

Dr. 6-BK. 96

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plat Survey

COUNTY ROAD "B"

From W. B. Ave To E. Co. Line

Road Acc't. No. 15

Filed Jan. 1937 File K96D.6

8-11-36

①

ALIGNMENT

CO. RD. "B"

WHITE BEAR AVE. TO EAST CO. LINE

STA. PT. Δ LT. Δ RT.

2609.60 E
2609.95 W

498+48.55 MONT $0^{\circ}20'$

26013.60 E
26014.10

487+87.80 P.O.T

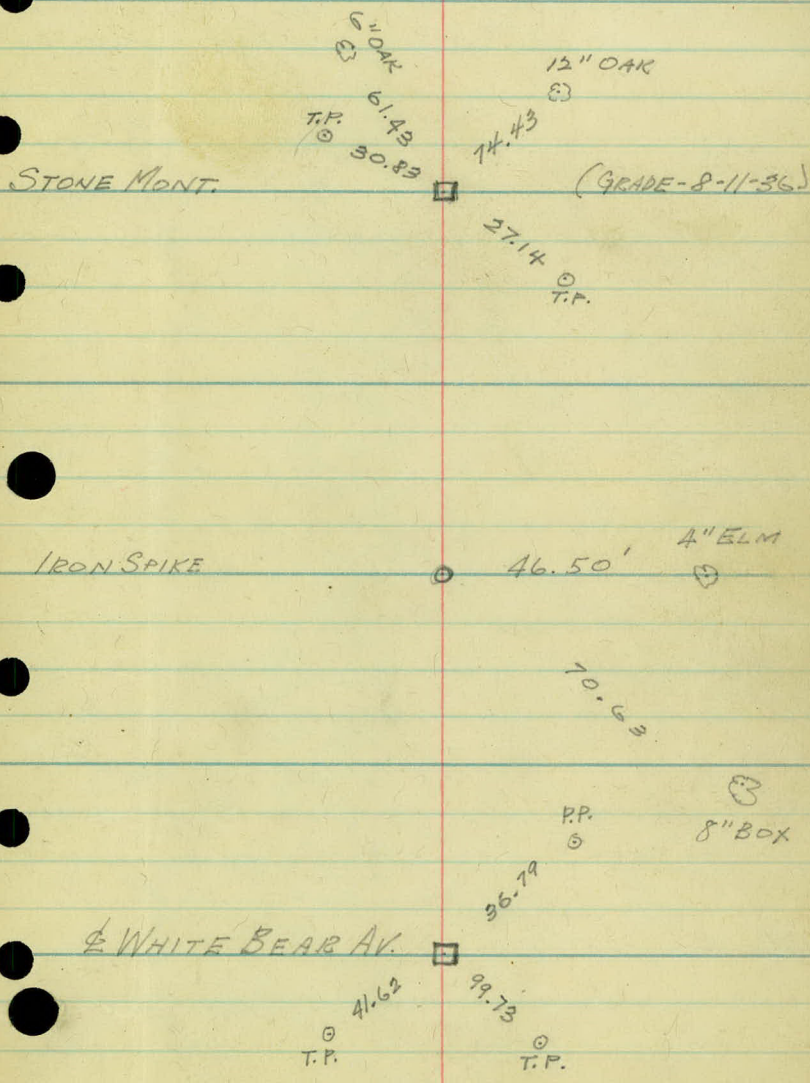
472+34.45 MONT

E PAVEMENT

{ GOLDBERG
GILLEN

T AWL
8-11-36

CLEAR & HOT - 95°
(2)



STA. PT. Δ LT. Δ RT.

538+96.52 P.O.T

2627.35 R
2627.80 M

530+97.10 P.O.T. ∇ N. ST. PAUL RD.

524+58.50 MONT. $0^{\circ} 39'$

GOLDBERG
GILLEN
MARK'S

7 A.W.L.

8-12-30

85°

CLOUDY & WARM

(3)

HOUSE

IRON SPIKE

HO.

POE. BRICK
FOUNDATION.

85.63

66.10

P.P.

37°21'

53.72

X IN PAVEMENT

N. 57° E. 1/2 P.
89.75
T.P.

T.P.

76.23

1" IRON BAR

(GRADE-8-12-30)

55.68

T.P.

STA. PT. Δ LT. Δ RT.

563+12.95 P.O.T.

2610.00 R.
2609.74 M

550+86.30 MONT. $0^{\circ}40'$

546+51.20 P.O.T.

④

24" OAK

③

40.15

47.02

③

NAIL IN TOP
OF STUMP
COR. OF HEDGE

IRON SPIKE

HYD. (TOP OF SHUTOFF)

○

38.52

STONE MONT.

(GRADE-8-12-36)

□

34.17

52.93

10" B.O.

③

18" W.O.

③

10" BOX ELDER

③

59.57

IRON SPIKE

○

52.55

18" BOX

③

STA. PT. ALT. DIST.

576+96.04 MONT EAST CO. LINE

5

HOUSE

T.P.
0

STONE MONT.

85.53

47.28

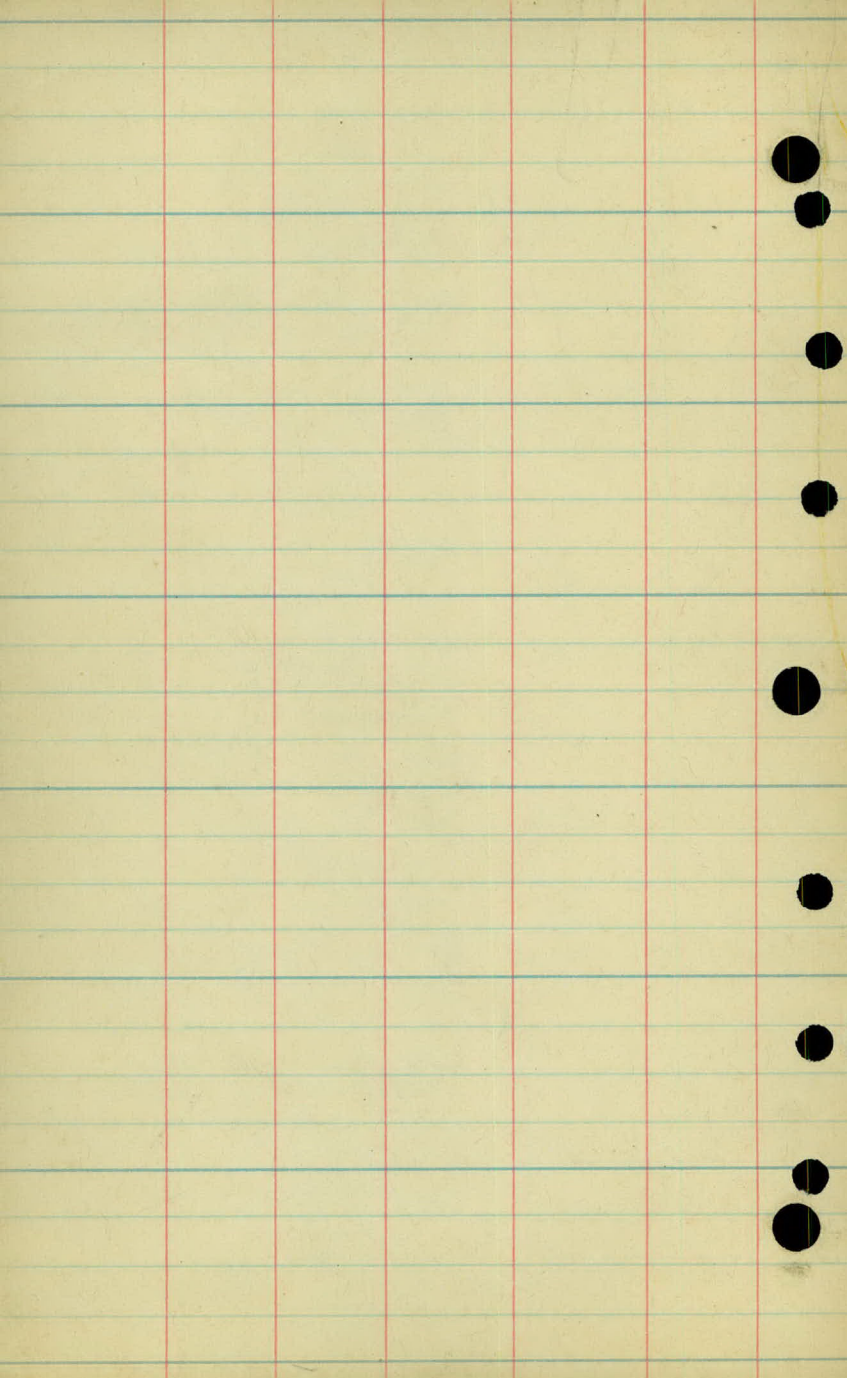
46.57

72.57

12" OAK

DOWN. 5'
(8/12/36)

HOUSE



D. L. Mink
7/28/36

(1)

TOPOGRAPHY

Co. Rd. "B"

White Bear Ave -

STA

77+34

~~5+00~~

76+34

~~4+00~~

End of Jack Oak & Hazel Brush

75+34

~~3+00~~

74+34

~~2+00~~

73+34

~~1+00~~

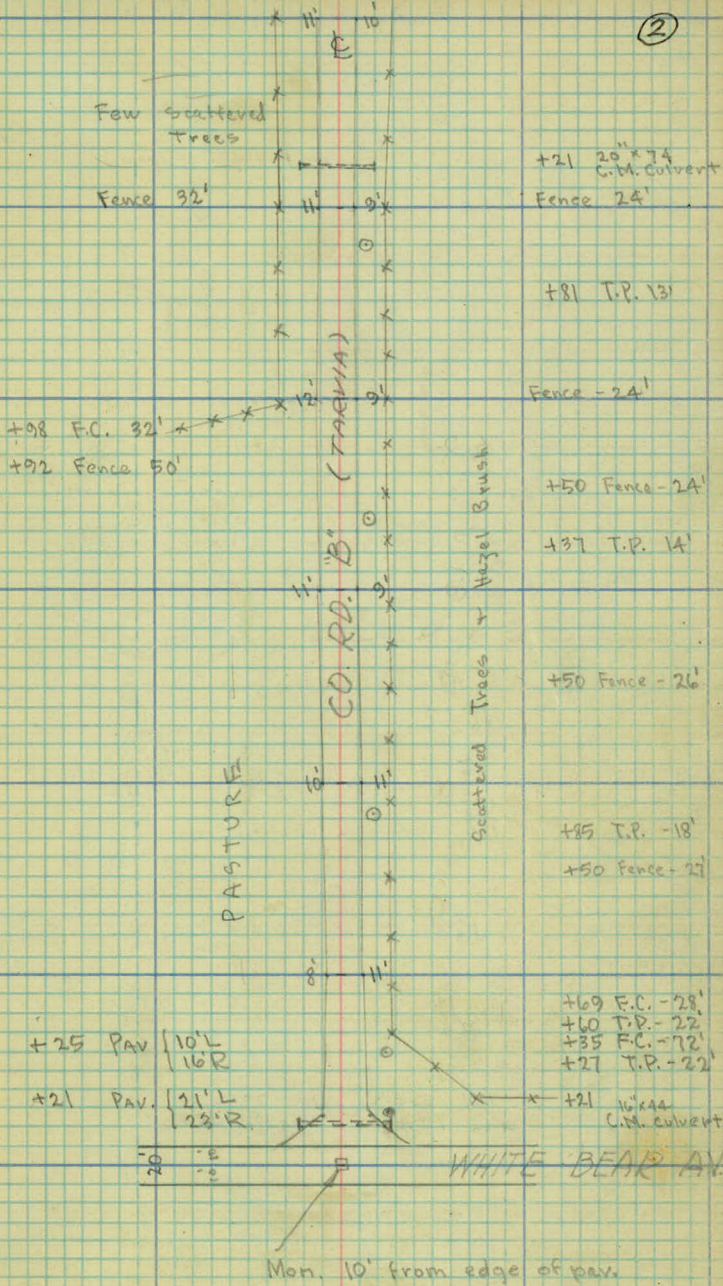
Begins Scattered Oaks & Hazel Brush on right

472+34

~~0+00~~

B.M. Top of Mon. Co. Rd. "B" & White Bear Av

El. 922.14



Danish Hedge goes back 47'
from E

84+34

~~12+00~~

+10 End of Woods on left

83+34

~~11+00~~

Ho 6 STEPS

82+34

~~10+00~~

81+34

~~9+00~~

Brush out 22' on left

80+34

~~8+00~~

79+34

~~7+00~~

Woods begins at F.C. on left.

478+34

~~6+00~~

+86 P.P.
 +10 2" Elm 32'
 +27 8" gravel road
 +12 Ho. Cor. 84'
 +15 End Hedge 21'
 +66 8" Oak 52'
 +58 6" Elm 30'
 +62 P.P. 16'
 +53 Bag. Danish Hedge
 Tarvia 9' 22'

+27 12" 20 C.N. Culvert

+89 End Hedge on left 21'
 +88 Box Elder 36'
 +85 Guy P. also Box E 13' 25'
 +50 T.P. 14'
 +38 Hedge on left 20'
 +62 T.P. 14'
 +44 4" B. Elder 24'
 +18, +39 2" Elms 29'
 +9 4" Box Elder 25'
 +5 3" Walk 18'
 Tarvia 10'
 +92 Ho. Cor. 14'
 +65 12" Cottonwood 60'
 +77, +58 2" Elm 29'
 +54 T.P. out 14'
 +38 2" Elm 29'
 +22 12" Driven 12'
 +22 12" 20 C.N. Culvert 17'

+98 6" Box Elder on Right 23'
 +97 2" Elm on Right 29'

CO. RD. B (790114)

Brush

HEAVY WOODED AREA

Brush

+2 14" Willow 31'

+43 End of Fence 29'

+17 T.P. 14'

Fence 31'

+35 15" 36 C.M. Culvert

Fence 36'

+91 T.P. 14'

Fence 35'

+68 3" OAK 39' 43' 48'

+55 8" OAK 32'
 +55 Fence Cor. 32'

+60 8" OAK 38'

+35 5" 16" OAK 40'

+52 Fence Cor. 35'

+35 Fence 32'

17 +00

88+84
+50

88+34
+6+00

87+84
+50

87+34
+5+00

+77

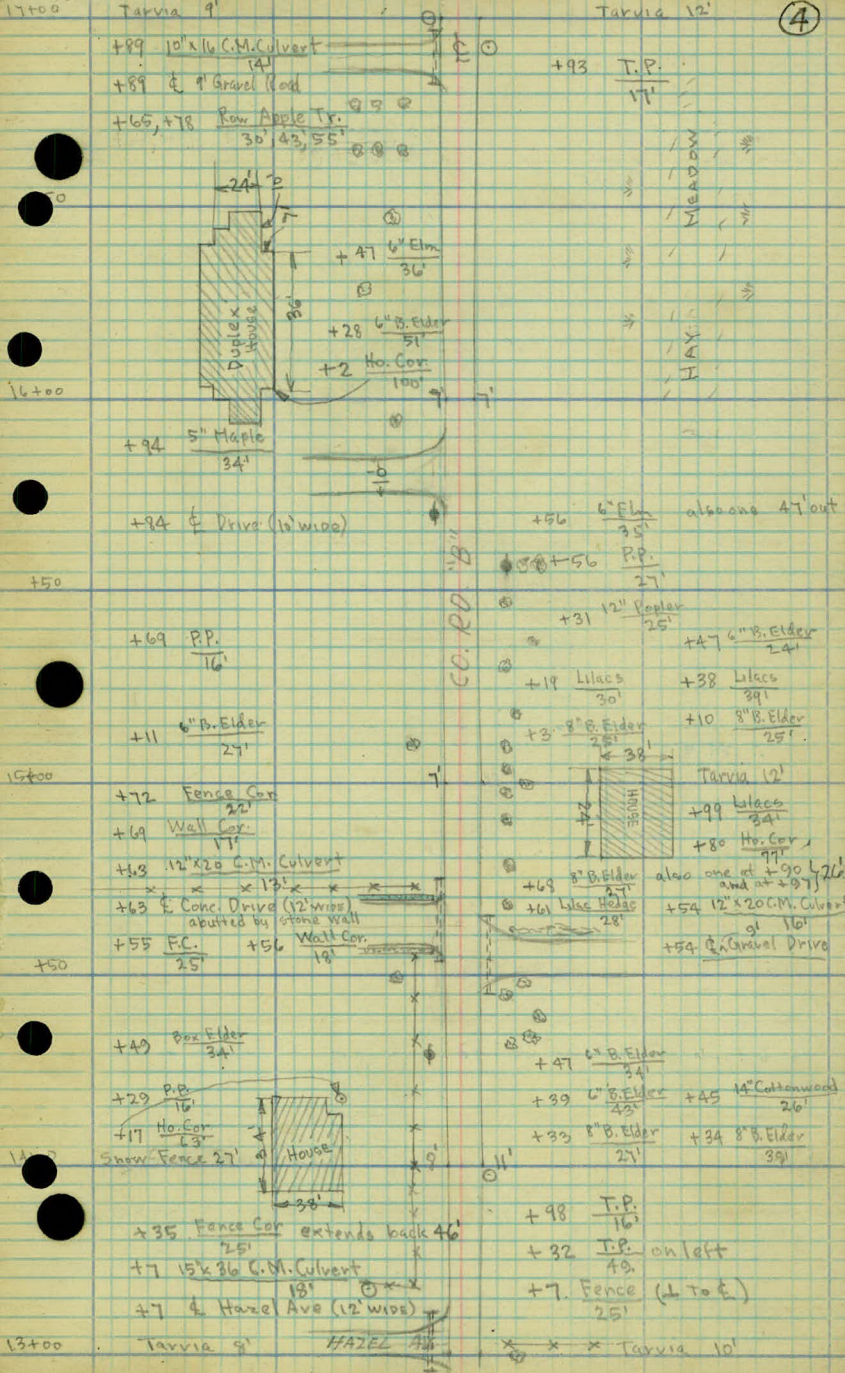
8" B. Elder on Rt.
27'

86+84
+50

86+34
+1+00

85+34
+2+00

6" B. Elder on right
29'



+85 End of Hedge
23'

492+84
-+50

+47 Eq. Like Hedge on Rt.
23'

492+34
20+00-

Apple Orchard directly in Back of Willows
on left

491+84
+50

+33 End of Cult. Field on Lt.

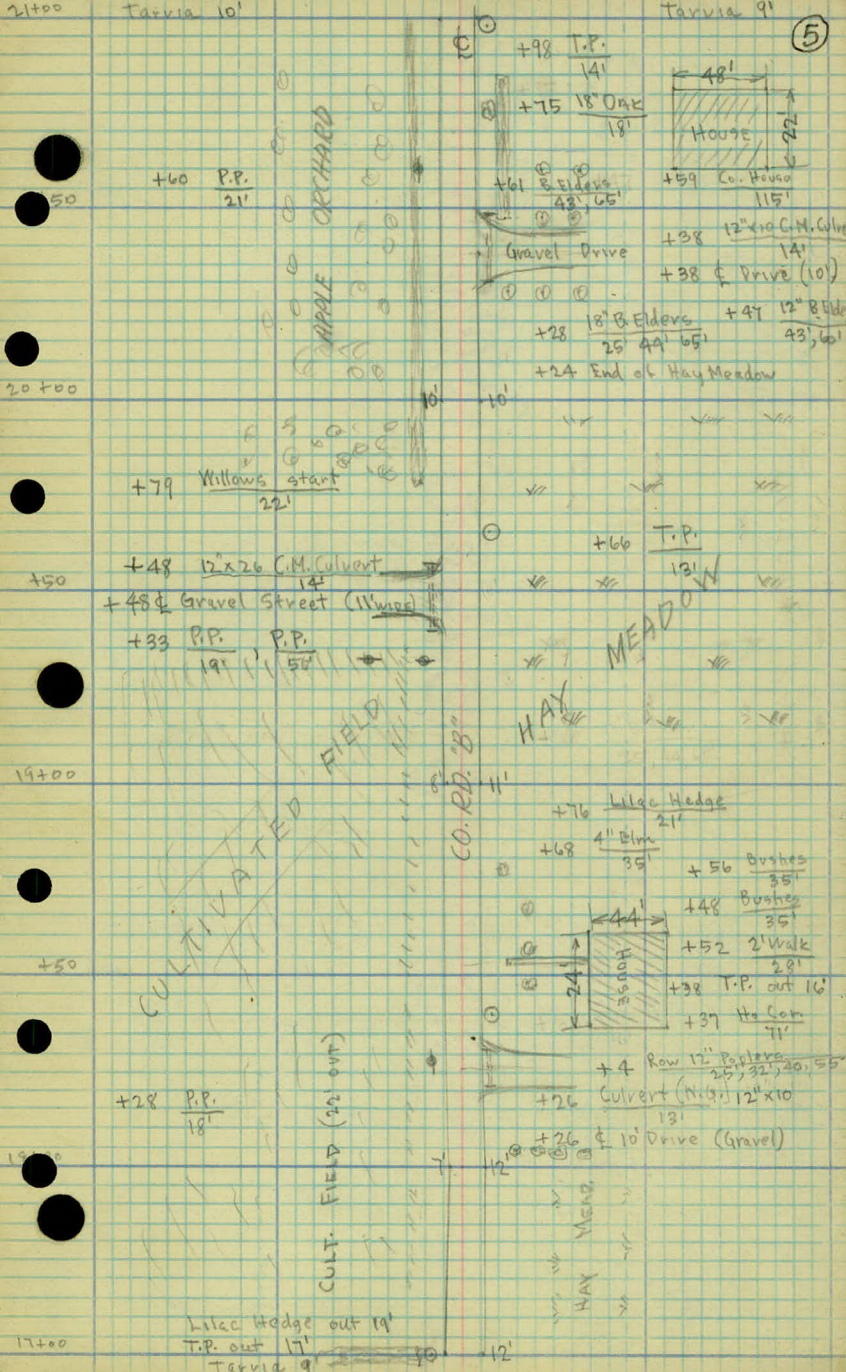
491+34
-19+00

490+84
-+50

Small Garage to rear of House

490+34
+19+00

489+34
17+00



498+34
26100

+20 Beg. Wooded Area on Lt.

497+34
25100

496+34
24100

495+34
23100

+89 $\frac{18" \text{ OAK}}{32'}$ on Lt.

494+34
22100

494+34
22100

+63 End of Apple Orchard

493+34
21100

Fence 32'

x 11' 9'

HEAVY WOODED

AREA

+29' T.P.
14'

Fence 32'

x 12' 8'

+76 P.P.
26'

+22 18" Oak
47'

x

Fence 31'

x 11' 8'

+42 F.C.
32'

+26 P.P.
26'

scattered trees

x

+73 16" Stump out 25'

+70 20" Oak
48'

+74 Fence Co.

+66 12" x 16 C.M. Culvert

15'

+66 9' Entrance

+53 6" Ash
23'

+49 18" Oak
65'

+33 6" Spruce
25'

+25 6" Spruce
27'

+43 Catopa
23'

+15 Road

12" x 20 C.M. Culvert

9' Gravel Road 15' Out

+69 P.P.
22'

+63 End of Willows

25'

MEADOW

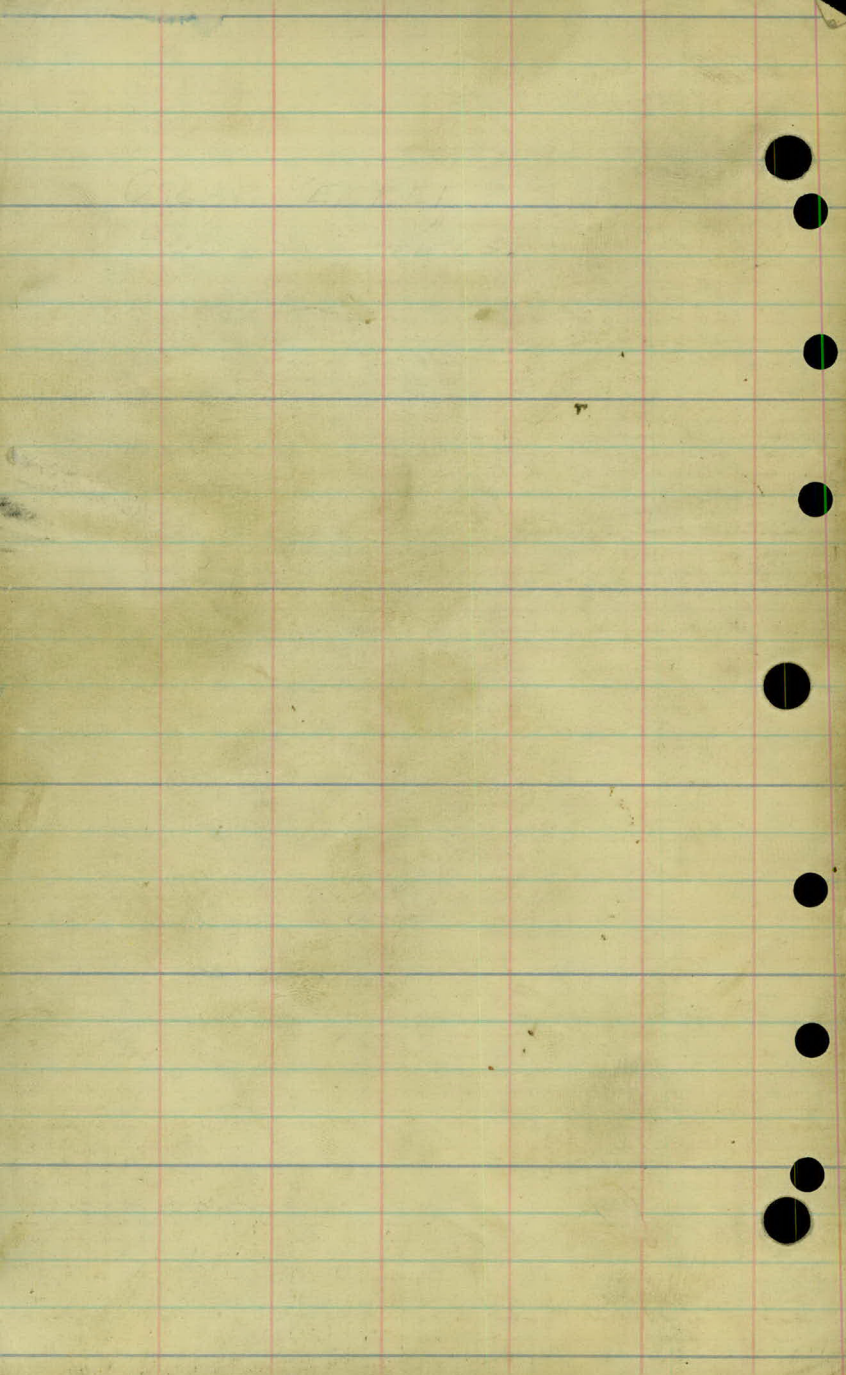
Scattered Trees

+77 T.P.
14'

MEADOW

+39 T.P.
14'

HAY

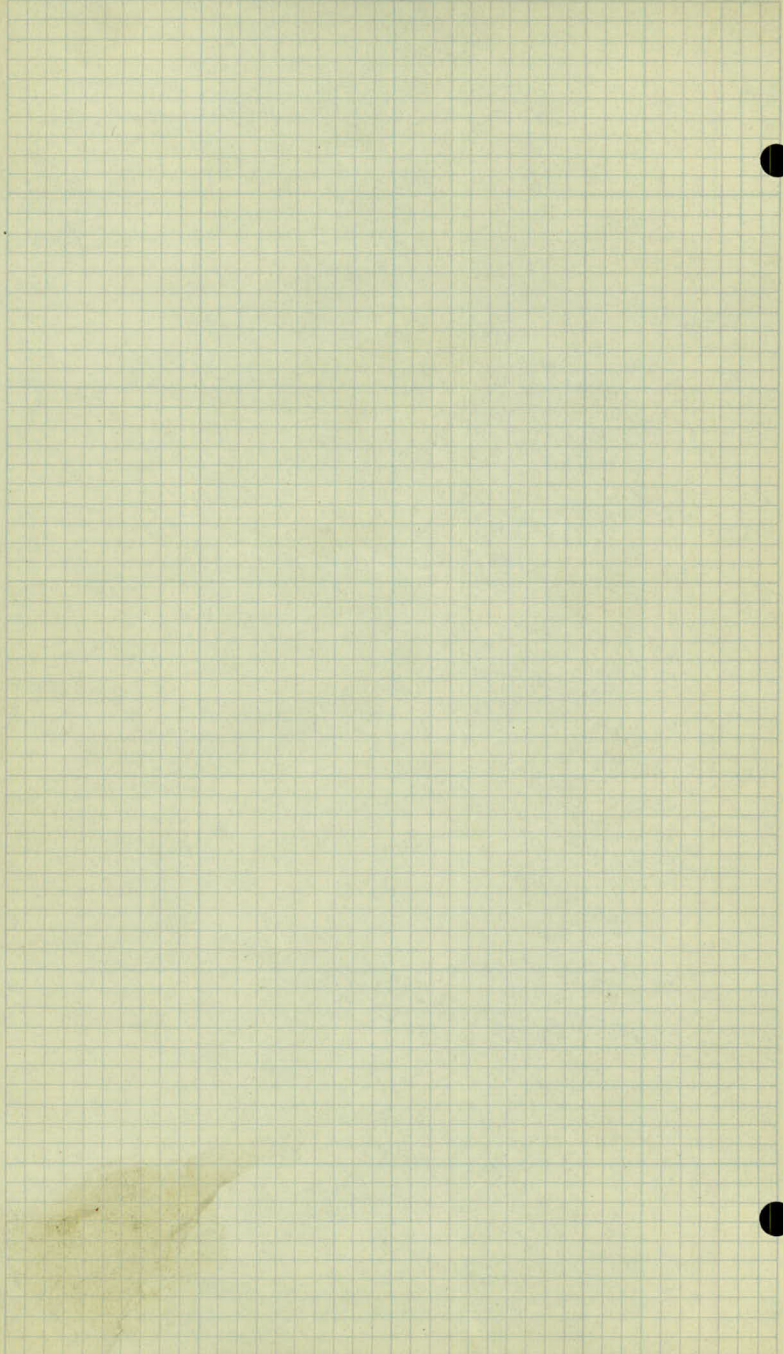


Alr Over
EM

Plans for County Rd "B"

W. H. Carlson.

892.76



Topography

Co. Road "B"

498 - 576

500

10 - 10

499

11 - 9.5

Tallia

498

11 - 9.5

$+98 = 2'' \text{ Eugreen } 25'$
 $+76 = \text{Ent } \frac{15' \times 20'}{17'} \text{ C.M. } 0.1$
 $+58 = \text{T.R } 14'$

 $+35 = 8'' \text{ Oak } 22'$
$$+12 = 8'' \text{ Oak } 24'$$

192 - T.P. 15.5

715

+69-T.P. 13'

26 = P.P. 26.5

F. 32.5

Timber

F- 32,5

+68-P.R 27

20/7

White Lead.

507

11 12

Taxvia

506

12-9

505



504

11-9

Taxvia

503

11-9

+ 83- $\frac{1}{2}$ 24' x 30' N.
Good-

16-14'

502

10-10

Taxvia

501

10-10

+39=PP-27 ✓

F 33'

Cultivated

+12 PP 27' X
F 33.5

+23=Guy Pole-27'
+18=F Corner 33'

+85=RR 27' X
+84=F Corner 33.5

+38=Guy Pole-18'

+12 sho.

+90 sho.

+82=T.P. 17.5'

F 33

+83=10" + rec 32

+58=T.P. 26

Timber

Waste land

+23=5" oak 27.5'
+14=8" oak 31'

+56=T.P. 16.5'

F 33

pot hole

+37=T.P. 16.5'

F 33

+86 PP 27.

+75=8" oak 26'
+66=8" oak 26'

pond

+48=10" oak 26'
+25=2" + rec 30'
+20=8" rec 24'
+17=T.P. 16.5'
+08=12" oak 29'
+03=10" oak 27'

514 +05. = 18" X 30' C.M.
Fait

Torvia
16' 10 9 14'

513

10 9.5

Torvia

512

10 10

511

9 11.5

Torvia

510

10 12

509

10 11

Torvia

508

10 11

+90 = P.P. 24'
T.P. 24'
OK

500-PR
-32'

+92 = P.P. 23' OK

+80 = T.P. 16

+39 = Ent

+86 = P.P. 24' OK

11

+93 = P.P. 17'
+86 = P.P. 24'

+43 = R.P. 24.6' OK
+33 = End Fence 32'

F. 33

waste land

F. 33' + 04 P.P. 25' OK
Meadow

F. 33'

lower

+70 = P.P. 27' OK

Cultivated

+18 = 12" oak 33'

Timber

+48 = 10" oak 28'

+53 = 8" oak 30'

+28 = 8" oak 30'

F. 33.5

+6 = Twin 8" oaks 29'

521

10 8

Taruia

520

10 8

519

9 8

Taruia

518

9 7

Taruia

+29 30"X 36' C.M.
Good

18' 18'

9 8

517

516

8 8'

Taruia

515

10' 6.5'

Pasture

F. 35'

F - 35'

+56 End Fence 25'



F - 24'

+95 ~~RP~~ 28' ~~Trolley~~ ~~RP~~ 12

F - 36'

+91 F. 23

Street car track

Bush

+35 F. car - 39'

+88 = F - 25

+83 = ~~RP~~ - 14
~~Trolley~~

+66 = F 25'

Swamp

Swamp

+85 = F - 26

528

9 10

527

10 18

tarvia

526

10.5 8

525

12 8

tarvia

524

11 8

+36 = 30" x 30" c.m.
0.15

15 15'

523

11 8.5

tarvia

522

11 9

+80 = Guy Pole - 19' 110 06

+70 = 12" oak 29'

+47 = 16" oak 34'
+35 = 16" oak 33'

+98 = Ent. 16" x 20' c.m.
+78 = T.P. 23 16' 95.
P.P. - mine!

+88 = 16" oak 28'
+68 = 16" oak - 33'

yard

P.P.
+67 = T.P. 21.5

+32 = P.P. 22' OK

+04 = Ent. 19'
8" wide

Cultivated

+90 = 2x5 Stone walk 14'

waste land

waste land

+93 = Ent. 28'
10' wide

+58.50 = Iron Pin

+07 = T.P. 23'

+83 = Ecor 33.5'

F 31.5

Pasture

F 30'

535

11 10

534

10 9

533

10 9

tarvia

532

10 11

+29 = 12" x 58 G.M.
Poor

34"

24'

531

530

7.5 11

tarvia

529

9 11

+80 = 14" oak 32'

+34 = 2-10" oak 20'

+15 = 1/2" oak 23'

+13 = 8" oak 29'

+89

+60 = 10-10" oak out 26'

+60

+47 = Ent 20'
14" wide

+12 = P.P. 30'

+98 = man hole 3.5

+61 = 6'x6' shed - 28'

+60 = Flow run bed - 19'

+42 F. 2-3

F-23'

+98 = F. cor 26'

To Ho.

+03 = P.P. 23'

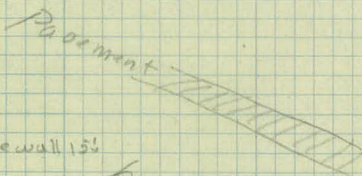
move

+68 = Ent - 23'
11" wide

ard
sh

ard
sh

W e a d o w



+12 = Edge Pavement

+80 = Stonewall 15'

+80 = Edge Pavement

7 1/2

4 0.0

Ho 5.7, P. 41

+32 = stone wall 15'

+24 = Ent 11.5' 12" x 20' C.M.
12 o.k.

+11 = T.P. 25' 41'
move

ard
sh
W e a d o w

+08 = T.P. 20'

542

10 9

541

10 8

Tarvia

540

10 10

539

13 9

Tarvia

538

11 8

488 = Int 2nd St NW.

537

11 9

Tarvia

536

10 9

yard

yard

yard

Waste

Cultivated

yard

yard

waste

Meadow

+98 = 8" Tree 33'
 +75 = 8" Tree 33'
 +60 = 10" Tree 33'
 +57 = P.P. - 25'
 +50 = 10" Tree 33'
 +37 = 10" Tree 33'
 +23 = 10" Tree 33'

+06 = 8" Box Elm 33' 10" x 26 c.m. Poor

+96 = Ent 10' 13' wide

+78 End Stone Wall 32

+38 = 4' steps 33

+18 Beg. Stone Wall 32'

+18 = P.P. 24'

+06 = 8" Oak 23'

+00 = 12" Oak 20'

+80 = 4' Conc. Walk steps 12'

+61 = 10" Oak 31'

+64 = 4' Conc. Wall 16'

+50 = End Conc. curb 17'

+43 = End Conc. curb - 24'

+39 = 8" Elm 26'

+00 = 6" Elm 25'

+84 = Ent 22' 21' wide

+59 = 10" Elm 24'

+17 = 4" Elm 24'

+91 = Hydrant 33'

+15 = 8" Oak 33

+06 = 14" Oak 32'

549

6 11

548

7 11

547

7 10

546

7 10

545

8 11

+40 = 18" X 44	Cim	Fair	14	25
+27 = Int. Q.	1st	St. N.W.		
+12 = 18" X 38	Cim		13'	25'
544	Fair		8	10

543

11 9

+85 = 16" Oak 22'
+70 = 16" Oak 26' - Corr. Fence

+96 = 18" Oak 26'
+88 = 4' wooden steps 18'

Pasture

Yard

+46 = 4" Elm 25'
+36 Cor Hedge.

Hedge 33'

+97 = 4" Birch 26'
+73 = 4" Birch 26'
+63 = Ent $\frac{12 \times 20}{12}$ c.m. good
+52 = 4" Birch - 26'
+41 = 4' step & walk 13'

+28 = 1" Tree 28'
+14 = Hedge - 33'
+12 = 3" Elm 26'

+96 = 2' Elm 26'

+63 = 2' Elm 26'
+50 = Stone steps 4' 13'

+35 = 3" Elm - 26'
+32 = Corr. Hedge 32'
+05 = 6" Elm 26'
Hedge 32'

+71 = 8" Elm 26'

+39 = 4" Elm 26'

+10 = 4" Elm 26'
Hedge - 33'

+79 = 12" Elm 26'
+62 Hydrant 19'
+55 Beg in Hedge 32'
+53 = 4' wall 15'
+48 = P.P. 26'

+93 = F. Cor. 33'

+50 = F. Cor. 33'

Cultivated

Yard

+26 = P.P. 22'

+82 = 3" Box Elder 28'

+66 = 4" Oak 25'

+46 = Ent $\frac{12 \times 20}{16}$ c.m. good

+29 = 4" Elm 26'

+11 = 5" Elm 25'

+74 = P.P. 29'

+36 = 4" Poplar 28'
+27 = Ent $\frac{10 \times 16}{14}$ c.m. good

+55 = P.P. - 28'

+36 = 2' Cont wall 26'
+16 = water shut off 25'
+ Ent $\frac{10 \times 16}{17}$ c.m. Fair

+02 = P.P. 26'

+53 = 4' walk 18'

+04 = P.P. 26'
+93 = 8" Tree 38'
+93 = 12" Tree 33'
+65 = 10" Tree 33'
+47 = 10" Tree 33'
+36 = 10" Tree 33'
+28 = 10" Tree 33'

556

13 5

555

12 6

554

11 8

553

9 9

+40 = 30" X 34' C.M.
Good.

15 19

552

8 11

551

8 10

550

7 9

+72 = 10" oak 29'

+55 = RA 25' *gray Rd*
Model.

+32 = E corner 29'

F. 28'

E. corner 16" oak 29'

+50 = 16" oak 28'

F. 20'

F. 15'

+78 = 12" oak 32'

F. 18'

+98 = 15" oak 34'
1724'

F. 25'

F. 23'

F. 24'

F. 24'

F. 24'

+74 = 14" oak 28'
+61 = 16" oak 24'

+27 = 14" oak 19'
F. 24'

+18 = Hydrant 19'

F. 27'

+84 = E corner 27'

+84 = R.P. 20'

+40 = 18" oak 28'
+32 = Ent 15" x 16" C.M.
17' good

+21 = 14" oak 27'

563

14 7

562

12 7

561

14 7

560

13 5

559

15 5

558

14 5

+55 = intersection Margaret St N12

557

13 4

✓ Vacant

+79 = Ent $\frac{12'' \times 20'}{13}$ C.M. Good

Garden

+56 = 3' Bulk 20'
+42 = 20" Oak 31'

~~P.P. 17' gone~~

+86 = Ent $\frac{10'' \times 42'}{13}$ C.M. Full

+58 = Cone. steps 17'

Orchard

+21 = Cor. Hedge 30'

~~+71 = P.P. 15' gone~~

Garden

~~+50 = P.P. 17' gone~~

+21 = 2" tree 29'

+05 = Ent 30' 10' wide

+95 = Hedge 36

+36 = 12" maple 33'

Hedge 36

+94 = 18" maple 33'

+47 = 18" maple 34'

+67 = Ent 19'

10' wide

+27 = 8" apple tree 34'

Cor. Hedge 34'

+13 = Ent $\frac{12'' \times 20'}{15}$ C.M. Poor

Cor. Hedge 33'

+91 = 6" Elm 26'

+44 = 3" Elm 25'

+61 = Cor. Hedge 33'

~~+25 = P.P. 17' gone~~

Cor. Hedge 33'

$\frac{12'' \times 20'}{13}$ C.M. Good

+83 = Ent 13'

+73 = 8" Elm 25'

+50 = 4" Elm 26'

+45 = Corner Hedge 33'

+38 = 2" evergreen 25'

+90 = End Hedge 29'

+74 = P.P. 27'

+55 = $\frac{16'' \times 44'}{15}$ Poor C.M.

+31 = P.P. 19' ~~Missing~~

+27 = 10" Oak 27'

14" Oak 28'

✓ Vacant

+89 = Hydrant 20'

+84 = 4.5' walk 19'

#83 = St Intersection to Lt.

#41 = St. Intersection to Rt.

570 11 8

569 8 8

568 9 10

567 8 11

566 10 9

565 11 8

#42 = Intersection To West Charles St. NE

564 11 8

+70 = Cut Hedge 28'

+55 = RR 20 *move*

+36 = 12" oak 22'

+27 = 16" oak 20

~~+20 = A.P. 19~~ *gone*
~~+16 = T.P. 18~~ *gone*
~~+16 = 9" wide~~ *move*

+70 = 8 oak 17'

+60 = 16" oak 15'

Orchard cultivated

+88 = 10" oak 20'

+70 = 2-12" oaks 22'

+61 = 12" oak 17'

+53 = 18" oak 15'

+11 = Twin 10" oak 16'

Cultivated

~~RR 19~~ *gone*
~~+93 = T.P. 11~~

+40 = Ent 15' wide

+22 = 16" oak 26'

+16 = 10" oak 28'

+08 = 2-8" oaks 23' F. corner
F. 23

~~+40 = A.P. 18~~ *gone*
~~+63 = T.P. 17~~ *gone*

+31 = 10" oak 30'

Pasture

+20 = 10" oak 25'

+08 = 6" twin oaks 25'

F. 25

+91 = 14" oak F. corner 25'

+81 = 8" oak 23'

+73 = 18" oak 23'

+59 = 8" oak 25'

~~RR 19~~ *gone*
~~+45 = 8" oak 24'~~

+20 = Ent 16' 16' wide

Hazel Brush

+62 = Hydrant 34'

+65 = 5' steps 22'

~~+42 = A.P. 18~~ *gone*

~~+16 = T.P. 17~~ *gone*

576

10 11

575

9 12

574

9 10

+14 = 18" X 30'

G.M.
Fair

15 15
8 9

573

572

9 8

571

10 7

+74 = P.P. 26' - ~~Meadow~~
 +74 = T.P. 24' - ~~Meadow~~
 +54 = 1" E/m 28'

+25 = 2" E/m 28'

+09 = 2" E/m 28'

+93 = 2" E/m 28'

+80 = 2" E/m 28'

Yard

+67 = Ent. 10' wide

+37 = Cor. Fence 27'

+21 = R.P. 23' ~~move.~~

F. 27'

~~T.P. + R.P.~~

+03 = ~~R.P.~~ 22' ~~move.~~
 F. 26'

Cultivated

Meadow

+30 = 3" tree 28'

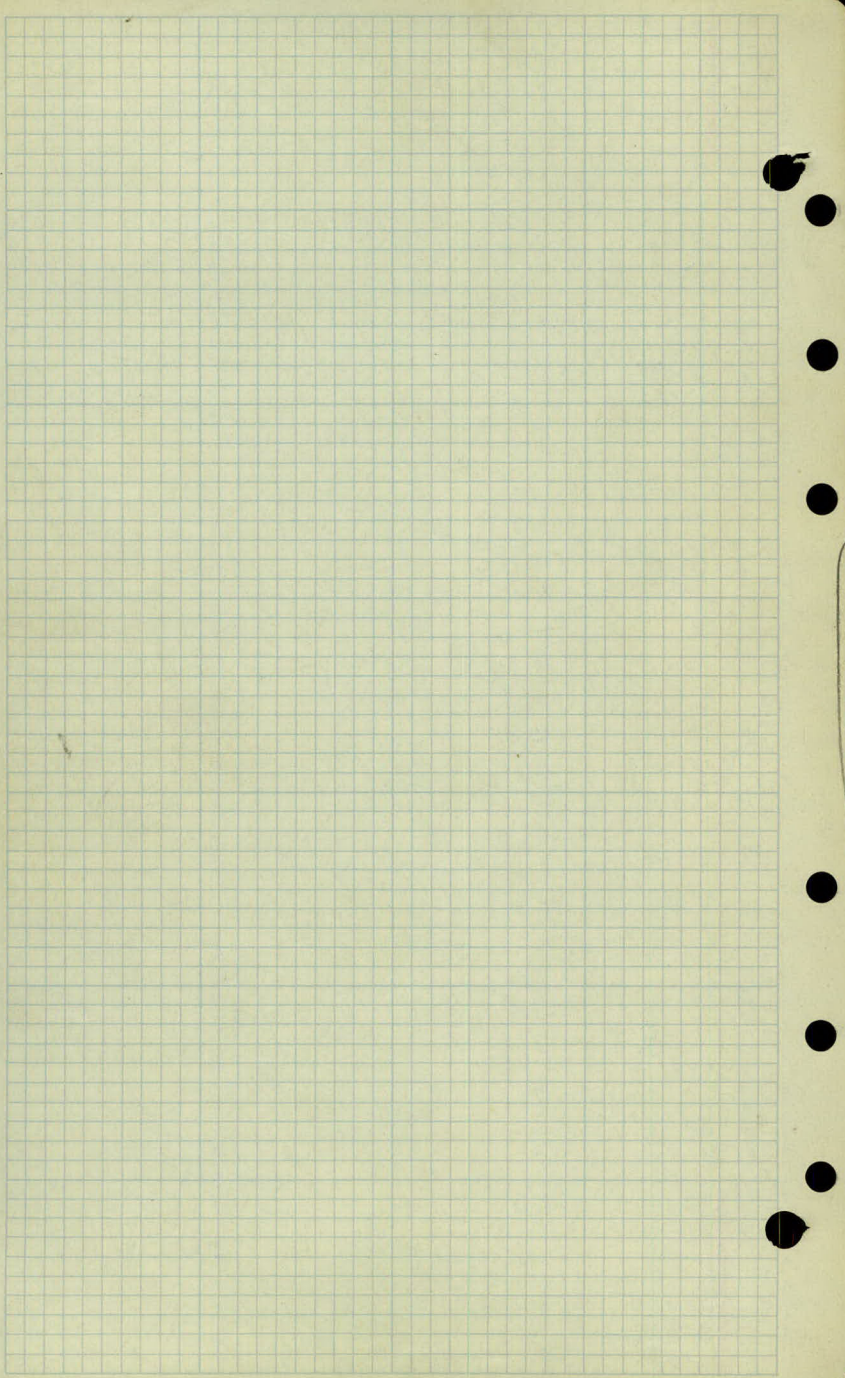
F. 24'

+82 = T.P. 21' ~~move.~~

Yard

+91 = F. Cox. 26'

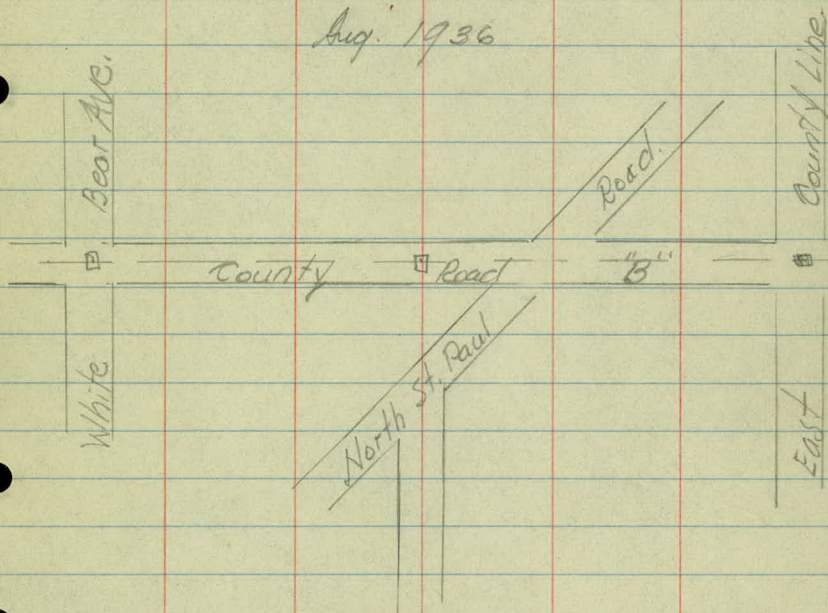
+75 = Ent. 12 x 16
 +65 = T.P. 20' 17' P.O.
 +54 = R.A. 20' ~~move.~~



Cross-Sections.
County Road "B"

White Bear to E. Co. Line.

Aug. 1936



Sta.	+	π	-	Elev.
	7.07	929.21 ✓		922.14

4/72 + 34.45

11

922.14-

+44.45 E. edge Pav.

22.06-

+56

22.5-

+67

22.7-

4/73

23.3-

+50

24.0-

4/74

24.5-

+40

24.6-

+70

24.5-

4/75

24.0-

Aug. 21, 1936

2

W.H.C.

L.B.H.

A.M.

M.G.

H.B. R.

L

L

Top Mon Co. Rd. B & White Bear Ave

Mon L White Bear Rd.

$\frac{6.1}{50}$

7.07

$\frac{8.3}{50}$

$\frac{6.2}{50}$

$\frac{7.15}{50}$

$\frac{8.4}{50}$

$\frac{7.5}{50}$	$\frac{8.7}{21}$	$\frac{7.5}{20}$	$\frac{6.7}{50}$	$\frac{7.8}{19}$	$\frac{8.3}{23}$	$\frac{9.3}{24}$	$\frac{9.8}{50}$
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$\frac{2.5}{50}$	$\frac{2.3}{41}$	$\frac{5.3}{26}$	$\frac{6.4}{14}$	$\frac{6.9}{13}$	$\frac{6.5}{50}$	$\frac{7.7}{17}$	$\frac{5.5}{22}$	$\frac{7.1}{35}$	$\frac{7.7}{50}$
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$\frac{8.8}{50}$	$\frac{8.2}{29}$	$\frac{6.9}{22}$	$\frac{6.2}{7}$	$\frac{5.9}{50}$	$\frac{6.4}{13}$	$\frac{6.9}{17}$	$\frac{6.3}{20}$	$\frac{4.6}{22}$	$\frac{4.8}{50}$
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$\frac{9.8}{50}$	$\frac{8.0}{24}$	$\frac{7.0}{21}$	$\frac{5.6}{8}$	$\frac{5.2}{50}$	$\frac{5.7}{11}$	$\frac{6.7}{15}$	$\frac{5.4}{17}$	$\frac{6.6}{40}$	$\frac{7.3}{50}$
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$\frac{5.5}{33}$	$\frac{4.7}{18}$	$\frac{5.5}{14}$	$\frac{5.1}{9}$	$\frac{4.7}{50}$	$\frac{5.1}{11}$	$\frac{5.7}{16}$	$\frac{3.5}{21}$	$\frac{4.1}{33}$	$\frac{5.7}{50}$
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$\frac{4.8}{33}$	$\frac{2.7}{19}$	$\frac{5.5}{15}$	$\frac{5.1}{10}$	$\frac{4.6}{50}$	$\frac{5.1}{11}$	$\frac{5.5}{15}$	$\frac{3.0}{21}$	$\frac{4.5}{38}$
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$\frac{1.3}{33}$	$\frac{0.6}{20}$	$\frac{5.4}{15}$	$\frac{5.1}{10}$	$\frac{4.7}{50}$	$\frac{5.1}{10}$	$\frac{5.1}{16}$	$\frac{2.4}{20}$	$\frac{4.5}{33}$	$\frac{6.0}{45}$
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$\frac{1.3}{33}$	$\frac{0.6}{23}$	$\frac{6.0}{18}$	$\frac{5.6}{10}$	$\frac{5.2}{50}$	$\frac{5.8}{10}$	$\frac{6.1}{15}$	$\frac{5.0}{17}$	$\frac{6.9}{35}$
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Sta.	+	✓ T	-	Elev.
		929.21		
475+30				923.1 -
+60				21.9 -
476+0				20.9 -
+50				20.8 -
477				21.0 -
+50				21.6 -
478				23.0 -
+55		✓		24.8 -
T.P.	11.73	939.63	131	✓ 927.90
479				26.9 -
+50				29.8 -
479+80				31.2 -

$\frac{1.0}{33}$	$\frac{26}{27}$	$\frac{68}{18}$	$\frac{62}{11}$	$\frac{61}{-}$	$\frac{68}{9}$	$\frac{7.5}{14}$	$\frac{10.5}{20}$	$\frac{13.1}{33}$
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$\frac{2.1}{40}$	$\frac{5.1}{30}$	$\frac{6.6}{23}$	$\frac{7.8}{16}$	$\frac{7.3}{10}$	$\frac{8.0}{9}$	$\frac{8.6}{12}$	$\frac{13.8}{22}$	$\frac{15.1}{33}$
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$\frac{2.8}{33}$	$\frac{3.6}{28}$	$\frac{82}{19}$	$\frac{93}{76}$	$\frac{84}{11}$	$\frac{8.3}{9}$	$\frac{8.8}{9}$	$\frac{13.7}{23}$	$\frac{14.8}{33}$
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7.2	9.0	10.5	10.3	8.5	8.4	9.1	10.9	9.6	9.9
9.3	7.6	2.3	1.7	1.2	1.3	1.6	2.0	3.3	

139	127	912	84	<u>82</u>	89	133	145
<u>33</u>	<u>21</u>	<u>16</u>	<u>12</u>		<u>12</u>	<u>21</u>	<u>33</u>

15.0	13.8	9.4	7.7	7.6	8.0	8.6	17.3	18.0
33	28	19	12		9	16	28	33

$\frac{11.5}{33}$	$\frac{10.2}{25}$	$\frac{7.5}{21}$	$\frac{6.5}{12}$	$\frac{6.2}{9}$	$\frac{6.6}{9}$	$\frac{7.3}{14}$	$\frac{18.1}{33}$	$\frac{20.0}{40}$
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$\frac{63}{33}$	$\frac{51}{22}$	$\frac{46}{12}$	$\frac{44}{1}$	$\frac{47}{10}$	$\frac{54}{16}$	$\frac{153}{33}$	$\frac{170}{50}$
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Nail in T.P. Rt. Sta. 479

$\frac{9.2}{35}$	$\frac{9.0}{23}$	$\frac{13.0}{16}$	$\frac{13.1}{11}$	$\frac{12.7}{10}$	$\frac{13.1}{10}$	$\frac{13.5}{10}$	$\frac{11.2}{21}$	$\frac{15.2}{32}$
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(7.50) (46.0) 8.7 10.5 10.3 9.8 10.2 10.4 41.7 1.0
50 43 73 14 10 11 17 34 40

$$\left(\begin{array}{cccccccccc} +108 & -108 & 3.1 & 8.1 & 8.8 & 24 & 8.8 & 8.8 & 3.0 & +46 & +3.0 \\ 50 & 37 & 26 & 16 & 10 & & 10 & 16 & 27 & 26 & 50 \end{array} \right)$$

Sta	+	π	-	Elev.
		939.63 [✓]		
480+20				32.8-
480+40				33.5-
481+0				35.6-
T.P.	12.73	950.56 [✓]	1.80.	937.83 [✓]
+50				37.9-
482				40.4-
+40				42.8-
483				46.4-
T.P.	12.47	962.06 [✓]	0.97	949.59 [✓]
+50				49.6-
484				52.7-
+50				55.8-
485				58.8-
+25				60.6-

4.

E

Rt.

Aug. 24, 1926⁴
Net.

$\frac{4.5}{33}$	$\frac{7.2}{19}$	$\frac{7.1}{10}$	$\frac{6.8}{-}$	$\frac{7.2}{10}$	$\frac{7.7}{15}$	$\frac{10.1}{25}$	$\frac{10.6}{33}$
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$\frac{9.0}{33}$	$\frac{8.9}{20}$	$\frac{7.2}{16}$	$\frac{6.4}{10}$	$\frac{6.1}{-}$	$\frac{6.5}{9}$	$\frac{7.1}{16}$	$\frac{12.0}{23}$	$\frac{13.4}{33}$
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$\frac{8.0}{33}$	$\frac{7.6}{20}$	$\frac{5.6}{16}$	$\frac{4.3}{9}$	$\frac{4.0}{-}$	$\frac{4.8}{8}$	$\frac{4.9}{12}$	$\frac{8.6}{19}$	$\frac{10.6}{33}$
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$\frac{17.0}{33}$	$\frac{16.1}{19}$	$\frac{14.0}{16}$	$\frac{13.1}{11}$	$\frac{12.7}{-}$	$\frac{13.2}{8}$	$\frac{14.4}{15}$	$\frac{16.7}{20}$	$\frac{18.0}{33}$
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$\frac{13.5}{33}$	$\frac{11.2}{19}$	$\frac{10.6}{11}$	$\frac{10.2}{-}$	$\frac{10.6}{10}$	$\frac{11.3}{17}$	$\frac{8.5}{23}$	$\frac{8.1}{33}$
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$\frac{7.9}{33}$	$\frac{7.9}{17}$	$\frac{9.2}{16}$	$\frac{8.2}{9}$	$\frac{7.8}{-}$	$\frac{8.2}{10}$	$\frac{8.8}{17}$	$\frac{5.5}{21}$	$\frac{4.6}{33}$
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$\frac{3.8}{33}$	$\frac{3.2}{18}$	$\frac{4.9}{16}$	$\frac{4.4}{9}$	$\frac{4.2}{-}$	$\frac{4.6}{10}$	$\frac{4.8}{16}$	$\frac{3.0}{21}$	$\frac{2.6}{33}$
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Yard.

$\frac{10.4}{33}$	$\frac{9.8}{23}$	$\frac{14.0}{18}$	$\frac{13.2}{15}$	$\frac{18.4}{12}$	$\frac{12.9}{9}$	$\frac{12.5}{-}$	$\frac{13.1}{10}$	$\frac{13.6}{16}$	$\frac{12.7}{19}$	$\frac{12.6}{33}$
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Yard.

$\frac{7.7}{33}$	$\frac{7.7}{21}$	$\frac{11.4}{16}$	$\frac{10.0}{14}$	$\frac{10.0}{8}$	$\frac{9.4}{-}$	$\frac{9.9}{11}$	$\frac{10.4}{16}$	$\frac{10.2}{19}$	$\frac{12.0}{33}$
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$\frac{6.1}{33}$	$\frac{6.1}{20}$	$\frac{7.5}{16}$	$\frac{6.7}{12}$	$\frac{7.1}{11}$	$\frac{6.7}{8}$	$\frac{6.3}{-}$	$\frac{6.8}{9}$	$\frac{7.4}{13}$	$\frac{8.8}{17}$	$\frac{9.8}{33}$
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$\frac{3.4}{33}$	$\frac{3.4}{19}$	$\frac{5.2}{17}$	$\frac{3.7}{14}$	$\frac{3.8}{9}$	$\frac{3.3}{-}$	$\frac{3.7}{10}$	$\frac{4.3}{14}$	$\frac{6.7}{19}$	$\frac{7.7}{33}$
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$\frac{0.0}{33}$	$\frac{1.2}{17}$	$\frac{1.9}{14}$	$\frac{1.9}{9}$	$\frac{1.5}{-}$	$\frac{2.0}{13}$	$\frac{3.1}{17}$	$\frac{4.9}{33}$
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Sta.	+	π ✓	-	Elev
T.P.		962.06	0.57	✓ 961.49
	13.21	974.70	0.57	

485+65 63.6-

486+00 66.5-

+50		✓		70.2-
T.P.	7.54	980.47	1.77	✓ 972.93
486+97				72.8-

487+10 73.5-

+50 75.4-

✓ 88 76.3-

+50 75.6-

489		✓		74.9-
13.21	5.84	980.47	5.84	✓ 974.63

Lt.

E

Rt.

5

$\frac{8.8}{33}$	$\frac{9.5}{20}$	$\frac{12.5}{16}$	$\frac{11.4}{7}$	$\frac{11.1}{-}$	$\frac{11.6}{11}$	$\frac{12.3}{17}$	$\frac{11.1}{20}$	$\frac{11.9}{33}$
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$\frac{3.8}{33}$	$\frac{4.2}{24}$	$\frac{8.4}{16}$	$\frac{8.6}{8}$	$\frac{8.2}{-}$	$\frac{8.8}{11}$	$\frac{9.4}{17}$	$\frac{6.3}{24}$	$\frac{6.6}{33}$
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Yard.	$\frac{1.5}{50}$	$\frac{1.5}{20}$	$\frac{5.0}{15}$	$\frac{4.7}{6}$	$\frac{4.5}{-}$	$\frac{5.2}{13}$	$\frac{5.8}{18}$	$\frac{1.7}{25}$	$\frac{2.4}{33}$
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17.9	75.8	73.0	72.62	72.8				
$\frac{7.6}{50}$	$\frac{4.7}{20}$	$\frac{7.5}{15}$	$\frac{7.85}{6.5}$	$\frac{7.7}{-}$	$\frac{8.2}{12}$	$\frac{8.9}{18}$	$\frac{7.5}{21}$	$\frac{7.6}{33}$

← Conc. Drive →



13	26	4.9	6.9	7.6	7.2	7.0	7.5	8.1	6.8	7.5
33	21	18	17	12	10	-	12	17	20	33

Yard.

$\frac{1.03}{33}$	$\frac{0.0}{22}$	$\frac{5.4}{15}$	$\frac{5.2}{7}$	$\frac{5.1}{-}$	$\frac{5.6}{11}$	$\frac{6.0}{17}$	$\frac{4.2}{20}$	$\frac{5.8}{33}$
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$\frac{1.05}{33}$	$\frac{0.0}{21}$	$\frac{4.0}{16}$	$\frac{4.2}{7}$	$\frac{4.2}{-}$	$\frac{5.1}{13}$	$\frac{5.3}{18}$	$\frac{3.7}{21}$	$\frac{4.2}{33}$
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Yard

$\frac{0.2}{33}$	$\frac{1.6}{20}$	$\frac{5.2}{16}$	$\frac{5.0}{9}$	$\frac{4.9}{-}$	$\frac{5.4}{11}$	$\frac{5.9}{18}$	$\frac{5.6}{19}$	$\frac{6.5}{33}$
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$\frac{2.4}{33}$	$\frac{3.7}{20}$	$\frac{6.1}{16}$	$\frac{5.7}{7}$	$\frac{8.6}{-}$	$\frac{6.3}{12}$	$\frac{6.7}{14}$	$\frac{5.3}{20}$	$\frac{6.0}{33}$
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R.R. Spike in T.P. Rt. Sta. 489 + 30

Sta	+	π ✓	-	Elev.
489+50		980.47		73.1-
490				70.5-
+50		✓		68.2-
T.P.	2.22	970.36	12.33	968.14 ✓
491+0				65.7-
+50				63.2-
492+00				60.9-
+50				59.0-
493		✓		57.7-
T.P.	1.98	959.69	12.65	957.71 ✓
+50				56.7-
494				55.9-
+50				55.2-

Lt

E

Rt

$\frac{2.0}{33}$	$\frac{6.4}{19}$	$\frac{7.9}{14}$	$\frac{7.7}{8}$	$\frac{7.4}{1}$	$\frac{8.0}{12}$	$\frac{8.3}{18}$	$\frac{6.5}{20}$	$\frac{6.6}{33}$
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$\frac{7.8}{33}$	$\frac{9.5}{18}$	$\frac{10.6}{14}$	$\frac{10.1}{8}$	$\frac{10.0}{1}$	$\frac{10.5}{12}$	$\frac{11.3}{17}$	$\frac{10.2}{19}$	$\frac{10.4}{33}$
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$\frac{11.1}{33}$	$\frac{10.9}{17}$	$\frac{12.8}{14}$	$\frac{12.7}{8}$	$\frac{12.3}{1}$	$\frac{12.7}{12}$	$\frac{12.9}{18}$	$\frac{13.4}{33}$	begin yard
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$\frac{2.0}{33}$	$\frac{2.4}{17}$	$\frac{5.0}{15}$	$\frac{4.9}{7}$	$\frac{4.7}{1}$	$\frac{5.2}{11}$	$\frac{5.6}{14}$	$\frac{5.3}{16}$	$\frac{4.6}{20}$	$\frac{4.3}{33}$
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$\frac{5.2}{33}$	$\frac{5.5}{18}$	$\frac{8.0}{15}$	$\frac{7.5}{8}$	$\frac{7.2}{1}$	$\frac{7.7}{11}$	$\frac{8.1}{16}$	$\frac{7.3}{17}$	$\frac{6.6}{33}$
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Rd Lt. 491+40

$\frac{8.3}{33}$	$\frac{9.4}{20}$	$\frac{12.2}{15}$	$\frac{9.7}{9}$	$\frac{9.5}{1}$	$\frac{9.9}{10}$	$\frac{11.2}{23}$	$\frac{11.1}{33}$
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$\frac{11.0}{33}$	$\frac{11.1}{17}$	$\frac{11.9}{15}$	$\frac{11.8}{9}$	$\frac{11.4}{1}$	$\frac{11.5}{10}$	$\frac{12.7}{15}$	$\frac{12.5}{17}$	$\frac{12.0}{33}$
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$\frac{13.5}{33}$	$\frac{13.3}{15}$	$\frac{12.9}{9}$	$\frac{12.7}{1}$	$\frac{13.1}{10}$	$\frac{13.5}{13}$	$\frac{14.1}{14}$	$\frac{13.7}{15}$	$\frac{14.0}{33}$	Yard
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TOP E

$\frac{4.0}{33}$	$\frac{3.5}{17}$	$\frac{3.3}{10}$	$\frac{3.0}{1}$	$\frac{3.4}{10}$	$\frac{4.7}{14}$	$\frac{4.7}{20}$	$\frac{5.2}{33}$
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$\frac{4.5}{33}$	$\frac{4.4}{17}$	$\frac{3.8}{9}$	$\frac{3.8}{1}$	$\frac{4.4}{9}$	$\frac{5.5}{15}$	$\frac{5.1}{14}$	$\frac{5.3}{33}$
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$\frac{4.0}{33}$	$\frac{4.4}{14}$	$\frac{5.2}{15}$	$\frac{4.8}{12}$	$\frac{4.5}{1}$	$\frac{4.8}{9}$	$\frac{5.2}{13}$	$\frac{6.0}{16}$	$\frac{5.0}{20}$	$\frac{4.8}{33}$
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Sta. + $\bar{1}$ - Elev.

959.69

495

54.2-

+50

53.2-

496

52.0-

+50

50.8-

497

50.0-

T.P.

3.51

953.50

9.70

949.99

+50

49.1-

498

48.7-

(Bench Levels.)

B.M.

4.84

953.50

4.84

948.66

T.P.

6.27

953.35

6.42

947.08

T.P.

0.97

949.03

5.29

948.06

B.M.

4.00

949.03

4.00

945.03

T.P.

4.99

949.47

4.55

944.48

5154

3.95

945.52

5154

3.68

946.62

T.P.

4.74

948.29

5.92

943.55

B.M.

1.72

Cont. on P.

+

946.57

$\frac{4.3}{33}$	$\frac{4.3}{20}$	$\frac{6.1}{15}$	$\frac{5.6}{9}$	$\frac{5.5}{-}$	$\frac{5.9}{9}$	$\frac{6.5}{15}$	$\frac{5.1}{20}$	$\frac{5.5}{33}$
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$\frac{2.3}{33}$	$\frac{2.2}{23}$	$\frac{7.2}{16}$	$\frac{6.9}{10}$	$\frac{6.5}{-}$	$\frac{6.7}{10}$	$\frac{7.2}{15}$	$\frac{5.7}{20}$	$\frac{6.3}{33}$
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$\frac{4.9}{33}$	$\frac{5.4}{24}$	$\frac{8.4}{17}$	$\frac{8.0}{11}$	$\frac{7.7}{-}$	$\frac{8.0}{9}$	$\frac{8.6}{15}$	$\frac{8.4}{18}$	$\frac{9.0}{33}$
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$\frac{6.8}{33}$	$\frac{7.4}{29}$	$\frac{8.9}{26}$	$\frac{9.7}{15}$	$\frac{9.1}{11}$	$\frac{8.9}{-}$	$\frac{9.3}{9}$	$\frac{11.1}{16}$	$\frac{12.2}{33}$
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$\frac{8.3}{33}$	$\frac{10.0}{28}$	$\frac{10.4}{16}$	$\frac{10.1}{12}$	$\frac{9.7}{-}$	$\frac{10.2}{8}$	$\frac{10.7}{11}$	$\frac{13.9}{20}$	$\frac{14.8}{33}$
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$\frac{5.4}{33}$	$\frac{5.8}{28}$	$\frac{5.4}{17}$	$\frac{4.6}{12}$	$\frac{4.4}{-}$	$\frac{4.9}{8}$	$\frac{5.8}{13}$	$\frac{9.3}{21}$	$\frac{10.2}{33}$
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$\frac{5.4}{33}$	$\frac{6.5}{28}$	$\frac{6.6}{19}$	$\frac{5.4}{15}$	$\frac{5.0}{11}$	$\frac{4.8}{-}$	$\frac{5.2}{8}$	$\frac{8.3}{16}$	$\frac{9.3}{33}$
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Top Mon 498 + 48.55

X-Sections contd pg

R.R. Spike in 12. R. Tel. P. 33 Rt. Sta. 512 + 26

Top West Rail }
 " East Rail } LINE

Iron Mon 524 + 58.80

Sta.

T

T

-

Elev.

x

Sta.	+	π ✓	-	Elev. ✓
B.M.	3.73	952.39		948.66
498+48.5				48.7-
499+50				48.6-
499+50				48.3-
500+00				48.0-
500+50				47.6-
501+00				47.2-
501+50				47.1-
502+00				46.6-
T.P.	5.76	957.86 ✓	6.29	946.10 ✓
502+50				45.9-
503+00				45.8-

Top Stone Mon. Sta 498+485

$$\frac{4.5}{33} \quad \frac{5.5}{26} \quad \frac{5.6}{19} \quad \frac{4.1}{14} \quad 3.7 \quad \frac{3.8}{9} \quad \frac{4.4}{15} \quad \frac{4.8}{29} \quad \frac{5.8}{33}$$

$$\frac{4.3}{33} \quad \frac{4.4}{24} \quad \frac{4.9}{17} \quad \frac{4.0}{11} \quad \frac{3.8}{10} \quad \frac{4.3}{10} \quad \frac{5.3}{14} \quad \frac{4.7}{16} \quad \frac{4.5}{33}$$

$$\frac{4.7}{33} \quad \frac{4.8}{17.5} \quad \frac{5.3}{15} \quad \frac{4.4}{11} \quad 4.1 \quad \frac{4.6}{9} \quad \frac{5.2}{15} \quad \frac{4.1}{18} \quad \frac{4.1}{33}$$

$$\frac{6.1}{33} \quad \frac{5.4}{17} \quad \frac{5.7}{14} \quad \frac{4.8}{10} \quad 4.4 \quad \frac{4.7}{10} \quad \frac{5.4}{16} \quad \frac{4.0}{21} \quad \frac{4.2}{33}$$

$$\frac{6.8}{33} \quad \frac{5.7}{16} \quad \frac{6.0}{14} \quad \frac{5.3}{10} \quad 4.8 \quad \frac{5.1}{10} \quad \frac{5.6}{16} \quad \frac{4.0}{21} \quad \frac{3.7}{33}$$

$$\frac{7.1}{33} \quad \frac{7.2}{26} \quad \frac{6.0}{16.5} \quad \frac{6.3}{14} \quad \frac{5.8}{10} \quad \frac{5.2}{10} \quad \frac{5.5}{10} \quad \frac{5.1}{17} \quad \frac{4.0}{21} \quad \frac{3.6}{33}$$

$$\frac{4.8}{33} \quad \frac{4.8}{31} \quad \frac{5.4}{28} \quad \frac{4.6}{20.5} \quad \frac{6.2}{14.5} \quad \frac{5.8}{11} \quad \frac{5.3}{10} \quad \frac{5.8}{9} \quad \frac{6.6}{16} \quad \frac{4.4}{22} \quad \frac{4.1}{33}$$

$$\frac{5.1}{33} \quad \frac{5.8}{28} \quad \frac{5.7}{19.5} \quad \frac{7.0}{15.5} \quad \frac{6.3}{10} \quad 5.8 \quad \frac{6.1}{9} \quad \frac{7.9}{18} \quad \frac{8.3}{26} \quad \frac{8.0}{33}$$

Nail in T.P.-RT- Sta 503+45

$$\frac{9.0}{33} \quad \frac{9.0}{18} \quad \frac{6.7}{11} \quad \frac{6.0}{10} \quad \frac{6.4}{10} \quad \frac{7.7}{19} \quad \frac{7.5}{24} \quad \frac{9.8}{33}$$

$$\frac{10.2}{33} \quad \frac{10.1}{20} \quad \frac{6.7}{10} \quad \frac{6.3}{10} \quad \frac{6.6}{9.5} \quad \frac{8.7}{16} \quad \frac{9.7}{22} \quad \frac{10.1}{33}$$

Sta	+	π ✓ 951.86	-	Elev.
503+50				46.1-
504+00				47.3-
504+50				48.4-
504+85				49.3-
+90				49.4-
505+13				49.7-
+18				49.7-
505+50				49.7-
T.P	4.25	✓ 954.20	1.91	✓ 949.95
506+00				49.9-
506+50				49.7-
507+00				49.1-
T.P	1.83	✓ 955.15	0.88	✓ 953.32

Lt.

P

Pt.

10

$$\begin{array}{r} 8.6 \\ 33 \end{array} \quad \begin{array}{r} 8.5 \\ 20 \end{array} \quad \begin{array}{r} 7.6 \\ 16 \end{array} \quad \begin{array}{r} 6.5 \\ 11 \end{array} \quad \begin{array}{r} 5.8 \\ 9 \end{array} \quad \begin{array}{r} 6.2 \\ 9 \end{array} \quad \begin{array}{r} 8.8 \\ 19 \end{array} \quad \begin{array}{r} 9.2 \\ 30 \end{array} \quad \begin{array}{r} 9.1 \\ 33 \end{array}$$

$$\begin{array}{r} 4.1 \\ 33 \end{array} \quad \begin{array}{r} 4.1 \\ 30 \end{array} \quad \begin{array}{r} 5.6 \\ 25 \end{array} \quad \begin{array}{r} 6.2 \\ 19 \end{array} \quad \begin{array}{r} 5.2 \\ 11 \end{array} \quad 4.6 \quad \begin{array}{r} 5.6 \\ 9 \end{array} \quad \begin{array}{r} 6.5 \\ 22 \end{array} \quad \begin{array}{r} 5.8 \\ 26 \end{array} \quad \begin{array}{r} 6.1 \\ 33 \end{array}$$

$$\begin{array}{r} 3.1 \\ 33 \end{array} \quad \begin{array}{r} 4.2 \\ 27 \end{array} \quad \begin{array}{r} 4.6 \\ 17 \end{array} \quad \begin{array}{r} 4.2 \\ 12 \end{array} \quad 3.5 \quad \begin{array}{r} 3.8 \\ 8 \end{array} \quad \begin{array}{r} 4.9 \\ 17 \end{array} \quad \begin{array}{r} 4.5 \\ 29 \end{array} \quad \begin{array}{r} 4.5 \\ 33 \end{array}$$

$$\begin{array}{r} 1.8 \\ 33 \end{array} \quad \begin{array}{r} 2.0 \\ 29 \end{array} \quad \begin{array}{r} 3.4 \\ 24 \end{array} \quad \begin{array}{r} 2.6 \\ 12 \end{array} \quad \begin{array}{r} 3.4 \\ 12 \end{array} \quad \begin{array}{r} 4.2 \\ 22 \end{array} \quad \begin{array}{r} 4.4 \\ 33 \end{array}$$

$$\begin{array}{r} 3.0 \\ 33 \end{array} \quad \begin{array}{r} 2.8 \\ 15 \end{array} \quad \begin{array}{r} 2.5 \\ 10 \end{array} \quad \begin{array}{r} 2.9 \\ 10 \end{array} \quad \begin{array}{r} 3.5 \\ 21 \end{array} \quad \begin{array}{r} 3.5 \\ 33 \end{array}$$

X Road

$$\begin{array}{r} 2.8 \\ 33 \end{array} \quad \begin{array}{r} 2.8 \\ 29 \end{array} \quad \begin{array}{r} 2.8 \\ 21 \end{array} \quad \begin{array}{r} 2.6 \\ 13 \end{array} \quad \begin{array}{r} 2.2 \\ 11 \end{array} \quad \begin{array}{r} 2.7 \\ 11 \end{array} \quad \begin{array}{r} 3.2 \\ 25 \end{array} \quad \begin{array}{r} 3.0 \\ 33 \end{array}$$

$$\begin{array}{r} 0.8 \\ 33 \end{array} \quad \begin{array}{r} 1.8 \\ 23 \end{array} \quad \begin{array}{r} 2.9 \\ 17 \end{array} \quad \begin{array}{r} 2.7 \\ 14 \end{array} \quad \begin{array}{r} 2.2 \\ 10 \end{array} \quad \begin{array}{r} 2.7 \\ 10 \end{array} \quad \begin{array}{r} 3.3 \\ 16 \end{array} \quad \begin{array}{r} 2.9 \\ 21 \end{array} \quad \begin{array}{r} 3.2 \\ 33 \end{array}$$

$$\begin{array}{r} 1.6 \\ 33 \end{array} \quad \begin{array}{r} 1.2 \\ 20 \end{array} \quad \begin{array}{r} 3.1 \\ 16 \end{array} \quad \begin{array}{r} 2.7 \\ 12 \end{array} \quad \begin{array}{r} 2.2 \\ 9 \end{array} \quad \begin{array}{r} 2.7 \\ 9 \end{array} \quad \begin{array}{r} 3.0 \\ 13 \end{array} \quad \begin{array}{r} 1.6 \\ 16 \end{array} \quad \begin{array}{r} 2.1 \\ 33 \end{array}$$

$$\begin{array}{r} 5.2 \\ 33 \end{array} \quad \begin{array}{r} 4.5 \\ 20 \end{array} \quad \begin{array}{r} 5.7 \\ 16.5 \end{array} \quad \begin{array}{r} 5.0 \\ 12.5 \end{array} \quad 4.3 \quad \begin{array}{r} 4.7 \\ 9 \end{array} \quad \begin{array}{r} 5.0 \\ 13 \end{array} \quad \begin{array}{r} 3.0 \\ 23 \end{array} \quad \begin{array}{r} 2.9 \\ 33 \end{array}$$

$$\begin{array}{r} 4.9 \\ 33 \end{array} \quad \begin{array}{r} 4.4 \\ 19 \end{array} \quad \begin{array}{r} 5.5 \\ 15 \end{array} \quad \begin{array}{r} 5.2 \\ 13 \end{array} \quad 4.5 \quad \begin{array}{r} 4.7 \\ 8.5 \end{array} \quad \begin{array}{r} 5.2 \\ 15 \end{array} \quad \begin{array}{r} 4.1 \\ 19 \end{array} \quad \begin{array}{r} 3.8 \\ 33 \end{array}$$

$$\begin{array}{r} 2.3 \\ 33 \end{array} \quad \begin{array}{r} 3.1 \\ 29 \end{array} \quad \begin{array}{r} 3.1 \\ 21 \end{array} \quad \begin{array}{r} 6.0 \\ 14.5 \end{array} \quad \begin{array}{r} 5.6 \\ 11 \end{array} \quad 5.1 \quad \begin{array}{r} 3.6 \\ 10 \end{array} \quad \begin{array}{r} 6.1 \\ 15 \end{array} \quad \begin{array}{r} 4.9 \\ 21 \end{array} \quad \begin{array}{r} 5.0 \\ 33 \end{array}$$

Mail in P.P. Lt. Sta 507 + 40

+xx

Sta	+	π ✓	-	Elev
507+40		955.15		48.8-
508+00				48.1-
508+50				47.4-
509+00				46.6-
509+25				45.4-
510+00				45.9-
510+40				45.6-
T.P.	3.04	✓ 948.09	10.10	✓ 945.05
511+00				44.6-
511+30				44.2-
511+50				43.8-
512+00				43.2-
B.M.			3.08	✓ 945.01 945.03

LH

Φ

RH

11

 $\frac{2.5}{33}$ $\frac{2.3}{23}$ $\frac{7.3}{15}$ $\frac{6.7}{11}$ $\frac{6.4}{-}$ $\frac{6.7}{9}$ $\frac{7.2}{14}$ $\frac{6.0}{20}$ $\frac{6.2}{30}$ $\frac{6.2}{33}$
 $\frac{5.5}{23}$ $\frac{5.6}{20}$ $\frac{8.3}{15}$ $\frac{7.5}{10}$ $\frac{7.1}{-}$ $\frac{7.5}{11}$ $\frac{7.9}{14}$ $\frac{5.0}{19}$ $\frac{4.7}{33}$
 $\frac{6.4}{33}$ $\frac{6.3}{22}$ $\frac{9.1}{14}$ $\frac{8.2}{11}$ $\frac{7.8}{-}$ $\frac{8.4}{11}$ $\frac{8.5}{14}$ $\frac{4.8}{22}$ $\frac{4.5}{33}$
 $\frac{7.7}{33}$ $\frac{8.0}{27}$ $\frac{7.4}{21}$ $\frac{9.7}{14}$ $\frac{9.4}{11}$ $\frac{8.6}{-}$ $\frac{9.2}{12}$ $\frac{9.8}{15}$ $\frac{9.0}{18}$ $\frac{6.6}{22}$ $\frac{5.9}{30}$ $\frac{5.8}{33}$
 $\frac{8.3}{33}$ $\frac{8.5}{28}$ $\frac{7.6}{23}$ $\frac{10.0}{15}$ $\frac{9.5}{11}$ $\frac{9.8}{-}$ $\frac{9.5}{12}$ $\frac{10.0}{15}$ $\frac{9.4}{18}$ $\frac{9.5}{24}$ $\frac{5.6}{31}$ $\frac{5.5}{33}$
 $\frac{8.0}{33}$ $\frac{8.1}{29}$ $\frac{9.7}{24}$ $\frac{9.5}{17}$ $\frac{10.3}{15}$ $\frac{9.7}{11}$ $\frac{9.3}{-}$ $\frac{9.9}{13}$ $\frac{10.4}{21}$ $\frac{9.9}{29}$ $\frac{5.5}{37}$
 $\frac{6.7}{33}$ $\frac{6.8}{28}$ $\frac{9.3}{22}$ $\frac{9.9}{18}$ $\frac{10.8}{14}$ $\frac{10.0}{10}$ $\frac{9.6}{-}$ $\frac{10.3}{13}$ $\frac{10.9}{20}$ $\frac{10.5}{21}$ $\frac{9.5}{30.5}$
 $\frac{3.7}{33}$ $\frac{3.6}{29.5}$ $\frac{4.1}{25}$ $\frac{3.7}{17.5}$ $\frac{4.4}{13}$ $\frac{3.8}{10}$ $\frac{3.5}{-}$ $\frac{3.9}{11}$ $\frac{4.9}{21}$ $\frac{4.7}{33}$
 $\frac{7.1}{33}$ $\frac{6.5}{25}$ $\frac{6.1}{18}$ $\frac{4.3}{10}$ $\frac{3.7}{-}$ $\frac{4.2}{10}$ $\frac{5.0}{21}$ $\frac{5.3}{33}$
 $\frac{8.2}{33}$ $\frac{8.3}{20}$ $\frac{4.8}{10}$ $\frac{4.3}{-}$ $\frac{4.3}{11}$ $\frac{5.0}{15}$ $\frac{5.2}{24}$ $\frac{5.4}{33}$
 $\frac{8.9}{33}$ $\frac{8.8}{20}$ $\frac{5.4}{12}$ $\frac{4.9}{-}$ $\frac{4.9}{10}$ $\frac{5.3}{17}$ $\frac{5.8}{27}$ $\frac{5.4}{26}$ $\frac{5.5}{30}$ $\frac{6.2}{33}$

R.R. spike in T.P. 33' Pt-Sta. 5/2+26

Sta	+	Δ ✓	-	Elev
512+50		948.09		43.6

513+00				44.0
--------	--	--	--	------

513+50				44.3
--------	--	--	--	------

514+00				44.4
--------	--	--	--	------

514+50				44.5
--------	--	--	--	------

T.P	4.4.2	950.00 ✓	2.51	945.58 ✓
-----	-------	----------	------	----------

515+00				45.1
--------	--	--	--	------

515+47				45.6
--------	--	--	--	------

515+72				45.8
--------	--	--	--	------

516+00				45.6
--------	--	--	--	------

516+40				45.5
--------	--	--	--	------

517+00				45.0
--------	--	--	--	------

L+

Q

Rit

12

$$\frac{8.7}{33} \quad \frac{8.6}{20} \quad \frac{5.4}{12} \quad \frac{4.5}{12} \quad \frac{4.6}{12} \quad \frac{5.7}{18} \quad \frac{5.2}{23} \quad \frac{5.8}{29} \quad \frac{3.8}{33}$$

$$\frac{7.8}{33} \quad \frac{7.0}{20} \quad \frac{4.7}{11} \quad \frac{4.1}{11} \quad \frac{4.3}{13} \quad \frac{5.8}{18} \quad \frac{5.4}{22} \quad \frac{5.3}{27} \quad \frac{4.5}{33}$$

$$\frac{6.4}{33} \quad \frac{5.6}{16} \quad \frac{4.4}{11} \quad \frac{3.8}{11} \quad \frac{4.1}{10} \quad \frac{4.2}{14} \quad \frac{5.7}{18} \quad \frac{5.2}{26} \quad \frac{1.5}{35} \quad \frac{0.40}{40} \text{ Top of Rail}$$

$$\frac{5.3}{33} \quad \frac{5.8}{25} \quad \frac{5.7}{17} \quad \frac{4.2}{12} \quad \frac{3.7}{12} \quad \frac{4.0}{11} \quad \frac{5.5}{16} \quad \frac{5.5}{19} \quad \frac{1.9}{28} \quad \frac{0.80}{32} \text{ Top of Rail}$$

$$\frac{8.4}{33} \quad \frac{8.7}{25} \quad \frac{7.6}{20} \quad \frac{6.9}{17} \quad \frac{4.3}{12} \quad \frac{3.6}{12} \quad \frac{3.5}{9} \quad \frac{3.5}{14.5} \quad \frac{2.7}{16.5} \quad \frac{1.50}{22} \text{ Top of Rail}$$

$$\frac{11.8}{33} \quad \frac{11.1}{22} \quad \frac{6.1}{13.5} \quad \frac{5.7}{10} \quad \frac{4.9}{10} \quad \frac{4.7}{6} \quad \frac{4.0}{10} \quad \frac{4.9}{21} \quad \frac{8.8}{29}$$

$$\frac{12.1}{33} \quad \frac{12.0}{25} \quad \frac{5.4}{14} \quad \frac{5.0}{13} \quad \frac{4.62}{3} \quad \frac{4.4}{14} \quad \frac{4.1}{9} \quad \frac{5.6}{14} \quad \frac{11.4}{23} \quad \frac{11.8}{33}$$

$$\frac{12.1}{33} \quad \frac{8.5}{21} \quad \frac{5.7}{15} \quad \frac{4.32}{6} \quad \frac{4.6}{4} \quad \frac{4.2}{4} \quad \frac{4.16}{8} \quad \frac{5.6}{11} \quad \frac{11.2}{21} \quad \frac{11.7}{33}$$

$$\frac{11.8}{37} \quad \frac{7.9}{30} \quad \frac{6.2}{26} \quad \frac{4.39}{12} \quad \frac{4.4}{11} \quad \frac{4.4}{11} \quad \frac{5.0}{9} \quad \frac{5.8}{13} \quad \frac{11.0}{19} \quad \frac{11.2}{33}$$

$$\frac{11.8}{30} \quad \frac{5.3}{27} \quad \frac{6.3}{21} \quad \frac{6.6}{15} \quad \frac{4.9}{11} \quad \frac{4.5}{11} \quad \frac{5.0}{9} \quad \frac{5.7}{12} \quad \frac{10.8}{21} \quad \frac{10.7}{33}$$

$$\frac{12.3}{33} \quad \frac{11.9}{22} \quad \frac{5.9}{13} \quad \frac{5.5}{10} \quad \frac{5.0}{10} \quad \frac{5.5}{9} \quad \frac{6.0}{12} \quad \frac{10.8}{20} \quad \frac{10.8}{23} \quad \frac{9.7}{33}$$

Sta	+	π ✓	-	Elev
		950.00		
517+50				44.7.
				↓
517+90				45.5.
518+27			4.07	945.93 ✓
518+30				45.9.
+34			4.20	945.80 ✓
518+70				44.4.
T.P	4.96	948.36 ✓	6.60	943.40 ✓
519+00				43.6.
+50				42.8.
520+00				43.0.
+50				43.2.
521+00				43.6.
+50				43.9.
-				
522+00				44.3.

$$\begin{array}{r} 12.4 \\ 33 \end{array} \quad \begin{array}{r} 12.4 \\ 25 \end{array} \quad \begin{array}{r} 5.2 \\ 13 \end{array} \quad 5.3 \quad \begin{array}{r} 5.6 \\ 6 \end{array} \quad \begin{array}{r} 5.8 \\ 12 \end{array} \quad \begin{array}{r} 11.2 \\ 23 \end{array} \quad \begin{array}{r} 16.3 \\ 18 \end{array} \quad \begin{array}{r} 10.3 \\ 33 \end{array}$$

$$\begin{array}{r} 12.3 \\ 33 \end{array} \quad \begin{array}{r} 12.2 \\ 25 \end{array} \quad \begin{array}{r} 6.6 \\ 15 \end{array} \quad \begin{array}{r} 5.3 \\ 11 \end{array} \quad \begin{array}{r} 4.5 \\ 9 \end{array} \quad \begin{array}{r} 4.4 \\ 9 \end{array} \quad \begin{array}{r} 4.9 \\ 13 \end{array} \quad \begin{array}{r} 5.8 \\ 14 \end{array} \quad \begin{array}{r} 4.7 \\ 17 \end{array} \quad \begin{array}{r} 4.4 \\ 20 \end{array}$$

4.07 To P West Rail

$$\begin{array}{r} 11.6 \\ 33 \end{array} \quad \begin{array}{r} 11.5 \\ 27 \end{array} \quad \begin{array}{r} 5.3 \\ 14 \end{array} \quad \begin{array}{r} 4.3 \\ 9 \end{array} \quad 4.1 \quad \begin{array}{r} 4.1 \\ 11 \end{array} \quad \begin{array}{r} 5.1 \\ 13 \end{array} \quad \begin{array}{r} 10.6 \\ 26 \end{array} \quad \begin{array}{r} 10.4 \\ 33 \end{array}$$

4.20

Top East Rail

$$\begin{array}{r} 6.2 \\ 30 \end{array} \quad \begin{array}{r} 6.3 \\ 25 \end{array} \quad \begin{array}{r} 6.6 \\ 21 \end{array} \quad \begin{array}{r} 6.1 \\ 15 \end{array} \quad \begin{array}{r} 5.6 \\ 10 \end{array} \quad 5.6 \quad \begin{array}{r} 6.0 \\ 9.5 \end{array} \quad \begin{array}{r} 7.1 \\ 12 \end{array} \quad \begin{array}{r} 10.8 \\ 19 \end{array} \quad \begin{array}{r} 10.9 \\ 32 \end{array} \quad \begin{array}{r} 9.8 \\ 36 \end{array}$$

$$\begin{array}{r} 10.1 \\ 25 \end{array} \quad \begin{array}{r} 10.6 \\ 21 \end{array} \quad \begin{array}{r} 8.7 \\ 19 \end{array} \quad \begin{array}{r} 6.2 \\ 13 \end{array} \quad \begin{array}{r} 5.3 \\ 9 \end{array} \quad 4.8 \quad \begin{array}{r} 5.3 \\ 9.5 \end{array} \quad \begin{array}{r} 6.1 \\ 13 \end{array} \quad \begin{array}{r} 9.2 \\ 20 \end{array} \quad \begin{array}{r} 9.1 \\ 29 \end{array} \quad \begin{array}{r} 7.3 \\ 33 \end{array}$$

$$\begin{array}{r} 9.5 \\ 33 \end{array} \quad \begin{array}{r} 9.6 \\ 30 \end{array} \quad \begin{array}{r} 10.9 \\ 23 \end{array} \quad \begin{array}{r} 9.1 \\ 20 \end{array} \quad \begin{array}{r} 7.8 \\ 15 \end{array} \quad \begin{array}{r} 6.4 \\ 10 \end{array} \quad \begin{array}{r} 5.6 \\ 9 \end{array} \quad \begin{array}{r} 5.9 \\ 9 \end{array} \quad \begin{array}{r} 6.8 \\ 15 \end{array} \quad \begin{array}{r} 9.2 \\ 20 \end{array} \quad \begin{array}{r} 9.6 \\ 23 \end{array} \quad \begin{array}{r} 9.6 \\ 28 \end{array} \quad \begin{array}{r} 5.8 \\ 33 \end{array}$$

$$\begin{array}{r} 9.8 \\ 33 \end{array} \quad \begin{array}{r} 10.3 \\ 23 \end{array} \quad \begin{array}{r} 9.6 \\ 15 \end{array} \quad \begin{array}{r} 6.2 \\ 9 \end{array} \quad \begin{array}{r} 5.4 \\ 9 \end{array} \quad 5.8 \quad \begin{array}{r} 6.6 \\ 14 \end{array} \quad \begin{array}{r} 8.6 \\ 19 \end{array} \quad \begin{array}{r} 9.3 \\ 23 \end{array} \quad \begin{array}{r} 9.9 \\ 29 \end{array} \quad \begin{array}{r} 4.9 \\ 33 \end{array}$$

$$\begin{array}{r} 9.4 \\ 33 \end{array} \quad \begin{array}{r} 9.7 \\ 24 \end{array} \quad \begin{array}{r} 6.8 \\ 15 \end{array} \quad \begin{array}{r} 5.8 \\ 10 \end{array} \quad \begin{array}{r} 5.2 \\ 9 \end{array} \quad \begin{array}{r} 5.7 \\ 8 \end{array} \quad \begin{array}{r} 6.3 \\ 13 \end{array} \quad \begin{array}{r} 8.5 \\ 18 \end{array} \quad \begin{array}{r} 9.2 \\ 24 \end{array} \quad \begin{array}{r} 6.5 \\ 33 \end{array}$$

$$\begin{array}{r} 7.6 \\ 33 \end{array} \quad \begin{array}{r} 7.7 \\ 29 \end{array} \quad \begin{array}{r} 9.6 \\ 25 \end{array} \quad \begin{array}{r} 6.7 \\ 20 \end{array} \quad \begin{array}{r} 5.5 \\ 14 \end{array} \quad 4.8 \quad \begin{array}{r} 5.3 \\ 9 \end{array} \quad \begin{array}{r} 6.2 \\ 14 \end{array} \quad \begin{array}{r} 8.1 \\ 19 \end{array} \quad \begin{array}{r} 8.4 \\ 27 \end{array} \quad \begin{array}{r} 5.5 \\ 33 \end{array}$$

$$\begin{array}{r} 6.0 \\ 33 \end{array} \quad \begin{array}{r} 6.4 \\ 28 \end{array} \quad \begin{array}{r} 9.3 \\ 25 \end{array} \quad \begin{array}{r} 6.2 \\ 20 \end{array} \quad \begin{array}{r} 5.9 \\ 13 \end{array} \quad 4.5 \quad \begin{array}{r} 4.9 \\ 10 \end{array} \quad \begin{array}{r} 5.9 \\ 15 \end{array} \quad \begin{array}{r} 8.3 \\ 21 \end{array} \quad \begin{array}{r} 7.6 \\ 28 \end{array} \quad \begin{array}{r} 5.0 \\ 33 \end{array}$$

$$\begin{array}{r} 5.1 \\ 33 \end{array} \quad \begin{array}{r} 7.2 \\ 27 \end{array} \quad \begin{array}{r} 9.6 \\ 23 \end{array} \quad \begin{array}{r} 6.0 \\ 18 \end{array} \quad \begin{array}{r} 4.7 \\ 13 \end{array} \quad 4.1 \quad \begin{array}{r} 4.7 \\ 10 \end{array} \quad \begin{array}{r} 5.4 \\ 13 \end{array} \quad \begin{array}{r} 8.0 \\ 21 \end{array} \quad \begin{array}{r} 3.6 \\ 33 \end{array}$$

Sta + π ✓ - Elev

948.36

522+50

44.3

523+00

44.2

+50

44.6

524+00

48.6

1.79

✓
946.57

L/1

2

B/1

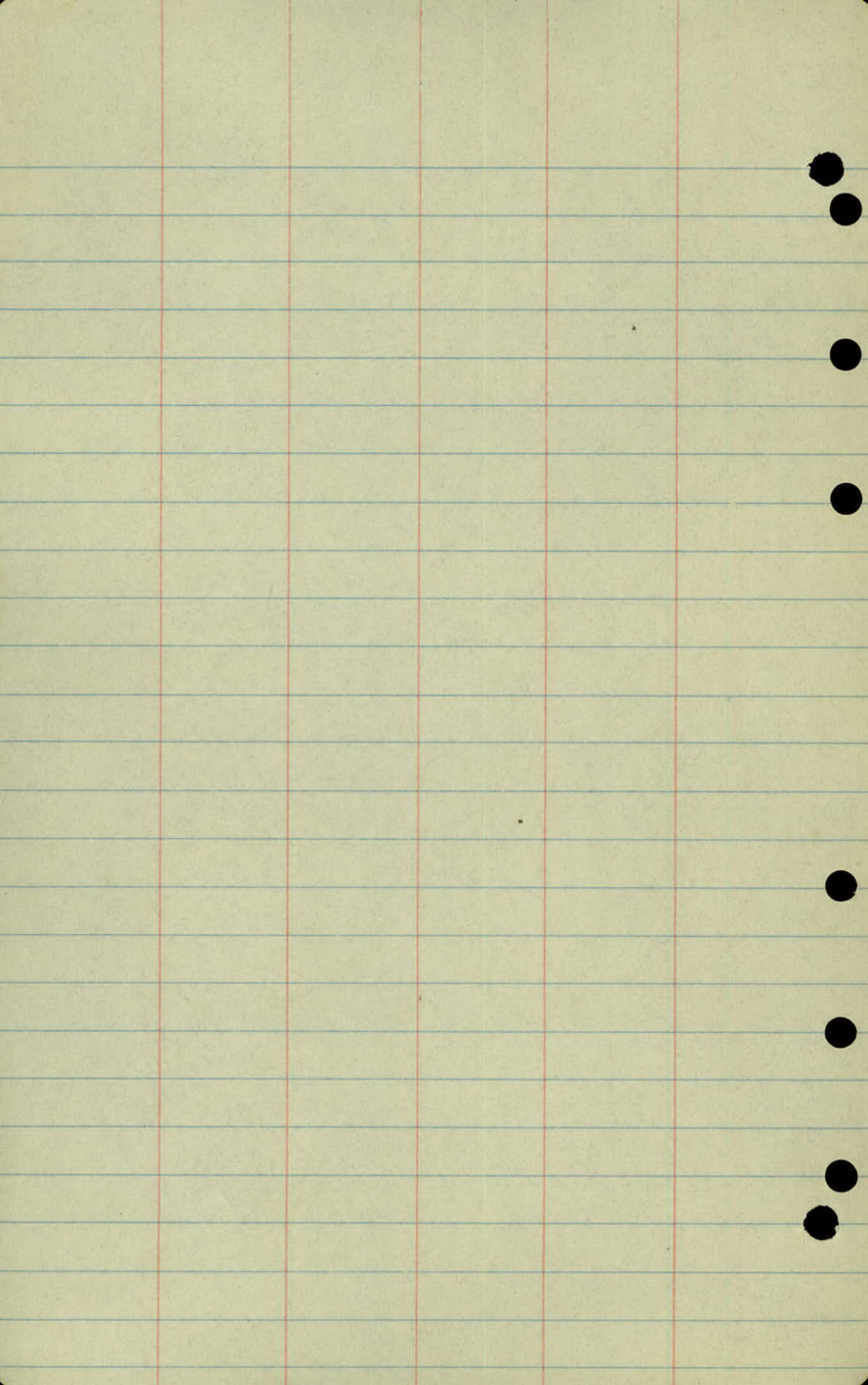
$\frac{7.4}{33}$ $\frac{7.4}{31}$ $\frac{9.6}{27}$ $\frac{6.0}{21}$ $\frac{4.6}{12}$ $\frac{4.1}{-}$ $\frac{4.6}{9}$ $\frac{5.3}{13}$ $\frac{7.7}{19}$ $\frac{8.2}{23}$ $\frac{7.3}{27}$ $\frac{4.4}{30}$ $\frac{4.3}{33}$

$\frac{7.9}{33}$ $\frac{9.3}{26}$ $\frac{7.4}{21}$ $\frac{6.2}{16}$ $\frac{4.7}{11}$ $\frac{4.2}{-}$ $\frac{4.7}{8}$ $\frac{5.4}{12}$ $\frac{7.9}{20}$ $\frac{7.9}{27}$ $\frac{7.0}{33}$

$\frac{7.8}{33}$ $\frac{7.6}{27}$ $\frac{8.7}{23}$ $\frac{7.5}{20}$ $\frac{6.2}{16}$ $\frac{4.3}{10}$ 3.8 $\frac{4.3}{10}$ $\frac{5.2}{14}$ $\frac{7.9}{22}$ $\frac{2.5}{27}$ $\frac{6.9}{33}$

$\frac{6.0}{33}$ $\frac{6.1}{25}$ $\frac{7.1}{21}$ $\frac{4.1}{14}$ $\frac{3.2}{11}$ $\frac{2.8}{-}$ $\frac{3.2}{9}$ $\frac{3.9}{13}$ $\frac{7.1}{23}$ $\frac{6.9}{28}$ $\frac{3.7}{33}$

X-Section Contd P. 16



Lt.

£

Rt.

X-Sections cont'd from P. 14

Sta.	+	π	-	Elev.
B.M.	13.22	✓ 959.79		✓ 946.57
524+58.5	-(Eas/Ave not graded)			✓ 46.6
525+0				✓ 47.6
+50				✓ 49.2
526				✓ 51.3
+50				✓ 53.8
527		✓		✓ 56.8
T.P.	13.19	972.22	0.76	✓ 959.03
+50				✓ 59.8
528				✓ 63.2
+50				✓ 66.9
T.P.	12.74	✓ 983.11	1.85	✓ 970.37
529				✓ 70.4
+50				✓ 73.5

Aug. 24, 1936
Not.

lt. ♀ Rt.

Top Iron Man. 526/158.50

$\frac{16.6}{26}$	$\frac{16.3}{28}$	$\frac{17.5}{22}$	$\frac{15.3}{18}$	$\frac{13.8}{12}$	$\frac{13.2}{12}$	$\frac{13.6}{8}$	$\frac{14.5}{14}$	$\frac{17.5}{22}$	$\frac{17.5}{30}$	$\frac{15.7}{34}$
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$\frac{13.5}{33}$	$\frac{13.5}{27}$	$\frac{12.5}{12}$	$\frac{12.2}{12}$	$\frac{12.6}{8}$	$\frac{14.6}{20}$	$\frac{14.3}{33}$
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$\frac{13.1}{33}$	$\frac{12.2}{18}$	$\frac{11.0}{13}$	$\frac{10.8}{12}$	$\frac{10.9}{8}$	$\frac{11.8}{12}$	$\frac{13.3}{16}$	$\frac{13.0}{32}$	$\frac{10.4}{37}$
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$\frac{10.4}{33}$	$\frac{10.4}{19}$	$\frac{8.9}{12}$	$\frac{8.5}{12}$	$\frac{8.9}{8}$	$\frac{10.7}{21}$	$\frac{9.0}{27}$	$\frac{6.4}{46}$
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$\frac{7.8}{33}$	$\frac{7.7}{20}$	$\frac{6.4}{11}$	$\frac{6.0}{11}$	$\frac{6.2}{9}$	$\frac{6.8}{15}$	$\frac{8.2}{21}$	$\frac{4.2}{26}$	$\frac{2.2}{37}$
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$\frac{4.0}{53}$	$\frac{3.8}{20}$	$\frac{3.8}{10}$	$\frac{3.0}{10}$	$\frac{3.4}{9}$	$\frac{4.2}{18}$	$\frac{1.6}{26}$	$\frac{0.0}{35}$
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$\frac{11.9}{32}$	$\frac{12.2}{20}$	$\frac{13.0}{14}$	$\frac{12.6}{10}$	$\frac{12.4}{10}$	$\frac{12.7}{10}$	$\frac{13.0}{14}$	$\frac{12.4}{18}$	$\frac{11.4}{38}$
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$\frac{6.0}{33}$	$\frac{6.5}{26}$	$\frac{10.4}{14}$	$\frac{9.2}{9}$	$\frac{9.0}{10}$	$\frac{9.5}{11}$	$\frac{9.8}{15}$	$\frac{8.4}{17}$	$\frac{9.1}{33}$
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$\frac{7.6}{33}$	$\frac{3.0}{26}$	$\frac{4.3}{17}$	$\frac{6.2}{14}$	$\frac{5.8}{8}$	$\frac{5.3}{10}$	$\frac{5.8}{10}$	$\frac{6.0}{15}$	$\frac{3.1}{19}$	$\frac{3.7}{33}$
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$\frac{11.0}{33}$	$\frac{11.3}{18}$	$\frac{13.3}{13}$	$\frac{13.3}{9}$	$\frac{12.7}{12}$	$\frac{13.2}{11}$	$\frac{13.2}{15}$	$\frac{10.0}{20}$	$\frac{9.3}{33}$
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$\frac{7.0}{33}$	$\frac{8.4}{18}$	$\frac{10.2}{12}$	$\frac{10.0}{8}$	$\frac{9.6}{10}$	$\frac{10.0}{11}$	$\frac{10.4}{16}$	$\frac{5.9}{20}$	$\frac{5.6}{33}$
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Sta.	+	$\bar{A}$	-	Elev.
		983.41 ✓		
530				76.4
+35				78.7
+81.	W. edge Pav. ✓			82.1
B.M.	9.95	992.52 ✓	0.54	982.57 ✓
530 + 97.1 =	E. N. St. Rd. @ A			82.6
531 + 13 ✓	E. edge Pav.			82.9
+60				84.4
532				85.4
+50				86.9
533				89.1
T.P.	10.15	✓ 1006.12	1.55	✓ 990.97
+50				90.9
534				92.3

4. ± R+

$\frac{46}{33}$	$\frac{5.5}{16}$	$\frac{7.3}{12}$	$\frac{7.0}{7}$	$\frac{6.7}{-}$	$\frac{7.0}{12}$	$\frac{7.1}{17}$	$\frac{4.7}{20}$	$\frac{4.0}{30}$	$\frac{5.1}{40}$
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Yard = $\frac{18}{30}$ Top Rail $\frac{2.3}{14}$ $\frac{4.0}{14}$ $\frac{4.5}{9}$ $\frac{4.4}{-}$ $\frac{4.2}{10}$ $\frac{4.0}{22}$ $\frac{3.00}{35}$ - W. edge Pav.

$\frac{0.4}{33}$	$\frac{1.4}{19}$	$\frac{2.0}{17}$	$\frac{1.5}{14}$	$\frac{1.00}{0}$
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± N. St. Pav/Rd Top & Conc Pav.

$\frac{7.8}{36}$	$\frac{10.4}{27}$	$\frac{10.0}{23}$	$\frac{9.7}{13.7}$	$\frac{9.95}{-}$	$\frac{10.30}{13.70}$	$\frac{11.1}{22}$	$\frac{11.9}{33}$	$\frac{7.5}{46}$	$\frac{9.6}{50}$
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$\frac{9.6}{Pav = 0}$	$\frac{10.4}{14}$	$\frac{12.3}{19}$	$\frac{7.9}{31}$	$\frac{8.0}{30}$
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$\frac{7.6}{Pav = 39}$	$\frac{7.9}{32}$	$\frac{10.1}{25}$	$\frac{7.8}{21}$	$\frac{7.8}{18}$	$\frac{8.7}{16}$	$\frac{8.2}{10}$	$\frac{8.1}{-}$	$\frac{8.6}{11}$	$\frac{8.9}{15}$	$\frac{6.4}{18}$	$\frac{5.9}{33}$
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$\frac{6.0}{33}$	$\frac{6.6}{20}$	$\frac{7.6}{15}$	$\frac{7.1}{14}$	$\frac{7.1}{-}$	$\frac{7.2}{12}$	$\frac{2.8}{16}$	$\frac{6.8}{19}$	$\frac{6.5}{29}$	$\frac{5.5}{33}$
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$\frac{3.0}{33}$	$\frac{4.4}{24}$	$\frac{5.3}{17}$	$\frac{6.1}{15}$	$\frac{5.6}{13}$	$\frac{5.3}{-}$	$\frac{5.9}{12}$	$\frac{6.0}{15}$	$\frac{5.1}{18}$	$\frac{4.5}{33}$
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$\frac{2.0}{33}$	$\frac{2.4}{23}$	$\frac{3.1}{16}$	$\frac{4.0}{15}$	$\frac{3.8}{11}$	$\frac{3.4}{-}$	$\frac{3.9}{10}$	$\frac{4.1}{15}$	$\frac{1.4}{19}$	$\frac{1.7}{33}$
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$\frac{9.1}{33}$	$\frac{9.5}{21}$	$\frac{10.1}{17}$	$\frac{10.7}{13}$	$\frac{10.2}{-}$	$\frac{10.7}{11}$	$\frac{10.6}{16}$	$\frac{9.0}{19}$	$\frac{8.8}{33}$
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$\frac{9.1}{33}$	$\frac{9.6}{16}$	$\frac{9.4}{12}$	$\frac{8.8}{-}$	$\frac{9.3}{11}$	$\frac{10.2}{20}$	$\frac{10.2}{33}$
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Sta-

+

x

-

Elev

1001.12

534+40

93.3

+75

94.4

535

95.2

B.M.

7.85

1004.04

4.93

996.19

+50

96.9

536

99.1

+P

9.09

1011.14

1.99

1002.05

+50

1002.1

537

05.1

+50

07.6

+55

07.9

+P

13.77

1022.78

2.13

1009.01

538

1010.0

+40

11.5

+75

13.0

4/

L

2+

$\frac{8.5}{33}$	$\frac{8.8}{19}$	$\frac{8.3}{12}$	$\frac{7.8}{11}$	$\frac{8.3}{11}$	$\frac{9.7}{19}$	$\frac{9.0}{33}$
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$\frac{7.6}{33}$	$\frac{7.4}{25}$	$\frac{7.6}{15}$	$\frac{7.2}{12}$	$\frac{6.7}{9}$	$\frac{7.0}{9}$	$\frac{7.2}{15}$	$\frac{6.5}{17}$	$\frac{5.7}{33}$
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$\frac{6.1}{32}$	$\frac{5.9}{17}$	$\frac{6.4}{16}$	$\frac{6.4}{12}$	$\frac{5.9}{9}$	$\frac{6.3}{10}$	$\frac{6.3}{15}$	$\frac{5.9}{19}$	$\frac{5.7}{33}$
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R.R. spike in B.D. 23 Rt. 535+03

$\frac{9.5}{33}$	$\frac{9.8}{30}$	$\frac{9.2}{24}$	$\frac{9.5}{21}$	$\frac{8.6}{19}$	$\frac{7.9}{13}$	$\frac{7.1}{11}$	$\frac{7.5}{10}$	$\frac{8.4}{15}$	$\frac{10.5}{21}$	$\frac{10.5}{33}$
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$\frac{8.3}{33}$	$\frac{8.1}{30}$	$\frac{7.2}{22}$	$\frac{6.7}{18}$	$\frac{6.0}{15}$	$\frac{5.4}{11}$	$\frac{4.9}{9}$	$\frac{5.5}{13}$	$\frac{8.4}{18}$	$\frac{9.2}{25}$	$\frac{9.4}{33}$
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$\frac{8.0}{33}$	$\frac{7.7}{28}$	$\frac{8.5}{20}$	$\frac{9.1}{16}$	$\frac{9.9}{14}$	$\frac{9.6}{11}$	$\frac{9.0}{9}$	$\frac{9.6}{5}$	$\frac{9.6}{16}$	$\frac{9.4}{18}$	$\frac{9.9}{23}$	$\frac{10.4}{24}$	$\frac{9.6}{36}$
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$\frac{4.6}{33}$	$\frac{4.0}{30}$	$\frac{4.8}{22}$	$\frac{5.9}{17}$	$\frac{7.1}{14}$	$\frac{6.5}{10}$	$\frac{6.0}{9}$	$\frac{6.5}{13}$	$\frac{6.2}{18}$	$\frac{2.5}{24}$	$\frac{2.1}{31}$	$\frac{2.1}{33}$
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$\frac{1.5}{33}$	$\frac{1.8}{27}$	$\frac{2.2}{21}$	$\frac{3.3}{19}$	$\frac{4.0}{14}$	$\frac{3.5}{9}$	$\frac{3.9}{10}$	$\frac{4.0}{12.5}$	$\frac{3.7}{15}$	$\frac{2.6}{18}$	$\frac{3.1}{25}$	$\frac{3.5}{33}$
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$\frac{2.9}{33}$	$\frac{2.7}{26}$	$\frac{2.8}{22}$	$\frac{3.5}{18}$	$\frac{3.8}{14}$	$\frac{3.2}{9}$	$\frac{3.5}{10}$	$\frac{3.3}{14}$	$\frac{2.5}{19}$	$\frac{3.4}{24}$	$\frac{3.5}{33}$
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yard	$\frac{13.9}{33}$	$\frac{13.9}{26}$	$\frac{14.1}{18}$	$\frac{13.3}{12}$	$\frac{12.8}{9}$	$\frac{13.1}{10}$	$\frac{13.5}{14}$	$\frac{13.9}{17}$	$\frac{14.5}{21}$	$\frac{15.0}{33}$
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yard	$\frac{11.2}{33}$	$\frac{12.3}{27}$	$\frac{11.9}{18}$	$\frac{12.2}{16}$	$\frac{11.7}{12}$	$\frac{11.3}{9}$	$\frac{11.4}{10}$	$\frac{11.5}{11}$	$\frac{11.6}{19}$	$\frac{11.5}{24}$	$\frac{11.6}{30}$	$\frac{10.9}{35}$
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yard	$\frac{10.2}{33}$	$\frac{10.3}{28}$	$\frac{10.3}{19}$	$\frac{10.7}{12}$	$\frac{9.8}{9}$	$\frac{10.0}{11}$	$\frac{9.8}{16}$	$\frac{6.9}{23}$	$\frac{7.4}{28}$	$\frac{7.4}{33}$
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Sta.	+	π	-	Elev
		1022.78		
539+15				1014.0
+55				14.3
540+00				14.4
T.P.	3.84	✓ 1018.21	8.41	✓ 1014.37
+50				13.3
				12.
541				12.2
+40		✓		10.6
T.P.	2.22	✓ 1010.13	10.30	✓ 1007.91
542+00				07.8
+50				05.5
543+00				03.4
+50				01.7
544+00				1000.9

LT.

Q

R+

19

Yard

$\frac{8.1}{33}$	$\frac{8.7}{18}$	$\frac{9.5}{16}$	$\frac{9.3}{14}$	$\frac{9.8}{14}$	$\frac{9.4}{14}$	$\frac{2.8}{21}$	$\frac{6.5}{28}$	$\frac{6.6}{33}$
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Yard

$\frac{8.3}{33}$	$\frac{8.3}{18}$	$\frac{9.0}{16}$	$\frac{8.5}{14}$	$\frac{8.6}{10.5}$	$\frac{8.2}{14}$	$\frac{0.9}{26}$	$\frac{1.6}{32}$	$\frac{2.4}{36}$	$\frac{2.6}{40}$
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$\frac{9.5}{33}$	$\frac{9.4}{30}$	$\frac{8.8}{18}$	$\frac{9.2}{15}$	$\frac{8.4}{14}$	$\frac{8.5}{13}$	$\frac{7.4}{16}$	$\frac{6.0}{21}$	$\frac{5.7}{33}$	$\frac{5.4}{40}$
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$\frac{6.1}{33}$	$\frac{5.5}{18}$	$\frac{5.7}{16}$	$\frac{4.9}{14}$	$\frac{4.9}{13}$	$\frac{3.3}{16.5}$	$\frac{1.0}{20}$	$\frac{1.3}{27}$	$\frac{0.6}{33}$
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$\frac{9.7}{33}$	$\frac{7.7}{21}$	$\frac{6.7}{15}$	$\frac{6.0}{14}$	$\frac{6.3}{13}$	$\frac{4.3}{17}$	$\frac{1.3}{22}$	$\frac{0.6}{28}$	$\frac{0.6}{33}$
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$\frac{14.6}{35}$	$\frac{12.3}{28}$	$\frac{9.1}{18}$	$\frac{8.2}{12}$	$\frac{7.6}{14}$	$\frac{7.8}{12}$	$\frac{7.9}{15}$	$\frac{5.2}{20}$	$\frac{3.5}{27}$	$\frac{2.8}{33}$
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$\frac{4.1}{33}$	$\frac{3.5}{22}$	$\frac{3.0}{14}$	$\frac{2.3}{14}$	$\frac{1.9}{12}$	$\frac{1.1}{21}$	$\frac{0.3}{33}$
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$\frac{8.0}{33}$	$\frac{7.3}{26}$	$\frac{6.1}{19}$	$\frac{5.3}{12}$	$\frac{4.6}{14}$	$\frac{4.7}{11}$	$\frac{5.7}{18}$	$\frac{4.8}{23}$	$\frac{3.8}{33}$
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Garden

$\frac{12.6}{33}$	$\frac{10.9}{21}$	$\frac{8.2}{14.5}$	$\frac{7.5}{11}$	$\frac{6.7}{14}$	$\frac{6.9}{16}$	$\frac{8.3}{21}$	$\frac{7.8}{28}$	$\frac{7.1}{33}$
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$\frac{14.2}{33}$	$\frac{13.0}{22}$	$\frac{9.7}{16}$	$\frac{9.2}{12}$	$\frac{8.4}{14}$	$\frac{8.5}{11}$	$\frac{8.8}{17}$	$\frac{9.9}{24}$	$\frac{9.1}{27}$	$\frac{8.7}{37}$
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$\frac{11.2}{33}$	$\frac{10.8}{27}$	$\frac{10.3}{17}$	$\frac{9.7}{8}$	$\frac{9.2}{14}$	$\frac{9.3}{12}$	$\frac{9.3}{21}$	$\frac{10.2}{24}$	$\frac{9.8}{27}$	$\frac{8.9}{33}$
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Sta	+	*	-	Elev
		1010.13		
B.M	0.56	✓ 1002.98	7.71	✓ 1002.42
544+50				1000.3
545+00				999.8
+50				998.9
546+00				998.0
+50				997.0
+80				996.3
547+00				995.7
T.P	3.07	✓ 998.73	7.32	✓ 995.66
+50				994.0
548				991.6
+50				989.0
T.P	2.20	✓ 990.34	10.59	988.14
549+00				985.7

LT

E

RT

20

Top of Hydrant N.W. Cor. Intersection Co. B & 1st ave. N.W.

Hedge	$\frac{4.5}{33}$	$\frac{4.1}{23}$	$\frac{3.6}{12}$	$\frac{2.7}{11}$	$\frac{2.5}{14}$	$\frac{2.2}{25}$	$\frac{1.9}{33}$
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Hedge	$\frac{4.1}{33}$	$\frac{3.7}{19}$	$\frac{4.0}{11}$	3.2	$\frac{3.3}{11}$	$\frac{3.8}{19}$	$\frac{3.2}{19}$	$\frac{3.1}{28}$	$\frac{2.9}{33}$
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Hedge	$\frac{4.6}{33}$	$\frac{4.7}{23}$	$\frac{5.0}{15}$	$\frac{4.9}{11}$	$\frac{4.1}{11}$	$\frac{4.2}{12}$	$\frac{4.5}{17}$	$\frac{4.2}{19}$	$\frac{3.1}{25}$	$\frac{2.4}{33}$ yard
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Hedge	$\frac{3.8}{33}$	$\frac{4.3}{21}$	$\frac{4.8}{15}$	$\frac{5.7}{12}$	5.0	$\frac{5.9}{14}$	$\frac{5.1}{23}$	$\frac{5.0}{33}$	yard
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yard	$\frac{3.2}{33}$	$\frac{3.7}{24}$	$\frac{4.8}{17}$	$\frac{6.6}{12}$	6.0	$\frac{6.4}{14}$	$\frac{6.6}{18}$	$\frac{4.3}{22}$	$\frac{4.4}{28}$	$\frac{4.9}{33}$ yard
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yard	$\frac{3.5}{33}$	$\frac{4.1}{25}$	$\frac{5.0}{18}$	$\frac{6.8}{13}$	$\frac{7.4}{9}$	6.7	$\frac{7.5}{15}$	$\frac{5.4}{19}$	$\frac{2.2}{27}$	$\frac{2.2}{30}$	$\frac{2.8}{33}$ yard
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yard	$\frac{4.3}{33}$	$\frac{4.6}{23}$	$\frac{5.6}{16}$	$\frac{7.8}{10}$	7.3	$\frac{7.9}{16}$	$\frac{5.1}{22}$	$\frac{2.7}{30}$	$\frac{2.6}{33}$	yard
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yard	$\frac{3.3}{33}$	$\frac{3.3}{30}$	$\frac{3.9}{17}$	$\frac{5.6}{12}$	$\frac{5.1}{10}$	4.7	$\frac{4.9}{10}$	$\frac{5.0}{15}$	$\frac{1.3}{21}$	$\frac{+0.5}{33}$	yard
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yard	$\frac{6.6}{34}$	$\frac{6.6}{31}$	$\frac{6.8}{16}$	$\frac{7.8}{11}$	7.1	$\frac{7.5}{14}$	$\frac{4.8}{19}$	$\frac{4.3}{29}$	$\frac{4.0}{33}$	yard
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	$\frac{11.3}{33}$	$\frac{11.1}{30}$	$\frac{10.0}{15}$	$\frac{10.6}{12}$	9.7	$\frac{9.9}{11}$	$\frac{8.8}{20}$	$\frac{6.3}{27}$	$\frac{5.8}{33}$	yard
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	$\frac{10.3}{33}$	$\frac{9.4}{24}$	$\frac{8.1}{17}$	$\frac{5.1}{9}$	4.6	$\frac{4.6}{12}$	$\frac{5.1}{19}$	$\frac{1.0}{29}$	$\frac{0.2}{33}$	yard
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Sta	+	π	-	Elev
		990.34		
549+50				982.1
550+00		980.46		979.6
T.P.	1.17	(980.26)	11.05	979.29 ✓
+ 22				978.7
+ 50				77.5
551+00				76.1
B.M.			2.83	977.63
				(977.43)

Lt

E

Rt

$\frac{16.3}{3.3}$	$\frac{13.3}{2.2}$	$\frac{9.0}{1.3}$	$\frac{8.4}{.8}$	8.2	$\frac{8.0}{1.3}$	$\frac{8.4}{1.7}$	$\frac{5.6}{2.6}$	$\frac{4.4}{3.3}$
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yard

Pasture

$\frac{17.3}{3.3}$	$\frac{15.1}{2.1}$	$\frac{11.6}{1.3}$	10.7	$\frac{11.4}{1.5}$	$\frac{8.9}{2.3}$	$\frac{8.2}{3.3}$
--------------------	--------------------	--------------------	------	--------------------	-------------------	-------------------

yard

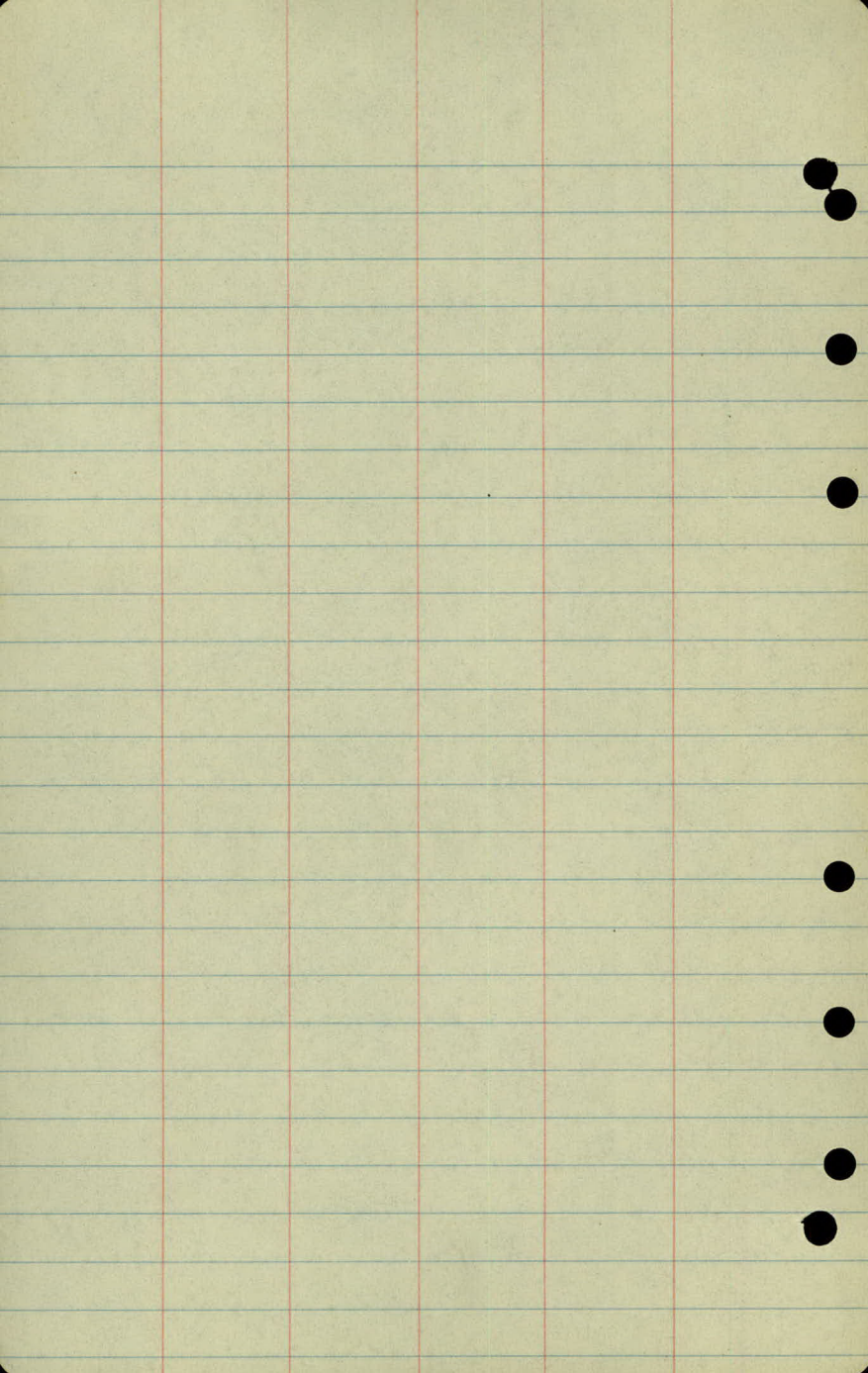
$\frac{6.9}{3.3}$	$\frac{5.8}{2.5}$	$\frac{4.2}{1.5}$	$\frac{2.4}{1.0}$	1.8	$\frac{2.0}{1.3}$	$\frac{3.0}{1.7}$	$\frac{2.40}{Flowline}$	$\frac{1.8}{2.4}$	$\frac{1.9}{3.3}$	yard
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$\frac{6.4}{3.3}$	$\frac{5.3}{1.6}$	$\frac{3.9}{1.2}$	$\frac{3.0}{1.3}$	$\frac{3.2}{1.7}$	$\frac{3.6}{2.9}$	$\frac{3.5}{3.3}$
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yard

$\frac{9.2}{3.3}$	$\frac{8.8}{1.9}$	$\frac{5.1}{1.3}$	$\frac{4.9}{1.0}$	4.4	$\frac{4.7}{1.1}$	$\frac{6.2}{1.8}$	$\frac{6.5}{2.6}$	$\frac{6.5}{3.3}$
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Top of Hydrant 17' Lt - Sta 557 + 20



+

A

-

Elev

B.M.

B.M.

1.00

978.63

(978.43)

977.63

(977.43)

551 +50

74.6

552

73.6

+40

73.6

553

74.0

+35

75.1

554

T.P.

9.30

985.95

-1.98

77.2

976.65

+50

78.7

555

80.7

+50

82.4

T.P.

7.54

991.55

-1.94

984.01

556

84.2

Top Hyd. 17' Lt. Sta. 551+20

9.1	8.8	7.6	5.3	4.4	4.0	4.2	5.9	5.5	5.1
$\frac{9.1}{33}$	$\frac{8.8}{28}$	$\frac{7.6}{20}$	$\frac{5.3}{14}$	$\frac{4.4}{10}$	$\frac{4.0}{-}$	$\frac{4.2}{12}$	$\frac{5.9}{19}$	$\frac{5.5}{28}$	$\frac{5.1}{33}$

9.4	7.9	6.2	5.6	5.0	5.2	7.2	7.5	7.0
$\frac{9.4}{33}$	$\frac{7.9}{21}$	$\frac{6.2}{15}$	$\frac{5.6}{10}$	$\frac{5.0}{-}$	$\frac{5.2}{12}$	$\frac{7.2}{20}$	$\frac{7.5}{25}$	$\frac{7.0}{33}$

9.3	9.1	5.6	5.0	5.3	9.3	8.1
$\frac{9.3}{33}$	$\frac{9.1}{24}$	$\frac{5.6}{11}$	$\frac{5.0}{-}$	$\frac{5.3}{10}$	$\frac{9.3}{21}$	$\frac{8.1}{33}$

7.1	7.0	5.0	4.6	4.5	5.6	6.0	5.0
$\frac{7.1}{33}$	$\frac{7.0}{20}$	$\frac{5.0}{13}$	$\frac{4.6}{-}$	$\frac{4.5}{12}$	$\frac{5.6}{21}$	$\frac{6.0}{22}$	$\frac{5.0}{33}$

4.0	4.1	4.6	4.0	3.5	3.7	3.9	4.1	2.4	2.0
$\frac{4.0}{33}$	$\frac{4.1}{24}$	$\frac{4.6}{18}$	$\frac{4.0}{15}$	$\frac{3.5}{-}$	$\frac{3.7}{11}$	$\frac{3.9}{20}$	$\frac{4.1}{23}$	$\frac{2.4}{29}$	$\frac{2.0}{33}$

+0.2	0.6	2.0	2.3	1.4	2.0	2.5	1.3	1.0	0.1
$\frac{+0.2}{33}$	$\frac{0.6}{25}$	$\frac{2.0}{19}$	$\frac{2.3}{15}$	$\frac{1.4}{-}$	$\frac{2.0}{10}$	$\frac{2.5}{14}$	$\frac{1.3}{16}$	$\frac{1.0}{22}$	$\frac{0.1}{33}$

7.9	7.6	7.5	7.8	7.3	7.8	6.4	5.6	5.0
$\frac{7.9}{33}$	$\frac{7.6}{24}$	$\frac{7.5}{18}$	$\frac{7.8}{14}$	$\frac{7.3}{-}$	$\frac{7.8}{9}$	$\frac{6.4}{16}$	$\frac{5.6}{23}$	$\frac{5.0}{33}$

4.9	4.5	6.2	5.7	5.3	4.7	4.3	3.6	3.0
$\frac{4.9}{33}$	$\frac{4.5}{22}$	$\frac{6.2}{16}$	$\frac{5.7}{13}$	$\frac{5.3}{-}$	$\frac{4.7}{15}$	$\frac{4.3}{21}$	$\frac{3.6}{29}$	$\frac{3.0}{33}$

3.6	3.4	3.3	4.2	3.6	3.8	4.3	2.5	2.1	1.8
$\frac{3.6}{33}$	$\frac{3.4}{27}$	$\frac{3.3}{22}$	$\frac{4.2}{15}$	$\frac{3.6}{-}$	$\frac{3.8}{8}$	$\frac{4.3}{11}$	$\frac{2.5}{16}$	$\frac{2.1}{29}$	$\frac{1.8}{33}$

7.3	7.1	6.9	8.2	7.9	7.4	7.7	8.2	4.5	3.7
$\frac{7.3}{33}$	$\frac{7.1}{24}$	$\frac{6.9}{23}$	$\frac{8.2}{18}$	$\frac{7.9}{14}$	$\frac{7.4}{-}$	$\frac{7.7}{7}$	$\frac{8.2}{12}$	$\frac{4.5}{18}$	$\frac{3.7}{33}$

+	X ✓	-	Elev
	991.55		

556 + 50		85.7
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557		86.6
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+50	- App 2 May.	88.2 ✓
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T.P.	8.75	997.43 ✓	2.27	989.28
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B.M.	5.45	997.43 ✓	5.45	991.98 ✓
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558 + 0		89.3
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+50		91.3
-----	--	------

559		93.4 ✓
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T.P.	9.29	1004.57 ✓	2.16	996.28
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+45		95.6
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560 + 00		98.3
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+50		100.7
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561 + 00		103.4
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T.P.	10.04	1013.46 ✓	1.15	1003.42 ✓
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+50		105.0
-----	--	-------

LT

C

RT

$\frac{7.8}{3.3}$	$\frac{7.4}{2.8}$	$\frac{6.5}{2.2}$	$\frac{6.1}{1.9}$	$\frac{6.3}{1.3}$	$\frac{5.9}{-}$	$\frac{6.3}{2}$	$\frac{6.5}{1.3}$	$\frac{7.2}{1.5}$	$\frac{6.0}{1.5}$	$\frac{4.1}{2.1}$	$\frac{3.3}{3.3}$
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$\frac{6.7}{3.3}$	$\frac{5.5}{3.0}$	$\frac{4.8}{2.2}$	$\frac{5.6}{1.9}$	$\frac{5.5}{1.6}$	$\frac{5.3}{1.4}$	$\frac{5.0}{-}$	$\frac{5.1}{8}$	$\frac{5.3}{1.3}$	$\frac{5.8}{1.6}$	$\frac{5.3}{1.7}$	$\frac{4.4}{2.2}$	$\frac{4.3}{2.8}$	$\frac{3.7}{3.3}$
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$\frac{4.1}{5.0}$	$\frac{3.8}{2.1}$	3.4	$\frac{3.1}{2.5}$	$\frac{2.8}{5.0}$
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Kyd. N.E. Corner Margret

$\frac{8.1}{3.3}$	$\frac{8.2}{2.7}$	$\frac{8.4}{2.0}$	$\frac{8.9}{1.7}$	$\frac{8.5}{1.2}$	$\frac{8.1}{-}$	$\frac{8.3}{7}$	$\frac{8.3}{1.1}$	$\frac{8.5}{1.4}$	$\frac{7.6}{1.6}$	$\frac{7.5}{2.7}$	$\frac{8.0}{3.3}$
-------------------	-------------------	-------------------	-------------------	-------------------	-----------------	-----------------	-------------------	-------------------	-------------------	-------------------	-------------------

$\frac{6.3}{3.3}$	$\frac{6.6}{2.4}$	$\frac{6.4}{2.1}$	$\frac{7.1}{2.0}$	$\frac{6.7}{1.6}$	$\frac{6.1}{-}$	$\frac{6.5}{9}$	$\frac{6.7}{1.1}$	$\frac{6.8}{1.4}$	$\frac{5.9}{1.6}$	$\frac{4.8}{1.9}$	$\frac{4.1}{3.2}$
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$\frac{4.6}{3.3}$	$\frac{4.6}{2.8}$	$\frac{4.4}{2.0}$	$\frac{4.9}{1.9}$	$\frac{4.4}{1.5}$	$\frac{4.0}{-}$	$\frac{4.3}{7}$	$\frac{4.4}{1.4}$	$\frac{2.4}{1.8}$	$\frac{2.1}{2.7}$	$\frac{1.4}{3.3}$
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$\frac{9.1}{3.3}$	$\frac{9.2}{2.5}$	$\frac{8.8}{2.0}$	$\frac{9.9}{1.8}$	$\frac{9.7}{1.4}$	$\frac{9.0}{-}$	$\frac{9.1}{1.0}$	$\frac{9.6}{1.1}$	$\frac{9.9}{1.4}$	$\frac{8.2}{1.6}$	$\frac{5.4}{2.4}$	$\frac{6.5}{3.1}$	$\frac{6.5}{3.3}$
-------------------	-------------------	-------------------	-------------------	-------------------	-----------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

Hedge

$\frac{5.9}{3.3}$	$\frac{5.9}{2.0}$	$\frac{7.1}{1.8}$	$\frac{6.7}{1.4}$	$\frac{6.3}{-}$	$\frac{6.7}{8}$	$\frac{7.3}{1.5}$	$\frac{5.3}{2.3}$	$\frac{4.7}{3.3}$
-------------------	-------------------	-------------------	-------------------	-----------------	-----------------	-------------------	-------------------	-------------------

Hedge

$\frac{3.7}{3.3}$	$\frac{3.5}{2.0}$	$\frac{4.1}{2.4}$	$\frac{3.2}{2.0}$	$\frac{4.5}{1.7}$	$\frac{4.3}{1.4}$	$\frac{3.9}{-}$	$\frac{4.2}{7}$	$\frac{4.4}{1.5}$	$\frac{2.9}{2}$	$\frac{2.3}{2.9}$	$\frac{2.4}{3.3}$
-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-----------------	-----------------	-------------------	-----------------	-------------------	-------------------

$\frac{2.9}{3.3}$	$\frac{2.4}{2.0}$	$\frac{1.8}{2.2}$	$\frac{1.7}{1.5}$	$\frac{1.2}{-}$	$\frac{1.5}{9}$	$\frac{1.8}{1.6}$	$\frac{2.6}{1.9}$	$\frac{0.2}{2.9}$	$\frac{1.0}{3.3}$
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$\frac{8.9}{3.3}$	$\frac{8.8}{2.0}$	$\frac{9.0}{1.8}$	$\frac{9.1}{1.4}$	$\frac{8.5}{-}$	$\frac{8.7}{8}$	$\frac{9.2}{1.4}$	$\frac{6.3}{1.9}$	$\frac{5.2}{2.5}$	$\frac{5.7}{3.3}$
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Sta + π - Elev

✓
1013.46

562+00

06.2 ✓

+50

07.0 ✓

563+00

06.5 ✓

T.P.

5.66 1012.53 6.59 1006.87

+50

06.7

564+00

06.5

+40

approx 4 Charles St. N.E. to Lost

B.M.

3.77 1012.53 3.77 1008.76

565+00

07.0 ✓

+50

06.6

566+00

05.7

+50

04.8 ✓

T.P.

8.82 1003.71

Lt

L

Pt

$$\begin{array}{r} 9.8 \\ 33 \end{array} \quad \begin{array}{r} 7.7 \\ 19 \end{array} \quad 7.3 \quad \begin{array}{r} 7.6 \\ 6 \end{array} \quad \begin{array}{r} 8.4 \\ 13 \end{array} \quad \begin{array}{r} 3.2 \\ 22 \end{array} \quad \begin{array}{r} 2.3 \\ 20 \end{array} \quad \begin{array}{r} 2.5 \\ 33 \end{array}$$

$$\begin{array}{r} 8.5 \\ 33 \end{array} \quad \begin{array}{r} 8.7 \\ 30 \end{array} \quad \begin{array}{r} 7.4 \\ 18 \end{array} \quad \begin{array}{r} 6.8 \\ 13 \end{array} \quad 6.5 \quad \begin{array}{r} 6.7 \\ 10 \end{array} \quad \begin{array}{r} 7.5 \\ 14 \end{array} \quad \begin{array}{r} 4.7 \\ 20 \end{array} \quad \begin{array}{r} 2.9 \\ 27 \end{array} \quad \begin{array}{r} 2.6 \\ 29.0 \end{array} \quad \text{Hedge} \quad \begin{array}{r} 2.6 \\ 33 \end{array}$$

$$\begin{array}{r} 9.4 \\ 33 \end{array} \quad \begin{array}{r} 8.1 \\ 20 \end{array} \quad \begin{array}{r} 7.3 \\ 14 \end{array} \quad 7.0 \quad \begin{array}{r} 7.1 \\ 11 \end{array} \quad \begin{array}{r} 7.5 \\ 14 \end{array} \quad \begin{array}{r} 4.3 \\ 20 \end{array} \quad \begin{array}{r} 3.9 \\ 25 \end{array} \quad \begin{array}{r} 3.0 \\ 29 \end{array} \quad \begin{array}{r} 2.4 \\ 33 \end{array}$$

$$\begin{array}{r} 7.9 \\ 33 \end{array} \quad \begin{array}{r} 9.7 \\ 31 \end{array} \quad \begin{array}{r} 8.5 \\ 23 \end{array} \quad \begin{array}{r} 6.8 \\ 17 \end{array} \quad \begin{array}{r} 6.0 \\ 14 \end{array} \quad 5.8 \quad \begin{array}{r} 6.0 \\ 11 \end{array} \quad \begin{array}{r} 6.4 \\ 14 \end{array} \quad \begin{array}{r} 5.8 \\ 16 \end{array} \quad \begin{array}{r} 4.1 \\ 23 \end{array} \quad \begin{array}{r} 2.7 \\ 33 \end{array}$$

$$\begin{array}{r} 11.0 \\ 33 \end{array} \quad \begin{array}{r} 10.0 \\ 24 \end{array} \quad \begin{array}{r} 7.3 \\ 18 \end{array} \quad \begin{array}{r} 6.5 \\ 13 \end{array} \quad 6.0 \quad \begin{array}{r} 6.1 \\ 8 \end{array} \quad \begin{array}{r} 6.3 \\ 14 \end{array} \quad \begin{array}{r} 5.4 \\ 18 \end{array} \quad \begin{array}{r} 4.6 \\ 33 \end{array}$$

$$\begin{array}{r} 8.1 \\ 50 \end{array} \quad \begin{array}{r} 7.2 \\ 25 \end{array} \quad \begin{array}{r} 6.2 \\ 11 \end{array} \quad 5.8 \quad \begin{array}{r} 6.0 \\ 14 \end{array} \quad \begin{array}{r} 4.8 \\ 20 \end{array} \quad \begin{array}{r} 3.9 \\ 28 \end{array} \quad \begin{array}{r} 3.1 \\ 33 \end{array}$$

Hydrant NE corner Charles & South

8834

$$\begin{array}{r} 6.7 \\ 33 \end{array} \quad \begin{array}{r} 4.7 \\ 23 \end{array} \quad \begin{array}{r} 4.1 \\ 17 \end{array} \quad \begin{array}{r} 6.2 \\ 15 \end{array} \quad \begin{array}{r} 6.0 \\ 11 \end{array} \quad 5.5 \quad \begin{array}{r} 5.3 \\ 14 \end{array} \quad \begin{array}{r} 4.7 \\ 18 \end{array} \quad \begin{array}{r} 0.0 \\ 33 \end{array}$$

$$\begin{array}{r} 4.3 \\ 33 \end{array} \quad \begin{array}{r} 3.6 \\ 18 \end{array} \quad \begin{array}{r} 6.4 \\ 13 \end{array} \quad \begin{array}{r} 6.3 \\ 11 \end{array} \quad 5.9 \quad \begin{array}{r} 6.2 \\ 10 \end{array} \quad \begin{array}{r} 6.3 \\ 15 \end{array} \quad \begin{array}{r} 3.0 \\ 20 \end{array} \quad \begin{array}{r} 2.1 \\ 26 \end{array} \quad \begin{array}{r} 2.5 \\ 28 \end{array} \quad \begin{array}{r} 2.8 \\ 30 \end{array} \quad \begin{array}{r} 2.3 \\ 33 \end{array}$$

$$\begin{array}{r} 6.1 \\ 33 \end{array} \quad \begin{array}{r} 6.3 \\ 25 \end{array} \quad \begin{array}{r} 6.2 \\ 17 \end{array} \quad \begin{array}{r} 7.6 \\ 12 \end{array} \quad \begin{array}{r} 7.3 \\ 8.5 \end{array} \quad 6.8 \quad \begin{array}{r} 7.1 \\ 9 \end{array} \quad \begin{array}{r} 7.3 \\ 14 \end{array} \quad \begin{array}{r} 6.1 \\ 19 \end{array} \quad \begin{array}{r} 5.7 \\ 23 \end{array} \quad \begin{array}{r} 5.4 \\ 33 \end{array}$$

$$\begin{array}{r} 5.2 \\ 33 \end{array} \quad \begin{array}{r} 4.2 \\ 29 \end{array} \quad \begin{array}{r} 5.0 \\ 17 \end{array} \quad \begin{array}{r} 8.5 \\ 11 \end{array} \quad \begin{array}{r} 6.3 \\ 8 \end{array} \quad 7.7 \quad \begin{array}{r} 8.1 \\ 10 \end{array} \quad \begin{array}{r} 8.5 \\ 15 \end{array} \quad \begin{array}{r} 6.3 \\ 19 \end{array} \quad \begin{array}{r} 6.5 \\ 25 \end{array} \quad \begin{array}{r} 7.3 \\ 28 \end{array} \quad \begin{array}{r} 7.6 \\ 33 \end{array}$$

T.P.

2.70

✓
1005.91

1003.71

567

0
03.7

+50

02.5

568

01.7

+50

01.2

569

00.8

+40

00.4

569+80

00.1

21.

2

24.

$$\begin{array}{r} 0.5 \\ 33 \end{array} \quad \begin{array}{r} 1.3 \\ 16 \end{array} \quad \begin{array}{r} 2.9 \\ 12 \end{array} \quad \begin{array}{r} 2.7 \\ 9 \end{array} \quad \begin{array}{r} 2.2 \\ 11 \end{array} \quad \begin{array}{r} 2.6 \\ 11 \end{array} \quad \begin{array}{r} 2.9 \\ 15 \end{array} \quad \begin{array}{r} 1.8 \\ 19 \end{array} \quad \begin{array}{r} 1.9 \\ 24 \end{array} \quad \begin{array}{r} 2.0 \\ 33 \end{array}$$

$$\begin{array}{r} 4.6 \\ 33 \end{array} \quad \begin{array}{r} 4.3 \\ 18 \end{array} \quad \begin{array}{r} 3.8 \\ 10 \end{array} \quad \begin{array}{r} 3.4 \\ 11 \end{array} \quad \begin{array}{r} 3.9 \\ 11 \end{array} \quad \begin{array}{r} 4.2 \\ 18 \end{array} \quad \begin{array}{r} 3.5 \\ 22 \end{array} \quad \begin{array}{r} 2.8 \\ 33 \end{array}$$

$$\begin{array}{r} 6.3 \\ 33 \end{array} \quad \begin{array}{r} 5.8 \\ 24 \end{array} \quad \begin{array}{r} 5.5 \\ 15 \end{array} \quad \begin{array}{r} 4.7 \\ 10 \end{array} \quad \begin{array}{r} 4.2 \\ 11 \end{array} \quad \begin{array}{r} 4.5 \\ 11 \end{array} \quad \begin{array}{r} 4.8 \\ 17 \end{array} \quad \begin{array}{r} 4.3 \\ 23 \end{array} \quad \begin{array}{r} 4.0 \\ 33 \end{array}$$

$$\begin{array}{r} 6.5 \\ 33 \end{array} \quad \begin{array}{r} 6.0 \\ 19 \end{array} \quad \begin{array}{r} 5.1 \\ 9 \end{array} \quad \begin{array}{r} 4.7 \\ 10 \end{array} \quad \begin{array}{r} 5.1 \\ 10 \end{array} \quad \begin{array}{r} 5.2 \\ 14 \end{array} \quad \begin{array}{r} 4.8 \\ 16 \end{array} \quad \begin{array}{r} 4.1 \\ 23 \end{array} \quad \begin{array}{r} 3.8 \\ 33 \end{array}$$

$$\begin{array}{r} 7.6 \\ 33 \end{array} \quad \begin{array}{r} 7.4 \\ 21 \end{array} \quad \begin{array}{r} 6.6 \\ 18 \end{array} \quad \begin{array}{r} 6.1 \\ 14 \end{array} \quad \begin{array}{r} 5.5 \\ 10 \end{array} \quad \begin{array}{r} 5.1 \\ 10 \end{array} \quad \begin{array}{r} 5.4 \\ 20 \end{array} \quad \begin{array}{r} 5.4 \\ 20 \end{array} \quad \begin{array}{r} 4.2 \\ 26 \end{array} \quad \begin{array}{r} 3.7 \\ 33 \end{array}$$

$$\begin{array}{r} 4.4 \\ 33 \end{array} \quad \begin{array}{r} 5.1 \\ 19 \end{array} \quad \begin{array}{r} 6.3 \\ 16 \end{array} \quad \begin{array}{r} 5.8 \\ 10 \end{array} \quad \begin{array}{r} 5.5 \\ 11 \end{array} \quad \begin{array}{r} 5.8 \\ 11 \end{array} \quad \begin{array}{r} 5.3 \\ 14 \end{array} \quad \begin{array}{r} 3.6 \\ 21 \end{array} \quad \begin{array}{r} 2.9 \\ 33 \end{array}$$

$$\begin{array}{r} 6.1 \\ 33 \end{array} \quad \begin{array}{r} 5.0 \\ 24 \end{array} \quad \begin{array}{r} 7.6 \\ 19 \end{array} \quad \begin{array}{r} 6.3 \\ 11 \end{array} \quad \begin{array}{r} 5.8 \\ 10 \end{array} \quad \begin{array}{r} 6.2 \\ 10 \end{array} \quad \begin{array}{r} 6.6 \\ 14 \end{array} \quad \begin{array}{r} 5.6 \\ 20 \end{array} \quad \begin{array}{r} 2.7 \\ 22 \end{array} \quad \begin{array}{r} 2.0 \\ 33 \end{array}$$

Sta.	+	π ✓	-	Elev	✓
B.M.	7.40	1004.27	9.04		996.87

570 00.0

+25 99.6

+ 1/2 App. St. South 99.2

+65 98.8

+83 App. St. North 98.8 ✓

B.M. as Above 6.37 1003.24 7.40 996.87

571 98.7

+50 98.7

572 98.9

+30 98.7

+65 98.2

573 98.2

A. # Rt.

R.R. Spike in Po. P. 50' Lt. 1st. 570+55

$\frac{6.0}{33}$	$\frac{5.2}{22}$	$\frac{5.8}{17}$	$\frac{4.8}{11}$	43	$\frac{4.7}{9}$	$\frac{4.9}{27}$	$\frac{0.3}{33}$	$\frac{0.3}{50}$
------------------	------------------	------------------	------------------	----	-----------------	------------------	------------------	------------------

$\frac{8.2}{33}$	$\frac{6.8}{18}$	$\frac{5.6}{13}$	$\frac{5.2}{10}$	$\frac{4.7}{9}$	$\frac{4.5}{9}$	$\frac{4.0}{24}$	$\frac{7.2}{29}$	$\frac{1.8}{33}$	$\frac{1.1}{50}$
------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{8.9}{40}$	$\frac{7.9}{19}$	$\frac{6.0}{14}$	$\frac{5.2}{9}$	$\frac{5.1}{9}$	$\frac{4.9}{10}$		$\frac{3.7}{28}$	$\frac{2.2}{50}$
------------------	------------------	------------------	-----------------	-----------------	------------------	--	------------------	------------------

$\frac{8.8}{40}$	$\frac{7.9}{27}$	$\frac{6.8}{23}$	$\frac{5.8}{10}$	$\frac{5.5}{9}$	$\frac{5.5}{10}$	$\frac{5.2}{18}$	$\frac{4.2}{26}$	$\frac{3.3}{37}$
------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------

$\frac{7.8}{50}$	$\frac{6.2}{18}$		$\frac{5.8}{10}$	$\frac{5.5}{9}$	$\frac{5.6}{10}$	$\frac{6.0}{13}$	$\frac{5.7}{22}$	$\frac{4.8}{28}$	$\frac{4.4}{33}$
------------------	------------------	--	------------------	-----------------	------------------	------------------	------------------	------------------	------------------

$\frac{7.0}{33}$		$\frac{5.9}{22}$	$\frac{4.8}{10}$	45	$\frac{4.7}{8}$	$\frac{5.1}{14}$	$\frac{4.5}{21}$	$\frac{4.2}{28}$	$\frac{4.0}{33}$
------------------	--	------------------	------------------	----	-----------------	------------------	------------------	------------------	------------------

$\frac{6.6}{33}$	$\frac{5.2}{12}$	$\frac{4.8}{9}$	$\frac{4.5}{9}$	$\frac{4.6}{9}$	$\frac{5.2}{15}$	$\frac{4.7}{19}$		$\frac{4.2}{33}$
------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	--	------------------

$\frac{5.2}{33}$	$\frac{5.2}{30}$	$\frac{6.2}{24}$	$\frac{5.7}{15}$	$\frac{4.7}{9}$	43	$\frac{4.6}{10}$	$\frac{4.8}{13}$	$\frac{5.4}{15}$	$\frac{5.5}{17}$	$\frac{4.1}{19}$	$\frac{3.8}{33}$
------------------	------------------	------------------	------------------	-----------------	----	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{4.5}{33}$	$\frac{6.6}{28}$	$\frac{6.8}{20}$	$\frac{5.6}{15}$	$\frac{4.7}{9}$	$\frac{4.5}{9}$	$\frac{5.0}{9}$	$\frac{5.8}{15}$	$\frac{5.7}{22}$	$\frac{6.1}{28}$	$\frac{5.7}{33}$
------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{7.1}{33}$	$\frac{7.0}{18}$	$\frac{5.5}{14}$	$\frac{5.2}{8}$	$\frac{5.0}{9}$	$\frac{5.7}{10}$	$\frac{6.0}{15}$	$\frac{7.2}{20}$		$\frac{7.4}{33}$
------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------	--	------------------

$\frac{7.7}{33}$	$\frac{7.4}{17}$	$\frac{5.8}{13}$	$\frac{5.2}{8}$	$\frac{5.0}{9}$	$\frac{5.6}{10}$	$\frac{6.0}{14}$	$\frac{7.6}{19}$		$\frac{8.0}{33}$
------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------	--	------------------

Sta.	+	Σ ✓	-	Elev.
		1003.24		
573+50				98.5
574+0				99.1
+50		✓		99.3
T.P.	12.99	1015.16	1.07	✓ 1002.17
575				02.2
+50				04.5
576				06.6
+50				08.1
+75				09.0
196.04 ± E. Co. Line.				09.4
B.M.			4.93	✓ 1010.23

H.

E

Rt.

Camp Winding

$$\begin{array}{r} 66 \\ 33 \\ \hline \end{array} \quad \begin{array}{r} 63 \\ 24 \\ \hline \end{array} \quad \begin{array}{r} 68 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 54 \\ 12 \\ \hline \end{array} \quad \begin{array}{r} 49 \\ 8 \\ \hline \end{array} \quad \begin{array}{r} 47 \\ \hline \end{array} \quad \begin{array}{r} 53 \\ 11 \\ \hline \end{array} \quad \begin{array}{r} 61 \\ 17 \\ \hline \end{array} \quad \begin{array}{r} 73 \\ 19 \\ \hline \end{array} \quad \begin{array}{r} 75 \\ 33 \\ \hline \end{array}$$

$$\begin{array}{r} 50 \\ 33 \\ \hline \end{array} \quad \begin{array}{r} 46 \\ 23 \\ \hline \end{array} \quad \begin{array}{r} 51 \\ 18 \\ \hline \end{array} \quad \begin{array}{r} 43 \\ 9 \\ \hline \end{array} \quad \begin{array}{r} 41 \\ 2 \\ \hline \end{array} \quad \begin{array}{r} 41 \\ 0 \\ \hline \end{array} \quad \begin{array}{r} 47 \\ 11 \\ \hline \end{array} \quad \begin{array}{r} 53 \\ 14 \\ \hline \end{array} \quad \begin{array}{r} 63 \\ 17 \\ \hline \end{array} \quad \begin{array}{r} 64 \\ 33 \\ \hline \end{array}$$

$$\begin{array}{r} 20 \\ 33 \\ \hline \end{array} \quad \begin{array}{r} 27 \\ 22 \\ \hline \end{array} \quad \begin{array}{r} 29 \\ 14 \\ \hline \end{array} \quad \begin{array}{r} 34 \\ 12 \\ \hline \end{array} \quad \begin{array}{r} 35 \\ 8 \\ \hline \end{array} \quad \begin{array}{r} 31 \\ \hline \end{array} \quad \begin{array}{r} 35 \\ 10 \\ \hline \end{array} \quad \begin{array}{r} 43 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 53 \\ 26 \\ \hline \end{array} \quad \begin{array}{r} 53 \\ 33 \\ \hline \end{array}$$

$$\begin{array}{r} 98 \\ 33 \\ \hline \end{array} \quad \begin{array}{r} 102 \\ 23 \\ \hline \end{array} \quad \begin{array}{r} 131 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 130 \\ 11 \\ \hline \end{array} \quad \begin{array}{r} 134 \\ 9 \\ \hline \end{array} \quad \begin{array}{r} 130 \\ \hline \end{array} \quad \begin{array}{r} 138 \\ 12 \\ \hline \end{array} \quad \begin{array}{r} 139 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 148 \\ 28 \\ \hline \end{array} \quad \begin{array}{r} 151 \\ 33 \\ \hline \end{array}$$

$$\begin{array}{r} 112 \\ 33 \\ \hline \end{array} \quad \begin{array}{r} 77 \\ 20 \\ \hline \end{array} \quad \begin{array}{r} 104 \\ 17 \\ \hline \end{array} \quad \begin{array}{r} 112 \\ 11 \\ \hline \end{array} \quad \begin{array}{r} 111 \\ 8 \\ \hline \end{array} \quad \begin{array}{r} 107 \\ \hline \end{array} \quad \begin{array}{r} 112 \\ 11 \\ \hline \end{array} \quad \begin{array}{r} 116 \\ 13 \\ \hline \end{array} \quad \begin{array}{r} 110 \\ 19 \\ \hline \end{array} \quad \begin{array}{r} 112 \\ 33 \\ \hline \end{array}$$

$$\begin{array}{r} 59 \\ 33 \\ \hline \end{array} \quad \begin{array}{r} 58 \\ 19 \\ \hline \end{array} \quad \begin{array}{r} 78 \\ 15 \\ \hline \end{array} \quad \begin{array}{r} 90 \\ 12 \\ \hline \end{array} \quad \begin{array}{r} 90 \\ 8 \\ \hline \end{array} \quad \begin{array}{r} 86 \\ \hline \end{array} \quad \begin{array}{r} 90 \\ 11 \\ \hline \end{array} \quad \begin{array}{r} 92 \\ 15 \\ \hline \end{array} \quad \begin{array}{r} 86 \\ 18 \\ \hline \end{array} \quad \begin{array}{r} 92 \\ 33 \\ \hline \end{array}$$

Yard.

$$\begin{array}{r} 54 \\ 33 \\ \hline \end{array} \quad \begin{array}{r} 47 \\ 23 \\ \hline \end{array} \quad \begin{array}{r} 52 \\ 19 \\ \hline \end{array} \quad \begin{array}{r} 73 \\ 13 \\ \hline \end{array} \quad \begin{array}{r} 71 \\ \hline \end{array} \quad \begin{array}{r} 75 \\ 12 \\ \hline \end{array} \quad \begin{array}{r} 26 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 69 \\ 18 \\ \hline \end{array} \quad \begin{array}{r} 74 \\ 33 \\ \hline \end{array}$$

Yard

$$\begin{array}{r} 60 \\ 33 \\ \hline \end{array} \quad \begin{array}{r} 58 \\ 24 \\ \hline \end{array} \quad \begin{array}{r} 67 \\ 20 \\ \hline \end{array} \quad \begin{array}{r} 65 \\ 15 \\ \hline \end{array} \quad \begin{array}{r} 62 \\ \hline \end{array} \quad \begin{array}{r} 69 \\ 18 \\ \hline \end{array} \quad \begin{array}{r} 64 \\ 23 \\ \hline \end{array} \quad \begin{array}{r} 68 \\ 33 \\ \hline \end{array}$$

$$\begin{array}{r} 53 \\ 50 \\ \hline \end{array}$$

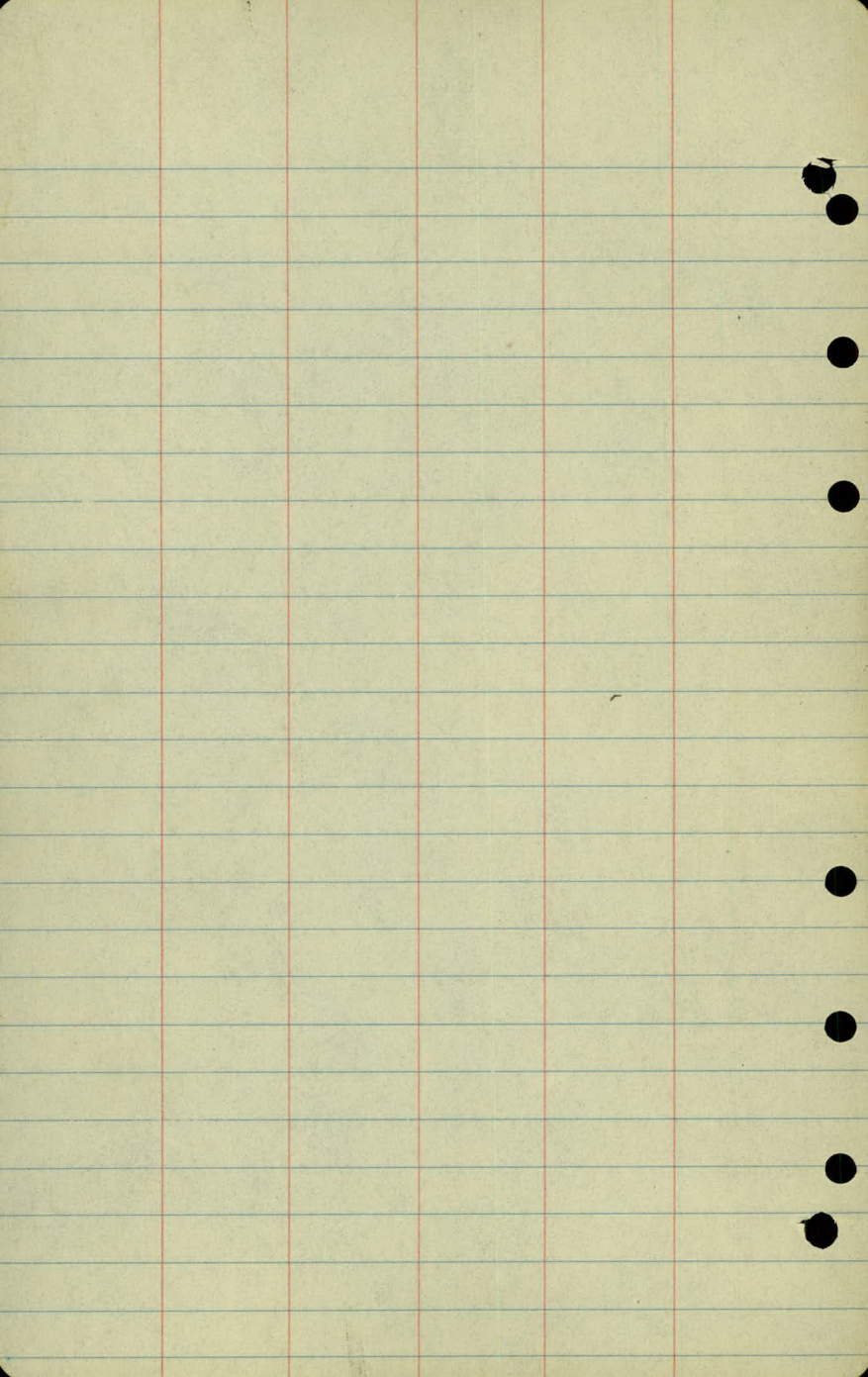
$$\begin{array}{r} 55 \\ 25 \\ \hline \end{array}$$

$$58$$

$$\begin{array}{r} 63 \\ 75 \\ \hline \end{array}$$

$$\begin{array}{r} 70 \\ 50 \\ \hline \end{array}$$

Spike in T.P. S.E. corner E. Co. Line & Co. Rd ¹¹¹ B



Check Levels.

East Ave.

+

π

-

Elev

B.M. spike in T.P. 42' Lt Sta 4760 958.96 East Ave

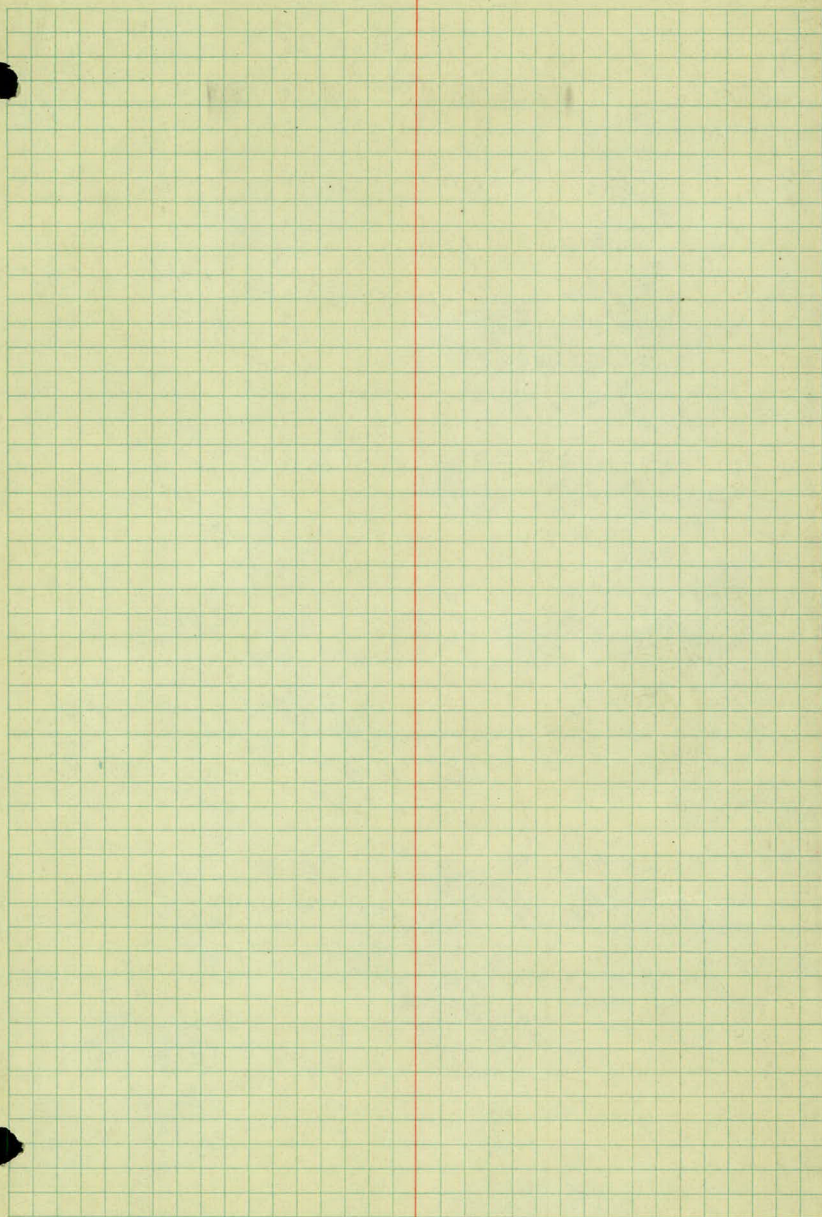
2.54 961.50 6.73 954.77

1.08 955.85 9.64 946.21 946.57

Co. Rd "B"

5.34 948.74 943.40

2.20 946.54 946.57



Check Levels between Margaret + Charles

check Levels.

X-Sections

Co. Rd. B

White Bear Ave- E. Co. Line.

Sta.	+	π	-	Grade
472+34.45	7.12	929.26		922.14
+68				21.7
473				21.7
+50				21.6
474				21.5
+40				21.4
+70				21.4
475				21.3
+20				21.2
T.P.	3.29	928.26	7.29	921.97
+60				21.2
476				21.2

Oct 7, 1936

32

WNC.
K.A.
L.B.H.
A.M.

(Carley)

Mont. Co. Ed. B + White Bear Ave.
Gr. Rock U. E Rt.

$$7.6 \quad 33' \left| \begin{array}{r} 46 \\ +30 \end{array} \right. \quad \begin{array}{r} 46 \\ +10 \end{array} \quad \begin{array}{r} 7.0/33' \\ +0.6/33' \end{array}$$

$$7.6 \quad 33' \left| \begin{array}{r} 8.1 \\ +1.5 \end{array} \right. \quad \begin{array}{r} 59 \\ +1.7 \end{array} \quad \begin{array}{r} 4.2/33' \\ +3.4/33' \end{array}$$

$$7.7 \quad 33' \left| \begin{array}{r} 8.5 \\ +1.2 \end{array} \right. \quad \begin{array}{r} 53 \\ +2.4 \end{array} \quad \begin{array}{r} 6.2/33' \\ +1.5/33' \end{array}$$

$$7.8 \quad 33' \left| \begin{array}{r} 5.6 \\ +2.2 \end{array} \right. \quad \begin{array}{r} 48 \\ +3.0 \end{array} \quad \begin{array}{r} 4.1/33' \\ +3.7/33' \end{array}$$

$$7.9 \quad 33' \left| \begin{array}{r} 4.6 \\ +3.2 \end{array} \right. \quad \begin{array}{r} 4.6 \\ +3.3 \end{array} \quad \begin{array}{r} 4.1/33' \\ +3.8/33' \end{array}$$

$$7.9 \quad 33' \left| \begin{array}{r} 1.1 \\ +6.5 \end{array} \right. \quad \begin{array}{r} 48 \\ +3.1 \end{array} \quad \begin{array}{r} 4.6/33' \\ +2.3/33' \end{array}$$

$$8.0 \quad 33' \left| \begin{array}{r} 9.6 \\ +7.4 \end{array} \right. \quad \begin{array}{r} 5.2 \\ +2.8 \end{array} \quad \begin{array}{r} 7.0/33' \\ +1.0/33' \end{array}$$

$$8.1 \quad 33' \left| \begin{array}{r} 2.0 \\ +6.1 \end{array} \right. \quad \begin{array}{r} 6.2 \\ +1.9 \end{array} \quad \begin{array}{r} 12.8/30.1 \\ -4.7/30.1 \end{array}$$

$$4.1 \quad 33' \left| \begin{array}{r} 8.0 \\ +4.1 \end{array} \right. \quad \begin{array}{r} 3.3 \\ +0.8 \end{array} \quad \begin{array}{r} 11.1/33' \\ -7.0/33' \end{array} \quad \text{Var.}$$

$$4.1 \quad 33' \left| \begin{array}{r} +1.2 \\ +5.8 \end{array} \right. \quad \begin{array}{r} 4.3 \\ -0.2 \end{array} \quad \begin{array}{r} 11.1/33' \\ -7.0/33' \end{array} \quad \text{Var.}$$

Sta.	+	π	-	Grade
------	---	-------	---	-------

975.76

476+50

21.6.

477

22.2.

+50

23.1.

478

24.3.

+55

25.8.

12.10

936.85

0.51

924.75

479

27.5.

B.10

8.94

927.91

+50

29.6.

+80

30.9.

480+20

32.8.

+60

33.8.

481

36.7.

9.81

945.52

-1.14

935.71

Gr. Rock.

H

E

B+

$$3.7 \quad 33' \frac{5.1}{100.6} \quad \frac{4.5}{-0.8} \quad \frac{5.6}{-1.9/21.7}$$

$$3.1 \quad \text{Slope} \quad \text{Var. } 33' \frac{9.7}{-6.6} \quad \frac{4.3}{-1.2} \quad \frac{10.7}{-7.6/33'} \quad \text{Var. Slope}$$

$$2.2 \quad \text{Var. } 33' \frac{10.0}{-7.8} \quad \frac{3.6}{-1.4} \quad \frac{14.3}{-8.9/33'} \quad \text{Var.}$$

$$1.0 \quad \text{Var. } 33' \frac{7.7}{-6.7} \quad \frac{2.4}{-1.4} \quad \frac{14.4}{-13.4/33'} \quad \text{Var.}$$

$$+0.5 \quad 20.8' \frac{1.1}{-1.6} \quad \frac{0.5}{-1.0} \quad \frac{11.6}{-12.1/33'} \quad \text{Var.}$$

$$9.4 \quad 33' \frac{6.4}{120} \quad \frac{21.0}{\frac{9.8}{-0.4}} \quad \frac{11.4}{100.0/33'}$$

9-7.90 Nail T.P. Labe Model'

$$7.3 \quad 33' \frac{11.6}{18.9} \quad \frac{21.8}{\frac{3.0}{+0.3}}$$

$$6.0 \quad 33' - \quad \frac{5.5}{+0.5} \quad -/33'$$

$$4.1 \quad 33' \frac{2.2}{+1.9} \quad \frac{4.0}{+0.1} \quad \frac{6.1}{100.0/33'}$$

$$3.1 \quad 76.5' \frac{6.6}{-3.5} \quad \frac{3.8}{-0.2} \quad \frac{10.5}{-7.2/33'}$$

$$0.2 \quad 31' \frac{5.2}{-5.0} \quad \frac{2.6}{\frac{1.2}{-1.0}} \quad \frac{8.1}{-7.9/33'}$$

Sta.	+	π	-	grade
		945.52		
481+50				39.3
482				42.0
+40				44.3
T.P.	11.55	956.52	0.55	948.97
483				47.8
+50				50.8
484				53.9
T.P.	13.39	969.22	0.69	956.83
484+50				57.0
485				60.1
+75				61.7
+65				64.1
T.P.	12.68	989.23	2.67	966.55
486				66.3

70. Rad.

L⁺

E

121.

6.2

$$30.4 \begin{array}{r} 11.0 \\ -8.8 \\ \hline \end{array}$$

$$7.7 \\ -4.5 \\ \hline$$

$$12.7 \\ -8.5 \quad 32.5$$

8.5

$$27.4 \begin{array}{r} 7.3 \\ -3.8 \\ \hline \end{array}$$

$$5.1 \\ -7.6 \\ \hline$$

$$3.2 \begin{array}{r} 1 \\ +13/33 \\ \hline \end{array}$$

1.2

$$20.5 \begin{array}{r} 2.7 \\ -1.5 \\ \hline \end{array}$$

$$2.7 \\ -1.5 \\ \hline$$

$$10.5 \\ +1.7/33$$

8.7

$$33 \begin{array}{r} 9.5 \\ +12.2 \\ \hline \end{array}$$

$$10.2 \\ -4.5 \\ \hline$$

$$8.7 \\ +0.9/33$$

5.7

$$33 \begin{array}{r} 5.5 \\ +0.2 \\ \hline \end{array}$$

$$6.9 \\ -1.2 \\ \hline$$

$$7.0 \\ +0.7/33$$

2.6

$$33 \begin{array}{r} 1.6 \\ +1.0 \\ \hline \end{array}$$

$$6 \\ 5.9 \\ -1.3 \\ \hline$$

$$4.8 \\ -2.2/22.6$$

12.2

$$33 \begin{array}{r} 12.9 \\ +13.3 \\ \hline \end{array}$$

$$13.5 \\ -1.3 \\ \hline$$

$$16.9 \\ -2.7/30.1$$

14.1

$$33 \begin{array}{r} 10.3 \\ +0.8 \\ \hline \end{array}$$

$$10.4 \\ -1.3 \\ \hline$$

$$14.6 \\ -5.5/32.5$$

7.5

$$33 \begin{array}{r} 7.1 \\ +0.4 \\ \hline \end{array}$$

$$8.5 \\ -1.0 \\ \hline$$

$$11.7 \\ -4.2/28.6$$

5.1

$$33 \begin{array}{r} 3.2 \\ +1.4 \\ \hline \end{array}$$

$$5.6 \\ -0.5 \\ \hline$$

$$6.5 \\ +0.6/33$$

13.9

$$33 \begin{array}{r} 8.3 \\ +1.6 \\ \hline \end{array}$$

$$12.7 \\ +1.2 \\ \hline$$

$$11.3 \\ +1.6/33$$

Sta.	+	π	-	Grade
		977.23		
486+50				69.1.
486+97				71.1.
487+10				71.5.
487+50				72.7.
488				73.5.
+50				73.7.
489				73.2.
+50				72.1.
T.P.	0.70	977.22	8.71	970.52
490				70.3.
+50				68.2.
491				66.1.

90 Rod.

H

L

RT

10.1

$$33 \frac{1.8}{+8.3}$$

$$\frac{9.0}{+1.1}$$

$$\frac{6.8}{+3.3/33}$$

7.7

$$33 \frac{10.5}{+7.2}$$

$$\frac{5.7}{+2.0}$$

$$\frac{6.1}{+12.0/33}$$

6.5

$$33 \frac{11.5}{+8.0}$$

$$\frac{3.8}{+2.7}$$

$$\frac{3.8}{+2.7/33}$$

5.0

$$33 \frac{12.1}{+7.8}$$

$$\frac{3.0}{+2.7}$$

$$\frac{2.8}{+2.8/33}$$

5.5

$$33 \frac{10.9}{+6.4}$$

$$\frac{2.6}{+1.9}$$

$$\frac{5.1}{+10.4/33}$$

6.0

$$33 \frac{12.2}{+4.8}$$

$$\frac{4.4}{+1.6}$$

$$\frac{4.8}{+1.2/33}$$

7.1

$$33 \frac{4.6}{+2.5}$$

$$\frac{6.1}{+1.0}$$

$$\frac{5.3}{+1.8/33}$$

0.9

$$33 \frac{0.4}{+0.5}$$

$$\frac{0.7}{+0.2}$$

$$\frac{1.1}{+0.8/33}$$

3.0

$$33 \frac{1.8}{+1.2}$$

$$\frac{3.1}{-0.1}$$

$$\frac{4.1}{+0.9/33}$$

3.8

$$33 \frac{2.8}{+1.3}$$

$$\frac{5.6}{-0.5}$$

$$\frac{5.1}{+1.0/33}$$

Sta.	+	Σ	-	Grade
		972.22		
491	+50			64.1.
492				62.2.
T.P.	3.76	962.84	12.14	959.08
+50				60.5.
493				58.9.
+50				57.5.
494				56.2.
T.P.	3.87	959.80	6.91	955.93
+50				55.1
495				54.1.
+50				53.2
496				52.3.
+50				51.4

Gr. Red.

H.

E

RL

$$7.1 \quad 33 \overline{) \frac{6.0}{+1.1}} \quad \frac{80}{-0.9} \quad \frac{7.4}{21.7} / 33$$

$$9.0 \quad 33 \overline{) \frac{9.1}{+1.9}} \quad \frac{103}{-1.3} \quad \frac{12.1}{-3.1} / 25.3$$

$$1.3 \quad 29 \overline{) \frac{3.6}{-2.3}} \quad \frac{3.7}{-2.4} \quad \frac{4.9}{-7.6} / 26.8$$

$$3.9 \quad 20 \overline{) \frac{5.9}{-2.0}} \quad \frac{5.1}{-1.2} \quad \frac{6.3}{-2.4} / 23.8$$

$$5.3 \quad 21.7 \overline{) \frac{1.4}{-1.9}} \quad \frac{6.1}{-0.8} \quad \frac{8.1}{-2.8} / 24.4$$

$$6.6 \quad 33 \overline{) \frac{1.1}{+1.1}} \quad \frac{6.9}{-0.3} \quad \frac{8.4}{-1.8} / 21.4$$

$$4.7 \quad 23 \overline{) \frac{4.1}{+0.6}} \quad \frac{4.6}{+0.1} \quad \frac{4.9}{20.8} / 33'$$

$$5.7 \quad 33 \overline{) \frac{4.1}{+1.6}} \quad \frac{5.6}{+0.1} \quad \frac{5.5}{+0.2} / 33$$

$$2.6 \quad 33 \overline{) \frac{2.4}{+2.2}} \quad \frac{6.5}{+0.1} \quad \frac{6.4}{+0.2} / 33$$

$$7.5 \quad 32 \overline{) \frac{4.8}{+2.7}} \quad \frac{27}{-0.2} \quad \frac{9.1}{20.4} / 33'$$

$$8.4 \quad 33 \overline{) \frac{7.0}{+1.4}} \quad \frac{8.9}{-0.5} \quad \frac{12.0}{-3.6} / 26.8$$

Sta	+	T	-	Grade
		959.80		
497				50.7
	2.13	953.09	8.84	950.96
+50				50.0
498				49.4
+48.5				48.8
B.M.			4.41	948.68
499				48.4
+50				48.0
500				47.7
+50				47.4
501				47.2
+50				47.0
J.P	5.33	951.93	5.49	946.60
502				46.8

Gr. Rod.	Lt.	±	Rt.
9.1	$33 \frac{8.0}{+1.1}$	$\frac{9.8}{-0.7}$	$\frac{150}{-5.9/33.0}$
Nail in T.P. 6d. 547+			
3.1	$33 \frac{5.0}{+0.1}$	$\frac{4.0}{-0.9}$	$\frac{9.6}{-6.5/33'}$ Var.
3.7	$33.8 \frac{6.3}{-2.6}$	$\frac{4.4}{-0.7}$	$\frac{8.6}{-4.9/30.7}$
4.3	$33 \frac{5.1}{+1.2}$	$\frac{4.4}{-0.1}$	$\frac{6.3}{100.0/33'}$
(94866) Top Mod.			
4.7	$33 \frac{4.9}{+1.8}$	$\frac{4.4}{+0.3}$	$\frac{5.2}{+1.5/33'}$
5.1	$33 \frac{5.3}{+1.8}$	$\frac{4.8}{+0.3}$	$\frac{4.9}{+0.2/33'}$
5.4	$33 \frac{6.9}{+0.5}$	$\frac{5.1}{+0.3}$	$\frac{5.1}{+0.3/33'}$
5.7	$33 \frac{7.4}{+0.3}$	$\frac{5.5}{+0.2}$	$\frac{4.5}{+1.2/33'}$
5.9	$33 \frac{7.9}{+0.0}$	$\frac{5.8}{+0.1}$	$\frac{4.2}{+1.7/33'}$
6.1	$33 \frac{5.9}{+0.2}$	$\frac{6.0}{+0.1}$	$\frac{4.8}{+1.3/33'}$
5.1	$33 \frac{4.8}{+0.3}$	$\frac{5.3}{-0.2}$	$\frac{7.8}{-2.7/24.1}$

951.93

502+50

46.6

503

46.5

Diffr.

+50

Spec. Diff.

46.3

43.0

504

46.2

43.3

+50

46.1

43.7

+85

46.1

43.9

+90

46.1

505+13

46.1

+18

46.1

J.P.

556

955.20

2.29

949.64

+50

46.05

506

46.0

$$5.3 \quad 28.3 \overline{) 94} \\ \underline{-4.1} \quad 5.1$$

$$\frac{61}{-0.8}$$

$$\frac{98}{-4.5} / 28.5$$

$$5.4 \quad 31.3 \overline{) 10.5} \\ \underline{-5.1}$$

$$\frac{63}{-0.9}$$

$$\frac{10.2}{-4.8} / 30.4$$

DITD

$$5.6 \quad 89 \quad 81 \quad 28 \overline{) 28} \\ \underline{-5.8} \quad 28 \quad 3.3$$

$$\frac{59}{-0.3}$$

$$\frac{9.2}{-26} / 26.8 \quad \frac{9.2}{100.0}$$

$$5.7 \quad 86 \quad 33 \overline{) 4.0} \\ \underline{-12.4} \quad 4.6$$

$$\frac{47}{+1.0}$$

$$\frac{63}{122.3} / 33$$

$$5.8 \quad 8.2 \quad 33 \overline{) 3.0} \\ \underline{-12.8}$$

$$\frac{36}{+22}$$

$$\frac{46}{+1.2} / 33$$

$$5.8 \quad 33 \overline{) 1.9} \\ \underline{-13.9}$$

$$\frac{2.7}{+3.1}$$

$$\frac{46}{+1.2} / 33$$

5.8

$$5.8 \quad 33 \overline{) 0.9} \\ \underline{-14.9}$$

$$\frac{23}{+3.5}$$

$$\frac{38}{+3.5} / 33$$

$$9.15 \quad 33 \overline{) 48} \\ \underline{-14.4}$$

$$\frac{56}{+3.6}$$

$$\frac{5.3}{+3.9} / 33$$

$$9.2 \quad 33 \overline{) 62} \\ \underline{-13.0}$$

$$\frac{53}{+3.9}$$

$$\frac{40}{+5.2} / 33$$

955.20

506+50

45.95

507

45.9

+40

45.85

508

45.8

+50

45.75

509

45.7

+50

45.65

T.P.

6.32

952.21

9.31

945.89

510

45.6

+40

45.55

511

45.5

+20

45.5

$$\begin{array}{r} 9.2 \\ 7.9 \\ \hline 33 \overline{) 5.9} \\ \underline{+3.3} \end{array}$$

$$\begin{array}{r} 5.5 \\ \hline +3.7 \end{array}$$

$$\begin{array}{r} 48 \\ \hline +4.4 \end{array} 63$$

$$\begin{array}{r} 9.3 \\ \hline 33 \overline{) 3.2} \\ \underline{+6.1} \end{array}$$

$$\begin{array}{r} 6.1 \\ \hline +3.2 \end{array}$$

$$\begin{array}{r} 6.0 \\ \hline +3.3 \end{array} / 33'$$

$$\begin{array}{r} 9.35 \\ 9.1 \\ \hline 33 \overline{) 2.4} \\ \underline{+7.0} \end{array}$$

$$\begin{array}{r} 6.5 \\ \hline +2.9 \end{array}$$

$$\begin{array}{r} 5.1 \\ \hline +3.3 \end{array} / 33'$$

$$\begin{array}{r} 9.4 \\ \hline 33 \overline{) 5.6} \\ \underline{+3.8} \end{array}$$

$$\begin{array}{r} 7.1 \\ \hline +2.3 \end{array}$$

$$\begin{array}{r} 4.7 \\ \hline +4.7 \end{array} / 33'$$

$$\begin{array}{r} 9.45 \\ \hline 33 \overline{) 6.2} \\ \underline{+3.3} \end{array}$$

$$\begin{array}{r} 7.8 \\ \hline +1.7 \end{array}$$

$$\begin{array}{r} 4.5 \\ \hline +5.0 \end{array} / 33'$$

34

$$\begin{array}{r} 9.5 \\ 7.7 \\ \hline 33 \overline{) 7.7} \\ \underline{+1.8} \end{array}$$

$$\begin{array}{r} 8.6 \\ \hline +0.9 \end{array}$$

$$\begin{array}{r} 5.6 \\ \hline +2.9 \end{array} / 33'$$

36

$$\begin{array}{r} 9.55 \\ \hline 33 \overline{) 8.2} \\ \underline{+1.4} \end{array}$$

$$\begin{array}{r} 9.0 \\ \hline +0.6 \end{array}$$

$$\begin{array}{r} 6.2 \\ \hline +3.4 \end{array} / 33'$$

$$\begin{array}{r} 6.6 \\ \hline 33 \overline{) 5.2} \\ \underline{+1.4} \end{array}$$

$$\begin{array}{r} 6.3 \\ \hline +0.3 \end{array}$$

$$\begin{array}{r} 4.7 \\ \hline +1.9 \end{array} / 33'$$

$$\begin{array}{r} 6.66 \\ \hline 33 \overline{) 2.8} \\ \underline{+2.0} \end{array}$$

$$\begin{array}{r} 6.6 \\ \hline +0.0 \end{array}$$

$$\begin{array}{r} 7.3 \\ \hline +0.4 \end{array} / 33'$$

$$\begin{array}{r} 6.7 \\ \hline 33 \overline{) 8.1} \\ \underline{+0.6} \end{array}$$

$$\begin{array}{r} 7.6 \\ \hline +0.9 \end{array}$$

$$\begin{array}{r} 8.8 \\ \hline +0.0 \end{array} / 33'$$

$$\begin{array}{r} 6.7 \\ \hline 33 \overline{) 10.8} \\ \underline{+4.1} \end{array}$$

$$\begin{array}{r} 8.1 \\ \hline +1.4 \end{array}$$

$$\begin{array}{r} 9.0 \\ \hline +2.2 \end{array} / 21.6$$

952.21

511+50

45.5

Dt 6.18.

512

45.5

420

B.M.

4.53

949.55

7.19

(945.02)

+50

45.5

422

513

45.5

425

+50

45.5

425

514

45.5

44.5

+50

515

+47

+72

516

$$6.7 \quad \text{Var} - 33' / \frac{12.8}{-6.4}$$

$$\frac{8.4}{-1.7}$$

$$-\frac{9.4}{2.7} / 24.1$$

DTRD. 10

$$6.7 \quad 10.2 \quad 33' / \frac{13.1}{-6.4}$$

$$\frac{9.0}{-2.3}$$

$$\frac{9.7}{-2.0} / 33$$

$$4.05 \quad \frac{7.30}{-} \quad 33' / \frac{10.7}{-6.6}$$

$$\frac{6.0}{-2.0}$$

$$\frac{6.7}{-2.6} / 23.8 \quad \frac{5.4}{-2.0} / 32$$

$$4.05 \quad 7.30 \quad 33' / \frac{9.3}{-5.3}$$

$$\frac{5.5}{-2.5}$$

$$\frac{6.8}{-2.7} / 24.1 \quad \frac{6.6}{-2.0} / 29$$

$$4.05 \quad 6.0 \quad 33' / \frac{7.0}{-2.5}$$

$$\frac{5.2}{-2.2}$$

$$\frac{6.5}{-2.5} / 23.5 \quad \frac{6.5}{-2.6} / 26$$

$$4.05 \quad 33' / \frac{7.1}{-3.0}$$

$$\frac{5.2}{-2.2}$$

$$\frac{5.8}{-2.8} / 21.4$$

$$4.05 \quad 33' / \frac{10.0}{-6.0}$$

$$\frac{5.0}{-1.0}$$

$$4.05 \quad 33' / \frac{11.2}{-7.2}$$

$$4.05 \quad 33' / \frac{11.9}{-7.8}$$

$$\frac{11.35}{-7.4} / 33$$

$$4.05$$

$$4.05$$

$$\frac{3.95}{-1.0}$$

$$\frac{10.8}{-1.8} / 33$$

949.55

516 + 40

945.5

517

+50

+90

518 ~~100~~

T.P.

1.98

947.89

3.64

945.91

518 + 30

945.5

+70

519

Dit 9r.

+50

39.0 Rt + Lt

520

39.15

+50

39.3

5.32

948.82

4.39

945.50

521

945.5

39.45

Mr. Reed

41.

2

21.

4.05

$$205 \frac{5.5}{-7.5}$$

$$\frac{4.05}{-}$$

$$\frac{10.3}{-6.2/33}$$

4.05

$$33 \frac{11.5}{-7.5}$$

$$\frac{4.5}{-0.5}$$

$$\frac{9.0}{-5.0/31}$$

4.05

$$33 \frac{11.9}{-7.9}$$

$$\frac{4.8}{-0.8}$$

$$\frac{9.4}{-5.4/32.2}$$

4.05

$$33 \frac{11.4}{-7.4}$$

37

$$\frac{33}{16}$$

24

$$\frac{8.5}{-6.1/33}$$

24

$$20.8 \frac{4.0}{-1.6}$$

$$\frac{3.4}{-1.0}$$

$$\frac{8.4}{-4.0/33}$$

24

9.1

$$33 \frac{9.6}{-7.2}$$

$$\frac{4.3}{-1.9}$$

$$\frac{8.9}{-6.5/28} \frac{6.9}{22.2/33}$$

24

8.9

$$33 \frac{9.2}{-6.8}$$

$$\frac{5.2}{-2.8}$$

$$\frac{8.8}{-6.4/28} \frac{6.4}{22.5/33}$$

24

8.7

$$33 \frac{9.4}{-7.0}$$

$$\frac{5.0}{-2.4}$$

$$\frac{8.6}{-6.2/28} \frac{6.6}{22.1/33}$$

24

8.6

$$33 \frac{9.1}{-6.7}$$

$$\frac{4.8}{-2.4}$$

$$\frac{8.6}{-6.2/28} \frac{6.2}{22.4/33}$$

3.3

9.4

$$33 \frac{8.2}{21.1/28} \frac{23}{30}$$

$$\frac{5.3}{-2.0}$$

$$\frac{27}{24/28} \frac{6.0}{22.0/33}$$

948.82

527450

945.5

39.6

527400

45.5

39.75

527350

45.5

39.9

527300

45.5

40.2

527250

45.5

40.2

527200

45.7

B.M.

2.74

946.58

✓

2.19

948.76

946.57

✓

4.15

944.61

$$3.3 \quad 9.2 \quad 33 \frac{6.3}{2.91} \quad 28/- \quad \frac{50}{-1.7} \quad \frac{29/}{-46/28} \frac{5.5}{23.7/33}$$

$$3.3 \quad 9.0 \quad 33 \frac{5.8}{2.32} \quad 28.0/43 \quad \frac{46}{-1.3} \quad \frac{39}{25.1/33}$$

$$3.3 \quad 8.9 \quad 33 \frac{8.2}{2.07} \quad \frac{46}{-1.3} \quad \frac{46}{2.42/33}$$

$$3.3 \quad 8.7 \quad 33 \frac{8.5}{2.02} \quad \frac{47}{-1.4} \quad \frac{80/}{-47/28.0} \frac{7.7}{21.0/33}$$

$$3.3 \quad 8.6 \quad 33 \frac{8.3}{2.03} \quad 28/-47 \quad \frac{43}{-1.0} \quad \frac{81/}{-48/28} \frac{7.0}{21.1/33}$$

$$2.1 \quad 7.4 \quad 20.5 \frac{6.6}{2.5} \quad \frac{33}{-0.2} \quad \frac{74/}{-43/28} \frac{4.1}{23.3/33}$$

top Mon.

Top Step S. E. Con. Step, conc, Cottage¹⁵⁰ L. Sta. 524

Sta.	+	π	-	Grade.
	10.60	957.37		946.57
524+585				46.6
525				47.5
+50				49.1
526				51.2
+50				53.7
	13.02	969.99	0.40	956.97
527				56.7
+50				59.8
528				63.4
				BJ op.
+50				67.2
	12.90	981.91	0.98	969.01
529				71.2

L- d R+

$$10.6 \quad 126 \quad 26.2 \quad \frac{140}{-3.4} \quad \frac{10.6}{0.0} \quad \frac{149}{-4.3} / 289$$

$$9.9 \quad 11.9 \quad 33' \quad \frac{11.0}{0.09} \quad \frac{9.6}{+0.3} \quad \frac{19.5}{-0.6} / 179 \quad \frac{103}{16} / 33'$$

$$8.3 \quad 295 \quad \frac{103}{0.02} \quad 208 \quad \frac{99}{-1.6} \quad \frac{80}{+0.3} \quad \frac{109}{-2.6} / 239$$

$$6.2 \quad 8.2 \quad 33' \quad \frac{8.0}{0.02} \quad 214 \quad \frac{8.0}{-1.8} \quad \frac{59}{+0.3} \quad \frac{82}{-2.0} / 22.0 \quad \frac{52}{+1.0} / 33'$$

$$3.7 \quad 5.7 \quad 33' \quad \frac{4.6}{0.11} \quad 193 \quad \frac{4.8}{-1.1} \quad \frac{33}{+0.4} \quad \frac{52}{-1.5} / 20.5 \quad \frac{+0.3}{+4.0} / 33'$$

$$13.3 \quad 11.3 \quad 33' \quad \frac{13.3}{0.15} \quad \frac{13.6}{1.6} \quad \frac{130}{+0.3} \quad \frac{140}{1.6} \quad \frac{104}{+2.9} / 33'$$

$$10.2 \quad 33' \quad \frac{9.7}{+0.5} \quad \frac{100}{+0.2} \quad \frac{9.8}{+0.4} / 33'$$

$$6.6 \quad 33' \quad \frac{3.5}{+3.1} \quad \frac{6.6}{0.0} \quad \frac{6.7}{0.1.9} / 33'$$

$$2.8 \quad 33' \quad \frac{10.4}{+2.4} \quad \frac{2.9}{-0.1} \quad \frac{1.5}{+1.3} / 33'$$

$$10.7 \quad 33' \quad \frac{9.9}{+0.8} \quad \frac{11.4}{-0.7} \quad \frac{7.8}{+1.9} / 33'$$

Sta. + π - Grade

981.91

529+50

975.2

530+0

78.6

530+25

80.2

T.P.

8.66

987.48

3.09

978.82

530+50

80.70

530+81

81.75

4.75

H.

S

B.

$$6.7 \quad 33 \frac{57}{F1.0} \quad \frac{78}{16} \quad \frac{82}{-7.5} \quad \frac{8.2}{16} \quad \frac{3.9}{+2.8} / 33'$$

$$3.3 \quad 32 \frac{+0.1}{33} \quad \frac{42}{16} \quad \frac{53}{-20} \quad \frac{30}{+0.3} / 33$$

$$1.7 \quad 33' \frac{0.4}{+1.3} \quad \frac{30}{-1.3} \quad \frac{2.8}{20}$$

$$5.73 \quad 33' \frac{47}{+1.0}$$

Sta.	+	π	-	Grade
B.M.	8.41	990.98		982.57
531+13 - E. edge Pav.				82.7
531+60				84.2
532				85.5
+50				87.1
T.P.	11.26	1000.38	1.86	989.12
533				88.7
+50				90.4
534				92.1
+40				93.6
+75				95.0
535				96.0
+50			4.20	98.1
				996.18 00

4.

2

24.

8.3

8.3

$$\frac{5.6}{+2.7} / 31'$$

6.8

$$\frac{6.6}{+0.2}$$

$$\frac{4.1}{+2.7} / 31'$$

5.5

$$31' / \frac{4.9}{+0.6}$$

$$\frac{5.4}{+0.1}$$

$$\frac{4.6}{+0.9} / 31'$$

3.9

$$31' / \frac{1.3}{+1.6}$$

$$\frac{3.8}{+0.1}$$

$$\frac{3.3}{+0.8} / 31'$$

11.7

$$31' / \frac{10.2}{+1.5}$$

$$\frac{11.3}{+0.4}$$

$$\frac{9.5}{+2.2} / 31'$$

10.0

$$31' / \frac{8.4}{+1.6}$$

$$\frac{9.4}{+0.6}$$

$$\frac{8.0}{+2.0} / 31'$$

8.3

9.8

$$31' / \frac{2.5}{+1.3}$$

$$\frac{8.9}{16}$$

$$\frac{8.1}{+0.2}$$

$$\frac{8.3}{+0.5} / 31'$$

6.8

8.3

$$31' / \frac{2.8}{+0.5}$$

$$\frac{7.1}{-0.3}$$

$$\frac{9.1}{+2.3} / 22.9$$

$$\frac{8.3}{+0.8} / 31'$$

5.4

6.9

$$31' / \frac{6.7}{+0.2}$$

$$14.6 / \frac{6.6}{+1.2}$$

$$\frac{6.0}{-0.6}$$

$$\frac{5.3}{+0.1} / 31'$$

4.4

5.9

$$31' / \frac{5.4}{+0.5}$$

$$18.1 / \frac{5.1}{-0.7}$$

$$\frac{5.1}{-0.7}$$

$$\frac{5.0}{+0.9} / 31'$$

2.3

$$27.1 / \frac{6.0}{-3.7}$$

$$\frac{3.5}{+1.2}$$

$$\frac{6.9}{-4.5} / 12.5$$

1000.38

536

1000.3

1285

1012.01

1.22

999.16

+25

1001.5

537+50

02.7

537

05.1

+50

07.6

539

1022

1021.01

1.22

1010.79 = Top Hat
1010.70 = d.H.P.

+55

07.9

538

10.0

+40

11.5

538+75

17.6

539+15

13.2

T.P.

8.89

1023.65

6.75

1014.76

$$0.1 \quad 28.9 \left| \begin{array}{r} 4.4 \\ -4.3 \\ \hline \end{array} \right. \quad \frac{1.2}{-1.1} \quad -\frac{5.9}{5.1} / 31'$$

\$ 536

$$10.5 \quad 31' \left| \begin{array}{r} 12.0 \\ 100.0 \\ \hline \end{array} \right. \quad \frac{11.1}{16} \quad \frac{11.5}{-1.0} \quad -\frac{13.5}{3.0} / 25.0$$

$$9.3 \quad 31' \left| \begin{array}{r} 8.7 \\ 10.6 \\ \hline \end{array} \right. \quad \frac{10.0}{-0.7} \quad -\frac{10.4}{1.1} / 19.3 \quad \frac{10.9}{100.0} / 31'$$

$$(6.1) 6.9 \quad 31' \left| \begin{array}{r} 5.3 \\ 10.8 \\ \hline +1.6 \end{array} \right. \quad (7.0) \quad \frac{7.0}{-0.7} \quad -0.1 \quad \frac{3.0}{+3.9} / 31'$$

$$4.4 \quad 31' \left| \begin{array}{r} 2.4 \\ 7.0 \\ \hline \end{array} \right. \quad \frac{4.4}{0.0} \quad \frac{4.5}{16} \quad \frac{4.2}{+0.2} / 31'$$

Top Hyd. N.E. Cor. Indiana

$$13.1 \quad 31' \left| \begin{array}{r} 12.4 \\ 10.7 \\ \hline \end{array} \right. \quad \frac{11.1}{7.0} \quad \frac{12.9}{+0.2} / 31'$$

$$11.0 \quad 31' \left| \begin{array}{r} 12.4 \\ 10.1 \\ \hline \end{array} \right. \quad \frac{11.1}{-0.1} \quad \frac{12.9}{100.0} / 31'$$

$$9.5 \quad 31' \left| \begin{array}{r} 10.0 \\ 10.1 \\ \hline \end{array} \right. \quad \frac{11.1}{-0.1} \quad \frac{10.0}{10.0} / 31'$$

$$8.4 \quad 31' \left| \begin{array}{r} 8.5 \\ 1.4 \\ \hline \end{array} \right. \quad \frac{8.1}{70.3} \quad \frac{5.7}{+2.7} / 31'$$

$$7.8 \quad 31' \left| \begin{array}{r} 7.0 \\ 7.8 \\ \hline \end{array} \right. \quad \frac{7.1}{+0.7} \quad \frac{4.6}{+2.2} / 31'$$

Top E. end curb (L + 24 + 50)

1023.65

539+55

13.6

540

13.7

+50

13.1

541

11.9

+20

+40

10.5

T.P.

1.64

1012.29

13.00

1010.65

541+40

10.5

+76

542

07.9

+50

05.8

543

03.9

T.P.

3.15

1005.04

10.40

1001.89

+50

02.4

1001.89

544

01.1

B.M.

0.64

1002.96

2.72

1002.32

0.54

1002.42

10.0	31' $\frac{9.2}{70.8}$	$\frac{+0.9}{2.7}$	$\frac{9.4}{+0.6}$	$\frac{2.2}{+7.8} / 31'$
9.9	31' $\frac{10.1}{10.13}$	$\frac{+0.3}{2.3}$	$\frac{9.3}{+0.6}$	$\frac{6.2}{+3.7} / 31'$
10.5	31' $\frac{11.6}{20.4}$	$\frac{+0.4}{2.4}$	$\frac{10.3}{+0.2}$	$\frac{6.3}{+4.2} / 31'$
11.7	21' $\frac{12.2}{20.0}$	$\frac{+0.3}{2.3}$	$\frac{11.5}{+0.2}$	$\frac{6.0}{+5.7} / 31'$
13.2			$\frac{13.0}{+0.2}$	$\frac{8.3}{+4.9} / 31'$
1.8	31' $\frac{6.8}{-5.0}$			$\frac{12.1}{32}$ $\frac{+9.5}{38}$
4.4	31' $\frac{6.8}{20.0}$	$\frac{+5.7}{-1.3}$	$\frac{4.4}{0.0}$	$\frac{14.7}{32}$ $\frac{+0.7}{37}$ $\frac{+7.6}{42.6}$ $\frac{2.2}{+2.2} / 31'$
6.5	26.2 $\frac{9.9}{3.4}$		$\frac{6.8}{-0.3}$	$\frac{7.5}{16}$ $\frac{6.5}{201.5} / 31'$
8.4	Var. 33' $\frac{14.6}{-6.2}$		$\frac{8.9}{-0.5}$	$\frac{9.2}{16}$ $\frac{8.7}{200.2} / 31'$
26	28' $\frac{9.2}{-6.6}$		$\frac{3.3}{-0.7}$	$\frac{4.1}{200.0} / 31'$
39	20.5 $\frac{5.4}{21.5}$		$\frac{4.1}{-0.2}$	$\frac{4.0}{16}$ $\frac{2.6}{+0.9} / 31'$

Deep ditch

at +7.0
32

+8.6
36

+9.2 / 43.4

54 / 31'

Hyd 1st St. N.W. N.E. cor.
Top Hyd " " " " " "

0.64 1002.96

1002.32

544+55

1000.2

545

99.5

+50

98.9

546

97.9

+50

96.6

+80

95.7

547

95.1

+50

93.2

T.P.

3.43

995.07

11.32

991.64

548

91.1

+50

88.6

549

85.9

$$2.8 \quad 19 \overline{) 5.8} \quad \begin{array}{r} 2.7 \\ +0.1 \end{array} \quad \begin{array}{r} 2.0 \\ +0.8/31 \end{array}$$

$$3.5 \quad 24.7 \overline{) 3.8} \quad \begin{array}{r} 3.2 \\ +0.3 \end{array} \quad \begin{array}{r} 3.0 \\ +0.5/31 \end{array}$$

$$4.1 \quad 244 \overline{) 4.7} \quad \begin{array}{r} 4.1 \\ +0.0 \end{array} \quad \begin{array}{r} 2.7 \\ +1.4/31 \end{array}$$

$$5.1 \quad 75.0 \overline{) 4.0} \quad \begin{array}{r} 5.0 \\ +0.1 \end{array} \quad \begin{array}{r} 4.9 \\ +0.2/31 \end{array}$$

$$6.4 \quad 25 \overline{) 3.6} \quad \begin{array}{r} 6.0 \\ +0.4 \end{array} \quad \begin{array}{r} 4.8 \\ +1.6/31 \end{array}$$

$$7.9 \quad 24 \overline{) 4.5} \quad \begin{array}{r} 7.3 \\ +0.6 \end{array} \quad \begin{array}{r} 2.6 \\ +1.5/31 \end{array}$$

$$9.8 \quad 23 \overline{) 3.9} \quad \begin{array}{r} 9.0 \\ +0.8 \end{array} \quad \begin{array}{r} 3.8 \\ +6.0/31 \end{array}$$

2 548

$$4.0 \quad 22 \overline{) 2.8} \quad 3.4 \quad \begin{array}{r} 0.6 \\ +3.4/31 \end{array}$$

$$6.5 \quad 22 \overline{) 6.5} \quad \begin{array}{r} 6.0 \\ +0.5 \end{array} \quad \begin{array}{r} 2.2 \\ +4.3/31 \end{array}$$

$$9.2 \quad 33 \overline{) 15.8} \quad \begin{array}{r} 9.4 \\ -0.2 \end{array} \quad \begin{array}{r} 5.7 \\ +3.5/31 \end{array}$$

995.07

2.53

984.75

12.85

982.22

549+50

83.0

550

80.3

+22

79.3

+50

78.2

B.M.

0.92

978.55

7.12

977.63

551

76.5

+50

75.2

552

74.5

+50

74.3

553

74.5

+50

75.2

554

76.4

1.8

$$33 \overline{) 108} \\ -85 \\ \hline$$

$$\frac{25}{-0.7}$$

$$\frac{7 \frac{1.2}{+2.0}}{31'}$$

4.5

$$33 \overline{) 115} \\ -70 \\ \hline$$

$$\frac{51}{-0.6}$$

$$\frac{25}{+2.0} / 31'$$

5.5

$$\frac{61}{-0.6}$$

$$20.7 / 25.2$$

6.6

$$38 \overline{) 106} \\ -40 \\ \hline$$

$$\frac{73}{-0.7}$$

$$\frac{78}{20.3} / 18.1$$

2.1

$$32.5 \overline{) 76} \\ -55 \\ \hline$$

$$\frac{25}{-0.4}$$

$$\frac{46}{27.8} / 23.5$$

3.4

$$32.5 \overline{) 89} \\ -55 \\ \hline$$

$$\frac{34}{-0.5}$$

$$\frac{58}{-2.4} / 23.2$$

4.1

$$32.8 \overline{) 97} \\ -56 \\ \hline$$

$$\frac{48}{-0.7}$$

$$\frac{74}{-3.3} / 25.9$$

4.3

$$39.5 \overline{) 88} \\ -45 \\ \hline$$

$$\frac{48}{-0.5}$$

$$\frac{8.0}{-3.7} / 27.1$$

4.1

$$35.3 \overline{) 72} \\ -21 \\ \hline$$

$$\frac{45}{-0.4}$$

$$\frac{55}{+1.4} / 20.2 \quad \frac{51}{20.5} / 31'$$

3.4

$$31 \overline{) 32} \\ +0.2 \\ \hline$$

$$\frac{24}{+0.5}$$

$$\frac{1.9}{+1.5} / 31'$$

2.2

$$31 \overline{) 04} \\ +1.8 \\ \hline$$

$$\frac{14}{+0.8}$$

$$\frac{05}{+1.7} / 31$$

1		978.55			
T.P.	13.77	990.98	1.34		977.21
554+50				78.0	977.21
555				79.9	
+50				81.8	
556				83.7	
+50				85.6	
557				87.5	
+30				88.6	
+55 = 1 Margaret				89.6	
+75				90.4	
558				91.3	
T.P.	8.85	999.07	0.73		990.25
B.M.	9.12	999.10	7.12		991.98
558				91.3	

+3.8% grade.

13.0

$$31 \overline{) \frac{129}{101}}$$

$$\frac{123}{107}$$

$$\frac{143}{127} / 31$$

11.1

$$31 \overline{) \frac{100}{111}}$$

$$\frac{104}{107}$$

$$\frac{85}{126} / 31$$

9.2

$$31 \overline{) \frac{86}{105}}$$

$$\frac{86}{105}$$

$$\frac{72}{120} / 31$$

7.3

$$31 \overline{) \frac{66}{107}}$$

$$\frac{68}{105}$$

$$\frac{32}{141} / 31$$

5.4

$$292 \overline{) \frac{61}{1000}}$$

$$\frac{54}{100}$$

$$\frac{28}{126} / 186$$

3.5

$$304 \overline{) \frac{50}{1000}}$$

$$\frac{44}{109}$$

$$\frac{3.8}{101.2} / 15.7$$

2.4

$$31 \overline{) \frac{36}{1003}}$$

$$\frac{37}{113}$$

$$\frac{34}{100.5} / 25.0$$

0.6

$$226 \overline{) \frac{28}{12}}$$

$$\frac{22}{116}$$

$$\frac{21}{50.1} / 105$$

9.9
7.8

$$226 \overline{) \frac{100}{122}}$$

$$\frac{98}{120}$$

$$\frac{9.5}{11.7} / 21.1$$

999.10

558+50

93.2

559+0

95.1

+50

97.0

+70

98.0

T.P.

10.28

1008.80

0.58

998.52

560

989

+50

1000.7

561

02.2

T.P.

9.23

1014.20

3.83

1004.97

+50

03.6

562

562

04.7

+50

05.6

563

06.3

B.M.

B.M.

5.86

1008.34

1008.76

5.26

1014.62

~~Equation~~

$$5.9 \quad 299 \left| \begin{array}{r} 83 \\ -23 \\ \hline \end{array} \right. \quad \begin{array}{r} 78 \\ -1.8 \\ \hline \end{array} \quad \begin{array}{r} 63 \\ 20.1 \end{array} / 24.5$$

$$4.0 \quad 273 \left| \begin{array}{r} 61 \\ -21 \\ \hline \end{array} \right. \quad \begin{array}{r} 57 \\ -1.7 \\ \hline \end{array} \quad \begin{array}{r} 35 \\ 20.5 \end{array} / 31$$

$$2.1 \quad 31 \left| \begin{array}{r} 3.3 \\ 20.3 \\ \hline \end{array} \right. \quad \begin{array}{r} 33 \\ -1.2 \\ \hline \end{array} \quad \begin{array}{r} +1.8 \\ 31 \end{array} ?$$

$$1.1 \quad 279 \left| \begin{array}{r} 10 \\ -1.1 \\ \hline \end{array} \right. \quad \begin{array}{r} 10 \\ 20.1 \end{array} / 25.5$$

Top end West end c.m. calc Rt side.

$$9.9 \quad 31 \left| \begin{array}{r} 10.4 \\ 20.0 \\ \hline \end{array} \right. \quad \begin{array}{r} 10.6 \\ -0.7 \\ \hline \end{array} \quad \begin{array}{r} 9.8 \\ 20.1 \end{array} / 25.5$$

$$8.1 \quad 31 \left| \begin{array}{r} 7.9 \\ 20.2 \\ \hline \end{array} \right. \quad \begin{array}{r} 8.2 \\ -0.1 \\ \hline \end{array} \quad \begin{array}{r} 6.6 \\ 21.5 \end{array} / 31$$

$$6.6 \quad 20 \left| \begin{array}{r} 6.8 \\ 21.3 \\ \hline \end{array} \right. \quad \begin{array}{r} 5.5 \\ +1.1 \\ \hline \end{array} \quad \begin{array}{r} 4.3 \\ 22.3 \end{array} / 31$$

$$10.6 \quad 20 \left| \begin{array}{r} 10.0 \\ 20.6 \\ \hline \end{array} \right. \quad \begin{array}{r} 9.2 \\ +1.4 \\ \hline \end{array} \quad \begin{array}{r} 6.2 \\ 24.4 \end{array} / 31$$

$$9.5 \quad 30 \left| \begin{array}{r} 8.4 \\ 21.1 \\ \hline \end{array} \right. \quad \begin{array}{r} 10.6 \\ 8.1 \\ +1.4 \\ \hline \end{array} \quad \begin{array}{r} 3.2 \\ 26.3 \end{array} / 28$$

$$8.6 \quad 31 \left| \begin{array}{r} 9.4 \\ 20.7 \\ \hline \end{array} \right. \quad \begin{array}{r} 10.7 \\ 7.2 \\ \hline \end{array} \quad \begin{array}{r} 3.4 \\ 25.2 \end{array} / 28$$

$$2.9 \quad 24 \left| \begin{array}{r} 9.4 \\ 20.0 \\ \hline \end{array} \right. \quad \begin{array}{r} 10.6 \\ 8.9 \\ -1.0 \\ \hline \end{array} \quad \begin{array}{r} 7.7 \\ 20.7 \\ \hline \end{array} \quad \begin{array}{r} 3.8 \\ 24.1 \end{array} / 28$$

Top NE Corner Charles St.

Sta.	+	$\bar{x}$	-	Grade
		1014.62		
563+50				06.7
564				06.9
+22				06.9
+50				06.9
+72				06.8
565'				06.7
+50				06.4
T.P.	5.28	1011.05	8.85	1005.77
566				05.8
+50				05.1
567				04.2
T.P.	3.42	1005.92	8.85	1002.5
+50				03.2

Gr. Rod.

Lt.

R

Rt.

3

7.9

$$227 \overline{) 118} \\ -39$$

$$\frac{73}{20}$$

$$\frac{55}{124} / 28'$$

7.7

$$38 \overline{) 123} \\ -66$$

$$\frac{81}{-0.4}$$

$$\frac{70}{107} / 18'$$

7.7

$$21.4 \overline{) 9.5} \\ -1.8$$

7.7

$$\frac{78}{-0.1}$$

$$\frac{4.2}{13.1} / 28'$$

7.8

$$31 \overline{) 90} \\ \underline{120} 3$$

$$\frac{1066.6}{76} \\ \underline{10.3}$$

7.9

$$31 \overline{) 7.7} \\ \underline{102}$$

$$\frac{25}{15.4} / 31'$$

8.2

$$31 \overline{) 6.1} \\ \underline{12.1}$$

$$\frac{39}{10.3}$$

$$\frac{46}{13.6} / 31'$$

5.3

$$31 \overline{) 46} \\ \underline{107}$$

$$\frac{5.3}{20}$$

$$\frac{3.7}{11.6} / 31'$$

6.0

$$31 \overline{) 2.7} \\ \underline{173}$$

$$\frac{6.2}{-0.2}$$

$$\frac{3.6}{10.4} / 31'$$

6.9

$$31 \overline{) 58} \\ \underline{111}$$

$$\frac{73}{-0.4}$$

$$\frac{70}{11.4} / 31'$$

7.7

$$\frac{4.2}{200}$$

$$\frac{3.4}{20.4}$$

$$\frac{2.9}{12.3} / 31'$$

Sta.	+	Δ	-	Grade	
		1005.92			
568				02.3	1.7
+50				01.4	
569				00.7	
+40				00.1	
+80				99.7	
B.M.	8.29	1005.16	9.02		996.90
	8.29	1005.16			996.87
570				99.5	
+25				99.2	
+65				98.9	
571				98.7	
+50				98.4	
572				98.2	

P. Col.

H

L

B.

3.6

$$229 \begin{array}{r} 59 \\ -23 \\ \hline \end{array}$$

$$\begin{array}{r} 41 \\ -0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 42 \\ -10.09 \\ \hline \end{array} / 31'$$

4.5

$$208 \begin{array}{r} 61 \\ -1.6 \\ \hline \end{array}$$

$$\begin{array}{r} 46 \\ -0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 39 \\ -10.6 \\ \hline \end{array} / 31'$$

5.2

$$222 \begin{array}{r} 76 \\ -24 \\ \hline \end{array}$$

$$\begin{array}{r} 51 \\ -10.1 \\ \hline \end{array}$$

$$\begin{array}{r} 39 \\ -11.3 \\ \hline \end{array} / 31'$$

5.9

$$31 \begin{array}{r} 44 \\ +1.5 \\ \hline \end{array}$$

$$\begin{array}{r} 54 \\ -10.5 \\ \hline \end{array}$$

$$\begin{array}{r} 30 \\ -12.9 \\ \hline \end{array} / 31'$$

6.2

$$31 \begin{array}{r} 60 \\ -10.2 \\ \hline \end{array}$$

$$\begin{array}{r} 58 \\ -10.4 \\ \hline \end{array}$$

$$\begin{array}{r} 20 \\ -14.2 \\ \hline \end{array} / 31'$$

P.P. N.W. of

5.7

$$31 \begin{array}{r} 69 \\ -10.2 \\ \hline \end{array}$$

$$\begin{array}{r} 52 \\ -10.5 \\ \hline \end{array}$$

$$\begin{array}{r} 5.8 \\ -10.4 \\ \hline \end{array} / 280$$

6.0

$$222 \begin{array}{r} 84 \\ -24 \\ \hline \end{array}$$

$$\begin{array}{r} 56 \\ -10.4 \\ \hline \end{array}$$

$$\begin{array}{r} 27 \\ -13.3 \\ \hline \end{array} / 31'$$

6.3

$$196 \begin{array}{r} 75 \\ -1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 63 \\ -10.0 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ -11.0 \\ \hline \end{array} / 27.0$$

(X)

6.5

$$198 \begin{array}{r} 78 \\ -1.3 \\ \hline \end{array}$$

$$\begin{array}{r} 64 \\ -10.1 \\ \hline \end{array}$$

$$\begin{array}{r} 6.3 \\ -10.2 \\ \hline \end{array} / 27$$

(X)

6.8

$$202 \begin{array}{r} 82 \\ -1.4 \\ \hline \end{array}$$

$$\begin{array}{r} 64 \\ -10.4 \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ -10.4 \\ \hline \end{array} / 27'$$

(X)

7.0

$$31 \begin{array}{r} 69 \\ -10.1 \\ \hline \end{array}$$

$$\begin{array}{r} 63 \\ -10.7 \\ \hline \end{array}$$

$$\begin{array}{r} 6.0 \\ -11.0 \\ \hline \end{array} / 31$$

Sta + π - Grade

1005.16

T.P. 5.50 1003.91 6.75 998.41

572+50 98.2

573 98.5

+50 99.1

574 1000.1

+50 014

T.P. 10.48 1012.66 1.73 1002.18

575 030

+50 048

576 06.6

+50 08.1

+75 08.7

B.M.

24/2

10 12.24

Margaret & Co. Rd. "B."

	+	A	-	grade
B. 10-	0.75	992.73		991.98

6+50

6+0

150

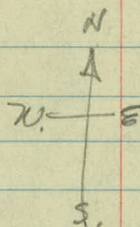
5+00 = 557+53 = 100 Rd. B.

89.6

4+50

4+0

Tr. Rod -

0.4 Crown6.7
6.3 $\frac{6.0}{15}$

6.3

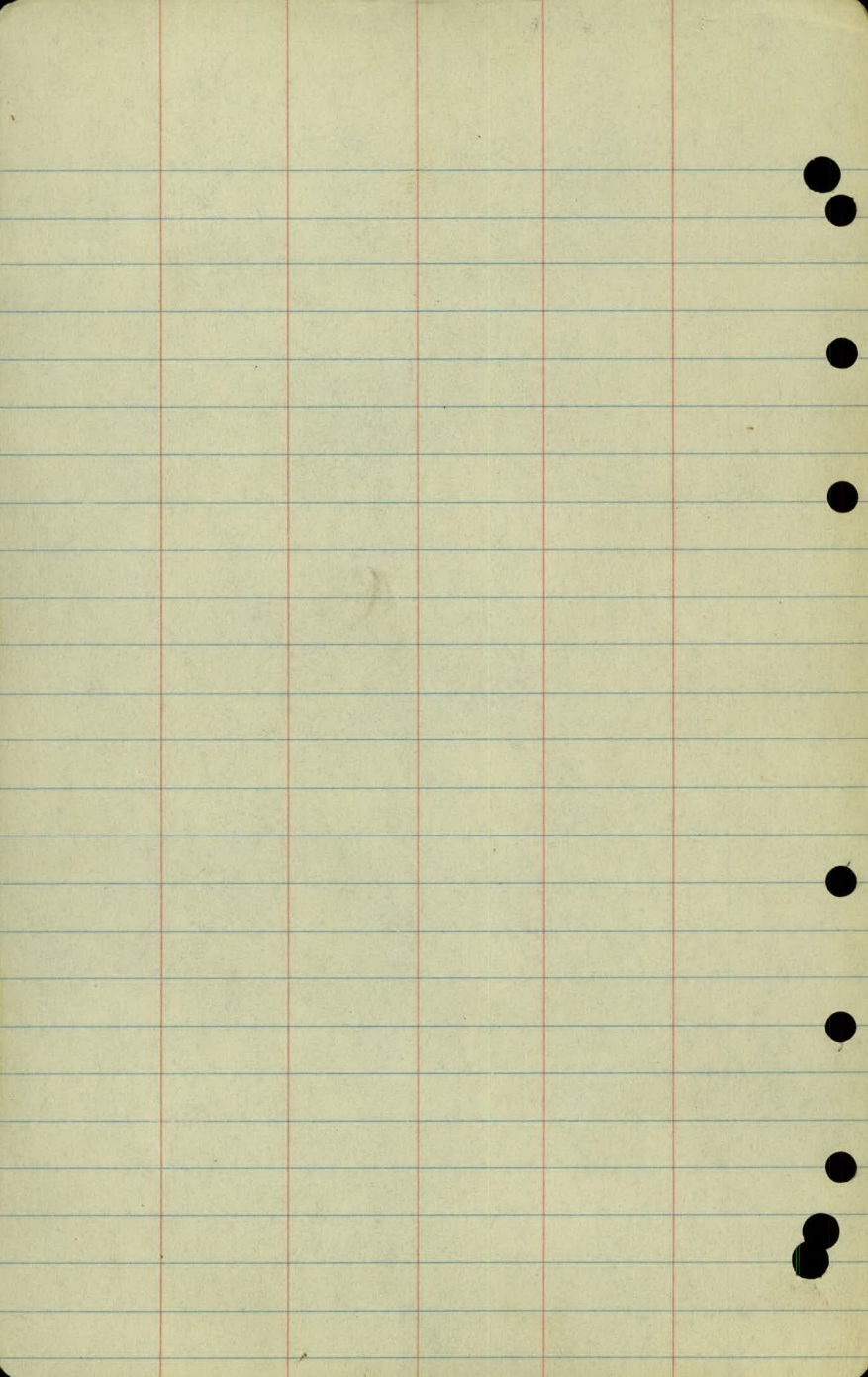
 $\frac{6.7}{15} / 10$ 5.7 5.7
5.3 $\frac{6.1}{15}$ $\frac{5.7}{-0.4}$ $\frac{6.0}{15}$ 4.7 4.7
4.3 $\frac{5.8}{15}$ $\frac{5.2}{-0.9}$ $\frac{5.2}{15}$

3.1

 $\frac{4.5}{-1.4}$ $\frac{4.0}{15}$ 3.7 3.3
2.9 $\frac{4.3}{15}$ 4.0 $\frac{4.0}{15}$

2.7

 $\frac{2.7}{15}$ 2.8



Hutchins on Driveway.

Co. Road "B"

East of White Bear Ave.

W. H. Carlson
June 8, 1937

+75- 5 - 4'

5.5 5.0

+33

6.0 5.0

+73 (6.0 x 12.0)
12' x 19.5)

10.5 - 9.0

499-NE Cor. 15⁰
+ 499 Conc. Drive 8.5

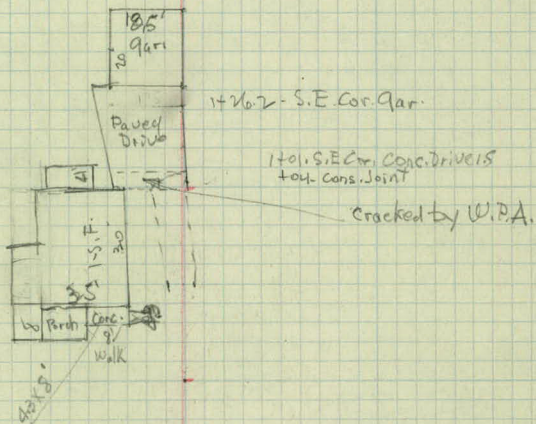
4695 S.E. Cor. 14.5

46, 5-63 Walk 11.5

07

433 10" Ex. El. 14

416 - Shoulder Road



Oto & Co. Rd B



X-Sections.

Hutchinson Drive.

Co. Rd "B"

East of White Bear Ave.

W.N.C.
6/8/37

5.8

✓
976.7

970.9 ✓

Slope Stk.

T.B.M.

2.9

973.8

0400

E.B.

0416

0423 - E Ditch

T.P

11.40

✓
985.5

2.60

✓
974.1

0434

0450

0466.5

0475

140

+16.6

1476.1

Gar. Ent.

11.70

✓
972.8

E

H. = EAST

Sta 476

Top Stone Marker Hilltop So. Side

$$\begin{array}{r} 71.5 \\ 52 \end{array}$$

$$\begin{array}{r} 6.6 \\ 20 \end{array}$$

$$\begin{array}{r} 71.3 \\ 54 \end{array}$$

$$\begin{array}{r} 4.8 \\ 20 \end{array}$$

$$\begin{array}{r} 10 \\ 10 \end{array}$$

$$\begin{array}{r} 71.8 \\ 49 \end{array}$$

$$\begin{array}{r} 7.9 \\ 20 \end{array}$$

$$\begin{array}{r} 7.4 \\ 10.5 \end{array}$$

$$\begin{array}{r} 5.8 \\ 10.5 \end{array}$$

$$\begin{array}{r} 4.8 \\ 9 \end{array}$$

$$\begin{array}{r} 6.6 \\ 9 \end{array}$$

$$\begin{array}{r} 6.2 \\ 20 \end{array}$$

$$\begin{array}{r} 10 \\ 0 \end{array}$$

$$\begin{array}{r} 72.9 \\ 12.6 \\ 0 \end{array}$$

$$\begin{array}{r} 7.0 \\ 20 \end{array}$$

$$\begin{array}{r} 7.0 \\ 12 \end{array}$$

$$\begin{array}{r} 12.6 \\ 6 \end{array}$$

$$\begin{array}{r} 12.6 \\ 5.6 \end{array}$$

$$\begin{array}{r} 6.8 \\ 9.5 \end{array}$$

$$\begin{array}{r} 6.2 \\ 20 \end{array}$$

$$\begin{array}{r} 75.2 \\ 19.3 \\ 5.5 \end{array}$$

$$\begin{array}{r} 4.5 \\ 20 \end{array}$$

$$\begin{array}{r} 4.2 \\ 11.5 \end{array}$$

$$\begin{array}{r} 10.5 \\ 5 \end{array}$$

$$\begin{array}{r} 19.3 \\ 5.5 \end{array}$$

$$\begin{array}{r} 5.7 \\ 9 \end{array}$$

$$\begin{array}{r} 5.5 \\ 20 \end{array}$$

$$\frac{3.55}{11.5} = \text{Top of 3' Walk (Build steps to meet)}$$

$$\begin{array}{r} 10 \\ 10 \end{array}$$

$$\begin{array}{r} 78.5 \\ 7.0 \\ 4.5 \end{array}$$

$$\begin{array}{r} 3.6 \\ 14.5 \end{array}$$

$$\begin{array}{r} 3.4 \\ 10.5 \end{array}$$

$$\begin{array}{r} 6.4 \\ 6 \end{array}$$

$$\begin{array}{r} 7.0 \\ 4.5 \end{array}$$

$$\begin{array}{r} 3.4 \\ 8 \end{array}$$

$$\begin{array}{r} 3.2 \\ 20 \end{array}$$

$$\begin{array}{r} 82.0 \\ 3.5 \\ 1 \end{array}$$

$$\begin{array}{r} 3.07 \\ 8.6 \end{array}$$

$$\begin{array}{r} 3.5 \\ 1 \end{array}$$

$$\begin{array}{r} 6.4 \\ 7 \end{array}$$

$$\begin{array}{r} 6.4 \\ 20 \end{array}$$

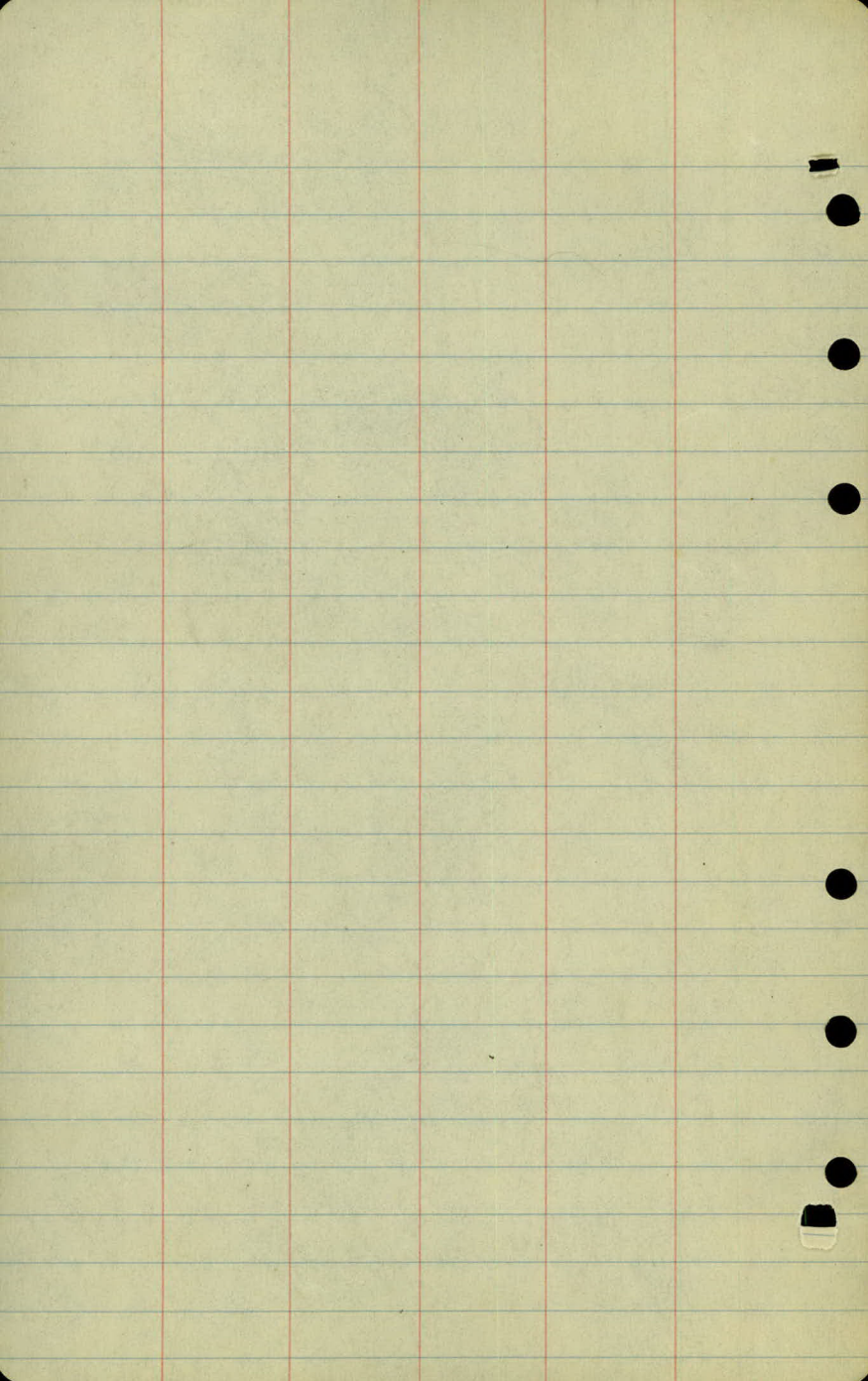
$$\begin{array}{r} 82.94 \\ 3.56 \\ 3.5 \end{array}$$

$$\begin{array}{r} 7.57 \\ 21 \end{array}$$

$$\begin{array}{r} 3.07 \\ 8.6 \end{array}$$

$$\begin{array}{r} 1.79 \\ 18 \end{array}$$

$$\begin{array}{r} 83.71 \\ 1.79 \\ 0 \end{array}$$



Final X-Sections.
Co. Road "B"
Street Ely. to East Ave.

W. N. Carlson
June 9, 1937

Sta.	+	-	Grade
B.M.	1.45	948.02	946.57

518+30			945.91
--------	--	--	--------

+57 = West end of Culv thru St. R.R. (East end Buried)

+70			45.8
-----	--	--	------

519+0			45.7
-------	--	--	------

+50			45.7
-----	--	--	------

+85 East end ^{24" x 25"} C.I. Pipe thru St. R.R.

520+0			45.7
-------	--	--	------

+50			45.8
-----	--	--	------

521			45.8
-----	--	--	------

+50			45.9
-----	--	--	------

459

Top 1000 Mon Co. Rd "B" East Ave.

945.9157

2.11 Top Rail

45.8 40.2 39.8
2.2 78 82
15 32 37

938.18

Fl. Line St. R.R. Culv. 938.1

Top Rail 45.0 43.8 45.3 44.9 39.9 40.3
3.0 4.2 2.7 2.2 3.1 2.1 2.7
24 21 16 16 33 39

38.9 38.1 45.1 44.9 40.1 41.0
21 21 29 3.1 7.9 7.9
33 28 16 16 27 31

38.3 38.8 39.1 45.0 45.0 40.1 39.7 41.6
9.7 9.2 8.9 3.0 3.0 7.9 8.3 6.1
75 43 32 16 16 26 30 33 = 22.5

39.1
890
116

38.0 38.4 38.7 44.9 45.1 40.2 39.6 41.3
100 96 93 3.1 2.3 2.9 7.8 8.4 6.7
100 55 33 17 16 26 30 33 = 22.1

40.6 38.5 38.9 39.2 44.9 44.9 40.1 39.7 41.6
7.4 7.5 7.6 8.8 3.1 3.1 7.9 8.3 6.4
100 63 50 33 17 16 25 29 33 = 22.4

40.0 38.9 39.9 40.7 40.7 45.2 45.2 40.6 40.4 39.9 42.8
8.9 9.1 8.1 7.3 7.3 2.8 2.8 7.4 7.6 5.2 5.2
100 75 60 39 27 17 16 26 29 31 33 = 22.4

40.2 39.0 41.1 42.5 41.9 45.5 45.2 41.3 41.1 43.3
78 80 69 5.5 6.1 2.6 2.8 6.7 6.9 4.7
135 105 76 33 26 17 25 28 33 33 = 22.5

Sta	+	π	-	Grade
-----	---	-------	---	-------

908.02

522+00

45.8

+50

45.8

523+00

45.7

+36 = $\frac{1}{2}$ Cul. 24" X 60" C.M.

+50

45.9

524+0

46.4

+58.8

46.8

B.M.

1.45

946.57

Die Ditch Ent. 525 ft.
place ent. Culvert 5220.

[illegible]

Sta.	+	π	-	Grade
------	---	-------	---	-------



Dr. 6-BK 96

Ditch Grade

Co. Road "B"

St. RR. to East Ave.

W. H. Carlson.

July 12, 1937

3.70 950.27

D.H.R. Lt.

523+36 f.c.u.

938.92

73

38.8

+50

38.65

22

38.5

+50

38.30

21

38.2

+50

41 1 33

38.05

20

37.9

+

+50

37.70

19

37.6

18+

946.57

Dit Red.

11.8

11.5

11.65

11.8

11.95

12.1

12.25

12.4

12.6

12.7

938.92

11.35

31.6

38.2

39.4

49.8

47.0

38.71

36.6

36.6

37.8

10.8
10.9

10.2
10.3

10.4
10.6

7.6
12.4.2

8.5
12.5

10.9
10.9

11.4
10.9

11.5
10.9

11.3
10.2

Cut
1.0 = B/No Top

940.02

10.75

9.2
10.0

6.0
10.4

5.4
10.7

7.0
10.3

7.4
10.6

✓

✓

✓

Dit 9.8

Fill Dit

(10.2)

10.5

10.4

10.9

10.0

9.95

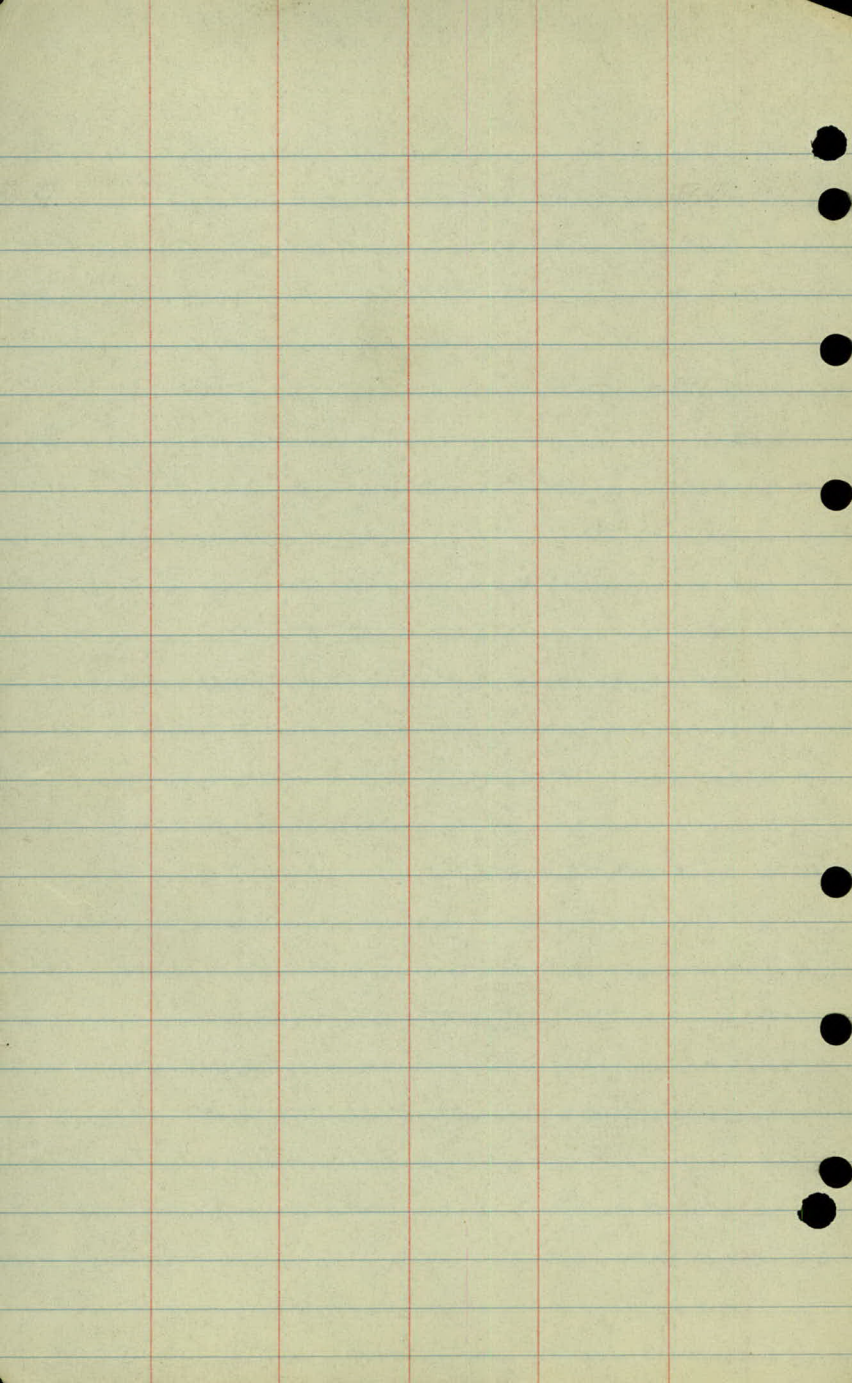
9.90

9.85

9.80

17.0

937.30
12.97 R.R. Cal W.



Co. Rd "B"

Ditch Grade

West of RR Tracks.

B.M.	4.55	751.12			946.57
		741.12			
	410	750.59		745.89	
		740.89	5.23	935.89	

510+ 00

+50

511

+50

512

+50

513

+50

514

512+00 Plos. & Culy 24" X 56' C.M.

Rod.

Top of Iron Pin East Ave & Co. Rd. "B"

6.8

7.0

7.0

$\frac{5.8}{12.12} / 33.0$

7.5

7.1

$\frac{7.1}{12.09} / 33.0$

8.0

8.0

$\frac{7.3}{12.02} / 33.0$

8.5

8.0

$\frac{7.6}{12.09} / 33.0$

8.2

7.7

$\frac{6.2}{12.19} / 33.0$

7.9

7.8

$\frac{7.8}{12.21} / 28.0$

7.6

7.6

$\frac{7.6}{12.20} / 26.0$

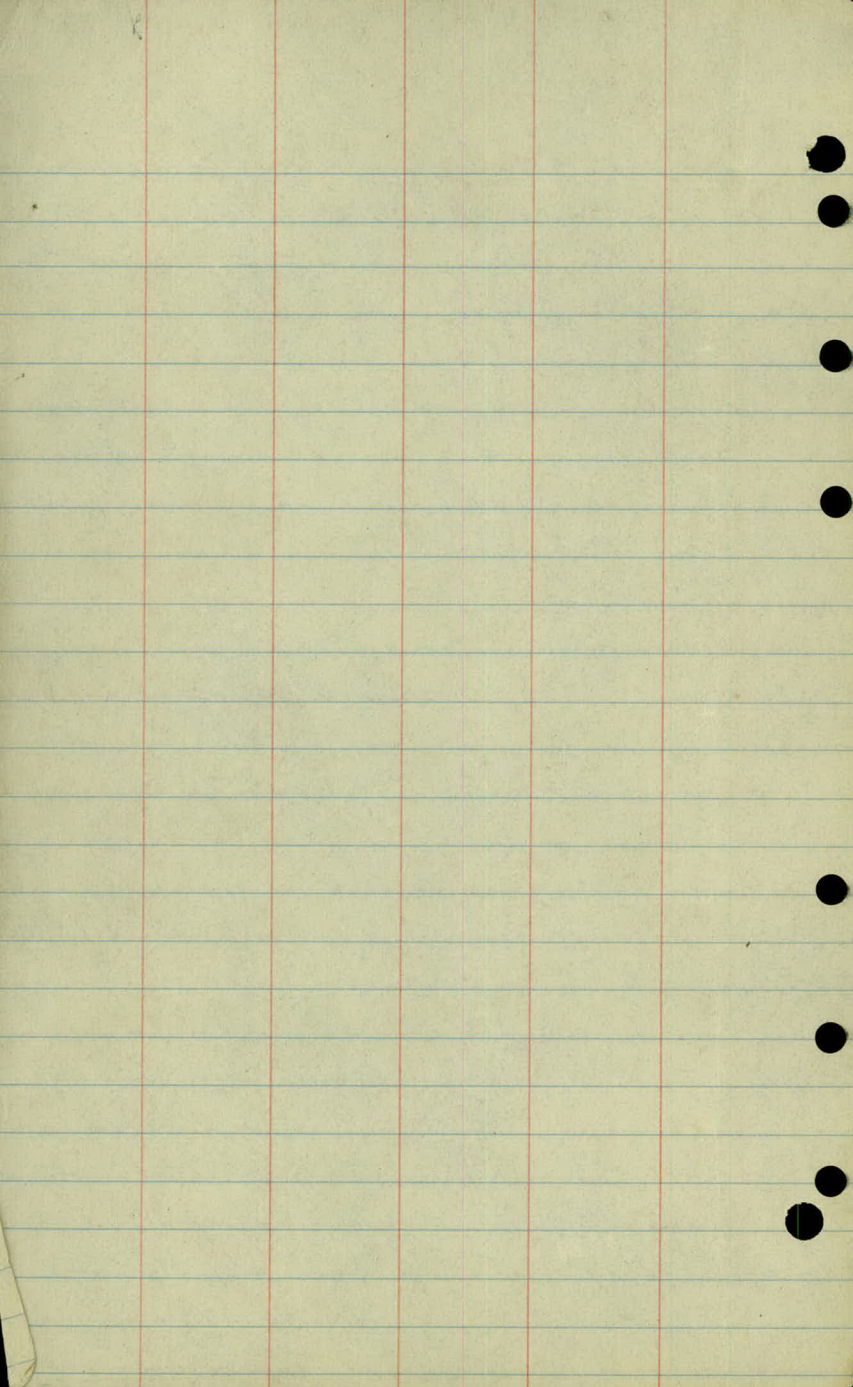
6.7

$\frac{11.3}{31.0} / 929.3$ Elev.

39.29

$\frac{5.5}{Elev. 320.9} / 25.0$

42.09



Co Rd "B"

White Bear Ave to No. St. Paul Road

Locations for Paving

Sta

£

10+21

Ent Rt .

9+59

Ent Rt .

9+47 Ent Lt

8+92

Ent Rt .

8+08

Ent Rt .

7+72 Ent Lt

6+57 £ 20' Street Lt



4+13

Ent Rt .

3+64

Ent Rt .

0+00

£ White Bear Ave



FK
LC
AB
CW

2 March 14, 1956
Cold Clear 11° 2

16+05

Ent Rt.

15+85 Ent Lt.

14+66 Ent Lt.

14+53

Ent Rt.

13+23

Ent Rt.

13+06. 2 16' Hazel Ave Left

✓

12+28

Ent Rt.

12+27 Ent Lt.

12+00

Ent Rt.

10+90 Ent Lt.

Sta

27+43

Ent Rt.

26+47

Ent Rt.

26+00

Ent Rt.

22+63 Ent Lt.

22+14 Ent Lt.

20+36

Ent Rt.

German

19+60 $\angle$ German Lt 20' top $\checkmark$

18+24

Ent Rt.

17+31

Ent Rt.

16+ 89 Ent Lt.

March 19, 1956
\$

3

52+45 Ent Lt .

52+13

✓
East Ave Rt 20'
wide

50+81

Ent Rt .

49+77

Ent Rt .

49+18

Ent Rt .

40+98 Ent Lt .

40+63 Ent Lt .

✓
39+23 6th St Left 20' Wide

✓ \$
32+68 20' W Seventh St 15'
W

28+43

Ent Rt .

2

Sta

58+62.5 · E N. St. Paul Road

58+79 End Rad 20' ·

58+30 Beg Rad 12' Lt ·

58+00 End Rad 33' ·

57+80 Beg Rad 12' ·

57+91 Ent Lt ·

57+21 Ent Lt ·

55+54 Ent Lt ·

55+13 Ent Lt ·

54+63 Ent Lt ·

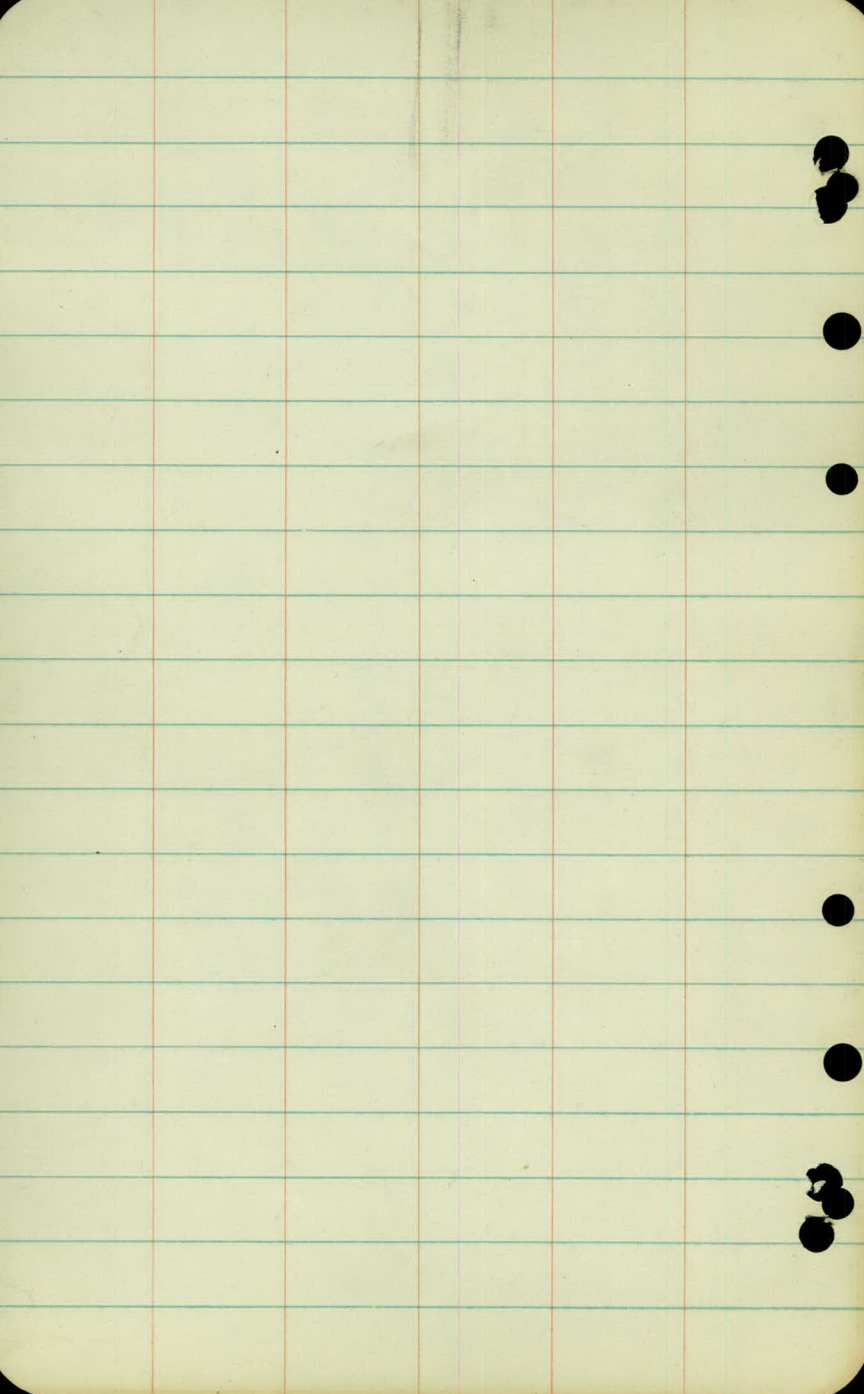
54+25 Ent Rt ·

54+04 Ent Lt ·

53+41 Ent Lt ·

March 14, 1956

4



Co Rd B at

N.P. X-ing

Sight Distances

For

TRAFFIC SIGNALS

A

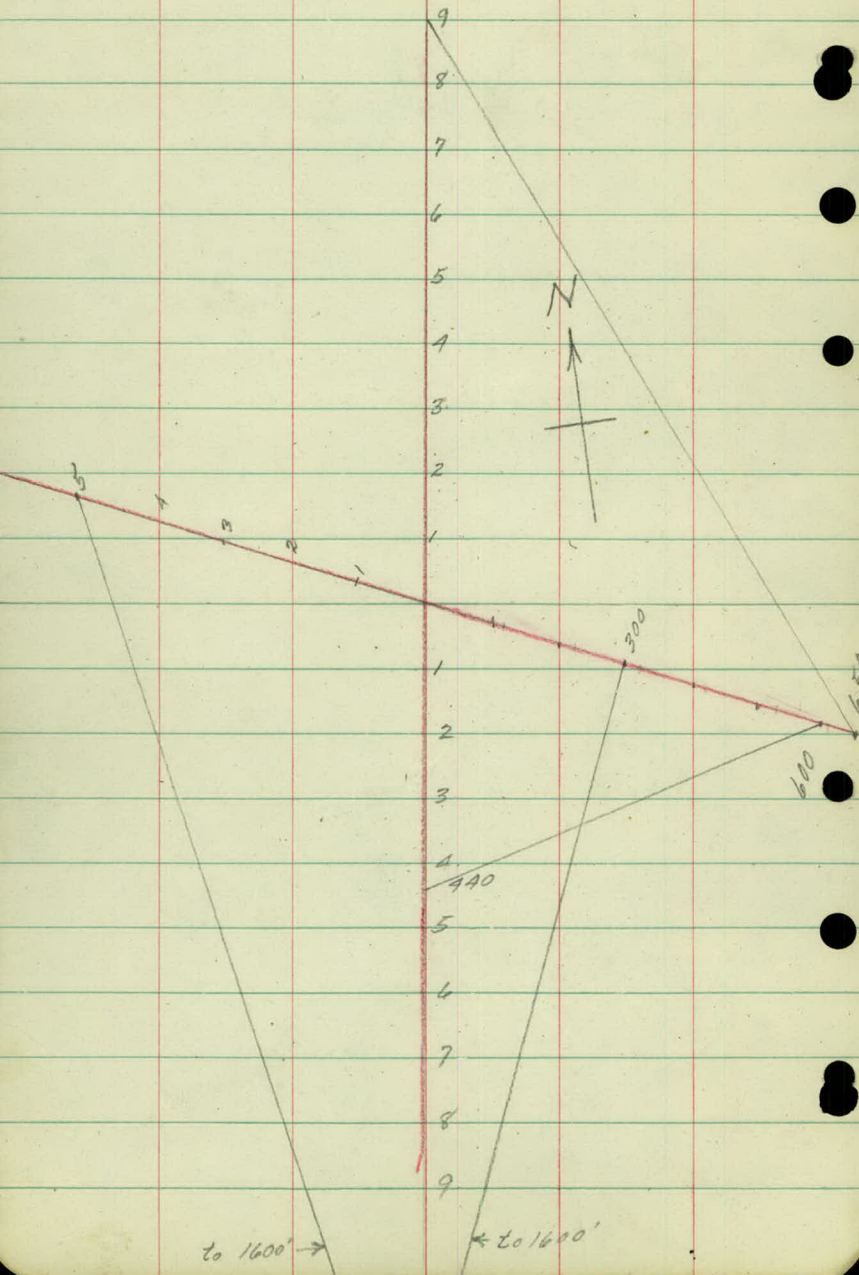
2 pages

35154. $\frac{1}{2}$
N.B. Tra
+ B.

Elev

+ Other Sight Dist

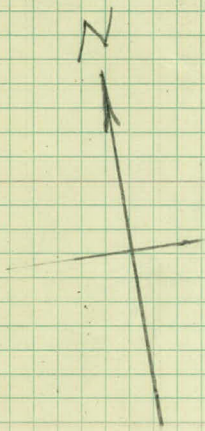
Platted
Hwy
1-76 S.S.



FK
LC

Dec. 27, 1955

2



1/2 Mi.

4
C

3
R

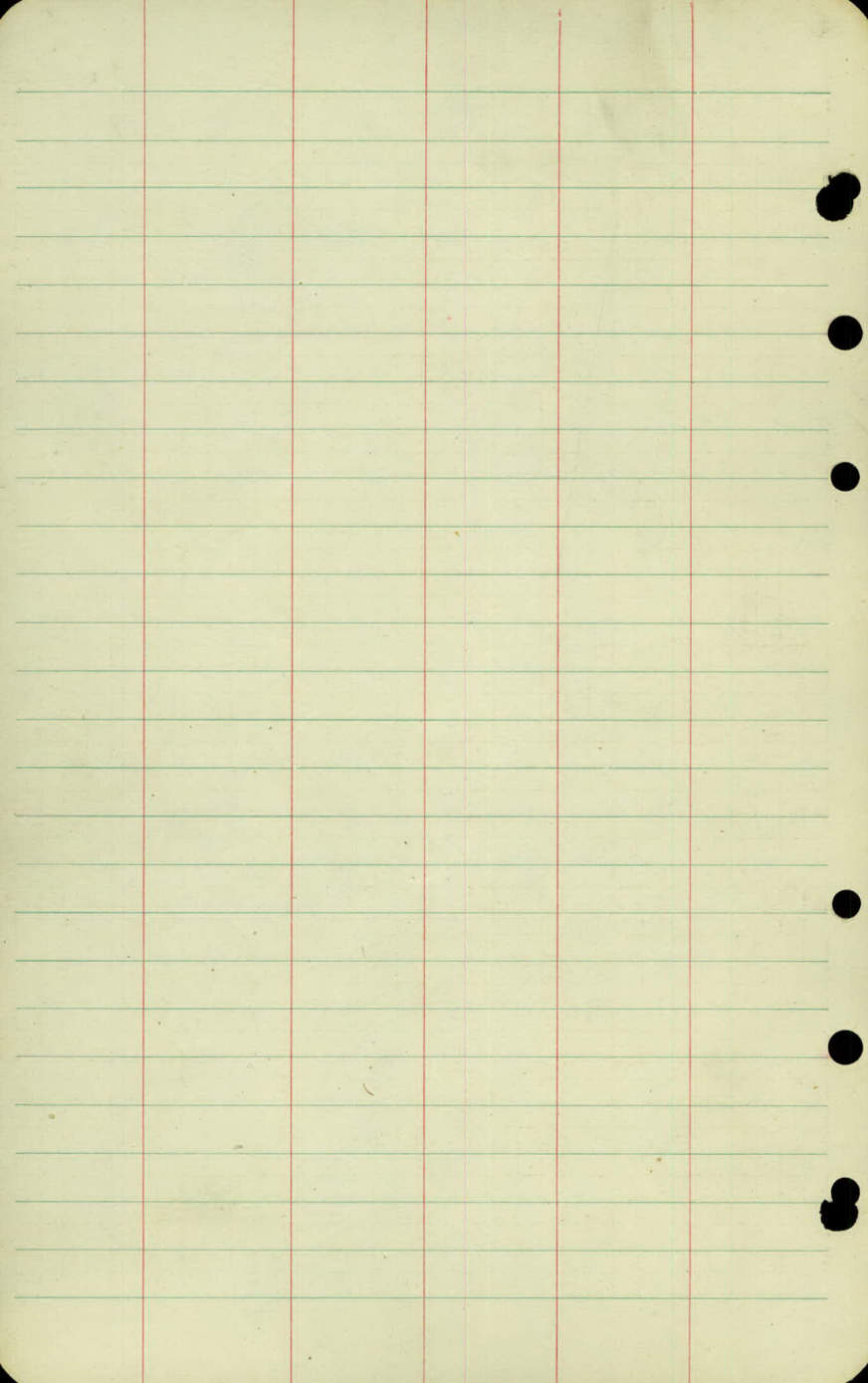
2
B

Dirt
Knoll

6
5
4
3
2
1
R R - R/W

+150
+35

+85
+70
+60



Jan 6, 1956

3

DIST.

VERT.
ANGLE

ROD
EQUIV.

ROD

DIFF.

ELEV.

Knoll Elevations

OBJECT

AZ.

STADIA

π at $\angle$ Co RL "B" and $\angle$ RR-RW
to $\angle$ RR-R/W North $0^{\circ}00'$

$\angle$ Tracks	358°10'	215'
"	358°55'	350'
Top of bank	315°30'	79'
$\angle$ Tracks	359°10'	468'
Top of Bank	341°55'	180'
$\angle$ Tracks	359°20'	600'
Top of bank	348°35'	255'
"	351°15'	340'
"	353°25'	416'
"	350°—	304'
"	335°55'	140'
G. E	329°—	195'
"	325°20'	251'
"	321°25'	325'
"	343°—	345'

Jan 6, 1956

4

DIST.

VERT.
ANGLEROD
EQUIV.

ROD

DIFF.

ELEV.

36°
40'
36°

H.I. 5.4

6.0

5.9

1.2

6.0

2.3

5.9

1.4

0.3

7.0

+ 0° 45'

3.0

+ 1° 20'

2.0

+ 1° 20'

6.1

+ 1° 20'

7.1

4.3

3.1

OBJECT

AZ.

STADIA

FK
LC
AB
CW
HAW

Jan 13, 1956

1

Topography

Co RLB at NP Tracks

5 pages

1/13/56

Co Rd B to West

sh Road sh
19 10 10 19

5

+41 Cor Fo 77 R.T/c
+76 Fo

+41 Trip 16" BE
75

+36 16" BE
85

4

sh Road sh
16 10-10 16

3

+85 X-Road Sign
16

2

+02 Curve Sign
15

1

sh B.T. sh
16 11-10 15

+32 Speed Sign
18

+61 Breather Pipe
22

+63 IP
52

+42 Fo +54 R.T/c +31 Xing Sign
38 Fe 17

+62 Breather Pipe
28

+24 IP
65

0

Jan 13, 1956

2

~~ES 10~~
~~10~~

0

0

0

x x x x

x x x x

+41 Stop sign
39

+52 End R
46

+73 E.R
28

+28 Beg R
10

+47 Beg R
10

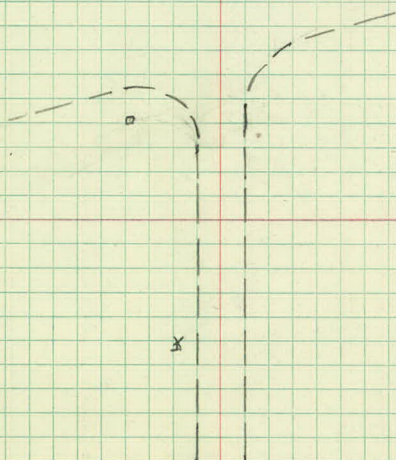
6 Sight Dis South 185'

+48 RR Xing
18

5

Jan 13, 1956

3



Co Rd B East

3

2

sh Road sh
15 10-10 15

1

sh Road sh
16 11 11 10

+03 Speed Sign
17

+39 Fe^{Ext} 44 +53 R. Tie Fe +48 Br. Pipe 30

+65 Fe^{Ext}
35

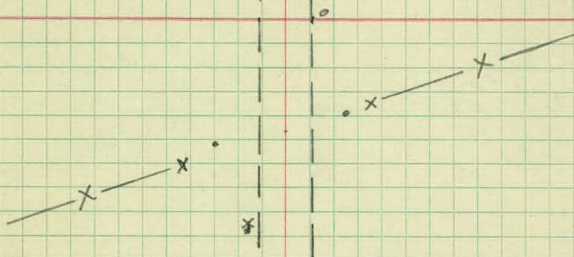
+16 R.R. Xing
17

+60 Br. Pipe
25

0

Jan 13, 1956

4



+35 $\frac{Cn Ho}{59}$

+05 $\frac{Cor Ho}{59}$

5

$\frac{Sh}{16}$ $\frac{Road}{10}$ $\frac{Sh}{13}$

+94 $\frac{RR Xing Sign}{17}$

+66 $\frac{PP}{28}$

4

Jan 13, 1956

5

25x30



