

Dr. 6 - BK. 92

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ Plan _____ Survey

_____ LEXINGTON AVE. _____

From Co. Rd. "E" _____ To Co. Rd. "I" _____

Road Acc't. No. 3 _____

Date Filed. 1936 _____

File _____

Alignment
Lexington Ave
From Co. Rd "E" to Co. Rd I

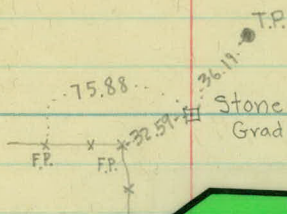
Sta.	Point	Lt	Rt.
26+41.95	P.L.		00° 07'

3+12.5	P.O.T.		
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2+97.0	P.O.T.		
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0+00	P.L.	00° 11'	
------	------	---------	--

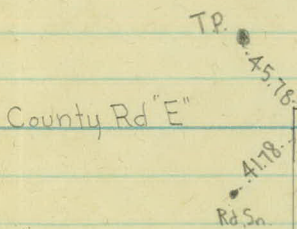
N 0° 56' W



Stone Mont E 1/4 Cor. Sec 27
Grade 8/5/35



S00 LINE RY.



County Rd "E"

Stone Mont NE. Cor. Sec. 34
Grade 8/5/35

27 Pavement

Station	Point	Lt	Rt
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79+18.73	P.I.		
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		00° 01'	
--	--	---------	--

67 +119	P.O.T.		
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63 +150	P.O.T.		
---------	--------	--	--

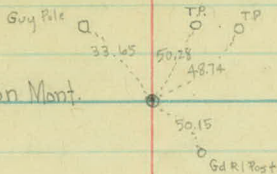
52+82.88	P.I.		
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		00° 05'	
--	--	---------	--

N 0° 45' W N 0° 44' W

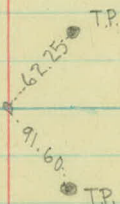
Victoria St. Iron Mont.

Ties 8/30/35



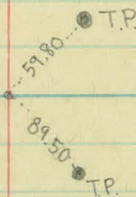
Nail

Ties 8/5/35



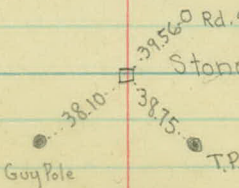
Nail

Ties 8/5/35



Co Rd "F"

Rd. Sign
Stone Mont. NE Cor Sec. 77



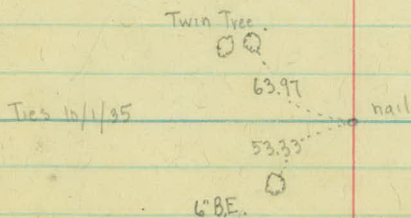
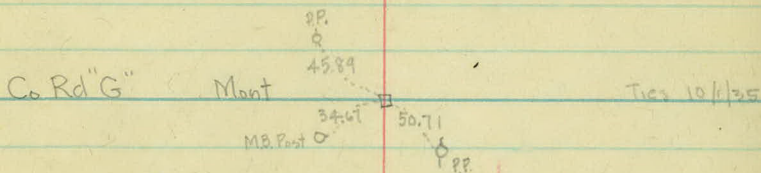
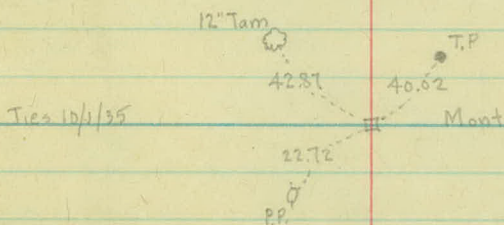
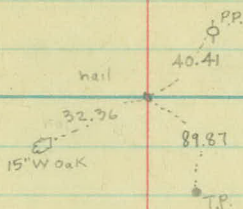
Sta	Point	Lt.	Rt.
-----	-------	-----	-----

147+00	P.O.T.		
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131+89.20	P.I.	0° 01'	
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105+56.7	P.I.	0° 11'	
----------	------	--------	--

96+34.26	P.O.T.		
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Sta

Point

Δ
Lt

Δ
Rt.

210+96.75

P.I.

L'

193+99.45

P.O.T

184+60.63

P.I.

$0^{\circ}12'30''$

174+07.91

P.O.T

158+20.53

P.I.

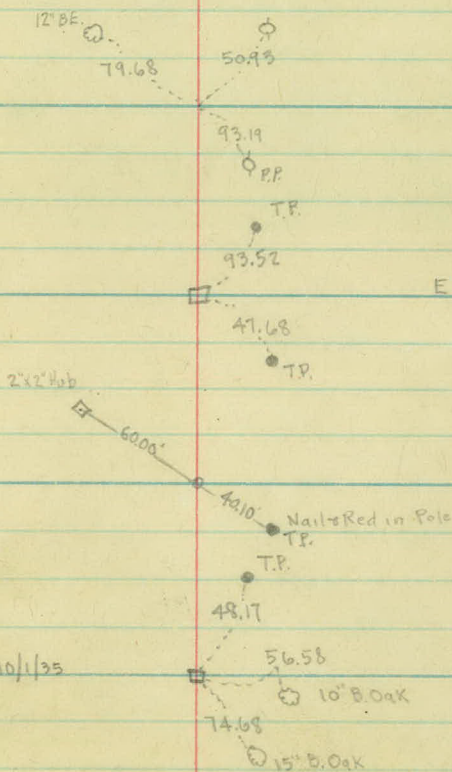
$0^{\circ}14'$

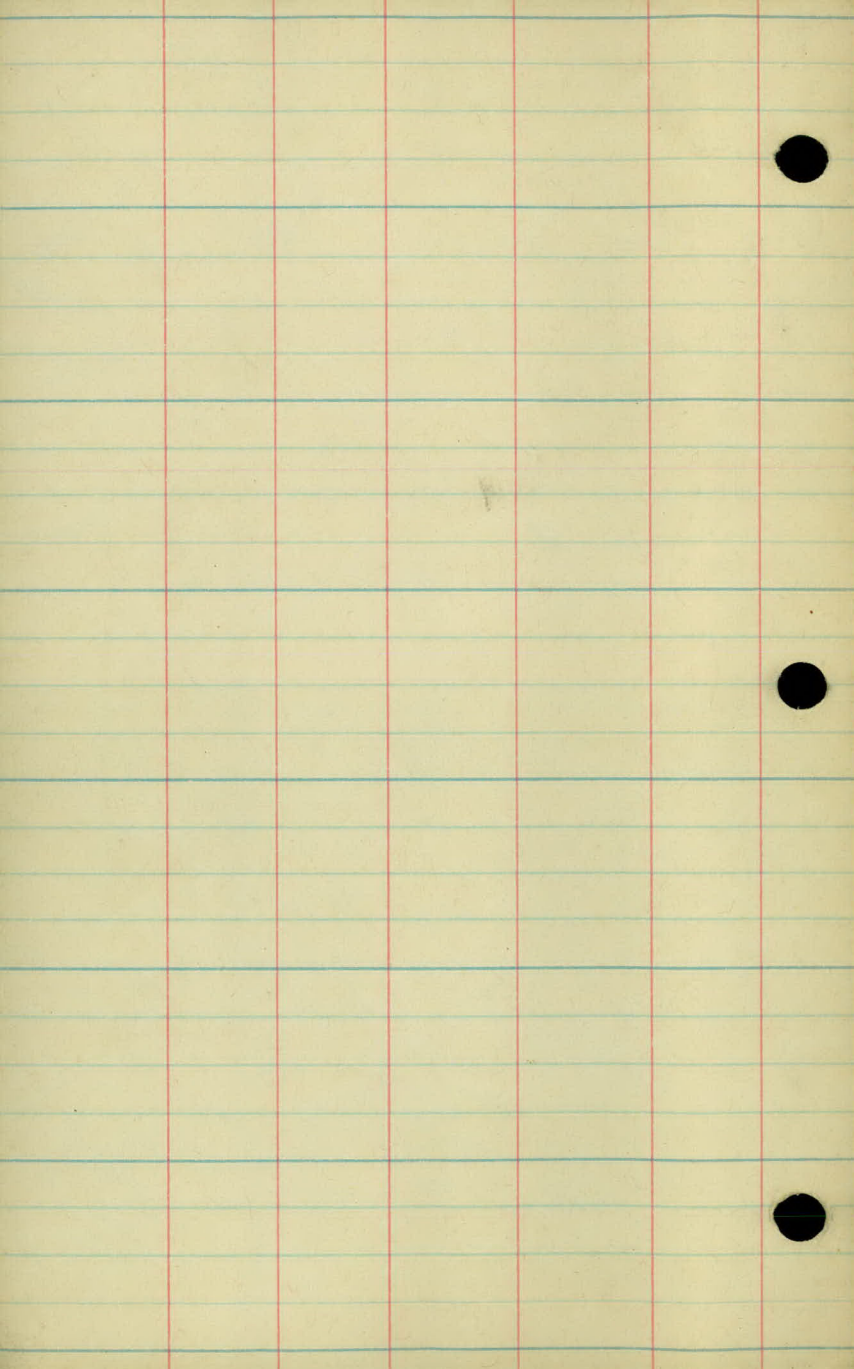
Co Rd I

Mont.

E 1/4 Cor Sec 10

NE Cor S 15 Mont. Ties 10/1/35





TOPOG
LEXINGTON AVE
CO. RD. E TO CORDI

Fce 20
RA 9-10

$$\begin{array}{r} +09 \text{ Rd Sn} \\ \hline 20 \end{array}$$

$$\begin{array}{r} +43 \text{ TP} \\ \hline 28 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ \hline 10 \quad 10 \end{array}$$

$$\begin{array}{r} +65 \text{ T.P.} \\ \hline 28 \\ +32 \text{ Xing Sn} \\ \hline 15 \end{array}$$

$$\begin{array}{r} +53 \text{ F.Cov} \\ \hline 22 \\ +12.5 \text{ Trk} \end{array}$$

$$\begin{array}{r} +10 \text{ Trk} \\ \hline 50 \end{array}$$

$$+17 \text{ Trk}$$

$$\begin{array}{r} +66 \text{ TP} \\ +54 \text{ F.Cov} \quad 40 \\ \hline 22 \\ +37 \text{ TP} \\ \hline 27 \end{array}$$

$$\begin{array}{r} +74 \text{ End Oil Spv} \\ \hline 18 \\ +43 \text{ TP} \quad +78 \text{ RR Xing Sn} \\ \hline 51 \quad 16 \end{array}$$

$$\begin{array}{r} +11 \text{ F.Cov} \\ \hline 21 \\ +39 \text{ TP} \\ \hline 28 \end{array}$$

$$\begin{array}{r} +83 \text{ W.C.} \\ \hline 171 \\ +37 \text{ PP} \\ \hline 29 \\ +10 \text{ Car Mix Plant} \\ \hline 48 \end{array}$$

$$\begin{array}{r} +94 \text{ Cor Tanks} \\ \hline 21 \\ +84 \text{ Cor Tanks} \\ \hline 167 \\ +68 \text{ Cor Shed} \\ \hline 167 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ \hline 8 - 12 \end{array}$$

$$\begin{array}{r} +36 \text{ PP} \\ \hline 28 \end{array}$$

$$\begin{array}{r} +18 \text{ Shoulder} \\ \hline 50 - 82 \\ +01 \text{ End Pave} \end{array}$$

$$\begin{array}{r} +96 \text{ RR Sn} \\ \hline 24 \\ +37 \text{ Cor Gar} \\ \hline 159 \end{array}$$

$$\begin{array}{r} -10 \text{ Shoulder} \\ \hline 47 - 140 \end{array}$$

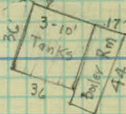
Pasture

Hay Field

300' LINE RX



Oil Tanks



Crapper 5' 5'
Shed 8' 12'



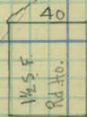
Gar 16'

CO. RD "E" OIL SURFACE



Macadam

q' Conc



$$\frac{Fce}{25}$$

$$\frac{Rd}{11-10}$$

$$\frac{+44 TP}{28}$$

11

$$\frac{Fce}{25}$$

$$\frac{Rd}{11-10}$$

10

$$\frac{Rd}{11-10}$$

$$\frac{+68 T.P.}{28}$$

9

$$\frac{Fce}{25}$$

$$\frac{Rd}{11-10}$$

8

$$\frac{Rd}{11-10}$$

$$\frac{+94 TP}{29}$$

7

$$\frac{Fce}{25}$$

$$\frac{Rd}{10-10}$$

$$\begin{array}{r} PR \\ +02(Rd)Sn \\ 21 \\ \hline Fce \\ 25 \end{array}$$

$$\frac{Rd}{10-10}$$

$$\frac{+18 TP}{30}$$

6

5

Pasture

Hay Field

$$\frac{Fee}{27}$$

$$\frac{Rd}{11-10}$$

$$\frac{+03 Fee Cor}{50}$$

$$\frac{+23 TP}{26}$$

18

$$\frac{Fee}{29}$$

$$\frac{Rd}{11-10}$$

$$\begin{array}{r} +24-24 Tr \\ 31 \\ +13 Ent \end{array}$$

17

$$\frac{Fee}{31}$$

$$\frac{Rd}{11-10}$$

$$+96-20 Tr$$

$$\begin{array}{r} 32 \\ +66 TP \\ 27 \end{array}$$

$$\begin{array}{r} +77-15 Tr \\ 30 \end{array}$$

$$\begin{array}{r} +54-24 StP - 12 StP \\ 21 \quad 29 \end{array}$$

16

$$\begin{array}{r} +09-24 \times 48 CM \quad \#3-45 \\ 24 - 24 \end{array}$$

15

$$\frac{Fee}{27}$$

$$\frac{Rd}{11-10}$$

$$\begin{array}{r} +95 TP \\ 27 \end{array}$$

$$\begin{array}{r} +68 Field Ent - 18 \times 16 V.P. \\ 25 \end{array}$$

14

$$\frac{Rd}{11-10}$$

$$\begin{array}{r} +18 TP \\ 27 \end{array}$$

13

$$\begin{array}{r} +57 Fee Cor \\ 25 \end{array}$$

12

Pasture

Hay Field

c=p

nn

$$\frac{Fce}{27}$$

$$\frac{Rd}{11-10}$$

$$\frac{+89 F. Cor.}{55}$$

25

$$\frac{Rd}{11-9}$$

$$\frac{+92 TP}{27}$$

24

$$\frac{Fce}{53-23}$$

$$+58 F Cor$$

$$26$$

$$+18 TP$$

$$27$$

23

$$\frac{Rd}{10-9}$$

$$+11-24' \times 68' CM 3-96$$

$$+35 End Culv$$

$$25$$

22

$$\frac{Fce}{27}$$

$$\frac{Rd}{11-10}$$

$$\frac{Fce}{26}$$

$$\frac{+85 End Culv}{24}$$

$$\frac{+41 TP}{27}$$

21

$$+41 TP$$

20

$$\frac{Fce}{50}$$

$$\frac{Fce}{27}$$

$$\frac{Rd}{11-10}$$

$$\frac{Fce}{27}$$

$$+69 F Cor$$

$$26$$

$$+68 TP$$

$$27$$

19

Pasture



Hay Field



Cattle Lane

Pasture

3 Bot. Ditch
(Dry)



$$\begin{array}{r} \text{Brush} \\ 100 - 27 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 11 - 11 \end{array}$$

$$\begin{array}{r} +42 \text{ PP} \\ 27 \end{array}$$

32

$$\begin{array}{r} \text{Rd} \\ 11 - 11 \end{array}$$

$$\begin{array}{r} +30 \text{ Beg Brush} \\ 27 \\ +14 - 12 \text{ Tr} \\ 19 \end{array}$$

31

$$\begin{array}{r} +96 \text{ PP} \\ 27 \end{array}$$

30

$$\begin{array}{r} +51 \text{ PP} \\ 27 \end{array}$$

29

$$\begin{array}{r} \text{Rd} \\ 11 - 10 \end{array}$$

28

$$\begin{array}{r} +05 \text{ PP} \\ 27 \end{array}$$

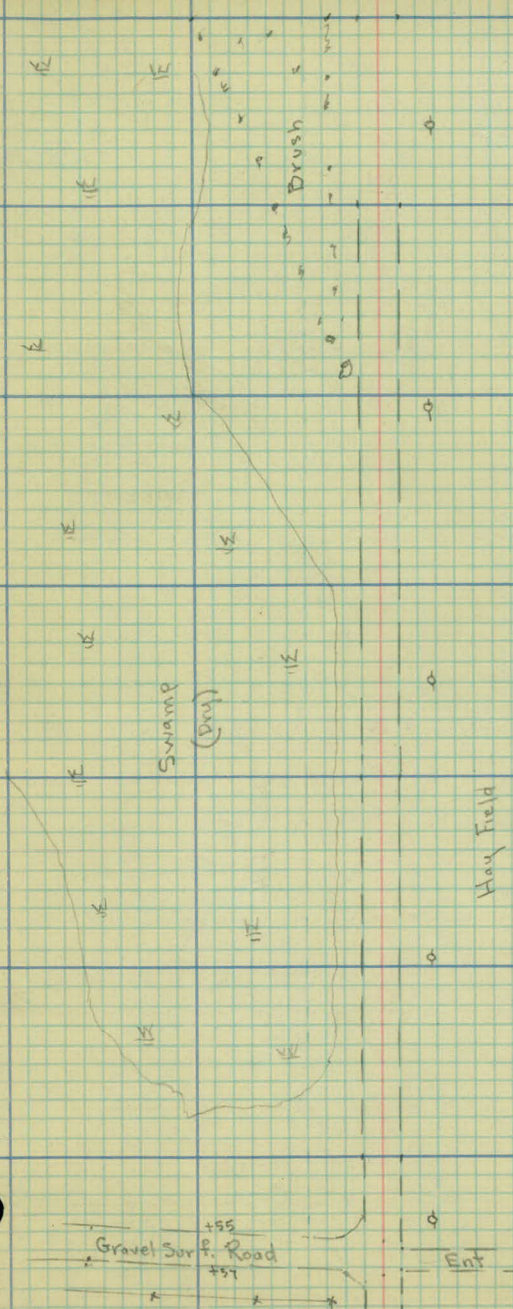
27

$$\begin{array}{r} \text{Rd} \\ 11 - 10 \end{array}$$

$$\begin{array}{r} +67 \text{ PP} \\ 26 \\ +44 \text{ Ent} \end{array}$$

26

$$\begin{array}{r} +23 \text{ F Cur} \\ 27 \end{array}$$



Woods
31

39

Rd
11 - 10

+ 69 PP
27

38

+ 36 Woods
29

+ 48 F. Ent - 15' x 20' CM
27
+ 24 PP
27

37

Woods
80

Rd
11 - 10

36

Woods
34

+ 58 - 15' x 42' v.s. #3-41 + 79 PP
19 - 23 27

35

+ 55 End Brush Beg Wood
34

+ 33 PP
27

34

Brush
125 - 51

Rd
11 - 11

+ 88 PP
27

33

Hay

WOODS

Rot Hole
(Dry)

517

2' Bot Ditch

Hay Field

Bvush

46

$$\frac{\text{Woods}}{33}$$

$$\frac{\text{Rd}}{13-7}$$

$$\frac{+97 \text{ PP}}{27}$$

$$\frac{+24-20 \text{ Tr}}{11}$$

$$+15 \text{ Ent}$$

$$\frac{+96-18 \text{ Tr}}{14}$$

$$\frac{+96 \text{ FCor}}{29}$$

$$\frac{+84-18 \text{ Tr}}{13}$$

$$\frac{+51 \text{ PP}}{26}$$

45

$$\frac{\text{Rd}}{12-8}$$

$$\frac{\text{Fce}}{31}$$

$$\frac{+36 \text{ FCor}}{31}$$

$$\frac{+05 \text{ TP}}{26}$$

44

$$\frac{\text{Woods}}{30}$$

$$\frac{\text{Rd}}{11-9}$$

$$\frac{+61 \text{ PP}}{26}$$

42

$$\frac{+55 \text{ Woods}}{34}$$

$$\frac{+14 \text{ PP.}}{27}$$

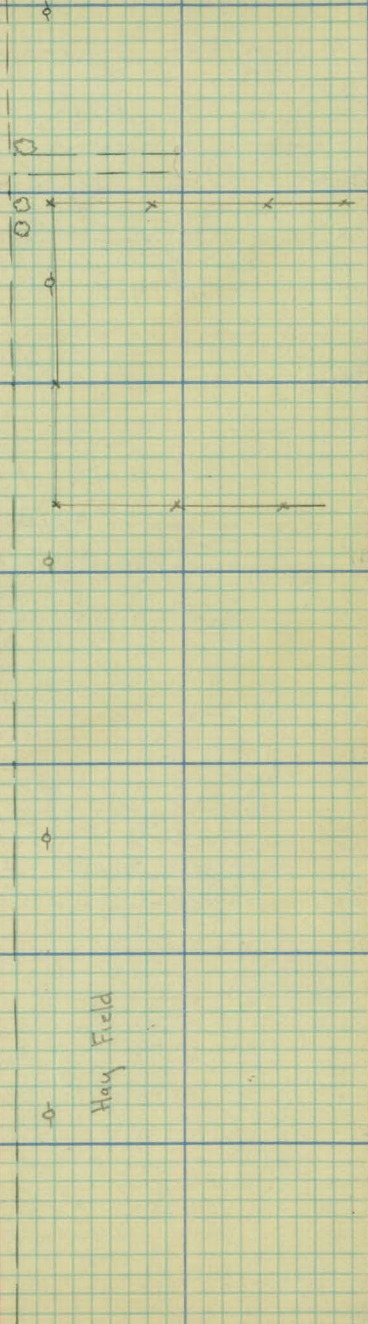
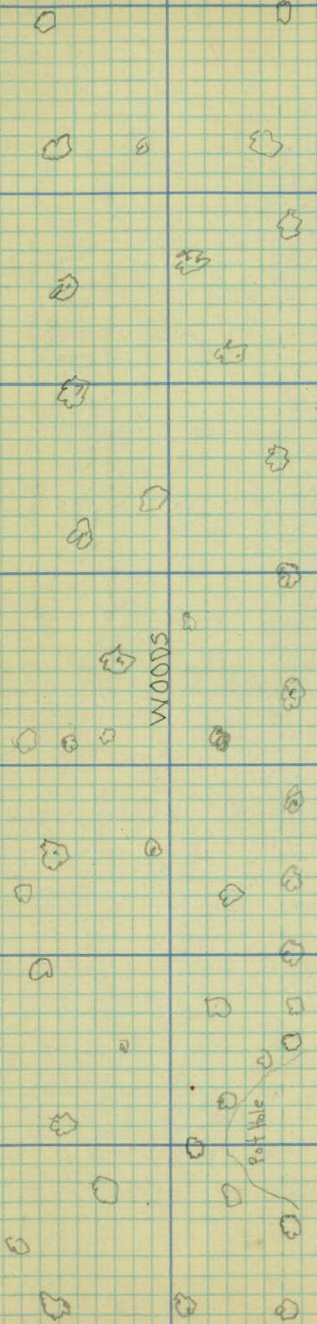
41

$$\frac{\text{Woods}}{85}$$

$$\frac{\text{Rd}}{11-10}$$

$$\frac{+60 \text{ Woods}}{31}$$

40



$$\begin{array}{r} \text{Rd} \\ 11 - 9 \end{array}$$

$$\begin{array}{r} +91 \text{ T.P.} \\ 27 \end{array}$$

$$\begin{array}{r} +18 \text{ Rd} \\ 12 - 9 \end{array}$$

$$\begin{array}{r} +27 \text{ Rd Sn} \\ 17 \end{array}$$

$$\begin{array}{r} +10 \text{ Rd Sn} \\ 28 \end{array}$$

$$\begin{array}{r} +93 \text{ Shoulde} \\ 40 - 33 \end{array}$$

$$\begin{array}{r} +56 \text{ Gng Po} \\ 26 \end{array}$$

$$\begin{array}{r} +70 \text{ Shoulder} \\ 42 - 31 \end{array}$$

$$\begin{array}{r} +58 \text{ F Cor} \\ 25 \end{array}$$

$$\begin{array}{r} +82 - 15 \times 40' \text{ CM} \\ 19 \end{array}$$

$$\begin{array}{r} +29 \text{ Rd Sn.} \\ 16 \end{array}$$

$$\begin{array}{r} +55 \text{ PP} \\ 27 \end{array}$$

$$\begin{array}{r} +35 \text{ Rd} \\ 12 - 10 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 11 - 9 \end{array}$$

$$\begin{array}{r} +17 \text{ PP} \\ 27 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 11 - 9 \end{array}$$

$$\begin{array}{r} \text{Fce} \\ 25 \end{array}$$

$$\begin{array}{r} +76 \text{ PP} \\ 27 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 12 - 8 \end{array}$$

$$\begin{array}{r} +99 \text{ Rd Sn} \\ 22 \end{array}$$

$$\begin{array}{r} +36 \text{ PP} \\ 27 \end{array}$$

$$\begin{array}{r} \text{Woods} \\ 100 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 12 - 7 \end{array}$$

$$\begin{array}{r} \text{Fce} \\ 25 \end{array}$$

$$+17 - 12'' \times 62' \text{ CM}$$

$$\begin{array}{r} +05 \text{ F Cor} \\ 25 \end{array}$$

$$\begin{array}{r} \text{Woods} \\ 33 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 12 - 7 \end{array}$$

COORDINATE

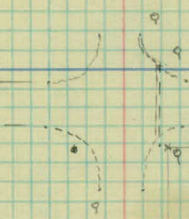
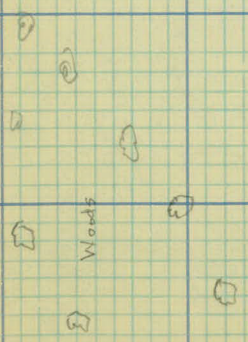
OIL SURFACE

$\frac{1}{C_3H}$

$\frac{1}{C_3H}$

Brush

Woods



$$\frac{Rd}{11-10}$$

60

$$\frac{8d}{11-10}$$

$$\frac{+89 PP}{27}$$

$$\frac{+50 PP}{27}$$

59

$$\frac{Rd}{11-10}$$

$$\frac{+09 PP}{27}$$

58

$$\frac{Rd}{11-10}$$

$$\frac{+71 PP}{27}$$

$$\frac{+68 Rd Sn}{21}$$

$$\frac{+58 Ent-12" \times 20' CM}{24}$$

56

$$\frac{Rd}{11-10}$$

$$\frac{+29 PP}{27}$$

$$\frac{Rd}{11-10}$$

55

54

Cultivated

-0

0

Cultivated

0

0

0

0

$$\frac{+99 \text{ PP}}{27}$$

67

$$\frac{Rd}{11-11}$$

$$\frac{Fce}{25}$$

+90 Trs + Br

100

+62 Fd Ent 12'x20CM

$$\frac{+54 \text{ PP}}{27}$$

+38 Fd. Ent

$$\frac{+55 \text{ Brz Trs}}{33}$$

$$\frac{Fce}{26}$$

66

+85 Sm. Trs + Brush

45

+25 Fd. Ent 12'x4CM

$$\frac{+08 \text{ Brz Fce-PP}}{22 \quad 26}$$

65

25

$$\frac{Rd}{11-10}$$

$$\frac{+29-4'SW}{13}$$

+92 Ent

$$\frac{+15 \text{ Cor Ho}}{81}$$

$$\frac{+64 \cdot 12'' \text{ Tr} - 12'' \text{ Tr}}{18 \quad 33}$$

64

$$\frac{+91 \text{ Apple E}}{39}$$

$$\frac{+74 \text{ Row Fruit Trs}}{23}$$

$$\frac{+68 \text{ PP.}}{26}$$

63

$$\frac{Rd}{11-11}$$

$$\frac{+30 \text{ PP}}{27}$$

62

61

②

Brush Smith

③

④

⑤

⑥

⑦ ⑧ ⑨ ⑩

==

X

⑪ ⑫

At this point

2 S.F.

46'

30

⑬ ⑭ ⑮ ⑯ ⑰

Cult.

Cult.

$$\frac{F_{cc}}{43}$$

$$\frac{+90 \text{ P. Line } 4" \text{ Frame}}{40}$$

74

$$\frac{+70 \text{ H-Ten Tower}}{62}$$

$$\frac{+75 \text{ PP}}{22}$$

$$\frac{+52 \text{ TP}}{93}$$

73

$$\frac{+40 \text{ H" Frame}}{62}$$

$$\frac{+30 \text{ PP}}{25}$$

72

$$\frac{F_{cc}}{36}$$

71

$$\frac{+86 \text{ PP}}{27}$$

70

$$\frac{F_{cc}}{40}$$

$$\frac{+42 \text{ PP}}{27}$$

69

$$\frac{R1}{11-11}$$

$$\frac{F_{cc}}{31}$$

68

Cult.

High Tension
Power Lines

KW Fee Omitted &
Po Line Xing - See X-See Notes

Cult.

$$\begin{array}{r} \text{Fc} \\ 76 \end{array} \quad \begin{array}{r} \text{G.R.} \\ 12 \end{array} \quad \begin{array}{r} \text{Rd} \\ 9 - 13 \end{array}$$

$$\begin{array}{r} \text{Fcc} \\ 34 \end{array}$$

$$\begin{array}{r} +50 \text{ Water Hole} \\ 100 \end{array}$$

$$\begin{array}{r} \text{G.R.} \\ 13 \end{array}$$

$$\begin{array}{r} +90 \text{ Bay Orchard} \\ 45 \\ +81 \text{ End GR} \\ 19 \end{array}$$

$$\begin{array}{r} \text{G.R.} \\ 19 \end{array}$$

$$\begin{array}{r} +99 \text{ PP} \\ 27 \\ +90 \text{ Spillway} \\ 18 \end{array}$$

$$\begin{array}{r} +43 \text{ Spillway} \\ 4 \end{array}$$

$$\begin{array}{r} +28 \text{ Water Hole} \\ 100 \end{array}$$

$$\begin{array}{r} \text{Fc} \\ 44 \end{array}$$

$$\begin{array}{r} \text{G.R.} \\ 14 \end{array}$$

$$\begin{array}{r} \text{G.R.} \\ 18 \end{array}$$

$$\begin{array}{r} \text{Fc} \\ 28 \end{array}$$

$$\begin{array}{r} +56 \text{ End Culv} \\ 60 \end{array}$$

$$\begin{array}{r} +47 \text{ Guy R.} \\ 19 \end{array}$$

$$\begin{array}{r} +21 \text{ Rd Sn} \\ 15 \end{array}$$

$$\begin{array}{r} \text{Fcc} \\ 40 \end{array}$$

$$\begin{array}{r} \text{G.R.} \\ 15 \end{array}$$

$$\begin{array}{r} +70 \text{ Rd} \\ 9 - 13 \end{array}$$

$$\begin{array}{r} +52 \text{ TP} \\ 26 \end{array}$$

$$\begin{array}{r} +32 \text{ Shoulder} \\ 53 \end{array}$$

$$\begin{array}{r} +04 \text{ Shoulder} \\ 50 \end{array}$$

$$\begin{array}{r} +59 \text{ G.R.} \\ 18 \end{array}$$

$$\begin{array}{r} +42 \text{ G.R.} \\ 30 \end{array}$$

$$\begin{array}{r} +34 \text{ G.R.} \\ 53 \end{array}$$

$$\begin{array}{r} +63 \text{ PP} - \text{Fc} \\ 27 \end{array}$$

$$\begin{array}{r} +57 \text{ Rd Sn} \\ 20 \end{array}$$

$$\begin{array}{r} \text{G.R.} \\ 52 \end{array}$$

$$\begin{array}{r} +72 \text{ G.R.} \\ 17 \end{array}$$

$$\begin{array}{r} +92 \text{ G.R.} \\ 29 \end{array}$$

$$\begin{array}{r} +52 \text{ Rubble Spillway} \\ 15 \end{array}$$

$$\begin{array}{r} +70 \text{ Rd} \\ 11 - 11 \end{array}$$

$$\begin{array}{r} +14 \text{ PP} \\ 24 \end{array}$$

$$\begin{array}{r} +78 \text{ Fcc} \\ 27 \end{array}$$

$$\begin{array}{r} +62 \text{ End Culv} \\ 65 \end{array}$$

$$\begin{array}{r} \text{Fc} \\ 28 \end{array}$$

$$\begin{array}{r} \text{G.R.} \\ 15 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 11 - 11 \end{array}$$

$$\begin{array}{r} \text{G.R.} \\ 18 \end{array}$$

$$\begin{array}{r} \text{Fc} \\ 24 \end{array}$$

$$\begin{array}{r} \text{Fcc} \\ 28 \end{array}$$

$$\begin{array}{r} \text{Fcc} \\ 26 \end{array}$$

$$\begin{array}{r} +67 \text{ PP} \\ 22 \end{array}$$

$$\begin{array}{r} +74 \text{ Clump(?) Willows} \\ 57 \end{array}$$

$$\begin{array}{r} \text{Fcc} \\ 28 \end{array}$$

$$\begin{array}{r} \text{G.R.} \\ 16 \end{array}$$

$$\begin{array}{r} \text{Gd.R.} \\ 16 \end{array}$$

$$\begin{array}{r} \text{Fcc} \\ 24 \end{array}$$

$$\begin{array}{r} +34 \text{ Fcc} \\ 30 \end{array}$$

$$\begin{array}{r} +37 \text{ Bay Gd.R.} \\ 10 \end{array}$$

$$\begin{array}{r} +76 \text{ Fcc} \\ 24 \end{array}$$

$$\begin{array}{r} +18 \text{ PP} \\ 20 \end{array}$$

$$\begin{array}{r} +07 \text{ Bay Gd.R.} - \text{Rd Sn} \\ 16 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 11 - 11 \end{array}$$

$$\begin{array}{r} +13 \text{ TP} \\ 31 \end{array}$$

$$\begin{array}{r} +49 \text{ Fcc} \\ 43 \end{array}$$

$$\begin{array}{r} +48 \text{ 101011 Ten To.} \\ 36 \end{array}$$

$$\begin{array}{r} 19 \end{array}$$

$$75$$

Water Hole

3.5' R. Spillway

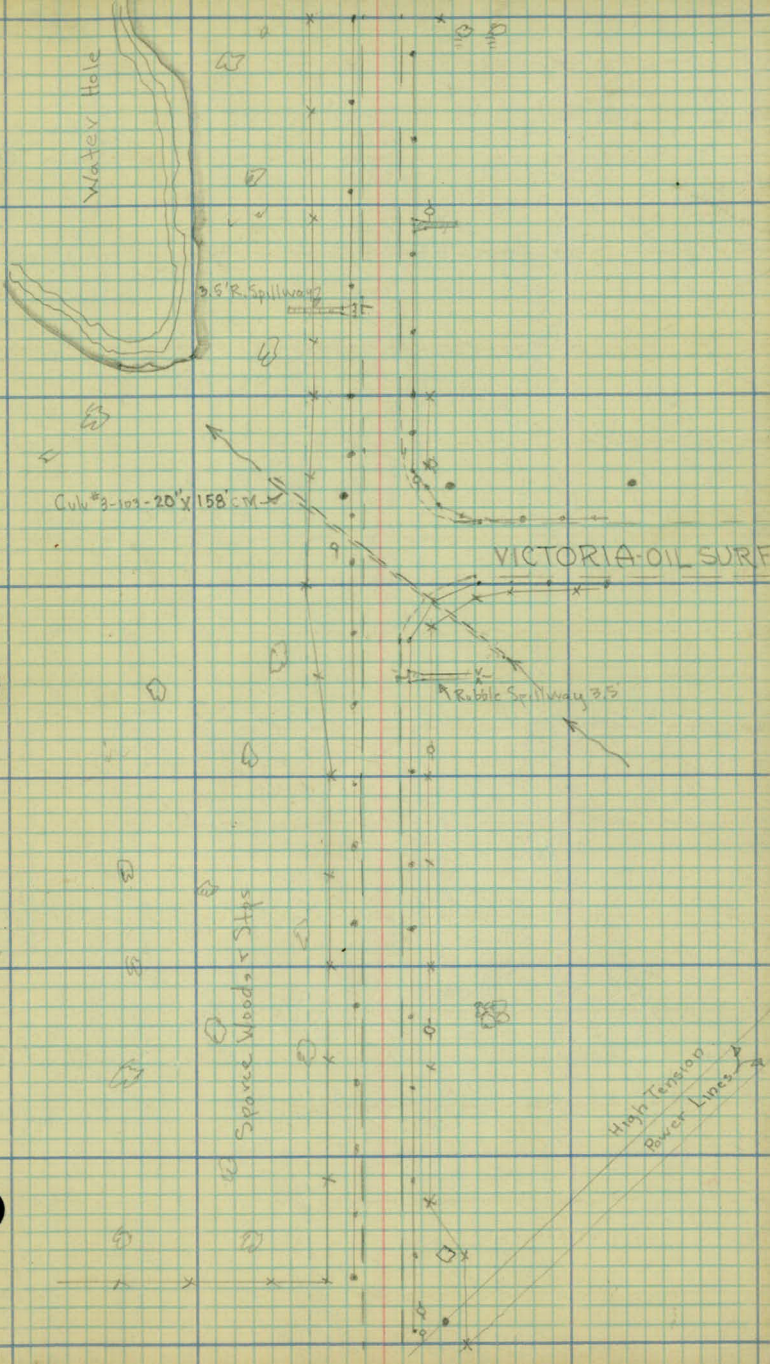
Culv #3-109-20'x158' CM

VICTORIA OIL SURF

Rubble Spillway 3.5'

Spaced Woods & Steps

High Tension
Power Lines



89

$$\begin{array}{r}
 +27 \text{ PP} \\
 \hline
 28 \\
 +22 \text{ Cor Ho} \\
 \hline
 117 \\
 +16 \text{ Ent-12'x20'CM} \\
 \hline
 22 \\
 +100 \text{ End Orch.} \\
 \hline
 38
 \end{array}
 \quad
 \begin{array}{r}
 +79.10 \text{ Win Oak} \\
 \hline
 26 \\
 +56-8'' \text{ Tr} \\
 \hline
 26
 \end{array}$$

88

$$\begin{array}{r}
 +42 \text{ Beg Orchard} \\
 \hline
 36
 \end{array}$$

87

$$\begin{array}{r}
 \text{Rd} \\
 \hline
 11-10
 \end{array}$$

$$\begin{array}{r}
 +70 \text{ PP} \\
 \hline
 27
 \end{array}$$

86

$$\begin{array}{r}
 +54 \text{ Ent} \\
 +80 \text{ F Cor} \\
 \hline
 82 \\
 +24 \text{ 10'' Tr}
 \end{array}$$

$$\begin{array}{r}
 +82.5 \text{ Cor} \\
 \hline
 26 \\
 +74 \text{ Fd Ent} \\
 \hline
 27 \\
 +42 \text{ End Orchard} \\
 \hline
 87
 \end{array}$$

85

$$\begin{array}{r}
 +15 \text{ Cor Barn} \\
 \hline
 26 \\
 105 \text{ F.c} \\
 \hline
 34
 \end{array}$$

$$\begin{array}{r}
 \text{Rd} \\
 \hline
 11-11
 \end{array}$$

$$\begin{array}{r}
 +12 \text{ PP} \\
 \hline
 27 \\
 \text{Fce} \\
 \hline
 27
 \end{array}$$

$$\begin{array}{r}
 +65 \text{ PP} \\
 \hline
 21
 \end{array}$$

$$\begin{array}{r}
 +83 \text{ F Ent-12'x16'CM} \\
 \hline
 24
 \end{array}$$

84

$$\begin{array}{r}
 +95 \text{ Fd Ent-12'x16'CM} \\
 \hline
 24
 \end{array}$$

$$\begin{array}{r}
 +67 \text{ Cor Ho} \\
 \hline
 169
 \end{array}$$

$$\begin{array}{r}
 +75 \text{ PP - Orchard} \\
 \hline
 27 \quad 47
 \end{array}$$

$$\begin{array}{r}
 +44 \text{ F Cor} \\
 \hline
 32
 \end{array}$$

$$\begin{array}{r}
 \text{Fce} \\
 \hline
 33
 \end{array}$$

$$\begin{array}{r}
 \text{Fce} \\
 \hline
 34
 \end{array}$$

83

$$\begin{array}{r}
 +51 \text{ End GR - Rd Sn} \\
 \hline
 12 \quad 17
 \end{array}$$

$$\begin{array}{r}
 +37 \text{ PP} \\
 \hline
 26
 \end{array}$$

82



24'
2 S.F.
H₀
46'

Yard

H₀₄
B₀₂
A₀₄
26'

Cult

H₀₄
28'

2 S.F.
H₀
28'

Orchard

Row Apples

$$\frac{Rd}{13-9}$$

$$\frac{+99 PP}{27}$$

$$+17 Ent$$

$$\frac{+03 F Cor}{29}$$

$$\frac{Rd}{11-9}$$

95

$$\frac{+42 PP}{27}$$

$$\frac{+38 Bill Sn}{37}$$

94

$$\frac{Fz}{28}$$

93

$$\frac{Fz}{27}$$

$$\frac{Rd}{11-11}$$

$$\frac{+88 TP}{27}$$

$$\frac{+33 F Cor}{26}$$

92

$$\frac{+84-12 \times 50 CM}{24-26}$$

$$\frac{+35 PP}{27}$$

91

$$\frac{Rd}{11-11}$$

$$\frac{+05 Pat Ho}{60}$$

90

$$+15 Clump Will + Pat Ho$$

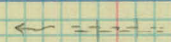
$$\frac{+28 Pat Ho la}{65}$$

$$\frac{+79 PP}{27}$$

89



Pasture



Hay

Hay Field

Cult



Willows

$$\frac{Rd}{13-10}$$

102

$$\frac{09 PP}{27}$$

$$\frac{+18 K45n}{29}$$

101

$$\frac{Rd}{13-10}$$

100

$$\frac{Rd}{14-9}$$

$$\frac{+60 PP}{27}$$

99

$$\frac{+67-15' \times 44' CM}{22-20}$$

$$\frac{Rd}{14-9}$$

$$\frac{+08 PP}{27}$$

98

$$\frac{Rd}{14-9}$$

$$\frac{+78 FCv}{48}$$

$$\frac{+09 PP}{45}$$

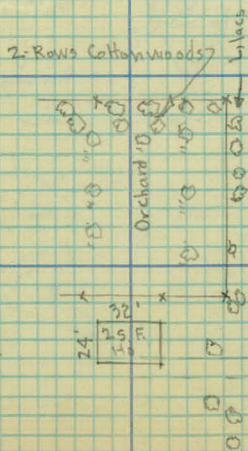
$$\frac{+53 PP}{26}$$

97

$$\frac{Rd}{14-9}$$

$$\begin{array}{r} +53-10' Tr \\ +44 Ent-12' \times 16' CM \\ +29-15' Tr \\ +13-10' Tr \\ +03-8' Tr \\ \hline 28 \\ 96 \\ 45 \\ 44 \end{array} \quad \begin{array}{r} +34 FCv \\ +81 Tw.Tv \\ +46 Cor Ho \\ \hline 47 \\ 43 \\ 85 \end{array}$$

96



109

$$\begin{array}{r} +83 \text{ Rd Sn} \\ \hline 16 \\ +81 \text{ PP} \\ \hline 14 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ \hline 8-13 \end{array}$$

$$\begin{array}{r} +79 \text{ Cor Ho} \\ \hline 70 \\ +40 \text{ End + Orch} \\ \hline 32 \\ +34 \text{ Rd Sn} \\ \hline 19 \\ +27 \text{ PP} \\ \hline 22 \\ \text{Fc} \\ \hline 32 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ \hline 10-13 \end{array}$$

$$\begin{array}{r} +89 \text{ Orch} \\ \hline 27 \\ \text{Fce} \\ \hline 31 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ \hline 11-12 \end{array}$$

$$\begin{array}{r} +73 \text{ Beg Orch} \\ \hline 28 \\ +17 \text{ Sn} \\ \hline 33 \end{array}$$

$$\begin{array}{r} +93 \text{ PP} \\ \hline 21 \\ +10 \text{ Rd} \\ \hline 12-12 \end{array}$$

$$\begin{array}{r} +65 \text{ Rd Sn} \\ \hline 23 \end{array}$$

106

$$\begin{array}{r} +84 \text{ PP} \\ \hline 36 \\ +80 \text{ Rd Sn} \\ \hline 35 \end{array}$$

$$\begin{array}{r} +94 \text{ Rd Sn} \\ \hline 34 \\ +83 \text{ Fce} \\ \hline 24 \end{array}$$

$$\begin{array}{r} +73 \text{ Shoulder} \\ \hline 50-50 \end{array}$$

$$\begin{array}{r} +17 \text{ End Corv} \\ \hline 21 \end{array}$$

$$\begin{array}{r} +78 \text{ Rd Sn} \\ \hline 25 \end{array}$$

$$\begin{array}{r} +13 \text{ PP, Rd Sn and Store Sn} \\ \hline 28 \end{array}$$

$$\begin{array}{r} +32 \text{ End Corv} \\ \hline 27 \end{array}$$

$$\begin{array}{r} +46 \text{ Shoulder} \\ \hline 50-66 \end{array}$$

$$\begin{array}{r} \text{Conc. Pier} \\ \hline 50 \end{array}$$

$$\begin{array}{r} +85 \text{ Corv. Store} \\ \hline 58 \end{array}$$

$$\begin{array}{r} +30 \text{ Rd} \\ \hline 12-12 \\ \text{Rd} \\ \hline 12-12 \end{array}$$

$$\begin{array}{r} +52 \text{ Cor Store} \\ \hline 83 \end{array}$$

104

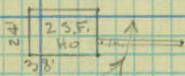
$$\begin{array}{r} +67 \text{ Ice Ho} \\ \hline 24 \end{array}$$

$$\begin{array}{r} +61 \text{ PP} \\ \hline 27 \end{array}$$

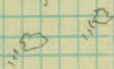
$$\begin{array}{r} +03 \text{ Rd Sn} \\ \hline 23 \end{array}$$

103

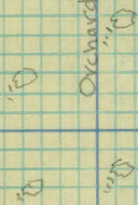
96



8 Stumps
in yard



Orchard

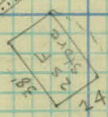


CO. RD "G"

15' x 50' CM



BLACK TOP



$$\frac{Fc}{37}$$

$$\frac{Fc}{32}$$

116

$$\frac{+74 PP}{13}$$

$$\frac{Fc}{40}$$

$$\frac{Fc}{32}$$

115

$$\frac{Fc}{32}$$

$$\frac{Rd}{8-13}$$

$$\frac{Fc}{33}$$

$$\begin{array}{r} +72 Tr \\ 29 \\ +11 Stp \\ 24 \\ +08-Tr \\ 30 \\ +03 Tr \\ 27 \\ \hline Fc \\ 35 \end{array} \quad \begin{array}{r} +18 PP \\ 13 \\ +66 Tr \\ 26 \\ +55 Stp \\ 28 \\ +47 Tr \\ 27 \\ \hline \end{array}$$

114

$$\frac{Fc}{35}$$

$$\frac{Rd}{8-13}$$

$$\frac{Fc}{33}$$

$$\begin{array}{r} +89-15 Tr \\ 28 \\ +21 PP \\ 14 \\ \hline Fc \\ 37 \end{array}$$

113

$$\frac{+36 F.Cov}{43} - \frac{Stps(2)}{45}$$

$$\frac{+63 F.Cov}{33}$$

$$\frac{Rd}{9-13}$$

112

$$\frac{+47 PP}{14}$$

$$+85 Ent$$

$$+93-8 Tr$$

$$\frac{+78 F.Cov}{33}$$

$$+74-10 Tr$$

$$+40-10 Tr$$

$$+51-10 Tr$$

$$+29-12 Tr$$

111

$$\frac{Rd}{8-13}$$

$$+74-8 Tr$$

$$+51-5-8 E.C. Tr$$

$$+19 R.P.$$

$$+34 Ent$$

$$+88 10 Tr$$

$$+16-5-8 Ever G.Trs$$

$$\frac{+01 Ent-12 \times 32 CM}{20}$$

110

Cult

Pasture

2-SF
40

38

13

123

$$\frac{+57 PP}{13}$$

$$\frac{+98 F. Cor}{31}$$

$$\frac{Rd}{8-14}$$

122

$$\frac{+87 PP}{14}$$

121

$$\frac{Fc}{33}$$

$$\frac{Rd}{9-13}$$

$$\frac{Fc}{20}$$

$$\frac{+23-25 PP}{32}$$

$$\frac{+18 PP}{14}$$

$$\frac{+16 StP}{24}$$

120

$$\frac{Fc}{33}$$

$$\frac{Rd}{9-13}$$

$$\frac{Fc}{31}$$

119

$$\frac{Rd}{8-13}$$

$$+84 Fd. Ent$$

$$\frac{+76 F. Cor}{33}$$

$$\frac{46 PP}{13}$$

$$\frac{+76 F. Cor}{32}$$

$$\frac{+73-14 DOK}{76}$$

118

$$\frac{Fc}{35}$$

$$\frac{Fc}{32}$$

117

Hay Field

Pasture

$$\frac{Fc}{33}$$

$$\frac{Ra}{7-14}$$

130

$$\frac{+45 PP}{13}$$

$$\frac{Fc}{33}$$

$$\frac{Ra}{7-14}$$

$$\frac{Woods}{70}$$

129

$$\frac{+75 PP}{13}$$

128

$$\frac{Fc}{33}$$

$$\frac{Ra}{7-16}$$

127

$$\frac{+67 R15n}{26} \quad \frac{Woods}{60}$$

$$\frac{Ra}{7-15}$$

$$\frac{+75 Deg Wood}{100}$$

126

$$\frac{+95 PP}{13}$$

$$\frac{Fc}{33}$$

$$\frac{+25 TP}{13}$$

125

$$\frac{Fc}{33}$$

$$\frac{Ra}{8-14}$$

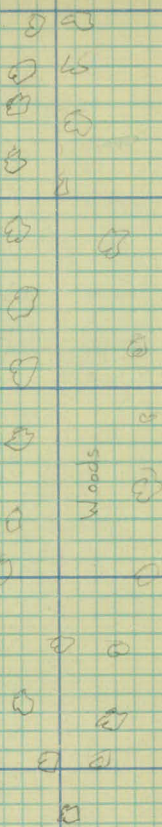
124

$$\frac{+13 Ent(Fd) 15 \times 20 CM}{22}$$

Honey Field

Waste Land

Woods



+85 End Woods

100

+73 F Cor
32

137

Rd
9-10

Fc
33

+23 Rd Sn
21

+54-15¹¹ x 36 G.M.
21-15

+17 TP
27

136

Woods

Fc

130

32

+42 TP
27

135

Woods
75

Rd
9-11

+17 TP
27

134

Woods
40

Fc
31

+17 Wood
25

Rd
9-13

Fc
31

133

+35 Rd
9-14

+20 TP
26
+17 Fc
30

100 Shoulder

50

132

+96 F Cor-Beg Woods

+92 Rd Sn
23

35

+79 Shoulder
50

+50 End Woods
10

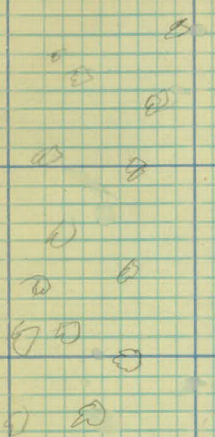
+71 TP
14

+79 End Culv
15

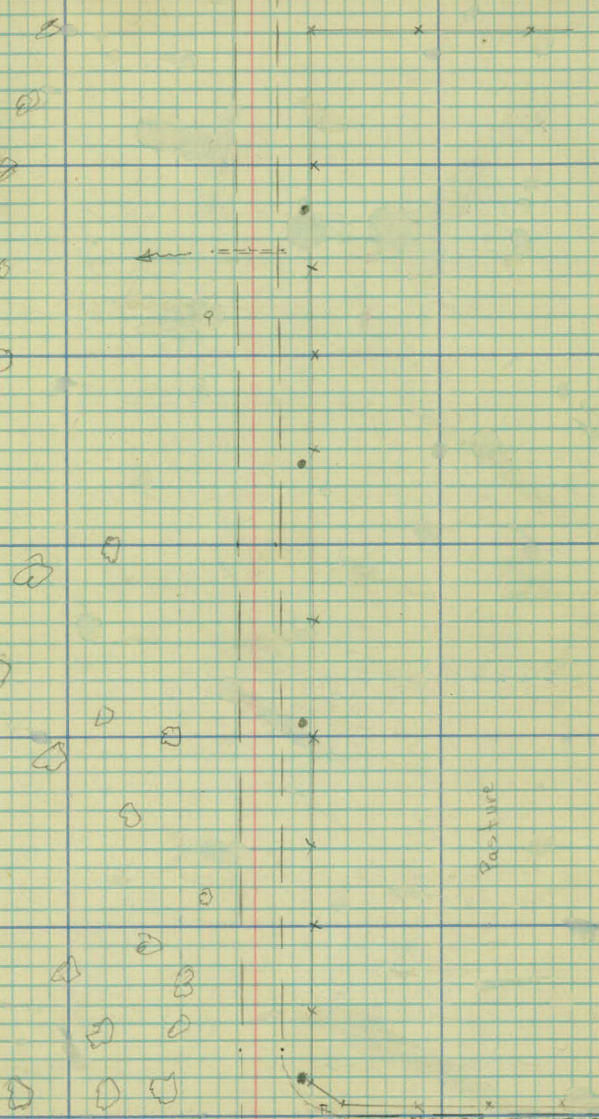
+45 Rd
7-16

+69 End Culv
31

131

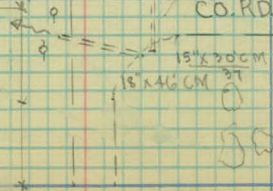


Woods



Pasture

CO. RD G² BL. TOP



$$\begin{array}{r} Rd \\ 11-11 \end{array}$$

$$\begin{array}{r} Fc \\ 33 \end{array}$$

$$\begin{array}{r} +22 \text{ Beg Rwy } 8'' \text{ Pop} \\ 29 \\ +14 \text{ F Cor} \\ 34 \\ \hline 35 \end{array}$$

$$\begin{array}{r} +50 \text{ TP} \\ 27 \end{array}$$

144

$$\begin{array}{r} +71 \text{ End Fce} \\ 34 \\ +24 \text{ TP} \\ 28 \\ \hline 35 \end{array}$$

$$\begin{array}{r} +98 \text{ Cor H/D} \\ 264 \\ +88 \text{ Ent} \\ \hline 35 \end{array}$$

$$\begin{array}{r} +74 \text{ 10' Tr} \\ 40 \\ \hline Fc \\ 35 \end{array}$$

143

$$\begin{array}{r} Rd \\ 10-11 \end{array}$$

$$\begin{array}{r} Fc \\ 35 \end{array}$$

142

$$\begin{array}{r} +98 \text{ TP} \\ 27 \end{array}$$

141

$$\begin{array}{r} Fce \\ 33 \end{array}$$

$$\begin{array}{r} +68 \text{ TP} \\ 27 \end{array}$$

140

$$\begin{array}{r} Rd \\ 10-11 \end{array}$$

$$\begin{array}{r} +92 \text{ Beg Fce} \\ 33 \\ +40 \text{ TP} \\ 27 \end{array}$$

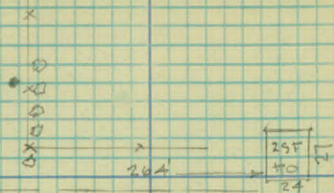
139

+78 Fd Ent

$$\begin{array}{r} +106 \text{ TP} \\ 27 \end{array}$$

138

$$\begin{array}{r} Rd \\ 9-11 \end{array}$$



Waste band

2014

Rd
11-10

151

$$\begin{array}{r} +03 \quad PP \\ \hline 36 \end{array} \quad \begin{array}{r} +07 TP \\ 28 \end{array}$$

$$\frac{+56-10" Tr}{36}$$

150

$$\begin{array}{r} +79 TP-PP \\ \hline 28-36 \end{array}$$

149

Rd
11-9

$$\frac{+81-12 \times 54 V+P}{36-18}$$

$$\begin{array}{r} +41 TP-PP \\ \hline 28 \quad 36 \end{array}$$

148

147

$$\begin{array}{r} Rd \\ 11-9 \end{array} \quad \begin{array}{r} +19 PP \\ 36 \end{array} \quad \begin{array}{r} +21 TP \\ 28 \end{array}$$

$$\frac{+95-12" Tr}{32}$$

146

$$\begin{array}{r} +14 PP \\ 37 \end{array} \quad \begin{array}{r} +14 TP \\ 27 \end{array} \\ +03 \text{ End Row } 30p \\ \hline 36 \\ +00 FCov \\ \hline 33$$

145

$$\frac{+36-10" Tr}{70}$$

Waste Land
+ 5m Brush

Hay

RA
10-12

+ 15: End Brush
33

+ 61 TP
26

+ 21 End Hedge
30

+ 14-3-12" Tr
55

+ 00 20" Tr
56

+ 65-15" Tr. Cor Ho

49-93 + 50 Beg Hedge
31

+ 35 TP
28

+ 45 Ent

+ 23 PP
35

+ 80-2-12" Tr
54

+ 21 F Cor
33

Rd
11-11

+ 66-6" Tr
31

+ 09. TP-PP
28-37

Fc
32

+ 56-8" Tr
32

+ 82 TP-PP
29-37

Rd
11-10

Fc
35

+ 57 PP
37

+ 58 TP
29

Fc

33-96

+ 57 F Cor Beg Woods
23

+ 29 TP-PP

28-56

Hand

Hand

15.5
26

Waste land = 5m Bush

Woods

$$\frac{Rd}{10-10}$$

165

$$\frac{+05 TP - End Fee}{28 \quad 32}$$

164

$$\frac{Rd}{9-11}$$

$$\frac{Fc}{33}$$

163

$$\frac{Rd}{9-11}$$

$$\frac{+35 TP}{28}$$

$$\frac{Fc}{33}$$

162

$$\frac{+39 TP - F.Cov}{28 \quad 32}$$

161

$$\frac{Rd}{9-11}$$

$$\frac{+14 TP}{27}$$

160

$$\frac{+00 Rd Ent - 12x16 cov}{24}$$

159

$$\frac{Rd}{11-12}$$

$$\frac{+88 TP}{26}$$

Cult

Hay Field

12-19

172

$$\begin{array}{r} +48 TP \\ \hline 28 \end{array}$$

+34 Ent

$$\begin{array}{r} +50 Ent \quad +70 Woods \\ +40 Gyr Po \quad 132 \\ \hline +31 End Woods \\ \hline +15 TP \\ \hline 26 \\ \hline Wood \\ \hline 38 \end{array}$$

171

$$\begin{array}{r} +50 Woods \\ \hline 38 \end{array}$$

170

$$\begin{array}{r} Rd \\ 10-10 \end{array}$$

$$\begin{array}{r} +14 TP \\ \hline 25 \\ +44 Beg Woods \\ \hline +42 End Ev Gr Wind break \\ \hline 32-50 \end{array}$$

169

$$\begin{array}{r} EG Trs \\ \hline 33-53 \end{array}$$

168

$$\begin{array}{r} Rd \\ 10-10 \end{array}$$

$$\begin{array}{r} +65 TP \\ \hline 25 \end{array}$$

$$\begin{array}{r} +53 Beg Ev Gr Trs \\ \hline 31-50 \\ +39 Ent to Ho 30x30 \\ \hline 400 \pm \end{array}$$

167

$$\begin{array}{r} +29 TP \\ \hline 28 \end{array}$$

$$\begin{array}{r} +28 Row 4" Ev Grs \\ \hline 34 \\ +20 Row 4" Ev Grs \\ \hline 30 \end{array}$$

166

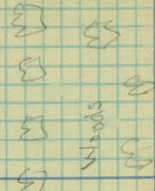
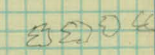
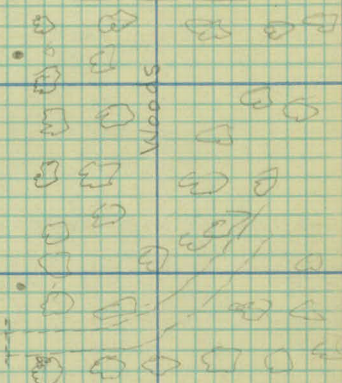
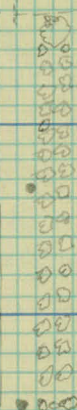
Cult

Hay Field

Waste land

Woods

Woods



$$\begin{array}{r} +0.4TP \\ \hline 29 \end{array}$$

$$\begin{array}{r} \underline{21} \\ 10-9 \end{array}$$

179

178

$$\begin{array}{r} +6.7TP \\ \hline 29 \end{array}$$

$$\begin{array}{r} \underline{Rd} \\ 12-8 \end{array}$$

177

$$\begin{array}{r} +6.2 \text{ Ent} \\ +7.3 \text{ End Culw} \\ \hline 22 \\ +4.1 \text{ Ent } 12' \times 48' \text{ CM} \\ \hline 24 \\ +1.4 TP \\ \hline 29 \\ +3.0 \text{ End Woods} \\ \hline 132 \end{array}$$

176

$$\begin{array}{r} +0.8 TP \\ \hline 28 \end{array}$$

$$\begin{array}{r} \underline{Rd} \\ 12-9 \end{array}$$

175

174

$$\begin{array}{r} \underline{Rd} \\ 12-8 \end{array}$$

$$\begin{array}{r} +7.9 TP \\ \hline 28 \\ +5.5 \text{ Ent } 15' \times 20' \text{ CM} \\ \hline 21 \end{array}$$

173

142

A collection of hand-drawn sketches of various geometric shapes, including circles, squares, and irregular polygons, arranged in a grid-like pattern. The sketches are drawn on a blue-lined background.

186

$$\begin{array}{r}
 +41 \text{ Guy P} \\
 \underline{20} \\
 +14 \text{ Billboard} \\
 \underline{29}
 \end{array}$$

$$\begin{array}{r}
 +26 \text{ Fee Lov} \\
 \underline{20} \\
 +24 \text{ Row P} \quad +40 \text{ PP} \\
 \underline{32} \quad \underline{29} \\
 +13 \text{ Ent-12"x24" V.P.} \\
 \underline{29} \\
 +04 \text{ Row P} \\
 \underline{22}
 \end{array}$$

185

$$\begin{array}{r}
 \text{Rd} \\
 \underline{11-10}
 \end{array}$$

$$\begin{array}{r}
 +50 \text{ TP} \\
 \underline{28}
 \end{array}$$

$$\begin{array}{r}
 +60 \text{ Fee} \\
 \underline{22} \\
 +47 \text{ Ent Fd}
 \end{array}
 \quad
 \begin{array}{r}
 +61-12"x52" V+P \\
 \underline{28-24}
 \end{array}$$

184

$$\begin{array}{r}
 +22 \text{ TP} \\
 \underline{28}
 \end{array}$$

183

$$\begin{array}{r}
 \text{Rd} \\
 \underline{11-10}
 \end{array}$$

$$\begin{array}{r}
 +92 \text{ TP} \\
 \underline{28}
 \end{array}$$

$$\begin{array}{r}
 +31-1' \text{ Dt} \\
 \underline{29} \\
 +21 \text{ Ent}
 \end{array}
 \quad
 \begin{array}{r}
 +82-12"x46" V+P \\
 \underline{22-24}
 \end{array}$$

182

$$\begin{array}{r}
 +08-1' \text{ Ditch} \\
 \underline{29}
 \end{array}$$

$$\begin{array}{r}
 +60 \text{ TP} \\
 \underline{29}
 \end{array}$$

181

$$\begin{array}{r}
 \text{Rd} \\
 \underline{16-10}
 \end{array}$$

$$\begin{array}{r}
 +32 \text{ TP} \\
 \underline{29}
 \end{array}$$

$$\begin{array}{r}
 +29 \text{ Ent (Fd)} \\
 +15-1' \text{ Ditch} \\
 \underline{150}
 \end{array}$$

180

Schmidt's

1/2
3/4

Cult

Cult

Hay Field

Pot Hole

1 Pot Pitoh

Cult.

$$\frac{Rd}{10-10}$$

$$\frac{Nursery}{47}$$

193

$$\frac{Fc}{56}$$

$$\frac{+10 PP}{29}$$

$$\frac{Nursery}{43}$$

$$+92 Ent$$

192

$$\frac{Fc}{53}$$

$$\frac{Rd}{10-10}$$

$$\frac{Nursery}{35}$$

$$\frac{+20 Cor Nursery}{42}$$

$$\frac{+79 PP}{29}$$

$$\frac{+28 F Cor}{53}$$

$$+107 Ent$$

191

$$\frac{+98 PP}{29}$$

190

$$\frac{+49 End Ev Grs}{37}$$

$$\frac{+17 PP}{29}$$

189

$$\frac{Rd}{11-10}$$

$$\frac{Ev Grs}{37}$$

$$+48 Ent (Fd)$$

$$\frac{+13 Beg Row Ex Grs}{36}$$

$$\frac{+10 Bullbo}{33}$$

188

$$\frac{+86 Guy Po}{21}$$

$$\frac{+98 Ent - 12' x 20 CM}{20}$$

$$\frac{+29 Fc}{32}$$

$$\frac{+87 PP}{28}$$

$$\frac{+78 Fc}{18}$$

187

$$\frac{Rd}{11-10}$$

$$\frac{Fc}{18}$$

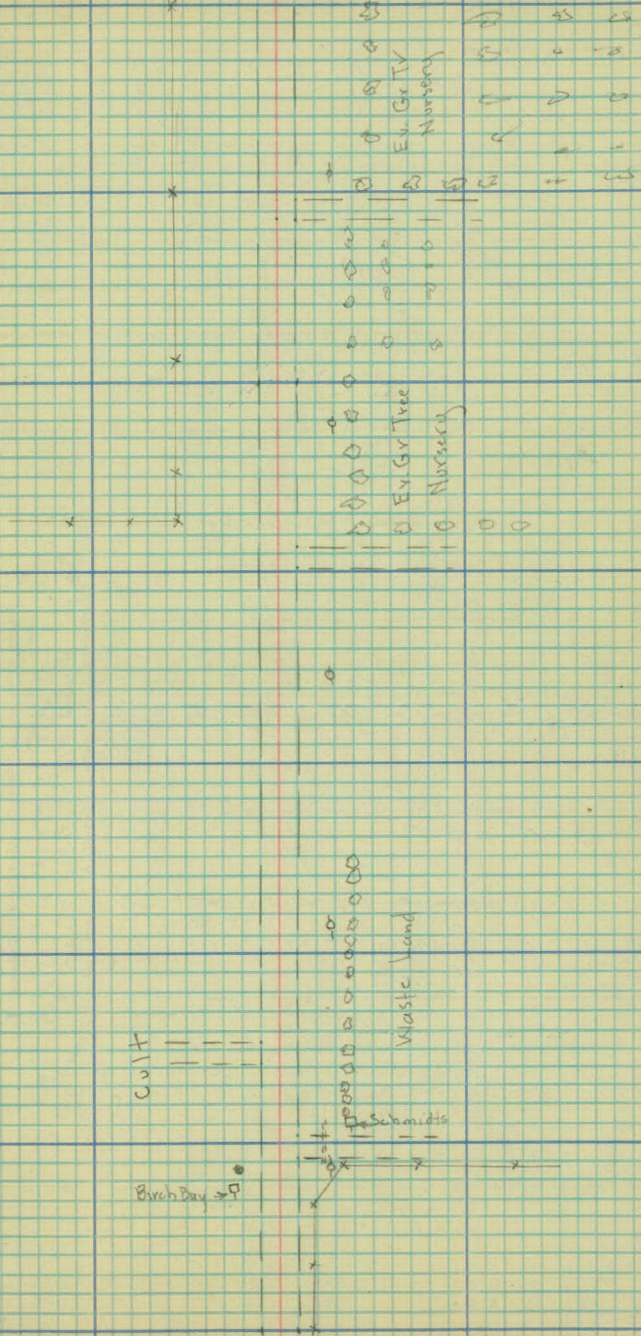
Cult

Birch Bay

Waste Land
Schmidt's

Ev. Gr Tree
Nursery

Ev. Gr TV
Nursery



$$\frac{Fc}{19}$$

$$\frac{Pd}{10-10}$$

$$\frac{+92 \text{ Road-12"x20' CM}}{26}$$

$$\frac{+23 PP}{29}$$

$$\frac{+04 \cdot 10'' Tr}{65}$$

200

$$\frac{Fc}{20}$$

$$\frac{Pd}{20-10}$$

+50 End Wood-Bey Brush

$$\frac{+43 \text{ End Grove}}{35-55}$$

199

$$\frac{Fc}{27}$$

$$\frac{+83 PP}{28}$$

$$\frac{Pd}{10-10} \frac{+65 \text{ Bay Grove Sm Trs}}{39-59}$$

198

$$\frac{Fc}{32}$$

$$\frac{+92 \text{ Row Oaks}}{64}$$

$$\frac{+85 \text{ Ent-10'x16' CM}}{21}$$

$$\frac{+79 \text{ Row Oak Trs}}{40}$$

$$\frac{+62 \text{ Ent-10'x16' CM}}{22}$$

$$\frac{+46 TP}{28}$$

$$\frac{+80-12'' Tr}{34}$$

$$\frac{+35 Stp}{31}$$

$$\frac{+43-36'' Tr}{36}$$

$$\frac{+22-10'' Tr}{34}$$

$$\frac{+18-24'' Tr}{37}$$

197

$$\frac{Fc}{37}$$

$$\frac{+91-20'' Tr}{37}$$

$$\frac{+05 Fcov}{42}$$

$$\frac{+02 \text{ End Row Trs}}{43}$$

$$\frac{+66-30'' Tr}{36}$$

$$\frac{+15-30'' Tr}{37}$$

196

$$\frac{Pd}{10-10}$$

$$\frac{+93 PP}{23}$$

$$\frac{+64 Stp}{37}$$

$$\frac{+20 \text{ Cor Ho}}{31}$$

$$\frac{+38 Stp}{37}$$

195

$$\frac{+58 \text{ Row B.E.}}{29}$$

$$\frac{+93 PP}{27}$$

$$\frac{+87 Stp}{36}$$

$$\frac{+56 \text{ Ent}}{36}$$

$$\frac{+52 Fcov}{56}$$

$$\frac{+90 \text{ Cor 3'' Trs}}{38}$$

$$\frac{+74 \text{ Ent}}{38}$$

$$\frac{+42 PP}{28}$$

$$\frac{- \text{End Nursery}}{50}$$

194

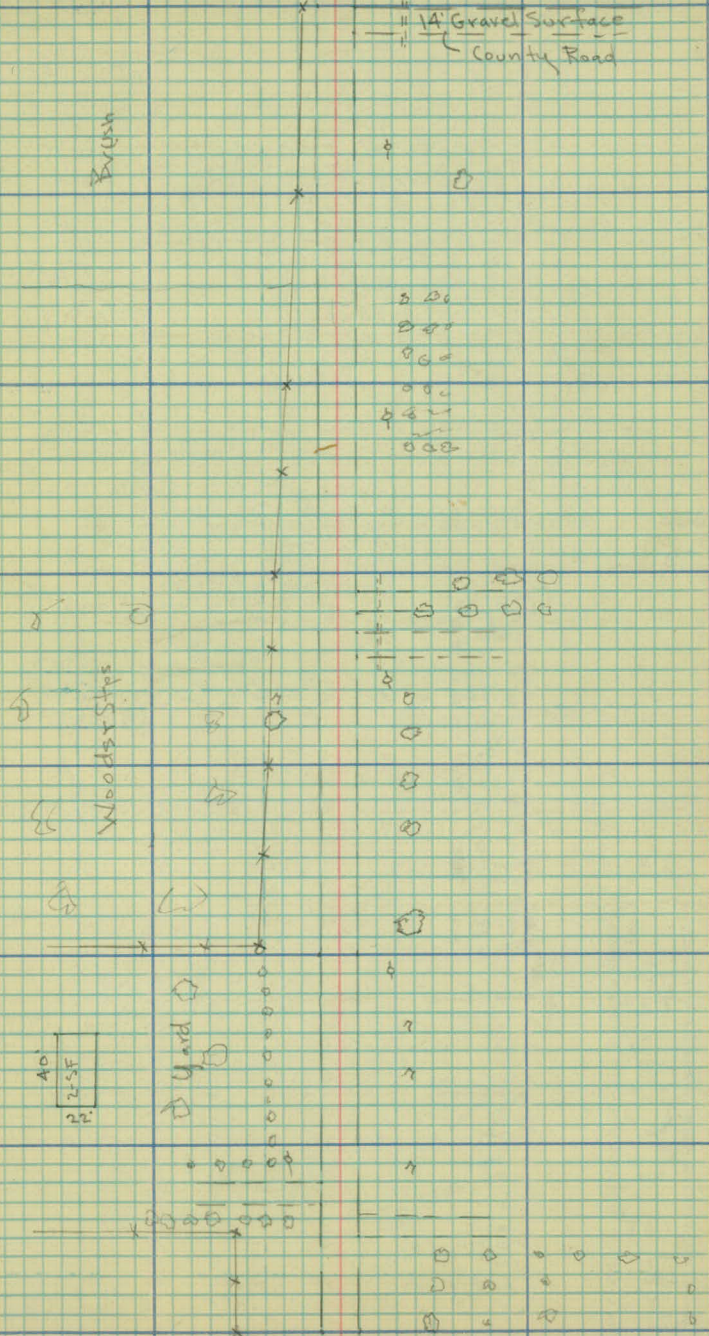
14' Gravel Surface
County Road

Brush

Woods & Steps

40' x 22.5' x 12'

Yard



$$\frac{Fc}{21}$$

$$\frac{Rd}{9-12}$$

207

$$\frac{Fc}{21}$$

$$\begin{array}{r} +16 PP \\ \hline 34 \\ +100 Rd Sn. \\ \hline 21 \end{array}$$

$$\frac{Ditch}{30}$$

206

$$\frac{Fc}{20}$$

$$\frac{Rd}{9-12}$$

205

$$\begin{array}{r} +78 PP \\ \hline 33 \end{array}$$

204

$$\frac{Fc}{20}$$

$$\frac{Rd}{8-12}$$

$$\begin{array}{r} +38 PP \\ \hline 32 \end{array}$$

203

$$\frac{Fc}{20}$$

$$\frac{Rd}{9-11}$$

$$\frac{PP}{30}$$

$$\begin{array}{r} +25 - Fd. Ent. 24" \times 20" CM \\ \hline 26 \end{array}$$

202

$$\frac{Fc}{19}$$

$$\frac{Ditch}{26}$$

$$+62 PP$$

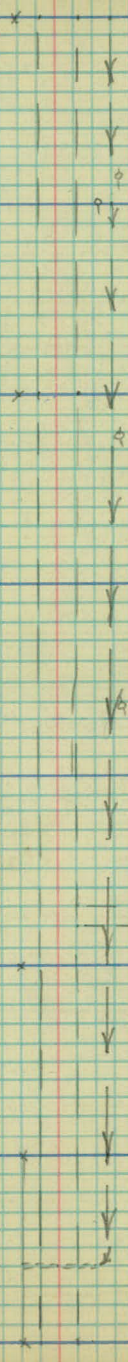
$$\begin{array}{r} +40 - 20" \times 42" V.P. \\ \hline 22 - 20 \end{array}$$

201

← 480 ft. Ditch →

Brush & Waste Land

Hay Field



211

$$\begin{array}{r} +29 \text{ Rd Sn} \\ +27 \text{ PP } 14 \\ \hline 14 \\ +14 \text{ Rd Sn} \\ \hline 12 \end{array}$$

$$\begin{array}{r} +25 \text{ PP} \\ 27 \\ +18 \text{ Beg Fec} \\ 33 \\ +45 \text{ Conduit} +12 \text{ End Culv} \\ 35 \\ +30 \text{ Rd} +16 \text{ Shoulder} \\ 7 -16 \quad 45 \end{array}$$

$$\begin{array}{r} +85 \text{ FCor} \\ 34 \end{array}$$

$$+95 \text{ Ent}$$

$$\begin{array}{r} +77 \text{ Guy Rd} \\ 26 \end{array}$$

$$\begin{array}{r} +86 \text{ Shoulder} \\ 50 - 140 - 292 \\ +18 \text{ Rd Sn} - \text{IP} \\ 42 \quad 48 \\ +70 \text{ Beg Culv} - 24' \times 42' \\ 34 \\ +50 \text{ Rd} \\ 16 - 115 - 161 \\ +64 \text{ PP} \\ 37 \\ \text{Rd} \\ 17 \end{array}$$

210

$$\begin{array}{r} +77 \text{ FCor} \\ 21 \\ +72 \text{ Rd} \\ 16 - 40 - 68 \\ +87 \text{ End Culv} \\ 33 \\ +89 \text{ PP} \\ 35 \\ \text{Ditch} \\ 86 \end{array}$$

209

$$\begin{array}{r} \text{Fc} \\ 21 \\ \text{Rd} \\ 8 - 38 \\ \text{Ditch} \\ 43 \end{array}$$

208

$$\begin{array}{r} +77 \text{ Beg Culv} - \text{E. Rd} \\ 32 \quad 19 \\ +56 \text{ PP} \\ 55 \end{array}$$

60" Water Dept Conduit →

Hay

DEG 011 SURF

Brush

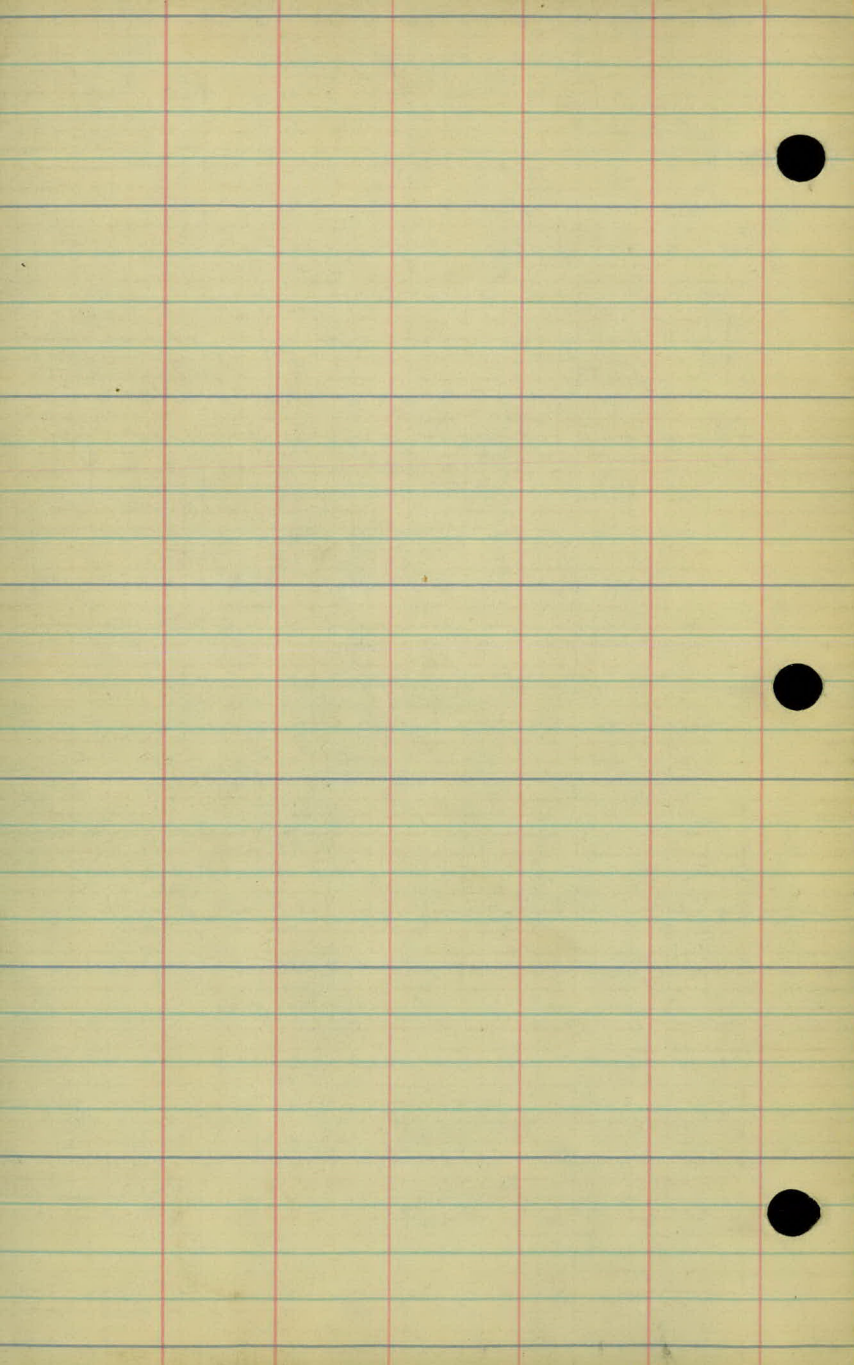
3 Bot Ditch
CO. RD. 1 BL TOP

22' BL TOP

3' Bot Ditch

24' x 110' CM.

Hay



-1-

Oct. - 4 - 35

Benah Levels

lex. Ave.

From Co. Rd. E. To I

B.M.	+	H.I.	—	E.I.V.	-1-
	11.80	976.59		964.79	
B.M.			10.53	966.06	✓
T.P.	12.71	988.95	0.35	976.24	
○	13.25	1001.73	0.47	988.48	
○	8.44	1010.00	0.17	1001.56	
B.M.			7.06	1003.94	X 1002.94
				1001.94	
○	1.67	1011.05	0.62	1009.38	
○	1.33	1000.24	12.14	998.91	
○	0.47	988.23	12.48	987.76	
○	0.27	976.34	12.16	976.07	
B.M.			9.62	966.72	
○	2.19	966.21	12.32	964.02	
○	5.27	968.16	3.32	962.89	
○	4.55	966.70	6.01	962.15	

R.R. Spike in T.P. Sta. 52+55 - 25' RT.

Top of Mont. Co. Rd. F & ley. Ave.

R.R. Spike in 12" B.E. Sta. 64+70 - 30' RT.

R.R. Spike in 20" W.O. 150' S.W. ley. & F. 2

	+	H.I.	-	Elv.	
		966.70 ✓			
○	2.95	958.79 ✓	10.86	955.84 ✓	
B.M.			6.57	952.22 ✓	
○	4.20	956.55 ✓	6.44	952.35 ✓	
B.M.			0.38	956.17 ✓	
B.M.			4.20	952.35 ✓	
○	0.98	945.25 ✓	12.28	944.27 ✓	
○	0.08	933.50 ✓	11.83	933.42 ✓	
○	0.19	921.78 ✓	11.91	921.59 ✓	
○	0.20	909.50 ✓	12.48	909.30 ✓	
B.M.			11.99	897.51 ✓	
○	3.45	900.71 ✓	12.24	897.26 ✓	
○	5.22	899.97 898.61 898.07	6.86	893.85 ✓	
B.M.			4.85	894.22 893.82 893.22	= 893.80

R.R. Spike in 12" Cottonwood Sta. 97+83 - 100' L.T.

Top Concrete platform N.E. Cor. Sina's Tavern

Top Mont. 1/4. Ave. & Co. Rd. G.

R.R. Spike in 12" W.O. Sta. 118+75 - 60' R.T.

R.R. Spike in T.P. S.W. Cor 1/4. & G 2

	+	H.I. 899.70 99.10	-	Elv.	-5-
B.M.	5.88	899.70 99.10		893.82 893.22	894.22
B.M.			6.36	93.74 92.74	
0	10.81	08.53 908.13 07.53	2.38	97.72 897.32 96.72	
0	5.10	13.54 913.14 12.54	0.09	08.44 908.04 07.44	
B.M.			9.99	03.53 903.15 02.55	
0	12.10	20.72 920.32 19.72	4.92	08.62 908.22 07.62	
0	5.04	23.99 923.59 22.99	1.77	18.95 918.55 17.95	
B.M.			3.84	20.15 919.75 19.15	
B.M.			5.17	18.82 918.42 17.82	
0	2.91	18.74 918.34 17.74	8.16	15.83 915.43 14.83	
0	6.55	19.44 919.04 18.44	5.85	12.89 912.49 11.89	
B.M.			0.26	19.18 918.78 18.18	
0	0.23	07.30 906.90 06.30	12.37	07.07 906.67 06.07	
0	6.51	02.65 902.25 01.65	11.16	96.14 895.74 895.14	

R.R. Spike in T.P. S.W. Cor. 1st & G. 2

Top Mont. 1st Ave. & G. 2

R.R. Spike in 12" W.O. Sta. 145+35 - 60' LT.

R.R. Spike in 18" B.O. Sta. 159+15 - 60' RT.

Top Mont. Sta. 158+20⁵³ 1st & H.

R.R. Spike in 15" W.O. Sta. 173+45 - 125' RT.

	+	H. 1.65 02.25 01.65	-	Elv.	-7-
B.M.			6.55	96.10 895.70 95.10	
B.M.			6.42	96.23 895.83 95.23	
o	7.60	08.20 907.80 07.26	2.05	09.50 900.20 99.60	
o	1.42	99.19 898.79 98.19	10.43	97.77 897.37 96.77	
B.M.			4.80	94.39 893.99 93.39	
o	4.94	98.19 897.79 97.19	5.94	93.25 892.85 92.25	
B.M.			5.17	892.62 92.02	893.02 891.85

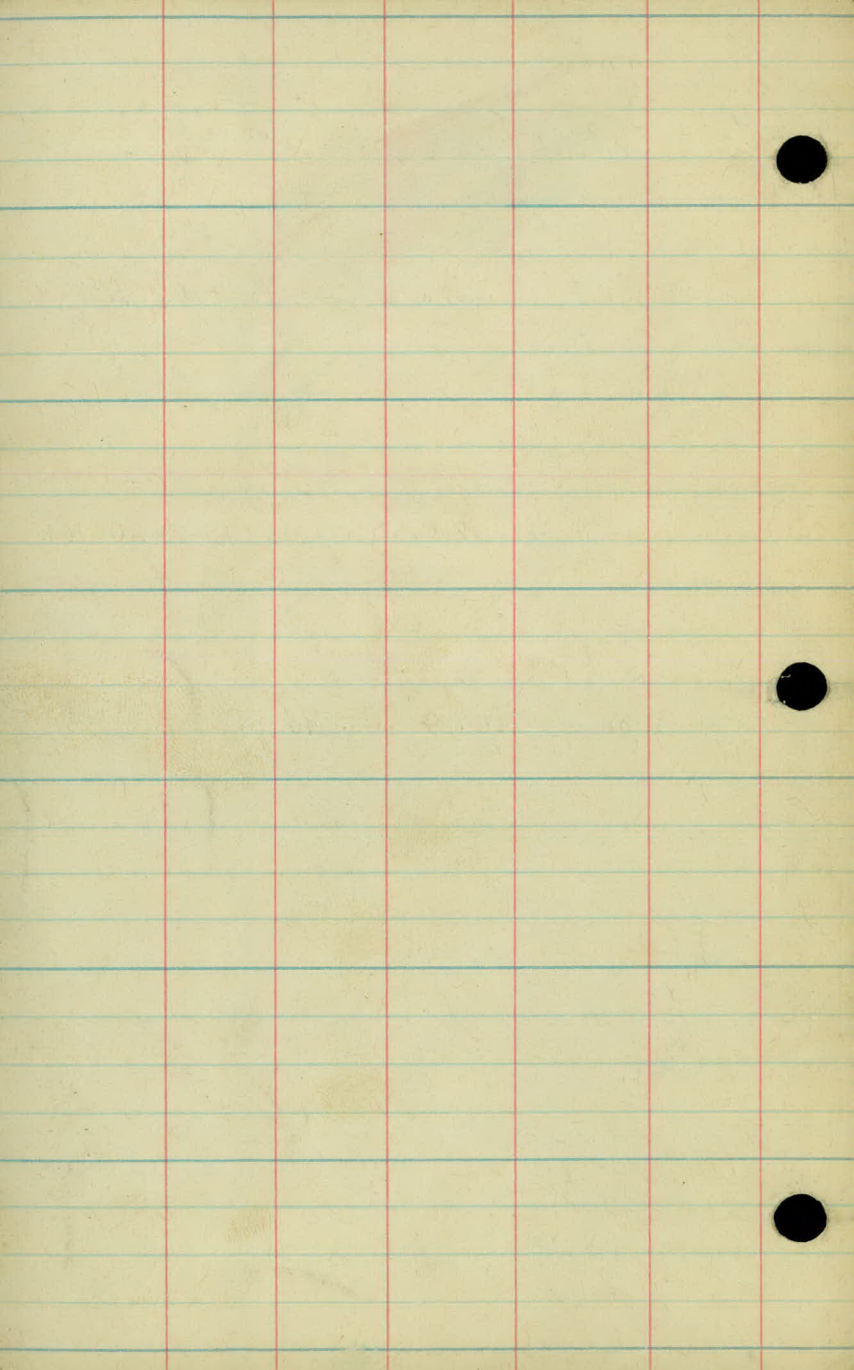
891.9 1

Top Mont. Sta. $184+60.63$ ley. & H₂

R.R. Spike in 18" Cottonwood Sta. $186+18-60$ RT

Bolt Spike in 24" W.O. Sta. $197+93-60$ RT.

Top Mont. ley. & Co. Rd. I



11/22/35

Levels Co Rd E

Sta

+

π

Levels to the East

BM

659

656.69

950.10

0+00

1

2

3

4

5

6

7

6.6

5.6

4.4

4.3

4.6

6.1

8.0

10.2

8

9

10

Levels to the West

B.M. 0.64

0+00

+13

+20

+50

1

11.1

9.5

7.5

0.64

0.70

1.1

2.2

3.0

1 + 25

+ 62

Beg Conc Pavement

2

3

4

5

6

7

8

9

10

3.1

2.79

3.6

5.8

7.7

8.7

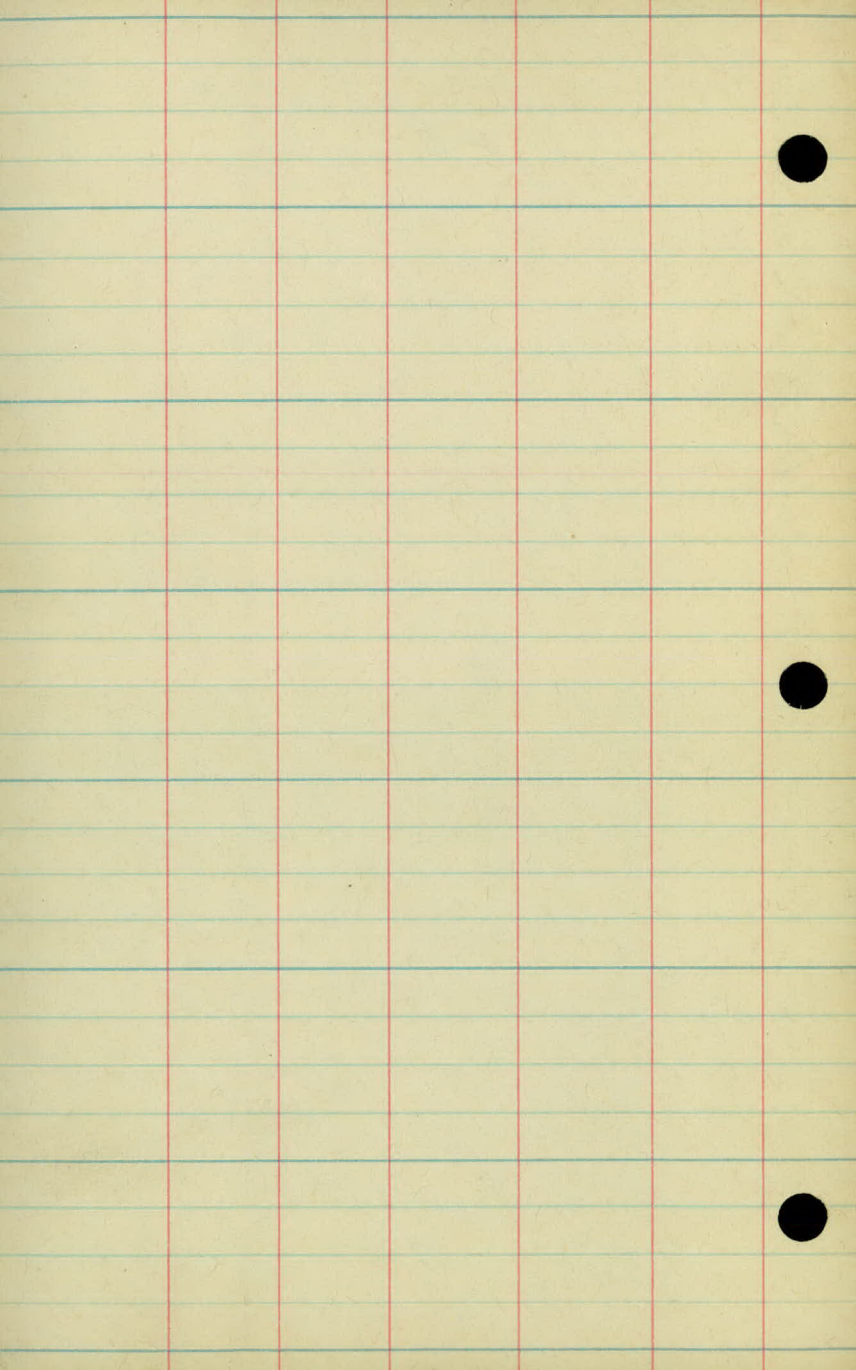
8.9

8.6

8.3

8.0

7.6



11/22/35

Levels on Soo Line RR
1000' E + W of Lexington Av.

Sta. + π - W.B. M E.B. M

Levels to the East

B. M. 1.48 949.68

948.20

0+00 44.26 44.39

0+25 End Spur 44.35 44.42

1 44.75 44.72

2 45.17 45.13

3 45.62 45.68

+48 H.B. Spur

4 46.09 46.17

5 46.62 46.76

Six Pier of oil Tanks

WB. EB.

5.42 5.29

533 5.26 ^{spur} 5.77

4.93 4.96 5.27

4.51 4.55 4.60

4.06 4.00

3.78

3.59 3.51 3.52

3.06 2.92

Sta

+

K

-

WB. NLEB. NL

949.68

6

47.18

47.40

7

47.61

47.87

8

48.25

48.48

9

48.23

10

48

WBM

EBM

2.50

2.28

2.07

1.81

1.43

1.20

1.43

0.90

0.66

Sta

+

$\times$

-

levels to the West

1

2

3

4

5

6

7

8

10

EBN

579

WBN

5.60

6.24

5.97

6.30

6.62

6.73

6.90

7.09

7.10

7.58

7.40

7.92

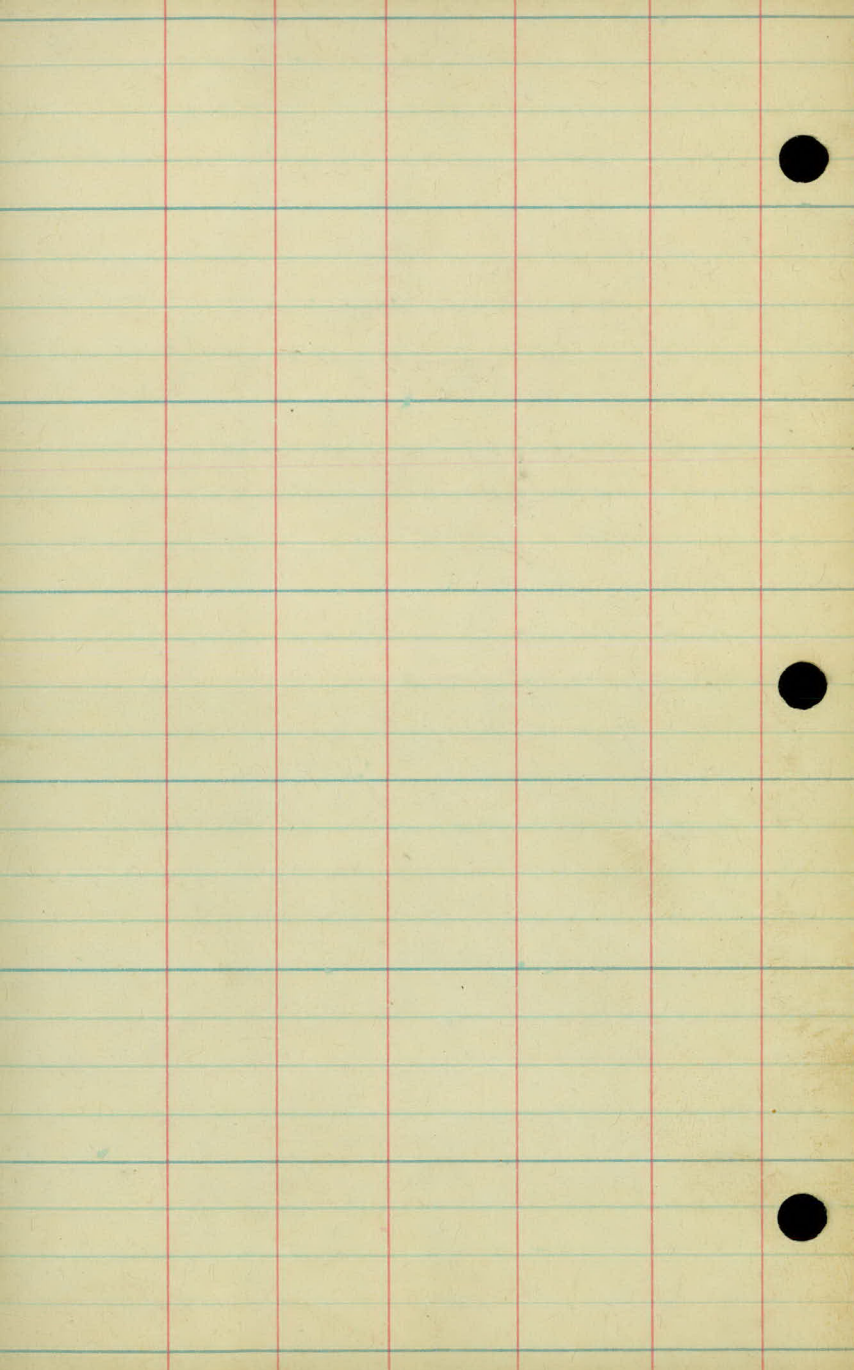
7.68

8.21

8.08

8.45

8.42



11/23/35

Levels Kowalska
Road
West of Sta. 26+46

Sta	+	π	-
B.M.	8.98	947.21	938.23
0+00			38.2
1			38.8
2			40.3
3			42.3
4			42.5
5			38.4
6			37.2
7			37.2
8			38.4
9			41.9
10			45.6

Top Mont $\frac{1}{2}$ M₁ No. Co. Rd. E

9.0

8.4

6.9

4.9

4.7

8.8

10.0

10.0

8.8

5.

5.3

1.6

Co Rd F - to the West

+ x -

BM. 5.74 969.53 963.79

0 + 00 65.0

1 63.2

2 61.2

3 59.4

4 57.8

5 56.6

6 57.7

7 59.8

8 62.0

9 64.1

10 66.2

To the East

1 66.7

2 68.0

SpK in P.P. SE Cor "G" & Hwy.

4.5

6.3

8.3

10.1

11.7

12.9

11.8

9.7

7.5

5.4

3.3

2.8

1.5

Sta

+

Co Rd F. East

 π

-

969.53

3

68.8

0

10.15

979.29

0.39

969.14

4

70.3

5

72.6

6

75.1

7

76.3

8

76.2

9

75.1

10

73.3

0.7

9.0

6.7

4.2

3.0

3.1

4.2

6.0

Victoria (F²) to East

B.M. 11.92 974.18 962.26

0+00

1

2

3

4

5

0

6

7

8

9

10

2.67

0.27

66.8

$$\begin{array}{r} 705 \\ 359 \\ \hline 346 \end{array}$$

$$\begin{array}{r} 965.72 \\ 3.46 \\ \hline 962.26 \end{array}$$

Top Iron Pin Intersection Lex + F2

11.9

14.9

14.3

10.0

4.9

1.3

1.5

2.4

6.8

13.2

16.2

Co Rd G - to The West

Sta	+	π	-
B.M.	4.69	956.04	951.35

0+00	51.3
------	------

1	48.9
---	------

2	47.3
---	------

3	46.3
---	------

4	45.4
---	------

5	45.0
---	------

6	45.3
---	------

7	46.6
---	------

8	49.0
---	------

9	51.5
---	------

10	54.1
----	------

Levels to the East

1	51.8
---	------

2	52.3
---	------

Top Mont G + Lex

4.7

7.1

8.7

9.7

10.6

11.0

10.7

9.4

7.0

4.5

1.9

4.2

3.7

3

956.04

5

52.4

4

52.0

5

52.0

6

49.8

7

46.0

8

42.2

9

38.2

10

34.2

Co. Rd. G² To East

Sta.

+

π

-

Elv.

B. M.

13.50

905.91

892.41

0+00

82.5

1

92.3

2

93.2

3

93.4

4

94.0

3.6

4.0

4.0

6.2

10.0

13.8

17.8

21.8

Top Mont. Co. Rd. G.² & Ley.

13.4

13.6

12.7

12.5

11.9

905.91

5

6

7

8

+

π

-

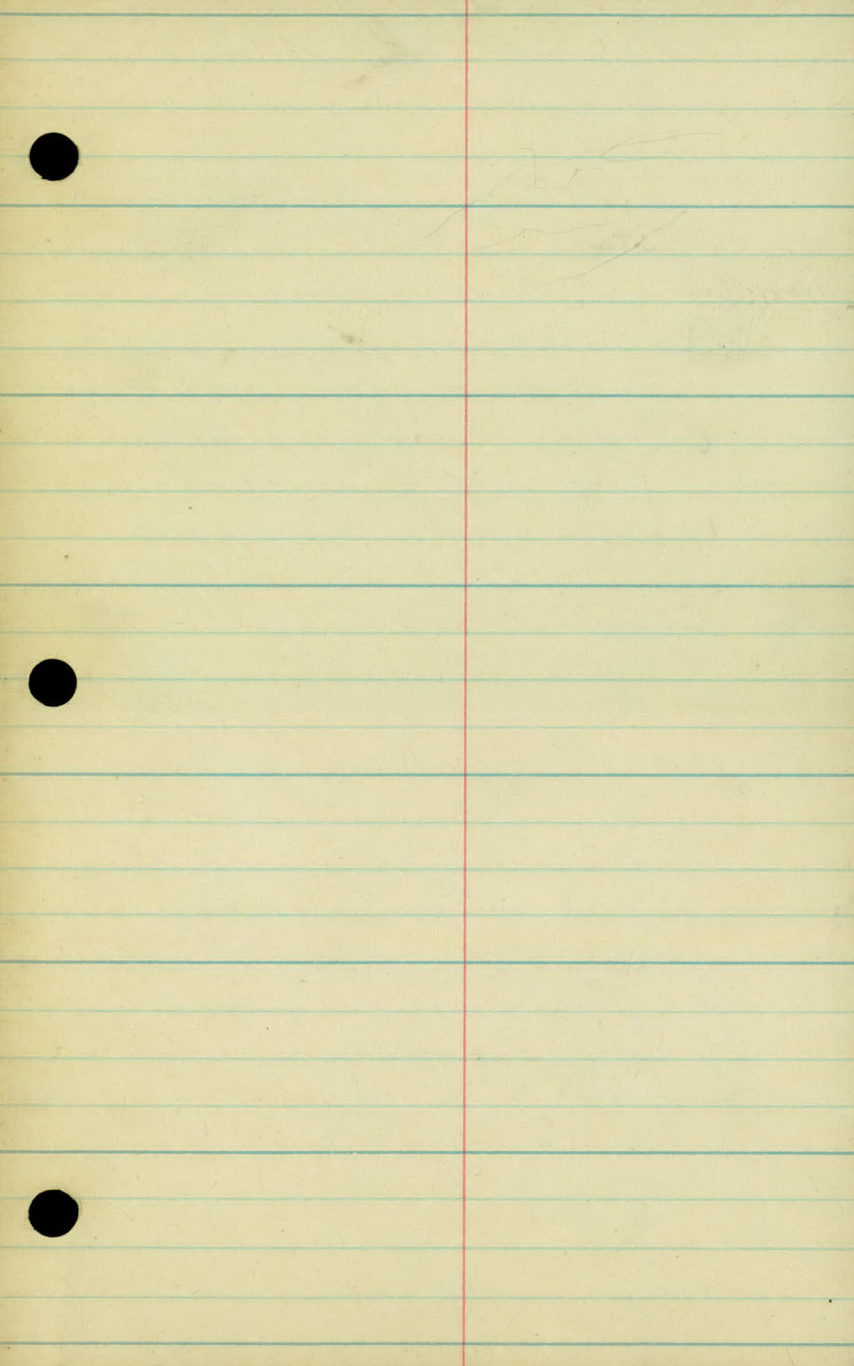
0

10.79

1.27

9

10



Levels on Lex. from Co. Rd. I. North

Sta.	+	π	-	Elv.
------	---	-------	---	------

B.M.	10.66			
------	-------	--	--	--

0+00				
------	--	--	--	--

1				
---	--	--	--	--

2				
---	--	--	--	--

3				
---	--	--	--	--

4				
---	--	--	--	--

5				
---	--	--	--	--

6				
---	--	--	--	--

7				
---	--	--	--	--

8				
---	--	--	--	--

9				
---	--	--	--	--

10				
----	--	--	--	--

Top Mont. Co. Rd E. & Lex. Ave.

10.4

9.6

10.0

9.4

7.9

6.7

4.9

3.0

1.8

1.5

1.8

Levels on Curve Running off Tex. into Co. Rd. I.

Sta.	+	π	-	Elev.
------	---	-------	---	-------

B.M	3.77			
-----	------	--	--	--

0+00				
------	--	--	--	--

1				
---	--	--	--	--

2				
---	--	--	--	--

3				
---	--	--	--	--

4				
---	--	--	--	--

5				
---	--	--	--	--

6				
---	--	--	--	--

7				
---	--	--	--	--

8				
---	--	--	--	--

9				
---	--	--	--	--

10				
----	--	--	--	--

Top Mont. Lex. Ave. & Co. Rd. I.

3.3

4.5

4.6

5.0

5.4

5.2

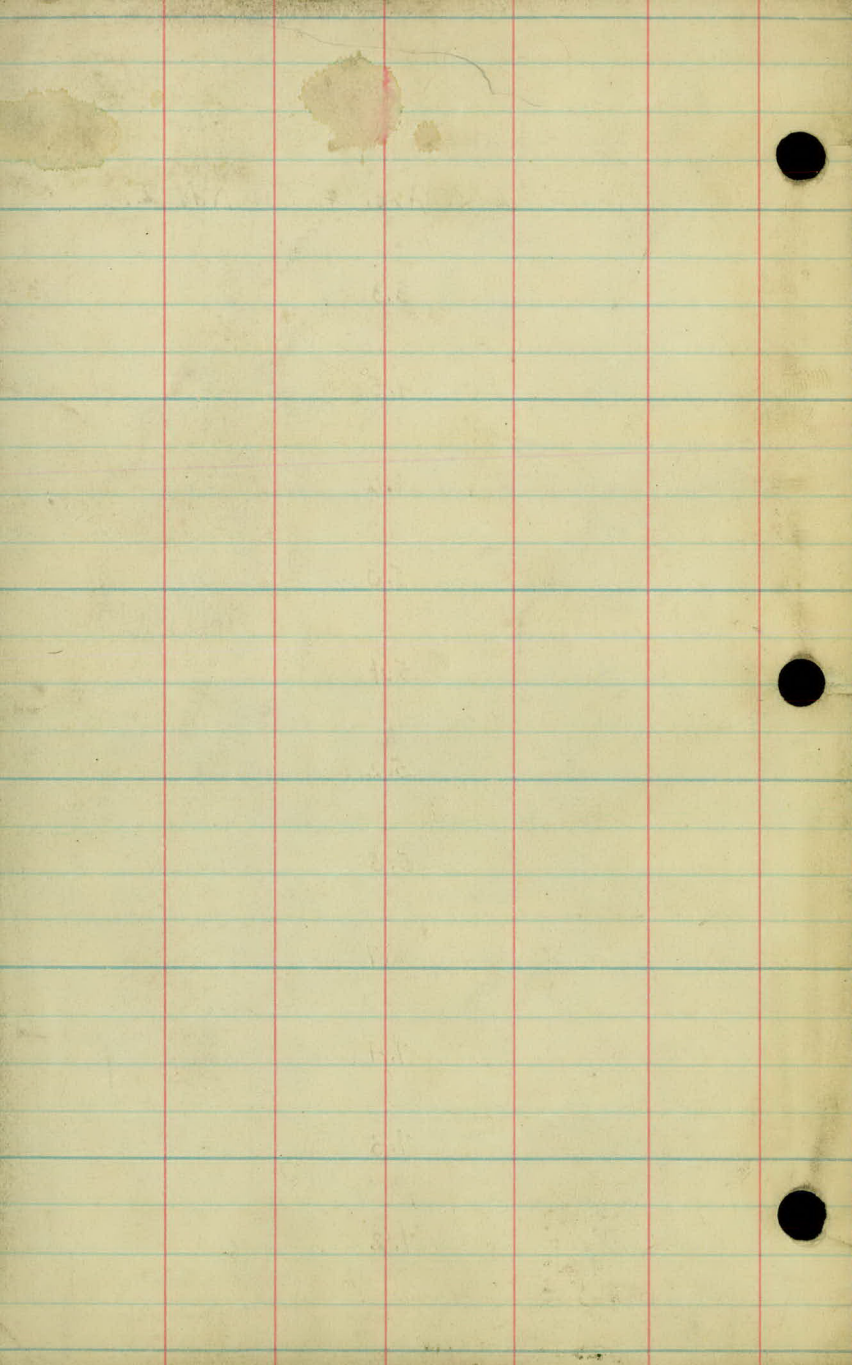
5.5

6.7

7.4

7.3

7.2



Check Levels

Lexington Avenue

Co Rd. E to Co Rd I

	+	+	-	Elev	
B.M.	2.46	948.77			946.31
⊙	0.58	936.83 ✓	12.52	936.25 ✓	
⊙	4.66	936.86 ✓	4.63	932.20 ✓	
	5.09	937.35 ✓	4.60	932.26 ✓	
B.M.	5.53	942.71 ✓	0.14	937.21 ✓	937.18 ✓
⊙	5.40	945.83 ✓	2.28	940.43 ✓	
B.M.			7.12	938.71	938.70
⊙	8.73	951.50 ✓	3.06	942.77 ✓	
⊙	12.94	962.67 ✓	1.77	949.73 ✓	
⊙	11.53	973.70 ✓	0.50	962.17 ✓	
B.M.			9.95	963.75	963.74
⊙	13.35	986.61 ✓	0.44	973.26 ✓	
⊙	12.17	998.43 ✓	0.35	986.26 ✓	
⊙	11.54	1009.39 ✓	0.58	997.85 ✓	

Top Mont "E" and Lex

Top Mont $\frac{1}{2}$ M₁ North "E"

SpK in 10" Oak

SpK in PP. SE. Cor Fand Lexington

	+	π ✓	-		
		1009.39			
BM.	7.87	1009.74	7.52	1001.87 ✓	1001.85
o	2.28	1010.93	109	1008.65	
o	0.86	1009.25	11.54	999.39	
o	0.18	988.06	12.37	987.88	
o	0.19	976.23	12.02	976.04	
BM			10.60	OK 65.63 ✓	965.56
o	2.55	967.34	11.44	964.79	
BM	2.50	964.68	5.16	62.18 ✓	965.55
o	5.19	967.12	275	961.93	
o	0.55	961.74	593	961.19	
BM.			10.62	951.12	951.07
o	4.63	955.81	10.56	951.18	
BM	0.37	951.58	460	951.21	951.17
o	0.20	939.48	12.30	939.28	
o	0.59	927.56	12.51	926.97	

SpK 10 12" BE 30' Rt. Sta 64+70

SpKin Tree SW Cor Vic rlex

Iron Pin Int Lex and Victoria

SpKin 12" Pop 100' L[±] Sta 97+

Ctr. Mont G & Lex

	+	+	-	Elev	
		927.56			
○	0.58	915.92	12.22	915.34	
○	0.25	903.27	12.90	903.02	
○	2.98	898.22	8.03	895.24	
B.M.			5.20	893.02	893.05
B.M.			5.50	892.72	
○	6.83	899.85	5.20	893.02	
○	10.20	909.42	0.63	899.22	
○	3.87	912.34	0.95	908.47	
B.M.			9.92	902.42	902.34
○	12.36	920.95	3.75	908.59	
B.M.			1.95	919.00	918.95
B.M.	2.65	920.27	3.27	917.68	917.62
	4.80	917.26	7.81	912.46	

Top Mont G² and Lex

T.P. Gons

Spk in 15 Ton NW Cor G² + Lex

9 PK in 12" Oak 60' Lt Sta 145+35

Spk in 18" Oak 60' Rt. Sta 157+57

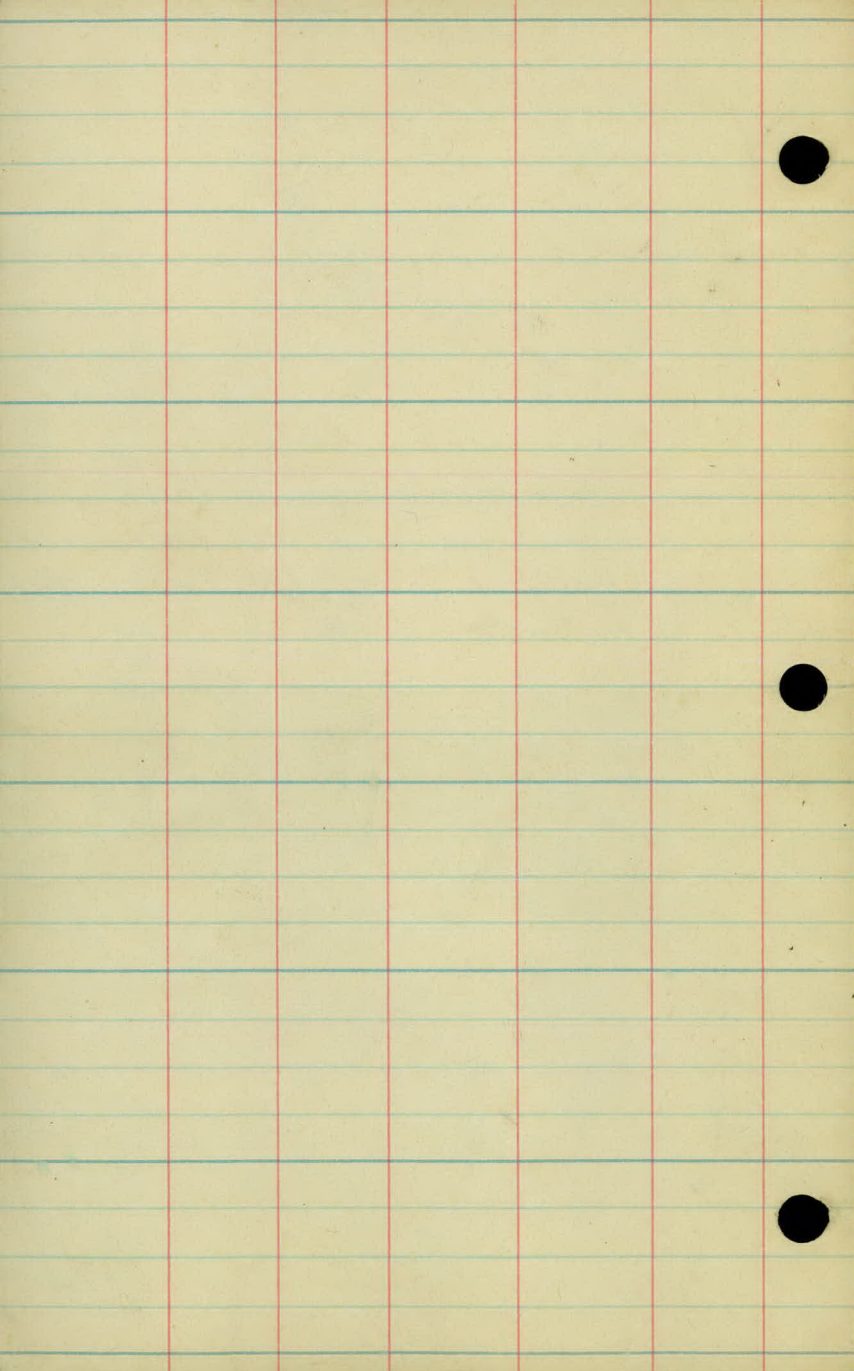
Top Mont

	+	π	-	Elev.	
		917.26			
o	10.13	919.90	7.49	909.77	
B.M.			1.93	917.97	917.97 ✓
o	0.59	908.12	12.37	907.53	
o	4.03	900.04	12.11	896.01	
B.M.			5.00	895.04	895.04
o	8.27	906.96	13.5	898.69	
o	1.59	897.86	10.69	896.27	
B.M.			4.70	893.16	893.18
o	4.88	896.94	5.80	892.06	
B.M.			494	892.00	891.82
				893.12	

SpK in 15" Oak 125' Rt. Sta 173+45

SpK in 18" Pop Rt. Sta 186+18

SpK in 24" Oak Rt. Sta 197+93



10/10/35

Purcell

X- Sections

Lexington Ave

Co. Rd "E" to Co. Rd "I"

Sta

+

K

-

Elev.

B.M.

374

950.05

946.31

0+00

± Co. Rd "E"

46.4

+17

45.9

+28

45.7-

+35

45.6-

1

44.8-

2

43.8

0.49

947.64

2.90

947.15

$$\begin{array}{r}
 47.36 \\
 46.18 \\
 \hline
 1.18
 \end{array}$$

Top Mont. Co. Rd. "E" and Lexington

Top Conc. Bv. 2

$$\begin{array}{r}
 5.90 \\
 162
 \end{array}
 \quad
 \begin{array}{r}
 6.1 \\
 100
 \end{array}
 \quad
 \begin{array}{r}
 5.2 \\
 46
 \end{array}
 \quad
 3.7
 \quad
 \begin{array}{r}
 3.5 \\
 53
 \end{array}
 \quad
 \begin{array}{r}
 2.7 \\
 100
 \end{array}$$

$$\begin{array}{r}
 6.2 \\
 100
 \end{array}
 \quad
 \begin{array}{r}
 5.8 \\
 51
 \end{array}
 \quad
 \begin{array}{r}
 4.3 \\
 6
 \end{array}
 \quad
 4.2
 \quad
 \begin{array}{r}
 4.2 \\
 11
 \end{array}
 \quad
 \begin{array}{r}
 4.3 \\
 79
 \end{array}
 \quad
 \begin{array}{r}
 3.8 \\
 100
 \end{array}$$

$$\begin{array}{r}
 5.0 \\
 100
 \end{array}
 \quad
 \begin{array}{r}
 5.7 \\
 56
 \end{array}
 \quad
 \begin{array}{r}
 5.4 \\
 28
 \end{array}
 \quad
 \begin{array}{r}
 4.4 \\
 7
 \end{array}
 \quad
 4.4
 \quad
 \begin{array}{r}
 4.4 \\
 11
 \end{array}
 \quad
 \begin{array}{r}
 5.5 \\
 38
 \end{array}
 \quad
 \begin{array}{r}
 4.7 \\
 61
 \end{array}
 \quad
 \begin{array}{r}
 3.8 \\
 100
 \end{array}$$

$$\begin{array}{r}
 5.0 \\
 100
 \end{array}
 \quad
 \begin{array}{r}
 5.8 \\
 57
 \end{array}
 \quad
 \begin{array}{r}
 5.5 \\
 28
 \end{array}
 \quad
 \begin{array}{r}
 4.4 \\
 7
 \end{array}
 \quad
 4.5
 \quad
 \begin{array}{r}
 4.5 \\
 10
 \end{array}
 \quad
 \begin{array}{r}
 5.9 \\
 54
 \end{array}
 \quad
 \begin{array}{r}
 5.9 \\
 86
 \end{array}
 \quad
 \begin{array}{r}
 5.8 \\
 100
 \end{array}$$

$$\begin{array}{r}
 7.0 \\
 100
 \end{array}
 \quad
 \begin{array}{r}
 7.9 \\
 65
 \end{array}
 \quad
 \begin{array}{r}
 9.7 \\
 22
 \end{array}
 \quad
 \begin{array}{r}
 5.8 \\
 13
 \end{array}
 \quad
 \begin{array}{r}
 5.7 \\
 7
 \end{array}
 \quad
 5.3
 \quad
 \begin{array}{r}
 5.5 \\
 11
 \end{array}
 \quad
 \begin{array}{r}
 6.2 \\
 21
 \end{array}
 \quad
 \begin{array}{r}
 6.2 \\
 27
 \end{array}
 \quad
 \begin{array}{r}
 6.1 \\
 50
 \end{array}
 \quad
 \begin{array}{r}
 6.2 \\
 100
 \end{array}$$

$$\begin{array}{r}
 12.7 \\
 100
 \end{array}
 \quad
 \begin{array}{r}
 11.6 \\
 66
 \end{array}
 \quad
 \begin{array}{r}
 10.4 \\
 21
 \end{array}
 \quad
 \begin{array}{r}
 7.5 \\
 16
 \end{array}
 \quad
 \begin{array}{r}
 6.7 \\
 9
 \end{array}
 \quad
 6.3
 \quad
 \begin{array}{r}
 6.5 \\
 10
 \end{array}
 \quad
 \begin{array}{r}
 6.8 \\
 32
 \end{array}
 \quad
 \begin{array}{r}
 7.0 \\
 100
 \end{array}$$

Grd @ Oil Tanks

Top SW Cor Oil Tank Per

Sta

+

X

-

947.64

2 + 88

43.8 -

3

43.6 -

+17

43.5 -

+55

41.2 -

4

40.0

+47

38.7 -

0

3.32

939.09

11.87

935.77

5

36.8 -

6

34.0 -

EBM WBM
Base P/B/R

$$\begin{array}{ccccccccc} 13.3 & 12.2 & 9.0 & 4.3 & 4.1 & 38 & 4.1 & 4.23 & 4.02 & 4.1 \\ 100-53 & 65 & 29 & 15 & 9 & & 8 & 12 & 91 & 100 \end{array}$$

$$\begin{array}{ccccccccc} 13.3 & 12.6 & 5.2 & 4.6 & 4.0 & 4.0 & 4.34 & 4.5 & 4.8 \\ 100-90 & 79 & 46 & 36 & 8 & 8 & 27 & 68 & 100 \end{array}$$

$$\begin{array}{ccccccccccc} & & BR & & BR & & & & & & & \\ 5.1 & 4.62 & 4.56 & 4.1 & 4.0 & 5.4 & 5.7 & 8.9 & 9.5 & 11.1 \\ 100 & 64 & 26 & 8 & 8 & 27 & 57 & 88 & 100 & 140 \end{array}$$

T.T.

$$\begin{array}{ccccccccccc} 5.0 & 6.1 & 12.8 & 13.6 & 7.5 & 6.7 & 6.4 & 6.5 & 6.2 & 12.2 & 12.3 & 13.0 \\ 127 & 100 & 50 & 27 & 16 & 8 & 9 & 16 & 16 & 30 & 67 & 100 \end{array}$$

$$\begin{array}{ccccccccccc} 12.1 & 14.8 & 13.6 & 8.5 & 8.1 & 7.6 & 8.0 & 8.2 & 11.8 & 15.0 & 15.6 \\ 100 & 63 & 26 & 15 & 9 & 9 & 16 & 16 & 29 & 82 & 100 \end{array}$$

$$\begin{array}{ccccccccccc} 15.2 & 13.1 & 11.2 & 7.8 & 9.2 & 8.9 & 7.3 & 12.9 & 13.5 \\ 100 & 63 & 29 & 18 & 9 & 10-17 & 10-17 & 28-77 & 100 \end{array}$$

$$\begin{array}{ccccccccccc} 7.3 & 9.1 & 7.8 & 2.9 & 2.2 & 2.3 & 2.8 & 6.8 & 5.57 \\ 100 & 64 & 27 & 16 & 9 & 17 & 17 & 29-72 & 84-100 \end{array}$$

$$\begin{array}{ccccccccccc} 11.5 & 10.8 & 6.6 & 5.6 & 5.1 & 5.7 & 6.4 & 10.7 & 10.9 \\ 100 & 55 & 26 & 16 & 10 & 9 & 16 & 25-75 & 100 \end{array}$$

Sta

+

π

-

939.09

6+50

32.7-

7

31.9-

8

31.9-

+50

32.3-

9

32.5-

B.M.

5.86

937.01

7.94

931.15

931.2

10

31.9-

11

31.9

$\frac{10.8}{100}$	$\frac{11.1}{57}$	$\frac{11.6}{25}$	$\frac{7.8}{15}$	$\frac{6.9}{10}$	6.4	$\frac{6.9}{9}$	$\frac{7.7}{16}$	$\frac{12.0}{27}$	$\frac{11.5}{28-64}$	$\frac{11.8}{100}$
--------------------	-------------------	-------------------	------------------	------------------	-----	-----------------	------------------	-------------------	----------------------	--------------------

$\frac{11.4}{100}$	$\frac{11.2}{52}$	$\frac{11.5}{26}$	$\frac{8.4}{16}$	$\frac{7.7}{10}$	7.2	$\frac{7.6}{8}$	$\frac{8.0}{15}$	$\frac{12.2}{27}$	$\frac{11.7}{28}$	$\frac{11.1}{73}$	$\frac{10.8}{100}$
--------------------	-------------------	-------------------	------------------	------------------	-----	-----------------	------------------	-------------------	-------------------	-------------------	--------------------

$\frac{11.7}{100}$	$\frac{11.1}{59}$	$\frac{11.7}{23}$	$\frac{12.3}{22}$	$\frac{8.0}{15}$	$\frac{7.9}{11}$	7.2	$\frac{7.6}{9}$	$\frac{8.2}{18}$	$\frac{11.9}{26}$	$\frac{11.1}{28}$	$\frac{10.4}{70}$	$\frac{9.4}{100}$
--------------------	-------------------	-------------------	-------------------	------------------	------------------	-----	-----------------	------------------	-------------------	-------------------	-------------------	-------------------

6.8

$\frac{12.0}{100}$	$\frac{11.4}{47}$	$\frac{11.1}{25}$	$\frac{11.5}{24}$	$\frac{7.6}{16}$	$\frac{7.1}{10}$	6.6	$\frac{7.0}{9}$	$\frac{7.4}{17}$	$\frac{11.9}{26}$	$\frac{10.9}{28}$	$\frac{10.0}{58}$	$\frac{8.1}{88}$	$\frac{7.8}{100}$
--------------------	-------------------	-------------------	-------------------	------------------	------------------	-----	-----------------	------------------	-------------------	-------------------	-------------------	------------------	-------------------

Spk in T.R. 28' Rt 5kg 9+70

$\frac{9.5}{100}$	$\frac{9.7}{57}$	$\frac{9.8}{25}$	$\frac{10.3}{24}$	$\frac{6.2}{16}$	$\frac{5.6}{11}$	5.1	$\frac{5.3}{9}$	$\frac{5.7}{16}$	$\frac{9.9}{26}$	$\frac{9.2}{29}$	$\frac{7.6}{77}$	$\frac{6.7}{100}$
-------------------	------------------	------------------	-------------------	------------------	------------------	-----	-----------------	------------------	------------------	------------------	------------------	-------------------

$\frac{9.7}{100}$	$\frac{9.9}{68}$	$\frac{9.9}{24}$	$\frac{10.1}{23}$	$\frac{6.0}{15}$	$\frac{5.5}{10}$	5.1	$\frac{5.3}{9}$	$\frac{5.8}{15}$	$\frac{10.1}{27}$	$\frac{9.4}{28}$	$\frac{8.3}{61}$	$\frac{6.2}{100}$
-------------------	------------------	------------------	-------------------	------------------	------------------	-----	-----------------	------------------	-------------------	------------------	------------------	-------------------

Sta

+

π

-

937.01

12

32.4 -

13

32.0 -

14

31.7 -

15

31.9 -

+09

24.48 CM

16

32.3 -

+80

33.0 -

17

33.0

$\frac{9.3}{100}$ $\frac{9.5}{62}$ $\frac{10.1}{27}$ $\frac{9.1}{22}$ $\frac{5.6}{17}$ $\frac{5.0}{10}$ 4.6 $\frac{4.9}{9}$ $\frac{5.2}{17}$ $\frac{5.7}{24}$ $\frac{10.0}{25-27}$ $\frac{8.5}{28}$ $\frac{7.6}{70}$ $\frac{6.9}{100}$

$\frac{8.3}{100}$ $\frac{9.9}{55}$ $\frac{10.3}{27}$ $\frac{6.1}{16}$ $\frac{5.5}{10}$ 5.0 $\frac{5.4}{9}$ $\frac{5.7}{15}$ $\frac{10.8}{26}$ $\frac{10.3}{28}$ $\frac{10.1}{67}$ $\frac{9.7}{100}$

$\frac{9.1}{100}$ $\frac{9.7}{56}$ $\frac{10.8}{25}$ $\frac{6.6}{17}$ $\frac{5.8}{11}$ 5.3 $\frac{5.5}{9}$ $\frac{6.0}{17}$ $\frac{10.7}{26}$ $\frac{10.3}{28}$ $\frac{8.2}{88}$ $\frac{8.0}{100}$

$\frac{9.4}{100}$ $\frac{10.1}{63}$ $\frac{10.3}{28}$ $\frac{11.2}{25}$ $\frac{6.8}{17}$ $\frac{5.7}{11}$ 5.1 $\frac{5.5}{9}$ $\frac{6.0}{16}$ $\frac{10.2}{25-27}$ $\frac{9.6}{28}$ $\frac{8.8}{71}$ $\frac{7.6}{100}$

FL. $\frac{11.52}{24}$

FL. $\frac{10.61}{24}$

$\frac{7.5}{100}$ $\frac{8.9}{53}$ $\frac{9.7}{28}$ $\frac{10.9}{27}$ $\frac{11.0}{25}$ $\frac{6.4}{18}$ $\frac{5.2}{11}$ 4.7 $\frac{5.0}{10}$ $\frac{5.7}{18}$ $\frac{8.5}{26}$ $\frac{8.6}{65}$ $\frac{8.0}{100}$

$\frac{6.1}{100}$ $\frac{4.5}{59}$ $\frac{4.3}{31}$ $\frac{9.5}{25-23}$ $\frac{8.1}{22}$ $\frac{5.1}{17}$ $\frac{4.4}{11}$ 4.0 $\frac{4.2}{18}$ $\frac{4.5}{17}$ $\frac{7.8}{23}$ $\frac{8.0}{25}$ $\frac{3.8}{31}$ $\frac{3.5}{68}$ $\frac{3.2}{100}$

$\frac{5.1}{92}$ $\frac{4.7}{58}$ $\frac{4.0}{31}$ $\frac{9.4}{25-23}$ $\frac{7.9}{22}$ $\frac{5.1}{16}$ $\frac{4.4}{12}$ 4.0 $\frac{4.2}{11}$ $\frac{4.5}{19}$ $\frac{7.3}{23-26}$ $\frac{3.3}{32}$ $\frac{3.0}{65-100}$
 $\frac{7.8}{100}$

Sta

+

A

-

937.01

①

3.68

936.26

4.43

932.58

17+25

33.0-

18

32.6.

19

31.9.

20

31.3.

①

8.71

940.21

4.76

931.50

21

30.9-

22

31.4

+11

24" X 68' C.M.

23

32.7

$\frac{5.1}{96}$ $\frac{5.4}{85}$ $\frac{4.7}{54}$ $\frac{4.5}{29}$ $\frac{8.8}{24}$ $\frac{7.3}{23}$ $\frac{4.4}{22}$ $\frac{3.7}{16}$ $\frac{3.7}{11}$ 3.3 $\frac{3.6}{10}$ $\frac{3.8}{18}$ $\frac{6.4}{22}$ $\frac{6.7}{26}$ $\frac{2.5}{31}$ $\frac{3.0}{100}$
 $\frac{7.7}{100}$

$\frac{8.0}{100}$ $\frac{8.5}{60}$ $\frac{8.0}{28}$ $\frac{9.4}{27}$ $\frac{7.8}{24}$ $\frac{4.7}{22}$ $\frac{4.2}{15}$ $\frac{4.2}{11}$ 3.7 $\frac{4.1}{9}$ $\frac{4.3}{17}$ $\frac{8.2}{25}$ $\frac{7.2}{28}$ $\frac{6.5}{65}$ $\frac{5.3}{100}$

$\frac{9.3}{100}$ $\frac{9.1}{51}$ $\frac{9.0}{28}$ $\frac{10.1}{26}$ $\frac{9.8}{23}$ $\frac{9.1}{22}$ $\frac{5.4}{15}$ $\frac{4.9}{11}$ 4.4 $\frac{4.7}{9}$ $\frac{5.3}{17}$ $\frac{8.3}{24}$ $\frac{6.8}{63}$ $\frac{4.8}{100}$

$\frac{9.3}{100}$ $\frac{9.2}{51}$ $\frac{9.6}{27}$ $\frac{10.0}{25}$ $\frac{6.8}{17}$ $\frac{5.7}{12}$ 5.0 $\frac{5.4}{9}$ $\frac{5.9}{16}$ $\frac{9.1}{24}$ $\frac{8.5}{51}$ $\frac{7.5}{100}$

Top Culv Post Rt Sta 22+11

$\frac{12.2}{100}$ $\frac{12.7}{51}$ $\frac{12.8}{27}$ $\frac{13.4}{26}$ $\frac{12.7}{24}$ $\frac{10.7}{23}$ $\frac{9.9}{19}$ $\frac{9.9}{12}$ 9.3 $\frac{9.6}{10}$ $\frac{10.2}{18}$ $\frac{9.4}{25}$ $\frac{13.0}{27}$ $\frac{13.1}{59}$ $\frac{12.8}{100}$

$\frac{12.5}{100}$ $\frac{12.8}{52}$ $\frac{9.9}{22}$ $\frac{9.3}{17}$ $\frac{9.3}{11}$ 8.8 $\frac{9.2}{10}$ $\frac{9.9}{17}$ $\frac{12.9}{25}$ $\frac{12.5}{60}$ $\frac{12.7}{100}$

In Dt 100' W of Outlet
 16.6 F.L. 15.06

F.L. 13.91

In Dt 100' E of Inl.
 12.4

$\frac{10.0}{100}$ $\frac{10.6}{52}$ $\frac{11.1}{22}$ $\frac{8.3}{17}$ $\frac{7.9}{10}$ 7.5 $\frac{7.9}{9}$ $\frac{8.3}{16}$ $\frac{12.0}{24}$ $\frac{12.4}{54}$ $\frac{11.7}{75}$ $\frac{11.0}{87}$ $\frac{12.5}{91-94}$ In Dt 11.1 100

Sta + π -
940.21

24 34.2-

25 35.6-

B.M. 10.52 947.70 3.03 937.18

+37 36.0-

26 36.7-

+42 37.2

27 37.2-

○ 6.88 943.76 10.82 936.88

28 37.1-

L.O. = Level Out
S.S. = Same Slope

$\frac{10.3}{100}$ $\frac{9.3}{54}$ $\frac{8.3}{25}$ $\frac{6.9}{14}$ $\frac{6.3}{10}$ 6.0 $\frac{6.3}{9-16}$ $\frac{9.1}{23}$ $\frac{9.5}{60}$ $\frac{8.2}{100}$

$\frac{7.8}{100}$ $\frac{8.1}{53}$ $\frac{7.7}{30}$ $\frac{7.8}{22}$ $\frac{5.5}{17}$ $\frac{5.0}{10}$ 4.7 $\frac{5.0}{9-18}$ $\frac{6.0}{22-25}$ $\frac{4.8}{28}$ $\frac{4.2}{74}$ $\frac{4.0}{100}$

Top Mont $\frac{1}{2}$ M. No Co. Rd "E"

$\frac{17.4}{100}$ $\frac{14.9}{54}$ $\frac{12.7}{28}$ $\frac{13.3}{24-18}$ $\frac{12.5}{15}$ $\frac{12.0}{11}$ 11.7 $\frac{12.0}{9}$ $\frac{11.9}{17}$ $\frac{12.7}{25}$ $\frac{8.8}{32}$ $\frac{4.9}{59}$ $\frac{4.4}{100}$

$\frac{13.8}{100}$ $\frac{12.4}{80}$ $\frac{10.6}{45}$ $\frac{9.4}{26}$ $\frac{11.8}{22}$ $\frac{11.9}{16}$ $\frac{11.4}{12}$ 11.0 $\frac{11.1}{10}$ $\frac{11.3}{18}$ $\frac{12.0}{23}$ $\frac{9.7}{32}$ $\frac{5.0}{38}$ $\frac{2.1}{60}$ $\frac{0.0}{100}$ $\frac{0.0}{100}$

$\frac{12.0}{100}$ $\frac{10.4}{52}$ $\frac{10.6}{10}$ 10.5 $\frac{10.5}{8}$ $\frac{11.6}{22}$ $\frac{6.8}{38}$ $\frac{1.8}{100}$ $\frac{1.1}{125}$ $\frac{2.0}{150}$ $\frac{5.5}{250}$

$\frac{12.5}{100}$ $\frac{13.3}{68}$ $\frac{12.7}{23}$ $\frac{11.4}{17}$ $\frac{11.0}{13}$ 10.5 $\frac{10.6}{9}$ $\frac{10.8}{15}$ $\frac{12.3}{20}$ $\frac{11.7}{27}$ $\frac{8.4}{31}$ $\frac{4.4}{73}$ $\frac{3.1}{100}$ $\frac{4.3}{150}$
5.8
200

$\frac{11.8}{100}$ $\frac{12.8}{46}$ $\frac{11.6}{23}$ $\frac{8.1}{17}$ $\frac{7.3}{11}$ 6.7 $\frac{7.0}{9}$ $\frac{7.4}{17}$ $\frac{11.5}{25}$ $\frac{10.8}{64}$ $\frac{13.0}{80}$ $\frac{9.1}{100}$

Sta

+

 π

-

943.76

28 + 50

37.3

29

37.6

30

38.0

31

39.0

32

40.0

33

40.4

+30

40.6

O

11.15

951.75

3.16

940.60

34

40.9

$$\frac{13.4}{100} \quad \frac{13.2}{59} \quad \frac{11.9}{23} \quad \frac{7.6}{15} \quad \frac{7.1}{11} \quad 6.5 \quad \frac{6.8}{10} \quad \frac{7.4}{17} \quad \frac{11.8}{26} \quad \frac{10.7}{86} \quad \frac{9.6}{100} \quad \frac{6.3}{150}$$

$$\frac{55}{200}$$

$$\frac{13.3}{100} \quad \frac{13.3}{63} \quad \frac{12.8}{28} \quad \frac{7.5}{16} \quad \frac{6.8}{11} \quad 6.2 \quad \frac{6.6}{10} \quad \frac{7.0}{16} \quad \frac{11.3}{26} \quad \frac{10.5}{62} \quad \frac{8.2}{81} \quad \frac{6.6}{100} \quad \frac{3.9}{150-20}$$

$$\frac{12.7}{100-67} \quad \frac{10.8}{26} \quad \frac{7.0}{16} \quad \frac{6.3}{11} \quad 5.8 \quad \frac{6.1}{10} \quad \frac{6.4}{16} \quad \frac{8.7}{22} \quad \frac{7.9}{32} \quad \frac{6.6}{38} \quad \frac{5.8}{56} \quad \frac{6.0}{94} \quad \frac{8.0}{120}$$

$$\frac{11.1}{100} \quad \frac{11.2}{60} \quad \frac{10.1}{27} \quad \frac{5.9}{19} \quad \frac{5.2}{11} \quad 4.8 \quad \frac{5.1}{16} \quad \frac{5.8}{19} \quad \frac{5.4}{42} \quad \frac{8.0}{74} \quad \frac{8.4}{100}$$

$$\frac{4.0}{37} \quad \frac{3.4}{35} \quad \frac{2.9}{32} \quad \frac{5.7}{26} \quad \frac{6.0}{20} \quad \frac{4.5}{15} \quad \frac{4.1}{10} \quad 3.8 \quad \frac{4.0}{10} \quad \frac{4.2}{17} \quad \frac{5.3}{21} \quad \frac{5.2}{33} \quad \frac{8.8}{100}$$

$$\frac{10.8}{100}$$

$$\frac{7.0}{100} \quad \frac{6.8}{80} \quad \frac{5.6}{36} \quad \frac{4.2}{34} \quad \frac{3.8}{32} \quad \frac{5.2}{28} \quad \frac{5.4}{19} \quad \frac{4.0}{14} \quad \frac{3.5}{10} \quad 3.4 \quad \frac{3.7}{11} \quad \frac{3.9}{17} \quad \frac{5.8}{23} \quad \frac{5.2}{35} \quad \frac{7.6}{63} \quad \frac{8.5}{100}$$

$$\frac{5.0}{100} \quad \frac{4.1}{56} \quad \frac{2.7}{30} \quad \frac{5.0}{25} \quad \frac{3.8}{14} \quad \frac{3.4}{10} \quad 3.2 \quad \frac{3.5}{11} \quad \frac{3.7}{15} \quad \frac{5.2}{21-28} \quad \frac{6.0}{40} \quad \frac{7.6}{62} \quad \frac{8.2}{100}$$

$$\frac{13.0}{100} \quad \frac{6.3}{46} \quad \frac{3.7}{21} \quad \frac{11.5}{19} \quad \frac{11.1}{10} \quad 10.9 \quad \frac{11.4}{9} \quad \frac{12.0}{17} \quad \frac{13.2}{21-37} \quad \frac{14.4}{52} \quad \frac{15.6}{78}$$

$$\frac{16.3}{100}$$

Sta + π -
951.75

34 +60

40.9 ✓

35

40.9 ✓

+50

41.0 ✓

①

5.29

946.12 ✓

10.92

940.83 ✓

36

40.7 ✓

36 + 58

BM,

7.42

938.70 ✓

37

40.9 ✓

+58

15" X 42 VP

①

7.63

946.33 ✓

7.42

938.70 ✓

38

41.1 ✓

$\frac{13.3}{100}$ $\frac{8.1}{68}$ $\frac{2.3}{33}$ $\frac{9.1}{24}$ $\frac{11.2}{17}$ $\frac{11.1}{11}$ 10.9 $\frac{11.2}{11}$ $\frac{11.6}{15}$ $\frac{13.8}{22}$ $\frac{15.1}{51}$ $\frac{16.3}{100}$

$\frac{5.5}{100}$ $\frac{6.8}{62}$ $\frac{3.2}{33}$ $\frac{11.0}{20}$ $\frac{11.2}{10}$ 10.9 $\frac{11.2}{12}$ $\frac{11.6}{17}$ $\frac{14.5}{23}$ $\frac{15.5}{64}$ $\frac{17.0}{100}$

$\frac{8.0}{100}$ $\frac{3.2}{59}$ $\frac{5.2}{36}$ $\frac{11.6}{25}$ $\frac{11.0}{14-9}$ 10.8 $\frac{11.3}{11}$ $\frac{11.4}{17}$ $\frac{15.1}{25}$ $\frac{16.7}{62}$ $\frac{17.6}{100}$

$\frac{11.0}{88}$ $\frac{1.5}{62}$ $\frac{6.2}{52}$ $\frac{7.0}{38}$ $\frac{8.1}{29}$ $\frac{8.6}{21}$ $\frac{5.7}{14}$ $\frac{5.6}{10}$ 5.4 $\frac{5.7}{10}$ $\frac{6.1}{16}$ $\frac{9.9}{24}$ $\frac{11.6}{62}$ $\frac{12.0}{100}$ $\frac{11.9}{130}$
 $\frac{11.7}{134}$ $\frac{12.6}{133-131}$

SPK in 10' oak 38 + 25 - 50' Lt

$\frac{5.9}{100}$ $\frac{9.7}{57}$ $\frac{9.8}{24}$ $\frac{6.3}{18}$ $\frac{5.6}{12}$ 5.2 $\frac{5.4}{9}$ $\frac{5.7}{16}$ $\frac{9.7}{23}$ $\frac{10.7}{34}$ $\frac{9.5}{35}$ $\frac{9.6}{70}$ $\frac{9.9}{100}$

FL 7
10.86

FL 7
12.69

$\frac{9.7}{100}$ $\frac{10.0}{50}$ $\frac{8.7}{20}$ $\frac{6.0}{14}$ $\frac{5.5}{10}$ 5.2 $\frac{5.3}{10}$ $\frac{5.4}{17}$ $\frac{9.8}{26}$ $\frac{7.6}{31}$ $\frac{7.4}{33}$ $\frac{8.1}{78}$ $\frac{7.8}{100}$

Sta

+

T

-

946.33

38+85

41.6 ✓

39

+85

42.5 ✓

40

+25

42.8 ✓

41

43.3 ✓

+50

43.8 ✓

D

10.76

954.56

2.53

943.80

42

44.4 ✓

$$\frac{8.8}{100} \quad \frac{8.4}{65} \quad \frac{5.8}{27} \quad \frac{7.2}{23} \quad \frac{5.4}{16} \quad \frac{5.0}{11} \quad 4.1 \quad \frac{4.7}{9} \quad \frac{4.8}{13} \quad \frac{5.8}{21} \quad \frac{7.8}{24} \quad \frac{8.9}{26} \quad \frac{8.1}{28} \quad \frac{3.1}{31} \quad \frac{5.7}{100} \quad \frac{6.2}{76}$$

4.5

$$\frac{5.2}{100} \quad \frac{3.6}{75} \quad \frac{3.4}{53} \quad \frac{4.7}{29} \quad \frac{6.2}{27} \quad \frac{6.1}{20} \quad \frac{4.0}{15} \quad \frac{3.9}{10} \quad 3.8 \quad \frac{4.0}{9} \quad \frac{5.1}{21} \quad \frac{8.6}{26} \quad \frac{6.1}{31} \quad \frac{6.7}{64} \quad \frac{6.0}{100}$$

3.7

$$\frac{3.4}{100} \quad \frac{2.3}{56} \quad \frac{4.4}{30} \quad \frac{6.3}{28} \quad \frac{6.5}{23} \quad \frac{4.4}{17} \quad \frac{3.8}{11} \quad 3.5 \quad \frac{3.8}{9} \quad \frac{4.4}{16} \quad \frac{7.2}{24} \quad \frac{8.6}{47} \quad \frac{7.9}{100}$$

$$\frac{4.8}{100} \quad \frac{5.2}{60} \quad \frac{7.3}{28} \quad \frac{6.9}{23} \quad \frac{4.4}{18} \quad \frac{3.2}{10} \quad 3.0 \quad \frac{3.2}{10} \quad \frac{4.3}{17} \quad \frac{8.1}{25} \quad \frac{9.2}{68} \quad \frac{9.6}{100}$$

$$\frac{2.7}{100} \quad \frac{3.5}{63} \quad \frac{4.1}{47} \quad \frac{5.2}{30} \quad \frac{6.2}{28} \quad \frac{6.0}{23} \quad \frac{3.1}{16} \quad \frac{2.7}{10} \quad 2.5 \quad \frac{2.9}{9} \quad \frac{3.7}{17} \quad \frac{8.2}{27} \quad \frac{9.3}{65} \quad \frac{9.6}{100}$$

$$\frac{8.3}{49} \quad \frac{11.6}{40} \quad \frac{11.9}{29} \quad \frac{13.4}{27} \quad \frac{10.8}{24} \quad \frac{10.5}{16} \quad \frac{10.5}{10} \quad 10.2 \quad \frac{10.5}{9} \quad \frac{11.3}{17} \quad \frac{15.9}{26} \quad \frac{17.7}{78} \quad \frac{18.0}{100}$$

$$\frac{5.6}{73} \quad \frac{3.9}{100}$$

Sta

+

x

-

954.56

42+80

45.5 ✓

43

+20

46.0 ✓

+70

46.6 ✓

44

46.9 ✓

45

47.7 ✓

46

48.4 ✓

+45

48.9 ✓

$\frac{+0.5}{100}$ $\frac{0.6}{40}$ $\frac{3.6}{34}$ $\frac{11.1}{24}$ $\frac{11.2}{18}$ $\frac{9.5}{15}$ $\frac{9.3}{10}$ 9.1 $\frac{9.3}{9}$ $\frac{9.7}{16}$ $\frac{13.6}{24}$ $\frac{16.3}{73}$ $\frac{16.7}{100}$

8.8

$\frac{4.6}{100}$ $\frac{1.1}{62}$ $\frac{3.3}{35}$ $\frac{10.7}{22}$ $\frac{10.8}{19}$ $\frac{8.7}{14}$ $\frac{8.8}{10}$ 8.6 $\frac{8.8}{8}$ $\frac{8.9}{15}$ $\frac{12.7}{33}$ $\frac{14.7}{72}$ $\frac{15.6}{100}$

$\frac{8.4}{100}$ $\frac{5.7}{75}$ $\frac{5.6}{38}$ $\frac{6.8}{30}$ $\frac{10.5}{23}$ $\frac{10.2}{18}$ 8.1 $\frac{8.1}{14-11}$ 8.0 $\frac{8.1}{9}$ $\frac{8.2}{15}$ $\frac{10.4}{23}$ $\frac{9.5}{27}$ $\frac{4.9}{33}$ $\frac{11.3}{100}$

$\frac{8.5}{100}$ $\frac{7.1}{70}$ $\frac{7.0}{27}$ $\frac{10.0}{23}$ $\frac{9.7}{18}$ $\frac{7.9}{14}$ $\frac{7.8}{11}$ 7.7 $\frac{7.8}{7}$ $\frac{8.0}{15}$ $\frac{9.2}{19}$ $\frac{10.1}{24}$ $\frac{9.5}{27}$ $\frac{6.1}{32}$ $\frac{7.7}{100}$

$\frac{9.4}{84}$ $\frac{8.2}{57}$ $\frac{7.6}{27}$ $\frac{9.2}{25-19}$ $\frac{6.9}{14-12}$ 6.9 $\frac{7.0}{8}$ $\frac{7.1}{13}$ $\frac{8.3}{18}$ $\frac{9.5}{30}$ $\frac{10.7}{85}$ $\frac{10.1}{100}$

$\frac{10.6}{100}$ $\frac{7.7}{67}$ $\frac{6.3}{29}$ $\frac{8.4}{25}$ $\frac{8.1}{20}$ $\frac{6.4}{15-12}$ 6.2 $\frac{6.3}{6}$ $\frac{6.6}{13}$ $\frac{6.8}{46}$ $\frac{4.9}{100}$

$\frac{10.1}{100}$ $\frac{9.3}{88}$ $\frac{7.1}{62}$ $\frac{7.5}{28}$ $\frac{8.5}{25-22}$ $\frac{6.0}{14}$ 5.7 $\frac{5.8}{6}$ $\frac{6.1}{12}$ $\frac{6.2}{51}$ $\frac{2.7}{100}$

Sta + π —
954.56

47 49.3

0 5.58 954.87 5.27 949.29

48 50.3

49 52.4

0 13.22 968.02 0.07 954.80

+75 54.9

50 55.7

+45 57.2

51 58.9

$\frac{7.1}{100}$	$\frac{11.2}{72}$	$\frac{11.1}{27}$	$\frac{6.5}{17}$	$\frac{5.7}{12}$	5.3	$\frac{5.4}{8}$	$\frac{6.1}{17}$	$\frac{10.2}{25}$	$\frac{9.1}{50}$	$\frac{7.0}{80}$	$\frac{4.8}{100}$
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Top Pavement Sta 47+00

F.L. 12.78 +09 End Curb
30

12'x62CM

+25 End Curb F.L. 11.55
31

$\frac{4.7}{100}$	$\frac{8.2}{67}$	$\frac{8.1}{24}$	$\frac{5.5}{17}$	$\frac{4.8}{11}$	4.6	$\frac{4.7}{8}$	$\frac{5.5}{14}$	$\frac{11.3}{26}$	$\frac{11.9}{48}$	$\frac{10.0}{100}$
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$\frac{5.5}{100}$	$\frac{6.9}{70}$	$\frac{4.8}{23}$	$\frac{3.0}{16}$	$\frac{2.6}{10}$	2.5	$\frac{2.7}{7}$	$\frac{3.2}{18}$	$\frac{7.5}{26}$	$\frac{8.4}{61}$	$\frac{4.8}{100}$
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$\frac{7.6}{100}$	$\frac{6.4}{68}$	$\frac{6.6}{33}$	$\frac{14.3}{21}$	$\frac{14.5}{18}$	$\frac{13.5}{15-11}$	13.1	$\frac{13.4}{9}$	$\frac{13.3}{16}$	$\frac{15.4}{21}$	$\frac{15.6}{38}$	$\frac{13.8}{52}$	$\frac{16.8}{100}$
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$\frac{5.7}{100}$	$\frac{3.8}{68}$	$\frac{4.3}{33}$	$\frac{11.4}{26}$	$\frac{13.3}{12-20}$	$\frac{12.4}{15}$	$\frac{12.6}{11}$	12.3	$\frac{12.5}{9}$	$\frac{12.6}{16}$	$\frac{14.9}{24}$	$\frac{14.8}{37}$	$\frac{12.9}{51}$	$\frac{17.1}{100}$
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$\frac{2.1}{100}$	$\frac{3.1}{72}$	$\frac{4.2}{33}$	$\frac{11.3}{25}$	$\frac{12.2}{20}$	$\frac{12.2}{18}$	$\frac{11.0}{14}$	$\frac{11.1}{11}$	10.8	$\frac{11.1}{9-15}$	$\frac{13.6}{23-40}$	$\frac{12.6}{47}$	$\frac{15.7}{100}$
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$\frac{7.3}{100}$	$\frac{9.6}{66}$	$\frac{10.6}{30}$	$\frac{10.9}{25-19}$	$\frac{9.6}{16}$	$\frac{9.3}{11}$	9.1	$\frac{9.4}{9}$	$\frac{9.5}{14}$	$\frac{11.1}{17}$	$\frac{11.4}{23}$	$\frac{10.9}{26}$	$\frac{12.6}{55}$
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$\frac{14.5}{100}$

Sta

+

π

-

968.02

51 +55

60.7

BM

8.80

972.54

4.28

963.74

963.74

62.2

52

15.3

+65

64.4

+70

64.5

+83

L. Co Rd "F"

964.99

15.3

53

65.5

+25

66.2

962.78

Rain

$\frac{13.1}{100}$ $\frac{12.6}{50}$ $\frac{9.7}{21}$ $\frac{7.7}{16}$ $\frac{7.5}{12}$ 7.3 $\frac{7.6}{9}$ $\frac{7.4}{12}$ $\frac{9.0}{17}$ $\frac{8.9}{22}$ $\frac{6.7}{25}$ $\frac{7.2}{44}$ $\frac{12.2}{100}$

SpK in PP. SE Cor Lcv r "F"

$\frac{13.8}{100}$ $\frac{13.2}{65}$ $\frac{12.2}{21}$ $\frac{10.8}{16}$ $\frac{10.5}{11}$ 10.3 $\frac{10.6}{9}$ $\frac{10.7}{12}$ $\frac{12.3}{17}$ $\frac{12.1}{23}$ $\frac{10.8}{24}$ $\frac{12.5}{59}$
 $\frac{14.8}{100}$

$\frac{8.8}{100}$ $\frac{9.0}{38}$ $\frac{8.3}{10}$ 8.1 $\frac{8.1}{7}$ $\frac{8.6}{26}$ $\frac{8.8}{41}$ $\frac{7.8}{100}$

$\frac{10.1}{100}$ $\frac{9.0}{50}$ 8.0

$\frac{7.9}{50}$ $\frac{6.6}{100}$

Top Mont
 $\frac{9.4}{100}$ $\frac{8.6}{52}$ 7.55 $\frac{7.0}{51}$ $\frac{5.9}{100}$

$\frac{9.7}{100}$ $\frac{9.0}{50}$ 7.3 $\frac{7.4}{50}$ $\frac{6.2}{100}$

$\frac{12.5}{100}$ $\frac{11.2}{75}$ $\frac{9.3}{37}$ $\frac{8.4}{30}$ 7.0 $\frac{7.4}{20}$ $\frac{8.0}{50}$ $\frac{7.2}{100}$

$\frac{9.5}{100}$ $\frac{8.9}{60}$ $\frac{7.2}{27}$ $\frac{8.2}{22}$ $\frac{7.4}{19}$ $\frac{6.8}{13}$ 6.3 $\frac{6.6}{9}$ $\frac{7.1}{14}$ $\frac{8.5}{18}$ $\frac{8.6}{22}$ $\frac{6.1}{25}$ $\frac{5.9}{68}$ $\frac{5.8}{100}$

Sta

+

x

-

972.54

54

68.3

55

71.4

O

13.01

985.35

0.20

972.34

x

56

74.8

57

78.3

58

82.3

O

13.50

998.68

0.17

985.18

+70

85.2

59

86.5

$\frac{9.5}{100}$ $\frac{9.3}{64}$ $\frac{7.9}{24}$ $\frac{5.1}{17}$ $\frac{4.6}{11}$ 4.2 $\frac{4.5}{9}$ $\frac{4.8}{13}$ $\frac{6.5}{17}$ $\frac{6.9}{22}$ $\frac{6.1}{26}$ $\frac{6.4}{63}$ $\frac{6.0}{100}$

$\frac{7.5}{100}$ $\frac{6.4}{70}$ $\frac{5.7}{33}$ $\frac{2.4}{21}$ $\frac{1.3}{11}$ 1.1 $\frac{1.4}{9}$ $\frac{1.8}{14}$ $\frac{3.9}{21}$ $\frac{4.4}{61}$ $\frac{1.4}{100}$

$\frac{15.3}{100}$ $\frac{13.3}{61}$ $\frac{12.8}{29}$ $\frac{11.2}{18}$ $\frac{11.0}{11}$ 10.6 $\frac{10.9}{10}$ $\frac{11.2}{16}$ $\frac{12.3}{21}$ $\frac{12.7}{66}$ $\frac{10.4}{100}$

$\frac{11.3}{100}$ $\frac{11.0}{62}$ $\frac{9.7}{32}$ $\frac{7.6}{17}$ $\frac{7.5}{11}$ 7.1 $\frac{7.3}{9-15}$ $\frac{8.4}{18}$ $\frac{8.3}{25}$ $\frac{6.4}{29}$ $\frac{4.4}{65}$ $\frac{2.4}{100}$

$\frac{4.8}{100}$ $\frac{5.7}{72}$ $\frac{5.3}{36}$ $\frac{3.3}{31}$ $\frac{5.5}{26}$ $\frac{5.4}{19}$ $\frac{3.4}{15-11}$ 3.1 $\frac{3.4}{9}$ $\frac{3.9}{14}$ $\frac{4.5}{16}$ $\frac{4.6}{24}$ $\frac{0.7}{32}$ $\frac{7.0.3}{100}$

$\frac{15.1}{100}$ $\frac{16.3}{74}$ $\frac{16.5}{27}$ $\frac{13.9}{31}$ $\frac{15.3}{18}$ $\frac{14.1}{14}$ $\frac{13.8}{11}$ 13.5 $\frac{13.7}{9}$ $\frac{14.1}{15}$ $\frac{14.8}{18-25}$ $\frac{11.1}{32}$ $\frac{10.3}{60}$
 $\frac{8.5}{100}$

$\frac{14.5}{100}$ $\frac{15.1}{79}$ $\frac{14.5}{38}$ $\frac{12.2}{32}$ $\frac{14.3}{27-18}$ $\frac{12.6}{14-10}$ 12.2 $\frac{12.5}{10}$ $\frac{12.7}{15}$ $\frac{13.5}{19-23}$ $\frac{7.4}{33}$ $\frac{6.6}{74}$ $\frac{6.0}{100}$

Sta

+

 π

-

798.68

59+50

88.7

60

90.9

+40

92.5

61

94.6

62

10.18

1007.76

1.10

997.58

62

97.6

+45

98.6

63

99.7

$\frac{12.1}{100}$ $\frac{12.2}{82}$ $\frac{10.4}{37}$ $\frac{9.2}{33}$ $\frac{11.7}{27-19}$ $\frac{10.4}{16-11}$ 10.0 $\frac{10.3}{16}$ $\frac{10.4}{16}$ $\frac{11.4}{17-20}$ $\frac{10.0}{24}$ $\frac{3.0}{35}$
 $\frac{4.1}{100}$ $\frac{3.1}{75}$

$\frac{7.4}{100}$ $\frac{5.0}{71}$ $\frac{2.4}{33}$ $\frac{8.3}{25}$ $\frac{9.4}{22-19}$ $\frac{8.1}{15-10}$ 7.8 $\frac{8.1}{11}$ $\frac{8.3}{17}$ $\frac{9.1}{19}$ $\frac{8.3}{23}$ $\frac{0.2}{34}$ $\frac{2.9}{64}$ $\frac{3.7}{100}$

$\frac{3.1}{100}$ $\frac{0.8}{62}$ $\frac{1.0}{33}$ $\frac{6.3}{25}$ $\frac{8.0}{21}$ $\frac{6.3}{15-11}$ 6.2 $\frac{6.5}{10}$ $\frac{6.4}{18}$ $\frac{7.3}{19-22}$ $\frac{6.8}{24}$ $\frac{0.7}{33}$ $\frac{3.9}{72}$ $\frac{5.1}{100}$

$\frac{5.4}{100}$ $\frac{3.8}{80}$ $\frac{1.0}{32}$ $\frac{5.9}{20}$ $\frac{4.6}{15}$ $\frac{4.3}{11}$ 4.1 $\frac{4.4}{10}$ $\frac{4.6}{15}$ $\frac{5.3}{18-24}$ $\frac{4.3}{27}$ $\frac{0.7}{32}$ $\frac{2.7}{65}$ $\frac{5.1}{100}$

$\frac{10.0}{100}$ $\frac{7.4}{58}$ $\frac{7.1}{32}$ $\frac{10.4}{27}$ $\frac{11.9}{23}$ $\frac{11.7}{20}$ $\frac{10.8}{15}$ $\frac{10.4}{11}$ 10.2 $\frac{10.4}{11}$ $\frac{10.5}{17}$ $\frac{11.5}{20-25}$ $\frac{10.8}{28}$ $\frac{8.1}{32}$ $\frac{11.0}{88}$
 $\frac{13.5}{100}$

$\frac{9.5}{100}$ $\frac{8.1}{67}$ $\frac{8.0}{30}$ $\frac{10.8}{25-20}$ $\frac{9.7}{15}$ $\frac{9.5}{10}$ 9.2 $\frac{9.5}{10}$ $\frac{9.6}{16}$ $\frac{10.8}{20-26}$ $\frac{9.9}{30}$ $\frac{11.0}{84}$ $\frac{12.3}{100}$

$\frac{9.2}{100}$ $\frac{8.1}{77}$ $\frac{8.1}{32}$ $\frac{9.1}{27-18}$ $\frac{8.6}{15}$ $\frac{8.5}{11}$ 8.1 $\frac{8.3}{10}$ $\frac{8.2}{17}$ $\frac{10.4}{24}$ $\frac{12.5}{67}$ $\frac{13.3}{100}$

Sta

+

π

-

1007.76 ✓

64

01.8 ✓

BM

6.35

1008.22 ✓ 5.91

1001.85 ✓

Elev. To
Charged Here
1001.87

65

03.3 ✓

66

05.6 ✓

+40

06.4 ✓

0

13.03

1020.38 ✓ 0.87

1007.35 ✓

10/17/35

67

07.8 ✓

+55

08.7 ✓

68

08.5 ✓

T.P.

4.72

1015.66 ✓

$\frac{6.8}{100}$ $\frac{5.3}{67}$ $\frac{4.4}{32}$ $\frac{7.9}{25}$ $\frac{6.5}{20}$ $\frac{6.3}{16}$ $\frac{6.0}{12}$ $\frac{6.3}{7}$ $\frac{6.6}{15}$ $\frac{7.5}{19}$ $\frac{8.5}{56}$ $\frac{7.6}{82}$ $\frac{8.0}{100}$

SpK in 12" BE, 30' Rt Sta. 64+70

Floor House 5.13

$\frac{4.9}{100}$ $\frac{5.3}{35}$ $\frac{4.3}{32}$ $\frac{6.7}{16}$ $\frac{5.4}{20}$ $\frac{5.2}{12}$ $\frac{5.3}{10}$ $\frac{7.3}{31}$ $\frac{8.9}{100}$

$\frac{6.0}{100}$ $\frac{5.4}{46}$ $\frac{4.8}{24}$ $\frac{3.5}{18}$ $\frac{2.9}{11}$ $\frac{2.8}{10}$ $\frac{3.6}{19}$ $\frac{3.9}{25}$ $\frac{7.2}{69}$ $\frac{8.2}{99}$ $\frac{9.1}{100}$

$\frac{5.6}{100}$ $\frac{4.6}{41}$ $\frac{4.1}{30}$ $\frac{3.8}{25}$ $\frac{3.6}{23}$ $\frac{2.1}{11}$ $\frac{2.0}{9}$ $\frac{1.9}{26}$ $\frac{2.4}{52}$ $\frac{2.4}{100}$

$\frac{11.0}{100}$ $\frac{10.5}{52}$ $\frac{9.2}{34}$ $\frac{13.9}{26}$ $\frac{13.8}{20}$ $\frac{13.0}{16}$ $\frac{12.9}{12}$ $\frac{12.8}{11}$ $\frac{13.1}{16}$ $\frac{13.6}{18}$ $\frac{13.4}{23}$ $\frac{12.7}{26}$ $\frac{8.3}{31}$
 $\frac{4.8}{100}$ $\frac{6.9}{69}$

$\frac{4.2}{100}$ $\frac{2.7}{33}$ $\frac{12.0}{22}$ $\frac{12.7}{18}$ $\frac{12.0}{12}$ $\frac{11.8}{11}$ $\frac{12.0}{11}$ $\frac{12.4}{16}$ $\frac{13.4}{18}$ $\frac{13.5}{24}$ $\frac{9.7}{31}$ $\frac{9.3}{20}$ $\frac{5.6}{100}$

$\frac{0.9}{100}$ $\frac{4.0}{39}$ $\frac{13.9}{25}$ $\frac{12.5}{19}$ $\frac{12.1}{16}$ $\frac{11.9}{11}$ $\frac{12.4}{12}$ $\frac{12.9}{17}$ $\frac{14.5}{21}$ $\frac{14.5}{27}$ $\frac{12.8}{31}$ $\frac{12.3}{71}$ $\frac{10.3}{100}$

Top SpK 100' Lt Sta 67+42

Sta

+

π

-

^{21.83}
1020.38 ✓

68+55

07.5 ✓

I.P.

0.61

1019.77 ✓

○

0.48

^{08.52}
1007.45 ✓ 13.41

1006.97 ✓

69

06.5 ✓

+65

04.6 ✓

70

03.1 ✓

+60

00.3 ✓

71

98.7 ✓

72

94.5 ✓

$\frac{+1.0}{100-71}$ $\frac{0.0}{49}$ $\frac{3.7}{46}$ $\frac{15.9}{28}$ $\frac{13.7}{21}$ $\frac{13.1}{15}$ $\frac{12.9}{11}$ $\frac{13.3}{11}$ $\frac{13.7}{17}$ $\frac{15.8}{21-27}$ $\frac{12.7}{31}$ $\frac{10.5}{84}$ $\frac{9.1}{100}$

Top Stk 100' Rt Sta 69+00

$\frac{2.7}{30}$ $\frac{3.8}{24-20}$ $\frac{1.6}{15}$ $\frac{1.2}{11}$ 1.0 $\frac{1.2}{11}$ $\frac{1.4}{15}$ $\frac{3.4}{21-24}$ $\frac{2.0}{30}$

$\frac{4.0}{32}$ $\frac{5.6}{24-21}$ $\frac{3.8}{16}$ $\frac{3.4}{11}$ 2.9 $\frac{3.3}{13}$ $\frac{3.4}{17}$ $\frac{5.1}{22-24}$ $\frac{3.0}{34}$

$\frac{5.2}{31}$ $\frac{6.8}{25-20}$ $\frac{5.0}{16}$ $\frac{4.8}{11}$ 4.4 $\frac{4.8}{13}$ $\frac{5.0}{17}$ $\frac{6.5}{20-25}$ $\frac{4.4}{32}$

$\frac{5.3}{33}$ $\frac{9.0}{24}$ $\frac{8.6}{19}$ $\frac{7.7}{16}$ $\frac{7.6}{16}$ 7.2 $\frac{7.5}{13}$ $\frac{7.6}{16}$ $\frac{8.9}{19-27}$ $\frac{7.2}{32}$

$\frac{6.4}{34}$ $\frac{9.8}{19}$ $\frac{9.2}{15}$ $\frac{9.0}{11}$ 8.8 $\frac{9.2}{12}$ $\frac{9.3}{15}$ $\frac{10.4}{18}$ $\frac{9.7}{25}$ $\frac{8.8}{30}$

$\frac{7.4}{38}$ $\frac{12.4}{29}$ $\frac{13.1}{10}$ 13.0 $\frac{13.4}{12}$ $\frac{13.6}{16}$ $\frac{14.3}{19}$ $\frac{12.5}{32}$

Sta

+

T

-

1007.45 ✓

0

0.32

994.79 ✓

12.98

994.47 ✓

73

90.0 ✓

74

85.3 ✓

+80

81.7 ✓

0

0.20

982.04 ✓

12.95

981.84 ✓

75

80.5 ✓

+25

79.2 ✓

76

75.6 ✓

0

7.90

(974.74) ✓

$$\frac{2.6}{32} \quad \frac{5.1}{11} \quad 4.8 \quad \frac{5.2}{13} \quad \frac{5.5}{16} \quad \frac{6.5}{21} \quad \frac{4.7}{30}$$

$$\frac{0.5}{42} \quad \frac{8.3}{28} \quad \frac{9.7}{11} \quad 9.5 \quad \frac{10.0}{12} \quad \frac{10.1}{15} \quad \frac{11.3}{19} \quad \frac{10.5}{28} \quad \frac{3.7}{37}$$

$$\frac{7.4}{39} \quad \frac{13.4}{28} \quad \frac{14.1}{21} \quad \frac{13.7}{20} \quad \frac{13.2}{11} \quad 13.1 \quad \frac{13.6}{11} \quad \frac{14.0}{16} \quad \frac{18.1}{22-24}$$

$$\frac{1.4}{23} \quad \frac{2.4}{19} \quad \frac{1.5}{10} \quad 1.5 \quad \frac{1.9}{11} \quad \frac{2.4}{18} \quad \frac{6.1}{24-26} \quad \frac{2.8}{27} \quad \frac{0.3}{32-35} \quad \frac{5.7}{82} \quad \frac{6.0}{100}$$

$$\frac{+1.0}{27} \quad \frac{3.3}{22} \quad \frac{3.0}{10} \quad 2.8 \quad \frac{3.2}{11} \quad \frac{4.0}{21} \quad \frac{8.1}{31} \quad \frac{8.6}{37} \quad \frac{10.1}{82} \quad \frac{12.3}{100}$$

$$\frac{5.9}{100} \quad \frac{8.9}{87} \quad \frac{9.3}{58} \quad \frac{15.9}{40} \quad \frac{7.0}{24} \quad \frac{6.8}{10} \quad 6.4 \quad \frac{7.0}{11} \quad \frac{8.0}{21} \quad \frac{17.4}{39} \quad \frac{17.8}{64} \quad \frac{19.5}{100}$$

Sta

+

BM

6.78

1026.55

1019.77

69+00

06.5

+65

04.6

70

03.1

+60

00.3

71

98.7

72

94.5

73

90.0

74

85.3

0

1.99

1015.36

13.18

1013.37

Top Stk 100' R+ Sta 69+00

$$\frac{4.3}{100} \quad \frac{4.2}{79} \quad \frac{6.3}{49}$$

20.1

$$\frac{11.4}{47} \quad \frac{9.5}{75} \quad \frac{7.6}{100}$$

$$\frac{4.2}{100} \quad \frac{3.6}{78} \quad \frac{2.6}{52}$$

22.0

$$\frac{4.5}{52} \quad \frac{4.7}{79} \quad \frac{4.8}{100}$$

$$\frac{4.2}{100} \quad \frac{3.7}{80} \quad \frac{2.7}{51}$$

23.5

$$\frac{6.7}{51} \quad \frac{7.3}{79} \quad \frac{6.2}{100}$$

$$\frac{4.5}{100} \quad \frac{4.7}{84} \quad \frac{4.9}{54}$$

26.3

$$\frac{12.0}{51} \quad \frac{11.4}{78} \quad \frac{9.3}{100}$$

$$\frac{5.0}{100} \quad \frac{4.7}{85-53}$$

27.9

$$\frac{9.0}{50-79} \quad \frac{7.7}{100}$$

$$\frac{7.0}{100} \quad \frac{7.5}{85} \quad \frac{6.6}{52}$$

32.1

$$\frac{8.5}{48} \quad \frac{9.1}{79} \quad \frac{10.1}{100}$$

$$\frac{10.4}{100} \quad \frac{10.7}{80} \quad \frac{10.8}{58}$$

36.6

$$\frac{10.8}{48} \quad \frac{14.9}{75} \quad \frac{18.8}{100}$$

$$\frac{14.8}{100} \quad \frac{16.4}{86} \quad \frac{19.2}{54}$$

41.3

$$\frac{9.6}{49} \quad \frac{12.5}{75} \quad \frac{16.7}{100}$$

L Side

R Side

Sta

+

 π

-

1015.36

74+80

81.7 ✓

75

80.5 ✓

75 +25

79.2 ✓

①

0.45

04.21 ✓
1003.16

12.65

1002.71 ✓

②

0.86

91.69 ✓
990.63

13.39

989.77 ✓

74+80

81.7 ✓

①

0.07

977.52 ✓

13.18

977.45 ✓

T.P. (check)

344

977.52 ✓

3.44

974.08 ✓

76+80

71.9 ✓

①

0.42

72.68 ✓
971.57

6.37

971.15 ✓

B.M.

5.99

72.71 ✓
971.62

5.99

965.58 ✓ = 965.63

$$\frac{12.8}{100} \quad \frac{14.6}{80} \quad \frac{15.8}{52}$$

33.7 ✓

$$\frac{15.4}{100} \quad \frac{18.1}{81} \quad \frac{21.4}{40}$$

34.9 ✓

$$\frac{19.5}{100} \quad \frac{22.4}{79} \quad \frac{31.4}{25}$$

36.1 ✓

$$\frac{11.9}{100} \quad \frac{9.6}{84} \quad \frac{4.4}{50} \quad \frac{0.9}{36}$$

8.9 ✓

$$\frac{19.1}{100} \quad \frac{20.0}{46} \quad \frac{6.8}{22} \quad \frac{6.0}{10} \quad 5.6 \quad \frac{6.0}{11} \quad \frac{7.4}{22} \quad \frac{16.4}{37-100}$$

SpK in 20° OAK 150 SW. Lex and F²

Sta

+

~~+~~

-

971.62

77

71.2 ✓

+ 55

69.0 ✓

78

67.0 ✓

+35

65.4 ✓

BM,

1.87

967.50 ✓

5.99

965.63 ✓

+70

64.0 ✓

79

62.9 ✓

+19

±

F²

62.2 ✓

35 = Same Slope

$$\frac{17.4}{100} \quad \frac{16.8}{84} \quad \frac{13.7}{41} \quad \frac{1.5}{20} \quad \frac{0.6}{11} \quad 0.4 \quad \frac{0.7}{11} \quad \frac{1.4}{23} \quad \frac{8.7}{37} \quad \frac{11.7}{100}$$

$$\frac{18.9}{100} \quad \frac{16.7}{52} \quad \frac{13.3}{38} \quad \frac{3.4}{20} \quad \frac{2.9}{10} \quad 2.6 \quad \frac{2.9}{11} \quad \frac{3.7}{22} \quad \frac{13.2}{40} \quad \frac{20.0}{100}$$

$$\frac{3.9}{130} \quad \frac{16.3}{100} \quad \frac{10.9}{77} \quad \frac{8.1}{48} \quad \frac{8.8}{29} \quad \frac{5.1}{23} \quad \frac{4.9}{10} \quad 4.6 \quad \frac{5.1}{11} \quad \frac{6.1}{21} \quad \frac{13.9}{31} \quad \frac{22.9}{50} \quad \frac{28.4}{100}$$

$$\frac{5.5}{160} \quad \frac{9.4}{100} \quad \frac{6.1}{92} \quad \frac{5.4}{72} \quad \frac{13.4}{31-33} \quad \frac{6.8}{22} \quad \frac{6.5}{10} \quad 6.2 \quad \frac{6.8}{12} \quad \frac{7.8}{21} \quad \frac{13.8}{29} \quad \frac{27.6}{53} \quad \frac{30.1}{94} \quad \frac{29.5}{100}$$

Top Iron Pin Victoria + Lex

$$\frac{7.0}{100} \quad \frac{10.3}{70} \quad \frac{15.1}{39} \quad \frac{4.6}{21} \quad \frac{3.8}{10} \quad 3.5 \quad \frac{4.0}{11} \quad \frac{5.2}{22} \quad \frac{13.3}{34} \quad \frac{2.46}{56} \quad \frac{27.6}{66} \quad \frac{24.6}{72}$$

$$\text{FL Colu} \quad \frac{13.7}{150} \quad \frac{21.1}{100}$$

$$\frac{12.0}{100} \quad \frac{13.1}{87} \quad \frac{20.2}{47} \quad \frac{19.2}{41} \quad \frac{5.5}{17} \quad \frac{4.8}{8} \quad 4.6 \quad \frac{5.0}{11} \quad \frac{7.2}{34} \quad \frac{9.2}{68} \quad \frac{9.3}{100} \quad \frac{9.1}{150}$$

$$\frac{13.0}{100} \quad \frac{24.0}{52-26} \quad \frac{6.3}{18} \quad \frac{5.5}{10} \quad 5.3 \quad \frac{5.8}{11} \quad \frac{7.7}{50} \quad \frac{8.3}{100} \quad \frac{8.3}{150}$$

Sta

+

x

-

967.50

79+35

61.4 ✓

+60

60.5 ✓

①

4.68

963.08

9.10

958.40 ✓

80

59.4 ✓

81

58.4 ✓

①

4.33

964.73 ✓

2.68

960.40 ✓

+55

59.0 ✓

82

59.5 ✓

$\frac{16.1}{120}$ $\frac{18.5}{100}$ $\frac{27.4}{65}$ $\frac{26.2}{49}$ $\frac{6.8}{19}$ $\frac{6.2}{10}$ 6.1 $\frac{6.4}{11}$ $\frac{9.0}{50}$ $\frac{8.9}{100}$ $\frac{8.9}{150}$

$\frac{18.9}{130}$ $\frac{22.2}{100}$ $\frac{91.1}{74}$ $\frac{27.1}{52}$ $\frac{8.1}{20}$ $\frac{7.1}{10}$ 7.0 $\frac{7.8}{15}$ $\frac{8.8}{27}$ $\frac{20.1}{48}$ $\frac{20.9}{82}$ $\frac{13.3}{115}$

FL Culv 33.0

$\frac{28.6}{100}$ $\frac{27.6}{57}$ $\frac{4.9}{19}$ $\frac{4.0}{9}$ 3.7 $\frac{4.0}{12}$ $\frac{4.5}{23}$ $\frac{15.4}{41}$ $\frac{19.4}{55}$ $\frac{17.2}{79}$ $\frac{12.1}{100}$ $\frac{25}{125}$

WS surface
 $\frac{31.5}{71}$ $\frac{29.4}{53}$ $\frac{6.0}{14}$ $\frac{5.2}{8}$ 4.7 $\frac{5.0}{13}$ $\frac{5.4}{23}$ $\frac{15.4}{39}$ $\frac{10.5}{74}$ $\frac{6.5}{100}$

on Gd Rl. Rt Sta

WS
 $\frac{31.5}{73}$ $\frac{29.3}{55}$ $\frac{7.1}{14}$ $\frac{6.1}{8}$ 5.9 $\frac{6.0}{12}$ $\frac{6.6}{23}$ $\frac{10.0}{31}$ $\frac{8.5}{43}$ $\frac{1.1}{100}$

WS
 $\frac{31.5}{115}$ $\frac{24.2}{68}$ $\frac{15.1}{33}$ $\frac{5.8}{17}$ $\frac{5.5}{8}$ 5.2 $\frac{5.4}{13}$ $\frac{5.9}{22}$ $\frac{6.8}{24}$ $\frac{2.2}{26}$ $\frac{2.2}{34}$ $\frac{0.0}{67}$ $\frac{+1.0}{100}$

Sta

+

X

-

964.73 ✓

①

5.26

966.51 ✓

348

961.25 ✓

82+50

60.0 ✓

83

60.7 ✓

+60

61.5 ✓

84

61.7 ✓

85

61.6 ✓

+75

62.0 ✓

86

62.0 ✓

$$\frac{5.5}{135} \quad \frac{2.1}{110} \quad \frac{8.0}{29} \quad \frac{9.3}{26} \quad \frac{7.3}{19} \quad \frac{6.8}{8} \quad 6.5 \quad \frac{6.6}{13} \quad \frac{6.4}{26} \quad \frac{1.2}{34} \quad \frac{+1.0}{68} \quad \frac{+1.8}{100}$$

$$\frac{5.5}{200} \quad \frac{9.6}{100} \quad \frac{4.5}{61} \quad \frac{4.6}{30} \quad \frac{7.5}{25-20} \quad \frac{6.3}{18} \quad \frac{6.1}{9} \quad 5.8 \quad \frac{6.1}{12} \quad \frac{5.5}{26} \quad \frac{+0.2}{33} \quad \frac{+1.2}{100}$$

$$\frac{2.7}{100} \quad \frac{1.3}{61} \quad \frac{3.9}{29} \quad \frac{6.5}{24-19} \quad \frac{5.4}{17} \quad \frac{5.3}{11} \quad 5.0 \quad \frac{5.3}{13} \quad \frac{5.4}{18} \quad \frac{6.3}{21} \quad \frac{6.5}{22-23} \quad \frac{6.0}{24} \quad \frac{2.1}{33} \quad \frac{+0.5}{72} \quad \frac{+1.0}{100}$$

Floor No 196

$$\frac{3.0}{100} \quad \frac{2.0}{65} \quad \frac{4.3}{26} \quad \frac{5.7}{25-21} \quad \frac{5.0}{18} \quad \frac{4.9}{12} \quad 4.8 \quad \frac{4.9}{13} \quad \frac{5.0}{21} \quad \frac{7.0}{24-25} \quad \frac{4.2}{29} \quad \frac{+0.3}{65} \quad \frac{+0.5}{100}$$

$$\frac{5.9}{100} \quad \frac{3.2}{60} \quad \frac{4.7}{27} \quad \frac{5.7}{24-20} \quad \frac{5.1}{18-11} \quad 4.9 \quad \frac{5.2}{11} \quad \frac{5.4}{19} \quad \frac{6.3}{21} \quad \frac{7.3}{22-23} \quad \frac{6.4}{24} \quad \frac{3.4}{66} \quad \frac{2.6}{100}$$

$$\frac{6.8}{100} \quad \frac{5.5}{65} \quad \frac{3.8}{28} \quad \frac{5.5}{25} \quad \frac{4.7}{11} \quad 4.5 \quad \frac{4.9}{11} \quad \frac{6.6}{19} \quad \frac{7.5}{37} \quad \frac{5.4}{72} \quad \frac{4.6}{100}$$

$$\frac{7.7}{100} \quad \frac{5.0}{36} \quad \frac{5.4}{19} \quad \frac{4.7}{11} \quad 4.5 \quad \frac{4.9}{10} \quad \frac{5.0}{16} \quad \frac{5.8}{19-21} \quad \frac{4.4}{28} \quad \frac{4.0}{79} \quad \frac{4.2}{100}$$

Sta

+

-

966.51✓

86+55

62.0✓

87

62.1✓

+75

62.4✓

88

62.5✓

○

388

966.06

4.33

962.18✓

89

62.2✓

+60

61.8✓

90

61.5✓

+09

61.5✓

$$\frac{9.2}{100} \frac{8.1}{65} \frac{5.7}{19} \frac{4.9}{11} 4.5 \frac{4.8}{10} \frac{5.0}{21} \frac{2.4}{29} \frac{3.8}{60} \frac{7.2}{100}$$

$$\frac{8.8}{100} \frac{7.6}{70} \frac{6.0}{21} \frac{5.0}{16} \frac{4.8}{11} 4.4 \frac{4.6}{11} \frac{4.9}{20} \frac{5.2}{21-24} \frac{4.6}{25} \frac{2.9}{56} \frac{3.7}{77} \frac{7.0}{100}$$

$$\frac{8.2}{100} \frac{4.1}{36} \frac{4.9}{19} \frac{4.5}{11} 4.1 \frac{4.3}{10} \frac{4.9}{20} \frac{5.4}{21-23} \frac{4.3}{25} \frac{3.3}{27} \frac{1.4}{77} \frac{0.3}{100}$$

$$\frac{8.3}{100} \frac{4.5}{37} \frac{5.0}{19} \frac{4.4}{11} 4.0 \frac{4.2}{10-19} \frac{5.3}{22-25} \frac{3.5}{26} \frac{2.5}{81} \frac{1.3}{100}$$

Floor House + 0.65

$$\frac{10.1}{100} \frac{6.4}{42} \frac{5.0}{20} \frac{4.4}{17} \frac{4.2}{11} 3.9 \frac{4.4}{11} \frac{4.9}{17} \frac{6.4}{20-39} \frac{3.8}{100}$$

$$\frac{9.7}{100} \frac{5.6}{40-24} \frac{4.6}{11} 4.3 \frac{4.7}{11} \frac{5.3}{17} \frac{8.0}{22} \frac{8.6}{31} \frac{9.7}{33} \frac{10.9}{74} \frac{10.5}{100} \frac{10.3}{115} \frac{8.4}{117}$$

$$\frac{8.6}{100} \frac{6.3}{49} \frac{6.6}{21} \frac{5.3}{16} \frac{5.0}{10} 4.6 \frac{5.0}{12} \frac{5.8}{18} \frac{8.3}{23} \frac{8.7}{40} \frac{9.6}{43} \frac{10.3}{69} \frac{10.6}{100-108} \frac{8.3}{110}$$

$$\frac{8.5}{100} \frac{6.3}{49} \frac{6.5}{20} \frac{5.3}{16} \frac{5.0}{10} 4.6 \frac{5.0}{12} \frac{5.8}{18} \frac{8.3}{23-100}$$

Sta

+

x

-

977.54 ✓
966.06 ✓

91

61.4 ✓

92

61.2 ✓

93

61.2 ✓

94

61.2 ✓

○

13.54

974.50 ✓

5.10

960.96 ✓

+65

61.1 ✓

95

61.1 ✓

+75

60.5 ✓

96

60.1 ✓

$\frac{8.2}{100}$ $\frac{7.6}{73}$ $\frac{8.2}{24}$ $\frac{5.4}{17}$ $\frac{5.0}{10}$ 4.7 $\frac{5.0}{11}$ $\frac{4.9}{18}$ $\frac{7.9}{25-80}$ $\frac{7.7}{100}$

FL. Culk 10.91

FL. Culk 9.82

$\frac{9.8}{100}$ $\frac{10.3}{69}$ $\frac{10.0}{24}$ $\frac{6.1}{17}$ $\frac{5.3}{11}$ 4.9 $\frac{5.2}{11}$ $\frac{5.3}{18}$ $\frac{8.4}{24}$ $\frac{6.8}{60}$ $\frac{2.5}{100}$

$\frac{11.8}{100}$ $\frac{10.2}{24}$ $\frac{6.2}{17}$ $\frac{5.4}{11}$ 4.9 $\frac{5.1}{11}$ $\frac{5.2}{19}$ $\frac{6.8}{24}$ $\frac{5.7}{69}$ $\frac{8.2}{100}$

$\frac{10.9}{100}$ $\frac{8.2}{24}$ $\frac{6.0}{18}$ $\frac{5.4}{12}$ 4.9 $\frac{5.0}{9}$ $\frac{4.6}{18}$ $\frac{4.8}{40}$ $\frac{0.8}{100}$

$\frac{17.5}{100}$ $\frac{16.8}{60}$ $\frac{13.7}{28}$ 26 $\frac{13.8}{22}$ $\frac{13.9}{19}$ $\frac{13.8}{13}$ 13.4 $\frac{13.4}{10-15}$ $\frac{13.8}{17}$ $\frac{13.3}{23}$ $\frac{9.6}{28}$ $\frac{7.2}{68}$ $\frac{3.8}{100}$

$\frac{13.5}{100}$ $\frac{15.4}{69}$ $\frac{12.0}{30}$ $\frac{13.9}{27}$ $\frac{14.5}{25-22}$ $\frac{14.2}{21}$ $\frac{13.7}{11}$ 13.4 $\frac{13.4}{9}$ $\frac{12.0}{23}$ $\frac{9.4}{28}$ $\frac{6.2}{29}$ $\frac{3.7}{66}$ $\frac{0.4}{100}$

$\frac{13.2}{100}$ $\frac{8.8}{35}$ $27-22$ $\frac{15.2}{20}$ $\frac{14.5}{14}$ $\frac{14.4}{14}$ 14.0 $\frac{14.1}{11}$ $\frac{9.1}{28}$ $\frac{4.9}{33}$ $\frac{0.3}{36}$ $\frac{0.0}{64}$ $\frac{+1.0}{100}$

$\frac{13.2}{100}$ $\frac{11.5}{83}$ $\frac{9.6}{36}$ $\frac{14.3}{30}$ $\frac{15.8}{27-22}$ $\frac{14.7}{19-15}$ 14.4 $\frac{14.6}{11}$ $\frac{9.9}{27}$ $\frac{9.8}{31}$ $\frac{0.2}{34}$ $\frac{0.4}{56}$ $\frac{+0.6}{100}$

Sta + x -
974.50 ✓

○ 1.22 964.24 ✓ 11.48 963.02 ✓

○ 2.96 960.56 ✓ 6.64 957.60 ✓

B.M. 9.42 951.14 ✓ 951.12

T.P. 7.50 965.08 ✓ 2.96 957.58 ✓

97 58.4 ✓

+70 56.8 ✓

98 56.1 ✓

99 54.3 ✓

○ 8.06 962.08 ✓ 11.06 954.02 ✓

Spk in 12" Pop 100 Lt Sta 97+85

$\frac{3.4}{40}$	$\frac{2.7}{45}$	$\frac{5.6}{28}$	$\frac{6.7}{32}$	$\frac{8.5}{27-24}$	$\frac{7.3}{21-15}$	6.7	$\frac{6.9}{9-15}$	$\frac{7.3}{17}$	$\frac{7.0}{20}$	$\frac{6.3}{23}$	$\frac{0.5}{31}$	$\frac{+1.0}{100}$
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$\frac{14.5}{100}$	$\frac{12.1}{34}$	33	$\frac{11.3}{25}$	$\frac{9.1}{21}$	$\frac{5.9}{14}$	8.3	$\frac{8.6}{9-18}$	$\frac{9.2}{19-23}$	$\frac{8.1}{27}$	$\frac{4.5}{100}$
--------------------	-------------------	----	-------------------	------------------	------------------	-----	--------------------	---------------------	------------------	-------------------

$\frac{16.4}{100}$	$\frac{15.8}{46}$	$\frac{12.4}{26}$	$\frac{10.2}{22}$	$\frac{9.6}{14}$	9.0	$\frac{9.1}{9}$	$\frac{7.3}{18}$	$\frac{10.3}{24}$	$\frac{7.0}{100}$
--------------------	-------------------	-------------------	-------------------	------------------	-----	-----------------	------------------	-------------------	-------------------

$\frac{17.6}{100}$	$\frac{14.5}{25}$	$\frac{12.0}{21}$	$\frac{11.1}{13}$	10.8	$\frac{10.9}{9-18}$	$\frac{12.1}{23}$	$\frac{10.7}{64}$	$\frac{6.2}{100}$
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F.L. Colv 13.03

F.L. Colv 11.42

Sta

+

x

-

962.08

100

53.0

101

52.4

102

51.9

103

51.3

104

51.1

+45

51.0

○

4.30

955.24

11.14

950.94

BM.

0.19

955.05

955.11

BM.

4.02

951.22

951.21

$\frac{16.1}{20}$ $\frac{13.7}{24}$ $\frac{13.0}{29}$ $\frac{10.0}{22}$ $\frac{9.5}{13}$ 9.1 $\frac{9.4}{9}$ $\frac{9.6}{21}$ $\frac{7.3}{66}$ $\frac{1.6}{100}$

$\frac{17.1}{100}$ $\frac{13.5}{26}$ $\frac{10.7}{14}$ $\frac{10.1}{12}$ 9.7 $\frac{9.8}{9}$ $\frac{10.2}{17}$ $\frac{10.4}{23}$ $\frac{7.4}{29}$ $\frac{5.4}{53}$ $\frac{0.6}{81}$ $\frac{55}{100}$

$\frac{16.5}{100}$ $\frac{12.9}{25}$ $\frac{11.1}{20}$ $\frac{10.5}{13}$ 10.2 $\frac{10.4}{10-24}$ $\frac{8.5}{23}$ $\frac{6.6}{51}$ $\frac{0.0}{88}$ $\frac{5.5}{100}$

$\frac{13.8}{100}$ $\frac{13.3}{23}$ $\frac{11.8}{18}$ $\frac{11.2}{13}$ 10.8 $\frac{10.9}{11}$ $\frac{11.0}{16}$ $\frac{11.5}{18}$ $\frac{11.0}{25}$ $\frac{8.9}{29}$ $\frac{7.3}{41}$ $\frac{0.0}{95}$ $\frac{55}{100}$

Floor Lc Ho. 10.70

$\frac{13.2}{100}$ $\frac{12.1}{27}$ $\frac{12.9}{25-27}$ $\frac{11.8}{19}$ $\frac{11.4}{12}$ 11.0 $\frac{11.3}{12}$ $\frac{11.6}{24}$ $\frac{7.0}{30}$ $\frac{2.7}{100}$

$\frac{13.9}{100}$ $\frac{12.2}{27}$ $\frac{13.2}{26-27}$ $\frac{11.7}{17}$ $\frac{11.4}{12}$ 11.1 $\frac{11.4}{12}$ $\frac{10.8}{26}$ $\frac{8.0}{30}$ $\frac{6.1}{68}$

NE Cor Conc Steps Sinal's Tavern
 Top Mont Co. Rd G + Lex

955.23 ✓

104+80

50.8 ✓

105

50.8 ✓

+57 ± Co. Rd "G"

51.21 ✓

+74

50.9 ✓

+78

50.8 ✓

106

50.4 ✓

+45

49.6 ✓

107

48.5 ✓

$$\begin{array}{ccccccc} \frac{6.4}{100} & \frac{6.1}{27} & \frac{6.6}{26-24} & \frac{4.8}{19} & \frac{4.7}{10} & 4.4 & \frac{4.6}{10} & \frac{3.0}{49} & \frac{1.7}{58} \end{array}$$

TAVERA Floor +0.14

$$\begin{array}{ccccccc} \frac{5.7}{100} & \frac{6.2}{24} & \frac{6.5}{23-22} & \frac{4.7}{17} & \frac{4.6}{9} & 4.4 & \frac{4.5}{11} & \frac{2.6}{64} \end{array}$$

edgeBHy Conc Gas Per 2.26

FL. Culv 7.32 FL. Culv 6.27

$$\begin{array}{ccccccc} \frac{9.34}{300} & \frac{8.23}{200} & \frac{6.65}{100} & \frac{5.82}{64} & 4.02 & \frac{3.95}{57} & \frac{3.43}{100} & \frac{3.08}{200} & \frac{2.97}{300} \end{array}$$

$$\begin{array}{ccccccc} \frac{7.6}{100} & \frac{6.2}{39} & \frac{4.6}{12} & 4.3 & \frac{4.5}{10} & \frac{4.8}{34} & \frac{4.1}{100} \end{array}$$

$$\begin{array}{ccccccc} \frac{5.7}{100} & \frac{4.1}{38} & \frac{6.0}{32} & \frac{4.8}{12} & 4.4 & \frac{4.6}{10} & \frac{4.8}{32} & \frac{3.8}{33} & \frac{3.2}{100} \end{array}$$

$$\begin{array}{ccccccc} \frac{6.4}{100} & \frac{3.8}{29} & \frac{6.2}{23} & \frac{5.5}{12} & 4.8 & \frac{5.1}{12} & \frac{5.2}{20} & \frac{5.7}{23-26} & \frac{2.7}{31} & \frac{3.6}{88} & \frac{2.8}{100} \end{array}$$

$$\begin{array}{ccccccc} \frac{9.4}{100} & \frac{6.4}{69} & \frac{2.6}{29} & \frac{6.2}{23-11} & 5.6 & \frac{5.9}{11} & \frac{6.2}{17} & \frac{6.8}{19-22} & \frac{6.6}{25} & \frac{3.5}{30} & \frac{3.6}{58} & \frac{6.9}{100} \end{array}$$

$$\begin{array}{ccccccc} \frac{11.7}{100} & \frac{7.4}{75} & \frac{5.2}{25} & \frac{7.5}{21} & \frac{7.1}{10} & 6.7 & \frac{7.1}{16} & \frac{7.2}{17} & \frac{8.2}{19-24} & \frac{5.1}{30} & \frac{8.2}{100} \end{array}$$

Sta

+

x

955.23 ✓

107 +35

47.6 ✓

108

45.6 ✓

+65

43.3 ✓

○

0.23

942.10 ✓

13.36

941.87 ✓

109

41.9 ✓

+60 ✓

39.6 ✓

110

38.3 ✓

+65

35.6 ✓

○

0.39

940.04 ✓

2.45

939.65 ✓

$$\frac{9.9}{100} \quad \frac{7.4}{47} \quad \frac{6.2}{25} \quad \frac{8.5}{20} \quad \frac{8.0}{10} \quad 7.6 \quad \frac{7.7}{12} \quad \frac{8.2}{17} \quad \frac{9.0}{11} \quad \frac{7.3}{24} \quad \frac{7.2}{29} \quad \frac{9.2}{100}$$

$$\frac{11.0}{100} \quad \frac{10.4}{70} \quad \frac{9.0}{25} \quad \frac{10.4}{22} \quad \frac{10.1}{17} \quad 9.6 \quad \frac{10.1}{13} \quad \frac{10.3}{17} \quad \frac{11.4}{22-24} \quad \frac{8.4}{29} \quad \frac{9.5}{77} \quad \frac{11.0}{100}$$

$$\frac{12.8}{100} \quad \frac{13.3}{26-19} \quad \frac{12.4}{14} \quad \frac{12.2}{9} \quad 11.9 \quad \frac{12.4}{13} \quad \frac{12.6}{16} \quad \frac{13.6}{19-70} \quad \frac{13.0}{100}$$

$$\begin{array}{c} H_0 \\ 06 \\ 62 \end{array} \quad \frac{1.1}{22} \quad \frac{2.3}{20} \quad \frac{0.8}{16} \quad \frac{0.6}{9} \quad 0.2 \quad \frac{0.7}{13} \quad \frac{1.1}{18} \quad \frac{2.7}{23} \quad \frac{3.1}{58} \quad \frac{2.4}{100}$$

Floor H₀ + 1.80

$$\frac{6.0}{100} \quad \frac{5.2}{20} \quad \frac{3.2}{16} \quad \frac{2.8}{8} \quad 2.5 \quad \frac{2.8}{13-17} \quad \frac{4.7}{20-76} \quad \frac{3.6}{100}$$

$$\frac{6.6}{100} \quad \frac{5.8}{31} \quad \frac{4.0}{7} \quad 3.8 \quad \frac{4.1}{13} \quad \frac{4.4}{30} \quad \frac{5.8}{23-24} \quad \frac{5.2}{26} \quad \frac{5.0}{53} \quad \frac{1.2}{100}$$

$$\frac{6.2}{100} \quad \frac{5.9}{45} \quad \frac{6.2}{26} \quad \frac{7.9}{21-17} \quad \frac{7.3}{18} \quad \frac{6.8}{7} \quad 6.5 \quad \frac{6.8}{13} \quad \frac{7.4}{18} \quad \frac{4.1}{31} \quad \frac{2.3}{100}$$

Floor House
+ 1.10

Top Rock @ Ent to

Sta

+

π

-

940.04 ✓

111

34.1 ✓

+35

32.7 ✓

+90

30.7 ✓

112

30.4 ✓

+35

29.1 ✓

+47

28.7 ✓

113

26.6 ✓

114

22.3 ✓

$$\frac{1.6}{100} \quad \frac{2.3}{56} \quad \frac{4.6}{27} \quad \frac{7.3}{23} \quad \frac{6.9}{17} \quad \frac{6.2}{8} \quad 5.9 \quad \frac{6.2}{14} \quad \frac{6.8}{18} \quad \frac{3.3}{29} \quad \frac{1.0}{100}$$

$$\frac{4.1}{100} \quad \frac{2.4}{76} \quad \frac{2.1}{47} \quad \frac{4.0}{28} \quad \frac{8.5}{21} \quad \frac{7.8}{8} \quad 7.3 \quad \frac{7.7}{14} \quad \frac{8.2}{20} \quad \frac{5.3}{28} \quad \frac{4.6}{61} \quad \frac{5.1}{100}$$

$$\frac{4.9}{100} \quad \frac{5.1}{65} \quad \frac{6.6}{63} \quad \frac{6.3}{52} \quad 39-33 \quad \frac{1.7}{19} \quad \frac{10.2}{9} \quad \frac{9.7}{9} \quad 9.3 \quad \frac{9.7}{14} \quad \frac{11.2}{21} \quad \frac{10.0}{26} \quad \frac{11.5}{34} \quad \frac{12.8}{56} \quad \frac{11.4}{100}$$

$$\frac{7.1}{100} \quad \frac{4.1}{71} \quad \frac{6.1}{68} \quad \frac{6.0}{48} \quad \frac{6.8}{36} \quad \frac{5.6}{30} \quad \frac{10.5}{19} \quad \frac{10.0}{8} \quad 9.6 \quad \frac{10.1}{14} \quad \frac{11.6}{20-22} \quad \frac{10.0}{25} \quad \frac{12.1}{37} \quad \frac{12.9}{58} \quad \frac{12.5}{100}$$

$$\frac{6.2}{100} \quad \frac{4.8}{79} \quad \frac{1.2}{44} \quad \frac{9.2}{29} \quad \frac{11.5}{23} \quad \frac{11.2}{8} \quad 10.9 \quad \frac{11.3}{13} \quad \frac{13.3}{22} \quad \frac{9.6}{28} \quad \frac{11.3}{34} \quad \frac{12.1}{45} \quad \frac{12.9}{100}$$

$$\frac{6.1}{100} \quad \frac{1.4}{39} \quad \frac{11.1}{24} \quad \frac{11.7}{9} \quad 11.3 \quad \frac{11.8}{13} \quad \frac{13.7}{20} \quad \frac{10.0}{27} \quad \frac{11.0}{33} \quad \frac{13.5}{58} \quad \frac{14.5}{100}$$

$$\frac{4.0}{100} \quad \frac{2.3}{36} \quad \frac{4.1}{19} \quad \frac{13.8}{8} \quad 13.4 \quad \frac{13.9}{13} \quad \frac{14.3}{15} \quad \frac{15.1}{21} \quad \frac{15.0}{23} \quad \frac{13.5}{28} \quad \frac{17.4}{82} \quad \frac{20.0}{112}$$

$$\frac{5.8}{100} \quad \frac{5.3}{36}$$

17.8

Sta

+

x

-

940.04✓

0

0.37

926.90✓

13.51

926.53✓

114

22.3✓

115

17.9✓

+25

16.9✓

0

3.68

918.45✓

12.13

914.77✓

+65

15.5✓

116

14.0✓

117

09.8✓

09.9

0

0.95

907.21✓

12.19

906.26✓

$$\frac{5.6}{21.8} \quad \frac{5.3}{16} \quad \frac{5.1}{8} \quad 4.6 \quad \frac{5.0}{13} \quad \frac{5.1}{16} \quad \frac{8.0}{28} \quad \frac{8.5}{34-87} \quad \frac{10.0}{100} \quad \frac{13.2}{150}$$

$$\frac{2.6}{82} \quad \frac{6.8}{37} \quad \frac{7.8}{32} \quad \frac{10.0}{30} \quad \frac{11.1}{28-22} \quad \frac{9.3}{18} \quad \frac{9.1}{8} \quad 9.0 \quad \frac{9.4}{12} \quad \frac{9.7}{16} \quad \frac{13.4}{24} \quad \frac{15.7}{33} \quad \frac{15.0}{47} \quad \frac{15.9}{100} \quad \frac{3.5}{150}$$

$$\frac{55}{150}$$

$$\frac{0.0}{100} \quad \frac{2.0}{42} \quad \frac{6.8}{62} \quad \frac{9.4}{35} \quad \frac{11.1}{30} \quad \frac{14.7}{21} \quad \frac{10.4}{15} \quad \frac{10.2}{7} \quad 10.0 \quad \frac{10.6}{13} \quad \frac{10.9}{15} \quad \frac{17.8}{26} \quad \frac{19.5}{42} \quad \frac{19.1}{62} \quad \frac{19.8}{83} \quad \frac{20.5}{100} \quad \frac{55}{135}$$

$$\frac{55}{175}$$

$$\frac{55}{100} + \frac{4.2}{62} + \frac{1.4}{36} \quad \frac{0.2}{32} \quad \frac{5.7}{27-23} \quad \frac{3.7}{19} \quad \frac{3.3}{9} \quad 3.0 \quad \frac{3.5}{12} \quad \frac{3.9}{15} \quad \frac{12.0}{26} \quad \frac{16.0}{46} \quad \frac{19.5}{88} \quad \frac{20.5}{100}$$

$$\frac{55}{200} \quad \frac{10.2}{100} + \frac{1.9}{38} \quad \frac{7.3}{26-22} \quad \frac{5.2}{18} \quad \frac{5.0}{8} \quad 4.5 \quad \frac{4.8}{12} \quad \frac{5.2}{15} \quad \frac{13.0}{26} \quad \frac{19.5}{60} \quad \frac{20.5}{100}$$

$$\frac{55}{150} + \frac{2.8}{100} + \frac{1.9}{90} \quad \frac{0.2}{36} \quad \frac{11.0}{21-18} \quad \frac{9.6}{16} \quad \frac{9.0}{8} \quad 8.7 \quad \frac{9.2}{12} \quad \frac{9.5}{17} \quad \frac{16.5}{30} \quad \frac{17.4}{37} \quad \frac{24.8}{82} \quad \frac{25.3}{100}$$

Sta + π -

907.21 ✓

118

05.7 ✓

+75

02.7 ✓

B.M.

10.88

896.33 ✓

964.6

+90

02.2 ✓

119

01.8 ✓

120

98.4 ✓

+50

96.4 ✓

121

95.1 ✓

○

4.35

899.47 ✓

12.09

895.92 ✓

$\frac{+10.5}{100}$ $\frac{+11.6}{35}$ $\frac{3.2}{22}$ $\frac{2.1}{18}$ $\frac{1.8}{8}$ 1.5 $\frac{1.9}{12}$ $\frac{2.3}{15}$ $\frac{7.1}{22}$ $\frac{11.8}{53}$ $\frac{13.6}{70}$ $\frac{14.4}{100}$

$\frac{55}{130}$ $\frac{+6.1}{100}$ $\frac{5.2}{33}$ $\frac{5.5}{19}$ $\frac{4.7}{8}$ 4.5 $\frac{4.9}{12}$ $\frac{5.0}{15}$ $\frac{10.8}{25}$ $\frac{12.7}{74}$ $\frac{12.4}{100}$

3PK in 12" Oak 60' Rt Sta 118+75

$\frac{3.1}{100}$ $\frac{6.0}{40}$ $\frac{5.5}{20}$ $\frac{5.2}{18}$ $\frac{5.0}{8}$ $\frac{5.4}{12}$ $\frac{5.6}{14}$ $\frac{10.5}{25}$ $\frac{13.7}{71}$ $\frac{12.7}{100}$

$\frac{4.2}{100}$ $\frac{5.6}{100}$ $\frac{6.8}{33}$ $\frac{5.8}{16}$ $\frac{5.6}{8}$ $\frac{5.4}{12}$ $\frac{5.7}{15}$ $\frac{6.0}{15}$ $\frac{11.1}{26}$ $\frac{14.0}{70}$ $\frac{13.2}{100}$

$\frac{7.8}{100}$ $\frac{10.5}{80}$ $\frac{10.0}{33}$ $\frac{9.2}{8}$ 8.8 $\frac{9.2}{13}$ $\frac{9.5}{16}$ $\frac{14.0}{26}$ $\frac{14.5}{100}$

10.8

$\frac{13.8}{100}$ $\frac{14.4}{31}$ $\frac{14.2}{23}$ $\frac{12.9}{15}$ $\frac{12.4}{8}$ 12.1 $\frac{12.5}{13}$ $\frac{13.1}{17}$ $\frac{14.4}{20-22}$ $\frac{13.8}{23}$ $\frac{14.4}{32-100}$

Sta

+

T

-

899.47 ✓

122

94.7 ✓

123

94.7 ✓

124

95.0 ✓

BM.

5.26

898.28

6.38

893.09 ✓ 893.02

125

93.6 ✓

126

92.9 ✓

127

92.8 ✓

128

93.0 ✓

$$\frac{6.1}{100} \quad \frac{6.6}{32-22} \quad \frac{5.5}{16} \quad \frac{4.9}{8} \quad 4.8 \quad \frac{5.2}{13} \quad \frac{5.9}{18} \quad \frac{6.7}{21} \quad \frac{7.2}{100}$$

$$\frac{6.1}{100} \quad \frac{7.1}{35} \quad \frac{7.2}{23} \quad \frac{7.1}{20} \quad \frac{5.5}{14} \quad \frac{5.1}{8} \quad 4.8 \quad \frac{5.1}{14} \quad \frac{5.6}{18} \quad \frac{6.5}{21-24} \quad \frac{7.0}{100}$$

$$\frac{4.2}{100} \quad \frac{6.5}{24} \quad \frac{6.8}{12-21} \quad \frac{4.9}{14} \quad \frac{4.7}{7} \quad 4.5 \quad \frac{4.8}{14} \quad \frac{5.2}{23} \quad \frac{6.8}{27} \quad \frac{7.2}{62-100}$$

SpK in TP. $G^2 + \text{Lex.}$

$$\frac{6.6}{100-22} \quad \frac{5.3}{15} \quad \frac{4.9}{8} \quad 4.7 \quad \frac{4.8}{14} \quad \frac{5.3}{18} \quad \frac{5.9}{20-22} \quad \frac{5.4}{23-25} \quad \frac{6.2}{28} \quad \frac{6.7}{48} \quad \frac{7.2}{100}$$

$$\frac{7.2}{100} \quad \frac{7.1}{34} \quad \frac{7.1}{16} \quad \frac{6.0}{12} \quad \frac{5.6}{7} \quad 5.4 \quad \frac{5.7}{15} \quad \frac{6.0}{19} \quad \frac{6.4}{20-21} \quad \frac{5.9}{22} \quad \frac{6.6}{29-50} \quad \frac{6.7}{100}$$

$$\frac{6.8}{100} \quad \frac{7.0}{34} \quad \frac{7.2}{17} \quad \frac{6.1}{11} \quad \frac{5.7}{7} \quad 5.5 \quad \frac{5.7}{15} \quad \frac{6.1}{23} \quad \frac{6.5}{25} \quad \frac{6.3}{50} \quad \frac{6.0}{100}$$

$$\frac{7.6}{100} \quad \frac{7.2}{34} \quad \frac{7.1}{15} \quad \frac{6.0}{11} \quad \frac{5.6}{7} \quad 5.3 \quad \frac{5.6}{15} \quad \frac{5.9}{24} \quad \frac{6.9}{26-27} \quad \frac{6.7}{100}$$

Sta

+

x

-

898.28 ✓

129

93.4 ✓

130

92.9 ✓

131

92.3 ✓

131+89

92.6 ✓

BM.

out.

5.77

892.51

132

92.6 ✓

tot

BM

5A7

898.49 ✓

526

92.6 ✓

893.02

$\frac{7.0}{100}$ $\frac{6.6}{34}$ $\frac{6.9}{17}$ $\frac{5.5}{12}$ $\frac{5.2}{7}$ $\frac{5.2}{17}$ $\frac{5.6}{20}$ $\frac{5.5}{26}$ $\frac{6.5}{27}$ $\frac{6.7}{52}$ $\frac{6.4}{100}$

$\frac{6.9}{100}$ $\frac{7.0}{34}$ $\frac{7.2}{16}$ $\frac{6.1}{12}$ $\frac{5.5}{7}$ $\frac{5.6}{16}$ $\frac{6.4}{23}$ $\frac{5.9}{28}$ $\frac{7.0}{31}$ $\frac{7.2}{59}$ $\frac{6.9}{100}$

$\frac{7.6}{100}$ $\frac{7.5}{34}$ $\frac{7.7}{17}$ $\frac{6.7}{12}$ $\frac{6.3}{8}$ $\frac{6.4}{16}$ $\frac{6.6}{18}$ $\frac{7.2}{21-23}$ $\frac{6.9}{25}$ $\frac{6.3}{29}$ $\frac{7.2}{31}$ $\frac{7.7}{73}$

S.E. Colv FL 8.27 } Thru G²
 NE " FL 8.55 }

FL Colv 8.67 Thru Lev.

FL Colv 8.40

O.T. D+ 35' 8.1

" " 100' 8.2

" " 200' 8.7

$\frac{5.70}{13}$ $\frac{5.68}{100}$ $\frac{5.82}{200}$ $\frac{4.89}{300}$ $\frac{4.61}{300}$

Top Mont G² & Lex

$\frac{7.4}{100}$ $\frac{7.0}{28}$ $\frac{6.7}{13}$ $\frac{6.4}{12}$ $\frac{6.1}{8}$ $\frac{5.72}{13}$ $\frac{5.78}{65}$ $\frac{6.13}{100}$

$\frac{7.4}{100}$ $\frac{7.0}{29}$ $\frac{6.4}{12}$ $\frac{6.1}{8}$ $\frac{5.7}{13}$ $\frac{5.9}{29}$ $\frac{6.2}{32}$ $\frac{6.7}{39}$ $\frac{8.0}{41}$ $\frac{7.0}{61-100}$

Spk in T.P. SW Cor G² & Lex

Sta

+

x

-

898.19 ✓

133

92.9 ✓

134

94.0 ✓

135

93.5 ✓

136

93.8 ✓

137

95.1 ✓

138

97.2 ✓

0

10.47

908.16 ✓

0.80

877.69 ✓

139

99.2 ✓

+ 40

99.9 ✓

140

00.9 ✓

$$\frac{8.1}{100} \quad \frac{7.8}{32} \quad \frac{7.4}{17} \quad \frac{6.7}{15} \quad \frac{5.9}{10} \quad 5.6 \quad \frac{5.9}{13} \quad \frac{6.9}{27} \quad \frac{7.6}{32-81} \quad \frac{7.4}{100}$$

$$\frac{7.8}{100} \quad \frac{7.4}{40} \quad \frac{7.0}{16} \quad \frac{5.6}{13} \quad \frac{4.9}{10} \quad 4.5 \quad \frac{4.8}{12} \quad \frac{5.4}{17} \quad \frac{6.3}{20} \quad \frac{6.4}{28} \quad \frac{7.7}{33} \quad \frac{7.6}{100}$$

$$\frac{8.0}{100} \quad \frac{7.6}{40} \quad \frac{7.5}{16} \quad \frac{6.0}{13} \quad \frac{5.4}{9} \quad 5.0 \quad \frac{5.1}{11} \quad \frac{6.5}{28} \quad \frac{7.9}{33} \quad \frac{7.6}{100}$$

$$\frac{8.1}{100} \quad \frac{7.6}{48} \quad \frac{7.0}{16} \quad \frac{5.5}{12} \quad \frac{5.0}{9} \quad 4.7 \quad \frac{4.8}{11} \quad \frac{5.7}{18} \quad \frac{6.6}{22} \quad \frac{6.0}{26} \quad \frac{7.5}{34} \quad \frac{7.2}{100}$$

$$\frac{7.9}{200} \quad \frac{7.7}{100} \quad \text{F.L. Colv. } 8.29$$

$$\text{F.L. Colv. } 7.39$$

$$\frac{8.1}{100} \quad \frac{7.5}{48} \quad \frac{6.6}{19} \quad \frac{4.4}{14} \quad \frac{3.8}{9} \quad 3.4 \quad \frac{3.7}{11} \quad \frac{4.5}{17} \quad \frac{6.0}{21-24} \quad \frac{5.4}{26} \quad \frac{5.9}{32} \quad \frac{7.3}{36} \quad \frac{6.8}{43} \quad \frac{5.1}{81}$$

$$\frac{5.0}{100}$$

$$\frac{8.4}{100} \quad \frac{7.8}{68} \quad \frac{7.5}{52} \quad \frac{5.8}{23} \quad \frac{2.5}{14} \quad \frac{1.7}{9} \quad 1.3 \quad \frac{1.5}{11} \quad \frac{2.3}{19} \quad \frac{3.4}{24} \quad \frac{3.7}{31} \quad \frac{4.4}{35-82} \quad \frac{4.0}{100}$$

$$\frac{14.6}{100} \quad \frac{14.4}{80} \quad \frac{14.7}{21} \quad \frac{10.2}{16} \quad \frac{9.4}{10} \quad 9.0 \quad \frac{9.2}{11} \quad \frac{10.4}{28} \quad \frac{11.3}{32} \quad \frac{9.6}{72} \quad \frac{9.3}{100}$$

$$\frac{12.8}{100} \quad \frac{11.4}{50-23} \quad \frac{9.9}{17} \quad \frac{8.8}{10} \quad 8.3 \quad \frac{8.6}{11} \quad \frac{9.3}{30} \quad \frac{9.4}{46} \quad \frac{7.6}{73} \quad \frac{7.3}{100}$$

$$\frac{13.7}{100} \quad \frac{10.0}{56} \quad \frac{9.7}{33} \quad \frac{10.0}{23} \quad \frac{8.6}{17} \quad \frac{7.7}{9} \quad 7.3 \quad \frac{7.5}{11} \quad \frac{8.7}{23-28} \quad \frac{6.5}{35} \quad \frac{3.6}{74} \quad \frac{2.8}{100}$$

Sta

+

x

-

908.16

141

02.8 ✓

142

04.3 ✓

+50

05.1 ✓

143

06.2 ✓

0

11.15

918.20

1.11

907.05 ✓

+75

07.4 ✓

+85

07.5 ✓

+98

✓

07.7 ✓

144

07.8 ✓

$$\frac{13.0}{100} \frac{10.9}{60} \frac{8.1}{27} \frac{6.6}{18} \frac{5.7}{9} 5.4 \frac{5.6}{11} \frac{7.7}{22} \frac{7.2}{28} \frac{4.5}{36} \frac{0.9}{59} \frac{+0.5}{85} \frac{00}{100}$$

$$\frac{13.5}{100} \frac{12.9}{82} \frac{10.5}{58} \frac{6.9}{27} \frac{5.2}{19} \frac{4.2}{9} 3.9 \frac{4.2}{11} \frac{4.9}{32} \frac{2.4}{36} \frac{00}{58} \frac{+1.8}{100}$$

3.1

$$\frac{11.6}{100} \frac{10.1}{85} \frac{5.3}{45} \frac{4.5}{28} \frac{3.2}{18} \frac{2.3}{10} 2.0 \frac{2.3}{11} \frac{3.1}{28} \frac{00}{33} \frac{+1.7}{36} \frac{+4.5}{80} \frac{+5.0}{100}$$

$$\frac{18.5}{100} \frac{13.7}{57} \frac{12.2}{33} \frac{13.5}{31} \frac{13.2}{21} \frac{12.2}{17} \frac{11.2}{10} 10.8 \frac{11.1}{11} \frac{10.5}{27} \frac{7.3}{36} \frac{4.2}{53} \frac{0.6}{100}$$

$$\frac{18.5}{10} \frac{14.4}{64} \frac{11.6}{33} \frac{13.1}{30} \frac{11.9}{21} \frac{11.1}{17} \frac{11.1}{10} 10.7 \frac{10.8}{9} \frac{10.1}{36} \frac{5.9}{74} \frac{3.9}{100}$$

$$\frac{18.8}{100} \frac{13.1}{61} \frac{11.0}{33} \frac{12.9}{30} \frac{12.4}{21} \frac{11.7}{17} \frac{10.9}{10} 10.5 \frac{10.5}{9} \frac{7.3}{39} \frac{7.6}{66} \frac{4.1}{100}$$

10.4

Sta + π -
 918.20

144+05 07.8 ✓

+50 08.2 ✓

145 08.5 ✓

+50 08.3 ✓

146 08.0 ✓

+20 07.9 ✓

147 07.1 ✓

0 A.27 912.04 ✓ 10.43 907.97 ✓

B.M. 9.73 912.04 ✓ 9.73 902.31 ✓ 902.42

$\frac{18.8}{100}$ $\frac{13.2}{64}$ $\frac{10.5}{33}$ $\frac{12.8}{30}$ $\frac{12.1}{20}$ $\frac{11.5}{18}$ $\frac{10.8}{11}$ 10.4 $\frac{10.4}{9}$ $\frac{9.3}{31}$ $\frac{7.0}{35}$ $\frac{5.8}{50}$ $\frac{2.4}{57}$ $\frac{0.2}{100}$

10.0

$\frac{20.5}{100}$ $\frac{16.4}{75}$ $\frac{9.5}{34}$ $\frac{11.9}{29}$ $\frac{11.0}{23}$ $\frac{10.2}{17}$ $\frac{10.2}{11}$ 9.7 $\frac{10.0}{10}$ $\frac{10.3}{25}$ $\frac{6.6}{34}$ $\frac{6.4}{43}$ $\frac{1.7}{50}$ $\frac{0.0}{83}$ $\frac{+1.0}{100}$

9.9

$\frac{24.0}{100}$ $\frac{20.6}{70}$ $\frac{13.9}{28}$ $\frac{11.7}{22}$ $\frac{11.1}{17}$ $\frac{10.7}{11}$ 10.2 $\frac{10.6}{10}$ $\frac{9.9}{26}$ $\frac{5.7}{33}$ $\frac{5.3}{38}$ $\frac{2.6}{44}$ $\frac{0.4}{69}$ $\frac{+0.5}{100}$

$\frac{24.0}{100}$ $\frac{20.6}{70}$ $\frac{14.1}{28}$ $\frac{11.8}{22}$ $\frac{11.1}{17}$ $\frac{10.8}{11}$ 10.3 $\frac{10.6}{9}$ $\frac{10.4}{23}$ $\frac{5.0}{32}$ $\frac{2.3}{56}$ $\frac{0.0}{84}$ $\frac{+0.5}{100}$

$\frac{25.0}{100}$ $\frac{21.0}{49}$ $\frac{18.3}{31}$ $\frac{12.6}{21}$ $\frac{11.7}{12}$ 11.1 $\frac{11.3}{8}$ $\frac{11.7}{17}$ $\frac{10.6}{25}$ $\frac{6.6}{33}$ $\frac{3.0}{76}$ $\frac{1.9}{100}$

S.P.K. in 12" Oak 60' Rt Sta 145+35

Sta

+

 π

-

912.04 ✓

148

06.5 ✓

+80

06.4 ✓

149

06.4 ✓

150

07.3 ✓

○

11.25

920.36 ✓

2.93

909.11 ✓

151

09.1 ✓

152

11.2 ✓

+50

12.5 ✓

$\frac{16.5}{100}$ $\frac{16.0}{62}$ $\frac{12.0}{27}$ $\frac{7.0}{19}$ $\frac{5.8}{10}$ 5.5 $\frac{5.7}{9}$ $\frac{6.0}{25}$ $\frac{5.0}{29}$ $\frac{2.4}{82}$ $\frac{1.1}{100}$

$\frac{17.1}{100}$ $\frac{14.3}{60}$ $\frac{14.05}{37}$ $\frac{11.4}{28}$ $\frac{6.9}{19}$ $\frac{6.0}{11}$ 5.6 $\frac{5.7}{9}$ $\frac{6.3}{16}$ $\frac{8.56}{19}$ $\frac{7.7}{21}$ $\frac{7.2}{25}$ $\frac{6.0}{27}$ $\frac{2.5}{83}$ $\frac{0.7}{100}$

$\frac{16A}{100}$ $\frac{15.3}{67}$ $\frac{11.0}{26}$ $\frac{7.2}{19}$ $\frac{6.0}{11}$ 5.6 $\frac{5.7}{9}$ $\frac{6.2}{16}$ $\frac{7.6}{21-23}$ $\frac{5.5}{26}$ $\frac{3.8}{65}$ $\frac{1.2}{100}$

$\frac{16.5}{100}$ $\frac{15.8}{58}$ $\frac{11.7}{29}$ $\frac{6.0}{14}$ $\frac{5.2}{11}$ 4.7 $\frac{4.8}{9}$ $\frac{5.6}{4}$ $\frac{6.0}{22-23}$ $\frac{5.1}{27}$ $\frac{2.4}{73}$ $\frac{1.0}{100}$

Nail in Pave Sta 151 + 00

$\frac{25.0}{100}$ $\frac{22.1}{74}$ $\frac{16.5}{33}$ $\frac{12.9}{22}$ $\frac{11.7}{12}$ 11.3 $\frac{11.4}{9}$ $\frac{11.5}{25}$ $\frac{9.8}{28}$ $\frac{8.3}{47}$ $\frac{2.4}{100}$

$\frac{16.7}{100}$ $\frac{9.7}{64}$ $\frac{6.2}{28}$ $\frac{10.7}{14}$ $\frac{10.3}{16}$ $\frac{7.6}{11}$ 9.2 $\frac{9.4}{10}$ $\frac{9.3}{26}$ $\frac{6.3}{30}$ $\frac{5.7}{34}$ $\frac{2.1}{40}$ $\frac{1.6}{100}$

7.9

Sta

+

 π

-

920.36 ✓

153

13.9 ✓

+50

15.1 ✓

0

6.78

922.83 ✓ 4.31

916.05 ✓

154

16.0 ✓

+50

16.8 ✓

155

17.5 ✓

+50

17.7 ✓

156

✓

17.7 ✓

$\frac{8.8}{100}$ $\frac{3.4}{62}$ $\frac{2.8}{28}$ $\frac{8.6}{21-19}$ $\frac{7.6}{16}$ $\frac{6.8}{11}$ 65 $\frac{6.7}{9}$ $\frac{6.6}{17}$ $\frac{7.5}{18-23}$ $\frac{3.6}{28-30}$ $\frac{2.0}{33}$ $\frac{0.7}{88}$ $\frac{+0.5}{100}$

$\frac{5.6}{100}$ $\frac{1.3}{66}$ $\frac{0.6}{31}$ $\frac{7.0}{10-18}$ $\frac{6.2}{15}$ $\frac{5.7}{12}$ 53 $\frac{5.4}{9-16}$ $\frac{6.3}{18-23}$ $\frac{1.3}{30}$ $\frac{+1.0}{100}$

$\frac{10.0}{100}$ $\frac{4.4}{66}$ $\frac{3.4}{28}$ $\frac{8.6}{22-19}$ $\frac{7.8}{17}$ $\frac{7.3}{11}$ 68 $\frac{6.9}{10-16}$ $\frac{8.0}{18-22}$ $\frac{4.0}{28}$ $\frac{2.6}{87}$ $\frac{2.0}{100}$

6.0³

$\frac{11.6}{100}$ $\frac{7.6}{61}$ $\frac{6.6}{59}$ $\frac{6.3}{28}$ $\frac{7.6}{26-22}$ $\frac{6.5}{18}$ $\frac{5.8}{11}$ 53 $\frac{5.6}{10}$ $\frac{5.9}{16}$ $\frac{6.8}{19-23}$ $\frac{5.2}{27}$ $\frac{4.2}{62}$ $\frac{2.0}{100}$

51

$\frac{13.1}{100}$ $\frac{11.1}{80}$ $\frac{9.6}{51}$ $\frac{9.1}{41}$ $\frac{7.8}{21}$ $\frac{6.2}{17}$ $\frac{5.4}{11}$ 51 $\frac{5.3}{10}$ $\frac{5.6}{17}$ $\frac{6.5}{20}$ $\frac{6.7}{32}$ $\frac{5.1}{74}$ $\frac{3.8}{100}$

Sta

+

 π

-

922.83[✓]

157

17.8[✓]

B.M.

3.91

918.92[✓]

919.00

158

17.6[✓]

B.M.

5.24

922.86[✓]

5.24

917.59[✓]

917.62

159

17.9[✓]

160

17.5[✓]

161

16.1[✓]

①

1.65

917.67[✓]

6.84

916.02[✓]

162

14.9[✓]

$\frac{12.6}{100}$ $\frac{8.1}{52}$ $\frac{5.9}{29}$ $\frac{7.1}{26-19}$ $\frac{6.0}{16}$ $\frac{5.3}{10}$ 5.0 $\frac{5.2}{10}$ $\frac{4.8}{20}$ $\frac{6.0}{22}$ $\frac{6.1}{33}$ $\frac{5.8}{44}$ $\frac{4.6}{100}$

SpK in 18" D.K. 60' Rt. Sta 157+51

$\frac{7.5}{100}$ $\frac{6.1}{40}$ $\frac{5.9}{27}$ $\frac{6.3}{25-18}$ $\frac{5.8}{15}$ $\frac{5.5}{10}$ 5.2 $\frac{5.5}{12}$ $\frac{5.7}{16}$ $\frac{6.2}{24}$ $\frac{5.2}{28}$ $\frac{4.4}{60}$ $\frac{4.0}{100}$

Floor Ht 1.45

Top Man F I.M. So Co. Rd I" Sta 158+20.5

$\frac{5.9}{100}$ $\frac{5.4}{64}$ $\frac{5.2}{28}$ $\frac{6.1}{27-17}$ $\frac{5.0}{14}$ $\frac{5.2}{10}$ 5.0 $\frac{5.2}{11}$ $\frac{5.4}{15}$ $\frac{6.1}{17-23}$ $\frac{4.6}{28}$ $\frac{4.8}{75}$ $\frac{5.1}{100}$

$\frac{4.8}{100}$ $\frac{5.4}{30}$ $\frac{6.9}{21-17}$ $\frac{5.6}{13-9}$ 5.4 $\frac{5.6}{11}$ $\frac{6.0}{16}$ $\frac{6.3}{23}$ $\frac{4.7}{27}$ $\frac{5.4}{77}$ $\frac{5.7}{100}$

$\frac{6.6}{100}$ $\frac{6.4}{43}$ $\frac{7.8}{23-18}$ $\frac{7.4}{15}$ $\frac{6.9}{9}$ 6.8 $\frac{7.0}{11}$ $\frac{7.1}{15}$ $\frac{7.8}{17-22}$ $\frac{6.7}{25}$ $\frac{9.0}{60}$ $\frac{13.1}{100}$

$\frac{1.3}{100}$ $\frac{2.0}{41}$ $\frac{4.0}{23-18}$ $\frac{3.4}{15}$ $\frac{3.1}{9}$ 2.8 $\frac{3.1}{11}$ $\frac{3.2}{15}$ $\frac{4.9}{19-22}$ $\frac{3.9}{25}$ $\frac{4.7}{32}$ $\frac{8.3}{61}$ $\frac{9.4}{100}$

Sta

+

 π

-

917.67[✓]

162+65

13.9[✓]

163

13.3[✓]

+50

12.7[✓]

164

12.5[✓]

+35

12.6[✓]

165

12.5[✓]

166

12.7[✓]

167

12.9[✓]

$\frac{1.7}{100}$ $\frac{3.7}{42}$ $\frac{5.2}{26-19}$ $\frac{4.3}{75}$ $\frac{4.0}{9}$ 3.8 $\frac{4.1}{11}$ $\frac{4.3}{16}$ $\frac{9.6}{26}$ $\frac{10.4}{33}$ $\frac{11.7}{56}$ $\frac{9.4}{100}$

$\frac{2.4}{100}$ $\frac{3.2}{81}$ $\frac{7.9}{24}$ $\frac{7.2}{19}$ $\frac{4.9}{16}$ $\frac{4.6}{8}$ 4.4 $\frac{4.7}{11}$ $\frac{5.2}{17}$ $\frac{10.9}{26}$ $\frac{11.8}{33-50}$ $\frac{8.4}{100}$

$\frac{5.3}{100}$ $\frac{10.4}{42}$ $\frac{9.5}{21}$ $\frac{5.5}{15}$ $\frac{5.2}{9}$ 5.0 $\frac{5.2}{11}$ $\frac{5.6}{19}$ $\frac{9.6}{27}$ $\frac{10.3}{33}$ $\frac{8.8}{69}$ $\frac{6.5}{100}$

$\frac{5.3}{200}$ $\frac{8.4}{100}$ $\frac{11.5}{55}$ $\frac{9.7}{22}$ $\frac{5.9}{15}$ $\frac{5.4}{9}$ 5.2 $\frac{5.3}{10}$ $\frac{5.9}{20}$ $\frac{7.8}{23}$ $\frac{7.9}{29}$ $\frac{5.8}{67}$ $\frac{4.4}{100}$

$\frac{10.0}{100}$ $\frac{11.6}{72}$ $\frac{9.1}{24}$ $\frac{5.7}{15}$ $\frac{5.3}{10}$ 5.1 $\frac{5.3}{10}$ $\frac{5.7}{17}$ $\frac{6.4}{19-22}$ $\frac{6.0}{35}$ $\frac{4.4}{65}$ $\frac{4.0}{100}$

$\frac{11.7}{100}$ $\frac{7.1}{24}$ $\frac{5.4}{15}$ $\frac{5.3}{9}$ 5.2 $\frac{5.2}{10}$ $\frac{5.1}{15}$ $\frac{6.0}{18-23}$ $\frac{4.8}{26}$ $\frac{4.5}{54}$ $\frac{4.1}{100}$

$\frac{9.7}{100}$ $\frac{5.3}{47}$ $\frac{5.6}{19}$ $\frac{5.0}{15}$ $\frac{5.1}{10}$ 5.0 $\frac{5.1}{10}$ $\frac{4.9}{16}$ $\frac{5.4}{18-23}$ $\frac{4.6}{25}$ $\frac{4.2}{72}$ $\frac{3.6}{100}$

$\frac{5.0}{100}$ $\frac{5.5}{25}$ $\frac{4.8}{14}$ $\frac{4.9}{10}$ 4.8 $\frac{4.9}{10-15}$ $\frac{5.7}{17-24}$ $\frac{5.1}{25}$ $\frac{4.2}{73}$ $\frac{3.4}{100}$

Sta

+

 π

-

^{15.21}
917.67 ✓

168

12.9 ✓

0

353

^{17.2}
916.23 ✓ 497^{3.22}
912.70 ✓

169

12.4 ✓

170

11.7 ✓

171

10.9 ✓

172

10.2 ✓

173

09.6 ✓

174

08.8 ✓

42.718

$\frac{6.0}{100}$	$\frac{5.6}{57}$	$\frac{5.9}{17}$	$\frac{5.1}{14}$	$\frac{5.0}{10}$	4.8	$\frac{5.0}{10}$	$\frac{5.1}{14}$	$\frac{5.7}{16-21}$	$\frac{4.2}{24}$	$\frac{3.0}{66}$	$\frac{2.4}{100}$
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88.718

84.818

7.2 6.8 5.2 4.3 4.1 3.8 4.0 4.6 2.7 0.2

$\frac{7.2}{100}$	$\frac{6.8}{62}$	$\frac{5.2}{18}$	$\frac{4.3}{15}$	$\frac{4.1}{10}$	3.8	$\frac{4.0}{9-14}$	$\frac{4.6}{16-20}$	$\frac{2.7}{25}$	$\frac{0.2}{100}$
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12.3 10.8 7.2 5.3 4.8 4.5 4.7 5.6 4.0 1.9

$\frac{12.3}{100}$	$\frac{10.8}{69}$	$\frac{7.2}{21}$	$\frac{5.3}{16}$	$\frac{4.8}{10}$	4.5	$\frac{4.7}{9-13}$	$\frac{5.6}{17-20}$	$\frac{4.0}{25}$	$\frac{1.9}{67}$
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17.0 12.9 8.4 6.0 5.5 5.3 5.4 6.0 4.8 2.8 0.8 0.0

$\frac{17.0}{100}$	$\frac{12.9}{60}$	$\frac{8.4}{22}$	$\frac{6.0}{17}$	$\frac{5.5}{11}$	5.3	$\frac{5.4}{9-14}$	$\frac{6.0}{16-21}$	$\frac{4.8}{25}$	$\frac{2.8}{55}$	$\frac{0.8}{82}$	$\frac{0.0}{100}$
--------------------	-------------------	------------------	------------------	------------------	-----	--------------------	---------------------	------------------	------------------	------------------	-------------------

18.5 9.2 7.0 6.2 6.0 6.2 6.1 6.9 4.5 3.1 0.4

$\frac{18.5}{100}$	$\frac{9.2}{23}$	$\frac{7.0}{17}$	$\frac{6.2}{11}$	6.0	$\frac{6.2}{9}$	$\frac{6.1}{15}$	$\frac{6.9}{18-22}$	$\frac{4.5}{30}$	$\frac{3.1}{56}$	$\frac{0.4}{100}$
--------------------	------------------	------------------	------------------	-----	-----------------	------------------	---------------------	------------------	------------------	-------------------

18.4 8.8 7.6 7.0 6.6 6.8 6.7 7.5 5.0 0.2

$\frac{18.4}{100}$	$\frac{8.8}{21}$	$\frac{7.6}{18}$	$\frac{7.0}{12}$	6.6	$\frac{6.8}{9}$	$\frac{6.7}{15}$	$\frac{7.5}{19-23}$	$\frac{5.0}{30}$	$\frac{0.2}{100}$
--------------------	------------------	------------------	------------------	-----	-----------------	------------------	---------------------	------------------	-------------------

19.0 9.6 8.4 7.9 7.4 7.6 8.1 5.1 0.3

$\frac{19.0}{100}$	$\frac{9.6}{22}$	$\frac{8.4}{18}$	$\frac{7.9}{12}$	7.4	$\frac{7.6}{8-13}$	$\frac{8.1}{17-22}$	$\frac{5.1}{30}$	$\frac{0.3}{100}$
--------------------	------------------	------------------	------------------	-----	--------------------	---------------------	------------------	-------------------

Sta

+

 π

-

916.23

175

07.4 ✓

O

12.87 920.07 9.03

907.20 ✓

B.M.

2.10 920.07 2.10

917.97 917.97

O

195 909.15 12.87

907.20 ✓

176

05.7 ✓

177

04.0 ✓

178

02.4 ✓

179

00.5 ✓

180 ↘

98.5 ✓

O

2.06 899.88 11.33

897.82 ✓

L.O. = Level Out

$\frac{19.5}{100}$ $\frac{11.2}{23}$ $\frac{9.7}{17}$ $\frac{9.3}{13}$ 8.8 $\frac{9.1}{8}$ $\frac{9.0}{14}$ $\frac{9.6}{17}$ $\frac{9.8}{20}$ $\frac{9.5}{22}$ $\frac{5.8}{32}$ $\frac{0.5}{100}$

SpK in 15" Oak 125' Rt Sta 173+45

$\frac{144}{100}$ $\frac{5.9}{21}$ $\frac{4.2}{16}$ $\frac{3.9}{12}$ 3.5 $\frac{3.7}{8-15}$ $\frac{4.2}{20}$ $\frac{3.8}{25}$ $\frac{0.4}{33}$ $\frac{+2.0}{100}$

L.O. $\frac{18.2}{110}$ $\frac{16.2}{94}$ $\frac{14.0}{85}$ $\frac{8.2}{21}$ $\frac{6.0}{16}$ $\frac{5.5}{12}$ 5.2 $\frac{5.4}{8}$ $\frac{5.8}{25}$ $\frac{3.9}{29}$ $\frac{1.2}{62}$ $\frac{+2.0}{100}$

$\frac{17.8}{110}$ $\frac{17.0}{106}$ $\frac{15.3}{85}$ $\frac{9.1}{22}$ $\frac{7.6}{17}$ $\frac{7.2}{11}$ 6.8 $\frac{7.0}{8}$ $\frac{7.1}{14}$ $\frac{8.0}{17}$ $\frac{8.2}{26}$ $\frac{6.0}{31}$ $\frac{1.3}{100}$

$\frac{12.7}{100}$ $\frac{15.4}{84}$ $\frac{10.0}{21}$ $\frac{9.4}{18}$ $\frac{8.9}{11}$ 8.7 $\frac{8.8}{8}$ $\frac{9.0}{13}$ $\frac{10.1}{19}$ $\frac{10.0}{26}$ $\frac{8.0}{34}$ $\frac{6.3}{51}$ $\frac{4.6}{100}$

$\frac{18.6}{100}$ $\frac{12.7}{62}$ $\frac{12.8}{21}$ $\frac{11.5}{16}$ $\frac{11.0}{10}$ 10.7 $\frac{10.9}{9}$ $\frac{11.0}{15}$ $\frac{12.0}{19-27}$ $\frac{6.5}{100}$

Sta

+

Σ

-

899.88^{01.05}✓

181

96.8 ✓

182

95.6 ✓

183

95.0 ✓

B.M.

4.97

894.91 ✓ 895.10

B.M.

7.05

902.09

484

895.04 ✓ 895.04

184

94.7 ✓

185

95.3 ✓

186

96.2 ✓

187

97.1 ✓

10 Ditch

$\frac{9.4}{101}$ $\frac{11.0}{100-99}$ $\frac{9.4}{98}$ $\frac{6.8}{21}$ $\frac{4.1}{15}$ $\frac{3.5}{11}$ 3.1 $\frac{3.4}{9}$ $\frac{3.5}{15}$ $\frac{4.7}{20-27}$ $\frac{1.6}{100}$

10 Ditch

$\frac{8.9}{100}$ $\frac{9.3}{35}$ $\frac{10.6}{34}$ $\frac{10.6}{33}$ $\frac{9.4}{33}$ $\frac{7.9}{21}$ $\frac{5.6}{16}$ $\frac{4.7}{10}$ 4.3 $\frac{4.6}{10}$ $\frac{4.8}{15}$ $\frac{7.1}{20}$ $\frac{6.0}{62}$ $\frac{5.0}{100}$

FL. Culv - 10.53

FL. Culv - 10.26

10 Ditch

$\frac{9.1}{100}$ $\frac{8.8}{26}$ $\frac{7.8}{22}$ $\frac{5.5}{17}$ $\frac{5.4}{11}$ 4.9 $\frac{5.2}{9}$ $\frac{5.5}{15}$ $\frac{8.0}{22}$ $\frac{8.2}{29}$ $\frac{9.9}{30-31}$ $\frac{8.2}{32}$ $\frac{9.0}{100}$

Top Mont 1/2 Mi. So. Co. Rd "I"

SPK in 18" Top 60' Rt. Sta. 186+18

$\frac{11.7}{100}$ $\frac{10.6}{25}$ $\frac{8.1}{19}$ $\frac{7.7}{11}$ 7.4 $\frac{7.5}{9}$ $\frac{7.8}{15}$ $\frac{10.4}{21}$ $\frac{11.5}{100}$

$\frac{12.5}{200}$ $\frac{12.4}{100}$

FL. Culv. 12.92

FL. Culv 12.82 $\frac{12.4}{80}$ $\frac{12.3}{100}$

$\frac{11.2}{100}$ $\frac{10.1}{27}$ $\frac{7.8}{21}$ $\frac{7.5}{12}$ 6.8 $\frac{7.0}{9}$ $\frac{7.7}{17}$ $\frac{10.6}{22}$ $\frac{11.1}{100}$

$\frac{10.3}{100}$ $\frac{10.5}{28}$ $\frac{6.2}{18}$ $\frac{6.3}{12}$ 5.9 $\frac{6.1}{9}$ $\frac{7.3}{18}$ $\frac{10.1}{30}$ $\frac{9.7}{100}$

$\frac{7.0}{100}$ $\frac{9.6}{39}$ $\frac{7.9}{25}$ $\frac{5.2}{19}$ $\frac{5.3}{12}$ 5.0 $\frac{5.2}{8-17}$ $\frac{7.1}{22}$ $\frac{6.4}{57}$ $\frac{4.5}{100}$

Sta

+

 π

-

902.09

187+40

97.6 ✓

188

98.0 ✓

189

98.8 ✓

0

9.44

908.89

264

900.63
899.45 ✓

190

99.6 ✓

191

00.7 ✓

192

01.5 ✓

+60

02.0 ✓

$$\frac{5.5}{100} \quad \frac{6.3}{30} \quad \frac{4.7}{19-11} \quad 4.5 \quad \frac{4.5}{8} \quad \frac{4.3}{18} \quad \frac{5.5}{23} \quad \frac{4.6}{32} \quad \frac{2.0}{100}$$

$$\frac{3.9}{100} \quad \frac{4.0}{22} \quad \frac{4.4}{11} \quad 4.1 \quad \frac{4.1}{8} \quad \frac{3.9}{25-28} \quad \frac{1.2}{37} \quad \frac{0.0}{85} \quad \frac{+0.5}{100}$$

$$\frac{1.8}{100} \quad \frac{1.6}{25} \quad \frac{3.7}{16} \quad \frac{3.6}{10} \quad 3.3 \quad \frac{3.5}{9-19} \quad \frac{3.9}{21-23} \quad \frac{2.8}{29} \quad \frac{+1.5}{34} \quad \frac{+0.5}{100}$$

$$\frac{6.0}{100} \quad \frac{5.4}{76} \quad \frac{5.2}{25} \quad \frac{9.3}{17} \quad \frac{9.5}{11} \quad 9.3 \quad \frac{9.5}{10-23} \quad \frac{8.3}{35} \quad \frac{3.8}{36} \quad \frac{2.3}{100} \quad \frac{2.5}{100}$$

7.0
2.8 ↑

$$\frac{2.1}{100} \quad \frac{2.7}{63} \quad \frac{3.2}{26} \quad \frac{8.0}{16} \quad \frac{8.5}{11} \quad 8.2 \quad \frac{8.4}{9} \quad \frac{7.8}{16} \quad \frac{8.3}{18} \quad \frac{7.4}{23} \quad \frac{5.8}{29} \quad \frac{3.2}{35} \quad \frac{1.6}{36} \quad \frac{2.2}{100}$$

$$\frac{1.4}{100} \quad \frac{3.4}{55} \quad \frac{4.2}{41} \quad \frac{3.8}{26} \quad \frac{7.5}{16-11} \quad 7.4 \quad \frac{7.7}{10} \quad \frac{7.6}{16} \quad \frac{9.2}{21-25} \quad \frac{7.2}{31} \quad \frac{8.7}{68} \quad \frac{8.6}{100}$$

$$\frac{+0.8}{100} \quad \frac{3.3}{55} \quad \frac{4.9}{26} \quad \frac{6.9}{18} \quad \frac{7.1}{10} \quad 6.9 \quad \frac{7.2}{10} \quad \frac{7.3}{18} \quad \frac{7.9}{20} \quad \frac{9.0}{31} \quad \frac{10.6}{33} \quad \frac{12.8}{72} \quad \frac{11.0}{100}$$

Sta

+

π

-

908.89^{10.68}

193

02.1

+70

02.2

194

01.9

○

10.68

912.59^{10.68} 698

901.91

195

00.4

196

98.9

○

4.96

904.23^{4.96} 13.32

899.27

197

97.3

BM

11.05

893.18^{11.05} 893.18

+70

96.0

893.34 8.5 in 24" Oak
60' RT Sta 197+93

$\frac{+0.5}{100}$ $\frac{3.5}{55}$ $\frac{6.4}{21}$ $\frac{7.2}{18}$ $\frac{7.0}{15}$ $\frac{6.9}{11}$ 6.8 $\frac{7.0}{9}$ $\frac{7.2}{20}$ $\frac{9.0}{39}$ $\frac{10.0}{65}$ $\frac{8.1}{100}$

$\frac{1.0}{100}$ $\frac{4.1}{55}$ $\frac{6.2}{24}$ $\frac{8.0}{14}$ $\frac{7.2}{15}$ $\frac{7.0}{10}$ 6.7 $\frac{7.1}{10}$ $\frac{7.2}{17}$ $\frac{8.2}{19-26}$ $\frac{7.1}{29}$ $\frac{7.9}{35}$ $\frac{7.2}{57}$ $\frac{3.2}{100}$

$\frac{1.0}{100}$ $\frac{4.0}{56}$ $\frac{5.6}{26}$ $\frac{8.0}{18}$ $\frac{7.3}{14}$ $\frac{7.1}{10}$ 7.0 $\frac{7.4}{11}$ $\frac{7.3}{14}$ $\frac{8.4}{20-24}$ $\frac{5.6}{32}$ $\frac{4.5}{40}$ $\frac{3.5}{75}$ $\frac{1.6}{100}$

Nail in Pavement Sta. 193+99.45

$\frac{1.0}{100}$ $\frac{4.6}{33}$ $\frac{7.7}{31}$ $\frac{12.5}{19-11}$ $\frac{12.4}{12.2}$ $\frac{11.6}{11}$ $\frac{3.4}{25}$ $\frac{+1.0}{35}$ $\frac{+1.0}{100}$

Fl. House +0.9

$\frac{0.3}{100}$ $\frac{1.2}{39}$ $\frac{13.2}{22}$ $\frac{13.8}{11}$ 13.7 $\frac{13.8}{10}$ $\frac{13.5}{17}$ $\frac{9.6}{26}$ $\frac{1.2}{37}$ $\frac{0.0}{70}$ $\frac{+1.0}{100}$

$\frac{0.3}{100}$ $\frac{0.7}{33}$ $\frac{8.0}{20}$ $\frac{7.0}{16}$ $\frac{7.2}{11}$ 6.9 $\frac{7.2}{9}$ $\frac{7.4}{21}$ $\frac{2.1}{30}$ $\frac{1.5}{77}$ $\frac{0.2}{100}$

Boat SpK in 24" Oak 60' RT Sta 197+93

$\frac{11.6}{100}$ $\frac{10.6}{50}$ $\frac{10.0}{31}$ $\frac{8.7}{19}$ $\frac{8.5}{12}$ 8.2 $\frac{8.4}{10-4}$ $\frac{9.9}{21}$ $\frac{8.7}{23}$ $\frac{9.2}{100}$

Sta

+

 π

-

904.23

198

95.7

0

403

897.08

11.18

893.05

199

93.1

200

90.5

+92

Road Right

91.7

201

91.8

201 + 04

91.8

201 + 40

Ditch Lt.

92.0

202

92.2

203

92.2

$\frac{13.2}{100} \frac{12.3}{33} \frac{12.0}{29} \frac{12.9}{17} \frac{12.0}{11} \frac{8.7}{10} \frac{9.1}{17} \frac{9.0}{21} \frac{10.1}{28} \frac{11.3}{39} \frac{12.6}{100} \frac{15.3}{100}$

Nail Sta 199+00

$\frac{8.6}{100} \frac{7.8}{38} \frac{7.5}{22} \frac{4.4}{16} \frac{4.2}{11} \frac{4.3}{10} \frac{4.5}{17} \frac{7.2}{22} \frac{7.7}{32} \frac{6.7}{100}$

$\frac{11.0}{100} \frac{10.3}{46} \frac{7.9}{22} \frac{7.9}{20} \frac{6.7}{12-10} \frac{6.6}{9} \frac{6.8}{19} \frac{7.6}{25} \frac{10.3}{100} \frac{9.1}{100}$

$\frac{5.4}{9} \frac{5.7}{47} \frac{7.5}{100} \frac{7.1}{100}$

5.3

$\frac{10.0}{100} \frac{9.6}{21} \frac{6.5}{17} \frac{5.4}{14-10} \frac{5.2}{9} \frac{5.6}{14} \frac{5.8}{14} \frac{10.3}{36-27} \frac{8.7}{30} \frac{8.3}{47} \frac{8.3}{100}$

17 Ditch

$\frac{13.4}{300} \frac{12.7}{200} \frac{12.3}{100} \frac{11.9}{50} \frac{11.6}{34} \frac{12.0}{21} \frac{8.6}{19} \frac{5.2}{14-10} \frac{5.1}{9} \frac{5.4}{10} \frac{5.8}{15} \frac{10.8}{30} \frac{10.6}{28} \frac{8.6}{30} \frac{8.9}{55} \frac{8.6}{100}$
 F.L. 11.69 (30) 11.64 20"
 Ditch
 F.L. Culv 10.74

$\frac{10.2}{100} \frac{9.6}{21} \frac{5.3}{15} \frac{5.0}{9} \frac{4.9}{10} \frac{5.1}{17} \frac{5.8}{24} \frac{10.7}{29} \frac{8.3}{32} \frac{8.4}{100}$

$\frac{9.3}{100} \frac{8.8}{21} \frac{6.6}{17} \frac{5.2}{8} \frac{4.9}{11} \frac{5.4}{16} \frac{10.7}{24-28} \frac{8.6}{31} \frac{8.4}{100}$

Sta	+	π	-
		98.1 897.08	

204			92.1
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0	5.14	98.3 897.19	503 892.05
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205			92.0
-----	--	--	------

206			92.3
-----	--	--	------

207			92.3
-----	--	--	------

208			91.0
-----	--	--	------

209			91.5
-----	--	--	------

+84			91.0
-----	--	--	------

$\frac{10.1}{100} \quad \frac{9.3}{22} \quad \frac{5.6}{15} \quad \frac{5.3}{9} \quad 5.0 \quad \frac{5.4}{12} \quad \frac{6.0}{18} \quad \frac{10.5}{25} \quad \frac{10.8}{27} \quad \frac{9.0}{31} \quad \frac{8.7}{64/100}$

Nail in Pavement Sta 204+00

$\frac{10.5}{100} \quad \frac{9.6}{21} \quad \frac{5.8}{15} \quad \frac{5.4}{9} \quad 5.2 \quad \frac{5.4}{11} \quad \frac{5.9}{18} \quad \frac{10.1}{27-30} \quad \frac{8.0}{34} \quad \frac{8.3}{75/100}$

$\frac{9.4}{100} \quad \frac{8.5}{21} \quad \frac{5.5}{15} \quad \frac{5.2}{8} \quad 4.9 \quad \frac{5.2}{12} \quad \frac{5.8}{18} \quad \frac{7.3}{23} \quad \frac{10.7}{28-31} \quad \frac{8.0}{34} \quad \frac{8.6}{70/100}$

$\frac{9.5}{100} \quad \frac{8.3}{22} \quad \frac{5.3}{16} \quad \frac{5.2}{8} \quad 4.9 \quad \frac{5.3}{11} \quad \frac{5.7}{17} \quad \frac{7.4}{21} \quad \frac{7.9}{26} \quad \frac{10.9}{29-31} \quad \frac{8.1}{34} \quad \frac{9.0}{100}$

$\frac{8.3}{100} \quad \frac{8.0}{86} \quad \frac{8.6}{27} \quad \frac{6.1}{19} \quad \frac{6.3}{9} \quad 6.2 \quad \frac{6.4}{11} \quad \frac{6.7}{18} \quad \frac{8.4}{23} \quad \frac{8.8}{26} \quad \frac{10.7}{29-32} \quad \frac{8.3}{37}$

FL 24' CM. $\frac{9.3}{100-74}$

ER

1105
EL 24' CM. (ER)

$\frac{7.6}{100} \quad \frac{8.5}{44} \quad \frac{8.1}{22} \quad \frac{6.1}{17} \quad \frac{5.7}{8} \quad 5.7 \quad \frac{5.6}{4} \quad \frac{6.1}{18} \quad \frac{6.6}{26-34} \quad \frac{7.8}{40} \quad \frac{10.8}{42-44}$

$\frac{8.3}{100-46}$

ER ER & ER

$\frac{8.0}{150} \quad \frac{9.0}{100} \quad \frac{8.0}{20} \quad \frac{6.6}{15} \quad \frac{6.3}{9} \quad 6.2 \quad \frac{6.7}{16} \quad \frac{6.6}{48} \quad \frac{6.5}{64} \quad \frac{6.9}{79} \quad \frac{7.9}{92} \quad \frac{10.8}{94-96}$

$\frac{8.2}{150-78}$

Sta

+

π

-

90.77
897.19

210

91.1

+70

91.9

+97

4 "I" Rt.

BM

5.19

537

892.00

891.69

BM.

FL 24CMLH 11.11

$\frac{7.2}{100}$	$\frac{8.7}{71}$	$\frac{8.2}{21}$	$\frac{6.6}{16}$	$\frac{6.3}{8}$	61	$\frac{6.5}{15}$	$\frac{7.3}{27}$	$\frac{7.7}{28}$	$\frac{11.0}{31-35}$	$\frac{7.4}{39}$	$\frac{7.7}{47}$
	$\frac{8.4}{150-139}$	$\frac{8.1}{112}$	$\frac{10.7}{110}$	$\frac{10.8}{108}$		$\frac{7.6}{105}$	ER	$\frac{7.8}{78}$	$\frac{6.6}{63}$	$\frac{6.8}{49}$	

$\frac{3.8}{100}$	$\frac{4.2}{86}$	$\frac{7.0}{41}$	$\frac{6.8}{19}$	$\frac{5.6}{13-10}$	53	$\frac{5.7}{21.2}$	$\frac{5.8}{27}$	$\frac{10.8}{23-35}$	$\frac{7.9}{40-100}$	$\frac{7.8}{119}$
						$\frac{10.6}{251}$	$\frac{8.0}{244}$	$\frac{7.6}{200}$	$\frac{7.3}{175}$	ER $\frac{7.1}{143}$

FL Culy 11.11

EF

$\frac{3.0}{100}$	$\frac{4.5}{51}$	$\frac{5.3}{8}$	5.2	$\frac{5.1}{4}$	$\frac{5.0}{11}$	$\frac{5.3}{53}$	$\frac{6.2}{100}$	$\frac{6.5}{200}$	$\frac{7.0}{300}$
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FL Culy Rt.
10.68

$$\begin{array}{r} 9300 \\ 1118 \\ \hline 91.82 \end{array}$$

