

Dr. 8 - Bk 150

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ PLAN _____ Survey

_____ BIRCH LAKE BLVD. NORTH _____

From 1/2 Mile West _____ To Centerville Rd. _____

Road Acc't. No. 11 _____

Date Filed 12-29-38 _____

File _____

Alignment

Birch Lake Blvd No

From 1/2 Mi. West to Centerville Rd.

Sec 16 T30 R22W.

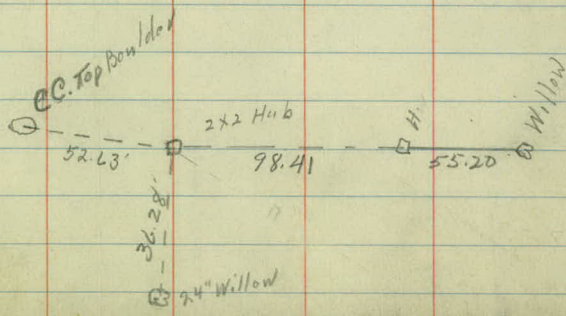
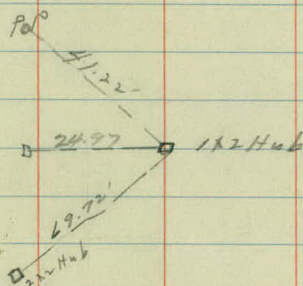
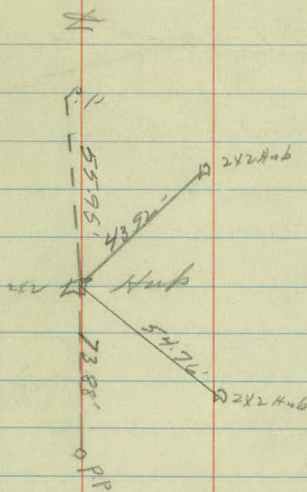
7/38

~~not Designed~~
D.P.

Sta	Point	$\Delta-Lt$	$\Delta-Rt$	Def
12+39 ²²	PT			2°36'
12				2°14'
+50				1°44'
11+08 ⁵⁶	P.I		5°15'	
11				1°14' Δ 5°15'
+50				0°44' Δ 2°00'
10				0°14' T. 131.34
9+77 ²²	P.C			0°00' L 262.50 R 2864.9

7+26⁰⁰ P.I 1°45'

0+00 P.I 43°00'



Sta PT A L+ A-R+ Def

19+79³⁵ P.O.T 31°14' to 200 R.R.

17+12² P.T

26°07'

17

24°58'

+50

19°58'

16

14°58' A 52°30'

15+92¹⁰ P.I 52°30'

D 20°00'

+50

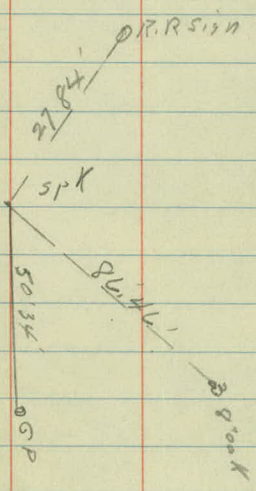
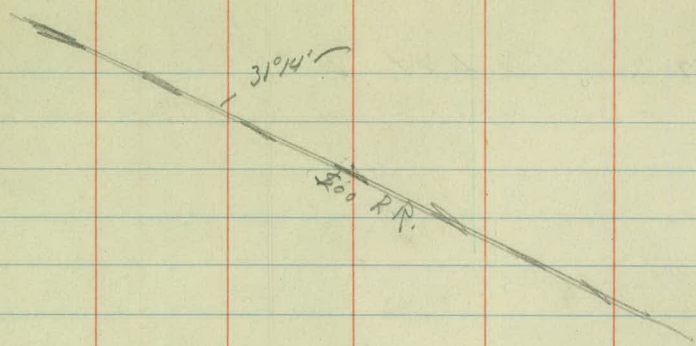
9°58' T 141.99

15

4°58' L 262.50

14+50¹¹ P.C

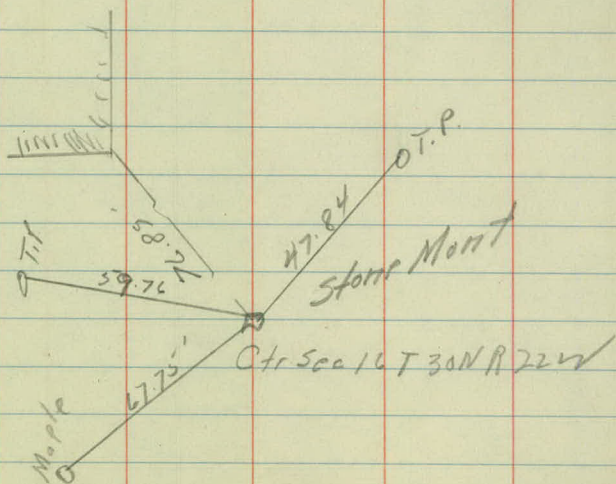
0°00'

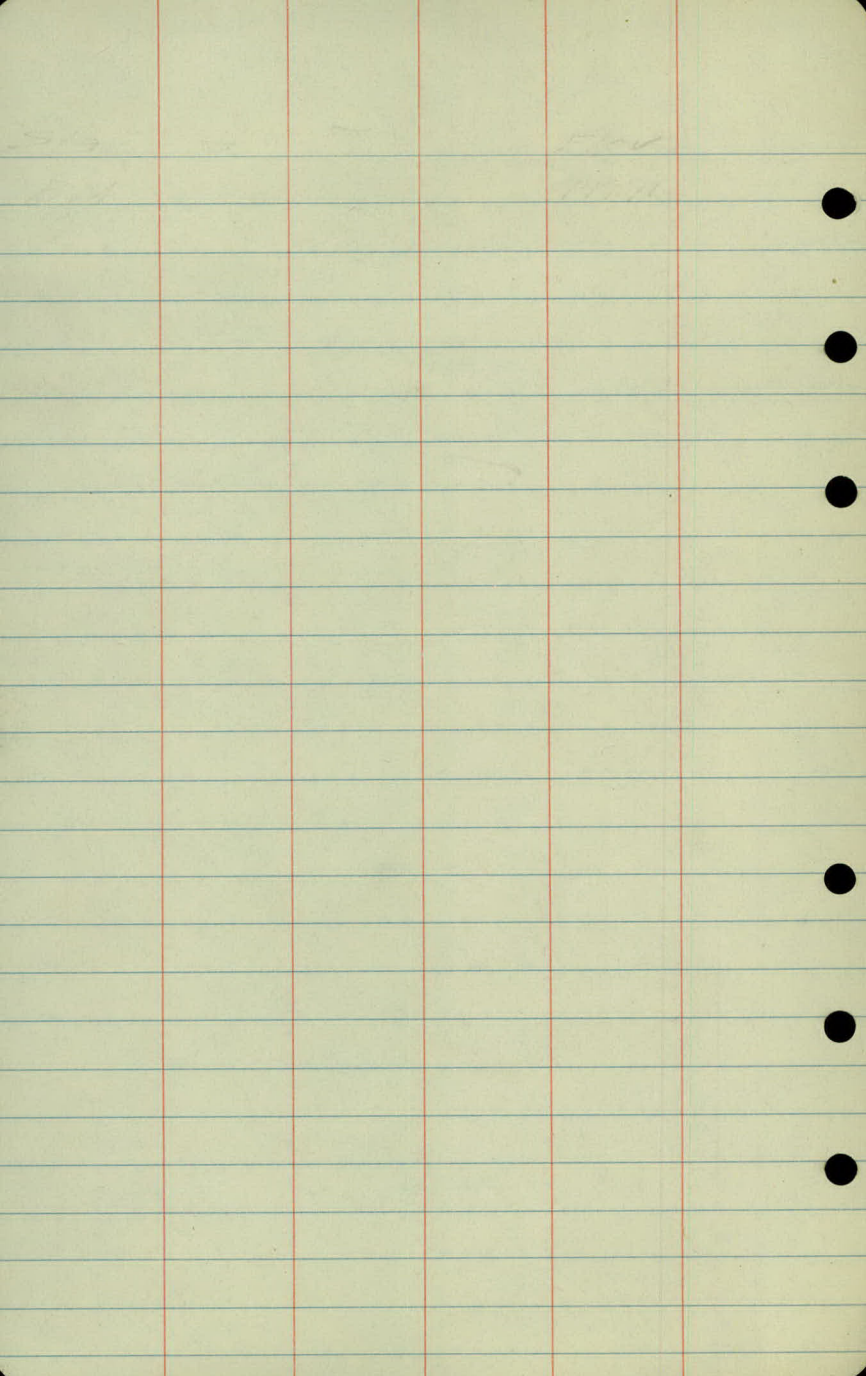


Sta Pt Alt Lat

24+86.02

89°49'





5
Topography

No Birch Lake Blvd No

From 1/2 Mi West to Centerville Rd

2

5

15-6 Rd

4

16-8 Rd

3

17-9 Rd

2

17-9 Rd

1

17-9 Rd

0+00

20-10 Rd

Cultivated

Hay Meadow

+79 P.P. 23'

+42 P.P. 23'

+29 12" Willow 22'

+28 24" x 20 CM 2'

2' x 3' Ditch

+3/10" Willow 2'

10' Roadway

Cultivated

Cultivated

+02 P.P. 23'

+70 P.P. 23'

12

Rd
6-14'

11

Rd
3-13'

10

Rd
2-8

9

Rd
7-3

8

Rd
7-3'

7

Rd
16-7

6

Rd
16-8

+99 P.P. 3'

Ent +80 12X120M.22'

+64 P.P. 3'

+34 P.P. 5'

+97 P.P. 11'

+63 P.P. 18'

+14 P.P. 23'

Hay Field

Scatter 00 1/5

+100 Fg 5.2'

+54 Fg 21

+100 Fg 68'

+150 Fg 123'

+100 Fg 176

Cultivated

Hay Meadow

19

Rd
8-1

18

Rd
6-4

17

Rd
2-10

Rd
6-15

16

Rd
18-29'

Rd
18-29'

15

Rd
8-18.5

14

Rd
4-13

13

Rd
5-14'

See Next Page For RR Xing
Details

+46 P.P. 12'

+38 F.C. 24' 430'

+00 Fg. 22'

+23 P.P. 9'

SWAMP

+00 Fg. 22'

+67 12x18 CM. 12'
East End
+57 Ent

Cultivated

+49 CM. 12'
+16 P.P. 11'
+02 Xing Sign 32'
+05 CM. 33' East End
+00 Fg. 42'
(+86 CM. 13' West End 13'
12x80 CM
+66-10x18 CM. 43'
+62 Fg. 70'
+57 P.P. 11'
+50 Fg. 62'
+50 G. Pole 62'

+32 P.P. 4'

Hay Field

24

Rd
4-6

23

Rd
4-6

22

Rd
4-5

21

Rd
4-4
126
12X32'CM

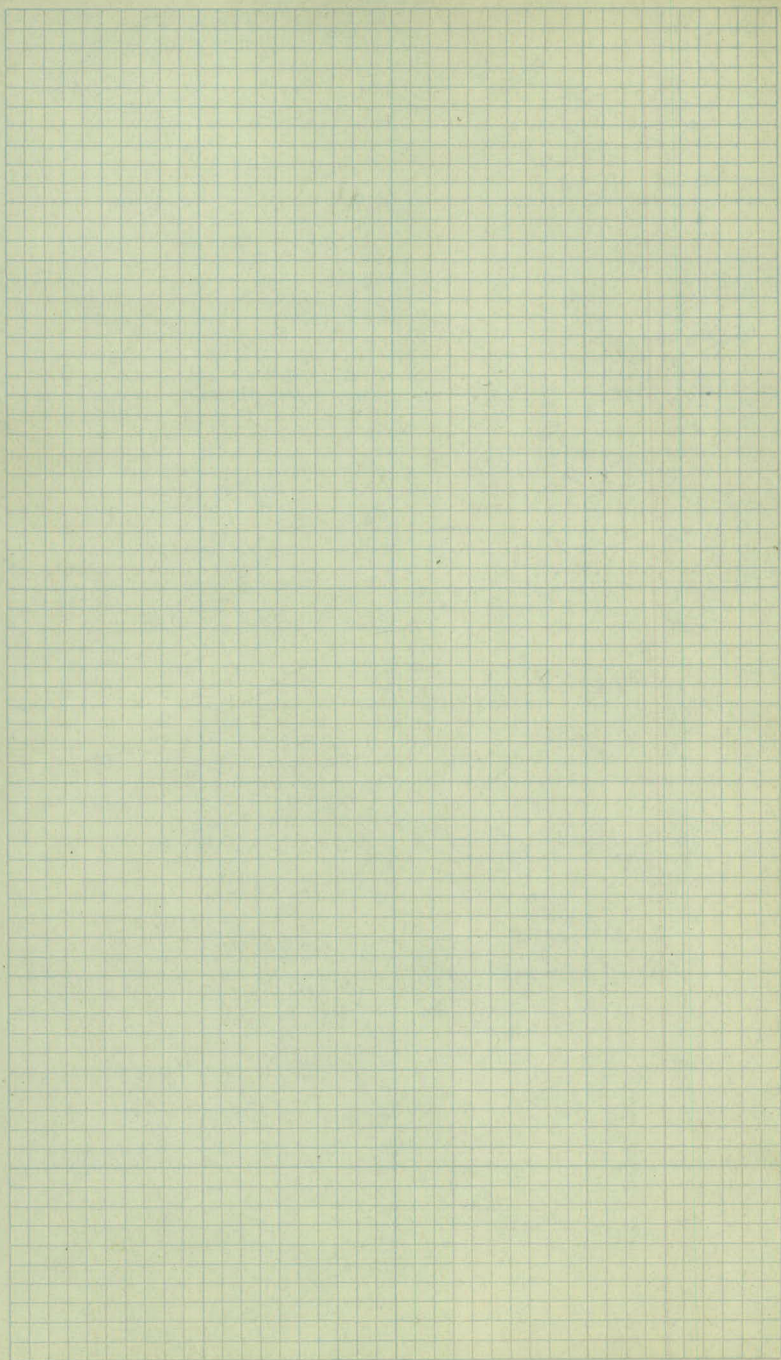
20

Rd
6-2

19

Rd
8-1

18



Bench levels
No Birch Lake Blvd.

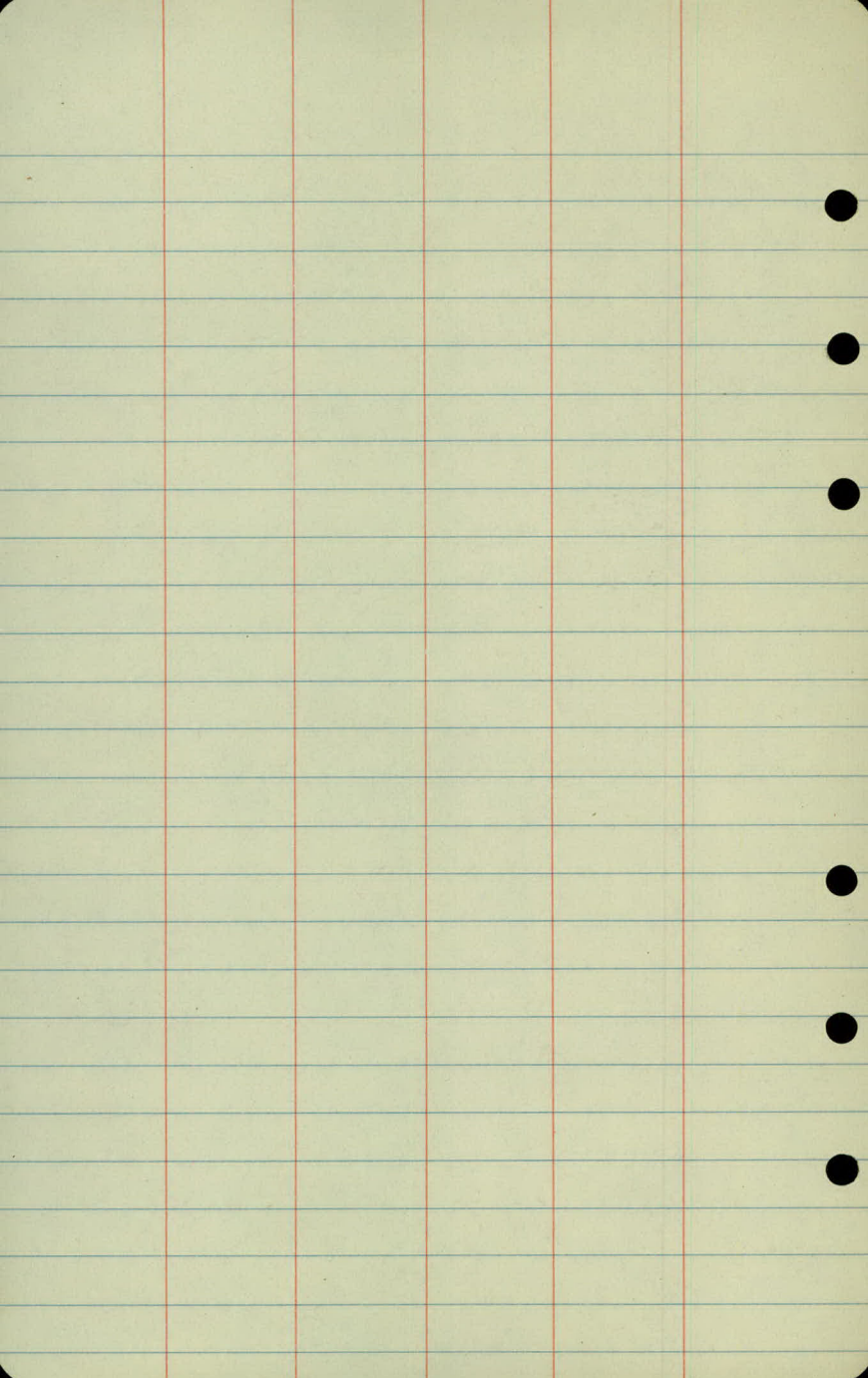
Sta	+	π	-	Elev
B.M	1.85	951.76 [✓]		949.91 [✓]
	0.16	939.87 [✓]	12.05	939.71 [✓]
B.M	8.42	939.87 [✓]	8.42	931.45 [✓]
	8.53	940.26 [✓]	8.14	931.73 [✓]
	3.95	932.62 [✓]	11.59	928.67 [✓]
	5.03	934.37 [✓]	3.28	929.34 [✓]
B.M.			8.53	925.84 [✓]

11
Desc

Top of Mont G. 2 x Centerville

Sph in G.P. 60' Bt Stg 15' + 50'

Sph in 18" Willow 140' Rt Stg 0 to 0



12

Cross Sections of Birch Lake
Blvd. No. from $\frac{1}{4}$ Mi. West
to Centerville Rd.

7/9/38

{ Bratager
{ Wilke
{ Goldberg
{ Moeschter

Sta.	+	K	-	Elev.
B.M.	9.64	935.48		925.84

0+00

925.8

+32

29.6

+50

31.0

1+00

30.6

+50

28.1

2+00

26.4

+50

24.5

3+00

22.7

T.P.

5.74

919.00

14.22

913.26

+28

24" C.M.

+40

22.0

4+00

22.5

Lt.

L

Rt.

13

Spike in 18" Willow 140' Rt. Sta. 0+00

$$\frac{62}{50} \quad \frac{68}{26} \quad \frac{64}{20} \quad \frac{63}{6} \quad \frac{94}{1} \quad \frac{97}{\cancel{1}} \quad \frac{110}{25} \quad \frac{122}{50}$$

$$\frac{21}{50} \quad \frac{30}{27} \quad \frac{47}{22} \quad \frac{50}{4} \quad \frac{59}{\cancel{1}} \quad \frac{66}{16} \quad \frac{112}{50}$$

$$\frac{10}{50} \quad \frac{08}{40} \quad \frac{22}{26} \quad \frac{38}{22} \quad \frac{38}{5} \quad \frac{45}{\cancel{1}} \quad \frac{54}{16} \quad \frac{104}{50}$$

$$\frac{51}{50} \quad \frac{42}{25} \quad \frac{48}{26} \quad \frac{48}{23} \quad \frac{46}{22} \quad \frac{45}{4} \quad \frac{49}{3} \quad \frac{49}{\cancel{1}} \quad \frac{51}{14} \quad \frac{80}{39} \quad \frac{95}{50}$$

$$\frac{85}{50} \quad \frac{79}{41} \quad \frac{68}{20} \quad \frac{68}{8} \quad \frac{74}{\cancel{1}} \quad \frac{75}{19} \quad \frac{82}{38} \quad \frac{93}{50}$$

$$\frac{93}{50} \quad \frac{88}{37} \quad \frac{89}{21} \quad \frac{85}{5} \quad \frac{91}{\cancel{1}} \quad \frac{93}{18} \quad \frac{104}{50}$$

$$\frac{141}{50} \quad \frac{141}{40} \quad \frac{129}{27} \quad \frac{111}{21} \quad \frac{109}{5} \quad \frac{110}{\cancel{1}} \quad \frac{99}{24} \quad \frac{90}{50}$$

$$\frac{139}{50} \quad \frac{136}{23} \quad \frac{120}{18} \quad \frac{118}{6} \quad \frac{125}{3} \quad \frac{128}{\cancel{1}} \quad \frac{122}{50}$$

919.10

100

99

719.0

100

10.0

$$\frac{77}{50} \quad \frac{73}{24} \quad \frac{59}{19} \quad \frac{58}{5} \quad \frac{70}{\cancel{1}} \quad \frac{75}{11} \quad \frac{74}{50}$$

$$\frac{73}{50} \quad \frac{73}{33} \quad \frac{67}{25} \quad \frac{52}{20} \quad \frac{48}{18} \quad \frac{50}{4} \quad \frac{65}{\cancel{1}} \quad \frac{68}{11} \quad \frac{74}{50}$$

Sta	+	π	-	Elev
		929.00		
4+50		✓		925.7 ✓
T.P.	7.59	935.18	1.41	917.59
5+00				28.3
+38				29.4
+67				29.4
6+00				27.8
+80				25.2
7+00				25.0
+26.0				24.2
+50				25.6
8+00		✓		26.0 ✓
T.P.	4.81	933.50	0.49	928.69
+50				26.1
9+00				26.2

44

2

24

$$\frac{2.3}{50} \quad \frac{22}{23} \quad \frac{28}{22} \quad \frac{28}{20} \quad \frac{28}{17} \quad \frac{20}{3} \quad \frac{23}{3} \quad \frac{34}{10} \quad \frac{44}{41} \quad \frac{46}{50}$$

$$\frac{41}{50} \quad \frac{37}{40} \quad \frac{42}{24} \quad \frac{64}{21} \quad \frac{65}{16} \quad \frac{66}{3} \quad \frac{69}{6} \quad \frac{62}{6} \quad \frac{63}{13} \quad \frac{82}{30} \quad \frac{90}{50}$$

$$\frac{17}{50} \quad \frac{26}{26} \quad \frac{50}{23} \quad \frac{54}{5} \quad \frac{57}{2} \quad \frac{58}{6} \quad \frac{48}{6} \quad \frac{51}{16} \quad \frac{73}{44} \quad \frac{83}{50}$$

$$\frac{10}{50} \quad \frac{25}{26} \quad \frac{53}{22} \quad \frac{63}{7} \quad \frac{58}{2} \quad \frac{60}{2} \quad \frac{55}{6} \quad \frac{59}{12} \quad \frac{91}{44} \quad \frac{98}{50}$$

$$\frac{12}{50} \quad \frac{35}{26} \quad \frac{59}{22} \quad \frac{61}{7} \quad \frac{63}{4} \quad \frac{74}{9} \quad \frac{86}{9} \quad \frac{108}{33} \quad \frac{125}{50}$$

$$\frac{36}{50} \quad \frac{58}{27} \quad \frac{75}{24} \quad \frac{77}{7} \quad \frac{80}{4} \quad \frac{100}{4} \quad \frac{105}{4} \quad \frac{121}{26} \quad \frac{136}{50}$$

$$\frac{32}{50} \quad \frac{49}{40} \quad \frac{63}{26} \quad \frac{85}{23} \quad \frac{85}{6} \quad \frac{87}{3} \quad \frac{102}{2} \quad \frac{108}{2} \quad \frac{125}{18} \quad \frac{138}{50}$$

$$\frac{33}{50} \quad \frac{48}{38} \quad \frac{65}{25} \quad \frac{83}{22} \quad \frac{88}{5} \quad \frac{92}{3} \quad \frac{110}{4} \quad \frac{119}{4} \quad \frac{130}{8} \quad \frac{136}{28} \quad \frac{137}{50}$$

$$\frac{41}{50} \quad \frac{60}{35} \quad \frac{65}{22} \quad \frac{89}{18} \quad \frac{90}{2} \quad \frac{96}{4} \quad \frac{115}{4} \quad \frac{133}{14} \quad \frac{136}{50}$$

$$\frac{67}{50} \quad \frac{80}{31} \quad \frac{84}{17} \quad \frac{84}{14} \quad \frac{92}{5} \quad \frac{107}{5} \quad \frac{121}{33} \quad \frac{135}{28} \quad \frac{136}{50}$$

$$\frac{76}{50} \quad \frac{84}{39} \quad \frac{80}{18} \quad \frac{81}{13} \quad \frac{80}{11} \quad \frac{74}{3} \quad \frac{74}{3} \quad \frac{84}{24} \quad \frac{107}{50}$$

$$\frac{110}{50} \quad \frac{107}{23} \quad \frac{96}{20} \quad \frac{90}{13} \quad \frac{77}{9} \quad \frac{73}{6} \quad \frac{75}{6} \quad \frac{109}{110} \quad \frac{117}{50}$$

Sta. + Σ - Elev.

933.50

9+40

927.1

+77

28.4

10+00

29.6 ✓

T.P.

14.61

945.38 ✓

0.73

934.77

+50

32.9

11+00

35.8

+50

37.0

+78

36.2

12+00

35.4 ✓

T.P.

5.05

941.51 ✓

8.92

936.46 ✓

+40

33.8

+70

32.4 ✓

T.P.

6.49

939.11 ✓

8.89

934.62 ✓

13+00

32.2

+50

31.4

Lt.

Z

Rt.

$\frac{115}{50}$ $\frac{110}{28}$ $\frac{96}{23}$ $\frac{89}{13}$ $\frac{74}{11}$ $\frac{66}{5}$ $\frac{64}{7}$ $\frac{65}{7}$ $\frac{102}{13}$ $\frac{106}{38}$ $\frac{95}{50}$

$\frac{100}{50}$ $\frac{90}{35}$ $\frac{73}{25}$ $\frac{70}{11}$ $\frac{5.5}{7}$ $\frac{5.1}{7}$ $\frac{5.0}{8}$ $\frac{62}{14}$ $\frac{58}{19}$ $\frac{34}{39}$ $\frac{25}{45}$ $\frac{29}{50}$

$\frac{84}{50}$ $\frac{57}{15}$ $\frac{56}{14}$ $\frac{45}{6}$ $\frac{39}{7}$ $\frac{36}{12}$ $\frac{46}{16}$ $\frac{42}{20}$ $\frac{30}{24}$ $\frac{17}{32}$ $\frac{13}{50}$

$\frac{161}{50}$ $\frac{118}{8}$ $\frac{118}{4}$ $\frac{12.5}{7}$ $\frac{120}{6}$ $\frac{120}{12}$ $\frac{12.5}{15}$ $\frac{122}{20}$ $\frac{91}{26}$ $\frac{94}{42}$ $\frac{93}{50}$

$\frac{110}{50}$ $\frac{87}{4}$ $\frac{96}{7}$ $\frac{90}{9}$ $\frac{94}{16}$ $\frac{82}{20}$ $\frac{36}{27}$ $\frac{35}{50}$

$\frac{114}{50}$ $\frac{93}{35}$ $\frac{71}{7}$ $\frac{79}{3}$ $\frac{84}{5}$ $\frac{78}{22}$ $\frac{76}{22}$ $\frac{19}{27}$ $\frac{00}{50}$

$\frac{142}{50}$ $\frac{104}{32}$ $\frac{80}{10}$ $\frac{77}{4}$ $\frac{91}{9}$ $\frac{84}{16}$ $\frac{86}{21}$ $\frac{75}{26}$ $\frac{40}{30}$ $\frac{12}{50}$ $\frac{+0.5}{50}$

$\frac{166}{50}$ $\frac{130}{30}$ $\frac{95}{10}$ $\frac{88}{3}$ $\frac{10.0}{6}$ $\frac{94}{18}$ $\frac{94}{22}$ $\frac{80}{29}$ $\frac{2.2}{50}$ $\frac{10}{50}$

$\frac{158}{50}$ $\frac{120}{16}$ $\frac{106}{12}$ $\frac{101}{7}$ $\frac{80}{2}$ $\frac{77}{7}$ $\frac{73}{8}$ $\frac{73}{15}$ $\frac{73}{23}$ $\frac{55}{26}$ $\frac{45}{41}$ $\frac{29}{50}$

$\frac{166}{50}$ $\frac{136}{16}$ $\frac{118}{6}$ $\frac{50}{2}$ $\frac{91}{4}$ $\frac{86}{14}$ $\frac{84}{24}$ $\frac{50}{25}$ $\frac{80}{38}$ $\frac{68}{38}$ $\frac{45}{50}$

$\frac{143}{50}$ $\frac{117}{14}$ $\frac{108}{7}$ $\frac{69}{7}$ $\frac{69}{4}$ $\frac{66}{15}$ $\frac{67}{20}$ $\frac{71}{24}$ $\frac{73}{23}$ $\frac{64}{23}$ $\frac{34}{50}$

$\frac{136}{50}$ $\frac{114}{13}$ $\frac{105}{8}$ $\frac{99}{4}$ $\frac{80}{2}$ $\frac{7.7}{4}$ $\frac{73}{15}$ $\frac{72}{19}$ $\frac{78}{23}$ $\frac{78}{25}$ $\frac{66}{34}$ $\frac{55}{34}$ $\frac{39}{39}$ $\frac{19}{50}$

Sta.	+	π	-	Elev.
		939.11		

14+00				931.2
-------	--	--	--	-------

+50				31.4
-----	--	--	--	------

15				30.5
----	--	--	--	------

B.M.	1.82	933.27 ✓	7.66	931.45 ✓
------	------	----------	------	----------

+50				26.6
-----	--	--	--	------

16+00				27.0
-------	--	--	--	------

+50				27.6
-----	--	--	--	------

17				28.5
----	--	--	--	------

+50				29.8 ✓
-----	--	--	--	--------

T.P.	9.59	941.27 ✓	1.59	931.68
------	------	----------	------	--------

18				31.8
----	--	--	--	------

+50				34.5
-----	--	--	--	------

T.P.	7.33	945.35 ✓	3.25	938.07 ✓
------	------	----------	------	----------

Lt

E

Rt

16

143	109	102	95	83	79	74	74	78	81	81	68	20	+07
<u>50</u>	<u>11</u>	<u>9</u>	<u>3</u>	<u>2</u>	<u>1</u>	<u>3</u>	<u>14</u>	<u>18</u>	<u>20</u>	<u>22</u>	<u>25</u>	<u>37</u>	<u>50</u>

138	128	104	25	27	77	76	81	78	50	+30
<u>50</u>	<u>48</u>	<u>11</u>	<u>6</u>	<u>2</u>	<u>7</u>	<u>14</u>	<u>17</u>	<u>21</u>	<u>24</u>	<u>50</u>

119	136	126	121	97	86	81	85	53	53	67	60	45
<u>50</u>	<u>44</u>	<u>41</u>	<u>40</u>	<u>15</u>	<u>8</u>	<u>18</u>	<u>22</u>	<u>23</u>	<u>27</u>	<u>29</u>	<u>50</u>	<u>50</u>

Spike in Guy Pole 60' Rt Sta, 15+50

54	64	73	73	68	67	63	47	43	39	42	48	48
<u>50</u>	<u>20</u>	<u>18</u>	<u>16</u>	<u>15</u>	<u>7</u>	<u>8</u>	<u>13</u>	<u>17</u>	<u>18</u>	<u>31</u>	<u>34</u>	<u>37</u>

40
50

49	58	63	64	56	50	54	68	71
<u>50</u>	<u>33</u>	<u>13</u>	<u>17</u>	<u>29</u>	<u>30</u>	<u>29</u>	<u>50</u>	<u>50</u>

43	48	52	57	54	54	69	68	69
<u>50</u>	<u>26</u>	<u>5</u>	<u>7</u>	<u>6</u>	<u>17</u>	<u>20</u>	<u>28</u>	<u>50</u>

35	48	51	55	55	48	48	68	71
<u>50</u>	<u>18</u>	<u>7</u>	<u>6</u>	<u>5</u>	<u>2</u>	<u>9</u>	<u>15</u>	<u>50</u>

+30	10	24	33	41	40	36	35	35	44	55	59	70
<u>50</u>	<u>28</u>	<u>28</u>	<u>9</u>	<u>7</u>	<u>6</u>	<u>4</u>	<u>35</u>	<u>7</u>	<u>14</u>	<u>14</u>	<u>22</u>	<u>50</u>

35	82	54	100	100	96	95	95	102	127	140	142
<u>50</u>	<u>20</u>	<u>10</u>	<u>9</u>	<u>8</u>	<u>6</u>	<u>9</u>	<u>9</u>	<u>11</u>	<u>23</u>	<u>35</u>	<u>50</u>

21	64	68	74	74	70	68	68	109	115	110	98	90
<u>50</u>	<u>21</u>	<u>14</u>	<u>11</u>	<u>9</u>	<u>7</u>	<u>6</u>	<u>7</u>	<u>13</u>	<u>20</u>	<u>36</u>	<u>46</u>	<u>50</u>

Sta. + K - Elev.

945.35

19+00.

937.2

+32

39.3

+63

42.3

+79.35

43.6

20

43.1

+25

41.9

+50

40.9

+75

40.4

+76 = CM Culvert

21

40.2 ✓

T.P.

10.16

951.17 ✓

4.34

941.01

+50

40.2

22

41.1

+50

43.5

Lt.

E.

Rt.

7

23
50
$$\frac{67}{50} \frac{78}{44} \frac{80}{27} \frac{99}{23} \frac{90}{16} \frac{80}{12} \frac{81}{9} \frac{82}{5} \frac{81}{11} \frac{117}{12} \frac{116}{18} \frac{94}{26} \frac{87}{35} \frac{81}{38} \frac{25}{43} \frac{23}{50}$$

T.T.

$$\frac{85}{50} \frac{105}{44} \frac{126}{40} \frac{137}{34} \frac{130}{30} \frac{77}{16} \frac{71}{12} \frac{60}{9} \frac{61}{11} \frac{58}{10} \frac{64}{16} \frac{28}{21} \frac{23}{25} \frac{23}{35} \frac{24}{37} \frac{30}{50} \frac{107}{50}$$

T.T. T.T.

Rail 0.5 H.

$$\frac{133}{50} \frac{137}{47} \frac{123}{26} \frac{107}{30} \frac{89}{26} \frac{62}{16} \frac{53}{10} \frac{32}{4} \frac{31}{4} \frac{24}{7} \frac{23}{15} \frac{23}{19} \frac{26}{37} \frac{139}{50} \frac{152}{60} \frac{152}{60}$$

T.T.

$$\frac{140}{60} \frac{125}{50} \frac{119}{40} \frac{104}{34} \frac{65}{24} \frac{40}{17} \frac{20}{13} \frac{20}{8} \frac{18}{18} \frac{26}{10} \frac{189}{27} \frac{152}{40} \frac{152}{50} \frac{152}{60}$$

T. Rail

$$\frac{121}{60} \frac{123}{50} \frac{117}{44} \frac{99}{26} \frac{22}{24} \frac{21}{6} \frac{23}{7} \frac{27}{24} \frac{141}{43} \frac{147}{50} \frac{145}{50} \frac{140}{60}$$

T.T.

$$\frac{101}{50} \frac{21}{35} \frac{21}{23} \frac{24}{16} \frac{45}{11} \frac{26}{6} \frac{35}{8} \frac{40}{22} \frac{136}{24} \frac{140}{53} \frac{140}{50} \frac{140}{50}$$

$$\frac{24}{50} \frac{24}{32} \frac{87}{21} \frac{20}{19} \frac{83}{15} \frac{47}{7} \frac{45}{8} \frac{47}{17} \frac{105}{20} \frac{120}{24} \frac{109}{34} \frac{119}{44} \frac{105}{48} \frac{104}{50}$$

$$\frac{25}{50} \frac{29}{46} \frac{24}{37} \frac{100}{51} \frac{105}{20} \frac{85}{16} \frac{84}{13} \frac{52}{7} \frac{50}{6} \frac{50}{9} \frac{26}{16} \frac{106}{15} \frac{106}{18} \frac{82}{19} \frac{79}{24} \frac{76}{50}$$
100
10.5100
11.0
$$\frac{86}{50} \frac{100}{43} \frac{91}{26} \frac{88}{13} \frac{56}{6} \frac{52}{9} \frac{55}{16} \frac{27}{19} \frac{27}{22} \frac{67}{22} \frac{65}{34} \frac{54}{50}$$

$$\frac{152}{50} \frac{141}{48} \frac{141}{40} \frac{126}{11} \frac{112}{7} \frac{110}{8} \frac{111}{11} \frac{118}{13} \frac{124}{30} \frac{114}{30} \frac{92}{50}$$

$$\frac{131}{50} \frac{109}{16} \frac{112}{14} \frac{111}{10} \frac{102}{5} \frac{101}{7} \frac{102}{11} \frac{107}{18} \frac{105}{23} \frac{73}{27} \frac{74}{50} \frac{56}{50}$$

$$\frac{101}{50} \frac{81}{48} \frac{76}{17} \frac{88}{14} \frac{81}{7} \frac{77}{7} \frac{77}{12} \frac{50}{19} \frac{80}{23} \frac{58}{26} \frac{24}{26} \frac{20}{50}$$

Sta.	+	Σ	-	Elev.
		951.17		
22+85				945.6
23+00				46.5
+50				48.6
T.P.	5.48	954.35 ✓	2.30	948.87 ✓
24+00				49.4
+50				49.8
+70				50.0
+76				49.9
+86				50.1
B.M			4.42	949.8 949.91

L.

E

R+

$$\begin{array}{cccccccccccc} \frac{4.5}{50} & \frac{4.5}{33} & \frac{4.8}{19} & \frac{6.1}{14} & \frac{6.0}{9} & \cancel{5.6} & \frac{5.7}{7} & \frac{5.4}{13} & \frac{5.0}{19} & \frac{2.3}{26} & \frac{2.1}{30} & \frac{2.4}{38} & \frac{3.6}{50} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{3.6}{50} & \frac{3.6}{40} & \frac{4.6}{19} & \frac{5.1}{14} & \cancel{4.7} & \frac{4.9}{9} & \frac{5.6}{15} & \frac{5.8}{21} & \frac{4.9}{25} & \frac{3.1}{29} & \frac{4.5}{40} & \frac{4.4}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{2.7}{50} & \frac{2.3}{17} & \cancel{2.6} & \frac{2.8}{9} & \frac{4.3}{16} & \frac{3.7}{21} & \frac{5.3}{26} & \frac{5.3}{42} & \frac{5.9}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{3.3}{50} & \frac{4.1}{29} & \frac{4.4}{12} & \frac{5.2}{10} & \cancel{5.0} & \frac{5.3}{10} & \frac{6.5}{17} & \frac{7.1}{26} & \frac{8.5}{34} & \frac{9.1}{50} \end{array}$$

$$\begin{array}{ccccccc} \frac{4.0}{50} & \frac{4.3}{14} & \frac{4.9}{11} & \cancel{4.6} & \frac{4.9}{10} & \frac{5.9}{15} & \frac{6.9}{32} & \frac{7.9}{50} \end{array}$$

$$\begin{array}{cccc} \frac{5.4}{50} & \frac{5.0}{24} & \cancel{4.4} & \frac{4.8}{19} & \frac{6.1}{29} & \frac{6.6}{30} \end{array}$$

$$\begin{array}{ccc} \frac{5.4}{50} & \cancel{4.5} & \frac{4.1}{50} \end{array}$$

$$\begin{array}{ccc} \frac{5.1}{50} & \cancel{4.3} & \frac{3.6}{50} \end{array}$$

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