

Dr. 8 - BK 148

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

.....PLAN.....Survey

.....COUNTY ROAD B2.....

From Edgerton St. To Arcade St.

Road Acc't. No. 66.....

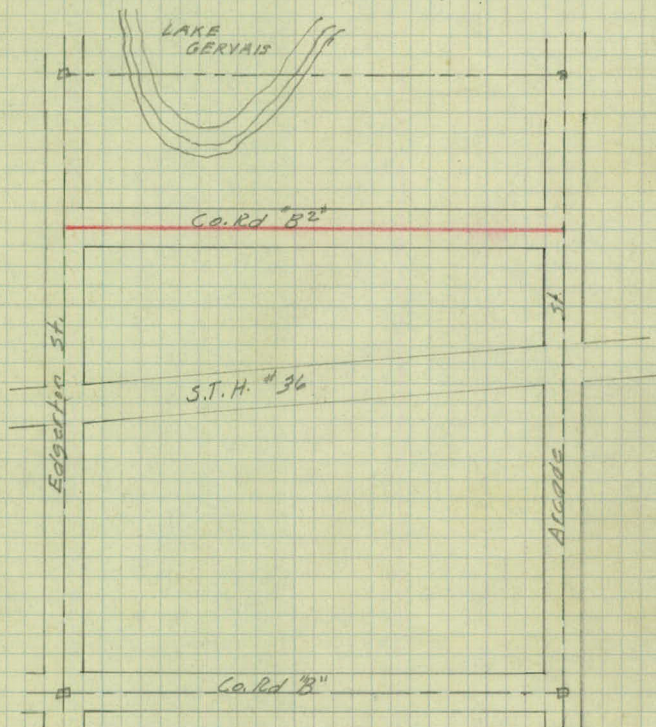
ite Filed 12-29-38.....

File.....

PLAN SURVEY

CO. RD. "B2"

Edgerton St. to Arcade St.



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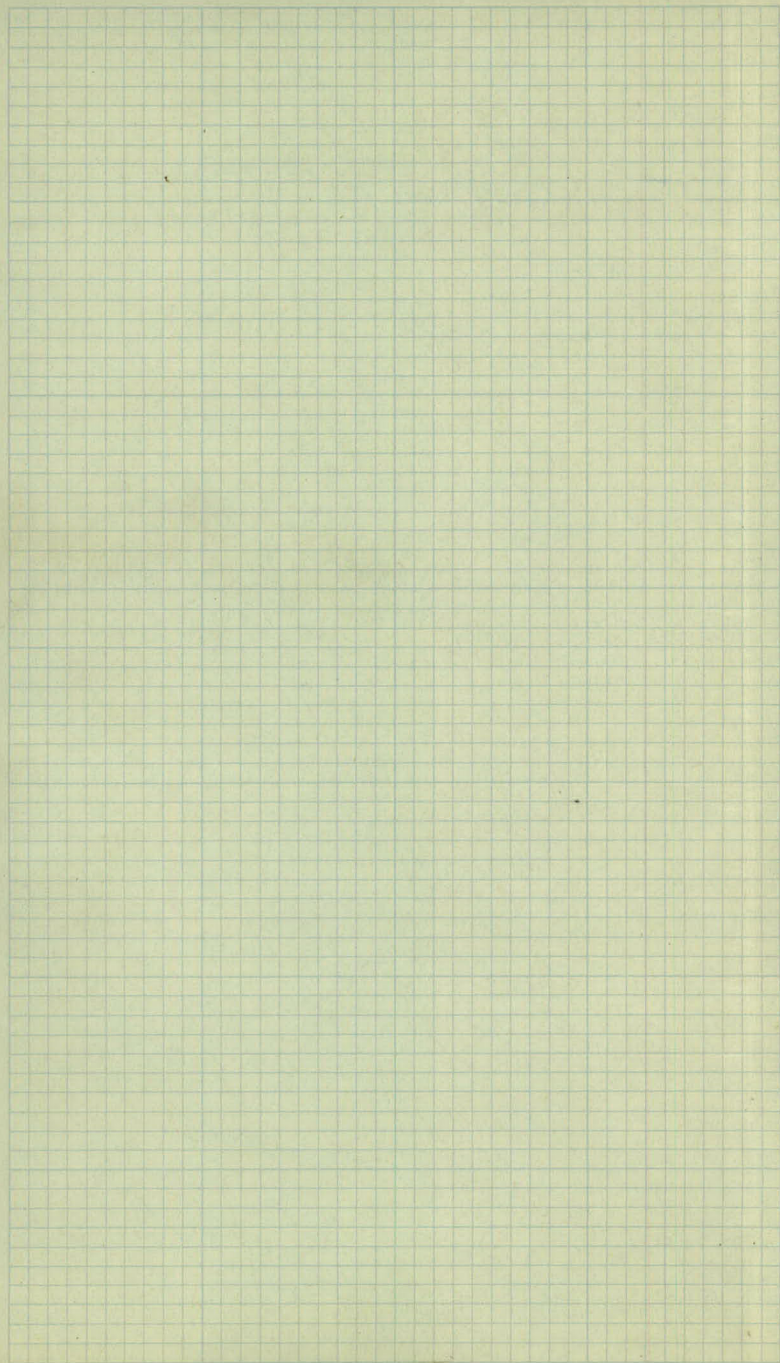
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Additional Xsections 23A-23C.

10/25/38



1

Alignment

Sta.	Point	ΔL	ΔR
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26	+43.22 = E. Arcade St.		
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22	+98.74	P.O.T.	
----	--------	--------	--

13	+21.73	P.I.	0°11'
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10	+90.35	100m	34.13'
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8	+62.05	100m	32.08'
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5	+61.40	100m	31.36'
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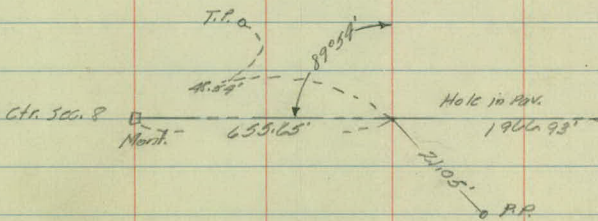
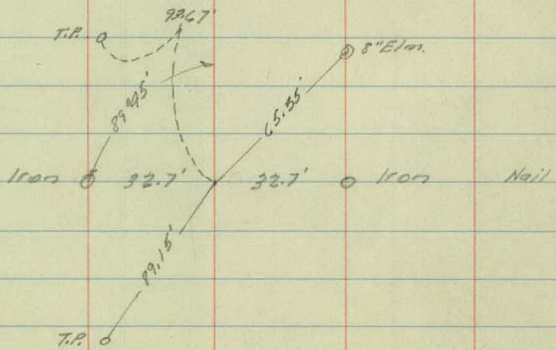
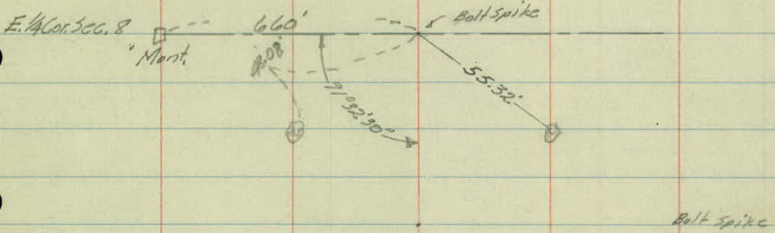
4	+60.72	100m	33.50'
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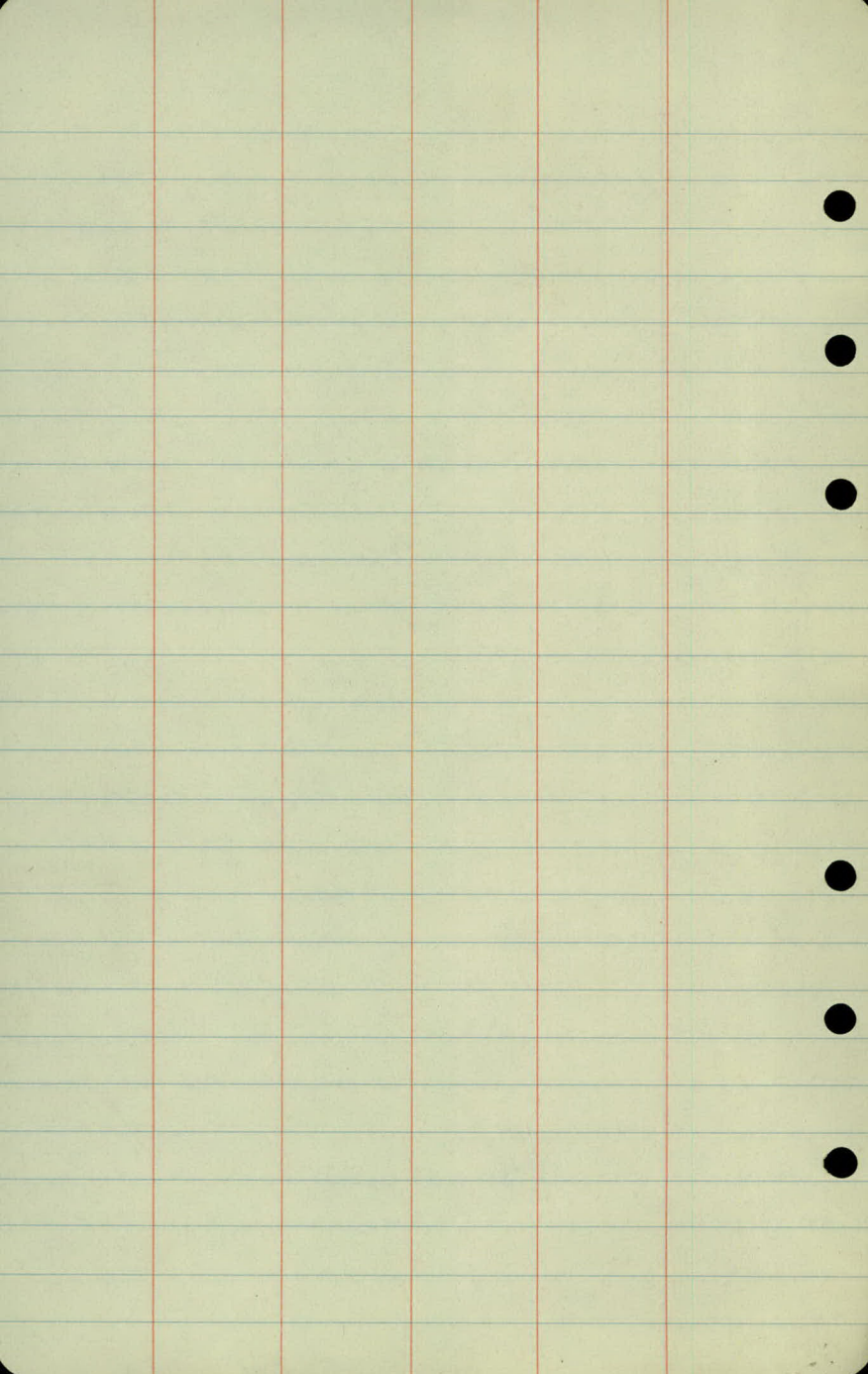
33.96'

0	+00	= E. Edgerton St.	
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K.H.
L.B.H.
L.C.
M.V.G.
10/21/38

2





Topography

+73-End Woods-46'

+55-T.P. & P.R.-24'

5 Woods-30'

10'

13'

Woods-42'

+35-Woods-31'

+27-G.R.-25'

4

(P.R.)
+12-T.P. & P.R.-24'

8'

13'

+75-Woods-27'

+25-20' Cott.-30'

8 Woods-30'

9'

13'

Woods-40'

+58-T.P.-24'

+31-Beg Woods-28'

+48-Beg Woods-40'

2

+18-Exp.-12' X 6' G.M.-11'

9'

11'

(P.R.)
+07-T.P. & P.R.-25'

1

12'

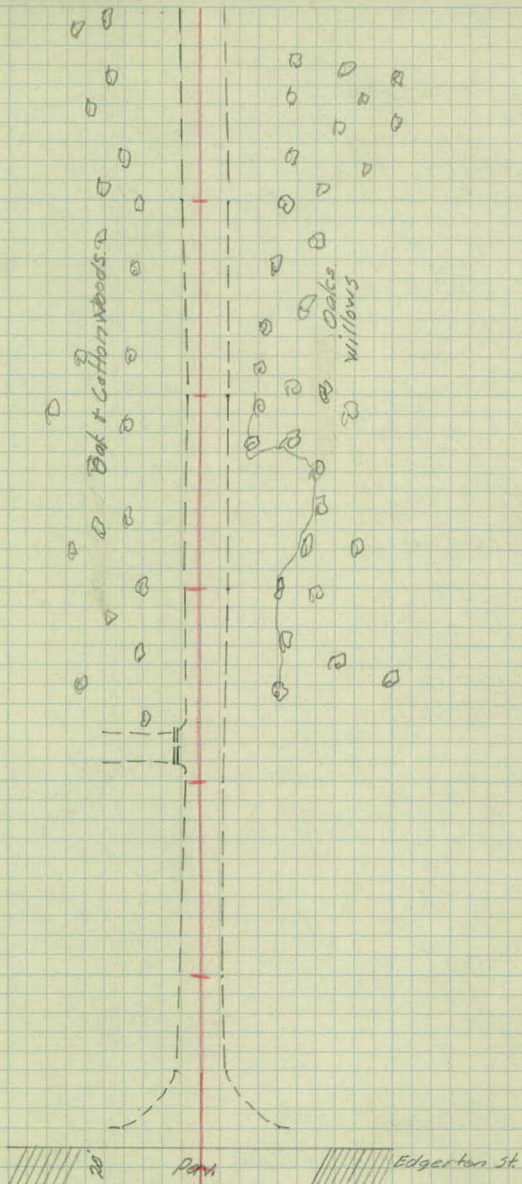
11'

13'

13'

+28-T.P.-40'

0 +00



+36-T.P.-26'

12

10'

14'

+62-Fc. Cor-32'

11

11'

15

+85-T.P.-26'

+29-6.18"X20' C.M. 17.

17

23'

+18-Fc. Cor-31'

10

10'

13'

+75-Beg. Swamp-28'

+54-T.P.-26'

+60-Beg. Swamp-25'

9

5x6 Cor. Ho.-107'

9'

12'

+71-Ent.-15"X20' C.M.-21'

+62-Fc. Cor-33'

+54-End Scot. Oak-32'

+46-T.P.-23'

+30-Ent.-15"X20' C.M.-16'

+68-Ent.-18"X25' C.M.-21'

+58-End Woods-15'

8 T.Linc-32'

9'

13'

Woods-36'

+09-S.W. Cor. Cottage-87'

+05-T.P.-24'

7

T.Linc-31'

11'

10'

+98-Ent.-15"X20' C.M.-16'

+84-Beg Woods-44'

+71-Ent.-15"X20' C.M.-27'

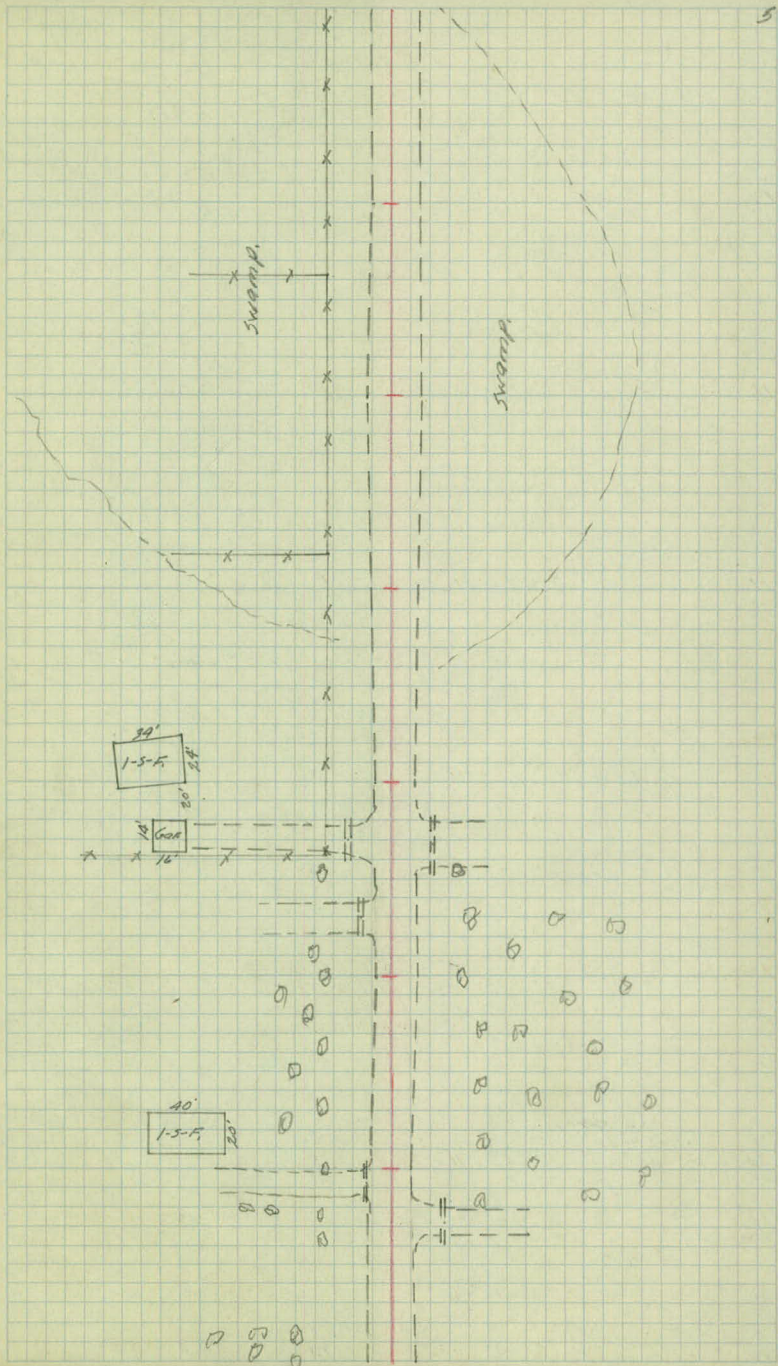
+62-Beg Scot. Oak-35'

+12-End Woods-50'

6

11'

12'



+77-30" Elm-34'

+58-Ent-15" X 40" C. Oak & Y. L-25'

19 +110-T.P.-27'

+70-Bco.Fe.-40'

+56-6" Elm-24'

+65-80g.Woods-10'

+22-6" Elm-22'

18

10'

12'

+59-T.P.-27'

17

11'

11'

+80-Group of 4" Whiteoaks-26'

+67-48" Stump-22'

16

A-18" X 50" C. M.

12' (25' 25') 12'

+83-T.P.-26'

15

+110-Pe.Cor.-34'

12'

12'

+97-Range Tie to Fe.

+57-Ent.

14

+22-82" X 92" C. M.

21'

21'

+11-T.P.-26'

11'

13'

+74-Ent.

13

FC-83'

10'

14'

+33-Edge Bl. Top.

+18-W. End 10' L. 1A-34'
+07-12" Oak-42'

26 +12-End Woods-39'

17'

18'

+67-T.P.-28'

+75

14'

13' +80-18" Oak-36'

+68-18" Oak End Fe.-35'

25 +12-Beg. Woods-40'

11'

10'

Tr. Line & Fe. 46'

+32-T.P.-25'

+36-12" Oak-35'

24

10'

11'

Tr. Line & Fe.-45'

23

12'

12'

Tr. Line & Fe.-35'

+60-T.P.-27'

22

11'

10'

Fe.-42'

21

10'

9'

Woods & Fe.-30'

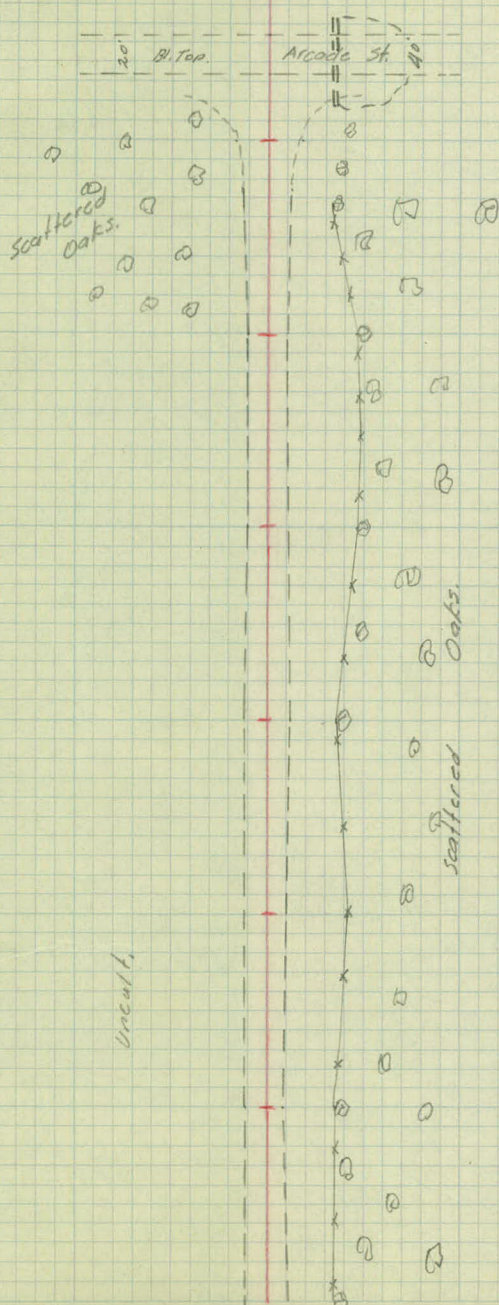
+59-T.P.-28'

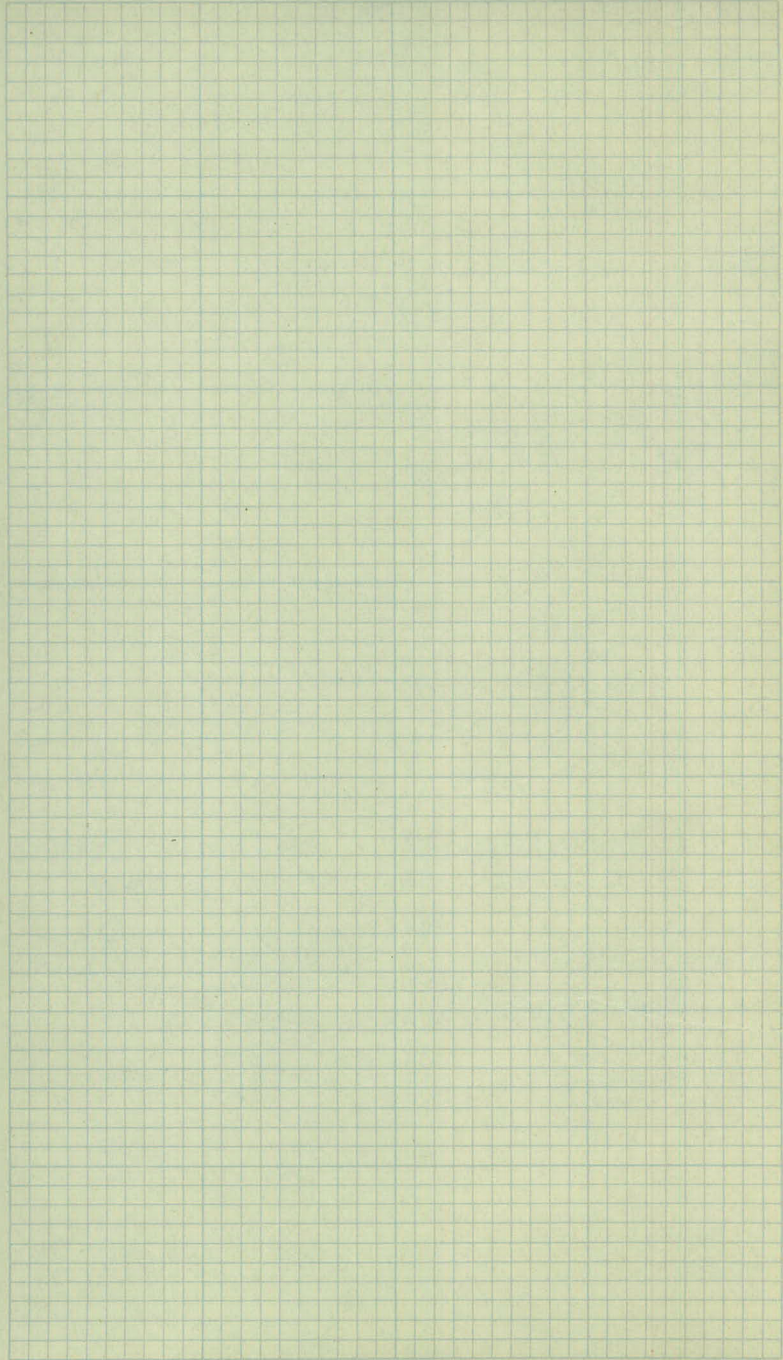
20

11'

11'

Woods & Fe.-34'





Bench Levels

Sta.	+	π	-	Elev.	
B.M.	3.89	876.69			872.80
T.P.	4.03	876.50	4.22	872.47	
T.P.	6.50	874.11	8.89	867.61	
T.P.	12.05	885.66	0.50	873.61	
T.P.	11.62	876.63	0.65	885.01	
B.M.			7.03	887.60	
T.P.	12.46	908.11	0.98	895.65	
T.P.	11.47	919.04	0.54	907.57	
B.M.			3.19	915.85	
T.P.	0.53	906.59	12.98	906.06	
T.P.	1.00	894.39	13.20	893.39	
T.P.	0.28	880.92	13.75	880.69	
B.M.	2.72	870.43	13.21	867.71	
T.P.	7.83	869.94	8.32	862.11	
T.P.	11.59	881.38	0.15	869.79	
T.P.	12.39	893.71	0.06	881.32	
B.M.			3.91	889.80	
T.P.	7.89	903.52	0.08	893.63	
T.P.	1.25	891.42	13.35	890.17	
B.M.			6.52	884.90	

K.A.
L.C.
L.B.H.
M.G.
10/21/38

9

Descriptions

Top Mont. Edgerton St. + Little Canada Rd.

Top Mont. ctn 556.8

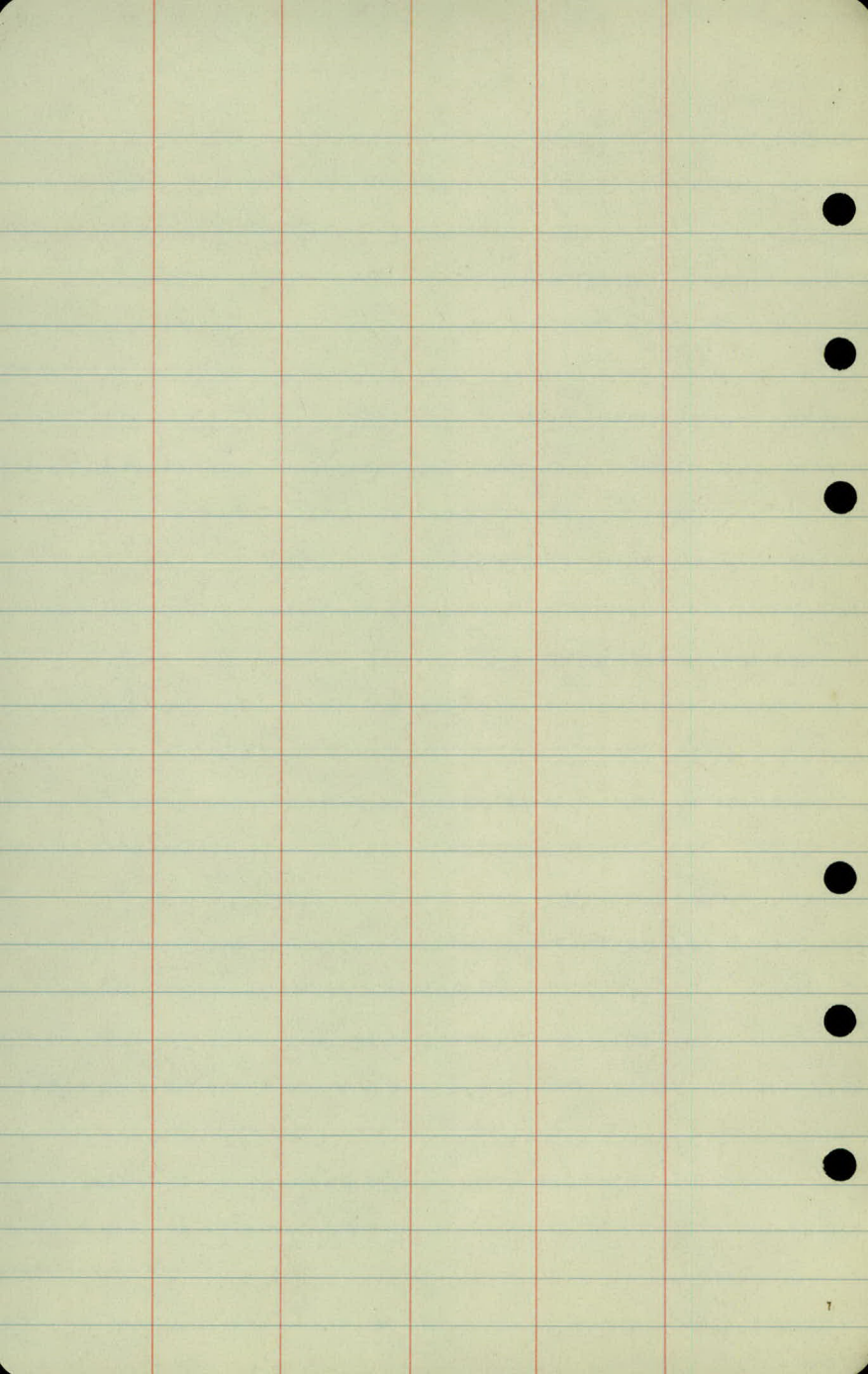
909.40

Top Hole in Pav. Cor'd. 8" + Edgerton St.

Spk. in 18" Oak - 23' Lt. 8 + 95

Spk. in Root of 20" Elm 34' Lt. 5 + 9.19 + 77

Spk. in Root of 18" Oak. 43' Lt. 25 + 8.2



X sections

Sta.	+	π	-	Elev.
B.M.	462	877.42		872.80
T.P.	3.16	874.97	3.61	871.81
T.P.	7.84	875.24	3.57	867.40
T.P.	12.23	887.11	0.36	874.88
T.P.	13.69	900.24	0.56	886.35
B.M.			10.61	889.63 889.60
T.P.	13.65	913.63	0.26	899.98
T.P.	5.94	919.27	0.30	913.33
B.M.	468	920.54	3.40	915.87 915.86 915.85

0 +00

15.86

+10

15.81

+16

15.7

+21

15.5

+31

15.2

Lt.

C.

Rt.

Top Mont. Edgerton St. & Little Canada Rd.

Top Mont. G. to Sec. 8

Top Hole in par. "B" & Edgerton St.

968 $\frac{695}{50}$ 973 $\frac{255}{50}$ $\frac{69}{50}$ $\frac{60}{25}$ $\frac{48}{25}$ $\frac{37}{25}$ $\frac{29}{50}$ $\frac{67}{50}$ $\frac{63}{25}$ 50 $\frac{40}{25}$ $\frac{35}{46}$ $\frac{47}{51}$ $\frac{60}{50}$ $\frac{65}{45}$ $\frac{76}{37}$ $\frac{65}{27}$ $\frac{62}{15}$ 53 $\frac{48}{21}$ $\frac{47}{36}$ $\frac{58}{37}$ $\frac{56}{44}$ $\frac{47}{47}$ $\frac{38}{30}$ $\frac{15}{61}$ $\frac{10}{75}$

Sta	+	X	-	E/cx
		92054		

0	+50			14.3
---	-----	--	--	------

	+81			12.5
--	-----	--	--	------

1				11.4
---	--	--	--	------

	+50			08.7
--	-----	--	--	------

T.P	#1		13.47	907.07
-----	----	--	-------	--------

T.P	13.85	932.58	1.81	918.73
-----	-------	--------	------	--------

0	+50			
---	-----	--	--	--

	+81			
--	-----	--	--	--

1				
T.P	10.75	941.83	1.50	941.08

0	+50			
---	-----	--	--	--

Lt

L

Rt

$$\frac{60}{38} \quad \frac{65}{23} \quad \frac{78}{13} \quad \frac{62}{-} \quad \frac{68}{17} \quad \frac{76}{19} \quad \frac{72}{29} \quad \frac{53}{31} \quad \frac{50}{35}$$

$$\frac{26}{38} \quad \frac{76}{22} \quad \frac{89}{14} \quad \frac{80}{-} \quad \frac{85}{13} \quad \frac{95}{15} \quad \frac{95}{17} \quad \frac{18}{26} \quad \frac{0.7}{32}$$

$$\frac{31}{30} \quad \frac{46}{24} \quad \frac{99}{18} \quad \frac{91}{-} \quad \frac{95}{16} \quad \frac{104}{16} \quad \frac{104}{18} \quad \frac{44}{24} \quad \frac{0.0}{37}$$

$$\frac{-5.7}{75} \quad \frac{0.0}{50} \quad \frac{13.2}{36} \quad \frac{11.4}{25} \quad \frac{12.9}{12} \quad \frac{11.8}{-} \quad \frac{12.1}{18} \quad \frac{13.0}{19} \quad \frac{13.0}{21} \quad \frac{8.6}{24}$$

$$S.S. \quad \frac{69}{75} \quad \frac{39}{53}$$

18.3

$$S.S. \quad \frac{66}{75} \quad \frac{15}{48}$$

20.1

$$S.S. \quad \frac{73}{75} \quad \frac{19}{40}$$

21.2

27.5

$$\frac{145}{60} \quad \frac{144}{75}$$

Sta.	+	π	-	E/cr.	
		941.83			
0	+81				
1					
	+50				
T.P.	0.78	929.69	12.92	928.91	
2	+00				
T.P.	1.20	918.44	12.55	917.14	
T.P.	#1	910.13	11.38	907.06	907.07
2	+00			06.0	
	+28			04.3	
	+54			02.7	
3				899.7	
T.P.	0.76	899.96	10.98	899.20	

14

2

14.

29.3

$$\frac{25}{65} \quad \frac{30}{100}$$

30.4

$$\frac{33}{65} \quad \frac{22}{100}$$

33.1

$$\frac{100}{52} \quad \frac{20}{100}$$

23.7

$$\frac{98}{41} \quad \frac{30}{75}$$

From T.C. #1

$$\frac{25}{30} \quad \frac{106}{25} \quad \frac{48}{18} \quad \frac{17}{9} \quad \frac{41}{16} \quad \frac{45}{17} \quad \frac{57}{20} \quad \frac{55}{20}$$

$$\frac{72}{30} \quad \frac{52}{23}$$

$$\frac{63}{8}$$

$$\frac{58}{15} \quad \frac{62}{16} \quad \frac{73}{16} \quad \frac{75}{18} \quad \frac{62}{19} \quad \frac{55}{29} \quad \frac{453}{41} \quad \frac{470}{50}$$

$$\frac{225}{30} \quad \frac{217}{30} \quad \frac{96}{14} \quad \frac{74}{16} \quad \frac{78}{17} \quad \frac{86}{17} \quad \frac{86}{19} \quad \frac{75}{20} \quad \frac{68}{33} \quad \frac{90}{30}$$

$$\frac{262}{36} \quad \frac{250}{29} \quad \frac{192}{13} \quad \frac{112}{10} \quad \frac{109}{17} \quad \frac{108}{18} \quad \frac{119}{20} \quad \frac{119}{21} \quad \frac{105}{41} \quad \frac{118}{41} \quad \frac{92}{50}$$

Sta.	+	X	-	Elev.
		897.96		
3	+50			96.7
4				94.1
	+72			91.7
I.R.	468	894.09	10.55	883.41
	+80			89.6
5				88.7
	+50			85.5
	+78			83.9
	+88			83.4

Lt.

E

Rt.

$$\frac{20.6}{50} \quad \frac{17.5}{30} \quad \frac{41}{10} \quad \frac{33}{33} \quad \frac{35}{13} \quad \frac{36}{20} \quad \frac{4.3}{21} \quad \frac{4.3}{22} \quad \frac{3.5}{23} \quad \frac{4.2}{50}$$

$$\frac{16.4}{50} \quad \frac{16.8}{28} \quad \frac{7.3}{11} \quad \frac{5.9}{12} \quad \frac{5.9}{19} \quad \frac{6.5}{19} \quad \frac{6.4}{23} \quad \frac{6.0}{23} \quad \frac{7.0}{50}$$

$$\frac{21.0}{50} \quad \frac{16.3}{34} \quad \frac{13.5}{18} \quad \frac{11.2}{14} \quad \frac{9.4}{10} \quad \frac{8.3}{14} \quad \frac{8.3}{19} \quad \frac{8.5}{20} \quad \frac{9.3}{22} \quad \frac{9.3}{23} \quad \frac{8.5}{23} \quad \frac{10.0}{50}$$

$$\frac{12.3}{50} \quad \frac{7.9}{31} \quad \frac{5.6}{16} \quad \frac{5.4}{10} \quad \frac{4.5}{13} \quad \frac{4.8}{13} \quad \frac{5.0}{19} \quad \frac{5.9}{21} \quad \frac{5.9}{22} \quad \frac{5.1}{23} \quad \frac{5.6}{50}$$

$$\frac{12.1}{50} \quad \frac{8.8}{37} \quad \frac{6.2}{23} \quad \frac{7.1}{17} \quad \frac{6.5}{11} \quad \frac{5.4}{15} \quad \frac{6.1}{20} \quad \frac{6.5}{21} \quad \frac{7.2}{23} \quad \frac{7.2}{23} \quad \frac{6.5}{24} \quad \frac{6.3}{35} \quad \frac{3.6}{40} \quad \frac{4.8}{50}$$

$$\frac{7.1}{50} \quad \frac{6.1}{41} \quad \frac{4.4}{27} \quad \frac{11.3}{22} \quad \frac{10.9}{15} \quad \frac{9.5}{12} \quad \frac{8.6}{16} \quad \frac{8.7}{21} \quad \frac{9.8}{25} \quad \frac{9.8}{25} \quad \frac{9.2}{24} \quad \frac{9.0}{27} \quad \frac{10.5}{39} \quad \frac{0.0}{50}$$

$$\frac{7.5}{50} \quad \frac{4.8}{30} \quad \frac{12.5}{22} \quad \frac{12.6}{17} \quad \frac{11.7}{15} \quad \frac{11.0}{10} \quad \frac{10.2}{12} \quad \frac{10.6}{20} \quad \frac{10.6}{20} \quad \frac{11.1}{21} \quad \frac{11.7}{27} \quad \frac{0.7}{40} \quad \frac{0.3}{50}$$

$$\frac{7.6}{50} \quad \frac{5.5}{31} \quad \frac{12.8}{23} \quad \frac{12.3}{20} \quad \frac{11.7}{4} \quad \frac{10.7}{12} \quad \frac{11.2}{12} \quad \frac{11.3}{19} \quad \frac{11.7}{20} \quad \frac{11.7}{26} \quad \frac{7.5}{33} \quad \frac{5.7}{50}$$

Sta + T - Elev.

894.09

6 +00

82.7 •

+57

79.5 •

T.R

0.26

880.71

12.64

880.45

+04

78.1 •

7

77.1 •

+50

74.2 •

8

71.7 •

+50

69.2 •

B.M.

1.19

868.90

12.96

867.75

(867.71)

+75

68.0 •

Lt

A

Rt.

$$\frac{81}{50} \frac{61}{31} \frac{133}{22} \frac{129}{19} \quad \frac{122}{10} \quad \frac{114}{73} \frac{119}{21} \frac{120}{22} \frac{125}{26} \frac{125}{35} \frac{78}{41} \frac{63}{50} \frac{60}{50}$$

$$\frac{133}{50} \frac{129}{27} \frac{168}{22} \frac{148}{17} \frac{155}{11} \frac{146}{11} \frac{147}{25} \frac{147}{26} \frac{164}{27} \frac{164}{27} \frac{140}{29} \frac{140}{33} \frac{97}{41} \frac{87}{50}$$

$$\frac{40}{50} \frac{44}{35} \frac{42}{18} \frac{52}{15} \frac{34}{11} \frac{26}{10} \frac{27}{24} \frac{31}{26} \frac{50}{28} \frac{50}{30} \frac{31}{39} \frac{31}{37} \frac{18}{50} \frac{64}{50}$$

$$\frac{57}{50} \frac{52}{30} \quad \frac{42}{11} \quad \frac{56}{11} \frac{41}{24} \frac{40}{26} \frac{51}{28} \frac{51}{29} \frac{42}{33} \frac{40}{36} \frac{33}{50} \frac{13}{50}$$

$$\frac{28}{50} \frac{92}{40} \frac{95}{13} \frac{75}{11} \frac{65}{13} \frac{70}{32} \frac{72}{30} \frac{42}{50}$$

$$\frac{114}{50} \frac{107}{26} \frac{119}{14} \quad \frac{100}{10} \quad \frac{90}{13} \frac{96}{33} \frac{104}{50} \frac{95}{50}$$

$$\frac{137}{50} \frac{138}{22} \frac{147}{21} \frac{142}{16} \frac{122}{12} \frac{115}{15} \frac{118}{21} \frac{130}{40} \frac{125}{50} \frac{124}{50}$$

Spk. in 18" Oak 33' Lt. 8145

$$\frac{48}{50} \frac{56}{32} \frac{13}{10} \frac{09}{14} \frac{13}{50} \frac{00}{50}$$

Sta.

+

A

-

E/cv.

868.90

8 129

67.6

9

66.9

150

65.1

10

63.8

129

150

62.6

11

61.9

Lt

L

Rt

57.71

 $\frac{11.19}{50}$
 Fl. Lake Gervais

$$\frac{51}{50} \frac{55}{32} \frac{57}{20} \frac{20}{12}$$

$$\frac{13}{19} \frac{21}{21} \frac{42}{21} \frac{46}{34} \frac{53}{50}$$

$$\frac{67}{50} \frac{72}{30} \frac{68}{19} \frac{23}{11} \frac{20}{17} \frac{25}{17} \frac{51}{22} \frac{52}{34} \frac{57}{50}$$

$$\frac{82}{50} \frac{88}{29} \frac{91}{20} \frac{47}{13} \frac{43}{7} \frac{38}{16} \frac{44}{24} \frac{83}{50} \frac{85}{50}$$

$$\frac{96}{50} \frac{96}{29} \frac{96}{19} \frac{66}{14} \frac{58}{7} \frac{51}{13} \frac{56}{16} \frac{60}{24} \frac{95}{50} \frac{93}{50}$$

57.65

 $\frac{11.25}{50}$
 Fl. Gervais

57.9

 $\frac{11.0}{50}$
 Fl. Gervais

$$\frac{86}{50} \frac{80}{37} \frac{99}{31} \frac{100}{21} \frac{80}{16} \frac{69}{11} \frac{63}{16} \frac{69}{26} \frac{98}{22} \frac{97}{50}$$

$$\frac{94}{50} \frac{97}{32} \frac{100}{21} \frac{87}{17} \frac{79}{12} \frac{70}{17} \frac{78}{21} \frac{97}{21} \frac{97}{50}$$

Sta.	+	π	-	Elev.
		86890		
11	+50			61.5
12				62.1
	+50			62.7
T.P.	833	871.97	576	862.14
13				63.2
	+55			63.5
14				63.6
	+22			63.8
	+40			64.0

Lt.

K.

Rt.

$$\frac{99}{50} \frac{78}{32} \frac{99}{21} \frac{87}{18} \frac{79}{12} \frac{74}{-}$$

$$\frac{79}{18} \frac{97}{21} \frac{97}{28} \frac{94}{50}$$

$$\frac{95}{50} \frac{95}{33} \frac{95}{18} \frac{77}{13}$$

$$\frac{98}{-} \frac{75}{14} \frac{81}{19} \frac{97}{23} \frac{93}{50}$$

$$\frac{87}{50} \frac{87}{32} \frac{89}{19} \frac{72}{15} \frac{69}{10} \frac{62}{-}$$

$$\frac{70}{15} \frac{77}{19} \frac{92}{22} \frac{93}{29} \frac{93}{50}$$

$$L.O. \frac{121}{32} \frac{118}{19} \frac{100}{15} \frac{90}{10} \frac{83}{-} \frac{92}{12} \frac{98}{17} \frac{113}{21} \frac{115}{30} \frac{107}{36} \frac{100}{50}$$

$$L.O. \frac{120}{32} \frac{111}{17} \frac{87}{12} \frac{80}{-} \frac{92}{10} \frac{90}{21} \frac{95}{38} \frac{90}{50}$$

$$L.O. \frac{123}{32} \frac{112}{21} \frac{88}{12} \frac{77}{-} \frac{80}{11} \frac{96}{29} \frac{98}{15} \frac{99}{50}$$

59.37

58.72

58.37

$$\frac{115}{50} \frac{113}{35} \frac{108}{21} \frac{1275}{FL. G.W.} \frac{94}{17} \frac{85}{11} \frac{77}{12} \frac{79}{20} \frac{102}{FL. G.W.} \frac{1210}{25} \frac{114}{25} \frac{108}{50}$$

$$\frac{118}{33} \frac{112}{20} \frac{83}{15} \frac{75}{-}$$

$$\frac{75}{12} \frac{77}{21} \frac{97}{31} \frac{100}{50}$$

Sta.	+	π	-	Elev.
		871.47		
14	+50			64.1 •
	+76			64.5 •
15				64.7 •
	+25			64.9 •
	+61			65.4 •
16				65.8 •
	+50			66.3 •
17				67.7 •

Lt.

L

Rt.

$$60. \quad \frac{121}{33} \quad \frac{118}{22} \quad \frac{94}{15} \quad \frac{83}{12}$$

$$\frac{74}{12} \quad \frac{74}{12} \quad \frac{58}{30}$$

$$\frac{123}{50} \quad \frac{119}{36} \quad \frac{108}{26} \quad \frac{85}{18} \quad \frac{77}{12} \quad \frac{70}{12} \quad \frac{72}{11} \quad \frac{70}{22} \quad \frac{74}{31} \quad \frac{62}{50}$$

$$\frac{121}{50} \quad \frac{101}{36} \quad \frac{97}{30}$$

$$\frac{76}{16}$$

$$\frac{68}{16} \quad \frac{72}{22} \quad \frac{77}{22} \quad \frac{35}{50}$$

$$\frac{87}{50} \quad \frac{83}{34} \quad \frac{72}{15} \quad \frac{66}{15} \quad \frac{69}{17} \quad \frac{78}{22} \quad \frac{58}{34} \quad \frac{27}{50}$$

$$\frac{62}{50} \quad \frac{77}{32} \quad \frac{85}{25} \quad \frac{70}{15}$$

$$\frac{61}{18} \quad \frac{68}{27} \quad \frac{81}{40} \quad \frac{74}{40} \quad \frac{68}{50}$$

59.04

H.C.W.

$$\frac{120}{50} \quad \frac{1293}{25} \quad \frac{71}{15} \quad \frac{57}{15}$$

$$\frac{64}{17} \quad \frac{1241}{25} \quad \frac{103}{50}$$

59.06

H.C.W.

$$\frac{121}{50} \quad \frac{118}{26} \quad \frac{65}{17}$$

$$\frac{52}{14} \quad \frac{58}{14} \quad \frac{113}{25} \quad \frac{122}{50}$$

$$\frac{122}{50} \quad \frac{120}{27} \quad \frac{51}{16} \quad \frac{38}{16}$$

$$\frac{47}{14} \quad \frac{129}{29} \quad \frac{123}{50}$$

Sta + π - E/cv

871.47

17 +50

70.7 •

18

+90

T.P.

11.47

882.61

0.33

871.14

18

74.5 •

+90

77.4 •

+70

79.3 •

19

81.0 •

+88

82.5 •

T.P.

13.24

895.93

0.02

882.59

Lt.

L

Rt.

$$\frac{111}{50} \quad \frac{105}{28} \quad \frac{25}{17} \quad \frac{13}{11} \quad \frac{08.12}{9} \quad \frac{23}{14} \quad \frac{11.0}{28} \quad \frac{12.0}{50} \quad L.O.$$

$$\frac{76}{50} \quad \frac{68}{29}$$

$$\textcircled{+3.0}$$

$$\frac{93}{53} \quad \frac{113}{50} \quad L.O.$$

$$\frac{3.7}{50} \quad \frac{37}{27}$$

$$\textcircled{+5.9}$$

$$\frac{64}{33} \quad \frac{84}{50} \quad L.O.$$

$$\frac{94}{16} \quad \frac{87}{10} \quad \frac{81}{10} \quad \frac{85}{10} \quad \frac{93}{15}$$

$$\frac{68}{16} \quad \frac{61}{11} \quad \frac{52}{15} \quad \frac{58}{15}$$

$$\frac{13.2}{50} \quad \frac{12.7}{40} \quad \frac{11.6}{27} \quad \frac{4.8}{16} \quad \frac{4.2}{10} \quad \frac{3.3}{14} \quad \frac{3.7}{29} \quad \frac{14.5}{50} \quad \frac{16.8}{50}$$

$$\frac{11.0}{50} \quad \frac{9.0}{29} \quad \frac{2.8}{17} \quad \frac{2.2}{16} \quad \frac{1.6}{16} \quad \frac{2.0}{12} \quad \frac{2.8}{19} \quad \frac{9.1}{33} \quad \frac{10.3}{42} \quad \frac{9.7}{50}$$

$$\frac{2.8}{50} \quad \frac{4.6}{26} \quad \frac{0.8}{20} \quad \frac{0.6}{13} \quad \frac{0.1}{16} \quad \frac{1.1}{16} \quad \frac{3.1}{23} \quad \frac{9.7}{35} \quad \frac{2.3}{44} \quad \frac{1.9}{50}$$

Sta.	+	T.	-	Elev.
		895.83		
19	+91			83.1 •
	+65			84.4 •
	+78			85.1 •
B.M.	6.08	895.88	6.08	889.75 (889.80)
20				86.3 •
	+50			88.9 •
21				91.5 •
	+50			94.2 •
I.P.	2.67	904.52	1.05	894.83
22				96.6 •

Lt

R

Rt

$$\begin{array}{r} 11.7 \\ 50 \end{array} \quad \begin{array}{r} 12.8 \\ 54 \end{array} \quad \begin{array}{r} 12.9 \\ 12 \end{array} \quad \begin{array}{r} 12.7 \\ 11 \end{array} \quad \begin{array}{r} 13.3 \\ 27 \end{array} \quad \begin{array}{r} 13.8 \\ 50 \end{array} \quad \begin{array}{r} 11.0 \\ 50 \end{array}$$

$$\begin{array}{r} 11.0 \\ 50 \end{array} \quad \begin{array}{r} 11.3 \\ 26 \end{array} \quad \begin{array}{r} 11.5 \\ 11 \end{array}$$

$$\begin{array}{r} 11.4 \\ 17 \end{array} \quad \begin{array}{r} 12.1 \\ 21 \end{array} \quad \begin{array}{r} 8.7 \\ 21 \end{array} \quad \begin{array}{r} 6.8 \\ 50 \end{array}$$

$$\begin{array}{r} 5.9 \\ 50 \end{array} \quad \begin{array}{r} 6.0 \\ 32 \end{array} \quad \begin{array}{r} 11.7 \\ 22 \end{array} \quad \begin{array}{r} 11.2 \\ 11 \end{array} \quad \begin{array}{r} 10.7 \\ 11 \end{array}$$

$$\begin{array}{r} 11.3 \\ 16 \end{array} \quad \begin{array}{r} 6.0 \\ 22 \end{array} \quad \begin{array}{r} 5.5 \\ 33 \end{array} \quad \begin{array}{r} 4.3 \\ 50 \end{array}$$

Spk. in Root of 20° Elm 24' Lt. 19-77

$$\begin{array}{r} 9.1 \\ 50 \end{array} \quad \begin{array}{r} 5.0 \\ 27 \end{array} \quad \begin{array}{r} 10.3 \\ 19 \end{array} \quad \begin{array}{r} 10.3 \\ 11 \end{array}$$

$$\begin{array}{r} 9.6 \\ 16 \end{array} \quad \begin{array}{r} 10.1 \\ 23 \end{array} \quad \begin{array}{r} 9.7 \\ 33 \end{array} \quad \begin{array}{r} 9.0 \\ 30 \end{array} \quad \begin{array}{r} 0.9 \\ 50 \end{array}$$

$$\begin{array}{r} 10.6 \\ 50 \end{array} \quad \begin{array}{r} 0.4 \\ 29 \end{array} \quad \begin{array}{r} 7.8 \\ 18 \end{array} \quad \begin{array}{r} 7.5 \\ 11 \end{array} \quad \begin{array}{r} 7.0 \\ 14 \end{array} \quad \begin{array}{r} 7.6 \\ 24 \end{array} \quad \begin{array}{r} 11.1 \\ 35 \end{array} \quad \begin{array}{r} 12.1 \\ 50 \end{array} \quad \begin{array}{r} 13.8 \\ 50 \end{array}$$

$$\begin{array}{r} 4.7 \\ 18 \end{array} \quad \begin{array}{r} 5.0 \\ 12 \end{array} \quad \begin{array}{r} 4.1 \\ 15 \end{array} \quad \begin{array}{r} 4.8 \\ 15 \end{array}$$

$$\begin{array}{r} 16.7 \\ 28 \end{array} \quad \begin{array}{r} 2.6 \\ 16 \end{array} \quad \begin{array}{r} 1.7 \\ 13 \end{array} \quad \begin{array}{r} 2.2 \\ 18 \end{array} \quad \begin{array}{r} 0.3 \\ 18 \end{array}$$

$$\begin{array}{r} 11.5 \\ 51 \end{array} \quad \begin{array}{r} 0.4 \\ 16 \end{array} \quad \begin{array}{r} 7.9 \\ 13 \end{array} \quad \begin{array}{r} 8.3 \\ 22 \end{array} \quad \begin{array}{r} 1.8 \\ 22 \end{array}$$

Sta.

t

 π

-

E/cv.

709.52

22 t50

98.5 •

23

99.5 •

t58

99.5 •

t70

98.4 •

24

96.9 •

t50

93.7 •

t78

91.6 •

25

90.4 •

T.P. #2

13.34

851.18

lt x rt.

$$\frac{+30}{29} \quad \frac{63}{16} \quad \frac{60}{14} \quad \frac{66}{14} \quad \frac{+4.2}{28}$$

$$\frac{+16}{29} \quad \frac{54}{18} \quad \frac{50}{14} \quad \frac{55}{14}$$

$$\frac{54}{19} \quad \frac{56}{12} \quad \frac{50}{15} \quad \frac{53}{15}$$

$$\frac{+1.7}{30} \quad \frac{+1.2}{38} \quad \frac{+0.9}{30} \quad \frac{65}{19} \quad \frac{65}{12} \quad \frac{61}{11} \quad \frac{6.9}{17} \quad \frac{6.2}{17} \quad \frac{+0.1}{28} \quad \frac{+0.1}{50}$$

$$\frac{10}{30} \quad \frac{20}{31} \quad \frac{78}{22} \quad \frac{85}{18} \quad \frac{76}{14} \quad \frac{81}{17} \quad \frac{85}{17} \quad \frac{58}{30} \quad \frac{36}{50}$$

$$\frac{30}{30} \quad \frac{64}{30} \quad \frac{11.7}{20} \quad \frac{11.4}{11} \quad \frac{108}{12} \quad \frac{115}{12} \quad \frac{115}{18} \quad \frac{8.7}{29} \quad \frac{7.8}{50}$$

$$\frac{24}{30} \quad \frac{59}{29} \quad \frac{136}{20} \quad \frac{133}{12} \quad \frac{129}{12} \quad \frac{135}{20} \quad \frac{134}{20} \quad \frac{9.0}{32} \quad \frac{9.0}{30} \checkmark$$

$$\frac{42}{30} \quad \frac{72}{30} \quad \frac{151}{20} \quad \frac{146}{10} \quad \frac{141}{11} \quad \frac{149}{20} \quad \frac{149}{20} \quad \frac{108}{30} \quad \frac{9.8}{50}$$

Sta	t	X	-	Elev
B.M.	12.71	902.51		887.80

T.P.	12.06	913.73	089	901.67
------	-------	--------	-----	--------

21				
T.P.	11.53	924.38	088	912.85

+50

22

+50

23

+50

T.P.	4.95	926.85	2.48	921.90
------	------	--------	------	--------

22

+50

Lt

E

Rt

Spk. in Root of 80' Elm 34' Lt 19177

$$\frac{76}{78} \quad \frac{101}{59} \quad \frac{94}{42} \quad \frac{99}{32} \quad (22.2) \quad \frac{68}{33} \quad \frac{51}{61} \quad \frac{49}{75}$$

$$\frac{119}{75} \quad \frac{112}{58} \quad \frac{118}{35} \quad (30.2) \quad \frac{77}{42} \quad \frac{71}{75}$$

$$\frac{80}{75} \quad \frac{65}{36} \quad (27.8)$$

$$\frac{70}{75} \quad \frac{74}{60} \quad \frac{68}{34} \quad (25.9)$$

$$\frac{86}{75} \quad \frac{96}{34} \quad (24.9)$$

$$\frac{126}{75} \quad \frac{140}{34} \quad (24.9)$$

$$(30.3) \quad \frac{28}{42} \quad \frac{2.5}{75}$$

$$(28.4) \quad \frac{68}{36} \quad \frac{6.5}{75}$$

3/2	+	X	-	E/cv
		926.85		

23				
T.P.	1.56	915.01	1340	918.45

+38				
T.P.	1.36	903.29	1108	901.93

T.P.	0.52	891.70	12.16	891.18
------	------	--------	-------	--------

25	+50			86.4
----	-----	--	--	------

26				82.6
----	--	--	--	------

+19				81.3
-----	--	--	--	------

14522				80.5
-------	--	--	--	------

B.M.		680	884.90	884.90
------	--	-----	--------	--------

K.H.
L.B.H.
L.C.
Midd.
10/25/98

Lt

k

Rt

27.4

$\frac{12.8}{50}$ $\frac{12.3}{75}$

15.5

$\frac{50}{27}$ $\frac{41}{51}$ $\frac{2.7}{75}$

T.P. #2 from Page 22

$\frac{14}{50}$ $\frac{27}{27}$ $\frac{64}{18}$ $\frac{60}{9}$ $\frac{53}{12}$ $\frac{57}{18}$ $\frac{59}{24}$ $\frac{2.5}{42}$ $\frac{11}{92}$ $\frac{0.7}{50}$

$\frac{106}{50}$ $\frac{110}{32}$ $\frac{102}{26}$ $\frac{108}{20}$ $\frac{100}{13}$ $\frac{91}{17}$ $\frac{9.5}{27}$ $\frac{101}{59}$ $\frac{10.5}{50}$ $\frac{9.7}{50}$

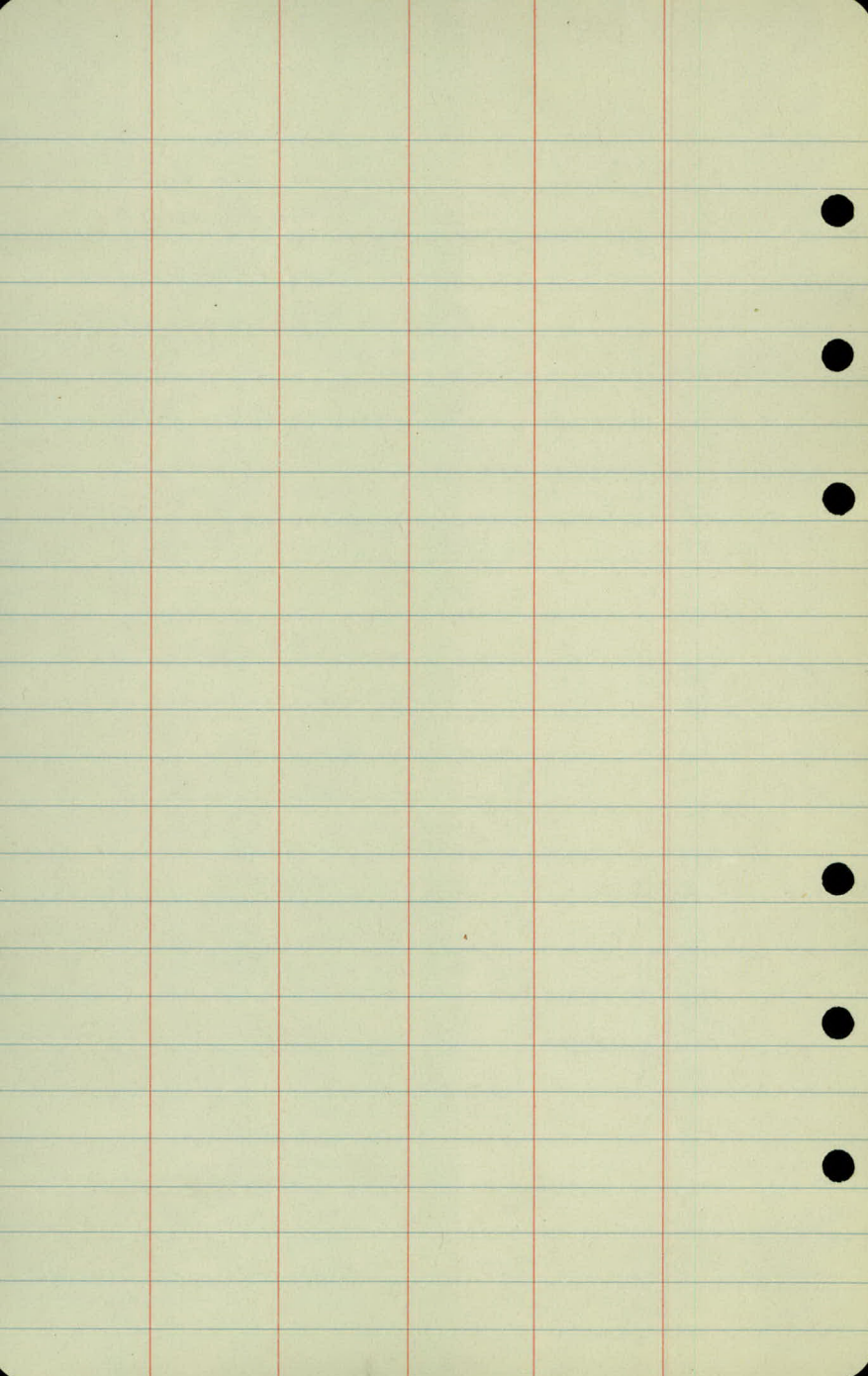
$\frac{12.9}{50}$ $\frac{120}{39}$ $\frac{128}{32}$ $\frac{118}{24}$ $\frac{104}{22}$ $\frac{10.2}{34}$ $\frac{11.3}{50}$ $\frac{9.7}{50}$

$\frac{12.5}{50}$

$\frac{11.2}{50}$

$\frac{9.7}{50}$

Sph. in Root of 18" Oak 43' Lt. 25182



Additional x Sections

Co. Rd. B²"

Sta 0+21 to Sta 2+36

Sta	+	-	Elev
B.M.	528	921.13	915.85
I.P. #1		0.63	920.50
0	+21		15.4
	+31		15.2
	+55		14.1
	+81		12.6
1	+00		11.5
	+50		08.8
T.P. #2	1.82	910.68	12.27 908.86
2	+00		06.1
			6
	+36		03.9
T.P. #3		0.02	910.66
T.P. #1	10.51	931.01	920.50
0	+31		15.2
	+55		14.1

K.A.
L.G.
M.B.
C.N.
2-27-40

23B

Lt

&

Rt

Top Drill Hole & Pav. Edgerton St. & Co. Rd. "B"

$\frac{76}{50} \frac{74}{43} \frac{70}{30} \frac{64}{20} \frac{57}{23} \frac{47}{42} \frac{40}{50} \frac{38}{50}$

$\frac{76}{100} \frac{66}{75} \frac{58}{42} \frac{69}{25} \frac{65}{16} \frac{59}{17} \frac{53}{35} \frac{48}{47} \frac{42}{50} \frac{32}{50}$ P-23B

$\frac{44}{100} \frac{36}{52} \frac{55}{29} \frac{78}{18} \frac{76}{9} \frac{70}{17} \frac{69}{25} \frac{77}{29} \frac{49}{29}$ P-23-B

$\frac{40}{100} \frac{31}{71} \frac{40}{50} \frac{71}{25} \frac{80}{19} \frac{91}{13} \frac{85}{11} \frac{89}{14} \frac{101}{18} \frac{103}{26} \frac{45}{26}$ P-23C

$\frac{45}{100} \frac{46}{63} \frac{66}{38} \frac{96}{20} \frac{102}{11} \frac{96}{14} \frac{100}{15} \frac{112}{19} \frac{109}{24} \frac{48}{36} \frac{11}{36}$ P-23C

$\frac{72}{100} \frac{127}{90} \frac{109}{46} \frac{126}{17} \frac{131}{11} \frac{123}{15} \frac{127}{17} \frac{136}{22} \frac{137}{28} \frac{65}{28}$ P-23C

$\frac{73}{100} \frac{48}{64} \frac{40}{41} \frac{46}{18} \frac{56}{10} \frac{46}{16} \frac{52}{17} \frac{65}{22} \frac{42}{26} \frac{00}{26}$ P-23C

$\frac{145}{100} \frac{117}{78} \frac{76}{48} \frac{61}{37} \frac{68}{25} \frac{74}{9} \frac{68}{15} \frac{73}{17} \frac{84}{19} \frac{82}{20} \frac{70}{29} \frac{69}{29}$ P-23C

Nail in Tree

15.8 $\frac{115}{72} \frac{101}{100}$

16.9 $\frac{113}{38} \frac{70}{48} \frac{58}{54} \frac{25}{100}$

Sta	+	π	-	Elev.
		936.01		
0	+81			12.5
1	+00			11.5
	+50			08.9
2				06.1
	+36			03.9
B.M.			15.09	915.92 (915.85)

Lt

K

Rt

$$\textcircled{17.4} \quad \frac{106}{33} \quad \frac{7.7}{38} \quad \frac{5.2}{44} \quad \frac{3.7}{72} \quad \frac{1.5}{100}$$

$$\textcircled{18.5} \quad \frac{83}{40} \quad \frac{50}{45} \quad \frac{43}{50} \quad \frac{33}{75} \quad \frac{1.1}{100}$$

$$\textcircled{21.2} \quad \frac{98}{36} \quad \frac{60}{41} \quad \frac{51}{52} \quad \frac{32}{74} \quad \frac{15}{100}$$

$$\textcircled{239} \quad \frac{169}{31} \quad \frac{111}{38} \quad \frac{98}{50} \quad \frac{58}{76} \quad \frac{7.6}{100}$$

$$\textcircled{261} \quad \frac{196}{37} \quad \frac{163}{45} \quad \frac{125}{69} \quad \frac{5.4}{100}$$

Sta

+

π

-

Elev

Soundings

Sta	Depth		Depth
	33' Lt.	\$	33' Rt.
8 +00	0.0		0.0
9 +50	5'		8'
10	6'		11'
11	16'		24'
12	14'		16'
13	6'		4'
14	10'		
15	0.0		

	50' Lt.		50' Rt.
15 +90	0.0		
16	5'		0.0
17	12'	+50	6'
			12"
+50	2'		10'
+75	0.0		
18			6'
+90			0.0

Soft Clay

