

Dr. 8 - Bk 147

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ PLAN _____ Survey

_____ COUNTY ROAD "I" _____

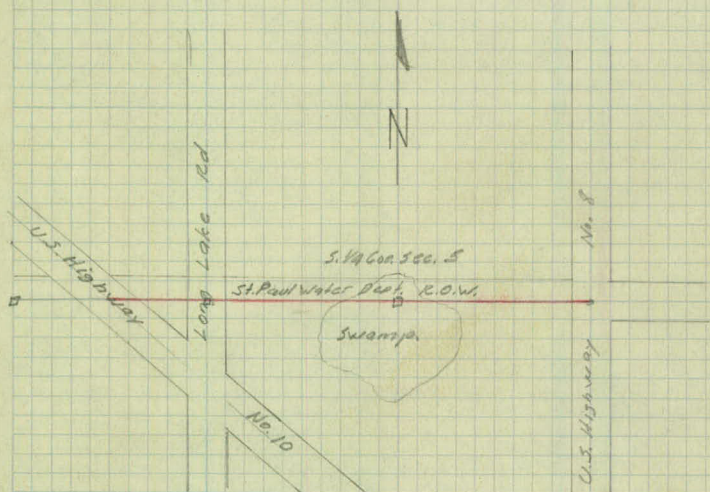
From S.T.H. #10 _____ To S.T.H. #8 _____

Road Acc't. No. 60 _____

Date Filed 12-29-38 _____

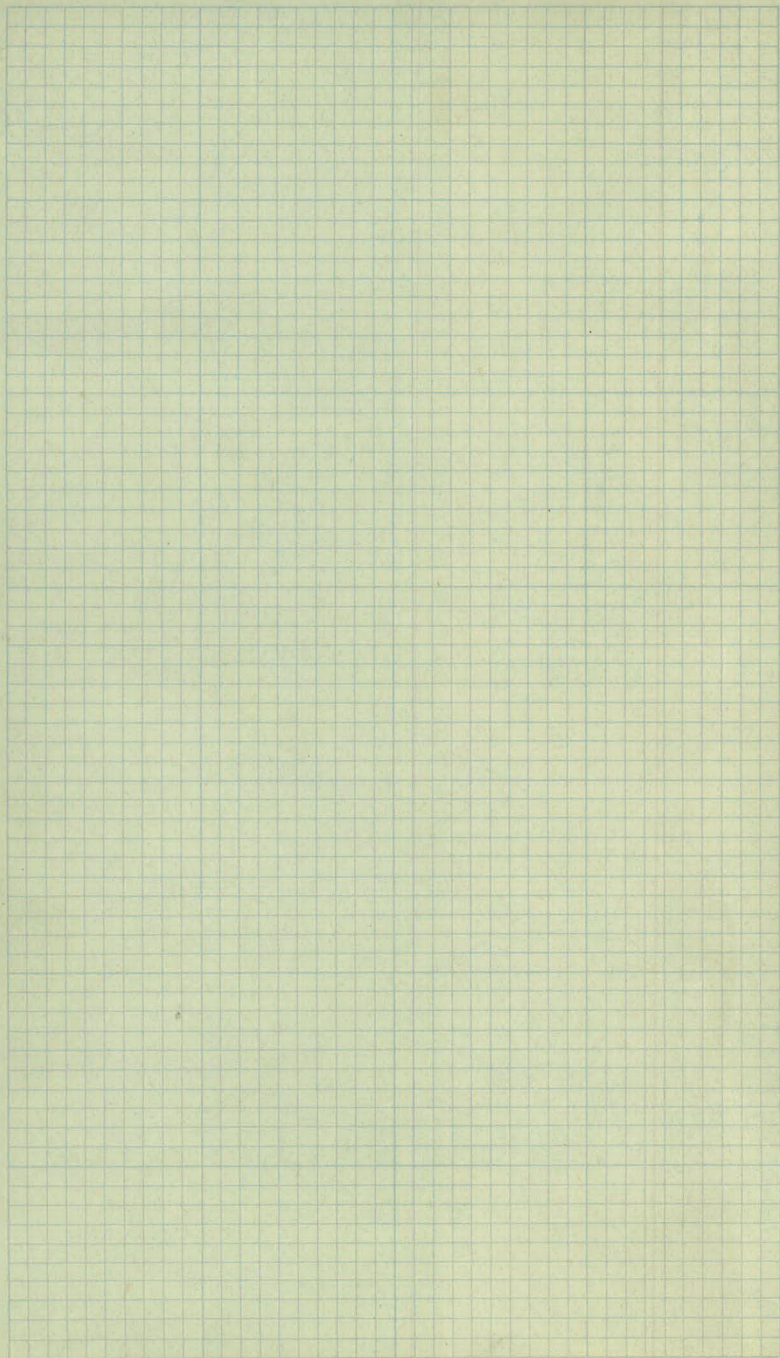
File _____

PLAN SURVEY
CO. RD. "I"
U.S. #10 to U.S. #8



INDEX

Align - 1-4
Topog. - 5-15
Levels - 16-17
& Levels - 18-34



Alignment

Sta

Point

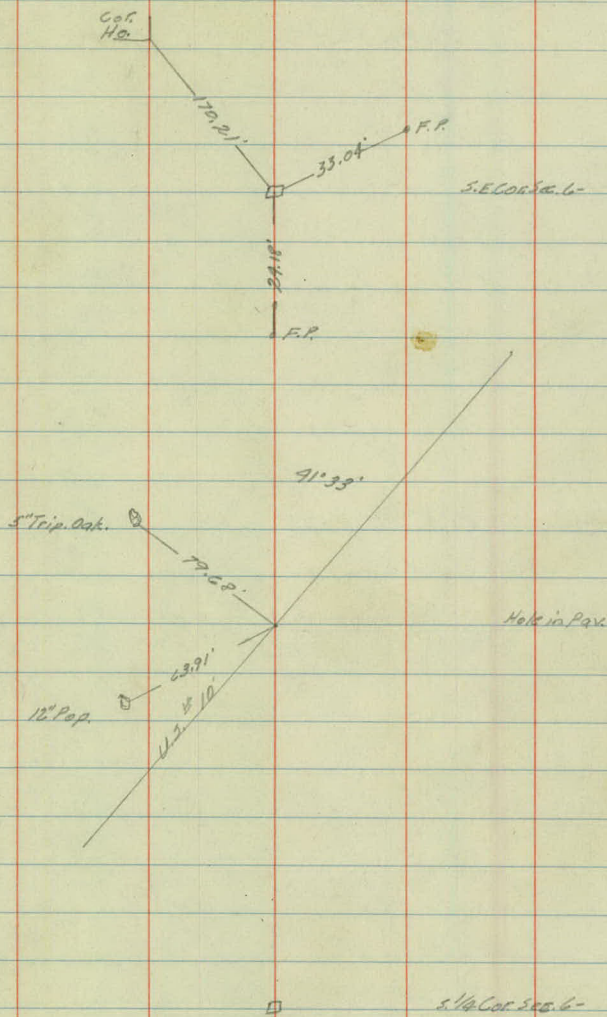
Δ Lt

Δ Rt

12 + 92.63

1° 27'

0 + 00 = ~~U.S.~~ U.S. Highway #10



Sta.

Point

Δ Lt.

Δ Rt.

29 +31.23

P.L.

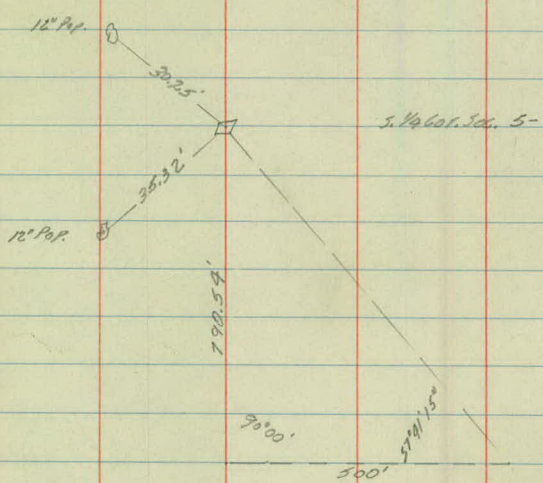
$0^{\circ} 11' 30''$

31 +41.37

P.O.T.

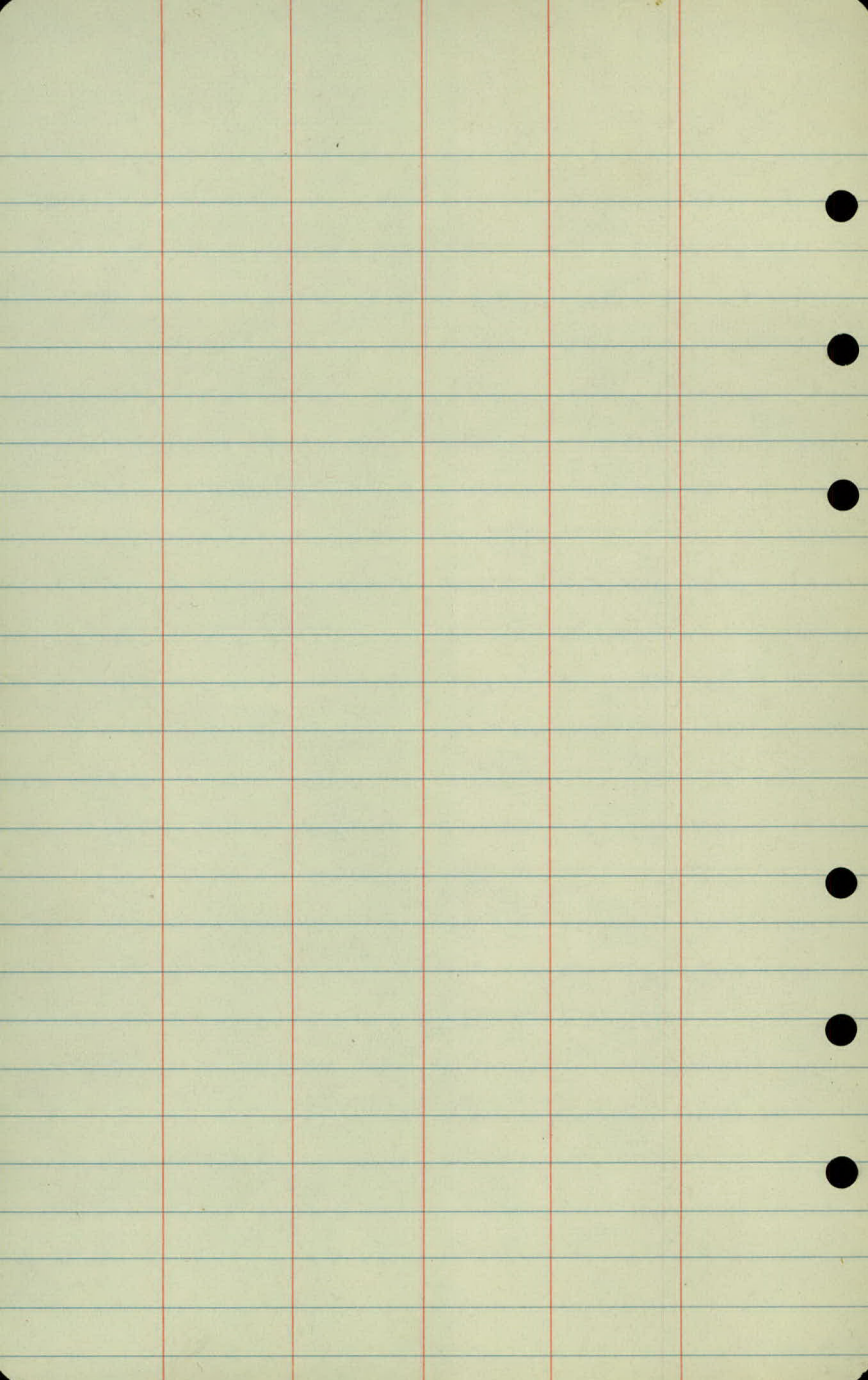
27 +23.53

P.O.T.



68 +10.25 to U.S. 48

Brass Plus in Pav.



Topography

4

3

2

1

0+00

+10-Tr. Ling - 15'

+85-Tr. Ling - 33'-60'

+90-Pes. Pop. Brush & Trs. 33'

+40-Ed Oak Brush & Trs - 25'-15'

+67-Water Vent. - 44'
Long. Weir Box - 48'
5' Square

Brush & Trs - 12'-36'-60'

+40-Brush & Trs - 15'

+25-Bes Oak. Trs & Brush 35'

+66-Long. Weir Box - 48'

+75.5 Trs Oak. - 60'

+35-RK - 33'

inc. 0.0024
Top

Brush

Meadow

Hay

Oaks & Brush

Cult

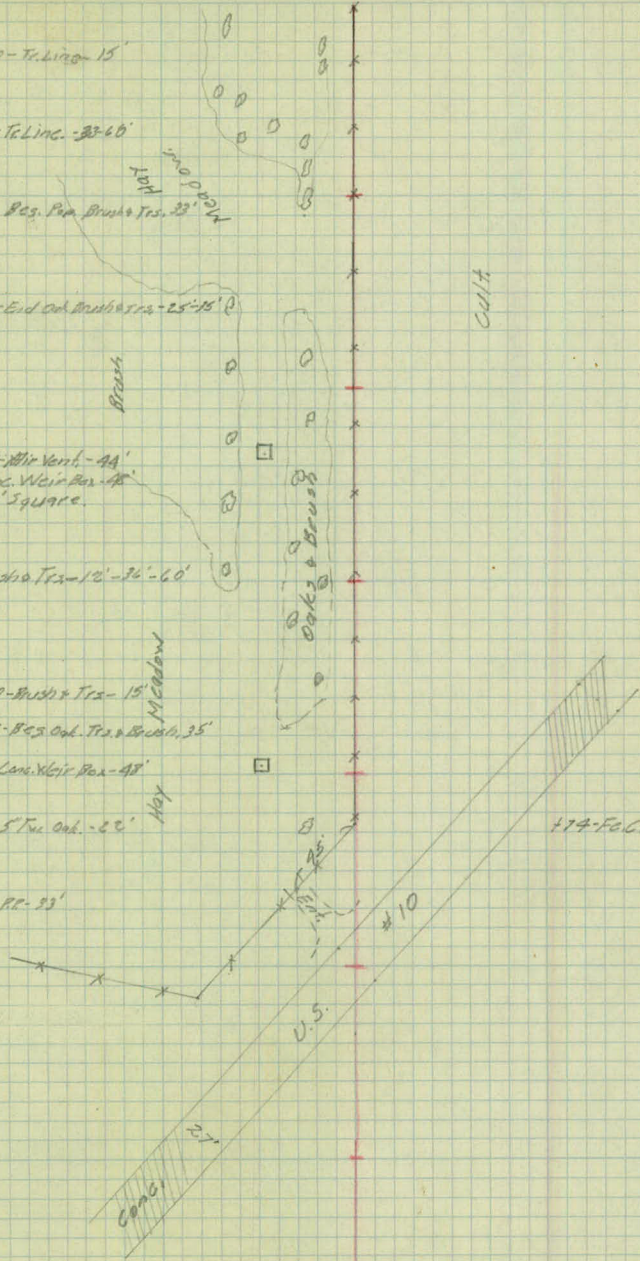
+74-Fa Cor. 00

#10

U.S.

2.7

Comp



11

10

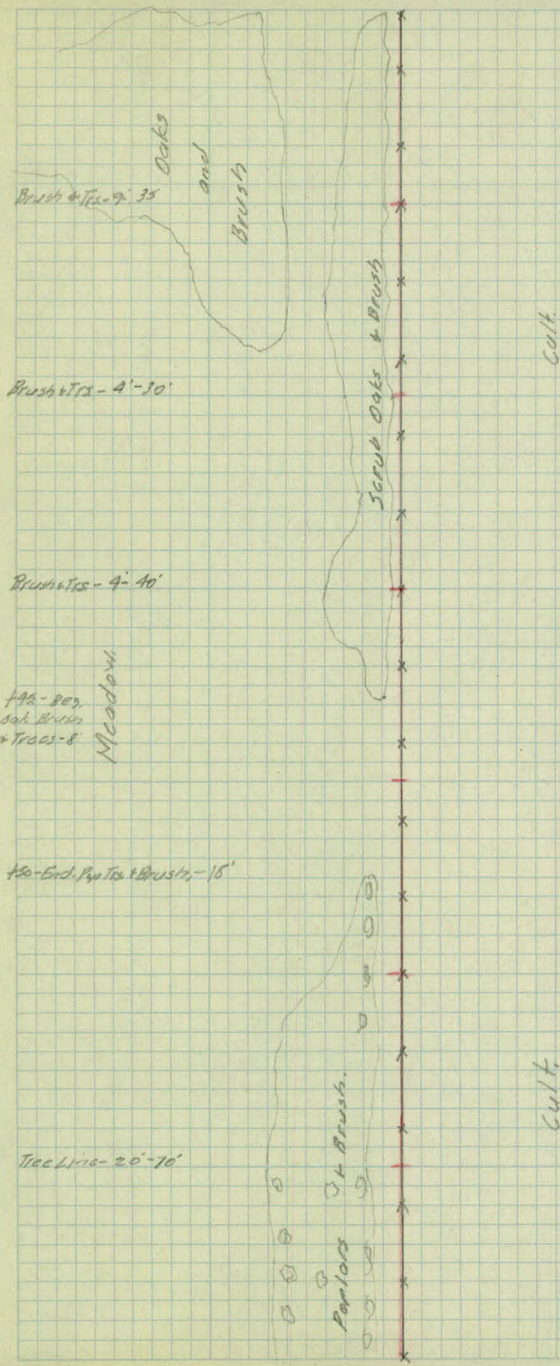
9

8

7

6

5



18

17

16

15

14

13

104-E Shoulder Line

183-W Shoulder Line

12

+53-Weir Box ctr.-48'
 Fir Vent-45'

Cult

Fc.-1'-20'

Fc.-1'-20'

+45 Fc. Cor.-5'

Pasture.

+73-Δ in Fc.-1'
 +60-15" Fir. Oak.-20'

+73-24" Oak.-11' *Fc. Cor.

+79 Fc. Cor.-23'

Fc.-19'

1-S.F.
 20'
 24'

+37-3. W. Cor. Ho.-79'

+62-Fc. Cor.-23'
 +55-15" Oak.-19'

+02-15" Oak. 21'
 Fc.-21'

Ed.

+11 Fc. Fc. Cor.-28'

Long Lake

Ed.

+67-Fc. Cor.-00

25

24

23

22

21

20

19


$$F_2 - 92'$$

$F_c = 20'$

 $F_c \cdot 8'$

185-FC Con-8'

$F_c - 4'$

Fe-1'

Meadows.

Postura

FC-4'

Cult

FC-14

496-Fe. Cor. - 19'

Feb-19

32

31

30

29

28

27

26

+70-Swamp

Fc - 60'-3'

+70-End. Trees - 17'

Tr Line - 24'-28'

1 5' 15' Can.

+56-Weir Box Ctr - 48'

Air Vent. - 45'

Fc - 60'-2' Tr Line - 39'-12'

Fc - 60'-3' Tr Line - 36'

+15-Res. Fa - 3'

Fc - 60'-Tr Line - 37'

Fc - 60' Tr Line - 35'

+31-Woods - 30'

+13-Fc Cor - 00'

Oak Woods

Oaks & Brush

Oak woods

Meadow

+60-Woods - 5'

Tr Line - 10'

Tr Line - 15'

Tr Line - 15'

+21-Woods - 20'

33

38

37

36

35

34

33

+31-Fc Cor-60' x

Water 12'
Tr. Line - 21-55'

Cult.

Water 38' Fc-60'
Tr. Line 28-55'

Water 33' Fc-60'
Tr. Line - 26-55'

Water 40' Fc-60'
Tr. Line - 27-43'

Cult

+10-End-Fc-1'
Water-13' Fc
Tr. Line - 26'

+25-Ber Grove Trees-20'

Fc 1'

+15-Fc Cor-20'
Fc-2

Poplars & Cottonwoods

Swamp

+30-Water-00

46

45

44

43

42

41

40

cult

cult

cult

cult

H15- End Grave Trees 25-30'

H10- Swamp.

53

52

51

50

49

48

47

#14- Weir Box c.k. A¹
 & Bir Vent.

Cult.

#19- F.C. Cor. - 2'

Oaks & Brush

#45- 29° Oak - 2'

Cult.

#10- 20° Oak - 1'

Cult.

Cult.

60

59

58

57

56

55

54

+50-End 15" X 54' C.M. - 21'

+22-So. End 15" X 45' C.M. 28'

+70-End 4" Iron Pipe - 31'

Cult.

Moss
as
Lowland

Wasteland

+32-Fe Coc - 4'

FC - 3'

FC - 2'

Cult.

Cult.

+15-End Woods

Oaks & Brush

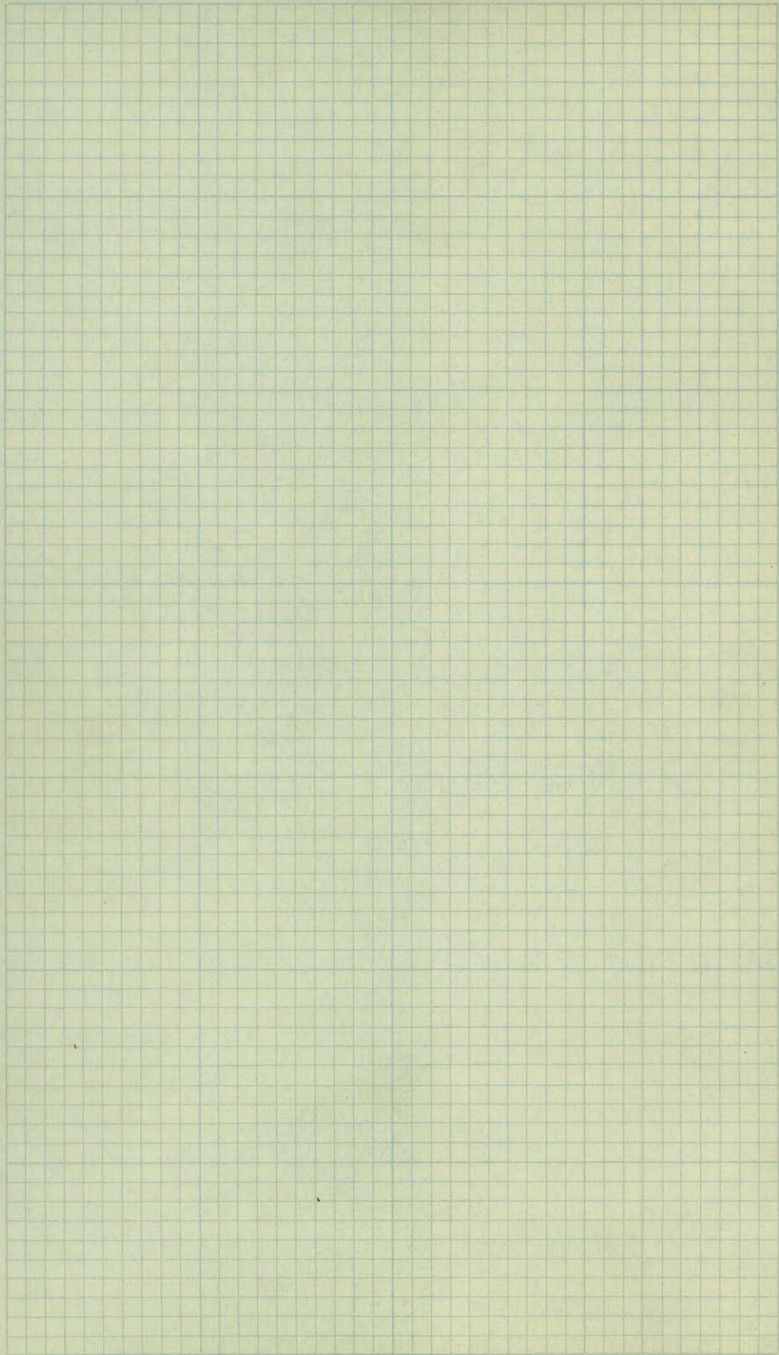
65

64

63

62

61



Bench Levels

Sta	+	-	Elev	
B.M.	4.73	917.90		913.17
I.P.	7.35	918.25	4.00	913.90
I.P.	2.85	914.22	6.88	911.37
I.P.	5.45	914.12	5.55	908.67
B.M.	4.33	914.52	3.93	910.19
I.P.	5.57	912.06	7.03	907.49
I.P.	3.52	917.33	1.25	911.81
B.M.			5.37	911.96
I.P.	4.98	917.92	4.29	912.94
I.P.	1.18	912.89	6.21	911.71
I.P.	5.97	919.19	5.67	907.22
B.M.	2.35	915.26	0.28	912.71
I.P.	2.94	909.39	8.51	906.45
I.P.	5.79	912.66	2.52	916.87
I.P.	2.62	914.23	1.05	911.61
B.M.			3.29	910.94
I.P.	3.55	916.39	1.29	912.84
I.P.	4.01	911.56	9.04	907.35
I.P.	8.15	914.43	5.11	906.25
B.M.			7.06	907.37

Description

Top Pav. Graveland St. & U.S. #10

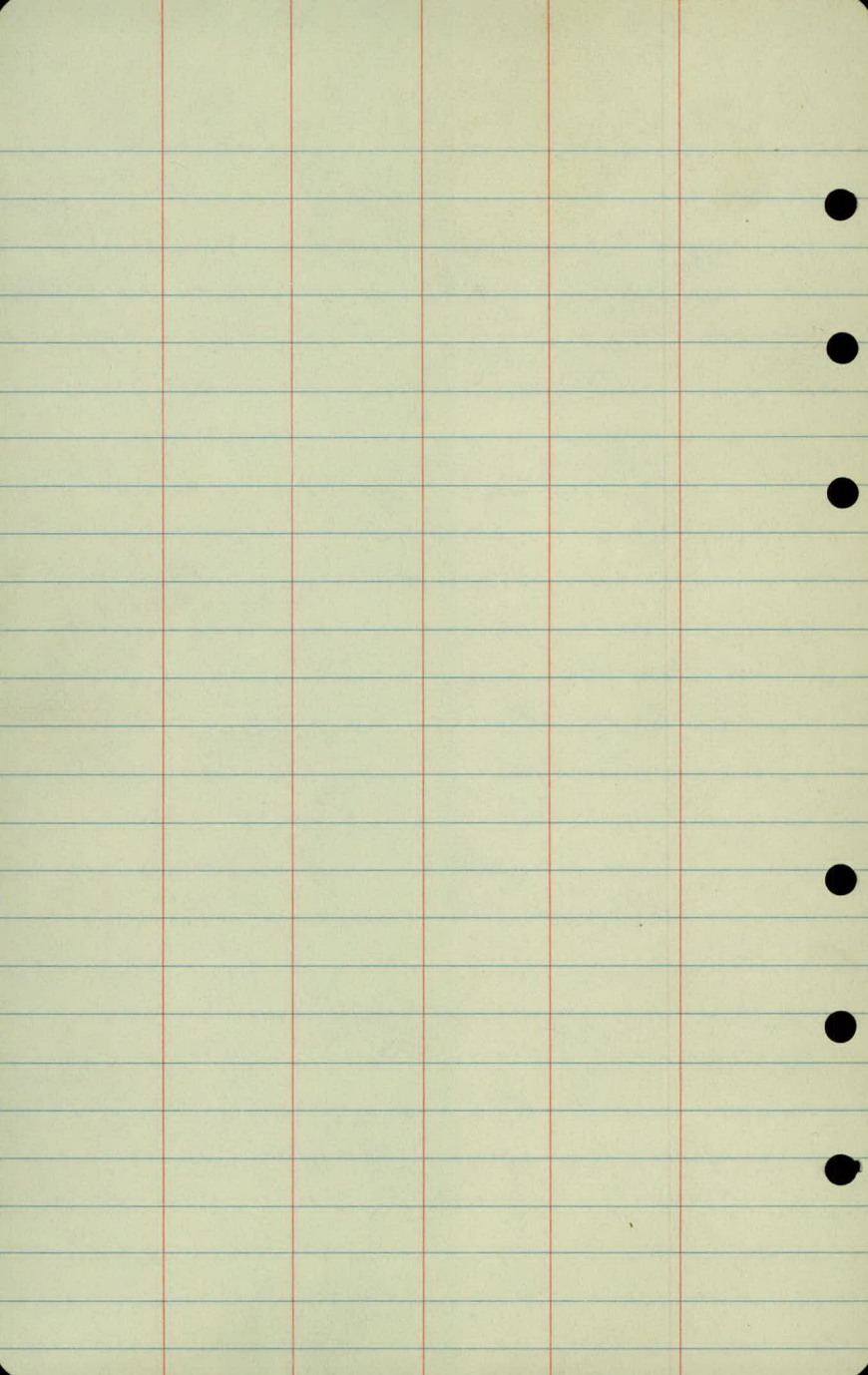
Top Hole in Pav. 0100

Top Mont. Co. Rd. 1" & Long Lake Rd.

Belt 3pk. Top 3ump 2, 29+23.53

Spk. in 20" Oak 1" Rt, 49+10

Brass Plug in Pav. Co. Rd. 1" & U.S. #8



X sections

Note. - X sections from 0 to 42
are + 4 - from R.

Sta	+	Δ	-	Elev.	
B.M.	4.54	917.71			913.17
I.P.	4.19	918.18	3.72	918.99	
I.P.	2.72	913.80	7.10	910.8	
I.P.	5.44	914.06	5.18	908.62	
B.M.	4.21	914.40	3.90	910.16	910.19
0	+00		4.21	10.19	
	+203		4.26	10.14	
	+34		4.4	10.0	
	+47		5.7	08.5	
	+70		5.9	09.0	
1			5.0	09.4	
	+50		4.7	09.7	
2			4.0	10.4	
	+20		3.8	10.6	

Lt

K

Rt.

Top Pav. Graveland St. 94.5 #10

Top Hela in Pav. 0400

$$\frac{-16}{50} \quad \frac{-17}{52} \quad \frac{-09}{20}$$

$$\frac{-17}{50} \quad \frac{-17}{59} \quad \frac{-15}{30} \quad \frac{-09}{14} \quad \frac{+03}{14}$$

$$\frac{0.0}{50} \quad \frac{+01}{24} \quad \frac{+06}{5} \quad \frac{+15}{14} \quad \frac{+15}{25}$$

$$\frac{-07}{50} \quad \frac{0.0}{35} \quad \frac{+02}{21} \quad \frac{-07}{14} \quad \frac{-12}{26} \quad \frac{-01}{39} \quad \frac{+07}{50}$$

$$\frac{-08}{50} \quad \frac{-06}{31} \quad \frac{-02}{7} \quad \frac{-12}{15} \quad \frac{-14}{29} \quad \frac{-13}{50}$$

$$\frac{-0.6}{50} \quad \frac{-0.3}{18} \quad \frac{-0.6}{8} \quad \frac{-0.9}{12} \quad \frac{-1.0}{35} \quad \frac{-0.7}{50}$$

$$\frac{-0.5}{50} \quad \frac{-0.8}{13} \quad \frac{-0.5}{6} \quad \frac{-0.7}{7} \quad \frac{-0.7}{30} \quad \frac{-0.9}{50}$$

$$\frac{-0.5}{50} \quad \frac{-0.5}{20} \quad \frac{-0.4}{15} \quad \frac{-0.4}{7} \quad \frac{-0.8}{8} \quad \frac{-0.7}{40} \quad \frac{-0.8}{50}$$

Sta	t	x	-	Flux
		914.40		
2	+50		3.8	10.6
3			4.7	09.7
	+50		5.3	09.1
4			7.1	07.3
	+50		7.3	07.1
5			7.7	06.7
T.P.	550	912.98	6.92	907.98
	+50		6.8	07.2
6			5.2	07.8
	+30		4.9	08.1
	+60		4.8	08.2
7			5.1	07.9

LH

E

RH

$$\begin{array}{r} -0.8 \\ 53 \end{array} \quad \begin{array}{r} -0.8 \\ 34 \end{array} \quad \begin{array}{r} -0.0 \\ 19 \end{array} \quad \begin{array}{r} -0.4 \\ 9 \end{array} \quad \begin{array}{r} -0.8 \\ 6 \end{array} \quad \begin{array}{r} -0.9 \\ 20 \end{array} \quad \begin{array}{r} -0.7 \\ 35 \end{array} \quad \begin{array}{r} -0.7 \\ 50 \end{array}$$

$$\begin{array}{r} 0.0 \\ 50 \end{array} \quad \begin{array}{r} -0.0 \\ 19 \end{array} \quad \begin{array}{r} -0.3 \\ 5 \end{array} \quad \begin{array}{r} -0.7 \\ 7 \end{array} \quad \begin{array}{r} -0.3 \\ 36 \end{array} \quad \begin{array}{r} -0.3 \\ 50 \end{array}$$

$$\begin{array}{r} +0.5 \\ 50 \end{array} \quad \begin{array}{r} +0.5 \\ 46 \end{array} \quad \begin{array}{r} -0.5 \\ 38 \end{array} \quad \begin{array}{r} -0.4 \\ 11 \end{array} \quad \begin{array}{r} -0.5 \\ 7 \end{array} \quad \begin{array}{r} -0.1 \\ 33 \end{array} \quad \begin{array}{r} 0.0 \\ 50 \end{array}$$

$$\begin{array}{r} +1.7 \\ 44 \end{array} \quad \begin{array}{r} +1.7 \\ 44 \end{array} \quad \begin{array}{r} +0.1 \\ 32 \end{array} \quad \begin{array}{r} +0.1 \\ 19 \end{array} \quad \begin{array}{r} -0.4 \\ 50 \end{array}$$

$$\begin{array}{r} +1.0 \\ 50 \end{array} \quad \begin{array}{r} +1.0 \\ 46 \end{array} \quad \begin{array}{r} -0.3 \\ 35 \end{array} \quad \begin{array}{r} -0.4 \\ 14 \end{array} \quad \begin{array}{r} -0.1 \\ 15 \end{array} \quad \begin{array}{r} -0.5 \\ 50 \end{array}$$

$$\begin{array}{r} +0.9 \\ 50 \end{array} \quad \begin{array}{r} +0.9 \\ 43 \end{array} \quad \begin{array}{r} -0.3 \\ 33 \end{array} \quad \begin{array}{r} -0.5 \\ 12 \end{array} \quad \begin{array}{r} +0.3 \\ 13 \end{array} \quad \begin{array}{r} +0.7 \\ 31 \end{array} \quad \begin{array}{r} +0.7 \\ 50 \end{array}$$

$$\begin{array}{r} +1.0 \\ 50 \end{array} \quad \begin{array}{r} +1.0 \\ 47 \end{array} \quad \begin{array}{r} -0.4 \\ 34 \end{array} \quad \begin{array}{r} 0.0 \\ 16 \end{array} \quad \begin{array}{r} -0.2 \\ 13 \end{array} \quad \begin{array}{r} +0.2 \\ 30 \end{array} \quad \begin{array}{r} 0.0 \\ 50 \end{array}$$

$$\begin{array}{r} +0.9 \\ 50 \end{array} \quad \begin{array}{r} -0.4 \\ 34 \end{array} \quad \begin{array}{r} +1.0 \\ 18 \end{array} \quad \begin{array}{r} -0.2 \\ 14 \end{array} \quad \begin{array}{r} 0.0 \\ 33 \end{array} \quad \begin{array}{r} 0.0 \\ 50 \end{array}$$

$$\begin{array}{r} +0.4 \\ 50 \end{array} \quad \begin{array}{r} +0.3 \\ 37 \end{array} \quad \begin{array}{r} -0.3 \\ 33 \end{array} \quad \begin{array}{r} -0.1 \\ 20 \end{array} \quad \begin{array}{r} -0.2 \\ 12 \end{array} \quad \begin{array}{r} -0.1 \\ 34 \end{array} \quad \begin{array}{r} -0.2 \\ 50 \end{array}$$

$$\begin{array}{r} +0.3 \\ 50 \end{array} \quad \begin{array}{r} +1.0 \\ 35 \end{array} \quad \begin{array}{r} -0.4 \\ 30 \end{array} \quad \begin{array}{r} -0.2 \\ 23 \end{array} \quad \begin{array}{r} -0.4 \\ 13 \end{array} \quad \begin{array}{r} -0.1 \\ 30 \end{array} \quad \begin{array}{r} -0.2 \\ 50 \end{array}$$

$$\begin{array}{r} +0.6 \\ 50 \end{array} \quad \begin{array}{r} +0.5 \\ 34 \end{array} \quad \begin{array}{r} -0.6 \\ 30 \end{array} \quad \begin{array}{r} -0.4 \\ 16 \end{array} \quad \begin{array}{r} 0.0 \\ 15 \end{array} \quad \begin{array}{r} +0.3 \\ 30 \end{array} \quad \begin{array}{r} +0.4 \\ 50 \end{array}$$

Sta.	+	Σ	-	Elev
		912.98		
7	+50		5.1	07.9
8			9.5	08.5
	+60		3.1	09.9
9			2.6	10.4
	+50		2.4	10.6
10			2.2	10.8
I.P.	5.78	917.58	1.18	911.80
	+50		6.1	11.5
11			6.0	11.6
	+50		7.1	10.5
12			8.6	09.0
	+50		8.9	09.2

Lt.

R

Rt.

$$\begin{array}{r} +0.7 \\ 50 \end{array} \quad \begin{array}{r} +0.8 \\ 42 \end{array} \quad \begin{array}{r} 0.8 \\ 33 \end{array} \quad \begin{array}{r} -0.5 \\ 15 \end{array} \quad \begin{array}{r} -0.1 \\ 13 \end{array} \quad \begin{array}{r} +0.7 \\ 40 \end{array} \quad \begin{array}{r} +0.8 \\ 50 \end{array}$$

$$\begin{array}{r} +0.7 \\ 50 \end{array} \quad \begin{array}{r} +0.7 \\ 45 \end{array} \quad \begin{array}{r} +0.1 \\ 36 \end{array} \quad \begin{array}{r} 0.0 \\ 13 \end{array} \quad \begin{array}{r} -0.4 \\ 10 \end{array} \quad \begin{array}{r} +0.4 \\ 32 \end{array} \quad \begin{array}{r} +0.8 \\ 50 \end{array}$$

$$\begin{array}{r} -0.6 \\ 50 \end{array} \quad \begin{array}{r} +0.3 \\ 20 \end{array} \quad \begin{array}{r} -0.1 \\ 13 \end{array} \quad \begin{array}{r} +0.3 \\ 24 \end{array} \quad \begin{array}{r} +0.5 \\ 50 \end{array}$$

$$\begin{array}{r} -1.2 \\ 50 \end{array} \quad \begin{array}{r} 0.0 \\ 17 \end{array} \quad \begin{array}{r} -0.1 \\ 14 \end{array} \quad \begin{array}{r} +0.6 \\ 12 \end{array} \quad \begin{array}{r} +0.9 \\ 50 \end{array}$$

$$\begin{array}{r} -1.7 \\ 50 \end{array} \quad \begin{array}{r} +0.2 \\ 18 \end{array} \quad \begin{array}{r} -0.2 \\ 16 \end{array} \quad \begin{array}{r} +0.6 \\ 12 \end{array} \quad \begin{array}{r} +1.2 \\ 50 \end{array}$$

$$\begin{array}{r} -1.3 \\ 50 \end{array} \quad \begin{array}{r} -1.3 \\ 40 \end{array} \quad \begin{array}{r} -0.1 \\ 30 \end{array} \quad \begin{array}{r} 0.0 \\ 16 \end{array} \quad \begin{array}{r} +0.7 \\ 15 \end{array} \quad \begin{array}{r} +1.3 \\ 35 \end{array} \quad \begin{array}{r} +1.5 \\ 50 \end{array}$$

$$\begin{array}{r} -0.6 \\ 50 \end{array} \quad \begin{array}{r} +0.1 \\ 25 \end{array} \quad \begin{array}{r} +0.6 \\ 30 \end{array} \quad \begin{array}{r} 1.0 \\ 50 \end{array}$$

$$\begin{array}{r} -1.3 \\ 50 \end{array} \quad \begin{array}{r} -1.3 \\ 39 \end{array} \quad \begin{array}{r} -0.1 \\ 29 \end{array} \quad \begin{array}{r} +0.3 \\ 15 \end{array} \quad \begin{array}{r} 0.0 \\ 15 \end{array} \quad \begin{array}{r} +1.0 \\ 50 \end{array}$$

$$\begin{array}{r} 0.0 \\ 50 \end{array} \quad \begin{array}{r} +0.7 \\ 32 \end{array} \quad \begin{array}{r} +1.2 \\ 15 \end{array} \quad \begin{array}{r} +0.2 \\ 10 \end{array} \quad \begin{array}{r} -0.1 \\ 16 \end{array} \quad \begin{array}{r} +1.5 \\ 50 \end{array}$$

$$\begin{array}{r} +0.8 \\ 50 \end{array} \quad \begin{array}{r} +0.8 \\ 41 \end{array} \quad \begin{array}{r} +1.6 \\ 15 \end{array} \quad \begin{array}{r} 0.0 \\ 9 \end{array} \quad \begin{array}{r} +0.5 \\ 13 \end{array} \quad \begin{array}{r} +2.5 \\ 50 \end{array}$$

$$\begin{array}{r} +0.6 \\ 50 \end{array} \quad \begin{array}{r} +1.4 \\ 18 \end{array} \quad \begin{array}{r} -0.4 \\ 12 \end{array} \quad \begin{array}{r} +0.6 \\ 15 \end{array} \quad \begin{array}{r} +1.6 \\ 37 \end{array} \quad \begin{array}{r} +2.4 \\ 50 \end{array}$$

Sta	+	π	-	Elev
		917.58		
12	+69		7.6	10.0
	+79		6.9	10.7
	+83		6.0	11.6
	+94		5.2	12.4
B.M.			5.63	911.75 (911.96)
13			5.8	12.3
	+07		2.7	11.9
	+11		6.9	10.7
	+50		7.1	10.5
14			7.4	10.2
	+50		7.2	10.4
15			6.2	11.4

Lt

K

Rt

$$\frac{90}{50}$$

$$\frac{+1.0}{18}$$

$$\frac{0.0}{12}$$

$$\frac{+0.6}{22}$$

$$\frac{+2.0}{50}$$

$$\frac{-0.9}{50}$$

$$\frac{0.0}{31}$$

$$\frac{+0.8}{12}$$

$$\frac{+0.5}{25}$$

$$\frac{+1.7}{50}$$

$$\frac{-1.3}{50}$$

$$\frac{+1.7}{50}$$

$$\frac{-1.6}{50}$$

$$\frac{+1.7}{50}$$

Top Mont Co Rd 1' & Long Lake Cal.

$$\frac{-1.5}{50}$$

$$\frac{+1.5}{50}$$

$$\frac{-1.2}{50}$$

$$\frac{-0.5}{30}$$

$$\frac{+1.3}{50}$$

$$\frac{0.0}{50}$$

$$\frac{+0.8 + 0.6 + 0.2}{30 \quad 13 \quad 7}$$

$$\frac{+0.6}{26}$$

$$\frac{+1.8}{50}$$

$$\frac{+0.2}{50}$$

$$\frac{+1.0}{22}$$

$$\frac{+0.1}{11}$$

$$\frac{+1.6}{22}$$

$$\frac{+1.8}{30}$$

$$\frac{+1.8}{50}$$

$$\frac{+0.5}{50}$$

$$\frac{+1.0}{21}$$

$$\frac{-0.2}{7}$$

$$\frac{+2.4}{22}$$

$$\frac{+2.5}{50}$$

$$\frac{0.0}{50}$$

$$\frac{+0.7}{19}$$

$$\frac{+0.5}{15}$$

$$\frac{+0.7}{3}$$

$$\frac{+3.0}{27}$$

$$\frac{3.4}{50}$$

$$\frac{-0.5}{50}$$

$$\frac{0.0}{25}$$

$$\frac{+1.4}{19}$$

$$\frac{+2.9}{42}$$

$$\frac{+3.5}{50}$$

Sta	+	X	-	Elev
		917.58		
15	+50		5.4	12.2
16			5.2	12.4
T.P.	508	918.02	4.64	912.94
	+50		5.3	12.7
17			4.4	13.6
	+30		2.7	14.3
	+60		4.4	13.6
18			5.0	13.0
	+50		5.2	12.8
19			5.0	13.0
	+50		5.4	12.6
20			5.7	12.1

LH

Z

RH

$$\frac{-0.4}{50}$$

$$\frac{-0.4}{20}$$

$$\frac{+1.6}{23}$$

$$\frac{+3.2}{50}$$

$$\frac{-0.9}{50}$$

$$\frac{-0.9}{35}$$

$$\frac{0.0}{22}$$

$$\frac{+0.3}{14}$$

$$\frac{+1.7}{23}$$

$$+\frac{2.7}{50}$$

$$\frac{-0.6}{50}$$

$$\frac{-0.6}{40}$$

$$\frac{-0.3}{20}$$

$$\frac{+1.0}{21}$$

$$+\frac{2.0}{50}$$

$$\frac{+1.6}{50}$$

$$\frac{-1.3}{25}$$

$$\frac{+1.0}{20}$$

$$+\frac{1.5}{50}$$

$$\frac{-1.9}{50}$$

$$\frac{-1.3}{25}$$

$$\frac{-0.8}{10}$$

$$\frac{+1.0}{20}$$

$$+\frac{1.3}{50}$$

$$\frac{-1.2}{50}$$

$$\frac{-1.1}{25}$$

$$\frac{-0.7}{10}$$

$$\frac{+0.6}{20}$$

$$+\frac{1.1}{50}$$

$$\frac{-0.7}{50}$$

$$\frac{-0.7}{25}$$

$$\frac{-0.5}{10}$$

$$\frac{+0.7}{20}$$

$$+\frac{1.4}{50}$$

$$\frac{0.0}{50}$$

$$\frac{-0.4}{25}$$

$$\frac{-0.3}{10}$$

$$\frac{0.0}{20}$$

$$+\frac{0.7}{50}$$

$$\frac{-0.6}{50}$$

$$\frac{-0.7}{25}$$

$$\frac{-0.4}{10}$$

$$\frac{+0.5}{20}$$

$$+\frac{1.0}{50}$$

$$\frac{-0.6}{50}$$

$$\frac{-0.5}{25}$$

$$\frac{-0.6}{10}$$

$$+\frac{0.7}{25}$$

$$+\frac{1.7}{50}$$

$$-\frac{1.2}{50}$$

$$\frac{-1.3}{25}$$

$$\frac{-1.0}{10}$$

$$\frac{-0.5}{4}$$

$$+\frac{0.8}{13}$$

$$\frac{-0.5}{25}$$

$$\frac{-0.5}{50}$$

Sta.	+	π	-	Elev.
		918.02		
20	150		6.8	11.2
21			6.8	11.2
R.P.	0.97	912.68	6.91	911.71
	150		2.6	10.1
22			4.3	08.4
	127		5.6	07.1
	150		5.9	06.8
23			6.4	06.3
	150		6.6	06.1
24			6.4	06.3
	150		5.7	07.0
25			5.5	07.2

Lt

L

Rt

$$\frac{-0.8}{50}$$

$$\frac{-0.7}{25}$$

$$\frac{-0.6}{10}$$

$$\frac{+1.1}{18}$$

$$\frac{0.0}{27}$$

$$\frac{-0.3}{50}$$

$$\frac{-0.3}{50}$$

$$\frac{-0.3}{43}$$

$$\frac{-0.7}{28}$$

$$\frac{-0.7}{13}$$

$$\frac{+1.0}{14}$$

$$\frac{-0.3}{27}$$

$$\frac{-0.2}{50}$$

$$\frac{-1.2}{50}$$

$$\frac{-1.2}{40}$$

$$\frac{-0.9}{13}$$

$$\frac{+0.9}{12}$$

$$\frac{-0.5}{28}$$

$$\frac{-0.5}{50}$$

$$\frac{-0.5}{50}$$

$$\frac{-0.9}{29}$$

$$\frac{-0.4}{8}$$

$$\frac{+1.0}{13}$$

$$\frac{+0.2}{33}$$

$$\frac{+0.5}{50}$$

$$\frac{+0.3}{50}$$

$$\frac{-0.3}{30}$$

$$\frac{-1.0}{8}$$

$$\frac{+1.0}{15}$$

$$\frac{+1.1}{50}$$

$$\frac{+0.4}{50}$$

$$\frac{+0.3}{39}$$

$$\frac{-0.3}{35}$$

$$\frac{+0.9}{30}$$

$$\frac{+1.4}{50}$$

$$\frac{+0.1}{50}$$

$$\frac{-0.1}{38}$$

$$\frac{+0.3}{20}$$

$$\frac{+0.7}{25}$$

$$\frac{+1.0}{50}$$

$$\frac{+0.5}{50}$$

$$\frac{0.0}{33}$$

$$\frac{+0.1}{25}$$

$$\frac{+0.7}{20}$$

$$\frac{+0.5}{35}$$

$$\frac{+0.7}{50}$$

$$\frac{+0.4}{50}$$

$$\frac{+0.3}{40}$$

$$\frac{0.0}{34}$$

$$\frac{+0.9}{25}$$

$$\frac{+1.0}{50}$$

$$\frac{0.0}{50}$$

$$\frac{-0.5}{42}$$

$$\frac{-0.2}{25}$$

$$\frac{+0.1}{8}$$

$$\frac{+1.0}{18}$$

$$\frac{1.0}{50}$$

$$\frac{+0.3}{50}$$

$$\frac{+0.3}{35}$$

$$\frac{+0.2}{9}$$

$$\frac{+0.2}{11}$$

$$\frac{+1.1}{19}$$

$$\frac{+0.6}{28}$$

$$\frac{+0.9}{50}$$

Sta.	+	X	-	Elev.
		912.68		
25	+50		50	07.7
26			4.3	08.4
27	6.06	915.19	3.55	909.13
	+50		6.9	08.3
27			6.7	08.5
	+50		6.2	09.0
28			5.4	09.8
	+50		4.8	10.4
29			4.7	10.5
B.M.			2.28	912.91
	+50		4.3	10.9
30			3.5	11.7
	+50		40	11.2

(912.91)

Lt.

R.

Rt.

$$\frac{0.0}{50}$$

$$\frac{-0.4}{35}$$

$$\frac{-0.3}{15}$$

$$\frac{+1.2}{15}$$

$$\frac{+0.9}{29}$$

$$\frac{0.7}{50}$$

$$\frac{-0.3}{50}$$

$$\frac{-0.5}{35}$$

$$\frac{-0.5}{9}$$

$$\frac{+0.8}{19}$$

$$\frac{+0.5}{30}$$

$$\frac{+0.3}{50}$$

$$\frac{0.0}{50}$$

$$\frac{-0.4}{33}$$

$$\frac{-0.8}{30}$$

$$\frac{-0.3}{15}$$

$$\frac{+1.3}{19}$$

$$\frac{+1.0}{28}$$

$$\frac{+0.7}{50}$$

$$\frac{0.0}{50}$$

$$\frac{-0.1}{36}$$

$$\frac{0.0}{18}$$

$$\frac{+1.3}{18}$$

$$\frac{+0.5}{35}$$

$$\frac{+0.5}{50}$$

$$\frac{+1.0}{50}$$

$$\frac{+0.9}{41}$$

$$\frac{+0.4}{17}$$

$$\frac{0.0}{18}$$

$$\frac{+1.1}{19}$$

$$\frac{+0.6}{35}$$

$$\frac{+0.6}{50}$$

$$\frac{0.0}{50}$$

$$\frac{+0.1}{15}$$

$$\frac{+0.1}{13}$$

$$\frac{+0.7}{16}$$

$$\frac{+0.5}{30}$$

$$\frac{+0.5}{50}$$

$$\frac{+0.5}{50}$$

$$\frac{+0.2}{19}$$

$$\frac{-0.2}{13}$$

$$\frac{+0.2}{17}$$

$$\frac{-0.1}{50}$$

$$\frac{0.0}{50}$$

$$\frac{+0.3}{15}$$

$$\frac{+0.4}{19}$$

$$\frac{-0.3}{30}$$

$$\frac{-0.5}{50}$$

Ball & Spk, Top 3 bump 2.29+22.53

$$\frac{+1.0}{50}$$

$$\frac{0.0}{15}$$

$$\frac{-0.8}{50}$$

$$\frac{+0.1}{50}$$

$$\frac{+0.3}{20}$$

$$\frac{-0.9}{18}$$

$$\frac{-1.9}{50}$$

$$\frac{+0.8}{50}$$

$$\frac{+0.3}{20}$$

$$\frac{-0.7}{15}$$

$$\frac{-1.3}{35}$$

$$\frac{-1.6}{50}$$

Sta.	+	π	-	E/cv.
		915.19		
30	+80		9.2	11.0
31			4.5	10.7
T.P.	076	912.15	3.80	911.39
	+60		3.0	09.2
	+78		3.8	08.4
32			5.5	06.7
	+30		7.2	05.0
	+65		8.4	03.8
33			8.8	0.34
	+50		9.7	02.5
34			10.5	01.7
	+50		10.9	01.3

lt

R

ct

$$\begin{array}{r} +0.5 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +0.3 \\ \hline 16 \end{array}$$

$$\begin{array}{r} -1.4 \\ \hline 25 \end{array}$$

$$\begin{array}{r} -2.1 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +0.5 \\ \hline 50 \end{array}$$

$$\begin{array}{r} -1.0 \\ \hline 16 \end{array}$$

$$\begin{array}{r} -2.6 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +0.5 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +0.5 \\ \hline 28 \end{array}$$

$$\begin{array}{r} +1.0 \\ \hline 14 \end{array}$$

$$\begin{array}{r} -1.0 \\ \hline 10 \end{array}$$

$$\begin{array}{r} -1.7 \\ \hline 32 \end{array}$$

$$\begin{array}{r} -1.4 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +1.4 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +0.7 \\ \hline 29 \end{array}$$

$$\begin{array}{r} +0.7 \\ \hline 12 \end{array}$$

$$\begin{array}{r} -1.5 \\ \hline 15 \end{array}$$

$$\begin{array}{r} -0.6 \\ \hline 44 \end{array}$$

$$\begin{array}{r} -1.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +2.3 \\ \hline 38 \end{array}$$

$$\begin{array}{r} +2.3 \\ \hline 38 \end{array}$$

$$\begin{array}{r} +0.9 \\ \hline 30 \end{array}$$

$$\begin{array}{r} +0.7 \\ \hline 16 \end{array}$$

$$\begin{array}{r} -0.3 \\ \hline 32 \end{array}$$

$$\begin{array}{r} -1.0 \\ \hline 41 \end{array}$$

$$\begin{array}{r} -1.1 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +3.0 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +2.6 \\ \hline 36 \end{array}$$

$$\begin{array}{r} +1.0 \\ \hline 30 \end{array}$$

$$\begin{array}{r} +0.4 \\ \hline 16 \end{array}$$

$$\begin{array}{r} -0.4 \\ \hline 11 \end{array}$$

$$\begin{array}{r} -0.4 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +2.7 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +2.7 \\ \hline 45 \end{array}$$

$$\begin{array}{r} +0.3 \\ \hline 32 \end{array}$$

$$\begin{array}{r} 0.0 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +1.6 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +1.6 \\ \hline 38 \end{array}$$

$$\begin{array}{r} 0.0 \\ \hline 28 \end{array}$$

$$\begin{array}{r} 0.0 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +1.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +1.3 \\ \hline 42 \end{array}$$

$$\begin{array}{r} +0.6 \\ \hline 37 \end{array}$$

$$\begin{array}{r} +0.1 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 0.0 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +1.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +1.0 \\ \hline 36 \end{array}$$

$$\begin{array}{r} +1.3 \\ \hline 16 \end{array}$$

$$\begin{array}{r} +0.1 \\ \hline 11 \end{array}$$

$$\begin{array}{r} 0.0 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +1.0 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +1.0 \\ \hline 42 \end{array}$$

$$\begin{array}{r} +1.0 \\ \hline 17 \end{array}$$

$$\begin{array}{r} +0.1 \\ \hline 10 \end{array}$$

$$\begin{array}{r} -0.3 \\ \hline 50 \end{array}$$

Sta.	+	π	-	Elev.	
		912.15			
36			11.4	00.8	sand Hard Bottom
Elev. Water			1095		
+50			11.8	00.4	
36			12.0	900.2	
+50			12.3	899.9	
37			12.5	899.7	sand Hard Bottom
T.P.	6.04	908.39	980	902.35	
+50			84	900.0	
38			82	00.2	
+50			82	00.2	
39			80	00.4	
+50			79	901.0	

L.F.

L

R.F.

$$\begin{array}{r} +1.3 \\ \hline 50 \end{array} \quad \begin{array}{r} +0.2 \\ \hline 40 \end{array} \quad \begin{array}{r} +1.0 \\ \hline 25 \end{array} \quad \begin{array}{r} +1.1 \\ \hline 15 \end{array}$$

$$\begin{array}{r} -0.3 \\ \hline 50 \end{array}$$

901.20 Water Level

$$\begin{array}{r} +1.9 \\ \hline 50 \end{array} \quad \begin{array}{r} +1.9 \\ \hline 45 \end{array} \quad \begin{array}{r} +0.9 \\ \hline 38 \end{array} \quad \begin{array}{r} +1.0 \\ \hline 20 \end{array}$$

$$\begin{array}{r} -0.4 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +2.3 \\ \hline 50 \end{array} \quad \begin{array}{r} +2.1 \\ \hline 44 \end{array} \quad \begin{array}{r} +1.0 \\ \hline 38 \end{array}$$

$$\begin{array}{r} -0.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +1.8 \\ \hline 50 \end{array} \quad \begin{array}{r} +1.6 \\ \hline 42 \end{array} \quad \begin{array}{r} +0.6 \\ \hline 36 \end{array}$$

$$\begin{array}{r} -0.2 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 11.2 \\ \hline 60 \end{array} \quad \begin{array}{r} 10.3 \\ \hline 53 \end{array} \quad \begin{array}{r} 10.5 \\ \hline 46 \end{array} \quad \begin{array}{r} 12.4 \\ \hline 37 \end{array}$$

$$\begin{array}{r} -0.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +2.3 \\ \hline 50 \end{array} \quad \begin{array}{r} +2.1 \\ \hline 41 \end{array} \quad \begin{array}{r} +1.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -0.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +2.1 \\ \hline 50 \end{array} \quad \begin{array}{r} +1.6 \\ \hline 40 \end{array} \quad \begin{array}{r} +0.7 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -0.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +2.4 \\ \hline 50 \end{array} \quad \begin{array}{r} +2.3 \\ \hline 41 \end{array} \quad \begin{array}{r} +0.5 \\ \hline 28 \end{array}$$

$$\begin{array}{r} -0.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 6.2 \\ \hline 60 \end{array} \quad \begin{array}{r} 5.9 \\ \hline 51 \end{array} \quad \begin{array}{r} 6.3 \\ \hline 43 \end{array} \quad \begin{array}{r} 7.3 \\ \hline 27 \end{array} \quad \begin{array}{r} 6.6 \\ \hline 24 \end{array} \quad \begin{array}{r} 6.6 \\ \hline 17 \end{array} \quad \begin{array}{r} 7.7 \\ \hline 11 \end{array}$$

$$\begin{array}{r} -0.2 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +1.3 \\ \hline 50 \end{array} \quad \begin{array}{r} +1.3 \\ \hline 44 \end{array} \quad \begin{array}{r} +0.5 \\ \hline 39 \end{array} \quad \begin{array}{r} +0.8 \\ \hline 25 \end{array} \quad \begin{array}{r} +0.8 \\ \hline 15 \end{array} \quad \begin{array}{r} 0.0 \\ \hline 10 \end{array}$$

$$\begin{array}{r} -0.1 \\ \hline 50 \end{array}$$

Sta.	+	π	-	Elev.
		908.39		
40			6.3	02.1
+52			5.0	03.4
41			3.8	04.6
+47			2.1	06.3
42			2.1	06.3
T.P.	6.00	912.92	1.47	906.92
+50				05.9
43				06.3
+50				07.1
				07.0
44				07.7
+50				08.4
45				09.3

L.F.

C

R.F.

$$L.O. \quad \frac{+0.3}{42} - \frac{0.3}{40} \quad \frac{0.0}{33} \quad - \frac{1.0}{28} + \frac{0.7}{22} \quad - \frac{0.4}{13} \quad \frac{+0.4}{50}$$

$$- \frac{0.4}{50} \quad - \frac{0.1}{30} \quad \frac{+0.3}{22} \quad \frac{0.0}{50}$$

$$\frac{-0.8}{50} \quad \frac{-0.2}{25} \quad \frac{0.0}{25} \quad \frac{0.0}{50}$$

$$\frac{-0.9}{50} \quad \frac{-0.6}{27} \quad \frac{-1.0}{30} \quad \frac{-1.5}{50}$$

$$- \frac{0.7}{50} \quad - \frac{0.3}{25} \quad - \frac{0.6}{23} \quad - \frac{1.5}{50}$$

$$\frac{6.0}{50} \quad \frac{6.9}{33} \quad \frac{7.0}{11} \quad \frac{7.0}{8} \quad \frac{6.8}{27} \quad \frac{8.0}{50}$$

$$\frac{5.9}{50} \quad \frac{6.8}{33} \quad \frac{6.7}{15} \quad \frac{6.5}{7} \quad \frac{6.8}{29} \quad \frac{7.9}{50}$$

$$\frac{5.9}{50} \quad \frac{6.8}{33} \quad \frac{6.8}{15} \quad \frac{5.9}{8} \quad \frac{6.8}{28} \quad \frac{7.1}{50}$$

$$\frac{5.2}{50} \quad \frac{5.6}{36} \quad \frac{5.5}{15} \quad \frac{5.2}{7} \quad \frac{5.9}{29} \quad \frac{6.5}{50}$$

$$\frac{4.9}{50} \quad \frac{5.2}{30} \quad \frac{5.0}{12} \quad \frac{4.5}{8} \quad \frac{4.6}{28} \quad \frac{5.3}{50}$$

$$\frac{4.6}{50} \quad \frac{4.9}{35} \quad \frac{4.8}{17} \quad \frac{3.6}{7} \quad \frac{3.9}{27} \quad \frac{4.3}{30}$$

Sta.	+	Σ	-	Elev.
		912.72		
45	+50			10.4
46				10.2
	+50			10.6
47				11.0
T.P.	2.27	913.73	1.26	911.66
	+50			11.2
48				11.2
	+50			10.6
49				09.9
B.M.	2.94	913.88	2.94	910.99 (910.94)
	+50			09.9
50				10.2
	+50			10.1

Lt

L

Lt

$$\frac{41}{50} \quad \frac{38}{28} \quad \frac{31}{7} \quad \frac{25}{7} \quad \frac{28}{7} \quad \frac{34}{27} \quad \frac{41}{50}$$

$$\frac{37}{50} \quad \frac{35}{31} \quad \frac{30}{9}$$

$$\frac{27}{7} \quad \frac{30}{27} \quad \frac{34}{50}$$

$$\frac{32}{50} \quad \frac{33}{37} \quad \frac{27}{11} \quad \frac{23}{6} \quad \frac{27}{27} \quad \frac{32}{50} \quad \frac{35}{50}$$

$$\frac{32}{50} \quad \frac{32}{40} \quad \frac{25}{22}$$

$$\frac{19}{6} \quad \frac{23}{26} \quad \frac{25}{50} \quad \frac{27}{50}$$

$$\frac{49}{50} \quad \frac{35}{13} \quad \frac{31}{9} \quad \frac{27}{13} \quad \frac{30}{25} \quad \frac{34}{50} \quad \frac{33}{50}$$

$$\frac{46}{50} \quad \frac{43}{33} \quad \frac{39}{9}$$

$$\frac{27}{6} \quad \frac{30}{25} \quad \frac{34}{50}$$

$$\frac{52}{50} \quad \frac{49}{35} \quad \frac{38}{10} \quad \frac{33}{6} \quad \frac{26}{24} \quad \frac{41}{50} \quad \frac{43}{50}$$

$$\frac{48}{50} \quad \frac{50}{29} \quad \frac{42}{11}$$

$$\frac{40}{7} \quad \frac{43}{29} \quad \frac{49}{50} \quad \frac{55}{50}$$

Sph. in 24" out 1' at 49+10

$$\frac{46}{50} \quad \frac{45}{31} \quad \frac{42}{10} \quad \frac{40}{5} \quad \frac{49}{23} \quad \frac{52}{43} \quad \frac{57}{50}$$

$$\frac{46}{50} \quad \frac{47}{29} \quad \frac{44}{19}$$

$$\frac{37}{19} \quad \frac{45}{30} \quad \frac{54}{50} \quad \frac{55}{50}$$

$$\frac{47}{50} \quad \frac{53}{30} \quad \frac{44}{10} \quad \frac{38}{6} \quad \frac{42}{23} \quad \frac{48}{50} \quad \frac{50}{50}$$

Sta.	+	π	-	Elev.
		913.88		
51				09.7
+50				09.2
52				09.5
T.P.	6.46	916.35	3.99	909.89
+50				910.0
53				10.7
+50				11.5
54				11.5
+50				10.8
55				11.0
+50				11.9
T.P.	1.94	915.08	3.21	913.14
56				12.8

Lt.

2

Rt.

$$\frac{50}{50} \quad \frac{55}{30} \quad \frac{47}{9} \quad \frac{42}{9} \quad \frac{46}{9} \quad \frac{53}{30} \quad \frac{52}{50}$$

$$\frac{56}{50} \quad \frac{58}{28} \quad \frac{50}{9} \quad \frac{47}{9} \quad \frac{48}{9} \quad \frac{54}{24} \quad \frac{54}{50}$$

$$\frac{51}{50} \quad \frac{53}{37} \quad \frac{50}{15} \quad \frac{44}{9} \quad \frac{49}{9} \quad \frac{52}{26} \quad \frac{52}{50}$$

$$\frac{66}{50} \quad \frac{66}{21} \quad \frac{64}{28} \quad \frac{71}{28} \quad \frac{74}{50}$$

$$\frac{49}{50} \quad \frac{54}{30} \quad \frac{57}{25} \quad \frac{65}{25} \quad \frac{66}{50}$$

$$\frac{52}{50} \quad \frac{51}{23} \quad \frac{49}{10} \quad \frac{54}{10} \quad \frac{57}{50}$$

$$\frac{54}{50} \quad \frac{56}{30} \quad \frac{49}{20} \quad \frac{54}{20} \quad \frac{56}{50}$$

$$\frac{56}{50} \quad \frac{60}{27} \quad \frac{58}{8} \quad \frac{56}{8} \quad L.O.$$

$$\frac{56}{50} \quad \frac{60}{30} \quad \frac{56}{8} \quad \frac{54}{15} \quad \frac{58}{15} \quad \frac{58}{30}$$

$$\frac{56}{50} \quad \frac{50}{28} \quad \frac{47}{10} \quad \frac{45}{15} \quad \frac{53}{15} \quad \frac{53}{50}$$

$$\frac{45}{50} \quad \frac{36}{30} \quad \frac{30}{8} \quad \frac{23}{10} \quad \frac{37}{10} \quad \frac{47}{32} \quad \frac{49}{50}$$

Sta.	+	7	-	Elev.
		91308		
56	+50			13.0
57				12.8
	+50			12.0
58				09.4
	+32			08.0
	+62			05.6
59				901.8
T.P.	0.39	904.12	11.29	903.79
	+34			898.6
	+67			97.1
	+70	End 4" Pipe	899.82 4.30	
60				91.6
	+22			90.2

$$\frac{45}{50} \frac{26}{29} \frac{30}{8} \frac{21}{11} \frac{14}{12} \frac{41}{50} \frac{45}{50}$$

$$\frac{51}{50} \frac{38}{29} \frac{21}{10} \frac{23}{12} \frac{40}{28} \frac{46}{50} \frac{49}{50}$$

$$\frac{57}{50} \frac{49}{29} \frac{40}{10} \frac{31}{11} \frac{45}{26} \frac{50}{50} \frac{53}{50}$$

$$\frac{46}{50} \frac{67}{31} \frac{59}{10} \frac{57}{10} \frac{67}{25} \frac{78}{50} \frac{80}{50}$$

$$\frac{73}{50} \frac{81}{29} \frac{77}{10} \frac{71}{17} \frac{87}{50} \frac{95}{50}$$

$$\frac{81}{50} \frac{92}{33} \frac{96}{13} \frac{95}{16} \frac{117}{34} \frac{129}{50} \frac{142}{50}$$

$$\frac{110}{75} \frac{83}{33} \frac{82}{48} \frac{109}{29} \frac{124}{20} \frac{123}{6} \frac{133}{13} \frac{151}{36} \frac{168}{50} \frac{168}{50}$$

$$\text{Cont.} \frac{46}{30} \frac{52}{19} \frac{48}{7} \frac{55}{15} \frac{79}{33} \frac{88}{50} \frac{95}{50}$$

$$\frac{24}{28} \frac{81}{17} \frac{78}{7} \frac{90}{15} \frac{98}{27} \frac{120}{50} \frac{139}{50}$$

$$\frac{100}{27} \frac{113}{18} \frac{108}{7} \frac{125}{15} \frac{148}{15} \frac{153}{30} \frac{155}{50}$$

494.75
(987)
FL. 6. 6. 14

$$\frac{106}{27} \frac{120}{18} \frac{117}{10} \frac{139}{9} \frac{150}{30} \frac{152}{50} \frac{158}{50}$$

Sta. + A - Elev.

709.12

60 +40

89.4

+50 Stand 15' W.

891.22
12.9

+69

89.7

61

93.3

+60

898.3

62

901.0

T.P.

7.21

910.70

2.63

901.49

59 +34

898.6

+70

97.1

60

91.6

+22

90.2

+40

89.4

+69

89.7

Lt.

E

Rt.

$$\frac{109}{27} \quad \frac{129}{16} \quad \frac{141}{6} \quad \frac{147}{1}$$

$$\frac{158}{31} \quad \frac{159}{50}$$

$$\frac{113}{26} \quad \frac{131}{15}$$

$$\frac{144}{24} \quad \frac{151}{24} \quad \frac{156}{50}$$

$$\frac{100}{27} \quad \frac{106}{19} \quad \frac{104}{6} \quad \frac{108}{1}$$

$$\frac{116}{24} \quad \frac{122}{50}$$

$$\frac{47}{33} \quad \frac{58}{21} \quad \frac{55}{7} \quad \frac{58}{11} \quad \frac{73}{32} \quad \frac{87}{50} \quad \frac{94}{50}$$

$$\frac{10}{37} \quad \frac{28}{19} \quad \frac{28}{9} \quad \frac{25}{5} \quad \frac{31}{1} \quad \frac{43}{10} \quad \frac{58}{27} \quad \frac{65}{50}$$

$$\frac{92}{85} \quad \frac{91}{68} \quad \frac{96}{56} \quad \frac{94}{50} \quad \frac{96}{43} \quad (121)$$

$$\frac{120}{80} \quad \frac{109}{70} \quad \frac{41}{36} \quad \frac{38}{50} \quad \frac{46}{43} \quad (13.6)$$

$$\frac{135}{88} \quad \frac{125}{72} \quad \frac{56}{39} \quad \frac{47}{50} \quad \frac{58}{42} \quad (19.1)$$

$$\frac{144}{85} \quad \frac{137}{75} \quad \frac{58}{39} \quad \frac{46}{50} \quad \frac{58}{44} \quad (20.5)$$

$$\frac{147}{88} \quad \frac{139}{71} \quad \frac{58}{38} \quad \frac{43}{50} \quad \frac{60}{43} \quad (21.3)$$

$$\frac{151}{85} \quad \frac{139}{71} \quad \frac{57}{38} \quad \frac{42}{50} \quad \frac{55}{43} \quad (21.0)$$

Sta	+	Σ	-	Elev
		910.70		
61				93.3
	+60			898.3
62				901.0
	+50			03.7
63				05.7
	+50			08.0
64				09.9
T.P.	2.77	913.97	0.48	910.22
	+50			11.0
	+6.2			09.6
65	+00			09.2
	+2.5			09.2

Lt

K

Kt

$$\frac{144}{85} \frac{185}{74} \frac{53}{59} \frac{37}{50} \frac{51}{44} \quad (17.4)$$

$$\frac{109}{85} \frac{100}{69} \frac{51}{79} \frac{39}{50} \frac{52}{43} \quad (12.4)$$

$$\frac{78}{85} \frac{76}{70} \frac{51}{59} \frac{43}{50} \frac{54}{42} \quad (9.7)$$

$$\frac{35}{50} \frac{52}{40} \frac{62}{18} \frac{61}{5} \frac{70}{5} \frac{79}{9} \frac{91}{29} \frac{98}{50}$$

$$\frac{27}{50} \frac{40}{41} \frac{44}{29} \frac{52}{7} \frac{44}{5} \frac{50}{5} \frac{61}{8} \frac{72}{26} \frac{93}{50}$$

$$\frac{24}{50} \frac{31}{23} \frac{34}{7} \frac{22}{9} \frac{27}{7} \frac{39}{7} \frac{54}{24} \frac{65}{50}$$

$$\frac{17}{50} \frac{23}{36} \frac{26}{19} \frac{20}{9} \frac{0.0}{5} \frac{0.8}{5} \frac{1.9}{6} \frac{3.3}{22} \frac{4.4}{50}$$

$$\frac{48}{50} \frac{51}{37} \frac{48}{18} \frac{44}{10} \frac{27}{4} \frac{30}{4} \frac{4.3}{8} \frac{5.9}{29} \frac{6.1}{50}$$

$$\frac{48}{50} \frac{52}{36} \frac{47}{15}$$

$$\frac{44}{50} \frac{42}{9} \frac{47}{26} \frac{5.8}{50}$$

$$\frac{48}{50} \frac{51}{35} \frac{48}{15} \frac{41}{8} \frac{48}{50} \quad \frac{6.0}{26} \quad \frac{6.7}{50}$$

$$\frac{38}{50} \frac{44}{18} \frac{48}{18} \frac{5.8}{22} \frac{6.9}{50}$$

Sta	+	π	-	Elev.
		913.99		
1.5	+36			06.6
	+45			05.5
	+50			07.5
	+36.75	Edge Pav. Curb.		07.45
	+70.25		6.62	07.37
2.17			6.62	907.37
				907.37

Lt

L

Rt

$\frac{47}{30}$	$\frac{48}{96}$	$\frac{7.9}{37}$	$\frac{87}{19}$	$\frac{7.9}{15}$	$\frac{9.2}{25}$	$\frac{6.6}{49}$	$\frac{6.7}{49}$	$\frac{10.3}{52}$
-----------------	-----------------	------------------	-----------------	------------------	------------------	------------------	------------------	-------------------

$\frac{47}{30}$	$\frac{4.9}{96}$	$\frac{81}{33}$	$\frac{9.0}{12}$	$\frac{8.5}{12}$	$\frac{7.9}{8}$	$\frac{6.9}{16}$	$\frac{7.0}{41}$	$\frac{9.4}{46}$	$\frac{10.0}{50}$
-----------------	------------------	-----------------	------------------	------------------	-----------------	------------------	------------------	------------------	-------------------

$$\frac{7.7}{30}$$

$$\frac{6.5}{30}$$

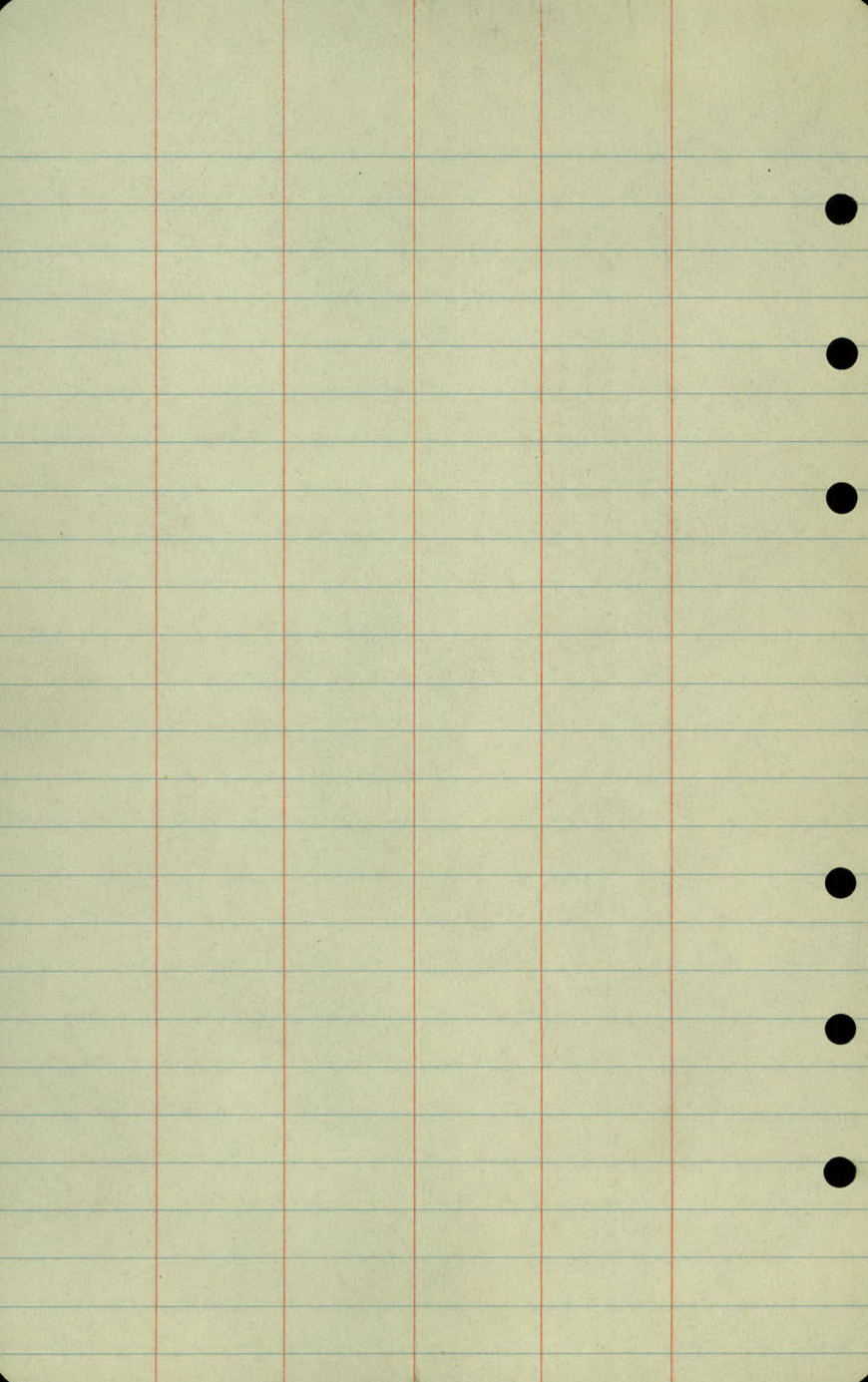
$$\frac{5.2}{30}$$

$$\frac{5.42}{30}$$

$$\frac{6.54}{30}$$

$$\frac{7.7}{30}$$

Bress Plug in Pav. U.S. #10 & Co. Rd. #14



Pick F.E. From Plan

0+50 E No Cully Regd.

5+00 E 18" X ? Conc

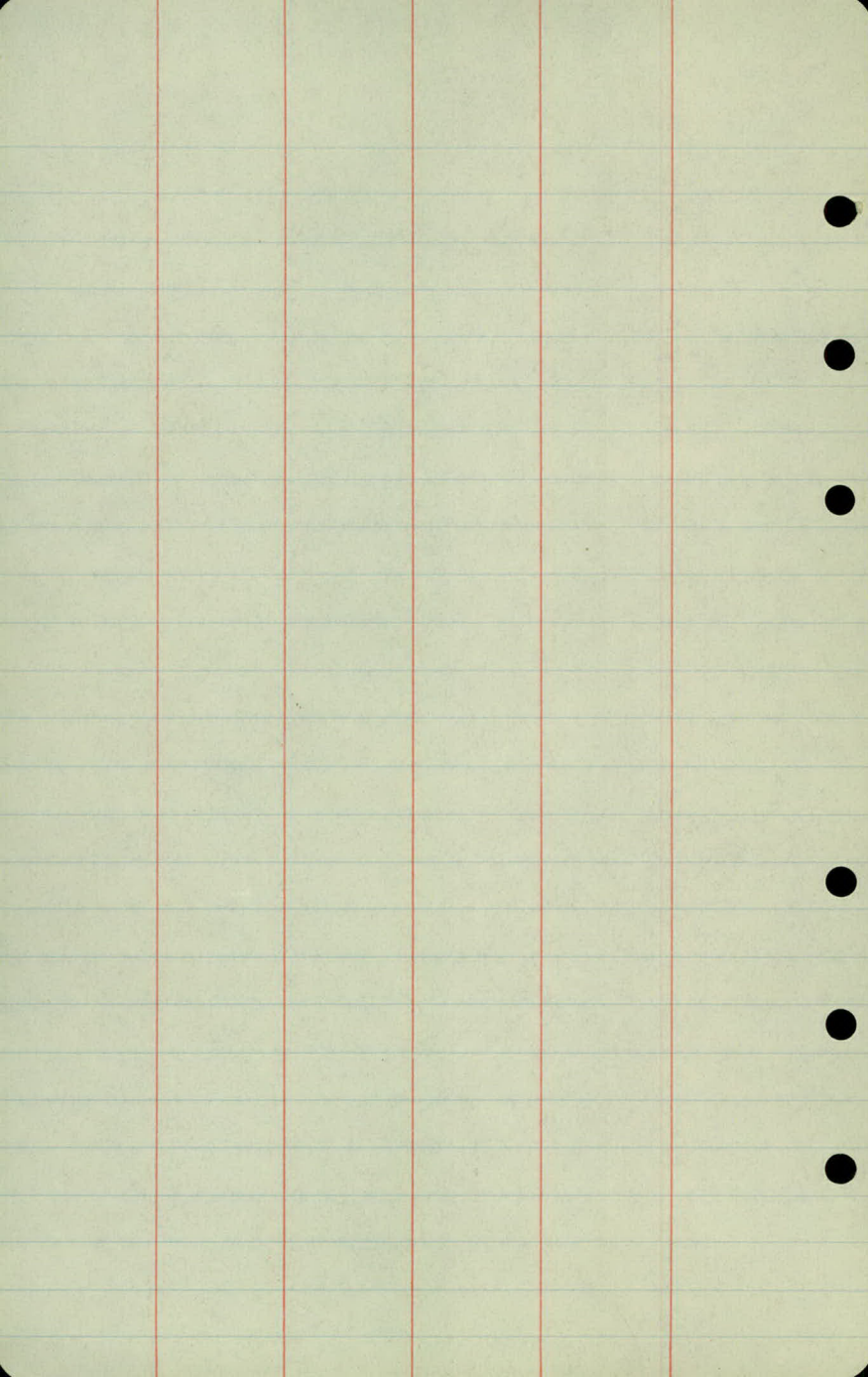
7+50 To 12+00 Sp. Ditch Rt. + Lt.

13+30 E 18" X ? Conc. Dr Lt. ?

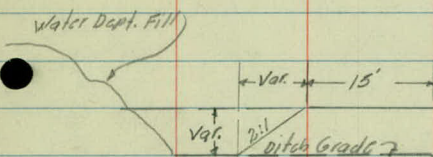
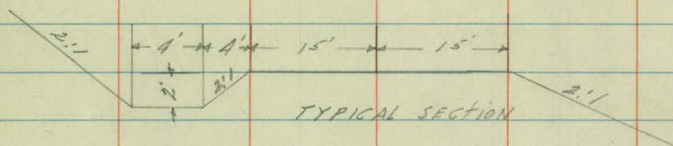
16+00 Lt No Cully Regd.

23+50 To East Sp. Ditch R + L.

37+00 E 36" X ? C.M.



slope stakes
 Co. Rd "1"
 STH. #10 to STH. #8



SPECIAL DITCH SECTION
 Sta. 59+00 to Sta. 62+00 Lt.

14 Pages

Sta	+	π	-	Grade
B.M.	4.02	914.21		910.19

0	100			910.19
---	-----	--	--	--------

	120.3			09.8
--	-------	--	--	------

	124			09.8
--	-----	--	--	------

	147			09.7
--	-----	--	--	------

	170			09.7
--	-----	--	--	------

1				09.6
---	--	--	--	------

	150			09.4
--	-----	--	--	------

2				09.3
---	--	--	--	------

	120			09.2
--	-----	--	--	------

	150			09.1
--	-----	--	--	------

3				09.0
---	--	--	--	------

21/3/37
K.A.
L.B.H.
L.C.
M.D.B.

Gr. Rod Lt R Rt

Top Hole cfr. Por. 0100

$$4.5 \quad \begin{array}{r} 25.6 / 5.2 \\ 25.6 / 2.15 \\ \hline \end{array} \quad \begin{array}{r} 53 \\ -08 \\ \hline \end{array}$$

$$4.6 \quad \begin{array}{r} 26.0 / 51 \\ 26.0 / 12.15 \\ \hline \end{array} \quad \begin{array}{r} 47 \\ -01 \\ \hline \end{array} \quad \begin{array}{r} 63 \\ 1803 / 22.6 \\ \hline \end{array}$$

$$4.8 \quad \begin{array}{r} 26.8 / 49 \\ 26.8 / 2.19 \\ \hline \end{array} \quad \begin{array}{r} 44 \\ +09 \\ \hline \end{array} \quad \begin{array}{r} 58 \\ 1810 / 25.0 \\ \hline \end{array}$$

$$4.9 \quad \begin{array}{r} 28.0 / 44 \\ 28.0 / 10.5 \\ \hline \end{array} \quad \begin{array}{r} 39 \\ +10 \\ \hline \end{array} \quad \begin{array}{r} 48 \\ 1811 / 27.2 \\ \hline \end{array}$$

5.0

$$5.1 \quad \begin{array}{r} 28.1 / 41 \\ 28.1 / 11.0 \\ \hline \end{array} \quad \begin{array}{r} 35 \\ +16 \\ \hline \end{array} \quad \begin{array}{r} 47 \\ 1809 / 27.8 \\ \hline \end{array}$$

$$5.2 \quad \begin{array}{r} 28.6 / 44 \\ 28.6 / 10.8 \\ \hline \end{array} \quad \begin{array}{r} 44 \\ +08 \\ \hline \end{array} \quad \begin{array}{r} 53 \\ 1819 / 26.8 \\ \hline \end{array}$$

Sta	+	π	-	Grade
		714.21		
2	+50			08.8
4				08.7
	+50			08.6
T.P.	5.86	713.38	6.69	907.52
5				08.5
	+50			08.6
6				08.8
	+20			08.7
	+50			9.0
	+60			09.0
7				09.2
	+50			09.4
8				09.6

Gr. Rod

Lt

d

Rt

5.4	$27.4 / \frac{5.2}{10.2}$	$\frac{5.1}{10.3}$	$\frac{5.7}{10.17} / 26.4$
5.5	$29.6 / \frac{6.7}{10.8}$	$\frac{6.9}{-1.4}$	$\frac{6.7}{10.8} / 29.6$
5.6	$24.0 / \frac{7.1}{10.5}$	$\frac{7.1}{-1.5}$	$\frac{7.1}{10.5} / 24.0$
4.9	$24.0 / \frac{6.4}{10.5}$	$\frac{6.5}{-1.6}$	$\frac{6.2}{10.7} / 24.4$
4.8	$24.8 / \frac{5.9}{10.9}$	$\frac{6.1}{-1.3}$	$\frac{6.2}{10.6} / 24.2$
4.6	$25.4 / \frac{5.4}{10.12}$	$\frac{5.4}{-0.8}$	$\frac{5.8}{10.8} / 24.6$
4.4	$25.6 / \frac{5.1}{10.13}$	$\frac{5.1}{-0.7}$	$\frac{5.3}{10.7} / 24.8$
4.9			
4.2	$26.2 / \frac{5.7}{10.05}$	$\frac{5.4}{-1.2}$	$\frac{5.4}{10.8} / 24.6$
4.0	$23.8 / \frac{5.6}{10.4}$	$\frac{5.4}{-1.4}$	$\frac{5.4}{10.6} / 24.2$
3.8	$25.4 / \frac{4.6}{10.12}$	$\frac{4.8}{-1.0}$	$\frac{4.8}{10.10} / 25.0$

Sta	+	X	-	Grade
		713.38		

8	+60			098
---	-----	--	--	-----

9				10.0
---	--	--	--	------

	+50			10.2
--	-----	--	--	------

10				10.4
----	--	--	--	------

T.P.	6.15	717.98	1.55	911.83
------	------	--------	------	--------

	+50			10.6
--	-----	--	--	------

11				10.8
----	--	--	--	------

	+50			11.0
--	-----	--	--	------

12				11.2
----	--	--	--	------

	+50			11.4
--	-----	--	--	------

	+70			11.4
--	-----	--	--	------

B.M.			6.02	716.96
------	--	--	------	--------

13	+10			11.7
----	-----	--	--	------

911.96

Gr. Rod

L_tL_cL_t

3.6

$$27.6 / \frac{3.3}{10.3}$$

$$\frac{3.4}{10.2}$$

$$\frac{3.5}{10.1} / 27.2$$

3.4

$$28.0 / \frac{2.9}{10.5}$$

$$\frac{2.9}{10.5}$$

$$\frac{2.5}{10.9} / 28.8$$

3.2

$$28.0 / \frac{2.7}{10.5}$$

$$\frac{2.6}{10.6}$$

$$\frac{2.0}{11.2} / 29.4$$

3.0

$$28.4 / \frac{2.3}{10.7}$$

$$\frac{2.5}{10.5}$$

$$\frac{1.8}{11.2} / 29.4$$

2.4

$$28.4 / \frac{1.7}{10.7}$$

$$\frac{1.4}{11.0}$$

$$\frac{1.3}{11.1} / 29.2$$

2.2

$$28.8 / \frac{1.3}{10.9}$$

$$\frac{1.4}{10.8}$$

$$\frac{1.4}{10.8} / 28.6$$

2.0

$$28.2 / \frac{1.4}{10.6}$$

$$\frac{1.4}{10.4}$$

$$\frac{1.5}{10.5} / 28.0$$

1.8

$$29.8 / \frac{1.9}{10.9}$$

$$\frac{1.9}{10.7}$$

$$\frac{1.3}{10.5} / 29.0$$

1.6

$$25.2 / \frac{1.5}{10.1}$$

$$\frac{1.7}{10.1}$$

$$\frac{1.0}{10.6} / 29.2$$

1.6

$$26.4 / \frac{1.9}{10.7}$$

$$\frac{1.9}{10.3}$$

$$\frac{1.3}{10.3} / 25.6$$

Top Man & Gr. Rod 7" Along Lake Rd.

6.3

$$\frac{1.5}{10.5}$$

$$\frac{1.5}{10.8} / 26.6$$

Sta	+	Σ	-	Grade
		917.98		
13	+50			11.7
14				11.8
B.M.	5.71	912.67		(911.96)
	+50			11.9
15				12.0
	+50			12.1
16				12.2
	+50			12.3
T.P.	3.78	917.93	3.52	914.15
17				12.3
	+30			12.3
	+60			12.3
18				12.2

Gr. Rod.

Lt

A

El

6.3

$$\frac{7.5}{-1.2}$$

$$\frac{5.9}{+0.9/27.8}$$

6.2

$$\frac{26.4}{+1.7} \frac{6.5}{-1.7}$$

$$\frac{7.7}{-1.5}$$

$$\frac{5.8}{+0.4/27.8}$$

Top Mont Co. Rd. 1" + Long Lake Rd.

5.8

$$\frac{24.8}{+0.9} \frac{6.9}{-1.5}$$

$$\frac{7.3}{-1.5}$$

$$\frac{4.5}{+1.3/29.6}$$

5.7

$$\frac{24.4}{+0.7} \frac{7.0}{-0.5}$$

$$\frac{6.2}{-0.5}$$

$$\frac{5.2}{+0.5/28.0}$$

5.6

$$\frac{25.4}{+1.2} \frac{6.4}{-0.3}$$

$$\frac{5.9}{-0.3}$$

$$\frac{4.0}{+1.6/30.2}$$

5.5

$$\frac{27.2}{+0.1} \frac{5.4}{+0.2}$$

$$\frac{5.3}{+0.2}$$

$$\frac{4.0}{+1.5/30.0}$$

5.4

$$\frac{27.2}{+0.1} \frac{5.3}{+0.9}$$

$$\frac{5.0}{+0.9}$$

$$\frac{4.0}{+1.4/29.8}$$

5.6

$$\frac{28.0}{+0.5} \frac{5.1}{+1.3}$$

$$\frac{4.3}{+1.3}$$

$$\frac{3.8}{+1.8/30.6}$$

5.6

$$\frac{28.4}{+0.7} \frac{4.7}{+1.9}$$

$$\frac{3.7}{+1.9}$$

$$\frac{3.2}{+2.4/31.8}$$

5.6

$$\frac{28.4}{+0.7} \frac{4.9}{+1.6}$$

$$\frac{4.0}{+1.6}$$

$$\frac{3.6}{+2.0/31.0}$$

5.7

$$\frac{28.0}{+0.5} \frac{4.9}{+0.8}$$

$$\frac{4.9}{+0.8}$$

$$\frac{4.4}{+1.3/29.6}$$

Sta	+	π	-	Grade
		917.93		
18	+50			12.0
19				11.8
	+50			11.6
20				11.4
	+50			11.1
21				10.7
	+50			10.7
T.P.	3.31	912.22	7.02	908.91
22				10.4
	+27			10.3
	+50			10.2
23				10.0

Gr. Rod

Lt.

L

Rt.

5.9

$$28.6 / \frac{51}{+0.8}$$

$$\frac{50}{+0.9}$$

$$\frac{48}{+1.1} / 29.2$$

6.1

$$28.8 / \frac{52}{+0.9}$$

$$\frac{49}{+1.2}$$

$$\frac{48}{+1.3} / 29.6$$

6.3

$$28.0 / \frac{58}{+0.5}$$

$$\frac{53}{+1.0}$$

$$\frac{44}{+1.9} / 30.8$$

6.5

$$26.6 / \frac{67}{+1.8}$$

$$\frac{58}{+0.7}$$

$$\frac{65}{+0.0} / 27.0$$

6.8

$$26.0 / \frac{73}{+1.5}$$

$$\frac{67}{+0.1}$$

$$\frac{71}{+1.7} / 26.9$$

7.0

$$26.4 / \frac{73}{+1.7}$$

$$\frac{67}{+0.3}$$

$$\frac{74}{+1.6} / 26.2$$

7.2

$$24.9 / \frac{85}{+0.7}$$

$$\frac{78}{-0.6}$$

$$\frac{81}{+1.1} / 25.2$$

1.8

21

$$19.8 / \frac{4.2}{-2.4}$$

$$\frac{39}{-1.1}$$

$$\frac{34}{+5.04} / 23.8$$

1.7

22

$$\frac{39}{-2}$$

19

2.0

22.2

$$21.4 / \frac{5.2}{-3.2}$$

$$\frac{54}{-3.4}$$

$$\frac{50}{-5.0} / 21.0$$

205

2.2

20.8

$$21.4 / \frac{5.4}{-3.2}$$

$$\frac{58}{-3.6}$$

$$\frac{56}{-3.4} / 21.8$$

208

					Ditch Grade	
Sta.	+	x	-	Grade	Lt.	Rt.
		712.22				
23	+50			09.7	<u>6.0</u> 06.2	<u>5.4</u> 06.8
24				09.5	6.1 06.1	5.3 06.7
	+50			09.3	6.1 06.1	5.5 06.7
25				09.0	6.2 06.2	5.6 06.6
I.P.	826	918.93	4.15	908.07	7.3 06.0	6.7 06.6
	+50			08.8	7.4 05.9	6.8 06.5
26				08.6	7.4 05.9	
	+50			08.3	7.5 05.8	
27				08.1	7.5 05.8	
	+50			07.8		
28				07.6		
I.P.	492	916.32	2.93	910.40		
	+50			07.4		

Gr. Bod

Lt

K

Rt.

$$2.5 \quad 21.5 \quad 26.6 / \begin{array}{r} 5.7 \\ 120.3 \end{array} \quad \begin{array}{r} 5.7 \\ -3.4 \end{array} \quad \begin{array}{r} 5.2 \\ 120.2 / 25.4 \end{array} \quad 21$$

$$2.7 \quad 21.8 \quad 26.6 / \begin{array}{r} 5.7 \\ 120.4 \end{array} \quad \begin{array}{r} 5.7 \\ -3.0 \end{array} \quad \begin{array}{r} 5.0 \\ 120.5 / 25.6 \end{array} \quad 20.5$$

$$2.7 \quad 19.6 \quad 26.8 / \begin{array}{r} 5.4 \\ 120.7 \end{array} \quad \begin{array}{r} 5.2 \\ -2.3 \end{array} \quad \begin{array}{r} 8.7 \\ 120.8 / 25.8 \end{array} \quad 24$$

$$3.2 \quad 23.5 \quad 27.4 / \begin{array}{r} 5.0 \\ 121.2 \end{array} \quad \begin{array}{r} 4.7 \\ -1.7 \end{array} \quad \begin{array}{r} 4.4 \\ 121.2 / 26.2 \end{array} \quad 24.5$$

4.5/4.25

$$4.5 \quad 23.8 \quad 27.4 / \begin{array}{r} 5.7 \\ 121.4 \end{array} \quad \begin{array}{r} 5.5 \\ -1.0 \end{array} \quad \begin{array}{r} 4.7 \\ 121.2 / 27.4 \end{array} \quad 26$$

$$4.7 \quad 25 \quad 28.2 / \begin{array}{r} 5.5 \\ 121.9 \end{array} \quad \begin{array}{r} 4.9 \\ -0.2 \end{array} \quad \begin{array}{r} 4.6 \\ 122.2 / 27.6 \end{array} \quad 27$$

$$5.0 \quad 23.5 \quad 27.6 / \begin{array}{r} 5.5 \\ 121.9 \end{array} \quad \begin{array}{r} 5.0 \end{array} \quad \begin{array}{r} 1.4 \\ 120.6 / 28.2 \end{array} \quad 27$$

$$5.2 \quad 27.8 \quad 29.4 / \begin{array}{r} 4.6 \\ 122.9 \end{array} \quad \begin{array}{r} 4.7 \\ 12.3 \end{array} \quad \begin{array}{r} 4.4 \\ 120.8 / 28.6 \end{array} \quad 2$$

$$5.5 \quad 30.6 / \begin{array}{r} 3.7 \\ 121.8 \end{array} \quad \begin{array}{r} 4.3 \\ 11.2 \end{array} \quad \begin{array}{r} 3.9 \\ 11.6 / 30.2 \end{array}$$

$$5.7 \quad 32.6 / \begin{array}{r} 2.9 \\ 122.8 \end{array} \quad \begin{array}{r} 1.5 \\ 12.2 \end{array} \quad \begin{array}{r} 3.3 \\ 124 / 31.8 \end{array}$$

$$7.9 \quad \begin{array}{r} 4.7 \\ 12.2 \end{array} \quad \begin{array}{r} 5.4 \\ 120.3 / 2.0 \end{array}$$

Sta	+	π	-	Grade	
		715.32			
29				07.1	
B.M.	2.90	715.81	2.42	912.90	912.91
+50				06.9	
E.V.					(912.91)
30				06.7	
+50				06.5	
+80				06.4	
31				06.3	
+60				06.2	
+78				06.2	
32				06.2	
T.P.	1.26	907.92	7.15	906.66	
+30				06.2	
+65					

Gr. Rod.

Lt.

4.

Rt.

8.2

$$\begin{array}{r} 35.4 / 40 \\ 14.2 \end{array}$$

$$\begin{array}{r} 47 \\ 12.3 \end{array}$$

$$\begin{array}{r} 56 \\ 12.6 / 32.2 \end{array}$$

5 pt. in Stamp R. 29+23.53

8.7

$$\begin{array}{r} 37.2 / 38 \\ 15.1 \end{array}$$

$$\begin{array}{r} 48 \\ 14.1 \end{array}$$

$$\begin{array}{r} 59 \\ 13.0 / 33.0 \end{array}$$

9.1

$$\begin{array}{r} 37.6 / 38 \\ 15.3 \end{array}$$

$$\begin{array}{r} 42 \\ + 4.9 \end{array}$$

$$\begin{array}{r} 61 \\ 13.0 / 33.0 \end{array}$$

9.3

$$\begin{array}{r} 37.8 / 39 \\ 15.4 \end{array}$$

$$\begin{array}{r} 46 \\ 14.7 \end{array}$$

$$\begin{array}{r} 62 \\ 13.1 / 33.0 \end{array}$$

9.4

9.5

$$\begin{array}{r} 37.2 / 44 \\ 15.1 \end{array}$$

$$\begin{array}{r} 52 \\ 14.3 \end{array}$$

$$\begin{array}{r} 73 \\ 12.2 / 31.4 \end{array}$$

9.6

$$\begin{array}{r} 35.6 / 5.3 \\ 19.3 \end{array}$$

$$\begin{array}{r} 66 \\ 13.0 \end{array}$$

$$\begin{array}{r} 88 \\ 10.8 / 28.6 \end{array}$$

9.6

9.6

$$\begin{array}{r} 29.8 / 8.2 \\ 11.4 \end{array}$$

$$\begin{array}{r} 9.2 \\ 10.4 \end{array}$$

$$\begin{array}{r} 10.1 \\ 12.5 / 20.0 \end{array}$$

1.7

$$\begin{array}{r} 26.8 / 1.8 \\ 12.17 \end{array}$$

$$\begin{array}{r} 3.2 \\ 1.5 \end{array}$$

$$\begin{array}{r} 36 \\ 12.1 / 23.2 \end{array}$$

1.7

$$\begin{array}{r} 23.0 / 39 \\ 20.0 \end{array}$$

$$\begin{array}{r} 40 \\ - 2.3 \end{array}$$

$$\begin{array}{r} 44 \\ - 2.7 / 21.4 \end{array}$$

16' top

54.

+

A

-

Grade

907.92
 3.59
 902.33

33

06.2

+50

34

R.M.

1.39

906.53

+50

35

+50

36

+50

37

+50

38

06.2

Cor. Rod

Lt

R

Rt.

16' Top

1.7

$$19.8 / \frac{4.1}{-2.9}$$

$$\frac{4.5}{-2.8}$$

$$\frac{5.0}{-3.3} / 22.6$$

1.7

$$22.2 / \frac{5.3}{-3.6}$$

$$\frac{5.4}{-3.7}$$

$$\frac{5.7}{-4.2} / 24.4$$

1.7

$$21.2 / \frac{4.8}{-3.1}$$

$$\frac{6.2}{-4.5}$$

$$\frac{6.7}{-5.0} / 26.0$$

Nail in 18" Oak 125 Lt. 33415

Sta.	+	x	-	Grade
38	+50			06.2
39				
	+50			
40				06.2
3.14	2.53	909.06		906.53
	+52			06.2
41				06.2
	+50			06.2
42	+50			06.2
	+50			06.2
43	+50			06.3
T.P.	6.98	913.80	224	906.82
43	+50			06.4

Gr. Rod Lt K Rt.

Nail in 18" Oak 135' Lt 33415'

2.7	$19.8 / \frac{5.3}{2.4}$	$\frac{56}{-2.7}$	$\frac{54}{-25/20.0}$	2-14-37 4" 86 low.
-----	--------------------------	-------------------	-----------------------	-----------------------

2.7	$24.2 / \frac{9.3}{40.6}$	$\frac{4.4}{-1.5}$	$\frac{46}{40.3/23.6}$
-----	---------------------------	--------------------	------------------------

2.7	$27.0 / \frac{2.9}{10.0}$	$\frac{2.8}{10.1}$	$\frac{3.7}{41.2/25.4}$
-----	---------------------------	--------------------	-------------------------

2.7	$27.4 / \frac{2.7}{10.2}$	$\frac{2.8}{10.1}$	$\frac{3.7}{42.2/25.4}$
-----	---------------------------	--------------------	-------------------------

2.7	$26.6 / \frac{3.1}{41.8}$	$\frac{3.2}{-0.3}$	$\frac{3.7}{47.0/25.0}$
-----	---------------------------	--------------------	-------------------------

2.8	$26.8 / \frac{2.9}{41.9}$	$\frac{2.8}{+0.0}$	$\frac{3.5}{45.3/25.6}$
-----	---------------------------	--------------------	-------------------------

2.4	$27.6 / \frac{7.1}{10.3}$	$\frac{6.8}{10.6}$	$\frac{7.3}{10.1/27.2}$
-----	---------------------------	--------------------	-------------------------

Sta	+	π	-	Grade
		913.80		
44				06.6
	+50			06.8
45				07.0
	+50			07.2
46				07.4
	+50			07.6
47				07.8
T.P.	2.45	914.07	2.18	911.62
	+50			08.0
48				08.2
	+50			08.4
49				08.6
B.M.			3.13	910.94
				910.94

G.C. Rod.

LH

R

Rt

7.2

$$28.2 / \frac{66}{10.6}$$

$$\frac{61}{11.1}$$

$$\frac{63}{10.8} / 27.6$$

7.0

$$28.8 / \frac{61}{10.7}$$

$$\frac{54}{11.6}$$

$$\frac{62}{10.8} / 28.6$$

6.8

$$29.4 / \frac{56}{11.2}$$

$$\frac{45}{12.3}$$

$$\frac{51}{11.7} / 30.4$$

6.6

$$30.6 / \frac{48}{11.0}$$

$$\frac{34}{13.2}$$

$$\frac{44}{12.2} / 31.4$$

6.4

$$31.0 / \frac{44}{12.0}$$

$$\frac{36}{12.8}$$

$$\frac{45}{11.9} / 30.8$$

6.2

$$31.4 / \frac{40}{12.2}$$

$$\frac{32}{13.0}$$

$$\frac{40}{12.2} / 31.4$$

6.0

$$31.4 / \frac{37}{12.3}$$

$$\frac{28}{13.2}$$

$$\frac{35}{12.5} / 32.0$$

4.5/9.47

6.1

$$31.6 / \frac{38}{12.3}$$

$$\frac{28}{13.3}$$

$$\frac{35}{12.6} / 32.2$$

5.9

$$30.2 / \frac{4.3}{11.6}$$

$$\frac{2.9}{13.0}$$

$$\frac{3.5}{12.4} / 31.8$$

5.7

$$29.0 / \frac{4.7}{11.0}$$

$$\frac{3.5}{13.2}$$

$$\frac{4.2}{11.5} / 30.0$$

5.5

$$28.5 / \frac{5.0}{10.5}$$

$$\frac{4.1}{11.4}$$

$$\frac{5.0}{10.5} / 28.0$$

3pk in 20" oak 1' at 49+10

Sta.	+	Σ	-	Grade
		914.07		
49	+50			08.8
50				09.0
	+50			09.2
51				09.4
	+50			09.6
52				09.8
T.P.	582	915.71	4.18	909.89
	+50			10.0
53				10.2
	+50			10.4
54				10.6
	+50			10.8

Gr. Red.

LA

A

RA

5.3

$$28.2 / \frac{4.7}{10.6}$$

$$\frac{4.2}{11.1}$$

$$\frac{5.5}{18.8} / 26.6$$

5.1

$$27.9 / \frac{4.9}{10.2}$$

$$\frac{3.9}{11.2}$$

$$\frac{5.1}{10.0} / 27.0$$

4.9

$$26.2 / \frac{5.3}{11.6}$$

$$\frac{4.0}{10.9}$$

$$\frac{5.0}{12.19} / 26.8$$

4.7

$$25.4 / \frac{5.5}{11.2}$$

$$\frac{4.4}{10.3}$$

$$\frac{5.4}{11.3} / 25.6$$

4.5

$$24.8 / \frac{5.6}{10.9}$$

$$\frac{4.1}{10.2}$$

$$\frac{5.5}{11.0} / 25.0$$

4.3

$$23.9 / \frac{5.3}{11.0}$$

$$\frac{4.6}{10.3}$$

$$\frac{5.1}{11.1} / 25.2$$

stake

RM. 2.88 93.82

910.94

4.52

5.7

$$26.6 / \frac{5.9}{11.8}$$

$$\frac{5.5}{10.2}$$

3.8

$$\frac{4.4}{11.4} / 25.8$$

5.5

$$28.6 / \frac{4.7}{10.8}$$

$$\frac{5.0}{10.5}$$

3.6

$$\frac{3.9}{11.7} / 26.4$$

5.3

$$28.8 / \frac{4.4}{10.9}$$

$$\frac{4.3}{11.0}$$

3.4

$$\frac{3.2}{10.2} / 27.4$$

T.P.

3.94

914.03

173

912.09

5.1

$$27.6 / \frac{4.8}{10.3}$$

$$\frac{4.2}{10.9}$$

3A

$$\frac{5.3}{10.1} / 27.2$$

4.7

$$25.2 / \frac{5.3}{11.6}$$

$$\frac{4.1}{10.1}$$

5.2

$$\frac{5.6}{11.6} / 26.2$$

Atk 11

Sta.	+	π	-	Grade	
		915.71			
55.				11.0	
	+50			11.2	
56				11.2	
	+50			10.9	
57				10.2	
	+50			9.1	
58				07.7	
	+32			06.6	
	+62			05.5	
59				04.0	
T.P.	1.93	904.29	13.35	904.26	Gr. Rod. Grade
	+34			02.8	2.3 01.0

Gr. Rod.

Lt

R

Rk

916.03

4.7

$$258 / \frac{53}{42.4}$$

$$\frac{47}{90}$$

5.0

$$\frac{5.8}{26.12} / 25.4$$

$$T.P. 5.46$$

917.17

432

911.71

4.5

$$27.0 / \frac{45}{100}$$

$$\frac{38}{107}$$

6.0

$$\frac{6.3}{26.17} / 26.4$$

4.5

$$27.4 / \frac{42}{10.3}$$

$$\frac{29}{116}$$

6.0

$$\frac{6.4}{26.16} / 26.2$$

4.8

$$28.2 / \frac{42}{106}$$

$$\frac{27}{121}$$

6.3

$$\frac{6.2}{10.1} / 27.2$$

5.5

$$28.8 / \frac{46}{10.9}$$

$$\frac{29}{126}$$

7.0

$$\frac{6.5}{10.5} / 28.0$$

6.6

$$29.2 / \frac{55}{11.1}$$

$$\frac{34}{132}$$

8.1

$$\frac{7.1}{11.0} / 29.0$$

8.0

$$28.4 / \frac{73}{10.7}$$

$$\frac{62}{12.1}$$

9.5

$$\frac{9.8}{25.17} / 26.4$$

9.1

$$27.8 / \frac{87}{10.4}$$

$$\frac{76}{115}$$

10.6

$$\frac{10.9}{26.17} / 26.4$$

$$T.P. 0.76$$

907.74

1019

906.98

10.2

$$27.2 / \frac{10.1}{10.1}$$

$$\frac{10.2}{10.0}$$

2.2

$$\frac{2.2}{26.00} / 19.0$$

11.7

$$26.4 / \frac{120}{47.7}$$

$$\frac{137}{20.0}$$

3.7

$$\frac{8.6}{4.9} / 29.8$$

21/06/18

1.5

$$333 / \frac{33}{26.00}$$

$$\frac{56}{4.1}$$

4.8

$$\frac{12.5}{26.00} / 30.2$$

T.P.

2.99

898.96

11.77

895.97

9/12 79

Pitch Grade Lt.

Sta	+	X	-	Grade	
		904.29			
59	+67			01.9	4.3 900.00
60				01.1	5.3 899.00
	+22			900.7	5.6 898.7
	+40			00.4	5.9 98.4
	+69			00.2	6.3 98.0
61				900.0	6.8 97.5
	+60			00.3	6.0 98.3
R.P.	11.27	9/12.79	2.76	901.53	901.52 173.8
2				00.9	92.0
	+50			01.8	
63				02.7	
	+50			03.6	

Gr Rod

Lt

R

Rt

898.96

2.4

$$\begin{array}{r} \text{ditch } 1.9 \\ 33.9 / 0.00 \\ \hline 4.3 \end{array}$$

$$\begin{array}{r} 9.1 \\ -6.7 \\ \hline \end{array}$$

-2.9

$$\begin{array}{r} 7.8 \\ -10.7 / 33.0' \\ \hline \end{array}$$

3.2

$$\begin{array}{r} \text{ditch } 2.9 \\ 34.6 / 0.00 \\ \hline 5.3 \end{array}$$

$$\begin{array}{r} 12.6 \\ -7.4 \\ \hline \end{array}$$

-2.7

$$\begin{array}{r} 10.0 \\ -12.1 / 33.0' \\ \hline \end{array}$$

T.P. 9.33

701.60

6.9

892.27

3.6

$$\begin{array}{r} \text{ditch } -2.0' \\ 34.3 / 0.00 \\ \hline 5.6 \end{array}$$

$$\begin{array}{r} -10.4 \\ -0.9 \\ \hline \end{array}$$

-0.9

$$\begin{array}{r} 12.5 \\ -11.6 / 33.0' \\ \hline \end{array}$$

3.9

$$\begin{array}{r} \text{ditch } -2.0' \\ 33.3 / 0.00 \\ \hline 5.9 \end{array}$$

$$\begin{array}{r} 12.0 \\ -10.8 \\ \hline \end{array}$$

-1.2

$$\begin{array}{r} 13.0 \\ -11.8 / 33.0' \\ \hline \end{array}$$

4.1

$$\begin{array}{r} \text{ditch } 2.1' \\ 32.6 / 0.00 \\ \hline 6.3 \end{array}$$

$$\begin{array}{r} 12.0 \\ -10.6 \\ \hline \end{array}$$

1.4

$$\begin{array}{r} 12.6 \\ -11.2 / 33.0' \\ \hline \end{array}$$

4.3

$$\begin{array}{r} \text{ditch } 2.5' \\ 32.7 / 0.00 \\ \hline 6.4 \end{array}$$

$$\begin{array}{r} 12.0 \\ -0.7 \\ \hline \end{array}$$

1.6

$$\begin{array}{r} 9.0 \\ -7.4 / 29.8' \\ \hline \end{array}$$

9.0

$$\begin{array}{r} 23.0 / 0.00 \\ \hline 6.0 \end{array}$$

$$\begin{array}{r} 8.9 \\ -1.9 \\ \hline \end{array}$$

1.3

$$\begin{array}{r} 5.4 \\ -4.1 / 28.2 \\ \hline \end{array}$$

11.7

$$\begin{array}{r} 29.6 / 1.3 \\ \hline 10.6 \end{array}$$

$$\begin{array}{r} 11.9 \\ 0.0 \\ \hline \end{array}$$

0.7

$$\begin{array}{r} 2.5 \\ 40.2 / 23.4' \\ \hline \end{array}$$

T.P. 12.86

912.70

1.76

899.84

11.0

$$\begin{array}{r} 33.0 / 1.3 \\ \hline 12.3 \end{array}$$

$$\begin{array}{r} 9.0 \\ 12.0 \\ \hline \end{array}$$

10.9

$$\begin{array}{r} 11.0 \\ 21.9 / 26.8' \\ \hline \end{array}$$

10.1

$$\begin{array}{r} 33.0 / 1.3 \\ \hline 13.6 \end{array}$$

$$\begin{array}{r} 6.9 \\ 12.2 \\ \hline \end{array}$$

10.0

$$\begin{array}{r} 9.4 \\ 10.6 / 28.2' \\ \hline \end{array}$$

9.2

$$\begin{array}{r} 33.0 / 1.3 \\ \hline 13.5 \end{array}$$

$$\begin{array}{r} 4.6 \\ 12.6 \\ \hline \end{array}$$

9.1

$$\begin{array}{r} 1.7 \\ 4.5 / 30.0 \\ \hline \end{array}$$

sta	+	π	-	Grade
		912.79		

64				04.5
----	--	--	--	------

+50				05.4
-----	--	--	--	------

+62				05.6
-----	--	--	--	------

65				06.3
----	--	--	--	------

+25				06.7
-----	--	--	--	------

+36				06.9
-----	--	--	--	------

+45				07.1
-----	--	--	--	------

+70.25				07.37
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B.M.

542

907.37

Gr. Rod.

712.70

8.3

$$\begin{array}{r} 33.0 \\ + 11.0 \\ \hline 44 \end{array}$$

$$\begin{array}{r} 29 \\ + 5.4 \\ \hline 34 \end{array}$$

8.2

$$\begin{array}{r} 56 \\ + 2.7 \\ \hline 58.7 \end{array}$$

7.4

$$\begin{array}{r} 33.0 \\ + 3.7 \\ \hline 36.7 \end{array}$$

$$\begin{array}{r} 19 \\ + 5.5 \\ \hline 24.5 \end{array}$$

7.3

$$\begin{array}{r} 42 \\ + 3.1 \\ \hline 45.1 \end{array}$$

6.5

$$\begin{array}{r} 32.6 \\ + 3.7 \\ \hline 36.3 \end{array}$$

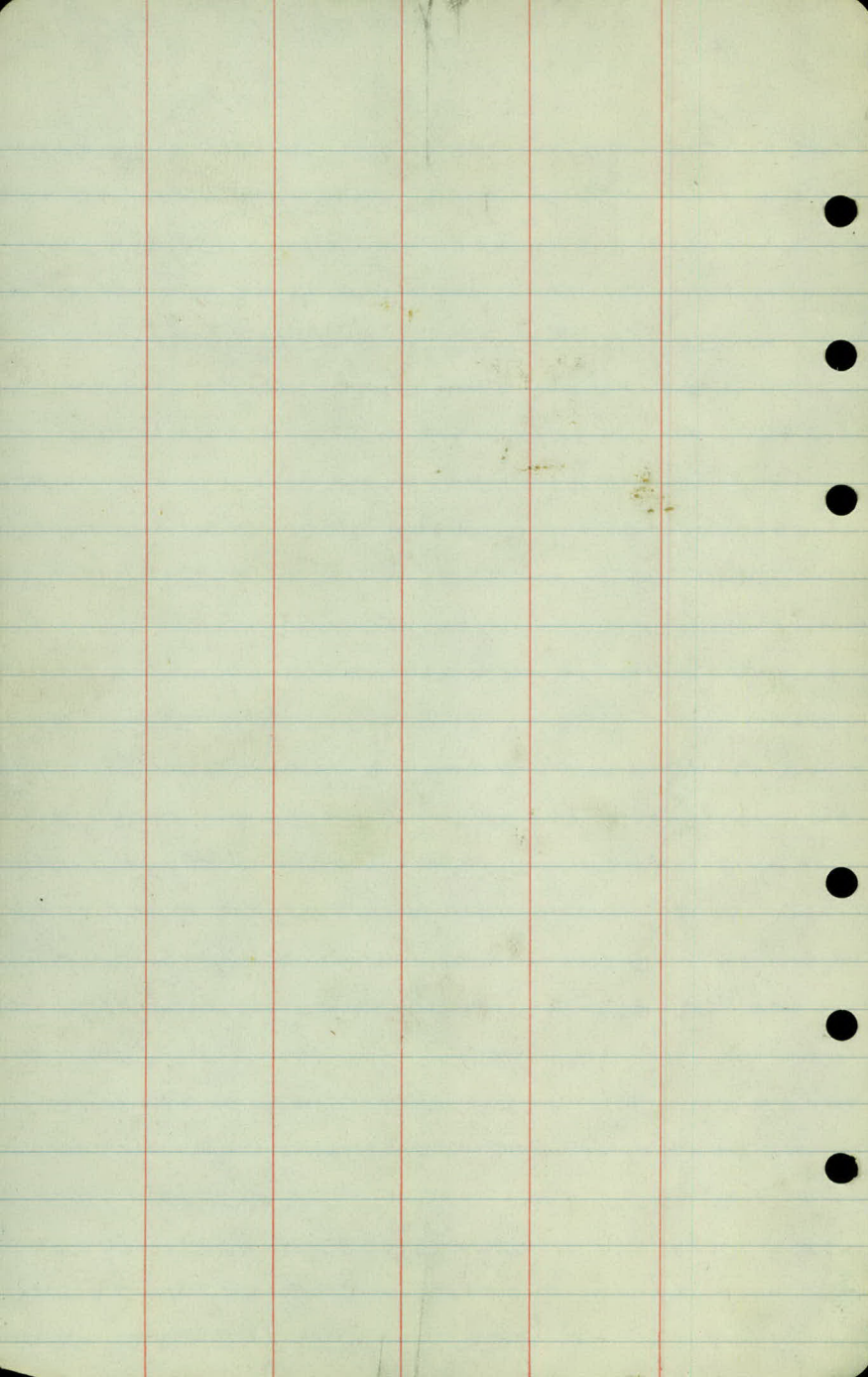
$$\begin{array}{r} 36 \\ + 2.9 \\ \hline 38.9 \end{array}$$

6.4

$$\begin{array}{r} 50 \\ + 4.4 \\ \hline 54.4 \end{array}$$

Tap Brass Plug in Box.

5.32 907.38



Co. Rd. "1"

Grade Change

Slope Stakes

Sta 11450 to - Sta 11600

Sta.	+	π	-	Grade
B.M.	3.25	917.32		(914.07)

11	+50			11.0
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12				11.4
----	--	--	--	------

	+50			11.8
--	-----	--	--	------

13	+50			12.4
----	-----	--	--	------

T.P.	3.98	916.27	5.03	912.29
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14				12.3
----	--	--	--	------

	+50			12.3
--	-----	--	--	------

15				12.2
----	--	--	--	------

	+50			12.2
--	-----	--	--	------

16				12.2
----	--	--	--	------

Gr. Rod

Lk.

d.

Ch

Spk. in 24" Golt. 100' N.E Co. Rd. 7" + Longlake Rd.

5.9

$$\begin{array}{r} 84 \\ -25 \\ \hline \end{array}$$

5.5

$$\begin{array}{r} 81 \\ -26 \\ \hline \end{array}$$

4.9

$$\begin{array}{r} 254 \\ 56 \\ \hline 21.3 \end{array}$$

$$\begin{array}{r} 67 \\ -20 \\ \hline \end{array}$$

$$\begin{array}{r} 52 \\ 17 \\ \hline 26.4 \end{array}$$

4.0

$$\begin{array}{r} 252 \\ 49 \\ \hline 21.1 \end{array}$$

$$\begin{array}{r} 40 \\ -20 \\ \hline \end{array}$$

$$\begin{array}{r} 42 \\ 18 \\ \hline 26.6 \end{array}$$

4.0

$$\begin{array}{r} 238 \\ 56 \\ \hline 20.9 \end{array}$$

$$\begin{array}{r} 59 \\ -19 \\ \hline \end{array}$$

$$\begin{array}{r} 31 \\ 10.9 \\ \hline 20.8 \end{array}$$

4.1

$$\begin{array}{r} 244 \\ 64 \\ \hline 20.7 \end{array}$$

$$\begin{array}{r} 49 \\ -0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 36 \\ 10.5 \\ \hline 28.0 \end{array}$$

4.1

