

Dr. 8 - Bk. 149

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ PLAN _____ Survey

_____ EDGERTON STREET _____

From Labore Rd. To 1/2 Mile North

Road Acc't. No. 2 _____

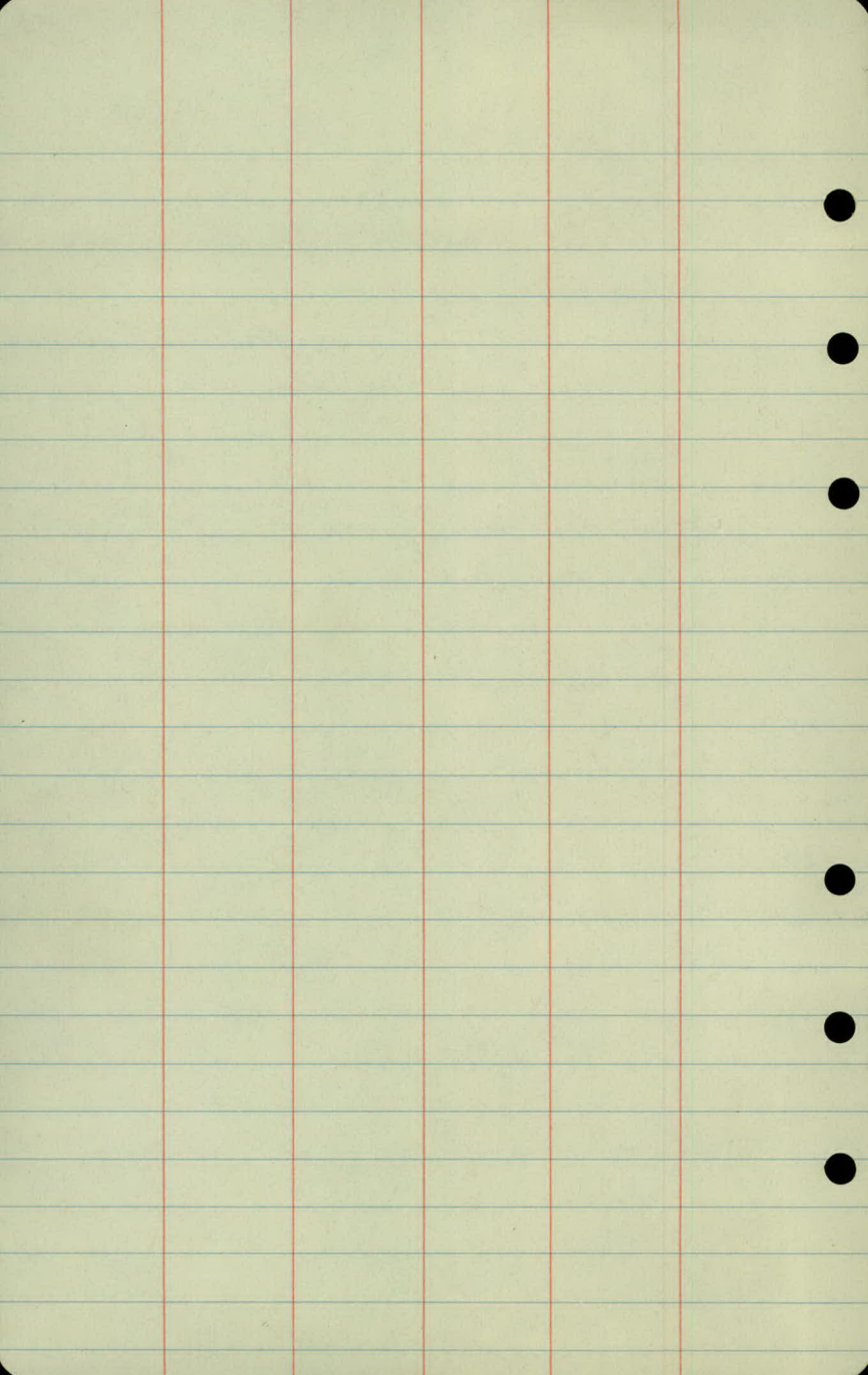
Date Filed 12-29-38 _____

File _____

R-22-38
K.A.
B.P.
L.C.
M.G.
L.R.H.

Plan Survey

EDGERTON ST.
from Labore Rd. to $\frac{1}{2}$ Mi. North



PLAN SURVEY

Edgerton St.

Alignment

Sta 125 to 162

160 + 40.45 Mont. N 1/4 Cor. Sec. 5

121 + 59.2 P.O.T. = ctr sec. 5 Found Nail and assumed
it to be ctr sec. 5

Topography

127

126

125

161465 - 2 Culv. Box

160+87 - 18" x 20" C.M. -

161452 - T.H. - 30'

160+69 - T.R.
 158+57 - T.P.
 157+08 - T.P.
 155+68 - T.P.
 154+40 - T.P.
 153+09 - T.P.
 151+82 - T.P.
 150+56 - T.P.
 150+00 - Ent. - 15" x 20" C.M.
 149+85 - T.P.
 147+96 - T.P.
 146+92 - T.P.
 145+62 - T.P.
 144+31 - T.P.
 143+03 - T.P.
 141+71 - T.P.
 141+23 - 15" x 20" C.M.
 140+42 - T.P.
 139+11 - T.P.
 137+80 - T.P.
 136+50 - T.P.
 135+21 - T.P.
 133+71 - T.P.
 132+75 - Ent. 15" x 20" C.M.
 132+63 - T.P.
 131+63 - Ent. 21" x 21"
 131+32 - T.P.
 130+03 - T.P. - 30'
 128+68 - T.P. - 30'

139+60 - 24" Tw. Golt. 18'

110 - Ent. 15" x 20" C.M. - 23'
 105 - Fe. Cor. - 36'
 197 - G.P. - 29'

Fe - 91'

192 - 12" Oak - 57'
 170 - 10" Oak - 18' 12" - 73'
 147 - 24" Oak - 16"
 134 - 8" Oak - 30'
 131 - T.R. - 29'

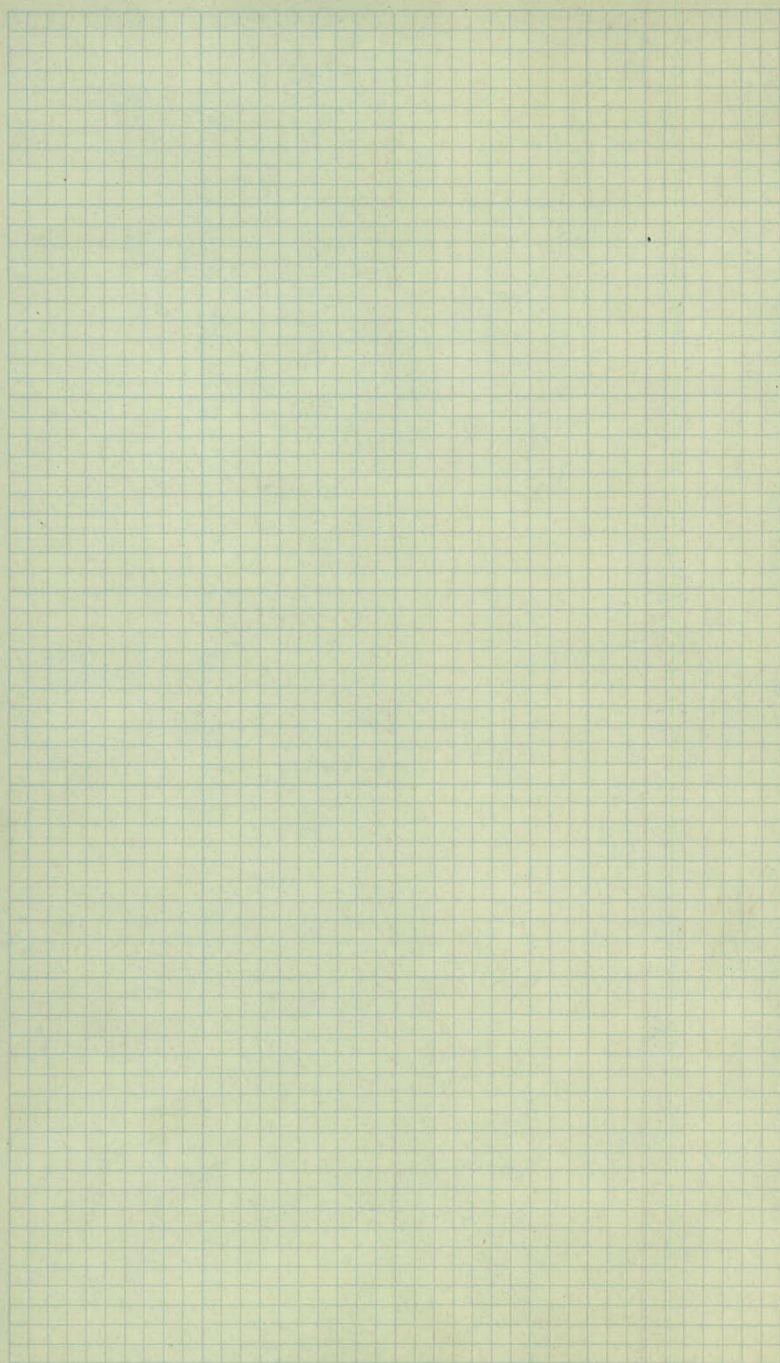
Fe - 37'

156 - T.R.

144 - N. End 15" C.M.

117 - 29' - 59' - 94'
 B. Top - 74'

150 - B. Top - 48'



Bench Levels

Special Digging

2000 - 2000

Sta.	+	Σ	-	Elev.	
B.M.	5.41	914.36			908.95
T.P.	3.08	914.87	4.57	909.79	
T.P.	5.42	915.35	4.24	909.93	
T.P.	4.62	915.44	4.53	910.82	
B.M.			4.04	911.40	
T.P.	4.65	915.50	4.59	910.85	
T.P.	2.00	910.45	7.05	908.45	
B.M.			13.46	896.99	

Description

Top. Mont. A. 140140.45

Spk in 36" Gott. Lt. 139160

R.R. Spikes G.R. W side of Edgerton & Co. Ry. Rd.

				Ditch	
				Grade	
Sta.	+	-		Lt.	Rt.
B.M.	4.98	713.93			908.95
0	+00			05.5	05.5
	+50			05.6	05.6
1				05.7	05.7
	+50			05.8	05.8
2				05.9	05.9
	+50			06.0	06.0
3				06.1	06.1
	+50			06.2	06.2
4				06.3	06.3
	+50			06.4	06.4
5				06.5	06.5
T.P.	4.65	714.38	42.0	909.79	

x sections

Sta	+	T	-	Elev
B.M.	1.19	898.18 ✓		896.99

125				890.2
-----	--	--	--	-------

+50				91.8
B.M.	5.72	902.71 ✓		896.99

126.				93.5
------	--	--	--	------

+50				95.2
-----	--	--	--	------

127				96.7
-----	--	--	--	------

+30				97.5
-----	--	--	--	------

+44				98.0
-----	--	--	--	------

128				99.7 ✓
T.P.	12.85	915.09 ✓	0.47	902.24

127	+44			98.0
-----	-----	--	--	------

+15				99.0
-----	--	--	--	------

LT

X

RT

R.R. Spk in G.P. Lt 126+97

168 12.8 148 120 95 125 123 87 809 893
150 125 100 76 70 95 24 15 10

104 90 24 0.2 103 94 87 70 482 632
150 135 100 90 62 28 21 18 10

R.R. Spk in G.P. Lt 126+97

144 64 95 0.3 34 95 114 116 99 818 918
180 140 107 60 54 44 38 36 20 10

133 50 90 12.7 126 0.2 19 79 89 7.7 753 750
200 167 230 110 88 62 40 33 24 17 10

70 407 417 21 14 73 4.3 605 602
200 145 118 65 32 23 16 10

43 37 26 56 10 70 53 525 518 531 30 24 20 Ed disc & top
60 37 39 32 24 21 17 10 10 43 66 70 Lo Bor Card

48 38 27 27 66 6.6 50 450 476 485 47 6.39 Flight
60 38 34 32 29 21 16 10 10 14 16 15% N. N. End

47 30 30 67 07 49 49 31 30 298 311 30 3.5 36
60 48 39 33 31 25 20 16 10 10 15 16 17

170 6.6 6.2 14.5 129 4.7
73 55 75 75 14 Bor Card

16.1 162 160 169 169 133 7.2 53 41 3.5
10 14 15 16 23 34 42 61 79

13.7 109 119 48 3.5
120 110 84 80

Sta	+	π	-	Elev.
		915.09		
128				899.7
	+50			901.5
129				02.8
	+50			04.3
130				05.5
	+50			06.1
131				07.8
	+50			09.0
T.P.	6.26	915.59 ✓	586	909.23 ✓
132				09.8
	+50			10.4
133				10.7

44

4

104

$$\frac{15.4}{34} \frac{6.3}{58} \frac{4.9}{77} \frac{2.8}{130} \frac{6.7}{160} \frac{10.1}{160}$$

$$\frac{157}{60} \frac{193}{40} \frac{114}{33} \frac{114}{30} \frac{158}{24} \frac{158}{21} \frac{140}{16} \frac{1370}{10} \frac{1763}{10} \frac{1385}{10} \frac{190}{19} \frac{143}{15} \frac{143}{16} \frac{129}{17} \frac{50}{30} \frac{51}{30} \frac{41}{110}$$

$$\frac{141}{60} \frac{124}{40} \frac{104}{34} \frac{104}{31} \frac{140}{23} \frac{140}{19} \frac{126}{16} \frac{126}{10} \frac{123}{10} \frac{123}{10} \frac{1235}{10} \frac{123}{18} \frac{42}{29} \frac{52}{77} \frac{96}{110}$$

$$\frac{96}{60} \frac{96}{47} \frac{100}{39} \frac{90}{30} \frac{90}{28} \frac{126}{22} \frac{126}{20} \frac{112}{18} \frac{1092}{10} \frac{1083}{10} \frac{1095}{10} \frac{114}{19} \frac{63}{25} \frac{52}{37} \frac{55}{60}$$

$$\frac{71}{60} \frac{77}{46} \frac{81}{31} \frac{112}{23} \frac{112}{21} \frac{99}{17} \frac{970}{10} \frac{961}{10} \frac{972}{10} \frac{100}{19} \frac{70}{25} \frac{66}{30} \frac{66}{60}$$

$$\frac{64}{60} \frac{74}{40} \frac{71}{39} \frac{89}{26} \frac{118}{23} \frac{100}{20} \frac{87}{15} \frac{839}{10} \frac{897}{10} \frac{899}{10} \frac{88}{19} \frac{69}{24} \frac{70}{46} \frac{70}{60}$$

085

064

$$\frac{58}{60} \frac{66}{33} \frac{80}{29} \frac{70}{25} \frac{87}{23} \frac{87}{20} \frac{75}{16} \frac{732}{10} \frac{726}{10} \frac{731}{10} \frac{80}{19} \frac{85}{26} \frac{68}{30} \frac{60}{37} \frac{66}{60}$$

087

073

075

086

$$\frac{58}{60} \frac{64}{33} \frac{65}{26} \frac{78}{29} \frac{78}{21} \frac{65}{16} \frac{618}{10} \frac{608}{10} \frac{617}{10} \frac{63}{16} \frac{76}{19} \frac{76}{29} \frac{66}{26} \frac{65}{45} \frac{69}{60}$$

088

079

079

096

$$\frac{61}{60} \frac{68}{39} \frac{80}{29} \frac{76}{26} \frac{77}{23} \frac{63}{17} \frac{586}{10} \frac{576}{10} \frac{586}{10} \frac{62}{17} \frac{77}{21} \frac{77}{22} \frac{66}{25} \frac{60}{37} \frac{67}{52} \frac{69}{60}$$

089

080

080

091

$$\frac{63}{60} \frac{61}{48} \frac{67}{32} \frac{76}{29} \frac{70}{27} \frac{70}{24} \frac{75}{22} \frac{63}{16} \frac{527}{10} \frac{520}{10} \frac{530}{10} \frac{61}{18} \frac{76}{21} \frac{69}{23} \frac{69}{26} \frac{63}{60}$$

091

084

079

093

$$\frac{62}{60} \frac{64}{43} \frac{65}{31} \frac{75}{28} \frac{67}{26} \frac{72}{23} \frac{72}{20} \frac{56}{15} \frac{502}{10} \frac{493}{10} \frac{503}{10} \frac{53}{16} \frac{77}{23} \frac{77}{25} \frac{66}{27} \frac{63}{39} \frac{66}{60}$$

Sta.	+	Σ	-	Elev.
		715.59		
133	+50			910.8
134				10.9
	+50			11.0
135				11.0
	+50			11.1
136				11.0
	+50			11.0
137				10.9
T.P.	4.55	715.52	4.62	910.97 ✓
	+50			10.9
138				10.7
	+50			10.8

Lt

R

Rt

09.5 07.9 08.0 09.4
 $\frac{6.2}{60} \frac{60.7}{30} \frac{6.1}{38} \frac{7.7}{32} \frac{7.7}{28} \frac{5.3}{16} \frac{4.86}{10} \frac{4.78}{10} \frac{4.90}{18} \frac{5.3}{28} \frac{7.6}{25} \frac{6.5}{28} \frac{6.2}{42} \frac{6.5}{60}$

09.9 07.6 07.6 09.4
 $\frac{6.5}{60} \frac{6.8}{36} \frac{5.7}{39} \frac{5.7}{32} \frac{8.0}{26} \frac{8.0}{22} \frac{5.2}{15} \frac{4.80}{10} \frac{4.73}{10} \frac{4.8}{10} \frac{5.0}{16} \frac{8.0}{23} \frac{8.0}{25} \frac{6.8}{27} \frac{6.8}{31} \frac{6.5}{36} \frac{6.8}{60}$

09.9 07.2 07.9 09.6
 $\frac{6.6}{60} \frac{6.2}{35} \frac{6.4}{37} \frac{5.7}{32} \frac{8.4}{26} \frac{8.0}{22} \frac{5.4}{15} \frac{4.71}{10} \frac{4.60}{10} \frac{4.76}{10} \frac{5.3}{16} \frac{7.7}{23} \frac{7.7}{26} \frac{6.3}{28} \frac{6.0}{41} \frac{6.6}{60}$

09.1 07.6 07.6 09.6
 $\frac{6.3}{60} \frac{6.5}{37} \frac{5.9}{31} \frac{8.0}{26} \frac{8.0}{22} \frac{5.2}{15} \frac{4.65}{10} \frac{4.55}{10} \frac{4.63}{10} \frac{5.1}{15} \frac{8.0}{22} \frac{8.0}{25} \frac{6.4}{28} \frac{6.0}{39} \frac{6.4}{60}$

09.3 07.3 07.9 09.3
 $\frac{6.5}{60} \frac{6.0}{45} \frac{6.3}{30} \frac{8.3}{26} \frac{8.3}{22} \frac{5.1}{18} \frac{4.59}{10} \frac{4.59}{10} \frac{4.61}{15} \frac{8.2}{22} \frac{7.7}{25} \frac{7.7}{28} \frac{6.2}{40} \frac{6.3}{60}$

09.1 07.4 08.2 09.7
 $\frac{6.6}{60} \frac{6.5}{38} \frac{6.5}{29} \frac{8.2}{26} \frac{8.2}{22} \frac{5.1}{16} \frac{4.65}{10} \frac{4.66}{10} \frac{4.69}{10} \frac{5.3}{17} \frac{7.4}{21} \frac{7.4}{23} \frac{6.1}{27} \frac{5.9}{39} \frac{6.2}{60}$

09.4 07.6 08.3 09.8
 $\frac{6.6}{60} \frac{6.6}{37} \frac{6.2}{34} \frac{6.2}{28} \frac{8.0}{25} \frac{8.0}{21} \frac{5.1}{15} \frac{4.67}{10} \frac{4.61}{10} \frac{4.69}{10} \frac{5.3}{17} \frac{7.3}{21} \frac{7.3}{23} \frac{5.8}{27} \frac{5.9}{39} \frac{6.1}{60}$

09.1 07.5 07.7 09.6
 $\frac{6.8}{60} \frac{6.5}{28} \frac{8.1}{25} \frac{8.1}{22} \frac{5.0}{15} \frac{4.73}{10} \frac{4.68}{10} \frac{4.79}{10} \frac{5.2}{18} \frac{7.9}{23} \frac{7.9}{25} \frac{6.3}{28} \frac{6.0}{37} \frac{6.1}{60}$

08.3 07.4 07.8 09.5
 $\frac{7.2}{60} \frac{7.2}{37} \frac{6.7}{29} \frac{8.1}{21} \frac{8.1}{15} \frac{5.0}{15} \frac{4.67}{10} \frac{4.63}{10} \frac{4.71}{10} \frac{5.3}{17} \frac{7.7}{23} \frac{7.7}{29} \frac{6.6}{28} \frac{7.4}{29} \frac{6.0}{34} \frac{6.2}{60}$

08.5 07.3 07.2 09.1
 $\frac{6.8}{60} \frac{6.8}{37} \frac{7.0}{28} \frac{6.3}{25} \frac{8.2}{22} \frac{5.2}{16} \frac{4.73}{10} \frac{4.67}{10} \frac{4.79}{10} \frac{5.3}{15} \frac{8.3}{23} \frac{8.3}{25} \frac{6.2}{28} \frac{6.3}{29} \frac{6.3}{60}$

09.5 07.4 07.0 09.0
 $\frac{6.6}{60} \frac{6.8}{37} \frac{6.0}{39} \frac{6.0}{29} \frac{8.1}{25} \frac{8.1}{22} \frac{5.3}{14} \frac{4.73}{10} \frac{4.68}{10} \frac{4.78}{10} \frac{5.3}{15} \frac{8.5}{22} \frac{8.5}{26} \frac{6.5}{30} \frac{6.0}{41} \frac{6.2}{60}$

Sta.	+	π	-	Elev.
		915.52		
139				10.7
+50				10.8
140				10.9
B.M.	4.23	✓ 915.63	4.09	911.43 ✓
+50				11.0
141				11.0
+50				11.0
142				10.9
+50				10.9
143				10.9
+50				10.8
144				10.7

911.40

Lt

R

Rt

09.1

07.4

07.7

09.3

6.5	6.8	6.9	6.9	8.1	8.8	5.5	4.90	4.77	4.86	5.5	7.8	7.8	6.8	9.2	5.8	6.0
60	36	33	33	26	22	15	10		10	16	21	24	26	32	40	60

09.2

07.5

07.6

09.3

6.5	6.7	6.3	6.3	8.0	8.0	5.3	4.75	4.92	4.76	5.2	7.7	7.9	6.2	5.7	6.0
60	38	34	29	26	23	16	10	10	16	22	25	29	43		60

06.6

07.5

07.5

06.9

7.2	6.9	6.4	8.0	8.0	5.8	4.76	4.7	4.73	5.4	8.0	8.0	6.6	5.8	6.2
60	36	28	26	22	17	10		10	16	22	24	27	42	60

Spk 12 30 Colt LL 129+60

07.0

07.0

09.2

7.9	7.0	6.6	4.7	8.6	8.6	5.3	4.74	4.61	4.77	5.3	8.6	8.6	7.1	7.1	6.9	6.6
60	36	35	32	26	23	15	10			15	23	25	27	31	33	60

09.4

07.1

Rt 7 side

Lt 7 side

07.3

09.2

6.2	6.2	7.2	7.1	8.5	8.5	5.3	4.74	4.66	4.71	5.3	7.9	7.9	6.9	6.7
60	39	31	28	26	22	15	10		10	16	22	27	33	60

09.6

07.5

Lt

Rt 07.2

09.6

6.6	6.0	8.1	7.9	5.5	4.72	4.62	4.71	5.2	8.4	8.4	7.0	7.1	6.0	5.7
60	32	27	21	16	10		10	15	22	24	27	31	33	60

09.4

07.3

06.7

09.1

6.8	6.2	8.3	8.3	5.5	4.78	4.70	4.76	5.9	8.9	8.9	6.5	6.0	6.3
60	33	27	22	15	10		10	16	24	27	32	47	60

08.8

07.0

06.6

08.6

6.7	6.8	8.6	8.6	5.4	4.84	4.78	4.90	5.6	9.0	9.0	7.0	6.3	6.6
60	32	27	22	14	10		10	15	23	26	30	48	60

09.2

06.8

07.5

09.0

6.6	6.4	8.8	8.4	5.9	4.84	4.78	4.83	5.5	8.1	7.8	6.6	6.4
60	32	27	21	15	10		10	17	23	27	32	60

08.9

06.8

06.6

09.0

6.9	7.0	6.7	8.8	8.7	5.6	4.9	4.85	4.91	5.6	8.7	9.0	6.6	6.1
60	47	32	26	22	16	10		10	16	24	29	33	60

08.0

06.6

07.1

09.3

7.9	7.6	7.2	7.0	8.8	5.5	5.06	4.95	5.04	5.8	8.9	8.5	6.3	6.1
50	46	29	27	22	15	10		10	16	21	26	36	60

Sta	+	π	-	Elev.
		913.63		
144	+50			10.7
145				10.6
T.P.	4.08	914.72 ✓	499	910.64 ✓
	+50			10.7
146				10.6
	+50			10.6
147				10.4
	+50			10.2
148				10.0
	+50			10.1
149				10.0
	+50			09.9

L.

K.

K.

07.8

06.2

80	78	75	94	98	38	505	995	509	57	87	72	66	58	63
60	40	29	26	23	15	10		10	15	22	29	33	42	60

06.4

07.0

08.4

06.4

75	72	69	72	89	56	508	508	5.11	57	88	92	54	6.2
60	45	29	26	22	15	10		10	15	22	29	39	60

06.4

09.7

08.6

06.7

66	61	59	80	77	48	418	904	412	49	78	80	51	5.3
60	46	28	25	21	15	10		10	17	22	28	37	60

06.7

09.6

08.4

06.7

70	63	59	80	79	51	424	410	421	48	76	81	53	5.5
60	43	29	26	22	15	10		10	15	20	28	35	60

06.6

09.4

08.3

06.6

65	64	61	81	79	48	425	414	4.22	49	79	83	57	5.9
60	41	29	26	21	14	10		10	15	22	28	34	60

06.4

09.0

07.5

06.3

76	77	72	72	84	83	54	453	436	446	50	77	84	74	6.2
60	47	40	28	26	22	16	10		10	15	21	29	32	60

06.3

07.3

06.9

06.0

79	79	78	87	87	53	468	449	4.60	55	88	88	78	7.5
60	43	29	27	22	15	10		10	15	23	28	35	60

05.9

06.9

06.2

05.0

82	85	86	77	95	56	486	468	488	57	91	84	87	80	8.2
60	41	29	26	22	14	10		10	15	22	27	33	42	60

05.3

06.0

06.1

05.2

83	84	86	94	75	54	48	464	480	56	93	79	83	7.9
60	45	30	28	22	14	10		10	15	23	28	33	60

04.8

06.4

06.9

05.9

80	78	78	88	88	55	485	475	486	57	82	88	79	6.9	6.3
60	45	30	27	23	14	10		10	16	22	30	32	44	60

05.9

07.1

08.1

06.5

66	67	66	80	82	53	485	480	488	55	88	81	68	5.9	6.3
60	50	30	27	22	14	10		10	16	24	29	31	44	60

06.2

07.9

Sta	+	Σ	-	Elev.
		919.72		
150				10.1
T.P.	439	919.47 ✓	469	910.08 ✓
+50				10.1
151				10.1
+50				10.0
152				9.8
+50				9.7
153				9.7
+50				9.8
154				9.8
+50				9.8
155				9.7
T.P.	441	919.12 ✓	476	909.71 ✓

Lt

K

Rt

09.5

06.3

$\frac{56}{60}$	$\frac{49}{39}$	$\frac{83}{28}$	$\frac{84}{23}$	$\frac{54}{15}$	$\frac{479}{10}$	$\frac{467}{10}$	$\frac{471}{15}$	$\frac{53}{15}$	$\frac{77}{22}$	$\frac{81}{26}$	$\frac{66}{29}$	$\frac{57}{44}$	$\frac{62}{60}$
-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

09.3

06.3

$\frac{55}{60}$	$\frac{54}{47}$	$\frac{52}{33}$	$\frac{82}{26}$	$\frac{81}{22}$	$\frac{50}{16}$	$\frac{492}{10}$	$\frac{483}{10}$	$\frac{491}{15}$	$\frac{50}{22}$	$\frac{81}{28}$	$\frac{80}{32}$	$\frac{56}{45}$	$\frac{53}{60}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------

06.4

08.9

09.2

06.3

$\frac{57}{60}$	$\frac{56}{42}$	$\frac{53}{39}$	$\frac{82}{28}$	$\frac{80}{23}$	$\frac{51}{15}$	$\frac{447}{10}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------

06.2

08.7

$\frac{439}{10}$	$\frac{445}{15}$	$\frac{51}{20}$	$\frac{72}{27}$	$\frac{83}{31}$	$\frac{58}{44}$	$\frac{52}{60}$
------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------

08.7

06.5

$\frac{57}{60}$	$\frac{57}{49}$	$\frac{58}{32}$	$\frac{80}{27}$	$\frac{81}{22}$	$\frac{51}{15}$	$\frac{451}{10}$	$\frac{448}{10}$	$\frac{455}{15}$	$\frac{51}{22}$	$\frac{80}{27}$	$\frac{80}{31}$	$\frac{60}{44}$	$\frac{52}{60}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------

06.5

08.5

08.6

07.0

$\frac{59}{60}$	$\frac{59}{45}$	$\frac{58}{28}$	$\frac{75}{26}$	$\frac{76}{21}$	$\frac{52}{14}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

06.2

08.7

$\frac{443}{10}$	$\frac{475}{15}$	$\frac{53}{22}$	$\frac{81}{27}$	$\frac{83}{31}$	$\frac{58}{44}$	$\frac{52}{60}$
------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------

08.2

06.8

$\frac{61}{60}$	$\frac{63}{44}$	$\frac{67}{29}$	$\frac{77}{25}$	$\frac{74}{20}$	$\frac{54}{15}$	$\frac{476}{10}$	$\frac{473}{10}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------

06.2

08.6

$\frac{472}{10}$	$\frac{55}{15}$	$\frac{83}{21}$	$\frac{82}{27}$	$\frac{82}{31}$	$\frac{59}{44}$	$\frac{55}{60}$
------------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

08.2

06.5

$\frac{61}{60}$	$\frac{63}{42}$	$\frac{60}{28}$	$\frac{80}{23}$	$\frac{79}{20}$	$\frac{53}{14}$	$\frac{479}{10}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------

06.0

08.7

$\frac{471}{10}$	$\frac{483}{15}$	$\frac{51}{22}$	$\frac{85}{27}$	$\frac{84}{31}$	$\frac{58}{44}$	$\frac{58}{60}$
------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------

08.2

06.2

$\frac{62}{60}$	$\frac{58}{44}$	$\frac{63}{30}$	$\frac{83}{27}$	$\frac{83}{22}$	$\frac{53}{15}$	$\frac{476}{10}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------

06.3

08.4

$\frac{468}{10}$	$\frac{476}{15}$	$\frac{53}{21}$	$\frac{80}{27}$	$\frac{82}{31}$	$\frac{61}{44}$	$\frac{62}{60}$
------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------

08.5

06.3

$\frac{63}{60}$	$\frac{60}{31}$	$\frac{82}{27}$	$\frac{81}{22}$	$\frac{53}{15}$	$\frac{475}{10}$
-----------------	-----------------	-----------------	-----------------	-----------------	------------------

06.2

08.1

$\frac{466}{10}$	$\frac{474}{15}$	$\frac{53}{22}$	$\frac{83}{27}$	$\frac{84}{31}$	$\frac{62}{44}$	$\frac{59}{60}$
------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------

08.4

06.3

$\frac{62}{60}$	$\frac{61}{31}$	$\frac{82}{27}$	$\frac{80}{21}$	$\frac{53}{15}$	$\frac{473}{10}$	$\frac{465}{10}$	$\frac{478}{10}$
-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------

06.0

08.0

$\frac{52}{15}$	$\frac{85}{23}$	$\frac{81}{29}$	$\frac{65}{32}$	$\frac{64}{44}$	$\frac{66}{60}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

08.1

06.1

$\frac{64}{60}$	$\frac{63}{41}$	$\frac{69}{31}$	$\frac{84}{27}$	$\frac{84}{22}$	$\frac{55}{16}$	$\frac{486}{10}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------

05.7

07.9

$\frac{476}{10}$	$\frac{488}{15}$	$\frac{55}{22}$	$\frac{85}{27}$	$\frac{88}{32}$	$\frac{66}{44}$	$\frac{62}{60}$
------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------

Sta	+	π	-	Elev
		9/4.12		

155	+50			9.7
-----	-----	--	--	-----

156				9.6
-----	--	--	--	-----

	+50			9.5
--	-----	--	--	-----

157				9.4
-----	--	--	--	-----

	+50			9.3
--	-----	--	--	-----

158				9.3
-----	--	--	--	-----

	+50			9.2
--	-----	--	--	-----

159				9.0
-----	--	--	--	-----

T.P.	4.80	913.51 ✓	5.11	909.01 ✓
------	------	----------	------	----------

	+50			9.0
--	-----	--	--	-----

160				08.9
-----	--	--	--	------

	+50			08.9
--	-----	--	--	------

Lt

Z

Rt

078 058

057 079

$\frac{65}{60}$	$\frac{63}{32}$	$\frac{83}{28}$	$\frac{81}{22}$	$\frac{49}{14}$	$\frac{491}{10}$	$\frac{442}{10}$	$\frac{448}{10}$	$\frac{51}{16}$	$\frac{82}{22}$	$\frac{84}{28}$	$\frac{62}{32}$	$\frac{58}{26}$	$\frac{65}{60}$
-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

076 058

058 077

$\frac{65}{60}$	$\frac{65}{31}$	$\frac{83}{28}$	$\frac{81}{21}$	$\frac{52}{15}$	$\frac{442}{10}$	$\frac{453}{10}$	$\frac{441}{10}$	$\frac{53}{16}$	$\frac{80}{23}$	$\frac{83}{30}$	$\frac{64}{33}$	$\frac{60}{45}$	$\frac{64}{60}$
-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

076 056

058 081

$\frac{67}{60}$	$\frac{65}{32}$	$\frac{85}{28}$	$\frac{84}{22}$	$\frac{52}{15}$	$\frac{471}{10}$	$\frac{463}{10}$	$\frac{473}{10}$	$\frac{66}{15}$	$\frac{75}{21}$	$\frac{83}{28}$	$\frac{60}{34}$	$\frac{59}{41}$	$\frac{66}{60}$
-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

071

055

053 074

$\frac{68}{60}$	$\frac{70}{31}$	$\frac{85}{21}$	$\frac{86}{22}$	$\frac{53}{15}$	$\frac{479}{10}$	$\frac{475}{10}$	$\frac{471}{10}$	$\frac{51}{15}$	$\frac{87}{22}$	$\frac{88}{27}$	$\frac{67}{34}$	$\frac{65}{46}$	$\frac{68}{60}$
-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

071

052

052 069

$\frac{71}{60}$	$\frac{70}{32}$	$\frac{89}{28}$	$\frac{89}{23}$	$\frac{56}{15}$	$\frac{492}{10}$	$\frac{484}{10}$	$\frac{495}{10}$	$\frac{55}{15}$	$\frac{86}{21}$	$\frac{89}{28}$	$\frac{72}{31}$	$\frac{69}{49}$	$\frac{75}{60}$
-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

063 052

049 064

$\frac{76}{60}$	$\frac{78}{30}$	$\frac{89}{27}$	$\frac{89}{22}$	$\frac{59}{16}$	$\frac{503}{70}$	$\frac{486}{10}$	$\frac{496}{10}$	$\frac{55}{14}$	$\frac{91}{22}$	$\frac{92}{27}$	$\frac{77}{30}$	$\frac{78}{45}$	$\frac{76}{60}$
-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

060

048

036 075

$\frac{82}{60}$	$\frac{81}{31}$	$\frac{92}{30}$	$\frac{93}{23}$	$\frac{57}{15}$	$\frac{503}{10}$	$\frac{492}{10}$	$\frac{501}{10}$	$\frac{58}{15}$	$\frac{104}{23}$	$\frac{105}{29}$	$\frac{66}{34}$	$\frac{67}{43}$	$\frac{70}{60}$
-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	------------------	------------------	-----------------	-----------------	-----------------

066 048

040 076

$\frac{80}{60}$	$\frac{75}{32}$	$\frac{93}{29}$	$\frac{92}{23}$	$\frac{57}{16}$	$\frac{510}{10}$	$\frac{509}{10}$	$\frac{518}{10}$	$\frac{57}{15}$	$\frac{101}{22}$	$\frac{101}{29}$	$\frac{68}{34}$	$\frac{65}{43}$	$\frac{70}{60}$
-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	------------------	------------------	-----------------	-----------------	-----------------

078 048

045 071

$\frac{67}{60}$	$\frac{65}{36}$	$\frac{85}{29}$	$\frac{79}{21}$	$\frac{50}{15}$	$\frac{432}{10}$	$\frac{424}{10}$	$\frac{442}{10}$	$\frac{52}{15}$	$\frac{83}{21}$	$\frac{88}{26}$	$\frac{62}{31}$	$\frac{57}{43}$	$\frac{63}{60}$
-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

075

048

049 073

$\frac{64}{60}$	$\frac{62}{34}$	$\frac{88}{36}$	$\frac{82}{31}$	$\frac{85}{23}$	$\frac{48}{14}$	$\frac{433}{10}$	$\frac{439}{10}$	$\frac{449}{10}$	$\frac{52}{14}$	$\frac{72}{20}$	$\frac{89}{27}$	$\frac{60}{31}$	$\frac{63}{60}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------

071

036

051 072

$\frac{61}{60}$	$\frac{62}{35}$	$\frac{97}{29}$	$\frac{97}{21}$	$\frac{50}{14}$	$\frac{436}{10}$	$\frac{437}{10}$	$\frac{448}{10}$	$\frac{52}{15}$	$\frac{75}{20}$	$\frac{82}{26}$	$\frac{61}{31}$	$\frac{61}{43}$	$\frac{69}{60}$
-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

Sta + π - Elev.

713.31

161

08.8

+56

08.7

+65 = E.C. Bottom Ditch

08.7

B.M.

4.37

908.94

✓
908.95

Lt

K

Rt

06.4

04.4

$$\frac{70}{60} \frac{6.7}{34} \frac{8.7}{29} \frac{8.9}{24} \frac{5.5}{15}$$

$$\frac{4.55}{10}$$

$$\frac{4.52}{10}$$

$$\frac{4.63}{10}$$

$$\frac{5.4}{15}$$

$$\frac{7.7}{19}$$

$$\frac{8.8}{24}$$

$$\frac{6.7}{31}$$

$$\frac{6.8}{46} \frac{6.8}{60}$$

04.5 06.6

05.8

02.7

$$\frac{8.0}{60} \frac{7.6}{32} \frac{10.6}{26} \frac{10.6}{23}$$

$$\frac{5.2}{19}$$

$$\frac{4.65}{10}$$

$$\frac{4.6}{10}$$

$$\frac{4.71}{10}$$

$$\frac{5.6}{15}$$

$$\frac{7.9}{22}$$

$$\frac{10.1}{26}$$

$$\frac{7.6}{30}$$

$$\frac{7.2}{43} \frac{7.6}{60}$$

03.2 05.7

$$\frac{12.2}{150}$$

$$\frac{12.0}{100}$$

$$\frac{11.4}{50}$$

$$\frac{11.4}{16}$$

$$\frac{4.8}{16}$$

$$\frac{4.64}{10}$$

$$\frac{4.60}{10}$$

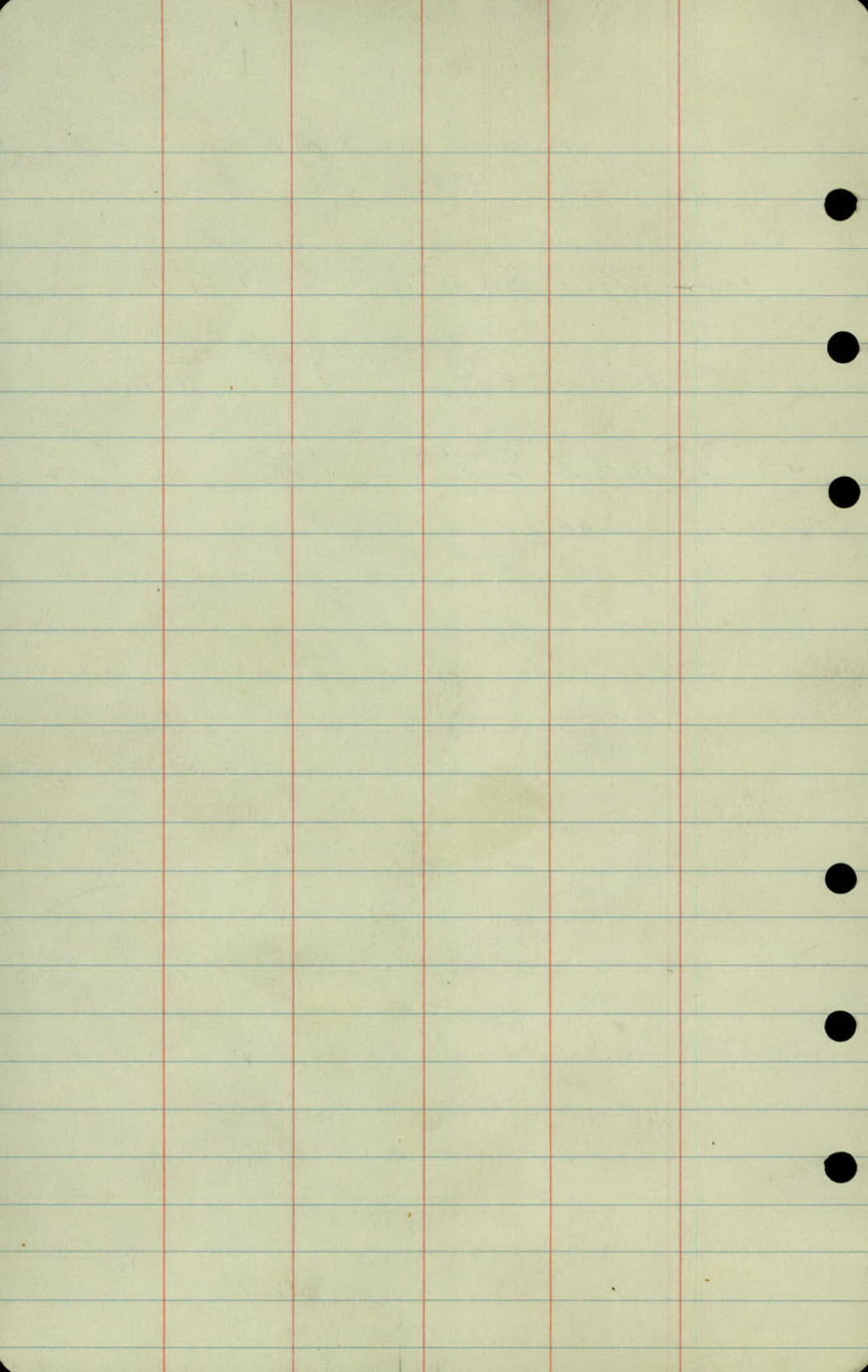
$$\frac{4.73}{10}$$

$$\frac{5.1}{16.6}$$

$$\frac{11.2}{16.6}$$

$$\frac{10.9}{60}$$

Top Mant 160 + 90.95



1
Edgerton St.
slope stakes.

1 Pages

Sta	+	-	Ditch Grade	
B.M.	9.75	906.74		896.99
T.P.	10.24	915.30	1.68	903.06
			Lt Rt	
131			07.0	06.7
+40			07.05	06.75
132			07.1	06.8
+50			07.15	06.85
133			07.2	06.9
+50			07.25	06.95
134			07.3	07.0
+50			07.35	07.05
T.P.	4.67	918.72	4.25	911.05
135			07.4	07.1
+50			07.45	07.15
136			07.5	07.2

Gr. Rod.

Lt

Rt

Lt

Rt

Rt

3pk. in G.P. Edgerton & Lo Rod

8.3

8.6

7.3 $\frac{8.1}{R.05/22.6}$

11.6

8.25

8.55

12.6

 $\frac{258}{R.16} \frac{6.7}{16}$ 6.4 $\frac{6.7}{R.19/27.2}$

13.4

8.2

8.5

14.6

 $\frac{270}{R.12} \frac{7.0}{12}$ 5.4 $\frac{6.4}{R.21/29.4}$

15.2

8.15

8.45

15.8

 $\frac{288}{R.12} \frac{7.0}{12}$ 4.8 $\frac{6.0}{R.25/31.4}$

16.4

8.1

8.40

16.0

 $\frac{280}{R.10} \frac{7.1}{10}$ 4.6 $\frac{6.2}{R.22/31.0}$

16.6

8.05

8.35

16.2

 $\frac{282}{R.10} \frac{7.1}{10}$ 4.5 $\frac{6.6}{R.18/30.4}$

16.8

8.0

8.3

16.2

 $\frac{172}{R.05} \frac{7.5}{5}$ 4.4 $\frac{8.9}{R.2.9/31.6}$

16.8

7.95

8.25

16.4

 $\frac{312}{R.2.4} \frac{5.6}{2.4}$ 4.3 $\frac{5.9}{R.2.9/31.8}$

17.0

8.22

8.62

4.7 $\frac{6.3}{R.2.5/32.4}$

16.8

8.27

8.57

4.6 $\frac{6.2}{R.2.4/31.8}$

17.0

8.22

8.52

4.7 $\frac{6.3}{R.2.3/31.0}$

16.6

Sta.	+	π	-	Ditch Grade	
		915.72		Lt.	Rt.
136	+50			07.55	07.25
R.M.,	4.15	915.59	9.28	911.44	911.40
137				07.6	07.3
	+50			07.65	07.35
138				07.7	07.4
	+50			07.75	07.45
139				07.8	07.5
	+50			07.85	07.55
140				07.9	07.6
	+50			07.95	07.65
141				08.0	07.7
	+50			08.05	07.75
T.P.	4.35	915.32	4.62	910.97	

Gr. Rod.

Lt.

Rt.

8.17	8.7	<u>9.7</u>	$\frac{6.2}{2.5/21.2}$	16.6
------	-----	------------	------------------------	------

36" 50 ft.

8.0	8.3	<u>9.65</u>	$\frac{6.2}{2.1/20.4}$	16.2
-----	-----	-------------	------------------------	------

7.95	8.25	<u>9.7</u>	$\frac{6.8}{2.15/19.2}$	16.2
------	------	------------	-------------------------	------

7.7	8.2	<u>9.75</u>		16.0
-----	-----	-------------	--	------

7.85	8.15	<u>9.75</u>		
------	------	-------------	--	--

7.8	8.1	<u>9.85</u>	$\frac{6.4}{2.17/28.8}$	15.4
-----	-----	-------------	-------------------------	------

7.75	8.05	<u>9.7</u>	✓	
------	------	------------	---	--

7.7	8.0	<u>9.7</u>	✓	15.6
-----	-----	------------	---	------

7.65	7.95	<u>9.6</u>	✓	15.6
------	------	------------	---	------

7.6	7.9	9.55	✓	
-----	-----	------	---	--

7.65	7.85	<u>9.5</u>	✓	15.6
------	------	------------	---	------

				Ditch Grade Lt Rt
141	+	+	-	
		915.32		

142				08.1 07.8
-----	--	--	--	-----------

150				07.9 07.85
-----	--	--	--	------------

143				07.7 07.9
-----	--	--	--	-----------

150				07.5 07.55
-----	--	--	--	------------

144				07.3 08.0
-----	--	--	--	-----------

150				07.2 08.05
-----	--	--	--	------------

145				06.9 08.1
-----	--	--	--	-----------

150				06.7 07.7
-----	--	--	--	-----------

146				06.5 07.1
-----	--	--	--	-----------

150				06.3 06.9
-----	--	--	--	-----------

147				06.1 06.5
-----	--	--	--	-----------

T.R	4.52	914.74	510	910.22
-----	------	--------	-----	--------

Camp Rod

Lt.	Rt.	Lt.	Rt.	Rt.
-----	-----	-----	-----	-----

7.2	7.5		<u>955</u>	✓
-----	-----	--	------------	---

7.4	7.45		<u>4.95</u>	✓
-----	------	--	-------------	---

7.6	7.4	✓	<u>4.9</u>	✓
-----	-----	---	------------	---

7.8	7.35	✓	<u>4.5</u>	✓
-----	------	---	------------	---

8.0	7.3	✓	<u>4.65</u>	✓
-----	-----	---	-------------	---

8.2	7.25	✓	<u>4.6</u>	✓
-----	------	---	------------	---

8.4	7.2	✓	<u>4.65</u>	✓
-----	-----	---	-------------	---

8.6	7.6	17.0	$32.2 / \frac{6.0}{15.46}$	<u>4.6</u>	✓
-----	-----	------	----------------------------	------------	---

8.8	8.0	17.2	$21.8 / \frac{6.5}{12.3}$	<u>4.7</u>	✓
-----	-----	------	---------------------------	------------	---

9.0	8.7	17.6	$32.0 / \frac{6.5}{12.2}$	<u>4.65</u>	
-----	-----	------	---------------------------	-------------	--

9.2	8.5	17.8	$31.2 / \frac{7.5}{12.7}$	4.85	
-----	-----	------	---------------------------	------	--

17.0

Ditch
Grade
L.R. Rb

Sta

+

X

-

914.74

147 +50

059 061

148

057 057

+50

05.65

149

05.6

+50

05.55

150

05.5

+50

05.45

151

05.4

+50

05.35

152

05.3

+50

05.25

T.P.

4.71

914.54

4.91

909.83

Gr. Rod.

Lt. Rt.

8.85 865 17.8

29.4 / 8.1
45.08452

✓

9.05 905 17.6

✓

47

✓

9.1 18.0

✓

46

✓

9.5 17.5

31.4 / 7.4
42.1947

15 / 42.17 / 31.2

9.2 17.8

39.0 / 6.3
42.29475

66 / 42.6 / 33.0

9.25 18.9

32.2 / 7.4
42.19455

58 / 42.5 / 33.0

9.2 18.4

39.0 / 5.7
42.3646

57 / 42.6 / 33.0

9.35 18.6

39.0 / 5.5
42.3946

59 / 42.5 / 33.0

9.4 18.4

39.9 / 5.4
42.4047

57 / 42.7 / 33.0

9.45 18.2

39.0 / 5.7
42.36485

58 / 42.8 / 33.0

9.5 18.2

330 / 6.3
42.3249

60 / 42.8 / 33.0

Sta.	+	X	-	Ditch Grade Lt. Rt.
		914.54		
153				05.2
+50				05.15
154				05.1
+50				05.05
155				05.0
+50				04.95
156				04.9
+50				04.85
157				04.8
T.P.	4.19	913.58	3.15	909.39
+50				04.75
158				04.7

Gr. Rod.
Lt. Rt.

Lt.

Rt.

Rt.

$$9.35 \quad 18.4 \quad \begin{array}{r} 33.0 / 5.7 \\ 12.35 \end{array} \quad \underline{4.7} \quad \begin{array}{r} 5.7 \\ 12.35 / 33.0 \end{array}$$

$$9.4 \quad 18.4 \quad \begin{array}{r} 33.0 / 5.7 \\ 12.37 \end{array} \quad \underline{4.7} \quad \begin{array}{r} 6.4 \\ 12.30 / 33.0 \end{array}$$

$$9.45 \quad 18.6 \quad \begin{array}{r} 33.0 / 5.8 \\ 12.37 \end{array} \quad \underline{4.65} \quad \begin{array}{r} 6.4 \\ 12.31 / 33.0 \end{array}$$

$$9.5 \quad 18.6 \quad \begin{array}{r} 33.0 / 6.1 \\ 12.34 \end{array} \quad \underline{4.65} \quad \begin{array}{r} 6.3 \\ 12.32 / 33.0 \end{array}$$

$$9.55 \quad 18.6 \quad \begin{array}{r} 33.0 / 6.2 \\ 12.34 \end{array} \quad \underline{4.75} \quad \begin{array}{r} 6.6 \\ 12.30 / 33.0 \end{array}$$

$$9.6 \quad 18.6 \quad \begin{array}{r} 33.0 / 6.7 \\ 12.29 \end{array} \quad \underline{4.75} \quad \begin{array}{r} 6.6 \\ 12.30 / 33.0 \end{array}$$

$$9.65 \quad 18.6 \quad \begin{array}{r} 33.0 / 6.5 \\ 12.22 \end{array} \quad \underline{4.9} \quad \begin{array}{r} 6.7 \\ 12.30 / 33.0 \end{array}$$

$$9.7 \quad 18.4 \quad \begin{array}{r} 33.0 / 6.8 \\ 12.29 \end{array} \quad \underline{5.0} \quad \begin{array}{r} 6.5 \\ 12.32 / 33.0 \end{array}$$

$$9.75 \quad 18.2 \quad \begin{array}{r} 33.0 / 7.0 \\ 12.28 \end{array} \quad \underline{5.15} \quad \begin{array}{r} 6.9 \\ 12.27 / 33.0 \end{array}$$

$$9.85 \quad 18.4 \quad \begin{array}{r} 33.0 / 6.2 \\ 12.27 \end{array} \quad \underline{4.2} \quad \begin{array}{r} 6.6 \\ 12.23 / 33.0 \end{array}$$

$$9.90 \quad 18.2 \quad \begin{array}{r} 32.2 / 6.2 \\ 12.20 \end{array} \quad \underline{4.3} \quad \begin{array}{r} 7.0 \\ 12.19 / 33.0 \end{array}$$

Sta.

+

X

-

Ditch
Grade.

919.58

158 +50

09.65

159

04.6

+50

09.55

160

04.50

R.M.

4.58

909.00

895.95

+50

09.45

161

04.4

7/23/38
K.D.
L.H.
L.C.
M.D.G.

Gr. Rod.

Lt.

Rt.

Rt.

$$8.95 \quad 18.2 \quad 21.0 / \frac{7.6}{R.14} \quad \underline{435} \quad \frac{6.5}{R.27/33.0}$$

$$9.0 \quad 18.0 \quad 31.2 / \frac{7.4}{R.14} \quad \underline{45} \quad \frac{6.0}{R.50/33.0}$$

$$9.05 \quad 18.2 \quad 31.6 / \frac{7.4}{R.17} \quad \underline{45} \quad \frac{6.9}{R.27/33.0}$$

$$9.1 \quad 18.0 \quad 31.2 / \frac{7.5}{R.16} \quad \underline{46} \quad \frac{6.3}{R.28/33.0}$$

$$9.15 \quad \quad \quad \underline{46} \quad \frac{6.6}{R.26/33.0}$$

$$9.2 \quad 17.8 \quad \quad \underline{47.5} \quad \frac{7.0}{R.22/32.2}$$

