

Dr. 6 - Bk. 72

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

----- Plan ----- Survey

VICTORIA STREET

From Owas Blvd. to Lexington

Road Acc't. No. 21

Date Filed July 1936

File Dr. 6 Bk 72

12/9/35

Porte 11

Alignment
Victoria St

9+1833

P.L.

A 0° 29' Rt.

4+00

P.O.T.

0+00

Mont
N¹/₄ Cor Sec 2

Boat 2nd E

Mont
Cor Sec 2

41 + 87.65 P.O.T.

36 + 93.10 P.T.

13° 15

+ 75

11° 56.3

+ 50

10° 07.5

+ 25

8° 18.8

36 + 03.40 P.I.

36

6° 30

+ 75

4° 41.3

+ 50

2° 52.5

+ 25

1° 03.8

35 + 10.34 P.C.

15.72 38.75
 TP. 10" Oak

24°30'

Boat Spk

TP.
 82.59
 25.91

Δ 26°30' Rt
 L 182.76 ✓
 T 93.06
 D 14°36'
 R 395.21
 E 10.81

TP.
 79.91

56.60
 TP.

61+68.22 PT.

61+13.45 P.I.

A 5° 27' Rt

D 5° 00

T 54.90 ✓

L 109.67 ✓

E 1.31

60+58.55 PC

59+00 P.O.T.

57+89 - 1/4 Line Xs

53+75.14 =

52+75.34 PT.

51+89.95 P.I.

51+04.92 PC.

51+04.72

Boat SpK

RR 70K

T.P.

Steel FP

X 23.37

26.83

120° 18'

1008.75

Ctr Sec 35

Δ 03° 24' 30" R

T 85.03 85.23

L 170.42 ✓

D 2° 00' Boat SpK

53.25

15" Oak F.P.

68.75

15" Oak

Well in F.P.

POT.

64+85.53 PT

63+96.07 PI

ctr. Curve 63+93.03

25' Chords

Δ 35° 09' LT

D 190.00.

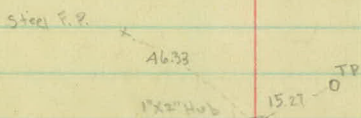
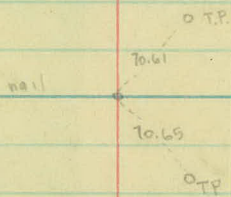
T 95.54

L 185.00

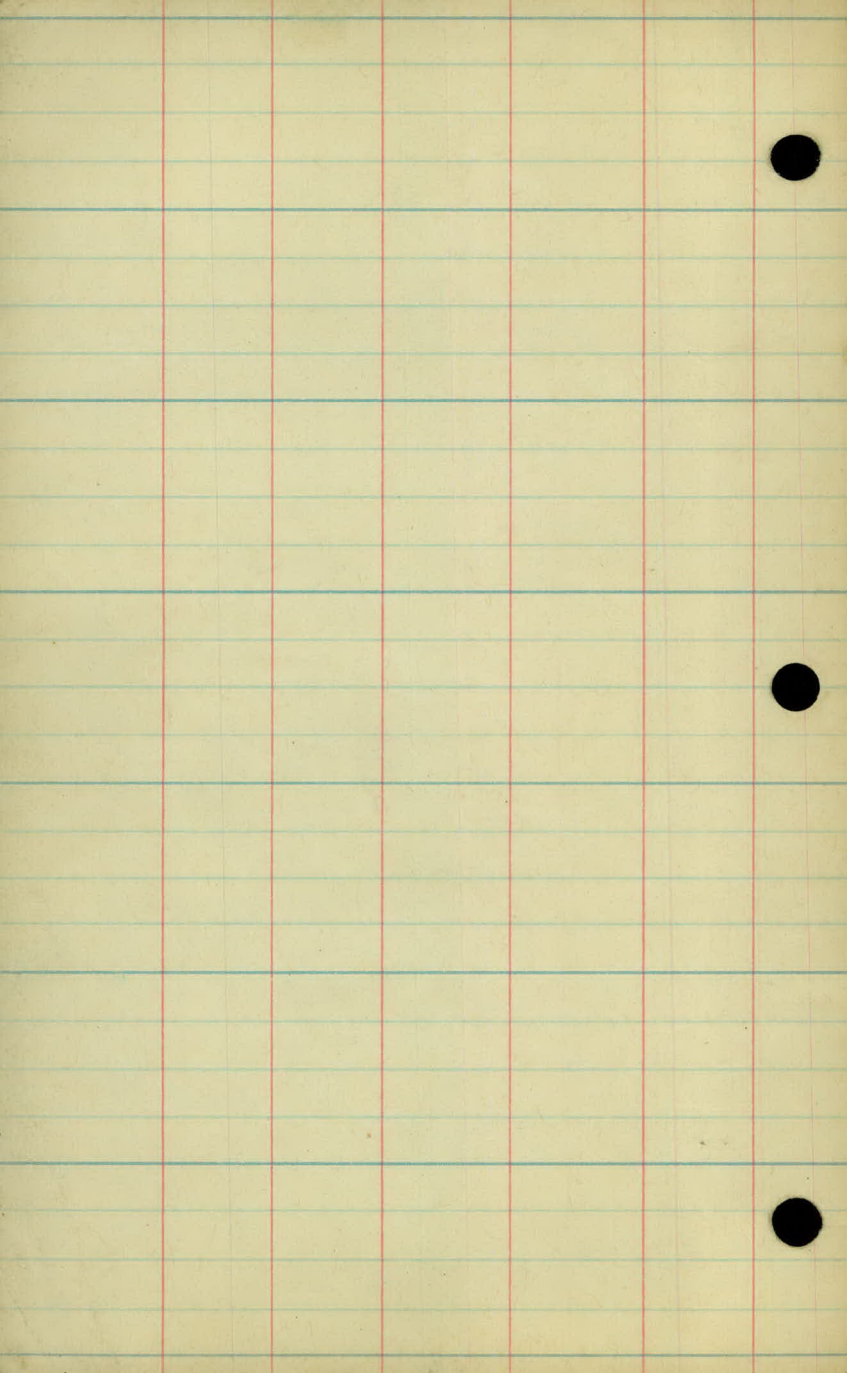
E 14.77

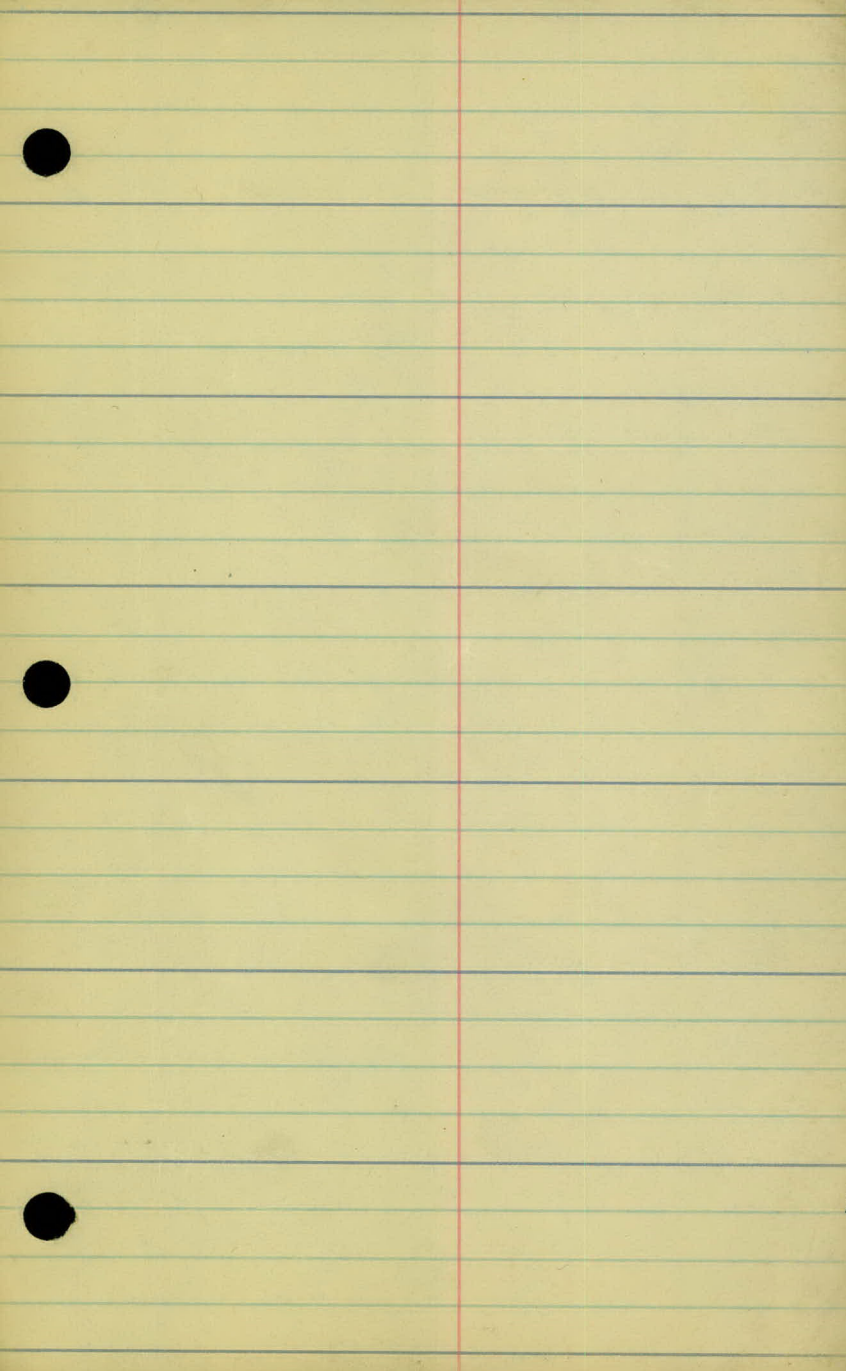
R 301.64

63+00.53 PC



Boat Spk.





79+21.33 PC.

74+37.54 PT.

73+43.27 P.I.

72+34.47 PC.

67+21.40 POT.

(25' Chords)

T.P.

58.11

2x2 Hub

30.41

T.P.

Δ $50^{\circ}46'$ Lt

T 108.80

D $25^{\circ}00'$

L 203.07

R 229.30

Nail

70.61

T.P.

70.65

T.P.

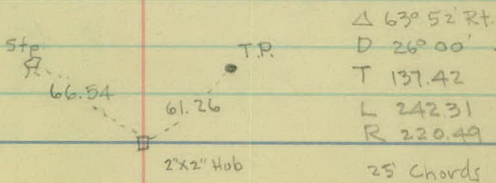
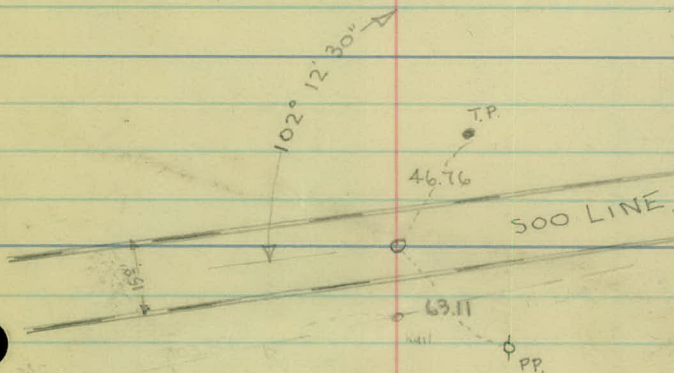
95+29.17 P.I. Δ 0°18' Rt

89+22.55 P.I. Δ 2°19' Lt

87+94.50 P.O.T.

81+63.64 P.T.

80+58.73 P.I.



Δ 63° 52' Rt.
 D 260' 00"
 T 137.42
 L 242.31
 R 220.49
 25 Chords

+57.89 P.T.

116 5° 21.1

115 3° 51.1

+51.37 P.T.

114 2° 21.1

113 0° 51.1

112+43.17 P.C.

$\Delta 12^{\circ} 26.5' Lt$

D $3^{\circ} 00'$

T 208.70 ✓

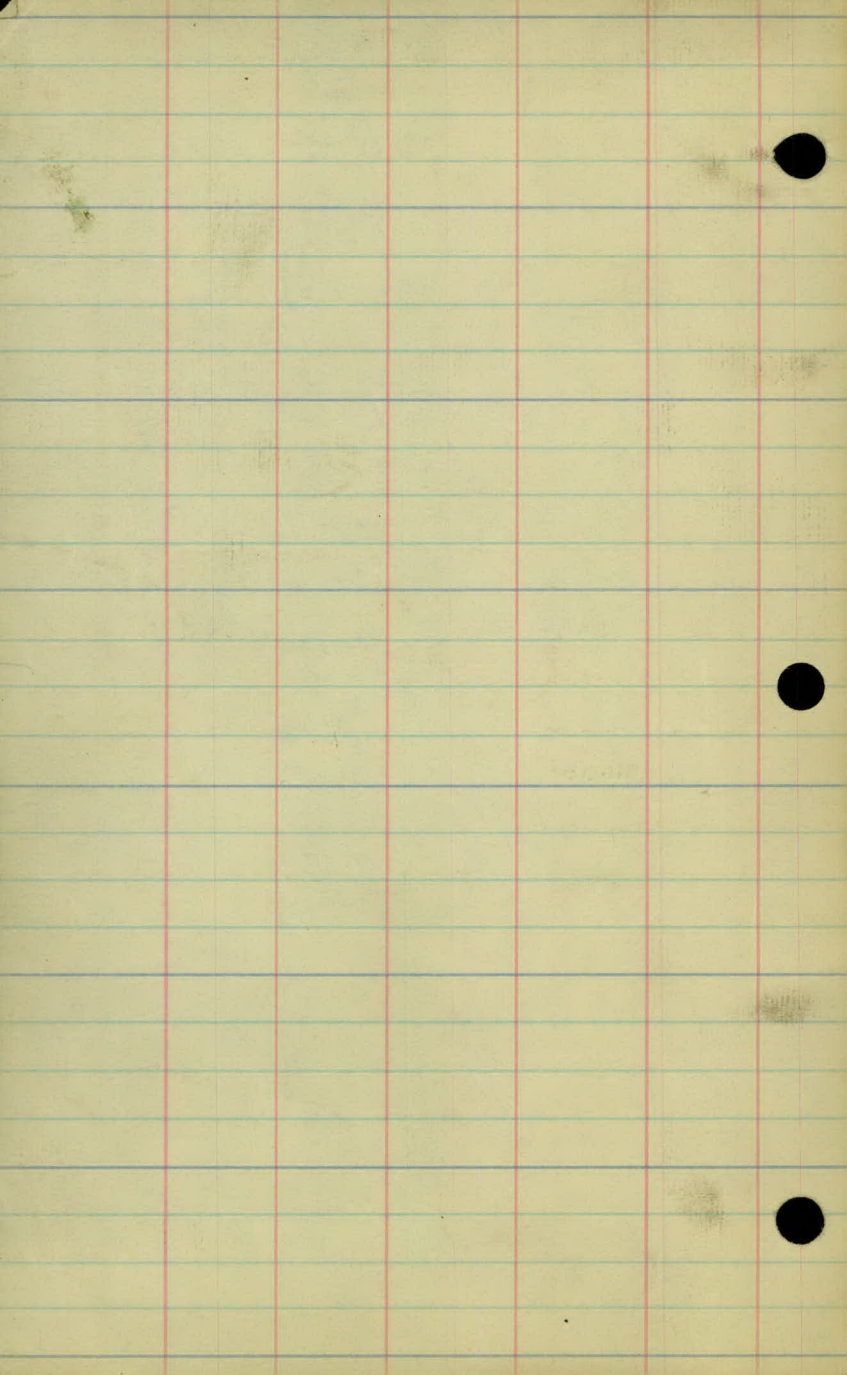
L 414.72 ✓

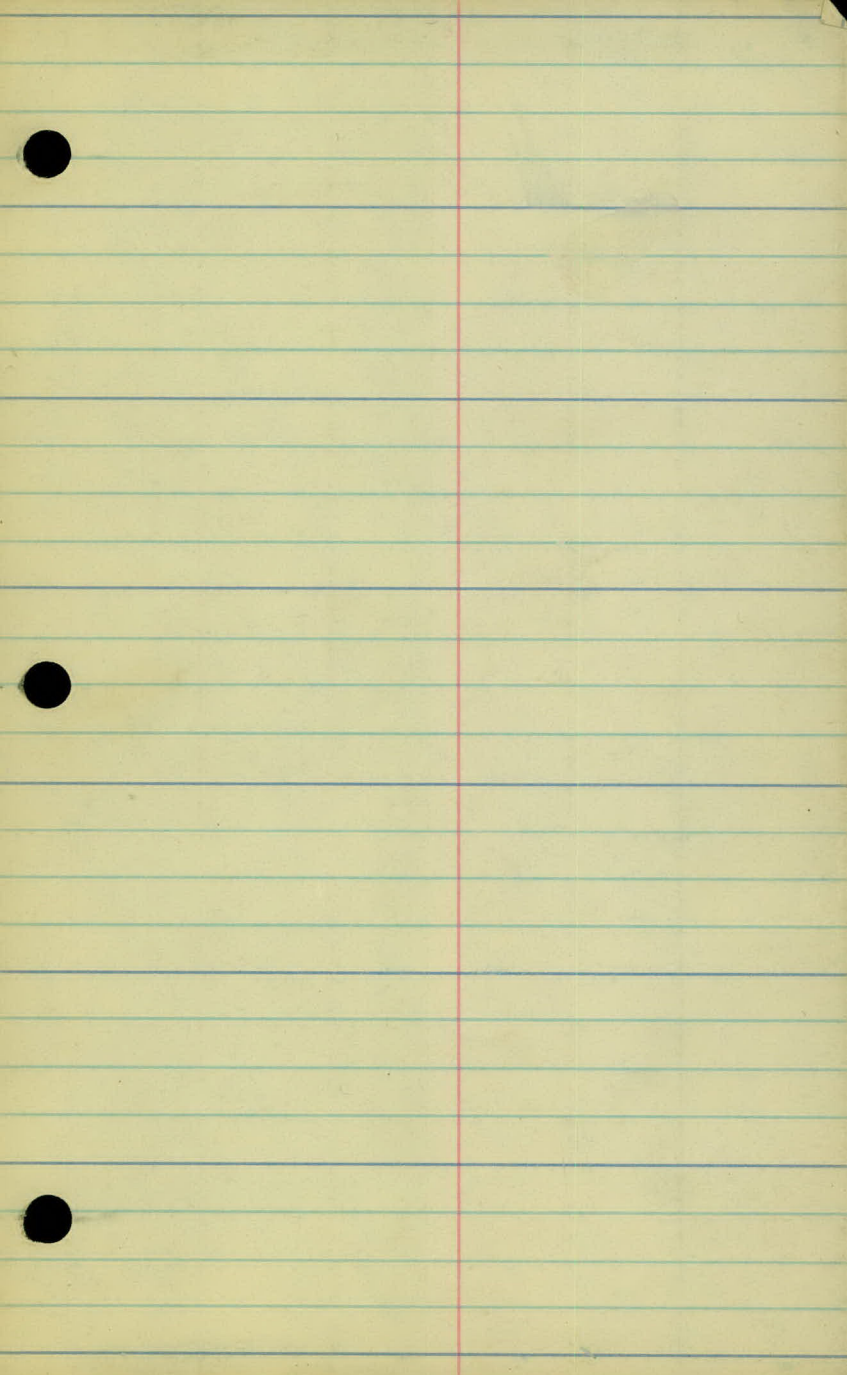
R 1910.08 ✓

RR SpK

2x2 Hub

RR SpK





132 + 02.69 P.T. $2^{\circ} 24'$

131 $2^{\circ} 08.6'$

130 $1^{\circ} 53.6'$

POST 251.35' Ahead of P.I.

129 $1^{\circ} 38.6'$

128 $1^{\circ} 23.6'$

127 + 22.95 P.I.

127 $1^{\circ} 08.6'$

126 $0^{\circ} 53.6'$

125 $0^{\circ} 38.6'$

124 $0^{\circ} 23.6'$

123 $0^{\circ} 08.6'$

122 + 42.69 P.C.

RR3PK

R.R. SpK

Hub

BoatSpK

Hub

80'

251.35

$\Delta 4^{\circ} 48' \text{ Lt}$

T 480.26 ✓

New Canada
Church Steeple

D $0^{\circ} 30'$

L 960.00 ✓

R.R. SpK

142+28.45 PT $4^{\circ}20.5$

142 $3^{\circ}46.4$

+50 $2^{\circ}46.4$

141+20.16 P.I.

141 $1^{\circ}46.4$

+50 $0^{\circ}46.4$

140+89.93 POST.

So Line Sec 23

140+11.37 P.C.

138+00 P.O.T

R.R. SpK

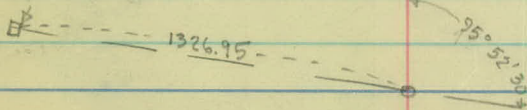
$\Delta 8^{\circ}41'Lt$

D $4^{\circ}00'$

T 108.79

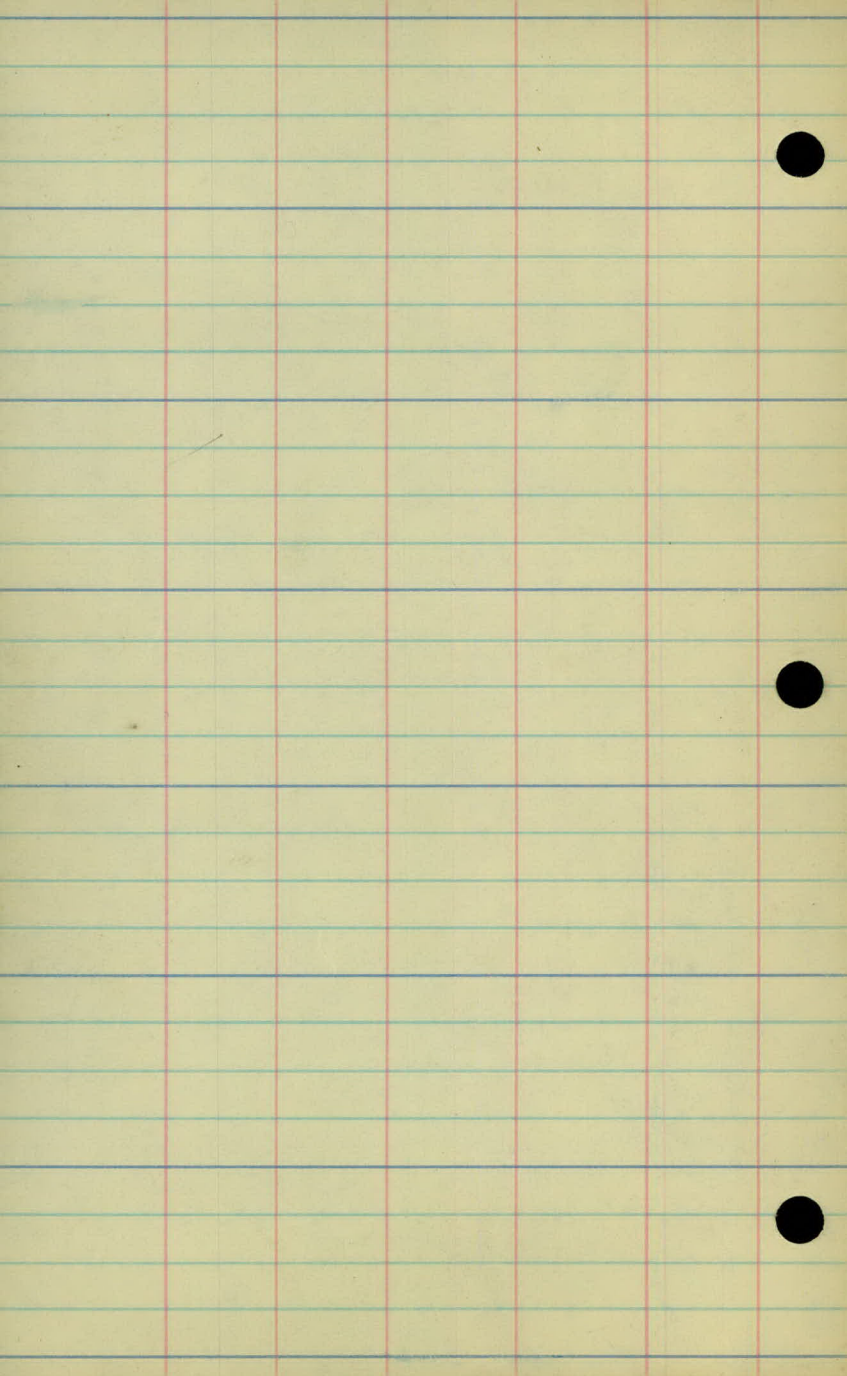
L 217.08

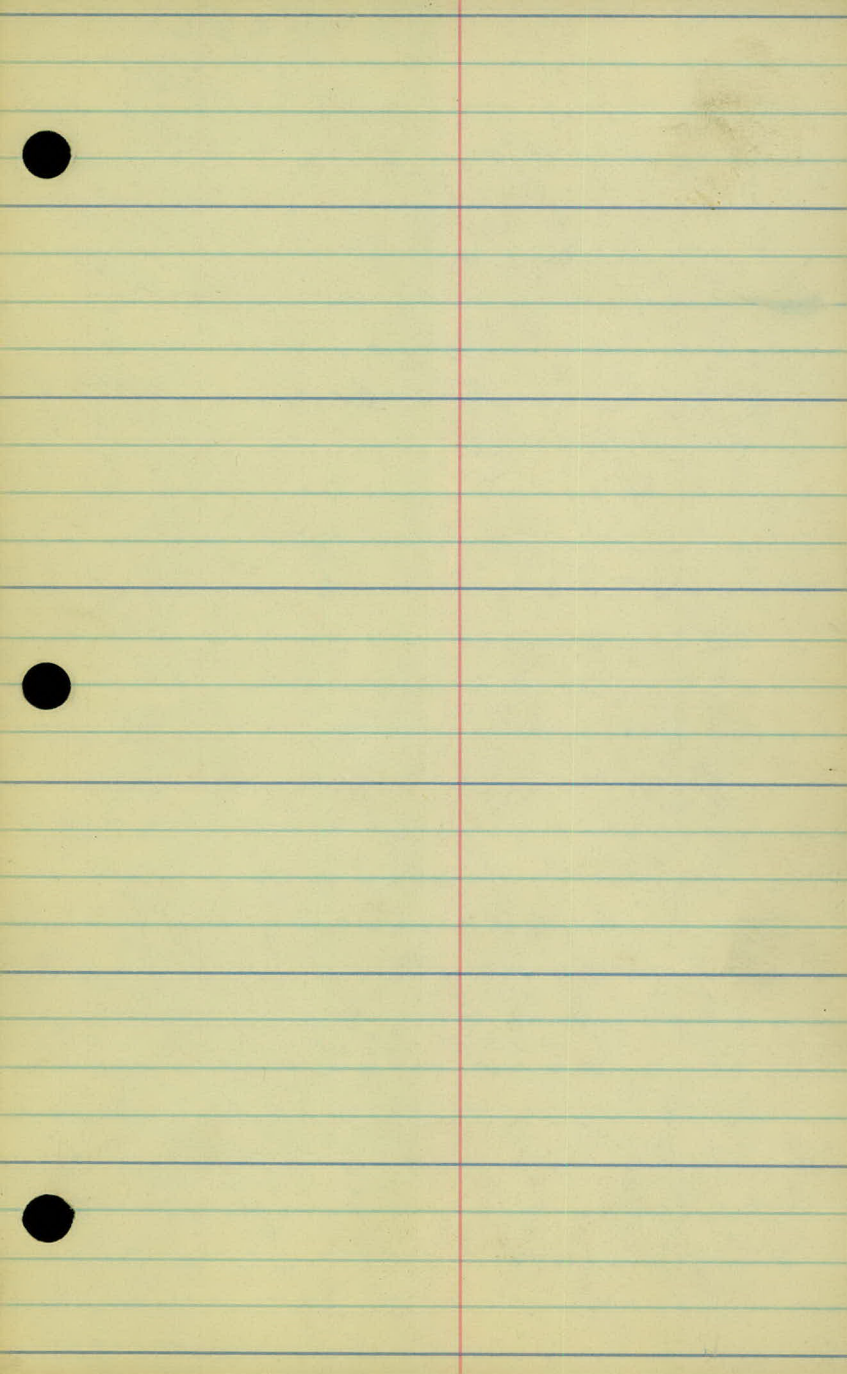
So $\frac{1}{4}$ Cor Sec 23



RR SpK

R.R.





153 + 26.73 P.O.T.

+ 38.05 P.T. $5^{\circ}39'$

151 $5^{\circ}10.5'$

50 $3^{\circ}50.5'$

+ 12.8 P.I.

149 $2^{\circ}40.5'$

148 $1^{\circ}45.5'$

147 $0^{\circ}10.5'$

146 + 86.05 P.C.

145 + 00.78 P.O.T.

253.3
5.1
3-15

Hub

LT
 $\Delta 11^{\circ} 18' R$
T 226.75
L 452.00
D 2030'

+76.46 P.T. 20° 18'

+50

19° 45'

159

17° 45'

+50

15° 45'

158

13° 45'

+50

11° 45'

+33.94 P.I.

157

9° 45'

+50

7° 45'

156

5° 45'

+50

3° 45'

155

1° 45'

154 +68.96 P.C.

Hub

~~$\Delta 40^{\circ}36' Lt$~~

~~T 264.98~~

~~L 607.5~~

~~D 8900'~~

+50

15°32.3

164

13°47.3

+50

12°02.3

163

10°17.3

+50

8°32.3'

162

6°47.3

+50

5°02.3

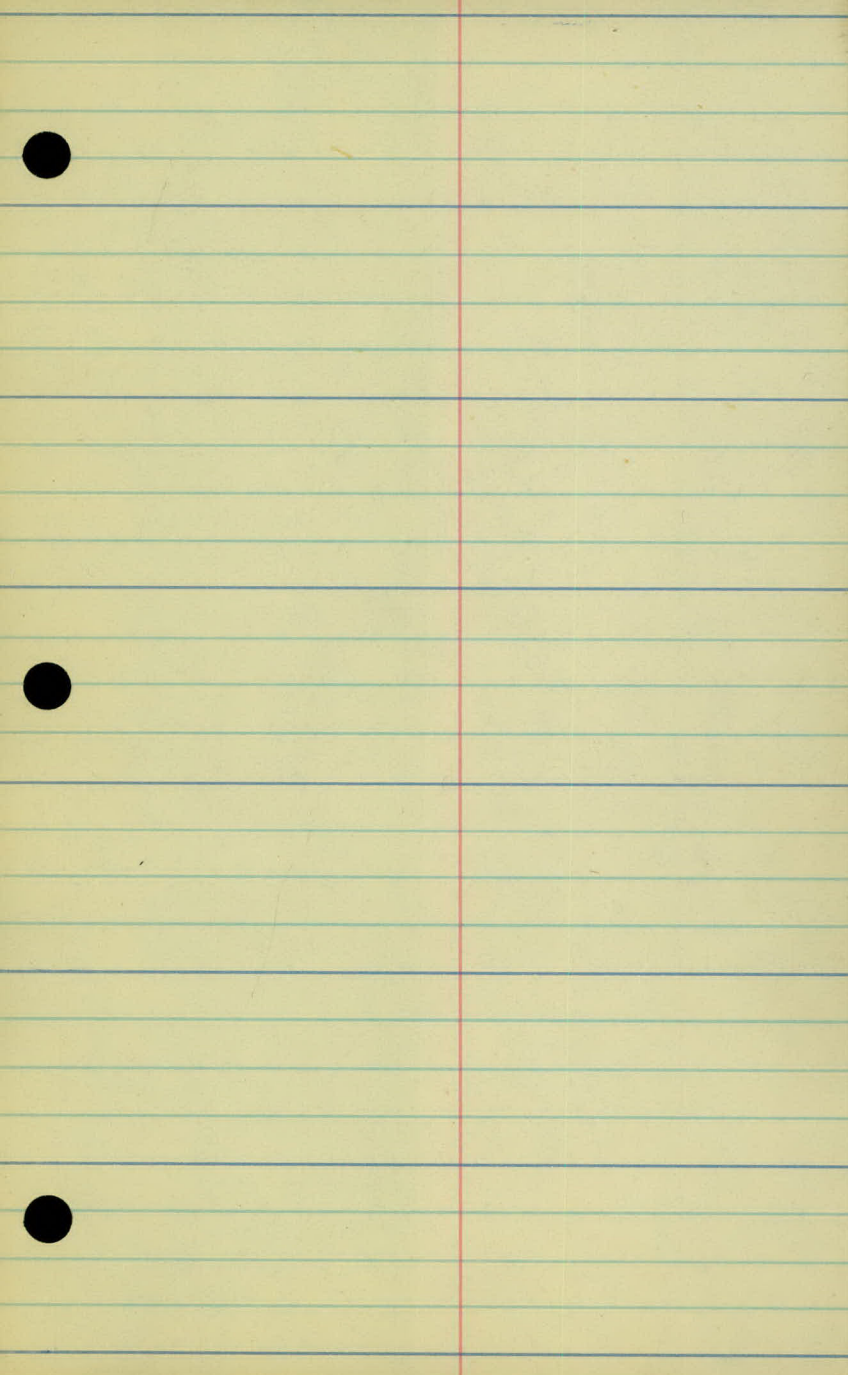
161

3°17.3

+50

1°32.3

160+06.03 P.C.



+56.51 P.T. 33° 16'

+50

169 31° 17.3

+50 29° 32.3

168 27° 47.3

+50 26° 02.3

167 24° 17.3

+50 22° 32.3

166 20° 47.3

+50 19° 02.3

+43.09 P.L.

165 17° 17.3'

$\Delta 66^{\circ} 32' R+$

D 7°00'

L 950.48

T 537.06

Hub

172		35° 00.7
+90		33° 30.7
+80		32° 00.7
+70		30° 30.7
+60		29° 00.7
+53.53	P.I. =	(Etr Sec 23-33' Ahead of P.I.)
+50		27° 30.7
+40		26° 00.7
+30		24° 30.7
+20		23° 00.7
+10		21° 30.7

171		20° 00.7
+90		18° 30.7
+80		17° 00.7
+70		15° 30.7
+60		14° 00.7
+50		12° 30.7
+40		11° 00.7
+30		9° 30.7
+20		8° 00.7
+10		6° 30.7

170		5° 00.7
+90		3° 30.7
+80		2° 00.7
+70		0° 30.7

169+66.59 P.C.

Void
See next.

88°46'

23

CE

0

Void
see revision

48846' Lt

T 186.94

R 191.01

E 76.26

L 29589

D 30°00'

198+16.15

E Lexington Ave

191+16.20

P.O.T.

184+96.15

P.I.

A 1° 26' 30" Lt

~~North
survey.~~

+62.48 PT

44° 23'

+60

44° 00.7

+50

42° 30.7

+40

41° 00.7

+30

39° 30.7

+20

38° 00.7

172 +10

36° 30.7

Iron Pn



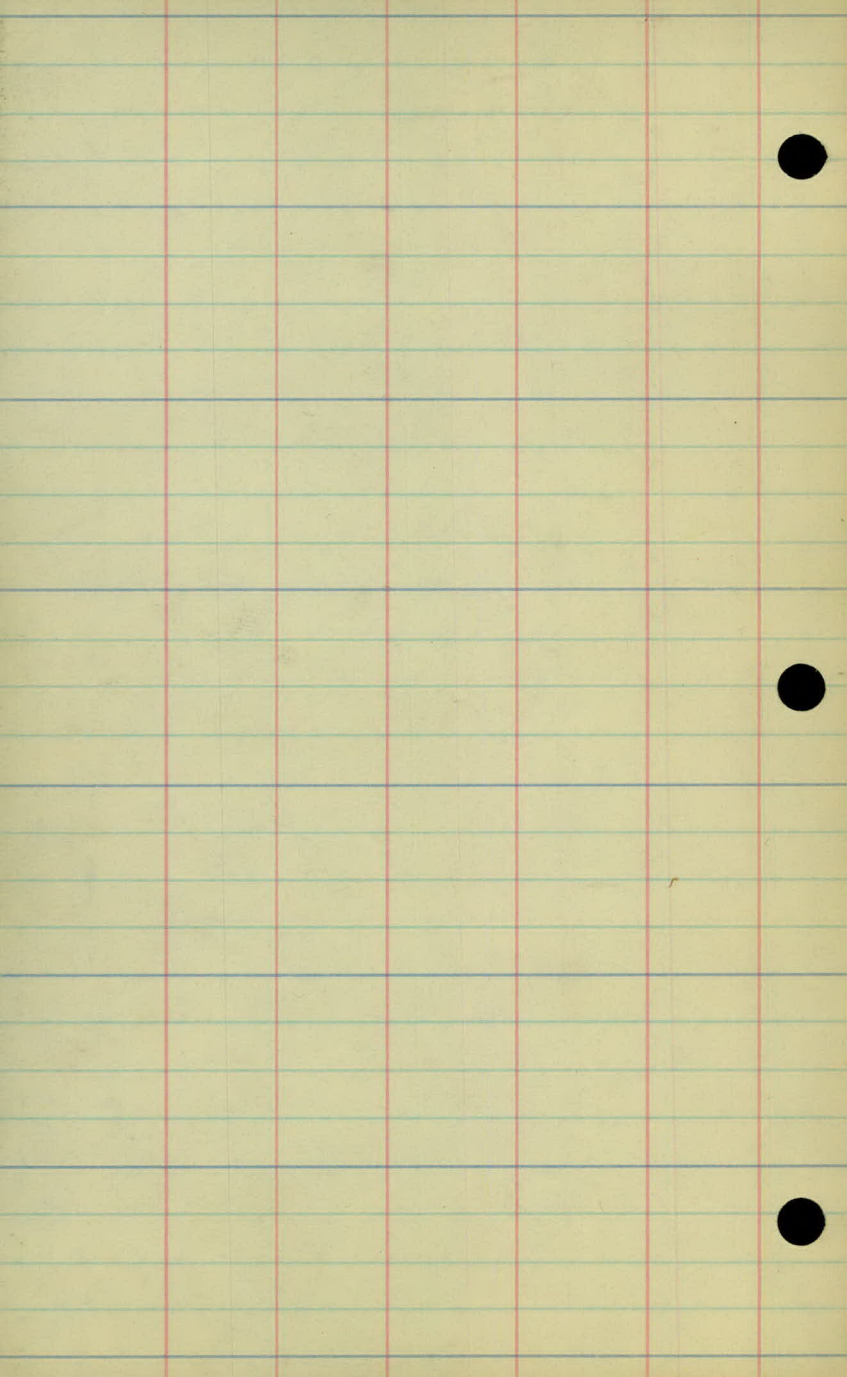
RRSpK



RRSpK



~~void
see row.~~



6/22/36

H.T. Fortell

Revision

@

Lundgrens

P.L.

172+90.61 P.T.

171+77.00 P.L.

169+90.04 P.C.

P.T. 168+97.39 P.T.

A $87^{\circ}10'14$

D $29^{\circ}00$

T 186.96

L 300.57 ✓

E 75.18

25' chords

$$4 \text{ } \#$$
$$183 + 96.65$$

$$184 + 25.2 =$$

$$199 + 55.51 \text{ PT.}$$

$$177 + 28.09 \text{ PT.}$$

$$175 + 00.51 \text{ PC}$$

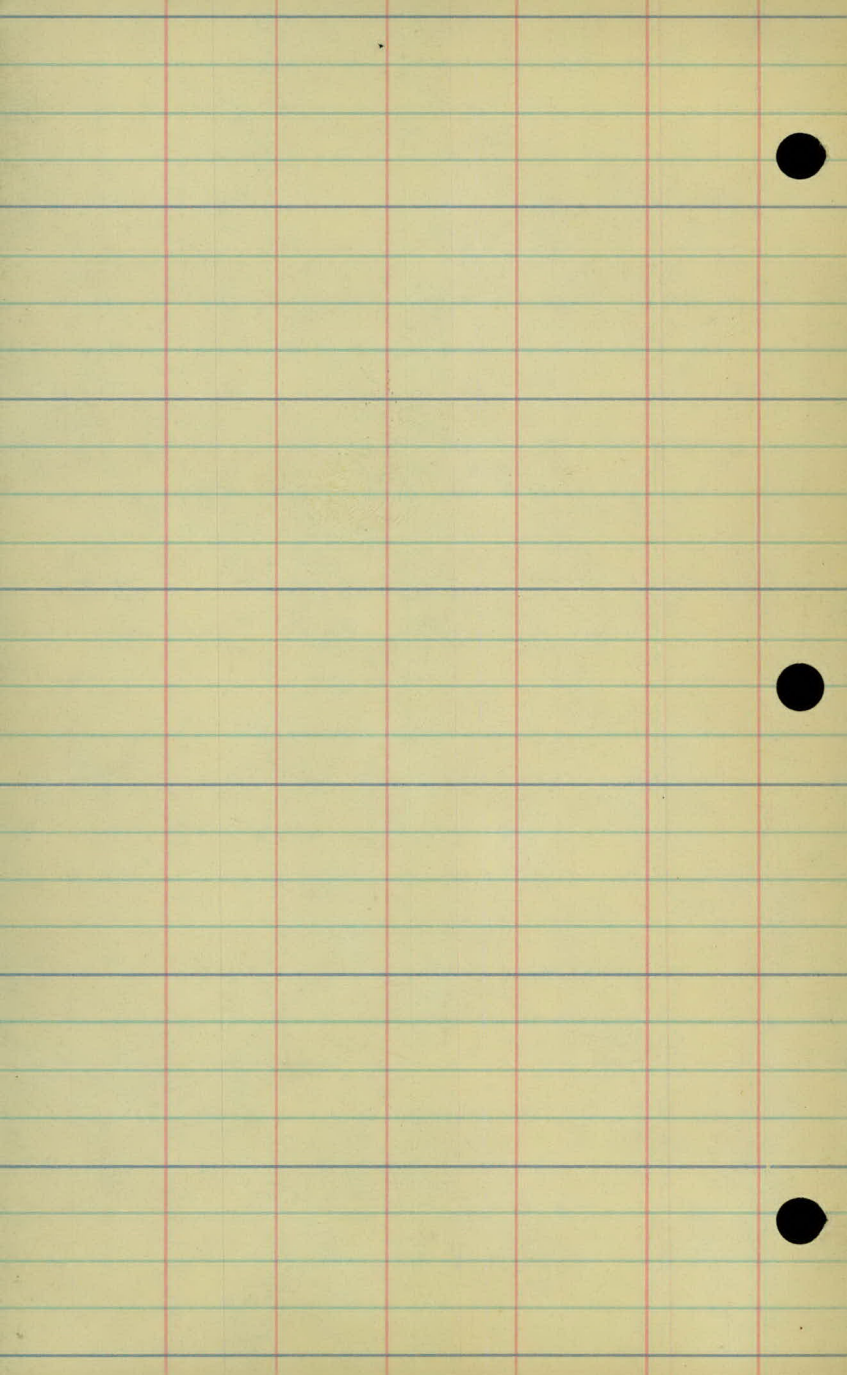
$\Delta 3^{\circ} 02' 14''$

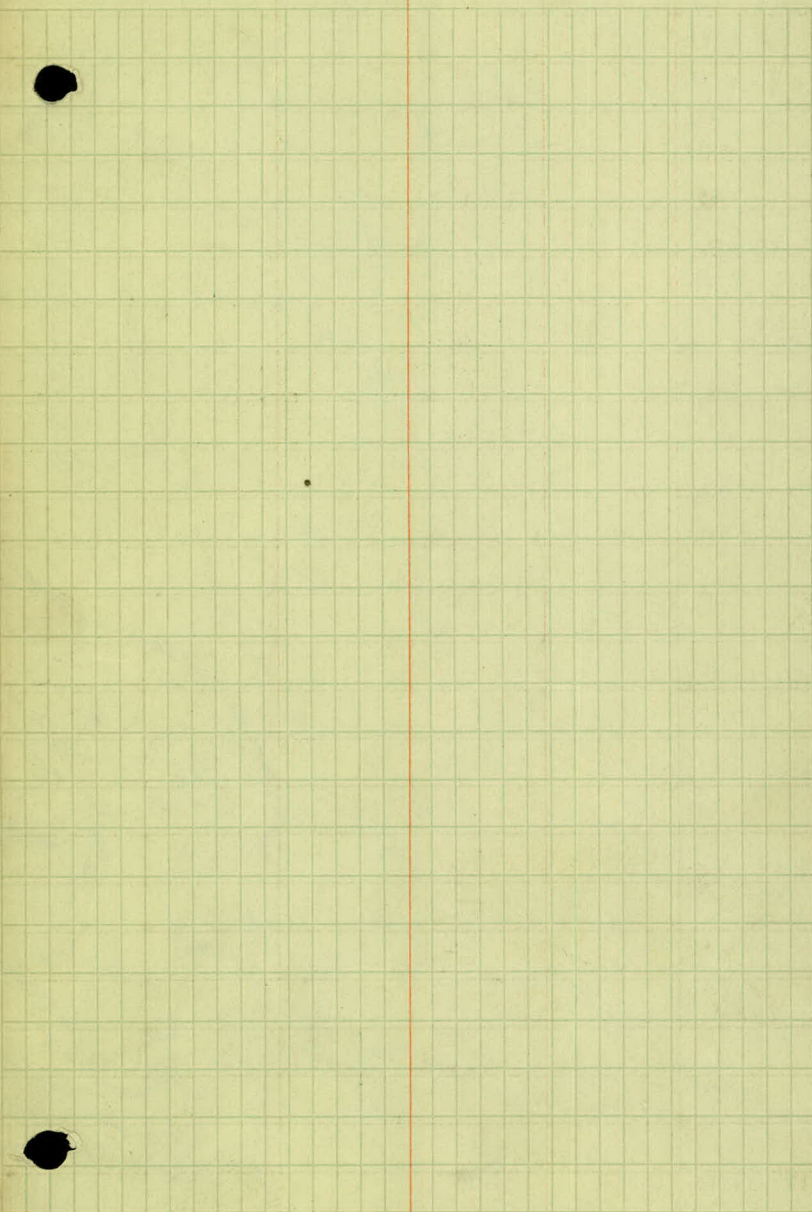
$D 0^{\circ} 40'$

$T 227.58$

$L 455.0$

$E 30'$





81 24° 59.26

+75 22° 14.26

+50 19° 29.26

80+21.95 P.I.

+25 16° 44.26

80 13° 59.26

+75 11° 14.26

+50 8° 29.26

+25 5° 44.26

79 2° 59.26

L 78+72.84 P.C.

L 74+37.35 P.T.

73+43.27 P.I.

L 72+36.31 P.C.

L 72+34.47 P.C.

L 72+34.47 P.O.T.

0
9
abad
see
D
10
K

Δ 59° 34' Rt

T 149.11 -

L 270.76

D 22° 00

R 260.54

75' E Hub
 510
 $\Delta = 48^\circ 15' \text{ Lt}$
 T 106.96
 R 238.84 -
 L 201.04
 E 22.86
 D 24° 00'

90+12.34

L 89+81.95 =

P.I.

Δ

10° 30' 30" Lt

L 90+37.9

P.O.T.

L 87+61.72

L 87+31.35

P.I.

Δ 0° 59' 30" Rt.

L 87+26.89

L 86+96.50

Sec Line Xs

L 81+43.60

P.T.

29° 47'



+25

27° 44.26

RR Spk

87+68.81

(87+38.42)
P.O.T.

15'

78°37'

SOOLINE

Nail in Pk @ EDM
of Sooline

Mountain Trk

N Line Sec 35

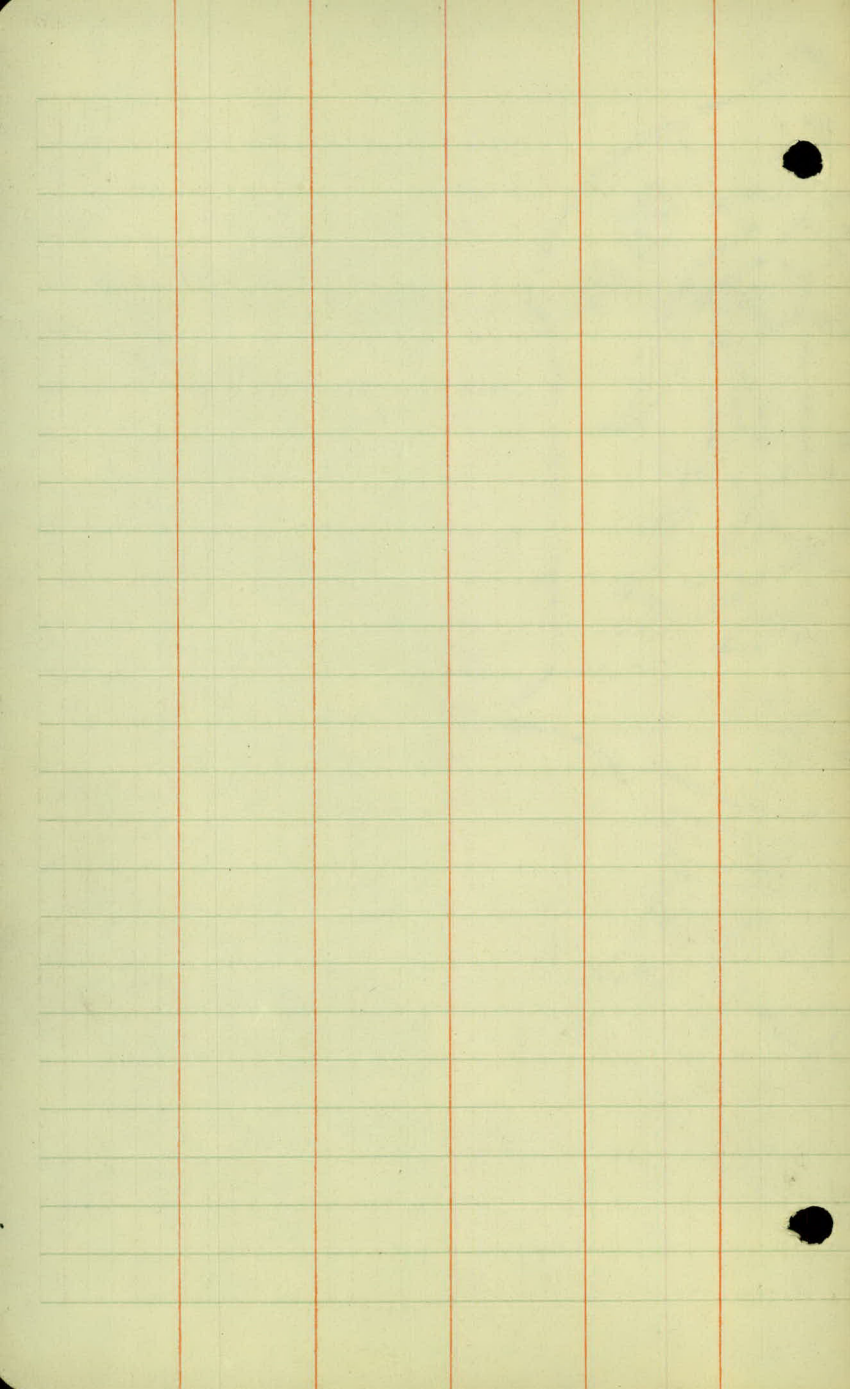
M.C.

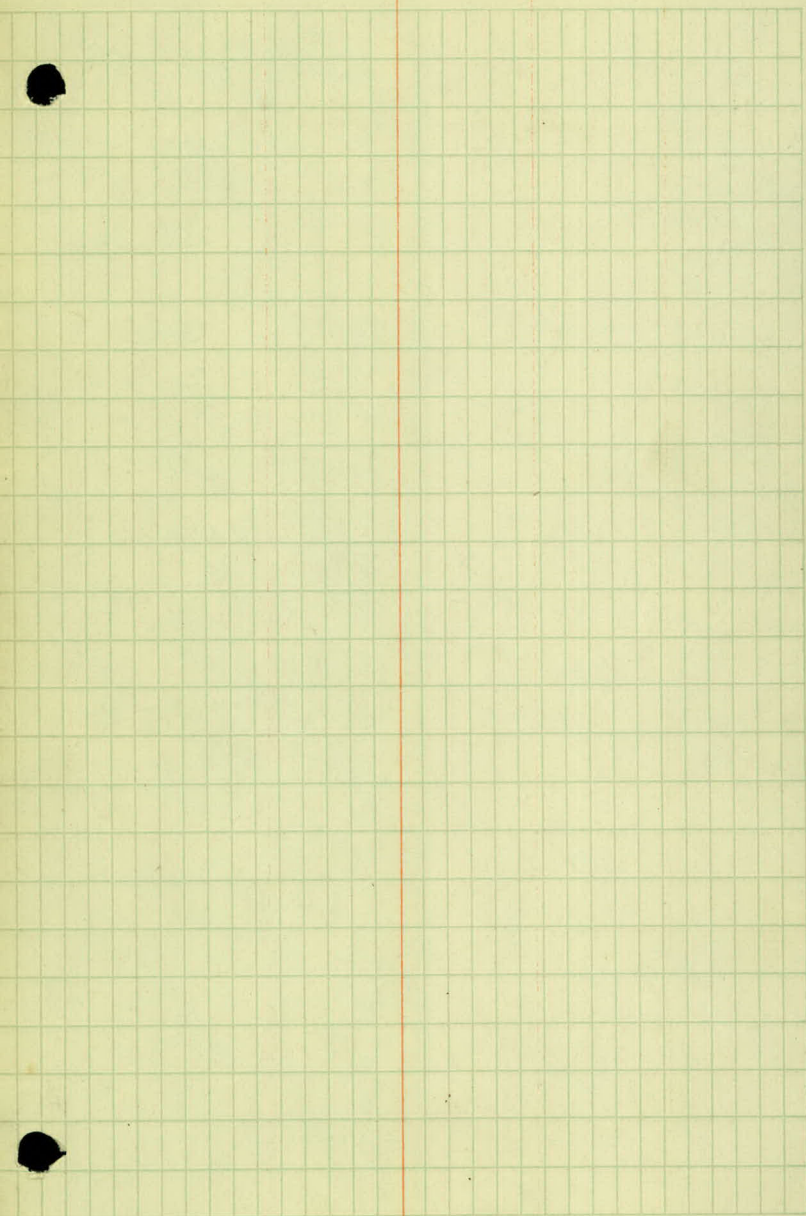
803.87

1690.82

NE Cor Sec 35

78°21'





+25

24° 23.7

81

21° 38.7

+75

18° 53.7

80 + 52.34 Pl.

+56 Fee Xs

+50

16° 08.7

+25

13° 23.7

80

10° 38.7

+75

7° 53.7

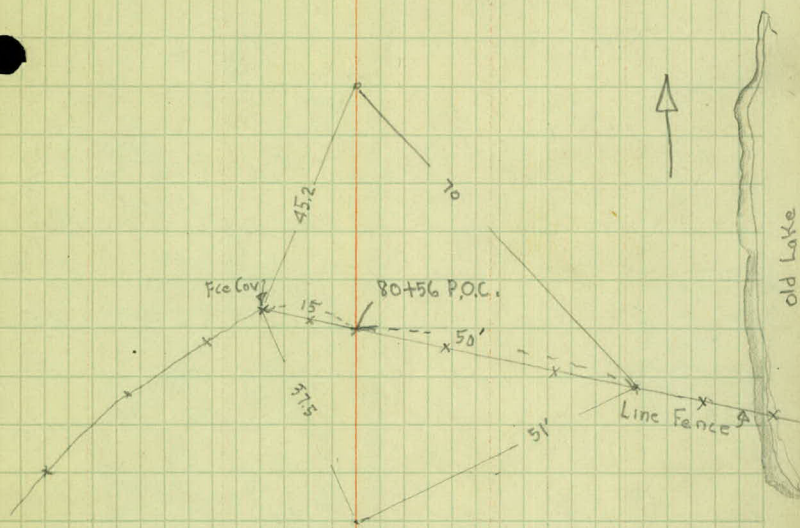
+50

5° 08.7

+25

2° 23.682

79 + 03.23 PC



81+73.99

P.T.

29°47'

81 +50

27°08.7

6/2/36

H.T.P.

Alignment
@
Lundberg's

80

+75

80+40.95

RL

80+42.34

+50

+25

79

78+84.25

PC

78+85.64

12°44'

7°59'

7°14'

4°29'

1°43.95'

74+39.42

PT

74+40.81

73+43.27

PI

72+31.09

PC

$\Delta 62^{\circ}04$

T 156.70 ✓

L 282.13 ✓

D $22^{\circ}00$

25' Ch.

$\Delta 50^{\circ}20$ Lt

T 112.18 ✓

209.72 ← L 208.33

D $24^{\circ}00$

E 25.05

25' Ch

$\frac{87+74.83}{87+73.44}$ P.I. (Equation) $\Delta 0^\circ 33' 30'' \text{ Rt.}$

$\frac{87+40.01}{87+38.62}$ Sec Line

$\frac{81+66.38}{81+67.77}$	PT	$31^\circ 02'$
		29 14
+25		26 29
81		23.44
+15		$20^\circ 59'$
+50		$18^\circ 14'$
+25		$15^\circ 29'$

RR Spk

NE Cor Sec 35

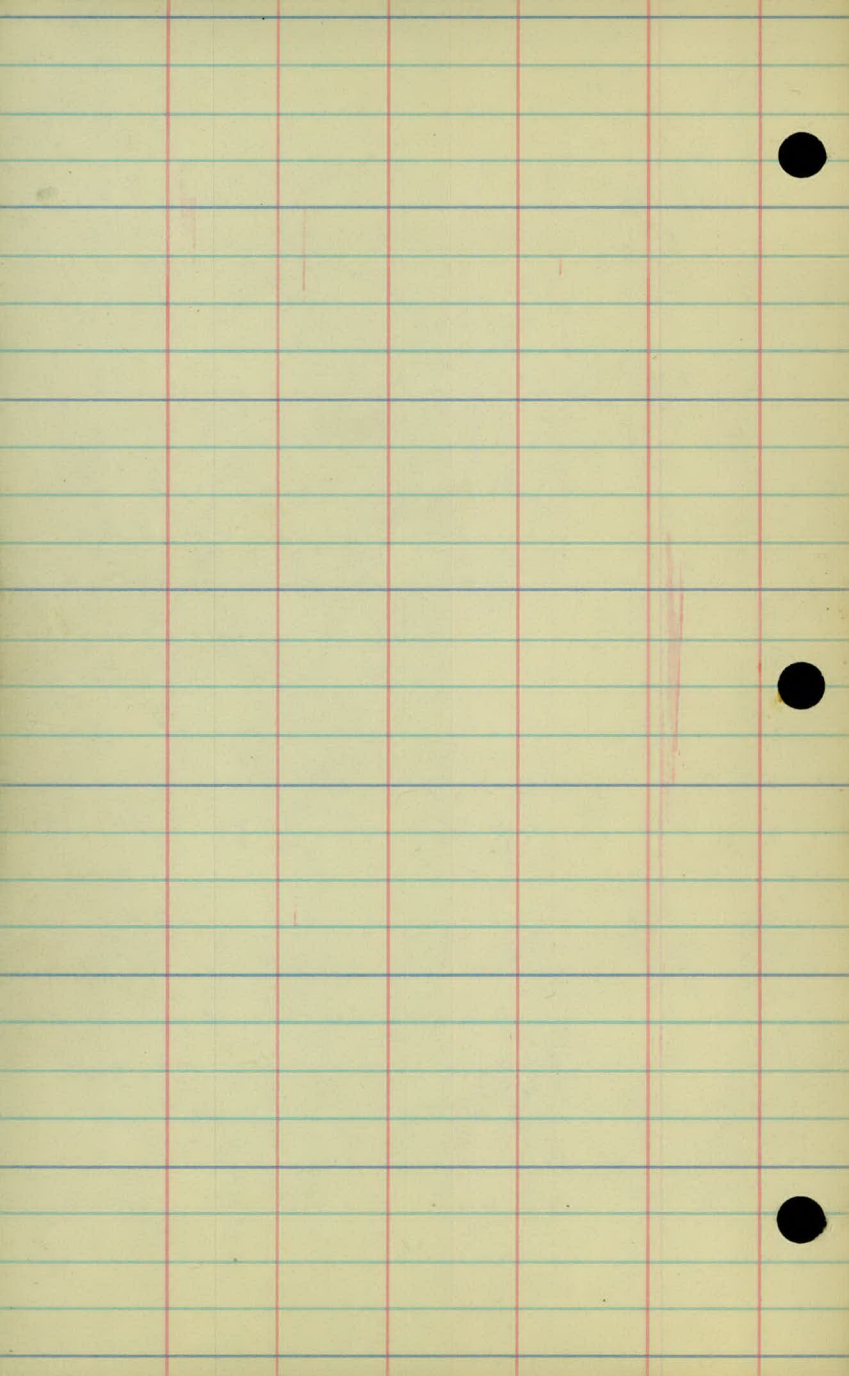
102°06'

1691.07

MC

803.60

RR Spk



6/36

H.T. Purcell

Victoria
Line Revision
at
Fabyanski's

+60.89 P.T. 21°30'

159 18°45.6

+50 16°30.6

158 14°15.6

+50 12°00.6

+33.94 P.I.

157 9°45.6

+50 7°30.6

156 5°15.6

+50 3°00.6

155 0°45.6

154+83.11 P.C.

$\Delta 43^{\circ}00L$

T 250.83

D $9^{\circ}00$

L 477.78

+50

24° 34.3

166

22° 34.3

+50

20° 34.3

+27.43 P1.

165

18° 34.3

+50

16° 34.3

165 + 27.43

164

14° 34.3

+50

12° 34.3

163

10° 34.3

+50

8° 34.3

162

6° 34.3

+50

4° 34.3

161

2° 34.3

+50

0° 34.3

160 + 35.72 PC

$\Delta 68^{\circ}56' R$

T 491.71

D $8^{\circ}00'$

L 861.67

169 + 90.08 = PC.

169 + 66.59 = PC

168 + 97.39 = PT.

34° 28'

+50

32° 34.3

168

30° 34.3

+50

28° 34.3

167

26° 34.3

TOPOG

Victoria Street
from
Owasso Blvd. North

4

$$\begin{array}{r} \text{Rd} \\ 10 - 13 \end{array}$$

$$\begin{array}{r} +64 \text{ TP} \\ 21 \end{array}$$

3

$$\begin{array}{r} \text{Rd} \\ 12 - 12 \end{array}$$

$$\begin{array}{r} +29 \text{ TP} \\ 21 \end{array}$$

2

$$\begin{array}{r} +54 \text{ Rd Sn} \\ 27 \\ +50 \text{ TP} \\ 41 \\ +61 \text{ End Colv} \\ 29 \\ +17 \text{ End Colv} \\ 10 \end{array}$$

$$\begin{array}{r} +61 \text{ Rd - Gough} \\ 22 - 31 \\ +50 \text{ Rd} \\ 32 \\ +25 \text{ Rd} \\ 0 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 75 - 46 \end{array}$$

$$\begin{array}{r} +69 \text{ Rd} \\ 15 \end{array}$$

$$\begin{array}{r} +38 \text{ Sh. Rd} \\ 65 \end{array}$$

$$\begin{array}{r} +25 \text{ F. Cor} \\ 16 \end{array}$$

$$\begin{array}{r} \text{Fee} \\ 14 \end{array}$$

$$\begin{array}{r} +69 \text{ PP} \\ 22 \end{array}$$

$$\begin{array}{r} +63 \text{ Sh. Rd} \\ 50 \end{array}$$

$$\begin{array}{r} +27 \text{ End Colv} \\ 13 \end{array}$$

$$\begin{array}{r} +71 \text{ End Colv} \\ 16 \end{array}$$

1

$$\begin{array}{r} \text{Rd} \\ 168 - 131 \end{array}$$

$$\begin{array}{r} \text{Fee} \\ 9 \end{array}$$

0

Cultivated

(Victoria) GRAVEL SURF

Cultivated

(Onasso Blvd) BLACKTOP

18' x 48 CM

12' x 44 CM

24' BLACKTOP

Mont Ctr of Sec. 2

11

$$\frac{Rd}{9-15}$$

$$\frac{+25TP}{19}$$

10

$$\frac{Rd}{9-15}$$

$$\frac{+99TP}{19}$$

9

$$\frac{Rd}{10-17}$$

$$\frac{+63TP}{20}$$

8

$$\frac{Rd}{15-13}$$

$$\frac{+28TP}{21}$$

7

$$\frac{Rd}{10-13}$$

$$\frac{+41RdSn}{19}$$

6

$$\frac{Rd}{10-13}$$

$$\frac{+91TP}{20}$$

5

$$\frac{Rd}{10-12}$$

Cultivated

Cultivated

Cultivated

Cultivated

$$\begin{array}{r} +535TP \\ 28 \\ +155TP \\ 35 \\ +67Tr \\ 34 \end{array}$$

$$\frac{Fcc}{24}$$

$$\frac{Rd}{12-9}$$

$$\frac{+93TP}{23}$$

$$\begin{array}{r} +89Tr \\ 36 \\ +39Tr \\ 34 \\ +63Tr \\ 34 \end{array}$$

$$\begin{array}{r} +965TP \\ 37 \\ +48Tr \\ 33 \\ +28Tr \\ 36 \end{array}$$

$$\frac{Fcc}{26}$$

$$36$$

$$\frac{Rd}{13-8}$$

$$\frac{+23Tr}{41}$$

$$\frac{+74Tr}{34}$$

$$\frac{Fcc}{26}$$

$$\frac{Rd}{13-9}$$

$$\frac{+52TP}{19}$$

$$\frac{+94Tr}{34}$$

$$\begin{array}{r} +60-2TP \\ 35 \\ +97-45TP \\ 38 \end{array}$$

$$\frac{+36Tr}{34}$$

$$\frac{+47Tr}{33}$$

$$\frac{+155TP}{32}$$

$$\frac{+26Tr}{33}$$

$$\frac{Fcc}{23}$$

$$\frac{Rd}{13-10}$$

$$\frac{+24TP}{19}$$

$$+39Ent$$

$$\frac{+32FCor}{21}$$

$$\begin{array}{r} +45Tr \\ 35 \\ +89Tr \\ 31 \\ +60Tr \\ 35 \end{array}$$

$$+27FieldEnt$$

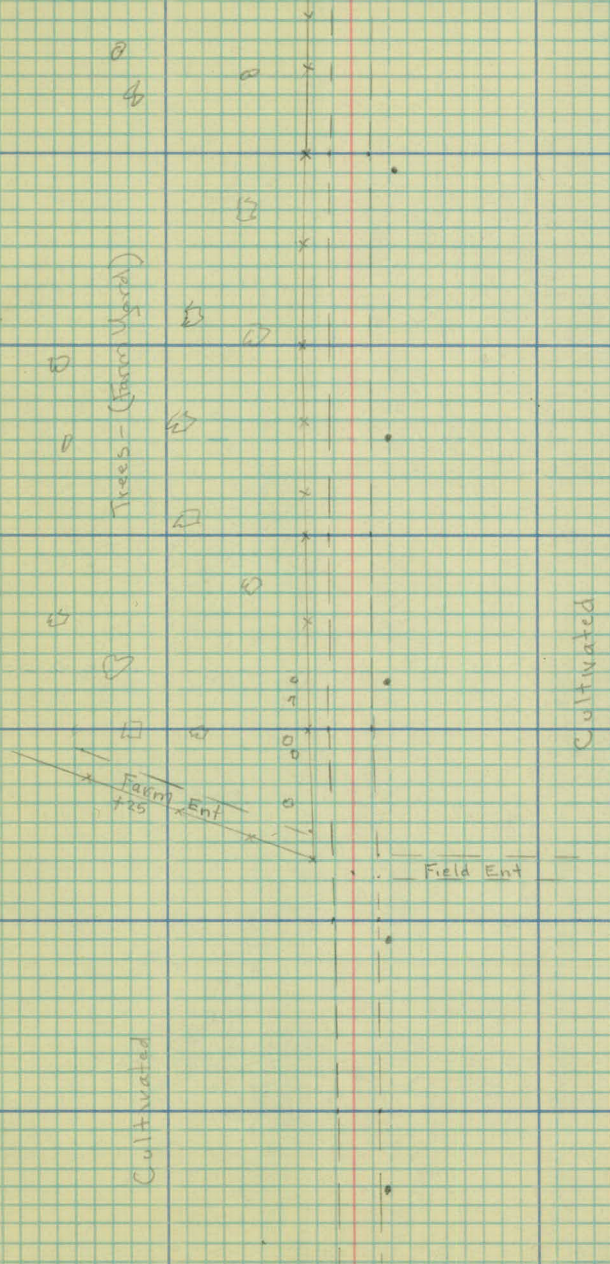
$$\frac{Rd}{11-12}$$

$$\frac{+90TP}{16}$$

$$\frac{Rd}{9-14}$$

$$\frac{+58TP}{19}$$

$$\frac{Rd}{9-14}$$



25

$$\frac{Fcc}{19}$$

$$\frac{Rd}{8-14}$$

$$\frac{+53 TP}{21}$$

24

$$\frac{Fcc}{21}$$

$$\frac{Rd}{9-15}$$

$$\frac{+28 TP}{21}$$

23

$$\frac{Fcc}{23}$$

$$\frac{Rd}{8-14}$$

$$\frac{+03 TP}{20}$$

22

$$\frac{Fcc}{22}$$

$$\frac{Rd}{7-14}$$

$$\frac{+76 T.P.}{20}$$

+45 Ent

21

$$\frac{Fcc}{24}$$

$$\frac{Rd}{7-13}$$

$$\frac{+51 TP}{20}$$

20

$$\frac{Fcc}{24}$$

$$\frac{Rd}{10-12}$$

$$\frac{+83 Tr}{37}$$

$$\frac{+45 Tr}{35}$$

$$\frac{+24 Tr}{35}$$

$$\frac{+14 FCoV}{24}$$

$$\frac{+72 Tr}{30}$$

$$\frac{+22 TP}{20}$$

19

$$\frac{Fcc}{24}$$

$$\frac{Rd}{11-12}$$

Cultivated

Trees & Stumps

Ent

5

12

10

11

13

14

15

16

17

18

19

20

21

22

23

24

25

26

27

28

29

30

31

32

33

34

35

36

37

38

39

40

41

42

43

44

$$\frac{+99 - 16 \times 40 \text{ CM}}{19 - 21}$$

32

$$\frac{\text{Rd}}{10 - 12}$$

$$\frac{+69 \text{ End orch.}}{30}$$

$$\frac{+99 \text{ TP}}{21}$$

$$\frac{+13 \text{ Beg orch. ant}}{34}$$

$$\frac{+07 - 12 \text{ Tr}}{25}$$

$$+01 \text{ Ent}$$

31

$$\frac{\text{Rd}}{9 - 13}$$

$$\frac{+75 \text{ Cor Ho}}{78}$$

$$\frac{+54 \text{ Ent} \quad +91 - 15 \text{ Tr}}{26}$$

$$\frac{+35 \text{ Ex W Fce}}{30}$$

$$\frac{+67 \text{ TP}}{21}$$

30

$$\frac{\text{Rd}}{7 - 14}$$

$$\frac{+95 \text{ 16" Tr}}{28}$$

$$\frac{+41 \text{ TP}}{21}$$

29

$$\frac{\text{Rd}}{7 - 14}$$

$$\frac{+14 \text{ TP}}{20}$$

28

$$\frac{\text{Rd}}{7 - 14}$$

27

$$\frac{\text{Rd}}{7 - 15}$$

$$\frac{+24 \text{ TP}}{21}$$

$$\frac{+42 \text{ Fc Cor}}{17}$$

26

$$\frac{\text{Fce}}{18}$$

$$\frac{\text{Rd}}{8 - 15}$$

2-5-10-15

10 10 10 10

Orchard 10

10 10 10 10

Ent

2-5-F 10
38

Ent

x x x x

Cultivated

Cultivated

x x x x
x
x

$$\begin{array}{r} +52 \text{ Pot H. TP} \\ 88 \quad 18 \end{array}$$

39

$$\begin{array}{r} \text{P.H.} \\ 150 - 15 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 15 - 10 \end{array}$$

$$\begin{array}{r} +23 \text{ TP} \\ 18 \end{array}$$

38

$$\begin{array}{r} \text{P.H.} \\ 100 - 15 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 12 - 10 \end{array}$$

+23 Field Ent

$$\begin{array}{r} +90 \text{ Pot Hole} \\ 15 \end{array}$$

$$\begin{array}{r} +54 - 12' \times 24' \text{ CM} \\ 12 - 12' \end{array}$$

$$\begin{array}{r} - \text{Pot Hole} \\ 15 - 140 \end{array}$$

$$\begin{array}{r} +30 \text{ Bag Pot Hole} \\ 15 \end{array}$$

37

$$\begin{array}{r} \text{Rd} \\ 11 - 11 \end{array}$$

$$\begin{array}{r} +17 \text{ Bag Pot Hole} \\ 15 \end{array}$$

$$\begin{array}{r} +82 \text{ TP} \\ 18 \end{array}$$

36

$$\begin{array}{r} \text{Rd} \\ 10 - 9 \end{array}$$

$$\begin{array}{r} +90 \text{ TP} \\ 12 \end{array}$$

35

$$\begin{array}{r} \text{Rd} \\ 7 - 14 \end{array}$$

$$\begin{array}{r} +58 \text{ TP} \\ 20 \end{array}$$

34

$$\begin{array}{r} \text{Rd} \\ 9 - 13 \end{array}$$

$$\begin{array}{r} +29 \text{ TP} \\ 20 \end{array}$$

33

$$\begin{array}{r} \text{Rd} \\ 10 - 12 \end{array}$$

Pot Hole

En-

Pot Hole

Cultivated

Cultivated

46

$$\frac{+48 TP}{15}$$

+50 Fc

16

$$\frac{Rd}{9-13}$$

45

$$\frac{+08 TP}{17}$$

+95 F Cor

19

$$\frac{Rd}{6-15}$$

44

$$\frac{+63 TP}{17}$$

+22 Ent (Field)

$$\frac{Rd}{5-15}$$

43

$$\frac{Rd}{7-14}$$

+95 Field Ent

42

$$\frac{+27 TP}{12}$$

$$\frac{Rd}{9-12}$$

41

$$\frac{Rd}{10-11}$$

$$\frac{+88 TP}{17}$$

$$\frac{RA}{11-11}$$

40

Cultivated

Ent

Cultivated

Cultivated

Ent

Cultivated

Woods + Brush

$$\begin{array}{r} +96TP \\ 12 \end{array}$$

$$\begin{array}{r} D+ \\ 30 \\ +88-2' Bat Ditch \\ 17 \end{array}$$

$$\begin{array}{r} +02 \quad 12' \times 30' CM \\ 14 - 16' \end{array}$$

$$\begin{array}{r} Rd \\ 9-9 \end{array}$$

$$\begin{array}{r} Fce \\ 14 \end{array}$$

53

$$\begin{array}{r} +69TP \\ 11 \end{array}$$

$$\begin{array}{r} Fce \\ 15 \end{array}$$

52

$$\begin{array}{r} +44TP \\ 11 \end{array}$$

$$\begin{array}{r} Rd \\ 10-12 \end{array} \quad \begin{array}{r} Fce \\ 16 \end{array}$$

51

$$\begin{array}{r} +19TP \\ 14 \end{array}$$

$$+90 Ent$$

$$\begin{array}{r} +16TP \\ 15 \end{array}$$

$$\begin{array}{r} Rd \\ 11-11 \end{array}$$

$$\begin{array}{r} Fce \\ 20 \end{array}$$

49

$$\begin{array}{r} Rd \\ 12-11 \end{array}$$

$$\begin{array}{r} Fce \\ 17 \end{array}$$

48

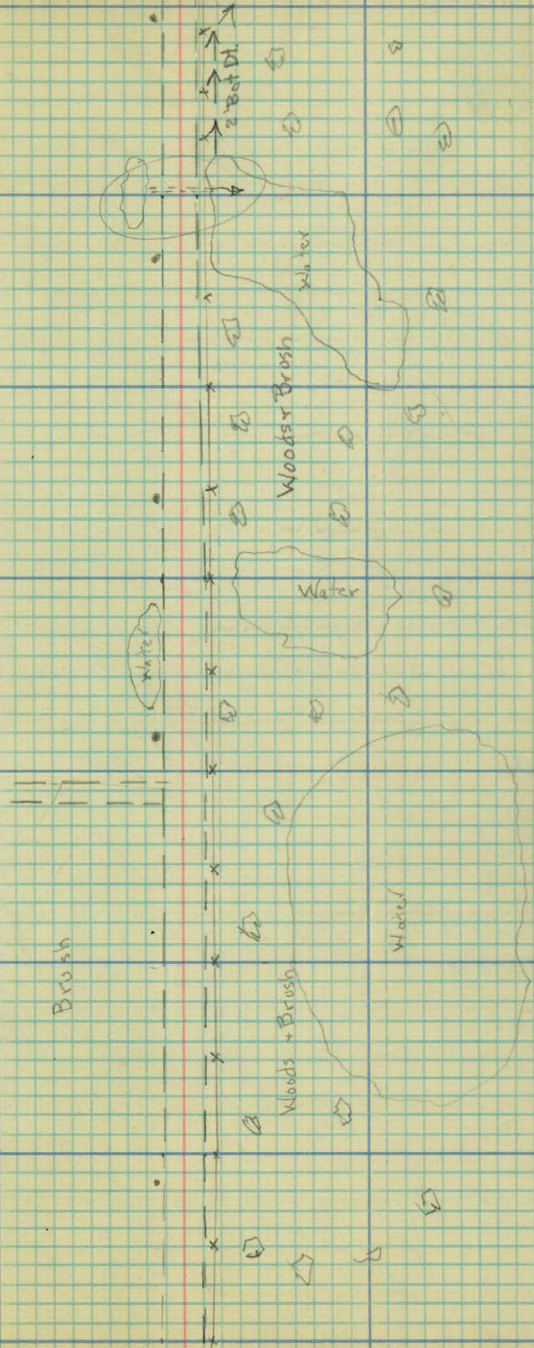
$$\begin{array}{r} +85 TP \\ 15 \end{array}$$

$$\begin{array}{r} Beg Brush \\ 25 \end{array}$$

$$\begin{array}{r} Rd \\ 12-10 \end{array}$$

$$\begin{array}{r} Fce \\ 14 \end{array}$$

47



60

$$\frac{Fcc}{22}$$

$$\frac{Rd}{19-8}$$

$$\frac{+50 TP}{22}$$

$$\frac{Water Hole}{22-25d}$$

59

$$\frac{Fcc}{23}$$

$$\frac{+21 TP}{17}$$

$$\frac{Water Hole}{62}$$

58

$$\frac{+18 TP}{14}$$

$$\frac{+55 Rd}{13-6}$$

$$\begin{aligned} &\frac{+37 Shoulder}{35} \\ &\frac{+15 Shoulder}{40} \end{aligned}$$

$$\begin{aligned} &\frac{+16 Fc. +89 \checkmark}{23} \quad \frac{+90 Rd}{12-10} \quad \frac{+93 Fc. +89}{13} \end{aligned}$$

57

$$\frac{Rd}{11-9}$$

$$\frac{Fcc}{13}$$

$$\frac{+91 TP}{14}$$

$$\frac{+82-18" X 30 CM (New)}{16-14}$$

56

$$\frac{+49 TP}{13}$$

55

$$\frac{Rd}{9-11}$$

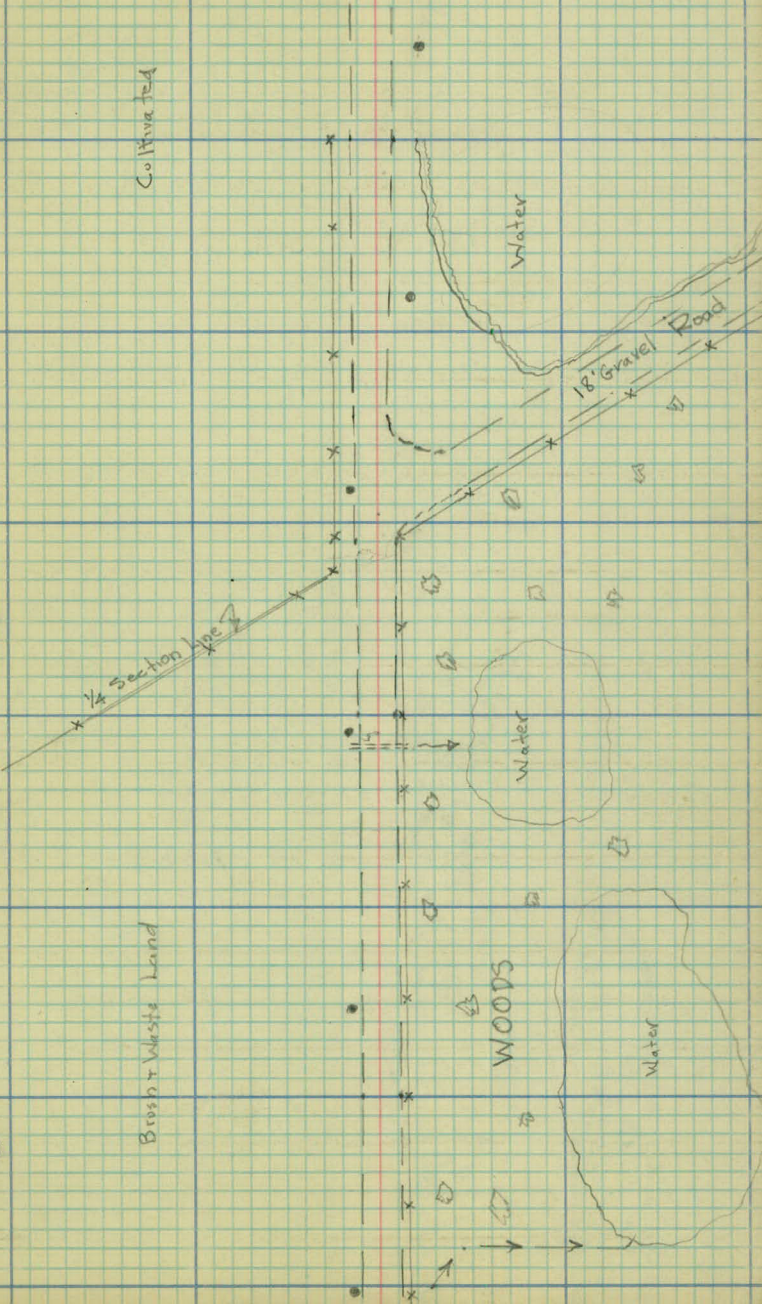
$$\frac{Fcc}{15}$$

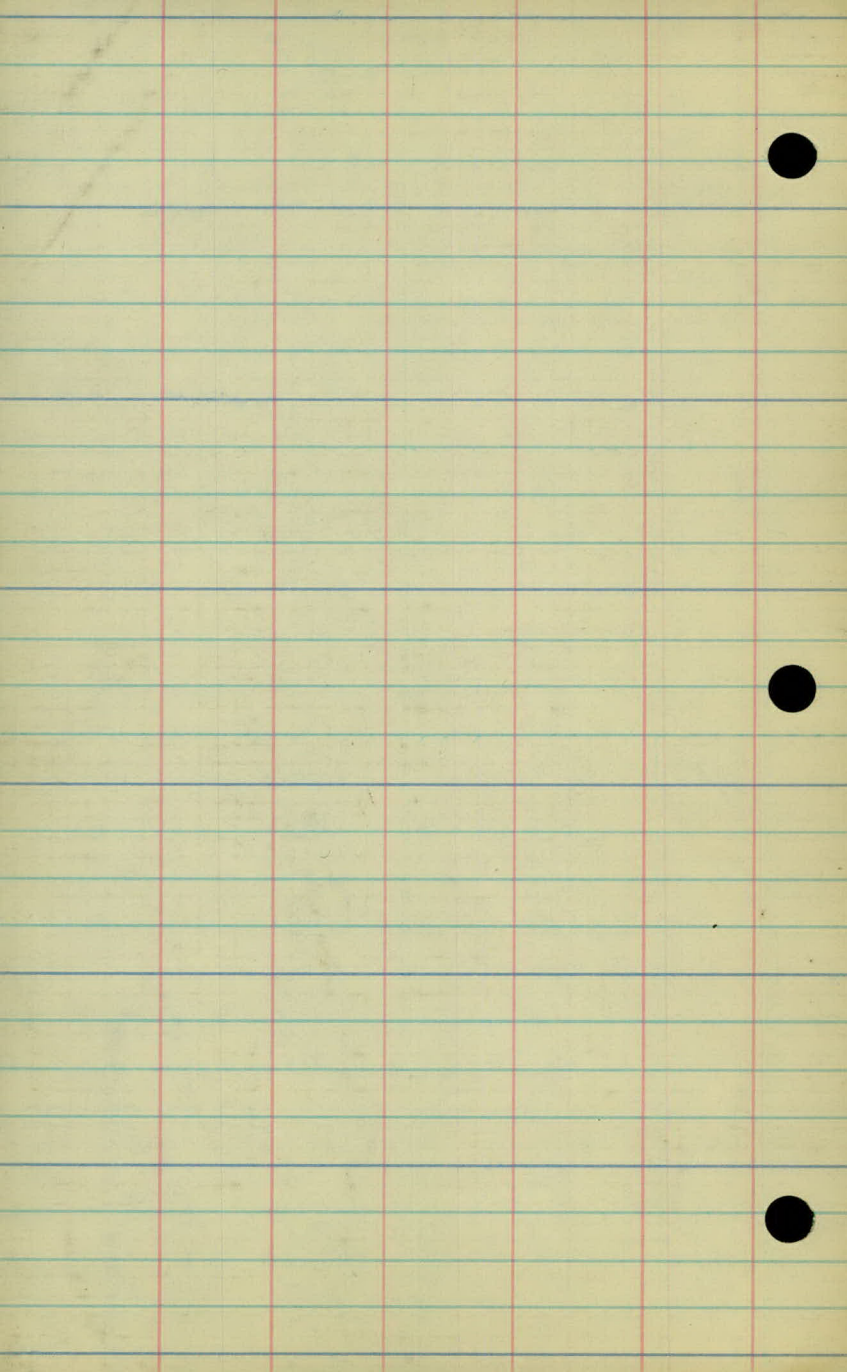
54

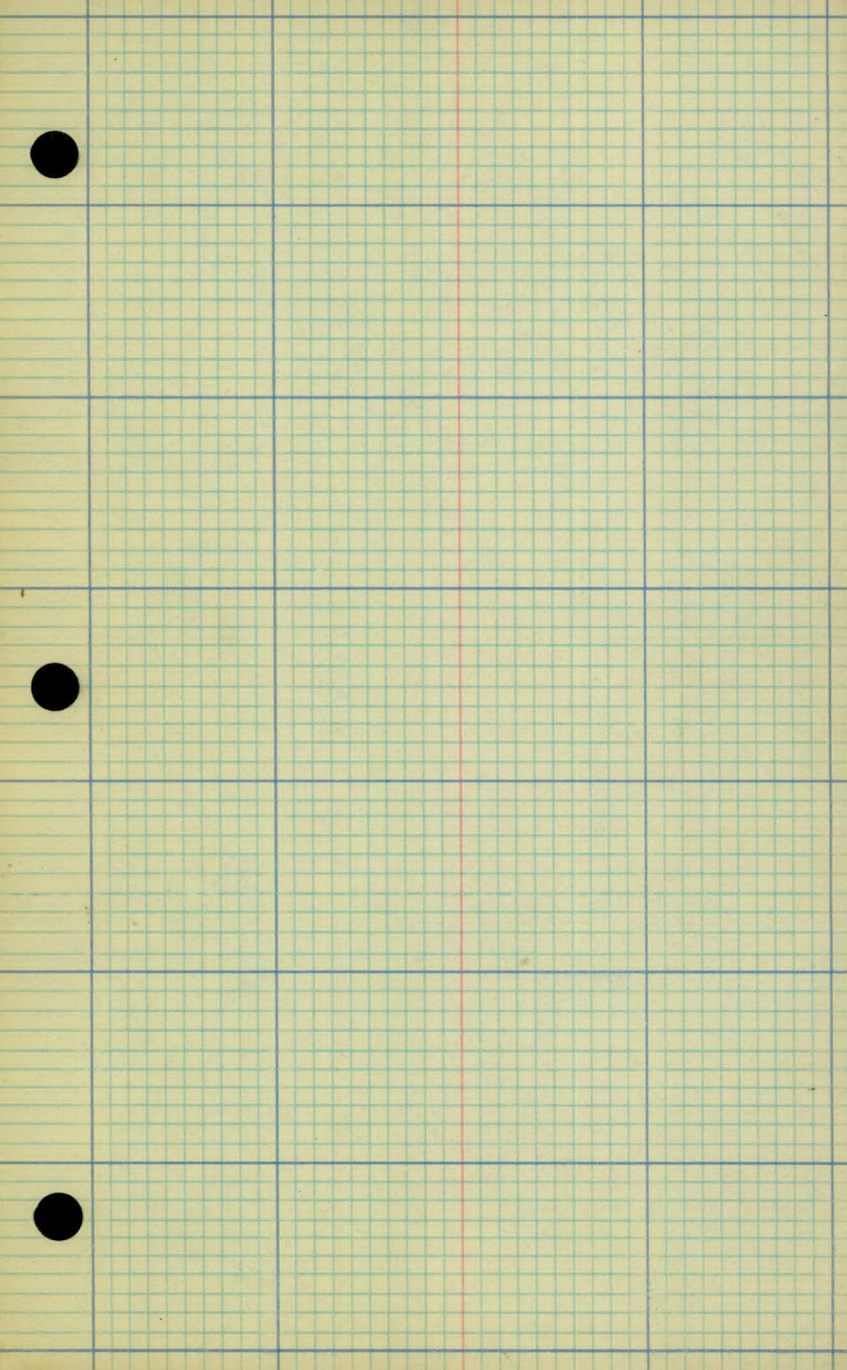
$$\frac{+20-2' Root D.t}{45}$$

Cultivated

Brush & Waste Land







66

$$\frac{Fc}{20}$$

$$\frac{Rd}{11-12}$$

$$\frac{+54TP}{32}$$

65

$$\frac{Fc}{20}$$

$$\frac{Rd}{9-12}$$

$$\frac{+21TP}{33}$$

64

$$\frac{Fcc}{22}$$

$$\frac{Rd}{12-11}$$

$$\frac{+97TP}{28}$$

63

$$\frac{Fc}{19}$$

$$\frac{Rd}{11-13}$$

$$\frac{+82TP}{31}$$

62

$$\frac{Fc}{18}$$

$$\frac{Rd}{11-11}$$

$$\frac{+90-12" \times 27CM}{11-16}$$

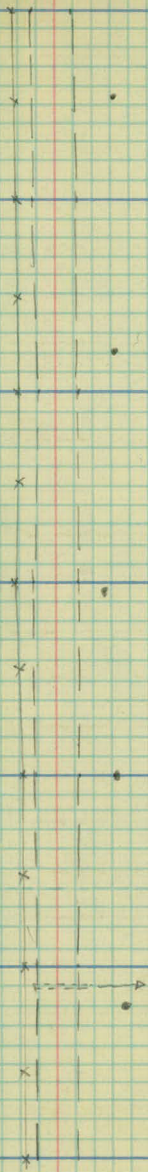
$$\frac{+80TP (New)}{37}$$

61

$$\frac{Fcc}{17}$$

Cult.

Meadow



F.c
27

$$\begin{array}{r} +89TP \\ \hline 29 \\ +81FC \\ \hline 30 \end{array} \quad \begin{array}{r} +70 \\ +88-4Tr5 \\ \hline 48 \end{array}$$
$$\begin{array}{r} +09TP \\ \hline 29 \end{array}$$

73

72

$$\begin{array}{r} Rd \\ 12-11 \end{array}$$

$$\begin{array}{r} +88TP \\ \hline 16 \end{array}$$

71

$$\begin{array}{r} Rd \\ 10-10 \end{array}$$

$$\begin{array}{r} +56TP \\ \hline 19 \end{array}$$

70

$$\begin{array}{r} Rd \\ 13-9 \end{array}$$

$$\begin{array}{r} +28TP \\ \hline 19 \end{array}$$

$$\begin{array}{r} +22Pa+Hb \\ \hline 19-70 \end{array}$$

69

$$\begin{array}{r} +45EndFce \\ \hline 23 \end{array}$$

$$\begin{array}{r} +68Pa+Hb \\ \hline 18-68 \end{array}$$

68

$$\begin{array}{r} Rd \\ 14-8 \end{array}$$

$$\begin{array}{r} +70TP \text{ (old)} \\ \hline 19 \end{array}$$

$$\begin{array}{r} +65-12 \times 30 \\ \hline 16-14 \end{array}$$

67

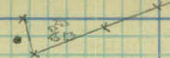
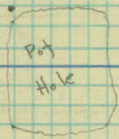
$$\begin{array}{r} Fc \\ 22 \end{array}$$

$$\begin{array}{r} Rd \\ 13-9 \end{array}$$

Cult

Meadow

Pot
Hole



$$\frac{+58 \text{ EC.}}{15}$$

$$+56 \text{ Fec Xs}$$

$$\frac{+30 \text{ Sch. Ent } 12 \times 26 \text{ CM}}{46}$$

$$+58 \text{ PP G.P.}$$

$$17 \quad 56$$

$$\frac{RA}{42 - 21}$$

$$\frac{Fec}{14}$$

$$+45 \text{ Ent}$$

$$40$$

$$\frac{+22 \text{ StP}}{1}$$

$$\text{End Tr Row}$$

$$56$$

$$+32 \text{ TA PP}$$

$$11$$

$$+01 \text{ StP}$$

$$2$$

$$\frac{Rd}{11 - 17}$$

$$\frac{Fec}{6}$$

$$+49 \text{ StP}$$

$$19$$

$$+40 \quad 2 \text{ StPs}$$

$$\frac{+02 \text{ StP}}{27}$$

$$+55 \text{ StP}$$

$$9$$

$$\frac{+62 \text{ StP}}{27}$$

$$+96 \text{ StP}$$

$$+58 \text{ StP - StP}$$

$$5$$

$$+45 \text{ StP}$$

$$12$$

$$+125 \text{ StP}$$

$$50$$

$$\frac{+02 \text{ StP}}{5}$$

$$+80 \text{ StP}$$

$$17$$

$$+49 \quad 5 \text{ StP}$$

$$5$$

$$+21 \quad 2 \text{ TVs}$$

$$5$$

$$+06 \text{ Tr}$$

$$12$$

$$+13 \text{ TP}$$

$$1$$

$$\frac{Tr}{55}$$

$$\frac{Rd \quad Fc}{37 - 14 - 6}$$

$$+87 \text{ Ent - Tr } 12 \times 24 \text{ CM}$$

$$+26 \text{ Tr}$$

$$46$$

$$+23 \quad 12 \times 36 \text{ CM}$$

$$38 - 2$$

$$\frac{+78 \text{ Tr}}{1}$$

$$\frac{+82 \text{ Tr} - \text{Tr} \cdot \text{StP}}{4 \quad 17 \quad 33}$$

$$\frac{Rd}{30 - 9}$$

$$\frac{Fec Xs}{0}$$

$$+70 \text{ Ent}$$

$$+62 \text{ TP}$$

$$1$$

$$\frac{Rd}{23 - 1}$$

$$\frac{Fec}{3}$$

$$\frac{+80 \text{ RA}}{22 - 0}$$

$$\frac{+20 \text{ TP}}{10}$$

$$\frac{RA}{17 - 6}$$

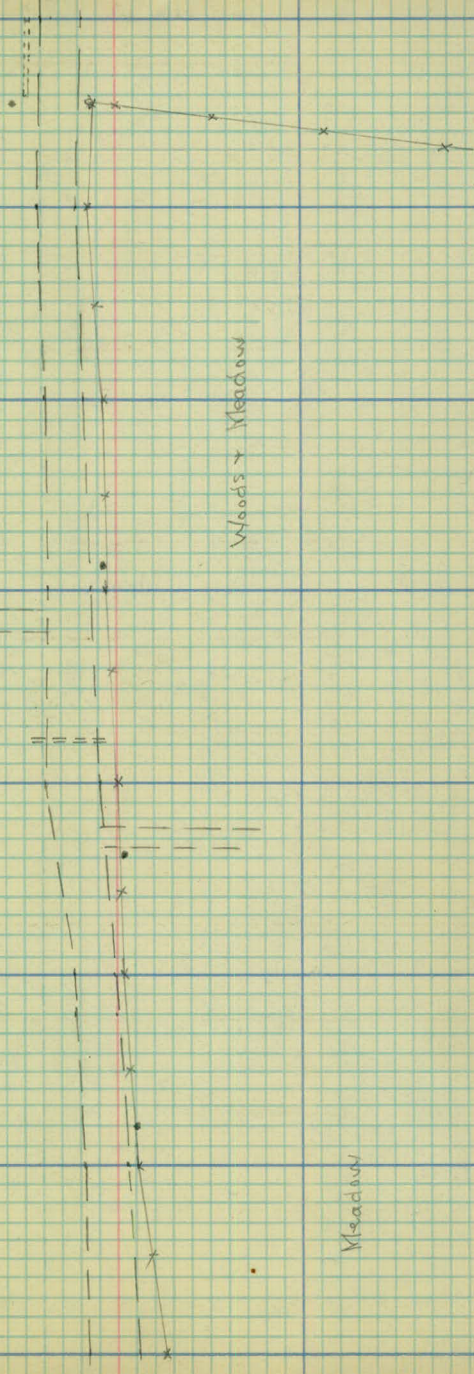
$$\frac{Fec}{12}$$

$$\frac{RA}{15 - 12}$$

Farm Yard

Woods & Meadow

Meadow



+176.5 + WBM. 2 +92 18'x34' CM in NRR.Dt.
+61.5 EBM

+12 End RREn
+05 Guy P.
+02 Sh
42

+46 WigWag
+50 Rd
11-9
+2+RP
19

BatWell
18.4
+09 PP
23

87

+87 E. +94
+10 Tr. Tr
+18 End Tr
14

+80 Rd Sh.
+65 Rd
17-6

+98 Dead E Sn
+84 Ent. 15

86

+74 PP
+04 - 12'x30 CM
23-7
Trs
33

85

+94 Beg Row Trs
+33 - 4' Cor. Steps
+28 Cor Ho
+01 Tr

+43 PP
+05 Ent.

84

+83 End Row Trs
+71 Ent
+44 Cor Bar
Beg Row Trs

+50 Rd
21-0
Rd
23-2

+26 RR Sn
+15 PP
14

83

+52 Sudo Rd Sn

82

29-7 Rd

+33 SE Cor School 47'x25'
+26 PP
11

81

169.39

136

50

355.39

30564

304.28

136

35505

355

860

M.S. 61 98.10.

61 77 30.

20,80.

2 31 17 65

End Bridge 25 197.65

PC = 253 + 16.90

T = 208.91

1478037

x x x x

Co Rd "E" (Gravel)

00

.

9

Ent

30

0

20
20

0

Ent

Ent

12

9

0

9

0

47'
25
Dist Sch
#28

90

$$\begin{array}{r} +12 \text{ TV} \\ \hline 19 \end{array}$$

+11 Ent

89

$$\begin{array}{r} +99 \text{ Tr} \\ \hline 18 \\ +85 \text{ Tr Beg Yard} \\ \hline 19 \\ +79 \text{ Tr} \\ \hline 36 \end{array}$$

+85 Beg Yard

$$\begin{array}{r} +35 \text{ PP} \\ \hline 24 \end{array}$$

$$\begin{array}{r} +85 \text{ RA} \\ \hline 7-14 \end{array} \quad \begin{array}{r} +55 \text{ 4" E" } \text{RA} \\ \hline 50 \end{array}$$

+42 Dead End So

+35 Shoulder

$$\begin{array}{r} +62 \text{ Sh} \\ \hline 43 \end{array}$$

$$\begin{array}{r} +11 \text{ King So} \\ \hline 12 \\ +06 \text{ GPs} \\ \hline 17 \end{array}$$

$$\begin{array}{r} +07 \text{ PP} \\ \hline 26 \end{array}$$

RA

$$\begin{array}{r} +21 \text{ St So} \\ \hline 27 \end{array}$$

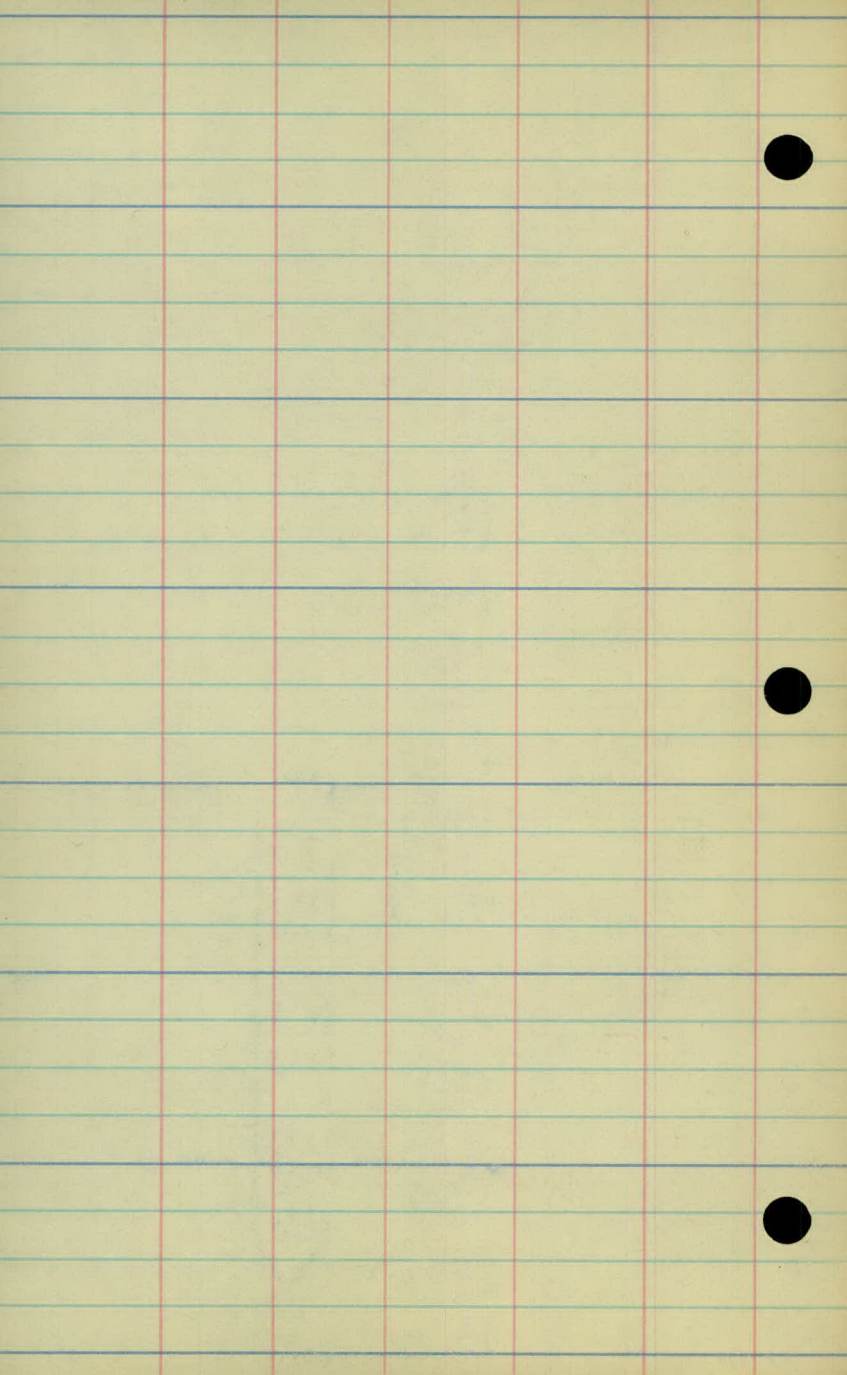
88

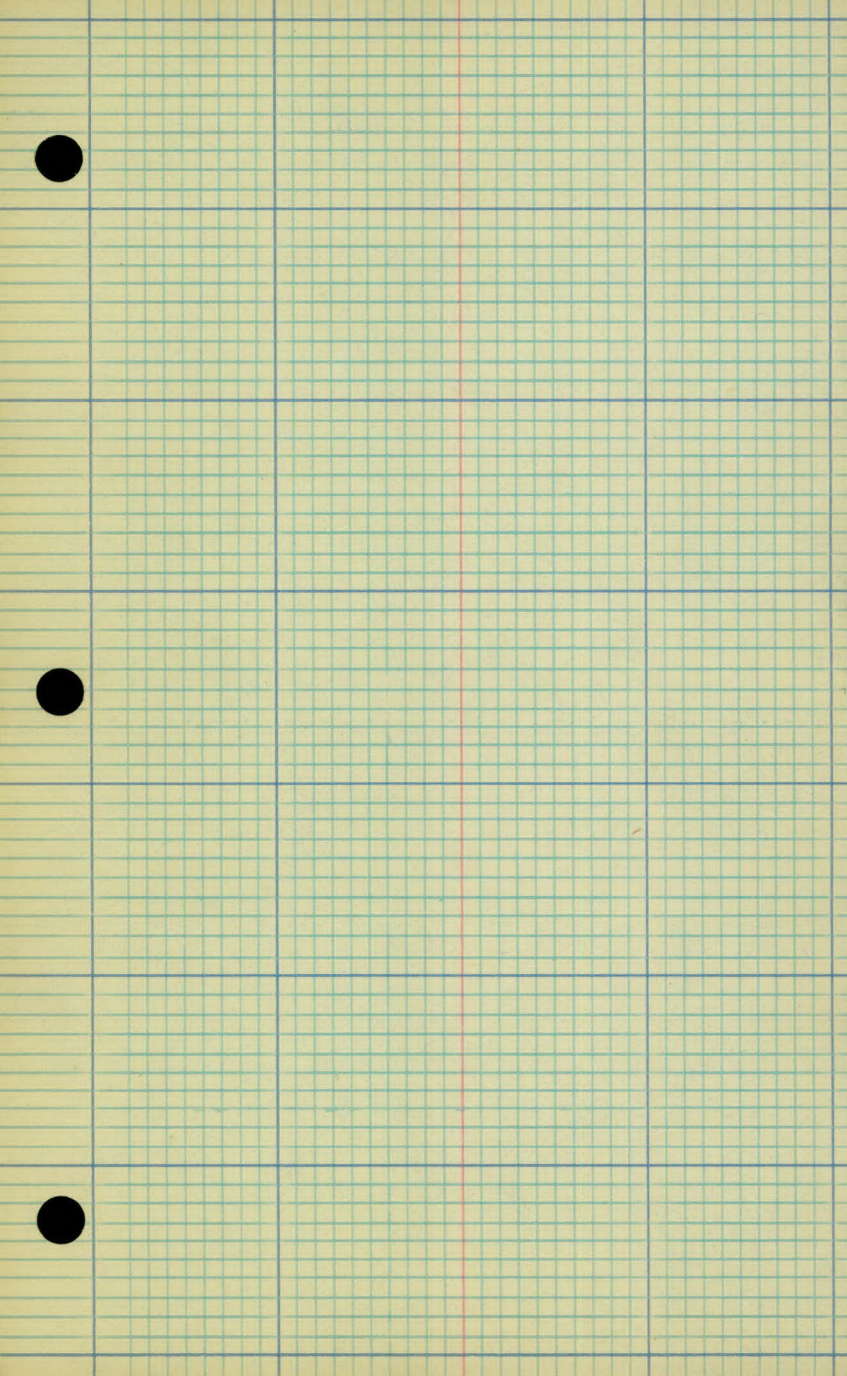
7-12

Cult.

Cult.

Co. Rd "E"





96

$$\frac{Fc}{16}$$

$$\frac{Rd}{10-10}$$

$$\frac{+49 PP}{28}$$

95

$$\frac{+66 PP}{28}$$

94

$$\begin{array}{r} +4Tr \\ 44 \\ +09 FccCo +11 \\ 15 \end{array}$$

$$\frac{Fcc}{15}$$

$$\frac{RM}{9-10}$$

$$+98 Ent$$

$$\begin{array}{r} +19 Tr \\ 44 \\ +19 Tr \\ 22 \\ +18 R5n \\ 14 \end{array}$$

$$\begin{array}{r} +66 PP \\ 18 \\ +44 Tr \\ 24 \end{array}$$

$$\frac{+66 PP}{27}$$

$$+40 Ent$$

93

$$\begin{array}{r} +52 Tr \\ 18 \\ +15 Ent \\ 19 \end{array}$$

$$\frac{+47 FC}{17}$$

$$\frac{+21 PP}{25}$$

92

$$\frac{Tr}{43}$$

$$43$$

$$\begin{array}{r} +40 Trs \\ 19-40-54 \\ +26 Tr2 \\ 19-40-54 \\ +19 S4 \\ 19 \\ +44 RR5n \\ 15 \end{array}$$

$$\begin{array}{r} +46 Tr \\ 19 \\ +57 Tr^{30} \\ 19 \end{array}$$

$$\begin{array}{r} +80 MB \\ 11 \\ 98 \\ 23 \end{array}$$

91

$$\frac{Rd}{11-9}$$

$$\begin{array}{r} +98 S4p \\ 19 \\ +24 Tr \\ 38 \\ +57 Tr \\ 37 \end{array}$$

$$\frac{+80 Cor Ho}{150}$$

$$\frac{+61 Cor Ho}{68}$$

90

Pasture

Barn Yard

Cult

Cult

37
254
Fr

29

1st Stages

25

37

$$\frac{+96 \text{ 10' } \times 26 \text{ Vit}}{13 - 13}$$

$$\frac{+90 \text{ PP}}{27}$$

103

$$\frac{+41 \text{ PP}}{28}$$

102

$$\frac{Fc}{14}$$

$$\frac{Rd}{8 - 12}$$

$$\frac{+90 \text{ 8' } \times 28' \text{ CM and Vit}}{10 - 18}$$

101

$$\frac{+91 \text{ PP}}{27}$$

100

$$\frac{Fc}{15}$$

$$\frac{Rd}{8 - 12}$$

$$\frac{+41 \text{ PP}}{27}$$

99

$$\frac{Fc}{16}$$

$$\frac{Rd}{10 - 10}$$

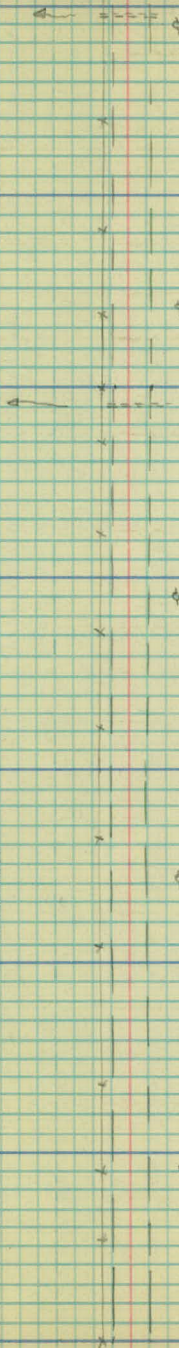
98

$$\frac{+90 \text{ PP}}{27}$$

97

Meadow

Cult.



+98 Ent

$$\frac{+39 \text{ FC} +29}{20}$$

$$\frac{+44.12 \times 48 \text{ CM}}{21}$$

$$\frac{+20 \quad 21 \quad 17 \quad +30}{20}$$

110

$$\frac{+89 \text{ PP}}{26}$$

$$\frac{+33 \text{ FL}}{19}$$

109

$$\frac{\text{Fc}}{16}$$

$$\frac{\text{Rd}}{9 \quad 13}$$

108

$$\frac{+40 \text{ PP}}{26}$$

107

$$\frac{\text{Fc}}{16}$$

$$\frac{\text{Rd}}{9 \quad 13}$$

106

$$\frac{+90 \text{ PP}}{27}$$

105

$$\frac{\text{Fc}}{14}$$

$$\frac{\text{Rd}}{8 \quad 13}$$

104

$$\frac{+40 \text{ PP}}{27}$$

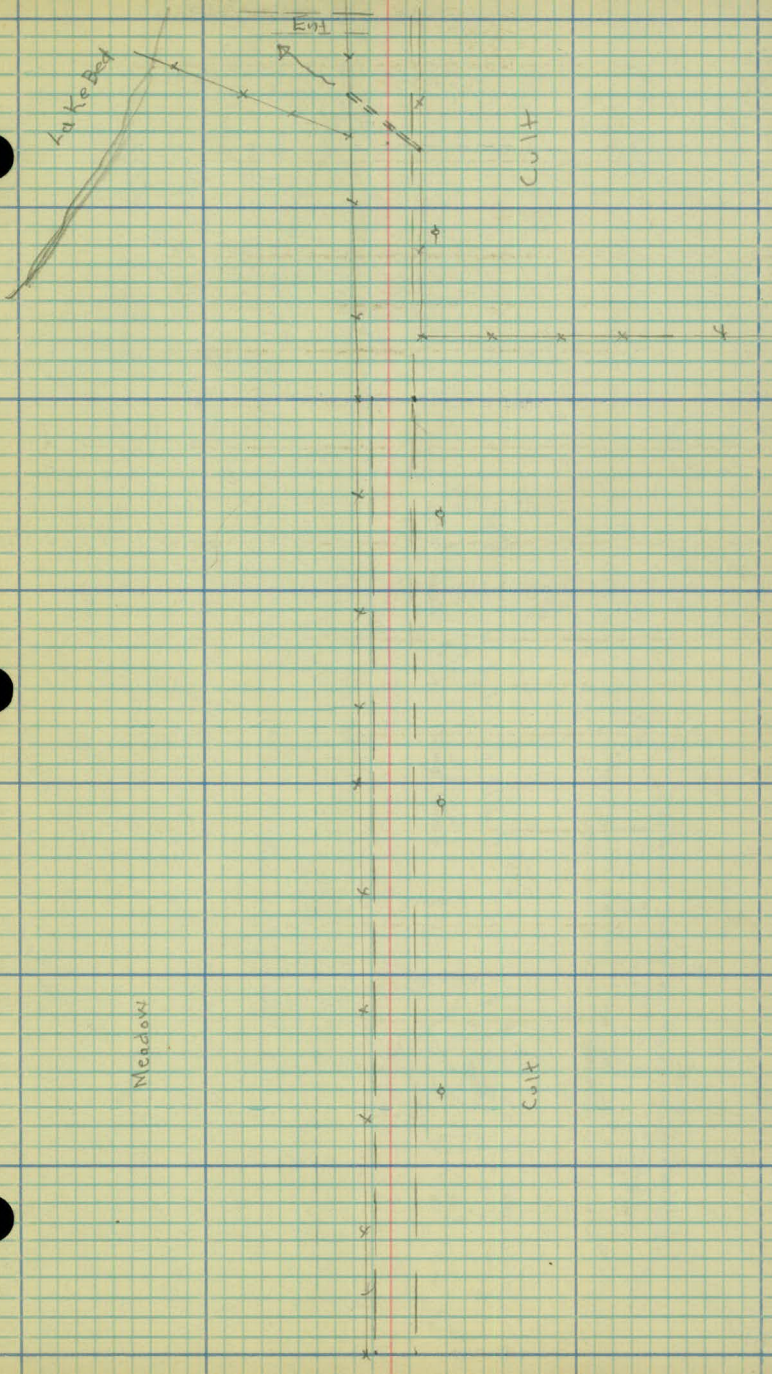
Lake Bed

E 191

Cult

Meadow

Cult



117

116

$$\frac{+69 \text{ PP}}{27}$$

115

$$\frac{Fc}{15}$$

$$\frac{Rd}{11-9}$$

114

$$\frac{+31 \text{ FC} +33}{18}$$

$$\frac{+36 \text{ FC} +33}{16}$$

$$\frac{+35 \text{ PP}}{26}$$

113

$$\frac{Fc}{22}$$

$$\frac{Rd}{15-6}$$

$$\frac{Fc}{11}$$

$$\frac{+65 \text{ PP}}{24}$$

112

$$\frac{+38 \text{ PP}}{22}$$

111

$$\frac{Fc}{20}$$

$$\frac{Rd}{11-9}$$

$$\frac{Fc}{16}$$

Old Lake Bed

Cult

Meadow

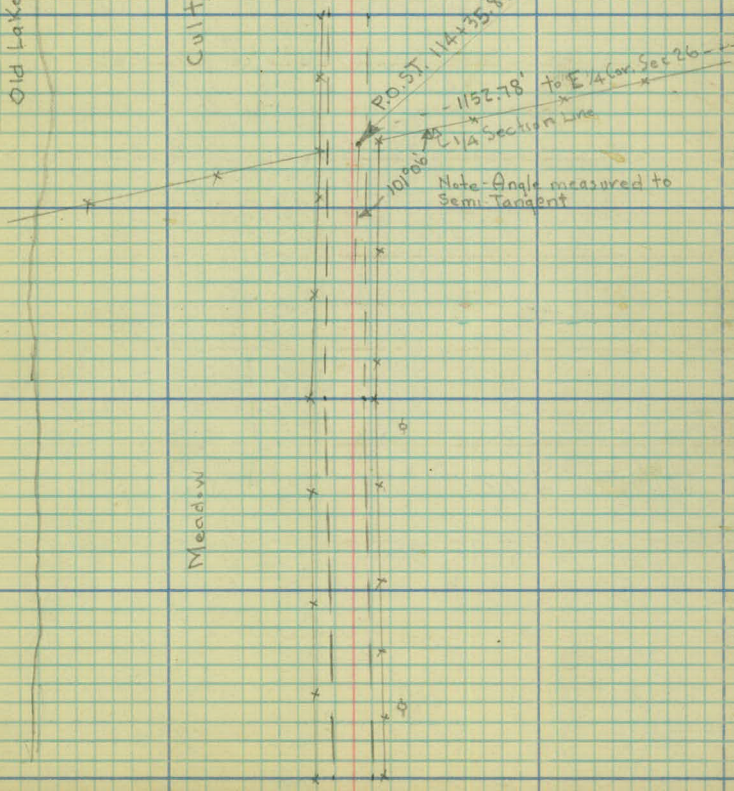
P.O. ST. 114+35.87

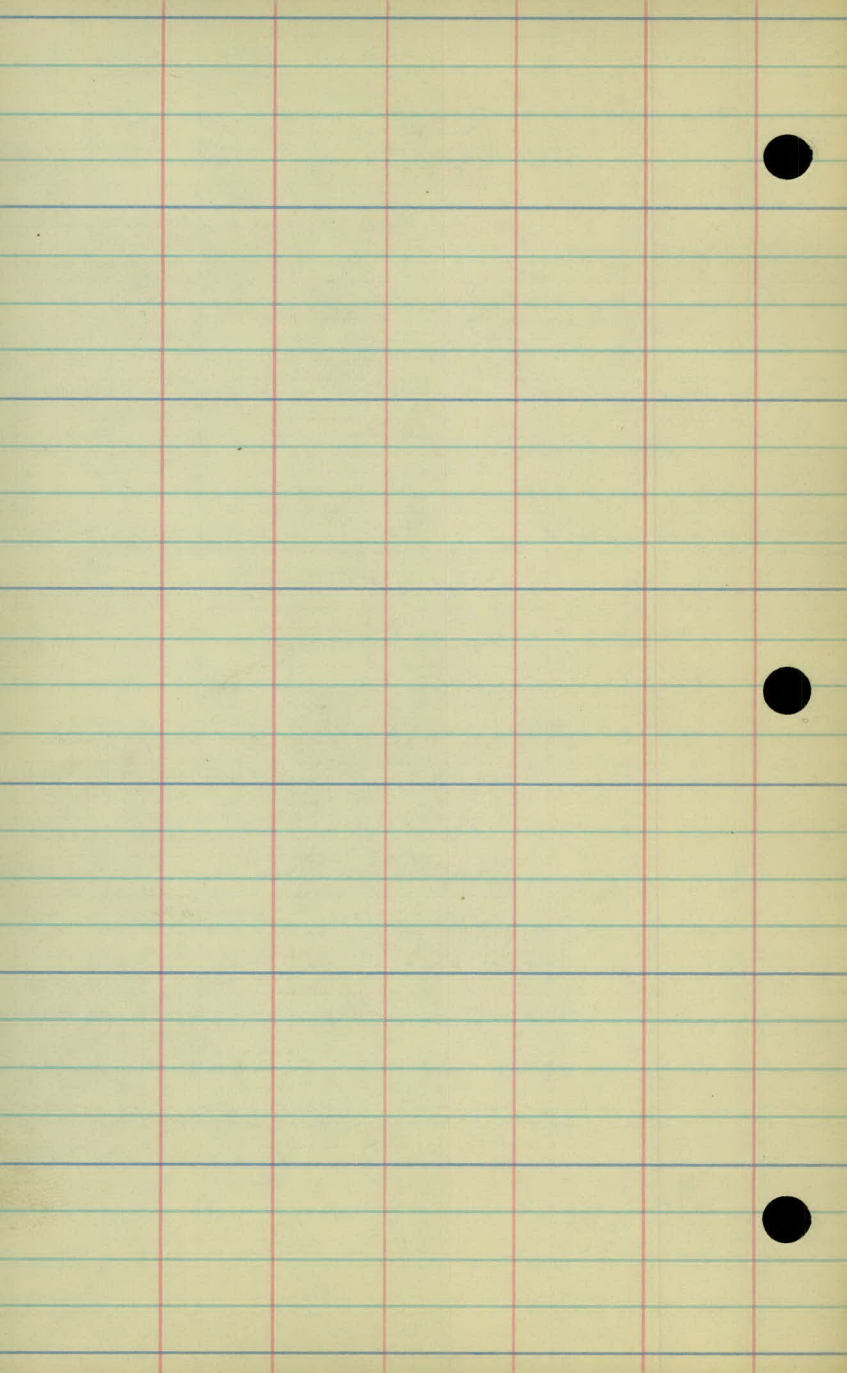
-1152.78' to E 4 for Sec 26

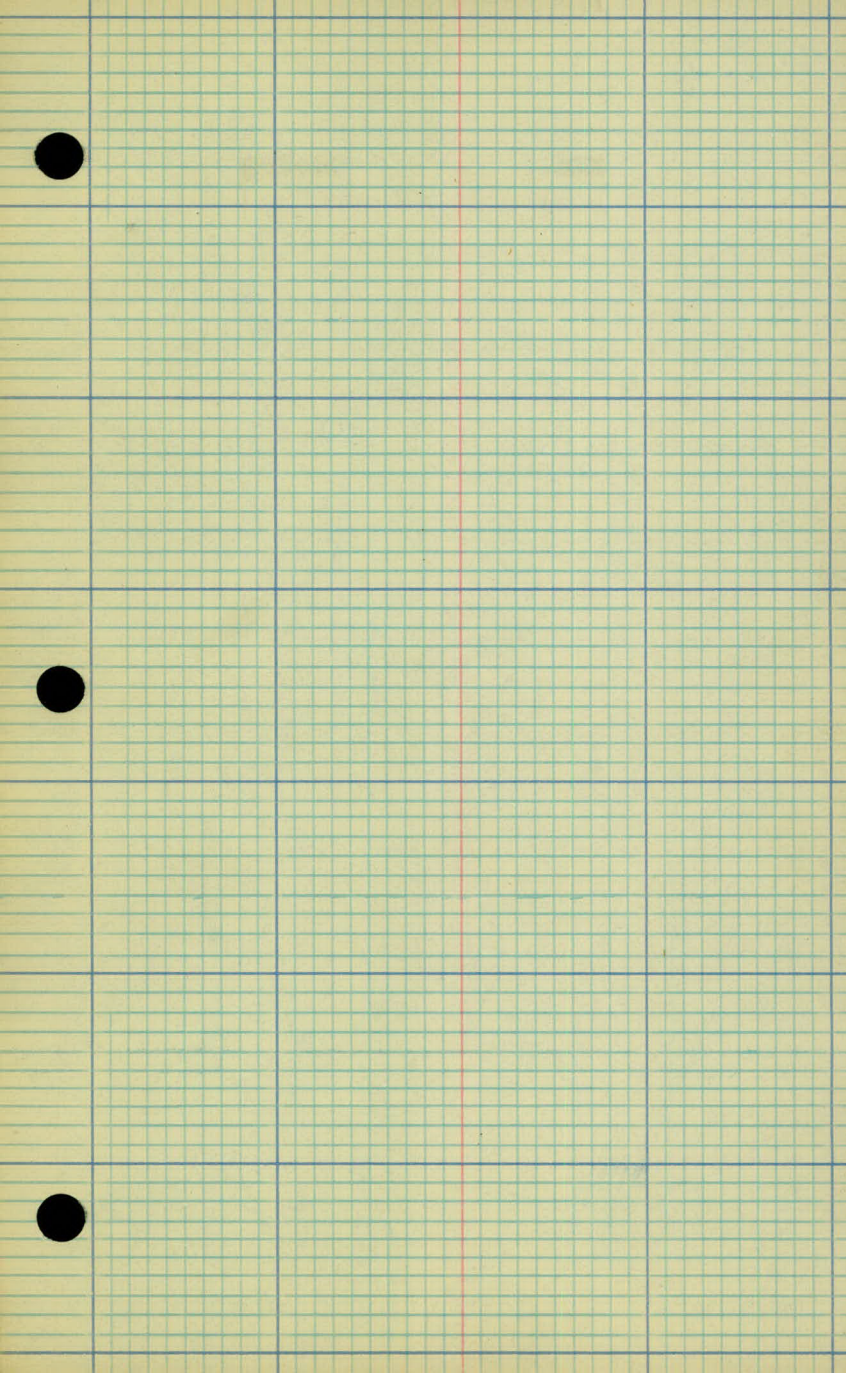
LIA Section Line

101°06'

Note - Angle measured to Semi-Tangent







120

$$\frac{+46 \text{ Bay orch.}}{28}$$

$$\frac{+04 \text{ End orch.}}{24}$$

$$\frac{Rd}{11-11}$$

$$\frac{+80 PP}{21}$$

$$\frac{+10 FC}{19}$$

$$\frac{+52 \text{ E.G. Tr}}{19} \quad \frac{+59 \text{ Bay Orchard}}{24}$$

$$\frac{+40 \text{ Ent } 12 \times 20' \text{ CM}}{14}$$

$$\frac{+25 \text{ Ev Gr Tr}}{19}$$

$$+50 PP$$

$$\frac{22}{+40 \text{ Ent}}$$

119

$$\frac{+02 \text{ Tr}}{18}$$

$$+93 \text{ Cor Hb}$$

$$\frac{+59 \text{ Lilac}}{17}$$

$$\frac{+19 \text{ Tr}}{19}$$

$$\frac{+49 \text{ PP}}{50}$$

$$+49 \cdot 12' \times 26' \text{ CM}$$

$$13-13$$

$$\frac{+610 \text{ cor David}}{106}$$

$$\frac{+46 \text{ FC}}{14}$$

$$\frac{+42 \text{ PP}}{29}$$

$$\frac{+19 \text{ Tr}}{16}$$

118

117

$$\frac{Fc}{15}$$

$$\frac{Rd}{11-11}$$

$$\frac{+05 \text{ PP}}{24}$$

116

$$\frac{Lake}{200}$$

$$\frac{Fc}{16}$$

$$\frac{Rd}{11-8}$$

$$\frac{+69 \text{ PP}}{26}$$

115

Lake

Cult.

40'
1 1/2
5
Fv

Yard

Garden

1110
Orchard

Ent

Ent

Cult.

46
Barn

Cult.

+63 1/4 1/4 line Xs

$$\begin{array}{r} +51 \text{ End Orch} \\ \hline 27 \end{array}$$

$$\begin{array}{r} R_d \\ 10 - 12 \end{array}$$

$$\begin{array}{r} +54 PP \\ \hline 26 \end{array}$$

127

$$\begin{array}{r} +25 PP \\ \hline 24 \end{array}$$

126

$$\begin{array}{r} R_d \\ 10 - 12 \end{array}$$

125

$$\begin{array}{r} +94 PP \\ \hline 22 \end{array}$$

124

$$\begin{array}{r} R_d \\ 13 - 9 \end{array}$$

$$\begin{array}{r} +62 PP \\ \hline 26 \end{array}$$

$$\begin{array}{r} +77 \text{ End orch} \\ \hline 44 \end{array}$$

$$\begin{array}{r} +12 \text{ Beg Orch} \\ \hline 46 \end{array}$$

123

$$\begin{array}{r} R_d \\ 14 - 8 \end{array}$$

$$\begin{array}{r} +48 Tr \\ 31 \end{array} \quad \begin{array}{r} +88 Tr \\ 29 \end{array} \quad \begin{array}{r} +84 Tr \\ 15 \end{array} \quad \begin{array}{r} +90 Tr \\ 21 \end{array} \quad \begin{array}{r} +76 Tr \\ 16 \end{array} \quad \begin{array}{r} +67 Tr \\ 29 \end{array}$$

$$\begin{array}{r} +70 \text{ Beg Orch} \\ \hline 40 \end{array}$$

$$\begin{array}{r} +20 \text{ Ent 12'x32'VP} \\ \hline 15 \end{array}$$

$$\begin{array}{r} +18 \text{ Cor Ho} \\ \hline 175 \end{array}$$

122

$$\begin{array}{r} R_d \\ 13 - 8 \end{array}$$

$$\begin{array}{r} +32 PP \\ \hline 21 \end{array}$$

$$\begin{array}{r} +63 Tr \\ \hline 24 \end{array}$$

$$\begin{array}{r} +20 \text{ Ent 12'x3'} \\ \hline 9 \end{array}$$

$$\begin{array}{r} +64 \text{ End Fe} \\ \hline 17 \end{array}$$

$$\begin{array}{r} +56 25 Tr \\ \hline 18 \end{array}$$

$$\begin{array}{r} +55 \text{ End Orchs Gar} \\ \hline 21 \end{array}$$

$$\begin{array}{r} +09 FC. +12 \\ \hline 19 \end{array}$$

121

Brush $\frac{1}{4}$ $\frac{1}{4}$ Line

ORCHARD

2017.

40

25F

28.

25. F

49

0.25 1.00 1.25 1.50 1.75 2.00 2.25 2.50 2.75 3.00 3.25 3.50 3.75 4.00 4.25 4.50 4.75 5.00 5.25 5.50 5.75 6.00 6.25 6.50 6.75 7.00 7.25 7.50 7.75 8.00 8.25 8.50 8.75 9.00 9.25 9.50 9.75 10.00

22

1

10

$$\begin{array}{r} +97 \text{ 1.5' Walk} \\ \hline 32 \end{array}$$

$$\begin{array}{r} +75 \text{ Ent} \\ \hline 51 \end{array}$$

$$\begin{array}{r} +13 \text{ Dog Row Maples} \\ \hline 48' \end{array}$$

$$\begin{array}{r} 33-10 \text{ Rd} \\ \hline \end{array}$$

$$\begin{array}{r} +0.1 \text{ PP} \\ \hline 7 \end{array}$$

$$\begin{array}{r} \text{Fc} \\ \hline 11 \end{array}$$

$$+99 \text{ Ent}$$

$$\begin{array}{r} +91 \text{ Tr} \\ \hline 48' \end{array}$$

$$+90 \text{ Field Ent}$$

$$\begin{array}{r} +0.5 \text{ P} \\ \hline 0 \end{array}$$

$$\begin{array}{r} +39.5 \text{ P} \\ \hline 9 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 37-17 \end{array}$$

$$\begin{array}{r} \text{Fc} \\ \hline 11 \end{array}$$

$$\begin{array}{r} +81 \text{ Tr} \\ \hline 52 \end{array}$$

$$\begin{array}{r} +89 \text{ FC} \\ \hline 10 \end{array}$$

$$\begin{array}{r} +89 \text{ FC} \\ \hline 11 \end{array}$$

$$\begin{array}{r} +50.2 \text{ P} \\ \hline 53 \end{array}$$

$$\begin{array}{r} +69 \text{ Gup Po} \\ \hline 51 \end{array}$$

$$\begin{array}{r} +19 \text{ Tr} \\ \hline 54 \end{array}$$

$$\begin{array}{r} +69 \text{ PD} \\ \hline 1 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 40-18 \end{array}$$

$$\begin{array}{r} \text{Fc} \\ \hline 9 \end{array}$$

$$+87 \text{ Tr}$$

$$54$$

$$+54 \text{ Tr}$$

$$54$$

$$+30 \text{ Tr}$$

$$54$$

$$\begin{array}{r} +50 \text{ PP} \\ \hline 5 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ \text{Fc} \end{array}$$

$$\begin{array}{r} \text{Fc} \\ \hline 13 \end{array}$$

$$\begin{array}{r} +47.12 \times 92 \text{ V.B.} \\ \hline 76-16' \end{array}$$

$$+47 \text{ E 3' Bot. Ditch}$$

$$+38 \text{ Fields}$$

$$\begin{array}{r} +75 \text{ St} \\ \hline 50 \end{array}$$

$$\begin{array}{r} +62 \text{ Tr} \\ \hline 52' \end{array}$$

$$\begin{array}{r} +11 \text{ PP} \\ \hline 12 \end{array}$$

$$\begin{array}{r} +10 \text{ FC} \\ \hline 1.4' \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 26-5 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 17-3 \end{array}$$

$$\begin{array}{r} +66 \text{ PP} \\ \hline 19 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 11-10 \end{array}$$

38'

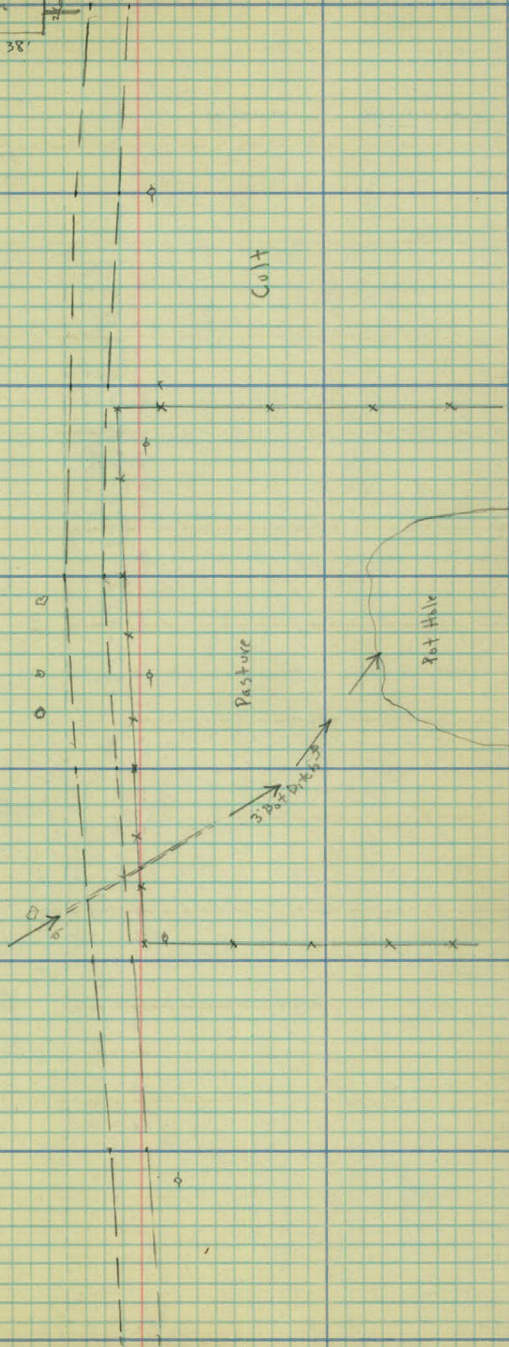
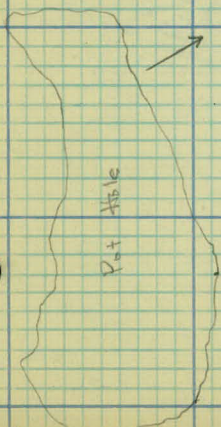
Colt

Pasture

Rot Hole

Rot Hole

3 Dot + Dot + 3



141

$$\begin{array}{r} +18 \text{ Rd} \\ 10 - 12 \\ \hline +18 \text{ WnS Sn} \\ 13 \end{array} \quad \begin{array}{r} +94 \text{ PP} \\ 27 \end{array}$$

140

$$\begin{array}{r} +76 \text{ Shoulder} \\ 23 - 40 \\ \hline +65 \text{ Rd} \\ 8 - 25 \end{array} \quad \begin{array}{r} +58 \text{ PP} \\ 39 \end{array} \quad \begin{array}{r} +73 \text{ RdSn} \\ 93 \end{array}$$

139

$$\begin{array}{r} \text{Rd} \\ 4 - 16 \end{array} \quad \begin{array}{r} +10 \text{ PP} \\ 33 \end{array}$$

138

$$\begin{array}{r} \text{Rd} \\ 9 - 13 \end{array}$$

137

$$\begin{array}{r} \text{Rd} \\ 15 - 8 \end{array} \quad \begin{array}{r} +82 \text{ PP} \\ 27 \end{array} \quad \begin{array}{r} +16 \text{ RdSn} \\ 16 \end{array}$$

136

$$\begin{array}{r} +30 \text{ End Orch} \\ 80 \end{array} \quad \begin{array}{r} +15 \text{ End Culv} \\ 21 \end{array} \quad \begin{array}{r} +55 \text{ PP} \\ 20 \end{array} \quad \begin{array}{r} +27 \text{ FC} + 29 \\ 11 \end{array}$$

$$\begin{array}{r} +12 \text{ Bay Orch} \\ 45 \end{array}$$

$$\begin{array}{r} +34 \text{ End Maple} \\ 41 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 20 - 0 \end{array} \quad \begin{array}{r} +03 \text{ EnCulv} \\ 5 \end{array}$$

$$\begin{array}{r} \text{Fc} \\ 9 \end{array}$$

$$\begin{array}{r} +28 \text{ FC} \\ 3 - 10 \end{array}$$

$$\begin{array}{r} +24 \text{ StP} \\ 10 \end{array}$$

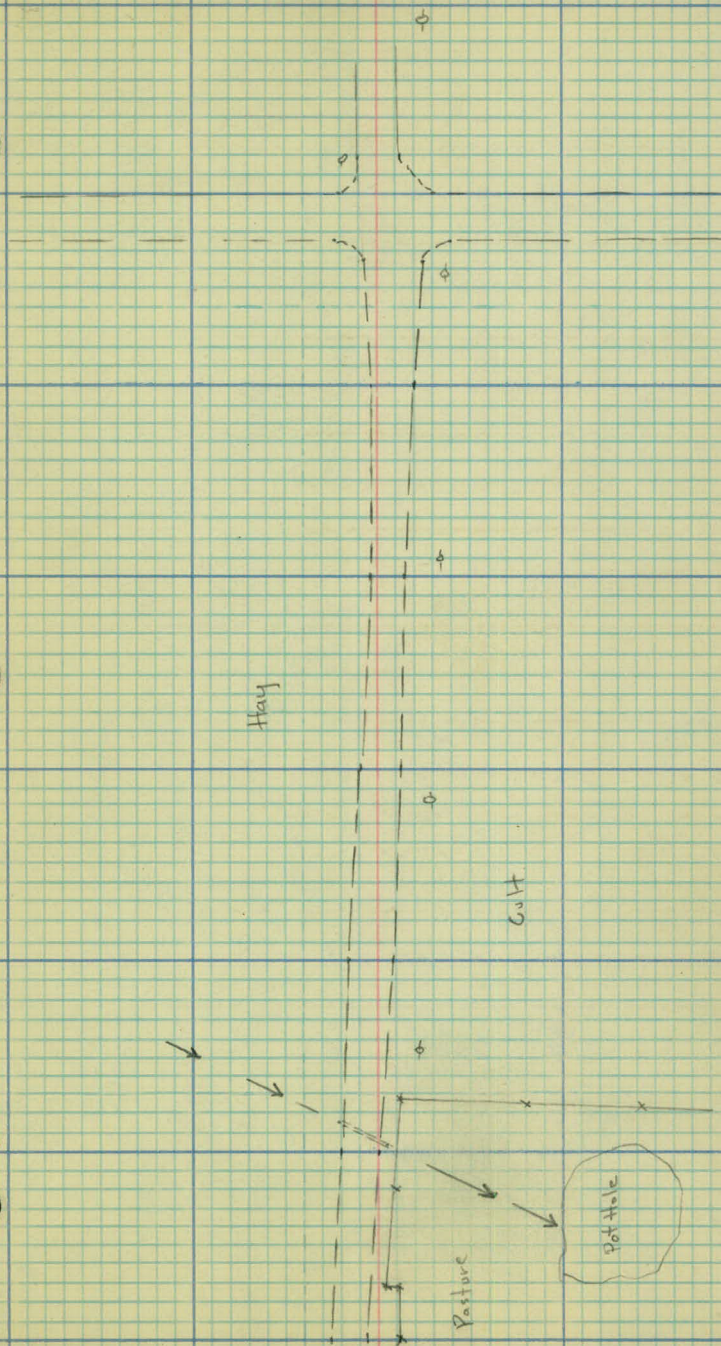
$$\begin{array}{r} +27 \text{ PP} \\ 13 \end{array}$$

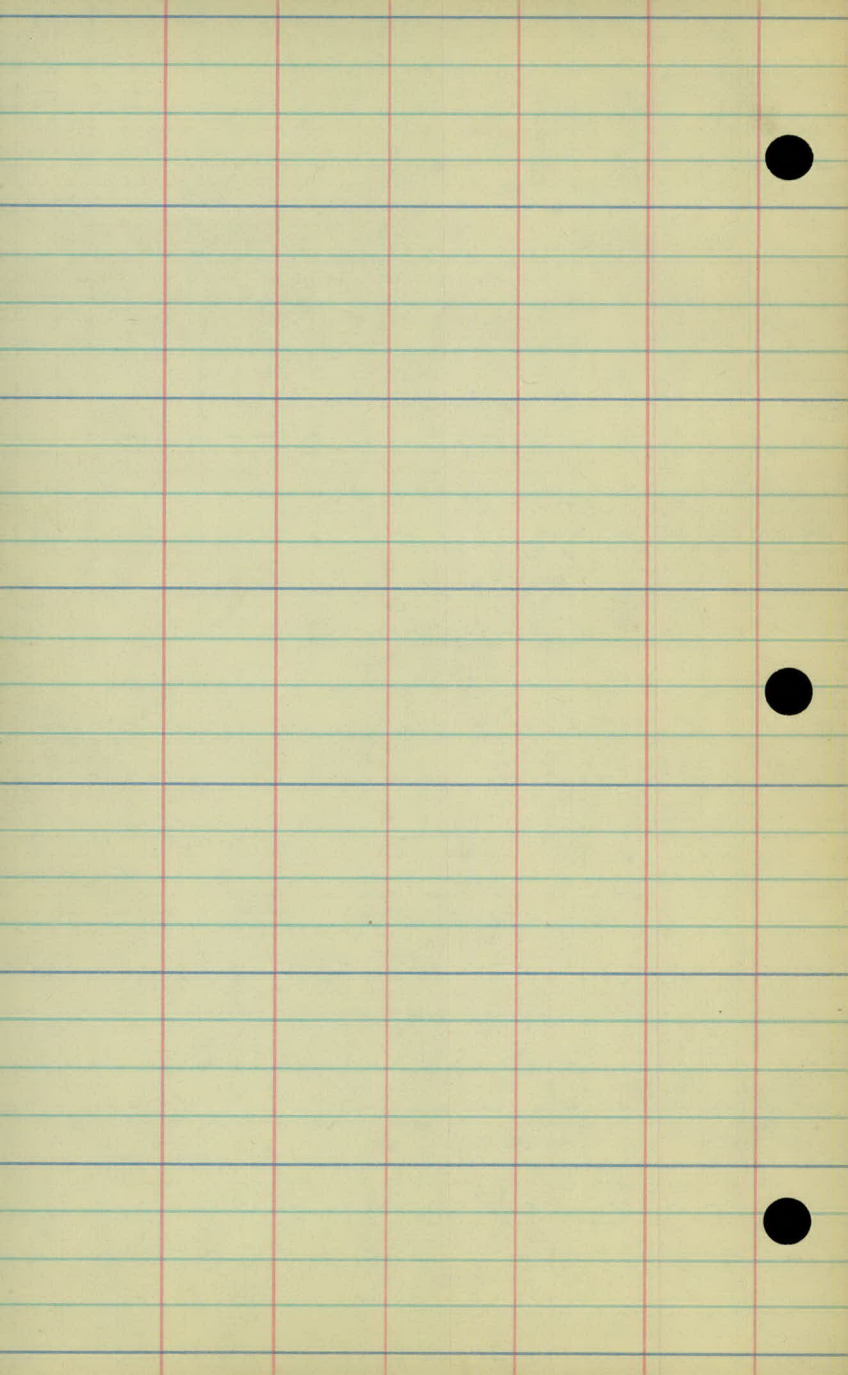
$$\begin{array}{r} +55 \text{ StP} \\ 10 \end{array}$$

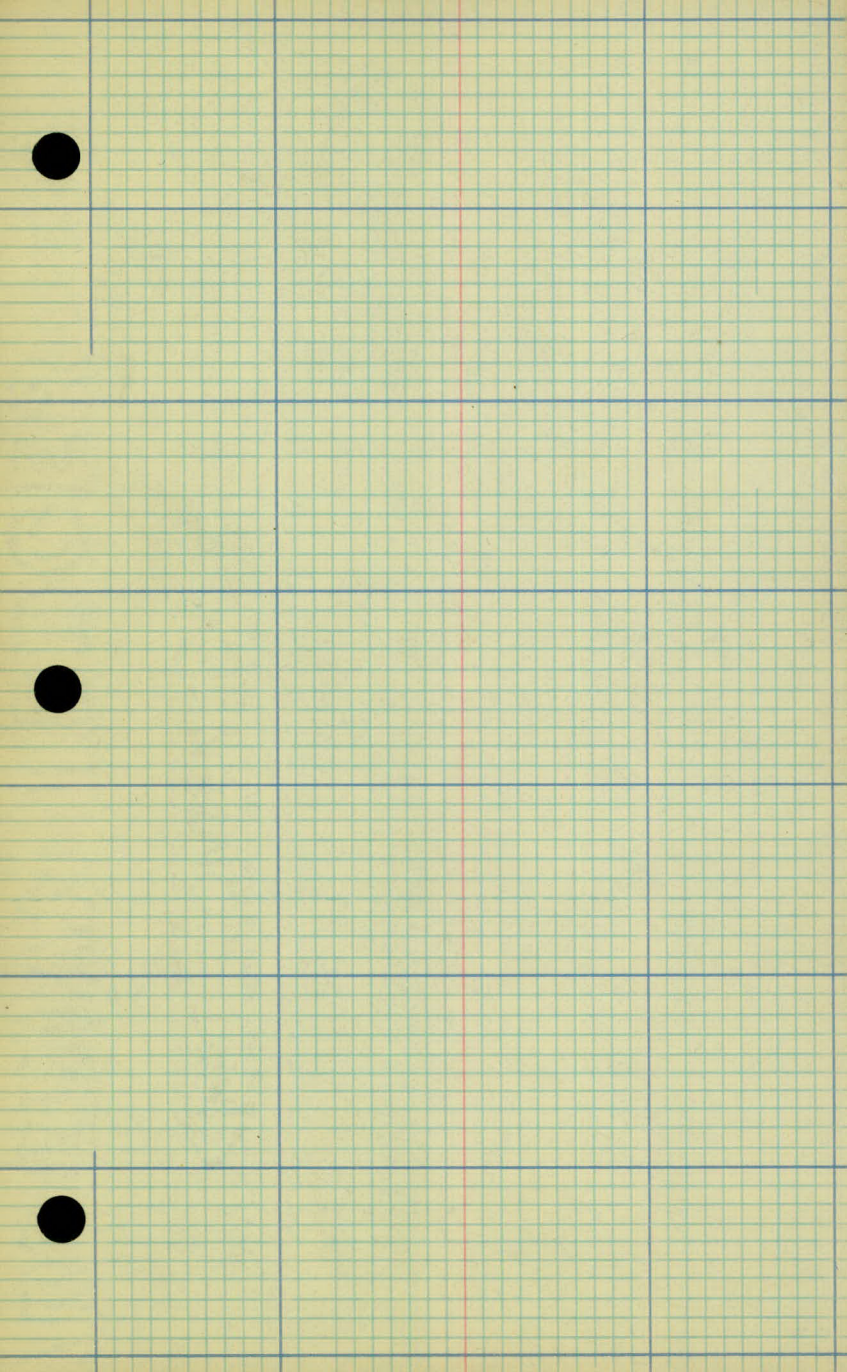
$$\begin{array}{r} \text{Fc} \\ 12 \end{array}$$

135

$$\begin{array}{r} \text{Rd} \\ 25 - 5 \end{array}$$







146

$$\frac{Rd}{12-9}$$

$$\frac{+38 TP}{19}$$

145

$$\frac{Rd}{11-12}$$

$$\frac{+86 R+Sn}{17}$$

$$\frac{+90 TP}{22}$$

144

$$\frac{Rd}{11-12}$$

$$\frac{+41 TP}{24}$$

143

$$\frac{Rd}{11-12}$$

142

$$\frac{Rd}{12-13}$$

$$\frac{+94 TP}{28}$$

141

Hand

Hand

153

$$\frac{R1}{10-10}$$

$$\frac{+31TP}{24}$$

$$\frac{+12Tr}{16}$$
$$\frac{+24Tr}{16}$$

152

$$\frac{R1}{10-11}$$

$$\frac{+11Tr}{13}$$
$$\frac{+02TP}{24}$$

151

$$\frac{R9}{12-9}$$

$$\frac{+12TP}{21}$$
$$\frac{+17Cor Ho}{155}$$
$$+95Ent$$

150

$$\frac{R9}{11-10}$$

149

$$\frac{R1}{12-10}$$

$$\frac{+36TP}{25}$$

148

$$\frac{R1}{12-8}$$

$$\frac{+81TP}{18}$$

$$+63 \frac{12" \times 30 CM}{21-9'}$$

147

$$\frac{R1}{13-8}$$

Hay

Colt

DD

40'
JIS Fr

Hay

Colt

11

160

$$\begin{array}{r} +50 \text{ Rd} \\ 28-5 \end{array}$$

Rd

$$24-0$$

$$\begin{array}{r} +07 \text{ TP} \\ 15 \end{array}$$

159

$$\begin{array}{r} +50 \text{ Rd} \\ 20-4 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ 15-7 \end{array}$$

158

$$\begin{array}{r} +50 \text{ Rd} \\ 9-11 \end{array}$$

Rd

$$8-14$$

$$\begin{array}{r} +14 \text{ TP} \\ 25 \end{array}$$

157

$$\begin{array}{r} \text{Rd} \\ 11-10 \end{array}$$

$$\begin{array}{r} +41 \text{ TP} \\ 27 \end{array}$$

156

$$\begin{array}{r} +50 \text{ RA} \\ 14-8 \end{array}$$

$$\begin{array}{r} \text{RA} \\ 17-4 \end{array}$$

$$\begin{array}{r} +05 \text{ TP} \\ 16 \end{array}$$

155

$$\begin{array}{r} \text{RA} \\ 17-4 \end{array}$$

154

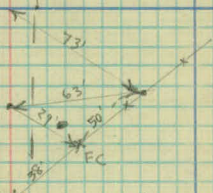
$$\begin{array}{r} \text{Rd} \\ 11-9 \end{array}$$

$$\begin{array}{r} +65 \text{ TP} \\ 16 \end{array}$$

Hay

Hay

Cut



167

$$\begin{array}{r}
 +39 \text{ GuyPo} \\
 \hline
 21 \\
 +50 \text{ Rd} \\
 \hline
 15 - 5 \\
 \hline
 \text{Rd} \\
 18 - 5
 \end{array}
 \qquad
 \begin{array}{r}
 +51 \text{ StP} \\
 \hline
 21 \\
 +37 \text{ TP} \\
 \hline
 7 \\
 +33 \text{ Rd Sn} \\
 \hline
 8 \\
 +02 \text{ Tr} \\
 \hline
 22
 \end{array}
 \qquad
 \begin{array}{r}
 +75 \text{ GuyPo} \\
 \hline
 21 \\
 +63 \text{ Tr} \\
 \hline
 26 \\
 +77 \text{ Tr} \\
 \hline
 26
 \end{array}$$

166

$$\begin{array}{r}
 +90 \text{ FC} \\
 \hline
 17 \\
 +58 \text{ FC} \\
 \hline
 17 \\
 +50 \text{ Rd} \\
 \hline
 14 - 8 \\
 \hline
 \text{Rd} \\
 8 - 14
 \end{array}
 \qquad
 \begin{array}{r}
 +97 \text{ Tr} \\
 \hline
 32 \\
 +45 \text{ Ent} \\
 \hline
 +02 \text{ TP} \\
 \hline
 20
 \end{array}$$

165

$$\begin{array}{r}
 +95 \text{ GuyPo} \\
 \hline
 21 \\
 +50 \text{ Rd} \\
 \hline
 2 - 17 \\
 \hline
 \text{Rd} \\
 0 - 20
 \end{array}
 \qquad
 +23 \text{ Ent}$$

164

$$\begin{array}{r}
 +96 \text{ 15"X40' CM} \\
 \hline
 10 - 30 \\
 +50 \text{ Rd} \\
 \hline
 1 - 20 \\
 \hline
 \text{Rd} \\
 6 - 16
 \end{array}
 \qquad
 \begin{array}{r}
 +47 \text{ TP} \\
 \hline
 32
 \end{array}$$

163

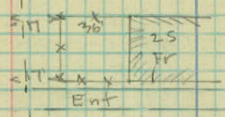
$$\begin{array}{r}
 +50 \text{ Rd} \\
 \hline
 12 - 11 \\
 \hline
 \text{Rd} \\
 20 - 2
 \end{array}$$

162

$$\begin{array}{r}
 +99 \text{ GuyPo} \\
 \hline
 34 \\
 +50 \text{ Rd} \\
 \hline
 29 - 7 \\
 \hline
 \text{Rd} \\
 37 - 14
 \end{array}
 \qquad
 \begin{array}{r}
 +96 \text{ TP} \\
 \hline
 16
 \end{array}$$

161

$$\begin{array}{r}
 +50 \text{ GuyPo} \\
 \hline
 48 \\
 +50 \text{ Rd} \\
 \hline
 39 - 16 \\
 \hline
 \text{Rd} \\
 34 - 11
 \end{array}
 \qquad
 \begin{array}{r}
 +49 \text{ TP} \\
 \hline
 1
 \end{array}$$



Hau

Hau

$$\frac{+71 R d S n}{75}$$

$$\frac{+38 F c + 34}{24}$$

174

$$\frac{R d}{74 - 55}$$

$$\frac{F c}{25}$$

$$\frac{+95 T P}{49}$$

$$\frac{+54 12 \times 28 C M}{86 - 58}$$

173

$$\frac{R d}{85 - 65}$$

$$\frac{F c}{27}$$

$$\frac{+62 T P}{66}$$

172

$$\frac{R d}{90 - 67}$$

$$\frac{F c}{42}$$

171

$$\frac{R d}{58 - 35}$$

$$\frac{+87 T P}{19}$$

$$\frac{+40 R d}{22 - 0}$$

$$\frac{+40 T r}{48}$$

$$\frac{+71 T r}{19}$$

$$\frac{+17 F c}{45}$$

170

$$\frac{R d}{11 - 11}$$

$$\frac{T P}{26}$$

$$\frac{F c}{40}$$

$$\frac{+61 R d}{1 - 20}$$

$$\frac{+30 T r}{38}$$

$$\frac{+57 F c}{+8.5}$$

169

$$\frac{R d}{0 - 22}$$

$$\frac{+15 T r}{38}$$

$$\frac{F c}{38}$$

$$\frac{T r}{38}$$

$$\frac{+50 R d}{4 - 17}$$

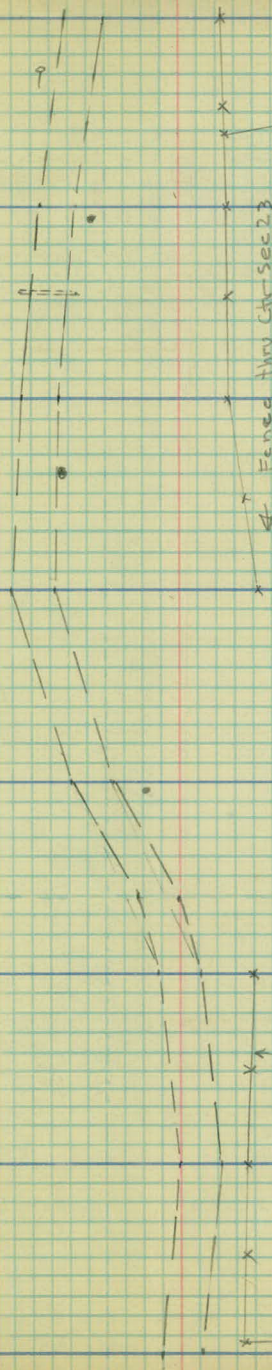
$$\frac{+65 T P}{24}$$

168

$$\frac{R d}{10 - 11}$$

$$\frac{+05 F c}{32}$$

Cult



Fence to
15' E of Ctr. Sec. 23

Pasture

181

$$\frac{Rd}{0-21}$$

$$\frac{+27TP}{27}$$

$$\begin{array}{r} +95FC \\ 11 \\ +64Tr \\ \hline +50Tr \\ 31 \\ +58Tr \\ 31 \\ \hline +05CorHo \\ 66 \end{array}$$

$$+36Ent+5x16CM$$

180

$$\frac{Rd}{0-22}$$

$$\begin{array}{r} +99Tr \\ 25 \\ +30Tr \\ 29 \\ +34Tr \\ 36 \\ +41Tr \\ 29 \\ \hline +14Ent+12x20CM \\ 15 \\ \hline +10FC \\ 41 \end{array}$$

$$\frac{+98TP}{34}$$

179

$$\frac{+44FC}{21}$$

$$\frac{+86TP}{19}$$

178

$$\frac{Fc}{28}$$

$$\frac{Rd}{17-2}$$

$$Fc$$

$$+9820x36VP$$

$$\frac{+90EndFc}{15}$$

$$+92Ent+2x20CM$$

$$37$$

$$+68Tr$$

$$\frac{+46FC + 50}{31}$$

$$\frac{+50TP}{1}$$

177

$$\frac{Rd}{29-10}$$

$$\frac{Fc}{17}$$

$$\frac{+36TP}{14}$$

176

$$\frac{Rd}{45-23}$$

$$\frac{Fc}{20}$$

$$\frac{+31TP}{29}$$

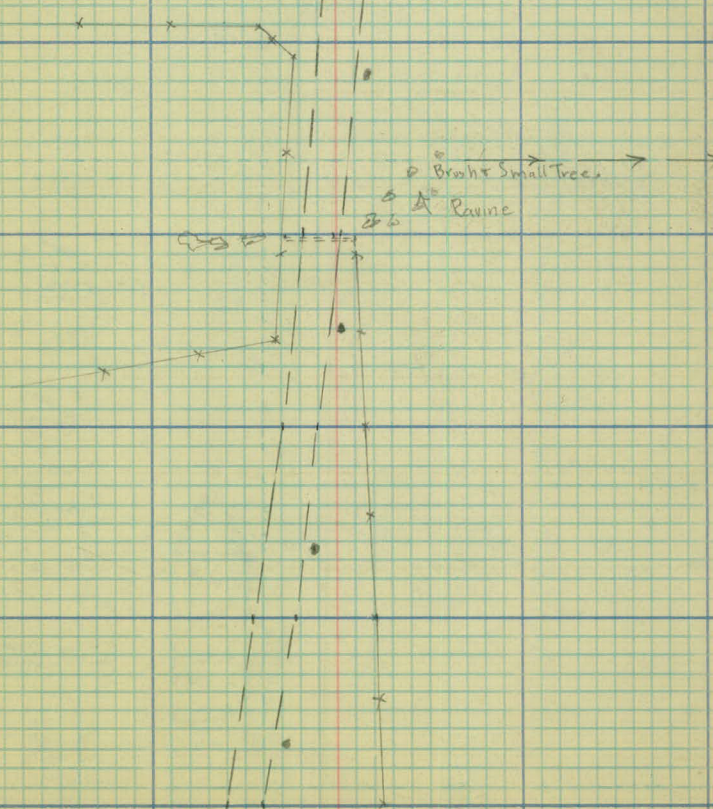
$$\frac{Rd}{60-40}$$

$$\frac{Fc}{22}$$

175

41
 1/25
 80

Ent



188

$$\frac{Rd}{12-2}$$

$$\frac{+69 TP}{6}$$

$$\frac{Fc}{5}$$

$$\frac{+95 \text{ } 12' \times 30' \text{ CM}}{29-1}$$

$$\frac{+44 TP}{5}$$

$$Rq$$

187

186

$$\frac{Rd}{21-0}$$

$$\frac{Fc}{4}$$

185

$$\frac{+15 TP}{8}$$

$$\frac{Rd}{11-2}$$

$$\frac{Fc}{10}$$

184

$$\frac{Rq}{16-6}$$

$$\frac{+96 Fc}{29}$$

$$\frac{+96 Fc}{12}$$

183

$$\frac{Fc}{24}$$

$$\frac{Rd}{10-11}$$

182

$$\frac{Fc}{17}$$

$$\frac{+32 \text{ } 12' \times 28'}{9-14}$$

$$\frac{+61 TP}{10}$$

$$\frac{Rd}{3-16}$$

Hay

Hay

$\frac{1}{4}$ Line $\frac{1}{4}$

Hay

Hay

$$\frac{+46 \text{ Steel H. Tan. Tower} + 33}{20}$$

$$\frac{+01 \text{ FC} + 08}{15}$$

$$\frac{+09 \text{ TP}}{26}$$

195

$$\frac{Rd}{3-16} \quad \frac{Fc}{27}$$

$$+70 \text{ Ent}$$

194

$$\frac{Rd}{2-18} \quad \frac{Fc}{26}$$

$$\frac{+87 \text{ TP}}{22}$$

$$\frac{+84 \text{ Rd Sn}}{24}$$

193

$$\frac{Rd}{6-16} \quad \frac{Fc}{24}$$

$$\frac{+60 \text{ TP}}{18}$$

192

$$\frac{Rd}{9-13} \quad \frac{Fc}{20}$$

$$\frac{+26 \text{ TP}}{14}$$

191

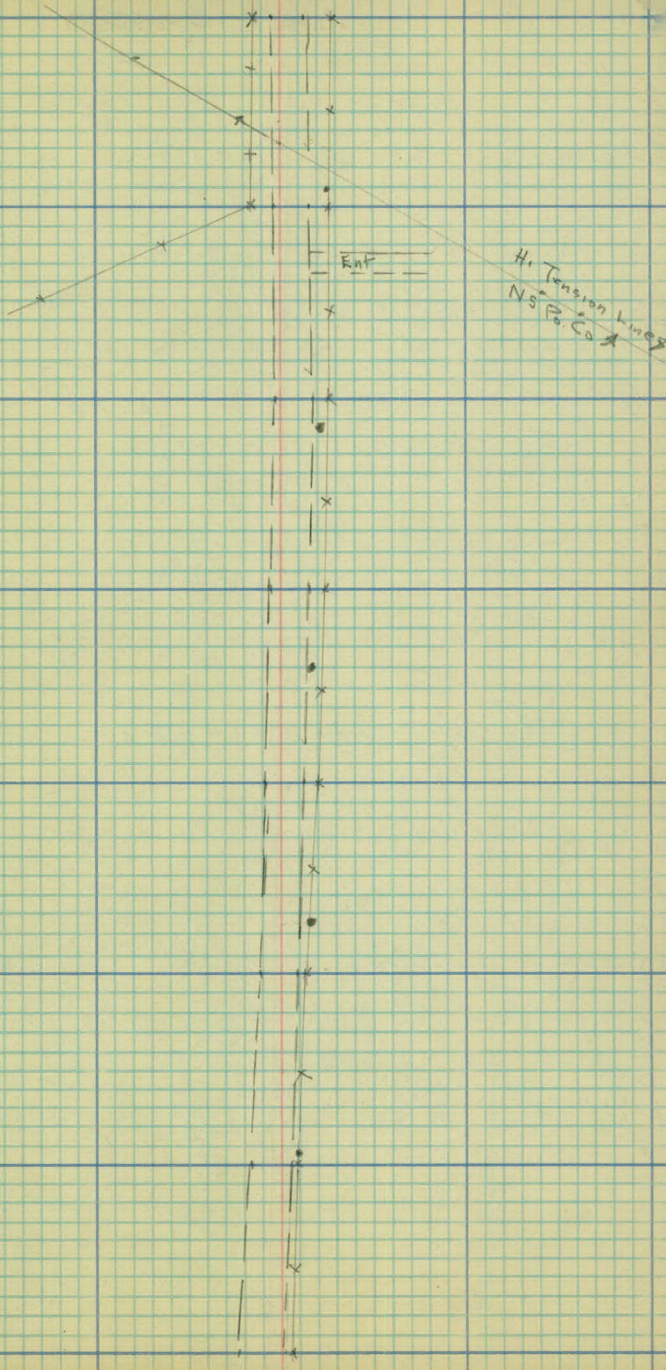
$$\frac{Rd}{11-9} \quad \frac{Fc}{17}$$

190

$$\frac{Rd}{17-4} \quad \frac{+04 \text{ TP}}{9} \quad \frac{Fc}{9}$$

189

$$\frac{Rd}{23-1} \quad \frac{Fc}{6}$$



+31 G.R.
+26 Shoulder
+16.5 Ex

198

$$\frac{GR}{47}$$

$$\frac{Sh}{45}$$

$$\frac{Should}{33}$$

$$\frac{GR}{40}$$

$$\begin{array}{r} Fc \quad GR \quad + 62 Rd \quad GR \\ 21 \quad 17 \quad 13 - 12 \quad 15 \\ + 06 A' Conc. Spillway \\ 40 - 16 \end{array}$$

$$\begin{array}{r} + 70 Rd Sn \\ 17 \end{array}$$

197

$$\frac{Fc}{20}$$

$$\frac{G.R.}{17}$$

$$\frac{Rd}{10 - 12}$$

$$\frac{GR}{15}$$

$$\begin{array}{r} + 03 TP \\ EC \quad 33 \\ 32 \end{array}$$

$$\begin{array}{r} + 69 Beg GR \\ 17 \end{array}$$

$$\begin{array}{r} + 65 Beg GR \\ 15 \end{array}$$

$$\begin{array}{r} + 07 \\ 29 \end{array}$$

196

$$\frac{Fc}{14}$$

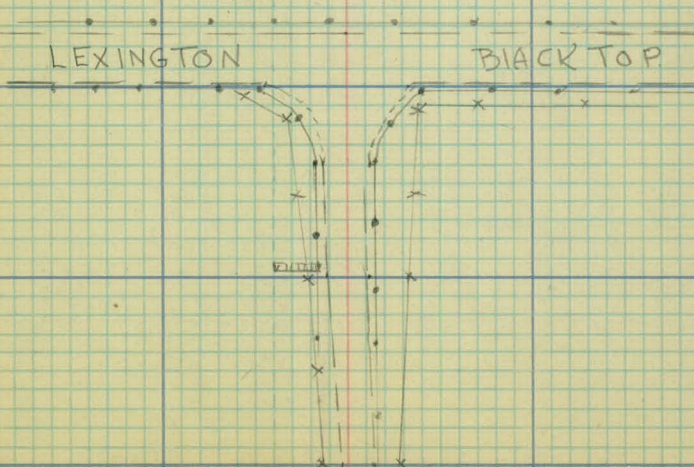
$$\frac{Rd}{7 - 13}$$

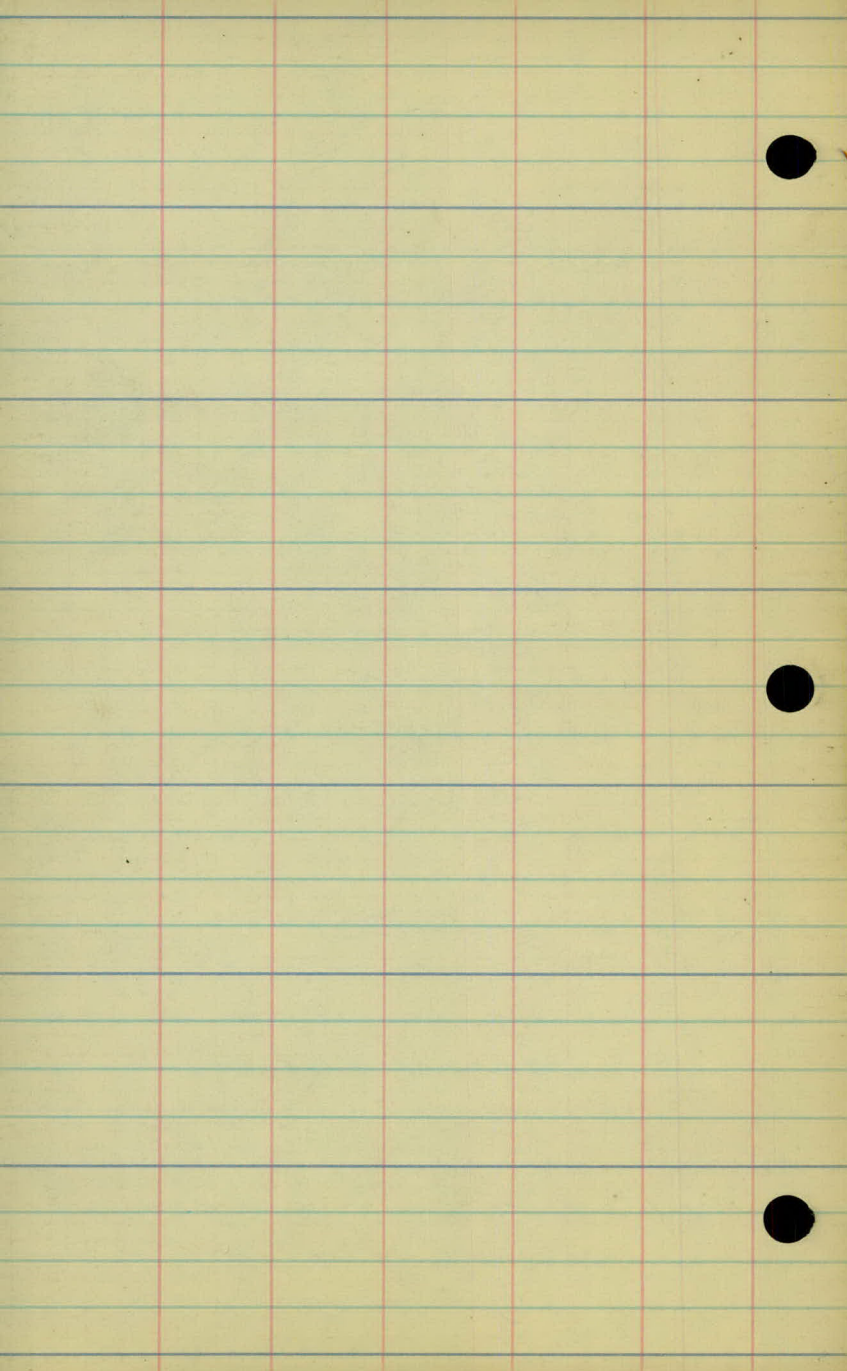
$$\frac{Fc}{29}$$

LEXINGTON

BLACK TOP

WILDER





12/5/35

X-Sections

Victoria Street

Sta	+	π	-	
B.M.	10.55	✓ 911.56 ✓		901.01
0	10.43	921.70 ✓	0.29	911.27 ✓
B.M.			11.70	910.00 ✓
2 + 00				09.0 ✓
+21				10.4 ✓
+25				11.7 ✓
+50				13.7 ✓
+65				13.9 ✓
3				14.6 ✓

SpK in 12" Oak 20' W. & 275' So. Victoria + C²

SpK in PP S.W. of Victoria + Owasso Blvd Int.

ER ₂		ER				Fcc			
$\frac{12.5}{83}$	$\frac{11.0}{80}$	$\frac{10.1}{71}$	$\frac{10.6}{57}$	$\frac{11.0}{43}$	$\frac{12.5}{33}$	$\frac{13.0}{29}$	$\frac{12.7}{22}$	$\frac{12.7}{12}$	$\frac{10.5}{46}$
									$\frac{6.1}{100}$
$\frac{13.1}{100}$									

ER ₂		ER ₂				DT ₂ ER			
$\frac{13.3}{100}$	$\frac{12.2}{66}$	$\frac{10.7}{63}$	$\frac{9.9}{55}$	$\frac{9.3}{37}$	$\frac{9.9}{10}$	$\frac{10.9}{3}$	$\frac{11.3}{11.3}$	$\frac{11.2}{14}$	$\frac{9.8}{16}$
								$\frac{7.7}{46}$	$\frac{9.0}{64}$
								$\frac{7.7}{95}$	$\frac{7.4}{100}$

10.0

ER ₂		ER ₂					
$\frac{13.4}{100}$	$\frac{11.2}{46}$	$\frac{9.3}{42}$	$\frac{7.1}{34}$	$\frac{8.3}{18}$	$\frac{8.0}{8.0}$	$\frac{7.4}{50}$	$\frac{6.9}{100}$

ER ₂		ER ₂							
$\frac{13.3}{100}$	$\frac{10.8}{39}$	$\frac{8.5}{33}$	$\frac{8.9}{26}$	$\frac{8.0}{14}$	$\frac{7.8}{7.8}$	$\frac{8.3}{21}$	$\frac{8.0}{30}$	$\frac{6.4}{35}$	$\frac{4.6}{57}$
								$\frac{5.4}{78}$	$\frac{7.3}{100}$

ER ₂		ER ₂							
$\frac{12.9}{100}$	$\frac{8.5}{30}$	$\frac{9.6}{20}$	$\frac{7.6}{16}$	$\frac{7.7}{13}$	$\frac{7.1}{7.1}$	$\frac{7.4}{14}$	$\frac{7.6}{20}$	$\frac{4.4}{28}$	$\frac{4.7}{52}$
								$\frac{8.0}{79}$	$\frac{9.0}{100}$

Sta	+	Δ	-	
		921.70		
4				17.8 ✓
5				21.1 ✓
6	12.42 ✓	933.50 ✓	0.62	921.08 ✓
				23.7 ✓
+50				24.9 ✓
7				26.5 ✓
+15				28.8 ✓
8				29.7 ✓
9	13.21	946.08 ✓	0.63	932.87 ✓

$$\begin{array}{cccccccccccc} & & & & & & ER7 & & ER & & & & & \\ \frac{8.3}{100} & \frac{7.5}{12} & \frac{1.6}{49} & \frac{2.0}{26} & \frac{3.1}{76} & \frac{4.5}{12} & \frac{4.3}{9} & 3.9 & \frac{4.3}{14-16} & \frac{5.4}{26} & \frac{6.6}{33} & \frac{10.0}{100} \end{array}$$

$$\begin{array}{cccccccccccc} & & & & & & & & ER & & & & & \\ \frac{+9.0}{100} & \frac{+0.7}{51} & \frac{+0.4}{24} & \frac{0.9}{14} & \frac{0.7}{9} & 0.6 & \frac{1.3}{12} & \frac{1.5}{14} & \frac{5.4}{20} & \frac{7.5}{100} \end{array}$$

$$\begin{array}{cccccccccccc} & & & & & & ER & & ER2 & & & & & \\ \frac{16.0}{100} & \frac{10.4}{27} & \frac{11.3}{15} & \frac{10.2}{12} & \frac{10.0}{9} & 9.8 & \frac{10.2}{13} & \frac{10.4}{17} & \frac{13.3}{22} & \frac{15.2}{83} & \frac{14.4}{100} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{15.9}{100} & \frac{14.7}{62} & \frac{7.6}{22} & \frac{7.0}{12} & \frac{8.8}{9} & 8.6 & \frac{8.8}{13} & \frac{9.0}{14} & \frac{10.3}{19} & \frac{8.9}{25-100} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{13.6}{100} & \frac{11.7}{47} & & \frac{8.3}{20-14} & & \frac{7.4}{12-9} & 7.0 & \frac{7.4}{13} & \frac{7.7}{15} & \frac{8.7}{18} & \frac{9.4}{100} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{5.9}{100} & \frac{6.2}{41} & \frac{5.3}{18} & \frac{6.0}{14} & \frac{5.2}{11} & \frac{5.1}{9} & 4.7 & \frac{5.1}{14} & \frac{5.4}{17} & \frac{5.9}{20} & \frac{7.6}{76} & \frac{8.2}{100} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{4.2}{100} & \frac{4.0}{40} & \frac{4.8}{14} & \frac{4.2}{14-10} & 3.8 & \frac{4.1}{14} & \frac{4.0}{17} & \frac{3.2}{21} & \frac{3.9}{25} & \frac{5.3}{87} & \frac{5.7}{100} \end{array}$$

Sta

+

x

-

94608

9

34.4 ✓

10

40.7 ✓

11

13.43

959.35 ✓

0.16

94592 ✓

11

44.8 ✓

+60

50.3 ✓

12

52.5 ✓

+60

55.0 ✓

13

56.3 ✓

13

424

961.91 ✓

1.68

95767 ✓

$$\frac{8.2}{100} \quad \frac{8.5}{58} \quad \frac{10.6}{21} \quad \frac{12.0}{10} \quad \frac{12.5}{9} \quad 11.7 \quad \frac{12.1}{13} \quad \frac{11.8}{18} \quad \frac{10.0}{22} \quad \frac{11.7}{100}$$

$$\frac{4.2}{100} \quad \frac{2.4}{50} \quad \frac{4.6}{14} \quad \frac{3.6}{12} \quad \frac{5.5}{10} \quad \frac{5.7}{8} \quad 5.4 \quad \frac{6.0}{15} \quad \frac{4.1}{21} \quad \frac{6.1}{79} \quad \frac{5.2}{100}$$

$$\frac{12.0}{100} \quad \frac{10.1}{50} \quad \frac{10.7}{24} \quad \frac{11.9}{13} \quad \frac{11.4}{11} \quad \frac{13.0}{9} \quad \frac{12.9}{7} \quad 12.6 \quad \frac{12.9}{15} \quad \frac{12.3}{18} \quad \frac{10.2}{22} \quad \frac{9.9}{100}$$

$$\frac{7.9}{100} \quad \frac{4.3}{43} \quad \frac{8.0}{12} \quad \frac{9.5}{10} \quad \frac{9.4}{7} \quad 9.1 \quad \frac{9.6}{15} \quad \frac{9.0}{18} \quad \frac{6.3}{22} \quad \frac{5.1}{36} \quad \frac{5.3}{100}$$

$$\frac{6.7}{100} \quad \frac{4.4}{79} \quad \frac{2.7}{41} \quad \frac{6.9}{10} \quad \frac{7.5}{8} \quad \frac{7.3}{6} \quad 6.9 \quad \frac{7.1}{14} \quad \frac{6.7}{18} \quad \frac{4.4}{22} \quad \frac{2.0}{37} \quad \frac{1.7}{92-100}$$

$$\frac{5.5}{100} \quad \frac{1.5}{43} \quad \frac{4.8}{10-7} \quad 4.4 \quad \frac{4.3}{14} \quad \frac{1.9}{22} \quad \frac{0.4}{39} \quad \frac{+2.0}{100}$$

$$\frac{4.0}{100} \quad \frac{1.3}{42} \quad \frac{3.7}{11} \quad \frac{3.4}{7} \quad 3.1 \quad \frac{3.2}{14} \quad \frac{3.3}{18} \quad \frac{1.8}{21} \quad \frac{1.2}{42} \quad \frac{+1.3}{68} \quad \frac{+2.6}{100}$$

Top Boat Spk. Sta 14+00 E

Sta

+

π

-

961.91

B.M.

414

957.77 ✓

13 +65

57.6 ✓

14

57.7 ✓

+30

57.8 ✓

+80

57.3 ✓

15

56.7 ✓

+50

54.6 ✓

16

52.4 ✓

Spk 10 10" W 62K 33' Lt 5 to 14+95

$\frac{7.3}{100}$ $\frac{4.8}{26}$ $\frac{5.3}{14}$ $\frac{4.9}{11}$ 4.3 $\frac{4.3}{12}$ $\frac{4.7}{16}$ $\frac{2.1}{20}$ $\frac{0.6}{52}$ $\frac{+2.9}{100}$

$\frac{7.5}{100}$ $\frac{4.9}{21}$ $\frac{5.4}{14}$ $\frac{4.7}{12}$ $\frac{4.5}{10}$ 4.2 $\frac{4.2}{11}$ $\frac{4.7}{16}$ $\frac{2.7}{21}$ $\frac{1.3}{50}$ $\frac{0.0}{78}$

$\frac{8.8}{100}$ $\frac{7.5}{67}$ $\frac{5.2}{21}$ $\frac{4.5}{17-14}$ 4.1 $\frac{4.2}{10-16}$ $\frac{3.2}{22}$ $\frac{1.2}{100}$

For
 $\frac{12.5}{100}$ $\frac{4.4}{30}$ $\frac{4.7}{22}$ $\frac{4.5}{21}$ $\frac{5.4}{18}$ $\frac{4.9}{13}$ 4.6 $\frac{5.1}{10}$ $\frac{5.5}{14}$ $\frac{4.9}{17}$ $\frac{1.2}{21}$ $\frac{3.6}{100}$

$\frac{14.2}{100}$ $\frac{4.6}{30}$ $\frac{5.3}{27}$ $\frac{4.9}{21}$ $\frac{5.9}{18}$ $\frac{5.3}{14}$ 5.2 $\frac{5.6}{10}$ $\frac{5.2}{12}$ $\frac{6.2}{14}$ $\frac{6.1}{16}$ $\frac{1.5}{21}$ $\frac{1.9}{57}$ $\frac{2.7}{100}$

$\frac{14.9}{100}$ $\frac{12.2}{70}$ $\frac{5.2}{30}$ $\frac{7.0}{27}$ $\frac{6.9}{21}$ $\frac{8.1}{18}$ $\frac{7.4}{14}$ 7.3 $\frac{7.8}{8}$ $\frac{7.4}{11}$ $\frac{8.2}{13}$ $\frac{8.1}{15}$ $\frac{4.3}{20}$ $\frac{4.0}{42}$ $\frac{1.8}{75}$ $\frac{2.3}{100}$

$\frac{15.0}{100}$ $\frac{12.7}{60}$ $\frac{10.1}{22}$ $\frac{10.8}{19}$ $\frac{9.8}{17}$ $\frac{9.6}{13}$ 9.5 $\frac{9.7}{8}$ $\frac{9.6}{10}$ $\frac{10.5}{13-16}$ $\frac{9.5}{21}$ $\frac{10.3}{27}$ $\frac{3.3}{100}$

Sta + π -

961.91

16 + 60

50.9 ✓

17

50.6 ✓

18

51.3 ✓

2

2.24

958.02 ✓

6.13

955.78 ✓

9

52.9 ✓

+75

52.9 ✓

20

52.8 ✓

+60

52.0 ✓

21

51.1 ✓

Foot

$\frac{16.9}{10}$ $\frac{15.9}{46}$ $\frac{14.8}{26}$ $\frac{11.4}{19}$ $\frac{11.1}{13}$ 11.0 $\frac{11.2}{7}$ $\frac{11.5}{12}$ $\frac{12.9}{15}$ $\frac{13.4}{19}$ $\frac{12.4}{45}$ $\frac{6.2}{100}$

Foot

$\frac{16.9}{100}$ $\frac{15.9}{44}$ $\frac{14.8}{26}$ $\frac{11.9}{17}$ $\frac{11.4}{13}$ 11.3 $\frac{11.4}{9-10}$ $\frac{13.8}{16}$ $\frac{14.1}{19}$ $\frac{13.5}{22}$ $\frac{14.1}{31}$ $\frac{9.7}{100}$

$\frac{7.1}{100-69}$ $\frac{11.5}{22-19}$ $\frac{10.6}{16}$ $\frac{10.7}{12}$ 10.6 $\frac{11.2}{10-11}$ $\frac{13.2}{18}$ $\frac{13.0}{21}$ $\frac{15.1}{31}$ $\frac{23.0}{91}$

Top Step 30' 1 + Sta 18 + 65

$\frac{2.3}{100}$ $\frac{3.3}{23}$ $\frac{4.5}{16}$ $\frac{5.6}{4}$ $\frac{5.3}{12}$ 5.1 $\frac{5.8}{12}$ $\frac{6.8}{14-17}$ $\frac{5.0}{21}$ $\frac{10.5}{60}$ $\frac{15.8}{100}$

70 - 40 $\frac{0.8}{24}$ $\frac{3.4}{21}$ $\frac{4.0}{16}$ $\frac{5.6}{12}$ $\frac{5.5}{10}$ 5.1 $\frac{5.5}{12}$ $\frac{6.2}{14}$ $\frac{6.1}{16}$ $\frac{5.2}{17}$ $\frac{6.0}{41}$ $\frac{10.9}{84}$ $\frac{13.8}{100}$

$\frac{1.0}{47}$ $\frac{2.7}{22}$ $\frac{4.6}{19}$ $\frac{5.8}{12}$ $\frac{5.4}{10}$ 5.2 $\frac{5.7}{13}$ $\frac{6.5}{15}$ $\frac{5.8}{22}$ $\frac{7.5}{50}$ $\frac{13.1}{100}$

$\frac{9.8}{100}$ $\frac{6.0}{42}$ $\frac{5.4}{22}$ $\frac{6.5}{12}$ $\frac{6.1}{9}$ 6.0 $\frac{6.5}{13}$ $\frac{6.9}{15}$ $\frac{8.0}{19}$ $\frac{10.2}{57}$ $\frac{9.6}{100}$

$\frac{12.0}{100}$ $\frac{7.9}{51}$ $\frac{7.0}{22}$ $\frac{7.2}{15}$ $\frac{7.5}{12}$ $\frac{7.0}{10}$ 6.9 $\frac{7.3}{12}$ $\frac{7.7}{18-24}$ $\frac{9.8}{88}$ $\frac{10.8}{100}$

Sta

+

A

-

958.02

22

50.3 ✓

+70

50.9 ✓

23

51.6 ✓

+55

52.7 ✓

24

52.8 ✓

+60

52.4 ✓

O

3.27

960.60 ✓

0.69

957.33 ✓

BM

478

955.82

$\frac{112}{100}$ $\frac{117}{24}$ $\frac{113}{23}$ $\frac{109}{18}$ $\frac{86}{14}$ $\frac{81}{8}$ 7.7 $\frac{79}{12}$ $\frac{82}{14}$ $\frac{93}{18}$ $\frac{89}{23}$ $\frac{100}{41}$ $\frac{116}{100}$

$\frac{56}{100}$ $\frac{48}{60}$ $\frac{90}{14}$ $\frac{77}{12}$ $\frac{75}{8}$ 7.1 $\frac{75}{13}$ $\frac{77}{16}$ $\frac{100}{20}$ $\frac{110}{75}$ $\frac{100}{100}$

$\frac{55}{100}$ $\frac{50}{67}$ $\frac{44}{22}$ $\frac{78}{12}$ 11 $\frac{68}{9}$ 6.4 $\frac{68}{13}$ $\frac{80}{16}$ $\frac{103}{55}$ $\frac{111}{100}$

$\frac{55}{100}$ $\frac{31}{46}$ $\frac{16}{19}$ $\frac{25}{17}$ $\frac{62}{11}$ $\frac{58}{9}$ 5.3 $\frac{57}{15}$ $\frac{62}{17}$ $\frac{23}{24}$ $\frac{44}{74}$ $\frac{91}{100}$

$\frac{41}{100}$ $\frac{15}{57}$ $\frac{21}{19}$ $\frac{30}{15}$ $\frac{59}{11}$ $\frac{57}{7}$ 5.2 $\frac{53}{17}$ $\frac{61}{17}$ $\frac{51}{21}$ $\frac{34}{23}$ $\frac{46}{76}$ $\frac{67}{100}$

$\frac{71}{92}$ $\frac{38}{54}$ $\frac{34}{76}$ $\frac{65}{11}$ $\frac{61}{7}$ 5.6 $\frac{57}{14}$ $\frac{58}{17}$ $\frac{15}{24}$ $\frac{28}{72}$ $\frac{47}{100}$

Top Stp 40' Lt Sta 24+40

SpK in 16" B.O.R 50' Lt Sta 23+55

Sta	+	x	-
		960.60	

25			51.8 ✓
----	--	--	--------

26			50.6 ✓
----	--	--	--------

27			52.1 ✓
----	--	--	--------

28			55.8 ✓
----	--	--	--------

29			51.0 ✓
----	--	--	--------

BM		4.00	956.60 ✓
----	--	------	----------

30			56.5 ✓
----	--	--	--------

31			55.8 ✓
----	--	--	--------

32			54.7 ✓
----	--	--	--------

0	7.76	962.46 ✓	5.88	954.72 ✓
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$\frac{13.0}{100}$ $\frac{11.1}{76}$ $\frac{9.2}{19}$ $\frac{10.4}{13}$ $\frac{9.1}{10}$ $\frac{9.1}{7}$ 8.8 $\frac{9.0}{15}$ $\frac{9.2}{18}$ $\frac{7.5}{23}$ $\frac{7.8}{51}$ $\frac{12.8}{100}$

$\frac{15.0}{100}$ $\frac{13.4}{12}$ $\frac{10.4}{7}$ 10.0 $\frac{10.1}{15}$ $\frac{10.0}{16}$ $\frac{13.2}{21}$ $\frac{12.6}{23}$ $\frac{13.8}{100}$

$\frac{6.7}{100}$ $\frac{11.3}{64}$ $\frac{9.5}{19}$ $\frac{8.7}{15}$ $\frac{9.4}{10}$ $\frac{8.8}{7}$ 8.5 $\frac{8.6}{14}$ $\frac{9.2}{18}$ $\frac{7.5}{24-31}$ $\frac{6.6}{79}$ $\frac{6.2}{100}$

$\frac{35}{100}$ $\frac{42}{35}$ $\frac{4.1}{12}$ $\frac{5.3}{7}$ 4.8 $\frac{5.0}{14}$ $\frac{5.5}{17}$ $\frac{4.8}{19}$ $\frac{4.4}{24}$ $\frac{5.2}{28}$ $\frac{6.1}{56}$ $\frac{5.5}{100}$

$\frac{2.4}{100}$ $\frac{2.1}{20}$ $\frac{3.7}{13}$ $\frac{3.5}{7}$ 3.6 $\frac{3.8}{14}$ $\frac{4.3}{18}$ $\frac{3.8}{21}$ $\frac{4.1}{36}$ $\frac{6.0}{78}$ $\frac{5.4}{100}$

Top Mnt Sta 29+18.33

$\frac{16}{100}$ $\frac{3.7}{13}$ $\frac{4.5}{11}$ $\frac{4.2}{8}$ 4.1 $\frac{4.4}{14}$ $\frac{4.2}{17}$ $\frac{4.6}{18-23}$ $\frac{4.3}{32}$ $\frac{5.1}{34}$ $\frac{5.9}{78}$ $\frac{5.7}{54}$

Floor Ht 0.25

$\frac{2.6}{78}$ $\frac{3.1}{52}$ $\frac{4.8}{8}$ 4.8 $\frac{5.2}{14}$ $\frac{6.0}{21}$ $\frac{7.1}{37}$ $\frac{9.9}{80}$ $\frac{10.2}{100}$

Pt 2

$\frac{2.4}{100}$ $\frac{4.2}{48}$ $\frac{6.7}{14}$ $\frac{6.0}{9}$ 5.9 $\frac{6.5}{12}$ $\frac{6.7}{14}$ $\frac{7.3}{17}$ $\frac{11.0}{76}$ $\frac{12.1}{77-79}$ $\frac{11.2}{80-100}$

Nail in Road Sta 32+00

Sta	+	π	-
		962.48	

32+99	16'x40 CM.	54.6 ✓
-------	------------	--------

33		54.6 ✓
----	--	--------

34		55.0 ✓
----	--	--------

35		56.0 ✓
----	--	--------

+50		56.3 ✓
-----	--	--------

36		55.9 ✓
----	--	--------

37		54.2 ✓
----	--	--------

+5A	12" x 24' CM.	54.1 ✓
-----	---------------	--------

38		54.0 ✓
----	--	--------

$$\frac{32+99.16 \times 40}{19-21} \text{ CM}$$

$$\begin{array}{cccccccccccccccc} & & \text{FL.2} & & & & & & \text{FL.2} & \text{D/2} & & & & & & & \\ \frac{10.6}{100} & \frac{11.36}{19} & \frac{8.3}{13} & \frac{8.2}{7} & 7.9 & \frac{8.4}{11} & \frac{9.1}{16} & \frac{11.42}{21} & \frac{11.8}{21} & \frac{10.6}{26} & \frac{9.8}{75} & \frac{8.7}{100} \end{array}$$

$$7.9$$

$$\frac{7.9}{100} \frac{8.9}{52} \frac{8.1}{31} \frac{8.5}{14} \frac{7.9}{11} \frac{7.8}{9} 7.5 \frac{7.7}{13} \frac{7.4}{14} \frac{8.1}{17} \frac{7.6}{22} \frac{4.0}{28} \frac{3.4}{100}$$

$$\frac{2.8}{100} \frac{6.4}{10} \frac{6.7}{7} 6.5 \frac{6.7}{14} \frac{5.9}{29} \frac{3.1}{100}$$

$$\frac{2.1}{100} \frac{2.2}{33} \frac{4.5}{10} \frac{6.2}{6} 6.2 \frac{6.7}{3} \frac{6.0}{15} \frac{5.4}{25} \frac{6.3}{79} \frac{5.6}{100}$$

$$\frac{2.1}{100} \frac{3.4}{39} \frac{4.8}{16} \frac{6.4}{12} \frac{6.8}{10} 6.6 \frac{7.0}{10} \frac{5.8}{11} \frac{4.8}{21} \frac{8.2}{100}$$

$$\frac{10.5}{100} \frac{10.8}{59} \frac{9.6}{15} \frac{8.4}{11} 8.3 \frac{8.6}{11} \frac{9.0}{14} \frac{9.7}{11} \frac{9.8}{100}$$

$$\begin{array}{cccccccccccc} & & & & & & & \text{FL.2} & & & & & \\ \frac{12.4}{100} & \frac{12.2}{43} & \frac{11.1}{12} & \frac{11.90}{12} & \frac{9.0}{11} & 8.4 & \frac{8.8}{10-12} & \frac{11.65}{12} & \frac{11.2}{14} & \frac{11.8}{55} & \frac{11.0}{100} \end{array}$$

$$\frac{13.3}{100} \frac{12.14}{59} \frac{10.8}{14} \frac{9.3}{11} \frac{9.0}{10} 8.5 \frac{8.6}{10} \frac{9.7}{12} \frac{9.4}{14-65} \frac{9.7}{100}$$

Sta	+	π	-	
		962.48		
39				54.3 ✓
○	2.29	956.95 ✓	7.82	954.66 ✓
40				54.7 ✓
41				53.2 ✓
42				51.3 ✓
43				49.3 ✓
B.M.	6.60	953.13 ✓	10.42	946.53 ✓
	+25			48.9 ✓
44				48.4 ✓
45				48.0 ✓

$\frac{13.1}{100}$ $\frac{12.4}{73}$ $\frac{10.9}{16}$ $\frac{8.7}{10}$ 8.2 $\frac{8.4}{12}$ $\frac{7.7}{13}$ $\frac{6.1}{17}$ $\frac{3.8}{38}$ $\frac{4.7}{100}$

Nail Sta 40+00

$\frac{6.4}{100}$ $\frac{2.8}{18-11}$ 2.3 $\frac{2.5}{12}$ $\frac{1.7}{15}$ $\frac{0.8}{18}$ $\frac{0.3}{27}$ $\frac{0.0}{46}$ $\frac{0.0}{100}$

$\frac{5.7}{100}$ $\frac{5.2}{77}$ $\frac{3.9}{15}$ $\frac{4.8}{13}$ $\frac{4.2}{11}$ 3.8 $\frac{4.2}{13}$ $\frac{3.0}{17}$ $\frac{1.0}{100}$

$\frac{6.8}{100}$ $\frac{4.9}{57}$ $\frac{4.8}{22}$ $\frac{4.6}{15}$ $\frac{6.0}{13}$ 5.7 $\frac{6.2}{13}$ $\frac{5.0}{16}$ $\frac{1.6}{100}$

$\frac{8.4}{100}$ $\frac{8.2}{23}$ $\frac{7.6}{17}$ $\frac{8.8}{15-11}$ $\frac{8.0}{7}$ 7.7 $\frac{7.9}{15}$ $\frac{8.1}{20}$ $\frac{7.9}{23}$ $\frac{7.1}{74}$ $\frac{5.2}{100}$

Spk in T.P. Lt. Sta 43+65

$\frac{5.9}{100}$ $\frac{7.2}{46}$ $\frac{6.2}{12}$ $\frac{4.7}{6}$ 4.2 $\frac{4.3}{15}$ $\frac{4.4}{18}$ $\frac{5.0}{20-27}$ $\frac{4.2}{29}$ $\frac{3.7}{61}$ $\frac{0.5}{100}$

$\frac{9.3}{100}$ $\frac{8.5}{27}$ $\frac{8.0}{11}$ $\frac{5.0}{6}$ 4.7 $\frac{4.6}{15}$ $\frac{5.9}{19-29}$ $\frac{5.5}{32}$ $\frac{3.9}{100}$

$\frac{4.7}{100}$ $\frac{6.4}{57}$ 5.0 $\frac{8.3}{22}$ $\frac{7.3}{10}$ $\frac{5.5}{7}$ 5.1 $\frac{5.2}{15}$ $\frac{6.2}{17}$ $\frac{5.5}{38}$ $\frac{5.2}{72}$ $\frac{3.3}{100}$

Sta

+

π

-

953.13

46

47.8 ✓

47

48.0 ✓

+50

48.3 ✓

48

48.5 ✓

B.M.

454

948.59 ✓

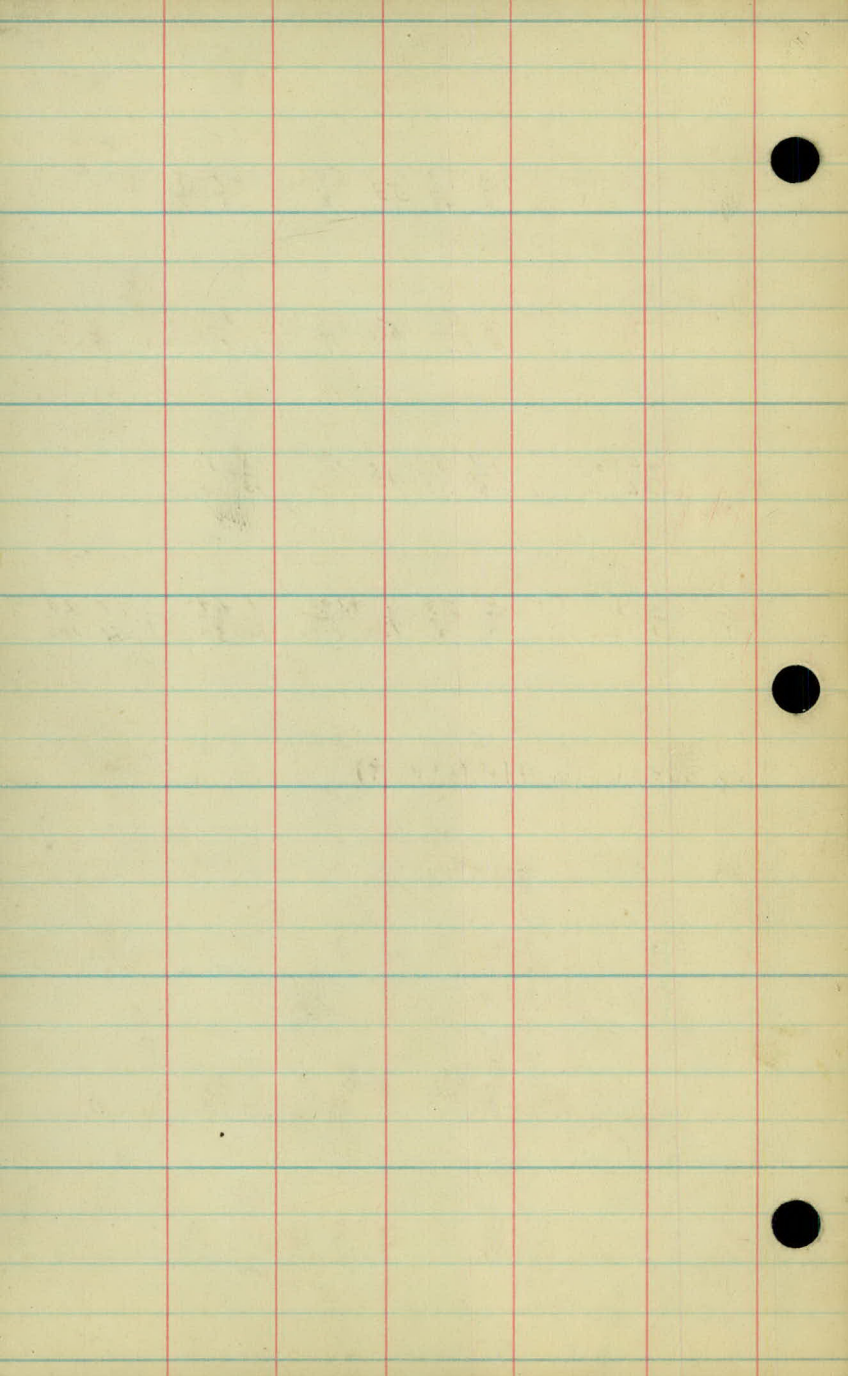
$$\frac{6.0}{100} \quad \frac{6.4}{58} \quad \frac{7.0}{52} \quad \frac{5.7}{14} \quad \frac{5.3}{9} \quad \frac{5.6}{13} \quad \frac{6.4}{15} \quad \frac{6.7}{19} \quad \frac{8.7}{100}$$

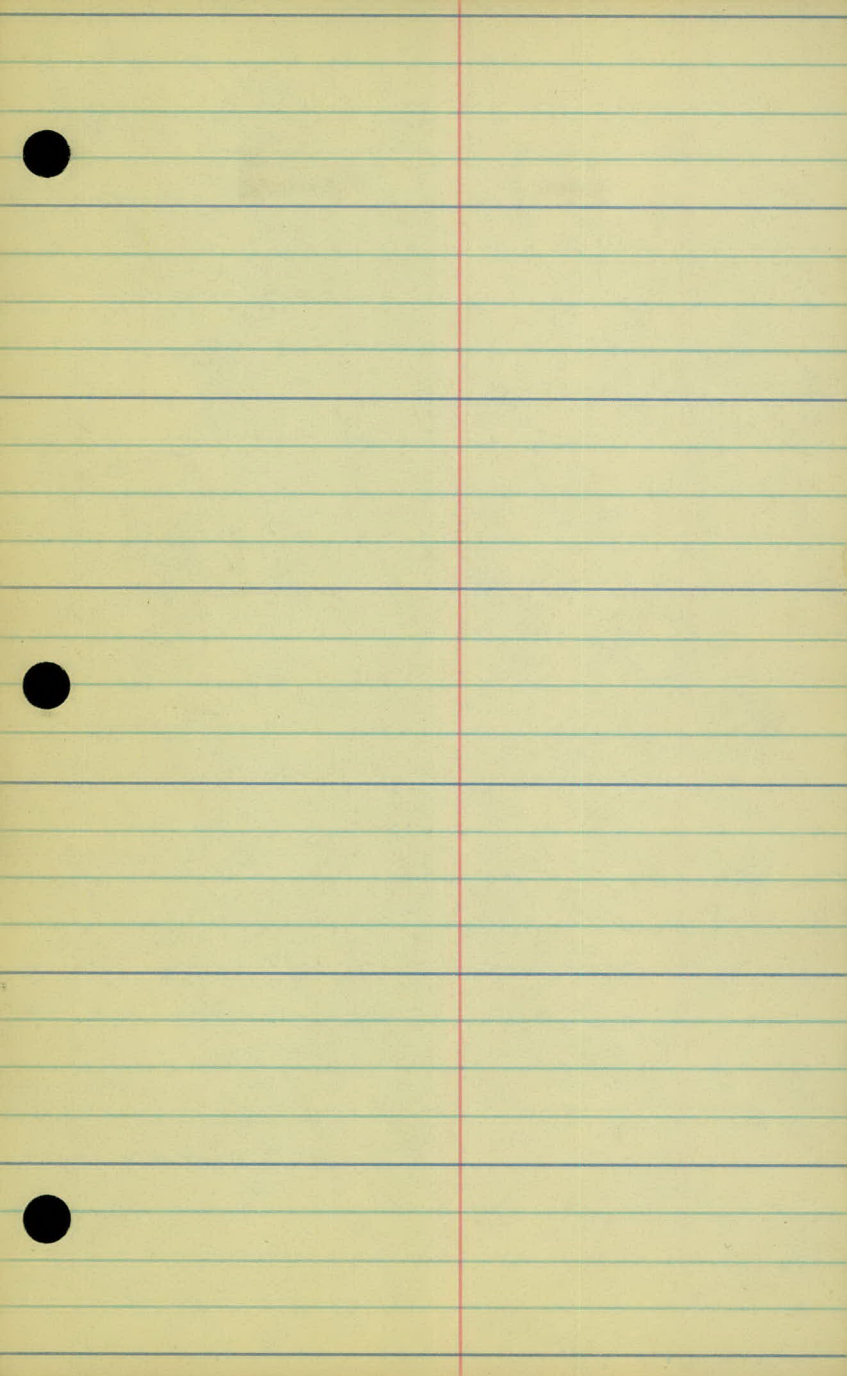
$$\frac{4.8}{100} \quad \frac{6.2}{71} \quad \frac{5.5}{18} \quad \frac{6.2}{16} \quad \frac{5.2}{11} \quad 5.1 \quad \frac{5.6}{11} \quad \frac{8.1}{15} \quad \frac{9.1}{45-100}$$

$$\frac{4.2}{62} \quad \frac{3.3}{21} \quad \frac{5.8}{17} \quad \frac{5.7}{15} \quad \frac{5.0}{13} \quad 4.8 \quad \frac{5.1}{10-12} \quad \frac{9.8}{43} \quad \frac{10.0}{100}$$

$$\frac{6.6}{100} \quad \frac{6.4}{89} \quad \frac{3.2}{22} \quad \frac{5.4}{18} \quad \frac{5.6}{16} \quad \frac{5.3}{13} \quad 4.6 \quad \frac{4.7+6}{10 \quad 13} \quad \frac{2.4}{18} \quad \frac{2.4}{30} \quad \frac{8.1}{49} \quad \frac{9.7}{57} \quad \frac{9.3}{100}$$

Top SpK & Sta 47+89 (POT)





Sta	+	π	-	
	6.95	953.48		946.53
49			42.6 -	
50			46.8 -	
+50			46.2 -	
51			45.4 -	
①	1.62	948.46	6.64	941.84
52			43.9 -	
53			42.8 -	
54			42.7 -	
55			43.3 -	
56			44.0 -	
57			43.4 -	

RR SpK in TP Lt. Sta. 43+65

$$\frac{8.9}{100} \frac{4.5}{18} \frac{6.5}{17-14} 5.9 \frac{6.0}{14} \frac{4.8}{17} \frac{8.8}{53} \frac{11.9}{100}$$

$$\frac{8.2}{100} \frac{6.1}{25} \frac{8.1}{17} \frac{7.0}{11} 6.7 \frac{7.1}{14} \frac{8.1}{18} \frac{5.4}{30} \frac{8.9}{100}$$

$$\frac{5.5}{100} \frac{6.0}{37} 29 \frac{10.4}{15} \frac{7.9}{10} 7.3 \frac{7.6}{13} \frac{8.0}{35} \frac{9.6}{67-100}$$

$$\frac{2.6}{100} \frac{5.5}{50} \frac{6.3}{25} \frac{9.1}{15} \frac{8.3}{11} 8.1 \frac{8.7}{13} \frac{9.9}{33} \frac{9.6}{100}$$

Top Rock Lt Sta 51+30

$$\frac{43.0}{100} \frac{0.0}{85} \frac{2.3}{50} \frac{4.4}{32} \frac{6.5}{20} \frac{6.2}{13} \frac{5.0}{10} 46 \frac{5.2}{12} \frac{6.4}{47} \frac{8.4}{100}$$

$$\frac{5.9}{100} \frac{6.9}{46} \frac{7.9}{42} \frac{8.2}{13} \frac{6.1}{10} 5.7 \frac{6.1}{11} \frac{8.9}{14-75} \frac{7.0}{125}$$

F.L. 8.4

F.L. 8.8

$$\frac{5.5}{100} \frac{6.6}{50} \frac{8.2}{25} \frac{7.1}{13} \frac{6.1}{10} 5.8 \frac{6.3}{11} \frac{7.3}{16} \frac{8.5}{54} \frac{9.6}{100}$$

$$\frac{2.8}{100} \frac{3.3}{64} \frac{5.4}{17} \frac{6.1}{15} \frac{5.5}{11} 5.2 \frac{5.6}{12} \frac{6.4}{38} \frac{10.6}{100}$$

$$\frac{3.6}{106} \frac{3.9}{52} \frac{3.5}{19} \frac{5.3}{14} \frac{5.0}{12} 41.5 \frac{4.9}{12} \frac{5.5}{17} \frac{4.8}{22} \frac{8.0}{65} \frac{11.5}{100}$$

F.L. 7.3

43.5

43.3

F.L. 8.3

40.2

31.9

32.9

$$\frac{5.1}{100} \frac{7.0}{31} \frac{6.0}{16} \frac{5.6}{12} 5.1 \frac{5.4}{10} \frac{6.3}{14-19} \frac{5.0}{30} \frac{6.9}{72} \frac{10.0}{100}$$

Sta + K -
948.46

58 42.8 -

BM. 3.83 947.93 4.36 944.10

+10 Road Rt. E levels 42.7 -

57 +65 42.7 -

59 42.6 -

60 42.6 -

61 41.7 -

① 2.20 945.73

$\frac{7.1}{100}$ $\frac{6.0}{21}$ $\frac{6.8}{19}$ $\frac{5.7}{17-12}$ 5.7 $\frac{6.4}{10}$ $\frac{7.2}{25-55}$ $\frac{5.9}{100}$

R.R. SpKin 10" Stp 45' Rt Stg 57+20

$\frac{42.7}{5.2}$ $\frac{41.6}{6.3}$ $\frac{41.0}{6.9}$ $\frac{37.3}{10.6}$ $\frac{36.9}{11.0}$ $\frac{36.1}{11.5}$ $\frac{36.7}{11.2}$ $\frac{37.5}{10.4}$

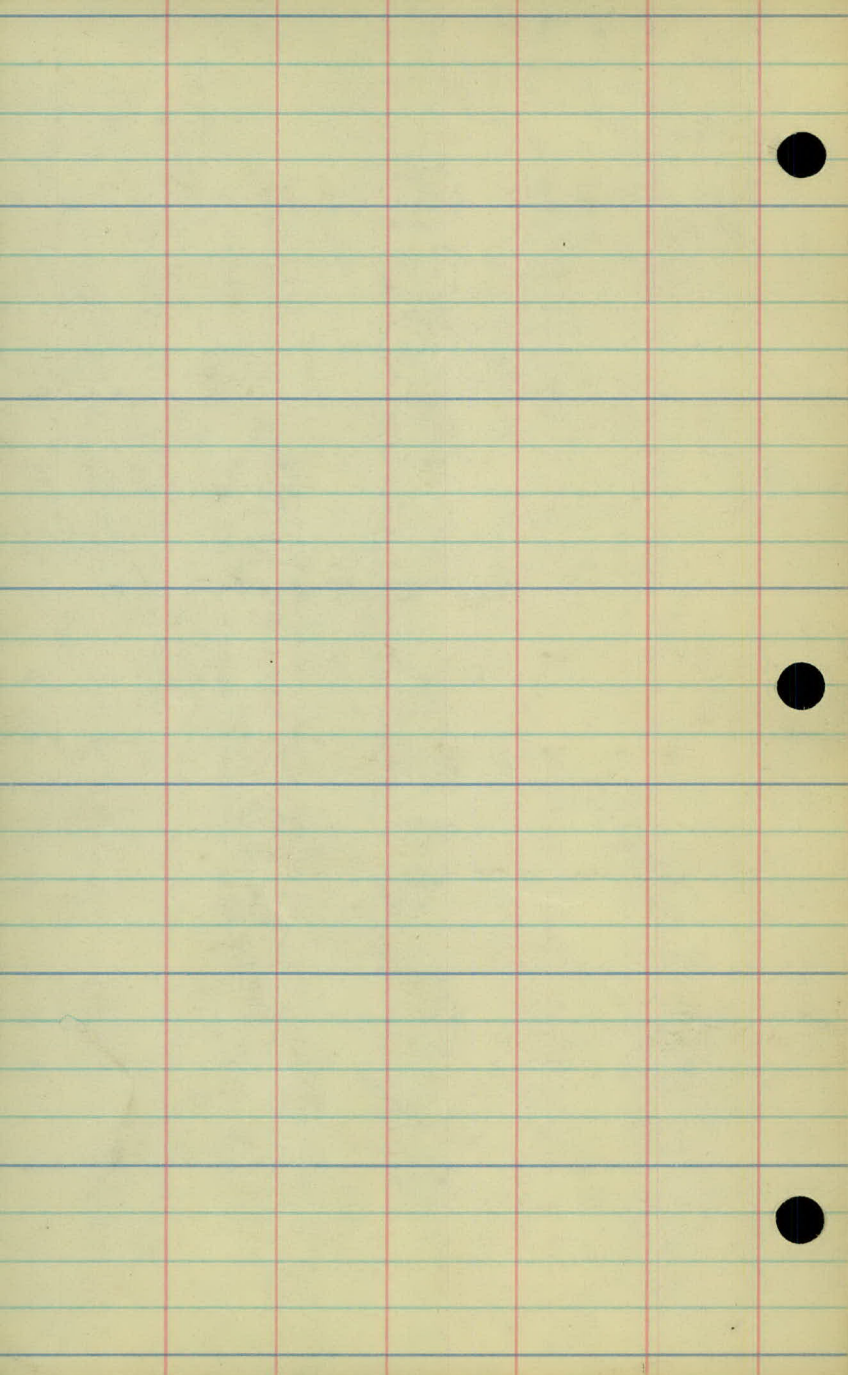
$\frac{3.0}{100}$ $\frac{5.3}{36}$ $\frac{6.3}{20}$ $\frac{5.5}{15}$ 5.2 $\frac{5.6}{7}$ $\frac{5.9}{12}$ $\frac{5.2}{15}$ $\frac{6.7}{68}$ $\frac{9.6}{94}$ $\frac{9.7}{100}$ $\frac{10.1}{120}$

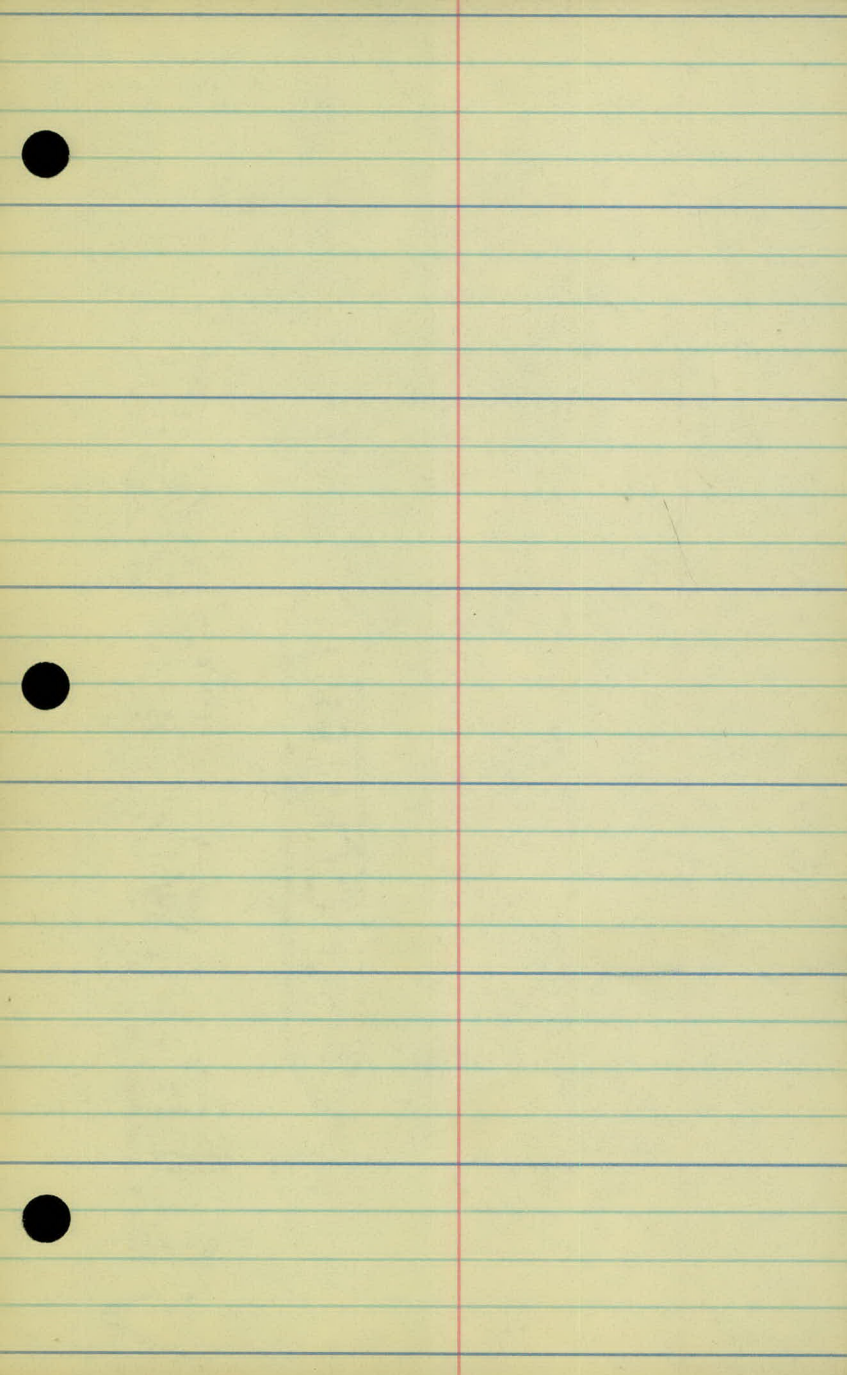
$\frac{1.0}{100}$ $\frac{5.5}{29}$ $\frac{5.6}{16}$ 5.3 $\frac{5.8}{8}$ $\frac{6.5}{10}$ $\frac{8.6}{45}$ $\frac{11.8}{61}$ $\frac{11.4}{60}$ $\frac{16.0}{100}$

$\frac{41.0}{18}$ $\frac{0.6}{51}$ $\frac{3.4}{31}$ $\frac{4.2}{20}$ $\frac{5.5}{15}$ 6.3 $\frac{5.8}{8}$ $\frac{7.0}{16}$ $\frac{12.0}{22}$ $\frac{18.0}{100}$

$\frac{2.6}{100}$ $\frac{4.8}{60}$ $\frac{5.4}{32}$ $\frac{6.1}{18}$ $\frac{6.0}{11}$ 6.2 $\frac{6.6}{11}$ $\frac{9.7}{18}$ $\frac{11.2}{31}$ $\frac{11.7}{41}$ $\frac{16.0}{100}$

Nail in T.P. Rt Stg. 64





0

6.78

952.51 ✓

945.73 ✓

62

42.6

63

44.7

64

48.2

0

12.57

964.53 ✓

0.55

951.96 ✓

65

52.7

66

56.7

67

58.5

+40

58.7

+564 Culv

68

58.9

0

7.44

969.56 ✓

2.39

962.14 ✓

Nail in T.P. Rt. Sta. 64+00

$\frac{6.0}{100}$ $\frac{9.9}{60}$ $\frac{11.0}{18}$ $\frac{10.4}{10}$ $\frac{9.9}{11}$ $\frac{10.2}{11}$ $\frac{10.8}{14}$ $\frac{14.0}{22}$ $\frac{16.7}{67}$ -100

F.L. Culy 11.9

+89
 $\frac{12 \times 266M}{10-16}$

F.L. Culy 12.7

$\frac{7.0}{100}$ $\frac{8.8}{54}$ $\frac{9.2}{23}$ $\frac{8.4}{7}$ $\frac{7.8}{12}$ $\frac{8.0}{25}$ $\frac{8.3}{91}$ $\frac{7.0}{67}$ $\frac{6.2}{100}$

$\frac{5.4}{100}$ $\frac{5.9}{57}$ $\frac{5.6}{22}$ $\frac{5.1}{13}$ $\frac{4.3}{12}$ $\frac{4.5}{16}$ $\frac{4.7}{19-23}$ $\frac{5.4}{25}$ $\frac{4.6}{35}$ $\frac{3.3}{35}$

$\frac{1.3}{100}$

Top Stk Rt. Sta 64+85.63

$\frac{10.1}{100}$ $\frac{7.9}{73}$ $\frac{9.9}{20}$ $\frac{12.1}{11}$ $\frac{11.8}{12}$ $\frac{12.3}{17}$ $\frac{11.8}{22}$ $\frac{9.7}{38}$ $\frac{9.9}{100}$

$\frac{8.3}{100}$ $\frac{6.6}{62}$ $\frac{7.0}{19}$ $\frac{8.2}{11}$ $\frac{7.8}{12}$ $\frac{8.0}{18}$ $\frac{7.9}{24}$ $\frac{5.6}{44}$ $\frac{6.0}{44}$ $\frac{12.3}{100}$

$\frac{7.9}{100}$ $\frac{7.6}{60}$ $\frac{6.7}{22}$ $\frac{6.5}{19}$ $\frac{6.0}{13}$ $\frac{6.2}{9}$ $\frac{6.9}{16}$ $\frac{5.9}{20}$ $\frac{8.7}{67}$ $\frac{11.2}{100}$

$\frac{8.0}{100}$ $\frac{8.1}{62}$ $\frac{7.7}{15}$ $\frac{6.4}{12}$ $\frac{5.8}{11}$ $\frac{6.1}{16}$ $\frac{9.7}{56}$ $\frac{10.2}{100}$ $\frac{8.9}{100}$

F.L. 8.7

F.L. Culy 9.2

$\frac{3.3}{100}$ $\frac{7.7}{58}$ $\frac{6.4}{20}$ $\frac{5.6}{13}$ $\frac{5.9}{9}$ $\frac{7.2}{15}$ $\frac{6.4}{20}$ $\frac{6.5}{59}$ $\frac{5.5}{100}$

T.P. Rt. Sta 70+60

Sta + π ✓ -
 969.58

69 60.1

70 61.7

71 62.9

72 64.3

 +55 64.5

 4
 80'
 ↓
 73 + 35 See line revision 1017 64.6

 4
 100'
 ↓
 74 + 35 63.7

B.M. 5.36 964.22 ✓

75 62.8

76 62.7

77 63.1

+50 63.9

$\frac{9.1}{100}$ $\frac{11.1}{65}$ $\frac{10.5}{22}$ $\frac{9.9}{13}$ 9.5 $\frac{9.8}{10}$ $\frac{12.6}{15-100}$

$\frac{7.0}{100}$ $\frac{8.9}{53}$ $\frac{7.9}{35}$ $\frac{8.3}{23}$ $\frac{8.1}{11}$ 7.9 $\frac{8.1}{12}$ $\frac{8.3}{17}$ $\frac{7.6}{38}$ $\frac{7.2}{100}$

$\frac{6.9}{100}$ $\frac{8.8}{47}$ $\frac{9.0}{14}$ $\frac{7.4}{11}$ 6.7 $\frac{7.1}{11}$ $\frac{7.4}{19}$ $\frac{5.6}{47}$ $\frac{6.3}{100}$

$\frac{+5.0}{100}$ $\frac{0.0}{50}$ $\frac{4.3}{17}$ $\frac{5.9}{15}$ $\frac{5.2}{10}$ 5.5 $\frac{5.6}{10-14}$ $\frac{1.5}{21}$ $\frac{1.7}{44}$ $\frac{7.2}{100}$

$\frac{+5.0}{100}$ $\frac{0.3}{55}$ $\frac{3.5}{35}$ $\frac{4.9}{17}$ $\frac{5.9}{13}$ 5.1 $\frac{5.3}{12}$ $\frac{6.6}{18}$ $\frac{8.2}{37}$ $\frac{8.7}{83-100}$

$\frac{0.0}{100}$ $\frac{1.3}{53}$ $\frac{3.3}{19}$ $\frac{3.9}{14}$ 5.0 $\frac{5.1}{13}$ $\frac{6.9}{27}$ $\frac{10.0}{75}$ $\frac{11.3}{100}$

$\frac{1.3}{100}$ $\frac{4.3}{100}$ $\frac{5.2}{17}$ $\frac{6.3}{16}$ $\frac{6.5}{12}$ 5.9 $\frac{6.3}{13}$ $\frac{7.0}{18}$ $\frac{5.9}{23}$ $\frac{7.0}{58}$ $\frac{13.0}{100}$

R.R. Spk 15" Oak 40' Rt Stg 73+90

$\frac{0.3}{100}$ $\frac{5.2}{38}$ $\frac{6.2}{18}$ $\frac{7.2}{16}$ $\frac{7.0}{11}$ 6.8 $\frac{7.4}{14}$ $\frac{12.0}{24}$ $\frac{11.4}{100}$

$\frac{+6.0}{100}$ $\frac{0.0}{50}$ $\frac{3.7}{24}$ $\frac{7.5}{20}$ $\frac{7.0}{12}$ 6.9 $\frac{7.3}{10}$ $\frac{9.0}{18}$ $\frac{13.2}{55}$ $\frac{15.6}{100}$

$\frac{+4.0}{100}$ $\frac{0.0}{56}$ $\frac{5.6}{43}$ $\frac{7.0}{26}$ $\frac{8.0}{23}$ $\frac{6.7}{13}$ 6.5 $\frac{7.0}{9}$ $\frac{11.5}{21}$ $\frac{15.3}{80}$ $\frac{17.0}{100}$

F.L. 8.2 +22 C.O. F.L. 10.8

$\frac{9.0}{100}$ $\frac{3.0}{85}$ $\frac{3.4}{54}$ $\frac{6.8}{33}$ $\frac{6.7}{22}$ 5.7 $\frac{5.7}{14}$ $\frac{6.7}{10}$ $\frac{12.1}{20}$ $\frac{16.5}{58}$ $\frac{20.0}{100}$

Sta

+

π

-

✓
969.58

78

65.2

0

12.35

✓
977.82

4.11

✓
965.47

79

69.1

+30

69.5

↑
113'

↓

80+ 43

65.7

⊙

13.36

✓
964.46

$\frac{3.3}{100}$	$\frac{4.3}{75}$	$\frac{3.8}{28}$	$\frac{5.2}{23}$	$\frac{4.3}{10}$	4.4	$\frac{5.0}{8}$	$\frac{5.7}{13}$	$\frac{6.7}{19}$	$\frac{10.2}{45}$	$\frac{12.6}{75}$	$\frac{20.5}{100}$
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Nail in T.P. Rd. Sta 78+10

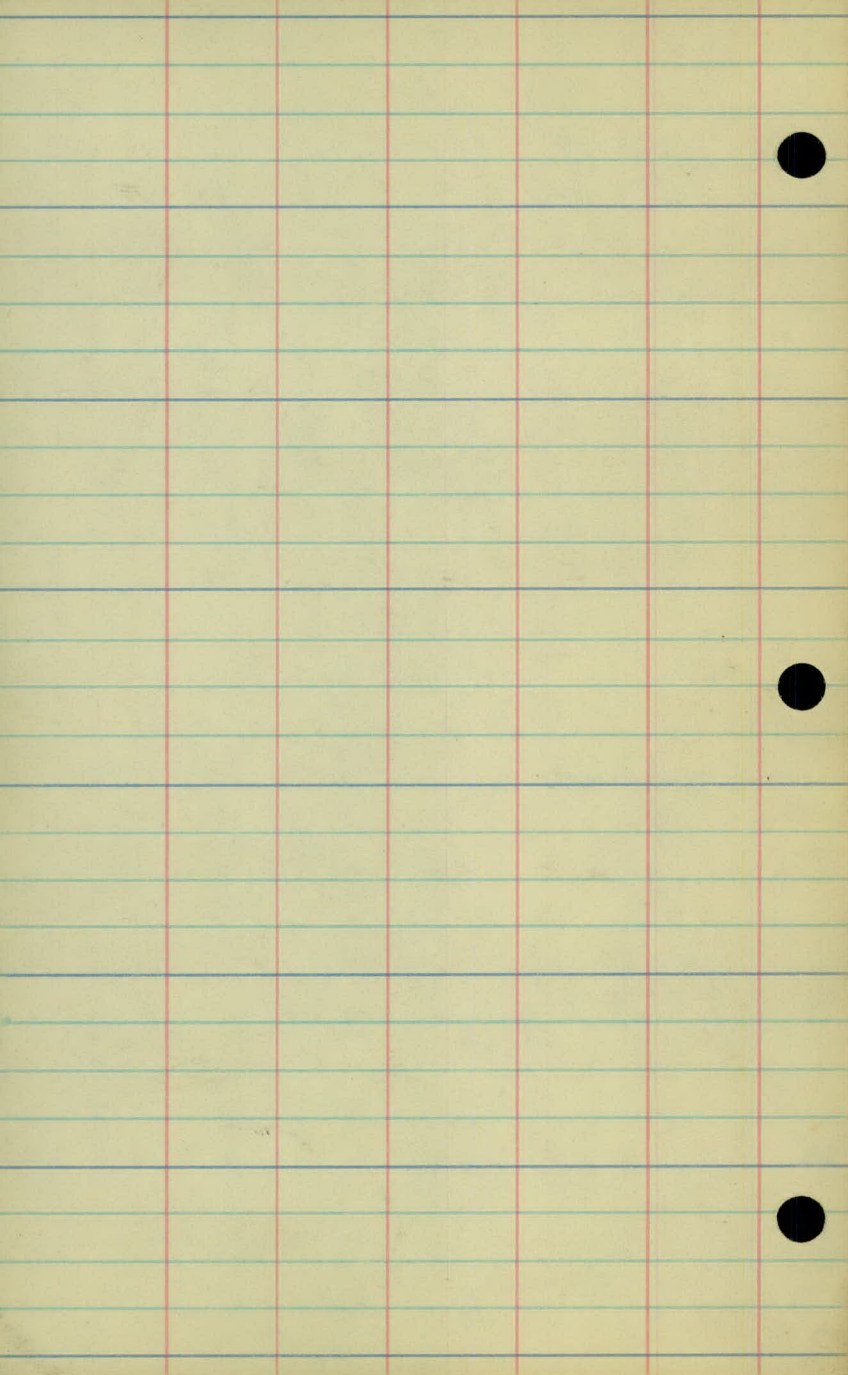
Floor Hoz

$\frac{1.9}{91}$	$\frac{3.8}{90}$	$\frac{4.8}{49}$	$\frac{5.4}{20}$	$\frac{7.2}{15}$	8.7	$\frac{9.0}{10}$	$\frac{3.4}{18}$	$\frac{4.3}{23}$	$\frac{7.4}{100}$
------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	-------------------

$\frac{4.3}{100}$	$\frac{5.0}{65}$	$\frac{5.6}{18}$	$\frac{8.4}{13}$	8.3	$\frac{8.8}{11}$	$\frac{2.5}{19}$	$\frac{1.7}{52}$	$\frac{4.0}{81}$	$\frac{8.1}{100}$	$\frac{33.1}{150}$
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$\frac{8.5}{100}$	$\frac{8.1}{67}$	$\frac{9.8}{42}$	$\frac{11.5}{15}$	$\frac{12.3}{13}$	12.1	$\frac{12.8}{16}$	$\frac{12.0}{17}$	$\frac{13.2}{31}$	$\frac{12.9}{51}$	$\frac{11.8}{76}$	$\frac{13.8}{100}$
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Top So End Culv @ Ent to School Yard Ht



May 2, 1936

Sta + A -

B.M. 5.70 770.16 964.46

81 +64 60.9

82 59.4

+60 57.6

① 147 958.65 12.98 957.18

+82 57.3

83 56.8

84 55.3

85 53.7

86 53.9

+90 54.4

Top 50 End Cule @ School Ho Wards

1.3 9.4 9.3 9.3 10.3 9.5 11.2 12.6 16.0
111-38 21 11 10 13 20 80 100

1.3 10.2 10.7 10.8 11.6 12.1 14.7 20.5 23.5
100-43 26 16 11 15 19 53 100

2.5 12.4 12.8 12.6 13.0 13.7 15.6 24.0 25.1
110-52 30 12 10 14 19 72 100

5.0 4.9 3.3 2.5 1.8 1.4 1.2 2.3 3.5 5.5 10.5 12.2
100 82 44 17 12 10 15 18 41 67 100

5.4 4.2 2.2 1.4 2.2 2.9 4.6 5.1 9.9 12.4
110 18 11 11 16 20 38 60 100

6.5 6.2 4.3 3.5 3.4 3.8 5.1 9.7 12.8
100 67 15 12 12 29 55 100

3.5 1.5 3.7 5.7 5.9 5.2 5.0 5.7 9.4 16.1 13.0
100 55 37 22 16 13 11 18 54 100

Floor Ho 00.

F.L. 6.4

F.L. 8.2

5.0 4.4 5.4 6.0 5.2 4.8 5.3 6.7 6.9 9.4 11.0
100 47 20 17 13 10 14 42 63 100

3.4 2.4 5.2 4.7 4.3 4.7 2.1 3.5 9.3 10.3
100-73 21 18 13 11-14 19 43 75 100

958.65

87

54.2

+15 $\pm$ Co Rd E Lt

54.0

+32

+39

+67

+78

+85 $\pm$ E. Bound Trk.

+95 $\pm$ Double Trk Taken on Ballast

88 +05 $\pm$ W Bound Trk

88 + 15

B.M.

321

955.44

+28

$$\frac{6.0}{100} \quad \frac{5.4}{31} \quad \frac{4.6}{14} \quad 4.5 \quad \frac{4.8}{11-17} \quad \frac{2.0}{19} \quad \frac{4.3}{46} \quad \frac{9.5}{79} \quad \frac{10.3}{100}$$

$$\frac{5.8}{100} \quad \frac{5.1}{70} \quad \frac{4.8}{15} \quad 4.7 \quad \frac{5.0}{11} \quad \frac{5.3}{36} \quad \frac{8.2}{100}$$

$$\frac{6.0}{100} \quad \frac{5.8}{31} \quad \frac{5.1}{14} \quad 5.0 \quad \frac{5.5}{12} \quad \frac{3.3}{15} \quad \frac{4.3}{47} \quad \frac{7.6}{59} \quad \frac{9.0}{100}$$

$$\frac{3.9}{100} \quad \frac{4.0}{31} \quad \frac{6.0}{26} \quad \frac{5.3}{14} \quad 5.1 \quad \frac{5.6}{12} \quad \frac{3.4}{15} \quad \frac{4.4}{47} \quad \frac{7.6}{62} \quad \frac{8.8}{100}$$

$$100 - \frac{7.3}{66} \quad \frac{4.0}{41} \quad \frac{3.0}{23} \quad \frac{6.0}{16} \quad 5.6 \quad \frac{5.9}{10} \quad \frac{3.8}{13} \quad \frac{4.2}{38} \quad \frac{8.7}{68-100}$$

RR Atch, RR Ditch

$$\frac{7.5}{100} \quad \frac{6.1}{54} \quad 100 - \frac{6.5}{66} \quad \frac{6.3}{13} \quad 5.8 \quad \frac{6.1}{10} \quad \frac{7.0}{42} \quad \frac{8.7}{100}$$

$$\frac{52.65}{6.00 \text{ T/R}}$$

$$100 - \frac{6.4}{65} \quad \frac{6.6}{14} \quad \frac{6.1}{10} \quad 6.1 \quad \frac{6.2}{12} \quad \frac{6.8}{16} \quad \frac{7.0}{100}$$

$$5.90 \text{ T/R}$$

F.L. Colly

$$\frac{7.7}{100} \quad \frac{7.4}{69} \quad \frac{9.0}{23} \quad \frac{6.3}{19} \quad \frac{5.7}{10} \quad 5.9 \quad \frac{6.6}{11} \quad \frac{9.0}{13} \quad \frac{8.5}{100}$$

F.L. Colly

Top NW. Anchor Bolt on RR. W. Wag Pier

$$100 - \frac{4.3}{57} \quad \frac{4.8}{20} \quad \frac{6.2}{14} \quad \frac{5.7}{12} \quad 5.8 \quad \frac{6.5}{10-13} \quad \frac{4.9}{18} \quad \frac{5.2}{41} \quad \frac{8.4}{65}$$

958.65

88 + 55

+75

± Co. Rd E Rt.

①

8.60 965.56 1.69

956.96

↑

89

Liize Revision

55.8

90

59.5

91

59.9

92

59.7

93

59.6

94

61.6

95

62.8

96

61.7

97

61.2

$$\frac{4.1}{100-63} \quad \frac{3.4}{16} \quad \frac{5.5}{11} \quad 5.4 \quad \frac{5.7}{12} \quad \frac{6.9}{97} \quad \frac{10.1}{100}$$

$$\frac{4.5}{100} \quad \frac{3.8}{53} \quad \frac{1.4}{17} \quad \frac{4.8}{12} \quad 4.1 \quad \frac{5.0}{12} \quad \frac{5.8}{40} \quad \frac{6.9}{100}$$

Top RR Spk & Sta. 89+22.55

$$\frac{11.1}{100} \quad \frac{10.0}{63} \quad \frac{6.5}{17} \quad \frac{10.2}{11} \quad 9.8 \quad \frac{10.6}{13} \quad \frac{12.1}{21} \quad \frac{11.4}{49} \quad \frac{16.5}{100}$$

X

$$\frac{9.3}{100} \quad \frac{4.9}{29} \quad \frac{5.4}{14} \quad \frac{6.3}{10} \quad 6.1 \quad \frac{6.7}{11} \quad \frac{6.0}{20} \quad \frac{7.4}{64} \quad \frac{8.6}{80} \quad \frac{9.2}{100}$$

Kf. House = 4.18

$$\frac{3.8}{100} \quad \frac{4.8}{80} \quad \frac{6.6}{14} \quad \frac{6.2}{12} \quad 5.7 \quad \frac{6.1}{11} \quad \frac{7.1}{17} \quad \frac{7.1}{62} \quad \frac{10.4}{100}$$

Floor Ht. 0.2

$$\frac{5.4}{100} \quad 4.2 \quad \frac{6.2}{13} \quad 5.9 \quad \frac{6.3}{11} \quad \frac{7.4}{16} \quad \frac{7.0}{41} \quad \frac{5.3}{100}$$

$$\frac{5.6}{100} \quad \frac{8.4}{58} \quad \frac{9.2}{36} \quad \frac{8.1}{18} \quad \frac{6.3}{11} \quad 6.0 \quad \frac{6.5}{11} \quad \frac{7.5}{16} \quad \frac{7.3}{60} \quad \frac{5.6}{100} \quad 6.$$

$$\frac{7.9}{100} \quad \frac{6.0}{29} \quad \frac{4.5}{21} \quad \frac{4.3}{10} \quad 4.0 \quad \frac{4.3}{11} \quad \frac{3.5}{15} \quad \frac{4.2}{38} \quad \frac{7.0}{45} \quad \frac{6.0}{100}$$

$$\frac{3.1}{100} \quad \frac{2.5}{51} \quad \frac{1.8}{13} \quad \frac{3.3}{10} \quad 2.8 \quad \frac{3.0}{11} \quad \frac{1.3}{15} \quad \frac{6.0}{33} \quad \frac{7.8}{100}$$

$$\frac{7.4}{100} \quad \frac{5.4}{65} \quad \frac{3.8}{14} \quad \frac{4.2}{11} \quad 3.9 \quad \frac{4.5}{11} \quad \frac{7.0}{47} \quad \frac{8.2}{100}$$

$$\frac{11.8}{100} \quad \frac{6.1}{19} \quad \frac{5.0}{12} \quad 4.4 \quad \frac{4.7}{11} \quad \frac{3.8}{40} \quad \frac{3.1}{70} \quad \frac{5.6}{100}$$

Sta	+	π	-
		965.56	

98			60.4
----	--	--	------

0	6.00	964.67	6.89	958.67
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99			60.2
----	--	--	------

100			60.4
-----	--	--	------

101			56.6
-----	--	--	------

102			54.1
-----	--	--	------

103			53.9
-----	--	--	------

104			53.0
-----	--	--	------

0	5.26	959.82	10.11	954.56
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105			53.6
-----	--	--	------

106			54.1
-----	--	--	------

$\frac{12.8}{100}$ $\frac{4.8}{24}$ $\frac{5.5}{11}$ 5.2 $\frac{6.1}{12}$ $\frac{9.0}{18}$ $\frac{15.3}{73-100}$

Nail T.P. Rt Sta 97+90

$\frac{10.0}{100}$ $\frac{9.0}{60}$ $\frac{5.6}{35}$ $\frac{4.3}{14}$ $\frac{4.8}{11}$ 4.5 $\frac{5.0}{12}$ $\frac{5.9}{33}$ $\frac{10.4}{100}$

$\frac{5.1}{100}$ $\frac{4.0}{50}$ $\frac{2.8}{16}$ $\frac{4.5}{9}$ 4.3 $\frac{4.4}{12}$ $\frac{3.2}{15}$ $\frac{1.1}{30}$ $\frac{4.1}{84}$

$\frac{2.1}{100}$ $\frac{7.1}{37}$ $\frac{7.7}{13}$ $\frac{8.6}{10}$ 8.1 $\frac{8.6}{12}$ $\frac{7.8}{14}$ $\frac{8.4}{57}$ $\frac{9.8}{100}$

$\frac{15.3}{100-71}$ $\frac{14.0}{13}$ $\frac{10.7}{9}$ 10.6 $\frac{10.9}{14}$ $\frac{13.0}{18-75}$

F.L. 14.7 CUL

F.L. 13.9 CUL

$\frac{14.1}{100}$ $\frac{15.0}{63}$ $\frac{12.3}{18}$ $\frac{11.3}{8}$ 10.8 $\frac{11.1}{12}$ $\frac{10.0}{17}$ $\frac{7.2}{38}$ $\frac{7.4}{100}$

$\frac{13.1}{100}$ $\frac{17.0}{46}$ $\frac{14.0}{14}$ $\frac{12.0}{9}$ 11.7 $\frac{12.2}{14}$ $\frac{10.5}{49}$ $\frac{2.4}{100}$

F.L. CUL 15.6

F.L. 13.9

Nail in T.P. Rt Sta 103+95

$\frac{11.8}{100}$ $\frac{9.8}{55}$ $\frac{6.4}{17}$ $\frac{7.0}{13}$ $\frac{6.6}{9}$ 6.2 $\frac{6.5}{13}$ $\frac{5.4}{15}$ $\frac{0.0}{50}$ $\frac{+3.5}{100}$

$\frac{9.1}{100}$ $\frac{7.7}{28}$ $\frac{7.5}{14}$ $\frac{6.3}{10}$ 5.7 $\frac{5.8}{14}$ $\frac{5.1}{17}$ $\frac{0.3}{70}$ $\frac{2.6}{100}$

959.82

107 54.6

108 54.3

109 51.4

110 51.2

111 52.0

112 54.1

0 13.00 ~~969.79~~ 3.03 956.79

113 55.7

114 58.8

+34 Section Line E+W

+80

115 63.0

116 65.2

$$\frac{0.0}{150} \quad \frac{+4.3}{100} \quad \frac{0.2}{44} \quad \frac{4.0}{17} \quad \frac{6.1}{12} \quad \frac{5.5}{10} \quad 5.2 \quad \frac{6.2}{14} \quad \frac{5.7}{18} \quad \frac{3.7}{68} \quad \frac{5.7}{100}$$

$$\frac{+2.0}{100} \quad \frac{+3.5}{90} \quad \frac{0.0}{44} \quad \frac{1.8}{18} \quad \frac{5.9}{9} \quad 5.5 \quad \frac{5.9}{15} \quad \frac{4.7}{18} \quad \frac{4.4}{49} \quad \frac{2.4}{100} \quad \frac{3.7}{125}$$

$$\frac{+0.6}{100} \quad \frac{3.4}{49} \quad \frac{6.8}{19} \quad \frac{8.5}{10} \quad 8.4 \quad \frac{8.7}{14} \quad \frac{9.7}{66} \quad \frac{5.0}{100}$$

$$\frac{8.1}{100} \quad \frac{6.0}{68} \quad \frac{10.0}{28} \quad \frac{10.4}{14} \quad \frac{9.3}{12} \quad 8.6 \quad \frac{9.2}{13} \quad \frac{12.1}{17.50} \quad \frac{12.6}{100}$$

FL Colv 13.4

F.L. Colv 13.0

$$\frac{14.0}{100} \quad \frac{12.7}{50} \quad \frac{8.1}{12} \quad 7.8 \quad \frac{8.3}{11} \quad \frac{7.4}{16} \quad \frac{6.3}{42} \quad \frac{8.5}{100}$$

$$\frac{17.4}{100} \quad \frac{13.5}{63} \quad \frac{6.9}{22} \quad \frac{6.5}{14} \quad 5.7 \quad \frac{5.9}{10-12} \quad \frac{2.3}{18} \quad \frac{8.0}{57} \quad \frac{7.1}{100}$$

T.P. R+S₂ 112+83

$$\frac{30.0}{100} \quad \frac{20.0}{41} \quad \frac{14.2}{18} \quad \frac{14.6}{15} \quad 14.1 \quad \frac{14.6}{7} \quad \frac{13.4}{10} \quad \frac{11.0}{73} \quad \frac{8.1}{100}$$

$$\frac{30.0}{100} \quad \frac{19.5}{44} \quad \frac{13.1}{21} \quad \frac{11.6}{13} \quad 11.0 \quad \frac{11.4}{8} \quad \frac{9.3}{14} \quad \frac{5.4}{48} \quad \frac{0.8}{100}$$

7.4

$$\frac{24.5}{100} \quad \frac{13.4}{54} \quad \frac{8.0}{28} \quad \frac{6.8}{14} \quad \frac{7.4}{11} \quad 6.8 \quad \frac{7.0}{9} \quad \frac{4.5}{13} \quad \frac{2.3}{48} \quad \frac{0.0}{100}$$

$$\frac{30.0}{100} \quad \frac{9.9}{49} \quad \frac{6.8}{15} \quad \frac{5.2}{13} \quad 4.6 \quad \frac{5.0}{9} \quad \frac{2.9}{12} \quad \frac{0.3}{40} \quad \frac{+1.0}{80} \quad \frac{0.0}{100}$$

969.79

117

68.2

○

13.42

981.01

2.20

967.59

118

67.5

BM

11.47

969.54

119

68.4

120

70.7

121

71.7

122

74.6

BM

19.0

979.11

123

76.6

○

9.00

987.47

2.54

978.47

$\frac{30.0}{100}$	$\frac{11.1}{58}$	$\frac{2.7}{17}$	$\frac{3.4}{14}$	$\frac{2.5}{12}$	1.6	$\frac{1.8}{11}$	$\frac{0.0}{17}$	$\frac{+1.0}{100}$
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Nail in F.P. Lt. Sta 118+45

$\frac{30.0}{100}$	$\frac{20.0}{66}$	$\frac{18.5}{35}$	$\frac{15.2}{13}$	$\frac{14.0}{11}$	13.5	$\frac{13.8}{12}$	$\frac{12.7}{18-55}$
F.L. 14.8					F.L. 15.6		

118+90 100' Rt. Nail NW Cor Barn

Floor H₂

11.4	$\frac{13.5}{73}$	$\frac{13.4}{21}$	$\frac{13.8}{13}$	$\frac{13.2}{11}$	12.6	$\frac{13.0}{12}$	$\frac{13.2}{48}$	$\frac{14.4}{100}$
------	-------------------	-------------------	-------------------	-------------------	------	-------------------	-------------------	--------------------

$\frac{12.6}{100}$	$\frac{13.1}{47}$	$\frac{10.7}{15}$	$\frac{11.2}{12}$	10.3	$\frac{10.5}{13}$	$\frac{9.4}{21}$	$\frac{10.5}{56}$	$\frac{11.6}{100}$
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$\frac{8.2}{100}$	$\frac{8.7}{65}$	$\frac{9.3}{15}$	$\frac{9.9}{13}$	9.3	$\frac{9.8}{11}$	$\frac{10.9}{18-59}$	$\frac{9.8}{100}$
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$\frac{4.3}{175}$	$\frac{6.4}{100}$	$\frac{7.2}{57}$	$\frac{7.1}{18}$	$\frac{7.9}{16}$	$\frac{6.8}{12}$	6.4	$\frac{6.9}{10}$	$\frac{5.5}{14}$	$\frac{5.3}{48}$	$\frac{6.2}{58}$	$\frac{7.6}{100}$
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Floor H₃ 1.3

Top Conc Steps Lt Sta 122 - 125' Lt.

Floor H₄ + 0.7

See Revision 17

$\frac{9.0}{100}$	$\frac{7.0}{62}$	$\frac{5.1}{41}$	$\frac{4.5}{19}$	$\frac{5.1}{16}$	4.4	$\frac{4.8}{9}$	$\frac{4.0}{11}$	$\frac{1.7}{51}$	$\frac{0.0}{100}$	↓
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Top Rock 30' Rt Sta 124+20

Sta

+

Δ

-

987.47

124 78.0

125 77.7

126 79.0

127 80.0

B.M. 680 980.67

128 81.1

129 82.2

130 82.2

+45 82.8

131 83.3

+50 84.5

132 84.2

Revised

$$\frac{12.4}{100} \frac{8.8}{71} \frac{9.9}{32} \frac{9.7}{21} \frac{9.7}{16} 9.5 \frac{10.2}{9-18} \frac{8.4}{69} \frac{7.0}{100}$$

$$\frac{12.9}{100} \frac{11.7}{68} \frac{10.7}{31} \frac{11.4}{20} \frac{11.5}{17} 9.8 \frac{10.5}{9} \frac{10.0}{12} \frac{9.6}{41} \frac{10.7}{100}$$

$$\frac{12.6}{100} \frac{11.4}{67} \frac{9.2}{35} \frac{9.8}{20} \frac{9.2}{16} 8.5 \frac{9.1}{9} \frac{9.7}{13} \frac{10.9}{65} \frac{12.0}{100}$$

$$\frac{10.8}{74} \frac{8.5}{33} \frac{8.9}{21} \frac{8.3}{14} 7.5 \frac{8.2}{11} \frac{9.2}{14-5.8} \frac{8.2}{100}$$

RR Spk in TP Rt 126+30 (Old B.M.) Gramsey Road Survey

$$\frac{12.6}{100} \frac{11.7}{75} \frac{6.6}{27} \frac{7.5}{15} \frac{7.0}{12} 6.4 \frac{6.9}{12} \frac{6.3}{15} \frac{7.2}{32} \frac{8.0}{100}$$

$$\frac{12.8}{100} \frac{11.8}{77} \frac{8.3}{41} \frac{4.4}{21} \frac{5.6}{13} \frac{4.6}{11} 4.3 \frac{4.8}{12} \frac{3.6}{14-29} \frac{5.5}{69} \frac{7.0}{100}$$

$$\frac{10.0}{69} \frac{8.3}{35} \frac{6.7}{28} \frac{5.0}{11} 4.3 \frac{4.5}{11} \frac{4.1}{13} \frac{7.8}{66} \frac{10.0}{100}$$

F.L. Culv 13.8

F.L. Culv 16.1

$$\frac{10.0}{100} \frac{8.5}{59} \frac{7.0}{18} \frac{5.4}{12} 4.7 \frac{5.3}{11} \frac{7.9}{16} \frac{12.3}{55} \frac{13.0}{100}$$

$$\frac{5.5}{100} \frac{1.5}{58} \frac{4.0}{18} \frac{4.4}{12} 4.2 \frac{4.9}{11} \frac{6.7}{17} \frac{12.8}{62} \frac{14.9}{100}$$

$$\frac{3.4}{100} + \frac{1.0}{52} \frac{1.6}{16} \frac{3.2}{12} 3.0 \frac{4.0}{13} \frac{4.7}{21} \frac{14.8}{64} \frac{18.0}{100}$$

$$\frac{12.6}{100} \frac{1.0}{79} \frac{2.4}{21} \frac{4.1}{16} \frac{3.6}{12} 3.3 \frac{4.6}{12} \frac{5.8}{20} \frac{13.2}{65} \frac{16.0}{100}$$

987.47

133

84.7

0

3.53

989.41

159

985.88

134

85.0

135

83.7

136

82.1

137

83.4

138

84.9

0

2.60

986.81

Rev 5

$$\frac{5.0}{100} \quad \frac{3.2}{12} \quad 2.8 \quad \frac{3.3}{11} \quad \frac{4.5}{41} \quad \frac{7.0}{100}$$

Nail in Stp 20 Lr. 132+50

$$\frac{5.8}{100} \quad \frac{4.8}{48} \quad \frac{4.9}{12} \quad 4.4 \quad \frac{5.0}{72} \quad \frac{5.3}{16} \quad \frac{4.5}{54} \quad \frac{7.6}{100}$$

Floor Ho
Lr 3.8

$$\frac{5.0}{35} \quad \frac{5.5}{19} \quad \frac{6.0}{14} \quad 5.7 \quad \frac{6.1}{11} \quad \frac{6.8}{16-21} \quad \frac{7.5}{63-100}$$

$$\frac{9.2}{100} - \frac{9.0}{39} \quad \frac{9.0}{15} \quad \frac{7.8}{12} \quad 7.3 \quad \frac{7.8}{11} \quad \frac{10.2}{21} \quad \frac{13.1}{89} \quad \frac{16.0}{100}$$

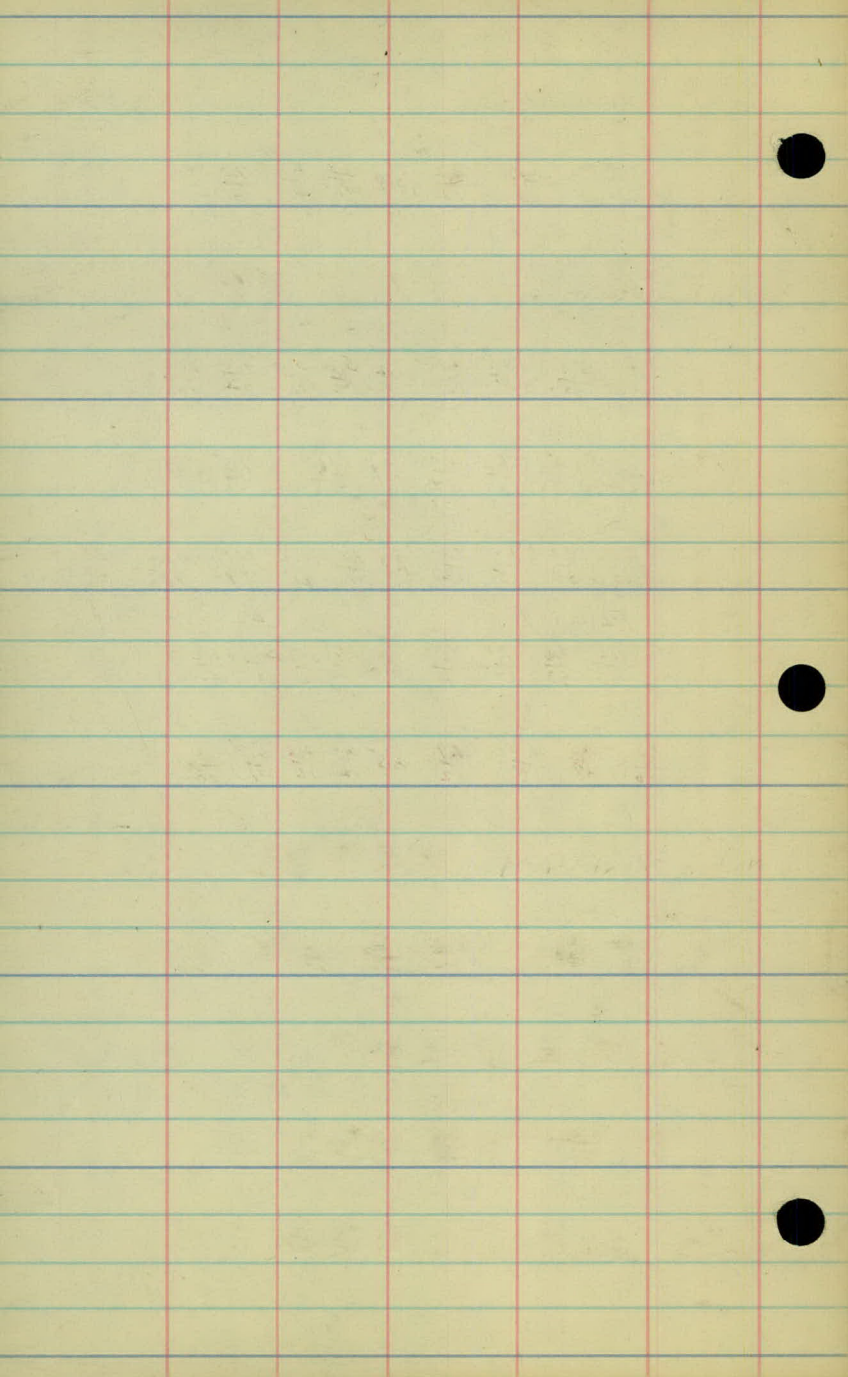
FL. Culv 10.8

FL. Culv 12.3

$$\frac{11.6}{100} \quad \frac{9.6}{63} \quad \frac{7.1}{32} \quad \frac{6.7}{12} \quad 6.0 \quad \frac{6.8}{11} \quad \frac{5.7}{13} \quad \frac{5.0}{31} \quad \frac{10.2}{100}$$

$$\frac{9.0}{100} \quad \frac{4.7}{38} \quad \frac{4.2}{15} \quad \frac{4.9}{12} \quad 4.5 \quad \frac{5.0}{12} \quad \frac{4.6}{16} \quad \frac{5.9}{41} \quad \frac{8.6}{100}$$

Nail in T.P. Rt. Sta-139



H.T. Purcell

6/18/36

Rec.-6-23-36

X- Sections

Line Revision @ Gramsey Rd
on Victoria

123 To 142

Sta	+	π	-
B.M.	11.24	980.78	969.54

123			76.6 -
-----	--	--	--------

+55			77.7 -
-----	--	--	--------

124			78.0 -
-----	--	--	--------

125			77.8 -
-----	--	--	--------

126			79.1 -
-----	--	--	--------

127	8.85	988.24	139 979.39
-----	------	--------	------------

128			79.8 -
-----	--	--	--------

129			81.0 -
-----	--	--	--------

130			82.9 -
-----	--	--	--------

+55			83.9 -
-----	--	--	--------

131	4.49	990.01	266 985.76
-----	------	--------	------------

132			83.1 -
-----	--	--	--------

+40			78.9 -
-----	--	--	--------

Nail in NW. Cor. Barn Rt Sta 118+90

$\frac{7.0}{100}$ $\frac{6.7}{65}$ $\frac{5.0}{41}$ $\frac{4.4}{18}$ $\frac{4.8}{16}$ 4.2 $\frac{4.5}{9}$ $\frac{4.3}{10}$ $\frac{3.8}{11}$ $\frac{1.5}{52}$ $\frac{+0.5}{100}$

$\frac{6.8}{100}$ $\frac{5.9}{61}$ $\frac{4.0}{38}$ $\frac{3.8}{22}$ $\frac{3.9}{17}$ 3.1 $\frac{3.6}{10}$ $\frac{2.3}{14}$ $\frac{0.3}{46}$ $\frac{+1.2}{100}$

$\frac{7.0}{100}$ $\frac{4.5}{63}$ $\frac{2.5}{36}$ $\frac{2.4}{24}$ $\frac{3.3}{20}$ $\frac{2.9}{15}$ 2.8 $\frac{3.5}{11}$ $\frac{3.2}{14}$ $\frac{3.7}{20}$ $\frac{2.6}{55}$ $\frac{1.9}{100}$

$\frac{6.0}{100}$ $\frac{4.8}{62}$ $\frac{4.3}{33}$ $\frac{4.0}{17}$ $\frac{3.6}{14}$ 3.0 $\frac{3.7}{12}$ $\frac{3.3}{20}$ $\frac{2.8}{42}$ $\frac{3.3}{62}$ $\frac{4.0}{100}$

$\frac{3.5}{54}$ $\frac{2.4}{27}$ $\frac{2.8}{17}$ $\frac{2.3}{12}$ 1.7 $\frac{2.2}{13}$ $\frac{2.9}{18}$ $\frac{3.2}{43}$ $\frac{4.1}{100}$

$\frac{12.0}{100}$ $\frac{11.4}{73}$ $\frac{10.0}{54}$ $\frac{9.2}{25}$ $\frac{9.4}{21}$ $\frac{9.1}{11}$ 8.4 $\frac{9.0}{13}$ $\frac{10.0}{18-52}$ $\frac{9.5}{88}$ $\frac{10.2}{110}$

$\frac{14.0}{100}$ $\frac{12.3}{75}$ $\frac{7.2}{30}$ $\frac{7.7}{20-12}$ 7.2 $\frac{7.6}{11}$ $\frac{7.1}{16}$ $\frac{7.4}{39}$ $\frac{8.5}{75}$ $\frac{9.0}{100}$

$\frac{14.0}{100}$ $\frac{12.0}{82}$ $\frac{10.2}{61}$ $\frac{5.1}{36}$ $\frac{4.8}{21}$ $\frac{5.4}{18}$ 5.3 $\frac{5.5}{4}$ $\frac{4.3}{7}$ $\frac{4.8}{33}$ $\frac{5.9}{59}$ $\frac{6.9}{100}$

$\frac{12.0}{100}$ $\frac{10.8}{86}$ $\frac{7.1}{49}$ $\frac{4.2}{26}$ $\frac{5.3}{23}$ $\frac{4.8}{11}$ $\frac{5.0}{2}$ 4.3 $\frac{2.4}{15}$ $\frac{4.3}{42}$ $\frac{7.5}{80}$ $\frac{8.5}{100}$

RR SpK in 24' BE, 53' Lt Sta 139+20

$\frac{13.0}{100}$ $\frac{11.9}{61}$ $\frac{8.5}{31}$ $\frac{7.2}{26}$ $\frac{6.8}{15}$ $\frac{7.1}{5}$ 7.0 $\frac{7.0}{17}$ $\frac{9.4}{55}$ $\frac{11.9}{90-100}$

$\frac{12.0}{100}$ $\frac{10.3}{69}$ $\frac{13.8}{44}$ $\frac{10.1}{36}$ $\frac{7.9}{36}$ $\frac{7.3}{17}$ $\frac{7.7}{8}$ $\frac{10.7}{4}$ 11.2 $\frac{12.8}{16}$ $\frac{14.5}{35}$ $\frac{15.4}{60}$ $\frac{13.0}{100}$

Sta	+	π ✓	-	
	+50	990.07 ✓ ditch		74.8 -
	+58			77.8 -
131				80.3 -
132				80.7 -
133				83.8 -
134				84.2 -
135				82.6 -
B.M.		501	985.06 ✓	
136				81.7 -
137				83.4 -
138				84.8 -
B.M.	2.80	989.61 ✓	3.23	986.84 ✓ 986.81
139				84.8 -

$\frac{8.0}{100}$ $\frac{10.3}{53}$ $\frac{9.6}{38}$ $\frac{7.9}{32}$ $\frac{7.3}{19}$ $\frac{8.0}{9}$ 153 $\frac{12.8}{16}$ $\frac{15.0}{39}$ $\frac{15.5}{84}$ $\frac{14.5}{100}$ F.L. Culv. 17.8

$\frac{9.4}{100-60}$ $\frac{9.6}{37}$ $\frac{7.7}{31}$ $\frac{7.3}{19}$ $\frac{7.9}{9}$ 12.3 $\frac{12.8}{7}$ $\frac{13.6}{17}$ $\frac{17.8}{24}$ $\frac{14.5}{36}$ $\frac{15.9}{57}$ $\frac{15.0}{100}$

$\frac{5.8}{100}$ $\frac{3.7}{74}$ $\frac{5.7}{54}$ $\frac{6.6}{39}$ $\frac{7.0}{35}$ $\frac{6.8}{22}$ $\frac{7.7}{11}$ 9.8 $\frac{15.6}{46}$ $\frac{12.3}{75}$ $\frac{18.4}{79}$ $\frac{12.1}{82}$

$\frac{3.8}{100}$ $\frac{3.4}{80}$ $\frac{3.8}{60}$ $\frac{6.7}{43}$ $\frac{6.0}{41}$ $\frac{5.9}{28}$ $\frac{7.1}{14}$ 9.4 $\frac{11.2}{11}$ $\frac{16.6}{50}$ $\frac{19.0}{70}$ Pot Hole

$\frac{5.9}{100-77}$ $\frac{6.0}{36}$ $\frac{5.4}{28}$ $\frac{5.9}{16}$ 6.3 $\frac{7.3}{30}$ $\frac{11.4}{100}$

$\frac{6.6}{100}$ $\frac{5.2}{65}$ $\frac{5.1}{20}$ $\frac{5.7}{9}$ 5.9 $\frac{5.4}{14}$ $\frac{5.2}{45}$ $\frac{8.7}{90}$ $\frac{9.3}{100}$

$\frac{5.8}{51}$ $\frac{6.7}{28}$ $\frac{6.3}{15}$ $\frac{6.7}{3}$ 7.5 $\frac{7.6}{18}$ $\frac{8.3}{41}$ $\frac{7.9}{83}$ $\frac{10.0}{100}$

SE Cor Conc Step Lt Sta 135+00

$\frac{9.2}{100}$ $\frac{10.0}{40}$ $\frac{9.8}{24}$ $\frac{8.4}{20}$ $\frac{7.9}{9}$ 8.4 $\frac{8.7}{3}$ $\frac{12.2}{7}$ $\frac{10.3}{17}$ $\frac{11.2}{56}$ $\frac{15.0}{100}$ $\frac{17.1}{110}$

F.L. 13.1 77.07

F.L. Culv 13.1 76.97

$\frac{9.7}{61}$ $\frac{7.7}{35}$ $\frac{7.2}{16}$ $\frac{6.6}{3}$ 6.7 $\frac{7.1}{8}$ $\frac{6.0}{11}$ $\frac{5.6}{26}$ $\frac{9.6}{75}$ $\frac{10.1}{100}$

$\frac{9.3}{100}$ $\frac{8.3}{72}$ $\frac{5.5}{36}$ $\frac{5.0}{13}$ $\frac{5.5}{10}$ 5.3 $\frac{5.7}{14}$ $\frac{5.2}{17}$ $\frac{7.4}{58}$ $\frac{7.2}{100}$

Nail in T.P. Rt Sta 139 (Caution - Pole to be moved)

$\frac{4.0}{100}$ $\frac{3.6}{81}$ $\frac{2.0}{51}$ $\frac{1.9}{22}$ $\frac{3.7}{7}$ $\frac{4.9}{5}$ 4.8 $\frac{4.7}{6}$ $\frac{5.0}{17}$ $\frac{3.8}{20}$ $\frac{3.7}{37}$ $\frac{7.3}{95-100}$

Sta

+

Σ

-

989.61 ✓

140

82.4 -

+10

79.9 -

+16

79.8 -

+29

Σ CORd "F"

79.7 -

(4)

79.7 -

+05

79.6 -

+09

79.6 -

+50

80.0 -

42

80.4 -

B.M.

8.38

981.23 ✓

$$\frac{7.0}{100} \quad \frac{6.2}{89} \quad \frac{4.5}{53} \quad \frac{4.2}{23} \quad \frac{6.4}{8} \quad \frac{7.4}{4} \quad 7.2 \quad \frac{7.0}{7} \quad \frac{7.6}{20} \quad \frac{7.0}{26} \quad \frac{8.1}{57} \quad \frac{9.6}{100}$$

$$\frac{9.4}{64} \quad \frac{8.9}{21} \quad \frac{10.0}{13} \quad 9.7 \quad \frac{9.9}{7} \quad \frac{11.4}{17} \quad \frac{10.9}{32} \quad \frac{11.5}{77} \quad \frac{12.2}{100}$$

$$\frac{10.5}{62} \quad \frac{11.3}{37}$$

$$9.8 \quad \frac{11.6}{33} \quad \frac{12.2}{81}$$

$$\frac{10.0}{80}$$

$$9.9$$

$$\frac{12.6}{80}$$

$$9.9$$

$$\frac{11.5}{100} \quad \frac{11.2}{67} \quad \frac{10.5}{19}$$

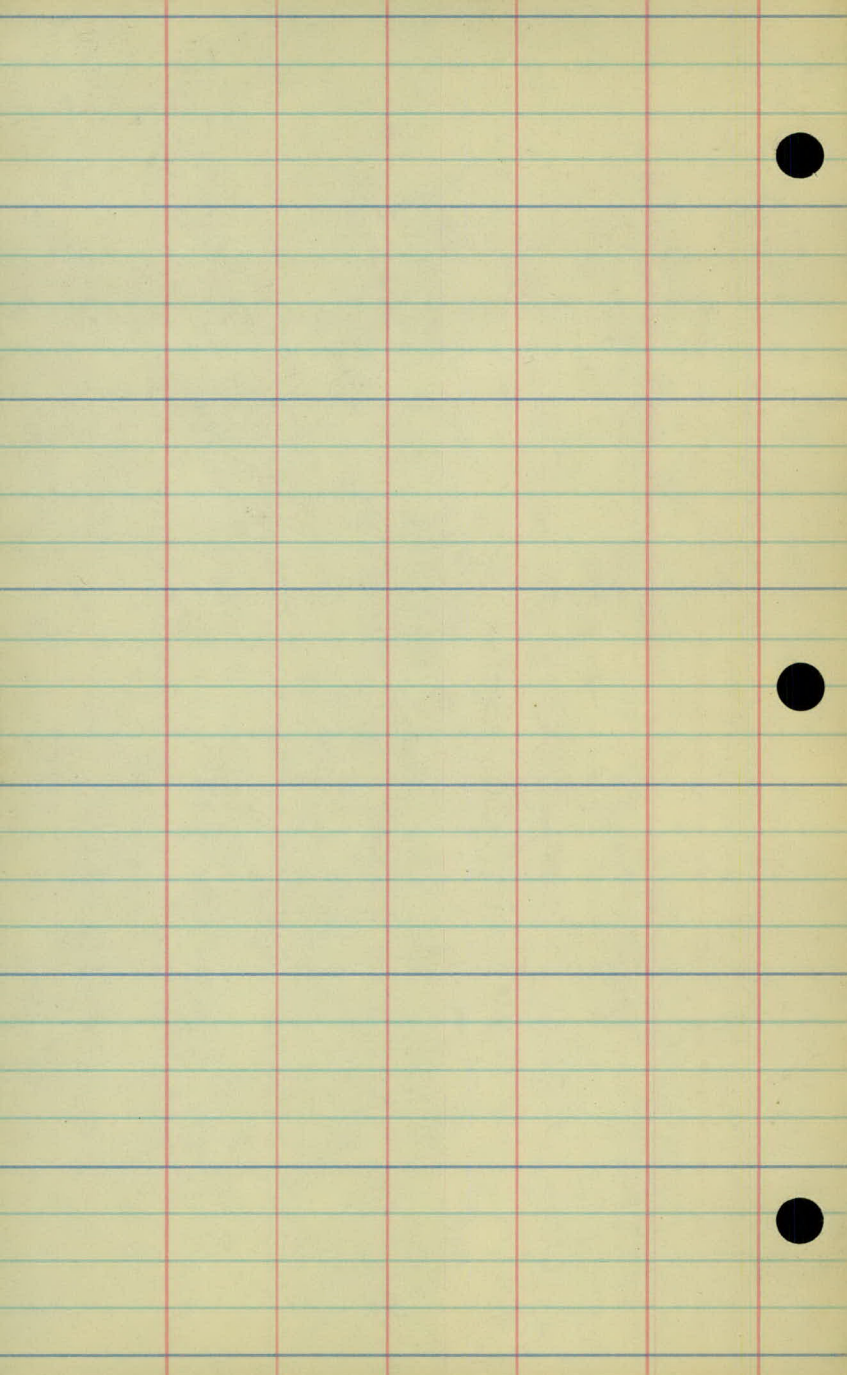
$$10.0 \quad \frac{11.4}{32} \quad \frac{12.8}{81}$$

$$\frac{10.9}{78} \quad \frac{9.1}{39} \quad \frac{9.4}{16} \quad \frac{11.4}{13} \quad 10.0 \quad \frac{10.9}{19} \quad \frac{12.0}{33} \quad \frac{12.0}{90}$$

$$\frac{12.6}{94} \quad \frac{9.2}{59} \quad \frac{8.3}{35} \quad \frac{9.0}{16} \quad \frac{10.0}{13} \quad 9.6 \quad \frac{10.2}{16} \quad \frac{11.8}{20} \quad \frac{9.9}{24} \quad \frac{11.5}{64} \quad \frac{12.1}{100}$$

$$\frac{12.5}{100} \quad \frac{7.8}{38} \quad \frac{8.7}{18} \quad \frac{9.7}{15} \quad 9.2 \quad \frac{9.8}{15} \quad \frac{10.0}{18} \quad \frac{9.1}{19} \quad \frac{9.9}{61} \quad \frac{10.6}{100}$$

R.R. SpK SW Cor in PP. Victoria r "F"



Wilke
Bell
Goldberg

VICTORIA ST.

CROSS SECTIONS

LINE REVISION.

73 To 90

MAY. 14, 1936

+	H.I.	-	Elev.
3.30	958.74 ✓		955.44 ✓
13.18	971.11 ✓	0.81	957.93 ✓
3.47	967.75	6.83	964.28 ✓

L. P. 73 + 43.27 64.6

74 + 37 63.6

74 + 67 63.0

75 + 00 62.4

75 + 50 62.1

76 + 00 62.0

76 + 55 61.5

77 + 00 57.9

77 + 25 57.7

78 + 00 65.5

T. P. 12.47 977.91 ✓ 2.31 965.44 ✓

78 + 50 72.6

79 + 00 75.7

Top of Nut on Wig Wag Signal

$\frac{+2.0}{100}$ $\frac{0.0}{55}$ $\frac{1.6}{21}$ $\frac{4.1}{17}$ $\frac{3.5}{6}$ 3.2 $\frac{3.4}{11}$ $\frac{4.8}{23}$ $\frac{7.0}{58}$ $\frac{9.5}{100}$

$\frac{0.20}{100}$ $\frac{2.6}{63}$ $\frac{3.5}{23}$ $\frac{4.7}{21}$ $\frac{4.7}{17}$ $\frac{4.3}{9}$ 4.2 $\frac{4.6}{8}$ $\frac{5.2}{13}$ $\frac{4.1}{18}$ $\frac{5.1}{33}$ $\frac{7.4}{60}$ $\frac{11.4}{100}$

$\frac{0.0}{100}$ $\frac{2.8}{67}$ $\frac{4.3}{24}$ $\frac{5.0}{22}$ $\frac{4.7}{7}$ 4.8 $\frac{6.0}{11}$ $\frac{7.4}{17}$ $\frac{10.8}{55}$ $\frac{13.8}{100}$

$\frac{+2.0}{100}$ $\frac{0.50}{55}$ $\frac{4.1}{36}$ $\frac{5.4}{26}$ $\frac{5.2}{20}$ $\frac{5.1}{10}$ 5.4 $\frac{6.0}{6}$ $\frac{8.9}{12}$ $\frac{12.7}{43}$ $\frac{15.3}{100}$

$\frac{8.8}{100}$ $\frac{0.0}{55}$ $\frac{2.5}{35}$ $\frac{5.0}{31}$ $\frac{5.7}{28}$ $\frac{5.2}{23}$ $\frac{5.1}{12}$ 5.7 $\frac{8.6}{9}$ $\frac{11.0}{35}$ $\frac{13.0}{65}$ $\frac{14.4}{100}$

$\frac{8.8}{100}$ $\frac{0.30}{54}$ $\frac{2.3}{39}$ $\frac{5.1}{35}$ $\frac{5.8}{33}$ $\frac{5.0}{16}$ $\frac{5.4}{4}$ 5.8 $\frac{7.3}{11}$ $\frac{10.5}{40}$ $\frac{11.7}{76}$ $\frac{12.4}{100}$

$\frac{8.8}{100}$ $\frac{0.0}{80}$ $\frac{3.1}{65}$ $\frac{4.8}{42}$ $\frac{6.2}{38}$ $\frac{5.2}{30}$ $\frac{4.9}{19}$ $\frac{5.3}{7}$ 6.3 $\frac{7.6}{3}$ $\frac{8.6}{27}$ $\frac{11.2}{68}$ $\frac{15.1}{86}$

$\frac{0.50}{100}$ $\frac{1.3}{74}$ $\frac{4.7}{52}$ $\frac{5.9}{42}$ $\frac{4.3}{34}$ $\frac{4.3}{22}$ $\frac{5.2}{9}$ $\frac{9.0}{2}$ 9.9 $\frac{12.6}{27}$ $\frac{14.8}{63}$ $\frac{18.7}{80}$

$\frac{1.0}{100}$ $\frac{1.8}{80}$ $\frac{4.9}{54}$ $\frac{3.9}{37}$ $\frac{3.8}{25}$ $\frac{4.6}{10}$ 10.1 $\frac{11.7}{5}$ $\frac{15.0}{38}$ $\frac{16.8}{50}$ $\frac{19.8}{85}$

$\frac{0.0}{100}$ $\frac{0.20}{75}$ $\frac{0.70}{48}$ $\frac{2.1}{43}$ $\frac{1.5}{28}$ $\frac{2.4}{11}$ $\frac{1.4}{9}$ 2.3 $\frac{4.6}{23}$ $\frac{6.0}{33}$ $\frac{7.8}{53}$ $\frac{11.0}{63}$ $\frac{17.5}{75}$

Nail in T.P 77+85

$\frac{5.1}{82}$ $\frac{6.0}{45}$ $\frac{10.0}{41}$ $\frac{9.4}{27}$ $\frac{10.0}{15}$ $\frac{5.2}{9}$ 5.3 $\frac{7.2}{28}$ $\frac{9.9}{50}$ $\frac{13.6}{68}$ $\frac{20.0}{80}$ $\frac{26.0}{100}$ $\frac{26.2}{125}$

$\frac{5.3}{100}$ $\frac{5.8}{45}$ $\frac{8.5}{40}$ $\frac{8.4}{27}$ $\frac{8.8}{15}$ $\frac{2.5}{8}$ 2.2 $\frac{2.3}{33}$ $\frac{4.6}{53}$ $\frac{12.6}{87}$ $\frac{25.6}{120}$ $\frac{26.0}{140}$

977.91

79+50

T.P

0.55

968.99

9.47

968.44

70.3

80+00

63.8

80+50

62.2

81+00

59.4

81+45

56.2

82+00

T.P.

1.92

959.85

11.06

957.93

55.9

82+30

56.3

83+00

55.5

83+35

55.1

84+00

53.9

84+50

53.3

85+00

53.5

85+60

53.9

86+00

54.2

$\frac{3.0}{100}$ $\frac{3.5}{83}$ $\frac{8.1}{50}$ $\frac{10.3}{47}$ $\frac{10.1}{42}$ $\frac{9.9}{31}$ $\frac{10.6}{18}$ $\frac{7.5}{14}$ 7.6 $\frac{5.1}{30}$ $\frac{8.7}{61}$ $\frac{13.3}{90}$ $\frac{16.3}{100}$ $\frac{27.6}{120}$ $\frac{28.0}{130}$

H. Point on Rock

$\frac{0.30}{80}$ $\frac{2.8}{47}$ $\frac{3.6}{45}$ $\frac{3.4}{31}$ $\frac{4.0}{17}$ $\frac{3.1}{16}$ $\frac{4.4}{9}$ 5.2 $\frac{4.7}{50}$ $\frac{9.9}{72}$ $\frac{19.3}{100}$

$\frac{0.0}{90}$ $\frac{2.2}{79}$ $\frac{4.9}{42}$ $\frac{5.2}{31}$ $\frac{6.1}{19}$ $\frac{4.4}{16}$ $\frac{6.2}{7}$ 6.8 $\frac{9.0}{27}$ $\frac{16.7}{56}$ $\frac{19.5}{100}$

$\frac{0.0}{100}$ $\frac{0.10}{58}$ $\frac{7.5}{40}$ $\frac{7.7}{24}$ $\frac{8.8}{12}$ $\frac{7.7}{10}$ $\frac{8.9}{3}$ 9.6 $\frac{14.0}{33}$ $\frac{16.8}{53}$ $\frac{21.3}{73}$ $\frac{21.5}{100}$

$\frac{0.20}{100}$ $\frac{0.20}{61}$ $\frac{9.3}{43}$ $\frac{9.4}{21}$ $\frac{10.5}{4}$ 12.8 $\frac{19.2}{33}$ $\frac{21.2}{65}$ $\frac{22.0}{100}$

$\frac{1.5}{100}$ $\frac{1.4}{67}$ $\frac{11.3}{45}$ $\frac{11.3}{18}$ $\frac{11.6}{5}$ 13.1 $\frac{17.4}{29}$ $\frac{21.4}{57}$ $\frac{22.14}{100}$

on Rock

$\frac{5.0}{100}$ $\frac{4.5}{61}$ $\frac{4.0}{33}$ $\frac{3.1}{25}$ $\frac{3.1}{4}$ 3.6 $\frac{4.8}{4}$ $\frac{6.5}{25}$ $\frac{10.9}{44}$ $\frac{13.5}{100}$

$\frac{7.5}{100}$ $\frac{7.0}{62}$ $\frac{6.7}{31}$ $\frac{4.6}{22}$ $\frac{4.0}{10}$ 4.4 $\frac{4.4}{2}$ $\frac{6.5}{7}$ $\frac{7.8}{24}$ $\frac{11.2}{45}$ $\frac{12.2}{100}$

$\frac{7.6}{100}$ $\frac{7.5}{56}$ $\frac{5.7}{26}$ $\frac{4.9}{21}$ $\frac{4.6}{9}$ 4.8 $\frac{5.4}{15}$ $\frac{10.9}{44}$ $\frac{13.4}{100}$

$\frac{3.2}{100}$ $\frac{3.2}{71}$ $\frac{3.6}{31}$ $\frac{6.2}{24}$ $\frac{5.7}{19}$ $\frac{5.7}{9}$ 6.0 $\frac{6.5}{3}$ $\frac{8.2}{7}$ $\frac{11.0}{47}$ $\frac{12.4}{100}$

$\frac{3.2}{100}$ $\frac{3.2}{67}$ $\frac{5.2}{35}$ $\frac{7.2}{31}$ $\frac{7.2}{24}$ $\frac{6.4}{20}$ $\frac{6.2}{10}$ 6.6 $\frac{7.1}{4}$ $\frac{10.7}{10}$ $\frac{12.5}{44}$ $\frac{13.0}{100}$

$\frac{6.7}{100}$ $\frac{6.6}{56}$ $\frac{7.3}{73}$ $\frac{6.6}{20}$ $\frac{6.2}{9}$ 6.4 $\frac{7.1}{5}$ $\frac{9.4}{10}$ $\frac{12.5}{56}$ $\frac{13.5}{100}$

$\frac{5.5}{100}$ $\frac{5.5}{52}$ $\frac{6.1}{26}$ $\frac{6.9}{21}$ $\frac{6.5}{17}$ 6.0 $\frac{6.4}{7}$ $\frac{6.5}{11}$ $\frac{6.5}{40}$ $\frac{10.8}{76}$ $\frac{11.8}{100}$

$\frac{6.4}{100}$ $\frac{4.9}{55}$ $\frac{4.4}{22}$ $\frac{6.3}{19}$ $\frac{5.1}{7}$ 5.7 $\frac{6.2}{7}$ $\frac{3.7}{14}$ $\frac{4.3}{33}$ $\frac{9.1}{73}$ $\frac{11.5}{100}$

	+ H.I.	- Elev	
6.47	961.91	4.40	955.45 955.44

86+40			54.2
-------	--	--	------

86+47			54.1
-------	--	--	------

86+80			53.5
-------	--	--	------

86+83			53.5
-------	--	--	------

87+00			53.2
-------	--	--	------

87+15			52.9
-------	--	--	------

87+20			52.8
-------	--	--	------

87+55			52.7
-------	--	--	------

87+60			52.8
-------	--	--	------

87+67			52.8
-------	--	--	------

88+00		53.3	South Shoulder Co. Rd E.
-------	--	------	--------------------------

88+30	← To Here	54.8	North Shoulder Co. Rd E
-------	-----------	------	-------------------------

89+00			58.1
-------	--	--	------

89+82			60.0
-------	--	--	------

$$\frac{7.5}{100} \quad \frac{7.1}{70} \quad \frac{6.2}{24} \quad \frac{8.5}{22} \quad 7.7 \quad \frac{8.0}{13} \quad \frac{5.3}{18} \quad \frac{8.1}{50} \quad \frac{12.8}{80}$$

$$\frac{9.5}{100} \quad \frac{7.1}{70} \quad \frac{8.1}{21} \quad 7.8 \quad \frac{8.0}{13} \quad \frac{5.3}{18} \quad \frac{8.1}{50} \quad \frac{12.8}{80}$$

$$\frac{9.4}{73} \quad \frac{8.9}{26} \quad 8.4 \quad \frac{8.9}{12} \quad \frac{6.7}{14} \quad \frac{7.7}{46} \quad \frac{11.3}{59} \quad \frac{12.0}{100}$$

$$\frac{7.2}{73} \quad \frac{7.2}{37} \quad \frac{9.1}{30} \quad 8.5 \quad \frac{8.9}{12} \quad \frac{6.8}{14} \quad \frac{7.8}{46} \quad \frac{11.3}{58} \quad \frac{12.2}{100}$$

$$\frac{7.8}{100} \quad \frac{7.2}{70} \quad \frac{6.9}{25} \quad \frac{9.3}{20} \quad 8.7 \quad \frac{9.1}{12} \quad \frac{6.8}{15} \quad \frac{7.6}{40} \quad \frac{8.6}{48} \quad \frac{12.0}{68}$$

$$\frac{7.9}{100} \quad \frac{7.3}{65} \quad \frac{6.6}{26} \quad \frac{9.5}{16} \quad 9.0 \quad \frac{9.3}{11} \quad \frac{7.4}{14} \quad \frac{6.1}{27} \quad \frac{8.6}{48} \quad \frac{12.0}{56} \quad \frac{12.8}{100}$$

$$\frac{11.0}{100} \quad \frac{10.3}{65} \quad \frac{10.1}{37} \quad \frac{9.2}{11} \quad 9.1 \quad \frac{9.3}{10} \quad \frac{10.6}{54} \quad \frac{10.9}{100}$$

North Rail 9.18 South Rail 9.28

$$\frac{10.3}{13} \quad \frac{9.9}{22} \quad \frac{9.0}{10} \quad 9.2 \quad \frac{9.7}{12} \quad \frac{10.3}{52} \quad \frac{10.3}{80}$$

$$\frac{10.9}{70} \quad \frac{11.2}{47} \quad \frac{12.2}{21} \quad \frac{9.1}{16} \quad 9.1 \quad \frac{9.7}{12} \quad \frac{12.1}{14} \quad \frac{12.2}{45} \quad \frac{12.2}{70}$$

$$\frac{7.1}{75} \quad \frac{7.6}{56} \quad \frac{7.6}{22} \quad \frac{9.7}{14} \quad \frac{9.0}{11} \quad 9.1 \quad \frac{9.7}{15} \quad \frac{8.1}{20} \quad \frac{9.1}{55} \quad \frac{11.5}{72}$$

$$\frac{6.8}{100} \quad \frac{7.3}{70} \quad \frac{6.4}{13} \quad \frac{8.7}{9} \quad 8.6 \quad \frac{9.7}{33} \quad \frac{10.6}{81}$$

$$\frac{6.5}{100} \quad \frac{7.0}{55} \quad \frac{4.1}{15} \quad \frac{7.3}{9} \quad 7.1 \quad \frac{7.9}{24} \quad \frac{9.5}{53} \quad \frac{10.3}{100}$$

$$\frac{5.3}{63} \quad \frac{1.3}{14} \quad \frac{4.0}{10} \quad 3.8 \quad \frac{4.3}{13} \quad \frac{3.3}{18} \quad \frac{4.6}{70}$$

$$\frac{2.2}{60} \quad \frac{2.8}{15} \quad \frac{2.2}{12} \quad 1.9 \quad \frac{2.7}{11} \quad \frac{2.4}{39} \quad \frac{3.3}{60}$$

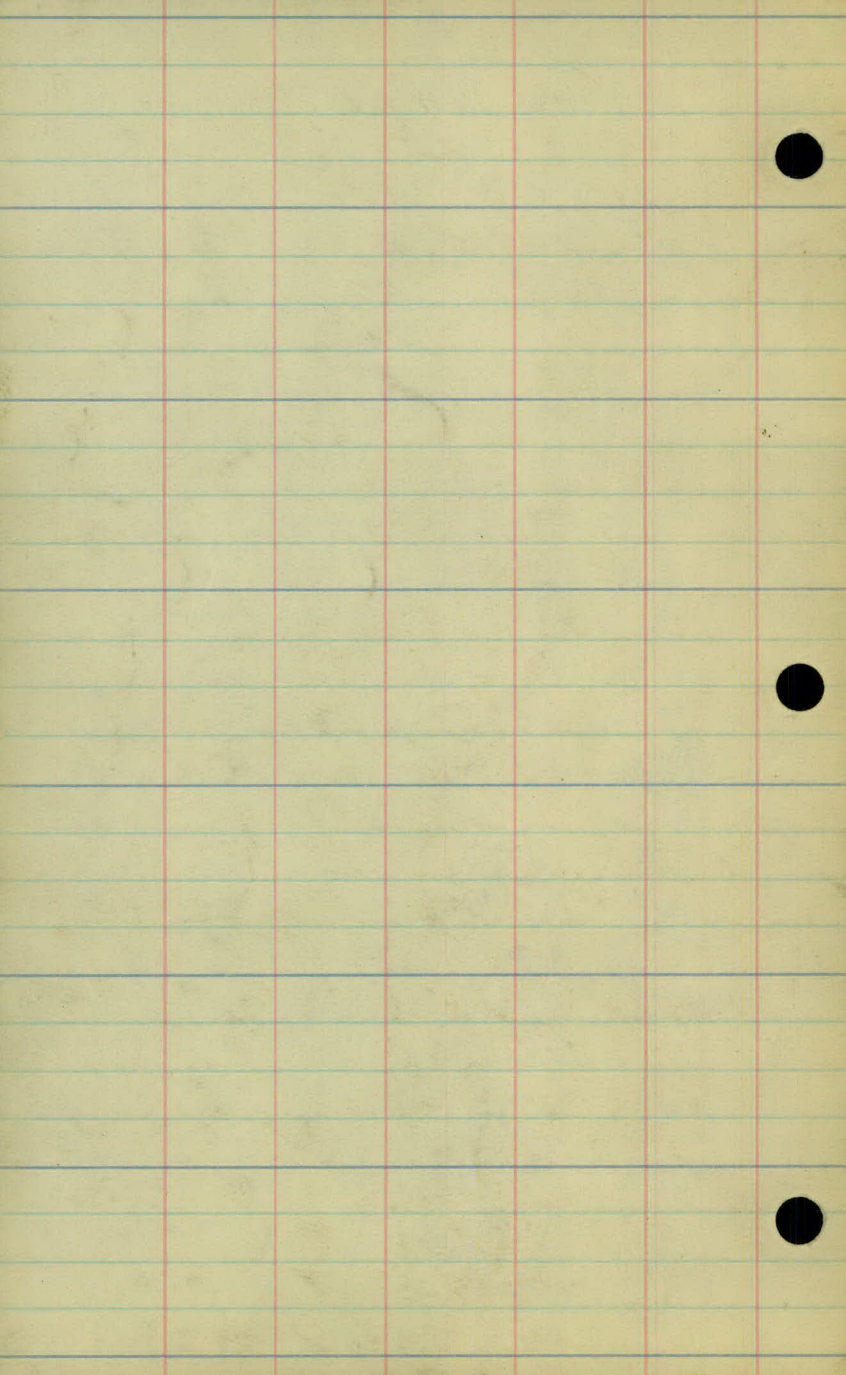
B.M

- H.I

- Elev

6.47 955.44 ✓

Top of Nut on Wig Wag



Location of Fabianski
Property
1926 Road Map Stationing.

Victoria Street.

309

+22 Sec Line

$$\begin{array}{r}
 +40 \text{ SW Cor Ho} \\
 71 \\
 +33 \text{ SE Cor Ho} \\
 \hline
 88
 \end{array}$$

308

$$\begin{array}{r}
 +27 \text{ EC} \\
 35 \\
 +36 \text{ EC} \\
 \hline
 25 \\
 +24 \text{ SW Cor Ho} \\
 65 \\
 +16 \text{ SE Cor Ho} \\
 \hline
 91
 \end{array}$$

307

$$\begin{array}{r}
 +83 \text{ SW Cor Barn} \\
 142 \\
 +46 \text{ SE Cor Barn} \\
 \hline
 169
 \end{array}$$

306

+81 Culv

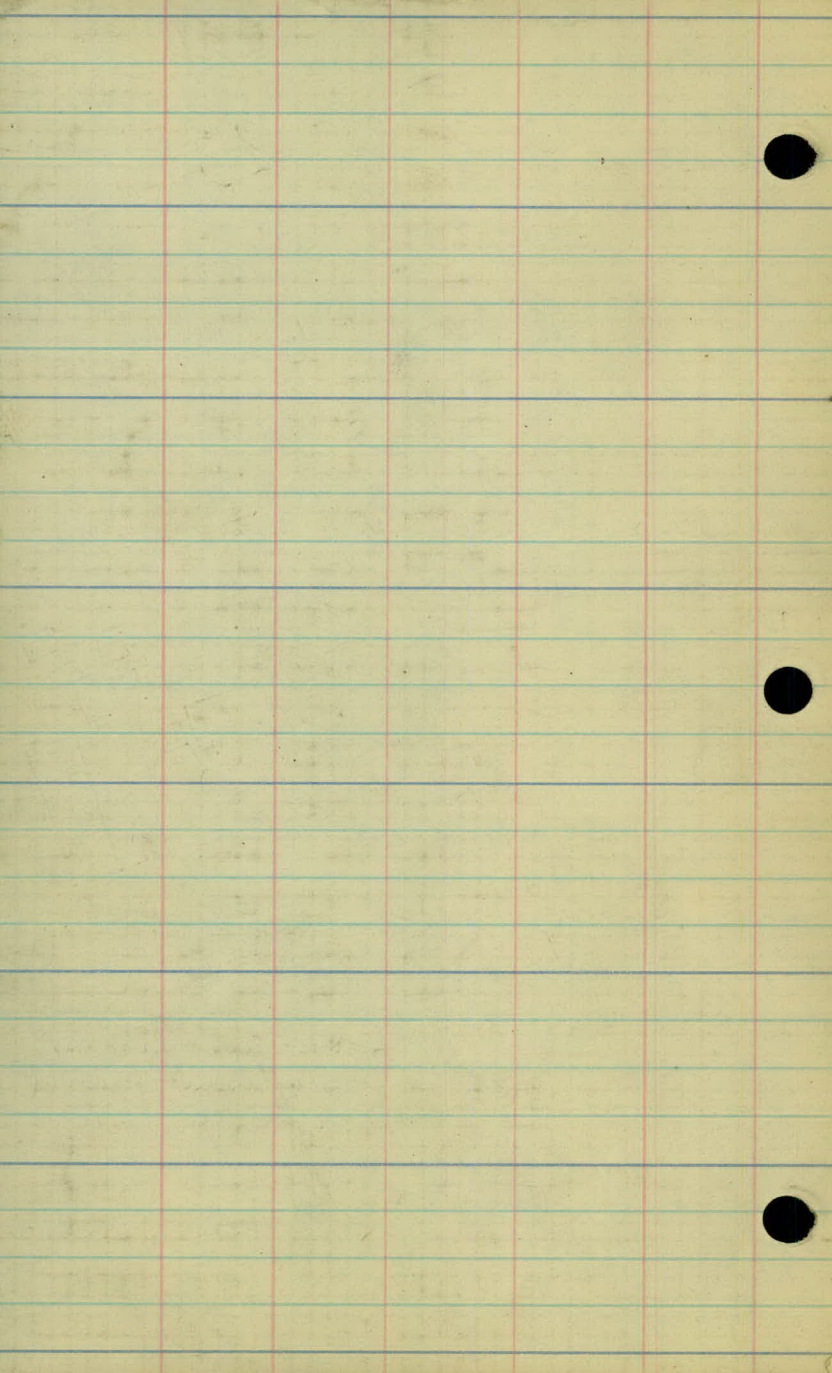
458.0

Base Line 7

530,81

The diagram shows a house layout on graph paper. The main structure is a large rectangle with dimensions 36' by 75'. Inside this main structure, there is a smaller rectangle with dimensions 24' by 26' on the left side. To the right of this 24' by 26' area is a kitchen area with dimensions 10' by 12'. Above the kitchen is a bathroom with dimensions 5' by 7'. To the right of the bathroom is a bedroom with dimensions 12' by 14'. The main structure also has a front porch area with dimensions 24' by 26' and a back porch area with dimensions 10' by 12'. The diagram includes various symbols for fixtures like a fireplace, sink, stove, and toilet.

← Note, - Topog taken on this tangent produced - Stationing as per Rd. map of 1926



6/27/36

HT Portell

Line Revision
@

Fabyanski's

165+83.80

P.C.

164+83.80

P.C.

✓
163+48.32

P.T.

160+18.99

P.C.

159+60.88

P.T.

Δ 2°00 Rt

D 2°00

Δ 32.56 Rt.

10° Curve

$$168 + 97.39$$

$$168 + 83.80 \quad \text{PT.}$$



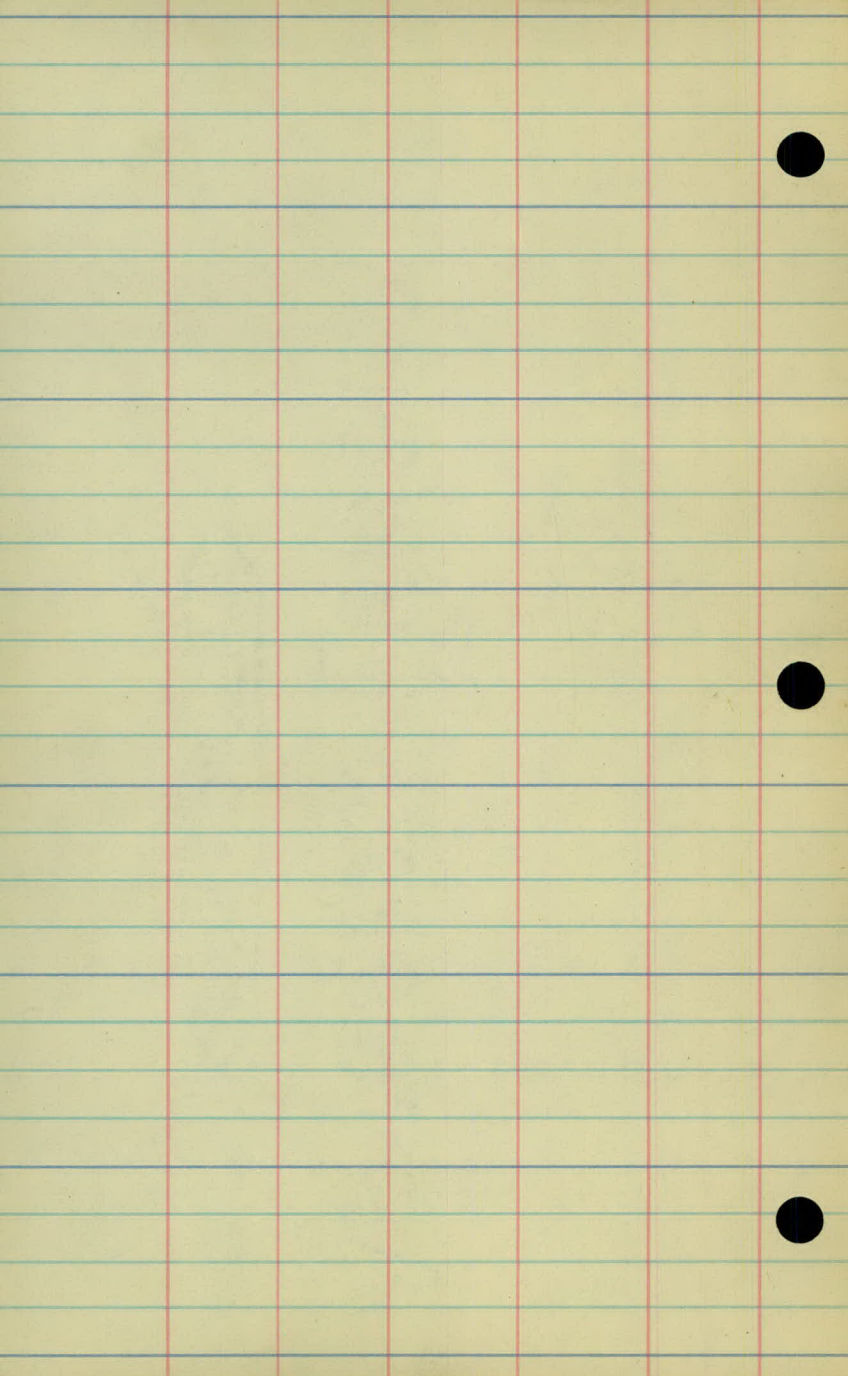
$$166 + 83.80 \quad \text{P.C.C.}$$

$\Delta 20^{\circ}00' R+$

D $10^{\circ}00'$

$\Delta 14^{\circ}00' R+$

D $14^{\circ}00'$



6/29/36

H.T. Portell

Levels
on
Co. Rd. "F"
East & West
of
Victoria

Sta + π -

B.M. 3.33 984.56 981.23

West

0+00 Int. "F" r/vict 79.6

1 79.5

2 80.5

3 81.5

4 81.3

5 79.5

East

1 76.7

2 72.9

3 68.1

4 63.1

5

SpK in PP SW Cor Vic + F

5.0

5.1

4.1

3.1

3.3

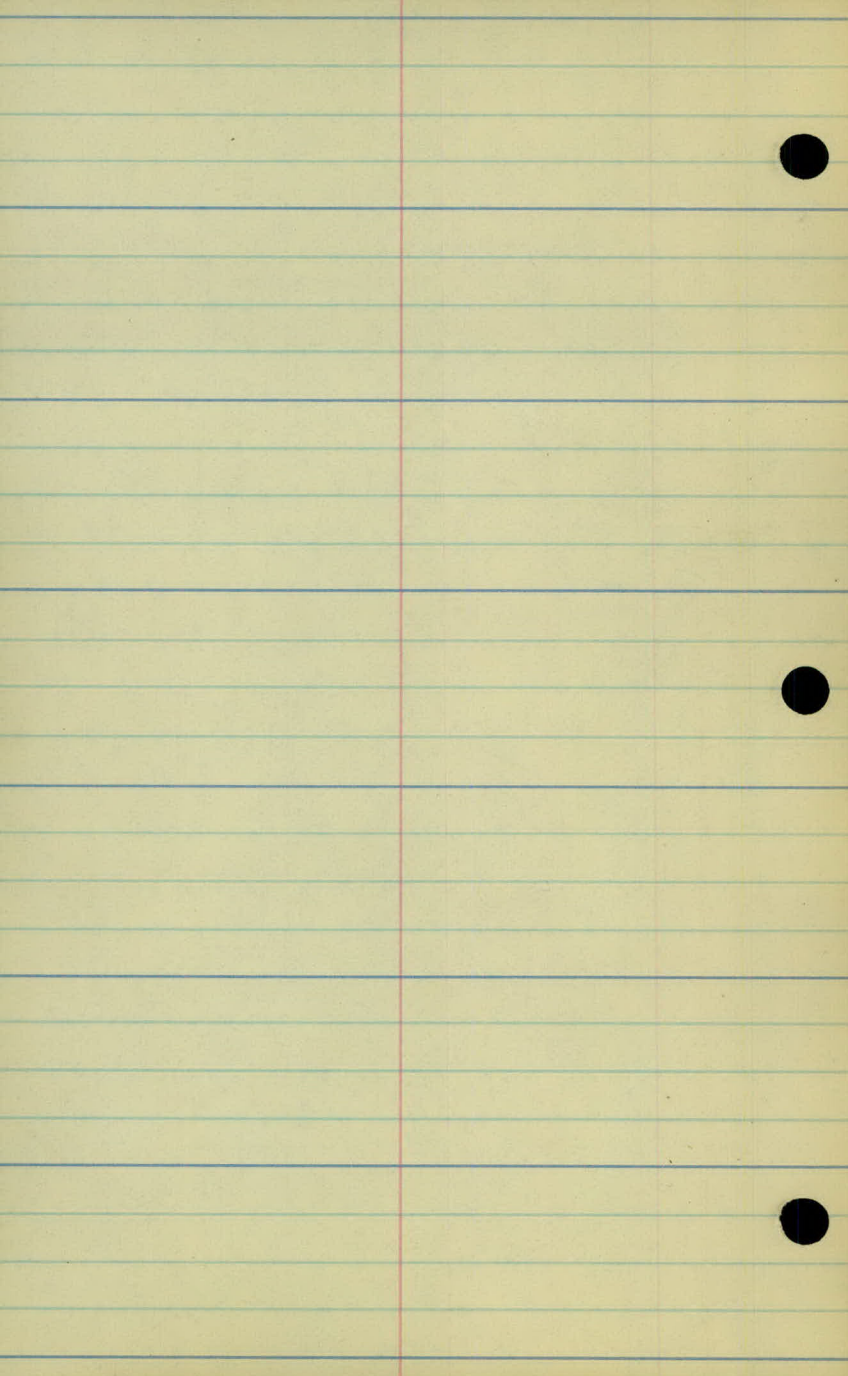
5.1

7.9

11.7

16.5

21.5



6/29/36

H.T. Purfell

X- Sections

Victoria St.

Sta	+	π	-	
BM	7.69	✓ 988.92		✓ 981.23
143				80.9.
144		✓		✓
0	9.64	990.87	7.69	981.23
BM			3.25	987.62
145				84.2.
146				85.0.
147				86.3.
148		✓		✓
0	13.15	1002.30	1.72	989.15
149				89.7.
150				92.9.
151				96.8.
152	+40			97.7.

Spk in PP. SW Cor F + Victoria

$$\frac{12.7}{100} \quad \frac{12.2}{50} \quad \frac{10.2}{33} \quad \frac{9.4}{21} \quad \frac{8.5}{16} \quad 8.0 \quad \frac{8.5}{15} \quad \frac{7.2}{18} \quad \frac{6.6}{50} \quad \frac{5.5}{100}$$

$$\frac{11.6}{50} \quad \frac{11.0}{44} \quad \frac{8.8}{28} \quad \frac{6.8}{16} \quad 6.2 \quad \frac{6.6}{14} \quad \frac{2.3}{19-50} \quad \frac{2.5}{100}$$

RR Spk in TP. 30' Rst Sta 14A+90

$$\frac{12.0}{50} \quad \frac{9.6}{21} \quad \frac{8.8}{17} \quad \frac{7.6}{14} \quad 6.7 \quad \frac{7.1}{14} \quad \frac{3.9}{19} \quad \frac{4.0}{33} \quad \frac{3.4}{50}$$

$$\frac{10.2}{50} \quad \frac{9.1}{33} \quad \frac{7.9}{18} \quad \frac{6.4}{12} \quad 5.9 \quad \frac{5.9}{13} \quad \frac{2.6}{17} \quad \frac{1.9}{50}$$

$$\frac{8.8}{50} \quad \frac{6.7}{33} \quad \frac{5.8}{20} \quad \frac{4.9}{16} \quad 4.6 \quad \frac{4.8}{10} \quad \frac{1.7}{15} \quad \frac{1.9}{33} \quad \frac{2.0}{50}$$

$$\frac{8.2}{100} \quad \frac{7.4}{33} \quad \frac{6.4}{18} \quad \frac{4.1}{12} \quad 3.8 \quad \frac{4.3}{10} \quad \frac{4.8}{14} \quad \frac{3.4}{19} \quad \frac{2.3}{50}$$

$$\frac{16.2}{50} \quad \frac{14.7}{33} \quad \frac{14.0}{19} \quad \frac{13.1}{18} \quad 12.6 \quad \frac{13.0}{13} \quad \frac{10.9}{17} \quad \frac{10.5}{47}$$

$$\frac{14.3}{50} \quad \frac{12.4}{33} \quad \frac{10.8}{20} \quad \frac{10.0}{18} \quad 9.4 \quad \frac{9.8}{11} \quad \frac{8.7}{15} \quad \frac{4.3}{22-50}$$

$$\frac{4.9}{50} \quad \frac{4.0}{18} \quad \frac{6.3}{13} \quad 5.5 \quad \frac{5.7}{13} \quad \frac{3.6}{16} \quad \frac{5.3}{50}$$

$$\frac{1.4}{50} \quad \frac{1.8}{33} \quad \frac{2.1}{18} \quad \frac{5.2}{12} \quad 4.6 \quad \frac{5.0}{11} \quad \frac{5.5}{18} \quad \frac{7.4}{33} \quad \frac{7.9}{50}$$

Sta + π -
 1002.30

152 98.8 ✓
 0 7.14 1006.24 3.20 999.10

+75 00.1 -

153 00.6 -

+50 01.0 -

154 99.9 -

155 96.5 - ✓
 0 2.69 998.27 10.66 995.58

156 93.7 -

157 89.5 -

158 85.7 -

BM 419 993.98 -

0 1.73 987.78 12.22 986.05 ✓

$$\frac{6.0}{50} \quad \frac{0.7}{12} \quad \frac{1.8}{18} \quad \frac{3.7}{13} \quad 3.5 \quad \frac{4.1}{11} \quad \frac{3.5}{14} \quad \frac{7.0}{17} \quad \frac{5.8}{39} \quad \frac{5.6}{50}$$

$$\frac{7.5}{50} \quad \frac{8.1}{29} \quad \frac{7.6}{15} \quad \frac{6.7}{12} \quad 6.1 \quad \frac{6.9}{11} \quad \frac{7.1}{15} \quad \frac{9.4}{23} \quad \frac{10.2}{50}$$

$$\frac{6.9}{50} \quad \frac{7.0}{38} \quad \frac{6.7}{18} \quad \frac{5.9}{10} \quad 5.6 \quad \frac{6.4}{12} \quad \frac{8.1}{17} \quad \frac{9.0}{28} \quad \frac{9.7}{50}$$

$$\frac{2.4}{50} \quad \frac{1.2}{33} \quad \frac{1.8}{19} \quad \frac{5.4}{13} \quad 5.2 \quad \frac{5.8}{12} \quad \frac{5.3}{14} \quad \frac{4.5}{18} \quad \frac{6.6}{50}$$

$$\frac{5.6}{50} \quad \frac{4.3}{20} \quad \frac{6.9}{14} \quad 6.3 \quad \frac{6.8}{10} \quad \frac{7.0}{13} \quad \frac{8.4}{44} \quad \frac{8.9}{50}$$

$$\frac{12.8}{50} \quad \frac{9.7}{25} \quad \frac{10.2}{18} \quad \frac{10.0}{14} \quad 9.7 \quad \frac{10.3}{10} \quad \frac{10.9}{26} \quad 50$$

$$\frac{7.6}{50} \quad \frac{5.8}{28} \quad \frac{5.1}{19} \quad \frac{4.5}{7} \quad 4.6 \quad \frac{4.8}{6} \quad \frac{2.7}{16} \quad \frac{2.9}{33} \quad \frac{1.8}{50}$$

$$\frac{15.3}{50} \quad \frac{13.0}{33} \quad \frac{11.1}{22} \quad \frac{9.7}{16} \quad 8.8 \quad \frac{9.2}{15} \quad \frac{5.4}{20} \quad \frac{5.9}{33} \quad \frac{6.4}{50}$$

$$\frac{18.0}{50} \quad \frac{17.0}{33} \quad \frac{15.0}{15} \quad \frac{13.2}{8} \quad 12.6 \quad \frac{12.4}{7} \quad \frac{12.5}{18} \quad \frac{10.9}{23} \quad \frac{10.2}{50}$$

SpK 10 12" Oak 50' Rt. Sta 157+40

Sta	+	π	-
		✓ 987.78	

159			83.1
-----	--	--	------

160			79.1
-----	--	--	------

✓ +25			78.1
----------	--	--	------

161			75.8
-----	--	--	------

0	139	✓ 976.25	12.92	✓ 774.86
---	-----	-------------	-------	-------------

+50			74.2
-----	--	--	------

162			73.2
-----	--	--	------

+50			72.3
-----	--	--	------

163			70.7
-----	--	--	------

164			66.6
-----	--	--	------

165			63.8
-----	--	--	------

B.M.	3.47	✓ 967.32	12.40	963.85 ✓
------	------	-------------	-------	----------

$$\frac{54}{50} \quad 33 - \frac{5.7}{22} \quad \frac{5.2}{12} \frac{5.6}{10} \quad 4.7 \quad \frac{4.9}{19} \frac{3.3}{23} \frac{3.5}{33} \frac{3.7}{50} \frac{5.5}{100}$$

$$\frac{9.0}{50} \quad \frac{8.5}{33} \quad \frac{8.3}{16} \quad \frac{9.3}{13} \quad 8.7 \quad \frac{9.3}{15} \frac{8.3}{17} \frac{8.6}{26} \frac{8.3}{31} \frac{9.5}{50}$$

$$\frac{12.0}{50} \quad \frac{11.2}{33} \quad \frac{10.3}{18} \quad \frac{10.4}{15} \quad 9.7 \quad \frac{10.0}{14} \quad \frac{9.7}{17} \quad \frac{10.0}{33} \quad \frac{11.7}{50}$$

~~2Rd~~

$$\frac{15.0}{50} \quad \frac{13.8}{40} \quad \frac{13.1}{20} \quad \frac{12.6}{18} \quad \frac{12.0}{7} \quad 12.0 \quad \frac{12.4}{6} \quad \frac{14.0}{9} \quad \frac{15.7}{18} \quad \frac{17.5}{50}$$

~~2Rd~~

$$\frac{4.4}{50} \quad \frac{2.2}{33} \quad \frac{2.0}{23} \quad \frac{1.6}{11} \quad 2.1 \quad \frac{2.1}{1} \quad \frac{3.5}{4} \quad \frac{4.9}{12} \quad \frac{6.7}{30} \quad \frac{8.0}{50}$$

~~2Rd~~

$$\frac{6.7}{50} \quad \frac{3.3}{34} \quad \frac{2.8}{24} \quad \frac{2.5}{11} \quad 3.1 \quad \frac{3.1}{1} \quad \frac{4.0}{8} \quad \frac{5.9}{29} \quad \frac{8.1}{50}$$

~~2Rd~~

$$\frac{9.5}{50} \quad \frac{6.6}{33} \quad \frac{4.3}{18} \quad \frac{3.8}{7} \quad 4.0 \quad \frac{4.3}{5} \quad \frac{3.3}{9} \quad \frac{4.1}{19} \quad \frac{4.9}{33} \quad \frac{6.5}{50}$$

~~2Rd~~

$$\frac{8.0}{50} \quad \frac{5.2}{23} \quad \frac{5.0}{21} \quad \frac{6.0}{15} \quad \frac{5.7}{10} \quad 5.6 \quad \frac{6.1}{10} \quad \frac{4.8}{16} \quad \frac{5.7}{33} \quad \frac{7.3}{50}$$

$$\frac{12.7}{50} \quad \frac{9.4}{30} \quad \frac{9.4}{16} \quad \frac{10.3}{11} \quad 9.7 \quad \frac{10.1}{17} \quad \frac{9.7}{20} \quad \frac{10.5}{50}$$

~~2Rd~~

$$\frac{18.5}{50} \quad \frac{17.4}{24} \quad \frac{15.0}{10} \quad \frac{12.7}{2} \quad 12.5 \quad \frac{12.0}{8} \quad \frac{12.3}{19} \quad \frac{14.5}{24} \quad \frac{15.2}{50}$$

Top NW Cor Conc Step to Ch. Coop Rt Sta 166

10.33

165+03 CalW

10.40 →

Sta

+ π ✓ -

967.32

166

63.3 -

+35

62.6 -

167

61.3 -

168

57.9 -

168 + 83.80 =

168 + 97.39

B.M.

13.55

✓
953.77

$$\begin{array}{ccccccccc} \cancel{42} & & & & & & & & \\ \frac{4.0}{50} & \frac{4.4}{46} & \frac{4.4}{30} & \frac{3.0}{5} & \frac{4.0}{2} & 4.0 & \frac{3.7}{11} & \frac{4.1}{23} & \frac{3.8}{25} & \frac{5.0}{36} & \frac{7.1}{50} \end{array}$$

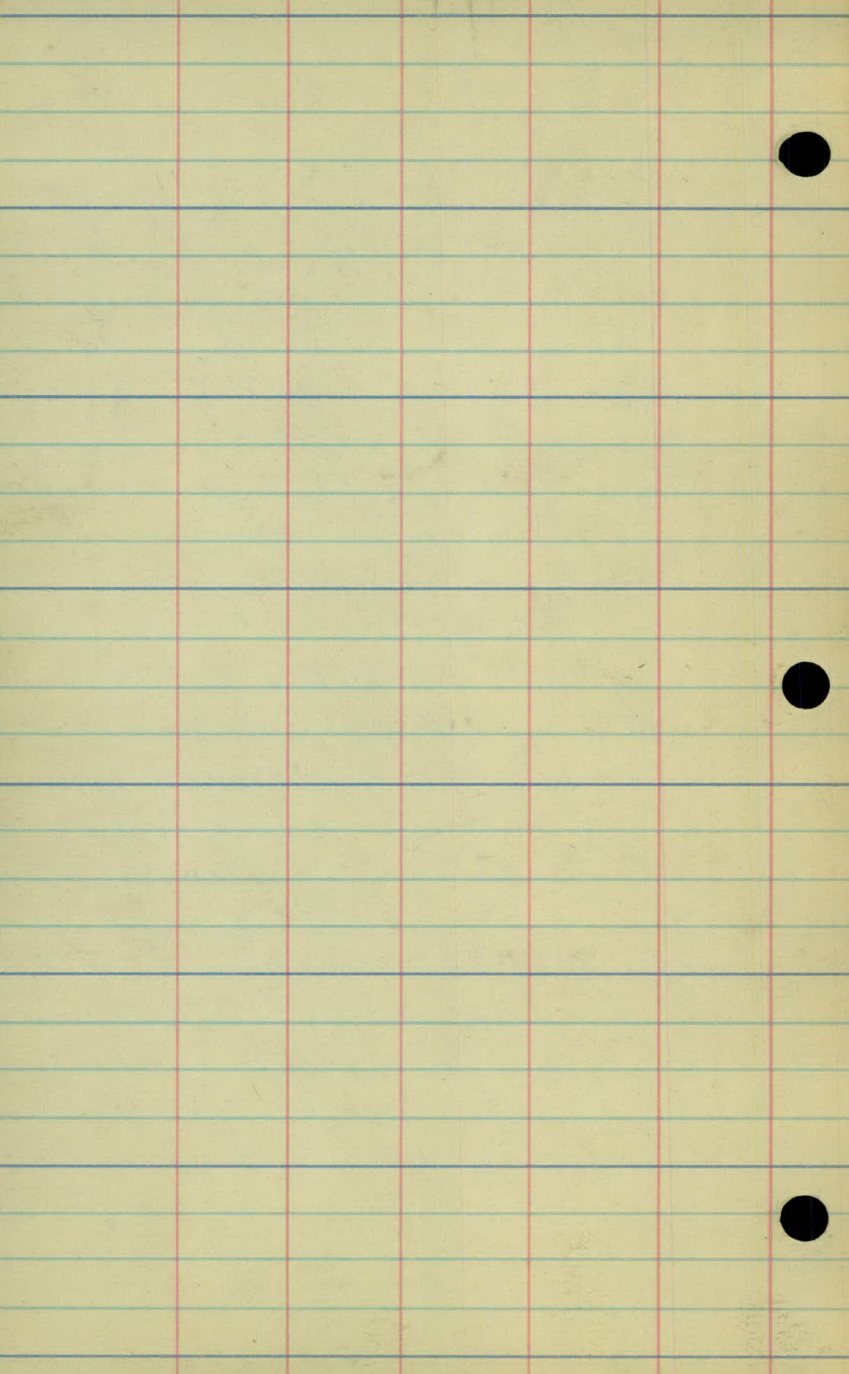
$$\begin{array}{ccccccccc} \cancel{42} & & & & & & & & \\ \frac{1.6}{30} & \frac{2.0}{33} & \frac{2.3}{7} & \frac{4.8}{2} & 4.7 & \frac{4.3}{10} & \frac{4.7}{23} & \frac{4.5}{28} & \frac{6.5}{45} & \frac{7.0}{50} \end{array}$$

$$\begin{array}{ccccccccc} \cancel{42} & & & & & & & & \text{Floor Hub} \\ \frac{7.1}{50} & \frac{6.7}{21} & \frac{6.3}{17} & \frac{6.0}{7} & \frac{4.3}{5} & 6.0 & \frac{5.8}{9} & \frac{6.1}{20} & \frac{5.9}{21} & \frac{5.6}{50} & 3.26 \end{array}$$

$$\begin{array}{ccccccc} \cancel{42} & & & & & & \\ \frac{10.2}{50} & \frac{9.7}{7} & 9.4 & \frac{8.8}{9.21} & \frac{5.1}{30} & \frac{3.9}{44} & \text{Floor Cottage} \\ & & & & & & 1.46 \end{array}$$

1355

Top Hub $\neq$ Sta. 168+83.80



7/2/36

H.T. Portell

X- Sections

Victoria

Sta 168+9739 to Lex. Ave.

Sta + π -



B.M. 940 963.17 953.77

169 53.7 -

170 50.1 -

B.M. 2.21 953.12 12.26 950.91

+50 48.2 -

171 43.7 -

172 41.3 -

173 39.7 -

Q 4.37 944.90 12.59 940.53

+60 36.4 -

174 35.7 -

+60 37.9 -

Top Hub Sta 168+97.39

$$\begin{array}{cccccccccccc} 13.2 & 13.0 & 12.2 & 11.4 & & & & & & & & \\ 50 & 33 & 18 & 3 & 9.5 & 8.8 & 8.2 & 8.6 & 5.1 & 4.0 & 3.5 \\ & & & & & 2 & 13 & 24 & 31 & 40 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} & & & & & & & & & & & \\ 13.7 & 15.9 & 15.0 & & & & & & & & & \\ 50 & 26 & 6 & 13.1 & 11.9 & 12.0 & 11.4 & 5.0 & 3.9 & 2.8 \\ & & & & 10 & 21 & 27 & 36 & 44 & 50 \end{array}$$

SpK in Stp Rt Stp 170+50

$$\begin{array}{cccccccc} 5.3 & & 5.7 & 5.2 & 5.3 & & & \\ 50 & 46 & 31 & 17 & 6 & 4.9 & 6.4 & 7.2 & 6.3 \\ & & & & & & 5 & 20 & 50 \end{array}$$

$$\begin{array}{ccccccc} 6.5 & 7.2 & 8.5 & & 9.7 & 9.2 \\ 50 & 35 & 28 & 9.4 & 31 & 50 \end{array}$$

$$\begin{array}{ccc} 11.0 & & 10.6 \\ 50 & 11.8 & 34 & 11.5 \\ & & & 50 \end{array}$$

$$\begin{array}{ccc} 13.9 & 13.4 & 13.5 & 13.2 \\ 50 & & 31 & 50 \end{array}$$

Top Hub Sta 172+106.1

$$\begin{array}{ccccccc} 6.5 & 8.7 & & 8.5 & 8.0 & 7.9 \\ 50 & 23 & & & 19 & 50 \end{array}$$

$$\begin{array}{ccccccc} 6.7 & 8.5 & & 10.2 & 10.6 \\ 50 & 23 & 9.2 & 16 & 50 \end{array}$$

$$\begin{array}{ccccccc} 4.4 & 6.5 & & 7.1 & 10.4 \\ 50 & 17 & 7.0 & 15 & 50 \end{array}$$

Sta

+

X

-

944.90.

175

36.7

176

38.3

+70

43.3.

177

44.7.

②

12.67

953.31.

4.26

940.64.

+40

46.3

+80

44.0

178

39.3

See next page for ts

179

39.5

+50

43.3

180

45.3

+40

46.9

$$\frac{6.4}{50} \quad 8.2 \quad \frac{8.3}{12} \quad \frac{7.0}{44} \quad \frac{7.1}{50}$$

~~4217~~

$$\frac{4.3}{50} \quad \frac{4.8}{41} \quad \frac{5.6}{36} \quad 6.6 \quad \frac{7.2}{50}$$

~~48~~

$$\frac{3.7}{50} \quad \frac{3.5}{44} \quad \frac{4.1}{31} \quad \frac{1.9}{26} \quad 1.6 \quad \frac{2.2}{50}$$

~~4~~

$$\frac{3.8}{50} \quad \frac{3.5}{39} \quad \frac{4.4}{25} \quad \frac{0.5}{16} \quad 0.2 \quad \frac{3.2}{50}$$

Top East End Est Culu Lt. Sto 177+10

~~48~~

$$\frac{14.0}{50} \quad \frac{13.2}{43} \quad \frac{12.4}{31} \quad \frac{12.6}{23} \quad \frac{13.2}{20} \quad \frac{6.9}{10} \quad 7.0 \quad \frac{6.7}{16} \quad \frac{8.8}{50}$$

~~48~~

$$\frac{12.9}{50-47} \quad \frac{13.5}{70} \quad \frac{12.8}{26} \quad \frac{13.3}{17} \quad \frac{14.4}{16-13} \quad 9.3 \quad \frac{8.9}{4} \quad \frac{6.5}{40} \quad \frac{7.0}{50}$$

~~48~~

$$\frac{19.5}{50} \quad \frac{16.7}{45} \quad \frac{13.3}{37} \quad \frac{12.7}{26} \quad \frac{13.2}{15} \quad \frac{15.2}{8-3} \quad 14.0 \quad \frac{10.2}{9} \quad \frac{8.8}{50}$$

~~48~~

$$\frac{9.8}{50} \quad \frac{12.8}{33} \quad \frac{12.6}{27} \quad \frac{12.1}{24} \quad \frac{11.6}{12} \quad \frac{12.1}{4} \quad 13.8 \quad \frac{15.2}{4} \quad \frac{16.4}{15} \quad \frac{17.6}{50}$$

$$\frac{9.5}{50} \quad \frac{8.3}{39} \quad \frac{8.8}{29} \quad \frac{10.2}{26} \quad \frac{10.0}{17} \quad \frac{9.7}{8} \quad 10.0 \quad \frac{10.3}{5} \quad \frac{11.0}{8} \quad \frac{15.0}{50}$$

$$\frac{2.3}{50} \quad \frac{3.4}{27} \quad \frac{8.0}{17} \quad \frac{8.5}{14} \quad 8.0 \quad \frac{8.6}{12} \quad \frac{3.7}{20} \quad \frac{7.5}{50}$$

$$\frac{10.5}{50} \quad \frac{1.5}{21} \quad \frac{6.7}{11} \quad 6.4 \quad \frac{7.3}{15} \quad \frac{1.4}{19} \quad \frac{6.7}{50}$$

Sta	+	T	-
		953.31	

181			48.9
-----	--	--	------

+50			50.0
-----	--	--	------

BM		1.51	951.80
----	--	------	--------

0	3.23	943.87	12.67	940.64
---	------	--------	-------	--------

178+27			32.9
--------	--	--	------

178+70			39.4
--------	--	--	------

0	3.23	940.64	940.64
---	------	--------	--------

	3.66	955.46	951.80
--	------	--------	--------

181+80			50.5
--------	--	--	------

182			50.4
-----	--	--	------

+50			50.2
-----	--	--	------

183			50.3
-----	--	--	------

$\frac{2.4}{50}$ $\frac{2.6}{31}$ $\frac{4.7}{13}$ 4.4 $\frac{5.0}{16}$ $\frac{5.3}{19}$ $\frac{4.0}{20}$ $\frac{5.4}{50}$

$\frac{0.5}{50}$ $\frac{1.2}{18}$ $\frac{3.7}{11}$ 3.3 $\frac{3.6}{16}$ $\frac{1.1}{23}$ $\frac{5.0}{50}$

SpK in 24" Oak 40' Lt Sto 181

AL No End Cdr

FL No End Cdr

$\frac{9.8}{50}$ $\frac{10.2}{42}$ $\frac{3.5}{34}$ $\frac{3.0}{25}$ $\frac{4.0}{14}$ $\frac{11.94}{4}$ 11.0 $\frac{11.0}{4}$ $\frac{4.3}{12}$ $\frac{2.6}{50}$

$\frac{6.2}{50}$ $\frac{6.1}{37}$ $\frac{3.0}{29}$ $\frac{2.7}{17}$ $\frac{3.2}{6}$ 4.5 $\frac{13.0}{14}$ $\frac{15.3}{25}$ $\frac{16.0}{50}$

Top Cdr Lt 177+10

SpK in 24" Oak 40' Lt Sto 181

$\frac{2.1}{50}$ $\frac{0.5}{17}$ $\frac{5.3}{11}$ 5.0 $\frac{5.7}{14}$ $\frac{5.2}{23}$ $\frac{8.8}{50}$

5.1

$\frac{2.2}{50}$ $\frac{8.0}{23}$ $\frac{8.0}{14}$ $\frac{5.7}{10}$ 5.3 $\frac{5.7}{10}$ $\frac{9.5}{19}$ $\frac{12.4}{50}$

$\frac{2.3}{50}$ $\frac{4.3}{23}$ $\frac{5.8}{14}$ $\frac{5.4}{12}$ 5.2 $\frac{5.7}{9}$ $\frac{6.9}{13}$ $\frac{10.5}{50}$

Sta + π -
955.46

+50

51.0

184

52.1

184 + 2520 =

184 + 96.65

BM 13.41 966.15 · 2.72 952.74 ·

185 52.9

+40

54.7

186 57.5

+50

58.2

187 58.4

188 58.9

189 61.9

+50

64.9

0 13.20

✓
977.24 · 2.11

✓
964.04 ·

$$\frac{6.0}{50} \quad \frac{6.3}{20} \quad \frac{4.5}{15} \quad 4.5 \quad \frac{5.5}{9} \quad \frac{11.0}{19} \quad \frac{14.8}{50}$$

$$\frac{3.5}{50} \quad \frac{5.4}{40} \quad \frac{4.8}{22} \quad \frac{3.1}{18} \quad 3.4 \quad \frac{4.2}{8} \quad \frac{9.8}{18} \quad \frac{14.4}{50}$$

SpK @ $\frac{1}{4}$ Cor Sta 183+96.65

$$\frac{7.8}{50} \quad \frac{13.3}{17} \quad \frac{13.0}{7} \quad 13.3 \quad \frac{13.8}{6} \quad \frac{18.5}{50}$$

$$\frac{7.1}{50} \quad \frac{6.1}{35} \quad \frac{7.5}{24} \quad \frac{12.0}{18} \quad \frac{10.2}{8} \quad 11.5 \quad \frac{12.0}{6} \quad \frac{10.9}{9} \quad \frac{7.3}{12} \quad \frac{7.0}{20} \quad \frac{11.4}{50}$$

$$\frac{0.4}{50} \quad \frac{0.2}{45} \quad \frac{70.6}{37} \quad \frac{8.8}{22} \quad \frac{8.4}{10} \quad 8.7 \quad \frac{8.8}{2} \quad \frac{7.1}{6} \quad \frac{4.1}{8} \quad \frac{5.0}{16} \quad \frac{3.8}{52}$$

$$\frac{5.1}{50} \quad \frac{5.7}{33} \quad \frac{6.7}{28} \quad \frac{8.1}{24} \quad \frac{7.6}{12} \quad 8.0 \quad \frac{8.1}{7} \quad \frac{7.0}{8} \quad \frac{7.1}{19} \quad \frac{5.0}{50}$$

$$\frac{7.5}{50} \quad \frac{7.3}{43} \quad \frac{8.0}{26} \quad \frac{7.2}{23} \quad \frac{7.0}{12} \quad 7.8 \quad \frac{7.0}{6} \quad \frac{7.8}{50}$$

$$\frac{7.5}{50} \quad \frac{7.7}{27} \quad \frac{6.3}{21} \quad \frac{6.0}{12} \quad 7.3 \quad \frac{9.3}{5} \quad \frac{10.3}{16} \quad \frac{11.4}{50}$$

FlkLw 7.00

16.06 Fl. Lulu

$$\frac{6.4}{50} \quad \frac{5.4}{33} \quad \frac{3.6}{24} \quad \frac{3.2}{12} \quad 4.3 \quad \frac{8.4}{7} \quad \frac{10.3}{23} \quad \frac{10.8}{50}$$

$$+3.2 \quad \frac{1.3}{50} \quad \frac{1.5}{40} \quad \frac{0.7}{23} \quad \frac{0.7}{10} \quad 13 \quad \frac{1.3}{1} \quad \frac{5.7}{7} \quad \frac{9.4}{25} \quad \frac{11.0}{50}$$

Top Fcc Post Rt. Sta. 188+95

Sta

977.24.

190

68.4

+50

71.8

191

73.2

0

12.66

989.11.

0.79

976.45.

190 + 50

191

191 + 50

75.0

192

75.4

+50

74.8

193

73.5

0

0.32

976.82.

12.61

976.50.

+50

71.5

$$\frac{2.8}{50} \quad \frac{7.31}{45} \quad \frac{3.0}{33} \quad \frac{6.8}{26} \quad \frac{7.0}{22} \quad \frac{8.8}{18} \quad \frac{8.4}{8} \quad 8.8 \quad \frac{9.1}{5} \quad \frac{8.7}{9} \quad \frac{14.2}{31} \quad \frac{17.4}{50}$$

$$\frac{3.8}{21} \quad \frac{4.5}{17} \quad \frac{5.8}{16} \quad \frac{5.4}{6} \quad 5.4 \quad \frac{6.1}{10} \quad \frac{2.8}{14} \quad \frac{5.5}{32} \quad \frac{8.7}{50}$$

$$4.0 \quad \frac{4.5}{12} \quad \frac{+0.5}{17} \quad \frac{1.4}{33} \quad \frac{3.3}{50}$$

$$\frac{2.8}{50} \quad \frac{2.3}{43} \quad \frac{4.2}{40} \quad \frac{5.9}{31}$$

$$(17.3)$$

$$\frac{3.9}{50} \quad \frac{3.5}{38} \quad \frac{4.6}{36} \quad \frac{6.2}{24}$$

$$(15.9)$$

$$\frac{4.9}{50} \quad \frac{6.1}{26} \quad \frac{7.4}{21} \quad \frac{12.6}{16} \quad \frac{14.6}{18} \quad 14.1 \quad \frac{14.5}{12} \quad \frac{13.5}{14} \quad \frac{10.5}{17} \quad \frac{12.0}{35} \quad \frac{12.7}{50}$$

$$\frac{5.7}{50} \quad \frac{7.2}{20} \quad \frac{11.6}{16} \quad \frac{14.0}{11} \quad 13.7 \quad \frac{14.0}{14} \quad \frac{12.9}{17} \quad \frac{8.1}{26} \quad \frac{12.5}{50}$$

$$\frac{8.9}{50} \quad \frac{9.1}{42} \quad \frac{8.3}{18} \quad \frac{14.5}{9} \quad 14.3 \quad \frac{14.6}{15} \quad \frac{13.7}{18} \quad \frac{10.2}{20} \quad \frac{11.7}{31} \quad \frac{12.7}{50}$$

$$\frac{16.4}{50} \quad \frac{16.0}{29} \quad \frac{14.9}{10} \quad \frac{16.0}{4} \quad 15.6 \quad \frac{15.8}{17} \quad \frac{15.0}{14} \quad \frac{11.7}{23} \quad \frac{11.2}{50}$$

Nail in T.P. Rt Sta. 192+50

$$\frac{7.0}{50} \quad \frac{6.9}{17} \quad \frac{7.7}{11} \quad \frac{5.7}{6} \quad 5.3 \quad \frac{5.0}{6} \quad \frac{5.2}{14} \quad \frac{4.6}{23-50}$$

Sta + π -

976.82.

194

69.9

+90

65.8

195

65.3

196

0

0.44 965.11. 12.15 964.67.

B.M

2.68

Victoria
962.43.2 965.63^{Lexington}

196

60.4

196 +50

59.6

197

59.5

+50

59.6

+67

60.1

198

61.7

+1620

Ley

62.4

For Culv Elev See Ley Notes

$$\frac{8.3}{50} \quad \frac{8.2}{8} \quad \frac{7.1}{6} \quad 6.9 \quad \frac{6.8}{7} \quad \frac{7.1}{18} \quad \frac{6.5}{21} \quad \frac{5.5}{50}$$

$$\frac{5.2}{50} \quad \frac{3.4}{12} \quad \frac{11.1}{5} \quad 11.0 \quad \frac{10.8}{7} \quad \frac{11.2}{18} \quad \frac{10.2}{20} \quad \frac{8.9}{23} \quad \frac{4.8}{26} \quad \frac{3.4}{50}$$

11.5

$$\frac{13.0}{50} \quad \frac{12.5}{39} \quad \frac{14.1}{18} \quad (16.4) \quad \frac{11.2}{24} \quad \frac{10.3}{31} \quad \frac{10.2}{50}$$

Top Rock 10' Wt Sta 195+65

Top Iron Pin Viet. + Lex Intersection

$$12-9 \quad \frac{6.1}{7} \quad \frac{5.0}{7} \quad 4.7 \quad \frac{5.3}{15} \quad \frac{5.1}{17}$$

$$\frac{8.4}{50} \quad \frac{7.8}{42} \quad \frac{8.6}{24} \quad \frac{6.2}{17} \quad \frac{6.0}{14} \quad 5.5 \quad \frac{6.5}{14} \quad \frac{7.3}{19} \quad \frac{4.7}{25} \quad \frac{4.9}{36} \quad \frac{4.0}{50}$$

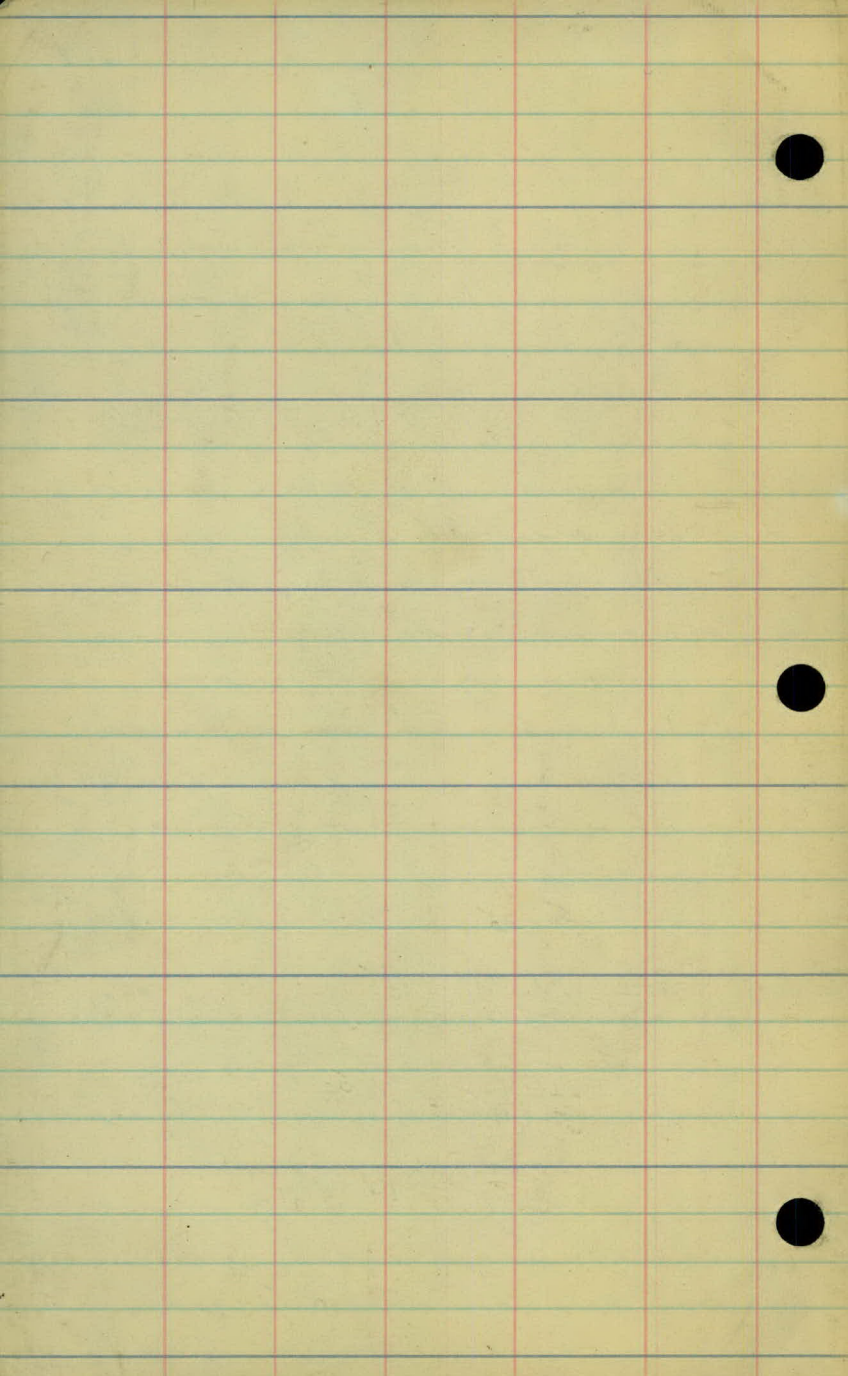
$$\frac{17.2}{50} \quad \frac{16.0}{35} \quad \frac{6.5}{18} \quad 5.6 \quad \frac{6.0}{12} \quad \frac{12.1}{26} \quad \frac{12.0}{32} \quad \frac{9.0}{50}$$

$$\frac{21.5}{50} \quad \frac{20.5}{44} \quad \frac{7.1}{21} \quad \frac{6.1}{14} \quad 5.5 \quad \frac{6.0}{14} \quad \frac{6.9}{19} \quad \frac{18.4}{44} \quad \frac{19.7}{50}$$

$$\frac{22.4}{50} \quad \frac{21.0}{46} \quad \frac{6.3}{24} \quad \frac{5.5}{13} \quad 5.0 \quad \frac{5.6}{15} \quad \frac{7.5}{19} \quad \frac{19.0}{44} \quad \frac{20.2}{50}$$

$$\frac{1.9}{50} \quad \frac{2.0}{41} \quad 3.4 \quad \frac{4.0}{17} \quad \frac{5.1}{38-50}$$

$$\frac{0.8}{50} \quad \frac{1.5}{27} \quad 2.7 \quad \frac{4.0}{30} \quad \frac{4.6}{50}$$



74
Little Revision

75+00 To 87+00

Grade + Line Revision

@
Lundgren's Property 6/2/36

B.M.	3.52	967.74	✓			964.22
75					64.8	62.8 -
76					66.2	62.8.
77					67.4	62.9
0	11.14	976.55	✓	2.33	965.41	✓
	54.80	4" Wid Rt				
78	+0.3 -0.3	0 0			67.8	65.0 -
79	+1.1 -1.1	3.0			67.4	69.0 -
80	+1.1 -1.1	3.7			66.2	68.7 -
0	0.91	965.33	✓	12.13	964.42	✓
81	+1.1 -1.1	3.7			64.4	63.5
82	+0.7 -0.7	0.3			61.8	57.9
83	+0.0 -0.0	0.0			58.7	56.2
0	2.63	958.65	✓	9.31	956.02	✓
84					55.8	54.8
85					54.3	53.4

SpK in 15" Oak Rt Sta 74

$$\begin{array}{r} D.C. 1.2 \\ 3.7 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 4.4 \\ 20 \end{array} \quad \begin{array}{r} 5.3 \\ 18 \end{array} \quad \begin{array}{r} 5.2 \\ 12 \end{array}$$

$$\begin{array}{r} F2.1 \\ 5.0 \end{array} \quad \begin{array}{r} 5.7 \\ 11 \end{array} \quad \begin{array}{r} 9.5 \\ 21 \end{array}$$

$$\begin{array}{r} F8.4 \\ 11.3 \\ \hline 32.5 \end{array}$$

$$\begin{array}{r} D.C. 2.8 \\ 0.7 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 1.8 \\ 27 \end{array} \quad \begin{array}{r} 5.0 \\ 23 \end{array} \quad \begin{array}{r} 5.7 \\ 19 \end{array} \quad \begin{array}{r} 5.2 \\ 14 \end{array}$$

$$\begin{array}{r} F3.5 \\ 5.0 \\ \hline 0 \end{array}$$

$$\begin{array}{r} 5.5 \\ 8 \end{array} \quad \begin{array}{r} 7.0 \\ 15 \end{array}$$

$$\begin{array}{r} F7.4 \\ 9.1 \\ \hline 31.2 \end{array}$$

$$\begin{array}{r} F5.6 \\ 5.9 \\ \hline 27.2 \end{array}$$

$$\begin{array}{r} 5.2 \\ 30 \end{array} \quad \begin{array}{r} 6.2 \\ 27 \end{array} \quad \begin{array}{r} 4.8 \\ 18 \end{array}$$

$$\begin{array}{r} F4.6 \\ 4.8 \end{array} \quad \begin{array}{r} 5.3 \\ 6 \end{array} \quad \begin{array}{r} 8.7 \\ 15 \end{array}$$

$$\begin{array}{r} F9.7 \\ 16.0 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} D.C. 0.0 \\ 10.8 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 10.8 \\ 31 \end{array} \quad \begin{array}{r} 12.2 \\ 27 \end{array} \quad \begin{array}{r} 11.3 \\ 19 \end{array}$$

$$\begin{array}{r} F2.8 \\ 11.6 \end{array} \quad \begin{array}{r} 14.2 \\ 17 \end{array}$$

$$\begin{array}{r} F7.0 \\ 16.1 \\ \hline 30.0 \end{array}$$

D.C. 6.3

$$\begin{array}{r} 3.8 \\ 33.0 \end{array} \quad \begin{array}{r} 4.1 \\ 25 \end{array} \quad \begin{array}{r} 7.8 \\ 20 \end{array} \quad \begin{array}{r} 7.6 \\ 14 \end{array}$$

$$\begin{array}{r} C. 1.5 \\ 7.7 \end{array} \quad \begin{array}{r} 7.6 \\ 6 \end{array} \quad \begin{array}{r} 2.1 \\ 12 \end{array}$$

$$\begin{array}{r} D.C. 10.9 \\ 1.9 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} D.C. 4.5 \\ 6.9 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 9.4 \\ 30 \end{array} \quad \begin{array}{r} 9.2 \\ 15 \end{array} \quad \begin{array}{r} 10.1 \\ 2 \end{array}$$

$$\begin{array}{r} C. 2.4 \\ 7.9 \end{array} \quad \begin{array}{r} 8.2 \\ 7 \end{array}$$

$$\begin{array}{r} D.C. 6.3 \\ 7.7 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} D.C. 0.0 \\ 1.9 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 2.4 \\ 18 \end{array} \quad \begin{array}{r} 3.2 \\ 6 \end{array} \quad \begin{array}{r} 1.6 \\ 4 \end{array}$$

$$\begin{array}{r} F0.9 \\ 1.8 \end{array} \quad \begin{array}{r} 3.4 \\ 5 \end{array}$$

$$\begin{array}{r} F4.6 \\ 5.5 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} F3.5 \\ 16.7 \end{array}$$

$$\begin{array}{r} F3.4 \\ 6.2 \\ \hline 22.8 \end{array}$$

$$\begin{array}{r} 6.5 \\ 14 \end{array}$$

$$\begin{array}{r} F3.9 \\ 7.4 \end{array} \quad \begin{array}{r} 10.4 \\ 6 \end{array}$$

$$\begin{array}{r} F11.0 \\ 15.2 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} F2.9 \\ 9.5 \\ \hline 21.8 \end{array}$$

$$\begin{array}{r} 10.7 \\ 27 \end{array} \quad \begin{array}{r} 9.2 \\ 22 \end{array}$$

$$\begin{array}{r} F2.5 \\ 9.1 \end{array} \quad \begin{array}{r} 9.7 \\ 5 \end{array} \quad \begin{array}{r} 12.0 \\ 10 \end{array} \quad \begin{array}{r} 12.7 \\ 27 \end{array}$$

$$\begin{array}{r} F6.7 \\ 13.3 \\ \hline 29.4 \end{array}$$

$$\begin{array}{r} D.C. 1.9 \\ 3.5 \\ \hline 27.0 \end{array}$$

$$\begin{array}{r} 4.5 \\ 22 \end{array} \quad \begin{array}{r} 3.8 \\ 18 \end{array}$$

$$\begin{array}{r} F1.0 \\ 3.9 \end{array} \quad \begin{array}{r} 4.4 \\ 6 \end{array} \quad \begin{array}{r} 6.3 \\ 26 \end{array}$$

$$\begin{array}{r} D.C. 0.0 \\ 5.4 \\ \hline 19.8 \end{array}$$

$$\begin{array}{r} D.C. 0.4 \\ 6.0 \\ \hline 18.2 \end{array}$$

$$\begin{array}{r} 5.9 \\ 22 \end{array} \quad \begin{array}{r} 5.2 \\ 18 \end{array}$$

$$\begin{array}{r} F0.9 \\ 5.3 \end{array} \quad \begin{array}{r} 5.7 \\ 5 \end{array} \quad \begin{array}{r} 9.3 \\ 12 \end{array}$$

$$\begin{array}{r} F6.0 \\ 10.4 \\ \hline 28.0 \end{array}$$

32' Top - 2.5' Ditch Section Right - 2.0' Dt. Sec Lt. 2:1 Fill Slopes

✓
958.65

86

52.5

53.8

87

52.5

53.9

B.M.

3.24

955.41

✓
955.41

6.2
82 8.7

DC.3.0
5.2
23.0

21 $\frac{5.7}{19}$ $\frac{5.4}{17}$

C1.3
4.9 $\frac{5.2}{8}$ $\frac{5.9}{11}$ $\frac{5.7}{13}$

DC.3.1
5.6
33.0

6.2
82 8.7

(No SK Set) → DC.3.1
Cm R4E $\frac{5.1}{33}$

C1.5
4.7 $\frac{DC.3.4}{5.3}$
33.0

NW. Anchor bolt Sash line Wq Wag

323.83 20

218 + 41.30

105 + 41.90

CROSS SECTIONS
VICTORIA ST.
FABYANSKI PROPERTY

9-26-40

Party:
R. P.
A. M.
L. G.
C. F.

plotted 9/27/40

Sta.	t	π	-	Elev.
B.M.	0.33	952.13.		951.80
T.P.	3.21	945.46.	9.88	942.25
T.P.	13.45.	958.16.	0.75	944.71.
B.M.	13.71	967.69.	4.18	953.98.
167+25	Sec. thru Ent.		9.0	58.7
+ 30			9.2	58.5
+ 32			9.2	58.5
+ 50			9.7	58.0
+ 75			10.4	57.3
168			11.2	56.5
+ 17			11.8	55.9
+ 25			12.1	55.6
+ 50			13.0	54.7
B.M.			13.71	953.98

953.98

E

(stump)
Spike 24" Oak 40' Lt. Sto. 181+00

Spike P.P. Lt. 168+60

9.6 9.4 8.6 7.4
9.0 10 22 34 50

9.2 9.6 9.0 7.6
14 29 50

South FL - 15° 20'

FL 15" to C.M.

9.7 9.7 11.75 10.8 10.7 9.3 4.9 5.0
9.2 13 17 24 20 26 29 33 50

11.33

10.2 10.4 11.2 11.0 9.6 5.0 4.6
9.7 9 16 18 25 28 32 50

10.9 11.2 11.9 11.4 9.4 5.1 4.6 3.7
10.4 8 16 19 25 29 33 45 50

12.0 12.2 12.9 12.7 10.5 5.3 4.3 (House)
11.2 12 18 21 25 29 34 43

12.4 12.7 13.6 13.2 10.0 5.3 4.9 4.6
11.8 10 18 22 26 31 36 39.5 43

Fr. Cor

12.6 12.9 14.1 13.7 9.9 5.3 5.1 4.7
12.1 10 18 22 26 31 35 39 43

13.6 13.9 14.8 14.8 11.2 7.1 6.6 5.9
13.0 11 18 21 26 32 34.5 41 43

Spike P.P. Lt. 168+60

E

