360.6 ✓

154

358.4 ✓

+50

357.9 356.9

155

355.5 ✓

+50

354.1 ✓

156

352.4 ✓

+50

350.6 ✓

157

349.5 ✓

+50

348.6 ✓

158

347.9 ✓

+50

346.7 ✓

Lt

E

Rt.

(47)

$$\begin{array}{r} +4.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +0.5 \\ \hline 29 \end{array}$$

$$\begin{array}{r} -0.5 \\ \hline 13 \end{array}$$

$$\begin{array}{r} +6.3 \\ \hline 24 \end{array}$$

$$\begin{array}{r} +1.5 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -0.5 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -1.0 \\ \hline 13 \end{array} \quad \begin{array}{r} -0.5 \\ \hline 15 \end{array} \quad \begin{array}{r} -1.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -0.7 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -0.5 \\ \hline 10 \end{array} \quad \begin{array}{r} -4.5 \\ \hline 17 \end{array} \quad \begin{array}{r} -5.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +0.9 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -1.0 \\ \hline 10 \end{array} \quad \begin{array}{r} -4.5 \\ \hline 16 \end{array} \quad \begin{array}{r} -6.1 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +2.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +0.2 \\ \hline 16 \end{array}$$

$$\begin{array}{r} -1.0 \\ \hline 11 \end{array}$$

$$\begin{array}{r} -3.7 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +4.7 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -0.7 \\ \hline 21 \end{array}$$

$$\begin{array}{r} -0.3 \\ \hline 11 \end{array}$$

$$\begin{array}{r} -1.5 \\ \hline 15 \end{array}$$

$$\begin{array}{r} +0.5 \\ \hline 17 \end{array}$$

$$\begin{array}{r} -2.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +1.5 \\ \hline 23 \end{array}$$

$$\begin{array}{r} +4.6 \\ \hline 25 \end{array}$$

$$\begin{array}{r} +3.7 \\ \hline 22 \end{array}$$

$$\begin{array}{r} -0.6 \\ \hline 17 \end{array}$$

$$\begin{array}{r} -1.6 \\ \hline 15 \end{array}$$

$$\begin{array}{r} -1.3 \\ \hline 17 \end{array}$$

$$\begin{array}{r} -4.5 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -1.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -2.0 \\ \hline 22 \end{array}$$

$$\begin{array}{r} -2.1 \\ \hline 14 \end{array}$$

$$\begin{array}{r} -0.6 \\ \hline 11 \end{array}$$

$$\begin{array}{r} -1.0 \\ \hline 9.0 \end{array}$$

$$\begin{array}{r} -9.0 \\ \hline 24 \end{array}$$

$$\begin{array}{r} -1.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -5.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -5.0 \\ \hline 17 \end{array}$$

$$\begin{array}{r} -0.7 \\ \hline 11 \end{array}$$

$$\begin{array}{r} -0.5 \\ \hline 8.0 \end{array}$$

$$\begin{array}{r} -15.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -6.4 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -4.5 \\ \hline 18 \end{array}$$

$$\begin{array}{r} -0.5 \\ \hline 12 \end{array}$$

$$\begin{array}{r} -1.0 \\ \hline 9.0 \end{array}$$

$$\begin{array}{r} -13.4 \\ \hline 30 \end{array}$$

$$\begin{array}{r} -14.0 \\ \hline 32 \end{array}$$

$$\begin{array}{r} +0.2 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +0.5 \\ \hline 31 \end{array}$$

$$\begin{array}{r} +0.2 \\ \hline 21 \end{array}$$

$$\begin{array}{r} -1.0 \\ \hline 16 \end{array}$$

$$\begin{array}{r} -0.8 \\ \hline 11 \end{array}$$

$$\begin{array}{r} -2.7 \\ \hline 17 \end{array}$$

$$\begin{array}{r} -5.0 \\ \hline 30 \end{array}$$

$$\begin{array}{r} -6.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +1.2 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +5.0 \\ \hline 28 \end{array}$$

$$\begin{array}{r} +0.1 \\ \hline 19 \end{array}$$

$$\begin{array}{r} +0.1 \\ \hline 14 \end{array}$$

$$\begin{array}{r} -0.3 \\ \hline 13 \end{array}$$

$$\begin{array}{r} -1.0 \\ \hline 13 \end{array}$$

$$\begin{array}{r} -0.7 \\ \hline 16 \end{array}$$

$$\begin{array}{r} +3.0 \\ \hline 22 \end{array}$$

$$\begin{array}{r} +2.2 \\ \hline 33 \end{array}$$

5+9.

159

345.7 ✓

+50

344.4 ✓

160

343.5

+50

343.0 342.1

161

341.2

+50

340.4

162

339.5

+50

338.6

163

338.4

+50

337.9

164

338.2

+50

338.2 ✓

LT.

F

RT

(48)

$$\begin{array}{ccccc} +7.0 & +7.0 & +0.9 & +0.3 & -0.3 \\ 33 & 30 & 18 & 14 & 12 \end{array}$$

$$\begin{array}{ccc} +0.8 & +4.3 & +4.5 \\ 15 & 23 & 33 \end{array}$$

$$\begin{array}{cccc} +8.0 & +7.0 & -0.4 & -0.4 \\ 33 & 18 & 17 & 12 \end{array}$$

$$\begin{array}{ccc} 0.0 & +6.0 & +5.0 \\ 15 & 23 & 32 \end{array}$$

$$\begin{array}{ccc} +0.2 & +0.3 & -1.0 \\ 33 & 17 & 15 \end{array}$$

$$\begin{array}{cccc} -0.7 & -0.8 & -2.0 & -3.5 \\ 10 & 12 & 19 & 33 \end{array}$$

$$\begin{array}{ccc} -6.8 & -5.0 & -0.8 \\ 33 & 16 & 9.0 \end{array}$$

$$\begin{array}{ccc} -0.8 & -4.8 & -6.4 \\ 12 & 18 & 33 \end{array}$$

$$\begin{array}{cccc} -6.0 & -6.0 & -4.8 & -0.7 \\ 33 & 27 & 17 & 11 \end{array}$$

$$\begin{array}{cccc} -0.7 & -2.2 & -2.4 & -0.5 \\ 13 & 16 & 18 & 22 \end{array}$$

$$\begin{array}{ccccc} -3.0 & -3.3 & -3.4 & -2.7 & -0.9 \\ 30 & 24 & 24 & 17 & 16 \end{array}$$

$$\begin{array}{ccccc} -0.8 & -1.5 & -1.2 & +4.0 & +5.0 \\ 12 & 15 & 23 & 31 & 33 \end{array}$$

$$\begin{array}{ccccc} -3.3 & -2.8 & -3.4 & -2.6 & -0.8 \\ 33 & 28 & 27 & 17 & 13 \end{array}$$

$$\begin{array}{ccccc} -0.8 & -1.5 & -1.0 & +3.9 & +4.2 \\ 12 & 16 & 19 & 27 & 32 \end{array}$$

$$\begin{array}{ccccc} -2.5 & -3.2 & -2.9 & -0.9 & -0.9 \\ 33 & 29 & 26 & 16 & 12 \end{array}$$

$$\begin{array}{cccc} -0.9 & -4.6 & -5.0 & -4.6 \\ 10 & 16 & 27 & 33 \end{array}$$

$$\begin{array}{ccc} -3.8 & -3.5 & -0.8 \\ 33 & 16 & 12 \end{array}$$

$$\begin{array}{cccc} -0.8 & -7.0 & -8.4 & -8.4 \\ 9.0 & 20 & 27 & 33 \end{array}$$

$$\begin{array}{ccc} -3.0 & -2.1 & -0.5 \\ 36 & 14 & 11 \end{array}$$

$$\begin{array}{cccc} -0.8 & -7.0 & -8.4 & -9.4 \\ 11 & 22 & 28 & 33 \end{array}$$

$$\begin{array}{cccc} -0.5 & -2.8 & -3.1 & -0.6 \\ 32 & 21 & 19 & 13 \end{array}$$

$$\begin{array}{ccc} -0.6 & -7.9 & -7.9 \\ 11 & 26 & 33 \end{array}$$

$$\begin{array}{ccccc} +13.0 & +3.0 & +3.2 & -1.6 & -1.0 \\ 42 & 31 & 27 & 16 & 14 \end{array}$$

$$\begin{array}{cccc} -0.7 & -2.2 & -2.4 & -6.3 \\ 10 & 17 & 20 & 33 \end{array}$$

stg.

165

338.0 ✓

+50

337.7 ✓

166

337.7 ✓

+50

337.3 ✓

167

336.9 ✓

+50

336.6 ✓

168

336.4 ✓

+50

336.3 ✓

169

335.9 ✓

+50

335.7 ✓

170

335.3 ✓

+50

335.0 ✓

Lt.

#

Rt

(49)

$$\begin{array}{r} +11.0 \\ 31 \end{array} \quad \begin{array}{r} +0.3 \\ 18 \end{array} \quad \begin{array}{r} -0.6 \\ 14 \end{array} \quad \begin{array}{r} -0.7 \\ 13 \end{array} \quad \begin{array}{r} +0.3 \\ 19 \end{array} \quad \begin{array}{r} +11.0 \\ 32 \end{array}$$

$$\begin{array}{r} +5.8 \\ 33 \end{array} \quad \begin{array}{r} +5.8 \\ 26 \end{array} \quad \begin{array}{r} -0.8 \\ 19 \end{array} \quad \begin{array}{r} -0.8 \\ 14 \end{array} \quad \begin{array}{r} -0.8 \\ 14 \end{array} \quad \begin{array}{r} 0.0 \\ 20 \end{array} \quad \begin{array}{r} +8.0 \\ 32 \end{array}$$

$$\begin{array}{r} +1.7 \\ 33 \end{array} \quad \begin{array}{r} +1.7 \\ 27 \end{array} \quad \begin{array}{r} -0.2 \\ 24 \end{array} \quad \begin{array}{r} -0.7 \\ 14 \end{array} \quad \begin{array}{r} -0.2 \\ 19 \end{array} \quad \begin{array}{r} +7.0 \\ 29 \end{array} \quad \begin{array}{r} +7.5 \\ 33 \end{array}$$

$$\begin{array}{r} -0.4 \\ 28 \end{array} \quad \begin{array}{r} -0.1 \\ 17 \end{array} \quad \begin{array}{r} -0.9 \\ 14 \end{array} \quad \begin{array}{r} -0.8 \\ 17 \end{array} \quad \begin{array}{r} +3.6 \\ 23 \end{array} \quad \begin{array}{r} +4.5 \\ 32 \end{array}$$

$$\begin{array}{r} -1.5 \\ 31 \end{array} \quad \begin{array}{r} -1.3 \\ 14 \end{array} \quad \begin{array}{r} -0.5 \\ 14 \end{array} \quad \begin{array}{r} +0.8 \\ 17 \end{array} \quad \begin{array}{r} +0.9 \\ 31 \end{array}$$

$$\begin{array}{r} -0.1 \\ 30 \end{array} \quad \begin{array}{r} -1.2 \\ 16 \end{array} \quad \begin{array}{r} -0.7 \\ 13 \end{array} \quad \begin{array}{r} -0.3 \\ 15 \end{array} \quad \begin{array}{r} -1.5 \\ 31 \end{array}$$

$$\begin{array}{r} +4.4 \\ 30 \end{array} \quad \begin{array}{r} +3.0 \\ 20 \end{array} \quad \begin{array}{r} -0.9 \\ 14 \end{array} \quad \begin{array}{r} -1.1 \\ 17 \end{array} \quad \begin{array}{r} -0.2 \\ 19 \end{array} \quad \begin{array}{r} -1.5 \\ 32 \end{array}$$

$$\begin{array}{r} +12.3 \\ 33 \end{array} \quad \begin{array}{r} +0.2 \\ 18 \end{array} \quad \begin{array}{r} -0.5 \\ 11 \end{array} \quad \begin{array}{r} -0.6 \\ 14 \end{array} \quad \begin{array}{r} +1.5 \\ 19 \end{array} \quad \begin{array}{r} +11.0 \\ 31.0 \end{array}$$

$$\begin{array}{r} +3.0 \\ 33 \end{array} \quad \begin{array}{r} +4.0 \\ 27 \end{array} \quad \begin{array}{r} -1.0 \\ 18 \end{array} \quad \begin{array}{r} -0.5 \\ 13 \end{array} \quad \begin{array}{r} -0.2 \\ 18 \end{array} \quad \begin{array}{r} +7.4 \\ 28 \end{array} \quad \begin{array}{r} +7.4 \\ 33 \end{array}$$

$$\begin{array}{r} -4.5 \\ 33 \end{array} \quad \begin{array}{r} -3.2 \\ 21 \end{array} \quad \begin{array}{r} -1.0 \\ 14 \end{array} \quad \begin{array}{r} -0.9 \\ 13 \end{array} \quad \begin{array}{r} -4.0 \\ 19 \end{array} \quad \begin{array}{r} -3.7 \\ 33 \end{array}$$

$$\begin{array}{r} -8.0 \\ 33 \end{array} \quad \begin{array}{r} -8.0 \\ 25 \end{array} \quad \begin{array}{r} -0.8 \\ 12 \end{array} \quad \begin{array}{r} -0.7 \\ 12 \end{array} \quad \begin{array}{r} -9.9 \\ 28 \end{array} \quad \begin{array}{r} -10.7 \\ 33 \end{array}$$

$$\begin{array}{r} -9.8 \\ 33 \end{array} \quad \begin{array}{r} -9.1 \\ 26 \end{array} \quad \begin{array}{r} -0.8 \\ 10 \end{array} \quad \begin{array}{r} -0.8 \\ 12 \end{array} \quad \begin{array}{r} -11.9 \\ 33 \end{array}$$

5+9

171

334.9 ✓

+50

335.4 ✓

172

335.6 ✓

+50

335.6 ✓

173

335.9 ✓

+50

335.8 ✓

174

336.0 ✓

+50

336.2 ✓

175

336.3 ✓

+50

336.3 ✓

176

336.4 ✓

+50

336.3 ✓

Lt.

E

Rt.

(50)

$$\begin{array}{r} -10.0 \\ 33 \end{array} \quad \begin{array}{r} -7.3 \\ 27 \end{array} \quad \begin{array}{r} -0.8 \\ 12 \end{array}$$

$$\begin{array}{r} -0.5 \\ 10 \end{array} \quad \begin{array}{r} -9.3 \\ 23 \end{array} \quad \begin{array}{r} -10.8 \\ 33 \end{array}$$

$$\begin{array}{r} -8.0 \\ 33 \end{array} \quad \begin{array}{r} -8.0 \\ 28 \end{array} \quad \begin{array}{r} -7.4 \\ 24 \end{array} \quad \begin{array}{r} -0.7 \\ 11 \end{array}$$

$$\begin{array}{r} -0.9 \\ 12 \end{array} \quad \begin{array}{r} -6.1 \\ 22 \end{array} \quad \begin{array}{r} 7.0 \\ 33 \end{array}$$

$$\begin{array}{r} -4.3 \\ 33 \end{array} \quad \begin{array}{r} -4.3 \\ 26 \end{array} \quad \begin{array}{r} -3.2 \\ 16 \end{array} \quad \begin{array}{r} -0.6 \\ 12 \end{array}$$

$$\begin{array}{r} -1.1 \\ 16 \end{array} \quad \begin{array}{r} -2.4 \\ 22 \end{array} \quad \begin{array}{r} -1.5 \\ 33 \end{array}$$

$$\begin{array}{r} -0.2 \\ 33 \end{array} \quad \begin{array}{r} 0.0 \\ 29 \end{array} \quad \begin{array}{r} +1.8 \\ 20 \end{array} \quad \begin{array}{r} -1.2 \\ 15 \end{array}$$

$$\begin{array}{r} -0.2 \\ 17 \end{array} \quad \begin{array}{r} +10.2 \\ 33 \end{array}$$

$$\begin{array}{r} +3.8 \\ 33 \end{array} \quad \begin{array}{r} +6.7 \\ 23 \end{array} \quad \begin{array}{r} -0.5 \\ 12 \end{array}$$

$$\begin{array}{r} -0.3 \\ 15 \end{array} \quad \begin{array}{r} +1.2 \\ 24 \end{array} \quad \begin{array}{r} +10.2 \\ 33 \end{array}$$

$$\begin{array}{r} -2.2 \\ 33 \end{array} \quad \begin{array}{r} +0.2 \\ 18 \end{array} \quad \begin{array}{r} -0.9 \\ 15 \end{array}$$

$$\begin{array}{r} -1.3 \\ 21 \end{array} \quad \begin{array}{r} +0.7 \\ 26 \end{array} \quad \begin{array}{r} -0.5 \\ 33 \end{array}$$

$$\begin{array}{r} -4.6 \\ 33 \end{array} \quad \begin{array}{r} -2.5 \\ 15 \end{array} \quad \begin{array}{r} -1.0 \\ 11 \end{array}$$

$$\begin{array}{r} -0.2 \\ 15 \end{array} \quad \begin{array}{r} -2.2 \\ 25 \end{array} \quad \begin{array}{r} +1.2 \\ 30 \end{array} \quad \begin{array}{r} +1.2 \\ 33 \end{array}$$

$$\begin{array}{r} -1.2 \\ 33 \end{array} \quad \begin{array}{r} -1.3 \\ 24 \end{array} \quad \begin{array}{r} -2.0 \\ 16 \end{array} \quad \begin{array}{r} -0.4 \\ 11 \end{array}$$

$$\begin{array}{r} -1.2 \\ 17 \end{array} \quad \begin{array}{r} -2.5 \\ 24 \end{array} \quad \begin{array}{r} -0.8 \\ 31 \end{array} \quad \begin{array}{r} -0.8 \\ 33 \end{array}$$

$$\begin{array}{r} -3.3 \\ 33 \end{array} \quad \begin{array}{r} -2.5 \\ 20 \end{array} \quad \begin{array}{r} -3.0 \\ 15 \end{array} \quad \begin{array}{r} -0.8 \\ 11 \end{array}$$

$$\begin{array}{r} -0.7 \\ 12 \end{array} \quad \begin{array}{r} -2.3 \\ 17 \end{array} \quad \begin{array}{r} -2.2 \\ 33 \end{array}$$

$$\begin{array}{r} +2.2 \\ 33 \end{array} \quad \begin{array}{r} +2.8 \\ 24 \end{array} \quad \begin{array}{r} +2.0 \\ 19 \end{array} \quad \begin{array}{r} -0.7 \\ 13 \end{array}$$

$$\begin{array}{r} -0.8 \\ 14 \end{array} \quad \begin{array}{r} +0.2 \\ 18 \end{array} \quad \begin{array}{r} +0.9 \\ 33 \end{array}$$

$$\begin{array}{r} +5.6 \\ 33 \end{array} \quad \begin{array}{r} +7.0 \\ 23 \end{array} \quad \begin{array}{r} -0.4 \\ 10 \end{array}$$

$$\begin{array}{r} -0.6 \\ 12 \end{array} \quad \begin{array}{r} -0.2 \\ 15 \end{array} \quad \begin{array}{r} +5.0 \\ 20 \end{array} \quad \begin{array}{r} +3.6 \\ 30 \end{array}$$

$$\begin{array}{r} +4.0 \\ 33 \end{array} \quad \begin{array}{r} +5.5 \\ 23 \end{array} \quad \begin{array}{r} -0.6 \\ 14 \end{array}$$

$$\begin{array}{r} -0.8 \\ 12 \end{array} \quad \begin{array}{r} +3.5 \\ 20 \end{array} \quad \begin{array}{r} +3.0 \\ 33 \end{array}$$

5+9.

177

336.0 ✓

+50

335.9 ✓

178

335.9 ✓

+50

336.0 ✓

179

336.2 ✓

+50

336.7 ✓

180

337.4 ✓

+50

338.3 ✓

181

338.9 ✓

+50

339.9 ✓

182

340.1 ✓

+25

+03

340.4 ✓

$R+$

51

$$\begin{array}{r} +0.5 \\ \hline 36 \end{array} \quad \begin{array}{r} +1.3 \\ \hline 22 \end{array} \quad \begin{array}{r} +0.9 \\ \hline 17 \end{array} \quad \begin{array}{r} -1.0 \\ \hline 14 \end{array}$$

$$\begin{array}{ccccc} +2.1 & +3.2 & +2.0 & -0.2 & -1.0 \\ \hline 33 & 25 & 20 & 18 & 16 \end{array}$$

$$\begin{array}{r} +2.0 \\ 33 \end{array} \quad \begin{array}{r} +2.7 \\ 27 \end{array} \quad \begin{array}{r} -1.3 \\ 21 \end{array} \quad \begin{array}{r} -1.5 \\ 14 \end{array} \quad \begin{array}{r} -0.7 \\ 11 \end{array}$$

$$\begin{array}{r} -2.5 \\ 33 \end{array} \quad \begin{array}{r} -1.0 \\ 27 \end{array} \quad \begin{array}{r} -3.6 \\ 20 \end{array} \quad \begin{array}{r} -0.5 \\ 11 \end{array}$$

$$\begin{array}{r} -5.0 \\ 33 \end{array} \quad \begin{array}{r} -5.2 \\ 18 \end{array} \quad \begin{array}{r} -0.8 \\ 10 \end{array}$$

$$\begin{array}{r} -9.0 \\ 33 \end{array} \quad \begin{array}{r} -5.0 \\ 16 \end{array} \quad \begin{array}{r} -0.5 \\ 10 \end{array}$$

$$\begin{array}{r} -3.4 - 3.4 - 4.6 - 4.0 - 0.7 \\ \hline 33 \quad 27 \quad 20 \quad 16 \quad 10 \end{array}$$

$$\begin{array}{r} -4.2 \\ 33 \end{array} \quad \begin{array}{r} -2.8 \\ 16 \end{array} \quad \begin{array}{r} -0.7 \\ 11 \end{array}$$

$$\begin{array}{ccccc} +1.6 & +2.7 & +2.2 & -0.6 & -0.7 \\ \hline 3.3 & 2.5 & 2.1 & 1.5 & 1.2 \end{array}$$

$$\begin{array}{r} +6.7 \\ \underline{33} \\ 33 \end{array} \quad \begin{array}{r} +6.7 \\ \underline{24} \\ 24 \end{array} \quad \begin{array}{r} +0.5 \\ \underline{1.8} \\ 1.8 \end{array} \quad \begin{array}{r} -0.3 \\ \underline{16} \\ 16 \end{array}$$

$$\begin{array}{r} +1.0 \\ \hline 33 \end{array} \quad \begin{array}{r} +2.4 \\ \hline 25 \end{array} \quad \begin{array}{r} -1.0 \\ \hline 17 \end{array} \quad \begin{array}{r} -0.4 \\ \hline 12 \end{array}$$

$$\begin{array}{r} -1.4 \\ \hline 33 \end{array} \quad \begin{array}{r} -1.7 \\ \hline 17 \end{array} \quad \begin{array}{r} -1.8 \\ \hline 13 \end{array}$$

5+9.

+75 00 340.8 ✓

183 ← 340.8 ✓

+50 340.9 ✓

184 340.9 ✓

+50 341.3 ✓

185 341.5 ✓

+50 341.6 ✓

186 341.4 ✓

+20 -0.2 341.6 ✓

+27 341.5 ✓

+31 341.4 ✓

+54 +1.0 340.7 ✓

+62 340.2 ✓

187 339.7 ✓

Lt.

E

Rt.

52

$$\begin{array}{cccccc} -1.8 & -0.8 & -1.0 & -1.5 & -0.8 & \\ \hline 33 & 30 & 23 & 18 & 13 & \end{array}$$

$$\begin{array}{ccc} -1.0 & +0.7 & +0.7 \\ \hline 17 & 26 & 33 \end{array}$$

$$\begin{array}{cccc} -2.8 & -2.4 & -2.0 & -0.8 \\ \hline 33 & 29 & 16 & 13 \end{array}$$

$$\begin{array}{cccc} -0.8 & +1.2 & +2.0 & +1.7 \\ \hline 15 & 21 & 26 & 33 \end{array}$$

$$\begin{array}{ccc} -5.7 & -3.7 & -1.0 \\ \hline 33 & 18 & 14 \end{array}$$

$$\begin{array}{cccc} -1.0 & -1.8 & -0.1 & -0.1 \\ \hline 13 & 17 & 20 & 33 \end{array}$$

$$\begin{array}{ccc} -3.8 & -3.0 & -0.8 \\ \hline 33 & 18 & 12 \end{array}$$

$$\begin{array}{cccc} -0.6 & -3.5 & -3.2 & -3.4 \\ \hline 13 & 20 & 27 & 33 \end{array}$$

$$\begin{array}{ccc} -4.0 & -3.0 & -1.1 \\ \hline 33 & 19 & 12 \end{array}$$

$$\begin{array}{ccc} -0.9 & -1.7 & -1.0 \\ \hline 14 & 29 & 33 \end{array}$$

$$\begin{array}{cc} +1.2 & -0.7 \\ \hline 33 & 09 \end{array}$$

$$\begin{array}{ccc} -0.8 & +3.2 & +3.2 \\ \hline 16 & 23 & 33 \end{array}$$

$$\begin{array}{ccc} +3.5 & +3.5 & -1.0 \\ \hline 33 & 25 & 14 \end{array}$$

$$\begin{array}{cccc} -0.4 & 0.0 & +5.0 & +5.5 \\ \hline 10 & 18 & 24 & 33 \end{array}$$

$$\begin{array}{cc} +0.9 & -0.8 \\ \hline 33 & 13 \end{array}$$

$$\begin{array}{ccc} 0.0 & +5.7 & +5.7 \\ \hline 17 & 24 & 33 \end{array}$$

$$\begin{array}{cc} +1.1 & -0.5 \\ \hline 33 & 13 \end{array}$$

$$\begin{array}{ccc} -0.4 & +4.7 & +4.9 \\ \hline 18 & 27 & 33 \end{array}$$

$$\begin{array}{cc} +1.1 & -0.5 \\ \hline 33 & 13 \end{array}$$

$$\begin{array}{ccc} -0.2 & -0.3 & -0.1 \\ \hline 10 & 21 & 33 \end{array}$$

$$\begin{array}{c} -0.9 \\ \hline 33 \end{array}$$

$$\begin{array}{ccc} -0.2 & -0.3 & -0.2 \\ \hline 10 & 21 & 33 \end{array}$$

$$\begin{array}{c} -0.7 \\ \hline 33 \end{array}$$

$$\begin{array}{c} +0.2 \\ \hline 33 \end{array}$$

$$\begin{array}{ccc} +3.3 & +1.6 & -0.7 \\ \hline 33 & 24 & 18 \end{array}$$

$$\begin{array}{ccc} -0.7 & +0.8 & +1.2 \\ \hline 15 & 21 & 33 \end{array}$$

5 + 9,

187

339.7 ✓

+50

338.9 ✓

188

337.2 ✓

+50

336.2 ✓ 336.0

189

334.7 ✓

+50

332.9 ✓

190

331.0 ✓

+50

329.3 ✓

+75

+0.8

328.6 ✓

191

↖

327.8 ✓

+25

↘
-0.5

327.3 ✓

192

323.8 ✓

+50

322.2 ✓

193

321.8 ✓

15.

五

13+

53

$$\begin{array}{r} 33 + 0.5 \\ \hline 28 \end{array} \quad \begin{array}{r} -1.3 \\ \hline 24 \end{array} \quad \begin{array}{r} -1.3 \\ \hline 17 \end{array} \quad \begin{array}{r} -0.4 \\ \hline 19 \end{array}$$

$$\begin{array}{r} -0.9 \\ 17 \end{array} \quad \begin{array}{r} +0.4 \\ 20 \end{array} \quad \begin{array}{r} +0.2 \\ 31 \end{array}$$

$$\begin{array}{ccccc} +3.0 & +2.0 & -0.9 & -1.3 & -0.9 \\ 33 & 26 & 21 & 16 & 13 \end{array}$$

$$\begin{array}{r} -1.0 \\ \hline 15 \end{array} \quad \begin{array}{r} +1.1 \\ \hline 21 \end{array} \quad \begin{array}{r} +1.4 \\ \hline 31 \end{array}$$

$$\begin{array}{r} +6.7 \\ \hline 33 \end{array} \quad \begin{array}{r} +7.6 \\ \hline 25 \end{array} \quad \begin{array}{r} +0.6 \\ \hline 17 \end{array} \quad \begin{array}{r} -0.2 \\ \hline 12 \end{array}$$

$$\begin{array}{r} -0.6 \\ 12 \end{array} \quad \begin{array}{r} -0.2 \\ 16 \end{array} \quad \begin{array}{r} +8.8 \\ 26 \end{array} \quad \begin{array}{r} +11.0 \\ 33 \end{array}$$

$$\begin{array}{r} +0.4 \\ 33 \\ \hline \end{array} \quad \begin{array}{r} +3.0 \\ 21 \\ \hline \end{array} \quad \begin{array}{r} -1.2 \\ 15 \\ \hline \end{array}$$

$$\begin{array}{r} -0.6 \\ N. \\ +14.0 \\ \hline 37 \end{array}$$

$$\begin{array}{r} -3.3 \\ \hline 33 \end{array} \quad \begin{array}{r} -1.0 \\ \hline 19 \end{array} \quad \begin{array}{r} -16 \\ \hline 16 \end{array}$$

$$\begin{array}{r} -0.8 \\ 16 \end{array} \quad \begin{array}{r} +4.0 \\ 20 \end{array} \quad \begin{array}{r} +7.2 \\ 33 \end{array}$$

$$\begin{array}{cccc} -3.0 & -1.1 & -1.8 & -0.9 \\ 33 & 19 & 15 & 14 \end{array}$$

$$\begin{array}{r} -1.4 \\ 16 \end{array} \quad \begin{array}{r} +0.6 \\ 18 \end{array} \quad \begin{array}{r} +0.5 \\ 25 \end{array} \quad \begin{array}{r} +1.7 \\ 33 \end{array}$$

$$\begin{array}{cccc} -0.5 & -0.3 & -1.4 & -0.6 \\ \hline 3.2 & 1.9 & 1.7 & 1.3 \end{array}$$

$-1.0 \quad -0.4 \quad -1.5 \quad +0.5 \quad +1.7$
 $\frac{1}{11} \quad \frac{1}{13} \quad 17 \quad 22 \quad 33$

	+ 5.6	+ 5.6	- 0.5
	<u>33</u>	<u>25</u>	<u>15</u>
+ 8.6	+ 8.6	+ 0.6	- 0.2
<u>33</u>	<u>28</u>	<u>17</u>	<u>12</u>
	+ 3.6	+ 3.5	- 1.0
	<u>33</u>	<u>24</u>	<u>16</u>

$$\begin{array}{r} -0.7 \\ 13 \end{array} \quad \begin{array}{r} -1.8 \\ 14 \end{array} \quad \begin{array}{r} -1.7 \\ 19 \end{array} \quad \begin{array}{r} +3.8 \\ 28 \end{array} \quad \begin{array}{r} +0.0 \\ 27 \end{array} \quad \begin{array}{r} 33 \end{array}$$

$$\begin{array}{r} -6.2 \\ 23 \end{array} \quad \begin{array}{r} -5.0 \\ 20 \end{array} \quad \begin{array}{r} -0.6 \\ 12 \end{array}$$

$$\begin{array}{r} -0.9 \\ 14 \end{array} \quad \begin{array}{r} -4.8 \\ 24 \end{array} \quad \begin{array}{r} -6.2 \\ 33 \end{array}$$

$$\begin{array}{r} -6.7 \\ \hline 33 \end{array} \quad \begin{array}{r} -6.2 \\ \hline 21 \end{array} \quad \begin{array}{r} -1.1 \\ \hline 12 \end{array}$$

$$\begin{array}{r} -0.5 \\ 10 \end{array} \quad \begin{array}{r} -6.0 \\ 20 \end{array} \quad \begin{array}{r} -6.5 \\ 33 \end{array}$$

$$\begin{array}{r} -16 \\ \hline 33 \end{array} \quad \begin{array}{r} -5.6 \\ \hline 22 \end{array} \quad \begin{array}{r} -5.2 \\ \hline 19 \end{array} \quad \begin{array}{r} -0.5 \\ \hline 12 \end{array}$$

$$\begin{array}{r} -0.8 \\ \hline 12 \end{array} \quad \begin{array}{r} -4.9 \\ \hline 20 \end{array} \quad \begin{array}{r} -5.9 \\ \hline 32 \end{array}$$

$$\begin{array}{r} -5.3 \\ \underline{33} \end{array} \quad \begin{array}{r} -5.0 \\ \underline{23} \end{array} \quad \begin{array}{r} -0.7 \\ \underline{12} \end{array}$$

$$\begin{array}{r} -0.9 \\ \hline 12 \end{array} \quad \begin{array}{r} -4.3 \\ \hline 18 \end{array} \quad \begin{array}{r} -4.3 \\ \hline 33 \end{array}$$

Sta.

+50

321.3 ✓

194

320.7 ✓

+50

320.2 ✓

195

319.6 ✓

+50

319.1 ✓

196

318.7 ✓

+50

318.3 ✓

197

317.6 ✓

+50

316.7 ✓

198

315.8 ✓

+50

315.9 ✓

199

315.9 ✓

$$\begin{array}{ccccc} +2.0 & -1.0 & -1.7 & -1.5 & -0.7 \\ \frac{31}{33} & \frac{26}{22} & \frac{22}{16} & \frac{16}{13} & \end{array}$$

$$\begin{array}{ccc} -1.5 & +2.6 & +3.0 \\ \frac{16}{19} & \frac{19}{33} & \end{array}$$

$$\begin{array}{ccccc} +2.6 & +2.4 & -1.3 & -1.7 & -1.1 \\ \frac{33}{28} & \frac{28}{21} & \frac{21}{14} & \frac{14}{14} & \end{array}$$

$$\begin{array}{ccc} -1.1 & +0.5 & +0.2 \\ \frac{17}{21} & \frac{21}{33} & \end{array}$$

$$\begin{array}{ccccc} +2.2 & +1.7 & -1.5 & -2.0 & -1.0 \\ \frac{33}{24} & \frac{24}{20} & \frac{20}{17} & \frac{17}{14} & \end{array}$$

$$\begin{array}{cccc} -1.0 & -1.5 & -0.9 & -1.8 \\ \frac{14}{17} & \frac{17}{24} & \frac{24}{33} & \end{array}$$

$$\begin{array}{ccccc} +1.4 & +1.4 & -0.7 & -1.6 & -0.9 \\ \frac{33}{31} & \frac{31}{28} & \frac{28}{18} & \frac{18}{15} & \end{array}$$

$$\begin{array}{ccc} -1.0 & -1.7 & -2.5 \\ \frac{14}{18} & \frac{18}{33} & \end{array}$$

$$\begin{array}{ccc} +6.1 & +0.3 & -0.8 \\ \frac{33}{26} & \frac{26}{14} & \end{array}$$

$$\begin{array}{ccc} -1.6 & -1.4 & -3.0 \\ \frac{16}{19} & \frac{19}{33} & \end{array}$$

$$\begin{array}{ccc} +4.8 & -1.0 & -1.2 \\ \frac{34}{26} & \frac{26}{13} & \end{array}$$

$$\begin{array}{ccccc} -1.0 & -2.1 & -2.2 & -0.7 & -1.0 \\ \frac{14}{17} & \frac{17}{20} & \frac{20}{22} & \frac{22}{33} & \end{array}$$

$$\begin{array}{ccccc} -4.3 & -1.6 & -1.2 & -1.6 & \\ \frac{32}{22} & \frac{22}{15} & \frac{15}{14} & & \end{array}$$

$$\begin{array}{cccc} -0.7 & -2.0 & -2.0 & +3.0 \\ \frac{15}{20} & \frac{20}{23} & \frac{23}{28} & \frac{28}{33} \end{array}$$

$$\begin{array}{ccc} -7.0 & -5.2 & -1.2 \\ \frac{33}{19} & \frac{19}{11} & \end{array}$$

$$\begin{array}{cccc} -0.9 & -2.4 & -2.5 & -0.6 \\ \frac{17}{21} & \frac{21}{26} & \frac{26}{29} & \frac{29}{33} \end{array}$$

$$\begin{array}{ccc} -6.5 & -6.0 & -1.4 \\ \frac{33}{19} & \frac{19}{11} & \end{array}$$

$$\begin{array}{ccc} -0.9 & -3.7 & -3.7 \\ \frac{16}{26} & \frac{26}{33} & \end{array}$$

$$\begin{array}{ccc} -5.9 & -5.0 & -1.2 \\ \frac{33}{16} & \frac{16}{11} & \end{array}$$

$$\begin{array}{cccc} -0.3 & -3.0 & -3.6 & -3.6 \\ \frac{15}{26} & \frac{26}{27} & \frac{27}{33} & \end{array}$$

$$\begin{array}{ccc} -5.7 & -5.2 & -0.9 \\ \frac{53}{16} & \frac{16}{20} & \end{array}$$

$$\begin{array}{cccc} -0.3 & -1.7 & -2.0 & -1.2 \\ \frac{17}{22} & \frac{22}{26} & \frac{26}{33} & \end{array}$$

$$\begin{array}{ccc} -0.7 & -0.3 & -0.8 \\ \frac{33}{13} & \frac{13}{11} & \end{array}$$

$$\begin{array}{cccc} -0.3 & -1.8 & -1.5 & +3.1 \\ \frac{16}{19} & \frac{19}{23} & \frac{23}{33} & \end{array}$$

319.

+50

315.9 ✓

200

315.5 ✓

+50

314.9 ✓

201

314.4 ✓

+50

314.1 ✓

202

313.8 ✓

+50

313.3 ✓

203

312.9 ✓

+50

312.4 ✓

204

311.4 ✓

+50

310.5 ✓

205

309.0 ✓

55

$$\begin{array}{ccccc} +2.2 & +1.0 & +0.6 & -0.8 & -0.8 \\ 33 & 20 & 15 & 12 & 10 \end{array}$$

$$\begin{array}{ccccc} -1.1 & -2.4 & -2.7 & +1.0 & +1.0 \\ 17 & 20 & 24 & 30 & 33 \end{array}$$

$$\begin{array}{ccccc} +0.8 & -1.3 & -1.6 & -0.9 & \\ 33 & 17 & 13 & 10 & \end{array}$$

$$\begin{array}{ccccc} -1.0 & -1.8 & -1.8 & -0.2 & -1.0 \\ 16 & 19 & 21 & 22 & 33 \end{array}$$

$$\begin{array}{ccccc} +0.5 & -0.2 & -2.0 & -1.6 & -0.7 \\ 33 & 28 & 23 & 13 & 10 \end{array}$$

$$\begin{array}{ccc} -0.7 & -2.1 & -2.8 \\ 15 & 18 & 33 \end{array}$$

$$\begin{array}{ccccc} +0.1 & -1.8 & -1.6 & -0.9 & \\ 30 & 25 & 16 & 12 & \end{array}$$

$$\begin{array}{ccc} -0.7 & -2.0 & -3.2 \\ 15 & 18 & 33 \end{array}$$

$$\begin{array}{ccccc} +0.8 & +0.5 & -2.0 & -1.7 & -0.7 \\ 33 & 29 & 25 & 18 & 13 \end{array}$$

$$\begin{array}{ccc} -0.7 & -1.8 & -1.3 \\ 14 & 18 & 33 \end{array}$$

$$\begin{array}{ccccc} +2.0 & -0.6 & -1.7 & -2.0 & -1.1 \\ 31 & 26 & 22 & 16 & 13 \end{array}$$

$$\begin{array}{ccc} -1.4 & -3.0 & -4.0 \\ 15 & 20 & 33 \end{array}$$

$$\begin{array}{ccccc} +3.0 & +3.0 & -0.5 & -1.5 & -0.8 \\ 33 & 30 & 24 & 16 & 13 \end{array}$$

$$\begin{array}{ccc} -1.0 & -2.4 & -4.1 \\ 13 & 18 & 33 \end{array}$$

$$\begin{array}{ccccc} +0.5 & +0.7 & -0.6 & -1.6 & -1.0 \\ 33 & 29 & 26 & 16 & 14 \end{array}$$

$$\begin{array}{cc} -0.7 & -4.0 \\ 14 & 33 \end{array}$$

$$\begin{array}{ccccc} -1.2 & -1.2 & 0.0 & -1.0 & \\ 33 & 30 & 17 & 13 & \end{array}$$

$$\begin{array}{ccc} -1.4 & -0.5 & -3.0 \\ 16 & 18 & 33 \end{array}$$

$$\begin{array}{ccccc} -1.7 & -1.7 & -1.0 & -1.0 & \\ 33 & 29 & 16 & 13 & \end{array}$$

$$\begin{array}{ccc} -1.0 & +0.6 & +0.6 \\ 15 & 19 & 33 \end{array}$$

$$\begin{array}{ccccc} -3.3 & -2.8 & -0.8 & & \\ 33 & 27 & 12 & & \end{array}$$

$$\begin{array}{ccc} -0.7 & +3.7 & +3.7 \\ 16 & 23 & 33 \end{array}$$

$$\begin{array}{ccccc} -1.2 & +0.2 & -1.2 & & \\ 33 & 17 & 15 & & \end{array}$$

$$\begin{array}{ccc} 0.0 & +5.8 & +6.3 \\ 17 & 25 & 33 \end{array}$$

Sta.

+50

308.0 ✓

206

306.7 ✓

+50

305.5 ✓

207

304.2 ✓

+50

302.4 ✓

208

300.8 ✓

+50

299.6 ✓

209

298.7 ✓

+25

298.4 ✓

+50

297.9 ✓

+75

298.2 ✓

210

298.6 ✓

+25

298.8 ✓

Lt

E

Rt.

(56)

$$\begin{array}{r} +0.5 \\ 33 \end{array} \quad \begin{array}{r} +1.5 \\ 22 \end{array} \quad \begin{array}{r} -1.6 \\ 17 \end{array}$$

$$\begin{array}{r} +0.2 \\ 16 \end{array} \quad \begin{array}{r} +0.5 \\ 19 \end{array} \quad \begin{array}{r} +7.4 \\ 29 \end{array} \quad \begin{array}{r} +9.4 \\ 33 \end{array}$$

$$\begin{array}{r} +0.5 \\ 33 \end{array} \quad \begin{array}{r} +1.5 \\ 20 \end{array} \quad \begin{array}{r} -1.3 \\ 16 \end{array}$$

$$\begin{array}{r} -0.6 \\ 15 \end{array} \quad \begin{array}{r} +0.5 \\ 19 \end{array} \quad \begin{array}{r} +9.8 \\ 32 \end{array} \quad \begin{array}{r} +9.8 \\ 33 \end{array}$$

$$\begin{array}{r} -2.7 \\ 33 \end{array} \quad \begin{array}{r} -1.8 \\ 19 \end{array} \quad \begin{array}{r} -2.1 \\ 16 \end{array} \quad \begin{array}{r} -1.0 \\ 12 \end{array}$$

$$\begin{array}{r} -1.0 \\ 19 \end{array} \quad \begin{array}{r} +0.2 \\ 22 \end{array} \quad \begin{array}{r} +7.0 \\ 30 \end{array} \quad \begin{array}{r} +7.0 \\ 33 \end{array}$$

$$\begin{array}{r} -5.2 \\ 33 \end{array} \quad \begin{array}{r} -3.0 \\ 23 \end{array} \quad \begin{array}{r} -1.0 \\ 10 \end{array}$$

$$\begin{array}{r} -0.7 \\ 18 \end{array} \quad \begin{array}{r} -0.9 \\ 23 \end{array} \quad \begin{array}{r} +3.2 \\ 29 \end{array} \quad \begin{array}{r} +3.8 \\ 33 \end{array}$$

$$\begin{array}{r} -7.0 \\ 33 \end{array} \quad \begin{array}{r} -3.5 \\ 19 \end{array} \quad \begin{array}{r} -0.8 \\ 11 \end{array}$$

$$\begin{array}{r} -1.1 \\ 24 \end{array} \quad \begin{array}{r} -0.8 \\ 33 \end{array}$$

$$\begin{array}{r} -8.0 \\ 33 \end{array} \quad \begin{array}{r} -4.5 \\ 21 \end{array} \quad \begin{array}{r} -0.9 \\ 10 \end{array}$$

$$\begin{array}{r} -1.0 \\ 15 \end{array} \quad \begin{array}{r} -3.5 \\ 19 \end{array} \quad \begin{array}{r} -4.0 \\ 27 \end{array} \quad \begin{array}{r} -4.2 \\ 30 \end{array} \quad \begin{array}{r} -5.0 \\ 33 \end{array}$$

$$\begin{array}{r} -6.2 \\ 33 \end{array} \quad \begin{array}{r} -4.3 \\ 18 \end{array} \quad \begin{array}{r} -0.7 \\ 10 \end{array}$$

$$\begin{array}{r} -1.0 \\ 15 \end{array} \quad \begin{array}{r} -2.0 \\ 16 \end{array} \quad \begin{array}{r} -2.3 \\ 21 \end{array} \quad \begin{array}{r} -5.1 \\ 21 \end{array} \quad \begin{array}{r} -5.1 \\ 26 \end{array} \quad \begin{array}{r} -3.3 \\ 28 \end{array} \quad \begin{array}{r} -3.3 \\ 33 \end{array}$$

$$\begin{array}{r} -6.5 \\ 33 \end{array} \quad \begin{array}{r} -4.9 \\ 17 \end{array} \quad \begin{array}{r} -0.8 \\ 10 \end{array}$$

$$\begin{array}{r} -0.6 \\ 15 \end{array} \quad \begin{array}{r} -2.9 \\ 20 \end{array} \quad \begin{array}{r} -2.3 \\ 23 \end{array} \quad \begin{array}{r} -4.7 \\ 25 \end{array} \quad \begin{array}{r} -2.4 \\ 30 \end{array}$$

$$\begin{array}{r} -7.2 \\ 33 \end{array} \quad \begin{array}{r} -5.3 \\ 18 \end{array} \quad \begin{array}{r} -1.0 \\ 10 \end{array}$$

$$\begin{array}{r} -0.5 \\ 16 \end{array} \quad \begin{array}{r} -4.9 \\ 25 \end{array} \quad \begin{array}{r} -3.5 \\ 29 \end{array} \quad \begin{array}{r} -4.1 \\ 33 \end{array}$$

$$\begin{array}{r} -6.5 \\ 33 \end{array} \quad \begin{array}{r} -4.2 \\ 16 \end{array} \quad \begin{array}{r} -2.3 \\ 13 \end{array}$$

$$\begin{array}{r} -0.1 \\ 17 \end{array} \quad \begin{array}{r} -3.0 \\ 21 \end{array} \quad \begin{array}{r} -4.2 \\ 27 \end{array} \quad \begin{array}{r} -2.5 \\ 30 \end{array} \quad \begin{array}{r} -3.4 \\ 33 \end{array}$$

$$\begin{array}{r} -6.0 \\ 33 \end{array} \quad \begin{array}{r} -4.1 \\ 16 \end{array} \quad \begin{array}{r} -2.1 \\ 11 \end{array}$$

$$\begin{array}{r} -0.0 \\ 15 \end{array} \quad \begin{array}{r} -1.2 \\ 23 \end{array} \quad \begin{array}{r} -2.3 \\ 30 \end{array} \quad \begin{array}{r} -4.1 \\ 33 \end{array}$$

$$\begin{array}{r} -6.1 \\ 33 \end{array} \quad \begin{array}{r} -4.1 \\ 17 \end{array} \quad \begin{array}{r} -1.4 \\ 13 \end{array}$$

$$\begin{array}{r} -0.6 \\ 14 \end{array} \quad \begin{array}{r} -1.4 \\ 20 \end{array} \quad \begin{array}{r} -3.8 \\ 23 \end{array} \quad \begin{array}{r} -5.5 \\ 33 \end{array}$$

$$\begin{array}{r} -6.0 \\ 33 \end{array} \quad \begin{array}{r} -3.5 \\ 17 \end{array} \quad \begin{array}{r} -1.3 \\ 13 \end{array}$$

$$\begin{array}{r} -1.0 \\ 14 \end{array} \quad \begin{array}{r} -3.5 \\ 20 \end{array} \quad \begin{array}{r} -5.2 \\ 33 \end{array}$$

5+9

+50

298.8 ✓

+834

P.C.

298.8 298.9

211

298.9 ✓

+25

298.9 ✓

+50

299.0 ✓

+75

299.0 ✓

212

299.1 ✓

+276

P.T.

299.0 ✓

+50

298.9 ✓

213

299.0 ✓

+50

299.0 ✓

214

298.9 ✓

+25

299.0 ✓

L

#

Rt.

(57)

$$\begin{array}{ccc} -\frac{5.0}{33} & -\frac{2.8}{16} & -\frac{1.4}{13} \end{array}$$

$$\begin{array}{ccc} -\frac{1.1}{13} & -\frac{3.8}{19} & -\frac{5.1}{33} \end{array}$$

$$\begin{array}{ccc} -\frac{5.1}{33} & -\frac{4.7}{28} & -\frac{2.3}{16} & -\frac{1.1}{13} \end{array}$$

$$\begin{array}{ccc} -\frac{0.9}{10} & -\frac{3.6}{17} & -\frac{5.3}{33} \end{array}$$

$$\begin{array}{ccc} -\frac{4.0}{33} & -\frac{3.7}{20} & -\frac{1.1}{14} \end{array}$$

$$\begin{array}{ccc} -\frac{1.0}{11} & -\frac{3.4}{16} & -\frac{5.0}{33} \end{array}$$

$$\begin{array}{ccc} -\frac{3.2}{33} & -\frac{2.9}{28} & -\frac{1.8}{17} & -\frac{1.8}{13} \end{array}$$

$$\begin{array}{ccc} -\frac{1.5}{12} & -\frac{2.4}{15} & -\frac{4.8}{33} \end{array}$$

$$\begin{array}{ccc} -\frac{2.2}{33} & -\frac{2.0}{24} & -\frac{3.2}{20} & -\frac{0.7}{15} \end{array}$$

$$\begin{array}{ccc} -\frac{1.5}{10} & -\frac{1.5}{15} & -\frac{0.3}{22} & -\frac{2.2}{33} \end{array}$$

$$\begin{array}{ccc} -\frac{2.0}{33} & -\frac{2.2}{24} & -\frac{3.0}{21} & -\frac{1.5}{17} \end{array}$$

$$\begin{array}{ccc} -\frac{0.9}{10} & -\frac{1.1}{33} & \end{array}$$

$$\begin{array}{ccc} -\frac{1.0}{33} & -\frac{1.3}{24} & -\frac{3.0}{22} & -\frac{2.8}{16} & -\frac{1.1}{13} \end{array}$$

$$\begin{array}{ccc} -\frac{1.0}{15} & -\frac{0.3}{25} & -\frac{0.5}{33} \end{array}$$

$$\begin{array}{ccc} -\frac{1.1}{33} & -\frac{1.1}{23} & -\frac{2.9}{21} & -\frac{2.1}{15} & -\frac{1.1}{14} \end{array}$$

$$\begin{array}{ccc} -\frac{0.5}{13} & -\frac{1.2}{18} & -\frac{0.6}{20} & -\frac{0.2}{32} \end{array}$$

$$\begin{array}{ccc} -\frac{1.0}{33} & -\frac{1.2}{23} & -\frac{2.7}{21} & -\frac{2.1}{14} & -\frac{0.8}{12} \end{array}$$

$$\begin{array}{ccc} -\frac{0.7}{13} & -\frac{1.0}{20} & -\frac{0.2}{22} & \frac{0.0}{33} \end{array}$$

$$\begin{array}{ccc} -\frac{1.8}{33} & -\frac{1.5}{23} & -\frac{2.6}{19} & -\frac{2.5}{17} & -\frac{0.8}{13} \end{array}$$

$$\begin{array}{ccc} -\frac{1.0}{12} & -\frac{1.5}{16} & -\frac{1.1}{21} & -\frac{0.4}{24} & -\frac{0.3}{33} \end{array}$$

$$\begin{array}{ccc} -\frac{2.0}{33} & -\frac{1.7}{18} & -\frac{0.8}{10} \end{array}$$

$$\begin{array}{ccc} -\frac{1.0}{14} & -\frac{2.0}{19} & -\frac{2.0}{21} & -\frac{1.3}{22} & -\frac{0.7}{25} & -\frac{0.3}{33} \end{array}$$

$$\begin{array}{ccc} -\frac{2.7}{33} & -\frac{2.3}{21} & -\frac{2.6}{18} & -\frac{0.6}{10} \end{array}$$

$$\begin{array}{ccc} -\frac{0.5}{12} & -\frac{1.8}{16} & -\frac{1.8}{18} & -\frac{0.6}{21} & -\frac{0.4}{33} \end{array}$$

$$\begin{array}{ccc} -\frac{3.5}{33} & -\frac{1.7}{15} & -\frac{0.9}{12} \end{array}$$

$$\begin{array}{ccc} -\frac{1.0}{11} & -\frac{1.8}{18} & -\frac{0.8}{21} & -\frac{0.6}{24} & -\frac{1.7}{33} \end{array}$$

Sta

+50

299.1 ✓

+75

299.3 ✓

215

299.5 ✓

+25

299.4 ✓

+45

P.T.

299.5 ✓

+91.0

P.C.

299.8 ✓

216

299.9 ✓

+25

300.0 ✓

+50

300.1 ✓

+75

300.4 ✓

217

301.2 ✓

+25

302.3 ✓

+50

302.9 ✓

$$\begin{array}{r} -4.0 \\ 33 \end{array} \quad \begin{array}{r} -3.3 \\ 17 \end{array} \quad \begin{array}{r} -0.6 \\ 12 \end{array}$$

$$\begin{array}{r} -0.9 \\ 11 \end{array} \quad \begin{array}{r} -1.0 \\ 12 \end{array} \quad \begin{array}{r} -2.0 \\ 15 \end{array} \quad \begin{array}{r} -1.2 \\ 20 \end{array} \quad \begin{array}{r} -3.7 \\ 28 \end{array}$$

$$\begin{array}{r} -4.8 \\ 33 \end{array} \quad \begin{array}{r} -4.2 \\ 19 \end{array} \quad \begin{array}{r} -0.6 \\ 12 \end{array}$$

$$\begin{array}{r} -1.3 \\ 16 \end{array} \quad \begin{array}{r} -1.0 \\ 21 \end{array} \quad \begin{array}{r} -3.6 \\ 33 \end{array}$$

$$\begin{array}{r} -5.2 \\ 33 \end{array} \quad \begin{array}{r} -0.8 \\ 19 \end{array} \quad \begin{array}{r} -0.5 \\ 12 \end{array}$$

$$\begin{array}{r} -0.8 \\ 13 \end{array} \quad \begin{array}{r} -2.1 \\ 16 \end{array} \quad \begin{array}{r} -2.1 \\ 25 \end{array} \quad \begin{array}{r} -4.0 \\ 33 \end{array}$$

$$\begin{array}{r} -5.4 \\ 33 \end{array} \quad \begin{array}{r} -5.1 \\ 23 \end{array} \quad \begin{array}{r} -4.2 \\ 17 \end{array} \quad \begin{array}{r} -0.9 \\ 11 \end{array}$$

$$\begin{array}{r} -0.3 \\ 13 \end{array} \quad \begin{array}{r} -2.4 \\ 18 \end{array} \quad \begin{array}{r} -3.3 \\ 28 \end{array} \quad \begin{array}{r} -4.6 \\ 33 \end{array}$$

$$\begin{array}{r} -6.0 \\ 33 \end{array} \quad \begin{array}{r} -4.5 \\ 19 \end{array} \quad \begin{array}{r} -1.2 \\ 12 \end{array}$$

$$\begin{array}{r} -0.3 \\ 13 \end{array} \quad \begin{array}{r} -0.7 \\ 17 \end{array} \quad \begin{array}{r} -3.8 \\ 22 \end{array} \quad \begin{array}{r} -4.7 \\ 33 \end{array}$$

$$\begin{array}{r} -6.0 \\ 33 \end{array} \quad \begin{array}{r} -6.0 \\ 27 \end{array} \quad \begin{array}{r} -4.8 \\ 20 \end{array} \quad \begin{array}{r} -1.2 \\ 14 \end{array}$$

$$\begin{array}{r} -0.5 \\ 12 \end{array} \quad \begin{array}{r} -3.7 \\ 23 \end{array} \quad \begin{array}{r} -5.2 \\ 33 \end{array}$$

$$\begin{array}{r} -6.0 \\ 33 \end{array} \quad \begin{array}{r} -6.0 \\ 27 \end{array} \quad \begin{array}{r} -4.8 \\ 20 \end{array} \quad \begin{array}{r} -1.2 \\ 14 \end{array}$$

$$\begin{array}{r} -0.5 \\ 12 \end{array} \quad \begin{array}{r} -3.7 \\ 23 \end{array} \quad \begin{array}{r} -5.2 \\ 33 \end{array}$$

$$\begin{array}{r} -6.3 \\ 33 \end{array} \quad \begin{array}{r} -6.0 \\ 29 \end{array} \quad \begin{array}{r} -5.0 \\ 21 \end{array} \quad \begin{array}{r} -0.8 \\ 13 \end{array}$$

$$\begin{array}{r} -0.7 \\ 11 \end{array} \quad \begin{array}{r} -2.4 \\ 15 \end{array} \quad \begin{array}{r} -4.3 \\ 21 \end{array} \quad \begin{array}{r} -5.2 \\ 33 \end{array}$$

$$\begin{array}{r} -6.1 \\ 33 \end{array} \quad \begin{array}{r} -5.4 \\ 27 \end{array} \quad \begin{array}{r} -4.1 \\ 19 \end{array} \quad \begin{array}{r} -0.7 \\ 12 \end{array}$$

$$\begin{array}{r} -1.3 \\ 12 \end{array} \quad \begin{array}{r} -3.0 \\ 15 \end{array} \quad \begin{array}{r} -4.4 \\ 21 \end{array} \quad \begin{array}{r} -4.5 \\ 33 \end{array}$$

$$\begin{array}{r} -5.2 \\ 33 \end{array} \quad \begin{array}{r} -4.9 \\ 27 \end{array} \quad \begin{array}{r} -3.8 \\ 21 \end{array} \quad \begin{array}{r} -1.1 \\ 16 \end{array} \quad \begin{array}{r} +0.2 \\ 0.4 \end{array}$$

$$\begin{array}{r} -1.6 \\ 11 \end{array} \quad \begin{array}{r} -2.8 \\ 14 \end{array} \quad \begin{array}{r} -3.3 \\ 21 \end{array} \quad \begin{array}{r} -5.2 \\ 28 \end{array} \quad \begin{array}{r} -5.3 \\ 33 \end{array}$$

$$\begin{array}{r} -3.6 \\ 32 \end{array} \quad \begin{array}{r} -3.1 \\ 23 \end{array} \quad \begin{array}{r} -0.7 \\ 17 \end{array}$$

$$\begin{array}{r} -1.1 \\ 11 \end{array} \quad \begin{array}{r} -3.5 \\ 17 \end{array} \quad \begin{array}{r} -5.2 \\ 26 \end{array} \quad \begin{array}{r} -6.4 \\ 33 \end{array}$$

$$\begin{array}{r} -1.0 \\ 33 \end{array} \quad \begin{array}{r} -2.0 \\ 22 \end{array} \quad \begin{array}{r} -0.6 \\ 17 \end{array}$$

$$\begin{array}{r} -0.9 \\ 10 \end{array} \quad \begin{array}{r} -3.8 \\ 17 \end{array} \quad \begin{array}{r} -6.6 \\ 24 \end{array} \quad \begin{array}{r} -6.9 \\ 33 \end{array}$$

$$+5.0 \quad +2.6 \quad +0.4 \quad 0.0 \quad -0.3 \\ 33 \quad 30 \quad 20 \quad 16 \quad 14$$

$$\begin{array}{r} -0.7 \\ 12 \end{array} \quad \begin{array}{r} -4.8 \\ 18 \end{array} \quad \begin{array}{r} -7.2 \\ 24 \end{array} \quad \begin{array}{r} -8.0 \\ 33 \end{array}$$

5+9

+75

304.0 ✓

218

304.8 ✓

+13.2

P.T.

305.3 ✓

+50

306.5 ✓

219

308.3 ✓

+31.9

P.C.

309.4 ✓

+75

310.6 ✓

220

311.5 ✓

+25

312.5 ✓

+50

313.3 ✓

+75

313.7 ✓

221

314.2 ✓

+22.3

P.T.

314.5 ✓

59

$$\begin{array}{r} +9.8 \\ 34 \end{array} \quad \begin{array}{r} +1.4 \\ 20 \end{array} \quad \begin{array}{r} -0.1 \\ 13 \end{array}$$

$$\begin{array}{r} -0.4 \\ 13 \end{array} \quad \begin{array}{r} -8.0 \\ 25 \end{array} \quad \begin{array}{r} -8.8 \\ 33 \end{array}$$

$$\begin{array}{r} +10.1 \\ 33 \end{array} \quad \begin{array}{r} +0.7 \\ 17 \end{array} \quad \begin{array}{r} -0.2 \\ 12 \end{array}$$

$$\begin{array}{r} -0.4 \\ 12 \end{array} \quad \begin{array}{r} -7.7 \\ 24 \end{array} \quad \begin{array}{r} -9.0 \\ 32 \end{array}$$

$$\begin{array}{r} +10.1 \\ 33 \end{array} \quad \begin{array}{r} +0.7 \\ 17 \end{array} \quad \begin{array}{r} -0.2 \\ 12 \end{array}$$

$$\begin{array}{r} -0.4 \\ 12 \end{array} \quad \begin{array}{r} -7.7 \\ 24 \end{array} \quad \begin{array}{r} -9.0 \\ 32 \end{array}$$

$$\begin{array}{r} +4.0 \\ 33 \end{array} \quad \begin{array}{r} +4.8 \\ 30 \end{array} \quad \begin{array}{r} +3.2 \\ 22 \end{array} \quad \begin{array}{r} -0.9 \\ 16 \end{array} \quad \begin{array}{r} -0.4 \\ 10 \end{array}$$

$$\begin{array}{r} -0.8 \\ 13 \end{array} \quad \begin{array}{r} -9.2 \\ 24 \end{array} \quad \begin{array}{r} -11.2 \\ 33 \end{array}$$

$$\begin{array}{r} +1.5 \\ 31 \end{array} \quad \begin{array}{r} +2.0 \\ 22 \end{array} \quad \begin{array}{r} -0.7 \\ 17 \end{array} \quad \begin{array}{r} -1.0 \\ 13 \end{array}$$

$$\begin{array}{r} -0.7 \\ 14 \end{array} \quad \begin{array}{r} -1.1 \\ 20 \end{array} \quad \begin{array}{r} -6.9 \\ 28 \end{array} \quad \begin{array}{r} -8.7 \\ 33 \end{array}$$

$$\begin{array}{r} +3.2 \\ 26 \end{array} \quad \begin{array}{r} +3.0 \\ 25 \end{array} \quad \begin{array}{r} 1.3 \\ 15 \end{array} \quad \begin{array}{r} -1.3 \\ 12 \end{array} \quad \begin{array}{r} -0.7 \\ 6.0 \end{array}$$

$$\begin{array}{r} -0.8 \\ 12 \end{array} \quad \begin{array}{r} -1.5 \\ 16 \end{array} \quad \begin{array}{r} -2.2 \\ 18 \end{array} \quad \begin{array}{r} -1.7 \\ 22 \end{array} \quad \begin{array}{r} -0.4 \\ 26 \end{array} \quad \begin{array}{r} -5.0 \\ 30 \end{array}$$

$$\begin{array}{r} +2.5 \\ 33 \end{array} \quad \begin{array}{r} +2.9 \\ 27 \end{array} \quad \begin{array}{r} +3.4 \\ 22 \end{array} \quad \begin{array}{r} +2.6 \\ 17 \end{array} \quad \begin{array}{r} -0.8 \\ 14 \end{array}$$

$$\begin{array}{r} -0.2 \\ 15 \end{array} \quad \begin{array}{r} -2.5 \\ 21 \end{array} \quad \begin{array}{r} -2.9 \\ 26 \end{array} \quad \begin{array}{r} +0.3 \\ 33 \end{array}$$

$$\begin{array}{r} +1.9 \\ 33 \end{array} \quad \begin{array}{r} +2.5 \\ 24 \end{array} \quad \begin{array}{r} +1.9 \\ 18 \end{array} \quad \begin{array}{r} -1.1 \\ 15 \end{array}$$

$$\begin{array}{r} -0.6 \\ 15 \end{array} \quad \begin{array}{r} -1.8 \\ 21 \end{array} \quad \begin{array}{r} -3.5 \\ 25 \end{array} \quad \begin{array}{r} -3.5 \\ 29 \end{array} \quad \begin{array}{r} -1.0 \\ 33 \end{array}$$

$$\begin{array}{r} +1.9 \\ 33 \end{array} \quad \begin{array}{r} +1.7 \\ 18 \end{array} \quad \begin{array}{r} -0.5 \\ 16 \end{array} \quad \begin{array}{r} -0.9 \\ 13 \end{array}$$

$$\begin{array}{r} -0.6 \\ 15 \end{array} \quad \begin{array}{r} -3.0 \\ 21 \end{array} \quad \begin{array}{r} -3.6 \\ 27 \end{array} \quad \begin{array}{r} -1.5 \\ 29 \end{array} \quad \begin{array}{r} -1.5 \\ 29 \end{array}$$

$$\begin{array}{r} +2.7 \\ 33 \end{array} \quad \begin{array}{r} +3.2 \\ 23 \end{array} \quad \begin{array}{r} -0.8 \\ 20 \end{array} \quad \begin{array}{r} -0.8 \\ 17 \end{array}$$

$$\begin{array}{r} -0.8 \\ 12 \end{array} \quad \begin{array}{r} -1.7 \\ 16 \end{array} \quad \begin{array}{r} -3.4 \\ 33 \end{array}$$

$$\begin{array}{r} +4.3 \\ 33 \end{array} \quad \begin{array}{r} +4.2 \\ 26 \end{array} \quad \begin{array}{r} -0.6 \\ 21 \end{array} \quad \begin{array}{r} -0.6 \\ 16 \end{array}$$

$$\begin{array}{r} -0.2 \\ 9.0 \end{array} \quad \begin{array}{r} -3.1 \\ 15 \end{array} \quad \begin{array}{r} -3.3 \\ 20 \end{array} \quad \begin{array}{r} -2.5 \\ 21 \end{array} \quad \begin{array}{r} -3.8 \\ 23 \end{array}$$

$$\begin{array}{r} +6.3 \\ 33 \end{array} \quad \begin{array}{r} +5.3 \\ 28 \end{array} \quad \begin{array}{r} -0.4 \\ 23 \end{array} \quad \begin{array}{r} -0.4 \\ 18 \end{array}$$

$$\begin{array}{r} -0.7 \\ 10 \end{array} \quad \begin{array}{r} -3.1 \\ 15 \end{array} \quad \begin{array}{r} -3.5 \\ 19 \end{array} \quad \begin{array}{r} -2.5 \\ 20 \end{array} \quad \begin{array}{r} -4.5 \\ 33 \end{array}$$

$$\begin{array}{r} +7.0 \\ 33 \end{array} \quad \begin{array}{r} +6.5 \\ 27 \end{array} \quad \begin{array}{r} -0.6 \\ 22 \end{array} \quad \begin{array}{r} -0.6 \\ 11 \end{array}$$

$$\begin{array}{r} -0.4 \\ 10 \end{array} \quad \begin{array}{r} -1.3 \\ 14 \end{array} \quad \begin{array}{r} -2.0 \\ 17 \end{array} \quad \begin{array}{r} -2.3 \\ 22 \end{array} \quad \begin{array}{r} -1.6 \\ 25 \end{array} \quad \begin{array}{r} -3.9 \\ 33 \end{array}$$

5+9

+50

314.9 ✓

222

314.8 ✓

+50

314.3 ✓

223

313.5 ✓

+50

312.3 ✓

224

310.7 ✓

+50

309.1 ✓

225

307.5 ✓

+50

306.0 ✓

226

304.7 ✓

+50

303.2 ✓

227

302.0 ✓

+50

301.1 ✓

60

$$\begin{array}{r} +7.6 \\ 33 \end{array} \quad \begin{array}{r} +7.0 \\ 26 \end{array} \quad \begin{array}{r} -1.0 \\ 19 \end{array} \quad \begin{array}{r} -1.0 \\ 14 \end{array}$$

$$\begin{array}{r} -0.7 \\ 16 \end{array} \quad \begin{array}{r} -1.8 \\ 20 \end{array} \quad \begin{array}{r} -2.0 \\ 22 \end{array} \quad \begin{array}{r} -1.0 \\ 23 \end{array} \quad \begin{array}{r} -2.0 \\ 29 \end{array} \quad \begin{array}{r} -2.0 \\ 33 \end{array}$$

$$\begin{array}{r} +7.9 \\ 33 \end{array} \quad \begin{array}{r} +7.7 \\ 27 \end{array} \quad \begin{array}{r} -0.8 \\ 17 \end{array} \quad \begin{array}{r} -0.8 \\ 12 \end{array}$$

$$\begin{array}{r} +0.1 \\ 7.0 \end{array} \quad \begin{array}{r} -1.0 \\ 20 \end{array} \quad \begin{array}{r} -2.0 \\ 34 \end{array}$$

$$\begin{array}{r} +8.8 \\ 33 \end{array} \quad \begin{array}{r} +8.8 \\ 30 \end{array} \quad \begin{array}{r} -0.7 \\ 16 \end{array} \quad \begin{array}{r} -0.7 \\ 8.0 \end{array}$$

$$\begin{array}{r} -0.6 \\ 16 \end{array} \quad \begin{array}{r} -1.0 \\ 22 \end{array} \quad \begin{array}{r} -0.6 \\ 33 \end{array}$$

$$\begin{array}{r} +11.3 \\ 30 \end{array} \quad \begin{array}{r} -0.6 \\ 18 \end{array} \quad \begin{array}{r} -0.6 \\ 8.0 \end{array}$$

$$\begin{array}{r} -0.3 \\ 14 \end{array} \quad \begin{array}{r} -1.5 \\ 27 \end{array} \quad \begin{array}{r} +1.0 \\ 30 \end{array} \quad \begin{array}{r} +1.2 \\ 33 \end{array}$$

$$\begin{array}{r} +14.2 \\ 33 \end{array} \quad \begin{array}{r} -0.5 \\ 17 \end{array} \quad \begin{array}{r} -0.5 \\ 4.0 \end{array}$$

$$\begin{array}{r} 0.0 \\ 8.0 \end{array} \quad \begin{array}{r} -1.0 \\ 24 \end{array} \quad \begin{array}{r} -1.5 \\ 30 \end{array} \quad \begin{array}{r} 0.0 \\ 32 \end{array}$$

$$\begin{array}{r} +16.2 \\ 40 \end{array} \quad \begin{array}{r} -0.5 \\ 16 \end{array} \quad \begin{array}{r} -0.3 \\ 4.0 \end{array}$$

$$\begin{array}{r} -0.3 \\ 10 \end{array} \quad \begin{array}{r} -0.5 \\ 32 \end{array} \quad \begin{array}{r} -0.3 \\ 33 \end{array}$$

$$\begin{array}{r} +13.2 \\ 34 \end{array} \quad \begin{array}{r} -0.5 \\ 14 \end{array}$$

$$\begin{array}{r} -0.2 \\ 8.0 \end{array} \quad \begin{array}{r} -1.2 \\ 25 \end{array} \quad \begin{array}{r} -1.0 \\ 33 \end{array}$$

$$\begin{array}{r} +8.3 \\ 33 \end{array} \quad \begin{array}{r} +7.0 \\ 27 \end{array} \quad \begin{array}{r} -0.7 \\ 16 \end{array}$$

$$\begin{array}{r} 0.0 \\ 6.0 \end{array} \quad \begin{array}{r} -2.0 \\ 27 \end{array} \quad \begin{array}{r} -2.0 \\ 33 \end{array}$$

$$\begin{array}{r} +2.7 \\ 33 \end{array} \quad \begin{array}{r} +2.0 \\ 29 \end{array} \quad \begin{array}{r} +0.4 \\ 23 \end{array} \quad \begin{array}{r} -2.0 \\ 15 \end{array} \quad \begin{array}{r} -2.1 \\ 14 \end{array} \quad \begin{array}{r} -0.8 \\ 10 \end{array}$$

$$\begin{array}{r} -0.1 \\ 7.0 \end{array} \quad \begin{array}{r} -0.8 \\ 15 \end{array} \quad \begin{array}{r} -3.0 \\ 23 \end{array} \quad \begin{array}{r} -4.0 \\ 33 \end{array}$$

$$\begin{array}{r} -4.2 \\ 33 \end{array} \quad \begin{array}{r} -3.5 \\ 15 \end{array} \quad \begin{array}{r} -0.7 \\ 10 \end{array}$$

$$\begin{array}{r} -0.2 \\ 7.0 \end{array} \quad \begin{array}{r} -0.9 \\ 15 \end{array} \quad \begin{array}{r} -2.0 \\ 33 \end{array}$$

$$\begin{array}{r} -6.3 \\ 33 \end{array} \quad \begin{array}{r} -5.7 \\ 18 \end{array} \quad \begin{array}{r} -0.7 \\ 10 \end{array}$$

$$\begin{array}{r} 0.0 \\ 5 \end{array} \quad \begin{array}{r} -0.7 \\ 16 \end{array} \quad \begin{array}{r} -6.7 \\ 28 \end{array} \quad \begin{array}{r} -7.5 \\ 33 \end{array}$$

$$\begin{array}{r} -7.0 \\ 33 \end{array} \quad \begin{array}{r} -5.9 \\ 16 \end{array} \quad \begin{array}{r} -0.8 \\ 10 \end{array}$$

$$\begin{array}{r} -0.6 \\ 16 \end{array} \quad \begin{array}{r} -5.9 \\ 24 \end{array} \quad \begin{array}{r} -6.4 \\ 33 \end{array}$$

$$\begin{array}{r} -6.3 \\ 34 \end{array} \quad \begin{array}{r} -5.3 \\ 18 \end{array} \quad \begin{array}{r} -0.9 \\ 10 \end{array}$$

$$\begin{array}{r} -0.5 \\ 14 \end{array} \quad \begin{array}{r} -4.5 \\ 20 \end{array} \quad \begin{array}{r} -5.0 \\ 33 \end{array}$$

Sta

228

300.4 ✓

+50

300.1 ✓

229

300.0 ✓

+50

299.6 ✓

230

299.7 ✓

+50

299.7 ✓

231

299.7 ✓

+50

299.8 ✓

232 ✓

300.2 ✓

+50

300.3 ✓

233

300.3 ✓

+50

300.4 ✓

234

300.6 ✓

+50

300.8 ✓

21.

#

RT.

(61)

-3.7 -3.7 -0.4
33 18 10

-0.6 -3.6 -3.6 5.3 -4.0
15 28 27 29 33

3.4
-2.4 -2.4 -0.5
33 16 8

-0.3 -2.0 -2.3 -4.0 -2.6
16 17 27 30 33

-2.0 -2.7 -0.6
32 16 11

-0.8 -2.7 -4.8 -2.5 -2.2
16 21 24 28 33

-2.0 -2.5 -0.5
33 16 11

-0.8 -2.1 -2.1
16 30 33

-2.8 -2.7 -0.8
33 17 12

-0.5 -2.7 -3.5
18 19 33

-3.1 -3.1 -0.7
33 16 12

-0.5 -2.5 -3.2 -3.7 -3.3 -3.3
14 18 22 24 25 33

-3.1 -3.1 -0.7
33 15 10

-0.7 -2.5 -2.9 -3.5 -3.2 -3.0
15 17 20 23 24 33

-2.5 -2.3 -0.6
33 15 11

-0.7 -2.0 -2.6 -3.6 -2.5 -2.5
15 19 21 23 25 33

-2.1 -1.8 -0.7
33 15 12

-0.7 -2.0 -3.8 -1.9 -1.8
16 20 23 24 33

-1.5 -0.6
33 9

-0.6 -2.1 -3.3 -3.3 -1.9 -1.9
16 21 22 24 26 33

-1.1 -1.1 -0.5
33 19 10

-0.5 -1.4 -3.3 -3.3 -1.5 -1.5
16 21 22 24 25 33

-1.5 -1.5 -0.8
33 19 12

-0.5 -1.7
15 33

-1.7 -1.7 -0.7
33 13 12

-0.6 -1.7 -4.0 -4.0 -2.0 -2.1
12 16 19 21 24 33

-1.6 -1.5 -0.8
33 15 11

-1.0 -2.6 -4.2 -4.2 -2.5 -2.4
14 18 19 21 24 33

235

300.9 ✓

+50

301.0 ✓

236

301.2 ✓

+50

301.0 ✓

237

300.9 ✓

+50

300.0 ✓

238

299.7 ✓

+50

299.0 ✓

239

298.2 ✓

+50

297.9 ✓

240

297.8 ✓

+50

298.0 ✓

241

297.9 ✓

+50

297.7 ✓

62

-0.4 -0.8 -1.5 -1.7 -0.7
33 24 20 16 12

-0.7 -3.0 -4.5 -4.5 -2.4 -2.6
12 18 19 22 24 33

-0.7 -0.7 -2.0 -2.0 -1.0
33 26 20 15 12

-0.8 -2.0 -4.4 -4.4 -2.2 -3.0
13 17 19 22 24 33

-0.5 -0.8 -2.0 -0.8
33 25 16 14

-0.6 -3.0 -4.4 -4.4 -3.0 -2.4
13 17 18 21 25 33

20 -1.0 -1.7 -0.8
31 25 14 12

-0.5 -2.3 -4.0 -4.4 -1.2 -1.6 -2.2
14 18 19 23 26 30 33

-0.7 -0.7 -0.4
33 17 11

-0.2 -0.6 -0.6
10 26 33

+0.3 +0.3 -2.8 -2.9 -0.7
33 27 23 16 12

-0.6 -1.0 -0.7
10 19 33

20 20 -2.8 -2.8 -1.0
33 28 24 16 13

-1.0 -3.0 -3.0 -0.4 -0.2
12 17 19 22 33

-2.0 -3.0 -2.4 -0.7
32 29 16 13

-1.0 -2.7 -2.7 -1.3 -1.3
12 15 17 19 33

-4.5 -4.5 -4.2 -0.8
33 24 18 12

-0.8 -4.0 -2.8
13 17 33

-3.2 -3.2 -4.5 -4.5 -3.4 -3.2 -0.8
33 30 28 26 23 17 13

-1.0 -4.0 -1.2
12 18 33

-2.9 -2.7 -1.5
33 20 15

-0.8 -2.3 -3.2
11 15 33

-1.4 -1.3 -0.8
33 21 15

-0.8 -1.9
11 33

+2.0 -1.6 -1.8 -0.8
33 28 21 12

-0.6 -1.5 -1.7 -0.0 -0.4
11 16 18 21 33

+1.0 +1.0 -2.3 -2.0 -0.8
33 30 25 17 14

-0.8 -1.7 -1.7 -0.7 -1.0 -1.6
12 16 18 19 29 33

242

298.0 ✓

+50

298.0 ✓

243

298.1 ✓

+50

298.2 ✓

244

298.5 ✓

+50

299.1 ✓

245

299.4 ✓

+50

300.0 ✓

246

300.1 ✓

+50

300.5 ✓

247

300.8 ✓

+50

300.9 ✓

248

300.9 ✓

+50

300.9 ✓

-1.8 -2.6 -2.4 -1.0
33 21 18 15

-0.5 -2.8 -2.8
13 17 33

-2.3 -2.5 -0.5
33 21 16

-0.8 -3.0 -3.6 -3.6
12 17 21 36

-2.3 -2.0 -0.5
33 21 17

-0.6 -2.5 -3.1
11 16 33

-0.8 -2.1 -0.5
33 21 17

-0.6 -2.7 -3.0
12 18 33

-3.2 -2.7 -2.5 -1.0
33 26 23 19

-0.8 -1.9 -1.2
14 18 31

-2.1 -2.3 -0.8
34 21 16

-0.8 -2.7 -2.7 -1.9 -0.8
12 16 20 21 34

-1.2

33 -1.2 -2.4 -2.2 -1.1 -0.4
25 24 19 18 9

-0.8 -2.3 -2.4 0.0 +0.5
13 18 24 27 33

-1.6 -2.3 -2.0 -0.8
33 24 17 12

-0.7 -2.3 -2.5 +1.0 +1.0
14 18 23 28 33

-1.3 -2.0 -1.5 -0.5
33 24 16 12

-0.8 -2.0 -2.5 -2.0 -2.4
13 18 22 26 33

-1.9 -1.7 -0.4
33 14 11

-0.7 -2.4 -3.8
12 18 33

-0.8 -0.8 -0.3
33 25 13

+0.1 -3.1 -3.1
12 19 33

+2.0 +0.9 -4.4 -1.4 -0.3
33 27 26 15 12

-0.6 -1.7 -2.3
12 16 33

+3.5 +2.8 -1.5 -1.7 -1.0
33 28 24 15 12

-0.4 -1.2 -1.8 -2.4 +1.8
13 17 20 29 35

-1.2 -1.5 -0.7
33 25 12

-0.4 -1.2 -1.1 -2.0 +0.5 +0.5
13 16 21 25 31 33

249

300.9 ✓

+50

301.0 ✓

250

301.2 ✓

+50

301.0 ✓

251

300.7 ✓

+50

300.6 ✓

252 ✓

300.4 ✓

+50

300.2 ✓

253

300.6 ✓

+50

301.1 ✓

254

301.9 ✓

+50

302.7 ✓

255

303.3 ✓

+50

303.8 ✓ 303.9

(64)

-3.7 -3.1 -0.8 -0.8 -2.6 -3.3 -2.8
33 16 12 14 18 27 33

-2.8 -2.4 -2.4 -0.5 -0.8 -2.1 -2.7 -1.7
33 25 16 11 15 17 23 33

-0.2 -0.2 -1.2 -2.3 -2.4 -1.0 -0.9 -2.9 -2.6 -0.2
33 30 22 20 16 14 14 19 29 35

+0.2 +0.2 -3.2 -2.1 -0.8 -0.5 -2.3 -1.8 -0.2
33 28 23 16 12 14 18 29 33

-1.0 -1.0 -3.8 -4.0 -0.5 -0.7 -2.5 -3.0 -0.9
33 30 25 18 11 13 17 28 33

-3.6 -3.6 -4.5 -4.4 -3.8 -3.1 -0.7 -0.5 -4.0 -4.6 -4.6
33 26 24 19 17 14 9 13 19 23 33

-5.0 -5.0 -4.3 -0.5 -0.5 -4.5 -5.2 -5.2
33 26 17 12 13 20 24 33

-4.9 -4.9 -4.5 -0.7 -0.5 -4.3 -5.2 -5.2
33 25 18 10 13 20 25 33

-5.0 -5.0 -4.2 -0.6 -0.7 -4.5 -5.2 -5.2
33 26 17 11 13 20 25 33

-5.3 -5.3 -4.5 -1.0 -0.6 -4.4 -5.4 -5.4
33 25 16 10 13 20 25 33

-1.5 -3.2 -2.7 -0.5 -0.9 -4.7 -5.3 -5.3
33 24 17 11 14 23 25 33

+1.8 -2.3 -3.0 -2.5 -0.8 -0.7 -2.0 -3.0 -3.0
33 27 24 17 12 12 20 30 33

+2.5 -2.4 -2.6 -0.8 -0.6 -1.5 -1.5
33 26 16 10 12 18 33

+2.1 -2.2 -3.1 -1.3 -0.3 -0.5
33 24 16 11 10 33

286

304.0 ✓

+ 50

304.1 ✓

+ 75

304.0 ✓

+ 81

304.0 ✓

257

303.9 ✓

65

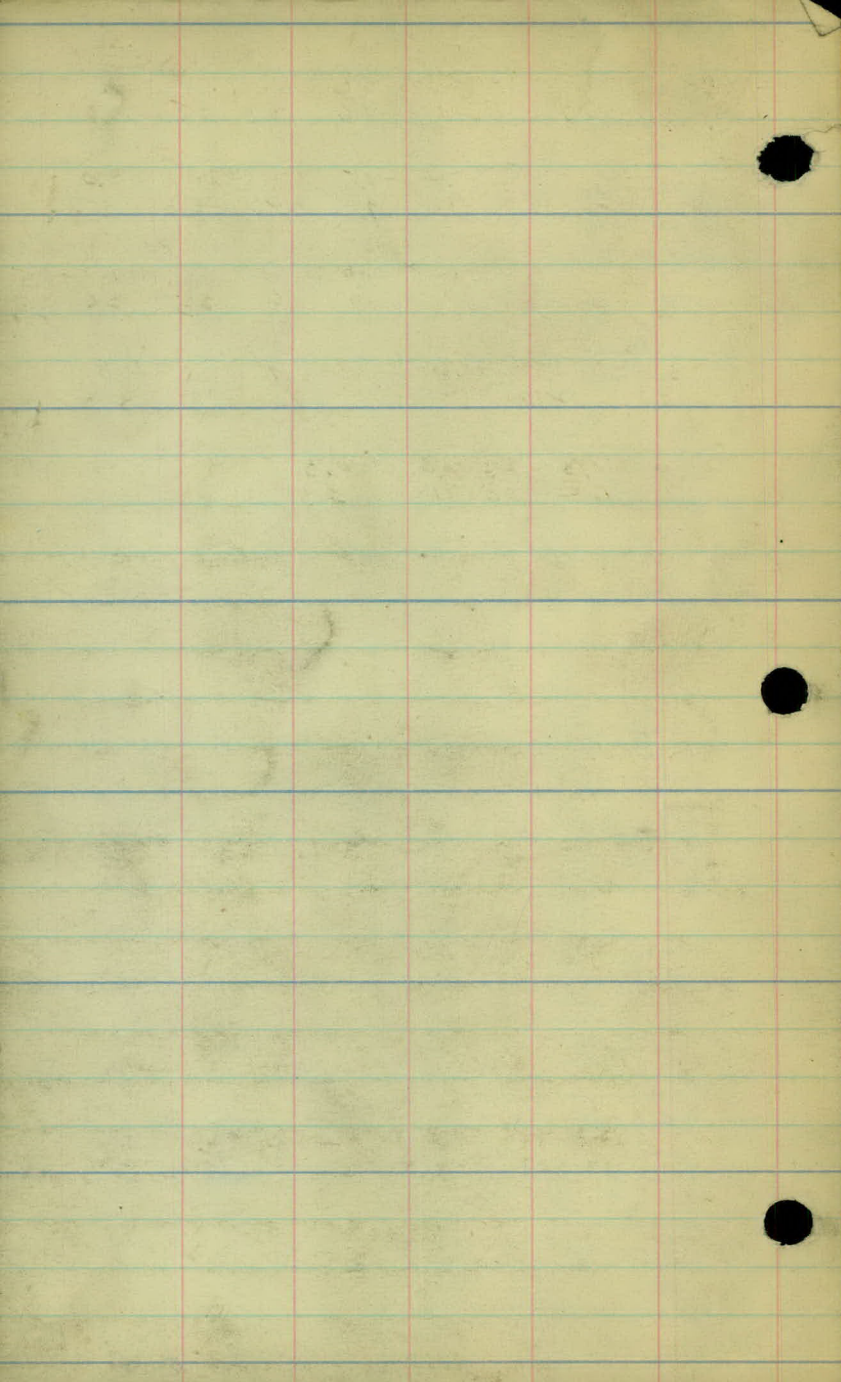
+3.5 +3.5 -2.8 -3.0 -0.8 -0.6 -0.6 +2.1 +2.1
33 30 23 15 11 16 21 28 31

+1.3 -1.0 -1.5 -0.4 -0.5 -0.7 +3.0 +3.0
33 26 15 7 9 20 28 33

+3.4 -1.8 -1.6 -0.4 -1.0 -0.6 +1.3 +1.3
33 23 14 9 16 23 26 33

+3.4 -1.8 -1.6 -0.9 -0.8
33 23 14 16 33

+3.0 -0.3 -2.1 -0.6 -0.3
33 24 16 11 33



Ref # 24 Sep 22

R.J.W.
H.D.V.K.
M.W.C.

1+50 L. Sheet no Culv. Reg.

4+50 - L. Pl. - 12" X 22' C.M.

5+00 - R. F.E. - Pl. 12" X 24' C.M.

6+10 - Leave Tree on L. -

6+75 - P. 18" C.M. - Drains L

8+00 - L - Ext. - P. 12" X 24' C.M. -

Lower Grade from Sta 2+00 to 8

Narrow Ditch on L. from (4+50)
Town Section ditch. - (10+50)

8+50 L. St. P. - 12" X 24' C.M.

9+90 $\frac{1}{2}$ Inp 10" X 20" C.M. Rem^d Rep.

10+45 Inp 10" X 16" C.M. Rem^d P 12" X 24'

12+25 - F.E. R. - ~~P 12" X 50' C.M.~~ -

12+50 to 14+50 Ditch Gr. ahead on R. -

Lower Grade 11+40 to 18

No not widens on L 9/10 of trees

14+60 - P - 24" x P3 Drain L.

Town Sec. on L - 15+00 to 18+00

15+58 - L No Cul. Req.

16+40 - Garage Ent. L. no Cul. Req.

17+20 - Ent. L - P 12" x 24" C.M.

18+00 Garage Ent L - P 12" x 24" C.M.

19+70 F.E. shown in truck

22+30 F.E. R - Imp 15" x 26" O.K. -

23+00 + 32+00 Lower Grade
widens fill to take dirt

30+00 No Cul. Req.

32+30 L - Imp 10" x 24" - O.K.

32+00 to 36+00 - Put 2' x 8' bitul
on L. -

36 to 38 Lower Grade slightly

34+00 - L - Lys 10" x 26' O.K.

34+65 - L - Lys 10' x 24 O.K.

35+90 L. - No Cals. Reg. -

37+70 - L - Lys 10" x 24' O.K.

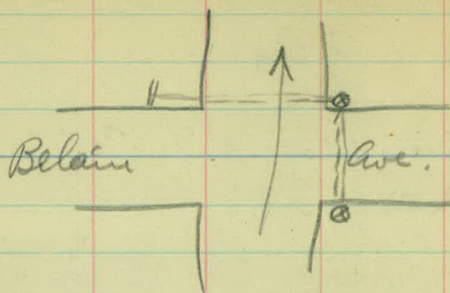
38 to 42 - Same pitch as 32 to 36 -

39+50 - L. - Lys 10" x 24' O.K.

40+30 - L. - 10" x 24 C.M. Lys O.K.

41+70 - L. P - 12" x 24' C.M. -

Lower Grade slightly between 42
and 44 - widen to get rid of dirt. -



Lower Grade 44+50 to 47

47+50 - Ent. L. - P-12" X 24" C. M.

48+00 - Ent. L. - P-12" X 24" C. M.

48+50 - Ent. L. No Cul. Req.

49+00 R, ²/₄ L. - P-12" X 24" C. M.

50+80 Ent. R. - P-12" X 20" C. M.

51+20 2-Ent. L. - P-12" X 40" C. M.

52+20 - Ent. L. - - P-12" X 20" C. M.

52+75 - 2 Ent. L. - No Cul. Req.

53+60 - R. - No Culo. Reg.

54+20^L - L. - 10" X 18' C.M. - O.K.

54+85^L - L. - 10" X 18' C.M. - O.K.

55+60^L - L. - L. - 10" X 18' C.M. - Remove
P - 12" X 20' C.M. -

56+15^R - R. - P. 12" X 20' C.M. each -

56+75^L - L. - P. 12" X 20' C.M. -

57+75^R - R - P - 15" X 30' C.M. -

58+30^P - P - 18" X C.M. Drains L. -

58+65^R - R - No Culo. Reg.

" " L. - No Culo. Reg.

59+30^R - R - P 12" X 20' C.M.

59+90^L - L - No Culo. Reg.

61+50^R - R - P 15" X 40'

62+50^L - L - L. - 10" X 16' C.M. - Remove
P - 12" X 20' C.M.

63+85 - L. - No Culo. - Reg.

64+15 - R. - P - 15" X 40' C.M. -

64+15 L. - No Culo. Reg. -

65+10 - L. - Imp. - 10" X 14' C.M. Rem.
P - 12" X 20' C.M.

65+80 L - 10" X 18' C.M. - O.K.

64+00 to 78 - ^{change} ~~to~~ Grade

67+00 - R. - Imp - 10" X 18' C.M. O.K.

67+20 - L. Imp - 10" X 18' C.M. - O.K.

67+90 - L. - Imp. - 12" X 16' C.M. - O.K.

68+30 - R. - P. - 12" X 24' C.M.

68+35 - L. - Imp. - 12" X 24' O.K. -

69+20 L. - Imp. - 12" X 30' C.M. O.K.

70+50 L. - Imp 12" X 12' C.M. O.K.

71+50 Imp - 24" X 64' C.M. O.K.

79+00 - L. - P - 18" X 40' C.M. -

80+85 - L. - Imp - 12" X 70' Vit. Pipe O.K.
~~Imp~~

81+00 - R. Imp - 12" X 34' C.M. - O.K. -
P - 18" X 36' C.M.

84+10 - R. P - 15" X 24' C.M.

84+70 - L. - Imp. - 10" X 30' Vit. P. - Remove
P - 15" X 30' C.M.

85+70 - R. - Imp - 12" X 12' Vit. Pipe Rem. -
P - 15" X 24' C.M.

86+50 L. Imp - 12" X 22' Vit. Pipe - O.K. -

87+50 R. Imp. 10" X 18' Vit. Pipe Rem.
P. 12" X 24' C.M.

88+00 L. Imp. - 12" X 30. - Vit Pipe. - O.K. -

89+00 R. 12" X 40' C.M. Imp. - O.K. -

89+60-L, 12" X 30' Vit. Pipe - O.K.

92+15 R. No Culo. Reg. -

94+25 - L. - P. 12" X 30' C.M. -

~~100+15 - Lower and wider Grade~~

99+50 F.F. R. - No Culo. Reg. -

100+80 F.F. L. " "

104+40 - P-24" X P₃ Drains R. -

(109+80) - Imp - 8" X 44' Vit. Pipe Rem. -
P-24" P₃ Drains R. -

111+60 - L - No Culo. Reg. -

115+20 - R. - " "

128+10 - Imp 15" X 50' Vit. Pipe Remove
P-24" X P₃ -

30.15	30.45
4.50	10.15
259	
16.78	
	4060

13.91 54.02

17.57

61.82

9.80	14.10
59.85	2.75

69.60	19.65	4.50
17.39	15.13	2135
86.99	84.78	

3.85
38.10
28.28

21.13
8.00
10.45
260
64.53

70.20

32.60
22.60

5

83 21.90
36.15 4.15
30.45 2606
5.50

10.50
1.58
33.82
45.90

8293

3.85
52.20
5605

56.70
4

4.00
9.63
22.80
31.43

C. Rd E. - 24" X 18 on R. -
No Carb. Reg. on L. -

136+10 - L. - No Carb. Reg. -

137+75 - L - No Carb. Reg. -

138+10 - R. - P- 12" X 24' C.M.,

140+70 - Inp 15" X 50' Vit Pipe then
P. 24" X P₂ -

144+65 - R²/L. - P- 2 - 12" X 24' C.M.

150+30 - L - P 12" X 40' C.M. -

154+50 - L - P 12" X 44' C.M. -

157+40 - Inp 15" X 41' Vit. Pipe - Remove
Place 24" X P₃

163+30 Inp 15" X 36' Vit. Pipe Ren.-
P₁ - 24" P₃

165+80 - F.E. L. - P- 12" X 30' C.M.

- 167+30 Imp. - 12" X 30' V.I. Pipe Rem.
No Culv. Req.
- 170+50 Imp 12" X 50' V.I. Pipe Rem.
P-24" P₃
- 179+30 Imp 12" X 42' V.I. Pipe - Rem.
P-24" P₃
- 183+90 Imp 12" X 40' V.I. Pipe Rem.
No Culv. Req.
- 185+00 F.E. - L No Culv. Req.
County Road "D." No Culv. Req.
- 190+10 F.E.L. - P-12" X 24' C.M. -
- 192+50 - P-24" X P₃
- 197+20 F.E. - R - P 12" X 24' C.M.
- 198+20 Imp 12" X 48' V.I. Pipe Rem.
P-24" X
- 202+15 - F.E. R²/L. P-12" X 24' C.M. - L
No Culv. Req. R₁

213+50 F.E. L- No Cub. Reg.

214+45- R- No Cub. Reg.

216+90- R. " " "

217+43- Lnp 12" Iron Pipe Remove.

218+75- F.E. L- P 12" X 24' C.M. -

220+25- F.E. L- P 12" X 24' C.M. -

220+50- F.E. R- P- 12" X 20' C.M.

↖ Lnp 8" X 12' Vit. Pipe

221+95- Ent. R- ~~No Cub. Reg.~~
~~P 12" X 20' C.M.~~

222+50- " R- P 12" X 20' C.M.

223+65- " R- P 12" X 20' C.M.

224+40- " R- P. 12" X 20' C.M. -

225+30- " R- P- 12" X 20' C.M. -

225+65 L. - P 12" x 24' C. M.

225+90 R. - Imp. - 12" 16' C. M. O.K.

227+30 - P - 24" XP3 - Egn. -

227+75 - FE. R. - No Curb. Reg.

229+60 - Sh. R. - Imp 12" x 40' Vnt Pipe
P. - 15" x 40' C. M. -

233+30 - Sh. R. - FE. L. - - P. - 15" x 50' C. M. R.
P. - 12" x 24' C. M. L. -

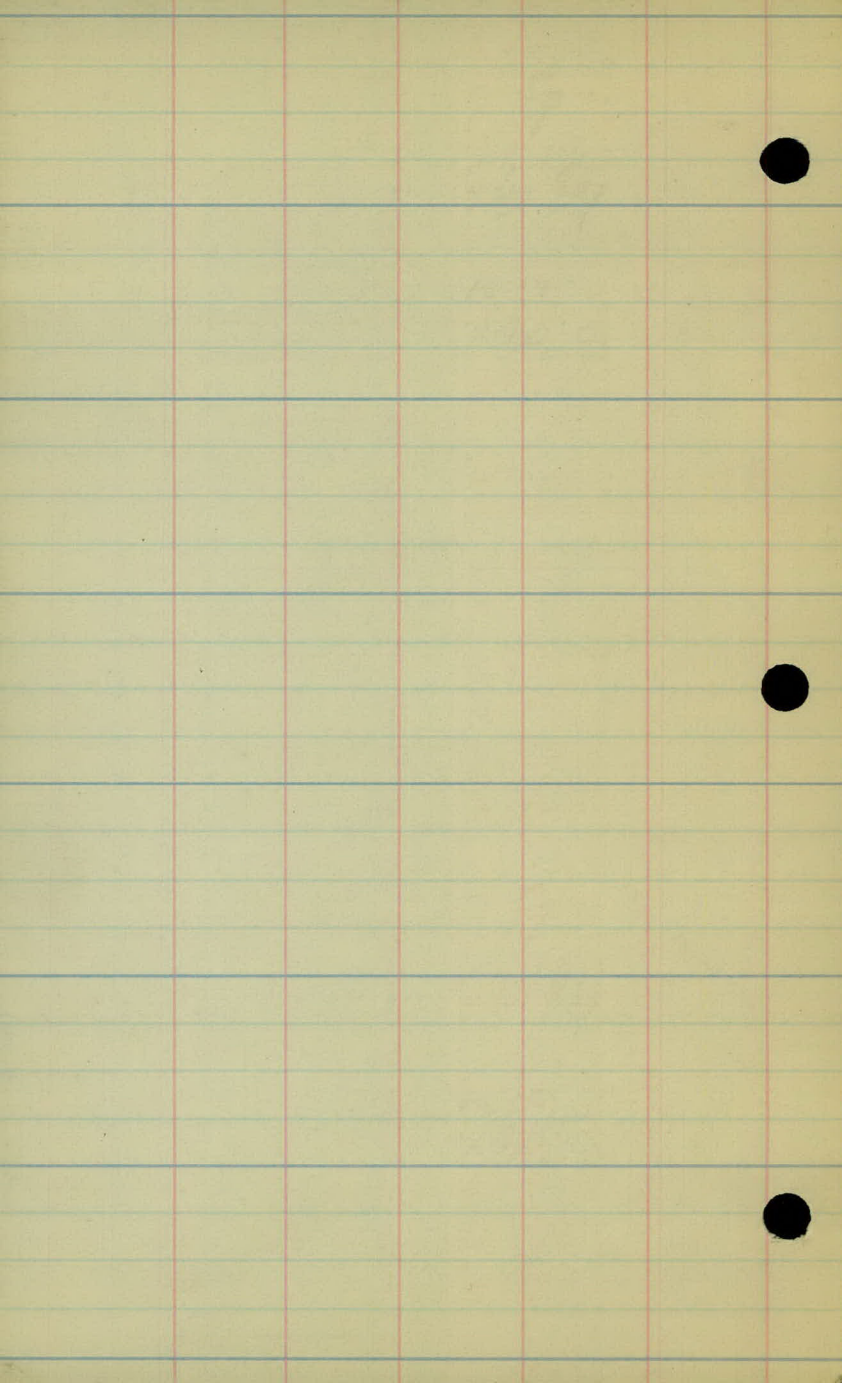
234+70 - FE. L. - P 12" x 24' C. M.

5-2-24

N.D.C.

Proj. 27-58

4/30/24



Average Tax - Motor Vehicle

1922 - 16.11

1923 - 16.93

1924 - 16.23 1st 7000 cars

4 cyl. car	\$ 17 ⁰⁶	- ave, U.S.	Ford	9 Minn.	16 ⁹⁴
" " "	\$ 24 ⁵⁰	" "	Dodge		
6 "	\$ 31 ³⁸	" "	Buick		
8 " "	58 ³⁶	" "	Cadillac		55 ²⁴
12 " "	76 ³⁸	" "	Packard	5	74 ¹¹

Paving in 1923

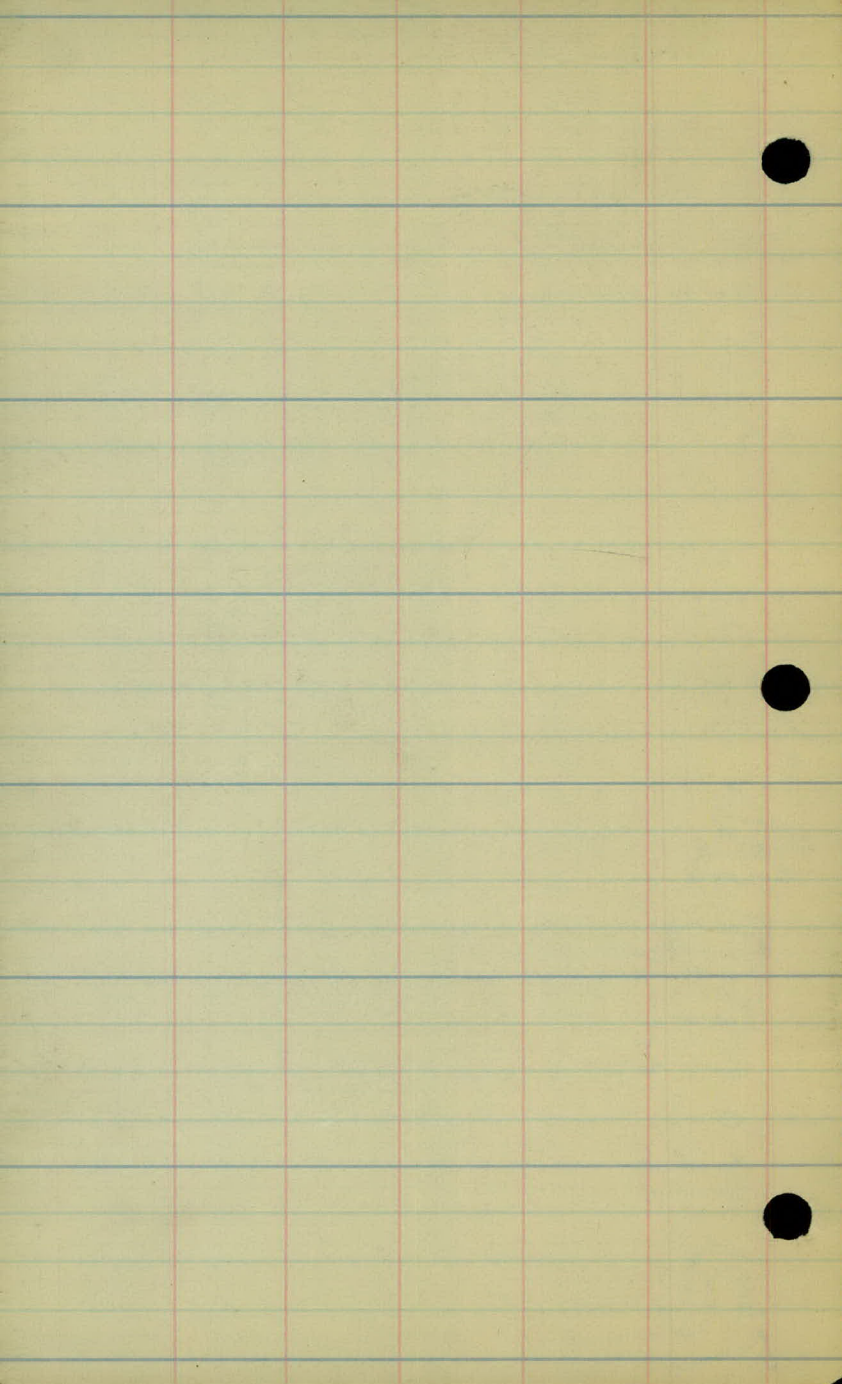
42 mi. Minn.

430 mi. Wis.

1077 " Ill.

Conservation of Gravel Deposits

The gravel deposits in some sections of the state are being used up on heavily traveled trunk highway, these trunk highways should be paved.



Acquiring R/W for Road Purposes

Co. may expend money directly on towns designated by town boards. Town boards may expend money on county roads and the money shall be placed in the R & B. fund. (State law - recent)

Highway Dept. secures easements where possible,

In proceedings where County condemns, the Co. Board acts as the appraising committee and determines the benefit & damage.

Handed
Shigley

T-O.R. Van Krevelen

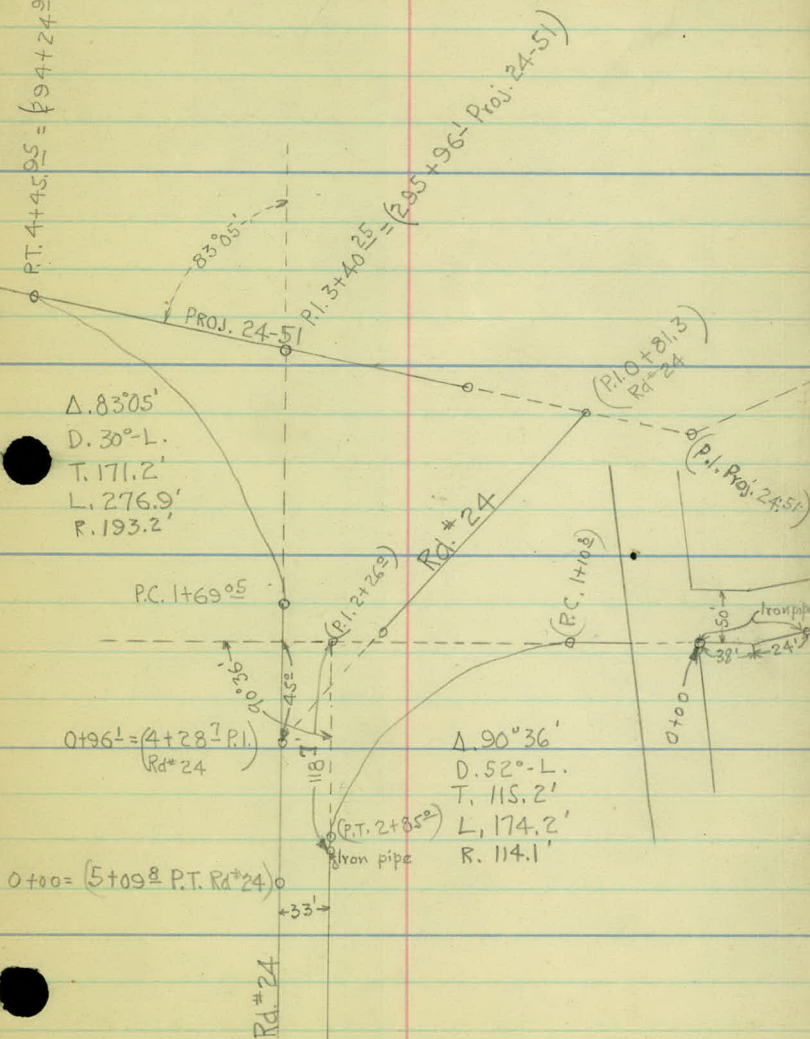
H.C. - D. Skooglund

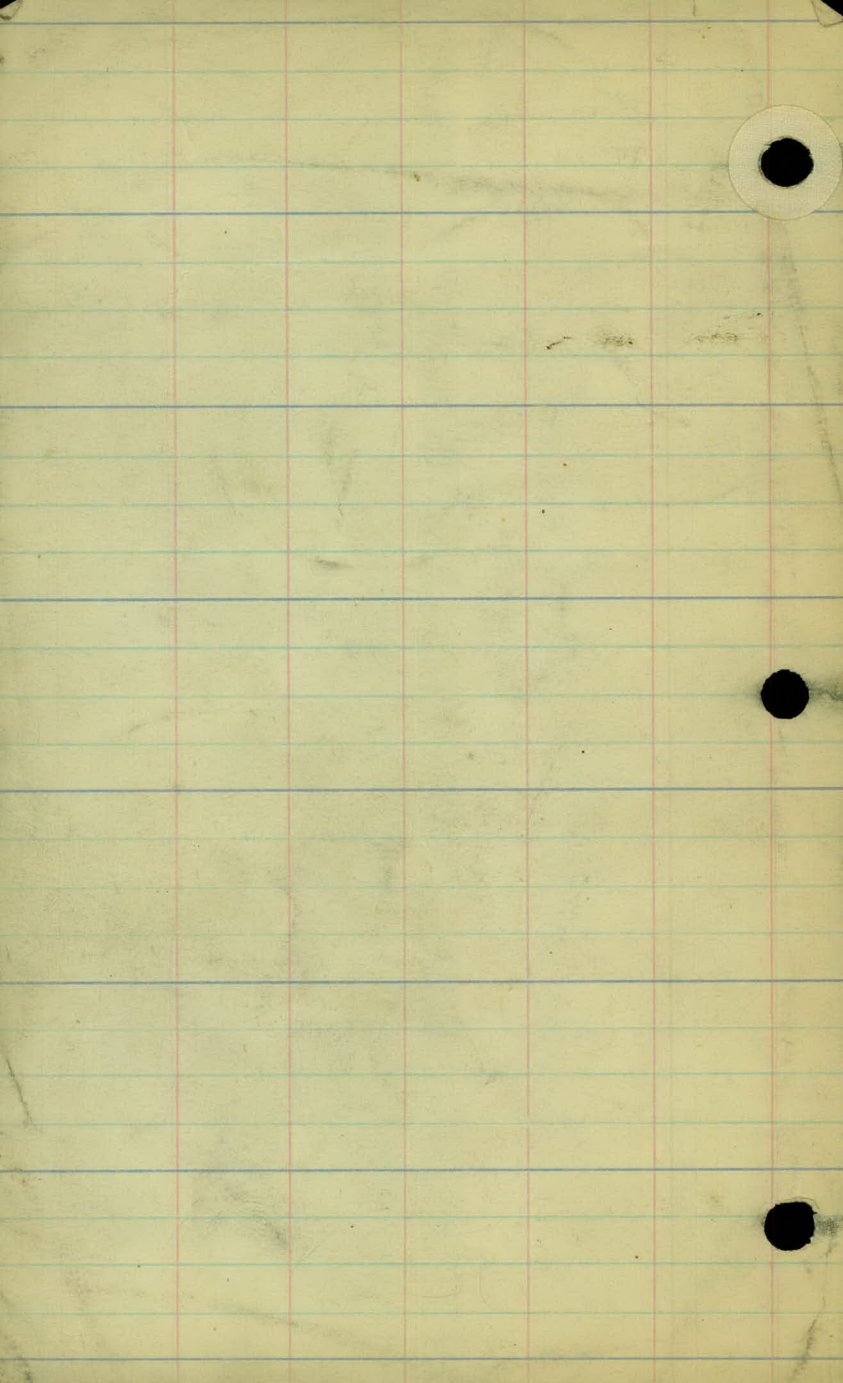
R.C. - W. Maloney

Stake - M. Galvin

May 10th 1924.

Cloudy - Cool





(X Line) Connection Rd#24 to Proj. 24-51

R.O.W. - Connection Rd#24 & Detour (Y Line)

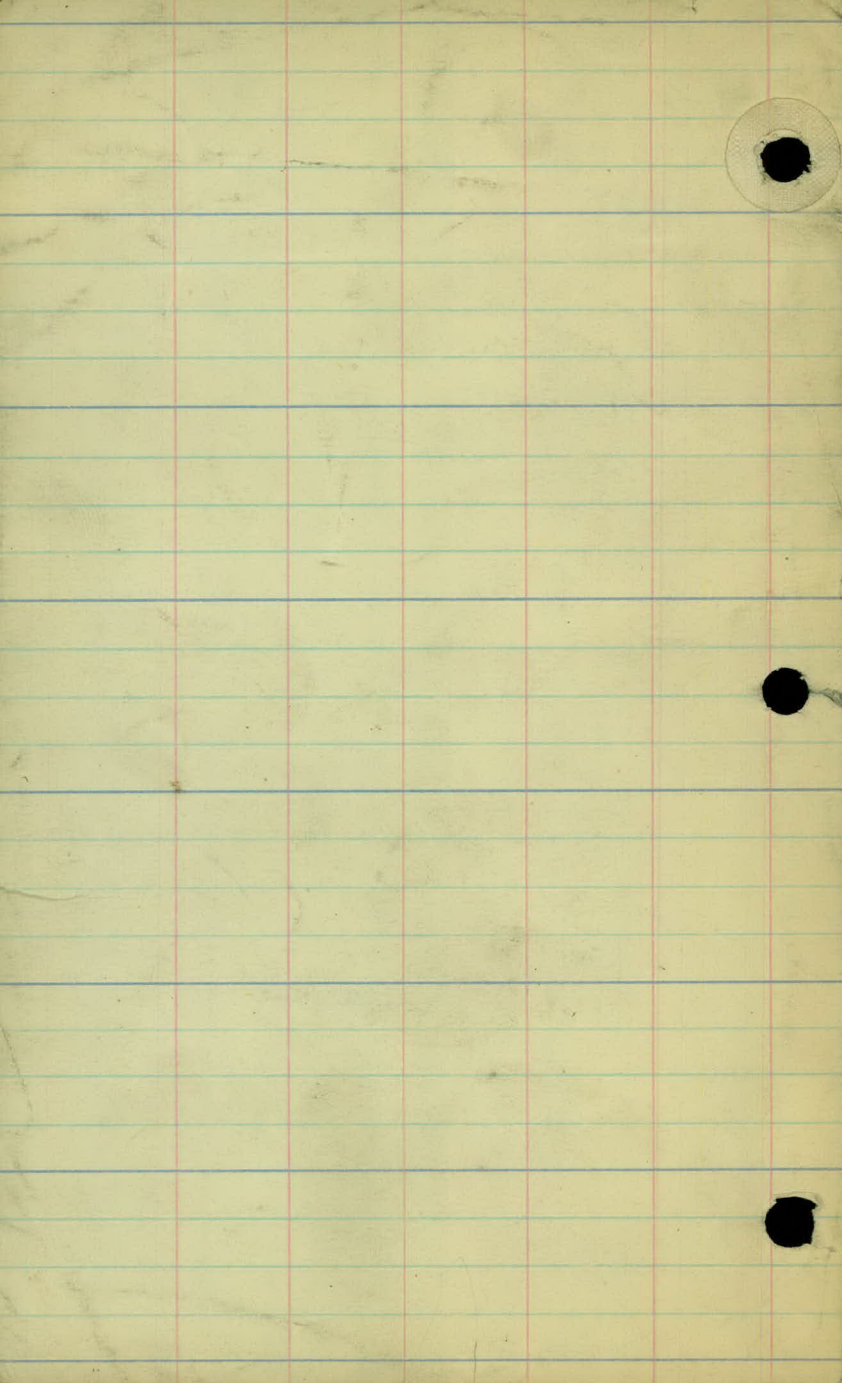
Office of Ramsey Co. Engineer
ST. PAUL, MINN.

5/12/24

Date Filed

File No. "13"

~~Road No 24~~



Final X-Sec.

Maint Project

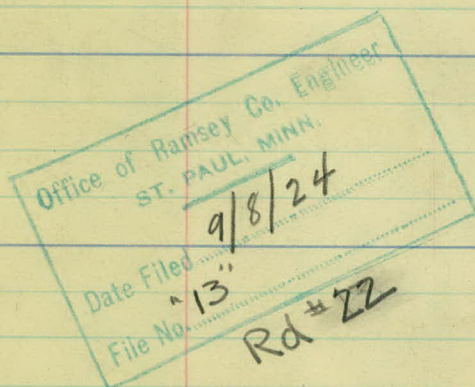
Acct #22

East County Line Road.

Sta 78+14.5 — Sta. 133+67.5

White Bear Blvd — Co. Road "E"

10- pages.



Station	+	H.I	-	Elev
B.M.	10.15	251.06		240.91
72+14.5			7.3	243.8
78+50			4.6	246.5
79+00			0.6	250.5
T.P.	11.33	261.74	0.65	250.41
79+50			7.0	254.7
80+00			2.8	258.9
T.P.	10.25	270.59	1.40	260.34
80+50			7.3	263.3
80+70			5.5	265.1
21400 Vane				
81+15			3.2	267.4
T.P.	11.16	278.92	2.83	267.76
81+25			11.3	267.6
81+30			1.1	267.8
82+00			8.6	270.3
T.P.	8.74	284.08	3.58	275.34
83+00			9.8	274.3
131+50			8.0	276.1

Lt. L Rt. W.H.G. 2
 Eck. Aug 29
 Go Nip 1924
 Frooke

R.R. spike in R.P. 13' Lt. 75+55

11.5 11.8 7.1 7.3 7.8 13.2
 33 24 76 14 22

8.3 7.5 4.8 4.4 4.6 4.5 5.2 10.2 7.0 9.0
 33 20 17 12 34 10 15 23 31 33

3.2 1.2 0.6 1.0 6.0 5.9 5.9
 33 18 0.7 15 22 30 33

6.9 6.9 9.7 10.4 7.3 7.0 7.0 7.5 11.0 10.6
 33 31 26 72 76 7.1 10 16 25 31

0.0 0.2 4.1 4.5 5.0 2.6 2.8 2.7 3.3 3.2
 33 29 24 21 18 14 3.0 12 18 33

3.3 3.7 9.2 9.2 7.1 7.3 7.4 7.6 8.0 7.4 7.1
 33 27 21 18 76 4.0 12 16 18 23 33

4.8 5.5 5.5 5.8 5.9
 33 16 18 17 33

2.8 3.4 3.2 3.2 3.5
 33 15 5.2 16 33

5.8 5.8 13.4 13.4 11.4 11.3 11.4 11.7
 33 27 18 16 13 11.4 15 33

5.2 5.2 13.2 13.2 11.3 11.1 11.2 12.3 12.3 8.9 8.9
 33 27 18 76 13 11.1 15 17 21 28 33

1.8 1.8 10.0 10.0 8.6 8.6 8.6 10.2 10.2 4.5 4.1
 33 29 19 76 14 8.6 15 18 22 29 33

3.5 3.3 11.5 11.5 9.9 9.8 10.1 11.8 11.8 6.1 5.4
 33 29 19 76 13 9.8 15 19 22 29 33

0.9 0.9 9.3 9.3 8.0 8.0 8.3 9.4 9.4 5.3 5.0
 33 29 19 76 14 7.8 76 19 23 29 33

Station	+	H.I	-	Elev.
		284.08		
84+00			5.8	284.3
84+55			3.6	280.5
+64			3.2	280.9
+75			2.7	281.4
T.P.	11.17	293.40	1.85	282.23
84+80			11.9	281.5
85+00			11.2	282.2
85+50			9.0	284.4
86+00			7.2	286.2
86+50			5.5	287.9
87+00			4.0	289.4
87+50			2.2	291.2
88+00			0.7	292.7
T.P.	11.81	304.53	0.68	292.12
88+50			10.0	294.5

L.

Z

RT.

3

0.5	0.8	7.6	7.6	5.9	5.8	5.8	7.6	7.6	5.0	5.0
<u>33</u>	<u>28</u>	<u>19</u>	<u>16</u>	<u>13</u>	<u>5.8</u>	<u>15</u>	<u>18</u>	<u>23</u>	<u>27</u>	<u>33</u>

0.0	0.5	4.8	4.8	3.4	3.6	3.7	5.6	5.6	2.3	1.9
<u>33</u>	<u>23</u>	<u>18</u>	<u>16</u>	<u>14</u>	<u>3.5</u>	<u>15</u>	<u>19</u>	<u>22</u>	<u>27</u>	<u>33</u>

2.3	2.7	2.9	3.2	3.4	5.2	5.2	2.0	1.8
<u>33</u>	<u>16</u>	<u>10</u>	<u>3.2</u>	<u>15</u>	<u>18</u>	<u>21</u>	<u>26</u>	<u>33</u>

2.4	2.4	2.7	2.7	4.6	4.6	2.1	2.0
<u>33</u>	<u>15</u>	<u>2.7</u>	<u>15</u>	<u>18</u>	<u>21</u>	<u>26</u>	<u>33</u>

8.5	8.6	13.0	13.0	11.8	11.9	12.0	13.9	13.9	11.6	11.3
<u>32</u>	<u>26</u>	<u>20</u>	<u>17</u>	<u>15</u>	<u>11.8</u>	<u>16</u>	<u>19</u>	<u>22</u>	<u>26</u>	<u>33</u>

7.4	8.1	12.3	12.3	11.1	11.2	11.3	13.1	13.1	11.7	11.6
<u>33</u>	<u>25</u>	<u>20</u>	<u>16</u>	<u>14</u>	<u>11.0</u>	<u>15</u>	<u>19</u>	<u>23</u>	<u>26</u>	<u>33</u>

4.4	5.0	10.1	10.1	9.0	9.0	9.0	10.8	10.8	8.6	9.1
<u>53</u>	<u>16</u>	<u>20</u>	<u>17</u>	<u>15</u>	<u>9.0</u>	<u>14</u>	<u>18</u>	<u>22</u>	<u>25</u>	<u>33</u>

4.8	5.3	8.8	8.8	7.4	7.2	7.3	9.0	9.0	6.2	6.2
<u>33</u>	<u>25</u>	<u>21</u>	<u>18</u>	<u>15</u>	<u>7.1</u>	<u>13</u>	<u>16</u>	<u>23</u>	<u>26</u>	<u>33</u>

3.6	3.9	6.5	6.5	5.6	5.5	5.9	7.6	7.6	5.7	6.3
<u>33</u>	<u>24</u>	<u>21</u>	<u>16</u>	<u>14</u>	<u>5.5</u>	<u>14</u>	<u>17</u>	<u>24</u>	<u>26</u>	<u>33</u>

3.7	3.9	5.8	5.8	4.0	4.0	4.1	6.1	6.1	3.9	4.7
<u>33</u>	<u>23</u>	<u>21</u>	<u>17</u>	<u>10</u>	<u>4.0</u>	<u>13</u>	<u>17</u>	<u>23</u>	<u>26</u>	<u>33</u>

3.9	3.5	4.1	4.1	2.4	2.2	2.4	3.9	3.9	2.2	3.1
<u>33</u>	<u>22</u>	<u>21</u>	<u>17</u>	<u>14</u>	<u>2.3</u>	<u>13</u>	<u>18</u>	<u>23</u>	<u>25</u>	<u>33</u>

2.2	1.5	2.1	2.1	0.8	0.7	0.7	2.9	2.9	2.0	2.5	4.6
<u>28</u>	<u>22</u>	<u>21</u>	<u>18</u>	<u>15</u>	<u>0.7</u>	<u>14</u>	<u>18</u>	<u>21</u>	<u>23</u>	<u>28</u>	<u>33</u>

11.1	11.3	12.3	12.3	10.7	10.0	10.3	12.3	12.3	11.8	13.8
<u>31</u>	<u>24</u>	<u>22</u>	<u>18</u>	<u>16</u>	<u>10.0</u>	<u>13</u>	<u>16</u>	<u>19</u>	<u>21</u>	<u>33</u>

Station	+	H. I	-	Elev.
		304.53		
89+00			8.3	296.2
89+50			7.0	297.5
B.M.	10.66	314.22	0.97	303.56
90+00			15.2	299.0
90+50			14.2	300.0
91+00			13.6	300.6
91+50			13.1	301.1
92+00			12.8	301.4
T.P.	3.18	306.65	10.75	303.47
92+50			5.2	301.5
93+00			5.5	301.2
93+50			5.4	301.3
94+00			5.1	301.6
+50			4.8	301.9
95+00			4.8	301.9

Lt.

L

Rt.

4

7.9	8.4	10.1	10.1	8.7	8.3	8.3	9.1	7.3
33	24	21	18	15	8.2	11	22	33

5.1	6.0	7.5	7.5	6.6	7.0	7.2	8.4	8.4	7.3	7.6
33	22	19	16	14	6.8	15	17	21	22	33

R.R. spike in T.P. 25' Lt. 89+96

Aug. 22, 1924

8.9	9.4	16.6	16.6	15.4	15.2	15.5	17.6	17.6	14.3	13.6
33	27	20	17	16	15.2	13	16	21	26	33

4.8	4.8	14.9	14.9	14.3	14.2	14.3	16.0	16.0	8.5	8.2
33	32	20	17	16	14.3	13	17	21	30	33

3.6	14.1	14.1	13.7	13.6	13.7	14.4	14.4	4.9	4.8
33	22	19	17	13.4	14	16	20	31	33

5.0	5.4	14.1	14.1	13.3	13.1	13.5	14.2	14.2	6.1	7.1
40	36	23	19	15	13.0	13	15	19	29	33

6.1	12.0	14.1	14.1	12.8	12.9	13.6	14.1	14.1	12.8	12.8
33	27	22	18	14	12.7	14	17	23	28	33

Top large Boulder. Lt. 92+18

5.7	6.0	6.6	6.5	5.5	5.2	6.0	6.9	7.8	11.0
33	24	22	19	15	5.4	14	17	23	33

6.1	6.3	7.0	7.0	5.7	5.5	6.3	7.4	7.4	7.9	13.1
33	24	22	20	16	5.5	15	16	20	23	33

6.5	6.5	7.0	7.0	5.9	5.4	5.8	7.7	7.8	6.3	6.3
33	23	22	18	16	5.3	14	16	20	30	33

6.7	6.6	7.0	7.0	5.6	5.1	5.3	6.4	6.4	1.9	1.7
33	22	21	18	15	5.1	14	16	23	28	33

5.3	5.4	6.0	6.0	5.3	4.8	5.0	6.2	6.0	1.6	1.0
33	22	21	16	14	4.9	14	17	23	28	33

4.2	4.5	5.7	5.9	4.9	4.8	5.1	6.4	6.4	3.4	3.0
33	23	21	17	15	4.8	14	17	24	27	33

Station	+	H.I	-	Elev.
		306.65		
95+50			5.0	301.7
96+00			5.0	301.7
96+50			4.7	302.0
T.P.	5.54	307.24	4.95	301.70
97+00			5.2	302.0
97+50			5.3	301.9
98+00			5.4	301.8
98+50			5.3	301.9
99+00			5.0	302.2
99+50			4.9	302.3
B.M.	3.80	307.24	3.80	303.44
100+00			5.2	302.0
100+50			5.4	301.8
101+00			5.5	301.7
101+50			5.9	301.3

LH

2

RT

6

5.6	6.2	6.2	5.2	5.0	5.2	6.5	6.8	6.2	5.6
33	24	18	15	(4.9)	14	16	21	22	33

5.0	4.0	5.8	6.0	5.1	5.0	5.0	6.5	6.5	5.4	7.1
33	24	22	18	16	(4.9)	14	16	20	22	33

4.7	4.2	4.6	5.8	6.0	4.8	4.7	5.0	5.9	6.0	4.4	4.4
33	32	25	22	18	15	(4.8)	15	17	20	23	33

6.4	6.5	7.0	6.9	5.7	5.2	5.4	6.6	6.4	4.6	5.5
33	23	21	16	14	(5.2)	14	17	21	23	33

7.2	7.2	7.0	5.4	5.3	5.3	6.8	7.1	5.1	4.0
33	20	16	13	(5.3)	14	16	19	22	33

6.7	6.7	7.1	6.9	5.5	5.4	5.6	7.0	7.3	6.4	5.7
33	24	22	17	14	(5.3)	14	16	20	21	33

7.2	7.6	7.3	5.3	5.3	5.3	6.5	6.6
33	22	16	12	(5.1)	14	17	33

5.4	6.1	6.8	6.8	5.1	5.0	5.1	6.7	7.7	6.8
33	24	22	17	13	(5.0)	14	17	23	33

5.0	5.3	6.7	6.7	5.0	4.9	5.0	6.2	6.2	5.0	4.4
33	24	22	17	13	(5.0)	15	17	21	23	33

R.R. Spike in T.P 30' L. 99+45

9.1	9.6	6.6	7.2	7.5	5.4	5.2	5.4	6.6	6.7	6.0	5.8
36	33	26	22	17	12	(5.1)	15	17	22	23	33

angul	6.9	5.6	5.4	5.6	7.1	6.6	2.7	2.7
	17	13	(5.3)	14	17	23	28	33

3.0	6.7	7.0	5.7	5.5	5.7	7.0	6.8	1.1	1.1
33	26	18	15	(5.5)	14	16	21	27	33

0.4	6.7	7.1	5.8	5.9	6.0	7.5	7.5	2.3	2.3
33	25	18	15	(5.1)	13	17	22	29	33

Station	+	H.I	-	Elev.
		307.24		
102+00			6.2	301.0
102+50			6.6	300.6
103+00			7.4	299.8
103+50			7.9	299.3
T.P.	3.66	302.39	8.51	298.73
104+00			4.1	298.3
104+50			4.8	297.6
105+00			5.1	297.3
105+50			5.4	297.0
106+00			5.7	296.7 296.4
106+50			6.2	296.2
107+00			7.2	295.2
B.M.	3.84	297.33	8.89	293.49
107+50			7.8	294.5
108+00			3.3	294.0

0.01 off
293.50

Lt.

L

Rt.

6

4.7	7.9	8.0	6.5	6.2	6.6	7.8	7.4	0.5	0.4
33	25	19	15	(6.2)	14	17	23	31	33

5.8	8.5	8.5	6.9	6.6	7.0	8.0	7.5	307.9
33	27	20	15	(6.8)	15	18	23	33

3.2	8.8	9.2	7.2	7.4	7.8	8.8	8.5	308.4	308.4
33	25	19	14	(7.4)	14	17	22	32	33

8.0	7.3	10.0	9.9	8.1	7.9	8.1	9.6	9.3	4.0	4.0
33	19	24	19	14	(8.1)	14	17	23	31	33

Nail in F.R. Lt. 103+55

8.8	8.8	6.8	5.9	3.9	4.1	4.4	11.7	12.5
33	31	26	18	14	(4.1)	16	27	33

10.0	9.5	7.2	6.5	5.0	4.8	5.0	15.8
33	26	21	18	14	(4.5)	15	33

5.0	6.1	7.4	7.1	5.3	5.1	5.4	13.1	15.8
33	25	23	17	14	(5.0)	15	25	33

2.1	2.0	6.5	7.0	5.3	5.4	5.1	6.4	13.3	14.5
33	31	23	17	14		11	17	27	33

203.4	303.2	6.3	6.6	5.4	5.7	6.1	7.5	12.2	13.3
33	36	22	17	15	(5.7)	16	21	29	33

1.0	1.4	2.1	7.3	6.6	6.1	6.2	6.3	7.1	8.4	10.1
33	29	21	18	15	10	(6.4)	15	20	24	33

5.1	5.7	8.4	8.8	2.3	7.2	7.3	8.8	10.1
33	28	23	19	14	(7.2)	16	19	33

R.R. spike in T.P. 30' Lt. 107+65

3.2	3.5	4.2	4.4	3.0	2.8	3.1	4.4	6.0	6.4
33	28	27	19	16		15	18	29	33

5.1	5.4	3.4	3.3	3.8	6.8	8.2
33	20	17	(3.2)	16	22	33

station	+	H. I.	-	Elev.
		297.33		
108+70			4.1	293.2
109+00			4.5	292.8
109+65			4.9	292.4
110			4.6	292.7
+50			3.4	293.9
T.P.	10.64	305.91	2.06	295.27
111			10.6	295.3
+50			9.6	296.3
112+00			8.1	297.8
+50			6.4	299.5
112+50			4.5	301.4
113			0.5	305.4
T.P.	10.91	316.37	0.45	305.46
114+50			8.9	307.5
115+00			6.7	309.7

Lt.

x

Rt.

Aug. 25, 1924

⑦

$\frac{5.9}{33}$	$\frac{5.3}{21}$	$\frac{4.1}{17}$	$\frac{4.1}{4.0}$	$\frac{4.7}{16}$	$\frac{8.4}{23}$	$\frac{7.9}{33}$
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$\frac{7.1}{33}$	$\frac{7.3}{21}$	$\frac{4.4}{16}$	$\frac{4.5}{4.4}$	$\frac{4.7}{13}$	$\frac{5.2}{17}$	$\frac{7.5}{25}$	$\frac{10.4}{33}$
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$\frac{11.4}{33}$	$\frac{10.3}{23}$	$\frac{5.5}{14}$	$\frac{4.8}{11}$	$\frac{4.7}{4.4}$	$\frac{5.1}{14}$	$\frac{7.5}{21}$	$\frac{11.3}{33}$
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$\frac{8.8}{33}$	$\frac{7.4}{20}$	$\frac{5.0}{15}$	$\frac{4.6}{12}$	$\frac{4.6}{4.4}$	$\frac{4.9}{13}$	$\frac{5.3}{16}$	$\frac{8.1}{21}$	$\frac{9.9}{33}$
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$\frac{0.6}{33}$	$\frac{0.7}{28}$	$\frac{5.0}{21}$	$\frac{5.0}{19}$	$\frac{3.3}{16}$	$\frac{3.4}{3.7}$	$\frac{3.6}{17}$	$\frac{5.2}{20}$	$\frac{5.2}{33}$
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$\frac{5.8}{33}$	$\frac{6.3}{27}$	$\frac{12.2}{20}$	$\frac{12.2}{17}$	$\frac{10.8}{15}$	$\frac{10.6}{10.6}$	$\frac{10.8}{15}$	$\frac{11.8}{18}$	$\frac{11.6}{22}$	$\frac{12.2}{33}$
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$\frac{8.6}{33}$	$\frac{8.9}{26}$	$\frac{10.5}{22}$	$\frac{10.5}{19}$	$\frac{9.4}{17}$	$\frac{9.6}{9.3}$	$\frac{9.6}{14}$	$\frac{11.7}{19}$	$\frac{12.0}{21}$	$\frac{11.4}{28}$	$\frac{11.0}{26}$	$\frac{10.1}{28}$
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$\frac{10.9}{33}$	$\frac{10.4}{19}$	$\frac{8.2}{15}$	$\frac{8.1}{8.1}$	$\frac{8.5}{11}$	$\frac{8.9}{16}$	$\frac{11.5}{22}$	$\frac{11.5}{26}$	$\frac{11.0}{33}$
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$\frac{13.0}{33}$	$\frac{11.6}{24}$	$\frac{6.8}{15}$	$\frac{6.4}{11}$	$\frac{6.4}{6.3}$	$\frac{6.5}{12}$	$\frac{6.8}{16}$	$\frac{11.7}{25}$	$\frac{11.2}{29}$	$\frac{11.5}{33}$
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$\frac{12.0}{33}$	$\frac{12.1}{30}$	$\frac{7.0}{24}$	$\frac{4.4}{16}$	$\frac{4.5}{4.4}$	$\frac{4.6}{12}$	$\frac{5.0}{16}$	$\frac{10.2}{28}$	$\frac{11.8}{33}$
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$\frac{7.0}{33}$	$\frac{1.5}{23}$	$\frac{0.4}{16}$	$\frac{0.5}{0.4}$	$\frac{0.4}{17}$	$\frac{1.4}{21}$	$\frac{6.4}{33}$
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$\frac{4.6}{33}$	$\frac{10.6}{22}$	$\frac{10.3}{18}$	$\frac{8.8}{15}$	$\frac{8.9}{8.9}$	$\frac{7.0}{18}$	$\frac{10.4}{26}$	$\frac{14.7}{33}$
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$\frac{4.0}{33}$	$\frac{10.5}{30}$	$\frac{8.5}{27}$	$\frac{7.0}{18}$	$\frac{6.7}{14}$	$\frac{6.7}{6.6}$	$\frac{6.8}{17}$	$\frac{7.5}{22}$	$\frac{12.3}{33}$
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station	+	H.I	-	Elev
		316.37		
115+50			4.7	311.7
T.P.	11.96	325.43	2.90	312.47
116+00			12.0	313.4
T.P.	11.18	331.92	4.69	320.74
117+00			13.9	318.0
118			10.5	321.4
119			8.8	323.1
120			9.0	322.9
T.P.	2.80	326.04	8.68	323.24
121			4.1	321.9
121+50			5.2	320.8
122			6.5	319.5
122+50			7.9	318.1
T.P.	4.04	321.38	8.70	317.34
123+00			4.0	317.4
B.M.	5.83	corrected 321.33	5.83	315.55 315.50
123+50			5.0	316.43
124				
124			6.0	315.43

Lt.

L

Rt.

8

21	20	53	33	46	47	47	6.0	60	47	59	70
33	27	23	18	17	4.2	15	18	22	24	31	33

1.9	122	124	116	120	12.1	13.1	13.1	71
34	23	19	18	11.8	18	20	23	33

46	7.5	149	149	141	139	14.3	14.8	148	3.7
33	32	22	18	16	14.0	16	18	22	34

35	109	113	105	105	10.7	11.4	11.0	2.0	2.0
33	22	18	16	10.4	15	17	20	32	33

2.8	91	94	89	88	9.1	9.5	9.3	2.3	2.3
33	23	19	16	8.6	14	17	21	32	33

5.8	9.8	100	9.2	90	9.1	10.0	10.0	2.4
33	24	20	17	8.8	16	18	22	33

Top sticks 120.

43	3.8	5.5	5.5	4.4	41	4.2	5.3	6.2	0.0	00
33	28	25	19	17	4.0	14	17	22	31	33

64	63	7.1	7.0	5.5	52	51	6.0	61	4.5	3.9
33	26	24	19	17	5.1	14	17	22	24	33

109	65	82	70	65	6.5	84	8.1	7.0	73
33	24	19	16	6.4	14	18	24	28	33

16.7	13.2	80	79	8.0	11.5	10.8	11.1
33	25	17	7.5	15	19	28	33

13.0	11.6	43	40	4.2	6.3	6.7
33	28	16	40	14	19	33

R.R. in 8" Oak 30' Lt. 123 + 27

4.2	41	64	65	5.2	50	5.4	68	6.8	3.0	33
33	28	23	18	15	4.9	14	17	25	31	33

1.7	2.0	7.2	7.3	6.0	60	5.6	7.0	7.1	0.7	0.2
33	30	22	17	13	5.8	13	17	23	32	33

Station	+	M.F	-	Elev
		321.33		
125+00				313.3
T.P.	1.67	313.15	9.85	311.48
126+00			1.7	314.5
+15 0.00 Ditch L & R.				
127+00			4.0	309.2
127+70			5.3	307.9
128+00			5.6	307.6
128+50			5.8	307.4
129+00			5.6	307.6
129+50			5.4	307.8
129				
130+00			5.3	307.9
131+00			5.3	307.9
131+60			5.1	308.1
132+00			4.9	308.3
T.P.	11.45	322.57	2.03	311.12

Lt

±

Rt.

9

$\frac{2.2}{33}$	$\frac{9.0}{23}$	$\frac{9.2}{17}$	$\frac{7.9}{13}$	$\frac{8.0}{8.1}$	$\frac{8.2}{15}$	$\frac{9.5}{19}$	$\frac{9.5}{22}$	$\frac{2.3}{32}$	$\frac{2.3}{33}$
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$\frac{1.7}{33}$	$\frac{2.0}{23}$	$\frac{3.5}{20}$	$\frac{3.7}{17}$	$\frac{2.0}{13}$	$\frac{1.7}{19}$	$\frac{2.0}{15}$	$\frac{4.2}{21}$	$\frac{4.0}{26}$	$\frac{3.3}{33}$
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$\frac{12.0}{33}$	$\frac{12.0}{2.1}$	$\frac{3.7}{19}$	$\frac{4.1}{12}$	$\frac{4.0}{4.0}$	$\frac{4.0}{15}$	$\frac{9.0}{25}$	$\frac{10.2}{33}$
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$\frac{14.1}{33}$	$\frac{14.1}{30}$	$\frac{5.7}{18}$	$\frac{5.3}{6.1}$	$\frac{5.4}{15}$	$\frac{11.5}{26}$	$\frac{12.5}{33}$
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$\frac{13.3}{33}$	$\frac{13.0}{29}$	$\frac{6.3}{18}$	$\frac{5.6}{5.6}$	$\frac{5.5}{16}$	$\frac{11.8}{25}$	$\frac{13.0}{33}$
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$\frac{13.0}{33}$	$\frac{12.3}{25}$	$\frac{6.1}{15}$	$\frac{5.8}{5.7}$	$\frac{5.6}{15}$	$\frac{8.4}{20}$	$\frac{8.4}{24}$	$\frac{7.7}{33}$
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$\frac{12.6}{33}$	$\frac{12.3}{25}$	$\frac{6.1}{16}$	$\frac{5.6}{5.7}$	$\frac{5.6}{15}$	$\frac{6.9}{19}$	$\frac{6.9}{28}$	$\frac{6.2}{33}$
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$\frac{14.2}{33}$	$\frac{10.5}{24}$	$\frac{5.5}{16}$	$\frac{5.4}{5.5}$	$\frac{5.6}{14}$	$\frac{6.9}{18}$	$\frac{6.7}{25}$	$\frac{2.5}{32}$	$\frac{2.5}{33}$
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$\frac{3.1}{33}$	$\frac{2.5}{35}$	$\frac{6.6}{21}$	$\frac{6.6}{18}$	$\frac{5.5}{15}$	$\frac{5.3}{5.4}$	$\frac{5.3}{14}$	$\frac{6.3}{19}$	$\frac{6.1}{24}$
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$\frac{6.2}{21}$	$\frac{6.3}{17}$	$\frac{5.1}{14}$	$\frac{5.3}{5.3}$	$\frac{5.1}{14}$	$\frac{6.4}{18}$	$\frac{6.4}{22}$
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$\frac{5.7}{20}$	$\frac{6.0}{17}$	$\frac{5.2}{13}$	$\frac{5.1}{4.9}$	$\frac{5.0}{15}$	$\frac{6.3}{19}$	$\frac{6.1}{22}$
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$\frac{6.0}{23}$	$\frac{6.3}{18}$	$\frac{5.0}{14}$	$\frac{4.9}{4.9}$	$\frac{4.8}{15}$	$\frac{6.0}{19}$	$\frac{6.0}{22}$
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x-sec. cont'd

x-sec. cont'd

Station + H.I. - Elev.

322.57

130+00

131

+60

132+00

132+50

T.P.

0.55

313.01

10.11

312.46

132+50

4.7

308.3

133

4.6

308.5

133+10

4.6

308.5

133+50

4.3

308.8

133+67.5

4.4

308.6

B.M. (new)

4.67

308.34

4.89

313.23

308.34

B.M.

1.40

311.83

Lt.

L

Rt.

10

14.8

5.0
372.0
36

14.7

6.0
333.0
372.0
402.4
35cont'd
X-sections.

14.3

3.5
362.0
417.3
34

14.1

1.5
378.6
364.2 4.2
33 326.9
266.8
194.8
164.7
465.1
166.2
196.3
27

3.3

9.1
338.0
194.9
144.6
464.7
145.8
195.8
284.0
3310.2
338.4
205.1
134.6
464.9
156.2
197.2
336.8
455.1
174.3
444.7
174.8
307.3
426.8
456.0
335.0
144.4
434.67
10 = End of
Pay4.70
33

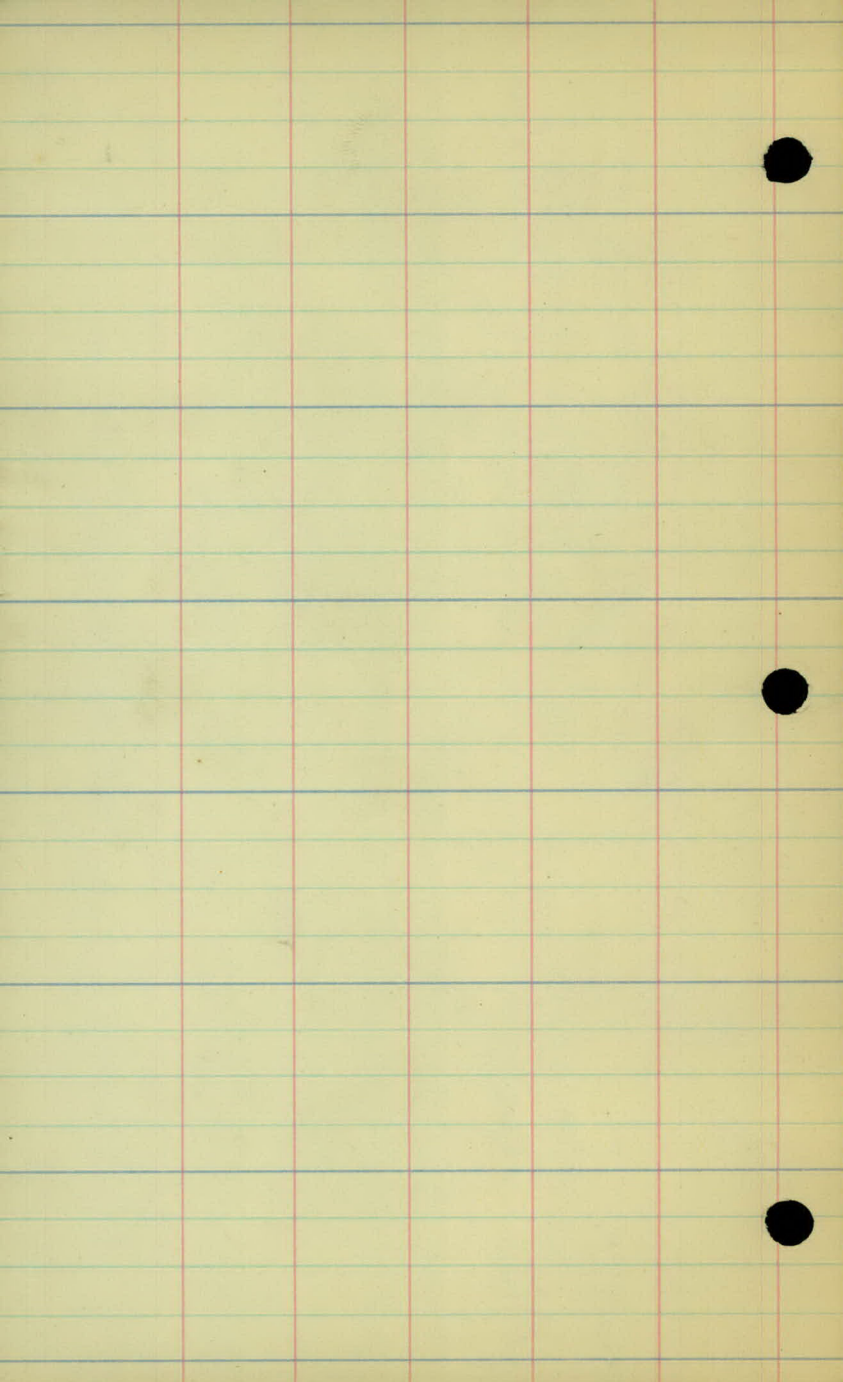
Top. L and end of Co. Rd. "E" Pavement.

(Co. Road "E")

R.R. Spike 10 stump. 50' Lt. 218455

W.H.C.

Eck.
Galvin
FrankelFinished
Aug 25, 1924311.95
- .13
311.82 = corners
diff.



Check Levels

Road # 22.

Co Rd "E" to

	+	H.I	-	Elev.	
B.M.	5.61	299.10		293.49	
T.P.	10.84	309.42	0.52	298.58	
T.P.	11.19	320.32	0.29	309.13	
T.P.	7.14	327.12	0.34	319.98	
⑦			3.84	23.28	OLD T.P.
B.M.	3.45	318.95	11.62	315.50	✓
T.P.	2.05	312.15	8.85	310.10	
T.P.	5.22	313.20	4.17	307.98	
T.P.	5.10	313.19	5.11	308.09	
B.M. 			1.39	311.80	
				311.82	
	5.59	317.54		311.95	
T.P.	10.94	327.81	0.67	316.87	
T.P.	11.86	339.18	0.49	327.32	
Old T.P.			6.28		
T.P.	10.89	349.53	0.54	338.64	
T.P.	6.42	355.63	0.32	349.21	
			3.71	351.92	52.12

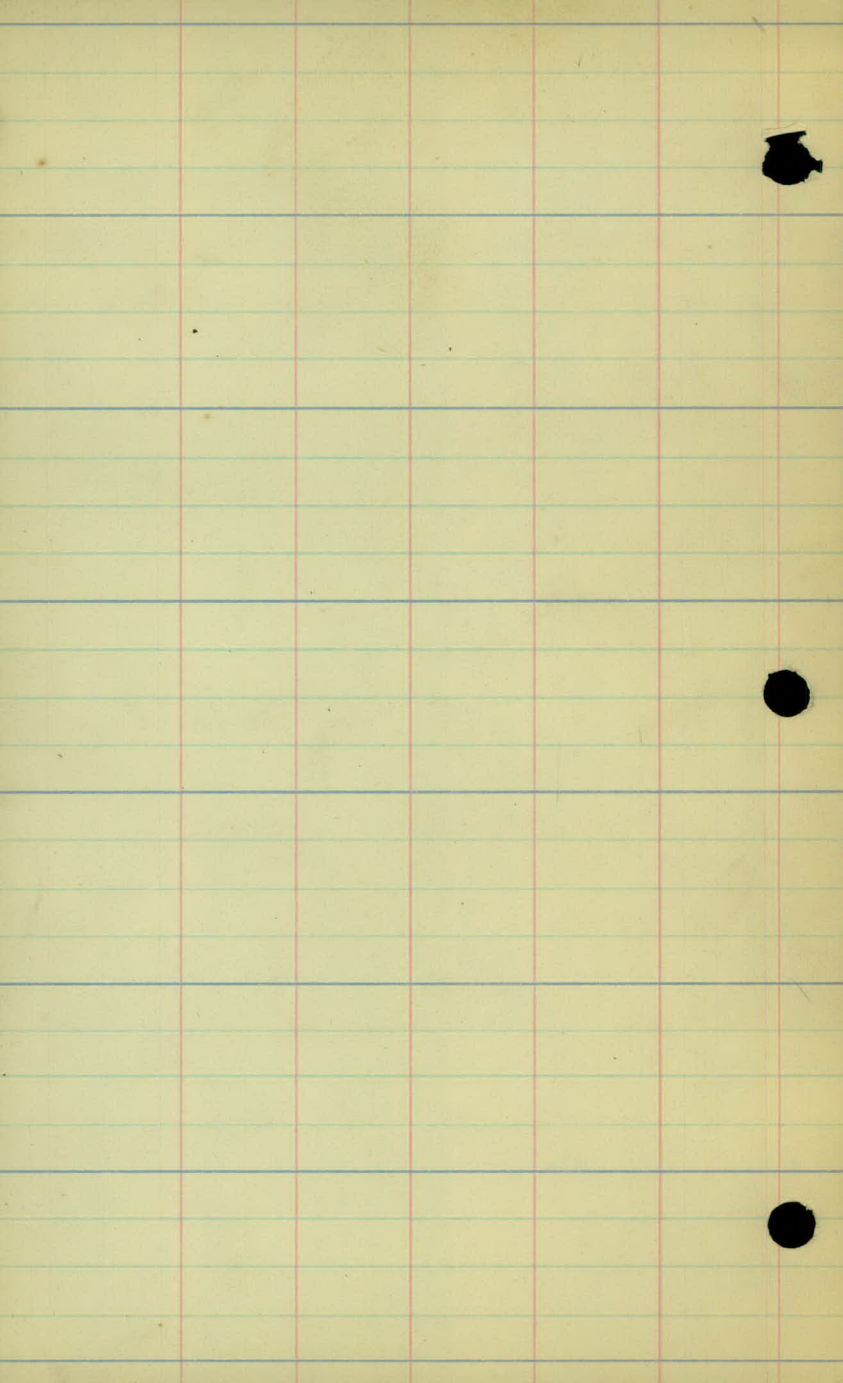
R.R. spike in T.P. 30' Lt. 107+65

R.R. spike in 8" Oak 30' Lt. 123+27

R.R. spike dump 50' Lt. 218+55

" " " " "

" " " " " Co. Rd. "E"



Final X-sec.

Maint. Project.

Co. Rd "E" to 800' No. of Co. Rd "C"

Sta. 133+67.5 - 232+00

Station	+	H. I	-	Elev	
B.M. New	4.67	313.14 ✓			308.34 + .13 308.47 ✓
133+67.5			4.4	308.7	
133+75			4.4	308.7	
134			4.7	308.4	
+50			5.0	308.1	
135			4.7	308.4	
+50			4.0	309.1	
136			3.3	309.8	10°
+50			2.1	311.0	✓
T.P.	11.46	323.97 ✓	0.63		312.51 ✓
137			2 11.5	312.5	
+50			2 9.8	314.2	
138			2 8.2	315.7	
+50			2 6.6	317.4	
139			2 5.0	319.0	

H					Rt.		W.H.C.		Aug 25,	
Top & End Co. Rd					F ¹¹ Pavement		Eck		1924	
6.8	6.0	5.0	4.4	4.67	4.70					
4.4	3.3	1.4	4.6	10 = End of Ave	3.3					
4.8	7.2	5.3	4.4	4.8	4.8	x				
4.5	1.9	4.6	1.0	3.3						
1.6	5.3	4.7	4.9	5.5	4.5	12.2				
3.3	2.0	4.6	1.0	1.9	2.8	3.3				
14.9	14.2	5.2	5.0	5.2	14.0					
3.3	2.9	1.5	4.8	1.6	3.3					
13.1	12.4	5.0	4.7	5.3	13.0	13.2				
3.3	2.1	1.5	4.6	1.7	2.9	3.3				
5.7	5.5	8.7	8.3	4.7	4.0	4.3	7.4	7.4	6.1	6.7
3.3	3.1	2.7	2.3	1.7	3.9	1.7	2.2	2.5	3.0	3.3
5.8	4.7	6.3	6.3	3.4	2.3	3.5	5.9	5.2	2.0	316.5
3.3	2.7	2.4	2.0	1.7	3.1	1.6	1.9	2.4	3.0	3.3
8.9	7.9	6.8	6.0	2.1	2.1	3.6	3.5	2.2	2.0	
3.3	2.9	2.7	2.2	1.6	2.0	1.6	1.9	2.6	3.0	3.3
13.1	12.1	13.1	13.1	11.6	11.5	16.2	13.0	13.0	6.2	
3.3	2.8	2.5	1.9	1.6	(11.4)	1.5	2.1	2.6	3.3	
10.5	9.7	11.2	11.2	10.3	9.8	9.5	11.4	11.4	6.5	6.5
3.3	2.8	2.5	2.0	1.6	(9.6)	1.4	1.9	2.5	3.0	3.3
12.7	11.0	8.6	8.3	8.1	10.2	11.1	10.5	8.1	8.1	
3.3	2.2	1.7	(8.1)	1.5	2.0	2.6	3.0	3.2	3.3	
12.7	11.6	7.1	6.6	6.7	10.3	9.6	8.0	8.0		
3.3	2.2	1.6	(6.4)	1.5	2.3	3.1	3.2	3.3		
6.5	5.5	6.1	5.0	5.0	5.1	7.7	8.2	8.2	7.0	
3.3	2.6	2.3	1.5	(4.8)	1.5	2.1	2.2	3.0	3.3	

station	+	H.I	-	Elev.	
		323.97			
139+50			3.0	321.0	
140+00			1.0	323.0	
T.P.	10.27	333.23 ✓	1.01		322.96 ✓
140+50			8.3	324.9	
141+00			6.0	327.2	
141+50			3.4	329.8	
T.P.	11.75	344.69 ✓	0.29		332.94 ✓
142			12.0	332.7	
142+50			7.2	335.5	
T.P.	8.89	350.47 ✓	3.11		341.58 ✓
143			12.4	338.1	
143+50			9.9	340.6	
144+00			7.5	343.0	
144+50			4.9	345.6	
145+00			2.4	348.1	
T.P.	10.92	360.80 ✓	0.59		349.88 ✓
145+50			10.5	350.3	

Lt.

8

Rt

②

2.5	1.8	6.2	6.2	3.6	3.0	3.0	5.3	7.0
33	28	23	21	15	(2.9)	17	22	33

6.6	5.8	1.3	1.0	1.2	6.5	7.9
33	28	76	(0.9)	17	26	39

18.8	9.0	8.3	8.7	15.6	15.8
38	17	(8.2)	17	29	33

17.0	6.3	6.0	6.0	13.7	13.7
34	77	(5.8)	18	31	33

9.7	9.7	2.6	3.4	3.4	9.1	9.8
33	26	16	(3.4)	19	27	33

top stake Lt. 142

Aug. 26 1924

8.1	8.1	12.8	12.8	12.2	12.0	12.1	12.5	12.5	11.7	11.7
33	29	22	18	14	(12.1)	18	21	25	26	33

2.9	2.9	9.8	10.2	9.3	9.2	9.1	10.1	11.0	10.6	5.4	5.6
33	30	21	17	14	(9.2)	14	16	31	24	31	33

4.1	12.4	13.1	12.2	12.4	12.4	13.1	14.0	12.6	6.3	6.3
33	22	16	14	(12.5)	14	17	20	23	32	33

2.8	10.5	11.0	10.0	9.9	9.9	10.8	9.7	2.9
33	23	19	14	(9.8)	14	17	26	34

3.3	8.9	9.0	7.8	7.5	7.6	8.8	8.5	4.2
34	26	18	16	(7.1)	15	19	28	34

1.6	4.8	6.1	6.1	5.1	4.9	5.0	6.8	6.3	3.3
33	28	23	18	15	(4.9)	15	18	28	33

0.2	3.1	2.6	3.4	2.4	2.4	2.3	3.7	3.6	0.7	0.6
33	23	22	17	15	(2.4)	14	18	26	31	33

8.9	11.6	12.0	12.0	10.7	10.5	10.3	11.4	11.4	2.9
33	20	19	16	13	(10.3)	14	18	22	33

Station	+	H.I	-	Elev.
		360.80		
B.M.	6.17	358.22	8.87	356.93 ✓
"		358.29 ✓		352.12 ✓
146+00			5.2	353.1
T.P.	8.84	364.49 ✓	2.64	355.65 ✓
146+50			9.6	354.9
147+00			7.9	356.6
147+50			6.0	358.5
148+00			5.0	359.5 ✓
148+50			4.1	360.4
149+00			3.5	361.0
149+50			3.9	361.6
T.P.	10.20	372.07 ✓	2.62	361.87 ✓
150+00			9.6	362.5
150+50			8.9	363.2
151			8.0	364.1
151+50			7.2	364.9

Lt. L Rt.

8

R.R. spike in 12" Oak 30' Lt. 146 to 0

6.5	6.7	7.4	7.4	5.9	5.2	5.3	6.3	5.9	5.1
33	25	24	19	16	(5.2)	15	17	22	36.5
									34

9.7	9.1	11.1	11.1	9.7	9.6	9.3	10.3	10.2	2.6
33	31	28	18	14	(9.1)	15	18	23	33

7.9	7.9	9.7	9.7	8.1	7.9	7.5	8.8	8.4	0.0
33	30	24	19	13	(8.0)	14	18	23	33

6.2	8.3	8.4	6.6	6.0	6.0	7.2	6.9	0.5
33	25	18	14	(6.1)	15	20	25	34

7.6	8.2	7.8	5.2	5.0	4.7	6.2	5.5	1.9
33	28	22	17	(5.0)	14	19	28	33

10.6	9.6	4.5	4.1	4.1	5.5	5.0	0.7
33	25	17	(3.9)	15	21	28	33

10.1	9.4	4.1	3.5	3.4	4.6	3.9	0.0
33	26	18	(3.3)	15	20	28	33

3.6	4.3	3.2	2.9	2.8	4.1	3.6	0.0
33	20	18	(2.8)	15	19	27	33

top stake Rt. 150

8.6	9.5	9.6	9.6	11.2	10.7	7.5
28	18	(9.7)	16	20	27	34

7.5	8.5	9.0	8.9	9.0	10.7	10.4	8.2	8.2
33	26	15	(8.9)	15	19	27	32	32

5.2	7.4	8.0	8.0	8.1	9.8	9.8	7.4
33	27	15	(8.1)	17	21	28	33

4.2	6.7	7.2	7.2	7.4	8.6	8.5	5.0
33	27	16	(7.4)	16	20	27	33

Station	+	HI	-	Elev.
		372.07 ✓		
152+00			7.3	364.8
152+50			8.4	363.7
153+00			10.2	361.9
T.P.	0.25	360.99 ✓	11.33	360.74 ✓
153+50			0.7	360.3
154+00			2.8	358.2
154+50			4.3	356.7
155+00			5.7	355.3
155+50			7.0	353.7 354.0
156+00			8.7	352.3
T.P.	1.36	353.70 ✓	8.65	352.34 ✓
156+50			3.0	350.7
157+00			4.1	349.6
157+50			5.0	348.7
158+00			5.8	347.9

L

K

RT

14

$$\begin{array}{r} 5.1 \\ 33 \end{array} \quad \begin{array}{r} 6.7 \\ 28 \end{array} \quad \begin{array}{r} 7.1 \\ 14 \end{array} \quad \begin{array}{r} 7.3 \\ 7.3 \end{array} \quad \begin{array}{r} 7.3 \\ 16 \end{array} \quad \begin{array}{r} 8.1 \\ 20 \end{array} \quad \begin{array}{r} 8.6 \\ 26 \end{array} \quad \begin{array}{r} 2.5 \\ 33 \end{array}$$

$$\begin{array}{r} 6.6 \\ 33 \end{array} \quad \begin{array}{r} 8.0 \\ 28 \end{array} \quad \begin{array}{r} 8.7 \\ 16 \end{array} \quad \begin{array}{r} 8.3 \\ 11 \end{array} \quad \begin{array}{r} 8.4 \\ 8.4 \end{array} \quad \begin{array}{r} 8.5 \\ 16 \end{array} \quad \begin{array}{r} 7.7 \\ 19 \end{array} \quad \begin{array}{r} 7.6 \\ 24 \end{array} \quad \begin{array}{r} 1.5 \\ 34 \end{array}$$

$$\begin{array}{r} 8.2 \\ 33 \end{array} \quad \begin{array}{r} 7.5 \\ 29 \end{array} \quad \begin{array}{r} 10.4 \\ 15 \end{array} \quad \begin{array}{r} 10.2 \\ 10.0 \end{array} \quad \begin{array}{r} 9.8 \\ 16 \end{array} \quad \begin{array}{r} 11.0 \\ 19 \end{array} \quad \begin{array}{r} 10.7 \\ 24 \end{array} \quad \begin{array}{r} 4.7 \\ 33 \end{array}$$

$$\begin{array}{r} 1.3 \\ 33 \end{array} \quad \begin{array}{r} 1.0 \\ 16 \end{array} \quad \begin{array}{r} 0.6 \\ 14 \end{array} \quad \begin{array}{r} 0.7 \\ 0.5 \end{array} \quad \begin{array}{r} 0.8 \\ 12 \end{array} \quad \begin{array}{r} 1.2 \\ 17 \end{array} \quad \begin{array}{r} 2.8 \\ 21 \end{array} \quad \begin{array}{r} 2.4 \\ 25 \end{array} \quad \begin{array}{r} 1.4 \\ 28 \end{array} \quad \begin{array}{r} 1.7 \\ 33 \end{array}$$

$$\begin{array}{r} 3.2 \\ 33 \end{array} \quad \begin{array}{r} 3.2 \\ 17 \end{array} \quad \begin{array}{r} 2.8 \\ 14 \end{array} \quad \begin{array}{r} 2.8 \\ 2.1 \end{array} \quad \begin{array}{r} 2.8 \\ 14 \end{array} \quad \begin{array}{r} 3.4 \\ 18 \end{array} \quad \begin{array}{r} 7.2 \\ 26 \end{array} \quad \begin{array}{r} 7.9 \\ 33 \end{array}$$

$$\begin{array}{r} 3.3 \\ 33 \end{array} \quad \begin{array}{r} 4.0 \\ 15 \end{array} \quad \begin{array}{r} 4.5 \\ 12 \end{array} \quad \begin{array}{r} 4.3 \\ 10 \end{array} \quad \begin{array}{r} 4.3 \\ 4.1 \end{array} \quad \begin{array}{r} 4.3 \\ 18 \end{array} \quad \begin{array}{r} 10.0 \\ 28 \end{array} \quad \begin{array}{r} 10.3 \\ 33 \end{array}$$

$$\begin{array}{r} 3.2 \\ 33 \end{array} \quad \begin{array}{r} 4.3 \\ 28 \end{array} \quad \begin{array}{r} 5.5 \\ 13 \end{array} \quad \begin{array}{r} 5.5 \\ 11 \end{array} \quad \begin{array}{r} 5.7 \\ 5.5 \end{array} \quad \begin{array}{r} 6.0 \\ 13 \end{array} \quad \begin{array}{r} 6.0 \\ 19 \end{array} \quad \begin{array}{r} 8.6 \\ 24 \end{array} \quad \begin{array}{r} 9.5 \\ 33 \end{array}$$

$$\begin{array}{r} 1.3 \\ 33 \end{array} \quad \begin{array}{r} 7.6 \\ 28 \end{array} \quad \begin{array}{r} 7.8 \\ 19 \end{array} \quad \begin{array}{r} 6.4 \\ 16 \end{array} \quad \begin{array}{r} 7.0 \\ 6.9 \end{array} \quad \begin{array}{r} 7.6 \\ 17 \end{array} \quad \begin{array}{r} 8.6 \\ 19 \end{array} \quad \begin{array}{r} 8.8 \\ 22 \end{array} \quad \begin{array}{r} 7.6 \\ 25 \end{array} \quad \begin{array}{r} 8.8 \\ 33 \end{array}$$

$$\begin{array}{r} 3.0 \\ 33 \end{array} \quad \begin{array}{r} 9.7 \\ 24 \end{array} \quad \begin{array}{r} 9.8 \\ 19 \end{array} \quad \begin{array}{r} 8.2 \\ 16 \end{array} \quad \begin{array}{r} 8.7 \\ 8.6 \end{array} \quad \begin{array}{r} 8.7 \\ 16 \end{array} \quad \begin{array}{r} 11.0 \\ 20 \end{array} \quad \begin{array}{r} 11.2 \\ 23 \end{array} \quad \begin{array}{r} 11.0 \\ 24 \end{array} \quad \begin{array}{r} 13.0 \\ 33 \end{array}$$

$$\begin{array}{r} 4.3 \\ 33 \end{array} \quad \begin{array}{r} 4.9 \\ 30 \end{array} \quad \begin{array}{r} 5.6 \\ 28 \end{array} \quad \begin{array}{r} 5.6 \\ 22 \end{array} \quad \begin{array}{r} 3.0 \\ 15 \end{array} \quad \begin{array}{r} 3.0 \\ 3.1 \end{array} \quad \begin{array}{r} 3.0 \\ 15 \end{array} \quad \begin{array}{r} 3.5 \\ 19 \end{array} \quad \begin{array}{r} 15.3 \\ 37 \end{array}$$

$$\begin{array}{r} 9.8 \\ 33 \end{array} \quad \begin{array}{r} 7.2 \\ 26 \end{array} \quad \begin{array}{r} 3.9 \\ 16 \end{array} \quad \begin{array}{r} 4.1 \\ 4.2 \end{array} \quad \begin{array}{r} 4.3 \\ 18 \end{array} \quad \begin{array}{r} 19.1 \\ 40 \end{array}$$

$$\begin{array}{r} 10.8 \\ 33 \end{array} \quad \begin{array}{r} 10.3 \\ 25 \end{array} \quad \begin{array}{r} 5.1 \\ 17 \end{array} \quad \begin{array}{r} 5.0 \\ 5.1 \end{array} \quad \begin{array}{r} 5.2 \\ 16 \end{array} \quad \begin{array}{r} 19.0 \\ 38 \end{array}$$

$$\begin{array}{r} 5.0 \\ 33 \end{array} \quad \begin{array}{r} 5.0 \\ 32 \end{array} \quad \begin{array}{r} 7.4 \\ 27 \end{array} \quad \begin{array}{r} 7.8 \\ 20 \end{array} \quad \begin{array}{r} 5.9 \\ 16 \end{array} \quad \begin{array}{r} 5.8 \\ 5.8 \end{array} \quad \begin{array}{r} 6.6 \\ 20 \end{array} \quad \begin{array}{r} 8.6 \\ 23 \end{array} \quad \begin{array}{r} 10.9 \\ 33 \end{array}$$

Station	+	H.I.	-	Elev
		353.70 ✓		
158+50			7.1	346.6
159+00			8.0	345.7
159+50			9.3	344.4
160+00			10.4	343.3
T.P.	3.16	346.39 ✓	10.47	343.23 ✓
B.M.			4.55	341.84 ✓
"	2.76	344.59 ✓		341.83 ✓
160+50			2.5	342.1
161+00			3.5	341.1
161+50			4.3	340.3
162+00			5.1	339.5
162+50			6.0	338.6
163+00			6.4	338.2
163+50			6.7	337.9
164+00			6.4	338.2
T.P.	10.16	348.33 ✓	6.42	338.17 ✓

35.40 7.8 8.0 6.8 7.1 7.2 8.7 8.4 4.6
33 23 19 15 7.0 18 19 25 33

0.8 8.6 8.8 7.8 8.0 8.2 9.0 8.8 2.7
33 22 18 15 8.0 16 19 23 33

1.6 7.7 7.8 9.4 7.3 9.4 10.3 9.9 5.1
33 23 19 17 9.3 15 18 27 33

10.4 10.4 12.1 11.9 10.5 10.4 10.8 13.2 13.5 14.3
33 31 26 22 18 10.2 15 21 25 33

R.R. Spike in 12" Oak 30 Rt. 160x75

Aug. 27-1924

9.2 9.2 3.2 2.4 2.5 2.4 2.5 9.2
33 26 16 12 2.5 17 28 33

7.1 9.1 9.1 3.6 3.5 3.8 6.1 8.0 3.1 3.1
33 29 26 17 3.4 18 22 32 33

7.0 7.0 6.6 7.3 7.1 4.2 4.3 4.3 5.9 340.9 345.9
33 30 24 24 21 16 4.2 12 17 20 33 33?

8.3 7.8 8.4 8.2 5.2 5.1 5.2 6.1 5.9 0.6
33 28 27 23 17 5.1 18 21 25 33

8.6 8.6 9.1 9.2 6.0 6.0 5.9 10.0 10.3 10.0
33 29 27 22 16 6.0 17 24 29 33

10.0 10.4 6.5 6.4 6.4 14.6
33 22 15 6.5 18 33

10.1 10.1 6.5 6.7 6.7 7.5 16.0
33 23 15 6.7 13 19 33

6.6 6.6 9.6 9.3 6.6 6.4 7.0 14.1 14.5
33 37 30 22 16 6.4 18 30 33

station	+	HI	-	elev.
		348.33 ✓		
164+50			10.2	338.1
165+00			10.3	338.0
165+50			10.5	337.8
166+00			10.6	337.7
166+50			11.0	337.3
167+00			11.5	336.8
167+50			11.7	336.6
168+00			11.9	336.4
168+50			12.0	336.3
169+00			12.5	335.8
T.P	3.66	340.09 ✓	1.90	336.43 ✓
169+50			4.5	335.6
170+00			4.8	335.3
170+50			5.0	335.1

Lt.

L

Rt.

6

7.8	11.5	11.7	10.2	10.2	10.1	16.6	17.0
30	24	19	16	(10.1)	17	27	33

only
Er.

0.0	11.0	11.5	10.4	10.3	10.2	11.1	11.0	348.9	348.9
35	21	18	17	(10.3)	15	17	21	32	33

4.5	11.0	11.4	10.7	10.5	10.4	10.7	11.6	11.2	43	29
35	26	18	16	(10.6)	13	17	19	33	31	33

9.2	9.1	10.7	11.0	10.7	10.6	10.5	11.4	10.8	3.7
33	27	23	18	15	(10.1)	15	18	22	33

11.4	11.0	11.8	11.9	11.1	11.0	11.0	12.0	11.5	6.5	6.5
33	24	22	18	14	(11.0)	15	17	23	30	33

13.0	13.0	11.9	11.5	12.5	11.6	11.9	12.3	12.2	10.8	10.6
33	17	15	12	(11.4)	15	17	18	23	26	33

12.0	12.9	11.6	12.7	11.9	13.4	13.4	13.0	13.4
33	16	13	(11.7)	17	19	24	27	33

+90 0.0 Cut Lt. & Rt

7.1	12.3	12.3	11.6	11.9	12.0	13.9	14.0	12.5	12.8
33	22	16	14	(11.9)	17	21	27	30	33

0.3	12.5	12.9	11.9	12.0	12.0	13.0	13.0	1.8
36	22	18	15	(12.0)	14	18	24	35

8.9	14.1	14.1	12.5	12.5	12.4	13.4	13.4	6.0
33	25	19	14	(12.4)	16	18	24	33

9.0	8.3	8.3	4.1	1.5	4.7	8.2	8.1
33	28	24	17	(4.4)	18	25	33

12.1	11.7	5.2	4.8	4.8	5.3	15.6
33	29	18	13	(4.8)	14	33

14.6	5.2	5.0	5.3	15.7
33	17	(5.1)	18	33

station	+	H.I	-	Elev.
		340.09 ✓		
171+00			5.1	335.0
171+50			4.8	335.3
172+00			4.6	335.5
172+50			4.7	335.4
173+00			4.7	335.4
173+50			4.3	335.8
174+00			4.4	335.7
174+50			4.1	336.0
T.P.	10.74	346.49 ✓	4.34	335.75 ✓
174+50			10.4	336.1
175+00			10.2	336.3
175+50			10.2	336.3
176+00			10.0	336.5
176+50			10.3	336.2
177+00			10.6	335.9

Lt.

L

Rt.

⑦

15.0	5.5	5.1	5.5	15.6
33	18	(5.2)	19	33

12.5	12.0	4.9	4.8	5.1	11.1	11.7
33	29	18	(4.7)	20	30	33

8.8	4.7	4.6	4.8	7.5	7.8	6.5	6.4
orig. 25	76	(4.5)	76	23	26	30	33

5.4	5.0	6.3	6.3	4.8	4.7	4.4	6.0	5.5	547.3
33	31	26	19	16	(4.5)	76	20	26	39
	3.2	6.2	6.2	4.8	4.7	1.6	5.9	5.6	540.6
	33	27	19	15	4.7	76	20	25	40
0.4	5.3	5.8	4.8	4.3	4.3	4.5	5.7	5.7	345.1
33	24	18	16	12	(4.2)	76	19	24	35

67.56	6.8	6.8	4.7	4.4	4.1	4.4	5.0	6.0	6.0	4.3	4.3
3328	24	19	15	10	(4.3)	13	17	21	28	31	33

8.6	8.3	4.5	4.7	4.0	5.9	5.9	2.9
33	24	16	(4.1)	15	22	28	33

Top Rock Rt.

11.6	11.5	11.9	12.1	11.2	10.4	10.6	12.5	12.5	12.0	11.1
33	25	23	20	16	(10.3)	15	19	26	30	33

12.1	13.6	10.1	10.2	10.1	12.8	12.4
33	24	15	(10.2)	13	18	33

8.2	11.2	11.2	10.3	10.2	10.4	11.9	12.0	9.2
33	26	21	17	(10.2)	16	20	28	33

4.5	10.8	11.1	10.1	10.0	10.1	11.7	11.7	6.8
33	26	19	17	10.1	16	20	26	33

5.8	11.2	11.3	10.2	10.3	10.4	11.4	11.2	7.0	7.0
34	26	19	16	10.2	14	17	26	31	33

9.5	12.0	12.3	10.8	10.6	11.0	11.8	11.8	10.8	11.0
33	28	20	16	10.5	16	19	25	27	33

Station	+	H.I	-	Elev.
		346.49	✓	
177+50			10.7	335.8
178+00			10.8	335.7
178+50			10.6	335.9
179+00			10.4	336.1
179+50			9.9	336.6
180+00			9.1	337.4
	8.45	345.85	✓	
			9.09	337.40
180+50			7.5	38.4
181+00			6.8	39.1
181+50			6.0	39.9
182+00			5.7	40.2
182+25			5.6	40.3
182+75			5.3	40.6
183+00			5.1	40.8

Lt. K Rt.

(8)

8.8 11.7 12.3 10.8 10.7 11.0 11.9 11.7 10.2 9.3
35 28 20 16 10.6 15 18 27 32 33.

8.5 12.4 12.9 10.7 10.8 10.8 12.3 12.3 10.4 10.4
34 26 20 17 10.6 15 18 27 31 33

13.2 12.6 13.4 13.3 10.8 10.6 10.8 12.8 13.0
33 29 27 25 18 10.5 16 20 33

15.5 15.5 10.4 10.4 10.8 17.8 17.8
33 29 20 10.3 17 28 33

13.6 13.4 14.1 9.8 9.9 10.2 16.1 16.3
33 29 26 18 9.8 17 28 33

12.4 12.5 9.5 9.1 9.1 9.1 13.3 13.3
33 25 18 12 9.1 18 25 33

11.4 10.5 7.4 7.5 7.6 8.9 8.9 7.9 8.1
33 24 18 7.5 16 21 26 28 33

5.2 8.2 8.4 7.1 6.8 6.8 8.1 7.6 3.7 4.0
33 27 20 17 7.0 16 19 26 31 33

0.1 6.6 7.0 6.2 6.0 6.2 7.7 7.8 6.3 6.3
35 26 21 19 6.0 15 19 26 30 33

3.6 7.0 7.0 5.6 5.7 5.8 7.0 7.0 6.0 6.6
36 27 20 17 5.8 16 19 25 27 33

6.4 6.4 7.6 7.5 5.7 5.6 6.7 6.9 5.7 6.4
33 29 27 20 16 15 18 23 26 33

6.5 6.0 7.6 7.5 5.5 5.4 6.2 6.2 4.6 4.6
33 28 26 20 15 15 18 24 28 33

7.7 7.1 8.1 8.0 5.4 5.1 5.0 5.6 5.1 3.2 3.2
33 29 26 20 16 5.1 15 18 23 28 33

Station	+	H.I	-	Elev
		345.85 ✓		
183+50			5.0	340.9
184+00			5.0	340.9
T.P.	9.70	350.24 ✓	5.21	340.54 ✓
184+50			9.0	341.2
185+00			8.9	341.3
185+50			8.6	341.6
186+00			8.6	341.6
186+20			8.7	341.5
186+27			8.7	341.5
186+31			8.7	341.5
186+54			9.2	341.0
186+62			9.5	340.7
187+00			10.6	339.6
187+50			11.5	338.7

Lt. £ R4.

10.6	9.0	5.6	5.0	5.0	6.6	6.5	5.1	5.5
33	22	76	5.0	74	18	24	28	33

8.4	7.7	5.3	5.0	4.8	8.5	9.0	8.2	8.2
33	19	15	5.0	13	19	24	26	33

12.7	11.5	9.5	9.0	9.1	11.0	10.8	10.2	10.2
33	19	15	8.9	15	20	26	31	33

7.4	8.9	8.9	8.9	8.8	9.9	10.0	5.7
33	24	12	8.7	16	20	27	33

4.8	5.0	8.8	8.9	8.6	8.8	9.0	9.5	2.8
33	29	23	15	8.6	18	23	27	35

7.6	8.0	7.6	9.4	8.9	8.6	8.7	8.8	9.1	2.1	
33	24	22	19	16	8.6	18	31	48	52	60

7.4	7.9	9.8	9.1	8.7	8.7	8.6	8.8	3.4
33	27	24	18	8.6	50	72	84	91

7.4	10.1	9.6	9.1	8.7	8.6	8.5
38	32	29	16	8.7	50	80

10.3	10.0	9.2	8.7	8.4	8.4
40	33	16	8.8	50	80

13.0	13.0	12.0	10.4	9.6	9.2	8.8
96	91	87	50	21	9.5	40

6.1	11.1	11.3	10.3	9.5	9.5	9.4	8.6	8.6
95	78	73	50	16	10.0	29	32	33

9.0	9.9	10.7	10.6	11.0	12.3	12.2	9.8	10.4	10.6
46	34	27	10.5	14	18	22	26	31	33

8.3	12.4	12.8	11.8	11.3	11.6	12.2	13.2	9.8	9.7
33	26	20	15	11.3	13	17	23	28	33

Station	+	H.I	-	Elev.
		350.24 ✓		
188			13.2	337.0
188+50				35.9
	1.54	341.22 ✓	10.56	339.68 ✓
188+50			5.3	335.9
B.M.	0.67	341.25 ✓	0.67	340.55 ✓
		341.26 ✓		340.58
189+00			6.7	334.5
189+50			8.4	332.8
190+00			10.3	330.9
190+50			12.0	329.2
190+75				328.5
191+00				327.6
T.P.	0.38	330.76 ✓	10.88	330.38 ✓
190+75			2.2	328.5
191+00			3.1	327.6
191+25			4.0	326.7
192+00			1.0	323.7

H.

2

Rt.

(10)

6.9	6.2	13.7	13.7	13.2	13.2	13.2	14.0	14.0	3.3	2.3
33	31	23	19	17	(13.0)	12	17	20	30	33

(14.2)

11.5	6.5	1.0
24	31	33

5.2	5.0	7.1	6.9	5.5	5.3	4.8	6.0	5.8
33	32	26	19	15	(5.2)	12	15	21

B.M. R.R. spike in T.P 30 Rt. 127+30

10.3	9.8	8.9	9.4	9.1	7.3	6.7	6.7	8.0	7.6	0.0
33	30	27	25	20	16	(6.5)	12	15	20	30

11.4	10.5	10.6	10.3	8.9	8.4	8.5	10.6	10.0	6.7	6.6
33	26	25	20	16	(8.3)	13	18	24	28	33

10.8	10.8	11.3	11.3	10.6	10.3	10.4	12.2	12.0	8.8	8.3
33	30	25	20	16	(10.3)	13	17	25	30	33

6.0	13.4	12.4	12.2	12.0	12.3	11.8	11.8	7.1	7.5
36	27	21	18	(12.0)	15	17	22	30	33

4.3
34

(12.7)

6.0	6.5
30	33

8.6
33

(13.5)

10.8	11.9
30	33

2.8	3.1	2.3	2.2	2.4	4.0	3.7
25	20	17	(2.2)	13	17	20

3.9	4.1	3.3	3.1	3.2	5.1	4.7
24	19	16	(3.1)	12	17	23

10.0	9.2	4.4	4.0	4.0	8.1	9.4
33	26	18	(3.5)	15	26	33

14.1	18.6	7.7	7.0	7.1	13.3	13.3
33	28	19	(7.0)	17	27	33

Station	+	H.I	-	Elev.
		330.76 ✓		
192+50			8.6	332.1
193+00			9.1	331.6
193+50			9.4	321.3
194+00			10.0	320.7
T.P.	2.35	323.26 ✓	9.85	320.91 ✓
194+50			3.0	320.2
195+00			3.7	319.5
195+50			4.2	319.0
195+74			4.4	318.9
196+00			4.6	318.7
196+50			5.1	318.2
B.M.	5.91		8.86	314.40 ✓
B.M.	5.92	310.37 ✓		314.45
197+00			2.7	317.7
197+50			3.7	316.7

Lt.

L

Rt.

(11)

14.2	14.2	9.0	8.6	8.7	13.0	13.5
33	27	18	(8.6)	16	23	33

14.1	13.3	9.3	9.1	9.4	12.9	12.9
33	25	18	(9.0)	16	22	33

140 = 0.0 cut Lt.

6.8	10.8	10.7	9.4
33	28	18	15

(9.5)

125 = 0.0 cut Rt.

9.2	10.4	10.2	6.2	6.4
16	18	23	28	33

7.4	14.5	11.5	10.6	10.1	10.0	9.9	11.7	11.5?	9.1	9.7
33	28	19	15	11	(10.1)	16	19	(2.5)	27	33

0.8	4.1	4.6	3.3	3.0	3.0	4.5	4.7	4.0	4.6
33	27	19	14	(3.1)	13	18	24	25	33

2.2	4.8	5.2	3.7	3.7	3.7	5.2	5.4	6.0
33	29	19	15	(3.7)	15	19	25	33

32.4	5.2	5.6	4.5	4.2	4.3	5.6	6.4	6.4
33	27	18	15	(4.2)	15	18	26	33

26.1	5.2	5.8	4.7	4.4	4.4	6.0		6.2
33	27	18	15	4.4	15	18		30
323.9	6.0	6.0	5.2	4.6	4.6	6.4	6.5	4.9
33	26	18	15	(4.6)	14	17	21	23
								78
								33

9.0	7.7	8.1	7.8	5.4	5.1	5.1	7.0	6.8	1.5	2.0
33	27	25	22	15	(5.0)	14	20	23	29	33

R.R. Sp. Ke in T.P. 47+80 30' Rt.

Aug-29-1924

" " " "

9.5	8.5	3.6	2.7	2.6	4.8	5.0	2.8	3.0
33	28	18	(2.8)	14	19	26	29	33

10.0	9.7	4.3	3.7	3.8	6.3	7.1	7.0
33	27	16	(3.7)	16	24	28	33

station	H.I		Elev.	
		320.37 ✓		
198			4.5	315.9
198 +50			4.6	315.8
199			4.4	316.0
+50			4.4	316.0
200			4.8	315.6
+50			5.4	315.0
201			6.1	314.3
+50			6.2	314.2
202			6.6	313.8
+50			6.9	
203			7.4	
T.P.	4.61	317.58 ✓	7.40	312.97 ✓
+50			5.1	
204			6.1	

24

2

Rt.

(12)

10.1	10.1	5.4	4.5	4.3	5.8	7.3	8.0	8.1
<u>33</u>	<u>28</u>	<u>18</u>	<u>46</u>	<u>16</u>	<u>18</u>	<u>26</u>	<u>28</u>	<u>33</u>

10.1	9.3	5.2	4.6	4.3	5.7	6.3	5.8
<u>33</u>	<u>23</u>	<u>16</u>	<u>45</u>	<u>16</u>	<u>22</u>	<u>27</u>	<u>33</u>

6.0	5.7	5.7	4.7	4.4	4.3	6.2	5.5	1.0	1.1
<u>33</u>	<u>24</u>	<u>16</u>	<u>13</u>	<u>45</u>	<u>16</u>	<u>20</u>	<u>24</u>	<u>30</u>	<u>33</u>

2.3	5.8	6.0	4.6	4.4	4.7	6.6	6.7	5.2	3.3	3.3
<u>33</u>	<u>28</u>	<u>16</u>	<u>12</u>	<u>45</u>	<u>17</u>	<u>21</u>	<u>26</u>	<u>29</u>	<u>31</u>	<u>33</u>

3.6	6.8	6.9	5.6	4.8	4.9	6.4	6.6	4.8	5.2
<u>33</u>	<u>78</u>	<u>19</u>	<u>15</u>	<u>49</u>	<u>15</u>	<u>18</u>	<u>21</u>	<u>23</u>	<u>33</u>

4.6	5.7	7.3	7.2	5.8	5.4	5.5	7.3	7.9	8.1	8.1
<u>33</u>	<u>27</u>	<u>25</u>	<u>18</u>	<u>15</u>	<u>55</u>	<u>13</u>	<u>18</u>	<u>26</u>	<u>32</u>	<u>32</u>

5.9	5.8	7.4	7.5	6.2	6.1	6.2	8.0	9.0	9.0
<u>33</u>	<u>31</u>	<u>27</u>	<u>18</u>	<u>15</u>	<u>60</u>	<u>13</u>	<u>18</u>	<u>21</u>	<u>33</u>

5.7	5.4	7.9	7.9	6.7	6.2	6.5	7.8	8.4
<u>33</u>	<u>30</u>	<u>26</u>	<u>19</u>	<u>15</u>	<u>65</u>	<u>13</u>	<u>16</u>	<u>33</u>

4.4	4.6	6.1	7.7	7.9	6.9	6.6	7.0	9.0	10.7
<u>33</u>	<u>31</u>	<u>29</u>	<u>24</u>	<u>18</u>	<u>15</u>	<u>63</u>	<u>12</u>	<u>18</u>	<u>33</u>

3.7	3.7	5.8	7.8	7.5	7.1	6.9	7.1	9.0	10.9
<u>33</u>	<u>31</u>	<u>28</u>	<u>26</u>	<u>19</u>	<u>14</u>	<u>61</u>	<u>13</u>	<u>17</u>	<u>33</u>

6.6	6.2	8.8	8.8	7.8	7.4	7.8	8.9	10.0	11.2
<u>33</u>	<u>31</u>	<u>27</u>	<u>18</u>	<u>15</u>	<u>75</u>	<u>13</u>	<u>17</u>	<u>23</u>	<u>33</u>

6.5	5.9	7.1	7.1	5.6	5.1	5.7	6.5	7.0	7.9
<u>33</u>	<u>28</u>	<u>26</u>	<u>20</u>	<u>15</u>	<u>52</u>	<u>14</u>	<u>17</u>	<u>23</u>	<u>33</u>

7.8	7.5	8.5	8.6	6.5	6.1	6.4	7.9	7.8	5.2
<u>33</u>	<u>28</u>	<u>25</u>	<u>20</u>	<u>14</u>	<u>61</u>	<u>14</u>	<u>19</u>	<u>28</u>	<u>33</u>

station	+	H.T	-	Elev
		317.58 ✓		
204+50			7.0	310.6
205+00			8.4	309.2
205+50			9.4	308.2
206			10.7	306.9
+50			12.0	305.6
T.P.	0.20	306.20 ✓	11.58	306.00 ✓
207			2.1	304.1
+50			3.8	302.4
208			5.5	300.7
+50			6.7	299.5
209			7.5	298.7
B.M.	8.79	303.61 ✓	11.38	294.82 ✓
209 + 20			5.1	298.5
+50			5.5	298.1
209 + 75			5.3	298.3

Lt.

L

R

(13)

10.1	9.5	10.7	10.7	7.4	7.0	6.8	8.5	8.5	9.0
<u>33</u>	<u>28</u>	<u>26</u>	<u>21</u>	<u>14</u>	<u>7.11</u>	<u>14</u>	<u>19</u>	<u>26</u>	<u>33</u>

9.2	9.5	11.3	11.3	8.5	8.4	8.5	10.0	9.8	2.6
<u>33</u>	<u>29</u>	<u>26</u>	<u>20</u>	<u>13</u>	<u>8.6</u>	<u>15</u>	<u>19</u>	<u>24</u>	<u>33</u>

8.8	8.5	11.9	11.9	7.6	7.4	7.4	10.5	10.1	0.5
<u>33</u>	<u>30</u>	<u>26</u>	<u>20</u>	<u>14</u>	<u>9.6</u>	<u>14</u>	<u>18</u>	<u>22</u>	<u>33</u>

10.1	7.7	13.2	13.2	11.1	10.7	10.8	11.9	11.4	1.3
<u>33</u>	<u>30</u>	<u>24</u>	<u>18</u>	<u>14</u>	<u>10.9</u>	<u>15</u>	<u>18</u>	<u>23</u>	<u>33</u>

14.1	14.1	14.9	14.9	12.4	12.0	12.3	13.6	13.6	5.4
<u>33</u>	<u>26</u>	<u>25</u>	<u>19</u>	<u>14</u>	<u>12.1</u>	<u>15</u>	<u>18</u>	<u>24</u>	<u>33</u>

7.0	6.4	4.8	3.9	2.5	2.1	2.2	4.0	4.0	30.75
<u>33</u>	<u>28</u>	<u>24</u>	<u>16</u>	<u>13</u>	<u>2.6</u>	<u>16</u>	<u>20</u>	<u>26</u>	<u>33</u>

10.8	10.0	4.3	3.8	4.0	5.7	5.7	4.4	4.4
<u>33</u>	<u>28</u>	<u>16</u>	<u>3.8</u>	<u>15</u>	<u>21</u>	<u>27</u>	<u>30</u>	<u>33</u>

12.1	12.0	6.7	5.5	5.6	8.6	9.3	10.3	10.3
<u>33</u>	<u>26</u>	<u>17</u>	<u>5.4</u>	<u>15</u>	<u>20</u>	<u>29</u>	<u>31</u>	<u>33</u>

12.6	12.2	7.8	7.2	6.7	6.7	8.5	8.5	12.5	11.5	8.9
<u>33</u>	<u>30</u>	<u>22</u>	<u>13</u>	<u>6.6</u>	<u>15</u>	<u>18</u>	<u>21</u>	<u>25</u>	<u>28</u>	<u>33</u>

13.9	9.4	8.7	7.5	7.4	10.2	10.9	12.5	9.9	10.5
<u>39</u>	<u>32</u>	<u>19</u>	<u>7.5</u>	<u>15</u>	<u>20</u>	<u>24</u>	<u>27</u>	<u>31</u>	<u>33</u>

R.R. Sp. 10. INT. P 30' RT. 210 + 50

11.1	7.6	6.2	5.1	4.8	6.2	9.8	8.8	8.8
<u>41</u>	<u>35</u>	<u>19</u>	<u>5.2</u>	<u>14</u>	<u>17</u>	<u>24</u>	<u>29</u>	<u>33</u>

14	8.1	6.2	5.5	4.6	5.2	8.7	9.3	9.8
<u>42</u>	<u>38</u>	<u>19</u>	<u>5.7</u>	<u>13</u>	<u>17</u>	<u>22</u>	<u>28</u>	<u>33</u>

10.6	7.6	6.2	5.3	4.8	5.3	6.7	9.1
<u>43</u>	<u>37</u>	<u>20</u>	<u>5.4</u>	<u>8</u>	<u>16</u>	<u>24</u>	<u>33</u>

Station.	+	H.I	-	Elev.
		303.61 ✓		
210+00			5.0	298.6
+25			4.8	298.8
+50			4.7	298.9
+83.4			4.7	298.9
211+00			4.7	298.9
+25			4.7	298.9
+50			4.7	298.9
+75'			4.6	299.0
212+00			4.6	299.0
+27.5			4.7	298.9
+50			4.7	298.9
213+00			4.7	298.9
+27.5			4.7	298.9
T.P.	5.58	304.84 ✓	4.35 4.35	299.26 ✓

Lt.

X

Rt.

(14)

10.5	6.7	6.0	5.0	5.0	5.6	6.3	7.9	7.6
$\frac{43}{36}$	$\frac{36}{19}$	$\frac{5.0}{5.0}$	$\frac{5.0}{10}$	$\frac{5.6}{16}$	$\frac{6.3}{20}$	$\frac{7.9}{22}$	$\frac{7.6}{33}$	

9.4	6.6	5.8	4.8	4.8	5.2	8.7	10.2
$\frac{38}{35}$	$\frac{20}{20}$	$\frac{4.8}{4.8}$	$\frac{4.8}{8}$	$\frac{5.2}{17}$	$\frac{8.7}{24}$	$\frac{10.2}{33}$	

9.3	5.9	5.5	4.7	4.7	5.6	9.0	9.9
$\frac{37}{31}$	$\frac{18}{18}$	$\frac{4.7}{4.8}$	$\frac{4.7}{10}$	$\frac{5.6}{18}$	$\frac{9.0}{24}$	$\frac{9.9}{33}$	

9.4	9.4	5.6	5.6	4.7	5.1	8.7	9.8
$\frac{33}{32}$	$\frac{25}{14}$	$\frac{4.7}{4.7}$	$\frac{5.1}{16}$	$\frac{8.7}{23}$	$\frac{9.8}{33}$		

8.6	8.6	5.3	5.3	4.7	5.1	7.9	9.3
$\frac{33}{31}$	$\frac{23}{12}$	$\frac{4.7}{4.7}$	$\frac{5.1}{14}$	$\frac{7.9}{21}$	$\frac{9.3}{33}$		

7.6	7.9	5.4	4.7	5.3	7.4	8.6
$\frac{33}{23}$	$\frac{18}{18}$	$\frac{4.7}{4.7}$	$\frac{5.3}{15}$	$\frac{7.4}{22}$	$\frac{8.6}{33}$	

6.7	6.6	5.1	4.7	5.2	5.4	3.7	7.1
$\frac{33}{24}$	$\frac{21}{21}$	$\frac{4.7}{4.6}$	$\frac{5.2}{14}$	$\frac{5.4}{16}$	$\frac{3.7}{24}$	$\frac{7.1}{36}$	

6.3	6.4	6.6	5.0	4.6	5.0	5.7	5.1
$\frac{33}{28}$	$\frac{24}{20}$	$\frac{4.6}{4.6}$	$\frac{5.0}{12}$	$\frac{5.7}{27}$	$\frac{5.1}{33}$		

5.8	5.7	6.5	6.6	5.2	4.6	4.9	4.0	4.9
$\frac{33}{28}$	$\frac{26}{23}$	$\frac{5.2}{18}$	$\frac{4.6}{4.5}$	$\frac{4.9}{17}$	$\frac{4.0}{23}$	$\frac{4.9}{33}$		

5.5	5.7	6.3	6.0	4.9	4.7	5.2	5.6	4.9	4.4
$\frac{33}{25}$	$\frac{24}{21}$	$\frac{4.7}{10}$	$\frac{4.6}{4.6}$	$\frac{5.2}{13}$	$\frac{5.6}{18}$	$\frac{4.9}{23}$	$\frac{4.4}{33}$		

5.6	5.6	6.5	6.3	5.2	4.7	5.2	5.6	4.9	4.6
$\frac{33}{27}$	$\frac{26}{21}$	$\frac{5.2}{19}$	$\frac{4.7}{4.7}$	$\frac{5.2}{12}$	$\frac{5.6}{19}$	$\frac{4.9}{22}$	$\frac{4.6}{33}$		

6.3	5.8	6.6	6.3	5.0	4.7	5.1	5.8	5.5	4.9	4.8	No
$\frac{33}{24}$	$\frac{23}{21}$	$\frac{5.0}{18}$	$\frac{4.7}{4.6}$	$\frac{5.1}{11}$	$\frac{5.8}{17}$	$\frac{5.5}{22}$	$\frac{4.9}{24}$	$\frac{4.8}{33}$			
6.6	6.2	5.5	5.2	4.7	5.0	5.6	6.5	6.6	5.7	4.2	
$\frac{33}{24}$	$\frac{19}{14}$	$\frac{4.7}{4.6}$	$\frac{5.0}{11}$	$\frac{5.6}{16}$	$\frac{6.5}{18}$	$\frac{6.6}{21}$	$\frac{5.7}{23}$	$\frac{4.2}{33}$			

Nail in tree - Rt 13 + 24

Exc. on Right.

Station	+	H.I	-	Elev.
		304.84		
214+00			6.0	298.8
+25			5.8	299.0
+50			5.7	299.1
+75			5.6	299.2
215+00			5.3	299.5
+25			5.3	299.5
+45			5.3	299.5
+91			5.0	299.8
216			5.0	299.8
+25			4.9	299.9
+50			4.7	300.1
+75			4.5	300.3
217			3.8	301.0

Lt. Lt Rt

87	78	60	60	6.2	7.6	7.6	6.3	6.0	6.7
33	20	76	5.9	12	16	18	73	30	33

7.0	7.9	5.8	5.8	6.3	6.7	6.7	6.2	7.5
33	21	16	5.8	9	13	18	22	33

9.6	8.7	5.8	5.7	6.5	7.0	7.0	6.6	9.5	10.0
33	24	17	5.7	12	14	17	21	29	33

10.3	9.6	5.4	5.6	6.2	6.7	6.5	8.6	9.4
33	27	19	5.5	11	18	22	29	33

10.1	9.8	5.7	5.3	5.9	7.2	7.1	7.0	8.9
33	27	19	5.3	14	15	18	20	33

11.0	10.3	5.2	5.3	5.6	7.3	9.3
33	28	19	5.4	14	17	33

11.0	10.6	5.6	5.3	5.3	6.9	9.8
33	29	20	5.3	12	18	33

11.0	5.3	5.0	5.4	6.5	9.9
33	20	5.0	12	15	33

10.7	10.0	5.3	5.0	5.5	6.6	10.3
33	29	22	4.9	12	15	33

11.0	10.5	4.8	4.9	4.8	6.8	9.1	9.9
33	32	23	4.8	10	13	21	33

10.1	4.2	4.7	4.7	4.7	7.5	8.3	9.0
35	25	4.7	7	12	19	33	

9.1	3.8	3.9	4.5	4.8	2.0	7.7	9.7
33	26	14	4.4	9	14	22	33

7.2	3.4	3.3	3.8	4.0	7.2	9.4
34	28	16	3.6	11	17	33

Rt.
00
16.2x0.

Station	+	U.I	-	Elev.
		304.84 ✓		
217+75			2.6	302.2 ✓
+50			1.9	302.9
+75			0.9	303.9
218			0.0	304.8
+13.2				305.2
750				306.5
219+00				308.3
T.P.	10.71	315.54 ✓	0.01	304.83 ✓
217+75				303.9
218+00				304.8
218+13.2			10.3	305.2
218+50			9.0	306.5
219+00			1.2	308.3
219+31.9			6.1	309.4
B.M.	7.61	318.91 ✓	4.24	311.30 ✓

Lt.

L

Rt.

(16)

4.1	2.6	2.1	2.3	2.6	2.6	7.4	8.7	9.6
33	28	24	14	(2.5)	12	19	24	33

308.8	2.6	2.6	1.4	1.5	1.9	2.4	7.2	8.9	9.6
36	28	26	24	18	(1.9)	12	20	24	33

1.6	1.5	0.9	0.7	0.9	1.1	7.6	8.6	10.0
26	21	29	15	(0.8)	12	22	24	33

0.7	0.8	0.2	0.0	0.0	0.2	5.3	7.7	8.9	8.9
22	19	18	14	(0.0)	13	21	26	29	32

4.7	8.0	9.6
19	25	33

5.8	7.4	9.0
21	25	33

3.2	4.8
28	33

See below
av. not
complete

2.6
36

0.6
34

0.5	1.0	1.0	1.3	1.2	1.3	10.5
34	22	19	18	13	(11.2)	12

31	10.1	10.0	9.3	9.3	9.0	9.1
37	28	25	23	14	(9.0)	13

6.8	8.7	8.7	8.2	7.7	7.7	7.2	7.7	8.3
40	36	32	31	26	20	(7.2)	13	20

4.1	7.3	7.6	6.5	6.5	6.1	6.9	7.4	8.3	8.0	6.6	11.0
43	40	37	35	21	(6.1)	7	14	16	18	20	26

R.R. spike 30" W. Oak 35' Rt. Sta. 220

Station	+	H.J	-	Elev.
		318.91 ✓		
219+75			8.2	310.7
220+00			7.2	311.7
220+25			6.4	312.5
220+50			5.7	313.2
220+75			5.2	313.7
221+00			4.7	314.2
221+25			4.4	314.5
221+50			4.1	314.8
T.P.	4.36	319.83 ✓	3.41	315.47 ✓
222			5.0	314.8
222+50			5.6	314.2
223+00			6.4	313.4
223+50			7.5	312.3
224+00			9.1	310.7

4.

L

Rt.

(17)

59 9.0 9.6 8.1 8.4
 44 41 38 35 20

8.2
 (8.3)

8.0 8.4 10.4 11.1 9.7 7.8
 8 15 20 20 27 33

5.1 8.6 8.6 7.9 7.6
 43 39 36 34 20

7.2
 (7.4)

7.3 7.6 8.6 10.4 10.7 8.0
 8 15 19 24 29 33

3.9 7.5 7.5 7.0 7.0
 40 37 33 32 21

6.4
 (6.4)

6.7 7.4 7.7 7.8 7.8
 14 21 27 30 33

2.5 6.9 6.9 6.4 6.0
 37 34 30 28 15

5.7
 (5.6)

6.0 7.2 8.1 8.8
 12 17 24 33

0.5 6.1 6.4 5.7 5.6
 37 32 29 26 17

5.2
 (5.2)

5.4 8.3 8.6 7.6 8.4 9.1
 11 16 20 21 25 33

320.4 5.4 5.8 5.2 5.1
 37 31 27 25 18

4.7
 (4.7)

4.7 5.0 7.8 8.2 8.2 7.9 8.5
 8 12 16 21 22 25 33

322.0 5.3 5.4 5.0 4.8
 36 29 25 23 14

4.4
 (4.4)

4.6 6.4 6.6 5.9 7.6
 13 17 22 23 33

322.9 4.6 5.0 4.7 4.4
 34 27 21 19 13

4.1
 (4.0)

3.9 4.2 6.0 6.0 5.3 6.0
 16 16 21 24 28 33

(Red)

Top of Rock Rt Sta 221+70

11.1
 11.1
 11.1

322.6 5.0 5.1
 33 25 18

5.0
 (5.0)

5.2 5.7 6.8 5.6 5.9
 13 19 27 29 33

323.3 6.3 6.4 5.9
 33 22 18 16

5.6
 (5.5)

5.7 6.4 6.3 5.0
 15 26 29 33

324.6 7.3 7.1 6.6
 34 19 14 12

6.4
 (6.3)

6.8 7.1 7.6 7.7 5.3 5.3
 15 23 24 28 32 33

326.3 8.2 8.1 7.7
 35 17 15 13

7.5
 (7.5)

7.8 8.4 8.2 7.0 7.1 5.0
 15 23 27 31 32 38

327.8 7.5 7.8 7.2
 35 18 14 12

9.1
 (9.1)

9.5 9.7 10.1
 16 22 33

station	+	4.5	-	Elev.
		319.83 ✓		
224+50			10.7	
T.P.	1.60	310.08 ✓	11.35	308.48 ✓
225+00			2.5	307.6
225+50			4.1	306.0
226+00			5.5	304.6
T.P.	2.51	305.42 ✓	7.17	302.91 ✓
226+50			2.3	303.1
227+00			3.5	301.9
227+50			4.5	300.9
228+00			5.0	300.4
228+50			5.4	300.0
229+00			5.6	299.8
229+50			5.9	299.5
230+00			5.9	299.5
T.P.	5.54	305.07 ✓	5.89	299.53 ✓
230+50			5.5	299.4

Lt.

R

Rt.

15

(98)
205

3202	110	110	106	107	109	113	116
33	16	13	12	15	21	33	

(10.1)

(101)
203

316.4	3.1	3.6	2.6	2.7	3.4	4.1	4.0
34	22	17	16	12	20	25	33

(21.6)

0.6	5.2	5.2	4.6	4.2	4.3	5.0	7.0	8.0
33	22	18	16	10	12	16	22	33

(4.1)

94	9.2	5.1	5.8	7.5	10.1
33	24	17	13	25	33

(5.4)

8.2	8.2	2.8	2.3	2.6	2.8	8.9	9.7
33	27	18	12	16	27	33	

(7.2)

10.2	7.0	4.2	3.5	4.0	9.1	7.1
33	25	17	15	24	33	

(3.4)

10.4	9.8	5.1	4.5	4.8	9.1	10.0
33	25	17	14	22	33	

(4.3)

8.5	8.0	5.1	5.0	5.4	9.0	9.3
33	24	16	14	23	33	

(5.0)

8.9	8.6	5.4	5.4	5.8	8.1	9.1	10.3	10.3	8.8	8.0
33	24	18	15	21	24	25	27	28	33	

(5.3)

8.4	8.0	6.0	5.6	5.8	6.2	10.1	9.0	8.0	7.6
33	21	16	11	16	22	24	28	33	

(5.4)

8.3	8.3	5.9	5.9	6.2	6.8	7.9
33	22	16	12	18	33	

(5.8)

9.0	8.1	6.0	5.9	6.3	8.6	7.2
33	23	17	15	28	33	

(5.7)

8.4	8.4	6.0	5.5	5.9	6.1	8.4
33	23	17	15	19	33	

(5.4)

No Filling done on Right.

station	+	H.I	-	Elev.
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305.07 ✓

231+00			5.4	299.7
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231+50			5.2	299.9
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232+00			4.9	300.2
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End of County Work Aug 30, 1924.

checking.

T.P.	4.09	304.85 ✓	4.31	300.76 ✓
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B.M.			7.18	197.67 ✓
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L.

Z

Rt.

19

8.3	8.3	6.0	5.4	6.1	8.0	8.9	8.9	8.5	8.5
<u>33</u>	<u>23</u>	<u>7</u>	<u>54</u>	<u>14</u>	<u>18</u>	<u>22</u>	<u>23</u>	<u>25</u>	<u>33</u>

7.7	7.7	5.5	5.2	5.8	7.0	8.5	8.5	7.6	7.4
<u>33</u>	<u>22</u>	<u>18</u>	<u>53</u>	<u>14</u>	<u>18</u>	<u>21</u>	<u>23</u>	<u>25</u>	<u>33</u>

6.9	6.9	5.0	4.9	5.4	6.4	8.4	8.4	6.7	6.4
<u>33</u>	<u>20</u>	<u>15</u>	<u>49</u>	<u>14</u>	<u>20</u>	<u>21</u>	<u>23</u>	<u>24</u>	<u>33</u>

R.R. to T.P. N.W. cor. Co Rd "C" & E. Co. Line

Lake Imp = Elev. 991.17

Finish.

W.H.C.

Aug 30, 1924

Eck

Gahlin

Fronke.

