

Dr. 8 - Bk. 121

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

NORTH ST. PAUL RD.

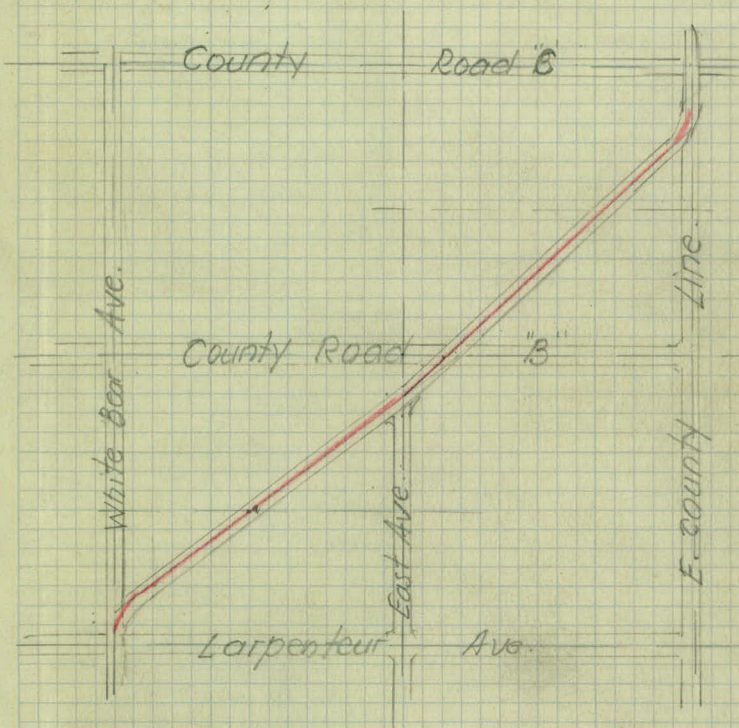
From White Bear Ave To East Co. Line Rd.

Road Acc't. No. 13

Date Filed 1937

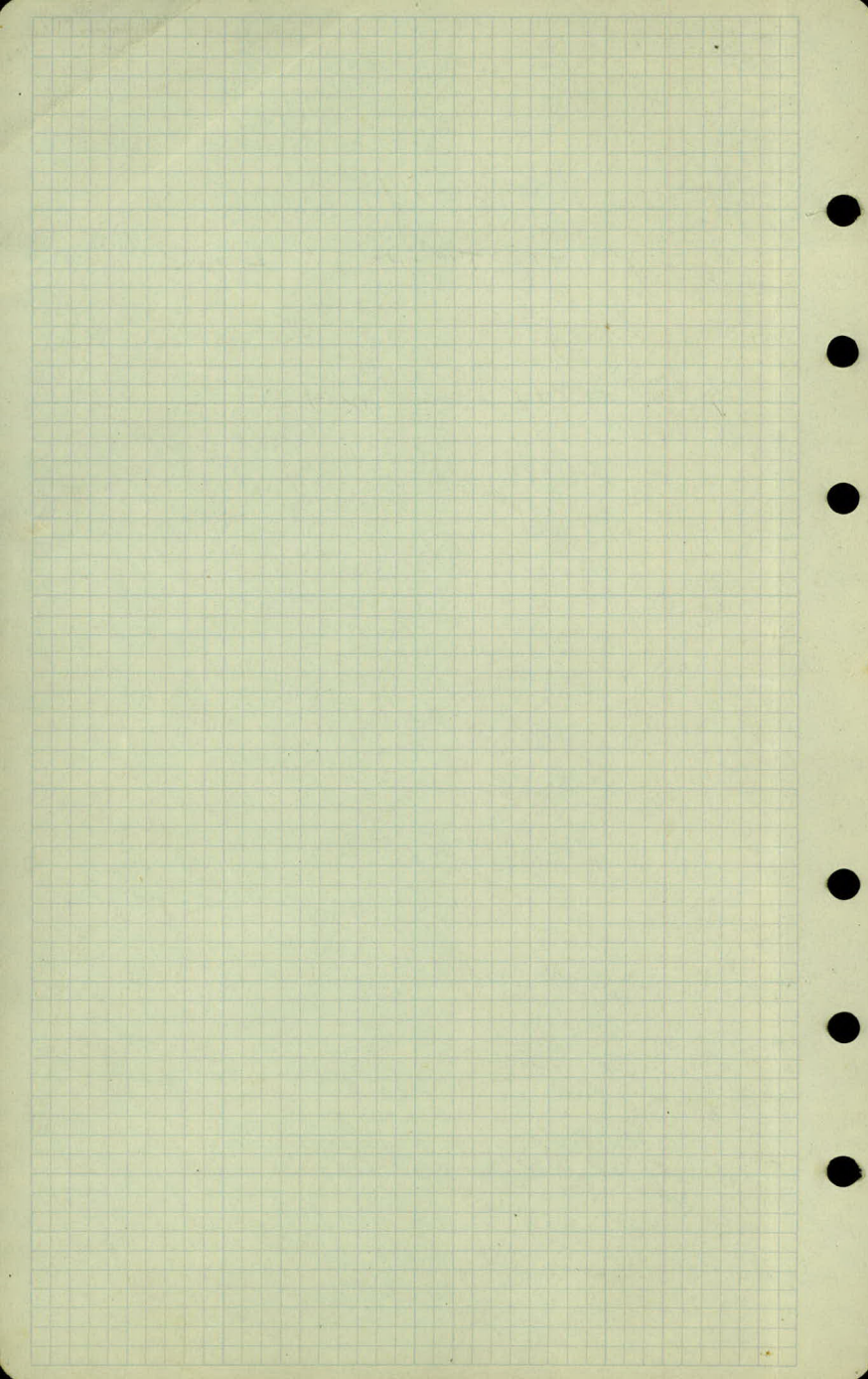
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Plan Survey
North St. Paul Road.
White Bear Ave. to E. Co. Line.



For alig See Rd Map Survey.

W. H. Carlson
June, 29, 1937



Topography

North St. Paul Road

White Bear to E. Co. Line

except from Sta. 96 to 122

5 10.3 11.4

10 12.8

4 G.R. 10 10 12.7

1. Plank

10 12.5

3 G.R. 10 10 12.3

G. Rail 10 10.0 12.2

2 51 12.2

33 12.0

1 21.7 12.0

14.4 98-11.3

→ Sloping Curb

0.0 12 12.0

+47-End Sloping Curb

+34-P.P. 28

+90-End G.R. 14
+81-G.P. 25'

+83-P.P. 30'

+47-G.P. 28'

+40-P.P. 28'

+39-P.P. Ch.P. 24'
+45-End Rad. 10'
+44-Manhole 33'
+34-End Curb. 27'
18" C.M.
+38-End Rad. 40'+36-P.P. 29'
+22-Manhole 17'

+37 P.P. 27'

+93-Spillway Door
+90-S. end 18" Conc. curb
+92-15" Maple 27' 20"
+69-Manhole 17'
+65-30" Maple 30"
+49-P.P. 25'

1. plank

15' scale

Sloping Curb

Full Dirt

Lapenteur

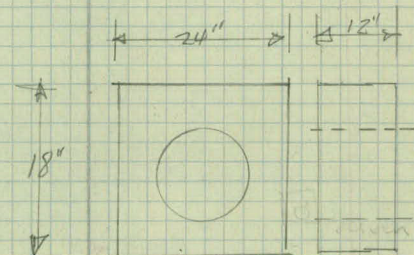
171.2'

+ 55-2 24" X 65' 32-33'
Concrete Goal

12

11

10



Note: See Const. Plans
for location of Tile Drains
These Tile Drains are
scattered as shown, it
will be necessary to
extend these in case
of widening.

9

8

7

6

+86-P.P. 78

Water

Low Land

1-Plant

+23-P.P. 78

+101-Range tie to fence
Line South 11

M.S.

+95-N. end T. & Drain - 76' } See Const. Plan.
+63-Beg. 9.R. 14'

+80-Beg. 9.R. 14'

+62-P.P. 28'

Hay Meadow

cut

+97-P.P. 28'

+83-Ent. 12" X 16" C.M.
21

+83-Ent 12" X 16" C.M.
23' 1/2"

+47-End Sloping Curb
+94-P.P. 78

19

18

17

+18 - Approx E Road.

16

+60 63 - 35

15

14

13

+48-T.P. & F.
33'

+23-P.P. 28'

Cult.

+22-T.P. & Fence
33'

+67-P.D. 28'

+52-T.D. & F. 34'

+19-T.P. & Fence 44'
+18-N. end 15" C.M. 23'

Cult. OK

15' x 50'

+41-Grub Pole 28'

+10-P.P. 28'

+02-End G.R. 14'

+90-Ramp tie to Fence 26'

+95-Grub Pole 26'

+67-End G.R. 14'

+66-S. end 15" C.M. 22'

N. St. P. Cont.

E. & W.

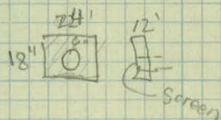
1-plank

+49-P.P. 28'

Posture.

26

25



24

23

22

21

20

+81-End G.R.
14
+69-T.P. & F.
34

+81-End G.R.
14
1-Plan K.

+38-~~Bag~~ G.R. 14
+43-T.P. & F. 34
+18-End 6" D. Tile - 27'
See Const. Plan.

1-Plan K

+58-P.P. 8
611
+54-End D. Tile
24'

+56-~~Bag~~ G.R. 14

+15-T.P. & F. 30

+98-P.P. 28

Cult.

Cult.

+73-T.P. & F. 30

+11-P.P. 28

20' concrete

+42-T.P. & F. 33

+83-P.P. 28

+14-T.P. & Fence
33

33

32

31

30

195 - G. L. P. L. Xing.

29

28

27

+01-T.P. 25'
Fence

+83-End G.R. 14'

+76-T.P. + Fence

+64-End 6" D.I.C. N.W.
25'
+47-T.P. + Fence.

+19-Beg. G.R. 14'

+24-T.P. + Fence.

+91-T.P. + Fence
35'
+78-Ent. Field

+41-P.P. 28'

+86-P.P.

+78-End G.R. 14'

+27-P.P. 28'
to 3-Beg G.R. 14'
+28-End Dr. 6" T.I.C.
N.W. - Broken
along

+73-P.P.

+92-Field Ent.

+18-P.P. 28'

Quik

Quik

1-P. plank

1-P. plank

40

39

38

37

36

35

34

+70-T.P.-34'

Scattered
Oak 45'

+44-T.P.

+54-R.P.

+08-T.P.

Scattered
Oak 45'

+06-R.P.

+45-End 6" Dr. T. 1/2 (110. Broken
25' away)

+22-Beg. Q.R. 14'

+15-F. Cor. 76'

+91-T.P. 34'

+84-F. Cor. 37'

+63- Stone Mon. 11'

+54-Range Tie to Fence No.

Scattered
Brush

Cult.

+09-End 6" Dr. T. 1/2 - 24'
H.W.

+13-Beg. Q.R. 14'

+54 R.P.

+62-T.P. & F.

+97-R.P.

+31 T.P. & F.

47

46

418-4 Morris St. N.Y.S.

45

44

43

42

41

Scatter
Small Trees

+61-12" BxL 41
+64-10" BxL 40
+57-8 1/2" x 7 1/2" 37 2x24
+41-8" W 37

+28 Ent 12"x20" CW
+10 P.P. 22' on

+10 T.P. 32'

+81 T.P. 32'

+96 Ent 15"x20" C.M.
25' 9' on
+62 P.P. 34'

+11-Bin F.R.G. 37'
+61-F.B.T. 32'
+68-End G.R. 24'

+88-Bin G.R. 4'
+67-15" Co H-36'
+56-End 6" Co. T. 625'
+54-18" Co # N.W.

+76 T.R. 32'

+05-24" Co #
F. 37 33

+78 9x9 P. 6 34'
+77-End G.R. P
+64-B.G.R. 14

+76-End 6" Lr. T. 6 H.W.

+23-15" Co H- 44'
+14-P.R. 34'

+06-15" Co # 46
+08-N.W. Cor. 2-5 F. 66

+84-15" Co # 45
+62-S.W. Cor. Ho. 55
+53-15" Co H- 46

+33-15" Pop. 46'

+22-T.P. 32' & Fens

Ha Rang, Tie Fa
West

+62-P.P.

+98-T.P.

+08-P.P.

54

161.5 - E St. R.R. Single Track

53

52

51

50

49

48

462-T.P.33'

403-Dr. Telle H.W. 26'
+ 12-Tro H Pole
33'

+97-809 Q.R. 1st
+88-Xing Signal - 15'

+39- 2 Ref. Lt.
+38-T.P. 34'

4th & 5th Lt.

128-T, R33

+47-15" Bx. E/c.
45

793- T.P. 32

421-15' Box-End
34

763-T.R.

+36-T.P.

LP/om/K

4/10/04

Berries

A23-P.P. 34'

+77-Beq. G. R. 14
+50-Troll Pole 45'

434-XingSheng-15

455-ENG 3 C.M.
26

+28 - Sep. 15th Vit 20th
+27 - End Oct. 18th H.V. 2.

120-Troll/Bolt

421-² S + S₂ 21'

478 P.P. 34

+ 75 - T.P. 38

~~7-11-20.~~

464-P.P. 34'

414-RP

138-ENT 12" X 76' C.M.
78'

172-12" Bx. El. HS

167-12 Bx. E. 4/9
167-12 Bx. E. 4/9

70. P. = 24

1

61

60

59

58

57

56

55

194-~~25~~ LT

1.5a.

11

+70-P.P.

+08-T.R+P.P.

+48-Ent 6" Dr. 7' 1/2 N.W.
22

+18-R.P.

+72-T.R+P.P.

+40-T.R.P.P.

+67-P.P.

+96-Ent. 12' x 24' C.M.
22

+38-T.R.P.P.

+18 P.P. 84'
+13-Wa/K 15' x 8' C.M.
21

+54-Ent 9' R. 14

+54-Ent 9' R. 14
+41-18" Bx Ent. 47'

+88-T.R+P.P.

+73-P.P.

68

67

66

+24 & 20" x 38.5 c.m.

(24"x4" c.m. Ext'd RT)
Very Poor

65

64

63

62

+67-T.P. & R.P.
52'

+42-Beg. G.R. 14
+86-R.P.

+93-2nd St. Lt.

+55-End G.R. 14
+52-Fire Hyd. 53'
+25-T.P. & R.P.

6" W.

+62-Ent. 15" X 20" CM
25' 0" 2"
+38-2-S.F. 87'

1/4 rd.

+77-End G.R. 14

+43-R.P. 34'

+05-T.P. & R.P.

+29
21

+19
16'

+76-T.P. & R.P.

+77-R.P.

+52-Beg. G.R. 14

+55-Beg. G.R. 14

+46-T.P. & R.P.

+24-R.P.

+43-T.P. & R.P.

75

74

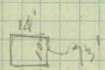
73

72

71

70

450-2 Fill Ha.
73



69

165-P.P. 33'

+13-T.P. & P.D. Trans
31'+95-End G.R.
14'

+25-P.P. 33'

+89-T.P. & P.D.
31'+28-Fire Hyd.
37.5'

+61-T.P. & P.D.

+78-P.D.

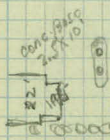
95-End Dr. T. 1/66"
22'+32-T.P. & P.D.
30'

+27-P.P. 33'

+53-Gas Pump 51'
+07-Gas Pump 51'
+50-Conc. Sign Post 32'

+10-S.E. Ch. 2-S.F. 72'

+15-Hedge 34'

+19-T.P. & P.D.
20'East Ave 32' P.D.
New Circle
South

+38-E East Ave

20' x 66' c.m. (new)

+85-P.P. 34'

+85-End G.R. 14'

+63-W. end 24' c.m.
42'

82

81

80

79

1401-2 Co. R. 1. B (East x West)

78

77

76

+81-T.P. P.P.D.

+57-P.P.

+76-Ent. 12'x20' C.M.

23' 9" R.

+17-6" Elm 45'

+01-6" Elm 45'

+83-5' E. cor. Hts 80'

+77-10' Elm 45'

+70-F. cor. 33'

+52-T.P. P.P.D.

34

+21-T.P. P.P.D.

+55-Fence cor. 38'

+47-Fire Hydr.

36.5

+97-T.D. P.P.D.

6'x12' Walk

12'x6'5" C.M.

+51
35

+69-T.P. P.P.D.

32'

+04-End G.R.

12'

+50-? End 6" Dr. Pipe-

+10-T.A. P.P.D. 31'

+22-6" Elm 44'

+04-6" Elm 44'

+95-8" Elm 44'

+87-2'x6" 80'

+81-3' Brick Walk

15 steps

21.5' 26'

+80-6" Elm 44'

+43-P.P. 33'

+16-2'x6" 100'

+60-F. cor.

38

+99-P.P.

+61-Fence cor.

41

+19

24'x68' C.M.
C.R.

+26-P.P. 33

+87-P.P. 33'

+36-End 6" Dr. Pipe Hts
75'

89

88

+15-25t. No. 150.

87

+15-25t. No. 150.

86

85

84

83

+87-15" x 10" S4
+87-5"E. Cor. Ho. 71'
+77-Ent. 12" x 20" C.M.
27'

+88-F. Cor. 50
+88-12" Box E. 50'
+67-1-5" F. (Small)
100'

+64-End C "Dr. T. to H. W."
25'

+44-Ent.

+12-R.P.

+42-2' Walk + 49'
+78-20" Oak R 52
+74-24" Oak-52
+65-Ent 12" x 20" C.M.
26' OK.

Circular Walk

+89-5 E. Cor. Ho. 68

+89-R.P. 34'
+78-Fire Hyd.
50'

+15-15" x 34" C.M.

+15-Guy Pole 33'

+85-P.R. 35'
+65-Guy Pole 34

15" x ? C.M.

+24-5 E. Cor. 1-5" F.
28'
+13-Ent 12" x 20" C.M.
18'

+40-R.P. 56

+65-T.P. + A.P.
35'

+36-2 No. 70

+35-T.P.

+75-12" Tree 53'

+65-8" E. 52'
+54-12" Box E. 52'
+45-8" Walk + Steps
+45-2 No. 79'
+37-12" Box E. 52'
+29-8" 2 No. 52'
+20-10" Tree-31'

+72-R.P. Ent. 33'

+45-Ent. 12" x ? C.M.
19' Buried.

+63-E. St. L. + 15" x 31"
21'

+33-8" Box 53
+40-N.W. Cor.
1st. +11-8" Box 83
+10-S.W. Cor. 80

+07-T.P. + P.R.

+92-R.P. 33'

$\frac{48}{1500}$
 +50 St. NTS. +50 36.1
 +25- 24.1

+20-Boehm
51

95

19.2 -

+71-Boehm 15.8 - 18.1
 +50 13.9 14.8 $\frac{40}{51.3}$

94

$+10 - \begin{cases} 11.0 \\ 10.0 \end{cases}$ $\frac{11.0}{10.0} + 10$

93

92

91

90

+60-2 Conc. Box 4x2 50
50

+45-R.R. 35'
+14-P.R. 35'
+12-S. end Curb 12'x
Cinder Walk 44'-40' 29'
+93-W.E. Cor. No. 71'
+84-2' Walk 50

+63-Ent. 12"x14' C.M.
30'

+43-End Hedge 48'

+16-W.E. Cor. No. 66'

+12-R.R. 35'

+90-S.E. Cor. No. 65'

+70-Cor. Hedge 48'

+62-Penn. Pl. 12"x20' C.M.
32'

Cinder Walk 45'-39'

+89-R.R. 35'

+83-E. No. 100'

+62-R.R. 35'

+44-S.E. Cor. No. 67'

+45-E. 2' Walk 48'

+37-Ent. 12"x24' C.M.
28' 84'

Cinder Walk
46'-41'

+40-R.R. 34'

(+75 10'x15' V.I.)
not in Use

+66-2' Walk 44.5'

+88-Rail Pt. 317

+49-Conc. Box Curb
61'

+11-W. end curb
65'

+89-S. end Curb 53'

+78-S. end 12'x14' 30'

+77-Guy 4x6 36'

+73-18" Br. E.D. 35'

+43-2'x4' Maple 76'

+12-Cor. Walk 41'-2' W

+03-18" to 40'

+97-S.W. Cor. No. 55'

+95-12" to 38'

+85-2'x4' to 36'

+71-2'x4' to 38'

+78-Ent. 12"x20' C.M.
26' 84'

+62-End Hedge 51'

+45-S.W. Cor. No. 76'

+39-Hedge 50'

+33-Ent. 12"x18' C.M.
26' 84'

+40-S.W. Cor. - 34'

+64-15" Br. E.D. 50'

+62-H. Cor. 53'

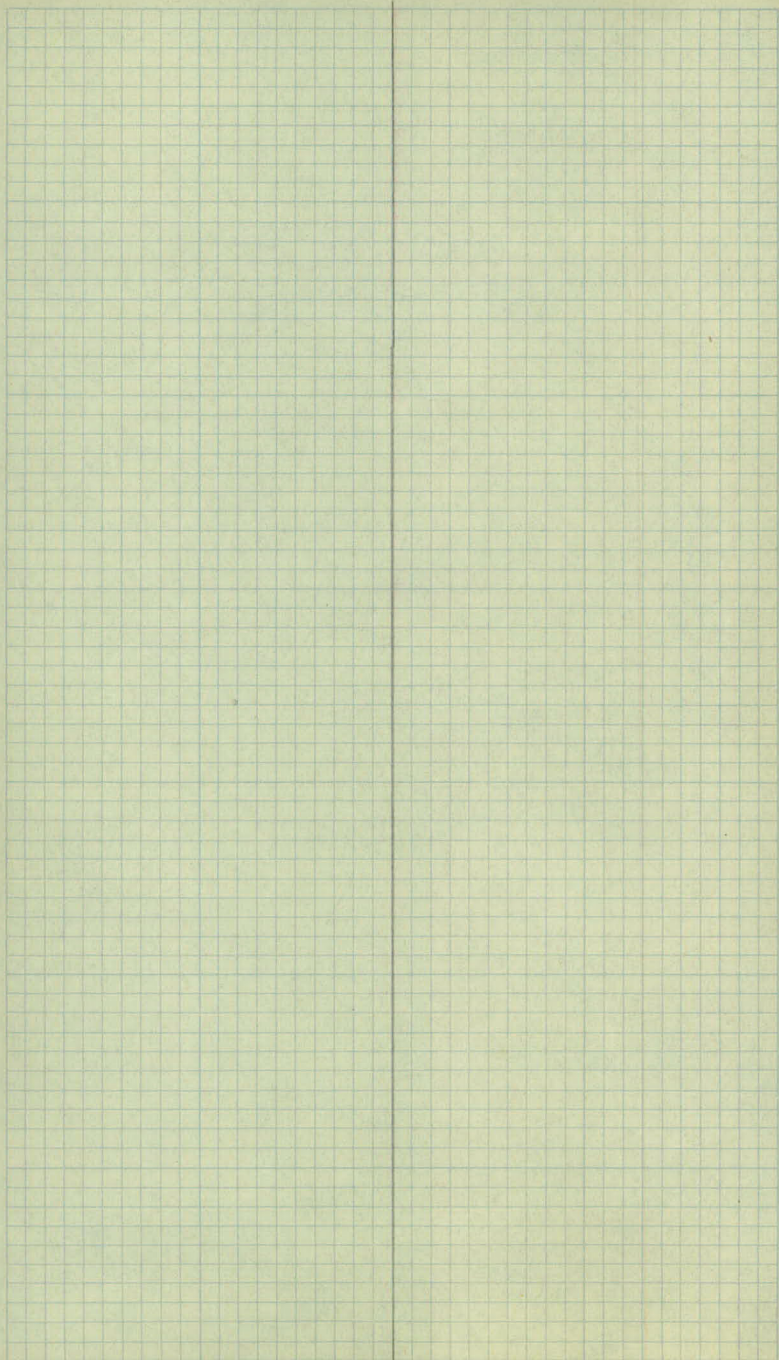
+66-Ent. 12"x20' C.M.
26'

+32-R.R. 33'

+29-N.W. Cor. No.

+16-E. 8' Walk 48'

+05-S.W. Cor. No. 90'



City paving

See donor plans or Road Map Survey.

124

123

122

+45- 11.1-10.0 10.0-10.9
+20 12.1 11.5-12.0
16.2 13.9

+85-24.4 18.2
+66
10
16.7 +75
19.7 +50
26.3 +25

121

+85-25.4 N. 75

40.3

+89
50

120

+90-Ent.

+57-N. Cor. Church

+42-E Church. 58'

+42-E 4' Conc. 31'

+28-S. Cor. Church.

+07-Ent.

+58-Ent.

+26-Cor. 2

+03-Cor 2 S.F. 50'

+13 Cor.
+88-Cor. 2 S.F. 70'

+12-N.W. 2 S.F.
+05-E 4 Steps Boff 49'
+89-Cor. 2 S.F. 69'
+08-End curb 72.3'

+38-Boff 4' 48'
+55-Cor.
+31-Cor. 1 S.F. 67'
+28-2' E 1/2 36'
+18-Begin curb 32' 32'

+35-End Wall
51-55

+80

+67-E Steps
+45-Cor. Hall-87

Top Rip Rap, SS
+14-Cor. W. K. S. 1
+11-Cor. W. K. 42

+70-P.R. 37

+17.8

Conc.

Gravel
Oiled.

Conc.

131

130

129

128

127

126

125

105 - 105 10

Begin Sloping Curb
End Curb

+03-149 145 10°

115 - 115 10

137

+80 148 144 10

136

116 113 10

135

134

133

132

+40-P.P. 72.5

10' 20'

+61-E.G.R. 14'
 +63-4 Conc. Spillway - 186
 +59-Beg. Curbing.

+86-P.P. 36



+97-Cor. Conc. Pav.

+70-Cor. Gar. 53.5

+51-Cor. Gar. 63'

+42-Ice/Hea 38.5

+36-P.P. 32

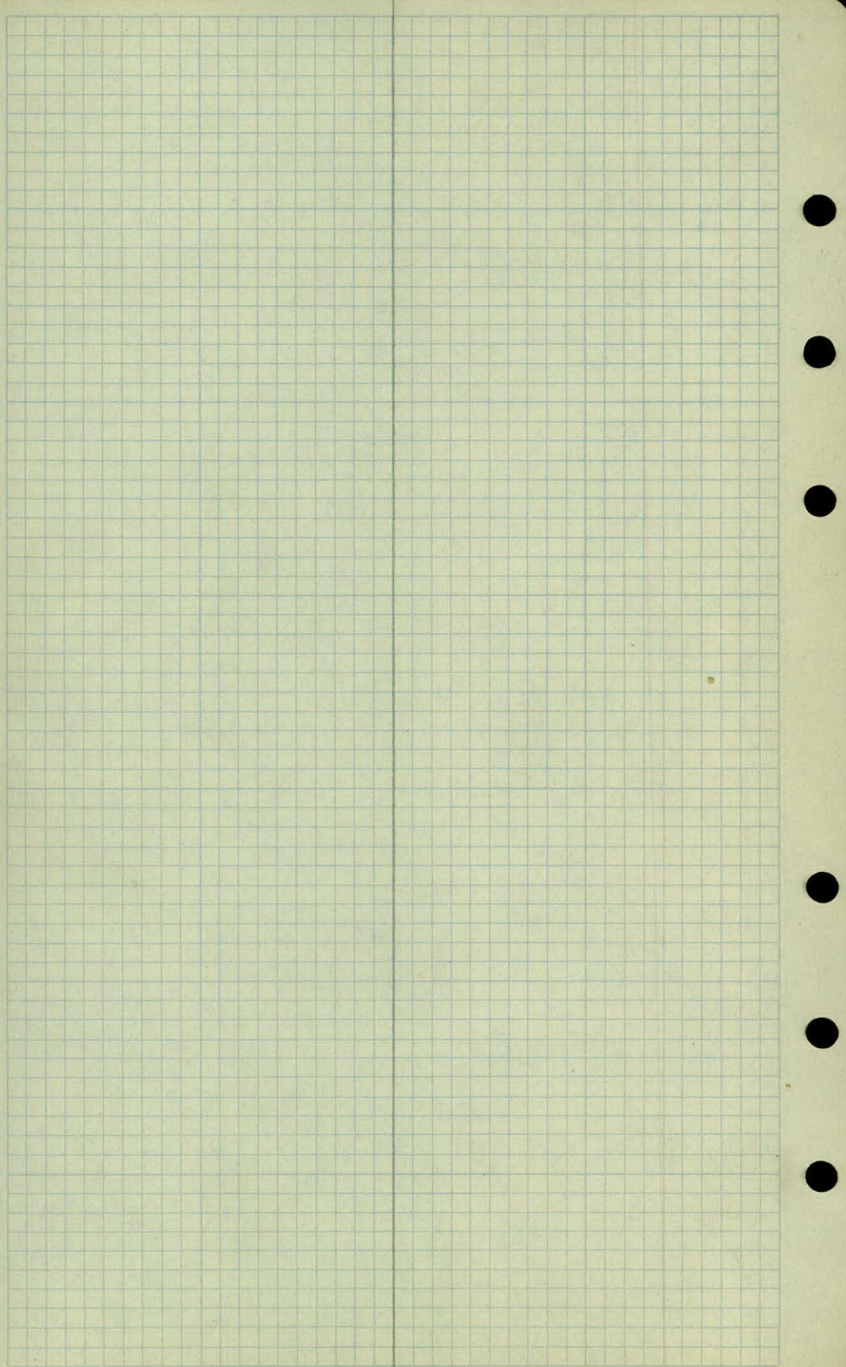
+35-Cor. Ice 41.5
 Hts. 6' X 8'

+17-Beg. G.R. 14

+70-P.P. 36

+33-P.P. 37

+48-E.G.R. 45



Bench Levels.

No. St. Paul Road,
White Bear Ave to

	+	-	Elev.	
B.M.	10.69	952.66	941.97	
T.P.	11.89	964.19	0.26	952.30
✓	7.41	969.55	2.05	962.14
B.M.	4.92	969.55	4.92	964.63
T.P.	13.53	979.11	3.97	965.58
✓	10.63	989.08	0.66	978.45
✓	5.54	990.47	4.15	984.93
B.M.	5.86	990.47	5.86	984.61
T.P.	1.37	988.37	3.47	987.00
B.M.	5.26	988.37	5.26	983.11
T.P.	10.67	995.37	3.67	984.70
B.M.	9.54	995.37	9.54	985.83
T.P.	0.09	988.79	6.67	988.70
✓	0.66	976.05	13.40	975.39
B.M.	1.73	974.88	2.90	973.15
	0.06	963.41	11.53	963.35
B.M.	10.14	964.84	8.71	954.70
T.P.	12.38	977.05	0.17	964.67
B.M.	9.79	977.05	9.79	967.26
T.P.	13.52	989.92	0.65	976.40
B.M.			7.26	
✓			2.90	987.02
T.P.	7.22	997.05	0.09	989.83
B.M.			7.24	970.81
				989.81
T.P.	0.06	983.40	13.71	983.34

W.H.C.
K.A.
G.G.
A.M.

22

June 21,
1937

Hyd. S.W. Cor. Loop & White Bear Ave

(964.64) Top of Pav. Sta 10+0

(984.63) Top of Pav. Sta 25+0

(983.08) Top of Pav. Sta 40+0

Top Five ¹²⁵ ft

(973.14) Top of Pav. Sta 57+0

954.70) Top Hyd.

967.24

Top of Pavement Co Rd B

986.99

Top Hyd. 36.5 ft. Sta 79+47

Top Hyd.

+ π - Elev.

983.40

T.R. 0.48 972.41 11.47 971.93

B.M. 5.21 966.91 10.71 961.70

" 7.31 972.79 1.43 965.48

T.R. 8.45 980.96 0.28 972.51

✓ 11.20 990.00 2.07 978.89 x

B.M. 3.09 987.00 x

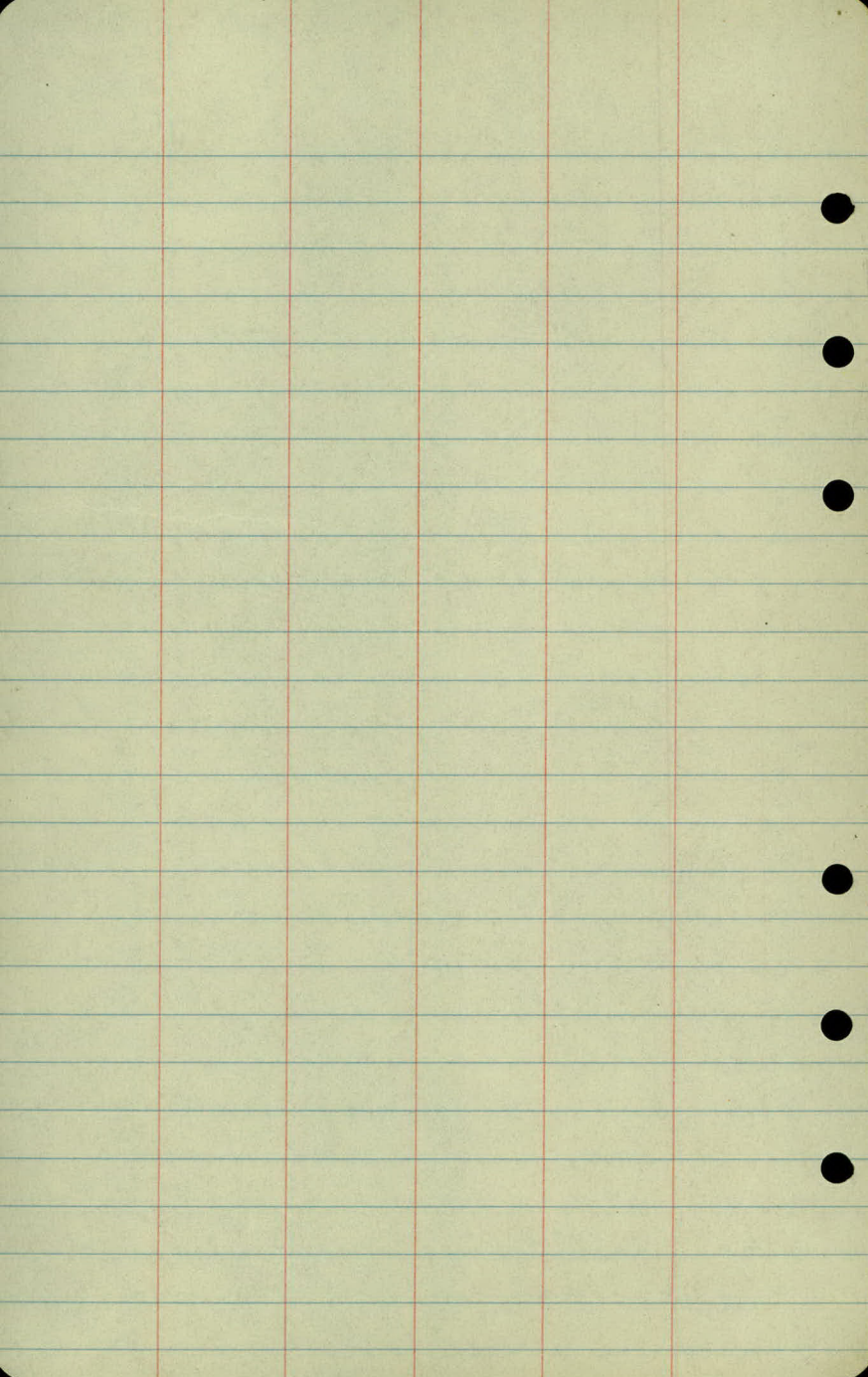
(961.71) Top Hyd. Lt. Sta 96+

" " Lt.

✓ Res. widening

✓

Top Hyd. Lt. Sta. 120+90



Lt. E Rt.

X-sections.

No. 5th Paul Road.

White Bear Ave to E. Co. Line.

Sta	+	π	-	Elev
B.M.	10.33	952.30		941.97 1035
-0+30				42.5
0+00				43.1
0+80				44.1
				44.9
1+0				45.0
1+50				45.8
2+0				47.2
2+50				49.2
3+0				51.4
T.P.	12.20	961.49	0.01	952.29
3+50				53.7
4+0				55.9

W.N.C.
K.A.
L.B.H.
S.H.

LT E RT May 3, 1937

Top Hyd. S.W. Cor. Large White Bear Ave.

(9.8)

9.78 9.94 10.0
w. T2 39 50eq Line

(9.2)

9.2 9.32 9.8 11.6 11.4
w. T2 T9 34 50

(8.2)

8.2 8.34 8.49 8.7 10.7 10.2 10.6
w. T2 T6 21 35 50

8.50
17 = Top Man hole

10.85
20 Flow Line 18' 10" 00

(7.4)

7.35 7.65 7.45 7.6 9.9 9.6
w. T1 T2 T6 22 50

(6.5)

6.48 6.70 6.52 6.5 8.2 8.1
w. T1 T2 T6 23 50

(5.1)

5.13 5.52 5.32 5.1 6.3 5.2
w. T1 T2 T6 21 50

(3.1)

3.11 3.69 3.52 3.7 5.3 5.3 4.6 3.6
w. T1 T2 T6 21 28 26 50

(0.9)

0.86 1.62 1.08 1.6 3.9 3.9 0.8 1.03
w. T1 T2 T6 21 28 23 50

(10.8)

11.1 10.1 11.8 11.8 9.9 10.18 10.6 11.58 11.34 11.5 13.3 8.6 8.1
50 23 28 23 17 10 11.2 12.4 19 23 23 50

(8.6)

10.4 9.1 10.1 10.1 7.8 8.0 8.4 9.24 9.27 9.4 11.2 11.2 5.1 4.9
50 31 28 21 16 10 11.5 12.7 18 23 28 40 50

White Bear Ave
Pavement

11' 0" 00

7.35 7.65
27' = Flow Line
w. T1 T2 T6 21 28 26 50

W. N. C.
K. A.
L. B. H.
S. H.

Sta.	+	π	-	Elev
		962.49		
2+50				57.7
3+0				59.4
4+50				60.9
T.P.	10.69	972.85	2.33	962.16
6				62.2
7+50				63.1
7+0				63.8
8+50			64.5	64.4
8+0				64.7
9+50				64.8
9+0				64.8
10+50				64.7

Lt. E Rt.

(6.8)

carb

10.2	9.2	8.4	6.3	6.2	6.8	7.6	7.2	7.8	9.7	9.7	4.3	4.2
50	28	20	15	10	—	11.5	11.6	18	70	75	34	50

(5.1)

6.6	6.0	7.4	7.0	4.8	4.7	5.1	5.58	5.36	5.7	7.8	6.7	3.6	3.8
50	31	25	19	14	10	—	10.5	11.6	17	23	28	33	50

(3.6)

2.1	1.8	2.0	4.0	3.4	3.0	3.59	3.90	3.68	3.9	5.2	5.6	4.3	3.6	3.5
50	33	24	78	14	10	—	9.5	10.5	15	19	24	30	33	50

(10.7)

7.8	7.4	10.7	11.5	10.7	10.6	10.69	10.80	10.60	10.9	12.3	12.4	11.6	10.2	11.2
50	33	25	20	16	10	—	9	10	16	19	26	30	34	50

(9.8)

End Carb +

8.6	8.6	10.9	11.1	11.0	10.0	9.78	9.79	9.82	9.9	11.3	12.1	11.6	10.0	9.9
50	31	25	23	20	17	10	—	10	16	21	25	31	34	50

(9.1)

9.5	9.7	11.2	10.9	9.3	9.05	9.10	9.15	9.4	11.2	11.8	10.9	9.0	8.8
50	31	28	19	15	10	—	10	15	20	25	31	35	50

(8.4)

8.3	8.3	10.0	10.8	10.4	8.6	8.4	8.43	8.49	9.0	10.3	11.2	10.6	8.4	8.3
50	32	28	23	19	15	10	—	10	16	19	23	31	35	50

(8.2)

7.9	8.2	10.0	10.3	9.9	8.4	8.18	8.17	8.21	8.4	10.8	10.8	10.2	8.1	7.6
50	32	26	23	19	15	10	—	10	16	21	26	31	35	50

(8.1)

9.9	9.5	10.7	10.8	10.1	8.4	8.08	8.06	8.1	8.4	10.5	10.5	10.0	6.6	6.2
50	31	29	23	18	14	10	—	10	16	21	26	27	33	50

(8.0)

10.1	9.1	10.9	11.3	10.2	8.4	8.13	8.13	8.05	8.4	9.8	10.2	9.0	4.3	3.2
50	32	28	24	19	15	10	—	10	16	18	20	27	33	50

(8.1)

9.9	8.6	11.1	10.9	8.4	8.18	8.11	8.17	8.3	10.1	9.5	8.3	2.8	1.8
50	31	27	21	15	10	—	10	15	20	24	27	34	50

Sta	+	π	-	Elev
		972.85		
1040				64.6
T.P.	4.66	969.30	8.21	964.64
+50				64.5
11				63.9
+50				63.8
12				63.9
+55	24" Cont. P.P.			64.6
13				65.6
+50				66.7
14				67.8
T.P.	8.94	977.43	0.81	968.49
+50				69.2
15				70.5
+50				71.8

LT. E RT.

(9495 $\frac{12.6}{26.1}$ = F.L. Line Drain 1/10)

(8.2)

13.0	11.8	13.2	13.0	11.2	8.6	8.28	8.21	8.27	8.3	11.0	10.1	5.6	4.0
50	33	31	27	22	15	10		10	15	21	25	34	50

Top of Pav. Sta. 10+00

(4.8)

12.2	11.2	5.1	4.97		4.84	4.8	5.2	8.6	6.6	5.6
50	29	10	10		10	14	24	31	35	50

(5.4)

13.2	13.0	12.2	5.6	5.56	5.42	5.42	5.4	9.4	8.2	8.4
50	41	28	10	10		10	14	25	36	50

(5.5)

13.6	13.1	6.0	5.50	5.47	5.53	5.5	10.9	11.0	9.3
50	31	15	10		10	15	25	35	50

(5.4)

13.6	12.9	6.1	5.51	5.41	5.42	5.9	11.7	12.1	10.0
50	31	15	10		10	15	27	40	50

13.6	Flow	13.5	5.4	4.95	4.7	Flow	5.0	13.2	12.5
50	37.6	15	10	10	4.74	4.85	15	33.6	50

(3.7)

12.5	10.8	4.0	3.53	3.69	3.67	3.5	11.4	12.3
50	29	15	10		10	15	29	50

(2.6)

5.8	5.4	2.9	2.66	2.60	2.60	2.6	9.3	10.8
50	28	15	10		10	14	27	50

(1.5)

4.6	4.6	6.5	6.6	1.7	1.54	1.48	1.56	1.4	5.5	11.3
50	33	28	27	15	10		10	14	28	50

(8.3)

9.1	8.5	11.8	12.0	8.8	8.4	8.32	8.42	8.7	14.0	14.8	16.6
50	34	30	27	24	15	10	10	15	25	29	50

(6.9)

15.4	13.2	7.2	2.06	6.94	6.98	7.1	10.2	10.8	9.1	8.9
50	27	13	10	10	10	14	26	30	35	50

(5.7)

5.0	5.8	8.8	8.8	6.0	5.71	5.66	6.85	6.2	12.0	13.4
4.2	8.2	27	25	15	10		10	14	20	50

4.9
5.6

Sta	+	π	-	Elev
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977.43

15+70

72.4

Side Culvert Left.

16

73.2

T.P.

13.74

988.69

2.48

974.95

74.0

+25

+50

74.7

17

76.3

+50

77.6

18

78.8

+50

80.0

19

80.9

+50

81.8

LT. E RT.

$\frac{45}{50}$ $\frac{44}{40}$ $\frac{45}{37}$ $\frac{5.2}{17}$ $\frac{5.13}{10}$ $\frac{5.1}{8.08}$ $\frac{5.14}{10}$ $\frac{5.2}{15}$ $\frac{10.3}{32}$ $\frac{12.0}{50}$

Flow line

$\frac{6.6}{30 \text{ End.}}$

$\frac{5.2}{No \text{ End.}}$

(4.2)

$\frac{10.4}{60}$ $\frac{16}{56}$ $\frac{16}{49}$ $\frac{3.4}{44}$ $\frac{3.5}{35}$ $\frac{3.7}{22}$ $\frac{4.22}{10}$ $\frac{4.21}{10}$ $\frac{4.26}{10}$ $\frac{4.2}{14}$ $\frac{6.0}{22}$ $\frac{7.2}{29}$ $\frac{5.9}{35}$ $\frac{8.7}{50}$

(14.7)

$\frac{11.1}{39}$ $\frac{12.4}{36}$ $\frac{12.9}{32}$ $\frac{15.7}{34}$ $\frac{15.7}{22}$ $\frac{14.55}{20}$ $\frac{14.73}{10}$ $\frac{14.78}{10}$ $\frac{14.9}{14}$ $\frac{12.2}{22}$ $\frac{17.2}{24}$ $\frac{13.3}{32}$ $\frac{15.9}{50}$
 $\frac{7.0}{53}$ $\frac{11.0}{44}$

(14.0)

$\frac{4.2}{50}$ $\frac{4.0}{48}$ $\frac{9.5}{37}$ $\frac{9.7}{34}$ $\frac{15.1}{24}$ $\frac{15.1}{19}$ $\frac{14.0}{15}$ $\frac{14.04}{10}$ $\frac{13.95}{10}$ $\frac{14.06}{10}$ $\frac{14.3}{13}$ $\frac{15.9}{21}$ $\frac{15.9}{26}$ $\frac{9.7}{37}$ $\frac{10.7}{42}$ $\frac{13.6}{50}$

(12.4)

$\frac{4.2}{50}$ $\frac{4.2}{37}$ $\frac{8.3}{29}$ $\frac{14.0}{21}$ $\frac{14.0}{18}$ $\frac{12.6}{13}$ $\frac{12.43}{10}$ $\frac{12.42}{10}$ $\frac{12.8}{12}$ $\frac{15.3}{19}$ $\frac{15.3}{23}$ $\frac{10.5}{33}$ $\frac{10.6}{41}$ $\frac{8.8}{45}$ $\frac{9.5}{50}$

(11.1)

$\frac{5.2}{50}$ $\frac{4.9}{32}$ $\frac{12.7}{21}$ $\frac{12.0}{17}$ $\frac{11.2}{14}$ $\frac{11.13}{10}$ $\frac{11.10}{10}$ $\frac{11.21}{10}$ $\frac{11.3}{15}$ $\frac{13.7}{20}$ $\frac{13.6}{23}$ $\frac{9.2}{33}$ $\frac{9.7}{44}$ $\frac{10.7}{50}$

(9.9)

$\frac{4.0}{50}$ $\frac{3.7}{41}$ $\frac{2.6}{21}$ $\frac{11.3}{19}$ $\frac{11.5}{17}$ $\frac{10.0}{13}$ $\frac{9.94}{10}$ $\frac{9.96}{10}$ $\frac{9.95}{10}$ $\frac{10.0}{13}$ $\frac{12.2}{19}$ $\frac{12.3}{23}$ $\frac{8.0}{32}$ $\frac{10}{50}$

(8.7)

$\frac{2.2}{50}$ $\frac{0.8}{33}$ $\frac{5.0}{28}$ $\frac{10.2}{19}$ $\frac{10.3}{18}$ $\frac{5.8}{13}$ $\frac{5.82}{10}$ $\frac{8.74}{10}$ $\frac{8.82}{10}$ $\frac{8.5}{14}$ $\frac{11.4}{20}$ $\frac{11.3}{23}$ $\frac{7.0}{31}$ $\frac{8.7}{49}$ $\frac{9.6}{50}$

(7.8)

$\frac{4.0}{50}$ $\frac{3.7}{32}$ $\frac{6.2}{27}$ $\frac{5.3}{22}$ $\frac{5.4}{19}$ $\frac{8.0}{24}$ $\frac{7.82}{10}$ $\frac{7.75}{10}$ $\frac{7.8}{13}$ $\frac{8.1}{18}$ $\frac{9.5}{24}$ $\frac{6.0}{31}$ $\frac{6.9}{35}$ $\frac{6.8}{46}$ $\frac{8.6}{50}$

(6.9)

$\frac{6.4}{50}$ $\frac{6.1}{27}$ $\frac{5.8}{21}$ $\frac{5.6}{18}$ $\frac{7.2}{14}$ $\frac{7.02}{10}$ $\frac{6.92}{10}$ $\frac{6.94}{10}$ $\frac{7.1}{15}$ $\frac{5.8}{20}$ $\frac{5.8}{32}$ $\frac{7.7}{27}$ $\frac{5.6}{33}$ $\frac{5.9}{45}$ $\frac{7.4}{50}$

Sta + π - Elev

988.69

20

82.4

82.5

+50

83.1

21

83.7

T.P

7.85

991.13

5.01

983.68

+50

84.0

22

84.3

+ 20

84.3

+50

84.3

23

84.4

+50

84.4

24

84.5

+50

84.5

Lt. £ Rt.

(6.2)

$\frac{65}{50}$	$\frac{53}{34}$	$\frac{47}{26}$	$\frac{76}{27}$	$\frac{76}{18}$	$\frac{63}{14}$	$\frac{620}{10}$	$\frac{626}{10}$	$\frac{63}{14}$	$\frac{75}{19}$	$\frac{74}{24}$	$\frac{41}{37}$	$\frac{40}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------

(5.6)

$\frac{46}{50}$	$\frac{32}{37}$	$\frac{67}{31}$	$\frac{68}{21}$	$\frac{68}{17}$	$\frac{57}{13}$	$\frac{559}{10}$	$\frac{559}{10}$	$\frac{566}{10}$	$\frac{58}{15}$	$\frac{67}{19}$	$\frac{67}{27}$	$\frac{41}{30}$	$\frac{40}{37}$	$\frac{34}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

(5.0)

$\frac{07}{50}$	$\frac{02}{31}$	$\frac{21}{28}$	$\frac{57}{21}$	$\frac{60}{18}$	$\frac{52}{14}$	$\frac{504}{10}$	$\frac{501}{10}$	$\frac{515}{10}$	$\frac{53}{15}$	$\frac{62}{19}$	$\frac{63}{21}$	$\frac{53}{25}$	$\frac{31}{37}$	$\frac{32}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

6.1 + 0

(7.5)

$\frac{32}{50}$	$\frac{30}{31}$	$\frac{85}{20}$	$\frac{85}{18}$	$\frac{87}{15}$	$\frac{759}{10}$	$\frac{752}{10}$	$\frac{762}{10}$	$\frac{77}{14}$	$\frac{85}{19}$	$\frac{83}{27}$	$\frac{44}{33}$	$\frac{41}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------

(7.3)

$\frac{49}{50}$	$\frac{40}{31}$	$\frac{85}{27}$	$\frac{85}{18}$	$\frac{74}{14}$	$\frac{732}{10}$	$\frac{726}{10}$	$\frac{731}{10}$	$\frac{75}{14}$	$\frac{85}{18}$	$\frac{79}{27}$	$\frac{26}{34}$	$\frac{24}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------

(7.2)

$\frac{56}{50}$	$\frac{57}{37}$	$\frac{53}{31}$	$\frac{67}{28}$	$\frac{86}{27}$	$\frac{85}{19}$	$\frac{75}{15}$	$\frac{729}{10}$	$\frac{720}{10}$	$\frac{730}{10}$	$\frac{73}{14}$	$\frac{82}{17}$	$\frac{79}{27}$	$\frac{32}{78}$	$\frac{27}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------

(7.2)

$\frac{53}{50}$	$\frac{58}{31}$	$\frac{71}{28}$	$\frac{85}{24}$	$\frac{85}{18}$	$\frac{75}{15}$	$\frac{727}{10}$	$\frac{721}{10}$	$\frac{730}{10}$	$\frac{74}{14}$	$\frac{84}{18}$	$\frac{84}{27}$	$\frac{58}{27}$	$\frac{51}{37}$	$\frac{41}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

(7.1)

$\frac{37}{50}$	$\frac{38}{36}$	$\frac{45}{31}$	$\frac{83}{23}$	$\frac{83}{19}$	$\frac{73}{14}$	$\frac{722}{10}$	$\frac{712}{10}$	$\frac{720}{10}$	$\frac{71}{13}$	$\frac{83}{17}$	$\frac{80}{27}$	$\frac{48}{37}$	$\frac{53}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------

(7.1)

$\frac{63}{50}$	$\frac{64}{26}$	$\frac{86}{27}$	$\frac{85}{20}$	$\frac{73}{14}$	$\frac{714}{10}$	$\frac{710}{10}$	$\frac{720}{10}$	$\frac{74}{14}$	$\frac{85}{18}$	$\frac{84}{27}$	$\frac{48}{28}$	$\frac{42}{38}$	$\frac{34}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

(7.1)

$\frac{64}{50}$	$\frac{65}{27}$	$\frac{81}{23}$	$\frac{82}{19}$	$\frac{73}{15}$	$\frac{709}{10}$	$\frac{707}{10}$	$\frac{716}{10}$	$\frac{72}{14}$	$\frac{82}{18}$	$\frac{82}{23}$	$\frac{61}{30}$	$\frac{49}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------

(7.0)

$\frac{7.9}{50}$	$\frac{7.4}{30}$	$\frac{8.8}{26}$	$\frac{8.6}{21}$	$\frac{7.3}{14}$	$\frac{7.05}{10}$	$\frac{7.02}{10}$	$\frac{7.12}{10}$	$\frac{7.1}{14}$	$\frac{8.3}{15}$	$\frac{8.1}{25}$	$\frac{7.0}{29}$	$\frac{5.1}{31}$	$\frac{3.9}{50}$
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Sta	+	π	-	Elev
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991.53

25

84.6

BM

5.00

989.63

6.90

(984.61 - v levels)
984.63

+182

+54

6" Drain

+35

84.7

26

84.7

+42

84.8

+80

84.9

27

84.9

+34

85.0

+68

85.0

28

85.0

+50

85.1

29

85.1

LT. £ RT.

6.9

$\frac{110}{50}$ $\frac{103}{34}$ $\frac{106}{29}$ $\frac{105}{25}$ $\frac{74}{15}$ $\frac{702}{10}$ $\frac{690}{10}$ $\frac{698}{10}$ $\frac{71}{15}$ $\frac{82}{19}$ $\frac{84}{24}$ $\frac{51}{37}$ $\frac{52}{50}$

Top Bar & Sta. 7500

9.20

9.40

50

$\frac{122}{30}$ $\frac{121}{40}$ $\frac{109}{29}$ $\frac{52}{14}$ $\frac{510}{10}$ $\frac{496}{10}$ $\frac{504}{10}$ $\frac{52}{15}$ $\frac{80}{22}$ $\frac{77}{26}$ $\frac{67}{31}$ $\frac{63}{50}$

4.9

$\frac{148}{50}$ $\frac{129}{27}$ $\frac{55}{25}$ $\frac{504}{10}$ $\frac{490}{10}$ $\frac{494}{10}$ $\frac{23}{16}$ $\frac{119}{29}$ $\frac{122}{46}$ $\frac{119}{50}$

4.8

$\frac{131}{50}$ $\frac{133}{39}$ $\frac{122}{28}$ $\frac{54}{16}$ $\frac{491}{10}$ $\frac{480}{10}$ $\frac{486}{10}$ $\frac{50}{15}$ $\frac{67}{20}$ $\frac{100}{28}$ $\frac{100}{50}$

4.7

$\frac{56}{50}$ $\frac{74}{40}$ $\frac{68}{27}$ $\frac{78}{25}$ $\frac{76}{21}$ $\frac{49}{14}$ $\frac{485}{10}$ $\frac{472}{10}$ $\frac{475}{10}$ $\frac{48}{16}$ $\frac{73}{25}$ $\frac{71}{29}$ $\frac{48}{34}$ $\frac{47}{50}$

4.7

$\frac{63}{10}$ $\frac{46}{39}$ $\frac{43}{31}$ $\frac{71}{25}$ $\frac{70}{21}$ $\frac{52}{15}$ $\frac{485}{10}$ $\frac{469}{10}$ $\frac{473}{10}$ $\frac{52}{17}$ $\frac{68}{23}$ $\frac{67}{26}$ $\frac{30}{33}$ $\frac{31}{50}$

4.6

$\frac{57}{50}$ $\frac{40}{40}$ $\frac{37}{31}$ $\frac{65}{27}$ $\frac{65}{21}$ $\frac{52}{16}$ $\frac{478}{10}$ $\frac{464}{10}$ $\frac{472}{10}$ $\frac{47}{15}$ $\frac{65}{22}$ $\frac{64}{27}$ $\frac{31}{34}$ $\frac{41}{46}$ $\frac{42}{50}$

4.6

$\frac{54}{50}$ $\frac{78}{39}$ $\frac{73}{33}$ $\frac{68}{25}$ $\frac{52}{15}$ $\frac{475}{10}$ $\frac{460}{10}$ $\frac{468}{10}$ $\frac{49}{15}$ $\frac{65}{20}$ $\frac{68}{31}$ $\frac{60}{33}$ $\frac{68}{50}$

4.6

$\frac{52}{50}$ $\frac{27}{45}$ $\frac{69}{34}$ $\frac{68}{19}$ $\frac{51}{15}$ $\frac{474}{10}$ $\frac{461}{10}$ $\frac{467}{10}$ $\frac{48}{15}$ $\frac{71}{34}$ $\frac{77}{42}$ $\frac{77}{50}$

4.5

$\frac{31}{50}$ $\frac{18}{39}$ $\frac{23}{33}$ $\frac{66}{26}$ $\frac{66}{19}$ $\frac{48}{14}$ $\frac{460}{10}$ $\frac{452}{10}$ $\frac{460}{10}$ $\frac{48}{15}$ $\frac{65}{19}$ $\frac{63}{29}$ $\frac{52}{32}$ $\frac{59}{41}$ $\frac{66}{50}$

4.5

$\frac{24}{50}$ $\frac{07}{39}$ $\frac{07}{33}$ $\frac{60}{24}$ $\frac{61}{18}$ $\frac{48}{14}$ $\frac{456}{10}$ $\frac{450}{10}$ $\frac{458}{10}$ $\frac{47}{15}$ $\frac{63}{20}$ $\frac{58}{30}$ $\frac{15}{36}$ $\frac{21}{50}$

Sta + π - Elev

789.63

29+35

85.1

+80

85.3

30

85.3

+80

85.4

31

85.6

T.P.

9.47

795.21

3.89

785.74

20+28
+64 6" Tile Drain

31+50

85.8

32

86.1

32+50

86.2

+85

86.3

33

86.4

+50

86.6

Lt. E Rt.

(4.5)

$\frac{1.9}{50}$	$\frac{1.0}{40}$	$\frac{1.0}{32}$	$\frac{5.9}{24}$	$\frac{5.8}{17}$	$\frac{4.7}{14}$	$\frac{4.54}{10}$	$\frac{4.50}{10}$	$\frac{4.58}{10}$	$\frac{4.7}{15}$	$\frac{6.0}{18}$	$\frac{5.3}{28}$	$\frac{4.12}{37}$	$\frac{4.05}{50}$
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(4.4)

$\frac{3.2}{50}$	$\frac{3.5}{39}$	$\frac{4.5}{30}$	$\frac{6.0}{26}$	$\frac{5.9}{20}$	$\frac{4.6}{15}$	$\frac{4.47}{10}$	$\frac{4.38}{10}$	$\frac{4.49}{10}$	$\frac{4.5}{16}$	$\frac{5.5}{21}$	$\frac{5.6}{29}$	$\frac{5.3}{33}$	$\frac{3.6}{36}$	$\frac{3.6}{50}$
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(4.3)

$\frac{4.7}{50}$	$\frac{4.9}{39}$	$\frac{5.4}{34}$	$\frac{6.0}{28}$	$\frac{5.6}{20}$	$\frac{4.4}{14}$	$\frac{4.40}{10}$	$\frac{4.34}{10}$	$\frac{4.45}{10}$	$\frac{4.4}{15}$	$\frac{5.9}{19}$	$\frac{6.0}{30}$	$\frac{6.5}{37}$	$\frac{6.5}{50}$
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(4.2)

$\frac{6.6}{50}$	$\frac{6.7}{38}$	$\frac{2.2}{33}$	$\frac{2.1}{22}$	$\frac{4.4}{15}$	$\frac{4.31}{10}$	$\frac{4.21}{10}$	$\frac{4.30}{10}$	$\frac{4.3}{15}$	$\frac{5.6}{19}$	$\frac{5.4}{24}$	$\frac{9.4}{50}$
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(4.0)

$\frac{8.1}{50}$	$\frac{8.1}{37}$	$\frac{8.5}{34}$	$\frac{8.1}{22}$	$\frac{4.4}{15}$	$\frac{4.15}{10}$	$\frac{4.03}{10}$	$\frac{4.13}{10}$	$\frac{4.2}{15}$	$\frac{8.8}{27}$	$\frac{9.3}{41}$	$\frac{9.8}{50}$
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Flow
line
13.3

Flow
line
14.2

(9.4)

$\frac{1.32}{50}$	$\frac{1.32}{38}$	$\frac{1.35}{36}$	$\frac{1.30}{21}$	$\frac{9.9}{14}$	$\frac{9.54}{10}$	$\frac{9.42}{10}$	$\frac{9.56}{10}$	$\frac{9.5}{15}$	$\frac{10.9}{21}$	$\frac{1.34}{26}$	$\frac{1.31}{41}$	$\frac{1.30}{50}$
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(9.2)

$\frac{1.17}{50}$	$\frac{1.31}{42}$	$\frac{1.31}{37}$	$\frac{1.39}{35}$	$\frac{1.38}{23}$	$\frac{9.7}{14}$	$\frac{9.36}{10}$	$\frac{9.6}{10}$	$\frac{9.25}{10}$	$\frac{9.4}{15}$	$\frac{10.7}{20}$	$\frac{10.8}{30}$	$\frac{10.0}{41}$	$\frac{10.0}{50}$
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(9.0)

$\frac{1.21}{50}$	$\frac{1.35}{34}$	$\frac{1.35}{26}$	$\frac{1.10}{18}$	$\frac{9.5}{14}$	$\frac{9.15}{10}$	$\frac{9.02}{10}$	$\frac{9.12}{10}$	$\frac{9.3}{14}$	$\frac{10.7}{21}$	$\frac{10.8}{22}$	$\frac{12.3}{27}$	$\frac{12.3}{40}$	$\frac{11.7}{50}$
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(8.9)

$\frac{10.3}{50}$	$\frac{11.0}{38}$	$\frac{11.6}{34}$	$\frac{11.6}{27}$	$\frac{11.6}{22}$	$\frac{10.1}{16}$	$\frac{8.1}{14}$	$\frac{8.88}{10}$	$\frac{8.97}{10}$	$\frac{8.96}{10}$	$\frac{9.1}{15}$	$\frac{10.3}{19}$	$\frac{10.5}{23}$	$\frac{11.1}{25}$	$\frac{11.1}{50}$	$\frac{9.8}{34}$	$\frac{5.2}{50}$
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(8.8)

$\frac{8.0}{50}$	$\frac{8.1}{38}$	$\frac{8.4}{32}$	$\frac{11.2}{26}$	$\frac{11.1}{21}$	$\frac{8.5}{17}$	$\frac{9.0}{15}$	$\frac{8.91}{10}$	$\frac{8.79}{10}$	$\frac{8.89}{10}$	$\frac{9.1}{14}$	$\frac{10.3}{20}$	$\frac{10.5}{25}$	$\frac{11.0}{30}$	$\frac{9.0}{35}$	$\frac{8.3}{50}$
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(8.6)

$\frac{5.8}{50}$	$\frac{5.6}{43}$	$\frac{5.8}{34}$	$\frac{10.7}{27}$	$\frac{10.7}{20}$	$\frac{8.8}{15}$	$\frac{8.68}{10}$	$\frac{8.61}{10}$	$\frac{8.71}{10}$	$\frac{9.0}{15}$	$\frac{10.2}{19}$	$\frac{10.5}{33}$	$\frac{6.9}{37}$	$\frac{6.9}{50}$
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Sta	+	Σ	-	Elev
		995.21		
34				86.8
+50				87.0
35				87.0
+50				86.9
36				86.8
+50				86.5
T.R.	2.41	988.78	8.84	986.37
37				86.0
+50				85.5
37+09 } +45 }	6" Tile Drain See Topog			
38				85.0
+50				84.6
+60				84.4

LT

E

RT

(8.4)

$$\begin{array}{cccccccccccccccc} 6.4 & 7.1 & 11.0 & 10.6 & 8.7 & 8.52 & 8.41 & 8.47 & 8.9 & 10.2 & 10.6 & 6.7 & 6.0 & 6.4 & 6.3 \\ 50 & 33 & 27 & 19 & 14 & 10 & 8.41 & 10 & 16 & 19 & 21 & 37 & 40 & 42 & 50 \end{array}$$

(8.3)

$$\begin{array}{cccccccccccccccc} 7.1 & 7.1 & 10.6 & 10.2 & 8.4 & 8.52 & 8.25 & 8.33 & 8.6 & 8.9 & 10.2 & 5.9 & 5.8 \\ 50 & 32 & 26 & 19 & 15 & 10 & 8.25 & 10 & 15 & 18 & 32 & 38 & 50 \end{array}$$

(8.2)

$$\begin{array}{cccccccccccccccc} 6.7 & 6.4 & 10.3 & 10.0 & 8.4 & 8.31 & 8.21 & 8.29 & 8.4 & 5.6 & 8.7 & 5.4 & 5.8 & 5.5 \\ 50 & 32 & 26 & 20 & 15 & 10 & 8.21 & 10 & 15 & 18 & 34 & 38 & 43 & 50 \end{array}$$

(8.1)

$$\begin{array}{cccccccccccccccc} 5.2 & 4.7 & 10.2 & 10.0 & 8.7 & 8.43 & 8.28 & 8.30 & 8.5 & 10.1 & 9.7 & 6.0 & 6.6 \\ 50 & 33 & 25 & 19 & 15 & 10 & 8.28 & 10 & 15 & 20 & 32 & 38 & 50 \end{array}$$

(8.4)

$$\begin{array}{cccccccccccccccc} 4.3 & 4.8 & 9.7 & 10.1 & 8.8 & 8.54 & 8.44 & 8.54 & 8.7 & 8.4 & 10.6 & 8.9 & 7.7 & 8.6 \\ 50 & 35 & 28 & 20 & 15 & 10 & 8.44 & 10 & 14 & 22 & 29 & 32 & 37 & 50 \end{array}$$

(8.7)

$$\begin{array}{cccccccccccccccc} 5.3 & 6.1 & 10.2 & 10.2 & 9.1 & 8.77 & 8.72 & 8.81 & 9.0 & 11.2 & 11.3 & 13.9 \\ 50 & 33 & 27 & 19 & 15 & 10 & 8.72 & 10 & 15 & 21 & 30 & 50 \end{array}$$

(2.8)

$$\begin{array}{cccccccccccccccc} 2.5 & 2.7 & 4.5 & 4.4 & 3.0 & 2.86 & 2.80 & 2.87 & 3.0 & 2.0 & 8.7 & 9.2 \\ 50 & 30 & 27 & 23 & 15 & 10 & 2.80 & 10 & 15 & 23 & 41 & 50 \end{array}$$

(3.3)

$$\begin{array}{cccccccccccc} 8.4 & 8.7 & 3.8 & 3.37 & 3.34 & 3.4 & 9.2 & 9.9 & 10.1 \\ 50 & 25 & 14 & 10 & 3.26 & 10 & 15 & 25 & 29 & 50 \end{array}$$

flow
line
8.7flow line
7.8

(3.8)

$$\begin{array}{cccccccccccc} 11.5 & 10.2 & 4.4 & 3.90 & 3.82 & 3.9 & 5.0 & 5.3 & 5.3 \\ 50 & 26 & 14 & 10 & 3.80 & 10 & 15 & 18 & 26 & 50 \end{array}$$

(4.2)

$$\begin{array}{cccccccccccc} 11.2 & 9.3 & 4.6 & 4.32 & 4.23 & 4.33 & 4.7 & 6.9 & 5.9 & 3.6 & 3.1 \\ 50 & 25 & 14 & 10 & 4.23 & 10 & 16 & 25 & 32 & 36 & 50 \end{array}$$

(4.4)

$$\begin{array}{cccccccccccc} 11.0 & 8.4 & 4.6 & 4.45 & 4.35 & 4.43 & 4.5 & 4.8 & 7.8 & 7.1 \\ 50 & 24 & 14 & 10 & 4.35 & 10 & 15 & 17 & 25 & 50 \end{array}$$

Sta	+	π	-	Elev
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988.75

39				84.1
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+50				83.6
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+80				83.3
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40				83.1
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B.A.	3.21	986.29	5.70	983.08
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+15				82.9
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+50				82.6
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41				82.1
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+65				81.7
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42			81.8	81.7
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+50				82.0
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43				82.5
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LT. £ RT.

(4.7)

$\frac{10.0}{50}$	$\frac{71}{31}$	$\frac{73}{28}$	$\frac{50}{14}$	$\frac{4.80}{10}$	$\frac{4.72}{10}$	$\frac{4.82}{10}$	$\frac{50}{15}$	$\frac{2.5}{25}$	$\frac{10.4}{50}$
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(5.2)

$\frac{13.2}{50}$	$\frac{101}{25}$	$\frac{65}{15}$	$\frac{5.28}{10}$	$\frac{5.19}{10}$	$\frac{5.28}{10}$	$\frac{55}{15}$	$\frac{6.8}{19}$	$\frac{11.1}{26}$	$\frac{13.1}{50}$
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(5.5)

$\frac{14.8}{50}$	$\frac{120}{26}$	$\frac{5.9}{15}$	$\frac{5.67}{10}$	$\frac{5.52}{10}$	$\frac{5.59}{10}$	$\frac{5.6}{15}$	$\frac{9.7}{27}$	$\frac{11.0}{50}$
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(5.7)

$\frac{14.4}{50}$	$\frac{115}{26}$	$\frac{6.0}{15}$	$\frac{5.84}{10}$	$\frac{5.70}{10}$	$\frac{5.81}{10}$	$\frac{5.9}{15}$	$\frac{9.6}{26}$	$\frac{12.2}{50}$
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£ Amount 612 40+00

(3.4)

$\frac{10.9}{50}$	$\frac{88}{26}$	$\frac{40}{14}$	$\frac{3.53}{16}$	$\frac{3.81}{10}$	$\frac{3.48}{10}$	$\frac{36}{14}$	$\frac{6.9}{21}$	$\frac{8.8}{28}$	$\frac{9.8}{50}$
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(3.7)

$\frac{13.8}{50}$	$\frac{12.5}{30}$	$\frac{4.4}{14}$	$\frac{3.83}{10}$	$\frac{3.73}{10}$	$\frac{3.83}{10}$	$\frac{4.2}{14}$	$\frac{14.2}{34.0}$	$\frac{16.3}{50}$
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(4.2)

$\frac{15.5}{50}$	$\frac{19.7}{31}$	$\frac{4.8}{14}$	$\frac{4.98}{10}$	$\frac{4.22}{10}$	$\frac{4.30}{10}$	$\frac{4.5}{14}$	$\frac{12.9}{29}$	$\frac{15.8}{50}$
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(4.6)

$\frac{14.3}{50}$	$\frac{11.3}{27}$	$\frac{4.9}{14}$	$\frac{4.61}{10}$	$\frac{4.55}{10}$	$\frac{4.69}{10}$	$\frac{4.9}{14}$	$\frac{9.8}{28}$	$\frac{10.8}{50}$
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(4.5)

$\frac{14.6}{50}$	$\frac{11.6}{26}$	$\frac{5.1}{14}$	$\frac{4.63}{10}$	$\frac{4.60}{10}$	$\frac{4.61}{10}$	$\frac{4.9}{14}$	$\frac{12.8}{28.0}$	$\frac{13.8}{50}$
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(4.3)

$\frac{15.7}{50}$	$\frac{18.9}{20}$	$\frac{5.2}{14}$	$\frac{4.47}{10}$	$\frac{4.31}{10}$	$\frac{4.40}{10}$	$\frac{4.4}{100}$	$\frac{14.7}{32}$	$\frac{14.9}{50}$
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(3.8)

$\frac{16.4}{50}$	$\frac{15.3}{23}$	$\frac{4.9}{19}$	$\frac{3.96}{10}$	$\frac{3.76}{10}$	$\frac{3.85}{10}$	$\frac{4.3}{14}$	$\frac{14.4}{31}$	$\frac{14.8}{50}$
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Sta	+	T	-	Elev
		986.29		
13+50				83.4

44				84.7
I.P.	9.00	986.14	0.15	986.14
+50				86.0

+65				86.4
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+80				86.8
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45				87.4
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+85				88.1
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+50				88.8
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+75				89.5
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46				90.1
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+50				91.3
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B.M.	9.32	995.14	9.32	985.82
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Lt £ Rt.

(2.9)

$\frac{12.3}{50}$	$\frac{12.3}{44}$	$\frac{13.5}{38}$	$\frac{13.5}{33.0}$	$\frac{35}{14}$	$\frac{30.1}{10}$	2.88	$\frac{30}{10}$	$\frac{3.8}{14}$	$\frac{11.0}{29}$	$\frac{11.0}{37}$	$\frac{10.8}{50}$
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(1.6)

$\frac{10.1}{50}$	$\frac{9.9}{29.0}$	$\frac{2.1}{14.0}$	$\frac{1.72}{10}$	1.60	$\frac{1.72}{10}$	$\frac{1.9}{14}$	$\frac{7.6}{27}$	$\frac{9.5}{37}$	$\frac{5.5}{50}$
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(9.1)

$\frac{15.6}{50}$	$\frac{13.9}{26}$	$\frac{7.9}{14}$	$\frac{8.12}{10}$	9.1	$\frac{9.3}{10}$	$\frac{9.5}{14}$	$\frac{12.7}{26}$	$\frac{15.1}{33}$	$\frac{14.9}{50}$
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(8.7)

$\frac{12.7}{50}$	$\frac{12.3}{26}$	$\frac{9.1}{14}$	$\frac{8.72}{10}$	8.72	$\frac{8.86}{10}$	$\frac{8.9}{14}$	$\frac{11.8}{26}$	$\frac{12.0}{42}$	$\frac{10.8}{50}$
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(8.3)

$\frac{18.2}{50}$	$\frac{11.0}{23}$	$\frac{8.3}{14}$	$\frac{8.32}{10}$	8.31	$\frac{8.45}{10}$	$\frac{8.7}{15}$	$\frac{10.5}{50}$
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(7.8)

$\frac{10.9}{50}$	$\frac{9.9}{26}$	$\frac{8.4}{18}$	$\frac{7.85}{10}$	7.85	$\frac{7.91}{10}$	$\frac{8.7}{26}$	$\frac{9.5}{36}$	$\frac{8.4}{50}$
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(7.1)

$\frac{10.5}{50}$	$\frac{9.5}{40}$	$\frac{7.14}{10}$	7.09	$\frac{7.19}{10}$	$\frac{7.3}{14}$	$\frac{7.1}{21}$	$\frac{8.7}{30}$	$\frac{6.2}{36}$	$\frac{5.7}{50}$
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(6.4)

$\frac{10.4}{50}$	$\frac{8.9}{28}$	$\frac{6.40}{10}$	6.38	$\frac{6.46}{10}$	$\frac{6.4}{15}$	$\frac{8.1}{20}$	$\frac{8.3}{28}$	$\frac{4.9}{38}$	$\frac{4.1}{50}$
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(5.7)

$\frac{9.8}{50}$	$\frac{8.3}{30}$	$\frac{7.8}{21}$	$\frac{6.3}{14}$	$\frac{5.74}{10}$	5.69	$\frac{5.78}{10}$	$\frac{5.8}{14}$	$\frac{7.3}{20}$	$\frac{8.2}{26}$	$\frac{4.3}{30}$	$\frac{3.1}{50}$
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(5.0)

$\frac{10.0}{50}$	$\frac{7.8}{29}$	$\frac{8.3}{27}$	$\frac{7.8}{20}$	$\frac{5.5}{14}$	$\frac{5.08}{10}$	5.08	$\frac{5.12}{10}$	$\frac{5.3}{14}$	$\frac{7.8}{20}$	$\frac{7.8}{26}$	$\frac{4.2}{38}$	$\frac{3.8}{50}$
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(3.9)

$\frac{7.7}{50}$	$\frac{6.7}{37}$	$\frac{7.2}{29}$	$\frac{7.8}{26}$	$\frac{7.0}{21}$	$\frac{4.1}{14}$	$\frac{3.93}{10}$	3.88	$\frac{3.96}{10}$	$\frac{4.0}{15}$	$\frac{6.5}{22}$	$\frac{6.8}{26}$	$\frac{5.7}{31}$	$\frac{4.7}{50}$
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Top Hyd. 12.5' Lt. Sta 46+35

Sta	+	π	-	Elev
		995.14		
47				92.2
	+35			92.7
	+45			92.8
T.P.	3.37	1002.77	1.74	993.40
	+45			
	+80			93.2
48				93.4
	+50			93.7
49				93.7
	+42			93.5
	+50			93.5
50				92.9
T.P.	3.24	996.19	9.82	992.95

Lt. E Rt.

(3.0)

$\frac{83}{50}$	$\frac{42}{38}$	$\frac{61}{24}$	$\frac{58}{19}$	$\frac{33}{15}$	$\frac{30}{10}$	295	$\frac{303}{10}$	$\frac{31}{15}$	$\frac{52}{20}$	$\frac{50}{29}$	$\frac{33}{33}$	$\frac{36}{50}$
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(2.5)

$\frac{51}{50}$	$\frac{34}{36}$	$\frac{30}{27}$	$\frac{47}{33}$	$\frac{47}{19}$	$\frac{28}{14}$	$\frac{288}{10}$	296	$\frac{35}{10}$	$\frac{26}{16}$	$\frac{36}{19}$	$\frac{49}{24}$	$\frac{28}{27}$	$\frac{11}{50}$
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(2.3)

$\frac{40}{50}$	$\frac{17}{26}$	$\frac{44}{21}$	$\frac{43}{18}$	$\frac{26}{15}$	$\frac{284}{10}$	232	$\frac{238}{10}$	$\frac{23}{15}$	$\frac{41}{19}$	$\frac{43}{23}$	$\frac{13}{28}$	$\frac{13}{31}$
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(10.0)

$\frac{70}{340}$	$\frac{56}{50}$
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(9.6)

$\frac{66}{50}$	$\frac{52}{39}$	$\frac{48}{33}$	$\frac{116}{22}$	$\frac{118}{18}$	$\frac{99}{14}$	$\frac{96}{16}$	955	$\frac{962}{10}$	$\frac{98}{15}$	$\frac{11.5}{18}$	$\frac{114}{26}$	$\frac{2.9}{37}$	$\frac{2.7}{50}$
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(9.4)

$\frac{67}{50}$	$\frac{45}{38}$	$\frac{47}{33}$	$\frac{114}{23}$	$\frac{113}{18}$	$\frac{98}{14}$	$\frac{950}{10}$	938	$\frac{945}{10}$	$\frac{98}{15}$	$\frac{114}{18}$	$\frac{117}{24}$	$\frac{1.2}{39}$	$\frac{1.2}{50}$
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(9.1)

$\frac{64}{50}$	$\frac{58}{31}$	$\frac{110}{21}$	$\frac{111}{17}$	$\frac{94}{16}$	$\frac{915}{10}$	906	$\frac{912}{10}$	$\frac{92}{15}$	$\frac{106}{18}$	$\frac{102}{24}$	$\frac{43}{35}$	$\frac{3.2}{50}$
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(9.1)

$\frac{26}{50}$	$\frac{32}{32}$	$\frac{111}{21}$	$\frac{108}{17}$	$\frac{93}{14}$	$\frac{916}{10}$	907	$\frac{912}{10}$	$\frac{9.3}{15}$	$\frac{110}{18}$	$\frac{110}{25}$	$\frac{8.7}{32}$	$\frac{6.7}{34}$	$\frac{6.6}{50}$
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(9.3)

$\frac{1.2}{50}$	$\frac{30}{39}$	$\frac{10.2}{23}$	$\frac{10.8}{18}$	$\frac{75}{15}$	935	926	$\frac{935}{10}$	$\frac{95}{15}$	$\frac{119}{22}$	$\frac{89}{27}$	$\frac{7.2}{50}$
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(9.3)

$\frac{27}{50}$	$\frac{29}{32}$	$\frac{10.6}{22}$	$\frac{148}{17}$	$\frac{97}{16}$	$\frac{936}{10}$	930	$\frac{94}{10}$	$\frac{94}{17}$	$\frac{116}{21}$	$\frac{11.6}{25}$	$\frac{84}{30}$	$\frac{45}{37}$	$\frac{48}{50}$
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(9.8)

$\frac{50}{50}$	$\frac{51}{33}$	$\frac{11.4}{23}$	$\frac{11.6}{17}$	$\frac{10.2}{15}$	$\frac{993}{10}$	989	$\frac{988}{10}$	$\frac{101}{16}$	$\frac{11.4}{18}$	$\frac{111}{30}$	$\frac{40}{37}$	$\frac{4.9}{50}$
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£ Rev. 50 to 5000

Sta	+	π	-	Elev
		996.19		
50+50				92.3
51				91.4
+50				90.2
+85				89.1
52				88.7
+35				87.6
+70				86.6
53				85.7
T.P.	0.88	985.53	11.54	984.65
+35				84.7
+72				83.7
54				82.9

LT £ Rt. 6/10/37

3.9

8.1 13 4.4 6.1 8.9 4.4 4.00 3.9 4.00 4.1 5.9 6.3 5.6 5.6 0.0
50 30 76 21 18 15 10 - 10 15 19 25 30 36 50

4.8

1.1 2.2 7.0 7.0 5.3 4.0 4.82 4.93 5.3 6.4 7.2 2.6 2.2
50 32 23 18 15 10 10 10 15 20 29 35 50

6.0

3.7 2.3 2.3 8.6 8.3 6.4 6.13 6.0 6.12 6.4 8.2 9.0 3.1 4.2
50 41 32 22 17 14 10 - 10 15 19 28 36 50

5.4 6.4 5.5 5.5 9.2 9.2 7.4 7.2 7.6 7.1 7.4 9.4 9.8 4.9 6.2
50 33 32 29 22 17 12 10 10 15 20 28 37 50

7.1

7.5

5.7 6.4 6.4 7.3 9.6 9.2 7.9 7.6 7.4 7.57 7.8 9.8 10.1 7.1 7.8
50 27 26 24 23 17 15 10 10 15 21 27 33 50

8.6

9.7 8.8 10.4 10.4 8.8 8.62 8.58 8.66 8.7 10.5 10.8 10.2
50 27 23 21 17 10 10 15 19 29 50

9.6

11.3 11.2 11.6 9.8 9.2 9.60 9.7 9.6 11.6 11.7 10.7 11.2
50 24 17 14 10 - 10 14 19 27 32 50

10.5

12.3 12.2 12.3 10.9 10.64 10.50 10.6 11.2 11.6 12.7 12.3
50 26 19 15 10 10 19 20 33 50

0.9

2.6 2.5 2.3 1.2 1.02 0.88 0.92 0.9 1.3 0.9
50 26 14 15 10 10 15 16 32

Top Rail to Rail

Re Topq.

3.1 3.4 3.6 2.2 2.1 2.03 1.33 1.90 2.2 7.3 8.5
46 26 32 11.5 Top Rail 14 10 10 16 27 50

2.6

3.06 3.0 3.6 3.7 5.8 3.7 2.8 2.79 2.3 2.7 2.7 3.1 8.8 9.7
50 Rail 4.25 12 33 29 18 14 10 10 14 17 26 50

5.4 6.6 2.6 1.1 2.0 1.1 2.0 1.1 2.0 1.1 2.0 1.1 2.0 1.1 2.0
50 Rail 4.25 12 33 29 18 14 10 10 14 17 26 50

Sta	+	π	-	Elev
		985.53		
54+50				81.4
55+0				79.8
+50				78.1
56+0				76.5
+50				74.9
T.P.	1.14	974.30	12.37	973.16
57+0				73.2
+50				71.6
58+0				69.9
+50				68.3
59+0				66.6
+50				64.9

Lt. £ Rt.

(4.2)

89	96	97	63	47	435	415	431	111	44	60	110	109
50	36	25	17	14	10	10	10		14	18	28	50

(5.7)

11.3	10.6	6.2	5.86	5.73	5.91	6.3	7.4	12.5	12.4	12.5
50	76	14	10	10	10	10	18	27	37	50

(7.4)

126	126	7.8	7.57	7.92	7.55	7.9	9.3	13.3	13.3	13.3
50	24	14	10	10	10	14	19	27	37	50

(9.1)

130	132	9.4	9.2	9.04	9.16	9.4	10.8	13.9	13.2
50	23	14	10	10	10	14	19	29	50

(10.7)

13.1	12.8	13.0	10.9	10.73	10.66	10.84	11.0	13.0	13.9	12.7
50	32	21	14	10	10	10	14	19	23	50

Top of Page. 59 to

(1.1)

29	3.3	1.4	1.14	1.14	1.34	1.4	3.1	3.1	3.9	3.2	2.9	2.1
50	20	14	10	10	10	14	16	18	20	23	26	50

(2.8)

5.2	4.7	5.5	5.1	2.9	2.92	2.75	2.86	3.0	4.8	4.8	4.1	3.5
50	32	26	21	14	10	10	10	14	19	23	26	50

(4.4)

6.0	5.4	7.4	7.2	4.9	4.58	4.46	4.5	4.9	6.3	6.3	5.0	6.0
50	31	27	18	14	10	10	10	15	22	26	20	50

(6.0)

5.5	4.5	8.5	8.4	6.4	6.21	6.0	6.12	6.3	7.9	7.9	6.0	7.0
50	31	26	19	15	10	10	10	15	19	29	33	50

(7.7)

7.1	7.2	10.5	10.3	8.1	7.81	7.67	7.78	8.0	7.5	7.6	6.7	6.9
50	32	27	20	15	10	10	10	14	19	28	32	50

(9.4)

11.5	10.6	12.0	11.0	9.7	9.49	9.36	9.52	9.8	11.6	11.4	8.3	8.4
50	32	28	18	15	10	10	10	15	22	33	38	50

Sta	+	π	-	Elev.
		974.30		
60+0				63.3
T.P.	2.34	964.22	12.42	961.88
60+50				61.9
61+0				
				60.7
+50				59.7
62+0				59.1
+50				58.5
63+0				58.1
+50				57.6
64+0			57.1	57.2
+50				56.7
T.P.	4.76	961.08	7.90	956.32
65+0				56.3

+ 24-l Culo. See Topog.

Lt. E Rt.

(11.0)

14.2/34	133	135	113	1105	1096	1011	114	127	132	102	161
50 39	32	20	15	10		10	16	19	34	37	50

(2.3)

6.2	5.4	5.0	2.8	2.53	2.34	2.49	2.7	4.1	4.3	1.8	3.5	3.6
50 30	19	15	10			10	15	19	28	33	44	50

6048 $\frac{5.8}{22}$ Dr. Tile.

(3.5)

6140	8.2	7.1	7.5	6.8	4.1	3.68	3.54	3.64	4.2	5.3	5.3	5.6
	50	33	31	21	15	10		10	15	20	31	50

(4.5)

150	8.9	7.9	7.9	5.0	4.61	4.49	4.61	4.6	5.3	6.4	6.2	5.7
	50	31	21	14	10		10	13	19	22	36	50

(5.2)

6240	8.4	8.1	7.3	5.5	5.27	5.16	5.27	5.9	7.2	7.2	7.4
	50	33	22	16	10		10	15	20	30	50

(5.8)

67150	7.9	9.2	8.1	7.6	6.4	5.87	5.75	5.84	6.0	7.8	8.0	7.9
	50	47	29	18	15	10		10	14	22	33	50

6340	9.5	8.5	9.0	8.5	6.6	6.29	6.13	6.28	6.7	8.1	8.7	9.2
	50	32	28	22	15	10	(6.1)	10	15	21	35	50

(6.7)

9.0	8.4	9.6	9.0	7.2	6.84	6.66	6.81	7.1	9.4	9.7	10.5	10.2
50	34	31	20	15	10		10	16	21	29	40	50

(7.1)

9.6	9.1	9.9	9.7	7.6	7.2	7.1	7.15	7.6	10.1	11.2	11.0
50	30	27	20	15	10	0	10	15	20	38	50

(7.6)

10.8	10.5	9.7	7.6	7.68	7.55	7.68	7.8	11.4	11.5	12.2
50	29	21	15	10		10	15	23	33	50

(4.8)

8.9	8.8	7.9	4.7	4.80	4.76	4.90	4.7	9.5	9.7
50	34	21	14	10		10	14	22	50

Fl. Line $\frac{10.14}{}$ $\frac{10.02}{}$ Fl. Line.

Sta	+	Σ	-	Elev.	
		961.08			
65+50				56.2	
66+0				56.2	
+50				56.2	
67				56.2	
B.N.	6.38	961.08	6.38		954.70
+50				56.2	
68+0				56.4	
+50				56.7	
69+0				57.2	
+50				57.7	
+70				57.9	
69+85				58.1	
T.P.	9.05	967.39	2.74		958.34

LT. E. RT.

(4.9)

10.1 10.0 5.0 4.99 4.89 4.99 4.9 9.0 8.5
50 27 14 10 10 15 24 50

(4.9)

11.3 10.5 5.10 5.00 4.92 4.98 5.0 8.6 8.2
50 25 14 10 10 14 22 50

(4.9)

11.5 10.2 4.9 4.98 4.88 5.00 5.2 8.6 8.1 7.7
50 25 14 10 10 14 23 85 50

(4.9)

11.4 11.1 5.0 5.00 4.91 5.00 5.0 8.2 7.9 7.2 6.9
50 25 14 10 10 15 22 34 85 50

TOP Fire Hyd. 53' Lt. 50. 67+52

9.9 9.1 8.1 5.0 4.99 4.94 4.93 5.1 7.5 7.6 6.4 5.5
50 47 23 14 10 10 15 20 27 31 50

(4.8)

(4.7)

8.8 7.7 8.0 4.9 4.94 4.93 4.9 4.8 6.6 6.7 7.9
50 31 21 15 10 10 14 19 27 50

(4.3)

8.5 7.4 6.9 4.6 4.46 4.44 4.39 4.2 6.0 7.6 7.0
50 28 19 15 10 10 15 19 32 50

(3.9)

7.3 6.2 7.3 7.1 4.2 4.02 3.93 4.04 4.0 8.8 8.8
50 33 20 21 15 10 10 14 23 50

3.4

5.5 5.9 6.6 6.2 3.4 3.43 3.37 3.51 3.8 8.6 8.0
50 34 31 20 14 10 10 15 24 50

6.9463 = 8.55 / 4.2 = F/Lin

(3.2)

5.7 4.4 6.1 5.7 3.3 3.23 3.16 3.25 3.3 7.8 8.5 8.0 3.8
50 34 31 19 15 10 10 14 19 23 31 24 57 W. Sh. Dr. Ave.

(3.0)

2.4 3.2 4.9 5.1 3.0 3.02 2.96 3.02 3.0 3.8 3.8
50 34 30 19 14 10 10 10 10 37 W. Sh. Dr. Ave.

TOP 2 Ave. 86.70 to

Sta.	+	π	-	Elev
		967.39		
70+15				58.6
70+50				59.1
+75				59.5
71+0				59.9
+50				60.9
72+0				62.0
B.M.	6.80	974.04	0.15	967.24
+50				63.2
73+0				64.7
+50				66.1
74+0				67.7
+50				69.3

LT E RT

Yard-

(8.8)

Hill } 7.2 74 82 87 8.85 8.80 8.90 8.5 8.6
 Dta. } 50 39 31 28 10 10 37- 50 = E. St. Dr. E. Ave.

(8.3)

no } 82 7.8 8.32 8.34 8.7 10.6 11.9
 Ditches } 50 32 10 10 24 31 50

(7.9)

7.9 83 Hill } 8.02 7.94 8.01 8.1 10.6 10.0 9.1 10.7
 50 39 Dta. } 10 10 17 22 31 43 50

(7.5)

9.7 84 } 7.50 7.46 7.54 7.8 9.9 9.9 8.9 6.4 8.8
 50 33 } 10 10 17 23 24 32 38 50

(6.5)

9.1 84 86 6.6 6.54 6.45 6.44 6.7 7.0 9.2 8.4 8.5 4.5 4.7
 50 29 19 15 10 10 16 22 28 30 37 44 50

(5.4)

9.1 7.5 8.0 7.9 5.5 5.45 5.39 5.45 5.5 7.8 7.7 4.3 0.8
 50 25 23 18 15 10 10 15 19 26 37 50

Top Fire Hyd. 37.5 Lt. Sta. 73+28

14.8 13.8 14.1 13.4 14.0 14.90 10.80 10.86 11.1 12.5 13.0 7.3 4.8
 50 27 24 20 15 10.0 10.8 10 15 19 24 33 50

(9.1)

12.8 11.5 9.5 9.44 9.39 9.45 9.7 11.1 11.1 7.5 5.2
 50 21 15 10 10 15 20 26 32 50

(8.0)

9.7 10.0 10.3 8.1 8.05 7.97 8.10 8.2 9.6 9.7 7.4 5.9
 50 30 22 15 10 10 15 22 29 32 50

(6.3)

8.5 8.2 8.4 6.4 6.4 6.33 6.46 6.5 8.0 8.3 5.1 3.2
 50 28 20 16 10 10 15 20 27 31 50

(7.8)

8.1 6.8 7.2 5.0 4.90 4.75 4.74 6.0 7.3 7.1 2.0 1.0
 50 30 19 16 10 10 14 18 20 25 31 50

Sta.	+	Σ	-	Elev
		974.04		
75+0				70.9
	8.80	981.35	1.49	972.55
+50				72.6
76				74.2
+50				75.8
77				77.5
	10.08	989.27	2.16	979.19
+50				79.2
78+0				80.8
+45				82.4
B.M.			6.36	982.91
B.M. + 53.3			6.62	989.65
+75				83.4
				982.65
79+0				84.8
+50				85.7
B.M.	9.09	996.08	2.28	986.99

4

E

12

(3.1)

54	45	52	47	36	3.21	3.13	3.18	3.3	49	4.8
50	39	30	20	16	10	10	15	19		50

(8.8)

170	137	120	92	892	880	896	92	125	127	118
50	29	20	4	10	10	10	15	19	22	50

(7.1)

160	148	107	104	80	724	711	725	74	52	105	106
50	32	24	19	16	10	10	10	15	21	35	50

(5.5)

112	97	84	61	564	552	551	59	76	80	86
50	32	20	15	10	10	10	15	20	34	50

76+50

(3.8)

49	5.5	6.1	60	39	3.96	3.23	3.88	44	56	5.5	3.2	3.7
50	34	30	19	14	10	0	10	15	19	28	31	50

(10.1)

13.8	131	105	117	115	102	1016	10.08	10.15	104	115	122	10.7	83	84
50	44	39	27	19	15	10	10	10	15	18	26	29	34	50

Co. Rd. "B" D.R.

(8.4)

Co. Rd. "B" 50	73	852	843	8.51	9.2	10.7	10.7	93	76	7.1
		10	10	10	16	21	25	30	33	50

(6.9)

6.9

68	68	98	93	7.9	7.1	6.94	6.87	96	70	9.2	9.2	4.3	4.1
50	46	42	34	30	16	700	700	100	18	21	24	33	50

Top Bolt & Pavement

78+60.0

(98.57) (B)

58	64	70	70	61	5.99	5.99	5.99	5.7	5.7	5.7
50	28	25	20	15	10	10	10	10	10	10

= 2. Shldr "B"

(4.5)

53	48	55	5.8	4.5	4.86	4.50	4.55	4.7	7.78	7.78	4.1	3.5
50	31	25	19	16	10	10	10	15	21	21	24	33

(3.5)

35	38	49	47	3.7	3.85	3.85	3.85	3.85	3.85	3.85	3.85	3.85	3.85
50	35	28	18	15	10	10	10	15	18	21	24	33	50

Top Fire Hyd. 36.5 41. 84. 197 47

Sta.	+	π	-	Elev.
		996.08		
80 to				87.3
+50				88.7
81				89.8
+50				90.9
82 to				91.5
	8.68	1000.74	4.02	992.06
+50				92.1
83				92.5
+50				92.6
+68				92.6
84 +				92.5
+35				92.4
+45				92.4

(8.7)

8.3	8.4	10.3	10.7	10.7	9.0	8.7	8.6	9.0	10.3	10.4	7.6	7.6
5.0	3.2	3.2	2.9	2.0	1.6	1.2	1.0	1.5	1.7	2.0	2.4	5.0

(7.4)

6.7	7.0	9.5	9.3	7.6	7.48	7.4	7.51	7.6	8.8	8.8	6.3	6.2
5.0	3.2	2.5	2.0	1.5	1.0		1.0	1.4	1.7	2.0	2.4	5.0

(6.3)

5.8	5.7	8.1	8.6	6.5	6.8	6.26	6.30	6.5	7.5	7.5	4.9	5.0
5.0	3.2	2.6	2.1	1.4	1.0		1.0	1.5	1.7	2.0	2.5	5.0

(5.2)

4.6	4.6	7.5	7.6	5.6	5.9	5.6	5.24	5.4	6.2	5.9	3.3	2.0
5.0	3.2	2.6	2.0	1.4	1.0		1.0	1.4	1.7	2.0	2.5	5.0

(4.6)

2.8	2.9	6.4	6.5	4.8	4.67	4.60	4.66	4.7	5.4	5.4	2.1	1.6	0.5
5.0	3.3	2.5	2.0	1.0	1.0		1.0	1.5	1.7	1.9	2.5	3.3	3.5
													4.0
													5.0

(8.7)

4.9	5.8	10.7	10.8	9.0	8.77	8.77	8.9	9.8	9.7	6.6	6.0	4.6
5.0	3.4	2.3	1.9	1.5	1.0	8.68	1.0	1.4	1.6	1.9	2.5	3.2
												3.9
												4.0
												5.0

(8.2)

3.3	4.1	9.9	10.2	9.5	8.25	8.25	8.2	9.1	8.8	6.2	5.1	5.1
5.0	3.2	2.3	1.8	1.4	1.0	8.20	1.0	1.4	1.7	2.1	2.4	3.6
												4.0
												5.0

(8.2)

4.0	3.3	9.9	9.9	8.2	8.21	8.22	8.4	9.0	8.9	5.7	4.7	3.5
5.0	3.3	2.3	1.8	1.5	1.0	8.16	1.0	1.4	1.9	2.5	3.6	5.0

(8.2)

6.8	6.5	7.4	10.0	9.8	8.3	8.22	8.22	8.3	9.0	8.4	5.6	4.6	4.6
5.0	4.0	2.7	2.2	1.8	1.4	8.17	1.0	1.4	1.7	2.0	2.0	3.8	5.0

(8.2)

5.5	4.6	5.3	9.3	9.1	8.4	8.37	8.31	8.4	9.3	8.8	5.4	4.7	4.3
5.0	3.8	2.7	2.1	1.8	1.5	8.22	1.0	1.5	1.8	2.1	2.7	3.7	5.0

(6.3)

5.4	5.4	6.1	9.3	9.3	8.8	8.41	8.31	8.1	9.0	9.0	5.7	4.6	4.4
5.0	3.7	2.7	2.0	1.8	1.6	1.0	8.31	1.0	1.6	1.7	2.0	2.7	5.0

(8.3)

10.2	9.0	8.43	8.33	8.1	9.0	9.0	3.7	4.6	4.2
5.0	2.1	1.0	1.0	1.6	1.7	2.0	2.7	3.6	5.0

Sta.	+	π	-	Elev
		1000.74		
84+78				92.2
+88				92.1
85				91.9
+50				91.2
86				90.4
+50			89.5	89.6
+11	5.18	993.40	12.52	988.22
+77				89.0
87				88.2
+50				86.8
BM	0.66	990.45	3.61	989.79
88				85.2
+50				83.3

Lt

E

Rt

(8.6)

$\frac{10.1}{50}$	$\frac{9.0}{27}$	$\frac{8.68}{10}$	8.59	$\frac{8.63}{10}$	$\frac{8.5}{15}$	$\frac{9.2}{17}$	$\frac{8.8}{20}$	$\frac{5.6}{26}$	$\frac{50.2}{41}$	$\frac{2.1}{44}$
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(8.7)

$\frac{6.0}{50}$	$\frac{5.3}{35}$	$\frac{7.0}{25}$	$\frac{9.5}{20}$	$\frac{9.8}{18}$	$\frac{8.8}{15}$	$\frac{8.88}{10}$	8.69	$\frac{8.76}{10}$	$\frac{8.5}{15}$	$\frac{9.2}{17}$	$\frac{8.8}{20}$	$\frac{5.6}{26}$	$\frac{50.2}{41}$	$\frac{2.1}{44}$
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(8.8)

$\frac{6.7}{50}$	$\frac{6.4}{24}$	$\frac{10.0}{19}$	$\frac{10.0}{17}$	$\frac{9.0}{15}$	8.92	$\frac{8.92}{10}$	8.82	$\frac{8.90}{10}$	$\frac{8.7}{14}$	$\frac{9.4}{16}$	$\frac{8.5}{21}$	$\frac{5.9}{26}$	$\frac{50.2}{42}$	$\frac{2.2}{50}$
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(9.5)

$\frac{7.5}{50}$	$\frac{7.3}{24}$	$\frac{10.4}{20}$	$\frac{10.5}{18}$	$\frac{9.6}{15}$	$\frac{9.67}{10}$	9.54	$\frac{9.60}{10}$	$\frac{9.2}{14}$	$\frac{10.2}{16}$	$\frac{10.0}{19}$	$\frac{8.8}{24}$	$\frac{7.1}{31}$	$\frac{5.5}{45}$
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(10.3)

$\frac{7.8}{50}$	$\frac{8.9}{25}$	$\frac{11.3}{21}$	$\frac{11.6}{18}$	$\frac{10.40}{15}$	$\frac{10.41}{10}$	$\frac{10.410.3}{10}$	$\frac{11.5}{14}$	$\frac{11.4}{18}$	$\frac{9.4}{20}$	$\frac{8.6}{32}$	$\frac{7.3}{45}$	$\frac{3.3}{50}$
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(11.1)

$\frac{9.5}{50}$	$\frac{9.3}{38}$	$\frac{10.6}{31}$	$\frac{10.8}{24}$	$\frac{12.6}{21}$	$\frac{12.9}{18}$	$\frac{11.6}{15}$	$\frac{11.24}{10}$	11.11	$\frac{11.22}{10}$	$\frac{11.2}{14}$	$\frac{12.5}{18}$	$\frac{12.6}{20}$	$\frac{10.2}{27}$	$\frac{9.2}{33}$
------------------	------------------	-------------------	-------------------	-------------------	-------------------	-------------------	--------------------	-------	--------------------	-------------------	-------------------	-------------------	-------------------	------------------

(4.4)

$\frac{2.1}{50}$	$\frac{3.2}{45}$	$\frac{3.3}{36}$	$\frac{4.2}{30}$	$\frac{4.2}{24}$	$\frac{5.8}{21}$	$\frac{5.6}{17}$	$\frac{4.7}{15}$	$\frac{4.51}{10}$	$\frac{4.57}{10}$	$\frac{3.5}{32}$	$\frac{2.3}{50}$	= st.
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(5.2)

$\frac{4.3}{50}$	$\frac{5.6}{46}$	$\frac{6.5}{24}$	$\frac{5.6}{20}$	$\frac{5.25}{14}$	$\frac{5.25}{10}$	$\frac{5.18}{10}$	$\frac{5.25}{10}$	$\frac{5.0}{27}$	$\frac{3.0}{45}$	$\frac{0.5}{50}$
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(6.6)

$\frac{7.0}{50}$	= st.	$\frac{5.7}{25}$	$\frac{5.65}{10}$	$\frac{6.7}{10}$	$\frac{6.9}{21}$	$\frac{6.4}{34}$	$\frac{5.6}{44}$	$\frac{3.3}{50}$
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Top Five Hyd 50' Lt St 87+78

$\frac{4.7}{50}$	$\frac{5.7}{45}$	$\frac{5.6}{40}$	$\frac{6.3}{35}$	$\frac{6.5}{20}$	$\frac{5.4}{15}$	$\frac{5.36}{10}$	$\frac{5.5}{10}$	$\frac{5.39}{15}$	$\frac{5.5}{17}$	$\frac{6.0}{32}$	$\frac{6.2}{36}$	$\frac{5.7}{50}$
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(7.1)

$\frac{7.3}{50}$	$\frac{7.3}{48}$	$\frac{8.1}{48}$	$\frac{8.0}{37}$	$\frac{9.1}{34}$	$\frac{9.0}{24}$	$\frac{8.1}{20}$	$\frac{7.2}{16}$	$\frac{7.19}{10}$	$\frac{7.12}{10}$	$\frac{7.25}{16}$	$\frac{7.2}{18}$	$\frac{7.8}{36}$	$\frac{7.4}{41}$	$\frac{7.9}{50}$
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Sta.	+	π	-	Elev.
		990.45		
8940				81.5
+50				79.5
T.P.	1.46	979.16	12.75	977.70
90400				77.7
+50				75.8
91400				73.9
+50				71.9
9240				70.0
T.P.	0.88	969.06	10.98	968.18
+50				68.2
9340				66.6
+50				65.2
9440				63.9

4.

8

RT.

(9.0)

104	104	115	114	123	111	9.2	9.10	9.00	9.10	8.9	9.6	102	98	103
90	46	38	34	28	23	16	10		10	16	18	35	48	50
50														

(11.0)

12.1	12.9	12.8	14.0	13.5	13.4	11.1	11.03	11.5	11.00	11.2	12.3	12.6	12.3
90	47	36	34	27	25	16	10		10	16	21	37	50

(15)

3.3	3.5	4.0	4.0	1.8	1.53	1.46	1.58	1.6	3.0	4.8	3.0
50	37	34	25	16	10		10	16	21	29	50

(34)

6.7	5.6	5.7	6.6	6.5	5.7	3.6	3.51	3.58	3.46	3.6	5.4	6.0	5.5	5.0
50	46	32	28	25	21	15	10		10	15	22	26	29	50

(5.3)

10.3	8.2	8.2	8.8	8.6	5.5	5.48	5.31	5.42	5.5	7.3	7.4	7.9	8.2
5	24	37	33	24	15	10		10	14	19	28	31	50

(7.2)

10.8	10.3	11.1	11.0	11.4	7.29	7.23	7.32	7.3	9.5	10.2	10.5
50	37	28	25	15	10		10	15	21	26	50

(9.1)

16.8	17.6	12.5	13.1	12.6	9.4	9.25	9.14	9.20	9.2	12.2	17.6	12.0	11.8
56	47	39	34	22	15	10		10	14	22	27	29	50

(0.9)

5.9	4.1	4.0	4.3	4.5	3.9	1.2	0.93	0.88	0.90	0.9	4.4	4.5	4.0	3.4
50	53	46	40	35	30	21	15	10		10	14	25	27	29
														50

(2.5)

7.5	5.6	5.5	5.8	4.6	2.6	2.57	2.48	2.54	2.5	6.0	6.0	5.4
54	43	38	24	18	14	10		10	15	24	34	50

(3.8)

8.4	6.8	6.8	6.8	7.0	5.9	4.6	3.99	3.8	3.81	3.7	6.4	7.2	6.8	7.0
55	48	45	40	33	23	16	10		10	14	21	26	33	50

(5.1)

7.2	7.2	7.5	7.7	7.0	5.6	5.27	5.13	5.11	5.0	7.8	8.1	7.7	7.1
50	46	37	26	20	15	10		10	14	25	33	35	50

St.	+	-	Elev.
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969.06

94+50

62.8

94+70

62.4

+90

95 61.7

+75

61.3

+68

B.M.

7.35

961.71

H.

L

R1.

(6.3)

80	80	86	87	80	66	643	676	621	63	83	85	80	7.80	74
50	37	33	28	21	16	13.9	148	17	23	32	33	40.5	54	50

(6.7)

87	87	81	7.2	7.03	6.67	681	69	9.2	8.2	7.6	8.05	7.6
50	40	25	18	15.8	18.1	22	29	32	35	44	21	50

8.00
51.35 Paul.

(7.3)

75	70	90	25	74	7.50	7.33
52	48	39	30	24	192	

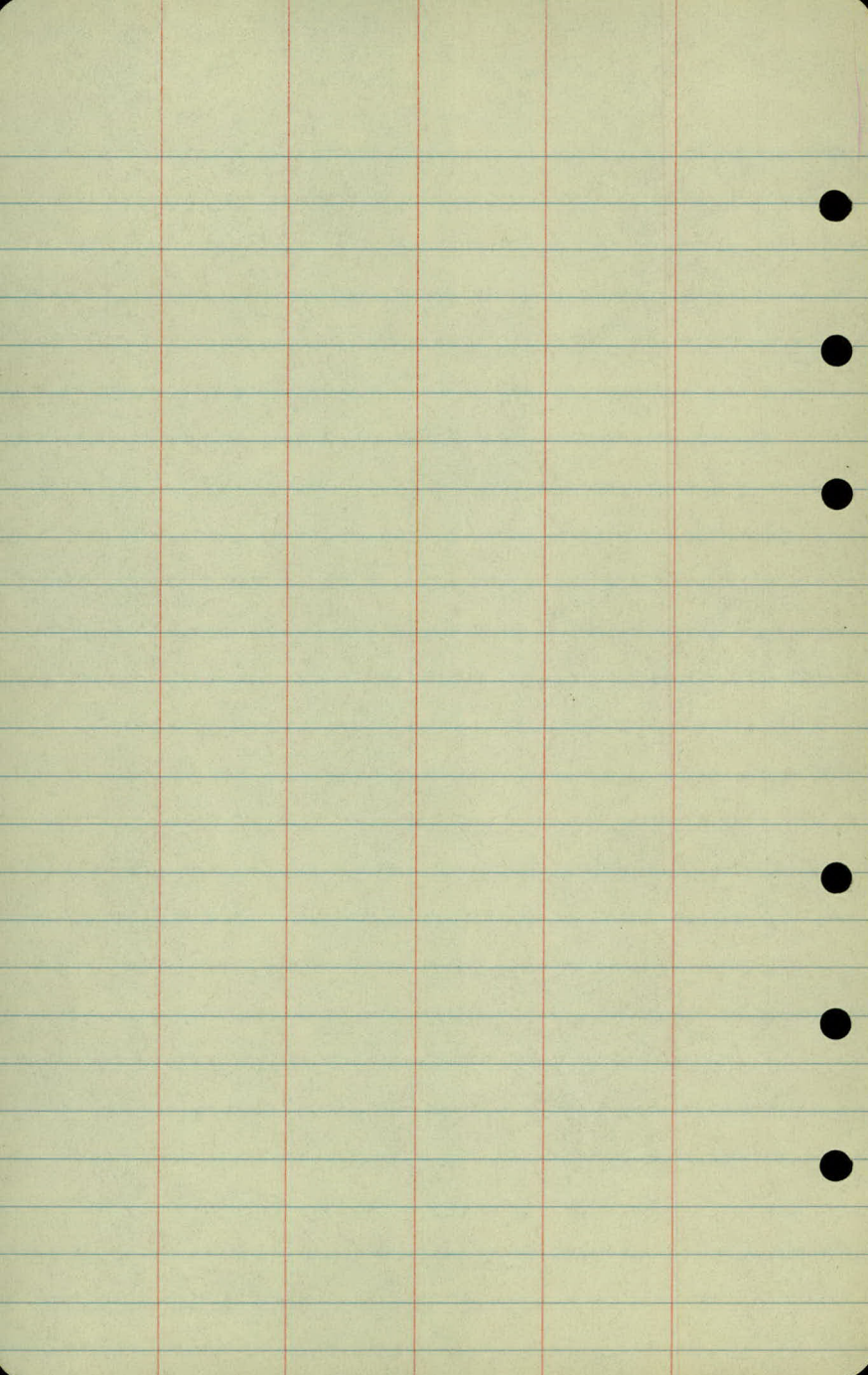
(7.8)

11.8	9.5	9.5	82	8.15	7.8
56	48	35	28	24.1	

9.33
50

Hyd. H-96+

5118
400
725
195
9



Sta.	+	-	Elev.
	4.95	991.95	987.00
120+89			83.7
121+20			84.6
121+66			85.2
122+0			85.6
+50			85.9
123			86.4
+50			86.8
124+0			87.1
+50			87.4

4. 2 124

825

 $\frac{83}{50}$

738

 $\frac{759}{28}$ $\frac{67}{50}$

(6.8)

 $\frac{8.08}{50}$ $\frac{6.76}{18}$ $\frac{6.84}{18}$ $\frac{6.0}{50}$

(6.4)

 $\frac{7.3}{50}$ $\frac{7.6}{28}$ $\frac{6.9}{23}$ $\frac{6.58}{16.2}$ $\frac{6.40}{13.4}$ $\frac{6.58}{13.4}$ $\frac{6.3}{29}$ $\frac{6.0}{50}$

(6.0)

 $\frac{6.5}{50}$ $\frac{7.1}{35}$ $\frac{7.2}{20}$ $\frac{6.1}{16}$ $\frac{6.12}{10}$ $\frac{6.02}{10}$ $\frac{6.10}{10}$ $\frac{6.2}{25}$ $\frac{6.0}{48}$ $\frac{2.4}{54}$

(5.6)

 $\frac{3.1}{50}$ $\frac{5.9}{41}$ $\frac{6.6}{24}$ $\frac{5.75}{10}$ $\frac{5.60}{10}$ $\frac{5.70}{10}$ $\frac{5.9}{28}$ $\frac{5.7}{48}$ $\frac{3.1}{55}$ 123+18 $\left\{ \begin{array}{l} 5.14 \\ 3.20 \end{array} \right.$ 139.0mb

(5.2)

 $\frac{2.9}{54}$ $\frac{5.7}{41}$ $\frac{6.0}{24}$ $\frac{5.30}{10}$ $\frac{5.20}{10}$ $\frac{5.30}{10}$ $\frac{5.4}{32}$ $\frac{4.90}{32}$ $\frac{5.0}{48}$ $\frac{2.0}{53}$ 173 + 168 $\left\{ \begin{array}{l} 4.74 \\ 3.20 \end{array} \right.$ 199.0mb

(4.8)

 $\frac{5.5}{50}$ $\frac{5.4}{26}$ $\frac{4.87}{10}$ $\frac{4.83}{10}$ $\frac{4.95}{10}$ $\frac{5.2}{26}$ $\frac{5.4}{34}$ $\frac{4.8}{36}$ $\frac{4.0}{49}$ $\frac{1.5}{56}$

(4.5)

 $\frac{4.6}{50}$ $\frac{4.6}{23}$ $\frac{4.9}{20}$ $\frac{4.60}{10}$ $\frac{4.52}{10}$ $\frac{4.60}{10}$ $\frac{4.8}{10}$ $\frac{4.61}{24}$ $\frac{6.4}{28}$ $\frac{5.2}{34}$ $\frac{5.2}{35}$ $\frac{4.6}{47}$ $\frac{4.0}{54}$ $\frac{5.9}{54}$

Sta.	+	±	-	Elev.
125+0		991.95		87.6
+50				87.5
B.M.	1.62	990.88	2.69	989.26
126+0				87.2
+50				86.9
127+0				86.4
+50				86.1
128+0				85.8
+50				85.4
129+0				85.4
128+59				
128+61				
129+01				
129+40				

4.4 4.4 4.4
 4.4 4.8 5.5 5.0 4.52 4.36 4.54 4.7 5.4 5.8 4.8 4.3 3.1 0.4
 5.0 3.8 3.2 2.9 7.0 10 10 14 18 24 28 37 50 58

4.5
 5.0 5.5 4.9 4.62 4.50 4.57 4.7 5.7 5.2 4.6 3.9 2.8
 5.0 2.5 1.6 1.0 10 10 19 22 33 35 50 54

Top Fire Hyd. 3.4 4.4 4.6 1.25 + 8.1

3.9 4.8 4.8 4.0 3.75 3.65 3.75 3.9 5.0 5.3 5.6 4.7 3.9 3.7 1.0
 5.0 3.7 2.0 1.5 1.0 3.7 10 15 19 23 28 33 26 48 50

4.1
 5.8 5.2 5.8 5.9 4.1 4.13 4.02 4.13 4.3 5.9 5.9 5.0 5.0
 5.0 3.9 3.4 2.0 1.5 1.0 10 15 21 22 35 50

4.4
 6.9 6.5 6.8 7.8 7.3 4.5 4.55 4.44 4.52 4.8 6.4 6.5 5.9 5.5
 5.0 3.8 2.8 2.6 2.1 1.4 1.0 10 15 19 22 34 50

4.7
 2.3 7.1 7.6 7.2 4.9 4.89 4.74 4.86 4.9 7.1 7.2 6.5 6.4 7.2
 5.0 2.9 2.4 2.0 1.4 1.0 10 14 20 31 35 44 50

5.1
 10.0 7.7 7.4 7.9 7.2 5.2 5.35 5.12 5.21 5.4 8.0 7.9 7.4 7.3 9.8
 5.3 4.7 3.7 3.4 2.8 1.4 1.0 10 14 20 32 34 46 54

5.5
 12.1 9.7 9.2 8.2 5.5 5.60 5.48 5.56 7.4 9.2 10.0
 5.4 4.9 3.5 2.2 1.4 1.0 10 31 42 56

5.5
 12.3 9.3 9.5 8.6 6.0 5.72 5.52 5.61 6.7 7.8 9.3
 5.5 4.5 3.6 2.4 1.6 1.0 10 18 24 53

$$\frac{10.42}{5.2} = \text{Fl. Co. 11.24"}$$

$$\frac{10.16}{6.6} = \text{Fl. Co. 18"}$$

$$\frac{10.4}{5.8}$$

$$\frac{12.06}{4.9} = \text{Fl. Line 24"}$$

990.88

Sta.	+	T	-	Elev.
	7.77	993.02	543	985.25
129+50				85.3

Int. of Henry St. N.E + 10th Ave. N.E

120+0				85.6
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+50				86.1
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131				86.6
-----	--	--	--	------

+50				87.1
-----	--	--	--	------

132				87.8
-----	--	--	--	------

+50				88.6
-----	--	--	--	------

133				89.4
-----	--	--	--	------

+50				90.1
-----	--	--	--	------

T.P.	9.48	1000.67	1.83	991.19
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134				91.2
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21.

2

21

(7.8)

$$2st = \frac{198}{50} \quad \frac{100}{32} \quad \frac{28}{19} \quad \frac{80}{13} \quad \frac{792}{10} \quad \frac{777}{10} \quad \frac{780}{10} \quad \frac{80}{14} \quad \frac{116}{22} \quad \frac{11.1}{50}$$

18.0

Henry Grade South - 1st St Rd
10th Ave in Level east.

(7.4)

$$\frac{114}{50} \quad \frac{110}{44} \quad \frac{12.5}{42} \quad \frac{110}{38} \quad \frac{106.72}{20} \quad \frac{75.37}{10} \quad \frac{743}{10} \quad \frac{7.8}{14} \quad \frac{10.7}{21} \quad \frac{11.4}{50}$$

(6.9)

$$\frac{114}{50} \quad \frac{105}{48} \quad \frac{114}{34} \quad \frac{116}{22} \quad \frac{7.3}{14} \quad \frac{7.01}{10} \quad \frac{6.90}{10} \quad \frac{6.93}{10} \quad \frac{70}{14} \quad \frac{10.1}{19} \quad \frac{7.6}{47} \quad \frac{11.1}{50}$$

(6.4)

$$\frac{132}{56} \quad \frac{96}{46} \quad \frac{96}{36} \quad \frac{109}{33} \quad \frac{78}{19} \quad \frac{66}{14} \quad \frac{68.6}{10} \quad \frac{6.42}{10} \quad \frac{6.6}{10} \quad \frac{9.3}{21} \quad \frac{9.4}{34} \quad \frac{8.6}{20} \quad \frac{9.3}{48} \quad \frac{9.8}{52}$$

(5.9)

$$\frac{125}{56} \quad \frac{8.4}{48} \quad \frac{8.4}{38} \quad \frac{9.9}{34} \quad \frac{9.5}{21} \quad \frac{60}{14} \quad \frac{602}{10} \quad \frac{5.91}{10} \quad \frac{6.0}{10} \quad \frac{6.1}{14} \quad \frac{8.2}{19} \quad \frac{8.9}{27} \quad \frac{7.9}{45} \quad \frac{9.7}{53} \quad \frac{9.5}{60}$$

(5.2)

$$\frac{108}{55} \quad \frac{7.9}{47} \quad \frac{7.9}{35} \quad \frac{9.2}{34} \quad \frac{80}{19} \quad \frac{5.5}{14} \quad \frac{5.28}{10} \quad \frac{5.28}{10} \quad \frac{5.32}{10} \quad \frac{5.4}{14} \quad \frac{8.1}{21} \quad \frac{8.0}{31} \quad \frac{9.0}{32} \quad \frac{7.5}{34} \quad \frac{7.5}{50}$$

(4.4)

$$\frac{9.7}{54} \quad \frac{7.6}{50} \quad \frac{7.3}{36} \quad \frac{8.2}{33} \quad \frac{8.3}{21} \quad \frac{4.7}{14} \quad \frac{4.56}{10} \quad \frac{4.43}{10} \quad \frac{4.46}{10} \quad \frac{4.5}{16} \quad \frac{7.2}{20} \quad \frac{7.0}{34} \quad \frac{6.3}{37} \quad \frac{5.9}{50}$$

(3.6)

$$\frac{9.1}{54} \quad \frac{7.1}{48} \quad \frac{6.4}{42} \quad \frac{6.7}{36} \quad \frac{7.8}{31} \quad \frac{7.7}{23} \quad \frac{3.5}{16} \quad \frac{3.76}{10} \quad \frac{3.6}{10} \quad \frac{3.66}{10} \quad \frac{3.5}{16} \quad \frac{6.4}{21} \quad \frac{5.5}{29} \quad \frac{5.6}{50}$$

(2.9)

$$\frac{8.0}{56} \quad \frac{6.4}{50} \quad \frac{6.0}{45} \quad \frac{5.8}{22} \quad \frac{2.9}{17} \quad \frac{3.05}{10} \quad \frac{2.91}{10} \quad \frac{2.93}{10} \quad \frac{3.0}{16} \quad \frac{5.1}{21} \quad \frac{6.3}{34} \quad \frac{6.2}{50}$$

(9.5)

$$\frac{152}{54} \quad \frac{12.4}{46} \quad \frac{12.2}{38} \quad \frac{130}{34} \quad \frac{12.9}{23} \quad \frac{9.8}{17} \quad \frac{9.58}{10} \quad \frac{9.48}{10} \quad \frac{9.53}{10} \quad \frac{9.5}{16} \quad \frac{12.4}{22} \quad \frac{12.8}{50}$$

Sta	+	π	-	Elev.
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100067

134+50

92.3

135+0

93.6

+40

94.4

136+0

95.6

+50

95.7

137

96.4

B.M.

1.01

999.66

T.P.

1.97

999.75
~~1001.63~~

2.89

997.78

B.M.

8.00

991.75
~~993.63~~

L E R

(8.4)

143	124	114	124	115	85	88	83	85	114	113	116
56	51	38	32	22	17	10	16	2	36	53	

(7.1)

125	103	101	107	69	72	71	71	72	95	99
56	48	34	25	17	10	10	10	16	23	50

(6.3)

107	95	95	93	66	65	63	61	60	60	
54	49	33	24	19	10	10	10	20	50	= End grading Right

(5.1)

72	76	83	82	54	52	56	51	47
50	31	28	24	18	14	10	10	10

(4.2)

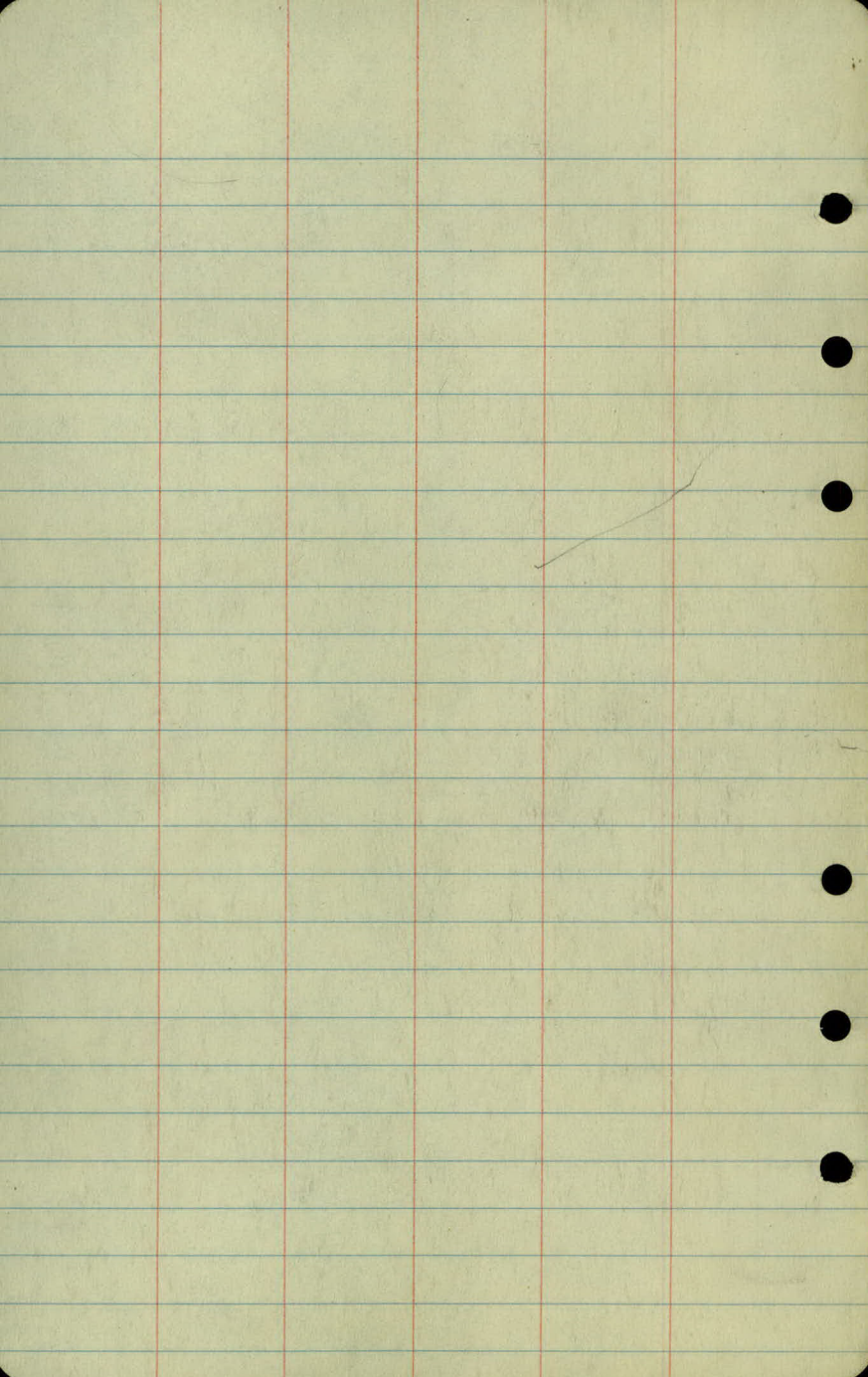
56	56	67	66	47	46	50	41	36
50	44	36	26	22	14	10	10	10

(3.4)

44	46	57	40	39	49	38	27
50	37	25	21	14	14	10	10

Top Conc. Base of Iron flag Pole Rd of Curve @ E. Co. Lk

Top W. end Culvert near Drive (991.46 - 4.10 100 + 96) Corn



No. St. Paul Rd.

4-25-38

Plans in Hand
M.W.C.
A.L.B.
X

57+13	R	Rem + Rep.	
57+96	R	" "	X
65+24	L	Ext. 10' L Ext. 10' R	X
67+62	R	Rem + Rep.	
67+93	L	No Culv. Req.	
70+38	R	OK. Leave	
76+14	R	Pl. 15" x 20' C.M.	X
78+84	R	Rem + Rep.	
78+56	L	O.K. Leave	
80+45	L	Inp. 18" x 5' C.M. Rem + Rep	
80+70	L	Inp. 15" x 20' C.M. " "	
81+25	R	Inp. 18" x 4' C.M. " "	
81+87	R	Rem. Pl. 12" x 5' C.M.	
82+26	L	Rem + Rep.	
84+45	R	Rem. No Culv. Req.	
84+63	L	" " " "	
85+40	R	Pl. 12" x 6' C.M.	
86+13	L	Rem + Rep.	
86+86	R	Inp. 15" x 48' C.M. Rem + Rep.	
87+32	L	Rem + Rep.	
88+65	L	" "	
89+44	R	Inp. Water Tank - Rem + Pl. 12" x 20' C.M.	
89+77	L	Rem + Rep.	
90+66	R	" "	
90+25	L	Rem. - No Culv. Req.	
91+37	L	Rem + Rep.	

92+33 R- Rem + Rep.

92+78 R- " "

93+62 L- " "

94+63 L- " " Ext 12"X6'C.M.

94+15 R- Pl. 12"X6'C.M.

95+35 L

95+15 R } O.K. Leave Pipes as Shown

95+15 R

95+60 L

X Denotes Work Already Done

1

North St. Paul Road.

Sta. 74+50 to 75+00

Special Section

dated 5/10/38

Walk Grade

Sta.	+	x	-	Elev.	Lt.	Rt.
B.M.				987.91		
B.M.	6.21	993.40		986.99		
79+50					85.7	85.7
80+00					87.1	87.1
+50					88.5	88.5
81+00					89.9	89.9
T.P.	9.41	1000.31	2.31	990.89		
+50					91.3	91.3
82+00					92.7	92.7
✓ +50					93.5	93.5
83+00					93.7	93.7

£

Rt.

Lt. Rt.

Top of bolt £ of Brement Sts. 78+60

Top of Hyd. 37' Lt. of Sts. 79+47

7.5	7.5		$\frac{B.Tops}{41 \quad 35}$	$\frac{B.T.}{35 \quad 41. out}$
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6.1	6.1		$\frac{5.1}{C1.0} \quad \frac{B.T.}{24.5}$ 43.0	$\frac{4.3}{C1.8} \quad \frac{B.T.}{44.6}$
-----	-----	--	--	--

4.7	4.7	42	$\frac{4.2}{C0.5} \quad \frac{B.T.}{24.5}$ 42.0	$\frac{3.1}{C1.6} \quad \frac{B.T.}{44.2}$
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3.3	3.3	41.5	$\frac{2.7}{C0.6} \quad \frac{B.T.}{24.5}$ 42.2	$\frac{2.3}{C1.0} \quad \frac{B.T.}{43.0}$
-----	-----	------	--	--

9.0	9.0	41.5	$\frac{8.2}{C0.8} \quad \frac{B.T.}{24.5}$ 42.4	$\frac{6.4}{C2.6} \quad \frac{B.T.}{46.2}$
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7.6	7.6	42	$\frac{7.6}{C0.6} \quad \frac{B.T.}{24.5}$ 42.4	$\frac{3.8}{C3.8} \quad \frac{B.T.}{48.6}$
-----	-----	----	--	--

6.8	6.8	41.5	$\frac{4.7}{C2.1} \quad \frac{B.T.}{24.5}$ 45.2	$\frac{3.7}{C3.1} \quad \frac{B.T.}{47.4}$
-----	-----	------	--	--

6.6	6.6	48	$\frac{2.7}{C3.9} \quad \frac{B.T.}{24.5}$ 48.8	$\frac{2.7}{C3.9} \quad \frac{B.T.}{48.8}$
-----	-----	----	--	--

Tide Walk
Grade.

Sta.	+	X	-	Elev.	Lt.	Rt.
		1000.31				
83+50					93.9	93.9
+68						94.0
84+00					94.2	94.2
+35					93.7	93.8
T.P.		282 999.11	4.02	996.29		
+45					93.5	93.7
+57						93.6
+78					93.0	93.3
+88					92.9	93.1
85+00					92.7	93.0
+50					91.9	92.4

Lt.		Rt.		Lt.		Rt.	
6.4	6.4	47	$\begin{array}{r} 2.9 \\ 3.5 \\ \hline 48.0 \end{array}$	BT 24.5		$\begin{array}{r} 24 \\ 4.0 \\ \hline 49.0 \end{array}$	47
6.3	6.3	41.5	$\begin{array}{r} BT \\ 71+35 \\ \hline \end{array}$			$\begin{array}{r} 4.2 \\ 0.21 \\ \hline 45.7 \end{array}$	46
6.1	6.1	43.5	$\begin{array}{r} 4.5 \\ 0.19 \\ \hline 44.7 \end{array}$			$\begin{array}{r} 3.9 \\ 0.22 \\ \hline 45.4 \end{array}$	45
6.6	6.5	44	$\begin{array}{r} 3.3 \\ 0.13 \\ \hline 43.6 \end{array}$			$\begin{array}{r} 3.8 \\ 0.27 \\ \hline 46.4 \end{array}$	46
Nail in T.P.							46
	5.5					$\begin{array}{r} 1.0 \\ 0.45 \\ \hline 50 \end{array}$	
	5.8						50
6.7	6.0	45.5	$\begin{array}{r} 4.0 \\ 0.22 \\ \hline 45.4 \end{array}$			$\begin{array}{r} 0.8 \\ 0.52 \\ \hline 50 \end{array}$	50
6.4	6.1	43.5	$\begin{array}{r} 4.0 \\ 0.24 \\ \hline 45.8 \end{array}$			$\begin{array}{r} 0.6 \\ 0.55 \\ \hline 50 \end{array}$	50
7.2	6.7	43.5	$\begin{array}{r} 5.9 \\ 0.13 \\ \hline 43.6 \end{array}$			$\begin{array}{r} 3.2 \\ 0.35 \\ \hline 48.0 \end{array}$	50

Side walk
Grade.

Sta.	+	π 999.11	-	Elev.	Lt.	Rt.
86+00					91.2	91.8
+50					90.4	91.2
+77					90.0	90.9
87+00					89.7	90.6
+50					87.4	88.3
B.M.	1.28	991.07	9.34	989.79		
88+00					85.1	85.9
+50					82.8	83.6
89+00					80.5	81.2

Grade Rod. Lt. $\emptyset$ Rt. 4

Lt.	Rt.						
7.9	7.3	43.5	$\frac{6.2}{6.17}$ 44.4		$\frac{5.5}{6.18}$ 44.6	46.5	
8.7	7.9	43.0	$\frac{7.9}{6.08}$ 44.6	$\frac{8.8}{8.7}$ 35	$\frac{8.0}{8.7}$ 35	$\frac{7.1}{6.0.8}$ 47.6	47
9.1		43	$\frac{5.1}{8.7}$ 41	$\frac{8.2}{8.7}$ 35			
9.4	8.5	42.5	$\frac{10.2}{6.08}$ 42.4	$\frac{9.4}{8.7}$ 41	$\frac{9.5}{8.7}$ 35	slope set slope up to 50' out 41 No Grade	
11.7	10.8				$\frac{10.8}{8.7}$ 41	slope up to 50'	50.

Top of Hydrant 50' Lt. of Sta. 87+78

6.0	5.2	43	$\frac{6.0}{8.7}$ 41	$\frac{5.2}{8.7}$ 41	$\frac{6.3}{8.11}$ 43.2	43.	
8.3	7.5	42	$\frac{8.9}{6.06}$ 42.2	$\frac{8.3}{8.7}$ 41	$\frac{9.2}{8.7}$ 24.1	$\frac{7.5}{8.7}$ 41	$\frac{8.0}{6.0.5}$ 44
10.6	9.9	42	$\frac{11.5}{6.06}$ 42.2	$\frac{10.6}{8.7}$ 41	$\frac{12.1}{8.7}$ 27.3	$\frac{9.9}{8.7}$ 41	$\frac{10.6}{6.0.7}$ 42.4

Sidewalk
Grade.

Sta.	+ K - Elev.	Lt.	Rt.
	991.07		
89+50		78.2	78.9
T.P.	2.55 980.19 13.43 977.64		
90+00		75.9	76.5
+50		73.6	74.4
T.P.	4.61 974.08 10.77 969.47		
91+00		71.3	72.3
+50		69.0	70.2
92+00		66.7	68.1
+50		65.3	66.0
93+00		63.9	63.9

Lt.

E

Rt.

Lt.

Rt.

P. 11.0

12.7

12.7

$$\begin{array}{r} 13.5 \\ 10.6 \ 12.9 \\ 42 \ 46 \ 41 \\ \hline 41 \end{array}$$

$$\begin{array}{r} 14.2 \\ 12.5 \\ \hline 27.8 \end{array}$$

$$\begin{array}{r} 12.2 \\ 8.1 \\ \hline 41 \end{array}$$

$$\begin{array}{r} 12.8 \\ 10.6 \\ \hline 42.2 \end{array}$$

43

P. 2.0

4.3

3.7

41.5

$$\begin{array}{r} 50 \ 43 \\ 40 \ 41 \\ \hline 41 \end{array}$$

$$\begin{array}{r} 5.2 \\ 12.6 \\ \hline 27.8 \end{array}$$

$$\begin{array}{r} 3.7 \\ 8.1 \\ \hline 41 \end{array}$$

41.5

P. 4.5

6.6

5.8

41.5

$$\begin{array}{r} 8.1 \\ 6.6 \\ \hline 41 \end{array}$$

$$\begin{array}{r} 2.2 \\ 12.7 \\ \hline 28.1 \end{array}$$

$$\begin{array}{r} 6.8 \\ 12.3 \\ \hline 26.9 \end{array}$$

$$\begin{array}{r} 5.8 \\ 8.1 \\ \hline 41 \end{array}$$

$$\begin{array}{r} 6.3 \\ 10.5 \\ \hline 42.9 \end{array}$$

42.0

rail stump Rt.

P. 0.4

7.8

1.8

42.0

$$\begin{array}{r} 2.8 \\ 8.1 \\ \hline 41 \end{array}$$

$$\begin{array}{r} 3.6 \\ 13.2 \\ \hline 29.6 \end{array}$$

$$\begin{array}{r} 2.3 \\ 11.9 \\ \hline 25.7 \end{array}$$

$$\begin{array}{r} 1.8 \\ 8.1 \\ \hline 41 \end{array}$$

$$\begin{array}{r} 3.0 \\ 11.2 \\ \hline 43.4 \end{array}$$

43.5

P. 2.2

5.1

3.9

42

$$\begin{array}{r} 8.1 \\ 5.1 \\ \hline 41 \end{array}$$

$$\begin{array}{r} 5.6 \\ 12.4 \\ \hline 30.2 \end{array}$$

$$\begin{array}{r} 5.0 \\ 12.8 \\ \hline 28.4 \end{array}$$

$$\begin{array}{r} 3.9 \\ 8.1 \\ \hline 41 \end{array}$$

$$\begin{array}{r} 5.1 \\ 11.2 \\ \hline 43.4 \end{array}$$

44

P. 4.1

7.4

6.0

41.5

$$\begin{array}{r} 8.1 \\ 2.4 \\ \hline 41 \end{array}$$

$$\begin{array}{r} 2.8 \\ 13.8 \\ \hline 31.4 \end{array}$$

$$\begin{array}{r} 2.0 \\ 12.9 \\ \hline 28.7 \end{array}$$

$$\begin{array}{r} 8.1 \\ 6.0 \\ \hline 41 \end{array}$$

$$\begin{array}{r} 6.8 \\ 10.8 \\ \hline 42.6 \end{array}$$

43

P. 6.0

8.8

8.1

42

$$\begin{array}{r} 8.8 \\ 8.1 \\ \hline 41 \end{array}$$

$$\begin{array}{r} 5.6 \\ 13.6 \\ \hline 30.8 \end{array}$$

$$\begin{array}{r} 8.9 \\ 12.9 \\ \hline 28.7 \end{array}$$

$$\begin{array}{r} 8.1 \\ 8.1 \\ \hline 41 \end{array}$$

$$\begin{array}{r} 8.7 \\ 10.6 \\ \hline 42.2 \end{array}$$

42

P. 7.6

10.2

10.2

42

$$\begin{array}{r} 10.2 \\ 8.1 \\ \hline 41 \end{array}$$

$$\begin{array}{r} 11.0 \\ 13.4 \\ \hline 30.2 \end{array}$$

$$\begin{array}{r} 10.8 \\ 13.2 \\ \hline 29.6 \end{array}$$

$$\begin{array}{r} 10.2 \\ 8.1 \\ \hline 41 \end{array}$$

42

Sta.	+	X	-	Elev.	Side walk Grade.	
					Lt.	Rt.

974.08

93+50

63.2 63.2

94+00

62.5 62.5

+50

61.8 61.8

+70

61.5 61.5

95+00

61.1

B.M. 17.35 974.08 17.35 961.73

T.P. 10.69 984.38 0.39 973.69

T.P. 10.33 983.87 0.84 983.54

B.M.

4.06 989.81

OK
989.79

Grade Rod.

Lt.

2

Rt.

6

Lt. Rt.

P. 8.8

B.T.

10.9 10.9

43 $\frac{11.9}{F. 8.8}$ $\frac{10.9}{B.T.}$ $\frac{11.9}{F. 8.8}$
 $\frac{43}{41}$ $\frac{41}{41}$ $\frac{27.4}{27.4}$

$\frac{12.0}{F. 8.8}$ $\frac{10.9}{41}$ $\frac{11.9}{F. 8.8}$
 $\frac{29.6}{29.6}$ $\frac{41}{41}$ $\frac{43.1}{43}$

43.1

P. 10.1

B.T.

11.6 11.6

43 $\frac{12.5}{F. 10.1}$ $\frac{11.6}{B.T.}$ $\frac{12.5}{F. 10.1}$
 $\frac{43}{41}$ $\frac{41}{41}$ $\frac{27.5}{27.5}$

$\frac{13.1}{F. 10.1}$ $\frac{11.6}{41}$ $\frac{12.5}{F. 10.1}$
 $\frac{29.0}{29.0}$ $\frac{41}{41}$ $\frac{44.6}{44.6}$

43

P. 11.3

12.3 12.3

42.5 $\frac{13.4}{F. 11.3}$ $\frac{12.3}{B.T.}$ $\frac{13.4}{F. 11.3}$
 $\frac{42.5}{41}$ $\frac{41}{41}$ $\frac{26.4}{26.4}$

$\frac{13.6}{F. 11.3}$ $\frac{12.3}{B.T.}$
 $\frac{26.9}{26.9}$ $\frac{41}{41}$

42.5

12.6 12.6

43 $\frac{12.6}{B.T.}$ $\frac{12.7}{B.T.}$
 $\frac{41}{41}$ $\frac{35}{35}$

$\frac{12.7}{B.T.}$ $\frac{12.6}{B.T.}$
 $\frac{35}{35}$ $\frac{41}{41}$

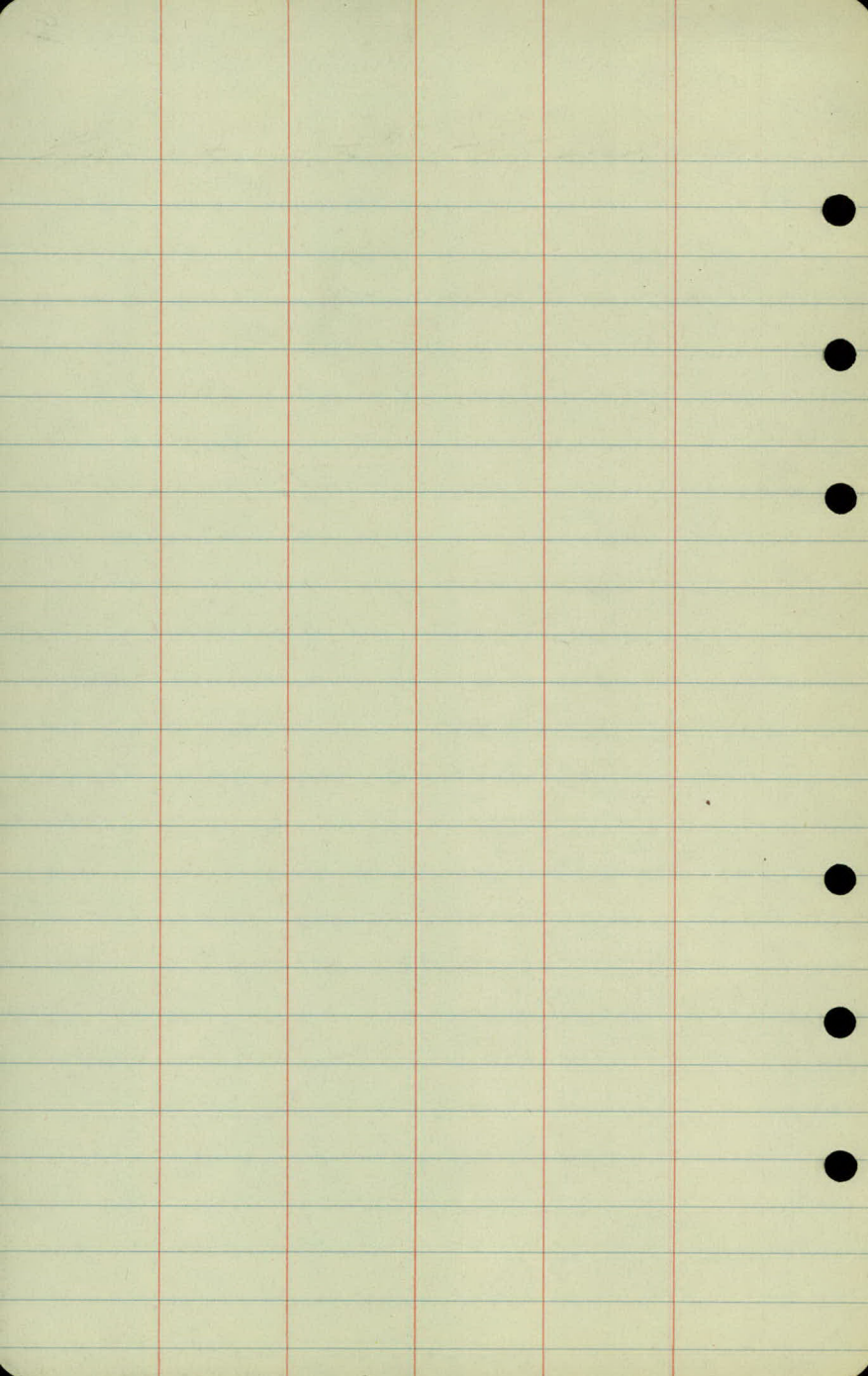
42

13.0

43 $\frac{B.T.}{13.0}$ $\frac{B.T.}{13.1}$
 $\frac{41}{41}$ $\frac{35}{35}$

Top Hydrant @ Penn Ave.

Top of Hyd. 50' Lt. of Sts. 87+78



1

North St. Paul Road.

Both Sides Now
Widen North side only
from Sta. 53+75 to 87+00 as
per plan dated October 1937.
using permanent as grade.

Grade
Rod.

Stb.

54 1.3

+50 2.8

55 4.4

+50 6.1

56 7.7

+50 9.3

57 11.0

+40 1.9

+78 3.2

58 3.6 5.1

+50 5.2 6.7

59 6.9 8.4

21.

21

$$\begin{array}{r} 41 \\ F28 \\ \hline 28.4 \end{array}$$

$$\begin{array}{r} 28 \\ F5.1 \\ \hline 35.3 \end{array}$$

$$\begin{array}{r} 9.9 \\ F5.5 \\ \hline 26.5 \end{array}$$

$$\begin{array}{r} 10.8 \\ F4.8 \\ \hline 34.4 \end{array}$$

$$\begin{array}{r} 11.3 \\ F36 \\ \hline 30.5 \end{array}$$

$$\begin{array}{r} 11.5 \\ F2.2 \\ \hline 26.6 \end{array}$$

$$\begin{array}{r} 12.9 \\ F1.9 \\ \hline 28.9 \end{array}$$

$$\begin{array}{r} 38 \\ F1.9 \\ \hline 28.7 \end{array}$$

$$\begin{array}{r} 5.6 \\ F2.6 \\ \hline 29.2 \end{array}$$

$$\begin{array}{r} 4.8 \\ D.C. 0.3 \\ \hline 29.1 \end{array}$$

$$\begin{array}{r} 3.8 \\ D.C. 2.9 \\ \hline 34.3 \end{array}$$

$$\begin{array}{r} 6.2 \\ D.C. 2.2 \\ \hline 32.9 \end{array}$$

Grade
Rod.

Lt.

575.

5950

8.8

113
F2.5
270

60

10.4

12.5
F2.1
26.3

+50

3.0

5.7
F2.2
28.1

61

4.2

7.7
F3.5
30.3

+50

5.2

8.4
F3.2
29.6

62

5.8

7.4
F1.6
14.8

+50

6.4

8.4
F2.0
26.0

63

6.8

9.5
F2.7
28.1

+50

3.8

6.5
F2.7
28.1

64

4.3

6.9
F2.5
27.8

+50

4.7

7.2
F2.0
27.5

65

5.1

8.8
F3.7
31.1

+30

5.2

11.2
F6.0
38.0

4.

Grade
Rod.

56.

65+50 5.2

9.9
F4.7
34.1

66 5.3

11.0
F5.7
37.1

+50 5.3

11.1
F5.8
37.4

67 5.2

11.5
F6.3
38.9

+50

68 5.7

8.4
F2.7
28.1

+50 5.3

8.6
F3.3
29.9

69 4.8

8.0
F3.2
29.6

+50 4.2

7.4
F3.2
29.6

+82 3.9

6.3
F2.4
27.2

70

+50

71

Grade

LX

Sta

Rod

71+24

6.9

$$\begin{array}{r} 8.4 \\ F1.5 \\ \hline 24.5 \end{array}$$

+50

6.3

$$\begin{array}{r} 8.3 \\ F2.0 \\ \hline 26.0 \end{array}$$

72

5.3

$$\begin{array}{r} 7.5 \\ F2.2 \\ \hline 26.6 \end{array}$$

+50

4.0

$$\begin{array}{r} 6.7 \\ F2.7 \\ \hline 28.1 \end{array}$$

73

2.6

$$\begin{array}{r} 4.7 \\ F2.1 \\ \hline 26.3 \end{array}$$

+50

1.2

$$\begin{array}{r} 3.2 \\ F2.0 \\ \hline 26.0 \end{array}$$

74

11.9

$$\begin{array}{r} 13.7 \\ F1.8 \\ \hline 25.4 \end{array}$$

+50

10.4

25.4

$$\begin{array}{r} 12.3 \\ F1.5 \\ \hline 20 \end{array}$$

75

5.7

$$\begin{array}{r} 10.3 \\ F4.6 \\ \hline 24.5 \end{array}$$

+50

7.1

$$\begin{array}{r} 14.6 \\ F7.5 \\ \hline 42.1 \end{array}$$

76

5.4

$$\begin{array}{r} 14.2 \\ F5.8 \\ \hline 46.4 \end{array}$$

+50

3.8

$$\begin{array}{r} 7.5 \\ F3.7 \\ \hline 31.1 \end{array}$$

5to

Grade
Rod.28.5.
1.5 ditch
4 to 1 Back
3 to 1 Fill

Bt.

4

54

2.5

$$\begin{array}{r} 8.4 \\ \hline F. 5.9 \\ \hline 37.7 \end{array}$$

+50

4.1

$$\begin{array}{r} 10.5 \\ \hline F. 6.4 \\ \hline 39.2 \end{array}$$

55

5.6

$$\begin{array}{r} 12.0 \\ \hline F. 6.4 \\ \hline 39.2 \end{array}$$

+50

7.3

$$\begin{array}{r} 12.9 \\ \hline F. 5.6 \\ \hline 36.8 \end{array}$$

56

8.9

$$\begin{array}{r} 13.1 \\ \hline F. 4.2 \\ \hline 37.6 \end{array}$$

+50

10.1

$$\begin{array}{r} 12.9 \\ \hline F. 2.4 \\ \hline 29.2 \end{array}$$

57

12.3 14.0

$$\begin{array}{r} 13.6 \\ \hline 17.0.4 \\ \hline 29.7 \end{array}$$

$$\begin{array}{r} 13.8 \\ \hline F. 1.5 \\ \hline 24.5 \end{array}$$

+40

13.5 15.0

$$\begin{array}{r} 14.5 \\ \hline D. C. 0.5 \\ \hline 30.5 \end{array}$$

+78

58

+50

59

+50

Sta.

Grade
Rod

Rt.

60

+50

61

+50

62

+50

63

+50

64

+50

65

+30

5/2

Grade
Road

47.

5

77

2.1

3.8
2.1
25.1

+ 45

0.6

2.1

0.9
0.6
D.C. 1.2
93.3

Grade
Rod.Lt.Rt

Sta.

76+24

13.3

$$\begin{array}{r} 15.7 \\ F.2.4 \\ \hline 27.2 \end{array}$$

76+50

12.4

$$\begin{array}{r} 14.4 \\ F.2.0 \\ \hline 26.6 \end{array}$$

76+75

11.6

$$\begin{array}{r} 13.0 \\ D.C.00 \\ \hline 28.5 \end{array}$$

77

10.8

14.3

$$\begin{array}{r} 10.8 \\ D.C.1.5 \\ \hline 34.5 \end{array}$$

+50

$$\begin{array}{r} 9.1 \\ 1.5 \\ \hline 10.6 \end{array}$$

$$\begin{array}{r} 7.3 \\ D.C.3.3 \\ \hline 41.7 \end{array}$$

78

$$\begin{array}{r} 7.4 \\ 8.9 \end{array}$$

$$\begin{array}{r} 6.3 \\ D.C.2.6 \\ \hline 38.9 \end{array}$$

+50

$$\begin{array}{r} 5.7 \\ 7.2 \end{array}$$

$$\begin{array}{r} 2.5 \\ D.C.4.2 \\ \hline 47.3 \end{array}$$

+72

$$\begin{array}{r} 5.0 \\ 6.5 \end{array}$$

$$\begin{array}{r} 5.2 \\ D.C.1.3 \\ \hline 33.7 \end{array}$$

79

$$\begin{array}{r} 4.1 \\ 5.6 \end{array}$$

$$\begin{array}{r} 4.4 \\ D.C.1.5 \\ \hline 34.5 \end{array}$$

+50

$$\begin{array}{r} 2.5 \\ 4.0 \end{array}$$

$$\begin{array}{r} 2.8 \\ D.C.1.2 \\ \hline 33.3 \end{array}$$

80

$$\begin{array}{r} 10.4 \\ 11.9 \end{array}$$

$$\begin{array}{r} 9.8 \\ D.C.2.1 \\ \hline 36.9 \end{array}$$

$$\begin{array}{r} 8.7 \\ D.C.3.2 \\ \hline 41.3 \end{array}$$

+50

$$\begin{array}{r} 9.1 \\ 10.6 \end{array}$$

$$\begin{array}{r} 8.6 \\ D.C.2.0 \\ \hline 36.5 \end{array}$$

$$\begin{array}{r} 26 \\ D.C.3.0 \\ \hline 40.5 \end{array}$$

Void

Sta.

Grade
Rod

Lt.

Rt. $\frac{C}{G}$

81

7.9
9.47.0
DC.24
38.16.4
DC.3.0
40.5

+10

6.8
8.35.5
DC.28
39.74.3
DC.4.0
44.5

+60

6.7
8.24.4
DC.3.3
41.71.8
DC.6.4
49.5

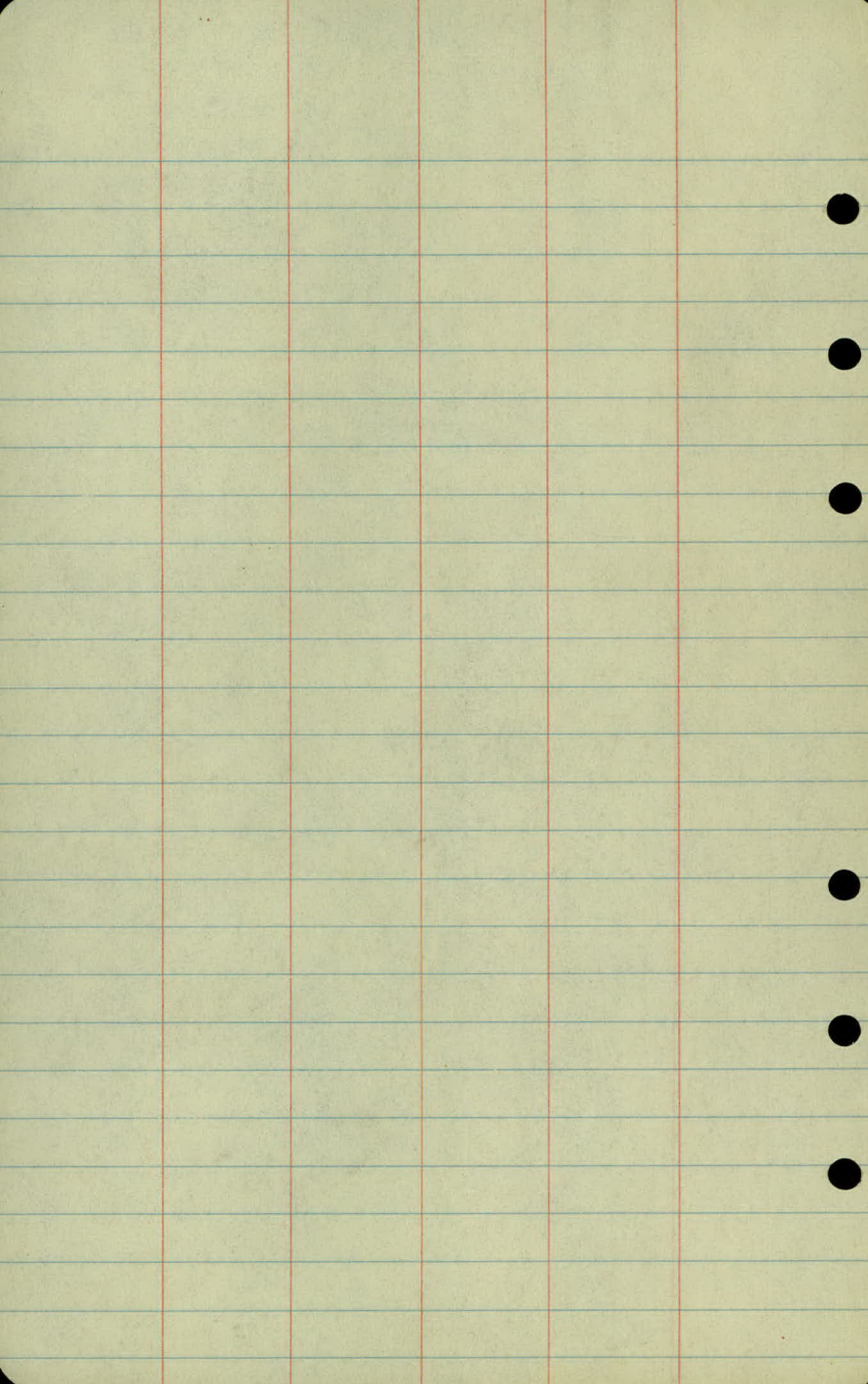
82

6.2
7.71.0
6.2
49.5

+10

5.7
7.21.6
DC.5.6
49.51.8
DC.5.4
49.5

Vord



Sts.

Grade
Rod

Rt.

7

87+80

4.1
5.6
$$\begin{array}{r} 2.7 \\ 0.604 \\ \hline 30.1 \end{array}$$

18+10

5.1
6.6
$$\begin{array}{r} 6.2 \\ 0.604 \\ \hline 30.1 \end{array}$$

18+50

6.4
7.9
$$\begin{array}{r} 6.4 \\ 0.615 \\ \hline 34.1 \end{array}$$

59

8.1
9.6
$$\begin{array}{r} 6.8 \\ 0.628 \\ \hline 39.7 \end{array}$$

+50

9.8
11.3
$$\begin{array}{r} 8.6 \\ 0.627 \\ \hline 39.3 \end{array}$$

60

11.4
12.9
$$\begin{array}{r} 10.8 \\ 0.621 \\ \hline 36.9 \end{array}$$

+50

12.8
14.3
$$\begin{array}{r} 12.6 \\ 0.617 \\ \hline 35.3 \end{array}$$

60+80

13
15.8
$$\begin{array}{r} 2.0 \\ 0.608 \\ \hline 31.7 \end{array}$$

61

1.6
3.1
$$\begin{array}{r} 3.4 \\ 1.18 \\ \hline 25.4 \end{array}$$

+50

2.7

$$\begin{array}{r} 4.5 \\ 1.18 \\ \hline 25.4 \end{array}$$

62

3.3

$$\begin{array}{r} 5.3 \\ 1.20 \\ \hline 26 \end{array}$$

+50

3.9

$$\begin{array}{r} 5.9 \\ 1.20 \\ \hline 26 \end{array}$$

63

4.4

$$\begin{array}{r} 6.5 \\ 1.21 \\ \hline 26.3 \end{array}$$

Sta.	Grade Rod	+
63+50	4.9	$\begin{array}{r} 7.7 \\ F2.8 \\ \hline 28.4 \end{array}$
64	5.4	$\begin{array}{r} 5.6 \\ F3.2 \\ \hline 29.6 \end{array}$
+50	5.8	$\begin{array}{r} 9.5 \\ F3.7 \\ \hline 31.1 \end{array}$
65	6.2	$\begin{array}{r} 10.7 \\ F4.7 \\ \hline 34.1 \end{array}$
+50	6.3	$\begin{array}{r} 10.1 \\ F3.8 \\ \hline 31.4 \end{array}$
66	6.3	$\begin{array}{r} 9.8 \\ F3.5 \\ \hline 30.3 \end{array}$
+50	6.3	$\begin{array}{r} 9.7 \\ F3.6 \\ \hline 30.8 \end{array}$
67	6.3	$\begin{array}{r} 9.3 \\ F3.0 \\ \hline 29.0 \end{array}$
+50	6.2	$\begin{array}{r} 8.6 \\ F2.1 \\ \hline 26.3 \end{array}$
+80	6.7	$\begin{array}{r} 8.8 \\ F2.1 \\ \hline 26.3 \end{array}$
68+50	6.2	$\begin{array}{r} 8.8 \\ F2.6 \\ \hline 27.8 \end{array}$
69	5.9	$\begin{array}{r} 10.7 \\ F4.8 \\ \hline 34.4 \end{array}$
+65	5.2	$\begin{array}{r} 10.0 \\ F4.8 \\ \hline 34.4 \end{array}$

Sta.

Grade
Rod

RT.

8

70+65

3.2
5.2
$$\begin{array}{r} 61 \\ \hline 524 \\ \hline 27.2 \end{array}$$

71

3.1
4.6
$$\begin{array}{r} 18 \\ \hline 00.28 \\ \hline 39.7 \end{array}$$

+50

2.0
3.5
$$\begin{array}{r} 46 \\ \hline 526 \\ \hline 27.8 \end{array}$$

+93

13.0
14.1
$$\begin{array}{r} 14.5 \\ \hline 00.00 \\ \hline 29.6 \end{array}$$

$$\begin{array}{r} 8.8 \\ \hline 5.7 \\ \hline 49.1 \end{array}$$

72

13.0
14.1
$$\begin{array}{r} 2.9 \\ \hline 6.6 \\ \hline 49.1 \end{array}$$

+25

12.4
13.9
$$\begin{array}{r} 5.6 \\ \hline 00.83 \\ \hline 49.1 \end{array}$$

+50

11.2
13.2
$$\begin{array}{r} 5.8 \\ \hline 00.74 \\ \hline 49.1 \end{array}$$

73

10.3
11.8
$$\begin{array}{r} 6.1 \\ \hline 00.53 \\ \hline 49.1 \end{array}$$

+50

8.9
10.4
$$\begin{array}{r} 2.4 \\ \hline 00.30 \\ \hline 40.1 \end{array}$$

74

7.3
8.8
$$\begin{array}{r} 3.9 \\ \hline 00.49 \\ \hline 48.1 \end{array}$$

+50

5.7
7.2
$$\begin{array}{r} 1.7 \\ \hline 00.55 \\ \hline 49.1 \end{array}$$

+75

4.8
6.3
$$\begin{array}{r} 3.1 \\ \hline 00.32 \\ \hline 41.3 \end{array}$$

75

4.0
5.5
$$\begin{array}{r} 5.5 \\ \hline 00.00 \\ \hline 20.1 \end{array}$$

+50

2.4
3.9
$$\begin{array}{r} 5.9 \\ \hline 00.35 \\ \hline 20.1 \end{array}$$

76

0.7

$$\begin{array}{r} 2.8 \\ \hline 02.1 \\ \hline 26.3 \end{array}$$

$$\begin{array}{r} 28.5 \\ 45 \\ \hline \end{array}$$

$$\begin{array}{r} 90 \quad 76.5 \\ 90+50 \quad 74.4 \\ \hline 2.1 \end{array}$$

$$\begin{array}{r} 7.4 \\ 2.1 \\ \hline 5.3 \end{array}$$

$$\begin{array}{r} 92 = 68.1 \\ 63.9 \\ \hline 4.2 \\ 4.2 \\ \hline 7.4 \end{array}$$

$$3.2$$

North St. Paul Road.

New slope stakes acct.
change of plans.

8/8/38

Brom
Pod.

C 33
DC 28.5
F 20.5 to 1

57.5

84.75

8.1

79

+19

6.8

+65

5.3

80

4.7

+50

2.9

81

6.1

+50

5.0

+80

8.1

82

7.9

Lt.

E

Rt.

33.0

$$\begin{array}{r} 8.5 \\ D.C. 1.1 \\ \hline 31.8 \end{array}$$

32.7

$$\begin{array}{r} 2.1 \\ D.C. 1.2 \\ \hline 32.1 \end{array}$$

36.3

O.O.D.C.
28.0

$$\begin{array}{r} 6.2 \\ D.C. 0.6 \\ \hline 30.3 \end{array}$$

$$\begin{array}{r} 4.3 \\ C. 1.0 \\ \hline 36.0 \end{array}$$

F.
22.3O.O.D.C.
30.0

$$\begin{array}{r} 3.9 \\ C. 0.3 \\ \hline 33.9 \end{array}$$

$$\begin{array}{r} 25 \\ C. 1.7 \\ \hline 38.1 \end{array}$$

$$\begin{array}{r} 2.7 \\ C. 0.2 \\ \hline 33.6 \end{array}$$

$$\begin{array}{r} 2.1 \\ C. 0.8 \\ \hline 35.4 \end{array}$$

$$\begin{array}{r} 5.4 \\ C. 0.7 \\ \hline 35.1 \end{array}$$

$$\begin{array}{r} 4.9 \\ C. 1.7 \\ \hline 36.6 \end{array}$$

$$\begin{array}{r} 3.9 \\ C. 1.1 \\ \hline 36.3 \end{array}$$

$$\begin{array}{r} \text{Pulled} \\ 30 \text{ in} \\ C. 2.0 \text{ Troc} \\ \hline 37.2 \end{array}$$

$$\begin{array}{r} 6.2 \\ C. 1.7 \\ \hline 38.1 \end{array}$$

$$\begin{array}{r} 23 \\ C. 4.6 \\ \hline 42.0 \end{array}$$

E
Rd.
Rod.

513.

87+50 7.3

83 6.8

+50 8.8

+68 8.8

84 8.9

+33- 9.0

+57- 9.1

+78

+88 8.7

LT

E

RT

$$\begin{array}{r} 4.1 \\ \hline 63.2 \\ \hline 42.6 \end{array}$$

More
in A
Tree

$$\begin{array}{r} 3.2 \\ \hline 64.1 \\ \hline 43.0 \end{array}$$

$$\begin{array}{r} 1.6 \\ \hline 65.2 \\ \hline 48.6 \end{array}$$

$$\begin{array}{r} 1.9 \\ \hline 64.9 \\ \hline 47.7 \end{array}$$

46.0

$$\begin{array}{r} 3.8 \\ \hline 65.0 \\ \hline 48.0 \end{array}$$

$$\begin{array}{r} 3.4 \\ \hline 65.4 \\ \hline 49.2 \end{array}$$

45.8

37.3

$$\begin{array}{r} 7.4 \\ \hline 61.4 \\ \hline 37.2 \end{array}$$

$$\begin{array}{r} 5.3 \\ \hline 63.5 \\ \hline 43.5 \end{array}$$

44.0

42.6

$$\begin{array}{r} 5.6 \\ \hline 63.3 \\ \hline 42.9 \end{array}$$

$$\begin{array}{r} 5.1 \\ \hline 63.8 \\ \hline 44.4 \end{array}$$

44.0

41.8

$$\begin{array}{r} 6.3 \\ \hline 62.7 \\ \hline 41.1 \end{array}$$

$$\begin{array}{r} 5.0 \\ \hline 64.0 \\ \hline 45.0 \end{array}$$

35.0

$$\begin{array}{r} 3.1 \\ \hline 66.0 \\ \hline 46.5 \end{array}$$

40.0

41.0

41.5

$$\begin{array}{r} 6.0 \\ \hline 63.2 \\ \hline 42.6 \end{array}$$

$$\begin{array}{r} 1.9 \\ \hline 66.3 \\ \hline 49.5 \end{array}$$

41.0

E
Paving

Rod

575.

85

8.3

+50

9.1

86

8.8

+50

9.6

+77

87

11.0

LT

Φ

RT

Polled in
1/2

39.0

$$\begin{array}{r} 5.1 \\ 6.3.2 \\ \hline 42.6 \end{array}$$

$$\begin{array}{r} 4.0 \\ 6.4.3 \\ \hline 43.5 \end{array}$$

42.0

39.0

$$\begin{array}{r} 7.0 \\ 6.2.1 \\ \hline 39.3 \end{array}$$

$$\begin{array}{r} 5.2 \\ 6.3.9 \\ \hline 43.9 \end{array}$$

Polled in
Feet cannot
steps
45.0

39.0

$$\begin{array}{r} 6.9 \\ 6.1.9 \\ \hline 38.7 \end{array}$$

$$\begin{array}{r} 6.1 \\ 6.2.7 \\ \hline 41.1 \end{array}$$

40.0

38.0

$$\begin{array}{r} 8.2 \\ 6.1.4 \\ \hline 37.2 \end{array}$$

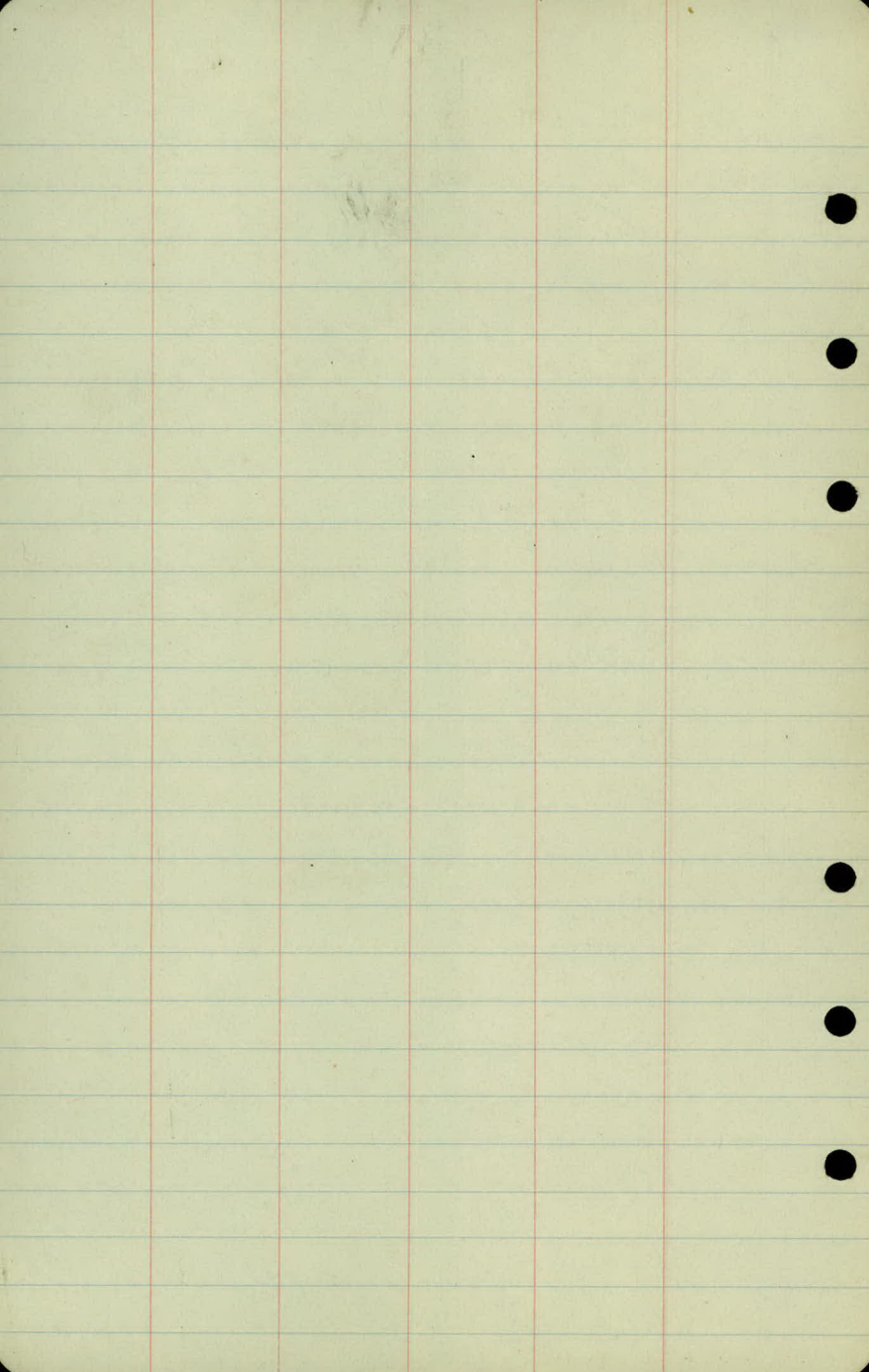
$$\begin{array}{r} 7.6 \\ 6.2.0 \\ \hline 39.0 \end{array}$$

46.0

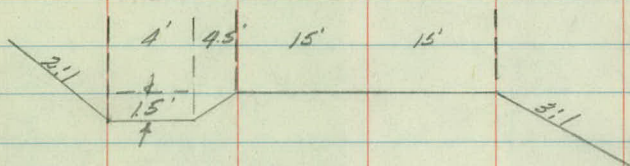
36.0

33.0

$$\begin{array}{r} 10.5 \\ 6.0.1 \\ \hline 34.1 \end{array}$$



slope stakes
N. St. Paul Road Conn.



Sta	+	Σ	-	Grade.
B.M.	-0.08	969.22		969.30
100				967.0
+21				66.6
+30				66.5
+50				66.1
1				65.2
+50				64.3
2				63.4
+50				62.6
3				62.0
+50				61.6
4				61.5

Spk. in T.P. West side of W. 17. Road Ave. N. St. Paul Rd. Green.

2.2

$$\begin{array}{r} 3 \\ 13161 \\ \hline 5 \end{array}$$

$$3.1 \quad \begin{array}{r} 28.7 \\ \hline 45 \\ 1001 \end{array} \quad \begin{array}{r} 40 \\ \hline -09 \end{array} \quad \begin{array}{r} 72 \\ \hline -41/27.3 \end{array}$$

$$4.0 \quad \begin{array}{r} 22.4 \\ \hline 68 \\ -38 \end{array} \quad \begin{array}{r} 53 \\ \hline -13 \end{array} \quad \begin{array}{r} 107 \\ \hline -69/33.0 \end{array}$$

$$4.9 \quad \begin{array}{r} 25.8 \\ \hline 85 \\ -36 \end{array} \quad \begin{array}{r} 58 \\ \hline -09 \end{array} \quad \begin{array}{r} 113 \\ \hline -66/33.0 \end{array}$$

$$5.8 \quad \begin{array}{r} 28.3 \\ \hline 102 \\ -44 \end{array} \quad \begin{array}{r} 44 \\ \hline -06 \end{array} \quad \begin{array}{r} 116 \\ \hline -58/32.4 \end{array}$$

$$6.6 \quad \begin{array}{r} 30.0 \\ \hline 116 \\ -50 \end{array} \quad \begin{array}{r} 47 \\ \hline -01 \end{array} \quad \begin{array}{r} 117 \\ \hline -61/30.3 \end{array}$$

$$7.2 \quad \begin{array}{r} 30.3 \\ \hline 123 \\ -51 \end{array} \quad \begin{array}{r} 70 \\ \hline 102 \end{array} \quad \begin{array}{r} 122 \\ \hline -50/30.0 \end{array}$$

$$7.6 \quad \begin{array}{r} 32.1 \\ \hline 133 \\ -57 \end{array} \quad \begin{array}{r} 73 \\ \hline 103 \end{array} \quad \begin{array}{r} 128 \\ \hline -53/30.9 \end{array}$$

$$7.7 \quad \begin{array}{r} 31.2 \\ \hline 131 \\ -54 \end{array} \quad \begin{array}{r} 74 \\ \hline 103 \end{array} \quad \begin{array}{r} 132 \\ \hline -55/31.5 \end{array}$$

