

Dr. 8 - Bk. 164

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

..... PLAN Survey

..... EAST AVENUE

From Minnehaha St to Maryland St.

Add Stillwater Rd. Conn. 1946

Road Acc't. No.

te Filed.

File.

LAKEWOOD DRIVE Profile 1960

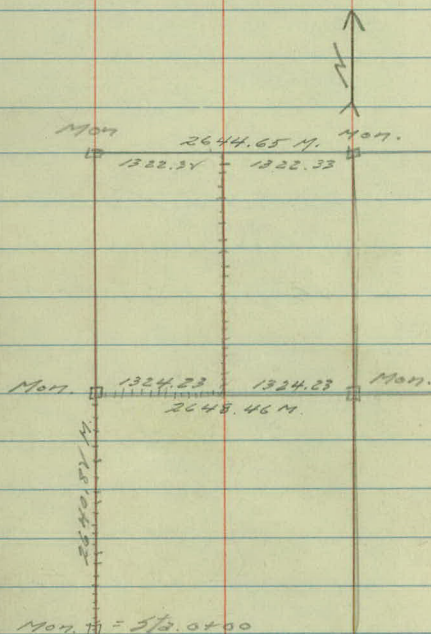
Plan Survey

East Avenue from Minnehaha St.
to Intersection with North
Line of Section 25, or
Maryland St.

12/28.

{ Bratager
Wilke
Goldberg
Moeschter

New Canada Township
Section 25



Alignment

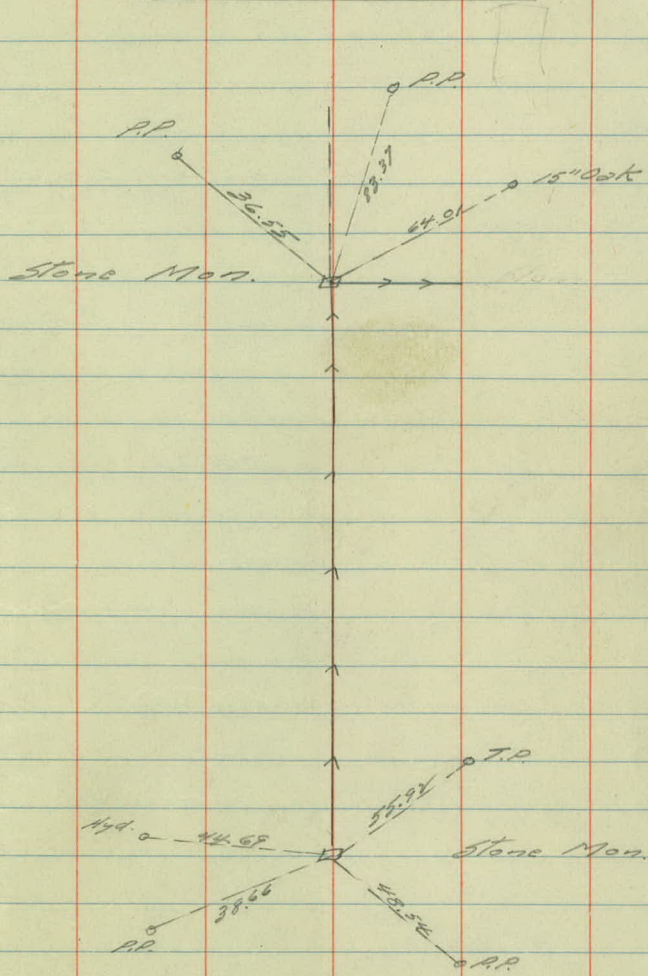
Angle

Sta.	Point	Lt.	Rt.	Defl.
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26+40 ⁸²	P.I.			
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0+00	Mon.			
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Reference Points



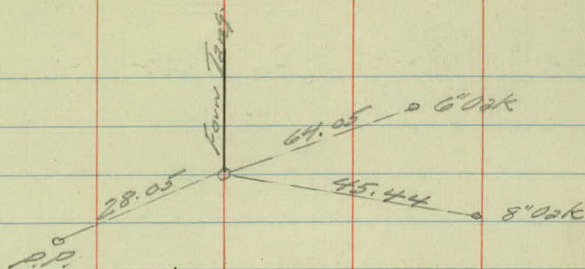
Angle

Sta.	Point	Lt.	Rt.	Defl.
+				
40+79.81	P.T.			44°32'
+50				40°21½'
40				33°21½'
39+65.05	P.I.	89°04'		D=22°00'
				T=203.34
+50				26°21½' L=318.10
39				19°21½'
+50				13°21½'
38				5°21½'
37+61.71	P.C.			

Reference Points

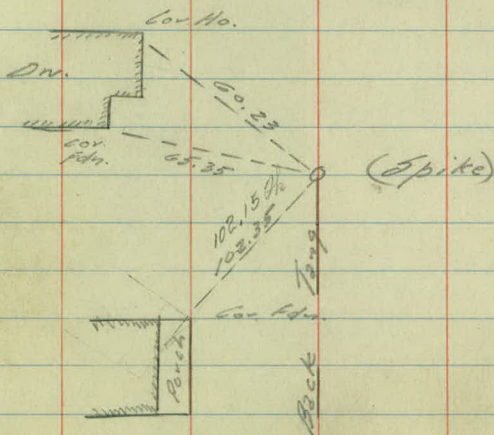
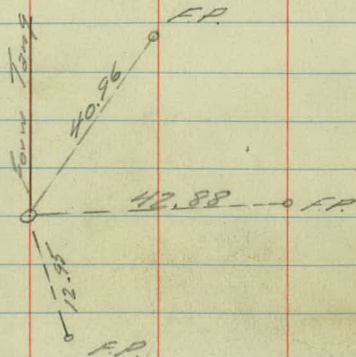
4

(Spike)



1/4 1/4 line

(Spike)

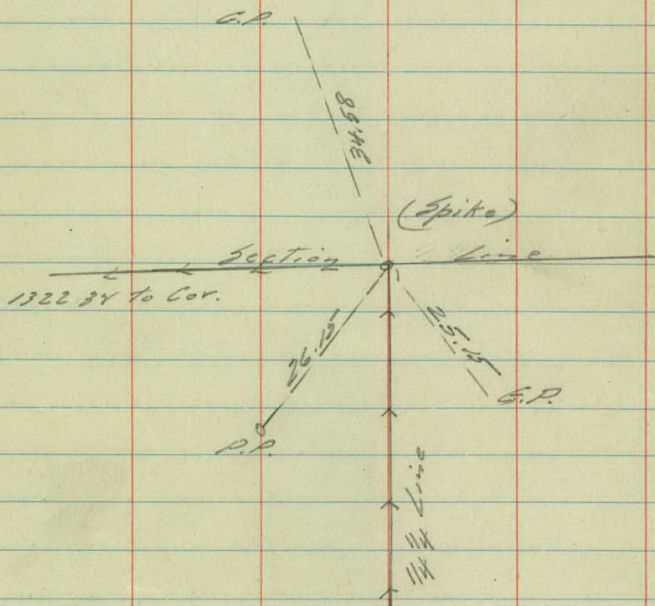


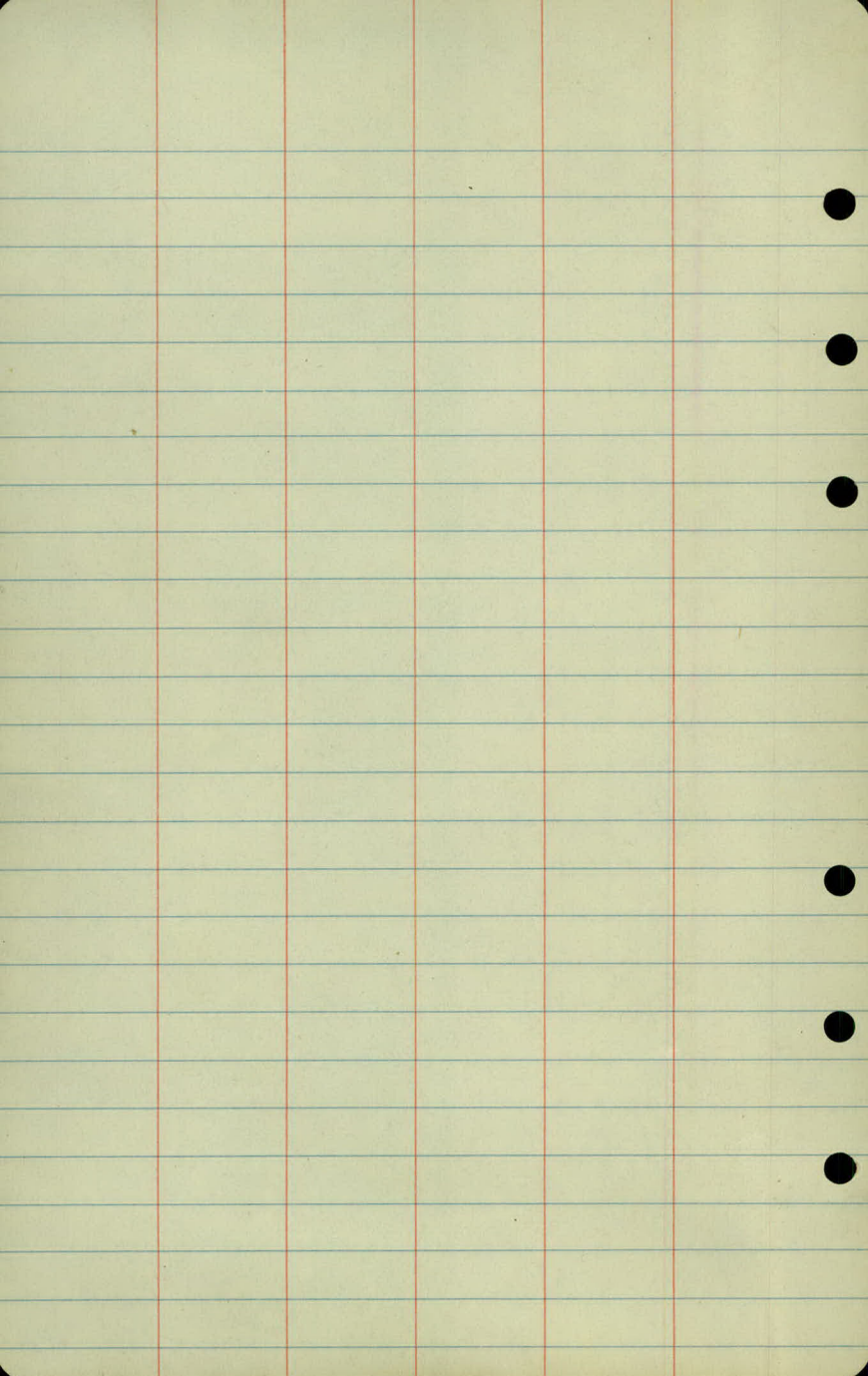
Angle.

Sta. Point Lt. Rt.

65+18.75 P.I. $90^{\circ}54'$

Reference Points

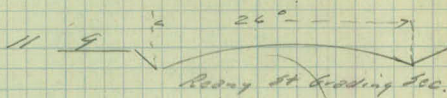




Artificial Topography

Back to
Limit
11 9

3



2

12 10

1

14 10

Rubble Gutter Section



0+00

Scattered Trees

+32 Approx of Heavy St.
+30 M.H. 30' Lt.

25' Spd.
37.00

+98 Rd 397 19°

+73 P.P. 21

+63 Approx of Alley

+52 = 15' x 24' C.M. 23'

170 P.P. 23

+57 End of No. 18°

+35 Rd. 394 22

+34 P.P. 23

0131 6th Basin to face 18°

+30 2

6" Conc Walk

Bl'd. +18 2

Conc.

0120 Hyd. 39°

25' Fr.
+84 On. 64°
10' Dist. Entr.
3458 = Combination
10' 4' 15" x 34' C.M. 22

3400 Fr. 26° 22'
Entr. to Lock Dr.
18' 6" 18°
32 10' 6" 83
N 1/2 S. Fr. Dr.
33 = Comb. 12' 4' 15"
x 68' C.M. 22°

1487 Fr. 31° 2'
1487 Rap from 30°

Back yard
Excav. in
Hillside

Black top Area
15' Story Stucco

155' Bl. 27° 34°
184' Bl. 27° 34°
25' 500
182
Pumps
18' x 24' C.M.

51' 11' 10°
10°
1/2 Rad.

+42 M.H. 24' 6" 24° Dr. in
+50 P.P. 26
+45 Rd. 394 21

59' 58"
53' 12"
9°
35'

Minnehaha St.

Note: Orig paving covered
with Blacktop.

+44' R. Radius 72' Lt.
134' Edge Paving 28' Lt.
+163 Edge Paving 4
+10' R. Radius 26' Lt.

Black 100
9 9

11

9 7

10

10 10

9

10 10

8

10 10

7

10 10

6

9 9

5

FC 35

+43 P.P. 22

FC 35

+05 P.P. 25

FC 35

+154 2

+67 P.P. 23

+39 P.P. 22

+03 P.P. 22

+94 Approx. Alley

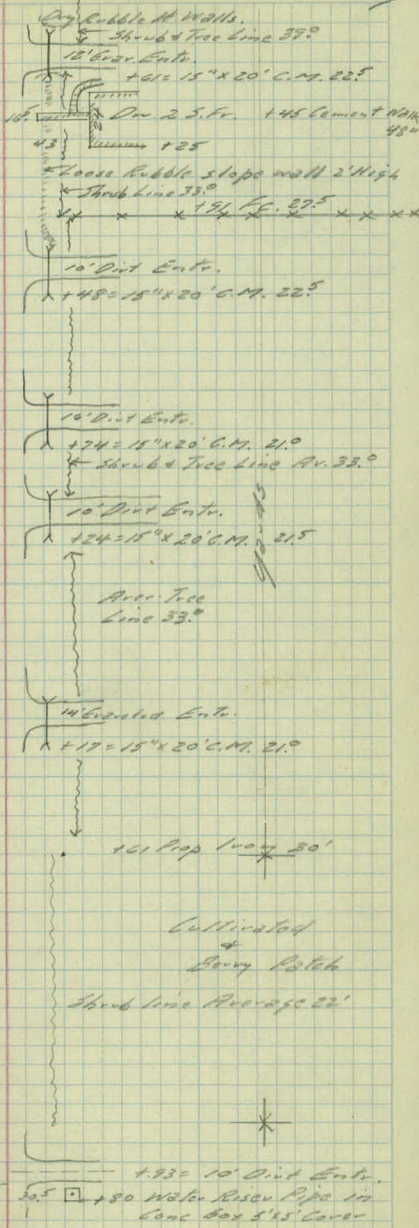
12' Dirt Entr.

+08 P.P. 20

Pasture

Cultivated

Scattered Trees & Bush



40-15

18

Backtop.
10 9

17

10 8

16

10 8

15

10 8

14

10 8

13

10 9

12

9 9

11

Ec. 34

Ec. 30°

1

+99PP.29

Ec. 34

Ec. 30°

+68PP.29

+139PP.29

Ec. 34

+10PP.28

Ec. 35

+154PP.29

End in Pasture

End in Cultivation

+13 Rd. 594.18

Dry Rubble Hood Walk. +24 Ec. 30°
Dirt Entr.

+08 = 15' x 20' c. r. 235

Tree Line 35'

Dry Rubble H. walls. +22 Ec. 28°
14' Dirt Entr.

+15 = 15' x 20' c. r. 32

155 = 2 Prop. Irons

27 28' 230'

Tree + Shrub Line @ 39°

yards

25

Blacktop.
12 7

24

9 7

23

8 9

22

7 9

21

8 10

+26

8 16

20

+50

12 11

19

10 9

18

+110 P.P. 29 -

FC 34 -

FC 30.

+41 Rd. 34m 14'

+46 Rd. 34m 15'

FC 34.

+83 P.P. 29 -

FC 30.

+55 P.P. 29 -

+24 = 18" x 66' C.M.

FC 35.

FC 34.

+35 P.P. 29.

+22 Hydrant 12"

+115 Edge Paving -

+885 Edge Paving -

+87 P.P. 34.

+855 Edge Paving -

+65 Fe. Cor. 36 -

+89 P.P. 29 -

+27 P.P. 30 -

+26 Bl. Top. +10 Rd. 34m 34'

+10 Fe. Cor. 35.0 -

20x12 Culvert 29'

15" x 62' Conc.

Conc. H. Rd. 12" x 4' x 6' Hi.

+41 End. Fe. 30.0 -

71.31'

Conc. Paved Hy.

Postline

Postline

Postline

Postline

Postline

Black Top.

25

27

9 11

26

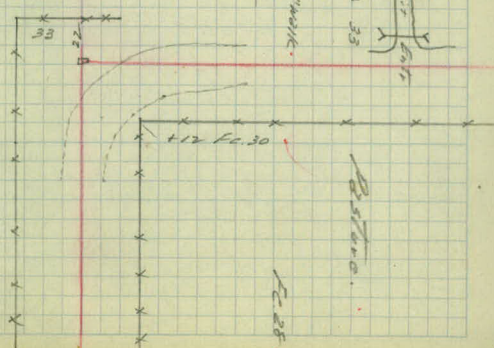
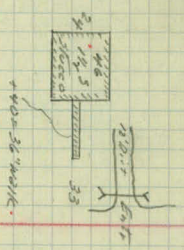
12 16

25

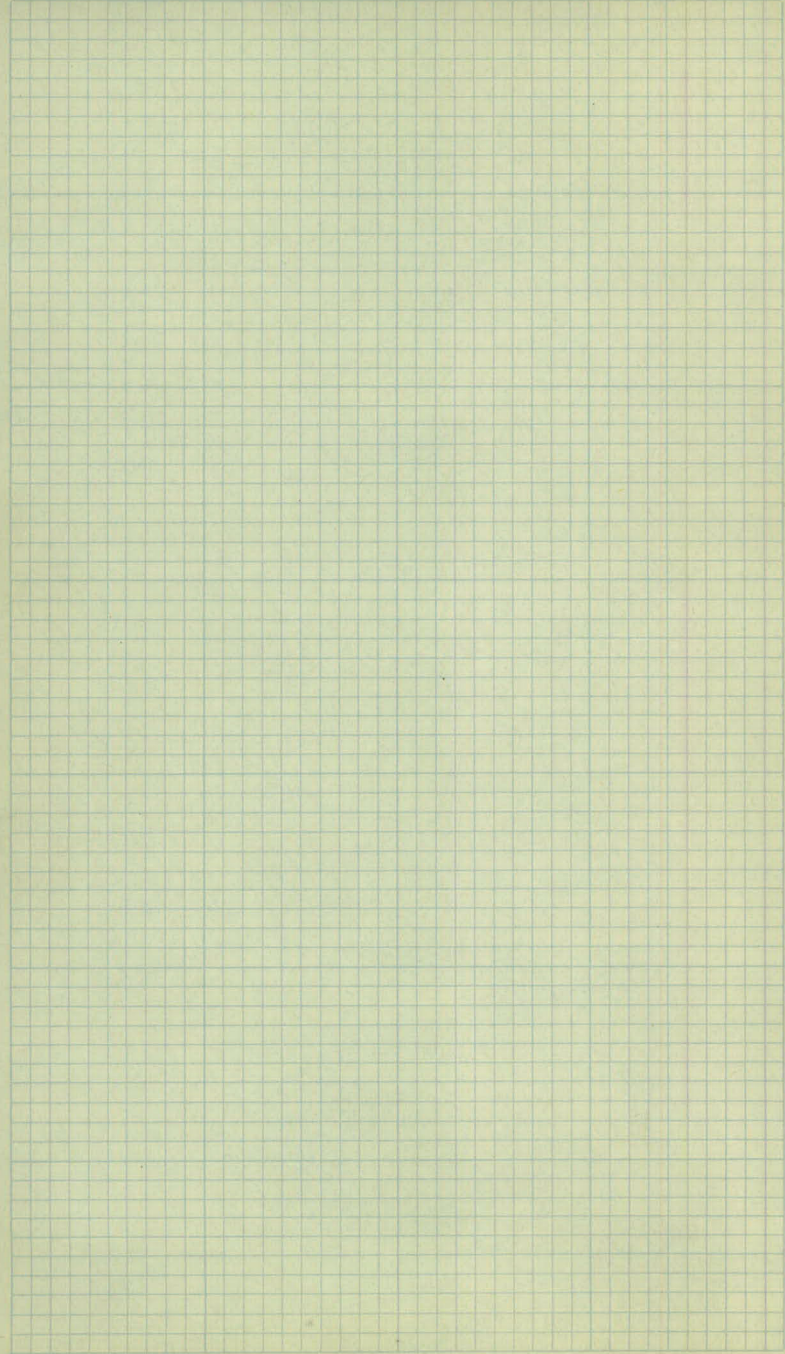
+ 87 = 12" x 20' C.M. 15.0
 + 61 = 8" Elm 26.
 + 30 = 6" 1/2 34.89
 + 30 Dm. 66.0

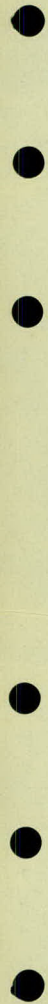
+ 81 = 6" Elm wood 27.
 27
 + 80 B.C. 42.0
 + 82 = 4" Elm 29.
 + 93 = 12" Oak 39.

+ 61 End. Fc. 21.0



+ 25 Bl. Top 41.24
 + 15 Bl. Top 28.24
 Fc. 34





33

Rd
10-9

32

Rd
9-10

31

Rd
9-10

30

Rd
10-9

29

Rd
10-9

28

Rd
10-9

+10 Ent -



Yards

+54 Garage 87'

+27 1/2" Oak 36' 37'

+00 House 79' 1500'

Fe 38'

+91 TP&PP 21'

+85 12" Oak 19'

Woods

Fe 39'

+21 TP&PP 21'

Fe 35'

Cultivated

+61 Rd Sign 14'

+51 TP&PP 22'

+15 Bay Woods 40'

Fe 38'

+25 End Berry Patch 29'

Fe 31'

Pasture

+00 Berry Patch 29'

Fe 29'

40

Rd
15-5

39

Rd
13-9

38

Rd
11-10

37

Rd
10-10

36

Rd
10-10

35

Rd
9-10

34

Rd
9-10

0.533"

17

Sea Handed Oaks
+ Stumps
150 Fc 16'

Fc 33'

+90 Bay Woods 35'

- +76 Prop Iron
- +63 T.P.P.P. 23'
- +44 12" Tree 31'
- +17 6" Tree 22'

- +52 6" Tree 30'
- +50 End E 30'
- +40 6" Tree 27'
- +24 10" Tree 23'

Woods

Fc 23'

Cultivated

- +48 Fc Cor 26' + End Yard
- +29 12" Tree 22'
- +18 15" Tree 40'

Yard

+60 End Woods
+50 Fc 43'

+24 X Drain
15' x 38' CM
18' RT

Fc 31'

- +79 15" Tree 40'
- +58 House 59'
- +48 T.P.P.P. 18'
- +38 Ent 12' x 18' CM 13'

1 1/2 Story
Frame
43'

- +27 End Row Trees 17'
- +15 Ent 12' x 16' CM 14'

- +90 15" Tree 24'
- +72 12" Tree 30'
- +61 Ent 12' x 6" CM 14'
- +51 House 28'

Small
Trees 17'

1 1/2 Story
Frame
34'

- +32 Bay Row 2" Trees 19'
- +28 T.P.P.P. 19'

Woods
+ Pasture

Fc 33'

Fc 43'

33.4" 0 +98 Prop Iron

Cultivated

+20 X Drain
15' x 38' CM - 18'

+08 Rd Sign 22'
Fc 41'

+59 T.P.P.P. 20'

+39 Ent 12' x 11' CM 14'

Woods

+29 End Yard + Row 2" Trees 29'

Fc 40'

47

Rel
14-7

46

Rel
13-7

45

Rel
12-7

44

Rel
11-8

43

Rel
10-8

42

Rel
10-8

41

Rel
10-7

+82 TRAPP 25' -

+27 10" Oak 38' -

+82 X Drain 30" X 36' CM -

+07 TP 24' -

+25 End Yard Beg Lowlands

+34 T.P. 25' -

+23 Ent 15" X 20' CM 17' -

+13 End Woods -

+64 Rd Sign 16'

+00 Beg Woods 33' -

+49 TP 25' -

+30 X Fc 25' -

Waste

Scattered Trees

Pasture

Fc 20' -

Fc 20' -

+70 Beg Marsh
End Woods

Fc 20' -

Fc 18' -

Fc 18' -

Fc 17' -

+40 End Woods
Fc 12' -

54

Rel
10-9

53

Rel
9-9

52

Rel
9-10

51

Rel
10-8

50

Rel
10-10

49

Rel
10-10

48

Rel
10-8

+68 T.P.P.P. 24'

+67 G. Pole 17'

+39 Ent 10 X 20.
G.M. 13'

+09 T.P.P.P. 25'

Cultivated

+84 X 17'

+32 T.P.P.P. 25'

Cultivated

Cultivated

+58 T.P.P.P. 25'

+80 Fe Cox 18'.
End Marsh.

XII XII
XII XII

Fe 23'

61

Rd
10-9

60

Rd
9-10

59

Rd
8-9

58

Rd
8-10

57

Rd
10-9

56

Rd
10-8

55

Rd
9-9

+69 TPIPP 22' -

Fc 24'

+98 Fc Cor.

Fc 23'.

+94 TPIPP 23'.

Fc 22'.

+92 Fc Cor 22'.

+50 Beg Marsh -

+44 TPIPP 25'.

+45 Ent.

Marsh / Brush

Marsh

19 19'

+73 XPrain.

36 x 36' C.M.

Marsh

Cultivated

Cultivated

65

718

Rd
30-11
Rd
19-7

64

Rd
6-12

63

Rd
7-8

62

Rd
10-8

Waste

+39 G.Pole 29'

+03 C.Pole 20'

+03 T.P.P.P 20'

+65 Emil Berry Patch -
 +35 Beg. Berry Patch 25'

Cultivated

Cultivated

+35 End Marsh -
 +35 T.P.P.P 21'

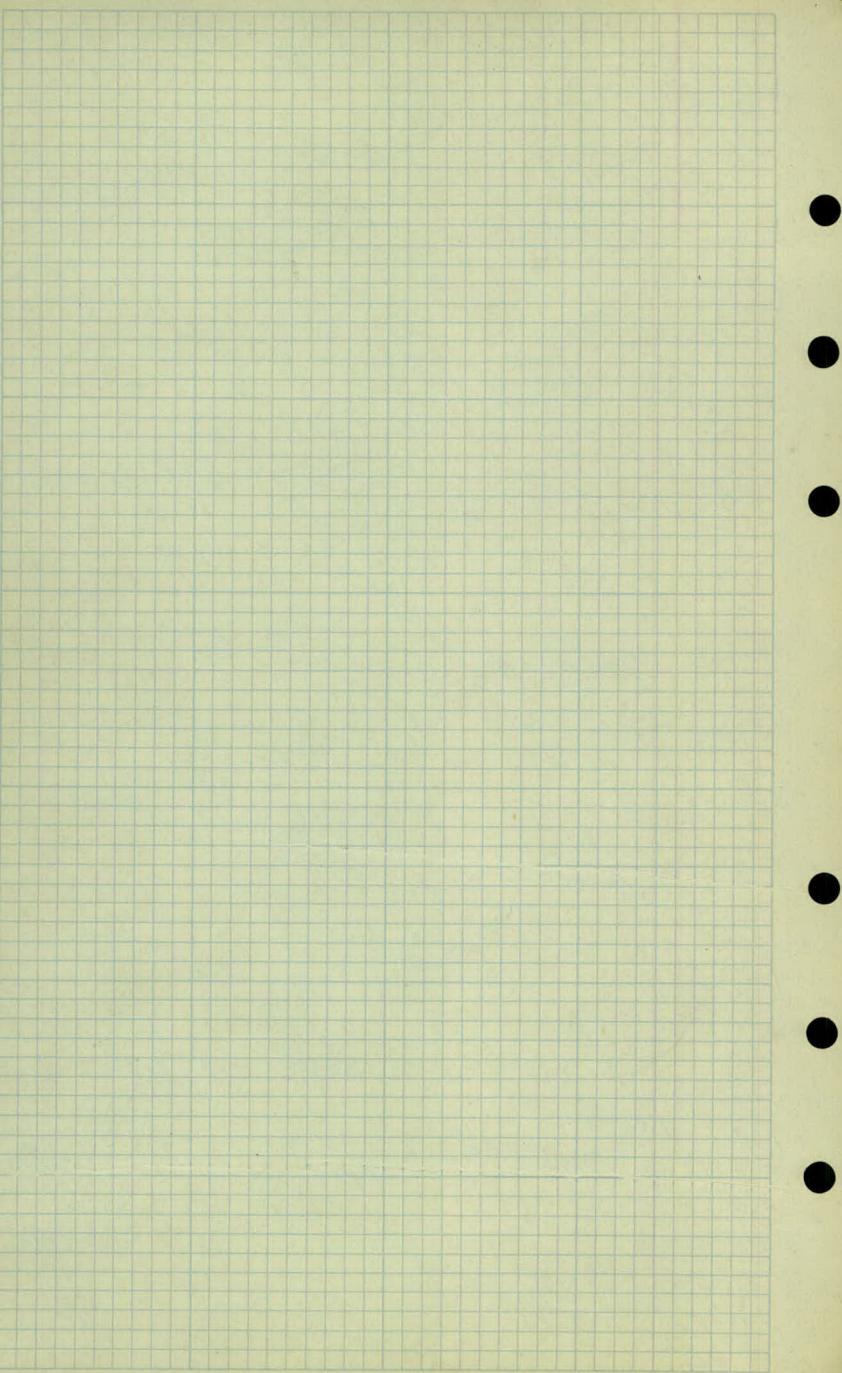
✓

x x x x x x x

Marsh & Brush

FC 22'

Cultivated



Bench Levels.

Sta.	+	-	-	Elev.
B.M.	9.25	1004.99		995.74
T.P.	1.65	1004.74	1.90	1003.09
B.M.	1.06	1004.74	1.06	1003.68
T.P.	1.00	998.27	13.47	991.27
T.P.	0.19	979.06	13.40	978.87
B.M.	10.85	976.41	13.50	965.56
B.M.	13.58	988.83	1.16	975.25
T.P.	10.69	999.46	0.06	988.77
T.P.	3.46	994.19	8.73	990.73
B.M.	3.58	994.19	3.58	990.61
T.P.	0.39	981.24	13.34	980.85
T.P.	0.16	967.77	13.63	967.61
T.P.	1.09	955.69	13.17	954.60
B.M.	3.94	955.69	3.94	951.75
T.P.	10.83	966.37	0.15	955.54
T.P.	17.84	978.13	0.08	966.29
T.P.	7.46	986.22	0.37	978.76
B.M.	7.78	986.22	7.78	978.44
T.P.	0.91	974.19	12.94	973.28
T.P.	0.68	961.64	13.17	961.04
B.M.			5.55	956.09

Description

Top of Hyd. N.W. Cor. East Ave. & Minnehaha St.

Top of Brick Ent. Step N.W. Cor. Rt. Sts. 10+45
Dwelling 4814

Top Hyd. N.W. Cor. Stillwater Canal & East Ave. 20+15

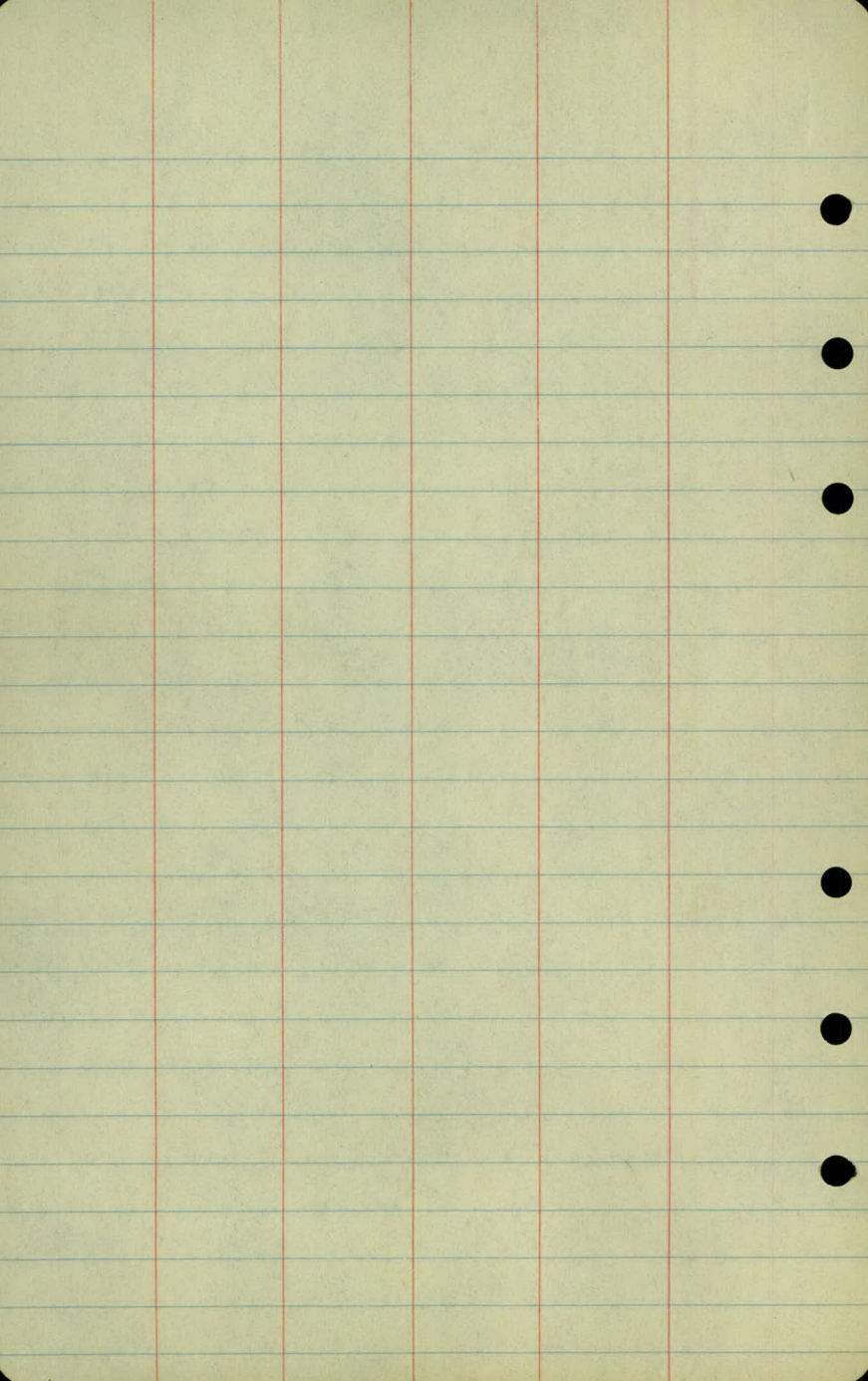
Top of Monument Sts. 26+40.85

Spike in 24" Oak 50' Rt. 37+95

Spike in 12" Oak 40' Lt. Sts. 47+30 ✓
↓

Spike in P.P. 30' Lt. Sts. 54+75

Spike in G.P. 20' Rt. Sts. 65+00



East Avenue

Cross Sections

12/38

Sta. + K - Elev.

B.M. 2.94 998.68 995.74

0+00

93.3

Lt.

Ct.

Rt.

Top of Hyd. M.W. Cor. East Ave. & Minnehaha

0+18 { Top of curb 40' Lt.

Black top at curb.

6.8

6.4

0+30 Top of walk & curb 19' Lt.

5.8

0+39 Catch basin Lt.

{ Top

5.44

{ Intake

6.55

{ Bottom

8.8

0+59 = Bottom rubble gutter Lt.

6.1

0+42 = M.H. Rt. { Elev grate top

5.2

{ Bottom of M.H.

10.9

0+58 Side culvert Rt.

{ So End

5.7

{ No End.

5.1

Oil pump platform Rt.

{ Top

3.5

{ Ground

3.4

floor fill etc. Rt 0+95

1.84

6.7
50

5.4

4.2
50

Sta.	+	π	-	Elev.
------	---	-------	---	-------

998.68

0+18				93.2
------	--	--	--	------

0+30				93.4
------	--	--	--	------

0+33				93.4
------	--	--	--	------

T.P.	6.93	1002.67	2.94	995.74
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0+63				94.3
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0+90				95.1
------	--	--	--	------

1+00				95.3
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+50				97.7
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+64	(Alley Lt.)			98.1
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+80				98.7
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T.P.	7.05	1006.76	2.96	999.71
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2				99.3
---	--	--	--	------

+33 Side Culvert Rt.

+50				1000.3
-----	--	--	--	--------

Lt.

E

Rt.

$$\begin{array}{ccccccc} & & 929 & & 922 & & \\ \frac{71}{30} & \frac{68}{40} & \frac{58}{16} & \frac{5.5}{\cancel{5.5}} & \frac{44}{36} & \frac{42}{50} & \end{array}$$

$$\frac{62}{50} \quad \frac{57}{27} \quad \frac{68}{19} \quad \frac{61}{19} \quad \frac{57}{11} \quad \frac{53}{\cancel{5.3}} \quad \frac{63}{11} \quad \frac{44}{38} \quad \frac{42}{50}$$

$$\frac{32}{50} \quad \frac{30}{53} \quad \frac{44}{32} \quad \frac{52}{28} \quad \frac{65}{20} \quad \frac{60}{14} \quad \frac{56}{9} \quad \frac{53}{\cancel{5.3}} \quad \frac{62}{15} \quad \frac{43}{45} \quad \frac{42}{50}$$

$$\frac{52}{51} \quad \frac{24}{30} \quad \frac{22}{19} \quad \frac{22}{20} \quad \frac{20}{17} \quad \frac{29}{13} \quad \frac{56}{8} \quad \frac{84}{\cancel{84}} \quad \frac{86}{11} \quad \frac{82}{20} \quad \frac{29}{38} \quad \frac{85}{50}$$

$$\frac{45}{50} \quad \frac{37}{30} \quad \frac{73}{27} \quad \frac{20}{22} \quad \frac{89}{19} \quad \frac{81}{16} \quad \frac{76}{7} \quad \frac{76}{\cancel{76}} \quad \frac{76}{5} \quad \frac{28}{10} \quad \frac{26}{16} \quad \frac{24}{21} \quad \frac{73}{39} \quad \frac{75}{50}$$

$$\frac{45}{50} \quad \frac{37}{30} \quad \frac{60}{28} \quad \frac{25}{23} \quad \frac{87}{18} \quad \frac{28}{16} \quad \frac{73}{9} \quad \frac{72}{\cancel{72}} \quad \frac{73}{7} \quad \frac{25}{9} \quad \frac{22}{16} \quad \frac{84}{18} \quad \frac{84}{19} \quad \frac{68}{21} \quad \frac{66}{31}$$

$$\frac{44}{50} \quad \frac{37}{28} \quad \frac{20}{24} \quad \frac{70}{20} \quad \frac{56}{16} \quad \frac{52}{8} \quad \frac{50}{\cancel{50}} \quad \frac{52}{6} \quad \frac{54}{9} \quad \frac{53}{13} \quad \frac{58}{19} \quad \frac{56}{22} \quad \frac{48}{46} \quad \frac{50}{50}$$

$$\frac{57}{50} \quad \frac{47}{30} \quad \frac{50}{18} \quad \frac{46}{6} \quad \frac{6}{\cancel{41}} \quad \frac{47}{6} \quad \frac{53}{14} \quad \frac{50}{14} \quad \frac{51}{17} \quad \frac{17}{19} \quad \frac{17}{22} \quad \frac{24}{28} \quad \frac{23}{37} \quad \frac{40}{40} \quad \frac{40}{50}$$

$$\frac{39}{50} \quad \frac{25}{28} \quad \frac{58}{24} \quad \frac{59}{18} \quad \frac{47}{15} \quad \frac{43}{8} \quad \frac{40}{\cancel{40}} \quad \frac{43}{7} \quad \frac{46}{10} \quad \frac{44}{14} \quad \frac{46}{19} \quad \frac{56}{21} \quad \frac{40}{31} \quad \frac{40}{50}$$

$$\frac{86}{50} \quad \frac{73}{30} \quad \frac{86}{24} \quad \frac{57}{19} \quad \frac{53}{15} \quad \frac{27}{7} \quad \frac{75}{\cancel{75}} \quad \frac{78}{5} \quad \frac{81}{10} \quad \frac{28}{15} \quad \frac{93}{21} \quad \frac{28}{26} \quad \frac{73}{28} \quad \frac{44}{30} \quad \frac{44}{50}$$

$$\frac{50 \text{ End.}}{92}$$

$$\frac{No. \text{ End.}}{80}$$

$$\frac{86}{50} \quad \frac{28}{29} \quad \frac{20}{26} \quad \frac{88}{18} \quad \frac{23}{15} \quad \frac{67}{6} \quad \frac{65}{\cancel{65}} \quad \frac{20}{9} \quad \frac{67}{14} \quad \frac{68}{16} \quad \frac{27}{18} \quad \frac{68}{23} \quad \frac{45}{28} \quad \frac{43}{50}$$

Sta. + - Elev.

1006.76

2+54 (Drive Rt) 01.2

3 01.4

3+06 01.5

+30 (2 Reedy St Lt) 01.9

+30 (M.H.) 30 Lt.

+46 Hydrant Lt.

02.1

+50

02.1

+60

+58 Side Culvert Rt.

02.2

+70

T.P. 3.12 1008.53 1.35 1005.41

4 02.4

+80 03.0

Lt.

E

Rt.

$\frac{45}{80}$	$\frac{56}{30}$	$\frac{68}{23}$	$\frac{65}{18}$	$\frac{60}{13}$	$\frac{56}{9}$	$\frac{58}{9}$	$\frac{54}{16}$	$\frac{43}{80}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	----------------	-----------------	-----------------

54

$\frac{73}{80}$	$\frac{59}{12}$	$\frac{55}{9}$	$\frac{53}{8}$	$\frac{55}{8}$	$\frac{54}{18}$	$\frac{72}{19}$	$\frac{69}{24}$	$\frac{53}{26}$	$\frac{47}{50}$
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$\frac{96}{100}$	$\frac{71}{80}$	$\frac{62}{33}$	$\frac{51}{10}$	$\frac{49}{8}$	$\frac{54}{8}$	$\frac{54}{15}$	$\frac{65}{18}$	$\frac{60}{25}$	$\frac{48}{28}$	$\frac{46}{50}$
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Top of Cover
5.3Road Surface
4.9Top
963Ground Surface
6.8

$\frac{74}{50}$	$\frac{68}{28}$	$\frac{52}{18}$	$\frac{59}{15}$	$\frac{49}{8}$	$\frac{47}{9}$	$\frac{52}{9}$	$\frac{50}{14}$	$\frac{67}{18}$	$\frac{67}{23}$	$\frac{45}{26}$	$\frac{34}{50}$
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$\frac{69}{50}$	$\frac{60}{34}$	$\frac{64}{23}$	$\frac{52}{12}$	$\frac{48}{7}$	$\frac{47}{9}$	$\frac{50}{9}$	$\frac{42}{21}$	$\frac{20}{50}$	Also Grade of Ent. Rt.
-----------------	-----------------	-----------------	-----------------	----------------	----------------	----------------	-----------------	-----------------	---------------------------

No End
7.5No End
6.5

$\frac{24}{50}$	$\frac{17}{31}$	$\frac{40}{34}$	$\frac{60}{26}$	$\frac{64}{19}$	$\frac{50}{16}$	$\frac{47}{6}$	$\frac{46}{10}$	$\frac{48}{29}$	$\frac{38}{50}$
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$\frac{38}{50}$	$\frac{27}{33}$	$\frac{79}{26}$	$\frac{80}{19}$	$\frac{65}{15}$	$\frac{64}{8}$	$\frac{61}{14}$	$\frac{64}{14}$	$\frac{80}{17}$	$\frac{78}{24}$	$\frac{50}{27}$	$\frac{42}{50}$
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$\frac{36}{50}$	$\frac{32}{31}$	$\frac{76}{21}$	$\frac{75}{18}$	$\frac{62}{14}$	$\frac{61}{8}$	$\frac{59}{13}$	$\frac{74}{18}$	$\frac{69}{22}$	$\frac{44}{28}$	$\frac{37}{37}$	$\frac{42}{40}$	$\frac{34}{50}$
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Sta. + K - Elev.

1008.53

4+80

4+94

03.4

4+93

5

03.5

+43

03.6

+73

03.6

6

03.5

+50

02.3

7

02.9

+17 C.M. Side drain

T.P. 2.54 1007.10 3.97 1004.56

+50

02.6

24.

2

Rt.

Top of water riser corer Rt 31

$\frac{37}{50}$ $\frac{40}{35}$ $\frac{54}{13}$ 51 Alley Lt.

Entr. Rt.

51 $\frac{54}{10}$ $\frac{41}{29}$ $\frac{40}{50}$

$\frac{24}{50}$ $\frac{22}{34}$ $\frac{74}{26}$ $\frac{76}{20}$ $\frac{56}{15}$ $\frac{52}{8}$ 50 $\frac{55}{11}$ $\frac{45}{24}$ $\frac{46}{37}$ $\frac{42}{50}$

$\frac{41}{50}$ $\frac{46}{28}$ $\frac{76}{25}$ $\frac{73}{18}$ $\frac{53}{14}$ 49 $\frac{55}{14}$ $\frac{66}{17}$ $\frac{61}{30}$ $\frac{45}{50}$

$\frac{66}{50}$ $\frac{63}{37}$ $\frac{69}{26}$ $\frac{77}{24}$ $\frac{79}{19}$ $\frac{53}{15}$ 49 $\frac{56}{14}$ $\frac{67}{18}$ $\frac{62}{19}$ $\frac{48}{50}$

$\frac{69}{50}$ $\frac{68}{28}$ $\frac{78}{25}$ $\frac{79}{20}$ $\frac{57}{15}$ 50 $\frac{56}{14}$ $\frac{66}{17}$ $\frac{59}{21}$ $\frac{47}{50}$

$\frac{66}{50}$ $\frac{63}{27}$ $\frac{78}{26}$ $\frac{78}{19}$ $\frac{57}{14}$ 57 $\frac{57}{14}$ $\frac{68}{18}$ $\frac{61}{22}$ $\frac{52}{26}$ $\frac{37}{40}$ $\frac{35}{50}$

$\frac{26}{50}$ $\frac{65}{41}$ $\frac{59}{29}$ $\frac{83}{25}$ $\frac{82}{19}$ $\frac{58}{14}$ 56 $\frac{60}{10}$ $\frac{59}{15}$ $\frac{73}{19}$ $\frac{73}{23}$ $\frac{43}{28}$ $\frac{37}{50}$

50 End
725

No End
815

Sec Two Entr. Rt.

57 $\frac{60}{10}$ $\frac{50}{34}$ $\frac{44}{50}$

$\frac{59}{50}$ $\frac{46}{30}$ $\frac{66}{27}$ $\frac{69}{19}$ $\frac{48}{14}$ $\frac{48}{11}$ 45 $\frac{48}{14}$ $\frac{61}{18}$ $\frac{63}{24}$ $\frac{43}{27}$ $\frac{33}{50}$

Sta. + π - Elev.

1007.10

8

02.4

+24 Side drain Rt.

Sec. Thru Entr.

+50

02.3

+74 Side drain Rt.

Sec. Thru Entr.

9

01.9

+48

01.4

+48 Side Drain Rt.

Sec. Thru Entr.

10

00.5

+60

19.8

B.M. 3.42 1007.10 3.42 1003.68

T.P. 1.97 1002.28 6.79 1000.31

Lt.

E

Rt.

41 39 42 70 70 50 47 51 48 65 64 47 43
50 44 31 27 19 14 11 15 19 25 26 50

So End
68

No End
69

47 51 44 37
11 45 50

40 40 47 72 72 51 52 48 53 50 68 67 48 43
50 44 30 26 20 18 11 11 18 18 24 29 50

So End
70

No End
71

50 54 50 44 45
11 27 37 50

51 54 53 48 73 73 56 55 52 55 53 71 68 46 37
50 46 36 31 27 19 18 10 10 16 16 19 24 28 50

91 80 73 84 83 63 62 57 61 58 95 75 57 48
50 24 29 26 19 16 11 11 10 14 78 24 28 50

So End
79

No End
80

59 80 63 56
12 20

103 93 87 84 80 72 66 21 74 81 81 56 62
50 22 29 24 19 16 10 16 19 23 26 50

105 96 88 90 89 88 76 78 73 75 74 84 83 63 56 56
50 26 26 24 20 14 10 11 10 16 21 24 26 43 50

Top of Brick wall at Entrance dwelling #812
N.W. Cor.

Sta. + x - Elev.

1002.28

+61 Side culvert Rt.

Sec thru Eutr.

11 98.9

+39 Side culvert Rt.

Sec thru Eutr.

+60 97.2

12 95.8

+50 94.0

13 91.4

+09 Side culvert Rt.

Sec thru Eutr.

T.P. 1.07 990.34 13.01 989.27

+50 98.4

14 97.3

+50 850

Lt.

E

Et.

So. End

44

No. End

51

28	26	13	07
8	21	50	

53	48	49	67	60	41	40	34	38	41	48	18	12
63	34	30	25	23	19	15	10	10	17	21	28	50
50												

So. End

60

No. End

67

48	50	30	24
7	37	50	

75	59	52	51	70	74	58	51	54	60	67	30	26
50	38	31	25	24	18	15	7	7	17	22	28	50

84	66	62	86	87	68	70	67	65	70	74	74	80	81	40	37
50	33	25	23	19	15	9	8	9	13	17	20	23	29	50	

75	80	73	107	105	87	88	83	87	87	98	58	55	53
50	34	27	23	19	16	10	10	17	17	19	23	29	50

108	104	107	130	121	113	104	106	108	115	115	78	66
50	34	26	22	18	15	10	11	17	22	24	28	50

So. End

130

No. End

139

114	116	108	104	94
10	15	30	50	

23	21	14	24	23	17	13	9	12	14	24	24	105	112
20	20	25	22	19	16	11	0	8	17	20	25	27	50

48	42	36	61	63	37	37	30	35	36	48	48	14	12	17
50	35	22	24	18	16	10	5	8	16	20	23	25	26	50

62	54	50	80	82	53	58	54	60	70	71	48	49	50
50	33	25	22	18	15	10	5	11	18	24	27	36	50

Sta + K - Elev.

990.34

15

82.6

+50

80.3

T.P.

1.12

980.47

10.99

979.35

+80

78.7

16

78.0

+50

76.0

17

74.2

+50

72.0

18

69.9

T.P.

225

968.94

13.78

966.69

+50

67.9

19

66.5

+50

65.0

+64

64.7

Lt.

E

Et.

$\frac{75}{50}$	$\frac{68}{33}$	$\frac{64}{27}$	$\frac{56}{24}$	$\frac{95}{18}$	$\frac{85}{15}$	$\frac{81}{10}$	$\frac{77}{1}$	$\frac{82}{9}$	$\frac{84}{16}$	$\frac{94}{19}$	$\frac{95}{23}$	$\frac{84}{26}$	$\frac{56}{88}$	$\frac{58}{33}$	$\frac{73}{50}$
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$\frac{102}{50}$	$\frac{100}{35}$	$\frac{53}{26}$	$\frac{121}{23}$	$\frac{121}{20}$	$\frac{105}{16}$	$\frac{104}{11}$	$\frac{100}{10}$	$\frac{105}{8}$	$\frac{105}{16}$	$\frac{116}{19}$	$\frac{121}{24}$	$\frac{105}{27}$	$\frac{116}{34}$	$\frac{126}{50}$
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$\frac{30}{50}$	$\frac{36}{38}$	$\frac{38}{34}$	$\frac{33}{26}$	$\frac{40}{25}$	$\frac{40}{22}$	$\frac{19}{17}$	$\frac{22}{11}$	$\frac{16}{1}$	$\frac{20}{8}$	$\frac{21}{16}$	$\frac{51}{20}$	$\frac{55}{30}$	$\frac{58}{50}$
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$\frac{51}{50}$	$\frac{52}{35}$	$\frac{54}{28}$	$\frac{57}{23}$	$\frac{56}{21}$	$\frac{30}{17}$	$\frac{30}{10}$	$\frac{35}{1}$	$\frac{30}{8}$	$\frac{31}{16}$	$\frac{59}{22}$	$\frac{63}{30}$	$\frac{68}{50}$
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$\frac{76}{50}$	$\frac{73}{35}$	$\frac{70}{30}$	$\frac{70}{25}$	$\frac{65}{19}$	$\frac{20}{15}$	$\frac{20}{11}$	$\frac{45}{1}$	$\frac{48}{7}$	$\frac{50}{16}$	$\frac{77}{23}$	$\frac{76}{26}$	$\frac{72}{30}$	$\frac{65}{43}$	$\frac{58}{50}$
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$\frac{85}{50}$	$\frac{83}{35}$	$\frac{78}{29}$	$\frac{83}{19}$	$\frac{110}{14}$	$\frac{66}{9}$	$\frac{63}{1}$	$\frac{67}{8}$	$\frac{72}{15}$	$\frac{91}{19}$	$\frac{91}{22}$	$\frac{66}{26}$	$\frac{68}{39}$	$\frac{67}{50}$
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$\frac{87}{50}$	$\frac{84}{34}$	$\frac{82}{27}$	$\frac{108}{24}$	$\frac{108}{19}$	$\frac{92}{15}$	$\frac{90}{10}$	$\frac{85}{1}$	$\frac{88}{8}$	$\frac{91}{15}$	$\frac{108}{19}$	$\frac{113}{23}$	$\frac{74}{27}$	$\frac{75}{33}$	$\frac{83}{50}$
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$\frac{88}{50}$	$\frac{85}{36}$	$\frac{81}{30}$	$\frac{132}{24}$	$\frac{130}{20}$	$\frac{112}{14}$	$\frac{110}{10}$	$\frac{106}{1}$	$\frac{109}{8}$	$\frac{112}{16}$	$\frac{129}{18}$	$\frac{130}{25}$	$\frac{86}{29}$	$\frac{94}{34}$	$\frac{104}{50}$
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$\frac{+14}{50}$	$\frac{+14}{30}$	$\frac{30}{25}$	$\frac{30}{20}$	$\frac{17}{15}$	$\frac{10}{1}$	$\frac{13}{10}$	$\frac{12}{15}$	$\frac{28}{15}$	$\frac{28}{24}$	$\frac{13}{27}$	$\frac{25}{34}$	$\frac{32}{50}$
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$\frac{32}{30}$	$\frac{40}{38}$	$\frac{37}{28}$	$\frac{45}{24}$	$\frac{44}{18}$	$\frac{35}{16}$	$\frac{28}{14}$	$\frac{24}{1}$	$\frac{26}{13}$	$\frac{48}{19}$	$\frac{56}{29}$	$\frac{58}{50}$
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$\frac{57}{30}$	$\frac{12}{35}$	$\frac{60}{24}$	$\frac{58}{18}$	$\frac{117}{10}$	$\frac{39}{1}$	$\frac{38}{15}$	$\frac{71}{24}$	$\frac{78}{28}$	$\frac{61}{30}$	$\frac{84}{35}$	$\frac{84}{37}$	$\frac{74}{38}$	$\frac{65}{39}$	$\frac{50}{50}$
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$\frac{54}{50}$	$\frac{58}{44}$	$\frac{67}{37}$	$\frac{62}{20}$	$\frac{50}{16}$	$\frac{51}{13}$	$\frac{42}{1}$	$\frac{40}{18}$	$\frac{36}{21}$	$\frac{38}{26}$	$\frac{52}{33}$	$\frac{43}{40}$	$\frac{40}{50}$
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Sta.	+	X	-	Elev.
		768.94		
19+55		Culvert Rt.		
				63.7
+85		Edge Pavement		
+88.5		E Paving		63.89
20+11.5		Edge Paving		63.6
B.M.	3.38	768.94	3.38	765.56
+31				63.4
+50				62.5
+75				63.8
21				64.2
+24		C.M X-Culvert		
+38				64.8
+70				65.5
22				66.5

LT

E

RT

So. End

No. End.

9.1
77 73 57 56
50 33 27 21 5.0

E Br 11.1
32
50

E Br
64 6.0 5.05 4.2 Edge Br 36
50 33 30 38 50
43

E Bring
66 62 5.3 51 67 71 54 45
50 36 21 25 34 37 50

Top of Hydrant N.W. Cor Stillwater Ave. + East Ave.

5/2 20+15
E Br Edge Br 64 68 59 55 51 57 96 96 78 71 54 53
76 70 40 26 8 15 21 30 31 33 38 45 50
82 50

103 127 122 91 66 58 51 56 97 97 85 62 59
50 44 34 25 18 7 14 19 28 30 33 43 50

154 140 70 58 51 55 10.4 10.6 87
50 34 18 14 16 25 35 50

160 155 62 52 4.7 52 11.0 11.2 11.4 10.4 10.1
50 35 16 8 13 24 32 34 44 50

120 120
16 13.5

162 156 55 46 41 45 48 10.6 11.2 54
50 33 14 8 11 16 27 34 50

168 145 51 40 34 38 48 8.4 8.6 7.5 5.3
50 34 15 9 11 17 25 30 35 50

161 130 34 28 24 27 34 6.9 6.8 3.7 1.0
50 32 16 9 11 16 22 25 34 50

Sta. + K - Elev.

968.94

T.P. 7.02 973.56 2.40 966.54

22+35 68.0

+73 69.3

23 70.1

+27 70.9

+60 71.9

24 73.2

T.P. 7.83 980.55 0.44 973.12

24

+50 74.9

25 75.9

+50 75.9

26 76.1

B.M. 5.69 980.94 5.70 975.25

Lt.

E

Rt.

$\frac{178}{50}$	$\frac{168}{33}$	$\frac{20}{18}$	$\frac{63}{14}$	$\frac{56}{10}$	$\frac{62}{10}$	$\frac{62}{15}$	$\frac{57}{20}$	$\frac{87}{22}$	$\frac{71}{28}$	$\frac{33}{31}$	$\frac{24}{38}$	$\frac{12}{50}$
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$\frac{180}{50}$	$\frac{157}{34}$	$\frac{57}{17}$	$\frac{47}{12}$	$\frac{43}{14}$	$\frac{51}{20}$	$\frac{70}{26}$	$\frac{63}{30}$	$\frac{23}{50}$
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$\frac{184}{50}$	$\frac{123}{42}$	$\frac{140}{29}$	$\frac{45}{16}$	$\frac{35}{9}$	$\frac{40}{15}$	$\frac{43}{21}$	$\frac{72}{24}$	$\frac{74}{27}$	$\frac{55}{50}$	$\frac{34}{50}$
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$\frac{163}{50}$	$\frac{136}{33}$	$\frac{38}{12}$	$\frac{27}{15}$	$\frac{31}{20}$	$\frac{60}{29}$	$\frac{68}{50}$
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$\frac{124}{50}$	$\frac{108}{37}$	$\frac{83}{27}$	$\frac{29}{16}$	$\frac{17}{15}$	$\frac{20}{21}$	$\frac{50}{24}$	$\frac{50}{27}$	$\frac{31}{50}$
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$\frac{78}{50}$	$\frac{51}{26}$	$\frac{52}{21}$	$\frac{10}{15}$	$\frac{0.9}{10}$	$\frac{0.4}{10}$
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$\frac{7.8}{9}$	$\frac{7.5}{14}$	$\frac{7.6}{19}$	$\frac{7.5}{23}$	$\frac{6.7}{28}$	$\frac{6.4}{34}$	$\frac{5.3}{50}$
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$\frac{100}{50}$	$\frac{80}{43}$	$\frac{85}{34}$	$\frac{80}{26}$	$\frac{94}{25}$	$\frac{50}{18}$	$\frac{67}{14}$	$\frac{61}{9}$	$\frac{62}{15}$	$\frac{61}{20}$	$\frac{81}{24}$	$\frac{77}{29}$	$\frac{36}{38}$	$\frac{38}{50}$
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$\frac{60}{50}$	$\frac{50}{34}$	$\frac{44}{26}$	$\frac{67}{25}$	$\frac{77}{19}$	$\frac{59}{15}$	$\frac{5.6}{11}$	$\frac{51}{14}$	$\frac{52}{8}$	$\frac{52}{14}$	$\frac{70}{20}$	$\frac{63}{26}$	$\frac{30}{29}$	$\frac{2.6}{50}$
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$\frac{54}{50}$	$\frac{47}{34}$	$\frac{41}{26}$	$\frac{66}{23}$	$\frac{66}{20}$	$\frac{54}{16}$	$\frac{51}{14}$	$\frac{50}{19}$	$\frac{68}{23}$	$\frac{68}{28}$	$\frac{37}{50}$
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$\frac{7.3}{50}$	$\frac{67}{44}$	$\frac{64}{34}$	$\frac{60}{25}$	$\frac{68}{23}$	$\frac{69}{19}$	$\frac{53}{15}$	$\frac{49}{17}$	$\frac{58}{17}$	$\frac{63}{20}$	$\frac{63}{26}$	$\frac{58}{28}$	$\frac{57}{50}$
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Top of Monument Sta. 26+40.85

Sta + K - Elev.

980.94

26+40.85

75.9

26+40.85

75.7

T.P. 8.61 983.86 5.69 975.25

27 74.6

+50

72.5

+66

Ent. Lt Culvert

78.2

28

78.9

+50

79.8

29

80.7

+35

81.7

+65

83.2

30

T.P. 12.30 995.58 0.58 983.28

T.P. 8.15 995.58 8.15 987.43

Lt.

E

Rt.

$$\begin{array}{r} 83 \ 6.9 \\ 50 \ 34 \ 25 \end{array} \quad \begin{array}{r} 6.2 \\ 23 \end{array} \quad \begin{array}{r} 7.2 \\ 19 \end{array} \quad \begin{array}{r} 7.0 \\ 14 \end{array} \quad \begin{array}{r} 5.2 \\ 14 \end{array} \quad \begin{array}{r} 5.2 \\ 29 \end{array} \quad \begin{array}{r} 4.5 \\ 29 \end{array} \quad \begin{array}{r} 4.4 \\ 50 \end{array}$$

$$\begin{array}{r} 6.7 \\ 50 \end{array} \quad \begin{array}{r} 5.8 \\ 23 \end{array} \quad \begin{array}{r} 5.4 \\ 16 \end{array} \quad \begin{array}{r} 5.2 \\ 22 \end{array} \quad \begin{array}{r} 5.0 \\ 22 \end{array} \quad \begin{array}{r} 4.9 \\ 50 \end{array}$$

$$\begin{array}{r} 9.4 \\ 50 \end{array} \quad \begin{array}{r} 7.2 \\ 18 \end{array} \quad \begin{array}{r} 7.1 \\ 11 \end{array} \quad 7.3 \quad \begin{array}{r} 7.9 \\ 11 \end{array} \quad \begin{array}{r} 8.1 \\ 13 \end{array} \quad \begin{array}{r} 8.7 \\ 16 \end{array} \quad \begin{array}{r} 8.9 \\ 29 \end{array} \quad \begin{array}{r} 8.3 \\ 50 \end{array}$$

$$\begin{array}{r} 7.8 \\ 50 \end{array} \quad \begin{array}{r} 7.4 \\ 20 \end{array} \quad \begin{array}{r} 7.8 \\ 18 \end{array} \quad \begin{array}{r} 7.7 \\ 15 \end{array} \quad \begin{array}{r} 6.5 \\ 11 \end{array} \quad 6.4 \quad \begin{array}{r} 6.7 \\ 11 \end{array} \quad \begin{array}{r} 7.5 \\ 13 \end{array} \quad \begin{array}{r} 7.7 \\ 29 \end{array} \quad \begin{array}{r} 6.8 \\ 50 \end{array}$$

$$\begin{array}{r} 7.4 \\ 50 \end{array} \quad \begin{array}{r} 7.0 \\ 18 \end{array} \quad \begin{array}{r} 6.3 \\ 11 \end{array} \quad 8.0 \quad 6.2 \text{ West End} \quad \begin{array}{r} 7.7 \\ \text{East End} \end{array}$$

$$\begin{array}{r} 6.4 \\ 50 \end{array} \quad \begin{array}{r} 6.1 \\ 29 \end{array} \quad \begin{array}{r} 6.7 \\ 15 \end{array} \quad \begin{array}{r} 5.9 \\ 11 \end{array} \quad 5.7 \quad \begin{array}{r} 6.1 \\ 9 \end{array} \quad \begin{array}{r} 6.7 \\ 13 \end{array} \quad \begin{array}{r} 6.6 \\ 29 \end{array} \quad \begin{array}{r} 6.2 \\ 50 \end{array}$$

$$\begin{array}{r} 4.9 \\ 50 \end{array} \quad \begin{array}{r} 4.7 \\ 24 \end{array} \quad \begin{array}{r} 6.3 \\ 16 \end{array} \quad \begin{array}{r} 5.7 \\ 14 \end{array} \quad \begin{array}{r} 5.3 \\ 11 \end{array} \quad 5.0 \quad \begin{array}{r} 5.3 \\ 10 \end{array} \quad \begin{array}{r} 6.1 \\ 14 \end{array} \quad \begin{array}{r} 5.0 \\ 16 \end{array} \quad \begin{array}{r} 5.4 \\ 20 \end{array} \quad \begin{array}{r} 5.4 \\ 32 \end{array} \quad \begin{array}{r} 5.0 \\ 50 \end{array}$$

$$\begin{array}{r} 4.3 \\ 50 \end{array} \quad \begin{array}{r} 4.5 \\ 23 \end{array} \quad \begin{array}{r} 5.8 \\ 18 \end{array} \quad \begin{array}{r} 5.8 \\ 16 \end{array} \quad \begin{array}{r} 4.7 \\ 13 \end{array} \quad \begin{array}{r} 4.4 \\ 10 \end{array} \quad 4.1 \quad \begin{array}{r} 4.4 \\ 10 \end{array} \quad \begin{array}{r} 4.5 \\ 12 \end{array} \quad \begin{array}{r} 6.1 \\ 14 \end{array} \quad \begin{array}{r} 4.9 \\ 17 \end{array} \quad \begin{array}{r} 5.3 \\ 22 \end{array} \quad \begin{array}{r} 6.0 \\ 31 \end{array} \quad \begin{array}{r} 4.3 \\ 50 \end{array}$$

$$\begin{array}{r} 5.2 \\ 50 \end{array} \quad \begin{array}{r} 5.6 \\ 25 \end{array} \quad \begin{array}{r} 6.1 \\ 23 \end{array} \quad \begin{array}{r} 5.7 \\ 18 \end{array} \quad \begin{array}{r} 3.8 \\ 13 \end{array} \quad 3.2 \quad \begin{array}{r} 3.4 \\ 10 \end{array} \quad \begin{array}{r} 6.3 \\ 16 \end{array} \quad \begin{array}{r} 6.7 \\ 21 \end{array} \quad \begin{array}{r} 6.3 \\ 28 \end{array} \quad \begin{array}{r} 5.9 \\ 40 \end{array} \quad \begin{array}{r} 5.5 \\ 50 \end{array}$$

$$\begin{array}{r} 4.9 \\ 50 \end{array} \quad \begin{array}{r} 5.4 \\ 24 \end{array} \quad \begin{array}{r} 5.6 \\ 18 \end{array} \quad \begin{array}{r} 2.7 \\ 12 \end{array} \quad \begin{array}{r} 2.2 \\ 6 \end{array} \quad 2.2 \quad \begin{array}{r} 2.5 \\ 10 \end{array} \quad \begin{array}{r} 5.8 \\ 16 \end{array} \quad \begin{array}{r} 6.0 \\ 20 \end{array} \quad \begin{array}{r} 5.1 \\ 27 \end{array} \quad \begin{array}{r} 5.3 \\ 34 \end{array} \quad \begin{array}{r} 5.0 \\ 50 \end{array}$$

$$\begin{array}{r} 3.8 \\ 50 \end{array} \quad \begin{array}{r} 4.4 \\ 18 \end{array} \quad \begin{array}{r} 1.3 \\ 12 \end{array} \quad 0.7 \quad \begin{array}{r} 1.2 \\ 11 \end{array} \quad \begin{array}{r} 2.8 \\ 16 \end{array} \quad \begin{array}{r} 3.1 \\ 30 \end{array} \quad \begin{array}{r} 3.8 \\ 35 \end{array} \quad \begin{array}{r} 5.1 \\ 50 \end{array}$$

P.P. 25' Lt Stn 33+25

Sta. + T - Elev.

995.58

30+50

85.4

31

87.9

+40

89.9

+70

90.9

T.P.

10.20

1002.85

2.93

992.65

3v

92.0

+25

92.7

+50

93.3

33

94.4

+47

95.0

+61

See the End Lt.

+80

95.0

34

94.8

Lt.

E

Rt.

$$\begin{array}{cccccccccccc} 116 & 117 & 124 & 120 & 105 & 102 & 107 & 126 & 128 & 138 \\ 50 & 44 & 23 & 14 & 10 & 11 & 16 & 34 & 20 \end{array}$$

$$\begin{array}{cccc} 109 & 104 & 93 & 81 \\ 50 & 23 & 15 & 11 \end{array}$$

$$\begin{array}{cccccccc} 77 & 83 & 87 & 87 & 86 & 81 & 81 \\ 10 & 13 & 31 & 37 & 44 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 53 & 70 & 65 & 66 & 68 & 57 & 62 & 65 & 36 & 46 & 50 & 51 \\ 50 & 21 & 18 & 15 & 13 & 9 & 14 & 18 & 29 & 36 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 62 & 49 & 22 & 60 & 60 & 54 & 48 & 47 & 51 & 53 & 09 & 07 & 14 \\ 50 & 24 & 18 & 15 & 14 & 13 & 5 & 10 & 13 & 19 & 36 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 111 & 108 & 103 & 102 & 117 & 109 & 111 & 114 & 116 & 102 & 77 & 75 & 75 \\ 50 & 31 & 19 & 14 & 11 & 6 & 10 & 14 & 17 & 19 & 37 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 104 & 59 & 80 & 115 & 115 & 108 & 102 & 107 & 98 & 58 & 57 & 46 \\ 50 & 34 & 24 & 18 & 14 & 11 & 11 & 16 & 21 & 38 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 94 & 81 & 77 & 110 & 110 & 101 & 96 & 100 & 87 & 38 & 41 & 36 \\ 50 & 27 & 18 & 14 & 13 & 10 & 11 & 16 & 22 & 38 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 56 & 61 & 57 & 97 & 91 & 85 & 88 & 90 & 95 & 85 & 55 & 48 & 41 \\ 50 & 18 & 14 & 14 & 10 & 9 & 14 & 13 & 15 & 19 & 39 & 50 \end{array}$$

$$\begin{array}{cccc} 52 & 38 & 78 & 80 \\ 50 & 20 & 15 & 17 \end{array}$$

$$\begin{array}{cccccccc} 79 & 83 & 87 & 87 & 54 & 64 & 68 \\ 10 & 12 & 14 & 18 & 39 & 50 \end{array}$$

$$\begin{array}{cccc} 65 & 66 & 78 & 78 \\ 50 & 45 & 10 & 10 \end{array}$$

$$\begin{array}{cccccccc} 54 & 40 & 35 & 84 & 83 & 79 & 93 & 84 \\ 50 & 32 & 20 & 13 & 10 & 10 & 13 & 14 \end{array}$$

$$\begin{array}{cccc} 52 & 44 & 43 & 87 & 84 \\ 50 & 35 & 19 & 13 & 8 \end{array}$$

$$\begin{array}{cccc} 81 & 84 & 86 & 51 & 57 & 57 \\ 10 & 13 & 18 & 42 & 50 \end{array}$$

Sta. + X - Elev.

1002.85

34+28

94.4

+48

94.1

T.P. 5.00 998.15 9.70 993.15

+70

93.8

35

93.3

+19 X-Culvert

93.1

+65

92.6

+77

92.5

36

92.2

+33

91.8

+57

91.5

37

90.9

T.P. 4.49 994.40 8.24 989.91

+80

90.1

Lt.

E

Rt.

$\frac{76}{50}$	$\frac{67}{34}$	$\frac{70}{18}$	$\frac{87}{14}$	$\frac{87}{13}$	$\frac{88}{10}$	$\frac{85}{/}$	$\frac{90}{11}$	$\frac{94}{13}$	$\frac{94}{14}$	$\frac{82}{18}$	$\frac{84}{39}$	$\frac{88}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{96}{50}$	$\frac{104}{22}$	$\frac{109}{17}$	$\frac{107}{14}$	$\frac{93}{11}$	$\frac{88}{/}$	$\frac{92}{12}$	$\frac{108}{16}$	$\frac{113}{40}$	$\frac{110}{50}$
-----------------	------------------	------------------	------------------	-----------------	----------------	-----------------	------------------	------------------	------------------

$\frac{85}{50}$	$\frac{87}{40}$	$\frac{83}{18}$	$\frac{49}{10}$	$\frac{44}{/}$	$\frac{48}{11}$	$\frac{81}{19}$	$\frac{83}{40}$	$\frac{85}{50}$
-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{106}{50}$	$\frac{109}{19}$	$\frac{54}{10}$		$\frac{49}{/}$	$\frac{53}{11}$	$\frac{106}{20}$	$\frac{111}{25}$	$\frac{105}{41}$	$\frac{104}{50}$
------------------	------------------	-----------------	--	----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{116}{50}$	$\frac{122}{19}$	$\frac{56}{9}$	$\frac{51}{/}$	$\frac{55}{11}$	$\frac{122}{113}$	$\frac{110}{30}$	$\frac{103}{50}$
------------------	------------------	----------------	----------------	-----------------	-------------------	------------------	------------------

$\frac{97}{50}$	$\frac{88}{24}$	$\frac{80}{17}$	$\frac{60}{10}$	$\frac{56}{/}$	$\frac{60}{11}$	$\frac{72}{16}$	$\frac{58}{19}$	$\frac{68}{42}$	$\frac{60}{50}$
-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{92}{50}$	$\frac{90}{47}$	$\frac{74}{40}$	$\frac{59}{10}$	$\frac{68}{13}$	$\frac{61}{9}$	$\frac{57}{/}$	$\frac{62}{14}$	$\frac{67}{13}$	$\frac{67}{15}$	$\frac{42}{17}$	$\frac{41}{26}$	$\frac{42}{44}$	$\frac{42}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{69}{50}$	$\frac{41}{17}$	$\frac{71}{14}$	$\frac{71}{13}$	$\frac{65}{10}$	$\frac{60}{/}$	$\frac{63}{11}$	$\frac{66}{13}$	$\frac{21}{18}$	$\frac{11}{44}$	$\frac{10}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{75}{50}$	$\frac{51}{18}$	$\frac{75}{14}$	$\frac{75}{17}$	$\frac{68}{10}$	$\frac{64}{/}$	$\frac{67}{11}$	$\frac{72}{13}$	$\frac{72}{15}$	$\frac{34}{20}$	$\frac{15}{41}$	$\frac{69}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{87}{50}$	$\frac{70}{17}$	$\frac{81}{14}$	$\frac{81}{13}$	$\frac{72}{11}$	$\frac{67}{/}$	$\frac{71}{11}$	$\frac{76}{14}$	$\frac{76}{15}$	$\frac{49}{19}$	$\frac{33}{38}$	$\frac{27}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{91}{50}$	$\frac{84}{41}$	$\frac{78}{17}$	$\frac{86}{14}$	$\frac{86}{12}$	$\frac{77}{10}$	$\frac{73}{/}$	$\frac{75}{14}$	$\frac{83}{14}$	$\frac{83}{16}$	$\frac{71}{19}$	$\frac{64}{35}$	$\frac{60}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{64}{50}$	$\frac{44}{17}$	$\frac{57}{15}$	$\frac{59}{13}$	$\frac{48}{11}$	$\frac{43}{/}$	$\frac{45}{12}$	$\frac{55}{15}$	$\frac{55}{16}$	$\frac{40}{21}$	$\frac{43}{31}$	$\frac{41}{39}$	$\frac{41}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

Sta.	+	π	-	Elev
		994.40		
B.M.	3.79	994.40	3.79	990.61
38				89.3
+23	X-Culvert			
+50				88.3
39				87.0
+50				84.7
T.P.	2.13	985.36	11.17	983.23
40				81.7
+50				78.4
T.P.	5.30	980.35	10.31	975.05
X +80				75.8
41				74.2
+50				70.0
T.P.	5.97	975.55	10.77	969.58
42				66.6
+50				63.8
+75				62.4

Lt.

E

Rt.

Spike in 24" oak 50' Rt. 215 37+95

$$\begin{array}{r} 81 \quad 83 \quad 86 \quad 63 \\ 50 \quad 39 \quad 18 \quad 14 \end{array} \quad \begin{array}{r} 61 \quad 49 \quad 75 \\ 10 \quad 16 \end{array} \quad \begin{array}{r} 80 \quad 76 \quad 60 \\ 23 \quad 34 \quad 50 \end{array}$$

$$\begin{array}{r} 144 \\ 103 \\ 109 \quad 78 \\ 50 \quad 37 \quad 22 \quad 14 \end{array}$$

$$\begin{array}{r} 124 \\ 92 \\ 61 \quad 55 \quad 61 \quad 62 \\ 13 \quad 16 \quad 26 \end{array} \quad \begin{array}{r} 67 \quad 53 \quad 38 \quad 21 \\ 31 \quad 35 \quad 43 \quad 50 \end{array}$$

$$\begin{array}{r} 159 \\ 50 \end{array} \quad \begin{array}{r} 126 \\ 24 \end{array} \quad \begin{array}{r} 84 \\ 15 \end{array} \quad \begin{array}{r} 79 \\ 4 \end{array} \quad \begin{array}{r} 74 \\ 74 \end{array} \quad \begin{array}{r} 67 \quad 70 \\ 13 \quad 16 \end{array} \quad \begin{array}{r} 65 \quad 00 \\ 25 \quad 37 \end{array} \quad \begin{array}{r} 114 \\ 41 \end{array} \quad \begin{array}{r} 104 \\ 50 \end{array}$$

$$\begin{array}{r} 178 \\ 50 \end{array} \quad \begin{array}{r} 123 \\ 31 \end{array} \quad \begin{array}{r} 111 \\ 20 \end{array} \quad \begin{array}{r} 116 \\ 18 \end{array} \quad \begin{array}{r} 100 \\ 5 \end{array} \quad \begin{array}{r} 97 \\ 97 \end{array} \quad \begin{array}{r} 90 \quad 61 \\ 12 \quad 25 \end{array} \quad \begin{array}{r} 15 \\ 34 \end{array} \quad \begin{array}{r} 164 \\ 48 \end{array} \quad \begin{array}{r} 180 \\ 62 \end{array} \quad \begin{array}{r} 1102 \\ 85 \end{array}$$

$$\begin{array}{r} 112 \\ 50 \end{array} \quad \begin{array}{r} 82 \\ 40 \end{array} \quad \begin{array}{r} 47 \\ 21 \end{array} \quad \begin{array}{r} 52 \\ 20 \end{array} \quad \begin{array}{r} 51 \\ 15 \end{array} \quad \begin{array}{r} 38 \\ 5 \end{array} \quad \begin{array}{r} 37 \\ 37 \end{array} \quad \begin{array}{r} 38 \quad 33 \quad 23 \\ 5 \quad 9 \quad 10 \end{array} \quad \begin{array}{r} 16 \\ 15 \end{array} \quad \begin{array}{r} 168 \\ 25 \end{array} \quad \begin{array}{r} 186 \\ 35 \end{array} \quad \begin{array}{r} 1132 \\ 67 \end{array}$$

$$\begin{array}{r} 125 \\ 50 \end{array} \quad \begin{array}{r} 113 \\ 24 \end{array} \quad \begin{array}{r} 89 \\ 18 \end{array} \quad \begin{array}{r} 71 \\ 4 \end{array} \quad \begin{array}{r} 70 \\ 70 \end{array} \quad \begin{array}{r} 68 \quad 67 \\ 8 \quad 11 \end{array} \quad \begin{array}{r} 26 \\ 17 \end{array} \quad \begin{array}{r} 124 \\ 50 \end{array}$$

$$\begin{array}{r} 127 \\ 50 \end{array} \quad \begin{array}{r} 117 \\ 38 \end{array} \quad \begin{array}{r} 100 \\ 28 \end{array} \quad \begin{array}{r} 54 \\ 13 \end{array} \quad \begin{array}{r} 46 \\ 46 \end{array} \quad \begin{array}{r} 45 \quad 54 \\ 8 \quad 11 \end{array} \quad \begin{array}{r} 54 \\ 17 \end{array} \quad \begin{array}{r} 22 \quad 00 \\ 31 \quad 41 \end{array} \quad \begin{array}{r} 113 \\ 50 \end{array}$$

$$\begin{array}{r} 146 \\ 50 \end{array} \quad \begin{array}{r} 132 \\ 30 \end{array} \quad \begin{array}{r} 110 \\ 21 \end{array} \quad \begin{array}{r} 70 \\ 11 \end{array} \quad \begin{array}{r} 62 \\ 62 \end{array} \quad \begin{array}{r} 86 \\ 8 \end{array} \quad \begin{array}{r} 88 \\ 13 \end{array} \quad \begin{array}{r} 59 \\ 18 \end{array} \quad \begin{array}{r} 24 \\ 34 \end{array} \quad \begin{array}{r} 50 \end{array}$$

$$\begin{array}{r} 170 \\ 50 \end{array} \quad \begin{array}{r} 167 \\ 27 \end{array} \quad \begin{array}{r} 108 \\ 12 \end{array} \quad \begin{array}{r} 104 \\ 10.4 \end{array} \quad \begin{array}{r} 105 \\ 8 \end{array} \quad \begin{array}{r} 145 \\ 15 \end{array} \quad \begin{array}{r} 153 \\ 30 \end{array} \quad \begin{array}{r} 141 \\ 50 \end{array}$$

$$\begin{array}{r} 131 \\ 50 \end{array} \quad \begin{array}{r} 131 \\ 21 \end{array} \quad \begin{array}{r} 94 \\ 13 \end{array} \quad \begin{array}{r} 90 \\ 90 \end{array} \quad \begin{array}{r} 94 \quad 134 \quad 139 \quad 136 \\ 9 \quad 16 \quad 19 \quad 50 \end{array}$$

$$\begin{array}{r} 84 \\ 50 \end{array} \quad \begin{array}{r} 101 \\ 30 \end{array} \quad \begin{array}{r} 111 \\ 22 \end{array} \quad \begin{array}{r} 142 \\ 17 \end{array} \quad \begin{array}{r} 119 \\ 13 \end{array} \quad \begin{array}{r} 118 \\ 18 \end{array} \quad \begin{array}{r} 123 \\ 9 \end{array} \quad \begin{array}{r} 145 \\ 16 \end{array} \quad \begin{array}{r} 148 \\ 18 \end{array} \quad \begin{array}{r} 145 \\ 50 \end{array}$$

$$\begin{array}{r} 26 \\ 50 \end{array} \quad \begin{array}{r} 45 \\ 42 \end{array} \quad \begin{array}{r} 74 \\ 25 \end{array} \quad \begin{array}{r} 145 \\ 16 \end{array} \quad \begin{array}{r} 134 \\ 13 \end{array} \quad \begin{array}{r} 132 \\ 132 \end{array} \quad \begin{array}{r} 136 \\ 10 \end{array} \quad \begin{array}{r} 145 \\ 13 \end{array} \quad \begin{array}{r} 145 \\ 15 \end{array} \quad \begin{array}{r} 132 \\ 16 \end{array} \quad \begin{array}{r} 150 \\ 26 \end{array} \quad \begin{array}{r} 148 \\ 50 \end{array}$$

151.75

Sta	+	A	-	Elev
		975.55		

43				41.1
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+40				59.6
-----	--	--	--	------

TP	1.61	965.76	11.40	964.15
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+22				58.1
-----	--	--	--	------

44				57.0
----	--	--	--	------

+18	Entr. Lt			
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+50				55.1
-----	--	--	--	------

45				53.5
----	--	--	--	------

TP	2.10	955.53	12.33	953.43
----	------	--------	-------	--------

+50				52.0
-----	--	--	--	------

46				51.1
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+50				50.7
-----	--	--	--	------

+81	Cross Culvert			
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BM	3.78	955.53	3.78	951.75
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Lt

R

Rt

$\frac{0.937}{50}$ $\frac{5.0}{34}$ $\frac{10.5}{28}$ $\frac{14.2}{17}$ $\frac{16.3}{16}$ $\frac{18.2}{13}$ $\frac{14.5}{14.5}$ $\frac{14.9}{10}$ $\frac{15.1}{13}$ $\frac{15.1}{14}$ $\frac{12.8}{18}$ $\frac{13.3}{22}$ $\frac{14.2}{30}$

$\frac{5.5}{50}$ $\frac{8.2}{26}$ $\frac{13.0}{24}$ $\frac{16.6}{16}$ $\frac{17.5}{14}$ $\frac{16.8}{11}$ $\frac{16.0}{16.0}$ $\frac{16.5}{10}$ $\frac{16.9}{11}$ $\frac{16.9}{14}$ $\frac{13.4}{20}$ $\frac{14.8}{34}$ $\frac{14.2}{50}$

$\frac{37}{50}$ $\frac{5.3}{21}$ $\frac{7.6}{20}$ $\frac{8.4}{17}$ $\frac{8.2}{11}$ $\frac{7.7}{10}$ $\frac{8.0}{13}$ $\frac{8.9}{15}$ $\frac{8.8}{19}$ $\frac{6.3}{37}$ $\frac{5.5}{43}$ $\frac{4.3}{50}$

$\frac{8.2}{50}$ $\frac{9.0}{30}$ $\frac{8.7}{21}$ $\frac{10.1}{18}$ $\frac{10.1}{17}$ $\frac{9.2}{14}$ $\frac{8.8}{10}$ $\frac{9.2}{13}$ $\frac{10.5}{15}$ $\frac{10.5}{18}$ $\frac{8.2}{37}$ $\frac{3.7}{50}$

$\frac{11.8}{50}$ $\frac{11.4}{27}$ $\frac{10.2}{17}$ $\frac{9.9}{10}$

$\frac{12.7}{50}$ $\frac{11.9}{25}$ $\frac{11.1}{19}$ $\frac{11.3}{13}$ $\frac{10.8}{8}$ $\frac{10.7}{10.7}$ $\frac{11.5}{8}$ $\frac{12.2}{11}$ $\frac{12.2}{14}$ $\frac{7.6}{19}$ $\frac{5.7}{29}$ $\frac{0.7}{50}$

$\frac{14.3}{50}$ $\frac{12.8}{26}$ $\frac{12.4}{21}$ $\frac{12.6}{14}$ $\frac{12.3}{12.3}$ $\frac{12.6}{7}$ $\frac{12.3}{8}$ $\frac{12.6}{14}$ $\frac{9.2}{18}$ $\frac{3.1}{50}$

$\frac{5.7}{50}$ $\frac{5.0}{23}$ $\frac{4.5}{18}$ $\frac{3.7}{11}$ $\frac{3.4}{4}$ $\frac{3.5}{7}$ $\frac{3.8}{8}$ $\frac{3.4}{14}$ $\frac{4.1}{14}$ $\frac{2.4}{33}$ $\frac{1.8}{50}$ $\frac{0.2}{50}$

$\frac{6.8}{50}$ $\frac{6.7}{21}$ $\frac{6.0}{18}$ $\frac{5.0}{14}$ $\frac{4.4}{4.4}$ $\frac{4.5}{6}$ $\frac{4.3}{8}$ $\frac{5.6}{14}$ $\frac{6.0}{20}$ $\frac{6.3}{31}$ $\frac{5.5}{50}$

$\frac{6.6}{50}$ $\frac{6.6}{18}$ $\frac{5.4}{15}$ $\frac{4.8}{4.8}$ $\frac{4.8}{7}$ $\frac{4.8}{8}$ $\frac{5.0}{10}$ $\frac{6.6}{15}$ $\frac{6.2}{50}$

$\frac{1.2}{7.7}$

$\frac{1.2}{7.3}$

Surface Beaver Lake Lt.

7.3

Spike in 12" Oak 40' Lt. Ho. 47+30

Sta + Δ - Elev

955.53

47 50.7

+50 50.8

48 51.8

+50 53.7

T.P. 9.25 963.77 1.06 954.47

49 56.3

+50 59.9

+85 62.7

T.P. 12.40 975.35 0.77 962.95

50 64.1

T.P. 10.53 979.91 5.97 969.38

+25 66.5

+50 69.1

T.P. 10.04 983.88 6.07 973.84

51 72.9

T.P. 9.90 987.41 6.37 977.51

+50 77.5

L+

L

R+

$\frac{70}{50}$ $\frac{71}{37}$ $\frac{66}{19}$ $\frac{52}{14}$ $\frac{48}{1}$ $\frac{51}{9}$ $\frac{66}{15}$ $\frac{69}{20}$ $\frac{67}{50}$

$\frac{60}{50}$ $\frac{51}{45}$ $\frac{57}{27}$ $\frac{63}{23}$ $\frac{60}{19}$ $\frac{48}{14}$ $\frac{47}{1}$ $\frac{51}{9}$ $\frac{68}{13}$ $\frac{67}{21}$ $\frac{66}{50}$

$\frac{57}{50}$ $\frac{50}{47}$ $\frac{59}{28}$ $\frac{63}{17}$ $\frac{39}{12}$ $\frac{37}{1}$ $\frac{43}{16}$ $\frac{68}{14}$ $\frac{68}{50}$

$\frac{52}{50}$ $\frac{42}{45}$ $\frac{41}{41}$ $\frac{58}{31}$ $\frac{57}{19}$ $\frac{19}{11}$ $\frac{18}{1}$ $\frac{21}{11}$ $\frac{65}{17}$ $\frac{68}{50}$

$\frac{82.6}{50}$ $\frac{50.5}{46}$ $\frac{92.1}{43}$ $\frac{52.9}{18}$ $\frac{56.4}{11}$ $\frac{56.3}{1}$ $\frac{55.9}{11}$ $\frac{50.5}{22}$ $\frac{50.1}{50}$

$\frac{53.5}{50}$ $\frac{54.3}{41}$ $\frac{56.4}{39}$ $\frac{56.9}{27}$ $\frac{56.9}{18}$ $\frac{59.5}{12}$ $\frac{59.9}{38}$ $\frac{58.9}{12}$ $\frac{55.7}{18}$ $\frac{55.1}{27}$ $\frac{54.1}{41}$ $\frac{54.7}{50}$ ✓

$\frac{62.1}{50}$ $\frac{63.2}{43}$ $\frac{61.7}{37}$ $\frac{61.4}{28}$ $\frac{60.0}{36}$ $\frac{60.2}{19}$ $\frac{62.3}{12}$ $\frac{62.7}{10}$ $\frac{62.1}{16}$ $\frac{61.7}{20}$ $\frac{61.3}{24}$ $\frac{61.2}{25}$ $\frac{62.8}{0.9}$ ✓

$\frac{64.7}{50}$ $\frac{65.7}{41}$ $\frac{64.9}{28}$ $\frac{63.0}{25}$ $\frac{62.7}{17}$ $\frac{63.7}{12}$ $\frac{64.0}{6}$ $\frac{64.1}{11}$ $\frac{63.6}{10}$ $\frac{63.2}{12}$ $\frac{64.2}{14}$ $\frac{64.8}{38}$ $\frac{65.3}{50}$ ✓

$\frac{68.4}{50}$ $\frac{69.4}{39}$ $\frac{68.9}{29}$ $\frac{66.3}{26}$ $\frac{67.1}{20}$ $\frac{65.4}{17}$ $\frac{65.4}{15}$ $\frac{66.1}{13}$ $\frac{66.5}{10}$ $\frac{65.9}{14}$ $\frac{65.3}{13}$ $\frac{65.9}{17}$ $\frac{69.1}{22}$ $\frac{68.6}{43}$ $\frac{67.8}{50}$ ✓

$\frac{73.0}{50}$ $\frac{72.9}{46}$ $\frac{74.7}{34}$ $\frac{73.4}{30}$ $\frac{71.1}{26}$ $\frac{70.7}{20}$ $\frac{67.9}{12}$ $\frac{68.8}{13}$ $\frac{69.1}{10}$ $\frac{68.6}{7}$ $\frac{67.9}{14}$ $\frac{72.9}{18}$ $\frac{72.0}{23}$ $\frac{72.1}{28}$ $\frac{68.2}{50}$ ✓

$\frac{78.9}{50}$ $\frac{82.4}{34}$ $\frac{82.4}{29}$ $\frac{73.9}{18}$ $\frac{72.8}{14}$ $\frac{73.4}{12}$ $\frac{73.9}{10}$ $\frac{73.4}{8}$ $\frac{72.8}{10}$ $\frac{73.2}{14}$ $\frac{74.3}{14}$ $\frac{72.8}{18}$ $\frac{70.2}{50}$ ✓

$\frac{83.8}{50}$ $\frac{86.1}{37}$ $\frac{79.8}{31}$ $\frac{77.8}{16}$ $\frac{76.8}{13}$ $\frac{77.0}{12}$ $\frac{77.5}{9}$ $\frac{77.0}{10}$ $\frac{77.8}{16}$ $\frac{80.5}{18}$ $\frac{78.9}{23}$ $\frac{78.2}{28}$ $\frac{72.6}{50}$ ✓

Sta	+	X	-	Elev
-----	---	---	---	------

987.41

52

80.5

T.P.

11.19

992.69

5.91

981.50

+50

82.7

53

83.7

+30

84.0

+66

83.3

54

82.4

+35

80.9

+76

78.8

T.P.

4.63

983.07

14.25

978.44

55

77.5

+50

Entr Lt.

74.9

56

72.2

+45

69.5

T.P.

2.95

974.02

12.00

971.07

L+

L

R+

86.2 16.6 86.0 80.1 80.4
 $\frac{12}{50} \frac{08}{27} \frac{14}{23} \frac{73}{74} \frac{70}{7}$

80.5 79.9 82.2 75.3
 $\frac{69}{12} \frac{75}{18} \frac{52}{18} \frac{121}{50}$

✓

86.6 87.4 82.9 82.4
 $\frac{61}{50} \frac{53}{22} \frac{98}{16} \frac{103}{11}$

82.7 81.9 84.6 78.2
 $\frac{100}{12} \frac{108}{18} \frac{81}{18} \frac{145}{50}$

✓

87.1 88.6 89.5 85.0 83.5
 $\frac{56}{50} \frac{41}{34} \frac{32}{21} \frac{77}{16} \frac{92}{11}$

83.7 83.4 83.2 86.7 85.7 84.2
 $\frac{50}{7} \frac{93}{11} \frac{95}{19} \frac{60}{19} \frac{70}{26} \frac{85}{50}$

✓

86.4 87.9 89.0 84.7 83.5
 $\frac{63}{50} \frac{48}{34} \frac{37}{20} \frac{50}{16} \frac{92}{12}$

84.0 83.4 84.6 87.8 87.4 86.8 86.8
 $\frac{97}{12} \frac{93}{16} \frac{81}{20} \frac{49}{20} \frac{53}{26} \frac{59}{39} \frac{59}{50}$

✓

83.8 86.0 86.8 83.7 82.8
 $\frac{89}{50} \frac{67}{27} \frac{59}{20} \frac{50}{16} \frac{89}{13}$

83.3 83.0 84.7 88.2 87.7 87.0
 $\frac{94}{11} \frac{77}{16} \frac{80}{21} \frac{45}{30} \frac{50}{50} \frac{57}{50}$

✓

81.1 83.1 84.0 81.8 81.7 82.1
 $\frac{46}{50} \frac{56}{26} \frac{27}{19} \frac{109}{15} \frac{110}{11} \frac{106}{6}$

82.4 82.1 82.8 87.1 86.8 86.5
 $\frac{103}{9} \frac{106}{14} \frac{59}{20} \frac{56}{25} \frac{59}{25} \frac{62}{50}$

✓

76.7 79.2 80.2 80.2 80.9
 $\frac{140}{50} \frac{135}{37} \frac{125}{21} \frac{125}{14} \frac{118}{10}$

80.5 81.5 82.9 85.4
 $\frac{122}{10} \frac{112}{13} \frac{98}{19} \frac{73}{50}$

✓

76.0 76.6 77.8 78.5 78.8
 $\frac{127}{50} \frac{161}{22} \frac{149}{13} \frac{142}{6} \frac{139}{12}$

78.5 78.2 79.9 83.6
 $\frac{142}{12} \frac{141}{13} \frac{128}{19} \frac{81}{50}$

✓

74.7 74.7 75.7 76.2 77.5 76.9 78.8 81.4
 $\frac{84}{50} \frac{84}{22} \frac{74}{15} \frac{64}{11} \frac{56}{12} \frac{62}{20} \frac{43}{20} \frac{17}{39} \frac{+01}{50}$

83.2
 $\frac{56}{12} \frac{54}{20} \frac{75}{39} \frac{83.2}{50}$

✓

71.2 72.3 74.6 74.9 74.2 74.6 79.2 72.6
 $\frac{115}{50} \frac{108}{31} \frac{85}{9} \frac{82}{52} \frac{59}{10} \frac{85}{15} \frac{39}{24} \frac{05}{50}$

72.2 71.7 73.5 79.5 82.3 83.8
 $\frac{109}{10} \frac{114}{19} \frac{96}{26} \frac{86}{50} \frac{08}{50} \frac{107}{75}$

✓

69.5 71.7 71.7 71.0 71.5 72.2 71.7 73.5 79.5 82.3 83.8
 $\frac{130}{50} \frac{44}{28} \frac{44}{19} \frac{121}{17} \frac{116}{17} \frac{109}{10} \frac{114}{19} \frac{96}{26} \frac{86}{50} \frac{08}{50} \frac{107}{75}$

69.5 69.6 68.8 69.3 69.5 69.1 68.9 69.8 70.8 80.8 82.4 82.7
 $\frac{135}{50} \frac{122}{41} \frac{96}{20} \frac{53}{21} \frac{135}{16} \frac{143}{12} \frac{138}{4} \frac{136}{136} \frac{140}{9} \frac{142}{12} \frac{133}{144} \frac{123}{18} \frac{23}{27} \frac{07}{35} \frac{04}{75}$

✓

67.6 70.5 73.5 73.8 69.6 68.8 69.3 69.5 69.1 68.9 69.8 70.8 80.8 82.4 82.7
 $\frac{135}{50} \frac{122}{41} \frac{96}{20} \frac{53}{21} \frac{135}{16} \frac{143}{12} \frac{138}{4} \frac{136}{136} \frac{140}{9} \frac{142}{12} \frac{133}{144} \frac{123}{18} \frac{23}{27} \frac{07}{35} \frac{04}{75}$

69.5 69.6 68.8 69.3 69.5 69.1 68.9 69.8 70.8 80.8 82.4 82.7
 $\frac{135}{50} \frac{122}{41} \frac{96}{20} \frac{53}{21} \frac{135}{16} \frac{143}{12} \frac{138}{4} \frac{136}{136} \frac{140}{9} \frac{142}{12} \frac{133}{144} \frac{123}{18} \frac{23}{27} \frac{07}{35} \frac{04}{75}$

✓

Sta. + π - Elev

974.02

56+75 22.7

57 26.1

T.P. 1.78 966.70 9.10 964.92

+30 64.5

+85 61.0

58 60.0

T.P. 0.72 960.03 7.39 959.31

+50 56.7

59 54.2

+50 52.3

+72 Cross Culvert

60 50.4

T.P. 0.17 956.26 3.94 956.09

+50 49.9

61 49.2

Lt

L

Rt

$$\frac{139}{50} \quad \frac{109}{48} \quad \frac{71}{34} \quad \frac{23}{21} \quad \frac{70}{15} \quad \frac{67}{9} \quad \frac{63}{8} \quad \frac{67}{10} \quad \frac{71}{13} \quad \frac{70}{14} \quad \frac{59}{29} \quad \frac{123}{40} \quad \frac{160}{40} \quad \frac{122}{25}$$

$$\frac{253}{86} \quad \frac{233}{67} \quad \frac{202}{53} \quad \frac{134}{36} \quad \frac{61}{20} \quad \frac{87}{14} \quad \frac{82}{8} \quad \frac{79}{9} \quad \frac{83}{13} \quad \frac{81}{16} \quad \frac{70}{16} \quad \frac{125}{30} \quad \frac{144}{41} \quad \frac{155}{66}$$

$$\frac{166}{61} \quad \frac{140}{40} \quad \frac{49}{21} \quad \frac{20}{17} \quad \frac{27}{10} \quad \frac{22}{9} \quad \frac{29}{15} \quad \frac{19}{15} \quad \frac{167}{28} \quad \frac{110}{23}$$

$$\frac{180}{75} \quad \frac{176}{50} \quad \frac{156}{27} \quad \frac{63}{11} \quad \frac{57}{8} \quad \frac{60}{10} \quad \frac{67}{10} \quad \frac{54}{17} \quad \frac{25}{21} \quad \frac{09}{28} \quad \frac{05}{40} \quad \frac{105}{50}$$

$$\frac{180}{50} \quad \frac{140}{27} \quad \frac{73}{10} \quad \frac{67}{10} \quad \frac{72}{18} \quad \frac{77}{25} \quad \frac{70}{35} \quad \frac{24}{50} \quad \frac{12}{50}$$

$$\frac{111}{50} \quad \frac{97}{22} \quad \frac{36}{9} \quad \frac{33}{10} \quad \frac{37}{12} \quad \frac{38}{16} \quad \frac{48}{16} \quad \frac{53}{38} \quad \frac{32}{46} \quad \frac{105}{52}$$

$$\frac{113}{50} \quad \frac{105}{23} \quad \frac{100}{18} \quad \frac{62}{10} \quad \frac{58}{11} \quad \frac{62}{16} \quad \frac{81}{16} \quad \frac{75}{43} \quad \frac{64}{50}$$

$$\frac{114}{50} \quad \frac{113}{19} \quad \frac{107}{15} \quad \frac{84}{10} \quad \frac{77}{11} \quad \frac{80}{11} \quad \frac{101}{16} \quad \frac{98}{20} \quad \frac{90}{50}$$

$$\frac{117.73}{12.3}$$

surface Reservoir

$$\frac{11.38}{11.4}$$

$$\frac{948.63}{11.4}$$

$$\frac{45}{80} \quad \frac{115}{17} \quad \frac{100}{10} \quad \frac{96}{11} \quad \frac{98}{17} \quad \frac{111}{24} \quad \frac{109}{50} \quad \frac{108}{50}$$

$$\frac{80}{50} \quad \frac{80}{37} \quad \frac{79}{15} \quad \frac{73}{12} \quad \frac{73}{9} \quad \frac{72}{9} \quad \frac{69}{12} \quad \frac{75}{14} \quad \frac{76}{22} \quad \frac{76}{38} \quad \frac{75}{50}$$

$$\frac{82}{50} \quad \frac{82}{32} \quad \frac{49}{23} \quad \frac{79}{15} \quad \frac{73}{11} \quad \frac{72}{10} \quad \frac{70}{11} \quad \frac{76}{15} \quad \frac{76}{50}$$

Sta + A - Elev

956.26

61+50 49.2

62 49.5

+50 49.8

63 50.3

+50 50.7

64 51.6

TP 9.07 965.16 0.17 956.09

+50 52.9

65 55.2

+18 56.5

+18 54.5
Going West on Maryland St

+50 57.0

LL 61.4

B.M. 9.07 956.09

L+

L

PX

$$\frac{7.9}{50} \quad \frac{7.7}{10} \quad \frac{7.2}{11} \quad \frac{7.3}{9} \quad 7.1 \quad \frac{7.1}{10} \quad \frac{7.2}{12} \quad \frac{7.6}{13} \quad \frac{7.5}{50}$$

$$\frac{8.0}{50} \quad \frac{7.9}{21} \quad \frac{8.0}{15} \quad \frac{7.0}{11} \quad 6.8 \quad \frac{7.1}{9} \quad \frac{6.8}{11} \quad \frac{7.4}{14} \quad \frac{7.4}{50}$$

$$\frac{8.0}{50} \quad \frac{7.8}{20} \quad \frac{7.5}{11} \quad \frac{6.6}{9} \quad 6.5 \quad \frac{6.7}{11} \quad \frac{7.3}{14} \quad \frac{7.1}{16} \quad \frac{6.8}{50}$$

$$\frac{8.0}{50} \quad \frac{7.6}{29} \quad \frac{7.7}{17} \quad \frac{6.2}{10} \quad 6.0 \quad \frac{6.3}{10} \quad \frac{6.2}{13} \quad \frac{6.7}{15} \quad \frac{6.1}{17} \quad \frac{6.2}{50}$$

$$\frac{7.4}{50} \quad \frac{6.8}{14} \quad \frac{5.7}{8} \quad 5.6 \quad \frac{5.9}{11} \quad \frac{6.0}{13} \quad \frac{6.5}{15} \quad \frac{6.2}{50}$$

$$\frac{5.9}{50} \quad \frac{5.7}{30} \quad \frac{5.1}{26} \quad \frac{5.8}{18} \quad \frac{5.5}{12} \quad 4.7 \quad \frac{5.1}{13} \quad \frac{6.1}{21} \quad \frac{5.8}{50}$$

$$\frac{11.1}{50} \quad \frac{12.6}{24} \quad \frac{13.1}{17} \quad \frac{12.8}{12} \quad \frac{12.3}{9} \quad 12.3 \quad \frac{12.8}{15} \quad \frac{12.6}{17} \quad \frac{14.4}{26} \quad \frac{14.5}{50}$$

$$\frac{8.5}{50} \quad \frac{10.3}{30} \quad \frac{10.0}{26} \quad \frac{10.2}{16} \quad \frac{10.6}{11} \quad 10.0 \quad \frac{10.1}{5} \quad \frac{10.0}{10} \quad \frac{10.6}{21} \quad \frac{12.4}{50}$$

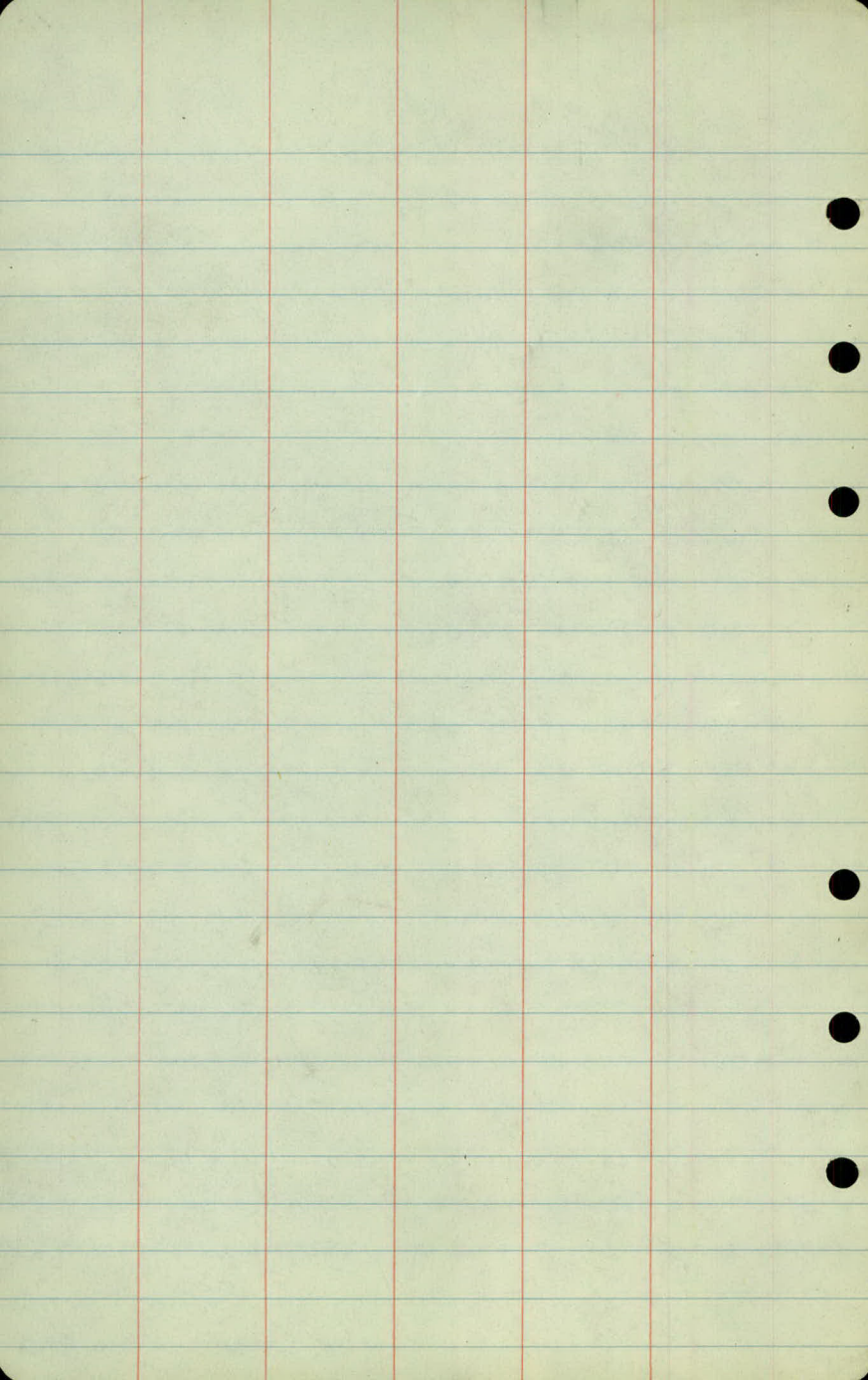
$$\frac{6.8}{50} \quad \frac{8.7}{26} \quad \frac{8.7}{15} \quad 8.7 \quad \frac{9.0}{13} \quad \frac{9.8}{23} \quad \frac{10.8}{40} \quad \frac{11.8}{50}$$

$$\frac{11.7}{50} \quad \frac{10.8}{30} \quad 8.7 \quad \frac{6.6}{50}$$

$$\frac{11.7}{50} \quad \frac{9.8}{8} \quad \frac{8.3}{6} \quad 8.2 \quad \frac{7.2}{9} \quad \frac{6.6}{18} \quad \frac{5.0}{30} \quad \frac{3.4}{50}$$

$$\frac{9.5}{50} \quad \frac{6.8}{25} \quad \frac{6.1}{7} \quad \frac{3.4}{1} \quad 3.8 \quad \frac{3.4}{11} \quad \frac{3.9}{20} \quad \frac{2.9}{23} \quad \frac{2.6}{28} \quad \frac{1.6}{32} \quad \frac{1.0}{50}$$

SpKin G. Polc 20' Rt Sta 65+00



East Ave.

slope stakes

Sta.	+	π	-	Grade
B.M.	425	956.00		(751.75)

45				541
----	--	--	--	-----

150				53.8
-----	--	--	--	------

46				53.8
----	--	--	--	------

150				
-----	--	--	--	--

182	Culv.			
-----	-------	--	--	--

47				
----	--	--	--	--

150				53.8
-----	--	--	--	------

48				54.2
----	--	--	--	------

150				55.3
-----	--	--	--	------

T.P.	8.49	962.57	1.62	954.58
------	------	--------	------	--------

49				57.2
----	--	--	--	------

150				59.9
-----	--	--	--	------

Gr. Rod.

LH

R

RH

Sph. in 12" o.d. 40' L. 47150

$$1.9 \quad 16.8' / \begin{array}{r} 2.8 \\ -0.9 \end{array} \quad \begin{array}{r} 26 \\ -0.7 \end{array}$$

$$2.2 \quad 20.0' / \begin{array}{r} 4.7 \\ -2.5 \end{array} \quad \begin{array}{r} 40 \\ -1.8 \end{array} \quad \begin{array}{r} 71 \\ -0.9 / 16.8' \end{array}$$

$$2.2 \quad 25.0' / \begin{array}{r} 7.2 \\ -5.0 \end{array} \quad \begin{array}{r} 5.0 \\ -2.8 \end{array} \quad \begin{array}{r} 6.3 \\ -0.1 / 23.2 \end{array}$$

$$2.2 \quad 25.0' / \begin{array}{r} 7.2 \\ -5.0 \end{array} \quad \begin{array}{r} 5.3 \\ -3.1 \end{array} \quad \begin{array}{r} 7.2 \\ -5.0 / 25.0 \end{array}$$

$$21.0' / \begin{array}{r} 8.0 \\ -4.0 \end{array}$$

$$EI. \begin{array}{r} 2.7 \\ 48.3 / 21.0 \end{array}$$

$$25.0' / \begin{array}{r} 7.2 \\ -5.0 \end{array}$$

$$\begin{array}{r} 5.4 \\ -3.2 \end{array}$$

$$\begin{array}{r} 1.9 \\ -5.1 / 26.4' \end{array}$$

$$2.2 \quad 24.0' / \begin{array}{r} 6.7 \\ -4.5 \end{array} \quad \begin{array}{r} 5.3 \\ -3.1 \end{array} \quad \begin{array}{r} 8.1 \\ -5.7 / 26.1 \end{array}$$

$$1.8 \quad 23.6' / \begin{array}{r} 6.6 \\ -4.8 \end{array} \quad \begin{array}{r} 4.2 \\ -2.4 \end{array} \quad \begin{array}{r} 8.2 \\ -6.4 / 27.8' \end{array}$$

$$0.7 \quad 26.2' / \begin{array}{r} 6.3 \\ -5.6 \end{array} \quad \begin{array}{r} 6.3 \\ -1.6 \end{array} \quad \begin{array}{r} 8.0 \\ -7.3 / 29.6 \end{array}$$

$$5.7 \quad 23.8' / \begin{array}{r} 10.1 \\ -7.4 \end{array} \quad \begin{array}{r} 6.5 \\ -0.8 \end{array} \quad \begin{array}{r} 13.1 \\ -7.4 / 29.8' \end{array}$$

$$3.0 \quad 21.6' / \begin{array}{r} 6.3 \\ -3.3 \end{array} \quad \begin{array}{r} 2.0 \\ -0.0 \end{array} \quad \begin{array}{r} 7.3 \\ -0.3 / 23.6' \end{array}$$

Sta	+	π	-	Grade
B.M.		958.17		956.09

58	100			59.5
----	-----	--	--	------

	+50			57.0
--	-----	--	--	------

59				54.8
----	--	--	--	------

	+50			53.3
--	-----	--	--	------

60				52.3
----	--	--	--	------

	+50			52.0
--	-----	--	--	------

61		culv. 10.2/19.0'		
----	--	---------------------	--	--

I.P.	6.98	955.87	928.	949.87
------	------	--------	------	--------

	+50			
--	-----	--	--	--

62				
----	--	--	--	--

	+50			
--	-----	--	--	--

63				52.0
----	--	--	--	------

Gr. Rod Lt 2 Rt

Spk. in G.P. 20' Pt. 65400

$$11.3 \quad 33.0' / \begin{array}{r} 86 \\ -99 \end{array}$$

$$1.2 \quad 30.2' / \begin{array}{r} 8.8 \\ -7.6 \end{array} \quad \begin{array}{r} 15 \\ -0.3 \end{array} \quad \begin{array}{r} 3.0 \\ -18/8.6' \end{array}$$

$$3.4 \quad 26.2' / \begin{array}{r} 9.0 \\ -5.6 \end{array} \quad \begin{array}{r} 4.0 \\ -0.6 \end{array} \quad \begin{array}{r} 6.6 \\ -24/21.4' \end{array}$$

$$4.9 \quad 24.2' / \begin{array}{r} 9.5 \\ -4.6 \end{array} \quad \begin{array}{r} 6.0 \\ -1.1 \end{array} \quad \begin{array}{r} 8.2 \\ -2.3/21.6 \end{array}$$

$$5.9 \quad 23.0' / \begin{array}{r} 9.9 \\ -4.0 \end{array} \quad \begin{array}{r} 7.9 \\ -2.0 \end{array} \quad \begin{array}{r} 9.6 \\ -3.7/22.4' \end{array}$$

$$6.2 \quad 22.8' / \begin{array}{r} 10.1 \\ -3.9 \end{array} \quad \begin{array}{r} 9.0 \\ -2.8 \end{array} \quad \begin{array}{r} 9.7 \\ -3.5/22.0' \end{array}$$

$$6.2 \quad 22.6' / \begin{array}{r} 10.0 \\ -3.8 \end{array} \quad \begin{array}{r} 9.3 \\ -3.1 \end{array} \quad \begin{array}{r} 9.5 \\ -3.7/22.4' \end{array} \quad \text{Calc. - 19'}$$

$$3.9 \quad 22.6' / \begin{array}{r} 7.7 \\ -3.8 \end{array} \quad \begin{array}{r} 1.0 \\ -3.1 \end{array} \quad \begin{array}{r} 7.7 \\ -3.8/22.6 \end{array}$$

$$2.9 \quad 23.0' / \begin{array}{r} 7.7 \\ -4.0 \end{array} \quad \begin{array}{r} 6.7 \\ -2.8 \end{array} \quad \begin{array}{r} 7.3 \\ -4.4/22.2' \end{array}$$

$$3.9 \quad 22.4' / \begin{array}{r} 7.6 \\ -3.7 \end{array} \quad \begin{array}{r} 6.3 \\ -2.4 \end{array} \quad \begin{array}{r} 6.9 \\ -3.0/21.0' \end{array}$$

$$3.9 \quad 21.6' / \begin{array}{r} 7.2 \\ -3.3 \end{array} \quad \begin{array}{r} 5.9 \\ -2.0 \end{array} \quad \begin{array}{r} 6.0 \\ -2.1/19.2 \end{array}$$

5/0	+	π	-	Grade
		955.87		

63	+50			52.2
----	-----	--	--	------

64				52.8
----	--	--	--	------

	+50			53.8
--	-----	--	--	------

65				55.2
----	--	--	--	------

B.M.			-0.22	
------	--	--	-------	--

(956.09)

Gr. Eod.

Lt.

L

Rt.

3.7

$$21.0 / \frac{6.7}{-3.0}$$

$$\frac{5.4}{-1.7}$$

$$\frac{6.2}{-2.5} / 20.0$$

3.1

$$20.2 / \frac{5.7}{-2.6}$$

$$\frac{4.6}{-1.5}$$

$$\frac{5.6}{-2.5} / 20.0$$

2.1

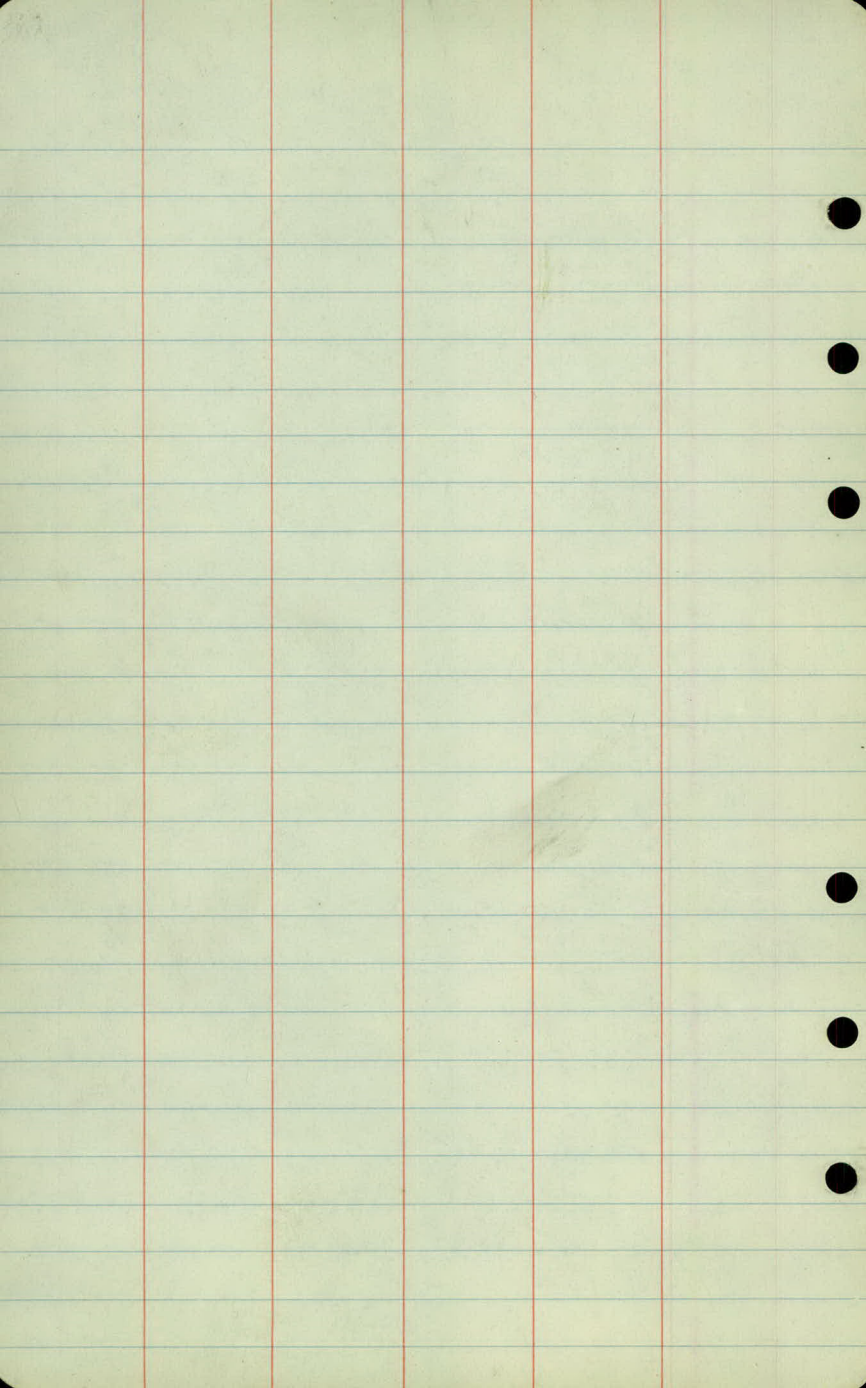
$$18.0 / \frac{3.6}{-1.5}$$

$$\frac{3.2}{-1.1}$$

$$\frac{4.2}{-2.1} / 19.2$$

0.7

Spk. in G.P. 20' Rt. 65+00'



9/4/46

Alignment

East Ave Ext.
Stillwater Rd. conn.

7- Pages

Sta	Point	Δ Lt	Δ Rt
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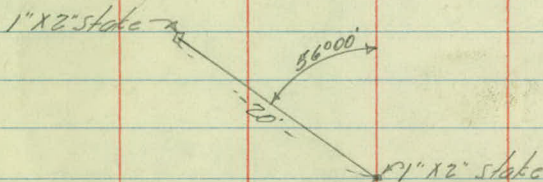
3 +07	P.O.T. = Proposed location of steps		
-------	-------------------------------------	--	--

2 +27.3	P.I.	0°23'±	
---------	------	--------	--

0 +00 =	Stillwater Cut Off		
---------	--------------------	--	--

9-4-76 Cloudy & Windy
 K.A.
 A.M.
 M.B.
 C.F.

43

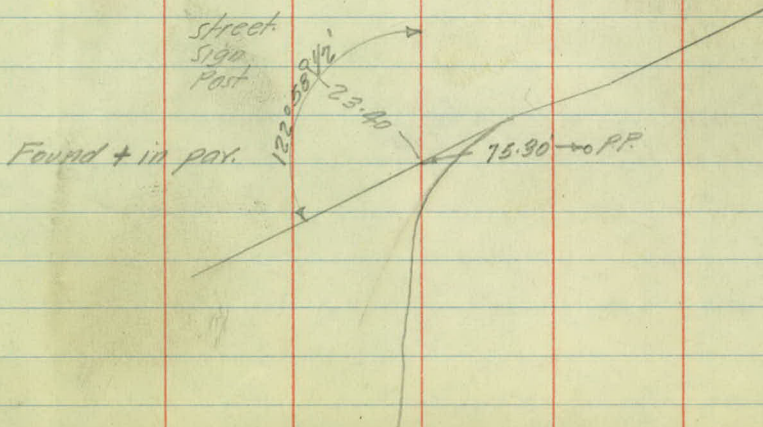


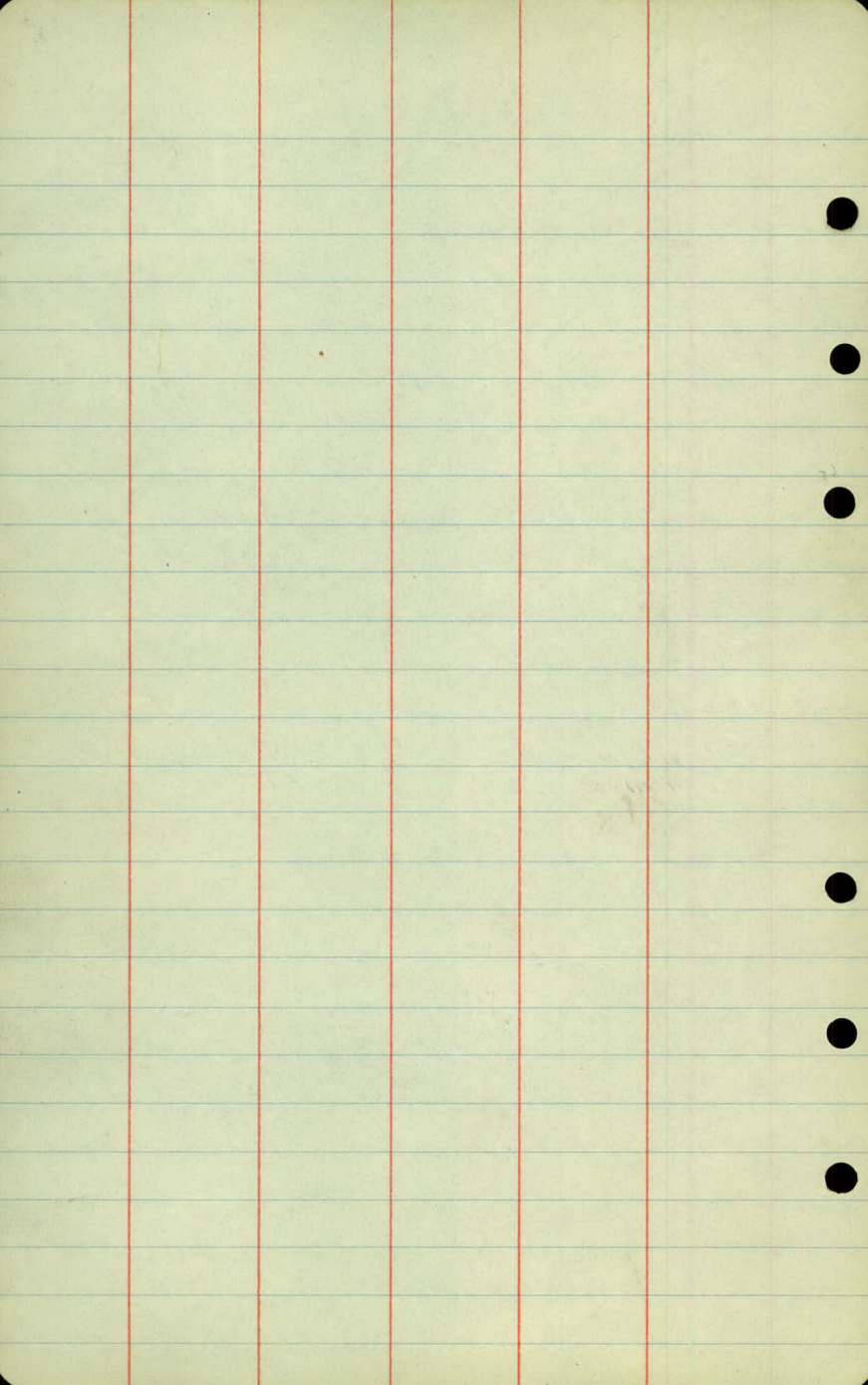
Found iron assumed
 iron on sec. line

$\uparrow \frac{1}{4} \frac{1}{4}$

ASSUMING IRON AS P.I.
 of East Ave.

(Lakewood Drive)
 91' 11" 1/2





Topography

5

4

3

Road - 39'

+24 Cor Woods - 19'
50-60 = Trail

+56 T.P - 25'

14-23 = Trail

2

T

3-10 = Trail

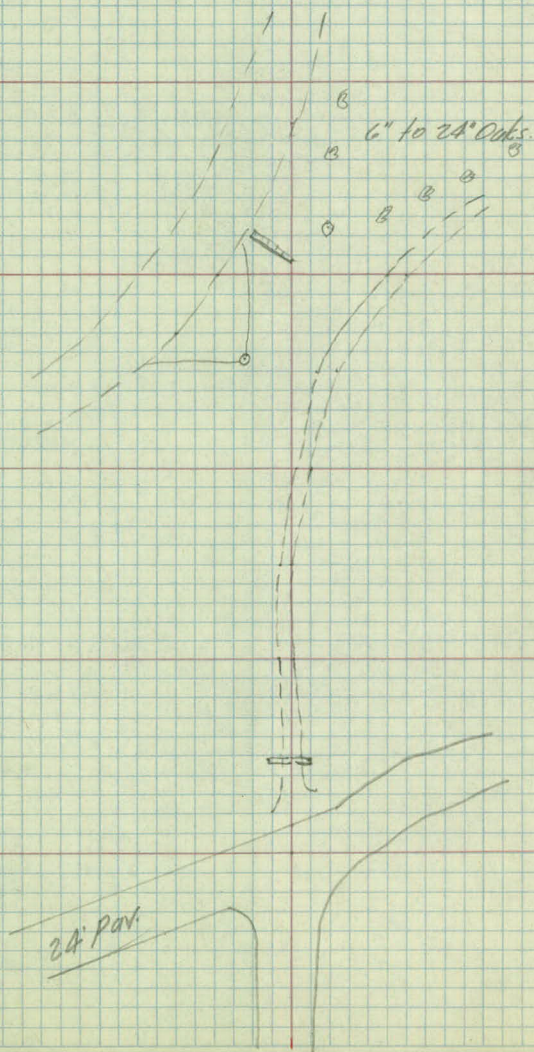
+50 Trail 6-0'

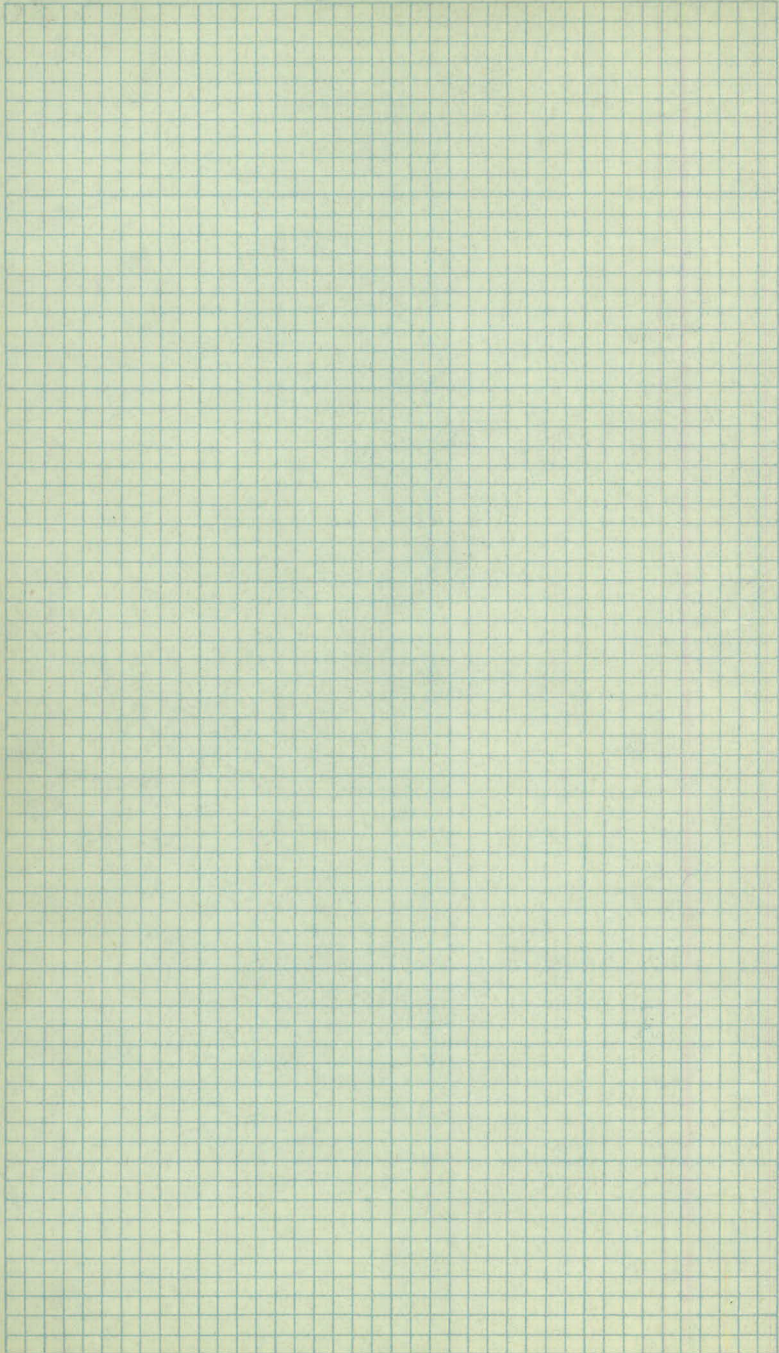
1

Trail = 6-0

+48-12" x 20' Dredge & Spoil 12-8'
+50 Trail 7-5'

0





Levels

Sta	+	π	-	Elev
B.M.	1.28	101.28		100.00

0 100			1.28	100.00
-------	--	--	------	--------

H44			1.18	100.1
-----	--	--	------	-------

+ 48 12" X 20' IRON CURV				98.7
--------------------------	--	--	--	------

1				97.5
---	--	--	--	------

+ 50				96.3
------	--	--	--	------

2				93.5
---	--	--	--	------

+ 20				92.1
T.P.	2.47	94.26	9.49	91.79

+ 41				90.6
------	--	--	--	------

lt. & Bl.
+ 10 par sta 0100 (assume data)

4.88	2.9	2.6	2.8	F.L.
12	8		6	4.50
				8

49	41	38	40	2.8	2.8
34	18		13	17	41

54	6.2	50	5.0	4.2
20	20		12	15

14.6	11.3	9.4	7.8	6.9	5.8	5.4
50	34	17		12	24	34

16.5	13.2	11.1	9.2	8.2	6.6	6.2
50	35	19		15	36	50

Top Iron & sta 2127.3

14.4	12.8	37	21	0.2	0.0
50	14		24	43	50

Sta	+	π	-	Elev.
		94.26		

2	+70			87.8
---	-----	--	--	------

3				84.3
---	--	--	--	------

407				83.0
-----	--	--	--	------

Profile of proposed location of steps

415				81.7
-----	--	--	--	------

474				65.3
-----	--	--	--	------

T.P.	900	102.60	0.66	93.60
------	-----	--------	------	-------

B.M.			2.60	100.00
------	--	--	------	--------

(100.00)

LT

C

RT

22.1 21.5 16.1 14.5 14.3 6.8 6.5 5.1 3.2
52 44 31 21 13 2 27 50

Shoulder

23.6 23.9 22.3 21.8 10.3 10.0 8.0 6.6
50 39 33 20 4 32 50

E road

Edge road

25.8 25.7 24.0 23.2 17.1 11.8 11.3
41 26 23 18.5 8 2.5

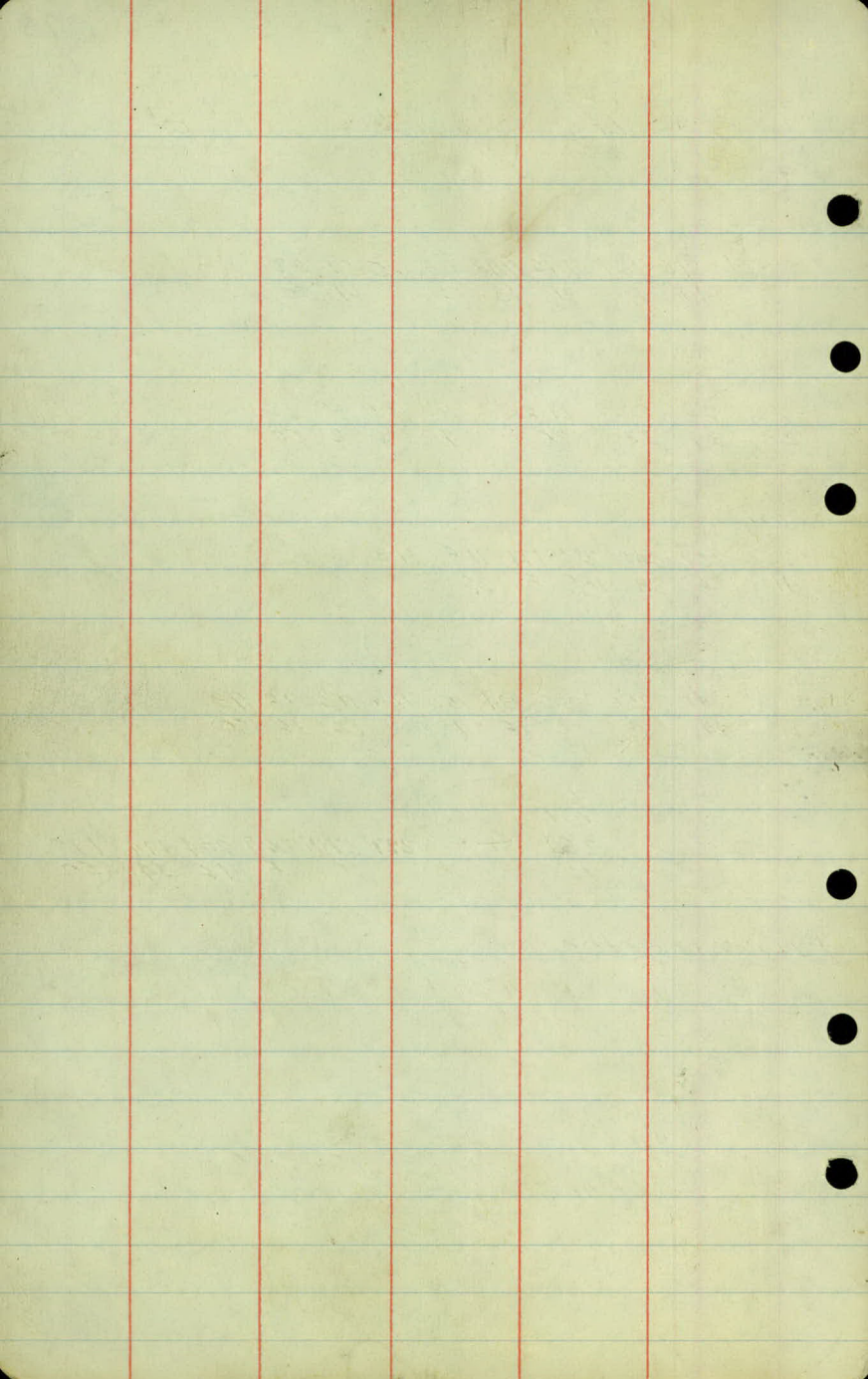
Shoulder

24.9 25.3 23.5 23.4 15.7 12.6 11.2 9.8 9.3
44 25 22 18 4 12 36 50

E road

28.7 29 29.0 27.7 26.9 20.4 19.4 19.0
16 0 6 16 34 50

+ in pos. sta 0+00



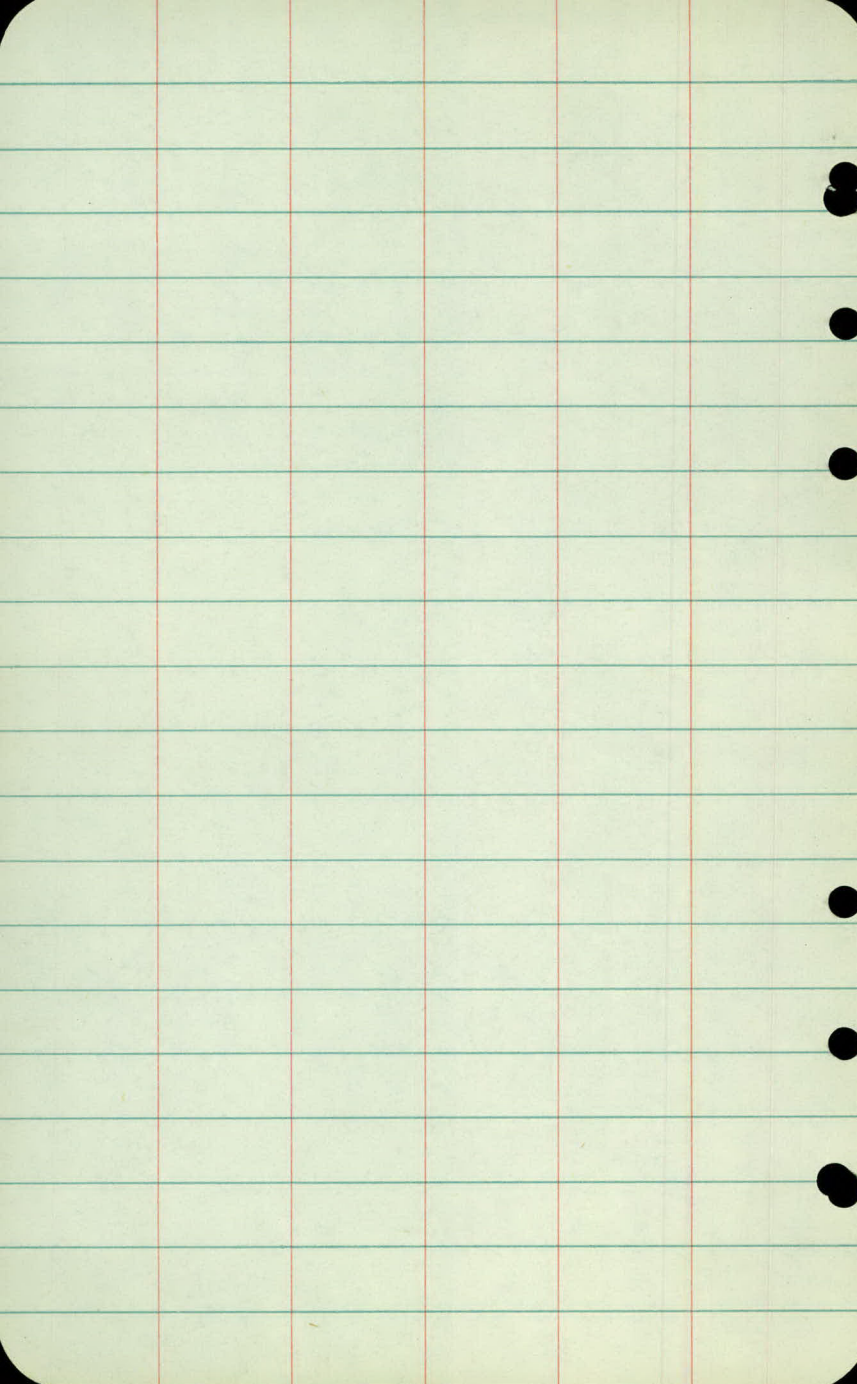
1
LAKEWOOD DRIVE

Case to Maryland

Profile

13 pages

Rec. 7/21/60



Profile

956.09 G.P.

Sta	+	·	-	Elev.
		988.17		
BM	9.15	987.59		978.44 979.02
		982.90		982.29
BM	0.61	982.32	5.88	981.71
		969.38		969.38
B.M.	0.00	968.80	13.52	968.80
		958.91		956.74
T.P.	2.17	958.33	12.69	956.16
		961.50		957.41
B.M.	4.09	960.92	1.50	956.83

43+

0.00 61.5

+50

2.0 59.5

44

3.3 58.2

+50

4.7 56.8

45

5.9 55.6

+50

7.0 54.5

46

7.7 53.8

July 11, 1960

3

Spike in PP 30' Lt Sta 54+75

SE CORNER OF BOTTOM STEP^{HOUSE} #1075

NW CORNER OF TOP STEP HOUSE #1068

S Edge of M.H

NE Edge of Pumping Stn. 45+30 40' Lt

STA	+	Δ	-	ELV
-----	---	----------	---	-----

961.50
960.92

46+50

8.1

53.4

47

7.9

53.6

+50

8.1

53.4

48

7.9

53.6

+50

6.9

54.6

49

4.6

56.9

T.P

12.99

969.82

969.15

4.67

956.83

956.25

(956.16)

+50

9.4

60.4

+77

7.52

62.30

+96

6.90

62.92

50

5.1

64.7

FK
JL
WM
JH

July 20, 1960

4

MH

Cor Conc Ent Lt

" " " "

Sta	+	Σ	-	Elev.
		969.82		
		969.15		

50+24			3.28	66.54
-------	--	--	------	-------

+29			3.24	66.58
-----	--	--	------	-------

+43			0.88	68.94
-----	--	--	------	-------

T.P.	13.26	982.04 981.37	1.04	968.78 968.11
------	-------	------------------	------	------------------

+50			12.2	69.8
-----	--	--	------	------

51			7.6	74.4
----	--	--	-----	------

+50			3.7	78.3
-----	--	--	-----	------

+55				
-----	--	--	--	--

✓

July 20, 1960

5

End Conc Ent Ribbon 28' Rt

" " " " "

± 9' Conc Ent 32' Rt

75.33

75.90

76.57

77.54

6.71 6.14 5.47 4.50

60 49 39 29

Joint

75.26

75.42

→ 6.78 6.62

65 68

Garage floor

Sta	+	π	-	Elev
-----	---	-------	---	------

982.04
981.37

52			0.88	81.16
----	--	--	------	-------

T.P.	8.78	989.96 989.29	0.86	981.18 980.51
------	------	------------------	------	------------------

+50			6.4	83.6
-----	--	--	-----	------

53			5.4	84.6
----	--	--	-----	------

+05			5.30	84.66
-----	--	--	------	-------

+35			4.4	85.6
-----	--	--	-----	------

+50			5.4	84.6
-----	--	--	-----	------

+80			11.66	78.30
-----	--	--	-------	-------

54			7.04	82.92
----	--	--	------	-------

+50			9.26	80.70
-----	--	--	------	-------

BM	0.58	979.73 979.02	10.81	978.48
----	------	------------------	-------	--------

979.15

979.02

978.44

July 20, 1960

6

Top M H £

House 73' Lt

Garage ent Lt 85'

Spike in PP 30' Lt Sta 54+75

Sta	+	π	-	Elev
		979.73 979.02		

55			1.94	77.79
----	--	--	------	-------

+50			4.36	75.37
-----	--	--	------	-------

+80			6.16	73.57 972.86
-----	--	--	------	----------------------------

56			7.2	72.5
----	--	--	-----	------

+50			9.9	69.8
-----	--	--	-----	------

57			12.7	67.0
----	--	--	------	------

TP	0.71	967.76 967.05	12.68	967.05 966.34
----	------	------------------	-------	------------------

+50			4.1	63.7
-----	--	--	-----	------

+66			5.42	962.34 961.63
-----	--	--	------	-----------------------------

58			7.1	60.7
----	--	--	-----	------

+50			10.0	57.8
-----	--	--	------	------

59			11.8	56.0
----	--	--	------	------

July 20, 1960

7

Top MH £

612
432
180

Begin 15' fill Lt

Clean
Fill
Wanted Sign

Top MH £

Sta	+	π	-	Elev.
		967.76 967.05		
59+16		.	12.76	55.0
		958.12		955.0
TP	3.12	957.41	12.76	954.29
+50			3.4	54.7
60			4.1	54.0
+50			4.6	53.5
61			4.7	53.4
+50			4.6	53.5
62			4.2	53.9
+16			3.80	954.32 53.61
+50			4.1	54.0

£ July 20, 1960

8

Top MH £

S. Rim MH

49.1	49.0	51.0	53.1	54.0	53.6	50.7	50.4
9.0	9.1	7.1	5.0	4.1	4.5	7.4	7.7
50	44	30	21		20	26	40

Top MH £

Sta	+	π	-	Elev
		958.12 957.41		
63			3.9	54.2
+50			3.7	54.4
TP	7.80	962.08 961.37	3.84	953.57 954.28 957.11
BM	1.94	959.19 958.48	4.83	957.25 956.54 956.09
62+16			4.89	954.30 953.59 953.61
TP		967.11		954.99
59+16	12.12	966.40	4.20	959.28 954.24
57+66			4.81	962.30 961. 61+63
TP	13.63	979.92 979.21	0.82	966.29 965.58
55+80		X	5.17	78 974.75 972.86
BM			0.81	979.11 978.40 978.49
62+16	3.66	957.26		953.60 ?
61+00	{		9.45	947.81 ?
			10.60	946.66 ?

July 20, 1960

9

Spike in GP 20' Rt Sta 65+00

M H

M H

M H

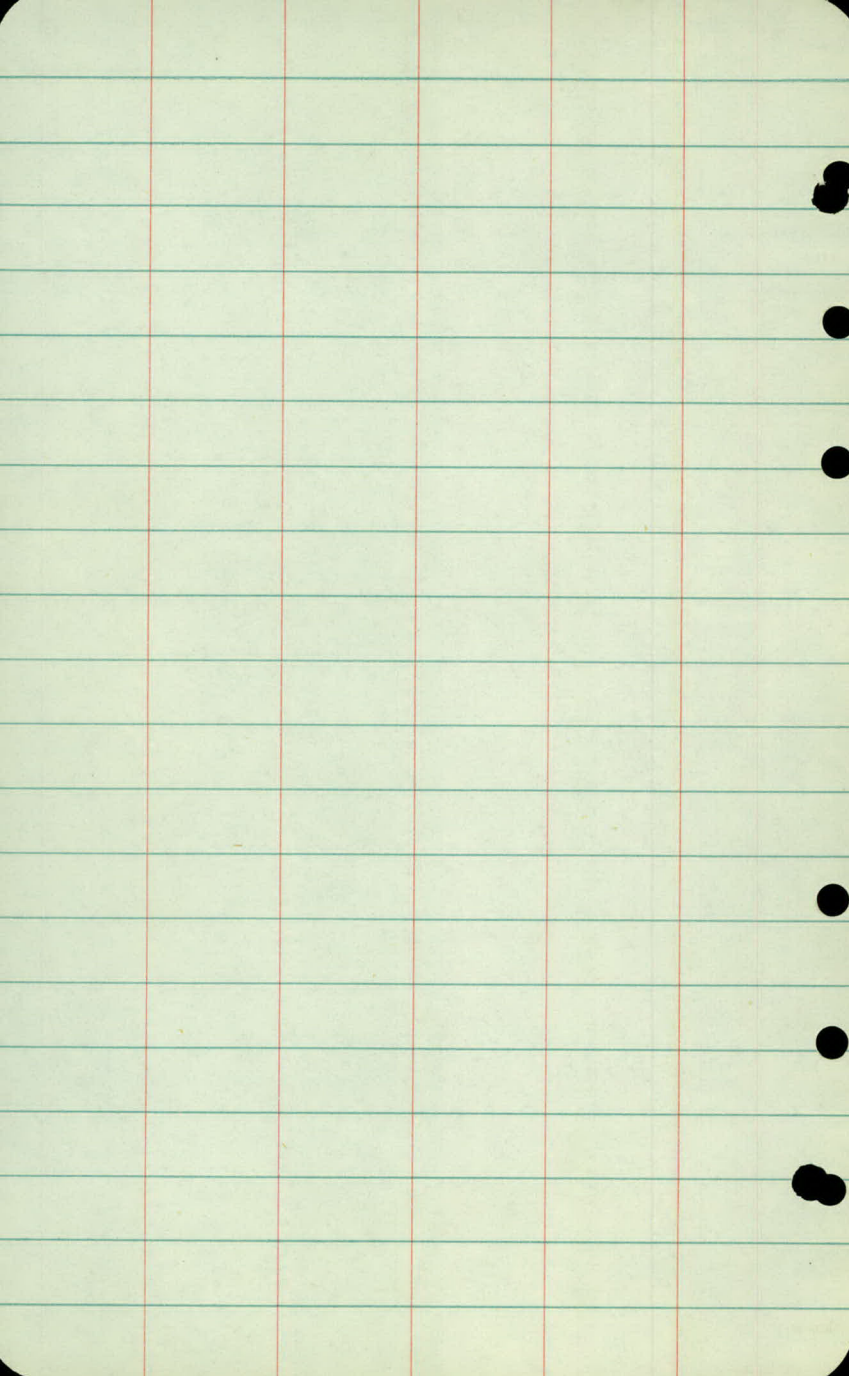
Spike in PP 30' Lt Sta 54+75

M H

FL inv E

FL inv W

} 36" X Drain



Additional Topography

48

47

46

+63 ^{MH}
61

+34 S.E. Cor Pump Sta
51

45

+07 End Conc Ent
36

+67 SW Cor Ho
104

+445 Rtre
Gav

+15 S.E. Cor Gav-Brez Ho
125

44

+30 S.W. Cor Ho
113

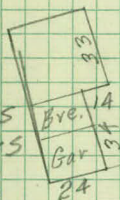
43

+01 MH
E

FK
JL
WM
RL
JH

July 11, 1960

11



53

$$+24 \text{ L.O.} + 29 \frac{\text{Wall}}{18}$$

52

$$+47 \frac{\text{S.E. Cor Ho.}}{68} \quad +47 \frac{\text{Cor Conc Ent}}{29}$$

51

$$+50 \frac{\text{SW Cor Ho.}}{62} \\ +43 \frac{\text{Cor Conc Ent}}{32} \\ +26 \frac{\text{Conc Ribbon Ent}}{28} \quad +34 \frac{\text{2' Wall}}{35}$$

50

$$+77 \frac{\text{Cor Conc Ent}}{30}$$

$$+75 \frac{\text{SE Cor Ho}}{67}$$

$$+88 \frac{\text{SW Cor Ho}}{64}$$

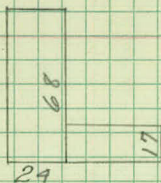
49

$$+95 \frac{\text{MH}}{2}$$

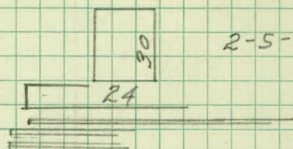
48

Rock Wall

1-5-5



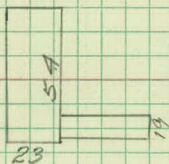
2-5-F



1 1/2-5-F



1-5-B



+ 45 $\frac{\text{Ent} \neq}{1+}$

55

154 $\frac{\text{Ent } 15" \times 20" \text{ CM}}{23}$

54

+30 $\frac{\text{SE Cor Ho}}{73}$

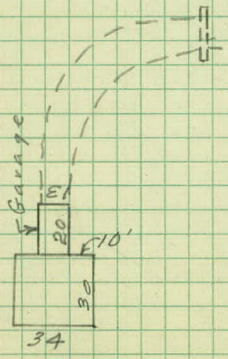
+19 $\frac{\text{Partially Used}}{\text{Ent}}$

53

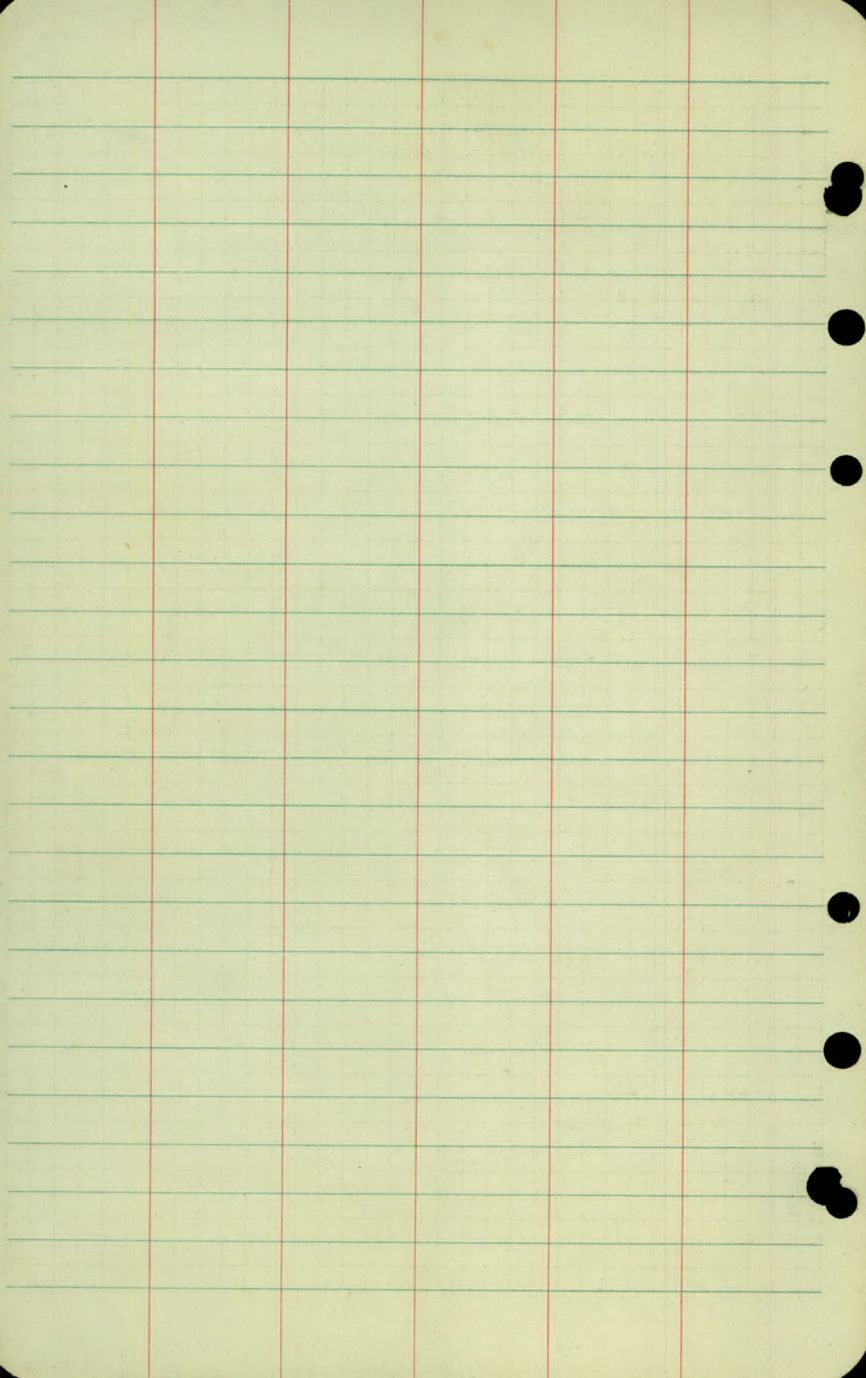
+05 $\frac{\text{M II}}{2}$

July 11, 1960

13



1-5-F

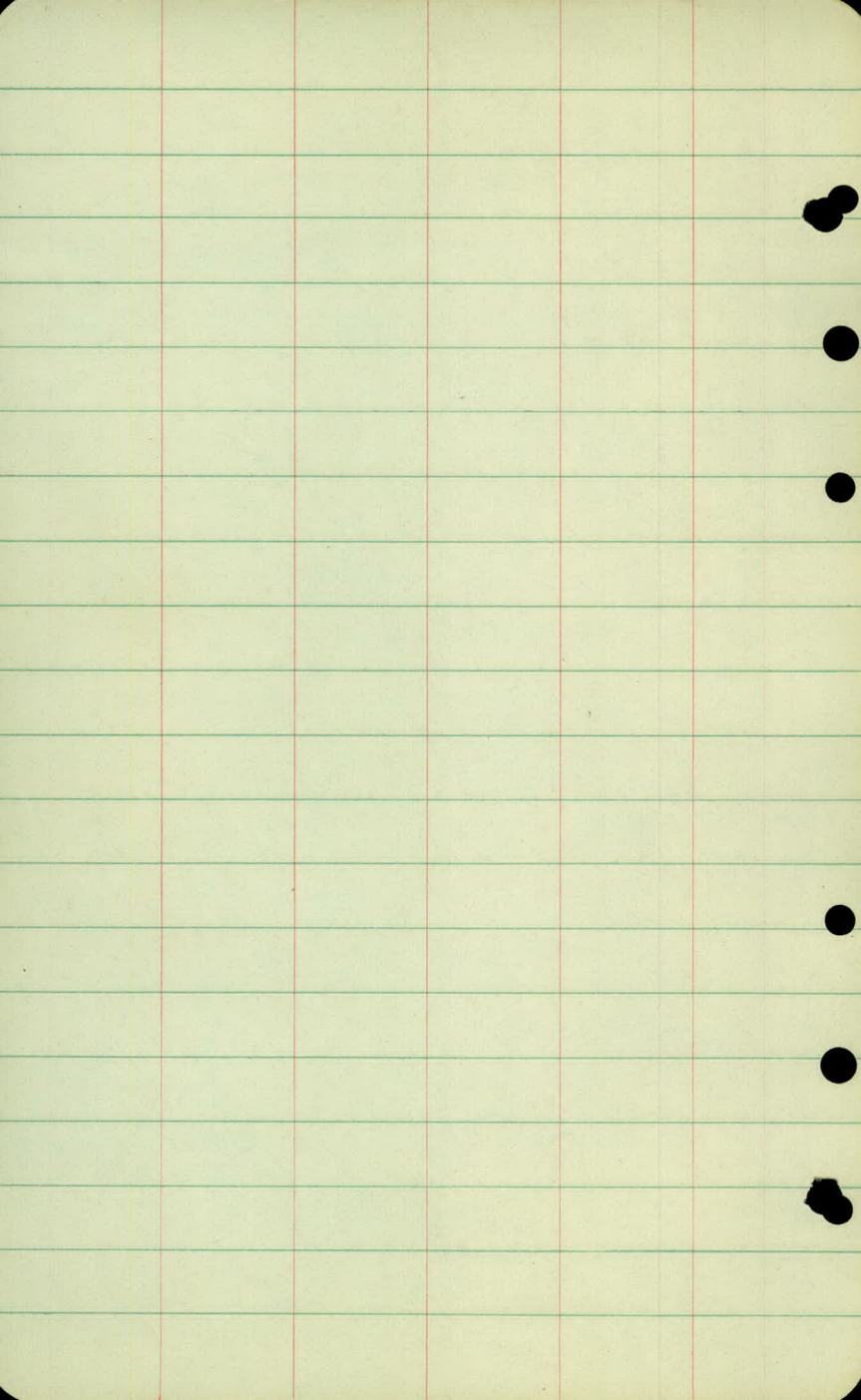


1
Beaver Lake

House Locations

Stationing same as East Ave Plan

3 pages



FK
AM
LC
MMc

May 27, 1954
60° Overcast, Damp

2

Locations

Sta

33+26 SW Cor Ho 90' Lt.

32+70 SW Cor Double Gar. 90' Lt.

30+73 SW Cor Ho 90' Lt.

29+85 SW Cor Ho 90' Lt.

29+10 SW Cor Ho 90' Lt.

Sta

67+90 NE Cor garage 45' Lt.

66+79 Double garage NE Cor. 35' Lt.

54+45 SE Cor Garage 180' Lt.

54+05 Range tie South side Ho Lt.

53+80 SE Cor Ho 200' Lt.

53+30 SE Cor Ho 70' Lt.

44+80 Range tie So side Ho.

44+60 SE Cor Ho 110' Lt.

Bear Lake

4

72+53 NE Cor Ho 45'

68+12 NE Cor Ho 60'