

Dr. 14
OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey

LABORE ROAD
From Edgerton St. To Centerville Rd.

Road Acct. No. 1

Date Filed 12-28-38

LABORE ROAD

Plan survey account
proposed improvement

9-38

{ H.B.
H.W.
L.G.
A.M.

New Canada & White Bear Township

Angle.

Def.

Sta. Point Lt. Rt.

3+10.1

37° 12' 30"

3

36° 00'

+50

30° 00'

2+00

24° 00'

24° Rt

482.6

P.I.

74° 25'

T. 182.6

L. 310.1

1+50

18° 00'

1+00

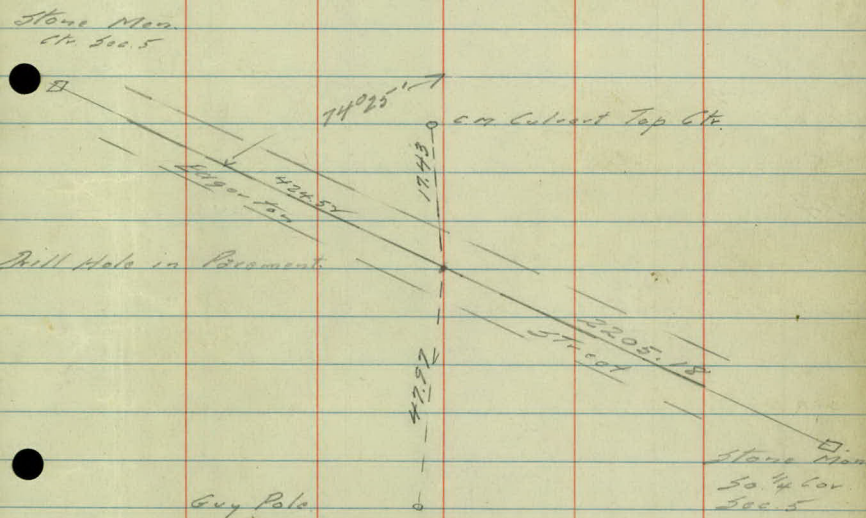
12° 00'

0+50

6° 00'

0+00

Section Tie.



See pg. 1 of 9 of
Original Survey of 1923

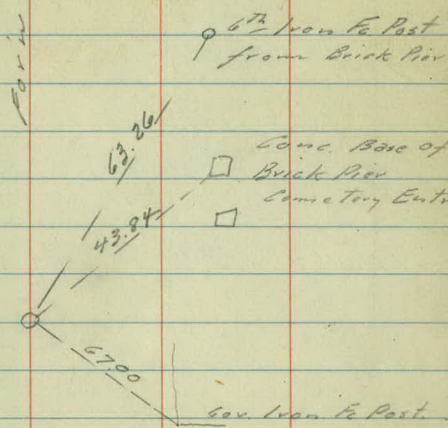
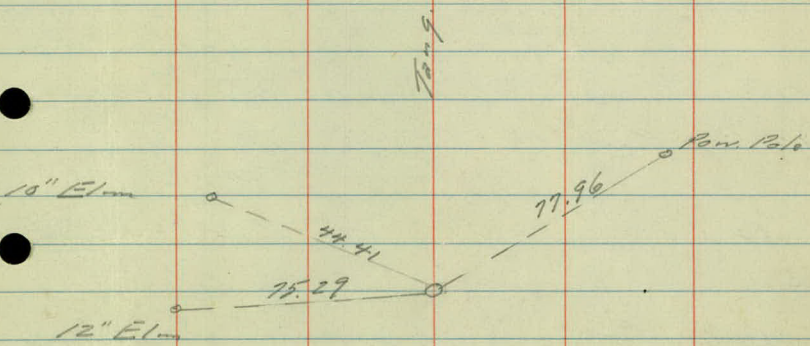
Angle

Defl

Sta. Point Lt. Rt.

14+85.29	P.T.			3°53'30"
+75				3°35'
+50				2°50'
14+20.59	P.I.	7°47'		0-620'
+25				T-65.00
14				2°05'
				L. 129.7
				1°20'
				0°35'
13+55.59	P.C.			0°00'

7+48.6 P.O.T.



Angle

Sta.	Point	Lt.	Rt.	Defl.
25+06.06	P.T.			+538N 1°37'
25				
+50				1°22'
24				1°07'
+50				0°52' $D=1^\circ$
23+41.25	P.I.		3°17'	T=164.22
23				0°37' L=328.33
+50				0°22'
22				0°07'
21+77.73	P.C.			
17+43.16	E.C.			1°59'
17				1°33'
+50				1°03'
16+43.61	P.I.		3°59'	$D=2^\circ$ T=99.64 L=199.17
16				0°33'
+50				0°3'
15+43.29	B.C.			

orig. loc.

Stump

18-29

24" Elm.

36" Cottonwood

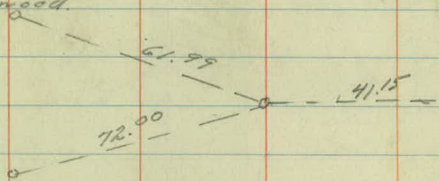


18-29

48" Cottonwood

Cov. of Dwelling

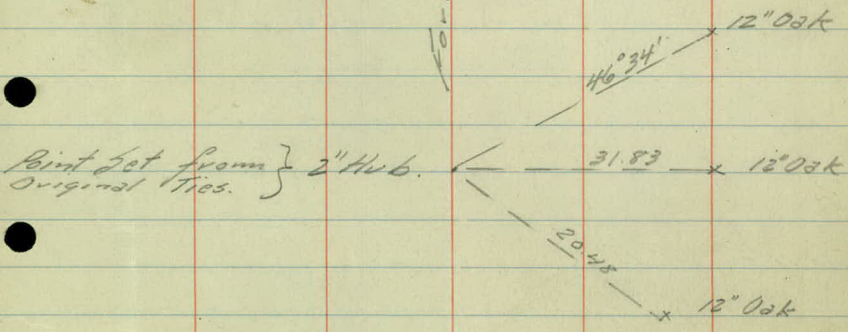
20" Maple



Angle.

Sta.	Point	Lt.	Rt.	Defl.
✓ 39+13.3	P.T.			17°28'
39				16°56'
+50				14°56'
38				12°56' D=8°
+50				10°56' T=225.56
37+02.19	P.I.	34°56'		L=436.70
37				8°56'
+50				6°56'
36				4°56'
+50				2°56'
35				0°56'
✓ 34+76.6	P.C.			
28+92.42	P.O.T.		Arcade St.	

Perin. Tang.



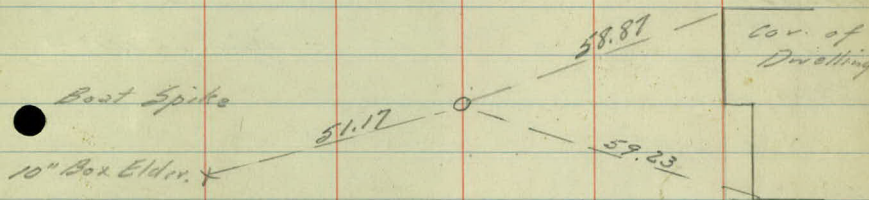
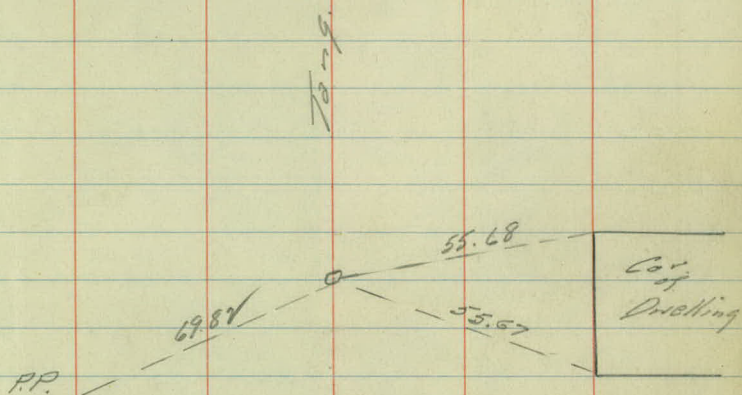
Angle

Sta. Point Lt. Rt.

51+11¹⁰ P.I. 0°26'

45+84.3 P.T.¹ 7°48' D=180
+50 4°43' T=438'
45+41.4 P.I. 15°36' L=86.7
45 0°13'

44+97.6 P.C.¹



Angle.

Sta. Point Lt. Rt. Defl.

62+16.80 P.O.T. Co. Rd. "D"

61+95.32 P.T.

1°03' 1/4

+50

0°56' 1/4

61

0°49'

+50

0°41' 1/4

60

0°34'

59+83.67 P.I. 2°07'

D=0°30'

+50

0°26' 1/4 T=211.78

59

0°19' L=423.35

+50

0°11' 1/2

58

0°04'

57+71.93 P.C.

24" Elm.

Cor. Dwelling

Co. in 1829

99.99

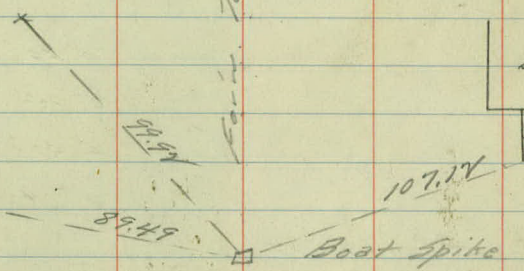
89.49

107.14

Boat Spike

Dwelling

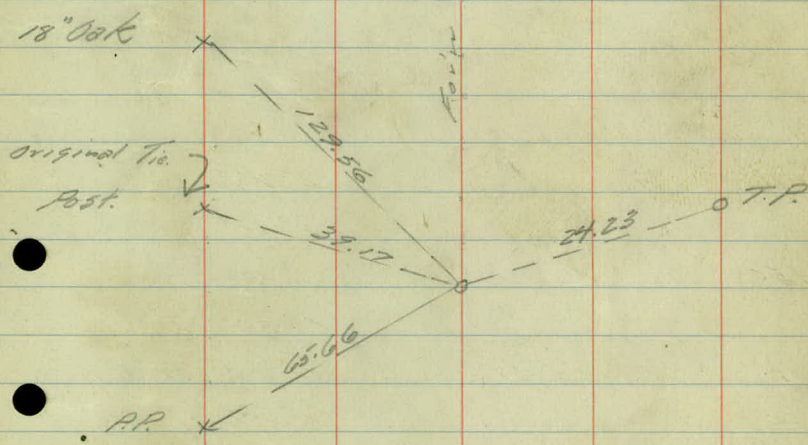
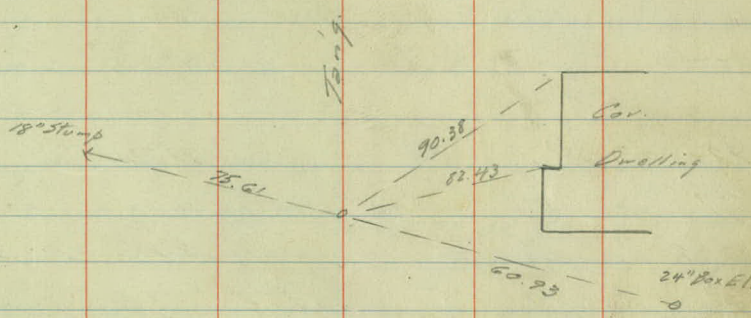
Cor. of Harbor



Angle.

Defl.

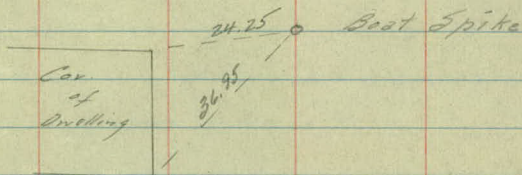
Sta.	Point	Lt.	Rt.	
87+02.00 [↓]				5°08'
87				5°5 $\frac{1}{4}$ '
+50				4°5 $\frac{1}{4}$ '
86				3°5 $\frac{1}{4}$ '
85+74.00		10°16'		D=40° T=128.7 [↓]
+50				2°5 $\frac{1}{4}$ '
85				1°5 $\frac{1}{4}$ '
+50 [↓]				0°5 $\frac{1}{4}$ '
84+45.30	P.C.			
77+67.08 [↓]	P.T.			8°35'
+50				8°04'
77				6°34'
+50				5°04'
76+25.18	P.I.	17°10'		D=6° T=144.2 [↓] L=286.1 [↓]
76				3°34'
+50				2°04'
75				0°34'
74+80.98 [↓]	P.C.			



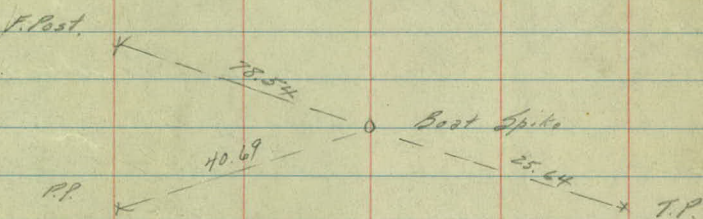
Angle.

Sta.	Point	Lt.	Rt.	Defl.
↓ 97+25 ²³	P.T.			28°21'
97				24°56 ¹ / ₄ '
+50				18°11 ³ / ₄ ' D=27°
96+30. ⁸	P.I.	56°42'		T=115.57 [✓]
96				11°26 ³ / ₄ ' ✓ L=210 ⁰⁰
+50				4°41 ¹ / ₂ ' ✓
↓ 95+15.23	P.C.			
90+49.36	P.T.			2°59 ³ / ₄ '
90				2°30'
+50				2°00'
89				1°30' D=2°
88+99.86	P.I.	5°59'		T=149.7 [✓]
+50				1°00' L=299.44 [✓]
88				0°30'
↓ 87+50.16	P.C.			

Long.

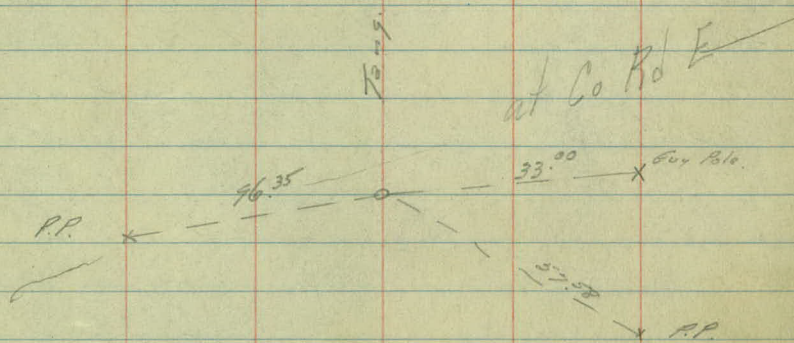


For in.

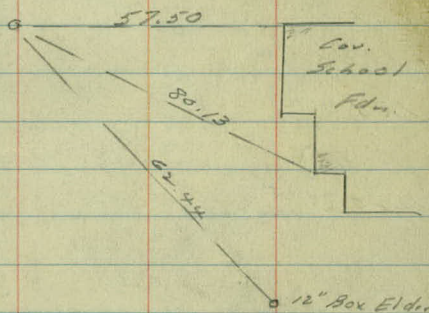


Angle.

Sta.	Point	Lt.	Rt.	Defl.
↓ 122+08.20	P.T.			14°06' ¹ / ₄
122				12°50' ¹ / ₂
+25				9°13' D=29° ¹ / ₂
121+61.60	P.I.	28°13'		T=50.2 ¹ / ₂
+50				5°35' ¹ / ₂ L=97.3 ¹ / ₂
+25				1°58'
↓ 121+11.40	P.C.			
↓ 109+88.72	P.T.			5°27' ¹ / ₄
+50				4°58' ¹ / ₄
109				4°21'
+50				3°43' ¹ / ₄
108				3°06' D=2°30'
107+71.05	P.I.	10°55'		T=219° ¹ / ₂
+50				2°28' ¹ / ₄ L=436.67 ¹ / ₂
107				1°51'
+50				1°13' ¹ / ₄
106				0°36'
↓ 105+52.05	P.C.			

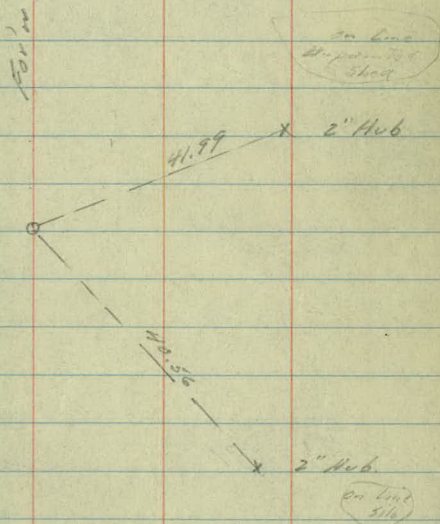
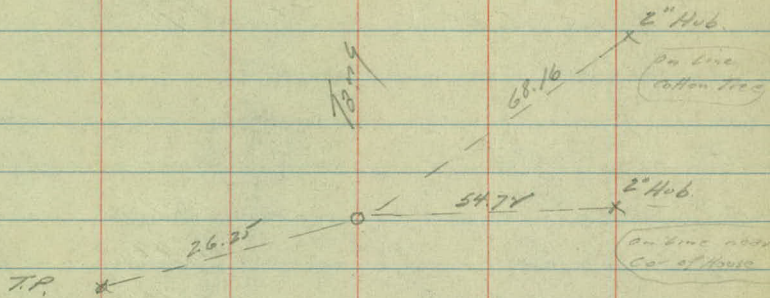


To 1st



Angle.

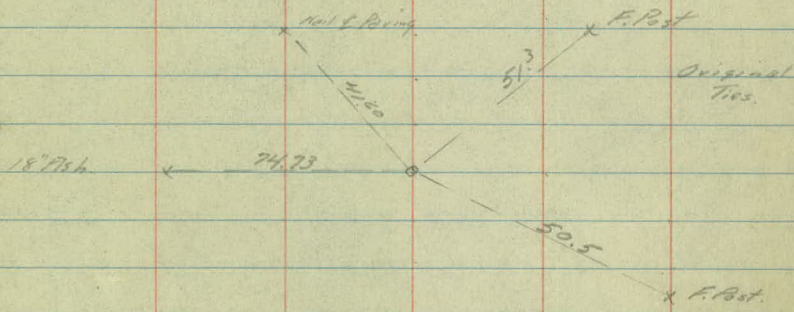
Sta.	Point	Lt.	Rt.	Defl.
138	6045	P.T.		2°25'
+50				2°19'
138				1°49'
+50				1°19' D=2°08'
137	3958	P.L.	4°50'	T=120.9
137				0°49' L=241.7
+50				0°19'
136	1878	P.C.		
131	3835	P.T.		20°16'
131				15°21'
+50				15°51'
130				13°21'
+50				10°51' D=10°
129	4485	P.L.	40°32'	T=211.8
129				8°21' L=405.3
+50				5°51'
128				3°21'
+50				0°51'
127	3305	P.C.		



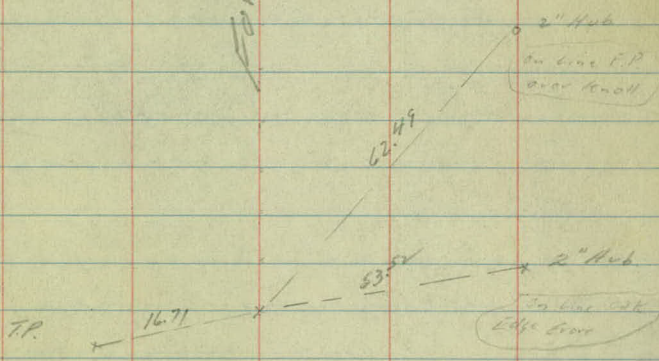
Angle.

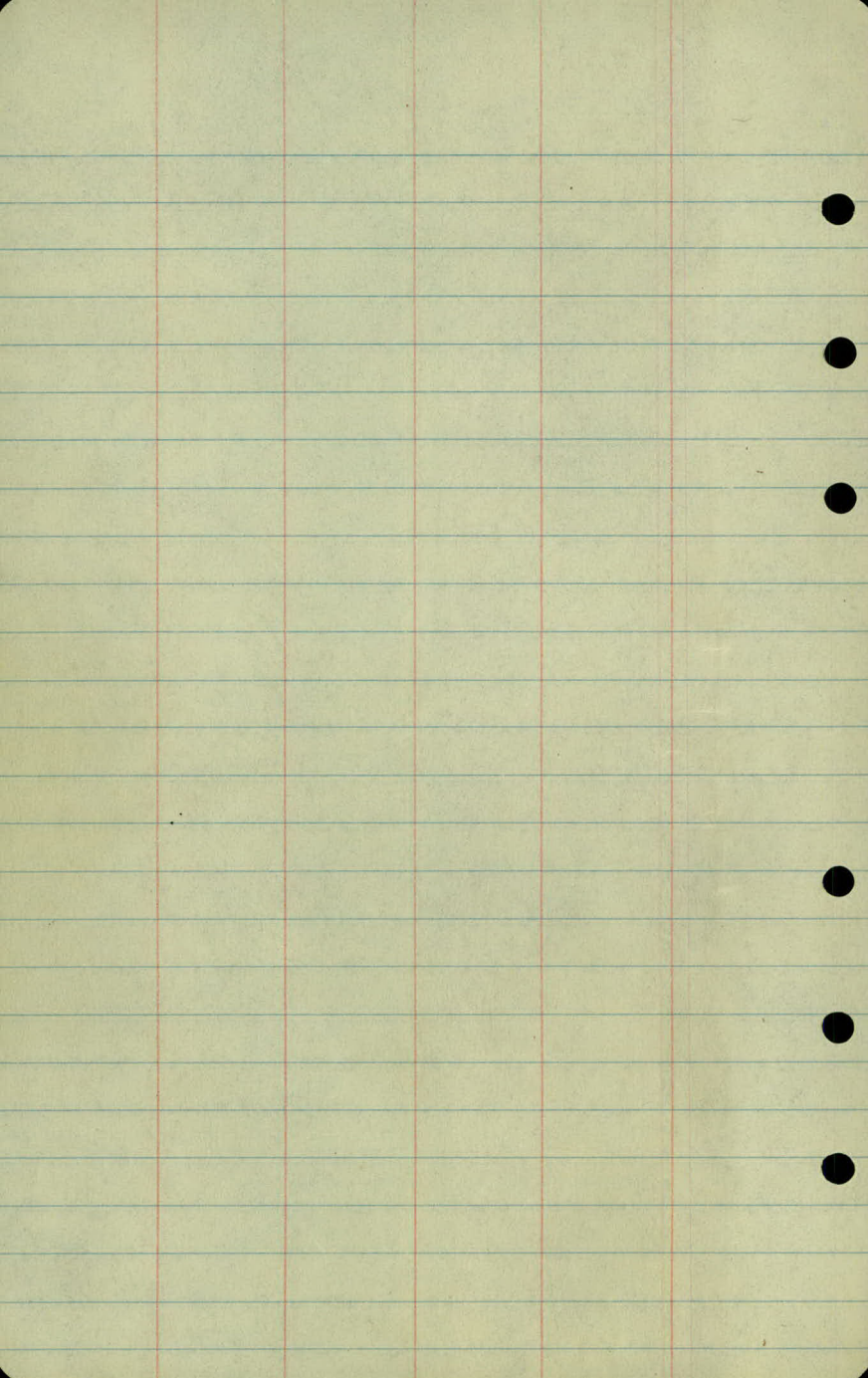
Sta.	Point	Lt.	Rt.	Defl.
159+02 ⁸³	P.T.			8°15'
159				8°11'
+50				6°56'
158				5°41' D=5°00'
+50				4°26' T=166.2
157+39 ⁸³	P.I.		16°30'	L=330.00
157				3°11'
+50				1°56'
156				0°41'
155+72 ⁸³	P.C.			
152+26 ⁸³	P.O.T.	2 RR		
146+93 ⁹⁸	P.I.		0°36'	

Long.



Corner.

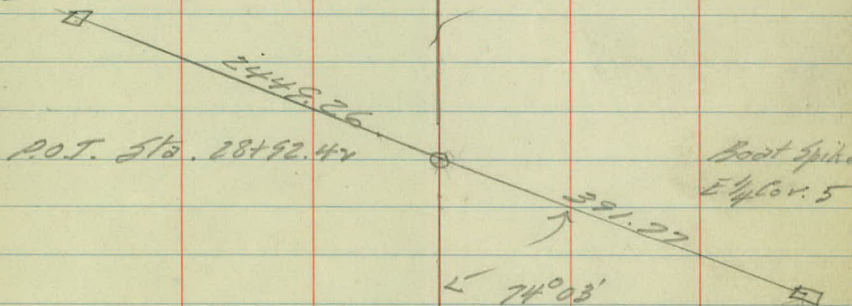




P.I. Sta. 37+02.10

Stone Mon.

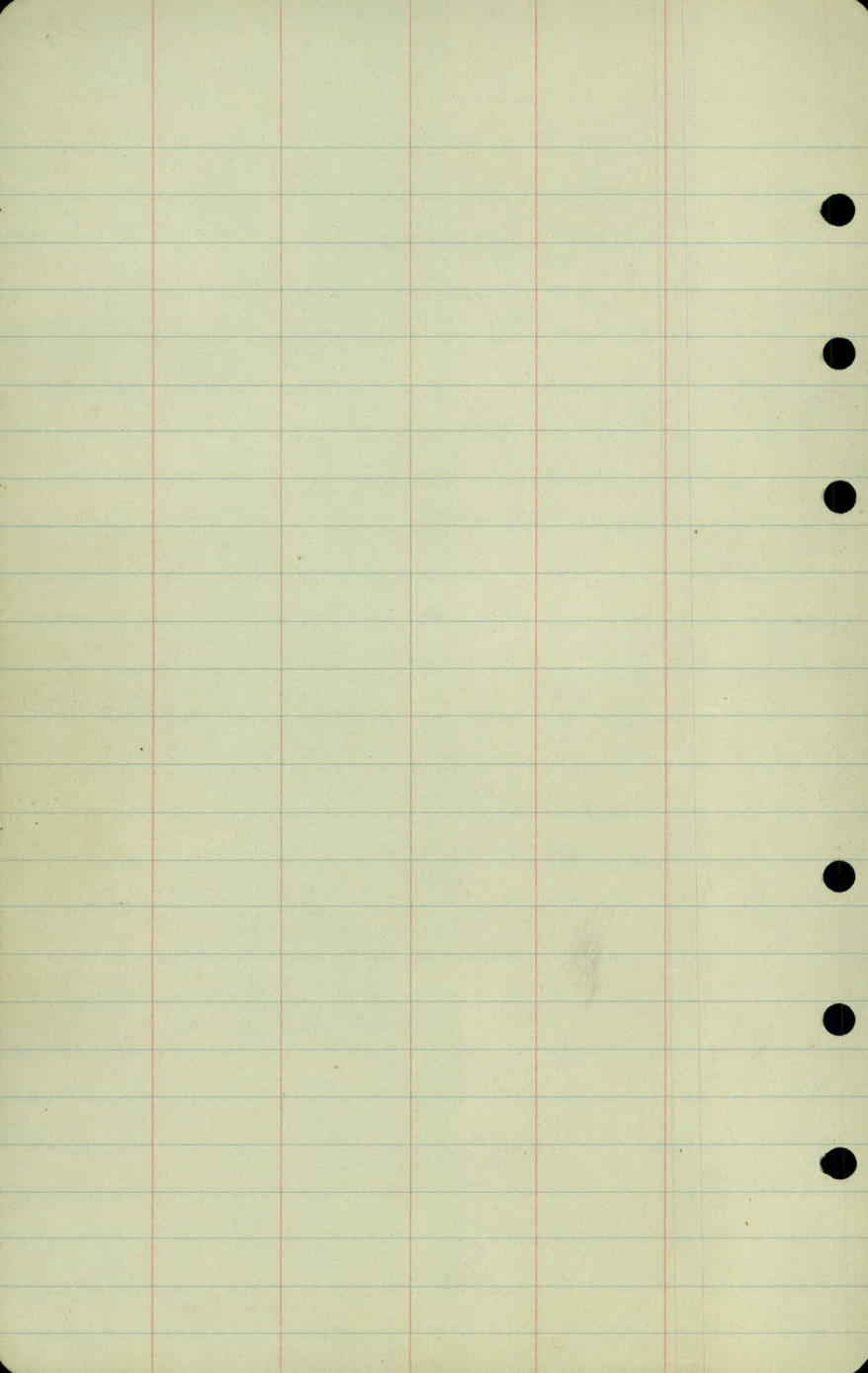
N.E. Cor. Sec. 5



Note:

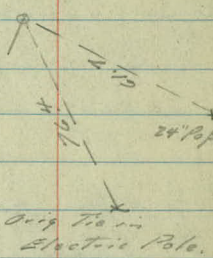
This Boat Spike represents
Mon. which was washed
out and re-established
in 1931

P.I. Sta. 231+41.85



Section Tie.

M.C. Gone.



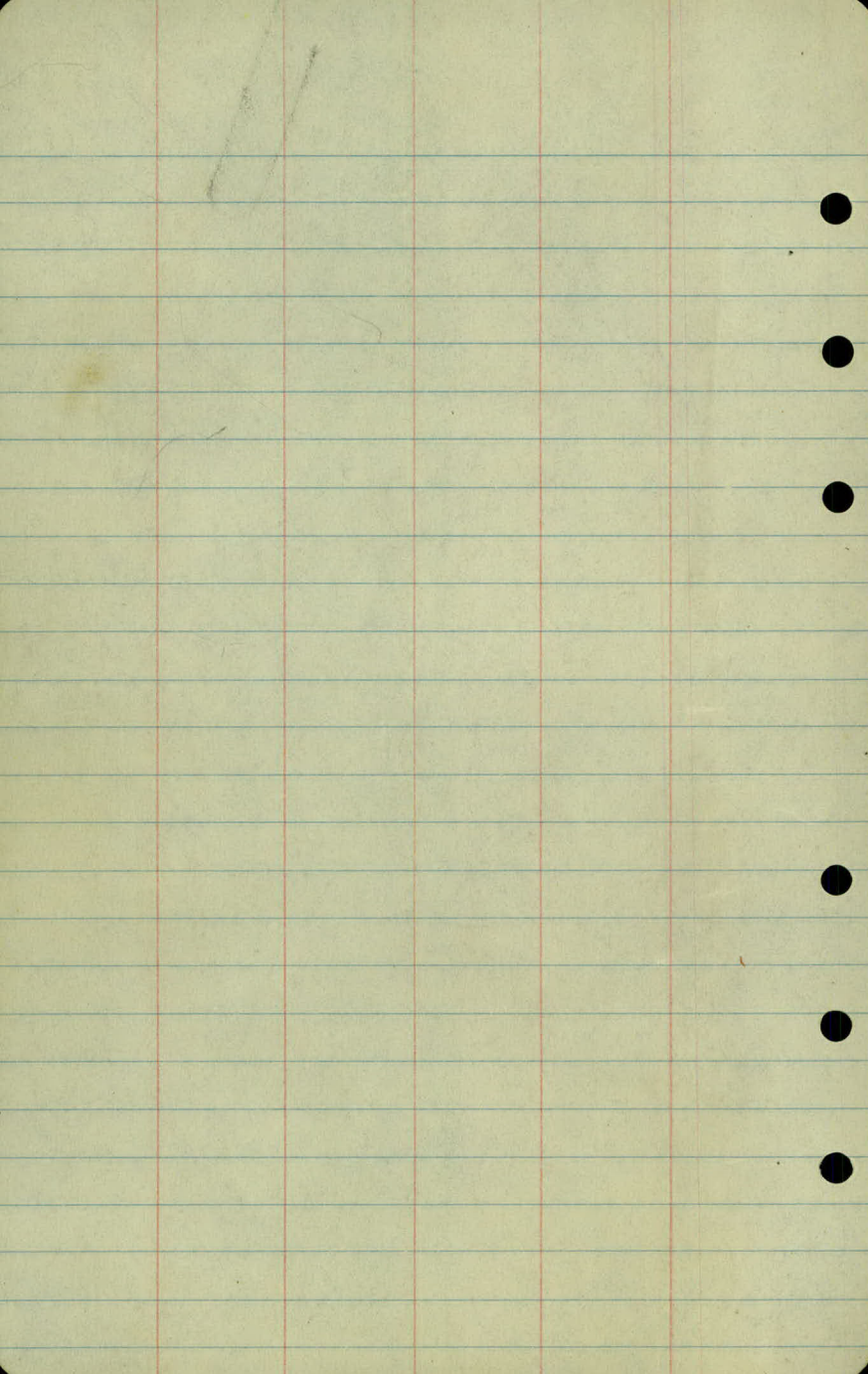
38 x 92.41 P.O.T.

109 x 2

1020 1/4

SK

Refer to Road Map Survey
pg. 2 of 9 of 1923. P.O.T. as estab.
checks angle & distance to missing
M.C. as established from orig. ties



Section Tie.

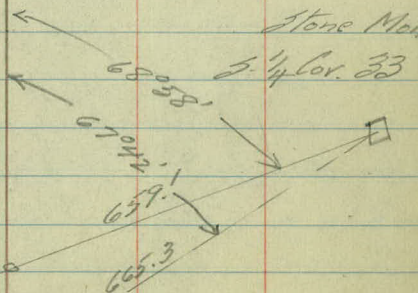
14
80

P.I. Sta. 76+25¹⁸

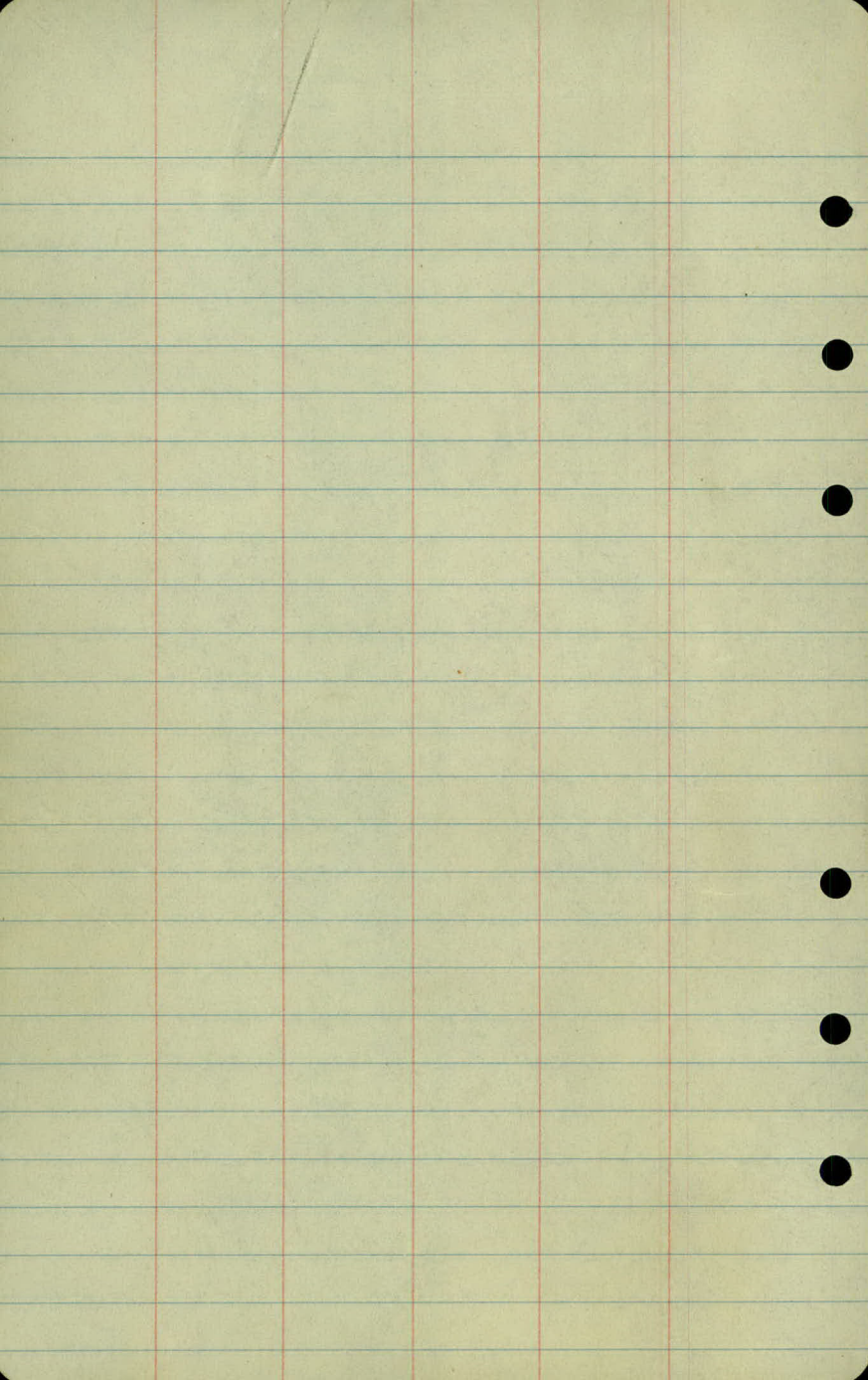
P.O.T. 62+16⁸⁰

Stone Mon.
S.W. Cor. Sec. 33.

P.I. 59+83⁶⁷



✓ 62+00.2 = 62+02.1 on
original Survey of
1923. Pg 4 of 9.



Section Tie.

P.L. Sta. 96+30.8

Stone Man
W. 1/4 Cor. 33.

P.L. Sta. 88+99.86 =

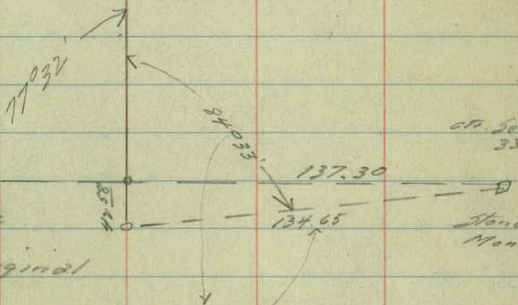
P.L. Sta. 89+02.8 Original

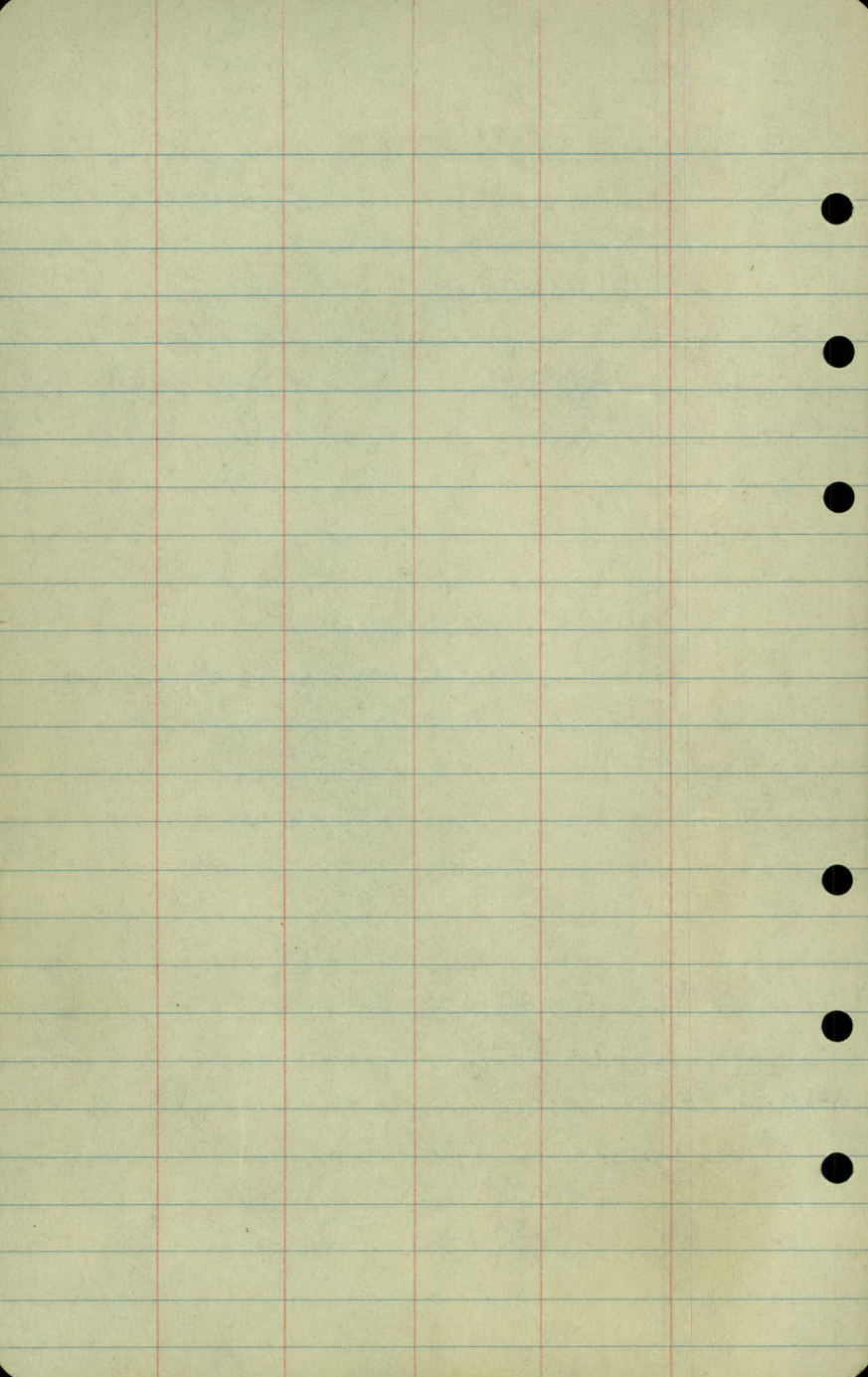
Survey of 1923.

See pg. 6 of 8 Road Map
Survey of 1923 for check
on this Tie.

cr. Sec.
33.

Stone
Man.





Section Tie.

P.L. 121+61.50

*

P.C. Sta. 121+11.40 =

Sta. 121+17.5 Original

Survey 1923.

2" Iron Pin.
In Conc. Paving
N.E. Cor Sec 33

P.C. 121+11.40

1277.35'

1270.1'

570.11'

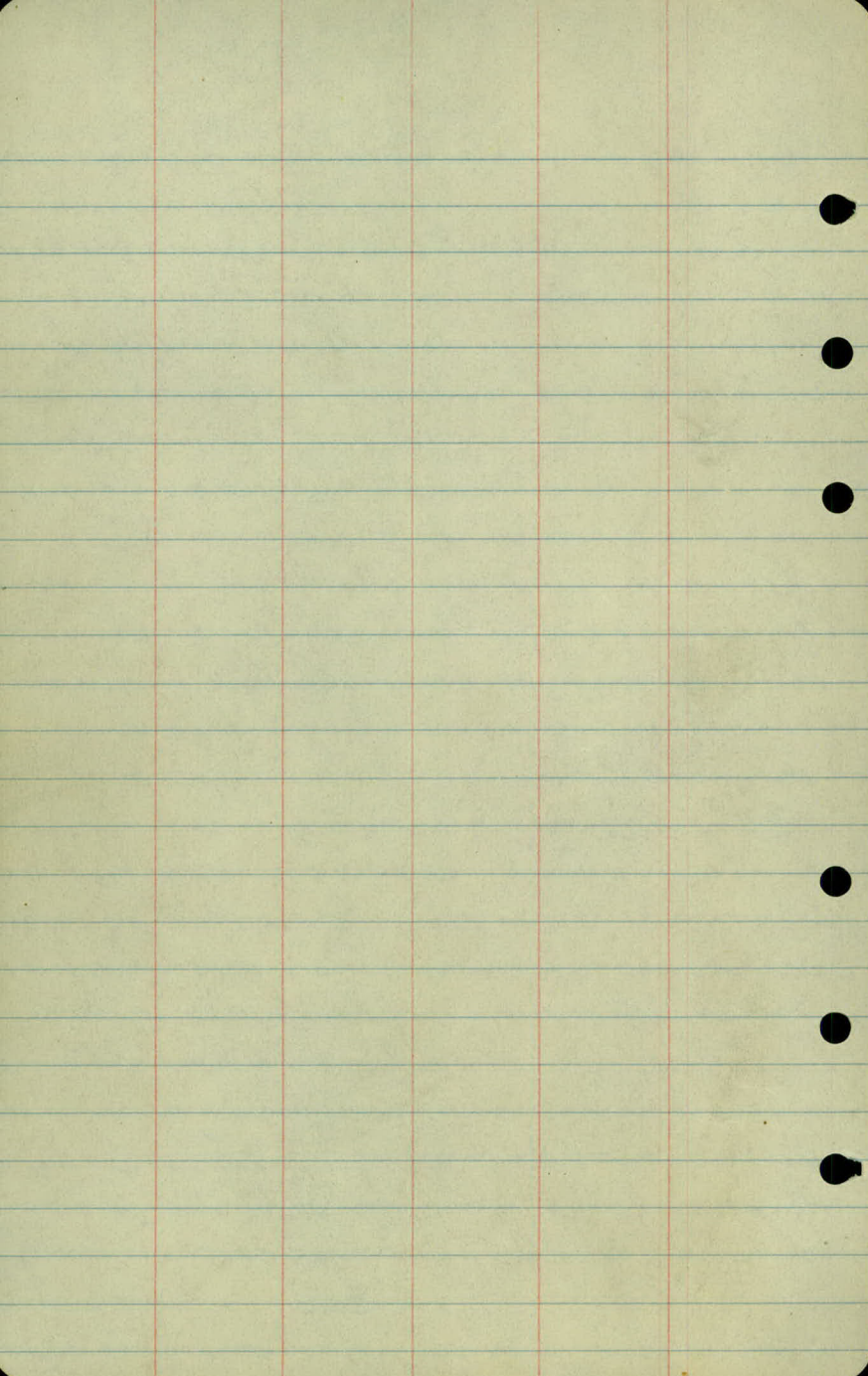
56°38'

Stone Mont.
N. 1/4 Cor B
Sec 33

Refer to Road Map
Survey pg. 7 of 9 to
check

P.L. 107+71.05

*



Section Tie.

157+39.03 P.I.

P.O.T. Sta. 152+26.55 =
P.O.T. Sta. 152+32.30 on
Original Survey of 1923

Stone Mon.
Etc. Sec. 28

152+26.55 P.O.T.

178.8

N.P.R.R.

76°30'

202.71

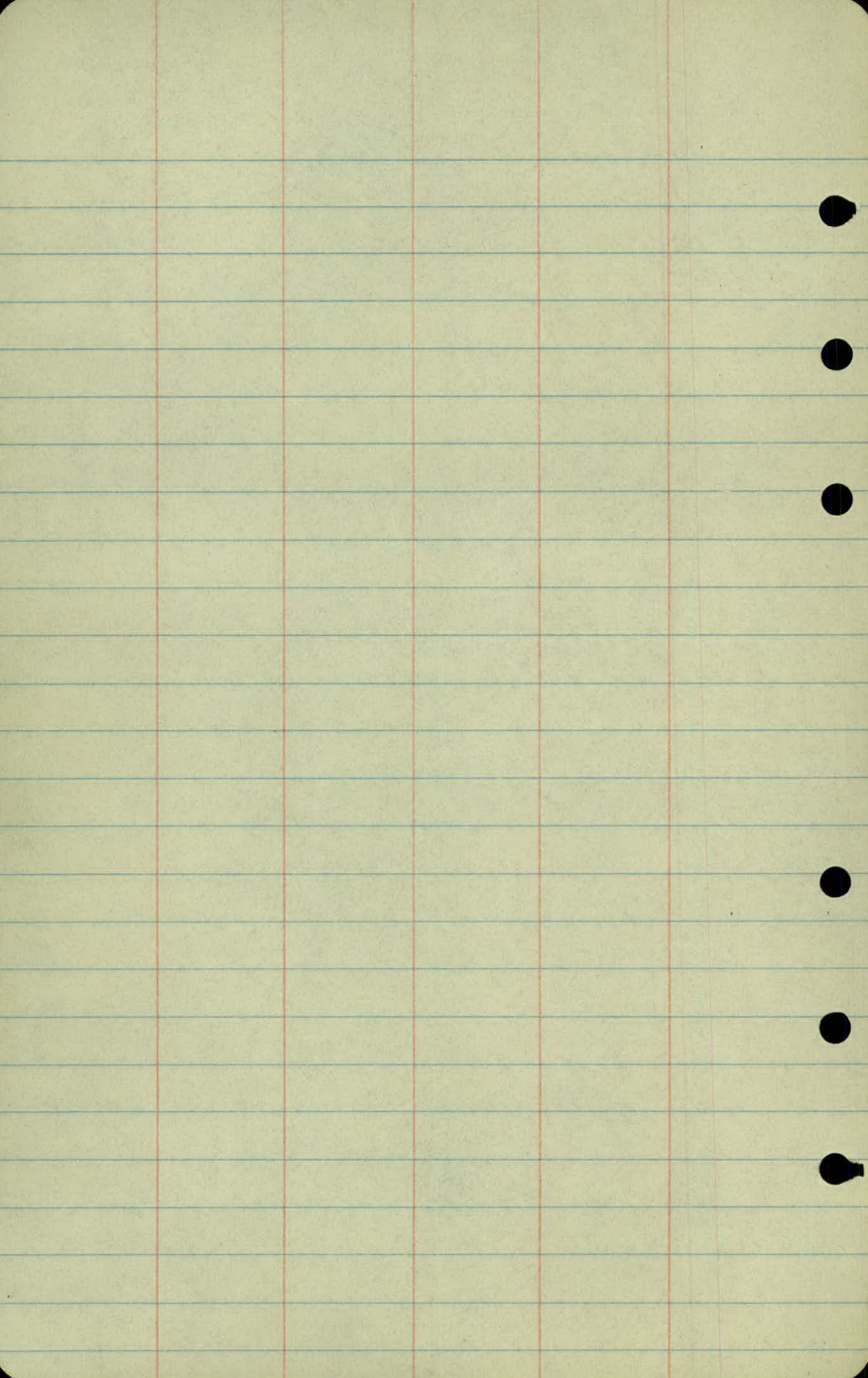
P.O.T. 150+93.6

Stone Mon.
East 1/4 Cor.
Sec. 28

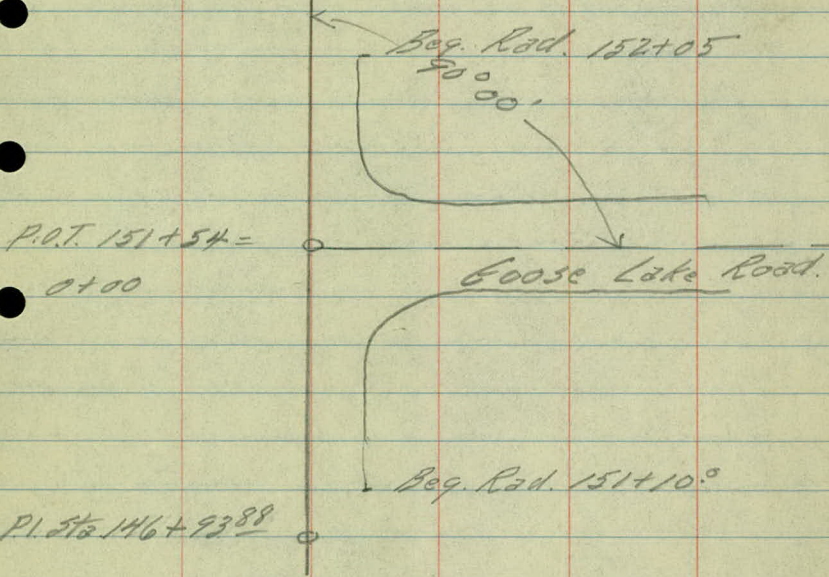
79°42'

60°07'

137+39.68 P.I.

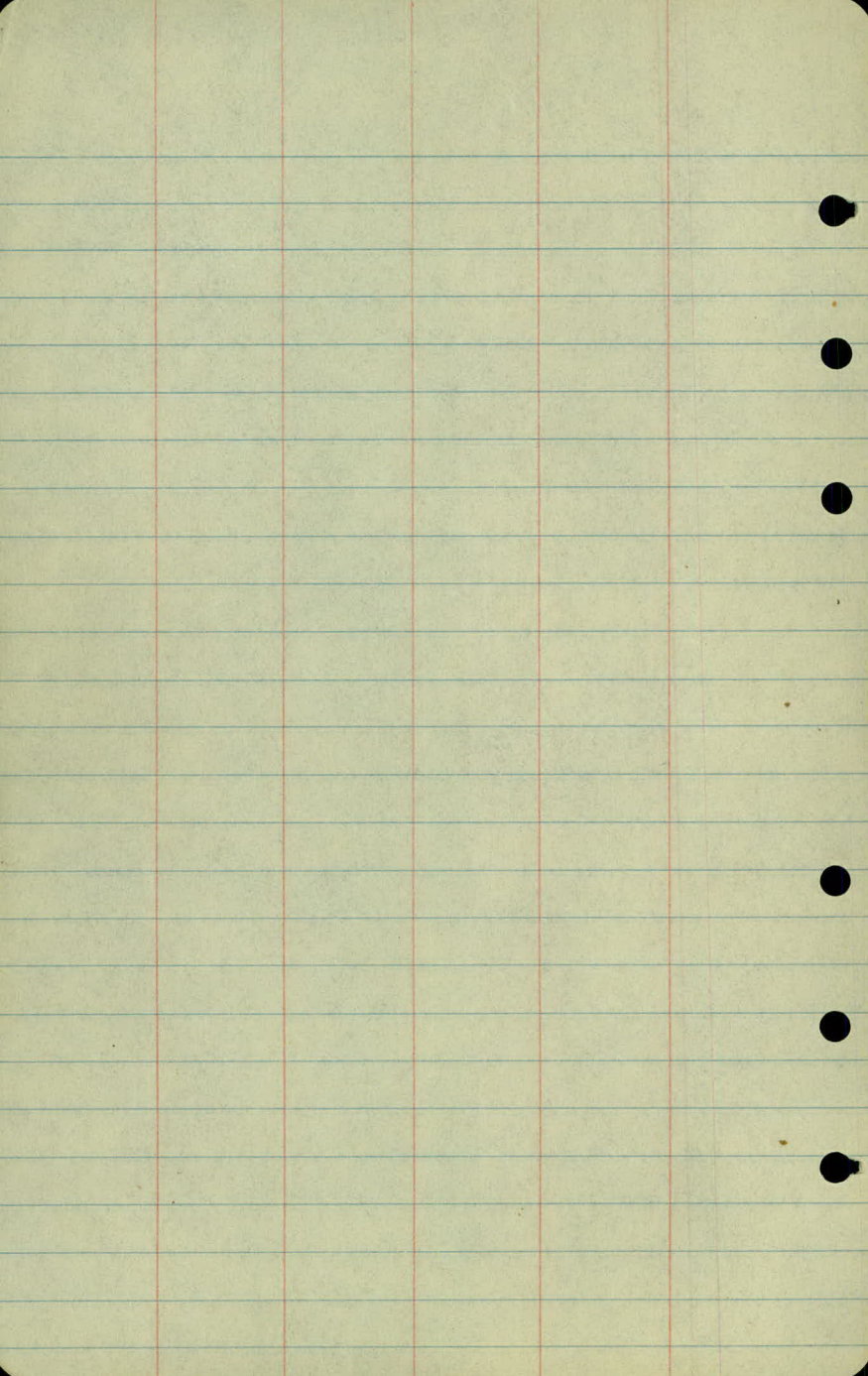


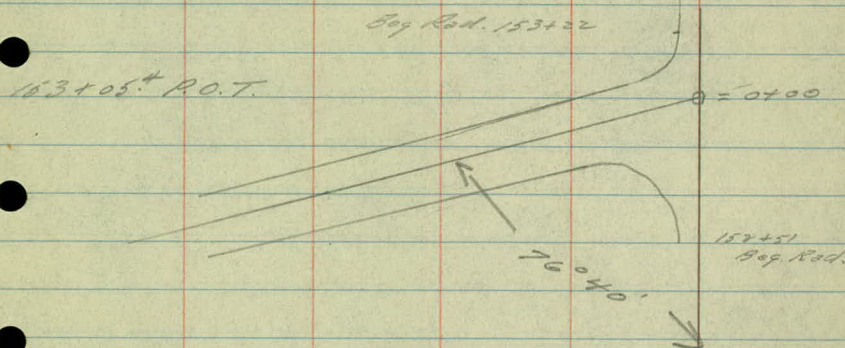
P.I. Sta. 157+39 $\frac{03}{6}$



Traveled Road.

Sta.	Lt.	Rt.
0+20	33	24
0+35	19	15
0+50	14	11
1	10	10
2	10	10
3	11	9

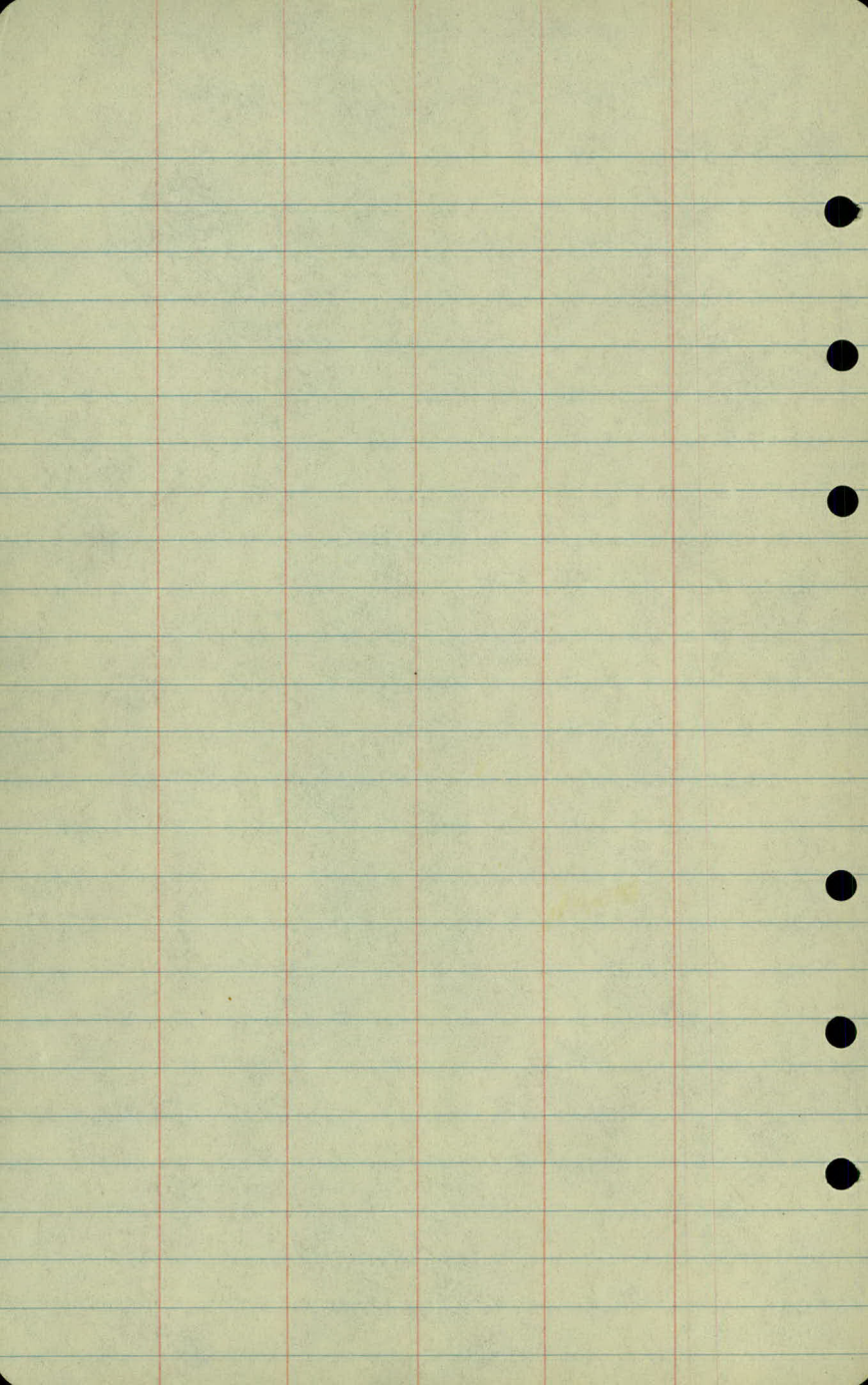




Labore Centerville Conn.

Sta.	Traveled Road.	Rt.
0+31	38	1
0+50	17	3
0+75	10	5
1	7	6
2	6	8
3	8	7

137+39.68 P.I.



159+02.83 P.T. = 0+00 B.C.

Reflections

$$0+50 = 3^{\circ}05'$$

$$1 = 4^{\circ}30'$$

$$+50 = 6^{\circ}05'$$

$$1+86 = P.T. = 7^{\circ}12'$$

$$2 = 7^{\circ}35'$$

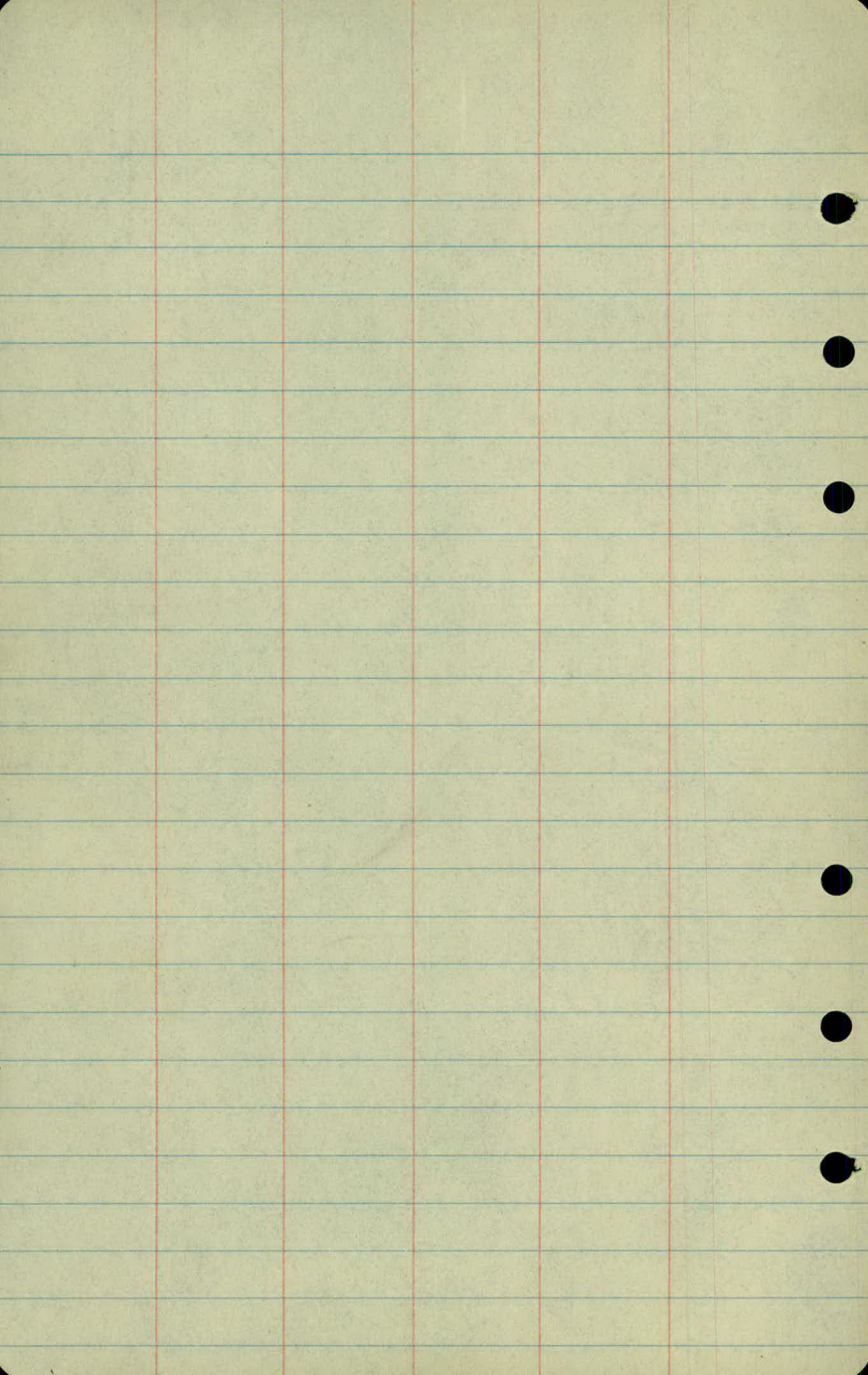
$$3 = 9^{\circ}10'$$

$$4 = 9^{\circ}58'$$

Center ville
20' Conc.
Road
Paving

NE
#3

P.I. Sta. 157+39.03



Labore Road.

From Edgerton St. to
Centerville Road.

1/38

4
Black top.
10 10

6 9 10

5 10 10

4 9 10

3 7 13

150 5 16

2 3 19

150 19

1 15

0

North →

Edger Ten Street 20' Concrete Pavement

2100 T.P. 28.0

Chert 16' RT

Labore Road.

Blacktop.

+64 T.P. 27.0

+64 Rd. Sp. 23.0

24" C.I. 6x6 Drain with 3'x3' Stone Cover.

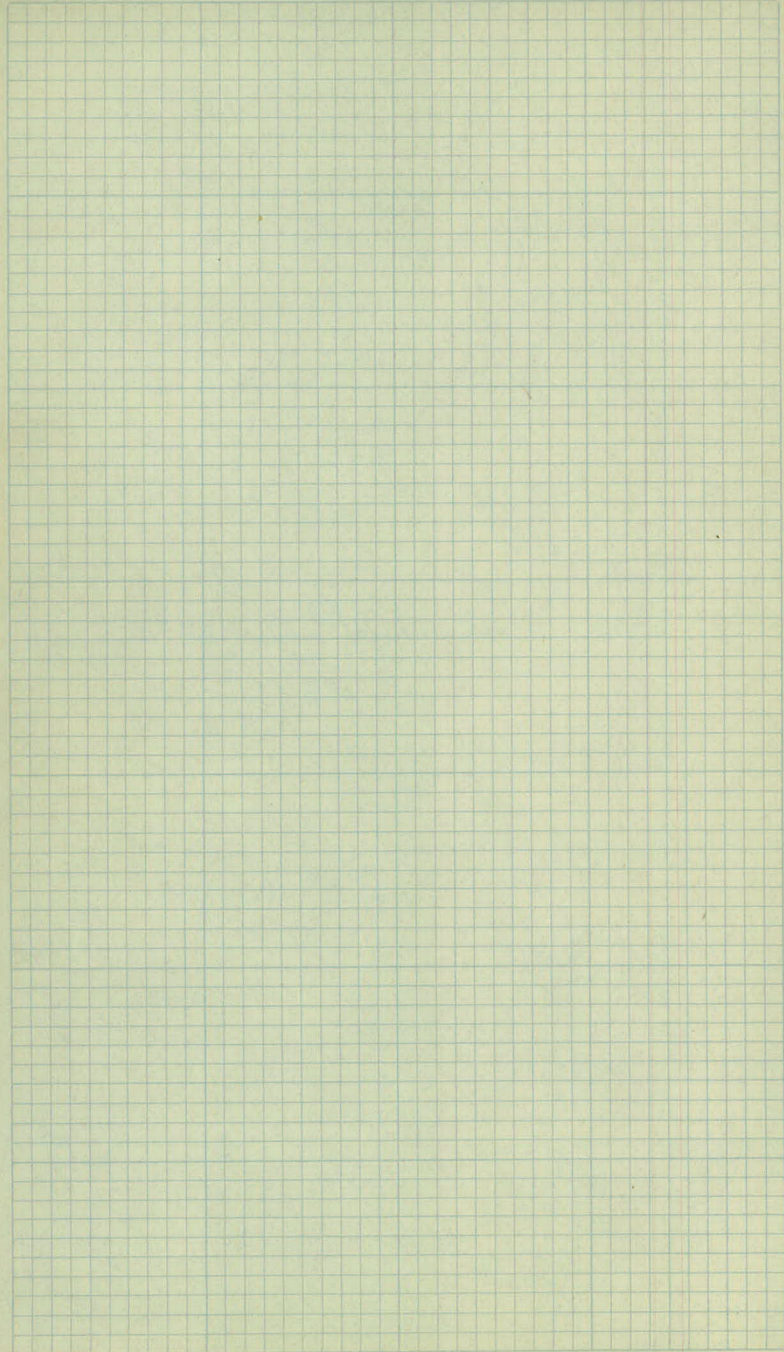
10' Oil Entry +41

131 T.P. 17

Chert 25' RT

0+22 = 15" x 162' C.M.

P.C. Labore Road = 0+00



+94 = 8" T. 33

+68 = 12" T. 33

+15 = 12" T. 33
+13 Rd. Syn. 20

+35 = 14" T. 34
+35 End. Fe. 30

Fe. 31

Fe. 33

+88 Reg. Fe. 36

+85 Reg. Rd. 24

+83 Rd. Syn. 10

+73 Fe. 27.0

+50 T.P. 30

+27 T.P. 31

+05 T.P. 34

+11 T.P. 34

+37 T.P. 25

+78 Rd. Syn. 27

+06 T.P. 35

14

Back 10p.
8 11a

13

5 12

12

5 4

11

7 13

10

7 12

9

8 12

8

9 11

7

187=10' Grd. Entr.

+80=18" Tr. 41
+53=24" Tr. 41
+49=PP 15

+26=24" Tr. 41

+58=18" Tr. 40

+75=18" Tr. 40

+25 P.P. 11
+22=18" Tr. 37
+21=Fc. Cor. 35
+12=8' Dist. Entr.

+57=24" Tr. 37

+61=12" Tr. 37

+45=12" Tr. 36

+30=12" Tr. 36

+96=12" Tr. 35
+95=P.P. 14
+25 Fc. 33.0

+47=36 Tr. 35

+96=12" Tr. 33
+77=8' Dist. Entr.
+90=12" Tr. 35
+57=8' Dist. Entr.

+38 P.P. 16

+17=36" Tr. 34

+53=24" Tr. 35

+67=24" Tr. 36

+44=10" Tr. 33

+99=12" Tr. 33

+77=8" Tr. 33

+46=12" Tr. 33
+20=12" Tr. 33

129 P.P. 24

+41=12" Tr. 26

+01=T.P. 27
+14=8' Dist. Entr.
+05=24" Gate Drain 22.5
To Gate 3'x3' Stone Corner.

+68 P.P. 28

+76=8' Dist. Entr.
+54=30" Tr.
+44 Fc. 46

+26 T.P. 29

Ornamental Iron
Fencing

8100=T.P. 29

+54=6" Pine 30
Brick 2'x2'
To Gate
+35=12' Grd. Entr.
+22=12"x31" C.M. 15.5
Brick 2'x2'
+24=12" Pine 30
+02 Fc. 44.0

21

Black top.
9 16

20

10 9

19

9 8

18

9 11

17

7 13

16

6 12

15

8 10

14

+58=12" Tr. 33
 +45=12" Tr. 33
 +36=10" Tr. 35
 +29=10" Tr. 34
 +23= R.P. 15
 +13=10" Tr. 33

+90=24" Tr. 31

+73=24" Stmp. 31

+63=12" Tr. 31

+36=12" Stmp. 31
 +23=24" Stmp. 30

+81=14" Tr. 31

+83 R.P. 15

+63=8' Dint. Entr.

+52 Fe. Cor. 33

+50=54" Tr. 24

+28 Fe. Cor. 33

+20=24" Tr.

+01 Fe. Cor. 34.5

Conc. Blk.
 +25 60' age 37.0

+61=24" Tr. 25

+50=8' Dint. Entr.

+40 R.P. 15

+83 Fe. Cor. 37 8' Dint. Entr.

+66=12" X 38" C.M. 17

+62=18" Tr. 22

+25=18" Tr. 21

+08=15" Tr. 21

8' Dint. Entr.

+13=12" X 20" C.M. 19.0

+08 R.P. 17

+22=12" X 38" Comb. 4 T.P. 4 C.M.

+68=24" Tr. 21

+53=24" Tr. 33

+47=24" Tr. 33

+35=18" Tr. 33

8' Dint. Entr.

+96=15" X 20" C.M. 15.0

+80=48" Tr. 22

+71= R.P. 18

+58=10" Tr. 28

+58=48" Tr. 20

+41=48" Tr. 20

+12=12" Tr. 43

+05=14" Tr. 41

Fe. 30.0

+80= T.P. 17

+48=24" Tr. 32

+20 R.P. 17

+15=18" M2 p/c 33

+08= R.P. 17

+06=8' Oak 33

Fe. 33.0

+58=12" Stmp. 33

+90=30" Stmp. 33

+79=24" Tr. 33

+62=8' Dint. Entr.

+66=14" Tr. 33

+53= T.P. 16

+50=18" Tr. 32

+11=10" Tr. 32

+02=12" Tr. 32

Fe. 28.0

+56=12" Tr. 33

10' Dint. Entr.

+75=16' Gate 30.0

+66=14" Tr. 36

+45=12" Tr. 21

+30=18" Tr. 31

+30 T.P. 15

+18 Fe. Cor. 29

+32 R.P. 28.5

12" Conc. Retaining Wall

Steps Down

Dr. 45' Lt.

Conc. Block Drilling

+57 Out 37'

+59= T.P. 19

+09=24" Tr.

+44 R.P. 18

+45=8' Dint. Entr.

+18 R.P. 60" Tr. 33

28

Blacktop.
11 9

27

9 10

26

9 9

25

9 9

24

8 10

23

8 11

22

8 12

21

Fig. 30

+84 = 24" Tr. 30

+57 = 24" Stmp. 30

+50 = 24" Stmp. 30

+30 = 24" Stmp. 29

P.C. 29

+62 = 30" Tr. 28

+53 = P.P. 18

+39 = 24" Tr. 29

+22 = 14" Tr. 29

P.C. 28

Fig. 31

+73 = 24" Tr. 32

+47 G. y. P.P. 21

+41 = 24" Stmp. 33

+11 = 24" Stmp. 33

+82 = 30" Tr. 33

+75 = 8' Dist. Ent.

+72 P.C. 35

+29 = 24" Tr. 33

+22 = 12" Tr. 33

+14 P.P. 17

+00 = 8' Dist. Ent.

+85 End. P.C. 32

+85 = 30" Stmp. 32

+65 = 30" Tr. 32

+28 = 36" Tr. 31

+10 = 14" Tr. 31

P.C. 31

+71 P.P. 15

+33 = 12" Tr. 33

+22 = 6" Tr. 33 8' Dist. Ent.

+13 B.P. P.C. 32

+002 = 12" x 20" C.M. 15

Scattered Trees

+90 = 20" Stmp. 33

+77 = 24" Tr. 33

+08 = T.P. 14

+87 = 30" Tr. 32

+71 = 24" Stmp. 32

+50 = 24" Tr. 28

+25 = 12" x 20" C.M. 24

+83 = 12" Tr. 28

+74 P.P. 15

+10' Girdered Ent.

+50 = 8" x 16" V.T.P. 22

+50 = 30" Tr. 28

+39 = 4" Tr. 29

+38 = 24" Stmp. 17

+16 = 18" Tr. 29

+88 = 14" Tr. 29

+80 = 4" Tr. 29

+70 = 14" Tr. 29

+45 P.P. 14

+38 = 8" Tr. 28

+28 = 30" Tr. 27

+06 = 24" Tr. 29

+89 = 6" Tr. 32

+81 = 12" Tr. 30

+79 P.C. 28

+21 = 30" Tr. 32

+14 = T.P. 18

+06 = 10" Tr. 28

P.C. 30.0

+50 = 12" Tr. 32

+74 = 12" Tr. 32

+66 = 12" Tr. 33

+45 = 30" Tr. 36

+36 = 6" Tr. 32

P.C. 31.0

+15 = 12' G. var. Ent.

P.C. 31.0

+89 = P.P. 15

+83 = 12" Tr. 34

+52 = 12" Tr. 33

+35 = 12" Tr. 33

+20 = 24" Tr. 33

P.C. 31.0

+11 = 8' Dist. Ent.

P.C. 30.0

35

Black top.
12 9

34

11 10

33

11 11

32

11 10

31

12 8

30

12 8

+29

12

29

10 31

+41

10

28

Fe. 29

Fe. 25

6/25

+86 = 18" Tr. 26
 +76 = 24" Tr. 26
 +67 = T.P. 16
 +62 = 12" Tr. 27
 +49 = 18" Tr. 27
 +37 = 30" Tr. 27

+16 = 12" Tr. 32
 Fe. 29

Fe. 24

+83 = 24" Stump. 30

+66 = 24" Tr. 28

+55 = 24" Tr. 32
 +42 P.P. 16
 +27 = 30" Stump. 30
 +15 = 18" Stump. 31
 +02 = 18" Stump. 31
 Fe. 26

+31 = 14" Tr. 29
 +24 = 12" Tr. 29
 Fe. 26

+87 = 36" Tr. 29
 +70 = 12" Tr. 32

+17 Rd. Sp. 26
 Fe. 27

+38 = 24" Tr. 31
 +23 Tr. 16
 Fe. 25

+58 = 12" Tr. 23
 +41 = 18" Tr. 27
 +41 Bag. Fe. 27

+75 = 36" Stump. 30

+56 = 24" Tr. 25

+06 = 24" Tr. 25
 Fe. 26

+91 = T.P. 14
 +89 = 24" Tr. 25

Cut in road

Tree

Intake Ditch to Pipe +37 Out 24'
 +45 End Culvert 12" C.M.
 +34 = 8' D. & 1' Hole Ent. 32" Pipe
 +24 M.H. 20'
 Head Wall
 12" x 18" x 6' Hi. Conc.

12" Wire Gate
 +34 = 12" x 18" C.M. 15'

Fe. 26

+59 = 14" Tr. 28

+86 = 18" Stump. 25

+18 = 12" Tr. 37
 +10 = 30" Tr. 41
 +07 Rd. Sp. 28

+56 T.P. 15
 +54 Fe. 37
 +41 Fe. 35
 +22 Fe. 52

+99 M.H. 20'
 No Dirt Road

20' Black Top
 2' At Top = 6' and Line = Arcade St.

+75 End Fe. 32
 +74 = 12" x 35" v. T.P. 21

Drains to M.H.
 40' Rod.

+55 = 14" Tr. 29
 +41 = 14" Tr. 38

Scattered
 Trees.

+34 = 12" Tr. 36
 +19 = 24" Stump. 30

+37 T.P. 15

Cut in

44

Back Top.
10 10

41

10 10

40

10 10

39

11 8

38

12 9

37

11 10

36

11 11

35

Fe. 26

+80 = 14" Twin Tr. 26

+48 = 24" Tr. 26

809 Fe. 22

+28 = 12" Tr. 24

+57 = 24" Tr. 23

+65 = 12" Tr. 18

+50 End Fe. 21

+96 = 24" Tr. 18

+86 T.P. 23

+56 T.P. 22

+08 = 8" Field Ent.

+33 = T.P. 21

+20 T.P. 26

+57 = 8" Tr. 40
+48 = 10" Twin Tr. 37
+35 = 14" Tr. 38
+24 = 30" Stamp 36

+51 = T.P. 19
+82 = 18" Stamp 31

+39 = 12" Tr. 30
+34 = 14" Tr. 30
+20 = 12" Tr. 30
+17 = 8" Tr. 33

+99 = 12" Tr. 32
+50 = 12" Stamp 27
+80 T.P. 18
+68 Fe. 18, 28

+10 = 36" Stamp 26

Back 9 Top 11

49

48

9 11

47

8 11

46

12 9

45

12 9

44

10 10

43

10 10

42

Fe. 21

+90 R.P. 26

+48 Bog. Fe. 20

+94 = 30" Tr. 28

+28 = 8" Tr. 25

+78 = Stone (Bollands) Fe. 14

+58 = 20" Pump. 31" base 2" x 18"
+38 = 14" 25" 15" 20" 4" 18" pole 21"
+38 = 12" x 12" 18" 20"

+35 = 24" Tr. 28

+15 End 4. Fe. 21.9
Fe. 22

+81 = 24" Tr. 27

+64 = 15" Tr. 25

+50 = 24" Tr. 24

+39 = R.P. 19

+30 = 6" Tr. 26

+23 = Bog. Fe. 25

+18 = 15" Tr. 22

+10 = 18" Dist. Ent.

+99 = 6" Tr. 28

+54 = 18" Tr. 26

+61 = 24" Tr. 27

+28 = 24" Tr. 28

+06 = 15" Tr. 27

+06 End Fe. 27

+65 = 24" Tr. 27

+28 = 12" Tr. 27

+19 = 18" Tr. 26

+76 T.P. 24

+49 = 8" Dist. Ent.

+37 = T.P. 25

+22 T.P. 24

10' 8" 8" 10' 10" Ent.

+72 = 12" x 16" C.M. 11.0

+50 = 12" Pine 42

23 F. Drilling

+34

+22 T.P. 21

+39 = Refl. Sp. 22

+38 = T.P. 22

+13 = T.P. 22

56

Black top.
11 10

55

10 10

54

10 10

53

10 10

52

9 10

51

9 11

50

9 11

49

+99 = 14" Tr. 26

+75 = 14" Tr. 27

+59 R.P. 28

+53 = 12" Tr. 29

+34 = 10" Tr. 28

+25 = 12" Tr. 25

+77 = 6" Tr. 24

+67 = 24" Tr. 27

+61 R.P. from 23° ?

+77 = 8' Dirt Entr.

+70 R.P. 28

+67 End Ec. 23

Ec. 22

Ec. 22

+98 R.P. 28

Ec. 21

+46 R.P. 27

Ec. 21

yard Cultiv.

+10

+48 = 2" Tr. 31

+38 = 2" Tr. 35

+28 = T.P. 21

+00 = 10' Lind Entr.

Cultiv.

+98 H.P. 19 & 25

+87 = 16' Graveled Entr.

yard

+17

+66 T.P. 23

Cultivated

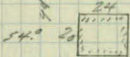
+33 = T.P. 24

+19 = 10" Tr. 41

1.5' Drilling

+10

+89 = 16' Dirt Entr.



Cultivated

63

Black Top.

10 9

62

10 25

61

12 10

60

12 9

59

12 10

58

12 9

57

12 9

56

+162 = 12' Graveled Entr.
+206 = 4" Pole 40
+100 Rd. Section 32m. 27
+90 Guy Pole 19

+71 = R.P. 26

+50 = 12' Graveled Entr.

+22 = 12" Tr. 28

+12 = 6" Tr. 28

+04 = 15" Tr. 28

+94 = 12" Tr. 28

+78 = 12" Tr. 28

+70 = R.P. 26

+47 = 2" Tr. 28

+25 = 18" Tr. 26

+13 = 18" Tr. 34

+95 = 14" Tr. 32

+90 = 10" Tr. 33

+73 = 18" Tr. 32

+55 = 24" Tr. 31

+38 = 6" Tr. 32

+28 = 15" Tr. 31

+16 = 12" Tr. 32

+06 = R.P. 26

+99 = 12" Tr. 32

+62 = 6" Tr. 31

+49 = 18" 5' Temp. 31

+07 = 24" Tr. 32

+87 = 15" Tr. 31

+20 R.P. 28

+88 = 14" Tr. 25

+80 = 10" Tr. 34

+61 = 8" Tr. 29

+44 = 10" Tr. 30

+42 = 10" Tr. 27

+34 = 12" Tr. 29

+65 T.P. 23

+48 Rd. Sgn. 26+29

Co. Rd. "D" 20' Bl. Top 2m

+95 Rd. Sgn. 33

+80 T.P. 23

+13 T.P. 21

+00 = 8' Dirt Entr.

+08 T.P. 19

+95 = 8' Dirt Entr.

+89 = T.P. 18

+55 Rd. Sgn. 20

+40 = 8' Dirt Entr.

1-5-Ft. Drilling

+15

+95 = 24" Tr. 32

+80 = 10" Tr. 39

+67 = T.P. 19

+66 = 24" Tr. 39

+37 = 24" Tr. 41

8' Dirt Entr.

+55 T.P. 20

70

Black top.
10 10

69

10 10

68

10 10

67

10 10

66

9 10

65

9 10

64

10 9

63

10 9

+94 P.P. 27

+90 T.P. 23

Orchard 4x

+38 = 6" Pine 35

+10 Orchard 4x

+69 T.P. 23

+00 P.P. 27

+44 T.P. 23

+18 P.P. 27

+16 T.P. 23

+90 = Rd. Spr. 21

+91 T.P. 22

+65 = 8' Dist. Entry

+02 = P.P. 27

+83 T.P. 22

+30 = 4" Pine 39
+14 = 6" Birch 35

+08 Guy Pole 24

77

Black Top.
10 7

76

11 8

75

12 7

74

9 9

73

10 9

72

9 10

71

9 9

70

+00 = 10' Dirt Entr. ¹²/₅

+65 = 8' Dirt Entr.

+42 = P.P. 25

+05 = 8' Dirt Field Entr.

+68 P.P. 23

+27 P.P. 16

+20 = 4" T. 38

+05 = 8' Dirt Entr.

+65 = 4" T. 38

+89 P.P. 27

+84 T.P. 18

yards

+45 = 8' Dirt Entr.
+33 Property line 188?

+31 = 8" T. 39

+37 H. Pole 17+23

+92 = P.P. 27

yards

+13 = 8' Dirt Entr.

+12 = T.P. 22

Cultivated

Dwelling 25.F.

+31-30" T. 39



46
48
45

84

~~Black Top~~
10 7

83

9 10

82

8 11

81

11 8

80

9 11

79

9 9

78

9 9

77

+57-10' Dirt Entr.

g-d.

+36=12" Tr. 28

+20= P.P. 28

+07=12" Tr. 27

x

+83=12" Tr. 27

+86 T.P. 17

Cultivated

+33 P.P. 28

+62 T.P. 18

Cultivated

+61=8' Dirt Entr.

x

+23 T.P. 18

g-d

* +70

+45= P.P. 28

+40=8' Dirt Entr.

+22=4" Tr. 37

+90=6" Tr. 35

+55= P.P. 28

+49=12" Tr. 25

g-ds + Cultivation

+96 T.P. 18

Cultivated

+56 T.P. 19

91

Back top.

90

89

8

10

88

8

10

87

8

10

86

10

9

85

11

9

84

Mississippi St.
Being Graded

+116 P.C. Cor. 25.5

+69 P.P. 25

P.C. 24

+91 T.P. 20

P.C. 25

+02 T.P. 20

P.C. 29

+137 P. 22

+00 = 8' Dirt Entr.

+78 = 24" Slope 29
+64 = 24" Slope 38

+119 P.C. Cor. 29

8' Dirt Entr.

+109 P.P. 26

+04 T.P. 16

+155 Bush 34

+139 Bush 34
+121 Bush 34

+06 T.P. 16

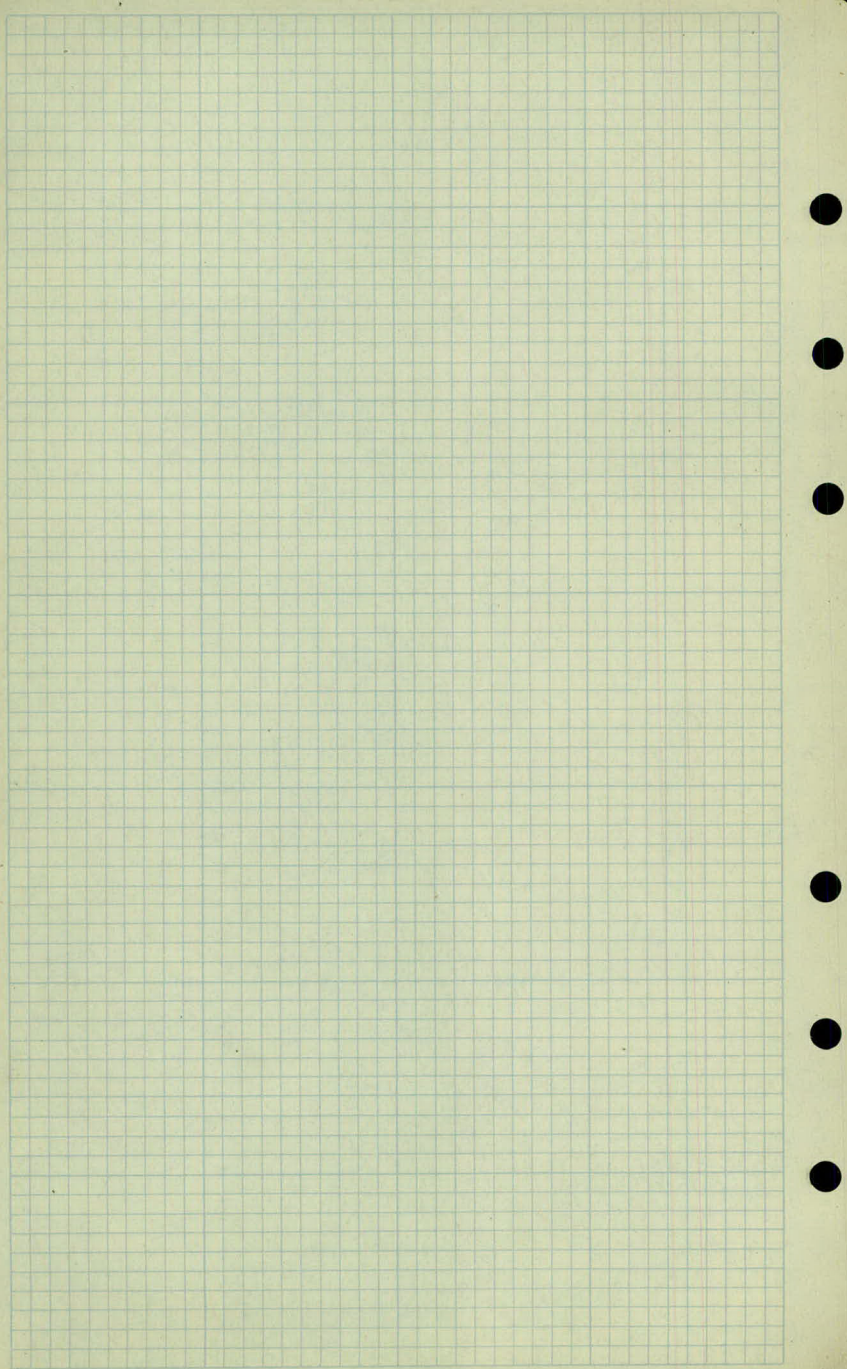
Cultivated

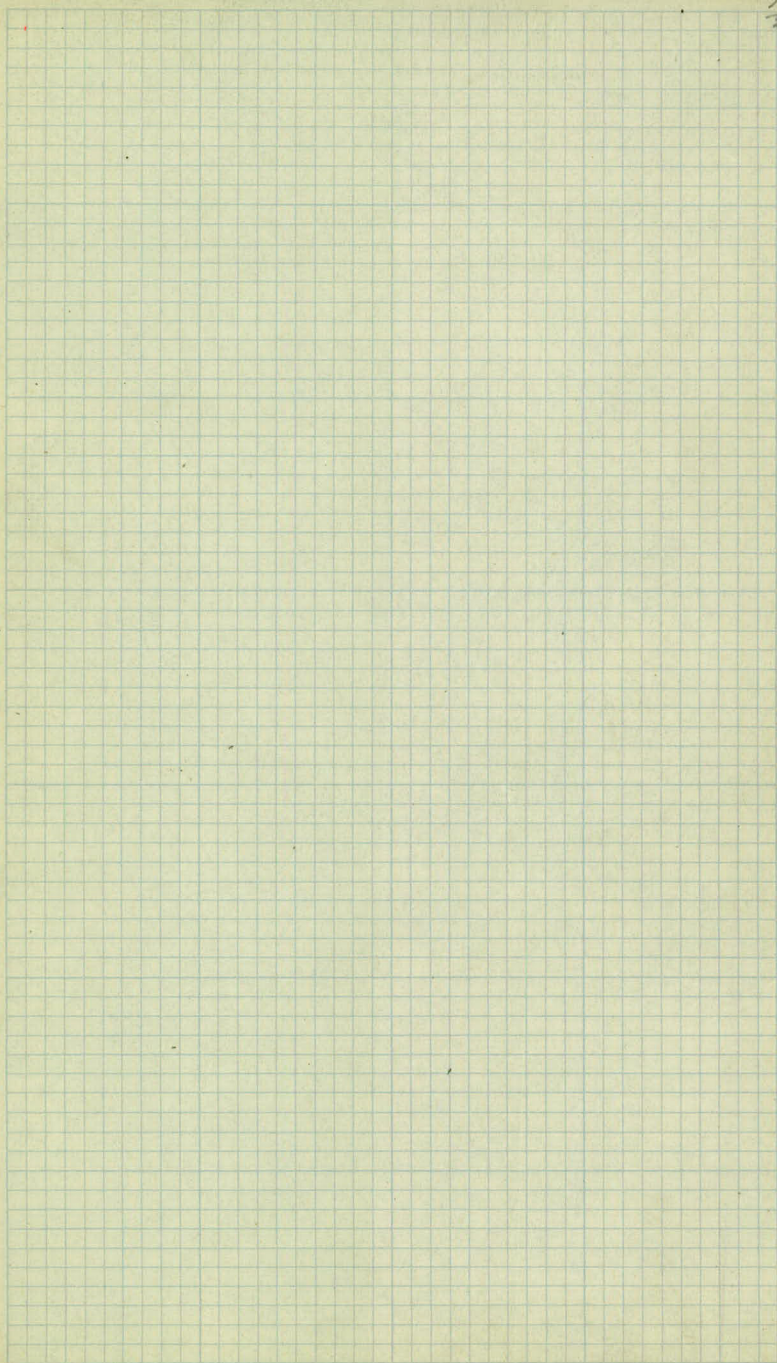
yard

Cultivated

yard

Cultivated





+50 $\frac{Rd}{7-13}$

95

$\frac{Rd}{8-10}$

94

$\frac{Rd}{8-10}$

93

$\frac{Rd}{7-10}$

92

$\frac{Rd}{7-10}$

91

$\frac{Rd}{8-9}$

90

$\frac{Rd}{7-10}$

89

Old End Fence 26'



+70. En. Cor 31'

+67 B. R. 18 23'

+59 End Berry Patch 19'

+54 T.P. 18'

93 - +18 T.P. 28'

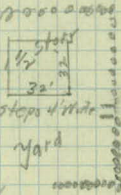
+58 1305 Berry Patch 17'

+78 T.P. 21'

+48 Ent

+41 End Wall 17'

+26 House 44'



94 +94 Cor House 43'

+89 Conc steps 4' wide

+57 T.P. 20'

+49 Beg 1' Rubble Wall 17'

+40 Ent

+30 P.P. 27'

93

+35 T.P. 20'
+28 R/S 20'

+21 P.P. 27'

Out/Hatched

Out/Hatched

+05 T.P. 19'

+37 P.P. 26'

+86 T.P. 19'

Mississippi St

102

Rd
9-10

101

Rd
8-10

100

Rd
9-8

99

Rd
9-9

98

Rd
9-9

97

Rd
6-12

Rd
7-13

96

Rd
8-74

F027

yard

17
25

+76 Ent
+68 2" Tree 28'
+28 Entlines 23'
+15 Rd Sign 19'
+08 Grapellies 25'

Garden

Cultivated

+29 T.P 25'

F026'

+04 T.P 22'

F023' Ditch 83'
F028'

+57 P.P 27'

+72 Rd Sign 17'

+35 A Ditch 20'

+32 F0 Cor 24'

+20 A Ditch 21'

F024' +02 X Drain
18" x 40 CM

2' Ditch

Cultivated

+51 2' Ditch 2'
+11 P.P 27'

Ditch 25'
190 CM 15'

+65 T.P 21'

F024'

+73 T.P 19'

F024'

4 strand Barb Wire

4' Ditch

Ditch 109'

+44 Ditch 160'

Meadow

Meadow

+84 P.P 27'

+65 T.P 16'

+00 F0 Cor 27'

+84 X Drain ? x 40

4' Ditch

20' 20'

+70 P.P 28'

+50 Ditch 40'

+110 T.P 38'

+46 Ent 12" x 28 CM 20'

+35 Ent Hedge 28'

+23 12" Tree 35'

+10 Beg L. Loc Hedge 26'

200 2 1/2" x 1/2"

yard

5' Ditch

+19 A Ditch 60'

$\frac{Rd}{8'-11'}$

109

$\frac{Rd}{8'-11'}$

108

$\frac{Rd}{9'-10'}$

107

$\frac{Rd}{10'-8'}$

106

$\frac{Rd}{11'-7'}$

105

$\frac{Rd}{10'-10'}$

104

$\frac{Rd}{10'-9'}$

103

$\frac{Rd}{10'-10'}$

182 T.P. 17'

163 T.P. 14'

127 T.P. 25'

106 T.P. 30'

161 X Drain
10" CM x 30'
12" K.T. x 30' }

190 T.P. 29'

177 F.C. 30'

F.C. 29' Foldo.

168 T.P. 27'

F.C. 29'

Meadow

Cultivated

School Yard

Cultivated

yard

197.8" Tree 44'

168 End School Yard

168 P.P. 28'

180 12" Tree 30'

150 End

111 12" Tree 30'

194 P.P. 22'

152 CM 19'

142 End

132 12" x 28" CM 33'

110 P.P. 29'

150 4" Apple Tree 32'

150 End yard

146 P.P. 28'

117

Rd
8-11

116

Rd
8-10

115

Rd
7-11

114

Rd
7-11

113

Rd
8-10

112

Rd
7-11

+84 T.P. 18'

Fe. 20

+49 T.P. 18'

Fe 20'

+38 Fe Cor 19'

+16 T.P. 18'

+74 Rd Sign 18'

+70 T.P. 18'

+58 Foot

+47 6" Elm 39'

+44 T.P. 18'

+24 6" BE 38

+95 8" BE 38'

+82 No 14 10x6" CM 12'

+47 Ent 12x18" CM 12

+13 T.P. 18'

28'

Pat
Hole

+70 End Pat Hole 27'

+68 12" Tree 27

+63 12" Tree 27'

+42 P.P. 28'

+24 Rd Sign 21'

+24 Pat hole 40'

+67 P.P. 28'

+93 P.P. 28'

+18 P.P. 28'

+43 P.P. 29'

Cultivated

Cultivated

yard

124

Rd
10-12

123

Rd
7-13

122

Rd
10-12

121

120

Rd
9-10

119

Rd
10-10

118

Rd
8-11

FC 22'

Pasture

XXXXXX

+81 Rd Sign 16'

+77 Fc Cor 22'

+18 T.P 18'

+81 T.P 17

Cultivated

Gravel Road

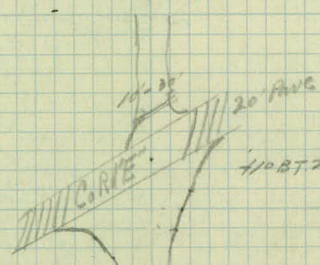
Cultivated

+99 P.P 22'

+62 T.P 14'
+59 Rd Sign 10'
+49 X Drain
18" X 40' CM NG

+70 P.P 33'
+65 Fc Cor 43'
+61 Fc Cor 24'
+55 T.P 19'
+42 Fc 21'
Fc 20

+85 BT 30'
+75 BT 20'
+60 BT 11'



+75 G Pole 28'
+68 G Pole 38'
+68 Rd Sign 32'

+10 BT 20' +10 P.P 28'
+03 Rd Sign 27
+00 BT 16
+90 BT 13

+17 T.P 18'
Fc 20'

+15 P.P 28'

FC 20

131

Rd
11-11

130

Rd
11-11

129

Rd
12-11

128

Rd
13-10'

127

Rd
11-12'

126

Rd
10'-12'

125

Rd
10'-12'

Fc 16'

21
25

+44 T.P 15'

+88 P.P 24'

+41 G.Pole 21'

+12.30"E/127'

Fc 17'

+50 Fc 17'

+34 T.P 87'

Fc 19'

Cultivated

+50 Fc 17'

+02 T.P 38'

Fc 20'

pasture

+95 P.P 21'

+50 Fc 21'

+00 T.P 19'

+00 End Trees Fc 18'

+04 G Pole 15'

+00 24" Stamp 26'

+79 Ent'

+80 Ent'

Fc 21'

Fc 21

+81 T.P 17'

Scattered oaks & Stumps

+22 X.Drain
12" x 24" CM.

135.15

Fc 21

Cultivated

+53 T.P 18'

+97 P.P 21'

Fc 22'

pasture

136

Rd
8-13'

137

Rd
10-13'

136

Rd
12-11

135

Rd
11-11'

134

Rd
10-12

133

Rd
9-12

132

Rd
7-13

+20 T.P. 16'

+17 T.P. 18'

Hay Field

+09 H.Pole 13' 20'

+24 48' Cottonwood

+71 G.Pole 19'

+70 P.P. 20'

+44 Ent. C.M. 18'
Buried

+90 T.P. 16'

Hay Field

Cultivated

+65 T.P. 14'

+45 T.P. 14'

+17 Fe. Cor. 16

+17 End Pasture

Fe 16

Pasture

650

145

Rd
7-13'

144

Rd
10-12'

143

Rd
11-13'

142

Rd
10-13'

141

Rd
10-12'

140

Rd
9-13'

139

Rd
9-13'

152

Rel
8-12

151

Rel
10-12

150

Rel
12-11

149

Rel
10-10

148

Rel
11-12

147

Rel
10-12'

146

Rel
10-14

+40 RR Sign 21'
+36 X Drain 12" X 36 V.I.
+16 X Drain 12" X 30 V.I. 29' 12"
N.P.R.C. 20' 16'

+80 FCor 26
+81 FCor 22

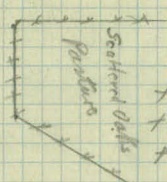
+52 RR Sign 17'
R.O.W. Fence
+87 FCor 37
+84 Rd Sign 36'
+81 G Pole 50'

+83 T.P. 17'

+56 Rd Sign 14'

+54 X Goose Lake Rd 22' Gravel Rd.

+24 X Drain 12" X 30 CM NG 12' 18'



+21 FCor 33'
Fc 33'
+83 Stump 20'
+74 FCor 33'
+62 Stump 27'

+62 T.P. 17'

+99 36" Stump 25'
+67 Stump 28'
+44 Ent 12" X 16 CM 13

+35 T.P. 17'

+17 RR Sign 21'

+04 T.P. 16'

Hay Field

+77 30" Stump 28'
+18 Stump 28'
+07 Rd Sign 22'

Hay Field

+87 T.P. 15'

159

$$\begin{array}{r} \text{Pave} \\ 10-5 \end{array} \quad \begin{array}{r} \text{Pave} \\ 9-0 \end{array}$$

$$\begin{array}{r} \text{Edge Pave} \\ 14' \end{array}$$

$$\begin{array}{r} \text{Edge Pave} \\ 6' \end{array}$$

158

$$\begin{array}{r} \text{Edg. Pave} \\ 3-9 \end{array} \quad \begin{array}{r} \text{Rd} \end{array}$$

$$\begin{array}{r} \text{Edge Pave} \\ 12' \end{array}$$

157

$$\begin{array}{r} \text{Edg. Pave} \\ 36' \end{array} \quad \begin{array}{r} \text{Rd} \\ 9-12 \end{array}$$

156

$$\begin{array}{r} \text{Rd} \\ 8-12 \end{array}$$

155

$$\begin{array}{r} \text{Rd} \\ 10-10 \end{array}$$

154

$$\begin{array}{r} \text{Rd} \\ 8 \end{array}$$

153

$$\begin{array}{r} \text{Rd} \\ 10-8 \end{array}$$

Fc 37'

+50 End 8 Top

+15 Edge Pav

+50 Fc 36'

+08 End EM 12'

+03 T.P 33'

Fc 36'

+65 Rd Sign 16'

+49 Drains 18" x P.P.M. 156 Rd Sign 23

Sq. End
Buried

+50 Fc 32

+18 Box Fc 32'

Centerville Rd/Pav.

+78 T.P 16'

+17 Ent

+06 End Fc 26'

Fc 26'

+97 Rd Sign 15'

+46 T.P 14'

+00 Rd Sign 15'

+42 T.P 16'

Waste

Waste Water & 1 Strand Barb W.

Fc 23

Cu / Hivestall

+20 30' Elm 12

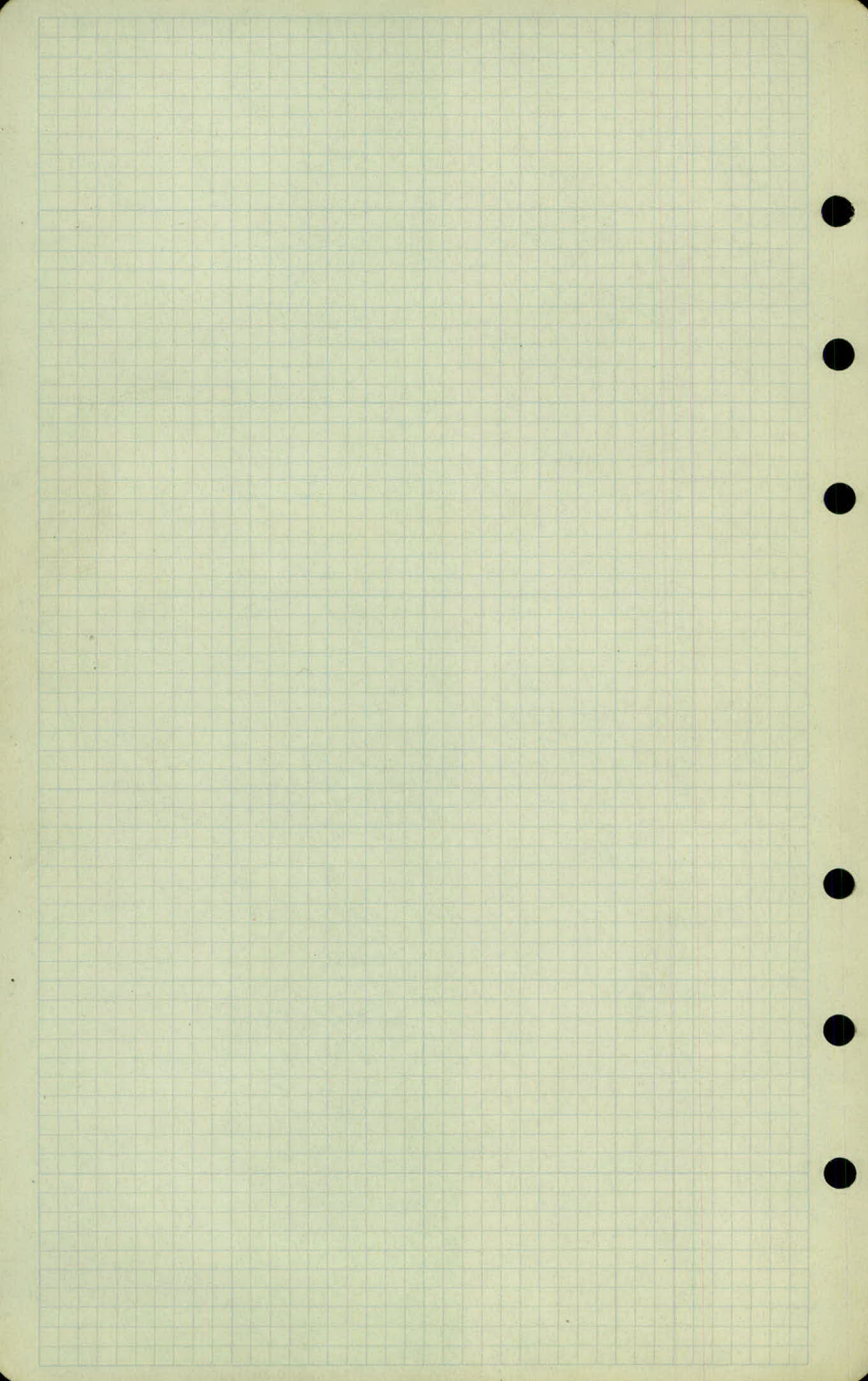
+15 Rd Sign 15'

Fc 22

+30 G. Hiv 16

Fc 26

+30 T.P 16'



Labore Road.

Bench Levels from
Edgerton St. to Centerville Road.

	+	-	-	Elev.
B.M.	3.58	929.46		925.88
	4.97	925.49	8.94	920.52
	4.59	925.39	4.69	920.80
B.M.	3.08	925.39	3.08	922.31
	6.95	928.99	3.35	922.04
B.M.	2.79	926.75	5.03	923.96
	1.00	919.73	8.02	918.73
B.M.	2.99	919.73	2.99	916.74
	8.52	922.39	5.86	913.87
	0.30	918.07	4.62	917.77
B.M.	11.09	918.07	11.09	906.98
	7.96	921.61	4.42	913.65
	1.09	919.18	3.52	918.09
	1.47	907.56	13.09	906.09
B.M.			10.60	896.96
				896.99
B.M.	4.29	930.17		925.88
	6.00	931.56	4.61	925.56
B.M.	3.95	931.56	3.95	927.61
	4.04	927.88	7.72	923.84
	5.91	928.62	5.17	922.71
B.M.	3.38	928.62	3.38	925.24
T.P.	3.14	926.85	4.91	923.71
B.M.	3.50	926.85	3.50	923.35
	3.30	920.41	9.74	917.11

21

Spike in Guy Pole N.W. Cor. Labore & "D"

Top of So. Cor. of conc base for gas pumps
25' Lt. Sta. 46+60.

Spike in 15" Oak 36' Rt. Sta. 37+40

Spike in 12" stump 32' Rt. Sta. 29+40

Top of Retaining wall N.W. Cor. 20' Rt. 16+90

Spike in Guy Pole 50' Lt. Sta. 1+25

Spike in Guy Pole Labore & "D"

S.E. Cor. floor of house 60' Lt. Sta. 72+50

S.E. Cor. Bottom conc. step 50' Lt. Sta. 84+35

Boat spike & Labore & D²

S.W. Cor. top conc. step 25' Lt. Sta. 93+90

	+	K	-	Elev.
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		920.41		
--	--	--------	--	--

	5.76	922.06	4.11	916.30
--	------	--------	------	--------

	8.53	927.27	3.32	918.74
--	------	--------	------	--------

B.M.	3.14	927.27	3.14	924.13
------	------	--------	------	--------

	5.77	930.74	2.30	924.97
--	------	--------	------	--------

	12.46	941.81	1.39	929.25
--	-------	--------	------	--------

B.M.	6.24	941.81	6.24	935.57
------	------	--------	------	--------

	6.47	945.54	2.74	939.07
--	------	--------	------	--------

	3.85	941.94	7.45	938.09
--	------	--------	------	--------

B.M.	1.20	941.94	1.20	940.74
------	------	--------	------	--------

	2.60	933.46	11.08	930.86
--	------	--------	-------	--------

	2.63	928.55	7.54	925.92
--	------	--------	------	--------

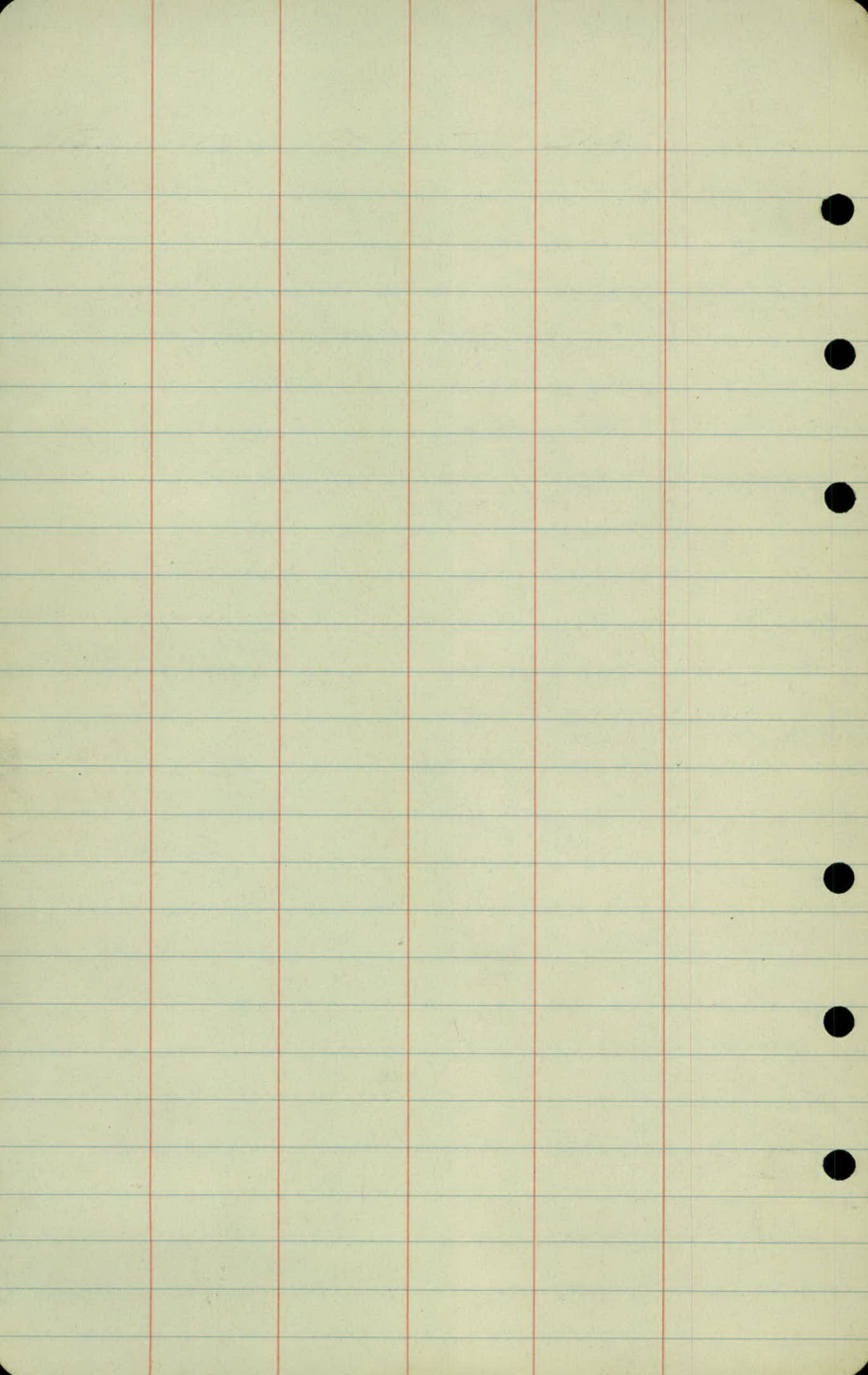
B.M.			8.02	920.53
------	--	--	------	--------

N.W. cor. bottom step of school 85' Rt. Sta. 107+75

Drill hole in pavement $\frac{1}{2}$ " "E" at ^{Sta. 121+10} Labore.

Spike in 8" poplar. 80' Rt. Sta. 134+85

Spike in 24" Elm Tree 15' Rt. Sta. 154+00



120.00 ✓

16.00 ✓

744.75 ✓

16.00 ✓

125.00 ✓

1021.75 X 32

32,696^π

175.00

23.42

198.42

160.

258.42 X 32

8,629.00

8269

12000

23000

81,051

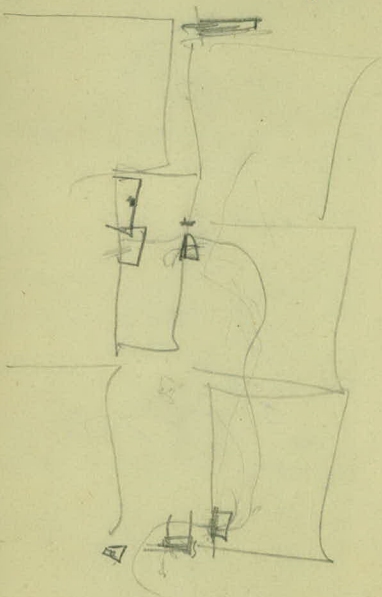
14,592

48,549

16,000

$$\begin{array}{r} 64.23 \\ 3.56 \\ \hline 57.73 \end{array}$$

$$\begin{array}{r} 64.23 \\ 6.5 \\ \hline 54.73 \end{array}$$



$$\begin{array}{r} 1308.56 \\ 116.3 \\ \hline 1424.86 \end{array}$$

$$\begin{array}{r} 1028 \\ 280.7 \\ \hline 1308.7 \\ 116.3 \\ \hline 1425.0 \end{array}$$

$$\begin{array}{r} 48 \\ 33 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 15 \\ 100 \\ \hline 1500 \end{array}$$

$$\begin{array}{r} 160613 \\ 1500 \\ \hline 159113 \end{array}$$

$$\begin{array}{r} 159.113^a \\ 3.652 \text{ az} \end{array}$$

$$\begin{array}{r} 34925 \checkmark \\ 13,786 \checkmark \\ \hline 48,711^a \end{array}$$

$$\begin{array}{r} 1.118 \\ 1.12 \end{array}$$

$$\begin{array}{r} 80 \\ 32 \\ \hline 112 \end{array}$$

9-29-23

Labare Road.

Cross sections from Edgerton St.
to Centerville Road.

11/38.

Sta.	+	π	-	Elev.
B.M.	6.35	903.31		896.96

0+00		98.7		
------	--	------	--	--

+50				
-----	--	--	--	--

1				
---	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

T.P.	13.49	914.53	2.27	901.04
------	-------	--------	------	--------

+85				
-----	--	--	--	--

2				
---	--	--	--	--

+50				
-----	--	--	--	--

3				
---	--	--	--	--

+50				
-----	--	--	--	--

Lt.

E

Et.

2

Spike in Guy Pole 50' Lt. Sta. 1425

$$\begin{array}{r} 113 \\ \hline 9 \end{array} \quad \begin{array}{r} 113 \\ \hline 15 \end{array} \quad \begin{array}{r} 117 \\ \hline 23 \end{array} \quad \begin{array}{r} 155 \\ \hline 35 \end{array} \quad \begin{array}{r} 161 \\ \hline 50 \end{array} \quad \begin{array}{r} 154 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 9.7 \\ \hline 5 \end{array} \quad \begin{array}{r} 9.7 \\ \hline 11 \end{array} \quad \begin{array}{r} 9.6 \\ \hline 50 \end{array} \quad \begin{array}{r} 13.5 \\ \hline 50 \end{array}$$
No End. F.L. line
20

Cry Culvert

$$\begin{array}{r} 14.5 \\ \hline 14.5 \end{array}$$
Top M.H.
9.1
$$\begin{array}{r} 12. \\ \hline 10.9 \end{array}$$

$$\begin{array}{r} \text{out. F.L.} \\ \hline 12.0 \end{array}$$

E.P.R.

$$\begin{array}{r} 76 \\ \hline 24 \end{array} \quad \begin{array}{r} 78 \\ \hline 14 \end{array} \quad \begin{array}{r} 74 \\ \hline 4 \end{array} \quad \begin{array}{r} 74 \\ \hline 10 \end{array} \quad \begin{array}{r} 78 \\ \hline 16 \end{array} \quad \begin{array}{r} 85 \\ \hline 18 \end{array} \quad \begin{array}{r} 82 \\ \hline 26 \end{array} \quad \begin{array}{r} 51 \\ \hline 34 \end{array} \quad \begin{array}{r} 50 \\ \hline 41 \end{array} \quad \begin{array}{r} 57 \\ \hline 50 \end{array}$$

E.P.R.

$$\begin{array}{r} 57 \\ \hline 57 \end{array} \quad \begin{array}{r} 58 \\ \hline 50 \end{array} \quad \begin{array}{r} 60 \\ \hline 43 \end{array} \quad \begin{array}{r} 48 \\ \hline 10 \end{array} \quad \begin{array}{r} 44 \\ \hline 17 \end{array} \quad \begin{array}{r} 48 \\ \hline 25 \end{array} \quad \begin{array}{r} 54 \\ \hline 34 \end{array} \quad \begin{array}{r} 18 \\ \hline 42 \end{array} \quad \begin{array}{r} 38 \\ \hline 42 \end{array} \quad \begin{array}{r} 46 \\ \hline 50 \end{array}$$

E.P.R.

$$\begin{array}{r} 46 \\ \hline 80 \end{array} \quad \begin{array}{r} 52 \\ \hline 63 \end{array} \quad \begin{array}{r} 61 \\ \hline 59 \end{array} \quad \begin{array}{r} 48 \\ \hline 47 \end{array} \quad \begin{array}{r} 31 \\ \hline 52 \end{array} \quad \begin{array}{r} 36 \\ \hline 10 \end{array} \quad \begin{array}{r} 37 \\ \hline 5 \end{array} \quad \begin{array}{r} 33 \\ \hline 33 \end{array} \quad \begin{array}{r} 31 \\ \hline 9 \end{array} \quad \begin{array}{r} 40 \\ \hline 22 \end{array} \quad \begin{array}{r} 38 \\ \hline 28 \end{array} \quad \begin{array}{r} 0.7 \\ \hline 33 \end{array} \quad \begin{array}{r} 10 \\ \hline 40 \end{array} \quad \begin{array}{r} 27 \\ \hline 45 \end{array} \quad \begin{array}{r} 24 \\ \hline 50 \end{array}$$

← Down

$$\begin{array}{r} 12.3 \\ \hline 60 \end{array} \quad \begin{array}{r} 5.6 \\ \hline 50 \end{array} \quad \begin{array}{r} 4.8 \\ \hline 30 \end{array} \quad \begin{array}{r} 14.0 \\ \hline 18 \end{array} \quad \begin{array}{r} 13.9 \\ \hline 8 \end{array} \quad \begin{array}{r} 13.8 \\ \hline 23 \end{array} \quad \begin{array}{r} 14.8 \\ \hline 29 \end{array} \quad \begin{array}{r} 14.6 \\ \hline 24 \end{array} \quad \begin{array}{r} 11.6 \\ \hline 40 \end{array} \quad \begin{array}{r} 11.8 \\ \hline 47 \end{array} \quad \begin{array}{r} 14.5 \\ \hline 50 \end{array} \quad \begin{array}{r} 15.0 \\ \hline 50 \end{array}$$

Inv. Lt.

1490

15.9

$$\begin{array}{r} 48 \\ \hline 63 \end{array} \quad \begin{array}{r} 43 \\ \hline 43 \end{array} \quad \begin{array}{r} 33 \\ \hline 33 \end{array} \quad \begin{array}{r} 38 \\ \hline 30 \end{array} \quad \begin{array}{r} 12.4 \\ \hline 17 \end{array} \quad \begin{array}{r} 14.4 \\ \hline 11 \end{array} \quad \begin{array}{r} 13.4 \\ \hline 5 \end{array} \quad \begin{array}{r} 13.3 \\ \hline 13.3 \end{array} \quad \begin{array}{r} 13.3 \\ \hline 8 \end{array} \quad \begin{array}{r} 14.2 \\ \hline 21 \end{array} \quad \begin{array}{r} 14.1 \\ \hline 25 \end{array} \quad \begin{array}{r} 10.8 \\ \hline 30 \end{array} \quad \begin{array}{r} 11.5 \\ \hline 38 \end{array} \quad \begin{array}{r} 15.0 \\ \hline 46 \end{array} \quad \begin{array}{r} 15.4 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 8.0 \\ \hline 50 \end{array} \quad \begin{array}{r} 2.4 \\ \hline 43 \end{array} \quad \begin{array}{r} 3.9 \\ \hline 36 \end{array} \quad \begin{array}{r} 2.2 \\ \hline 26 \end{array} \quad \begin{array}{r} 10.8 \\ \hline 19 \end{array} \quad \begin{array}{r} 11.0 \\ \hline 6 \end{array} \quad \begin{array}{r} 11.0 \\ \hline 11.0 \end{array} \quad \begin{array}{r} 11.0 \\ \hline 6 \end{array} \quad \begin{array}{r} 12.2 \\ \hline 17 \end{array} \quad \begin{array}{r} 12.1 \\ \hline 21 \end{array} \quad \begin{array}{r} 9.5 \\ \hline 25 \end{array} \quad \begin{array}{r} 13.4 \\ \hline 28 \end{array} \quad \begin{array}{r} 15.4 \\ \hline 37 \end{array} \quad \begin{array}{r} 16.7 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 1.7 \\ \hline 50 \end{array} \quad \begin{array}{r} 2.8 \\ \hline 37 \end{array} \quad \begin{array}{r} 5.6 \\ \hline 28 \end{array} \quad \begin{array}{r} 8.7 \\ \hline 20 \end{array} \quad \begin{array}{r} 8.8 \\ \hline 8 \end{array} \quad \begin{array}{r} 8.7 \\ \hline 8.7 \end{array} \quad \begin{array}{r} 9.7 \\ \hline 12 \end{array} \quad \begin{array}{r} 10.1 \\ \hline 19 \end{array} \quad \begin{array}{r} 8.7 \\ \hline 24 \end{array} \quad \begin{array}{r} 9.0 \\ \hline 34 \end{array} \quad \begin{array}{r} 14.0 \\ \hline 48 \end{array} \quad \begin{array}{r} 14.1 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 3.1 \\ \hline 50 \end{array} \quad \begin{array}{r} 4.9 \\ \hline 39 \end{array} \quad \begin{array}{r} 4.8 \\ \hline 24 \end{array} \quad \begin{array}{r} 2.1 \\ \hline 19 \end{array} \quad \begin{array}{r} 2.1 \\ \hline 11 \end{array} \quad \begin{array}{r} 6.7 \\ \hline 6.7 \end{array} \quad \begin{array}{r} 2.6 \\ \hline 12 \end{array} \quad \begin{array}{r} 2.3 \\ \hline 18 \end{array} \quad \begin{array}{r} 5.7 \\ \hline 26 \end{array} \quad \begin{array}{r} 6.2 \\ \hline 31 \end{array} \quad \begin{array}{r} 14.0 \\ \hline 44 \end{array} \quad \begin{array}{r} 14.7 \\ \hline 50 \end{array}$$

Sta.	+	π	-	Elev.
------	---	-------	---	-------

		914.53		
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4				
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+50				
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B.M.	11.25	924.58	1.20	913.33
------	-------	--------	------	--------

5				
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+50				
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6				
---	--	--	--	--

+50				
-----	--	--	--	--

7				
---	--	--	--	--

+50				
-----	--	--	--	--

8				
---	--	--	--	--

+50				
-----	--	--	--	--

9				
---	--	--	--	--

Lt.

E

Rt.

$\frac{26}{50}$ $\frac{36}{35}$ $\frac{34}{20}$ $\frac{55}{16}$ $\frac{55}{11}$ $\frac{50}{10}$ $\frac{56}{19}$ $\frac{58}{25}$ $\frac{41}{38}$ $\frac{58}{50}$ $\frac{68}{50}$

$\frac{22}{50}$ $\frac{24}{40}$ $\frac{27}{30}$ $\frac{20}{26}$ $\frac{27}{19}$ $\frac{40}{16}$ $\frac{37}{10}$ $\frac{34}{10}$ $\frac{41}{10}$ $\frac{44}{16}$ $\frac{41}{19}$ $\frac{34}{22}$ $\frac{46}{50}$

Nail in Top of Stump 40' Rt. Sta. 4+75

$\frac{112}{50}$ $\frac{111}{31}$ $\frac{116}{19}$ $\frac{128}{16}$ $\frac{127}{11}$ $\frac{121}{11}$ $\frac{127}{14}$ $\frac{130}{18}$ $\frac{131}{20}$ $\frac{114}{46}$ $\frac{107}{50}$ $\frac{113}{50}$

$\frac{96}{50}$ $\frac{102}{35}$ $\frac{114}{16}$ $\frac{112}{11}$ $\frac{106}{11}$ $\frac{113}{17}$ $\frac{115}{21}$ $\frac{92}{37}$ $\frac{95}{50}$ $\frac{92}{50}$

$\frac{86}{50}$ $\frac{90}{36}$ $\frac{87}{19}$ $\frac{98}{16}$ $\frac{92}{11}$ $\frac{97}{18}$ $\frac{101}{22}$ $\frac{72}{50}$ $\frac{74}{50}$

$\frac{75}{50}$ $\frac{73}{47}$ $\frac{77}{30}$ $\frac{71}{18}$ $\frac{81}{16}$ $\frac{78}{12}$ $\frac{73}{11}$ $\frac{79}{17}$ $\frac{82}{19}$ $\frac{73}{22}$ $\frac{46}{48}$ $\frac{42}{50}$ $\frac{49}{50}$

$\frac{59}{50}$ $\frac{56}{30}$ $\frac{50}{18}$ $\frac{66}{15}$ $\frac{63}{10}$ $\frac{56}{10}$ $\frac{61}{17}$ $\frac{62}{20}$ $\frac{53}{23}$ $\frac{33}{34}$ $\frac{22}{50}$ $\frac{40}{50}$

$\frac{50}{50}$ $\frac{42}{37}$ $\frac{42}{18}$ $\frac{53}{15}$ $\frac{52}{10}$ $\frac{47}{11}$ $\frac{49}{18}$ $\frac{47}{19}$ $\frac{40}{44}$ $\frac{41}{50}$ $\frac{42}{50}$

$\frac{47}{50}$ $\frac{51}{23}$ $\frac{54}{18}$ $\frac{51}{10}$ $\frac{46}{11}$ $\frac{52}{17}$ $\frac{54}{19}$ $\frac{48}{45}$ $\frac{54}{50}$ $\frac{59}{50}$

$\frac{46}{50}$ $\frac{56}{21}$ $\frac{60}{14}$ $\frac{57}{10}$ $\frac{53}{13}$ $\frac{59}{17}$ $\frac{63}{21}$ $\frac{59}{25}$ $\frac{61}{38}$ $\frac{58}{45}$ $\frac{61}{50}$ $\frac{64}{50}$

$\frac{50}{50}$ $\frac{57}{25}$ $\frac{63}{21}$ $\frac{61}{14}$ $\frac{62}{9}$ $\frac{59}{13}$ $\frac{71}{17}$ $\frac{65}{23}$ $\frac{61}{39}$ $\frac{71}{46}$ $\frac{75}{50}$

Sta.	+	π	-	Elev.
------	---	-------	---	-------

		924.58		
--	--	--------	--	--

9+50				
------	--	--	--	--

T.P.	1.42	920.33	5.67	918.91
------	------	--------	------	--------

10				
----	--	--	--	--

		6.6		
		913.73		

+50				
-----	--	--	--	--

11				
----	--	--	--	--

+50				
-----	--	--	--	--

12				
----	--	--	--	--

+50				
-----	--	--	--	--

13				
----	--	--	--	--

+50				
-----	--	--	--	--

14				
----	--	--	--	--

+50				
-----	--	--	--	--

15				
----	--	--	--	--

Lt.

E

Rt.

4

$$\frac{51}{50} \quad \frac{58}{26} \quad \frac{63}{7} \quad \frac{62}{17} \quad \frac{69}{27} \quad \frac{65}{27} \quad \frac{74}{50}$$

$$\frac{12}{20} \quad \frac{12}{31} \quad \frac{19}{18} \quad \frac{27}{13} \quad \frac{23}{15} \quad \frac{30}{21} \quad \frac{23}{21} \quad \frac{30}{21} \quad \frac{47}{50}$$

$$\frac{14}{50} \quad \frac{14}{34} \quad \frac{22}{22} \quad \frac{33}{14} \quad \frac{28}{5} \quad \frac{28}{14} \quad \frac{33}{14} \quad \frac{30}{24} \quad \frac{37}{33} \quad \frac{50}{50}$$

$$\frac{19}{50} \quad \frac{16}{26} \quad \frac{19}{23} \quad \frac{36}{14} \quad \frac{37}{8} \quad \frac{33}{6} \quad \frac{33}{15} \quad \frac{38}{15} \quad \frac{36}{26} \quad \frac{61}{50}$$

$$\frac{25}{50} \quad \frac{22}{38} \quad \frac{22}{24} \quad \frac{31}{16} \quad \frac{43}{13} \quad \frac{44}{7} \quad \frac{40}{7} \quad \frac{40}{14} \quad \frac{45}{14} \quad \frac{42}{23} \quad \frac{46}{33} \quad \frac{69}{50}$$

$$\frac{23}{50} \quad \frac{25}{38} \quad \frac{30}{27} \quad \frac{48}{14} \quad \frac{44}{9} \quad \frac{45}{15} \quad \frac{52}{15} \quad \frac{57}{20} \quad \frac{64}{23} \quad \frac{70}{50}$$

$$\frac{\text{Top Gate}}{66} \quad \frac{\text{Nonhole}}{10.2} \quad \frac{\text{Inv. Out.}}{10.2}$$

$$\frac{31}{50} \quad \frac{27}{44} \quad \frac{36}{23} \quad \frac{54}{13} \quad \frac{52}{6} \quad \frac{49}{14} \quad \frac{54}{19} \quad \frac{63}{23} \quad \frac{63}{23} \quad \frac{62}{29} \quad \frac{78}{39} \quad \frac{87}{50}$$

$$\frac{37}{50} \quad \frac{34}{39} \quad \frac{44}{25} \quad \frac{54}{19} \quad \frac{59}{11} \quad \frac{54}{14} \quad \frac{57}{22} \quad \frac{22}{28} \quad \frac{21}{38} \quad \frac{88}{38} \quad \frac{103}{50}$$

$$\frac{37}{50} \quad \frac{35}{39} \quad \frac{46}{25} \quad \frac{58}{19} \quad \frac{61}{12} \quad \frac{57}{14} \quad \frac{63}{21} \quad \frac{81}{26} \quad \frac{80}{36} \quad \frac{110}{36} \quad \frac{130}{50}$$

$$\frac{28}{50} \quad \frac{38}{24} \quad \frac{62}{17} \quad \frac{65}{9} \quad \frac{62}{13} \quad \frac{66}{20} \quad \frac{80}{20} \quad \frac{118}{50}$$

$$\frac{33}{50} \quad \frac{37}{39} \quad \frac{40}{24} \quad \frac{77}{11} \quad \frac{75}{9} \quad \frac{71}{11} \quad \frac{76}{11} \quad \frac{113}{21} \quad \frac{114}{30} \quad \frac{104}{35} \quad \frac{126}{50}$$

$$\frac{50}{50} \quad \frac{57}{21} \quad \frac{87}{17} \quad \frac{87}{11} \quad \frac{80}{13} \quad \frac{80}{14} \quad \frac{84}{20} \quad \frac{111}{28} \quad \frac{121}{30} \quad \frac{114}{30} \quad \frac{139}{50}$$

Sta.	+	-	Elev.
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920.33

T.P.	3.80	916.13	8.00	912.33
------	------	--------	------	--------

15+25

+50

16

+50

+86

17

B.M.	9.15	916.13	9.15	906.98	(906.98)
------	------	--------	------	--------	----------

+43

T.P.	8.63	921.27	3.49	918.64
------	------	--------	------	--------

18

+50

19

+50

27.

£

名大

$$\begin{array}{cccccccccccc} 15 & 23 & 38 & 58 & 58 & 58 & 47 & & 48 & 84 & 104 & 117 \\ \hline 50 & 34 & 28 & 21 & 17 & 15 & 13 & 41 & 13 & 20 & 36 & 50 \end{array}$$

21	32	50	57	62	62	50	46	44	51	84	101	117	134
50	30	26	19	17	18	12	8	14	20	26	39	50	

[illegible]

$\frac{16}{50}$	$\frac{25}{34}$	$\frac{44}{28}$	$\frac{48}{23}$	$\frac{60}{18}$	$\frac{60}{17}$	$\frac{52}{14}$	$\frac{51}{7}$	$\frac{50}{50}$	$\frac{54}{14}$	$\frac{96}{25}$	$\frac{123}{37}$	$\frac{147}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	------------------	------------------

$\frac{22}{60}$ $\frac{38}{35}$ $\frac{43}{18}$ $\frac{49}{5}$ $\frac{48}{13}$ $\frac{54}{18}$ $\frac{61}{24}$ $\frac{80}{22}$ $\frac{88}{32}$ $\frac{102}{29}$

								Top Cat		Wap	Wark
11	17	42	4.7	46	5.3	5.7	20	20	52	146	146
50	38	28	5	14	18	24	31	36	36	42	

Top of Retaining Wall N.W. Cor. 36' Rt. Sta. 16+90

$\frac{00}{50}$	$\frac{11}{28}$	$\frac{25}{22}$	$\frac{40}{8}$	$\frac{36}{12}$	$\frac{43}{18}$	$\frac{55}{18}$	$\frac{52}{20}$	$\frac{74}{32}$	$\frac{96}{50}$
-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

George Floor

7.6

37	48	58	28	25	70	27	79	75	97
<u>60</u>	<u>34</u>	<u>27</u>	<u>15</u>	<u>10</u>	<u>11</u>	<u>22</u>	<u>32</u>	<u>50</u>	

$\frac{31}{20}$	$\frac{35}{23}$	$\frac{49}{17}$	$\frac{61}{14}$	$\frac{63}{10}$	$\frac{8}{5}$	$\frac{62}{10}$	$\frac{63}{16}$	$\frac{46}{19}$	$\frac{46}{32}$	$\frac{63}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	---------------	-----------------	-----------------	-----------------	-----------------	-----------------

$$\frac{28}{50} \quad \frac{28}{38} \quad \frac{6}{18} \quad \frac{13}{14} \quad \frac{50}{9} \quad \frac{46}{1} \quad \frac{51}{11} \quad \frac{53}{17} \quad \frac{36}{20} \quad \frac{40}{28} \quad \frac{30}{33} \quad \frac{40}{38} \quad \frac{47}{60}$$

$\frac{2^6}{2^0}$ $\frac{2^9}{18}$ $\frac{4^2}{14}$ $\frac{4^0}{10}$ $\frac{3^2}{10}$ $\frac{4^0}{10}$ $\frac{4^3}{12}$ $\frac{3^9}{17}$ $\frac{3^1}{19}$ $\frac{3^1}{29}$ $\frac{3^1}{36}$ $\frac{3^1}{42}$ $\frac{3^8}{50}$

Sta.	+	π	-	Elev.
		921.27		

T.P.	5.87	923.70	3.44	917.83
------	------	--------	------	--------

20				18.5
----	--	--	--	------

+50				18.9
-----	--	--	--	------

21				19.1
----	--	--	--	------

+50				19.0
-----	--	--	--	------

22				19.1
----	--	--	--	------

+50				19.0
-----	--	--	--	------

23				18.3
----	--	--	--	------

T.P.	1.39	921.57	3.52	920.18
------	------	--------	------	--------

+50				17.9
-----	--	--	--	------

24				17.7
----	--	--	--	------

+50				17.0
-----	--	--	--	------

25				16.4
----	--	--	--	------

+50				16.1
-----	--	--	--	------

LT.

E

RT.

$\frac{46}{50}$ $\frac{49}{37}$ $\frac{44}{30}$ $\frac{52}{28}$ $\frac{50}{18}$ $\frac{60}{14}$ $\frac{57}{10}$ $\frac{52}{/}$ $\frac{56}{11}$ $\frac{61}{14}$ $\frac{56}{17}$ $\frac{58}{28}$ $\frac{46}{33}$ $\frac{50}{50}$

$\frac{45}{10}$ $\frac{49}{38}$ $\frac{45}{20}$ $\frac{42}{21}$ $\frac{47}{17}$ $\frac{57}{14}$ $\frac{53}{9}$ $\frac{48}{/}$ $\frac{53}{11}$ $\frac{56}{14}$ $\frac{53}{16}$ $\frac{54}{28}$ $\frac{43}{31}$ $\frac{49}{50}$

$\frac{48}{50}$ $\frac{50}{41}$ $\frac{43}{32}$ $\frac{49}{28}$ $\frac{48}{19}$ $\frac{55}{15}$ $\frac{53}{9}$ $\frac{46}{/}$ $\frac{52}{11}$ $\frac{56}{21}$ $\frac{48}{30}$ $\frac{54}{50}$

$\frac{49}{50}$ $\frac{47}{34}$ $\frac{43}{31}$ $\frac{59}{25}$ $\frac{58}{14}$ $\frac{52}{9}$ $\frac{47}{/}$ $\frac{53}{11}$ $\frac{53}{20}$ $\frac{51}{29}$ $\frac{47}{32}$ $\frac{53}{50}$

$\frac{53}{50}$ $\frac{49}{34}$ $\frac{44}{31}$ $\frac{60}{26}$ $\frac{58}{15}$ $\frac{50}{10}$ $\frac{46}{/}$ $\frac{51}{14}$ $\frac{51}{17}$ $\frac{46}{31}$ $\frac{53}{50}$

$\frac{50}{50}$ $\frac{46}{32}$ $\frac{54}{28}$ $\frac{58}{21}$ $\frac{61}{18}$ $\frac{53}{14}$ $\frac{49}{9}$ $\frac{47}{/}$ $\frac{57}{12}$ $\frac{58}{20}$ $\frac{54}{21}$ $\frac{53}{31}$ $\frac{53}{34}$ $\frac{55}{50}$

$\frac{51}{50}$ $\frac{56}{33}$ $\frac{58}{11}$ $\frac{54}{/}$ $\frac{59}{12}$ $\frac{62}{14}$ $\frac{61}{23}$ $\frac{62}{26}$ $\frac{53}{30}$ $\frac{57}{33}$ $\frac{57}{50}$

$\frac{29}{50}$ $\frac{29}{38}$ $\frac{23}{33}$ $\frac{48}{25}$ $\frac{52}{18}$ $\frac{41}{11}$ $\frac{41}{10}$ $\frac{37}{/}$ $\frac{41}{11}$ $\frac{43}{17}$ $\frac{48}{22}$ $\frac{49}{24}$ $\frac{36}{29}$ $\frac{36}{32}$ $\frac{36}{50}$

$\frac{33}{50}$ $\frac{36}{44}$ $\frac{30}{32}$ $\frac{46}{23}$ $\frac{50}{19}$ $\frac{48}{14}$ $\frac{44}{10}$ $\frac{39}{/}$ $\frac{44}{12}$ $\frac{54}{25}$ $\frac{40}{28}$ $\frac{40}{10}$

$\frac{37}{50}$ $\frac{39}{37}$ $\frac{32}{31}$ $\frac{43}{26}$ $\frac{54}{24}$ $\frac{52}{15}$ $\frac{55}{13}$ $\frac{50}{10}$ $\frac{46}{/}$ $\frac{48}{10}$ $\frac{56}{24}$ $\frac{42}{27}$ $\frac{41}{50}$

$\frac{36}{50}$ $\frac{38}{31}$ $\frac{32}{31}$ $\frac{58}{23}$ $\frac{55}{11}$ $\frac{52}{/}$ $\frac{54}{10}$ $\frac{63}{24}$ $\frac{42}{27}$ $\frac{42}{50}$

$\frac{57}{50}$ $\frac{58}{29}$ $\frac{64}{22}$ $\frac{59}{10}$ $\frac{55}{/}$ $\frac{57}{11}$ $\frac{67}{24}$ $\frac{40}{28}$ $\frac{46}{50}$

Sta.	+	K	-	Elev.
		721.57		

26				15.5
----	--	--	--	------

+50				14.8
-----	--	--	--	------

27				14.3
----	--	--	--	------

T.P.	5.10	918.74	7.95	913.6 ✓
------	------	--------	------	---------

+50				13.6
-----	--	--	--	------

28				13.1
----	--	--	--	------

+50				12.6
-----	--	--	--	------

+58				12.5
-----	--	--	--	------

+80				12.5
-----	--	--	--	------

+85				12.5
-----	--	--	--	------

29				12.7
----	--	--	--	------

+05				12.9
-----	--	--	--	------

+20				12.9
-----	--	--	--	------

Lt.

E

Rt.

$\frac{40}{50}$ $\frac{42}{28}$ $\frac{72}{23}$ $\frac{70}{15}$ $\frac{64}{10}$ $\frac{61}{/}$ $\frac{65}{13}$ $\frac{73}{24}$ $\frac{46}{28}$ $\frac{44}{50}$

$\frac{49}{50}$ $\frac{57}{29}$ $\frac{79}{24}$ $\frac{82}{14}$ $\frac{75}{11}$ $\frac{68}{/}$ $\frac{72}{15}$ $\frac{82}{24}$ $\frac{61}{28}$ $\frac{63}{50}$

$\frac{58}{50}$ $\frac{64}{36}$ $\frac{78}{29}$ $\frac{81}{23}$ $\frac{83}{14}$ $\frac{78}{10}$ $\frac{73}{/}$ $\frac{78}{13}$ $\frac{86}{17}$ $\frac{90}{22}$ $\frac{78}{26}$ $\frac{106}{34}$ $\frac{112}{50}$

$\frac{81}{50}$ $\frac{85}{37}$ $\frac{68}{22}$ $\frac{70}{17}$ $\frac{54}{11}$ $\frac{51}{/}$ $\frac{55}{11}$ $\frac{67}{17}$ $\frac{69}{21}$ $\frac{60}{25}$ $\frac{88}{31}$ $\frac{109}{50}$

$\frac{23}{50}$ $\frac{35}{31}$ $\frac{25}{23}$ $\frac{26}{17}$ $\frac{60}{11}$ $\frac{56}{/}$ $\frac{61}{10}$ $\frac{73}{17}$ $\frac{72}{21}$ $\frac{66}{25}$ $\frac{81}{30}$ $\frac{101}{50}$

$\frac{08}{50}$ $\frac{08}{41}$ $\frac{23}{34}$ $\frac{78}{33}$ $\frac{78}{18}$ $\frac{64}{14}$ $\frac{61}{/}$ $\frac{72}{14}$ $\frac{76}{15}$ $\frac{84}{18}$ $\frac{87}{22}$ $\frac{58}{25}$ $\frac{76}{50}$

$\frac{10}{50}$ $\frac{15}{34}$ $\frac{75}{23}$ $\frac{79}{18}$ $\frac{67}{14}$ $\frac{62}{/}$ $\frac{66}{8}$ $\frac{85}{23}$ $\frac{102}{25}$ $\frac{118}{50}$

$\frac{07}{50}$ $\frac{19}{34}$ $\frac{80}{24}$ $\frac{80}{19}$ $\frac{63}{12}$ $\frac{62}{/}$ $\frac{67}{10}$ $\frac{100}{50}$

Side Culvert to M.H.

W. End. East End

$\frac{81}{/}$ $\frac{84}{/}$

$\frac{85}{/}$ $\frac{87}{/}$

$\frac{44}{50}$ $\frac{28}{31}$

$\frac{61}{13}$ $\frac{60}{/}$

$\frac{62}{4}$ $\frac{78}{27}$

$\frac{100}{50}$ $\frac{100}{/}$

$\frac{100}{50}$ $\frac{100}{/}$

$\frac{100}{50}$ $\frac{100}{/}$

$\frac{100}{50}$ $\frac{100}{/}$

$\frac{100}{50}$ $\frac{100}{/}$

$\frac{100}{50}$ $\frac{100}{/}$

$\frac{100}{50}$ $\frac{100}{/}$

$\frac{100}{50}$ $\frac{100}{/}$

$\frac{100}{50}$ $\frac{100}{/}$

$\frac{08}{50}$ $\frac{09}{38}$

$\frac{51}{33}$ $\frac{62}{23}$

$\frac{82}{18}$ $\frac{60}{12}$

$\frac{78}{18}$ $\frac{62}{10}$

$\frac{83}{30}$ $\frac{84}{40}$

$\frac{75}{50}$ $\frac{75}{/}$

$\frac{75}{50}$ $\frac{75}{/}$

$\frac{75}{50}$ $\frac{75}{/}$

$\frac{75}{50}$ $\frac{75}{/}$

$\frac{75}{50}$ $\frac{75}{/}$

$\frac{75}{50}$ $\frac{75}{/}$

$\frac{75}{50}$ $\frac{75}{/}$

$\frac{75}{50}$ $\frac{75}{/}$

$\frac{75}{50}$ $\frac{75}{/}$

$\frac{11}{50}$ $\frac{11}{34}$

$\frac{73}{29}$ $\frac{77}{18}$

$\frac{63}{11}$ $\frac{78}{18}$

$\frac{62}{8}$ $\frac{73}{16}$

$\frac{64}{25}$ $\frac{66}{47}$

$\frac{47}{53}$ $\frac{47}{/}$

$\frac{47}{53}$ $\frac{47}{/}$

$\frac{47}{53}$ $\frac{47}{/}$

$\frac{47}{53}$ $\frac{47}{/}$

$\frac{47}{53}$ $\frac{47}{/}$

$\frac{47}{53}$ $\frac{47}{/}$

$\frac{47}{53}$ $\frac{47}{/}$

$\frac{47}{53}$ $\frac{47}{/}$

$\frac{47}{53}$ $\frac{47}{/}$

On Lt.

M.H. E. Line 138

Top Cover

5.6

Sta.	+	π	-	Elev.
		918.74		
B.M.	1.98	918.74	1.98	916.74
29+50				13.3
30				14.5
T.P.	6.47	921.85	3.34	915.38
+50				15.6
31				16.5
+50				17.4
32				18.1
+50				19.0
33				19.9
+50				20.3
T.P.	6.95	927.41	1.39	920.46
34				20.4
+50				20.8

Lt.

E

Rt.

Spike in 12" Stump 33 Rt. Sta. 29+40

$\frac{19}{50}$ $\frac{23}{31}$ $\frac{63}{23}$ $\frac{69}{18}$ $\frac{55}{13}$ $\frac{54}{/}$ $\frac{61}{13}$ $\frac{55}{17}$ $\frac{51}{22}$ $\frac{36}{26}$ $\frac{40}{34}$ $\frac{51}{50}$

$\frac{15}{50}$ $\frac{24}{30}$ $\frac{54}{23}$ $\frac{21}{17}$ $\frac{48}{13}$ $\frac{42}{/}$ $\frac{53}{22}$ $\frac{37}{26}$ $\frac{39}{31}$ $\frac{17}{37}$ $\frac{17}{50}$

30+37 Intake at Ditch 12.5

12" x 15" x 6" Ht.
conc H.W.

69.35

M.H.

M.H.

Core

Flankline

08.35

15.4

$\frac{46}{50}$ $\frac{46}{29}$ $\frac{22}{22}$ $\frac{70}{13}$ $\frac{63}{/}$ $\frac{69}{11}$ $\frac{21}{22}$ $\frac{45}{25}$ $\frac{43}{50}$

$\frac{42}{50}$ $\frac{38}{38}$ $\frac{34}{29}$ $\frac{64}{23}$ $\frac{61}{13}$ $\frac{54}{/}$ $\frac{58}{9}$ $\frac{63}{21}$ $\frac{36}{26}$ $\frac{34}{50}$

$\frac{35}{50}$ $\frac{32}{40}$ $\frac{24}{36}$ $\frac{25}{28}$ $\frac{54}{23}$ $\frac{53}{14}$ $\frac{45}{/}$ $\frac{50}{9}$ $\frac{53}{15}$ $\frac{52}{22}$ $\frac{34}{25}$ $\frac{36}{50}$

$\frac{36}{50}$ $\frac{33}{34}$ $\frac{30}{27}$ $\frac{45}{23}$ $\frac{46}{18}$ $\frac{44}{14}$ $\frac{38}{/}$ $\frac{42}{10}$ $\frac{47}{16}$ $\frac{47}{22}$ $\frac{34}{24}$ $\frac{20}{50}$

$\frac{33}{50}$ $\frac{29}{34}$ $\frac{25}{27}$ $\frac{40}{22}$ $\frac{35}{13}$ $\frac{29}{/}$ $\frac{35}{14}$ $\frac{43}{24}$ $\frac{25}{26}$ $\frac{29}{50}$

$\frac{27}{50}$ $\frac{21}{29}$ $\frac{35}{24}$ $\frac{27}{13}$ $\frac{20}{/}$ $\frac{26}{11}$ $\frac{35}{23}$ $\frac{18}{25}$ $\frac{23}{50}$

$\frac{24}{50}$ $\frac{17}{27}$ $\frac{33}{21}$ $\frac{29}{17}$ $\frac{22}{11}$ $\frac{16}{/}$ $\frac{22}{11}$ $\frac{24}{19}$ $\frac{20}{21}$ $\frac{18}{50}$

Rec 3034

$\frac{16}{50}$ $\frac{10}{28}$ $\frac{86}{21}$ $\frac{76}{14}$ $\frac{72}{10}$ $\frac{73}{10}$ $\frac{31}{17}$ $\frac{74}{22}$ $\frac{73}{30}$ $\frac{68}{24}$ $\frac{71}{50}$

$\frac{12}{50}$ $\frac{74}{41}$ $\frac{76}{27}$ $\frac{74}{21}$ $\frac{73}{14}$ $\frac{60}{/}$ $\frac{70}{11}$ $\frac{75}{20}$ $\frac{74}{24}$ $\frac{69}{34}$ $\frac{74}{50}$

Sta.	+	π	-	Elev.
		927.41		

35				21.2
----	--	--	--	------

+50				21.6
-----	--	--	--	------

36				22.2
----	--	--	--	------

+50				23.1
-----	--	--	--	------

37				23.6
----	--	--	--	------

+50				24.0
-----	--	--	--	------

B.M.	5.40	929.36	348	923.96
------	------	--------	-----	--------

38				24.2
----	--	--	--	------

+50				24.3
-----	--	--	--	------

39				24.2
----	--	--	--	------

+50				24.3
-----	--	--	--	------

40				24.5
----	--	--	--	------

+50				24.7
-----	--	--	--	------

Lt.

E

Rt.

$\frac{21}{50}$ $\frac{63}{30}$ $\frac{76}{27}$ $\frac{69}{13}$ $\frac{62}{11}$ $\frac{69}{15}$ $\frac{74}{18}$ $\frac{74}{23}$ $\frac{67}{24}$ $\frac{76}{50}$

$\frac{68}{50}$ $\frac{52}{27}$ $\frac{66}{23}$ $\frac{66}{10}$ $\frac{58}{14}$ $\frac{63}{18}$ $\frac{69}{18}$ $\frac{70}{24}$ $\frac{65}{26}$ $\frac{73}{50}$

$\frac{56}{50}$ $\frac{48}{26}$ $\frac{50}{20}$ $\frac{63}{15}$ $\frac{62}{11}$ $\frac{52}{12}$ $\frac{55}{12}$ $\frac{63}{21}$ $\frac{53}{22}$ $\frac{61}{50}$

$\frac{43}{50}$ $\frac{39}{28}$ $\frac{40}{18}$ $\frac{54}{15}$ $\frac{43}{14}$ $\frac{49}{14}$ $\frac{54}{16}$ $\frac{53}{21}$ $\frac{46}{23}$ $\frac{54}{50}$

$\frac{41}{50}$ $\frac{36}{21}$ $\frac{51}{17}$ $\frac{38}{12}$ $\frac{42}{12}$ $\frac{47}{13}$ $\frac{44}{22}$ $\frac{52}{50}$

$\frac{40}{50}$ $\frac{38}{39}$ $\frac{33}{24}$ $\frac{48}{20}$ $\frac{44}{15}$ $\frac{34}{12}$ $\frac{38}{12}$ $\frac{48}{11}$ $\frac{47}{25}$ $\frac{43}{28}$ $\frac{50}{50}$

Spike in 15" oak 36' Rt 512 37+40

$\frac{54}{50}$ $\frac{50}{31}$ $\frac{50}{24}$ $\frac{63}{19}$ $\frac{62}{11}$ $\frac{52}{14}$ $\frac{57}{14}$ $\frac{65}{22}$ $\frac{59}{25}$ $\frac{69}{50}$

$\frac{53}{50}$ $\frac{53}{23}$ $\frac{63}{18}$ $\frac{51}{12}$ $\frac{55}{12}$ $\frac{62}{23}$ $\frac{54}{27}$ $\frac{61}{50}$

$\frac{52}{50}$ $\frac{50}{20}$ $\frac{60}{17}$ $\frac{52}{11}$ $\frac{55}{11}$ $\frac{62}{15}$ $\frac{63}{24}$ $\frac{56}{27}$ $\frac{60}{50}$

$\frac{51}{50}$ $\frac{43}{22}$ $\frac{58}{16}$ $\frac{51}{11}$ $\frac{54}{11}$ $\frac{61}{17}$ $\frac{63}{25}$ $\frac{53}{27}$ $\frac{60}{50}$

$\frac{51}{50}$ $\frac{44}{24}$ $\frac{58}{18}$ $\frac{51}{10}$ $\frac{49}{11}$ $\frac{54}{11}$ $\frac{49}{30}$ $\frac{61}{50}$

$\frac{44}{50}$ $\frac{42}{38}$ $\frac{58}{22}$ $\frac{53}{13}$ $\frac{47}{11}$ $\frac{50}{11}$ $\frac{55}{18}$ $\frac{49}{22}$ $\frac{49}{36}$ $\frac{59}{50}$

Sta.	+	π	-	Elev.
		929.36		

41				24.6
----	--	--	--	------

+50				24.1
-----	--	--	--	------

42				23.3
----	--	--	--	------

+50				22.9
-----	--	--	--	------

43				22.4
----	--	--	--	------

+50				22.3
-----	--	--	--	------

44				22.2
----	--	--	--	------

T.P.	4.01	925.70	7.67	921.69
------	------	--------	------	--------

+50				22.0
-----	--	--	--	------

45				21.6
----	--	--	--	------

21.0

+50				21.3
-----	--	--	--	------

46				21.3
----	--	--	--	------

21.2

+50				21.2
-----	--	--	--	------

Lt.

E

Rt.

10

$$\frac{41}{50} \quad \frac{32}{28} \quad \frac{64}{21} \quad \frac{64}{18} \quad \frac{52}{12} \quad \frac{48}{14} \quad \frac{58}{20} \quad \frac{24}{23} \quad \frac{76}{28} \quad \frac{50}{36} \quad \frac{45}{60}$$

$$\frac{47}{50} \quad \frac{35}{31} \quad \frac{43}{25} \quad \frac{70}{19} \quad \frac{60}{12} \quad \frac{53}{12} \quad \frac{61}{12} \quad \frac{85}{19} \quad \frac{86}{22} \quad \frac{65}{27} \quad \frac{78}{50}$$

$$\frac{42}{50} \quad \frac{42}{28} \quad \frac{74}{19} \quad \frac{72}{16} \quad \frac{66}{13} \quad \frac{61}{12} \quad \frac{66}{12} \quad \frac{94}{19} \quad \frac{93}{22} \quad \frac{85}{24} \quad \frac{107}{50}$$

$$\frac{52}{50} \quad \frac{50}{31} \quad \frac{85}{21} \quad \frac{85}{18} \quad \frac{69}{13} \quad \frac{65}{12} \quad \frac{76}{12} \quad \frac{102}{19} \quad \frac{132}{50}$$

$$\frac{59}{50} \quad \frac{63}{30} \quad \frac{80}{24} \quad \frac{82}{18} \quad \frac{75}{13} \quad \frac{70}{12} \quad \frac{76}{11} \quad \frac{113}{21} \quad \frac{137}{60}$$

$$\frac{62}{50} \quad \frac{69}{28} \quad \frac{86}{21} \quad \frac{77}{12} \quad \frac{71}{12} \quad \frac{81}{13} \quad \frac{110}{24} \quad \frac{150}{50}$$

$$\frac{55}{50} \quad \frac{55}{28} \quad \frac{90}{21} \quad \frac{89}{19} \quad \frac{77}{12} \quad \frac{72}{12} \quad \frac{78}{11} \quad \frac{110}{20} \quad \frac{120}{23} \quad \frac{96}{28} \quad \frac{112}{50}$$

$$\frac{21}{50} \quad \frac{20}{32} \quad \frac{27}{25} \quad \frac{53}{19} \quad \frac{52}{16} \quad \frac{44}{12} \quad \frac{37}{12} \quad \frac{42}{11} \quad \frac{71}{18} \quad \frac{72}{23} \quad \frac{62}{27} \quad \frac{74}{50}$$

$$\frac{32}{50} \quad \frac{29}{31} \quad \frac{58}{23} \quad \frac{58}{17} \quad \frac{49}{13} \quad \frac{41}{12} \quad \frac{48}{13} \quad \frac{24}{20} \quad \frac{78}{25} \quad \frac{63}{30} \quad \frac{81}{50}$$

$$\frac{35}{50} \quad \frac{40}{26} \quad \frac{63}{19} \quad \frac{52}{16} \quad \frac{44}{12} \quad \frac{51}{10} \quad \frac{62}{14} \quad \frac{80}{32} \quad \frac{92}{50}$$

$$\frac{37}{50} \quad \frac{42}{24} \quad \frac{51}{15} \quad \frac{49}{11} \quad \frac{44}{12} \quad \frac{47}{12} \quad \frac{60}{11} \quad \frac{73}{26} \quad \frac{90}{50}$$

$$\frac{32}{50} \quad \frac{42}{28} \quad \frac{41}{15} \quad \frac{46}{12} \quad \frac{54}{14} \quad \frac{63}{20} \quad \frac{74}{31} \quad \frac{90}{50}$$

Top Pump Platform 34

Sta.	+	π	-	Elev.
		925.70		
B.M.	3.36	925.67	3.39	922.31
47				21.1
+50				21.0
48				21.1
+50				21.2
49				21.4
T.P.	4.12	925.17	4.62	921.05
+50				21.3
50				21.1
+50				20.8
51				20.3
+50				20.4
52				20.4

Lt.

2

Rt.

11

Top of 20 Cor. of concrete base gasoline
pump platform 25' Lt. 518. 46160

$\frac{35}{50}$ $\frac{45}{18}$ $\frac{46}{15}$ $\frac{52}{15}$ $\frac{57}{20}$ $\frac{74}{31}$ $\frac{86}{50}$

$\frac{32}{50}$ $\frac{40}{26}$ $\frac{48}{15}$ $\frac{47}{11}$ $\frac{53}{11}$ $\frac{67}{20}$ $\frac{81}{50}$

$\frac{27}{50}$ $\frac{37}{27}$ $\frac{45}{18}$ $\frac{52}{16}$ $\frac{48}{14}$ $\frac{46}{14}$ $\frac{53}{14}$ $\frac{58}{17}$ $\frac{68}{28}$ $\frac{81}{50}$

$\frac{35}{50}$ $\frac{40}{21}$ $\frac{55}{17}$ $\frac{48}{11}$ $\frac{45}{14}$ $\frac{52}{14}$ $\frac{68}{17}$ $\frac{74}{24}$ $\frac{67}{29}$ $\frac{80}{50}$

$\frac{37}{50}$ $\frac{40}{31}$ $\frac{35}{21}$ $\frac{50}{17}$ $\frac{47}{11}$ $\frac{43}{14}$ $\frac{51}{14}$ $\frac{20}{18}$ $\frac{77}{28}$ $\frac{82}{50}$

$\frac{31}{50}$ $\frac{36}{24}$ $\frac{28}{21}$ $\frac{48}{17}$ $\frac{46}{14}$ $\frac{43}{11}$ $\frac{39}{14}$ $\frac{47}{14}$ $\frac{74}{22}$ $\frac{75}{26}$ $\frac{74}{30}$ $\frac{84}{50}$

$\frac{35}{50}$ $\frac{34}{26}$ $\frac{30}{24}$ $\frac{52}{17}$ $\frac{52}{14}$ $\frac{46}{11}$ $\frac{41}{14}$ $\frac{46}{11}$ $\frac{53}{17}$ $\frac{20}{25}$ $\frac{80}{28}$ $\frac{91}{50}$

$\frac{38}{50}$ $\frac{35}{31}$ $\frac{37}{22}$ $\frac{54}{16}$ $\frac{53}{14}$ $\frac{47}{11}$ $\frac{44}{14}$ $\frac{51}{11}$ $\frac{52}{13}$ $\frac{81}{22}$ $\frac{78}{29}$ $\frac{90}{50}$

$\frac{42}{50}$ $\frac{40}{22}$ $\frac{55}{17}$ $\frac{56}{14}$ $\frac{52}{11}$ $\frac{49}{11}$ $\frac{54}{11}$ $\frac{71}{11}$ $\frac{79}{20}$ $\frac{89}{50}$

$\frac{41}{50}$ $\frac{46}{22}$ $\frac{68}{16}$ $\frac{52}{11}$ $\frac{48}{11}$ $\frac{51}{17}$ $\frac{81}{19}$ $\frac{85}{24}$ $\frac{93}{50}$

$\frac{41}{50}$ $\frac{44}{24}$ $\frac{43}{22}$ $\frac{60}{17}$ $\frac{60}{15}$ $\frac{51}{11}$ $\frac{48}{11}$ $\frac{53}{11}$ $\frac{77}{17}$ $\frac{80}{21}$ $\frac{78}{24}$ $\frac{96}{110}$

Sta.	+	Σ	-	Elev.
		925.17		
52 +50				20.8
53				20.8
+50				20.7
54				20.5
B.M.	6.87	924.97	2.07	918.10
+50				20.4
55				20.4
+50				20.5
+70				20.7
56				20.9
+50				21.5
57				22.3
+50				23.1

11.

12.

13.

$\frac{41}{50}$ $\frac{37}{23}$ $\frac{57}{18}$ $\frac{57}{16}$ $\frac{50}{13}$ $\frac{44}{9}$ $\frac{50}{9}$ $\frac{67}{17}$ $\frac{85}{50}$

$\frac{37}{50}$ $\frac{37}{33}$ $\frac{33}{22}$ $\frac{54}{18}$ $\frac{54}{16}$ $\frac{47}{14}$ $\frac{44}{11}$ $\frac{50}{4}$ $\frac{72}{25}$ $\frac{79}{50}$

$\frac{41}{50}$ $\frac{41}{34}$ $\frac{34}{29}$ $\frac{35}{22}$ $\frac{47}{18}$ $\frac{51}{15}$ $\frac{45}{11}$ $\frac{49}{11}$ $\frac{65}{22}$ $\frac{72}{33}$ $\frac{75}{50}$

$\frac{42}{50}$ $\frac{46}{33}$ $\frac{40}{23}$ $\frac{59}{18}$ $\frac{59}{16}$ $\frac{51}{13}$ $\frac{47}{10}$ $\frac{53}{10}$ $\frac{61}{16}$ $\frac{67}{19}$ $\frac{68}{23}$ $\frac{65}{24}$ $\frac{73}{50}$

N.W. Cor. of lower conc. step 60' R + 51/2 53 + 60

$\frac{45}{50}$ $\frac{51}{22}$ $\frac{60}{18}$ $\frac{61}{13}$ $\frac{46}{11}$ $\frac{52}{11}$ $\frac{71}{19}$ $\frac{64}{25}$ $\frac{72}{31}$ $\frac{66}{39}$ $\frac{66}{50}$

$\frac{53}{50}$ $\frac{53}{33}$ $\frac{56}{30}$ $\frac{58}{17}$ $\frac{50}{13}$ $\frac{46}{10}$ $\frac{51}{10}$ $\frac{57}{50}$ —

$\frac{54}{50}$ $\frac{55}{25}$ $\frac{60}{26}$ $\frac{59}{17}$ $\frac{49}{13}$ $\frac{45}{13}$ $\frac{52}{13}$ $\frac{52}{21}$ $\frac{49}{50}$

$\frac{56}{50}$ $\frac{60}{36}$ $\frac{59}{19}$ $\frac{48}{13}$ $\frac{43}{10}$ $\frac{50}{10}$ $\frac{53}{14}$ $\frac{61}{20}$ $\frac{56}{25}$ $\frac{56}{50}$

$\frac{54}{50}$ $\frac{61}{36}$ $\frac{59}{21}$ $\frac{47}{13}$ $\frac{41}{10}$ $\frac{46}{10}$ $\frac{58}{17}$ $\frac{57}{19}$ $\frac{50}{24}$ $\frac{45}{50}$

$\frac{39}{50}$ $\frac{40}{37}$ $\frac{41}{24}$ $\frac{42}{14}$ $\frac{35}{11}$ $\frac{40}{9}$ $\frac{46}{16}$ $\frac{44}{19}$ $\frac{36}{24}$ $\frac{30}{50}$

$\frac{27}{50}$ $\frac{20}{41}$ $\frac{27}{27}$ $\frac{31}{23}$ $\frac{38}{20}$ $\frac{34}{14}$ $\frac{27}{10}$ $\frac{31}{10}$ $\frac{31}{28}$ $\frac{19}{50}$

$\frac{10}{50}$ $\frac{12}{29}$ $\frac{27}{24}$ $\frac{23}{13}$ $\frac{19}{11}$ $\frac{24}{11}$ $\frac{26}{19}$ $\frac{11}{24}$ $\frac{01}{50}$

Sta.	+	π	-	Elev.
		924.97		
T.P.	6.16	929.35	1.78	923.19
58				23.7
+50				24.4
59				24.6
+22				24.6
+37				24.6
+60				24.7
60				25.2
+50				25.4
61				25.4
+50				25.3
W				25.1
B.M.	4.32	930.20	3.47	925.88

27.

2

84

$\frac{48}{50}$ $\frac{50}{31}$ $\frac{51}{24}$ $\frac{62}{21}$ $\frac{63}{14}$ $\frac{57}{21}$ $\frac{61}{8}$ $\frac{66}{14}$ $\frac{61}{19}$ $\frac{60}{23}$ $\frac{54}{28}$ $\frac{48}{50}$

$\frac{52}{50}$ $\frac{53}{33}$ $\frac{54}{23}$ $\frac{58}{21}$ $\frac{58}{12}$ $\frac{50}{21}$ $\frac{56}{9}$ $\frac{61}{17}$ $\frac{56}{22}$ $\frac{57}{50}$

$\frac{49}{50}$ $\frac{51}{31}$ $\frac{54}{23}$ $\frac{59}{20}$ $\frac{54}{13}$ $\frac{48}{21}$ $\frac{52}{9}$ $\frac{56}{14}$ $\frac{52}{22}$ $\frac{55}{50}$

$\frac{50}{50}$ $\frac{49}{31}$ $\frac{50}{24}$ $\frac{58}{21}$ $\frac{55}{14}$ $\frac{48}{21}$ $\frac{52}{9}$ $\frac{53}{13}$ $\frac{44}{18}$ $\frac{21}{35}$ $\frac{17}{44}$ $\frac{29}{50}$

$\frac{52}{50}$ $\frac{49}{33}$ $\frac{50}{24}$ $\frac{57}{20}$ $\frac{53}{13}$ $\frac{48}{21}$ $\frac{53}{9}$ $\frac{54}{14}$ $\frac{47}{19}$ $\frac{40}{37}$ $\frac{46}{50}$

$\frac{51}{50}$ $\frac{48}{33}$ $\frac{54}{27}$ $\frac{51}{13}$ $\frac{47}{21}$ $\frac{50}{10}$ $\frac{54}{13}$ $\frac{45}{19}$ $\frac{52}{36}$ $\frac{48}{50}$

$\frac{48}{50}$ $\frac{50}{28}$ $\frac{52}{20}$ $\frac{48}{14}$ $\frac{42}{21}$ $\frac{47}{8}$ $\frac{50}{27}$ $\frac{48}{50}$

$\frac{45}{50}$ $\frac{46}{44}$ $\frac{49}{28}$ $\frac{47}{13}$ $\frac{41}{6}$ $\frac{40}{21}$ $\frac{45}{10}$ $\frac{45}{19}$ $\frac{40}{50}$

$\frac{45}{50}$ $\frac{49}{28}$ $\frac{47}{14}$ $\frac{41}{7}$ $\frac{40}{21}$ $\frac{44}{9}$ $\frac{49}{21}$ $\frac{44}{48}$ $\frac{43}{50}$

$\frac{42}{50}$ $\frac{45}{27}$ $\frac{46}{17}$ $\frac{42}{6}$ $\frac{41}{21}$ $\frac{45}{11}$ $\frac{42}{22}$ $\frac{35}{33}$ $\frac{45}{42}$ $\frac{46}{50}$

$\frac{46}{50}$ $\frac{48}{20}$ $\frac{50}{11}$ $\frac{46}{10}$ $\frac{43}{21}$ $\frac{44}{10}$ $\frac{50}{27}$ $\frac{34}{41}$ $\frac{38}{50}$

Spike in Guy pole N. in Cor. Laboret + "D"

Sta. + π - Elev.

930.20

62+17 2" D" 24.9

+50 24.9

63 25.2

+50 25.4

64 25.4

+50 25.3

65 25.5

+50 25.6

66 25.8

+50 25.6

67 25.6

+50 25.6

24.

2

14.

14

$$\frac{58}{50}$$

$$\frac{53}{50}$$

$$\frac{53}{50}$$

$$\frac{61}{50}$$

$$\frac{63}{20}$$

$$\frac{58}{15}$$

$$\frac{53}{50}$$

$$\frac{54}{5}$$

$$\frac{59}{19}$$

$$\frac{54}{21}$$

$$\frac{54}{50}$$

$$\frac{58}{50}$$

$$\frac{62}{24}$$

$$\frac{62}{17}$$

$$\frac{55}{10}$$

$$\frac{50}{50}$$

$$\frac{53}{10}$$

$$\frac{58}{17}$$

$$\frac{56}{18}$$

$$\frac{50}{24}$$

$$\frac{57}{26}$$

$$\frac{54}{50}$$

$$\frac{62}{50}$$

$$\frac{62}{34}$$

$$\frac{54}{30}$$

$$\frac{55}{20}$$

$$\frac{48}{50}$$

$$\frac{55}{17}$$

$$\frac{48}{22}$$

$$\frac{53}{24}$$

$$\frac{53}{50}$$

$$\frac{62}{50}$$

$$\frac{62}{34}$$

$$\frac{52}{21}$$

$$\frac{56}{19}$$

$$\frac{56}{14}$$

$$\frac{52}{11}$$

$$\frac{48}{50}$$

$$\frac{52}{16}$$

$$\frac{45}{20}$$

$$\frac{50}{23}$$

$$\frac{51}{50}$$

$$\frac{56}{50}$$

$$\frac{53}{11}$$

$$\frac{49}{50}$$

$$\frac{49}{15}$$

$$\frac{47}{50}$$

$$\frac{56}{50}$$

$$\frac{46}{20}$$

$$\frac{50}{10}$$

$$\frac{47}{50}$$

$$\frac{52}{12}$$

$$\frac{51}{22}$$

$$\frac{46}{50}$$

$$\frac{60}{50}$$

$$\frac{54}{34}$$

$$\frac{45}{21}$$

$$\frac{49}{14}$$

$$\frac{46}{50}$$

$$\frac{53}{16}$$

$$\frac{54}{19}$$

$$\frac{50}{22}$$

$$\frac{43}{50}$$

$$\frac{57}{50}$$

$$\frac{54}{37}$$

$$\frac{48}{30}$$

$$\frac{47}{18}$$

$$\frac{50}{14}$$

$$\frac{44}{50}$$

$$\frac{52}{19}$$

$$\frac{46}{28}$$

$$\frac{42}{50}$$

$$\frac{58}{50}$$

$$\frac{54}{35}$$

$$\frac{47}{31}$$

$$\frac{51}{17}$$

$$\frac{46}{50}$$

$$\frac{50}{11}$$

$$\frac{52}{11}$$

$$\frac{50}{22}$$

$$\frac{49}{50}$$

$$\frac{56}{50}$$

$$\frac{53}{36}$$

$$\frac{48}{27}$$

$$\frac{52}{15}$$

$$\frac{46}{50}$$

$$\frac{49}{11}$$

$$\frac{53}{14}$$

$$\frac{50}{21}$$

$$\frac{49}{50}$$

$$\frac{57}{50}$$

$$\frac{54}{37}$$

$$\frac{46}{28}$$

$$\frac{51}{15}$$

$$\frac{46}{50}$$

$$\frac{48}{14}$$

$$\frac{51}{17}$$

$$\frac{48}{33}$$

$$\frac{47}{50}$$

Sta	+	T	-	Elev.
		930.20		25.7
68				25.7
T.P.	5.91	931.42	4.69	925.51
+50				25.8
69				25.9
+50				25.9
70				25.9
+50				26.1
71				26.1
+50				26.2
72				26.4
+50				26.6
B.M.	3.81	931.42	3.81	927.61
73				26.7
+50				26.5

41.

42

41.

$$\frac{55}{50} \quad \frac{47}{27} \quad \frac{48}{19} \quad \frac{50}{14} \quad \frac{45}{11} \quad \frac{48}{19} \quad \frac{50}{24} \quad \frac{47}{24} \quad \frac{46}{50}$$

$$\frac{65}{50} \quad \frac{61}{36} \quad \frac{57}{27} \quad \frac{61}{16} \quad \frac{56}{14} \quad \frac{60}{20} \quad \frac{56}{20} \quad \frac{57}{50}$$

$$\frac{60}{50} \quad \frac{59}{31} \quad \frac{61}{16} \quad \frac{55}{11} \quad \frac{58}{17} \quad \frac{57}{22} \quad \frac{55}{22} \quad \frac{55}{50}$$

$$\frac{63}{50} \quad \frac{61}{23} \quad \frac{62}{15} \quad \frac{55}{17} \quad \frac{59}{23} \quad \frac{54}{23} \quad \frac{54}{50}$$

$$\frac{59}{50} \quad \frac{59}{23} \quad \frac{65}{17} \quad \frac{60}{10} \quad \frac{55}{18} \quad \frac{57}{22} \quad \frac{54}{22} \quad \frac{54}{50}$$

$$\frac{49}{42} \quad \frac{58}{26} \quad \frac{60}{18} \quad \frac{58}{10} \quad \frac{53}{10} \quad \frac{56}{10} \quad \frac{53}{23} \quad \frac{53}{50}$$

$$\frac{58}{50} \quad \frac{59}{19} \quad \frac{56}{10} \quad \frac{53}{8} \quad \frac{56}{11} \quad \frac{57}{17} \quad \frac{51}{23} \quad \frac{51}{50}$$

$$\frac{64}{50} \quad \frac{53}{17} \quad \frac{54}{10} \quad \frac{52}{10} \quad \frac{55}{10} \quad \frac{51}{24} \quad \frac{49}{50}$$

$$\frac{65}{50} \quad \frac{52}{13} \quad \frac{53}{10} \quad \frac{50}{11} \quad \frac{52}{15} \quad \frac{46}{26} \quad \frac{44}{26} \quad \frac{46}{50}$$

$$\frac{58}{50} \quad \frac{53}{21} \quad \frac{52}{10} \quad \frac{48}{10} \quad \frac{51}{18} \quad \frac{42}{31} \quad \frac{45}{31} \quad \frac{45}{50}$$

S.E. Cor. Floor of House 60' 61' 51 72 150

$$\frac{60}{50} \quad \frac{55}{27} \quad \frac{50}{11} \quad \frac{47}{11} \quad \frac{48}{11} \quad \frac{43}{11} \quad \frac{49}{20}$$

$$\frac{54}{50} \quad \frac{50}{29} \quad \frac{51}{11} \quad \frac{49}{11} \quad \frac{53}{10} \quad \frac{45}{13} \quad \frac{56}{50}$$

Sta.	+	π	-	Elev.
------	---	-------	---	-------

931.44

74				26.1
----	--	--	--	------

+50				25.8
-----	--	--	--	------

~~25~~

75				25.4
----	--	--	--	------

T.P.	4.01	928.70	6.73	924.69
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+50				24.9
-----	--	--	--	------

76				24.4
----	--	--	--	------

+50				24.0
-----	--	--	--	------

77				23.7
----	--	--	--	------

+50				23.7
-----	--	--	--	------

78				23.2
----	--	--	--	------

+50				23.6
-----	--	--	--	------

79				23.4
----	--	--	--	------

+50				23.3
-----	--	--	--	------

Lt.

E

Rt.

16

$$\frac{52}{50} \quad \frac{49}{34} \quad \frac{49}{14} \quad \frac{55}{9} \quad \frac{53}{\cancel{5}} \quad \frac{55}{10} \quad \frac{54}{11} \quad \frac{54}{22} \quad \frac{64}{50}$$

$$\frac{50}{50} \quad \frac{43}{31} \quad \frac{44}{19} \quad \frac{60}{11} \quad \frac{56}{\cancel{5}} \quad \frac{59}{10} \quad \frac{60}{21} \quad \frac{65}{50}$$

$$\frac{54}{50} \quad \frac{50}{22} \quad \frac{65}{15} \quad \frac{60}{\cancel{5}} \quad \frac{62}{8} \quad \frac{66}{23} \quad \frac{73}{50}$$

$$\frac{36}{50} \quad \frac{34}{22} \quad \frac{44}{17} \quad \frac{44}{13} \quad \frac{38}{\cancel{4}} \quad \frac{43}{12} \quad \frac{42}{19} \quad \frac{47}{50}$$

$$\frac{36}{50} \quad \frac{35}{22} \quad \frac{47}{17} \quad \frac{49}{11} \quad \frac{43}{\cancel{4}} \quad \frac{49}{18} \quad \frac{51}{50}$$

$$\frac{42}{50} \quad \frac{46}{29} \quad \frac{43}{21} \quad \frac{51}{15} \quad \frac{47}{\cancel{4}} \quad \frac{49}{10} \quad \frac{50}{14} \quad \frac{48}{27} \quad \frac{56}{50}$$

$$\frac{38}{50} \quad \frac{45}{22} \quad \frac{51}{17} \quad \frac{50}{\cancel{5}} \quad \frac{50}{10} \quad \frac{59}{50}$$

$$\frac{37}{50} \quad \frac{47}{22} \quad \frac{55}{18} \quad \frac{50}{\cancel{5}} \quad \frac{52}{10} \quad \frac{55}{17} \quad \frac{52}{19} \quad \frac{62}{38} \quad \frac{63}{50}$$

$$\frac{43}{50} \quad \frac{47}{31} \quad \frac{54}{17} \quad \frac{53}{11} \quad \frac{49}{\cancel{4}} \quad \frac{52}{11} \quad \frac{56}{21} \quad \frac{65}{50}$$

$$\frac{41}{50} \quad \frac{45}{20} \quad \frac{54}{11} \quad \frac{51}{\cancel{5}} \quad \frac{55}{10} \quad \frac{52}{18} \quad \frac{58}{22} \quad \frac{67}{38} \quad \frac{66}{50}$$

$$\frac{43}{50} \quad \frac{52}{17} \quad \frac{55}{9} \quad \frac{53}{\cancel{5}} \quad \frac{57}{10} \quad \frac{63}{21} \quad \frac{66}{38} \quad \frac{65}{50}$$

$$\frac{45}{50} \quad \frac{56}{28} \quad \frac{57}{11} \quad \frac{54}{\cancel{5}} \quad \frac{57}{10} \quad \frac{68}{13} \quad \frac{68}{33} \quad \frac{68}{50}$$

Sta.	+	π	-	Elev.
		928.70		
80				23.4
+50				23.4
81				23.4
+50				23.4
82				23.3
T.P.	5.65	928.59	5.76	922.94
+50				23.3
83				23.1
+50				23.3
84				23.6
B.M.	3.33	928.59 ^{..57}	3.33	925.26
+50				23.9
85				24.1
+50				24.3

Lt.

E

Rt.

17

$\frac{49}{50}$	$\frac{56}{22}$	$\frac{60}{16}$	$\frac{58}{4}$	$\frac{53}{11}$	$\frac{57}{11}$	$\frac{57}{13}$	$\frac{66}{18}$	$\frac{71}{34}$	$\frac{68}{50}$
-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{47}{50}$	$\frac{53}{22}$	$\frac{60}{17}$	$\frac{57}{11}$	$\frac{53}{10}$	$\frac{57}{10}$	$\frac{58}{14}$	$\frac{69}{22}$	$\frac{66}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{50}{50}$	$\frac{55}{34}$	$\frac{49}{26}$	$\frac{54}{20}$	$\frac{61}{18}$	$\frac{56}{18}$	$\frac{53}{17}$	$\frac{58}{17}$	$\frac{68}{17}$	$\frac{71}{33}$	$\frac{72}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{51}{50}$	$\frac{54}{35}$	$\frac{51}{29}$	$\frac{55}{22}$	$\frac{63}{19}$	$\frac{56}{11}$	$\frac{53}{14}$	$\frac{59}{17}$	$\frac{65}{17}$	$\frac{69}{24}$	$\frac{70}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{53}{50}$	$\frac{56}{35}$	$\frac{50}{28}$	$\frac{54}{21}$	$\frac{67}{19}$	$\frac{58}{15}$	$\frac{58}{18}$	$\frac{59}{13}$	$\frac{68}{17}$	$\frac{72}{21}$	$\frac{71}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{53}{50}$	$\frac{51}{24}$	$\frac{60}{19}$	$\frac{60}{17}$	$\frac{59}{14}$	$\frac{51}{9}$	$\frac{53}{53}$	$\frac{57}{10}$	$\frac{63}{16}$	$\frac{72}{19}$	$\frac{66}{24}$	$\frac{70}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{58}{50}$	$\frac{61}{23}$	$\frac{65}{20}$	$\frac{63}{16}$	$\frac{59}{10}$	$\frac{55}{11}$	$\frac{58}{11}$	$\frac{69}{19}$	$\frac{72}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{54}{50}$	$\frac{52}{11}$	$\frac{53}{53}$	$\frac{57}{11}$	$\frac{74}{19}$	$\frac{72}{32}$	$\frac{67}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{47}{50}$	$\frac{50}{29}$	$\frac{58}{25}$	$\frac{54}{12}$	$\frac{50}{50}$	$\frac{56}{11}$	$\frac{63}{19}$	$\frac{60}{24}$	$\frac{56}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

S. En. Coy Bottom Conc Steps 50 ft Sta 84+35-

$\frac{45}{50}$	$\frac{52}{30}$	$\frac{52}{26}$	$\frac{51}{11}$	$\frac{47}{47}$	$\frac{51}{10}$	$\frac{57}{14}$	$\frac{58}{33}$	$\frac{53}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{3.9}{50}$	$\frac{4.5}{27}$	$\frac{4.9}{24}$	$\frac{4.8}{12}$	$\frac{4.5}{45}$	$\frac{4.9}{10}$	$\frac{5.2}{23}$	$\frac{5.0}{38}$	$\frac{5.0}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{4.0}{50}$	$\frac{4.3}{34}$	$\frac{4.6}{11}$	$\frac{4.3}{43}$	$\frac{4.6}{8}$	$\frac{4.8}{16}$	$\frac{4.4}{20}$	$\frac{4.8}{33}$	$\frac{5.0}{50}$
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Sta.	+	π	-	Elev.
		928.59		
86				24.6
T.P.	3.93	928.66	3.86	924.73
+50				24.7
87				24.5
+50				24.4
88				24.4
+50				24.2
89				23.8
+50				23.8
90				23.4
+50				23.0
91				22.9
+50				22.7

L.

E

R.

$$\frac{3.7}{50} \quad \frac{3.7}{34} \quad \frac{3.8}{26} \quad \frac{4.2}{11} \quad 4.0 \quad \frac{4.2}{10} \quad \frac{4.3}{50}$$

$$2 \quad 86+50$$

$$\frac{4.1}{50} \quad \frac{3.7}{39} \quad \frac{4.2}{21} \quad \frac{3.8}{27} \quad \frac{3.8}{19} \quad \frac{4.2}{9} \quad 4.0 \quad \frac{4.3}{10} \quad \frac{3.8}{20} \quad \frac{4.5}{23} \quad \frac{5.0}{50}$$

$$\frac{4.5}{50} \quad \frac{4.4}{37} \quad \frac{4.7}{28} \quad \frac{4.4}{25} \quad \frac{4.6}{9} \quad 4.7 \quad \frac{4.5}{10} \quad \frac{4.5}{20} \quad \frac{5.0}{26} \quad \frac{5.3}{50}$$

$$\frac{5.1}{50} \quad \frac{4.8}{36} \quad \frac{5.2}{27} \quad \frac{5.0}{21} \quad \frac{4.6}{9} \quad 4.3 \quad \frac{4.7}{10} \quad \frac{4.5}{21} \quad \frac{5.3}{29} \quad \frac{5.7}{50}$$

$$\frac{5.0}{50} \quad \frac{5.2}{28} \quad \frac{4.9}{20} \quad \frac{5.1}{13} \quad \frac{4.8}{9} \quad 4.3 \quad \frac{4.8}{10} \quad \frac{5.0}{15} \quad \frac{4.9}{20} \quad \frac{5.5}{27} \quad \frac{6.1}{50}$$

$$\frac{4.7}{50} \quad \frac{4.7}{26} \quad \frac{5.1}{17} \quad \frac{5.0}{10} \quad 4.5 \quad \frac{5.0}{10} \quad \frac{5.4}{21} \quad \frac{5.9}{26} \quad \frac{6.4}{41} \quad \frac{7.0}{50}$$

$$\frac{4.9}{50} \quad \frac{5.0}{27} \quad \frac{4.8}{22} \quad \frac{5.3}{11} \quad \frac{5.0}{6} \quad 4.9 \quad \frac{5.3}{9} \quad \frac{5.0}{16} \quad \frac{5.3}{21} \quad \frac{7.1}{50}$$

$$\frac{5.1}{50} \quad \frac{5.3}{8} \quad 4.9 \quad \frac{5.4}{10} \quad \frac{4.9}{20} \quad \frac{6.5}{24} \quad \frac{8.4}{39} \quad \frac{9.6}{50}$$

$$\frac{6.0}{50} \quad \frac{5.9}{15} \quad \frac{5.8}{10} \quad 5.3 \quad \frac{5.8}{10} \quad \frac{5.7}{19} \quad \frac{7.0}{23} \quad \frac{8.3}{39} \quad \frac{10.4}{50}$$

$$\frac{5.9}{50} \quad \frac{5.9}{19} \quad \frac{6.1}{9} \quad 5.7 \quad \frac{6.0}{10} \quad \frac{5.9}{19} \quad \frac{6.9}{21} \quad \frac{8.8}{39} \quad \frac{10.8}{50}$$

$$\frac{5.9}{50} \quad \frac{5.9}{16} \quad \frac{6.7}{9} \quad 5.8 \quad \frac{6.2}{10} \quad \frac{5.9}{20} \quad \frac{7.2}{22} \quad \frac{8.7}{39} \quad \frac{10.7}{50}$$

$$\frac{5.6}{50} \quad \frac{5.8}{19} \quad \frac{6.4}{9} \quad 6.0 \quad \frac{6.4}{11} \quad \frac{5.9}{20} \quad \frac{6.9}{22} \quad \frac{9.6}{39} \quad \frac{10.7}{50}$$

Sto.	+	π	-	Elev.
		928.66		
92				22.3
+50				22.1
93				21.8
B.M.	1.62	924.97	5.31	923.35
+48				21.3
+50				21.3
94				20.7
+40				20.6
+41				20.6
95				20.1
+50				19.5
96				18.7
+50				17.6

Lt.

E

Rt.

19

 $\frac{53}{50} \quad \frac{57}{22} \quad \frac{67}{8} \quad \frac{64}{6} \quad \frac{68}{10} \quad \frac{63}{13} \quad \frac{66}{19} \quad \frac{78}{22} \quad \frac{101}{39} \quad \frac{108}{50}$
 $\frac{54}{50} \quad \frac{57}{33} \quad \frac{66}{14} \quad \frac{69}{8} \quad \frac{66}{6} \quad \frac{71}{10} \quad \frac{66}{13} \quad \frac{71}{20} \quad \frac{91}{22} \quad \frac{108}{39} \quad \frac{114}{50}$
 $\frac{50}{50} \quad \frac{55}{31} \quad \frac{72}{8} \quad \frac{69}{6} \quad \frac{74}{11} \quad \frac{68}{14} \quad \frac{74}{19} \quad \frac{93}{22} \quad \frac{109}{39} \quad \frac{118}{50}$

J.N. Cor. top conc. stop 25' Lt. Sta. 821+90

 $\frac{62}{50} \quad \frac{25}{40} \quad \frac{40}{17} \quad \frac{40}{9} \quad \frac{37}{6} \quad \frac{42}{10} \quad \frac{35}{16} \quad \frac{60}{23} \quad \frac{74}{39} \quad \frac{85}{50}$
 $\frac{12}{50} \quad \frac{21}{18} \quad \frac{35}{18} \quad \frac{41}{10} \quad \frac{37}{6} \quad \frac{42}{10} \quad \frac{35}{16} \quad \frac{60}{23} \quad \frac{74}{39} \quad \frac{85}{50}$
 $\frac{16}{42} \quad \frac{17}{32} \quad \frac{23}{17} \quad \frac{41}{17} \quad \frac{46}{9} \quad \frac{43}{6} \quad \frac{48}{11} \quad \frac{43}{15} \quad \frac{48}{20} \quad \frac{66}{24} \quad \frac{73}{27} \quad \frac{84}{41} \quad \frac{86}{50}$
 $\frac{17}{50} \quad \frac{18}{23} \quad \frac{22}{17} \quad \frac{42}{17} \quad \frac{45}{8} \quad \frac{44}{6} \quad \frac{51}{10} \quad \frac{45}{14} \quad \frac{47}{19} \quad \frac{65}{23} \quad \frac{84}{40} \quad \frac{88}{50}$
 $\frac{30}{50} \quad \frac{43}{16} \quad \frac{45}{9} \quad \frac{44}{6} \quad \frac{51}{10} \quad \frac{45}{14} \quad \frac{47}{15} \quad \frac{65}{23} \quad \frac{84}{40} \quad \frac{88}{50}$
 $\frac{28}{50} \quad \frac{42}{23} \quad \frac{51}{8} \quad \frac{49}{6} \quad \frac{55}{11} \quad \frac{52}{13} \quad \frac{54}{21} \quad \frac{65}{23} \quad \frac{81}{39} \quad \frac{88}{50}$
 $\frac{37}{50} \quad \frac{52}{17} \quad \frac{54}{8} \quad \frac{55}{6} \quad \frac{61}{12} \quad \frac{56}{15} \quad \frac{59}{19} \quad \frac{70}{21} \quad \frac{82}{32} \quad \frac{88}{50}$
 $\frac{50}{50} \quad \frac{63}{26} \quad \frac{69}{23} \quad \frac{69}{18} \quad \frac{62}{10} \quad \frac{63}{6} \quad \frac{71}{13} \quad \frac{69}{15} \quad \frac{78}{19} \quad \frac{87}{39} \quad \frac{101}{50}$
 $\frac{62}{50} \quad \frac{74}{31} \quad \frac{73}{9} \quad \frac{74}{6} \quad \frac{84}{14} \quad \frac{87}{17} \quad \frac{102}{21} \quad \frac{103}{28} \quad \frac{93}{32} \quad \frac{94}{39} \quad \frac{139}{43}$
 $\frac{139}{41} \quad \frac{118}{47} \quad \frac{116}{50}$

Sta. + π - Elev.

924.97

96+63

17.4

+82=15" C.M. cross culvert

97.

16.8

+50

16.5

98

16.2

+50

15.9

T.P.

5.70

921.17

9.50

915.47

99

15.7

+50

16.0

100

16.3

+02

18" C.M. cross Culvert

T.P.

6.18

922.53

4.82

916.35

+50

16.5

101

16.5

Lt.

E

Rt.

$\frac{86}{50}$ $\frac{87}{24}$ $\frac{82}{21}$ $\frac{74}{16}$ $\frac{76}{9}$ $\frac{76}{13}$ $\frac{88}{18}$ $\frac{88}{21}$ $\frac{100}{26}$ $\frac{98}{30}$ $\frac{132}{32}$ $\frac{132}{32}$ $\frac{115}{33}$ $\frac{115}{33}$

$\frac{100}{13.0}$ **12.0**

$\frac{100}{13.8}$ **11.2**

$\frac{113}{50}$ $\frac{114}{24}$ $\frac{121}{23}$ $\frac{121}{22}$ $\frac{112}{21}$ $\frac{106}{16}$ $\frac{87}{18}$ $\frac{81}{8}$ $\frac{82}{12}$ $\frac{89}{12}$ $\frac{88}{14}$ $\frac{93}{17}$ $\frac{111}{26}$ $\frac{117}{50}$

$\frac{114}{50}$ $\frac{112}{24}$ $\frac{122}{23}$ $\frac{122}{22}$ $\frac{110}{21}$ $\frac{108}{16}$ $\frac{88}{18}$ $\frac{85}{12}$ $\frac{90}{9}$ $\frac{94}{15}$ $\frac{112}{19}$ $\frac{115}{50}$

$\frac{115}{50}$ $\frac{113}{25}$ $\frac{120}{23}$ $\frac{120}{22}$ $\frac{114}{21}$ $\frac{107}{16}$ $\frac{93}{18}$ $\frac{88}{12}$ $\frac{92}{11}$ $\frac{95}{14}$ $\frac{114}{18}$ $\frac{115}{50}$

$\frac{120}{50}$ $\frac{120}{28}$ $\frac{112}{24}$ $\frac{113}{16}$ $\frac{98}{13}$ $\frac{91}{12}$ $\frac{99}{13}$ $\frac{111}{17}$ $\frac{117}{39}$ $\frac{117}{50}$

$\frac{78}{50}$ $\frac{78}{25}$ $\frac{78}{19}$ $\frac{60}{14}$ $\frac{57}{10}$ $\frac{55}{10}$ $\frac{60}{10}$ $\frac{64}{13}$ $\frac{75}{18}$ $\frac{81}{50}$

$\frac{82}{50}$ $\frac{82}{27}$ $\frac{80}{24}$ $\frac{78}{17}$ $\frac{57}{12}$ $\frac{52}{12}$ $\frac{58}{9}$ $\frac{63}{13}$ $\frac{70}{18}$ $\frac{73}{23}$ $\frac{65}{29}$ $\frac{61}{44}$ $\frac{50}{48}$ $\frac{53}{50}$

$\frac{82}{50}$ $\frac{78}{26}$ $\frac{68}{20}$ $\frac{57}{13}$ $\frac{53}{10}$ $\frac{49}{11}$ $\frac{54}{17}$ $\frac{84}{17}$ $\frac{84}{19}$ $\frac{88}{22}$ $\frac{85}{32}$ $\frac{58}{50}$

$\frac{100}{9.4}$ **11.8**

$\frac{100}{9.9}$ **11.3**

tail in T.P. Lt. 56. 101105

$\frac{87}{50}$ $\frac{106}{43}$ $\frac{88}{36}$ $\frac{89}{30}$ $\frac{87}{17}$ $\frac{67}{11}$ $\frac{60}{11}$ $\frac{61}{11}$ $\frac{97}{20}$ $\frac{68}{26}$ $\frac{71}{28}$ $\frac{67}{36}$ $\frac{67}{50}$

$\frac{91}{50}$ $\frac{88}{30}$ $\frac{77}{23}$ $\frac{81}{15}$ $\frac{82}{16}$ $\frac{66}{11}$ $\frac{60}{11}$ $\frac{64}{13}$ $\frac{79}{20}$ $\frac{75}{25}$ $\frac{70}{50}$

Sta.	+	-	Elev.
		922.53	
101450			16.5
102			16.8
+50			17.0
103			17.4
+50			17.5
104			17.5
+50			17.5
105			17.6
+50			17.7
12" Gross Culvert			
106			18.3
+50			18.9

Lt.

E

Rt.

$\frac{52}{50}$	$\frac{88}{31}$	$\frac{81}{24}$	$\frac{80}{16}$	$\frac{64}{10}$	$\frac{60}{/}$	$\frac{65}{13}$	$\frac{75}{19}$	$\frac{72}{33}$	$\frac{70}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{88}{50}$	$\frac{73}{26}$	$\frac{72}{20}$	$\frac{77}{18}$	$\frac{77}{17}$	$\frac{60}{14}$	$\frac{57}{/}$	$\frac{61}{13}$	$\frac{68}{19}$	$\frac{63}{22}$	$\frac{56}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{76}{50}$	$\frac{66}{28}$	$\frac{63}{20}$	$\frac{69}{17}$	$\frac{69}{16}$	$\frac{57}{14}$	$\frac{55}{/}$	$\frac{57}{11}$	$\frac{65}{21}$	$\frac{57}{27}$	$\frac{49}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{73}{50}$	$\frac{64}{28}$	$\frac{62}{19}$	$\frac{63}{16}$	$\frac{55}{11}$	$\frac{51}{/}$	$\frac{53}{14}$	$\frac{59}{17}$	$\frac{48}{25}$	$\frac{44}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{74}{50}$	$\frac{65}{28}$	$\frac{65}{18}$	$\frac{65}{16}$	$\frac{59}{14}$	$\frac{55}{11}$	$\frac{50}{/}$	$\frac{53}{10}$	$\frac{53}{16}$	$\frac{60}{18}$	$\frac{42}{30}$	$\frac{37}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{78}{50}$	$\frac{66}{28}$	$\frac{64}{22}$	$\frac{68}{19}$	$\frac{56}{14}$	$\frac{50}{/}$	$\frac{54}{13}$	$\frac{68}{17}$	$\frac{66}{23}$	$\frac{55}{28}$	$\frac{52}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{80}{50}$	$\frac{66}{30}$	$\frac{63}{22}$	$\frac{69}{20}$	$\frac{69}{18}$	$\frac{58}{16}$	$\frac{53}{11}$	$\frac{50}{/}$	$\frac{64}{11}$	$\frac{69}{17}$	$\frac{60}{29}$	$\frac{57}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{76}{50}$	$\frac{67}{18}$	$\frac{63}{14}$	$\frac{49}{/}$	$\frac{55}{13}$	$\frac{65}{17}$	$\frac{65}{35}$	$\frac{60}{50}$
-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{81}{50}$	$\frac{70}{20}$	$\frac{53}{14}$	$\frac{48}{/}$	$\frac{57}{11}$	$\frac{55}{26}$	$\frac{52}{50}$
-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------

$\frac{154}{74}$ 15.1

$\frac{156}{68}$ 15.7

$\frac{82}{50}$	$\frac{74}{22}$	$\frac{60}{13}$	$\frac{42}{5}$	$\frac{42}{/}$	$\frac{47}{9}$	$\frac{57}{20}$	$\frac{50}{34}$	$\frac{49}{50}$
-----------------	-----------------	-----------------	----------------	----------------	----------------	-----------------	-----------------	-----------------

$\frac{82}{50}$	$\frac{65}{21}$	$\frac{64}{11}$	$\frac{45}{14}$	$\frac{37}{4}$	$\frac{36}{/}$	$\frac{40}{10}$	$\frac{48}{23}$	$\frac{38}{50}$
-----------------	-----------------	-----------------	-----------------	----------------	----------------	-----------------	-----------------	-----------------

Sta.	+	K	-	Elev.
		922.53		
107				19.7
+50				20.5
T.P.	9.28	922.83	1.98	920.55
B.M.	5.70	929.83	5.70	924.13
				924.13
108				21.3
+50				22.0
109				22.7
+50				23.1
110				23.8
+50				24.1
111				24.3
+35				24.3
+50				24.4

Lt.

E

Rt.

$$\frac{71}{50} \quad \frac{58}{24} \quad \frac{40}{15} \quad \frac{35}{11} \quad \frac{28}{1} \quad \frac{32}{8} \quad \frac{35}{17} \quad \frac{28}{30} \quad \frac{17}{50}$$

$$\frac{47}{50} \quad \frac{29}{19} \quad \frac{23}{10} \quad \frac{20}{1} \quad \frac{24}{10} \quad \frac{18}{27} \quad \frac{03}{44} \quad \frac{00}{50}$$

N.W. Cor. bottom step at school house

85' Rt. Sta. 107+75

$$\frac{101}{50} \quad \frac{96}{16} \quad \frac{90}{9} \quad \frac{85}{1} \quad \frac{88}{11} \quad \frac{92}{15} \quad \frac{83}{19} \quad \frac{67}{38} \quad \frac{61}{50}$$

$$\frac{81}{50} \quad \frac{77}{15} \quad \frac{84}{14} \quad \frac{78}{1} \quad \frac{78}{5} \quad \frac{82}{12} \quad \frac{81}{18} \quad \frac{70}{21} \quad \frac{58}{36} \quad \frac{55}{50}$$

$$\frac{71}{50} \quad \frac{70}{17} \quad \frac{82}{13} \quad \frac{78}{14} \quad \frac{71}{5} \quad \frac{72}{11} \quad \frac{77}{11} \quad \frac{77}{17} \quad \frac{57}{23} \quad \frac{54}{50}$$

$$\frac{62}{50} \quad \frac{66}{17} \quad \frac{78}{13} \quad \frac{73}{11} \quad \frac{67}{1} \quad \frac{71}{11} \quad \frac{75}{15} \quad \frac{54}{21} \quad \frac{50}{50}$$

$$\frac{58}{50} \quad \frac{60}{18} \quad \frac{75}{14} \quad \frac{66}{9} \quad \frac{60}{1} \quad \frac{66}{13} \quad \frac{71}{16} \quad \frac{46}{21} \quad \frac{45}{50}$$

$$\frac{56}{50} \quad \frac{54}{28} \quad \frac{58}{18} \quad \frac{63}{14} \quad \frac{73}{13} \quad \frac{61}{9} \quad \frac{57}{1} \quad \frac{63}{13} \quad \frac{69}{16} \quad \frac{40}{22} \quad \frac{44}{50}$$

$$\frac{53}{50} \quad \frac{58}{20} \quad \frac{63}{13} \quad \frac{70}{14} \quad \frac{58}{9} \quad \frac{55}{1} \quad \frac{59}{14} \quad \frac{67}{16} \quad \frac{44}{22} \quad \frac{41}{50}$$

$$\frac{49}{50} \quad \frac{58}{15} \quad \frac{69}{13} \quad \frac{69}{11} \quad \frac{57}{10} \quad \frac{56}{1} \quad \frac{58}{14} \quad \frac{57}{14} \quad \frac{60}{16} \quad \frac{40}{21} \quad \frac{46}{31} \quad \frac{53}{35} \quad \frac{43}{43} \quad \frac{43}{50}$$

$$\frac{51}{50} \quad \frac{54}{14} \quad \frac{54}{1} \quad \frac{65}{13} \quad \frac{65}{16} \quad \frac{65}{18} \quad \frac{45}{21} \quad \frac{41}{50}$$

Sta.	+	Σ	-	Elev.
		929.83		
112				25.0
+50				25.1
113				25.2
+50				25.3
T.P.	8.30	930.77	5.36	924.47
114				25.3
+50				25.3
115				25.5
+50				25.7
116				26.1
+50				26.5
117				27.0

27.

2

27

$$\frac{41}{50} \quad \frac{49}{17} \quad \frac{60}{16} \quad \frac{66}{15} \quad \frac{66}{14} \quad \frac{52}{8} \quad \frac{48}{\cancel{11}} \quad \frac{53}{11} \quad \frac{55}{14} \quad \frac{63}{15} \quad \frac{63}{17} \quad \frac{46}{21} \quad \frac{46}{50}$$

$$\frac{50}{50} \quad \frac{48}{17} \quad \frac{61}{15} \quad \frac{61}{14} \quad \frac{51}{9} \quad \frac{47}{\cancel{13}} \quad \frac{52}{13} \quad \frac{63}{15} \quad \frac{63}{17} \quad \frac{47}{20} \quad \frac{45}{50}$$

$$\frac{53}{50} \quad \frac{53}{24} \quad \frac{58}{14} \quad \frac{51}{9} \quad \frac{46}{\cancel{12}} \quad \frac{49}{12} \quad \frac{61}{15} \quad \frac{61}{17} \quad \frac{42}{20} \quad \frac{38}{50}$$

$$\frac{56}{50} \quad \frac{54}{25} \quad \frac{58}{14} \quad \frac{50}{10} \quad \frac{45}{\cancel{13}} \quad \frac{50}{13} \quad \frac{58}{15} \quad \frac{58}{17} \quad \frac{38}{21} \quad \frac{36}{50}$$

6042 6750 140 14

$$\frac{93}{50} \quad \frac{88}{13} \quad \frac{81}{11} \quad \frac{75}{\cancel{13}} \quad \frac{81}{13} \quad \frac{89}{15} \quad \frac{72}{21} \quad \frac{67}{27} \quad \frac{73}{36} \quad \frac{67}{50}$$

$$\frac{100}{50} \quad \frac{87}{14} \quad \frac{82}{11} \quad \frac{75}{\cancel{13}} \quad \frac{78}{13} \quad \frac{85}{15} \quad \frac{78}{19} \quad \frac{72}{26} \quad \frac{72}{50}$$

$$\frac{103}{50} \quad \frac{89}{14} \quad \frac{82}{11} \quad \frac{78}{\cancel{11}} \quad \frac{73}{\cancel{14}} \quad \frac{78}{14} \quad \frac{83}{11} \quad \frac{74}{25} \quad \frac{71}{50}$$

$$\frac{101}{50} \quad \frac{92}{25} \quad \frac{87}{18} \quad \frac{77}{9} \quad \frac{71}{\cancel{11}} \quad \frac{76}{11} \quad \frac{80}{11} \quad \frac{73}{20} \quad \frac{71}{37} \quad \frac{64}{50}$$

$$\frac{97}{50} \quad \frac{86}{23} \quad \frac{80}{14} \quad \frac{73}{9} \quad \frac{67}{\cancel{14}} \quad \frac{73}{14} \quad \frac{77}{15} \quad \frac{72}{18} \quad \frac{63}{50}$$

$$\frac{86}{50} \quad \frac{74}{25} \quad \frac{70}{19} \quad \frac{74}{13} \quad \frac{69}{9} \quad \frac{63}{\cancel{14}} \quad \frac{71}{14} \quad \frac{62}{17} \quad \frac{61}{31} \quad \frac{56}{50}$$

$$\frac{79}{50} \quad \frac{63}{23} \quad \frac{60}{20} \quad \frac{63}{13} \quad \frac{62}{9} \quad \frac{58}{\cancel{11}} \quad \frac{64}{11} \quad \frac{65}{13} \quad \frac{54}{17} \quad \frac{49}{28} \quad \frac{45}{50}$$

Sta.	+	π	-	Elev
		932.77		
117+35				27.5
+60				27.8
118				28.1
+50				28.7
119				29.7
T.P.	11.83	941.48	3.12	928.65
+50				30.8
120				31.7
+50				33.0
+75				34.0
121				35.0
121				35.6
B.M.	7.73	943.30	2.91	935.57
				(935.57)

44.

2

24.

$$\frac{74}{50} \quad \frac{58}{24} \quad \frac{53}{21} \quad \frac{60}{14} \quad \frac{58}{9} \quad \frac{53}{5} \quad \frac{59}{11} \quad \frac{61}{26} \quad \frac{25}{31} \quad \frac{68}{50}$$

$$\frac{67}{50} \quad \frac{53}{24} \quad \frac{47}{20} \quad \frac{56}{14} \quad \frac{54}{9} \quad \frac{50}{5} \quad \frac{55}{11} \quad \frac{62}{18} \quad \frac{61}{30} \quad \frac{83}{34} \quad \frac{88}{50}$$

$$\frac{56}{50} \quad \frac{50}{43} \quad \frac{46}{24} \quad \frac{47}{20} \quad \frac{54}{10} \quad \frac{50}{4} \quad \frac{47}{5} \quad \frac{53}{11} \quad \frac{52}{20} \quad \frac{46}{34} \quad \frac{46}{43} \quad \frac{10}{50}$$

$$\frac{42}{50} \quad \frac{47}{24} \quad \frac{49}{19} \quad \frac{44}{10} \quad \frac{41}{5} \quad \frac{48}{11} \quad \frac{50}{15} \quad \frac{45}{26} \quad \frac{15}{31} \quad \frac{14}{50}$$

$$\frac{50}{50} \quad \frac{52}{28} \quad \frac{46}{21} \quad \frac{44}{18} \quad \frac{35}{11} \quad \frac{31}{5} \quad \frac{37}{11} \quad \frac{40}{15} \quad \frac{27}{19} \quad \frac{22}{33} \quad \frac{34}{50}$$

$$\frac{127}{50} \quad \frac{122}{23} \quad \frac{121}{16} \quad \frac{112}{10} \quad \frac{107}{5} \quad \frac{110}{10} \quad \frac{113}{14} \quad \frac{104}{20} \quad \frac{58}{32} \quad \frac{55}{50}$$

$$\frac{139}{50} \quad \frac{132}{23} \quad \frac{128}{20} \quad \frac{123}{11} \quad \frac{98}{5} \quad \frac{103}{12} \quad \frac{51}{22} \quad \frac{81}{50}$$

$$\frac{129}{50} \quad \frac{120}{26} \quad \frac{98}{16} \quad \frac{81}{10} \quad \frac{85}{5} \quad \frac{86}{11} \quad \frac{88}{15} \quad \frac{82}{21} \quad \frac{63}{50}$$

$$\frac{98}{50} \quad \frac{91}{25} \quad \frac{85}{21} \quad \frac{75}{5} \quad \frac{78}{12} \quad \frac{71}{18} \quad \frac{57}{37} \quad \frac{52}{50}$$

$$\frac{74}{50} \quad \frac{68}{23} \quad \frac{61}{5} \quad \frac{68}{18} \quad \frac{51}{24} \quad \frac{47}{30} \quad \frac{41}{50}$$

$$\frac{80}{50} \quad \frac{87}{46} \quad \frac{83}{38} \quad \frac{67}{31} \quad \frac{63}{14} \quad \frac{59}{5} \quad \frac{66}{22} \quad \frac{60}{31} \quad \frac{72}{44} \quad \frac{70}{50}$$

Drill hole in pairing 2" & 4" & 6" above.

Sta. + x - Elev.

943.30

C.M.X - Culvert.

121+50 36.3

121+75 37.0

122 37.6

+50 37.9

123 38.6

+50 39.1

124 39.4

+50 39.6

125 39.4

+50 39.1

126 38.8

C.M. x Culv.

L+

L

R+

25

Inv. 34.3

$$\frac{78}{50} \quad \frac{80}{21} \quad \frac{74}{21} \quad \frac{68}{13} \quad \frac{75}{8} \quad \frac{70}{8} \quad \frac{68}{16} \quad \frac{68}{31} \quad \frac{64}{50}$$

$$\frac{95}{50} \quad \frac{73}{16} \quad \frac{68}{10} \quad \frac{63}{10} \quad \frac{62}{10} \quad \frac{64}{18} \quad \frac{64}{24} \quad \frac{25}{36} \quad \frac{5.5}{50}$$

$$\frac{88}{50} \quad \frac{66}{16} \quad \frac{68}{13} \quad \frac{63}{10} \quad \frac{57}{14} \quad \frac{61}{22} \quad \frac{45}{37} \quad \frac{50}{50}$$

$$\frac{82}{50} \quad \frac{61}{14} \quad \frac{56}{10} \quad \frac{54}{13} \quad \frac{53}{20} \quad \frac{56}{50}$$

$$\frac{87}{50} \quad \frac{71}{17} \quad \frac{53}{8} \quad \frac{47}{14} \quad \frac{52}{16} \quad \frac{54}{28} \quad \frac{55}{50}$$

$$\frac{83}{50} \quad \frac{60}{17} \quad \frac{48}{10} \quad \frac{42}{12} \quad \frac{45}{20} \quad \frac{43}{50}$$

$$\frac{79}{50} \quad \frac{51}{26} \quad \frac{46}{14} \quad \frac{39}{13} \quad \frac{41}{40} \quad \frac{10}{50} \quad \frac{0.7}{50}$$

$$\frac{72}{50} \quad \frac{45}{27} \quad \frac{41}{11} \quad \frac{37}{13} \quad \frac{38}{33} \quad \frac{13}{50} \quad \frac{110}{50}$$

$$\frac{58}{50} \quad \frac{38}{31} \quad \frac{35}{21} \quad \frac{50}{15} \quad \frac{50}{13} \quad \frac{43}{10} \quad \frac{39}{13} \quad \frac{40}{21} \quad \frac{35}{41} \quad \frac{25}{50}$$

$$\frac{72}{50} \quad \frac{51}{31} \quad \frac{44}{18} \quad \frac{47}{17} \quad \frac{50}{14} \quad \frac{46}{10} \quad \frac{42}{14} \quad \frac{44}{16} \quad \frac{47}{26} \quad \frac{47}{50} \quad \frac{44}{50}$$

$$\frac{72}{50} \quad \frac{72}{27} \quad \frac{66}{20} \quad \frac{63}{14} \quad \frac{49}{10} \quad \frac{46}{13} \quad \frac{48}{20} \quad \frac{50}{10}$$

Inv. 36.1

Inv. 36.7

Sta.	+	π	-	Elev.
		943.30		
126+50				38.7
T.P.	11.75	950.87	4.18	939.12
127				39.2
+50				39.9
128				40.5
+50				40.7
129				40.3
+50				39.8
130				39.2
T.P.	0.61	944.04	7.44	943.43
+50				38.8
131				38.8
+50				38.8
132				38.2

L.

E

R.

$$\frac{98}{50} \quad \frac{92}{35} \quad \frac{82}{21} \quad \frac{68}{13} \quad \frac{52}{10} \quad \frac{46}{13} \quad \frac{46}{21} \quad \frac{44}{50}$$

$$\frac{169}{50} \quad \frac{137}{37} \quad \frac{149}{21} \quad \frac{134}{16} \quad \frac{124}{12} \quad \frac{117}{13} \quad \frac{119}{27} \quad \frac{112}{50}$$

$$\frac{164}{50} \quad \frac{146}{27} \quad \frac{133}{20} \quad \frac{129}{16} \quad \frac{128}{13} \quad \frac{110}{11} \quad \frac{110}{14} \quad \frac{92}{29} \quad \frac{74}{50}$$

$$\frac{148}{50} \quad \frac{133}{24} \quad \frac{115}{19} \quad \frac{110}{14} \quad \frac{104}{10} \quad \frac{105}{14} \quad \frac{105}{25} \quad \frac{64}{42} \quad \frac{40}{50} \quad \frac{33}{50}$$

$$\frac{134}{50} \quad \frac{108}{21} \quad \frac{100}{17} \quad \frac{110}{13} \quad \frac{102}{9} \quad \frac{105}{16} \quad \frac{103}{20} \quad \frac{94}{23} \quad \frac{60}{30} \quad \frac{43}{31} \quad \frac{30}{42}$$

$$\frac{133}{50} \quad \frac{118}{37} \quad \frac{101}{18} \quad \frac{113}{16} \quad \frac{114}{13} \quad \frac{106}{11} \quad \frac{107}{15} \quad \frac{111}{18} \quad \frac{107}{24} \quad \frac{95}{31} \quad \frac{43}{32} \quad \frac{32}{38}$$

$$\frac{144}{50} \quad \frac{123}{27} \quad \frac{117}{16} \quad \frac{117}{13} \quad \frac{120}{11} \quad \frac{111}{12} \quad \frac{114}{17} \quad \frac{121}{25} \quad \frac{111}{31} \quad \frac{66}{38} \quad \frac{60}{39} \quad \frac{63}{50}$$

$$\frac{168}{50} \quad \frac{160}{33} \quad \frac{140}{16} \quad \frac{126}{12} \quad \frac{117}{11} \quad \frac{116}{18} \quad \frac{118}{22} \quad \frac{115}{25} \quad \frac{101}{32} \quad \frac{88}{32} \quad \frac{81}{36}$$

Boulder R.

$$\frac{98}{50} \quad \frac{94}{34} \quad \frac{85}{16} \quad \frac{60}{11} \quad \frac{52}{14} \quad \frac{51}{17} \quad \frac{47}{24} \quad \frac{13}{36} \quad \frac{14}{43} \quad \frac{12}{50}$$

$$\frac{21}{50} \quad \frac{34}{25} \quad \frac{51}{19} \quad \frac{51}{14} \quad \frac{52}{11} \quad \frac{58}{15} \quad \frac{71}{27} \quad \frac{76}{27} \quad \frac{92}{50}$$

$$\frac{79}{50} \quad \frac{64}{30} \quad \frac{60}{14} \quad \frac{56}{10} \quad \frac{52}{14} \quad \frac{53}{16} \quad \frac{36}{22} \quad \frac{21}{40} \quad \frac{29}{50}$$

$$\frac{74}{50} \quad \frac{68}{33} \quad \frac{62}{11} \quad \frac{58}{11} \quad \frac{60}{15} \quad \frac{63}{17} \quad \frac{44}{22} \quad \frac{31}{50}$$

Sta.	+	π	-	Elev.
		944.04		
132+50				37.7
133				37.4
150				37.3
134				37.5
150				37.6
135				37.4
B.M.	2.37	943.11	2.30	940.74 (940.74)
150				37.3
136				36.9
150				36.3
137				35.5
150				34.3
138				33.1

Lt.

Ct.

Ct.

$$\frac{100}{50} \quad \frac{81}{15} \quad \frac{73}{13} \quad \frac{66}{9} \quad \frac{63}{1} \quad \frac{65}{15} \quad \frac{60}{16} \quad \frac{52}{30} \quad \frac{44}{50}$$

$$\frac{112}{50} \quad \frac{93}{17} \quad \frac{76}{13} \quad \frac{68}{9} \quad \frac{66}{1} \quad \frac{66}{14} \quad \frac{60}{16} \quad \frac{52}{30} \quad \frac{51}{50}$$

$$\frac{113}{50} \quad \frac{90}{30} \quad \frac{80}{15} \quad \frac{74}{13} \quad \frac{69}{10} \quad \frac{67}{1} \quad \frac{67}{14} \quad \frac{63}{15} \quad \frac{51}{31} \quad \frac{50}{50}$$

$$\frac{102}{50} \quad \frac{83}{26} \quad \frac{70}{10} \quad \frac{65}{1} \quad \frac{66}{13} \quad \frac{68}{20} \quad \frac{66}{26} \quad \frac{58}{31} \quad \frac{49}{50}$$

$$\frac{95}{50} \quad \frac{75}{16} \quad \frac{70}{11} \quad \frac{64}{1} \quad \frac{66}{12} \quad \frac{66}{22} \quad \frac{52}{33} \quad \frac{51}{50}$$

$$\frac{98}{50} \quad \frac{87}{24} \quad \frac{73}{13} \quad \frac{66}{1} \quad \frac{65}{16} \quad \frac{62}{30} \quad \frac{55}{18}$$

Spike in 8" Poplar 80' Rt 512. 154 + 00

$$\frac{86}{50} \quad \frac{64}{12} \quad \frac{58}{1} \quad \frac{56}{11} \quad \frac{50}{24} \quad \frac{45}{39} \quad \frac{43}{50}$$

$$\frac{79}{50} \quad \frac{77}{34} \quad \frac{63}{24} \quad \frac{62}{18} \quad \frac{71}{15} \quad \frac{62}{1} \quad \frac{63}{12} \quad \frac{65}{18} \quad \frac{54}{22} \quad \frac{53}{31} \quad \frac{47}{40} \quad \frac{50}{10}$$

$$\frac{85}{50} \quad \frac{78}{29} \quad \frac{67}{22} \quad \frac{70}{18} \quad \frac{77}{15} \quad \frac{73}{12} \quad \frac{68}{1} \quad \frac{70}{13} \quad \frac{76}{19} \quad \frac{70}{25} \quad \frac{57}{27} \quad \frac{54}{39} \quad \frac{53}{50}$$

$$\frac{94}{50} \quad \frac{84}{38} \quad \frac{70}{28} \quad \frac{78}{23} \quad \frac{81}{17} \quad \frac{58}{11} \quad \frac{52}{10} \quad \frac{76}{1} \quad \frac{80}{14} \quad \frac{85}{18} \quad \frac{84}{29} \quad \frac{61}{33} \quad \frac{66}{36} \quad \frac{60}{42} \quad \frac{63}{50}$$

$$\frac{106}{50} \quad \frac{97}{27} \quad \frac{91}{21} \quad \frac{91}{16} \quad \frac{99}{14} \quad \frac{92}{9} \quad \frac{88}{1} \quad \frac{90}{16} \quad \frac{98}{26} \quad \frac{94}{32} \quad \frac{75}{37} \quad \frac{70}{41} \quad \frac{75}{50}$$

$$\frac{117}{50} \quad \frac{100}{17} \quad \frac{105}{14} \quad \frac{103}{10} \quad \frac{100}{1} \quad \frac{101}{16} \quad \frac{108}{18} \quad \frac{106}{25} \quad \frac{81}{40} \quad \frac{81}{50}$$

Sta.	+	π	-	Elev.
		943.11		
138+50				32.0
139				31.3
T.P.	2.84	933.99	11.94	931.17
+50				30.8
140				30.5
+50				30.2
141				30.1
+50				30.0
142				29.7
+50				29.3
143				28.7
+50				28.0
144				27.4

4.

2

8.

$\frac{13^3}{50}$ $\frac{12^6}{23}$ $\frac{11^9}{19}$ $\frac{11^7}{10}$ $\frac{11^1}{/}$ $\frac{11^2}{15}$ $\frac{12^0}{20}$ $\frac{10^6}{26}$ $\frac{9^6}{42}$ $\frac{10^2}{50}$

$\frac{15^4}{50}$ $\frac{13^3}{24}$ $\frac{13^1}{19}$ $\frac{12^4}{10}$ $\frac{11^8}{/}$ $\frac{12^0}{14}$ $\frac{12^0}{18}$ $\frac{11^4}{21}$ $\frac{10^4}{28}$ $\frac{10^4}{50}$

$\frac{7^0}{50}$ $\frac{5^8}{22}$ $\frac{5^0}{13}$ $\frac{3^9}{11}$ $\frac{3^2}{/}$ $\frac{3^3}{15}$ $\frac{3^8}{18}$ $\frac{3^0}{20}$ $\frac{2^0}{26}$ $\frac{2^4}{40}$ $\frac{1^7}{50}$

$\frac{7^6}{50}$ $\frac{7^2}{29}$ $\frac{6^6}{19}$ $\frac{5^4}{13}$ $\frac{4^2}{11}$ $\frac{3^5}{/}$ $\frac{3^6}{13}$ $\frac{4^1}{18}$ $\frac{3^5}{19}$ $\frac{2^7}{28}$ $\frac{3^0}{43}$ $\frac{2^3}{50}$

$\frac{7^4}{50}$ $\frac{7^1}{28}$ $\frac{5^9}{18}$ $\frac{4^4}{11}$ $\frac{3^8}{/}$ $\frac{4^1}{13}$ $\frac{4^7}{17}$ $\frac{3^8}{19}$ $\frac{3^0}{29}$ $\frac{3^4}{39}$ $\frac{2^7}{50}$

$\frac{7^3}{50}$ $\frac{6^4}{29}$ $\frac{6^9}{21}$ $\frac{5^7}{15}$ $\frac{4^5}{11}$ $\frac{3^9}{/}$ $\frac{4^2}{13}$ $\frac{4^7}{18}$ $\frac{3^5}{20}$ $\frac{3^4}{29}$ $\frac{2^0}{50}$

$\frac{7^1}{50}$ $\frac{6^1}{21}$ $\frac{5^4}{15}$ $\frac{4^6}{12}$ $\frac{4^0}{/}$ $\frac{4^4}{13}$ $\frac{5^1}{18}$ $\frac{3^8}{23}$ $\frac{3^3}{29}$ $\frac{3^0}{50}$

$\frac{6^7}{50}$ $\frac{6^0}{28}$ $\frac{6^1}{24}$ $\frac{5^8}{20}$ $\frac{5^3}{18}$ $\frac{5^6}{15}$ $\frac{4^8}{11}$ $\frac{4^3}{/}$ $\frac{4^8}{14}$ $\frac{5^2}{17}$ $\frac{3^6}{24}$ $\frac{3^4}{44}$ $\frac{3^2}{50}$

$\frac{6^8}{50}$ $\frac{5^5}{28}$ $\frac{5^2}{18}$ $\frac{5^7}{13}$ $\frac{5^4}{11}$ $\frac{4^7}{/}$ $\frac{4^9}{14}$ $\frac{5^1}{16}$ $\frac{4^2}{19}$ $\frac{3^2}{29}$ $\frac{3^7}{37}$ $\frac{3^4}{50}$

$\frac{7^5}{50}$ $\frac{6^7}{41}$ $\frac{6^5}{28}$ $\frac{7^0}{24}$ $\frac{6^0}{19}$ $\frac{6^6}{14}$ $\frac{6^0}{11}$ $\frac{5^3}{/}$ $\frac{5^5}{14}$ $\frac{5^8}{15}$ $\frac{4^1}{22}$ $\frac{3^1}{50}$

$\frac{8^1}{50}$ $\frac{7^1}{20}$ $\frac{7^4}{15}$ $\frac{6^5}{11}$ $\frac{6^0}{/}$ $\frac{6^3}{14}$ $\frac{6^1}{16}$ $\frac{5^6}{20}$ $\frac{4^8}{31}$ $\frac{5^4}{38}$ $\frac{4^1}{50}$

$\frac{9^4}{50}$ $\frac{8^1}{24}$ $\frac{7^6}{18}$ $\frac{7^1}{13}$ $\frac{7^0}{10}$ $\frac{6^6}{/}$ $\frac{6^4}{13}$ $\frac{7^2}{17}$ $\frac{6^1}{28}$ $\frac{5^8}{50}$

Sta.	+	K	-	Elev.
		933.99		
144+50				26.9
145				26.8
+50				26.6
146				26.5
+50				26.3
147				26.2
T.P.	5.85	934.01	7.83	926.16
+50				25.9
148				25.6
+50				24.9
149				24.3
T.P.	7.38	930.92	8.47	923.54
+50				23.9
150				23.4

Lt.

E

Rt.

$$\frac{95}{50} \quad \frac{96}{41} \quad \frac{81}{19} \quad \frac{83}{15} \quad \frac{75}{10} \quad \frac{71}{7} \quad \frac{73}{14} \quad \frac{69}{16} \quad \frac{66}{25} \quad \frac{62}{34} \quad \frac{60}{50}$$

$$\frac{98}{50} \quad \frac{85}{19} \quad \frac{84}{15} \quad \frac{77}{11} \quad \frac{72}{7} \quad \frac{76}{14} \quad \frac{65}{29} \quad \frac{61}{50}$$

$$\frac{98}{50} \quad \frac{83}{19} \quad \frac{79}{15} \quad \frac{80}{12} \quad \frac{74}{7} \quad \frac{77}{15} \quad \frac{66}{27} \quad \frac{59}{50}$$

$$\frac{106}{50} \quad \frac{84}{16} \quad \frac{80}{11} \quad \frac{75}{7} \quad \frac{79}{15} \quad \frac{80}{19} \quad \frac{65}{28} \quad \frac{59}{50}$$

$$\frac{109}{50} \quad \frac{85}{15} \quad \frac{82}{10} \quad \frac{77}{7} \quad \frac{80}{14} \quad \frac{79}{19} \quad \frac{64}{30} \quad \frac{60}{50}$$

$$\frac{116}{50} \quad \frac{86}{16} \quad \frac{88}{13} \quad \frac{82}{10} \quad \frac{78}{7} \quad \frac{81}{13} \quad \frac{75}{16} \quad \frac{65}{33} \quad \frac{58}{50}$$

$$\frac{97}{50} \quad \frac{68}{15} \quad \frac{64}{11} \quad \frac{61}{7} \quad \frac{64}{12} \quad \frac{60}{14} \quad \frac{60}{19} \quad \frac{47}{30} \quad \frac{41}{50}$$

$$\frac{99}{50} \quad \frac{68}{18} \quad \frac{66}{16} \quad \frac{71}{14} \quad \frac{68}{18} \quad \frac{64}{12} \quad \frac{68}{14} \quad \frac{67}{14} \quad \frac{42}{38} \quad \frac{40}{50}$$

$$\frac{102}{50} \quad \frac{90}{28} \quad \frac{84}{17} \quad \frac{76}{11} \quad \frac{71}{7} \quad \frac{73}{12} \quad \frac{68}{14} \quad \frac{41}{33} \quad \frac{36}{50}$$

$$\frac{101}{50} \quad \frac{104}{37} \quad \frac{112}{27} \quad \frac{106}{18} \quad \frac{81}{11} \quad \frac{77}{7} \quad \frac{79}{11} \quad \frac{74}{14} \quad \frac{57}{32} \quad \frac{41}{50}$$

$$\frac{97}{50} \quad \frac{88}{41} \quad \frac{83}{17} \quad \frac{73}{11} \quad \frac{70}{7} \quad \frac{71}{11} \quad \frac{63}{14} \quad \frac{45}{24} \quad \frac{40}{38} \quad \frac{39}{50}$$

$$\frac{120}{50} \quad \frac{78}{25} \quad \frac{77}{12} \quad \frac{75}{7} \quad \frac{79}{11} \quad \frac{70}{17} \quad \frac{51}{20} \quad \frac{39}{26} \quad \frac{43}{40} \quad \frac{39}{50}$$

Sta.	+	π	-	Elev.
		930.94		
150+50				22.6
151				22.1
+23				21.7
+39				21.3
+25 CM. Culvert				
+50				21.0
+78				20.4
152				19.9
+18				19.6
+26 ⁵				
NRRR.				
+37				
VTP				
+37				19.6
+50				19.6

Lt.

E

Rt.

$\frac{106}{50}$ $\frac{83}{18}$ $\frac{84}{11}$ $\frac{83}{14}$ $\frac{86}{20}$ $\frac{67}{19}$ $\frac{61}{38}$ $\frac{45}{38}$ $\frac{41}{50}$

$\frac{99}{50}$ $\frac{83}{29}$ $\frac{83}{17}$ $\frac{92}{10}$ $\frac{88}{17}$ $\frac{90}{24}$ $\frac{51}{34}$ $\frac{54}{34}$ $\frac{54}{50}$

$\frac{99}{50}$ $\frac{75}{18}$ $\frac{103}{14}$ $\frac{86}{9}$ $\frac{94}{19}$ $\frac{94}{21}$ $\frac{100}{36}$ $\frac{55}{36}$ $\frac{54}{50}$

$\frac{99}{50}$ $\frac{74}{19}$ $\frac{84}{16}$ $\frac{112}{12}$ $\frac{109}{10}$ $\frac{96}{25}$ $\frac{92}{30}$ $\frac{85}{30}$

$\frac{145}{11.0}$ **19.9**

$\frac{145}{10.3}$ **20.6**

$\frac{99}{11.0}$

$\frac{81}{50}$ t Goose Lake Rd.

$\frac{106}{50}$ $\frac{87}{18}$ $\frac{120}{13}$ $\frac{120}{11}$ $\frac{109}{9}$ $\frac{105}{16}$ $\frac{101}{16}$ $\frac{89}{34}$ $\frac{76}{43}$ $\frac{73}{50}$

$\frac{114}{50}$ $\frac{92}{34}$ $\frac{85}{23}$ $\frac{98}{18}$ $\frac{127}{15}$ $\frac{113}{13}$ $\frac{110}{11}$ $\frac{108}{14}$ $\frac{106}{25}$ $\frac{84}{33}$ $\frac{79}{50}$

$\frac{133}{50}$ $\frac{134}{19}$ $\frac{122}{19}$ $\frac{114}{8}$ $\frac{113}{11}$ $\frac{113}{9}$ $\frac{120}{16}$ $\frac{133}{16}$ $\frac{129}{50}$

Top Rail $\frac{1144}{11.44}$ **19.48**

Top Rail $\frac{11.80}{11.80}$ **19.12**

$\frac{145}{14.5}$ **16.4**

$\frac{145}{14.5}$ **16.9**

$\frac{148}{50}$ $\frac{145}{24}$ $\frac{123}{23}$ $\frac{113}{10}$ $\frac{113}{11}$ $\frac{114}{8}$ $\frac{121}{12}$ $\frac{141}{13}$ $\frac{135}{29}$ $\frac{130}{50}$

$\frac{130}{50}$ $\frac{115}{30}$ $\frac{117}{17}$ $\frac{113}{11}$ $\frac{114}{9}$ $\frac{119}{13}$ $\frac{98}{22}$ $\frac{85}{30}$ $\frac{85}{50}$

Sta.	+	π	-	Elev.
		930.94		
153	Connection left.			19.6
+50				19.5
154				19.5
B.M.	5.17	925.77	10.37	920.55
+50				19.8
155				19.9
+50				19.6
156				19.4
+50				19.0
157				18.2
+50				17.4
158				17.1

Lt.

Q

Rt.

$\frac{129}{50}$ $\frac{114}{10}$ $\frac{113}{1}$ $\frac{115}{8}$ $\frac{105}{83}$ $\frac{95}{45}$ $\frac{90}{50}$

$\frac{134}{50}$ $\frac{137}{42}$ $\frac{118}{18}$ $\frac{124}{15}$ $\frac{117}{12}$ $\frac{114}{1}$ $\frac{117}{9}$ $\frac{110}{14}$ $\frac{107}{22}$ $\frac{102}{36}$ $\frac{106}{50}$

$\frac{138}{50}$ $\frac{120}{19}$ $\frac{124}{15}$ $\frac{117}{11}$ $\frac{114}{1}$ $\frac{117}{9}$ $\frac{121}{12}$ $\frac{107}{17}$ $\frac{103}{50}$

Spike in 24" Elm 54+29-12' Rt.

$\frac{85}{50}$ $\frac{87}{41}$ $\frac{61}{18}$ $\frac{71}{15}$ $\frac{63}{12}$ $\frac{59}{1}$ $\frac{61}{10}$ $\frac{64}{13}$ $\frac{51}{19}$ $\frac{57}{23}$ $\frac{49}{50}$

$\frac{83}{50}$ $\frac{82}{39}$ $\frac{66}{19}$ $\frac{22}{13}$ $\frac{61}{10}$ $\frac{58}{1}$ $\frac{61}{10}$ $\frac{64}{13}$ $\frac{51}{20}$ $\frac{63}{26}$ $\frac{55}{50}$

$\frac{23}{80}$ $\frac{25}{39}$ $\frac{58}{15}$ $\frac{68}{12}$ $\frac{63}{10}$ $\frac{61}{1}$ $\frac{65}{13}$ $\frac{54}{16}$ $\frac{56}{26}$ $\frac{51}{50}$

$\frac{69}{50}$ $\frac{68}{38}$ $\frac{55}{17}$ $\frac{70}{10}$ $\frac{66}{8}$ $\frac{63}{1}$ $\frac{67}{15}$ $\frac{56}{20}$ $\frac{52}{26}$ $\frac{50}{50}$

$\frac{96}{81}$ $\frac{110}{49}$ $\frac{110}{46}$ $\frac{50}{37}$ $\frac{54}{17}$ $\frac{69}{13}$ $\frac{70}{9}$ $\frac{67}{1}$ $\frac{21}{13}$ $\frac{68}{17}$ $\frac{74}{18}$ $\frac{51}{23}$ $\frac{52}{50}$

P P
 $\frac{98}{57}$ $\frac{23}{36}$ $\frac{33}{32}$ $\frac{110}{27}$ $\frac{110}{25}$ $\frac{80}{18}$ $\frac{81}{10}$ $\frac{75}{1}$ $\frac{76}{12}$ $\frac{80}{18}$ $\frac{53}{22}$ $\frac{55}{50}$

P P
 $\frac{98}{37}$ $\frac{88}{17}$ $\frac{83}{1}$ $\frac{82}{12}$ $\frac{81}{16}$ $\frac{65}{21}$ $\frac{63}{28}$ $\frac{66}{50}$

P
 $\frac{87}{23}$ $\frac{85}{3}$ $\frac{86}{1}$ $\frac{87}{11}$ $\frac{93}{14}$ $\frac{74}{19}$ $\frac{70}{29}$ $\frac{78}{38}$ $\frac{78}{50}$

Sta.	+	π	-	Elev.
------	---	-------	---	-------

		925.74		
--	--	--------	--	--

158150				
--------	--	--	--	--

				16.97
--	--	--	--	-------

159				
-----	--	--	--	--

				17.10
--	--	--	--	-------

4.

5

10

$$\begin{array}{r} P \\ 25 \\ \hline 13 \end{array}$$

$$\begin{array}{r} 2P \\ 885 \\ \hline 3 \end{array}$$

$$\begin{array}{r} P \\ 275 \\ \hline \end{array}$$

$$\begin{array}{r} P \\ 835 \\ \hline 7 \end{array}$$

$$\begin{array}{r} 84 \\ \hline 13 \end{array}$$

$$\begin{array}{r} 107 \\ \hline 18 \end{array}$$

$$\begin{array}{r} 99 \\ \hline 23 \end{array}$$

$$\begin{array}{r} 80 \\ \hline 27 \end{array}$$

$$\begin{array}{r} 762 \\ \hline 37 \end{array}$$

$$\begin{array}{r} P \\ 514 \\ \hline 10 \end{array}$$

$$\begin{array}{r} P \\ 852 \\ \hline \end{array}$$

$$\begin{array}{r} P \\ 83 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 81 \\ \hline 15 \end{array}$$

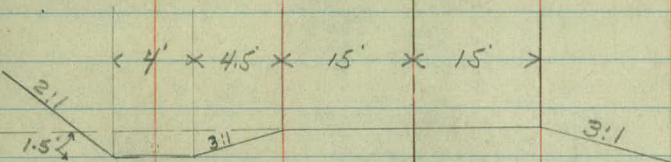
$$\begin{array}{r} 107 \\ \hline 22 \end{array}$$

$$\begin{array}{r} 104 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 84 \\ \hline 32 \end{array}$$

$$\begin{array}{r} 535 \\ \hline 41 \end{array}$$

Typical Section



Slope Stakes

La. Bore Rd.

Sta.	+	π	-	Grade
B.M.				(92.45)

92				22.1
----	--	--	--	------

	+50			21.9
--	-----	--	--	------

93				21.6
----	--	--	--	------

	+50			21.2
--	-----	--	--	------

94				20.8
----	--	--	--	------

	+50			20.3
--	-----	--	--	------

95				19.6
----	--	--	--	------

	+50			19.0
--	-----	--	--	------

96				18.4
----	--	--	--	------

	+50			17.8
--	-----	--	--	------

	+50			17.6
--	-----	--	--	------

Gr. Rod.

Lt

R

Rt

Top S.W. Cor. Conc. step. 25' Lt Sta 93490.

Sta	+	π	-	Grade	
97 S.M.	0.43	923.80		17.2	(923.35)
+50				16.7	
98				16.3	
+50				16.2	
99 S.M. T.R.	0.33 5.25	923.68 920.82	8.11	16.2 715.57	(923.35)
+50				16.4	
100				16.5	
+50				16.7	
101				16.8	
+50				17.0	
102				17.1	

Gr. Rod.

Lt.

R

Lt.

Top SW Cor. steps.

7.1

7.6

$$23.7 / \begin{array}{r} 10.5 \\ -2.9 \end{array}$$

$$\begin{array}{r} 7.7 \\ -0.1 \end{array}$$

$$\begin{array}{r} 10.3 \\ -2.7 \end{array} / 23.1$$

7.6

$$23.7 / \begin{array}{r} 10.5 \\ -2.9 \end{array}$$

$$\begin{array}{r} 8.2 \\ -0.6 \end{array}$$

$$\begin{array}{r} 10.4 \\ -2.8 \end{array} / 23.4$$

7.6

$$23.7 / \begin{array}{r} 10.4 \\ -2.8 \end{array}$$

$$\begin{array}{r} 8.2 \\ -0.6 \end{array}$$

$$\begin{array}{r} 10.6 \\ -3.0 \end{array} / 24.0$$

Top S.W. Cor. Conc. steps = 25.41 to 28.190

4.9

$$25.8 / \begin{array}{r} 7.8 \\ -2.4 \end{array}$$

$$\begin{array}{r} 5.1 \\ -0.7 \end{array}$$

$$\begin{array}{r} 7.0 \\ -2.6 \end{array} / 22.8$$

+57 Reg Proj

4.3

$$23.7 / \begin{array}{r} 7.2 \\ -2.9 \end{array}$$

$$\begin{array}{r} 7.7 \\ -0.4 \end{array}$$

$$\begin{array}{r} 5.0 \\ -2.9 \end{array} / 25.1$$

4.1

$$24.9 / \begin{array}{r} 7.4 \\ -3.3 \end{array}$$

$$\begin{array}{r} 4.9 \\ -0.3 \end{array}$$

$$\begin{array}{r} 3.1 \\ -2.0 \end{array} / 23.7$$

4.0

$$21.9 / \begin{array}{r} 6.3 \\ -2.3 \end{array}$$

$$\begin{array}{r} 4.9 \\ -0.4 \end{array}$$

$$\begin{array}{r} 6.1 \\ -2.1 \end{array} / 21.3$$

3.8

$$22.5 / \begin{array}{r} 6.3 \\ -2.5 \end{array}$$

$$\begin{array}{r} 4.5 \\ -0.7 \end{array}$$

$$\begin{array}{r} 5.7 \\ -1.9 \end{array} / 20.7$$

3.7

$$20.4 / \begin{array}{r} 5.5 \\ -1.8 \end{array}$$

$$\begin{array}{r} 4.2 \\ -0.5 \end{array}$$

$$\begin{array}{r} 4.7 \\ -2.6 \end{array} / 24.7$$

Sta	+	π	-	Grade	Lk.	Rt.
		920.82				
102	+50			17.3		
T.P.	5.01	922.10	3.53	917.29		
103				17.4		
	+50			17.6		
104				17.7		
	+50			17.9		
					4.4	2.9
105				18.1	4.4	2.9
	+50			18.3	4.5	3.4
106				18.7	4.1	2.8
	+50			19.1	3.7	2.3
107				19.5	3.3	1.9
T.P.	6.72	927.34	1.68	920.62		
	+50			20.0		
B.M.	3.19	927.32	3.19	924.15	924.13	

2 3/2
1

Gr. Rod

Lt

R

Rt

3.5

$$239 / \begin{array}{r} 48 \\ 20.2 \end{array}$$

$$\begin{array}{r} 38 \\ -0.3 \end{array}$$

$$\begin{array}{r} 39 \\ 20.11 / 25.7 \end{array}$$

4.9

$$241 / \begin{array}{r} 61 \\ 20.3 \end{array}$$

$$\begin{array}{r} 50 \\ -0.1 \end{array}$$

$$\begin{array}{r} 4.9 \\ 20.5 / 27.5 \end{array}$$

4.7

$$225 / \begin{array}{r} 62 \\ 20.0 \end{array}$$

$$\begin{array}{r} 47 \\ -0.1 \end{array}$$

$$\begin{array}{r} 43 \\ 20.6 / 27.5 \end{array}$$

4.6

$$236 / \begin{array}{r} 61 \\ 20.0 \end{array}$$

$$\begin{array}{r} 49 \\ -0.3 \end{array}$$

$$\begin{array}{r} 6.1 \\ 20.0 / 23.5 \end{array}$$

4.4

$$235 / \begin{array}{r} 53 \\ 20.0 \end{array}$$

$$\begin{array}{r} 48 \\ -0.4 \end{array}$$

$$\begin{array}{r} 6.7 \\ -23 / 21.9 \end{array}$$

4.2

$$219 / \begin{array}{r} 67 \\ -2.3 \end{array}$$

$$\begin{array}{r} 46 \\ -0.4 \end{array}$$

$$\begin{array}{r} 63 \\ -2.9 / 22.2 \end{array}$$

24.4

4.0

$$219 / \begin{array}{r} 68 \\ -2.3 \end{array}$$

$$\begin{array}{r} 46 \\ -0.6 \end{array}$$

$$\begin{array}{r} 52 \\ 20.3 / 25.9 \end{array}$$

25.3

3.6

$$255 / \begin{array}{r} 76 \\ -25 \end{array}$$

$$\begin{array}{r} 40 \\ -0.9 \end{array}$$

$$\begin{array}{r} 59 \\ -26 / 22.8 \end{array}$$

25.9

3.2

$$243 / \begin{array}{r} 68 \\ -3.1 \end{array}$$

$$\begin{array}{r} 34 \\ -0.2 \end{array}$$

$$\begin{array}{r} 44 \\ 20.3 / 21.8 \end{array}$$

26.2

2.8

$$125 / \begin{array}{r} 48 \\ -1.5 \end{array}$$

$$\begin{array}{r} 26 \\ +0.2 \end{array}$$

$$\begin{array}{r} 28 \\ 20.1 / 29.9 \end{array}$$

26.2

1.3

$$228 / \begin{array}{r} 72 \\ 20.9 \end{array}$$

$$\begin{array}{r} 67 \\ 10.6 \end{array}$$

$$\begin{array}{r} 63 \\ 20.0 / 31.2 \end{array}$$

26.2

Top N.W. Cor. Baltimore School

Sta	+	π	-	Grade	
		927.32			
108				20.4	
	+50			20.9	4.9 5.3
109				21.3	6.5 5.1
	+50			21.8	
110				22.2	
	+50			22.7	
111				23.1	
	+35			23.4	
	+50			23.6	
112				24.0	
T.P.	4.93	927.94	2.31	925.01	
	+50			24.3	

Gr. Rod.

L_tL_cR_tR_{0.0}

6.9 22.0

 $25.4 / 10.2$ $\frac{60}{+8.9}$ $\frac{95}{+24/33.0}$

26.2

-0.6
+0.9

6.4 22.0

 $27.6 / 5.1$ $\frac{53}{+1.1}$ $\frac{34}{+3.0/33.0}$

(1.1)

26.2

-0.6
+0.9

6.0 22.0

 $28.4 / 4.8$ $\frac{46}{+1.4}$ $\frac{6.9}{+3.1/33.0}$

26.2

-0.6
+0.8

5.5 22.0

 $28.9 / 3.8$ $\frac{42}{+1.3}$ $\frac{25}{+3.0/32.0}$

25.9

+0.5
-0.5

5.1 22.0

 $28.8 / 3.2$ $\frac{35}{+1.6}$ $\frac{23}{+2.8/33.0}$

25.0

-0.2
+0.2

4.6 22.0

 $29.3 / 2.9$ $\frac{32}{+1.9}$ $\frac{22}{+2.9/31.9}$

24.1

4.2

 $28.9 / 3.0$ $\frac{30}{+1.2}$ $\frac{17}{+2.5/31.5}$

3.9

 $29.3 / 2.5$ $\frac{29}{+1.0}$ $\frac{17}{+2.0/30.5}$

3.7

3.3

 $28.1 / 2.2$ $\frac{23}{+1.0}$ $\frac{19}{+1.9/29.3}$

3.6

 $28.1 / 1.8$ $\frac{49}{+0.1}$ $\frac{45}{+1.1/28.7}$

Sta	T	A	-	Grade	spec. pitch Lt.
170		928.99	1		24.2
113				24.6	5.8 24.1
+50				24.9	5.9 24.0
T.P.	652	931.55	4.91	925.03	
114				25.2	7.7 23.9
+50				25.4	
115				25.6	
+50				25.8	
116				26.0	
+50				26.4	
117				26.9	
+35				27.4	
+60				27.7	

Gr. Rod

Lt.

K

Rt.

5.3

22.5

$$22.1 / \frac{5.5}{R0.3}$$

$$\frac{4.8}{F9.5}$$

$$\frac{4.2}{+1.1/26.7}$$

5.0

21.7

$$22.3 / \frac{5.6}{R0.3}$$

$$\frac{4.7}{F0.3}$$

$$\frac{4.8}{+1.2/28.9}$$

Nail in T.C.Lt.

6.4

22.9

$$23.1 / \frac{7.6}{R0.1}$$

$$\frac{6.3}{F0.1}$$

$$\frac{5.7}{+0.7/27.9}$$

6.2

$$19.8 / \frac{7.8}{-1.6}$$

$$\frac{6.3}{-0.1}$$

$$\frac{6.0}{F0.2/26.9}$$

6.0

$$21.3 / \frac{8.1}{-2.1}$$

$$\frac{6.1}{-0.1}$$

$$\frac{6.2}{R0.13/26.1}$$

5.8

$$20.1 / \frac{7.5}{-1.7}$$

$$\frac{5.9}{-0.7}$$

$$\frac{5.9}{R1.19/26.3}$$

5.6

$$22.3 / \frac{7.1}{R0.0}$$

$$\frac{5.5}{F0.1}$$

$$\frac{5.6}{F0.9/26.5}$$

5.2

$$24.3 / \frac{6.3}{R0.4}$$

$$\frac{5.1}{F0.1}$$

$$\frac{4.9}{F0.3/27.1}$$

4.7

$$25.5 / \frac{5.2}{R1.0}$$

$$\frac{4.6}{+0.1}$$

$$\frac{3.7}{+1.0/28.5}$$

4.2

$$25.7 / \frac{4.6}{R1.1}$$

$$\frac{4.1}{+0.1}$$

$$\frac{4.3}{R0.28/25.1}$$

3.9

$$26.3 / \frac{4.0}{R1.4}$$

$$\frac{3.7}{F0.2}$$

$$\frac{3.2}{R0.2/23.9}$$

Sta.	+	π	-	Grade
		931.55		

118				28.3
-----	--	--	--	------

+50				29.2
-----	--	--	--	------

119				30.2
-----	--	--	--	------

T.P.	12.07	941.72	1.90	929.65
+50				31.4

120				32.6
-----	--	--	--	------

+50				33.8
-----	--	--	--	------

+75				34.4
-----	--	--	--	------

121				35.0
-----	--	--	--	------

B.M.	7.50	943.01	6.15	935.51	(935.57)
+25				35.6	

+50				36.1
-----	--	--	--	------

+70				36.5
-----	--	--	--	------

Gr. Rod.

Lt

4

Rt

2.3

$$259 / \frac{46}{27.2}$$

$$\frac{14}{-0.1}$$

$$\frac{44}{27.2} / 24.3$$

2.4

$$243 / \frac{35}{20.9}$$

$$\frac{2.9}{-0.5}$$

$$\frac{36}{27.2} / 24.1$$

1.4

$$207 / \frac{3.3}{-1.9}$$

$$\frac{1.9}{-1.5}$$

$$\frac{12}{20.2} / 26.9$$

10.3

$$219 / \frac{126}{-26}$$

$$\frac{11.0}{-0.7}$$

$$\frac{10.1}{20.2} / 26.9$$

9.1

$$27.4 / \frac{12.9}{-9.8}$$

$$\frac{10.0}{-0.9}$$

$$\frac{9.4}{27.2} / 25.9$$

1.7

$$26.4 / \frac{11.7}{-3.8}$$

$$\frac{8.5}{-0.9}$$

$$\frac{8.2}{27.2} / 25.9$$

7.3

$$\frac{7.5}{-0.5}$$

$$\frac{6.9}{20.4} / 27.3$$

Drill Hole in Pav. Co. Rd. "E"

6.6

$$25.5 / \frac{21}{27.0}$$

$$\frac{4.0}{20.6}$$

$$\frac{3.5}{27.1} / 32.7$$

Sta.	+	π	-	Grade	Lt	Rt
		943.07				
122				37.1		
B.M.	6.15	941.72			(935.57)	
+50				38.0		
123				38.6		
+50				39.1		
T.P.	3.53	944.99	0.76	940.96		
124				39.3		
+50				39.9		
125				39.5		
+50				39.6		
126				39.7		
+50				39.8	50	4.3
127				39.9	5.3	3.8
+33	P.C.					

Gr. Rod

Lt

R

Rt

6.0

$$247 / \frac{49}{R0.6}$$

$$\frac{55}{105}$$

$$\frac{46}{1.4} / 29.3$$

2.7

$$243 / \frac{48}{R0.9}$$

$$\frac{55}{102}$$

$$\frac{42}{R10} / 25.5$$

2.1

$$23.7 / \frac{6.0}{-2.9}$$

$$\frac{31}{00}$$

$$\frac{38}{R0.8} / 26.3$$

2.6

$$21.6 / \frac{18}{-2.2}$$

$$\frac{26}{00}$$

$$\frac{31}{R1.0} / 25.5$$

Nail in T.P.L. skates

5.2

$$245 / \frac{6.2}{R0.5}$$

$$\frac{51}{101}$$

$$\frac{36}{1.6} / 29.7$$

5.1

$$25.3 / \frac{51}{R0.9}$$

$$\frac{42}{102}$$

$$\frac{29}{12.2} / 30.9$$

5.0

$$26.9 / \frac{48}{102}$$

$$\frac{51}{-0.1}$$

$$\frac{1.3}{10.7} / 27.9$$

4.9

$$247 / \frac{5.1}{R0.6}$$

$$\frac{54}{-0.5}$$

$$\frac{59}{R0.5} / 24.5$$

Wicks

4.8

$$25.5 / \frac{8.3}{-25}$$

$$\frac{57}{-0.9}$$

$$\frac{6.3}{R0.0} / 23.5$$

$$\begin{matrix} +0.4 \\ -0.3 \end{matrix}$$

4.7

$$30.0 / \frac{1.00}{-50}$$

$$\frac{57}{-10}$$

$$\frac{60}{R0.2} / 25.1$$

+0.8

-0.7

4.6

$$26.9 / \frac{8.6}{-33}$$

$$\frac{54}{-0.8}$$

$$\frac{54}{R0.1} / 27.3$$

25.9

R-0.0

Sta	+	π	-	Grade	4	pt.
		944.49				
127	+50			39.9	56	34
128				39.9	56	31
I.P.	11.07	951.53	4.03	940.46		
	+50			39.9	12.6	
129				39.8	12.7	
	+50			39.6	12.9	
130				39.4	13.1	
I.P.	9.91	943.68	12.76	938.77		
	+50			39.2	5.5	30
131				38.9	5.8	27
	+38 P.T.					
	+50			38.7	5.8	3.7
132				38.4	5.7	4.7
	+50			38.2		

Ditch 1.5' below
Shoulder Grade
Sta. - 128 to - 132+50

6.8
3.8
3.2

Gr. Rod

Lt

R

Rt

Width

+ 1.2

- 1.0

4.6

2.0

22.1 / 17.3
- 1.7

46
80

26
12.0 / 33.8

25.8

2 1/2' 11
Shoulder slope

+ 1.5

- 1.0

4.6

2.3

27.3 / 6.2
- 0.9

90
106

111
+ 5.7 / 32.0

26.5

11.6

2.8

29.6 / 12.2
- 0.4

109
10.7

48
16.8 / 33.0

11.7

30.0 / 12.1
- 0.6

11.2
10.5

45
17.2 / 33.0

11.9

2.58

28.2 / 13.2
- 0.2

11.5
10.1

70
19.9 / 33.0

12.1

26.5 / 16.1
- 1.0

12.3
- 0.2

22
+ 2.9 / 32.3

+ 1.5

- 1.0

4.5

2.8

27.5 / 8.9
- 1.9

48
- 0.3

22
12.3 / 33.0

+ 1.4

- 1.0

4.8

2.3

26.0 / 7.2
- 0.1

48
0.0

23
12.5 / 33.0

25.8

+ 1.1

- 0.8

5.0

2.8

27.7 / 6.1
- 1.2

4.9
10.1

12.9
12.1 / 32.7

25.5

+ 0.6

- 0.4

5.3

25.3 / 6.3
- 0.9

5.5
- 0.2

3.9
11.9 / 32.1

25.3

+ 0.2

5.5

23.4 / 8.3
- 2.8

5.9
- 0.9

4.9
10.6 / 28.3

24.1

Sta	+	T	-	Grade
		943.68		
133				37.9
T.P.	2.90	940.75	5.83	937.85
+50				37.7
134				37.4
+50				37.1
B.M.				(940.75)
135				36.8
+50				36.5
136				36.1
+ 20 P.C.				
+50				35.7
137				35.2
+50				34.7
138				34.3

Gr. Rod. Lt. 4 Rt.

5.8 $23.8 / \frac{96}{-28}$ $\frac{62}{-0.4}$ $\frac{5.8}{195/27.5}$

Nail in TP. Lt. 183+

2.1 $21.3 / \frac{52}{-21}$ $\frac{34}{-0.3}$ $\frac{26}{195/27.5}$

2.4 $23.5 / \frac{49}{12.90}$ $\frac{32}{10.2}$ $\frac{31}{193/27.1}$

3.7 $24.7 / \frac{46}{12.96}$ $\frac{31}{10.6}$ $\frac{2.3}{11.9/27.3}$

Spk in 8° Pop 80' Rt. 134+85

4.0 $23.5 / \frac{55}{120.0}$ $\frac{11}{-0.6}$ $\frac{31}{109/28.3}$

4.3 $25.3 / \frac{98}{121.0}$ $\frac{36}{10.7}$ $\frac{25}{11.8/30.1}$

+ 0.2
- 0.2 47 $24.1 / \frac{40}{120}$ $\frac{39}{10.8}$ $\frac{29}{11.8/29.5}$ 22.2

+ 0.3
- 0.3 51 $26.9 / \frac{66}{120.0}$ $\frac{44}{10.7}$ $\frac{35}{11.6/28.8}$ 22.2

+ 0.4
- 0.4 56 $26.9 / \frac{60}{121.1}$ $\frac{53}{10.3}$ $\frac{64}{120.7/23.7}$ 22.2

61 $26.1 / \frac{69}{120.7}$ $\frac{65}{-0.9}$ $\frac{75}{120.1/22.5}$

+ 0.4
- 0.4 65 $22.3 / \frac{80}{120.0}$ $\frac{76}{-1.1}$ $\frac{86}{117/20.1}$ 22.2

Sta	+	Σ	-	Grade
		940.75		
138	+50			33.8
	+60	P.T.		
139				33.3
I.P.	2.98	934.15	10.58	930.17
	+50			32.8
140				32.3
	+50			31.9
141				31.4
	+50			30.9
142				30.4
	+50			29.9
143				29.5
	+50			29.0
T.P.	3.92	930.92	7.15	927.00

Gr. Rod

L_tL_tL_t

+ 0.3
- 0.3 7.0

$$26.1 / \begin{array}{r} 10.9 \\ - 8.7 \end{array}$$

$$\begin{array}{r} 88 \\ - 18 \end{array}$$

$$\begin{array}{r} 94 \\ - 21 \\ \hline 21.3 \end{array}$$

+ 0.1
- 0.1 7.5

$$28.1 / \begin{array}{r} 12.1 \\ - 4.7 \end{array}$$

$$\begin{array}{r} 85 \\ - 20 \end{array}$$

$$\begin{array}{r} 88 \\ - 20.2 \\ \hline 28.7 \end{array}$$

25.2

1.4

$$30.6 / \begin{array}{r} 6.6 \\ - 5.2 \end{array}$$

$$\begin{array}{r} 33 \\ - 19 \end{array}$$

$$\begin{array}{r} 27 \\ - 20.2 \\ \hline 23.9 \end{array}$$

1.9

$$30.6 / \begin{array}{r} 7.1 \\ - 5.2 \end{array}$$

$$\begin{array}{r} 37 \\ - 18 \end{array}$$

$$\begin{array}{r} 33 \\ - 20.1 \\ \hline 23.7 \end{array}$$

2.3

$$28.9 / \begin{array}{r} 7.1 \\ - 4.8 \end{array}$$

$$\begin{array}{r} 40 \\ - 17 \end{array}$$

$$\begin{array}{r} 37 \\ - 20.1 \\ \hline 23.7 \end{array}$$

2.8

$$27.0 / \begin{array}{r} 6.8 \\ - 4.0 \end{array}$$

$$\begin{array}{r} 41 \\ - 13 \end{array}$$

$$\begin{array}{r} 40 \\ - 20.3 \\ \hline 24.1 \end{array}$$

3.3

$$25.2 / \begin{array}{r} 6.7 \\ - 3.4 \end{array}$$

$$\begin{array}{r} 42 \\ - 09 \end{array}$$

$$\begin{array}{r} 35 \\ - 11.3 \\ \hline 26.1 \end{array}$$

3.8

$$21.6 / \begin{array}{r} 6.0 \\ - 2.2 \end{array}$$

$$\begin{array}{r} 45 \\ - 07 \end{array}$$

$$\begin{array}{r} 39 \\ - 10.9 \\ \hline 27.3 \end{array}$$

4.3

$$21.7 / \begin{array}{r} 5.8 \\ - 20.0 \end{array}$$

$$\begin{array}{r} 46 \\ - 06 \end{array}$$

$$\begin{array}{r} 34 \\ - 10.7 \\ \hline 28.3 \end{array}$$

4.7

$$21.6 / \begin{array}{r} 6.9 \\ - 2.2 \end{array}$$

$$\begin{array}{r} 55 \\ - 08 \end{array}$$

$$\begin{array}{r} 44 \\ - 10.3 \\ \hline 27.1 \end{array}$$

5.2

$$25.1 / \begin{array}{r} 7.9 \\ - 2.7 \end{array}$$

$$\begin{array}{r} 62 \\ - 10 \end{array}$$
Nail in T₁ L₁ 44+

Sta	+	π	-	Grade
		930.92		
144				28.5
	+50			28.0
145				27.5
	+50			27.1
146				26.6
	+50			26.1
147				25.6
	+50			25.0
148				24.4
	+50			23.9
149				23.3

Gr. Rod

Lt

Z

Rt

2.4

$$24.0 / \begin{array}{r} 5.4 \\ -3.0 \\ \hline \end{array}$$

$$\begin{array}{r} 35 \\ -1.1 \\ \hline \end{array}$$

$$\begin{array}{r} 3.9 \\ 20.0 / 22.9 \end{array}$$

2.9

$$24.0 / \begin{array}{r} 5.0 \\ -3.0 \\ \hline \end{array}$$

$$\begin{array}{r} 41 \\ -1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 3.1 \\ 20.7 / 24.9 \end{array}$$

3.4

$$21.9 / \begin{array}{r} 5.7 \\ -2.3 \\ \hline \end{array}$$

$$\begin{array}{r} 42 \\ -0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 4.1 \\ 20.8 / 25.1 \end{array}$$

3.8

$$20.1 / \begin{array}{r} 5.5 \\ -1.7 \\ \hline \end{array}$$

$$\begin{array}{r} 44 \\ -0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 3.6 \\ 20.2 / 20.9 \end{array}$$

4.3

$$19.7 / \begin{array}{r} 5.8 \\ 20.0 \\ \hline \end{array}$$

$$\begin{array}{r} 44 \\ -0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 3.4 \\ 10.7 / 29.3 \end{array}$$

4.8

$$22.7 / \begin{array}{r} 6.2 \\ 20.1 \\ \hline \end{array}$$

$$\begin{array}{r} 46 \\ +0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 3.2 \\ 44 / 29.3 \end{array}$$

5.3

$$24.1 / \begin{array}{r} 6.5 \\ 20.3 \\ \hline \end{array}$$

$$\begin{array}{r} 48 \\ +0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 3.5 \\ 118 / 30.1 \end{array}$$

5.9

$$25.1 / \begin{array}{r} 6.6 \\ 20.8 \\ \hline \end{array}$$

$$\begin{array}{r} 50 \\ 10.9 \\ \hline \end{array}$$

$$\begin{array}{r} 3.5 \\ 224 / 31.3 \end{array}$$

6.6

$$20.3 / \begin{array}{r} 6.6 \\ 21.4 \\ \hline \end{array}$$

$$\begin{array}{r} 54 \\ +1.1 \\ \hline \end{array}$$

$$\begin{array}{r} 3.5 \\ 12.0 / 32.5 \end{array}$$

7.0

$$24.9 / \begin{array}{r} 7.8 \\ 20.7 \\ \hline \end{array}$$

$$\begin{array}{r} 70 \\ 10.9 \\ \hline \end{array}$$

$$\begin{array}{r} 3.0 \\ 140 / 33.0 \end{array}$$

7.6

$$21.0 / \begin{array}{r} 9.6 \\ -2.0 \\ \hline \end{array}$$

$$\begin{array}{r} 66 \\ +1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 16 \\ 15.0 / 32.5 \end{array}$$

Sta	+	A	-	Grade
		990.92		
149	+50			22.7
150				22.1
	+50			21.5
T.P.	5.17	927.22	187	922.05
151				20.9
+23				20.6
	End	(13.0)		
+30	Calc. Rt = Elev,	918.8		18.8
+30				20.3
+65	End Calc. Lt =	917.5		
+78				19.8
152				19.7
+18				19.5
+37				19.4
+50				19.4

Gr. Rod.

Lt.

Q.

Rt.

8.2

$$251 / \frac{189}{208}$$

$$\frac{70}{+1.2}$$

$$\frac{40}{+4.2/33.0}$$

8.8

$$271 / \frac{85}{103}$$

$$\frac{75}{+1.3}$$

9.4

$$271 / \frac{91}{103}$$

$$\frac{82}{+1.2}$$

$$\frac{53}{+4.1/33.0}$$

6.3

$$293 / \frac{49}{114}$$

$$\frac{52}{+1.1}$$

$$\frac{1.5}{+2.8/33.0}$$

6.6

$$287 / \frac{55}{111}$$

$$\frac{63}{+0.3}$$

7.5

$$297 / \frac{59}{116}$$

$$\frac{72}{+0.3}$$

$$\frac{51}{+2.4/31.3}$$

7.7

$$\frac{77}{+0.3}$$

7.8

$$\frac{77}{+0.1}$$

$$\frac{6.3}{+1.5/29.5}$$

Sta	+	π	-	Grade	
		927.22			
153				19.5	
	+50			19.6	
154				19.7	
B.M.	3.33	923.86	6.66	920.56	(920.53)
	+50			19.7	
155				19.6	
	+50			19.4	
156				18.9	
	+50			18.4	
157				17.9	
	+50			17.4	
158				16.9	

Gr. Rod

Lt.

R

Rt.

7.7

 $\frac{76}{10.1}$ $\frac{6.2}{4.5/29.5}$

7.6

 $\frac{24.5}{2.05}$ $\frac{7.7}{-0.1}$ $\frac{6.9}{10.7/27.9}$

7.5

 $\frac{23.7}{2.01}$ $\frac{7.7}{-0.2}$ $\frac{7.4}{10.1/26.7}$

Spk in 24" Elm 15' Rt 154 +00

4.2

 $\frac{24.3}{2.04}$ $\frac{4.0}{10.2}$ $\frac{3.8}{10.9/27.3}$

4.3

 $\frac{24.7}{2.06}$ $\frac{4.0}{10.3}$ $\frac{4.4}{12.4/26.3}$

4.4

 $\frac{25.5}{2.10}$ $\frac{4.3}{-0.1}$ $\frac{3.7}{10.7/27.9}$

5.0

 $\frac{22.9}{2.07}$ $\frac{4.5}{10.5}$ $\frac{3.6}{4.9/29.3}$

5.5

 $\frac{26.1}{2.13}$ $\frac{4.9}{10.6}$ $\frac{5.7}{11.8/30.1}$

6.0

 $\frac{5.7}{10.3}$ $\frac{4.1}{11.7/30.3}$

6.5

 $\frac{6.5}{0.0}$ $\frac{5.2}{11.3/29.1}$

7.0

 $\frac{6.7}{10.3}$ $\frac{5.6}{11.4/29.3}$

Sta	+	-	Grade	Ditch Grade R.L.
B.M.	5.07	921.99		916.92

158			16.9	36
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450				6.4
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159				7.2
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Cor. Rod

R

Rt.

4.1

4.8

$2\frac{1}{2}:1$
Shoulder slope.

$\frac{4.2}{2.2} / 27.4'$

4.7

$2:1$
Shoulder slope.

$\frac{5.0}{4.8} / 27.6'$

