

Dr. 8 Bk. 160

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

----- PLAN ----- Survey

WHITE BEAR AVENUE

From Larpenteur to Prosperity Rd.

Road Acc't. No. 18-----

Date Filed 12-29-38

File-----

1

White Bear Ave.

Plan survey from
Larper Ave. to connection
with White Bear Road.

{ Bratger
Witte
Goldberg

7-38

Plot & div.
500' each side
of Forest Ave.

Refer to Road Map survey of
White Bear Ave. from Larper Ave.
to Co. Rd. "E". Road Acct. 18
File 10. Date filed 12-13-27

Angle.

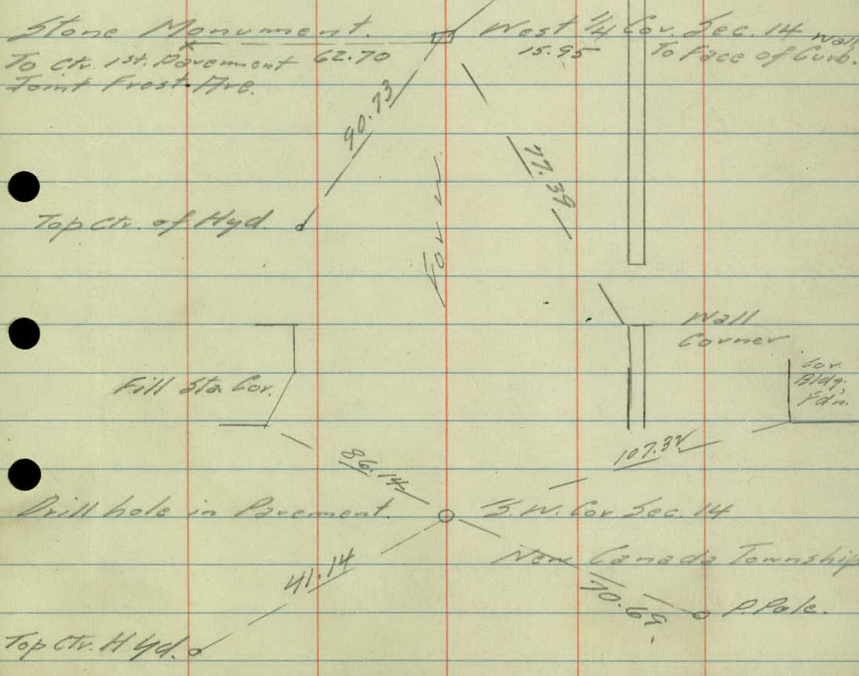
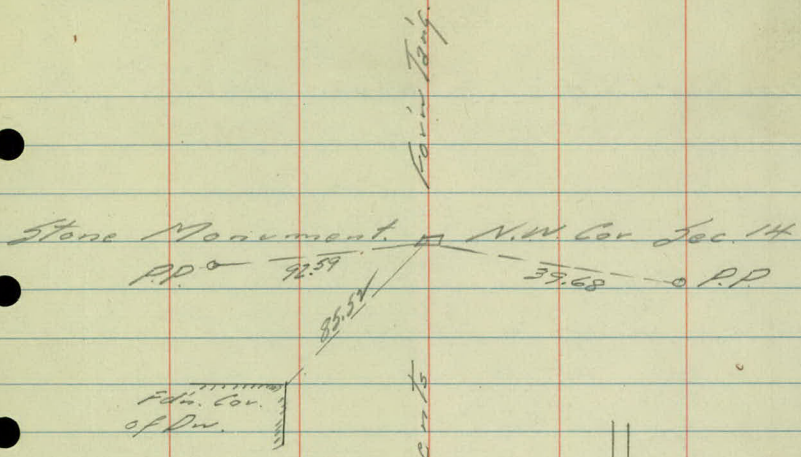
Sta. Point Left Right

52+72¹⁰ P.O.T.

36+23¹² P.I.

0°10'

0+00



Angle.

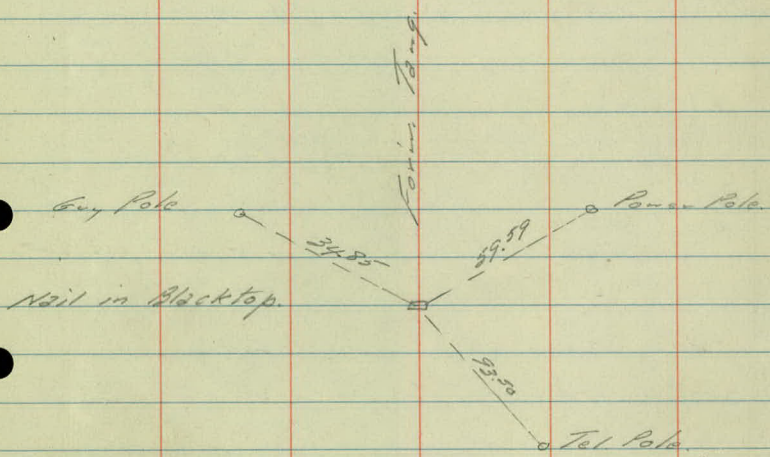
Sta. Point Left Right Defl.

The road bed is 24' conc. paving
to Sta. 28+10 narrowing to
20' at Sta. 29+10 to end.

62+70 ⁶⁵ P.T.	24°24'	
+50	22°20'	
62	17°20'	D=20° Rt.
61+57 ²⁵ P.I.	48°48'	T=130.6
+50	12°20'	C=244.°
61	7°20'	
+50	2°20'	
60+26 ⁶⁵ P.C.		

6270.65
6026.65
244

Reference Points



Guy Pole
3 nails

Tele. P.
3 nails

38+56 P.O.T.

Guy Pole
3 nails

Power Pole
3 nails

59.40

56.31

60.82

Topography

6

5

4

3

2

1

0

+40	Paving	55.64	80.7
+20	"	45.54	70.5
+20	End of Red.		
+13	"	"	43.0
4100	Paving	61.0	
+80	"	52.5	
+60	"	45.0	
+40	"	38.7	
+20	"	32.2	
2100	"	27.1	
+80	"	22.9	
+60	"	19.6	
+40	"	16.7	
+20	"	12+13.4	By Red.

24' Concrete

41.
 +50 Water shut off 9.7 2 feet pumps on
 +45 M. Hole, Water Dept. 24" lower 24 3' x 14" concrete base.
 +36 Water shut off 12" lower 9.5
 +31 Water shut off 12" lower 7.5

+85 R.P. 27.0

+34 T.P. 28.0

+60 = 15" x 20' C.M. 25.0

+06 T.P. 28.0

+86 End of yards

+58 Water shut off 41.0

+43 M.H. 16.0

+22 = 15" x 20' C.M. 23.0

+21 Rd. Sgn. 21.0

+17 Euy. Pole 20.0

+08 Manhole 15.0

+81 T.P. 29.0

+70 Rd. Sgn. 18.5

Entrance

+38 = 15" x 20' C.M. 24.0

+21 Water shut off 41.0

+15 Euy. Pole 20.0

+83 Beg. Lows 48.0

+17 End 10" C.M. 24.0

+16 = 3" x 4" 23.0

+03 Dr. 51.0

+00 End. rd. 16.29.0

+023 Angle Pt. 51.0

+047 Riv. Sta. 72.0

+037 8" Pipe Sgn. Full Sta. 24.0

+021 Drop Inlet 29.0 - 42" x 42" Stone

Carpenters Ave.

0-12 Drop Inlet 36.0

0-15 Rd. Sgn. 29.0

0-19 M.H. 7.5 Tel. Co. 15.0

0-37 4yd. 19.0

Paving

+70 Ed. Rl. 68

+24 Conc. Pavt. (Manhole) 32.5

+24 Manhole 27

+22 E. Pole 28

+13 R.P. 27.5

+09 Rd. Sgn. 26.0

+17 Ed. Rl. 16.0

+11 Ed. Rl. 36.5

+08 Ed. Rl. 30

+08 Ed. Rl. 25

+09 = 18" C.M. 23.5

+99 R.P. 47.0

+61 = 18" Maple

+65 Rd. Sgn. 25.0

+59 = 18" Conc. Pipe 27.5

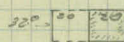
+36 Manhole 22.0

+32 = 24" Maple 34.0

+18 R.P. 27.0

+17 R.P. 27.0

+0184 Fr. Dr. 65.0



+134 Manhole 22.0

+34 Rd. Sgn. being remodelled

+27 R.P. 29.0

+27 1. Rd. Sgn. 29.0

20' Black Top.

13

12

11

10

9

8

7

6

Collected

+89 T.P. 28.0

+81 End Fc. 48.0

+84 = 26" Wood Picket Fc. 48.0

+59 T.P. 28.0

+21 T.P. 28.0

+54 T.P. 27.0

+51 Rd. Egn. 24.5

+60 T.P. 28

End in Grass but is plotted properly

End in Grass

+88 17.5x 24.0
+83 P.P. 27.0

+55 = 16" Tree 33

+93 = 10" Tree 38.0

+45 = 12" Oak 31.0

+18 P.P. 28.0

+72 Rd. Egn. 17.0

+23 Manhole 22.0

+41 P.P. 27.0

+65 P.P. 27.0

+93 Manhole 22.0
(Lower Missing)

19

18

17

16

15

14

See survey made short
time ago on N. R.R. Connection
for angle & location

13

12

+75 = 12' Entr.

+80 - U.S.G.S. Bench 34.0

+80 Manhole 18.0

+70 Rd. Spr. 22.0

+42 M. Box 16.0

+26 = 15" x 20' C.M. 23.0

+61 = 15" x 20' C.M. 24.0

+53 M. Box 15.0

+86 Entr. 10' Rd.

+66 Manhole 19.0

+29 T.P. 28.5

+23 Rd. Spr. 22.0

Fe. 33.0
+93 R.P. 28.0

+67 Rd. Spr. 26

+45 R.P. 28.0

Fe. 33.0

Fencing ex. m.
with metal posts

+97 R.P. 28.0

+14 = 12" Out. 27.0

Fe. 33.0

+59 = 12" Cok

+88 X Fe. 33.0

+62 = 12" Elm 35

Gate. Entr.

+42 R.P. 27.0

+39 = 15" x 26' C.M. 23.0

+41 3" Maple Tree 36.0

+24 = 4" Elm 36.0

Fencing

n.w. with

metal

posts.

+05 = 6' Elm 36.0

Fe. 34.5

+83 End Rod 14'

+58 Manhole 22.0

+61 Fe. Cor. 34.0

+44 Rd. Spr. 44.0

+45 Fe. Cor. 47.0

+32 Rod 60.0

N. 34.0 Conn. Black topped

+44 End Rod 50.0

+80 Beg. Rod 12.0

25

24

24' Rising 8" wall 14" Hi. to begin
conc. gutter betw
pavement & wall

+28 = 8' Elm 33°

23

22

21

20

19

County Pot
Grass.

+44 Beg Conc. Wall 15.4
+ End of curb

+ 91 Beg Curb + Cutter 12.⁰
+ 91 ¹⁰⁰ Dodge
+ 83 & 4 Cinc. Walk
+ 79 Beg Rod. 12.⁰

 $+60 = 10'' \text{ Elev } 30.0$

+54 End. Rod 38.0

Bl. Top Road. +51 Rd. 5945.34436

+ 35 End R2d. 44.0

+25 P.P. 28.0

+16 Fe. Cor. 33.0

+ 03 Beg. Rad. 12.^o
+ 03 = 12^o B. Cl. 34.^o

 $+59 = 10^\circ \text{ E/m } 30.0^\circ$

+ 22 = 8" E/m. 30.0

+0.8 Rd. 594.25.0

+94 R.P. 28.0

+33 = 12" Box El. 34

 $F_c = 33.0$
$$+55 = 6'' \text{ Elong } 34.0$$

+43 P.P. 28.0

+ 11 Rd. 59, 23.0

+ 94 Manhole 19.0

+ 87 End yards.

 $\phi 60 = 6''$ Lim 49.0

+28 = 6" Elms 49.0

+23 water. Shut off 41.0

20+00 = 6" Elev. 45.0

Double Entry.

$156 = 12'' \times 40' \text{ C.M. } 22.9$

 $+56 = 2'' \text{ Elms } 39.0$

+47 Water shut off 42?

 $108 = 3'' \text{ El. in } 39.0$

fencing n. or. with m. & 10 posts

12/12/2020

32

31

30

29

+10 Bcg. 20' Paving

+50 Paving 22.0

28

+10 Paving 24.0

27

Paving 24.0

Frost Pr. 20' Conc. Paving

26

25

20' Paving to end.

Fe 31.0

Field Entr. Gate

154 = 12" x 26' C.M. 20.0

+90 = 8" Trac 30.0

Cemetery
Pipe fencing with W. Wire

Entr. to Burns

Gate 12'

+41 Fe. 36.0

+21 = 18" x 30' C.M. 20.0

+04 P.P. 18.0

+06 End of Wall

Reg. fence

Gutter fills space
between paving & wall

Fe. 34.0

Wall 18.0

+34 P.P. 17.0

Fe 35.0

Face Wall 17.5

Wall 6' Hi.

Beta paving & wall

+50 End of Conc. gutter

Reg. pebble gutter

+45 Rd. Sign 16.0

Fe. 35

Posture

30' W. Fencing

Stonewalls

+75 P.P. 16.0

Fe. 51.0

Hedging stop wall

+30 Two W. Shut off 13.4

+29 W. Shut off 13.5

+27 W. Shut off 12.5

Wall Now 6' Hi.

16.5 out

Flament gutter

Paving to wall

+54 Reg. Rod 17.0

+65 Fe. 58.0

+63 Rd. Sign 34.0

+34 End Rd. 67.0

26' 23" of Post Rod.

+14 End Rod 67.0

+02 Rd. Sign 50.0

+93 P.P. 52.0

90° 22'

+76 18" x 110" Conc. Pipe 21.0

+64 Reg. Rod. 12.0

+04 Lg. Lt. Pole 15

+64 Hedge Cor 17

+60 Wall Cor 16

+49 Wall Cor. 16.0

+46 Hedge Cor 17.0

Entr. Steps up

+38 W. Shut off 10.0

+36 W. 27.0

County Bar Farm

39

38

12" Conc. H. W. 10' H.



37

36

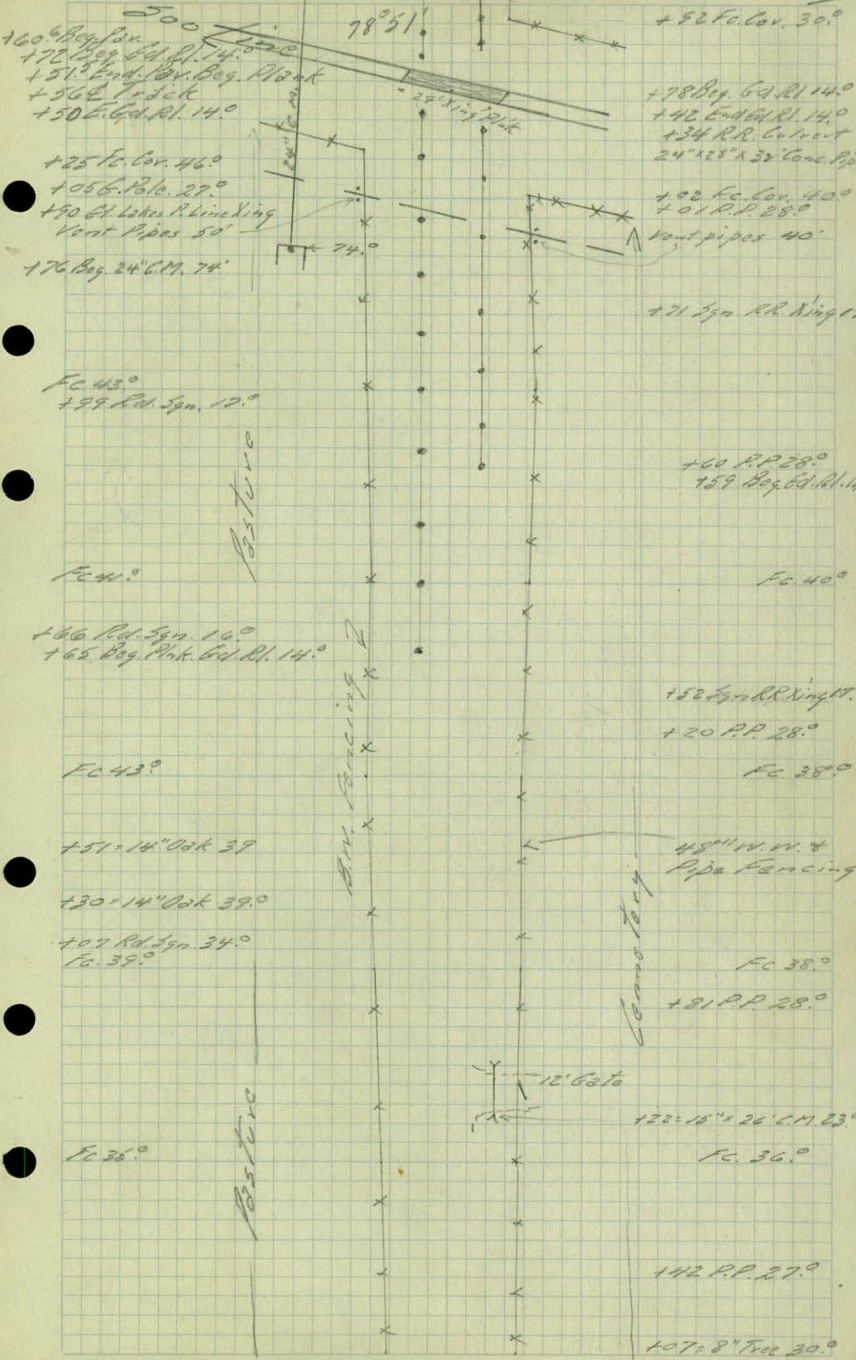
35

34

Reinment 20'

33

32



46

45

44

43

42

41



12" Conc. Walls, 9' High

40

39

B.W. Fencing →

+02 P.P. 28.0
Fc. 29.0

← B.W. Fencing

Fc. 32.0

+52 P.P. 28.0

Fc. 44.0

Fc. 29.0

+61 = 36" x 67' C.M.

34

Cultivated

Cultivated

+02 P.P. 28.0

+47 Rd. Sq. 16.0

Fc. 58.0

Fc. 29.0

+36 End. C.M. 41.0

+53 P.P. 28.0

Fc. 62.0

B.W. Fencing

B.W. Fencing

+39 Sq. R.P. 17.0

+19 Fc. Cor. 24.0
+076 Rd. 29.0

+05 P.P. 28.0
Fc. 30.0

52

51

50

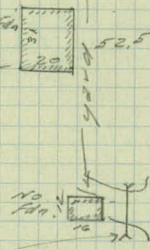
49

48

47

46

Conc. Block Fm
+79 Fr. Driveling 52.5
+62=12" B. El. 40.0
+46=8" B. El. 41.0
+25=6" B. Elder 41.0
+02 Fr. Garage 37.0
+92=12"x26" C.M. 22.0



Field Entry
+66=18"x20" C.M. 20.0



+39 Fc. Cor. 34.0

Cultivated

Fc. 33.0
+98 End. Ed. Al. 14.0

Fc. 37.0

+04 P.P. 28.0
Fc. 35.0

+54 P.P. 28.0

+91 Fc. 28.0
+91 Rd. 54 17.0

+02 P.P. 28.0

Fc. 28.0
+92 End. Ed. Al. 14.0

+22 P.P. 28.0

Scattered Trees & Brush

Cultivated

59

58

57

56

55

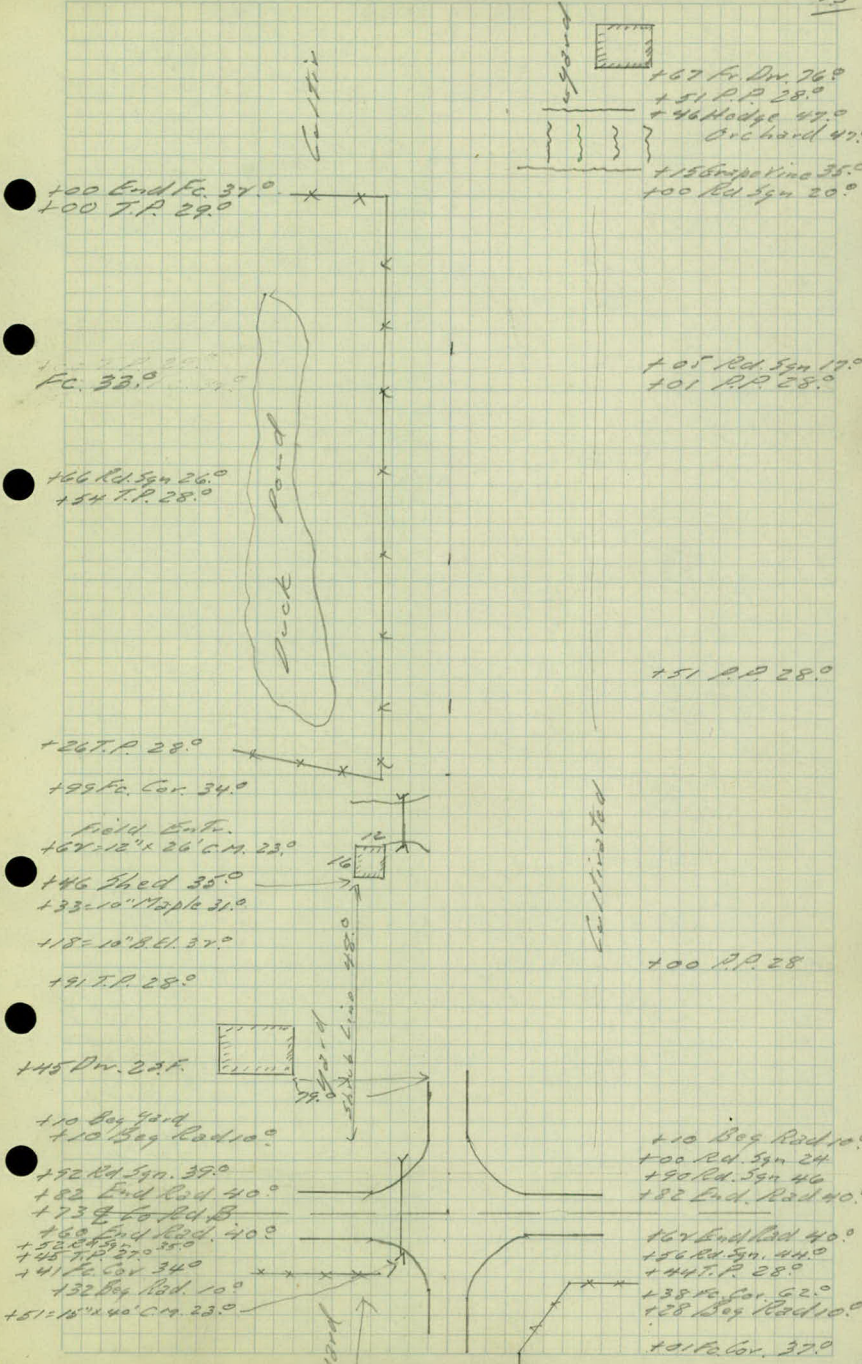
54

53

Co Rd "B" Blacktopped

52

20' Conc. Paving



64

63

62

61

60

59

+60 T.P. 28.0

+45 = 6" Oak 31.0
 +24 = 12" Oak 29.0
 +22.5 End Br. Curb.
 +20.5 E. Mid Transition
 +16 P.P. 29.0

+37 T.P. 29.0

+75 C. Pole 42.0
 +69 T.P. 44.0
 +58 Rd. Sign 35.0

+64 P.P. 29.0

Rd 63-38

+84 = 24" x 48' Conc. Pipe

10' Rd +14
 19 29
 11

+88 Driveway
 3' x 5'

+65 T.P. 36.0
 +50 Rd. 110-80

145-121

White Bear Rd.
 Blacktopped

Cultivated

+00 P.P. 27.0

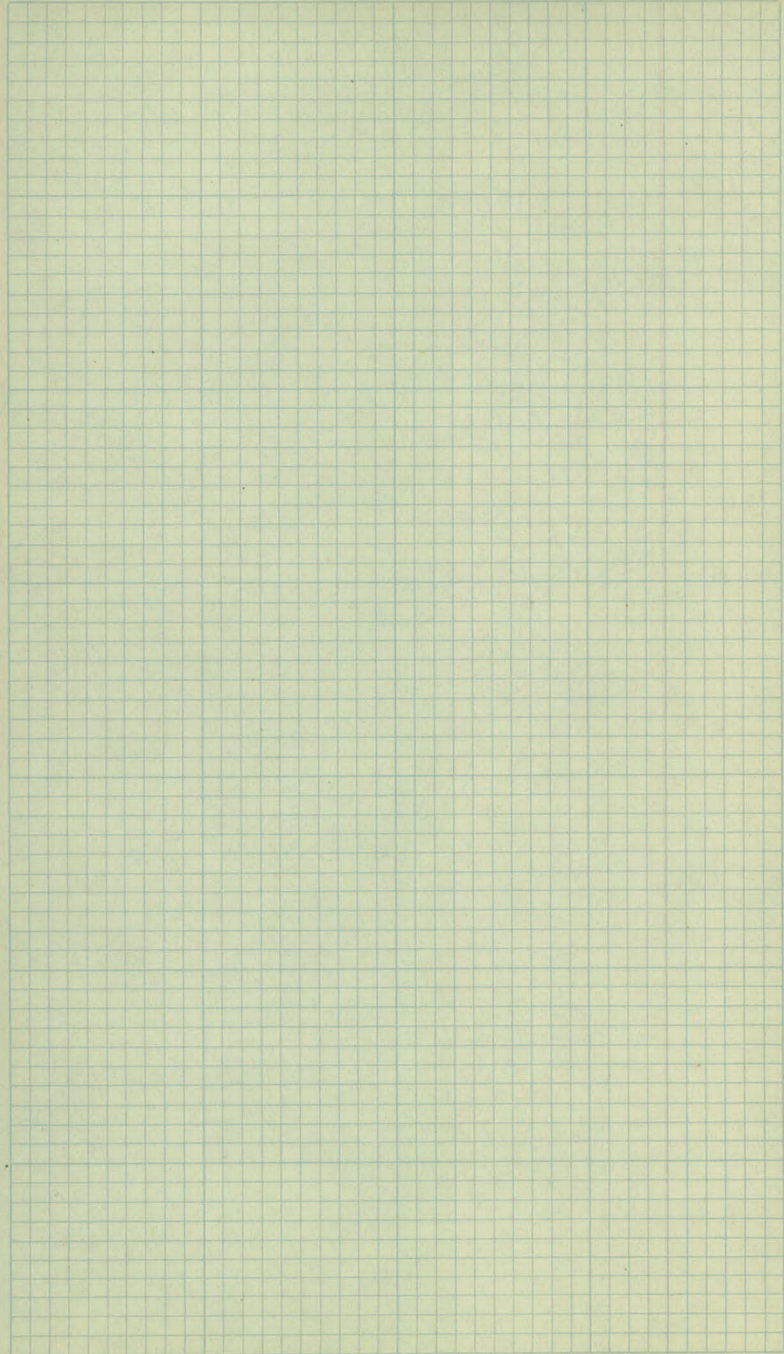
+76.5 - Beg W. de Transition
 +76 Beg Br. Curb.

+36 T.P. 34.0
 +22 = 6" B. Elder 33.0
 +02 = 8" B. Elder 33.0

yard

Ente.

+00 = 12" x 26' CM 22.0



Additional Topography at
500 Line Crossing

10+00 = P.I. Sta. 38+56

9+00

8+00

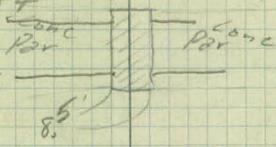
Note: Power Line adjacent to Hy
Sec 10p09
Power Co. for Voltage.

7+00

500
Ry. Co.

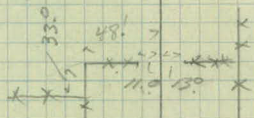
10+14.5 End Xing Plnt 4N

9+85 Beg Xing Plnt



9+60

East



+04 T.P. 38.0

50 37

+52 T.P. 38.2

Cultivated

R/W Fence

48.7

35

R/W Fence

waste

+19 Whistle Post 13.7

Cultivated

48.7 37.0

14+00

203 Defl. from
15+84 Back Tang.
14+84 4°48'
13+84 2°49'

13+00

+84 10°13' ↗

12+00

+84 0°24' ↗

11+00

+84 Beg Curve Lt. 00 ↘

10+00

+57 T.P. - 46.°

46.7

50.0

12+95

+90 Syn. R.R. King 14.5
1 mile

East

+35 T.P. - 37.°

42.8

47.8

R/W Fence

R/W Fence

+84 T.P. 37.°

46.7

46.°

Culvert

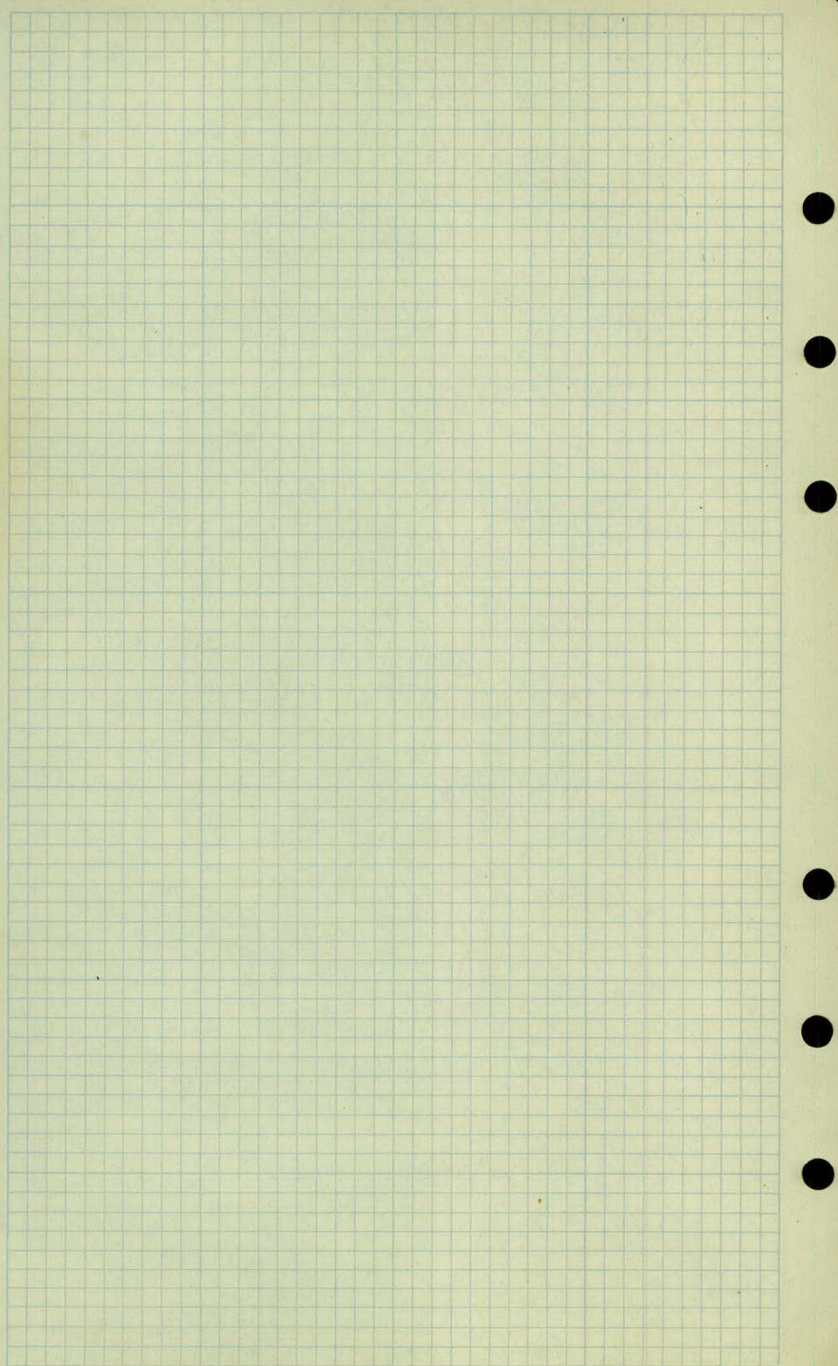
+47

18.7

176

10+26 - 3' Long

16.3



15
Bench Levels.

Sta.	+	π	-	Elev.
B.M.	8.10	950.07		941.97
T.P.	10.73	959.96	0.84	949.23
T.P.	12.19	971.65	0.50	959.46
B.M.	10.26	980.55	1.36	970.29
T.P.	2.07	975.90	6.72	973.83
B.M.	0.25	967.37	8.83	967.07
T.P.	0.08	953.63	13.77	953.55
T.P.	0.19	940.64	13.18	940.45
T.P.	0.78	928.49	12.93	927.71
T.P.	0.64	917.26	11.87	916.67
B.M.	9.79	917.22	9.83	907.43
T.P.	3.24	913.87	6.59	910.63
T.P.	11.43	925.18	0.12	913.75
B.M.	3.06	925.18	3.06	922.14
T.P.	6.37	929.99	1.56	923.67
B.M.			6.60	923.39

11

Description

Top Hyd. S.W. Cor. Corp. & W. Bear Ave.

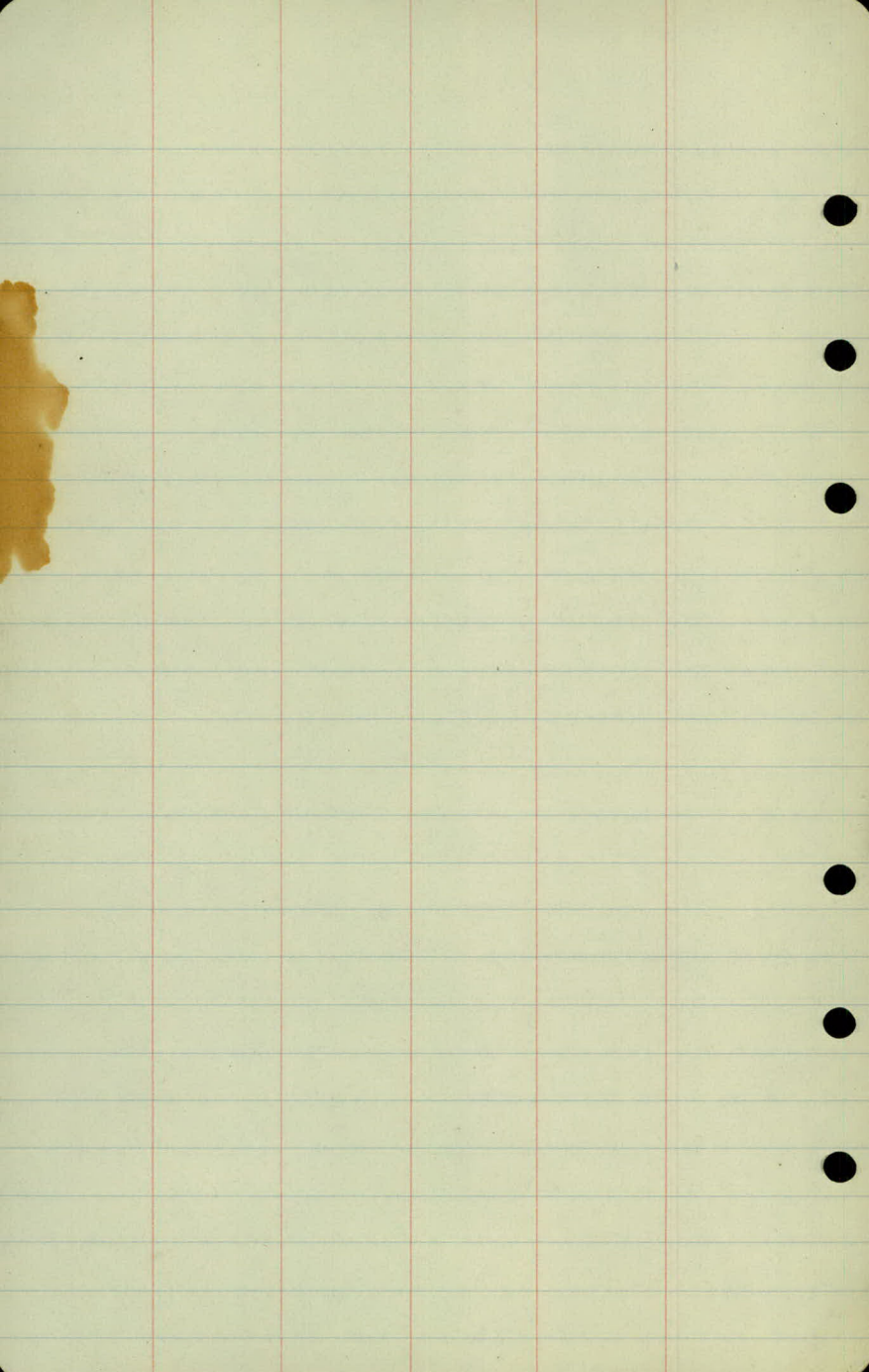
Top S.W. Cor. Slab Bottom of Stages Rt. 14+25 at Dwellings

Top Mont. & First & White Bear Ave. Sta 26+23.7

Top of N.E. Cor. No. End of East Wing Wall ^{Lt. 40+43}
cut out

Top of Mon. B & W. Bear Ave. Sta 57+72!

Top of ^{Gravement} curb, Rt. Sta. 60+26.65



Cross Sections

Sta.	+.	π	-	Elev.
B.M.	5.15	947.17		941.97

0+00				39.5
------	--	--	--	------

+50				40.8
-----	--	--	--	------

1+00				41.8
------	--	--	--	------

+50				42.8
-----	--	--	--	------

T.P.	9.52	951.49	5.15	941.97
------	------	--------	------	--------

1+17				
------	--	--	--	--

2+00				43.7
------	--	--	--	------

+35				44.4
-----	--	--	--	------

2+50		Drive Lt		44.6
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3+00				45.6
------	--	--	--	------

+32		Drive Lt		46.3
-----	--	----------	--	------

+30				46.6
-----	--	--	--	------

2+60 x		Went Rt. (see topog)		
--------	--	----------------------	--	--

Lt.

E

Rt.

Top of Hyd. S.W. Cor. Larp & W. Bear Arc.

$$\frac{5.9}{100} \quad \frac{6.3}{64} \quad \frac{6.6}{45} \quad \frac{7.6}{12} \quad \frac{7.8}{12} \quad \frac{7.7}{12} \quad \frac{6.6}{62} \quad \frac{6.5}{100}$$

$$\frac{5.6}{62} \quad \frac{6.0}{39} \quad \frac{6.5}{12} \quad \frac{6.3}{12} \quad \frac{6.4}{12} \quad \frac{6.7}{22} \quad \frac{6.0}{62} \quad \frac{6.9}{100}$$

$$\frac{2.8}{100} \quad \frac{2.7}{50} \quad \frac{5.5}{87} \quad \frac{5.7}{57} \quad \frac{5.8}{32} \quad \frac{5.5}{12} \quad \frac{5.3}{12} \quad \frac{5.4}{12} \quad \frac{5.9}{24} \quad \frac{5.6}{50} \quad \frac{5.2}{100}$$

$$\frac{2.3}{100} \quad \frac{4.5}{50} \quad \frac{4.5}{29} \quad \frac{6.9}{24} \quad \frac{6.3}{20} \quad \frac{4.5}{17} \quad \frac{4.6}{12} \quad \frac{4.3}{12} \quad \frac{4.5}{12} \quad \frac{4.8}{24} \quad \frac{4.6}{62} \quad \frac{4.9}{100}$$

39.19
123
 Forest Side Drain

$$\frac{7.0}{50} \quad \frac{7.8}{31} \quad \frac{7.8}{26} \quad \frac{11.3}{25} \quad \frac{10.6}{23} \quad \frac{10.2}{20} \quad \frac{8.1}{16} \quad \frac{8.0}{12} \quad \frac{7.8}{12} \quad \frac{8.0}{12} \quad \frac{8.1}{16} \quad \frac{8.9}{20} \quad \frac{8.7}{50} \quad \frac{8.4}{85} \quad \frac{7.9}{100}$$

$$\frac{4.9}{100}$$

$$\frac{3.8}{100} \quad \frac{5.7}{50} \quad \frac{6.9}{30} \quad \frac{9.8}{35} \quad \frac{9.6}{22} \quad \frac{7.2}{12} \quad \frac{7.3}{12} \quad \frac{7.2}{12} \quad \frac{7.2}{14} \quad \frac{7.2}{15} \quad \frac{7.2}{19} \quad \frac{7.7}{MH} \quad \frac{8.7}{26} \quad \frac{9.6}{28} \quad \frac{9.5}{30}$$

$$\frac{9.1}{100} \quad \frac{9.5}{50} \quad \frac{9.5}{44} \quad \frac{9.2}{32}$$

$$\frac{3.9}{100} \quad \frac{5.4}{50} \quad \frac{7.1}{12} \quad 6.9$$

$$\frac{1.3}{100} \quad \frac{4.3}{50} \quad \frac{4.3}{48} \quad \frac{5.2}{45} \quad \frac{6.3}{31} \quad \frac{9.4}{25} \quad \frac{9.4}{23} \quad \frac{6.3}{17} \quad \frac{6.0}{14} \quad \frac{6.1}{5.9} \quad \frac{6.3}{12} \quad \frac{5.9}{26} \quad \frac{6.1}{27} \quad \frac{7.2}{32} \quad \frac{7.8}{38} \quad \frac{7.3}{40} \quad \frac{7.7}{44} \quad \frac{6.1}{50} \quad \frac{5.6}{100}$$

$$\frac{1.2}{100} \quad \frac{4.5}{50} \quad \frac{4.9}{47} \quad \frac{5.3}{12} \quad 5.2$$

$$\frac{0.2}{10} \quad \frac{2.5}{65} \quad \frac{4.4}{50} \quad \frac{5.5}{46} \quad \frac{6.4}{31} \quad \frac{7.4}{26} \quad \frac{8.4}{22} \quad \frac{5.4}{16} \quad \frac{6.0}{14} \quad \frac{4.9}{12} \quad \frac{6.0}{14} \quad \frac{4.9}{18} \quad \frac{5.0}{29} \quad \frac{5.2}{39} \quad \frac{6.0}{40} \quad \frac{5.2}{45} \quad \frac{6.5}{57} \quad \frac{5.6}{45} \quad \frac{4.3}{80}$$

41.09
125
 104

Sta.	+	π	-	Elev.
		951.49		
3+85				47.4
4+00				47.8
4+11 ±	C.M. Culvert Rt (See Topog)			
4+14				48.0
T.P.	2.87	956.33	2.73	948.76
+50				48.8
+69 ±	Entr. Lt.			49.2
5+00				49.9
+50				51.0
6+00				52.3
T.P.	8.39	961.57	3.15	953.18
+50				53.3
7+00				54.4

4.

8

8.

$\frac{13}{100}$ $\frac{29}{65}$ $\frac{41}{80}$ $\frac{55}{47}$ $\frac{61}{31}$ $\frac{68}{27}$ $\frac{66}{21}$ $\frac{47}{16}$ $\frac{43}{14}$ $\frac{41}{14}$ $\frac{42}{14}$ $\frac{26}{29}$ $\frac{38}{41}$ $\frac{40}{53}$ $\frac{37}{54}$ $\frac{45}{57}$ $\frac{54}{70}$ $\frac{44}{72}$ $\frac{34}{72}$ ^{Exp.}

$\frac{33}{100}$ $\frac{60}{50}$ $\frac{66}{31}$ $\frac{62}{21}$ $\frac{44}{16}$ $\frac{40}{12}$ $\frac{37}{12}$ $\frac{29}{14}$ $\frac{28}{26}$ $\frac{30}{49}$ $\frac{33}{55}$ $\frac{21}{60}$ $\frac{37}{65}$ $\frac{47}{71}$ $\frac{49}{77}$ $\frac{40}{99}$ ^{Exp.}

$\frac{12}{70}$ 44, 49

$\frac{41}{100}$ $\frac{60}{50}$ $\frac{60}{39}$ $\frac{60}{23}$ $\frac{42}{16}$ $\frac{37}{14}$ $\frac{35}{14}$ $\frac{36}{14}$ $\frac{35}{18}$ $\frac{67}{23}$ $\frac{32}{31}$ $\frac{24}{35}$ $\frac{24}{41}$ $\frac{26}{53}$ $\frac{29}{64}$ $\frac{27}{65}$ $\frac{27}{71}$ ^P

$\frac{52}{100}$ $\frac{100}{75}$ $\frac{105}{50}$ $\frac{106}{32}$ $\frac{101}{21}$ $\frac{82}{16}$ $\frac{76}{14}$ $\frac{76}{14}$ $\frac{76}{19}$ $\frac{77}{23}$ $\frac{92}{27}$ $\frac{93}{28}$ $\frac{82}{33}$ $\frac{81}{47}$ $\frac{53}{55}$ $\frac{51}{55}$ $\frac{56}{72}$ $\frac{61}{83}$ <sup>88 50
84 90
P</sup>

$\frac{81}{100}$ $\frac{86}{50}$ $\frac{72}{14}$ $\frac{71}{14}$

$\frac{82}{100}$ $\frac{85}{75}$ $\frac{55}{75}$ $\frac{80}{50}$ $\frac{64}{35}$ $\frac{93}{28}$ $\frac{91}{12}$ $\frac{71}{16}$ $\frac{65}{14}$ $\frac{64}{14}$ $\frac{65}{14}$ $\frac{62}{19}$ $\frac{54}{22}$ $\frac{94}{25}$ $\frac{27}{30}$ $\frac{41}{35}$ $\frac{41}{44}$ $\frac{53}{50}$ $\frac{47}{64}$ $\frac{61}{68}$ $\frac{61}{72}$ $\frac{24}{83}$ $\frac{24}{90}$ }

$\frac{83}{100}$ $\frac{83}{80}$ $\frac{80}{32}$ $\frac{75}{14}$ $\frac{57}{17}$ $\frac{54}{12}$ $\frac{53}{14}$ $\frac{54}{14}$ $\frac{52}{16}$ $\frac{82}{23}$ $\frac{81}{25}$ $\frac{71}{29}$ $\frac{34}{34}$ $\frac{32}{50}$ $\frac{0.8}{100}$

$\frac{84}{100}$ $\frac{82}{44}$ $\frac{23}{24}$ $\frac{47}{17}$ $\frac{44}{14}$ $\frac{42}{14}$ $\frac{43}{14}$ $\frac{41}{17}$ $\frac{23}{23}$ $\frac{71}{28}$ $\frac{44}{35}$ $\frac{42}{60}$ $\frac{3.4}{100}$

$\frac{136}{100}$ $\frac{130}{50}$ $\frac{130}{31}$ $\frac{114}{24}$ $\frac{91}{17}$ $\frac{86}{14}$ $\frac{83}{14}$ $\frac{85}{14}$ $\frac{90}{18}$ $\frac{120}{22}$ $\frac{108}{29}$ $\frac{91}{34}$ $\frac{90}{50}$ $\frac{72}{72}$ $\frac{68}{100}$

$\frac{119}{100}$ $\frac{113}{50}$ $\frac{103}{31}$ $\frac{98}{24}$ $\frac{78}{16}$ $\frac{74}{14}$ $\frac{71}{14}$ $\frac{73}{14}$ $\frac{75}{17}$ $\frac{104}{22}$ ^{M.H. 83} $\frac{95}{30}$ $\frac{98}{33}$ $\frac{82}{60}$ $\frac{61}{100}$

Sta.	+	π	-	Elev.
		961.57		
7+50				55.4
8+00				56.5
T.P.	9.10	966.50	4.17	957.40
+50				57.4
9+00				58.3
+50				59.3
10+00				60.3
+50				61.3
T.P.	10.49	973.60	3.39	963.11
11+00				62.3
+50				63.3
12+00				64.4
+50				65.4
13+00				66.5

4.

2

2.

64 76 73 66 87 84 69 63 62 63 66 93 87 85 66 70 65
 100 80 50 31 25 22 17 14 6 14 19 23 25 30 25 50 100

20 27 39 46 76 76 87 82 51 52 58 82 76 76 82 58 39
 100 74 30 31 25 23 17 14 5 14 19 24 25 29 35 50 100

50 65 85 90 118 118 95 92 91 92 97 134 134 112 90 92 82
 100 25 50 31 26 22 16 14 9 14 18 21 23 29 33 50 75

67 75 78 90 108 108 88 84 82 83 90 115 120 102 95 96 94 87
 100 50 34 34 28 21 15 14 8 14 17 24 25 37 35 50 75 100

58 65 78 90 101 101 78 74 74 74 78 124 125 106 102 96 96 87
 100 75 50 31 27 23 16 14 7 14 16 24 24 25 33 36 50 75

38 53 65 83 81 87 68 64 62 63 68 98 97 92 92 83 80
 100 75 64 31 29 21 17 14 6 14 16 22 26 43 50 72 100

35 37 38 53 53 79 78 56 53 52 53 56 89 89 73 79 81 80
 100 88 75 50 30 26 22 17 14 5 14 16 21 25 34 50 75 100

10.3 108 111 136 138 116 114 113 114 115 148 140 132 143 160
 100 50 30 24 21 16 14 11 14 17 23 26 31 50 100

99 100 111 123 146 106 104 103 104 107 140 140 131 145 16.3
 100 50 34 27 24 16 14 10 14 19 21 23 26 50 100

80 88 92 117 117 98 94 94 94 100 121 121 122 153 169
 100 50 31 25 21 17 14 9 14 17 22 24 26 50 100

58 71 78 108 107 87 83 82 83 88 103 111 120 137 151 170
 100 50 33 25 21 16 14 8 14 16 24 25 31 41 50 100

60 64 73 86 86 74 72 71 71 71 72 90 100 130 141 141
 100 50 27 24 21 17 14 7 14 14 25 33 44 75 100

Sta.	+	π	-	Elev.
		973.60		
13+14	}			66.8
13+35				67.2
+43				67.4
14+00				68.8
B.M.	7.73	978.02	331	970.29
+50	Entr. Rt.			70.0
+65				70.4
15+00				71.1
+50				72.3
+72	Entr. Lt.			72.8
16+00				73.6
+35	Entr. Lt.			74.3
+50				74.6

Shoulders N. St. Paul Conn.

4.

8

12.

55 88 62 73 83 83 71 69 68 69 74 92 104
 100 50 37 25 23 20 17 14 12 12 27 50 100

82 81 52 74 78 67 64 64 64 72 89 96
 100 50 31 25 21 17 14 14 27 50 100

52 50 50 76 77 63 63 62 63 71 85 89 112
 100 50 31 24 20 16 12 14 25 36 50 100

+60± M.H. 700
 60

+52± M.H. 68

53 55 43 32 47 50 50 48 49 51 65 63 44 45 61 25
 100 75 30 44 28 18 14 14 16 19 26 31 34 41 62

Top S.W. Cor. slate slab at foot of Dwelling
 steps Rt. St. 14+25

80 81 81 76 63
 12 19 34 50

73 87 97 93 91 87 80 77 76 77 80 88 50 60 52 54 64
 100 88 62 50 46 22 16 14 14 18 22 24 30 50 75 100

50 62 79 86 83 72 70 69 70 71 84 86 60 56 80 54 61
 100 75 30 27 20 16 14 6 10 16 22 24 29 33 40 75 100

20 35 53 65 71 60 58 57 58 60 25 77 67 57 54 58
 100 75 60 31 21 17 14 12 16 22 28 33 41 83 100

20 46 53 53 52
 100 60 75 14 5

12 16 25 26 50 59 59 47 45 44 45 48 70 78 77 77 74 70 61
 100 88 75 60 29 26 19 16 14 14 16 22 29 30 33 38 60 100

35 40 38 31
 50 27 14 3

19 27 36 39 49 52 35 35 36 39 64 72 75 76
 100 75 50 38 25 21 17 14 14 16 23 33 60 100

Sta.	+	K	-	Elev.
		97804		

T.P.	8.94	984.20	2.76	975.26
------	------	--------	------	--------

17+00				75.3'
-------	--	--	--	-------

+50				75.7'
-----	--	--	--	-------

18+00				76.0'
-------	--	--	--	-------

+50				76.0'
-----	--	--	--	-------

+75	Entr Lt.			75.9'
-----	----------	--	--	-------

19+00				75.7'
-------	--	--	--	-------

+50				75.2'
-----	--	--	--	-------

+80	Entr Lt.			75.0'
-----	----------	--	--	-------

20+00				74.7'
-------	--	--	--	-------

T.P.	2.86	980.81	6.25	977.85
------	------	--------	------	--------

+50				74.3'
-----	--	--	--	-------

21+00				73.8'
-------	--	--	--	-------

+50				73.3'
-----	--	--	--	-------

Lt.

E

Rt

$\frac{72}{100} \frac{74}{85} \frac{61}{50} \frac{58}{37} \frac{101}{26} \frac{104}{20} \frac{92}{17} \frac{90}{14} \frac{89}{11} \frac{90}{14} \frac{95}{16} \frac{114}{21} \frac{114}{25} \frac{101}{33} \frac{104}{35} \frac{112}{38} \frac{128}{60} \frac{144}{100}$

$\frac{50}{100} \frac{57}{85} \frac{55}{50} \frac{51}{38} \frac{91}{26} \frac{97}{21} \frac{90}{17} \frac{86}{14} \frac{85}{11} \frac{86}{14} \frac{90}{16} \frac{107}{24} \frac{107}{26} \frac{81}{31} \frac{83}{33} \frac{83}{38} \frac{92}{100}$

181 M.H. Lt. 2 Canev
86

$\frac{14}{100} \frac{30}{75} \frac{44}{48} \frac{53}{33} \frac{56}{26} \frac{56}{17} \frac{83}{14} \frac{82}{11} \frac{83}{14} \frac{87}{16} \frac{103}{21} \frac{105}{25} \frac{82}{30} \frac{78}{33} \frac{77}{38} \frac{89}{107} \frac{140}{100}$

$\frac{13}{100} \frac{39}{64} \frac{42}{50} \frac{45}{35} \frac{84}{27} \frac{88}{23} \frac{85}{17} \frac{83}{14} \frac{82}{11} \frac{83}{14} \frac{88}{17} \frac{102}{21} \frac{103}{23} \frac{75}{33} \frac{75}{35} \frac{85}{38} \frac{100}{59} \frac{145}{100}$

$\frac{13}{100} \frac{50}{50} \frac{54}{14} \frac{83}{8}$

$\frac{26}{100} \frac{57}{50} \frac{67}{33} \frac{81}{26} \frac{86}{14} \frac{85}{11} \frac{86}{14} \frac{90}{17} \frac{105}{21} \frac{106}{24} \frac{75}{32} \frac{75}{35} \frac{90}{39} \frac{100}{54} \frac{150}{100}$

$\frac{30}{100} \frac{67}{50} \frac{77}{35} \frac{87}{29} \frac{93}{23} \frac{91}{14} \frac{90}{11} \frac{91}{14} \frac{94}{17} \frac{113}{21} \frac{113}{25} \frac{94}{31} \frac{89}{35} \frac{112}{39} \frac{131}{63} \frac{150}{100}$

$\frac{39}{100} \frac{71}{50} \frac{94}{14} \frac{92}{8}$

$\frac{45}{100} \frac{78}{50} \frac{86}{31} \frac{105}{25} \frac{106}{20} \frac{100}{16} \frac{97}{14} \frac{95}{11} \frac{96}{14} \frac{100}{15} \frac{123}{20} \frac{126}{25} \frac{115}{31} \frac{118}{35} \frac{127}{40} \frac{148}{100}$

$\frac{25}{100} \frac{48}{50} \frac{66}{30} \frac{77}{25} \frac{78}{19} \frac{69}{16} \frac{66}{14} \frac{65}{11} \frac{67}{14} \frac{69}{15} \frac{96}{21} \frac{107}{33} \frac{111}{36} \frac{120}{41} \frac{116}{69} \frac{109}{100}$

$\frac{26}{100} \frac{47}{50} \frac{57}{35} \frac{85}{26} \frac{88}{20} \frac{73}{16} \frac{71}{14} \frac{70}{11} \frac{72}{14} \frac{74}{16} \frac{109}{21} \frac{116}{33} \frac{123}{37} \frac{128}{43} \frac{128}{100}$

493 M.H.

$\frac{87}{100} \frac{44}{50} \frac{68}{33} \frac{69}{27} \frac{90}{20} \frac{92}{16} \frac{80}{14} \frac{77}{11} \frac{75}{14} \frac{77}{16} \frac{80}{21} \frac{123}{33} \frac{130}{37} \frac{133}{100}$

Sta.	+	π	-	Elev.
		980.81		
22+00				72.7
T.P.	6.57	978.74	8.64	977.17
+50				72.2
23+00				71.7
+25				71.4
+35				71.3
+53				71.1
+59				71.1
+83				70.9
T.P.	7.50	978.63	7.61	971.13
24+00				70.8
+50				70.1
25+00				69.9
+40				68.7

Lt.

E

Rt.

23

$\frac{5.1}{100}$ $\frac{6.0}{50}$ $\frac{7.2}{33}$ $\frac{8.8}{26}$ $\frac{9.5}{22}$ $\frac{8.3}{16}$ $\frac{8.2}{14}$ $\frac{8.1}{14}$ $\frac{8.2}{14}$ $\frac{8.6}{15}$ $\frac{12.6}{24}$ $\frac{13.1}{23}$ $\frac{13.1}{26}$ $\frac{13.6}{27}$ $\frac{13.8}{100}$

$\frac{3.7}{100}$ $\frac{4.0}{80}$ $\frac{4.7}{50}$ $\frac{5.9}{33}$ $\frac{7.7}{28}$ $\frac{8.8}{23}$ $\frac{2.1}{18}$ $\frac{6.6}{14}$ $\frac{6.5}{14}$ $\frac{6.7}{14}$ $\frac{7.2}{16}$ $\frac{10.8}{23}$ $\frac{11.5}{33}$ $\frac{11.9}{50}$ $\frac{11.4}{100}$

$\frac{5.4}{100}$ $\frac{5.6}{64}$ $\frac{7.1}{46}$ $\frac{7.6}{24}$ $\frac{8.5}{28}$ $\frac{9.1}{21}$ $\frac{7.7}{17}$ $\frac{7.1}{14}$ $\frac{7.0}{14}$ $\frac{7.1}{14}$ $\frac{7.8}{17}$ $\frac{10.8}{24}$ $\frac{11.4}{33}$ $\frac{11.8}{23}$ $\frac{11.6}{100}$

$\frac{6.4}{100}$ $\frac{6.6}{50}$ $\frac{7.5}{50}$ $\frac{8.5}{33}$ $\frac{9.1}{28}$ $\frac{9.0}{20}$ $\frac{7.8}{17}$ $\frac{7.4}{14}$ $\frac{7.3}{14}$ $\frac{7.4}{14}$ $\frac{7.8}{22}$ $\frac{10.3}{29}$ $\frac{11.5}{30}$ $\frac{11.5}{100}$

$\frac{7.1}{100}$ $\frac{7.4}{75}$ $\frac{8.1}{50}$ $\frac{8.8}{33}$ $\frac{8.2}{30}$ $\frac{8.2}{21}$ $\frac{7.8}{17}$ $\frac{7.5}{14}$ $\frac{7.4}{14}$ $\frac{7.4}{10}$ $\frac{7.2}{14}$ $\frac{7.8}{35}$ $\frac{8.4}{50}$ $\frac{9.4}{100}$

Shoulder

$\frac{8.6}{100}$ $\frac{9.0}{80}$ $\frac{9.5}{34}$ $\frac{8.7}{20}$ $\frac{7.7}{14}$ $\frac{7.7}{14}$ $\frac{7.6}{10}$ $\frac{7.6}{14}$ $\frac{7.4}{14}$ $\frac{7.8}{33}$ $\frac{8.4}{50}$ $\frac{9.3}{100}$

$\frac{8.8}{100}$ $\frac{9.2}{55}$ $\frac{9.7}{46}$ $\frac{9.2}{20}$ $\frac{7.9}{18}$ $\frac{7.7}{14}$ $\frac{7.6}{14}$ $\frac{7.7}{14}$ $\frac{8.0}{26}$ $\frac{8.8}{41}$ $\frac{9.5}{62}$ $\frac{10.4}{100}$

$\frac{9.0}{100}$ $\frac{9.9}{50}$ $\frac{9.6}{34}$ $\frac{10.2}{36}$ $\frac{8.8}{19}$ $\frac{7.8}{15}$ $\frac{8.0}{14}$ $\frac{7.8}{14}$ $\frac{7.8}{14}$ $\frac{7.8}{14}$ $\frac{7.8}{26}$ $\frac{7.8}{100}$

Wrist Rt.

$\frac{9.1}{100}$ $\frac{9.6}{50}$ $\frac{9.1}{20}$ $\frac{8.1}{15}$ $\frac{8.0}{14}$ $\frac{7.8}{14}$ $\frac{7.8}{14}$ $\frac{7.5}{13}$ $\frac{7.5}{13}$ $\frac{7.1}{100}$

$\frac{8.1}{100}$ $\frac{7.4}{50}$ $\frac{7.2}{33}$ $\frac{9.8}{24}$ $\frac{8.7}{21}$ $\frac{8.7}{17}$ $\frac{8.6}{14}$ $\frac{8.5}{14}$ $\frac{8.5}{14}$ $\frac{8.6}{13.5}$ $\frac{8.5}{15}$ $\frac{6.6}{14}$ $\frac{6.8}{100}$

$\frac{8.7}{100}$ $\frac{4.7}{70}$ $\frac{5.5}{50}$ $\frac{6.3}{36}$ $\frac{10.2}{24}$ $\frac{10.3}{24}$ $\frac{9.6}{18}$ $\frac{9.3}{14}$ $\frac{9.2}{14}$ $\frac{9.2}{14}$ $\frac{9.3}{14}$ $\frac{9.2}{14}$ $\frac{6.6}{14}$ $\frac{6.2}{100}$

$\frac{6.3}{100}$ $\frac{5.4}{50}$ $\frac{7.6}{41}$ $\frac{7.5}{36}$ $\frac{10.3}{25}$ $\frac{10.6}{21}$ $\frac{10.0}{14}$ $\frac{9.9}{14}$ $\frac{9.9}{14}$ $\frac{10.0}{14}$ $\frac{9.9}{14}$ $\frac{9.9}{14}$ $\frac{9.9}{14}$ $\frac{6.1}{100}$

Sta.	+	π	-	Elev.
		978.63		
25+65				68.3
+75				
+90				67.8
+95				67.7
26+04				67.6
26+23.7 $\frac{1}{2}$ Frost Lt.				67.0
+44				66.5
+52				66.2
+61				66.0
+85				
13. M	8.24	975.31	11.56	767.07
27+00				64.8
+50				63.1
28+00				61.3

4.

E

Et.

24

68
100

69 80 88 118 119 106 104 103 103 105 104 65 62
50 50 50 22 20 17 14 12 13.5 15.5 16 100

0.005 Pipe Lt

13.5

14.4 13.7 13.0 11.2 10.9 10.9 10.5 11.0 10.9 6.5 63
100 50 39 32 19 12 10.8 12 13.5 15.5 16 100

14.4 13.3 11.0 11.1 11.0 10.9 11.1 11.0 6.5 63
100 50 38 24 12 10.9 12 13.5 15.5 16 100

12.7 11.6 11.2 11.1 11.1 11.3 11.1 6.5 6.3
100 50 32 12 11.0 12 13.5 15.5 16 100

12.3 11.9 11.7 11.2 11.2 11.8 11.2 6.5 5.7 63
100 50 12 11.2 12 13.5 15.5 16 5.0 100

12.1 11.7 12.3 12.2 12.2 12.3 12.2 6.5 6.0
100 50 39 12 12 12 13.5 15.5 16 5.5

14.2 14.0 12.2 12.7 12.7 12.5 12.4 12.5 12.5 6.7 6.0
100 5 40 30 24 12 12.4 12 13.5 15.5 16 5.5

14.0 14.1 14.2 12.4 12.8 12.7 12.4 12.8 12.4 6.8 6.0
100 50 40 31 18 12 12.2 12 13.5 15.5 16 6.5

15.8

Invert Corrupt

Top Mont Frost & White Bear Aug

4.7 4.9 8.0 10.8 12.2 10.6 10.6 10.5 10.6 10.7 10.6 4.6 3.6
100 47 50 93 22 18 14 14 14 14 16 16.5 100

5.3 4.4 10.8 12.8 13.4 13.4 12.3 12.2 12.2 12.2 12.3 12.2 6.0 4.1
100 50 31 21 23 21 14 14 14 14 14 16 16.5 100

5.8 6.4 6.9 11.9 14.9 14.9 14.0 14.0 14.1 13.5 7.7 5.3
100 50 30 21 21 18 14 14 14 14 17 17.5 100

Sta. + π - Elev.

975.31

T.P. 9.68 971.73 ✓ 13.26 962.05 ✓

28+50

59.7

57.8

29+00

T.P. 8.75 966.77 ✓ 13.71 958.02 ✓

+50

56.0

30+00

54.4 ✓

T.P. 6.62 ✓ 960.39 ✓ 13.00 953.77

+50

52.6

31+00

50.9

+06

50.6

+06

50.6

+50.

49.0 ✓

T.P. 3.72 ✓ 957.83 ✓ 11.28 949.11

+75

94.7.9

32

46.9

+50

44.9

Lt.

E

Rt

$\frac{43}{100}$ $\frac{39}{75}$ $\frac{34}{50}$ $\frac{26}{34}$ $\frac{128}{23}$ $\frac{129}{19}$ $\frac{124}{19}$ $\frac{121}{11}$ $\frac{120}{11}$ $\frac{121}{11}$ $\frac{124}{14}$ $\frac{121}{17}$ $\frac{61}{175}$ $\frac{33}{100}$

$\frac{66}{100}$ $\frac{57}{75}$ $\frac{40}{34}$ $\frac{71}{33}$ $\frac{145}{21}$ $\frac{145}{19}$ $\frac{143}{16}$ $\frac{140}{10}$ $\frac{139}{10}$ $\frac{140}{125}$ $\frac{151}{15}$ $\frac{151}{17}$ $\frac{140}{175}$ $\frac{82}{100}$ $\frac{48}{100}$

$\frac{31}{100}$ $\frac{37}{70}$ $\frac{32}{50}$ $\frac{20}{33}$ $\frac{118}{22}$ $\frac{118}{18}$ $\frac{111}{14}$ $\frac{109}{10}$ $\frac{108}{10}$ $\frac{108}{13}$ $\frac{119}{15}$ $\frac{119}{18}$ $\frac{111}{18}$ $\frac{55}{180}$ $\frac{10}{100}$

$\frac{79}{100}$ $\frac{80}{50}$ $\frac{56}{31}$ $\frac{136}{23}$ $\frac{136}{19}$ $\frac{127}{16}$ $\frac{125}{10}$ $\frac{124}{10}$ $\frac{125}{10}$ $\frac{136}{13}$ $\frac{136}{15}$ $\frac{126}{18}$ $\frac{73}{18}$ $\frac{35}{100}$

$\frac{61}{100}$ $\frac{48}{60}$ $\frac{39}{50}$ $\frac{25}{31}$ $\frac{90}{23}$ $\frac{92}{20}$ $\frac{81}{16}$ $\frac{78}{10}$ $\frac{78}{10}$ $\frac{79}{13}$ $\frac{90}{15}$ $\frac{90}{18}$ $\frac{81}{18}$ $\frac{30}{18}$ $\frac{+08}{100}$

$\frac{80}{100}$ $\frac{85}{75}$ $\frac{64}{50}$ $\frac{47}{31}$ $\frac{108}{22}$ $\frac{110}{19}$ $\frac{98}{16}$ $\frac{96}{10}$ $\frac{95}{10}$ $\frac{96}{13}$ $\frac{106}{16}$ $\frac{106}{19}$ $\frac{99}{19}$ $\frac{50}{19}$ $\frac{28}{80}$ $\frac{+08}{100}$

$\frac{83}{100}$ $\frac{86}{75}$ $\frac{59}{36}$ $\frac{50}{31}$ $\frac{110}{22}$ $\frac{112}{20}$ $\frac{100}{17}$ $\frac{99}{10}$ $\frac{98}{10}$ $\frac{99}{14}$ $\frac{106}{14}$ $\frac{106}{18}$ $\frac{51}{25}$ $\frac{28}{50}$ $\frac{117}{100}$

$\frac{93}{100}$ $\frac{86}{75}$ $\frac{59}{36}$ $\frac{50}{31}$ $\frac{110}{22}$ $\frac{112}{20}$ $\frac{100}{17}$ $\frac{99}{10}$ $\frac{98}{10}$ $\frac{99}{14}$ $\frac{106}{14}$ $\frac{106}{18}$ $\frac{51}{25}$ $\frac{28}{50}$ $\frac{08}{100}$

$\frac{118}{100}$ $\frac{138}{75}$ $\frac{124}{50}$ $\frac{107}{33}$ $\frac{125}{22}$ $\frac{125}{19}$ $\frac{120}{15}$ $\frac{115}{10}$ $\frac{114}{10}$ $\frac{115}{15}$ $\frac{114}{20}$ $\frac{120}{23}$ $\frac{120}{28}$ $\frac{106}{37}$ $\frac{94}{50}$ $\frac{76}{50}$ $\frac{44}{100}$

$\frac{73}{100}$ $\frac{66}{80}$ $\frac{41}{31}$ $\frac{48}{24}$ $\frac{56}{24}$ $\frac{50}{10}$ $\frac{49}{10}$ $\frac{50}{17}$ $\frac{49}{27}$ $\frac{34}{33}$ $\frac{34}{39}$ $\frac{54}{44}$ $\frac{71}{64}$ $\frac{22}{83}$ $\frac{+01}{100}$

$\frac{76}{100}$ $\frac{71}{75}$ $\frac{65}{50}$ $\frac{37}{31}$ $\frac{71}{23}$ $\frac{72}{18}$ $\frac{61}{14}$ $\frac{69}{10}$ $\frac{59}{10}$ $\frac{60}{10}$ $\frac{61}{14}$ $\frac{63}{18}$ $\frac{61}{24}$ $\frac{48}{33}$ $\frac{45}{39}$ $\frac{63}{45}$ $\frac{88}{64}$ $\frac{92}{90}$ $\frac{93}{100}$

$\frac{75}{100}$ $\frac{75}{90}$ $\frac{61}{90}$ $\frac{44}{50}$ $\frac{33}{31}$ $\frac{84}{24}$ $\frac{87}{17}$ $\frac{81}{14}$ $\frac{80}{10}$ $\frac{79}{10}$ $\frac{80}{10}$ $\frac{84}{16}$ $\frac{95}{16}$ $\frac{96}{27}$ $\frac{48}{33}$ $\frac{61}{44}$ $\frac{96}{69}$ $\frac{107}{100}$

Sta. + π - Elev.

957.83

33 943.0

+50 41.1

T.P. 7.45 947.89 13.39 940.44

+80 40.0

34+00 39.2

+35 37.9

+80 36.2

35 35.3

+50 33.2

+70 32.4

T.P. 1.04 935.47 13.46 934.43

36 31.4

+10 31.0

+30 30.2

LH

E

RH

26

76 52 39 43 115 114 100 98 98 98 103 113 114 86 98 11 106 94 100
 100 75 80 34 25 18 14 10 10 15 18 26 31 36 49 64 84 100

53
 88 58 68 21 77 77 143 136 119 118 117 117 127 138 141 137 120 112 103 21
 100 75 80 37 28 31 23 20 14 10 11 10 16 21 23 31 37 60 84 100

124 82 68 72 64 64 64 56 55 82 80 79 80 83 109 108 82 74 60 33 43 26
 100 84 61 50 41 38 35 27 19 14 10 10 13 19 26 34 37 50 77 94 100

114 00 73 84 85 107 104 90 88 78 88 90 120 120 79 67 58 31 35
 100 75 68 20 20 30 19 14 10 8 10 14 21 25 30 37 50 79 100

107 60 91 98 123 123 105 101 100 101 102 132 132 68 58 54 55 46
 100 74 44 33 38 19 14 10 10 14 20 26 34 38 50 73 100

10 10 25 45 58 148 151 121 118 112 118 122 149 151 141 130 113 97 96
 100 50 29 47 42 27 21 14 10 11 10 14 20 25 28 38 50 79 100

25 05 00 26 50 153 156 128 127 6 127 130 161 167 166 134 129
 100 53 76 23 43 27 21 14 10 10 14 20 38 50 78 100

140 125 85 40 40 140 146 156 185 153 148 147 148 149 128 151 155 158 187 158
 100 74 66 50 44 27 26 25 22 16 10 14 14 19 23 27 38 45 50 100

201 122 55 47 200 200 148 154 131 154 156 180 180 187 150 164 151 205
 100 75 50 44 26 24 14 10 15 10 14 18 23 27 39 60 78 100

140 161 84 12 121 103 109 146 147 41 42 41 61 54 38 29 22 107 65 82
 100 40 60 41 36 29 23 11 10 10 11 19 25 30 40 45 23 84 100

210 184 140 118 14 13 127 47 116 45 46 119 64 60 115 27 132 44 75
 100 86 60 38 40 35 28 24 15 10 10 11 18 24 28 40 50 86 100

240 226 131 110 162 162 6 54 53 64 64 13 13 20 16 130 200
 100 81 49 38 31 26 14 10 10 14 14 24 30 40 50 74 100

Sta.	+	K	-	Elev.
		935.47		
36+5V				929.3
T.P.	1.51	929.17 ✓	7.81	927.66
+78				28.3
37				27.4
+50				25.5

Culvert Lt.

+8V				24.1 ✓
T.P.	2.67	924.10 ✓	7.74	921.43
38				23.3
+16				
+30				22.4
+41				
+50				21.8
39				
E 500 Line				21.6

R.R. Culvert Rt.

+66				21.4
+71				

Lt.

Q

Rt.

27°	20°	18°	68	63	62	63	64	93	90	41	32	23	108	12	08
<u>100</u>	<u>40</u>	<u>34</u>	<u>18</u>	<u>10</u>	<u>62</u>	<u>10</u>	<u>15</u>	<u>20</u>	<u>24</u>	<u>32</u>	<u>40</u>	<u>41</u>	<u>60</u>	<u>77</u>	<u>100</u>

204	172	147	13	10	0	9	10	12	58	66	50	12	160	66
<u>100</u>	<u>52</u>	<u>38</u>	<u>14</u>	<u>10</u>	<u>0</u>	<u>10</u>	<u>14</u>	<u>22</u>	<u>40</u>	<u>47</u>	<u>60</u>	<u>90</u>	<u>100</u>	

222	206	150	172	27	19	18	19	22	80	50	93	00	712
<u>100</u>	<u>77</u>	<u>48</u>	<u>39</u>	<u>15</u>	<u>10</u>	<u>10</u>	<u>14</u>	<u>26</u>	<u>41</u>	<u>55</u>	<u>90</u>	<u>100</u>	

28°	23°	22°	20°	44	38	37	38	38	103	122	135	140	125
<u>100</u>	<u>87</u>	<u>50</u>	<u>37</u>	<u>16</u>	<u>10</u>	<u>10</u>	<u>15</u>	<u>28</u>	<u>41</u>	<u>58</u>	<u>87</u>	<u>100</u>	

Top Conc. H. Wall

21.4	31.1
907.77	898.07

23°	22°	197	57	52	51	52	56	14	135	152	165
<u>100</u>	<u>50</u>	<u>38</u>	<u>18</u>	<u>10</u>	<u>10</u>	<u>17</u>	<u>25</u>	<u>41</u>	<u>65</u>	<u>100</u>	

17°	148	140	09	09	08	09	11	66	91	104	102
<u>100</u>	<u>47</u>	<u>38</u>	<u>15</u>	<u>16</u>	<u>10</u>	<u>15</u>	<u>26</u>	<u>41</u>	<u>50</u>	<u>100</u>	

16.3	137	103	21	18	17	18	18	73	77	90
<u>100</u>	<u>36</u>	<u>30</u>	<u>16</u>	<u>10</u>	<u>10</u>	<u>17</u>	<u>28</u>	<u>41</u>	<u>100</u>	

49	46	29	23	23	23	29	32	22
<u>100</u>	<u>50</u>	<u>14</u>	<u>10</u>	<u>10</u>	<u>21</u>	<u>50</u>	<u>100</u>	

T. Rail
3.7
100

T. Rail
2.5
100

T. Rail
1.3
100

Culvert Way High

28hr
no End.

1hr 7.2 50 End = 17540

49	44	30	27	27	27	25	33	29	30
<u>100</u>	<u>50</u>	<u>14</u>	<u>10</u>	<u>10</u>	<u>10</u>	<u>15</u>	<u>44</u>	<u>75</u>	<u>100</u>

Sta.	+	π	-	Elev.
		924.10		
38+85				920.7
+96				
39				30.1
+80				17.7
T.P.	2.22	918.46	7.86	916.24
40				15.6
+35				14.3
+40				14.1
	See thru Harwell Culvert Lt.			
B.M.	6.50	913.93	11.03	907.43
41+00				12.1
+50				10.7
42+00				09.6
+50				09.1
+60				08.9
	End Ditch Lt.			

Lt.

Lt.

Lt.

72	84	119	108	99	38	34	4	34	37	100	12	93	77	58
100	78	60	36	26	14	10	3	10	15	26	44	50	78	100

60	77	128	134	118	46	40	29.1	40	42	112	130	127	128
100	83	57	45	28	15	10	4.0	10	14	27	50	75	100

15	147	136	177	164	128	67	65	64	65	68	140	156	125	125
100	75	57	48	40	26	15	10	6	10	15	27	33	60	100

119	115	132	132	103	80	33	30	2.9	30	32	113	132	138	142
100	53	50	45	39	25	14	10	2	10	15	30	50	75	100

137	136	126	113	116	101	45	43	42	43	45	123	142	151
100	80	65	60	41	27	14	10	4	10	16	30	50	100

110	168	200	200	170	110	97	47	45	44	45	48	123	142	151
59	52	48	46	44	44	26	18	10	10	16	30	50	100	

145
200

140	130	113
100	65	60

Top of N.E. Cor. No End of East Wing wall

121	115	114	157	157	110	83	35	19	19	24	96	114	114
100	60	60	48	44	41	24	15	10	10	18	30	50	100

135	133	143	153	126	104	37	33	32	33	37	114	123	125	128
100	48	46	43	37	26	14	10	10	16	28	37	60	100	

142	137	140	158	168	145	140	50	44	48	130	146	154	147
100	60	46	44	42	40	30	15	10	15	29	36	60	100

140	138	141	165	165	131	144	55	50	49	66	131	143	155	145
100	60	44	43	40	38	30	16	10	10	16	28	33	60	100

142	137	143	162	162	126	58	51	50	51	58	135	165	132	145
100	60	43	41	34	26	14	10	10	10	14	38	32	60	100

Sta. + x - Elev.

913.93

+68

908.9

43

08.7

+50

08.5

44

08.5

+50

08.4

45

08.3

T.P.

5.48

913.44

5.97

907.96

+50

08.0

46

07.8

+50

08.1

47

08.4

+50

09.0

48

09.8

Lt.

P

Rt.

29

14.2	137	131	58	5.1	5.0	5.1	5.8	135	150	132	14.5
<u>100</u>	<u>60</u>	<u>30</u>	<u>14</u>	<u>10</u>	<u>5</u>	<u>10</u>	<u>16</u>	<u>38</u>	<u>41</u>	<u>60</u>	<u>100</u>

14.2	137	14.5	130	5.9	5.3	5.2	5.3	5.7	138	144	14.8	15.7
<u>100</u>	<u>49</u>	<u>38</u>	<u>27</u>	<u>15</u>	<u>10</u>	<u>5</u>	<u>10</u>	<u>15</u>	<u>28</u>	<u>31</u>	<u>60</u>	<u>100</u>

13.6	136	12.3	63	5.5	5.4	5.5	6.2	144	150	15.4
<u>100</u>	<u>50</u>	<u>24</u>	<u>15</u>	<u>10</u>	<u>5</u>	<u>10</u>	<u>15</u>	<u>31</u>	<u>50</u>	<u>100</u>

12.6	132	12.3	62	5.5	5.4	5.5	6.2	134	150	15.5
<u>100</u>	<u>50</u>	<u>26</u>	<u>15</u>	<u>10</u>	<u>5</u>	<u>10</u>	<u>16</u>	<u>28</u>	<u>60</u>	<u>100</u>

11.8	122	12.3	115	6.4	5.6	5.5	6.1	127	138	14.4	15.5
<u>100</u>	<u>60</u>	<u>32</u>	<u>26</u>	<u>16</u>	<u>10</u>	<u>10</u>	<u>15</u>	<u>25</u>	<u>31</u>	<u>50</u>	<u>100</u>

11.5	12.3	122	118	6.2	5.7	5.6	5.7	6.4	125	137	14.3	15.0
<u>100</u>	<u>50</u>	<u>34</u>	<u>24</u>	<u>15</u>	<u>10</u>	<u>5</u>	<u>10</u>	<u>15</u>	<u>26</u>	<u>34</u>	<u>60</u>	<u>100</u>

11.5	122	12.5	112	5.9	5.5	5.5	6.2	124	132	13.6	13.5	
<u>100</u>	<u>60</u>	<u>41</u>	<u>25</u>	<u>16</u>	<u>10</u>	<u>5</u>	<u>10</u>	<u>15</u>	<u>26</u>	<u>38</u>	<u>60</u>	<u>100</u>

12.4	130	12.6	112	6.2	5.7	5.6	5.7	6.4	118	134	14.1	13.6
<u>100</u>	<u>60</u>	<u>34</u>	<u>25</u>	<u>15</u>	<u>10</u>	<u>5</u>	<u>10</u>	<u>16</u>	<u>26</u>	<u>31</u>	<u>60</u>	<u>100</u>

12.8	128	12.3	108	6.0	5.4	5.4	5.7	113	128	130	12.2	11.4	
<u>100</u>	<u>60</u>	<u>34</u>	<u>25</u>	<u>15</u>	<u>10</u>	<u>5</u>	<u>10</u>	<u>15</u>	<u>26</u>	<u>34</u>	<u>50</u>	<u>75</u>	<u>100</u>

12.3	126	11.7	106	5.5	5.1	5.1	5.6	100	115	11.1	10.8	11.2	
<u>100</u>	<u>60</u>	<u>34</u>	<u>25</u>	<u>15</u>	<u>10</u>	<u>5</u>	<u>10</u>	<u>15</u>	<u>26</u>	<u>31</u>	<u>60</u>	<u>84</u>	<u>100</u>

11.4	115	10.8	93	4.9	4.1	4.1	4.5	4.9	88	106	10.1	10.5	
<u>100</u>	<u>60</u>	<u>33</u>	<u>23</u>	<u>14</u>	<u>10</u>	<u>5</u>	<u>10</u>	<u>14</u>	<u>23</u>	<u>36</u>	<u>60</u>	<u>70</u>	<u>100</u>

10.1	97	97	75	4.0	3.7	3.7	4.2	75	87	91	9.3
<u>100</u>	<u>60</u>	<u>34</u>	<u>23</u>	<u>14</u>	<u>10</u>	<u>5</u>	<u>14</u>	<u>22</u>	<u>31</u>	<u>40</u>	<u>100</u>

Sta.	+	K	-	Elev.
		913.44		
T.P.	6.74	918.67	1.51	911.93
48+50				10.9
49				12.1
+35				13.1
T.P.	10.56	924.90	4.33	914.34
+60				13.80
50				14.90
T.P.	7.98	930.16	2.72	922.18
+50				16.4
51				17.8
+50				19.16
B.M.	8.67	930.79	8.04	922.72
52				20.4
+33				21.2
+39				21.4
+46				21.5

Lt.

Q

Rt.

30

124 118 107 80 79 78 77 80 109 114 127 133
 100 50 24 15 10 7 10 14 22 28 50 100

10.8
 10.9
 10.8

104 100 89 68 67 66 67 67 84 100 111
 100 50 24 15 10 10 15 22 48 100

12.0
 12.1
 12.0

69 71 68 67 59 57 56 57 59 63 82 90 104
 100 50 26 18 16 10 10 16 23 37 50 100

13.0
 13.1
 13.0

107 107 104 123 123 116 112 111 112 113 120 116 82 96 115 133 152
 100 60 27 22 19 16 10 10 10 16 20 23 28 41 60 80 100

13.7
 13.8
 13.7

74 73 69 58 118 115 103 101 100 101 102 107 90 81 20 39 72 83
 100 50 37 29 23 18 15 10 10 10 15 18 24 33 33 61 83 100

14.8
 14.9
 14.8

69 77 71 98 134 155 155 140 139 138 137 141 144 144 63 30 29 48 89
 100 30 31 30 25 20 18 14 10 10 10 14 16 17 33 34 50 70 100

16.3
 16.4
 16.3

44 87 103 140 140 121 124 124 124 127 136 136 25 61 44
 100 30 36 23 19 15 10 10 10 14 17 20 29 50 100

40 90 114 119 130 130 113 111 110 111 112 130 130 92 85 65 34
 100 36 31 26 24 20 18 10 10 10 14 18 20 26 37 50 100

Top of Stone Men "B" & White Bear Ave.

12 20 60 22 107 103 118 113 108 105 104 105 105 119 117 108 95 65 72 87 93
 100 79 8 31 35 29 26 24 20 18 10 10 10 15 19 23 26 30 30 50 82 100

07 34 47 26 94 104 102 97 97 96 97 99 111 107 89 84 46 68 81
 100 80 50 33 27 24 20 16 10 10 10 15 19 22 26 47 54 74 100

05 31 47 56 98 99 95 95 94 95 96 100 107 85 76 49 65 77
 100 77 20 33 24 20 15 10 10 10 17 20 22 26 50 57 74 100

75 84 96 94 94 93 94 93 106 105 105
 100 50 31 24 20 10 10 14 24 50 100

52 + K - Elev.

930.79

52 + 52

21.8

+56

21.8

+72! 2 B

22.1

+88

22.4

+93

22.5

53

22.7

22

+05

22.8

T.P. 12.78 936.40 7.17 923.62

+50

23.6

+84

24.1

54

24.3

T.P. 10.84 935.42 11.82 924.58

+40

24.7

55

25.3

LT.

E

RT.

$\frac{72}{100}$ $\frac{8.8}{50}$ $\frac{9.4}{25}$ $\frac{8.5}{29}$ $\frac{9.1}{10}$ $\frac{9.0}{10}$ $\frac{9.1}{10}$ $\frac{9.2}{26}$ $\frac{10.4}{31}$ $\frac{10.2}{30}$ $\frac{10.7}{100}$

$\frac{6.0}{100}$ $\frac{7.6}{50}$ $\frac{8.5}{20}$ $\frac{9.1}{10}$ $\frac{9.0}{10}$ $\frac{9.1}{10}$ $\frac{8.7}{17}$ $\frac{9.0}{47}$ $\frac{9.2}{100}$

$\frac{5.7}{100}$ $\frac{7.3}{50}$ $\frac{8.7}{10}$ $\frac{8.7}{10}$ $\frac{8.8}{10}$ $\frac{8.5}{19}$ $\frac{8.2}{33}$ $\frac{8.4}{100}$

$\frac{5.7}{100}$ $\frac{7.6}{50}$ $\frac{8.3}{21}$ $\frac{8.5}{10}$ $\frac{8.4}{10}$ $\frac{8.5}{10}$ $\frac{8.5}{28}$ $\frac{8.8}{50}$ $\frac{9.2}{100}$

$\frac{7.1}{100}$ $\frac{8.1}{50}$ $\frac{8.0}{37}$ $\frac{9.4}{25}$ $\frac{8.4}{18}$ $\frac{8.4}{15}$ $\frac{8.4}{10}$ $\frac{8.3}{10}$ $\frac{8.4}{10}$ $\frac{8.6}{21}$ $\frac{10.4}{29}$ $\frac{10.7}{50}$ $\frac{10.8}{100}$

$\frac{6.5}{100}$ $\frac{7.2}{50}$ $\frac{8.0}{44}$ $\frac{9.0}{25}$ $\frac{8.9}{19}$ $\frac{8.2}{16}$ $\frac{8.2}{10}$ $\frac{8.1}{10}$ $\frac{8.2}{10}$ $\frac{8.3}{16}$ $\frac{10.1}{21}$ $\frac{10.0}{27}$ $\frac{10.7}{50}$ $\frac{11.0}{100}$

$\frac{+2.0}{100}$ $\frac{1.8}{50}$ $\frac{5.6}{37}$ $\frac{5.7}{31}$ $\frac{9.0}{25}$ $\frac{9.0}{18}$ $\frac{8.2}{15}$ $\frac{8.1}{10}$ $\frac{8.0}{10}$ $\frac{8.1}{10}$ $\frac{8.4}{16}$ $\frac{9.2}{19}$ $\frac{9.2}{23}$ $\frac{5.2}{33}$ $\frac{5.7}{42}$ $\frac{7.2}{50}$ $\frac{9.5}{64}$ $\frac{10.9}{100}$

$\frac{2.7}{100}$ $\frac{4.0}{50}$ $\frac{2.1}{60}$ $\frac{2.4}{50}$ $\frac{4.1}{43}$ $\frac{4.2}{37}$ $\frac{12.3}{25}$ $\frac{13.6}{16}$ $\frac{13.0}{14}$ $\frac{12.9}{10}$ $\frac{12.8}{10}$ $\frac{12.9}{10}$ $\frac{13.0}{15}$ $\frac{14.2}{18}$ $\frac{14.3}{22}$ $\frac{8.5}{29}$ $\frac{11.6}{40}$ $\frac{15.4}{55}$ $\frac{18.3}{75}$

$\frac{3.5}{100}$ $\frac{3.5}{87}$ $\frac{2.2}{67}$ $\frac{1.0}{66}$ $\frac{1.0}{37}$ $\frac{12.3}{21}$ $\frac{12.2}{16}$ $\frac{12.4}{13}$ $\frac{12.4}{10}$ $\frac{12.3}{10}$ $\frac{12.4}{10}$ $\frac{12.6}{14}$ $\frac{13.8}{17}$ $\frac{12.9}{22}$ $\frac{9.2}{28}$ $\frac{9.8}{31}$ $\frac{13.1}{43}$ $\frac{15.2}{50}$ $\frac{17.6}{75}$

$\frac{7.0}{100}$ $\frac{6.3}{84}$ $\frac{2.9}{81}$ $\frac{2.6}{34}$ $\frac{1.6}{22}$ $\frac{13.3}{17}$ $\frac{12.4}{14}$ $\frac{12.2}{10}$ $\frac{12.1}{10}$ $\frac{12.2}{10}$ $\frac{12.5}{14}$ $\frac{13.0}{18}$ $\frac{13.6}{21}$ $\frac{9.8}{27}$ $\frac{11.5}{38}$ $\frac{14.4}{50}$ $\frac{15.8}{54}$ $\frac{17.3}{100}$

$\frac{11.0}{100}$ $\frac{10.7}{34}$ $\frac{10.3}{36}$ $\frac{9.2}{36}$ $\frac{12.3}{22}$ $\frac{12.3}{18}$ $\frac{10.9}{14}$ $\frac{10.8}{10}$ $\frac{10.7}{10}$ $\frac{10.8}{10}$ $\frac{11.1}{15}$ $\frac{12.4}{18}$ $\frac{12.3}{21}$ $\frac{10.0}{21}$ $\frac{8.8}{45}$ $\frac{9.4}{60}$ $\frac{8.6}{100}$

$\frac{12.3}{100}$ $\frac{12.3}{50}$ $\frac{12.6}{33}$ $\frac{11.1}{24}$ $\frac{11.1}{27}$ $\frac{11.8}{19}$ $\frac{10.4}{14}$ $\frac{10.2}{10}$ $\frac{10.1}{10}$ $\frac{10.2}{10}$ $\frac{10.3}{14}$ $\frac{11.3}{17}$ $\frac{11.0}{21}$ $\frac{9.0}{30}$ $\frac{5.0}{50}$ $\frac{6.3}{55}$ $\frac{8.6}{100}$

Sta.	+	Σ	-	Elev.
		935.47		
55+25				25.4
+50				25.6
56				25.7
+50				25.8
T.P.	4.07	929.74	975	925.67
57				25.6
+35				25.4
+70				25.2
58				24.9
+28				24.6
+70				24.2
59				23.8
+24				23.6

L.

E

R.

$$\frac{13^2}{100} \frac{14^0}{96}$$

$$\frac{14^6}{83} \frac{14^4}{58} \frac{13^1}{24} \frac{12^2}{33} \frac{11^3}{25} \frac{11^6}{23} \frac{11^6}{19} \frac{10^2}{14} \frac{10^1}{10} \frac{10^0}{100} \frac{10^1}{10} \frac{10^2}{15} \frac{11^1}{17} \frac{11^1}{21} \frac{6^9}{28} \frac{8^2}{40} \frac{8^2}{60} \frac{10^9}{80} \frac{10^9}{100}$$

$$\frac{14^2}{100} \frac{14^4}{54} \frac{13^1}{47} \frac{11^9}{33} \frac{10^2}{24} \frac{11^5}{22} \frac{11^3}{18} \frac{10^2}{15} \frac{9^9}{10} \frac{8^9}{10} \frac{10^0}{14} \frac{11^4}{19} \frac{11^3}{22} \frac{10^1}{25} \frac{11^1}{37} \frac{12^2}{60} \frac{13^8}{100}$$

$$\frac{14^7}{100} \frac{14^6}{76} \frac{13^4}{68} \frac{10^6}{45} \frac{9^7}{33} \frac{11^2}{23} \frac{10^9}{18} \frac{10^0}{15} \frac{9^8}{10} \frac{9^7}{10} \frac{9^8}{14} \frac{9^9}{27} \frac{11^3}{33} \frac{12^6}{50} \frac{13^6}{75} \frac{14^5}{100}$$

$$\frac{14^0}{100} \frac{11^0}{49} \frac{10^5}{33} \frac{11^0}{26} \frac{11^4}{23} \frac{11^2}{19} \frac{9^9}{15} \frac{9^7}{10} \frac{9^6}{10} \frac{9^7}{10} \frac{9^8}{14} \frac{12^2}{21} \frac{13^1}{60} \frac{13^9}{100}$$

$$\frac{8^3}{100} \frac{8^3}{63} \frac{7^3}{33} \frac{5^9}{20} \frac{4^3}{15} \frac{4^2}{10} \frac{4^1}{10} \frac{4^2}{15} \frac{4^4}{18} \frac{5^9}{33} \frac{5^9}{60} \frac{5^7}{75} \frac{6^4}{100}$$

$$\frac{9^3}{100} \frac{8^8}{60} \frac{7^9}{47} \frac{6^9}{34} \frac{5^5}{24} \frac{5^8}{20} \frac{4^5}{15} \frac{4^4}{10} \frac{3^4}{10} \frac{4^6}{14} \frac{5^2}{16} \frac{5^2}{44} \frac{6^1}{60} \frac{5^7}{100}$$

$$\frac{7^9}{100} \frac{7^7}{48} \frac{7^2}{30} \frac{5^7}{24} \frac{6^4}{32} \frac{5^9}{19} \frac{4^7}{14} \frac{4^6}{10} \frac{4^5}{10} \frac{4^6}{14} \frac{5^0}{21} \frac{7^5}{33} \frac{7^4}{60} \frac{7^1}{100}$$

$$\frac{6^2}{100} \frac{6^2}{50} \frac{5^3}{30} \frac{5^9}{24} \frac{6^4}{23} \frac{6^2}{19} \frac{4^9}{14} \frac{4^9}{10} \frac{4^8}{10} \frac{4^9}{10} \frac{6^0}{14} \frac{6^6}{20} \frac{6^8}{24} \frac{6^6}{27} \frac{7^4}{60} \frac{8^8}{100}$$

$$\frac{4^8}{100} \frac{4^8}{50} \frac{4^9}{27} \frac{6^7}{23} \frac{6^6}{19} \frac{5^4}{15} \frac{5^2}{10} \frac{5^1}{10} \frac{5^2}{14} \frac{5^3}{17} \frac{6^2}{21} \frac{4^6}{28} \frac{4^5}{50} \frac{4^6}{75} \frac{6^6}{100}$$

$$\frac{3^1}{100} \frac{2^8}{44} \frac{3^5}{50} \frac{3^6}{36} \frac{3^3}{29} \frac{7^2}{24} \frac{6^5}{17} \frac{5^7}{14} \frac{5^6}{10} \frac{5^5}{10} \frac{5^6}{13} \frac{5^7}{17} \frac{6^6}{21} \frac{4^5}{27} \frac{3^7}{60} \frac{4^0}{100}$$

$$\frac{2^6}{100} \frac{1^6}{75} \frac{2^2}{50} \frac{2^6}{33} \frac{7^6}{23} \frac{7^6}{18} \frac{6^1}{14} \frac{6^0}{10} \frac{5^9}{10} \frac{6^0}{10} \frac{5^8}{15} \frac{7^0}{20} \frac{7^0}{23} \frac{5^2}{27} \frac{4^1}{60} \frac{3^9}{71} \frac{4^0}{100}$$

$$\frac{3^6}{100} \frac{1^1}{80} \frac{0^9}{64} \frac{1^3}{43} \frac{1^4}{33} \frac{7^7}{25} \frac{7^5}{17} \frac{6^2}{13} \frac{6^1}{10} \frac{6^1}{10} \frac{6^2}{10} \frac{6^3}{14} \frac{8^0}{19} \frac{8^0}{21} \frac{5^0}{31} \frac{4^6}{70} \frac{4^2}{100}$$

Sta.	+	π	-	Elev.
		929.74		
59+31				23.6
B.M.	5.32	928.71	6.35	923.39
60+00				23.1
+50				23.1
+86				23.0
Cross Culvert - Conc. Pipe + 90				
61				23.0
+50				23.2
62				23.4
+50				23.6
63+00				23.7
B.M.			6.84	921.88
				921.87

LH

E

RT

33

38	11	13	17	20	28	27	24	21	22	23	26	28	28	29	21	20
100	77	80	85	27	23	19	14	10	10	15	19	21	25	60	100	

Top of pavement curb 10' RT 512.60 + 26.6

24	53	33	25	21	53	28	69	56	53	56	59	55	59	25	76	63	72	72
100	84	60	53	33	27	21	18	14	10	5	10	14	19	22	35	50	100	

55	52	58	77	73	65	56	73	69	51	51	56	63	60	64	83	86	84	79	81
109	90	74	66	60	58	24	21	18	14	10	5	12	13	18	33	27	31	50	100

22	55	55	60	67	60	88	89	82	51	57	65	61	71	88	107	113	114
100	80	60	45	40	24	24	19	14	10	5	13	14	19	23	30	50	100

1st 9.1

19.61

1st 11.5

12.11

57	76	77	56	54	56	57	65	66	52	51	57	66	62	69	116	126	126
100	83	78	70	58	36	24	24	18	15	10	5	13	13	19	28	50	100

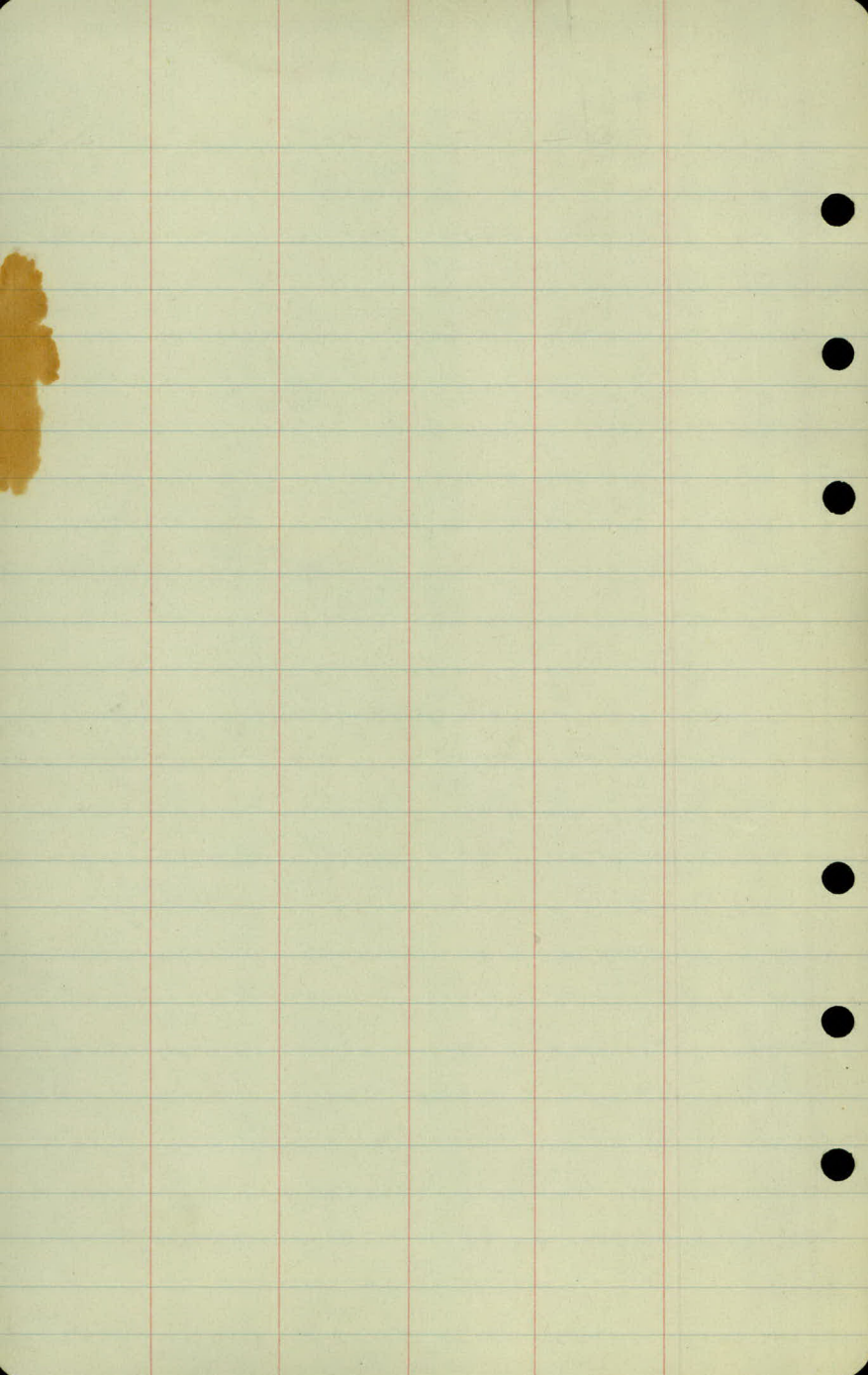
66	74	78	56	48	48	55	63	60	64	100	115	122	128	128
100	50	46	39	24	10	5	13	13	19	27	38	50	60	100

28	88	88	49	47	53	61	57	63	83	99	115	121	112
100	60	34	24	10	5	13	13	19	25	40	50	50	100

111	104	94	48	47	51	58	54	57	106	105	81	61
100	48	24	16	10	5	13	13	18	31	50	75	100

122	111	102	48	47	50	53	49	54	90	77	58	18
100	60	24	11	10	5	10	10	16	19	44	50	100

Spoke in 10" Oak 20' RT. 512.63 + 24



Additional X-Sec.

Rect proposed King Alaron

Sta	+	K	-	Elev.
B.M.	14.75	919.68		907.43
T.P.	7.70	925.14	2.26	917.42
38+16				922.9

38+41 22.0

21.2

38+71

38+96 20.2

Top of South Rail
 " " North "

Lt.

E

Rt.

Top of N.E. Cor. No. End. of East Conc. Wing
Wall of Culvert Lt. 512 40+45

18.0	15.3	14.5	12.1	3.0	2.4	2.5	2.2	2.1	8.8	10.1	11.3	11.2	10.1	9.6
100	50	41	31	14	10	25	10	14	28	35	50	76	86	100

16.8	15.6	13.5	10.5	7.0	4.6	3.5	3.7	3.1	3.1	3.2	4.6	4.3	3.5	3.3	4.1
100	73	50	34	20	18	15	10	2	10	16	26	38	50	53	100

5.3	4.9	5.6	5.8	4.4	4.0	3.9	4.0	4.0	6.7	8.7	8.2	9.2	8.4	6.8	6.2
100	50	36	22	15	10	2	10	15	20	28	31	44	50	70	100

2.1	2.8																	
100	84																	
11.0	13.8	14.0	15.0	13.8	12.8	11.8	5.3	5.0	4.9	5.0	5.1	11.8	13.5	13.8	13.5	12.3	15.3	
73	59	50	44	36	34	25	14	10	4	9	10	14	26	40	50	70	77	100

921.62

3.50

21.54

3.58

