

Dr. 8 - Bk. 157

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ PLAN _____ Survey

_____ COUNTY ROAD "C" _____

From Victoria St. To Rice St.

Road Acc't. No. 7

Date Filed 12-29-38

File _____

1

Co Road "C"

~~Preliminary~~ survey from
intersection with Victoria St.
to intersection with Rice St.

1/38

This alignment to follow approx
4 of present black top surface

Refer to previous Road Survey 1926

On Sec. line from Sts. 24+54.58
to Rice St. Sts. 83+40.33

Plan made
Feb. 1938
H.C.

Angle

Sta. Point Rt. Lt. Def.

7+59.19 P.T.

9°18'

+50

8°59'

7

7°14'

+50

5°29'

6+27.6 P.I. 18°36'

$D=7^{\circ}00'$

$T=134.12$

$L=265.71$

6

3°44'

+50

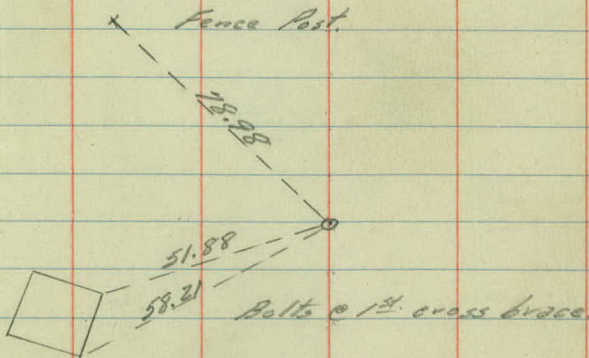
1°59'

5

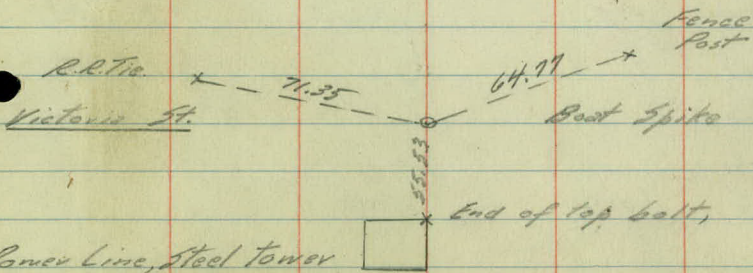
0°14'

4+93.48 P.C.

0+00 P.O.T.

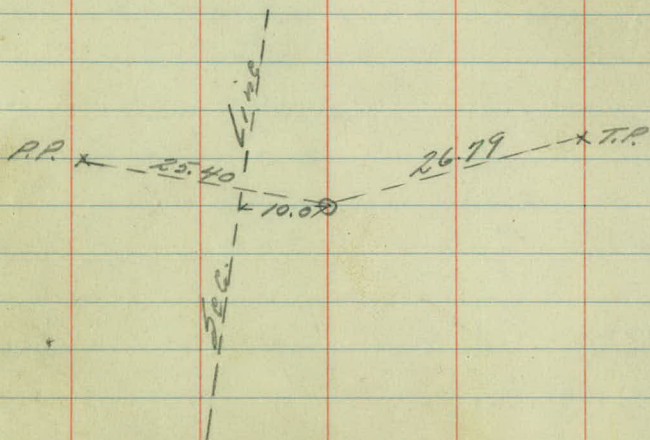
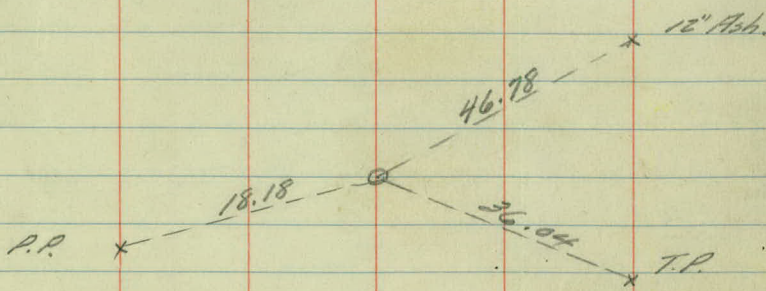
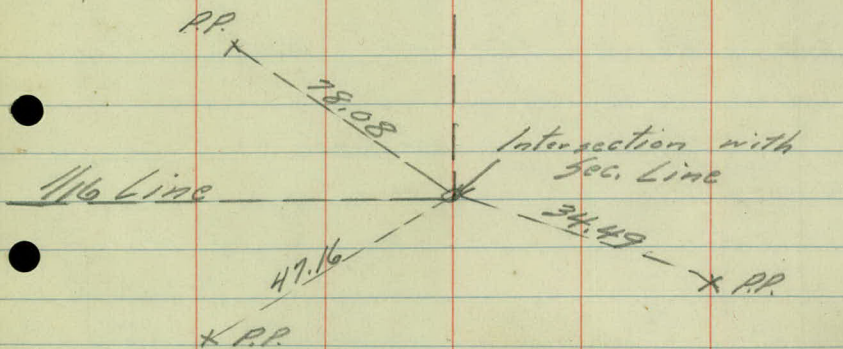


Power Line
Steel Tower #165



Angle.

Sta.	Point	Rt.	Lt.	Def.
24+54.58	P.I.	0°39'		
15+73.56	P.I.		0°26'	
11+61.04	P.T.			0°47 $\frac{1}{4}$ '
+50				0°44 $\frac{1}{4}$ '
11				0°29 $\frac{1}{2}$ '
				D=1°00'
10+81.9	P.I.	1°35'		T=79.19
				L=158.33
+50				0°14 $\frac{1}{2}$ '
10+02.71	P.C.			



Angle

Sta. Point Rt. Lt. Def.

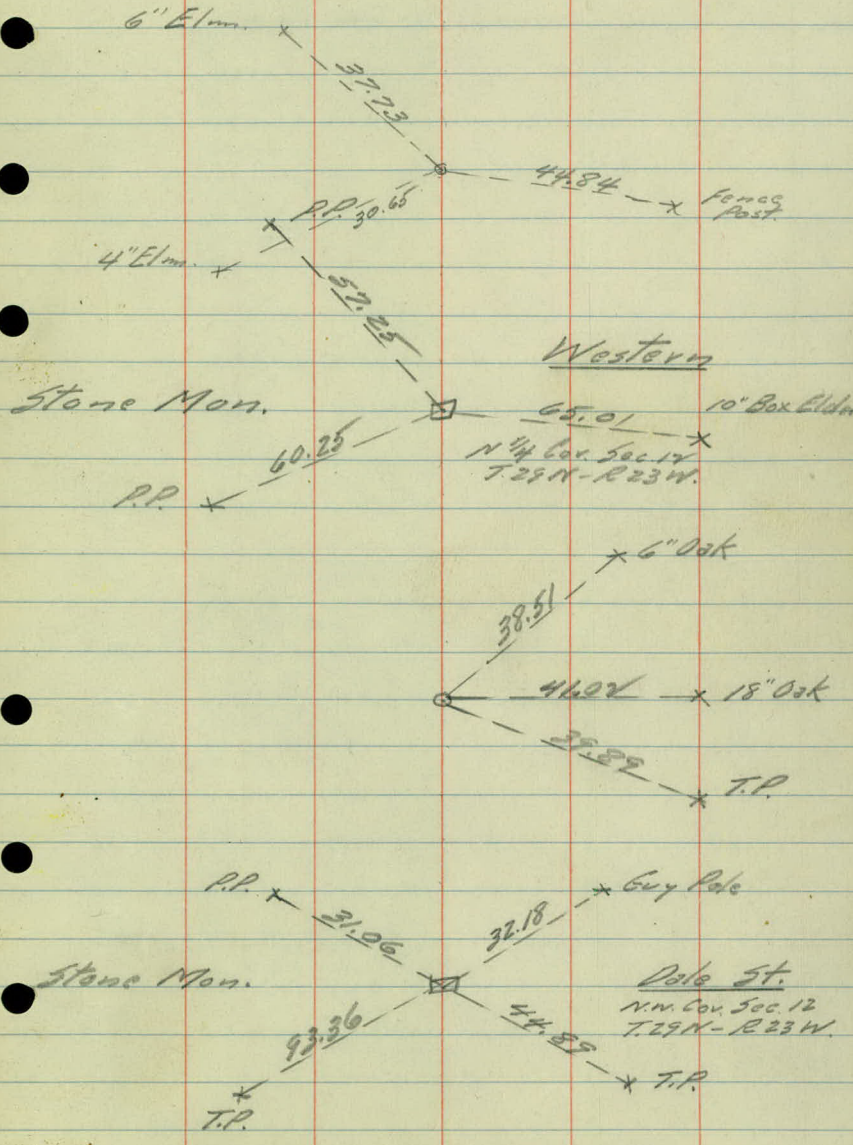
61+53.73 P.O.T.

57+22.45 P.O.T.

38+63.20 P.O.T.

31+14.33 P.I.

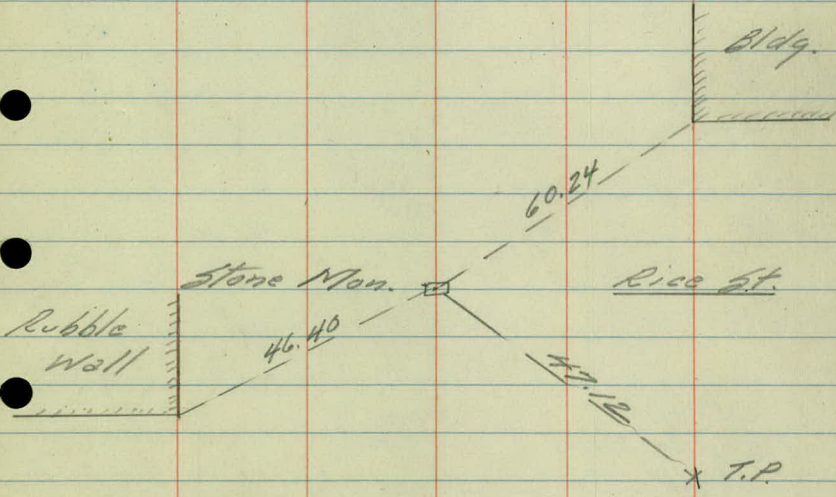
0°24'

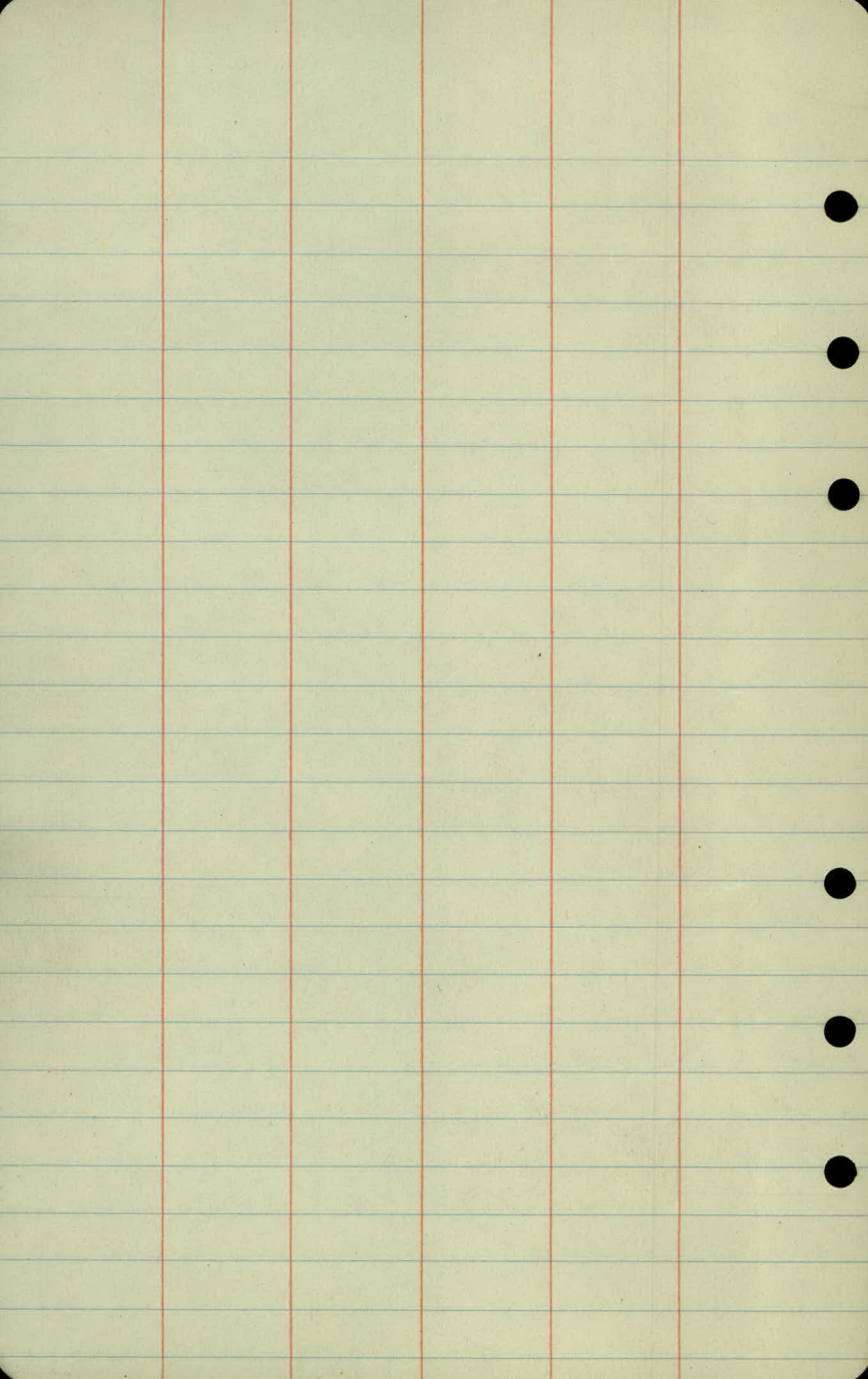


Angle.

Sta.	Point	Rt.	Lt.	Def.
------	-------	-----	-----	------

83+40.33 Mon.





E

← North

P.I. 6+27.6

Power Line
Steel Tower #165 Bottom Bolt.

T.P. X - 3950

Stone Mon.
N. 1/4 Cor. Sec. 11.

47.25

Sta. 4+70.2

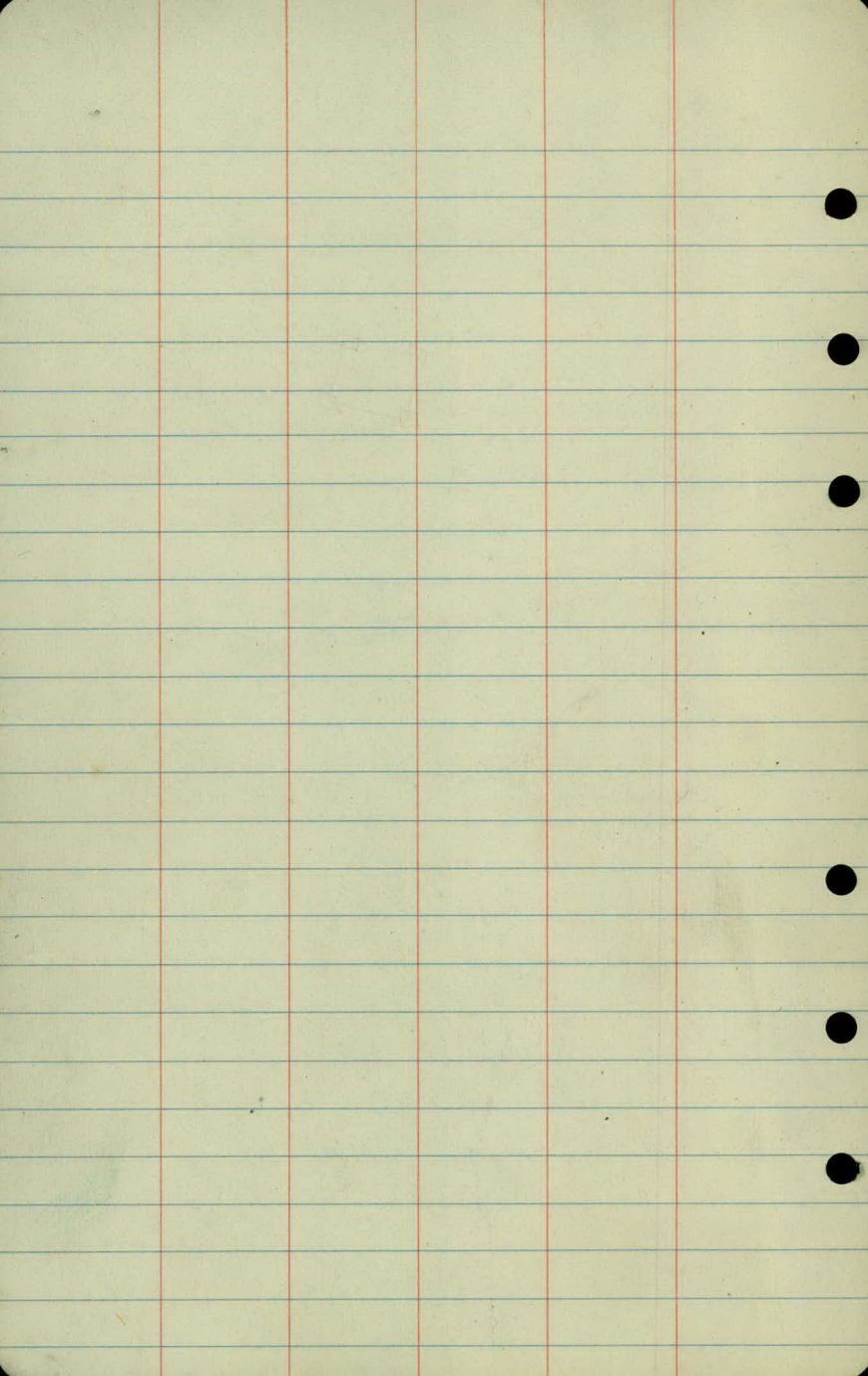
90.03

X R.R. Conc. Culv.
Drilled Hole @ Top.

73°30'

Stone Mon.
12

0+00



Cultivated

Cultivated

P.P. +87 • 24

22 • +99 P.P.

Black Top.

36.	Lt.	Rt.
12	12	10
11	12	9
10	12	10
9	9	11
8	11	11
7	10	12
6	11	9

P.P. +63 • 16

22 • +79 P.P.

+43 P.P. 17' • +55 • 15' • +70 End. Ed. Rl. & Fence. • +52 T.P. 24'

Cultivated

120 P.P. 12'

Ed. Rl. Fence • +50 T.P. 27'

+5 48" W. W. 1 B.W.

+50 • 4 B.W. 16' Dirt Rd. 205' 170' • +43 78

Cultivated

+38 = 30" x 32' C.M.

+55 120 S.P. +93 P.P.

17' Lt. 16' Lt. Run Line Steel Tower

53.5 48.0 81

+34' T.P. +88 = 13' • +94 W. W. Fence

Hay Land

+23 P.P. 13' • +08 S.W. P. 16 20' • +05 P.P. 22'

+36 T.P. 21'

19

8

18

Scattered
Trees

T.P. +95-22' Hedge +92

Orchard

+44 Hedge

+36 Entr. 12' Dirt

17

+09 R.P. 17'

+50 R.P. 17'

+55 Guy P. 18'

Stucco
Drilling

76'

46'

18" Box Elder

+57 T.P. - H. 15' x 20'

Cultivated

16

30' 12" willow +10 Hedge

+70 R.P. 18'

+46 T.P. 23'

15

Cultivated

+45 R.P. 21'

+42 T.P. 24'

Black Top

14

Cultivated

Stk.	Lt.	Rt.
19	9	9
18	8	10
17	8	10
16	9	10
15	10	10
14	10	10
13	10	10

+28 R.P. 22'

+36 T.P. 23'

13

Cultivated

+24 T.P. 22'

+09 R.P. 24'

12

26

+97 = 10' Dirt Entr.

• +54 T.P. 20'

+32 P.P. 17'

+20 Dirt Entr. 8'

25

+79 Dirt Entr. 8' wide

24

+09 P.P. 17'

• +30 T.P. 20'
• +27 P.P. 20'

Block Top

Stk.	Lt.	Rt.
26	11	12
25	9	12
24	10	10
23	9	9
22	8	10
21	10	10
20	9	9

23

+89 P.P. 17'

• +99 T.P. 4-18' 423'

22

+68 P.P. 18'

• +72 T.P. 20'

21

+54 P.P. 18'

• +42 T.P. 19'

20

Cultivated

+84 Entr. 8' 15"

Fr. Dm.



34

98'

+23 P.P. 18'

+21

5009,003.

Cultivated

40' + 12 Box Elder 14"

+02 Entr. 8'

40' + 54 = 14" Box Elder 46

110' →

29' + 70 = 8" Tree 85.

+87

Fr. Dm.

• +15 T.P. 19'

19

+50 Cd. Rl. 9'

9

Hay Land.

• T.P. +02-16'

Cultivated

+43 Rd. Sgn. 26'
+34=12" x 15" x 52'
+38 R.P. 21'

+38 Guy Rl. 22'

Dole St.

24' Black Top.

+98 T.P. 92'

+98 T.P. 42'

+91

31+00=15" x 65' C.M.

+94 Rd. Sgn. 47'

• +74 T.P. 16'

+35

yard



+15 R.P. 21'

67

Fr. Dw.

+11

+95 Ent. 12'

+65 x 28 W. x 26

+87

+57 Cottonwood 16" x 30

12" Masonry Wall

12" W. 2 1/2" Hi.

• +54 T.P. - H-15' x 20'

12" x 20' C.M.

+21 Ent. 16'



162'

+89 +94 R.P. 20'

Fr. Dw.

yard.

+40

Black Top.

Sts.	Lt.	Rt.
32	14	6
31		
30	13	11
29	11	8
28	11	9
27	11	10

• +22 T.P. 18'

• +18 R.P. 18'

Cultivated

Cultivated

+74 R.P. 19'

+58 Cottonwood 36" x 28'

• +52 T.P. 18'

Cultivated

• +92 T.P. 19'

• Sgn. x Road +73-19'

+51 R.P. 18'

+28 Cottonwood 36" x 26

26

39

+26 R.P. 16'
+23 T.P. 16'

38

Feathered Oak
&
Brush.

Cultivated

← Brush line 28'

37



+88 T.P. H. 15 4/13' +95

Cultivated

36

+32 End 64 R.L. 12'

12'

Hay Land.

+75 T.P. 15'

Block Top

56.	Lt.	Rt.
39	10	10
38	10	10
37	10	10
36	11	9
35	11	8
34	12	7
33	13	9

35

10'

+60 X Rd 59. 22'

+42 T.P. 16'

34

10'

Hay Land

+12 T.P. 16'

33

9'

Cultivated

Posture

West Land

3 B.N. - wd. 20.5

07 T.P. 15'
Brush line 20'

+06 T.P.-H-12'419'
+03 P.P.-H-12'419'
Brush line 20'

405 T. 12, 13

+96 C.D. Rk 15'
• +90 T.P. 16'

Brush line 28'

• 454 T.P. 16'

St.	Lt.	Rt.
46	10	9
45	10	9
44	7	7
43	10	7
42	11	9
41	9	9
40	10	10

52468 = 30" x 10' C.M. } Lt.
30" x 4' C.M. } Rt.
18" x 28" V.T.P. } Ctr.

52

Timber } line
& } 15'
Brush } out →

$$+ 72 = 24'' \times 50' \text{ C.M.}$$

57

5BW →

50

40654 R1 12'

49

Scattered Oak

Black Top.

5th	4th	3rd
53	5	11
52	6	11
51	8	11
50	9	10
49	10	8
48	10	7
47	13	9

48

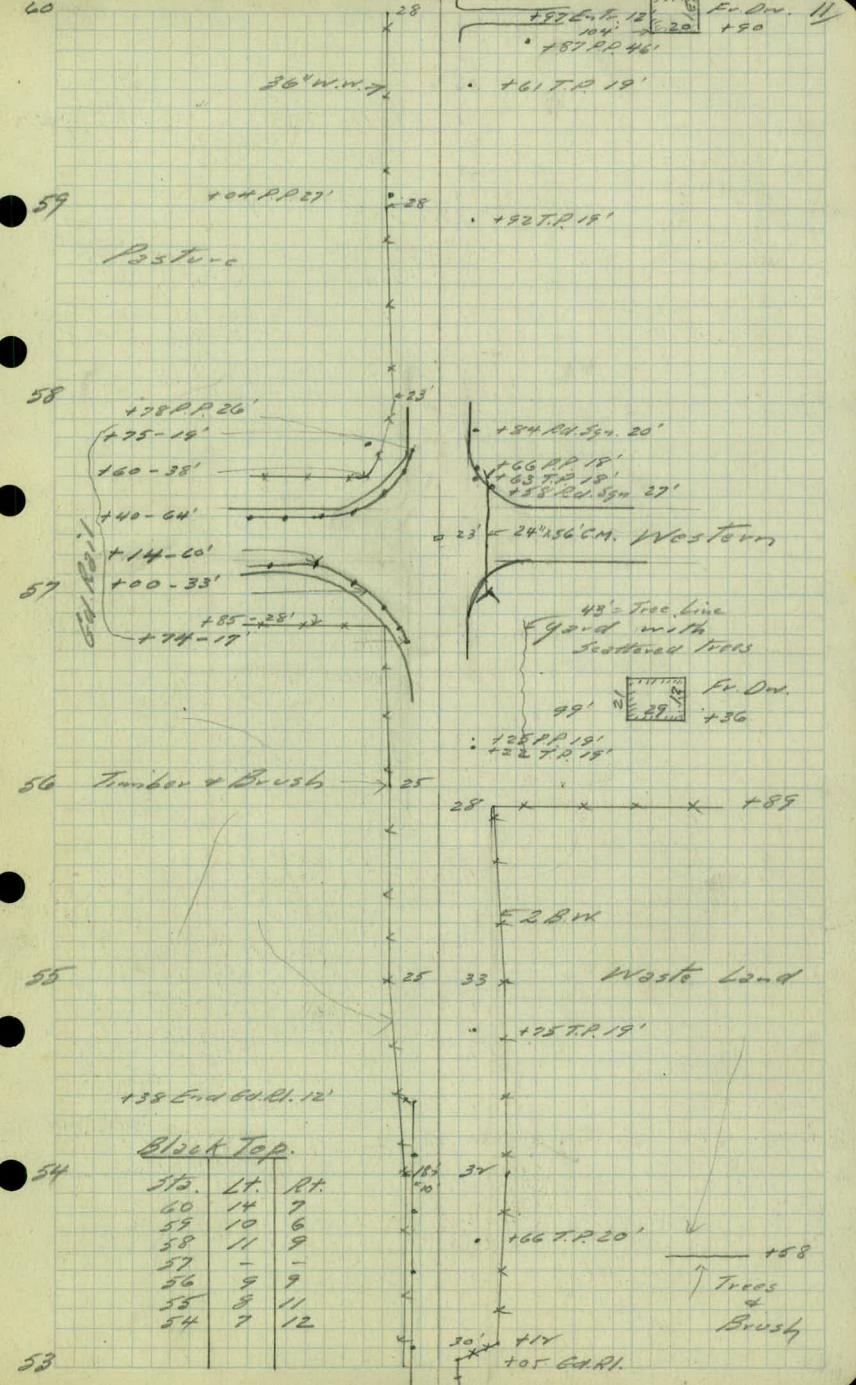
58 N. 7

47

Posture

46

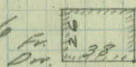
Waste land



67

Cultivated

66



+41 R.P. 28'
+24 Ent. 8'

42-4
134'
+85

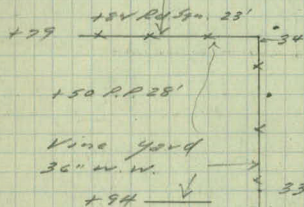
+55 Ent. 8'

65

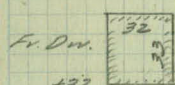
+96 R.P. 28'

Orchard
Tree Line 60'

64



63



+32

Yard
Foot
Trees
114'

+109 +41 R.P. 28'

62

+97 Ent. 16'
+86

From 61 to 63 +75 Lt.
8-4" to 6" Ash & Elms
on fence line

36" w.w.

61

Pasture

+71 R.P. 28' 36'

+50
+50 R.P. 27'

Pasture

60

27

+167 T.P. 19'

Scattered

Oak

Pasture

27

+49 T.P. 19' 16' x 22'

4 B.W., Angle Iron Posts.

27

+79 = 15" x 36' C.M.
Pasture

+147 T.P. 19'

27

+15" x 20' C.M.
+61 Ent. 8'

+15 T.P. 19'

27

150'



4 B.W. - Iron Posts

27

Pasture

Black Top

+130 T.P. 18'
+26

27

20

+78 Ent. 8'

+30 B.W.

+120 T.P. 19'

23 + 106 Begin Fence

Sta.	Lt.	Rt.
67	14	9
66	14	8
65	14	7
64	14	6
63	12	7
62	11	5
61	14	7

36 * * * * * +39
 184 P.P. 21
 180 T.P. 21

11.11.1918
 N
 24
 37

160'

+57 P.P. 28'

School

Play

Ground



+65. 28

+09 P.P. 28'

3 B.W. →

Cultivated

36 *

+55 T.P. 21
 15" x 20' C.M.

+40 Entr. 12'

19

4 B.W.

36

Scattered

Oak

Pasture

+33 T.P. 20'

37

11.11.1918
 N
 24

+58

12" x 20' C.M.

+38 Entr. 8'

21

37

10" x 20' Dredge Pipe

+84 Entr. 8'

19

+89 * * * * *

12" x 23' V.T.P. C.M.

+76 Road No. 16'

+61 P.P. 28'

22

+10 Fur. End. 30

30

37

Scattered Oak

& Pasture

Cultivated

+50 T.P. 20'

Block Top

+16 P.P. 28'

32

35

Sta.	Lt.	Rt.
51	11	8
50	11	7
79	11	8
78	11	9
77	11	11
76	10	10
75	10	10

+49 T.P. 21

Black Top

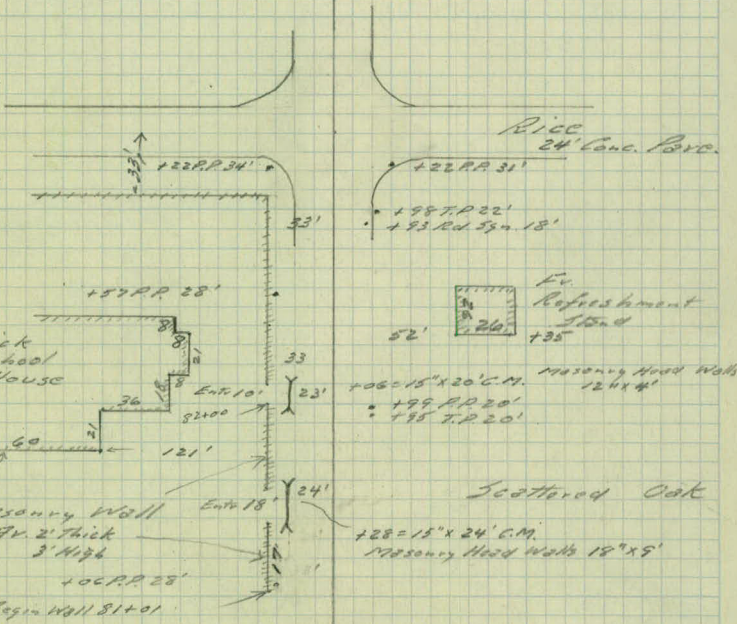
Sta.	Lt.	Rt.
83	14	11
84	17	9

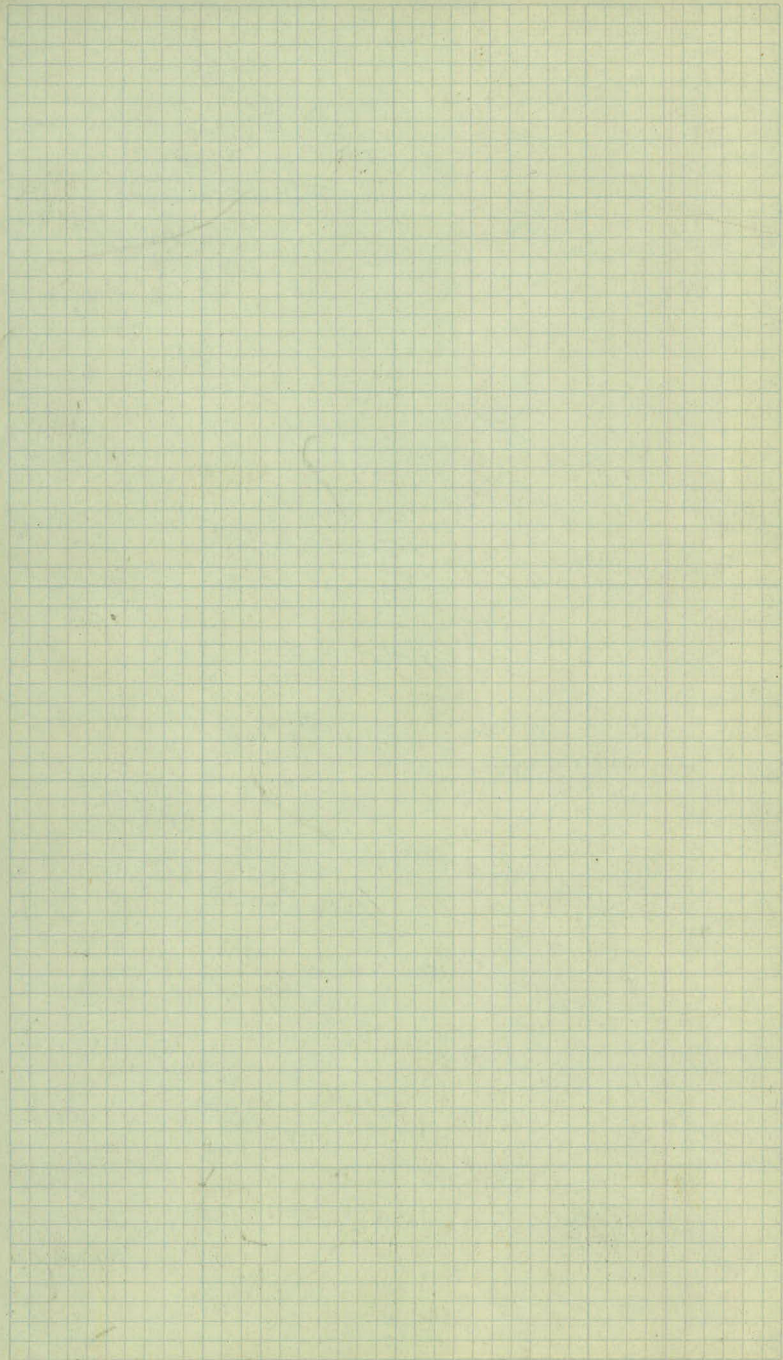
84

83

82

81





Bench Levels.

Co. Rd. "C" - Rice to Victoria

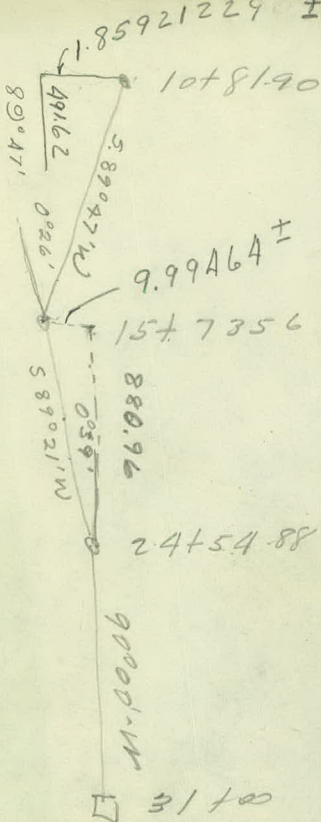
138

Sta.	+	x	-	Elev.
B.M.	0.89	958.80		959.91
	2.25	951.86	9.19	949.61
	2.63	947.62	6.87	944.99
B.M.	4.11	947.62	4.11	943.51
	3.99	939.45	12.16	925.46
	0.27	926.56	13.16	926.29
B.M.	2.98	926.56	2.98	923.58
	0.73	915.69	11.60	914.96
B.M.	4.01	915.69	4.01	911.68
	12.43	926.74	1.38	914.31
	13.49	939.35	0.88	925.86
	1.53	929.65	11.23	928.12
	9.78	929.65	9.78	919.87
B.M.	12.43	934.90	8.18	921.47
	7.62	941.98	0.54	934.36
	9.00	948.59	2.39	939.59
B.M.	5.25	948.59	5.25	943.34
	0.14	936.44	12.29	936.30
	0.87	925.30	12.01	924.43
	0.52	912.44	13.38	911.92
	3.30	902.47	13.27	899.17
B.M.			11.58	890.89

Open

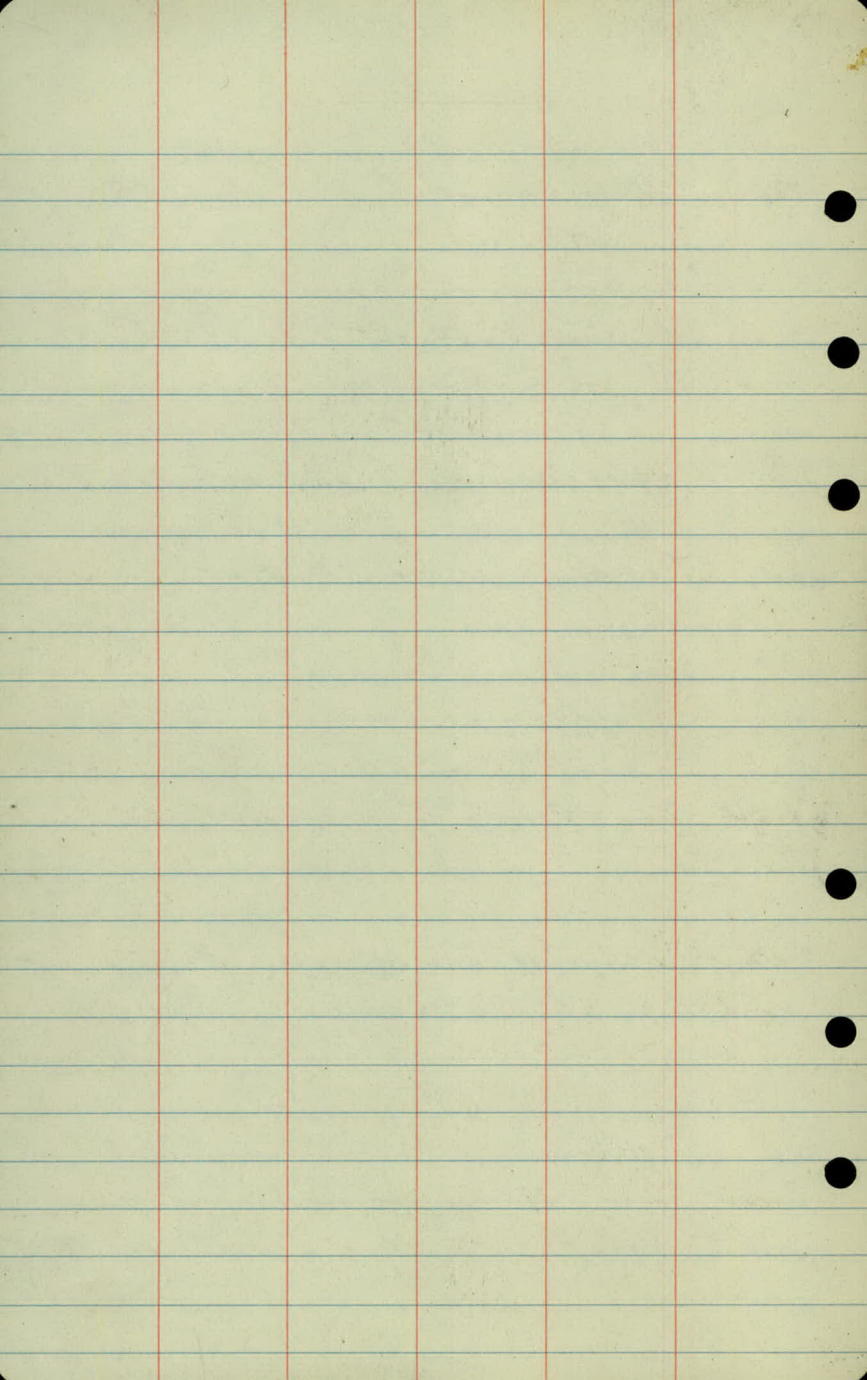
999.99928
0037815

9999.357
0113444



Description

- Top of stone Mon. @ "C" and Rice Sts.
- Spike in 18" Oak 150' Rt. Sta. 67+35
- Top of Stone Mon. @ "C" and Western
- Spike in 8" Elm 125' Rt. Sta. 51+50
- Top of Stone Mon. @ "C" and Dale St.
- North End, top of lower concrete step of dwelling, Rt. Sta. 16+80.
- Power Tower #165, top of bottom angle plate, West plate, N.W. Cor., Lt. Sta. 54+75



Preliminary X-Sections
1/38

Sta.	+	-	Elev.
B.M.	8.65	889.54	890.89

0+00			95.0	Victoria St.
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+15			95.0	
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+43			94.4	
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+65			93.5	
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+100			93.6	
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T.P.	3.09	895.91	6.72	892.82
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+50			91.8	
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2			91.2	
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+50			90.8	
-----	--	--	------	--

3			90.3	
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+50			90.0	
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4			90.5	
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Power line steel tower #165, top of bottom angle plate, West plate, N.W. Cor. Lt. Sta. 5+75

97.84
95.00
Top Rail 42 42 45 53 51 58 57 43
3.7 37 50 31 22 48 67 83 100
100 72

6.8 6.9 4.4 4.9 8.6 8.7 8.1 5.4 4.8 4.5 5.1 5.8 5.6 6.1 5.9
100 76 86 68 58 50 35 27 17 4.5 50 77 83 90 100

9.4 6.8 6.6 5.1 4.9 6.1 10.8 10.8 9.8 5.7 6.2 5.6 5.7 6.3 6.1
94 89 86 87 74 67 59 45 26 17 5.1 19 23 50 83 123
94 94 100

10.1 6.7 6.8 5.7 5.4 6.2 6.4 11.2 11.2 10.6 6.3 6.7 7.3 5.4 5.0 5.6
57 80 87 84 73 70 67 57 40 25 18 6.0 9 20 27 50 100
10.1 100

7.2 6.0 5.9 6.8 7.4 12.1 11.9 12.0 7.7 6.9 7.7 8.6 12.0 12.6 12.5
88 83 75 71 67 58 41 22 14 6.9 9 15 22 50 100
7.2 7.0 100

9.1 9.4 5.1 4.1 5.2 9.7 10.0
50 23 14 4 12 22 50

9.9 10.2 6.1 5.1 4.7 5.4 5.6 10.4 10.6
50 22 14 11 4 8 12 20 50

10.2 10.4 6.7 6.0 5.1 5.4 6.0 11.1 10.9
50 22 15 11 5 6 11 20 50

R.R. Culv. Lt.

11.15 10.9 7.0 6.4 5.8 5.6 5.6 6.3 11.2 11.0
884.76 23 15 12 10 5.6 8 13 21 50

11.2 11.4 7.3 6.2 5.9 6.2 7.0 11.3 11.1
50 23 15 10 5 9 12 21 50

11.4 11.5 7.3 6.2 5.4 5.6 6.2 10.6 11.0
50 22 15 11 5 9 12 21 50

84.9

84.8

Sta.	+	π	-	Elev.
4+50		895.91		90.9

+70

Culvert

5

92.3

+50

94.8

T.P.	10.80	901.69	5.02	890.89
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6				97.7
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+20

898.89 Road Lt

T.P.	6.91	906.80	1.80	899.89
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+50				900.1
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7

02.2

+50

04.7

T.P.	11.13	916.48	1.45	905.35
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Lt.

2

24

18

$$\frac{114}{50} \frac{106}{22} \frac{61}{14} \frac{53}{9} \frac{50}{50} \frac{54}{9} \frac{60}{12} \frac{107}{21} \frac{106}{50}$$

$$\frac{121}{120} \\ 883.91$$

$$\frac{121}{1185} \\ 884.06$$

$$\frac{104}{50} \frac{58}{23} \frac{72}{16} \frac{48}{12} \frac{41}{9} \frac{36}{8} \frac{40}{8} \frac{42}{12} \frac{86}{20} \frac{96}{24} \frac{103}{50}$$

$$\frac{94}{50} \frac{88}{26} \frac{18}{18} \frac{13}{8} \frac{11}{8} \frac{13}{8} \frac{14}{12} \frac{92}{25} \frac{92}{50}$$

$$\frac{108}{50} \frac{98}{37} \frac{89}{24} \frac{51}{18} \frac{43}{15} \frac{40}{9} \frac{43}{9} \frac{48}{15} \frac{107}{25} \frac{120}{28} \frac{131}{34} \frac{135}{50}$$

$$\frac{69}{100} \frac{67}{88} \frac{57}{50} \frac{48}{37} \frac{32}{19} \frac{28}{50}$$

$$\frac{107}{50} \frac{112}{26} \frac{75}{19} \frac{71}{13} \frac{67}{11} \frac{72}{11} \frac{75}{14} \frac{161}{30} \frac{171}{37} \frac{175}{50}$$

$$\frac{77}{50} \frac{93}{24} \frac{57}{17} \frac{47}{14} \frac{47}{9} \frac{46}{13} \frac{49}{13} \frac{59}{19} \frac{107}{30} \frac{139}{35} \frac{144}{50}$$

$$\frac{28}{50} \frac{63}{29} \frac{62}{22} \frac{28}{17} \frac{22}{11} \frac{21}{15} \frac{27}{15} \frac{33}{18} \frac{90}{27} \frac{101}{30} \frac{101}{50}$$

Sta.	+	π	-	Elev.
		916.48		

8				07.0
---	--	--	--	------

+50				09.7
-----	--	--	--	------

9		1.		12.7
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T.P.	13.08	928.68	0.88	915.60
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+50				15.5
-----	--	--	--	------

10				18.3
----	--	--	--	------

+50				21.1
-----	--	--	--	------

11				23.7
----	--	--	--	------

T.P.	13.12	938.33	3.47	925.21
------	-------	--------	------	--------

+50				25.9
-----	--	--	--	------

12				28.0
----	--	--	--	------

+50				30.1
-----	--	--	--	------

41424419

$\frac{25}{50}$ $\frac{8.5}{41}$ $\frac{11.5}{28}$ $\frac{11.7}{21}$ $\frac{10.1}{18}$ $\frac{5.7}{15}$ $\frac{9.7}{12}$ $\frac{9.5}{11}$ $\frac{10.0}{11}$ $\frac{10.2}{14}$ $\frac{15.2}{24}$ $\frac{15.5}{28}$ $\frac{15.8}{50}$

$\frac{4.0}{50}$ $\frac{4.8}{42}$ $\frac{7.6}{28}$ $\frac{7.8}{21}$ $\frac{2.3}{17}$ $\frac{7.0}{13}$ $\frac{6.8}{11}$ $\frac{7.0}{11}$ $\frac{7.5}{14}$ $\frac{7.8}{16}$ $\frac{12.3}{27}$ $\frac{13.0}{50}$

$\frac{0.0}{50}$ $\frac{0.8}{38}$ $\frac{3.3}{26}$ $\frac{3.8}{14}$ $\frac{3.8}{14}$ $\frac{4.3}{14}$ $\frac{4.5}{14}$ $\frac{5.4}{18}$ $\frac{7.3}{27}$ $\frac{9.6}{50}$

$\frac{8.3}{50}$ $\frac{5.3}{41}$ $\frac{11.6}{28}$ $\frac{13.3}{17}$ $\frac{13.2}{17}$ $\frac{14.0}{15}$ $\frac{17.1}{25}$ $\frac{20.5}{50}$

$\frac{7.0}{50}$ $\frac{7.5}{41}$ $\frac{9.5}{29}$ $\frac{10.2}{16}$ $\frac{10.6}{13}$ $\frac{10.4}{10}$ $\frac{10.8}{9}$ $\frac{11.1}{14}$ $\frac{12.0}{18}$ $\frac{14.5}{26}$ $\frac{18.0}{50}$

$\frac{3.1}{50}$ $\frac{6.6}{34}$ $\frac{7.6}{22}$ $\frac{8.0}{15}$ $\frac{7.7}{10}$ $\frac{7.6}{10}$ $\frac{8.0}{10}$ $\frac{8.8}{19}$ $\frac{7.6}{22}$ $\frac{11.9}{50}$

$\frac{10.3}{50}$ $\frac{5.0}{30}$ $\frac{6.0}{17}$ $\frac{8.6}{14}$ $\frac{8.2}{9}$ $\frac{5.0}{50}$ $\frac{5.3}{9}$ $\frac{5.8}{18}$ $\frac{2.1}{27}$ $\frac{6.6}{50}$

$\frac{6.3}{50}$ $\frac{11.5}{28}$ $\frac{13.1}{15}$ $\frac{12.6}{10}$ $\frac{12.4}{10}$ $\frac{12.7}{10}$ $\frac{13.2}{19}$ $\frac{9.0}{27}$ $\frac{9.1}{33}$ $\frac{12.5}{50}$

$\frac{4.9}{50}$ $\frac{9.4}{31}$ $\frac{10.4}{22}$ $\frac{10.6}{14}$ $\frac{10.3}{10}$ $\frac{10.8}{12}$ $\frac{11.1}{20}$ $\frac{6.5}{28}$ $\frac{6.6}{35}$ $\frac{10.4}{50}$

$\frac{2.7}{50}$ $\frac{7.6}{28}$ $\frac{8.6}{15}$ $\frac{8.2}{12}$ $\frac{8.5}{12}$ $\frac{8.5}{21}$ $\frac{2.5}{31}$ $\frac{2.1}{38}$ $\frac{4.6}{50}$

Sta.	+	π	-	Elev.
13		938.33		32.4

+50				34.6
T.P.	11.82	948.53	1.62	936.71
14				37.3

+50				39.8
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15				41.9
----	--	--	--	------

+50				43.4
-----	--	--	--	------

16				43.8
----	--	--	--	------

+50				43.9
-----	--	--	--	------

17				43.5
----	--	--	--	------

+32

43.3
Drive Rt.

T.P.	3.39	947.15	4.77	943.76
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B.M.	3.81	947.15	3.81	943.34
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Lt.

E

Rt.

20

$\frac{0.0}{50}$	$\frac{5.3}{29}$	$\frac{6.6}{15}$	$\frac{6.2}{9}$	$\frac{5.9}{5}$	$\frac{6.2}{9}$	$\frac{6.8}{15}$	$\frac{6.3}{21}$	$\frac{12.1}{35}$	$\frac{12.3}{41}$	$\frac{11.0}{50}$
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$\frac{12.2}{50}$	$\frac{0.0}{42}$	$\frac{3.3}{30}$	$\frac{4.1}{24}$	$\frac{4.4}{15}$	$\frac{4.0}{10}$	$\frac{3.7}{5}$	$\frac{3.8}{10}$	$\frac{4.1}{16}$	$\frac{3.8}{22}$	$\frac{13.8}{35}$	$\frac{15.3}{44}$	$\frac{15.8}{50}$
-------------------	------------------	------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	-------------------	-------------------	-------------------

$\frac{6.4}{50}$	$\frac{11.1}{30}$	$\frac{12.0}{15}$	$\frac{11.5}{9}$	$\frac{11.2}{5}$	$\frac{11.3}{9}$	$\frac{11.7}{16}$	$\frac{11.3}{23}$	$\frac{4.0}{34}$	$\frac{2.7}{41}$	$\frac{2.5}{50}$
------------------	-------------------	-------------------	------------------	------------------	------------------	-------------------	-------------------	------------------	------------------	------------------

$\frac{5.1}{50}$	$\frac{5.5}{44}$	$\frac{8.8}{24}$	$\frac{9.3}{14}$	$\frac{9.0}{7}$	$\frac{8.7}{5}$	$\frac{8.8}{10}$	$\frac{8.5}{16}$	$\frac{9.2}{22}$	$\frac{2.5}{34}$	$\frac{1.4}{38}$	$\frac{2.1}{50}$
------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{4.2}{50}$	$\frac{2.9}{38}$	$\frac{6.8}{26}$	$\frac{7.0}{14}$	$\frac{6.8}{9}$	$\frac{6.6}{5}$	$\frac{6.8}{7}$	$\frac{7.4}{16}$	$\frac{7.3}{22}$	$\frac{2.8}{29}$	$\frac{1.3}{37}$	$\frac{1.8}{50}$
------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------	------------------

$\frac{4.7}{50}$	$\frac{2.9}{25}$	$\frac{5.0}{19}$	$\frac{5.5}{12}$	$\frac{5.1}{5}$	$\frac{5.3}{8}$	$\frac{5.4}{22}$	$\frac{2.7}{28}$	$\frac{3.3}{50}$
------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------

$\frac{3.6}{50}$	$\frac{4.5}{21}$	$\frac{4.8}{10}$	$\frac{4.7}{5}$	$\frac{5.0}{11}$	$\frac{4.9}{17}$	$\frac{4.1}{26}$	$\frac{5.5}{50}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------

$\frac{3.9}{50}$	$\frac{4.5}{11}$	$\frac{4.8}{8}$	$\frac{4.6}{5}$	$\frac{5.0}{10}$	$\frac{5.4}{31}$	$\frac{6.2}{50}$
------------------	------------------	-----------------	-----------------	------------------	------------------	------------------

$\frac{4.1}{50}$	$\frac{4.0}{30}$	$\frac{5.1}{9}$	$\frac{5.0}{5}$	$\frac{5.3}{10}$	$\frac{5.2}{22}$	$\frac{5.5}{50}$
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$\frac{5.2}{5}$	$\frac{5.5}{23}$	$\frac{5.7}{50}$
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North end, top of tower concrete step of dwelling, Rt. of Sta. 16+80

Sta.	+	π	-	Elev.
17	+50	947.15		43.4

18				42.8
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+50				42.0
-----	--	--	--	------

19				41.8
----	--	--	--	------

+50				41.2
-----	--	--	--	------

+84				41.0
-----	--	--	--	------

Drive Lt.

20				40.7
----	--	--	--	------

Drive Rt.

+50				39.8
-----	--	--	--	------

21				39.2
----	--	--	--	------

+50				38.7
-----	--	--	--	------

22				38.2
----	--	--	--	------

+50				37.9
-----	--	--	--	------

T.P.	1.15	939.64	8.66	938.49
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Lt.

E

Rt.

21

$$\frac{3.8}{50} \quad \frac{3.7}{25} \quad \frac{4.1}{10} \quad \frac{3.8}{50} \quad \frac{4.2}{12} \quad \frac{4.5}{50}$$

$$\frac{4.5}{50} \quad \frac{4.8}{30} \quad \frac{4.8}{9} \quad \frac{4.4}{50} \quad \frac{4.7}{10} \quad \frac{4.4}{19} \quad \frac{4.0}{29} \quad \frac{4.0}{50}$$

$$\frac{4.9}{50} \quad \frac{5.2}{18} \quad \frac{5.3}{9} \quad \frac{5.2}{50} \quad \frac{5.3}{12} \quad \frac{5.0}{16} \quad \frac{4.4}{33} \quad \frac{4.2}{50}$$

$$\frac{5.8}{50} \quad \frac{5.8}{15} \quad \frac{6.0}{10} \quad \frac{5.4}{50} \quad \frac{5.4}{15} \quad \frac{4.6}{30} \quad \frac{4.8}{50}$$

$$\frac{5.3}{50} \quad \frac{6.4}{40} \quad \frac{6.4}{15} \quad \frac{6.3}{10} \quad \frac{6.0}{50} \quad \frac{6.3}{11} \quad \frac{4.7}{25} \quad \frac{4.5}{50}$$

$$\frac{6.2}{50} \quad \frac{6.5}{30} \quad \frac{6.2}{50}$$

$$\frac{6.6}{50} \quad \frac{6.3}{22} \quad \frac{6.9}{16} \quad \frac{6.5}{50} \quad \frac{6.5}{11} \quad \frac{5.6}{29} \quad \frac{4.9}{50}$$

$$\frac{10.6}{50} \quad \frac{10.1}{28} \quad \frac{9.4}{19} \quad \frac{8.0}{13} \quad \frac{7.4}{50} \quad \frac{7.6}{11} \quad \frac{7.4}{20} \quad \frac{6.5}{50}$$

$$\frac{10.9}{50} \quad \frac{11.0}{32} \quad \frac{10.9}{20} \quad \frac{8.6}{13} \quad \frac{8.0}{50} \quad \frac{8.9}{15} \quad \frac{9.8}{20} \quad \frac{8.4}{50}$$

$$\frac{11.0}{50} \quad \frac{11.2}{29} \quad \frac{11.2}{21} \quad \frac{9.1}{12} \quad \frac{8.5}{50} \quad \frac{9.2}{15} \quad \frac{10.3}{20} \quad \frac{11.1}{40} \quad \frac{11.4}{50}$$

$$\frac{10.1}{50} \quad \frac{10.4}{30} \quad \frac{10.2}{16} \quad \frac{9.4}{10} \quad \frac{9.0}{50} \quad \frac{9.4}{12} \quad \frac{10.5}{18} \quad \frac{11.6}{32} \quad \frac{12.1}{50}$$

$$\frac{8.4}{50} \quad \frac{8.4}{35} \quad \frac{8.3}{17} \quad \frac{9.5}{11} \quad \frac{9.3}{50} \quad \frac{9.7}{12} \quad \frac{10.0}{18} \quad \frac{9.6}{21} \quad \frac{11.2}{50}$$

Sta.

+

K

-

Elev.

938.64

23

37.8

+50

37.3

24

36.8

+50

35.9

25

35.9

+50

35.5

+90

35.2

26

35.1

+22

35.1

+50

35.0

27

34.6

+50

33.6

$$\frac{1.1}{50} \quad \frac{0.7}{34} \quad \frac{1.5}{18} \quad \frac{2.0}{11} \quad \frac{1.8}{1} \quad \frac{2.2}{10} \quad \frac{1.4}{21} \quad \frac{1.8}{50}$$

$$\frac{2.6}{50} \quad \frac{2.5}{20} \quad \frac{2.7}{12} \quad \frac{2.3}{1} \quad \frac{2.4}{11} \quad \frac{2.4}{18} \quad \frac{1.1}{25} \quad \frac{1.0}{50}$$

$$\frac{3.1}{50} \quad \frac{3.4}{19} \quad \frac{3.2}{11} \quad \frac{2.8}{1} \quad \frac{2.3}{10} \quad \frac{3.0}{20} \quad \frac{2.4}{50}$$

$$\frac{3.4}{50} \quad \frac{3.7}{18} \quad \frac{3.7}{9} \quad \frac{3.7}{1} \quad \frac{3.9}{11} \quad \frac{4.2}{21} \quad \frac{5.0}{50}$$

$$\frac{4.0}{50} \quad \frac{4.7}{29} \quad \frac{4.4}{10} \quad \frac{3.7}{1} \quad \frac{4.4}{10} \quad \frac{5.6}{21} \quad \frac{6.3}{42} \quad \frac{6.6}{50} \quad \text{Drive Rt.}$$

$$\frac{6.2}{50} \quad \frac{6.4}{38} \quad \frac{6.0}{17} \quad \frac{4.7}{9} \quad \frac{4.1}{1} \quad \frac{4.6}{10} \quad \frac{6.5}{21} \quad \frac{7.4}{50}$$

$$\frac{7.5}{50} \quad \frac{7.4}{35} \quad \frac{7.0}{24} \quad \frac{5.2}{11} \quad \frac{4.4}{1} \quad \frac{5.0}{10} \quad \frac{6.4}{23} \quad \frac{7.0}{43} \quad \frac{7.0}{50}$$

$$\frac{7.5}{50} \quad \frac{6.7}{19} \quad \frac{5.3}{12} \quad \frac{4.5}{1} \quad \frac{4.9}{9} \quad \frac{6.4}{28} \quad \frac{7.3}{50} \quad \text{Drive Rt.}$$

$$\frac{6.6}{50} \quad \frac{5.8}{25} \quad \frac{5.7}{16} \quad \frac{5.2}{10} \quad \frac{4.5}{1} \quad \frac{5.2}{12} \quad \frac{5.6}{23} \quad \frac{6.4}{50}$$

$$\frac{5.0}{50} \quad \frac{4.1}{20} \quad \frac{4.7}{17} \quad \frac{5.2}{12} \quad \frac{4.6}{1} \quad \frac{4.9}{9} \quad \frac{5.2}{14} \quad \frac{4.2}{22} \quad \frac{4.0}{50}$$

$$\frac{2.9}{50} \quad \frac{2.6}{33} \quad \frac{3.2}{19} \quad \frac{5.5}{14} \quad \frac{5.4}{10} \quad \frac{5.0}{1} \quad \frac{5.3}{9} \quad \frac{4.5}{17} \quad \frac{3.9}{26} \quad \frac{4.6}{50}$$

$$\frac{3.4}{50} \quad \frac{3.3}{34} \quad \frac{4.2}{22} \quad \frac{6.4}{14} \quad \frac{6.4}{11} \quad \frac{6.0}{1} \quad \frac{6.4}{9} \quad \frac{5.9}{15} \quad \frac{5.1}{26} \quad \frac{4.8}{50}$$

Sta.	+	π	-	Elev.
28		939.64		32.5

+50

31.5

29

30.5

+21

29.9
Drive
Lk.

+38

29.1

+85

26.6

30

25.8

Drive Rt.

T.P.	1.65	929.18	12.11	927.53
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+32

24.3

+50

23.5

+85

22.2

31

21.8

+14.33

21.5

B.M.	7.71	929.18	7.71	921.47
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44.4121.

23

$$\frac{5.2}{50} \quad \frac{5.7}{34} \quad \frac{6.5}{22} \quad \frac{7.3}{12} \quad \frac{7.1}{10} \quad \frac{7.3}{16} \quad \frac{7.0}{31} \quad \frac{5.9}{50} \quad \frac{5.4}{50}$$

$$\frac{6.1}{80} \quad \frac{6.0}{31} \quad \frac{7.2}{22} \quad \frac{8.7}{16} \quad \frac{8.5}{11} \quad \frac{8.1}{9} \quad \frac{8.4}{16} \quad \frac{7.9}{31} \quad \frac{6.6}{50} \quad \frac{6.4}{50}$$

$$\frac{4.9}{50} \quad \frac{5.0}{44} \quad \frac{6.1}{36} \quad \frac{7.8}{22} \quad \frac{9.2}{16} \quad \frac{9.3}{10} \quad \frac{9.1}{7} \quad \frac{9.4}{13} \quad \frac{9.0}{26} \quad \frac{7.3}{50} \quad \frac{7.0}{50}$$

$$\frac{6.5}{50} \quad \frac{8.4}{29} \quad \frac{9.9}{12} \quad \frac{9.7}{12}$$

$$\frac{4.8}{50} \quad \frac{5.2}{33} \quad \frac{6.1}{26} \quad \frac{10.9}{16} \quad \frac{10.7}{11} \quad \frac{10.5}{6} \quad \frac{11.0}{9} \quad \frac{11.9}{23} \quad \frac{8.5}{50} \quad \frac{7.9}{50}$$

$$\frac{9.6}{50} \quad \frac{9.5}{40} \quad \frac{10.6}{25} \quad \frac{13.6}{17} \quad \frac{13.4}{12} \quad \frac{13.0}{9} \quad \frac{13.6}{11} \quad \frac{13.8}{13} \quad \frac{12.1}{50} \quad \frac{12.4}{50}$$

$$\frac{10.3}{50} \quad \frac{9.9}{41} \quad \frac{12.2}{25} \quad \frac{14.1}{17} \quad \frac{13.9}{11} \quad \frac{13.8}{6} \quad \frac{14.2}{13} \quad \frac{14.4}{50} \quad \frac{14.5}{50}$$

$$\frac{2.1}{50} \quad \frac{2.1}{31} \quad \frac{4.6}{24} \quad \frac{5.2}{17} \quad \frac{5.0}{11} \quad \frac{4.9}{5} \quad \frac{5.3}{12} \quad \frac{5.5}{13} \quad \frac{5.1}{42} \quad \frac{4.7}{50} \quad \frac{4.6}{50}$$

$$\frac{5.3}{50} \quad \frac{5.6}{16} \quad \frac{6.1}{10} \quad \frac{6.0}{5} \quad \frac{5.7}{12} \quad \frac{5.8}{17} \quad \frac{6.0}{36} \quad \frac{5.3}{50} \quad \frac{4.2}{50}$$

$$\frac{6.5}{50} \quad \frac{7.4}{47} \quad \frac{7.5}{43} \quad \frac{7.2}{38} \quad \frac{7.1}{24} \quad \frac{6.8}{12} \quad \frac{7.0}{8} \quad \frac{7.5}{13} \quad \frac{7.1}{21} \quad \frac{7.2}{50}$$

$$\frac{7.2}{50} \quad \frac{7.3}{35} \quad \frac{7.0}{22} \quad \frac{7.4}{6} \quad \frac{7.7}{20} \quad \frac{8.1}{26} \quad \frac{10.3}{50} \quad \frac{10.9}{50}$$

$$\frac{6.0}{100} \quad \frac{6.8}{50} \quad \frac{7.7}{50} \quad \frac{10.8}{100} \quad \frac{12.9}{100}$$

Date St.

Top of Stone Mon. @ "C" + Date Sts.

Sta.	+	π	-	Elev.
		929.18		
31+38				21.3
+50				21.4
32				21.4
+40				21.5
+80				21.7
33				21.6
+50				21.8
34				22.6
+50				23.8
T.P.	6.33	934.64 [✓]	0.87	928.31 [✓]
35				25.5
+50				27.3
T.P.	10.25	941.76 [✓]	3.13	931.51 [✓]

Lt.

C

Rt.

$$\frac{8.3}{50} \quad \frac{8.8}{28} \quad \frac{8.1}{24} \quad \frac{7.8}{12} \quad \frac{7.9}{\cancel{1}} \quad \frac{8.2}{7} \quad \frac{8.0}{17} \quad \frac{9.8}{22} \quad \frac{10.4}{26} \quad \frac{10.9}{50}$$

$$\frac{5.5}{50} \quad \frac{6.2}{24} \quad \frac{6.7}{20} \quad \frac{8.2}{16} \quad \frac{7.8}{11} \quad \frac{7.8}{\cancel{12}} \quad \frac{8.4}{12} \quad \frac{10.1}{18} \quad \frac{9.8}{23} \quad \frac{9.2}{50}$$

$$\frac{6.3}{50} \quad \frac{6.7}{22} \quad \frac{7.8}{16} \quad \frac{7.8}{12} \quad \frac{7.8}{\cancel{11}} \quad \frac{8.2}{11} \quad \frac{9.2}{18} \quad \frac{8.9}{20} \quad \frac{9.5}{32} \quad \frac{11.3}{50}$$

$$\frac{7.2}{50} \quad \frac{7.3}{19} \quad \frac{7.8}{15} \quad \frac{7.8}{11} \quad \frac{7.7}{\cancel{9}} \quad \frac{8.0}{9} \quad \frac{8.2}{11} \quad \frac{10.4}{22} \quad \frac{14.2}{50}$$

$$\frac{3.8}{50} \quad \frac{4.4}{35} \quad \frac{7.4}{18} \quad \frac{7.6}{12} \quad \frac{7.5}{\cancel{5}} \quad \frac{7.8}{5} \quad \frac{8.1}{9} \quad \frac{12.7}{20} \quad \frac{13.7}{24} \quad \frac{16.7}{50}$$

$$\frac{3.3}{50} \quad \frac{4.3}{36} \quad \frac{7.2}{21} \quad \frac{7.4}{12} \quad \frac{7.6}{\cancel{10}} \quad \frac{8.4}{10} \quad \frac{16.2}{22} \quad \frac{17.0}{28} \quad \frac{18.7}{50}$$

$$\frac{4.1}{50} \quad \frac{6.5}{38} \quad \frac{7.4}{19} \quad \frac{7.2}{13} \quad \frac{7.4}{\cancel{10}} \quad \frac{8.4}{10} \quad \frac{17.4}{23} \quad \frac{18.8}{28} \quad \frac{21.4}{50}$$

$$\frac{2.4}{50} \quad \frac{5.2}{31} \quad \frac{6.0}{19} \quad \frac{6.7}{17} \quad \frac{6.6}{11} \quad \frac{6.6}{\cancel{10}} \quad \frac{7.5}{10} \quad \frac{16.7}{24} \quad \frac{17.8}{31} \quad \frac{20.5}{50}$$

$$\frac{+1.6}{50} \quad \frac{00}{35} \quad \frac{3.6}{19} \quad \frac{5.6}{12} \quad \frac{5.4}{\cancel{11}} \quad \frac{6.3}{11} \quad \frac{14.0}{24} \quad \frac{15.2}{28} \quad \frac{16.8}{40} \quad \frac{18.5}{50}$$

$$\frac{0.4}{50} \quad \frac{4.0}{34} \quad \frac{7.0}{20} \quad \frac{10.0}{15} \quad \frac{10.0}{11} \quad \frac{9.1}{\cancel{11}} \quad \frac{10.1}{11} \quad \frac{17.5}{25} \quad \frac{18.8}{30} \quad \frac{22.6}{50}$$

$$\frac{+1.6}{50} \quad \frac{00}{40} \quad \frac{4.7}{19} \quad \frac{7.3}{15} \quad \frac{7.6}{12} \quad \frac{7.3}{\cancel{12}} \quad \frac{8.2}{12} \quad \frac{17.5}{25} \quad \frac{19.0}{32} \quad \frac{22.6}{50}$$

Sta. + π - Elev.

36 941.76 29.2

+50 31.5

+85 32.8

37 33.6

+50 35.3

38 36.0

+50 35.8

39 35.2

T.P. 3.17 937.80 7.13 934.63

+50 34.6

+86

34.2
Drive Lt.

40 33.7

+15 33.3

T.P. 11.27 937.13 11.94 925.86

Lt.

L

Rt.

25

$$\frac{4.6}{50} \quad \frac{6.8}{35} \quad \frac{9.3}{21} \quad \frac{12.7}{15} \quad \frac{12.8}{11} \quad \frac{12.6}{-} \quad \frac{13.1}{9} \quad \frac{13.4}{14} \quad \frac{14.6}{24} \quad \frac{21.1}{28} \quad \frac{21.7}{33} \quad \frac{25.1}{50}$$

$$\frac{5.7}{50} \quad \frac{7.4}{22} \quad \frac{10.5}{15} \quad \frac{10.8}{11} \quad \frac{10.3}{-} \quad \frac{10.8}{9} \quad \frac{11.0}{19} \quad \frac{12.4}{25} \quad \frac{16.3}{50}$$

$$\frac{5.6}{50} \quad \frac{5.7}{22} \quad \frac{9.1}{15} \quad \frac{9.2}{11} \quad \frac{9.0}{-} \quad \frac{9.3}{8} \quad \frac{9.3}{13} \quad \frac{7.9}{21} \quad \frac{8.8}{32} \quad \frac{10.7}{50}$$

$$\frac{5.4}{50} \quad \frac{5.7}{21} \quad \frac{8.5}{15} \quad \frac{8.7}{12} \quad \frac{8.2}{-} \quad \frac{8.7}{9} \quad \frac{8.7}{14} \quad \frac{4.6}{23} \quad \frac{9.1}{50}$$

$$\frac{4.4}{50} \quad \frac{3.8}{20} \quad \frac{6.6}{15} \quad \frac{6.9}{10} \quad \frac{6.5}{-} \quad \frac{7.0}{11} \quad \frac{6.6}{16} \quad \frac{2.0}{24} \quad \frac{7.1}{50}$$

$$\frac{2.7}{50} \quad \frac{2.2}{19} \quad \frac{5.8}{13} \quad \frac{6.0}{9} \quad \frac{5.8}{-} \quad \frac{6.3}{11} \quad \frac{6.6}{15} \quad \frac{3.3}{21} \quad \frac{9.2}{50}$$

$$\frac{2.1}{50} \quad \frac{2.7}{20} \quad \frac{6.3}{12} \quad \frac{6.2}{8} \quad \frac{6.0}{-} \quad \frac{6.4}{9} \quad \frac{6.7}{16} \quad \frac{5.6}{20} \quad \frac{8.7}{34} \quad \frac{11.9}{50}$$

$$\frac{3.4}{50} \quad \frac{4.1}{29} \quad \frac{4.8}{19} \quad \frac{6.7}{13} \quad \frac{6.7}{8} \quad \frac{6.6}{-} \quad \frac{7.2}{8} \quad \frac{7.5}{15} \quad \frac{7.2}{22} \quad \frac{7.2}{26} \quad \frac{12.0}{36} \quad \frac{14.6}{50}$$

$$\frac{0.0}{50} \quad \frac{0.8}{20} \quad \frac{3.2}{13} \quad \frac{3.2}{9} \quad \frac{3.2}{-} \quad \frac{3.5}{8} \quad \frac{3.9}{13} \quad \frac{5.0}{18} \quad \frac{6.9}{25} \quad \frac{12.3}{50}$$

$$\frac{12.9}{29} \quad \frac{10.5}{50} \quad \frac{1.4}{33} \quad \frac{2.9}{17} \quad \frac{3.5}{9} \quad \frac{3.6}{-}$$

$$\frac{10.8}{50} \quad \frac{0.7}{29} \quad \frac{2.9}{18} \quad \frac{4.2}{8} \quad \frac{4.1}{-} \quad \frac{4.4}{8} \quad \frac{5.0}{16} \quad \frac{4.4}{19} \quad \frac{4.6}{21} \quad \frac{11.6}{50}$$

$$\frac{13.5}{50} \quad \frac{13.5}{25} \quad \frac{4.4}{13} \quad \frac{4.7}{9} \quad \frac{4.5}{-} \quad \frac{4.7}{8} \quad \frac{5.3}{15} \quad \frac{3.9}{19} \quad \frac{4.2}{21} \quad \frac{11.6}{50}$$

Sta.	+	π	-	Elev.
40+50		937.13		32.5
41				31.6
+50				30.2
42				28.7
T.P.	5.78	931.64	11.27	925.86
+50				27.5
43				26.9
+50				26.3
44				26.0
T.P.	4.11	929.97	5.78	925.86
+50				25.7
45				25.1
+50				24.8
46				23.6

Lt.

C

Rt.

26

$$\begin{array}{r} +6.2 \\ 50 \end{array} \quad \begin{array}{r} +4.9 \\ 25 \end{array} \quad \begin{array}{r} 3.1 \\ 15 \end{array} \quad \begin{array}{r} 4.6 \\ 8 \end{array} \quad \begin{array}{r} 4.6 \\ \cancel{4} \end{array} \quad \begin{array}{r} 5.0 \\ 7 \end{array} \quad \begin{array}{r} 5.4 \\ 15 \end{array} \quad \begin{array}{r} 4.0 \\ 19 \end{array} \quad \begin{array}{r} 5.2 \\ 27 \end{array} \quad \begin{array}{r} 13.4 \\ 50 \end{array}$$

$$\begin{array}{r} +6.1 \\ 50 \end{array} \quad \begin{array}{r} +4.1 \\ 28 \end{array} \quad \begin{array}{r} 4.0 \\ 17 \end{array} \quad \begin{array}{r} 5.5 \\ 13 \end{array} \quad \begin{array}{r} 5.8 \\ 8 \end{array} \quad \begin{array}{r} 5.5 \\ \cancel{5} \end{array} \quad \begin{array}{r} 5.7 \\ 9 \end{array} \quad \begin{array}{r} 6.8 \\ 18 \end{array} \quad \begin{array}{r} 12.0 \\ 29 \end{array} \quad \begin{array}{r} 19.0 \\ 50 \end{array}$$

$$\begin{array}{r} +3.6 \\ 50 \end{array} \quad \begin{array}{r} 0.8 \\ 27 \end{array} \quad \begin{array}{r} 4.2 \\ 23 \end{array} \quad \begin{array}{r} 6.7 \\ 16 \end{array} \quad \begin{array}{r} 6.9 \\ 9 \end{array} \quad \begin{array}{r} 6.9 \\ \cancel{6} \end{array} \quad \begin{array}{r} 7.4 \\ 7 \end{array} \quad \begin{array}{r} 8.5 \\ 14 \end{array} \quad \begin{array}{r} 18.4 \\ 30 \end{array} \quad \begin{array}{r} 22.7 \\ 40 \end{array} \quad \begin{array}{r} 26.4 \\ 50 \end{array}$$

$$\begin{array}{r} +1.6 \\ 50 \end{array} \quad \begin{array}{r} 3.1 \\ 34 \end{array} \quad \begin{array}{r} 5.4 \\ 26 \end{array} \quad \begin{array}{r} 8.0 \\ 19 \end{array} \quad \begin{array}{r} 8.4 \\ 9 \end{array} \quad \begin{array}{r} 8.4 \\ \cancel{8} \end{array} \quad \begin{array}{r} 9.0 \\ 11 \end{array} \quad \begin{array}{r} 20.4 \\ 27 \end{array} \quad \begin{array}{r} 25.2 \\ 40 \end{array} \quad \begin{array}{r} 29.0 \\ 50 \end{array}$$

$$\begin{array}{r} +4.2 \\ 50 \end{array} \quad \begin{array}{r} 2.3 \\ 22 \end{array} \quad \begin{array}{r} 4.2 \\ 18 \end{array} \quad \begin{array}{r} 4.2 \\ 10 \end{array} \quad \begin{array}{r} 4.1 \\ \cancel{4} \end{array} \quad \begin{array}{r} 4.5 \\ 7 \end{array} \quad \begin{array}{r} 5.0 \\ 12 \end{array} \quad \begin{array}{r} 14.8 \\ 25 \end{array} \quad \begin{array}{r} 17.1 \\ 31 \end{array} \quad \begin{array}{r} 23.8 \\ 50 \end{array}$$

$$\begin{array}{r} +0.8 \\ 50 \end{array} \quad \begin{array}{r} 3.2 \\ 23 \end{array} \quad \begin{array}{r} 5.1 \\ 18 \end{array} \quad \begin{array}{r} 4.8 \\ 10 \end{array} \quad \begin{array}{r} 4.7 \\ \cancel{4} \end{array} \quad \begin{array}{r} 5.5 \\ 9 \end{array} \quad \begin{array}{r} 11.1 \\ 19 \end{array} \quad \begin{array}{r} 13.0 \\ 21 \end{array} \quad \begin{array}{r} 17.4 \\ 31 \end{array} \quad \begin{array}{r} 25.6 \\ 50 \end{array}$$

$$\begin{array}{r} 1.9 \\ 50 \end{array} \quad \begin{array}{r} 3.6 \\ 36 \end{array} \quad \begin{array}{r} 5.9 \\ 20 \end{array} \quad \begin{array}{r} 5.4 \\ 10 \end{array} \quad \begin{array}{r} 5.3 \\ \cancel{5} \end{array} \quad \begin{array}{r} 5.7 \\ 10 \end{array} \quad \begin{array}{r} 13.0 \\ 21 \end{array} \quad \begin{array}{r} 21.7 \\ 46 \end{array} \quad \begin{array}{r} 24.1 \\ 50 \end{array}$$

$$\begin{array}{r} 2.4 \\ 50 \end{array} \quad \begin{array}{r} 3.9 \\ 35 \end{array} \quad \begin{array}{r} 6.2 \\ 19 \end{array} \quad \begin{array}{r} 6.0 \\ 12 \end{array} \quad \begin{array}{r} 5.6 \\ \cancel{5} \end{array} \quad \begin{array}{r} 6.4 \\ 10 \end{array} \quad \begin{array}{r} 12.5 \\ 20 \end{array} \quad \begin{array}{r} 16.5 \\ 33 \end{array} \quad \begin{array}{r} 22.0 \\ 50 \end{array}$$

$$\begin{array}{r} 1.6 \\ 50 \end{array} \quad \begin{array}{r} 2.8 \\ 47 \end{array} \quad \begin{array}{r} 3.2 \\ 28 \end{array} \quad \begin{array}{r} 3.7 \\ 14 \end{array} \quad \begin{array}{r} 4.1 \\ 11 \end{array} \quad \begin{array}{r} 4.3 \\ \cancel{4} \end{array} \quad \begin{array}{r} 4.8 \\ 8 \end{array} \quad \begin{array}{r} 5.4 \\ 14 \end{array} \quad \begin{array}{r} 6.7 \\ 19 \end{array} \quad \begin{array}{r} 11.8 \\ 26 \end{array} \quad \begin{array}{r} 14.4 \\ 50 \end{array}$$

$$\begin{array}{r} +5.2 \\ 60 \end{array} \quad \begin{array}{r} +5.2 \\ 50 \end{array} \quad \begin{array}{r} 4.9 \\ 34 \end{array} \quad \begin{array}{r} 5.2 \\ 21 \end{array} \quad \begin{array}{r} 4.9 \\ 12 \end{array} \quad \begin{array}{r} 4.9 \\ \cancel{4} \end{array} \quad \begin{array}{r} 5.3 \\ 8 \end{array} \quad \begin{array}{r} 5.9 \\ 12 \end{array} \quad \begin{array}{r} 9.5 \\ 20 \end{array} \quad \begin{array}{r} 11.0 \\ 33 \end{array} \quad \begin{array}{r} 12.7 \\ 50 \end{array}$$

$$\begin{array}{r} +2.2 \\ 50 \end{array} \quad \begin{array}{r} +1.7 \\ 40 \end{array} \quad \begin{array}{r} 0.0 \\ 28 \end{array} \quad \begin{array}{r} 5.4 \\ 21 \end{array} \quad \begin{array}{r} 5.6 \\ 17 \end{array} \quad \begin{array}{r} 5.2 \\ \cancel{5} \end{array} \quad \begin{array}{r} 5.6 \\ 9 \end{array} \quad \begin{array}{r} 6.3 \\ 13 \end{array} \quad \begin{array}{r} 8.4 \\ 19 \end{array} \quad \begin{array}{r} 9.8 \\ 25 \end{array} \quad \begin{array}{r} 10.8 \\ 50 \end{array}$$

$$\begin{array}{r} 2.0 \\ 50 \end{array} \quad \begin{array}{r} 2.5 \\ 37 \end{array} \quad \begin{array}{r} 6.7 \\ 25 \end{array} \quad \begin{array}{r} 7.3 \\ 20 \end{array} \quad \begin{array}{r} 7.3 \\ 16 \end{array} \quad \begin{array}{r} 6.4 \\ \cancel{6} \end{array} \quad \begin{array}{r} 6.8 \\ 10 \end{array} \quad \begin{array}{r} 7.3 \\ 14 \end{array} \quad \begin{array}{r} 8.0 \\ 21 \end{array} \quad \begin{array}{r} 8.0 \\ 36 \end{array} \quad \begin{array}{r} 8.0 \\ 50 \end{array}$$

Sta.	+	π	-	Elev.	Drive Rt.
46+28		929.97			

+50

22.6

47

22.0

+50

21.0

48

19.8

+15

19.5

+50

18.4

+72

17.7

49

16.8

T.P.

1.56

918.30

13.23

916.74

+50

14.8

50

12.6

B.M.

1.40

913.08

6.62

911.68 ✓

+50

10.8

Lt.

L

Rt.

27

$$\frac{7.1}{-} \quad \frac{7.1}{11} \quad \frac{2.3}{21} \quad \frac{7.0}{50}$$

$$\frac{5.6}{50} \quad \frac{6.0}{33} \quad \frac{8.2}{27} \quad \frac{7.8}{11} \quad \frac{7.4}{-} \quad \frac{2.7}{12} \quad \frac{7.9}{16} \quad \frac{7.5}{28} \quad \frac{6.0}{50}$$

$$\frac{8.4}{50} \quad \frac{9.6}{27} \quad \frac{8.7}{21} \quad \frac{8.4}{13} \quad \frac{8.0}{9} \quad \frac{8.0}{-} \quad \frac{8.5}{10} \quad \frac{8.3}{17} \quad \frac{5.7}{34} \quad \frac{3.7}{50}$$

$$\frac{6.1}{50} \quad \frac{7.7}{27} \quad \frac{8.2}{20} \quad \frac{9.7}{15} \quad \frac{9.4}{9} \quad \frac{9.0}{-} \quad \frac{9.1}{7} \quad \frac{8.8}{12} \quad \frac{8.4}{16} \quad \frac{7.0}{23} \quad \frac{4.9}{50}$$

$$\frac{2.5}{50} \quad \frac{3.5}{34} \quad \frac{5.7}{28} \quad \frac{6.2}{25} \quad \frac{9.1}{21} \quad \frac{10.7}{17} \quad \frac{10.2}{8} \quad \frac{10.2}{-} \quad \frac{10.5}{7} \quad \frac{10.4}{12} \quad \frac{8.5}{19} \quad \frac{6.6}{34} \quad \frac{5.6}{50}$$

$$\frac{9.9}{50} \quad \frac{10.7}{23} \quad \frac{11.3}{14} \quad \frac{10.6}{8} \quad \frac{10.5}{-} \quad \frac{11.0}{9} \quad \frac{10.3}{15} \quad \frac{7.0}{20} \quad \frac{6.6}{23} \quad \frac{5.8}{27} \quad \frac{5.5}{50}$$

$$\frac{9.6}{50} \quad \frac{11.7}{25} \quad \frac{12.2}{19} \quad \frac{12.2}{12} \quad \frac{11.8}{7} \quad \frac{11.6}{-} \quad \frac{11.8}{9} \quad \frac{11.3}{17} \quad \frac{6.9}{25} \quad \frac{5.8}{31} \quad \frac{5.4}{50}$$

$$\frac{2.0}{50} \quad \frac{2.6}{42} \quad \frac{8.1}{41} \quad \frac{11.8}{34} \quad \frac{12.5}{23} \quad \frac{13.1}{18} \quad \frac{12.6}{9} \quad \frac{12.3}{-} \quad \frac{12.7}{9} \quad \frac{12.7}{14} \quad \frac{12.0}{24} \quad \frac{13.2}{50}$$

$$\frac{7.4}{50} \quad \frac{5.7}{39} \quad \frac{8.4}{35} \quad \frac{13.0}{27} \quad \frac{13.9}{23} \quad \frac{14.3}{16} \quad \frac{13.6}{9} \quad \frac{13.2}{-} \quad \frac{13.8}{10} \quad \frac{13.8}{22} \quad \frac{12.9}{32} \quad \frac{12.1}{50}$$

$$\frac{4.7}{50} \quad \frac{0.4}{37} \quad \frac{3.6}{31} \quad \frac{4.5}{22} \quad \frac{4.6}{16} \quad \frac{3.8}{8} \quad \frac{3.5}{-} \quad \frac{3.9}{8} \quad \frac{4.3}{17} \quad \frac{3.3}{30} \quad \frac{6.4}{38} \quad \frac{6.7}{50}$$

$$\frac{15.5}{50} \quad \frac{13.1}{40} \quad \frac{9.0}{28} \quad \frac{5.4}{18} \quad \frac{6.0}{15} \quad \frac{5.8}{8} \quad \frac{5.7}{-} \quad \frac{6.2}{11} \quad \frac{7.0}{15} \quad \frac{8.9}{27} \quad \frac{9.2}{50}$$

Spike in 8" Elm 125' Rt. 515. 51450

$$\frac{15.2}{50} \quad \frac{12.5}{28} \quad \frac{9.1}{19} \quad \frac{2.8}{8} \quad \frac{2.3}{-} \quad \frac{2.8}{15} \quad \frac{2.5}{21} \quad \frac{1.4}{37} \quad \frac{2.6}{50}$$

Sta.	+	π	-	Elev.
51		913.08		08.1

+50				07.3
-----	--	--	--	------

+72

Culvert

52				06.7
----	--	--	--	------

+50

06.6

T.P.	0.04	911.72	1.40	911.68
------	------	--------	------	--------

+68

Culvert

53				06.6
----	--	--	--	------

+50

07.6

54				09.4
----	--	--	--	------

T.P.	12.89	923.26	1.35	910.37
------	-------	--------	------	--------

+50

11.7

55				13.7
----	--	--	--	------

+50

15.9

OK

Lt.

L

Rt.

28

$$\frac{17.2}{50} \quad \frac{15.4}{31} \quad \frac{11.8}{18} \quad \frac{5.6}{9} \quad \frac{5.0}{5} \quad \frac{5.0}{5} \quad \frac{4.9}{10} \quad \frac{5.2}{15} \quad \frac{8.2}{24} \quad \frac{9.0}{34} \quad \frac{6.0}{44} \quad \frac{5.7}{50}$$

$$\frac{15.5}{50} \quad \frac{15.6}{23} \quad \frac{6.4}{9} \quad \frac{5.8}{5} \quad \frac{6.2}{13} \quad \frac{6.9}{16} \quad \frac{11.4}{24} \quad \frac{12.8}{28} \quad \frac{13.0}{50}$$

$$\frac{14.1}{15.6}$$

$$\frac{14.1}{15.3}$$

$$\frac{14.2}{50} \quad \frac{15.1}{26} \quad \frac{14.3}{21} \quad \frac{7.3}{10} \quad \frac{6.7}{7} \quad \frac{6.4}{5} \quad \frac{6.4}{9} \quad \frac{6.9}{14} \quad \frac{7.5}{17} \quad \frac{11.5}{24} \quad \frac{12.2}{26} \quad \frac{13.2}{43} \quad \frac{13.1}{50}$$

$$\frac{14.8}{50} \quad \frac{13.2}{17} \quad \frac{7.3}{9} \quad \frac{6.7}{5} \quad \frac{6.5}{5} \quad \frac{6.4}{9} \quad \frac{6.9}{14} \quad \frac{9.8}{19} \quad \frac{10.4}{22} \quad \frac{10.7}{42} \quad \frac{7.6}{50}$$

$$\frac{14.1}{11.65}$$

$$\frac{14.1}{8.0}$$

$$\frac{13.4}{50} \quad \frac{12.2}{20} \quad \frac{10.4}{15} \quad \frac{6.0}{8} \quad \frac{5.1}{5} \quad \frac{5.0}{9} \quad \frac{5.2}{13} \quad \frac{8.2}{18} \quad \frac{8.0}{31} \quad \frac{8.0}{50}$$

$$\frac{13.7}{50} \quad \frac{13.0}{25} \quad \frac{5.6}{11} \quad \frac{4.7}{9} \quad \frac{4.1}{5} \quad \frac{4.1}{8} \quad \frac{4.4}{13} \quad \frac{6.1}{18} \quad \frac{5.7}{31} \quad \frac{4.5}{50}$$

$$\frac{12.6}{50} \quad \frac{8.4}{21} \quad \frac{4.2}{13} \quad \frac{2.7}{9} \quad \frac{2.4}{5} \quad \frac{2.3}{5} \quad \frac{2.5}{10} \quad \frac{2.9}{17} \quad \frac{3.1}{26} \quad \frac{0.7}{30} \quad \frac{+1.0}{50}$$

$$\frac{18.7}{50} \quad \frac{10.8}{18} \quad \frac{12.4}{14} \quad \frac{11.8}{7} \quad \frac{11.6}{5} \quad \frac{11.7}{10} \quad \frac{12.9}{16} \quad \frac{12.1}{17} \quad \frac{11.9}{22} \quad \frac{+1.0}{33} \quad \frac{+0.9}{45} \quad \frac{+0.1}{50}$$

$$\frac{8.4}{50} \quad \frac{3.7}{30} \quad \frac{2.0}{23} \quad \frac{5.1}{16} \quad \frac{10.1}{12} \quad \frac{9.7}{6} \quad \frac{9.6}{9} \quad \frac{9.6}{15} \quad \frac{10.4}{16} \quad \frac{9.6}{18} \quad \frac{+2.4}{33} \quad \frac{+3.1}{50}$$

$$\frac{6.7}{50} \quad \frac{4.5}{21} \quad \frac{7.7}{16} \quad \frac{8.0}{14} \quad \frac{7.5}{10} \quad \frac{7.4}{5} \quad \frac{7.4}{8} \quad \frac{8.3}{16} \quad \frac{6.6}{17} \quad \frac{+1.3}{30} \quad \frac{+3.4}{36} \quad \frac{+4.4}{50}$$

Sta.	+	Σ	-	Elev.
		923.26		
56				18.3
+60				20.5
+87				22.1
T.P.	8.56	931.20	0.62	922.64
B.M.	7.62	931.20	7.62	923.58
57				22.6
+12				23.1
+27.45				23.6
+40				24.2
+50				24.5
+82				25.8
58				26.5
T.P.	10.76	941.49	0.47	930.73
+50				28.9

Lt.

E

Lt.

29

$$\frac{8.1}{50} \quad \frac{5.7}{27} \quad \frac{4.6}{19} \quad \frac{6.0}{16} \quad \frac{5.3}{9} \quad \frac{5.0}{50} \quad \frac{5.5}{10} \quad \frac{6.3}{14} \quad \frac{6.2}{16} \quad \frac{4.4}{19} \quad \frac{10.8}{26} \quad \frac{15.5}{50}$$

$$\frac{6.6}{50} \quad \frac{3.4}{19} \quad \frac{4.1}{17} \quad \frac{3.1}{10} \quad \frac{2.8}{7} \quad \frac{3.0}{7} \quad \frac{3.8}{13} \quad \frac{4.6}{15} \quad \frac{3.7}{17} \quad \frac{3.3}{20} \quad \frac{10.3}{24} \quad \frac{16}{28} \quad \frac{16.3}{50}$$

$$\frac{10.6}{50} \quad \frac{7.7}{33} \quad \frac{2.5}{25} \quad \frac{1.9}{16} \quad \frac{1.3}{7} \quad \frac{1.2}{7} \quad \frac{1.4}{7} \quad \frac{1.8}{14} \quad \frac{3.2}{17} \quad \frac{3.1}{19} \quad \frac{0.8}{26} \quad \frac{0.0}{28} \quad \frac{12.0}{36} \quad \frac{4.4}{50}$$

Top of Stone Monument "C" & Western

$$\frac{16.1}{58} \quad \frac{10.1}{33} \quad \frac{8.6}{21} \quad \frac{8.8}{11} \quad \frac{8.6}{8} \quad \frac{8.7}{12} \quad \frac{8.7}{20} \quad \frac{10.6}{24} \quad \frac{9.9}{34} \quad \frac{5.8}{44} \quad \frac{5.4}{50}$$

$$\frac{8.2}{50} \quad \frac{9.1}{39} \quad \frac{8.4}{15} \quad \frac{8.1}{8} \quad \frac{8.3}{15} \quad \frac{8.1}{35} \quad \frac{8.7}{50}$$

$$\frac{9.1}{100} \quad \frac{8.2}{50} \quad \frac{7.6}{7} \quad \frac{7.5}{9} \quad \frac{7.5}{30} \quad \frac{7.3}{50} \quad \frac{6.4}{100}$$

$$\frac{8.4}{50} \quad \frac{8.3}{41} \quad \frac{7.7}{28} \quad \frac{7.0}{12} \quad \frac{7.0}{7} \quad \frac{7.0}{9} \quad \frac{7.5}{30} \quad \frac{7.3}{50}$$

$$\frac{12.4}{55} \quad \frac{8.4}{41} \quad \frac{7.8}{30} \quad \frac{6.7}{12} \quad \frac{6.7}{7} \quad \frac{7.0}{10} \quad \frac{7.0}{20} \quad \frac{7.5}{25} \quad \frac{8.6}{30} \quad \frac{8.6}{50}$$

$$\frac{13.0}{50} \quad \frac{9.4}{30} \quad \frac{6.2}{20} \quad \frac{5.7}{10} \quad \frac{5.4}{7} \quad \frac{5.6}{7} \quad \frac{6.0}{12} \quad \frac{6.2}{15} \quad \frac{6.2}{18} \quad \frac{4.0}{22} \quad \frac{2.1}{50}$$

$$\frac{10.7}{50} \quad \frac{9.9}{43} \quad \frac{8.3}{28} \quad \frac{4.8}{19} \quad \frac{5.0}{17} \quad \frac{5.0}{10} \quad \frac{4.7}{7} \quad \frac{5.0}{8} \quad \frac{4.9}{17} \quad \frac{1.0}{23} \quad \frac{10.8}{28} \quad \frac{12.0}{44} \quad \frac{12.4}{50}$$

$$\frac{15.8}{50} \quad \frac{13.8}{36} \quad \frac{12.7}{24} \quad \frac{11.7}{21} \quad \frac{13.7}{16} \quad \frac{13.0}{10} \quad \frac{12.6}{7} \quad \frac{12.5}{6} \quad \frac{12.9}{12} \quad \frac{12.9}{15} \quad \frac{6.0}{26} \quad \frac{6.7}{50}$$

Sta. + π - Elev.

941.49

59 30.7

+50 32.7

+87 33.9

+97

Drive
Ret.

60+30 34.7

+80 35.2

61 35.3

+50 35.4

62 35.3

Drive Lt.

T.P. 6.00 941.35 6.14 935.35

+50 35.3

63 35.3

+50 35.4

+61 Drive Lt.
Same Sec.

64 35.5

Lt.

C

Rt.

30

$$\frac{10.4}{50} \quad \frac{7.0}{33} \quad \frac{6.2}{26} \quad \frac{11.0}{18} \quad \frac{11.0}{10} \quad \frac{10.8}{15} \quad \frac{10.8}{8} \quad \frac{10.9}{15} \quad \frac{4.1}{24} \quad \frac{3.9}{33} \quad \frac{3.6}{50}$$

$$\frac{7.0}{50} \quad \frac{3.2}{28} \quad \frac{8.1}{18} \quad \frac{9.0}{9} \quad \frac{8.8}{7} \quad \frac{8.9}{7} \quad \frac{9.1}{11} \quad \frac{9.0}{16} \quad \frac{2.2}{24} \quad \frac{1.8}{50}$$

$$\frac{7.9}{50} \quad \frac{3.4}{24} \quad \frac{8.4}{19} \quad \frac{8.1}{11} \quad \frac{7.6}{7} \quad \frac{7.8}{7} \quad \frac{7.4}{16} \quad \frac{0.8}{24} \quad \frac{0.6}{38} \quad \frac{1.3}{50}$$

$$\frac{7.4}{5} \quad \frac{2.5}{5} \quad \frac{2.6}{18} \quad \frac{5.6}{50}$$

$$\frac{9.7}{50} \quad \frac{7.3}{23} \quad \frac{7.4}{19} \quad \frac{7.4}{11} \quad \frac{6.8}{6} \quad \frac{7.0}{6} \quad \frac{7.1}{14} \quad \frac{2.1}{20} \quad \frac{1.8}{29} \quad \frac{2.1}{46} \quad \frac{2.5}{50}$$

$$\frac{11.2}{50} \quad \frac{9.5}{31} \quad \frac{7.5}{26} \quad \frac{6.5}{11} \quad \frac{6.3}{6} \quad \frac{6.5}{8} \quad \frac{6.4}{24} \quad \frac{7.1}{50}$$

$$\frac{10.2}{50} \quad \frac{9.1}{29} \quad \frac{7.2}{19} \quad \frac{6.4}{12} \quad \frac{6.2}{6} \quad \frac{6.5}{8} \quad \frac{7.2}{16} \quad \frac{7.2}{22} \quad \frac{9.1}{50}$$

$$\frac{9.3}{50} \quad \frac{9.0}{29} \quad \frac{7.0}{20} \quad \frac{6.2}{11} \quad \frac{6.1}{6} \quad \frac{6.7}{10} \quad \frac{8.4}{16} \quad \frac{9.6}{26} \quad \frac{10.4}{50}$$

$$\frac{7.0}{50} \quad \frac{7.1}{41} \quad \frac{7.0}{26} \quad \frac{6.2}{15} \quad \frac{6.2}{6} \quad \frac{6.6}{11} \quad \frac{10.4}{21} \quad \frac{10.5}{28} \quad \frac{11.2}{50}$$

$$\frac{6.7}{50} \quad \frac{8.1}{29} \quad \frac{8.1}{25} \quad \frac{8.1}{23} \quad \frac{6.3}{17} \quad \frac{6.1}{6} \quad \frac{6.8}{11} \quad \frac{10.3}{21} \quad \frac{10.3}{28} \quad \frac{10.2}{50}$$

$$\frac{6.1}{50} \quad \frac{6.5}{33} \quad \frac{8.1}{27} \quad \frac{7.7}{22} \quad \frac{6.2}{15} \quad \frac{6.1}{6} \quad \frac{6.5}{7} \quad \frac{7.0}{12} \quad \frac{9.5}{20} \quad \frac{9.3}{23} \quad \frac{8.5}{50}$$

$$\frac{5.5}{50} \quad \frac{6.2}{35} \quad \frac{7.3}{28} \quad \frac{7.6}{23} \quad \frac{6.2}{15} \quad \frac{6.0}{6} \quad \frac{6.3}{7} \quad \frac{6.5}{14} \quad \frac{9.0}{17} \quad \frac{9.0}{19} \quad \frac{6.1}{28} \quad \frac{6.0}{50}$$

$$\frac{4.0}{50} \quad \frac{5.3}{32} \quad \frac{7.0}{27} \quad \frac{7.6}{22} \quad \frac{5.9}{16} \quad \frac{5.9}{6} \quad \frac{6.5}{10} \quad \frac{8.7}{15} \quad \frac{10.3}{20} \quad \frac{8.5}{23} \quad \frac{8.0}{32} \quad \frac{7.3}{50}$$

Sta.	+	π	-	Elev.
64+50		941.35		35.6

+79

Current

65 36.2

+50

37.2

T.P. 9.40 947.77 2.98 938.37 ✓

66 38.4

+24

Drive Lt.

+50

39.6

67 40.6

B.M. 4.26 947.77 4.26 943.51 ✓

+70 41.8

68 42.7

+50 43.7

Lt.

E

Rt.

31

$\frac{4.7}{50}$ $\frac{5.6}{31}$ $\frac{7.6}{25}$ $\frac{7.6}{19}$ $\frac{6.0}{17}$ $\frac{5.8}{11}$ $\frac{6.1}{8}$ $\frac{6.6}{11}$ $\frac{12.1}{21}$ $\frac{12.4}{46}$ $\frac{12.3}{50}$

$\frac{12.4}{8.4}$

$\frac{12.4}{9.7}$

$\frac{3.8}{50}$ $\frac{4.9}{33}$ $\frac{7.3}{26}$ $\frac{7.3}{21}$ $\frac{5.2}{14}$ $\frac{5.2}{11}$ $\frac{6.0}{11}$ $\frac{8.2}{15}$ $\frac{9.4}{21}$ $\frac{10.2}{28}$ $\frac{11.5}{39}$ $\frac{12.5}{50}$

$\frac{2.6}{50}$ $\frac{3.0}{38}$ $\frac{3.9}{26}$ $\frac{4.1}{16}$ $\frac{4.2}{11}$ $\frac{4.6}{9}$ $\frac{6.4}{18}$ $\frac{7.3}{27}$ $\frac{8.4}{50}$

$\frac{8.6}{50}$ $\frac{9.0}{34}$ $\frac{10.7}{26}$ $\frac{10.7}{20}$ $\frac{9.7}{16}$ $\frac{9.4}{11}$ $\frac{10.1}{11}$ $\frac{12.1}{16}$ $\frac{12.5}{20}$ $\frac{9.8}{25}$ $\frac{10.3}{50}$

$\frac{8.8}{50}$

$\frac{8.9}{25}$

$\frac{8.8}{11}$

$\frac{10.4}{50}$ $\frac{10.0}{30}$ $\frac{9.7}{21}$ $\frac{8.7}{15}$ $\frac{8.2}{11}$ $\frac{8.7}{10}$ $\frac{9.3}{15}$ $\frac{11.7}{20}$ $\frac{11.6}{25}$ $\frac{8.3}{31}$ $\frac{7.0}{50}$

$\frac{10.2}{50}$ $\frac{10.1}{35}$ $\frac{9.2}{20}$ $\frac{7.7}{15}$ $\frac{7.2}{11}$ $\frac{7.7}{12}$ $\frac{9.7}{18}$ $\frac{9.8}{27}$ $\frac{5.5}{50}$

Spike in 18" Oak 150' Rt. 56. 67+35

$\frac{5.3}{50}$ $\frac{5.0}{24}$ $\frac{6.4}{19}$ $\frac{5.9}{10}$ $\frac{6.0}{11}$ $\frac{6.0}{8}$ $\frac{7.0}{16}$ $\frac{7.8}{21}$ $\frac{8.7}{25}$ $\frac{8.8}{30}$ $\frac{8.1}{50}$

$\frac{1.5}{50}$ $\frac{1.4}{25}$ $\frac{5.7}{18}$ $\frac{5.4}{10}$ $\frac{5.1}{11}$ $\frac{5.2}{9}$ $\frac{6.0}{19}$ $\frac{7.1}{23}$ $\frac{7.6}{29}$ $\frac{8.0}{50}$

$\frac{+4.0}{50}$ $\frac{+3.9}{26}$ $\frac{3.9}{17}$ $\frac{4.2}{9}$ $\frac{4.1}{11}$ $\frac{4.5}{10}$ $\frac{5.2}{19}$ $\frac{6.6}{28}$ $\frac{7.9}{50}$

Sta.	+	π	-	Elev.
		✓ 947.77		

69				44.5
----	--	--	--	------

+50				45.2
-----	--	--	--	------

+70				
-----	--	--	--	--

Drive Rt.

70				45.6
----	--	--	--	------

T.P.	5.98	✓ 950.51	3.04	✓ 944.73
------	------	-------------	------	-------------

+33				45.7
-----	--	--	--	------

+50				45.7
-----	--	--	--	------

71				45.6
----	--	--	--	------

+50				45.2
-----	--	--	--	------

72				45.0
----	--	--	--	------

+45				45.0
-----	--	--	--	------

+75				
-----	--	--	--	--

Drive Lt.

+83				44.9
-----	--	--	--	------

△₊

£

Et

32

$$\frac{+7.0}{50} \quad \frac{+6.1}{26} \quad \frac{2.6}{14} \quad \frac{3.2}{10} \quad \cancel{3.3} \quad \frac{3.6}{8} \quad \frac{4.1}{12} \quad \frac{4.8}{19} \quad \frac{6.7}{30} \quad \frac{8.1}{50}$$

+8.0	+6.9	+6.5	0.3	1.8	2.6	2.6	0.9	3.5	5.0	6.8	7.0
<u>50</u>	<u>41</u>	<u>27</u>	<u>22</u>	<u>18</u>	<u>9</u>	<u>10</u>	<u>10</u>	<u>20</u>	<u>30</u>	<u>45</u>	<u>50</u>

$$\begin{array}{r} 24 \\ \hline 27 \\ \hline 36 \\ \hline 57 \\ \hline 65 \\ \hline \end{array}$$

$$\frac{+3.0}{50} \quad \frac{+2.9}{26} \quad \frac{1.9}{19} \quad \frac{2.1}{10} \quad \frac{2.2}{2} \quad \frac{2.5}{8} \quad \frac{3.3}{16} \quad \frac{4.2}{21} \quad \frac{6.9}{50}$$

$\frac{24}{30}$	$\frac{36}{30}$	$\frac{44}{18}$	$\frac{47}{9}$	$\frac{48}{7}$	$\frac{51}{7}$	$\frac{58}{13}$	$\frac{71}{16}$	$\frac{82}{24}$	$\frac{92}{50}$
-----------------	-----------------	-----------------	----------------	----------------	----------------	-----------------	-----------------	-----------------	-----------------

5.0	5.4	6.1	6.1	6.0	4.9	4.8	5.2	5.8	7.0	7.7	8.4	8.6
50	27	24	22	18	10	4	9	14	18	24	38	50

$\frac{4.1}{50} \frac{4.4}{33} \frac{6.6}{27} \frac{6.8}{19} \frac{5.4}{16} \frac{5.0}{10} \frac{4.9}{7} \frac{5.2}{12} \frac{5.8}{17} \frac{8.3}{20} \frac{8.6}{21} \frac{9.3}{21} \frac{9.6}{50}$

$\frac{20}{50}$	$\frac{26}{36}$	$\frac{23}{26}$	$\frac{24}{21}$	$\frac{61}{16}$	$\frac{55}{13}$	$\frac{53}{5}$	$\frac{58}{10}$	$\frac{85}{16}$	$\frac{88}{20}$	$\frac{93}{22}$	$\frac{91}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------

40	54	67	79	75	62	56		58	65	79	80	75	93
50	33	31	25	19	15	11	5.5	11	13	16	18	19	20

$$\frac{2.9}{50} \quad \frac{3.9}{35} \quad \frac{7.9}{28} \quad \frac{8.2}{19} \quad \frac{5.8}{12} \quad \frac{5.5}{11} \quad \frac{5.8}{8} \quad \frac{6.6}{13} \quad \frac{8.8}{18} \quad \frac{8.9}{24} \quad \frac{9.4}{50}$$

$$\begin{array}{r} 5.6 \\ 50 \end{array} \quad \begin{array}{r} 6.1 \\ 24 \end{array} \quad 5.6$$

$\frac{6.0}{50}$	$\frac{6.2}{22}$	$\frac{5.6}{12}$	$\frac{5.6}{7}$	$\frac{5.8}{7}$	$\frac{6.7}{13}$	$\frac{8.8}{16}$	$\frac{8.7}{23}$	$\frac{7.9}{50}$
------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------	------------------

Sta.	+	π	-	Elev.
73		✓ 950.51.		45.0

+09

Culvert

+50

45.5

74

45.3

+50

45.3

75

45.3

+50

45.3

+80

45.5

76

45.7

+50

46.2

+75

46.5

Drive Lt.

77

46.7

T.P.

5.24

✓
951.93

3.82

✓
946.69

Lt.

2

Rt.

22

$\frac{80}{50}$ $\frac{80}{34}$ $\frac{87}{30}$ $\frac{84}{20}$ $\frac{61}{14}$ $\frac{56}{10}$ $\frac{55}{5}$ $\frac{57}{8}$ $\frac{65}{12}$ $\frac{83}{16}$ $\frac{84}{22}$ $\frac{74}{31}$ $\frac{70}{50}$

$\frac{144}{875}$

$\frac{124}{8.50}$

$\frac{64}{50}$ $\frac{66}{33}$ $\frac{87}{29}$ $\frac{83}{19}$ $\frac{56}{12}$ $\frac{50}{5}$ $\frac{54}{12}$ $\frac{72}{17}$ $\frac{74}{19}$ $\frac{70}{22}$ $\frac{70}{30}$ $\frac{58}{32}$ $\frac{68}{50}$

$\frac{58}{50}$ $\frac{57}{45}$ $\frac{46}{35}$ $\frac{76}{28}$ $\frac{80}{24}$ $\frac{76}{19}$ $\frac{62}{15}$ $\frac{54}{12}$ $\frac{52}{5}$ $\frac{60}{15}$ $\frac{80}{19}$ $\frac{80}{22}$ $\frac{26}{24}$ $\frac{78}{34}$ $\frac{77}{50}$

$\frac{52}{50}$ $\frac{62}{34}$ $\frac{72}{31}$ $\frac{75}{27}$ $\frac{86}{26}$ $\frac{82}{22}$ $\frac{60}{14}$ $\frac{52}{5}$ $\frac{56}{11}$ $\frac{72}{17}$ $\frac{77}{23}$ $\frac{78}{35}$ $\frac{80}{50}$

$\frac{64}{50}$ $\frac{65}{36}$ $\frac{76}{31}$ $\frac{83}{27}$ $\frac{78}{20}$ $\frac{60}{14}$ $\frac{54}{8}$ $\frac{57}{5}$ $\frac{54}{9}$ $\frac{59}{14}$ $\frac{78}{21}$ $\frac{80}{24}$ $\frac{61}{30}$ $\frac{61}{36}$ $\frac{64}{50}$

$\frac{61}{50}$ $\frac{72}{37}$ $\frac{72}{31}$ $\frac{82}{26}$ $\frac{78}{20}$ $\frac{59}{13}$ $\frac{54}{8}$ $\frac{52}{5}$ $\frac{53}{8}$ $\frac{57}{13}$ $\frac{74}{20}$ $\frac{79}{25}$ $\frac{79}{37}$ $\frac{79}{50}$

$\frac{55}{50}$ $\frac{60}{36}$ $\frac{66}{30}$ $\frac{75}{27}$ $\frac{75}{21}$ $\frac{57}{14}$ $\frac{52}{10}$ $\frac{50}{5}$ $\frac{51}{6}$ $\frac{57}{12}$ $\frac{86}{19}$ $\frac{88}{37}$ $\frac{87}{50}$

$\frac{50}{50}$ $\frac{61}{31}$ $\frac{74}{27}$ $\frac{73}{22}$ $\frac{54}{13}$ $\frac{48}{8}$ $\frac{48}{5}$ $\frac{51}{8}$ $\frac{54}{12}$ $\frac{78}{18}$ $\frac{84}{22}$ $\frac{87}{37}$ $\frac{84}{50}$

$\frac{56}{50}$ $\frac{61}{33}$ $\frac{63}{24}$ $\frac{60}{16}$ $\frac{51}{13}$ $\frac{46}{10}$ $\frac{43}{5}$ $\frac{45}{7}$ $\frac{47}{14}$ $\frac{68}{20}$ $\frac{61}{27}$ $\frac{61}{37}$ $\frac{59}{50}$

$\frac{30}{50}$ $\frac{38}{31}$ $\frac{38}{16}$ $\frac{40}{5}$

$\frac{34}{50}$ $\frac{32}{38}$ $\frac{26}{32}$ $\frac{28}{29}$ $\frac{59}{23}$ $\frac{61}{21}$ $\frac{54}{20}$ $\frac{43}{14}$ $\frac{39}{10}$ $\frac{38}{5}$ $\frac{40}{10}$ $\frac{44}{14}$ $\frac{51}{17}$ $\frac{52}{21}$ $\frac{48}{26}$ $\frac{37}{31}$ $\frac{32}{38}$ $\frac{34}{50}$

Sta.	+	π	-	Elev.	
77+38		951.93 ^v		46.9	Drive Rt.
+50				46.9	
78				47.0	
+50				47.3	
79				47.4	
+40				47.5	Drive Rt.
+50				47.5	
80				47.8	
+50				48.5	
81				49.4	
+30				50.2	Drive Lt.
+28					Side Culvert Lt.
+50				50.7	
T.P.	11.50	961.15 ^v	2.28	949.65	

Lt.

C

Rt.

$$\frac{5.0}{50} \quad \frac{5.2}{9} \quad \frac{5.5}{20} \quad \frac{2.9}{45} \quad \frac{2.8}{50}$$

$$\frac{4.3}{50} \quad \frac{4.1}{30} \quad \frac{4.0}{27} \quad \frac{7.0}{23} \quad \frac{7.1}{20} \quad \frac{5.7}{18} \quad \frac{5.2}{11} \quad \frac{5.0}{50} \quad \frac{5.3}{12} \quad \frac{6.2}{18} \quad \frac{7.2}{20} \quad \frac{7.3}{21} \quad \frac{6.3}{22} \quad \frac{6.0}{28} \quad \frac{2.0}{33} \quad \frac{2.4}{50}$$

$$\frac{5.3}{50} \quad \frac{5.5}{30} \quad \frac{7.3}{25} \quad \frac{7.3}{22} \quad \frac{5.8}{17} \quad \frac{5.2}{12} \quad \frac{4.9}{11} \quad \frac{5.3}{12} \quad \frac{6.4}{15} \quad \frac{6.5}{18} \quad \frac{5.6}{20} \quad \frac{5.6}{36} \quad \frac{6.1}{50}$$

$$\frac{5.8}{50} \quad \frac{5.8}{30} \quad \frac{6.1}{27} \quad \frac{7.2}{24} \quad \frac{7.1}{19} \quad \frac{5.5}{14} \quad \frac{5.0}{12} \quad \frac{4.6}{11} \quad \frac{5.0}{10} \quad \frac{5.4}{12} \quad \frac{7.5}{16} \quad \frac{7.6}{36} \quad \frac{7.4}{50}$$

$$\frac{5.0}{50} \quad \frac{5.4}{34} \quad \frac{7.2}{28} \quad \frac{7.2}{21} \quad \frac{5.0}{13} \quad \frac{4.5}{11} \quad \frac{4.7}{8} \quad \frac{5.3}{12} \quad \frac{7.4}{16} \quad \frac{2.1}{31} \quad \frac{6.5}{44} \quad \frac{6.2}{50}$$

$$\frac{4.4}{50} \quad \frac{4.9}{9} \quad \frac{5.1}{16} \quad \frac{4.8}{50}$$

$$\frac{4.8}{50} \quad \frac{5.1}{33} \quad \frac{7.2}{27} \quad \frac{7.2}{23} \quad \frac{5.0}{14} \quad \frac{4.5}{10} \quad \frac{4.4}{11} \quad \frac{4.8}{9} \quad \frac{5.2}{11} \quad \frac{6.9}{17} \quad \frac{7.3}{24} \quad \frac{7.0}{36} \quad \frac{6.2}{50}$$

$$\frac{4.7}{50} \quad \frac{5.3}{32} \quad \frac{6.9}{28} \quad \frac{2.1}{23} \quad \frac{5.4}{16} \quad \frac{4.4}{12} \quad \frac{4.1}{11} \quad \frac{4.8}{11} \quad \frac{6.9}{16} \quad \frac{2.1}{20} \quad \frac{6.4}{36} \quad \frac{6.1}{50}$$

$$\frac{4.4}{50} \quad \frac{5.0}{31} \quad \frac{7.0}{26} \quad \frac{7.0}{23} \quad \frac{4.3}{14} \quad \frac{3.8}{10} \quad \frac{3.4}{11} \quad \frac{3.9}{10} \quad \frac{4.4}{13} \quad \frac{6.1}{16} \quad \frac{5.9}{20} \quad \frac{4.4}{23} \quad \frac{4.5}{50}$$

$$\frac{4.0}{50} \quad \frac{4.1}{34} \quad \frac{6.3}{26} \quad \frac{6.2}{23} \quad \frac{3.8}{16} \quad \frac{3.0}{12} \quad \frac{2.5}{11} \quad \frac{2.8}{9} \quad \frac{3.3}{12} \quad \frac{5.3}{17} \quad \frac{5.6}{20} \quad \frac{4.5}{23} \quad \frac{3.7}{50}$$

$$\frac{3.6}{50} \quad \frac{3.4}{34} \quad \frac{2.5}{20} \quad \frac{1.9}{11} \quad \frac{1.7}{11} \quad \frac{2.1}{7} \quad \frac{2.7}{12} \quad \frac{5.2}{20} \quad \frac{5.4}{24} \quad \frac{5.6}{50}$$

West End.

East End.

$$\frac{6.4}{45.5}$$

$$\frac{5.9}{46.0}$$

$$\frac{2.7}{50} \quad \frac{3.1}{33} \quad \frac{4.1}{25} \quad \frac{3.7}{22} \quad \frac{1.9}{18} \quad \frac{1.3}{16} \quad \frac{1.2}{11} \quad \frac{1.5}{8} \quad \frac{1.9}{12} \quad \frac{4.1}{18} \quad \frac{4.6}{31} \quad \frac{4.2}{50}$$

Sta. + x - Elev.

✓
961.15

82

52.8 Ent. Lt.

+06

Side Culvert
Lt.

+50

55.1

83

57.1

+18

57.7

+40.33

58.0

B.M.

3.24

957.91 ✓

Lt.

C

Rt.

35

$\frac{6.2}{50}$	$\frac{8.5}{30}$	$\frac{9.1}{19}$	$\frac{8.5}{9}$	$\frac{8.4}{1}$	$\frac{8.6}{8}$	$\frac{8.8}{11}$	$\frac{9.4}{16}$	$\frac{9.5}{30}$	$\frac{6.5}{35}$	$\frac{5.6}{50}$
------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------	------------------

<u>West End.</u>	<u>East End.</u>
------------------	------------------

10.8
(50.4)

10.2
(51.0)

$\frac{5.2}{33}$	$\frac{6.8}{23}$	$\frac{6.6}{18}$	$\frac{6.3}{12}$	$\frac{6.1}{1}$	$\frac{6.4}{9}$	$\frac{6.8}{17}$	$\frac{6.7}{24}$	$\frac{6.1}{31}$	$\frac{4.5}{36}$	$\frac{4.4}{50}$
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$\frac{3.8}{33}$	$\frac{4.6}{20}$	$\frac{3.9}{12}$	$\frac{4.1}{1}$	$\frac{4.3}{10}$	$\frac{4.4}{16}$	$\frac{3.9}{30}$	$\frac{3.5}{50}$
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$\frac{4.2}{50}$	$\frac{3.7}{22}$	$\frac{3.5}{1}$	$\frac{3.7}{18}$	$\frac{3.5}{50}$
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$\frac{4.0}{100}$

$\frac{3.7}{1}$

$\frac{3.5}{100}$

Rice St.

Top of Stone Monument "C" & Rice Sts.

