

Dr. 8 - Bk 139

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN.....Survey

BELLAIRE AVE
From CORD. "D" To Co. Rd. "E"

Road Acc't. No.

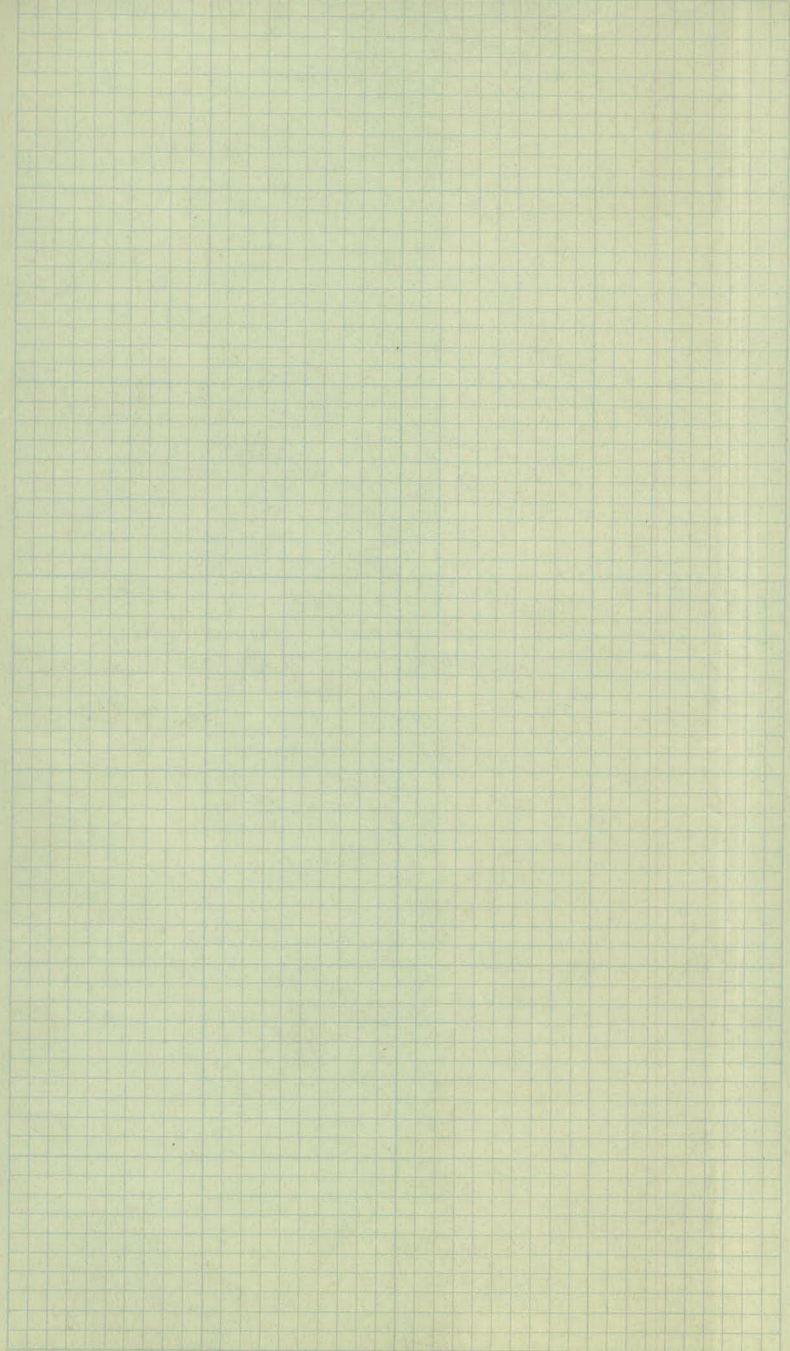
Date Filed.....

File.....

BELLAIRE Ave.

Plan Preliminary survey
from Co. Rd. "D" to "E" = 1/2 Mile

12/1
/37



Angle

Sta. Point Right Left.

Note - Existing ties to
monuments are sufficient
unless stones are to be
disturbed during
construction

52+59.56

Stone Monument
E & Bellevue.

48+97.16 P.O.T.

R.R. spike.

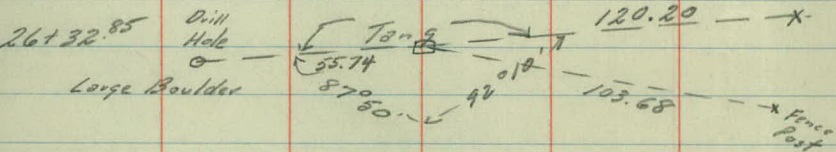
26+32.85 P.I. 0°1' Stone Monument

0+00 Stone Monument at
intersection "D" & Bellevue

Forw. Tang. →

Stone Monument

10" Oak



← Back Tangent

6

2

3

5

4

3

Cultivated

2-24" x 36' Conc. Culv.

15'

26' Branch Road

Cultivated

1

+34 Rd. 59m.

126 P.P.

x 40' 33' x

0

Stone Mon.

14

2

+19 Fence Cor.

13

25'

12

11

10

9

8

7

Cultivated

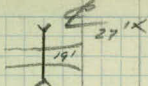
26' Gravel Road

Cultivated

x
x
x
x
x

x x x x x

22
180 Field Ent.
15" x 20' C.M.



149 End Gd. Rt.

21

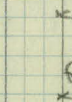


20



168 Begin Gd. Rt.

19



18

Cullington

26' Gravelled Road.

3 Strand Barb wire

Pasture

17

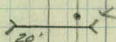
X

16

189 End Gd. Rail.

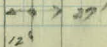


150-24" x 42' Conc. Pipe



15

1469 Begin Gd. Rt.



30

29

28

+85 Field Entr.

27

+97.85 Stone Mon

26

+45 Fence Cor.

25

24

23

2

26' Eroded Road



Cultivated

Cultivated

25'

3.540. End Wire

26'

+03-24"x56' Conc. Pipe
38

37- Begin Ed. Rl.
185 Begin Ed. Rl.

36

35
+89 End Ed. Rl.

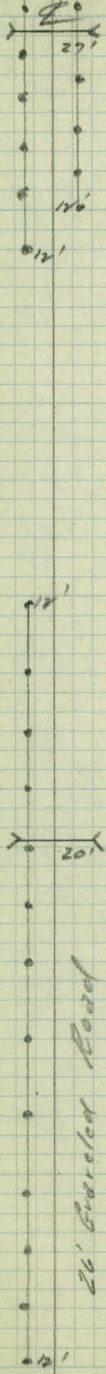
34

+74-24"x42' Conc. Pipe

33

32

+03 Begin Ed. Rl.
31



46

+61 End Ed. Rail

45
+98 End Ed. Rl.

44

43-24"x62' Conc. Pipe

+45 Begin Ed. Rl.

+37 Begin Ed. Rl.

42

41

40

+48 Field Ent.

15"x20' C.M.

+47 Field Ent.

+27 End Ed. Rl.

+22 End Ed. Rl.

39

Cultivated

26' Gravel Road

Cultivated

12'

12'

33'

12'

12'

21'

12'

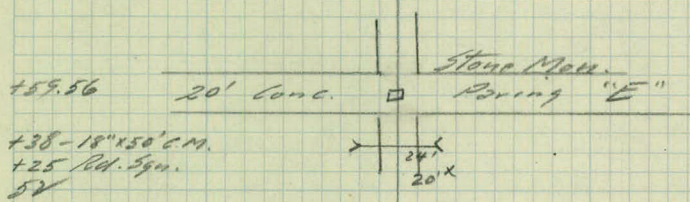
12'

15"x20' C.M.

17'

12'

12'



51

50

49 - Field Entry.

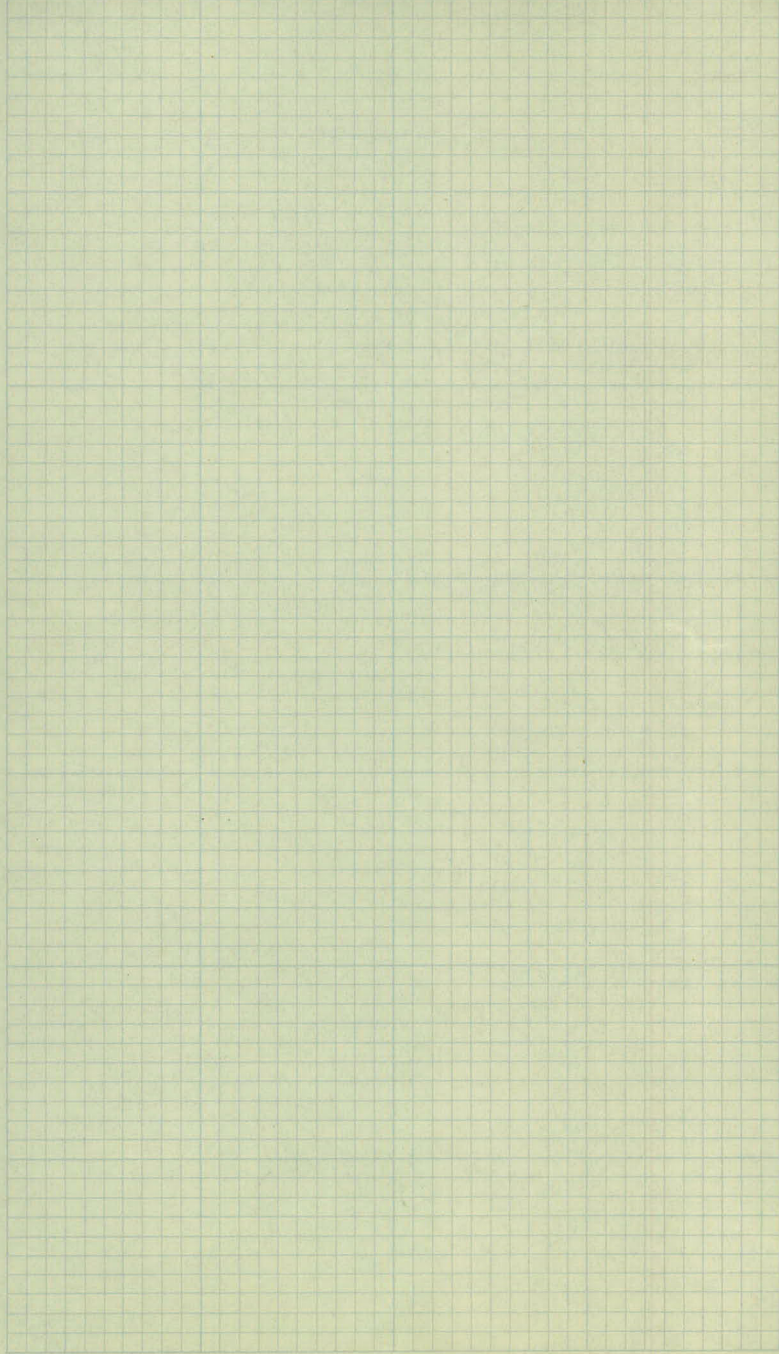
48

47

Cultivated

26' Elevated Road

Cultivated



Cross Sections

St.	+	K	-	Elev.
B.M.	3.65	1028.00		1024.35

0+00				24.8.
------	--	--	--	-------

+18				24.8.
-----	--	--	--	-------

+33				24.4.
-----	--	--	--	-------

+60				23.8.
-----	--	--	--	-------

1+00				23.2.
------	--	--	--	-------

+50				22.8.
-----	--	--	--	-------

2				22.6.
---	--	--	--	-------

+50				22.2.
-----	--	--	--	-------

3				22.0.
---	--	--	--	-------

+40				21.5.
-----	--	--	--	-------

4				20.8.
---	--	--	--	-------

Lt.

E

24

10

Stone monument Bellevue & "D"

$$\frac{5.0}{100} \quad \frac{4.0}{50} \quad 3.2 \quad \frac{2.4}{50} \quad \frac{1.2}{100}$$

Same section 25 Sta. 0+00

$$\frac{8.1}{100} \quad \frac{6.1}{50} \quad \frac{5.6}{31} \quad \frac{4.1}{23} \quad \frac{3.6}{14} \quad \frac{3.9}{14} \quad \frac{3.6}{26} \quad \frac{4.2}{28} \quad \frac{4.3}{32} \quad \frac{2.4}{37} \quad \frac{1.9}{50} \quad \frac{0.3}{100}$$

$$\frac{10.7}{100} \quad \frac{8.8}{50} \quad \frac{7.4}{22} \quad \frac{4.7}{13} \quad \frac{4.2}{14} \quad \frac{4.6}{16} \quad \frac{5.8}{20} \quad \frac{5.6}{21} \quad \frac{4.8}{23} \quad \frac{4.1}{50} \quad \frac{2.7}{100}$$

$$\frac{11.5}{100} \quad \frac{10.5}{50} \quad \frac{9.5}{23} \quad \frac{5.4}{13} \quad \frac{4.8}{14} \quad \frac{5.3}{14} \quad \frac{6.9}{18} \quad \frac{7.3}{23} \quad \frac{7.3}{50} \quad \frac{6.3}{100}$$

$$\frac{7.0}{100} \quad \frac{5.2}{50} \quad \frac{5.3}{20} \quad \frac{5.4}{14} \quad \frac{5.2}{14} \quad \frac{5.9}{14} \quad \frac{8.1}{18} \quad \frac{5.4}{26} \quad \frac{8.6}{50} \quad \frac{5.1}{100}$$

2400-24" Culv. $\frac{9.9}{100}$ $\frac{9.2}{100}$

$$\frac{10.5}{100} \quad \frac{10.0}{50} \quad \frac{10.1}{53} \quad \frac{5.8}{13} \quad \frac{5.4}{14} \quad \frac{6.0}{13} \quad \frac{8.5}{19} \quad \frac{10.1}{50} \quad \frac{7.9}{100}$$

$$\frac{11.2}{100} \quad \frac{10.4}{50} \quad \frac{9.6}{21} \quad \frac{9.4}{18} \quad \frac{6.2}{13} \quad \frac{5.8}{13} \quad \frac{6.2}{13} \quad \frac{7.7}{18} \quad \frac{7.9}{21} \quad \frac{7.5}{50} \quad \frac{6.3}{100}$$

$$\frac{10.4}{100} \quad \frac{9.5}{50} \quad \frac{8.6}{19} \quad \frac{6.4}{13} \quad \frac{6.0}{13} \quad \frac{6.4}{13} \quad \frac{7.6}{17} \quad \frac{7.6}{20} \quad \frac{6.1}{24} \quad \frac{5.9}{50} \quad \frac{5.0}{100}$$

$$\frac{8.7}{100} \quad \frac{7.6}{50} \quad \frac{6.5}{23} \quad \frac{7.8}{20} \quad \frac{8.1}{16} \quad \frac{7.1}{13} \quad \frac{6.5}{13} \quad \frac{7.0}{13} \quad \frac{8.5}{18} \quad \frac{8.5}{20} \quad \frac{5.1}{26} \quad \frac{5.3}{50} \quad \frac{4.8}{100}$$

$$\frac{6.6}{100} \quad \frac{4.6}{50} \quad \frac{4.0}{26} \quad \frac{5.5}{19} \quad \frac{8.7}{16} \quad \frac{7.9}{13} \quad \frac{7.2}{14} \quad \frac{7.5}{14} \quad \frac{8.3}{16} \quad \frac{8.0}{20} \quad \frac{4.2}{26} \quad \frac{5.0}{50} \quad \frac{5.4}{100}$$

Sta. + K - Elev.

✓
1028.00

4+50 20.3

5 19.8 ✓

T.P. 7.70 ✓
1027.38 8.32 1019.68 ✓

+50 19.4

6 19.0

+50 19.0

7 18.4

+50 18.1

8 18.1

+50 18.0

9 18.0

+50 18.0

10 18.0

+50 18.0

Lt.

E

Rt. 11

$$\begin{array}{cccccccccccc} 6.6 & 4.6 & 4.0 & 8.9 & 9.0 & 8.4 & 7.7 & 8.1 & 8.8 & 8.2 & 4.7 & 6.1 & 7.3 \\ 100 & 50 & 27 & 20 & 16 & 13 & 13 & 16 & 19 & 26 & 50 & 100 \end{array}$$

$$\begin{array}{cccccccccccc} 8.9 & 6.4 & 6.1 & 9.4 & 9.4 & 8.7 & 8.2 & 8.7 & 8.5 & 9.2 & 7.3 & 8.4 & 8.7 \\ 100 & 51 & 25 & 19 & 16 & 13 & 13 & 17 & 20 & 24 & 62 & 100 \end{array}$$

$$\begin{array}{cccccccccccc} 9.0 & 6.9 & 6.8 & 9.6 & 9.5 & 8.4 & 8.0 & 8.5 & 9.7 & 9.7 & 8.2 & 9.1 & 8.9 \\ 100 & 30 & 24 & 19 & 18 & 13 & 13 & 19 & 20 & 23 & 47 & 100 \end{array}$$

$$\begin{array}{cccccccccccc} 10.7 & 9.1 & 8.6 & 8.9 & 9.7 & 10.0 & 9.1 & 8.4 & 8.6 & 10.1 & 10.5 & 9.4 & 10.0 & 9.6 \\ 100 & 60 & 39 & 22 & 20 & 18 & 13 & 13 & 16 & 20 & 22 & 34 & 100 \end{array}$$

$$\begin{array}{cccccccccccc} 12.1 & 11.0 & 10.2 & 8.8 & 8.4 & 9.0 & 10.6 & 10.9 & 10.4 & 10.5 & 9.9 \\ 100 & 48 & 19 & 13 & 14 & 17 & 21 & 23 & 60 & 100 \end{array}$$

$$\begin{array}{cccccccccccc} 13.0 & 12.1 & 11.5 & 9.5 & 9.0 & 9.3 & 11.7 & 11.6 & 11.1 & 11.0 & 10.0 \\ 100 & 60 & 21 & 14 & 9 & 13 & 16 & 20 & 24 & 59 & 100 \end{array}$$

$$\begin{array}{cccccccccccc} 12.7 & 13.2 & 12.9 & 12.5 & 11.9 & 9.7 & 9.3 & 9.6 & 12.1 & 11.9 & 11.4 & 11.0 & 10.2 \\ 100 & 84 & 50 & 25 & 20 & 13 & 13 & 19 & 21 & 23 & 65 & 100 \end{array}$$

$$\begin{array}{cccccccccccc} 11.2 & 12.1 & 12.3 & 12.1 & 9.5 & 9.3 & 9.7 & 11.9 & 11.9 & 11.1 & 11.1 & 10.1 \\ 100 & 81 & 58 & 22 & 14 & 17 & 17 & 21 & 23 & 50 & 100 \end{array}$$

$$\begin{array}{cccccccccccc} 8.5 & 9.4 & 11.0 & 11.4 & 9.7 & 9.4 & 9.7 & 11.8 & 11.8 & 11.1 & 10.2 & 9.8 \\ 100 & 83 & 51 & 18 & 13 & 13 & 18 & 21 & 23 & 70 & 100 \end{array}$$

$$\begin{array}{cccccccccccc} 4.5 & 7.0 & 9.7 & 10.7 & 11.0 & 9.8 & 9.4 & 9.7 & 11.9 & 12.1 & 10.6 & 10.1 & 9.0 & 8.5 \\ 100 & 69 & 22 & 20 & 17 & 13 & 13 & 17 & 21 & 24 & 56 & 75 & 100 \end{array}$$

$$\begin{array}{cccccccccccc} +3.4 & 00 & 5.5 & 7.9 & 10.3 & 11.1 & 11.0 & 9.9 & 9.4 & 8.8 & 11.7 & 11.8 & 10.1 & 9.9 & 7.5 \\ 114 & 93 & 48 & 25 & 22 & 17 & 18 & 17 & 13 & 18 & 21 & 24 & 54 & 100 \end{array}$$

$$\begin{array}{cccccccccccc} +10.0 & 00 & 3.4 & 6.2 & 10.3 & 10.7 & 9.9 & 9.4 & 9.6 & 11.2 & 11.5 & 9.6 & 9.5 & 7.0 \\ 117 & 70 & 50 & 29 & 23 & 18 & 13 & 13 & 17 & 21 & 25 & 54 & 100 \end{array}$$

$$\begin{array}{cccccccccccc} +18.2 & +16.1 & +10.0 & 00 & 3.5 & 10.1 & 10.8 & 10.3 & 9.4 & 9.7 & 11.3 & 11.5 & 9.1 & 9.5 & 7.7 & 6.7 \\ 150 & 125 & 95 & 52 & 31 & 22 & 16 & 14 & 13 & 17 & 21 & 25 & 47 & 88 & 100 \end{array}$$

Sta.	+	π	-	Elev.
		1027.38		
11+00				17.8 ✓
+50				17.7
12+00				17.5
B.M.	3.56	1022.67 ✓	8.27	1019.11 ✓
+50				17.2
13				17.3
+50				17.3
14				17.1
+50				17.0
15				17.0
+50				17.2
16				17.5

INV LT. 24 PCP
 1017.08
 INV RT.
 1016.28

Lt.

C

Rt.

12

$$\begin{array}{r} +17.8 \\ 150 \end{array} \begin{array}{r} +17.2 \\ 132 \end{array} \begin{array}{r} +10.0 \\ 89 \end{array} \begin{array}{r} 00 \\ 47 \end{array} \begin{array}{r} 2.8 \\ 31 \end{array} \begin{array}{r} 9.8 \\ 22 \end{array} \begin{array}{r} 10.5 \\ 15 \end{array} \begin{array}{r} 10.1 \\ 13 \end{array} \begin{array}{r} 96.8 \\ 13 \end{array} \begin{array}{r} 11.6 \\ 78 \end{array} \begin{array}{r} 11.5 \\ 21 \end{array} \begin{array}{r} 8.7 \\ 26 \end{array} \begin{array}{r} 9.3 \\ 54 \end{array} \begin{array}{r} 7.1 \\ 100 \end{array}$$

$$\begin{array}{r} +18.0 \\ 134 \end{array} \begin{array}{r} +16.2 \\ 116 \end{array} \begin{array}{r} +10.0 \\ 84 \end{array} \begin{array}{r} 00 \\ 44 \end{array} \begin{array}{r} 2.9 \\ 30 \end{array} \begin{array}{r} 10.2 \\ 21 \end{array} \begin{array}{r} 11.0 \\ 16 \end{array} \begin{array}{r} 10.4 \\ 13 \end{array} \begin{array}{r} 9.7 \\ 13 \end{array} \begin{array}{r} 10.2 \\ 17 \end{array} \begin{array}{r} 11.7 \\ 21 \end{array} \begin{array}{r} 8.8 \\ 26 \end{array} \begin{array}{r} 9.5 \\ 51 \end{array} \begin{array}{r} 8.1 \\ 100 \end{array}$$

$$\begin{array}{r} +16.6 \\ 124 \end{array} \begin{array}{r} +10.0 \\ 93 \end{array} \begin{array}{r} +12.6 \\ 61 \end{array} \begin{array}{r} 3.7 \\ 35 \end{array} \begin{array}{r} 4.6 \\ 29 \end{array} \begin{array}{r} 10.7 \\ 21 \end{array} \begin{array}{r} 11.2 \\ 17 \end{array} \begin{array}{r} 10.4 \\ 13 \end{array} \begin{array}{r} 9.9 \\ 13 \end{array} \begin{array}{r} 10.4 \\ 16 \end{array} \begin{array}{r} 11.9 \\ 21 \end{array} \begin{array}{r} 12.1 \\ 26 \end{array} \begin{array}{r} 10.1 \\ 50 \end{array} \begin{array}{r} 11.1 \\ 100 \end{array}$$

$$\begin{array}{r} +12.5 \\ 145 \end{array}$$

Spike in fence post 150' Rt. 56, 13+15

$$\begin{array}{r} +17.3 \\ 138 \end{array} \begin{array}{r} +10.0 \\ 106 \end{array} \begin{array}{r} 00 \\ 54 \end{array} \begin{array}{r} 0.8 \\ 47 \end{array} \begin{array}{r} 3.0 \\ 25 \end{array} \begin{array}{r} 6.3 \\ 21 \end{array} \begin{array}{r} 6.9 \\ 16 \end{array} \begin{array}{r} 6.0 \\ 13 \end{array} \begin{array}{r} 5.5 \\ 5 \end{array} \begin{array}{r} 5.6 \\ 13 \end{array} \begin{array}{r} 7.5 \\ 17 \end{array} \begin{array}{r} 7.5 \\ 22 \end{array} \begin{array}{r} 6.5 \\ 23 \end{array} \begin{array}{r} 6.9 \\ 63 \end{array} \begin{array}{r} 6.5 \\ 100 \end{array}$$

$$\begin{array}{r} 1.2 \\ 100 \end{array} \begin{array}{r} 5.2 \\ 48 \end{array} \begin{array}{r} 6.1 \\ 23 \end{array} \begin{array}{r} 7.2 \\ 20 \end{array} \begin{array}{r} 6.9 \\ 16 \end{array} \begin{array}{r} 5.8 \\ 13 \end{array} \begin{array}{r} 5.4 \\ 54 \end{array} \begin{array}{r} 5.7 \\ 13 \end{array} \begin{array}{r} 7.7 \\ 17 \end{array} \begin{array}{r} 7.9 \\ 22 \end{array} \begin{array}{r} 7.3 \\ 26 \end{array} \begin{array}{r} 7.2 \\ 58 \end{array} \begin{array}{r} 6.7 \\ 100 \end{array}$$

$$\begin{array}{r} 4.4 \\ 100 \end{array} \begin{array}{r} 6.6 \\ 64 \end{array} \begin{array}{r} 7.5 \\ 37 \end{array} \begin{array}{r} 7.6 \\ 18 \end{array} \begin{array}{r} 5.8 \\ 13 \end{array} \begin{array}{r} 5.4 \\ 54 \end{array} \begin{array}{r} 5.7 \\ 17 \end{array} \begin{array}{r} 7.8 \\ 17 \end{array} \begin{array}{r} 7.9 \\ 23 \end{array} \begin{array}{r} 7.3 \\ 63 \end{array} \begin{array}{r} 6.9 \\ 100 \end{array}$$

$$\begin{array}{r} 4.2 \\ 100 \end{array} \begin{array}{r} 7.1 \\ 65 \end{array} \begin{array}{r} 8.8 \\ 36 \end{array} \begin{array}{r} 8.3 \\ 18 \end{array} \begin{array}{r} 6.0 \\ 13 \end{array} \begin{array}{r} 5.6 \\ 5 \end{array} \begin{array}{r} 5.9 \\ 13 \end{array} \begin{array}{r} 8.4 \\ 19 \end{array} \begin{array}{r} 8.4 \\ 23 \end{array} \begin{array}{r} 7.5 \\ 67 \end{array} \begin{array}{r} 7.2 \\ 100 \end{array}$$

$$\begin{array}{r} 00 \\ 100 \end{array} \begin{array}{r} 3.4 \\ 83 \end{array} \begin{array}{r} 7.9 \\ 54 \end{array} \begin{array}{r} 9.3 \\ 27 \end{array} \begin{array}{r} 8.8 \\ 18 \end{array} \begin{array}{r} 6.1 \\ 17 \end{array} \begin{array}{r} 5.7 \\ 5 \end{array} \begin{array}{r} 5.9 \\ 13 \end{array} \begin{array}{r} 8.6 \\ 19 \end{array} \begin{array}{r} 8.4 \\ 67 \end{array} \begin{array}{r} 8.2 \\ 100 \end{array}$$

$$\begin{array}{r} 00 \\ 87 \end{array} \begin{array}{r} 2.4 \\ 71 \end{array} \begin{array}{r} 6.8 \\ 57 \end{array} \begin{array}{r} 9.4 \\ 27 \end{array} \begin{array}{r} 9.0 \\ 18 \end{array} \begin{array}{r} 5.9 \\ 13 \end{array} \begin{array}{r} 5.7 \\ 5 \end{array} \begin{array}{r} 6.1 \\ 17 \end{array} \begin{array}{r} 9.5 \\ 20 \end{array} \begin{array}{r} 10.2 \\ 30 \end{array} \begin{array}{r} 10.3 \\ 77 \end{array} \begin{array}{r} 10.7 \\ 100 \end{array}$$

Calc.

103

11.1

$$\begin{array}{r} +18.8 \\ 100 \end{array} \begin{array}{r} 00 \\ 71 \end{array} \begin{array}{r} 2.7 \\ 61 \end{array} \begin{array}{r} 8.4 \\ 38 \end{array} \begin{array}{r} 9.3 \\ 25 \end{array} \begin{array}{r} 9.7 \\ 21 \end{array} \begin{array}{r} 6.1 \\ 13 \end{array} \begin{array}{r} 5.5 \\ 5 \end{array} \begin{array}{r} 5.6 \\ 13 \end{array} \begin{array}{r} 10.2 \\ 24 \end{array} \begin{array}{r} 10.2 \\ 40 \end{array} \begin{array}{r} 11.3 \\ 100 \end{array}$$

$$\begin{array}{r} +16.8 \\ 129 \end{array} \begin{array}{r} +10.0 \\ 107 \end{array} \begin{array}{r} 00 \\ 67 \end{array} \begin{array}{r} 3.1 \\ 56 \end{array} \begin{array}{r} 7.6 \\ 34 \end{array} \begin{array}{r} 8.0 \\ 17 \end{array} \begin{array}{r} 5.7 \\ 13 \end{array} \begin{array}{r} 5.2 \\ 5 \end{array} \begin{array}{r} 5.2 \\ 13 \end{array} \begin{array}{r} 8.4 \\ 21 \end{array} \begin{array}{r} 11.0 \\ 27 \end{array} \begin{array}{r} 11.0 \\ 53 \end{array} \begin{array}{r} 10.0 \\ 100 \end{array}$$

Sta.	+	π	-	Elev.
16+50		✓ 1022.67		18.0
17				18.7
+50				19.4
18				20.5

T.P.	7.52	✓ 1028.02	2.87	✓ 1020.10
16+50				(18.0)

17				(18.7)
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+50				(19.4)
-----	--	--	--	--------

18				(20.5)
----	--	--	--	--------

+50				22.0
-----	--	--	--	------

19				23.5
----	--	--	--	------

+50				24.9
-----	--	--	--	------

20				26.4
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T.P.	9.63	✓ 1036.63	1.02	✓ 1027.00
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Lt.

E

Rt. 13

$$\begin{array}{r} 26 \\ 40 \end{array} \quad \begin{array}{r} 66 \\ 23 \end{array} \quad \begin{array}{r} 67 \\ 17 \end{array} \quad \begin{array}{r} 52 \\ 13 \end{array} \quad \begin{array}{r} 47 \\ 13 \end{array} \quad \begin{array}{r} 50 \\ 13 \end{array} \quad \begin{array}{r} 91 \\ 22 \end{array} \quad \begin{array}{r} 102 \\ 29 \end{array} \quad \begin{array}{r} 110 \\ 62 \end{array} \quad \begin{array}{r} 97 \\ 100 \end{array}$$

$$\begin{array}{r} 18 \\ 25 \end{array} \quad \begin{array}{r} 53 \\ 19 \end{array} \quad \begin{array}{r} 55 \\ 16 \end{array} \quad \begin{array}{r} 46 \\ 13 \end{array} \quad \begin{array}{r} 40 \\ 14 \end{array} \quad \begin{array}{r} 43 \\ 22 \end{array} \quad \begin{array}{r} 82 \\ 28 \end{array} \quad \begin{array}{r} 87 \\ 63 \end{array} \quad \begin{array}{r} 101 \\ 100 \end{array}$$

$$\begin{array}{r} 36 \\ 20 \end{array} \quad \begin{array}{r} 40 \\ 16 \end{array} \quad \begin{array}{r} 35 \\ 13 \end{array} \quad \begin{array}{r} 33 \\ 13 \end{array} \quad \begin{array}{r} 36 \\ 20 \end{array} \quad \begin{array}{r} 71 \\ 20 \end{array} \quad \begin{array}{r} 80 \\ 30 \end{array} \quad \begin{array}{r} 86 \\ 34 \end{array} \quad \begin{array}{r} 110 \\ 100 \end{array}$$

$$\begin{array}{r} 26 \\ 22 \end{array} \quad \begin{array}{r} 29 \\ 16 \end{array} \quad \begin{array}{r} 26 \\ 13 \end{array} \quad \begin{array}{r} 22 \\ 13 \end{array} \quad \begin{array}{r} 26 \\ 22 \end{array} \quad \begin{array}{r} 61 \\ 22 \end{array} \quad \begin{array}{r} 74 \\ 28 \end{array} \quad \begin{array}{r} 80 \\ 47 \end{array} \quad \begin{array}{r} 102 \\ 73 \end{array} \quad \begin{array}{r} 107 \\ 100 \end{array}$$

$$\begin{array}{r} +6.0 \\ 103 \end{array} \quad \begin{array}{r} 00 \\ 74 \end{array} \quad \begin{array}{r} 5.2 \\ 50 \end{array} \quad (10.0)$$

$$\begin{array}{r} +5.5 \\ 112 \end{array} \quad \begin{array}{r} +3.1 \\ 78 \end{array} \quad \begin{array}{r} 00 \\ 62 \end{array} \quad \begin{array}{r} 35 \\ 44 \end{array} \quad (9.3)$$

$$\begin{array}{r} +4.4 \\ 114 \end{array} \quad \begin{array}{r} +3.2 \\ 81 \end{array} \quad \begin{array}{r} 00 \\ 57 \end{array} \quad \begin{array}{r} 2.7 \\ 41 \end{array} \quad \begin{array}{r} 5.3 \\ 27 \end{array} \quad (8.6)$$

$$\begin{array}{r} +3.1 \\ 100 \end{array} \quad \begin{array}{r} 00 \\ 55 \end{array} \quad \begin{array}{r} 1.2 \\ 47 \end{array} \quad \begin{array}{r} 2.3 \\ 30 \end{array} \quad (7.5)$$

$$\begin{array}{r} 65 \\ 20 \end{array} \quad \begin{array}{r} 70 \\ 15 \end{array} \quad \begin{array}{r} 65 \\ 13 \end{array} \quad \begin{array}{r} 60 \\ 14 \end{array} \quad \begin{array}{r} 65 \\ 21 \end{array} \quad \begin{array}{r} 50 \\ 21 \end{array} \quad \begin{array}{r} 110 \\ 37 \end{array} \quad \begin{array}{r} 129 \\ 52 \end{array} \quad \begin{array}{r} 150 \\ 100 \end{array}$$

$$\begin{array}{r} 52 \\ 20 \end{array} \quad \begin{array}{r} 55 \\ 17 \end{array} \quad \begin{array}{r} 51 \\ 15 \end{array} \quad \begin{array}{r} 45 \\ 14 \end{array} \quad \begin{array}{r} 50 \\ 17 \end{array} \quad \begin{array}{r} 60 \\ 24 \end{array} \quad \begin{array}{r} 68 \\ 34 \end{array} \quad \begin{array}{r} 89 \\ 64 \end{array} \quad \begin{array}{r} 123 \\ 100 \end{array}$$

$$\begin{array}{r} 40 \\ 20 \end{array} \quad \begin{array}{r} 42 \\ 16 \end{array} \quad \begin{array}{r} 37 \\ 14 \end{array} \quad \begin{array}{r} 31 \\ 13 \end{array} \quad \begin{array}{r} 34 \\ 18 \end{array} \quad \begin{array}{r} 50 \\ 24 \end{array} \quad \begin{array}{r} 56 \\ 34 \end{array} \quad \begin{array}{r} 79 \\ 57 \end{array} \quad \begin{array}{r} 113 \\ 100 \end{array}$$

$$\begin{array}{r} 31 \\ 21 \end{array} \quad \begin{array}{r} 31 \\ 16 \end{array} \quad \begin{array}{r} 21 \\ 13 \end{array} \quad \begin{array}{r} 16 \\ 12 \end{array} \quad \begin{array}{r} 19 \\ 21 \end{array} \quad \begin{array}{r} 62 \\ 32 \end{array} \quad \begin{array}{r} 97 \\ 67 \end{array} \quad \begin{array}{r} 136 \\ 100 \end{array}$$

Sta.	+	K	-	Elev.
18+50		1036.63		(22.0)

19				(23.5)
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+50				(24.9)
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20				(26.4)
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+50				27.9
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21				29.9
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+50				31.6
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T.P.	2.20	1036.63	2.20	1034.43
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22				33.0
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+50				34.1
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23				35.0
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+50				35.6
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24				35.8
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T.P.	3.00	1038.88	0.75	1035.88
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Lt.

2

Rt. 14

$$\frac{5.6}{105} \quad \frac{5.1}{72} \quad \frac{7.2}{45} \quad \frac{8.2}{31} \quad (14.6)$$

$$\frac{5.7}{100} \quad \frac{5.3}{83} \quad \frac{5.5}{50} \quad \frac{6.5}{30} \quad (13.1)$$

$$\frac{6.6}{100} \quad \frac{5.9}{55} \quad \frac{6.8}{29} \quad (11.7)$$

$$\frac{8.3}{100} \quad \frac{7.6}{70} \quad \frac{8.4}{26} \quad (10.2)$$

$$\frac{10.3}{100} \quad \frac{9.9}{53} \quad \frac{10.2}{22} \quad \frac{10.6}{20} \quad \frac{10.2}{15} \quad \frac{9.1}{13} \quad \frac{8.7}{8} \quad \frac{8.8}{11} \quad \frac{8.6}{12} \quad \frac{13.0}{19} \quad \frac{17.6}{28} \quad \frac{21.2}{50} \quad \frac{24.2}{100}$$

$$\frac{11.1}{100} \quad \frac{9.6}{55} \quad \frac{7.8}{26} \quad \frac{7.8}{22} \quad \frac{8.5}{21} \quad \frac{8.5}{16} \quad \frac{7.2}{14} \quad \frac{6.7}{6} \quad \frac{7.1}{11} \quad \frac{6.9}{13} \quad \frac{14.0}{24} \quad \frac{16.2}{30} \quad \frac{19.8}{51} \quad \frac{24.5}{100}$$

$$\frac{10.6}{100} \quad \frac{7.0}{55} \quad \frac{4.2}{26} \quad \frac{4.6}{23} \quad \frac{6.5}{20} \quad \frac{6.3}{16} \quad \frac{5.6}{14} \quad \frac{5.0}{5} \quad \frac{5.3}{11} \quad \frac{4.9}{13} \quad \frac{8.0}{22} \quad \frac{10.8}{28} \quad \frac{14.0}{44} \quad \frac{23.2}{100}$$

$$\frac{9.5}{100} \quad \frac{6.1}{61} \quad \frac{2.7}{27} \quad \frac{2.6}{23} \quad \frac{4.9}{19} \quad \frac{5.0}{15} \quad \frac{4.1}{13} \quad \frac{3.6}{8} \quad \frac{4.2}{14} \quad \frac{4.9}{16} \quad \frac{5.0}{20} \quad \frac{2.7}{24} \quad \frac{3.9}{28} \quad \frac{8.0}{50} \quad \frac{14.0}{75} \quad \frac{19.8}{100}$$

2

$$\frac{9.0}{100} \quad \frac{5.0}{53} \quad \frac{3.3}{27} \quad \frac{2.3}{23} \quad \frac{3.4}{21} \quad \frac{4.1}{19} \quad \frac{3.8}{16} \quad \frac{3.1}{14} \quad \frac{2.5}{8} \quad \frac{2.9}{13} \quad \frac{3.9}{16} \quad \frac{3.7}{19} \quad \frac{1.4}{24} \quad \frac{2.0}{32} \quad \frac{5.1}{50} \quad \frac{12.8}{75} \quad \frac{20.4}{100}$$

$$\frac{7.4}{100} \quad \frac{3.5}{55} \quad \frac{1.8}{25} \quad \frac{1.2}{23} \quad \frac{2.4}{21} \quad \frac{3.1}{17} \quad \frac{2.2}{13} \quad \frac{1.6}{8} \quad \frac{2.1}{13} \quad \frac{2.9}{16} \quad \frac{3.0}{19} \quad \frac{0.7}{23} \quad \frac{1.5}{31} \quad \frac{2.7}{41} \quad \frac{4.7}{50} \quad \frac{14.0}{85} \quad \frac{18.2}{100}$$

$$\frac{6.1}{100} \quad \frac{3.0}{59} \quad \frac{0.2}{23} \quad \frac{2.1}{20} \quad \frac{2.1}{15} \quad \frac{1.6}{13} \quad \frac{1.0}{8} \quad \frac{1.5}{13} \quad \frac{2.3}{17} \quad \frac{2.2}{20} \quad \frac{10.3}{25} \quad \frac{1.0}{35} \quad \frac{4.2}{54} \quad \frac{8.3}{70} \quad \frac{15.2}{100}$$

$$\frac{7.3}{100} \quad \frac{4.8}{58} \quad \frac{1.0}{21} \quad \frac{2.1}{16} \quad \frac{1.3}{13} \quad \frac{0.8}{8} \quad \frac{1.4}{14} \quad \frac{2.1}{16} \quad \frac{2.3}{20} \quad \frac{1.1}{23} \quad \frac{2.0}{30} \quad \frac{4.7}{50} \quad \frac{16.0}{100}$$

Sta.	+	π	-	Elev.
24+50		1038.88		35.5

25				34.9
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+50				34.2
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26				33.6
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+50				32.6
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B.M.	6.11	1038.88	6.11	1032.77
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27				31.5
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T.P.	3.41	1036.18	6.11	1032.77
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+50				30.4
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28				29.2
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+50				28.4
-----	--	--	--	------

29				27.7
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T.P.	9.68	1034.39	11.47	1024.71
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Lt.

E

Rt.

15

$\frac{11.3}{100}$ $\frac{8.6}{51}$ $\frac{7.0}{22}$ $\frac{4.2}{14}$ $\frac{3.4}{13}$ $\frac{3.7}{13}$ $\frac{4.9}{16}$ $\frac{5.0}{19}$ $\frac{4.5}{21}$ $\frac{5.3}{31}$ $\frac{7.2}{51}$ $\frac{17.3}{100}$

$\frac{13.1}{100}$ $\frac{11.0}{63}$ $\frac{8.3}{22}$ $\frac{4.4}{14}$ $\frac{4.0}{13}$ $\frac{4.4}{13}$ $\frac{5.4}{16}$ $\frac{5.5}{20}$ $\frac{5.2}{21}$ $\frac{5.5}{46}$ $\frac{6.4}{54}$ $\frac{14.3}{100}$

$\frac{13.1}{100}$ $\frac{10.3}{50}$ $\frac{8.2}{20}$ $\frac{5.4}{15}$ $\frac{4.7}{13}$ $\frac{5.0}{13}$ $\frac{6.0}{16}$ $\frac{5.9}{19}$ $\frac{5.2}{21}$ $\frac{5.0}{55}$ $\frac{8.7}{100}$

$\frac{12.1}{100}$ $\frac{10.5}{59}$ $\frac{9.4}{27}$ $\frac{7.9}{17}$ $\frac{6.0}{14}$ $\frac{5.3}{13}$ $\frac{5.8}{16}$ $\frac{6.7}{20}$ $\frac{4.0}{22}$ $\frac{6.2}{35}$ $\frac{5.6}{75}$ $\frac{4.0}{75}$ $\frac{6.0}{100}$

$\frac{13.0}{100}$ $\frac{12.0}{51}$ $\frac{10.0}{21}$ $\frac{7.0}{13}$ $\frac{6.3}{14}$ $\frac{6.7}{14}$ $\frac{7.8}{17}$ $\frac{7.6}{20}$ $\frac{6.2}{24}$ $\frac{5.0}{46}$ $\frac{3.1}{78}$ $\frac{2.9}{100}$

Ctr. Stone Monument Sta. 26+32.85

$\frac{15.2}{100}$ $\frac{13.8}{61}$ $\frac{11.0}{21}$ $\frac{8.0}{14}$ $\frac{7.4}{15}$ $\frac{7.8}{15}$ $\frac{8.7}{17}$ $\frac{8.8}{20}$ $\frac{6.1}{25}$ $\frac{4.2}{47}$ $\frac{3.3}{67}$ $\frac{0.6}{100}$

$\frac{14.5}{100}$ $\frac{12.4}{59}$ $\frac{9.5}{21}$ $\frac{6.3}{13}$ $\frac{5.8}{13}$ $\frac{6.1}{13}$ $\frac{7.2}{17}$ $\frac{7.1}{21}$ $\frac{5.9}{23}$ $\frac{4.9}{43}$ $\frac{3.6}{70}$ $\frac{1.6}{100}$

$\frac{16.5}{100}$ $\frac{14.0}{60}$ $\frac{11.6}{22}$ $\frac{7.4}{14}$ $\frac{7.0}{13}$ $\frac{7.1}{13}$ $\frac{8.1}{16}$ $\frac{8.1}{20}$ $\frac{7.2}{23}$ $\frac{6.1}{52}$ $\frac{3.2}{100}$

$\frac{17.1}{100}$ $\frac{14.3}{61}$ $\frac{7.4}{22}$ $\frac{8.3}{13}$ $\frac{7.8}{14}$ $\frac{7.9}{14}$ $\frac{9.0}{16}$ $\frac{8.9}{21}$ $\frac{7.5}{24}$ $\frac{4.8}{65}$ $\frac{2.1}{100}$

$\frac{16.8}{100}$ $\frac{14.0}{60}$ $\frac{10.9}{19}$ $\frac{9.1}{14}$ $\frac{8.5}{13}$ $\frac{8.7}{13}$ $\frac{9.7}{16}$ $\frac{9.7}{20}$ $\frac{7.6}{24}$ $\frac{5.6}{56}$ $\frac{1.8}{100}$

Sta.	+	π	-	Elev.
29+40		1034.39		27.0

30				25.8
T.P.	6.20	1030.91	9.68	1024.71
+50				25.0

31				24.0
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+50				23.2
T.P.	2.67	1027.38	6.20	1024.71

32				22.4
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+50				22.0
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33				21.7
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+50				21.6
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+ Pipe culvert see Topog for Sta.

34				21.3
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+50				21.2
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Lt.

E

Rt.

16

$$\frac{15.8}{100} \quad \frac{12.8}{59} \quad \frac{9.5}{19} \quad \frac{7.9}{13} \quad \frac{7.4}{14} \quad \frac{7.7}{14} \quad \frac{8.5}{16} \quad \frac{8.4}{20} \quad \frac{5.4}{25} \quad \frac{2.4}{60} \quad \frac{0.0}{80} \quad \frac{+1.5}{100}$$

$$\frac{17.0}{100} \quad \frac{13.6}{57} \quad \frac{11.0}{21} \quad \frac{9.0}{13} \quad \frac{8.6}{14} \quad \frac{8.7}{14} \quad \frac{9.8}{16} \quad \frac{9.7}{21} \quad \frac{7.0}{27} \quad \frac{5.7}{56} \quad \frac{3.2}{100}$$

$$\frac{14.3}{100} \quad \frac{11.2}{54} \quad \frac{8.0}{19} \quad \frac{6.4}{13} \quad \frac{5.5}{14} \quad \frac{6.4}{14} \quad \frac{7.4}{16} \quad \frac{7.4}{21} \quad \frac{5.7}{25} \quad \frac{4.7}{38} \quad \frac{2.2}{100}$$

$$\frac{15.2}{100} \quad \frac{13.0}{56} \quad \frac{11.4}{24} \quad \frac{10.4}{19} \quad \frac{6.9}{12} \quad \frac{6.9}{13} \quad \frac{7.4}{15} \quad \frac{8.3}{20} \quad \frac{8.7}{23} \quad \frac{7.7}{39} \quad \frac{4.8}{59} \quad \frac{0.0}{100}$$

$$\frac{15.3}{100} \quad \frac{14.0}{66} \quad \frac{12.2}{20} \quad \frac{7.9}{12} \quad \frac{7.7}{14} \quad \frac{8.2}{14} \quad \frac{9.7}{18} \quad \frac{8.9}{38} \quad \frac{5.8}{66} \quad \frac{1.6}{100}$$

$$\frac{12.4}{100} \quad \frac{11.7}{66} \quad \frac{10.0}{22} \quad \frac{5.4}{12} \quad \frac{5.0}{13} \quad \frac{5.5}{13} \quad \frac{11.2}{19} \quad \frac{11.1}{32} \quad \frac{4.8}{66} \quad \frac{1.5}{100}$$

$$\frac{13.2}{100} \quad \frac{12.5}{44} \quad \frac{10.9}{22} \quad \frac{5.8}{11} \quad \frac{5.4}{14} \quad \frac{6.0}{14} \quad \frac{8.4}{19} \quad \frac{8.5}{32} \quad \frac{5.7}{64} \quad \frac{1.2}{100}$$

$$\frac{14.3}{100} \quad \frac{13.7}{66} \quad \frac{12.1}{24} \quad \frac{6.0}{13} \quad \frac{5.7}{14} \quad \frac{6.3}{14} \quad \frac{8.2}{18} \quad \frac{9.1}{32} \quad \frac{8.7}{54} \quad \frac{5.1}{100}$$

$$\frac{14.7}{100} \quad \frac{13.9}{51} \quad \frac{12.6}{24} \quad \frac{6.2}{13} \quad \frac{5.8}{14} \quad \frac{6.4}{14} \quad \frac{9.4}{20} \quad \frac{9.6}{33} \quad \frac{8.9}{66} \quad \frac{8.1}{100}$$

$$\frac{12.0}{13.6}$$

$$\frac{12.0}{12.0}$$

$$\frac{15.1}{100} \quad \frac{14.2}{57} \quad \frac{12.8}{31} \quad \frac{12.0}{24} \quad \frac{6.6}{12} \quad \frac{6.1}{14} \quad \frac{6.7}{14} \quad \frac{9.6}{21} \quad \frac{9.7}{30} \quad \frac{9.4}{59} \quad \frac{8.7}{100}$$

$$\frac{14.9}{100} \quad \frac{13.8}{60} \quad \frac{11.8}{22} \quad \frac{6.6}{12} \quad \frac{6.2}{14} \quad \frac{6.8}{14} \quad \frac{8.9}{19} \quad \frac{9.2}{24} \quad \frac{9.2}{34} \quad \frac{9.0}{62} \quad \frac{8.6}{100}$$

Sta.	+	π	-	Elev.
		1027.38		

35				21.3
T.P.	4.67	1027.41	4.64	1022.74
+40				21.4

36				21.3
+42				21.7
+75				22.0

37				21.8
T.P.	4.90	1027.41	4.90	1022.51
+50				22.2

38 - Pipe culvert see top of				22.7
+50				23.3

39				23.9
+34				24.3
+44				24.5

B.M.	4.75	1030.13	2.03	1025.38
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Lt.

E

Rt.

17

13.1	113	95	65	61	67	85	86	82	85	82
100	17	19	13	6	14	18	22	25	66	100

10.0	8.0	6.2	8.2	7.8	6.5	0	6.5	7.6	7.8	5.5	6.4	6.8	7.3
100	86	24	20	14	12	6	13	16	20	25	31	33	100

7.0	4.8	3.5	2.2	6.7	7.3	7.5	6.5	1.6	6.6	7.4	6.7	0.7	1.7	3.2
100	67	37	27	20	18	15	12	6	13	16	20	31	60	100

8.6	6.3	4.6	3.5	6.5	7.0	6.1	5.7	6.1	6.6	6.3	0.0	0.9	0.4	0.3
100	60	31	24	21	13	12	5	13	15	20	31	34	60	100

11.4	10.0	9.0	7.2	7.1	5.8	5.4	6.2	7.0	6.8	4.0	4.0	1.6	1.4
100	60	37	20	15	14	5	13	15	21	25	37	69	100

13.7	12.8	10.9	9.4	5.8	5.6	5.8	7.6	7.8	9.0	6.5	3.1	0.8
100	63	26	20	14	5	13	16	19	22	36	72	100

16.6	16.0	13.8	11.8	5.7	5.2	5.5	10.6	9.5	4.5
100	65	33	23	12	5	13	24	53	100

16.8	16.1	15.5	14.3	5.0	4.7	5.1	12.8	12.8	11.3
100	61	35	30	12	4	13	30	63	100

13.8	13.4	13.1	12.0	4.4	4.1	4.5	12.2	14.2	14.3	13.6
100	69	35	26	12	4	13	26	34	64	100

9.6	9.6	9.4	3.8	3.5	3.9	8.4	11.0	12.4	13.4
100	59	25	13	2	12	21	30	38	100

6.2	6.5	6.6	6.5	3.4	3.1	3.6	6.8	6.4	8.6	10.8
100	65	31	24	14	3	14	21	28	65	100

2.0	2.5	2.7	2.9	3.3	2.9	3.4	3.8	6.5	8.6
100	62	33	24	14	2	14	21	67	100

Spike in Fence Post 200' Lt. 51. 39+44

Sta.	+	Σ	-	Elev.
40		1030.13		25.3
+50				25.5
41				26.2
+50				26.6
42				27.3
T.P. #1	12.17	1041.72	0.58	1029.55
40 + 50				(25.5)
41				(26.2)
+50				(26.6)
42				(27.3)
T.P.	3.04	1032.59	12.17	1029.55
+30				27.6
+66				27.8

Lt.

E

Rt.

18

$\frac{00}{100}$	$\frac{00}{54}$	$\frac{14}{27}$	$\frac{60}{21}$	$\frac{65}{15}$	$\frac{54}{12}$	$\frac{48}{13}$	$\frac{55}{17}$	$\frac{62}{21}$	$\frac{55}{26}$	$\frac{20}{34}$	$\frac{20}{62}$	$\frac{50}{100}$	$\frac{84}{100}$
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$\frac{21}{26}$	$\frac{48}{20}$	$\frac{52}{14}$	$\frac{47}{13}$	$\frac{46}{13}$	$\frac{49}{16}$	$\frac{50}{24}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{40}{19}$	$\frac{43}{12}$	$\frac{39}{14}$	$\frac{45}{18}$	$\frac{40}{23}$	$\frac{32}{29}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{34}{20}$	$\frac{42}{14}$	$\frac{38}{13}$	$\frac{35}{15}$	$\frac{40}{20}$	$\frac{37}{26}$	$\frac{20}{30}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{32}{21}$	$\frac{39}{17}$	$\frac{37}{14}$	$\frac{31}{12}$	$\frac{28}{13}$	$\frac{32}{16}$	$\frac{26}{22}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{85}{100}$	$\frac{65}{57}$	$\frac{64}{39}$	$\frac{63}{32}$	$\frac{16.2}{31}$	$\frac{86}{55}$	$\frac{110}{100}$	$\frac{162}{100}$
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$\frac{70}{100}$	$\frac{44}{56}$	$\frac{37}{41}$	$\frac{32}{39}$	$\frac{34}{34}$	$\frac{15.5}{35}$	$\frac{36}{46}$	$\frac{42}{49}$	$\frac{47}{100}$	$\frac{127}{100}$
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$\frac{51}{100}$	$\frac{32}{58}$	$\frac{25}{42}$	$\frac{20}{35}$	$\frac{15.1}{36}$	$\frac{25}{50}$	$\frac{31}{100}$	$\frac{112}{100}$
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$\frac{65}{100}$	$\frac{61}{61}$	$\frac{68}{42}$	$\frac{65}{34}$	$\frac{14.4}{28}$	$\frac{93}{61}$	$\frac{116}{100}$	$\frac{169}{100}$
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$\frac{13}{100}$	$\frac{42}{53}$	$\frac{53}{32}$	$\frac{49}{23}$	$\frac{60}{21}$	$\frac{61}{15}$	$\frac{53}{12}$	$\frac{50}{12}$	$\frac{51}{12}$	$\frac{60}{16}$	$\frac{61}{20}$	$\frac{63}{24}$	$\frac{94}{33}$	$\frac{113}{59}$	$\frac{129}{100}$
------------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------	-------------------

$\frac{71}{100}$	$\frac{81}{86}$	$\frac{108}{66}$	$\frac{121}{33}$	$\frac{108}{27}$	$\frac{76}{18}$	$\frac{50}{12}$	$\frac{48}{12}$	$\frac{51}{21}$	$\frac{105}{28}$	$\frac{138}{48}$	$\frac{166}{100}$	$\frac{180}{100}$
------------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	-------------------	-------------------

Sta. + π - Elev.

1032.59

43 28.1

Pipe culv. see topog

+45 28.8

44 29.6

+50 30.1

45 31.1

T.P. 8.53 1041.18 +0.06 1032.65

Lt.

E

$$7 \frac{14.0}{27}$$

Rt.

19

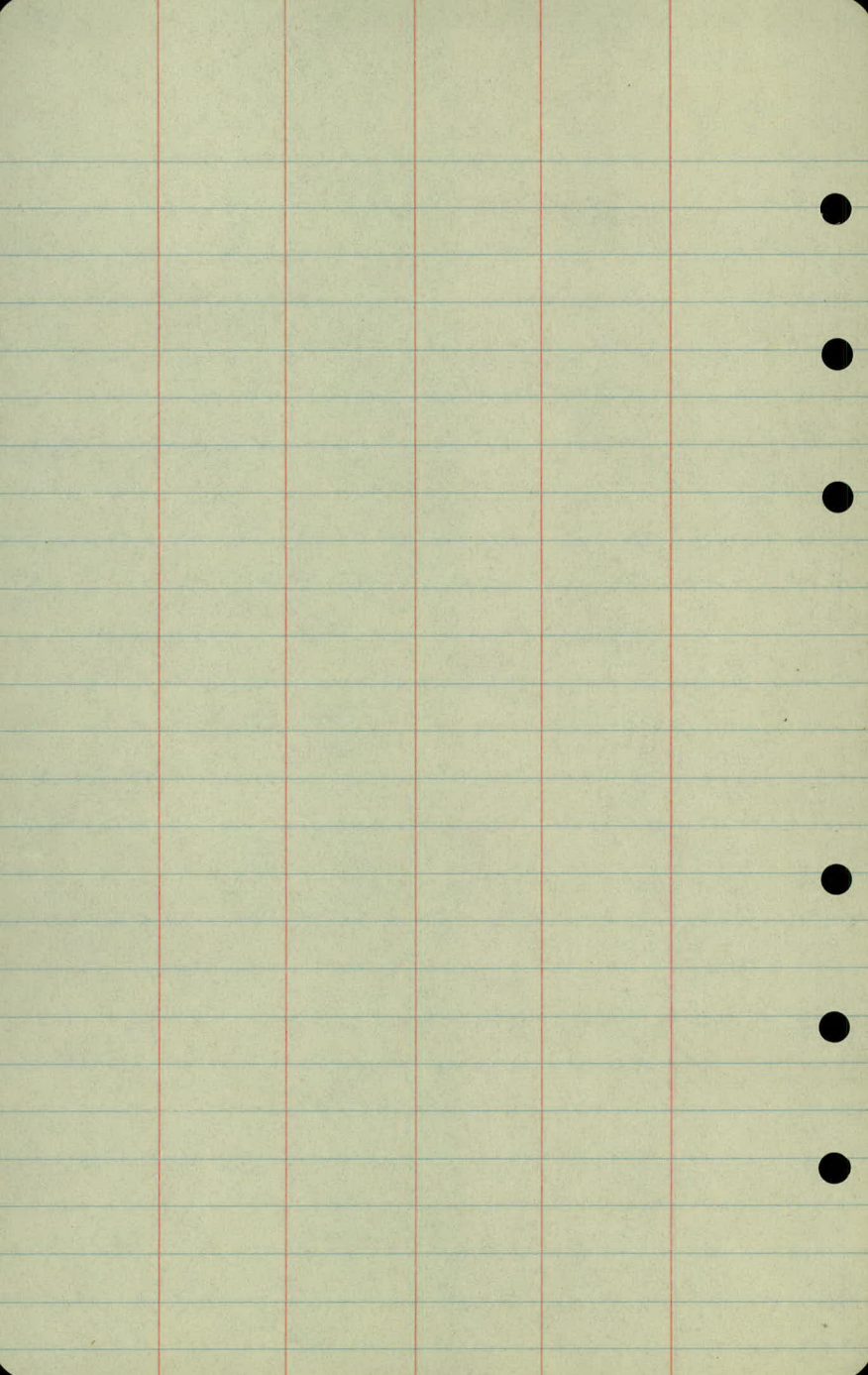
$\frac{108}{100}$	$\frac{138}{55}$	$\frac{142}{35}$	$\frac{150}{30}$	$\frac{118}{23}$	$\frac{49}{12}$	$\frac{45}{12}$	$\frac{48}{12}$	$\frac{40}{27}$	$\frac{16.7}{35}$	$\frac{190}{63}$	$\frac{205}{100}$
		$\frac{144}{15.9}$							$\frac{144}{18.0}$		

$\frac{125}{100}$	$\frac{133}{66}$	$\frac{131}{50}$	$\frac{122}{29}$	$\frac{108}{22}$	$\frac{42}{12}$	$\frac{38}{13}$	$\frac{40}{29}$	$\frac{136}{51}$	$\frac{174}{100}$	$\frac{205}{100}$
-------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	-------------------	-------------------

$\frac{123}{100}$	$\frac{130}{58}$	$\frac{120}{36}$	$\frac{107}{26}$	$\frac{100}{22}$	$\frac{33}{13}$	$\frac{30}{12}$	$\frac{33}{12}$	$\frac{106}{25}$	$\frac{136}{46}$	$\frac{144}{49}$	$\frac{168}{65}$	$\frac{185}{100}$
-------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------	-------------------

$\frac{78}{100}$	$\frac{83}{57}$	$\frac{83}{27}$	$\frac{76}{20}$	$\frac{28}{12}$	$\frac{25}{12}$	$\frac{28}{12}$	$\frac{103}{27}$	$\frac{124}{50}$	$\frac{127}{60}$	$\frac{124}{100}$
------------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-------------------

$\frac{2.8}{100}$	$\frac{2.0}{57}$	$\frac{3.2}{25}$	$\frac{3.7}{19}$	$\frac{2.5}{15}$	$\frac{16}{12}$	$\frac{15}{12}$	$\frac{18}{12}$	$\frac{8.8}{24}$	$\frac{10.4}{27}$	$\frac{10.0}{53}$	$\frac{9.7}{61}$	$\frac{5.6}{92}$	$\frac{5.6}{100}$
-------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	-------------------	-------------------	------------------	------------------	-------------------



Sta.	+	π ✓	-	Elev.
		1041.18		
45 + 60				32.3
46				33.0
+15				33.4
+42				33.9
47				34.7
+50				35.2
48				35.5
+50				35.6
49				35.4
T.P.	3.70	1039.10 ✓	5.78	1035.40 ✓
+50				35.2
50				34.5

Lt.

E

Rt.

21

$$\frac{111}{100} \quad \frac{114}{44} \quad \frac{115}{28} \quad \frac{111}{22} \quad \frac{93}{14} \quad \frac{89}{12} \quad \frac{92}{23} \quad \frac{150}{35} \quad \frac{164}{89} \quad \frac{124}{100} \quad \frac{132}{100}$$

$$\frac{106}{100} \quad \frac{99}{66} \quad \frac{93}{35} \quad \frac{87}{29} \quad \frac{102}{21} \quad \frac{99}{17} \quad \frac{87}{14} \quad \frac{82}{14} \quad \frac{86}{20} \quad \frac{114}{31} \quad \frac{128}{44} \quad \frac{134}{81} \quad \frac{111}{92} \quad \frac{114}{92} \quad \frac{127}{100}$$

$$\frac{90}{100} \quad \frac{74}{57} \quad \frac{70}{29} \quad \frac{73}{26} \quad \frac{82}{24} \quad \frac{95}{20} \quad \frac{93}{16} \quad \frac{85}{14} \quad \frac{78}{14} \quad \frac{81}{17} \quad \frac{96}{21} \quad \frac{99}{26} \quad \frac{95}{45} \quad \frac{107}{73} \quad \frac{98}{91} \quad \frac{103}{100} \quad \frac{111}{100}$$

$$\frac{49}{100} \quad \frac{28}{67} \quad \frac{19}{31} \quad \frac{35}{27} \quad \frac{83}{21} \quad \frac{84}{16} \quad \frac{79}{16} \quad \frac{73}{14} \quad \frac{77}{14} \quad \frac{85}{16} \quad \frac{88}{21} \quad \frac{62}{26} \quad \frac{77}{54} \quad \frac{106}{100}$$

$$\frac{13}{100} \quad \frac{04}{61} \quad \frac{23}{28} \quad \frac{52}{24} \quad \frac{78}{18} \quad \frac{76}{15} \quad \frac{69}{13} \quad \frac{65}{13} \quad \frac{70}{13} \quad \frac{81}{15} \quad \frac{79}{20} \quad \frac{70}{23} \quad \frac{107}{57} \quad \frac{150}{100}$$

$$\frac{38}{100} \quad \frac{20}{56} \quad \frac{22}{28} \quad \frac{43}{24} \quad \frac{70}{20} \quad \frac{73}{16} \quad \frac{66}{13} \quad \frac{60}{13} \quad \frac{65}{13} \quad \frac{71}{15} \quad \frac{74}{20} \quad \frac{59}{22} \quad \frac{92}{55} \quad \frac{156}{100}$$

$$\frac{26}{100} \quad \frac{19}{53} \quad \frac{28}{28} \quad \frac{35}{24} \quad \frac{75}{17} \quad \frac{62}{13} \quad \frac{57}{13} \quad \frac{61}{13} \quad \frac{71}{16} \quad \frac{68}{21} \quad \frac{48}{24} \quad \frac{81}{54} \quad \frac{136}{100}$$

$$\frac{51}{100} \quad \frac{50}{62} \quad \frac{47}{30} \quad \frac{48}{24} \quad \frac{74}{19} \quad \frac{70}{15} \quad \frac{62}{13} \quad \frac{56}{14} \quad \frac{60}{14} \quad \frac{70}{16} \quad \frac{71}{19} \quad \frac{58}{21} \quad \frac{91}{54} \quad \frac{147}{100}$$

$$\frac{73}{100} \quad \frac{62}{56} \quad \frac{53}{23} \quad \frac{68}{20} \quad \frac{65}{15} \quad \frac{59}{13} \quad \frac{58}{13} \quad \frac{63}{13} \quad \frac{72}{16} \quad \frac{73}{19} \quad \frac{60}{22} \quad \frac{72}{34} \quad \frac{77}{53} \quad \frac{125}{100}$$

$$\frac{61}{100} \quad \frac{47}{55} \quad \frac{30}{23} \quad \frac{56}{17} \quad \frac{46}{14} \quad \frac{39}{14} \quad \frac{44}{13} \quad \frac{51}{15} \quad \frac{53}{19} \quad \frac{33}{23} \quad \frac{47}{49} \quad \frac{88}{100}$$

$$\frac{75}{100} \quad \frac{65}{73} \quad \frac{29}{39} \quad \frac{16}{27} \quad \frac{61}{19} \quad \frac{61}{16} \quad \frac{54}{14} \quad \frac{46}{14} \quad \frac{53}{14} \quad \frac{61}{17} \quad \frac{60}{20} \quad \frac{39}{23} \quad \frac{57}{55} \quad \frac{76}{100}$$

Sta.	+	K	-	Elev.
		1039.10		
50+50				33.6
51				32.2
+50				31.0
52				29.4
+27				28.6
+38				28.3
+45				28.0
+59.56				27.6
B.M.			11.49	1027.61

Lt.

E

Rt.

$\frac{9.0}{100}$ $\frac{6.9}{63}$ $\frac{5.2}{28}$ $\frac{5.3}{23}$ $\frac{7.6}{19}$ $\frac{7.1}{15}$ $\frac{6.3}{13}$ $\frac{5.5}{/}$ $\frac{6.2}{14}$ $\frac{7.1}{16}$ $\frac{7.0}{20}$ $\frac{4.0}{25}$ $\frac{4.2}{29}$ $\frac{4.0}{66}$ $\frac{4.4}{100}$

$\frac{11.1}{100}$ $\frac{10.0}{75}$ $\frac{6.5}{37}$ $\frac{5.5}{26}$ $\frac{8.4}{19}$ $\frac{8.3}{16}$ $\frac{7.6}{14}$ $\frac{6.9}{/}$ $\frac{7.4}{14}$ $\frac{8.2}{16}$ $\frac{7.7}{21}$ $\frac{3.4}{27}$ $\frac{2.4}{59}$ $\frac{2.7}{82}$ $\frac{4.4}{100}$

$\frac{9.1}{100}$ $\frac{6.1}{46}$ $\frac{4.9}{27}$ $\frac{5.6}{21}$ $\frac{9.7}{16}$ $\frac{8.8}{14}$ $\frac{8.1}{/}$ $\frac{8.6}{14}$ $\frac{9.5}{16}$ $\frac{9.5}{20}$ $\frac{6.0}{26}$ $\frac{6.4}{29}$ $\frac{6.1}{66}$ $\frac{6.0}{100}$

$\frac{11.7}{100}$ $\frac{10.7}{82}$ $\frac{8.3}{47}$ $\frac{7.7}{37}$ $\frac{7.7}{25}$ $\frac{11.0}{21}$ $\frac{11.2}{17}$ $\frac{10.1}{14}$ $\frac{9.7}{/}$ $\frac{10.0}{14}$ $\frac{11.0}{16}$ $\frac{10.9}{21}$ $\frac{8.6}{25}$ $\frac{9.0}{29}$ $\frac{9.6}{55}$ $\frac{10.5}{100}$

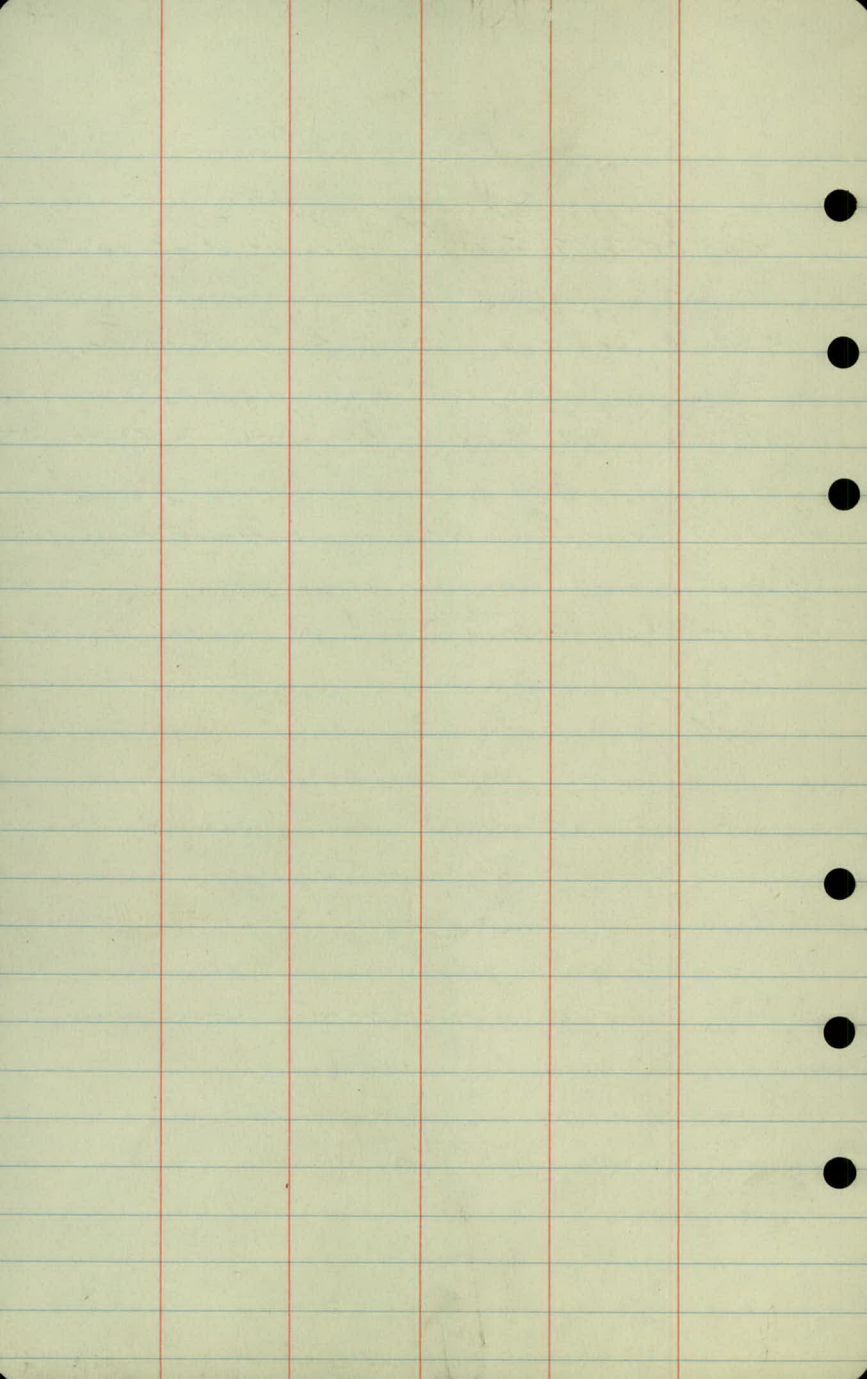
$\frac{15.4}{100}$ $\frac{14.3}{87}$ $\frac{9.2}{60}$ $\frac{8.8}{35}$ $\frac{9.4}{27}$ $\frac{12.0}{22}$ $\frac{12.2}{20}$ $\frac{11.1}{16}$ $\frac{10.5}{/}$ $\frac{10.7}{15}$ $\frac{11.0}{21}$ $\frac{9.1}{24}$ $\frac{10.0}{36}$ $\frac{11.0}{62}$ $\frac{11.8}{100}$

$\frac{16.5}{100}$ $\frac{15.2}{72}$ $\frac{12.9}{25}$ $\frac{11.8}{23}$ $\frac{10.8}{/}$ $\frac{11.1}{23}$ $\frac{12.9}{25}$ $\frac{12.8}{55}$ $\frac{12.6}{100}$

$\frac{14.3}{100}$ $\frac{12.8}{57}$ $\frac{12.1}{28}$ $\frac{11.1}{/}$ $\frac{11.2}{31}$ $\frac{11.1}{63}$ $\frac{11.1}{100}$

$\frac{14.3}{100}$ $\frac{13.1}{60}$ $\frac{11.5}{/}$ $\frac{11.2}{50}$ $\frac{10.9}{100}$

Top of Stone Monument Bellevue & E.



Bellaire Ave. D to E.

Slope stakes at culvert
locations

2/2/38

Sta.	+	K	-	Grade
B.M.	3.34	1027.69		1024.35

2+00			225	5.7
------	--	--	-----	-----

B.M.	2.90	1024.01		1019.11
------	------	---------	--	---------

15+50			17.5	4.8
-------	--	--	------	-----

Sta. 33+00	1.5	1023.4		1021.7
------------	-----	--------	--	--------

33+74			21.1	2.1
-------	--	--	------	-----

Lt.

L

Rt.

$$\begin{array}{r} 9.5 \\ F. 4.3 \\ \hline 33.2 \end{array}$$

$$\begin{array}{r} 8.2 \\ F. 3.0 \\ \hline 28.0 \end{array}$$

Plan Extension

10' Rt. - O.K.

12' Lt. - O.K.

Appears no relaying of culvert is
necessary

$$\begin{array}{r} 5.2 \\ F. 3.4 \\ \hline 29.6 \end{array}$$

$$\begin{array}{r} 9.4 \\ F. 4.6 \\ \hline 34.4 \end{array}$$

Plan extension

10' Lt. - O.K.

12' Rt. - O.K.

Appears no relaying of culvert
is necessary.

$$\begin{array}{r} 10.0 \\ F. 2.5 \\ \hline 47.6 \end{array}$$

$$\begin{array}{r} 6.4 \\ F. 4.3 \\ \hline 33.2 \end{array}$$

Plan Extension

22' Lt. - O.K.

8' Rt. - 10' would be better

Packed snow 4' deep but do not think
pipe needs to be relined

Sta.	+	π	-	Grade.
Sta. 38	0.70	1023.4		1022.7

38+03			22.5	0.9
-------	--	--	------	-----

Sta. 44+00	1.60	1028.90		1027.3
------------	------	---------	--	--------

43+00			28.0	0.9
-------	--	--	------	-----

Lt.LRt.

$$\begin{array}{r} 11.9 \\ \hline 11.0 \\ 60 \end{array}$$

$$\begin{array}{r} 9.3 \\ \hline 18.4 \\ 49.6 \end{array}$$

Plan Extension

30' Lt. - O.K.

20' Rt. - Believe 22' would be better.

As near as we can tell with 4' of
snow packed in here no relay is necessary

$$\begin{array}{r} 10.1 \\ \hline 19.2 \\ 52.8 \end{array}$$

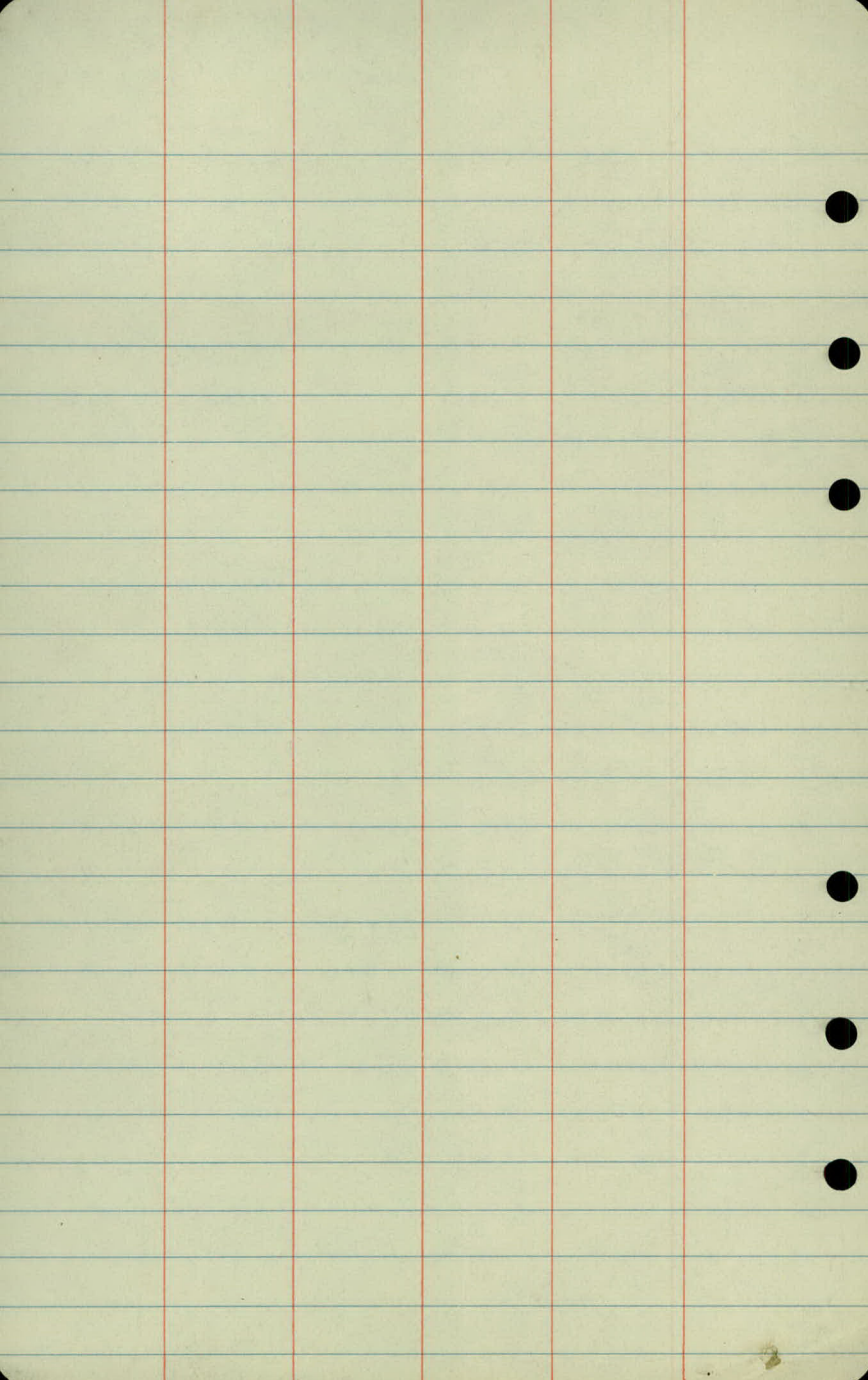
$$\begin{array}{r} 15.7 \\ \hline 14.8 \\ 75.2 \end{array}$$

Plan Extension:-

24' Lt. - O.K.

40' Rt. - O.K.

Same note as above.



Adjust Sta 43+00

24' L+ }
40' R+ } 62'

13.68
11.96
1.72
124
480
434
460

.0277
62
1662
17174

.0277
24
1108
154
6648

.0277
40
11080

5.6 ✓
7.9 ✓
5.6 ✓
2.1 ✓
1.6 ✓
5 break in grade

5.6 ✓
1.11 ✓
6.76 ✓
6.12 ✓
64

Calc Sta 38+03

30' Lt. }
22' Rt. } 56'

Pitch $\frac{13.6}{12.9} = 1.05$

12.7
11.5
1.2

125
16) 70
16
140
112
280
280

.0125 per foot
56
700
625
7000

.0125
56
700
250
2750 RT.

.0125
30
3750 Lt

6.22
93
1.8
91.8

1.8
4.0
1.2

5.4
4
5.8

One

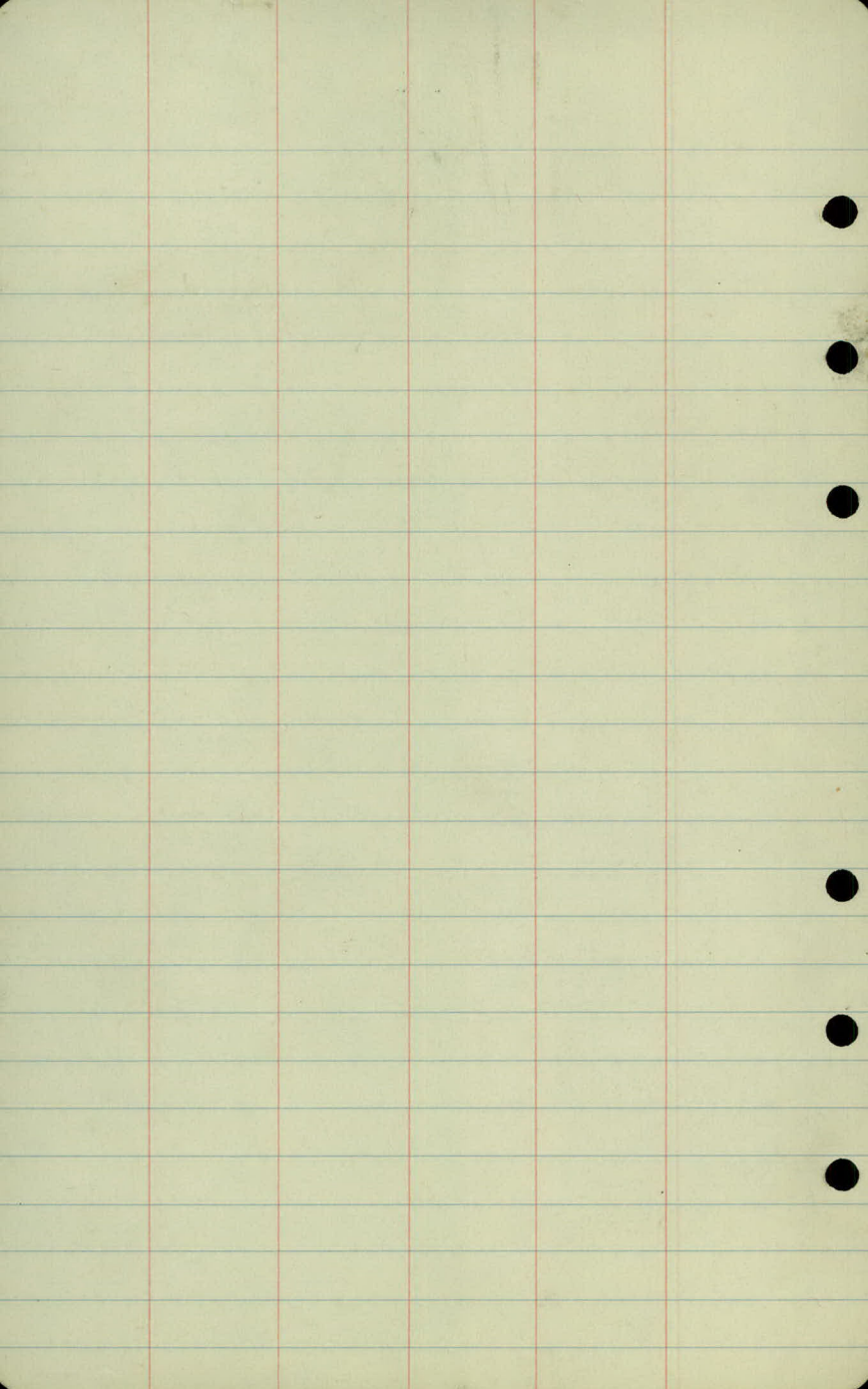
Calc. $33 + 74$

$$\begin{array}{r}
 6.17 \\
 8.17 \\
 \hline
 14.34
 \end{array}$$

$$\begin{array}{r} 0377 \\ \times 448 \\ \hline 1408 \\ 1408 \\ \hline 15488 \\ + 15488 \\ \hline 169472 \end{array}$$

$$\begin{array}{r} 638 \\ 20 \\ \hline 760 \end{array}$$

9.8³
9.8³
10.



Bellaire Ave.

Slope stakes "D" to "E" as
per plan dated Jan 1938.

32' Crown

25' to Ditch Slope.

4 to 1 Slopes Cut & Fill.
1.5' Ditch

Special Section

0+75 to 1+25 Lt.

3+50 to 5+75 Lt.

3+00 to 5+25 Rt.

9+00 to 12+75 Lt.

10+50 to 11+75 Rt.

16+40 to 20+25 Lt.)

33' Limit

Variable back slope

Sta.	+	π	-	Grade.
B.M.	3.53	1027.88		1024.35

0+00				24.5
------	--	--	--	------

+18				24.3
-----	--	--	--	------

+33				24.2
-----	--	--	--	------

+60				23.9
-----	--	--	--	------

1				23.5
---	--	--	--	------

+50				23.0
-----	--	--	--	------

2				22.5
---	--	--	--	------

+50				22.0
-----	--	--	--	------

Lt.

E

Rt.

21

Top of Monument Bellaire & D.

$$\begin{array}{r} 3.4 \\ 4.9 \end{array}$$

$$\begin{array}{r} 3.6 \\ 5.1 \end{array}$$

$$\begin{array}{r} 2.7 \\ 5.2 \end{array}$$

$$\frac{20 \text{ Meters}}{\text{Radius}}$$

$$\frac{3.5}{/}$$

$$\frac{2.9}{0.23} \\ 33$$

$$\begin{array}{r} 4.0 \\ 5.5 \end{array}$$

$$\frac{2.9}{F.39} \\ 31.6$$

$$\frac{4.1}{/}$$

$$\frac{4.6}{0.09} \\ 286$$

$$\begin{array}{r} 4.4 \\ 5.9 \end{array}$$

$$\frac{9.7}{F.53} \\ 33$$

$$\frac{4.6}{/}$$

$$\frac{7.2}{F.28} \\ 27.2$$

$$\begin{array}{r} 4.9 \\ 6.4 \end{array}$$

$$\frac{9.7}{F.48} \\ 93$$

$$\frac{5.0}{/}$$

$$\frac{8.2}{F.33} \\ 29.2$$

$$\begin{array}{r} 5.4 \\ 6.9 \end{array}$$

$$\frac{9.1}{F.41} \\ 93$$

$$\frac{5.3}{F.30} \\ 28.0$$

$$\begin{array}{r} 5.9 \\ 7.4 \end{array}$$

$$\frac{9.7}{F.38} \\ 31.2$$

$$\frac{5.7}{/}$$

$$\frac{7.7}{F.18} \\ 23.2$$

Sta. + π - Grade.

1027.88

3+00

21.5

+40

21.1

4

20.5

+50

20.0

5

19.5

T.P.

3.66

1023.43

8.11

1019.77

+50

19.0

6

18.7

+50

18.3

LT

Q

RT

6.4
7.9

8.7
F.2.3
21.2

5.9

6.0
DC 1.9
32.6

6.8
8.3

6.9
DC 1.4
30.6

6.4

5.1
DC 3.2
33

7.4
8.9

4.1
DC 4.8
33

7.1

4.3
DC 4.6
33

7.8
7.4

4.2
DC 1.2
33

7.7

5.4
DC 4.0
33

8.4
9.9

6.0
DC 3.9
33

8.2

2.5
DC 2.4
33

Req St2.5

1.5
4.4
5.9

2.9
DC 3.0
33.0

4.0

4.4
DC 1.5
31.0

1.5
4.7
6.2

4.4
DC 1.3
30.2

4.4

5.3
DC 0.5
27.0

5.1
6.6

6.6
DC 0.0
21.0

4.4

6.5
DC 0.1
25.4

St. + π - Grade.

1023.43

7+00

18.1

+50

17.9

8

17.9

+50

17.8

9

17.8

+50

17.7

B.M.

7.93

1027.04

4.37

1019.11

OK

10

17.7

+50

17.6

LT.

E

RT.

4

5.3
6.8

7.7
F.2.4
25.6

5.0

7.1
F.1.8
23.2

5.5
7.0

8.5
F.3.0
28.0

5.2

7.4
F.1.9
23.6

5.5
7.0

8.3
F.2.8
25.2

5.3

7.2
F.1.7
22.8

5.6
7.1

7.7
F.2.1
24.4

5.4

7.3
F.1.7
22.8

5.6
7.1

8.1
D.C.2.0
33

5.4

6.6
D.C.0.5
27.0

5.7
7.2

3.1
D.C.4.1
33.0

5.4

6.2
D.C.1.0
29.0

5.3
10.8

5.1
D.C.1.7
33

9.0

9.4
D.C.1.4
30.6

5.4
10.9

2.8
D.C.8.1
33

9.1

9.0
D.C.1.9
32.6

Sta.	+	x	-	Grade.
------	---	---	---	--------

1027.04

11

17.6

+50

17.5

12

17.5

+50

17.4

13

17.4

+50

17.3

B.M. 1315 R

1019.11

14

17.3

+50

17.2

Lt.

Z

Ch.

51

$$\begin{array}{r} 1.5 \\ 9.4 \\ 10.9 \end{array}$$

$$\begin{array}{r} 2.2 \\ 108.7 \\ 33 \end{array}$$

$$\frac{93}{/}$$

$$\begin{array}{r} 8.7 \\ 102.2 \\ 33 \end{array}$$

$$\begin{array}{r} 1.5 \\ 9.5 \\ 11.0 \end{array}$$

$$\begin{array}{r} 1.8 \\ 9.2 \\ 33 \end{array}$$

$$\frac{94}{/}$$

$$\begin{array}{r} 8.7 \\ 102.3 \\ 33 \end{array}$$

$$\begin{array}{r} 1.5 \\ 9.5 \\ 11.0 \end{array}$$

$$\begin{array}{r} 3.5 \\ 107.5 \\ 33 \end{array}$$

$$\frac{95}{/}$$

$$\begin{array}{r} 9.1 \\ 106.1 \\ 29.4 \end{array}$$

$$\begin{array}{r} 1.5 \\ 9.6 \\ 11.1 \end{array}$$

$$\begin{array}{r} 6.7 \\ 4.4 \\ 33 \end{array}$$

$$\frac{98}{/}$$

$$\begin{array}{r} 10.8 \\ 100.3 \\ 26.2 \end{array}$$

$$\begin{array}{r} 9.6 \\ 11.1 \end{array}$$

$$\begin{array}{r} 10.3 \\ 109.8 \\ 28.2 \end{array}$$

$$\begin{array}{r} 11.5 \\ 11.9 \\ 23.6 \end{array}$$

$$\begin{array}{r} 9.7 \\ 11.2 \end{array}$$

$$\begin{array}{r} 12.1 \\ 12.4 \\ 21.6 \end{array}$$

$$\frac{97}{/}$$

$$\begin{array}{r} 11.8 \\ 12.1 \\ 24.4 \end{array}$$

$$\begin{array}{r} 9.7 \\ 11.2 \end{array}$$

$$\begin{array}{r} 12.9 \\ 13.2 \\ 25.8 \end{array}$$

$$\frac{10.0}{/}$$

$$\begin{array}{r} 12.5 \\ 12.8 \\ 27.2 \end{array}$$

$$\begin{array}{r} 9.8 \\ 11.3 \end{array}$$

$$\begin{array}{r} 13.4 \\ 13.6 \\ 30.4 \end{array}$$

$$\frac{10.1}{/}$$

$$\begin{array}{r} 12.9 \\ 13.1 \\ 28.4 \end{array}$$

Sta. + K - Grade.

1027.04

15

17.2

+50

17.2

16

17.5

T.P.

4.53

1044.00

9.57

1017.47

+50

17.9

17

18.6

+50

18.4

18

20.5

+50

21.7

4.

2

24

6

8.8
11.3

133
F.3.5
20.0

10.1

14.5
F.4.7
34.8

9.8
11.3

13.2
F.3.4
29.6

14.6
F.4.6
34.4

9.5
11.0

12.2
F.2.7
26.8

9.6

14.8
F.4.4
37.6

Red Sta. 16

4.1
5.6

4.7
F.0.9
28.6

4.1

9.5
F.1.4
37.6

3.4

3.4

8.2
F.4.8
35.2

2.6

7.6
F.1.0
36.0

1.5

7.3
F.1.8
39.2

0.7

5.5
F.1.2
36.8

Sta. + π - Grade.

1024.00

19

23.2

+50

24.7

20

26.3

+50

27.8

21

29.4

+50

30.9

T.P.

4.53

1017.47

1037.37

22

32.5

37.37
2.96

34.41
34.37

39.78

+50

33.8

T.P.

5.37

1039.78

2.96

1034.41

LT.

2

RT.

7

+1.2

2.7
F.39
31.6

+2.1

2.7
F.5.2
36.8

+4.3

For LT.

7.1
F.11.4
61.6

see pg 18

+5.8

8.6
F.14.4
73.6

+7.4

2.7
F.15.1
76.4

+8.9

2.7
F.11.6
62.4

Rec'd Sta 16 + 00

See pg. 18.

4.4
6.4

4.0
DC 2.4
33.0

4.3

4.6
DC 1.8
32.2

3.6
8.1

3.7
DC 1.4
30.6

3.2

3.8
DC 2.3
34.2

Sto. + K - Grade.

1039.78

23

34.7

+50

35.3

24

35.4

+50

35.1

25

1039.75
7.03
1032.72
4.13
1036.90

34.4

+50

33.5

B.M.

4.13

1036.90

203

1037.77

26

32.6

OK

+50

31.7

26+31.85
B.M. Mount.
1037.77

L.A.

E

R.A.

8

$$\begin{array}{r} 5.1 \\ 6.6 \end{array}$$

$$\begin{array}{r} 5.0 \\ DC 1.6 \\ \hline 31.4 \end{array}$$

$$\frac{48}{\hline}$$

$$\begin{array}{r} 47 \\ DC 1.9 \\ \hline 32.6 \end{array}$$

$$\begin{array}{r} 4.5 \\ 6.0 \end{array}$$

$$\begin{array}{r} 3.9 \\ DC 2.1 \\ \hline 33.0 \end{array}$$

$$\frac{41}{\hline}$$

$$\begin{array}{r} 38 \\ DC 2.2 \\ \hline 33.8 \end{array}$$

$$\begin{array}{r} 4.4 \\ 5.9 \end{array}$$

$$\begin{array}{r} 5.4 \\ DC 0.5 \\ \hline 27.0 \end{array}$$

$$\frac{41}{\hline}$$

$$\begin{array}{r} 47 \\ DC 1.2 \\ \hline 29.8 \end{array}$$

$$\begin{array}{r} 4.7 \\ 6.2 \end{array}$$

$$\begin{array}{r} 8.2 \\ F 3.5 \\ \hline 30.0 \end{array}$$

$$\frac{43}{\hline}$$

$$\begin{array}{r} 5.9 \\ DC 0.3 \\ \hline 26.2 \end{array}$$

$$\begin{array}{r} 5.4 \\ 6.9 \end{array}$$

$$\begin{array}{r} 9.8 \\ F 4.4 \\ \hline 33.0 \end{array}$$

$$\frac{50}{\hline}$$

$$\begin{array}{r} 6.2 \\ DC 0.7 \\ \hline 27.9 \end{array}$$

$$\begin{array}{r} 6.3 \\ 7.8 \end{array}$$

$$\begin{array}{r} 9.9 \\ F 3.6 \\ \hline 30.4 \end{array}$$

$$5.5$$

$$\begin{array}{r} 5.7 \\ DC 2.1 \\ \hline 33.4 \end{array}$$

$$\begin{array}{r} 4.3 \\ 5.8 \end{array}$$

$$\begin{array}{r} 7.1 \\ F 2.8 \\ \hline 27.2 \end{array}$$

$$3.3$$

$$\begin{array}{r} 3.8 \\ DC 2.0 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 5.2 \\ 6.7 \end{array}$$

$$\begin{array}{r} 8.6 \\ F 3.6 \\ \hline 29.6 \end{array}$$

$$4.3$$

$$\begin{array}{r} 3.8 \\ DC 2.9 \\ \hline 36.6 \end{array}$$

Sta. + x - Grade.

1036.90

27

30.8

+50

29.9

28

29.0

+50

28.1

29

27.2

+40

26.5

Check OK on Sta 30

T.P.

5.80

1030.51

1024.71

30

25.4

+50

24.5

Lt.

E

Rt.

9

$$\begin{array}{r} 6.1 \\ 7.6 \end{array}$$

$$\begin{array}{r} 9.7 \\ F3.6 \\ \hline 30.4 \end{array}$$

5.4

$$\begin{array}{r} 2.2 \\ DC5.4 \\ \hline 46.6 \end{array}$$

$$\begin{array}{r} 7.0 \\ 8.5 \end{array}$$

$$\begin{array}{r} 11.2 \\ F4.2 \\ \hline 32.8 \end{array}$$

6.5

$$\begin{array}{r} 6.5 \\ DC2.0 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 7.9 \\ 9.4 \end{array}$$

$$\begin{array}{r} 13.8 \\ F5.8 \\ \hline 39.6 \end{array}$$

7.7

$$\begin{array}{r} 7.8 \\ DC1.6 \\ \hline 31.4 \end{array}$$

$$\begin{array}{r} 8.8 \\ 10.3 \end{array}$$

$$\begin{array}{r} 13.5 \\ F4.7 \\ \hline 34.8 \end{array}$$

8.5

$$\begin{array}{r} 7.8 \\ DC2.5 \\ \hline 35.0 \end{array}$$

$$\begin{array}{r} 9.7 \\ 11.2 \end{array}$$

$$\begin{array}{r} 12.0 \\ F2.3 \\ \hline 25.2 \end{array}$$

7.3

$$\begin{array}{r} 7.5 \\ DC3.7 \\ \hline 39.8 \end{array}$$

$$\begin{array}{r} 10.4 \\ 11.9 \end{array}$$

$$\begin{array}{r} 12.2 \\ F1.8 \\ \hline 23.2 \end{array}$$

9.9

$$\begin{array}{r} 5.7 \\ DC6.2 \\ \hline 49.8 \end{array}$$

See Bench Levels

$$\begin{array}{r} 8.1 \\ 6.6 \end{array}$$

$$\begin{array}{r} 25 \\ F2.4 \\ \hline 35.6 \end{array}$$

4.3

$$\begin{array}{r} 27 \\ DC3.9 \\ \hline 40.6 \end{array}$$

$$\begin{array}{r} 6.0 \\ 7.5 \end{array}$$

$$\begin{array}{r} 8.6 \\ F2.6 \\ \hline 26.4 \end{array}$$

6.6

$$\begin{array}{r} 5.2 \\ DC2.3 \\ \hline 34.2 \end{array}$$

Sta. + K - Grade.

1030.51

31

22.6

+50

22.8

32

22.1

T.P.

3.77

1046.27

8.01

1027.50

+50

21.6

33

21.3

+50

21.1

34

21.1

+50

21.1

Lt.

E

Rt.

10

6.9
8.4
$$\begin{array}{r} 11.5 \\ F46 \\ \hline 34.4 \end{array}$$

6.5

$$\begin{array}{r} 6.8 \\ DC1.6 \\ \hline 31.4 \end{array}$$
1.5
7.7
9.2
$$\begin{array}{r} 12.3 \\ F46 \\ \hline 34.4 \end{array}$$

7.3

$$\begin{array}{r} 9.0 \\ DC0.2 \\ \hline 21.8 \end{array}$$
1.5
8.4
9.9
$$\begin{array}{r} 13.9 \\ F5.5 \\ \hline 38.0 \end{array}$$

8.1

$$\begin{array}{r} 10.4 \\ F2.0 \\ \hline 24.0 \end{array}$$
4.7
6.5
$$\begin{array}{r} 11.1 \\ F6.4 \\ \hline 41.6 \end{array}$$

4.3

$$\begin{array}{r} 7.2 \\ F2.5 \\ \hline 26.0 \end{array}$$

5.0

$$\begin{array}{r} 12.1 \\ F2.0 \\ \hline 44.4 \end{array}$$

4.6

$$\begin{array}{r} 8.0 \\ F3.0 \\ \hline 28.0 \end{array}$$

5.2

$$\begin{array}{r} 12.5 \\ F2.3 \\ \hline 45.1 \end{array}$$

4.7

$$\begin{array}{r} 8.5 \\ F3.3 \\ \hline 29.2 \end{array}$$

5.2

$$\begin{array}{r} 12.1 \\ F2.3 \\ \hline 45.2 \end{array}$$

5.0

$$\begin{array}{r} 8.4 \\ F3.2 \\ \hline 28.8 \end{array}$$

5.2

$$\begin{array}{r} 12.0 \\ F6.8 \\ \hline 45.2 \end{array}$$

5.1

$$\begin{array}{r} 8.1 \\ F2.9 \\ \hline 27.6 \end{array}$$

Sta. + π - Grade.

1026.27

35

21.2

+40

T.P.

7.71

1030.20

3.78

21.2

St. to bench level
1022.49

36

21.3

+42

21.3

+75

BM

4.80

21.5

1025.40

37

0.40

1025.78

21.6

1025.38

+50

22.0

38

22.5

27

3

27

11

5.1

5.6
F. 3.7
30.8

5.0

7.2
F. 2.1
24.4

5.1
6.6

5.3
D.C. 1.3
30.7

4.9

5.3
D.C. 1.3
30.2

5.9
10.4

6.4
D.C. 4.0
41.0

8.9

4.2
D.C. 6.2
49.8

8.9
10.4

7.6
D.C. 2.9
36.7

8.5

3.1
D.C. 7.3
14.2

5.7
10.2

10.2
D.C. 0.0
42.1

8.3

6.7
D.C. 3.5
35.0

B.M. 1025.35

4.2
5.7

10.1
F. 5.9
39.6

4.8
D.C. 0.8
28.2

3.8
5.3

14.2
F. 10.4
57.6

9.2
F. 4.4
32.6

3.3
4.8

14.1
F. 10.8
54.2

11.7
F. 8.4
49.6

Sta.	+	X	-	Grade.
		1025.78		
38+50				23.0
39				23.6
+34				23.9
+44				24.0
T.P.	1267	1038.05	0.40	1025.38
40				24.7
+50				25.2
T.P.	5.81	1041.63	2.23	1035.82
41				25.8
+50				26.3

200' Lt. BM.
 1025.38

Lt.

E

Rt.

12

2.8

$$\begin{array}{r} 116 \\ F88 \\ \hline 51.2 \end{array}$$

$$\begin{array}{r} 126 \\ F88 \\ \hline 15.2 \end{array}$$

2.2

$$\begin{array}{r} 80 \\ F18 \\ \hline 39.2 \end{array}$$

$$\begin{array}{r} 108 \\ F86 \\ \hline 104 \end{array}$$

1.9

$$\begin{array}{r} 4.2 \\ F23 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} 46 \\ F27 \\ \hline 26.8 \end{array}$$

1.8
3.3

$$\begin{array}{r} 20 \\ DC13 \\ \hline 30.2 \end{array}$$

$$\begin{array}{r} 24 \\ DC09 \\ \hline 28.6 \end{array}$$

13.4
14.9

$$\begin{array}{r} 76 \\ DC73 \\ \hline 14.2 \end{array}$$

$$\begin{array}{r} 108 \\ DC41 \\ \hline 41.4 \end{array}$$

12.9
14.4

$$\begin{array}{r} 34 \\ DC110 \\ \hline 69.0 \end{array}$$

$$\begin{array}{r} 72 \\ DC72 \\ \hline 13.8 \end{array}$$

15.8
17.3

$$\begin{array}{r} 56 \\ DC117 \\ \hline 71.8 \end{array}$$

$$\begin{array}{r} 74 \\ DC99 \\ \hline 64.6 \end{array}$$

15.3
16.8

$$\begin{array}{r} 44 \\ DC124 \\ \hline 74.6 \end{array}$$

$$\begin{array}{r} 62 \\ DC86 \\ \hline 67.4 \end{array}$$

Sto.	+	π	-	Grade.
		1041.63		
42				26.9
T.P.	0.20	1029.72	12.11	1029.52
+20				27.2
T.P.	4.97	1025.34	9.35	1020.37
+66				27.6
43				28.0
+45				28.5
44				29.2
+50				30.0
45				30.9
T.P.	11.84	1035.54	1.64	1023.70

Lt.

E

Rt.

13

$$\begin{array}{r} 14.7 \\ 16.2 \end{array}$$

$$\begin{array}{r} 6.1 \\ DC 10.1 \\ \hline 65.4 \end{array}$$

$$\begin{array}{r} 10.1 \\ DC 5.7 \\ \hline 47.8 \end{array}$$

$$\begin{array}{r} 2.1 \\ 4.0 \end{array}$$

$$\begin{array}{r} 2.6 \\ DC 1.4 \\ \hline 30.6 \end{array}$$

+ 2.3

$$\begin{array}{r} 10.3 \\ F. 17.6 \\ \hline 66.4 \end{array}$$

+ 2.7

$$\begin{array}{r} 12.1 \\ F. 14.8 \\ \hline 75.2 \end{array}$$

+ 3.2

$$\begin{array}{r} 12.9 \\ F. 16.1 \\ \hline 80.4 \end{array}$$

+ 3.9

$$\begin{array}{r} 11.4 \\ F. 14.3 \\ \hline 77.2 \end{array}$$

+ 4.7

$$\begin{array}{r} 5.8 \\ F. 10.1 \\ \hline 58.0 \end{array}$$

+ 5.6

$$\begin{array}{r} 2.8 \\ F. 8.4 \\ \hline 49.6 \end{array}$$

Sta. + x - Grade.

1035.54

45+60

31.9

46

32.7

+15

32.9

+42

33.4

B.M.

9.48

1042.13

2.90

1032.64

1032.65

47

34.3

+50

34.9

1035.39
5.02
1040.41

48

35.2

+50

35.2

T.P.

5.02

1040.41

6.74

1035.39

Lt.

E

Rt.

14

3.6

$$\begin{array}{r} 10.0 \\ F 7.0 \\ \hline 44.0 \end{array}$$

1.5

$$\begin{array}{r} 2.8 \\ 4.3 \end{array}$$

$$\begin{array}{r} 7.2 \\ F 4.4 \\ \hline 33.6 \end{array}$$

1.5

$$\begin{array}{r} 2.6 \\ 4.1 \end{array}$$

$$\begin{array}{r} 3.8 \\ D 0.3 \\ \hline 26.2 \end{array}$$

1.5

$$\begin{array}{r} 3.1 \\ 3.6 \end{array}$$

$$\begin{array}{r} 1.1 \\ D 0.2.5 \\ \hline 35.0 \end{array}$$

1.5

$$\begin{array}{r} 7.8 \\ 9.3 \end{array}$$

$$\begin{array}{r} 1.5 \\ D 6.78 \\ \hline 76.2 \end{array}$$

$$\begin{array}{r} 8.6 \\ D 0.0.7 \\ \hline 27.8 \end{array}$$

1.5

$$\begin{array}{r} 7.2 \\ 8.7 \end{array}$$

$$\begin{array}{r} 2.8 \\ D 6.59 \\ \hline 48.6 \end{array}$$

$$\begin{array}{r} 7.7 \\ D 0.1.0 \\ \hline 29.0 \end{array}$$

1.5

$$\begin{array}{r} 6.9 \\ 8.4 \end{array}$$

$$\begin{array}{r} 3.0 \\ D 6.54 \\ \hline 46.6 \end{array}$$

$$\begin{array}{r} 6.7 \\ D 0.1.7 \\ \hline 31.8 \end{array}$$

1.5

$$\begin{array}{r} 6.9 \\ 8.4 \end{array}$$

$$\begin{array}{r} 5.9 \\ D 0.2.5 \\ \hline 35.0 \end{array}$$

$$\begin{array}{r} 7.5 \\ D 0.0.9 \\ \hline 28.6 \end{array}$$

Red 575 49

Sta. + K - Grade.

1040.41

49

35.1

+50

34.6

50

34.0

+50

33.1

51

32.0

+50

30.6

1040.41
1282
1027.59

52

29.1

+27

28.3

OK

B.M.

12.82

1027.59

1027.61

Lt.

Z

Rt.

15

$$\begin{array}{r} 15 \\ 5.3 \\ 6.8 \end{array}$$

$$\begin{array}{r} 48 \\ DC20 \\ 33.0 \end{array}$$

$$\begin{array}{r} 50 \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ DC0.9 \\ 28.6 \end{array}$$

$$\begin{array}{r} 15 \\ 5.8 \\ 7.3 \end{array}$$

$$\begin{array}{r} 5.0 \\ DC2.3 \\ 34.2 \end{array}$$

$$\begin{array}{r} 53 \\ \hline \end{array}$$

$$\begin{array}{r} 5.1 \\ DC2.2 \\ 33.8 \end{array}$$

$$\begin{array}{r} 15 \\ 6.4 \\ 7.9 \end{array}$$

$$\begin{array}{r} 42 \\ DC3.7 \\ 34.8 \end{array}$$

$$\begin{array}{r} 59 \\ \hline \end{array}$$

$$\begin{array}{r} 5.8 \\ DC2.1 \\ 33.4 \end{array}$$

$$\begin{array}{r} 15 \\ 7.3 \\ 8.8 \end{array}$$

$$\begin{array}{r} 70 \\ DC1.8 \\ 32.2 \end{array}$$

$$\begin{array}{r} 69 \\ \hline \end{array}$$

$$\begin{array}{r} 5.7 \\ DC3.1 \\ 37.4 \end{array}$$

$$\begin{array}{r} 15 \\ 8.4 \\ 9.9 \end{array}$$

$$\begin{array}{r} 78 \\ DC2.1 \\ 33.4 \end{array}$$

$$\begin{array}{r} 93 \\ \hline \end{array}$$

$$\begin{array}{r} 4.3 \\ DC5.6 \\ 47.8 \end{array}$$

$$\begin{array}{r} 15 \\ 9.8 \\ 11.3 \end{array}$$

$$\begin{array}{r} 71 \\ DC4.2 \\ 41.8 \end{array}$$

$$\begin{array}{r} 94 \\ \hline \end{array}$$

$$\begin{array}{r} 7.8 \\ DC2.5 \\ 39.0 \end{array}$$

$$\begin{array}{r} 15 \\ 11.3 \\ 12.8 \end{array}$$

$$\begin{array}{r} 94 \\ DC3.4 \\ 38.6 \end{array}$$

$$\begin{array}{r} 111 \\ \hline \end{array}$$

$$\begin{array}{r} 10.4 \\ DC2.4 \\ 34.6 \end{array}$$

$$\begin{array}{r} 15 \\ 12.1 \\ 13.6 \end{array}$$

$$\begin{array}{r} 97 \\ DC3.9 \\ 40.6 \end{array}$$

$$\begin{array}{r} 118 \\ \hline \end{array}$$

$$\begin{array}{r} 10.7 \\ DC2.9 \\ 36.6 \end{array}$$

Sta. + K - Grade.

+38

27.9

+45

27.7

+59.56

27.3

B.M.

1027.61
Top of 104.

Et.

Et

Et.

Sta
T.P.

+

K

-

Grade.

1.70

1031.24

1029.54

42+30

27.2

+66

27.6

43

28.0

+45

28.5

44

29.2

+50

30.0

45

30.9

B.M.

2.48

1044.13

1037.65

+60

31.9

Lt.

#

Rt.

17

~~See pg. 13~~4.0
5.8
$$\begin{array}{r} 38 \\ D21.2 \\ \hline 31.8 \end{array}$$

3.6

$$\begin{array}{r} 8 \\ 10/ \\ \hline F.22 \\ \hline 44. \end{array}$$

3.2

$$\begin{array}{r} 124 \\ \hline F9.2 \\ \hline 518 \end{array}$$

2.7

$$\begin{array}{r} 121 \\ \hline F9.4 \\ \hline 53.6 \end{array}$$

2.0

$$\begin{array}{r} 114 \\ \hline F9.4 \\ \hline 53.6 \end{array}$$

1.2

$$\begin{array}{r} 68 \\ \hline F.56 \\ \hline 38.4 \end{array}$$

0.3

$$\begin{array}{r} 23 \\ \hline F.20 \\ \hline 24.0 \end{array}$$

10.2

$$\begin{array}{r} 124 \\ \hline F.22 \\ \hline 248 \end{array}$$

Sta.	+	π	-	Grade
------	---	-------	---	-------

1042.13

46				32.7
----	--	--	--	------

+15				32.9
-----	--	--	--	------

+42				<u>33.4</u>
-----	--	--	--	-------------

T.P.	12.08	1029.55		1017.47
------	-------	---------	--	---------

17				186
----	--	--	--	-----

+50		1029.55 2.22		15.4
-----	--	-----------------	--	------

18		$ \begin{array}{r} 1026.33 \\ 11.04 \\ \hline 1037.37 \end{array} $		20.5
----	--	--	--	------

+50				21.7
-----	--	--	--	------

T.P.	11.04	1037.37	3.22	1026.33
------	-------	---------	------	---------

19				23.2
----	--	--	--	------

+50				24.7
-----	--	--	--	------

20				26.3
----	--	--	--	------

Lt.

E

Rt.

18

$$\begin{array}{r} 15 \\ 9.4 \\ \hline 10.9 \end{array}$$

$$\begin{array}{r} 94 \\ \hline DC.15 \\ \hline 31.0 \end{array}$$

$$\begin{array}{r} 15 \\ 9.2 \\ \hline 10.7 \end{array}$$

$$\begin{array}{r} 69 \\ \hline DC.28 \\ \hline 40.4 \end{array}$$

$$\begin{array}{r} 15 \\ 8.7 \\ \hline 10.2 \end{array}$$

$$\begin{array}{r} 31 \\ \hline DC.71 \\ \hline 534 \end{array}$$

$$\begin{array}{r} 15 \\ 11.0 \\ \hline 12.5 \end{array}$$

$$\begin{array}{r} 125 \\ \hline DC.57 \\ \hline 33 \end{array}$$

11.0

$$\begin{array}{r} 15 \\ 10.2 \\ \hline 11.7 \end{array}$$

$$\begin{array}{r} 58 \\ \hline DC.8.9 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 15 \\ 9.1 \\ \hline 10.6 \end{array}$$

$$\begin{array}{r} 44 \\ \hline DC.6.7 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 15 \\ 7.9 \\ \hline 9.4 \end{array}$$

$$\begin{array}{r} 6 \\ \hline DC.8.4 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 15 \\ 14.2 \\ \hline 15.7 \end{array}$$

$$\begin{array}{r} 69 \\ \hline DC.8.8 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 15 \\ 17.7 \\ \hline 14.2 \end{array}$$

$$\begin{array}{r} 76 \\ \hline DC.6.6 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 15 \\ 11.1 \\ \hline 12.6 \end{array}$$

$$\begin{array}{r} 90 \\ \hline DC.3.6 \\ \hline 33.0 \end{array}$$

Sta.

+

K

-

Elev.

1037.37

20+50

27.8

21+50

29.4

21+50

30.9

24.

2

24.

19

$$\begin{array}{r} 9.6 \\ 11.1 \end{array}$$

$$\begin{array}{r} 10.5 \\ DC.06 \\ \hline 27.4 \end{array}$$

$$\begin{array}{r} 9.3 \\ \hline \end{array}$$

$$\begin{array}{r} 8.0 \\ 9.5 \end{array}$$

$$\begin{array}{r} 8.5 \\ DC.10 \\ \hline 29.0 \end{array}$$

$$\begin{array}{r} 2.4 \\ \hline \end{array}$$

$$\begin{array}{r} 6.5 \\ 8.0 \end{array}$$

$$\begin{array}{r} 5.3 \\ DC.27 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 5.8 \\ \hline \end{array}$$

Sta.

+

π

-

Elev.

Bench Levels.

Sta.	+	-	Elev.
B.M.			1027.61
T.P.	12.85	1040.46	7.81 1032.65
T.P.	0.06	1032.71	10.20 1022.51
T.P.	4.27	1026.78	2.07 1024.71
B.M.	9.08	1033.79	1.02 1034.79
B.M.	6.73	1039.50	4.12 1035.38
T.P.	4.12	1039.50	5.05 1034.45
T.P.	0.37	1034.81	12.34 1022.48
B.M.	0.46	1022.94	3.83 1019.11
T.P.	4.04	1023.15	4.12 1019.03
B.M.	7.99	1027.02	2.67 1024.35

Old Bench.
1035.43

Description

Top of Mon @ Bellevue & "E"

Spike in Ed. Rail Post Rt. Sta. 45+00

" " " " " " 37+00

" " " " " Lt. " 31+00

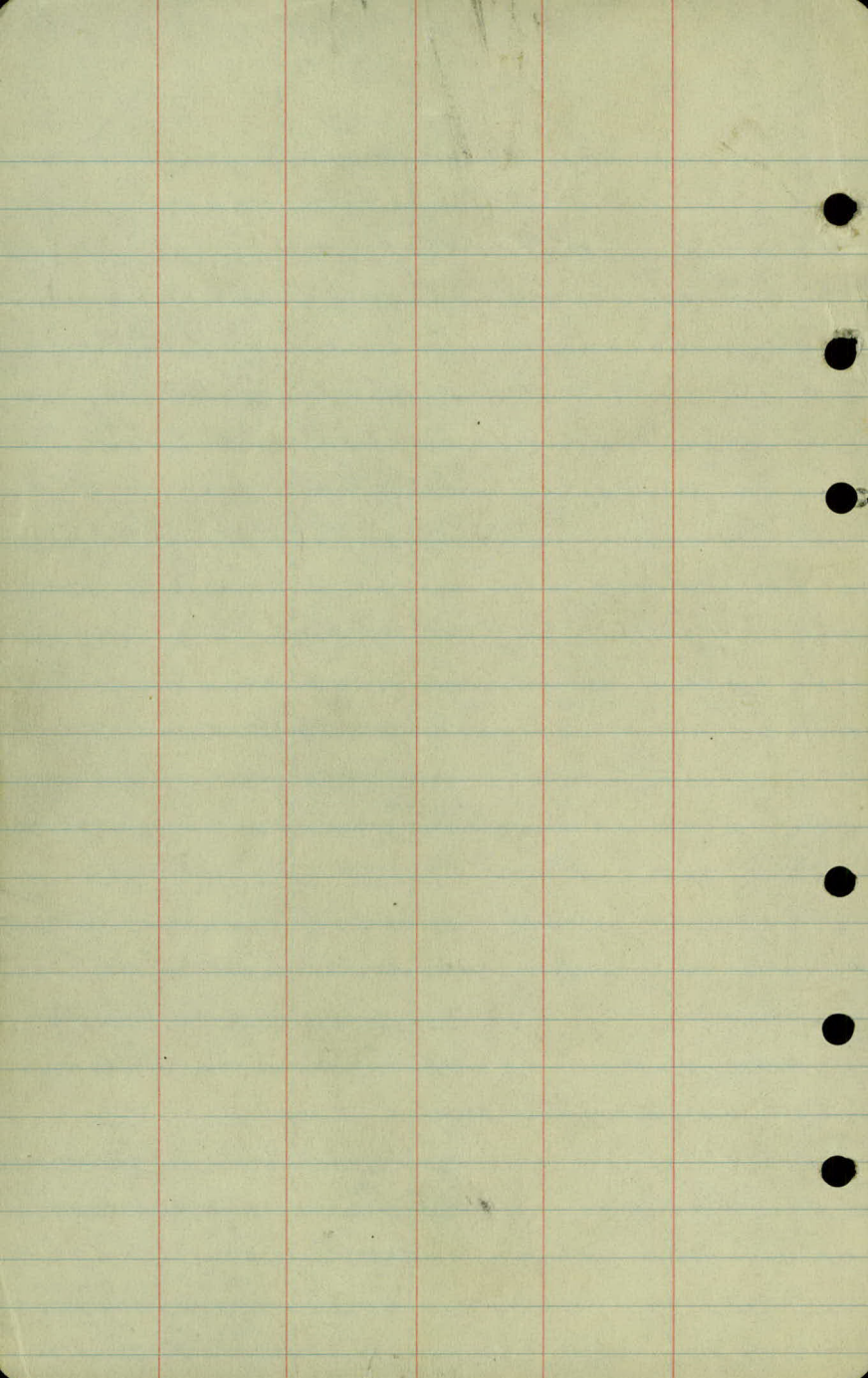
Ctr. of Stone Monument Sta. 26+34.58

Spike in 8" Oak 100' East & 7' So. of ctr. Sec. 36

Spike in top of Ed. Rail Post, Rt. Sta. 21+50

Spike in Fence post 150' Rt. Sta. 13+15

Stone monument Bellevue & "D"



Bellaire Ave

Slope Stakes

"D" to "E"

Sta.	+	x	-	Grade
B.M.	270	1027.05		1024.35

0	+33			24.2
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	+60			23.9
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1				23.5
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	+50			23.0
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2				22.5
---	--	--	--	------

	+50			22.0
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3				21.5
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	+40			21.1
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4				20.5
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	+50			20.0
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5				19.5
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T.P.	261	1025.19	7.97	1019.58
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Gr Rod L₁ L₂ P₁

Top Most Ballance #20

2.9 28.0 / $\frac{44}{25.00}$ $\frac{26}{103}$ 33.0

3.2 31.6 31.6 / $\frac{71}{-3.9}$ $\frac{33}{-0.1}$ $\frac{38}{27.07 / 25.6}$ 28.6

3.6 33.0 33.0 / $\frac{71}{-5.5}$ $\frac{39}{-0.3}$ $\frac{66}{-3.8 / 25.0}$ 27.2

4.1 33.0 33.0 / $\frac{71}{-5.0}$ $\frac{43}{-0.2}$ $\frac{77}{-3.6 / 30.4}$ 29.2

4.6 33 33.0 / $\frac{71}{-4.5}$ $\frac{45}{-0.1}$ $\frac{77}{7.4 / 28.8}$ 28.0

5.1 31.2 32.0 / $\frac{71}{-4.0}$ $\frac{50}{-0.1}$ $\frac{70}{-1.9 / 23.7}$ 23.2

5.6 25.2 25.2 / $\frac{79}{-2.3}$ $\frac{52}{104}$ $\frac{53}{103 / 32.2}$ 32.6

6.0 30.6 30.6 / $\frac{6.1}{20.19}$ $\frac{56}{-0.4}$ $\frac{42}{118 / 32.0}$ 33.0

6.6 33 32.9 / $\frac{3.3}{22.48}$ $\frac{62}{104}$ $\frac{54}{122 / 32.0}$ 33

7.1 33 32.0 / $\frac{33}{12.7}$ $\frac{68}{103}$ $\frac{42}{129 / 32.0}$ 33

7.6 33 32.0 / $\frac{5.2}{12.9}$ $\frac{73}{103}$ $\frac{68}{128 / 33.0}$ 33

Sta	+	π	-	Grade
		1022.19		
	+50			19.0
6				18.7
	+50			18.3
7				18.1
	+50			17.9
8				17.9
	+50			17.5
9				17.2
T.P.	10.89	1022.89	5.19	1018.00
	+50			17.7
10				17.7
	+50			17.6

G.R. Rod.	Lt	Φ	Rt.	
9.2	33	$32.0 / \frac{2.5}{4.4}$ 104	$\frac{4.4}{32.13} / 30.2$	31
9.5	30.2	$30.2 / \frac{R^*}{1.9}$ 103	$\frac{5.5}{32.95} / 27.0$	27.
9.9	25	$25.0 / \frac{6.9}{R^* 9.0}$ 105	$\frac{6.9}{32.00} / 25.0$	25.4
9.1	25.6	$26.0 / \frac{7.6}{-2.5}$ 103	$\frac{7.1}{-2.0} / 24.0$	23.2
5.3	28	$28.4 / \frac{8.9}{-3.1}$ 102	$\frac{7.2}{-1.9} / 23.6$	23.6
5.3	27.2	$27.2 / \frac{8.1}{-2.8}$ 101	$\frac{7.0}{-1.7} / 22.8$	22.8
5.4	24.4	$24.4 / \frac{7.5}{2.1}$ 102	$\frac{7.1}{-1.7} / 22.8$	22.8
5.4	33	$32.0 / \frac{4.9}{10.5}$ 90	$\frac{6.7}{32.02} / 25.8$	27.0
11.2	33	$32.0 / \frac{8.1}{12.5}$ 103	$\frac{11.8}{32.03} / 25.6$	27
11.2	33	$32.0 / \frac{7.5}{+9.0}$ 103	$\frac{11.3}{32.12} / 30.6$	29
11.3	33			32.6

Sta	+	A	-	Grade
11				17.6
	+50			17.5
12				17.5
	+50			17.4
13				17.4
	+50			17.3
14				17.3
	+50			17.2
15				17.2
	+50			17.2
16				17.5

Cor. Road

Lt

R

PL

57.2

49.6

51.2

53.2

57.2

50.4

25.2

2.8

30.2

20.6

Spk in P.C. Post 200' Lt. 93+44

54.2

41.4

69.0

50.2

71.8

64.6

74.6

67.4

63.4

47.8

20.6

Sta	+	-	Grade
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42	+66		27.6
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43			28.0
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	+95		28.5
--	-----	--	------

44			29.2
----	--	--	------

	+50		30.0
--	-----	--	------

45			30.9
----	--	--	------

	+60		31.9
--	-----	--	------

	282	942.54	954.72
--	-----	--------	--------

46			32.7
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	+15		32.9
--	-----	--	------

	+42		33.4
--	-----	--	------

B.M.

47			34.3
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GC Rod

Lt

R

Rt

6.4

752

804

772

80

496

100

7.5

336

7.6

$$37.4 / \frac{180}{116}$$

$$\frac{22}{104}$$

$$\frac{111}{1000} / 26.0$$

20.2

7.1

$$53.9 / \frac{35}{102}$$

$$\frac{86}{105}$$

350

82

502

$$54 / \frac{18}{104}$$

$$\frac{28}{104}$$

275

Sta	+	7	-	Grade
		942.54		
47	+50			349
1				
48				352
	4.30	939.84	7.00	935.54
	+50			352
49				351
	+50			346
50				340
	+50			331
51				320
	+50			306
52				291
	+27			283
B.M.			12.23	1027.61

16' Top
 41.15 lpc
 1.5' Pitch
 DS. 00 = 25'
 CUT 00 = 31'

Gr. Rod

Lt

Rt

Rt

7.6 486 $480 / \frac{31}{145}$ $\frac{74}{10.2}$ 29.0

7.3 466 $464 / \frac{34}{13.9}$ $\frac{70}{10.3}$ 31.8

4.6 350 $358 / \frac{36}{110}$ $\frac{42}{10.4}$ 28.0

4.7 330 $326 / \frac{44}{104}$ $\frac{44}{10.3}$ 28.6

5.2 342 $342 / \frac{44}{108}$ $\frac{42}{10.5}$ 33.8

5.8 398 $398 / \frac{36}{12.2}$ $\frac{38}{10.4}$ 33.4

6.7 322 $310 / \frac{6.5}{10.2}$ $\frac{63}{10.4}$ 37.4

7.8 33.4 $330 / \frac{73}{10.8}$ $\frac{7.7}{10.1}$ $\frac{24}{14.2} / 47.8$ 47.4

9.2 418 $424 / \frac{6.1}{10.6}$ $\frac{88}{10.4}$ 39.0

10.7 38.6 $38.2 / \frac{8.9}{11.8}$ $\frac{10.5}{10.2}$ $\frac{10.0}{10.7} / 33.8$ 34.6

11.3 40.2 $40.2 / \frac{9.2}{12.3}$ $\frac{11.2}{10.2}$ $\frac{10.2}{11.3} / 36.2$ 36.4

Top Most Bellows etc

