

300 K-68 Dr. 6

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

----- *Plan* ----- Survey

----- *RICE - CENTERVILLE CONN.* -----

From ----- To -----

Road Acc't. No. -----

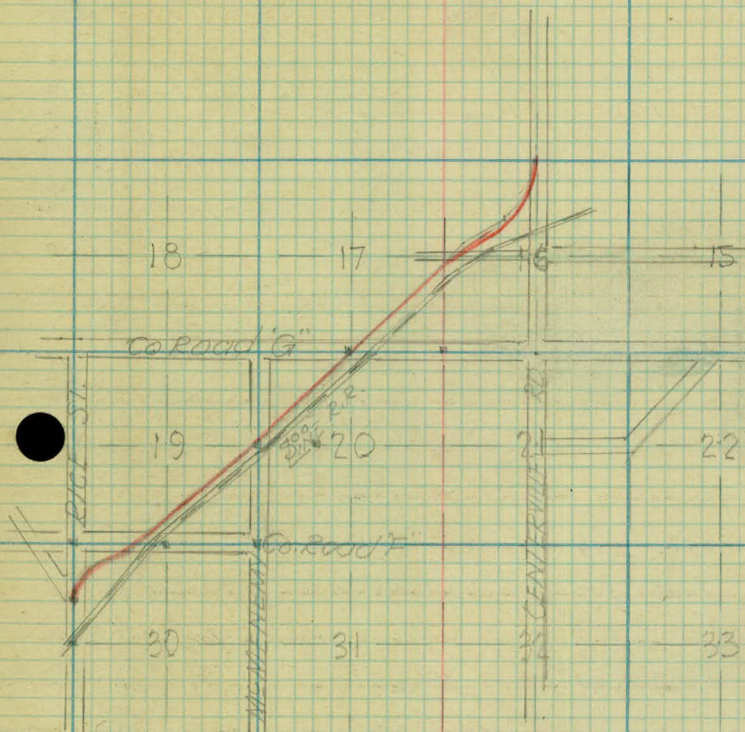
Date Filed *1935* -----

File -----

Plan Survey

Rice - Centerville Cut-off

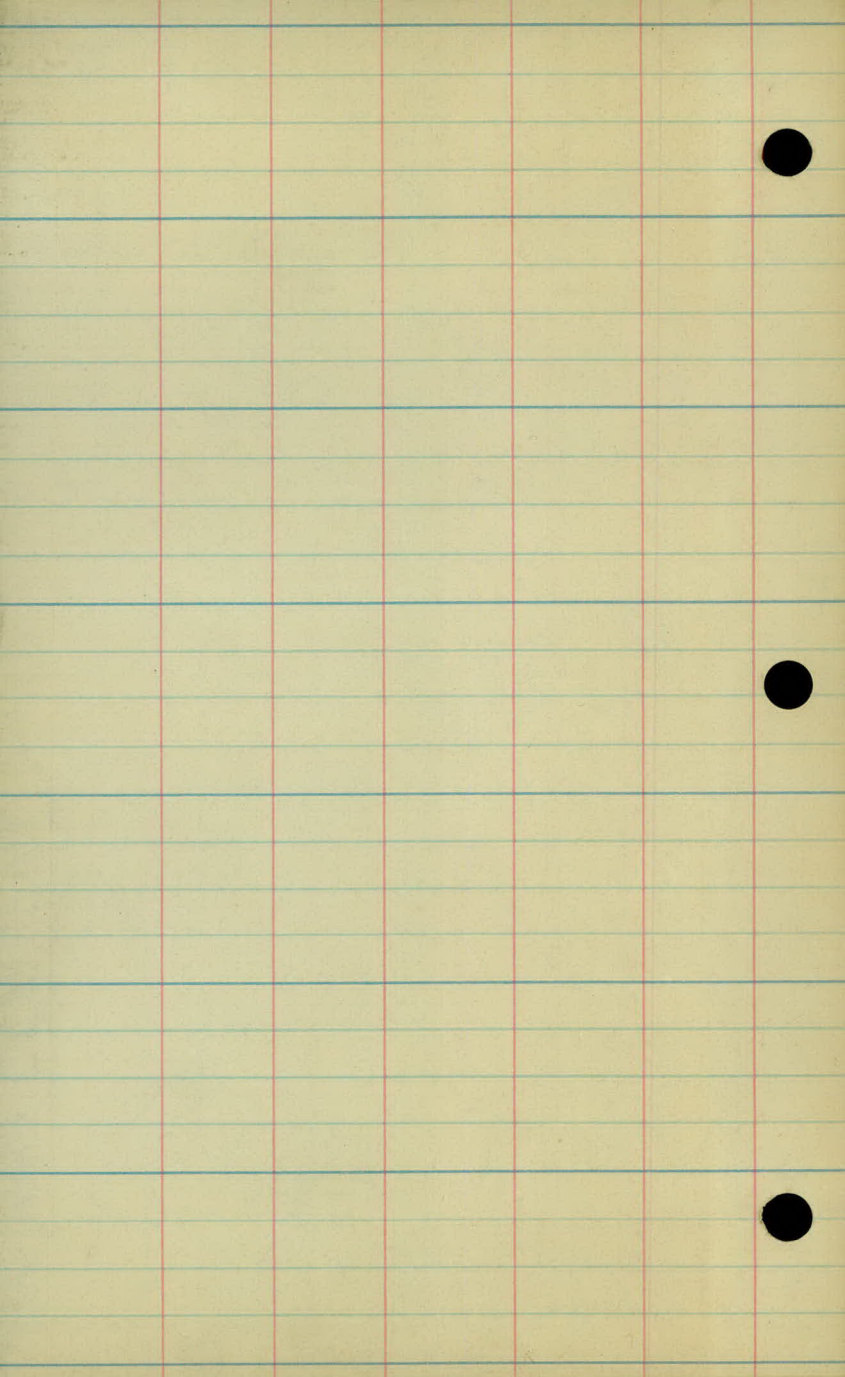
White Bear Township.



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W. H. Carlson
Oct. 12, 1935



alignment

Station Point Lt. ^{Angle} Rt.

14+44.9	P.T.	35°-00'	
14		32°-45.3'	
+50		30°-15.3'	
13		27°-45.3'	
+50		25°-15.3'	
12		22°-45.3'	
+50		20°-15.3'	Pt. 11+46.6
11		17°-45.3'	10°-00' Rt.
+50		15°-15.3'	Δ 70°-00'
10		12°-45.3'	T. 401.7' ✓
+50		10°-15.3'	L. 700.00 ✓
9		7°-45.3'	R= 573.69 ✓
+50		5°-15.3'	
8 ^{50.05'}		2°-45.3'	
7+44.9	P.C.	0°-00'	

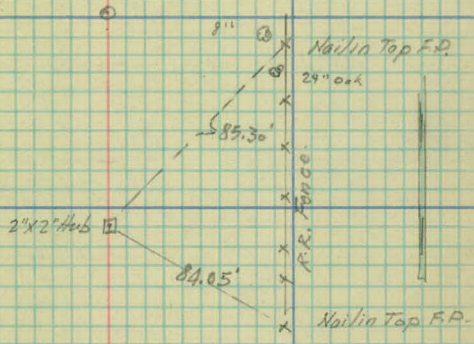
0+00 / ^{1.00} LINE R.R.

Sta.	Point	Lt.	Angle	Rt.
27+39.94	P.O.T.			
26+80.87	P.T.		9°29'	
+50			8°52'	
26			7°52'	
+50			6°52'	P.I. 244 46.0
25			5°52'	A 18°-58'
+50			4°52'	D° 4°00' Lt
24			3°52'	T. 239.3 ✓
+50			2°52'	L. 474.17 ✓
23			1°52'	R. 1432.69 ✓
+50			0°52'	
22+06.7	P.C.		0°00'	

21+39.17 P.O.T.

17+47.4 P.O.T.

7/20/25 2
Windy



Nail Top 6" Oak Stp.

Station	Point	Angle Lt	Rt.
---------	-------	-------------	-----

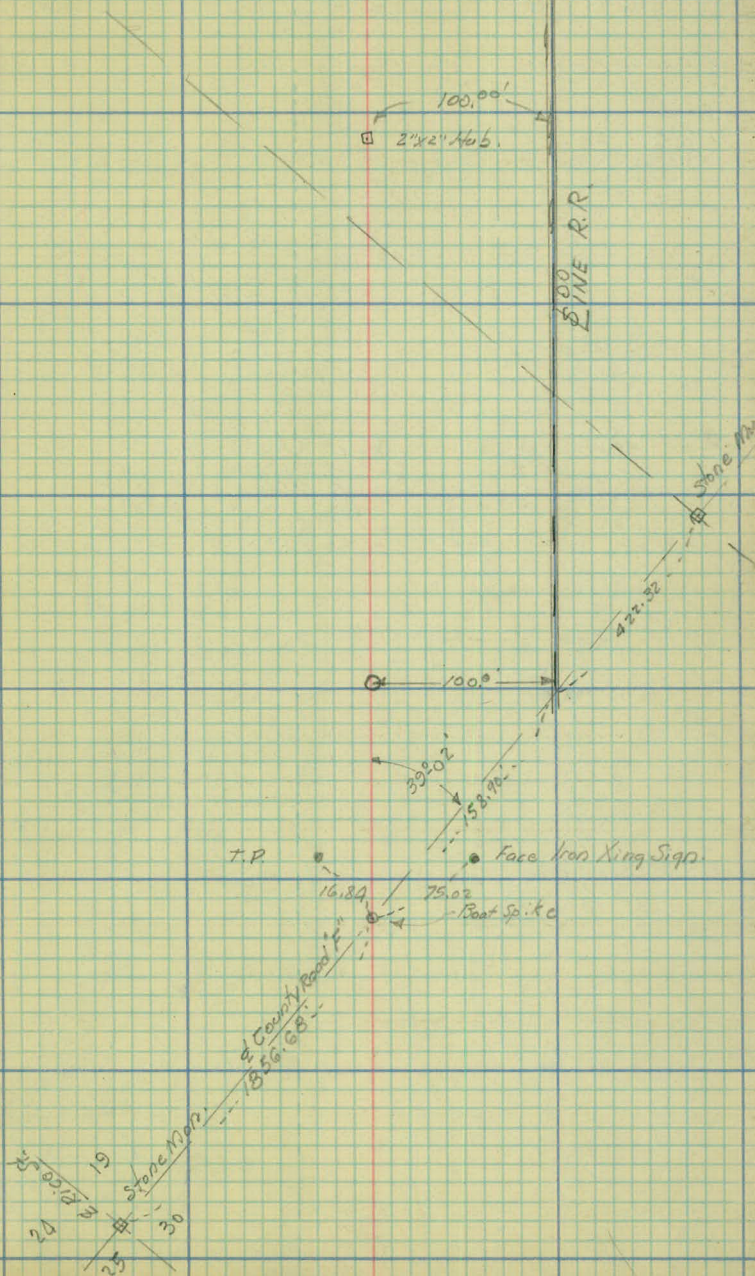
40+99.44	P.O.T.		
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32+58			
-------	--	--	--

31+30.45	P.O.T.		
----------	--------	--	--

9/20/35

5



Station	Point	Angle	
		Lt	Rt.
79+15.4	P.T.	3°-27'	
79		3°-22.4'	
+50		3°-07.4'	
78		2°-52.4'	
+50		2°-37.4'	
77		2°-22.4'	
+50		2°-07.4'	
76		1°-52.4'	
+70.4 = 2 curve		1°-03.5'	
+50		1°-37.4'	
			$P_1 = 75+70.8$
75		1°-22.4'	$\Delta 6°-54'$
+50		1°-07.4'	$D = 1200'$ Lt.
74		0°-52.4'	$T = 345.4$ ✓
+50		0°-37.4'	$L.C. 690.0$ ✓
73		0°-22.4'	$R = 5729.65$ ✓
+50		0°-07.4'	
72+25.40	P.C.	0°-00'	
71+91.15	P.O.T.		
60+00	P.O.T.		
54+50	P.O.T.		

R.T. 79+15.4

100.0

9/27/35

Windy

Mon.
Mr. Co. n

Ref Pt.

3 Nails
in T.R.

59°-24'

Ref. Point

45.02'

2"x2" Hub

38°-52'

Semi Tan

89°-41'

1/4 Cor.

30.27'

28.87'

89°-41'

PC-72+25.4

2"x2" Hub 99.85'

89-41

51-22

38-57

180-120

100.0

128.05'

100.001

S. FERR.

Co. Rd. 1
Mon.

2"x2" Hub

100.00

Station	Point	Lt	Angle	Rt.
---------	-------	----	-------	-----

98+73.5	P.T.		2°30.5'	
---------	------	--	---------	--

98			2°15.8'	
----	--	--	---------	--

+50			2°05.8'	
-----	--	--	---------	--

97			1°55.8'	
----	--	--	---------	--

+50			1°45.8'	
-----	--	--	---------	--

96			1°35.8'	
----	--	--	---------	--

+50			1°25.8'	
-----	--	--	---------	--

95			1°15.8'	P.I. 94+97.5
----	--	--	---------	--------------

				$\Delta 5°01'$ Rt.
--	--	--	--	--------------------

94			0°55.8'	D- 0°40'
----	--	--	---------	----------

				T. 376.5' ✓
--	--	--	--	-------------

93			0°35.8'	L. 752.5' ✓
----	--	--	---------	-------------

				R= 8594.42 ✓
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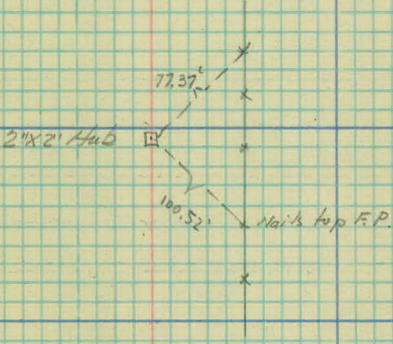
92			0°15.8'	
----	--	--	---------	--

91+21.0	P.O.		0°00'	
---------	------	--	-------	--

85+27.82	P.O.T.			
----------	--------	--	--	--

9/30/35
Very Windy

100.00'
P.T. 98+73.5



P.O. 91+21.0
100.00'

1"X2" Stake

Stone R.R.
100.00'

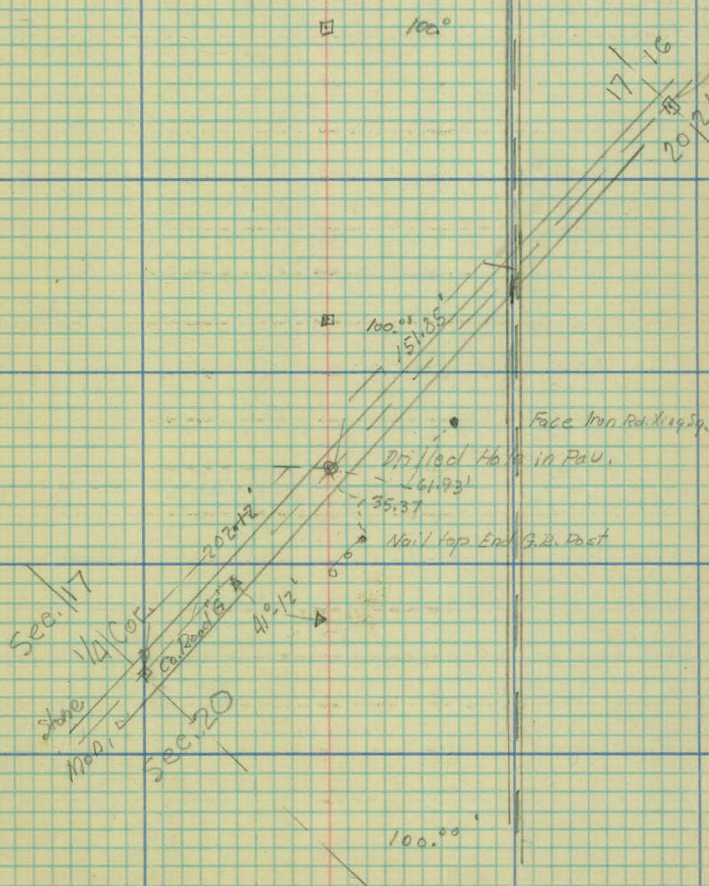
Station Point Angle
Lt Rt.

130+95.39 P.O.T.

117+45.0 P.O.T.

111+69.13 P.O.T.
± Co. Road "G"

10/2/35
Very Windy
Cold.



Station	Point	Angle	
		Lt.	Rt.
146+00.2	P.T.	14°00'	
+50		13°15'	
145		12°30'	
+50		11°45'	
144		11°00'	
+50		10°15'	
143		9°30'	
+50		8°45'	
142		8°00'	
+50	P.O.C.	7°15'	R.I. 141+43.03
141		6°30'	3°-G, Rt.
+50		5°45'	Δ 28°00'
140		5°00'	T. 476.24' ✓
+50		4°15'	L.C. 933.33 ✓
139		3°30'	R= 1910.08 ✓
+50		2°45'	
138		2°00'	
+50		1°15'	
137		0°29.9'	
136+66.79	P.C.	0°00'	

10/8/35

100.0'

2"x2" Hub - □

100.0'

Station	Point	Angle	
		Lt	Rt

166+54.29 P.O.T.

161+12.82 P.T. 92.11'

161 8°59.5'

+50 8°14.5'

160 7°29.5'

+50 6°44.5'

P.I. = 159+09.4

159 5°59.5'

3° C.Lt.

+50 5°14.5'

$\Delta 180.22'$

158 100.71 - center curve 4°25.5'

4°29.5'

T. 308.8' ✓

+50 3°44.5'

L.C. 612.22' ✓

157 2°59.5'

R = 1910.08' ✓

+50 2°14.5'

156 1°29.5'

+50 0°44.5'

155+00.6 P.C. 0°00'

10/9/25

① 100.00

① 100.00

B 6' Oak

6.17

H

16.83

B 6' Oak

① 100.0

Station	Point	Angle	Rt
---------	-------	-------	----

174+60.25	P.T.	29°28.5'	
-----------	------	----------	--

174		26°27.8'	
-----	--	----------	--

+50		23°57.8'	
-----	--	----------	--

173		21°27.8'	
-----	--	----------	--

+50		18°57.8'	
-----	--	----------	--

172		16°27.8'	
-----	--	----------	--

+50		13°57.8'	
-----	--	----------	--

171		11°27.8'	
-----	--	----------	--

+50		8°57.8'	
-----	--	---------	--

170		6°27.8'	
-----	--	---------	--

+50		3°57.8'	
-----	--	---------	--

169		1°27.8'	
-----	--	---------	--

168+70.75	P.C.		
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P.I. = 171+95.00

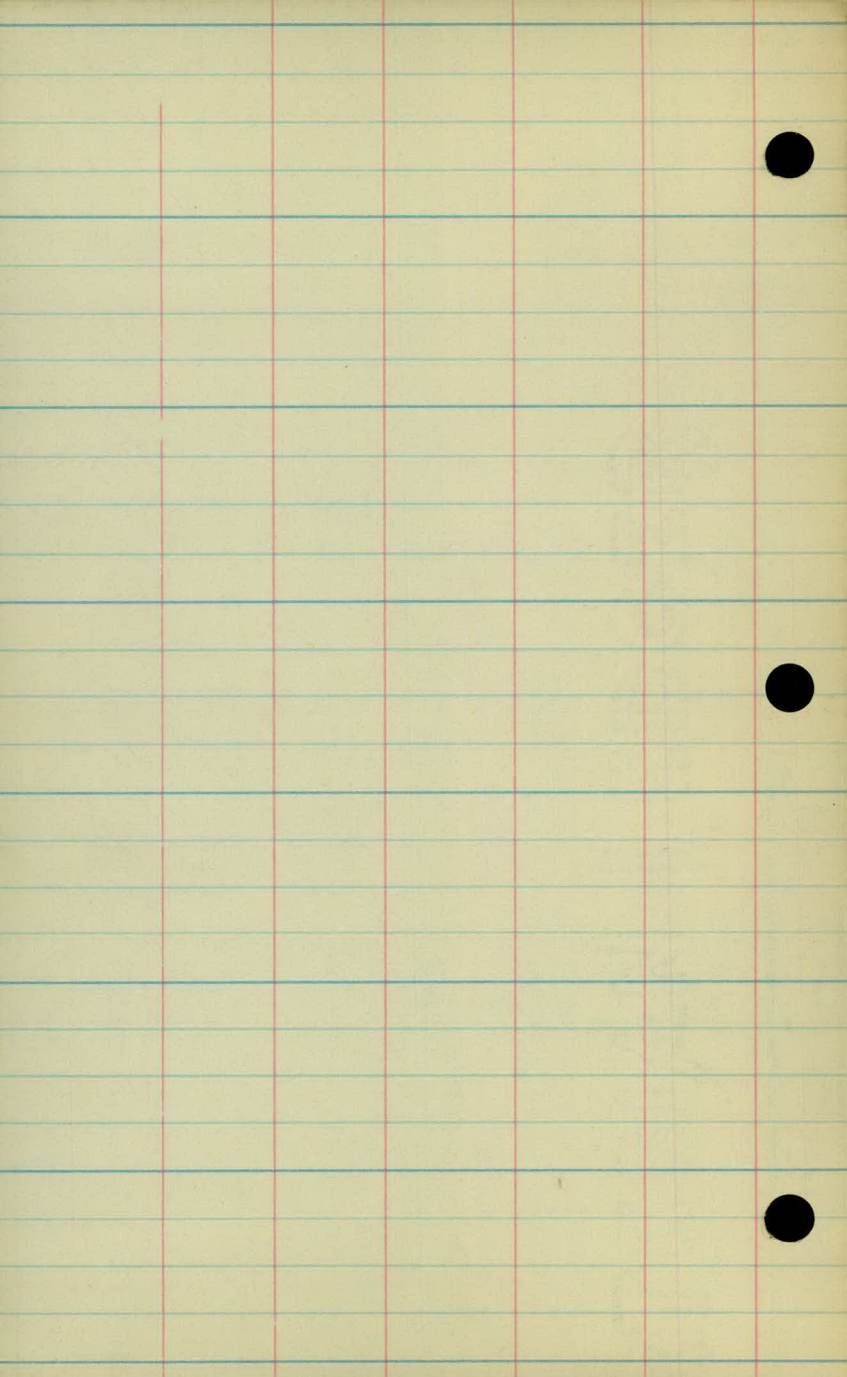
Δ 58°57'

D. 10° Lt.

T. 324.25' ✓

L.C. 589.5 ✓

R= 573.69 ✓



Topography-

5

4

3

2

1

oto 7 Five

+78-T.P.

+41-T.P. 28'

Sub Gutter
78'

+01-T.P. 28'

+64-Curb 11.5-120

+59-T.P. 28'

Face
Curb 17.6

+29-T.P. 28'

+22-Curb 17.6-19'

+15-Ain Curb 14.3

Curb 14.4

+0+10.5-Face Pier 14.9

+0+51.5-

Gutter & Curb

one Curb conc

Scattered Oaks

Timber 60'

Rub Graft 18'

+62-Beg. Timber 60'

+64-Curb 11.5-120

+28-Curb 16.6-17.5
+77-Ain Curb 14

+56-Face Pier 14.5

S Curb 14
+09.3-Face Pier 14.6

W.A.C.

K.A.

L.B.H.

9/21/55

12

11

E

10

150

545 - 27.5

9

35.3 - 9.5

150

227 2.7

8

150 9.5

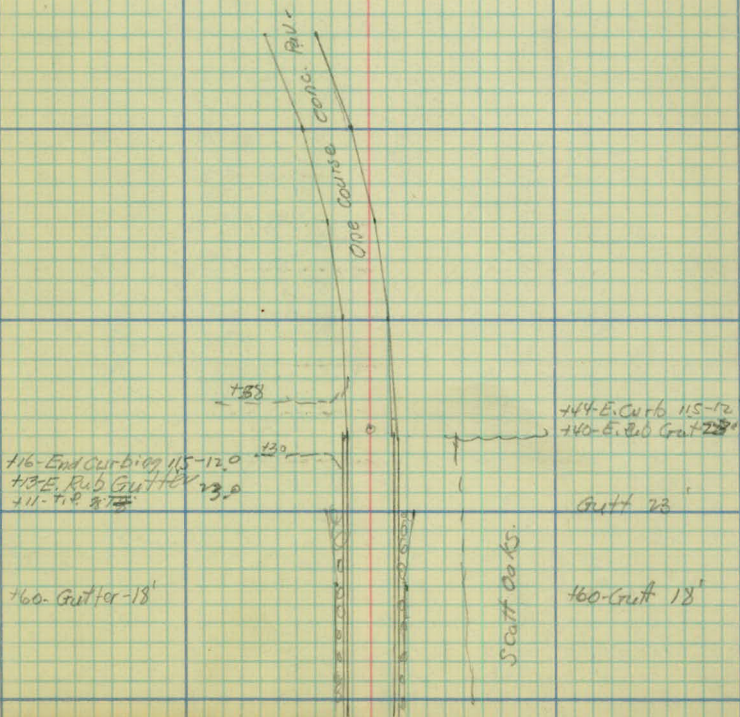
E

+49.9 = RC. 10°-C. Rt. = E Road Lt. and Ent Rt.

7

6 to

— Open Field. —
— Weeds —



19

18

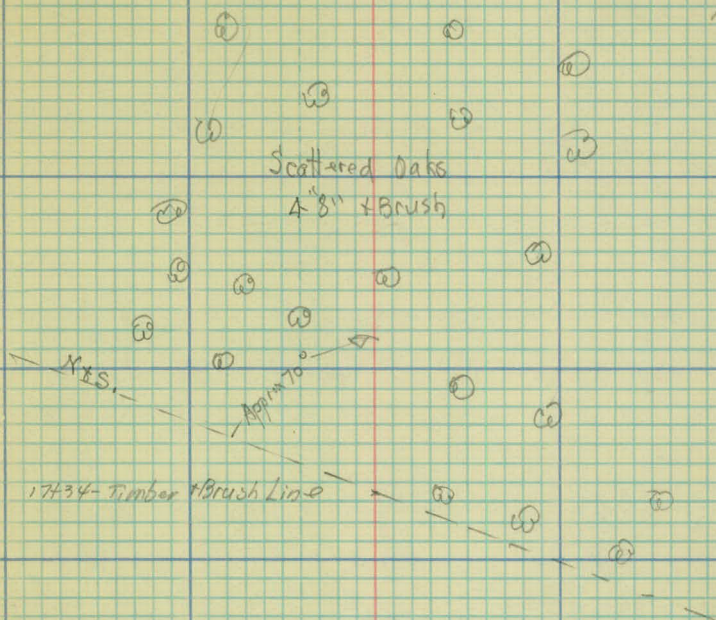
17

16

15

14

13



Open Field

180.87 P.T.

16 oaks

26

7 oaks

25

7 oaks

24

5 oaks.

23

3 oaks

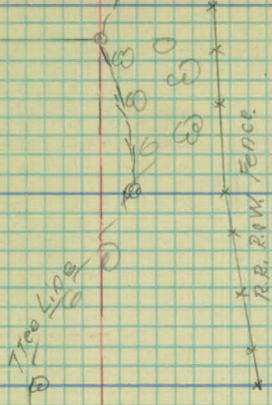
150 ~~~~~

106.7 = P.C. 4° C. Lt.

22

21

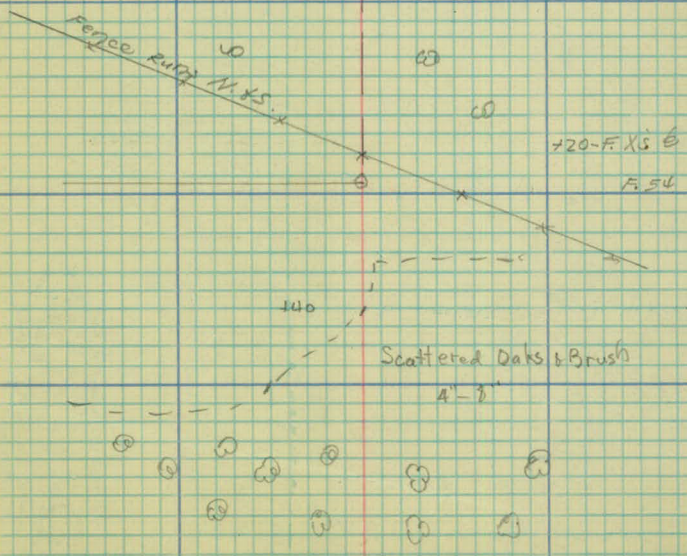
20



F.69

F.85

Water Dept Property
 Scattered Oaks (thin)
 w 4" 10" o
 Pine Seedlings.



+20-F X'S B

F.54

Good Way

33

32

38 - 67'

150 - 0 -

134.45 = 1 Co. 21" F

0 - 115"

31

130 oaks

30

10 - oaks

29

6 - oaks

28

12 - oaks.

27

+30-Brush-39'

Thick
Pop
Brush

+50-Trail/40'

Trail 1/2-3'

+40-2 Trail X's 2

Plank Xing

+58-2 Co. 84. F 100
+45-E. Feb. 51
+40-T.R. 69'

500
DUNE R.R.

+85-Fence X is E

+85-R.R. Xing Sq. 56

+56-T.P. 4'

+50-2 Trail 1 68'

+45-F. Cor. 48

+85-Fen X's 2

+84-Gulch

19

1/2 X 40' G.M.
M.Y.S.

F-20

260 Road 1/2" Groove + Dike

Water 20' of Road
500' Trail
Pine Seedling

F-52

F-56

Out Tree Line

F-59

F-62

40

39

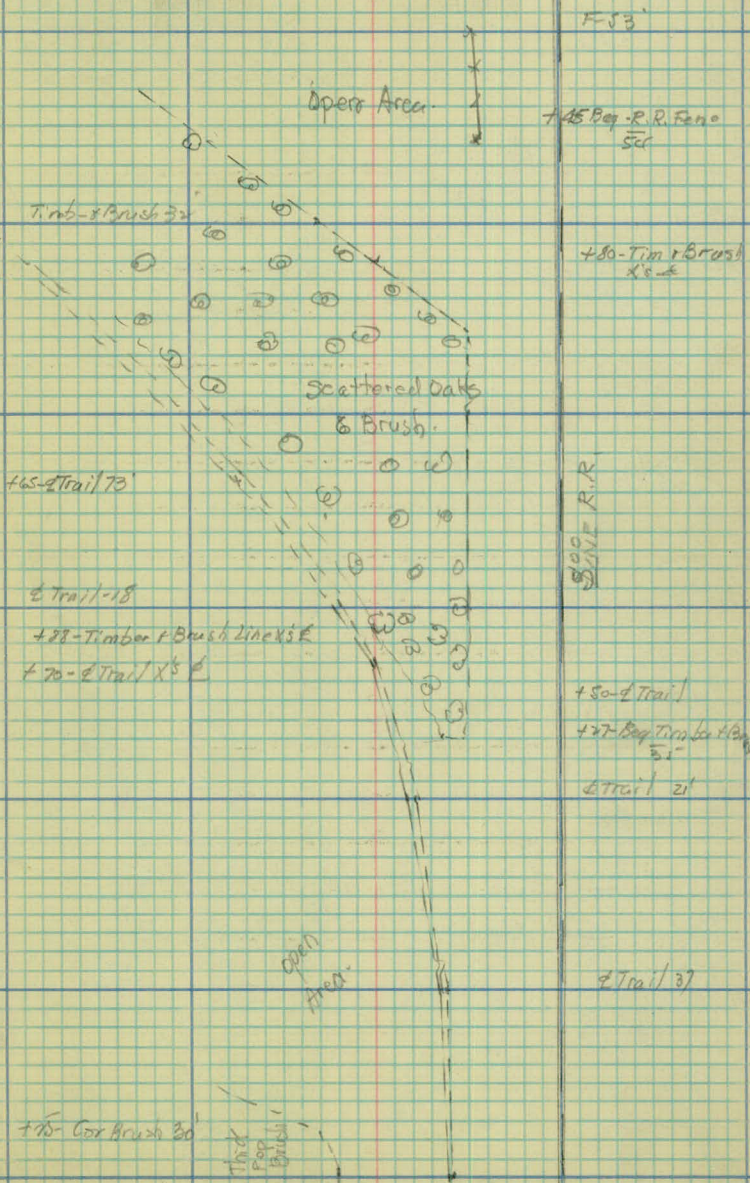
38

37

36

35

34



47

46

45

44

43

Log Bridge-

43+33 - 4 Bridge

201' - 20 ft →

Pile Trestle 10'-Ties -

+51 - E. Water 100'

+31 - E " 100'

42

41

9/26/35

Cultivated

40'

50'

70'

Marsh

150-80' Firm Bog Dry

P.R. Fence (W.G.)

500' LINE R.R.

+107-24" Oak 20'

Ditch 8' (Creek Sect)

+82-24" Oak 15'

150' Ditch Spills

+37 Ditch

F-50'

145-F. 52'

201'

Top Bank

Top Bank

+94 End Trestle

+84-80'

+71 ✓

+57 ✓

+44 ✓

+30 ✓

+16 ✓

+115-80' 1/2 Trestle

+96-8" Oak 40'

+76-12" Oak 23'

54

53

52

51

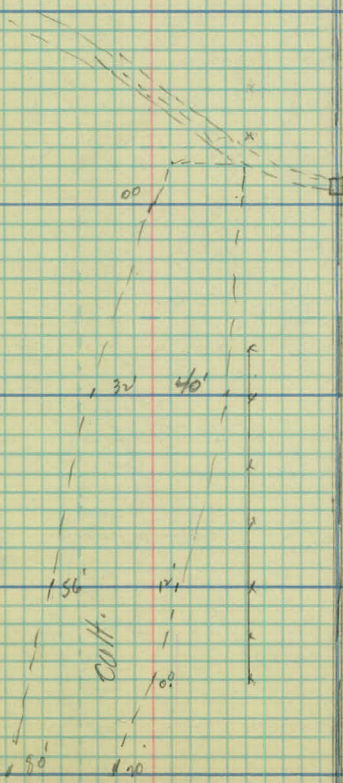
50

49

48

Fence N/G

+54 Trail X's E



500
2415

+37-51 F 53'
+10-2 RR X-02
100

+25-F 53'

Bep F 150-53'

61

60

59

58

57

56

55

140'

20

Meadow.

+50'
60'

+100' X 5'

to 4' Xing
100'

cultivated.

X 85' Line

46'

+30' X 5'

+15'
13

68

67

66

65

64

63

62

+18FXSE

+no

Willow
Brush

+185XSE

491

+193 SC 14
491Small Oaks
Brush

75

74

73

125.4 R.C. 12 Curve LT

72

71

70

69

9/28/35

+100 - E Trk 22
100.15
(50.89)

+50 - E Trk,
100.15

cultivated

17 M.G.

Sec. Line.

Rel. 74-41'

+66 - Solid X's E

+100 - Solid X's E

+215 - Fence X's E

+80 - 20" Oak 18'

+66 - 18" Oak 33'

+20 - 20" Oak 17'

+73 - 10" Oak 17'

+59 - 16" Oak 27'

+18 - 14" Oak 10'

+20 - 10" Oak 20'

+94 - 36" Oak 3'

Stone Man

Rubbish

Gravel

+25 - E Trk 99.85

+81 - 13 Fence 45
71+66 - E X. 179
100'

+72 - 18" Oak 47'

+16 - 24" Oak 27'

+12 - 26" Oak 91'

F.S.

Scattered Oaks
pasture

+05 - 24" Oak 4'

+97 - 18" Oak 35'

+95 - 12" Oak 11'

+25 - 14" Oak 18'

+73 - 18" Oak 25'

82

81

80

+15.4

P.T.

79

78

77

76

Field Ent.

+28 King
100

Right of Way fence down

+15.4 = ETRK.
99.73

Cultivated.

89

88

87

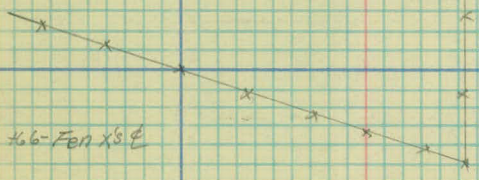
86

85

84

83

Scattered Oak
Shops.
Pasture.



+66-Fer x's &

+50-F. Cor 53

100.00

Cultivated

96

95

94

93

92

+210 P.O. 0°40' C. Rt.

91

90

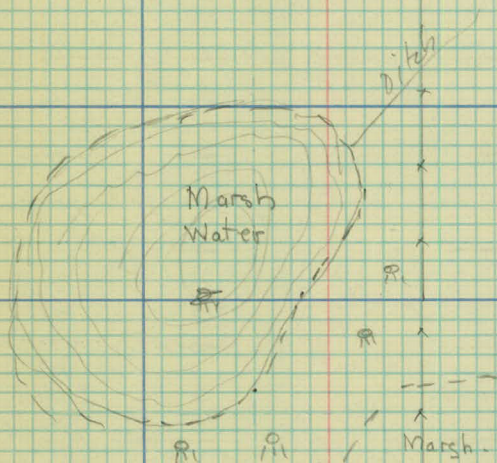
9/30/35
Windy

Scattered

Oak Stumps

Pasture

F- 52'



Scattered
Oak Stps
Pasture

(Note: Stumps
are rotten)

Marsh

E-52'

Marsh

103

102

101

100

99

173.5 RT.

98

97

- Peat -

Meadow.
Pasture.

+73.5-F-39.5

+6.1-Feg K's ②

+

①

Ga. 10

+45-F. Cor. 52

110

109

108

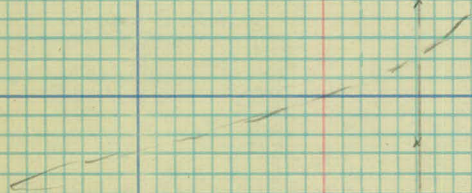
107

106

105

104

Cultivated.



Peat
Meadow
Pasture.

7000 A.P.P. 32

117

116

115

114

113

112

169, 13 & Co. Rd "G"

111

F-52'

Cultivated.

+15-Fence X's 6

+73-Cor. F. 40

+55-E.G.R. 30
+54-P.N.X's 6

+35-E.G.R. 9

+15-R.R. Warning 29'

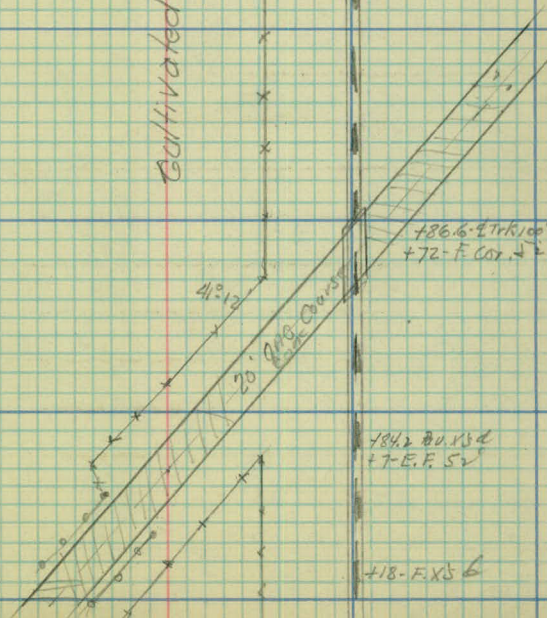
41:12

20' Aug. Course

+86.6-4 Tr. 100'
+72-F. Cor. 1/2

+84.2 Bu. X's 4
+7-E.F. 52'

+18-F. X's 6



124

123

122

121

120

119

118

$\begin{array}{r} 103 \\ \times 80 \\ \hline 000 \\ 8260 \\ \hline 82600 \end{array}$

8-8" books
Small Scotts-

Weeds.
Low Ground.

Cultivate

+26°20'00"K50'

131

130

129

128

127

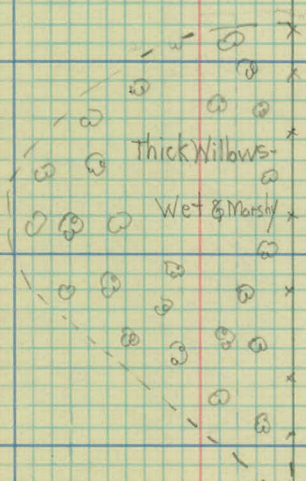
126

125

Cultivated

403-20' Oak 48'

19 12295
F-51'



Cultivated

F-50'

138

137

136

135

134

133

132

11
①

Weeds &
Brush

10^x

①

①

①

①

①

①

①

①

①

①

①

①

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①

①

①

①

①

①

①

①

①

①

①

①

Trk 101.5

Trk 100.9

194-18'00k 50'

F-52'

+40-20'00k 48'

F-52'

188-6'00k 50'

F-53'

Cult.

145

144

143

142

102.65
2.35
105.00

141

140

139

99.15
23.5
101.50

F53
Dit 3' 32

Dry
Peat

101.5

2 Ditch 18'

Fence 51'

103

2 Ditch 7'

Posture
Peat

104.3

+50 - Ditch 52'

+01 - Fence 182'

+02 - Ditch 156'

105.

+78 - Fence 56'

+17 - Cult. 136'

Cult.

105.

+50 - F. 55'
Dit 57'
27rk 105.0

105.

104.0

Cult.

Woods

152

151

150

57
27

149

148

147

146

Cultivated.

+37- Fen 152

+41- Fen. cor. 52'
+30- F. ENT.

Cult.
(peat Dry.)

+17- Fen 152

F-52'

Cultv.

+30 Bog Cult. 150

Deep
ditch 38'

(No peat.)

ditch

159

158

157

156

+00.6 P.C.

155

154

153

Timber 18

+80-Box Feb. 51

+46-E. Fence 52

top of Xing 100'

F-58

(41-47)

Thick Oaks
and Oak Brush

F-45

+70-Feg X's

+60 Fen Cor. 34'

Cut 1/20 feet

101.0

F-48

100.0

166

165

164

163

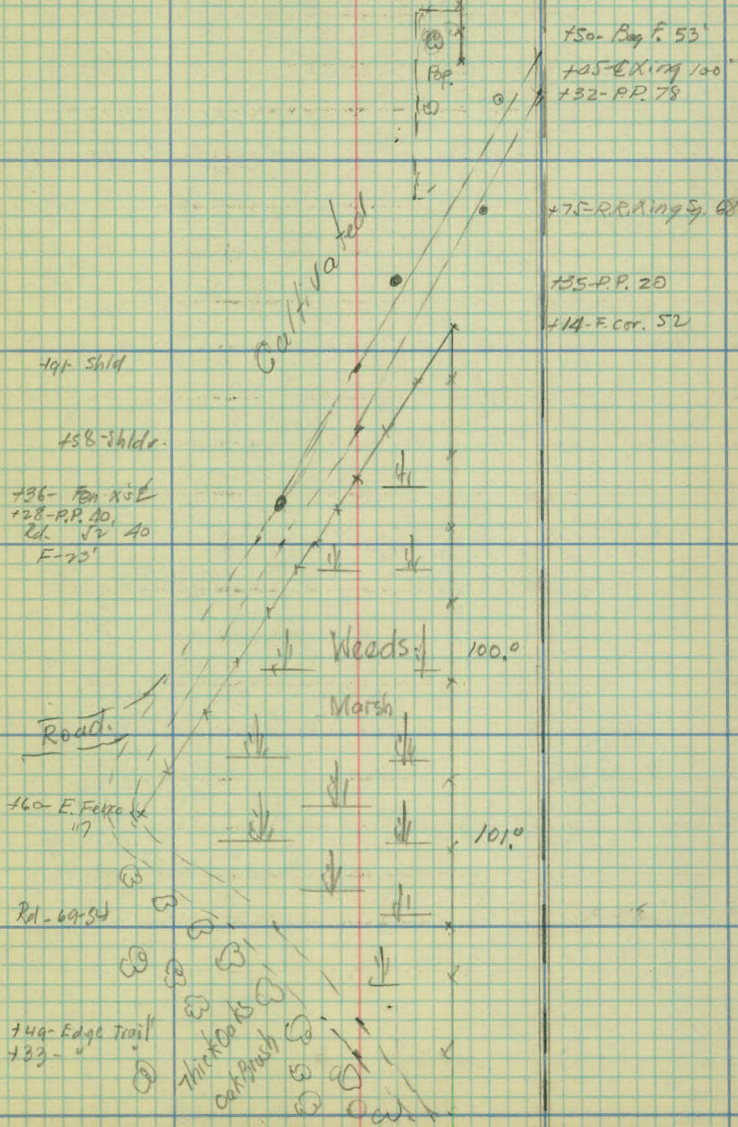
27

162

412.82 - P.T.

161

160



173

172

171

170

169

+70.75 = P.C. 10° C. L.

168

167

G.R. 7'
 Rd. 7'
 F-29'

G.R. 14'
 Rd. 14' 3/10

154-G.R. 54'
 F-2'

Pen. x 3 1/2 180

see center Red Map

Shld 16'-G.R. 15'

150-shld to 160-G.R. 34'

104-8" Tw. W. 11.2'
 F-35'

100-F. cor 10'

Pasture.

(Note: Track is Tangent ahead)

+75-30" Pop. 65

+78-F. 15 1/2
 +75-F. 53
 +50-F. 71

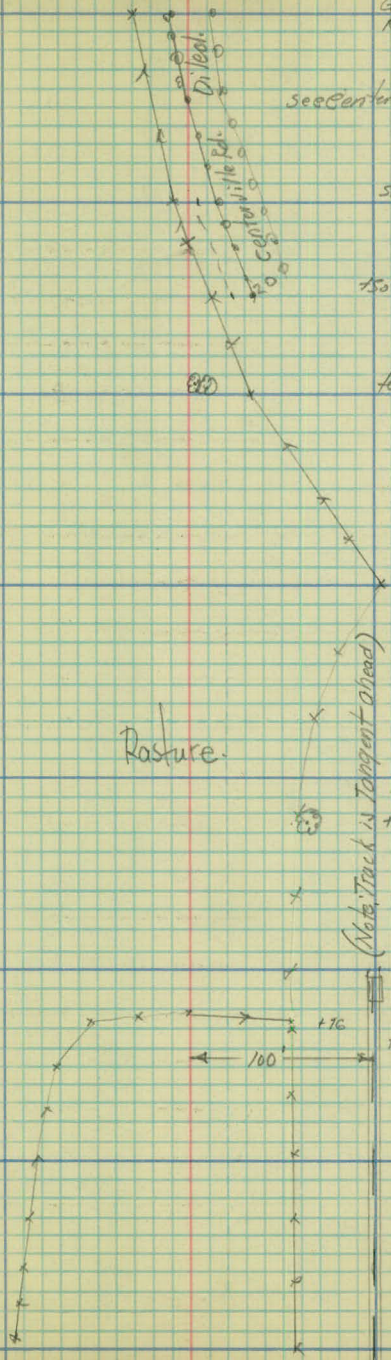
189-9' x 79' 100'

+71-Pen 55

F-84'

+07-F. 97'

F-51



176

175

174

W.H.C.
K.A.
L.B.H.

37

Oct. 12, 1935

Tangent ahead to Centerline
See cent Road Map Survey

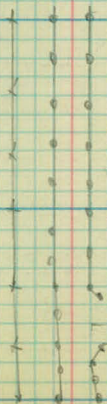
F-31.5 G.R. 10.

G.R. 10.5 F-33'

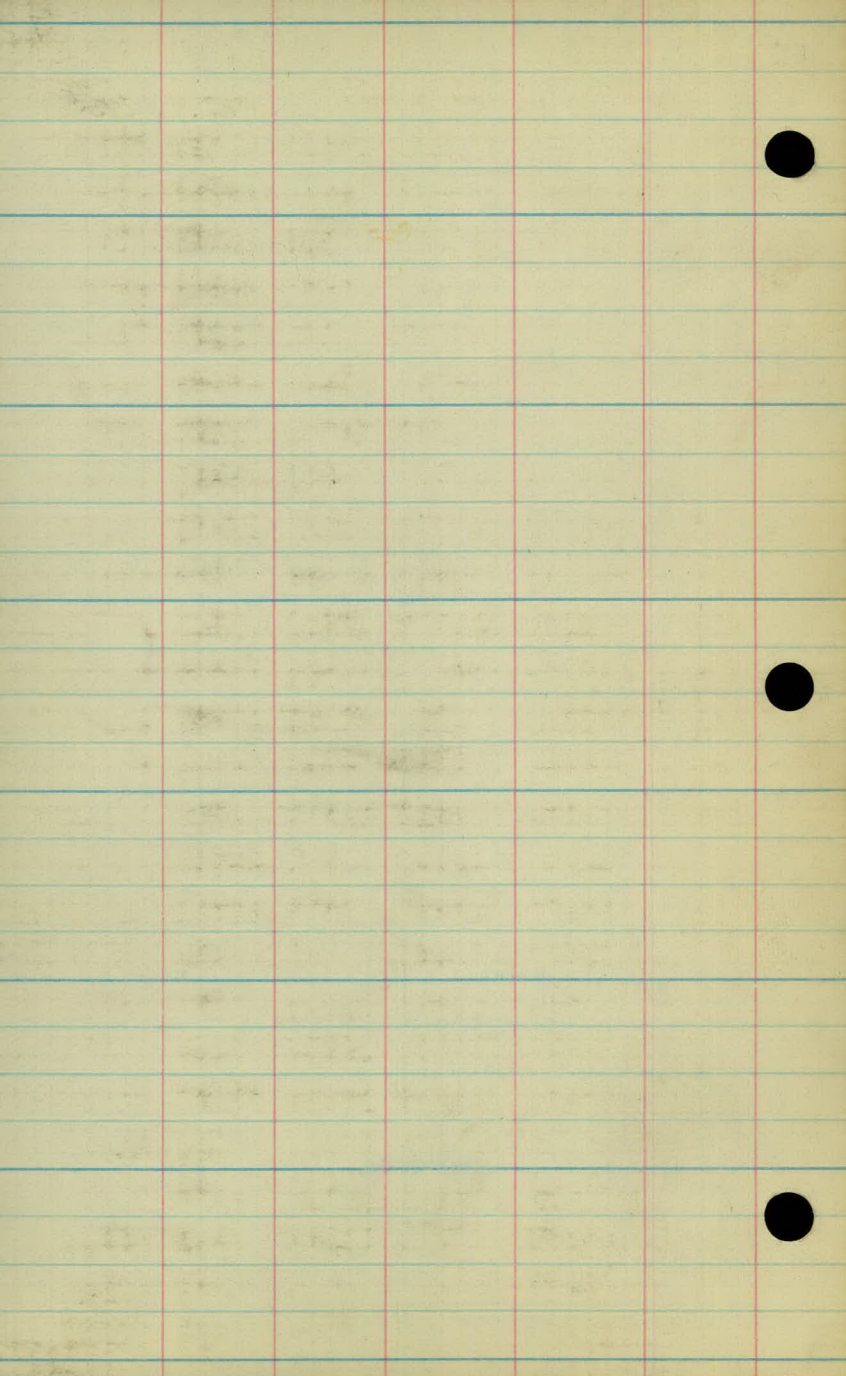
F-31.5
G.R. 9.5

+60 - G.R. 9.5
+60 - F-31.5

Pasture



G.R. 10.5 F-34.5
+60 1/2" TW 0. 24' - F-34.5
+56 - End C.V. 27'
+30 - 12' x 26' V.I.P.
+59 - G.R. 11'
+54 - Beg. G.R. 16
+40 - End.
+28 - End G.R. 17'
+20 - G.R. 12'



Cross - Sections

Station	+	π	-	Elev.
B.M.	4.09	928.01 ✓		923.92 ✓
6+0				915.37 ✓
+50				18.04 ✓
7+0				20.28 ✓
+40				21.58 ✓
+45				21.75 ✓
8+0				23.09 ✓
+50				23.50 ✓
+92				23.4 ✓
9+0				21.7 ✓
+28				23.7 ✓
+50				24.2 ✓
10+0				23.9 ✓
T.P.	5.60	931.40 ✓	3.21	924.80 ✓

Lt.

8

Rt.

39

P.R. Spike in 12" Oak 50 ft. Sta. 7154

60	55	11.8	12.3	13.0	12.40	12.76	12.64	12.71	12.36	12.8	12.1	12.0	6.2	6.3
50	35	24	18	16	11.5	11.5		11.5	11.5	17	19	24	37	50

(10.5)

5.8	6.0	9.9	9.5	10.7	9.65	10.00	9.97	10.07	9.71	10.2	9.6	9.3	6.2	6.0
50	30	24	18	16	11.5	11.5		11.5	11.5	16	18	25	33	50

(7.7)

5.4	5.7	8.7	7.8	7.46	7.83	7.73	7.81	7.50	7.5	8.3	7.0	5.7	5.5
50	26	22	17	11.5	11.5		11.5	11.5	16	20	25	34	50

(6.4)

5.4	6.3	6.53	6.43	6.48	6.15	6.0	7.3	5.9	5.3
50	25	12.0	PAV	11.5	11.5	16	21	25	50

(6.3)

5.4	6.36	6.36	6.34	5.2	5.4
50	12.0	PAV	12.0	30	50

(4.9)

3.5	3.8	7.1	6.8	5.1	4.98	4.92	5.00	5.1	5.3
50	38	31	28	21	15.0	PAV	9.5	30	50

2.8	6.9	6.6	4.6	4.53	4.40	4.51	4.53	5.0	5.0	4.8
48	40	34	28	22.7	11.0	PAV	2.7	27	50	100

4.50	4.41	4.51	4.9	4.6	4.7	5.4
33	70	7	4	50	100	

4.52	4.4	4.51	6.3	6.5	4.1	4.8	5.4
31.3	22	9.6		3	9	50	100

4.58	4.52	4.62	5.0	6.4	6.2	4.3	4.1	4.6	5.4
45	32	18	13	8	4		12	50	100

4.62	4.68	4.8	6.3	6.3	4.1	3.8	4.8	5.0
32.5	21	16	13	7			50	100

4.85	4.8	5.4	5.9	3.8	4.1	4.8	4.5
50	44	40	36	20		50	100

Station	+	π	-	Z/ev.
		931.40 ✓		
10+50				924.1 ✓
11+0				24.6 ✓
12+50				26.6 ✓
12+0				27.6 ✓
+50				27.1 ✓
13+0				26.1 ✓
+50				26.1 ✓
14				26.6 ✓
+45				26.4 ✓
15				26.9 ✓
16				26.4 ✓
17				26.6 ✓
T.P.	4.19	931.74 ✓	3.85	927.55 ✓

Lt

Z

Et.

40

$$\frac{6.5}{50}$$

$$\frac{7.3}{50}$$

$$\frac{7.3}{50}$$

$$\frac{7.4}{100}$$

$$\frac{6.2}{50}$$

$$\frac{6.8}{50}$$

$$\frac{6.6}{50}$$

$$\frac{6.9}{100}$$

$$\frac{5.4}{50}$$

$$\frac{4.8}{50}$$

$$\frac{5.4}{50}$$

$$\frac{6.0}{50}$$

$$\frac{5.2}{100}$$

$$\frac{4.0}{50}$$

$$\frac{3.8}{50}$$

$$\frac{5.0}{50}$$

$$\frac{5.8}{100}$$

$$\frac{4.1}{50}$$

$$\frac{4.3}{50}$$

$$\frac{4.7}{50}$$

$$\frac{5.3}{100}$$

$$\frac{4.8}{50}$$

$$\frac{5.3}{50}$$

$$\frac{4.9}{50}$$

$$\frac{4.8}{100}$$

$$\frac{5.3}{50}$$

$$\frac{5.3}{50}$$

$$\frac{5.0}{50}$$

$$\frac{4.4}{100}$$

$$\frac{5.2}{50}$$

$$\frac{4.8}{50}$$

$$\frac{4.9}{50}$$

$$\frac{4.6}{100}$$

$$\frac{5.5}{50}$$

$$\frac{5.0}{50}$$

$$\frac{5.0}{50}$$

$$\frac{4.3}{100}$$

$$\frac{5.6}{50}$$

$$\frac{4.5}{50}$$

$$\frac{4.7}{50}$$

$$\frac{4.5}{100}$$

$$\frac{5.0}{50}$$

$$\frac{5.0}{50}$$

$$\frac{4.7}{50}$$

$$\frac{4.4}{100}$$

$$\frac{5.3}{50}$$

$$\frac{4.8}{50}$$

$$\frac{3.5}{50}$$

$$\frac{3.0}{100}$$

50.1

Station	+	π	-	Elev.
		931.74 ✓		
17+50				27.3 ✓
18+0				26.3 ✓
19+0				23.8 ✓
T.P.	1.56	926.17 ✓	7.13	924.61 ✓
+50				21.7 ✓
20+0				20.7 ✓
+52				19.5 ✓
T.P.	1.76	917.33 ✓	10.60	915.57 ✓
21				15.4 ✓
+50				10.8 ✓
22				906.6 ✓
+50				04.9 ✓
T.P.	3.89	909.78 ✓	11.46	905.89 ✓
23				05.1 ✓
+50				05.6 ✓

Lt.

L

Rt.

41

$$\frac{47}{50}$$

$$\frac{44}{50}$$

$$\frac{45}{50}$$

$$\frac{40}{100}$$

$$\frac{62}{50}$$

$$\frac{54}{50}$$

$$\frac{44}{50}$$

$$\frac{42}{100}$$

$$\frac{84}{50}$$

$$\frac{79}{50}$$

$$\frac{69}{50}$$

$$\frac{60}{100}$$

$$\frac{49}{50}$$

$$\frac{45}{50}$$

$$\frac{40}{50}$$

$$\frac{35}{100}$$

$$\frac{63}{50}$$

$$\frac{55}{50}$$

$$\frac{49}{50}$$

$$\frac{46}{100}$$

$$\frac{82}{50} \quad \frac{78}{35}$$

$$\frac{67}{50}$$

$$\frac{59}{50}$$

$$\frac{53}{100}$$

$$\frac{36}{50}$$

$$\frac{19}{50}$$

$$\frac{07}{50}$$

$$\frac{109}{100}$$

$$\frac{75}{50}$$

$$\frac{65}{50}$$

$$\frac{53}{50}$$

$$\frac{26}{100}$$

$$\frac{120}{50}$$

$$\frac{107}{50}$$

$$\frac{91}{50}$$

$$\frac{49}{100}$$

$$\frac{147}{50} \quad \frac{143}{28}$$

$$\frac{124}{50}$$

$$\frac{99}{50}$$

$$\frac{91}{100}$$

Top stake 2250 ±

$$\frac{58}{100}$$

$$\frac{47}{50}$$

$$\frac{32}{50}$$

$$\frac{02}{100}$$

$$\frac{43}{50}$$

$$\frac{42}{50}$$

$$\frac{40}{50}$$

$$\frac{38}{100}$$

Station	+	π	-	Elev.
		909.78 ✓		
2440				905.5 ✓
+50				04.6 ✓
2540				02.4 ✓
+50				900.6 ✓
2640				03.0 ✓
+50				04.2 ✓
T.P.	1.63	907.17 ✓	4.24	905.54 ✓
27				05.1 ✓
+30				04.0 ✓
+65				906.1 ✓
28				897.7 ✓
+40				896.1
+75				897.1 ✓
	5.22	903.36 ✓	9.03	898.14 ✓

Lt.

C

Rt.

42

$$\frac{4.5}{50}$$

$$\frac{4.8}{30}$$

$$4.3$$

$$\frac{4.2}{50}$$

$$\frac{4.4}{150}$$

$$\frac{5.3}{50}$$

$$\frac{5.1}{35}$$

$$\frac{5.2}{50}$$

$$\frac{3.3}{50}$$

$$\frac{4.5}{100}$$

on R.R. App

$$\frac{6.5}{50}$$

$$7.4$$

$$\frac{4.3}{50}$$

$$\frac{3.4}{85} = \frac{R.R.}{Feo}$$

$$\frac{3.9}{100}$$

$$\frac{6.5}{50}$$

$$\frac{7.3}{32}$$

$$9.2$$

$$\frac{9.2}{12}$$

$$\frac{7.0}{30}$$

$$\frac{5.8}{50}$$

$$\frac{3.0}{75}$$

R.R. Force.

$$\frac{5.6}{50}$$

$$\frac{6.9}{25}$$

$$\frac{6.8}{50}$$

$$\frac{6.8}{23}$$

$$\frac{4.5}{50}$$

$$\frac{2.7}{69}$$

R.R. Force

$$\frac{5.5}{50}$$

$$\frac{5.4}{25}$$

$$\frac{5.6}{50}$$

$$\frac{4.1}{25}$$

$$\frac{2.8}{50}$$

$$\frac{1.0}{66}$$

= Force

$$\frac{2.4}{50}$$

$$\frac{2.1}{50}$$

$$\frac{+0.3}{50}$$

$$\frac{+0.6}{62}$$

Contd

$$\frac{3.0}{50}$$

$$\frac{2.9}{30}$$

$$3.2$$

$$\frac{1.2}{50}$$

$$\frac{0.2}{61}$$

$$\frac{4.5}{50}$$

$$\frac{5.7}{25}$$

$$6.1$$

$$\frac{5.1}{30}$$

$$\frac{2.7}{50}$$

$$\frac{1.3}{60}$$

$$\frac{7.0}{50}$$

$$\frac{8.0}{30}$$

$$7.5$$

$$\frac{9.3}{16}$$

$$\frac{6.0}{40}$$

$$\frac{2.8}{59}$$

$$\frac{8.7}{50}$$

$$\frac{8.9}{15}$$

$$10.9$$

$$\frac{10.6}{22}$$

$$\frac{5.2}{58}$$

$$\frac{10.3}{50}$$

$$10.1$$

$$\frac{9.8}{25}$$

$$\frac{6.8}{57}$$

Note: All sections on the right are continued see p. 72 to 100

Station	+	+	-	Elev.
		903.36 ✓		
2940				897.0 ✓
+50				96.4 ✓
3040				96.3 ✓
+30				96.0 ✓
+60				94.8 ✓
B.M.	9.16	903.36 ✓	9.16	894.20 ✓
3140				91.9 ✓
+15				96.6 ✓
+35 = 1 Co. Rd "F"				97.4 ✓
+55				97.2 ✓
T.B.M.			0.40	902.96 ✓
31477				90.2 ✓
T.P.	0.75	891.70 ✓	12.41	890.95 ✓
31477				90.2 ✓
3240				88.2 ✓

$$\frac{7.8}{50}$$

$$64$$

$$\frac{4.9}{25}$$

$$\frac{3.1}{56}$$

$$\frac{11.2}{50}$$

$$\frac{8.1}{15}$$

$$70$$

$$\frac{4.5}{27}$$

$$\frac{2.7}{50}$$

C
6
7
1
3
4
6
1

$$\frac{8.0}{107} \quad \frac{84}{92} \quad \frac{10.8}{86} \quad \frac{12.3}{72} \quad \frac{12.1}{54} \quad \frac{8.6}{17}$$

$$71$$

$$\frac{4.7}{25}$$

$$\frac{2.7}{48}$$

$$\frac{8.0}{80} \quad \frac{8.1}{64} \quad \frac{10.7}{58} \quad \frac{10.3}{41} \quad \frac{9.2}{21}$$

$$74$$

$$\frac{4.5}{32}$$

$$\frac{3.8}{48}$$

$$\frac{8.4}{74} \quad \frac{7.7}{57} \quad \frac{7.9}{42} \quad \frac{10.4}{37} \quad \frac{10.7}{20}$$

$$86$$

$$\frac{6.8}{25}$$

$$\frac{5.7}{45}$$

R.P. Spike in 12" oak 40' Lt. Sta. 30+50

$$\frac{14.6}{70} \quad \frac{13.7}{57} \quad \frac{8.0}{45} \quad \frac{9.1}{29} \quad \frac{7.1}{14} \quad \frac{7.2}{14}$$

$$\frac{10.5}{17}$$

$$\frac{11.2}{32}$$

$$\frac{9.7}{49}$$

14.4 outlet Culv. (See Top)

(13.0 = Inlet Culv. See Top)

$$\frac{14.3}{63} \quad \frac{13.7}{52} \quad \frac{7.8}{36} \quad \frac{6.7}{20}$$

$$6.8$$

$$\frac{12.2}{13}$$

$$\frac{11.7}{30}$$

$$\frac{11.6}{40}$$

$$\frac{10.8}{50}$$

$$\frac{14.7}{50} \quad \frac{13.8}{35} \quad \frac{7.0}{19}$$

$$60$$

$$\frac{6.1}{18}$$

$$\frac{11.8}{31}$$

$$\frac{12.4}{40}$$

$$\frac{11.7}{50}$$

$$\frac{11.3}{65}$$

$$\frac{10.1}{75}$$

Contd

$$\frac{15.3}{50}$$

$$\frac{14.0}{20}$$

$$62$$

$$\frac{5.2}{20}$$

$$\frac{5.2}{35}$$

$$\frac{10.6}{45}$$

$$\frac{12.4}{59}$$

$$\frac{12.2}{67}$$

$$\frac{8.1}{78}$$

Top Rail 98' RT. Sta.

$$132$$

$$\frac{4.8}{70}$$

$$\frac{3.9}{37}$$

$$\frac{3.9}{53}$$

$$\frac{3.9}{53}$$

Contd

$$\frac{3.5}{50}$$

$$11.5$$

$$\frac{3.4}{50}$$

$$\frac{3.5}{17}$$

$$\frac{1.6}{13}$$

Sta.	+	π	-	Elev.
		891.70 ✓		
32+50				88.1 ✓
33+0				86.5 ✓
34+0				84.7 ✓
35+0				84.7 ✓
36+0				85.7 ✓
T.P.	10.83	897.41 ✓	5.12	886.58 ✓
37+0				88.3 ✓
+65				95.6 ✓
T.P.	13.21	909.00 ✓	1.62	895.79 ✓
38+0				899.8 ✓
+45				905.3 ✓
T.P.	11.04	918.90 ✓	1.14	907.86 ✓
39+0				908.9 ✓
+50				911.9 ✓
40+0				914.2 ✓

$$\frac{5.5}{50}$$

$$\frac{4.0}{34}$$

$$3.6$$

$$\frac{2.9}{35}$$

$$\frac{0.8}{51}$$

- contd

$$\frac{7.3}{50}$$

$$\frac{6.6}{28}$$

$$\frac{5.2}{-}$$

$$\frac{4.0}{30}$$

$$\frac{3.3}{48}$$

$$\frac{4.2}{54}$$

$$\frac{2.2}{66}$$

✓

$$\frac{7.6}{50}$$

$$\frac{7.5}{21}$$

$$7.0$$

$$\frac{6.5}{22}$$

$$\frac{4.8}{37}$$

$$\frac{4.5}{51}$$

$$\frac{2.4}{64}$$

✓

$$\frac{6.8}{50}$$

$$7.0$$

$$\frac{6.2}{23}$$

$$\frac{4.9}{32}$$

$$\frac{3.3}{50}$$

$$\frac{2.0}{55}$$

$$\frac{0.8}{65}$$

✓

$$\frac{5.8}{50}$$

$$\frac{5.6}{27}$$

$$6.0$$

$$\frac{6.0}{10}$$

$$\frac{5.1}{18}$$

$$\frac{4.6}{28}$$

$$\frac{2.6}{45}$$

$$\frac{2.2}{62}$$

✓

$$\frac{11.6}{50}$$

$$\frac{11.7}{38}$$

$$\frac{10.4}{25}$$

$$\frac{10.1}{12}$$

$$\frac{9.1}{-}$$

$$\frac{8.8}{25}$$

$$\frac{9.5}{48}$$

$$\frac{7.8}{68}$$

✓

$$\frac{8.4}{60}$$

$$\frac{5.6}{43}$$

$$\frac{3.2}{25}$$

$$\frac{1.8}{-}$$

$$\frac{1.9}{20}$$

$$\frac{2.6}{45}$$

$$\frac{2.0}{65}$$

✓

$$\frac{8.5}{-}$$

$$\frac{10.3}{50}$$

$$\frac{8.2}{21}$$

$$9.2$$

$$\frac{10.0}{22}$$

$$\frac{11.1}{50}$$

✓

$$\frac{3.7}{50}$$

$$3.7$$

$$\frac{4.8}{22}$$

$$\frac{5.3}{54}$$

✓

$$\frac{8.9}{70}$$

$$\frac{8.6}{50}$$

$$\frac{8.5}{30}$$

$$10.0$$

$$\frac{11.7}{27}$$

$$\frac{12.0}{51}$$

$$\frac{13.4}{76}$$

✓

$$\frac{5.2}{75}$$

$$\frac{5.4}{50}$$

$$\frac{6.2}{20}$$

$$7.0$$

$$\frac{8.9}{34}$$

$$\frac{9.7}{54}$$

$$\frac{9.6}{68}$$

✓

$$\frac{5.1}{100}$$

$$\frac{3.8}{67}$$

$$\frac{3.8}{30}$$

$$4.7$$

$$\frac{6.0}{30}$$

$$\frac{6.2}{52}$$

$$\frac{6.9}{71}$$

Sta.	+	-	Elev.
		918.90 ✓	
40+40			915.8 ✓
41+40			914.4 ✓
T.P.	0.89	915.84 ✓	3.95 914.95 ✓
+15			13.4 ✓
+40			09.3 ✓
+65			03.8 ✓
+75			902.3 ✓
T.P.	1.84	905.27 ✓	12.41 903.43 ✓
42+0			891.9 ✓
T.P.	0.36	892.99 ✓	12.64 892.63 ✓
42+00	894.20		91.9
+16			85.5 ✓
+33			83.3 ✓
+60	Top Bank		84.3 ✓
+65	W.E		880.24 ✓

Lt.

E

Rt.

45

$\frac{5.3}{100}$	$\frac{4.0}{85}$	$\frac{3.5}{50}$	$\frac{2.8}{22}$	$\frac{3.1}{-}$	$\frac{3.6}{32}$	$\frac{3.0}{52}$	$\frac{4.3}{68}$	contd.
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$\frac{9.0}{75}$	$\frac{6.8}{53}$	$\frac{4.9}{27}$	$\frac{4.5}{0}$	$\frac{4.4}{29}$	$\frac{3.5}{51}$	$\frac{3.8}{66}$	✓
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Top Hub &

$\frac{8.5}{75}$	$\frac{5.2}{47}$	$\frac{3.0}{22}$	$\frac{2.4}{-}$	$\frac{2.0}{29}$	$\frac{1.7}{50}$	$\frac{6.6}{68}$	-
------------------	------------------	------------------	-----------------	------------------	------------------	------------------	---

$\frac{11.5}{75}$	$\frac{8.7}{40}$	$\frac{6.5}{-}$	$\frac{5.0}{30}$	$\frac{4.5}{55}$	$\frac{5.1}{71}$
-------------------	------------------	-----------------	------------------	------------------	------------------

$\frac{14.5}{50}$	$\frac{13.4}{25}$	$\frac{12.0}{-}$	$\frac{9.4}{52}$	$\frac{9.4}{76}$
-------------------	-------------------	------------------	------------------	------------------

$\frac{16.2}{50}$	$\frac{14.5}{25}$	$\frac{13.5}{-}$	$\frac{11.3}{34}$	$\frac{11.4}{62}$	$\frac{11.3}{78}$
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$\frac{13.4}{-}$	$\frac{12.1}{30}$	$\frac{11.7}{50}$	$\frac{12.2}{75}$
------------------	-------------------	-------------------	-------------------

Top Stake & 22

$\frac{2.5}{100}$	$\frac{1.7}{50}$	$\frac{2.0}{20}$	(1.1)
-------------------	------------------	------------------	-------

$\frac{8.4}{50}$	$\frac{8.0}{28}$	$\frac{7.5}{-}$	$\frac{7.6}{28}$	$\frac{7.5}{50}$	$\frac{5.4}{70}$	$\frac{1.0}{84}$	$\frac{2.2}{95}$
------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------

$\frac{9.6}{100}$	$\frac{9.6}{50}$	$\frac{9.5}{30}$	$\frac{9.7}{-}$	$\frac{10.2}{25}$	$\frac{9.1}{60}$	$\frac{9.2}{77}$	$\frac{12.25}{96}$	- E. No. 4
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$\frac{9.0}{50}$	$\frac{8.6}{37}$	$\frac{8.7}{-}$	$\frac{8.8}{7}$	$\frac{12.75}{78-10.9}$	$\frac{14.8}{48}$	= 4 ch.
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$\frac{9.0}{50}$	$\frac{8.5}{72}$	$\frac{12.75}{-}$	$\frac{14.8}{4}$	etchan.
------------------	------------------	-------------------	------------------	---------

Sta	+	π	-	E/cv.
		892.99 ✓		
+72	2 channel			878.1 ✓
+88	W.E			80.24 ✓
4340	Top Bank.			84.9 ✓
B.M.	7.29	892.99 ✓	7.29	885.70 ✓
+33				87.6 ✓
+64				87.6 ✓
T.P	5.40	894.24 ✓	4.15	888.84 ✓
4440				88.1 ✓
+37				86.3 ✓
+75				87.7 ✓
415				86.7 ✓
+50				86.3 ✓
416				86.5 ✓
+50				86.4 ✓

Lt.

E

Rt.

1146
65
33
16

149

Top Bank 98 $\frac{7.5}{12.68}$ W.E = 67 $\frac{14.9}{30}$ 12.75 $\frac{9.8}{24}$ = Top Bank $\frac{86}{47}$ $\frac{70}{74}$ Cont'd

Top Bank 151 $\frac{8.1}{12.65}$ W.E = 118 $\frac{8.1}{43}$ $\frac{7.6}{66}$ = 75 R.R. R.I.

4-Nails in 10" W. oak 100' Lt. Str. 4/2+75

$\frac{15.1}{20.1}$ $\frac{12.65}{10.8}$ $\frac{6.1}{70}$ $\frac{5.8}{49}$ $\frac{6.2}{28}$ 54 $\frac{7.2}{14}$ $\frac{6.4}{37}$ $\frac{2.7}{65}$ Cont'd

201 - Top Log Bridge - Inter of Channel 1.

$\frac{0.6}{50}$ $\frac{3.3}{33}$ $\frac{6.7}{7}$ 54 $\frac{2.5}{14}$ $\frac{1.6}{42}$ $\frac{0.5}{52}$ $\frac{12.0}{69}$ "

$\frac{0.7}{50}$ $\frac{1.5}{29}$ $\frac{7.4}{9.17}$ $\frac{7.4}{17}$ 61 $\frac{3.4}{7}$ $\frac{0.8}{18}$ $\frac{1.0}{37}$ $\frac{0.0}{47}$ $\frac{1.9}{62}$ $\frac{+0.9}{67}$ "

$\frac{3.5}{50}$ $\frac{3.4}{29}$ $\frac{3.7}{14}$ 79 $\frac{4.4}{11}$ $\frac{4.0}{35}$ $\frac{1.8}{48}$ $\frac{0.4}{66}$ "

$\frac{5.3}{50}$ $\frac{6.5}{6}$ $\frac{7.9}{12}$ $\frac{6.5}{42}$ $\frac{5.3}{65}$ $\frac{4.0}{65}$ "

$\frac{6.7}{50}$ $\frac{7.4}{22}$ $\frac{7.5}{18}$ $\frac{7.0}{50}$ $\frac{6.5}{65}$ $\frac{5.6}{65}$ "

$\frac{7.8}{50}$ $\frac{7.7}{30}$ $\frac{7.9}{48}$ $\frac{7.4}{63}$ "

$\frac{8.0}{50}$ $\frac{7.7}{28}$ $\frac{7.3}{50}$ $\frac{6.7}{68}$ "

$\frac{7.7}{50}$ $\frac{7.8}{60}$ $\frac{7.2}{60}$ "

Sta. + A - Elev.

894.24 ✓

4740

87.5 ✓

+26

88.2 ✓

+52

88.1 ✓

T.P.

6.73

895.74 ✓

5.23

889.01 ✓

4840

86.9 ✓

+50

86.8 ✓

49

88.0 ✓

+45

90.7 ✓

50

88.5 ✓

+50

89.1 ✓

51

92.7 ✓

T.P.

12.55

906.10

2.19

893.55 ✓

+50

95.0 ✓

52

95.3 ✓

Lt.

E

St.

47

$$\frac{6.8}{50}$$

$$\frac{7.4}{33}$$

$$\frac{6.7}{-}$$

$$\frac{6.5}{30}$$

$$\frac{6.0}{62}$$

Contd.

$$\frac{6.4}{50}$$

$$\frac{6.4}{32}$$

$$\frac{4.0}{-}$$

$$\frac{5.5}{20}$$

$$\frac{4.4}{64}$$

"

$$\frac{6.0}{50}$$

$$\frac{6.7}{31}$$

$$\frac{6.2}{21}$$

$$\frac{6.1}{-}$$

$$\frac{5.4}{35}$$

$$\frac{4.5}{68}$$

"

$$\frac{7.9}{50}$$

$$\frac{8.4}{30}$$

$$8.8$$

$$\frac{8.5}{44}$$

$$\frac{7.5}{62}$$

"

$$\frac{7.7}{50}$$

$$\frac{8.5}{25}$$

$$\frac{7.3}{12}$$

$$8.9$$

$$\frac{8.3}{36}$$

$$\frac{6.9}{63}$$

"

$$\frac{6.9}{50}$$

$$\frac{7.8}{28}$$

$$7.7$$

$$\frac{7.1}{30}$$

$$\frac{5.3}{63}$$

"

$$\frac{4.7}{50}$$

$$\frac{5.8}{37}$$

$$\frac{5.2}{25}$$

$$5.0$$

$$\frac{5.8}{27}$$

$$\frac{7.3}{62}$$

"

$$\frac{4.7}{50}$$

$$\frac{5.5}{32}$$

$$\frac{6.7}{21}$$

$$7.2$$

$$\frac{7.2}{16}$$

$$\frac{8.1}{40}$$

$$\frac{7.5}{62}$$

"

$$\frac{3.4}{50}$$

$$\frac{4.7}{18}$$

$$6.6$$

$$\frac{7.7}{17}$$

$$\frac{8.3}{38}$$

$$\frac{7.1}{66}$$

"

$$\frac{7.5}{50}$$

$$\frac{8.0}{29}$$

$$3.0$$

$$\frac{5.6}{28}$$

$$\frac{5.1}{50}$$

$$\frac{3.2}{70}$$

"

$$\frac{8.2}{50}$$

$$\frac{9.0}{35}$$

$$\frac{10.4}{19}$$

$$11.1$$

$$\frac{11.4}{75}$$

$$\frac{9.5}{75}$$

$$\frac{8.7}{60}$$

898.16

$$\frac{14.0}{50}$$

$$\frac{13.3}{21}$$

$$14.8$$

$$\frac{7.8}{23}$$

$$\frac{4.8}{43}$$

$$\frac{4.2}{56}$$

$$\frac{784}{100}$$

 Total

56.

+

A

-

Elev.

906.10 ✓

52+45

894.1 ✓

53+0

898.0 ✓

T.P.

7.94

911.59

2.45

903.65 ✓

+63

905.8 ✓

54

07.0 ✓

+50

07.1 ✓

T.P.

1.03

908.88 ✓

3.74

907.85 ✓

55

05.4 ✓

+45

03.9 ✓

56

901.0 ✓

+45

899.8 ✓

+75

901.5 ✓

57+0

903.1 ✓

+31

904.1 ✓

$$\frac{15.7}{50}$$

$$\frac{140}{21}$$

$$120$$

$$\frac{3.3}{43}$$

$$\frac{2.5}{50}$$

$$\frac{2.5}{56}$$

Cont'd

$$\frac{13.5}{50}$$

$$\frac{113}{21}$$

$$\frac{8.1}{21}$$

$$\frac{5.0}{18}$$

$$\frac{1.1}{39}$$

$$\frac{0.0}{50}$$

$$\frac{102}{55}$$

"

$$\frac{13.3}{50}$$

$$\frac{113}{35}$$

$$\frac{8.6}{18}$$

$$\frac{5.8}{18}$$

$$\frac{4.4}{11}$$

$$\frac{3.1}{35}$$

$$\frac{2.8}{53}$$

"

$$\frac{9.0}{50}$$

$$\frac{7.4}{35}$$

$$\frac{5.8}{18}$$

$$46$$

$$\frac{3.4}{18}$$

$$\frac{3.1}{38}$$

$$\frac{3.6}{54}$$

"

$$\frac{8.9}{70}$$

$$\frac{7.6}{50}$$

$$\frac{6.3}{34}$$

$$\frac{5.7}{23}$$

$$45$$

$$\frac{5.4}{30}$$

$$\frac{6.4}{50}$$

$$\frac{7.7}{62}$$

"

$$\frac{8.7}{50}$$

$$\frac{7.0}{33}$$

$$\frac{4.7}{15}$$

$$\frac{3.5}{15}$$

$$\frac{3.6}{18}$$

$$\frac{4.8}{33}$$

$$\frac{6.0}{50}$$

$$\frac{8.7}{68}$$

"

$$\frac{8.7}{50}$$

$$\frac{7.6}{36}$$

$$\frac{5.6}{12}$$

$$50$$

$$\frac{4.7}{11}$$

$$\frac{6.2}{38}$$

$$\frac{7.3}{51}$$

$$\frac{9.5}{59}$$

"

$$\frac{10.8}{50}$$

$$\frac{10.0}{31}$$

$$\frac{8.6}{13}$$

$$\frac{7.9}{19}$$

$$\frac{7.4}{19}$$

$$\frac{8.4}{52}$$

$$\frac{10.0}{59}$$

"

$$\frac{9.5}{50}$$

$$\frac{8.7}{15}$$

$$\frac{9.1}{15}$$

$$\frac{9.7}{20}$$

$$\frac{10.5}{52}$$

$$\frac{12.5}{68}$$

"

$$\frac{7.5}{50}$$

$$\frac{7.2}{28}$$

$$74$$

$$\frac{7.5}{25}$$

$$\frac{8.5}{45}$$

$$\frac{9.6}{63}$$

"

$$\frac{7.7}{50}$$

$$\frac{7.7}{22}$$

$$\frac{5.8}{22}$$

$$\frac{5.2}{11}$$

$$\frac{5.5}{28}$$

$$\frac{7.3}{58}$$

"

$$\frac{9.3}{50}$$

$$\frac{9.3}{40}$$

$$\frac{8.2}{25}$$

$$\frac{4.8}{22}$$

$$\frac{3.4}{22}$$

$$\frac{3.7}{41}$$

$$\frac{4.0}{56}$$

"

S/b.	+	π	-	E/eV.
		908.88 ✓		
57+64				902.9 ✓
58+0				897.9 ✓
T.P.	4.62	902.97 ✓	10.53	898.35 ✓
+30				892.8 ✓
+65				890.5 ✓
59				892.3 ✓
+50				898.8 ✓
T.P.	3.95	906.39 ✓	0.53	902.44 ✓
+75				901.1 ✓
60+0				901.8 ✓
+75				901.2 ✓
+65				895.0 ✓
61+0				891.9 ✓
T.P.	3.61	896.35 ✓	13.65	892.74 ✓
+50				888.9 ✓

Lt

E

Rt

49

$$\frac{124}{50}$$

$$\frac{9.0}{24}$$

$$\frac{6.0}{24}$$

$$\frac{3.7}{18}$$

$$\frac{2.7}{34}$$

$$\frac{2.2}{54}$$

Cont'd

$$\frac{15.7}{50}$$

$$\frac{14.7}{30}$$

$$\frac{12.8}{14}$$

$$\frac{11.0}{24}$$

$$\frac{8.0}{22}$$

$$\frac{5.7}{45}$$

$$\frac{4.2}{57}$$

"

Drain West.

$$\frac{12.9}{50}$$

$$\frac{12.5}{40}$$

$$\frac{11.6}{23}$$

$$\frac{10.2}{24}$$

$$\frac{8.7}{18}$$

$$\frac{6.4}{41}$$

$$\frac{4.5}{54}$$

$$\frac{1.8}{62}$$

"

$$\frac{11.2}{50}$$

$$\frac{11.3}{43}$$

$$\frac{12.1}{22}$$

$$\frac{12.5}{24}$$

$$\frac{12.0}{25}$$

$$\frac{10.7}{41}$$

$$\frac{9.7}{53}$$

$$\frac{8.2}{68}$$

"

$$\frac{8.5}{50}$$

$$\frac{9.2}{33}$$

$$\frac{10.7}{24}$$

$$\frac{12.0}{40}$$

$$\frac{11.6}{65}$$

"

$$\frac{0.2}{50}$$

$$\frac{1.7}{27}$$

$$\frac{4.2}{24}$$

$$\frac{6.6}{25}$$

$$\frac{8.2}{53}$$

$$\frac{10.0}{57}$$

$$\frac{10.0}{65}$$

"

$$\frac{4.0}{50}$$

$$\frac{3.5}{27}$$

$$\frac{3.7}{15}$$

$$\frac{5.3}{24}$$

$$\frac{6.4}{12}$$

$$\frac{8.7}{20}$$

$$\frac{9.6}{53}$$

$$\frac{11.5}{59}$$

$$\frac{11.5}{67}$$

"

$$\frac{4.6}{50}$$

$$\frac{3.6}{23}$$

$$\frac{4.6}{24}$$

$$\frac{7.3}{29}$$

$$\frac{7.5}{52}$$

$$\frac{7.8}{66}$$

"

$$\frac{4.5}{50}$$

$$\frac{5.0}{38}$$

$$\frac{4.8}{16}$$

$$\frac{5.2}{24}$$

$$\frac{8.0}{25}$$

$$\frac{7.6}{53}$$

$$\frac{11.0}{61}$$

$$\frac{10.7}{68}$$

"

$$\frac{6.0}{50}$$

$$\frac{8.7}{32}$$

$$\frac{11.2}{17}$$

$$\frac{11.4}{24}$$

$$\frac{12.7}{24}$$

$$\frac{13.4}{52}$$

$$\frac{13.5}{65}$$

"

$$\frac{12.3}{50}$$

$$\frac{13.5}{30}$$

$$\frac{14.5}{24}$$

$$\frac{15.7}{17}$$

$$\frac{15.7}{32}$$

$$\frac{17.0}{61}$$

"

$$\frac{5.0}{60}$$

$$\frac{6.0}{50}$$

$$\frac{7.3}{20}$$

$$\frac{7.5}{24}$$

$$\frac{7.8}{33}$$

$$\frac{8.6}{50}$$

$$\frac{8.1}{52}$$

$$\frac{9.0}{58}$$

"

Sta. + X - Elev.

896.35 ✓

62to

887.5 ✓

+35

87.2 ✓

63to

89.2 ✓

+50

90.0 ✓

64to

91.8 ✓

+35

91.9 ✓

+80

92.4 ✓

65to

92.1 ✓

+50

91.4 ✓

66to

890.9 ✓

T.P.

6.22

897.70 ✓

4.87

894.8 ✓

+40

88.6 ✓

+85

86.1 ✓

Lt.

L

Rt.

50

 $\frac{8.0}{50}$ $\frac{8.3}{25}$

8.9

 $\frac{8.8}{25}$ $\frac{9.0}{50}$ $\frac{9.0}{53}$ $\frac{9.8}{56}$ $\frac{9.5}{58}$

Contd

 $\frac{8.8}{60}$ $\frac{9.0}{25}$

9.2

 $\frac{9.0}{50}$ $\frac{9.2}{50}$ $\frac{9.5}{57}$ $\frac{9.5}{60}$

"

 $\frac{8.6}{50}$ $\frac{8.0}{25}$

7.2

 $\frac{6.2}{20}$ $\frac{7.2}{52}$ $\frac{8.4}{55}$ $\frac{7.2}{62}$

"

 $\frac{8.1}{50}$ $\frac{7.2}{20}$

6.4

 $\frac{5.8}{14}$ $\frac{4.4}{32}$ $\frac{5.6}{52}$ $\frac{5.4}{52}$ $\frac{4.7}{69}$ $\frac{7.7}{50}$ $\frac{6.0}{20}$

4.6

 $\frac{2.6}{21}$ $\frac{0.2}{20}$ $\frac{7.1}{50}$ $\frac{5.7}{22}$

4.5

 $\frac{2.8}{18}$ $\frac{7.1}{50}$ $\frac{6.1}{20}$ $\frac{4.6}{11}$

4.0

 $\frac{3.0}{10}$ $\frac{1.4}{15}$ $\frac{7.2}{50}$ $\frac{5.3}{15}$

4.3

 $\frac{2.0}{20}$ $\frac{1.1}{25}$ $\frac{40.7}{37}$ $\frac{7.6}{50}$ $\frac{5.2}{13}$

5.0

 $\frac{4.0}{20}$ $\frac{1.3}{40}$ $\frac{7.6}{60}$ $\frac{6.3}{17}$

5.5

 $\frac{5.0}{30}$ $\frac{4.0}{50}$ $\frac{12.0}{73}$

top stake @ Sta. 66

 $\frac{11.6}{50}$ $\frac{11.1}{47}$ $\frac{9.4}{25}$

9.1

 $\frac{2.0}{32}$ $\frac{5.5}{61}$ $\frac{13.1}{50}$ $\frac{13.8}{30}$

11.6

 $\frac{10.5}{18}$ $\frac{9.3}{43}$ $\frac{6.9}{56}$

66+43 - $\left\{ \begin{array}{l} \text{outlet cu/v.} \\ 24" \text{ C.I.P.} \end{array} \right. \frac{11.35}{49'}$

Sta.	+	π	-	Elev.
		897.70 ✓		
6740				84.6 ✓
+25				83.0 ✓
6840				82.9 ✓
+50				84.1 ✓
6940				87.6 ✓
+50				92.5 ✓
+80				897.1 ✓
T.P.	12.87	910.57 ✓	0.00	897.70 ✓
7040				902.8 ✓
T.B	12.22	922.40 ✓	0.39	910.18
+46				19.9 ✓
T.P.	10.08	931.78 ✓	0.70	921.70 ✓
+83				28.0 ✓
7140				27.7 ✓
71434				16.1 ✓
T.P.	0.01	918.40 ✓	13.39	918.39 ✓
71434				16.1

H.

2

Rt.

51

$$\frac{15.1}{50}$$

$$\frac{14.3}{28}$$

$$\frac{13.1}{-}$$

$$\frac{11.6}{20}$$

$$\frac{10.0}{35}$$

$$\frac{9.5}{51}$$

Contd

$$\frac{15.8}{50}$$

$$\frac{15.2}{30}$$

$$\frac{14.7}{-}$$

$$\frac{13.0}{26}$$

$$\frac{11.5}{41}$$

$$\frac{10.6}{52}$$

$$\frac{15.6}{50}$$

$$\frac{14.8}{-}$$

$$\frac{13.2}{25}$$

$$\frac{11.7}{40}$$

$$\frac{9.2}{60}$$

$$\frac{14.8}{50}$$

$$13.6$$

$$\frac{11.4}{35}$$

$$\frac{11.4}{58}$$

$$\frac{9.2}{50}$$

$$\frac{9.6}{31}$$

$$\frac{10.1}{-}$$

$$\frac{10.6}{36}$$

$$\frac{10.6}{48}$$

$$\frac{9.4}{55}$$

$$\frac{4.8}{50}$$

$$\frac{4.8}{35}$$

$$5.2$$

$$\frac{6.1}{35}$$

$$\frac{6.6}{50}$$

$$\frac{5.1}{67}$$

$$\frac{+5.1}{50}$$

$$\frac{+2.3}{28}$$

$$\frac{0.0}{13}$$

$$\frac{0.6}{-}$$

$$\frac{1.3}{25}$$

$$\frac{2.3}{52}$$

$$\frac{4.3}{63}$$

$$\frac{3.0}{72}$$

$$\frac{3.0}{75}$$

$$\frac{3.0}{50}$$

$$\frac{4.4}{23}$$

$$7.8$$

$$\frac{8.7}{25}$$

$$\frac{8.7}{52}$$

$$\frac{9.8}{68}$$

$$\frac{12.4}{75}$$

907.12

344

40

70.84

$$\frac{+4.1}{100}$$

$$\frac{+2.8}{80}$$

$$\frac{+0.4}{50}$$

$$\frac{0.5}{31}$$

$$2.5$$

$$\frac{4.0}{34}$$

$$\frac{5.4}{52}$$

$$\frac{6.8}{68}$$

$$- \text{Contd}$$

$$\frac{0.2}{100}$$

$$\frac{2.2}{57}$$

$$\frac{3.8}{-}$$

$$\frac{3.9}{36}$$

$$\frac{4.7}{53}$$

$$\frac{1.1}{100}$$

$$\frac{2.8}{50}$$

$$\frac{4.1}{-}$$

$$\frac{3.2}{14}$$

$$\frac{3.1}{44}$$

$$\frac{4.3}{51}$$

$$\frac{15.7}{-}$$

$$\frac{13.0}{34}$$

$$\frac{9.7}{53}$$

$$\frac{+2.3}{75}$$

$$\frac{0.7}{50}$$

$$\frac{2.2}{37}$$

$$\frac{3.0}{14}$$

$$-2.2$$

St.	+	π	-	Elev.
		918.40 ✓		
71466				12.4 ✓
7240				09.3 ✓
725				08.6 ✓
752	2 Rd.			08.4 ✓
B.M.	4.86	918.50 ✓	4.76	913.64 ✓
766				07.9 ✓
7340				03.9 ✓
750				07.6 ✓
74				09.9 ✓
750				11.4 ✓
75				13.14 14.1
T.P.	9.04	925.43 ✓	2.11	916.39 ✓
750				15.8 ✓
783				19.2 ✓

(Oct. 1-1935) 52

$$\begin{array}{r} 3.6 \\ \hline 50 \end{array} \quad \begin{array}{r} 5.0 \\ \hline 30 \end{array} \quad 6.0 \quad \begin{array}{r} 5.0 \\ \hline 34 \end{array} \quad \begin{array}{r} 7.4 \\ \hline 48 \end{array}$$
$$\begin{array}{r} 73 \\ 50 \end{array} \quad \begin{array}{r} 8.7 \\ 25 \end{array} \quad \begin{array}{r} 9.1 \\ \hline \end{array} \quad \begin{array}{r} 7.7 \\ 15 \end{array} \quad \begin{array}{r} 7.4 \\ 31 \end{array} \quad \begin{array}{r} 10.1 \\ 48 \end{array} \quad \begin{array}{r} 10.5 \\ 75 \end{array} = \text{Edge} \\ 127$$

		EQU			
10.4	11.0	98	10.5	10.6	10.8
<u>5.0</u>	<u>1.9</u>	<u>1</u>	<u>1.9</u>	<u>3.5</u>	<u>5.3</u>
					11.2
					<u>7.5</u>

13.0	12.0	10.0	10.0	10.7	11.2	9.9
50	38	21	1	12	48	87

R.R. Spike Top 3" Oak Stump 60 Lf. Sta. 72

$\frac{13.5}{63}$ $\frac{9.3}{44}$ $\frac{9.6}{19}$ $\frac{10.6}{54.4}$ $\frac{12.2}{26}$ $\frac{11.5}{37}$ $\frac{10.5}{62}$ $\frac{10.5}{89}$

	$\frac{12.1}{88}$	$\frac{8.1}{72.4}$	$\frac{8.1}{57}$	$\frac{8.1}{41.4}$	$\frac{13.8}{22}$	$\frac{14.6}{14.6}$		$\frac{11.6}{34}$	$\frac{11.4}{69}$	$\frac{10.6}{90}$
--	-------------------	--------------------	------------------	--------------------	-------------------	---------------------	--	-------------------	-------------------	-------------------

$$s_k = \frac{5.9}{100} \quad \frac{9.1}{85} \quad \frac{11.2}{38} \quad \frac{10.9}{37} \quad \frac{10.6}{69} \quad \frac{10.7}{86} \quad \frac{9.5}{86}$$

$\frac{41}{70}$	$\frac{63}{30}$	$\frac{86}{-}$	$\frac{96}{44}$	$\frac{92}{82}$
-----------------	-----------------	----------------	-----------------	-----------------

$$\begin{array}{r} 0.0 \\ 70 \end{array} \quad \begin{array}{r} 3.7 \\ 46 \end{array} \quad \begin{array}{r} 7.1 \\ \hline \end{array} \quad \begin{array}{r} 8.4 \\ 34 \end{array} \quad \begin{array}{r} 8.8 \\ 50 \end{array} \quad \begin{array}{r} 11.4 \\ 78 \end{array}$$

0.2	1.5	3.4	5.4	8.0	8.8	11.0	12.4
70	61	38		35	47	65	83

0.3	4.5	9.6	12.0	14.0	14.5
<u>70</u>	<u>33</u>		<u>13</u>	<u>36</u>	<u>50</u>

04	07	24	6.2	12.0	13.1
70	50	26		31	50

Sta.	+	7	-	Elev.
		925.43	✓	
7640				19.1 ✓
+50				13.8 ✓
7740				15.0 ✓
+50				18.0 ✓
7840				20.0 ✓
+50				21.7 ✓
T.P.	6.68	921.47	✓	924.79 ✓
79		0.64		24.3 ✓
+50				26.4 ✓
+75				27.0 ✓
80				24.7 ✓
+35				22.8 ✓
81				23.2 ✓

ct.

E

Rt.

53

$$\begin{array}{r} 2.8 \\ 70 \end{array}$$

$$\begin{array}{r} 2.2 \\ 54 \end{array}$$

$$\begin{array}{r} 2.8 \\ 20 \end{array}$$

$$\begin{array}{r} 6.3 \\ 1 \end{array}$$

$$\begin{array}{r} 11.6 \\ 33 \end{array}$$

$$\begin{array}{r} 12.9 \\ 50 \end{array}$$

$$\begin{array}{r} 10.8 \\ 50 \end{array}$$

$$\begin{array}{r} 10.6 \\ 25 \end{array}$$

$$\begin{array}{r} 11.6 \\ 1 \end{array}$$

$$\begin{array}{r} 13.0 \\ 30 \end{array}$$

$$\begin{array}{r} 13.4 \\ 50 \end{array}$$

$$\begin{array}{r} 11.4 \\ 50 \end{array}$$

$$\begin{array}{r} 10.6 \\ 30 \end{array}$$

$$\begin{array}{r} 10.4 \\ 1 \end{array}$$

$$\begin{array}{r} 10.3 \\ 30 \end{array}$$

$$\begin{array}{r} 10.0 \\ 52 \end{array}$$

$$\begin{array}{r} 7.6 \\ 50 \end{array}$$

$$\begin{array}{r} 6.4 \\ 56 \end{array}$$

$$\begin{array}{r} 7.4 \\ 1 \end{array}$$

$$\begin{array}{r} 8.4 \\ 30 \end{array}$$

$$\begin{array}{r} 9.3 \\ 53 \end{array}$$

$$\begin{array}{r} 2.1 \\ 50 \end{array}$$

$$\begin{array}{r} 1.2 \\ 37 \end{array}$$

$$\begin{array}{r} 2.4 \\ 21 \end{array}$$

$$\begin{array}{r} 2.4 \\ 1 \end{array}$$

$$\begin{array}{r} 10.0 \\ 25 \end{array}$$

$$\begin{array}{r} 12.3 \\ 50 \end{array}$$

$$\begin{array}{r} 4.0 \\ 50 \end{array}$$

$$\begin{array}{r} 4.5 \\ 38 \end{array}$$

$$\begin{array}{r} 0.0 \\ 17 \end{array}$$

$$\begin{array}{r} 3.7 \\ 1 \end{array}$$

$$\begin{array}{r} 9.5 \\ 28 \end{array}$$

$$\begin{array}{r} 12.2 \\ 50 \end{array}$$

$$\begin{array}{r} 3.2 \\ 50 \end{array}$$

$$\begin{array}{r} 2.7 \\ 45 \end{array}$$

$$\begin{array}{r} 3.3 \\ 28 \end{array}$$

$$\begin{array}{r} 7.2 \\ 1 \end{array}$$

$$\begin{array}{r} 12.9 \\ 29 \end{array}$$

$$\begin{array}{r} 16.3 \\ 52 \end{array}$$

$$\begin{array}{r} 4.2 \\ 50 \end{array}$$

$$\begin{array}{r} 2.7 \\ 23 \end{array}$$

$$\begin{array}{r} 5.1 \\ 1 \end{array}$$

$$\begin{array}{r} 9.7 \\ 32 \end{array}$$

$$\begin{array}{r} 11.3 \\ 50 \end{array}$$

$$\begin{array}{r} 13.5 \\ 69 \end{array}$$

$$\begin{array}{r} 4.2 \\ 50 \end{array}$$

$$\begin{array}{r} 3.1 \\ 33 \end{array}$$

$$\begin{array}{r} 3.2 \\ 20 \end{array}$$

$$\begin{array}{r} 4.5 \\ 1 \end{array}$$

$$\begin{array}{r} 9.0 \\ 24 \end{array}$$

$$\begin{array}{r} 11.2 \\ 50 \end{array}$$

$$\begin{array}{r} 12.6 \\ 70 \end{array}$$

$$\begin{array}{r} 4.2 \\ 50 \end{array}$$

$$\begin{array}{r} 4.2 \\ 35 \end{array}$$

$$\begin{array}{r} 4.8 \\ 17 \end{array}$$

$$\begin{array}{r} 6.8 \\ 1 \end{array}$$

$$\begin{array}{r} 9.6 \\ 25 \end{array}$$

$$\begin{array}{r} 11.5 \\ 50 \end{array}$$

$$\begin{array}{r} 13.7 \\ 70 \end{array}$$

$$\begin{array}{r} 7.3 \\ 50 \end{array}$$

$$\begin{array}{r} 6.6 \\ 25 \end{array}$$

$$\begin{array}{r} 8.7 \\ 1 \end{array}$$

$$\begin{array}{r} 10.6 \\ 21 \end{array}$$

$$\begin{array}{r} 12.0 \\ 42 \end{array}$$

$$\begin{array}{r} 15.8 \\ 70 \end{array}$$

$$\begin{array}{r} 7.0 \\ 50 \end{array}$$

$$\begin{array}{r} 6.4 \\ 35 \end{array}$$

$$\begin{array}{r} 6.8 \\ 21 \end{array}$$

$$\begin{array}{r} 8.3 \\ 1 \end{array}$$

$$\begin{array}{r} 9.8 \\ 25 \end{array}$$

$$\begin{array}{r} 13.0 \\ 46 \end{array}$$

$$\begin{array}{r} 16.0 \\ 62 \end{array}$$

$$\begin{array}{r} 17.5 \\ 75 \end{array}$$

Sta.	+	π	-	Elev.
		931.47 ✓		
81+30				23.0 ✓
+70				21.1 ✓
T.P.	5.76	924.44 ✓	12.79	918.68 ✓
82+0				18.0 ✓
+40				14.8 ✓
+70				14.8 ✓
83+0				14.3 ✓
+23				14.7 ✓
+65				18.2 ✓
84+0				20.7 ✓
T.P.	10.70	932.35 ✓	2.79	921.65 ✓
+55				25.9 ✓
85+0				25.0 ✓
+30				27.4 ✓

$$\begin{array}{r} 7.7 \\ 50 \end{array} \quad \begin{array}{r} 6.7 \\ 40 \end{array} \quad \begin{array}{r} 8.5 \\ 1 \end{array} \quad \begin{array}{r} 8.9 \\ 23 \end{array} \quad \begin{array}{r} 12.9 \\ 49 \end{array} \quad \begin{array}{r} 15.5 \\ 63 \end{array} \quad \begin{array}{r} 17.1 \\ 76 \end{array}$$

$$\begin{array}{r} 12.5 \\ 50 \end{array} \quad \begin{array}{r} 10.5 \\ 27 \end{array} \quad \begin{array}{r} 10.4 \\ 1 \end{array} \quad \begin{array}{r} 10.8 \\ 24 \end{array} \quad \begin{array}{r} 13.3 \\ 55 \end{array} \quad \begin{array}{r} 15.4 \\ 62 \end{array} \quad \begin{array}{r} 17.0 \\ 75 \end{array}$$

$$\begin{array}{r} 9.3 \\ 50 \end{array} \quad \begin{array}{r} 7.8 \\ 26 \end{array} \quad \begin{array}{r} 6.4 \\ 1 \end{array} \quad \begin{array}{r} 5.6 \\ 28 \end{array} \quad \begin{array}{r} 6.4 \\ 43 \end{array} \quad \begin{array}{r} 7.3 \\ 56 \end{array} \quad \begin{array}{r} 8.9 \\ 60 \end{array} \quad \begin{array}{r} 10.7 \\ 78 \end{array}$$

$$\begin{array}{r} 13.3 \\ 50 \end{array} \quad \begin{array}{r} 11.3 \\ 22 \end{array} \quad \begin{array}{r} 9.6 \\ 1 \end{array} \quad \begin{array}{r} 7.3 \\ 26 \end{array} \quad \begin{array}{r} 7.5 \\ 38 \end{array} \quad \begin{array}{r} 8.7 \\ 54 \end{array} \quad \begin{array}{r} 9.7 \\ 63 \end{array} \quad \begin{array}{r} 12.6 \\ 82 \end{array}$$

$$\begin{array}{r} 13.3 \\ 50 \end{array} \quad \begin{array}{r} 11.6 \\ 21 \end{array} \quad \begin{array}{r} 7.6 \\ 1 \end{array} \quad \begin{array}{r} 8.5 \\ 76 \end{array} \quad \begin{array}{r} 8.5 \\ 29 \end{array} \quad \begin{array}{r} 11.3 \\ 52 \end{array} \quad \begin{array}{r} 12.5 \\ 57 \end{array} \quad \begin{array}{r} 13.0 \\ 83 \end{array}$$

$$\begin{array}{r} 12.0 \\ 50 \end{array} \quad \begin{array}{r} 11.2 \\ 26 \end{array} \quad \begin{array}{r} 11.0 \\ 12 \end{array} \quad \begin{array}{r} 10.1 \\ 1 \end{array} \quad \begin{array}{r} 9.5 \\ 20 \end{array} \quad \begin{array}{r} 12.6 \\ 43 \end{array} \quad \begin{array}{r} 13.7 \\ 63 \end{array} \quad \begin{array}{r} 14.5 \\ 83 \end{array}$$

$$\begin{array}{r} 9.3 \\ 50 \end{array} \quad \begin{array}{r} 8.7 \\ 31 \end{array} \quad \begin{array}{r} 9.7 \\ 1 \end{array} \quad \begin{array}{r} 10.8 \\ 18 \end{array} \quad \begin{array}{r} 13.0 \\ 40 \end{array} \quad \begin{array}{r} 13.1 \\ 51 \end{array} \quad \begin{array}{r} 14.1 \\ 61 \end{array} \quad \begin{array}{r} 14.8 \\ 82 \end{array}$$

$$\begin{array}{r} 1.5 \\ 50 \end{array} \quad \begin{array}{r} 1.7 \\ 42 \end{array} \quad \begin{array}{r} 4.2 \\ 72 \end{array} \quad \begin{array}{r} 6.2 \\ 1 \end{array} \quad \begin{array}{r} 10.6 \\ 23 \end{array} \quad \begin{array}{r} 12.2 \\ 37 \end{array} \quad \begin{array}{r} 12.6 \\ 51 \end{array} \quad \begin{array}{r} 14.0 \\ 81 \end{array}$$

$$\begin{array}{r} 13.2 \\ 50 \end{array} \quad \begin{array}{r} 11.9 \\ 46 \end{array} \quad \begin{array}{r} 0.4 \\ 19 \end{array} \quad \begin{array}{r} 3.7 \\ 1 \end{array} \quad \begin{array}{r} 5.8 \\ 11 \end{array} \quad \begin{array}{r} 7.5 \\ 28 \end{array} \quad \begin{array}{r} 9.3 \\ 52 \end{array} \quad \begin{array}{r} 11.8 \\ 80 \end{array}$$

$$\begin{array}{r} 5.2 \\ 50 \end{array} \quad \begin{array}{r} 7.2 \\ 20 \end{array} \quad \begin{array}{r} 6.5 \\ 1 \end{array} \quad \begin{array}{r} 6.0 \\ 18 \end{array} \quad \begin{array}{r} 6.9 \\ 38 \end{array} \quad \begin{array}{r} 8.1 \\ 56 \end{array}$$

$$\begin{array}{r} 9.3 \\ 50 \end{array} \quad \begin{array}{r} 9.3 \\ 30 \end{array} \quad \begin{array}{r} 7.4 \\ 1 \end{array} \quad \begin{array}{r} 5.1 \\ 25 \end{array} \quad \begin{array}{r} 5.2 \\ 37 \end{array} \quad \begin{array}{r} 6.5 \\ 52 \end{array}$$

$$\begin{array}{r} 10.2 \\ 50 \end{array} \quad \begin{array}{r} 7.7 \\ 24 \end{array} \quad \begin{array}{r} 5.0 \\ 1 \end{array} \quad \begin{array}{r} 3.7 \\ 15 \end{array} \quad \begin{array}{r} 4.2 \\ 32 \end{array} \quad \begin{array}{r} 6.2 \\ 50 \end{array}$$

Sta. + π - Elev.

932.35 ✓

85+60

28.5 ✓

86+0

26.9 ✓

+60

25.2 ✓

87

22.9 ✓

+45

19.3 ✓

T.D

8.53

928.17 ✓

12.71

919.64 ✓

88

16.8 ✓

+75

20.1 ✓

89

19.5 ✓

+25

19.8 ✓

+75

21.4 ✓

90+0

20.1 ✓

+50

18.1 ✓

Lt.

S

Rt.

55

8.0	5.0	3.9	3.9	4.2	7.0	9.0
<u>5.0</u>	<u>2.5</u>	<u>8</u>	<u>0</u>	<u>1.4</u>	<u>7.3</u>	<u>4.8</u>

5.2	4.0	4.6	5.5	7.8	11.1	14.1
<u>5.0</u>	<u>2.9</u>	<u>7</u>	<u>1</u>	<u>1.5</u>	<u>3.0</u>	<u>4.8</u>

7.0	5.4	6.1	7.2	8.4	14.5	15.3
<u>5.0</u>	<u>2.3</u>	<u>7</u>	<u>1</u>	<u>9</u>	<u>3.6</u>	<u>5.0</u>

7.8	8.2	8.5	9.5	10.6	12.2	15.0	15.4
<u>5.0</u>	<u>3.1</u>	<u>1.4</u>	<u>1</u>	<u>1.1</u>	<u>2.2</u>	<u>4.1</u>	<u>5.1</u>

10.0	10.4	11.8	13.1	14.1	15.0	16.3	17.4
<u>5.0</u>	<u>3.9</u>	<u>2.0</u>		<u>2.3</u>	<u>5.3</u>	<u>7.6</u>	<u>8.1</u>

TOP Rail / 100' Bl. Sds. 28 to

11.6	11.3	11.1	11.5	11.3
<u>5.0</u>	<u>2.5</u>	<u>1</u>	<u>2.8</u>	<u>5.2</u>

9.7	8.6	8.1	8.0	7.9
<u>5.0</u>	<u>1.7</u>	<u>1</u>	<u>2.8</u>	<u>5.2</u>

8.2	8.4	8.7	8.7
<u>5.0</u>	<u>3.1</u>		<u>5.2</u>

5.0	6.8	8.4	9.1	9.4
<u>5.0</u>	<u>3.0</u>	<u>1</u>	<u>2.6</u>	<u>5.2</u>

1.1	3.5	6.8	9.7	11.5
<u>5.0</u>	<u>2.4</u>		<u>2.4</u>	<u>5.2</u>

0.7	1.8	6.1	8.1	10.4	11.7
<u>5.0</u>	<u>3.9</u>	<u>1.7</u>	<u>1</u>	<u>3.5</u>	<u>5.2</u>

2.4	4.7	8.1	10.1	11.4	12.2
<u>5.0</u>	<u>2.6</u>	<u>1.2</u>	<u>1</u>	<u>1.7</u>	<u>5.2</u>

Sta. + A - E/eV.

928.17 ✓

9140

17.5 ✓

+32

16.9 ✓

+65

16.9 ✓

9240

17.0 ✓

+50

18.8 ✓

9340

17.7 ✓

B.M.

4.46

928.61 ✓

6.98

921.19 ✓

921.15 ✓

+50

16.01 ✓

9440

16.8 ✓

+40

17.11 ✓

19.7

95

20.4 ✓

+30

20.6 ✓

+73

24.9 ✓

T.P.

6.94

931.94 ✓

0.61

925.00 ✓

Lt.

Z

Rt.

56

$\frac{5.9}{50}$	$\frac{6.1}{32}$	$\frac{10.7}{17}$	$\frac{11.7}{17}$	$\frac{12.2}{52}$
------------------	------------------	-------------------	-------------------	-------------------

$\frac{7.3}{50}$	$\frac{8.0}{32}$	$\frac{10.1}{16}$	$\frac{11.3}{17}$	$\frac{11.8}{17}$	$\frac{12.2}{52}$
------------------	------------------	-------------------	-------------------	-------------------	-------------------

$\frac{4.2}{50}$	$\frac{6.4}{31}$	$\frac{5.6}{18}$	$\frac{11.3}{17}$	$\frac{12.0}{25}$	$\frac{12.1}{52}$
------------------	------------------	------------------	-------------------	-------------------	-------------------

$\frac{4.6}{50}$	$\frac{4.4}{38}$	$\frac{7.0}{23}$	$\frac{11.2}{17}$	$\frac{12.1}{28}$	$\frac{12.0}{52}$
------------------	------------------	------------------	-------------------	-------------------	-------------------

$\frac{11.9}{50}$	$\frac{10.0}{34}$	$\frac{8.2}{17}$	$\frac{9.4}{17}$	$\frac{11.6}{30}$	$\frac{10.7}{52}$
-------------------	-------------------	------------------	------------------	-------------------	-------------------

$\frac{13.0}{50}$	$\frac{12.1}{17}$	$\frac{10.5}{17}$	$\frac{8.9}{26}$	$\frac{7.3}{52}$
-------------------	-------------------	-------------------	------------------	------------------

R.R. Spike in F.P. 52' Rt. Sta. 93 + 20

$\frac{10.6}{50}$	$\frac{9.60}{17}$	$\frac{8.2}{26}$	$\frac{6.3}{52}$
-------------------	-------------------	------------------	------------------

Ditch

$\frac{7.6}{50}$	$\frac{8.3}{31}$	$\frac{9.6}{74}$	$\frac{8.8}{17}$	$\frac{7.8}{25}$	$\frac{6.6}{52}$
------------------	------------------	------------------	------------------	------------------	------------------

$\frac{8.0}{50}$	$\frac{8.4}{30}$	$\frac{8.5}{17}$	$\frac{8.0}{29}$	$\frac{9.2}{40}$	$\frac{9.0}{52}$
------------------	------------------	------------------	------------------	------------------	------------------

$\frac{6.6}{50}$	$\frac{6.6}{26}$	$\frac{5.2}{17}$	$\frac{6.4}{37}$	$\frac{8.1}{52}$
------------------	------------------	------------------	------------------	------------------

$\frac{4.6}{50}$	$\frac{4.3}{21}$	$\frac{5.0}{17}$	$\frac{6.7}{22}$	$\frac{8.7}{52}$
------------------	------------------	------------------	------------------	------------------

$\frac{7.8}{50}$	$\frac{5.1}{21}$	$\frac{0.7}{17}$	$\frac{1.7}{16}$	$\frac{4.9}{34}$	$\frac{7.6}{52}$
------------------	------------------	------------------	------------------	------------------	------------------

Top Stone 50' Rt.

Station + π - E/ev.

93.94 ✓

25.4
26.4

96

+50

27.1 ✓

97

25.5 ✓

+50

25.7 ✓

98

22.4 ✓

+50

15.4 ✓

T.P.

3.62

92.13 ✓

13.43

918.51 ✓

+75

12.5 ✓

99

12.1 ✓

100

11.2 ✓

101

10.8 ✓

102

10.6 ✓

103

10.7 ✓

Lt.

Z

Rt.

57

$$\frac{9.0}{50}$$

$$\frac{6.7}{21}$$

$$\frac{6.5}{21}$$

$$\frac{6.8}{20}$$

$$\frac{9.4}{35}$$

$$\frac{11.0}{52}$$

$$\frac{8.2}{50}$$

$$\frac{5.7}{22}$$

$$\frac{4.8}{22}$$

$$\frac{3.8}{28}$$

$$\frac{4.0}{52}$$

$$\frac{9.7}{50}$$

$$\frac{8.0}{23}$$

$$\frac{6.4}{23}$$

$$\frac{5.0}{25}$$

$$\frac{4.7}{52}$$

$$\frac{10.7}{50}$$

$$\frac{8.0}{20}$$

$$\frac{6.2}{20}$$

$$\frac{3.9}{25}$$

$$\frac{2.7}{52}$$

$$\frac{14.1}{50}$$

$$\frac{12.3}{25}$$

$$\frac{9.5}{25}$$

$$\frac{6.3}{23}$$

$$\frac{3.8}{52}$$

$$\frac{12.0}{50}$$

$$\frac{17.5}{31}$$

$$\frac{12.5}{31}$$

$$\frac{15.0}{30}$$

$$\frac{13.6}{52}$$

$$\frac{9.6}{50}$$

$$\frac{9.5}{25}$$

$$\frac{9.6}{25}$$

$$\frac{9.2}{26}$$

$$\frac{7.8}{52}$$

$$\frac{10.3}{50}$$

$$\frac{10.0}{50}$$

$$\frac{9.4}{52}$$

$$\frac{11.0}{50}$$

$$\frac{10.9}{50}$$

$$\frac{10.7}{52}$$

$$\frac{11.2}{50}$$

$$\frac{11.3}{50}$$

$$\frac{11.3}{52}$$

$$\frac{11.5}{50}$$

$$\frac{11.5}{50}$$

$$\frac{11.9}{52}$$

$$\frac{11.6}{50}$$

$$\frac{11.4}{50}$$

$$\frac{11.4}{50}$$

Station	+	π	-	Elev.
		922.13 ✓		
104				911.1 ✓
T.P.	8.99	923.80 ✓	7.32	914.81 ✓
105				10.9 ✓
106				10.0 ✓
107				10.5 ✓
108				10.7 ✓
109				11.4 ✓
+30				12.6 ✓
+70				17.9 ✓
110+0				20.3 ✓
T.P.	4.37	925.60 ✓	2.57	921.23 ✓
+35				18.4 ✓
B.M.	4.68	926.05 ✓	4.23	921.37 ✓
+70				16.7 ✓
111				16.8 ✓

Lt.

L

Rt.

58

$$\begin{array}{r} 11.3 \\ 50 \end{array}$$

$$\begin{array}{r} 11.0 \\ 50 \end{array}$$

$$\begin{array}{r} 10.8 \\ 52 \end{array}$$

$$\begin{array}{r} 13.1 \\ 50 \end{array}$$

$$\begin{array}{r} 12.9 \\ 50 \end{array}$$

$$\begin{array}{r} 13.3 \\ 52 \end{array}$$

$$\begin{array}{r} 13.4 \\ 50 \end{array}$$

$$\begin{array}{r} 13.8 \\ 50 \end{array}$$

$$\begin{array}{r} 13.5 \\ 52 \end{array}$$

$$\begin{array}{r} 13.5 \\ 50 \end{array}$$

$$\begin{array}{r} 13.3 \\ 50 \end{array}$$

$$\begin{array}{r} 13.3 \\ 52 \end{array}$$

$$\begin{array}{r} 13.0 \\ 50 \end{array}$$

$$\begin{array}{r} 13.1 \\ 50 \end{array}$$

$$\begin{array}{r} 13.3 \\ 52 \end{array}$$

$$\begin{array}{r} 12.2 \\ 50 \end{array}$$

$$\begin{array}{r} 12.4 \\ 50 \end{array}$$

$$\begin{array}{r} 12.2 \\ 52 \end{array}$$

$$\begin{array}{r} 10.1 \\ 50 \end{array}$$

$$\begin{array}{r} 10.6 \\ 75 \end{array}$$

$$\begin{array}{r} 11.2 \\ 50 \end{array}$$

$$\begin{array}{r} 10.6 \\ 52 \end{array}$$

$$\begin{array}{r} 8.6 \\ 50 \end{array}$$

$$\begin{array}{r} 6.2 \\ 78 \end{array}$$

$$\begin{array}{r} 5.9 \\ 50 \end{array}$$

$$\begin{array}{r} 5.6 \\ 79 \end{array}$$

$$\begin{array}{r} 5.8 \\ 52 \end{array}$$

$$\begin{array}{r} 10.1 \\ 78 \end{array}$$

$$\begin{array}{r} 8.0 \\ 60 \end{array}$$

$$\begin{array}{r} 5.0 \\ 24 \end{array}$$

$$\begin{array}{r} 3.5 \\ 50 \end{array}$$

$$\begin{array}{r} 3.4 \\ 20 \end{array}$$

$$\begin{array}{r} 4.6 \\ 52 \end{array}$$

Oct. 8-1935

Edge Pav.	6.00	6.5	7.2	7.7	8.8	7.7	7.2	7.0	7.0
ho.	93	80	74	70	50	34	—	32	52

Top of Pav. & Co. Rd. G.

Edge Pav.	6.08	6.5	7.2	7.7	8.8	7.7	7.2	7.0	7.0
	83	72	56	45	16	—	—	20	52

Edge Pav.	5.58	6.3	7.2	7.7	8.8	7.7	7.2	7.0	7.0
	44	47	28	21	16	—	—	14	52

Station + π - Elev.

926.05 ✓

111+34

17.1 ✓

+46 - shldr

20.7 ✓

+54 E. Pav.

21.18 ✓

+84 E. Pav.

21.25 ✓

+94 shldr.

21.1 ✓

112+0

18.9 ✓

+09

18.9 ✓

+20

21.7 ✓

+70

20.0 ✓

113

19.6 ✓

+60

19.0 ✓

114

19.0 ✓

Lt

L

Rt

59

$\frac{13.2}{100}$	$\frac{11.4}{65}$	$\frac{5.5}{51}$	$\frac{5.45}{430}$	$\frac{5.11}{16.0}$	$\frac{5.4}{9}$	$\frac{9.0}{6}$	$\frac{9.3}{11}$	$\frac{7.2}{20}$	$\frac{6.7}{52}$
Avg.									

$\frac{12.0}{100}$	$\frac{12.6}{85}$	$\frac{11.0}{56}$	$\frac{5.3}{41}$	$\frac{5.25}{35.0}$	$\frac{5.01}{8.0}$	$\frac{5.4}{9}$	$\frac{8.5}{16}$	$\frac{8.7}{20}$	$\frac{6.4}{26}$	$\frac{6.1}{52}$	$\frac{5.8}{52}$
Avg.											

$\frac{12.5}{90}$	$\frac{10.0}{46}$	$\frac{5.3}{34}$	$\frac{5.14}{28.0}$	$\frac{5.4}{9}$	$\frac{4.87}{7}$	$\frac{5.0}{15}$	$\frac{8.4}{22}$	$\frac{8.3}{26}$	$\frac{5.8}{52}$	$\frac{5.3}{52}$
Avg.										

$\frac{10.4}{85}$	$\frac{7.5}{35}$	$\frac{7.0}{27}$	$\frac{8.1}{19}$	$\frac{5.0}{9}$	$\frac{4.8}{6}$	$\frac{4.65}{270}$	$\frac{5.2}{38}$	$\frac{7.4}{43}$	$\frac{4.3}{50}$
Avg.									

$\frac{10.2}{85}$	$\frac{8.9}{53}$	$\frac{5.9}{19}$	$\frac{7.8}{13}$	$\frac{7.5}{10}$	$\frac{5.0}{8}$	$\frac{4.8}{35}$	$\frac{4.53}{44}$	$\frac{4.8}{51}$	$\frac{6.1}{69}$	$\frac{5.7}{77}$	$\frac{7.2}{77}$
Avg.											

$\frac{10.3}{90}$	$\frac{8.1}{43}$	$\frac{5.4}{15}$	$\frac{7.4}{8}$	$\frac{7.2}{7}$	$\frac{4.8}{15}$	$\frac{4.65}{44}$	$\frac{4.48}{52}$	$\frac{4.6}{60}$	$\frac{6.5}{68}$	$\frac{6.0}{79}$	$\frac{6.0}{79}$	$\frac{2.1}{79}$
Avg.												

$\frac{10.0}{90}$	$\frac{8.8}{60}$	$\frac{4.9}{11}$	$\frac{4.7}{6}$	$\frac{7.2}{6}$	$\frac{7.3}{14}$	$\frac{5.0}{23}$	$\frac{4.55}{50}$	$\frac{4.42}{61}$	$\frac{4.7}{67}$	$\frac{6.0}{72}$	$\frac{6.0}{79}$	$\frac{7.8}{79}$
Avg.												

$\frac{9.8}{90}$	$\frac{8.5}{60}$	$\frac{6.0}{20}$	$\frac{4.4}{6}$	$\frac{7.3}{6}$	$\frac{7.3}{14}$	$\frac{4.9}{22}$	$\frac{4.50}{52}$	$\frac{4.28}{52}$	$\frac{4.28}{58}$
Avg.									

$\frac{7.8}{50}$	$\frac{7.1}{25}$	$\frac{6.1}{79}$	$\frac{5.3}{79}$	$\frac{4.0}{52}$
------------------	------------------	------------------	------------------	------------------

$\frac{7.7}{50}$	$\frac{7.4}{25}$	$\frac{6.5}{29}$	$\frac{5.9}{29}$	$\frac{4.6}{52}$
------------------	------------------	------------------	------------------	------------------

$\frac{7.3}{50}$	$\frac{7.5}{25}$	$\frac{7.1}{20}$	$\frac{6.6}{20}$	$\frac{5.0}{52}$
------------------	------------------	------------------	------------------	------------------

$\frac{8.5}{50}$	$\frac{8.0}{25}$	$\frac{7.1}{32}$	$\frac{5.0}{32}$	$\frac{1.7}{52}$
------------------	------------------	------------------	------------------	------------------

Station	+	π	-	Elev.
		926.05		
114+50				19.4 ✓
115				21.5 ✓
T.P	3.55	925.91 ✓	3.69	922.36 ✓
+50				19.5 ✓
116				17.5 ✓
+60				16.3 ✓
117				18.7 ✓
+30				21.9 ✓
+45				21.7 ✓
T.R	0.88	922.64 ✓	4.15	921.76 ✓
118				15.1 ✓
+25				12.9 ✓
+75				12.0 ✓
119				12.9 ✓

Lt.

♀

Rt.

60

$$\frac{9.6}{50}$$

$$\frac{8.6}{19}$$

$$\frac{6.7}{-}$$

$$\frac{1.5}{31}$$

$$\frac{+2.8}{52}$$

$$\frac{10.4}{50}$$

$$\frac{8.4}{17}$$

$$4.6$$

$$\frac{1.7}{12}$$

$$\frac{+2.0}{30}$$

$$\frac{+3.2}{52}$$

$$\frac{11.4}{50}$$

$$\frac{11.0}{36}$$

$$\frac{10.0}{22}$$

$$6.4$$

$$\frac{3.1}{16}$$

$$\frac{1.0}{29}$$

$$\frac{+1.1}{50}$$

$$\frac{12.0}{50}$$

$$\frac{10.7}{21}$$

$$\frac{8.4}{-}$$

$$\frac{5.9}{20}$$

$$\frac{3.6}{35}$$

$$\frac{3.5}{50}$$

$$\frac{11.0}{50}$$

$$\frac{10.2}{23}$$

$$9.6$$

$$\frac{8.6}{24}$$

$$\frac{8.0}{50}$$

$$\frac{9.7}{50}$$

$$\frac{8.3}{25}$$

$$\frac{7.2}{-}$$

$$\frac{8.0}{31}$$

$$\frac{7.7}{50}$$

$$\frac{8.3}{50}$$

$$\frac{6.6}{27}$$

$$\frac{4.0}{-}$$

$$\frac{4.5}{20}$$

$$\frac{7.0}{41}$$

$$\frac{6.6}{49}$$

$$\frac{8.2}{50}$$

$$\frac{7.0}{33}$$

$$\frac{5.0}{12}$$

$$\frac{4.2}{-}$$

$$\frac{4.1}{18}$$

$$\frac{6.3}{38}$$

$$\frac{6.6}{50}$$

Hub ♀

$$\frac{7.3}{50}$$

$$\frac{7.6}{27}$$

$$7.5$$

$$\frac{6.7}{33}$$

$$\frac{5.1}{50}$$

$$\frac{6.6}{52}$$

$$\frac{9.7}{50}$$

$$\frac{9.9}{24}$$

$$9.7$$

$$\frac{9.4}{18}$$

$$\frac{7.8}{46}$$

$$\frac{8.0}{52}$$

$$\frac{11.5}{50}$$

$$\frac{11.0}{25}$$

$$10.6$$

$$\frac{10.2}{23}$$

$$\frac{9.8}{52}$$

$$\frac{11.2}{50}$$

$$\frac{10.4}{29}$$

$$9.7$$

$$\frac{8.6}{33}$$

$$\frac{8.5}{40}$$

$$\frac{10.0}{50}$$

Station	+	π	-	Elev.
		922.64		
119+32				14.7 ✓
+60				14.8 ✓
120				13.4 ✓
+50				15.4 ✓
B.M.	5.58	923.02 ✓	5.20	917.44 ✓
121				12.0 ✓
+25				10.9 ✓
122				09.9 ✓
+60				13.0 ✓
122+87				15.0 ✓
123+08				23.0 ✓
123+20				23.0 ✓
123+60				14.4 ✓

Lt.

L

Rt.

61

 $\frac{10.6}{50}$ $\frac{9.5}{26}$

7.9

 $\frac{6.8}{22}$ $\frac{6.8}{45}$ $\frac{7.2}{49}$ $\frac{8.7}{61}$ $\frac{10.4}{50}$ $\frac{10.0}{78}$ $\frac{7.8}{-}$ $\frac{6.8}{19}$ $\frac{5.9}{47}$ $\frac{8.5}{52}$ $\frac{8.7}{60}$ $\frac{8.6}{50}$ $\frac{9.3}{25}$ $\frac{9.4}{-}$ $\frac{7.6}{31}$ $\frac{6.3}{52}$ $\frac{8.2}{56}$ $\frac{7.8}{63}$ $\frac{4.6}{50}$ $\frac{5.6}{21}$

7.2

 $\frac{7.2}{25}$ $\frac{5.2}{57}$ $\frac{6.8}{60}$ $\frac{6.7}{65}$

R. R. Spike in 20' Dak 50' Rt. Sta. 120 +26

 $\frac{10.5}{50}$ $\frac{11.0}{24}$ $\frac{11.0}{-}$ $\frac{10.3}{26}$ $\frac{9.1}{52}$ $\frac{8.6}{63}$ $\frac{12.4}{50}$ $\frac{12.6}{24}$ $\frac{12.1}{-}$ $\frac{12.0}{35}$ $\frac{11.4}{52}$ $\frac{11.0}{61}$ $\frac{12.2}{50}$ $\frac{12.8}{27}$ $\frac{13.1}{-}$ $\frac{13.0}{34}$ $\frac{13.0}{59}$ $\frac{10.3}{50}$ $\frac{9.1}{35}$

10.0

 $\frac{11.0}{25}$ $\frac{11.9}{60}$ $\frac{9.0}{50}$ $\frac{4.5}{25}$ $\frac{4.0}{15}$

8.0

 $\frac{9.2}{27}$ $\frac{10.2}{59}$ $\frac{9.8}{50}$ $\frac{8.2}{20}$ $\frac{1.6}{12}$

0.0

 $\frac{0.0}{31}$ $\frac{8.0}{32}$ $\frac{9.1}{50}$ $\frac{9.6}{56}$ $\frac{10.5}{50}$ $\frac{9.4}{36}$ $\frac{8.6}{24}$ $\frac{0.0}{-}$ $\frac{10.5}{15}$ $\frac{6.8}{40}$ $\frac{7.4}{52}$ $\frac{9.3}{54}$ $\frac{7.4}{60}$ $\frac{12.2}{50}$ $\frac{10.7}{33}$ $\frac{10.0}{20}$ $\frac{8.6}{-}$ $\frac{7.0}{6}$ $\frac{10.3}{33}$ $\frac{11.3}{52}$

Station	+	Δ	-	Elev.
		923.02 ✓		
124 to				12.7 ✓
+58				13.6 ✓
125 to				13.0 ✓
+56				17.0 ✓
126				22.5 ✓
	4.79	927.76 ✓	0.05	922.97 ✓
+36 27				23.8 ✓
+63				21.8 ✓
127				15.6 ✓
+40				12.6 ✓
128				12.6 ✓
+63				13.1 ✓
129				15.3 ✓
J.R.	13.45	931.11 ✓	10.10	917.66 ✓

Lt.

L

Rt.

62

$$\frac{144}{50}$$

$$\frac{124}{25}$$

$$103$$

$$\frac{9.0}{17}$$

$$\frac{6.3}{30}$$

$$\frac{11.1}{45}$$

$$\frac{11.9}{52}$$

$$\frac{12.8}{50}$$

$$\frac{11.1}{14}$$

$$94$$

$$\frac{6.3}{20}$$

$$\frac{2.6}{35}$$

$$\frac{10.6}{44}$$

$$\frac{10.0}{50}$$

$$\frac{8.8}{20}$$

$$\frac{10.0}{20}$$

$$\frac{10.4}{20}$$

$$\frac{10.0}{50}$$

$$\frac{11.6}{50}$$

$$\frac{20}{41}$$

$$\frac{2.3}{26}$$

$$\frac{6.0}{22}$$

$$\frac{8.6}{22}$$

$$\frac{9.0}{40}$$

$$\frac{10.5}{52}$$

$$\frac{10.5}{60}$$

$$\frac{+7.0}{75}$$

$$\frac{+10.1}{50}$$

$$\frac{+9.8}{43}$$

$$\frac{+4.8}{21}$$

$$\frac{0.5}{26}$$

$$\frac{5.8}{26}$$

$$\frac{7.0}{40}$$

$$\frac{8.5}{50}$$

$$\frac{8.5}{60}$$

$$\frac{+1.2}{70}$$

$$\frac{+4.5}{47}$$

$$\frac{+3.8}{33}$$

$$\frac{0.5}{14}$$

$$\frac{4.0}{26}$$

$$\frac{9.5}{26}$$

$$\frac{10.8}{39}$$

$$\frac{12.5}{50}$$

$$\frac{13.0}{60}$$

$$\frac{+0.6}{50}$$

$$\frac{+1.0}{41}$$

$$\frac{0.0}{29}$$

$$\frac{3.4}{11}$$

$$6.0$$

$$\frac{10.7}{21}$$

$$\frac{11.5}{34}$$

$$\frac{13.1}{50}$$

$$\frac{13.0}{59}$$

$$\frac{5.6}{50}$$

$$\frac{6.4}{37}$$

$$\frac{10.0}{18}$$

$$\frac{12.2}{15}$$

$$\frac{14.5}{15}$$

$$\frac{15.0}{30}$$

$$\frac{14.1}{60}$$

$$\frac{9.1}{50}$$

$$\frac{11.2}{39}$$

$$\frac{14.3}{20}$$

$$\frac{15.2}{15}$$

$$\frac{15.1}{50}$$

$$\frac{14.0}{57}$$

$$\frac{14.5}{50}$$

$$\frac{15.2}{30}$$

$$\frac{15.2}{15}$$

$$\frac{14.8}{50}$$

$$\frac{14.4}{62}$$

$$\frac{15.0}{50}$$

$$\frac{14.7}{15}$$

$$\frac{15.1}{50}$$

$$\frac{15.0}{63}$$

$$\frac{12.4}{50}$$

$$\frac{13.5}{35}$$

$$\frac{12.5}{15}$$

$$\frac{12.8}{50}$$

$$\frac{10.4}{70}$$

Station	+	π	-	Elev.
---------	---	-------	---	-------

931.11 ✓

129+60

19.3 ✓

130

25.1 ✓

T.P.

13.27

944.17

0.21

930.90 ✓

+50

35.9 ✓

T.P.

11.23

954.55 ✓

0.85

943.82 ✓

130+88

43.1 ✓

131+14

45.2 ✓

+50

44.8 ✓

132

47.8 ✓

+65

44.5 ✓

133

47.1 ✓

+50

46.7 ✓

134

47.2 ✓

+50

50.5 ✓

Lt.

L

et.

63

$$\frac{7.5}{50}$$

$$\frac{9.3}{25}$$

$$\frac{11.8}{-}$$

$$\frac{12.3}{23}$$

$$\frac{12.0}{51}$$

$$\frac{10.7}{74}$$

$$\frac{0.8}{50}$$

$$\frac{1.5}{40}$$

$$\frac{4.0}{16}$$

$$\frac{6.0}{-}$$

$$\frac{8.3}{20}$$

$$\frac{9.2}{44}$$

$$\frac{9.2}{76}$$

$$\frac{7.2}{50}$$

$$\frac{6.5}{76}$$

$$\frac{8.3}{-}$$

$$\frac{10.6}{35}$$

$$\frac{11.2}{52}$$

$$\frac{12.9}{50}$$

$$\frac{11.5}{41}$$

$$\frac{10.5}{22}$$

$$\frac{11.5}{-}$$

$$\frac{12.9}{21}$$

$$\frac{15.7}{52}$$

$$\frac{10.5}{50}$$

$$\frac{8.6}{37}$$

$$\frac{8.0}{23}$$

$$\frac{9.4}{-}$$

$$\frac{10.8}{32}$$

$$\frac{12.3}{52}$$

$$\frac{15.7}{70}$$

$$\frac{8.2}{50}$$

$$\frac{7.5}{32}$$

$$\frac{8.8}{18}$$

$$\frac{9.8}{-}$$

$$\frac{8.6}{27}$$

$$\frac{10.1}{52}$$

$$\frac{13.2}{68}$$

$$\frac{5.9}{50}$$

$$\frac{7.0}{22}$$

$$\frac{6.8}{-}$$

$$\frac{7.4}{17}$$

$$\frac{11.8}{44}$$

$$\frac{13.5}{54}$$

$$\frac{17.1}{72}$$

$$\frac{6.4}{50}$$

$$\frac{7.5}{31}$$

$$\frac{10.1}{-}$$

$$\frac{13.0}{31}$$

$$\frac{14.0}{53}$$

$$\frac{12.6}{68}$$

$$\frac{3.4}{75}$$

$$\frac{3.6}{50}$$

$$\frac{6.5}{22}$$

$$\frac{7.5}{-}$$

$$\frac{10.1}{29}$$

$$\frac{10.6}{44}$$

$$\frac{9.5}{53}$$

$$\frac{8.9}{63}$$

$$\frac{2.8}{75}$$

$$\frac{11.8}{62}$$

$$\frac{2.7}{50}$$

$$\frac{5.5}{23}$$

$$\frac{7.9}{-}$$

$$\frac{10.2}{31}$$

$$\frac{11.8}{52}$$

$$\frac{17.1}{78}$$

$$\frac{7.2}{75}$$

$$\frac{5.3}{50}$$

$$\frac{5.0}{31}$$

$$\frac{7.4}{-}$$

$$\frac{8.7}{78}$$

$$\frac{12.3}{44}$$

$$\frac{18.3}{72}$$

$$\frac{5.4}{50}$$

$$\frac{3.7}{23}$$

$$\frac{4.1}{-}$$

$$\frac{6.8}{25}$$

$$\frac{9.1}{45}$$

$$\frac{10.6}{52}$$

Station	+	π	-	Elev.
		954.55 ✓		
135				52.3 ✓
+50				50.8 ✓
136				50.9 ✓
B.M.	1.75	951.73 ✓	4.57	949.98 ✓
+50				48.1 ✓
137				42.9 ✓
+50				38.8 ✓
T.P.	6.42	946.28 ✓	11.87	939.86 ✓
138				39.6 ✓
+50				37.8 ✓
				36.8
139				37.3
+50				37.1 ✓
140				37.5 ✓
+50				39.2 ✓

Lt.

E

Rt.

64

$$\frac{7.8}{50}$$

$$\frac{3.5}{22}$$

$$\frac{2.3}{1}$$

$$\frac{3.5}{41}$$

$$\frac{4.2}{67}$$

$$\frac{10.6}{50}$$

$$\frac{7.4}{24}$$

$$\frac{3.8}{1}$$

$$\frac{2.1}{16}$$

$$\frac{1.6}{36}$$

$$\frac{1.0}{52}$$

$$\frac{2.2}{66}$$

$$\frac{8.1}{50}$$

$$\frac{5.1}{26}$$

$$\frac{3.6}{1}$$

$$\frac{4.0}{16}$$

$$\frac{5.2}{42}$$

$$\frac{9.0}{73}$$

R.R. Spike in 18" oak 50' Rt. Sta. 13544

Oct. 9-1935

$$\frac{4.0}{50}$$

$$\frac{0.6}{32}$$

$$\frac{0.8}{23}$$

$$\frac{3.6}{1}$$

$$\frac{8.8}{31}$$

$$\frac{11.3}{52}$$

$$\frac{4.0}{50}$$

$$\frac{3.7}{32}$$

$$\frac{5.0}{16}$$

$$\frac{8.8}{1}$$

$$\frac{12.0}{15}$$

$$\frac{13.7}{41}$$

$$\frac{15.0}{52}$$

$$\frac{5.1}{50}$$

$$\frac{8.8}{28}$$

$$\frac{12.9}{1}$$

$$\frac{14.7}{20}$$

$$\frac{15.2}{36}$$

$$\frac{16.6}{72}$$

$$\frac{2.2}{50}$$

$$\frac{4.4}{16}$$

$$\frac{6.7}{1}$$

$$\frac{9.1}{21}$$

$$\frac{9.8}{37}$$

$$\frac{11.5}{53}$$

$$\frac{3.1}{50}$$

$$\frac{5.1}{29}$$

$$\frac{8.5}{1}$$

$$\frac{9.8}{16}$$

$$\frac{10.0}{27}$$

$$\frac{13.1}{55}$$

$$\frac{2.5}{50}$$

$$\frac{6.4}{25}$$

$$\frac{9.7}{1}$$

$$\frac{10.0}{17}$$

$$\frac{12.8}{39}$$

$$\frac{13.3}{54}$$

$$\frac{1.2}{50}$$

$$\frac{5.8}{27}$$

$$\frac{9.2}{1}$$

$$\frac{10.0}{17}$$

$$\frac{12.7}{39}$$

$$\frac{13.6}{55}$$

$$\frac{3.7}{50}$$

$$\frac{6.5}{18}$$

$$\frac{8.8}{1}$$

$$\frac{9.8}{20}$$

$$\frac{13.0}{39}$$

$$\frac{13.0}{52}$$

$$\frac{2.3}{50}$$

$$\frac{5.3}{29}$$

$$\frac{7.1}{1}$$

$$\frac{9.1}{21}$$

$$\frac{9.6}{33}$$

$$\frac{12.6}{55}$$

Station + π - Elev.

946.28 ✓

141

39.9 ✓

+50

37.8 ✓

142

37.8 ✓

+50

35.7 ✓

+85

36.2 ✓

143

37.1 ✓

+15

37.5 ✓

+50

39.1 ✓

144

38.0 ✓

T.P.

6.52

943.19 ✓

7.61

938.67 ✓

+50

37.3 ✓

145

37.2 ✓

+50

37.1 ✓

Lt.

L

Rt.

65

$$\frac{2.3}{50}$$

$$\frac{4.9}{28}$$

$$\frac{7.3}{17}$$

$$\frac{8.4}{17}$$

$$\frac{9.7}{40}$$

$$\frac{10.0}{53}$$

$$\frac{1.2}{50}$$

$$\frac{5.3}{28}$$

$$\frac{8.5}{17}$$

$$\frac{10.6}{31}$$

$$\frac{11.0}{55}$$

$$\frac{5.2}{50}$$

$$\frac{6.2}{32}$$

$$\frac{8.5}{17}$$

$$\frac{10.0}{25}$$

$$\frac{10.0}{55}$$

$$\frac{10.0}{50}$$

$$\frac{10.0}{25}$$

$$\frac{10.6}{17}$$

$$\frac{10.1}{40}$$

$$\frac{9.1}{55}$$

$$\frac{9.5}{50}$$

$$\frac{10.1}{17}$$

$$\frac{9.0}{40}$$

$$\frac{10.2}{42}$$

$$\frac{10.2}{44}$$

$$\frac{8.4}{46}$$

$$\frac{7.2}{55}$$

(DIT)

$$\frac{9.3}{50}$$

$$\frac{9.6}{25}$$

$$\frac{9.2}{17}$$

$$\frac{9.4}{8}$$

$$\frac{10.3}{10}$$

$$\frac{10.8}{12}$$

$$\frac{9.0}{14}$$

$$\frac{8.4}{35}$$

$$\frac{7.3}{55}$$

(DIT)

$$\frac{9.5}{50}$$

$$\frac{9.5}{31}$$

$$\frac{11.1}{29}$$

$$\frac{11.1}{27}$$

$$\frac{9.2}{25}$$

$$\frac{8.8}{17}$$

$$\frac{7.1}{33}$$

$$\frac{6.2}{55}$$

(DIT)

$$\frac{9.4}{46}$$

$$\frac{9.0}{25}$$

$$\frac{7.2}{17}$$

$$\frac{5.5}{31}$$

$$\frac{2.1}{55}$$

$$\frac{9.6}{50}$$

$$\frac{9.6}{44}$$

$$\frac{11.3}{42}$$

$$\frac{11.3}{40}$$

$$\frac{9.2}{29}$$

$$\frac{8.3}{17}$$

$$\frac{6.0}{27}$$

$$\frac{4.9}{42}$$

$$\frac{0.1}{56}$$

(DIT)

$$\frac{8.6}{50}$$

$$\frac{8.4}{33}$$

$$\frac{10.0}{31}$$

$$\frac{10.0}{29}$$

$$\frac{7.7}{27}$$

$$\frac{7.9}{17}$$

$$\frac{6.8}{19}$$

$$\frac{4.2}{35}$$

$$\frac{4.0}{50}$$

$$\frac{1.5}{58}$$

(DIT)

$$\frac{8.6}{50}$$

$$\frac{8.3}{20}$$

$$\frac{10.0}{19}$$

$$\frac{10.0}{17}$$

$$\frac{8.2}{16}$$

$$\frac{8.0}{17}$$

$$\frac{7.0}{31}$$

$$\frac{4.5}{57}$$

(DIT)

$$\frac{8.5}{50}$$

$$\frac{8.8}{10}$$

$$\frac{10.3}{8}$$

$$\frac{10.3}{6}$$

$$\frac{8.1}{4}$$

$$\frac{8.1}{17}$$

$$\frac{7.9}{27}$$

$$\frac{7.6}{55}$$

(DIT)

Station	+	π	-	E/ev.
		945.19 ✓		
146				36.4 ✓
147				35.8 ✓
148				36.7 ✓
149				37.7 ✓
150				38.0 ✓
B.M.	11.99	955.62 ✓	456	943.63 ✓
151+00				47.6 ✓
+37				50.4 ✓
+57				48.0 ✓
152				49.0 ✓
+50				53.6 ✓
T.P.	13.69	962.11 ✓	0.20	955.42 ✓
153				61.0 ✓
+38				665.8 ✓

Lt.

L

Rt.

66

$$\begin{array}{r} 86 \\ 50 \end{array}$$

$$\begin{array}{r} 88 \\ 1 \end{array} \quad \begin{array}{r} 102 \\ 2 \end{array} \quad \begin{array}{r} 102 \\ 4 \end{array} \quad \begin{array}{r} 24 \\ 6 \end{array} \quad \begin{array}{r} 85 \\ 32 \end{array} \quad \begin{array}{r} 80 \\ 53 \end{array}$$

(Dit.)

$$\begin{array}{r} 93 \\ 50 \end{array}$$

$$\begin{array}{r} 94 \\ 50 \end{array}$$

(Dit.)

$$\begin{array}{r} 93 \\ 50 \end{array}$$

$$\begin{array}{r} 85 \\ 50 \end{array}$$

$$\begin{array}{r} 85 \\ 50 \end{array}$$

$$\begin{array}{r} 85 \\ 35 \end{array} \quad \begin{array}{r} 94 \\ 37 \end{array} \quad \begin{array}{r} 94 \\ 39 \end{array} \quad \begin{array}{r} 84 \\ 40 \end{array} \quad \begin{array}{r} 83 \\ 50 \end{array}$$

Dit.

$$\begin{array}{r} 75 \\ 50 \end{array}$$

$$\begin{array}{r} 75 \\ 50 \end{array}$$

$$\begin{array}{r} 78 \\ 50 \end{array}$$

$$\begin{array}{r} 62 \\ 50 \end{array}$$

$$\begin{array}{r} 72 \\ 50 \end{array}$$

$$\begin{array}{r} 72 \\ 50 \end{array}$$

Top Large Rock 50 Rt. Sta. 150 + 50

$$\begin{array}{r} 80 \\ 50 \end{array}$$

$$\begin{array}{r} 83 \\ 27 \end{array}$$

$$\begin{array}{r} 80 \\ 50 \end{array}$$

$$\begin{array}{r} 80 \\ 50 \end{array} \quad \begin{array}{r} 88 \\ 55 \end{array}$$

$$\begin{array}{r} 73 \\ 50 \end{array}$$

$$\begin{array}{r} 60 \\ 24 \end{array}$$

$$\begin{array}{r} 52 \\ 50 \end{array}$$

$$\begin{array}{r} 60 \\ 25 \end{array}$$

$$\begin{array}{r} 60 \\ 50 \end{array}$$

$$\begin{array}{r} 66 \\ 55 \end{array}$$

$$\begin{array}{r} 66 \\ 50 \end{array}$$

$$\begin{array}{r} 75 \\ 29 \end{array}$$

$$\begin{array}{r} 76 \\ 50 \end{array}$$

$$\begin{array}{r} 80 \\ 28 \end{array}$$

$$\begin{array}{r} 71 \\ 53 \end{array}$$

$$\begin{array}{r} 26 \\ 50 \end{array}$$

$$\begin{array}{r} 58 \\ 29 \end{array}$$

$$\begin{array}{r} 66 \\ 50 \end{array}$$

$$\begin{array}{r} 73 \\ 25 \end{array}$$

$$\begin{array}{r} 78 \\ 55 \end{array}$$

$$\begin{array}{r} +13.2 \\ 71 \end{array}$$

$$\begin{array}{r} +5.8 \\ 42 \end{array}$$

$$\begin{array}{r} 0.2 \\ 16 \end{array}$$

$$\begin{array}{r} 20 \\ 50 \end{array}$$

$$\begin{array}{r} 38 \\ 28 \end{array}$$

$$\begin{array}{r} 49 \\ 47 \end{array}$$

Contd

$$\begin{array}{r} 50 \\ 27 \end{array}$$

$$\begin{array}{r} 81 \\ 50 \end{array}$$

$$\begin{array}{r} 113 \\ 27 \end{array}$$

$$\begin{array}{r} 137 \\ 47 \end{array}$$

$$\begin{array}{r} 151 \\ 53 \end{array}$$

Contd

$$\begin{array}{r} 38 \\ 50 \end{array}$$

$$\begin{array}{r} 132 \\ 50 \end{array}$$

$$\begin{array}{r} 147 \\ 54 \end{array}$$

Station	+	π	-	$\pm$ lev.
		969.11 ✓		
154				71.6
+50				74.5
T.P.	13.70	982.26 ✓	0.55	968.56 ✓
153				61.0
+38				65.8
154				71.6 ✓
+50				74.5 ✓
155				77.7 ✓
+50				84.0
156				89.9
+50				92.2 ✓
T.P.	12.12	993.63 ✓	0.75	981.51 ✓
154				71.6
+50				74.5

Lt.

E

Rt.

67

$$\begin{array}{r} +2.5 \\ \text{Cont'd} \end{array}$$

$$\begin{array}{r} 76 \quad 8.1 \quad 9.3 \\ \hline 41 \quad 50 \quad 53 \end{array}$$

$$\begin{array}{r} +15.4 \\ \text{Cont'd} \end{array}$$

$$\begin{array}{r} 47 \quad 6.3 \quad 7.5 \\ \hline 35 \quad 50 \quad 52 \end{array}$$

978.3

$$\begin{array}{r} 40 \quad 10.0 \\ \hline 92 \quad 60. \end{array}$$

-11.3

$$\begin{array}{r} +5.5 \quad +3.0 \quad 2.0 \quad 84 \\ \hline 100 \quad 92 \quad 71. \quad 45. \end{array}$$

-16.6

Cont'd.

$$\begin{array}{r} 0.0 \quad 2.5 \quad 19.7 \\ \hline 46 \quad 37. \quad 7 \end{array}$$

$$\begin{array}{r} 0.5 \\ \hline 30 \end{array}$$

7.8

4.6

$$\begin{array}{r} 11.1 \\ \hline 22 \end{array}$$

$$\begin{array}{r} 14.6 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 15.3 \\ \hline 49 \end{array}$$

+1.7

$$\begin{array}{r} 2.8 \\ \hline 13 \end{array}$$

$$\begin{array}{r} 8.8 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 12.4 \\ \hline 46 \end{array}$$

+4.6

$$\begin{array}{r} 3.2 \\ \hline 24 \end{array}$$

$$\begin{array}{r} 7.1 \\ \hline 35 \end{array}$$

$$\begin{array}{r} 8.6 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 11.7 \\ \hline 50 \end{array}$$

+16.0

$$\begin{array}{r} 15.4 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 4.0 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 5.2 \\ \hline 46 \end{array}$$

$$\begin{array}{r} +4.5 \quad 0.5 \quad 4.2 \quad - \\ \hline 100 \quad 82 \quad 70 \quad 46 \end{array} \quad -22.0$$

$$\begin{array}{r} +7.0 \quad 0.0 \\ \hline 100 \quad 70 \end{array} \quad 30 \quad -18.1$$

Sta.	+	T	-	Elev.
		993.63 ✓		
155				77.7
+50				84.0 ✓
156				88.9 ✓
T.P.	4.20	992.22 ✓	0.61	993.02 ✓
+50				92.2 ✓
157				91.2 ✓
+50				86.8 ✓
158				83.4 ✓
T.P.	1.52	986.11 ✓	12.63	984.59 ✓
158				83.6 ✓
+50				79.0 ✓
T.P.	0.15	975.56 ✓	10.70	975.41 ✓
159				70.3 ✓
T.P.	0.15	962.13 ✓	13.58	961.98 ✓
+50				54.5 ✓
T.P.	0.01	948.58 ✓	13.56	948.57 ✓
160				38.8 ✓
F.B.M.	4.19	948.67 ✓	4.10	944.88 ✓
T.P.	1.42	936.87 ✓	13.22	935.45 ✓

Lt.

E

Rt.

68

$$\begin{array}{r} +90 \quad +80 \quad +45 \quad 1.0 \quad 4.6 \\ 120 \quad 100 \quad 70 \quad 51 \quad 38 \\ - 15.9 \\ \hline 0 \end{array}$$

$$\begin{array}{r} +7.2 \quad +7.0 \quad +5.0 \quad +2.3 \quad 1.0 \\ 120 \quad 100 \quad 70 \quad 46 \quad 30 \\ \hline 96 \end{array}$$

$$\begin{array}{r} +1.0 \quad +6.0 \quad +6.0 \quad +5.0 \quad 0.0 \\ 100 \quad 50 \quad 43 \quad 30 \quad 13 \\ \hline 47 \end{array}$$

Oct. 10 1935

Top Stake 156 +50

78.0 70.8

$$\begin{array}{r} 2.0 \quad +1.8 \quad +5.1 \quad +5.0 \quad +2.3 \quad 5.0 \\ 100 \quad 75 \quad 47 \quad 36 \quad 21 \quad \hline \end{array}$$

$$\begin{array}{r} 12.8 \quad 19.2 \quad 20.4 \\ 21 \quad 39 \quad 45 \end{array}$$

100 3.0

$$\begin{array}{r} \alpha.0. \quad +5.8 \quad +7.3 \quad +9.0 \quad +9.0 \quad 1.0 \\ 100 \quad 83 \quad 55 \quad 40 \quad 15 \\ \hline 6.0 \end{array}$$

$$\begin{array}{r} 13.6 \quad 21.0 \quad 22.0 \\ 21 \quad 41 \quad 46 \end{array}$$

$$\begin{array}{r} +1.3 \quad +2.5 \quad +1.7 \quad 2.0 \\ 100 \quad 67 \quad 48 \quad 26 \\ \hline 10.4 \end{array}$$

$$\begin{array}{r} 16.5 \quad 23.2 \\ 19 \quad 45 \end{array}$$

F-40'

$$\begin{array}{r} 0.0 \quad +1.3 \quad +1.3 \quad 0.2 \quad 4.5 \\ 100 \quad 85 \quad 71 \quad 50 \quad 26 \\ \hline -13.4 \end{array}$$

$$\begin{array}{r} 2.5 \quad 9.4 \quad 14.3 \quad 15.4 \\ 23 \quad 42 \quad 45 \end{array}$$

$$\begin{array}{r} +12.1 \quad +12.1 \quad +8.8 \quad +3.1 \quad 2.6 \quad 7.1 \\ 100 \quad 84 \quad 61 \quad 38 \quad 75 \quad \hline \end{array}$$

$$\begin{array}{r} 12.1 \quad 17.1 \quad 17.6 \\ 19 \quad 50 \quad 53 \end{array}$$

$$\begin{array}{r} +8.1 \quad +2.5 \quad +0.5 \quad 2.0 \quad 5.3 \\ 100 \quad 55 \quad 33 \quad 20 \quad \hline \end{array}$$

$$\begin{array}{r} 12.7 \quad 16.6 \quad 17.4 \\ 37 \quad 53 \quad \text{fence 58} \end{array}$$

$$\begin{array}{r} +7.0 \quad +4.4 \quad +2.3 \quad 7.6 \\ 100 \quad 70 \quad 42 \quad \hline \end{array}$$

$$\begin{array}{r} 12.5 \quad 16.1 \\ 21 \quad 51 \end{array}$$

$$\begin{array}{r} +9.1 \quad +7.0 \quad 1.4 \quad 9.8 \\ 100 \quad 50 \quad 22 \quad \hline \end{array}$$

$$\begin{array}{r} 16.0 \quad 14.0 \quad 15.0 \\ 20 \quad 50 \pm F. \quad 72 \end{array}$$

Top Rail Sta. 160

Sta. + π - Elev.

926.87 ✓

160+35

30.8 ✓

160+65

28.5 ✓

161.

27.7 ✓

162

25.6 ✓

163

26.1 ✓

+48

27.6 ✓

+60

30.2 ✓

164

32.3 ✓

B.M.

11.63

946.61 ✓

1.89

934.98 ✓

+45

37.1 ✓

165

41.7 ✓

T.P.

12.41

954.99 ✓

4.03

942.58 ✓

+50

44.9 ✓

166

46.8 ✓

Lt.

Rt.

Rt.

69

$\frac{+13.0}{85}$	$\frac{+5.7}{62}$	$\frac{+2.7}{35}$	$\frac{6.1}{-}$	$\frac{58}{12}$	$\frac{6.7}{20}$	$\frac{7.0}{48}$	$\frac{6.2}{68}$
--------------------	-------------------	-------------------	-----------------	-----------------	------------------	------------------	------------------

$\frac{2.2}{75}$	$\frac{7.2}{50}$	$\frac{7.0}{17}$	$\frac{8.4}{-}$		$\frac{8.4}{47}$	$\frac{8.8}{68}$
------------------	------------------	------------------	-----------------	--	------------------	------------------

$\frac{9.1}{50}$	$\frac{9.6}{27}$	$\frac{9.2}{-}$	$\frac{9.3}{47}$	$\frac{8.8}{65}$
------------------	------------------	-----------------	------------------	------------------

$\frac{11.0}{50}$	$\frac{11.2}{34}$	$\frac{11.3}{-}$	$\frac{11.2}{25}$	$\frac{10.3}{50}$	$\frac{9.0}{66}$
-------------------	-------------------	------------------	-------------------	-------------------	------------------

$\frac{8.6}{50}$	$\frac{8.5}{Rd. 37}$	$\frac{10.6}{30}$	$\frac{10.8}{-}$	$\frac{10.7}{30}$	$\frac{10.8}{51}$	$\frac{10.2}{66}$
------------------	----------------------	-------------------	------------------	-------------------	-------------------	-------------------

$\frac{6.1}{50}$	$\frac{7.3}{23}$	$\frac{7.1}{Rd. 7}$	$\frac{9.3}{-}$	$\frac{10.0}{25}$	$\frac{10.3}{54}$	$\frac{10.0}{66}$
------------------	------------------	---------------------	-----------------	-------------------	-------------------	-------------------

$\frac{4.8}{50}$	$\frac{6.4}{34}$	$\frac{6.9}{17}$	$\frac{6.7}{Rd. 0}$	$\frac{8.7}{12}$	$\frac{10.0}{25}$	$\frac{9.8}{66}$
------------------	------------------	------------------	---------------------	------------------	-------------------	------------------

$\frac{4.0}{50}$	$\frac{0.4}{40}$	$\frac{4.1}{9}$	$\frac{4.6}{-}$	$\frac{4.7}{5-Rd.}$	$\frac{4.2}{24}$	$\frac{6.5}{30}$	$\frac{6.7}{58}$	$\frac{5.5}{72}$
------------------	------------------	-----------------	-----------------	---------------------	------------------	------------------	------------------	------------------

RR Spike in P.R.

20 Rt. Sta.

14 Rt 33

$\frac{6.4}{50}$	$\frac{6.5}{38}$	$\frac{7.8}{15}$	$\frac{9.5}{-}$	$\frac{11.7}{15}$	$\frac{11.7}{30}$	$\frac{11.1}{Rd. 45}$	$\frac{15.5}{55}$	$\frac{15.8}{70}$
------------------	------------------	------------------	-----------------	-------------------	-------------------	-----------------------	-------------------	-------------------

$\frac{4.0}{50}$	$\frac{3.8}{37}$	$\frac{3.3}{7}$	$\frac{4.9}{-}$	$\frac{8.4}{15}$	$\frac{9.0}{31}$	$\frac{12.7}{39}$	$\frac{12.7}{43}$	$\frac{8.2}{62}$	$\frac{7.1}{-Rd. 81}$	$\frac{7.6}{85}$
------------------	------------------	-----------------	-----------------	------------------	------------------	-------------------	-------------------	------------------	-----------------------	------------------

$\frac{9.6}{50}$	$\frac{9.1}{30}$	$\frac{9.3}{8}$	$\frac{10.1}{-}$	$\frac{16.0}{24}$	$\frac{15.1}{30}$
------------------	------------------	-----------------	------------------	-------------------	-------------------

$\frac{9.3}{50}$	$\frac{7.8}{16}$	$\frac{8.2}{-}$	$\frac{8.9}{7}$	$\frac{15.4}{30}$	$\frac{15.4}{36}$
------------------	------------------	-----------------	-----------------	-------------------	-------------------

Sta.	+	π	-	Elev.
		954.99 ✓		
166+75				50.9 ✓
167				49.5 ✓
+57				45.5 ✓
168				39.3 ✓
+50				40.8 ✓
+70				42.8 ✓
168+80				46.1 ✓
169				45.6 ✓
+50				44.0 ✓
170				41.4 ✓
T.P.	1.42	942.79 ✓	13.62	941.37 ✓
170				
+50				38.0 ✓

Lt.

2

Rt.

70

$$\begin{array}{r} 2.0 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 3.0 \\ \hline 28 \end{array}$$

$$4.1$$

$$\begin{array}{r} 7.0 \\ \hline 29 \end{array}$$

$$\begin{array}{r} 10.4 \\ \hline 46 \end{array}$$

$$\begin{array}{r} 13.0 \\ \hline 54 \end{array}$$

$$\begin{array}{r} 4.2 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 4.6 \\ \hline 26 \end{array}$$

$$\begin{array}{r} 5.5 \\ \hline \end{array}$$

$$\begin{array}{r} 8.0 \\ \hline 27 \end{array}$$

$$\begin{array}{r} 10.2 \\ \hline 44 \end{array}$$

$$\begin{array}{r} 11.3 \\ \hline 49 \end{array}$$

$$\begin{array}{r} 10.1 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 9.5 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 9.5 \\ \hline \end{array}$$

$$\begin{array}{r} 13.0 \\ \hline 29 \end{array}$$

$$\begin{array}{r} 14.0 \\ \hline 46 \end{array}$$

$$\begin{array}{r} 15.6 \\ \hline 54 \end{array}$$

$$\begin{array}{r} 13.7 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 15.7 \\ \hline \end{array}$$

$$\begin{array}{r} 17.5 \\ \hline \end{array}$$

56 - Fence.

$$\begin{array}{r} 12.6 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 14.2 \\ \hline \end{array}$$

$$\begin{array}{r} 17.0 \\ \hline 54 \end{array}$$

$$\begin{array}{r} 10.2 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 12.2 \\ \hline \end{array}$$

$$\begin{array}{r} 13.5 \\ \hline 37 \end{array}$$

$$\begin{array}{r} 14.1 \\ \hline 54 \end{array}$$

$$\begin{array}{r} 8.4 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 8.9 \\ \hline \end{array}$$

$$\begin{array}{r} 10.2 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 12.6 \\ \hline 42 \end{array}$$

$$\begin{array}{r} 13.1 \\ \hline 55 \end{array}$$

$$\begin{array}{r} 8.4 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 9.2 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 9.4 \\ \hline \end{array}$$

$$\begin{array}{r} 10.4 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 10.0 \\ \hline 57 \end{array}$$

$$\begin{array}{r} 10.0 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 11.0 \\ \hline \end{array}$$

$$\begin{array}{r} 11.6 \\ \hline 37 \end{array}$$

$$\begin{array}{r} 12.0 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 12.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 13.3 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 13.6 \\ \hline \end{array}$$

$$-1.1$$

$$\begin{array}{r} 2.0 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 3.6 \\ \hline 45 \end{array}$$

$$\begin{array}{r} 5.2 \\ \hline 68 \end{array}$$

$$\begin{array}{r} 3.5 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 4.3 \\ \hline 26 \end{array}$$

$$\begin{array}{r} 4.8 \\ \hline \end{array}$$

$$\begin{array}{r} 7.6 \\ \hline 39 \end{array}$$

$$\begin{array}{r} 9.5 \\ \hline 64 \end{array}$$

$$\begin{array}{r} 12.4 \\ \hline 83 \end{array}$$

Sta.	+	Σ	-	Elev
		942.79 ✓		
170+70				35.6 ✓
171				29.6 ✓
T.P.	6.74	937.27 ✓	12.26	930.53 ✓
+50				25.0 ✓
172				22.9 ✓
+50				24.5 ✓
172+85				23.3 ✓
	2.60	929.82 ✓	10.05	927.22 ✓
173+50				28.2 ✓
174+0				26.6 ✓
+60				24.7 ✓
175				23.2 ✓
176				18.9 ✓
B.M.			5.88	923.94 ✓

Lt.

E

Rt.

71

5.3	6.0	7.2	11.7	13.7	12.0	12.1
<u>50</u>	<u>25</u>	<u>1</u>	<u>35</u>	<u>63</u>	<u>74</u>	<u>82</u>

8.2	10.5	13.2	14.6	14.2	16.0	12.2	12.0
<u>50</u>	<u>28</u>	<u>1</u>	<u>15</u>	<u>48</u>	<u>77</u>	<u>86</u>	<u>93</u>

7.5	11.0	12.3	12.7	13.9	12.4	11.0
<u>50</u>	<u>27</u>	<u>1</u>	<u>18</u>	<u>40</u>	<u>64</u>	<u>86 - Rd.</u>

12.8	13.8	14.4	14.1	12.2	11.5	14
<u>50</u>	<u>20</u>	<u>1</u>	<u>72</u>	<u>58 Rd</u>	<u>71</u>	<u>88</u>

15.2	13.6	12.8	12.0	4.6	3.7	3.5
<u>50</u>	<u>15</u>	<u>1</u>	<u>11</u>	<u>27</u>	<u>29</u>	<u>65</u>

18.0	16.2	14.0	6.5	5.1	5.6	10.0	9.0
<u>50</u>	<u>30</u>	<u>1</u>	<u>11 - Rd</u>	<u>29</u>	<u>41</u>	<u>53</u>	<u>68</u>

13.0	10.8	1.6	1.4	1.4	8.0	8.4	8.4
<u>50</u>	<u>18</u>	<u>0 - Rd</u>	<u>11</u>	<u>22</u>	<u>34</u>	<u>45</u>	<u>50</u>

11.6	12.3	3.5	3.2	3.2	3.3	9.0	9.3
<u>50</u>	<u>22</u>	<u>9 - Rd</u>	<u>4</u>	<u>14</u>	<u>26</u>	<u>50</u>	

12.0	12.4	11.2	5.6	5.3	5.1	5.2	6.3	11.0	11.0	8.4	10.1
<u>50</u>	<u>31</u>	<u>22</u>	<u>13</u>	<u>9</u>	<u>12 Rd</u>	<u>9</u>	<u>16</u>	<u>25</u>	<u>27</u>	<u>30</u>	<u>50</u>

12.6	13.0	13.4	7.5	6.9	6.6	6.8	7.4	11.6	12.0	10.1	11.1
<u>50</u>	<u>31</u>	<u>23</u>	<u>13</u>	<u>8</u>	<u>0.1</u>	<u>10</u>	<u>15</u>	<u>22</u>	<u>29</u>	<u>32</u>	<u>50</u>

14.0	14.6	16.0	16.0	11.3	10.9	11.1	17.6	17.8	16.0	16.8
<u>50</u>	<u>31</u>	<u>29</u>	<u>21</u>	<u>11</u>	<u>11</u>	<u>23</u>	<u>30</u>	<u>34</u>	<u>50</u>	

R.R. in NW Oak 34' Rl. Sta. 174 + 60

Oct. 10 1935

Sta.

t

T

-

Elev.

Additional X-Sections 72

on Right Side

Sta. 27+00 to Sta.

Sta.

+

A

-

Elev.

467 907.63 ✓

90296 ✓

Add X-Sec. on Rt.

27+0

05.1

+30

04.0

+65

01.1

28

897.7

+40

92.1

+75

97.1

29+0

97.0

+50

96.4

30+0

96.3

+70

96.0

+60

94.8

31

91.9

90796
467
907.63

Top W. Rail 100' Rtl. Sta. 32+58

73
Sept. 26-1935

Top T/C Top L.: 16.70
-2.5 ✓ $\begin{array}{r} 43.2 \\ 85 \end{array}$ $\begin{array}{r} 2.2 \\ 100 \end{array}$ $\begin{array}{r} 1.3 \\ 104.9 \end{array}$ $\begin{array}{r} 29.3 \\ 108.9 = 27.4 \end{array}$

-3.6 ✓ $\begin{array}{r} 42.1 \\ 85 \end{array}$ $\begin{array}{r} 2.4 \\ 96 \end{array}$ $\begin{array}{r} 2.0 \\ 100 \end{array}$ $\begin{array}{r} 1.4 \\ 104 \end{array}$ $\begin{array}{r} 1.05 \\ 108 \end{array}$ ✓

✓
-6.5 $\begin{array}{r} 41.1 \\ 86 \end{array}$ $\begin{array}{r} 2.5 \\ 96 \end{array}$ $\begin{array}{r} 2.5 \\ 98 \end{array}$ $\begin{array}{r} 1.6 \\ 103 \end{array}$ $\begin{array}{r} 1.20 \\ 107 \end{array}$

✓
-9.9 $\begin{array}{r} 40.0 \\ 85 \end{array}$ $\begin{array}{r} 2.6 \\ 90 \end{array}$ $\begin{array}{r} 2.6 \\ 97 \end{array}$ $\begin{array}{r} 1.8 \\ 104.7 \end{array}$ $\begin{array}{r} 1.28 \\ 108.7 \end{array}$

✓
-11.5 $\begin{array}{r} 38.8 \\ 85 \end{array}$ $\begin{array}{r} 3.3 \\ 89 \end{array}$ $\begin{array}{r} 3.1 \\ 96 \end{array}$ $\begin{array}{r} 2.1 \\ 99.7 \end{array}$ $\begin{array}{r} 1.65 \\ 102.7 \end{array}$

✓
-10.5 $\begin{array}{r} 37.2 \\ 87 \end{array}$ $\begin{array}{r} 3.3 \\ 95 \end{array}$ $\begin{array}{r} 2.4 \\ 99.3 \end{array}$ $\begin{array}{r} 1.90 \\ 103.3 \end{array}$

-10.6 $\begin{array}{r} 35.5 \\ 94 \end{array}$ $\begin{array}{r} 2.5 \\ 98.2 \end{array}$ $\begin{array}{r} 2.07 \\ 102.2 \end{array}$

-11.2 $\begin{array}{r} 34.7 \\ 64 \end{array}$ $\begin{array}{r} 3.3 \\ 77 \end{array}$ $\begin{array}{r} 4.0 \\ 91 \end{array}$ $\begin{array}{r} 2.9 \\ 97.6 \end{array}$ $\begin{array}{r} 2.07 \\ 101.6 \end{array}$

-11.3 $\begin{array}{r} 32.7 \\ 66 \end{array}$ $\begin{array}{r} 3.3 \\ 73 \end{array}$ $\begin{array}{r} 4.0 \\ 89 \end{array}$ $\begin{array}{r} 3.4 \\ 92 \end{array}$ $\begin{array}{r} 2.07 \\ 101.0 \end{array}$

-11.6 $\begin{array}{r} 31.3 \\ 60 \end{array}$ $\begin{array}{r} 3.4 \\ 69 \end{array}$ $\begin{array}{r} 4.8 \\ 90 \end{array}$ $\begin{array}{r} 3.6 \\ 96.7 \end{array}$ $\begin{array}{r} 3.14 \\ 100.7 \end{array}$

-12.8 $\begin{array}{r} 29.8 \\ 60 \end{array}$ $\begin{array}{r} 3.6 \\ 69 \end{array}$ $\begin{array}{r} 5.0 \\ 80 \end{array}$ $\begin{array}{r} 3.8 \\ 90 \end{array}$ $\begin{array}{r} 3.36 \\ 100.5 \end{array}$

-13.7 $\begin{array}{r} 26.1 \\ 60 \end{array}$ $\begin{array}{r} 3.7 \\ 65 \end{array}$ $\begin{array}{r} 5.3 \\ 73 \end{array}$ $\begin{array}{r} 4.7 \\ 91 \end{array}$ $\begin{array}{r} 3.71 \\ 100.3 \end{array}$

Station	+	Δ	-	Elev.
		907.63 ✓		
31415				96.6
135				97.4
155				97.2
177				90.2
3240				88.2
150				88.1
3340				86.5
340				84.7
35				84.7
36				85.7
T.P.	1.91	903.71 ✓	5.83	901.80 ✓
37				88.3
405				95.6

L

R

					Top Tie	Top Rail
-11.0	17.8	12.7	13.5	5.7	$\frac{43}{96}$	$\frac{3.85}{100.0} \pm Tr.$
	58	67	75	90		

-10.2	53	$\frac{45}{91}$	$\frac{400}{100.0}$
	91	96	

-10.4	57	$\frac{46}{92}$	$\frac{416}{100.0}$
	92	96	

-17.4	104	$\frac{146}{63}$	5.7	4.8	$\frac{431}{100.0}$
	63	75	92	96	

-19.4	79	70	71	115	115	5.8	$\frac{47}{96}$	4.42
	35	50	66	78	81	92	96	100.

-19-5	53	$\frac{462}{76}$	100
	76		

		Top Tie	Top Rail
-21.1	63	5.3	$\frac{4.81}{100}$
	87	96	

-22.9	6.1	5.6	$\frac{5.10}{100}$
	80	96	

-22.9	64	5.9	$\frac{5.45}{100.0}$
	80	96	

-21.9	7.0	6.3	$\frac{5.83}{100.0}$
	78	96	

15.4	41	2.8	$\frac{2.33}{100}$
	82	96	

4.1	5.0	3.7	$\frac{4.60}{100}$
	78	87	96

Station	+	π	-	Elev.
		903.71 ✓		
38				99.8
+45				905.3
39				08.9
+50				11.9
40 +0				14.2 ✓
40 +40				15.8
41 +00				14.4
T.B.M.	2.25	901.81 ✓	4.13	899.56 ✓
+15				13.4
+40				09.3
+65				03.8
+75				02.3
42				91.9
+16				85.9 ¹

2 Rt.

$$\begin{array}{r}
 \text{Top Tie} \quad \text{Top Rail} \\
 -3.9 \quad \frac{33}{85} \quad \frac{42}{88} \quad \frac{32}{96} \quad \frac{2.72}{100} = \text{Tr.}
 \end{array}$$

$$+1.6 \quad \frac{10}{83} \quad \frac{47}{89} \quad \frac{34}{96} \quad \frac{2.95}{100}$$

$$+5.2 \quad \frac{5.1}{90} \quad \frac{3.7}{96} \quad \frac{900.49}{3.22} \quad \frac{100}{100}$$

$$+8.2 \quad \frac{5.2}{90} \quad \frac{3.9}{96} \quad \frac{3.46}{100}$$

$$+10.5 \quad \frac{5.4}{90} \quad \frac{4.1}{96} \quad \frac{900.05}{3.66} \quad \frac{100}{100}$$

$$+12.1 \quad \frac{5.1}{91} \quad \frac{4.3}{96} \quad \frac{3.81}{100}$$

$$+10.7 \quad \frac{5.4}{91} \quad \frac{4.6}{96} \quad \frac{4.5}{100}$$

Top Rail 100' Rt. Sta. 41+0.0

$$+11.6 \quad \frac{3.7}{91} \quad \frac{2.8}{96} \quad \frac{2.40}{100}$$

$$+7.5 \quad \frac{3.9}{89} \quad \frac{3.0}{96} \quad \frac{2.51}{100}$$

$$+2.0 \quad \frac{4.3}{89} \quad \frac{3.2}{96} \quad \frac{2.70}{100}$$

$$+0.5 \quad \frac{4.4}{89} \quad \frac{3.2}{96} \quad \frac{2.74}{100}$$

$$-9.9 \quad \frac{4.4}{82} \quad \frac{3.3}{96} \quad \frac{898.96}{2.85} \quad \frac{100}{100}$$

$$-11.5 \quad \frac{2.88}{100} \quad \text{Tip Rail}$$

Sta.	+	π	-	Elev.
		901.81	✓	
42+33				83.3
+60				84.3
+65				7 80.24
+72				78.1
+88				80.24
43				84.9
+33				87.6
+64				87.4
44				88.1
+37				86.3
+75				87.7
45				86.7
+50				86.3

4.

2

R1.

76

Top Rail

-19.5

2.94

100 - 171K

Topic

-17.5

 $\frac{W.E}{75}$ $\frac{16.1}{90}$ $\frac{16.1}{100}$ $\frac{3.15}{100}$

-21.6

 $\frac{W.E}{65}$ $\frac{15.0}{80}$ $\frac{15.1}{100}$ $\frac{3.13}{100}$

-23.7

 $\frac{W.E}{60}$ $\frac{16.0}{75}$ $\frac{14.7}{80}$ $\frac{14.3}{100}$ $\frac{3.28}{100}$

-21.6

89845

 $\frac{8.7}{100}$ $\frac{3.36}{100}$

-16.9

 $\frac{4.7}{84}$ $\frac{3.9}{96}$ $\frac{3.4}{100}$

-14.2

 $\frac{4.0}{78}$ $\frac{4.0}{96}$ $\frac{3.51}{100}$

-14.2

 $\frac{1.9}{78}$ $\frac{4.6}{87}$ $\frac{4.0}{96}$ $\frac{3.58}{100}$

-13.7

 $\frac{1.6}{82}$ $\frac{4.4}{85}$ $\frac{4.1}{96}$ $\frac{3.59}{100}$

12

-15.5

 $\frac{2.0}{73}$ $\frac{4.3}{87}$ $\frac{4.0}{96}$ $\frac{3.61}{100}$

13

-14.1

 $\frac{3.4}{77}$ $\frac{5.0}{88}$ $\frac{4.15}{96}$ $\frac{3.66}{100}$

-15.1

 $\frac{4.8}{78}$ $\frac{5.1}{88}$ $\frac{4.2}{96}$ $\frac{3.70}{100}$

898.11

-15.5

 $\frac{4.2}{78}$ $\frac{5.3}{87}$ $\frac{4.3}{96}$ $\frac{3.80}{100}$

Sta.	+	π	-	Elev.	
		901.81 ✓			
46				886.5	
+50				86.4	
47				87.5	
+26				88.2	
+52				88.1	
48				86.9	
+50				86.8	
49				88.0	897.87 ✓
	3.98	901.85 ✓	3.94		896.87
+45				90.7	
50				88.5	
+50				89.1	
51				92.7	
+50				95.0	

E

Rt.

Drains. West. Sta 45+45 $\frac{15.0}{59} = \text{outlet of}$ 12" Top Rail

-15.3 $\frac{28}{78}$ $\frac{5.0}{88}$ $\frac{4.3}{96}$ $\frac{3.88}{100} = \text{Trk.}$

-15.4 $\frac{36}{78}$ $\frac{5.0}{88}$ $\frac{4.4}{96}$ $\frac{3.91}{100}$

-14.3 $\frac{35}{72}$ $\frac{4.9}{87}$ $\frac{4.3}{96}$ $\frac{3.95}{100}$

-13.6 $\frac{3.3}{73}$ $\frac{5.0}{88}$ $\frac{4.4}{96}$ $\frac{3.95}{100}$

-13.7 $\frac{3.6}{73}$ $\frac{5.2}{89}$ $\frac{4.4}{96}$ $\frac{3.95}{100}$

-14.9 $\frac{3.4}{72}$ $\frac{4.9}{87}$ $\frac{4.4}{96}$ $\frac{3.99}{100}$

-15.0 $\frac{3.2}{73}$ $\frac{4.7}{88}$ $\frac{4.5}{96}$ $\frac{3.98}{100}$

-13.8 $\frac{2.4}{72}$ $\frac{4.6}{84}$ $\frac{4.4}{96}$ $\frac{3.96}{100}$

-11.2 $\frac{3.1}{73}$ $\frac{4.8}{87}$ $\frac{4.4}{96}$ $\frac{3.98}{100}$

-13.4 $\frac{3.7}{73}$ $\frac{5.0}{88}$ $\frac{4.4}{96}$ $\frac{3.96}{100}$

-12.9 $\frac{4.7}{79}$ $\frac{5.2}{92}$ $\frac{4.4}{96}$ $\frac{3.93}{100}$

-9.2 $\frac{5.3}{83}$ $\frac{4.6}{92}$ $\frac{4.3}{96}$ $\frac{3.87}{100}$

-6.9 $\frac{5.5}{73}$ $\frac{5.1}{91}$ $\frac{4.3}{96}$ $\frac{3.80}{100}$

Sta.	+	π	-	Elev.
		901.85 ✓		895.3
52 to				898.15 898.16 ✓
+45				94.1
53				98.0
+63				905.8
54				07.0
	5.26	903.82 ✓	3.29	898.56 ✓
+50				07.1
55				05.4
+45				03.9
56				01.0
+45				899.8
+75				01.5
57				03.1
+31				04.1

21.	22.	24.	Top Tie	Top Rail
				78
				<u>898.15</u>
+2.6	$\frac{6.8}{6.8}$	$\frac{6.6}{83}$	$\frac{4.2}{96}$	$\frac{3.70}{100}$ 274
+7.8	$\frac{5.9}{71}$	$\frac{6.2}{81}$	$\frac{4.0}{96}$	$\frac{3.58}{100}$
+3.9	$\frac{5.0}{73}$	$\frac{5.5}{82}$	$\frac{3.9}{96}$	$\frac{3.46}{100}$
+5.1	$\frac{5.7}{71}$	$\frac{6.3}{86}$	$\frac{3.7}{96}$	$\frac{3.33}{100}$
+3.3	$\frac{6.0}{71}$	$\frac{5.9}{81}$	$\frac{3.6}{96}$	$\frac{3.29}{100}$
+1.6	$\frac{7.3}{74}$	$\frac{6.3}{86}$	$\frac{5.1}{96}$	$\frac{5.15}{100}$
+0.1	$\frac{8.4}{80}$	$\frac{6.5}{89}$	$\frac{5.5}{96}$	$\frac{5.02}{100}$
-2.8	$\frac{10.0}{73}$	$\frac{10.3}{82}$	$\frac{6.6}{90}$	$\frac{5.4}{96}$ 492
-4.0	$\frac{9.9}{73}$	$\frac{10.1}{82}$	$\frac{6.4}{90}$	$\frac{5.2}{96}$ 478
-2.3	$\frac{8.5}{78}$	$\frac{8.5}{83}$	$\frac{6.4}{89}$	$\frac{5.1}{96}$ 463
-0.7	$\frac{8.7}{72}$	$\frac{8.4}{81}$	$\frac{6.0}{89}$	$\frac{5.0}{96}$ 452
+0.3	$\frac{8.2}{72}$	$\frac{7.7}{84}$	$\frac{6.0}{89}$	$\frac{4.9}{96}$ 439
	$\frac{7.7}{74}$	$\frac{8.0}{85}$	$\frac{5.9}{90}$	$\frac{4.7}{96}$ 425

Sub.	+	π	-	Elev.	
		903.82	✓		
57+64				02.9	
58				97.9	
+30				92.8	
+65				90.5	
59				92.3	
+50				898.8	
+75				01.5	
60+0				01.8	
T.P.	471	905.11	✓	3.42	900.40 ✓
+75				01.2	
+65				95.0	
61+0				91.9	
+50				88.9	

H.

Z

RH.

79

Top Tie Top Rail

$$0.9 \quad \frac{2.3}{74} \quad \frac{7.7}{83} \quad \frac{5.7}{89} \quad \frac{4.6}{96} \quad \frac{4.11}{100} = 4.7K$$

$$5.9 \quad \frac{7.4}{73} \quad \frac{7.3}{81} \quad \frac{5.5}{87} \quad \frac{4.5}{96} \quad \frac{4.00}{100}$$

$$11.0 \quad \frac{6.7}{72} \quad \frac{5.3}{78} \quad \frac{4.3}{96} \quad \frac{3.87}{100}$$

$$13.3 \quad \frac{4.6}{78} \quad \frac{4.2}{96} \quad \frac{3.74}{100}$$

$$11.5 \quad \frac{4.5}{79} \quad \frac{4.2}{96} \quad \frac{3.68}{100}$$

$$5.0 \quad \frac{3.8}{78} \quad \frac{4.00}{96} \quad \frac{3.56}{100}$$

$$2.7 \quad \frac{3.6}{77} \quad \frac{3.9}{96} \quad \frac{3.48}{100}$$

700.40

$$2.0 \quad \frac{3.8}{75} \quad \frac{3.8}{96} \quad \frac{3.42}{100}$$

$$3.9 \quad \frac{3.8}{78} \quad \frac{5.1}{96} \quad \frac{4.57}{100}$$

$$10.1 \quad \frac{3.7}{78} \quad \frac{4.8}{96} \quad \frac{4.46}{100}$$

$$13.2 \quad \frac{4.0}{78} \quad \frac{4.7}{96} \quad \frac{4.23}{100}$$

$$16.2 \quad \frac{5.1}{78} \quad \frac{4.6}{96} \quad \frac{4.10}{100}$$

Sta	+	π	-	Elev.
		905.11	✓	
62				887.5
+35				87.2
63				87.2
+50				90.0
64				91.8
+35				91.9
+80				92.4
T.P.	6.43	909.82	✓	1.72
				903.39 ✓
65				92.1
+50				91.4
66				90.9
+40				88.6
+85				86.1

4.

2.

24.

80

Top Tie Top Rail

17.6

$$\frac{6.8}{76} \quad \frac{5.5}{85}$$

$$\frac{4.4}{96}$$

$$\frac{3.9}{100}$$

$$\frac{3.9}{100} = 27\%$$

17.9

$$\frac{6.6}{76}$$

$$\frac{4.2}{96}$$

$$\frac{3.72}{100}$$

15.9

$$\frac{4.6}{80}$$

$$\frac{3.7}{96}$$

$$\frac{3.26}{100}$$

15.1

$$\frac{4.3}{86}$$

$$\frac{3.3}{96}$$

$$\frac{2.84}{100}$$

13.3

$$\frac{5.7}{52} \quad \frac{6.0}{68}$$

$$\frac{6.3}{85}$$

$$\frac{3.8}{91}$$

$$\frac{2.9}{96}$$

$$\frac{2.47}{100}$$

13.2

$$\frac{+2.5}{34} \quad \frac{+4.3}{60} \quad \frac{+3.1}{76}$$

$$\frac{3.5}{87}$$

$$\frac{2.7}{96}$$

$$\frac{2.15}{100}$$

12.7

$$\frac{+5.9}{43} \quad \frac{+6.9}{52} \quad \frac{+6.4}{72}$$

$$\frac{3.0}{90}$$

$$\frac{2.3}{96}$$

$$\frac{1.87}{100}$$

17.7

$$\frac{+2.7}{57} \quad \frac{+1.7}{71}$$

$$\frac{4.0}{80}$$

$$\frac{7.7}{90}$$

$$\frac{6.9}{96}$$

$$\frac{6.43}{100}$$

14.4

$$\frac{+3.3}{61}$$

$$\frac{+4.3}{70}$$

$$\frac{7.2}{91}$$

$$\frac{6.6}{96}$$

$$\frac{6.06}{100}$$

18.9

$$\frac{8.3}{81}$$

$$\frac{6.7}{87}$$

$$\frac{6.2}{96}$$

$$\frac{5.69}{100}$$

21.2

$$\frac{5.1}{78}$$

$$\frac{5.9}{78}$$

$$\frac{5.8}{96}$$

$$\frac{5.34}{100}$$

23.7

$$\frac{5.4}{96}$$

$$\frac{4.96}{100}$$

Sta. + π - Elev.

909.82 ✓

67 84.6

+25 83.0

68 82.7

+50 84.1

69 87.6

+50 92.5

+80 97.1

70 02.8

T.D. 2.05 914.17 ✓ 270

907.13 }
907.12 } ✓

+46 19.9

+83 28.0

71 27.7

+34 16.1

L

Z

RT.

Top tie

Top Rail

$$25.2 \quad \frac{5.4}{78} \quad \frac{5.4}{96} \quad \frac{4.86}{100} = \text{dark}$$

$$24.8 \quad \frac{5.2}{78} \quad \frac{5.10}{96} \quad \frac{4.65}{100}$$

$$24.9 \quad \frac{7.0}{78} \quad \frac{5.9}{89} \quad \frac{4.7}{96} \quad \frac{4.24}{100}$$

$$25.7 \quad \frac{7.0}{78} \quad \frac{4.4}{96} \quad \frac{3.94}{100}$$

$$22.2 \quad \frac{7.0}{76} \quad \frac{4.0}{96} \quad \frac{3.57}{100}$$

$$17.3 \quad \frac{4.8}{86} \quad \frac{3.6}{96} \quad \frac{3.11}{100}$$

$$12.7 \quad \frac{4.5}{88} \quad \frac{3.3}{96} \quad \frac{2.85}{100}$$

$$7.0 \quad \frac{4.4}{88} \quad \frac{3.1}{96} \quad \frac{2.70}{100} \quad 907.12$$

$$7.7 \quad \frac{5.2}{84} \quad \frac{7.1}{96} \quad \frac{6.65}{100}$$

$$+ 13.8 \quad \frac{7.3}{85} \quad \frac{6.8}{96} \quad \frac{6.34}{100}$$

$$+ 13.5 \quad \frac{6.4}{81} \quad \frac{6.7}{96} \quad \frac{6.20}{100}$$

$$+ 1.9 \quad \frac{6.0}{75} \quad \frac{7.2}{84} \quad \frac{6.4}{87} \quad \frac{6.3}{96} \quad \frac{5.95}{100}$$

Sol.	+	π	-	E/ev.
		914.17 ✓		
71+66				12.4
72+0				09.3
+25				08.6
+52				08.4
B.M.	0.76	914.40 ✓	0.54	913.63 (913.64) ✓
+66				07.9
73				03.9
+50				07.6
74				09.9
+50				11.4
75				13.1
+50				15.8
+83				19.2

Oct 1, 1935
Very Windy.

Lt. E RT 82
Top Tie Top Rail

1.8 5.7 5.7 5.7
67 96 100 = 47.4

4.9 6.3 6.6 6.0 5.52
59 87 96 100

E.R.I.

5.6 6.7 5.9 5.38
90 96 100

5.8 6.3 5.7 5.20
90 96 100

R.R. Spike Top ^{oak} 8" Stump 60' Lt. Sta. 72 to 100

6.5 8.9 5.8 5.32
96 100

10.5 9.0 5.6 5.07
96 100

6.8 8.6 6.1 5.2 4.69
90 96 100

4.5 8.2 6.0 4.9 4.43
89 96 100

3.0 7.8 5.7 4.5 4.01
90 96

74 + 46 = 24" R3 87 On Rt.

1.3 8.3 5.6 4.1 3.63
90 96 100

+1.4 5.0 7.1 7.6 5.1 3.8 3.23
75 83 90 96 100

+4.8 5.0 7.1 4.7 3.4 2.90
82 89 96 100

Sta. + π - E/cv.

91.440 ✓

76 to

19.1

+50

13.8

T.P.

6.29

918.37 ✓

2.32

912.08 ✓

77

15.1

+50

18.0

78

20.0

+50

21.7

79

24.3

+50

26.4

+75

27.0

80

24.7

+35

22.8

81

23.2

8

Rt

83

Top Tie Top Bar

$$+4.7 \quad 50 \quad \begin{array}{r} 6.7 \\ 82 \end{array} \quad \begin{array}{r} 4.6 \\ 90 \end{array} \quad \begin{array}{r} 3.3 \\ 96 \end{array} \quad \begin{array}{r} 2.75 \\ 100 = 400 \end{array}$$

$$0.6 \quad 50 \quad \begin{array}{r} 5.1 \\ 82 \end{array} \quad \begin{array}{r} 3.8 \\ 87 \end{array} \quad \begin{array}{r} 2.8 \\ 96 \end{array} \quad \begin{array}{r} 1.32 \\ 100 \end{array}$$

$$3.4 \quad 52 \quad \begin{array}{r} 4.7 \\ 73 \end{array} \quad \begin{array}{r} 8.8 \\ 81 \end{array} \quad \begin{array}{r} 7.4 \\ 87 \end{array} \quad \begin{array}{r} 6.4 \\ 96 \end{array} \quad \begin{array}{r} 5.88 \\ 100 \end{array}$$

$$0.4 \quad 53 \quad \begin{array}{r} 6.5 \\ 75 \end{array} \quad \begin{array}{r} 10.1 \\ 81 \end{array} \quad \begin{array}{r} 7.5 \\ 87 \end{array} \quad \begin{array}{r} 6.1 \\ 96 \end{array} \quad \begin{array}{r} 5.54 \\ 100 \end{array}$$

$$+1.6 \quad 50 \quad \begin{array}{r} 10.7 \\ 80 \end{array} \quad \begin{array}{r} 7.0 \\ 90 \end{array} \quad \begin{array}{r} 5.7 \\ 96 \end{array} \quad \begin{array}{r} 5.10 \\ 100 \end{array}$$

$$+3.3 \quad 50 \quad \begin{array}{r} 10.6 \\ 82 \end{array} \quad \begin{array}{r} 6.2 \\ 92 \end{array} \quad \begin{array}{r} 5.2 \\ 96 \end{array} \quad \begin{array}{r} 4.73 \\ 100 \end{array}$$

$$+5.9 \quad 52 \quad \begin{array}{r} 6.1 \\ 66 \end{array} \quad \begin{array}{r} 9.0 \\ 80 \end{array} \quad \begin{array}{r} 5.8 \\ 87 \end{array} \quad \begin{array}{r} 4.9 \\ 96 \end{array} \quad \begin{array}{r} 4.35 \\ 100 \end{array}$$

$$+8.0 \quad 69 \quad \begin{array}{r} 7.1 \\ 83 \end{array} \quad \begin{array}{r} 5.4 \\ 88 \end{array} \quad \begin{array}{r} 4.5 \\ 96 \end{array} \quad \begin{array}{r} 4.02 \\ 100 \end{array}$$

$$+8.6 \quad 70 \quad \begin{array}{r} 6.6 \\ 81 \end{array} \quad \begin{array}{r} 4.9 \\ 87 \end{array} \quad \begin{array}{r} 4.3 \\ 96 \end{array} \quad \begin{array}{r} 3.84 \\ 100 \end{array}$$

$$+6.3 \quad 70 \quad \begin{array}{r} 5.0 \\ 79 \end{array} \quad \begin{array}{r} 4.6 \\ 87 \end{array} \quad \begin{array}{r} 4.2 \\ 96 \end{array} \quad \begin{array}{r} 3.72 \\ 100 \end{array}$$

$$+4.4 \quad 70 \quad \begin{array}{r} 3.5 \\ 88 \end{array} \quad \begin{array}{r} 4.0 \\ 96 \end{array} \quad \begin{array}{r} 3.59 \\ 100 \end{array}$$

$$+4.8 \quad 75 \quad \begin{array}{r} 6.8 \\ 80 \end{array} \quad \begin{array}{r} 4.8 \\ 89 \end{array} \quad \begin{array}{r} 3.5 \\ 96 \end{array} \quad \begin{array}{r} 3.10 \\ 100 \end{array}$$

Sta.	+	π	-	Elev.
81+30		91837 ✓		23.0
+70				21.1
82				18.0
T.P.	5.42	921.31 ✓	248	915.89 ✓
+40				14.8
+70				14.8
83				14.3
+23				14.7
+65				18.2
84+0				20.7
+55				25.9
85				25.0
+30				27.4

8

Rt.

84

Top Tie Top Rail

$$+4.6 \quad 76 \quad \begin{array}{r} 7.0 \\ 82 \end{array} \quad \begin{array}{r} 4.4 \\ 89 \end{array} \quad \begin{array}{r} 3.3 \\ 96 \end{array} \quad \begin{array}{r} 2.88 \\ 100 \end{array}$$

$$+2.7 \quad 75 \quad \begin{array}{r} 7.1 \\ 83 \end{array} \quad \begin{array}{r} 4.2 \\ 90 \end{array} \quad \begin{array}{r} 3.1 \\ 96 \end{array} \quad \begin{array}{r} 2.65 \\ 100 \end{array}$$

$$0.4 \quad 78 \quad \begin{array}{r} 6.7 \\ 85 \end{array} \quad \begin{array}{r} 3.6 \\ 91 \end{array} \quad \begin{array}{r} 2.0 \\ 96 \end{array} \quad \begin{array}{r} 915.89 \\ 2.48 \\ 100 \end{array}$$

$$6.5 \quad 82 \quad \begin{array}{r} 6.1 \\ 90 \end{array} \quad \begin{array}{r} 5.6 \\ 96 \end{array} \quad \begin{array}{r} 5.14 \\ 100 \end{array}$$

$$6.5 \quad 83 \quad \begin{array}{r} 6.2 \\ 90 \end{array} \quad \begin{array}{r} 5.5 \\ 96 \end{array} \quad \begin{array}{r} 5.00 \\ 100 \end{array}$$

$$7.0 \quad 83 \quad \begin{array}{r} 6.4 \\ 91 \end{array} \quad \begin{array}{r} 5.3 \\ 96 \end{array} \quad \begin{array}{r} 4.82 \\ 100 \end{array}$$

$$6.6 \quad 82 \quad \begin{array}{r} 6.0 \\ 92 \end{array} \quad \begin{array}{r} 5.1 \\ 96 \end{array} \quad \begin{array}{r} 4.69 \\ 100 \end{array}$$

$$3.1 \quad 81 \quad \begin{array}{r} 5.7 \\ 91 \end{array} \quad \begin{array}{r} 4.8 \\ 96 \end{array} \quad \begin{array}{r} 4.29 \\ 100 \end{array}$$

$$0.6 \quad 80 \quad \begin{array}{r} 5.8 \\ 89 \end{array} \quad \begin{array}{r} 4.6 \\ 96 \end{array} \quad \begin{array}{r} 4.16 \\ 100 \end{array}$$

$$+4.6 \quad 56 \quad \begin{array}{r} 9.3 \\ 73 \end{array} \quad \begin{array}{r} 9.3 \\ 77 \end{array} \quad \begin{array}{r} 4.8 \\ 85 \end{array} \quad \begin{array}{r} 4.4 \\ 96 \end{array} \quad \begin{array}{r} 3.87 \\ 100 \end{array}$$

$$13.1 \quad 52 \quad \begin{array}{r} 8.4 \\ 71 \end{array} \quad \begin{array}{r} 9.5 \\ 78 \end{array} \quad \begin{array}{r} 5.1 \\ 86 \end{array} \quad \begin{array}{r} 3.9 \\ 96 \end{array} \quad \begin{array}{r} 3.59 \\ 100 \end{array}$$

$$+6.1 \quad 50 \quad \begin{array}{r} 9.3 \\ 70 \end{array} \quad \begin{array}{r} 9.6 \\ 77 \end{array} \quad \begin{array}{r} 4.5 \\ 85 \end{array} \quad \begin{array}{r} 3.7 \\ 96 \end{array} \quad \begin{array}{r} 3.38 \\ 100 \end{array}$$

Sta.	+	π	-	Elev.
		921.31 ✓		
85+60				28.5 ✓
86				26.9
+60				25.2 ✓
87				22.9
+45				19.3
88				16.8
T.P.	5.68	925.28 ✓	1.71	919.60 ✓
+75				20.1
89				19.5
+25				19.8
+75				21.4
90				20.1
+50				18.1

2

At.

85

Top Tio Top Bai

+7.2

$$\begin{array}{r} 9.3 \quad 9.2 \quad 4.8 \quad 3.6 \quad 3.20 \\ 48 \quad 67 \quad 76 \quad 87 \quad 96 \quad 100 = 211 \end{array}$$

+5.6

$$\begin{array}{r} 8.6 \quad 9.8 \quad 9.4 \quad 8.2 \quad 4.1 \quad 3.4 \quad 2.97 \\ 48 \quad 56 \quad 66 \quad 78 \quad 86 \quad 92 \quad 96 \quad 100 \end{array}$$

+8.9

$$\begin{array}{r} 8.3 \quad 9.1 \quad 8.6 \quad 4.0 \quad 3.0 \quad 2.60 \\ 50 \quad 57 \quad 69 \quad 81 \quad 91 \quad 96 \quad 100 \end{array}$$

+1.6

$$\begin{array}{r} 7.9 \quad 8.7 \quad 6.8 \quad 6.3 \quad 3.7 \quad 2.8 \quad 2.34 \\ 51 \quad 57 \quad 66 \quad 76 \quad 85 \quad 92 \quad 96 \quad 100 \end{array}$$

2.0

81

$$\begin{array}{r} 3.6 \quad 2.5 \quad 2.07 \\ 91 \quad 96 \quad 100 \end{array}$$

4.5

52

$$\begin{array}{r} 4.2 \quad 5.3 \quad 3.3 \quad 2.1 \quad 1.71 \\ 76 \quad 82 \quad 89 \quad 96 \quad 100 \end{array}$$

5.2

52

$$\begin{array}{r} 7.3 \quad 8.1 \quad 6.6 \quad 5.8 \quad 5.35 \\ 78 \quad 83 \quad 88 \quad 96 \quad 100 \end{array}$$

5.8

52

$$\begin{array}{r} 6.1 \quad 6.3 \quad 8.1 \quad 6.6 \quad 5.7 \quad 5.21 \\ 70 \quad 79 \quad 82 \quad 89 \quad 96 \quad 100 \end{array}$$

5.5

52

$$\begin{array}{r} 6.7 \quad 8.0 \quad 6.1 \quad 5.6 \quad 5.12 \\ 70 \quad 82 \quad 86 \quad 96 \quad 100 \end{array}$$

3.9

52

$$\begin{array}{r} 8.5 \quad 8.2 \quad 6.5 \quad 5.3 \quad 4.85 \\ 65 \quad 83 \quad 89 \quad 96 \quad 100 \end{array}$$

5.2

52

$$\begin{array}{r} 8.8 \quad 6.3 \quad 5.2 \quad 4.72 \\ 80 \quad 88 \quad 96 \quad 100 \end{array}$$

7.2

52

$$\begin{array}{r} 8.7 \quad 6.0 \quad 4.90 \quad 4.40 \\ 80 \quad 90 \quad 96 \quad 100 \end{array}$$

Sta.	T	π	-	Elev.
		925.28		
9140				17.5
732				16.9
465				16.9
92				17.0
+50				18.8
93.				17.7
B.M.	3.95	925.10	4.13	921.15
+50				16.0
94				16.8
+40				17.1
95				20.4
+30				20.6
+73				24.9

Oct 5, 1935

					86
				Top Tie	Top Rail
7.8	52	$\frac{88}{82}$	$\frac{5.8}{91}$	$\frac{4.6}{96}$	$\frac{4.11}{100}$ - 11.1
8.4		$\frac{87}{82}$	$\frac{5.3}{91}$	$\frac{4.4}{96}$	$\frac{3.97}{100}$
8.4		$\frac{84}{80}$	$\frac{5.5}{89}$	$\frac{4.3}{96}$	$\frac{3.86}{100}$
8.3		$\frac{79}{82}$	$\frac{5.4}{89}$	$\frac{4.1}{96}$	$\frac{3.77}{100}$
6.5		$\frac{5.2}{76}$	$\frac{3.9}{84}$	$\frac{4.4}{83}$	$\frac{4.1}{96}$ 3.64 21.58
7.6		$\frac{3.2}{71}$	$\frac{2.8}{83}$	$\frac{5.0}{89}$	$\frac{4.2}{96}$ 3.70 100
9.1		$\frac{6.6}{73}$	$\frac{6.6}{81}$	$\frac{5.1}{70}$	$\frac{4.2}{96}$ 3.79 100
8.3		$\frac{6.5}{70}$	$\frac{6.3}{84}$	$\frac{4.9}{92}$	$\frac{4.4}{96}$ 3.92 100
8.0		$\frac{86}{83}$	$\frac{5.1}{91}$	$\frac{4.2}{96}$	$\frac{3.81}{100}$
4.7		$\frac{84}{69}$	$\frac{8.7}{84}$	$\frac{5.2}{91}$	$\frac{4.4}{96}$ 3.92 21.18
4.5		$\frac{86}{84}$	$\frac{5.4}{90}$	$\frac{4.5}{96}$	$\frac{4.02}{100}$
7.2	52	$\frac{76}{75}$	$\frac{6.1}{89}$	$\frac{4.6}{96}$	$\frac{4.16}{100}$

Sta.	+	π	-	Elev.
		925.10 ✓		
96				25.4
+50				27.1
97				25.5
+50				25.7
98				22.4
+50				15.4
T.P.	3.38	923.17 ✓	5.31	919.79 ✓
+75				12.5
99				12.1
100				11.2 ✓
101				10.8
102				10.6
103				10.7

2

Rt.

87

tie Rail

+0.3 52

3.5	6.1	4.7	4.28
81	87	96	100

+2.0 52

9.0	1.2	6.1	4.9	4.46
75	81	88	96	100

+0.4 52

+2.0	5.6	5.1	4.63
77	89	96	100

+0.6 52

+4.2	5.8	5.3	4.86
75	89	96	100

2.7 52

+2.5	6.1	5.5	5.07
76	89	96	100

9.7 52

8.6	6.7	5.7	5.31
83	88	96	100

10.7 52

8.6	5.0	4.0	3.50
82	89	96	100

11.1 52

10.3	5.2	4.1	3.60
80	90	96	100

12.0 52

11.2	5.9	4.3	3.87
79	89	96	100

12.4 52

11.8	5.9	4.4	3.98
75	88	96	100

12.6 52

13.3	8.0	4.6	4.16
74	84	96	100

12.5 52

12.7	6.2	5.9	4.6
64	77	87	96

Station	+	π	-	Elev.
		923.17 ✓		
104				11.1
T.P.	4.97	924.16 ✓	3.98	919.19 ✓
105				10.9
106				10.0
107				10.5
108				10.7
109				11.4
+30				12.6
+70				17.9
110				20.3
+35				18.4
T.P.	5.97	926.92 ✓	3.21	920.95 ✓
+70				16.7
111				16.8

2

Rt.

88

Top 1/2 Top 2/2

12.1 $\begin{array}{r} 12.1 \\ 52 \end{array}$ $\begin{array}{r} 40 \\ 64 \end{array}$ $\begin{array}{r} 5.3 \\ 77 \end{array}$ $\begin{array}{r} 4.5 \\ 89 \end{array}$ $\begin{array}{r} 4.5 \\ 96 \end{array}$ $\begin{array}{r} 3.98 \\ 100 \end{array}$ $\begin{array}{r} 100.0 \\ 100 \end{array}$

13.3 $\begin{array}{r} 14.1 \\ 54 \end{array}$ $\begin{array}{r} 13.8 \\ 63 \end{array}$ $\begin{array}{r} 5.6 \\ 78 \end{array}$ $\begin{array}{r} 6.6 \\ 90 \end{array}$ $\begin{array}{r} 5.3 \\ 96 \end{array}$ $\begin{array}{r} 4.90 \\ 100 \end{array}$ $\begin{array}{r} 10.26 \\ 100 \end{array}$

14.2 $\begin{array}{r} 13.7 \\ 64 \end{array}$ $\begin{array}{r} 6.8 \\ 77 \end{array}$ $\begin{array}{r} 6.4 \\ 90 \end{array}$ $\begin{array}{r} 5.1 \\ 96 \end{array}$ $\begin{array}{r} 4.74 \\ 100 \end{array}$

13.7 $\begin{array}{r} 12.1 \\ 64 \end{array}$ $\begin{array}{r} 5.5 \\ 78 \end{array}$ $\begin{array}{r} 5.1 \\ 91 \end{array}$ $\begin{array}{r} 5.0 \\ 96 \end{array}$ $\begin{array}{r} 4.47 \\ 100 \end{array}$

13.5 $\begin{array}{r} 16.0 \\ 54 \end{array}$ $\begin{array}{r} 15.0 \\ 66 \end{array}$ $\begin{array}{r} 13.0 \\ 71 \end{array}$ $\begin{array}{r} 4.4 \\ 78 \end{array}$ $\begin{array}{r} 5.6 \\ 90 \end{array}$ $\begin{array}{r} 4.6 \\ 96 \end{array}$ $\begin{array}{r} 4.14 \\ 100 \end{array}$ $\begin{array}{r} 20.0 \\ 100 \end{array}$

12.8 $\begin{array}{r} 13.1 \\ 59 \end{array}$ $\begin{array}{r} 14.2 \\ 61 \end{array}$ $\begin{array}{r} 13.3 \\ 62 \end{array}$ $\begin{array}{r} 12.2 \\ 71 \end{array}$ $\begin{array}{r} 6.1 \\ 82 \end{array}$ $\begin{array}{r} 5.4 \\ 90 \end{array}$ $\begin{array}{r} 4.2 \\ 96 \end{array}$ $\begin{array}{r} 3.72 \\ 100 \end{array}$

109+18 = 24" R2

A. Line Calc

$\begin{array}{r} 13.4 \\ 84 \end{array}$ - cu 10. $\begin{array}{r} 13.3 \\ 118 \end{array}$

11.6

$\begin{array}{r} 2.1 \\ 79 \end{array}$ $\begin{array}{r} 6.5 \\ 85 \end{array}$ $\begin{array}{r} 4.4 \\ 92 \end{array}$ $\begin{array}{r} 4.1 \\ 96 \end{array}$ $\begin{array}{r} 3.63 \\ 100 \end{array}$

6.3

$\begin{array}{r} 6.3 \\ 62 \end{array}$ $\begin{array}{r} 3.7 \\ 68 \end{array}$ $\begin{array}{r} 5.3 \\ 76 \end{array}$ $\begin{array}{r} 5.2 \\ 83 \end{array}$ $\begin{array}{r} 4.0 \\ 96 \end{array}$ $\begin{array}{r} 3.49 \\ 100 \end{array}$

3.9

$\begin{array}{r} 5.8 \\ 68 \end{array}$ $\begin{array}{r} 4.7 \\ 89 \end{array}$ $\begin{array}{r} 3.7 \\ 96 \end{array}$ $\begin{array}{r} 3.36 \\ 100 \end{array}$

5.8

$\begin{array}{r} 6.2 \\ 67 \end{array}$ $\begin{array}{r} 4.7 \\ 88 \end{array}$ $\begin{array}{r} 3.7 \\ 96 \end{array}$ $\begin{array}{r} 3.21 \\ 100 \end{array}$

10.2

$\begin{array}{r} 8.0 \\ 74 \end{array}$ $\begin{array}{r} 6.8 \\ 78 \end{array}$ $\begin{array}{r} 7.3 \\ 90 \end{array}$ $\begin{array}{r} 6.3 \\ 96 \end{array}$ $\begin{array}{r} 5.88 \\ 100 \end{array}$

10.1

$\begin{array}{r} 7.4 \\ 52 \end{array}$ $\begin{array}{r} 6.7 \\ 73 \end{array}$ $\begin{array}{r} 7.3 \\ 79 \end{array}$ $\begin{array}{r} 6.2 \\ 84 \end{array}$ $\begin{array}{r} 6.2 \\ 96 \end{array}$ $\begin{array}{r} 5.72 \\ 100 \end{array}$

Station + A - E/ev.

926.92 ✓

111+34

17.1

+46

20.7

+54

21.2

+84

21.3

+94

21.1

112

18.9

+09

18.9

B.M.

5.55

926.92 ✓

5.55

921.37 ✓

+20

21.7

+70

20.0

113

19.6

+60

19.0

114

19.0

4

RT.

89

Top Tie Top Rail

$$9.8 \quad \overline{52} \quad \begin{array}{r} 6.9 \quad 7.1 \quad 6.1 \quad 5.61 \\ 6.8 \quad 8.9 \quad 9.6 \quad 100 \end{array}$$

$$6.7 \quad \overline{52} \quad \begin{array}{r} 6.5 \quad 7.6 \quad 7.6 \quad 5.9 \quad 6.2 \quad 7.1 \quad 6.0 \quad 5.56 \\ 6.5 \quad 7.2 \quad 7.5 \quad 7.9 \quad 8.4 \quad 8.8 \quad 9.6 \quad 100 \end{array}$$

$$5.7 \quad \overline{52} \quad \begin{array}{r} 5.7 \quad 7.6 \quad 7.5 \quad 5.7 \quad 5.5 \quad 6.8 \quad 6.0 \quad 5.52 \\ 6.6 \quad 7.0 \quad 7.5 \quad 7.9 \quad 8.3 \quad 8.9 \quad 9.6 \quad 100 \end{array}$$

$$5.6 \quad \overline{50} \quad \begin{array}{r} 5.3 \quad 7.2 \quad 7.2 \quad 4.5 \quad 4.0 \quad 6.5 \quad 5.8 \quad 5.40 \\ 6.0 \quad 6.4 \quad 7.1 \quad 7.7 \quad 8.1 \quad 8.7 \quad 9.6 \quad 100 \end{array}$$

$$5.8 \quad \overline{77} \quad \begin{array}{r} 7.0 \quad 5.8 \quad 5.37 \\ 8.7 \quad 9.6 \quad 100 \end{array}$$

$$8.0 \quad \overline{79} \quad \begin{array}{r} 6.6 \quad 5.8 \quad 5.33 \\ 8.7 \quad 9.6 \quad 100 \end{array}$$

$$8.0 \quad \overline{79} \quad \begin{array}{r} 6.8 \quad 5.1 \quad 5.20 \\ 8.7 \quad 9.6 \quad 100 \end{array}$$

2 Co. Rd. "G" Top Pav.

$$5.7 \quad \overline{58} \quad \begin{array}{r} 5.5 \quad 6.8 \quad 6.7 \quad 5.7 \quad 5.26 \\ 6.4 \quad 7.4 \quad 8.8 \quad 9.6 \quad 100 \end{array}$$

$$6.9 \quad \overline{52} \quad \begin{array}{r} 6.7 \quad 5.2 \quad 5.20 \quad 5.03 \\ 6.1 \quad 6.7 \quad 7.3 \text{ - E Pav.} \quad 100 \end{array}$$

$$7.3 \quad \overline{52} \quad \begin{array}{r} 4.6 \quad 5.6 \quad 5.4 \quad 4.91 \\ 7.6 \quad 8.9 \quad 9.6 \quad 100 \end{array}$$

$$7.9 \quad \overline{52} \quad \begin{array}{r} 4.9 \quad 3.7 \quad 7.0 \quad 5.2 \quad 4.73 \\ 6.5 \quad 7.3 \quad 8.8 \quad 9.6 \quad 100 \end{array}$$

$$7.9 \quad \overline{52} \quad \begin{array}{r} 1.8 \quad 3.3 \quad 3.4 \quad 6.1 \quad 5.0 \quad 4.55 \\ 5.6 \quad 5.9 \quad 8.1 \quad 8.7 \quad 9.6 \quad 100 \end{array}$$

Station	+	π	-	Elev.
		926.92 ✓		
114+50				19.4
115				21.5
+50				19.5
T.P.	5.06	927.79 ✓	4.19	19 922.73 ✓
116				17.5
+60				16.3
117				18.7
+30				21.9
+45				21.7
118				15.1
T.P.	5.80	929.99 ✓	3.60	924.19 ✓
+25				12.9
+75				12.0
119				12.9

2 Rt. 90
Top 10. Top Rail
7.5 52 $\frac{25}{59}$ $\frac{29}{82}$ $\frac{6.2}{87}$ $\frac{5.0}{96}$ $\frac{4.45}{100}$

5.4 52 $\frac{24}{55}$ $\frac{27}{81}$ $\frac{59}{88}$ $\frac{48}{96}$ $\frac{4.31}{100}$

7.4 50 $\frac{36}{53}$ $\frac{3.5}{71}$ $\frac{43}{82}$ $\frac{64}{87}$ $\frac{4.7}{96}$ $\frac{4.20}{100}$

10.3 50 $\frac{62}{56}$ $\frac{64}{77}$ $\frac{85}{82}$ $\frac{86}{84}$ $\frac{66}{88}$ $\frac{5.3}{96}$ $\frac{4.87}{100}$

11.5 50 $\frac{75}{59}$ $\frac{79}{74}$ $\frac{10.5}{80}$ $\frac{12.5}{83}$ $\frac{58}{92}$ $\frac{5.1}{96}$ $\frac{4.63}{100}$

9.1 50 $\frac{114}{65}$ $\frac{118}{80}$ $\frac{62}{90}$ $\frac{5.0}{96}$ $\frac{4.49}{100}$

5.9 49 $\frac{108}{60}$ $\frac{116}{79}$ $\frac{62}{89}$ $\frac{4.9}{96}$ $\frac{4.38}{100}$

6.1 50 $\frac{105}{62}$ $\frac{114}{80}$ $\frac{6.0}{91}$ $\frac{4.7}{96}$ $\frac{4.30}{100}$

Oct. 11-1935

Top Rail Havana

17.7 $\frac{126}{61}$ $\frac{13.2}{76}$ $\frac{6.3}{89}$ $\frac{4.5}{96}$ $\frac{4.10}{100}$

17.1 52 $\frac{165}{70}$ $\frac{15.6}{79}$ $\frac{8.5}{89}$ $\frac{6.7}{96}$ $\frac{6.18}{100}$

18.0 52 $\frac{180}{60}$ $\frac{17.2}{75}$ $\frac{7.3}{92}$ $\frac{6.5}{96}$ $\frac{5.98}{100}$

17.1 50 $\frac{174}{53}$ $\frac{16.4}{64}$ $\frac{7.7}{88}$ $\frac{6.2}{96}$ $\frac{5.80}{100}$

Sta.

+

π

-

E/10V.

929.99 ✓

119+32

14.7

+60

14.8

120

13.4

B.M.

917.44

+50

15.4

121

12.0

+25

10.9

122

09.9

+60

13.0

122+87

15.0

123+08

23.0

+70

23.0

T.P.

6.67

934.28 ✓

2.38

927.61 ✓

+61

14.4

Lt.

Z

Rt.

91

Top Tie Top Bg: 1

15.3	61	$\frac{4.9}{79}$	$\frac{6.8}{87}$	$\frac{6.1}{96}$	$\frac{5.61}{100} = 5.61$
------	----	------------------	------------------	------------------	---------------------------

15.2	60	$\frac{4.8}{77}$	$\frac{6.3}{87}$	$\frac{5.9}{96}$	$\frac{5.46}{100}$
------	----	------------------	------------------	------------------	--------------------

16.6	63	$\frac{4.1}{78}$	$\frac{6.0}{87}$	$\frac{5.6}{96}$	$\frac{5.18}{100}$
------	----	------------------	------------------	------------------	--------------------

RR spike 20" oak 50' Bl. H. 120726

14.6	65	$\frac{4.0}{77}$	$\frac{5.9}{87}$	$\frac{5.4}{96}$	$\frac{4.91}{100}$
------	----	------------------	------------------	------------------	--------------------

18.0	63	$\frac{4.0}{78}$	$\frac{5.6}{87}$	$\frac{5.0}{96}$	$\frac{4.52}{100}$
------	----	------------------	------------------	------------------	--------------------

20.1	61	$\frac{4.6}{78}$	$\frac{5.6}{87}$	$\frac{4.8}{96}$	$\frac{4.39}{100}$
------	----	------------------	------------------	------------------	--------------------

21.1	59	$\frac{4.0}{78}$	$\frac{5.6}{87}$	$\frac{4.4}{96}$	$\frac{3.90}{100}$
------	----	------------------	------------------	------------------	--------------------

17.0	60	$\frac{3.4}{78}$	$\frac{4.7}{86}$	$\frac{3.8}{96}$	$\frac{3.34}{100}$
------	----	------------------	------------------	------------------	--------------------

15.0	59	$\frac{3.2}{78}$	$\frac{4.4}{85}$	$\frac{3.6}{96}$	$\frac{3.10}{100}$
------	----	------------------	------------------	------------------	--------------------

7.0	56	$\frac{2.3}{78}$	$\frac{4.1}{87}$	$\frac{3.40}{96}$	$\frac{2.91}{100}$
-----	----	------------------	------------------	-------------------	--------------------

7.0	60	$\frac{2.6}{78}$	$\frac{4.0}{87}$	$\frac{3.3}{96}$	$\frac{2.80}{100}$
-----	----	------------------	------------------	------------------	--------------------

19.9	52	$\frac{15.0}{60}$	$\frac{15.0}{60}$	$\frac{6.1}{78}$	$\frac{7.7}{87}$	$\frac{7.1}{96}$	$\frac{6.67}{100}$
------	----	-------------------	-------------------	------------------	------------------	------------------	--------------------

Sta.	+	π	-	Elev.
		934.28 ✓		
124				12.7
+58				13.6
125				13.0
+50				17.0
126				22.5
+36				23.8
+63	63 36 27			21.8
127				15.6
+40				12.6
128				12.6
+65				13.1
129				15.3

H.

Z

H.

92

Top
T₁₀Top
Rail

21.6	52	$\frac{16.0}{59}$	$\frac{16.0}{61}$	$\frac{7.0}{77}$	$\frac{7.7}{87}$	$\frac{6.7}{96}$	$\frac{6.32}{100}$
------	----	-------------------	-------------------	------------------	------------------	------------------	--------------------

20.7	44	$\frac{19.7}{57}$	$\frac{19.7}{59}$	$\frac{6.1}{79}$	$\frac{7.0}{87}$	$\frac{6.3}{96}$	$\frac{5.77}{100}$
------	----	-------------------	-------------------	------------------	------------------	------------------	--------------------

21.3	50	$\frac{20.6}{60}$	$\frac{4.5}{78}$	$\frac{6.4}{86}$	$\frac{5.8}{96}$	$\frac{28.88}{5.40}$	$\frac{100}{100}$
------	----	-------------------	------------------	------------------	------------------	----------------------	-------------------

17.3	60	$\frac{3.8}{77}$	$\frac{5.9}{87}$	$\frac{5.4}{96}$	$\frac{4.96}{100}$
------	----	------------------	------------------	------------------	--------------------

11.8	60	$\frac{3.4}{77}$	$\frac{5.7}{88}$	$\frac{5.1}{96}$	$\frac{4.65}{100}$
------	----	------------------	------------------	------------------	--------------------

10.5	60	$\frac{3.6}{77}$	$\frac{5.5}{87}$	$\frac{4.8}{96}$	$\frac{4.36}{100}$
------	----	------------------	------------------	------------------	--------------------

12.5	59	$\frac{4.0}{77}$	$\frac{5.3}{87}$	$\frac{4.6}{96}$	$\frac{4.15}{100}$
------	----	------------------	------------------	------------------	--------------------

18.7	60	$\frac{4.3}{78}$	$\frac{5.2}{86}$	$\frac{4.3}{96}$	$\frac{30.41}{3.87}$	$\frac{100}{100}$
------	----	------------------	------------------	------------------	----------------------	-------------------

21.7	57	$\frac{5.8}{77}$	$\frac{4.7}{88}$	$\frac{4.0}{96}$	$\frac{3.63}{100}$
------	----	------------------	------------------	------------------	--------------------

21.7	62	$\frac{5.2}{87}$	$\frac{3.7}{96}$	$\frac{3.28}{100}$
------	----	------------------	------------------	--------------------

21.2	65	$\frac{4.9}{89}$	$\frac{3.2}{96}$	$\frac{2.74}{100}$
------	----	------------------	------------------	--------------------

19.0	70	$\frac{4.3}{89}$	$\frac{2.9}{96}$	$\frac{2.55}{100}$
------	----	------------------	------------------	--------------------

Station	✓	Σ	-	Elev.
		934.28 ✓		
129+60				19.3
130				25.1
	7.58	940.30 ✓	1.56	932.72 ✓
+50				35.9
130+88				43.1
131+14				45.2 ✓
+50				44.8
132				47.8
465				44.5
133				47.1
+50				46.7
134				47.2
+50				50.5

4.

2

24.

Top Tie 93
Top Rail

$$15.0 \quad 74 \quad \begin{array}{r} 4.1 \\ 89 \end{array} \quad \begin{array}{r} 2.5 \\ 96 \end{array} \quad \begin{array}{r} 1.97 \\ 100 \end{array}$$

$$9.2 \quad 76 \quad \begin{array}{r} 3.1 \\ 90 \end{array} \quad \begin{array}{r} 2.0 \\ 96 \end{array} \quad \begin{array}{r} 34.12 \\ 100 \end{array}$$

$$4.4 \quad 52 \quad \begin{array}{r} 102 \\ 76 \end{array} \quad \begin{array}{r} 114 \\ 80 \end{array} \quad \begin{array}{r} 84 \\ 87 \end{array} \quad \begin{array}{r} 7.6 \\ 96 \end{array} \quad \begin{array}{r} 7.08 \\ 100 \end{array}$$

$$+2.8 \quad 52 \quad \begin{array}{r} 4.4 \\ 76 \end{array} \quad \begin{array}{r} 105 \\ 83 \end{array} \quad \begin{array}{r} 83 \\ 88 \end{array} \quad \begin{array}{r} 7.2 \\ 96 \end{array} \quad \begin{array}{r} 6.75 \\ 100 \end{array}$$

$$+4.9 \quad 70 \quad \begin{array}{r} 100 \\ 84 \end{array} \quad \begin{array}{r} 80 \\ 87 \end{array} \quad \begin{array}{r} 7.0 \\ 96 \end{array} \quad \begin{array}{r} 6.52 \\ 100 \end{array}$$

$$+4.5 \quad 68 \quad \begin{array}{r} 9.5 \\ 83 \end{array} \quad \begin{array}{r} 7.5 \\ 88 \end{array} \quad \begin{array}{r} 6.6 \\ 96 \end{array} \quad \begin{array}{r} 6.20 \\ 100 \end{array}$$

$$+7.5 \quad 72 \quad \begin{array}{r} 9.0 \\ 84 \end{array} \quad \begin{array}{r} 7.1 \\ 88 \end{array} \quad \begin{array}{r} 6.2 \\ 96 \end{array} \quad \begin{array}{r} 5.76 \\ 100 \end{array}$$

$$+4.7 \quad 68 \quad \begin{array}{r} 7.5 \\ 82 \end{array} \quad \begin{array}{r} 6.6 \\ 87 \end{array} \quad \begin{array}{r} 5.5 \\ 96 \end{array} \quad \begin{array}{r} 5.08 \\ 100 \end{array}$$

$$+6.8 \quad 63 \quad \begin{array}{r} 5.2 \\ 81 \end{array} \quad \begin{array}{r} 6.1 \\ 89 \end{array} \quad \begin{array}{r} 5.3 \\ 96 \end{array} \quad \begin{array}{r} 35.50 \\ 4.80 \\ 100 \end{array}$$

$$+6.4 \quad 78 \quad \begin{array}{r} 6.2 \\ 85 \end{array} \quad \begin{array}{r} 4.8 \\ 96 \end{array} \quad \begin{array}{r} 4.38 \\ 100 \end{array}$$

$$+6.9 \quad 72 \quad \begin{array}{r} 5.4 \\ 88 \end{array} \quad \begin{array}{r} 4.5 \\ 96 \end{array} \quad \begin{array}{r} 4.00 \\ 100 \end{array}$$

$$+10.7 \quad 52 \quad \begin{array}{r} 3.0 \\ 84 \end{array} \quad \begin{array}{r} 5.4 \\ 88 \end{array} \quad \begin{array}{r} 3.9 \\ 96 \end{array} \quad \begin{array}{r} 3.47 \\ 100 \end{array}$$

Station	+	-	Elev.	
		94030 ✓		
135			52.3	
+50			50.8	
136			50.9	
B.M.				949.98
+50			48.1	
T.P.	5.60	94410 ✓	1.80	93850 ✓
137			42.9	
+50			38.8	
138			39.6	
+50			37.8	
139			36.8	
+50			37.1	
140			37.5	
+50			39.2	

Lt. 2 Rt. 94
 Top Tie Top Rail
 40 34 37.35
 89 96 2.95
 100.0

+12.0 67

89 96 100.0

+10.5 66

3.5 2.9 2.53
 89 96 100

+10.6 73

3.9 2.5 2.13
 88 96 100

R.R Spike 18" Oak 50' H. Sta 135+0.4

(P.C. 136+6.79) 3° Curve.

+7.8 52 2.3 4.2 2.5 2.2 1.80
 83 88 92 96.8 100.8

1.2 52

100 6.0 5.7 38.72
 84 83 97.5 5.38
 101.5

5.3 52

10.5 11.2 11.2 7.5 5.5 5.18
 58 69 85 91 98 102.0

4.5 53

11.8 12.0 6.5 5.3 4.96
 73 84 93 98.3 102.3

6.3 55

11.8 6.5 5.1 4.73
 85 93 98.7 102.7

7.3 54

11.5 4.7 4.8 3.980
 86 96 99 4.20
 103

7.0 55

11.3 4.5 4.3 3.95
 85 96 99.5 103.5

6.6 52

11.7 4.5 3.9 40.54
 84 96 100 3.56
 104.0

4.9 55

11.2 11.0 4.4 3.6 3.20
 68 85 97 100.5 104.5

Sta. + π - Elev.

944.10 ✓

141

39.0

+50

37.8

142

37.8

+50

35.7

212

11.70

954.20 ✓

160

942.50 ✓

+85

36.2 ✓

143

37.1

+15

37.5

+50

39.1

144

38.0

+50

37.3

145

37.2

+50

37.1

Oct. 11, 1935

4

8

104

TOP
TIC

TOP
Rail

95

5.1 53

100 34 3.1 2.75
85 97 104 105.4
105.4
105.4

6.3 55

7.2 7.0 2.7 2.7 2.27
74 87 97 101 105

6.3 55

6.5 5.8 2.5 2.2 1.88
74 88 97 101 105

8.4 55

5.3 3.6 2.4 2.0 1.56
80 92 97 101 105

18.0 55

12.5 14.1 12.4 12.0 11.50
87 92 96 101 105

17.1 55

11.6 13.8 12.4 11.8 11.42
86 94 97 101 105

16.7 55

11.0 13.8 12.0 11.8 11.30
86 93 99 101 105

15.1 55

9.3 12.9 12.3 11.5 11.15
84 94 98 101 105

16.2 56

5.2 12.9 11.8 11.2 10.81
80 95 97 100.5 104.5

16.9 58

3.6 11.7 10.9 10.50
75 93 97.8 103.8

17.0 57

5.8 11.5 10.6 14.07
79 93 99.1 10.18
103

17.1 55

11.1 12.5 11.2 10.5 10.00
84 90 94 98.3 102.3

Sta.	+	π	-	Elev
		954.20 ✓		
146				36.4
T.P.	6.65	951.32 ✓	9.53	944.67 ✓
147				35.8
148				36.7
149				37.7
150				38.0
B.M.	7.69	951.32 ✓	7.69	943.63 ✓
151				47.6
+37				50.4
+57				48.0
T.P.	5.17	951.99 ✓	4.55	946.77 ✓
152				47.0
+50				53.5
153				61.0
+38				65.8

2	101.				96
				Top	Top
				Tic	Rail
17.8	53	14.6	13.5	11.0	102
		63	85	93	97.5
					101.5
					96

15.5	50	16.0	81	7.0	6.65
		81	91	96	100.0

14.6	50	14.2	8.8	6.7	45.00
		79	90	96	6.30
					100.

13.4	50	12.5	7.0	6.3	58.3
		78	90	96	100

13.3	50	11.3	6.7	5.7	46.00
		79	90	96	5.30
					100

Top Large Rock 50 Rt. Sch. 150+50

3.7	55	4.2	5.6	5.2	48.1
		83	89	96	100

0.9	55	7.8	5.9	5.2	4.71
		84	90	96	100

3.3	53	4.3	3.2	5.6	46.4
		72	84	89	96
					100.

2.9	55	4.0	6.1	5.6	46.77
		86	89	96	5.17
					100.

+1.7	47	4.5	6.2	5.5	5.03
		84	90	96	100

+9.9	53	2.7	6.1	5.3	47.07
		84	90	96	4.87
					100

+13.9	54	1.5	6.1	5.3	4.81
		80	89	96	100

Sta.	+	-	Elev.
------	---	---	-------

951.94 ✓

154

71.6

+50

74.5

51.5

155

77.7

+50

84.0

156

88.9

+50

92.2

157

91.2

+50

86.8

T.P

1.09

947.43 ✓

5.60

946.34 ✓

158

83.6

+50

79.0

159

70.3

+50

54.5

160

38.8

295

944.48

Z

At.

97

$$\begin{array}{r} \text{top} \\ \text{Tie Rail} \end{array}$$

$$+ 19.7 \quad 53 \quad \begin{array}{r} +50 \quad 30 \quad 59 \quad 54 \quad 510 \\ 71 \quad 85 \quad 90 \quad 96 \quad 100 \end{array} \quad \text{Link}$$

$$+ 22.6 \quad 52 \quad \begin{array}{r} +63 \quad 20 \quad 55 \quad 51 \quad 460 \\ 66 \quad 80 \quad 89 \quad 96 \quad 100 \end{array} \quad \begin{array}{r} 47.34 \\ 4.60 \\ 101 \end{array}$$

$$+ 25.8 \quad 49 \quad \begin{array}{r} +10.3 \quad 120 \quad 46 \quad 51 \quad 460 \\ 65 \quad 82 \quad 89 \quad 97 \quad 101 \end{array}$$

$$+ 32.1 \quad 46 \quad \begin{array}{r} 58 \quad 52 \quad 470 \\ 90 \quad 97 \quad 101 \end{array}$$

$$+ 37.0 \quad 50 \quad \begin{array}{r} 56 \quad 53 \quad 47.17 \\ 90 \quad 97 \quad 482 \\ 101 \end{array}$$

$$+ 40.3 \quad 46 \quad \begin{array}{r} 59 \quad 55 \quad 500 \\ 91 \quad 97 \quad 101 \end{array}$$

$$\begin{array}{r} 100 \quad 3.0 \\ 100 \end{array}$$

$$\begin{array}{r} 100 \quad 3.0 \\ 246.7 \\ 56.3 \end{array}$$

$$+ 39.3 \quad 46 \quad \begin{array}{r} 6.2 \quad 5.7 \quad 500 \\ 89 \quad 97 \quad 101 \end{array} \quad \begin{array}{r} 46.74 \\ 5.20 \\ 101 \end{array}$$

$$+ 34.9 \quad 45 \quad \begin{array}{r} 65 \quad 59 \quad 535 \\ 89 \quad 97 \quad 101 \end{array}$$

$$+ 36.4 \quad 45 \quad \begin{array}{r} 2.3 \quad 16 \quad 46.34 \\ 89 \quad 97 \quad 109 \\ 101 \end{array}$$

$$+ 31.4 \quad 53 \quad \begin{array}{r} 25 \quad 20 \quad 104 \\ 90 \quad 97 \quad 101 \end{array}$$

$$+ 22.9 \quad 58 \quad \begin{array}{r} 80 \quad 30 \quad 24 \quad 40.55 \\ 75 \quad 84 \quad 97 \quad 158 \\ 101 \end{array}$$

$$+ 7.1 \quad 51 \quad \begin{array}{r} 90 \quad 76 \quad 61 \quad 38 \quad 30 \quad 238 \\ 56 \quad 70 \quad 80 \quad 87 \quad 97 \quad 101 \end{array}$$

$$8.6 \quad 72 \quad \begin{array}{r} 43 \quad 35 \quad 295 \\ 87 \quad 97 \quad 101 \end{array}$$

Top Rail / Sta. 160

Sta. + π - E/OU.

947.43 ✓

160+35

30.8

+65

28.5

161

27.7

162

25.6

163

26.1

T.P.

3.52

946.70 ✓

4.75

943.18 ✓

+48

27.6

+60

30.2

164

32.3

B.M.

935.81

+45

37.1

165

41.7

+50

44.9

166

46.8

2

RT.

98

TAP

Tio-Rail

16.6 68

$$\begin{array}{r} 5.2 \\ 88 \end{array}$$

$$\begin{array}{r} 3.8 \\ 97 \end{array} \quad \begin{array}{r} 3.30 \\ 101 \end{array}$$

18.9 68

$$\begin{array}{r} 5.7 \\ 89 \end{array}$$

$$\begin{array}{r} 4.1 \\ 97 \end{array} \quad \begin{array}{r} 3.58 \\ 101 \end{array}$$

19.7 65

$$\begin{array}{r} 5.6 \\ 89 \end{array}$$

$$\begin{array}{r} 4.4 \\ 97 \end{array} \quad \begin{array}{r} 3.58 \\ 101 \end{array}$$

21.8 66

$$\begin{array}{r} 6.1 \\ 89 \end{array}$$

$$\begin{array}{r} 4.6 \\ 96 \end{array} \quad \begin{array}{r} 4.13 \\ 100 \end{array}$$

21.3 66

$$\begin{array}{r} 5.8 \\ 91 \end{array}$$

$$\begin{array}{r} 4.7 \\ 96 \end{array} \quad \begin{array}{r} 4.30 \\ 100 \end{array}$$

19.1 66

$$\begin{array}{r} 5.4 \\ 91 \end{array}$$

$$\begin{array}{r} 4.0 \\ 96 \end{array} \quad \begin{array}{r} 3.52 \\ 100 \end{array}$$

16.5 66

$$\begin{array}{r} 5.3 \\ 91 \end{array}$$

$$\begin{array}{r} 4.1 \\ 96 \end{array} \quad \begin{array}{r} 3.57 \\ 100 \end{array}$$

14.4 72

$$\begin{array}{r} 5.2 \\ 91 \end{array}$$

$$\begin{array}{r} 4.0 \\ 96 \end{array} \quad \begin{array}{r} 4.32 \\ 100 \end{array}$$

R.R. Spike in R.R. 20' RT. 160. 160+35

9.6 70

$$\begin{array}{r} 6.1 \\ 88 \end{array}$$

$$\begin{array}{r} 3.9 \\ 96 \end{array} \quad \begin{array}{r} 3.44 \\ 100 \end{array}$$

5.0 85

$$\begin{array}{r} 4.8 \\ 92 \end{array}$$

$$\begin{array}{r} 3.9 \\ 96 \end{array} \quad \begin{array}{r} 4.39 \\ 100 \end{array}$$

1.8 30

$$\begin{array}{r} 14.7 \\ 85 \end{array}$$

$$\begin{array}{r} 13.7 \\ 62 \end{array} \quad \begin{array}{r} 3.8 \\ 92 \end{array} \quad \begin{array}{r} 3.8 \\ 96 \end{array} \quad \begin{array}{r} 3.33 \\ 100 \end{array}$$

+ 0.9 36

$$\begin{array}{r} 13.3 \\ 58 \end{array}$$

$$\begin{array}{r} 13.1 \\ 72 \end{array} \quad \begin{array}{r} 4.6 \\ 91 \end{array} \quad \begin{array}{r} 3.8 \\ 96 \end{array} \quad \begin{array}{r} 3.31 \\ 100 \end{array}$$

Sta.	+	-	Elev.
------	---	---	-------

946.70 ✓

166+75

50.9

167

49.5

+57

45.5

168

39.3

+50

40.8

+70

42.8

T.P.

5.25

949.05 ✓

2.90

943.80 ✓

168+80

169

+50

170

+50

See next page

2

at.

99

$$\begin{array}{r} \text{top} \\ \hline \text{TiO} \end{array}$$

$$+4.2 \quad 54 \quad \begin{array}{r} 98 \\ 62 \end{array} \quad \begin{array}{r} 11.2 \\ 75 \end{array} \quad \begin{array}{r} 5.0 \\ 88 \end{array} \quad \begin{array}{r} 3.6 \\ 96 \end{array} \quad \begin{array}{r} 3.20 \\ 100 \end{array}$$

43.58

$$+2.8 \quad 49 \quad \begin{array}{r} 91 \\ 60 \end{array} \quad \begin{array}{r} 11.2 \\ 73 \end{array} \quad \begin{array}{r} 4.1 \\ 88 \end{array} \quad \begin{array}{r} 3.6 \\ 96 \end{array} \quad \begin{array}{r} 3.12 \\ 100 \end{array}$$

$$01.2 \quad 54 \quad \begin{array}{r} 11.7 \\ 69 \end{array} \quad \begin{array}{r} 9.6 \\ 81 \end{array} \quad \begin{array}{r} 4.3 \\ 91 \end{array} \quad \begin{array}{r} 3.5 \\ 96 \end{array} \quad \begin{array}{r} 3.08 \\ 100 \end{array}$$

43.51

$$7.4 \quad 56 \quad \begin{array}{r} 10.6 \\ 59 \end{array} \quad \begin{array}{r} 11.3 \\ 80 \end{array} \quad \begin{array}{r} 4.3 \\ 91 \end{array} \quad \begin{array}{r} 3.5 \\ 96 \end{array} \quad \begin{array}{r} 3.05 \\ 100 \end{array}$$

43.75

$$5.9 \quad 54 \quad \begin{array}{r} 10.5 \\ 80 \end{array} \quad \begin{array}{r} 4.3 \\ 91 \end{array} \quad \begin{array}{r} 3.4 \\ 96 \end{array} \quad \begin{array}{r} 2.75 \\ 100 \end{array}$$

43.80

$$3.9 \quad 54 \quad \begin{array}{r} 7.2 \\ 63 \end{array} \quad \begin{array}{r} 7.6 \\ 83 \end{array} \quad \begin{array}{r} 4.0 \\ 92 \end{array} \quad \begin{array}{r} 3.4 \\ 96 \end{array} \quad \begin{array}{r} 2.70 \\ 100 \end{array}$$

55

57

60

68

83

Sta. + π - Elev.

949.05 ✓

Levels + Sec. along Line

0+00 = 100' Pk. Sta. 1684 70.75

0+50

1+00

1+50

2+00

2+63.4 = Centerville Rd.

T.P.

6.48

954.13 ✓

1.40

957.65 ✓

B.M.

4.21

959.92 ✓

Lt.

L

Rt.

100

Oct 12, 1935

top Tie

$$\begin{array}{r} 63 \\ 39 \end{array} \quad \begin{array}{r} 5.7 \\ 13 \end{array} \quad \begin{array}{r} 6.4 \\ 9 \end{array} \quad \begin{array}{r} 5.7 \\ 4 \end{array} \quad \begin{array}{r} 5.18 \\ \text{top Rail} \end{array}$$

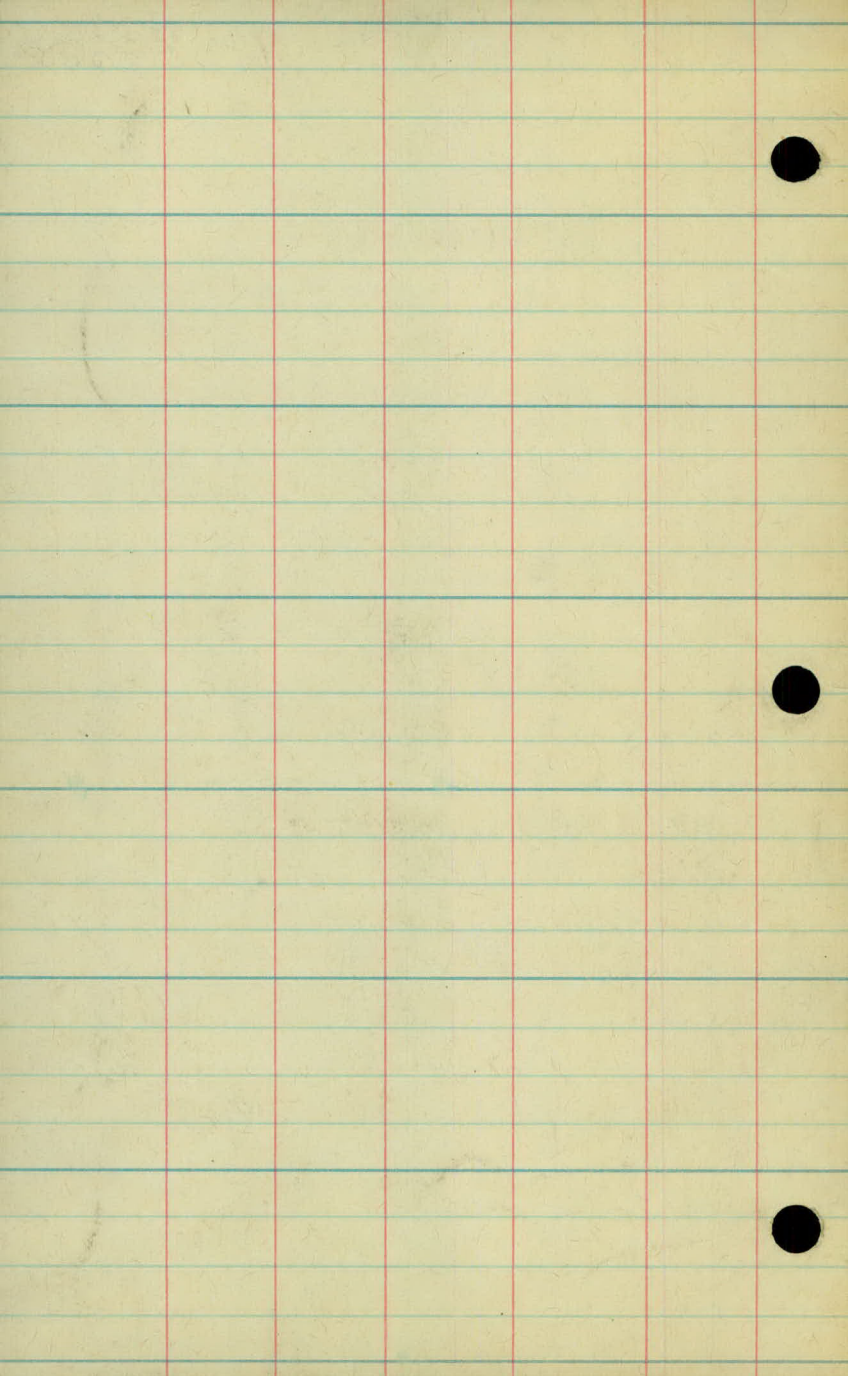
$$\begin{array}{r} 12.0 \\ 39 \end{array} \quad \begin{array}{r} 6.6 \\ 12 \end{array} \quad \begin{array}{r} 5.7 \\ 4 \end{array} \quad \begin{array}{r} 5.22 \\ \hline \end{array}$$

$$\begin{array}{r} 15.1 \\ 41 \end{array} \quad \begin{array}{r} 12.1 \\ 19 \end{array} \quad \begin{array}{r} 6.6 \\ 9 \end{array} \quad \begin{array}{r} 5.80 \\ 4 \end{array} \quad \begin{array}{r} 5.30 \\ \hline \end{array}$$

$$\begin{array}{r} 18.1 \\ 47 \end{array} \quad \begin{array}{r} 18.0 \\ 35 \end{array} \quad \begin{array}{r} 17.2 \\ 25 \end{array} \quad \begin{array}{r} 6.6 \\ 9 \end{array} \quad \begin{array}{r} 5.8 \\ 4 \end{array} \quad \begin{array}{r} 5.30 \\ \hline \end{array}$$

$$\begin{array}{r} 21 \\ 28 \end{array} \quad \begin{array}{r} 5.25 \\ \hline \end{array}$$

Top Mon. Co. Rd "G" & Centerville Rd.



check Levels

+ x - Elev.

Check Levels

B.M.

5.88 929.82 ✓

929.84 ✓

13.49 943.29 ✓

0.02

929.80 ✓

9.64 952.16 ✓

0.77

942.52 ✓

8.37 952.16 ✓

8.37

943.79 ✓

B.M.

10.53 960.44 ✓

2.25

949.91 ✓

3.19 961.58 ✓

2.05

958.39 ✓

11.17 967.92 ✓

4.83

956.75 ✓

B.M.

6.00

961.92 ✓

10/10/35

W.H.O.

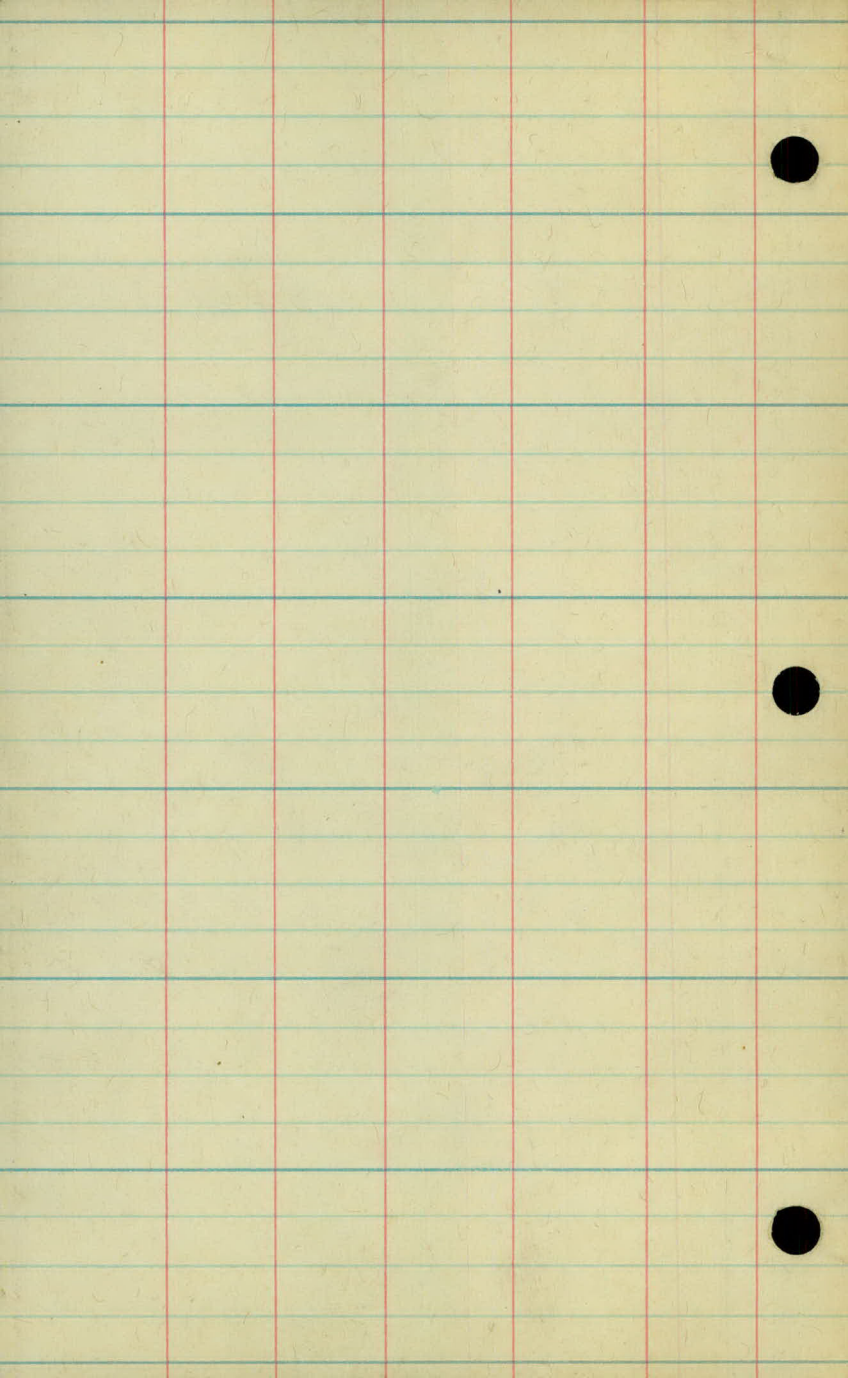
K.A.

L.B.N.

Top Rail ^{\$100} Line Inter Cent. Rd.

" Mon G2 & Centerville

Top & Paw. Co. Rd. 'G' & Centerville



200
153
84.7

Stone Mon

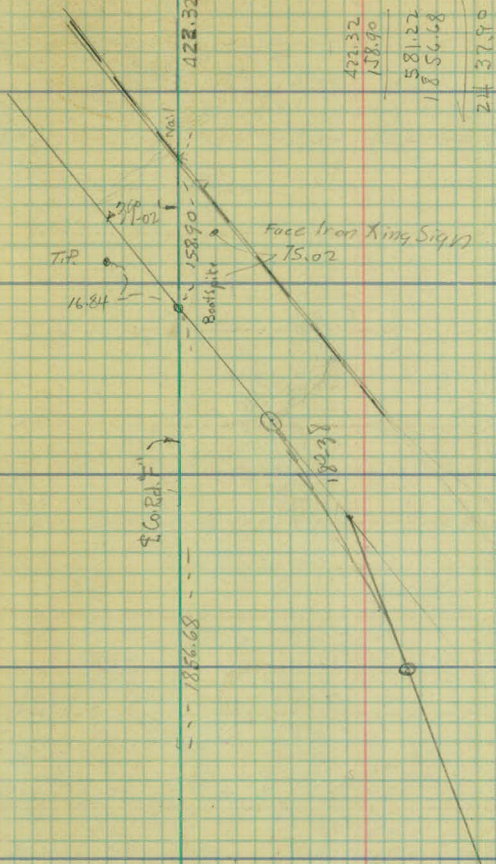
422.32

422.32
158.90

581.22
1856.68

24 37.80

581.22
422.32
158.90

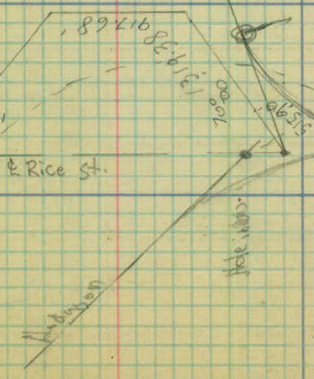


24

25

7 + 114.87

0.00



Hobson

Grassie

