

Book-63-D-6

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

County Rd. "D"

From W. Co. Line To Fairchild

Road Acc't. No. 6

Date Filed 5-6-35

File 6

—Align—

9+21 40

iron on E

1+57 92 P. O. T.

0+00

- 2 -

E

- R -

Hub.

- 5 -

50'

old iron

50'

Hub

12" oak

54.88

Hub

81.00

12" Twin oak.

So. line
Tracks

Mean. Cor.

90°

MONT.

67.88

48.18

P. R. Tel. Pole

Top. Hyp.

40.85

20.00

E 37th Ave N. E.

6' x 16'

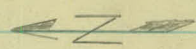
22+42⁰⁵ iron int Co. R. Dst + Fairhilo Ave.

21+01⁵⁰ P.O.T.

12+58⁷⁵ P.O.T.

P.P.
Q

4' left
0



16
10

iron

4435

G. Pole

Hub

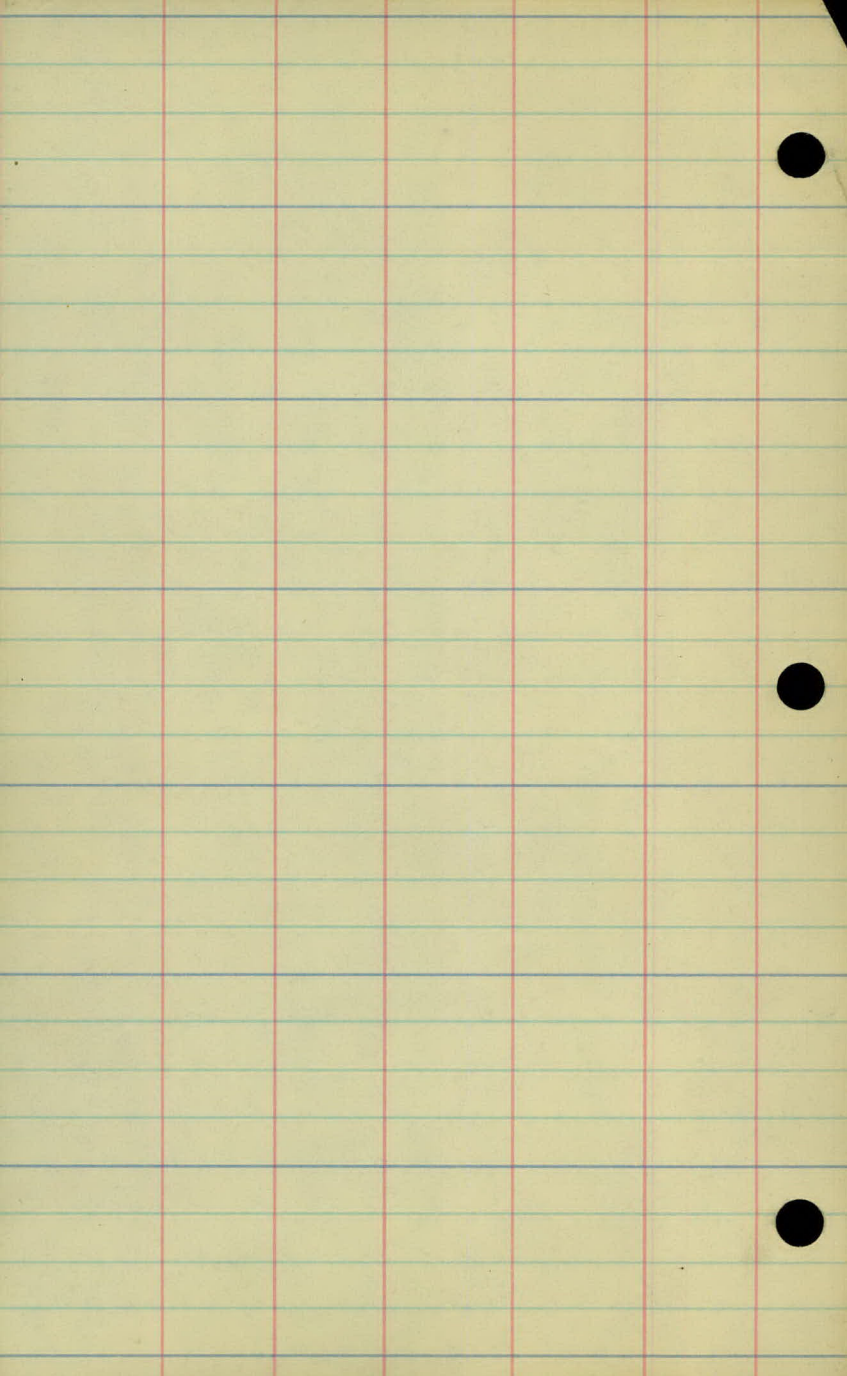
Hub

Hub

Hub

Hub

Top Water Tank.
①



- 1 -

- Topog -

- Co. Rd. - D¹¹

- Extension -

3+0

2+00

1+00

0+50

0+00

+50 Rd 50'L

E Rd 70'L

E Rd 70'L

E Rd 55'L

E Rd 45'L

E Rd 50'L

+50 Rd 50'L

F.L. 21'R.

+50 F 24'R

F. 40'R

+75 FL 52'R.

FL. 53'R

+67 F Cor. 54'R

10 Stumps

21 Stumps

10 Stumps

E So Trk.

Mont.

11025

- 12 Rd 50'

- 40 Rd 10'

0 Main 0-16-17'R

0 Main 0-22-10'R

0-4085 Beg. Carb.

0-42 Hy D.T.

22'R.

6" Carb

Trk.

500'

500'

500'

500'

500'

500'

500'

500'

500'

500'

500'

500'

500'

500'

500'

500'

500'

10+0

9+0

8+0

7+0

6+0

5+0

4+00

+74-2'R 6' Oak

-3-

E Rd 10' R

+48-12" Oak 1' R

E Rd 15' R

+00-180' R. End of tile

+79 Beg 6" tile 2' R

E Rd 10' R

Cultivated

E Rd 8' R

Cultivated

E Rd 8' R

+60 Edge Cult.

+35 F.L. 65' R

+18 F. Cor 22' R

F.L. 22' R E Rd 5' R

+20 Beg Cult.

F.L. 20' R

16+0

15+0

14+0

13+0

12+0

11+0

4-

+20-50' L 6" R

Cultivated

Pasture

+10-12" 37' R
E R 15' R

+80-12" 00' 47' R
+80-12" 00' 439' R
+78-12" 04' 36' R
+51-6" 00' 32' R

+12 C.C.B. 3' x 3' 2' 5' R.
E R 15' R

E R 18' R

+60 Peg Pasture

E R 13' R

Cultivated

E R 12' R

E R 12' R

22+0

21+0

20+0

19+0

18+0

17+0

+14 Edge Rd. R + L.
+10 P.R. 30' R

Fairchild Ave

+28 Rd. Sign E

Rd. 9' R

Cultivated

Rd. 9' R

PASTURE

Rd 10' R

Rd. 12' R

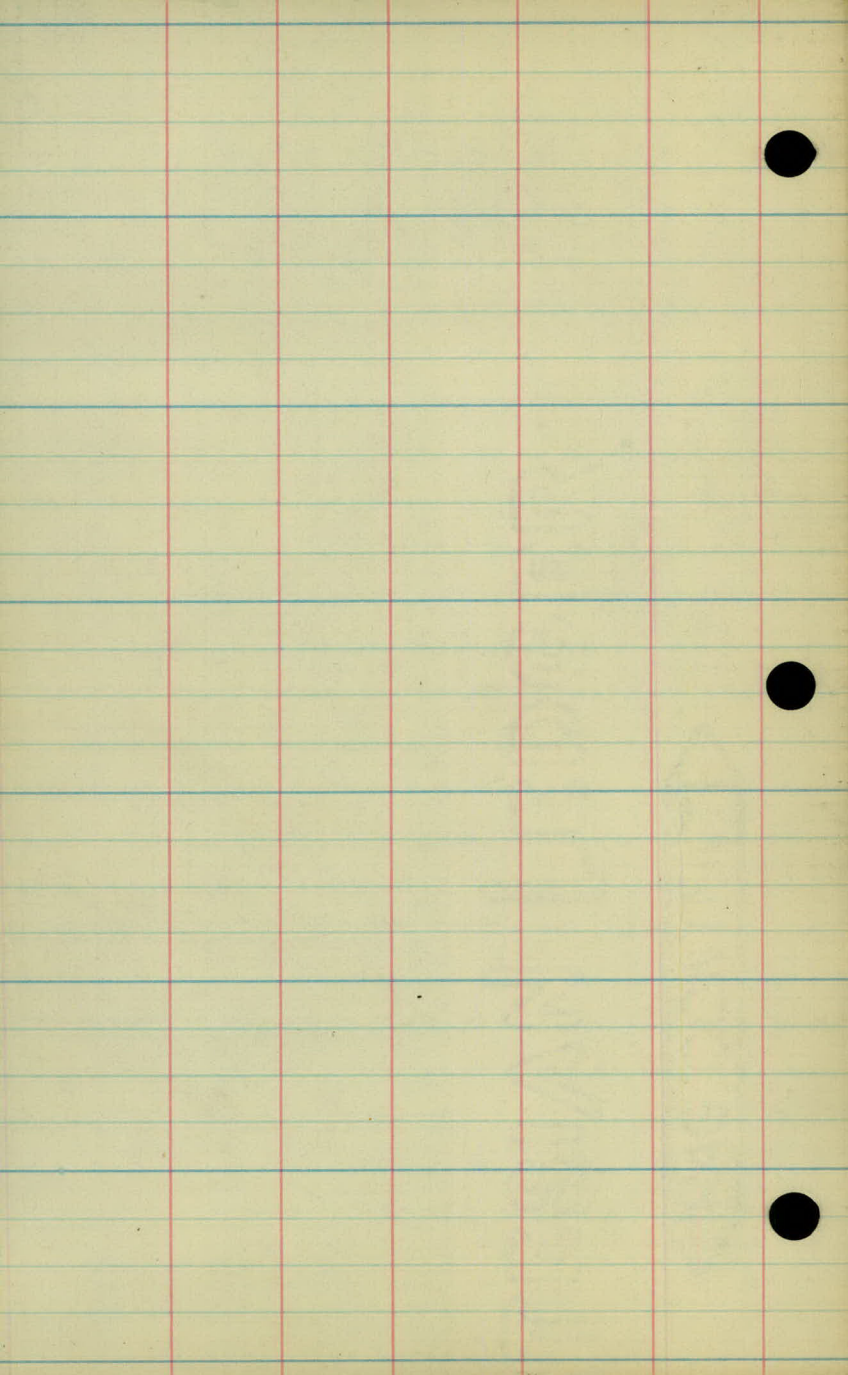
+11 16' L. tile

+20-6" tile 2.5' R
3' x 3' C.C. B

ERD 15' R

+75 6" tile 40' L

ERD. 18' R



- 1 -
4.25 { Skooglund
Steinman
Bell

Bench

Levels

Co. Rd. "D"

EXT.

+

- Check Levels -

	+	H.1	-	EIV	-/-
B.M	0 ⁰¹	944 ²⁵		944 ⁴⁴	

T.P.	8 ⁴⁵ ✓	951 ¹⁰ ✓	1 ⁸⁰ ✓	942 ⁶⁵ ✓	
------	-------------------	---------------------	-------------------	---------------------	--

T.P.	8 ⁴⁵ ✓	958 ⁴⁴ ✓	1 ¹¹ ✓	949 ⁹⁹ ✓	
------	-------------------	---------------------	-------------------	---------------------	--

T.P.	13 ¹³ ✓	971 ⁰⁷ ✓	0 ⁵⁰ ✓	957 ⁹⁴ ✓	
------	--------------------	---------------------	-------------------	---------------------	--

T.P.	4 ⁶⁰ ✓	973 ⁰⁴ ✓	2 ⁶³ ✓	968 ⁴⁴ ✓	
------	-------------------	---------------------	-------------------	---------------------	--

B.M		13 ⁷⁹ ✓		959 ²⁵ ✓	
-----	--	--------------------	--	---------------------	--

T.P.	1 ⁰¹	963 ²¹ ✓	10 ⁸⁴ ✓	962 ²⁰ ✓	
------	-----------------	---------------------	--------------------	---------------------	--

B.M	✓		11 ²⁸ ✓	951 ⁹³ ✓	
-----	---	--	--------------------	---------------------	--

	9 ⁵⁴	961 ⁴⁷ ✓			
T.P.	13 ⁶⁹ ✓	967 ¹⁷ ✓	7 ⁹⁹ ✓	953 ⁴⁸ ✓	

T.P.	5 ¹¹	968 ³⁵ ✓	3 ⁹³ ✓	963 ²⁴ ✓	
------	-----------------	---------------------	-------------------	---------------------	--

B.M			0 ¹⁴	968 ²¹ ✓	
-----	--	--	-----------------	---------------------	--

T.P.	5 ⁵³	962 ⁸³	11 ⁰⁵	957 ³⁰ ✓	
------	-----------------	-------------------	------------------	---------------------	--

B.M			2 ³²	960 ⁵¹ ✓	
-----	--	--	-----------------	---------------------	--

spt in 10" oak N.W. Cor Fairchild Ave
+ Silver Lake Rd.

Top of 3" Angle iron at base of Electric tower
So. Pier. N.E. Cor. Fairchild Ave + Co. Rd. "D".

spt. in 20" Willow 200' R. of Sta. 14+10

spt. in 12" oak 110' Right of Sta. 4+85

Top Hyd. S.W. Cor. Stinson Blvd +
37th Ave. N.E.

+ H.I - EIV

B.M 8.66 96791 ✓ 95925

T.P. 0.17 95915 ✓ 893 ✓ 95898

T.P. 3.57 95869 ✓ 4.03 ✓ 95512

B.M. 6.82 95187 ✓ = 95182

B.M 1.24 96175 ✓ 96051

T.P. 6.98 96841 ✓ 0.32 ✓ 96143

B.M 0.20 96821 ✓ = 96821

B.M. 1.87 97008 ✓ 96821

T.P. 4.06 96254 ✓ 11.60 ✓ 95848

B.M. 10.62 95193 ✓ = 95193

T.P. 8.58 97077 ✓ 0.35 96219

B.M 11.53 95924 ✓ = 95925

Top of 3" Angle iron at base of Electric tower
So. Pier N.E. Cor. Co. Rd. "D" Fairchild Ave

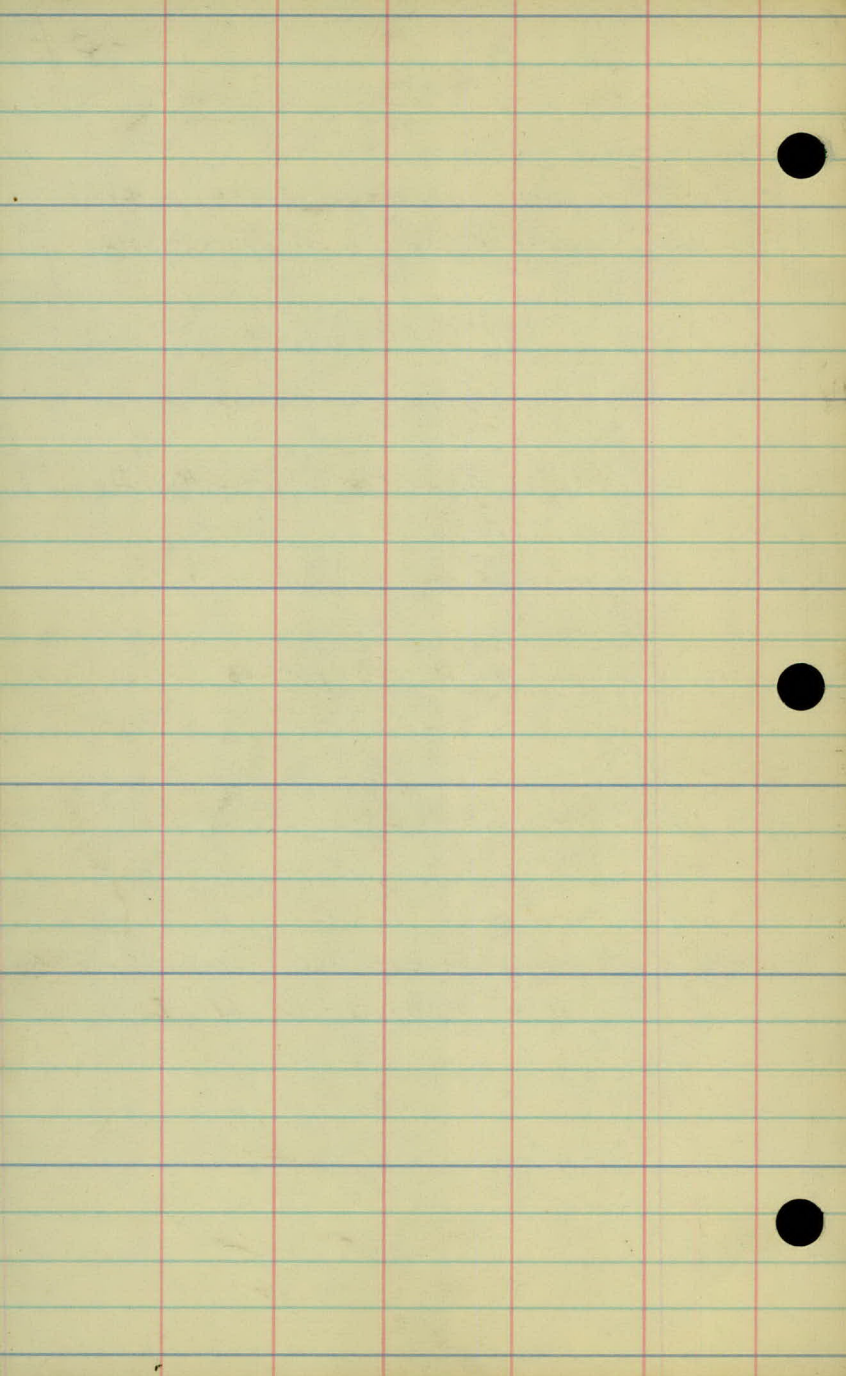
Spk in P. Pole N.E. Cor. Foss Rd. + Co. Rd. "D".

Top Hyp. S.W. Cor. Stinson + 37th Ave. N.E.

Spk. in 12" oak 110' R. of Sta 4+85

Spk. in 20" Willow 200' R. of Stg. 14+10

Top of 3" Angle iron at base of Electric tower
So. Pier N.E. Cor. Fairchild + Co. Rd. "D"



Apr 35

4.25 { Skoog / VV
Steinman
Bell

-1-

-X-

- Section's -

Co. Rd. "D" Ext.

Stinson Blvd to

"D" + Fairchild Ave.

+ H.I - EIV

B.M. 429 964[✓]80 960[✓]51

D+00 E of Stinson Blvd. 58.1[✓]

0+09 58.1[✓]

0+25 61.7[✓]

0+42 63.5[✓]

T.P. 1092 975[✓]45 027 964[✓]53

0+42

0+47 68.0[✓]

0+75 70.4[✓]

1+00 70.7[✓]

1+25 72.4[✓]

Top Hyp. Stinson Blvd + 37th Ave N.E.

$$\frac{57.7}{\frac{71}{50}}$$

$$\frac{68}{25}$$

$$67$$

$$\frac{68}{25}$$

$$\frac{57.8}{\frac{70}{50}}$$

$$\frac{57.4}{\frac{74}{50}}$$

$$\frac{70}{25}$$

$$67$$

$$\frac{67}{25}$$

$$\frac{57.7}{\frac{71}{50}}$$

$$\frac{57.5}{\frac{73}{50}}$$

$$\frac{70}{36}$$

$$\frac{60}{32}$$

$$\frac{51}{17}$$

$$31$$

$$\frac{27}{16}$$

$$\frac{44}{32}$$

$$\frac{56.0}{\frac{88}{50}}$$

$$\frac{57.2}{\frac{76}{50}}$$

$$\frac{75}{38}$$

$$\frac{66}{36}$$

$$\frac{63}{30}$$

$$\frac{36}{15}$$

$$1.3$$

$$(12.0) \frac{104}{5} \frac{70}{7} \frac{80}{15} \frac{135}{34} \frac{56.9}{\frac{186}{50}}$$

$$\frac{125}{6}$$

$$75$$

$$\frac{67}{5}$$

$$\frac{73}{12}$$

$$\frac{110}{26}$$

$$\frac{138}{36}$$

$$\frac{56.9}{\frac{186}{50}}$$

$$\frac{127}{20}$$

$$\frac{96}{15}$$

$$\frac{68}{7}$$

$$51$$

$$\frac{29}{6}$$

$$\frac{65}{19}$$

$$\frac{84}{25}$$

$$\frac{134}{40}$$

$$\frac{58.7}{\frac{168}{50}}$$

$$\frac{115}{17}$$

$$\frac{88}{12}$$

$$\frac{62}{5}$$

$$48$$

$$\frac{42}{6}$$

$$\frac{52}{16}$$

$$\frac{84}{28}$$

$$\frac{118}{38}$$

$$\frac{59.5}{\frac{160}{50}}$$

$$\frac{91}{16}$$

$$\frac{68}{12}$$

$$\frac{40}{5}$$

$$31$$

$$\frac{32}{7}$$

$$\frac{52}{18}$$

$$\frac{98}{33}$$

$$\frac{60.5}{\frac{150}{50}}$$

+ H.1 ✓ -
975⁴⁵

1+50

74.2 ✓

1+75

74.4 ✓

2+00

73.3 ✓

2+15

70.9 ✓

2+40

T.P.

070

✓
967⁴⁶

869

✓
966⁷⁶

66.4 ✓

0+42

0+47

0+75

1+00

1+25

1+50

1+75

2+00

-L-

-R-

-3-

$$\begin{array}{r} 117 \\ 23 \end{array} \quad \begin{array}{r} 72 \\ 16 \end{array} \quad \begin{array}{r} 32 \\ 7 \end{array} \quad 13 \quad \begin{array}{r} 20 \\ 9 \end{array} \quad \begin{array}{r} 55 \\ 23 \end{array} \quad \begin{array}{r} 91 \\ 35 \end{array} \quad \begin{array}{r} 61.5 \\ 140 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 92 \\ 22 \end{array} \quad \begin{array}{r} 56 \\ 16 \end{array} \quad \begin{array}{r} 30 \\ 9 \end{array} \quad 11 \quad \begin{array}{r} 06 \\ 7 \end{array} \quad \begin{array}{r} 16 \\ 16 \end{array} \quad \begin{array}{r} 56 \\ 32 \end{array} \quad \begin{array}{r} 65.4 \\ 101 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 107 \\ 23 \end{array} \quad \begin{array}{r} 78 \\ 17 \end{array} \quad \begin{array}{r} 34 \\ 6 \end{array} \quad 22 \quad \begin{array}{r} 25 \\ 13 \end{array} \quad \begin{array}{r} 43 \\ 35 \end{array} \quad \begin{array}{r} 68.2 \\ 73 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 142 \\ 32 \end{array} \quad \begin{array}{r} 110 \\ 24 \end{array} \quad \begin{array}{r} 83 \\ 16 \end{array} \quad \begin{array}{r} 52 \\ 6 \end{array} \quad 46 \quad \begin{array}{r} 55 \\ 24 \end{array} \quad \begin{array}{r} 69.1 \\ 64 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 126 \\ 32 \end{array} \quad \begin{array}{r} 96 \\ 22 \end{array} \quad \begin{array}{r} 85 \\ 9 \end{array} \quad 91 \quad \begin{array}{r} 105 \\ 15 \end{array} \quad \begin{array}{r} 104 \\ 32 \end{array} \quad \begin{array}{r} 66.5 \\ 90 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 57.2 \\ 103 \\ \hline 50 \end{array} \quad \begin{array}{r} 100 \\ 39 \end{array} \quad \begin{array}{r} 78 \\ 24 \end{array} \quad \begin{array}{r} 47 \\ 6 \end{array} \quad (4.0)$$

$$\begin{array}{r} 56.9 \\ 106 \\ \hline 50 \end{array} \quad \begin{array}{r} 102 \\ 39 \end{array} \quad \begin{array}{r} 90 \\ 31 \end{array} \quad \begin{array}{r} 54 \\ 12 \end{array} \quad (+5)$$

$$\begin{array}{r} 55.1 \\ 124 \\ \hline 50 \end{array} \quad \begin{array}{r} 120 \\ 38 \end{array} \quad \begin{array}{r} 117 \\ 28 \end{array} \quad (+2.9)$$

$$\begin{array}{r} 54.5 \\ 130 \\ \hline 50 \end{array} \quad \begin{array}{r} 123 \\ 34 \end{array} \quad \begin{array}{r} 108 \\ 26 \end{array} \quad (+3.2)$$

$$\begin{array}{r} 54.3 \\ 132 \\ \hline 50 \end{array} \quad \begin{array}{r} 130 \\ 40 \end{array} \quad \begin{array}{r} 117 \\ 28 \end{array} \quad (+4.9)$$

$$\begin{array}{r} 54.4 \\ 131 \\ \hline 50 \end{array} \quad \begin{array}{r} 128 \\ 41 \end{array} \quad \begin{array}{r} 120 \\ 33 \end{array} \quad (+6.7)$$

$$\begin{array}{r} 54.7 \\ 128 \\ \hline 50 \end{array} \quad \begin{array}{r} 128 \\ 42 \end{array} \quad \begin{array}{r} 116 \\ 35 \end{array} \quad (+6.9)$$

$$\begin{array}{r} 54.2 \\ 133 \\ \hline 50 \end{array} \quad \begin{array}{r} 116 \\ 40 \end{array} \quad \begin{array}{r} 61 \\ 30 \end{array} \quad (+5.8)$$

+ H.1 - E1V
967⁴⁶

2+15

2+40

2+75

63.1 ✓

3+00

62.8 ✓

3+25

61.5 ✓

3+50

58.5 ✓

T.P.

3³⁶

970¹² ✓

070

96676 ✓

B.M.

✓

1.91

96821 = 96821 ✓

T.P.

5⁰⁹

961⁸⁸

13³³

95679

4+00

51.8 ✓

4+30

50.4 ✓

+80

51.8 ✓

5+0

51.1 ✓

- L -

- R - - 4 -

55.0

$\frac{125}{50}$

$\frac{110}{41}$

$\frac{85}{37}$

(+3.4)

56.5

$\frac{110}{50}$

(1.1)

60.1

$\frac{74}{50}$

$\frac{32}{34}$

$\frac{17}{24}$

$\frac{12}{17}$

44

$\frac{63}{9}$

$\frac{71}{21}$

$\frac{78}{26}$

$\frac{65}{40}$

62.3

$\frac{52}{50}$

59.5

$\frac{80}{50}$

$\frac{45}{35}$

$\frac{25}{22}$

$\frac{26}{14}$

47

$\frac{67}{10}$

$\frac{85}{24}$

$\frac{85}{35}$

61.5

$\frac{60}{50}$

57.4

$\frac{10}{50}$

$\frac{56}{25}$

$\frac{51}{13}$

60

$\frac{74}{13}$

$\frac{80}{30}$

61.5

$\frac{60}{50}$

55.8

$\frac{117}{50}$

$\frac{93}{26}$

$\frac{86}{14}$

90

$\frac{98}{20}$

$\frac{88}{33}$

61.5

$\frac{60}{50}$

Spk. in 12" oak 110' R. of Sta. 4+85

53.1

$\frac{88}{50}$

$\frac{96}{20}$

101

$\frac{90}{19}$

$\frac{65}{34}$

57.9

$\frac{40}{50}$

51.8

$\frac{101}{50}$

$\frac{111}{26}$

$\frac{118}{10}$

115

$\frac{98}{18}$

$\frac{70}{35}$

57.9

$\frac{40}{50}$

50.2

$\frac{117}{50}$

$\frac{117}{29}$

$\frac{110}{15}$

101

$\frac{97}{8}$

$\frac{71}{28}$

59.5

$\frac{24}{50}$

49.9

$\frac{120}{50}$

$\frac{120}{28}$

108

$\frac{93}{19}$

$\frac{72}{34}$

58.3

$\frac{36}{50}$

961[✓]88

5+50

51.9 ✓

6+0

54.2 ✓

6+50

51.1 ✓

7+0

T.P

878

✓
958⁴⁸

1218

✓
94970

49.2 ✓

7+50

48.4 ✓

8+00

48.6 ✓

+50

48.5 ✓

8+80

E of 6" tile Right.

48.1 ✓

8+90

48.8 ✓

9+0

49.4 ✓

+50

51.5 ✓

+75

52.5 ✓

10+0

54.2 ✓

$$\begin{array}{r} 49.5 \\ \underline{12.4} \\ 50 \end{array} \quad \begin{array}{r} -L- \\ 108 \\ 31 \end{array} \quad \begin{array}{r} 103 \\ 18 \end{array} \quad 10^0 \quad \begin{array}{r} 28 \\ 25 \end{array} \quad \begin{array}{r} 87 \\ 45 \end{array} \quad \begin{array}{r} 54.25 \\ \underline{77} \\ 50 \end{array}$$

$$\begin{array}{r} 49.9 \\ \underline{12.0} \\ 50 \end{array} \quad \begin{array}{r} 102 \\ 33 \end{array} \quad \begin{array}{r} 85 \\ 14 \end{array} \quad 77 \quad \begin{array}{r} 80 \\ 21 \end{array} \quad \begin{array}{r} 52.5 \\ \underline{64} \\ 50 \end{array}$$

$$\begin{array}{r} 50.3 \\ \underline{11.6} \\ 50 \end{array} \quad \begin{array}{r} 104 \\ 24 \end{array} \quad \begin{array}{r} 108 \\ 10 \end{array} \quad 108 \quad \begin{array}{r} 115 \\ 4 \end{array} \quad \begin{array}{r} 105 \\ 24 \end{array} \quad \begin{array}{r} 53.3 \\ \underline{86} \\ 50 \end{array}$$

$$\begin{array}{r} 47.2 \\ \underline{14.7} \\ 50 \end{array} \quad \begin{array}{r} 140 \\ 25 \end{array} \quad 127 \quad \begin{array}{r} 117 \\ 14 \end{array} \quad \begin{array}{r} 110 \\ 29 \end{array} \quad \begin{array}{r} 52.9 \\ \underline{90} \\ 50 \end{array}$$

$$\begin{array}{r} 46.0 \\ \underline{12.5} \\ 50 \end{array} \quad \begin{array}{r} 121 \\ 33 \end{array} \quad \begin{array}{r} 114 \\ 13 \end{array} \quad 101 \quad \begin{array}{r} 91 \\ 3 \end{array} \quad \begin{array}{r} 81 \\ 13 \end{array} \quad \begin{array}{r} 51 \\ 33 \end{array} \quad \begin{array}{r} 57.4 \\ \underline{11} \\ 50 \end{array}$$

$$\begin{array}{r} 45.9 \\ \underline{12.6} \\ 50 \end{array} \quad \begin{array}{r} 121 \\ 33 \end{array} \quad \begin{array}{r} 117 \\ 16 \end{array} \quad 99 \quad \begin{array}{r} 88 \\ 3 \end{array} \quad \begin{array}{r} 80 \\ 14 \end{array} \quad \begin{array}{r} 40 \\ 34 \end{array} \quad \begin{array}{r} 57.0 \\ \underline{15} \\ 50 \end{array}$$

$$\begin{array}{r} 46.2 \\ \underline{12.3} \\ 50 \end{array} \quad \begin{array}{r} 116 \\ 22 \end{array} \quad \begin{array}{r} 106 \\ 12 \end{array} \quad 100 \quad \begin{array}{r} 82 \\ 4 \end{array} \quad \begin{array}{r} 68 \\ 20 \end{array} \quad \begin{array}{r} 42 \\ 31 \end{array} \quad \begin{array}{r} 57.7 \\ \underline{08} \\ 50 \end{array}$$

$$\begin{array}{r} 48.4 \\ \underline{10} \\ 2 \end{array} \quad \begin{array}{r} 53 \\ 180 \end{array} \quad \begin{array}{r} 445 \\ \text{TOP. C.B.} \\ 180 \end{array}$$

$$\begin{array}{r} 46.2 \\ \underline{12.3} \\ 50 \end{array} \quad \begin{array}{r} 120 \\ 28 \end{array} \quad \begin{array}{r} 103 \\ 2 \end{array} \quad 97 \quad \begin{array}{r} 83 \\ 5 \end{array} \quad \begin{array}{r} 72 \\ 19 \end{array} \quad \begin{array}{r} 53 \\ 30 \end{array} \quad \begin{array}{r} 55.1 \\ \underline{34} \\ 50 \end{array}$$

$$\begin{array}{r} 46.2 \\ \underline{12.3} \\ 50 \end{array} \quad \begin{array}{r} 117 \\ 32 \end{array} \quad \begin{array}{r} 104 \\ 3 \end{array} \quad 91 \quad \begin{array}{r} 68 \\ 19 \end{array} \quad \begin{array}{r} 56.1 \\ \underline{24} \\ 50 \end{array}$$

$$\begin{array}{r} 46.5 \\ \underline{12.0} \\ 50 \end{array} \quad \begin{array}{r} 112 \\ 30 \end{array} \quad \begin{array}{r} 84 \\ 4 \end{array} \quad 70$$

$$\begin{array}{r} 46.7 \\ \underline{11.8} \\ 50 \end{array} \quad \begin{array}{r} 91 \\ 22 \end{array} \quad \begin{array}{r} 76 \\ 5 \end{array} \quad 60$$

$$\begin{array}{r} 47.5 \\ \underline{10.8} \\ 50 \end{array} \quad \begin{array}{r} 85 \\ 25 \end{array} \quad \begin{array}{r} 66 \\ 6 \end{array} \quad \begin{array}{r} 49 \\ 3 \end{array} \quad 43$$

+ H.1 - EIV
✓
958⁴⁸

10+50

T, P.

767

✓
962⁴⁵

370

✓
954⁷⁸

51.2 ✓

9+50

9+75

10+0

10+50

11+0

51.5 ✓

11+50

53.1 ✓

12+0

55.5 ✓

+35

58.6 ✓

+60

60.6 ✓

+80

59.8 ✓

13+0

58.3 ✓

13+15

56.8 ✓

-L-

-R- -6-

$$\begin{array}{r} 47.2 \\ 113 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 97 \\ 27 \\ \hline \end{array}$$

$$\begin{array}{r} 88 \\ 8 \\ \hline \end{array}$$

$$73$$

$$\begin{array}{r} 60.2 \\ 23 \\ \hline 50 \end{array}$$

$$(11.0)$$

$$\begin{array}{r} 92 \\ 5 \\ \hline \end{array}$$

$$\begin{array}{r} 82 \\ 15 \\ \hline \end{array}$$

$$\begin{array}{r} 44 \\ 30 \\ \hline \end{array}$$

$$\begin{array}{r} 60.7 \\ 78 \\ \hline 50 \end{array}$$

$$(10.0)$$

$$\begin{array}{r} 72 \\ 5 \\ \hline \end{array}$$

$$\begin{array}{r} 44 \\ 16 \\ \hline \end{array}$$

$$\begin{array}{r} 09 \\ 38 \\ \hline \end{array}$$

$$\begin{array}{r} 61.9 \\ 06 \\ \hline 50 \end{array}$$

$$(8.3)$$

$$\begin{array}{r} 67 \\ 5 \\ \hline \end{array}$$

$$\begin{array}{r} 52 \\ 13 \\ \hline \end{array}$$

$$\begin{array}{r} 03 \\ 42 \\ \hline \end{array}$$

$$\begin{array}{r} 60.1 \\ 24 \\ \hline 50 \end{array}$$

$$(11.3)$$

$$\begin{array}{r} 88 \\ 15 \\ \hline \end{array}$$

$$\begin{array}{r} 46 \\ 36 \\ \hline \end{array}$$

$$\begin{array}{r} 46.9 \\ 156 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 143 \\ 30 \\ \hline \end{array}$$

$$\begin{array}{r} 124 \\ 6 \\ \hline \end{array}$$

$$110$$

$$\begin{array}{r} 95 \\ 8 \\ \hline \end{array}$$

$$\begin{array}{r} 93 \\ 15 \\ \hline \end{array}$$

$$\begin{array}{r} 72 \\ 33 \\ \hline \end{array}$$

$$\begin{array}{r} 57.7 \\ 48 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 47.5 \\ 150 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 130 \\ 27 \\ \hline \end{array}$$

$$\begin{array}{r} 110 \\ 5 \\ \hline \end{array}$$

$$94$$

$$\begin{array}{r} 80 \\ 7 \\ \hline \end{array}$$

$$\begin{array}{r} 75 \\ 15 \\ \hline \end{array}$$

$$\begin{array}{r} 56 \\ 36 \\ \hline \end{array}$$

$$\begin{array}{r} 58.0 \\ 45 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 48.5 \\ 140 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 118 \\ 28 \\ \hline \end{array}$$

$$\begin{array}{r} 82 \\ 3 \\ \hline \end{array}$$

$$70$$

$$\begin{array}{r} 48 \\ 6 \\ \hline \end{array}$$

$$\begin{array}{r} 41 \\ 15 \\ \hline \end{array}$$

$$\begin{array}{r} 28 \\ 31 \\ \hline \end{array}$$

$$\begin{array}{r} 61.5 \\ 10 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 50.1 \\ 124 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 111 \\ 39 \\ \hline \end{array}$$

$$\begin{array}{r} 60 \\ 14 \\ \hline \end{array}$$

$$39$$

$$\begin{array}{r} 29 \\ 5 \\ \hline \end{array}$$

$$\begin{array}{r} 17 \\ 25 \\ \hline \end{array}$$

$$\begin{array}{r} 61.2 \\ 13 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 52.4 \\ 101 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 87 \\ 39 \\ \hline \end{array}$$

$$\begin{array}{r} 34 \\ 13 \\ \hline \end{array}$$

$$19$$

$$\begin{array}{r} 05 \\ 7 \\ \hline \end{array}$$

$$\begin{array}{r} 13 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 20 \\ 27 \\ \hline \end{array}$$

$$\begin{array}{r} 58.1 \\ 34 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 55.2 \\ 73 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 35 \\ 20 \\ \hline \end{array}$$

$$27$$

$$\begin{array}{r} 25 \\ 7 \\ \hline \end{array}$$

$$\begin{array}{r} 35 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 45 \\ 30 \\ \hline \end{array}$$

$$\begin{array}{r} 56.2 \\ 63 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 57.4 \\ 51 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 31 \\ 24 \\ \hline \end{array}$$

$$\begin{array}{r} 92 \\ 6 \\ \hline \end{array}$$

$$42$$

$$\begin{array}{r} 42 \\ 4 \\ \hline \end{array}$$

$$\begin{array}{r} 63 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 78 \\ 29 \\ \hline \end{array}$$

$$\begin{array}{r} 53.0 \\ 95 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 58.3 \\ 42 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 38 \\ 32 \\ \hline \end{array}$$

$$\begin{array}{r} 52 \\ 9 \\ \hline \end{array}$$

$$57$$

$$\begin{array}{r} 60 \\ 5 \\ \hline \end{array}$$

$$\begin{array}{r} 80 \\ 11 \\ \hline \end{array}$$

$$\begin{array}{r} 98 \\ 30 \\ \hline \end{array}$$

$$\begin{array}{r} 51.5 \\ 110 \\ \hline 50 \end{array}$$

	+	14.1 ✓	-	EIV	
		96245 ✓			
T.P.	380	95588 ✓	1037	95208 ✓	
13+65					49.5 ✓
14+0					46.4 ✓
+50				✓	44.9 ✓
B.M.		395	95193	= 95193	
15+0					44.8 ✓
15+12					44.9 ✓
15+15					45.1 ✓
+50					45.3 ✓
+50					
16+0					45.1 ✓
+50					44.9 ✓
17+0					44.6 ✓
+50					44.1 ✓
18+0					43.5 ✓
18+20					
18+50					44.1 ✓

$$\begin{array}{r} 50.3 \\ 56 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 62 \\ 26 \end{array}$$

$$64$$

$$\begin{array}{r} 66 \\ 9 \end{array}$$

$$\begin{array}{r} 67 \\ 30 \end{array}$$

$$\begin{array}{r} 49.3 \\ 66 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 46.5 \\ 94 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 94 \\ 29 \end{array}$$

$$95$$

$$\begin{array}{r} 91 \\ 6 \end{array}$$

$$\begin{array}{r} 85 \\ 28 \end{array}$$

$$\begin{array}{r} 48.6 \\ 73 \\ \hline 50 \end{array}$$

$$44.7$$

$$\begin{array}{r} 112 \\ 50 \end{array}$$

$$\begin{array}{r} 112 \\ 25 \end{array}$$

$$\begin{array}{r} 104 \\ 2 \end{array}$$

$$110$$

$$\begin{array}{r} 112 \\ 1 \end{array}$$

$$\begin{array}{r} 92 \\ 6 \end{array}$$

$$\begin{array}{r} 90 \\ 22 \end{array}$$

$$\begin{array}{r} 49.5 \\ 64 \\ \hline 50 \end{array}$$

Spk. in 20" Willow 200' R. of 14 + 10

$$\begin{array}{r} 44.3 \\ 116 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 112 \\ 30 \end{array}$$

$$\begin{array}{r} 105 \\ 4 \end{array}$$

$$111$$

$$\begin{array}{r} 114 \\ 2 \end{array}$$

$$\begin{array}{r} 88 \\ 11 \end{array}$$

$$\begin{array}{r} 86 \\ 18 \end{array}$$

$$\begin{array}{r} 73 \\ 20 \end{array}$$

$$\begin{array}{r} 64 \\ 33 \end{array}$$

$$\begin{array}{r} 52.3 \\ 36 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 41.53 \\ 1435 \\ \hline 14 \end{array}$$

F.L. = 36" Culv.

$$2830$$

$$110$$

$$\begin{array}{r} 1135 \\ 25 \end{array}$$

$$\begin{array}{r} 128 \\ 25 \end{array}$$

$$\begin{array}{r} 44.3 \\ 116 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 116 \\ 50 \end{array}$$

$$\begin{array}{r} 112 \\ 28 \end{array}$$

$$108$$

$$\begin{array}{r} 110 \\ 3 \end{array}$$

$$\begin{array}{r} 94 \\ 11 \end{array}$$

$$\begin{array}{r} 91 \\ 17 \end{array}$$

$$\begin{array}{r} 66 \\ 23 \end{array}$$

$$\begin{array}{r} 63 \\ 31 \end{array}$$

$$\begin{array}{r} 53.1 \\ 28 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 116 \\ 50 \end{array}$$

$$\begin{array}{r} 110 \\ 27 \end{array}$$

$$106$$

$$\begin{array}{r} 104 \\ 4 \end{array}$$

$$\begin{array}{r} 96 \\ 5 \end{array}$$

$$\begin{array}{r} 92 \\ 17 \end{array}$$

$$\begin{array}{r} 50 \\ 39 \end{array}$$

$$\begin{array}{r} 30 \\ 43 \end{array}$$

$$\begin{array}{r} 24 \\ 50 \end{array}$$

$$44.1$$

$$\begin{array}{r} 118 \\ 50 \end{array}$$

$$\begin{array}{r} 112 \\ 26 \end{array}$$

$$108$$

$$\begin{array}{r} 107 \\ 4 \end{array}$$

$$\begin{array}{r} 95 \\ 11 \end{array}$$

$$\begin{array}{r} 92 \\ 20 \end{array}$$

$$\begin{array}{r} 56 \\ 41 \end{array}$$

$$\begin{array}{r} 51.8 \\ 41 \\ \hline 50 \end{array}$$

$$44.1$$

$$\begin{array}{r} 118 \\ 50 \end{array}$$

$$\begin{array}{r} 114 \\ 27 \end{array}$$

$$110$$

$$\begin{array}{r} 108 \\ 4 \end{array}$$

$$\begin{array}{r} 95 \\ 14 \end{array}$$

$$\begin{array}{r} 95 \\ 22 \end{array}$$

$$\begin{array}{r} 66 \\ 41 \end{array}$$

$$\begin{array}{r} 62 \\ 50 \end{array}$$

$$43.7$$

$$\begin{array}{r} 122 \\ 50 \end{array}$$

$$\begin{array}{r} 118 \\ 29 \end{array}$$

$$113$$

$$\begin{array}{r} 105 \\ 6 \end{array}$$

$$\begin{array}{r} 104 \\ 21 \end{array}$$

$$\begin{array}{r} 46.9 \\ 90 \\ \hline 50 \end{array}$$

$$43.3$$

$$\begin{array}{r} 126 \\ 50 \end{array}$$

$$\begin{array}{r} 122 \\ 25 \end{array}$$

$$118$$

$$\begin{array}{r} 112 \\ 23 \end{array}$$

$$\begin{array}{r} 45.7 \\ 102 \\ \hline 50 \end{array}$$

$$43.4$$

$$\begin{array}{r} 125 \\ 50 \end{array}$$

$$\begin{array}{r} 123 \\ 25 \end{array}$$

$$124$$

$$\begin{array}{r} 120 \\ 21 \end{array}$$

$$\begin{array}{r} 44.4 \\ 115 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 43.9 \\ 120 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 117 \\ 29 \end{array}$$

$$118$$

$$\begin{array}{r} 117 \\ 25 \end{array}$$

$$\begin{array}{r} 127 \\ 25 \end{array}$$

$$\begin{array}{r} 44.3 \\ 116 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 42.1 \\ 13.8 \\ \hline 2.5 \\ \hline F.L. \end{array}$$

+ H. 1 ✓ - EIV
955⁸⁸

19+0

45.5 ✓

19+57

49.7 ✓

T.P.

1047

✓
962¹⁷

418

✓
951⁷⁰

19+75

52.2 ✓

20+0

56.4 ✓

T.P.

1074

✓
972⁹¹

000

962¹⁷

20+35

61.6 ✓

+70

68.7 ✓

T.P.

263

✓
974⁹⁷

057

✓
972³⁴

21+00

71.8 ✓

+25

72.6 ✓

+50

71.0 ✓

+75

69.3 ✓

22+0

69.6 ✓

22+20

70.9 ✓

- L -

- R - 8 -

45.4

$$\frac{105}{50}$$

$$\frac{104}{30}$$

104

$$\frac{98}{25}$$

46.5

$$\frac{94}{50}$$

48.3

$$\frac{76}{50}$$

$$\frac{68}{35}$$

62

$$\frac{58}{4}$$

$$\frac{48}{13}$$

51.5

$$\frac{44}{50}$$

49.6

$$\frac{126}{50}$$

$$\frac{110}{25}$$

100

$$\frac{101}{25}$$

55.6

$$\frac{66}{50}$$

53.0

$$\frac{92}{50}$$

$$\frac{70}{28}$$

58

$$\frac{56}{15}$$

$$\frac{38}{33}$$

60.9

$$\frac{13}{50}$$

59.7

$$\frac{132}{50}$$

$$\frac{125}{28}$$

113

$$\frac{109}{14}$$

$$\frac{96}{30}$$

65.2

$$\frac{77}{50}$$

65.7

$$\frac{72}{50}$$

$$\frac{58}{28}$$

42

$$\frac{34}{13}$$

$$\frac{35}{33}$$

69.4

$$\frac{35}{50}$$

68.3

$$\frac{67}{50}$$

$$\frac{45}{24}$$

32

$$\frac{37}{7}$$

$$\frac{35}{27}$$

71.3

$$\frac{37}{50}$$

69.2

$$\frac{58}{50}$$

$$\frac{40}{26}$$

24

$$\frac{25}{27}$$

72.8

$$\frac{22}{50}$$

68.2

$$\frac{68}{50}$$

$$\frac{57}{26}$$

40

$$\frac{33}{14}$$

$$\frac{15}{31}$$

74.4

$$\frac{06}{50}$$

68.5

$$\frac{65}{50}$$

$$\frac{63}{27}$$

57

$$\frac{50}{14}$$

$$\frac{38}{31}$$

72.3

$$\frac{27}{50}$$

69.4

$$\frac{56}{50}$$

$$\frac{53}{20}$$

54

$$\frac{44}{26}$$

70.8

$$\frac{42}{50}$$

68.2

$$\frac{68}{50}$$

$$\frac{55}{25}$$

41

$$\frac{37}{13}$$

$$\frac{25}{26}$$

$$\frac{34}{36}$$

71.4

$$\frac{36}{50}$$

+ H.1 ✓
974⁹⁷

EIV

+29

72.7 ✓

22+42⁰⁵

72.9 ✓

T.P.

055

✓
969⁰¹

651

✓
968⁴⁶

B.M

9.76

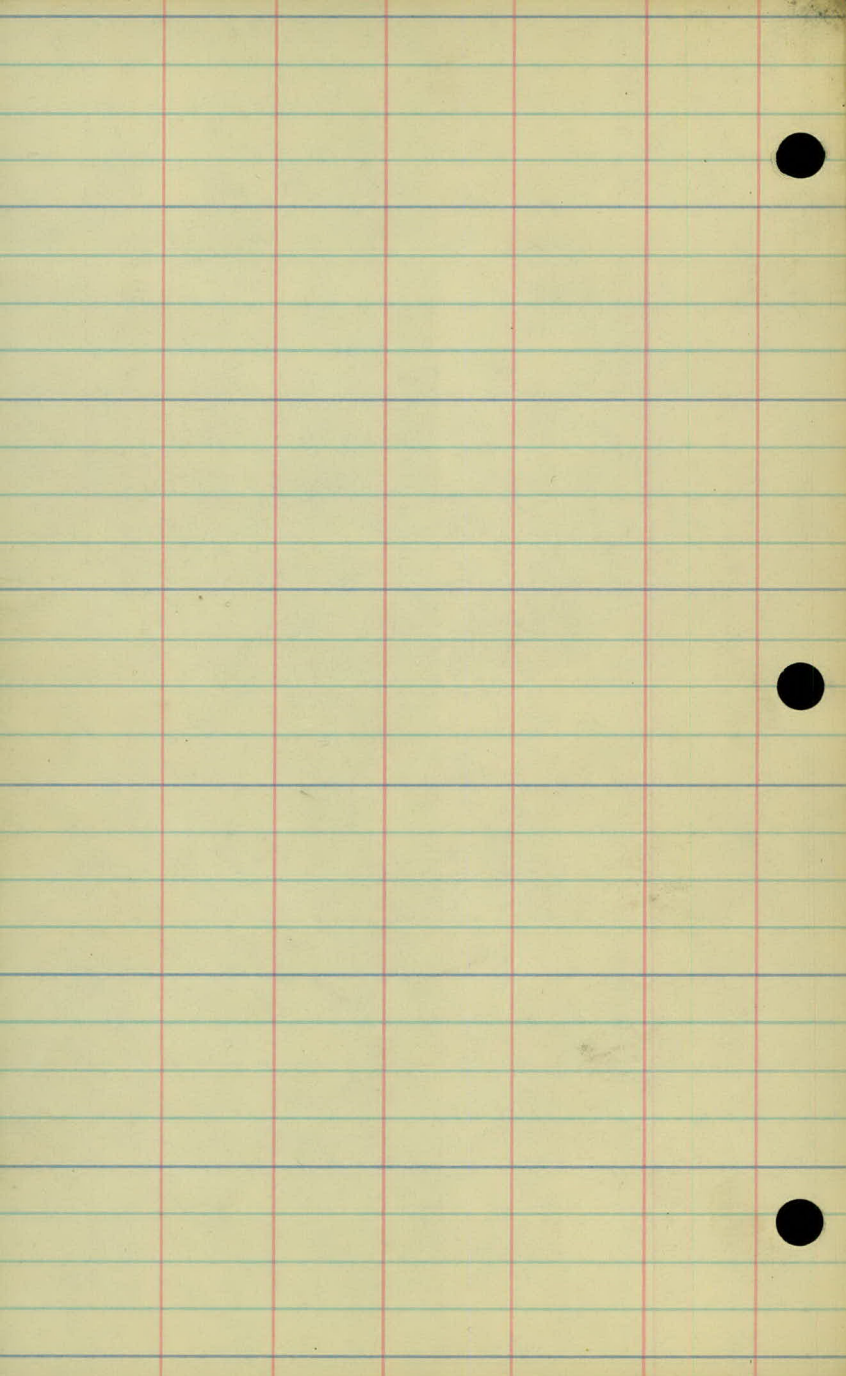
✓
95925 = 95925 ✓

- L -

- R - - 9 -

10.0				
50	40	23	1.5	73.8
50	30		25	1.2
				50
69.9				74.4
51	39	21	1.0	06
50	30		27	50

Top of 3" Angle iron at base of Electric tower
So. pier N.E. Cor. Fairchild + Co. Rd. "D".



Apr-35-

- 1 -

Stoag 1/41
STEINMAN
Bell

- Align. - snowing

Co. Rd. "D"

EXT.

SNOWING 1/41

Pages 1 to 6 -

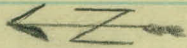
0+00

- L -

- 2 -

- R -

- 2 -



Silver L. West.

of So. Trks

Meqn. Cor.



100' 100' 100'

2300'

90'

40.85

MONT. E of Stinson BIRD.

40' Rdwy.

48' 18"

67.88

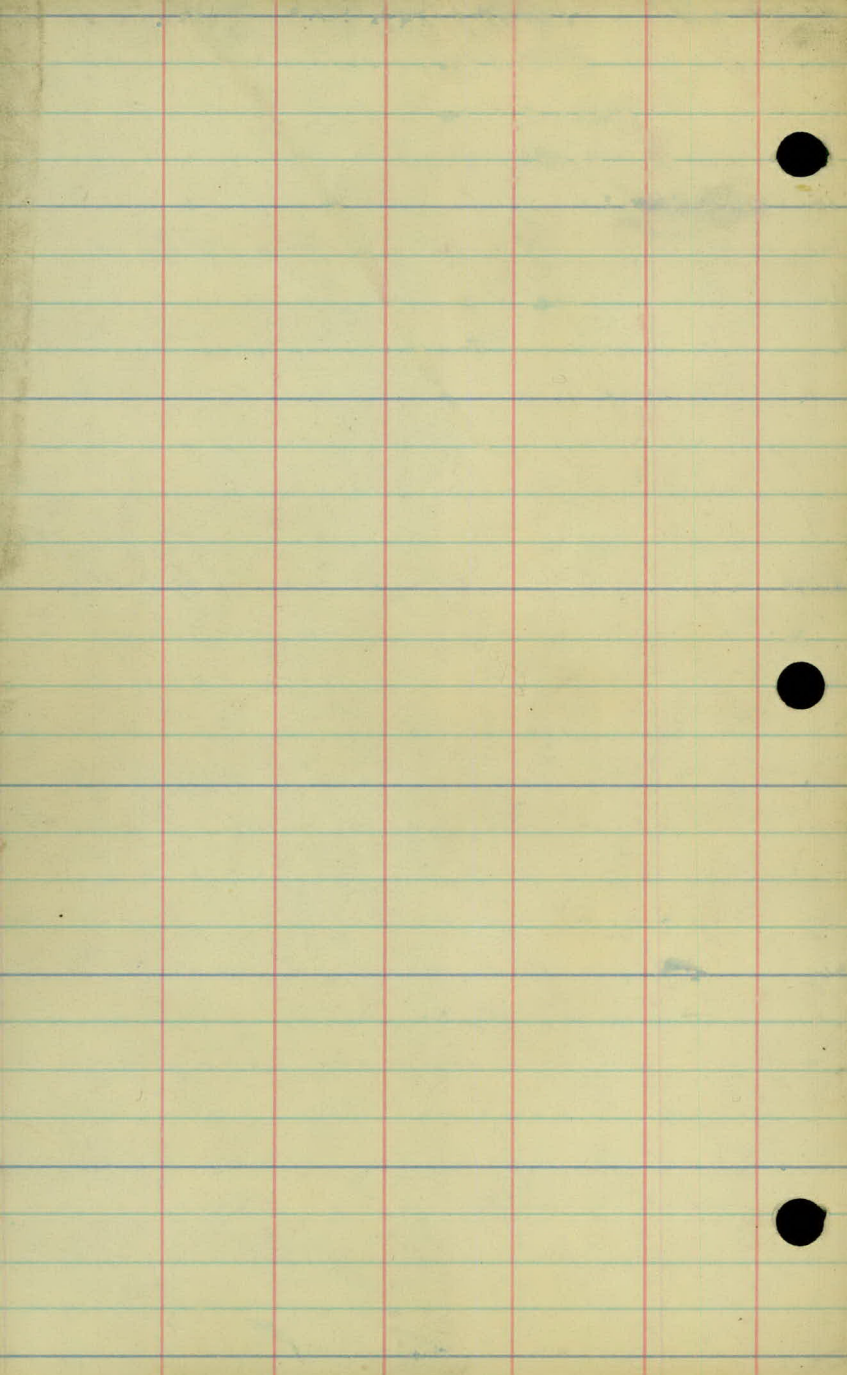
R.R. Tel. R.

Top of Hyd.

← -20' ->

6" Curb.

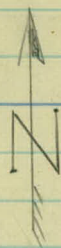
E of 37th Ave. N.E.



- L -

- R -

- 3 -



- silver lake West -

Mean. 66⁷⁵⁰ 10" Cotton.



1" Elm

2300.00

E of So. Trk.

100'

100'

74° 17'

R.R. T. Pole

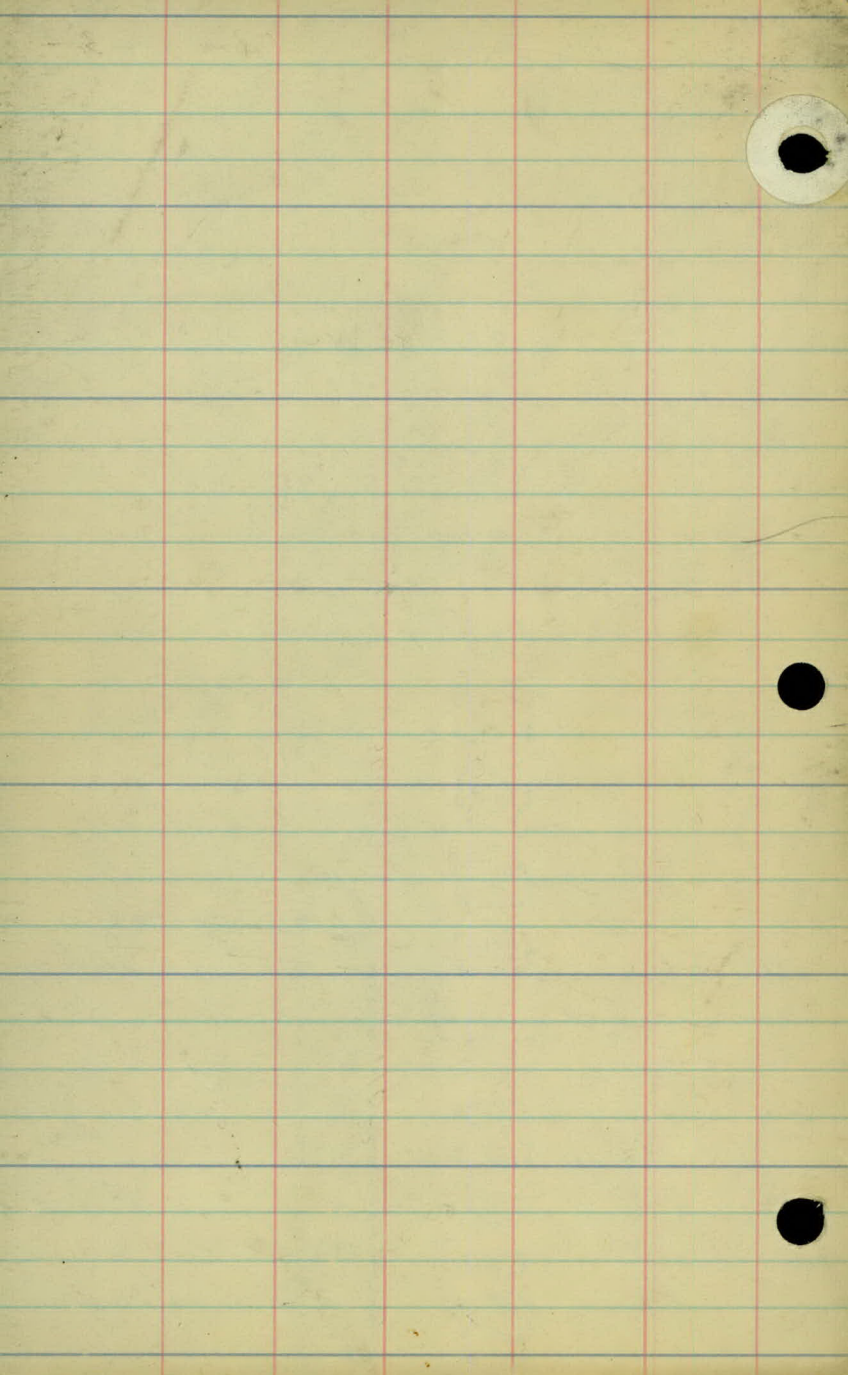
67.88

110.25

103° 44'

Hyd. 48.18

Mont. Estensen Blvd
+ 37 1/4 Ave N.E.



Slope Stakes.

Co. Rd. "D" between Stinson Blv.
& Fairchild Ave.

4/37

32' Crown

2 to 1 Slope on Fill

33' variable Back Slope ^{cuts}

Ditch 2' Deep

Sta.	+	π	-	Grade.
B.M.	11.84	974.35		960.51
0+00				58.0
+50				57.6
1+00				57.2
+50				56.8
2+00				56.4
+50				56.0
T.P.	6.54	965.11	13.76	958.59
3+00				55.6
+50				55.2

L1.

L

L1.

Top. H49. Hinson Bldg 27th Apr. 196.14.8
16.8
$$\begin{array}{r} 14.4 \\ \hline C. 0.4 \\ 33 \end{array}$$

$$\begin{array}{r} 4.4 \\ \hline 12.0 \\ \hline C. 2.8 \end{array}$$

$$\begin{array}{r} 9.5 \\ \hline C. 5.3 \\ 33 \end{array}$$
15.2
17.2
$$\begin{array}{r} 10.6 \\ \hline D. 0.6 \\ 33 \end{array}$$

$$\begin{array}{r} 11.4 \\ \hline 10.5 \\ \hline C. 5.0 \end{array}$$

$$\begin{array}{r} 7.1 \\ \hline C. 8.1 \\ 33 \end{array}$$
15.6
17.6
$$\begin{array}{r} 16.7 \\ \hline D. 0.9 \\ 33 \end{array}$$

$$\begin{array}{r} +11.8 \\ \hline 10.1 \\ \hline C. 5.5 \end{array}$$

$$\begin{array}{r} 5.7 \\ \hline C. 9.9 \\ 33 \end{array}$$

16.0

$$\begin{array}{r} 12.9 \\ \hline C. 3.1 \\ 33 \end{array}$$

$$\begin{array}{r} +10.9 \\ \hline 12.0 \\ \hline C. 4.0 \end{array}$$

$$\begin{array}{r} 1.1 \\ \hline C. 14.9 \\ 33 \end{array}$$

16.4

$$\begin{array}{r} 8.3 \\ \hline C. 8.1 \\ 33 \end{array}$$

$$\begin{array}{r} 6.0 \\ \hline 13.5 \\ \hline C. 7.9 \end{array}$$

$$\begin{array}{r} 8.9 \\ \hline C. 7.5 \\ 33 \end{array}$$

9.1

$$\begin{array}{r} 1.8 \\ \hline C. 7.7 \\ 33 \end{array}$$

$$\begin{array}{r} 2.3 \\ \hline 7.4 \\ \hline C. 2.1 \end{array}$$

$$\begin{array}{r} 5.7 \\ \hline C. 3.8 \\ 33 \end{array}$$

9.9

$$\begin{array}{r} 7.8 \\ \hline C. 2.1 \\ 33 \end{array}$$

$$\begin{array}{r} 6.6 \\ \hline 9.6 \\ \hline C. 0.3 \end{array}$$

$$\begin{array}{r} 6.7 \\ \hline C. 3.7 \\ 33 \end{array}$$

Sta. + π - Grade.

4+00

965.11

54.8

+50

54.4

7.63

957.21

10.53

954.58

5

54.0

+50

53.6

6

53.2

+50

52.8

7

52.4 -

+50

52.3

52.0 ✓

8

51.5

51.7 ✓

10.3
14.3

$$\begin{array}{r} 9 \\ 17 \\ \hline F. 7.6 \\ \hline 21.2 \end{array}$$

$$\begin{array}{r} 13.3 \\ 10.3 \\ \hline 00 \end{array} \text{ Luck}$$

$$\begin{array}{r} 10.3 \\ D.C. 1.0 \\ \hline 33 \end{array}$$

10.7
12.7

$$\begin{array}{r} 14.7 \\ F. 4.0 \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 11.1 \\ F. 0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 9.8 \\ C. 0.9 \\ \hline 33 \end{array}$$

3.2
5.2

$$\begin{array}{r} 7.0 \\ F. 3.8 \\ \hline 23.6 \end{array}$$

$$\begin{array}{r} 6.1 \\ 3.6 \\ \hline F. 0.4 \end{array}$$

$$\begin{array}{r} 2.6 \\ C. 0.6 \\ \hline 33 \end{array}$$

3.6
5.6

$$\begin{array}{r} 5.9 \\ F. 1.3 \\ \hline 20.6 \end{array}$$

$$\begin{array}{r} 5.3 \\ 3.8 \\ \hline F. 0.2 \end{array}$$

$$\begin{array}{r} 4.7 \\ D.C. 0.9 \\ \hline 33 \end{array}$$

4.0
6.0

$$\begin{array}{r} 5.6 \\ D.C. 0.4 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 3.0 \\ 4.1 \\ \hline F. 0.1 \end{array} \text{ Luck}$$

$$\begin{array}{r} 2.8 \\ C. 1.2 \\ \hline 33 \end{array}$$

4.4
6.4

$$\begin{array}{r} 6.2 \\ D.C. 0.2 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 6.1 \\ 5.2 \\ \hline F. 0.8 \end{array}$$

$$\begin{array}{r} 5.2 \\ D.C. 1.2 \\ \hline 33 \end{array}$$

4.8
6.8

$$\begin{array}{r} 9.3 \\ F. 4.5 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 8.0 \\ 5.4 \\ \hline F. 0.6 \end{array}$$

$$\begin{array}{r} 5.8 \\ D.C. 1.0 \\ \hline 33 \end{array}$$

5.2
7.2

$$\begin{array}{r} 10.6 \\ F. 5.4 \\ \hline 26.8 \end{array}$$

$$\begin{array}{r} 2.3 \\ 2.4 \\ \hline F. 0.1 \end{array}$$

$$\begin{array}{r} 3.8 \\ C. 1.4 \\ \hline 33 \end{array}$$

5.5
7.5

$$\begin{array}{r} 10.8 \\ F. 5.3 \\ \hline 26.6 \end{array}$$

$$\begin{array}{r} 5.0 \\ C. 0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 2.5 \\ C. 3.0 \\ \hline 33 \end{array}$$

Sta + π - Grade

8+50 957.21 51.7 51.4

9 10.46 963.53 4.14 51.1 913.07

+50 50.8

10 50.5

+50 50.3

11 50.0

+50 49.8

12 49.6

+50 49.4

4.

8

8

5.8
7.6

1014
F4.6
21.2

4.9
C.O.9

2.6
C3.2
33

6.1
8.1

10.2
F4.1
24.2

7.8
5.5
C.O.6

3.3
C.1.8
33

12.7
14.7

150
F.2.3
20.6

12.0
11.2
C.1.5

5.0
C.1.7
33

13.0
15.0

150
D.C.O.O
33

9.3
9.1
C3.9

2.2
C10.8
33

13.2
15.2

15.2
D.C.O.O
29

12.3
C.O.9

6.4
C6.8
33

13.5
15.5

15.5
D.C.O.O
33

12.0
C.1.1

8.2
C5.3
33

13.7
15.7

14.7
P.C.1.0
33

10.4
C3.3

7.0
C.6.7
33

13.9
15.9

13.9
D.C.2.0
33

8.0
C.5.9

3.8
C10.1
33

14.1
16.1

100
C4.1
33

3.8
C10.3

2.9
C11.2
33

Sta.	+	π	-	Grade	
		963.53			
13				49.2	
T.P.	5.21	957.62	11.12	952.41	
+50				49.0	
14				48.8	Spec Ditch Rt. 46.4
+50				48.6	46.2
		Hand changed			
15			48.6	48.7	46.0
B.M.	2.30	954.23	5.67		951.53
+50			48.8	48.2	45.8
16			49.5	50.4	45.6
+50			50.4	51.0	45.4
17			51.8	52.4	45.2

CT.

E

RT

14.3

$$\begin{array}{r} 4.9 \\ 9.4 \\ \hline C \quad 3.7 \end{array}$$

$$\begin{array}{r} 5.2 \\ 9.1 \\ \hline C \quad 3.7 \end{array}$$

$$\begin{array}{r} 9.4 \\ 4.9 \\ \hline 33 \end{array}$$

8.6
10.6

$$\begin{array}{r} 5.2 \\ 3.4 \\ \hline C \quad 3.7 \end{array}$$

$$\begin{array}{r} 5.9 \\ 5.7 \\ \hline C \quad 3.7 \end{array}$$

$$\begin{array}{r} 8.0 \\ 2.06 \\ \hline 33 \end{array}$$

8.8
10.8

(11.2)

$$\begin{array}{r} 11.0 \\ 2.2 \\ \hline 20.4 \end{array}$$

200' RT + 20' Willow

$$\begin{array}{r} 11.2 \\ 8.8 \\ \hline 00 \text{ side} \end{array}$$

$$\begin{array}{r} 9.9 \\ 0.13 \\ \hline 33 \end{array}$$

Bag Spec. Ditch 2.4 Days

9.0
11.0

(11.4)

$$\begin{array}{r} 12.8 \\ 3.8 \\ \hline 23.6 \end{array}$$

$$\begin{array}{r} 12.7 \\ 8.5 \\ \hline C.O. 5 \end{array}$$

$$\begin{array}{r} 9.2 \\ 0.2 \\ \hline 33 \end{array}$$

2.4 Days

9.0
11.0

(11.6)

$$\begin{array}{r} 12.6 \\ 3.6 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 12.8 \\ 8.7 \\ \hline C.O. 3 \end{array}$$

$$\begin{array}{r} 8.0 \\ 3.6 \\ \hline 33 \end{array}$$

2.9 Days

20" Willow - 200' RT + 14 + 10

5.4
7.4

(8.4)

$$\begin{array}{r} 9.3 \\ 3.9 \\ \hline 23.8 \end{array}$$

$$\begin{array}{r} 8.9 \\ 5.3 \\ \hline C.O. 1 \end{array}$$

$$\begin{array}{r} 3.4 \\ 4.4 \\ \hline 0.4.4.0 \\ 33 \end{array}$$

4.7
6.7

(8.6)

$$\begin{array}{r} 9.5 \\ 4.8 \\ \hline 25.6 \end{array}$$

$$\begin{array}{r} 9.1 \\ 5.4 \\ \hline F.O. 7 \end{array}$$

$$\begin{array}{r} 7.1 \\ 12.4 \\ \hline 20.8 \end{array}$$

$$\begin{array}{r} 5.1 \\ 0.3.5 \\ \hline 33 \end{array}$$

2.5 Days

3.8
5.8

(8.8)

$$\begin{array}{r} 9.8 \\ 6.0 \\ \hline 28.0 \end{array}$$

$$\begin{array}{r} 9.1 \\ 5.1 \\ \hline F. 1.3 \end{array}$$

$$\begin{array}{r} 7.7 \\ 3.9 \\ \hline 23.8 \end{array}$$

$$\begin{array}{r} 6.1 \\ 12.2.7 \\ \hline 36 \end{array}$$

2.6 Days

2.4

(9.0)

$$\begin{array}{r} 10.3 \\ 7.9 \\ \hline 31.8 \end{array}$$

$$\begin{array}{r} 4.6 \\ 4.5 \\ \hline F. 2.1 \end{array}$$

$$\begin{array}{r} 8.0 \\ 5.6 \\ \hline 27.2 \end{array}$$

$$\begin{array}{r} 7.5 \\ 1.5 \\ \hline 0.2.1.5 \\ 39 \end{array}$$

Sta.	+	K	-	Grade
		954.73		
17+50			53.4	52.9 46.0

18			55.4	55.8 44.8
----	--	--	------	----------------------

+50			57.7	57.9
-----	--	--	------	-----------------

19				60.2 ✓
----	--	--	--	--------

T.P.	10.08	963.40	0.91	953.32
------	-------	--------	------	--------

+50				62.7
-----	--	--	--	------

20				65.2
----	--	--	--	------

T.P.	12.84	975.56	0.68	962.22
------	-------	--------	------	--------

+50				67.8
-----	--	--	--	------

21				69.6
----	--	--	--	------

+50				71.0
-----	--	--	--	------

512

+

π

-

Grade

995.56

22

72.0

+42

72.9

B.M.

16.35

959.21

959.25

17.

$$\begin{array}{r} 6.1 \\ 1.15 \\ \hline 21 \end{array}$$

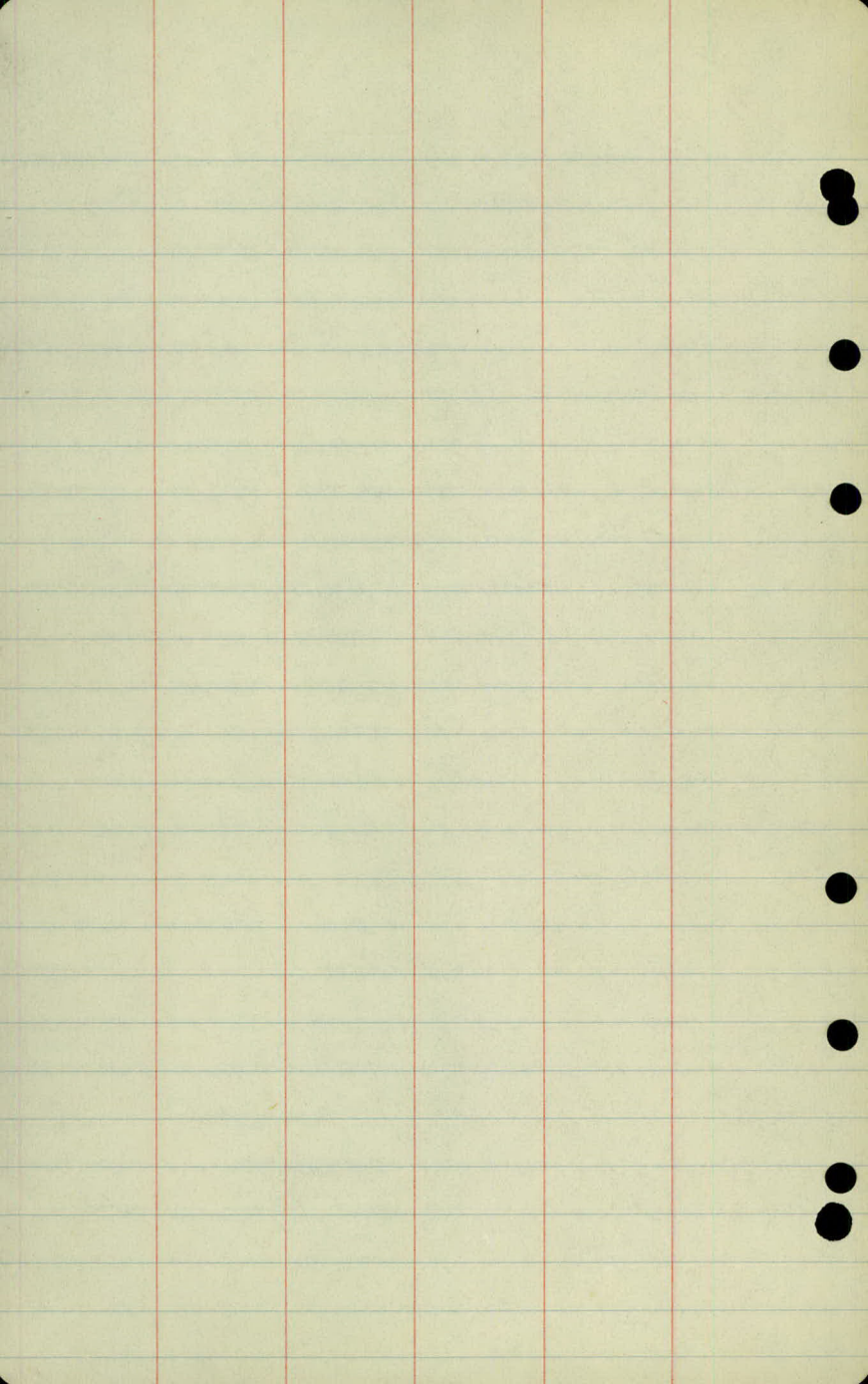
$$\begin{array}{r} 2 \\ 6.0 \\ 5.9 \\ \hline 22.3 \end{array}$$

$$\begin{array}{r} 27 \\ 4.8 \\ 20.0.8 \\ \hline 33 \end{array}$$

2.6
1.6

Top 3" L Iron Base elec Tower N.E. Con Fairchild 90.

$$\begin{array}{r} 27 \\ \hline 00 \end{array}$$



Co. Rd. "D" - X-Section between
slope stakes as set $4\frac{1}{2}$ to be
used in estimating yardage moved
to date. Use in conjunction with
slope stake notes, & grades as existing
= 0+00 Elev.

Sta.

Lt.

L

Rt.

0+50

$\frac{00}{19}$

$\frac{+0.4}{29}$

$\frac{+2.4}{33}$

1

$\frac{00}{18}$

$\frac{00}{27}$

$\frac{+3.2}{33}$

+50

$\frac{00}{23}$

$\frac{00}{26}$

$\frac{+4.4}{32.1}$

2

$\frac{+2.5}{27}$

$\frac{00}{22}$

$\frac{00}{27}$

$\frac{+10.9}{33}$

+50

$\frac{+5.2}{32}$

$\frac{00}{15}$

$\frac{00}{29}$

$\frac{+4.6}{33}$

3

$\frac{+5.6}{33}$

$\frac{00}{16}$

$\frac{00}{30}$

$\frac{+1.7}{31.5}$

+50

$\frac{+1.8}{30}$

$\frac{00}{28}$

$\frac{00}{30}$

$\frac{+2.9}{32}$

4

$\frac{-2.6}{19}$

$\frac{00}{13}$

$\frac{00}{13}$

$\frac{-2.0}{18} \quad \frac{-2.0}{24} \quad \frac{-0.3}{28}$

+50

5

$\frac{-3.3}{19}$

$\frac{00}{13}$

$\frac{00}{13}$

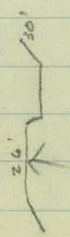
$\frac{-2.0}{16} \quad \frac{-2.0}{25} \quad \frac{-0.3}{28}$

+50

6

+50

9/10 x 108 incl
26' top
30' on Rt + 2' ditch Rt



5th.

Lt.

Z

Rt.

7

+ 0.8

+50

8

 $-\frac{5.7}{25}$ $\frac{00}{13}$ $\frac{00}{13}$ $-\frac{1.6}{17}$ $-\frac{1.6}{24}$ $+\frac{1.8}{29}$

+50

9

 $-\frac{4.6}{22}$ $\frac{00}{13}$ $\frac{00}{13}$ $-\frac{0.6}{18}$ $-\frac{0.6}{25}$ $+\frac{2.0}{30}$

+50

 $\frac{00}{13}$ $\frac{00}{26}$ $+\frac{6.0}{31}$

10

Not touched

 $\frac{00}{28}$ $+\frac{6.0}{33}$

+50

Not touched

11

+50

12

+50

13

+7.5

Not touched

Sta.

Lt.

C

Rt.

14

26' Crown 2-1 slope

+50

15

+50

16

+50

17

+80

18

apex for Culvert

+70

19

26' Crown 2 to 1 slopes

20

↓

56.

14.

2

27.

150

 $\frac{00}{33}$ $\frac{00}{33}$

21

 $\frac{+07}{33}$ $\frac{-08}{28}$ $\frac{+04}{30}$ $\frac{+12}{33}$

150

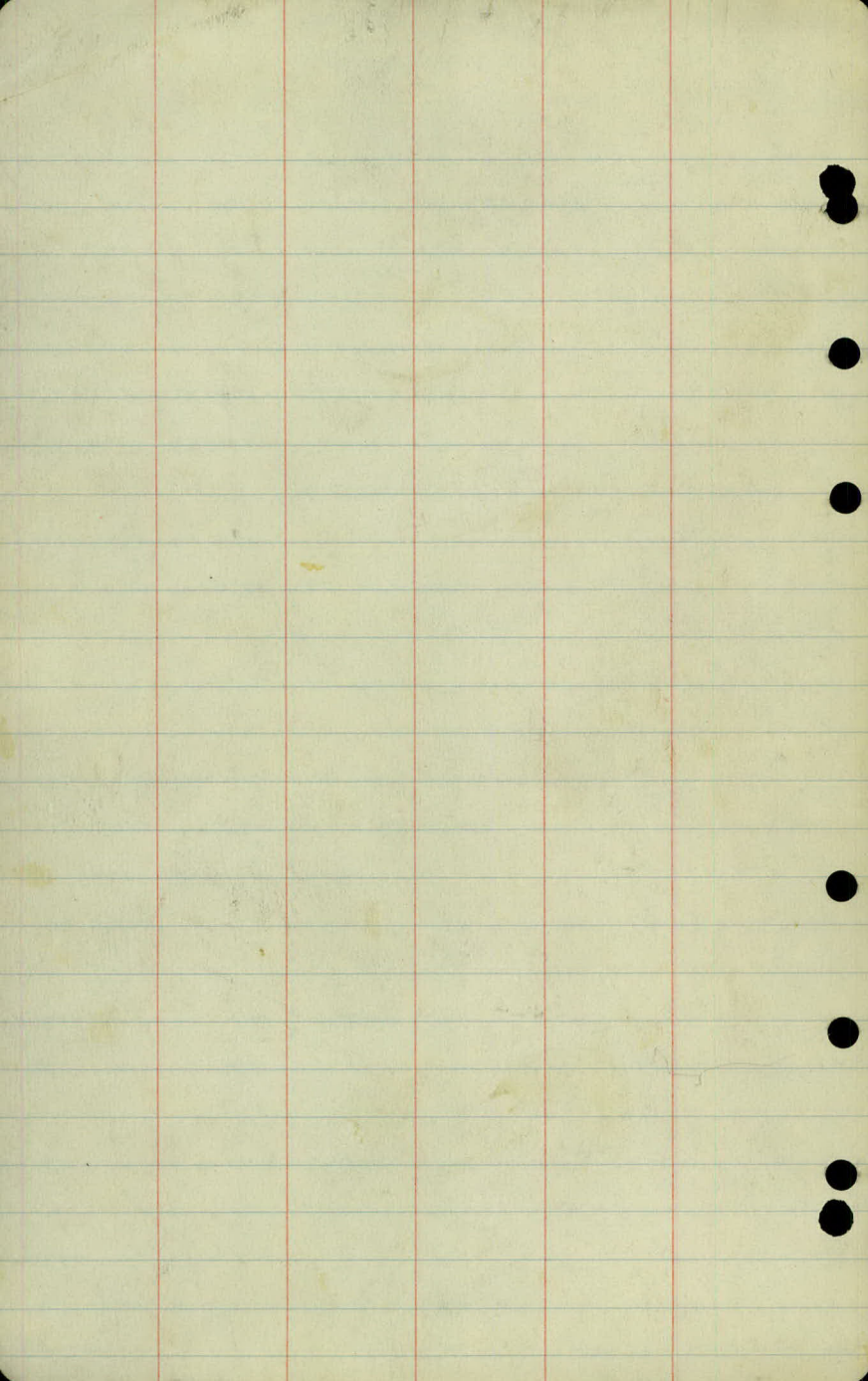
Not touched

 $\frac{+24}{36}$ $\frac{+16}{37}$

22



+45



	<u>Date</u>	<u>330-4</u>	<u>D.C.</u>	<u>Grade</u>
✓ 15 -	7.9	4.0	3.9	45.7
+50 -		3.9	2.0	47.7
16		4.9	1.3	47.4
+50		6.0	0.0	47.6 ✓

	<u>Grade</u>	<u>Grade</u> <u>Date</u>	<u>Below</u> <u>Grade</u>
15 -	48.6	45.7	2.9
+50 -	48.8	47.7	1.1
16 -	49.5	47.4	2.1
+50 -	50.4	47.6	2.8

5/2/37

Ditch Grade as
Established by Mr. Harris

"D"

8.47.8

5.5
4.8
5.5

5.5
4.8
5.5
4.8
5.5

5.5
4.8
5.5
4.8
5.5

$$\begin{array}{r} 10.7 \\ 2.8 \\ \hline 13.5 \end{array}$$

$$\begin{array}{r} 9'10'' \\ 2'5'' \\ \hline 12'15'' \end{array}$$

$$881$$

$$\begin{array}{r} 881.62 \\ 4.5 \\ \hline 886.13 \end{array}$$

$$\begin{array}{r} 886.1 \\ 5.1 \\ \hline 881 \end{array}$$

	+	+	-	
B.M.	0.45	891.55		891.10
			8.76	882.79
B.M. - Hobb.	5.05	887.84	5.75	882.09 X
T.P.	5.75	887.84	4.92	882.92
B.M.	5.07	887.99	2.80	885.19
				885.29

$$\begin{array}{r} 951.97 \\ 170 \\ \hline 950.63 \end{array}$$

$$\begin{array}{r} 0.68 \\ 1.1 \\ \hline \end{array}$$

$$\begin{array}{r} 0.11 \\ 1.4 \\ \hline \end{array}$$

$$\begin{array}{r} 0.54 \\ 1.2 \\ \hline \end{array}$$

35

$$\begin{array}{r} 6.276 \\ 1.9 \\ \hline \end{array} \checkmark$$

$$\begin{array}{r} 6.201 \\ 1.457 \\ \hline \end{array}$$

$$\begin{array}{r} -0.3 \\ -0.15 \\ 0.115 \\ \hline \end{array}$$

$$\begin{array}{r} 6.20 \\ 6.528 \\ \hline \end{array}$$

$$\begin{array}{r} -0.8 \\ 1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 5.6 \\ 6.26 \\ \hline \end{array}$$

$$-0.6$$

$$0.2$$

$$0.38$$

$$0.15$$

$$0.8$$

$$0.60$$

$$\begin{array}{r} 38.6 \\ 40.2 \\ \hline 78.8 \end{array}$$

6.2
5.6

County Road D.
Grade Plugs.

Sta.	+	∞	-	Grade	Grade rod.
B.M.				960.51	
0+00				58.0	
+50				57.6	
1				57.2	
+50				56.8	
2				56.4	
+50				56.0	
3				55.6	
+50				55.2	
4				54.8	
			2.58	968.38	968.21
10.49	970.86		0.73	960.37	
+50				54.4	6.7
B.M.					968.21
5				54.0	7.1
+50				53.6	7.50

Sta.	+	π	-	Grade.	² / ₁
	7.78	961.10	3.40	953.22	
6				53.2	3.4
+50				52.8	3.8.
7				52.4	4.2.
+50				52.0	4.6.
8				51.7	49.
+50				51.4	5.2.
9				51.1	5.5.
+50				50.8	5.8.
10				50.5	6.1.
	6.32	956.62	3.80	950.30	
+50		954.10		50.3	3.8
11				50.0	4.1
+50				49.8	4.3.
12		954.10		49.6	4.50.

Sta.	+	x	-	Grade	Grade Rod.
12+50				49.4	4.7
13	2.17	954.10		49.2	4.9
B.M.	1.95	953.88			951.73
+50				49.0	4.9
14				48.8	5.1
+50				48.6	5.3
15				48.6	5.3 5.2
+50				48.8	5.1 5.0
16				49.5	4.4 4.2
+50				50.4	3.5 3.3
17				51.8	2.1 1.8
T.P.	10.99	963.68	1.19	954.69	
+50				53.4	10.3 9.9
18				55.4	8.3 7.8
+50				57.7	6.0 5.5

Sta.

+

Σ

-

Grade

³
 Grade
 Rod.

963.68

19

60.2

3.5 3.0

+50

62.7

1.0 0.5

T.P.

11.62

974.99

0.31

963.37

20

65.2

9.8 7.5

+50

67.8

7.2

21

69.6

5.4

+50

71.0

4.0

22

72.0

3.0

+42

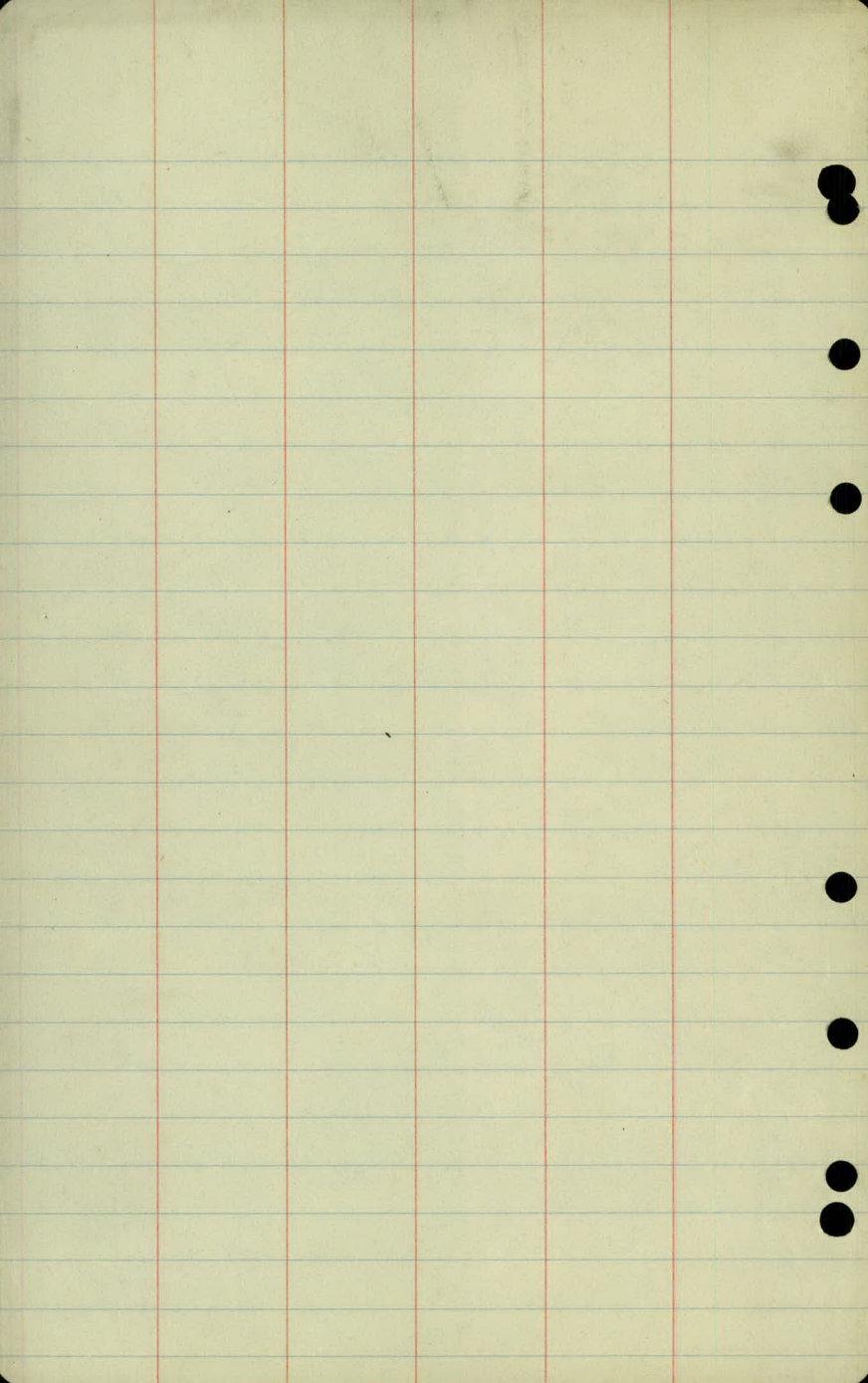
72.9

2.1

B.M.

15.22

~~919.25~~
 919.27



Profile Levels

Minn Trans. R.R Tracks
& Co Rd "D"

From 500' West of Tracks
To, 500' East of Tracks

Sta	+	π	-	Elev
-----	---	-------	---	------

B.M.		109.75		
------	--	--------	--	--

5+00

0+00 = 500' West of Tracks 02.0

+50

01.0

4

00.3

+50

99.7

3

99.3

+50

99.1

2

99.0

+50

99.0

Σ

Spk in P.P. NW Cor "D" + Tr.

28

38

45

51

55

57

58

58

Sta + Δ - Elev

104.75

1 99.1

+50 99.3

0 00.0

+50 99.9

1 00.2

+50 00.8

2 01.1

+50 01.6

ϕ

57

55

475

49

46

40

37

32

Sta

+

 Δ

-

Elev

109.75

3

01.8

+50

01.8

4

02.1

+50

02.1

5

02.3

R

3.0

30

27

27

2.5

