

DrG BK. 87

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

..... *Plan* Survey

COUNTY ROAD "I"

From *Lexington Ave.* To *Hodgson Rai.*

Road Acc't. No. *60*

Date Filed. *1935* File

1935

H.T. Purcell
8/35

- TOPOG -

COUNTY ROAD "I"
LEXINGTON TO HODGSON ROAD

Sta

$$\begin{array}{r} +88 \text{ PP} \\ 28 \end{array}$$

31

$$\begin{array}{r} +88 \text{ P.P} \\ 26 \end{array}$$

$$\begin{array}{r} +50 \text{ Rd-14 Top Gr. Surf.} \\ 87 \end{array}$$

$$\begin{array}{r} +88 \text{ TP} \\ 16 \end{array}$$

$$\begin{array}{r} +35 \text{ Sign} \\ 29 \end{array}$$

$$\begin{array}{r} +47 \text{ Rd Sn} \\ 24 \end{array}$$

$$\begin{array}{r} +12-12" \times 20' \text{ CM Road} \\ 24 \end{array}$$

30

$$\begin{array}{r} \text{Rd} \\ 11-8 \end{array}$$

$$\begin{array}{r} +87 \text{ PP} \\ 26 \end{array}$$

$$\begin{array}{r} +62 \text{ TP} \\ 16 \end{array}$$

29

$$\begin{array}{r} \text{Fcc Culv} \\ 89 \quad 40 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 10-11 \end{array}$$

$$\begin{array}{r} +29 \text{ P.P.} \\ 27 \end{array}$$

$$\begin{array}{r} \text{Fcc} \\ 87 \end{array}$$

$$\begin{array}{r} \text{Conduit} \\ 48 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 11-10 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ -45 \end{array}$$

28

$$\begin{array}{r} +84 \text{ Rd} \\ 30-56 \end{array}$$

$$\begin{array}{r} +73 \text{ PP} \\ 17 \end{array}$$

27

$$\begin{array}{r} \text{Conduit} \\ 47 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 9-10 \end{array}$$

$$\begin{array}{r} \text{Ed Rd} \\ 100-139 \end{array}$$

$$\begin{array}{r} +76 \text{ EW Fcc Cok} \\ 89 \end{array}$$

$$\begin{array}{r} +75-24" \times 42 \text{ CM} \\ 16-26 \end{array}$$

$$\begin{array}{r} +79 \text{ PP} \\ 27 \end{array}$$

$$\begin{array}{r} +76 \text{ N+S Fcc} \\ 21 \end{array}$$

$$+58 \text{ ERd}$$

$$+79 \text{ PP Tel}$$

$$\begin{array}{r} +83 \text{ Rd Sn} \\ 19 \end{array}$$

$$\begin{array}{r} +89 \text{ TP} \\ 19 \end{array}$$

$$\begin{array}{r} +29 \text{ Rd Sn} \\ 18 \end{array}$$

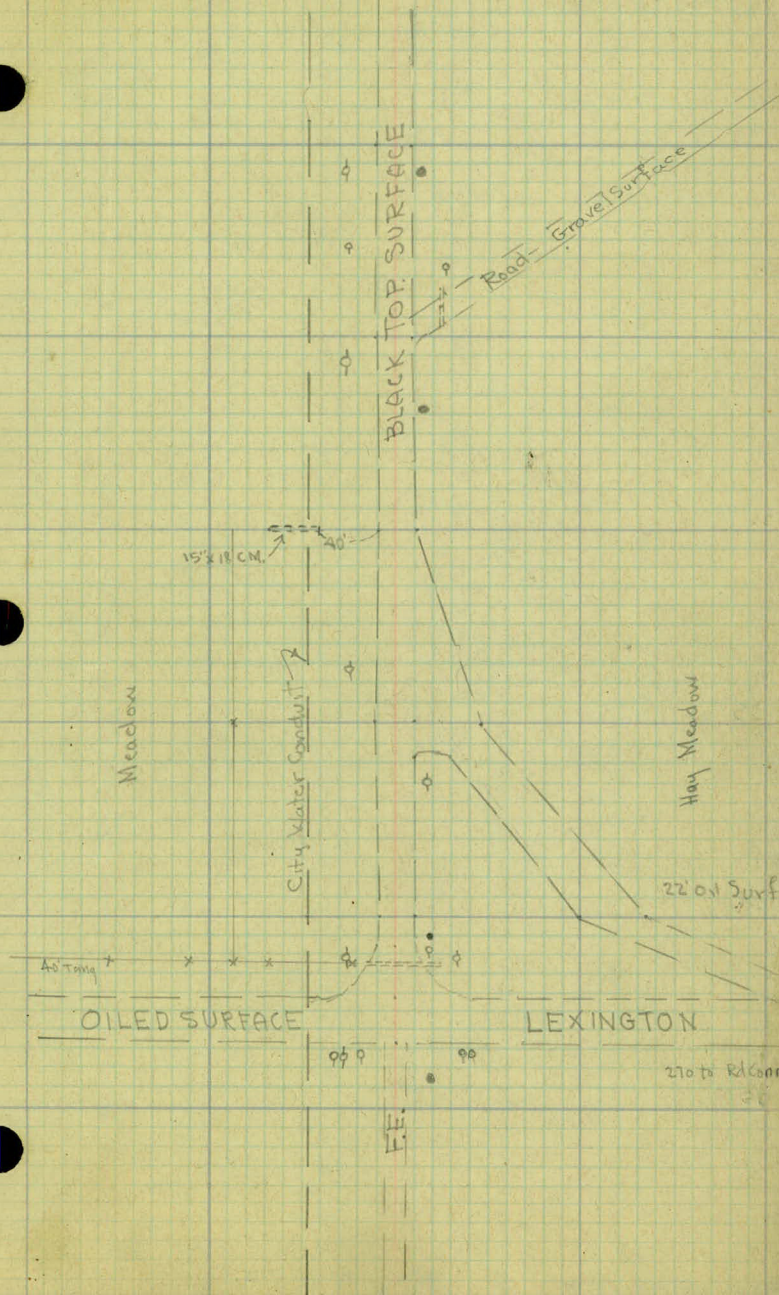
$$+34 \text{ E.Rd.}$$

$$\begin{array}{r} +14 \text{ Guy P} \\ 19 \end{array}$$

$$\begin{array}{r} +29 \text{ M Boxes} \\ 33 \end{array}$$

$$\begin{array}{r} +27 \text{ PP-Rd Sn} \\ 30 \quad 35 \end{array}$$

26



Ent 12' Top
106

+70 Ent-12"x22' CM
18'

38

Rd
13-8

+16 TP
14

+40 Ent
137

+61 PP
28

37

Rd
12-9

Cov Brush+Small Trs
31

+94 TP
14

+20 P.P.
27

+66 Sn Post +83 Ent-12"x20' CM
19

+06 Ctr. M.H. Conduit
48'

+60 P.P.
54

36

Rd
12-9

+73 P.P.
+66 Ent. 24"x18' CM
25

+55 N.S. Fee
70-27

+76 T.P.
14

35

Rd
11-10

+81 P.P.
28

+46 TP
15

Fee for N.S. Fee
88-71 27

Ent. 16' Top
82

34

+39 P.P.
27

+87 Ent 12"x22' CM
24

Rd
11-8

+23 TP
15

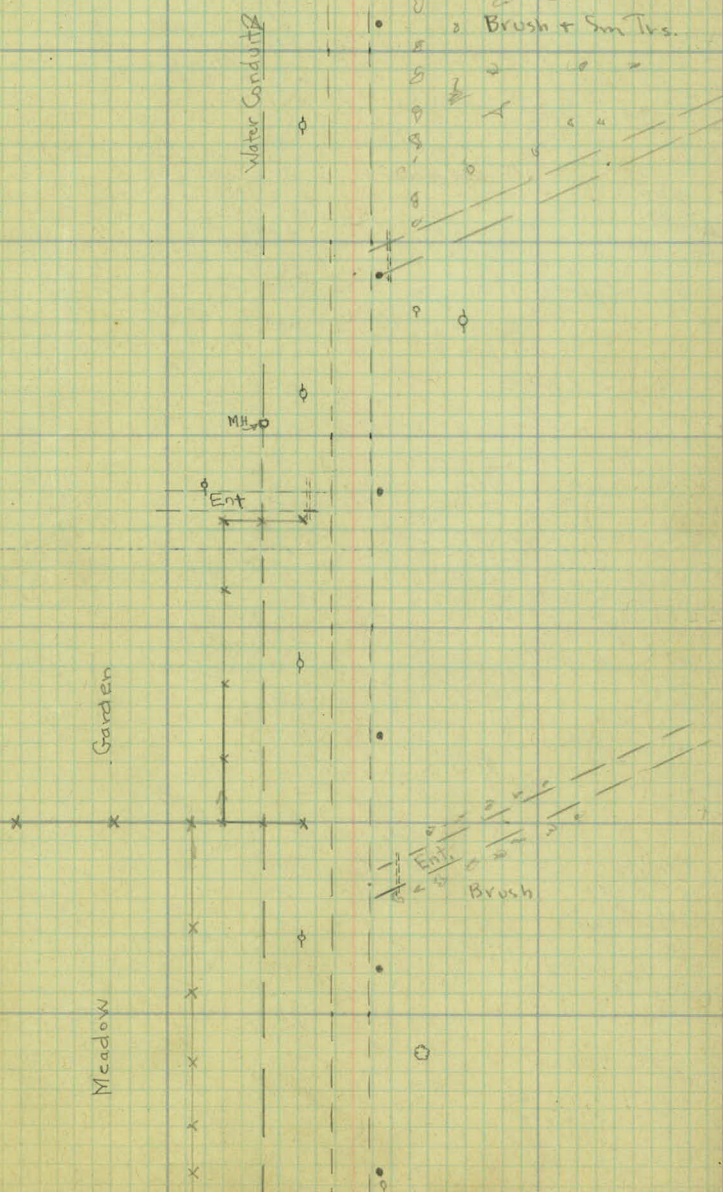
33

+80-Triple Birch
37

+17 TP
15

+12 Rd Sn
16

32



Fce	Rd
33	14-6

too Ent 12"x12" CM
16'

45

+ 40 P.P. -
29

$$\begin{array}{r}
 +58 \text{ Ent} \cdot \\
 +65 \text{ F Cor} \\
 +50 \text{ Cor Shed} \quad \quad +96-10^{\circ} \text{ W Oak} \\
 +40 \text{ T.P.} \quad \quad +44-19^{\circ} \text{ W Oak} - \text{Cor Shed} - 3-12^{\circ} \text{ Oaks} \\
 +04-20^{\circ} \text{ Oak} \quad \quad +32-12^{\circ} \text{ Oak} - 12^{\circ} \text{ Oaks} \\
 \hline
 30 \quad \quad \quad 37 \quad \quad \quad 57
 \end{array}$$

44

+ 17 P.P.
28

Fee
33

$+36 \text{ Cov Snd.}$
 $+16 \text{ Shed Cov } 12' \times 10'$
 $+213 \text{ gn}$
 $+10 \text{ Ent Rt.}$
 $+04 - 15' 80 \text{ aK}$
 $+50 \text{ Cov Fce}$
 $+50 \text{ Cov Bar-36' Rt.}$
 $+39 \text{ Cov Gar } 15' \times 12'$
 $+34 \text{ Can } 4 \times 6'$
 $+04 - 15' 80 \text{ aK}$
 $+13 - 24' 60 \text{ aK}$
 $+47$
 $+33$

43

$+100 \text{ Cor Bar} \cdot +52.8" \text{ W Oak}$
 $+43 \text{ Cor } 16 \times 20 \text{ Cor } 28$
 $+104 \cdot +12 \text{ Ent } 2 \times 16 \text{ VP}$
 $+22.20" \text{ BE}$
 $+22.24" \text{ W Oak}$
 $+06-12" \text{ BE} +09.24" \text{ W Oak}$

+98 P.P.
29

+92 File Cor
33

+ 93 T.P.
13
+ 69 Cor Fuel
61

Conduct
48

R4
12-7

42

+50 Ent 8' wide +80 TP
50 13
+29 Ent 15" x 18" CM
18
+25 Fee
120

+70 P.P.
29

41

$$\begin{array}{r} +95 \text{ Ent } 30' \times 52' \text{ V.P.} \\ 24 \end{array}$$

$$\begin{array}{r} +91 \text{ Fcc } \text{Cor} +95 \text{ Ent } 15' \times 18' \text{ CM} \\ 34 +86.3 \text{ BE Trs } 17 \\ \text{+64 T.P.} \\ 21 \end{array}$$

+56 p.p.
28

+41 Cor Tennis Court
70

40

$$\frac{Rd}{12-9}$$

+ 82 Car Tennis Court 62' X 123'
+ 70 Fee
+ 52 Fee Car 100
+ 53 Double Ent - 12' X 42 CM
18

$$\begin{array}{r} +68 \text{ N.S. Fce} - \text{P.P.} \\ \hline \quad \quad \quad 31 \quad \quad \quad 60 \end{array}$$
$$\begin{array}{r} + 10 \text{ pp} \\ \hline 28 \end{array}$$
$$\frac{+29TP}{13}$$

39

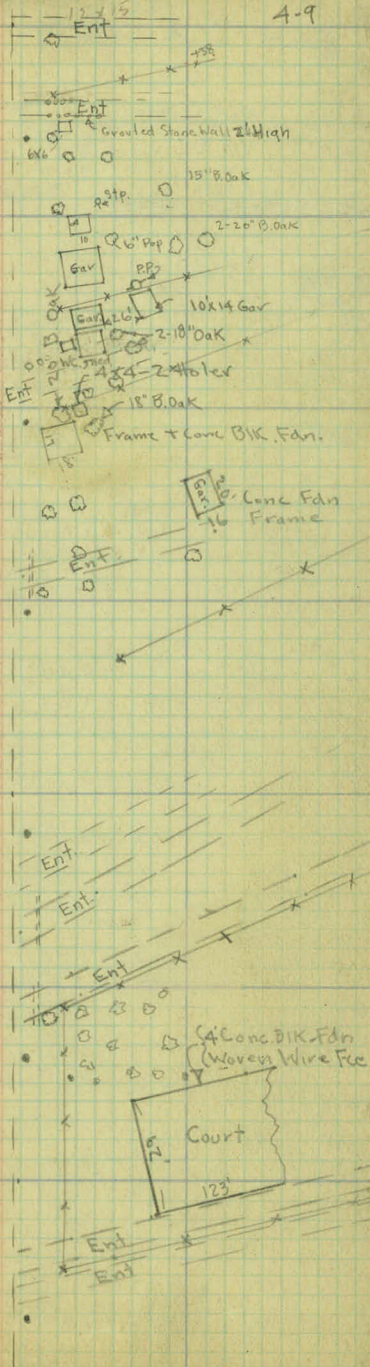
ON RIGHT SIDE

+99 Car Shed.
36.5
+91 Shed 10x8.
38
+81 Cor Gar.
+63 Cor. Gar. 20'x18'
34

ON RIGHT

+89 Gar Cor +93 TP
+73 Gar Cor. 17'x18'13
24
+75-24' BOAK - 20' BOAK
+67-12' BE. 105
78 +60 Ent Rt

Water Conduit



Rd
Fcc 33 15-5

+76 H+S Ditch - 15x18' CM

+82 F.C.
33

+70 F.C. +80 P.P.
33 29

Fcc
32

Rd
1A-5

+90 TP
12

+74 Ent

+69 End Fcc 42
20

Fcc
21

+81 Trip. Birch - P.P. - 24" P.P.
76 80

+69 P.P.
28

+47 F.C.
22

+70 T.P.
12

Fcc
20

Rd
1A-5

+52 P.P.
28

+39 Gate Post
20

+29 Gate Post
20

+15 F.C.
20

+54 TP

+34 Ent - 8'x14' CM

+27 Cor Gar
61

Rd
13-6

+93 W.C. 4x4

+78 Cor Gar 14'x10'

+77 Ent 12'x16' CM

+84 Gate Post
20

+70 Gate Post
20

+35 Ent - 12'x16' Steel
18

+27 T.P. - Cor Gar 12'x10'

+14 W.C. 3x3
39

+16 8" Pop
26

+31 P.P.
28

+84 Cor Gar
28

+68 Cor Gar 20x16 +70 End Willow

+33 M.H. on Conduit
48

+19 2" x 38' CM

22-16

+12 TP
12

+24 P.P.
67

+100 Ent 12'x18' CM
18

+48 Ent - 12'x16' CM
16

+08 Bay Willows
21

+03 P.P.
28

Fcc
33

+56 End Oak Grove

27-100

+64 Oak Grove
23-100

+76 Cor Gar
39

+56 Cor Gar 18x20
45

+41 End Group Oak

+23 Bay Gr. Oaks } 100aks

+11 8" Oak
53

+59 15" Oak
61

+07 8" Oak - 10" Oak
39

+48 Fcc Cor
26

+51 Cor Shed
44

+45 Cor Shed
45

+70 P.P.
28

46

52

51

50

49

48

47

A' Bot. Ditch $\rightarrow$ $\frac{x}{x} \rightarrow \frac{x}{x} \rightarrow$

Water Conductivity

TURTLE LAKE

Ent

Ent
Silver Pop
Woods

Woods

Ent

Gar

4x4 W.C.

Woods

Ent

Gar

W.C.

Wood Arch

Sm Trs & Brush

Ent

Gar

W.C.

W.C.

Brush

La Kc 192'

Gar

W.C.

4x4 W.C.

Ent

Ent

Ent

Ent

Ent

Ent

Ent

Ent

Ent

Ent

Ent

Ent

Ent

Ent

Ent

Ent

Ent

Ent

Ent

ON RIGHT SIDE

+83-18" Maple

+58 W.C.

+54 3x4 W.C.

+78 TP

+77 Cor Gar

+68 Cor Gar

+52-4" Pop

+90 End Birch Trs

+70 Beg Birch Trs

+64 Ent-12" W.C.M.

+79 Beg Oak Grove

4 Trs

W.C.

Gar

W.C.

Gar

W.C.

Gar

W.C.

Gar

W.C.

Gar

W.C.

Gar

W.C.

Gar

W.C.

Ent

Ent

Ent

Ent

Ent

Ent

Ent

Ent

Ent

Ent

Ent

Ent

Ent

Ent

$$\frac{+98-24 \times 38 \text{ CM.}}{20-18}$$

59

$$\frac{+100 \text{ RP}}{30} \quad \frac{\text{Fcc}}{33} \quad \frac{\text{Rd}}{14-6}$$

$$\frac{+61 \text{ PP}}{28}$$

$$\frac{+96 \text{ TP}}{11}$$

$$+10 \text{ Ent}$$

58

$$+100 \quad \frac{\text{Cor Grav}}{51}$$

$$\frac{+83 \text{ PP}}{30}$$

$$\frac{+80 \text{ TP}}{11}$$

$$\frac{+98 \text{ PP}}{27}$$

57

$$\frac{+56 \text{ PP.}}{30}$$

$$\frac{+55 \text{ TP.}}{55}$$

56

$$\frac{\text{Fcc}}{33}$$

$$\frac{\text{Rd}}{14-6}$$

$$\frac{+33 \text{ PP.}}{29}$$

$$\frac{+20-24 \times 42 \text{ CM.}}{21-21}$$

$$\frac{+33 \text{ TP}}{11}$$

55

$$\frac{\text{Rd}}{14-5}$$

54

$$\frac{+05 \text{ PP.}}{29} \quad \frac{\text{Conduit}}{48'} \quad \frac{\text{Fcc}}{32}$$

$$\frac{+11 \text{ TP}}{11}$$

$$\frac{+11 \text{ Rd Sn}}{27}$$

$$\frac{+15 \text{ Wire box } 19 \times 55}{134}$$

53

$$\frac{\text{Rd}}{15-5}$$

$$\frac{+05 \text{ Reg 8' Bot. dt}}{36 \text{ \#}}$$

Water Conduit

Lake 190'

Ent Gar 12
20

Lake 163'

Lake 166'

12" Spir. Dr. Pipe 7

1hp 18" x 36" C.M.
#60-2219 in
110
Well Box

TURTLE LAKE

66

$$\begin{array}{r} +10PP \\ 31 \\ \hline Fce Cor \\ 33 \end{array}$$

+60 Bag 2" Row Pop - 10' C-C

$$\begin{array}{r} 45 \\ +58 Fce \\ 43 \\ +23 Ent \\ \hline +10 T.P. \\ 11 \end{array} \quad \begin{array}{r} +74 Ent \\ +41-18" Oak \\ +36-8" Oak \\ +28-18" Oak \\ \hline 72 \end{array} \quad \begin{array}{r} +85-6" Birch \\ 46 \end{array}$$

65

+37 Ent

$$\begin{array}{r} +0.5-24" X 30 CM \\ 20.5-19.5 \end{array}$$

+56 Cor Gar 21' X 24'

46

64

$$\begin{array}{r} +91 PP \\ 31 \\ \hline +74 F Cor. \\ 33 \end{array}$$

$$\begin{array}{r} +92 T.P. \\ 11 \end{array}$$

$$\begin{array}{r} +76 N+6 Fce \\ 33 \\ +68 PP \\ 30 \end{array}$$

$$\begin{array}{r} +73 TP \\ 11 \end{array}$$

63

$$\begin{array}{r} Fce \\ 33 \end{array}$$

$$\begin{array}{r} 34 \\ 13-7 \end{array}$$

$$\begin{array}{r} +81 PP \\ 17 \end{array}$$

+78 End Hedge +75 End 8' Bot Ditch

43

36 t

$$\begin{array}{r} +56 PP \\ 30 \end{array}$$

$$\begin{array}{r} +56 T.P. \\ 11 \\ +26 Ent-15" X 30 CM \\ 36 \end{array}$$

62

$$\begin{array}{r} +67 Ent 15" X 20 CM \\ 35 +63 Gar 20" X 12 \\ +36 T.P. \\ 11 \\ +27 PP \\ 28 \end{array}$$

$$\begin{array}{r} +32 PP \\ 30 \end{array}$$

+07 Ent

+74 Bag Hedge

43

61

$$\begin{array}{r} 34 \\ 13-6 \end{array}$$

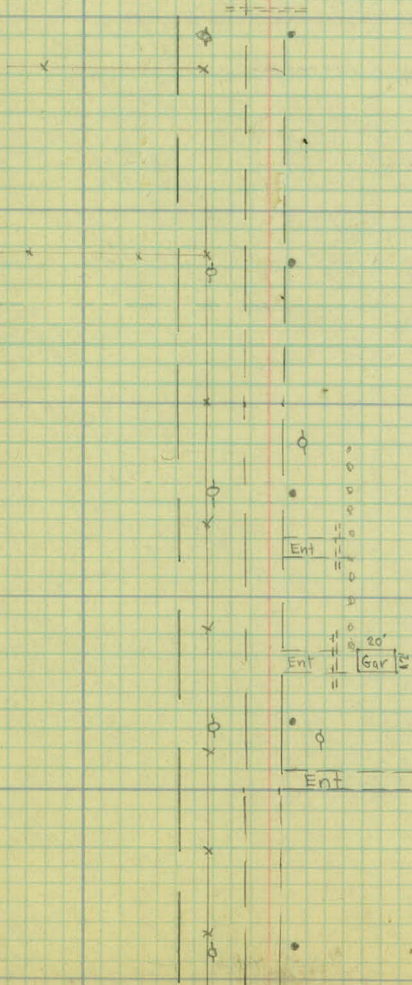
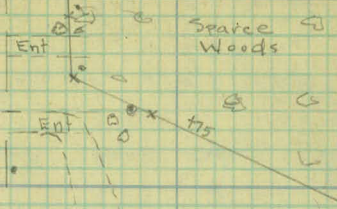
$$\begin{array}{r} +15 TP \\ 30 \end{array}$$

$$\begin{array}{r} +18 TP \\ 11 \end{array}$$

60

Cult.
Water Conductivity

Yard



73

$$\frac{+35 \text{ PP.}}{31}$$

$$\frac{\text{Rd}}{10-9}$$

$$\frac{+33 \text{ TP}}{15}$$

72

$$\frac{+14 \text{ RP.}}{31}$$

$$\frac{+28 \text{ F Cor}}{27}$$

$$\frac{+16 \text{ TP}}{14}$$

71

$$\frac{\text{Rd.}}{11-8}$$

$$\frac{\text{Fcc}}{26}$$

$$\frac{+99 \text{ PP.}}{31}$$

$$\frac{+99 \text{ TP.}}{14}$$

$$\frac{+36 \text{ Beg Fcc}}{26}$$

$$\frac{+74 \text{ F Cor}}{26}$$

$$+27 \text{ Ent}$$

$$\frac{+72 \text{ End 2nd Row Pop.}}{45}$$

70

$$\frac{+78 \text{ PP}}{31}$$

$$\frac{+60 \text{ Stp}}{31}$$

$$\frac{+88 \text{ Stp}}{34}$$

$$\frac{+76 \text{ TP.}}{13}$$

$$\frac{+68 \text{ Stp}}{31}$$

$$\frac{+47 \text{ Stp}}{34}$$

$$\frac{\text{Rd}}{12-7}$$

$$\frac{\text{End Woods}}{45}$$

69

68

$$\frac{+53 \text{ TP}}{13}$$

$$\frac{+47 \text{ Stp}}{39}$$

$$\frac{+55 \text{ PP}}{31}$$

$$\frac{+97 \text{ End Fcc}}{43}$$

$$\frac{+72 \text{ Stp}}{42}$$

$$\frac{+78 \text{ Stp}}{31}$$

$$\frac{+94 \text{ Stp}}{31}$$

$$\frac{+32 \text{ PP}}{31}$$

$$\frac{+11 \text{ Stp.}}{37}$$

$$\frac{+32 \text{ TP}}{13}$$

67

Water Conduit

Cultivated

Sparse Woods
(Oaks)Sparse Wood
(Oaks)

80

$$\begin{array}{r} +20 \text{ Cor Schr Ho} \\ 117 \end{array}$$

$$\begin{array}{r} +60 \text{ Rd Sm} \\ 19 \\ +49 \text{ F Cor} \\ 47 \\ +44 \text{ Rd Sm} \\ 29 \end{array}$$

$$\begin{array}{r} +60 \text{ P.P.} \\ 27 \\ +27 \text{ shoulder} \\ +43 \text{ F Cor} \\ 32 \end{array}$$

79

$$\begin{array}{r} +82 \text{ PP} \\ 32 \\ +73 \text{ Rd Sm} \\ 32 \end{array}$$

$$\begin{array}{r} +80 \text{ PP} \\ 41 \\ +59 \text{ T.P.} \\ 20 \\ \text{Rd} \\ 10-9 \\ \text{Fcc} \\ 32 \end{array}$$

$$\begin{array}{r} +77 \text{ F Cor} \\ 33 \\ +73 \text{ Rd Sm} \\ 17 \end{array}$$

78

$$\begin{array}{r} +49 \text{ PP} \\ 31 \end{array}$$

$$\begin{array}{r} +49 \text{ T.P.} \\ 19 \end{array}$$

$$\begin{array}{r} \text{Fcc} \\ 32 \end{array}$$

77

$$\begin{array}{r} +17 \text{ P.P.} \\ 32 \end{array}$$

$$\begin{array}{r} +17 \text{ T.P.} \\ 18 \end{array}$$

$$\begin{array}{r} \text{Fcc} \\ 31 \end{array}$$

76

$$\begin{array}{r} \text{Rd} \\ 10-9 \end{array}$$

$$\begin{array}{r} +35 \text{ Rd Sm} \\ 18 \end{array}$$

75

$$\begin{array}{r} +76 \text{ TP} \\ 17 \\ +39 \text{ Rd Sm} \\ 15 \end{array}$$

$$\begin{array}{r} +96 \text{ Fcc Cor} \\ 20 \end{array}$$

$$\begin{array}{r} +78 \text{ PP} \\ 31 \end{array}$$

$$\begin{array}{r} \text{Fcc} \\ 29 \end{array}$$

74

Sch. Hb

HODGSON ROAD

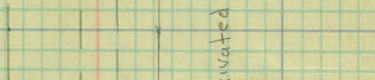
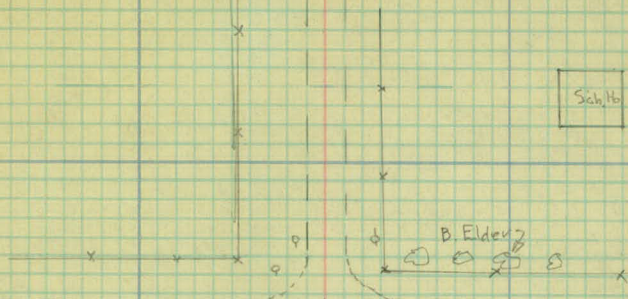
40' Tangents

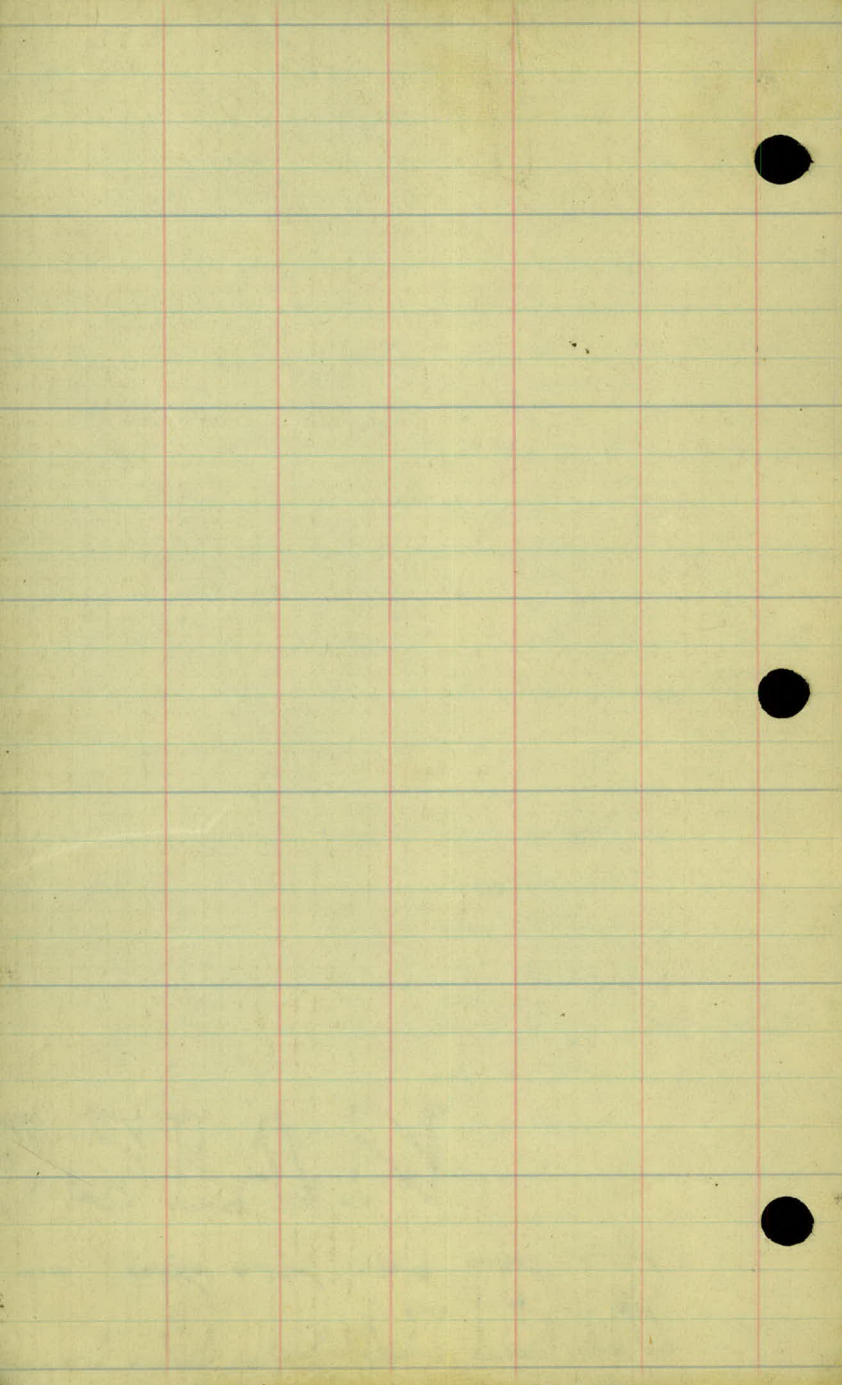
B. Eldenz

Cultivated

Water Conduit

Spars Woods





Alignment

79+10.70

POT

± Hodgson Road

2635.20

52+75.5

P.I.

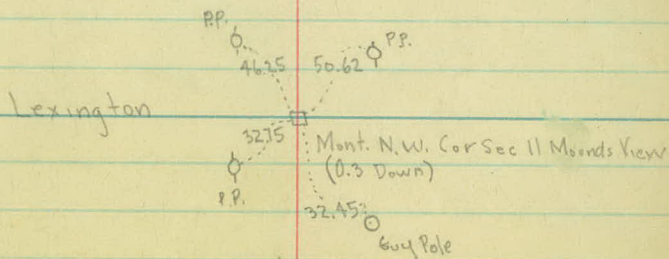
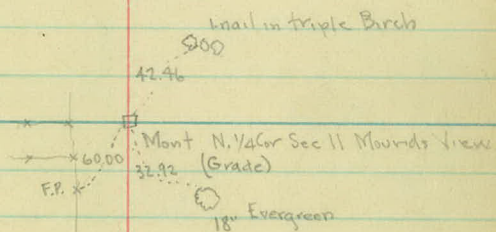
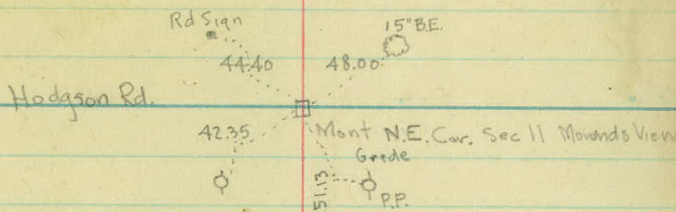
Δ 0° 00' 15" Rt

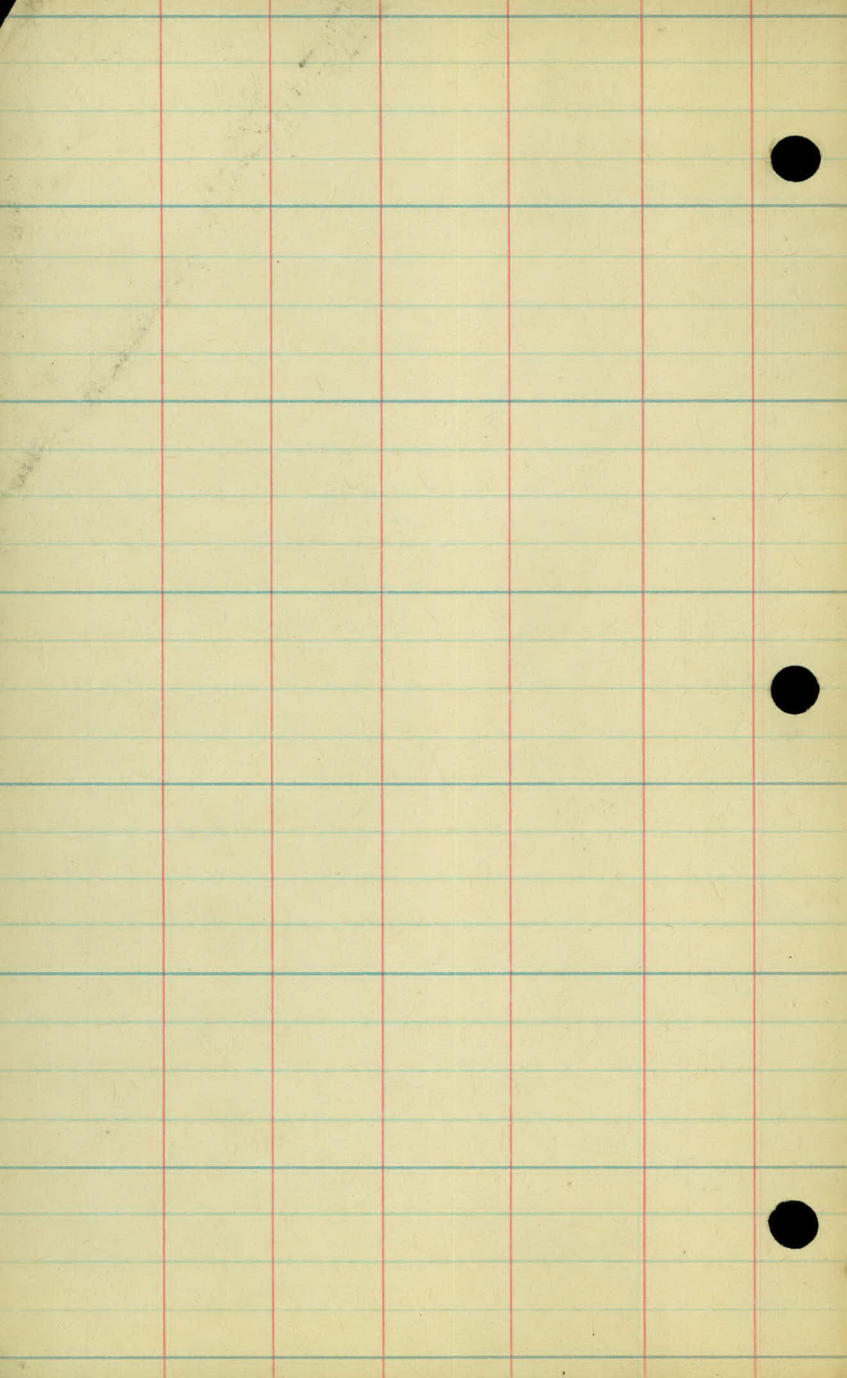
2634.25'

26+41.25

POT. ± Lexington A

Purcell
Ties 8/23/35





X- Sections

County Road "I" Lex. to Hodgson Rd.

Sta + K -

B.M. 2.85 904.93 902.08

B.M. 9.25 895.68 = 898.26

⊙ 1.68 903.56 3.05 901.88

B.M. 2.75 894.75 11.71 891.85 892.00
26+41.25 ± Lexington

± Lex. 92.2

+57 92.3

+58 92.2

+75 24" x 42' C.M. 92.1
24" x 112' C.M.
110' to No End

+78 92.1

SpK in 24" Oak. 850' W + 110' S of Lex. + "I"

SpK in 20" Oak 10' Rt. Sta. 17+50

Top Mount Lex + "I"

$\frac{1.6}{100}$ $\frac{2.2}{59}$ 2.58 $\frac{3.0}{50}$ $\frac{3.5}{100}$ $\frac{3.2}{150}$ $\frac{2.9}{200}$

$\frac{2.3}{100}$ $\frac{2.7}{33}$ $\frac{2.8}{17}$ 2.5 $\frac{3.0}{30}$ $\frac{4.0}{100}$ $\frac{3.6}{150}$ $\frac{3.3}{170}$ $\frac{3.5}{200}$

$\frac{2.1}{100}$ $\frac{2.5}{59}$ $\frac{2.6}{33}$ $\frac{3.2}{17}$ $\frac{2.9}{10}$ 2.6 $\frac{3.2}{22}$ $\frac{3.9}{64}$ $\frac{4.8}{110}$ $\frac{3.7}{125}$ $\frac{3.5}{155}$ $\frac{4.0}{200}$

$\frac{1.6}{50}$ $\frac{3.9}{41}$ $\frac{4.5}{25}$ $\frac{7.7}{20}$ $\frac{8.13}{15}$ $\frac{3.8}{15}$ $\frac{3.5}{12}$ $\frac{3.0}{9}$ 2.7 $\frac{3.2}{16}$ $\frac{4.1}{23}$ $\frac{8.50}{27}$ $\frac{8.5}{67}$ $\frac{8.85}{110}$ $\frac{4.0}{116}$ $\frac{3.6}{150}$
 $\frac{3.4}{59}$ $\frac{3.5}{100}$ $\frac{8.46}{222}$ $\frac{4.9}{220}$ $\frac{4.2}{192}$

$\frac{2.3}{47}$ $\frac{3.7}{42}$ $\frac{5.2}{22}$ $\frac{8.1}{19}$ $\frac{7.9}{16}$ $\frac{4.1}{14}$ $\frac{3.1}{7}$ 2.7 $\frac{3.2}{15}$ $\frac{4.1}{23}$ $\frac{7.4}{27}$ $\frac{5.8}{30}$ $\frac{6.3}{67}$ $\frac{6.2}{87}$ $\frac{4.2}{125}$
 $\frac{2.6}{54}$ $\frac{3.8}{61}$ $\frac{3.8}{88}$ $\frac{4.7}{100}$ $\frac{4.8}{200}$ $\frac{4.4}{171}$ $\frac{3.6}{144}$

Sta

+

K

-

Elev.

894.75

0

2.31

894.31

2.75

892.09

27

91.7

28

90.7

29

90.7

30

89.9

31

88.8

32

88.3

2.1	2.3	4.4	5.0	6.5	7.1	3.8	3.3		
50	44	39	41	19	16	12	10		
4.5	3.2	5.7	4.7	4.0	4.3	5.3	5.5		
58-74	76	80	82	82	100	200	146		

26	3.1	3.4	4.7	6.5	6.3	4.8	4.9
	10	15	24	26	37	29	80
	7.8	5.2	4.0	3.8	3.4	3.6	3.6
146	142	141	133	123	110	96	85

890.8 / 100

2.5	5.0	6.2	5.9	7.8	4.9	4.3			
46	34	33	30	22	20	17	15	10	
2.4	4.8	5.8	6.1	5.3	4.8				
52	44	64	70	73	93	100			

ER

36	5.8	4.1	4.4	5.2	7.3	5.3	5.4
	9	25	42	55	56	58	100

55 / 200

7.8!

3.0	2.7	4.8	5.9	11.8	7.5	4.5	4.0		
51	46	39	22	21	18	17	14	9	
5.1	6.3		6.9	5.2	4.8	5.0			
63	65		69	72	89	100			

4.7	2.7	5.6	6.1	8.1	7.7	4.8	4.7		
51	51	46	38	22	21	17	14	10	
5.3	6.9	7.0	5.3	5.8	5.5	5.6			
64	66	70	71	81	90	100			

+12 12x20 C.M. 7.74 F.L.D. 24 Rd

6.0	7.1	6.5	3.6	3.5	6.5	8.2	8.6	6.9	5.9
72	70	57	52	47	41	23	18	17	11
5.8	5.9								
89	100								

6.7	3.6	2.0	6.5	7.1	8.6	8.9	7.4	6.4	
55	31	45	41	24	23	19	17	10	
6.3	7.4								
62	65	70	72	83					

Sta + π - Elev

894.31

33

✓
88.4

34

✓
89.2

①

4.15

✓
894.39

4.07

✓
890.24

35

2

✓
90.8

BM

1.61

✓
892.78

36

✓
89.9

4.4 7.2 7.7 8.3 8.8 7.6 6.7 6.4 5.9 6.1 6.2 7.3 5.8 5.0 4.7
 46 43 26 25 20 19 14 10 9 18 19-22 23 120 200

888.3

4.0 6.8 6.6 6.3 6.4
 51 56-65 75 96 100

+ 67 12"x22" CM E1.86.55
 24RT

6.8 5.8 3.3 3.0 5.6 6.4 8.2 8.8 6.6 5.6 5.1 5.6 6.1 7.1 7.3 6.0 5.6 5.1
 68 61 53 45 42 28 27 21 19 11 9 17 18 21 22 88 100
 7.2 5.8 5.1
 100 200

888.6

888.3

2.4 2.5 5.3 5.5 8.0 8.2 5.0 4.2 4.2 4.9 7.0 5.4 6.1 6.5
 52 46 41 29 28 23 19 11 9 17 18-21 22 100 200
 4.8 5.0 6.2 4.7
 57 63 64 72-100

Sd=Drz FLZ
 +66- 24"x18" CM 7.32
 25 14

Set SE. Cor Conc. Slab Conduit M.H. Lt. Sta 36 to 6

888.5

6.3 6.1 3.3 3.2 5.3 5.8 7.6 7.3 5.6 4.9 4.5 4.9 5.4 6.6 6.8 5.4 5.9 6.2
 61 57 51 46 41 28 27 22 20 12 9 17 18 21 22 120 200
 5.3 5.5
 60 100

+83- 12"x20" CM 19RT

F.L. 7.32

Sta

+

x

-

894.39

37

89.9

38

✓
90.6

39

✓
91.5

40

8.75

✓
899.96

3.18

✓
891.21

40

✓
92.1

41

✓
93.0

42

✓
91.8

889.0

889.3

8

$\frac{3.5}{49} \quad \frac{3.4}{46} \quad \frac{5.9}{42} \quad \frac{6.2}{28} \quad \frac{7.6}{27} \quad \frac{7.1}{22} \quad \frac{5.9}{26} \quad \frac{5.1}{12}$

$4.5 \quad \frac{4.9}{9} \quad \frac{5.0}{15} \quad \frac{6.1}{17} \quad \frac{7.2}{19} \quad \frac{5.6}{20} \quad \frac{5.4}{100}$

$\frac{6.2}{54} \quad (\frac{6.4}{51}) \quad \frac{5.3}{62} \quad \frac{5.8}{100}$

$\frac{5.0}{20}$

$\frac{5.3}{58} \frac{5.2}{54} \frac{2.8}{57} \frac{5.2}{42} \frac{5.1}{28} \frac{1.5}{27} \frac{7.6}{23} \frac{5.0}{20} \frac{4.5}{11} \geq 8 \frac{4.1}{8} \frac{4.5}{14} \frac{6.4}{16} \frac{6.6}{19} \frac{5.2}{20} \frac{5.1}{26-100}$
 $\frac{6.3}{59} \frac{4.9}{62} \frac{5.1}{100}$

+70 $\frac{12' \times 22' \text{ CM}}{18' \text{ RT}}$ FL. 7.05

$\frac{50}{57} \frac{24}{51} \frac{2.2}{46} \frac{4.7}{40} \frac{4.1}{26} \frac{6.6}{25} \frac{6.6}{23} \frac{4.1}{19} \frac{3.5}{10} 2.9 \frac{3.4}{8} \frac{3.9}{14} \frac{6.6}{17-18} \frac{4.8}{20} \frac{4.9}{40}$
 $\frac{5.7}{60} \frac{4.7}{67} \frac{4.2}{100}$

+ 53 $\frac{12 \times 42 \text{ CM}}{18 \text{ Rt}}$ $\begin{matrix} \text{WE} \\ 6.90 \\ 6.55 \text{ EE} \end{matrix}$

43	56	62	79	118	91	81	79	85	88	114	118	103	96	85	75	46
100	78	58	42-30	25-23	19	11	8	13	16	18	20	33	71	78	80	

+95 30" x 52" V.P. 11.05 ^{FL 7}
24" 4

+95-15" X 18CM FL.
17 RT 12.03

$$\begin{array}{cccccccccccccccc} \underline{4.9} & \underline{5.2} & \underline{6.2} & \underline{7.4} & & \underline{11.1} & \underline{6.8} & & \underline{7.3} & \underline{7.9} & \underline{11.4} & \underline{8.7} & \underline{9.4} & \underline{9.3} & \underline{8.8} \\ \underline{100} & \underline{88} & \underline{42} & \underline{27} & & \underline{16} & \underline{22} & \underline{21} & & \underline{10} & \underline{8} & \underline{16} & \underline{18-20} & \underline{22} & \underline{42} & \underline{73} & \underline{88} \end{array}$$
$$\begin{array}{r} + 20 \text{ } 00 \\ \hline 200 \text{ } 780 \end{array} \quad \begin{array}{r} 44 \text{ } 74 \\ \hline 155 \text{ } 129 \end{array} \quad \begin{array}{r} 90 \\ \hline 100 \end{array}$$

+29 15' x 18 CM FL. 12/12
18' Rt

$$\begin{array}{r} 104 \\ \hline 58 - 100 \end{array}$$

$$\begin{array}{r} 55.00 \\ \hline 180 \end{array}$$

$$\begin{array}{r} 39.75 \\ \hline 110 \end{array}$$

$$\begin{array}{r} 10.00 \\ \hline 70 \end{array}$$

$$\begin{array}{r} 8 \times 18.48 \\ \hline 147.84 \end{array}$$

892.7 FL

$$\begin{array}{r} 9.82 \end{array}$$

Sta	+	$\bar{A}$	—	Elev.
		899.96		
43				92.3
44				92.7
45				92.8
⊙ 46	3.88	896.59	7.25	892.71 92.5
47	↙			92.1
48				92.0

81	99	10.2	9.5	10.0	9.2	8.3	7.7	7.9	8.6	9.6	8.8	9.0	6.1	2.0
49	42	33	28	23	14	12	7	14	18-20	21	37	67	100	
114	107	11.0												
57	60	100												

+12-8'x18'VP 9.82 FL
16 RT

7.1	5.7	7.0	9.2	8.8	7.4	7.6	7.3	7.3	6.7	1.1	0.8	1.0	0.9	
100	41	4	36	35	33	12	6	19	61	77	100	125		

+2.0 0.0
200 150

5.9	7.18	8.5	8.4	9.5	8.1	7.9	7.3	8.4	7.8	5.8	1.5	1.0	0.9	
48	41	37	33	24	22	21	19	12	17	24	31	35	150	
6.5	8.4													
68	100													

0.8
200

6.5	4.3	5.2	5.8	7.1	7.0	5.4	4.7	4.2	4.3	5.2	3.7	2.4	0.5	+0.5
100	60	32	26	24	22	20	14	7	13	16-18	21	36	63	100

+00 12'x12'CM. 5.80 FL
16 RT

+64-12'x16'CM. FL. 5.75
18 RT.

5.0	7.0	6.4	7.4	6.0	4.9	4.5	4.8	5.0	5.1	5.1	4.0	2.3	1.7	1.6
44	40	33	28	25	23	21	15	6	12	17	21	25	66	84
3.7	5.0	6.6	7.3											
50	55	63	100											

1.5 1.5
200 145

4.7	5.2	7.1	6.6	6.7	8.0	7.9	5.9	5.2	4.6	4.8	5.9	6.1	5.0	5.1
50	46	41	33	27	26	23	18	14	6	6	15	16-18	20	51
7.0	7.2													
55	100													

3.6 H₂O
190

+00 12'x18'CM FL. 6.90
18 RT.

Colv # 60-18 +18-12'x38'CM

22'-16'
FL 200 FL 8.11

+48-12'x16'CM FL. 20.5
16 RT

Sta + π -
896.57

B.M. 2.77 893.82

49 91.0

50 $\downarrow$ 90.2

51 $\downarrow$ 90.7

52 90.6

BM 4.73 95.65 5.67 90.92 ~~891.77~~

53 91.0

Sta + π -
95.65

53+75 18" CM x ? unable to locate End

54 91.0

55 90.6

+21 24" X 42" CM. 90.5

56 91.1

57 90.2

58 91.0

0 1.24 91.52 437 91.28

Lt.

Rt.

FL2
8.61

Fuc

$\frac{4.0}{48}$	$\frac{6.1}{43}$	$\frac{5.6}{32}$	$\frac{6.3}{26}$	$\frac{8.0}{25-21}$	$\frac{5.7}{19}$	$\frac{5.3}{14}$	4.7	$\frac{4.8}{6}$	$\frac{4.9}{20}$	$\frac{5.5}{29}$	$\frac{6.2}{31-40}$	$\frac{2.7}{45}$	$\frac{4.9}{50}$
$\frac{4.6}{54}$	$\frac{6.3}{58}$	$\frac{6.5}{43}$	$\frac{9.4}{64}$	$\frac{7.0}{67}$	$\frac{7.0}{100}$					$\frac{4.4}{166}$	$\frac{2.0}{144}$	$\frac{4.0}{100}$	$\frac{4.9}{72}$

Lake

Fuc

$\frac{4.4}{51-41}$	$\frac{6.7}{43}$	$\frac{6.1}{32}$	$\frac{6.7}{26}$	$\frac{7.6}{25-20}$	$\frac{6.1}{19}$	$\frac{5.3}{14}$	5.1	$\frac{5.3}{5}$	$\frac{5.8}{28}$	$\frac{6.6}{30-39}$	$\frac{4.2}{45}$	$\frac{6.0}{52}$	$\frac{4.9}{91}$
$\frac{6.5}{57-62}$	$\frac{8.7}{64}$	$\frac{8.4}{66}$	$\frac{6.5}{68}$	$\frac{7.3}{100}$						$\frac{4.7}{163}$	$\frac{2.3}{150}$	$\frac{1.4}{137}$	$\frac{4.0}{100}$

Lake

FL

8.29

5.2

F.L.
8.44

$\frac{4.1}{47}$	$\frac{6.2}{42}$	$\frac{6.1}{33}$	$\frac{6.4}{26}$	$\frac{7.8}{25-21}$	$\frac{5.4}{18}$	$\frac{5.1}{13}$	4.6	$\frac{4.9}{6}$	$\frac{5.8}{26}$	$\frac{6.7}{31}$	$\frac{6.6}{38}$	$\frac{4.3}{42}$	$\frac{5.7}{49}$	$\frac{4.8}{92}$
$\frac{5.0}{52}$	$\frac{6.8}{58}$	$\frac{6.7}{61}$	$\frac{8.4}{62}$	$\frac{8.5}{66}$	$\frac{7.3}{67}$	$\frac{7.8}{100}$					$\frac{4.6}{165}$			

$\frac{4.1}{50}$	$\frac{4.8}{46}$	$\frac{6.7}{42}$	$\frac{6.6}{33}$	$\frac{7.7}{26}$	$\frac{6.0}{25-20}$	$\frac{5.9}{18}$	5.5	$\frac{5.6}{6}$	$\frac{6.6}{39}$	$\frac{4.6}{44}$	$\frac{5.9}{49}$	$\frac{4.9}{48}$	$\frac{1.2}{128}$
$\frac{7.5}{58}$	$\frac{8.2}{63}$	$\frac{8.4}{65}$	$\frac{7.7}{67}$	$\frac{7.3}{100}$						$\frac{4.5}{170}$	$\frac{3.8}{164}$	$\frac{4.1}{156}$	

Fuc

$\frac{5.6}{43}$	$\frac{5.7}{32}$	$\frac{5.9}{26}$	$\frac{7.6}{25-20}$	$\frac{5.2}{18}$	$\frac{4.9}{13}$	4.7	$\frac{4.9}{6}$	$\frac{4.7}{49}$	$\frac{3.8}{99}$	$\frac{2.2}{124}$	$\frac{0.3}{127}$	$\frac{0.0}{159}$
$\frac{3.4}{48}$	$\frac{4.3}{54}$	$\frac{6.2}{61}$	$\frac{7.5}{62-65}$	$\frac{6.8}{66}$	$\frac{7.0}{100}$							$\frac{4.5}{175}$

Sta

+

A

97.52

59

91.5

+98

24" X 38' C.M.

60

90.8

61

90.9

62

91.7

63

92.5

B.M.

91.2

File

$$\begin{array}{cccccccc}
 \frac{7.0}{4.9} & \frac{6.7}{32} & \frac{8.1}{26} & \frac{9.0}{25-21} & \frac{6.3}{18} & \frac{6.1}{13} & 6.0 & \frac{6.2}{7} \\
 \frac{4.8}{41} & \frac{5.3}{51} & \frac{4.8}{60} & \frac{7.8}{62} & \frac{9.2}{63-66} & \frac{8.4}{67-70} & \frac{5.7}{100} & \frac{6.3}{110}
 \end{array}$$

$$\begin{array}{cccc}
 \frac{7.7}{38} & \frac{6.6}{43} & \frac{7.4}{48} & \frac{6.4}{119} \\
 \frac{4.4}{141} & & &
 \end{array}$$

LoRe

FL-957

FL-951

File

$$\begin{array}{cccccccc}
 \frac{5.7}{51} & \frac{5.6}{46} & \frac{7.5}{41} & \frac{7.4}{32} & \frac{7.6}{24} & \frac{9.2}{22-19} & \frac{6.9}{18} & \frac{6.6}{12} \\
 \frac{8.2}{60} & \frac{8.4}{64} & \frac{9.4}{63-65} & \frac{8.5}{66} & \frac{8.5}{100} & 6.7 & \frac{6.8}{6} & \frac{7.0}{29}
 \end{array}$$

$$\begin{array}{cccccc}
 \frac{7.7}{32-39} & \frac{6.6}{43} & \frac{7.4}{47} & \frac{6.5}{206} & \frac{5.6}{208} & \frac{4.4}{149}
 \end{array}$$

File

$$\begin{array}{cccccccc}
 \frac{7.5}{42} & \frac{7.9}{32} & \frac{9.1}{25} & \frac{6.7}{24-21} & \frac{6.9}{18} & \frac{6.6}{12} & \frac{6.8}{6-26} & \frac{7.2}{75}
 \end{array}$$

$$\begin{array}{cccccc}
 \frac{7.0}{100} & \frac{6.2}{150} & \frac{2.7}{260} & \frac{3.6}{215} & \frac{4.4}{49} & \frac{8.4}{61-65}
 \end{array}$$

File

$$\begin{array}{cccccccc}
 \frac{4.9}{51} & \frac{4.6}{48} & \frac{6.7}{42} & \frac{7.4}{32} & \frac{8.8}{23-20} & \frac{6.5}{18} & \frac{6.2}{13} & \frac{6.2}{7-34}
 \end{array}$$

$$\begin{array}{cccc}
 \frac{7.3}{34-37} & \frac{7.2}{42-85} & \frac{5.5}{150} & \frac{3.3}{111}
 \end{array}$$

File

$$\begin{array}{cccccccc}
 \frac{4.5}{51} & \frac{4.4}{41} & \frac{6.5}{43} & \frac{7.2}{32} & \frac{8.4}{23-20} & \frac{6.1}{18} & \frac{5.7}{13} & \frac{5.4}{7-12}
 \end{array}$$

$$\begin{array}{cccccc}
 \frac{6.9}{15} & \frac{6.6}{45} & \frac{4.4}{100} & \frac{2.4}{144} & \frac{7.9}{66} & \frac{7.3}{100}
 \end{array}$$

Sta + π -
897.52

64 93.0

0 10.58 903.09 5.01 92.51[✓]

65 93.1

66 94.7

67 96.4

+61 Vert Break in Sec Rt.

68 97.9

OBV. 10.40 902.91[✓] 10.58 92.51[✓]

0 10.65 911.37[✓] 1.59 901.32[✓]

10-12

$SS = \text{SameSlope}$

$\frac{6.8}{38} \frac{7.0}{32} \frac{7.1}{25} \frac{8.0}{24} \frac{5.8}{18} \frac{5.1}{12} 4.5 \frac{4.8}{7} \frac{4.7}{12} \frac{6.1}{14-15} \frac{5.3}{16} \frac{3.3}{55} \frac{2.1}{80}$
 $\frac{5.2}{44} \frac{4.9}{50} \frac{7.1}{58} \frac{7.3}{61} \frac{8.5}{62-65} \frac{7.6}{66} \frac{7.2}{100} \frac{3.8}{206} \frac{3.2}{161} \frac{2.9}{123} \frac{2.0}{100}$

$\frac{9.9}{100}$	$\frac{11.2}{25}$	$\frac{12.8}{24.20}$	$\frac{10.3}{18}$	$\frac{10.5}{15}$	$\frac{10.3}{12}$	10.0	$\frac{10.2}{7}$	$\frac{10.4}{12}$	$\frac{11.8}{15}$	$\frac{12.0}{37}$	$\frac{11.0}{68}$	$\frac{7.9}{157}$	$\frac{7.0}{20}$
-------------------	-------------------	----------------------	-------------------	-------------------	-------------------	------	------------------	-------------------	-------------------	-------------------	-------------------	-------------------	------------------

$\frac{5.8}{100}$ $\frac{7.3}{80}$ $\frac{9.0}{19}$ $\frac{8.1}{12}$ 8.4 $\frac{8.8}{7}$ $\frac{8.5}{14}$ $\frac{9.2}{17}$ $\frac{9.3}{45}$ $\frac{8.0}{75}$ $\frac{5.5}{98}$ $\frac{2.8}{145}$ $\frac{1.1}{200}$

$\frac{6.7}{100}$ $\frac{6.0}{49}$ $\frac{6.6}{33}$ $\frac{6.2}{20}$ $\frac{7.2}{12}$ 6.7 $\frac{7.1}{8}$ $\frac{7.6}{14}$ $\frac{7.2}{25}$ $\frac{3.7}{42}$ $\frac{2.9}{64}$ $\frac{1.0}{100}$ $\frac{3.5}{200}$

$$\frac{4.5}{100} \quad \frac{3.9}{88} \quad \frac{3.0}{58} \quad \frac{6.0}{41} \quad \frac{5.8}{12} \quad 5 \quad 2 \quad \frac{5.4}{7} \quad \frac{5.5}{15} \quad \frac{2.8}{20} \quad \frac{0.6}{22} \quad \frac{0.0}{34} \quad \frac{+4.2}{100}$$

Top Rd. Last TP.

Sta

+

K

-

911.37

69

99.4

70

00.4

71

01.5

72

02.8

73

04.2

74

05.8

75

06.9

O

6.37

913.75

3.99

907.38

$$\frac{10.1}{100} \quad \frac{9.0}{51} \quad \frac{12.1}{33} \quad \frac{12.4}{21} \quad \frac{12.6}{11} \quad 12.0 \quad \frac{12.3}{8-14} \quad \frac{7.1}{23} \quad \frac{6.4}{29} \quad \frac{5.5}{100} \quad \frac{4.8}{135} \quad \frac{5.8}{200}$$

$$\frac{10.3}{100} \quad \frac{9.3}{46} \quad \frac{11.6}{30-12} \quad 11.0 \quad \frac{11.2}{7} \quad \frac{11.0}{12} \quad \frac{8.5}{19} \quad \frac{8.2}{62} \quad \frac{8.9}{169} \quad \frac{9.5}{200}$$

$$\frac{10.3}{100} \quad \frac{10.2}{59} \quad \frac{8.2}{51-46} \quad \frac{10.0}{36} \quad \frac{9.9}{21} \quad \frac{10.3}{11} \quad 9.9 \quad \frac{10.4}{7-12} \quad \frac{12.5}{20} \quad \frac{12.7}{25} \quad \frac{13.2}{76-100} \quad \frac{14.5}{200}$$

$$\frac{9.4}{100} \quad \frac{10.1}{62} \quad \frac{5.9}{46-45} \quad \frac{8.7}{31} \quad \frac{8.9}{22} \quad \frac{8.5}{19} \quad \frac{8.9}{10} \quad 8.6 \quad \frac{9.1}{9} \quad \frac{9.5}{13} \quad \frac{11.0}{20} \quad \frac{11.9}{32} \quad \frac{13.7}{100} \quad \frac{12.7}{200}$$

$$\frac{8.1}{100} \quad \frac{7.7}{59} \quad \frac{4.9}{44-47} \quad \frac{7.8}{33} \quad \frac{8.0}{20} \quad \frac{7.5}{11} \quad 7.2 \quad \frac{7.6}{16} \quad \frac{7.5}{15} \quad \frac{6.6}{17} \quad \frac{6.7}{28} \quad \frac{7.0}{62} \quad \frac{7.1}{100} \quad \frac{5.2}{200}$$

$$\frac{4.4}{100} \quad \frac{3.7}{89} \quad \frac{2.8}{60} \quad \frac{2.1}{59} \quad \frac{2.4}{53} \quad \frac{5.8}{33} \quad \frac{6.0}{17} \quad \frac{6.4}{12} \quad 5.8 \quad \frac{6.2}{9} \quad \frac{6.0}{15} \quad \frac{6.5}{20} \quad \frac{6.2}{23} \quad \frac{2.8}{29} \quad \frac{2.5}{58} \quad \frac{1.9}{94} \quad \frac{7.5}{200}$$

$$\frac{0.5}{100} \quad \frac{0.3}{90} \quad \text{over 41.} \quad \frac{+50}{55} \quad \frac{3.7}{37} \quad \frac{4.9}{15} \quad \frac{5.1}{12} \quad 4.5 \quad \frac{4.7}{9} \quad \frac{4.6}{16} \quad \frac{3.9}{23} \quad \frac{0.2}{30} \quad \frac{1.2}{47} \quad \frac{2.5}{100} \quad \frac{4.1}{200}$$

913.75

76

07.5

77

08.4

78

09.0

+77

10.2

+83

10.3

+94

Shoulder

10.5

79

10.6

79+10.7

4 Hodgson Rd.

10.7

B.M.

153

912.22

~~912.07~~ = 912.06

$$\begin{array}{cccccccccccccccc} \frac{2.4}{100} & \frac{3.6}{73} & \frac{4.8}{51} & \frac{6.3}{39} & \frac{6.9}{29} & \frac{6.6}{19} & \frac{6.7}{11} & 6.3 & \frac{6.5}{9} & \frac{6.3}{17} & \frac{6.7}{20} & \frac{6.4}{25} & \frac{4.0}{31} & \frac{4.2}{35} & \frac{5.1}{72} \\ & & & & & & & & & & & & \frac{8.4}{200} & \frac{6.8}{100} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{7.0}{100} & \frac{7.3}{77} & \frac{6.8}{58} & \frac{5.8}{37} & \frac{5.3}{18} & \frac{5.6}{12} & \frac{5.9}{10} & 5.4 & \frac{5.8}{9} & \frac{6.0}{15} & \frac{7.7}{23} & \frac{8.2}{32} & \frac{8.6}{40} & \frac{8.7}{77} & \frac{8.4}{100} \\ & & & & & & & & & & & & \frac{6.3}{200} & \frac{7.7}{150} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{8.0}{100} & \frac{8.1}{67} & \frac{6.4}{41} & \frac{6.1}{23} & \frac{5.1}{14} & \frac{5.4}{11} & 4.8 & \frac{5.3}{9} & \frac{5.7}{13} & \frac{9.8}{25} & \frac{9.5}{29} & \frac{8.3}{32} & \frac{8.1}{37} & \frac{7.4}{73} & \frac{7.2}{100} \\ & & & & & & & & & & & & \frac{5.6}{200} & \frac{7.0}{150} \end{array}$$

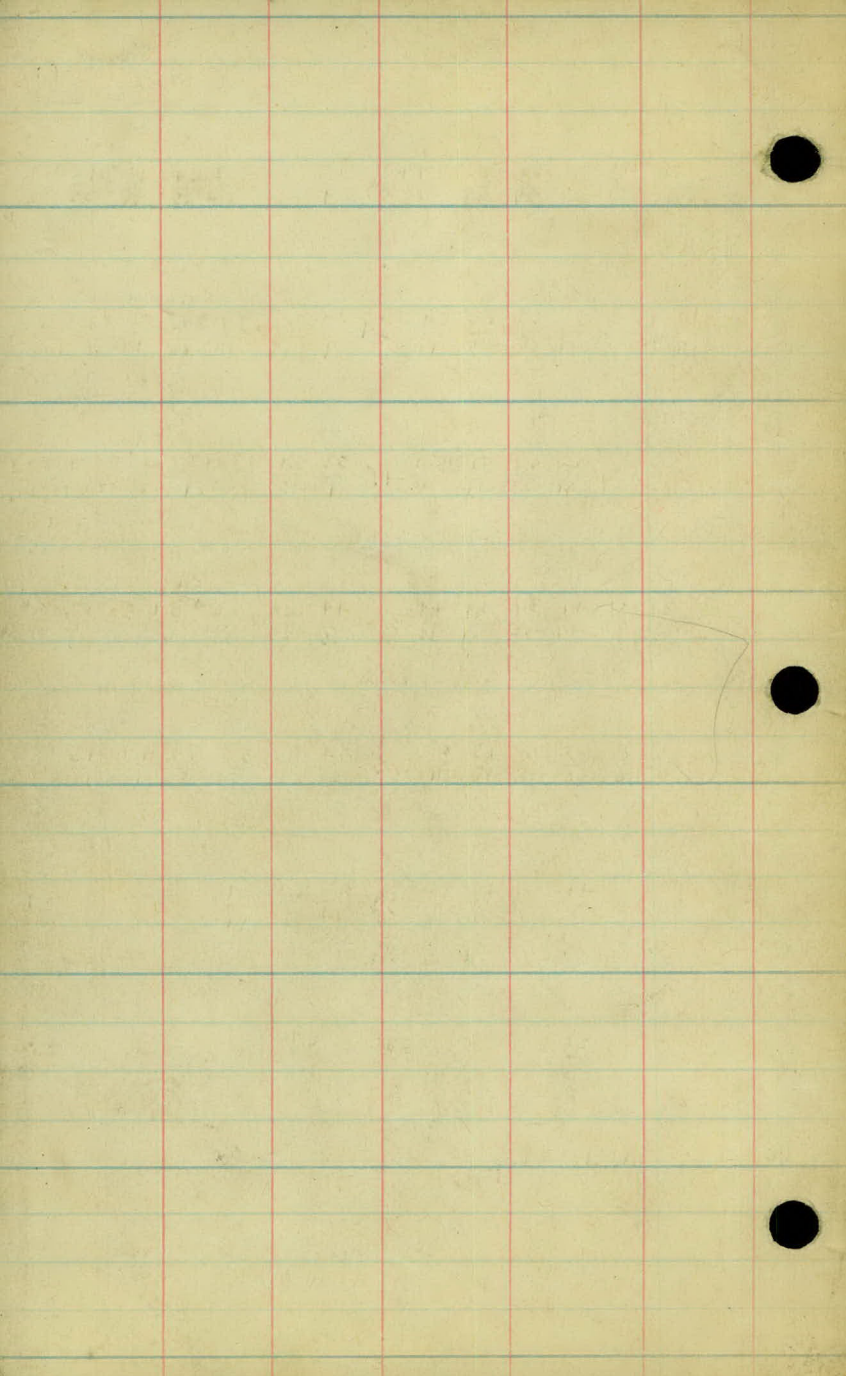
$$\begin{array}{cccccccccccccccc} \frac{2.7}{100} & \frac{3.1}{89} & \frac{4.1}{59} & \frac{3.7}{32} & \frac{3.9}{19} & \frac{4.4}{15} & 3.6 & \frac{4.4}{15} & \frac{6.2}{25} & \frac{6.6}{33} & \frac{5.9}{66} & \frac{5.0}{100} & \frac{5.2}{115} & \frac{3.8}{200} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{6.2}{100} & \frac{6.3}{66} & \frac{5.6}{30} & \frac{4.5}{22} & \frac{3.8}{11} & 3.5 & \frac{4.4}{20} & \frac{6.2}{33} & \frac{5.5}{59} & \frac{5.2}{83} & \frac{4.9}{100} & \frac{4.5}{165} & \frac{3.8}{200} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{4.1}{100} & \frac{4.0}{46} & \frac{3.8}{32} & \frac{3.8}{22} & 3.3 & \frac{3.6}{24} & \frac{3.7}{52} & \frac{2.9}{94} & \frac{2.7}{200} \\ & & & & 3.2 & & & & \end{array}$$

$$\begin{array}{cccc} \frac{3.8}{100} & 3.1 & \frac{2.7}{100} & \frac{2.3}{200} \end{array}$$

NE Cor Sub Ho Step



4/6/36

Alignment
Lexington Avenue
County Rd. I. to No. County Line

250+02.95 P.I.

249+27.97 P.C.

238+57.15 P.T.

Δ 52° 20' Lt.

D 36° 00

T 79.47

L 14537

237+91.25 P.I.

237+11.78 P.C.

210+96.73

3 Nails F. Coy - 34.35

3 Nails 15" B.O. 28.42 Bolt Spike

Δ 19° 18' Rt.

D 13° 00'

T 74.98

L 148.46

○ Nail

○ Nail

62.79 8" B.O. 3 Nails

○ Bolt Spike

26.78 18" B.O. 3 Nails

□ Mont E 1/4 Sec 3

○ Nail

County Rd I

□ Mont

285+62.18 P.C.

269+46

Hamline

263+52.80 P.O.T.

256+60.98 P.T.

A 56°43' Lt.

T 88.45

L 103.12

D 55°00'

E 14.77

256+16.31 P.I.

255+57.86 P.C.

250+76.43 P.T.

83.75 3 Nails 12" B. Elder

RR Spike

73.60

1 Nail 6" Apple Tree

Nail

61° 38.5

3 Nails 6" W.O.

3 Nails P.P.

44.22

32.13 - 0

Hub

3 Nails Old Stump

Nail

Nail

305+97.20

286+37.84 P.T.

286+08.00 P.I.

3 Nails 18" B. Elder



68.82

No C. Line

RR SpK

3 Nails P.P.

34.45

3 Nails P.P.

$\Delta 81^{\circ} 28' \text{ Rt}$

T 45.82'

D $140^{\circ} 00'$

L 7566

E 1701

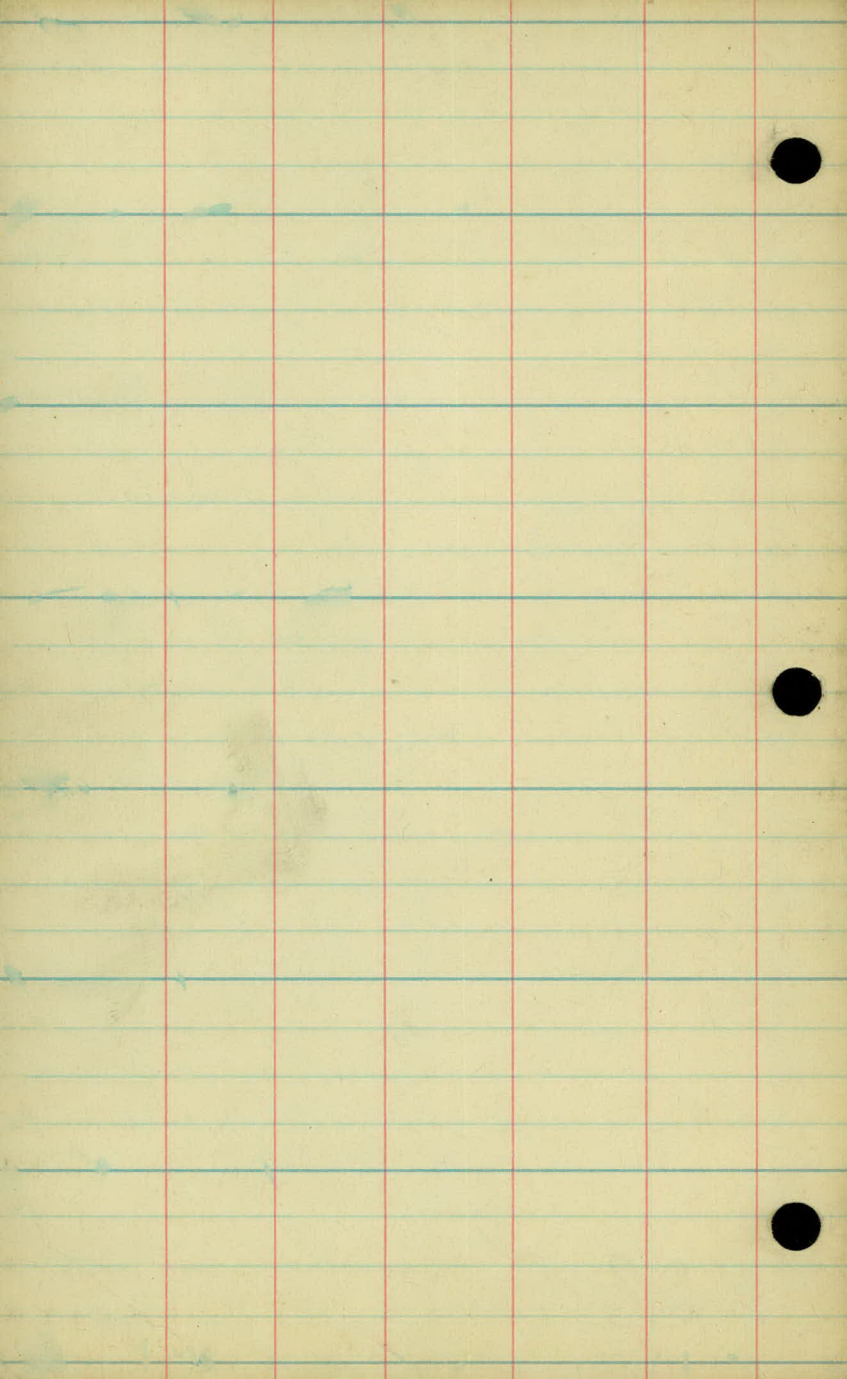
3 Nails F. Cor.

Boat SpK

21.12

39.42

3 Nails P.P.



4/11/36

H.T. Purcell

TOPOGRAPHY

LEXINGTON AVE

Co Road I to Hamline Ave

$$\frac{Rd}{7-15}$$

$$\frac{F.C.}{24}$$

$$\frac{+78 Rd Sn}{16}$$

$$\frac{+73 P.P.}{14}$$

$$\frac{+77 F.C.}{24-33}$$

215

214

$$\frac{Rd}{7-17}$$

$$\frac{+45 P.P.}{14}$$

213

212

$$\frac{Rd}{6-19}$$

$$\frac{+98 P.P.}{13}$$

$$\frac{+85 F.C.}{35}$$

211

Cultivated

Hay Field

Note.- For Lex. "I" Intersection
see Lex to "I" Survey

222

$$\frac{+97 \text{ PP}}{14}$$

$$\frac{\text{Fce}}{21}$$

221

$$\frac{\text{Rd}}{7-13}$$

$$\frac{\text{Fce}}{21}$$

220

$$\frac{+96 \text{ PP}}{14}$$

$$\frac{\text{Rd}}{7-14}$$

$$\frac{+86 \text{ 2 Trs}}{30}$$

$$\frac{+25 \text{ Tr}}{24}$$

$$\frac{+12 \text{ Tr}}{27}$$

$$\frac{\text{Fce}}{21}$$

219

$$\frac{+12 \text{ PP}}{14}$$

$$\frac{+81 \text{ Tr}}{31}$$

$$\frac{+61 \text{ 2 Trs}}{33}$$

$$\frac{+72 \text{ 2 Trs}}{38}$$

$$\frac{\text{Fce}}{22}$$

218

$$\frac{+86 \text{ 3 Trs}}{32}$$

$$\frac{\text{Rd}}{9-14}$$

$$\frac{+68 \text{ PP}}{14}$$

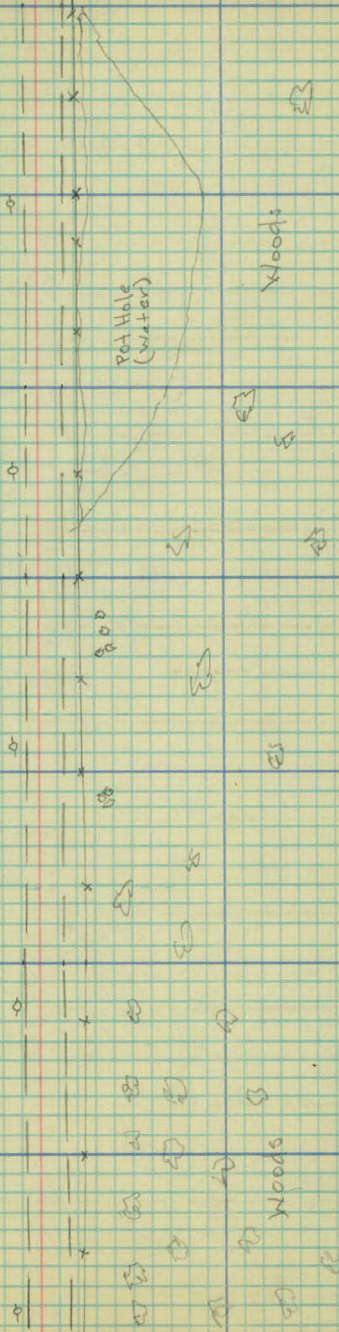
217

$$\text{Rd}$$

$$\frac{\text{Fce}}{23}$$

$$\frac{+19 \text{ PP}}{14}$$

216



$$\frac{Fcc}{11}$$

$$\frac{Fcc}{34}$$

$$\begin{array}{r} +12 Tr \\ 26 \\ +19 Tr \\ 29 \end{array} \quad \begin{array}{r} +15 Tr \\ 30 \\ +17 Tr \\ 30 \end{array} \quad \begin{array}{r} +13 Tr \\ 21 \end{array}$$

229

$$\frac{Fcc}{11}$$

$$R1 \\ 8-14$$

$$\frac{Fcc}{32}$$

$$\begin{array}{r} +13 PP \\ 10 \end{array}$$

$$\begin{array}{r} +18 Tr \\ 28 \\ +39 Stp \\ 29 \\ +55 Tr \\ 30 \\ +14 Tr \\ 26 \end{array} \quad \begin{array}{r} +85 Tr \\ 26 \\ +16 Tr \\ 28 \\ +38 Tr \\ 31 \end{array} \quad \begin{array}{r} +16 Tr \\ 26 \\ +17 Tr \\ 28 \end{array}$$

228

$$\frac{Fcc}{14}$$

$$\begin{array}{r} +37 Tr \\ 29 \\ +14 Tr \\ 26 \\ Fcc \\ 32 \end{array}$$

$$\begin{array}{r} +10 Tr \\ 29 \end{array}$$

$$\begin{array}{r} +35 PP \\ 11 \end{array}$$

$$\begin{array}{r} +11 Tr \\ 30 \\ +14 Tr \\ 30 \\ Fcc \\ 33 \end{array}$$

$$R1 \\ 8-13$$

$$\begin{array}{r} +13 Tr \\ 28 \\ +18 Stp - Tr \\ 27 \end{array}$$

$$\begin{array}{r} +19 Stp \\ 29 \\ +82 Tr \\ 26 \end{array}$$

227

$$\frac{Fcc}{14}$$

$$\begin{array}{r} +13 Stp \\ 21 \end{array}$$

$$\begin{array}{r} +11 PP \\ 12 \end{array}$$

$$\begin{array}{r} +55 Tr \\ 33 \\ +85 Tr \\ 34 \end{array}$$

226

$$\begin{array}{r} +12 Stp \\ 21 \\ +19 Stp \\ 23 \end{array}$$

$$\frac{Fcc}{19}$$

$$\begin{array}{r} +80 Tr \\ 34 \end{array}$$

$$\begin{array}{r} +88 Tr \\ 28 \end{array}$$

$$R4 \\ 9-15$$

$$\frac{Fcc}{38}$$

225

$$\begin{array}{r} +14 Stp \\ 17 \\ +13 PP \\ 13 \end{array}$$

$$\begin{array}{r} +15 FC \\ 17 \end{array}$$

$$\begin{array}{r} +15 FC \\ 21-33 \end{array}$$

$$\begin{array}{r} +10 Tr \\ 29 \end{array}$$

224

$$\begin{array}{r} +16 Tr \\ 27 \end{array}$$

$$\begin{array}{r} +52 Tr \\ 26 \end{array}$$

$$\begin{array}{r} +34 Tr \\ 34 \end{array}$$

$$\begin{array}{r} +18 Tr \\ 29 \end{array}$$

$$\begin{array}{r} +34 PP \\ 13 \end{array}$$

223

Brush & Steps

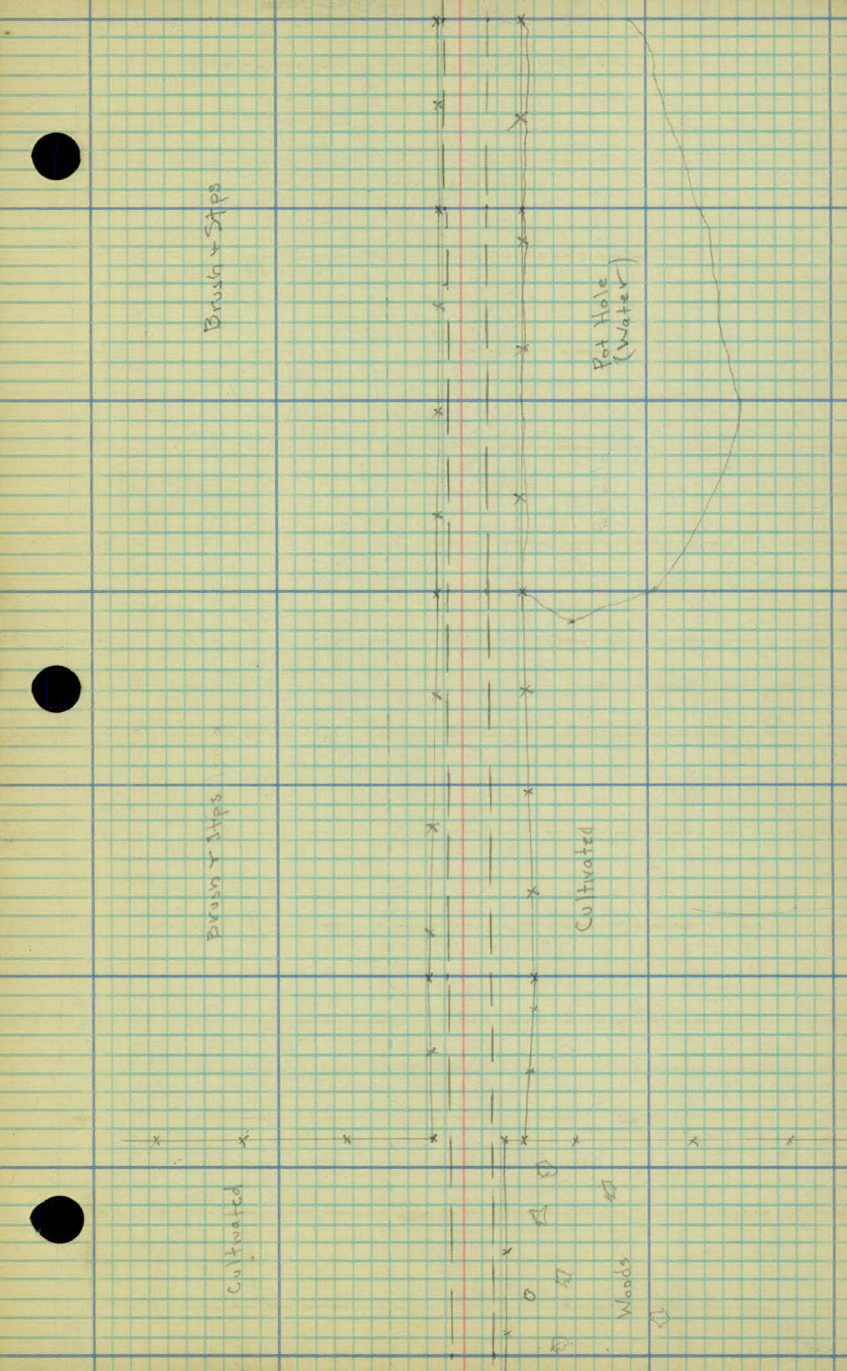
Brush & Steps

Pot Hole
(Water)

Cultivated

Cultivated

Woods



236

$$\frac{Rd}{10-15}$$

$$\frac{+75 Tr}{24}$$

$$\frac{+83 Tr}{23}$$

$$\frac{Fcc}{29}$$

$$\frac{+95 2 Trs}{31}$$

235

$$\frac{Fcc}{27}$$

234

$$\frac{Fcc}{27}$$

233

$$\frac{Rd}{9-13}$$

$$\frac{+92 Rd Sn}{25}$$

$$\frac{+15 Cor Ho}{153} \quad \frac{+55 Rd Ho}{17}$$

$$\frac{+65 Fc}{27}$$

232

$$\frac{+75 Tr}{24} \quad \frac{+92 PP}{09}$$

$$\frac{+90 Cor Ho}{207} \quad \frac{+68 Ent}{35}$$

$$\frac{+80 Tr}{35}$$

$$\frac{+27 Fc}{15} \quad \frac{+32 Tr}{32}$$

$$\frac{+47 Fc Cor}{26}$$

$$\frac{+57 Tr}{40}$$

$$\frac{+18 Tr}{20}$$

$$\frac{+09 Fc Cor}{34}$$

231

$$\frac{+57-12 \times 28 V.P.}{13-15} \quad \text{Flows West}$$

$$\frac{+44 PP}{10}$$

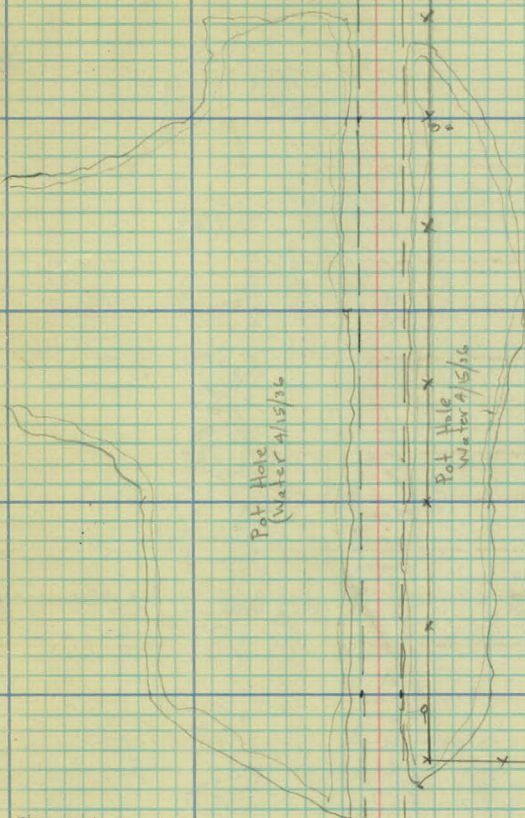
$$\frac{+40 Tr}{28}$$

$$\frac{+46 Tr}{28}$$

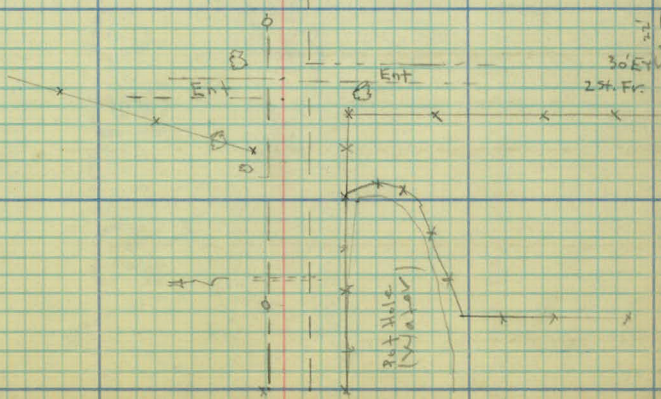
$$\frac{+06 Tr}{27}$$

$$\frac{+13 Tr}{30}$$

230



25 F. 18
37'



243

$$\frac{\text{Wood 3}}{50}$$

$$\frac{\text{Rd}}{13 \quad 10}$$

$$\frac{+85 \text{ Pot Hole}}{16}$$

242

$$\frac{+15 \text{ Brush \& Woods}}{33}$$

+15 Brush

241

$$\frac{+92 \text{ Rd Sh}}{9}$$

$$\frac{+33 \text{ Brush}}{32}$$

240

239

$$\frac{\text{Rd}}{13 \quad 12}$$

458

$$\frac{+85 \text{ Rd}}{24 \quad 9}$$

+28 Ent

$$\frac{+18 \text{ Floor}}{30}$$

+16 Tr

$$\frac{+00 \text{ Tr}}{21}$$

237

Cultivated

Woods

Pothole

Cultivated

Pothole

Brush

Ent

+45 Ent
+25 FC

250

+85 Tr
28

249

Fcc
19

Rd
12-11

248

Fcc
20

Rd
14-11

+58 StP
58

247

+97 StP
23

246

Rd
14-10

+45 Tr
21
+34 Tr
22

+61 Tr
25

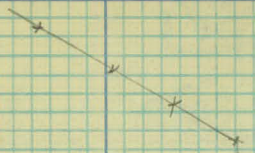
245

+94 Tr + Fc.

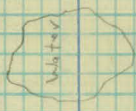
29
+88 Tr
35

+90 Tr
32

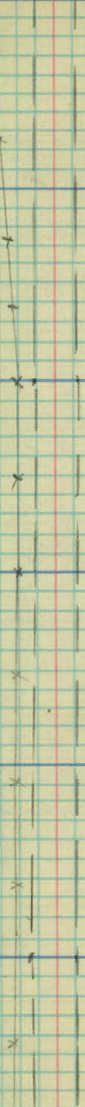
244



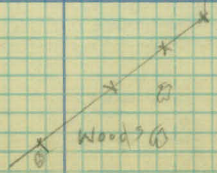
Cult.



Waste land



Wdy Field



Woods

256

+14 PP.

46

+92 Ent

+25-2 MB.

17

255

254

Rd
11-10

253

252

+57 No Amp Sn

14

251

250

Rd
12-9

Cult.

Cult



263

$$\frac{+100 PP}{29}$$

$$\frac{+76 \text{ Ap Trs}}{41-55}$$

262

$$\frac{Rd}{10-11}$$

$$+22 \text{ Ent}$$

261

$$\frac{+18 PP}{29}$$

260

$$\frac{+97 Rd Sm}{18}$$

$$\frac{+36 PP}{29}$$

259

258

$$\frac{Rd}{9-15}$$

$$\frac{+56 PP}{29}$$

257

W. Co

W. Co

W. Co

W. Co

W. Co Apple Trs.

W. Co

Cult.

Cult.

W. Co

W. Co

Water

270

$$\frac{+00 \text{ Rd}}{10-11}$$

$$\frac{+62 \text{ Shoulder}}{42}$$

$$+60 \text{ Ent}$$

$$\frac{+35 \text{ Shoulder}}{35}$$

$$\frac{+47 \text{ Rd Sn}}{15} \quad \frac{\text{Fcc Lbr}}{29}$$

269

$$\frac{+18 \text{ PP}}{58}$$

$$\frac{+16 \text{ Rd}}{12-11}$$

268

$$\frac{+88 \text{ P.P.}}{28}$$

$$\frac{\text{Fcc}}{29}$$

267

$$\frac{+08 \text{ PP}}{28}$$

$$\frac{\text{Fcc}}{29}$$

266

$$\frac{\text{Rd}}{10-13}$$

$$\frac{+87 \text{ Bq Fcc}}{28}$$

$$\frac{+53 \text{ S+P}}{14}$$

265

$$\frac{+42 \text{ Tr}}{51}$$

$$\frac{+65 \text{ P.R.}}{30}$$

$$\frac{+55 \text{ Ho}}{127}$$

$$+21 \text{ Ent}$$

$$\frac{+12 \text{ MB}}{13}$$

264

Hamline Ave

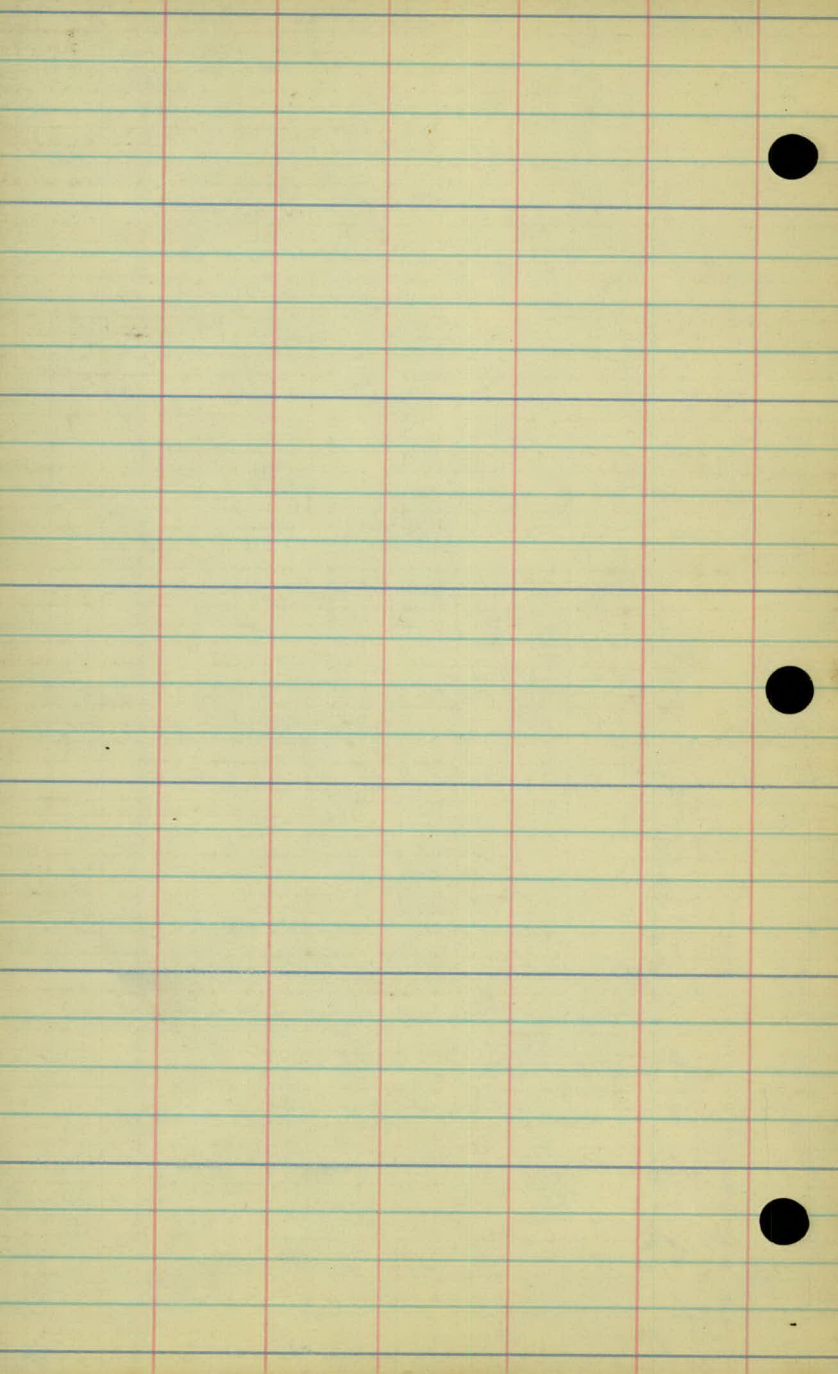
Colt

Water

Colt

0000

25-F



4/3/36

H.T. Portell

X-Section

Lexington Avenue

from

County Road I to No County Line

Sta	+	+	-	
BM.	8.16	900.16		892.00
211				92.4-
+10		Shoulder		
+15		Ditch		92.4-
212				93.1-
213				92.7-
214				94.2-
215				95.1-
①	9.78	908.71	123	898.93
216				96.4-

Top Mont Cor Lex. and Co. Rd. I

$$\frac{5.0}{100} \quad \frac{8.5}{62} \quad 7.8 \quad \frac{8.7}{100}$$

$$\frac{4.7}{100} \quad \frac{5.6}{28} \quad \frac{8.8}{18} \quad \frac{7.9}{7} \quad 7.8 \quad \frac{7.9}{12} \quad \frac{8.8}{27} \quad \frac{13.5}{33} \quad \frac{14.3}{100}$$

$$\frac{2.4}{100} \quad \frac{4.9}{32} \quad \frac{6.9}{15} \quad \frac{7.1}{6} \quad 7.1 \quad \frac{7.4}{18} \quad \frac{7.9}{26} \quad \frac{10.0}{32-100}$$

$$\frac{2.8}{100} \quad \frac{6.3}{32} \quad \frac{7.3}{14} \quad \frac{6.7}{14} \quad \frac{7.3}{7} \quad 7.5 \quad \frac{7.7}{19} \quad \frac{8.5}{20} \quad \frac{10.7}{35} \quad \frac{9.0}{100}$$

$$\frac{5.2}{100} \quad \frac{7.0}{32} \quad 29-20 \quad \frac{8.1}{20} \quad \frac{6.8}{11} \quad 6.0 \quad \frac{7.1}{18} \quad \frac{7.5}{25} \quad \frac{9.7}{35} \quad \frac{9.5}{100}$$

$$\frac{8.0}{80} \quad \frac{1.3}{42} \quad \frac{0.8}{26} \quad \frac{5.0}{20-13} \quad \frac{5.2}{9} \quad 5.1 \quad \frac{5.5}{15} \quad \frac{5.6}{21} \quad \frac{5.7}{31} \quad \frac{5.8}{41} \quad \frac{5.8}{100}$$

Nail in PP. 1st Sta 21L+15

$$\frac{3.4}{100} \quad \frac{3.1}{40} \quad \frac{11.2}{31} \quad \frac{11.5}{21} \quad \frac{12.4}{12} \quad 12.3 \quad \frac{12.6}{14} \quad \frac{13.0}{42} \quad \frac{8.9}{45} \quad \frac{10.1}{100}$$

Sta

+

K

-

908.71 ✓

217

98.5

218

900.0

219

01.0

BM.

7.56

901.15 ✓

220

00.9

221

00.6

0

0.76

903.85 ✓

562

903.09 ✓

222

99.7

223

99.4

224

98.7

L.O. $\frac{00}{100}$ $\frac{0.9}{80-47}$ $\frac{7.6}{42}$ $\frac{10.9}{36}$ $\frac{10.5}{8}$ 10.2 $\frac{10.5}{13}$ $\frac{10.6}{18}$ $\frac{10.1}{30}$ $\frac{9.5}{39}$ $\frac{5.8}{48}$ $\frac{10.3}{100}$

$\frac{4.7}{100-72}$ $\frac{2.3}{28}$ $\frac{7.3}{22}$ $\frac{9.0}{17}$ $\frac{8.8}{9}$ 8.7 $\frac{8.8}{12}$ $\frac{7.0}{19}$ $\frac{7.6}{29}$ $\frac{4.3}{30}$ $\frac{8.8}{100}$

$\frac{8.8}{100}$ $\frac{7.4}{99}$ $\frac{5.0}{24}$ $\frac{7.7}{18}$ $\frac{8.2}{12}$ $\frac{7.9}{8}$ 7.7 $\frac{7.9}{12}$ $\frac{8.0}{19}$ $\frac{7.2}{30}$ $\frac{3.7}{36}$ $\frac{5.5}{100}$

RRSpk Ctr Rd Sta 219409.97

$\frac{8.8}{100}$ $\frac{9.1}{40}$ $\frac{7.5}{19}$ $\frac{7.9}{9}$ 7.8 $\frac{8.0}{12}$ $\frac{7.8}{18}$ $\frac{7.1}{29}$ $\frac{5.8}{41}$ $\frac{5.5}{100}$

$\frac{6.1}{100}$ $\frac{7.0}{18}$ $\frac{6.7}{12}$ $\frac{8.0}{6}$ 8.1 $\frac{8.3}{13-22}$ $\frac{9.5}{27}$ $\frac{10.2}{39}$ $\frac{8.6}{100}$

Nail in P.P. Lt. 220+70

$\frac{2.2}{100}$ $\frac{1.9}{13}$ $\frac{4.3}{7}$ 4.2 $\frac{4.3}{13}$ $\frac{4.6}{19}$ $\frac{7.2}{25}$ $\frac{8.0}{30}$ $\frac{5.7}{75}$ $\frac{3.7}{100}$

$\frac{4.2}{100}$ $\frac{3.9}{18}$ $\frac{4.7}{9}$ 4.5 $\frac{4.7}{13}$ $\frac{4.4}{21}$ $\frac{5.3}{47}$ $\frac{1.7}{100}$

$\frac{11.0}{100}$ $\frac{9.2}{99}$ $\frac{8.3}{31}$ $\frac{5.6}{9}$ 5.2 $\frac{5.5}{14}$ $\frac{5.3}{19}$ $\frac{3.5}{29}$ $\frac{1.5}{36}$ $\frac{+3.0}{100}$

Sta. + π $\swarrow$ -
 903.85

0 582 $\swarrow$
 905.58 3.04 $\swarrow$
 908.76

225 98.1

226 97.0

B.M. 2.85 $\swarrow$
 899.63 9.80 $\swarrow$
 896.78

227 95.2

228 94.5

229 94.6

230 94.5

231 95.0

$$\begin{array}{cccccccccccc} \frac{13.4}{100} & \frac{13.1}{64} & \frac{8.5}{15} & \frac{8.9}{10} & 8.5 & \frac{9.2}{15} & \frac{9.5}{27} & \frac{8.9}{31} & \frac{2.2}{40} & \frac{1.6}{100} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{15.0}{100-84} & \frac{11.8}{39} & \frac{9.5}{19} & \frac{10.3}{15} & \frac{10.0}{10} & 9.6 & \frac{10.0}{13} & \frac{10.9}{24} & \frac{11.3}{30} & \frac{4.5}{41} & \frac{5.6}{100} \end{array}$$

RR. SpK in 30" Oak 50' Rt Sta 226+75

$$\begin{array}{cccccccccccc} \frac{7.9}{100-43} & \frac{7.2}{22} & \frac{5.3}{15} & \frac{4.7}{10} & 4.4 & \frac{4.6}{11} & \frac{4.7}{26} & \frac{6.3}{46} & \frac{6.1}{100} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{7.2}{100-37} & \frac{6.8}{17} & \frac{5.6}{12} & \frac{5.3}{8} & 5.1 & \frac{5.4}{14} & \frac{6.1}{28} & \frac{7.3}{33} & \frac{9.0}{100} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{7.0}{100} & \frac{7.1}{14} & \frac{5.2}{11-5} & 5.0 & \frac{5.3}{14} & \frac{5.9}{25} & \frac{7.4}{35} & \frac{9.4}{100} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{7.0}{100} & \frac{6.6}{13} & \frac{5.4}{10} & \frac{5.2}{4} & 5.1 & \frac{5.4}{15} & \frac{6.0}{23-30} & \frac{7.6}{35} & \frac{9.0}{100} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{7.6}{100-66} & \frac{6.6}{15} & \frac{5.0}{11} & \frac{4.7}{6} & 4.6 & \frac{4.8}{14} & \frac{5.4}{27} & \frac{6.1}{34} & \frac{5.7}{52} & \frac{3.0}{100} \end{array}$$

Sta	+	π	-
		899.63	

232			95.9
-----	--	--	------

233			96.1
-----	--	--	------

234			96.5
-----	--	--	------

0	4.77	902.06	2.34	897.29
---	------	--------	------	--------

235			96.3
-----	--	--	------

236			96.8
-----	--	--	------

237			98.1
-----	--	--	------

B.M.	6.88	905.71	3.23	898.83
------	------	--------	------	--------

+86	Ctr Curve		99.9
-----	-----------	--	------

239			00.2
-----	--	--	------

240			99.0
-----	--	--	------

$$\frac{1.6}{100} \quad \frac{1.9}{20} \quad \frac{4.1}{16} \quad \frac{3.8}{5} \quad 3.7 \quad \frac{3.9}{15} \quad \frac{4.9}{21} \quad \frac{3.7}{33} \quad \frac{3.0}{34} \quad \frac{+1.0}{87} \quad \frac{+2.0}{100}$$

$$\frac{6.2}{100} \quad \frac{6.8}{50} \quad \frac{6.2}{19} \quad \frac{4.2}{16} \quad \frac{4.0}{9} \quad 3.5 \quad \frac{3.9}{14} \quad \frac{4.8}{21} \quad \frac{5.4}{31} \quad \frac{5.7}{40} \quad \frac{4.2}{65} \quad \frac{0.8}{100}$$

$$\frac{6.0}{100} \quad \frac{6.3}{46} \quad \frac{6.4}{21} \quad \frac{4.2}{13} \quad \frac{3.6}{10} \quad 3.1 \quad \frac{3.6}{15} \quad \frac{4.8}{20} \quad \frac{5.4}{43} \quad \frac{4.9}{58} \quad \frac{6.0}{100}$$

$$\frac{8.5}{100} \quad \frac{7.6}{16} \quad \frac{6.7}{15} \quad \frac{6.0}{5} \quad 5.8 \quad \frac{6.2}{14} \quad \frac{7.4}{22} \quad \frac{8.4}{45} \quad \frac{6.4}{100}$$

$$\frac{10.8}{100} \quad \frac{8.8}{21} \quad \frac{7.7}{16} \quad \frac{6.4}{13} \quad \frac{5.7}{6} \quad 5.3 \quad \frac{6.2}{15} \quad \frac{6.8}{23} \quad \frac{6.0}{21} \quad \frac{7.6}{36} \quad \frac{6.5}{69} \quad \frac{3.2}{100}$$

$$\frac{5.7}{100} \quad \frac{2.7}{34} \quad \frac{4.9}{29} \quad \frac{6.0}{23} \quad \frac{4.5}{10} \quad 4.0 \quad \frac{4.4}{14} \quad \frac{4.8}{20} \quad \frac{3.1}{33} \quad \frac{5.0}{46} \quad \frac{2.4}{60} \quad \frac{6.8}{100}$$

SpK. in 24" Oak Rt. Sta 237

$$\frac{6.5}{100} \quad \frac{2.6}{36} \quad \frac{6.8}{29} \quad \frac{7.2}{21} \quad 5.8 \quad \frac{5.7}{7} \quad \frac{6.3}{17} \quad \frac{4.5}{28} \quad \frac{6.1}{34} \quad \frac{7.3}{100}$$

$$\frac{6.3}{100} \quad \frac{3.4}{28} \quad \frac{6.8}{21} \quad \frac{6.2}{14} \quad 5.5 \quad \frac{5.7}{14} \quad \frac{5.0}{15} \quad \frac{6.5}{100}$$

$$\frac{10.9}{100} \quad \frac{6.7}{46} \quad \frac{7.1}{21} \quad \frac{7.1}{13} \quad 6.7 \quad \frac{7.1}{11} \quad \frac{8.0}{68} \quad \frac{11.3}{100}$$

Sta + ∇ -
905.71

241 98.0

242 97.3

○ 818 ∇ 904.24 906.5 ∇ 896.06

243 96.0

244 95.7

245 96.3

246 97.0

247 97.6

BM 1.74 ∇ 902.50

$$\frac{9.9}{100} \quad \frac{8.8}{22} \quad \frac{8.0}{13} \quad 7.7 \quad \frac{8.3}{11} \quad \frac{10.0}{15} \quad \frac{13.6}{82} \quad \frac{14.3}{100}$$

$$\frac{8.3}{100} \quad \frac{10.0}{30} \quad \frac{10.8}{26} \quad \frac{11.1}{17} \quad \frac{9.2}{13} \quad 8.4 \quad \frac{8.7}{11} \quad \frac{9.6}{14} \quad \frac{11.1}{77} \quad \frac{13.0}{100}$$

Nail in Gr. Road 243+00

$$\frac{13.0}{100} \quad \frac{13.0}{40} \quad \frac{12.3}{19} \quad \frac{9.0}{14} \quad 8.2 \quad \frac{8.4}{8} \quad \frac{8.8}{12} \quad \frac{11.2}{16} \quad \frac{11.7}{27} \quad \frac{11.0}{100}$$

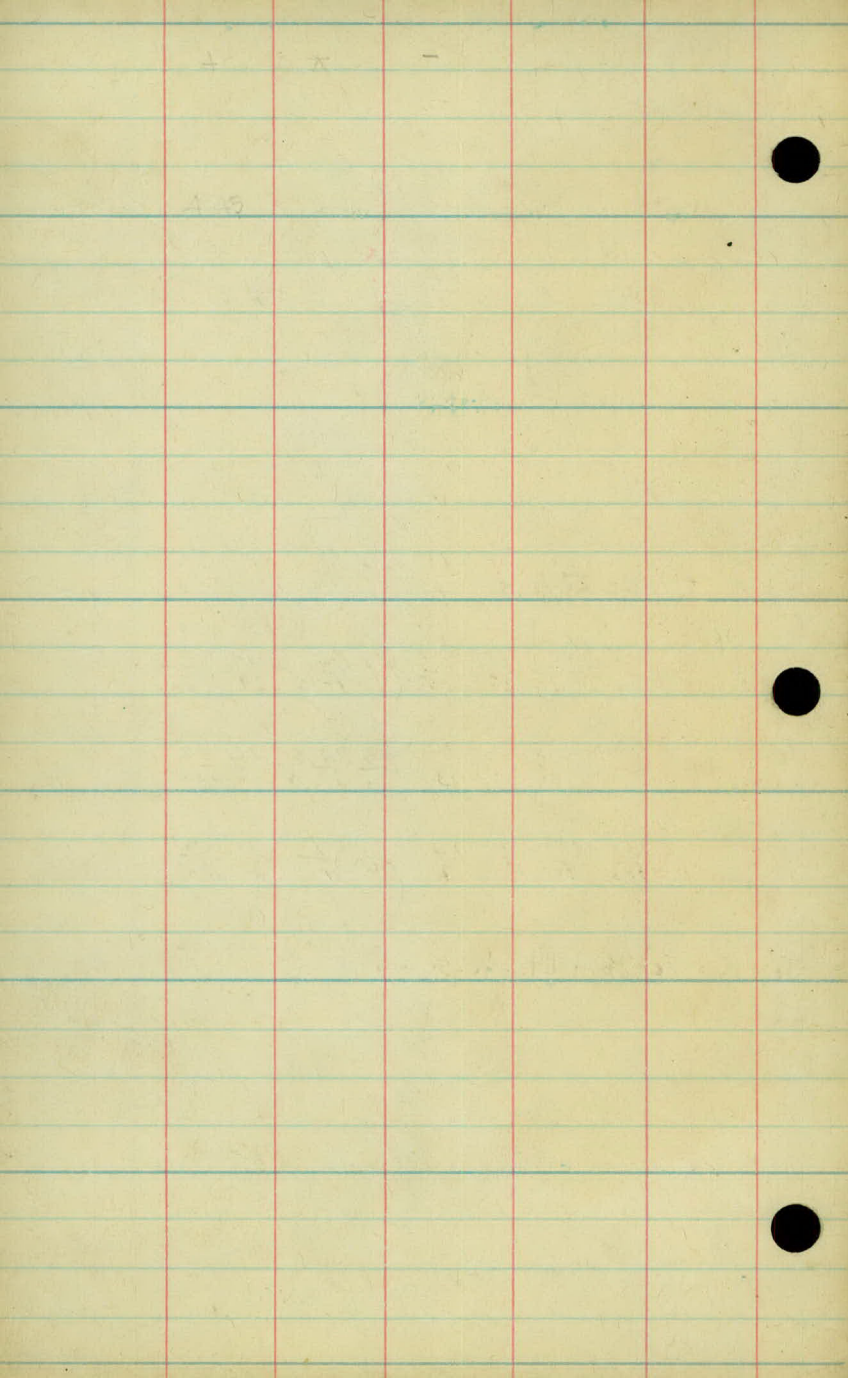
$$100 = \frac{13.0}{40} \quad \frac{11.9}{18} \quad \frac{9.3}{14} \quad 8.5 \quad \frac{8.8}{12} \quad \frac{11.3}{17} \quad \frac{10.5}{100}$$

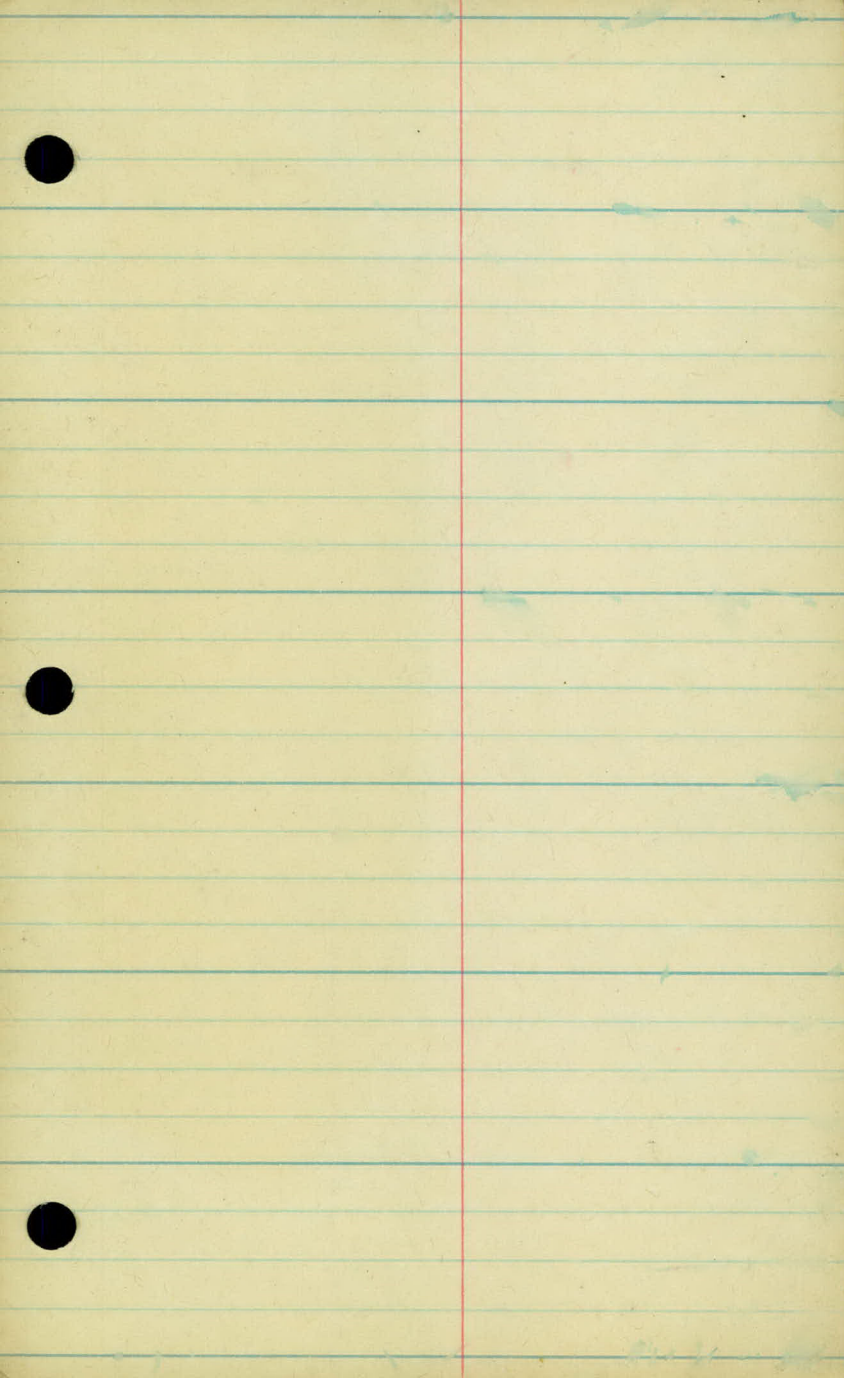
$$\frac{13.5}{100} \quad \frac{12.3}{66} \quad \frac{9.8}{28} \quad \frac{8.4}{15} \quad 7.9 \quad \frac{8.2}{9-15} \quad \frac{4.2}{29} \quad \frac{3.3}{100}$$

$$\frac{14.0}{100} \quad \frac{8.5}{38} \quad \frac{7.1}{18} \quad \frac{7.7}{13} \quad 7.2 \quad \frac{7.3}{8} \quad \frac{6.1}{18} \quad \frac{1.2}{48} \quad \frac{1.5}{100}$$

$$\frac{14.0}{100} \quad \frac{8.8}{20} \quad \frac{7.8}{18} \quad \frac{7.4}{14} \quad 6.6 \quad \frac{6.7}{11} \quad \frac{5.7}{16} \quad \frac{2.6}{100}$$

Top Cor Fac Post Lt. Sta 250+00





+ π -

0 7.10 909.60 ✓ 902.50 ✓

248 7.05 909.55 ✓ 710 902.50 ✓ 98.7

249 98.2

ctr Curve 98.7

251 98.8

252 99.8

253 01.2

354 02.8

Top Cor F.P. Lt Sta 250+

$\frac{17.2}{100}$ $\frac{12.4}{39}$ $\frac{11.5}{18}$ $\frac{10.8}{13}$ 10.9 $\frac{11.1}{10}$ $\frac{10.7}{16}$ $\frac{9.8}{27}$ $\frac{10.6}{100}$

$\frac{18.4}{100}$ $\frac{10.0}{40}$ $\frac{9.6}{25}$ $\frac{11.8}{15}$ $\frac{11.6}{12}$ 11.4 $\frac{11.7}{11}$ $\frac{10.9}{19}$ $\frac{9.4}{28}$ $\frac{12.5}{100}$

$\frac{17.4}{100}$ $\frac{9.8}{19}$ $\frac{10.8}{9}$ 10.7 $\frac{11.1}{12}$ $\frac{10.1}{21}$ $\frac{8.0}{50}$ $\frac{10.3}{100}$

$\frac{11.2}{100}$ $\frac{9.0}{57}$ $\frac{9.3}{19}$ $\frac{10.8}{10}$ 10.8 $\frac{11.0}{11}$ $\frac{11.7}{20}$ $\frac{12.1}{44}$ $\frac{8.7}{100}$

$\frac{5.0}{100}$ $\frac{5.2}{53}$ $\frac{8.2}{31}$ $\frac{8.8}{21}$ $\frac{9.8}{12}$ 9.8 $\frac{10.1}{8-13}$ $\frac{12.3}{18}$ $\frac{14.0}{32}$ $\frac{7.8}{100}$

$\frac{3.8}{100}$ $\frac{8.0}{48}$ $\frac{7.8}{17}$ $\frac{8.4}{10}$ 8.4 $\frac{8.6}{10}$ $\frac{8.8}{27}$ $\frac{5.0}{100}$

$\frac{5.1}{100}$ $\frac{3.7}{47}$ $\frac{4.2}{17}$ $\frac{7.4}{13}$ $\frac{6.9}{10}$ 6.8 $\frac{7.2}{10}$ $\frac{4.6}{43}$ $\frac{5.6}{87-100}$

✓
909.55

255

04.0

↑
111
↓

256+11

ctr curve

05.4

257

05.9

258

05.6

259

05.6

0

5.02

✓
910.57

4.00

✓
905.55

260

05.8

261

05.6

262

05.4

$$\frac{4.7}{100} \quad \frac{6.5}{49} \quad \frac{5.4}{16} \quad \frac{5.7}{10} \quad 5.6 \quad \frac{5.8}{10} \quad \frac{5.4}{23} \quad \frac{5.0}{100}$$

$$\frac{3.0}{100} \quad \frac{3.2}{23} \quad \frac{5.1}{16} \quad 4.2 \quad \frac{4.2}{9} \quad \frac{3.9}{18} \quad \frac{2.0}{23} \quad \frac{0.4}{100}$$

$$m - \frac{0.5}{75} \quad \frac{2.8}{17} \quad \frac{3.8}{8} \quad 3.7 \quad \frac{4.1}{15} \quad \frac{5.4}{27} \quad \frac{6.6}{35} \quad \frac{5.7}{100}$$

$$\frac{8.9}{100} \quad \frac{3.9}{11} \quad \frac{4.1}{7} \quad 4.0 \quad \frac{4.2}{15} \quad \frac{3.7}{20} \quad \frac{7.5}{55} \quad \frac{10.0}{100}$$

$$\frac{13.1}{100} \quad \frac{4.9}{13} \quad \frac{4.5}{8} \quad 4.0 \quad \frac{4.5}{14} \quad \frac{4.8}{22} \quad \frac{6.7}{23} \quad \frac{8.7}{20} \quad \frac{2.0}{100}$$

Nail in Road Sta 261+00

$$\frac{6.6}{100} \quad \frac{6.0}{57} \quad \frac{5.3}{10} \quad 4.8 \quad \frac{4.9}{12} \quad \frac{4.7}{32} \quad \frac{6.0}{100}$$

$$\frac{6.1}{100} \quad \frac{6.2}{57} \quad \frac{5.6}{16} \quad \frac{5.5}{11} \quad 5.0 \quad \frac{5.4}{12} \quad \frac{5.7}{17} \quad \frac{6.5}{24-56} \quad \frac{4.9}{100}$$

$$\frac{5.2}{100} \quad \frac{5.9}{62} \quad \frac{6.6}{15} \quad \frac{5.8}{10} \quad 5.2 \quad \frac{5.5}{11} \quad \frac{5.8}{14} \quad \frac{9.1}{20} \quad \frac{10.5}{41} \quad \frac{7.4}{59} \quad \frac{6.4}{100}$$

Sta + π -

910.57

263

05.5

264

05.2

265

03.3

266

01.1

+65

99.5

0

1.11

✓
900.04

11.64

✓
898.93

267

98.5

268

96.0

269

93.7

+20

93.5

$$\frac{1.7}{100} \quad \frac{4.4}{52} \quad \frac{5.5}{10} \quad 5.1 \quad \frac{5.5}{12} \quad \frac{6.4}{19} \quad \frac{5.2}{100}$$

$$\frac{1.9}{100} \quad \frac{2.9}{62} \quad \frac{4.4}{18} \quad \frac{5.3}{15} \quad \frac{5.6}{10} \quad 5.4 \quad \frac{5.6}{12} \quad \frac{4.9}{29} \quad \frac{2.6}{100}$$

$$\frac{3.1}{100} \quad \frac{3.6}{61} \quad \frac{3.8}{21} \quad \frac{6.3}{17} \quad \frac{7.8}{10} \quad 7.3 \quad \frac{7.4}{12-15} \quad \frac{2.1}{27} \quad \frac{1.7}{100} \quad 0.5 \text{ House F/}$$

$$\frac{10.3}{100} \quad \frac{9.4}{14} \quad \frac{9.9}{11} \quad 9.5 \quad \frac{9.8}{12} \quad \frac{9.6}{15} \quad \frac{7.7}{24-100}$$

$$\frac{16.3}{100} \quad \frac{12.9}{18} \quad \frac{11.7}{14} \quad \frac{11.8}{12} \quad 11.1 \quad \frac{11.6}{11} \quad \frac{11.8}{14} \quad \frac{13.3}{17} \quad \frac{13.7}{32} \quad \frac{14.2}{100}$$

Nail in PP.

$$\frac{7.9}{100} \quad \frac{6.2}{70} \quad \frac{4.3}{21} \quad \frac{2.3}{13} \quad 1.5 \quad \frac{2.0}{13} \quad \frac{4.8}{21} \quad \frac{4.8}{66} \quad \frac{5.3}{100}$$

$$\frac{7.2}{100} \quad \frac{8.2}{60-40} \quad \frac{7.5}{17} \quad \frac{4.8}{12} \quad 4.0 \quad \frac{4.9}{13} \quad \frac{7.3}{18} \quad \frac{8.0}{49} \quad \frac{7.5}{100}$$

$$\frac{2.2}{100} \quad \frac{5.7}{15} \quad \frac{6.5}{11} \quad 6.3 \quad \frac{6.7}{14} \quad \frac{7.6}{20} \quad \frac{7.4}{60} \quad \frac{6.8}{100}$$

$$\frac{2.0}{100} \quad \frac{5.9}{16} \quad \frac{6.7}{10} \quad 6.5 \quad \frac{6.9}{14} \quad \frac{7.8}{20} \quad \frac{7.0}{100}$$

✓
900.04

269+32

Shoulder Hamline Ave

93.2

+60

"

"

"

92.6

+70

92.5

270

91.9

+50

91.2

271

89.4

○

6.60

✓
894.42

12.22

✓
887.82

+70

86.8

272

86.6

$$\begin{array}{r} 7.2 \quad 6.9 \\ 100-60 \quad 12 \end{array} \quad 6.8 \quad \begin{array}{r} 7.0 \quad 7.3 \quad 6.5 \\ 14 \quad 56 \quad 100 \end{array}$$

$$\begin{array}{r} 7.4 \\ 100 \end{array} \quad \begin{array}{r} 7.6 \\ 12 \end{array} \quad 7.4 \quad \begin{array}{r} 7.6 \quad 7.4 \quad 7.0 \\ 13 \quad 54 \quad 100 \end{array}$$

$$\begin{array}{r} 5.3 \quad 6.7 \quad 8.3 \quad 7.8 \\ 100 \quad 43 \quad 26 \quad 12 \end{array} \quad 7.5 \quad \begin{array}{r} 8.0 \quad 9.1 \quad 8.5 \\ 12 \quad 21 \quad 68-100 \end{array}$$

$$\begin{array}{r} 7.4 \quad 8.1 \quad 9.1 \quad 8.3 \\ 100 \quad 39 \quad 19 \quad 12 \end{array} \quad 8.1 \quad \begin{array}{r} 8.8 \quad 10.7 \quad 10.4 \quad 9.7 \\ 13 \quad 20 \quad 79 \quad 100 \end{array}$$

$$\begin{array}{r} 12.2 \quad 12.3 \quad 9.8 \quad 8.8 \quad 9.5 \quad 12.6 \quad 13.3 \\ 100 \quad 18 \quad 13 \quad 13 \quad 20 \quad 100 \end{array}$$

$$\begin{array}{r} 13.0 \quad 14.0 \quad 11.5 \\ 100 \quad 20 \quad 15 \end{array} \quad 10.6 \quad \begin{array}{r} 11.3 \quad 13.9 \quad 13.7 \\ 13 \quad 19 \quad 100 \end{array}$$

Nail in PP Rt Stg 270+80

$$\begin{array}{r} 8.2 \quad 9.5 \quad 8.1 \\ 100-60 \quad 19 \quad 13 \end{array} \quad 7.6 \quad \begin{array}{r} 8.0 \quad 8.2 \quad 9.6 \quad 8.7 \\ 11 \quad 14 \quad 18 \quad 30-100 \end{array}$$

$$\begin{array}{r} 7.9 \quad 8.3 \quad 9.4 \quad 8.0 \\ 100 \quad 31 \quad 16 \quad 12 \end{array} \quad 7.8 \quad \begin{array}{r} 7.9 \quad 8.2 \quad 9.5 \quad 8.5 \quad 8.2 \\ 11 \quad 16 \quad 18 \quad 30 \quad 100 \end{array}$$

✓
894.42

273

87.4

274

88.9

275

89.1

276

89.7

0

591

✓
899.22

111

✓
893.31

277

89.7

278

89.5

279

88.8

280

87.8

$\frac{8.0}{100}$ $\frac{8.3}{30}$ $\frac{9.7}{18}$ $\frac{7.5}{14}$ 7.0 $\frac{7.2}{12}$ $\frac{7.7}{15}$ $\frac{8.7}{19}$ $\frac{8.4}{100}$

$\frac{8.3}{100}$ $\frac{9.5}{19}$ $\frac{6.2}{14}$ 5.5 $\frac{6.0}{12}$ $\frac{8.8}{20}$ $\frac{8.6}{44}$ $\frac{8.6}{100}$

274+43 { 15" x V.P. $\frac{9.6}{10.0}$ SE End No End

$\frac{7.5}{100}$ $\frac{8.0}{49}$ $\frac{7.8}{18}$ $\frac{5.8}{14}$ 5.3 $\frac{5.7}{13}$ $\frac{8.8}{19}$ $\frac{9.2}{76-100}$

$\frac{4.3}{100}$ $\frac{3.0}{33}$ $\frac{1.8}{24}$ $\frac{4.0}{17}$ $\frac{4.4}{13}$ 4.7 $\frac{5.2}{13}$ $\frac{5.6}{25}$ $\frac{7.0}{53}$ $\frac{8.0}{100}$

Nail Rt St 276+30

$\frac{7.0}{100}$ $\frac{5.4}{43}$ $\frac{2.7}{26}$ $\frac{9.8}{13}$ 9.5 $\frac{9.7}{13}$ $\frac{9.0}{20}$ $\frac{8.0}{28}$ $\frac{4.5}{32}$ $\frac{7.1}{66}$ $\frac{8.0}{100}$

$\frac{3.7}{100}$ $\frac{4.1}{49}$ $\frac{2.3}{29}$ $\frac{10.4}{15}$ 9.7 $\frac{9.7}{12}$ $\frac{9.3}{22}$ $\frac{6.5}{26}$ $\frac{3.4}{30}$ $\frac{6.3}{100}$

$\frac{4.1}{100}$ $\frac{4.7}{52}$ $\frac{2.7}{35}$ 2.5- $\frac{10.8}{13}$ 10.4 $\frac{11.0}{12}$ $\frac{12.0}{19}$ $\frac{10.2}{26}$ $\frac{4.8}{34}$ $\frac{7.0}{62}$ $\frac{8.5}{100}$

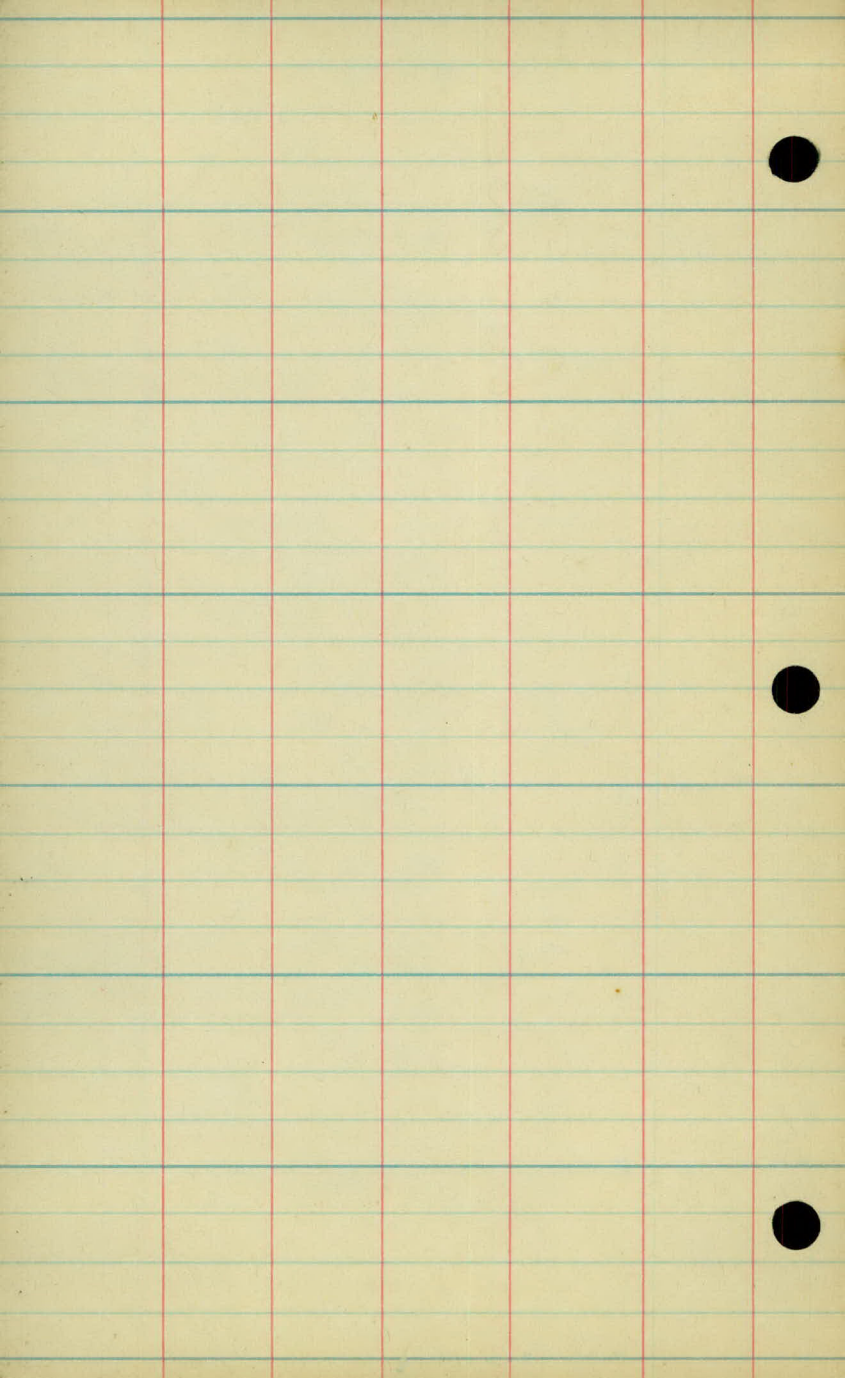
$\frac{10.3}{100}$ $\frac{10.7}{36}$ $\frac{12.0}{27}$ $\frac{12.4}{19}$ $\frac{11.7}{13}$ 11.4 $\frac{11.9}{15}$ $\frac{12.5}{16}$ $\frac{12.6}{25}$ $\frac{11.4}{40}$ $\frac{11.7}{100}$

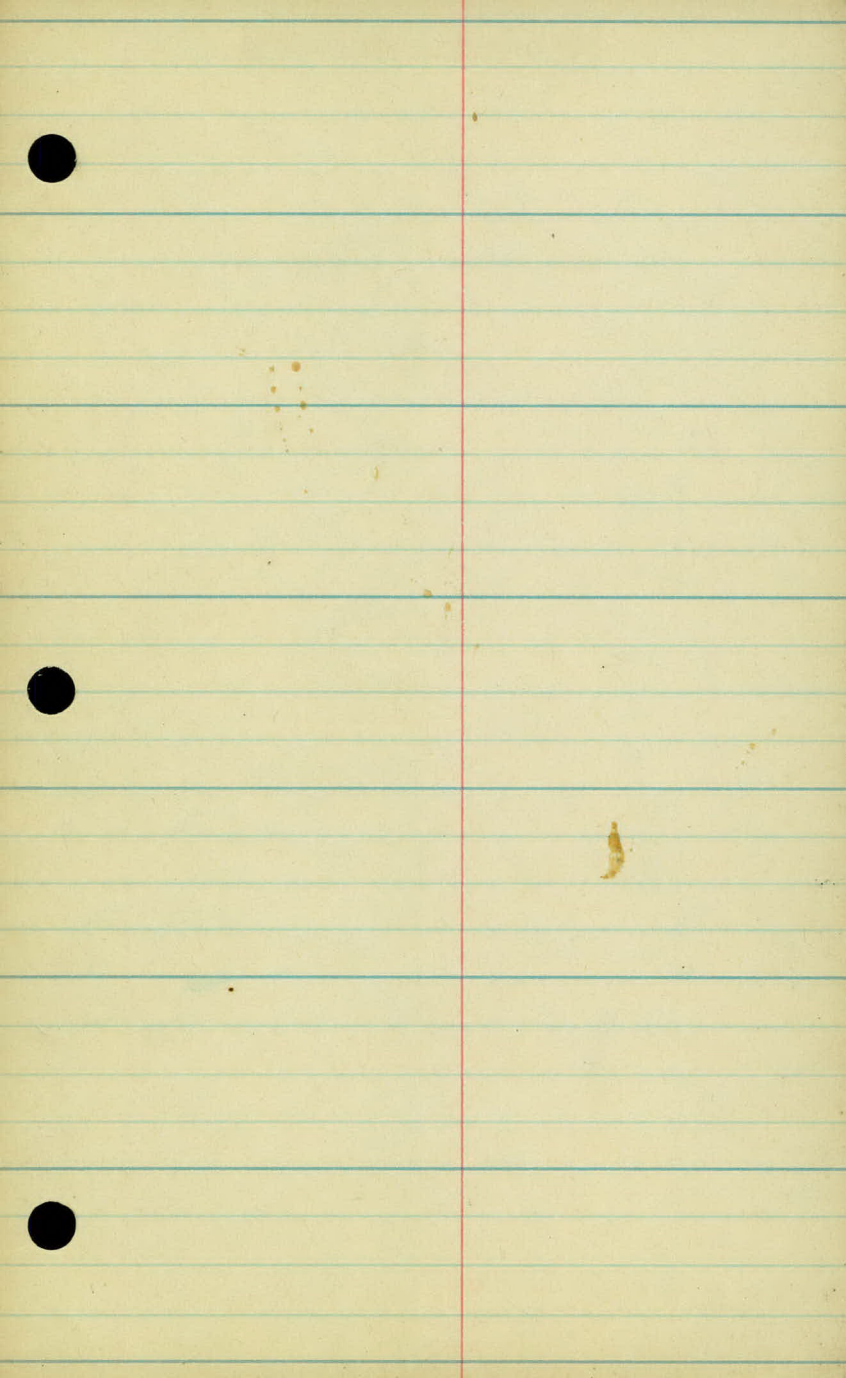
✓
899.22

12.04

✓
887.18

Nail in P.P. Rt. Sta 280+10





Sta	+	π	-		
①	4.47	891.65		887.18	
281				86.0	
282				86.0	
283				85.9	
284				86.3	
285				86.5	
286				86.0	
287				86.1	
288				86.0	
B.M.	4.66	891.75	4.56	887.09	
289				85.8	
290				86.0	
291				85.9	

Nail in P.P. Sta 281+10 Rt.

$$\frac{9.2}{100} \quad \frac{8.8}{52} \quad \frac{8.6}{18} \quad \frac{6.4}{14} \quad 57 \quad \frac{6.1}{11} \quad \frac{8.8}{20} \quad \frac{9.0}{44} \quad \frac{9.2}{100}$$

$$\frac{9.7}{100} \quad \frac{9.4}{46} \quad \frac{9.0}{19} \quad \frac{6.4}{15} \quad 57 \quad \frac{6.4}{12} \quad \frac{8.9}{18} \quad \frac{8.8}{52} \quad \frac{9.0}{100}$$

$$\frac{8.9}{100} \quad \frac{9.2}{33} \quad \frac{9.8}{20} \quad \frac{6.4}{15} \quad 58 \quad \frac{6.5}{12} \quad \frac{9.0}{17} \quad \frac{9.3}{53} \quad \frac{8.8}{100}$$

$$\frac{7.6}{100} \quad \frac{7.7}{20} \quad \frac{6.0}{16} \quad 54 \quad \frac{5.9}{12} \quad \frac{8.9}{19-45} \quad \frac{11.1}{47} \quad \frac{11.4}{63} \quad \frac{7.9}{75} \quad \frac{7.7}{100}$$

$$\frac{6.6}{100} \quad \frac{7.2}{43} \quad \frac{6.5}{22} \quad \frac{5.8}{17} \quad 52 \quad \frac{5.9}{12} \quad \frac{7.7}{17} \quad \frac{8.1}{63} \quad \frac{7.1}{100}$$

$$\frac{6.5}{100} \quad \frac{8.3}{59} \quad \frac{7.9}{51} \quad \frac{6.2}{25} \quad \frac{5.6}{12} \quad 57 \quad \frac{6.8}{16} \quad \frac{8.0}{19} \quad \frac{8.3}{46} \quad \frac{7.7}{100}$$

$$\frac{+1.5}{100} \quad \frac{0.4}{75} \quad \frac{4.7}{36} \quad \frac{6.4}{32} \quad \frac{7.0}{19} \quad \frac{6.0}{14} \quad 5.6 \quad \frac{6.3}{10} \quad \frac{8.4}{16} \quad \frac{9.1}{25} \quad \frac{8.8}{100}$$

$$\frac{+2.0}{100} \quad \frac{0.2}{39} \quad \frac{3.7}{36} \quad \frac{5.6}{33} \quad \frac{7.2}{15} \quad \frac{6.1}{11} \quad 5.7 \quad \frac{6.6}{12} \quad \frac{8.4}{18} \quad \frac{10.0}{48} \quad \frac{9.9}{100}$$

Nail in Cottonwood Rt Sta 288+80

$$\frac{9.2}{100} \quad \frac{6.7}{74} \quad \frac{5.5}{31} \quad \frac{7.4}{26} \quad \frac{8.0}{16} \quad \frac{6.1}{12} \quad 6.0 \quad \frac{6.5}{10} \quad \frac{9.0}{17} \quad \frac{9.8}{45} \quad \frac{11.6}{47-59} \quad \frac{7.8}{61} \quad \frac{9.0}{100}$$

$$\frac{12.0}{100} \quad \frac{11.9}{75} \quad \frac{7.9}{36} \quad \frac{8.3}{28-17} \quad \frac{6.5}{13} \quad 5.8 \quad \frac{6.4}{12} \quad \frac{9.9}{18} \quad \frac{10.0}{52} \quad \frac{12.1}{59} \quad \frac{12.2}{65} \quad \frac{10.0}{68} \quad \frac{10.2}{100}$$

$$\frac{11.0}{100} \quad \frac{11.7}{81} \quad \frac{8.4}{48} \quad \frac{8.3}{21} \quad \frac{6.4}{14} \quad 5.9 \quad \frac{6.5}{11} \quad \frac{9.9}{17} \quad \frac{10.0}{60} \quad \frac{13.0}{65} \quad \frac{13.1}{71} \quad \frac{10.1}{74} \quad \frac{9.9}{100}$$

Sta	+	π	-	
		891.75		
292				86.2
	+10			86.8
	+84			86.9
293				86.9
	+29			86.8
	+40			86.2
294				85.4
295				85.2
296				85.1
297				85.9
B.M.	2.11	890.72	3.14	888.61
298				86.0
299				86.1

$\frac{10.7}{100}$ $\frac{8.0}{62}$ $\frac{8.9}{19}$ $\frac{6.2}{13}$ 5.6 $\frac{6.2}{13}$ $\frac{8.1}{17}$ $\frac{10.5}{70}$ $\frac{14.8}{75-80}$ $\frac{9.0}{83}$ $\frac{9.2}{100}$

$\frac{8.7}{100}$ $\frac{6.6}{38}$ $\frac{8.4}{28}$ $\frac{8.2}{20}$ $\frac{5.5}{11}$ 5.0 $\frac{5.2}{10}$ $\frac{6.8}{17}$ $\frac{9.5}{73}$ $\frac{14.1}{80-88}$ $\frac{9.6}{91}$ $\frac{10.2}{100}$

$\frac{15.0}{100}$ $\frac{13.5}{34}$ $\frac{11.3}{21}$ $\frac{5.2}{11}$ 4.9 $\frac{4.9}{9}$ $\frac{8.3}{17}$ $\frac{8.4}{28}$ $\frac{9.5}{74}$ $\frac{14.5}{80-89}$ $\frac{9.7}{92}$ $\frac{9.6}{100}$

$\frac{15.4}{100}$ $\frac{13.9}{10}$ $\frac{5.0}{10}$ 4.9 $\frac{4.9}{8}$ $\frac{13.1}{8}$ $\frac{13.6}{34}$ $\frac{11.6}{47}$ $\frac{9.1}{75}$ $\frac{14.5}{81}$ $\frac{14.6}{91}$ $\frac{9.9}{100}$

$\frac{15.4}{100}$ $\frac{14.3}{10}$ $\frac{5.0}{10}$ 5.0 $\frac{5.0}{9}$ $\frac{13.9}{9}$ $\frac{13.5}{34}$ $\frac{12.5}{64}$ $\frac{10.2}{100}$

$\frac{13.9}{100}$ $\frac{11.8}{78}$ $\frac{10.1}{21}$ $\frac{5.2}{10}$ 5.2 $\frac{5.5}{9}$ $\frac{12.5}{18}$ $\frac{13.1}{43}$ $\frac{13.0}{70}$ $\frac{12.1}{100}$

$\frac{12.4}{100}$ $\frac{10.7}{83}$ $\frac{11.2}{56}$ $\frac{10.8}{21}$ $\frac{6.7}{13}$ 6.4 $\frac{6.8}{9}$ $\frac{7.8}{15}$ $\frac{10.5}{18}$ $\frac{11.6}{32}$ $\frac{12.9}{33-58}$ $\frac{11.8}{100}$

$\frac{11.6}{100}$ $\frac{10.3}{20}$ $\frac{7.3}{14}$ 6.6 $\frac{7.2}{11}$ $\frac{11.1}{17}$ $\frac{10.7}{51}$ $\frac{12.5}{57-87}$ $\frac{10.7}{100}$

$\frac{11.3}{100}$ $\frac{10.7}{21}$ $\frac{7.4}{13}$ 6.7 $\frac{7.1}{11}$ $\frac{10.4}{18}$ $\frac{10.6}{100}$

$\frac{7.5}{100}$ $\frac{6.7}{86}$ $\frac{6.2}{25}$ $\frac{6.1}{14}$ 5.9 $\frac{6.5}{10}$ $\frac{8.3}{15}$ $\frac{9.2}{77}$ $\frac{10.4}{100}$

Nail in Twin Cottonwood Sta 297+60

$\frac{0.2}{100}$ $\frac{1.0}{60}$ $\frac{3.7}{28}$ $\frac{4.9}{12}$ 4.7 $\frac{5.2}{11}$ $\frac{6.1}{19}$ $\frac{4.4}{47}$ $\frac{6.8}{100}$

$\frac{0.5}{100}$ $\frac{5.0}{34}$ $\frac{5.2}{17}$ $\frac{4.8}{12}$ 4.6 $\frac{5.2}{10}$ $\frac{5.6}{14}$ $\frac{3.4}{56}$ $\frac{3.8}{100}$

Sta

+

x

-

890.72

300

85.9

301

85.5

302

85.6

303

84.4

304

86.1

305

86.8

+72

87.9

+80

88.1

+98

No County Line

88.3

O

3.52

891.82

2.42

888.30

B.M.

0.88

890.94

871.47

$$\begin{array}{cccccccc} +4.0 & 0.9 & 4.4 & 5.2 & 4.9 & 4.8 & 5.2 & 7.2 & 8.8 \\ \hline 100 & 57 & 16 & 14 & 11 & & 9 & 18 & 100 \end{array}$$

$$\begin{array}{cccccccc} +6.0 & 0.2 & 4.2 & & 5.4 & 5.2 & 5.8 & 8.8 & 9.0 \\ \hline 100 & 58 & 27 & 23-12 & & & 10 & 17 & 100 \end{array}$$

$$\begin{array}{cccccccc} +2.5 & 0.3 & 3.5 & 5.1 & 5.3 & 5.1 & 5.8 & 6.2 & 7.7 & 7.2 \\ \hline 100 & 71 & 30 & 27 & 13 & & 10 & 13 & 16 & 100 \end{array}$$

$$\begin{array}{cccccccc} 0.9 & 6.8 & 6.4 & 6.3 & 6.8 & 8.6 & 8.5 & 7.5 \\ \hline 100 & 48 & 10 & & 9 & 14 & 45 & 100 \end{array}$$

$$\begin{array}{cccccccc} 0.7 & 2.0 & 5.6 & 4.9 & 4.6 & 5.2 & 5.4 & 7.1 & 7.5 \\ \hline 100 & 65 & 21 & 13 & & 9 & 12 & 15 & 100 \end{array}$$

$$\begin{array}{cccccccc} 00 & 2.8 & 5.2 & 4.1 & 3.9 & 4.6 & 6.6 & 7.6 & 8.0 \\ \hline 100 & 37 & 23 & 12 & & 11 & 16 & 54 & 100 \end{array}$$

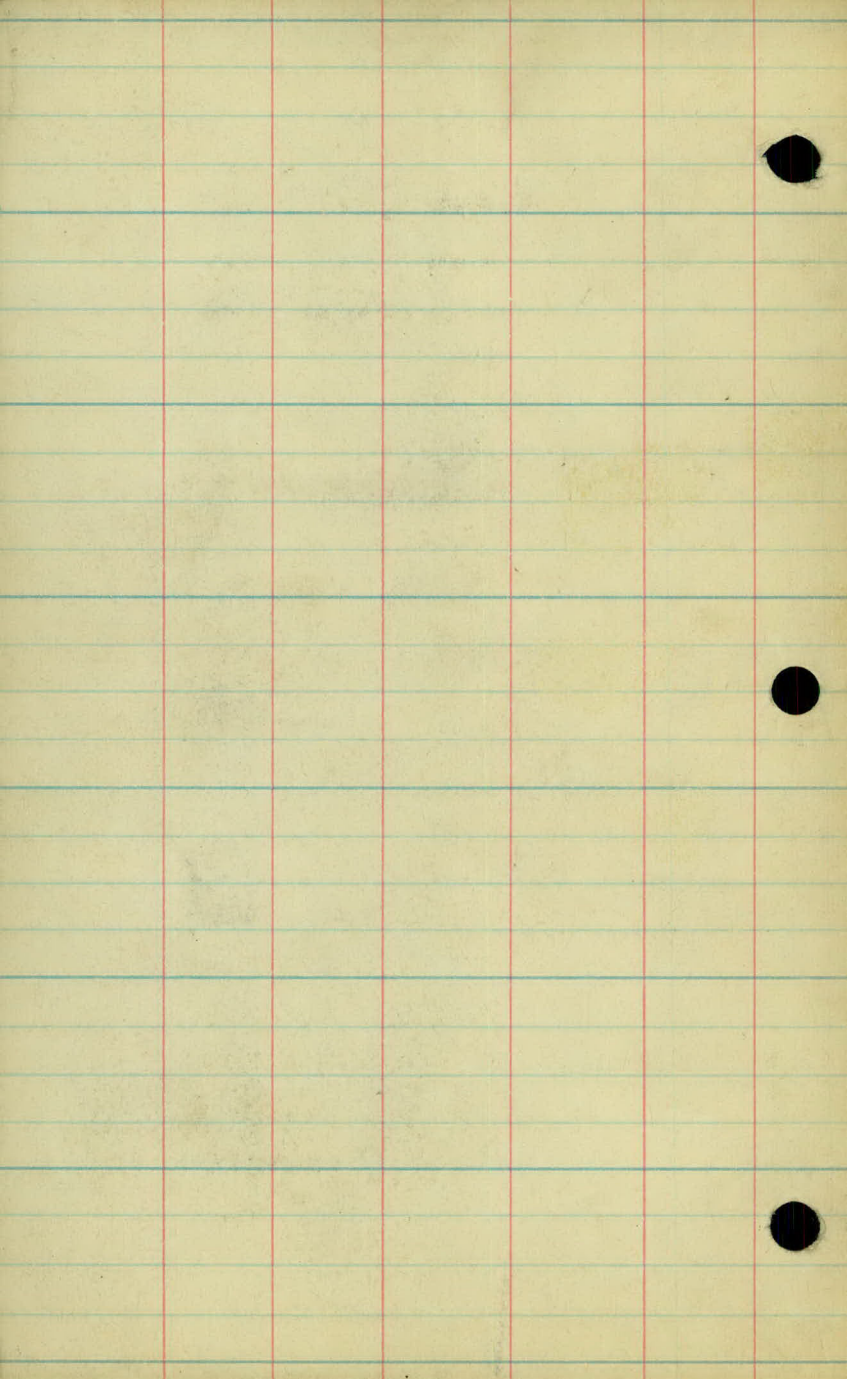
$$\begin{array}{cccccccc} 00 & 3.5 & 3.0 & 3.1 & 2.8 & 3.7 & 3.5 & 6.5 & 6.8 \\ \hline 100 & 33 & 24 & 14 & & 11 & 21 & 38 & 100 \end{array}$$

$$\begin{array}{cccccccc} 00 & 2.5 & 2.5 & 2.6 & 3.1 & 3.5 & 4.9 \\ \hline 100 & 35 & 14 & & 10 & 28 & 100 \end{array}$$

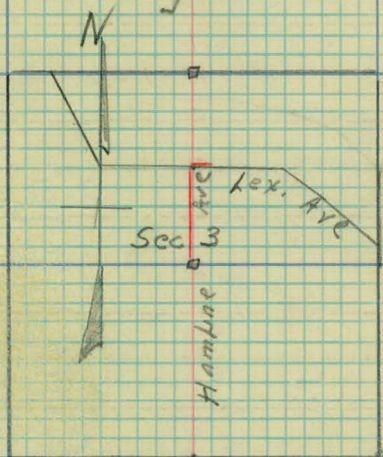
$$\begin{array}{cccc} 1.2 & 0.3 & 2.4 & 3.7 \\ \hline 100 & 60 & 50 & 100 \end{array}$$

RR SpK Int No Co Line + Lex Ave.

RR SpK in 24" B.E. NW Cor, No County Line + Lex.

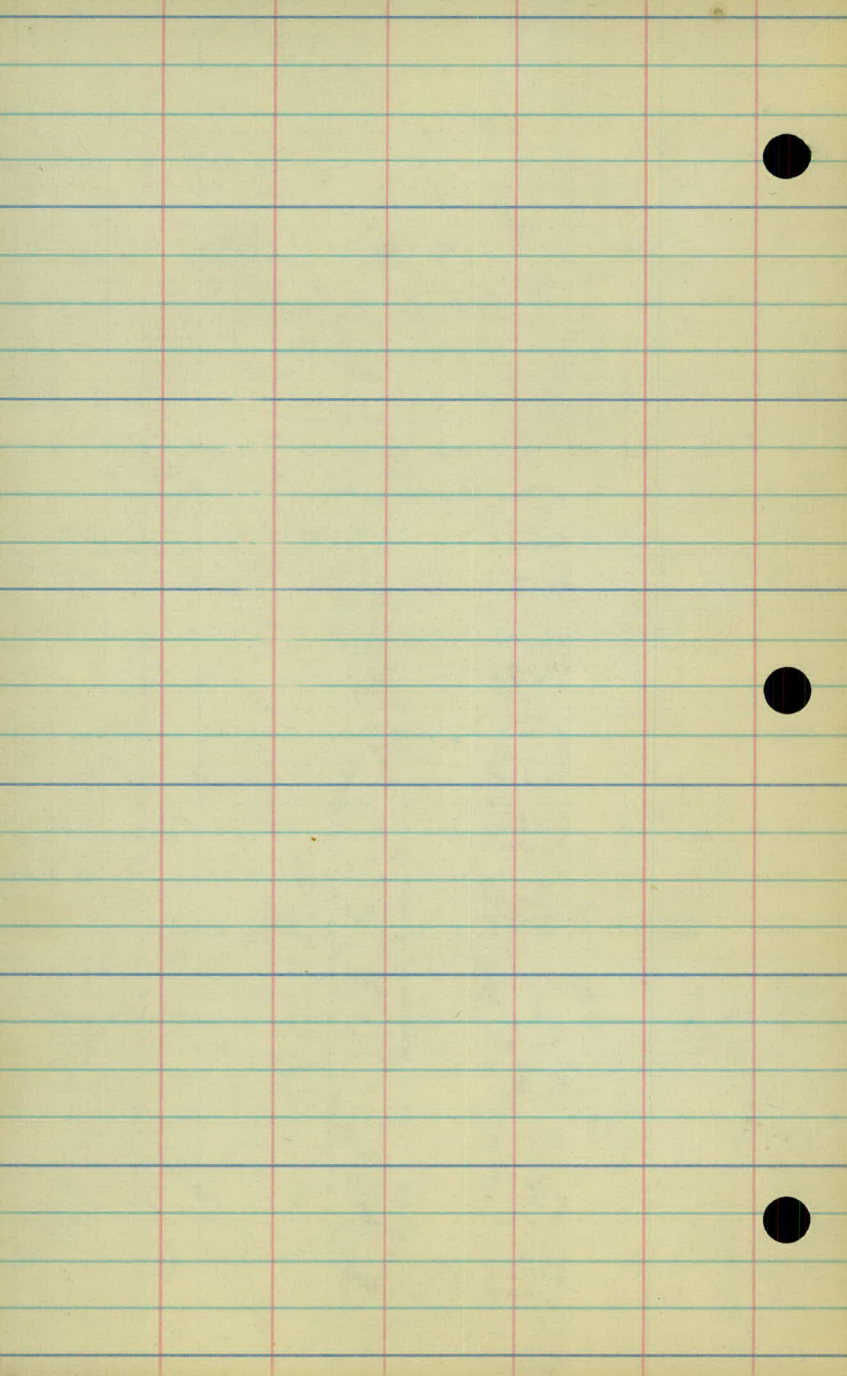


Plan Survey Hamline Ave Borrow Pits For Lexington Ave



Index	
alignment	P. 1-2
Topography	3-6
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H A Wilke
J P Bell
L D Goldberg
5/14/36



Alignment

Sta. Point Lt A Rt

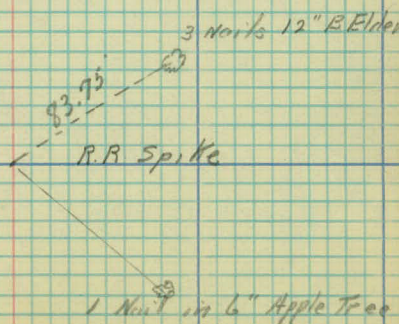
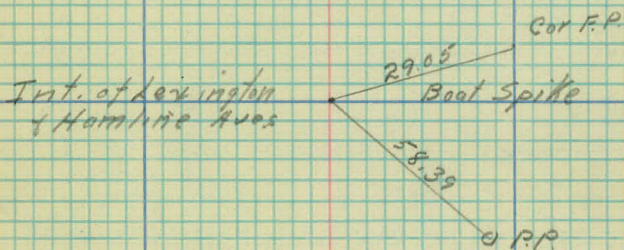
282+58⁶⁰ P.O.T. Men

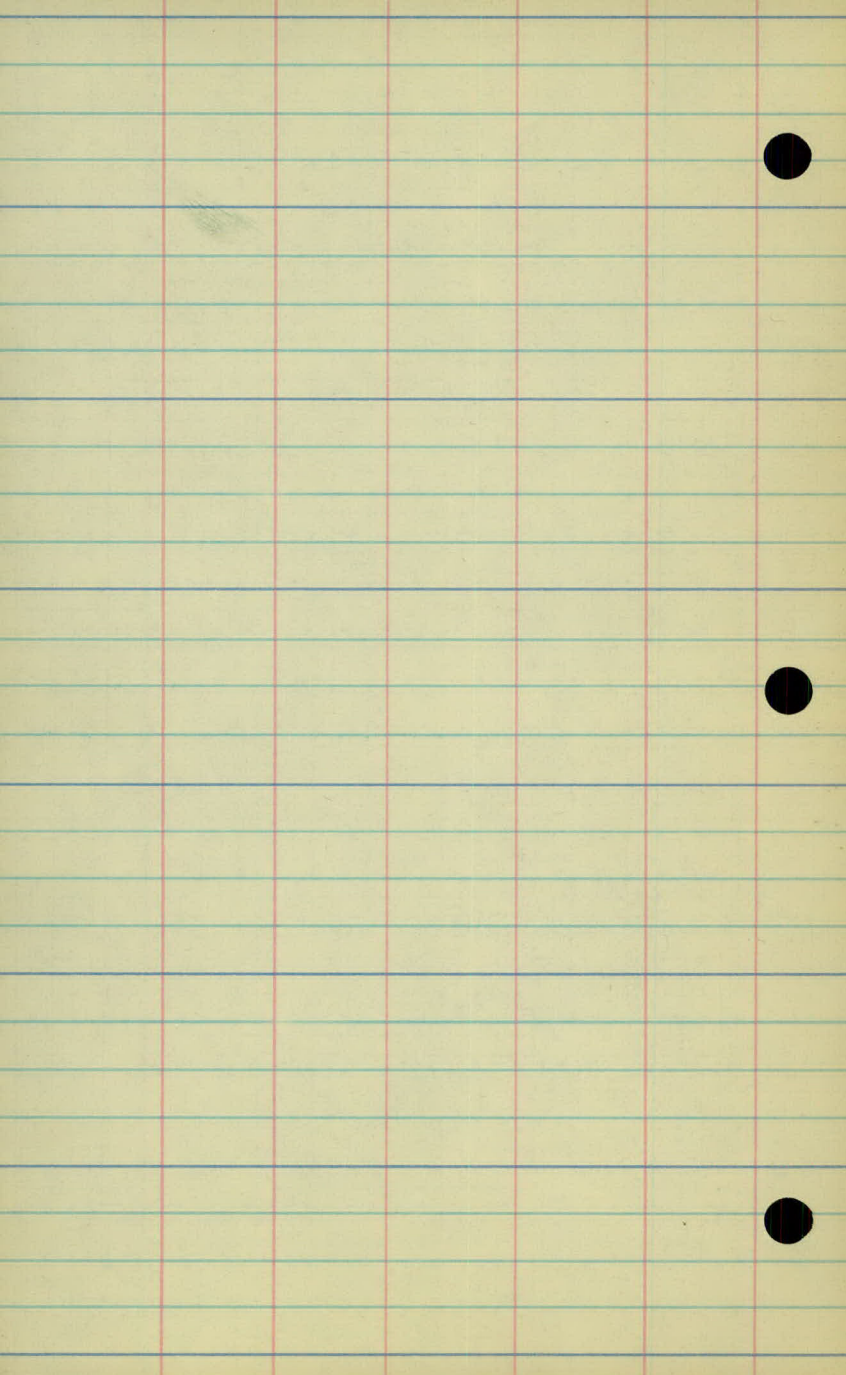
269+39⁶⁰ P.I. 90°13'

263+58.20 P.O.T.

Stone Man

see ties
in Sec Book
Center Sec 3





Topography

275

274

273

272

271

270

+38 P.P. 26'

Brush

+50 F.C. 19'

Cultivated

+55 F.C. 18'

F.F. 16'

+73 P.P. 24'

+92 P.P. 23'

Cult

Meadow

P.P. 21'

Gravel

Read

282

281

280

279

20x50
Granary

278

277

276

Cultivated

Old Fall Pa

Fence 18

+ 90 Fence Cor
+ 85 End of Tree 19'

Fence 16'

Fence 18

+ 42 Bog Run 8 Trees 19'

+ 08 20" Oak 20'
Fence 15'

+ 85 10" Oak 26'

+ 75 6" Elm 16'

+ 40 Farm Ent

Fence 18'

+ 80 Shed 30'

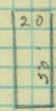
+ 57 P.P 28'

+ 30 Shed 29'

+ 19 18" Oak 22'

Fence 22'

Farm Yard



+ 40 Farm Ent

Fence 19
Down

Cultivated

Fence 18'

+ 28 30" Oak 19'
Fence 18'

Fence 18'

+ 88 P.P 28'

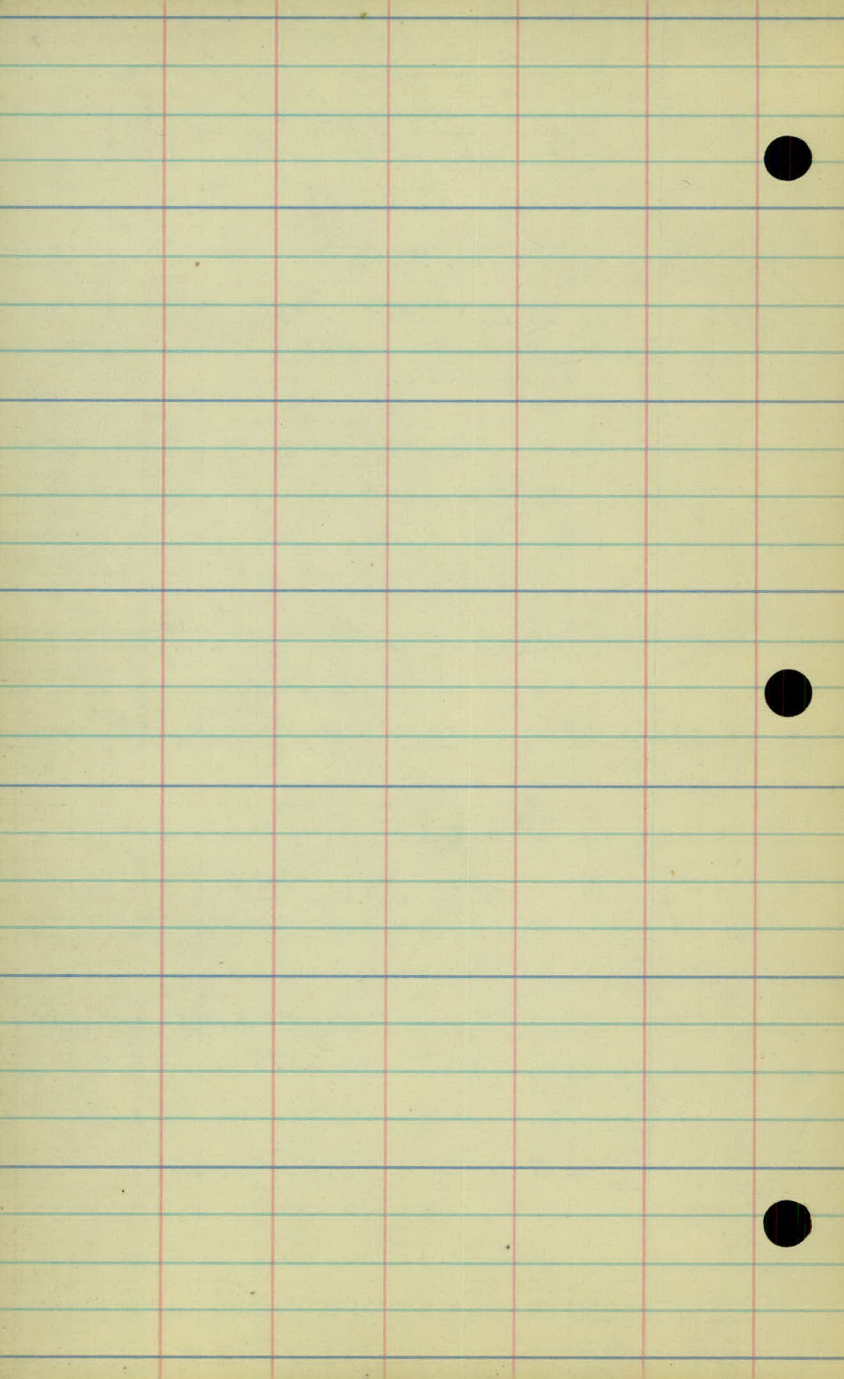
284

283

Cultivated

Cultivated

Persecution



Cross Sections

Sta	+	π	-	Elev
	4.40	903.33		898.93
269+40				93.0
+53				93.1
+56				93.1
270+00				92.8
+50				93.1
271+00				93.3
+50				93.6
272+00				94.1
+50				94.6
273+00				94.8
+50				94.9
T.P	9.23	904.52	8.04	895.29
274+00				95.3
+50				95.4

Lt

Z

Rt

8

Mail in P.P. Rt Sta 266+70 Lex. Ave Sta

 $\frac{9.5}{50}$ $\frac{9.8}{33}$ 10.3 $\frac{11.0}{36}$ $\frac{11.3}{50}$
 $\frac{9.7}{50}$ $\frac{10.5}{17}$ 10.2 $\frac{11.0}{30}$ $\frac{11.8}{50}$
 $\frac{9.1}{50}$ $\frac{9.0}{20}$ $\frac{10.5}{15}$ 10.2 $\frac{11.6}{43}$ $\frac{11.8}{50}$
 $\frac{7.8}{50}$ $\frac{6.3}{27}$ $\frac{6.8}{17}$ $\frac{10.6}{8}$ 10.5 $\frac{10.5}{8}$ $\frac{11.8}{27}$ $\frac{9.5}{31}$ $\frac{10.6}{50}$
 $\frac{5.5}{50}$ $\frac{3.9}{27}$ $\frac{4.8}{19}$ $\frac{10.1}{10}$ 10.2 $\frac{10.4}{10}$ $\frac{11.4}{19}$ $\frac{11.2}{23}$ $\frac{8.1}{26}$ $\frac{9.8}{50}$
 $\frac{3.2}{50}$ $\frac{2.5}{26}$ $\frac{4.0}{19}$ $\frac{10.0}{8}$ 10.0 $\frac{9.9}{8}$ $\frac{10.6}{19}$ $\frac{10.9}{25}$ $\frac{8.0}{32}$ $\frac{9.7}{50}$
 $\frac{2.7}{50}$ $\frac{2.4}{28}$ $\frac{2.4}{25}$ $\frac{8.4}{12}$ $\frac{9.7}{8}$ 9.7 $\frac{9.6}{9}$ $\frac{10.3}{18}$ $\frac{11.4}{22}$ $\frac{11.4}{25}$ $\frac{7.7}{32}$ $\frac{9.4}{50}$
 $\frac{2.5}{50}$ $\frac{2.0}{31}$ $\frac{2.9}{24}$ $\frac{2.4}{17}$ $\frac{9.3}{7}$ 9.2 $\frac{9.3}{7}$ $\frac{10.6}{17}$ $\frac{10.7}{20}$ $\frac{10.7}{22}$ $\frac{6.68.3}{30}$ $\frac{9.3}{50}$
 $\frac{2.0}{50}$ $\frac{1.5}{30}$ $\frac{6.3}{21}$ $\frac{7.4}{15}$ $\frac{8.9}{11}$ 8.7 $\frac{8.8}{7}$ $\frac{9.4}{18}$ $\frac{4.7}{28}$ $\frac{6.3}{50}$
 $\frac{1.6}{50}$ $\frac{1.4}{30}$ $\frac{6.5}{20}$ $\frac{8.2}{13}$ $\frac{8.8}{11}$ 8.5 $\frac{8.5}{7}$ $\frac{8.9}{17}$ $\frac{4.0}{26}$ $\frac{4.7}{50}$
 $\frac{2.3}{50}$ $\frac{2.5}{26}$ $\frac{6.4}{17}$ $\frac{7.5}{13}$ $\frac{8.4}{12}$ 8.4 $\frac{8.7}{14}$ $\frac{3.6}{24}$ $\frac{4.0}{50}$
 $\frac{6.5}{50}$ $\frac{5.7}{34}$ $\frac{6.9}{16}$ $\frac{9.4}{9}$ 9.2 $\frac{9.5}{12}$ $\frac{5.4}{19}$ $\frac{5.8}{50}$
 $\frac{8.6}{50}$ $\frac{9.0}{33}$ $\frac{10.4}{22}$ $\frac{9.4}{13}$ 9.1 $\frac{9.6}{11}$ $\frac{8.9}{13}$ $\frac{8.1}{50}$

Sta + H.I - Elev
904.52

274+65 95.5

275+00 95.4

+50 95.3

276+00 95.9

+50 96.5

277+00 97.1

+50 97.7

278+00 98.5

+50 99.0

279+00 99.2

+50 99.9

280+00 00.6

T.P. 6.39 907.43 3.48 901.04

+50 01.4

L+

≠

R7

9

$$\frac{13.6}{50} \frac{13.4}{19} \frac{9.5}{12} 9.0 \frac{9.7}{12} \frac{11.3}{17} \frac{11.3}{40} \frac{10.4}{50}$$

$$\frac{15.7}{50} \frac{15.9}{19} \frac{9.7}{12} 9.1 \frac{9.8}{12} \frac{14.5}{24} \frac{14.6}{35} \frac{13.5}{50}$$

$$\frac{15.1}{50} \frac{14.1}{18} \frac{9.8}{12} 9.2 \frac{9.9}{12} \frac{14.3}{22} \frac{14.5}{28} \frac{14.5}{50}$$

$$\frac{14.8}{50} \frac{14.0}{19} \frac{9.5}{12} 8.6 \frac{9.3}{13} \frac{13.4}{21} \frac{15.6}{27} \frac{15.6}{50}$$

$$\frac{13.3}{50} \frac{13.5}{19} \frac{8.7}{12} 8.0 \frac{8.6}{12} \frac{13.6}{22} \frac{15.0}{32} \frac{14.9}{50}$$

$$\frac{8.5}{50} \frac{10.5}{17} \frac{8.1}{13} 7.4 \frac{8.1}{12} \frac{11.6}{18} \frac{13.6}{50}$$

$$\frac{3.7}{50} \frac{5.1}{21} \frac{7.4}{11} 6.8 \frac{7.3}{12} \frac{7.1}{18} \frac{10.3}{50}$$

$$\frac{7.0}{50} \frac{0.9}{23} \frac{6.4}{11} 6.0 \frac{6.5}{12} \frac{3.3}{19} \frac{7.8}{50}$$

Barra on Bank $\frac{0.7}{50} \frac{1.4}{23} \frac{5.4}{14} \frac{5.9}{10} 5.5 \frac{5.9}{12} \frac{5.8}{16} \frac{3.6}{20} \frac{7.7}{50}$

$$\frac{3.3}{50} \frac{3.0}{18} \frac{5.7}{10} 5.3 \frac{5.6}{11} \frac{4.6}{19} \frac{7.3}{50}$$

$$\frac{4.7}{50} \frac{4.8}{11} 4.6 \frac{5.2}{12} \frac{5.0}{27} \frac{4.8}{50}$$

$$\frac{4.8}{50} \frac{5.0}{31} \frac{4.2}{10} 3.9 \frac{4.2}{11} \frac{2.5}{17} \frac{3.3}{50}$$

$$\frac{5.8}{50} \frac{5.3}{15} \frac{6.3}{10} 6.0 \frac{6.3}{10} \frac{2.8}{18} \frac{4.0}{50}$$

Sta.	+	H.I	-	Elev
		907.43		
281+00				02.0
+50				02.4
282+0				02.6
+50				02.8
			4.74	902.69.
283+0				02.7
+50				02.6
284+0				02.4

Check Levels	1.63	902.57	6.39	901.04.
	9.95	905.24	7.28	895.29.
			6.31	898.93.
			12.02	893.22

Lt

Z

Rt

10

$\frac{5.1}{50}$	$\frac{4.4}{34}$	$\frac{3.7}{16}$	$\frac{5.8}{10}$	5.4	$\frac{5.7}{11}$	$\frac{2.0}{18}$	$\frac{3.3}{50}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------

$\frac{6.2}{50}$	$\frac{6.1}{37}$	$\frac{4.5}{15}$	$\frac{5.4}{10}$	5.0	$\frac{5.1}{11}$	$\frac{1.5}{18}$	$\frac{3.4}{50}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------

$\frac{7.1}{50}$	$\frac{6.5}{37}$	$\frac{4.9}{13}$	$\frac{5.1}{10}$	4.8	$\frac{5.0}{10}$	$\frac{2.1}{20}$	$\frac{4.0}{50}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------

$\frac{6.0}{50}$	$\frac{4.4}{25}$	$\frac{4.8}{9}$	4.6	$\frac{4.9}{10}$	$\frac{3.7}{20}$	$\frac{5.2}{50}$
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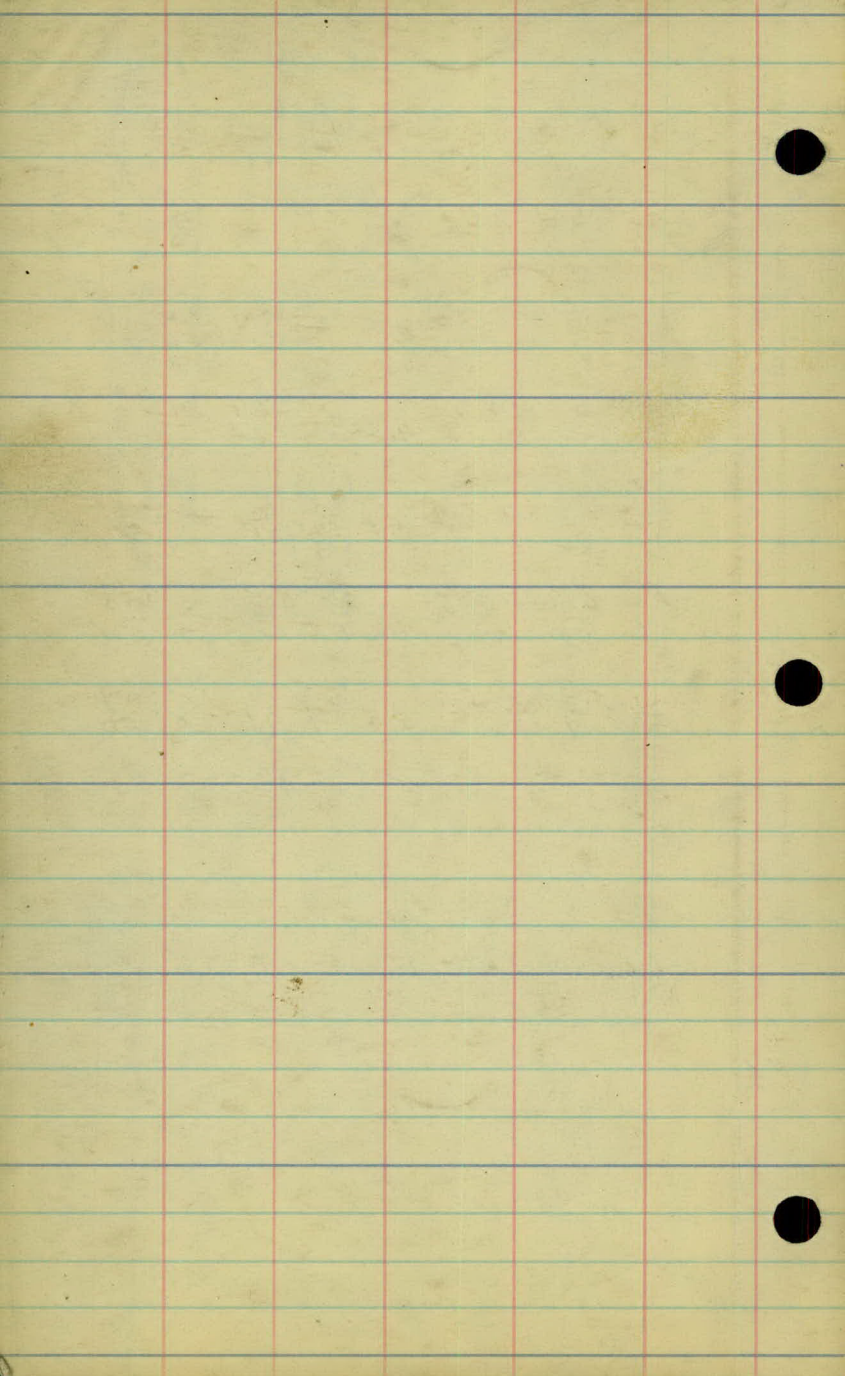
B.M. Top. Mont.

$\frac{6.4}{50}$	$\frac{4.3}{22}$	$\frac{3.7}{12}$	$\frac{5.0}{8}$	4.7	$\frac{5.1}{10}$	$\frac{6.1}{17}$	$\frac{5.6}{26}$	$\frac{6.6}{50}$
------------------	------------------	------------------	-----------------	-----	------------------	------------------	------------------	------------------

$\frac{6.8}{50}$	$\frac{4.1}{12}$	$\frac{5.0}{8}$	4.8	$\frac{5.4}{11}$	$\frac{5.5}{17}$	$\frac{7.3}{37}$	$\frac{6.3}{50}$
------------------	------------------	-----------------	-----	------------------	------------------	------------------	------------------

$\frac{6.4}{50}$	$\frac{5.3}{27}$	$\frac{4.3}{13}$	$\frac{5.3}{7}$	5.0	$\frac{5.3}{11}$	$\frac{4.1}{17}$	$\frac{5.0}{28}$	$\frac{4.7}{50}$
------------------	------------------	------------------	-----------------	-----	------------------	------------------	------------------	------------------

Nail T.P Lexington Ave
 Spike in P.P 268+90 25' Rt



Mr. Heas:

Herewith data to determine
drainage problem at Mr.
Bennings property on Co.
Rd. I. See Mr. Schulz letter
to yourself dated 5/28/37

H.B.

Simple way out is to
fill pot hole. ?

Book 87

Dr. 6

old

Sta.	+	π	-	Elev.
B.M.	4.65	898.47° 104.65		893.82
23+00	24" x 52' C.M.			
130			10.6	887.9
+70	15" x 20' C.M.			
24			10.3	88.2
35			10.3	88.2
36			10.0	88.5
36+85	15" x 30' C.M.		9.5	89.0
38				
38+76	15" x 20' C.M.			
39+47	15" x 38' C.M.			

E

2

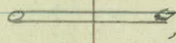
S.E. Cor. of Conc. Manhole 45' Lt. Sta. 48+35

Mr. Corley, I believe you have the Elev. of this point

885.8'
12.7

887.0'
11.5

593.62?



887.2'
11.3



887.2'
11.3

887.7'
10.8



887.8'
10.7

888.5'
10.0



888.9'
9.5



889.1'
9.4

889.4'
9.1

5 1/2.

+

K

-

Elev.

898.47
704.65

40

9.2

89.3

41+00 15" x 18" C.M.

41+16 Low Spot

41+33 15" x 20' C.M.

41+70

Sees thru low spots.

41+08

41+52

41+90

43+13 15" x 20' C.M.

889.9
86
 89.6
8.9
 89.8 91.7 90.4 89.9 89.7 88.9
8.9
 89.8 91.7 90.4 89.9 89.7 88.9
 893.7 92.8 91.5
5.7 7.0 8.3 8.1 8.2 8.8 9.6
 23 27 28 32 24 38 45 57
 89.1 89.0 89.8 90.1 91.7
9.4 9.1 8.7 8.4 6.8 CP
 69 78 96 100 115 127
8.8
 89.7

88 89.7
 893.6 92.8 90.7 89.8 89.4 89.0 89.9 89.8 89.9
4.9 5.7 7.8 8.7 8.1 9.5 8.6 8.7 8.6
 17 22 31 41 53 63 72 76
 91.1 92.8 93.3
7.4 5.7 5.2
 80 89 100 → CP

Cunningham

893.5 92.8 90.4 89.8 89.4 89.3 89.2 89.3 89.8
5.0 5.7 8.1 8.2 8.1 8.2 8.3 8.2 8.7
 17 23 29 35 44 51 52 78
 93.0 93.0
5.5
 100 → CP 70%

893.4 92.9 89.9 89.6 88.9 89.0 89.8 95.1
5.1 5.6 8.6 8.9 9.6 9.5 8.7 3.4
 17 24 28 33 41 56 100 79
 89.1 90.0 92.3 98.0
5.1 5.6 8.4 8.5 6.2 0.5
 17 24 31 35 56 100

8.4 890.1

8.4 890.1

Sta. + $\times$ - Elev.

898.47
~~104.65~~

43+61 15" x 20' C.M.

44+10 15" x 20' C.M. 7.1 891.4

45

+60 15" x 20' C.M.

46 15" x 20' C.M.

+67 15" x 20' C.M.

47 7.2 891.3

+50 7.1 891.4

48+05 15" x 20' C.M.

48+21 24" x 52' C.M.

B.M.

4.65

893.82

~~700.00~~

8.2 890.3

8.4 890.1

8.1 890.4

2.6 890.9

6.9 91.6

2.2 91.3

2.3 91.2

2.3 91.2

2.2 91.3

2.1 91.4

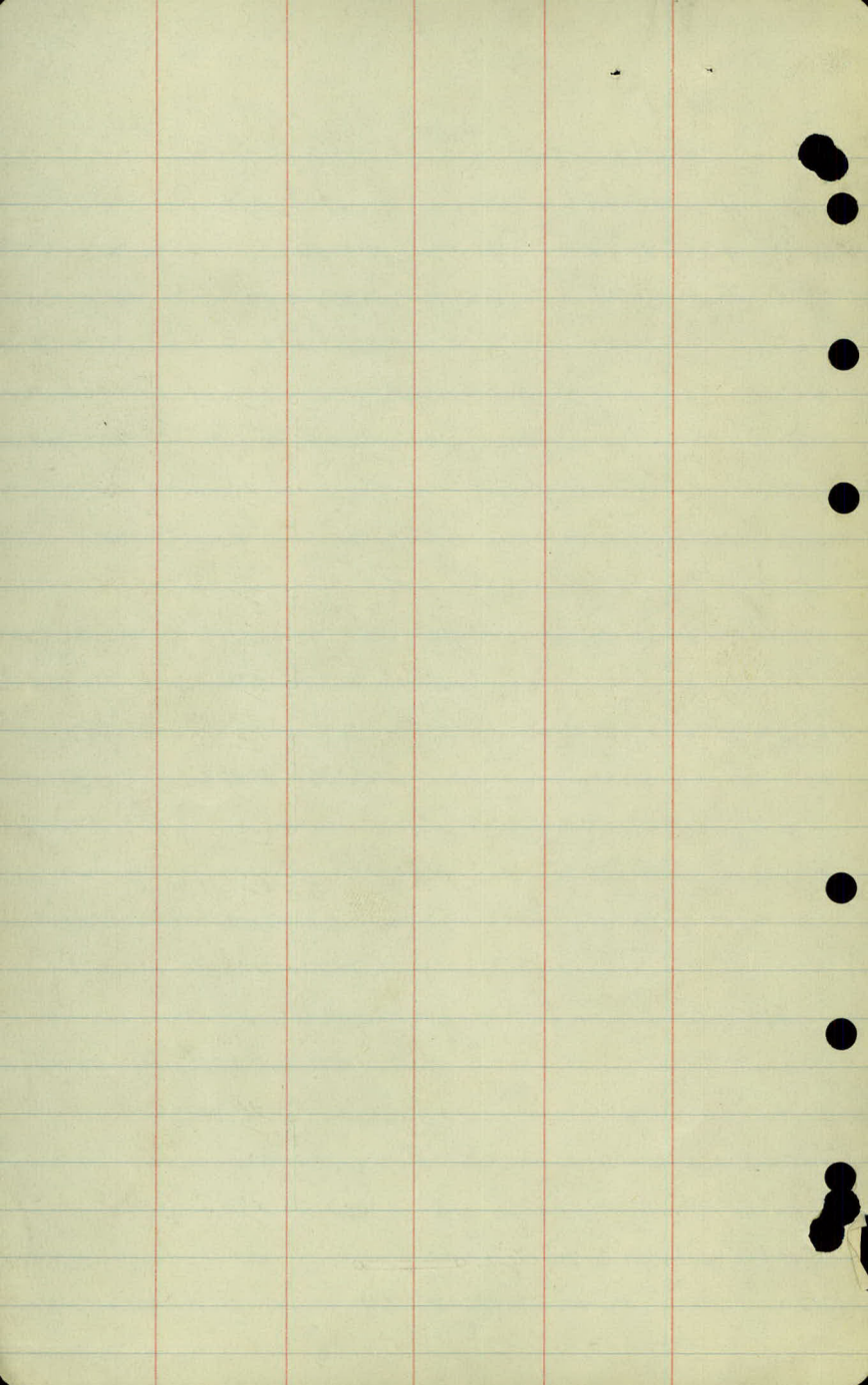
2.4 91.1

8.1 90.4

9.2 889.3

889.8

8.7



Pick up Sta. off Road plans
and tie into previous data taken in
connection with drawing for spot Mr. Cummings
property

Lt.

Rt.

H.I. = 900.0

Side Culverts
on Right

Sta.

0+00 - 24" C.M.

8.7 10.2

0+47

9.0

1+04

8.9

2+89

7.9

4+12

8.0

4+77

8.2 9.0

5+33

8.3

5+89

8.5

6+48

8.0

7+07 Mr. R.L. Ritt.

8.1

8+75 No pipe thru Entrance.

5.9

9+64

6.2

9+84

7.7 7.5

11+02

4.4

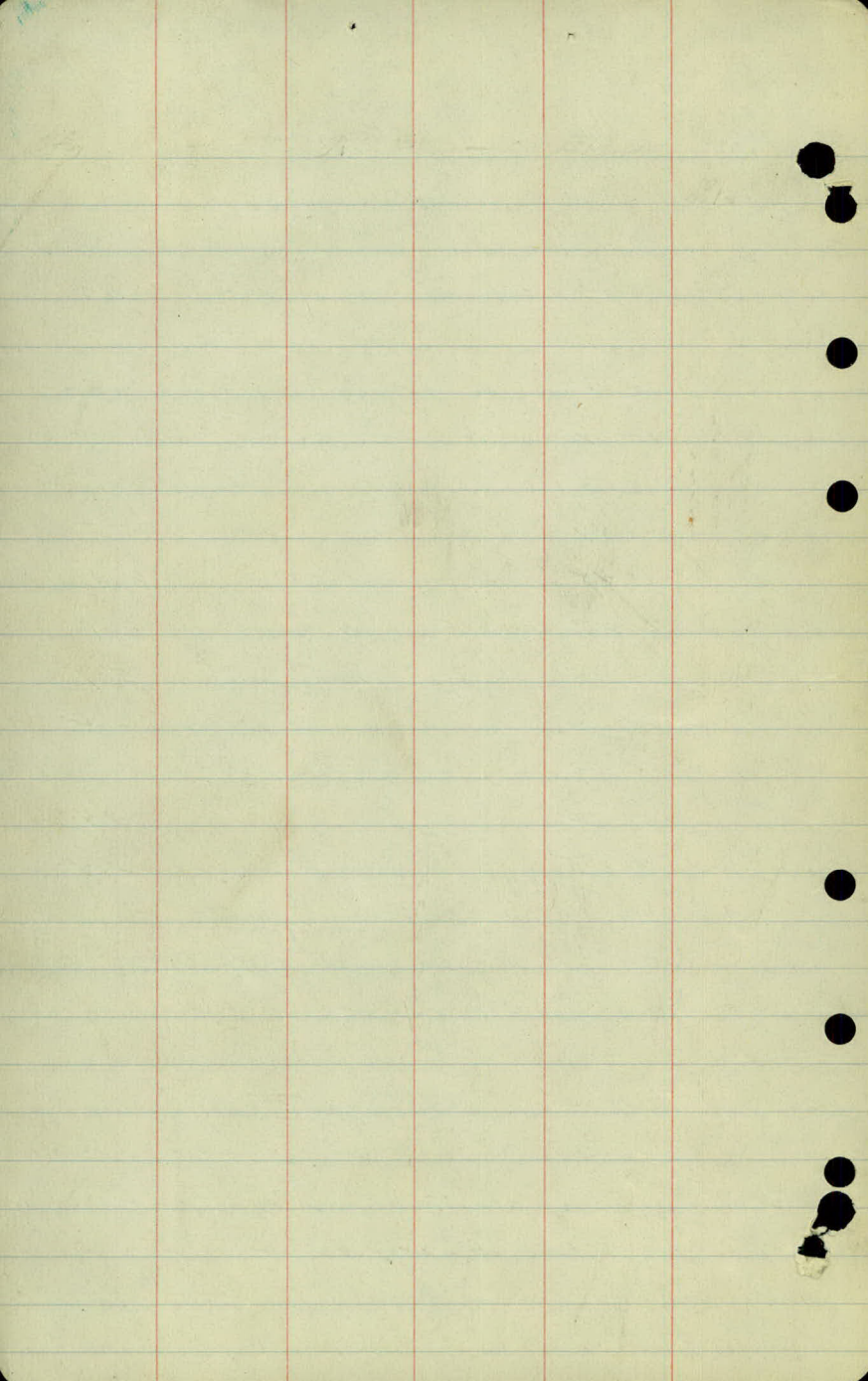
11+55

3.4

← East

County Road I.

Culverts in Vicinity of
R.L. Ritts on Right or
Lake Side.



Profile Levels Ditch S. Side

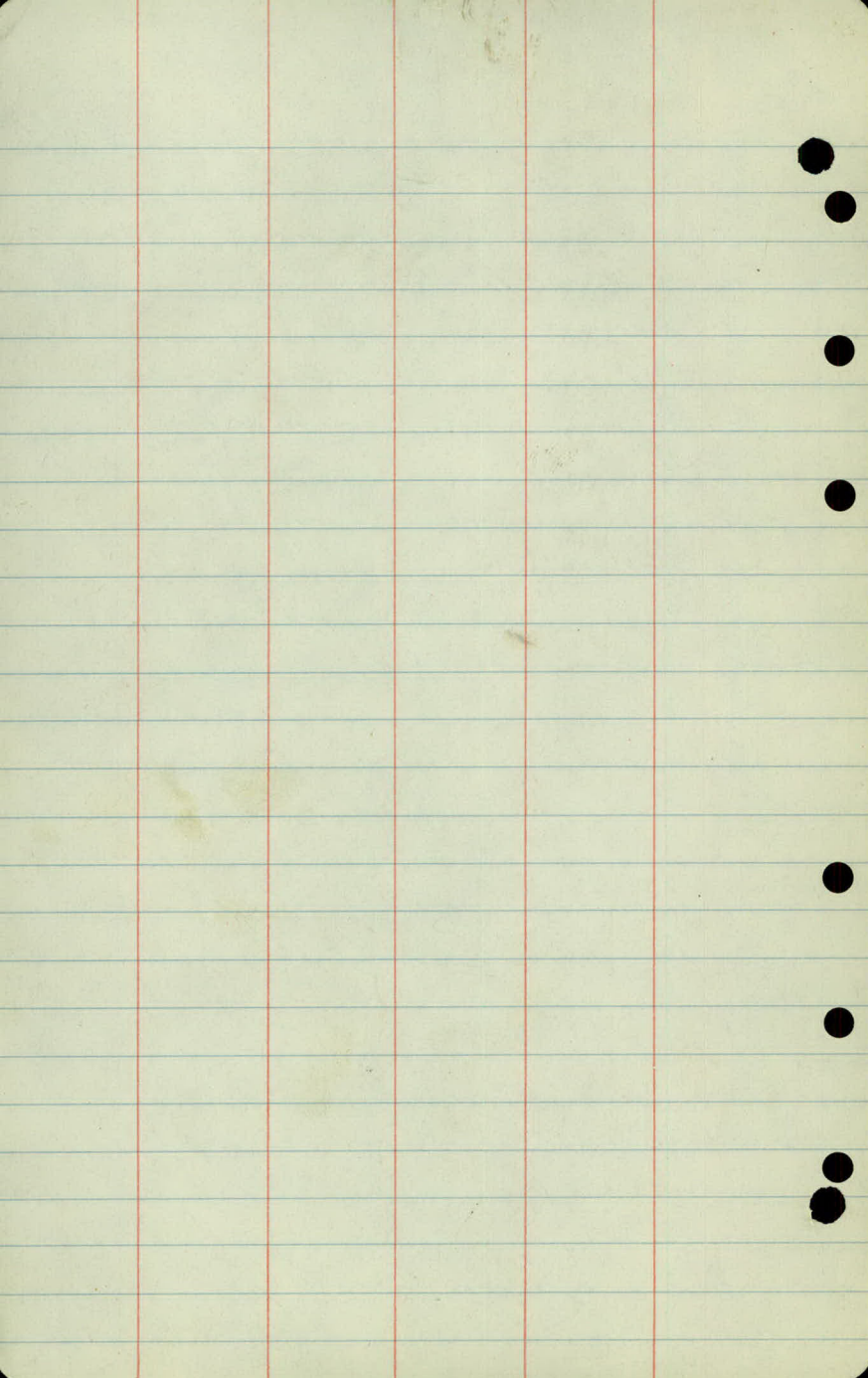
Co. Rd. I.

Sta	+	π	✓ -	Elev.
B.M.	3.44	895.44		892.00
24			9.2	86.2
+50			9.3	86.1
25	+50		9.8	85.6
+50			9.0	86.4
26			8.9	86.5
+50			8.5	86.9
27			8.6	86.8
+50			9.0	86.4
28			8.9	86.5
+50			8.7	86.7
29			8.1	87.3
+50			8.2	87.2
30			8.4	87.2
+	FL R		8.33	87.11
+	FL R		8.30	87.14
+50			7.9	87.5
31			7.7	87.7
+50			7.8	87.6
T.P	4.30	895.94 ✓	5.80	889.24 ✓
32			8.2	87.7
+50			8.2	87.7
33			7.8	88.1
+50			8.1	87.8
+	FL R.		8.50	87.44
+	FL R.		8.24	87.70

Top Mon. Lex. and Co. Rd. I

Sta	+	π	-	Elev
		895.94		
34			8.1	87.8
+50			8.0	87.9
35			8.1	87.8
+50			7.7	88.2
36		✓	7.6	88.3
B.M.	315	895.94	3.15	892.79 ✓
+50			7.4	88.5
+	F.L.R.	15"	7.78	88.16
37	F.L.R.	15"	7.65	88.29
+50			7.2	88.7
38			7.0	88.9
+50			6.9	89.0
39	F.L.R.	15"	7.0	88.94
+	F.L.R.	15"	7.10	88.84
39			6.8	89.1
+	FL	15"	6.80	89.1
+	F.L.	15"	6.90	89.0
40.			6.6	89.3

Top SE Cor M.H 33' L. 36400



Plan Survey

Ditch along Ea. Side Lex +
South Side Co. Rd "I"

Sta	+	Δ	-	Elev
	5.18	896.77		891.59
0+00				86.07

+50

1

+50

+77

Invert South

+78

Invert No

2

+50

3

+50

4

+50

Ditch

		86.07		
	Invert East End	10.70	Invert West End	0.8
Open	10.85		10.71	Sand
	85.92	Top of Water	86.06	
		9.70 87.07		
		10.9 85.87		
		10.8		
		10.8 85.97		
		10.7 86.07		
		10.8 85.97		
		10.9 85.87		
		10.6 86.17		
		10.7 86.07		
		10.8 85.97		
		10.6 86.17		
		10.7 86.07		
		10.4 86.37		

Sta	+	x	-	Elev
		896.77		

5				86.17
---	--	--	--	-------

+50				86.37
-----	--	--	--	-------

6				85.87
---	--	--	--	-------

T.P.	3.95	895.37	5.35	891.42
------	------	--------	------	--------

+41		Ditch East		86.17
-----	--	------------	--	-------

+50				85.9
-----	--	--	--	------

7				86.1
---	--	--	--	------

+35	X	Drain under Radius		
-----	---	--------------------	--	--

+50				86.4
-----	--	--	--	------

8				86.8
---	--	--	--	------

+50				86.8
-----	--	--	--	------

9				86.7
---	--	--	--	------

+50				87.1
-----	--	--	--	------

B.M.	3.36	895.37	3.36	892.01
------	------	--------	------	--------

(892.00)

4
Ditch

10.6

10.4

10.9

	86.4	86.6	86.8	87.2	87.2	87.2	87.6	87.6	87.4	87.4	87.3	87.6
9.2 -	$\frac{90}{4}$	$\frac{88}{31}$	$\frac{86}{62}$	$\frac{82}{100}$	$\frac{82}{160}$	$\frac{82}{200}$	$\frac{78}{260}$	$\frac{78}{300}$	$\frac{80}{360}$	$\frac{80}{400}$	$\frac{81}{450}$	$\frac{78}{500}$

(For add Shatzen Pitch) $\frac{87.8 \times 70}{514}$
see Page 10

9.5

9.3

86.45
8.92
Invert 50 End

86.59
8.78
Invert No End

9.0

8.6

8.6

8.7

8.3

Top of Mott It Lex.

Sta + A - Elev

895.37

10+00

87.1

+49 = 29+00

86.9

29+50

87.3

30+00

87.1

+06

Ditch West Side Ent

+26

Ditch East Side Ent

T.P

3.85

894.46

4.76

890.61

+50

87.6

31

87.8

+50

87.8

32

87.8

+50

87.4

33

X Drain under Lx

2

Ditch

83

8.5

8.1

8.3

87.22

8.15

Invert

87.22

8.15

Invert

87.4

8.6
50

87.6

78
100

87.8

7.6
150

88.0

7.4
200

88.7

67
250

88.7

67
300

87.6

78
350

87.7

77
400

87.1

8.3
50

87.1

8.3
100

87.3

8.1
150

87.7

7.7
200

87.8

7.6
250

88.0

7.4
300

88.1

7.3
350

69

6.7

6.7

6.7

7.1

88.0
6.5

87.53

6.93

Invert So Ent

87.16

7.30

Invert No Ent

Sta	+	$\nearrow$	-	Elev
		894.46		
33+32		Ditch	So	87.9
+50				87.6
+63				87.56
+83				87.73
34				87.7
+50				88.0
35				88.0
+50				88.2
+75		Ditch	So	88.3
			Beckleys	
B.M	3.02	895.81	1.66	892.80
36				88.3
+50				88.5

892.79

K
Ditch

	88.0	87.9
66	6.5	6.6
	<u>14</u>	<u>30</u>

6.9

6.9
Invert

6.73
Inv

6.8

6.5

6.5

6.3

	87.5	87.4	87.5	87.2	87.5	88.5	88.7	88.96
6.2	7.0	7.1	7.0	7.3	7.0	6.0	5.8	5.5
	<u>50</u>	<u>100</u>	<u>150</u>	<u>200</u>	<u>250</u>	<u>300</u>	<u>358</u>	<u>400</u>

Inv. Septic
Tank Outlet

298
↗

Branch to Newquist Ditch see Page 10

Top of Concrete Manhole SE Cor (36+64)

7.5

7.3

Sto + π - Elev
895.81

36 + 71 Westside Rd } 88.2
37 Eastside Rd } Boxley
Int 3 Rd.
Newquist
88.4

+50 88.7 88

38 89.0

+50 89.1

+68 89.1

+88 89.1

39 + 00 24" X Drain Under box

+33 89.2

+71 89.3

40 89.1

+50 89.5

£
Ditch

88.16	88.2	87.8	88.0	88.1	88.6	89.1	88.7
<u>7.65</u>	<u>7.6</u>	<u>8.0</u>	<u>7.8</u>	<u>7.7</u>	<u>7.2</u>	<u>6.7</u>	<u>7.1</u>
Invert	0	50	100	150	200	250	268
88.76	88.4	88.4	88.4	88.4	88.4	88.7	
<u>7.55</u>	<u>7.4</u>	<u>7.4</u>	<u>7.4</u>	<u>7.4</u>	<u>7.4</u>	<u>7.1</u>	
Invert	0	50	100	150	200	250	

7.1

6.8

6.7

6.7

88.81
7.00
Inv

6.7

6.7 89.1
Ditch

88.81
7.00
Invert 30 End

88.71
7.10
Invert No End

6.6

89.12
6.69
Invert

6.5

89.09
6.72
Inv

6.7

6.3

Sta	+	π	-	Elev
-----	---	-------	---	------

		895.81		
--	--	--------	--	--

40+28				89.4
-------	--	--	--	------

41+08				89.5
-------	--	--	--	------

+30				89.8
-----	--	--	--	------

+50				89.7
-----	--	--	--	------

42				90.1
----	--	--	--	------

+50				90.0
-----	--	--	--	------

43				90.2
----	--	--	--	------

+22				90.2
-----	--	--	--	------

6.4

89.51

6.30

Inv

6.3

6.30

Inv

6.0

6.00

Inv

6.1

6.60

Inv

5.7

5.8

5.2

5.6

Inv

5.6

5.8

Inv

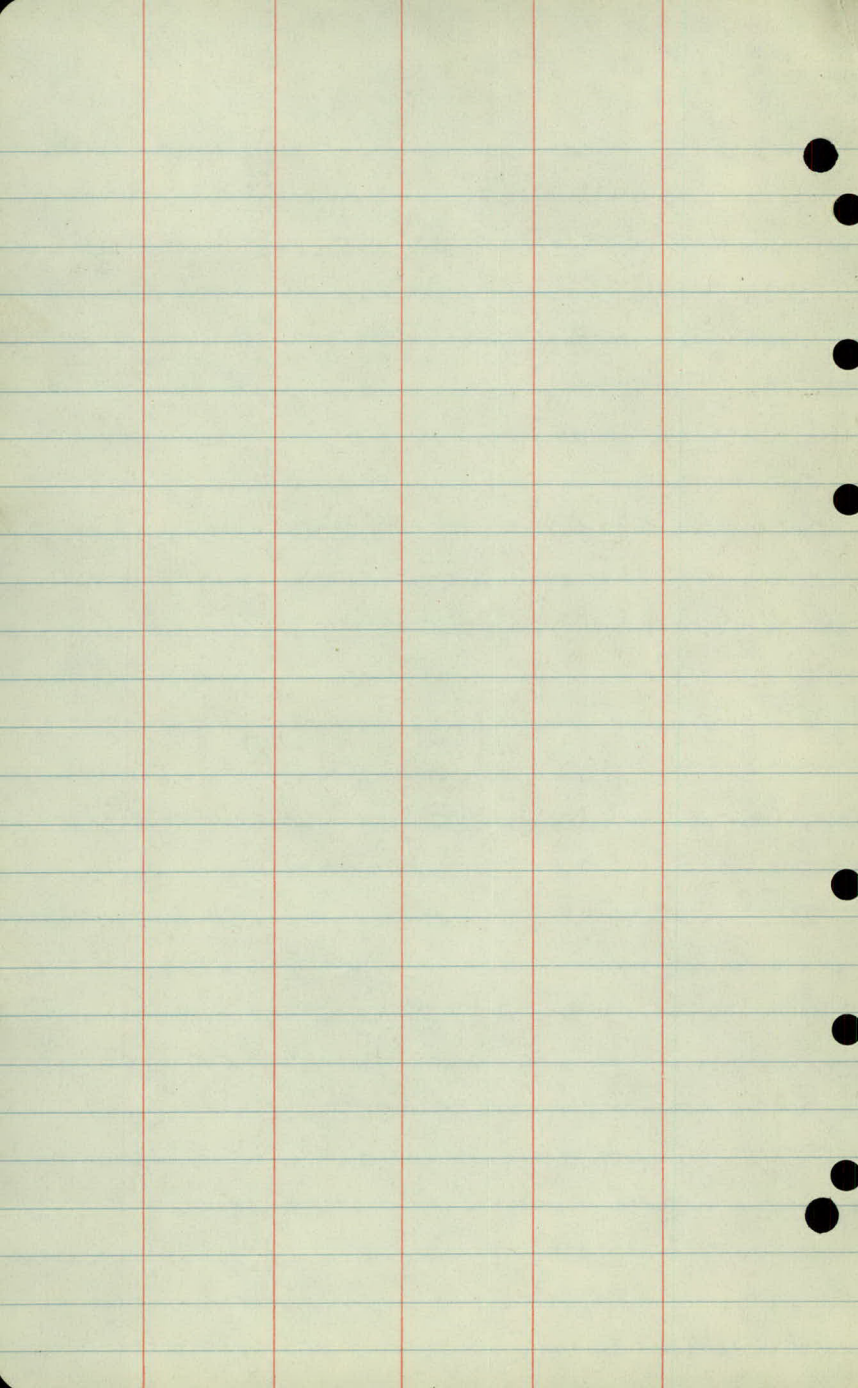
89.45

89.81

89.21

90.21

90.01



Drainage Ditches

East side + West side
OF Youngs Ent

Sta	+	π	-	Elev
	3.02	895.81		892.79

0 = 33+30 Lev Survey

+50

1
+50

2

+50

3

+50

+68

See Page 10 Δ in Pitch West

4

+25

+50

East

West

87.7 8.1

8.0 87.8

87.3 8.5

8.2 87.6

87.4 8.4

7.9 87.9

87.3 8.5

8.2 87.6

87.3 8.5

8.4 87.4

87.4 8.4

7.9 87.9

87.1 8.7

7.9 87.9

87.6 8.2

7.8 88.0

88.0 7.8

7.7 88.1

88.0 7.8

7.4 88.4

Sta	+	π	-	Elev
3.02		895.81		892.79

1.62		894.41		892.79
------	--	--------	--	--------

Top M.H Cover (Lt 36400 Lex)

88.0

7.8
298

From Ditch on Lex.

88.21

7.6
Inv

312

Newquist Septic Tank Outlet

87.61

6.8

368' From Lex A in Ditch Westside Youngs

87.8

6.6
80

87.91

Inv
6.5
58

87.8

6.6
100

87.5

6.9
150

87.4

7.0
200

87.7

6.7
275

Ent Ditch going West

Shots in Ditch going West

