

Dr. 8 - Bk. 155

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

..... PLAN Survey

..... DALE STREET

From Co Rd B2 To Owasso Blvd So.

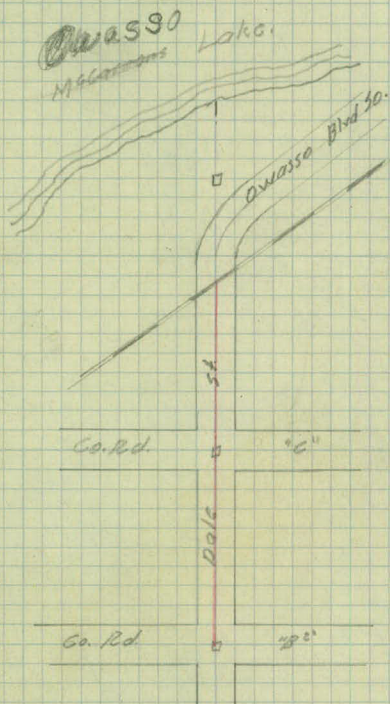
Road Acc't. No. 47

Date Filed 12-29-38

File

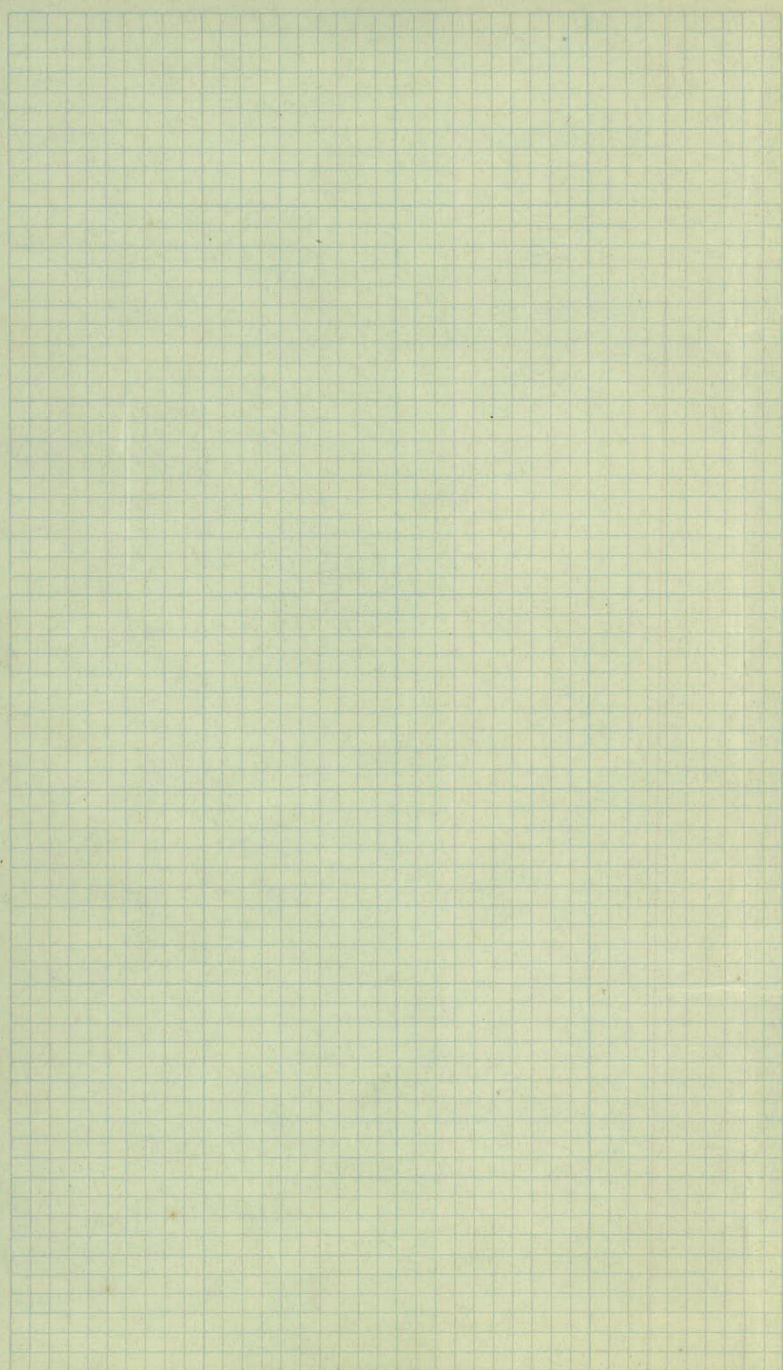
h.5
2.5

PLAN SURVEY
DALE ST.
Co. Rd. "B" to Owasso Blvd. 50.



INDEX.

- Align - 1-2
- Topog - 3-11
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Alignment

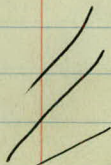
Sta.	Point	$\Delta Lt.$	$\Delta Rt.$
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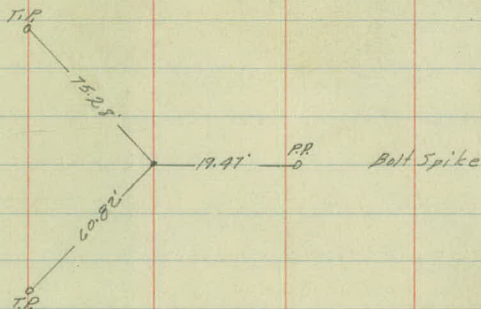
115	+24.65	P.O.T	
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107	+28.63	= P.I.	
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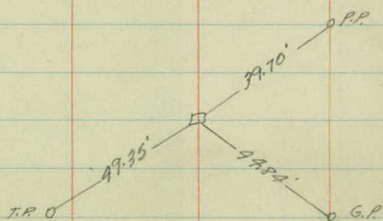
			0°02'
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80	+65.3	= A. Co. Rd. "22"	
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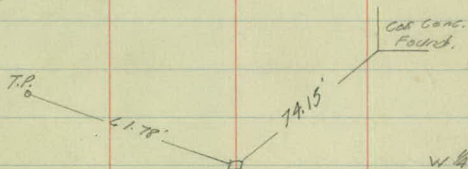




= 60.00' "C"



Mont.
S.W. Cor. Sec. 1-29-23

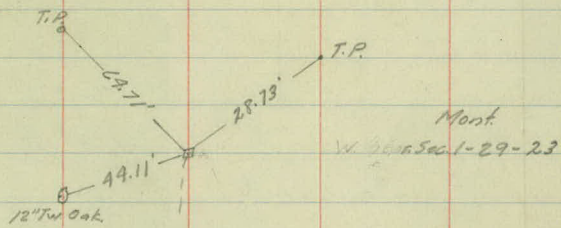


Mont.
W. 1/4 Cor. Sec. 12-29-23

9/14/38

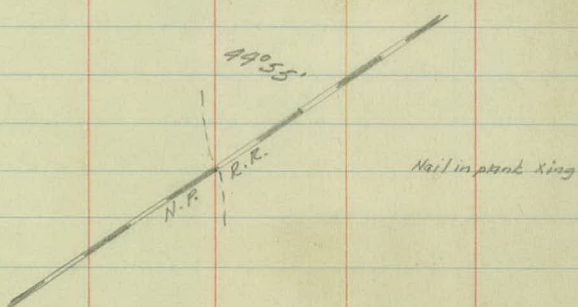
2

K.A.
L.R.H.
L.C.
MAG.



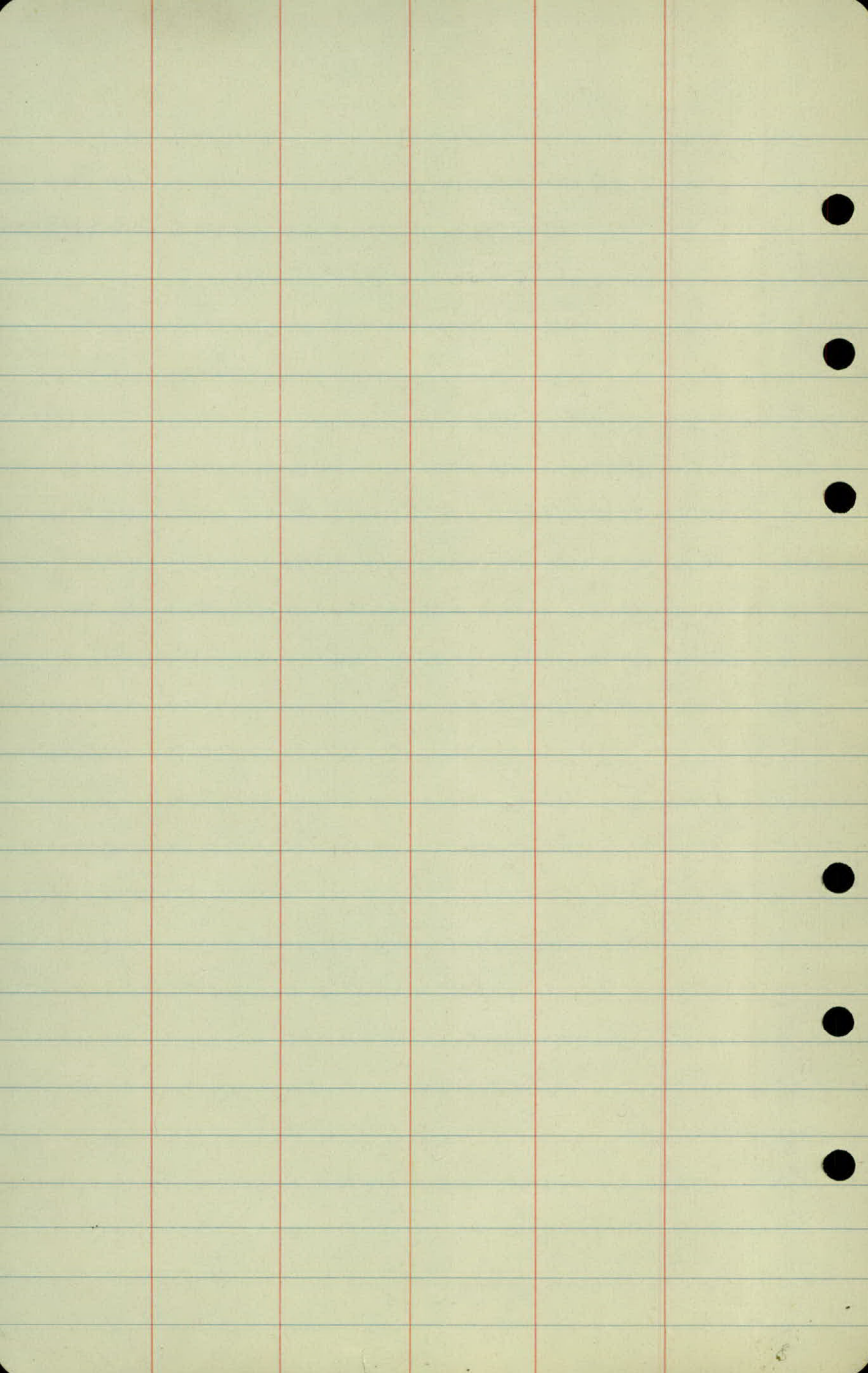
Mont.

W. 30.5 Sec. 1-29-23



Nail in plank Xing

Nail in plank X 105



Topography

85

11'

9'

84

10'

10'

83

12'

10'

82

10'

11'

81

12'

11'

+77 N.S. Moulder Line

80

+51-T.P.P.-28'

+10-T.P.P.P.-28'

+51-T.P.P.P.-28'

Cult.

Cult.

+98-T.P.-28'

+85-N End. 18' Conc. Culv - 33'

20'

50'
20'
2-S-F

+32-15" R.E. Id. C. - 84'
+26-12" R.E. Id. C. - 83'
+19-5" Id. C. Ha. - 51'

+95-G.P.-87'
+87-2" R.E. Id. C. - 90'
+85-N End. 18' Conc. Culv - 33'

40'

92

12'

7'

91

12'

7'

90

12'

7'

89

12'

6

88

12'

7'

87

11'

7'

86

11'

9'

+72-T.P.-21'

+57-Ent.

+93-T.P.-21'

+17-T.P.-21'

Cult.

+89-T.P.-23'

+94-15" B. Elder - 43'
+92-2" Elm - 33'

+52-2" Elm - 33'

+53-R.R.
12" x 30" 14-15'

+50-T.P.R.-28'

P.R.

Cult.

Cult.

+69-15" Stump - 27'

+97-18" B. Elder - 27'

+96-S.W. Cor. Ho. - 93'

+75-15" S. Elder - 25'

+61-8" B. Elder - 26'

+57-R.R.

P.R.

Cult.

1
0

0 0

0

0

0
0

0



99 9' 10'

98 9' 10'

+27- 24" X 34' C.M. 16' 18'

97 9' 11'

96 9' 10'

95 10' 10'

94 10' 9'
29' 24'

+95- 24" X 48' C.M.

+57- Pipe Line 15 ft

+74- Great Lakes Pipeline 1' 2'

93 11' 9'

+14-T.P.-20'

Cult.

+57-T.P.-20'

Wasteland

+60-T.P.-20'

+91-T.P.-20'

Swamp

+93-T.P.-20'

Barred

+87-Breather Pipe-87'

+74-Breather Pipe-20'

Swamp
Cult.

+74-Breather Pipe-20'

106

7'

11'

105

7'

11'

104

7'

11'

103

7'

11'

102

7'

11'

101

7'

11'

100

7'

11'

+87-T.P.-17'

+69-T.P.-17'

+35-T.P.-17'

+15-6" Triple Rga - 31'

+05-T.P.-18'

+76-T.P.-19'

+55 End Swamp -

+42-T.P.-19'

Cult.

Wasteland

Swamp

Cult.

Swamp

113

6'

11'

112

6'

11'

111

6'

10'

110

6'

11'

109

6'

11'

108

7'

11'

114.4 - N. Shoulderline

114.5 - shoulderline "B"

107

9'

12'

196-T.P.-17'

189-PP-21'

106-T.P.-17'

Cult.

Cult.

157-PP-21'

135-12° E 1/4 - 23'

181-T.P.-16'

107-F.C.Cot.-25'

116-PP-22'

197-T.P.-16'

F.C.-23'

187-PP-23'

Cult.

131-T.P.-16'

185-F.C.Cot.-26'

157-N. End 284° M.-25'

157-PP-28'

197-N. End 296° M.-31'

101-T.P.-42'

2. End 286° M.-22'

107-S. End 286° M.-31'

120

8'

7'

119

8'

6'

118

8'

7'

117

7'

8'

116

6'

9'

115

6'

10'

114

5'

9'

+55-Res. Row Cuts. - 27'

FG-18'

+06-P.R.-18'

+77-T.P.-17'

Cult.

Cult.

+82-Bog, FG-18'

+86-P.P.-18'

+50-T.P.-18'

+61-P.P.-18'

+20-T.P.-17'

+45-P.P.-19'

+98-T.P.-18'

+54-C^o Tw. Cuth.-19'

+24-P.P.-19'

+65-T.P.-17'

Cult.

Cult.

+03-P.P.-20'

127

9'

7'

193-212K? VitCov.

25'

126

8'

7'

125

8'

7'

124

9'

7'

123

9'

6'

122

8'

7'

121

5'

7'

+79-T.R.-17'

+30-P.P.-17'

G.R. 11'

G.R. 10' Fc. 27'

+35-T.R.-17'

G.R. -12'

+05-P.P.-15'
G.R. -10' Fc. 27'

+81-Fc. 12'

G.R. -11'

+94-T.R.-16'

G.R. 10'

+39-Bes. G.R. 12'

Fc. -25'

15" Oak 29' G.L. 10'

+80-Graysd Oaks - 22'

+63-4" Trim Oak - 25'

+62-T.R.-16'

+68-P.P.-18'
+58-12" Oak - 22'
+93-Bes. G.R. - 10'
+33-End 12" x 20 G.M. - 17'
+17 Range dia to End

Fc. -24'

+52-T.R.-17'

Fc. -26'

+06-T.R.-16'
Fc. -25'

+46-P.P.-18'

+28-End Row Oak - 24'
+27-P.P.-18'

131

130

8'

8'

129

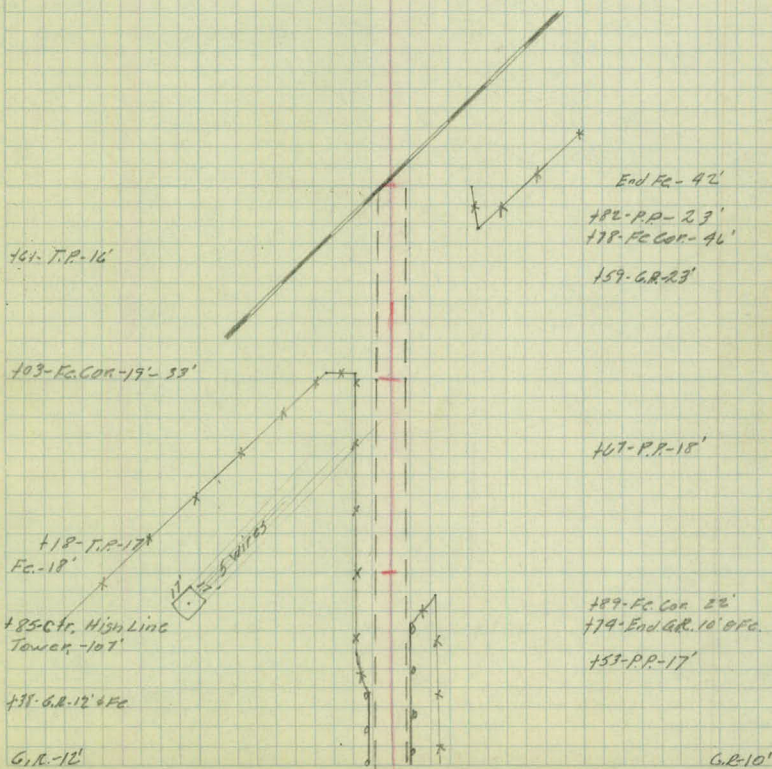
8'

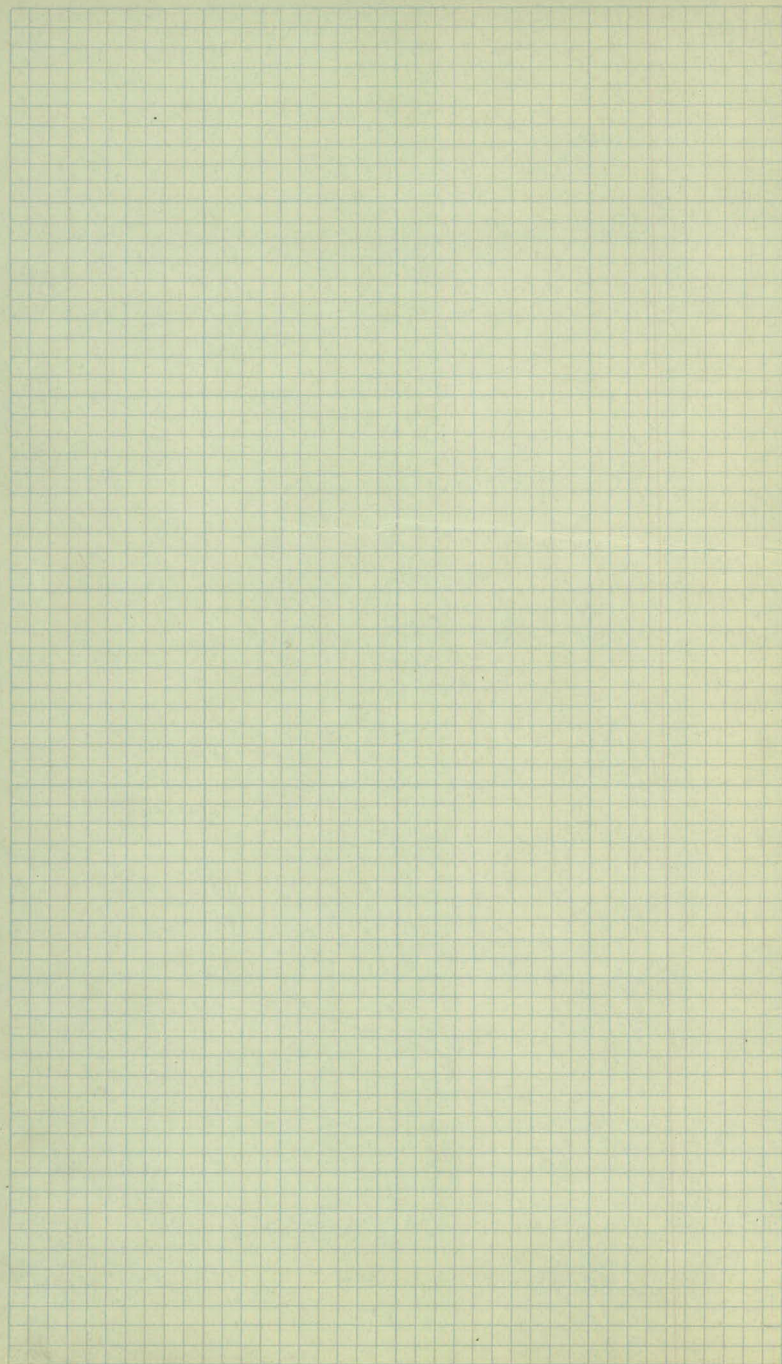
8'

128

9'

7'





Bench Levels

Sta	+	-	-	E/cv.	
B.M.	1.97	733.78			(731.81)
T.P.	11.84	744.98	0.64	733.14	
T.P.	5.32	745.51	4.79	740.17	
B.M.			8.31	737.20	
B.M.	2.58	734.39		731.81	
T.P.	11.99	745.35	10.3	733.36	
T.P.	4.76	745.24	9.87	740.48	
B.M.	3.97	741.20	2.01	737.23	(737.20)
T.P.	0.57	734.47	7.90	733.90	
T.P.	0.09	721.87	12.69	721.78	
T.P.	0.16	707.23	12.80	709.07	
B.M.	0.40	898.68	10.95	898.28	
T.P.	7.72	898.60	7.81	890.87	
T.P.	13.79	912.17	0.22	898.20	
T.P.	13.02	(924.84)	0.35	911.82	
B.M.	9.37	930.84	3.37	921.47	
T.P.	11.65	942.13	0.36	930.42	
T.P.	0.16	929.88	13.01	927.12	
B.M.			3.23	926.65	
T.P.	0.41	917.27	13.02	916.86	
T.P.	0.88	906.17	11.98	905.29	
T.P.	0.42	893.22	13.97	892.80	
T.P.	8.95	897.87	4.30	888.92	
B.M.			5.25	892.62	

Description

Spk. in P.P.N.E. Cor Dale St & Minnesota Ave.

Spk. in T.P.N.W. Cor Dale St & Co. Rd "82"

Spk. in P.P.N.E. Cor Dale St & Minnesota Ave.

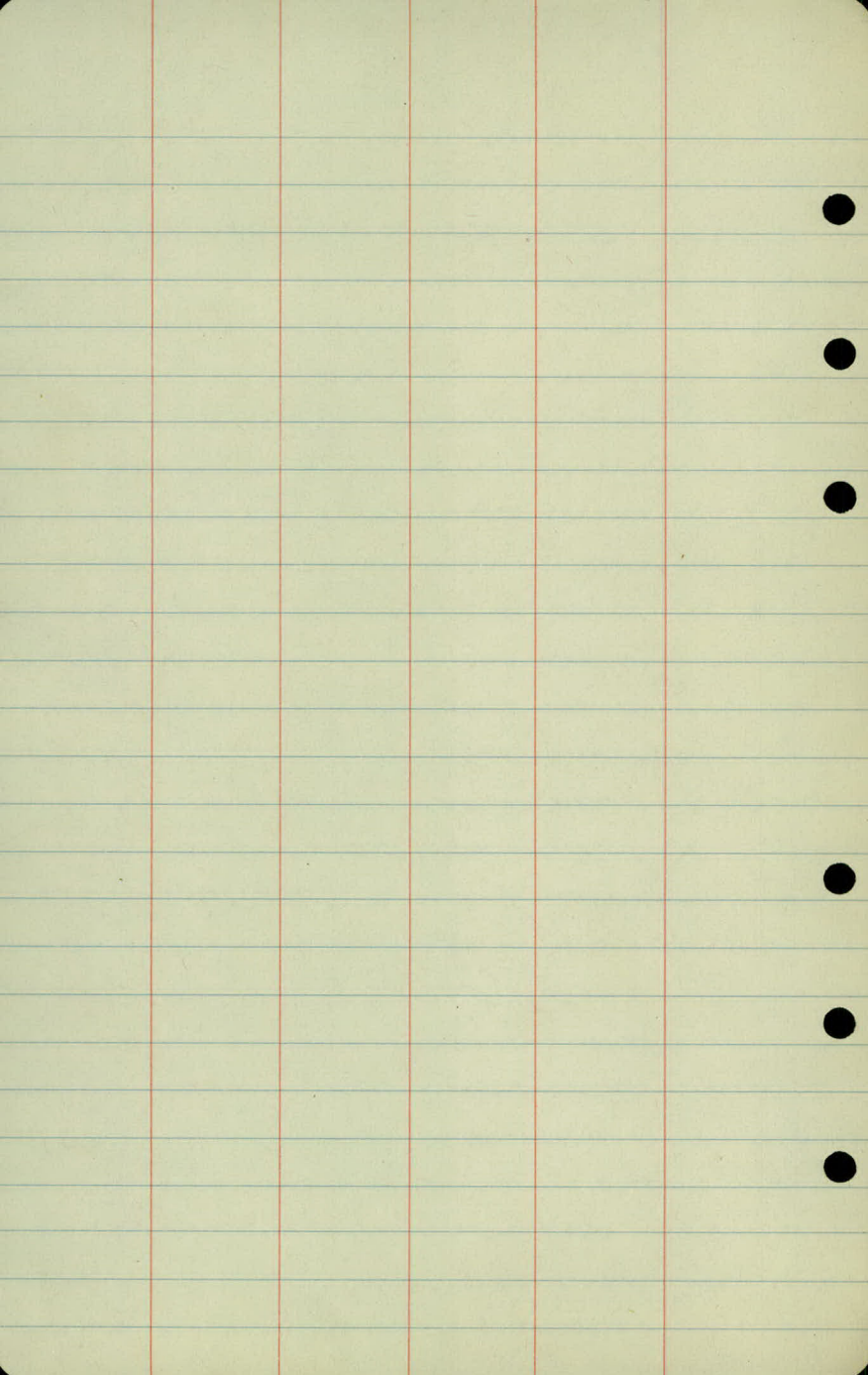
Spk. in T.P.N.W. Cor Dale St & Co. Rd "82"

Top Breather Pipe 27' Rt 93+79

2nd Spk. in P.P.N.E. Cor Dale St & Co. Rd "C" 28' Rt. 107+50

E.R. Spk. in R.P.Rt. 116+55

Spk. in G.P. 70' N. & 10' W. of R.R. Tracks.



X Sections

Sta	+	Σ	-	Elev.	
B.M.	5.37	942.62			937.23
80	+65.9			38.5	
	+80			38.3	
	+85			38.1	
	+87			38.1	
81	+20			37.9	
	+50			37.4	
82				37.1	
	+50			36.7	
83				36.3	
	+50			36.0	
84				35.7	
I.P.	2.15	938.03	739	✓ 935.28	

Lt.

L

Pt.

Spk. in T.P. H. & Gor. Dale & Co. Rd. 8th

$$\frac{41}{50}$$

$$\frac{41}{50}$$

$$\frac{43}{50}$$

$$\frac{50}{50}$$

$$\frac{49}{50}$$

$$\frac{46}{50}$$

$$\frac{35.15}{50}$$

$$\frac{60.1}{50}$$

$$\frac{FL. Curv.}{50}$$

$$\frac{35.48}{50}$$

$$\frac{7.14}{50}$$

$$\frac{FL. Curv.}{50}$$

$$\frac{68}{50} \quad \frac{71}{50} \quad \frac{50}{23} \quad \frac{45}{21} \quad \frac{52}{26} \quad \frac{64}{93} \quad \frac{68}{95} \quad \frac{58}{50}$$

$$\frac{49}{50} \quad \frac{53}{28} \quad \frac{67}{23} \quad \frac{69}{18} \quad \frac{504.7}{14} \quad \frac{51}{11} \quad \frac{52}{14} \quad \frac{65}{18} \quad \frac{67}{23} \quad \frac{55}{25} \quad \frac{54}{50}$$

$$\frac{56}{50} \quad \frac{56}{26} \quad \frac{65}{15} \quad \frac{58}{13} \quad \frac{53}{10} \quad \frac{52}{10} \quad \frac{52}{13} \quad \frac{58}{18} \quad \frac{71}{22} \quad \frac{71}{26} \quad \frac{61}{50} \quad \frac{60}{50}$$

$$\frac{60}{50} \quad \frac{59}{25} \quad \frac{65}{14} \quad \frac{56}{10} \quad \frac{55}{10} \quad \frac{57}{10} \quad \frac{61}{14} \quad \frac{73}{17} \quad \frac{76}{21} \quad \frac{69}{23} \quad \frac{74}{50}$$

$$\frac{66}{50} \quad \frac{69}{18} \quad \frac{66}{13} \quad \frac{61}{10} \quad \frac{59}{10} \quad \frac{61}{14} \quad \frac{69}{17} \quad \frac{76}{20} \quad \frac{76}{25} \quad \frac{64}{50} \quad \frac{77}{50}$$

$$\frac{72}{50} \quad \frac{73}{21} \quad \frac{77}{18} \quad \frac{78}{15} \quad \frac{68}{13} \quad \frac{65}{10} \quad \frac{63}{10} \quad \frac{65}{13} \quad \frac{70}{13} \quad \frac{77}{16} \quad \frac{75}{40} \quad \frac{77}{50} \quad \frac{83}{50}$$

$$\frac{80}{50} \quad \frac{83}{38} \quad \frac{79}{17} \quad \frac{72}{13} \quad \frac{69}{10} \quad \frac{66}{10} \quad \frac{68}{10} \quad \frac{73}{13} \quad \frac{81}{13} \quad \frac{82}{19} \quad \frac{93}{32} \quad \frac{97}{50}$$

$$\frac{83}{50} \quad \frac{83}{23} \quad \frac{72}{10} \quad \frac{69}{7} \quad \frac{72}{12} \quad \frac{75}{16} \quad \frac{87}{30} \quad \frac{94}{50}$$

Nail in T.P. Lt. 54 9+00

Sta

+

x

-

998.03

84 +50

35.5

85

35.4

+50

35.2

86

34.6

+50

33.9

87

32.9

+15

32.5

+22

32.2

+47

31.2

+58

30.7

88

28.9

Lt

A

Rt

$$\frac{3.2}{50} \frac{3.5}{29} \frac{2.9}{16} \frac{2.6}{10} \frac{2.5}{9} \frac{2.7}{15} \frac{3.0}{18} \frac{3.9}{50} \frac{5.6}{50}$$

$$\frac{3.1}{50} \frac{3.4}{32} \frac{2.8}{16} \frac{2.9}{13} \frac{2.8}{10} \frac{2.6}{9} \frac{2.8}{15} \frac{3.0}{24} \frac{4.1}{50}$$

$$\frac{2.9}{50} \frac{3.4}{25} \frac{2.9}{10} \frac{2.8}{9} \frac{3.0}{13} \frac{3.1}{15} \frac{3.5}{32} \frac{4.4}{50} \frac{4.8}{50}$$

$$\frac{2.6}{50} \frac{3.3}{26} \frac{3.3}{16} \frac{3.8}{14} \frac{3.6}{11} \frac{3.4}{9} \frac{3.6}{16} \frac{3.1}{30} \frac{4.2}{50}$$

$$\frac{2.4}{50} \frac{3.2}{32} \frac{4.0}{16} \frac{4.6}{14} \frac{4.4}{11} \frac{4.1}{9} \frac{4.3}{8} \frac{4.2}{12} \frac{3.5}{15} \frac{4.0}{30} \frac{3.7}{50}$$

$$\frac{2.2}{50} \frac{3.7}{29} \frac{5.6}{13} \frac{5.4}{11}$$

$$\frac{5.1}{7} \frac{5.8}{9} \frac{5.5}{9} \frac{4.0}{16} \frac{3.8}{34} \frac{3.6}{50}$$

$$\frac{1.9}{50} \frac{2.6}{39} \frac{4.9}{19} \frac{6.0}{13} \frac{5.5}{9} \frac{5.8}{17} \frac{4.4}{30} \frac{4.0}{30} \frac{3.1}{50}$$

$$\frac{4.6}{50} \frac{5.6}{31} \frac{6.2}{12} \frac{5.8}{9} \frac{6.1}{10} \frac{5.0}{32} \frac{4.0}{50}$$

$$\frac{4.6}{50} \frac{5.2}{32} \frac{6.9}{18} \frac{7.0}{12} \frac{6.8}{9} \frac{7.0}{18} \frac{6.6}{18} \frac{4.3}{30}$$

$$\frac{9.6}{50} \frac{3.5}{33} \frac{5.1}{24} \frac{7.6}{14} \frac{7.5}{12} \frac{7.3}{9} \frac{7.4}{6} \frac{1.9}{9} \frac{7.5}{15} \frac{2.4}{24} \frac{2.2}{50}$$

$$\frac{4.1}{50} \frac{2.9}{33} \frac{7.5}{21} \frac{9.6}{14} \frac{9.4}{12} \frac{9.1}{6} \frac{9.3}{12} \frac{10.0}{12} \frac{7.4}{19} \frac{2.3}{21} \frac{2.4}{43}$$

Sta	+	X	-	E/cv.
		998.03		
88	+26			27.5
	+65			25.4
T.P.	1.00	926.52	12.51	925.52
89				23.7
	+50			21.2
90				17.5
	+50			16.0
91				13.5
T.P.	0.91	914.47	12.96	912.56
	+50			10.8
92				08.3
	+24			7.1
	+69			04.9
T.P.	0.56	903.91	11.06	902.41

Lt

C

Rt

$$\begin{array}{r} 46 \\ 50 \end{array} \quad \begin{array}{r} 50 \\ 31 \end{array} \quad \begin{array}{r} 99 \\ 18 \end{array} \quad \begin{array}{r} 108 \\ 15 \end{array} \quad \begin{array}{r} 108 \\ 12 \end{array} \quad \begin{array}{r} 105 \\ 6 \end{array} \quad \begin{array}{r} 107 \\ 6 \end{array} \quad \begin{array}{r} 114 \\ 9 \end{array} \quad \begin{array}{r} 114 \\ 11 \end{array} \quad \begin{array}{r} 90 \\ 19 \end{array} \quad \begin{array}{r} 36 \\ 28 \end{array} \quad \begin{array}{r} 43 \\ 50 \end{array}$$

$$\begin{array}{r} 80 \\ 50 \end{array} \quad \begin{array}{r} 73 \\ 32 \end{array} \quad \begin{array}{r} 103 \\ 19 \end{array} \quad \begin{array}{r} 129 \\ 15 \end{array} \quad \begin{array}{r} 128 \\ 12 \end{array} \quad \begin{array}{r} 126 \\ 6 \end{array} \quad \begin{array}{r} 127 \\ 6 \end{array} \quad \begin{array}{r} 131 \\ 11 \end{array} \quad \begin{array}{r} 130 \\ 16 \end{array} \quad \begin{array}{r} 107 \\ 17 \end{array} \quad \begin{array}{r} 42 \\ 29 \end{array} \quad \begin{array}{r} 46 \\ 50 \end{array}$$

$$\begin{array}{r} 410 \\ 50 \end{array} \quad \begin{array}{r} 104 \\ 38 \end{array} \quad \begin{array}{r} 04 \\ 20 \end{array} \quad \begin{array}{r} 31 \\ 15 \end{array} \quad \begin{array}{r} 29 \\ 11 \end{array} \quad \begin{array}{r} 28 \\ 6 \end{array} \quad \begin{array}{r} 30 \\ 6 \end{array} \quad \begin{array}{r} 36 \\ 10 \end{array} \quad \begin{array}{r} 38 \\ 13 \end{array} \quad \begin{array}{r} 09 \\ 16 \end{array} \quad \begin{array}{r} 139 \\ 24 \end{array} \quad \begin{array}{r} 159 \\ 50 \end{array}$$

$$\begin{array}{r} 22 \\ 50 \end{array} \quad \begin{array}{r} 30 \\ 31 \end{array} \quad \begin{array}{r} 32 \\ 19 \end{array} \quad \begin{array}{r} 57 \\ 14 \end{array} \quad \begin{array}{r} 55 \\ 12 \end{array} \quad \begin{array}{r} 53 \\ 6 \end{array} \quad \begin{array}{r} 54 \\ 6 \end{array} \quad \begin{array}{r} 58 \\ 10 \end{array} \quad \begin{array}{r} 68 \\ 12 \end{array} \quad \begin{array}{r} 68 \\ 16 \end{array} \quad \begin{array}{r} 29 \\ 18 \end{array} \quad \begin{array}{r} 12 \\ 33 \end{array} \quad \begin{array}{r} 05 \\ 50 \end{array}$$

$$\begin{array}{r} 65 \\ 50 \end{array} \quad \begin{array}{r} 69 \\ 33 \end{array} \quad \begin{array}{r} 61 \\ 18 \end{array} \quad \begin{array}{r} 82 \\ 15 \end{array} \quad \begin{array}{r} 80 \\ 12 \end{array} \quad \begin{array}{r} 80 \\ 6 \end{array} \quad \begin{array}{r} 82 \\ 6 \end{array} \quad \begin{array}{r} 88 \\ 11 \end{array} \quad \begin{array}{r} 97 \\ 12 \end{array} \quad \begin{array}{r} 97 \\ 14 \end{array} \quad \begin{array}{r} 68 \\ 17 \end{array} \quad \begin{array}{r} 58 \\ 31 \end{array} \quad \begin{array}{r} 61 \\ 50 \end{array}$$

$$\begin{array}{r} 100 \\ 50 \end{array} \quad \begin{array}{r} 97 \\ 29 \end{array} \quad \begin{array}{r} 95 \\ 17 \end{array} \quad \begin{array}{r} 110 \\ 13 \end{array} \quad \begin{array}{r} 108 \\ 12 \end{array} \quad \begin{array}{r} 105 \\ 7 \end{array} \quad \begin{array}{r} 108 \\ 7 \end{array} \quad \begin{array}{r} 122 \\ 12 \end{array} \quad \begin{array}{r} 122 \\ 14 \end{array} \quad \begin{array}{r} 101 \\ 17 \end{array} \quad \begin{array}{r} 96 \\ 27 \end{array} \quad \begin{array}{r} 96 \\ 50 \end{array}$$

$$\begin{array}{r} 125 \\ 50 \end{array} \quad \begin{array}{r} 127 \\ 31 \end{array} \quad \begin{array}{r} 125 \\ 17 \end{array} \quad \begin{array}{r} 135 \\ 14 \end{array} \quad \begin{array}{r} 132 \\ 12 \end{array} \quad \begin{array}{r} 130 \\ 7 \end{array} \quad \begin{array}{r} 133 \\ 7 \end{array} \quad \begin{array}{r} 141 \\ 9 \end{array} \quad \begin{array}{r} 143 \\ 15 \end{array} \quad \begin{array}{r} 126 \\ 17 \end{array} \quad \begin{array}{r} 78 \\ 31 \end{array} \quad \begin{array}{r} 79 \\ 50 \end{array}$$

$$\begin{array}{r} 3.5 \\ 50 \end{array} \quad \begin{array}{r} 3.5 \\ 34 \end{array} \quad \begin{array}{r} 3.3 \\ 18 \end{array} \quad \begin{array}{r} 4.2 \\ 14 \end{array} \quad \begin{array}{r} 3.9 \\ 12 \end{array} \quad \begin{array}{r} 3.7 \\ 6 \end{array} \quad \begin{array}{r} 4.0 \\ 6 \end{array} \quad \begin{array}{r} 5.3 \\ 13 \end{array} \quad \begin{array}{r} 5.3 \\ 18 \end{array} \quad \begin{array}{r} 2.5 \\ 18 \end{array} \quad \begin{array}{r} 1.2 \\ 33 \end{array} \quad \begin{array}{r} 1.7 \\ 50 \end{array}$$

$$\begin{array}{r} 7.3 \\ 50 \end{array} \quad \begin{array}{r} 7.6 \\ 34 \end{array} \quad \begin{array}{r} 6.4 \\ 20 \end{array} \quad \begin{array}{r} 6.5 \\ 12 \end{array} \quad \begin{array}{r} 6.2 \\ 6 \end{array} \quad \begin{array}{r} 6.5 \\ 6 \end{array} \quad \begin{array}{r} 7.9 \\ 12 \end{array} \quad \begin{array}{r} 8.0 \\ 16 \end{array} \quad \begin{array}{r} 6.0 \\ 20 \end{array} \quad \begin{array}{r} 5.0 \\ 28 \end{array} \quad \begin{array}{r} 5.3 \\ 43 \end{array} \quad \begin{array}{r} 5.9 \\ 50 \end{array}$$

$$\begin{array}{r} 10.1 \\ 50 \end{array} \quad \begin{array}{r} 10.2 \\ 39 \end{array} \quad \begin{array}{r} 10.1 \\ 24 \end{array} \quad \begin{array}{r} 8.3 \\ 20 \end{array} \quad \begin{array}{r} 7.7 \\ 11 \end{array} \quad \begin{array}{r} 7.4 \\ 7 \end{array} \quad \begin{array}{r} 7.7 \\ 7 \end{array} \quad \begin{array}{r} 9.2 \\ 12 \end{array} \quad \begin{array}{r} 9.2 \\ 17 \end{array} \quad \begin{array}{r} 8.0 \\ 21 \end{array} \quad \begin{array}{r} 7.7 \\ 27 \end{array} \quad \begin{array}{r} 8.7 \\ 50 \end{array}$$

$$\begin{array}{r} 13.9 \\ 50 \end{array} \quad \begin{array}{r} 13.8 \\ 38 \end{array} \quad \begin{array}{r} 14.7 \\ 25 \end{array} \quad \begin{array}{r} 10.2 \\ 16 \end{array} \quad \begin{array}{r} 9.9 \\ 10 \end{array} \quad \begin{array}{r} 9.6 \\ 9 \end{array} \quad \begin{array}{r} 9.9 \\ 9 \end{array} \quad \begin{array}{r} 10.2 \\ 16 \end{array} \quad \begin{array}{r} 12.3 \\ 19 \end{array} \quad \begin{array}{r} 14.2 \\ 33 \end{array} \quad \begin{array}{r} 14.7 \\ 50 \end{array}$$

Sta	+	Σ	-	Elev
		903.91		
93				03.4
+50				00.7
I.M.	5.58	903.86	5.58	898.23
				(898.28)
+95				X
94				98.2
+50		896.80		96.0
I.P.	2.68	(896.85)	9.74	(894.17)
95				894.12
				94.1
+50				92.6
96				91.8
+50		896.15		91.4
I.P.	4.96	(896.20)	5.61	891.19
97				(891.24)
				91.2
+27				

Lt.

E.

Rt.

$\frac{6.0}{50}$	$\frac{7.0}{39}$	$\frac{5.6}{25}$	$\frac{1.4}{17}$	$\frac{0.7}{11}$	$\frac{0.5}{8}$	$\frac{0.8}{16}$	$\frac{1.3}{22}$	$\frac{4.6}{33}$	$\frac{5.3}{50}$	$\frac{5.7}{50}$
------------------	------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------

$\frac{9.3}{50}$	$\frac{9.0}{35}$	$\frac{8.0}{22}$	$\frac{4.0}{14}$	$\frac{3.5}{11}$	$\frac{3.2}{8}$	$\frac{3.5}{14}$	$\frac{4.0}{24}$	$\frac{8.4}{36}$	$\frac{9.5}{50}$	$\frac{9.5}{50}$
------------------	------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------

Top Breastclip alt. #74

87.96
Culv.

Culv. 88.21

$\frac{12.2}{50}$	$\frac{12.7}{31}$	$\frac{9.6}{19}$	$\frac{6.1}{12}$	$\frac{5.7}{50}$	$\frac{6.1}{10}$	$\frac{6.4}{13}$	$\frac{10.0}{22}$	$\frac{13.5}{31}$	$\frac{13.0}{50}$
-------------------	-------------------	------------------	------------------	------------------	------------------	------------------	-------------------	-------------------	-------------------

$\frac{14.0}{50}$	$\frac{13.9}{37}$	$\frac{14.6}{34}$	$\frac{14.6}{32}$	$\frac{12.0}{21}$	$\frac{8.1}{11}$	$\frac{7.9}{8}$	$\frac{8.2}{13}$	$\frac{8.3}{21}$	$\frac{12.0}{30}$	$\frac{14.2}{50}$
-------------------	-------------------	-------------------	-------------------	-------------------	------------------	-----------------	------------------	------------------	-------------------	-------------------

$\frac{7.5}{50}$	$\frac{7.2}{39}$	$\frac{8.2}{35}$	$\frac{6.3}{19}$	$\frac{3.4}{11}$	$\frac{3.0}{9}$	$\frac{2.7}{9}$	$\frac{3.0}{13}$	$\frac{3.4}{21}$	$\frac{6.2}{28}$	$\frac{7.6}{50}$
------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{7.7}{50}$	$\frac{7.5}{38}$	$\frac{8.7}{35}$	$\frac{8.7}{34}$	$\frac{8.0}{33}$	$\frac{8.0}{18}$	$\frac{4.6}{11}$	$\frac{4.3}{8}$	$\frac{4.2}{9}$	$\frac{4.4}{12}$	$\frac{4.7}{21}$	$\frac{8.1}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------

$\frac{8.1}{50}$	$\frac{8.5}{35}$	$\frac{9.0}{34}$	$\frac{8.9}{31}$	$\frac{7.9}{30}$	$\frac{8.0}{16}$	$\frac{5.5}{10}$	$\frac{5.2}{8}$	$\frac{5.0}{10}$	$\frac{5.2}{12}$	$\frac{5.5}{20}$	$\frac{8.3}{33}$	$\frac{8.4}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------

$\frac{8.4}{50}$	$\frac{8.5}{36}$	$\frac{9.2}{34}$	$\frac{9.2}{32}$	$\frac{8.7}{30}$	$\frac{8.8}{17}$	$\frac{5.7}{10}$	$\frac{5.4}{8}$	$\frac{5.4}{9}$	$\frac{5.6}{12}$	$\frac{5.9}{19}$	$\frac{8.9}{33}$	$\frac{8.7}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{8.5}{50}$	$\frac{8.9}{31}$	$\frac{7.8}{26}$	$\frac{8.6}{22}$	$\frac{8.4}{16}$	$\frac{5.4}{11}$	$\frac{5.0}{10}$	$\frac{5.3}{10}$	$\frac{5.6}{12}$	$\frac{8.8}{19}$	$\frac{8.4}{25}$	$\frac{9.6}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

86.94 Culv.
 $\frac{9.21}{16}$ Culv. 86.91
 $\frac{9.24}{18}$

87.2

Sta.	+	T 896.15 896.20	-	Elev
+50				91.2
98				91.1
+50				91.3
99				91.2
+50				91.2
100				91.2
+50				91.3
101				92.0
+50				93.4
T.P.	11.18	904.72 904.77	2.61	893.54 893.59
102				95.5
+50				98.0

L₁

E

R₁

$$\frac{8.7}{50} \quad \frac{8.7}{18} \quad \frac{5.3}{10} \quad \frac{5.0}{10} \quad \frac{5.7}{10} \quad \frac{5.6}{12} \quad \frac{8.8}{18} \quad \frac{8.6}{50}$$

$$\frac{8.9}{50} \quad \frac{8.9}{20} \quad \frac{5.8}{11} \quad \frac{5.4}{9} \quad \frac{5.1}{10} \quad \frac{5.5}{10} \quad \frac{6.2}{13} \quad \frac{9.0}{20} \quad \frac{8.7}{50}$$

$$\frac{8.9}{50} \quad \frac{9.3}{20} \quad \frac{5.6}{11} \quad \frac{4.9}{9} \quad \frac{5.4}{9} \quad \frac{5.9}{13} \quad \frac{9.0}{19} \quad \frac{8.7}{50}$$

$$\frac{9.1}{50} \quad \frac{9.2}{22} \quad \frac{6.5}{15} \quad \frac{5.5}{9} \quad \frac{5.0}{10} \quad \frac{5.4}{9} \quad \frac{5.7}{13} \quad \frac{9.1}{19} \quad \frac{8.8}{50}$$

$$\frac{9.1}{50} \quad \frac{9.6}{20} \quad \frac{5.7}{11} \quad \frac{5.0}{10} \quad \frac{5.5}{10} \quad \frac{6.0}{13} \quad \frac{9.3}{20} \quad \frac{8.7}{50}$$

$$\frac{9.2}{50} \quad \frac{9.5}{18} \quad \frac{5.9}{11} \quad \frac{5.4}{9} \quad \frac{5.0}{10} \quad \frac{5.6}{11} \quad \frac{6.2}{15} \quad \frac{9.2}{20} \quad \frac{8.6}{50}$$

$$\frac{8.9}{50} \quad \frac{9.0}{18} \quad \frac{5.5}{11} \quad \frac{5.2}{8} \quad \frac{4.9}{10} \quad \frac{5.3}{11} \quad \frac{5.6}{15} \quad \frac{9.0}{21} \quad \frac{8.6}{50}$$

$$\frac{8.6}{50} \quad \frac{8.9}{22} \quad \frac{4.9}{11} \quad \frac{4.4}{8} \quad \frac{4.2}{10} \quad \frac{4.6}{11} \quad \frac{5.2}{15} \quad \frac{8.8}{23} \quad \frac{8.8}{50}$$

$$\frac{8.4}{50} \quad \frac{7.0}{20} \quad \frac{3.2}{10} \quad \frac{2.8}{10} \quad \frac{3.2}{10} \quad \frac{3.6}{13} \quad \frac{8.0}{22} \quad \frac{8.1}{32} \quad \frac{8.1}{50}$$

$$\frac{13.0}{50} \quad \frac{12.6}{19} \quad \frac{9.8}{11} \quad \frac{9.5}{9} \quad \frac{9.2}{10} \quad \frac{9.6}{11} \quad \frac{10.0}{13} \quad \frac{12.8}{19} \quad \frac{14.1}{29} \quad \frac{14.7}{50}$$

$$\frac{9.2}{50} \quad \frac{8.7}{28} \quad \frac{7.5}{15} \quad \frac{6.9}{9} \quad \frac{6.7}{10} \quad \frac{7.0}{10} \quad \frac{7.2}{14} \quad \frac{7.9}{23} \quad \frac{9.5}{35} \quad \frac{9.5}{50}$$

Sta + $\overline{904.72}$ - Elev.
 $\overline{904.77}$

+ 83 99.6

T. P. 11.80 $\overline{915.63}$ 0.89 $\overline{903.83}$
 $\overline{903.88}$
 103+15 01.0

+ 60 03.1

104 05.0

+ 50 07.5

105 10.2

T. P. 12.91 $\overline{925.16}$ 3.38 $\overline{912.30}$ 912.25
 + 50 12.9

+ 80 14.3

106 15.2

+ 50 17.2

L.t.

K

P.T.

$$\begin{array}{r} 4.1 \\ 50 \end{array} \quad \begin{array}{r} 4.8 \\ 25 \end{array} \quad \begin{array}{r} 6.6 \\ 21 \end{array} \quad \begin{array}{r} 5.2 \\ 17 \end{array} \quad \begin{array}{r} 5.7 \\ 14 \end{array} \quad \begin{array}{r} 5.5 \\ 12 \end{array} \quad \begin{array}{r} 5.3 \\ 9 \end{array} \quad \begin{array}{r} 5.1 \\ \end{array} \quad \begin{array}{r} 5.5 \\ 10 \end{array} \quad \begin{array}{r} 5.6 \\ 14 \end{array} \quad \begin{array}{r} 6.0 \\ 19 \end{array} \quad \begin{array}{r} 4.5 \\ 22 \end{array} \quad \begin{array}{r} 3.3 \\ 50 \end{array}$$

$$\begin{array}{r} 5.8 \\ 50 \end{array} \quad \begin{array}{r} 6.3 \\ 35 \end{array} \quad \begin{array}{r} 13.4 \\ 25 \end{array} \quad \begin{array}{r} 14.4 \\ 19 \end{array} \quad \begin{array}{r} 15.2 \\ 16 \end{array} \quad \begin{array}{r} 14.9 \\ 9 \end{array} \quad \begin{array}{r} 14.6 \\ \end{array} \quad \begin{array}{r} 14.9 \\ 10 \end{array} \quad \begin{array}{r} 15.2 \\ 15 \end{array} \quad \begin{array}{r} 15.7 \\ 20 \end{array} \quad \begin{array}{r} 13.3 \\ 29 \end{array} \quad \begin{array}{r} 11.0 \\ 36 \end{array} \quad \begin{array}{r} 6.7 \\ 50 \end{array}$$

$$\begin{array}{r} 6.6 \\ 25 \end{array} + \begin{array}{r} 6.0 \\ 50 \end{array} \quad \begin{array}{r} 9.0 \\ 43 \end{array} \quad \begin{array}{r} 11.8 \\ 25 \end{array} \quad \begin{array}{r} 12.8 \\ 13 \end{array} \quad \begin{array}{r} 13.2 \\ 12 \end{array} \quad \begin{array}{r} 12.6 \\ 9 \end{array} \quad \begin{array}{r} 12.5 \\ \end{array} \quad \begin{array}{r} 13.0 \\ 11 \end{array} \quad \begin{array}{r} 13.2 \\ 14 \end{array} \quad \begin{array}{r} 13.3 \\ 19 \end{array} \quad \begin{array}{r} 10.3 \\ 23 \end{array} \quad \begin{array}{r} 8.1 \\ 35 \end{array} \quad \begin{array}{r} 4.6 \\ 44 \end{array} \quad \begin{array}{r} 3.8 \\ 50 \end{array}$$

$$\begin{array}{r} 8.8 + 8.2 \\ 65 \end{array} \quad \begin{array}{r} 9.0 \\ 39 \end{array} \quad \begin{array}{r} 9.8 \\ 22 \end{array} \quad \begin{array}{r} 10.8 \\ 15 \end{array} \quad \begin{array}{r} 11.3 \\ 14 \end{array} \quad \begin{array}{r} 11.0 \\ 13 \end{array} \quad \begin{array}{r} 10.8 \\ 9 \end{array} \quad \begin{array}{r} 10.6 \\ \end{array} \quad \begin{array}{r} 11.0 \\ 10 \end{array} \quad \begin{array}{r} 11.4 \\ 14 \end{array} \quad \begin{array}{r} 11.9 \\ 17 \end{array} \quad \begin{array}{r} 8.7 \\ 22 \end{array} \quad \begin{array}{r} 7.2 \\ 38 \end{array} \quad \begin{array}{r} 7.0 \\ 50 \end{array}$$

$$\begin{array}{r} 0.0 \\ 50 \end{array} \quad \begin{array}{r} 1.0 \\ 33 \end{array} \quad \begin{array}{r} 6.6 \\ 26 \end{array} \quad \begin{array}{r} 7.5 \\ 19 \end{array} \quad \begin{array}{r} 8.9 \\ 15 \end{array} \quad \begin{array}{r} 8.9 \\ 13 \end{array} \quad \begin{array}{r} 8.5 \\ 12 \end{array} \quad \begin{array}{r} 8.5 \\ 8 \end{array} \quad \begin{array}{r} 8.1 \\ \end{array} \quad \begin{array}{r} 8.3 \\ 11 \end{array} \quad \begin{array}{r} 8.4 \\ 14 \end{array} \quad \begin{array}{r} 8.7 \\ 16 \end{array} \quad \begin{array}{r} 8.3 \\ 17 \end{array} \quad \begin{array}{r} 9.1 \\ 50 \end{array}$$

$$\begin{array}{r} 0.8 \\ 50 \end{array} \quad \begin{array}{r} 3.0 \\ 33 \end{array} \quad \begin{array}{r} 4.4 \\ 20 \end{array} \quad \begin{array}{r} 5.5 \\ 19 \end{array} \quad \begin{array}{r} 5.5 \\ 17 \end{array} \quad \begin{array}{r} 5.1 \\ 16 \end{array} \quad \begin{array}{r} 5.5 \\ 8 \end{array} \quad \begin{array}{r} 5.4 \\ \end{array} \quad \begin{array}{r} 5.8 \\ 10 \end{array} \quad \begin{array}{r} 6.1 \\ 15 \end{array} \quad \begin{array}{r} 7.4 \\ 23 \end{array} \quad \begin{array}{r} 8.2 \\ 50 \end{array}$$

$$\begin{array}{r} 6.1 \\ 50 \end{array} \quad \begin{array}{r} 6.4 \\ 43 \end{array} \quad \begin{array}{r} 9.6 \\ 34 \end{array} \quad \begin{array}{r} 11.2 \\ 23 \end{array} \quad \begin{array}{r} 12.1 \\ 22 \end{array} \quad \begin{array}{r} 12.1 \\ 20 \end{array} \quad \begin{array}{r} 11.6 \\ 19 \end{array} \quad \begin{array}{r} 12.4 \\ 8 \end{array} \quad \begin{array}{r} 12.3 \\ \end{array} \quad \begin{array}{r} 12.7 \\ 11 \end{array} \quad \begin{array}{r} 13.2 \\ 16 \end{array} \quad \begin{array}{r} 14.5 \\ 22 \end{array} \quad \begin{array}{r} 16.4 \\ 50 \end{array}$$

$$\begin{array}{r} 2.7 \\ 32 \end{array} \quad \begin{array}{r} 3.0 \\ 47 \end{array} \quad \begin{array}{r} 4.9 \\ 39 \end{array} \quad \begin{array}{r} 11.0 \\ 23 \end{array} \quad \begin{array}{r} 11.0 \\ 21 \end{array} \quad \begin{array}{r} 10.4 \\ 20 \end{array} \quad \begin{array}{r} 10.9 \\ 8 \end{array} \quad \begin{array}{r} 10.9 \\ \end{array} \quad \begin{array}{r} 11.2 \\ 10 \end{array} \quad \begin{array}{r} 11.6 \\ 14 \end{array} \quad \begin{array}{r} 13.6 \\ 23 \end{array} \quad \begin{array}{r} 15.3 \\ 32 \end{array} \quad \begin{array}{r} 14.9 \\ 37 \end{array} \quad \begin{array}{r} 15. \\ 50 \end{array}$$

$$\begin{array}{r} 2.2 \\ 50 \end{array} \quad \begin{array}{r} 3.3 \\ 39 \end{array} \quad \begin{array}{r} 5.7 \\ 31 \end{array} \quad \begin{array}{r} 8.7 \\ 25 \end{array} \quad \begin{array}{r} 9.9 \\ 24 \end{array} \quad \begin{array}{r} 9.9 \\ 21 \end{array} \quad \begin{array}{r} 9.6 \\ 20 \end{array} \quad \begin{array}{r} 10.1 \\ 8 \end{array} \quad \begin{array}{r} 10.0 \\ \end{array} \quad \begin{array}{r} 10.4 \\ 10 \end{array} \quad \begin{array}{r} 10.7 \\ 14 \end{array} \quad \begin{array}{r} 13.0 \\ 18 \end{array} \quad \begin{array}{r} 14.0 \\ 24 \end{array} \quad \begin{array}{r} 12.6 \\ 27 \end{array} \quad \begin{array}{r} 12.5 \\ 37 \end{array} \quad \begin{array}{r} 13. \\ 50 \end{array}$$

$$\begin{array}{r} 1.8 \\ 50 \end{array} \quad \begin{array}{r} 2.9 \\ 35 \end{array} \quad \begin{array}{r} 6.9 \\ 26 \end{array} \quad \begin{array}{r} 8.4 \\ 23 \end{array} \quad \begin{array}{r} 8.4 \\ 21 \end{array} \quad \begin{array}{r} 7.7 \\ 20 \end{array} \quad \begin{array}{r} 8.0 \\ 8 \end{array} \quad \begin{array}{r} 8.0 \\ \end{array} \quad \begin{array}{r} 8.1 \\ 8 \end{array} \quad \begin{array}{r} 7.8 \\ 12 \end{array} \quad \begin{array}{r} 8.6 \\ 15 \end{array} \quad \begin{array}{r} 8.7 \\ 19 \end{array} \quad \begin{array}{r} 7.0 \\ 33 \end{array} \quad \begin{array}{r} 6.7 \\ 43 \end{array} \quad \begin{array}{r} 7.5 \\ 50 \end{array}$$

Sta	+	π 925.16 <u>925.21</u>	-	Elev.
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107				19.7
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+08				20.1
-----	--	--	--	------

+15				20.7
-----	--	--	--	------

+29				21.6
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B.M.	11.52	✓ 932.99	3.72	<u>921.49</u> 921.44	921.47
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+45				22.0
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+51				22.1
-----	--	--	--	------

+56				22.2
-----	--	--	--	------

+60				22.2
-----	--	--	--	------

+64				22.3
-----	--	--	--	------

108				22.7
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L+

±

Rt.

$$\frac{1.9}{50} \quad \frac{2.1}{43} \quad \frac{5.3}{35} \quad \frac{4.0}{25} \quad \frac{4.2}{24} \quad \frac{5.6}{8} \quad \frac{5.5}{12} \quad \frac{5.9}{19} \quad \frac{5.5}{19} \quad \frac{7.0}{22} \quad \frac{7.1}{28} \quad \frac{5.7}{31} \quad \frac{4.7}{50}$$

$$\frac{3.5}{50} \quad \frac{4.5}{39} \quad \frac{3.1}{33} \quad \frac{4.9}{13} \quad \frac{5.1}{14} \quad \frac{5.3}{14} \quad \frac{5.0}{25} \quad \frac{6.9}{29} \quad \frac{6.8}{33} \quad \frac{5.7}{50}$$

$$\frac{2.1}{50} \quad \frac{3.7}{21} \quad \frac{4.5}{21} \quad \frac{4.6}{23} \quad \frac{4.0}{50}$$

$$\frac{2.0}{50} \quad \frac{3.6}{50} \quad \frac{3.6}{50}$$

R.R. Sph. 14 P. N. E. Cor. Dale St. & Co. Rd. C. 28' Rt 107+58

$$\frac{9.6}{50} \quad \frac{11.0}{50} \quad \frac{11.5}{50}$$

$$\frac{10.9}{50} \quad \frac{10.3}{33}$$

$$\frac{10.9}{25} \quad \frac{11.2}{27} \quad \frac{13.3}{32} \quad \frac{13.3}{32} \quad \frac{13.7}{50}$$

$$\frac{12.1}{50} \quad \frac{13.4}{25} \quad \frac{10.5}{21} \quad \frac{10.8}{19} \quad \frac{11.1}{19} \quad \frac{13.7}{24} \quad \frac{13.7}{26} \quad \frac{11.9}{28} \quad \frac{11.3}{50}$$

$$\frac{11.9}{50} \quad \frac{13.2}{22} \quad \frac{10.5}{17}$$

$$\frac{10.8}{18} \quad \frac{11.1}{22} \quad \frac{13.0}{26} \quad \frac{13.1}{34} \quad \frac{9.8}{50} \quad \frac{7.8}{50}$$

$$\frac{9.8}{50} \quad \frac{10.9}{29} \quad \frac{13.0}{25} \quad \frac{12.9}{22} \quad \frac{10.9}{17} \quad \frac{10.7}{17} \quad \frac{11.1}{17} \quad \frac{12.8}{21} \quad \frac{12.9}{25} \quad \frac{9.6}{35} \quad \frac{9.7}{50}$$

$$\frac{8.6}{50} \quad \frac{9.8}{22} \quad \frac{11.5}{19} \quad \frac{11.6}{16} \quad \frac{10.3}{12}$$

$$\frac{10.3}{16} \quad \frac{10.5}{20} \quad \frac{11.7}{26} \quad \frac{11.7}{26} \quad \frac{9.2}{32} \quad \frac{9.1}{42}$$

Sta	+	π	-	Elev
		✓ 932.99		

108	+50			23.6
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109				24.4
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	+50			25.2
--	-----	--	--	------

110				26.4
-----	--	--	--	------

	+50			27.4
--	-----	--	--	------

111				28.6
-----	--	--	--	------

	+50			30.0
--	-----	--	--	------

T.P.	10.50	✓ 940.99	2.50	✓ 930.49
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112				31.3
-----	--	--	--	------

	+50			32.3
--	-----	--	--	------

113				33.3
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	+50			34.2
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9/19/38
K.A.
L.B.H.
L.C.
M.D.G.

22

LT E RT

$\frac{78}{50} \frac{91}{26} \frac{99}{17} \frac{100}{8} \frac{96}{6} \frac{74}{12} \frac{98}{12} \frac{101}{16} \frac{94}{21} \frac{92}{33} \frac{86}{50}$

$\frac{55}{50} \frac{73}{24} \frac{85}{13} \frac{91}{10} \frac{89}{6} \frac{86}{11} \frac{89}{13} \frac{92}{24} \frac{93}{26} \frac{90}{35} \frac{90}{30} \frac{88}{30}$

$\frac{29}{50} \frac{57}{25} \frac{74}{14} \frac{84}{9} \frac{79}{5} \frac{78}{9} \frac{80}{20} \frac{90}{25} \frac{85}{38} \frac{76}{30} \frac{72}{30}$

$\frac{10}{50} \frac{30}{31} \frac{57}{22} \frac{73}{14} \frac{68}{5} \frac{66}{11} \frac{71}{18} \frac{78}{22} \frac{88}{38} \frac{80}{30} \frac{68}{50}$

$\frac{0.9}{50} \frac{36}{25} \frac{56}{20} \frac{58}{13} \frac{64}{11} \frac{59}{50} \frac{56}{9} \frac{59}{18} \frac{67}{26} \frac{98}{35} \frac{107}{41} \frac{100}{50} \frac{90}{50}$

$\frac{113}{50} \frac{102}{45} \frac{19}{28} \frac{37}{23} \frac{48}{12} \frac{53}{12} \frac{48}{6} \frac{44}{11} \frac{48}{11} \frac{51}{19} \frac{111}{32} \frac{118}{50}$

$\frac{466}{50} \frac{429}{27} \frac{24}{20} \frac{32}{11} \frac{38}{11} \frac{33}{6} \frac{30}{11} \frac{34}{14} \frac{36}{21} \frac{39}{33} \frac{89}{33} \frac{96}{30}$

$\frac{04}{50} \frac{31}{28} \frac{85}{20} \frac{98}{11} \frac{103}{11} \frac{98}{6} \frac{97}{11} \frac{103}{11} \frac{106}{16} \frac{95}{18} \frac{12.7}{29} \frac{130}{36} \frac{144}{43} \frac{142}{50}$

$\frac{2.6}{50} \frac{42}{22} \frac{92}{11} \frac{88}{5} \frac{87}{11} \frac{91}{17} \frac{91}{21} \frac{73}{26} \frac{74}{28} \frac{85}{38} \frac{88}{39} \frac{100}{39} \frac{10.2}{50}$

$\frac{35}{50} \frac{46}{18} \frac{77}{10} \frac{81}{10} \frac{77}{10} \frac{81}{10} \frac{79}{18} \frac{32}{25} \frac{90}{37} \frac{56}{50}$

$\frac{24}{50} \frac{37}{23} \frac{39}{16} \frac{74}{10} \frac{6.9}{5} \frac{68}{9} \frac{70}{14} \frac{72}{20} \frac{64}{20} \frac{25}{26} \frac{27}{37} \frac{93}{50}$

Sta.	+	π	-	Elev
		✓ 940.99		

114				35.3
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	+90			36.4
T.P.	6.66	✓ 941.74	3.91	✓ 937.08

	+76			37.0
--	-----	--	--	------

115				37.2
-----	--	--	--	------

	+50			37.0
--	-----	--	--	------

116				36.0
-----	--	--	--	------

	+50			34.3
--	-----	--	--	------

117				32.2
-----	--	--	--	------

	+50			29.9
T.P.	2.30	✓ 933.00	13.04	✓ 930.70

118				27.1
-----	--	--	--	------

	+50			24.3
--	-----	--	--	------

B.M.			6.35	✓ 926.65
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926.65

LT E RT

$$\frac{32}{50} \quad \frac{34}{32} \quad \frac{47}{11} \quad \frac{59}{11} \quad \frac{57}{-} \quad \frac{58}{9} \quad \frac{58}{18} \quad \frac{32}{21} \quad \frac{36}{35} \quad \frac{41}{50}$$

$$\frac{26}{50} \quad \frac{34}{24} \quad \frac{46}{10} \quad \frac{46}{8} \quad \frac{48}{12} \quad \frac{51}{15} \quad \frac{40}{24} \quad \frac{46}{32} \quad \frac{68}{32} \quad \frac{79}{50}$$

$$\frac{23}{50} \quad \frac{26}{29} \quad \frac{67}{12} \quad \frac{67}{-} \quad \frac{70}{12} \quad \frac{56}{18} \quad \frac{68}{26} \quad \frac{89}{40} \quad \frac{100}{50}$$

$$\frac{22}{50} \quad \frac{20}{30} \quad \frac{67}{12}$$

$$\frac{65}{9} \quad \frac{68}{16} \quad \frac{68}{21} \quad \frac{45}{33} \quad \frac{67}{50} \quad \frac{86}{50}$$

$$\frac{20}{30} \quad \frac{18}{25} \quad \frac{59}{16} \quad \frac{71}{10} \quad \frac{67}{-} \quad \frac{70}{9} \quad \frac{72}{14} \quad \frac{52}{21} \quad \frac{52}{27} \quad \frac{95}{50}$$

$$\frac{21}{50} \quad \frac{23}{32} \quad \frac{32}{20} \quad \frac{83}{10} \quad \frac{79}{60} \quad \frac{77}{10} \quad \frac{81}{14} \quad \frac{80}{21} \quad \frac{54}{29} \quad \frac{70}{50} \quad \frac{111}{50}$$

$$\frac{46}{50} \quad \frac{44}{29} \quad \frac{70}{15} \quad \frac{102}{10} \quad \frac{96}{6} \quad \frac{94}{-} \quad \frac{96}{8} \quad \frac{101}{14} \quad \frac{65}{18} \quad \frac{76}{24} \quad \frac{91}{36} \quad \frac{113}{50}$$

$$\frac{73}{50} \quad \frac{67}{31} \quad \frac{15}{20} \quad \frac{89}{15} \quad \frac{122}{10} \quad \frac{118}{7} \quad \frac{115}{-} \quad \frac{116}{9} \quad \frac{119}{14} \quad \frac{108}{19} \quad \frac{71}{21} \quad \frac{81}{35} \quad \frac{101}{50}$$

$$\frac{86}{50} \quad \frac{77}{28} \quad \frac{93}{18} \quad \frac{149}{13} \quad \frac{140}{7} \quad \frac{138}{-} \quad \frac{140}{7} \quad \frac{145}{14} \quad \frac{122}{15} \quad \frac{79}{24} \quad \frac{76}{34} \quad \frac{80}{50}$$

$$\frac{18}{50} \quad \frac{07}{25} \quad \frac{17}{18} \quad \frac{69}{12} \quad \frac{64}{8} \quad \frac{59}{-} \quad \frac{62}{8} \quad \frac{62}{14} \quad \frac{38}{14} \quad \frac{05}{23} \quad \frac{06}{37} \quad \frac{00}{50}$$

$$\frac{47}{30} \quad \frac{38}{28} \quad \frac{37}{18} \quad \frac{95}{12} \quad \frac{90}{8} \quad \frac{87}{6} \quad \frac{89}{13} \quad \frac{90}{14} \quad \frac{72}{20} \quad \frac{19}{34} \quad \frac{41}{50} \quad \frac{33}{50}$$

Sta	+	Σ ✓ 999.00	-	Elev	
119				21.5	
	+50			18.6	
T.P.	2.15	✓ 921.47	13.68	✓ 917.32	
120				16.0	
	+35			14.4	
	+70			12.7	
121				11.2	
	+50			08.4	
T.P.	0.18	✓ 908.42	12.23	✓ 908.24	
122				05.5	
	+45			02.9	
123				99.8	
	+30			98.2	
T.P.	1.45	898.75 898.77	11.12	897.32	897.30

LT

E

RT

$$\frac{71}{50} \quad \frac{67}{20} \quad \frac{110}{19} \quad \frac{125}{13} \quad \frac{119}{8} \quad \frac{115}{7} \quad \frac{116}{7} \quad \frac{118}{13} \quad \frac{102}{13} \quad \frac{72}{19} \quad \frac{78}{29} \quad \frac{67}{50}$$

$$\frac{88}{50} \quad \frac{92}{20} \quad \frac{152}{11} \quad \frac{140}{8} \quad 1 \quad 144 \quad \frac{125}{7} \quad \frac{150}{13} \quad \frac{129}{13} \quad \frac{94}{19} \quad \frac{102}{28} \quad \frac{90}{37} \quad \frac{89}{50}$$

$$\frac{11}{50} \quad \frac{14}{19} \quad \frac{62}{13} \quad \frac{55}{7} \quad \frac{56}{14} \quad \frac{61}{21} \quad \frac{06}{27} \quad \frac{101}{50} \quad \frac{114}{50}$$

$$\frac{47}{50} \quad \frac{51}{17} \quad \frac{73}{72} \quad \frac{74}{7} \quad \frac{71}{6} \quad \frac{73}{13} \quad \frac{78}{13} \quad \frac{54}{17} \quad \frac{40}{21} \quad \frac{97}{21} \quad \frac{16}{26} \quad \frac{02}{50}$$

$$\frac{88}{50} \quad \frac{87}{23} \quad \frac{72}{17} \quad \frac{82}{14} \quad \frac{95}{12} \quad \frac{90}{7} \quad \frac{88}{7} \quad \frac{91}{15} \quad \frac{94}{16} \quad \frac{77}{22} \quad \frac{71}{26} \quad \frac{48}{33} \quad \frac{27}{50} \quad \frac{24}{50}$$

$$\frac{124}{50} \quad \frac{115}{24} \quad \frac{102}{17} \quad \frac{108}{13} \quad \frac{115}{11} \quad \frac{109}{9} \quad \frac{103}{7} \quad \frac{106}{14} \quad \frac{112}{19} \quad \frac{107}{28} \quad \frac{69}{35} \quad \frac{52}{50} \quad \frac{43}{50}$$

$$\frac{195}{50} \quad \frac{173}{28} \quad \frac{137}{19} \quad \frac{136}{10} \quad \frac{134}{6} \quad \frac{131}{8} \quad \frac{134}{24} \quad \frac{140}{27} \quad \frac{117}{37} \quad \frac{96}{37} \quad \frac{95}{50}$$

$$\frac{123}{50} \quad \frac{85}{23} \quad \frac{41}{21} \quad \frac{33}{9} \quad \frac{29}{8} \quad \frac{33}{17} \quad \frac{38}{19} \quad \frac{31}{23} \quad \frac{37}{29} \quad \frac{48}{40} \quad \frac{42}{46} \quad \frac{39}{50}$$

$$\frac{147}{50} \quad \frac{126}{28} \quad \frac{68}{17} \quad \frac{61}{9} \quad \frac{53}{6} \quad \frac{58}{17} \quad \frac{62}{26} \quad \frac{93}{42} \quad \frac{90}{50} \quad \frac{92}{50}$$

$$\frac{116}{50} \quad \frac{105}{23} \quad \frac{88}{9} \quad \frac{86}{7} \quad \frac{88}{19} \quad \frac{94}{28} \quad \frac{110}{50} \quad \frac{109}{50}$$

$$\frac{115}{50} \quad \frac{114}{24} \quad \frac{116}{20} \quad \frac{108}{15} \quad \frac{106}{8} \quad \frac{102}{6} \quad \frac{103}{16} \quad \frac{106}{27} \quad \frac{113}{50} \quad \frac{117}{50}$$

Sta	+	Σ 898.75 <u>898.77</u>	-	Elev
123	+75			95.9
124				94.7
	+25			93.5
	+82			91.1
125				90.4
	+50			88.6
T.P.	+45	892.35 <u>892.37</u>	10.15	<u>887.92</u> 887.90
126				87.4
	+50			86.7
127				86.8
	+50			87.3
128				87.7

LT

E

RT

$$\frac{42}{50} \frac{54}{50} \frac{50}{19} \frac{36}{15} \frac{32}{8} \frac{29}{6} \frac{30}{11} \frac{34}{16} \frac{58}{23} \frac{58}{26} \frac{49}{31} \frac{38}{50}$$

$$\frac{46}{50} \frac{64}{28} \frac{76}{20} \frac{47}{15} \frac{44}{7} \frac{41}{6} \frac{44}{11} \frac{47}{17} \frac{76}{25} \frac{76}{32} \frac{64}{41} \frac{64}{50}$$

$$\frac{60}{50} \frac{74}{32} \frac{79}{19} \frac{57}{14} \frac{56}{8} \frac{53}{6} \frac{58}{12} \frac{58}{17} \frac{88}{38} \frac{95}{50} \frac{84}{50}$$

$$\frac{93}{50} \frac{107}{28} \frac{107}{20} \frac{80}{11} \frac{81}{8} \frac{77}{6} \frac{79}{6} \frac{83}{11} \frac{123}{19} \frac{126}{31} \frac{119}{50}$$

$$\frac{100}{50} \frac{114}{27} \frac{118}{18} \frac{88}{13} \frac{86}{7} \frac{84}{6} \frac{86}{11} \frac{87}{20} \frac{133}{40} \frac{133}{50} \frac{128}{50}$$

$$\frac{139}{50} \frac{137}{18} \frac{105}{12} \frac{102}{6} \frac{104}{5} \frac{107}{11} \frac{156}{19} \frac{148}{26} \frac{170}{50}$$

$$\frac{99}{50} \frac{95}{20} \frac{53}{12} \frac{51}{6} \frac{50}{6} \frac{54}{10} \frac{56}{21} \frac{113}{28} \frac{131}{50} \frac{135}{50}$$

$$\frac{105}{50} \frac{106}{21} \frac{59}{12} \frac{57}{6} \frac{62}{11} \frac{128}{23} \frac{147}{35} \frac{149}{50}$$

$$\frac{106}{50} \frac{108}{18} \frac{60}{11} \frac{58}{7} \frac{56}{6} \frac{60}{11} \frac{62}{19} \frac{112}{30} \frac{146}{50} \frac{157}{50}$$

$$\frac{88}{50} \frac{103}{36} \frac{105}{22} \frac{56}{12} \frac{54}{7} \frac{51}{6} \frac{55}{7} \frac{55}{11} \frac{104}{17} \frac{139}{29} \frac{148}{50}$$

$$\frac{65}{50} \frac{74}{37} \frac{89}{21} \frac{50}{12} \frac{43}{8} \frac{47}{9} \frac{50}{9} \frac{52}{18} \frac{101}{23} \frac{120}{50} \frac{135}{50}$$

Sta.	+	π	-	Elev.
		892.35 <u>892.37</u>		
128	+34			88.2
		902.37		888.97
T.P.	13.40	<u>902.39</u>	3.38	<u>888.97</u>
	+60			88.8
129				89.8
	+50			90.9
	+82			91.5
130		898.19		91.9
				892.03
T.P.	6.16	<u>898.21</u>	10.34	<u>892.05</u>
	+90			92.6
	+65			92.8
	+82			93.1
	+99.5 = E. So. Rail			
131	+02.55			93.4
				892.65
B.M.			5.54	<u>892.67</u>
				892.62

Lt.

R.

Rt.

$\frac{120}{50}$ $\frac{68}{31}$ $\frac{63}{21}$ $\frac{45}{18}$ $\frac{43}{8}$ $\frac{42}{-}$ $\frac{44}{5}$ $\frac{47}{10}$ $\frac{94}{16}$ $\frac{107}{22}$ $\frac{111}{37}$ $\frac{117}{50}$

$\frac{25}{100}$ $\frac{26}{63}$ $\frac{52}{40}$ $\frac{140}{27}$ $\frac{146}{15}$ $\frac{139}{8}$ $\frac{134}{5}$ $\frac{139}{10}$ $\frac{141}{16}$ $\frac{179}{16}$ $\frac{199}{32}$ $\frac{204}{50}$

$\frac{31}{100}$ $\frac{37}{80}$ $\frac{16}{50}$ $\frac{20}{41}$ $\frac{111}{28}$ $\frac{130}{18}$ $\frac{129}{9}$ $\frac{126}{-}$

$\frac{130}{7}$ $\frac{143}{21}$ $\frac{146}{38}$ $\frac{153}{50}$

$\frac{59}{85}$ $\frac{51}{50}$ $\frac{51}{39}$ $\frac{103}{31}$ $\frac{126}{23}$ $\frac{119}{10}$ $\frac{115}{-}$ $\frac{119}{8}$ $\frac{121}{14}$ $\frac{160}{30}$ $\frac{178}{50}$

$\frac{95}{75}$ $\frac{85}{55}$ $\frac{84}{36}$ $\frac{126}{28}$ $\frac{120}{18}$ $\frac{114}{9}$ $\frac{107}{-}$ $\frac{114}{9}$ $\frac{117}{16}$ $\frac{140}{22}$ $\frac{130}{28}$ $\frac{71}{35}$ $\frac{57}{50}$ $\frac{59}{66}$ $\frac{131}{80}$ $\frac{68}{95}$

$\frac{180}{50}$ $\frac{96}{39}$ $\frac{111}{28}$ $\frac{114}{19}$ $\frac{110}{7}$ $\frac{105}{-}$ $\frac{111}{9}$ $\frac{115}{15}$ $\frac{134}{23}$ $\frac{126}{28}$ $\frac{88}{39}$ $\frac{81}{50}$ $\frac{68}{75}$ $\frac{57}{100}$

$\frac{61}{52}$ $\frac{104}{40}$ $\frac{103}{28}$ $\frac{100}{22}$ $\frac{64}{14}$ $\frac{60}{7}$ $\frac{56}{-}$ $\frac{60}{8}$ $\frac{63}{15}$ $\frac{80}{21}$ $\frac{81}{35}$ $\frac{77}{50}$

Top Rail

$\frac{453}{45}$ $\frac{52}{43}$ $\frac{64}{37}$ $\frac{103}{25}$ $\frac{85}{19}$ $\frac{62}{13}$ $\frac{56}{6}$ $\frac{54}{-}$ $\frac{57}{8}$ $\frac{61}{14}$ $\frac{86}{21}$ $\frac{90}{39}$ $\frac{90}{50}$

Top Rail

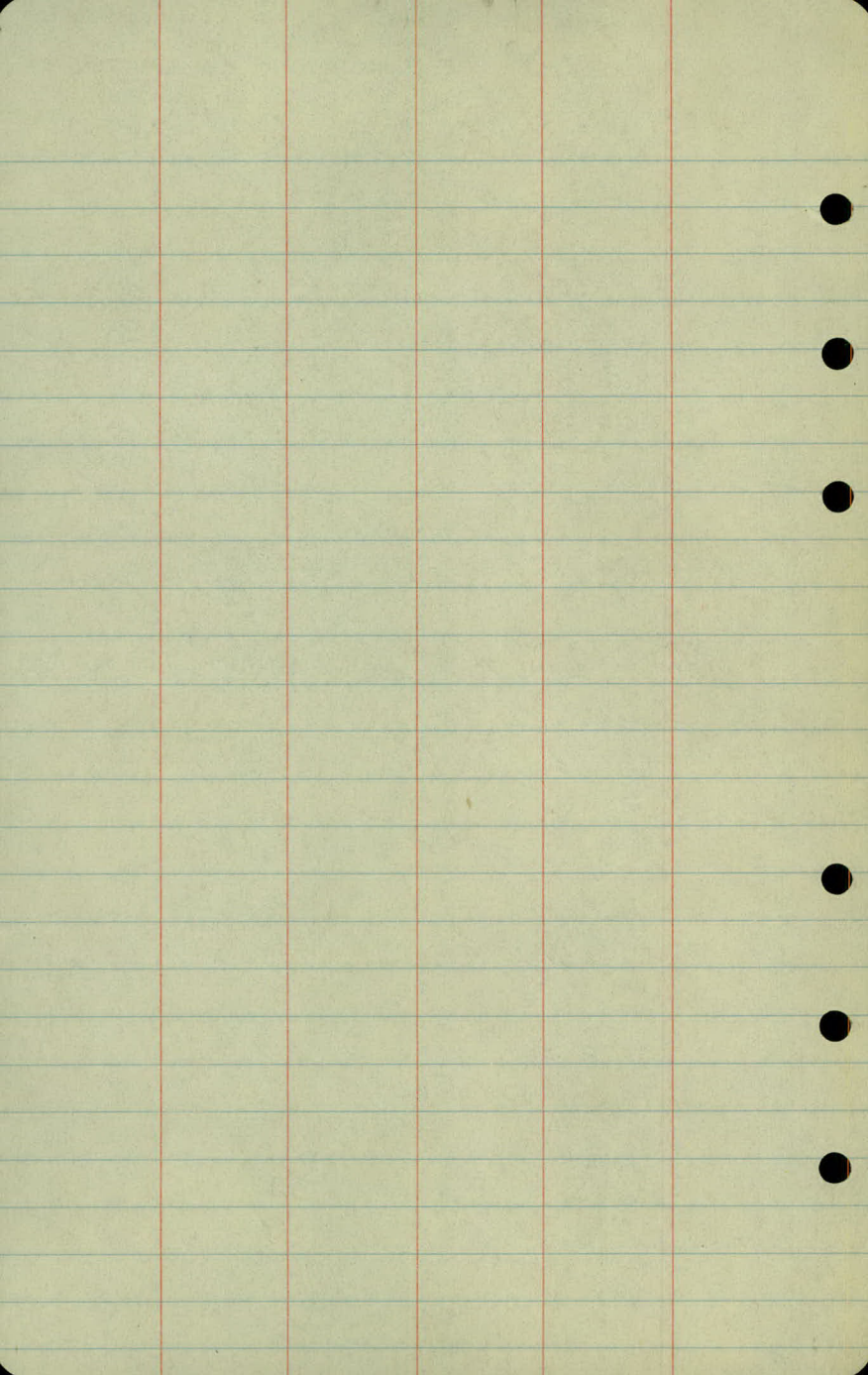
$\frac{465}{263}$ $\frac{54}{23}$ $\frac{62}{19}$ $\frac{55}{10}$ $\frac{52}{6}$ $\frac{51}{-}$ $\frac{53}{8}$ $\frac{56}{15}$ $\frac{96}{23}$ $\frac{98}{37}$ $\frac{99}{50}$

93.37

$\frac{482}{78 \text{ Rail}}$

$\frac{128}{50}$ $\frac{128}{23}$ $\frac{50}{11}$ $\frac{48}{-}$ $\frac{47}{8}$ $\frac{51}{14}$ $\frac{99}{21}$ $\frac{103}{37}$ $\frac{104}{50}$

Spk in G.P. 20' N. 10' W. of R.R. Tracks.



Dale St.
Slope stakes.

15 Pages

Sta.	+	π	-	Grade.
B.M.	4.29	941.49		937.20

80 +65.3

+80

+89

81

+50

82

+50

83

+50

84

+50

T.P.	1.12	936.54	6.07	933.42
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Ger. Rod. Lt K Rt.

Spk. in T.P.N.W. Ger. Rod. 40²⁴

✓ 3.9	$256 / \frac{46}{25.13}$	$\frac{44}{25.15 / 26.0}$
4.4	$268 / \frac{45}{25.19}$	$\frac{49}{25.15 / 26.0}$
4.7	$266 / \frac{59}{25.18}$	$\frac{58}{25.09 / 26.8}$
5.1	$260 / \frac{56}{25.15}$	$\frac{56}{25.15 / 26.0}$
5.5	$256 / \frac{62}{25.13}$	$\frac{65}{25.10 / 26.0}$
5.8	$298 / \frac{69}{25.09}$	$\frac{74}{25.04 / 23.8}$
6.1	$298 / \frac{72}{25.09}$	$\frac{78}{25.03 / 23.0}$
6.3	$258 / \frac{69}{25.14}$	$\frac{79}{25.04 / 23.8}$

349.

+

π

-

Grade

736.54

85

+50

86

+50

87

+15

+22

+47

+58

88

beg. gutter at 4th.

+26

Gr. Rod

Lt

Ls

Rt

$$1.4 \quad 26.0 / \frac{1.9}{\cancel{4.15}}$$

$$\frac{26}{\cancel{4.08}} / 2.46$$

$$1.6 \quad 26.2 / \frac{2.0}{\cancel{4.16}}$$

$$\frac{26}{\cancel{4.10}} / 2.50$$

$$2.3 \quad 28.0 / \frac{1.8}{\cancel{4.25}}$$

$$\frac{28}{\cancel{4.17}} / 2.68$$

$$3.0 \quad 29.2 / \frac{1.9}{\cancel{4.31}}$$

$$\frac{29}{\cancel{4.25}} / 2.80$$

$$3.9 \quad 30.8 / \frac{2.0}{\cancel{4.39}}$$

$$\frac{29}{\cancel{4.29}} / 3.00$$

$$4.4 \quad 32.0 / \frac{1.9}{\cancel{4.45}}$$

$$\frac{2.5}{\cancel{4.39}} / 3.08$$

$$6.1 \quad 33.0 / \frac{2.0}{\cancel{4.61}}$$

$$\frac{0.8}{\cancel{4.73}} / 3.00$$

$$8.0 \quad 35.0 / \frac{2.5}{\cancel{4.75}}$$

$$\frac{0.8}{\cancel{4.92}} / 3.00$$

$$9.4 \quad 35.0 / \frac{3.5}{\cancel{4.79}}$$

$$\frac{3.6}{\cancel{4.78}} / 3.00$$

Sto. + A - Grade

936.59

88 +65

89

T.P. 2.99 926.68 12.85 923.69

+50

90

+50

91

T.P. 0.05 913.58 13.15 913.53

+50

92

+25

+25 End gutter.

+69

T.P. 0.51 903.86 10.23 903.35

93

Gr. Rod.

Lt

Q

Rt

$$11.4 \quad \frac{330}{24} / \frac{7.9}{4.60}$$

$$\frac{28}{4.86} / 33.0$$

$$13.2 \quad \frac{33.0}{7.9} / \frac{7.9}{4.53}$$

$$\frac{55}{4.97} / 33.0$$

$$5.8 \quad \frac{32.2}{4.96} / \frac{3.2}{4.96}$$

$$\frac{1.1}{4.67} / 33.0$$

$$8.5 \quad \frac{30.6}{4.38} / \frac{6.7}{4.38}$$

$$\frac{5.9}{4.46} / 32.2$$

$$11.0 \quad \frac{29.6}{4.53} / \frac{9.7}{4.53}$$

$$\frac{7.7}{4.33} / 29.6$$

$$13.4 \quad \frac{28.6}{4.2.8} / \frac{12.6}{4.2.8}$$

$$\frac{11.8}{4.31} / 30.2$$

$$3.1 \quad \frac{28.2}{4.26} / \frac{2.5}{4.26}$$

$$\frac{0.3}{4.48} / 32.6$$

$$5.7 \quad \frac{25.8}{4.7.4} / \frac{6.3}{4.7.4}$$

$$\frac{3.7}{4.90} / 31.0$$

$$6.9 \quad \frac{6.4}{4.25} / 28.0$$

$$9.0 \quad \frac{25.4}{3.2} / \frac{14.2}{3.2}$$

$$\frac{11.6}{2.8} / 20.2$$

$$0.8 \quad \frac{15.0}{0.8} / \frac{0.8}{0.8}$$

$$\frac{4.4}{3.6} / 22.2$$

Sta. + π - Grade

903.86

93 +50

900.7

B.M.

5.58

898.28

898.28

94

898.4

+50

96.5

95

95.1

T.P.

1.68
0.37

895.16

898.65

9.78

894.08

898.25

+50

94.1

96

93.4

+50

92.2

97

92.2

+50

98

T.P.

5.91

897.00

7.56

891.09

+50

92.2

Gen. Rad.

Lt.

46

Rt.

3.2	$\frac{250}{-5.0} / \frac{82}{-5.0}$	$\frac{32}{-10}$	$\frac{87}{-57} / 26.4$
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Top Brother R.T. 93+74

5.5	$\frac{286}{-6.8} / \frac{123}{-6.8}$	$\frac{38}{-0.3}$	$\frac{135}{-80} / 21.0$
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7.4	$\frac{262}{-5.6} / \frac{130}{-5.6}$	$\frac{77}{-0.5}$	$\frac{135}{-0.7} / 27.2$
-----	---------------------------------------	-------------------	---------------------------

8.8	$\frac{244}{-5.7} / \frac{145}{-5.7}$	$\frac{98}{-1.0}$	$\frac{145}{-8.7} / 26.4$
-----	---------------------------------------	-------------------	---------------------------

4.6	$\frac{25.2}{-5.1} / \frac{97}{-5.1}$	$\frac{60}{-1.4}$	$\frac{99}{-53} / 25.6$
-----	---------------------------------------	-------------------	-------------------------

5.3	$\frac{244}{-4.7} / \frac{100}{-4.7}$	$\frac{68}{-1.5}$	$\frac{101}{-48} / 24.6$
-----	---------------------------------------	-------------------	--------------------------

5.5	$\frac{24.8}{-4.7} / \frac{104}{-4.7}$	$\frac{72}{-1.7}$	$\frac{107}{-5.2} / 25.4$
-----	--	-------------------	---------------------------

5.5	$\frac{250}{-5.0} / \frac{105}{-5.0}$	$\frac{75}{-2.0}$	$\frac{110}{-55} / 26.0$
-----	---------------------------------------	-------------------	--------------------------

5.5	$\frac{264}{-5.7} / \frac{110}{-5.7}$	$\frac{75}{-2.0}$	$\frac{118}{-58} / 26.6$
-----	---------------------------------------	-------------------	--------------------------

5.5	$\frac{270}{-6.0} / \frac{116}{-6.0}$	$\frac{76}{-2.1}$	$\frac{114}{-59} / 26.8$
-----	---------------------------------------	-------------------	--------------------------

3.8	$\frac{278}{-6.4} / \frac{102}{-6.4}$	$\frac{58}{-2.0}$	$\frac{98}{-64} / 27.0$
-----	---------------------------------------	-------------------	-------------------------

Sta.	+	π	-	Grade
		895.76 (897.00)		
99				93.2
	+50			
100				93.2
	+50			93.3
101				93.7
	+50			94.6
T.P.	10.04	905.58	0.25	895.51
102				95.9
	+50	Reg. Gutters		97.6
	+88			99.2
T.P.	13.03	914.15	4.43	901.12
103				900.5
	+15			

Car. Prod.

14

4

Rt.

(3.8)

$$280 / \frac{10.7}{-6.5}$$

$$\frac{39}{-2.1}$$

$$\frac{10.0}{-6.2} / 27.4$$

(3.8)

$$278 / \frac{10.2}{-6.4}$$

$$\frac{39}{-2.1}$$

$$\frac{10.2}{-6.4} / 27.8$$

(3.8)

$$27.8 / \frac{10.2}{-6.4}$$

$$\frac{38}{-2.0}$$

$$\frac{10.2}{-6.4} / 27.8$$

(3.8)

$$27.6 / \frac{10.1}{-6.3}$$

$$\frac{37}{-1.9}$$

$$\frac{10.1}{-6.3} / 27.6$$

(3.2)

$$28.0 / \frac{9.8}{-6.5}$$

$$\frac{31}{-1.8}$$

$$\frac{9.7}{-6.4} / 27.8$$

(2.4)

$$27.0 / \frac{8.9}{-6.0}$$

$$\frac{3.7}{-1.3}$$

$$\frac{8.9}{-6.5} / 28.0$$

(1.1)

9.7

$$228 / \frac{13.6}{-2.9}$$

$$\frac{15}{-0.4}$$

$$\frac{5.8}{-2.7} / 24.4$$

4
1.9

$$24.6 / \frac{7.1}{-2.8}$$

$$\frac{9.0}{-2.9} / 24.8$$

6.0

$$27.4 / \frac{4.8}{-6.3.2}$$

$$\frac{4.9}{-6.3.6} / 30.2$$

13.3

$$33.0 / \frac{6.3}{-2.9.0}$$

$$\frac{10.2}{-6.5.1} / 33.0$$

Sta	+	X	-	Grade
		719.15		
103	+60			902.8
104				
	+50	End Gutter Rt.		
105				909.9
T.P.	11.19	929.09	1.25	912.90
	+50			12.7
	+80			14.4
106				15.5
	+50			18.2
107	+90	End Gutter Lt.		20.4
	+08			20.8
	+15			21.1

Cor. Rod.

Lt.

R.

Rt.

$$11.3 \quad 33.0 / \begin{array}{r} 51 \\ R 52 \end{array}$$

$$67 \\ 42.64 / 33.0$$

$$9.4 \quad 32.0 / \begin{array}{r} 24 \\ R 94 \end{array}$$

$$62 \\ 42.52 / 33.0$$

$$6.9 \quad 31.0 / \begin{array}{r} 00 \\ R 89 \end{array}$$

$$72 \\ 42.17 / 26.4$$

$$4.3 \quad 32.6 / \begin{array}{r} 15 \\ R 48 \end{array}$$

$$59 \\ 42.94 / 23.5$$

$$11.4 \quad 32.8 / \begin{array}{r} 85 \\ R 49 \end{array}$$

$$134 \\ 42.90 / 33.0$$

$$9.7 \quad 33.0 / \begin{array}{r} 45 \\ R 72 \end{array}$$

$$28$$

$$121 \\ 27 / 19.8$$

$$8.6 \quad 33.0 / \begin{array}{r} 36 \\ R 70 \end{array}$$

$$90 \\ -04$$

$$122 \\ 36 / 22.2$$

$$5.9 \quad 33.0 / \begin{array}{r} 23 \\ R 56 \end{array}$$

$$69 \\ -10$$

$$68 \\ 42.11 / 25.2$$

$$3.7 \quad 32.8 / \begin{array}{r} 23 \\ R 34 \end{array}$$

$$51 \\ -14$$

$$47 \\ 42.10 / 25.0$$

Sta. + π - Grade

924.09

107 +29

+93

B.M. 6.28 927.75 2.67 921.42 921.47

+31

+86

+60

+64

108

+50

T.P. 10.20 939.69 3.31 929.44

109

+50

110

Cor. Road

Lt

Q

Rt.

Spk. in P.P. N.E. Cor. Dole & C

✓ 5.8

5.4

$$\begin{array}{r} 29.0 / 4.4 \\ \hline 12.90 \end{array}$$

$$\begin{array}{r} 6.2 \\ \hline 12.2 / 25.4 \end{array}$$

4.4

$$\begin{array}{r} 28.6 / 3.6 \\ \hline 12.8 \end{array}$$

$$\begin{array}{r} 3.9 \\ \hline 12.5 / 28.0 \end{array}$$

10.5

$$\begin{array}{r} 30.2 / 5.9 \\ \hline 12.6 \end{array}$$

$$\begin{array}{r} 10.8 \\ \hline 11.7 / 24.4 \end{array}$$

2.7

$$\begin{array}{r} 33.0 / 0.2 \\ \hline 12.55 \end{array}$$

$$\begin{array}{r} 10.2 \\ \hline 11.5 / 26.0 \end{array}$$

8.6

$$\begin{array}{r} 33.0 / 4.4 \\ \hline 12.2 \end{array}$$

$$\begin{array}{r} 10.5 \\ \hline 11.1 / 23.2 \end{array}$$

579

+

x

-

Grado

729.64

110

+50

111

+30

112

T.R.

2.87

742.14

2.37

932.27

+50

113

+50

114

+40

+70

115

$$\begin{array}{r} 11.3 \\ 76 \\ \hline 3.7 \end{array}$$

Gr. Red

LH

E

RH

7.6

$$33.0 / \frac{44}{10.52}$$

6.3

$$33.0 / \frac{28}{12.55}$$

$$\frac{6.3}{15.0}$$

.46

$$33.0 / \frac{4.3}{12.79}$$

3.7

$$33.0 / \frac{43.8}{12.95}$$

$$\frac{4.9}{12.08 / 24.6}$$

10.1

$$33.0 / \frac{4.5}{12.76}$$

$$\frac{7.5}{12.24 / 28.2}$$

9.1

$$33.0 / \frac{5.5}{12.56}$$

$$\frac{4.8}{12.43 / 33.0}$$

8.2

$$33.0 / \frac{4.2}{12.60}$$

$$\frac{3.7}{12.65 / 33.0}$$

7.1

$$32.1 / \frac{4.5}{12.40}$$

$$\frac{4.7}{12.49 / 31.8}$$

6.0

$$30.6 / \frac{4.2}{12.5.8}$$

$$\frac{6.6}{12.19 / 25.8}$$

5.5

$$33.0 / \frac{11}{12.6.4}$$

$$\frac{5.7}{12.18 / 20.6}$$

5.2

$$33.0 / \frac{0.8}{12.6.9}$$

$$\frac{4.2}{12.30 / 29.0}$$

Sta. + X - Grade

942.19

115 +50

116

+50

117

+50

T.P. 2.75 932.74 12.15 929.99

118

+50

610

926.64

926.65

119

+50

T.P. 0.27 919.34 12.67 919.07

120

+35

Gr. Rod

L

K

Rt.

$$5.4 \quad 33.0 / \frac{0.1}{R7.3}$$

$$\frac{9.2}{R7.2} / 29.4$$

$$6.4 \quad 33.0 / \frac{0.9}{R7.5}$$

$$\frac{5.5}{R2.9} / 29.8$$

$$8.1 \quad 33.0 / \frac{2.8}{R7.2}$$

$$\frac{6.8}{R5.3} / 29.6$$

$$10.1 \quad 33.0 / \frac{5.3}{R6.8}$$

$$\frac{6.3}{5.8} / 33.0$$

$$\frac{14.4}{12.4} \quad 33.0 / \frac{6.1}{R8.3}$$

$$\frac{6.0}{R8.4} / 33.0$$

$$5.9 \quad 33.0 / \frac{0.9}{R7.0}$$

$$\frac{0.9}{R7.0} / 33.0$$

$$8.8 \quad 33.0 / \frac{3.8}{R7.0}$$

$$\frac{4.5}{R6.2} / 33.0$$

$$11.5 \quad 33.0 / \frac{6.3}{R7.2}$$

$$\frac{7.1}{R6.4} / 33.0$$

$$14.3 \quad 33.0 / \frac{8.3}{R8.0}$$

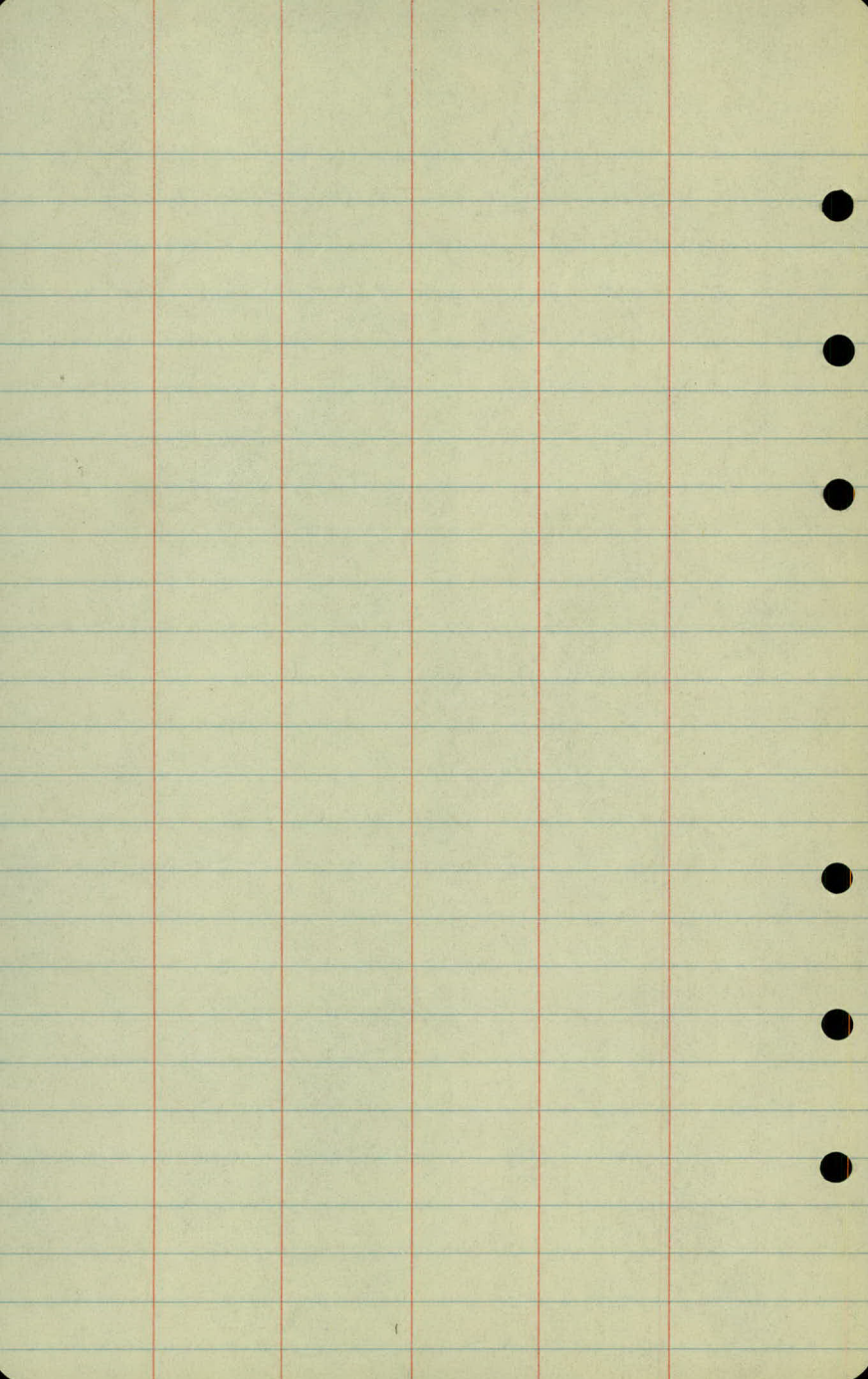
$$\frac{9.3}{R7.0} / 33.0$$

$$3.6 \quad 33.0 / \frac{11.5}{R1.1}$$

$$\frac{12.7}{R8.3} / 33.0$$

$$5.3 \quad 33.0 / \frac{2.2}{R5.1}$$

$$\frac{11.3}{R8.6} / 33.0$$



Spk. in P.P. Rt. 1181.85'

Sta. + A - Grade.

919.29

120 + 70

121

450

T.P.	010	906.54	13.50	905.84
------	-----	--------	-------	--------

122				905.3
-----	--	--	--	-------

195				03.0
-----	--	--	--	------

123				900.2
-----	--	--	--	-------

430				98.9
-----	--	--	--	------

T.P.	1.78	897.74	10.58	895.96
------	------	--------	-------	--------

+15				97.0
-----	--	--	--	------

124				96.0
-----	--	--	--	------

+25				95.1
-----	--	--	--	------

482				934
-----	--	--	--	-----

Gen. Recd.

Lt

£

Lt

$$6.7 \quad 27.4 / \frac{6.5}{42.22}$$

$$\frac{15}{272/320}$$

$$8.5 \quad 248 / \frac{96}{42.9}$$

$$\frac{36}{269/330}$$

$$11.3 \quad 226 / \frac{133}{42.00}$$

$$\frac{88}{225/320}$$

$$1.2 \quad 21.9 / \frac{32}{42.00}$$

$$\frac{11}{10.1}$$

$$\frac{18}{214/258}$$

$$3.5 \quad 19.2 / \frac{56}{42.1}$$

$$\frac{3.7}{-0.2}$$

$$\frac{55}{220/22.1}$$

$$6.3 \quad 20.0 / \frac{83}{42.00}$$

$$\frac{6.7}{-0.4}$$

$$\frac{83}{220/241}$$

$$7.6 \quad 25.2 / \frac{95}{42.01}$$

$$\frac{83}{-0.7}$$

$$\frac{93}{223/236}$$

$$0.70 \quad 22.2 / \frac{43}{42.36}$$

$$\frac{17}{-1.2}$$

$$\frac{50}{223/236}$$

$$1.7 \quad 22.8 / \frac{56}{42.29}$$

$$\frac{31}{-1.4}$$

$$\frac{65}{228/246}$$

$$2.6 \quad 23.8 / \frac{70}{42.4}$$

$$\frac{44}{-1.8}$$

$$\frac{78}{222/254}$$

$$4.3 \quad 26.4 / \frac{100}{42.57}$$

$$\frac{67}{-2.4}$$

$$\frac{117}{229/298}$$

Sta	+	T	-	Grade
		897.74		
125				92.8
T.P.	309	896.57	9.21	888.53
+50				91.5
126				90.6
+50				89.8
127				89.3
+50				89.1
128				89.0
+39				89.1
+60				89.4
T.P.	732	897.07	1.82	889.15
129				89.7
+50				90.5
B.M.			445	892.62
				892.62

Cal. Rod

Lt.

R.

Rt.

4.9	$266 / \begin{smallmatrix} 107 \\ -28 \end{smallmatrix}$	$\begin{smallmatrix} 74 \\ -25 \end{smallmatrix}$	$\begin{smallmatrix} 124 \\ -75 / 300 \end{smallmatrix}$
-----	--	---	--

0.1	$284 / \begin{smallmatrix} 68 \\ -6.7 \end{smallmatrix}$	$\begin{smallmatrix} 30 \\ -29 \end{smallmatrix}$	$\begin{smallmatrix} 97 \\ -96 / 320 \end{smallmatrix}$
-----	--	---	---

1.0	$306 / \begin{smallmatrix} 88 \\ -76 \end{smallmatrix}$	$\begin{smallmatrix} 43 \\ -33 \end{smallmatrix}$	$\begin{smallmatrix} 123 \\ -113 / 330 \end{smallmatrix}$
-----	---	---	---

1.8	$312 / \begin{smallmatrix} 99 \\ -87 \end{smallmatrix}$	$\begin{smallmatrix} 50 \\ -32 \end{smallmatrix}$	$\begin{smallmatrix} 128 \\ -120 / 338 \end{smallmatrix}$
-----	---	---	---

2.3	$308 / \begin{smallmatrix} 100 \\ -7.7 \end{smallmatrix}$	$\begin{smallmatrix} 47 \\ -26 \end{smallmatrix}$	$\begin{smallmatrix} 140 \\ -11.7 / 330 \end{smallmatrix}$
-----	---	---	--

2.5	$296 / \begin{smallmatrix} 98 \\ -7.3 \end{smallmatrix}$	$\begin{smallmatrix} 44 \\ -19 \end{smallmatrix}$	$\begin{smallmatrix} 132 \\ -10.7 / 330 \end{smallmatrix}$
-----	--	---	--

2.6	$256 / \begin{smallmatrix} 79 \\ -53 \end{smallmatrix}$	$\begin{smallmatrix} 40 \\ -14 \end{smallmatrix}$	$\begin{smallmatrix} 113 \\ 9.1 / 33.0 \end{smallmatrix}$
-----	---	---	---

2.5	$218 / \begin{smallmatrix} 57 \\ -32 \end{smallmatrix}$	$\begin{smallmatrix} 35 \\ -10 \end{smallmatrix}$	$\begin{smallmatrix} 104 \\ -29 / 304 \end{smallmatrix}$
-----	---	---	--

2.2	$266 / \begin{smallmatrix} 24 \\ -21.8 \end{smallmatrix}$	$\begin{smallmatrix} 28 \\ -0.6 \end{smallmatrix}$	$\begin{smallmatrix} 79 \\ -5.7 / 26.4 \end{smallmatrix}$
-----	---	--	---

7.4	$320 / \begin{smallmatrix} 28 \\ -26.6 \end{smallmatrix}$	$\begin{smallmatrix} 23 \\ -0.1 \end{smallmatrix}$	$\begin{smallmatrix} 90 \\ -20.9 / 238 \end{smallmatrix}$
-----	---	--	---

6.6	$264 / \begin{smallmatrix} 6.9 \\ -21.7 \end{smallmatrix}$	$\begin{smallmatrix} 6.2 \\ -0.7 \end{smallmatrix}$	$\begin{smallmatrix} 86 \\ -20.0 / 20.4 \end{smallmatrix}$
-----	--	---	--

Sta.

+

X

-

Grade

892.62

B.M.

5.09

897.71

129

+82

91.1

130

91.4

+90

92.1

+65

92.5

131

+02.55

B.M.

892.62

K. A.
L. B. H.
~~18.46~~
L. C.
10-17/28

Cor. Rod.

44

E

Bt

Guy Pole

$$1.6 \quad 29.6 / \begin{array}{r} 78 \\ \hline 5.02 \end{array}$$

$$6.2 / \begin{array}{r} 10.4 \end{array}$$

$$8.2 / \begin{array}{r} 1.6 \\ \hline 18.2 \end{array}$$

$$6.3 \quad 24.8 / \begin{array}{r} 6.4 \\ \hline 12.19 \end{array}$$

$$5.9 / \begin{array}{r} 10.4 \end{array}$$

$$7.1 / \begin{array}{r} 0.8 \\ \hline 16.6 \end{array}$$

$$5.6 \quad 20.4 / \begin{array}{r} 9.3 \\ \hline -2.7 \end{array}$$

$$5.2 / \begin{array}{r} 10.4 \end{array}$$

$$6.1 / \begin{array}{r} 0.5 \\ \hline 16.9 \end{array}$$

$$5.1 \quad 19.6 / \begin{array}{r} 7.4 \\ \hline -2.3 \end{array}$$

$$8.8 / \begin{array}{r} 5.7 \\ \hline 22.9 \end{array}$$

$$4.4$$

$$10.0 / \begin{array}{r} 5.6 \\ \hline 26.2 \end{array}$$

