

Dr. G - Bk. 99

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

----- *PLAT* Survey

NORTH CO. LINE ROAD.

From *S.T.H. 65* ----- To *Rice St. Ext.*

Road Acc't. No. ----- *30*

Date Filed ----- *1936*

File ----- *899 D*

Alignment

North County Line

S.T.H. #65 East

67+80.35 P.I. Long Lake Road Rt

56+00 P.O.T.

41+39.99 P.I. $\Delta 0^{\circ} 00' 30''$ Rt

20+17.43 P.I. $\Delta 0^{\circ} 04'$ Lt. W. County Line

0+00 $\pm$ Hwy # 65

Mant.

GR.

2035

22.55

GR.

Twin Elm

50.72

Boat Spk.

59.35

6" Elm

Mant

Mant

□

89° 49'

Hole in Pavement near #65

100+60.30

120+78.28[±] P.I. ± Hwy #2

94+29.14

P.I.

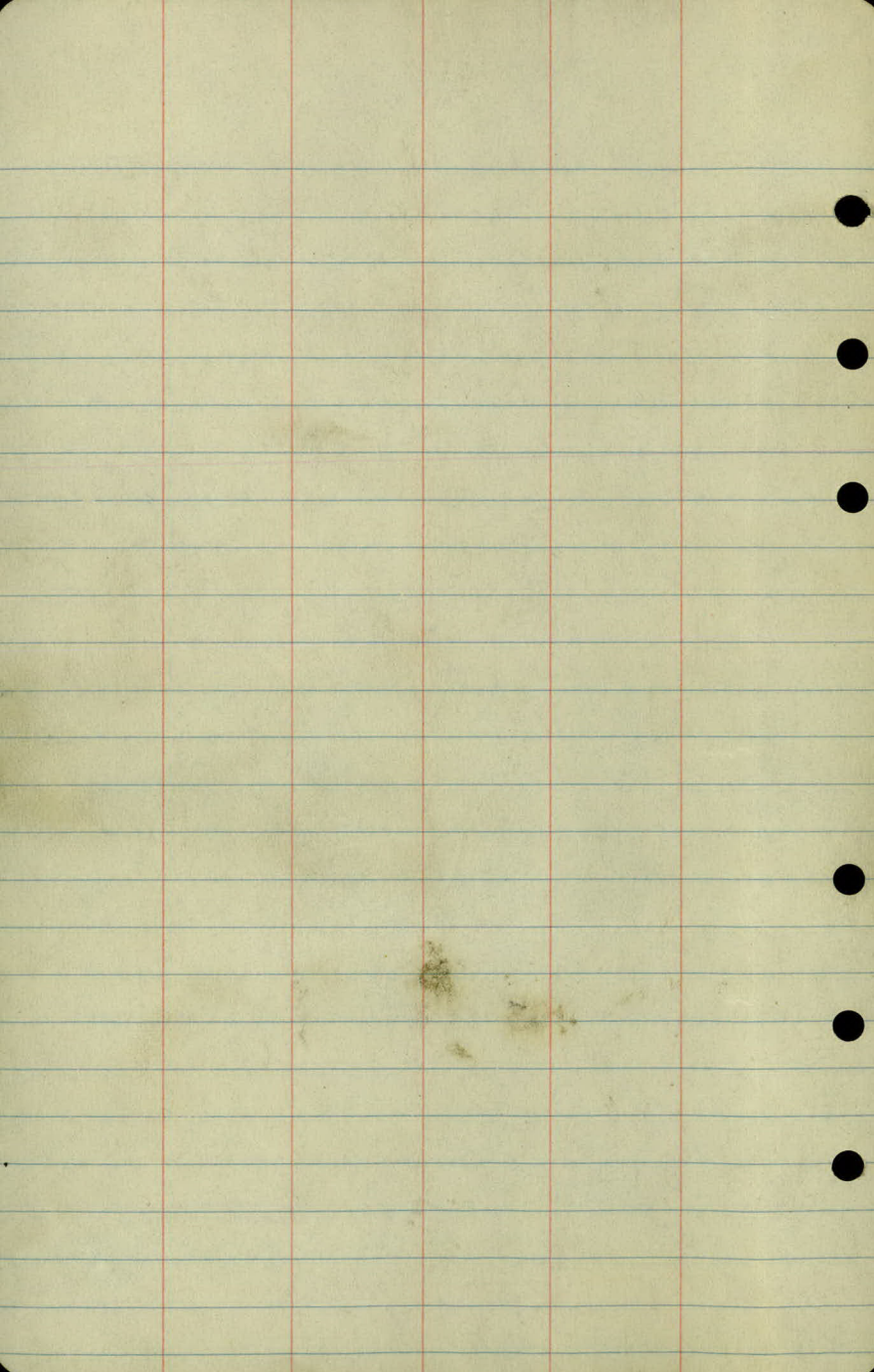
Δ 0' 01' Rt

Brass Plug

□

Mont

□



B.M. = 909.92 Brass Plug
in E Post #8 180+60.3

Bm Spike in 18" BE 69' NE of 100
Lex Ave. = 871.47

Bm Spike in 15" St 200' S. of 19+15.9 Min
= 867.77 on N. Co. Line

Sta

Alt A Rt.

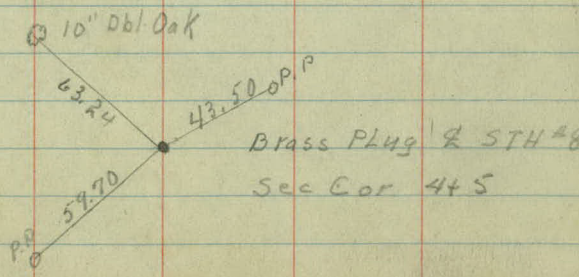
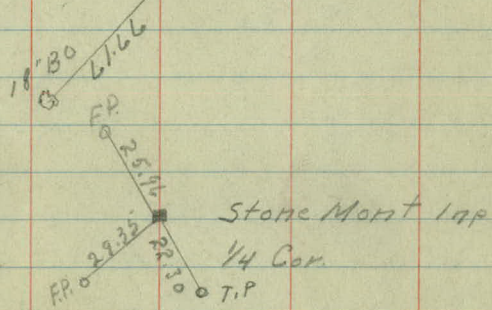
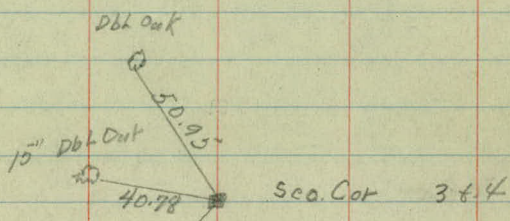
153+14.10 P.I

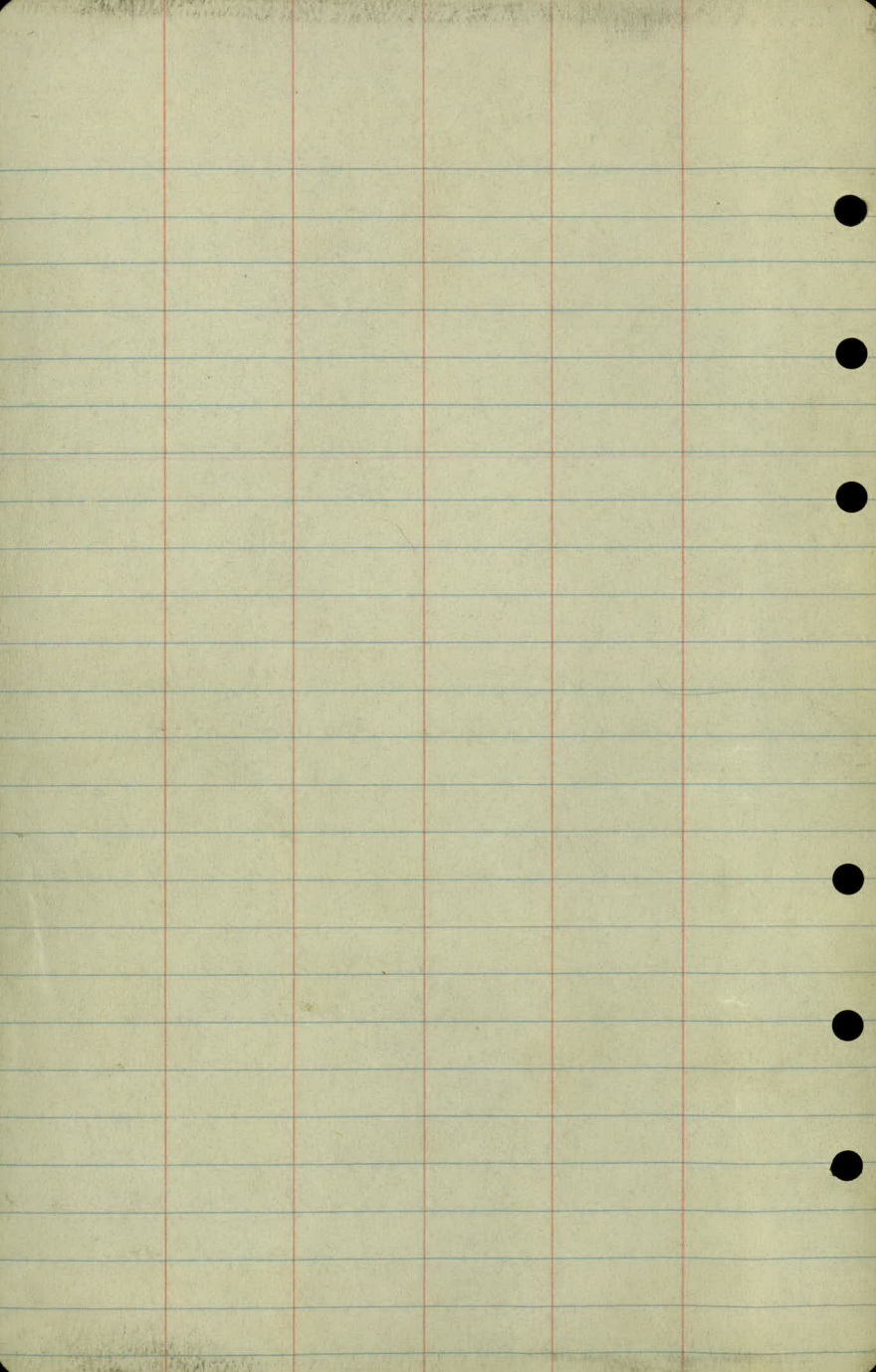
126+91.28 P.I

0°01

100+60.30 P.I 0°17'

2
8/28/36
Cloudy





9/29/36

H. R. Ruffell

Alignment
North County Line
Sta 153+14.10 East

258+70.70 P.I. Δ 0° 17' 30" Lt

242+70.74 P.O.T.

232+82 X-Cover

232+30.00 P.I. Δ 0° 08' Lt

222+90.75 P.O.T.

205+91.55 P.I. Δ 0° 52' Rt.

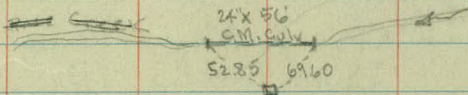
179+52.50 P.I. Δ 0° 44' 30" Lt

153+14.10 P.I. Δ 0° 31' Rt

Mont



DITCH #8



Mont

Mont

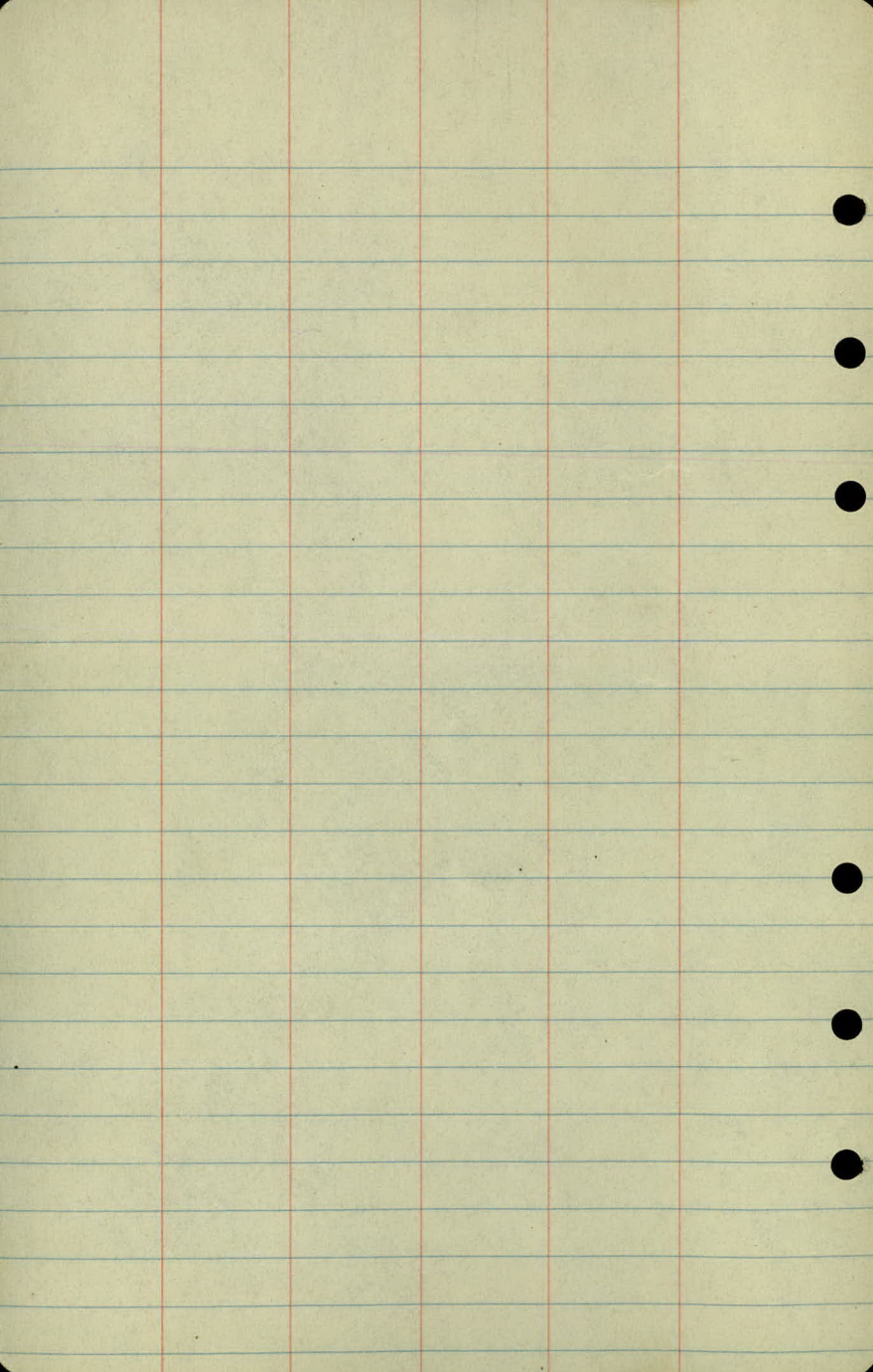
FR
+ 52.38

Mont
Ties 9/29/36

35.90 66.25
* FR * FR

Mont

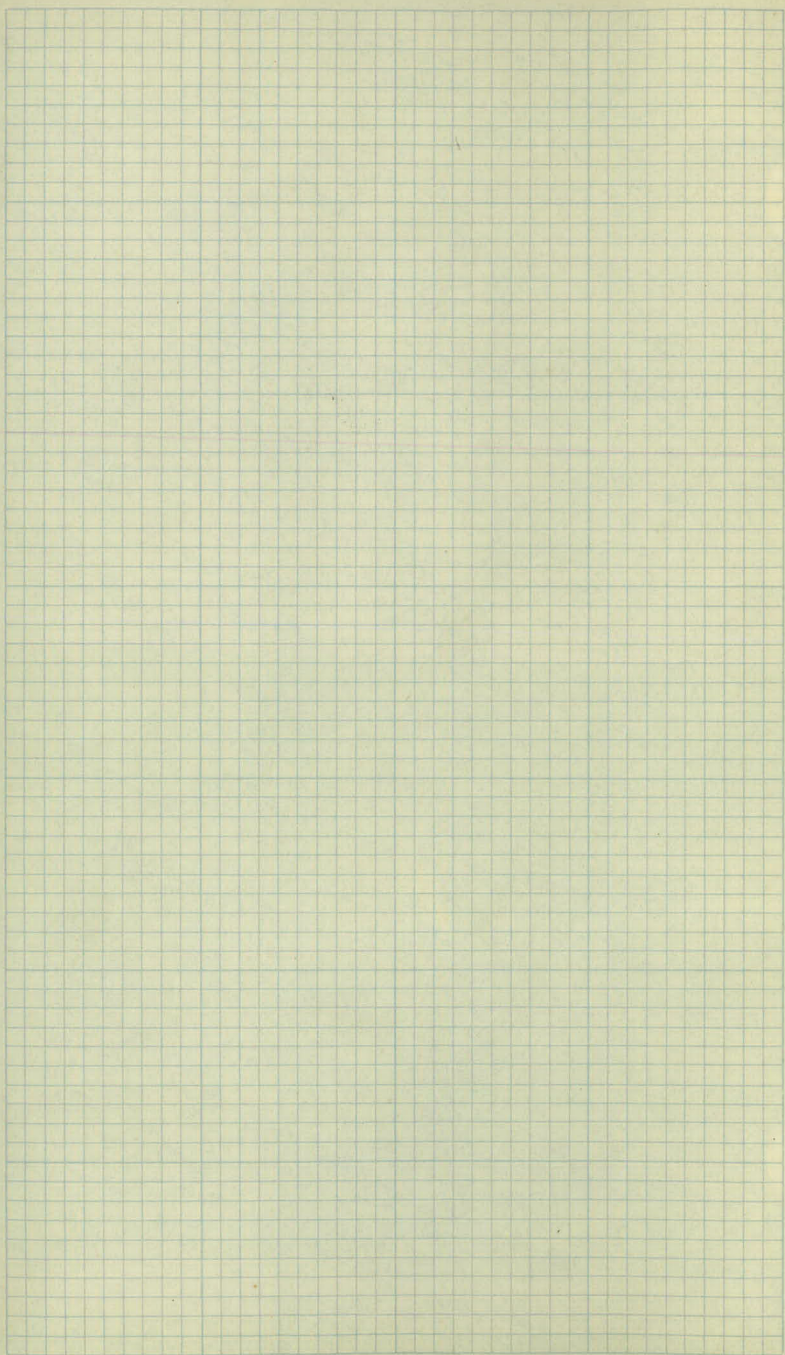




Hodgson 358+10.70 Mont
2.83+10.15 " Δ 0° 01' 15" Mont
511+50.17 " Mont

2.85 x 10.15	"	Δ 0° 01' 15"	1/6 ft
5.11 x 58.17	"		Mon +

North County Line



9/23/36

H.T. Portell
L. Goldberry
F. Dechurme

TOPOG

No. County Line from

S.T.H. #65

East

5

$$7 \text{ Rd } 3$$

4

$$5 \text{ Rd } 5$$

$$+53 \text{ Twin Cottonwood}$$

3

$$6 \text{ Rd } 5$$

2

$$6 \text{ Rd } 2$$

1

$$+27 \text{ Cor Bill B.}$$

64

$$+90 \text{ Cor Bill board}$$

79

$$+70 \text{ Rd}$$

8-6

$$+42 \text{ Rd } 31$$

21

$$+45 \text{ DP}$$

18

$$+21 \text{ Run } 31$$

32

$$+10 \text{ Rd}$$

46

$$+10 \text{ Shoulder}$$

28-33

$$+10 \text{ Edge Pave } +10 \text{ Rd}$$

50

0+00

$$-14 \text{ Edge Pave}$$

$$-29 \text{ TP}$$

6

Cultivated

Pasture

Conn to #10

S.H. #65

12

$$\frac{R_d}{9-2}$$

$$\frac{F_c}{29}$$

11

$$11-3$$

$$\frac{F_c}{29}$$

$$\frac{+50 F_c}{28}$$

10

$$\frac{R_d}{7-3}$$

$$\frac{F_c}{28}$$

9

$$\frac{R_d}{11-2}$$

$$\frac{F_c}{28}$$

8

$$\frac{R_d}{11-3}$$

$$\frac{F_c}{29}$$

7

$$\frac{R_d}{10-3}$$

$$\frac{+75 F_c}{29}$$

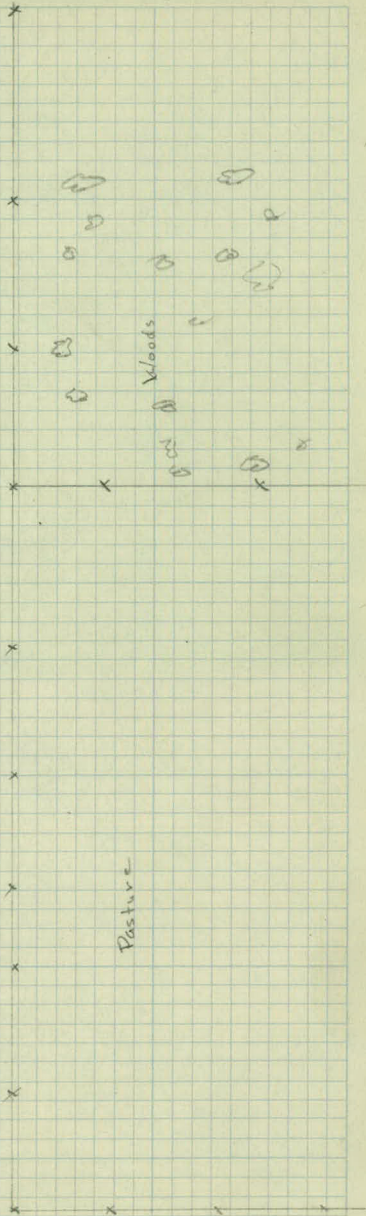
6

$$\frac{R_d}{7-3}$$

Cultivated

Pasture

Woods



19

$$\frac{Fc}{34}$$

2-8

$$\frac{Fc}{33}$$

18

$$\frac{Fc}{35}$$

$$\frac{Rd}{3-8}$$

$$\frac{Fc}{33}$$

$$\begin{array}{r} +43 Fc \\ 38 \\ +35 Ent \end{array}$$

17

$$\frac{Fc}{37}$$

$$\frac{Rd}{5-7}$$

$$\frac{Fc}{32}$$

16

$$\frac{Fc}{37}$$

$$\frac{Rd}{5-5}$$

$$\frac{Fc}{32}$$

$$\begin{array}{r} +60 Fc \\ 62 \end{array}$$

$$\begin{array}{r} +07 Fc \\ 146 \end{array}$$

+05 End Cult

15

4-7

$$\frac{Fc}{31}$$

14

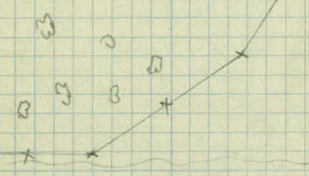
$$\frac{Rd}{6-5}$$

$$\frac{Fc}{31}$$

13

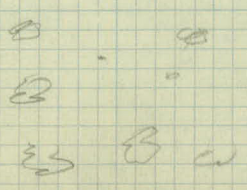
$$\frac{Rd}{6-2}$$

$$\frac{Fc}{30}$$



Cultivated

Woods & Pasture



+69 Road

$$\begin{array}{r} +45 \text{ FC} \\ \hline 33 \end{array}$$

+09 Ent

26

$$\begin{array}{r} \text{Fc} \\ \hline 33 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ \hline 4-6 \end{array}$$

$$\begin{array}{r} \text{Fc} \\ \hline 33 \end{array}$$

25

$$\begin{array}{r} \text{Fc} \\ \hline 34 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ \hline 4-6 \end{array}$$

$$\begin{array}{r} \text{Fc} \\ \hline 33 \end{array}$$

24

$$\begin{array}{r} \text{Fc} \\ \hline 34 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ \hline 3-6 \end{array}$$

$$\begin{array}{r} \text{Fc} \\ \hline 32 \end{array}$$

23

22

$$\begin{array}{r} \text{Fc} \\ \hline 34 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ \hline 3-7 \end{array}$$

21

$$\begin{array}{r} \text{Fc} \\ \hline 33 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ \hline 4-6 \end{array}$$

$$\begin{array}{r} \text{Fc} \\ \hline 33 \end{array}$$

20

$$\begin{array}{r} \text{Fc} \\ \hline 34 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ \hline 5-7 \end{array}$$

$$\begin{array}{r} +20 \text{ FC} \\ \hline 33 \end{array}$$

$$\begin{array}{r} \text{Fc} \\ \hline 33 \end{array}$$

Dastard k Woods

woods
(game refuge)

WOODS & PASTURE

23

$$\frac{Rd}{8-2}$$

$$\frac{Fc}{34}$$

32

$$\frac{Rd}{8-2}$$

$$\frac{Fc}{34}$$

31

$$\frac{Rd}{8-2}$$

$$\frac{Fc}{34}$$

30

$$\frac{Rd}{8-2}$$

$$\frac{Fc}{33}$$

29

$$\frac{Rd}{6-3}$$

$$\frac{Fc}{33}$$

28

$$\frac{Rd}{5-5}$$

$$\frac{Fc}{33}$$

27

$$\frac{Rd}{5-5}$$

$$\frac{Fc}{33}$$

Hay Land

Hay Land

x

x

x

x

x

x

x

x

x

x

x

Pasture

Woods

①

①

40

$$\frac{Rd}{3-8}$$

$$\frac{Fc}{8-2}$$

39

$$\frac{Rd}{3-7}$$

$$\frac{Fc}{3-3}$$

38

$$\frac{Rd}{3-7}$$

$$\frac{Fc}{3-3}$$

37

$$\frac{Rd}{4-7}$$

$$\frac{Fc}{7-3}$$

36

$$\frac{Rd}{6-5}$$

$$\frac{Fc}{7-2}$$

35

$$\frac{Rd}{8-3}$$

$$\frac{Fc}{8-4}$$

34

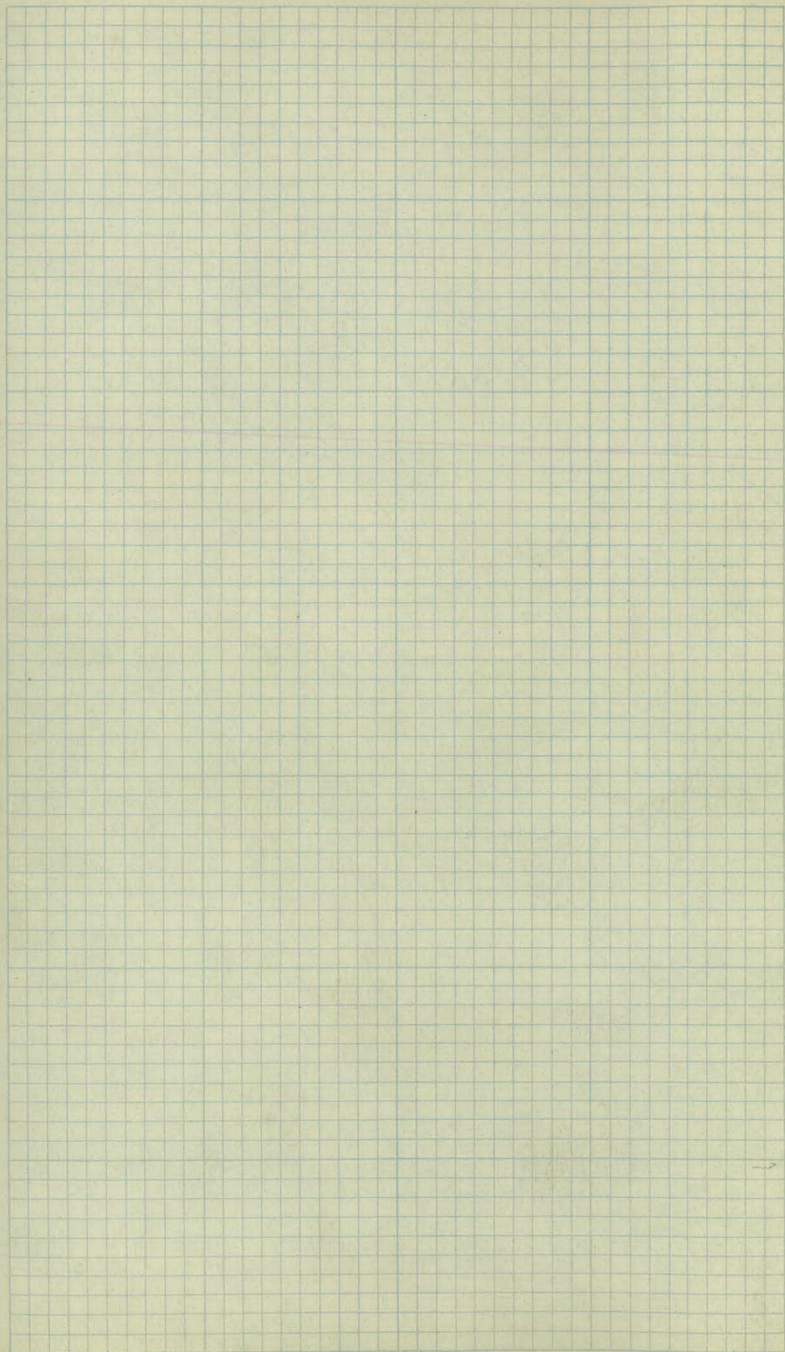
$$\frac{Rd}{8-2}$$

$$\frac{Fc}{3-4}$$

Cultivated

Hay Land

30, 20
W



H.T. Purcell
10/5/36

Topog
No County line
Sta 42 to East

47

~~Rd~~
8-9

46

~~5~~ ²⁶
-8~~Fcc~~
29

45

~~Rd~~
3-8

44

~~Rd~~
7-5~~Fcc~~
28

43

~~Rd~~
8-4

42

~~Rd~~
8-6~~Fcc~~
29

Cultivated

Hay Meadow

54

$$\frac{\text{Treas}}{37}$$

$$\frac{\text{Rd}}{8-7}$$

$$\frac{\text{Fcc}}{27}$$

53

$$\frac{\text{Rd}}{11-6}$$

+95 Bag Box Continued
37

$$\frac{+35 \text{ Tr}}{27}$$

52

$$\frac{\text{Rd}}{7-6}$$

$$\frac{\text{Fcc}}{28}$$

$$\frac{+66 \text{ FC}}{22}$$

51

$$\frac{\text{Rd}}{5-6}$$

+98 FC
+47 Ent $\frac{20}{29}$ +55 Tr
+27 End File
20

50

$$\frac{\text{Fcc}}{20}$$

$$\frac{\text{Rd}}{8-7}$$

$$\frac{\text{Fcc}}{29}$$

+99 Tr +92 Cor Ho
29 82

$$\frac{+59 \text{ FC}}{20}$$

49

$$\frac{\text{Rd}}{12-11}$$

48

$$\frac{\text{Rd}}{9-9}$$

$$\frac{\text{Fcc}}{31}$$

+92 End Row Trees

35

61

60

Fees
36

Rd
16-0

+52 Ent

+25 Ent

+06 Cor Ho
104

59

+46 Ent

+50 Fee
58

58

Trees
37

Rd
13-0

Fee
36

+87 Tr - Fee
24 24

57

Rd
10-2

56

Trees
37

Rd
10-5

Fee
27

+69 Tr
15

55

Rd
7-6

22'
25 F
42

yard

Ent

Ent

Ent

Cultivated

Hay Meadow

13
12

68

GR
12RM
10-10

+75 Long Lake Rd (12' Wide)

+62 Iron Rd Sn

20

+40-18' x 42' Conc.

22-20

+40 Bag Brush

35

67

+04 Bag G.R. (1 cable Post 12-c-c) Bag Gravel Surface
12'

66

Bag Brush
20RD
11-8

65

64

RD
15-2

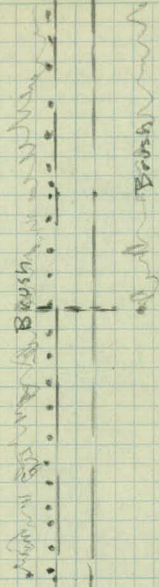
63

62

RD
17-0

Meadow

Light Brush



Meadow

75

+50 End Brush
35

74

RA
10-10

+47 Tr
34

73

72

RA
10-10

71

+48 End GR
12

70

GR
12

RA
10-10

69

Light Brush

Brush

Light Brush

Meadow

$$\frac{+80 - 18' \times 42' \text{ conc}}{25 - 17}$$

82

$$\frac{GR}{12} \quad \frac{RD}{10-10}$$

81

80

$$\frac{G.R.}{12} \quad \frac{RD}{10-10}$$

79

78

$$\frac{RD}{10-10}$$

$$\frac{+86 \text{ Bag G.R.}}{12}$$

$$\frac{+62 \text{ Ent (15' x 12' CM) old}}{36}$$

$$\frac{+80 \text{ Ent (15' x 20' CM) (New)}}{26}$$

77

76

$$\frac{RD}{10-10}$$

Light Brush

Meadow

Int

Ext

$$\begin{array}{r} + 65-30' \times 48' \text{ Conc} \\ \hline 23 - 25' \end{array}$$

89

$$\begin{array}{r} + 63 \text{ Bag GR} \\ \hline 12 \end{array}$$

88

$$\begin{array}{r} GR \\ \hline 12 \end{array}$$

$$\begin{array}{r} R4 \\ \hline 10-10 \end{array}$$

87

86

$$\begin{array}{r} GR \\ \hline 12 \end{array}$$

$$\begin{array}{r} R4 \\ \hline 10-10 \end{array}$$

85

$$\begin{array}{r} + 20 \text{ Bag Brush} \\ \hline 24 \end{array}$$

84

$$\begin{array}{r} GR \\ \hline 12 \end{array}$$

$$\begin{array}{r} R4 \\ \hline 10-10 \end{array}$$

83

Brush

Brush

+12 Ent-12'x20' (New)
19

96

81
10-10

FC
29

95

+05 End Brush FC
29

94

84
10-10

93

92

91

90

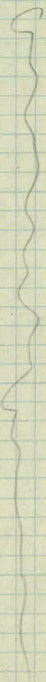
+06 End GR
12-12

Brush

Brush

Ent

Cultivated



103

102

Rd
10-10

Fcs
26

+10 End Brush

101

+60 Culv 24x60' Cont

+38 End Culv
19

100

Rd
10-10

Fcs
29

99

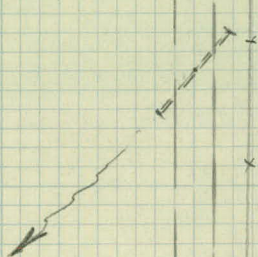
98

Rd
10 10

Fcs
29

97

Cultivated



Brush

Cultivated

+70 Ent

110

$$\frac{Fcc}{25}$$

$$\frac{Rd}{10-10}$$

$$\frac{Fcc}{25}$$

109

108

$$\frac{Fcc}{24}$$

$$\frac{Rd}{10-10}$$

$$\frac{Fcc}{24}$$

107

106

$$\frac{Fcc}{24}$$

$$\frac{Rd}{10-10}$$

$$\frac{Fcc}{25}$$

105

$$\frac{+15 Fc}{25}$$

$$\frac{Rd}{10-10}$$

$$\frac{Fcc}{25}$$

104

Ent

x

v

x

x

+42 Ent

+12 Rd Sn
23

117

+20 F.C.
30

116

FCC
30

Rd
10-10

Fcc
28

115

114

FCC
29

Rd
10-10

Fcc
25

113

+06 Ent (15x20' CM (new))
22'

112

FCC
25

Rd
10-10

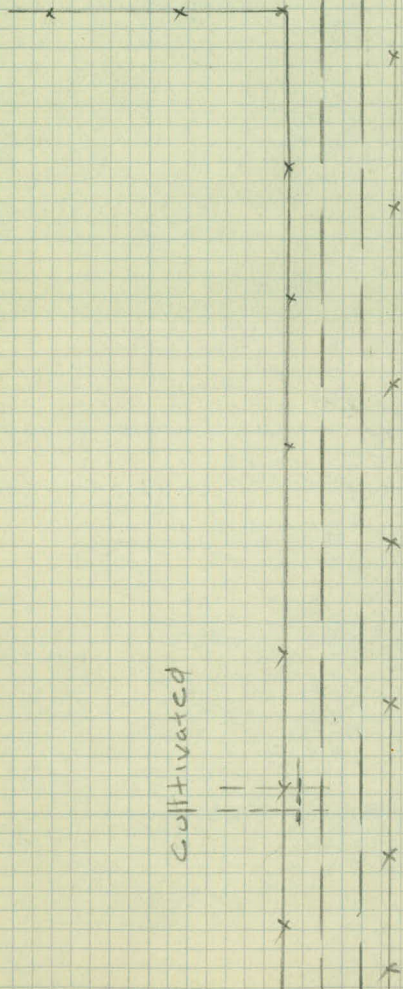
Fcc
25

111

Farm
Yard

Cultivated

Cultivated



$$20 + 77 = ?$$

$$\begin{array}{r} + 345n \\ 271 \\ + 10-31ns \\ \hline 31 \end{array}$$

120

$$\begin{array}{r} + 50 Corb. \\ 125 \end{array}$$

$$+ 15 Ent$$

119

118

$$\begin{array}{r} + 77 \text{ E}^{\#8} \\ + 65 \text{ Edge Paw} \\ + 575 \text{ holder} \\ 30 - 30 \\ \hline + 35 Rd \\ 10-10 \end{array}$$

$$\begin{array}{r} Rd \\ 10-10 \end{array}$$

$$\begin{array}{r} + 41 PP \\ 57 \\ \hline + 52 Rd Sm \\ 31 \end{array}$$

$$\begin{array}{r} + 34 FC - Rd Sm \\ 23 \\ \hline 13 \end{array}$$

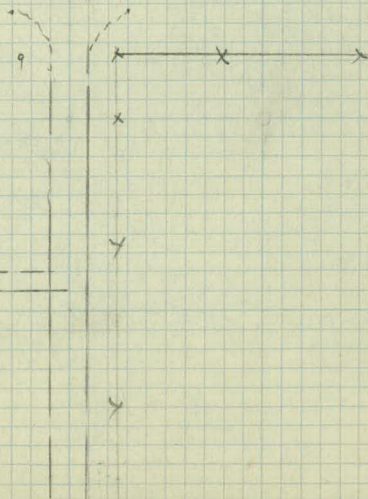
$$\begin{array}{r} FCB \\ 25 \end{array}$$

$$\begin{array}{r} Rd \\ 10-10 \end{array}$$

$$\begin{array}{r} FCB \\ 26 \end{array}$$

ST.H. #8 (21' Conc)

32'
25F
26'



41

$$\begin{array}{r} 3 \quad 14 \\ \underline{30} \\ 44 \end{array}$$

Topography

No Co Line Rd

From

STH #8 East

100+60³⁰ to

107

106

105

104

103

102

101

100+60 30 2 SFA #8

Rd 23' Fence 31'

Rd 0' Fence 14'

Rd 21' Fence 30'

Rd 0' Fence 14'

+73' P.P. 13'

Road 20' Fence 29'

Road 0' Fence 14'

Rd 20' Fence 28'

+23 P.P. 14'

Rd 0' Fence 14'

Rd 20' Fence 27'

Road 1' Fence 14'

+73' BP 13'

Fence 26'
Rd 19'

Fence 14'
Rd 2'

+18 Fent
+10 F.Cor 22'
+05 stop sign 19'
+01 Pole 27'

+23 T.P. 14'

+03 Fence Cor 17'
+96 Pole 38' + Fence Cor.
+73 E. Pole

S.T.H. #8

27' Conc. Pavc

114

113

112

111

110

109

108

107

Rd 22' Fence 32'

Rd 1' Fence 15'

Rd 22' Fence 32'

+07 T.P. 14'
Rd 0' Fence 15'

+47 F.Cor 31'

+28 & Town Rd North

+10 Fence 100'
Rd 23' Fence 67'

+15 P.P. 13'
Rd 0' Fence 15'

+71 F.Cor. 39'

Rd 24' Fence 36'

Rd 0' Fence 15'

Rd 23' Fence 33'

+56 P.P. 14'

Rd 0' Fence 15'

Rd 22' Fence 32'

Rd 0' Fence 15'
+98 P.P. 14'

Rd 23' Fence 31'

Rd 0' Fence 15'

Rd 23' Fence 31'

+38 P.P. 14'

Rd 0' Fence 14'

121

120

119

118

117

116

115

114

Rd 14' Fence 27'

Rd. 7' Fence 17'
+ 85 T.P 15'

Rd. 15' Fence 27'

Rd. 7' Force 16'

Rd 18' Fence 28'

+34 T.R. 15'

Rd 5' Fence 15'

Rd 18' Fence 29'

Rd 4' Fence 15'

Rd 18' Fem 30'

+76 T.P. 15'

Rd 3' Fence 15'

Rd. 20' Fence 31'

+22 T.P. 15'
Rd/3' Fence 15''

Rd 22' Fence 32

Rd R' Fence 15'

Rd 22' Fence 32'

+62 T.P 15'

Rd 1' Fence 15'

Gravel Rd

Cultivated

Alphalpa

127

126

125

124

123

122

121

+80 T.P 19'

+34 F.Cop 1 NYS Fence 22'

Rd. 11' Fence 22'

Rd. 11' Fence 20'

+30 T.P. 18'

Rd 11' Fence 23'

Rd. 11' Fence 19'

Rd 12' Fence 24'

Rd 10' Fence 19'

+83 T.P 18'

Rd 13' Fence 25'

Rd 9' Fence 18'

+36 T.P 17'

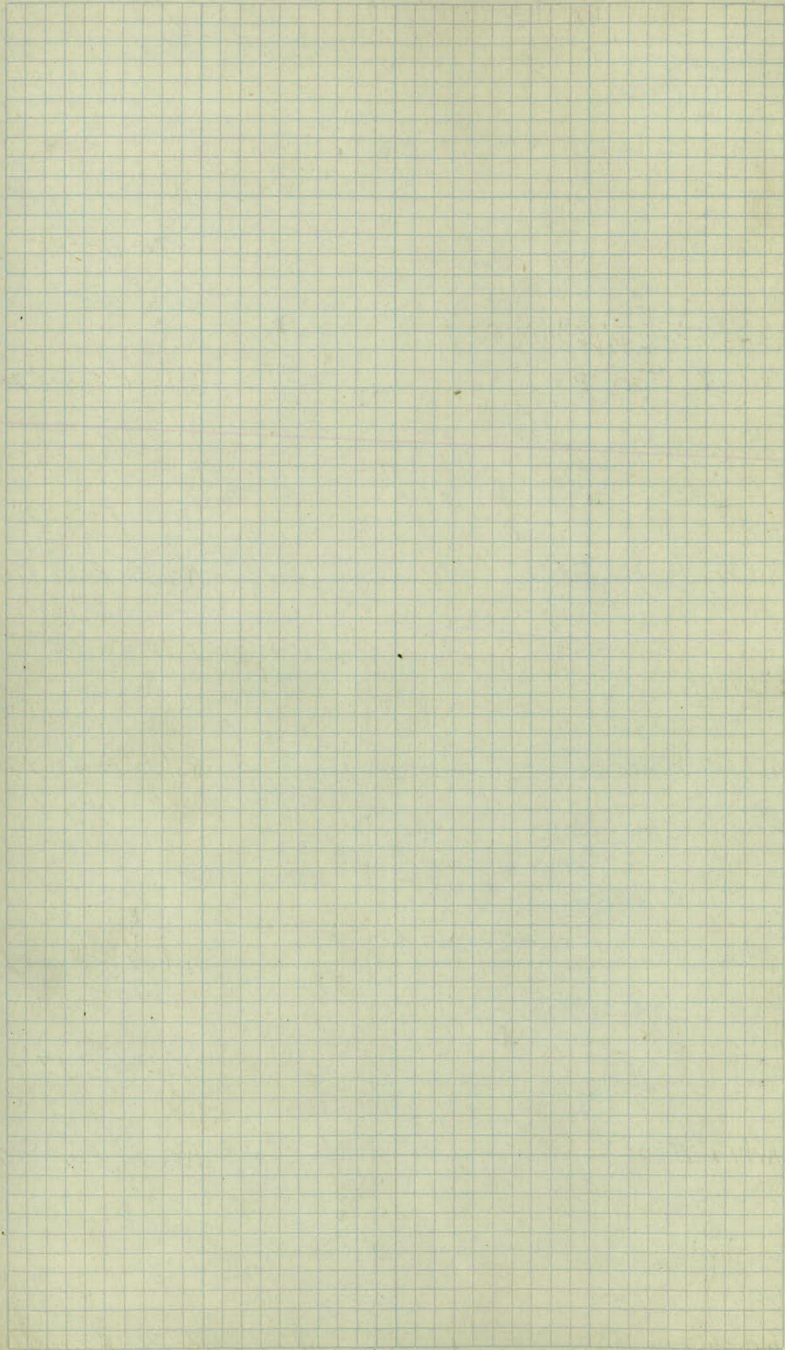
Rd 13' Fence 26'

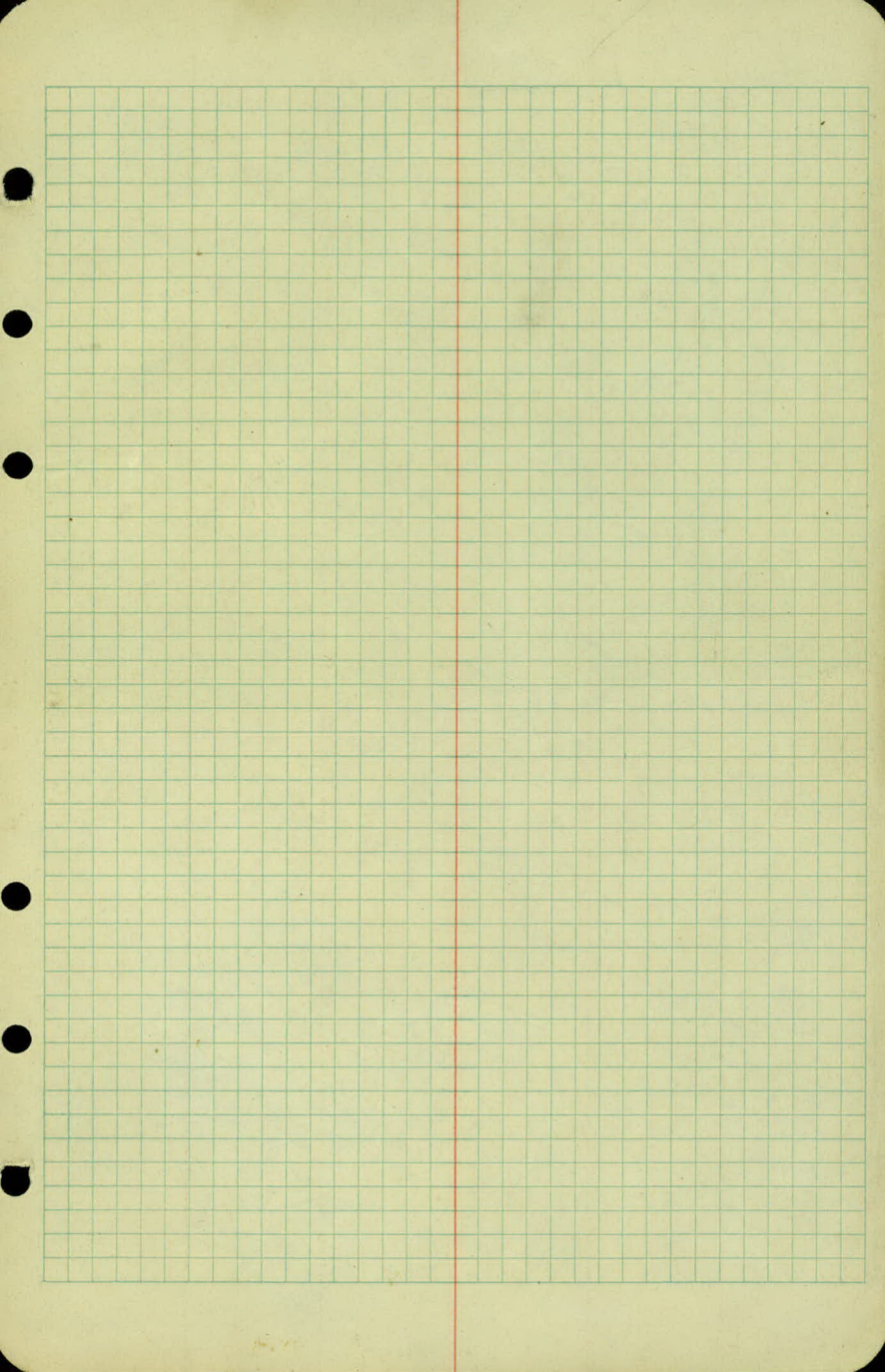
Rd 8' Fence 17'

Rd 14' Fence 27'

Rd 7' Fence 17'

Gravel Rd.





133+63 Side Fence

133

+69 Phone Pole 23.1 Rt

132

P

+15 Phone Pole 22.7 Rt

131

130

+65 Phone Pole 22.2 Rt

129

+26 Phone Pole 21.0 Rt.

128

127+00 Barb Wire Fence 20.8 Lt 20 Rt

126+91.28 Stone Monument

9/3/36

133+63

17.7 23.8

18.1 23.3

18.4 23.2

20.2 21.9

22.2

20.2 21.7

20.2 20.9

20.2 Phone Pole 126+80.6

Cultivated

Cultivated

+25 Phone Pole 24.8 Rt.

140

+95 Side Fence

139

+75 Phone Pole 25' Rt

+55 Fc. Cor. 20.7 Lt

138

+29 Phone Pole 25.3 Rt

137

136

+73 Phone Pole 25' Rt

135

+25 Phone Pole 24.0 Rt.

134

B.M. Fence

9/3/36

Cultivated

Cultivated

26.8

24.4

20.7

19.2

18.3

17.9

17.1

17.2

13.8 + 6.5

25.6

25.5

25.2

25.3

24.6

Wood Lot

+82 Phone Pole 17.8 Rt

147

+12 12" W. Oak 25' L

146 Phone Pole 20' Rt

145

+73 Phone Pole 22' Rt.

144

+66 12" Elm 27.5 Lt

+20 Phone Pole 23.7 Rt

143

+37 Fc. Cor 27.3 Lt

142

+72 Phone Pole 24.5 Rt

141

B.W. Fence on Rt.

9/3/36

147

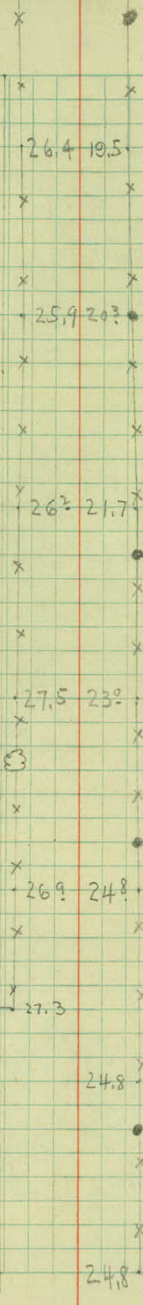
Cultivated

Pasture

142+37

cultivated

Pasture



+27 8" Plum 30' Rt
+12 8" Apple 30' Rt
153 +97 10" Dead Plum Tree 30' Rt | 14 B Oak 31' Lt
+90 Power & Phone Pole 21' Rt

+62 Fc. Cor 21 Rt
+43 4" Cottonwood 26 Lt
+08 Dbl. Oak 25.2 Lt
+01 20" B. Oak 37 Lt
152 +77 Power Pole 22.1 Rt (also phone)
+71 Fc. Cor 18.5 Rt
+59 27" Oak Tree 27.5 Lt
+49 28" Stump 30' Lt (Oak)

151
+92 Phone Pole 15.7 Rt

150

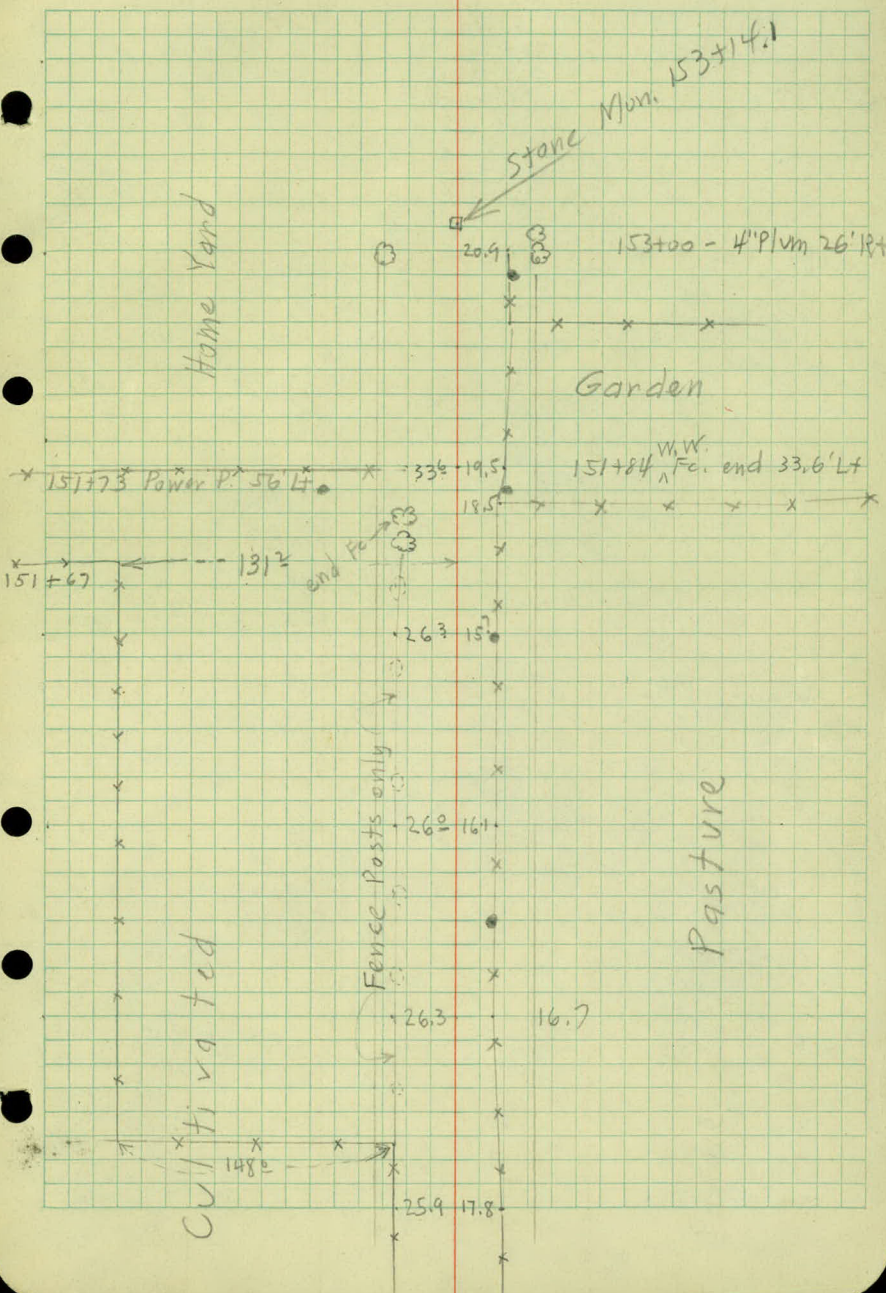
+33 Phone Pole 16.5 Rt

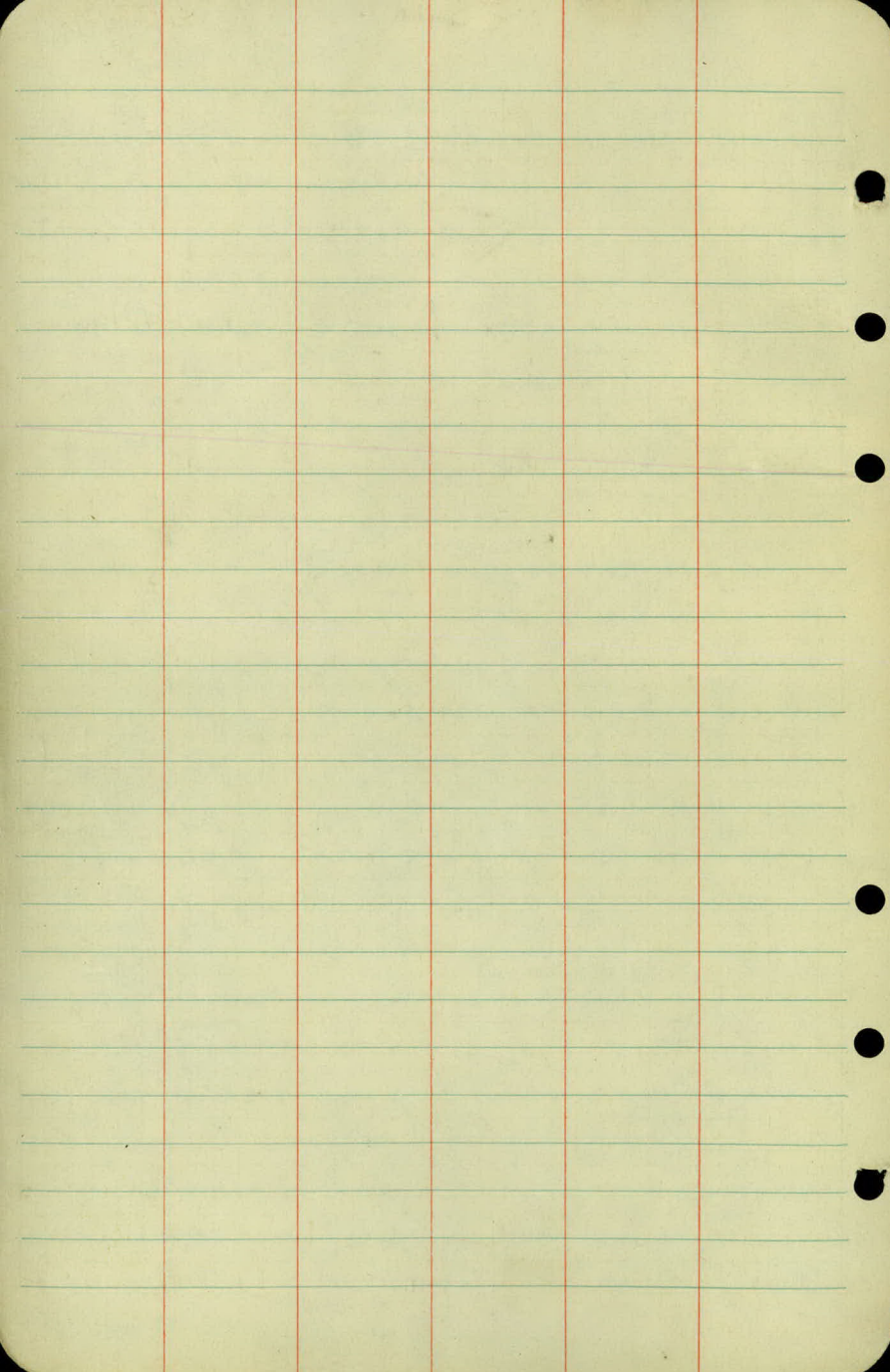
149

+32 Fc. Cor 26.2 Lt

148 B.W. Fences

9/3/36





Topography
No. Co Line
Sta. 154+00 to Hodgson Rd.

$$\begin{array}{r} +72 \text{ Tr} \\ 37 \end{array} \quad \begin{array}{r} +94 \text{ Tr} \\ 39 \end{array}$$

$$\begin{array}{r} +54 \text{ Tr} \\ 37 \end{array} \quad \begin{array}{r} +30 \text{ Tr} \\ 36 \end{array}$$

158

$$\begin{array}{r} R9 \\ 21-2 \end{array}$$

$$\begin{array}{r} +66 \text{ Tr} \\ 34 \end{array} \quad \begin{array}{r} +88 \text{ Tr} \\ 35 \end{array}$$

$$\begin{array}{r} +67 \text{ PP} \\ 17 \end{array}$$

$$\begin{array}{r} +38 \text{ FC} \\ 41 \end{array}$$

$$\begin{array}{r} +19 \text{ Tr} \\ 33 \end{array}$$

157

$$\begin{array}{r} R1 \\ 20-4 \end{array}$$

$$\begin{array}{r} +98 \text{ Tr} \\ 33 \end{array}$$

$$\begin{array}{r} +78 \text{ Tr} \\ 32 \end{array}$$

$$\begin{array}{r} +30 \text{ Tr} \\ 33 \end{array} \quad \begin{array}{r} +10 \text{ Tr} \\ 31 \end{array}$$

156

$$\begin{array}{r} F66 \\ 40 \end{array}$$

$$\begin{array}{r} +98 \text{ Tr} \\ 30 \end{array}$$

$$\begin{array}{r} R4 \\ 17-5 \end{array}$$

$$\begin{array}{r} +94 \text{ PP} \\ 18 \end{array}$$

$$\begin{array}{r} +64 \text{ Tr} \\ 30 \end{array}$$

$$\begin{array}{r} +27 \text{ F.C.} \\ 39 \end{array}$$

155

$$\begin{array}{r} R4 \\ 15-7 \end{array}$$

$$\begin{array}{r} +96 \text{ StP} \\ 29 \end{array}$$

$$\begin{array}{r} +66 \text{ StP} \\ 29 \end{array}$$

$$+56 \text{ Ent}$$

$$\begin{array}{r} +53 \text{ Cor Shed} \\ 113 \end{array}$$

$$\begin{array}{r} +24 \text{ StP} \\ 33 \end{array}$$

$$+10 \text{ Ent}$$

$$\begin{array}{r} +94 \text{ F.C.} \\ 19 \end{array}$$

$$+56 \text{ Ent}$$

$$\begin{array}{r} +31 \text{ Tr} \\ 30 \end{array}$$

$$\begin{array}{r} +13 \text{ PP - Tr} \\ 21 \quad 30 \end{array}$$

154

$$\begin{array}{r} R2 \\ 13-9 \end{array}$$

$$\begin{array}{r} +97 \text{ Tr} \\ 30 \end{array}$$

$$\begin{array}{r} +76 \text{ Tr} \\ 30 \end{array}$$

$$\begin{array}{r} +86 \text{ Cor Ho} \\ 78 \end{array}$$

$$\begin{array}{r} +88 \text{ Tr} \\ 28 \end{array}$$

$$\begin{array}{r} +60 \text{ Cor Shed} \\ 112 \end{array}$$

$$\begin{array}{r} +45 \text{ MB.} \\ 13 \end{array}$$

$$\begin{array}{r} +18 \text{ Tr} \\ 35 \end{array}$$

153

$$\begin{array}{r} R4 \\ 13-9 \end{array}$$

$$+38 \text{ End Orchard}$$

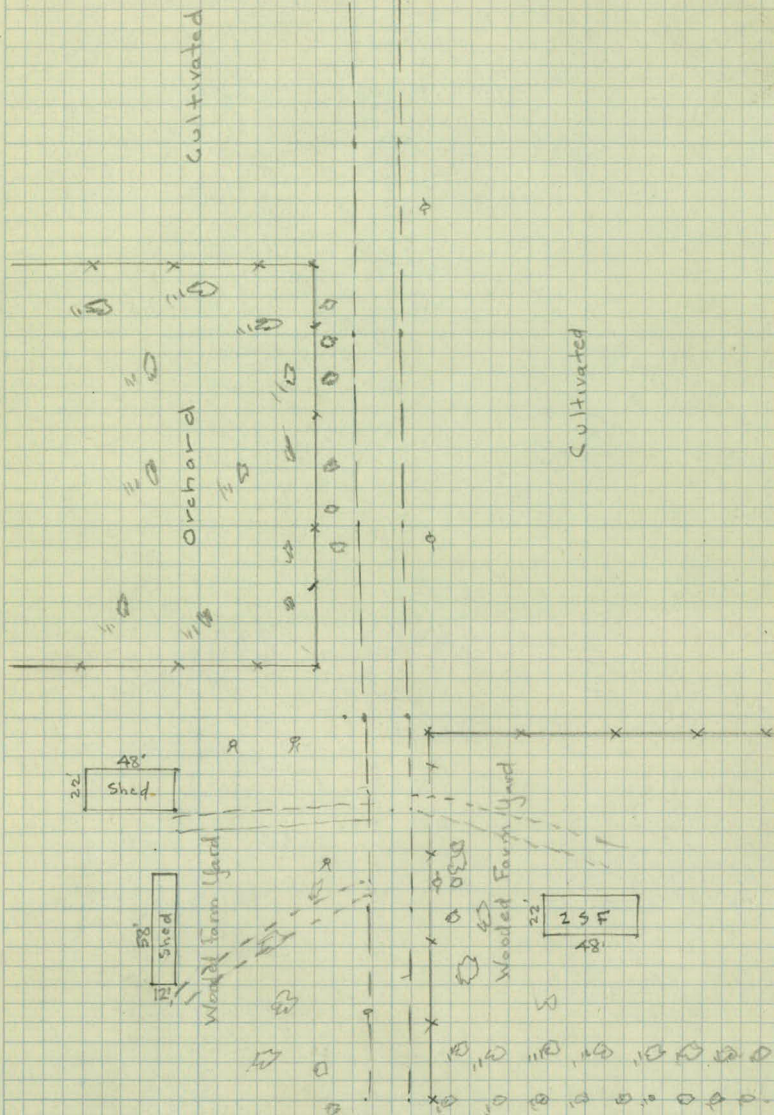
$$31-200$$

$$\text{Bag Orchard}$$

$$27-200$$

$$\begin{array}{r} F66 \\ 21 \end{array}$$

$$\begin{array}{r} +98 \text{ Tr} \\ 30 \end{array}$$



163

162

$$\frac{Rd}{12-12}$$

161

$$\frac{Rd}{12-12}$$

$$\frac{+58 RdSn \text{ (Soft Shoulder)}}{16}$$

$$\frac{+38 \text{ Should.}}{23}$$

$$\frac{+85 \text{ Shoulder (159+92)}}{15}$$

$$\frac{+54 Rd}{13-11}$$

$$\frac{+89 \text{ Shoulder (+05)}}{22}$$

160

$$\frac{Rd}{36}$$

$$\frac{+95 \text{ Shoulder +83}}{60}$$

$$\frac{+56 MB}{29}$$

$$\frac{+36 Tr}{20}$$

$$\frac{+40 Rd}{24-3}$$

$$\frac{+45 \text{ Inst. Sn}}{20}$$

159

$$\frac{+16 Tr}{29}$$

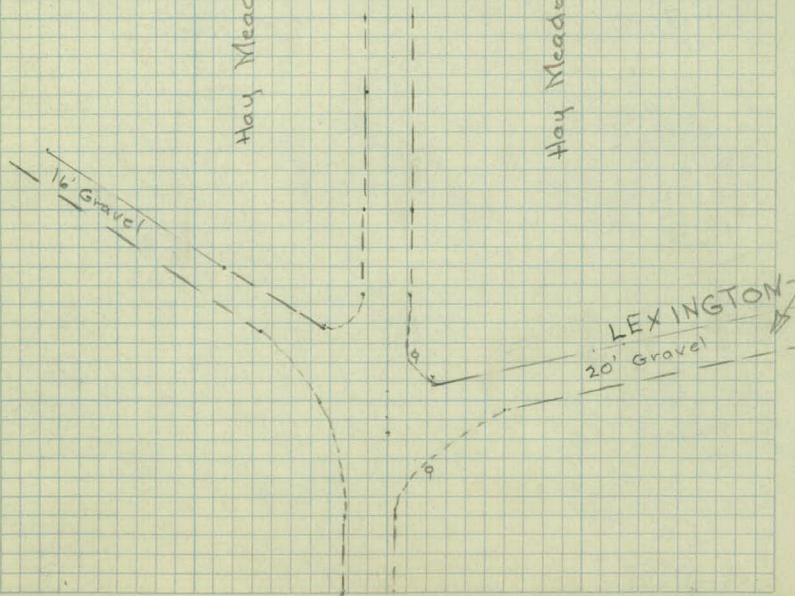
$$\frac{Rd}{24-2}$$

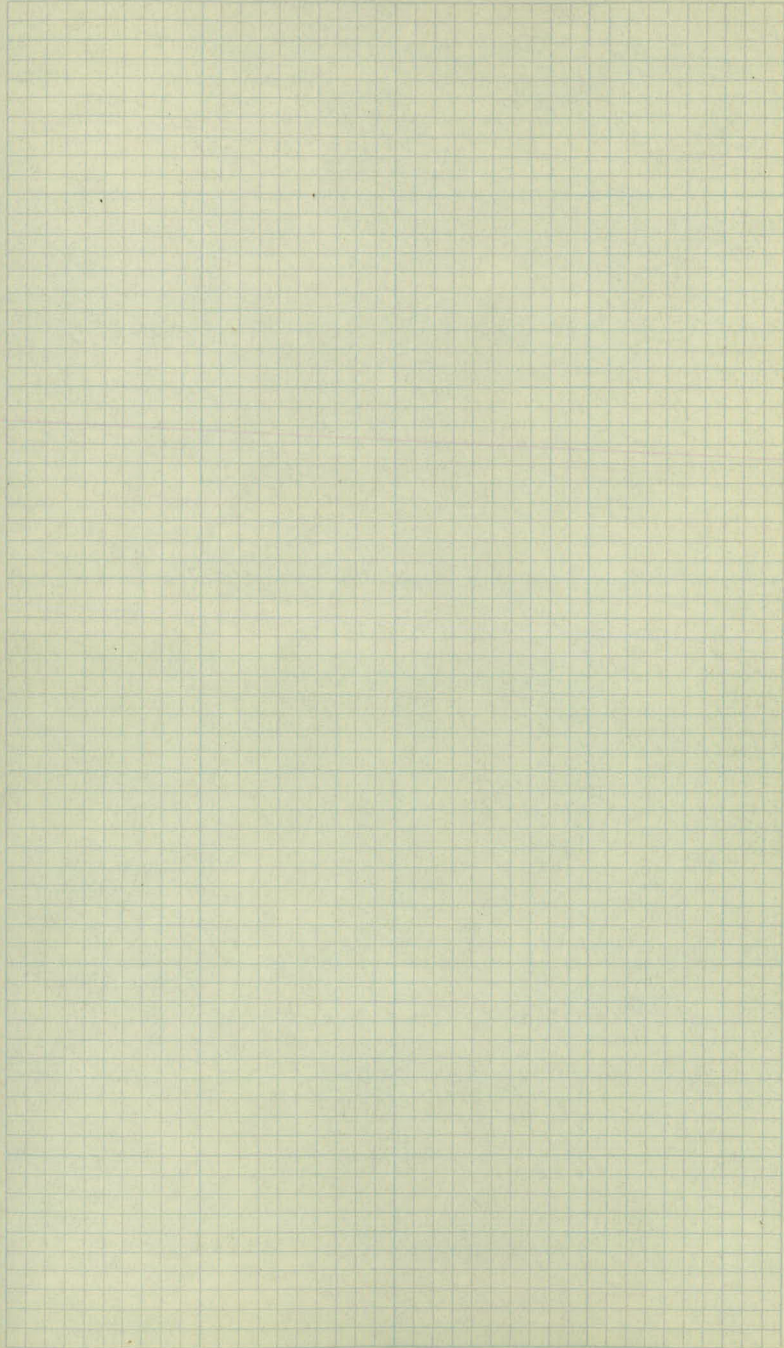
$$\frac{+27 PP}{15}$$

Hay Meadow

Hay Meadow

1/2 Gravel

LEXINGTON
20' Gravel



10/7/86

W.T. Bentley

TOPOG.
for
PROPOSED BRIDGE
AT
CO. RD. J and RICE CREEK

+75 Ent 9'x24' Box
20

169

old Bed
150
+90 End Creek

Cr
20-38

+50 old Creek Bed
40

168

Cr
24-49

Cr
21-35

+65 Cr
24-54

167

Cr
43-68

Cr
23-37

+70 old Dtl.
70

+35 Cr
60-85

166

Cr
51-56

Cr
23-27
+90 Cr
32-51

165

Cr
26

+15-18'x48' CNL
24-24

+88 FC
40

Cr
19-23

+90 old Creek Bed X3

+55 E Cr
40-150

164

163

Rd
10-10

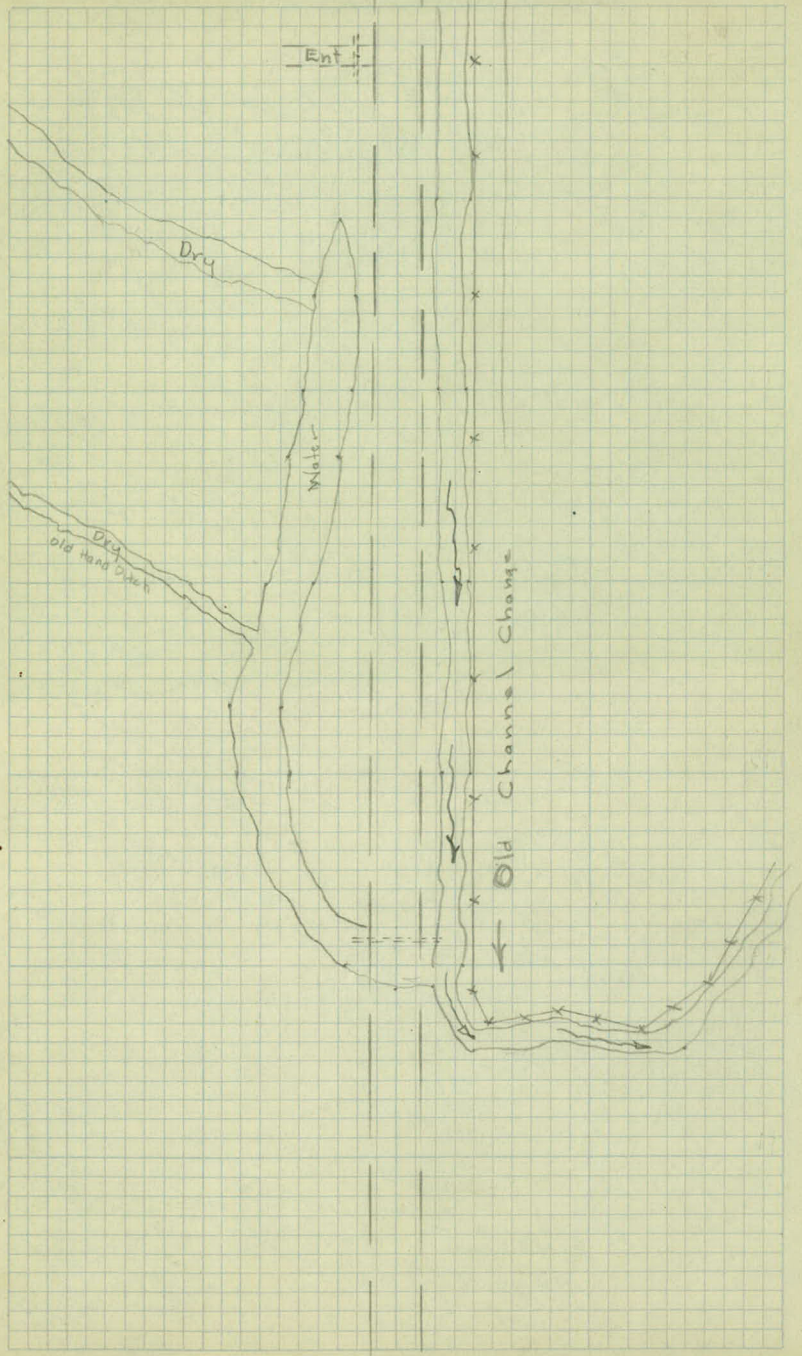
Ent

Dry

Water

Dry
old hand ditch

← Old Channel Change



$$\begin{array}{r} +83 \text{ Cr} \\ 20-295-315 \end{array}$$

$$\begin{array}{r} +97 \text{ 3 Lines } 48' \times 44' \\ 22-22 \\ \hline +40 \text{ Cr} \\ 60-75 \end{array}$$

$$\begin{array}{r} +87 \text{ Cr Pl} \\ 40-52 \\ \hline +63 \text{ FC} \\ 27 \\ \hline \text{Cr} \\ 190-170 \end{array}$$

$$\begin{array}{r} \text{Cr} \\ 185-200 \end{array}$$

176

$$\begin{array}{r} +20 \text{ Cr} \\ 222-242 \end{array}$$

175

$$\begin{array}{r} \text{Cr} \\ 133-163 \end{array}$$

174

$$\begin{array}{r} +70 \text{ Cr} \\ 20 \end{array}$$

$$\begin{array}{r} +73 \text{ E Cr} \\ 24 \end{array}$$

$$\begin{array}{r} +47 \text{ Cr} \\ 26 \end{array}$$

$$\begin{array}{r} +53 \text{ Cr (End Ch. Ch.)} \\ 24-37 \end{array}$$

173

$$\begin{array}{r} +10 \text{ Cr} \\ 82-110 \end{array}$$

$$\begin{array}{r} \text{Cr} \\ 23-37 \end{array}$$

172

$$\begin{array}{r} \text{Cr} \\ 36-61 \end{array}$$

$$\begin{array}{r} \text{Cr} \\ 23-37 \end{array}$$

$$\begin{array}{r} +70 \text{ Ed Cr} \\ 50-25 \end{array}$$

$$\begin{array}{r} +30 \text{ Ed Cr} \\ 22 \end{array}$$

171

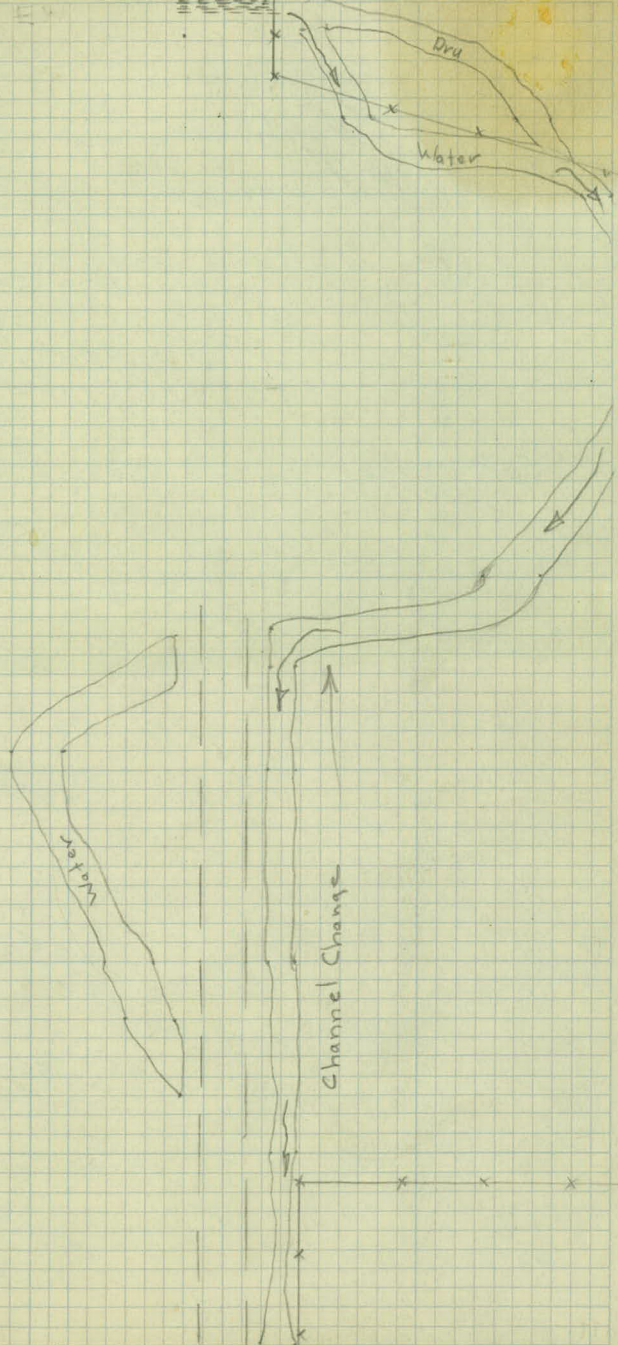
$$\begin{array}{r} \text{Cr} \\ 24-37 \end{array}$$

$$\begin{array}{r} +85 \text{ FC} \\ 40 \end{array}$$

170

$$\begin{array}{r} \text{old Bed} \\ 250 \end{array}$$

$$\begin{array}{r} \text{Cr} \\ 20-33 \end{array}$$



$$\begin{array}{r} +30 \text{ Cr} \\ 180-210 \\ +10 \text{ NoS Fcc} \\ \hline 27 \end{array}$$

179

$$\begin{array}{r} +53 \text{ FC} \\ 27 \\ +42 \text{ Ent (15" x 20CM)} \\ \hline 20 \end{array}$$

178

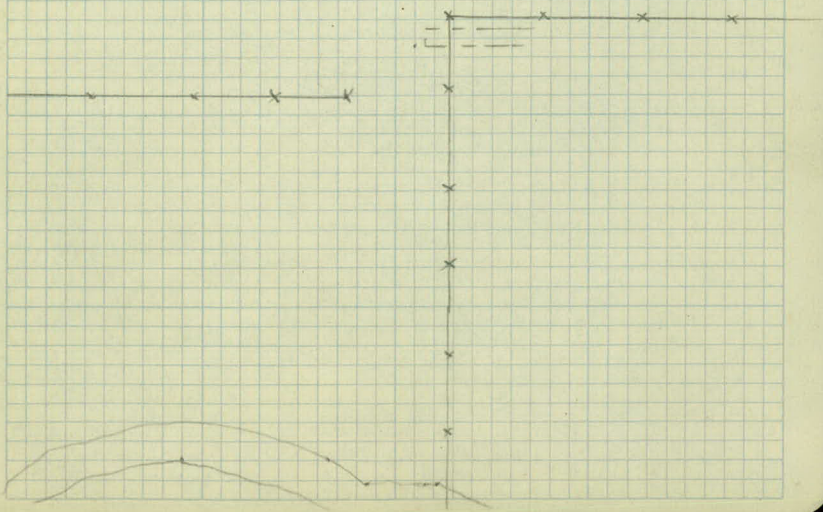
$$\begin{array}{r} \text{Cr} \\ 350 \text{ L} \\ \hline \end{array}$$

$$\begin{array}{r} \text{Fcc} \\ 27 \end{array}$$

$$\begin{array}{r} +21 \text{ Cr} \\ 34-110 \end{array}$$

177

$$\begin{array}{r} +08 \text{ Cr} \\ 16-24 \end{array}$$





4-16

184

Br & Woods
37-77Rd
10-10

183

Br & Woods
35-65+35 (U.S.G.S. B.M.)
34

182

Rd
10-10+82 Brush Woods
32'

181

180

Rd
9-10

179

Hay Meadow

Brush & Woods

Cultivated

191 Woods + Br
23-200

+70 Woods + Brush
70

190

Rd
10-10

189

188

Rd
11-9

187

+43-24" x 38" CM (New)
19-19

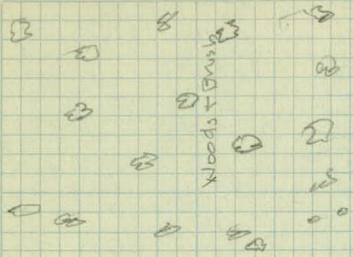
186

Rd
10-10

+35 Ent R/L

185

+20 End Br + Wood
37-75



Hay Meadow

Hay Meadow



Ent

Ent



$$\frac{+30 \text{ End Woods}}{37}$$

$$\frac{+30 \text{ End Woods}}{40}$$

198

$$\frac{Rd}{10-10}$$

$$\frac{Fce}{34}$$

$$\frac{+12-24 \times 36 \text{ CM}}{19-17}$$

197

$$\frac{+67 \text{ Bay Br. + Woods}}{40}$$

196

$$\frac{\text{Br. + Woods}}{36}$$

$$\frac{Rd}{10-10}$$

$$\frac{Fce}{34}$$

$$\frac{+90 \text{ Ent (15' 30' CM)}}{19}$$

195

194

$$\frac{\text{Br. + Woods}}{37}$$

$$\frac{Rd}{10-10}$$

$$\frac{Fce}{33}$$

193

$$\frac{+75 \text{ FC}}{33}$$

192

$$\frac{\text{Br. + Woods}}{27}$$

$$\frac{Rd}{10-10}$$

Brush

Brush

Brush Woods

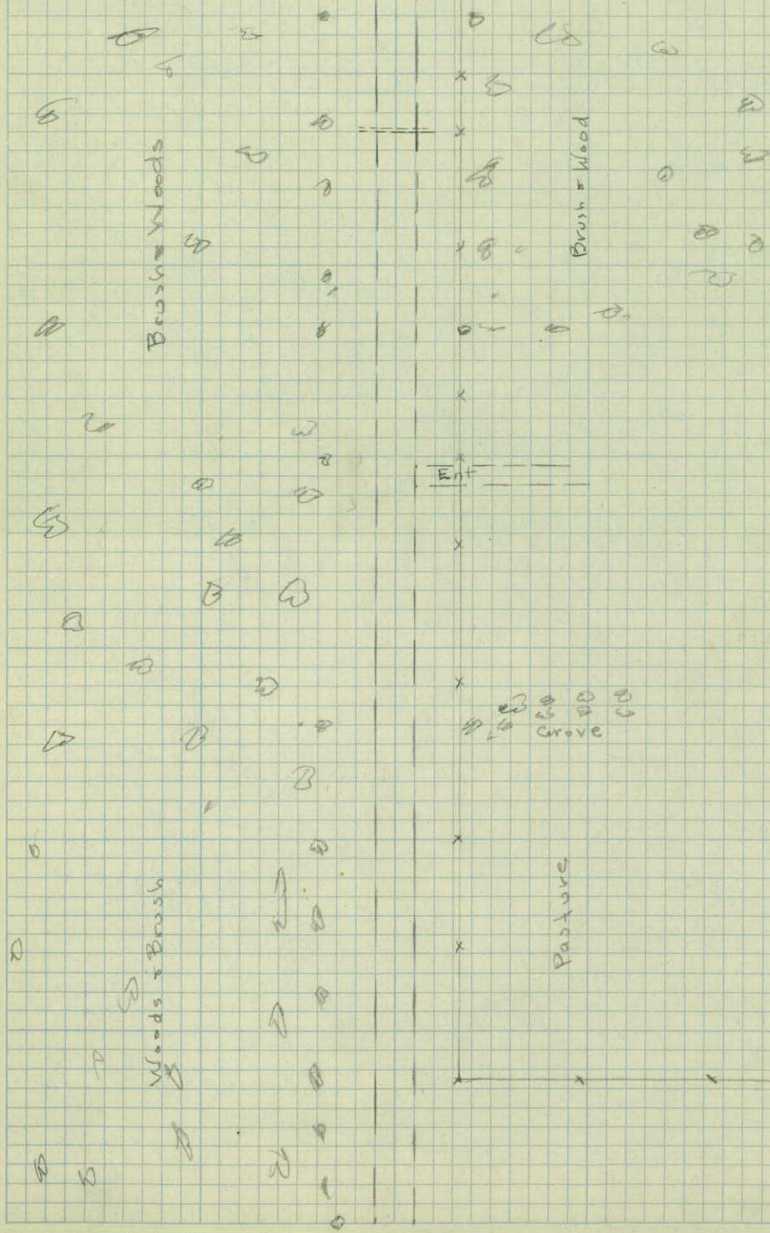
Brush & Wood

ENT

Crove

Pasture

Woods & Brush



+98 FS.

205

204

$\frac{R1}{10-19}$

+01 USGS BM

39

$\frac{Fcc}{42}$

203

+50 Ent

202

$\frac{R1}{10-10}$

$\frac{Fcc}{33}$

201

200

$\frac{Fcc}{33}$

199

Bush & Hay Meadow

Fm

Bush & Pasture



$$\begin{array}{r} +65 \text{ Grove} \\ \hline 85 \end{array}$$

2.12

$$\begin{array}{r} R1 \\ \hline 10-10 \end{array}$$

$$\begin{array}{r} +40 \text{ Grove} \\ \hline 35 \end{array}$$

$$\begin{array}{r} +62 \text{ End Br. r Woods} \\ \hline 35 \end{array}$$

$$\begin{array}{r} +62 \text{ End Br. r W.} \\ \hline 33 \end{array}$$

2.11

2.10

$$\begin{array}{r} \text{Woods} \\ \hline 33 \end{array}$$

$$\begin{array}{r} R1 \\ \hline 10-10 \end{array}$$

$$\begin{array}{r} \text{Woods} \\ \hline 33 \end{array}$$

2.09

$$\begin{array}{r} +43-24 \times 42' \text{ G.M.} \\ \hline 21-21 \end{array}$$

2.08

$$\begin{array}{r} R1 \\ \hline \end{array}$$

$$\begin{array}{r} \text{Br. r W.} \\ \hline 35 \end{array}$$

$$\begin{array}{r} +55 \text{ Beg Brush Woods} \\ \hline 34 \end{array}$$

2.07

+04 Ent

2.06

$$\begin{array}{r} R1 \\ \hline 10-10 \end{array}$$

$$\begin{array}{r} \text{Beg Woods + Brush} \\ \hline 35 \end{array}$$

9-16

Hay

Hay

Brush & Woods

Brush & Woods

Ent

219

218

$\frac{Rd}{10-10}$

$\frac{+63 Tree}{18}$

+70 Day Cult

217

216

$\frac{Rd}{10-10}$

215

$\frac{+83 Ent 15 \times 20' CM}{19}$
 $\frac{+60 End Grove}{35}$

$\frac{+83 Ent 15 \times 20' CM (New)}{19}$

214

$\frac{Rd}{10-10}$

$\frac{+10 Grove}{35}$

213

$\frac{+40 Grove}{150}$

Waste Land & Pasture

Cultivated

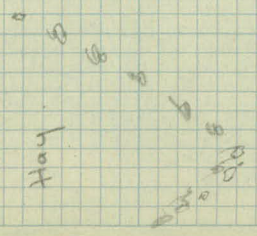
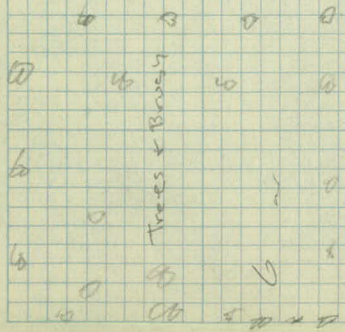
Waste Land & Pasture

Trees & Brushy

Hay

Ent

Ent



226

$$\frac{21}{10-10}$$

225

224

$$\frac{21}{10-10}$$

223

$$\frac{+35 \text{ Ents } 12 \times 20 \text{ CM}}{23}$$

222

$$\frac{21}{10-10}$$

221

220

$$\frac{21}{10-10}$$

Waste Land & Pasture

Waste Land & Pasture

Cultivated

Cultivated

$$\begin{array}{r} +95 \text{ Ent } 12" \times 20' \text{ CM} \\ \hline 23 \end{array}$$

233

$$+85 \text{ Culv } 24' \times 58$$

$$\begin{array}{r} +75 \text{ End Culv} \\ \hline 27 \end{array}$$

$$\begin{array}{r} +35 \text{ Ent } (12' \times 20' \text{ CM}) \\ \hline 21 \end{array}$$

232

$$\begin{array}{r} \text{Circle K} \\ \hline 2.00 \end{array}$$

231

230

$$\begin{array}{r} 24 \\ \hline 10-10 \end{array}$$

229

$$+60 \text{ End W.L.}$$

228

$$+70 \text{ End Culv}$$

227

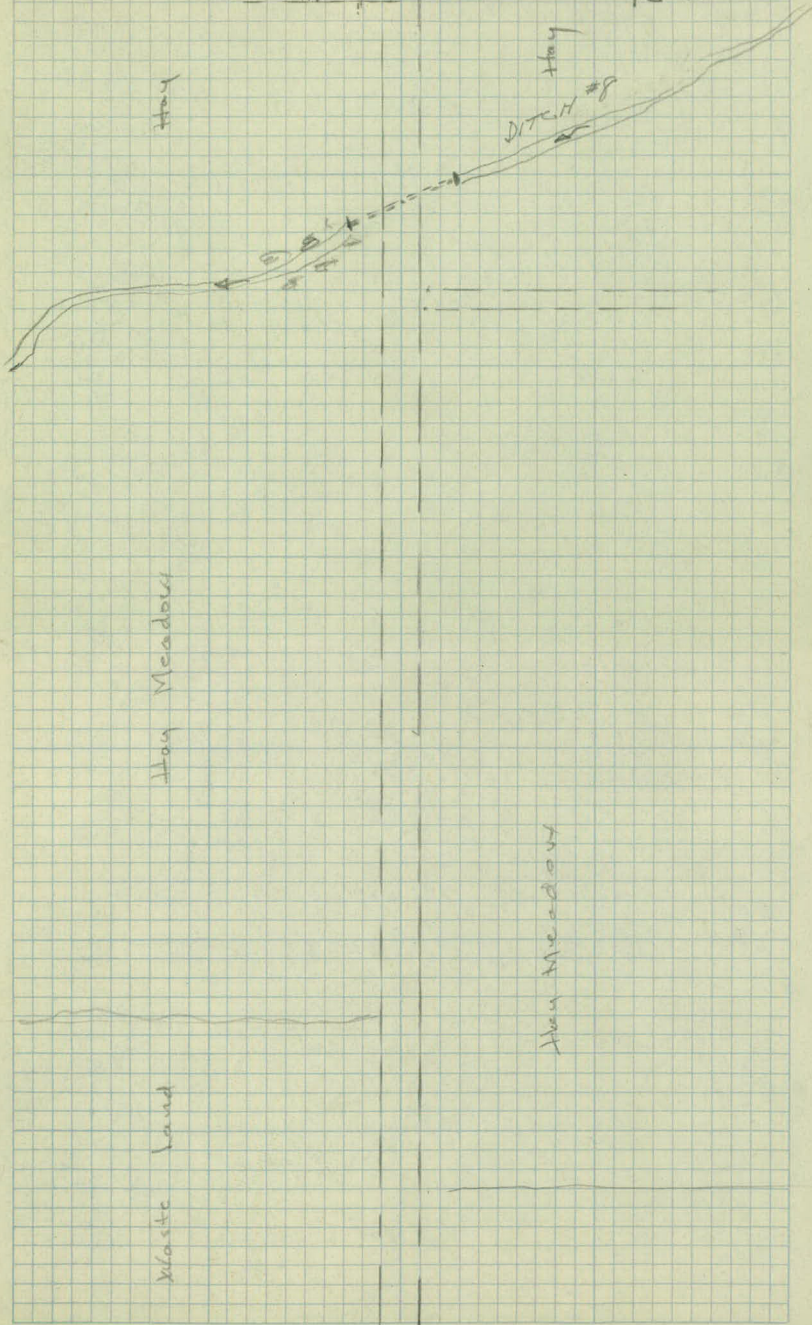
Hay

DITCH #8

Hay Meadow

Hay Meadow

Klastic land



240

$$\begin{array}{r} R_1 \\ 10-10 \end{array}$$

239

238

$$\begin{array}{r} R_1 \\ 10-10 \end{array}$$

237

236

$$\begin{array}{r} R_1 \\ 10-10 \end{array}$$

235

+55 Bag Cult

234

$$\begin{array}{r} R_1 \\ 10-10 \end{array}$$

Hay & waste land

Cultivated

247

246

$$\frac{R9}{10-10}$$

$$\frac{+50 Tr}{28}$$

245

$$\frac{+64 Tr}{28} \quad \frac{+78 Ent}{21}$$

$$\frac{+32 Tr}{30}$$

$$\frac{+13 Tr}{28}$$

244

$$\frac{R9}{10-10}$$

$$\frac{+92 Ent + 15' \times 20' CM}{20}$$

$$\frac{+93 Cor Ho}{60}$$

$$\frac{+63 Tr}{28}$$

$$\frac{+78 Tr}{27-37}$$

$$\frac{+38 Cor Shed}{60}$$

$$\frac{+12 End Row Willi.}{28}$$

243

$$\frac{+45 Beg Row Willows}{30}$$

242

$$\frac{R9}{10-10}$$

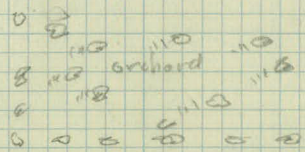
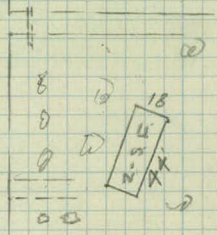
241

Beg Cult

18x44
14-16

Cultivated

Cultivated



25A

$$\frac{24}{-10}$$

253

252

$$\frac{R4}{10-10}$$

251

250

$$\frac{24}{10-10}$$

249

248

$$\frac{24}{10-10}$$

Cultivated

Cultivated

260

$$\frac{Rd}{10}$$

$$\frac{Fck}{26}$$

$$\begin{array}{r} +47 PP \\ \hline 27 \\ +18 \text{ Stop Sn} \\ \hline 19 \\ +08 \text{ 1c Rd Sn - Guy Pole} \\ \hline 32 \end{array} \quad \frac{93}{93}$$

259

$$\begin{array}{r} +89 \text{ Shoulder} \\ \hline 50 \end{array}$$

$$\begin{array}{r} +40 PP \\ \hline 18 \end{array}$$

258

$$\begin{array}{r} Rd Sn. \\ \hline 18 \end{array}$$

$$\begin{array}{r} +62 Tr \\ \hline 24 \\ +44 Tr \\ \hline 24 \\ +33 Rd \checkmark \\ \hline 12-12 \end{array} \quad \begin{array}{r} +83 Rd Sn \\ \hline 17 \\ +48 MB - Bag Fee \\ \hline 15 \end{array} \quad \begin{array}{r} +34 TP \\ \hline 18 \end{array}$$

$$\begin{array}{r} +85 \text{ Edge = B.T.} \\ +58 \text{ Edge = Black Top} \\ +54 \text{ Shoulder} \checkmark \\ \hline 32-36 \end{array} \quad \begin{array}{r} +89 \text{ Shoulder} \\ \hline 60 \end{array}$$

$$\begin{array}{r} +33 Rd \checkmark \\ \hline 10-10 \\ Rd \checkmark \\ \hline 10-10 \end{array}$$

$$\begin{array}{r} +40 \text{ 2 Rd Sns} \\ \hline 24 \end{array}$$

257

$$\begin{array}{r} +12 FC (+34) \\ \hline 38 \end{array}$$

256

$$\frac{Rd}{10 \times 10}$$

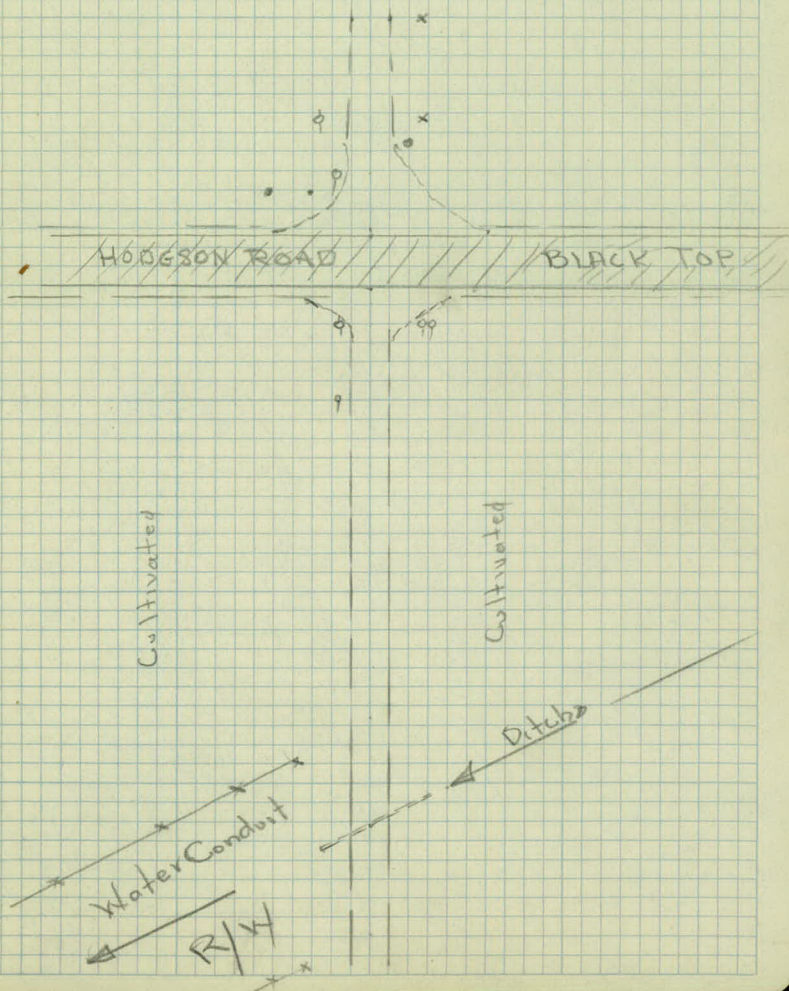
+43 Ent

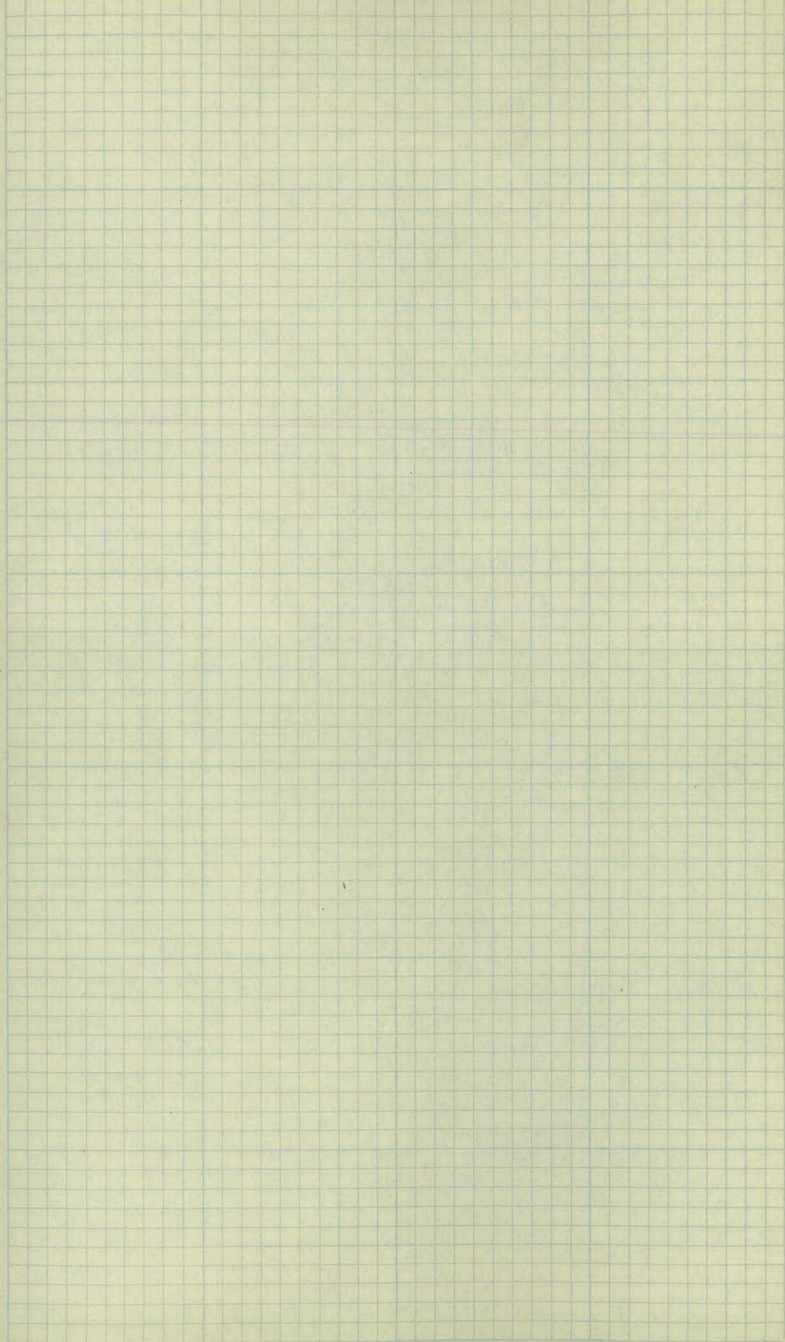
$$\begin{array}{r} +64 \text{ End GWH} \\ \hline 26 \end{array}$$

+75 ~~24" x 60" CM~~

255

$$\begin{array}{r} +04 FC (+21) \\ \hline 33 \end{array}$$





Topog
North County Line
Hodgson Road East

$$\begin{array}{r} 124 \\ 6-15 \\ \hline \end{array} \quad \begin{array}{r} Fc \\ 31 \\ \hline \end{array} \quad \begin{array}{r} Trees \\ 30 \\ \hline \end{array}$$

$$\begin{array}{r} +81PP \\ 27 \\ \hline \end{array}$$

265

$$+73 FEnt$$

$$\begin{array}{r} +11 TP - Beg Row Trees \\ 18 \quad 29 \\ \hline \end{array}$$

$$\begin{array}{r} +29 Rd50 \\ 11 \\ \hline \end{array}$$

264

$$\begin{array}{r} Rd \\ 6-13 \\ \hline \end{array} \quad \begin{array}{r} Fc \\ 29 \\ \hline \end{array}$$

$$\begin{array}{r} +91 TP \\ 17 \\ \hline \end{array}$$

$$\begin{array}{r} +61 PP \\ 27 \\ \hline \end{array}$$

263

$$\begin{array}{r} +73 TP \\ 17 \\ \hline \end{array}$$

$$\begin{array}{r} +17 Tr \\ 27 \\ \hline \end{array}$$

$$\begin{array}{r} +37 Tr \\ 26 \\ \hline \end{array}$$

$$\begin{array}{r} +61 Tr \\ 26 \\ \hline \end{array}$$

262

$$\begin{array}{r} Rd \\ 7-13 \\ \hline \end{array}$$

$$\begin{array}{r} Fc \\ 28 \\ \hline \end{array}$$

$$\begin{array}{r} +63 Tr \\ 27 \\ \hline \end{array}$$

$$\begin{array}{r} +44 Tr \\ 26 \\ \hline \end{array}$$

$$\begin{array}{r} +81 Tr \\ 26 \\ \hline \end{array}$$

$$\begin{array}{r} +52 TP \\ 17 \\ \hline \end{array}$$

$$\begin{array}{r} +29 P.P. \\ 27 \\ \hline \end{array}$$

261

$$\begin{array}{r} Rd \\ 9-11 \\ \hline \end{array}$$

$$\begin{array}{r} Fc \\ 27 \\ \hline \end{array}$$

$$\begin{array}{r} +34 TP \\ 17 \\ \hline \end{array}$$

260

Hay Field



Cultivated

$$\begin{array}{r} +87 \text{ PP} \\ \hline 29 \\ +84 \text{ End Cully} \\ \hline 12 \end{array}$$

+63 E 14 Town Road

$$\begin{array}{r} +73 \text{ Cully X 5 (12' x 36' CM)} \\ \hline +59 \text{ End Cully} \\ \hline 15 \end{array}$$

272

$$\begin{array}{r} R4 \\ \hline 5-15 \end{array}$$

$$\begin{array}{r} F5 \\ \hline 32 \end{array}$$

$$\begin{array}{r} +35 \text{ PP} \\ \hline 28 \end{array}$$

$$\begin{array}{r} +17 \text{ TP} \\ \hline 20 \end{array}$$

271

$$\begin{array}{r} +30 \text{ TP} \\ \hline 33 \end{array}$$

270

$$\begin{array}{r} R4 \\ \hline 4-16 \end{array}$$

$$\begin{array}{r} F5 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +55 \text{ PP} \\ \hline 27 \end{array}$$

$$\begin{array}{r} +93 \text{ TP} \\ \hline 20 \end{array}$$

$$\begin{array}{r} +84 \text{ End Row Trees} \\ \hline 32 \end{array}$$

269

$$\begin{array}{r} +16 \text{ T.P.} \\ \hline 18 \end{array}$$

268

$$\begin{array}{r} R4 \\ \hline 4-17 \end{array}$$

$$\begin{array}{r} \text{Trees} \\ \hline 32 \end{array}$$

$$\begin{array}{r} F5 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +69 \text{ PP} \\ \hline 28 \end{array}$$

$$\begin{array}{r} +51 \text{ TP} \\ \hline 18 \end{array}$$

267

$$\begin{array}{r} +16 \text{ Cor Ho} \\ \hline 69 \end{array}$$

$$+15 \text{ Ent}$$

$$\begin{array}{r} +32 \text{ TP} \\ \hline 18 \end{array}$$

$$\begin{array}{r} +12 \text{ Cor Gar} \\ \hline 78 \end{array}$$

266

+63-14' Town Road

Cultivated

Cultivated



Ent

$$8 \frac{RD}{-11} \quad \frac{Fc}{24}$$

$$+98 TP$$

$$\underline{20}$$

$$+51 PP$$

$$\underline{28}$$

279

$$+75 TP$$

$$\underline{20}$$

278

$$\frac{RD}{8-12} \quad \frac{Fc}{25}$$

$$+86 PP$$

$$\underline{28}$$

$$+52 TP$$

$$\underline{21}$$

277

$$+21 PP$$

$$\underline{28}$$

$$+29 TP$$

$$\underline{21}$$

276

$$\frac{RD}{8-12} \quad \frac{Fc}{25}$$

$$+53 Fc$$

$$\underline{26}$$

$$+08 TP$$

$$\underline{21}$$

275

$$+55 PP$$

$$\underline{28}$$

274

$$\frac{RD}{7-13} \quad \frac{Fc}{28}$$

$$+92 TP$$

$$\underline{21}$$

273

Hay Land

0

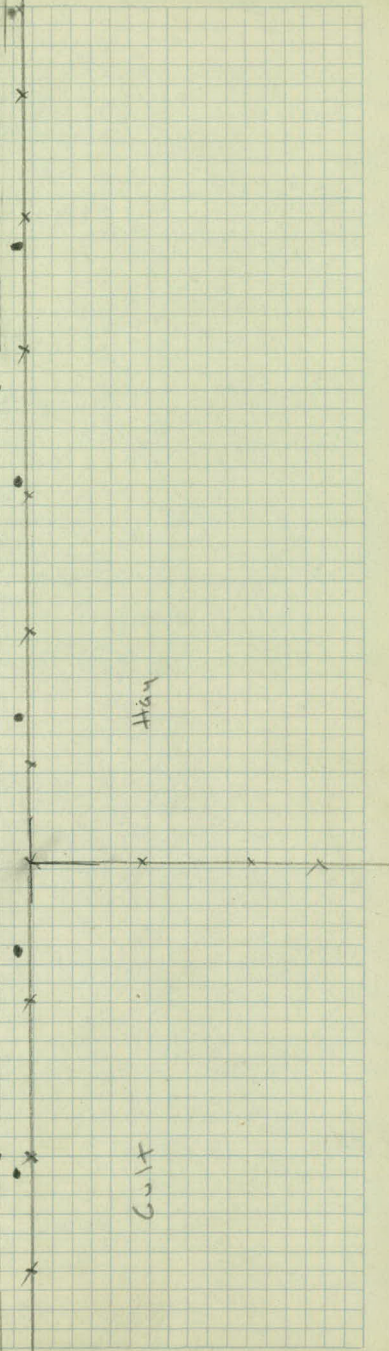
0

0

0

1
2
3

4
5
6



286

$$\frac{R9}{12-9}$$

285

$$\frac{+68TP - FC}{19} \quad \frac{(End Fce)}{23}$$

$$\frac{+51PP}{28}$$

284

$$\frac{R9}{9-10}$$

$$\frac{Fc}{23}$$

$$+89Ent$$

$$\frac{+80TP}{20}$$

283

$$\frac{+84PP}{28}$$

$$\frac{+52TP}{19}$$

282

$$\frac{R9}{8-10}$$

$$\frac{Fc}{23}$$

$$\frac{+17PP}{27}$$

$$\frac{+28TP}{19}$$

281

$$+30-12" \times 40CM$$

$$17-23 \quad +33-3TPs$$

$$\frac{+32FC (+27)}{23}$$

280

Hay Field

Hay Field

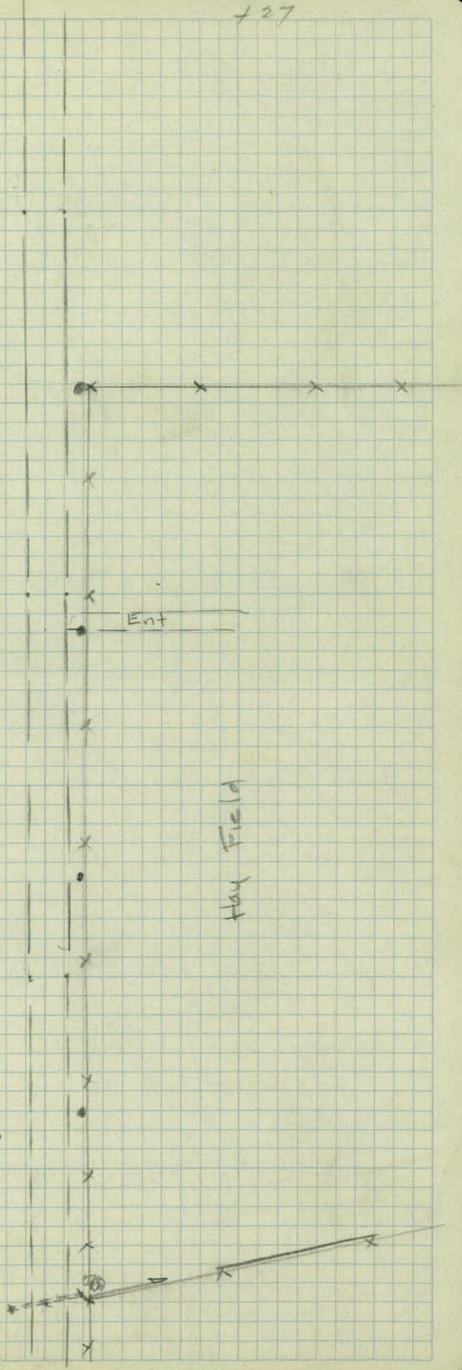
Ent

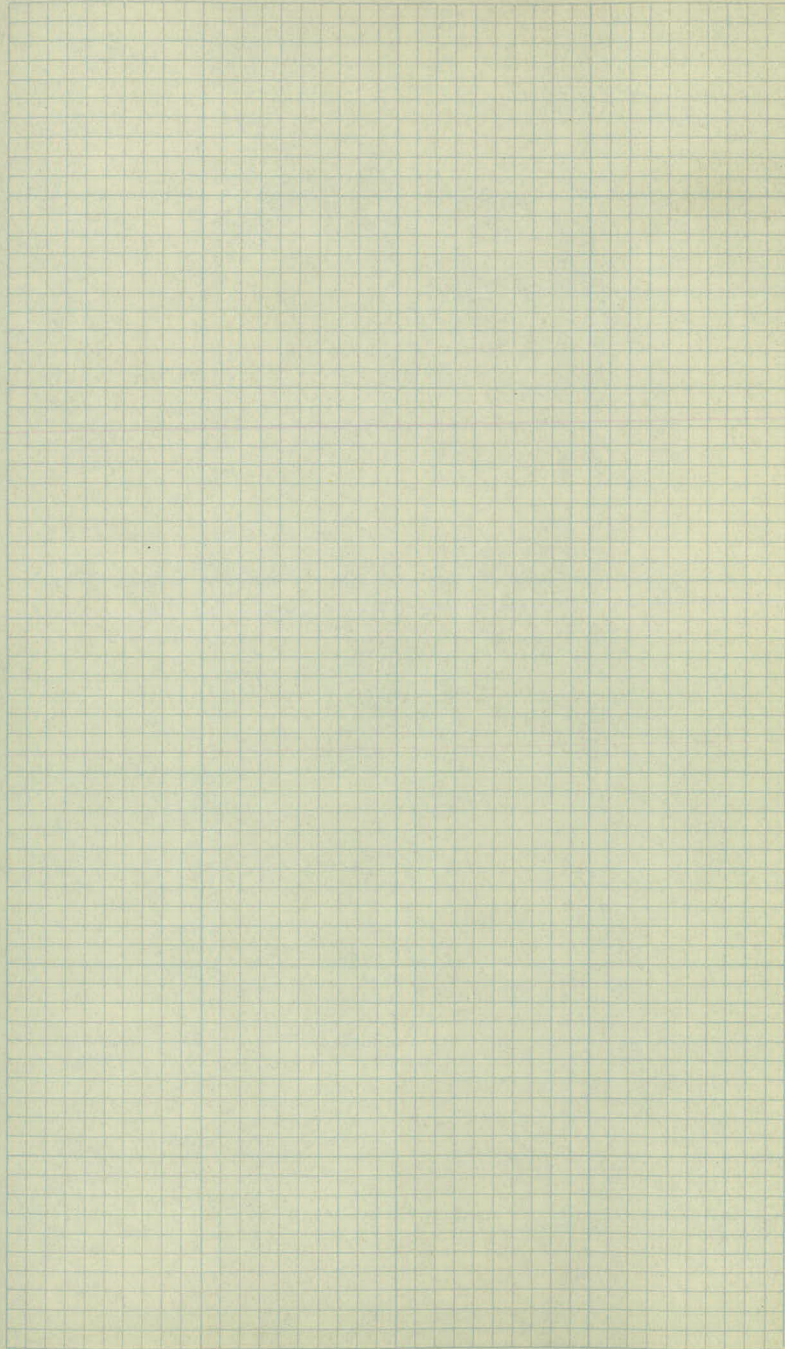
2' Bot Ditch

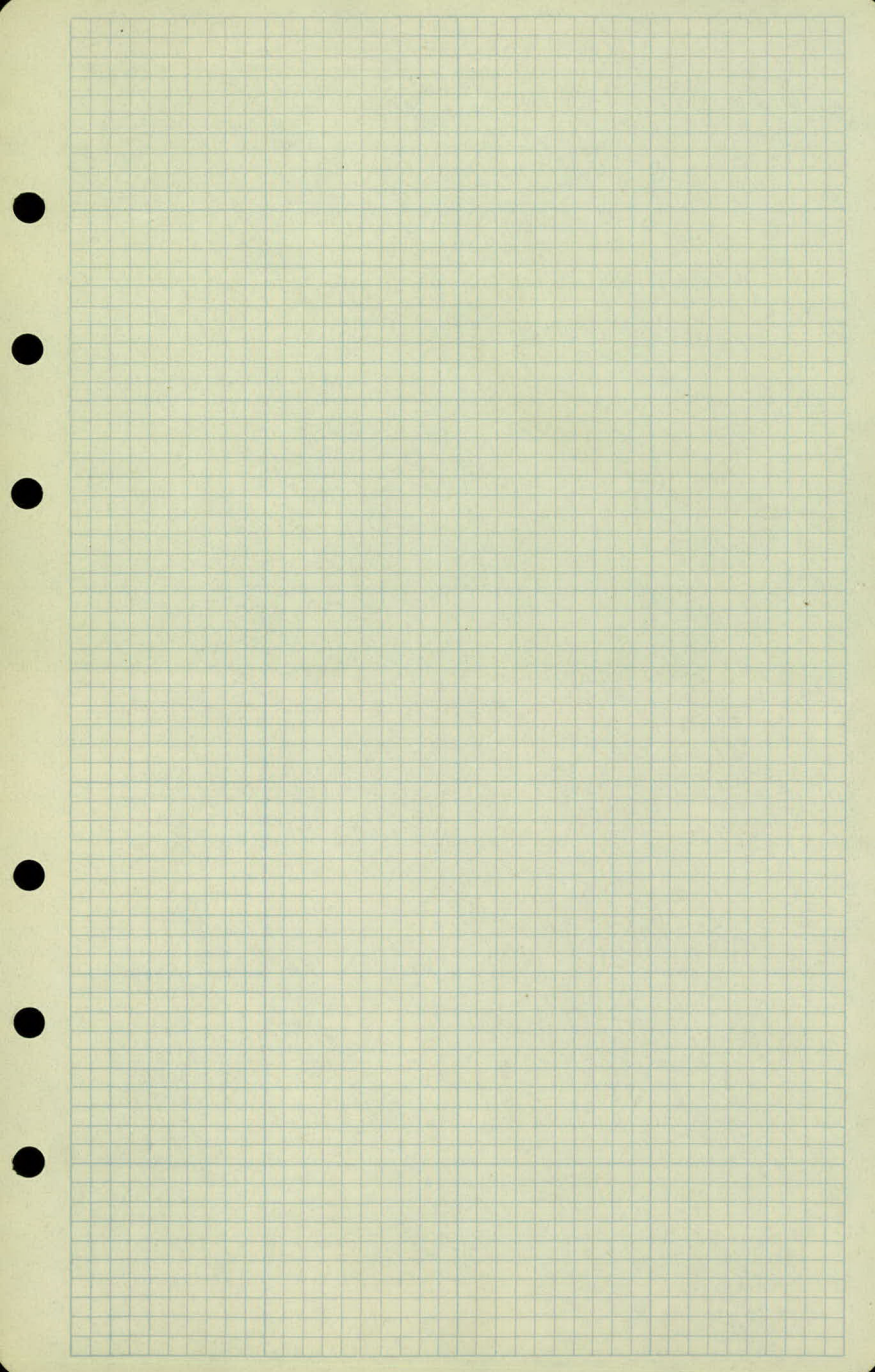
9

6

9







$$\begin{array}{r} +93 \text{ FC} \\ \hline 29 \end{array}$$

+97 Ent

+89 Ent

$$\begin{array}{r} +57 \text{ FC} \\ \hline 21 \end{array}$$

$$\begin{array}{r} +49 \text{ TP} \\ \hline 15 \end{array}$$

291

$$\begin{array}{r} +07 \text{ PP} \\ \hline 28 \end{array}$$

$$\begin{array}{r} +27 \text{ TP} \\ \hline 15 \end{array}$$

290

$$\begin{array}{r} Rq \\ 12-9 \end{array}$$

+61 Ent

+63 Rd Sn

$$\begin{array}{r} +50 \text{ PP} \\ \hline 28 \end{array}$$

$$\begin{array}{r} 16 \\ +48 \text{ Guy P} \\ \hline 16 \end{array}$$

289

$$\begin{array}{r} +98 \text{ TP} \\ \hline 16 \end{array}$$

288

$$\begin{array}{r} Rq \\ 13-8 \end{array}$$

$$\begin{array}{r} +86 \text{ PP} \\ \hline 28 \end{array}$$

$$\begin{array}{r} +68 \text{ TP} \\ \hline 17 \end{array}$$

287

$$\begin{array}{r} +17 \text{ P.P.} \\ \hline 28 \end{array}$$

$$\begin{array}{r} +39 \text{ TP} \\ \hline 18 \end{array}$$

286

Cultivated

Cultivated

$$\frac{+92 PP + FC}{28}$$

298

$$\frac{FC}{28}$$

$$\frac{Rd}{13-7}$$

$$\frac{+27 FC}{14}$$

$$\frac{FC}{12}$$

$$\frac{+98 TP}{13}$$

$$\frac{+35 PP}{28}$$

297

$$\frac{+68 TP}{14}$$

296

$$\frac{FC}{28}$$

$$\frac{Rd}{11-5}$$

$$\frac{FC}{14}$$

$$\frac{+77 PP}{28}$$

$$\frac{+47-9'' \times 30' CM}{16-14}$$

$$\frac{+36 TP}{14}$$

295

$$\frac{PP +22 Rd 30}{28 \quad 14}$$

294

$$\frac{FC}{29}$$

$$\frac{Rd}{12-8}$$

$$\frac{+07 TP}{14}$$

$$\frac{FC}{15}$$

293

$$+10 Ent$$

$$\frac{+68 PP}{28}$$

$$\frac{+75 TP}{14}$$

$$\frac{+77 FC}{14-22}$$

292

$$\frac{+06 FC}{28}$$

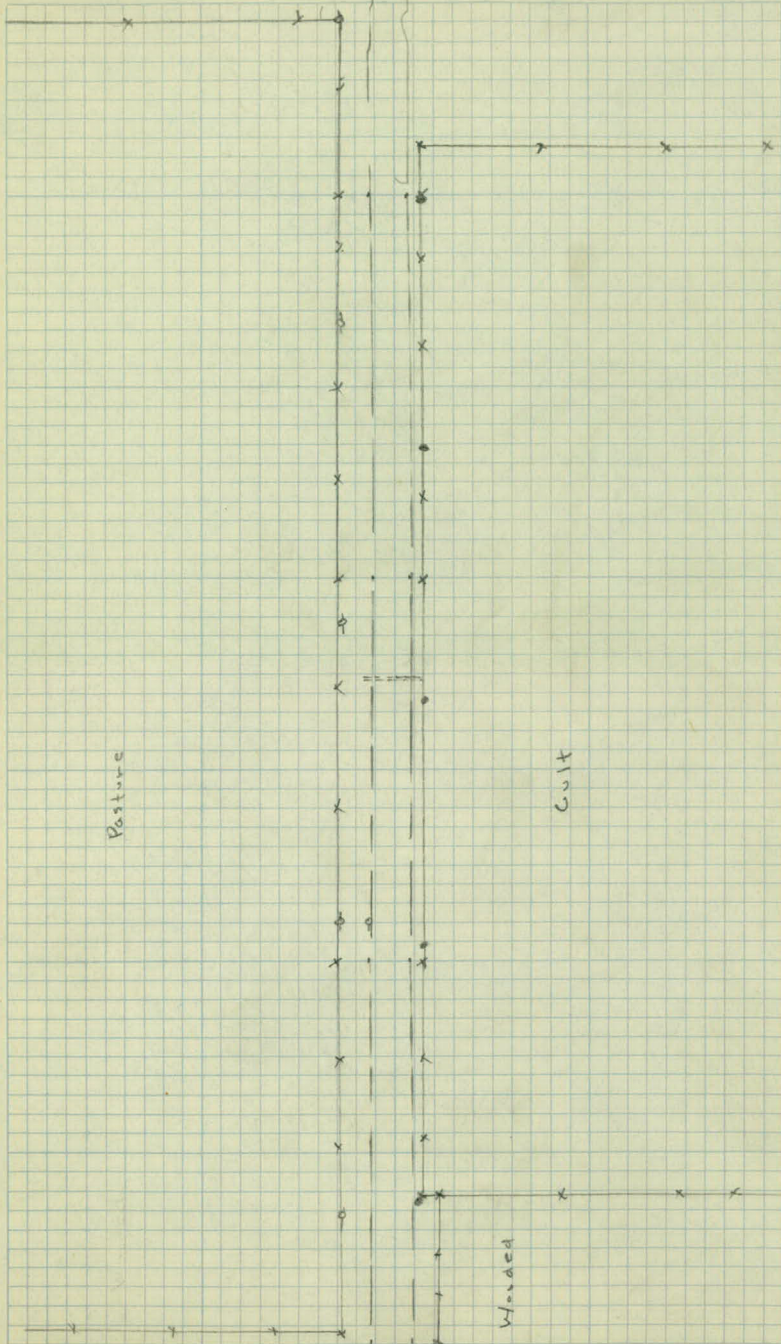
$$\frac{Rd}{13-9}$$

$$\frac{Ed}{21}$$

Pasture

Cult

Wooded



$$\frac{+44 \text{ PP}}{28}$$

305

$$\frac{+44 \text{ T.P.}}{12}$$

$$\frac{+152 \text{ or Ho}}{123}$$

$$\frac{+59 \text{ Ent} + 12' \times 20' \text{ CM}}{19}$$

304

$$\frac{+84 \text{ PP}}{28} \quad \frac{+99 \text{ Tr}}{20}$$

Rd
11-6

$$\frac{+25 \text{ TP}}{12}$$

303

$$\frac{+99 \text{ TP}}{12}$$

$$+52 \text{ Ent}$$

$$\frac{+20 \text{ PP}}{28}$$

302

Rd
13-6

$$\frac{+77 \text{ TP}}{12}$$

301

$$\frac{+57 \text{ PP}}{28}$$

$$\frac{+50 \text{ TP}}{12}$$

300

Rd
11-7

$$\frac{+25 \text{ TP}}{12}$$

299

$$+04 \text{ Ent}$$

25 F 24
30

Cult

Cult

312

311

$$\begin{array}{r} RA \\ 11-7 \\ \hline \end{array} \quad \begin{array}{r} FC \\ 26-42 \\ \hline \end{array}$$

$$\begin{array}{r} +50 TP \\ 12 \\ \hline \end{array}$$

310

$$\begin{array}{r} RA \\ 11-7 \\ \hline \end{array} \quad \begin{array}{r} FC \\ 26-42 \\ \hline \end{array}$$

309

$$\begin{array}{r} +27 TP \\ 12 \\ \hline +5 Ditch (+11) \\ 26 \end{array}$$

308

$$\begin{array}{r} RA \\ 12-7 \\ \hline \end{array} \quad \begin{array}{r} FC \\ 26-42 \\ \hline \end{array} \quad \begin{array}{r} TP \\ 11 \\ \hline \end{array}$$

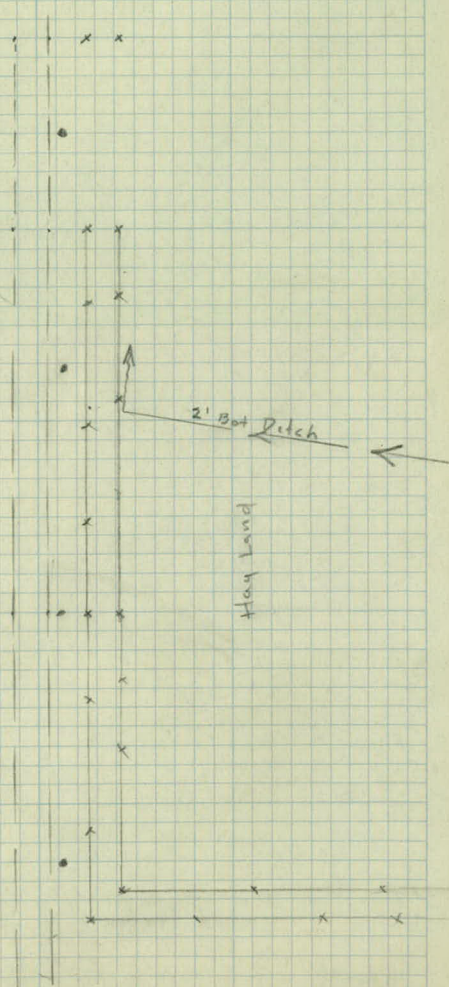
307

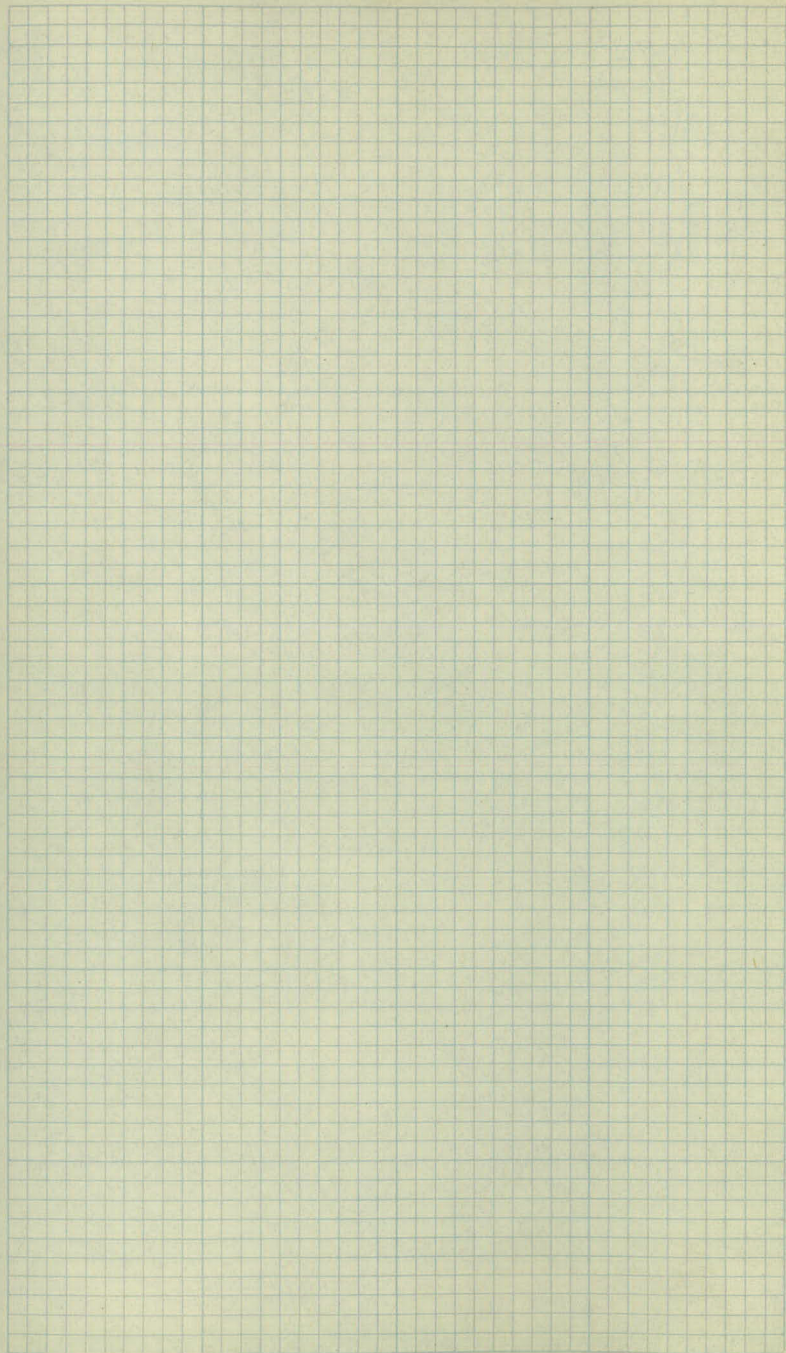
$$\begin{array}{r} +69 TP \\ 11 \\ \hline +54 FC \\ 42 \\ \hline \end{array}$$

$$\begin{array}{r} +40 FC \\ 27 \\ \hline \end{array}$$

306

Hay Land





1
Preliminary X-sections
Co. Rd. St. (No. Co. line)

Sta.	+ K -	Elev.
B.M.	5.78	918.71
		912.93
0+00	Intersection Co. Rd. J. & S.T.H. #12	912.9.
+50		
0+10	Edge of pavement.	913.0.
0+19		912.9.
0+25		913.1.
0+33		913.1.
0+42		913.1.
0+49		913.1.
B.M.	6.25	919.18.
		912.93.
1+00		913.8.
+50		14.2.
2+00		14.1.
+50		13.7.
3+00		12.9.

LZRV9/22/36
Clear

5.8
100

Top. Broomed.
5.8

5.8
100

5.7
100

5.7

5.7
100

5.8
100

5.5
40

5.8
55

5.8
55

5.6
100

7.3
100

6.7
38

5.4
26

5.6

6.3
33

6.8
44

7.0
100

7.3
100

6.7
38

5.4
26

5.6

6.3
33

6.8
44

7.0
100

6.0
100

6.0
52

6.1
21

5.2
17

5.5

5.7
24

4.6
100

3.7
100

3.7
89

3.4
22

5.2
18

5.6

4.9
21

3.2
27

4.3
13

4.2
100

4.3
100

4.3
50

4.2
22

5.0
15

5.4

5.2
6

4.5
17

3.8
21

4.3
50

4.2
100

4.8
100

4.7
50

4.2
22

4.9
17

5.0

4.9
6

4.3
18

3.2
23

4.4
50

4.0
100

5.0
100

5.0
50

3.7
21

4.5
12

5.1

5.0
14

4.0
19

2.6
23

3.7
32

3.9
50

3.0
100

5.4
100

5.1
56

4.8
21

4.7
15

5.3
6

5.5

5.4
5

4.7
20

3.7
24

4.7
35

4.7
100

6.0
100

5.9
44

5.0
23

5.7
17

6.2
7

6.3

6.0
9

6.5
24

7.6
41

8.0
50

7.8
100

Sta. + ∇ - Elev.

919.18.

3+50

912.3.

4+00

12.0

T.P. 285

915.43.

6.60

912.58.

+50

911.8.

5+00

11.4.

+50

11.2.

6

10.8.

+50

10.4.

7

10.5.

+50

10.5.

8

10.5.

+50

10.7.

9

11.1.

B.M.

2.74 912.69.

4Eet.3

$\frac{6.6}{100}$	$\frac{6.6}{50}$	$\frac{5.8}{21}$	$\frac{6.2}{18}$	$\frac{6.6}{7}$	6.9	$\frac{6.4}{12}$	$\frac{7.5}{18}$	$\frac{8.7}{42}$	$\frac{9.0}{50}$	$\frac{9.0}{50}$
-------------------	------------------	------------------	------------------	-----------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{7.5}{100}$	$\frac{7.5}{50}$	$\frac{6.4}{24}$	$\frac{6.8}{18}$	7.2	$\frac{6.8}{5}$	$\frac{4.7}{19}$	$\frac{6.4}{24}$	$\frac{7.2}{50}$	$\frac{7.2}{100}$
-------------------	------------------	------------------	------------------	-----	-----------------	------------------	------------------	------------------	-------------------

$\frac{4.5}{100}$	$\frac{4.5}{50}$	$\frac{3.4}{26}$	$\frac{3.3}{10}$	3.6	$\frac{3.2}{19}$	$\frac{2.6}{22}$	$\frac{3.2}{40}$	$\frac{3.2}{50}$	$\frac{3.2}{100}$
-------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	-------------------

$\frac{5.0}{100}$	$\frac{5.0}{50}$	$\frac{4.2}{23}$	$\frac{3.6}{16}$	$\frac{3.8}{9}$	4.0	$\frac{3.5}{5}$	$\frac{3.8}{16}$	$\frac{3.4}{23}$	$\frac{3.8}{35}$	$\frac{3.6}{50}$	$\frac{3.6}{100}$
-------------------	------------------	------------------	------------------	-----------------	-----	-----------------	------------------	------------------	------------------	------------------	-------------------

$\frac{5.9}{100}$	$\frac{6.4}{50}$	$\frac{6.2}{41}$	$\frac{6.0}{21}$	$\frac{4.4}{17}$	$\frac{4.1}{8}$	4.2	$\frac{3.5}{10}$	$\frac{4.4}{18}$	$\frac{4.6}{50}$	$\frac{4.1}{100}$
-------------------	------------------	------------------	------------------	------------------	-----------------	-----	------------------	------------------	------------------	-------------------

$\frac{6.9}{100}$	$\frac{7.4}{50}$	$\frac{7.4}{40}$	$\frac{6.9}{23}$	$\frac{5.2}{14}$	$\frac{4.2}{10}$	$\frac{4.6}{7}$	4.6	$\frac{4.3}{9}$	$\frac{5.1}{19}$	$\frac{5.2}{50}$	$\frac{5.3}{100}$
-------------------	------------------	------------------	------------------	------------------	------------------	-----------------	-----	-----------------	------------------	------------------	-------------------

$\frac{6.9}{100}$	$\frac{7.4}{50}$	$\frac{7.0}{35}$	$\frac{6.2}{22}$	$\frac{5.0}{15}$	$\frac{4.8}{10}$	$\frac{5.1}{8}$	5.0	$\frac{5.0}{2}$	$\frac{4.7}{5}$	$\frac{4.6}{13}$	$\frac{5.4}{20}$	$\frac{5.7}{50}$	$\frac{5.7}{100}$
-------------------	------------------	------------------	------------------	------------------	------------------	-----------------	-----	-----------------	-----------------	------------------	------------------	------------------	-------------------

$\frac{6.9}{100}$	$\frac{6.9}{50}$	$\frac{6.7}{24}$	$\frac{6.3}{22}$	$\frac{6.0}{16}$	$\frac{5.0}{11}$	4.9	$\frac{5.0}{12}$	$\frac{6.0}{17}$	$\frac{6.2}{22}$	$\frac{5.8}{30}$	$\frac{5.8}{50}$	$\frac{6.0}{100}$
-------------------	------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------	-------------------

$\frac{5.6}{100}$	$\frac{5.6}{50}$	$\frac{5.2}{23}$	$\frac{5.7}{18}$	$\frac{5.0}{11}$	4.9	$\frac{5.0}{13}$	$\frac{6.0}{16}$	$\frac{7.0}{25}$	$\frac{5.6}{30}$	$\frac{5.4}{50}$	$\frac{6.0}{100}$
-------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------	-------------------

$\frac{5.2}{100}$	$\frac{5.2}{50}$	$\frac{4.8}{23}$	$\frac{5.3}{18}$	$\frac{4.9}{12}$	4.9	$\frac{4.8}{13}$	$\frac{5.9}{17}$	$\frac{6.4}{20}$	$\frac{6.3}{23}$	$\frac{5.2}{27}$	$\frac{5.6}{50}$	$\frac{6.0}{100}$
-------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------	------------------	-------------------

$\frac{5.8}{100}$	$\frac{5.0}{50}$	$\frac{5.1}{19}$	$\frac{4.6}{11}$	4.7	$\frac{5.0}{15}$	$\frac{5.7}{19}$	$\frac{5.7}{23}$	$\frac{5.0}{27}$	$\frac{5.3}{50}$	$\frac{5.3}{100}$
-------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------	-------------------

$\frac{4.9}{100}$	$\frac{4.9}{50}$	$\frac{4.7}{24}$	$\frac{5.2}{20}$	$\frac{4.4}{15}$	$\frac{4.2}{11}$	4.3	$\frac{4.6}{16}$	$\frac{5.0}{18}$	$\frac{5.0}{22}$	$\frac{3.9}{25}$	$\frac{4.5}{50}$	$\frac{4.5}{100}$
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40 Rt Sta 9x10 12" Oak

5 1/2 + π - Elev.

915.43.

9+50

911.2.

10+00

11.3.

+50

11.6.

T.P

4.60

915.83.

4.20

911.23.

11

911.2.

+50

11.6.

12

11.7.

+50

11.7.

13

11.6.

+50

11.4.

14

11.0.

+50

10.8.

15

10.5.

LT

E

RT

$$\frac{4.5}{100} \frac{4.5}{50} \frac{4.2}{23} \frac{4.7}{18} \frac{4.3}{12} 4.2 \frac{4.3}{14} \frac{4.4}{21} \frac{4.0}{25} \frac{4.0}{3.0} \frac{4.2}{50} \frac{4.2}{100}$$

$$\frac{4.1}{100} \frac{4.1}{50} \frac{4.1}{26} \frac{4.6}{20} \frac{4.1}{13} 4.1 \frac{4.0}{13} \frac{4.7}{18} \frac{4.8}{22} \frac{4.3}{28} \frac{4.8}{50} \frac{5.0}{100}$$

$$\frac{4.2}{100} \frac{4.2}{50} \frac{4.0}{28} \frac{4.6}{21} \frac{4.5}{15} \frac{4.0}{12} 3.8 \frac{4.4}{12} \frac{5.1}{16} \frac{5.2}{22} \frac{4.9}{26} \frac{5.5}{31} \frac{5.5}{50} \frac{5.0}{100}$$

$$\frac{4.4}{100} \frac{4.3}{50} \frac{4.1}{29} \frac{4.9}{19} 4.6 \frac{4.2}{4} \frac{4.8}{13} \frac{5.1}{17} \frac{5.7}{23} \frac{5.3}{26} \frac{6.1}{31} \frac{5.8}{50} \frac{6.5}{100}$$

$$\frac{3.9}{100} \frac{3.8}{50} \frac{3.8}{30} \frac{4.2}{24} \frac{4.7}{18} \frac{4.2}{10} 4.2 \frac{4.5}{15} \frac{5.8}{22} \frac{4.7}{26} \frac{5.4}{32} \frac{5.1}{50} \frac{4.9}{100}$$

$$\frac{4.4}{100} \frac{4.4}{50} \frac{3.9}{29} \frac{3.8}{24} \frac{4.3}{17} \frac{3.9}{9} 4.1 \frac{4.3}{15} \frac{4.7}{21} \frac{4.0}{24} \frac{4.4}{31} \frac{4.4}{50} \frac{4.3}{100}$$

$$\frac{4.2}{100} \frac{4.1}{50} \frac{4.1}{24} \frac{4.4}{18} \frac{4.0}{9} 4.1 \frac{4.0}{13} \frac{4.3}{19} \frac{4.0}{29} \frac{4.2}{33} \frac{4.2}{50} \frac{3.9}{100}$$

$$\frac{4.8}{100} \frac{4.5}{50} \frac{4.0}{24} \frac{4.5}{17} \frac{4.1}{13} 4.2 \frac{4.1}{12} \frac{3.9}{14} \frac{3.9}{29} \frac{3.9}{50} \frac{3.4}{100}$$

$$\frac{5.3}{100} \frac{4.9}{50} \frac{4.9}{32} \frac{4.7}{19} 4.4 \frac{4.5}{20} \frac{3.9}{26} \frac{4.2}{33} \frac{4.2}{50} \frac{3.9}{100}$$

$$\frac{4.8}{100} \frac{4.4}{50} \frac{4.1}{25} \frac{4.9}{17} 4.8 \frac{4.6}{15} \frac{5.1}{20} \frac{4.6}{26} \frac{5.5}{33} \frac{5.5}{50} \frac{4.7}{100}$$

$$\frac{5.0}{100} \frac{4.7}{50} \frac{4.5}{25} \frac{4.9}{16} 5.0 \frac{4.5}{13} \frac{5.1}{16} \frac{5.0}{22} \frac{4.5}{26} \frac{5.3}{33} \frac{5.6}{50} \frac{5.3}{100}$$

$$\frac{4.9}{100} \frac{4.8}{50} \frac{4.8}{27} 5.3 \frac{5.1}{12} \frac{5.3}{22} \frac{4.9}{27} \frac{5.7}{33} \frac{6.0}{50} \frac{5.2}{100}$$

5/2. + π - Elev.
 915.83. 910.8.

15+50

16 10.9.

+50 10.7.

3.2
 100

17 10.7.

+35 11.0.
 Φ Farm Ent

+60 11.1.

18 10.6.

+50 10.0.

19 9.7.

+50 10.0.

20 10.4.

B.M. 7.72 918.34 5.20 910.62 910.63.

+50 11.4

Lt.

Z

Rt.

$\frac{4.6}{100}$ $\frac{5.6}{60}$ $\frac{5.8}{21}$ $\frac{5.0}{5}$ 5.0 $\frac{5.0}{7}$ $\frac{5.1}{14}$ $\frac{6.1}{19}$ $\frac{6.1}{24}$ $\frac{5.6}{27}$ $\frac{6.7}{34}$ $\frac{6.1}{50}$
 $\frac{5.7}{100}$

$\frac{4.1}{100}$ $\frac{5.1}{50}$ $\frac{6.1}{19}$ $\frac{5.6}{13}$ $\frac{5.1}{6}$ 4.9 $\frac{5.5}{13}$ $\frac{6.7}{19}$ $\frac{6.9}{24}$ $\frac{6.5}{26}$ $\frac{6.7}{33}$ $\frac{6.7}{50}$ $\frac{6.0}{100}$

$\frac{4.2}{50}$ $\frac{4.5}{39}$ $\frac{5.1}{27}$ $\frac{6.0}{20}$ $\frac{6.7}{19}$ $\frac{6.7}{16}$ $\frac{5.4}{13}$ $\frac{5.0}{5}$ 5.1 $\frac{5.3}{9}$ $\frac{5.9}{14}$ $\frac{7.1}{19}$ $\frac{7.3}{24}$ $\frac{6.7}{27}$ $\frac{6.9}{34}$ $\frac{6.9}{50}$ $\frac{6.4}{100}$

$\frac{3.3}{100}$ $\frac{3.8}{50}$ $\frac{4.1}{35}$ $\frac{5.3}{32}$ $\frac{6.4}{26}$ $\frac{6.1}{17}$ $\frac{5.1}{13}$ 5.1 $\frac{5.0}{9}$ $\frac{5.5}{14}$ $\frac{6.9}{19}$ $\frac{6.9}{24}$ $\frac{6.3}{26}$ $\frac{6.3}{50}$ $\frac{5.8}{100}$

$\frac{3.4}{100}$ $\frac{4.0}{50}$ $\frac{4.6}{30}$ 4.8 $\frac{5.1}{15}$ $\frac{6.3}{18}$ $\frac{6.4}{25}$ $\frac{5.4}{27}$ $\frac{5.6}{35}$ $\frac{5.5}{50}$ $\frac{5.3}{100}$

$\frac{4.0}{100}$ $\frac{4.2}{30}$ $\frac{4.2}{35}$ $\frac{5.7}{30}$ $\frac{6.0}{22}$ $\frac{4.4}{11}$ 4.7 $\frac{4.8}{14}$ $\frac{6.0}{18}$ $\frac{6.2}{23}$ $\frac{4.5}{26}$ $\frac{4.5}{50}$ $\frac{4.5}{100}$

$\frac{5.3}{100}$ $\frac{5.6}{50}$ $\frac{5.7}{35}$ $\frac{5.5}{24}$ $\frac{6.2}{23}$ $\frac{6.4}{18}$ $\frac{5.2}{13}$ 5.2 $\frac{5.1}{15}$ $\frac{6.2}{18}$ $\frac{6.4}{23}$ $\frac{4.1}{28}$ $\frac{4.2}{35}$ $\frac{4.2}{50}$ $\frac{4.1}{100}$

$\frac{8.3}{100}$ $\frac{8.2}{50}$ $\frac{7.9}{35}$ $\frac{7.3}{17}$ $\frac{5.7}{11}$ 5.8 $\frac{5.4}{14}$ $\frac{6.8}{20}$ $\frac{6.7}{25}$ $\frac{5.1}{28}$ $\frac{4.7}{35}$ $\frac{4.2}{50}$ $\frac{4.2}{100}$

$\frac{8.5}{100}$ $\frac{8.6}{50}$ $\frac{8.6}{36}$ $\frac{8.5}{23}$ $\frac{8.2}{17}$ $\frac{5.4}{11}$ 6.1 $\frac{5.8}{9}$ $\frac{7.0}{16}$ $\frac{7.5}{22}$ $\frac{7.1}{33}$ $\frac{5.9}{50}$ $\frac{4.9}{100}$

$\frac{7.1}{100}$ $\frac{7.5}{60}$ $\frac{8.0}{35}$ $\frac{7.9}{17}$ $\frac{5.8}{10}$ 5.8 $\frac{5.6}{13}$ $\frac{7.6}{16}$ $\frac{7.3}{36}$ $\frac{7.0}{50}$ $\frac{6.5}{100}$

$\frac{4.6}{100}$ $\frac{5.5}{50}$ $\frac{6.0}{36}$ $\frac{6.2}{27}$ $\frac{4.4}{24}$ $\frac{7.2}{16}$ $\frac{5.6}{11}$ 5.4 $\frac{5.3}{14}$ $\frac{7.0}{20}$ $\frac{6.7}{26}$ $\frac{5.8}{28}$ $\frac{5.6}{35}$ $\frac{5.1}{100}$

Top of Mount 579 20+1743

$\frac{5.3}{100}$ $\frac{5.8}{50}$ $\frac{6.1}{33}$ $\frac{8.3}{27}$ $\frac{8.6}{23}$ $\frac{7.7}{18}$ $\frac{6.7}{10}$ 7.0 $\frac{6.7}{11}$ $\frac{7.6}{19}$ $\frac{7.3}{28}$ $\frac{5.9}{30}$ $\frac{5.8}{50}$ $\frac{5.7}{50}$

Sta + H.I. - Elev

918.84³⁵

21 + 00

912.3.

+ 50

12.5.

22

12.8.

+ 50

13.1.

23

13.2.

+ 50

13.7.

24

13.4.

+ 50

13.2.

B.M

5.43 912.91⁹² 912.92.

25

913.1.

+ 50

13.3.

26

13.2.

+ 50

13.3.

4+

2

10+

4.7 5.2 5.5 8.3 8.4 7.0 5.8 6.1 5.1 6.2 6.8 4.8 5.1 5.1
100 50 34 29 22 19 11 15 21 21 21 31 34 50
5.0
100

6.1 6.1 9.1 8.9 7.0 6.8 5.7 5.9 6.1 6.8 4.7 4.9 4.5
50 35 28 23 19 16 12 12 21 25 30 34 100
5.6
100

5.6 8.6 9.0 8.5 7.8 6.8 5.5 5.7 7.2 7.3 5.8 5.7 5.8
100 50 35 22 18 11 8 16 21 22 29 50 100

4.9 6.2 7.4 6.8 5.1 5.1 6.4 7.3 5.8 5.6 5.4
100 50 34 18 9 11 18 26 30 50 100

5.0 5.8 5.2 7.3 7.3 5.8 5.1 5.2 7.2 7.1 4.8 5.0 5.0
100 50 33 27 22 16 10 17 22 26 29 60 100

5.2 5.2 5.3 7.4 6.8 5.6 4.9 4.9 5.8 6.6 6.6 5.1 5.0 5.0
100 50 35 30 21 16 10 12 18 21 26 30 50 100

5.7 5.7 5.7 7.3 7.3 6.7 5.3 5.1 6.9 7.2 6.8 5.8 5.8 4.8
100 50 33 29 24 21 10 13 20 24 28 30 50 100

6.5 6.5 7.5 7.2 6.0 5.2 5.4 7.4 7.4 6.2 6.1 5.3 4.3
100 31 27 18 12 3 11 18 27 30 35 50 100

Spike 12" Oak 50" x 1" 5" x 24" x 83"

6.7 6.5 6.5 7.4 7.1 5.7 5.1 5.8 7.0 7.4 7.2 5.3 4.5 4.5
100 50 32 29 20 12 10 16 19 23 26 31 50 100

6.2 6.3 6.3 7.3 7.1 5.6 5.3 7.7 8.3 4.5 4.4 3.4
100 50 31 29 21 12 13 21 25 30 50 100

5.8 5.8 7.0 6.9 5.6 5.0 5.3 6.8 6.6 4.1 3.4
100 29 29 20 14 5 12 23 28 31 100

5.2 5.2 5.0 4.7 5.3 7.4 7.4 4.5 4.0
100 39 6 6 14 20 28 32 100

Sta + HI - Elev

2 918 ³⁴ 35 913.3

26 + 70 2 Town Rd North

27 69 912.8

T.P 1.90 914 ⁶⁸ 5.56 912.78 79

+ 50 12.1

28 11.7

+ 50 10.8

29 10.5

+ 50 10.1

30 10.0

+ 50 10.0

31 10.2

+ 50 9.9

32 10.3

Lt

K

Rt

$$\frac{5.0}{100} \frac{5.4}{50} 5.1 \frac{5.0}{8} \frac{5.8}{16} \frac{8.3}{23} \frac{8.3}{28} \frac{4.8}{33} \frac{4.1}{100}$$

$$\frac{6.8}{100} \frac{6.8}{50} \frac{6.6}{21} \frac{6.0}{12} 5.6 \frac{6.1}{18} \frac{8.3}{22} \frac{8.3}{28} \frac{4.8}{31} \frac{5.0}{100}$$

$$\frac{3.9}{100} \frac{3.9}{50} \frac{3.5}{13} \frac{2.6}{8} 2.6 \frac{2.5}{10} \frac{3.1}{18} \frac{5.4}{22} \frac{5.4}{27} \frac{2.0}{31} \frac{2.0}{32} \frac{1.9}{100}$$

$$\frac{4.0}{100} \frac{3.9}{50} \frac{3.9}{14} \frac{3.0}{8} 3.0 \frac{3.5}{17} \frac{6.6}{23} \frac{6.6}{29} \frac{2.1}{33} \frac{2.1}{100}$$

$$\frac{4.1}{100} \frac{4.1}{50} \frac{4.4}{14} \frac{3.5}{8} 3.9 \frac{4.2}{12} \frac{5.2}{17} \frac{6.5}{19} \frac{6.5}{25} \frac{3.9}{29} \frac{2.9}{100}$$

$$\frac{4.8}{100} \frac{4.8}{50} \frac{5.0}{15} \frac{4.1}{7} 4.2 \frac{4.5}{11} \frac{6.9}{19} \frac{8.0}{24} \frac{8.0}{27} \frac{5.3}{31} \frac{5.1}{50} \frac{3.9}{100}$$

$$\frac{5.1}{100} \frac{5.6}{50} \frac{5.1}{16} \frac{4.7}{8} 4.6 \frac{5.0}{10} \frac{6.6}{19} \frac{9.0}{23} \frac{9.0}{26} \frac{6.5}{32} \frac{5.5}{100}$$

$$\frac{5.0}{100} \frac{5.5}{50} \frac{5.8}{18} \frac{4.8}{9} 4.7 \frac{4.8}{7} \frac{6.5}{18} \frac{9.0}{23} \frac{9.0}{28} \frac{6.6}{33} \frac{6.6}{100}$$

$$\frac{4.6}{100} \frac{5.2}{50} \frac{6.2}{17} \frac{5.0}{12} \frac{4.7}{9} 4.7 \frac{5.0}{9} \frac{6.3}{17} \frac{8.4}{23} \frac{8.8}{28} \frac{6.7}{33} \frac{6.7}{100}$$

$$\frac{4.6}{100} \frac{5.8}{50} \frac{5.7}{26} \frac{6.3}{20} \frac{5.9}{16} \frac{4.9}{12} 4.5 \frac{4.6}{8} \frac{7.0}{20} \frac{8.9}{23} \frac{9.0}{28} \frac{6.9}{32} \frac{6.4}{100}$$

$$\frac{4.3}{100} \frac{5.8}{50} \frac{6.6}{21} \frac{6.3}{15} \frac{5.3}{13} \frac{4.7}{9} 4.8 \frac{4.7}{8} \frac{6.5}{19} \frac{8.7}{23} \frac{8.9}{28} \frac{6.6}{32} \frac{6.4}{100}$$

$$\frac{4.2}{100} \frac{5.7}{50} \frac{6.2}{24} \frac{6.1}{16} \frac{4.8}{9} 4.4 \frac{4.5}{9} \frac{6.0}{19} \frac{8.0}{23} \frac{8.2}{28} \frac{7.1}{31} \frac{5.7}{32} \frac{5.7}{50} \frac{5.7}{100}$$

Sta	+	H.I	-	Elev
		914.68	69	

32 + 50				910.0
---------	--	--	--	-------

33				10.0
----	--	--	--	------

+ 50				10.1
------	--	--	--	------

34			66	9.9
----	--	--	----	-----

T.P	686	916.65	489	909.79	80
-----	-----	--------	-----	--------	----

+ 50				911.2
------	--	--	--	-------

35				11.2
----	--	--	--	------

+ 50				11.2
------	--	--	--	------

36				11.2
----	--	--	--	------

+ 50				11.4
------	--	--	--	------

37				11.5
----	--	--	--	------

+ 50				12.0
------	--	--	--	------

38				12.7
----	--	--	--	------

LT

♀

RH

 $\frac{4.7}{100} \frac{5.7}{50} \frac{6.3}{16} \frac{4.8}{9} 4.7 \frac{4.5}{8} \frac{6.1}{17} \frac{8.2}{24} \frac{8.6}{28} \frac{7.5}{32} \frac{5.7}{33} \frac{5.7}{100}$
 $\frac{4.9}{100} \frac{5.4}{50} \frac{6.0}{31} \frac{6.7}{23} \frac{6.6}{19} \frac{4.7}{12} 4.7 \frac{5.1}{11} \frac{7.0}{19} \frac{8.6}{24} \frac{9.2}{28} \frac{6.5}{33} \frac{6.6}{38} \frac{6.4}{100}$
 $\frac{5.4}{100} \frac{5.4}{50} \frac{5.1}{29} \frac{6.1}{20} \frac{4.8}{13} 4.6 \frac{4.7}{11} \frac{6.3}{19} \frac{7.7}{24} \frac{8.1}{29} \frac{6.2}{32} \frac{6.2}{100}$
 $\frac{5.7}{100} \frac{5.8}{50} \frac{6.2}{21} \frac{4.8}{14} 4.8 \frac{5.0}{11} \frac{6.4}{18} \frac{7.9}{23} \frac{8.2}{28} \frac{6.0}{32} \frac{6.1}{100}$
 $\frac{6.2}{100} \frac{6.2}{50} \frac{6.7}{21} \frac{5.4}{13} 5.5 \frac{5.5}{8} \frac{6.9}{18} \frac{8.7}{23} \frac{8.9}{28} \frac{8.1}{31} \frac{6.9}{32} \frac{7.0}{70}$
 $\frac{5.5}{100} \frac{5.5}{50} \frac{5.5}{39} \frac{6.1}{21} \frac{5.2}{16} 5.5 \frac{5.4}{9} \frac{7.1}{17} \frac{8.4}{21} \frac{9.9}{28} \frac{5.8}{32} \frac{5.7}{100}$
 $\frac{5.8}{100} \frac{5.8}{44} \frac{6.5}{22} \frac{5.5}{17} 5.5 \frac{5.5}{10} \frac{7.0}{19} \frac{7.7}{20} \frac{8.1}{25} \frac{7.4}{30} \frac{6.1}{31} \frac{6.6}{100}$
 $\frac{5.3}{100} \frac{5.8}{50} \frac{6.2}{19} \frac{5.3}{13} 5.5 \frac{5.9}{16} \frac{7.8}{22} \frac{8.4}{26} \frac{7.4}{30} \frac{6.2}{31} \frac{6.7}{100}$
 $\frac{5.3}{100} \frac{6.3}{50} \frac{6.3}{16} \frac{5.1}{12} 5.3 \frac{5.3}{13} \frac{6.2}{17} \frac{7.9}{20} \frac{8.6}{26} \frac{7.5}{29} \frac{5.9}{31} \frac{6.4}{100}$
 $\frac{4.5}{100} \frac{6.1}{50} \frac{6.4}{17} \frac{5.2}{9} 5.2 \frac{5.3}{12} \frac{6.5}{19} \frac{7.7}{21} \frac{8.0}{28} \frac{5.7}{32} \frac{6.0}{100}$
 $\frac{4.2}{100} \frac{4.7}{50} \frac{5.0}{19} \frac{4.6}{12} 4.7 \frac{5.2}{18} \frac{7.2}{22} \frac{7.4}{27} \frac{5.2}{30} \frac{5.2}{50} \frac{5.8}{100}$
 $\frac{3.8}{100} \frac{3.8}{50} \frac{4.3}{16} \frac{3.9}{12} 4.0 \frac{4.2}{16} \frac{6.0}{20} \frac{6.2}{26} \frac{4.5}{29} \frac{5.0}{50} \frac{5.5}{100}$

Sta	+	H.I	-	Elev
38 + 50		916.65 3.22	66	913.0.
39				13.0.
+ 50				13.0.
40				12.8.
+ 50				12.7.
41				12.7. 35
B.M		4.31	912.34	912.37

Lt

Q

Rt

$$\frac{3.6}{100} \frac{3.6}{50} \frac{4.0}{21} \frac{3.8}{11} 3.7 \frac{3.8}{14} \frac{5.5}{20} \frac{5.9}{27} \frac{4.2}{29} \frac{5.2}{100}$$

$$\frac{3.9}{100} \frac{3.9}{50} \frac{4.5}{17} \frac{3.8}{11} 3.7 \frac{3.7}{13} \frac{5.1}{19} \frac{6.4}{21} \frac{6.5}{24} \frac{5.3}{26} \frac{4.3}{29} \frac{5.1}{100}$$

$$\frac{4.1}{100} \frac{4.1}{50} \frac{4.4}{25} \frac{5.0}{18} \frac{4.5}{16} \frac{3.7}{4} 3.7 \frac{4.2}{16} \frac{6.6}{24} \frac{6.5}{27} \frac{4.5}{28} \frac{5.0}{50} \frac{5.5}{100}$$

$$\frac{3.6}{100} \frac{3.8}{50} \frac{4.2}{29} \frac{4.9}{17} \frac{3.8}{9} 3.9 \frac{4.0}{12} \frac{5.0}{16} \frac{7.0}{20} \frac{7.2}{25} \frac{5.3}{27} \frac{5.3}{50} \frac{5.2}{100}$$

$$\frac{3.6}{100} \frac{3.6}{50} \frac{4.2}{29} \frac{4.6}{18} \frac{3.8}{8} 4.0 \frac{4.4}{6} \frac{6.0}{17} \frac{7.8}{21} \frac{8.0}{26} \frac{5.8}{28} \frac{5.8}{100}$$

$$\frac{3.1}{100} \frac{3.6}{50} \frac{4.2}{31} \frac{4.2}{15} \frac{4.0}{7} 4.0 \frac{4.5}{12} \frac{5.5}{18} \frac{7.4}{23} \frac{7.0}{27} \frac{5.6}{28} \frac{4.6}{100}$$

Sta + H.I - Elev

No Co Line Rd

Prelim. Cross Section

Sta 42+00 to 120+77

Sta	+	±	✓	-	Elev
BM	4.38	916.75			912.37
42 + 00					11.9 ✓
43					12.6 ✓
44					12.2 ✓
45					11.8 ✓
T.P	4.95	916.34 ✓	5.3L		911.39 ✓
46					11.3 ✓
47					10.9 ✓
48					11.6 ✓
49					11.7 ✓
50					11.8 ✓
B.M			4.5		915.89 ✓
51					12.3 ✓
52					11.6 ✓
T.P	7.07	918.71 ✓	4.70		911.64 ✓
53					11.7 ✓

(No Co Line)

20 RT 41 + 20

$\frac{5.2}{100}$ $\frac{5.2}{50}$ $\frac{5.6}{20}$ $\frac{5.0}{16}$ 49 $\frac{5.3}{14}$ $\frac{7.0}{19}$ $\frac{7.0}{21}$ $\frac{6.0}{27}$ $\frac{5.5}{30}$ $\frac{5.0}{100}$

$\frac{5.1}{100}$ $\frac{5.2}{50}$ $\frac{5.1}{20}$ $\frac{4.4}{16}$ 42 $\frac{4.2}{15}$ $\frac{5.8}{18}$ $\frac{5.8}{22}$ $\frac{4.4}{25}$ $\frac{4.7}{50}$ $\frac{4.7}{100}$

$\frac{5.0}{100}$ $\frac{5.0}{50}$ $\frac{5.0}{21}$ $\frac{4.5}{14}$ 46 $\frac{4.7}{17}$ $\frac{5.8}{22}$ $\frac{5.8}{24}$ $\frac{4.8}{27}$ $\frac{5.0}{50}$ $\frac{5.0}{100}$

$\frac{6.4}{100}$ $\frac{5.9}{50}$ $\frac{5.5}{21}$ $\frac{4.8}{16}$ 50 $\frac{5.2}{10}$ $\frac{6.2}{17}$ $\frac{7.4}{24}$ $\frac{6.7}{28}$ $\frac{7.2}{50}$ $\frac{7.7}{100}$

$\frac{6.1}{100}$ $\frac{6.1}{50}$ $\frac{5.9}{19}$ $\frac{4.9}{11}$ 50 $\frac{5.0}{5}$ $\frac{5.6}{19}$ $\frac{6.2}{22}$ $\frac{6.2}{26}$ $\frac{6.1}{30}$ $\frac{7.2}{50}$ $\frac{8.2}{100}$

$\frac{6.6}{100}$ $\frac{6.6}{50}$ $\frac{6.6}{19}$ $\frac{5.1}{7}$ 54 $\frac{5.2}{9}$ $\frac{6.9}{21}$ $\frac{6.9}{25}$ $\frac{6.5}{30}$ $\frac{6.9}{50}$ $\frac{7.4}{100}$

$\frac{5.4}{100}$ $\frac{5.9}{50}$ $\frac{5.5}{19}$ $\frac{5.0}{10}$ 47 $\frac{4.5}{9}$ $\frac{5.3}{17}$ $\frac{7.1}{22}$ $\frac{7.6}{25}$ $\frac{5.0}{29}$ $\frac{5.1}{50}$ $\frac{6.0}{100}$

$\frac{3.4}{100}$ $\frac{4.4}{50}$ $\frac{4.8}{28}$ $\frac{5.4}{18}$ 46 $\frac{5.6}{19}$ $\frac{7.2}{21}$ $\frac{7.2}{23}$ $\frac{5.4}{27}$ $\frac{5.2}{50}$ $\frac{5.0}{100}$

$\frac{3.5}{100}$ $\frac{3.5}{50}$ $\frac{3.7}{17}$ $\frac{4.5}{13}$ 45 $\frac{4.4}{9}$ $\frac{5.5}{19}$ $\frac{6.2}{25}$ $\frac{5.3}{28}$ $\frac{6.1}{50}$ $\frac{7.1}{100}$

915.86 65' Lt of Sta 50 + 07

$\frac{3.7}{100}$ $\frac{3.7}{50}$ $\frac{3.7}{20}$ $\frac{4.8}{15}$ $\frac{3.9}{10}$ 4.0 $\frac{4.3}{14}$ $\frac{5.6}{21}$ $\frac{5.6}{24}$ $\frac{4.7}{28}$ $\frac{5.4}{50}$ $\frac{6.3}{100}$

$\frac{7.4}{100}$ $\frac{6.4}{50}$ $\frac{5.6}{34}$ $\frac{6.5}{27}$ $\frac{6.4}{17}$ $\frac{5.7}{15}$ $\frac{5.0}{12}$ 4.7 $\frac{4.7}{17}$ $\frac{5.7}{22}$ $\frac{5.2}{25}$ $\frac{4.4}{27}$ $\frac{4.6}{50}$ $\frac{5.6}{100}$

$\frac{9.0}{100}$ $\frac{9.4}{50}$ $\frac{8.6}{26}$ $\frac{9.5}{23}$ $\frac{9.5}{19}$ $\frac{8.3}{15}$ $\frac{7.3}{11}$ 7.0 $\frac{7.3}{16}$ $\frac{8.6}{18}$ $\frac{8.6}{25}$ $\frac{6.8}{26}$ $\frac{6.5}{40}$ $\frac{7.0}{50}$ $\frac{7.0}{100}$

2

Sta	+	π ✓	-	Elev	
		918.71			
54				11.7 ✓	
55				13.6 ✓	
56				13.5 ✓	9.5 100
57				12.7 ✓	
58				12.6 ✓	
TP	1.74	✓ 913.49	6.96		✓ 911.75
59				11.8 ✓	
60				09.7 ✓	
61				08.7 ✓	
BM	1.87	✓ 910.36	5.00		✓ 908.49
62				07.3 ✓	
63				06.0 ✓	
64				05.4 ✓	
65				05.8 ✓	

LT * PT

$\frac{9.0}{100} \frac{9.5}{50} \frac{8.5}{26} \frac{9.0}{24} \frac{9.0}{19} \frac{7.2}{12} \frac{7.0}{7.0} \frac{6.9}{12} \frac{7.9}{19} \frac{8.0}{22} \frac{6.7}{28} \frac{7.0}{50} \frac{6.5}{100}$

$\frac{7.5}{100} \frac{7.0}{50} \frac{6.2}{40} \frac{6.1}{27} \frac{7.1}{24} \frac{7.1}{20} \frac{5.5}{12} \frac{5.0}{7} 5.1 \frac{5.1}{12} \frac{6.1}{19} \frac{6.1}{22} \frac{5.1}{25} \frac{5.5}{50} \frac{6.1}{100}$

$\frac{7.3}{58} \frac{7.0}{43} \frac{6.2}{38} \frac{6.0}{28} \frac{7.2}{24} \frac{7.2}{20} \frac{5.5}{24} \frac{5.1}{8} 5.2 \frac{5.1}{7} \frac{5.7}{16} \frac{5.0}{22} \frac{5.1}{50} \frac{5.5}{100}$

$\frac{9.0}{100} \frac{8.0}{50} \frac{8.5}{48} \frac{7.0}{38} \frac{7.0}{28} \frac{7.5}{25} \frac{7.5}{21} \frac{6.7}{17} \frac{6.1}{10} 6.0 \frac{5.7}{10} \frac{6.5}{17} \frac{6.9}{18} \frac{6.7}{24} \frac{5.4}{26} \frac{5.7}{50} \frac{6.3}{100}$

$\frac{7.3}{100} \frac{6.7}{50} \frac{6.2}{15} 6.1 \frac{6.0}{26} \frac{6.1}{50} \frac{6.7}{100}$

$\frac{0.8}{100} \frac{0.8}{50} \frac{1.1}{25} \frac{1.2}{16} \frac{1.7}{15} 1.7 \frac{2.0}{24} \frac{2.6}{50} \frac{2.9}{100}$

$\frac{2.5}{100} \frac{3.0}{50} \frac{2.9}{32} \frac{3.9}{27} \frac{3.4}{15} \frac{3.8}{14} 3.8 \frac{3.4}{1} \frac{4.2}{14} \frac{4.8}{24} \frac{4.2}{32} \frac{3.7}{38} \frac{3.5}{50} \frac{3.5}{100}$

$\frac{4.3}{100} \frac{4.3}{50} \frac{3.5}{30} \frac{5.0}{24} \frac{4.4}{50} \frac{4.9}{13} 4.8 \frac{4.5}{1} \frac{4.4}{14} \frac{5.8}{20} \frac{5.4}{31} \frac{3.7}{35} \frac{3.2}{50} \frac{3.7}{100}$

908.44 33'44 54g 61+63

$\frac{3.0}{100} \frac{4.0}{50} \frac{4.0}{31} \frac{4.4}{25} \frac{2.9}{19} 3.1 \frac{3.2}{5} \frac{4.0}{10} \frac{2.8}{50} \frac{4.3}{100}$

$\frac{5.6}{100} \frac{5.6}{50} \frac{6.0}{24} \frac{4.3}{19} 4.4 \frac{4.1}{6} \frac{6.6}{13} \frac{6.6}{16} \frac{5.4}{19} \frac{5.0}{50} \frac{4.5}{100}$

$\frac{5.5}{100} \frac{6.5}{50} \frac{6.9}{24} \frac{6.5}{22} \frac{5.0}{10} 5.0 \frac{5.2}{6} \frac{6.9}{16} \frac{6.1}{50} \frac{6.1}{100}$

$\frac{5.9}{100} \frac{6.0}{50} \frac{6.0}{29} \frac{6.7}{27} \frac{6.7}{24} \frac{4.4}{17} \frac{4.7}{12} 4.6 \frac{4.7}{3} \frac{4.3}{6} \frac{4.3}{10} \frac{5.8}{11} \frac{6.6}{22} \frac{6.3}{50} \frac{6.3}{100}$

3

Sta	+	π ✓	-	Elev
		910.36 ✓		
66				06.0 ✓
+10				06.0 ✓
+25				06.0 ✓
+34				06.1 ✓
T.P	5.20	910.83 ✓	4.73	905.63 ✓
67				05.6 ✓
68				05.6 ✓
X				
+50				05.7 ✓
+76				05.5 ✓
69				05.6 ✓
+50				05.6 ✓
70				05.7 ✓
71				05.5 ✓

3.1
100

LT ♀ RT

$\frac{5.1}{100} \frac{5.1}{50} \frac{6.2}{31} \frac{7.2}{27} \frac{7.2}{23} \frac{4.5}{15} \frac{4.0}{11} 44 \frac{4.5}{13} \frac{6.0}{18} \frac{6.7}{24} \frac{6.4}{50} \frac{6.4}{100}$

Reg. New Grade 1933 Contract

$\frac{9.4}{100} \frac{9.7}{50} \frac{9.7}{35} \frac{8.9}{27} \frac{4.3}{14} 44 \frac{4.5}{13} \frac{6.0}{18} \frac{6.7}{24} \frac{6.4}{50} \frac{6.4}{100}$

Ditch
LT

$\frac{9.4}{100} \frac{9.7}{50} \frac{9.7}{35} \frac{8.9}{27} \frac{4.3}{14} 44 \frac{4.5}{13} \frac{6.0}{18} \frac{6.7}{24} \frac{6.4}{50} \frac{6.4}{100}$

$\frac{3.3}{100} \frac{5.8}{50} \frac{6.7}{40} \frac{9.2}{33} \frac{9.4}{24} \frac{4.6}{15} 43 \frac{4.4}{13} \frac{5.9}{18} \frac{6.7}{32} \frac{6.6}{50} \frac{6.6}{100}$

$\frac{6.5}{100} \frac{6.7}{50} \frac{6.7}{34} \frac{9.8}{30} \frac{9.5}{23} \frac{5.6}{14} 5.2 \frac{5.0}{15} \frac{6.9}{17} \frac{6.9}{20} \frac{5.0}{25} \frac{5.1}{29} \frac{7.3}{37} \frac{7.3}{50} \frac{7.3}{100}$

$\frac{7.6}{100} \frac{7.6}{50} \frac{6.0}{36} \frac{9.7}{30} \frac{9.4}{23} \frac{5.4}{14} 5.2 \frac{5.5}{13} \frac{6.8}{18} \frac{7.0}{32} \frac{7.5}{50} \frac{7.5}{100}$

$\frac{7.3}{100} \frac{7.3}{50} \frac{5.9}{36} \frac{9.7}{29} \frac{9.5}{22} \frac{5.4}{13} 5.1 \frac{5.5}{13} \frac{6.5}{17} \frac{6.5}{22} \frac{5.2}{24} \frac{7.5}{35} \frac{7.0}{50} \frac{6.6}{100}$

$\frac{6.7}{100} \frac{6.7}{54} \frac{5.2}{49} \frac{4.5}{39} \frac{9.5}{30} \frac{9.5}{23} \frac{5.6}{12} 5.3 \frac{5.8}{14} \frac{7.0}{18} \frac{6.5}{21} \frac{2.5}{27} \frac{2.6}{35} \frac{3.4}{38} \frac{3.2}{50} \frac{3.7}{100}$

$\frac{6.3}{100} \frac{6.2}{65} \frac{5.0}{50} \frac{3.8}{39} \frac{9.5}{30} \frac{9.4}{23} \frac{5.6}{13} 5.2 \frac{5.3}{12} \frac{6.7}{18} \frac{6.7}{21} \frac{4.0}{26} \frac{6.2}{34} \frac{6.5}{50} \frac{6.5}{100}$

$\frac{6.6}{100} \frac{6.6}{65} \frac{4.7}{50} \frac{4.7}{40} \frac{9.2}{32} \frac{9.8}{26} \frac{6.7}{16} \frac{5.4}{12} 5.2 \frac{5.2}{13} \frac{6.7}{16} \frac{6.4}{22} \frac{5.8}{24} \frac{6.1}{50} \frac{5.1}{100}$

$\frac{6.5}{100} \frac{6.5}{65} \frac{3.5}{50} \frac{8.5}{40} \frac{10.1}{34} \frac{10.2}{26} \frac{5.3}{13} 5.1 \frac{5.2}{12} \frac{7.1}{19} \frac{6.6}{22} \frac{5.4}{24} \frac{5.2}{33} \frac{5.2}{50} \frac{4.7}{100}$

$\frac{6.1}{74} \frac{9.4}{64} \frac{10.4}{56} \frac{6.2}{45} \frac{4.5}{34} \frac{7.6}{25} \frac{7.4}{19} \frac{5.5}{14} 5.3 \frac{5.4}{12} \frac{6.7}{16} \frac{6.8}{21} \frac{5.7}{25} \frac{5.3}{34} \frac{5.1}{50} \frac{4.0}{100}$

4

Sta	+	π ✓	-	Elev
		910.83		
72		✓		05.4 ✓
T.P	5.07	910.47 ✓	5.43	905.40 ✓
BM		910.41 ✓	2.44	908.03 ✓
73				05.3 ✓
74		✓		05.3 ✓
TP	7.57	912.50 ✓	5.48	904.93 ✓
75				05.1 ✓
76				05.0 ✓
77				04.8 ✓
78				04.4 ✓
79				04.2 ✓
80				03.9 ✓
T.P	4.86	908.74	8.62	903.88
T.P	4.07	910.75	2.06	906.68
T.P,			2.66	908.09

Lx

R

Rt

$\frac{11.4}{85} \frac{4.4}{70} \frac{4.0}{50} \frac{5.7}{43} \frac{6.2}{33} \frac{7.4}{32} \frac{7.5}{16} \frac{5.7}{14} \frac{5.4}{5.4} \frac{5.7}{13} \frac{6.8}{12} \frac{6.6}{22} \frac{5.0}{25} \frac{4.8}{50} \frac{4.9}{100}$
 $\downarrow \frac{4.4}{95}$

907.97 33' Rt Sta 73 + 50

$\frac{8.7}{105} \frac{1.7}{90} \frac{4.7}{75} \frac{4.7}{50} \frac{4.1}{32} \frac{7.6}{29} \frac{7.2}{18} \frac{5.2}{13} \frac{5.1}{5.1} \frac{5.5}{13} \frac{6.8}{16} \frac{6.8}{22} \frac{2.9}{27} \frac{2.7}{50} \frac{4.2}{100}$

$\frac{4.3}{100} \frac{4.3}{50} \frac{4.3}{33} \frac{7.0}{29} \frac{7.0}{17} \frac{5.4}{12} \frac{5.1}{5.1} \frac{5.2}{12} \frac{7.2}{18} \frac{7.2}{24} \frac{6.5}{28} \frac{2.8}{33} \frac{2.7}{50} \frac{3.7}{100}$

$\frac{4.7}{100} \frac{6.8}{90} \frac{6.9}{50} \frac{6.6}{33} \frac{9.2}{29} \frac{9.2}{18} \frac{7.4}{12} \frac{7.4}{7.4} \frac{7.7}{12} \frac{9.4}{17} \frac{9.1}{26} \frac{8.2}{30} \frac{6.5}{33} \frac{6.5}{50} \frac{6.5}{100}$

$\frac{18.6}{85} \frac{7.6}{80} \frac{6.0}{62} \frac{2.7}{38} \frac{8.1}{33} \frac{9.6}{30} \frac{9.5}{18} \frac{8.0}{14} \frac{7.5}{7.5} \frac{7.7}{12} \frac{9.4}{18} \frac{9.5}{26} \frac{8.8}{31} \frac{6.9}{33} \frac{6.7}{50} \frac{6.7}{100}$

$\frac{13.6}{90} \frac{7.6}{110}$

$\frac{6.7}{75} \frac{12.5}{60} \frac{12.5}{49} \frac{7.2}{41} \frac{5.9}{33} \frac{8.6}{29} \frac{9.7}{24} \frac{9.8}{20} \frac{8.0}{12} \frac{7.7}{7.7} \frac{8.0}{14} \frac{9.7}{18} \frac{9.9}{30} \frac{8.5}{33} \frac{8.5}{50} \frac{8.0}{100}$

$\downarrow \frac{3.9}{100}$

$\frac{4.7}{65} \frac{7.7}{46} \frac{12.8}{41} \frac{12.8}{30} \frac{10.3}{25} \frac{10.1}{19} \frac{8.1}{13} \frac{8.1}{8.1} \frac{8.4}{14} \frac{9.8}{17} \frac{10.0}{30} \frac{9.0}{33} \frac{9.3}{50} \frac{9.3}{100}$

$\downarrow \frac{7.5}{75} \frac{7.5}{100}$

$\frac{8.3}{100} \frac{9.3}{75} \frac{7.3}{57} \frac{9.6}{44} \frac{9.6}{39} \frac{12.7}{35} \frac{12.7}{24} \frac{8.5}{13} \frac{8.3}{8.3} \frac{8.5}{13} \frac{9.9}{17} \frac{10.5}{31} \frac{10.0}{34} \frac{10.0}{50} \frac{9.9}{100}$

$\frac{6.9}{65} \frac{8.3}{60} \frac{8.3}{53} \frac{10.3}{36} \frac{13.0}{31} \frac{13.0}{23} \frac{9.0}{13} \frac{8.6}{8.6} \frac{9.0}{14} \frac{10.3}{17} \frac{10.5}{30} \frac{10.6}{36} \frac{10.6}{50} \frac{10.6}{100}$

Sta	+	π ✓	-	Elev
81	3.49	908.70 ✓		905.21 ✓
82				03.4 ✓
T.P	5.54 ✓	✓ 909.40 ✓	4.84	✓ 903.86 ✓
83				03.9 ✓
84				04.1 ✓
85				04.4 ✓
86				04.7 ✓
87				05.0 ✓
T.P	3.53	✓ 910.47 ✓	2.46	✓ 906.94 ✓
88				05.0 ✓
89				05.3 ✓
+22				05.5 ✓
+40				05.7 ✓
+65				05.7 ✓

X 36" X Drain See Const Notes

LT 2 RT

5.2 6.2 6.5 7.6 9.5 9.5 7.7 5.4 5.1 6.7 6.6 6.8 6.8
 50 44 38 34 30 25 20 13 5.3 13 17 31 50 100

6.8 6.8
 60 100
 7.1 4.6 4.6 5.6 9.6 9.2 7.8 5.3 5.0 6.4 7.0 6.7 6.7
 70 60 50 40 33 23 20 12 5.1 13 12 33 50 100

7.1
 100
 6.9 4.9 5.0 6.9 7.8 10.4 10.4 8.0 5.1 5.5 7.1 7.2 6.7 7.2 7.2
 69 59 49 43 36 34 26 19 13 5.5 13 16 26 28 50 100

6.9
 100
 7.2 5.8 5.1 5.6 7.6 9.7 10.4 7.9 5.4 5.4 7.0 7.2 6.8 6.8 6.8
 70 60 50 47 38 34 27 19 12 5.3 13 18 32 34 50 100

7.2
 100
 9.3 9.3 5.3 5.1 6.9 9.4 9.1 7.8 5.2 5.0 6.3 6.8 6.7 6.2 6.2 6.2
 70 65 55 46 37 34 22 20 12 5.0 13 12 23 31 33 50 100

6.0 7.4 7.4
 80 100
 6.3 3.3 4.8 6.6 9.4 10.1 10.1 8.6 5.0 5.1 6.2 6.8 6.1 6.0 6.0
 70 55 49 39 31 29 26 23 13 4.7 13 17 29 34 50 100

6.3
 100
 6.8 6.8 3.8 3.8 6.2 9.9 9.9 4.6 5.0 6.4 6.6 4.7 4.7 4.6
 100 65 55 46 36 31 23 11 4.4 13 17 30 34 50 100

6.1 6.7 3.7 4.5 4.5 6.0 10.3 10.3 5.7 6.0 7.7 8.0 6.7 6.7 6.7
 100 76 62 50 50 44 31 24 13 5.5 13 17 25 32 50 100

3.6 3.6 6.1 7.3 11.2 11.4 10.3 5.2 5.0 8.2 8.4 5.3 4.5 7.5 7.5
 75 65 50 43 36 27 23 12 5.2 13 19 28 33 39 49 100

6.1 6.1
 85 100
 7.3 7.3 5.3 4.7 7.4 9.6 10.7 9.3 5.1 5.2 8.4 8.5 3.7 5.7 5.7
 100 85 70 50 39 35 23 20 12 5.0 13 19 29 34 50 100

13 7.3 5.3 4.7 7.4 9.6 10.7 9.3 5.1 5.2 10.5 12.0 12.5 12.5
 100 80 70 50 39 35 23 20 12 4.8 13 24 25 50 100

7.3 7.3 6.3 4.7 7.4 9.6 10.7 9.3 5.1 5.2 10.5 12.0 12.5 12.6
 100 85 70 50 39 35 23 20 12 4.8 13 24 25 50 100

11.4
 Invert
 12.0
 Invert

Sta + π ✓ - Elev

910.47

89 + 75

05.8 ✓

+ 85

05.8 ✓

90

05.9 ✓

+ 30

06.1 ✓

4.40

912.46 ✓

2.41

908.06 ✓

91

06.6 ✓

+ 50

07.0 ✓

92

07.3 ✓

+ 65

07.7 ✓

93

08.0 ✓

94

08.5 ✓

95

08.9 ✓

T.P

4.42

911.95 ✓

4.93

907.53 ✓

B.M

1.04

910.91 ✓

96

08.5 ✓

Lt Z Rt

 $\frac{11.1}{100} \quad \frac{11.1}{50} \quad \frac{11.0}{36} \quad \frac{9.7}{22} \quad \frac{4.7}{12} \quad 4.7 \quad \frac{4.8}{13} \quad \frac{8.7}{21} \quad \frac{8.8}{27} \quad \frac{6.8}{30} \quad \frac{5.8}{50} \quad \frac{5.8}{75} \quad \frac{4.3}{100}$
 $\frac{11.0}{100} \quad \frac{11.1}{50} \quad \frac{11.0}{36} \quad \frac{9.7}{22} \quad \frac{4.7}{12} \quad 4.7 \quad \frac{4.8}{13} \quad \frac{8.7}{21} \quad \frac{8.8}{27} \quad \frac{6.8}{30} \quad \frac{5.8}{50} \quad \frac{5.8}{75} \quad \frac{4.3}{100}$
 $\frac{7.4}{100} \quad \frac{5.4}{50} \quad \frac{4.9}{29} \quad \frac{7.4}{24} \quad \frac{7.4}{21} \quad \frac{4.7}{12} \quad 4.6 \quad \frac{4.5}{13} \quad \frac{7.7}{19} \quad \frac{7.1}{29} \quad \frac{7.1}{50} \quad \frac{7.0}{100}$
 $\frac{7.3}{100} \quad \frac{7.3}{50} \quad \frac{7.3}{35} \quad \frac{6.9}{20} \quad \frac{4.3}{14} \quad 4.4 \quad \frac{4.5}{13} \quad \frac{7.4}{19} \quad \frac{7.0}{29} \quad \frac{7.1}{50} \quad \frac{6.9}{100}$
 $\frac{9.0}{100} \quad \frac{8.8}{50} \quad \frac{8.8}{24} \quad \frac{8.5}{19} \quad \frac{5.8}{13} \quad 5.9 \quad \frac{6.2}{14} \quad \frac{8.5}{18} \quad \frac{8.8}{26} \quad \frac{8.9}{50} \quad \frac{8.9}{100}$
 $\frac{9.0}{100} \quad \frac{8.8}{50} \quad \frac{8.8}{24} \quad \frac{8.5}{19} \quad \frac{5.8}{13} \quad 5.5 \quad \frac{5.7}{13} \quad \frac{7.5}{17} \quad \frac{7.9}{50} \quad \frac{7.5}{100}$
 $\frac{8.7}{100} \quad \frac{8.1}{50} \quad \frac{7.6}{28} \quad \frac{7.1}{17} \quad \frac{5.3}{13} \quad 5.2 \quad \frac{5.2}{13} \quad \frac{7.1}{19} \quad \frac{7.2}{30} \quad \frac{5.7}{33} \quad \frac{4.5}{45} \quad \frac{4.1}{60} \quad \frac{4.1}{100}$
 $\frac{8.1}{100} \quad \frac{7.1}{50} \quad \frac{4.8}{34} \quad \frac{7.4}{28} \quad \frac{6.7}{17} \quad \frac{5.1}{13} \quad 4.8 \quad \frac{4.8}{14} \quad \frac{6.7}{18} \quad \frac{6.9}{29} \quad \frac{4.6}{33} \quad \frac{4.5}{50} \quad \frac{4.5}{100}$
 $\frac{7.9}{100} \quad \frac{6.9}{50} \quad \frac{5.3}{34} \quad \frac{7.2}{29} \quad \frac{6.6}{16} \quad \frac{4.8}{12} \quad 4.5 \quad \frac{4.7}{14} \quad \frac{6.3}{17} \quad \frac{6.5}{29} \quad \frac{4.3}{33} \quad \frac{4.4}{50} \quad \frac{4.4}{100}$
 $\frac{4.7}{100} \quad \frac{4.7}{50} \quad \frac{4.3}{34} \quad \frac{6.2}{31} \quad \frac{6.2}{24} \quad \frac{5.9}{16} \quad \frac{4.2}{13} \quad 4.0 \quad \frac{4.0}{14} \quad \frac{5.7}{17} \quad \frac{5.9}{30} \quad \frac{3.6}{33} \quad \frac{3.6}{50} \quad \frac{4.1}{100}$
 $\frac{3.6}{100} \quad \frac{3.5}{50} \quad \frac{3.5}{34} \quad \frac{6.0}{29} \quad \frac{5.8}{17} \quad \frac{3.8}{13} \quad 3.6 \quad \frac{3.8}{14} \quad \frac{6.2}{21} \quad \frac{5.9}{30} \quad \frac{3.7}{33} \quad \frac{3.7}{50} \quad \frac{3.8}{100}$

SpK. in Oak 40' Lt Sta 95+39

 $\frac{4.0}{100} \quad \frac{3.9}{50} \quad \frac{3.9}{33} \quad \frac{5.5}{30} \quad \frac{5.1}{18} \quad \frac{3.8}{13} \quad 3.5 \quad \frac{3.6}{13} \quad \frac{5.3}{17} \quad \frac{5.5}{29} \quad \frac{3.6}{33} \quad \frac{3.5}{50} \quad \frac{4.0}{100}$

Sta	+	Δ ✓	-	Elev
		911.95		
97				07.3 ✓
98				06.2 ✓
99				05.1 ✓
100				04.0 ✓
T.P	5.00	✓ 908.71 ✓	8.24	✓ 903.71 ✓
101				03.7 ✓
102				03.7 ✓
103				03.8 ✓
104				03.8 ✓
105				03.9 ✓
106				04.0 ✓
107				04.5 ✓
T.P	7.20	✓ 911.69 ✓	4.22	✓ 904.49 ✓
108				05.3 ✓

4 2 R4

$$\frac{5.3}{100} \frac{5.3}{50} \frac{5.3}{33} \frac{6.9}{30} \frac{6.6}{17} \frac{4.9}{13} 4.7 \frac{4.8}{13} \frac{6.9}{18} \frac{7.2}{30} \frac{5.4}{33} \frac{5.4}{50} \frac{5.1}{100}$$

$$\frac{6.2}{100} \frac{6.2}{50} \frac{6.0}{30} \frac{7.9}{31} \frac{8.4}{22} \frac{7.8}{18} \frac{6.3}{14} 5.8 \frac{5.9}{13} \frac{7.9}{19} \frac{7.6}{29} \frac{5.8}{31} \frac{5.8}{50} \frac{6.3}{100}$$

$$\frac{8.2}{100} \frac{8.2}{50} \frac{8.2}{34} \frac{9.4}{31} \frac{9.0}{17} \frac{7.2}{13} 6.9 \frac{7.1}{13} \frac{8.9}{17} \frac{9.4}{23} \frac{9.0}{29} \frac{7.6}{33} \frac{7.6}{50} \frac{7.9}{100}$$

$$\frac{11.0}{100} \frac{11.0}{65} \frac{13.0}{55} \frac{13.3}{45} \frac{10.5}{43} \frac{10.5}{33} \frac{10.1}{18} \frac{8.6}{14} 8.0 \frac{8.1}{13} \frac{9.3}{17} \frac{10.1}{22} \frac{9.7}{29} \frac{8.4}{33} \frac{7.8}{50} \frac{7.9}{100}$$

$$\frac{7.0}{100} \frac{7.0}{50} \frac{6.4}{25} \frac{7.0}{23} \frac{6.9}{17} \frac{5.4}{13} 5.0 \frac{5.2}{12} \frac{7.3}{17} \frac{7.7}{30} \frac{5.8}{50} \frac{4.7}{100}$$

$$\frac{5.2}{100} \frac{5.2}{50} \frac{4.6}{27} \frac{6.4}{23} \frac{6.5}{16} \frac{5.2}{13} 5.0 \frac{5.2}{13} \frac{6.8}{17} \frac{6.3}{23} \frac{4.5}{25} \frac{4.5}{50} \frac{5.0}{100}$$

$$\frac{4.2}{100} \frac{4.2}{50} \frac{4.8}{25} \frac{6.7}{22} \frac{6.2}{16} \frac{5.1}{13} 4.9 \frac{5.2}{13} \frac{6.9}{17} \frac{6.9}{23} \frac{5.4}{24} \frac{5.3}{50} \frac{5.3}{100}$$

$$\frac{4.8}{50} \frac{5.3}{50} \frac{5.3}{24} \frac{6.7}{22} \frac{6.6}{17} \frac{5.1}{13} 4.9 \frac{5.1}{13} \frac{6.7}{17} \frac{6.4}{22} \frac{5.1}{24} \frac{5.0}{50} \frac{5.0}{100}$$

$$\frac{6.2}{100} \frac{6.2}{50} \frac{6.7}{27} \frac{6.9}{18} \frac{5.0}{13} 4.8 \frac{5.0}{12} \frac{6.6}{17} \frac{6.7}{21} \frac{5.7}{23} \frac{5.7}{50} \frac{5.2}{100}$$

$$\frac{6.5}{100} \frac{6.0}{50} \frac{6.0}{25} \frac{6.6}{21} \frac{6.6}{17} \frac{4.8}{14} 4.7 \frac{4.7}{14} \frac{6.5}{18} \frac{6.5}{21} \frac{5.6}{24} \frac{5.7}{50} \frac{5.7}{100}$$

$$\frac{7.0}{100} \frac{7.0}{50} \frac{7.0}{27} \frac{6.5}{18} \frac{4.8}{14} 4.2 \frac{4.1}{13} \frac{6.1}{17} \frac{6.1}{22} \frac{5.5}{25} \frac{5.0}{50} \frac{4.0}{100}$$

$$\frac{9.3}{100} \frac{9.3}{50} \frac{8.7}{26} \frac{8.9}{22} \frac{8.1}{17} \frac{6.5}{14} 6.4 \frac{6.6}{13} \frac{8.2}{17} \frac{8.2}{21} \frac{7.5}{23} \frac{7.0}{50} \frac{6.0}{100}$$

549 + X ✓ - Elev
911.69

109 05.8.

110 06.6.

111 07.4.

112 07.9.

113 08.3.

114 ✓
T.P. 4.84 913.51 ✓ 3.02 08.7. ✓
908.67 ✓

115 08.7.

116 08.8.

+60 08.8.

117 08.8.

+75 08.6.

118 08.7.

LT & RT

$$\frac{7.7}{100} \frac{7.7}{50} \frac{7.5}{25} \frac{7.8}{21} \frac{7.6}{17} \frac{6.1}{13} 5.9 \quad \frac{5.1}{12} \frac{7.6}{16} \frac{7.6}{21} \frac{6.7}{23} \frac{5.7}{50} \frac{3.7}{100}$$

$$\frac{6.4}{100} \frac{6.1}{50} \frac{5.6}{24} \frac{6.6}{22} \frac{6.7}{17} \frac{5.2}{12} 5.1 \quad \frac{5.2}{13} \frac{6.6}{16} \frac{6.2}{22} \frac{4.7}{28} \frac{4.2}{50} \frac{3.2}{100}$$

$$\frac{6.5}{100} \frac{5.5}{50} \frac{5.0}{24} \frac{6.0}{21} \frac{6.2}{16} \frac{4.5}{13} 4.3 \quad \frac{4.9}{13} \frac{6.2}{17} \frac{6.0}{22} \frac{3.3}{27} \frac{2.8}{50} \frac{2.3}{100}$$

$$\frac{6.3}{100} \frac{6.1}{50} \frac{5.1}{24} \frac{5.6}{21} \frac{5.7}{18} \frac{4.2}{14} 3.8 \quad \frac{4.0}{13} \frac{5.6}{17} \frac{5.6}{21} \frac{4.0}{23} \frac{3.5}{50} \frac{2.5}{100}$$

$$\frac{4.4}{100} \frac{4.2}{50} \frac{4.5}{25} \frac{5.8}{22} \frac{5.6}{17} \frac{3.8}{13} 3.6 \quad \frac{3.7}{13} \frac{5.1}{17} \frac{5.1}{22} \frac{4.1}{23} \frac{3.6}{50} \frac{3.1}{100}$$

$$\frac{4.0}{100} \frac{3.0}{50} \frac{3.0}{28} \frac{5.2}{22} \frac{5.1}{17} \frac{3.2}{13} 3.0 \quad \frac{3.1}{13} \frac{4.7}{17} \frac{4.7}{21} \frac{3.8}{23} \frac{3.8}{50} \frac{3.3}{100}$$

$$\frac{5.5}{100} \frac{5.5}{50} \frac{5.0}{28} \frac{7.0}{23} \frac{6.8}{17} \frac{5.0}{13} 4.8 \quad \frac{5.1}{13} \frac{6.5}{16} \frac{6.5}{22} \frac{4.6}{25} \frac{4.6}{50} \frac{4.0}{100}$$

$$\frac{3.1}{100} \frac{3.1}{50} \frac{3.1}{29} \frac{5.8}{26} \frac{6.9}{22} \frac{6.9}{18} \frac{4.8}{13} 4.7 \quad \frac{5.0}{13} \frac{6.3}{16} \frac{6.4}{22} \frac{2.9}{28} \frac{3.4}{50} \frac{4.0}{100}$$

$$\frac{3.4}{100} \frac{3.4}{50} \frac{3.4}{30} \frac{6.2}{26} \frac{7.1}{22} \frac{6.8}{15} \frac{5.0}{11} 4.7 \quad \frac{4.9}{14} \frac{6.3}{17} \frac{6.3}{21} \frac{5.7}{24} \frac{3.0}{26} \frac{3.5}{50} \frac{4.5}{100}$$

$$\frac{3.6}{100} \frac{5.6}{50} \frac{5.8}{25} \frac{7.0}{22} \frac{6.6}{16} \frac{4.9}{13} 4.7 \quad \frac{4.9}{13} \frac{6.7}{17} \frac{6.7}{22} \frac{5.9}{24} \frac{5.5}{50} \frac{6.0}{100}$$

$$\frac{3.6}{100} \frac{3.6}{75} \frac{5.8}{50} \frac{6.4}{29} \frac{7.0}{27} \frac{7.3}{19} \frac{5.0}{12} 4.9 \quad \frac{4.9}{15} \frac{8.0}{21} \frac{8.6}{34} \frac{7.5}{50} \frac{5.5}{100}$$

$$\frac{1.6}{100} \frac{5.2}{50} \frac{6.3}{26} \frac{7.1}{23} \frac{7.0}{18} \frac{5.0}{13} 4.8 \quad \frac{4.8}{15} \frac{8.3}{21} \frac{8.4}{26} \frac{6.4}{50} \frac{4.4}{100}$$

Sta	+	π $\checkmark$	-	Elev
		913.51		

119				09.1
-----	--	--	--	------

120				09.4
-----	--	--	--	------

+34				09.3
-----	--	--	--	------

+45				09.4
-----	--	--	--	------

+57		West shoulder		09.4 STH #8
-----	--	---------------	--	----------------

+77		± STH #8		08.96
-----	--	----------	--	-------

BM		4.55		908.96
----	--	------	--	--------

Equation

120 + 77 = See A Line
Notes

LH A RH

$$\frac{3.1}{100} \quad \frac{5.1}{50} \quad \frac{5.2}{26} \quad \frac{6.2}{22} \quad \frac{6.1}{17} \quad \frac{4.4}{13} \quad 4.4 \quad \frac{4.5}{13} \quad \frac{6.3}{17} \quad \frac{6.2}{21} \quad \frac{4.8}{24} \quad \frac{3.8}{50} \quad \frac{2.8}{100}$$

$$\frac{3.5}{100} \quad \frac{3.6}{50} \quad \frac{3.6}{28} \quad \frac{6.0}{20} \quad \frac{6.0}{16} \quad \frac{4.4}{12} \quad 4.1 \quad \frac{4.3}{13} \quad \frac{5.8}{17} \quad \frac{6.7}{22} \quad \frac{3.8}{25} \quad \frac{3.8}{50} \quad \frac{3.6}{100}$$

$$\frac{4.9}{100} \quad \frac{4.9}{50} \quad \frac{4.7}{26} \quad \frac{5.6}{16} \quad \frac{4.5}{12} \quad 4.2 \quad \frac{4.5}{14} \quad \frac{6.1}{18} \quad \frac{6.1}{22} \quad \frac{5.2}{26} \quad \frac{4.8}{50} \quad \frac{3.9}{100}$$

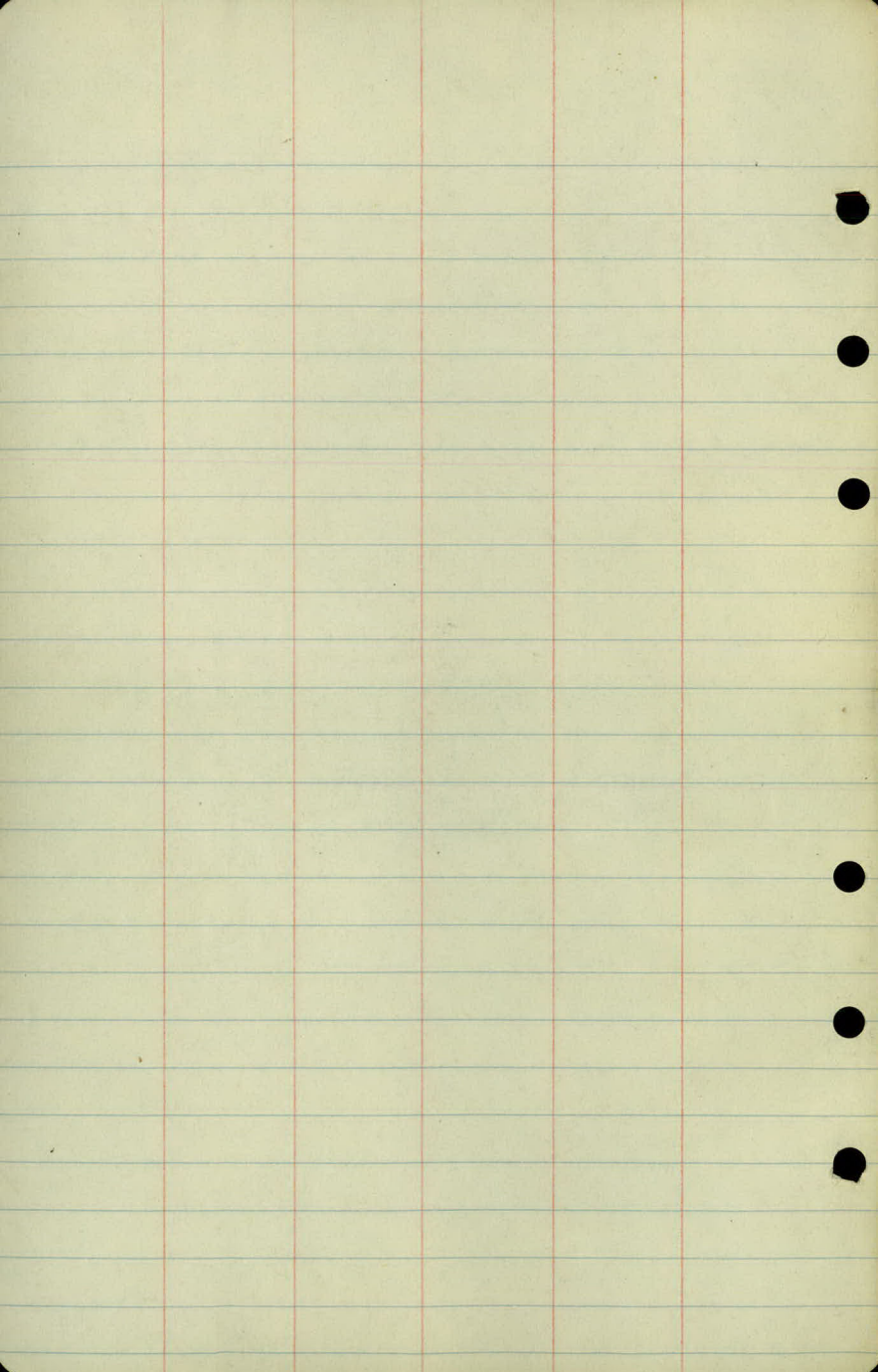
$$\frac{8.1}{100} \quad \frac{7.2}{50} \quad \frac{7.1}{35} \quad \frac{5.7}{20} \quad \frac{4.4}{14} \quad 4.1 \quad \frac{4.6}{13} \quad \frac{6.0}{20} \quad \frac{6.6}{26} \quad \frac{7.2}{50} \quad \frac{7.5}{100}$$

$$\frac{4.4}{100} \quad 4.1 \quad \frac{4.2}{100}$$

$$\frac{5.10}{100} \quad 4.55 \quad \frac{4.35}{100}$$

909.02

Brass Plug in STH #8



8
Level Notes.

North County Line

East from S.T.H. #8

by

W. P. A. Eng'r Crew

J. J. Howes

Superv. Engr.

9/1/36

Sta	+R.	H.I.	-R.	Elevn
B.M.	4.17	913.19		909.02
		914.09		909.92

100+74.2

5.1 ^{08.1}
~~909.02~~

100+83.2

5.0 ^{08.2}
~~909.1~~

100+90

5.0 ^{08.2}
~~909.1~~

101

4.8 ^{08.4}
~~09.3~~

+50

5.0 ^{08.2}
~~09.1~~

102

4.4 ^{08.8}
~~09.7~~

+50

4.6 ^{08.6}
~~09.5~~

103

5.0 ^{08.2}
~~09.1~~

+50

5.4 ^{07.8}
~~08.7~~

Sta 100+90
Provide 12" C.M. under new road.
Drainage is to the South.

9/1/36
T. J. Holmes

Spikes in Brass Piny E.P.T. Highway #8 (100+60.3)

= Edge of P.V.T. $\frac{5.0}{40^\circ \text{ Lt. } 5.1}$ $\frac{5.1}{40^\circ \text{ Rt.}}$

#8	$\frac{54}{50}$	$\frac{49}{37}$	$\frac{51}{25}$	5.0	$\frac{53}{30}$	$\frac{49}{45}$	$\frac{49}{55}$	Pavement has super-elevation
Shoulder								

$\frac{74}{50}$	$\frac{66}{27}$	$\frac{51}{19}$	5.0	$\frac{55}{17}$	$\frac{55}{24}$	$\frac{61}{50}$
-----------------	-----------------	-----------------	-----	-----------------	-----------------	-----------------

$\frac{73}{50}$	$\frac{62}{34}$	$\frac{49}{18}$	4.8	$\frac{53}{13}$	$\frac{56}{22}$	$\frac{61}{50}$
-----------------	-----------------	-----------------	-----	-----------------	-----------------	-----------------

$\frac{57}{50}$	Fce $\frac{46}{25}$	$\frac{52}{20}$	$\frac{46}{10}$	5.0	$\frac{6.0}{9.}$	$\frac{49}{12}$	$\frac{5.6}{50}$
-----------------	---------------------	-----------------	-----------------	-----	------------------	-----------------	------------------

$\frac{49}{50}$	$\frac{47}{31}$	$\frac{39}{24}$	$\frac{48}{18}$	$\frac{41}{8.0}$	4.4	$\frac{46}{10}$	$\frac{48}{16 \text{ Fce}}$	$\frac{56}{50}$
-----------------	-----------------	-----------------	-----------------	------------------	-----	-----------------	-----------------------------	-----------------

$\frac{43}{50}$	$\frac{44}{31}$	$\frac{36}{25}$	$\frac{47}{21}$	$\frac{42}{9.0}$	4.6	$\frac{5.6}{9.0}$	$\frac{52}{14.}$	$\frac{61}{50}$
-----------------	-----------------	-----------------	-----------------	------------------	-----	-------------------	------------------	-----------------

$\frac{45}{50}$	$\frac{46}{32}$	$\frac{40}{27}$	$\frac{52}{22}$	$\frac{45}{9.0}$	5.0	$\frac{6.0}{5.6}$	$\frac{5.3}{13.}$	$\frac{6.6}{50}$
-----------------	-----------------	-----------------	-----------------	------------------	-----	-------------------	-------------------	------------------

$\frac{45}{50}$	$\frac{49}{32}$	$\frac{44}{27}$	$\frac{54}{22}$	$\frac{47}{10}$	5.4	$\frac{58}{6}$	$\frac{53}{10}$	$\frac{58}{13}$	$\frac{68}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----	----------------	-----------------	-----------------	-----------------

Fce.

~~914.09~~
713.19

104+00

5.6

~~07.6~~
~~908.5~~

+50

5.7

~~07.5~~
~~08.4~~

T.P.

5.47

~~913.46~~
~~914.36~~ 5.20

~~07.79~~
~~908.89~~

105 4

6.0

~~07.5~~
~~08.4~~

+50

6.0

~~07.5~~
~~08.4~~

106

5.5

~~08.0~~
~~08.9~~

+50

5.5

~~08.0~~
~~08.9~~

107

5.2

~~08.3~~
~~09.2~~

+50

4.9

~~08.6~~
~~09.5~~

108

5.1

~~08.4~~
~~09.3~~ ✓

9/1/36

$$\begin{array}{cccccccccccc} \frac{4.9}{50} & \frac{5.4}{34} & \frac{4.8}{29} & \frac{5.9}{23} & \frac{4.9}{11} & \frac{6.2}{5.0} & \frac{6.4}{13} & \frac{6.9}{28} & \frac{6.9}{50} \\ & & & & & R_1 & F_1 & & \end{array}$$

$\frac{5.0}{50}$	$\frac{5.5}{35}$	$\frac{5.1}{Fe30}$	$\frac{5.9}{24}$	$\frac{5.1}{10}$	57	$\frac{6.2}{8}$	$\frac{6.1}{14Fe}$	$\frac{6.6}{24}$	$\frac{7.0}{50}$
------------------	------------------	--------------------	------------------	------------------	----	-----------------	--------------------	------------------	------------------

T.P. Top of Stake 105+00

$\frac{5.1}{50}$	$\frac{5.5}{37}$	$\frac{5.4}{31}$	$\frac{6.2}{24}$	$\frac{5.4}{7}$	$\frac{6.5}{5}$	$\frac{6.4}{14}$	$\frac{6.6}{23}$	$\frac{6.7}{50}$
		Fe		60		Feb		

$\frac{4.7}{50}$	$\frac{4.9}{38}$	$\frac{4.6}{32 F_c}$	$\frac{5.6}{25}$	$\frac{5.2}{12}$	$\frac{6.3}{5}$	$\frac{6.0}{13 F_c}$	$\frac{6.1}{20}$	$\frac{6.5}{50}$
------------------	------------------	----------------------	------------------	------------------	-----------------	----------------------	------------------	------------------

$\frac{4.6}{50}$	$\frac{4.8}{38}$	$\frac{4.2}{31}$	$\frac{5.3}{26}$	$\frac{4.9}{12}$	$\frac{6.2}{5}$	$\frac{5.7}{14}$	$\frac{6.2}{23}$	$\frac{6.5}{50}$
		F_c		55		F_c		

$$\frac{4.6}{50} \quad \frac{4.4}{38} \quad \frac{3.9}{31.5} \quad \frac{5.2}{26} \quad \frac{4.7}{11} \quad 55 \quad \frac{6.0}{6} \quad \frac{5.2}{13} \quad \frac{6.0}{23} \quad \frac{6.7}{50}$$

$\frac{48}{50}$	$\frac{48}{39}$	$\frac{40}{32}$	$\frac{51}{22}$	$\frac{45}{12}$	$\frac{59}{5}$	$\frac{50}{13}$	$\frac{55}{23}$	$\frac{64}{50}$
		Fe		52		Fe		

$\frac{5.1}{50}$	$\frac{4.9}{39}$	$\frac{4.1}{32}$	$\frac{5.2}{26}$	$\frac{4.3}{12}$	4.9	$\frac{5.5}{6}$	$\frac{4.5}{14 F_c}$	$\frac{5.1}{22}$	$\frac{5.9}{50}$
		F_c							

$$\frac{58}{50} \quad \frac{56}{39} \quad \frac{46}{33} \quad \frac{53}{26} \quad \frac{46}{11} \quad 51 \quad \frac{54}{5} \quad \frac{45}{14} \text{Fc} \quad \frac{49}{25} \quad \frac{57}{50}$$

~~914.36~~
~~913.46~~

108+50

~~07.5~~
~~908.4~~

109

~~07.2~~
~~08.1~~

+50

~~07.4~~
~~08.3~~

110

~~07.5~~
~~08.4~~

T.P.

4.05

~~913.50~~

~~914.40~~

4.01

~~909.45~~
~~910.35~~

110+50

~~08.1~~
~~09.0~~

111

~~08.8~~
~~09.7~~

+50

~~09.1~~
~~10.0~~

112

~~09.0~~
~~9.9~~

+28 = 2 N & S Rd

~~09.2~~
~~10.1~~

2

9/1/36

$\frac{6.9}{50}$ $\frac{6.5}{41}$ $\frac{6.0}{34 F_c}$ $\frac{6.3}{27}$ $\frac{5.4}{13 L_t}$ $\frac{6.2}{4 R_t}$ $\frac{6.0}{14 F_c}$ $\frac{6.1}{25}$ $\frac{6.2}{50}$

$\frac{7.0}{50}$ $\frac{7.0}{41}$ $\frac{6.2}{35 F_c}$ $\frac{6.7}{28}$ $\frac{5.5}{12}$ $\frac{7.2}{5}$ $\frac{6.7}{13 F_c}$ $\frac{6.8}{26}$ $\frac{6.4}{50}$

$\frac{6.5}{50}$ $\frac{6.6}{39}$ $\frac{5.9}{35 F_c}$ $\frac{6.6}{27}$ $\frac{5.5}{12}$ $\frac{7.0}{5}$ $\frac{6.4}{14 F_c}$ $\frac{6.9}{30}$ $\frac{6.7}{50}$

$\frac{5.7}{50}$ $\frac{5.7}{31}$ $\frac{5.2}{26}$ $\frac{6.1}{27}$ $\frac{5.3}{13}$ $\frac{6.5}{5}$ $\frac{6.2}{14 F_c}$ $\frac{6.5}{25}$ $\frac{6.6}{50}$

Stump of Post 35 It. of 110 + 100

$\frac{4.7}{50}$ $\frac{4.0}{36}$ $\frac{4.7}{31 F_c}$ $\frac{5.3}{23}$ $\frac{5.0}{13}$ $\frac{5.6}{10}$ $\frac{5.8}{14 F_c}$ $\frac{6.1}{27}$ $\frac{6.6}{50}$

$\frac{4.4}{50}$ $\frac{4.2}{43}$ $\frac{3.4}{36 F_c}$ $\frac{4.8}{24}$ $\frac{4.4}{14}$ $\frac{4.4}{11}$ $\frac{5.6}{22}$ $\frac{6.2}{50}$

$\frac{4.2}{50}$ $\frac{3.5}{38 F_c}$ $\frac{3.8}{31}$ $\frac{4.5}{28}$ $\frac{4.4}{13}$ $\frac{4.2}{14 F_c}$ $\frac{4.9}{25}$ $\frac{5.6}{50}$

$\frac{4.7}{65}$ $\frac{5.9}{44}$ $\frac{4.4}{30}$ $\frac{4.2}{13}$ $\frac{4.0}{6}$ $\frac{3.9}{14 F_c}$ $\frac{4.4}{25}$ $\frac{4.9}{50}$

$\frac{6.1}{100}$ $\frac{5.6}{50}$ $\frac{4.6}{30}$ $\frac{4.3}{13}$ $\frac{3.9}{15 F_c}$ $\frac{4.3}{25}$ $\frac{4.8}{50}$

~~914.40~~
913.50

112+50

4.4 ~~09.1~~
~~910.0~~

113

4.6 ~~08.9~~
~~09.8~~

+50

5.3 ~~08.2~~
~~09.1~~

114

5.9 ~~07.6~~
~~08.5~~

+50

6.2 ~~07.3~~
~~08.2~~

115

6.1 ~~07.4~~
~~08.3~~

+50

5.3 ~~08.2~~
~~08.3~~

T.P.

0.44

912.26
~~913.16~~ 1.68

911.82
~~912.72~~

116

5.3 ~~07.0~~
~~07.9~~

+50

5.7 ~~06.6~~
~~07.5~~

117

5.7 ~~06.6~~
~~07.5~~

9/1/36

$$\frac{5.5}{50}$$

$$\frac{4.9}{30 \text{ FC}}$$

$$\frac{4.4}{12 \text{ L} + 44}$$

$$\frac{4.0}{3 \text{ Rt.}}$$

$$\frac{3.7}{15 \text{ FC}}$$

$$\frac{4.3}{25}$$

$$\frac{4.9}{50}$$

$$\frac{5.8}{50}$$

$$\frac{4.9}{31 \text{ FC}}$$

$$\frac{5.5}{27}$$

$$\frac{4.5}{11}$$

$$\frac{4.1}{15 \text{ FC}}$$

$$\frac{4.8}{25}$$

$$\frac{5.4}{50}$$

$$\frac{6.2}{50}$$

$$\frac{3.4}{23 \text{ FC}}$$

$$\frac{6.0}{24}$$

$$\frac{4.9}{12}$$

$$53$$

$$\frac{4.2}{14}$$

$$\frac{5.6}{25}$$

$$\frac{6.0}{50}$$

$$\frac{7.0}{50}$$

$$\frac{6.4}{23 \text{ FC}}$$

$$\frac{7.0}{24}$$

$$\frac{6.1}{23}$$

$$\frac{5.5}{12}$$

$$59$$

$$\frac{6.2}{7}$$

$$\frac{5.5}{15 \text{ FC}}$$

$$\frac{6.1}{25}$$

$$\frac{6.8}{50}$$

$$\frac{6.2}{50}$$

$$\frac{6.3}{34 \text{ FC}}$$

$$\frac{7.1}{28}$$

$$\frac{5.7}{12}$$

$$62$$

$$\frac{7.0}{7}$$

$$\frac{6.4}{14 \text{ FC}}$$

$$\frac{6.8}{25}$$

$$\frac{8.0}{50}$$

$$\frac{5.3}{50}$$

$$\frac{4.8}{33 \text{ FC}}$$

$$\frac{6.0}{26}$$

$$\frac{6.1}{21}$$

$$\frac{5.5}{11}$$

$$62$$

$$\frac{6.9}{7}$$

$$\frac{6.4}{14 \text{ FC}}$$

$$\frac{7.2}{25}$$

$$\frac{8.3}{50}$$

$$\frac{4.9}{50}$$

$$\frac{4.2}{37 \text{ FC}}$$

$$\frac{5.9}{26}$$

$$\frac{5.5}{13}$$

$$61$$

$$\frac{6.7}{7}$$

$$\frac{6.2}{14 \text{ FC}}$$

$$\frac{7.1}{25}$$

$$\frac{8.3}{50}$$

Top of Fence-post 114+97 33' left

$$\frac{4.1}{50}$$

$$\frac{3.7}{32 \text{ FC}}$$

$$\frac{5.0}{25}$$

$$\frac{4.5}{12}$$

$$53$$

$$\frac{6.2}{8}$$

$$\frac{5.8}{14 \text{ FC}}$$

$$\frac{7.7}{50}$$

$$\frac{4.1}{50}$$

$$\frac{4.0}{32}$$

$$\frac{5.8}{25}$$

$$\frac{5.0}{12}$$

$$57$$

$$\frac{6.8}{7}$$

$$\frac{6.4}{14 \text{ FC}}$$

$$\frac{8.1}{50}$$

$$\frac{4.6}{50}$$

$$\frac{4.3}{32}$$

$$\frac{5.8}{21}$$

$$\frac{5.4}{9}$$

$$57$$

$$\frac{5.5}{4}$$

$$\frac{7.1}{8}$$

$$\frac{6.7}{14 \text{ FC}}$$

$$\frac{8.6}{50}$$

~~913.16~~
912.26

117 + 50

5.4

06.9

~~07.8~~

118

5.0

07.3

08.2

11 + 50

4.6

07.7

~~08.6~~

119

4.6

07.7

~~08.6~~

+ 50

4.4

07.9

~~08.8~~

120

4.5

07.8

~~08.7~~

+ 50

4.7

07.6

~~08.5~~

121

4.2

08.1

~~09.0~~

+ 50

3.2

09.1

~~10.0~~

122

2.7

09.6

~~10.5~~

$$\frac{4.5}{50} \quad \frac{4.0}{31} \text{ FC } \frac{5.5}{23} \quad \frac{5.0}{4} \text{ SA } \frac{5.9}{6} \quad \frac{6.9}{7} \quad \frac{6.3}{14} \text{ FC } \quad \frac{8.2}{50}$$

$$\frac{4.0}{50} \quad \frac{3.4}{30} \text{ FC } \quad \frac{5.2}{22} \quad \frac{4.5}{7} \quad \frac{5.0}{5} \quad \frac{5.3}{5} \quad \frac{6.3}{9} \quad \frac{5.9}{15} \text{ FC } \quad \frac{7.6}{50}$$

$$\frac{3.7}{50} \quad \frac{2.1}{30} \text{ FC } \quad \frac{4.5}{21} \quad \frac{4.3}{7} \quad \frac{5.0}{6} \quad \frac{6.0}{10} \quad \frac{5.5}{15} \text{ FC } \quad \frac{7.2}{50}$$

$$\frac{4.2}{50} \quad \frac{3.3}{30} \text{ FC } \quad \frac{4.9}{23} \quad \frac{4.3}{6} \quad \frac{4.9}{7} \quad \frac{6.0}{11} \quad \frac{5.3}{15} \text{ FC } \quad \frac{7.0}{50}$$

$$\frac{4.9}{50} \quad \frac{3.8}{29} \text{ FC } \quad \frac{5.1}{23} \quad \frac{4.4}{6} \quad \frac{4.4}{7} \quad \frac{4.5}{15} \text{ FC } \quad \frac{6.1}{50}$$

$$\frac{5.3}{50} \quad \frac{4.4}{28} \text{ FC } \quad \frac{5.6}{22} \quad \frac{5.0}{15} \quad \frac{4.5}{7} \quad \frac{4.4}{15} \text{ FC } \quad \frac{5.5}{50}$$

$$\frac{5.2}{50} \quad \frac{4.4}{28} \text{ FC } \quad \frac{5.6}{22} \quad \frac{5.2}{14} \quad \frac{4.7}{8} \quad \frac{4.1}{16} \text{ FC } \quad \frac{5.8}{50}$$

$$\frac{4.4}{50} \quad \frac{3.4}{27} \text{ FC } \quad \frac{4.7}{21} \quad \frac{4.4}{13} \quad \frac{4.4}{9} \quad \frac{4.8}{16} \text{ FC } \quad \frac{5.6}{50}$$

$$\frac{3.3}{50} \quad \frac{2.5}{39} \quad \frac{2.6}{27} \text{ FC } \quad \frac{4.0}{21} \quad \frac{3.5}{12} \quad \frac{3.7}{9} \quad \frac{4.6}{16} \text{ FC } \quad \frac{5.1}{50}$$

$$\frac{2.4}{50} \quad \frac{1.9}{27} \text{ FC } \quad \frac{3.3}{21} \quad \frac{2.4}{13} \quad \frac{3.4}{8} \quad \frac{3.0}{16} \text{ FC } \quad \frac{4.5}{50}$$

~~973.16~~
912.26

122+50

2.4

09.9

~~10.9~~

123

2.3

10.0

~~10.9~~

+ 50

2.7

09.6

10.5

124

3.7

08.6

09.5

T.P.

0.85

911.51

912.41 1.60

910.60

~~911.56~~

+ 50

4.1

07.4

~~08.3~~

125

4.4

07.1

~~08.0~~

+ 50

4.4

07.1

~~08.0~~

126

4.1

07.4

~~08.3~~

+ 50

4.6

06.9

~~07.8~~

B.M.

2.67

908.61

~~909.51~~ 5.57

905.94

~~906.84~~

2

9/1/36

$\frac{1.9}{30}$ $\frac{17}{26} \frac{2.9}{22}$ $\frac{27}{12} \frac{2.4}{11}$ $\frac{2.9}{11}$ $\frac{3.0}{17} \text{FC}$ $\frac{4.0}{50}$

$\frac{2.2}{50}$ $\frac{1.8}{23} \text{FC}$ $\frac{3.0}{20}$ $\frac{27}{13} \frac{2.3}{8} \frac{2.9}{8}$ $\frac{2.3}{17}$ $\frac{3.1}{27}$ $\frac{3.9}{50}$

$\frac{2.8}{50}$ $\frac{2.3}{25} \text{F}$ $\frac{3.3}{14}$ $\frac{3.2}{11} \frac{2.7}{8} \frac{3.0}{8}$ $\frac{2.7}{17} \text{FC}$ $\frac{3.5}{28}$ $\frac{4.1}{50}$

$\frac{4.2}{30}$ $\frac{3.4}{24} \text{FC}$ $\frac{4.3}{18}$ $\frac{4.2}{10} \frac{3.7}{9} \frac{4.3}{9}$ $\frac{4.0}{17} \text{FC}$ $\frac{4.6}{27}$ $\frac{5.2}{50}$

Top of Fence post 24+95 Left

$\frac{4.7}{50}$ $\frac{4.5}{27}$ $\frac{4.0}{23} \text{FC}$ $\frac{5.1}{17}$ $\frac{4.6}{10} \text{A}$ $\frac{4.5}{10}$ $\frac{4.8}{17} \text{FC}$ $\frac{5.1}{27}$ $\frac{5.7}{50}$

$\frac{5.1}{50}$ $\frac{4.4}{36}$ $\frac{4.8}{24}$ $\frac{4.5}{22} \text{FC}$ $\frac{5.5}{18}$ $\frac{4.8}{10} \text{A}$ $\frac{4.8}{9}$ $\frac{5.1}{14} \text{FC}$ $\frac{5.8}{28}$ $\frac{6.2}{50}$

$\frac{4.2}{50}$ $\frac{4.3}{24} \text{FC}$ $\frac{5.3}{17}$ $\frac{4.8}{10} \text{A}$ $\frac{4.8}{10}$ $\frac{4.9}{13} \text{FC}$ $\frac{5.6}{24}$ $\frac{6.0}{50}$

$\frac{3.9}{50}$ $\frac{3.4}{23}$ $\frac{4.6}{17}$ $\frac{4.6}{10} \text{A}$ $\frac{4.7}{10}$ $\frac{4.2}{18}$ $\frac{5.0}{26}$ $\frac{5.7}{50}$

$\frac{4.1}{50}$ $\frac{4.1}{23} \text{FC}$ $\frac{5.2}{17}$ $\frac{5.0}{10} \text{A}$ $\frac{5.1}{10}$ $\frac{4.9}{19} \text{FC}$ $\frac{5.5}{28}$ $\frac{6.2}{50}$

Stop M₁₂ 126+91.28

Sta

+

~~909.51~~
 908.61
 H.1

-

Elev.ⁿ

127

 06.1
~~907.0~~

+50

 05.2
~~906.1~~

128

 04.7
~~905.6~~

+50

 04.3
~~905.2~~

129

 04.3
~~905.2~~

+50

 03.8
~~904.7~~

130

 04.0
~~904.9~~

+50

 04.5
~~905.4~~

131

 05.3
~~906.2~~

+50

 06.2
~~907.1~~

 Need 18" CM about 130
 drainage to north

Lt.

E

Rt.

9/3/36

$\frac{22}{50}$	$\frac{23}{25}$	$\frac{16}{22}$	$\frac{30}{16}$	$\frac{29}{8}$		$\frac{32}{12}$	$\frac{30}{20}$	$\frac{39}{31}$	$\frac{42}{50}$
		F_c			2.5		F_c		

$\frac{32}{50}$	$\frac{32}{24}$	$\frac{23}{20}$	$\frac{35}{14}$	$\frac{38}{7}$	3.4	$\frac{39}{10}$	$\frac{42}{21 F_c}$	$\frac{48}{30}$	$\frac{54}{50}$
		F_c							

$\frac{45}{50}$	$\frac{41}{24}$	$\frac{36}{20 F_c}$	$\frac{44}{15}$	$\frac{43}{8}$	3.9	$\frac{44}{12}$	$\frac{49}{21 F_c}$	$\frac{54}{28}$	$\frac{61}{50}$

$\frac{49}{50}$	$\frac{49}{21 F_c}$	$\frac{55}{18}$	$\frac{46}{8}$	4.3	$\frac{47}{12}$	$\frac{51}{21 F_c}$	$\frac{59}{30}$	$\frac{63}{50}$

$\frac{63}{50}$	$\frac{61}{28}$	$\frac{65}{19 F_c}$	$\frac{49}{8}$	4.3	$\frac{47}{12}$	$\frac{60}{21 F_c}$	$\frac{57}{30}$	$\frac{60}{50}$

$\frac{73}{50}$	$\frac{69}{30}$	$\frac{71}{20 F_c}$	$\frac{52}{7}$	4.8	$\frac{50}{13}$	$\frac{60}{22 F_c}$	$\frac{50}{26}$	$\frac{50}{50}$

$\frac{71}{50}$	$\frac{62}{31}$	$\frac{67}{19 F_c}$	$\frac{50}{8}$	4.6	$\frac{49}{12}$	$\frac{55}{22 F_c}$	$\frac{47}{28}$	$\frac{42}{50}$

$\frac{61}{50}$	$\frac{50}{31}$	$\frac{58}{19 F_c}$	$\frac{46}{7}$	4.1	$\frac{44}{11}$	$\frac{45}{22 F_c}$	$\frac{37}{29}$	$\frac{34}{50}$

$\frac{53}{50}$		$\frac{42}{18 F_c}$	$\frac{27}{6}$	3.3	$\frac{39}{13}$	$\frac{43}{21 F_c}$	$\frac{27}{27}$	$\frac{27}{50}$

$\frac{43}{50}$	$\frac{34}{36}$	$\frac{31}{20}$	$\frac{38}{15}$	$\frac{29}{7}$	2.4	$\frac{31}{13}$	$\frac{36}{20.5 F_c}$	$\frac{16}{29}$	$\frac{16}{50}$
		F_c							

	+	909.51 908.61	-	Elev ² 07.3 908.2
132				
T.P.	6.47	914.85 915.75	0.23	908.38 909.28 08.4 909.2
+50				
133				09.0 909.8
+50				09.7 909.5
134				10.4 911.2
+50				11.0 911.8
135				11.4 912.2
+50				11.0 911.8
136				10.5 911.2
+50				10.0 910.8

L4

E

R4

9/3/36

$\frac{3.0}{50}$	$\frac{1.9}{19F}$	$\frac{2.5}{14}$	$\frac{1.9}{8}$	13	$\frac{2.0}{13}$	$\frac{2.4}{21F}$	$\frac{0.5}{30}$	$\frac{0.6}{50}$
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T.P. on dirt in ϕ 132 + 50

$\frac{8.0}{50}$	$\frac{7.1}{19F}$	$\frac{8.1}{14}$	$\frac{6.8}{6}$	✓ 6.5	$\frac{7.0}{14}$	$\frac{6.8}{23F}$	$\frac{6.1}{29}$	$\frac{5.8}{50}$
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$\frac{6.5}{50}$	$\frac{5.9}{19F}$	$\frac{7.2}{14}$	$\frac{6.3}{6}$	✓ 5.9	$\frac{6.2}{14}$	$\frac{7.2}{23F}$	$\frac{5.6}{29}$	$\frac{5.4}{50}$
------------------	-------------------	------------------	-----------------	----------	------------------	-------------------	------------------	------------------

$\frac{6.0}{50}$	$\frac{5.0}{19F}$	$\frac{6.4}{14}$	$\frac{5.5}{9}$	✓ 5.2	$\frac{5.7}{15}$	$\frac{5.8}{23F}$	$\frac{5.1}{29}$	$\frac{4.6}{50}$
------------------	-------------------	------------------	-----------------	----------	------------------	-------------------	------------------	------------------

$\frac{5.7}{50}$	$\frac{4.3}{18F}$	$\frac{5.6}{13}$	$\frac{4.9}{6}$	✓ 4.5	$\frac{4.4}{7}$	$\frac{4.8}{14}$	$\frac{5.1}{21}$	$\frac{4.6}{26F}$	$\frac{4.5}{50}$
------------------	-------------------	------------------	-----------------	----------	-----------------	------------------	------------------	-------------------	------------------

$\frac{5.3}{50}$	$\frac{3.7}{17F}$	$\frac{5.0}{12}$	$\frac{4.2}{5}$	✓ 3.9	$\frac{3.8}{9}$	$\frac{4.1}{17}$	$\frac{4.1}{24F}$	$\frac{3.7}{32}$	$\frac{3.9}{50}$
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$\frac{5.0}{50}$	$\frac{3.9}{21}$	$\frac{3.3}{16F}$	$\frac{4.6}{12}$	$\frac{3.8}{7.0}$	✓ 3.5	$\frac{3.8}{14}$	$\frac{4.0}{25F}$	$\frac{3.5}{50}$
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$\frac{5.7}{50}$	$\frac{4.2}{21}$	$\frac{3.7}{17F}$	$\frac{5.0}{12}$	$\frac{4.3}{8}$	✓ 3.9	$\frac{4.2}{14}$	$\frac{4.3}{25F}$	$\frac{3.9}{29}$	$\frac{3.1}{50}$
------------------	------------------	-------------------	------------------	-----------------	----------	------------------	-------------------	------------------	------------------

$\frac{6.5}{50}$	$\frac{5.4}{21}$	$\frac{4.7}{17F}$	$\frac{5.9}{12}$	$\frac{4.9}{9}$	✓ 4.4	$\frac{4.8}{15}$	$\frac{4.5}{24F}$	$\frac{4.5}{30}$	$\frac{4.6}{50}$
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$\frac{5.9}{50}$	$\frac{4.8}{18F}$	$\frac{5.7}{13}$	$\frac{5.1}{5}$	✓ 4.9	$\frac{4.6}{7}$	$\frac{5.0}{15}$	$\frac{4.8}{22F}$	$\frac{4.6}{28}$	$\frac{4.8}{50}$
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915.75

Sta

+

~~914.85~~

-

Elev'n

10.0

~~910.8~~

137

09.8

~~910.6~~

+50

10.3

~~911.1~~

138

10.5

~~911.3~~

+50

10.8

~~911.6~~

139

11.81

B.M.

3.29

915.10

~~916.00~~

3.04

~~912.71~~

+50

11.5

~~912.1~~

140

12.0

~~912.6~~

11.6

~~912.2~~

+50

11.6

~~912.2~~

141

11.3

~~911.9~~

+50

Sta	+	916.00 915.10 H.1	-	Elev
142			911.5	10.6
+50			910.1	09.2
143			908.5	07.6
+50			907.9	07.0
144			907.9	07.0
+50			908.4	07.5
145			909.1	08.2
+50			909.1	08.2
TP	0.06	912.86 913.96	2.30	913.70 912.80
146			911.5	08.4
+50			911.0	07.9
147			910.6	07.5
+50			909.9	06.8
148			909.6	06.5

Need 16" CM about 144
Drainage to south

L

E

R

9/3/36

$\frac{3.6}{50}$	$\frac{3.6}{22}$	$\frac{5.0}{7}$	4.5	$\frac{5.1}{21}$	$\frac{4.2}{24 Fc}$	$\frac{4.8}{50}$		
$\frac{5.2}{50}$	$\frac{5.6}{26 Fc}$	$\frac{6.7}{19}$	$\frac{6.5}{18}$	5.9	$\frac{6.7}{14}$	$\frac{7.7}{18}$	$\frac{8.2}{25 Fc}$	$\frac{9.3}{50}$
$\frac{5.4}{50}$	$\frac{7.1}{27 Fc}$	$\frac{8.5}{19}$	$\frac{7.9}{7}$	7.5	$\frac{8.1}{12}$	$\frac{11.5}{18}$	$\frac{4.2}{24 Fc}$	$\frac{13.6}{50}$
$\frac{5.3}{50}$	$\frac{6.9}{27 Fc}$	$\frac{8.9}{15}$	$\frac{8.1}{11}$	8.1	$\frac{8.5}{12}$	$\frac{13.4}{19}$	$\frac{18.6}{50}$	
$\frac{5.1}{50}$	$\frac{6.4}{27 Fc}$	$\frac{8.2}{20}$	$\frac{8.5}{13}$	8.1	$\frac{8.7}{11}$	$\frac{13.5}{17}$	$\frac{14.0}{24 Fc}$	$\frac{18.0}{50}$
$\frac{4.4}{50}$	$\frac{5.2}{25 Fc}$	$\frac{7.6}{20}$	$\frac{8.0}{13}$	7.6	$\frac{8.2}{10}$	$\frac{10.8}{16}$	$\frac{11.5}{23 Fc}$	$\frac{14.4}{50}$
$\frac{3.4}{50}$	$\frac{3.6}{24 Fc}$	$\frac{6.1}{21}$	$\frac{7.2}{13}$	6.9	$\frac{7.6}{10}$	$\frac{8.9}{22}$	$\frac{11.0}{50}$	
$\frac{4.5}{50}$	$\frac{3.3}{26 Fc}$	$\frac{6.3}{21}$	$\frac{7.3}{12}$	6.9	$\frac{7.0}{12}$	$\frac{6.0}{17}$	$\frac{6.9}{21}$	$\frac{8.1}{50}$

Top of Fence Post 17' Rt of 14.5 + 8.5

$\frac{4.4}{50}$	$\frac{4.7}{30}$	$\frac{4.0}{22}$	$\frac{5.1}{12}$	4.5	$\frac{5.0}{12}$	$\frac{4.7}{20 Fc}$	$\frac{5.1}{50}$	
$\frac{7.0}{50}$	$\frac{7.7}{33}$	$\frac{7.2}{25}$	$\frac{7.5}{18}$	5.3	$\frac{5.6}{8}$	$\frac{5.1}{19 Fc}$	$\frac{5.1}{50}$	
$\frac{7.3}{50}$	$\frac{7.4}{30}$	$\frac{6.8}{26}$	$\frac{7.0}{17}$	$\frac{6.0}{13}$	5.4	$\frac{6.0}{10}$	$\frac{5.3}{19}$	$\frac{4.4}{50}$
$\frac{7.0}{50}$	$\frac{7.4}{31}$	$\frac{7.0}{27}$	$\frac{7.9}{21}$	$\frac{6.7}{13}$	6.1	$\frac{6.6}{7}$	$\frac{7.1}{19}$	$\frac{5.9}{50}$
$\frac{6.8}{50}$	$\frac{6.9}{26 Fc}$	$\frac{7.6}{19}$	$\frac{6.8}{13}$	6.4	$\frac{7.0}{9}$	$\frac{8.8}{16}$	$\frac{9.0}{24}$	$\frac{8.5}{50}$

		913.76			
	+	912.86	-	Elev ¹	
Bm	3.08	916.04	0.80	912.96	912.06
148+50		915.14		06.8	
149				07.4	
+50				08.4	
150				09.4	
+50				10.0	
151				10.9	
+50				11.9	
152				12.3	
+50				12.5	
153		12.99		12.2	
Bm	0.93	913.89	3.08	912.96	912.06
T.P.	0.01	901.33	12.57	904.32	900.42
Bm		900.43	9.33	892.00	891.10

L+

E

13

Begin 9/4/36

Quit 9/3/36

B.m. on Stone Mon.

153+14.1

$\frac{8.0}{50}$	$\frac{8.5}{26}$	$\frac{9.4}{19}$	$\frac{8.9}{14}$	8.3
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$\frac{9.0}{8}$	$\frac{9.2}{10}$	$\frac{11.2}{15}$	$\frac{11.6}{18_{Fe}}$	$\frac{12.6}{50}$
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$\frac{6.9}{50}$	$\frac{7.4}{26}$	$\frac{8.6}{19}$	$\frac{8.1}{13}$	7.7
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$\frac{8.1}{9}$	$\frac{9.8}{12}$	$\frac{10.2}{17_{Fe}}$	$\frac{11.9}{50}$
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$\frac{5.6}{50}$	$\frac{6.2}{25}$	$\frac{7.5}{18}$	$\frac{7.2}{13}$	6.7
------------------	------------------	------------------	------------------	-----

$\frac{7.4}{9}$	$\frac{8.7}{13}$	$\frac{8.7}{16}$	$\frac{10.4}{50}$
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$\frac{4.5}{50}$	$\frac{5.1}{26}$	$\frac{6.1}{20}$	$\frac{6.3}{15}$	5.7
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$\frac{6.4}{9}$	$\frac{7.3}{15}$	$\frac{9.3}{50}$
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$\frac{3.8}{50}$	$\frac{4.1}{27}$	$\frac{5.3}{17}$	$\frac{5.3}{13}$	5.1
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$\frac{5.9}{9}$	$\frac{7.1}{16}$	$\frac{9.6}{50}$
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$\frac{3.2}{50}$	$\frac{3.6}{27}$	$\frac{4.6}{18}$	$\frac{4.5}{13}$	4.2
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$\frac{5.0}{10}$	$\frac{6.3}{16_{Fe}}$	$\frac{9.2}{50}$
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$\frac{2.3}{50}$	$\frac{2.2}{22}$	$\frac{3.5}{15}$	3.2
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$\frac{4.0}{8}$	$\frac{4.1}{15}$	$\frac{6.6}{50}$
-----------------	------------------	------------------

$\frac{1.9}{50}$	$\frac{1.8}{26}$	$\frac{3.0}{16}$	2.8
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$\frac{3.2}{9}$	$\frac{2.3}{13}$	$\frac{2.3}{20}$	$\frac{4.3}{50}$
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$\frac{3.0}{50}$	$\frac{2.6}{24}$	$\frac{3.3}{14}$	2.6
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$\frac{2.7}{10}$	$\frac{2.2}{20}$	$\frac{3.3}{50}$
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$\frac{3.1}{50}$	$\frac{3.1}{25}$	$\frac{3.7}{19}$	2.9
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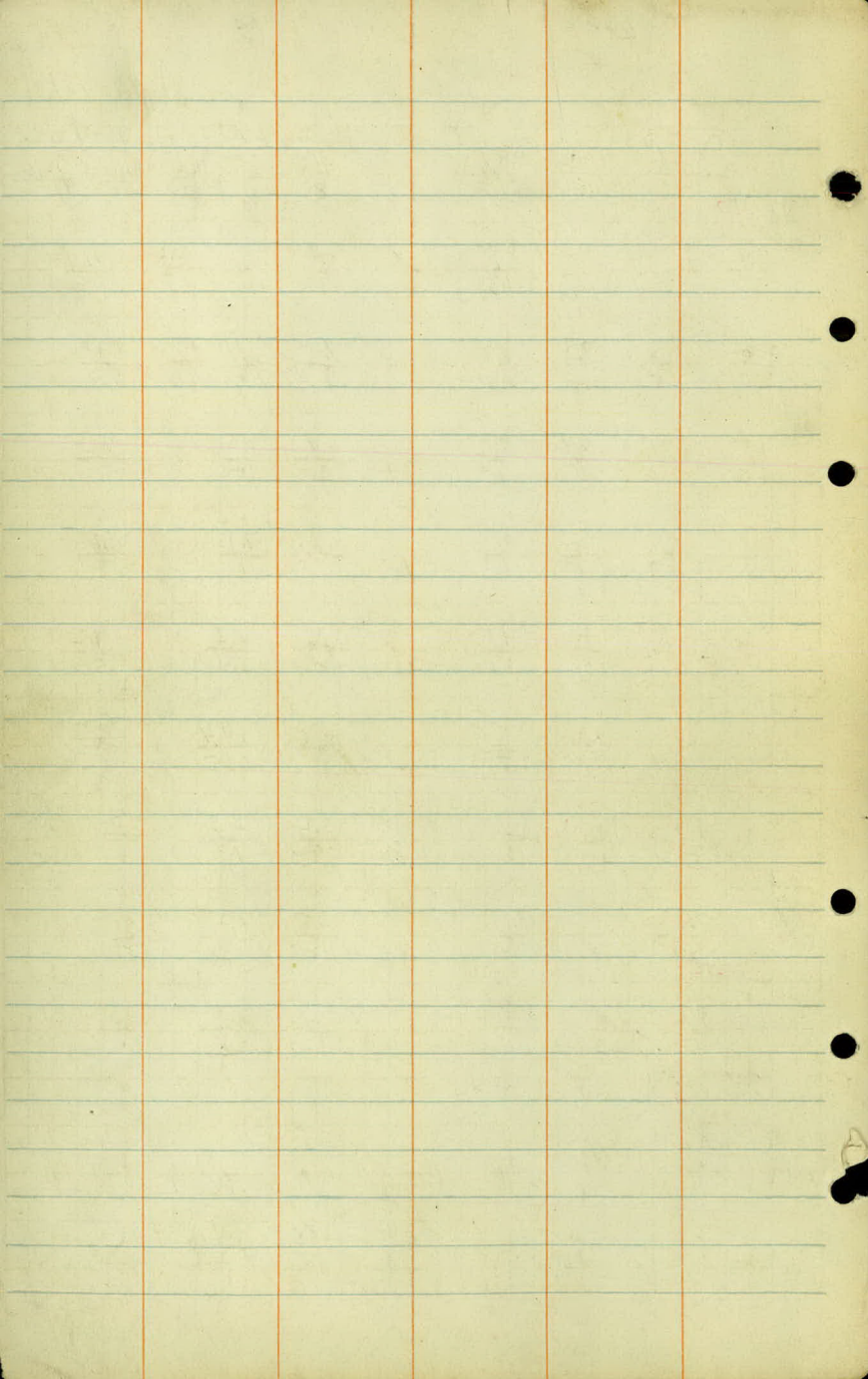
$\frac{3.4}{12}$	$\frac{2.3}{20}$	$\frac{2.3}{50}$
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Stone Mon. 153+14.1

□ mark in road

R.R. Spike in 18" Box elder

30' N & 60' W of E of
Lexington Ave



Prolim X Soc
H. Co. Line

Sta	+	π	-	Elev
T.P. ¹⁵	5.97	913.95		907.98
154				911.8.
155				09.2.
156				06.9.
T.P.	225	905.59	10.61	903.34.
157				902.5.
158				896.8.
T.P.	0.75	895.29	11.05	894.54.
159				891.8.
B.M.			411	891.18.
150				889.6.
160			$\angle$ Lex	88.4.
+07				88.3.
+14				87.9.
+50				87.3.
B.M.	0.60	891.77		891.17
161				86.9.

Lt # Pt

$$\frac{2.2}{100} \frac{2.2}{50} \frac{2.2}{23} \frac{2.7}{17} 2.2 \frac{2.6}{11} \frac{1.9}{13} \frac{1.9}{50} \frac{1.4}{100}$$

$$\frac{4.3}{100} \frac{4.5}{50} \frac{4.1}{29} \frac{5.3}{26} \frac{5.3}{24} \frac{4.7}{20} \frac{4.5}{5} 4.8 \frac{4.8}{8} \frac{6.1}{13} \frac{5.0}{18} \frac{4.8}{50} \frac{6.3}{100}$$

$$\frac{8.0}{100} \frac{7.6}{50} \frac{7.1}{41} \frac{7.1}{30} \frac{9.4}{26} \frac{9.4}{23} \frac{7.4}{19} \frac{6.6}{8} 7.1 \frac{7.5}{7} \frac{8.7}{12} \frac{9.1}{17} \frac{6.5}{19} \frac{8.1}{50} \frac{10.4}{100}$$

$$\frac{5.0}{50} \frac{4.0}{42} \frac{3.0}{32} \frac{4.3}{30} \frac{4.8}{25} \frac{4.8}{25} \frac{3.7}{21} \frac{2.7}{10} 3.1 \frac{3.2}{4} \frac{4.4}{9} \frac{5.0}{11} \frac{4.8}{15} \frac{4.7}{19} \frac{1.1}{50} \frac{3.1}{100}$$

$$\frac{7.0}{100}$$

$$\frac{9.0}{100} \frac{11.2}{65} \frac{9.7}{50} \frac{8.6}{35} \frac{9.7}{30} \frac{9.7}{26} \frac{8.6}{22} \frac{8.2}{12} 8.8 \frac{8.8}{3} \frac{9.8}{6} \frac{9.9}{12} \frac{5.6}{16} \frac{4.1}{50} \frac{3.6}{100}$$

$$\frac{1.0}{100} \frac{3.0}{50} \frac{3.9}{47} \frac{3.5}{29} \frac{3.2}{24} \frac{2.7}{13} 3.5 \frac{3.5}{3} \frac{4.0}{6} \frac{4.4}{12} \frac{3.0}{14} \frac{2.5}{50} \frac{2.5}{100}$$

$$159 + 36 \quad Lt \ 40'$$

$$\frac{5.1}{100} \frac{6.1}{50} \frac{6.2}{41} \frac{5.2}{11} 5.7 \frac{6.4}{14} \frac{6.7}{21} \frac{6.1}{22} \frac{6.5}{50} \frac{5.5}{50}$$

$$\frac{7.9}{100} \frac{8.0}{50} \frac{8.2}{45} \frac{7.7}{40} \frac{6.8}{20} 6.9 \frac{7.8}{50} \frac{8.3}{100}$$

$$\frac{9.3}{100} \frac{9.3}{50} \frac{7.8}{45} \frac{7.1}{29} 7.0 \frac{8.4}{50} \frac{9.0}{100}$$

$$\frac{9.3}{100} \frac{8.3}{50} \frac{7.8}{48} \frac{7.1}{22} 7.4 \frac{8.3}{28} \frac{10.5}{40} \frac{10.8}{100}$$

$$\frac{9.6}{120} \frac{9.6}{100} \frac{8.2}{90} \frac{8.6}{50} \frac{11.1}{35} \frac{10.5}{22} \frac{8.5}{16} 8.0 \frac{8.4}{14} \frac{11.1}{20} \frac{11.6}{50} \frac{11.6}{100}$$

$$891.17$$

$$18^\circ \text{ B.E. } 40' Lt \ 54 \ 159 + 36$$

$$\frac{7.4}{100} \frac{7.4}{50} \frac{7.1}{19} \frac{5.5}{14} 4.9 \frac{5.4}{14} \frac{8.0}{20} \frac{8.4}{50} \frac{8.4}{100}$$

Sta	+	+	-	Elev
		891.77		
162				85.5
163				84.8
164				83.3
+50				82.9
165				82.6
T.P	5.38	887.89	9.26	882.51
+16		18" C.M.P X Drain		
+50				82.6
166				82.5
167				82.8
168				82.9
169				83.0
170				83.0

Rice Creek
2' Water Running
on Rt 1' At

LX

Z

PX

$$\frac{9.0}{100} \frac{9.0}{50} \frac{8.9}{22} \frac{8.2}{17} \frac{6.5}{12} 6.3 \quad \frac{6.6}{15} \frac{8.6}{19} \frac{8.9}{23} \frac{9.2}{50} \frac{7.2}{100}$$

$$\frac{9.0}{100} \frac{9.0}{50} \frac{8.7}{21} \frac{8.4}{17} \frac{7.0}{13} 7.0 \quad \frac{7.1}{13} \frac{8.5}{16} \frac{8.5}{50} \frac{8.9}{100}$$

$$\frac{10.2}{100} \frac{10.2}{50} \frac{10.3}{19} \frac{10.0}{15} \frac{8.6}{12} 8.5 \quad \frac{8.9}{14} \frac{10.0}{17} \frac{11.1}{50} \frac{12.1}{100}$$

$$\frac{10.4}{100} \frac{10.4}{50} \frac{11.4}{19} \frac{9.1}{12} 8.9 \quad \frac{9.1}{12} \frac{11.6}{19} \frac{12.1}{34} \frac{12.0}{50} \frac{12.0}{100}$$

$$\frac{11.1}{100} \frac{11.6}{50} \frac{12.3}{34} \frac{12.3}{22} \frac{10.6}{17} \frac{9.3}{12} 9.2 \quad \frac{9.7}{14} \frac{14.0}{22} \frac{14.1}{32} \frac{12.1}{33} \frac{12.1}{50} \frac{12.1}{100}$$

$$\frac{10.2}{\text{Inv.}}$$

$$\frac{10.8}{\text{Inv.}}$$

$$\frac{878.81}{9.08}$$

Elev Water

$$\frac{7.4}{100} \frac{7.8}{28} \frac{9.2}{65} \frac{10.1}{40} \frac{9.1}{35} \frac{7.6}{19} \frac{5.3}{14} 5.3 \quad \frac{5.7}{17} \frac{8.0}{22} \frac{11.9}{23} \frac{11.8}{34} \frac{9.7}{35} \frac{7.7}{50} \frac{7.7}{100}$$

Ditch

$$\frac{8.1}{100} \frac{9.1}{90} \frac{9.7}{75} \frac{9.7}{65} \frac{8.7}{55} \frac{7.3}{36} \frac{7.6}{18} \frac{5.2}{12} 5.4 \quad \frac{6.1}{19} \frac{8.0}{22} \frac{10.3}{24} \frac{11.3}{28} \frac{10.2}{32} \frac{7.7}{35} \frac{7.7}{50} \frac{7.7}{100}$$

$$\frac{8.0}{100} \frac{8.0}{75} \frac{8.6}{70} \frac{10.0}{60} \frac{10.0}{45} \frac{8.7}{43} \frac{7.6}{20} \frac{5.3}{15} 5.1 \quad \frac{5.4}{16} \frac{8.0}{22} \frac{10.1}{23} \frac{11.3}{29} \frac{10.1}{35} \frac{7.8}{36} \frac{7.4}{50} \frac{7.4}{100}$$

Rice Break

$$\frac{7.2}{100} \frac{7.2}{50} \frac{7.2}{48} \frac{9.2}{45} \frac{10.1}{35} \frac{9.1}{25} \frac{7.7}{19} \frac{5.0}{13} 5.0 \quad \frac{5.2}{14} \frac{6.9}{19} \frac{9.1}{19} \frac{13.1}{24} \frac{13.1}{34} \frac{6.9}{34} \frac{6.9}{50} \frac{6.9}{100}$$

$$\frac{7.1}{100} \frac{6.9}{48} \frac{8.4}{36} \frac{8.8}{27} \frac{8.1}{20} \frac{6.0}{14} \frac{5.2}{11} 4.9 \quad \frac{5.4}{14} \frac{7.6}{18} \frac{9.2}{19} \frac{13.2}{23} \frac{13.2}{38} \frac{7.5}{42} \frac{6.5}{50} \frac{6.5}{100}$$

$$\frac{7.0}{100} \frac{6.5}{50} \frac{7.4}{31} \frac{7.5}{19} \frac{5.1}{14} 4.9 \quad \frac{5.3}{14} \frac{8.2}{19} \frac{8.8}{23} \frac{10.0}{25} \frac{10.0}{40} \frac{8.7}{42} \frac{7.7}{50}$$

$$\frac{6.2}{100}$$

Sta	+	π	-	Elev
		887.89		
171				83.0
T.P	4.97	887.99	4.87	883.02
+50				83.0
172				83.0
173				83.2
+50				83.2
+56				83.1
+72				83.1
+85				83.0
174				83.1
175				83.2
176				83.3
+50				83.3

Lt ~~E~~ Rk

$$\frac{6.3}{100} \frac{6.8}{50} \frac{7.4}{37} \frac{8.2}{32} \frac{8.7}{20} \frac{6.0}{15} \frac{5.2}{12} 49 \frac{5.3}{13} \frac{6.0}{16} \frac{7.8}{23} \frac{10.6}{24} \frac{10.6}{34} \frac{7.8}{36} \frac{6.8}{50} \frac{5.2}{100}$$

$$\frac{6.8}{100} \frac{7.8}{50} \frac{8.4}{41} \frac{10.0}{36} \frac{10.0}{25} \frac{8.8}{23} \frac{6.8}{18} \frac{5.3}{12} 5.0 \frac{5.4}{12} \frac{6.5}{16} \frac{7.6}{22} \frac{10.3}{24} \frac{10.3}{31} \frac{7.6}{33} \frac{7.1}{50} \frac{5.5}{100}$$

$$\frac{7.7}{100} \frac{7.7}{68} \frac{10.7}{63} \frac{10.7}{44} \frac{9.2}{38} \frac{7.6}{24} \frac{6.0}{18} \frac{5.4}{12} 5.0 \frac{5.3}{13} \frac{6.6}{17} \frac{7.9}{22} \frac{10.7}{24} \frac{10.7}{32} \frac{8.0}{34} \frac{8.0}{50} \frac{7.0}{100}$$

$$\frac{7.3}{120} \frac{9.9}{120} \frac{9.9}{100} \frac{8.9}{90} \frac{7.3}{65} \frac{7.3}{50} \frac{7.3}{23} \frac{6.8}{19} \frac{5.3}{13} 48 \frac{5.4}{14} \frac{7.6}{21} \frac{11.1}{23} \frac{11.1}{32} \frac{7.6}{33} \frac{7.6}{50} \frac{6.6}{100}$$

$$\frac{7.3}{120} \frac{7.3}{120} \frac{9.9}{100} \frac{9.9}{90} \frac{8.9}{65} \frac{7.3}{50} \frac{7.3}{23} \frac{6.8}{19} \frac{5.3}{13} 48 \frac{5.4}{14} \frac{7.6}{21} \frac{11.1}{23} \frac{11.1}{32} \frac{7.6}{33} \frac{7.6}{50} \frac{6.6}{100}$$

$$\frac{7.7}{125} \frac{7.7}{100} \frac{10.7}{75} \frac{10.7}{36} \frac{9.2}{26} \frac{7.6}{19} \frac{5.2}{11} 49 \frac{5.2}{14} \frac{7.3}{20} \frac{9.2}{24} \frac{10.7}{34} \frac{10.5}{100}$$

$$\frac{7.7}{120} \frac{7.7}{100} \frac{10.7}{75} \frac{10.7}{36} \frac{8.7}{26} \frac{7.6}{19} \frac{5.2}{11} 49 \frac{5.2}{14} \frac{7.3}{20} \frac{9.2}{24} \frac{10.7}{34} \frac{10.5}{100}$$

$$\frac{6.4}{100} \frac{7.4}{75} \frac{9.4}{65} \frac{9.4}{50} \frac{8.3}{26} \frac{7.4}{21} \frac{5.4}{14} 5.0 \frac{5.5}{13} \frac{7.4}{21} \frac{7.9}{50} \frac{7.9}{100}$$

$$\frac{6.4}{100} \frac{7.4}{75} \frac{9.4}{65} \frac{9.4}{50} \frac{8.3}{26} \frac{7.4}{21} \frac{5.4}{14} 49 \frac{5.5}{13} \frac{7.6}{21} \frac{7.9}{50} \frac{7.9}{100}$$

$$\frac{7.9}{100} \frac{7.4}{50} \frac{7.7}{25} \frac{7.4}{21} \frac{5.1}{13} 48 \frac{5.0}{14} \frac{6.8}{19} \frac{7.3}{27} \frac{6.9}{50} \frac{6.9}{100}$$

$$\frac{6.6}{100} \frac{6.6}{50} \frac{6.9}{19} \frac{5.2}{13} 47 \frac{5.2}{13} \frac{6.7}{19} \frac{7.1}{27} \frac{7.4}{50} \frac{7.4}{100}$$

$$\frac{7.7}{100} \frac{7.7}{50} \frac{7.7}{27} \frac{6.8}{19} \frac{5.1}{13} 47 \frac{5.2}{14} \frac{7.5}{20} \frac{8.3}{50} \frac{9.7}{55} \frac{9.7}{65} \frac{8.9}{67} \frac{8.4}{80} \frac{8.4}{100}$$

Sta	+	π	-	Elev
		887.99		
176+97		E of 3-48" C.M.P.		
177				83.0
+50				83.5
T.P.	9.81	893.28	4.52	883.47
178				83.8
179				83.8
+52				83.9
180				84.0
+50				84.1
181				84.1
+50				84.3
182				84.4
183				84.3
B.M.			1.49	891.79

Lt ✕ Rt

$\frac{9.84}{100}$
Inv

$\frac{10.38}{100}$
Inv

$\frac{5.8}{100} \frac{6.8}{45} \frac{9.8}{40} \frac{9.8}{22} \frac{9.2}{17} \frac{4.8}{11} 5.0$ $\frac{5.2}{13} \frac{10.4}{20} \frac{10.4}{50} \frac{9.4}{55} \frac{9.4}{80} \frac{7.4}{93} \frac{7.4}{100}$

$\frac{2.1}{105} \frac{9.1}{100} \frac{9.1}{80} \frac{7.1}{80} \frac{6.7}{50} \frac{6.1}{19} \frac{4.7}{13} 4.5$ $\frac{4.7}{14} \frac{5.9}{19} \frac{6.7}{30} \frac{6.7}{50} \frac{6.7}{100}$

Nail F.P. 33' Rt Sta 178 + 67

$\frac{11.5}{100} \frac{11.4}{50} \frac{11.5}{31} \frac{10.8}{17} \frac{9.8}{15} 9.5$ $\frac{9.7}{14} \frac{10.8}{17} \frac{11.3}{22} \frac{11.6}{50} \frac{11.7}{100}$

$\frac{11.5}{100} \frac{11.5}{50} \frac{10.8}{17} \frac{9.7}{13} 9.5$ $\frac{9.4}{13} \frac{10.6}{17} \frac{11.0}{24} \frac{11.0}{35} \frac{10.0}{50} \frac{9.0}{100}$

$\frac{12.9}{100} \frac{11.6}{50} \frac{11.0}{23} \frac{10.5}{17} \frac{9.5}{13} 9.4$ $\frac{9.5}{14} \frac{10.7}{18} \frac{10.7}{22} \frac{9.8}{23} \frac{8.5}{50} \frac{5.1}{100}$

$\frac{12.4}{100} \frac{12.4}{50} \frac{12.7}{45} \frac{12.0}{24} \frac{10.9}{17} \frac{9.6}{14} 9.3$ $\frac{9.4}{13} \frac{10.8}{15} \frac{10.7}{22} \frac{7.8}{25} \frac{6.1}{28} \frac{6.2}{50} \frac{4.1}{100}$

$\frac{12.0}{100} \frac{12.0}{50} \frac{12.6}{36} \frac{13.3}{26} \frac{12.9}{21} \frac{9.8}{13} 9.2$ $\frac{9.3}{13} \frac{10.4}{15} \frac{11.0}{20} \frac{10.2}{23} \frac{4.1}{32} \frac{4.0}{50} \frac{3.0}{100}$

$\frac{12.8}{100} \frac{12.4}{50} \frac{12.0}{27} \frac{11.0}{17} \frac{9.7}{13} 9.2$ $\frac{9.3}{12} \frac{10.7}{16} \frac{10.7}{23} \frac{4.7}{31} \frac{4.0}{50} \frac{3.0}{100}$

$\frac{11.5}{100} \frac{10.9}{50} \frac{9.8}{25} \frac{10.8}{22} \frac{10.9}{16} \frac{9.5}{13} 9.0$ $\frac{9.1}{13} \frac{10.1}{16} \frac{10.1}{24} \frac{6.2}{29} \frac{4.6}{50} \frac{3.1}{100}$

$\frac{11.0}{100} \frac{10.5}{48} \frac{8.8}{26} \frac{10.5}{24} \frac{10.7}{15} \frac{9.2}{13} 8.9$ $\frac{9.1}{13} \frac{10.6}{16} \frac{10.4}{28} \frac{7.5}{28} \frac{5.1}{31} \frac{4.2}{50} \frac{3.2}{100}$

$\frac{10.5}{100} \frac{7.7}{50} \frac{5.4}{29} \frac{10.2}{28} \frac{10.2}{16} \frac{9.3}{13} 9.0$ $\frac{9.1}{13} \frac{9.9}{15} \frac{10.1}{24} \frac{9.3}{29} \frac{2.3}{33} \frac{2.2}{50} \frac{3.7}{100}$

892.09

U.S.G.S 33 Rt Sta 183 + 36

Sta	+	π	-	Elev
		893.28		
184				84.5
T.P	3.96	889.25	7.99	885.29
185				84.7
186				83.8
+42		? X 24" C.M.P. X DRAIN		
187				84.0
188				84.2
189				83.9
190				84.1
191				84.6
192				84.6
T.P	8.87	893.67	4.45	884.80
+50				84.7
193				84.8

At X Pt

$\frac{7.1}{100} \frac{5.1}{50} \frac{4.0}{32} \frac{10.1}{28} \frac{10.5}{21} \frac{10.4}{16} \frac{9.0}{12} 8.8 \frac{9.1}{13} \frac{9.7}{19} \frac{9.4}{28} \frac{3.2}{32} \frac{3.6}{50} \frac{5.1}{100}$

885.29 Pole 25' Lt Sta 185 + 25'

$\frac{4.6}{100} \frac{7.6}{75} \frac{3.6}{50} \frac{3.8}{25} \frac{6.3}{23} \frac{6.3}{15} \frac{5.1}{12} 4.6 \frac{5.0}{12} \frac{6.2}{16} \frac{6.3}{21} \frac{5.2}{26} \frac{5.6}{50} \frac{5.6}{100}$

$\frac{6.4}{100} \frac{7.4}{50} \frac{7.9}{25} \frac{7.2}{19} \frac{5.7}{14} 5.5 \frac{6.2}{15} \frac{8.1}{20} \frac{8.0}{50} \frac{8.0}{100}$

$\frac{8.62}{Inv}$

$\frac{8.62}{Inv}$

See Const Notes 1934

$\frac{8.0}{100} \frac{8.1}{50} \frac{7.9}{23} \frac{6.9}{18} \frac{5.6}{14} 5.3 \frac{5.7}{13} \frac{7.4}{20} \frac{7.5}{25} \frac{8.0}{26} \frac{8.2}{29} \frac{7.4}{31} \frac{7.3}{50} \frac{6.8}{100}$

$\frac{7.5}{100} \frac{7.5}{50} \frac{7.1}{23} \frac{6.6}{20} \frac{5.2}{14} 5.1 \frac{5.0}{13} \frac{6.5}{20} \frac{6.8}{25} \frac{7.6}{26} \frac{7.7}{30} \frac{6.8}{32} \frac{6.4}{50} \frac{6.3}{100}$

$\frac{7.4}{100} \frac{7.5}{50} \frac{7.6}{20} \frac{5.7}{14} 5.4 \frac{5.6}{13} \frac{7.4}{19} \frac{7.7}{28} \frac{7.5}{50} \frac{6.5}{100}$

$\frac{7.1}{100} \frac{7.6}{50} \frac{7.5}{22} \frac{7.0}{18} \frac{5.4}{14} 5.2 \frac{5.0}{13} \frac{7.6}{19} \frac{7.7}{24} \frac{7.3}{25} \frac{6.6}{50} \frac{4.6}{100}$

$\frac{4.8}{100} \frac{4.8}{50} \frac{6.0}{23} \frac{6.4}{18} \frac{4.8}{15} 4.7 \frac{4.8}{14} \frac{7.0}{18} \frac{7.3}{23} \frac{6.7}{25} \frac{6.6}{50} \frac{4.0}{100}$

$\frac{8.7}{100} \frac{1.7}{50} \frac{3.7}{25} \frac{6.1}{21} \frac{6.2}{17} \frac{4.7}{14} 4.7 \frac{4.7}{14} \frac{7.4}{19} \frac{7.4}{23} \frac{5.2}{27} \frac{6.1}{50} \frac{5.1}{100}$

$\frac{4.3}{100} \frac{6.0}{50} \frac{7.3}{27} \frac{10.4}{24} \frac{10.4}{18} \frac{9.1}{14} 9.0 \frac{9.1}{13} \frac{11.3}{17} \frac{11.5}{23} \frac{8.6}{27} \frac{9.4}{35} \frac{10.0}{50} \frac{10.0}{100}$

$\frac{3.7}{100} \frac{4.6}{50} \frac{6.5}{28} \frac{10.5}{21} \frac{10.4}{17} \frac{9.1}{13} 8.9 \frac{9.1}{13} \frac{11.6}{19} \frac{11.7}{23} \frac{9.7}{26} \frac{10.1}{36} \frac{10.6}{50} \frac{10.6}{100}$

Sta.	+	π	-	Elev
		893.67		
194				84.7
+50				84.6
195				84.5
+50				84.5
196				84.6
T.P	6.78	893.89	6.56	887.11
+50				84.2
197				83.4
+52		PX 24" CMP		
198				83.2
199				84.6
+40				85.2
200				85.5
+75				85.9

LT

Z

RT

$\frac{0.3}{100}$	$\frac{1.8}{50}$	$\frac{3.1}{33}$	$\frac{10.6}{22}$	$\frac{10.6}{18}$	$\frac{9.2}{13}$	9.0	$\frac{9.1}{13}$	$\frac{11.0}{16}$	$\frac{11.0}{21}$	$\frac{9.0}{22}$	$\frac{9.7}{37}$	$\frac{10.3}{50}$	$\frac{10.3}{100}$
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$\frac{11.6}{100}$	$\frac{6.4}{50}$	$\frac{1.7}{34}$	$\frac{7.0}{28}$	$\frac{10.5}{22}$	$\frac{10.5}{18}$	$\frac{9.2}{13}$	9.1	$\frac{9.6}{13}$	$\frac{10.7}{17}$	$\frac{10.8}{21}$	$\frac{7.6}{26}$	$\frac{8.3}{36}$	$\frac{8.7}{50}$	$\frac{7.7}{100}$
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$\frac{13.1}{100}$	$\frac{11.5}{50}$	$\frac{0.2}{35}$	$\frac{6.1}{30}$	$\frac{7.5}{26}$	$\frac{9.9}{21}$	$\frac{9.4}{12}$	9.2	$\frac{9.5}{13}$	$\frac{11.0}{17}$	$\frac{11.0}{21}$	$\frac{4.6}{31}$	$\frac{5.4}{38}$	$\frac{6.4}{50}$	$\frac{8.5}{100}$
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$\frac{0.0}{100}$	$\frac{1.4}{42}$	$\frac{2.4}{32}$	$\frac{7.2}{28}$	$\frac{9.7}{22}$	$\frac{10.1}{17}$	$\frac{9.4}{14}$	9.2	$\frac{9.2}{13}$	$\frac{11.0}{17}$	$\frac{11.1}{21}$	$\frac{4.6}{32}$	$\frac{5.1}{50}$	$\frac{3.4}{100}$
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$\frac{8.1}{100}$	$\frac{8.1}{50}$	$\frac{8.1}{27}$	$\frac{10.7}{22}$	$\frac{10.7}{17}$	$\frac{9.3}{13}$	9.1	$\frac{9.2}{14}$	$\frac{10.8}{17}$	$\frac{10.8}{22}$	$\frac{9.4}{26}$	$\frac{9.5}{36}$	$\frac{9.5}{50}$	$\frac{9.5}{100}$
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887.11 F.P. 33' RT 549 199+51

$\frac{10.8}{100}$	$\frac{10.8}{50}$	$\frac{10.8}{38}$	$\frac{10.8}{23}$	$\frac{11.4}{21}$	$\frac{11.6}{17}$	$\frac{9.8}{14}$	9.7	$\frac{9.8}{14}$	$\frac{11.4}{18}$	$\frac{11.4}{35}$	$\frac{11.4}{50}$	$\frac{10.5}{100}$
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$\frac{12.1}{100}$	$\frac{12.2}{50}$	$\frac{12.2}{17}$	$\frac{10.7}{13}$	10.5	$\frac{10.7}{11}$	$\frac{11.9}{15}$	$\frac{12.1}{26}$	$\frac{12.1}{50}$	$\frac{11.1}{100}$
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12.8
Inv12.74
Inv

$\frac{11.8}{100}$	$\frac{11.8}{50}$	$\frac{11.8}{29}$	$\frac{12.8}{18}$	$\frac{10.8}{14}$	10.7	$\frac{10.7}{13}$	$\frac{12.8}{17}$	$\frac{12.2}{23}$	$\frac{12.2}{50}$	$\frac{11.2}{100}$
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$\frac{10.8}{100}$	$\frac{10.8}{50}$	$\frac{10.8}{27}$	$\frac{11.0}{20}$	$\frac{11.0}{18}$	$\frac{9.4}{14}$	9.3	$\frac{9.3}{13}$	$\frac{11.0}{16}$	$\frac{11.0}{20}$	$\frac{9.6}{23}$	$\frac{9.5}{36}$	$\frac{9.5}{50}$	$\frac{9.5}{100}$
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$\frac{10.8}{100}$	$\frac{10.8}{50}$	$\frac{10.5}{22}$	$\frac{11.0}{20}$	$\frac{11.0}{18}$	$\frac{9.4}{14}$	8.7	$\frac{9.1}{13}$	$\frac{10.8}{17}$	$\frac{10.8}{20}$	$\frac{8.9}{23}$	$\frac{8.1}{36}$	$\frac{7.0}{50}$	$\frac{5.5}{100}$
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$\frac{9.2}{100}$	$\frac{9.2}{50}$	$\frac{8.4}{25}$	$\frac{10.3}{23}$	$\frac{10.1}{17}$	$\frac{8.5}{14}$	8.4	$\frac{8.6}{13}$	$\frac{10.7}{17}$	$\frac{10.0}{22}$	$\frac{3.8}{31}$	$\frac{3.6}{37}$	$\frac{2.6}{50}$	$\frac{2.6}{100}$
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$\frac{10.0}{100}$	$\frac{10.0}{50}$	$\frac{9.2}{23}$	$\frac{9.8}{21}$	$\frac{9.8}{17}$	$\frac{8.2}{13}$	8.0	$\frac{8.2}{14}$	$\frac{10.3}{17}$	$\frac{10.3}{22}$	$\frac{6.7}{27}$	$\frac{6.7}{36}$	$\frac{5.2}{50}$	$\frac{4.1}{100}$
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Sta	+	π	-	Elev
		892.89		
201				85.9
+55				85.5
202				86.0
+50				87.0
203				87.3
T.P	13.23	900.54	6.58	887.31
+70				87.7
204				88.0
BM			3.66	896.88
+50				88.0
205				88.0
+50				88.3
206				88.2
+25				87.9

LH * RT

$\frac{9.8}{100}$ $\frac{10.3}{50}$ $\frac{10.5}{35}$ $\frac{9.8}{18}$ $\frac{8.3}{13}$ 9.0 $\frac{8.2}{12}$ $\frac{10.0}{16}$ $\frac{10.1}{21}$ $\frac{8.8}{23}$ $\frac{8.8}{36}$ $\frac{7.8}{50}$ $\frac{7.8}{100}$

86.1

83.7

83.7

$\frac{10.6}{100}$ $\frac{10.6}{50}$ $\frac{10.6}{30}$ $\frac{10.6}{19}$ $\frac{8.7}{14}$ 8.4 $\frac{8.4}{14}$ $\frac{10.6}{19}$ $\frac{10.4}{24}$ $\frac{10.2}{37}$ $\frac{10.2}{50}$ $\frac{9.7}{100}$

84.3

$\frac{8.5}{100}$ $\frac{10.1}{50}$ $\frac{10.1}{29}$ $\frac{10.0}{19}$ $\frac{7.9}{14}$ 7.9 $\frac{8.0}{13}$ $\frac{9.8}{19}$ $\frac{9.6}{34}$ $\frac{7.6}{50}$ $\frac{8.0}{100}$

87.1

$\frac{8.3}{100}$ $\frac{9.4}{50}$ $\frac{9.5}{41}$ $\frac{9.2}{29}$ $\frac{8.6}{18}$ $\frac{7.5}{13}$ 6.9 $\frac{7.1}{14}$ $\frac{8.7}{17}$ $\frac{9.0}{21}$ $\frac{7.4}{25}$ $\frac{6.8}{38}$ $\frac{6.8}{50}$ $\frac{6.8}{75}$ $\frac{7.3}{100}$

90.8

$\frac{7.5}{100}$ $\frac{6.5}{50}$ $\frac{6.0}{29}$ $\frac{7.7}{27}$ $\frac{8.4}{21}$ $\frac{8.6}{18}$ $\frac{7.0}{14}$ 6.6 $\frac{6.8}{13}$ $\frac{8.5}{17}$ $\frac{8.5}{22}$ $\frac{3.3}{29}$ $\frac{3.0}{42}$ $\frac{3.1}{50}$ $\frac{6.1}{100}$

94.8

$\frac{12.8}{100}$ $\frac{9.9}{50}$ $\frac{7.9}{31}$ $\frac{10.4}{27}$ $\frac{13.8}{27}$ $\frac{14.4}{21}$ $\frac{14.4}{16}$ $\frac{13.3}{14}$ 12.8 $\frac{13.2}{13}$ $\frac{14.8}{16}$ $\frac{14.8}{21}$ $\frac{13.9}{24}$ $\frac{5.4}{36}$ $\frac{5.7}{45}$ $\frac{6.3}{70}$ $\frac{9.8}{100}$

96.3

$\frac{10.6}{100}$ $\frac{6.6}{50}$ $\frac{5.1}{35}$ $\frac{13.8}{25}$ $\frac{14.0}{17}$ $\frac{12.9}{13}$ 12.5 $\frac{12.9}{13}$ $\frac{14.4}{16}$ $\frac{14.4}{21}$ $\frac{13.5}{24}$ $\frac{4.0}{37}$ $\frac{4.2}{45}$ $\frac{6.2}{75}$ $\frac{9.2}{100}$

94.8

W-6 U.S.G. 5. 38' RT 549 204+03

$\frac{9.0}{100}$ $\frac{1.8}{50}$ $\frac{0.8}{42}$ $\frac{8.7}{34}$ $\frac{13.8}{29}$ $\frac{13.9}{17}$ $\frac{12.9}{13}$ 12.5 $\frac{12.8}{13}$ $\frac{14.0}{16}$ $\frac{14.0}{23}$ $\frac{11.4}{27}$ $\frac{3.7}{37}$ $\frac{5.7}{50}$ $\frac{10.4}{75}$ $\frac{14.0}{100}$

86.3

89.4

$\frac{6.7}{100}$ $\frac{5.0}{80}$ $\frac{1.8}{50}$ $\frac{1.6}{41}$ $\frac{10.3}{27}$ $\frac{12.8}{27}$ $\frac{13.4}{16}$ $\frac{12.4}{13}$ 12.5 $\frac{12.8}{13}$ $\frac{14.0}{16}$ $\frac{14.2}{23}$ $\frac{12.1}{24}$ $\frac{7.2}{32}$ $\frac{10.7}{50}$ $\frac{14.2}{70}$ $\frac{14.2}{100}$

95.8

$\frac{6.5}{100}$ $\frac{6.7}{50}$ $\frac{6.3}{33}$ $\frac{12.2}{24}$ $\frac{13.2}{19}$ $\frac{13.3}{16}$ $\frac{12.5}{12}$ 12.2 $\frac{12.4}{11}$ $\frac{12.9}{15}$ $\frac{14.0}{18}$ $\frac{14.0}{23}$ $\frac{12.2}{24}$ $\frac{14.7}{41}$ $\frac{14.7}{50}$ $\frac{14.7}{100}$

85.5

$\frac{12.1}{100}$ $\frac{11.7}{50}$ $\frac{11.6}{25}$ $\frac{13.2}{21}$ $\frac{13.2}{16}$ $\frac{12.4}{11}$ 12.3 $\frac{12.7}{19}$ $\frac{14.2}{17}$ $\frac{15.0}{30}$ $\frac{15.0}{50}$ $\frac{15.0}{100}$

85.7

$\frac{14.7}{100}$ $\frac{14.9}{50}$ $\frac{14.9}{21}$ $\frac{13.6}{13}$ 12.6 $\frac{12.8}{14}$ $\frac{14.8}{21}$ $\frac{14.8}{50}$ $\frac{14.8}{100}$

Sta	+	π	-	Elev
		900.54		
207				87.4
208				86.4
+43			PX 24" C.M.P.	
209				87.1
210				88.2
T.P	7.43	895.67	12.30	888.24.
211				88.1
+50				88.9
212				88.9
213				88.3
+50				88.7
214				90.5
+70				92.4
215				92.7
T.P	11.58	906.14	1.11	894.56.

LT $\neq$ RT 84.9

$$\frac{15.8}{100} \frac{15.8}{50} \frac{15.8}{20} \frac{13.5}{14} 13.1 \frac{13.5}{10} \frac{15.2}{20} \frac{15.2}{50} \frac{15.2}{100}$$

84.7

$$\frac{12.4}{100} \frac{16.4}{50} \frac{16.4}{21} \frac{14.2}{15} 14.1 \frac{14.3}{15} \frac{15.8}{20} \frac{15.8}{50} \frac{15.8}{100}$$

85.0

$$\frac{14.7}{Inv.} \frac{16.7}{Inv.} \frac{15.7}{100} \frac{16.7}{21} \frac{13.2}{13} 13.4 \frac{13.4}{15} \frac{15.5}{20} \frac{15.5}{50} \frac{15.5}{100}$$

86.1

$$\frac{14.4}{100} \frac{14.4}{50} \frac{14.4}{19} \frac{12.5}{13} 12.3 \frac{12.6}{14} \frac{14.4}{19} \frac{14.4}{50} \frac{14.4}{100}$$

$$\frac{9.1}{100} \frac{9.1}{50} \frac{9.1}{18} \frac{7.6}{13} 7.6 \frac{9.1}{14} \frac{9.7}{18} \frac{9.7}{50} \frac{9.7}{100}$$

$$\frac{7.1}{100} \frac{7.1}{50} \frac{7.1}{26} \frac{9.0}{21} \frac{9.0}{17} \frac{7.2}{13} 6.8 \frac{7.2}{13} \frac{9.0}{16} \frac{8.6}{22} \frac{9.8}{26} \frac{9.8}{30} \frac{8.6}{32} \frac{8.6}{50} \frac{8.6}{100}$$

$$\frac{9.0}{100} \frac{9.0}{50} \frac{9.0}{26} \frac{8.5}{17} \frac{7.3}{13} 6.8 \frac{7.0}{13} \frac{8.0}{17} \frac{8.1}{23} \frac{9.3}{25} \frac{9.4}{29} \frac{6.7}{33} \frac{6.7}{50} \frac{7.7}{100}$$

$$\frac{11.7}{100} \frac{11.7}{50} \frac{11.7}{26} \frac{11.3}{21} \frac{7.8}{14} 7.4 \frac{7.4}{14} \frac{9.1}{19} \frac{9.4}{24} \frac{9.9}{27} \frac{9.9}{30} \frac{9.4}{31} \frac{9.0}{50} \frac{9.0}{100}$$

$$\frac{11.5}{100} \frac{11.5}{50} \frac{11.0}{28} \frac{10.4}{20} \frac{7.2}{13} 7.0 \frac{7.0}{14} \frac{9.7}{21} \frac{9.7}{50} \frac{9.7}{100}$$

$$\frac{9.5}{100} \frac{9.5}{50} \frac{9.2}{23} \frac{5.3}{14} 5.2 \frac{5.4}{14} \frac{8.9}{20} \frac{8.9}{50} \frac{8.9}{100}$$

$$\frac{3.5}{100} \frac{4.1}{50} \frac{4.6}{25} \frac{5.4}{23} \frac{5.3}{18} \frac{3.5}{14} 3.3 \frac{3.6}{14} \frac{5.2}{17} \frac{5.3}{21} \frac{4.2}{23} \frac{3.6}{50} \frac{3.1}{100}$$

$$\frac{0.5}{100} \frac{2.0}{50} \frac{2.1}{26} \frac{4.0}{21} \frac{4.4}{18} \frac{3.1}{14} 3.0 \frac{3.0}{13} \frac{4.3}{17} \frac{4.3}{21} \frac{1.6}{25} \frac{1.1}{50} \frac{40.5}{100}$$

Sta	+	π	-	Elev
		906.14		
215+00				93.4
B.M			7.23	898.91.
216				94.6
T.P	7.47	906.38		898.91
+50				95.8
217				96.8
+85				98.6
218				99.1
+50				00.1
219				01.2
220				02.9
221				04.3
T.P	6.05	910.30	2.13	904.25.
222				05.3
223				05.1

Lt Q R

$\frac{8.9}{100}$	$\frac{8.9}{50}$	$\frac{8.4}{30}$	$\frac{11.2}{27}$	$\frac{13.8}{20}$	$\frac{13.8}{17}$	$\frac{12.5}{12}$	$\frac{12.7}{12.7}$	$\frac{13.8}{13}$	$\frac{13.7}{10}$	$\frac{11.4}{20}$	$\frac{7.8}{27}$	$\frac{7.5}{31}$	$\frac{6.5}{50}$	$\frac{6.5}{100}$
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898.91 18' Oak 15' Lt 5' R 215' + 70'

$\frac{8.3}{57}$	$\frac{7.9}{30}$	$\frac{10.5}{26}$	$\frac{12.7}{21}$	$\frac{12.7}{17}$	$\frac{11.8}{13}$	$\frac{11.5}{11.5}$	$\frac{11.7}{13}$	$\frac{12.8}{17}$	$\frac{12.5}{23}$	$\frac{5.9}{32}$	$\frac{5.1}{50}$	$\frac{4.1}{100}$
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$\frac{8.0}{100}$	$\frac{9.1}{50}$	$\frac{9.0}{26}$	$\frac{12.1}{22}$	$\frac{12.1}{17}$	$\frac{10.8}{13}$	$\frac{10.6}{10.6}$	$\frac{10.7}{14}$	$\frac{11.6}{17}$	$\frac{10.8}{24}$	$\frac{6.5}{31}$	$\frac{5.7}{50}$	$\frac{4.7}{100}$
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$\frac{5.7}{100}$	$\frac{7.7}{50}$	$\frac{7.8}{27}$	$\frac{11.0}{22}$	$\frac{11.0}{17}$	$\frac{9.7}{13}$	$\frac{9.6}{9.6}$	$\frac{10.0}{14}$	$\frac{10.8}{17}$	$\frac{10.3}{23}$	$\frac{5.9}{29}$	$\frac{5.2}{50}$	$\frac{5.2}{100}$
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$\frac{4.6}{100}$	$\frac{4.6}{50}$	$\frac{4.7}{27}$	$\frac{8.8}{21}$	$\frac{9.3}{16}$	$\frac{8.1}{13}$	$\frac{7.8}{7.8}$	$\frac{8.1}{14}$	$\frac{9.2}{18}$	$\frac{9.0}{23}$	$\frac{4.8}{29}$	$\frac{4.8}{50}$	$\frac{4.8}{100}$
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$\frac{4.8}{100}$	$\frac{5.3}{50}$	$\frac{5.3}{27}$	$\frac{8.0}{23}$	$\frac{8.9}{19}$	$\frac{8.3}{14}$	$\frac{7.8}{12}$	$\frac{7.8}{7.8}$	$\frac{4.8}{14}$	$\frac{8.8}{18}$	$\frac{5.7}{23}$	$\frac{4.9}{28}$	$\frac{4.9}{50}$	$\frac{4.8}{100}$
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$\frac{6.3}{100}$	$\frac{7.3}{50}$	$\frac{7.0}{23}$	$\frac{7.9}{21}$	$\frac{8.0}{17}$	$\frac{6.4}{13}$	$\frac{6.3}{6.3}$	$\frac{6.4}{13}$	$\frac{7.6}{17}$	$\frac{7.6}{21}$	$\frac{6.1}{25}$	$\frac{5.6}{50}$	$\frac{5.1}{100}$
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$\frac{7.0}{100}$	$\frac{7.0}{50}$	$\frac{7.3}{27}$	$\frac{6.0}{16}$	$\frac{5.4}{13}$	$\frac{5.2}{5.2}$	$\frac{5.6}{13}$	$\frac{6.6}{17}$	$\frac{6.8}{22}$	$\frac{6.4}{24}$	$\frac{5.6}{50}$	$\frac{4.6}{100}$
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$\frac{4.9}{100}$	$\frac{5.4}{50}$	$\frac{5.3}{24}$	$\frac{4.9}{17}$	$\frac{3.7}{13}$	$\frac{3.5}{3.5}$	$\frac{3.6}{14}$	$\frac{4.2}{14}$	$\frac{4.7}{22}$	$\frac{4.1}{23}$	$\frac{3.8}{32}$	$\frac{3.5}{50}$	$\frac{1.0}{100}$
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$\frac{1.4}{100}$	$\frac{2.4}{50}$	$\frac{2.5}{24}$	$\frac{3.5}{21}$	$\frac{3.3}{17}$	$\frac{2.2}{14}$	$\frac{2.1}{2.1}$	$\frac{3.2}{12}$	$\frac{3.2}{17}$	$\frac{3.2}{22}$	$\frac{1.6}{25}$	$\frac{0.9}{50}$	$\frac{0.0}{100}$
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$\frac{2.8}{100}$	$\frac{2.8}{50}$	$\frac{2.7}{31}$	$\frac{6.3}{23}$	$\frac{6.2}{17}$	$\frac{5.1}{14}$	$\frac{5.0}{5.0}$	$\frac{5.4}{14}$	$\frac{6.8}{19}$	$\frac{6.5}{24}$	$\frac{1.8}{35}$	$\frac{2.0}{50}$	$\frac{2.0}{100}$
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$\frac{3.5}{100}$	$\frac{3.7}{50}$	$\frac{3.1}{35}$	$\frac{6.5}{25}$	$\frac{6.5}{18}$	$\frac{5.5}{13}$	$\frac{5.2}{5.2}$	$\frac{5.7}{14}$	$\frac{6.6}{19}$	$\frac{6.2}{26}$	$\frac{4.1}{34}$	$\frac{4.8}{50}$	$\frac{6.5}{100}$
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Sta	+	π	-	Elev
		910.30		
223 + 50				04.3
224				03.6
225				01.2
T.P	3.40	902.13	11.57	898.73
226				98.0
+70				95.7
227				94.9
+60				92.8
228				91.3
T.P	1.67	892.93	10.87	891.26
+50				90.2
229				89.1
230				87.9
B.M.			4.91	887.95
231				88.2

L+ R Pt

$$\frac{6.4}{100} \frac{5.4}{50} \frac{4.8}{35} \frac{7.3}{25} \frac{6.9}{18} \frac{6.1}{14} 60 \frac{6.0}{14} \frac{7.3}{19} \frac{7.3}{24} \frac{5.6}{32} \frac{4.1}{50} \frac{7.5}{100}$$

$$\frac{8.5}{100} \frac{8.5}{50} \frac{7.5}{33} \frac{8.2}{26} \frac{8.0}{19} \frac{6.9}{14} 67 \frac{6.8}{13} \frac{8.1}{18} \frac{8.2}{25} \frac{6.2}{32} \frac{6.6}{50} \frac{7.6}{100}$$

$$\frac{9.7}{100} \frac{9.7}{50} \frac{9.3}{34} \frac{10.5}{26} \frac{10.5}{19} \frac{9.3}{15} 9.1 \frac{9.1}{14} \frac{10.6}{19} \frac{10.5}{25} \frac{8.5}{31} \frac{9.2}{50} \frac{11.0}{100}$$

$$\frac{1.0}{100} \frac{0.4}{75} \frac{1.4}{50} \frac{1.8}{34} \frac{5.1}{25} \frac{5.3}{19} \frac{4.2}{14} 4.1 \frac{4.0}{14} \frac{5.3}{19} \frac{5.3}{27} \frac{4.1}{33} \frac{4.8}{50} \frac{7.0}{100}$$

$$\frac{0.2}{100} \frac{1.2}{50} \frac{1.8}{35} \frac{7.1}{24} \frac{7.3}{18} \frac{6.4}{14} 6.4 \frac{6.2}{14} \frac{7.5}{19} \frac{7.3}{25} \frac{5.7}{33} \frac{6.1}{50} \frac{6.2}{100}$$

$$\frac{1.4}{100} \frac{2.4}{50} \frac{3.0}{35} \frac{8.0}{23} \frac{8.5}{21} \frac{7.3}{14} 7.2 \frac{7.2}{13} \frac{8.6}{19} \frac{8.6}{25} \frac{7.4}{31} \frac{8.1}{50} \frac{9.1}{100}$$

$$\frac{2.1}{100} \frac{5.2}{50} \frac{6.5}{36} \frac{10.3}{25} \frac{10.3}{17} \frac{9.6}{14} 9.3 \frac{9.5}{13} \frac{10.6}{18} \frac{10.8}{24} \frac{10.7}{28} \frac{11.9}{50} \frac{13.4}{100}$$

$$\frac{3.0}{100} \frac{8.3}{50} \frac{9.4}{33} \frac{11.7}{29} \frac{11.4}{18} \frac{10.8}{14} 10.8 \frac{11.1}{15} \frac{14.1}{28} \frac{14.3}{38} \frac{15.3}{50} \frac{15.3}{100}$$

$$+1.2 \frac{1.8}{100} \frac{2.7}{50} \frac{3.7}{43} \frac{4.0}{40} \frac{4.7}{27} \frac{4.7}{25} \frac{4.8}{20} \frac{2.8}{14} 2.7 \frac{3.0}{14} \frac{5.8}{24} \frac{6.3}{50} \frac{6.3}{100}$$

$$\frac{1.4}{100} \frac{2.4}{75} \frac{5.9}{59} \frac{6.3}{50} \frac{6.1}{20} \frac{4.0}{14} 3.8 \frac{4.0}{13} \frac{6.0}{20} \frac{7.0}{50} \frac{7.0}{100}$$

$$\frac{7.4}{100} \frac{7.4}{50} \frac{7.1}{21} \frac{5.1}{13} 5.0 \frac{5.0}{13} \frac{6.8}{21} \frac{7.3}{50} \frac{7.3}{100}$$

897.95

12 Rt Sta 230 + 20

$$\frac{6.4}{100} \frac{6.4}{50} \frac{6.4}{35} \frac{6.1}{20} \frac{4.9}{13} 4.7 \frac{4.8}{14} \frac{6.2}{21} \frac{5.8}{29} \frac{5.8}{50} \frac{5.8}{100}$$

Sta	+	π	-	Elev
		894.93		
232				888.5
+82			X Drain	See Const Notes
233				88.9
234				90.2
T.P	9.59	899.84	2.70	890.23
235				91.8
236				93.6
+70				94.8
237				95.2
238				97.1
239				98.8
T.P	8.78	907.49	1.11	898.71
240				00.5
241				01.7
242				02.6

$$\begin{array}{r}
 892.93 \\
 10.75 \\
 \hline
 882.18
 \end{array}$$

$$\begin{array}{cccccccccccc}
 \frac{6.7}{100} & \frac{6.7}{50} & \frac{6.7}{33} & \frac{6.3}{21} & \frac{4.8}{14} & 4.4 & \frac{4.6}{14} & \frac{7.5}{22} & \frac{7.2}{28} & \frac{6.6}{31} & \frac{6.6}{50} & \frac{6.6}{100} \\
 & & 10.75 & & & & & 10.75 & & & & \\
 & & \text{Fin} & & & & & \text{Fin} & & & &
 \end{array}$$

$$\begin{array}{cccccccccccc}
 \frac{6.6}{100} & \frac{6.6}{50} & \frac{6.6}{28} & \frac{6.1}{22} & \frac{3.7}{14} & 4.0 & \frac{4.0}{14} & \frac{6.5}{25} & \frac{6.5}{50} & \frac{6.5}{100}
 \end{array}$$

$$\begin{array}{cccccccccccc}
 \frac{5.8}{100} & \frac{5.8}{50} & \frac{4.6}{20} & \frac{2.8}{14} & 2.7 & \frac{2.8}{14} & \frac{4.2}{21} & \frac{5.1}{50} & \frac{5.1}{100}
 \end{array}$$

$$\begin{array}{cccccccccccc}
 \frac{11.1}{100} & \frac{10.1}{50} & \frac{9.5}{31} & \frac{9.4}{20} & \frac{8.1}{14} & 8.0 & \frac{8.3}{14} & \frac{9.6}{19} & \frac{8.7}{26} & \frac{8.4}{31} & \frac{8.4}{50} & \frac{8.6}{100}
 \end{array}$$

$$\begin{array}{cccccccccccc}
 \frac{7.4}{100} & \frac{9.4}{50} & \frac{10.0}{32} & \frac{9.1}{23} & \frac{7.0}{15} & 6.2 & \frac{6.5}{14} & \frac{8.5}{22} & \frac{8.9}{29} & \frac{8.5}{50} & \frac{6.0}{100}
 \end{array}$$

$$\begin{array}{cccccccccccc}
 \frac{7.5}{100} & \frac{7.5}{50} & \frac{6.7}{22} & \frac{5.1}{14} & 5.0 & \frac{5.2}{15} & \frac{6.5}{20} & \frac{6.7}{30} & \frac{6.7}{50} & \frac{5.7}{100}
 \end{array}$$

$$\begin{array}{cccccccccccc}
 \frac{4.4}{100} & \frac{4.4}{50} & \frac{4.6}{32} & \frac{6.2}{25} & \frac{6.0}{19} & \frac{4.7}{14} & 4.6 & \frac{4.7}{15} & \frac{6.2}{22} & \frac{6.1}{27} & \frac{5.3}{33} & \frac{5.3}{50} & \frac{5.3}{100}
 \end{array}$$

$$\begin{array}{cccccccccccc}
 \frac{0.0}{100} & \frac{0.8}{50} & \frac{0.6}{39} & \frac{1.3}{25} & \frac{4.1}{24} & \frac{4.2}{18} & \frac{2.8}{14} & 2.7 & \frac{3.0}{15} & \frac{4.1}{19} & \frac{4.1}{25} & \frac{2.3}{34} & \frac{2.3}{50} & \frac{2.8}{100}
 \end{array}$$

$$\begin{array}{cccccccccccc}
 \frac{0.7}{100} & \frac{1.7}{50} & \frac{1.7}{33} & \frac{2.7}{27} & \frac{2.7}{19} & \frac{1.2}{14} & 1.0 & \frac{1.3}{15} & \frac{2.6}{19} & \frac{2.8}{24} & \frac{3.4}{50} & \frac{3.4}{100}
 \end{array}$$

$$\begin{array}{cccccccccccc}
 \frac{10.2}{100} & \frac{10.7}{25} & \frac{10.2}{50} & \frac{10.2}{35} & \frac{8.9}{21} & \frac{7.2}{14} & 7.0 & \frac{7.4}{15} & \frac{8.9}{20} & \frac{9.7}{25} & \frac{9.7}{50} & \frac{9.7}{100}
 \end{array}$$

$$\begin{array}{cccccccccccc}
 \frac{5.9}{100} & \frac{6.4}{75} & \frac{6.4}{31} & \frac{7.5}{25} & \frac{7.3}{19} & \frac{6.2}{14} & 5.8 & \frac{6.0}{13} & \frac{6.7}{17} & \frac{7.5}{22} & \frac{8.3}{50} & \frac{8.3}{100}
 \end{array}$$

$$\begin{array}{cccccccccccc}
 \frac{5.0}{100} & \frac{5.5}{50} & \frac{4.6}{35} & \frac{5.0}{30} & \frac{6.6}{24} & \frac{6.2}{18} & \frac{5.2}{14} & 4.9 & \frac{5.0}{14} & \frac{6.2}{17} & \frac{6.4}{20} & \frac{5.7}{23} & \frac{5.7}{50} & \frac{5.7}{100}
 \end{array}$$

Sta + π - Elev

907.49.

242+50

03.0

243

02.7

244

02.7

B.M

3.12

904.37.

245

02.0

+50

01.4

246

01.0

Lt Lt Rt

$\frac{5.1}{100}$ $\frac{5.1}{50}$ $\frac{4.2}{35}$ $\frac{4.7}{30}$ $\frac{6.2}{24}$ $\frac{6.1}{17}$ $\frac{4.7}{13}$ 45 $\frac{5.0}{19}$ $\frac{6.1}{17}$ $\frac{6.1}{21}$ $\frac{3.5}{27}$ $\frac{3.5}{50}$ $\frac{3.4}{100}$

$\frac{4.7}{100}$ $\frac{4.7}{50}$ $\frac{4.7}{32}$ $\frac{6.2}{25}$ $\frac{6.2}{19}$ $\frac{5.0}{15}$ 48 $\frac{5.1}{14}$ $\frac{6.3}{16}$ $\frac{6.4}{20}$ $\frac{3.0}{21}$ $\frac{3.0}{50}$ $\frac{3.0}{100}$

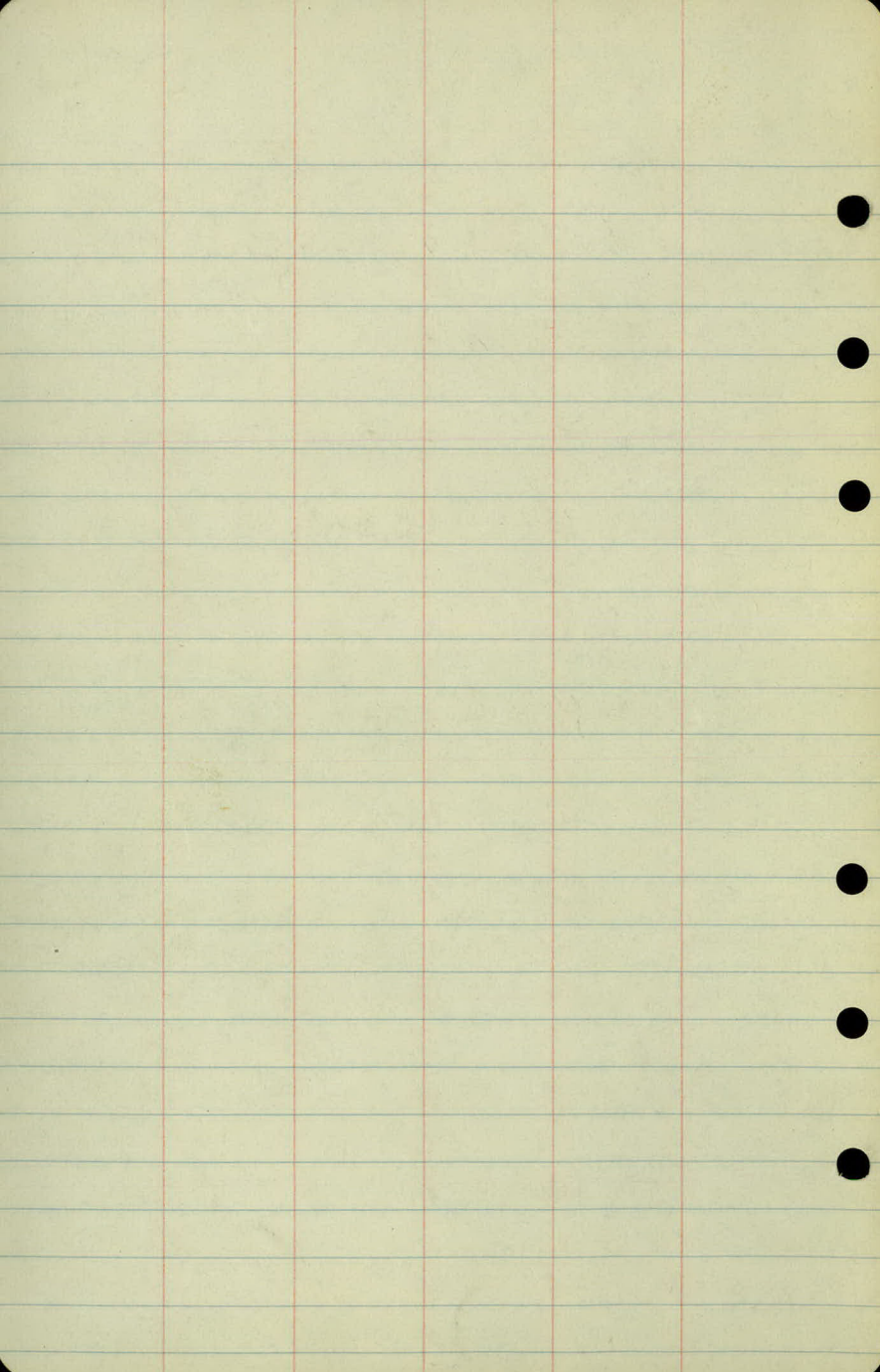
$\frac{8.5}{100}$ $\frac{7.0}{50}$ $\frac{6.1}{30}$ $\frac{6.8}{26}$ $\frac{6.7}{19}$ $\frac{5.1}{14}$ 48 $\frac{4.8}{14}$ $\frac{6.3}{18}$ $\frac{6.2}{22}$ $\frac{4.3}{21}$ $\frac{4.3}{50}$ $\frac{4.3}{100}$

904.37 Spike in Co Hollywood 33 Rt Stg 244+65

$\frac{10.3}{100}$ $\frac{8.7}{50}$ $\frac{7.3}{29}$ $\frac{7.0}{19}$ $\frac{5.8}{15}$ 5.5 $\frac{5.8}{14}$ $\frac{7.0}{17}$ $\frac{6.9}{21}$ $\frac{4.7}{27}$ $\frac{4.2}{50}$ $\frac{5.2}{100}$

$\frac{10.0}{100}$ $\frac{9.0}{50}$ $\frac{7.8}{33}$ $\frac{7.3}{18}$ $\frac{6.3}{15}$ 6.1 $\frac{6.5}{13}$ $\frac{7.4}{17}$ $\frac{7.4}{21}$ $\frac{4.8}{27}$ $\frac{4.8}{50}$ $\frac{6.3}{100}$

$\frac{11.0}{100}$ $\frac{9.3}{50}$ $\frac{8.7}{37}$ $\frac{8.2}{20}$ $\frac{6.8}{15}$ 6.5 $\frac{7.0}{14}$ $\frac{8.3}{17}$ $\frac{8.6}{23}$ $\frac{8.5}{50}$ $\frac{9.5}{100}$



X Sect
No Co Line Rd
Sta 246 to Hodgson Ref.

STA.	+	π	-	Elev
	1.29	905.66		904.37
246+60				00.8
247				00.8
248				00.8
249				01.0
250				01.6
T.P. #30	5.30	906.64	432	901.34.
251				01.9
252				02.0
253				01.8
254				01.6
255				01.5
+78	skew	? x 14" x Drain CMP 1935 Notes		
256				02.7
T.P. #31	6.29	909.35	3.58	903.06.
257				03.5

Lt L Rt

$$\frac{9.2}{100} \frac{9.4}{50} \frac{8.2}{25} \frac{5.3}{13} 4.9 \frac{5.4}{14} \frac{8.0}{23} \frac{9.2}{32} \frac{9.4}{50} \frac{9.7}{100}$$

i

$$\frac{7.8}{100} \frac{7.2}{50} \frac{7.8}{29} \frac{7.4}{23} \frac{5.2}{13} 4.9 \frac{5.3}{14} \frac{8.3}{24} \frac{8.9}{32} \frac{9.2}{50} \frac{9.4}{100}$$

$$\frac{6.2}{100} \frac{5.8}{75} \frac{6.8}{50} \frac{5.7}{36} \frac{7.0}{24} \frac{6.4}{17} \frac{5.0}{13} 4.9 \frac{5.2}{13} \frac{6.7}{19} \frac{7.4}{24} \frac{8.1}{50} \frac{8.1}{80} \frac{7.5}{100}$$

$$\frac{3.8}{100} \frac{4.1}{50} \frac{4.0}{37} \frac{6.4}{27} \frac{6.1}{20} \frac{5.1}{14} 4.7 \frac{5.1}{12} \frac{6.2}{18} \frac{6.6}{25} \frac{6.0}{33} \frac{6.0}{50} \frac{6.0}{100}$$

$$\frac{3.1}{100} \frac{3.1}{50} \frac{2.7}{39} \frac{5.6}{25} \frac{5.5}{19} \frac{4.5}{14} 4.1 \frac{4.5}{12} \frac{5.7}{18} \frac{6.2}{24} \frac{5.5}{34} \frac{5.5}{50} \frac{6.0}{100}$$

901.34 12' Rt 250 + 13

$$\frac{4.3}{100} \frac{4.3}{65} \frac{5.0}{42} \frac{5.7}{33} \frac{6.5}{27} \frac{6.3}{19} \frac{5.2}{13} 4.7 \frac{5.2}{13} \frac{6.7}{20} \frac{6.7}{50} \frac{6.7}{100}$$

$$\frac{5.0}{100} \frac{5.0}{50} \frac{4.8}{33} \frac{6.3}{25} \frac{6.2}{18} \frac{4.9}{14} 4.6 \frac{6.1}{14} \frac{6.3}{21} \frac{6.1}{37} \frac{6.5}{50} \frac{6.5}{100}$$

$$\frac{5.2}{100} \frac{5.2}{50} \frac{5.5}{33} \frac{6.6}{27} \frac{7.0}{20} \frac{4.9}{14} 4.8 \frac{5.0}{13} \frac{7.0}{20} \frac{8.1}{50} \frac{8.1}{100}$$

$$\frac{6.7}{100} \frac{5.7}{50} \frac{6.0}{32} \frac{6.7}{26} \frac{6.5}{19} \frac{5.2}{13} 5.0 \frac{5.4}{13} \frac{7.0}{19} \frac{7.8}{25} \frac{8.2}{50} \frac{8.2}{100}$$

$$\frac{5.0}{100} \frac{5.0}{50} \frac{5.1}{32} \frac{6.3}{26} \frac{6.3}{19} \frac{5.3}{14} 5.1 \frac{5.3}{13} \frac{6.5}{19} \frac{8.1}{50} \frac{8.6}{100}$$

24'

Ditch

9.6

100'

9.6

Inv.

9.7

Inv.

9.7

100'

7'

4'

9.7

100'

9.7

100'

9.7

100'

$$\frac{4.8}{100} \frac{4.8}{50} \frac{5.0}{35} \frac{5.9}{25} \frac{6.0}{19} \frac{4.9}{15} 4.4 \frac{4.9}{16} \frac{5.9}{20} \frac{7.0}{31} \frac{9.4}{38} \frac{9.7}{46} \frac{7.0}{50} \frac{6.5}{60} \frac{6.5}{100}$$

903.06 12' Rt 256 + 92 Stake

$$\frac{5.0}{100} \frac{4.4}{50} \frac{4.6}{44} \frac{5.2}{34} \frac{7.6}{24} \frac{7.3}{18} \frac{6.1}{14} 5.9 \frac{6.4}{14} \frac{7.4}{18} \frac{7.7}{21} \frac{7.2}{26} \frac{6.3}{31} \frac{6.1}{41} \frac{6.6}{50} \frac{8.1}{100}$$

Sta + X - Elev

909.35

258

04.6

+ 39

04.8

+ 44

04.9

+ 51

West Shoulder Line 04.9

+ 70 ⁷⁰/₁

B.M

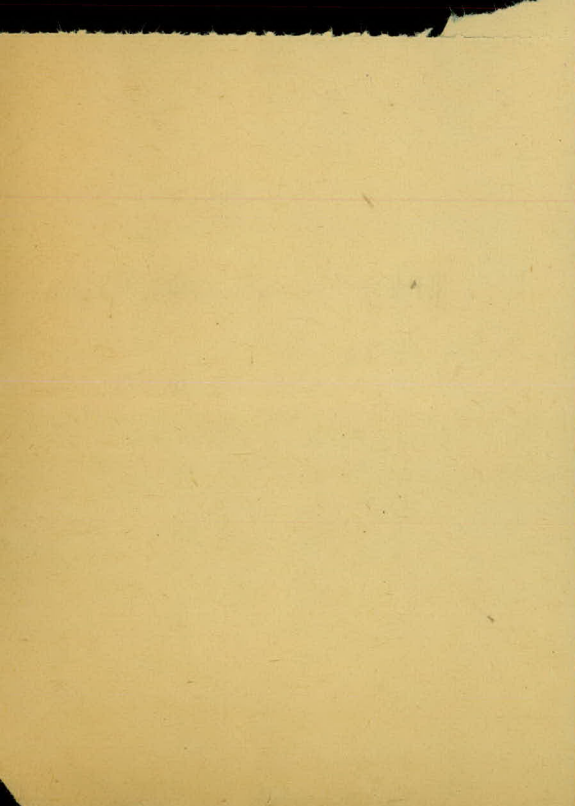
* Hodgson Rd

05.1

STH #49

4.34

905.01



L4 £ Rt

$\frac{3.4}{100}$ $\frac{2.8}{50}$ $\frac{3.2}{34}$ $\frac{5.3}{28}$ $\frac{6.1}{23}$ $\frac{6.1}{18}$ $\frac{5.1}{14}$ 4.8 $\frac{5.4}{15}$ $\frac{6.5}{18}$ $\frac{6.4}{23}$ $\frac{5.1}{29}$ $\frac{5.2}{50}$ $\frac{8.3}{100}$

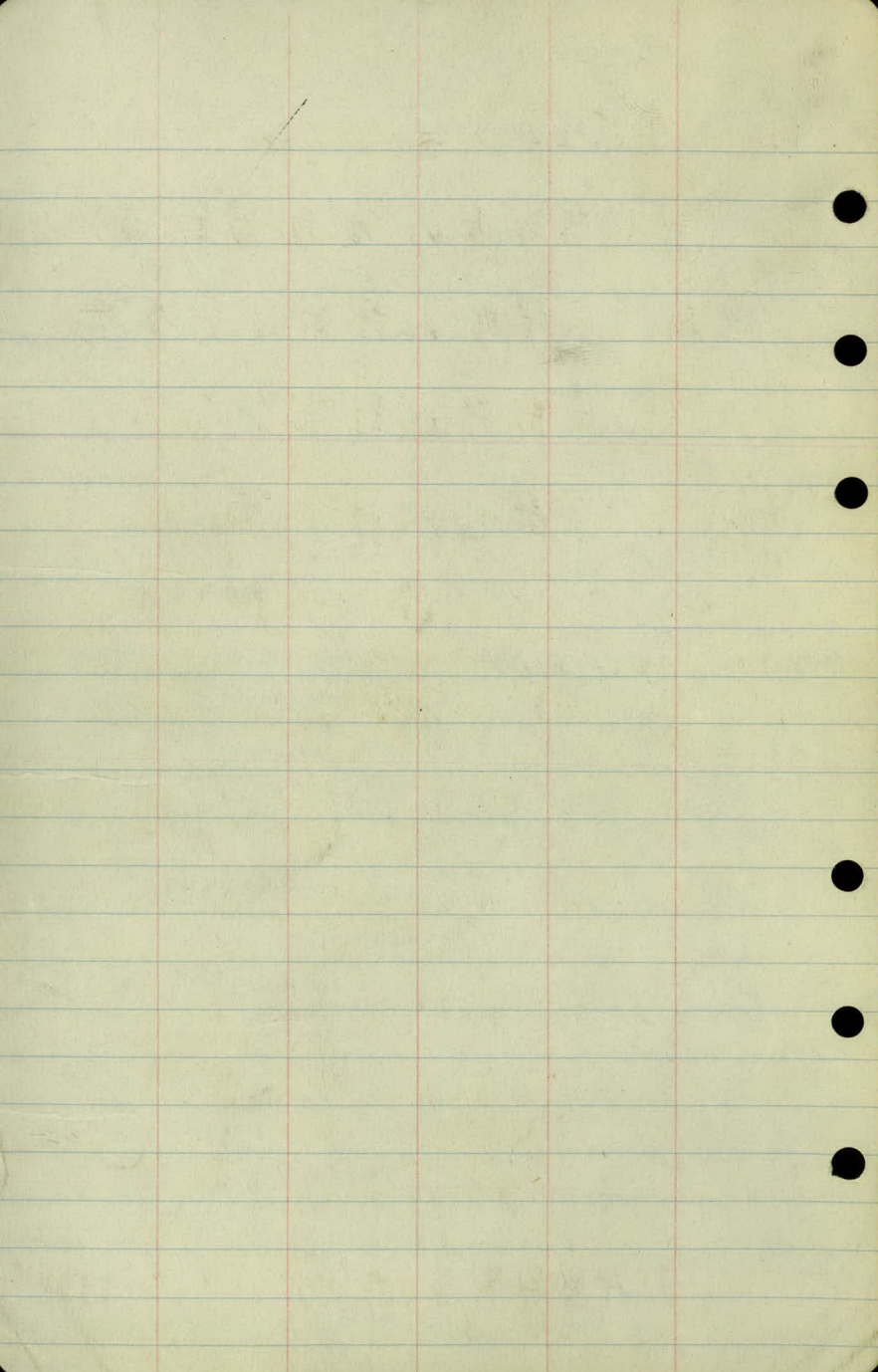
$\frac{3.9}{100}$ $\frac{3.0}{50}$ $\frac{2.9}{36}$ $\frac{5.7}{25}$ $\frac{5.8}{19}$ $\frac{4.7}{14}$ 4.6 $\frac{5.0}{15}$ $\frac{6.0}{20}$ $\frac{6.0}{25}$ $\frac{3.9}{33}$ $\frac{4.5}{50}$ $\frac{8.2}{100}$

$\frac{6.5}{100}$ $\frac{5.9}{41}$ $\frac{5.4}{27}$ $\frac{4.8}{19}$ 4.5 $\frac{5.0}{23}$ $\frac{5.7}{31}$ $\frac{6.6}{41}$ $\frac{7.0}{50}$ $\frac{8.2}{100}$

$\frac{5.4}{100}$ $\frac{5.0}{50}$ 4.5 $\frac{5.1}{50}$ $\frac{5.4}{100}$

$\frac{4.7}{100}$ 4.3 $\frac{5.0}{100}$

905.01 Top of Mont



X-Sections

No County Line

Hodgson Road East

3.51

908.52 ✓

905.01

259

04.5 ✓

+35

04.5 ✓

260

04.2 ✓

261

03.5 ✓

262

03.3 ✓

263

03.6 ✓

264

04.6 ✓

265

04.8 ✓

B.M.

4.85

910.79 ✓

2.58

905.94 ✓

266

05.3 ✓

Top Mant Hodgson + "J"

$$\frac{55}{50} \frac{42}{39} \frac{41}{18} 40 \frac{46}{18} \frac{43}{38} \frac{43}{50}$$

$$\frac{40}{50} \frac{38}{25} \frac{50}{16} \frac{42}{12} \frac{45}{11} 40 \frac{46}{14} \frac{40}{17} \frac{53}{20} \frac{57}{30} \frac{63}{24} \frac{68}{50}$$

$$\frac{42}{50} \frac{40}{39} \frac{29}{26} \frac{64}{18} \frac{63}{16} \frac{49}{12} 4.3 \frac{48}{11} \frac{50}{15} \frac{63}{17} \frac{70}{21} \frac{62}{25} \frac{65}{30} \frac{70}{50}$$

$$\frac{49}{50} \frac{49}{28} \frac{73}{20-17} \frac{51}{12} 5.0 \frac{56}{16} \frac{74}{20-23} \frac{66}{27} \frac{71}{37} \frac{82}{50}$$

$$\frac{71}{50} \frac{70}{40} \frac{66}{35} \frac{64}{26} \frac{75}{21-14} \frac{56}{10} 5.2 \frac{57}{16} \frac{74}{21-24} \frac{70}{28} \frac{76}{32} \frac{78}{50}$$

$$\frac{59}{50} \frac{52}{29} \frac{46}{26} \frac{55}{23} \frac{68}{16-14} \frac{54}{10} 4.9 \frac{51}{17} \frac{65}{21-24} \frac{58}{27} \frac{59}{31} \frac{65}{50}$$

$$\frac{46}{50} \frac{40}{29} \frac{36}{24} \frac{50}{14} \frac{54}{11} \frac{43}{8} 3.9 \frac{45}{13} \frac{38}{17} \frac{48}{21-24} \frac{38}{29} \frac{39}{32} \frac{48}{50}$$

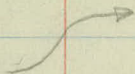
$$\frac{32}{50} \frac{28}{37} \frac{31}{22} \frac{42}{15} \frac{44}{10} \frac{39}{7} 3.7 \frac{38}{16} \frac{36}{17} \frac{45}{21} \frac{46}{25} \frac{39}{31} \frac{42}{34} \frac{48}{50}$$

SpK in 15" BE. Rt Sta 265+12 (25')

$$\frac{48}{50} \frac{43}{21} \frac{55}{14} \frac{51}{7} 5.5 \frac{56}{16} \frac{52}{18} \frac{56}{20-23} \frac{45}{26} \frac{33}{31} \frac{39}{35} \frac{47}{50}$$

✓
910.79

267



05.1 -

268

04.3 -

269

03.0 -

270

01.0 -

271

99.5 -

272

98.9 -

273

99.8 -

274

00.5 -

275 +50

00.8 -

275

00.4 -

BM

0.71

✓
904.03

7.47

✓
903.32

Floor No 2.0

$\frac{4.3}{50}$ $\frac{3.5}{26}$ $\frac{4.3}{21}$ $\frac{4.7}{9}$ $\frac{5.9}{6}$ 5.7 $\frac{5.5}{8}$ $\frac{5.8}{17}$ $\frac{5.4}{19-25}$ $\frac{4.0}{26}$ $\frac{3.9}{30}$ $\frac{2.2}{34}$ $\frac{2.3}{50}$

$\frac{5.4}{50}$ $\frac{6.5}{24}$ $\frac{6.4}{20}$ $\frac{6.7}{8}$ $\frac{6.7}{6}$ 6.5 $\frac{6.3}{7}$ $\frac{6.7}{18}$ $\frac{6.4}{20}$ $\frac{6.7}{22-25}$ $\frac{3.2}{32}$ $\frac{3.7}{50}$

$\frac{8.2}{50}$ $\frac{6.5}{31}$ $\frac{8.5}{20}$ $\frac{8.1}{5}$ 7.8 $\frac{7.7}{8}$ $\frac{8.4}{18}$ $\frac{7.5}{20}$ $\frac{6.6}{34}$ $\frac{7.2}{50}$

$\frac{11.5}{50}$ $\frac{10.7}{29}$ $\frac{11.2}{19-12}$ $\frac{10.1}{5}$ 9.8 $\frac{9.6}{6}$ $\frac{10.4}{18}$ $\frac{10.2}{21}$ $\frac{12.4}{25-29}$ $\frac{11.6}{32}$ $\frac{11.3}{36}$ $\frac{11.5}{50}$

$\frac{10.9}{50}$ $\frac{11.4}{27}$ $\frac{12.4}{21}$ $\frac{12.5}{11}$ $\frac{11.6}{5}$ 11.3 $\frac{11.0}{7}$ $\frac{11.2}{17}$ $\frac{11.4}{21}$ $\frac{13.8}{26}$ $\frac{14.0}{31}$ $\frac{13.1}{34}$ $\frac{13.1}{50}$

$\frac{12.6}{50}$ $\frac{13.3}{25}$ $\frac{13.6}{14}$ $\frac{12.9}{10}$ $\frac{12.2}{7}$ 11.9 $\frac{11.6}{7-15}$ $\frac{11.4}{18}$ $\frac{13.8}{25-26}$ $\frac{13.2}{27}$ $\frac{12.6}{50}$

F.L. Col IV 14.2

F.L. Col IV 14.15

$\frac{12.0}{50}$ $\frac{11.7}{15}$ $\frac{11.4}{9}$ 11.0 $\frac{11.0}{4}$ $\frac{11.5}{13}$ $\frac{9.4}{30}$ $\frac{9.5}{33}$ $\frac{9.2}{50}$

$\frac{10.6}{50}$ $\frac{9.9}{32}$ $\frac{10.5}{8}$ 10.3 $\frac{10.3}{4}$ $\frac{11.0}{14}$ $\frac{10.4}{21}$ $\frac{4.1}{28}$ $\frac{5.7}{37}$ $\frac{6.1}{50}$

$\frac{8.3}{50}$ $\frac{8.0}{35}$ $\frac{9.4}{20}$ $\frac{9.2}{10}$ $\frac{10.2}{7}$ $\frac{3.4}{50}$ 10.0 $\frac{10.1}{3}$ $\frac{10.7}{14}$ $\frac{9.4}{20}$ $\frac{3.3}{28}$ $\frac{5.0}{34}$

$\frac{8.0}{50}$ $\frac{7.4}{34}$ $\frac{10.0}{10}$ $\frac{10.6}{8}$ 10.4 $\frac{11.0}{13}$ $\frac{10.1}{19}$ $\frac{4.3}{27}$ $\frac{6.0}{36}$ $\frac{6.3}{50}$

3pk in P.P. 28' Lt 274+55

✓
904.03

276 99.0 -

277 97.9 -

278 97.3 -

279 96.1 -

280 94.9 -

B.M. 10.59
893.44 ✓

281 95.0 -

B.M. 5.89 900.75 ✓ 9.17 894.86 ✓

282 95.2 -

B.M. 7.05 893.70 ✓

283 94.8 -

$$\frac{6.5}{50} \quad \frac{6.1}{22} \quad \frac{5.0}{10-8} \quad 5.0 \quad \frac{5.7}{10} \quad \frac{5.3}{13} \quad \frac{5.0}{24} \quad \frac{5.2}{27} \quad \frac{6.0}{50}$$

$$\frac{7.8}{50} \quad \frac{8.0}{17} \quad \frac{6.5}{12} \quad 6.1 \quad \frac{6.3}{12} \quad \frac{7.9}{19} \quad \frac{7.4}{24} \quad \frac{9.1}{28} \quad \frac{10.0}{50}$$

$$\frac{7.7}{50} \quad \frac{7.8}{15} \quad \frac{7.0}{8} \quad 6.7 \quad \frac{7.2}{12} \quad \frac{8.0}{17} \quad \frac{7.2}{24} \quad \frac{9.3}{33} \quad \frac{8.2}{43-50}$$

$$\frac{10.7}{50} \quad \frac{10.3}{16} \quad \frac{8.1}{8} \quad 7.9 \quad \frac{8.4}{12} \quad \frac{9.4}{18-20} \quad \frac{8.6}{23} \quad \frac{10.2}{30} \quad \frac{9.6}{50}$$

$$\frac{11.7}{50} \quad \frac{12.0}{17} \quad \frac{9.4}{10} \quad 9.1 \quad \frac{9.3}{11} \quad \frac{10.7}{17} \quad \frac{9.7}{24} \quad \frac{12.0}{31} \quad \frac{11.8}{50}$$

F.L. Cul 14 12.90

F.L. Cul 11 12.90

11.9

SpR in Tree 200 Rt Sta 280+

$$\frac{9.5}{50} \quad \frac{10.6}{15} \quad \frac{9.5}{12} \quad 9.0 \quad \frac{9.2}{11} \quad \frac{10.7}{18} \quad \frac{9.2}{23} \quad \frac{10.8}{26} \quad \frac{11.3}{50}$$

Nail in PP 28' Lt Sta 281+15

$$\frac{7.2}{50} \quad \frac{7.2}{17} \quad \frac{6.0}{11} \quad 5.6 \quad \frac{6.0}{11} \quad \frac{6.8}{17} \quad \frac{5.2}{22} \quad \frac{6.7}{30} \quad \frac{6.9}{50}$$

T.P. #35 PP Lt Sta 282+85

$$\frac{8.1}{50} \quad \frac{8.5}{15} \quad \frac{6.2}{10} \quad 6.0 \quad \frac{6.1}{11} \quad \frac{7.4}{17} \quad \frac{6.4}{22} \quad \frac{8.1}{31} \quad \frac{7.3}{50}$$

✓
100.75

284

95.5.

285

95.8.

+50

96.4.

286

97.0.

287

97.9.

288

98.9.

289

99.7.

B.M

0.34

✓
100.41

$$\frac{6.6}{50} \quad \frac{7.0}{15} \quad \frac{5.7}{11} \quad 5.3 \quad \frac{5.5}{11} \quad \frac{6.4}{17} \quad \frac{5.2}{22-26} \quad \frac{6.6}{33} \quad \frac{5.9}{40} \quad \frac{5.6}{50}$$

$$\frac{7.4}{50} \quad \frac{6.4}{14} \quad \frac{5.5}{11} \quad 5.0 \quad \frac{4.8}{10} \quad \frac{6.1}{16} \quad \frac{4.9}{22} \quad \frac{5.2}{25} \quad \frac{6.4}{29} \quad \frac{6.1}{39} \quad \frac{6.3}{50}$$

$$\frac{6.6}{50} \quad \frac{6.0}{25} \quad \frac{6.9}{22} \quad \frac{6.0}{16} \quad \frac{5.0}{11} \quad 4.4 \quad \frac{4.7}{13} \quad \frac{5.5}{17} \quad \frac{5.4}{50}$$

$$50 - \frac{4.2}{27} \quad \frac{6.2}{25} \quad \frac{5.4}{17} \quad \frac{4.0}{13} \quad 3.8 \quad \frac{4.2}{10} \quad \frac{5.0}{16} \quad \frac{4.1}{19} \quad \frac{4.3}{50}$$

$$\frac{0.8}{50} \quad \frac{1.4}{29} \quad \frac{5.1}{26} \quad \frac{4.1}{18} \quad \frac{3.2}{13} \quad 2.9 \quad \frac{3.2}{13} \quad \frac{4.0}{16} \quad \frac{1.4}{17} \quad \frac{1.1}{22} \quad \frac{1.0}{50}$$

$$\frac{1.2}{50} \quad \frac{1.4}{29} \quad \frac{3.7}{25} \quad \frac{3.7}{20} \quad \frac{2.3}{15} \quad 1.9 \quad \frac{2.1}{11} \quad \frac{2.9}{15} \quad \frac{0.7}{17} \quad \frac{0.6}{50}$$

$$\frac{0.4}{50} \quad \frac{0.3}{31} \quad \frac{3.3}{25} \quad \frac{3.1}{31} \quad \frac{1.3}{14} \quad 1.1 \quad \frac{1.3}{11} \quad \frac{2.0}{15} \quad \frac{+1.0}{16} \quad \frac{+1.9}{50}$$

No. 1 in F.P. 70' Lt Sta 289+18

Sta	+	H.I.	-	Elev	T
	3.98	904.39			900.41
290				00.1.	
T.P #36	3.01	904.39	3.01		901.38
291				00.1.	
292				99.6.	
293				98.9.	
294				98.8.	
295				98.3.	
296				98.3.	
T.P	6.23	903.93	6.69		897.70
297				98.8.	
298				98.9.	
299				98.5.	
B.M	6.13	903.93	6.13		897.80
300				98.9.	
301				99.2.	

At 2 Rt

2.9 3.3 6.5 6.1 4.7 4.6 5.0 5.0 3.2 2.2
50 29 24 18 13 43 10 12 16 17 50

9013827' At Sta 289+50

4.8 4.4 6.4 6.1 4.4 4.7 5.4 3.1 2.6
50 28 25 19 10 43 9 14 12 50

4.1 4.2 6.8 6.6 5.3 5.1 6.3 6.4 5.2 5.0
50 27 25 19 13 48 12 10 19 21 50

6.2 7.2 6.8 7.3 7.1 6.2 5.9 7.3 7.8
50 32 25 23 17 14 5.5 11 16 50

8.5 9.0 9.1 6.3 6.0 8.4 8.4
50 31 20 13 5.6 9 16 50

8.0 8.5 8.1 9.0 9.0 6.8 6.6 8.3 8.3 8.0
50 31 24 21 18 13 6.1 10 14 18 50

9.5 9.1 8.7 9.1 6.6 6.4 7.9 6.9
50 31 25 17 13 6.1 10 16 50

89760#37 At 296

7.3 7.3 7.2 5.8 5.5 6.7 6.2
50 28 18 14 5.1 9 14 50

6.0 6.3 5.9 6.2 5.7 5.3 5.1 4.6
50 31 24 18 13 5.0 8 15 50

7.5 7.3 6.9 5.6 6.0 6.0 6.7 5.6
50 30 24 12 5.4 10 12 14 50

89770 Sp. Kx in Cottonwood

4.4 5.4 6.9 7.1 5.6 5.3 6.0 5.1 5.7
50 35 27 20 14 5.0 9 14 25 50

7.3 6.8 5.4 5.1 5.8 5.9
50 20 13 4.7 8 13 50

Sta + π - Elev

903.93

301+50

99.4.

302

99.5.

303

99.4.

T.P

3.90

903.93

3.90

900.03

304

99.6.

305

99.3.

T.P

2.04

901.39

900.39

4.58

898.35

306

98.7.

899.35

307

97.4.

308

96.6.

309

94.4.

310

94.0.

310+50

93.9.

311

T.P

8.56

94.0.

892.85

891.83

LT R RT

$\frac{7.0}{50}$ $\frac{6.9}{29}$ $\frac{6.7}{18}$ $\frac{4.9}{12}$ 4.5 $\frac{4.8}{8}$ $\frac{4.5}{11}$ $\frac{4.8}{16}$ $\frac{4.9}{50}$

$\frac{5.3}{50}$ $\frac{4.9}{28}$ $\frac{6.6}{26}$ $\frac{6.2}{20}$ $\frac{5.1}{10}$ 4.4 $\frac{4.8}{11}$ $\frac{5.4}{19}$ $\frac{4.7}{50}$

$\frac{3.6}{50}$ $\frac{4.0}{28}$ $\frac{6.2}{26}$ $\frac{5.8}{20}$ $\frac{4.9}{16}$ 4.5 $\frac{4.4}{11}$ $\frac{5.4}{18}$ $\frac{3.7}{50}$

#38 RT 51 9 303

$\frac{3.7}{50}$ $\frac{3.7}{23}$ $\frac{4.6}{18}$ $\frac{4.2}{13}$ 4.3 $\frac{4.2}{9}$ $\frac{6.6}{17}$ $\frac{4.2}{50}$

$\frac{4.7}{50}$ $\frac{4.9}{29}$ $\frac{6.7}{21}$ $\frac{6.4}{23}$ $\frac{5.7}{21}$ $\frac{4.9}{17}$ 4.6 $\frac{4.8}{7}$ $\frac{4.5}{10}$ $\frac{6.2}{16}$ $\frac{5.7}{30}$ $\frac{6.1}{50}$

$\frac{3.8}{50}$ $\frac{3.9}{32}$ $\frac{5.9}{31}$ $\frac{4.8}{20}$ $\frac{3.4}{16}$ 2.7 $\frac{2.0}{9}$ $\frac{4.0}{17}$ $\frac{3.7}{29}$ $\frac{3.4}{50}$

$\frac{4.8}{50}$ $\frac{5.3}{33}$ $\frac{6.7}{31}$ $\frac{6.1}{21}$ $\frac{4.3}{15}$ 4.0 $\frac{4.5}{8}$ $\frac{4.1}{12}$ $\frac{5.8}{15}$ $\frac{5.9}{24}$ $\frac{5.5}{26}$ $\frac{5.5}{50}$

$\frac{7.4}{50}$ $\frac{7.2}{27}$ $\frac{7.6}{26}$ $\frac{7.2}{20}$ $\frac{5.8}{15}$ 4.8 $\frac{5.4}{11}$ $\frac{7.1}{14}$ $\frac{7.7}{27}$ $\frac{8.3}{50}$

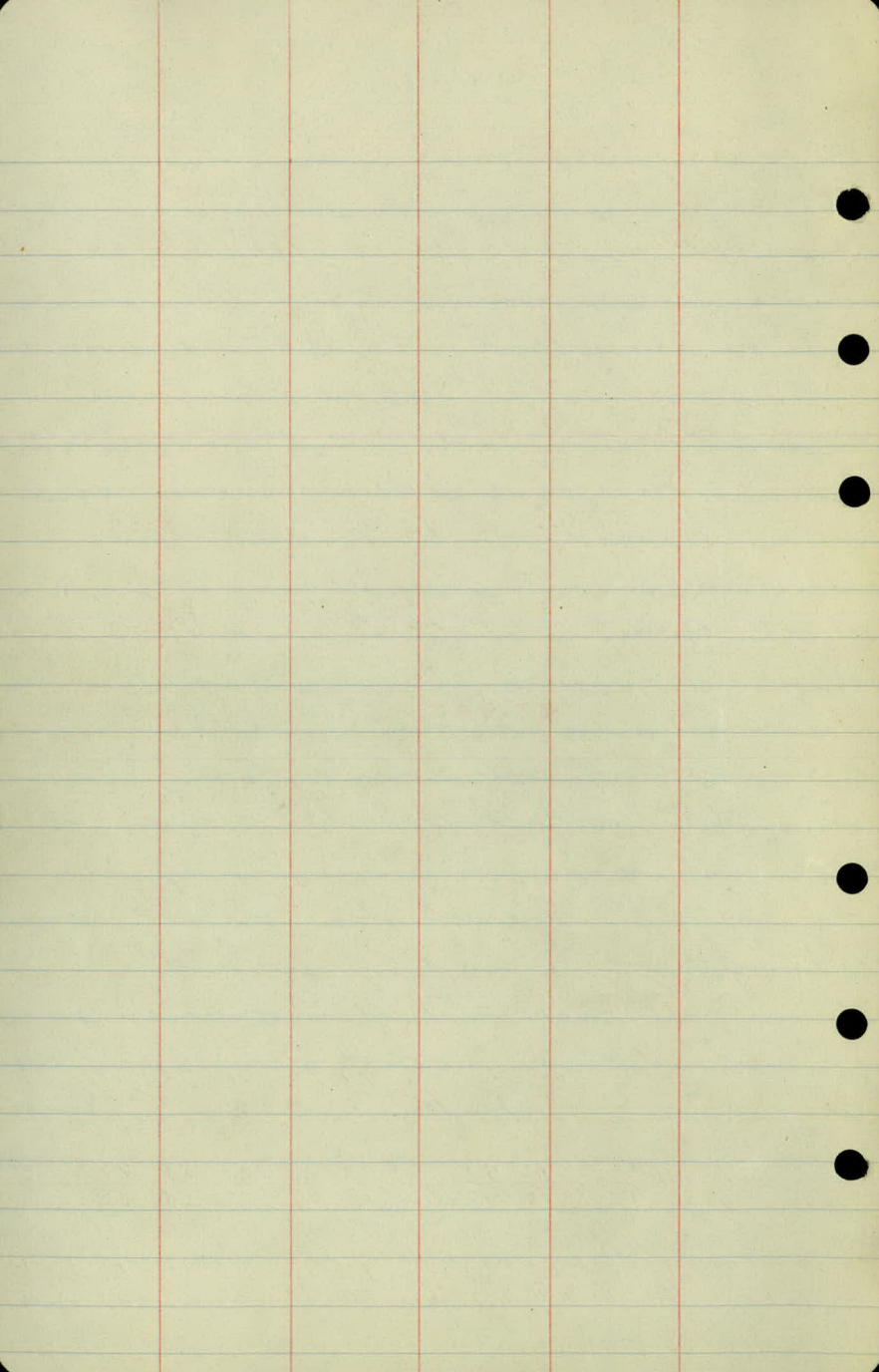
$\frac{9.3}{50}$ $\frac{9.5}{27}$ $\frac{10.5}{26}$ $\frac{9.9}{19}$ $\frac{7.3}{14}$ 7.0 $\frac{7.6}{11}$ $\frac{10.2}{17}$ $\frac{10.2}{23}$ $\frac{9.2}{26}$ $\frac{8.5}{50}$

$\frac{9.7}{50}$ $\frac{9.9}{27}$ $\frac{10.5}{26}$ $\frac{10.4}{20}$ $\frac{8.0}{13}$ 7.4 $\frac{7.9}{9}$ $\frac{10.5}{18}$ $\frac{11.1}{20}$ $\frac{10.0}{25}$ $\frac{10.1}{28}$ $\frac{9.5}{50}$

$\frac{9.4}{50}$ $\frac{9.4}{27}$ $\frac{9.8}{25}$ $\frac{9.5}{18}$ $\frac{7.8}{13}$ 7.5 $\frac{8.0}{11}$ $\frac{10.4}{19}$ $\frac{10.4}{23}$ $\frac{8.9}{25}$ $\frac{7.8}{50}$

892.71 $\frac{9.9}{50}$ $\frac{9.7}{27}$ $\frac{10.2}{25}$ $\frac{10.0}{20}$ $\frac{8.0}{13}$ 7.4 $\frac{7.7}{10}$ $\frac{9.2}{18}$ $\frac{10.2}{20}$ $\frac{10.3}{23}$ $\frac{9.4}{24}$ $\frac{8.5}{26}$ $\frac{7.5}{50}$

TP #39 Ch. 20 Notes



Cross sections

North Side of
North Co. Line

Sta- 167-178

167	5.33	988.13	82.8
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168

169

170

171

172

0	5.24	988.29	5.08	983.05
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173

174

175

176

177

178

2

$$\begin{array}{r} 8.1 \\ 500 \end{array} \quad \begin{array}{r} 8.1 \\ 400 \end{array} \quad \begin{array}{r} 7.8 \\ 300 \end{array} \quad \begin{array}{r} 8.4 \\ 200 \end{array} \quad \begin{array}{r} 8.1 \\ 150 \end{array}$$

$$\begin{array}{r} 7.5 \\ 500 \end{array} \quad \begin{array}{r} 8.0 \\ 400 \end{array} \quad \begin{array}{r} 7.8 \\ 300 \end{array} \quad \begin{array}{r} 7.2 \\ 200 \end{array} \quad \begin{array}{r} 6.9 \\ 165 \end{array} \quad \begin{array}{r} 8.1 \\ 150 \end{array}$$

$$\begin{array}{r} 6.4 \\ 500 \end{array} \quad \begin{array}{r} 6.2 \\ 400 \end{array} \quad \begin{array}{r} 6.3 \\ 365 \end{array} \quad \begin{array}{r} 8.1 \\ 350 \end{array} \quad \begin{array}{r} 6.6 \\ 300 \end{array} \quad \begin{array}{r} 5.9 \\ 200 \end{array} \quad \begin{array}{r} 6.7 \\ 170 \end{array} \quad \begin{array}{r} 8.3 \\ 150 \end{array}$$

$$\begin{array}{r} 5.1 \\ 500 \end{array} \quad \begin{array}{r} 5.2 \\ 400 \end{array} \quad \begin{array}{r} 7.6 \\ 300 \end{array} \quad \begin{array}{r} 8.2 \\ 200 \end{array} \quad \begin{array}{r} 8.7 \\ 150 \end{array}$$

$$\begin{array}{r} 0.8 \\ 500 \end{array} \quad \begin{array}{r} 1.0 \\ 400 \end{array} \quad \begin{array}{r} 3.8 \\ 340 \end{array} \quad \begin{array}{r} 4.0 \\ 300 \end{array} \quad \begin{array}{r} 5.8 \\ 200 \end{array} \quad \begin{array}{r} 6.6 \\ 150 \end{array}$$

$$\begin{array}{r} 0.0 \\ 300 \end{array} \quad \begin{array}{r} 3.0 \\ 250 \end{array} \quad \begin{array}{r} 6.0 \\ 200 \end{array} \quad \begin{array}{r} 7.8 \\ 150 \end{array}$$

Nail in 2 @ Sta. 172

$$\begin{array}{r} 0.0 \\ 287 \end{array} \quad \begin{array}{r} 6.2 \\ 250 \end{array} \quad \begin{array}{r} 6.9 \\ 200 \end{array} \quad \begin{array}{r} 6.8 \\ 150 \end{array}$$

$$\begin{array}{r} 1.7 \\ 500 \end{array} \quad \begin{array}{r} 4.0 \\ 400 \end{array} \quad \begin{array}{r} 5.4 \\ 300 \end{array} \quad \begin{array}{r} 6.5 \\ 270 \end{array} \quad \begin{array}{r} 6.5 \\ 200 \end{array} \quad \begin{array}{r} 6.6 \\ 150 \end{array}$$

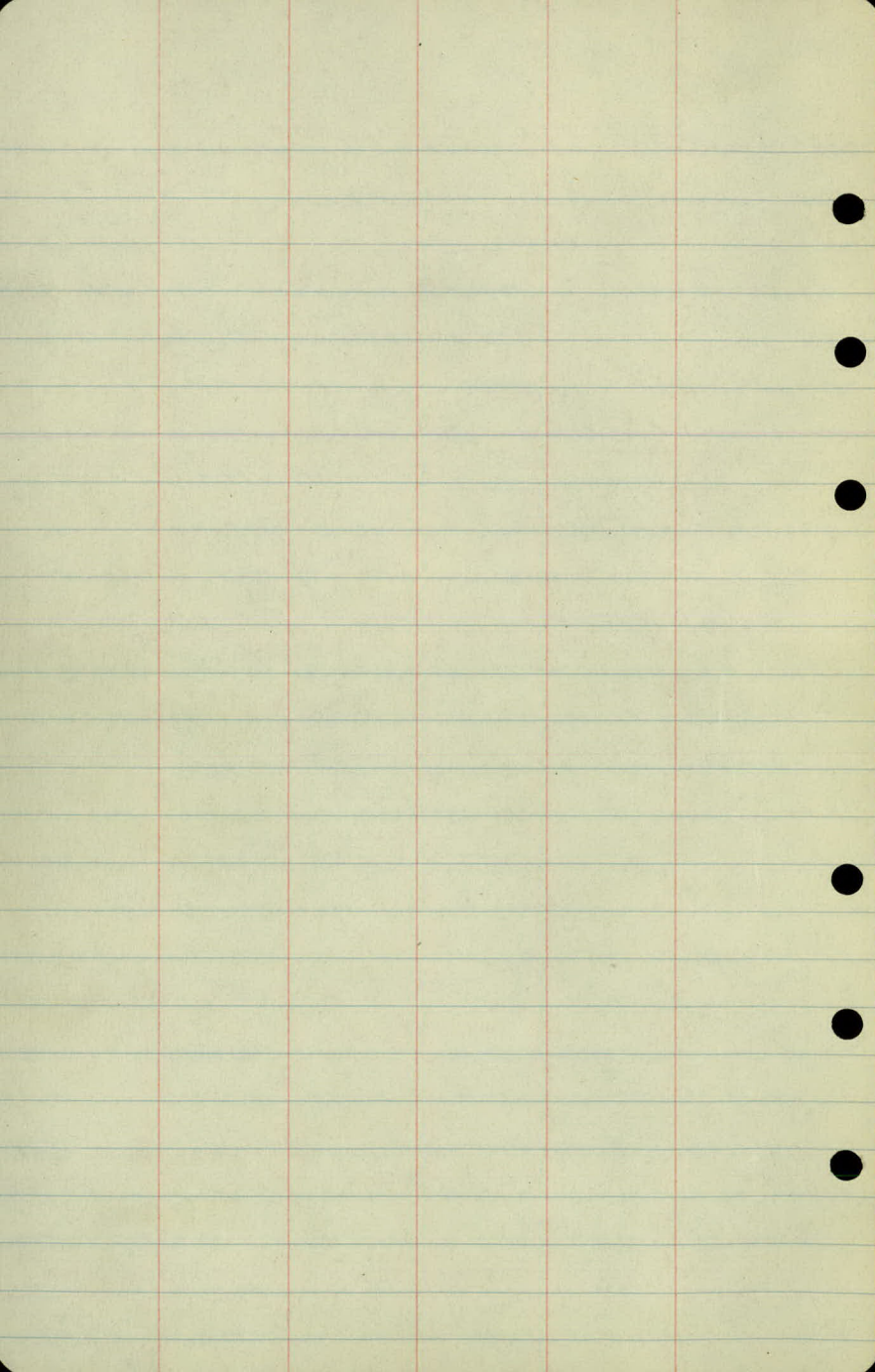
$$\begin{array}{r} 6.3 \\ 500 \end{array} \quad \begin{array}{r} 7.8 \\ 400 \end{array} \quad \begin{array}{r} 8.1 \\ 300 \end{array} \quad \begin{array}{r} 7.6 \\ 200 \end{array} \quad \begin{array}{r} 8.3 \\ 150 \end{array}$$

$$\begin{array}{r} 7.9 \\ 500 \end{array} \quad \begin{array}{r} 7.8 \\ 400 \end{array} \quad \begin{array}{r} 7.4 \\ 300 \end{array} \quad \begin{array}{r} 7.2 \\ 200 \end{array} \quad \begin{array}{r} 7.2 \\ 150 \end{array}$$

(Creek)

$$\begin{array}{r} 7.4 \\ 500 \end{array} \quad \begin{array}{r} 6.5 \\ 365 \end{array} \quad \begin{array}{r} 11.7 \\ 300 \end{array} \quad \begin{array}{r} 9.4 \\ 300 \end{array} \quad \begin{array}{r} 6.5 \\ 275 \end{array} \quad \begin{array}{r} 6.6 \\ 200 \end{array} \quad \begin{array}{r} 7.0 \\ 150 \end{array}$$

$$\begin{array}{r} 7.6 \\ 500 \end{array} \quad \begin{array}{r} 7.2 \\ 400 \end{array} \quad \begin{array}{r} 9.4 \\ 370 \end{array} \quad \begin{array}{r} 6.8 \\ 300 \end{array} \quad \begin{array}{r} 7.3 \\ 200 \end{array} \quad \begin{array}{r} 6.5 \\ 150 \end{array}$$



1

Fall of Rice Creek between County Road I & S.T.Hy. #8

Sta.	+	℥	-	Elev.
B.M.	1.22	882.84		881.62
0			10.1	872.74 I.
1			10.34	872.50
2			10.45	872.39
3			10.65	872.19
4			10.80	872.04
T.P.#1	3.71	881.16	5.39	877.45
7			9.20	871.96
9			9.20	871.96
T.P.#2	6.38	881.53	6.01	875.15
12			9.57	871.96
15			9.60	871.93
18			9.65	871.88
T.P.#3	7.26	884.06	4.83	876.70
21			12.20	871.86
24			12.20	871.86
26			12.20	871.86
T.P.#4	2.40	880.89	5.57	878.49
29			9.15	871.74
T.P.#4	4.93	880.90	5.42	875.47
33			8.76	871.65
36			8.75	871.65

Sta. 0 - E. Brady Co. Rd. I.
 going south.
 Elev. = top of water.

Sta.	+	T	-	Elev.
		880.40		
T.P.#5	484	879.85	5.39	875.01
39			8.20	871.65
42			8.30	871.55
45			8.30	871.55
T.P.#6	490	879.58	5.17	874.68
48			8.03	871.55
51			8.40	871.18
52			8.50	871.08
55			8.90	870.68
T.P.#7	5.75	879.76	5.57	874.01
58			9.40	870.36
64			10.00	869.76
67			10.30	869.46
68+40			10.80	869.26 STH.#8

Note: chaining follows the general meanderings of the creek.

①
Topography
Ent Lt. Sta 173
Co. Rd "J"

PROPOSED BRIDGE
STA. 173+00 LT.
Co. Rd. "J"

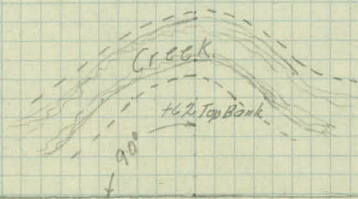
AT FAIR GROUNDS

8" I BEAMS - 24' L.G.

0+00 = Shoulder & Sta 172+00 on Lexington Ave.

Meadow

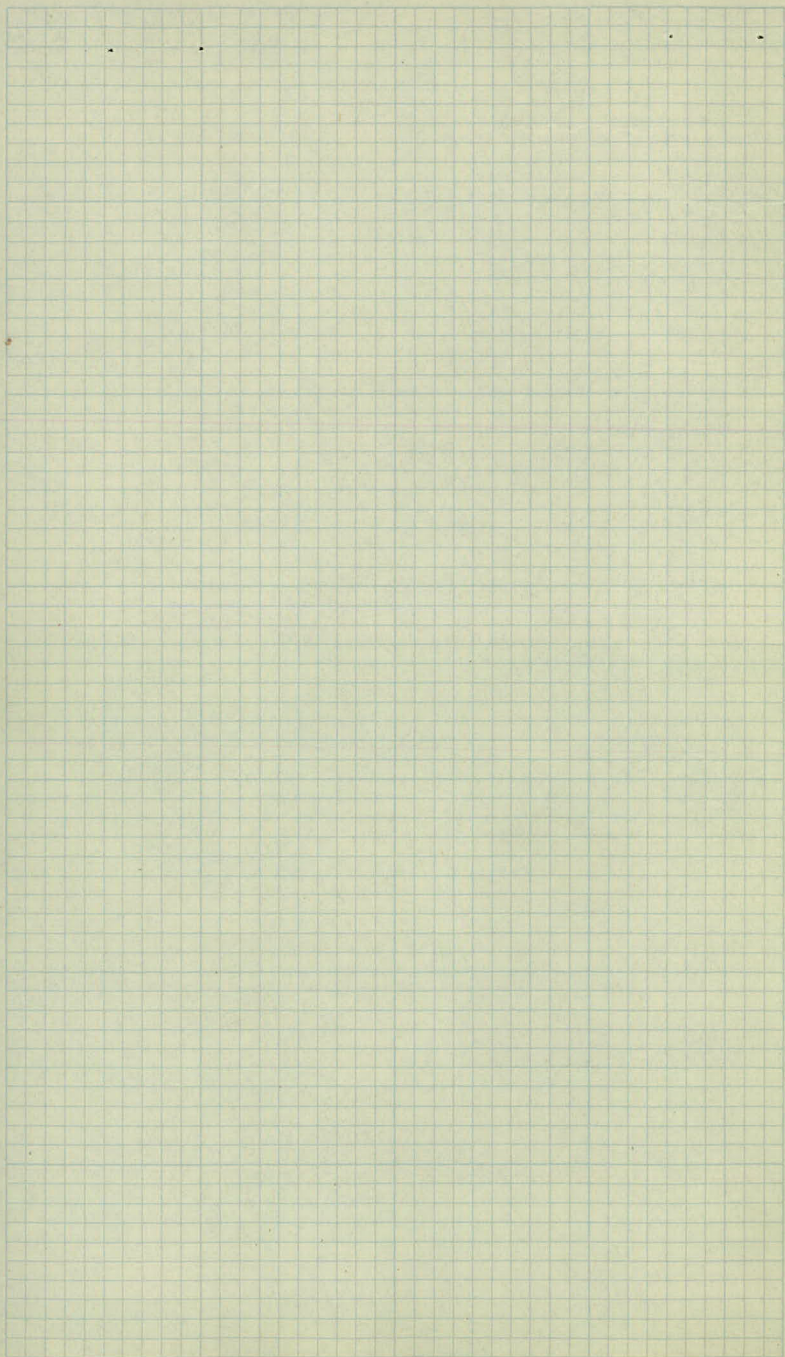
Top Bank 33'
Water 45'



+94 Top Bank
+91 Water's Edge
+70 Water's Edge

+50 Top Bank 20'
Water 35'

Co. Rd. "J"



X Sections

Ent Lit Sta 1734 00

0+00

+11

+50

+62

+70

+76

+87

+91

+99

1+00

51 Blue Top sta 173+00

$$\begin{array}{r} 10.0 \\ 15.0 \end{array}$$

$$\begin{array}{r} 9.5 \\ 15 \end{array}$$

$$\begin{array}{r} 9.5 \\ 15 \end{array}$$

$$\begin{array}{r} 9.5 \\ 15 \end{array}$$

$$\begin{array}{r} 9.3 \\ 15 \end{array}$$

$$\begin{array}{r} 10.0 \\ 15 \end{array}$$

$$\begin{array}{r} 10.6 \\ 15 \end{array}$$

$$\begin{array}{r} 10.2 \\ 15 \end{array}$$

$$\begin{array}{r} 11.4 \\ 15 \end{array}$$

$$\begin{array}{r} 11.7 \\ 15 \end{array}$$

$$\begin{array}{r} \text{Fair Water} \\ 11.4 \\ 15 \end{array}$$

$$\begin{array}{r} 11.8 \\ 15 \end{array}$$

$$\begin{array}{r} 12.3 \\ 15.0 \end{array}$$

$$\begin{array}{r} 12.2 \\ 15 \end{array}$$

$$\begin{array}{r} 12.4 \\ 15 \end{array}$$

$$\begin{array}{r} 12.0 \\ 15 \end{array}$$

$$\begin{array}{r} 12.0 \\ 15 \end{array}$$

$$\begin{array}{r} 12.0 \\ 15 \end{array}$$

Water

$$\begin{array}{r} 10.9 \\ 15 \end{array}$$

$$\begin{array}{r} 11.4 \\ 15 \end{array}$$

$$\begin{array}{r} 11.0 \\ 15 \end{array}$$

$$\begin{array}{r} 9.3 \\ 15 \end{array}$$

$$\begin{array}{r} 9.3 \\ 15 \end{array}$$

$$\begin{array}{r} 9.5 \\ 15 \end{array}$$

$$\begin{array}{r} 9.0 \\ 15 \end{array}$$

$$\begin{array}{r} 9.0 \\ 15 \end{array}$$

$$\begin{array}{r} 9.1 \\ 15 \end{array}$$

BM 1.66

Top
Mon.

232+82

Top Culvert

6.87

6.52

Ditch S. of Rd 6.5 on Muck

Ditch N. of Rd 6.65

21000.8

2776

~~988.67~~
~~18.7~~
~~4.87~~
~~5.3~~
~~1.6~~
888.67

~~70.7~~ 80'26.8
V55A
5.0
83.7
88.7
M of 2.1
156'506
V55A

555A 88.968
6.3
81.288
882.18
885

81.7
81.2
6.15 5.7
8.7
8.2

7.0
1.64
8.65



1
NORTH COUNTY LINE ROAD

Hamline to Lexington

Drainage

6 pages

44 3371

694

Alignment

To East.

0+00

N $\frac{1}{4}$ Cor. Sec. 3-30-22

FK
DS
TL

May 25, 1964

20

Elevations

Sta	+	x	-	Elev
BM		100.00		

0+00			7.58	92.42
------	--	--	------	-------

0+20			7.82	92.18
------	--	--	------	-------

6+90			10.03	89.97
------	--	--	-------	-------

6+90			9.65	90.35
------	--	--	------	-------

TP	4.50	99.88	4.62	95.38
----	------	-------	------	-------

8			4.03	95.85
---	--	--	------	-------

9			4.22	95.66
---	--	--	------	-------

10			4.49	95.39
----	--	--	------	-------

May 25, 1964

3

E End 15" Culvert Rt

W. End 15" Culvert Rt

N. End. " Culvert

S. End " Culvert

Sta 7 $\pm$

Sta	+	π	-	Elev.
		99.88		
11			4.14	95.74
12			3.85	96.03
13			3.89	95.99
14	4.22	100.17	3.93	95.95
15			4.27	95.90
16			4.31	95.86
17			4.38	95.79
+49.5			4.66	95.51
18			4.65	95.52

May 25, 1964

4

17150

6190

1060

91.68

7.79
N End

12" x 'C.M. Culu

NEW

7.49
S End

X - Sections
Sta + π - Elev

100.17

14

15

15

+50

16

17

+49.5

?

T.P.

3.81

99.87

4.11

96.06

✓

17+00

£

4.47

95.40

95.38

£

May 25, 1964

BT

5

95.95	95.77	95.07	93.67	93.87	93.57
4.22	4.4	5.1	6.5	6.3	6.6
	11	18	27	33	50

95.90	95.77	95.17	94.97	93.77	95.97	94.97
4.27	4.4	5.0	5.7	6.4	4.2	5.2
	11	20	22	27	33	50

95.77	95.67	94.87	94.17	99.17	98.17
4.4	4.5	5.3	6.0	1.0	2.0
	11	21	26	34	50

95.86	95.77	94.67	94.17	94.47	99.17	98.17
4.31	4.4	5.5	6.0	5.7	1.0	2.0
	11	22	24	27	33	50

95.79	95.67	93.57	93.17	93.37
4.39	4.5	6.6	7.0	6.8
	11	20	32	50

95.51	95.27	92.87	92.57	92.97	93.37
4.66	4.9	7.3	7.6	7.2	6.8
	11	19	29	32	50

Sta + π - Elev.

99.87

7

8

9

10

11

12

13

✓

May 25, 1964

RT

6

95.38	95.07	94.07	92.07	91.77
4.62	4.8	5.8	7.8	8.1
	11	21	25	50

95.85	95.57	95.27	92.67	92.47	93.27	93.17
4.03	4.3	4.6	7.2	7.4	6.6	6.7
	11	21	27	30	35	50

95.66	95.47	94.57	92.97	92.47	92.77
4.22	4.4	5.3	6.9	7.3	7.1
	11	23	27	33	50

95.39	95.27	95.47	92.67	92.77
4.49	4.6	4.4	7.2	7.1
	11	21	26	50

95.74	95.57	95.07	92.97	92.87
4.14	4.3	4.8	6.9	7.0
	11	20	27	50

96.03	95.77	95.27	93.77	93.57
3.85	4.1	4.6	6.1	6.3
	11	21	26	50

95.99	95.77	95.07	94.07	93.77	94.47	93.97
3.89	4.1	4.8	5.8	6.1	5.4	5.9
	11	19	22	30	32	50

