

3 7-26-00
OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

OTTER LAKE RD.

From Schuneman Rd to Co. Rd. "G"

Road Acc't. No. 25

Date Filed 1-6-36

File 6

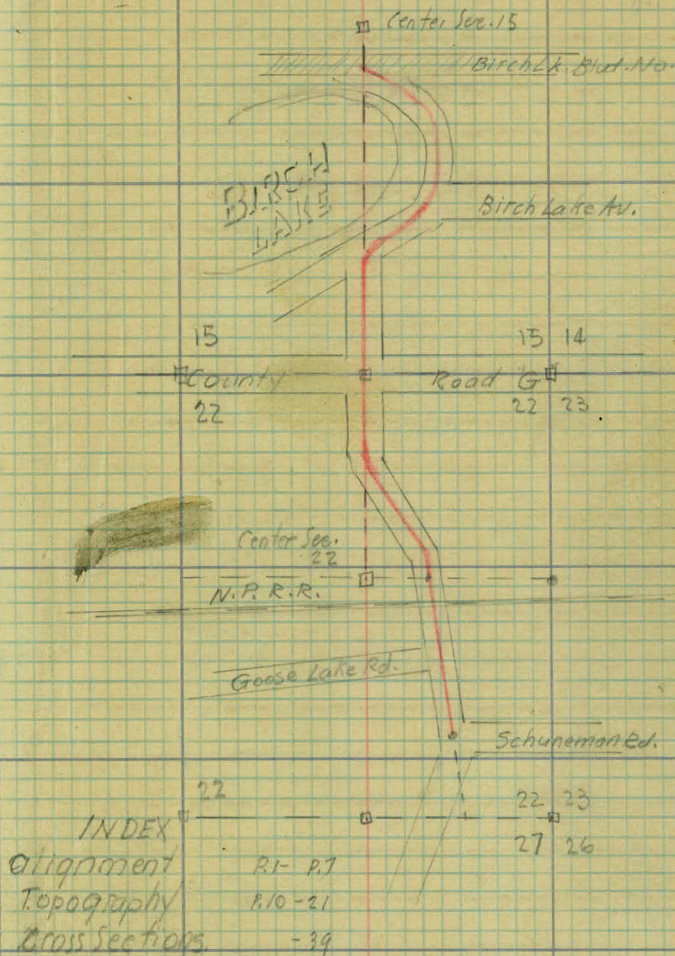
incomplete

Plan Notes

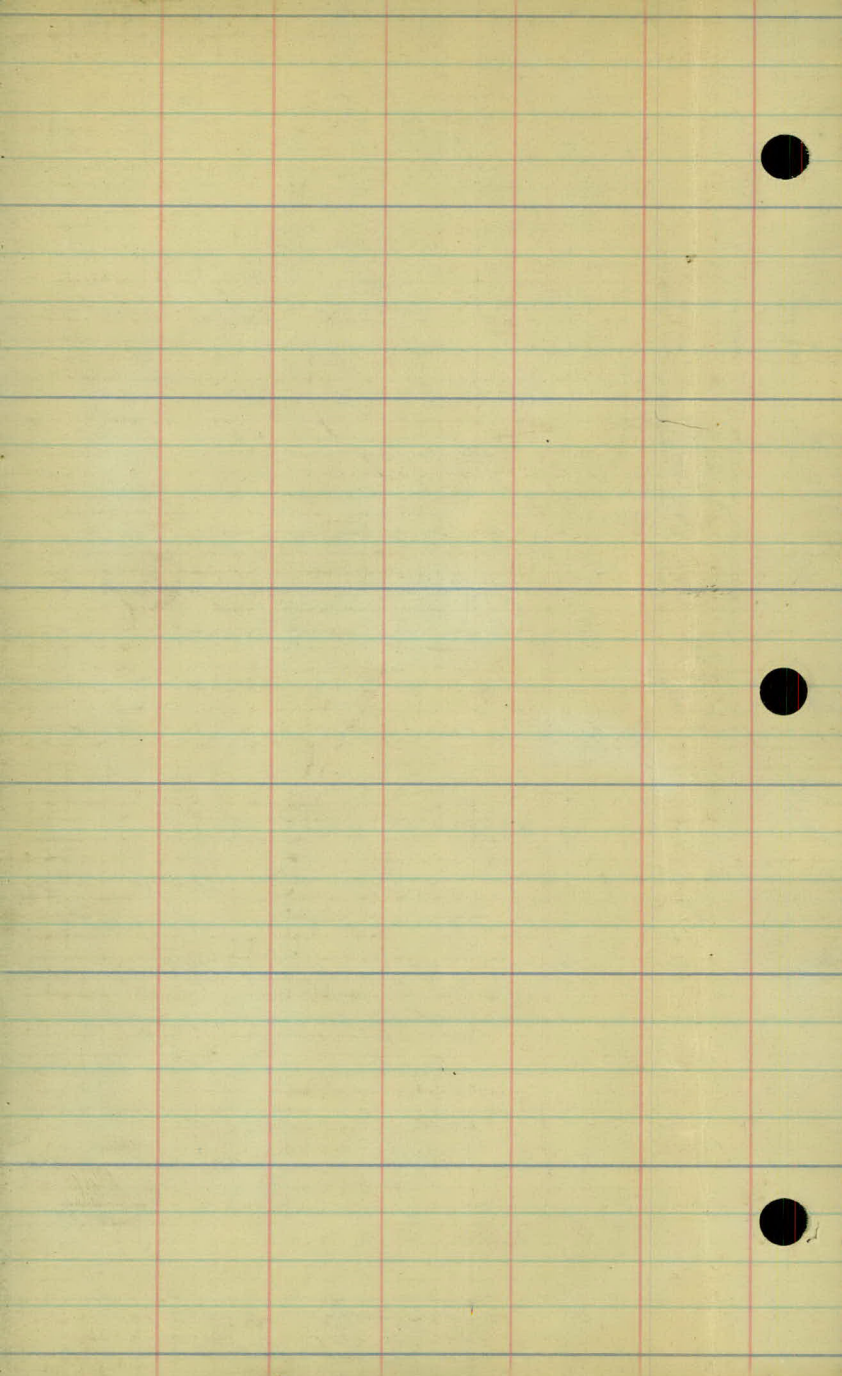
1832

716
1200
95

Plan Survey
 Otter Lake Road
 Schuneman Rd. to N. Birch Lake Blvd.



W. H. Carlson. Dec. 1935
 June 1936

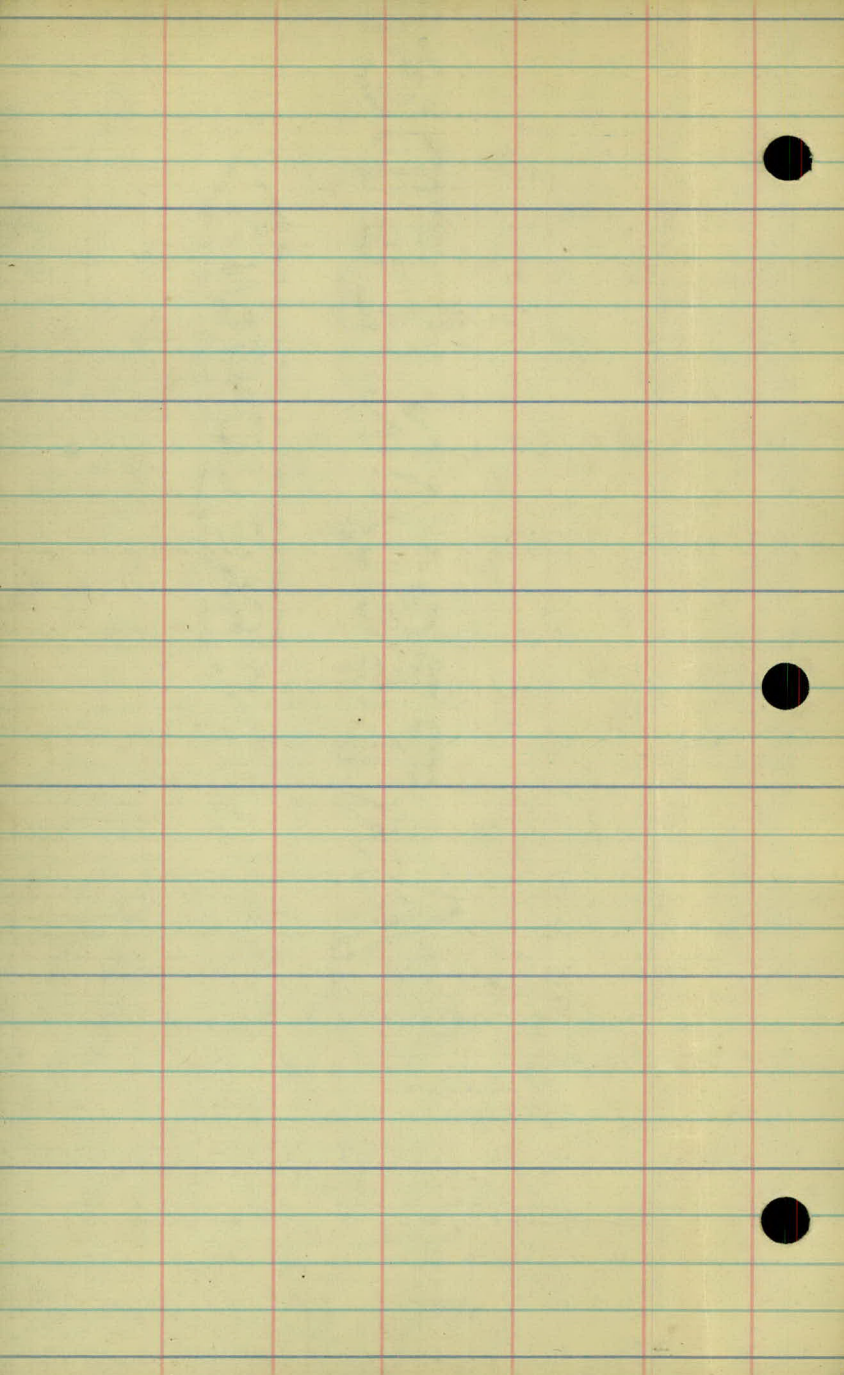


Otter Lake Road.

Schuneman Rd. to N. Birch Lake Blvd.

Book #6 Dr. 6

W. H. Carlson
Dec. 14/1935

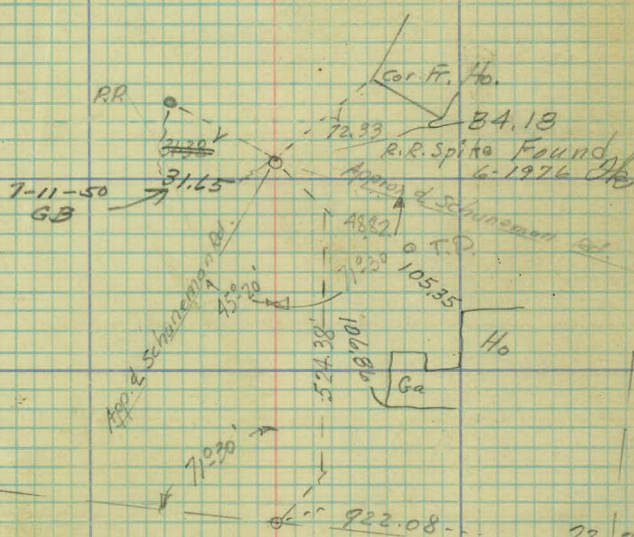
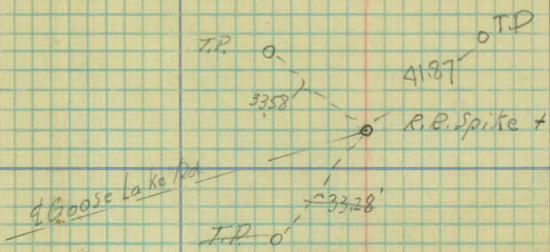


alignment.

Station	Point	Angle	Lt.	Rt.
---------	-------	-------	-----	-----

6+62.80	2	0°32'		Gooselake Rd.
---------	---	-------	--	---------------

0+00				Approach Schuneman Rd.
------	--	--	--	------------------------



5/14 Con.
5/22/72

Note:
Not the same
as Road Map

Post Transport

W.H.C.
K.A.
L.B.H.
E.D.

Dec. 3, 1925
Cold-Snow.

22/23
27/26

Station Point Angle
L RT

36+05.69 ✓ P.T. 5°41'

36 5°37.6'

PT 10.66 } 37 5°41' 5°07.6'

35 5°31.7' 4°37.6'

+50 4°46.7' 4°07.6'

34 4°01.7' 3°37.6'

+50 3°16.7' 3°07.6'

33 2°31.7' 2°37.6'

+50 1°46.7' 2°07.6'

32 1°01.7' 1°37.6'

+50 0°16.7' 1°07.6'

31+32.39 P.C. 0°00' 0°37.6'

30+37.36 ✓ P.C. 0°00'

3° C.Lt.

T 190.09

L.C. 378.9

P.L. 33+22.48

D= 2°00'

Δ 11°22' Lt.

T. 285.12 ✓

L.C. 568.33 ✓

R. 3864.93 ✓

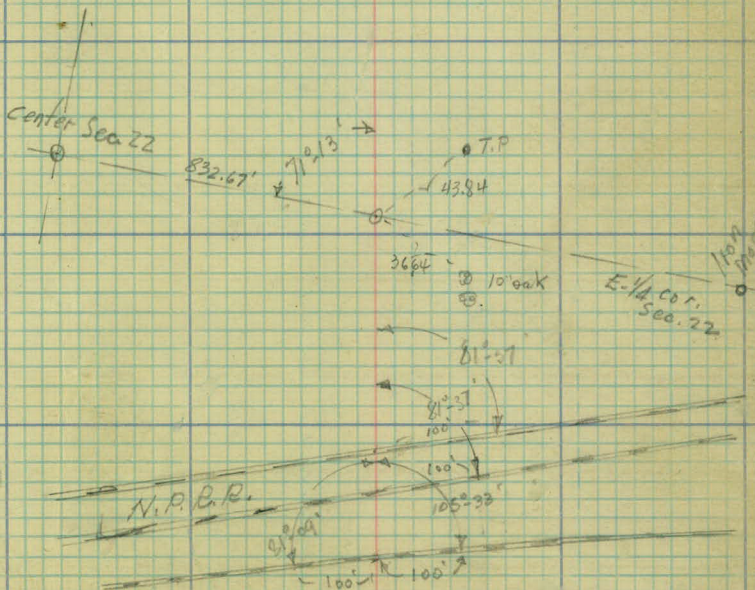
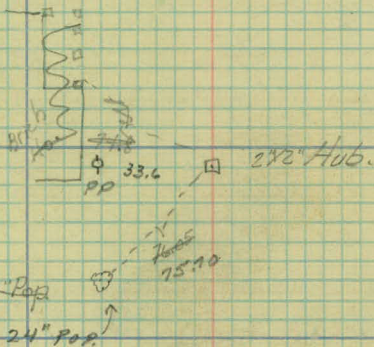
22+48.35 P.O.T. Sec Line

10+89.53 P.O.T. 9. Track

10+71.68 P.O.T. 2

10+194 P.O.T. 2

N.E. Cor.
Bench Post



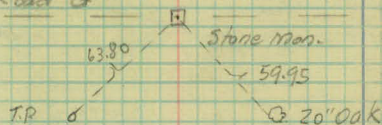
Station	Point	Angle Lt Rt.
---------	-------	-----------------

50+64.67	P.I. Mon Co. Rd 6	0°-17' Lt.
----------	----------------------	------------

44+20.17 ✓	RT.	15°01'	
44		13°48.4'	P.I. 42+98.21
+50		10°48.4'	D. 12°00'
43		7°48.4'	Δ 36°02' Rt.
+50		4°48.4'	T. 128.32' ✓
42 ^{28.7}		12°48.4'	L.C. 250.28' ✓
41+69.89 ✓ _{20.5}	P.C.	0°00'	R= 478.34' ✓

E Co. Road "G"

N. 1/4 Cor. Sec. 22



2"x2" Hub.

T.P.

31.66

9.73

T.P.

128.32

57.66 @ 10" Oak

82.26

80.28

25.75

50.85

O T.P. 43

PP

1/4 Sec. Line 7

Center Sec. 22

Iron Mon.

Station Point Angle
Lt Rt

61+54.97 ✓ P.T. 52°00'

61+00 3°22.3

60+50 1°52.3

60+0 0°22.3

59+88.30 ✓ P.C. 0°00'

59+87.60

58+99.22 ✓ P.T. 15°30'

P.I. 58+24.07

20°-C Rt.

10°-34.7 Δ 31°00'

T. 79.85 ✓

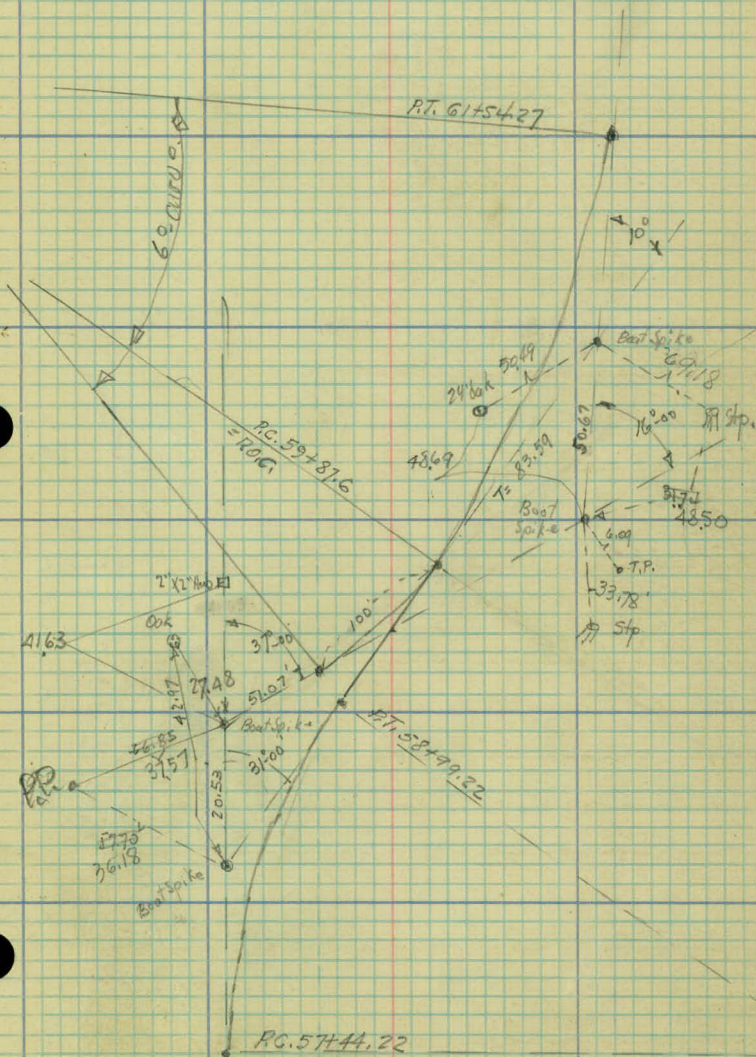
52°34.7 L.C. 155.20 ✓

R= 287.94 ✓

58

57+44.22 ✓ P.C.

0°00'



Sta Point Lt Rt

72+4.01 ✓ P.T. 17°30'

72 17°10.1'

P.I. 71+19.70

+50 12°10.1'

Δ 35°00' Lt.

71 7°10.1'

D. 20°

70+50 2°10.1'

T. 90.69 ✓

70+29.01 ✓ P.C. 0°00'

L. 175.00 ✓

R. 287.94 ✓

70+07.28 ✓ P.T. 9°46'

70 9°24.2'

P.I. 68+87.70

+50 7°24.2'

Δ = 19°20' Lt.

69 5°24.2'

D. 8°00'

+50 3°24.2'

T. 122.09 ✓

68 1°24.2'

L.C. 241.67 ✓

67+65.61 ✓ P.C. 0°00'

R. 716.78 ✓

65+65.15 ✓ P.T. 9°21'

65 6°46.3'

P.I. 64+49.42

+50 4°46.3'

Δ 18°42' Lt.

64 2°46.3'

D. 8°00'

+50 0°46.3'

T. 118.02 ✓

63+31.4 ✓ P.C. 0°00'

L.C. 233.75 ✓

R. 716.78 ✓

o P.P.

31.37

2"x2" Hub.

54.5 16" Elm

R Nail's Top Oak S/P

19.86

2"x2" Hub.

30.77

o P.P.

o G.P.

o P.P.

50.50

88.10

64.84

Approx 2 Birch LK. Ave.

43.02

o G.P.

26.

Point

73+55.57 End of curve

73+36.91 ✓ P.T.

18° 22'

73+00

13° 17.8'

P.I. 72+74.34

+75

9° 47.8'

Δ 36° 44'

+50

6° 17.8'

D-28°

+25

2° 47.8'

T. 68.62 ✓

72+05.72 ✓ P.C.

0° 00'

L.C. 13+19 ✓

L=200.68 ✓

BIRCH LAKE

near edge
15 RA Sign

center Sec 15

49.89

46.12

34.62
88-44'

PT. 73 + 36.91

46.12

44.16

T.R.

34.74

55.83

Bart Spikes

36.78'

3-nails G.R. Plank
tan extd.

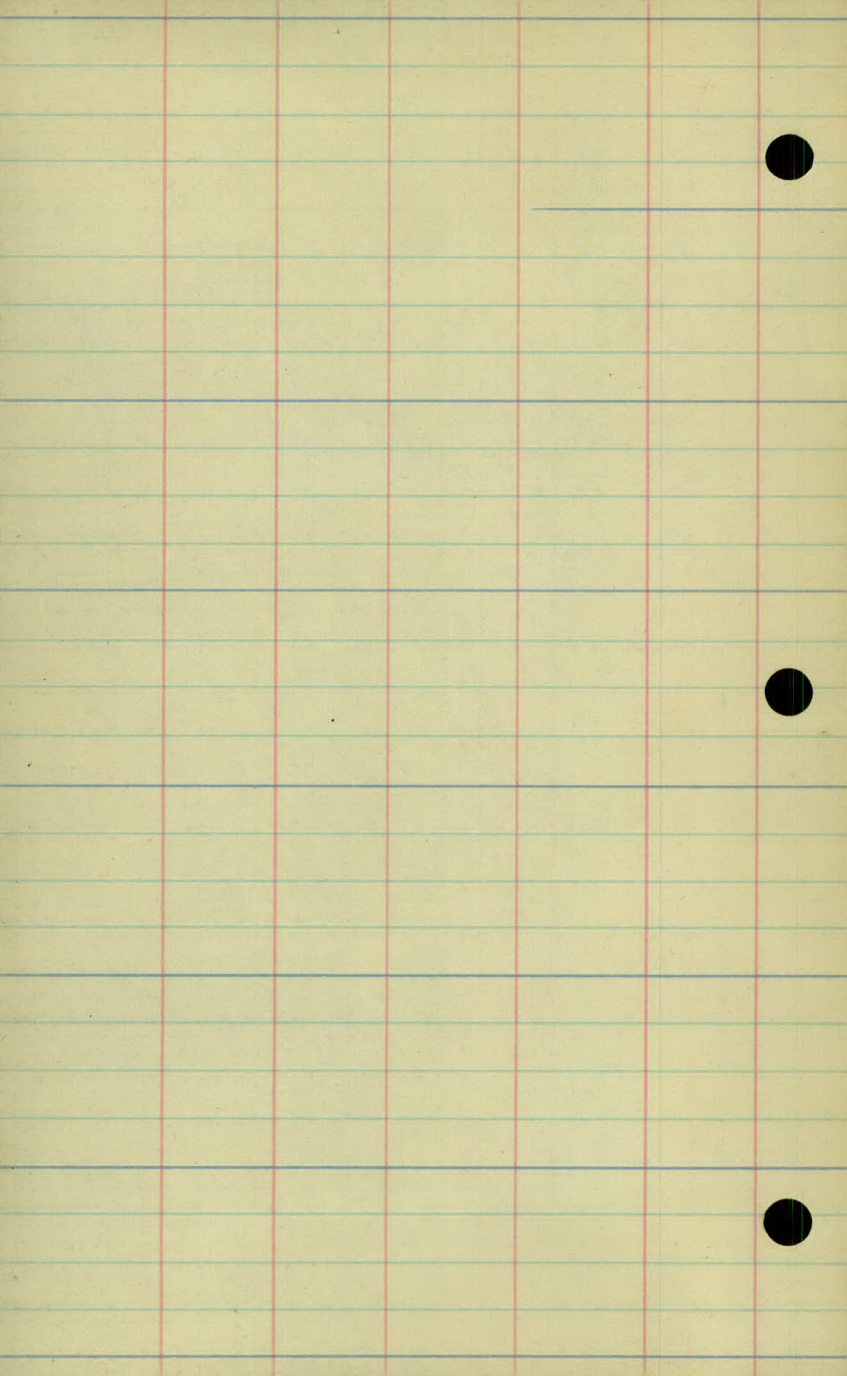
L.P. for Birch Lake Blvd

10°

EXT-1.8

P.C. 72 + 05.02
P.T. 72 + 03.31

9°19'



Topography

12-13

4-12T
Roadway

11-10'

3

13-9'

2

13-9

1

13' 10'

460 10-11'

130-12-19'

0+00 ^{20' 00'} Approx ± Schuneman Rd.

-0+50 31'

+99-T.P. 28'

11

+88-16 "Oak-39'

+99-8 "W. 28'

+96-18 "Oak 40'

+58-T.P. 28'

+70-Ent 21'

+20-T.P. 28'

+81-T.P. 28'

+78 Sign 17'
+76-RR 19'

-0 +20-Tatvia 36

-0 +52-T.P. 28'



+56-N.W. 1/4 Cor. 78

+34-S.W. 1/4 Cor. 64

+24-1/4 Br E. 47

+5

-0 +32-Torno 58

-0 +38-T.P. 50

W.H.C.
K.A.
Z.B.H.
E.D.

Dec. 4, 1935
Cold-Windy.

6' 10'

11

+189.53

12' Plank 8'

+71.68

12' Plank 9'

+19.4

8' Plank 8'

10

7-7

9

10-9'

8

11' - 8'

7

11' 8'

+62.8- L. Goose Lake Rd.

+30-11'

6

45-14-11'

+20 27'

+50 11-

5

+114-9.R.23'
+4-Xing Sp. 24'

+38

+0-4-14.W. Cor. 70'
+15-S.W. Cor. 70'
+174-F. Cor. 2'
+98-24° 58' E. 52'

+24-Cor. F. 22'
+13-F. R. 23'

81° 37'

81° 209'

105° 23'

100'

100'

+93-9.R.21'

+73-T. R. 22'

R.R. Tol. Po. 43'

+76 R.R. F. 36'

+43-T. R. 23'

+15-N.E. Cor. 58'

25° W. - 15° N
+00-S.E. Cor. 60 57'

+81-T. R. 29'
+84-6° 58' E. 53'

+50-T. R. 21'

+112-9.R.23'

+75

+39-T. R. 23'

cut

+02-17" Oak 35'

18

9-11

17

9-11

16

9' 12'

15

8'-11'

14

8'-9

13

7' 10'

12

+92-T.P. 20'

(12)

+55-T.P. 20'

+24-T.P. 21'

F-23'

Oaks-33'

+89-T.P. 21'

+78-F. Cor. 24'

+56-T.P. 21'

+26-F. Cor. 26'

Pasture

+69-F. Cor. 26'

+45-Ent.

+23-T.P. 22'

+12-18' SE 44'

Cultivated.

12-8

25

12-10

24

11 10

23

11 10

+48.35. Sec. Line

22

10 11

21

10 12

20

9 10

19

148-T.P. 20

120-T.P. 20

188-T.P. 20

132-T. Cor. 24

End Timber 33

155-T.P. 20

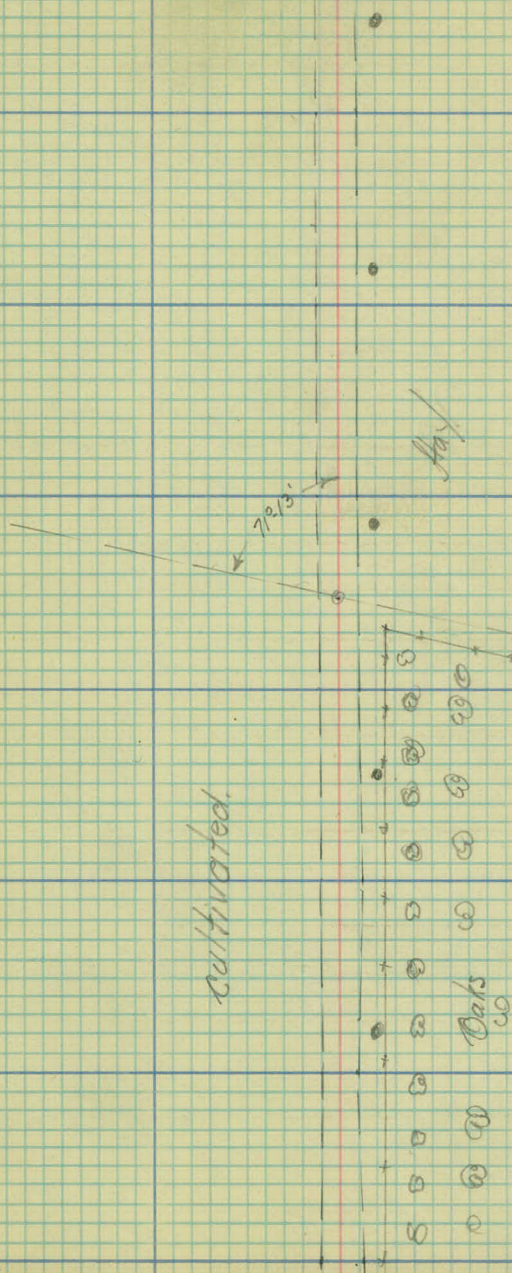
122-T.P. 20

cultivated.

Hay

72.13'

Oats



9 11

150 9-10

32

10-9

150-10-8

31

11-7

30

11-7

29

10-7

28

10 8

27

10 8

164- 36" X 30.5- C.M. { 17-13.5 } - Core H.W. 12" X 6'
Cuto
Ditch-

26

+70-Ent.

+26-T.P. 22'

+18-Ent.

+75-T.P. 18'

+37-T.P. 21'

+7 Trail 37'

+6 Trail 23'

+52-End F. 36'

+26-Int. of Ent.

+12-F. Cor. 27'

+12-T.P. 19'

+71-F. Cor. 45'

+82-F. Cor. 16'

+79-T.P. 19'

+65-12" Wid-26'

F-70

11-11

39

10 11

38

9 11

37

10 9

170-2 South St. (Due East)

36

9 9

10 - 7

35

9 8

150 = 8 10

34

8-11'

193 24' Bx E. 20

150 - 9-12

33

Timber 53

100-T.P. 17
Timber 39

16

Timber 55

Timber 34

+60-T.P. 23

+48-T.P. 17-2-10

Timber 48

Timber 35

Timber 47

+69-T.P. 21

Timber 27

+99-T.P. 17-2-10.00

+64-Culu. 43

18x34 C.M.

+35-Culu. 26

+86-T.P. 20

+75-16'-(240)
T.P.

+52-T.P. 22-300

+44-T.P. 20-200

+98-E.G.R. 12
+82-N.E.C. 45
+55 Cr. Ho. 140x453
+57-20' Cr. E.T. 15
+51-Pump 41
+50-Cr. G.R. 32
+32-55 Cr. Ho. 61
+26-18' Br. E.T. 36
+11-Pump G.R. 13

+42-T.P. 28
+33-T.P. 29

Timber 45
About 30 Jump

South St.
+27

cult.

cult.

Rail Force

6-13

46

5-14

45

4 14

44

4 14

43

150 6 10

9-10

150 10-9

42

10 10

41

11 11

40

Timber 35'

17

169-T.P. 28'

Timber 36'

194-T.P. 20'

133-T.P. 29'

Timber 40

145-T.P. 16' 2-Wire

Cult.

Timber 34
198-T.P. 31'

Oaks

118-Cor. Timber 36'
106-Ent.

188-G.P.X
187-T.P. 15'

187-T.P. 18'

102-Cor. Timber 35'

Cult.

Timber 42'

165-Cor. Timber 43
165-T.P. 29'

140-T.P. 16'

Timber 39'

112-T.P. 26'

15-5

53

12-5

13-7

52

13-7

51

13-8

+89- 15" x 30 CM new full of Dirt.

+64.67-Mon 2001.9"

+30- 12-9

50

11-8

49

10-9

48

8-10

47

+39-T.P. 28'

+20-T.P. 19'

+89-T.P. 28'

+29-T.P. 21'

+06-T.P. 27'

+76-N. Edge Torvia.

+36-S. edge Torvia

+06-T.P. 27'

+30-T.P. 22'
+19-18" Oak 41'

Duff

+89-T.P. 24'

+72

Forest
land+27-T.P. 25'
+25-18" Oak 43'

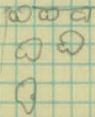
Scattered Oaks

+53-14" Oak 35'

+73-Ent.

+96-T.P. 27'

+38-T.P. 24'

+60-End Timber
30'

12-10

late Shore
104

150 13-11

60

12-12'

104

150- 12' 12'

59

14'-10'

150 26-7

58

47-23 14-5

2

145- 17-4

57

18-4

56

55

16-5

54

+90-8" 19k E/D 50 -19

19

+49-16" Oak 21
+39-16" Oak 37
+34-18" Oak 20

+21-T.P. 17'
+17-T.P. 16'

+64-16" Oak 19'
+54-P.P. 14'

+52-T.P. 26'

+12-8" Tw. Oak 32

+48-18" Oak 45
+43-14" Oak 42
+22-14" Oak 54
+19-P.P. 48

+84-T.P. 23'
+78-T.P. 27
+68-16" Oak 45
+56-16" Oak 41

+35-24" Oak 37
+28-24" Tw. Oak 42

+18-16" Rd. 33

+74-T.P. 12'
+71-18" Oak 37
+53-12" Oak 32
+43-30" Oak 32

+14-16" Oak 26'

+90-T.P. 16'

+30-T.P. 31'

+76-T.P. 17'

+90-T.P. 29'

+48-T.P. 18'

12-9

Lake Shore
4

75-11-70

67

11-12

71'

11-13'

66

12-13'

70'

13-12'

65

12' 16'

76

+ 49' Approx to Birch Lake Ho
750-9'

64

11-12

81'

+ 50- 11'-10'

63

12-11'

80'

62

10-10

84'

+ 50 12'-10'

61

104'

F-17'

+180-6" Birch 50'
+164-12" Birch 40'
+157-18" Oak 14'
+152-18" Oak 21'
+140-18" Oak 22'
+127-12" Oak 25'
+115-6" Oak 25'
+102-15" P 28'
F-14

+99-T.P. 40'

+73-10" Elm 45'

+24-10" Elm 48'
+107-8" Tw Oak 15'
+101-8" Oak 16'
F-15'

+97-10" Tw Oak 17'
+79-18" Oak 23'
+75-T.P. 30'
+73-15" Oak 18'
+50-12" Oak 19'
+37-8" Tw Oak 19'
+30-12" Tw Oak 17'
+109-9" P 16'
+102-18" Oak 30'
Fence 18'

+166-14" Elm 50'
+161-15" Oak 35'
+146-20" Oak 10'
+143-10" Elm 55'
+132-8" Elm 54'
+114-12" Tw Oak 13'
+105-P.P. 12'
+11-8" Tw Elm 55'

+98-15" Oak 14'
+96-9" P 12'
+51-15" Oak 16'
+49-15" Oak 16'

+20-18" Oak 34'
+15-18" Oak 27'
+13-18" Oak 17'

+96-24" Oak 24'
+81-24" Oak 25'
+56-P.P. 13'

+74-8" Tw Box E. 20'

+86-P.P. 15'

+165-10" Oak 28'
+165-F-16'

+78-24" Oak 30'
+77-T.P. 14'
+54-15" Oak 13'

Scattered
trees
near
Lake

100 ENT.

20

+91-F. Cor. 25'
+65-F-22'
+46-P.P. 16'

F-21'

+26-P.P. 19'
F-20'

+50-F-21'

+22-P.P. 24' Fence

+87-Δ in Fen 32'
+81-30" Oak 33'
+68-F-25'

Birch Lake Ave.

+28-36" Oak 42'
+16-30" Oak 22'

+86-T.P. 20'

+88-14" Maple 27'
+88-T.P. 16'
+55-24" Box E. 39'
+44-10" Maple 29'

+42-N.W. Cor. T.P. 76'
+29-24" Maple 21'
+24-12" " 30'
+16-S.W. Cor. Hg 72'
+99-14" Maple 31'

+54-T.P. 14'

+30-EN'

Pasture

Form
yard

74

Lake Shore

+54.87- 9.2 Pau. 11.7

53'

+76- 83 Pau. 13.8

73

1.0 Pau. 21.0

52'

+50

51'

72

11-12

38'

9' 14

71

9'-12

43

12'-10'

70

11'-14'

55'

9'-14

69

9'-13'

65'

+50 10-9

68

69'

+55-G.R. 13.5
 +72-3" Birch 25'
 +71-End Cable beg Plank G.R.
 +12-T.P. 28'
 G.R. 120

+90-3" Birch-30'
 +75-G.R. 14'

+50-G.R. 17'

+44-3" Birch 32'

+15-End Cul. 24" C&G
 G.R. 12. 30

+97-T.P. 26

+50-G.R. 9'

+12-F. cor. 17'

+09-Beg G.R. 10'

+55-T.P. 32'

+50-F-20

F-16'

+98-16" Will-45

+66-5-Trees 38'-41'

+56-

+56-24" Oak 14'

+82-18" Sp. 16'

+80-8" Elm 39'

+80-T.P. 30

+01-8" Birch 50'

F-13'

+82-18" Oak 19'

+95-End Row. 55

+50-F-14'

+39-15" x Elm 14'

+19-T.P. 40

+10-Beg Road 46'

Offer Lake Rd.

+78-T.P. 23

+24-4" G.R. 20

+05-E Pump 40.

G.R. 26. 54

+49-Cul. 69'

+50-Pav. 25. 49

+25-Pav. 49

+25-G.R. 37

+24-Drain-30

+01-Beg. G.R. 13'

+78-12" Oak 38'

+63-10" Elm 29'

+53-12" Elm 33'

+45-10" Elm 32'

+25-12" Elm 33'

+31-15" Elm 34'

+25-12" Elm 31'

+12-18" Elm 18'

+84-30" Elm 43'

+16-P.P. 20

+13-24" Oak 21'

+09-18" Oak 24'

+88-13" Oak Walk-S3

8x11.

+48-Cul. 8" 43'

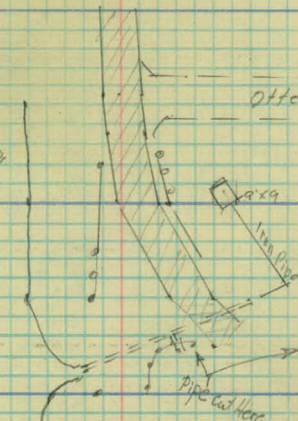
+30-30" Sp. 32'

+98-30" Sp. 27'

+55-T.P. 15'

+42-24" Sp. 17'

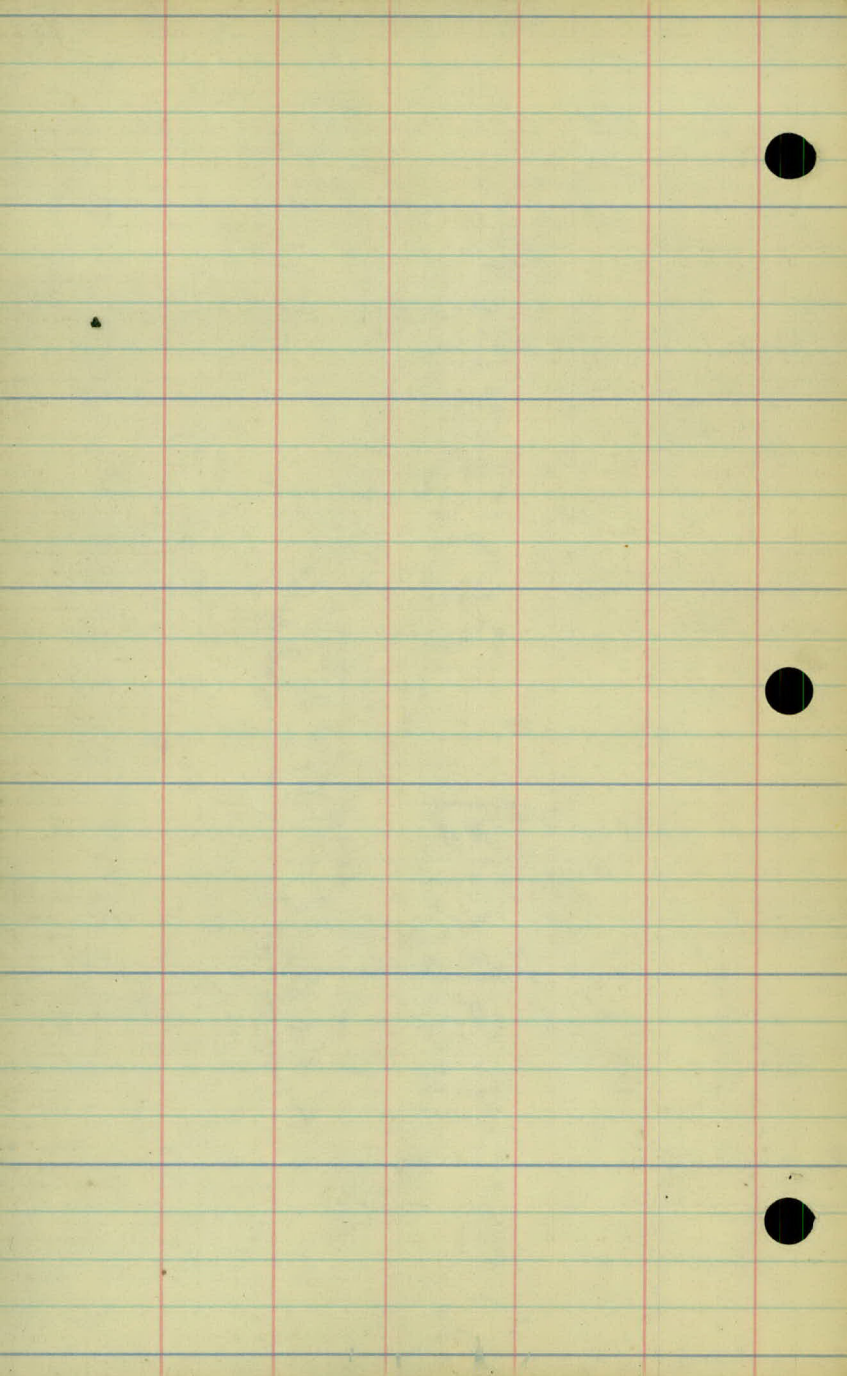
+29-24" Sp. 16'



Pipe Cul. 110
 +65-8" Elm 33
 +45-T.P. 20

Yard
 Yard

Brick Wall 10' 0\"/>



Cross-Sections.
Otter Lake Road

Station	+	π	-	Elev.
B.M.	7.27	937.07		929.80
B.M.	3.85	939.68	1.24	935.83

-0+25				32.1
-------	--	--	--	------

0+0				33.0
-----	--	--	--	------

0+30				33.6
------	--	--	--	------

1+0				34.5
-----	--	--	--	------

+50				34.8
-----	--	--	--	------

2+0				35.0
-----	--	--	--	------

+50				35.4
-----	--	--	--	------

3+0				35.8
-----	--	--	--	------

T.P.	8.66	944.86	3.48	936.20
------	------	--------	------	--------

+50				36.2
-----	--	--	--	------

4+0				36.5
-----	--	--	--	------

+20				36.6
-----	--	--	--	------

R.R. Spike Top 30" Stump. 75' H. - 0462

$$\frac{2.5}{76} \quad \frac{2.4}{84} = \frac{2.4}{50} \quad \frac{2.2}{30} = \text{t. Schumann} \quad \frac{7.6}{50} \quad \frac{7.3}{50} = \text{t. Schumann}$$

$$\frac{6.4}{50} \quad \frac{6.8}{33} \quad \frac{7.1}{27} \quad \frac{6.7}{12} \quad \frac{6.7}{50} \quad \frac{6.9}{18} \quad \frac{7.3}{43} \quad \frac{6.4}{46} \quad \frac{6.3}{50} = \frac{1}{10} \text{ and}$$

$$\frac{5.1}{50} \quad \frac{5.0}{29} \quad \frac{5.7}{14} \quad \frac{6.7}{13} \quad \frac{6.1}{50} \quad \frac{6.6}{18} \quad \frac{6.5}{36} \quad \frac{5.7}{50}$$

$$\frac{4.9}{50} \quad \frac{5.1}{14} \quad \frac{5.6}{13} \quad \frac{5.2}{50} \quad \frac{5.5}{10} \quad \frac{4.9}{12} \quad \frac{5.6}{50}$$

$$\frac{5.2}{50} \quad \frac{4.6}{34} \quad \frac{4.7}{15} \quad \frac{5.3}{14} \quad \frac{4.9}{50} \quad \frac{5.1}{10} \quad \frac{4.9}{19} \quad \frac{5.7}{50}$$

$$\frac{3.8}{50} \quad \frac{4.0}{18} \quad \frac{5.0}{14} \quad \frac{4.7}{50} \quad \frac{5.2}{9} \quad \frac{5.6}{18} \quad \frac{6.9}{50}$$

$$\frac{3.3}{50} \quad \frac{3.6}{20} \quad \frac{4.6}{15} \quad \frac{4.3}{50} \quad \frac{5.0}{9} \quad \frac{5.9}{14} \quad \frac{7.2}{32} \quad \frac{8.0}{50}$$

$$\frac{1.9}{50} \quad \frac{1.6}{37} \quad \frac{2.5}{20} \quad \frac{4.3}{15} \quad \frac{4.0}{7} \quad \frac{3.9}{50} \quad \frac{4.6}{9} \quad \frac{6.0}{18} \quad \frac{7.1}{33} \quad \frac{7.6}{50}$$

$$\frac{4.5}{50} \quad \frac{4.9}{39} \quad \frac{6.3}{22} \quad \frac{9.1}{16} \quad \frac{7.2}{13} \quad \frac{8.7}{50} \quad \frac{9.6}{10} \quad \frac{9.8}{17} \quad \frac{11.3}{35} \quad \frac{12.4}{50}$$

$$\frac{2.6}{50} \quad \frac{4.2}{27} \quad \frac{7.8}{20} \quad \frac{8.1}{15} \quad \frac{8.5}{11} \quad \frac{8.4}{50} \quad \frac{9.2}{10} \quad \frac{9.1}{15} \quad \frac{11.0}{36} \quad \frac{12.0}{50}$$

$$\frac{2.4}{58} \quad \frac{6.0}{44} \quad \frac{7.0}{31} \quad \frac{7.8}{15} \quad \frac{8.6}{12} \quad \frac{8.3}{50} \quad \frac{9.1}{10} \quad \frac{9.6}{15} \quad \frac{10.2}{27} \quad \frac{11.7}{50}$$

Station	+	π	-	Elev.
		944.86		
1140				36.6
540				36.0
450				35.3
640				34.6
T.P.	2.81	936.98	10.69	934.17
6450				34.0
740				33.0
B.M.	4.07	936.98	4.07	932.91
450				31.8
840				30.7
8492				28.8
T.P.	6.69	935.22	8.45	928.53
9408				28.5
450				28.2
1040				28.3

2.9	3.4	4.5	9.2	8.8	8.3	9.1	11.2	10.6	11.7
50	43	25	17	12	-	11	22	41	50

50	52	67	9.2	9.3	8.9	9.7	9.7	11.2	12.2
50	41	24	18	12	-	14	21	36	50

7.7	8.3	9.0	8.8	9.7	9.6	10.3	7.8	11.5	12.1
50	42	20	15	12	x	14	18	52	50

8.9	9.7	10.0	10.2	10.3	11.1	10.7	11.6	12.6
50	44	- Rt	20	4x	15	17	34	50

4.9	2.3	2.8	3.0	3.0	3.5	3.0	4.3	4.2
50	50	31	9	-	11	16	36	50

2.6	3.2	4.3	4.4	4.0	4.5	3.1	2.7	4.3
50	22	15	11	-	12	16	26	50

2.R. Spike in 1st oak 75' Rt. Ha 7405

2.5	3.2	5.7	5.5	5.2	5.3	2.9	2.8	3.5	3.8	1.2
50	22	17	13	-	12	19	27	32	39	50

2.6	2.9	6.7	6.7	6.3	7.0	7.0	3.5	2.1	1.6
50	23	17	11	-	11	13	19	36	50

1.7	1.8	9.0	8.2	8.5	3.2	2.9
50	29	16	-	14	43	50

Begin with R Drop.

2.8	8.2	7.2	6.7	7.1	7.7	8.7
50	18	11	-	9	16	50

2.9	7.9	7.3	7.0	7.2	8.1	7.9
50	26	10	-	10	17	50

8.4	2.9	8.1	7.2	6.9	7.2	7.4
50	35	14	8	7	30	50

Station	+	A ✓	-	Elev.
		935.22		
10+19.4 track 2.0 mi			6.90	28.32
10 + 50				28.5
10 + 71.68 track 7.2			6.47	28.75
10 + 89.53 track			6.21	29.01
11 + 0				29.0
114				29.1
+ 50				29.3
12 + 0				29.6
+ 50				29.7
13				29.6
+ 50				29.8
14				29.1

$$\frac{7.19}{100}$$

$$\frac{6.90}{100}$$

$$\frac{6.70}{100}$$

$$\frac{7.6}{50}$$

$$\frac{7.6}{76}$$

$$\frac{6.6}{8}$$

$$\frac{6.7}{100}$$

$$\frac{6.5}{8}$$

$$\frac{5.9}{24}$$

$$\frac{7.1}{50}$$

$$\frac{6.83}{100}$$

$$\frac{6.47}{100}$$

$$\frac{6.36}{100}$$

$$\frac{6.80}{100}$$

$$\frac{6.71}{100}$$

$$\frac{6.21}{100}$$

$$\frac{6.8}{50}$$

$$\frac{6.4}{22}$$

$$\frac{6.3}{10}$$

$$\frac{6.2}{100}$$

$$\frac{6.3}{8}$$

$$\frac{6.8}{14}$$

$$\frac{6.8}{50}$$

$$\frac{3.9}{50}$$

$$\frac{3.6}{25}$$

$$\frac{5.2}{16}$$

$$\frac{6.0}{11}$$

$$\frac{6.1}{100}$$

$$\frac{6.2}{7}$$

$$\frac{5.8}{10}$$

$$\frac{2.6}{20}$$

$$\frac{2.1}{50}$$

$$\frac{3.9}{50}$$

$$\frac{5.0}{12}$$

$$\frac{6.0}{7}$$

$$\frac{5.9}{100}$$

$$\frac{6.0}{9}$$

$$\frac{5.2}{11}$$

$$\frac{2.2}{22}$$

$$\frac{2.0}{50}$$

$$\frac{3.8}{50}$$

$$\frac{4.7}{15}$$

$$\frac{5.4}{7}$$

$$\frac{5.6}{100}$$

$$\frac{5.9}{9}$$

$$\frac{2.7}{22}$$

$$\frac{2.1}{50}$$

$$- \text{Yard.}$$

$$\frac{4.3}{50}$$

$$\frac{4.7}{10}$$

$$\frac{5.6}{6}$$

$$\frac{5.8}{100}$$

$$\frac{5.5}{9}$$

$$\frac{4.0}{32}$$

$$\frac{3.5}{50}$$

$$- \text{Ent}$$

$$\frac{5.3}{50}$$

$$\frac{5.2}{10}$$

$$\frac{5.7}{7}$$

$$\frac{5.6}{100}$$

$$\frac{5.7}{9}$$

$$\frac{4.5}{15}$$

$$\frac{4.4}{23}$$

$$\frac{4.2}{50}$$

$$\frac{6.1}{50}$$

$$\frac{6.2}{27}$$

$$\frac{5.6}{10}$$

$$\frac{5.9}{7}$$

$$\frac{5.7}{100}$$

$$\frac{6.0}{8}$$

$$\frac{5.4}{11}$$

$$\frac{4.8}{17}$$

$$\frac{4.6}{24}$$

$$\frac{4.5}{50}$$

$$\frac{7.1}{50}$$

$$\frac{7.0}{36}$$

$$\frac{6.7}{17}$$

$$\frac{6.4}{9}$$

$$\frac{6.1}{100}$$

$$\frac{6.6}{9}$$

$$\frac{6.3}{11}$$

$$\frac{5.5}{14}$$

$$\frac{4.7}{23}$$

$$\frac{4.5}{50}$$

Sta. + π - Elev

935.72 ✓

1450

28.0 ✓

T.P.

0.99

929.24 ✓

6.97

928.25 ✓

15+0

26.5

+50

25.1

16+0

24.3

+50

23.4

17+0

22.8

+50

22.4

18

22.1

T.P.

2.98

924.49 ✓

7.73

921.51 ✓

+50

21.5

19

20.9

+50

20.4

20+0

19.9

Lt.

Rt.

Rt.

29

$$\frac{8.3}{50}$$

$$\frac{7.9}{30}$$

$$\frac{7.1}{15}$$

$$\frac{7.6}{8}$$

$$\frac{7.2}{10}$$

$$\frac{7.6}{10}$$

$$\frac{7.3}{13}$$

$$\frac{6.6}{15}$$

$$\frac{5.9}{23}$$

$$\frac{6.3}{50}$$

Nail in T.R.

20' Rt.

14' + 90

June - 25 - 1936

$$\frac{3.8}{50}$$

$$\frac{3.8}{53}$$

$$\frac{3.0}{15}$$

$$\frac{3.3}{9}$$

$$\frac{2.7}{10}$$

$$\frac{3.3}{10}$$

$$\frac{2.1}{19}$$

$$\frac{2.0}{50}$$

$$\frac{5.2}{50}$$

$$\frac{4.4}{16}$$

$$\frac{4.7}{10}$$

$$\frac{4.1}{11}$$

$$\frac{4.5}{11}$$

$$\frac{3.5}{18}$$

$$\frac{3.2}{50}$$

$$\frac{6.3}{50}$$

$$\frac{5.8}{15}$$

$$\frac{5.4}{9}$$

$$\frac{4.9}{12}$$

$$\frac{5.7}{12}$$

$$\frac{5.2}{19}$$

$$\frac{4.9}{26}$$

$$\frac{4.4}{50}$$

$$\frac{7.2}{50}$$

$$\frac{6.8}{15}$$

$$\frac{6.3}{9}$$

$$\frac{5.8}{13}$$

$$\frac{5.7}{13}$$

$$\frac{6.4}{18}$$

$$\frac{6.5}{25}$$

$$\frac{6.4}{50}$$

$$\frac{7.6}{50}$$

$$\frac{7.6}{18}$$

$$\frac{6.7}{9}$$

$$\frac{6.4}{12}$$

$$\frac{7.3}{12}$$

$$\frac{7.7}{22}$$

$$\frac{7.6}{50}$$

$$\frac{7.4}{50}$$

$$\frac{7.8}{18}$$

$$\frac{7.3}{10}$$

$$\frac{6.8}{11}$$

$$\frac{7.4}{11}$$

$$\frac{8.1}{17}$$

$$\frac{7.7}{23}$$

$$\frac{7.4}{50}$$

$$\frac{8.0}{50}$$

$$\frac{8.2}{18}$$

$$\frac{7.6}{10}$$

$$\frac{7.1}{10}$$

$$\frac{7.6}{10}$$

$$\frac{8.3}{17}$$

$$\frac{7.4}{20}$$

$$\frac{7.2}{50}$$

$$\frac{4.4}{50}$$

$$\frac{4.0}{20}$$

$$\frac{3.4}{14}$$

$$\frac{3.0}{12}$$

$$\frac{3.5}{12}$$

$$\frac{4.2}{18}$$

$$\frac{3.1}{20}$$

$$\frac{3.2}{50}$$

$$\frac{5.0}{50}$$

$$\frac{4.7}{20}$$

$$\frac{4.1}{11}$$

$$\frac{3.6}{11}$$

$$\frac{4.2}{11}$$

$$\frac{4.8}{16}$$

$$\frac{3.7}{24}$$

$$\frac{3.5}{50}$$

$$\frac{5.6}{50}$$

$$\frac{5.1}{20}$$

$$\frac{4.7}{11}$$

$$\frac{4.1}{10}$$

$$\frac{4.5}{10}$$

$$\frac{5.0}{16}$$

$$\frac{4.0}{28}$$

$$\frac{3.2}{50}$$

$$\frac{6.1}{50}$$

$$\frac{5.6}{15}$$

$$\frac{5.2}{10}$$

$$\frac{4.6}{10}$$

$$\frac{5.0}{10}$$

$$\frac{5.7}{16}$$

$$\frac{5.5}{23}$$

$$\frac{4.5}{24}$$

$$\frac{4.1}{50}$$

Sta.	+	π	-	Elev.
		924.49		
20+50				19.6
21+0				19.3
+50				19.2
22+0				19.1
+50				19.0
B.M.	3.10	922.51	5.08	919.41
23				18.8
+50				18.6
24				18.2
+50				17.8
25				17.2
+50				16.1
26				15.4

L

S

RT

30

$\frac{6.7}{50}$	$\frac{6.2}{18}$	$\frac{5.4}{10}$	$\frac{4.9}{-}$	$\frac{5.6}{12}$	$\frac{6.3}{16}$	$\frac{5.6}{23}$	$\frac{5.0}{28}$	$\frac{4.6}{50}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------

$\frac{7.0}{50}$	$\frac{6.9}{17}$	$\frac{5.7}{10}$	$\frac{5.2}{-}$	$\frac{6.0}{12}$	$\frac{6.8}{17}$	$\frac{6.0}{25}$	$\frac{5.4}{50}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------

$\frac{7.1}{50}$	$\frac{6.8}{17}$	$\frac{5.9}{10}$	$\frac{5.3}{-}$	$\frac{6.1}{11}$	$\frac{7.0}{19}$	$\frac{6.2}{27}$	$\frac{5.8}{50}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------

$\frac{7.0}{50}$	$\frac{6.7}{15}$	$\frac{6.1}{10}$	$\frac{5.4}{-}$	$\frac{6.0}{10}$	$\frac{6.9}{16}$	$\frac{5.8}{24}$	$\frac{5.7}{50}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------

$\frac{6.9}{50}$	$\frac{6.8}{17}$	$\frac{6.3}{11}$	$\frac{5.5}{-}$	$\frac{6.0}{11}$	$\frac{6.8}{18}$	$\frac{6.4}{22}$	$\frac{6.1}{50}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------

R.E. Spike in 12" Oak 33' - Rt. Sta. 22+28

$\frac{5.1}{50}$	$\frac{4.2}{13}$	$\frac{4.5}{12}$	$\frac{3.7}{-}$	$\frac{4.1}{11}$	$\frac{4.9}{17}$	$\frac{4.1}{21}$	$\frac{3.9}{50}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------

$\frac{5.3}{50}$		$\frac{4.3}{12}$	$\frac{4.5}{11}$	$\frac{3.9}{-}$	$\frac{4.2}{10}$	$\frac{4.2}{13}$	$\frac{5.0}{15}$	$\frac{5.0}{24}$	$\frac{4.1}{50}$
------------------	--	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------

$\frac{6.1}{50}$	$\frac{5.0}{23}$	$\frac{4.9}{12}$	$\frac{4.3}{-}$	$\frac{4.7}{12}$	$\frac{4.4}{14}$	$\frac{5.4}{19}$	$\frac{3.6}{50}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------

$\frac{6.7}{50}$		$\frac{5.1}{14}$	$\frac{5.3}{12}$	$\frac{4.7}{-}$		$\frac{5.0}{10}$	$\frac{5.7}{19}$	$\frac{3.6}{50}$
------------------	--	------------------	------------------	-----------------	--	------------------	------------------	------------------

$\frac{7.3}{50}$	$\frac{5.8}{16}$	$\frac{5.7}{11}$	$\frac{5.3}{-}$	$\frac{5.7}{10}$	$\frac{6.1}{17}$		$\frac{4.3}{50}$
------------------	------------------	------------------	-----------------	------------------	------------------	--	------------------

$\frac{8.6}{50}$	$\frac{7.6}{22}$	$\frac{6.7}{12}$	$\frac{6.4}{-}$	$\frac{6.8}{10}$	$\frac{6.9}{16}$	$\frac{5.4}{20}$	$\frac{6.3}{26}$	$\frac{6.3}{50}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------

$\frac{9.4}{50}$	$\frac{8.8}{21}$	$\frac{7.7}{11}$	$\frac{7.1}{-}$	$\frac{7.6}{9}$	$\frac{8.4}{20}$	$\frac{8.2}{50}$
------------------	------------------	------------------	-----------------	-----------------	------------------	------------------

Sta.	+	π	-	Elev.
		922.51		
B.M.	8.27	922.16	8.62	913.89
+64 50				14.7
+64 - 2 Ditch Sta. West				14.6
+70				14.5
27				14.6
+50				15.3
28				16.6
+50				18.6
T.P.	9.00	928.73	1.43	919.73
29				19.7
+50				21.1
30 + 0				22.3
+37				23.0
31 + 0				23.7

1.

2

RT

3.1

Top E of West Head Wall Co. Ditch #14 Branch #1 ^{48 ft. Water}

9.9	9.4	8.0	7.5	7.8	8.5	9.7	9.4
<u>50</u>	<u>21</u>	<u>11</u>		<u>9</u>	<u>16</u>	<u>27</u>	<u>50</u>

Cur. 1/2 fuel Dist. ^{11.5} 5 ^{13.2} 17 ^{11.2} 17 ^{8.3} 17 7.6 8.1 14 ^{11.1} 14 ^{13.1} 14 ^{11.0} 50 = E Ditch

^{Fl. line}

^{H. line}

9.6	9.7	8.1	7.7	8.1	10.3	8.7
<u>50</u>	<u>22</u>	<u>11</u>	<u>5</u>	<u>9</u>	<u>19</u>	<u>50</u>

10.4	9.9	8.1	7.6	8.1	8.4	9.7	10.0
<u>50</u>	<u>21</u>	<u>11</u>		<u>9</u>	<u>11</u>	<u>14</u>	<u>50</u>

9.5	9.0	7.3	6.9	7.4	9.6	9.4
<u>50</u>	<u>23</u>	<u>12</u>	<u>5</u>	<u>10</u>	<u>23</u>	<u>50</u>

6.5	6.8	5.9	5.6	5.8	5.6	7.0	7.4
<u>50</u>	<u>17</u>	<u>11</u>	<u>5</u>	<u>9</u>	<u>11</u>	<u>22</u>	<u>50</u>

3.9	3.3	2.5	3.9	3.6	4.2	2.8	3.2	2.9
<u>50</u>	<u>18</u>	<u>14</u>	<u>10</u>	<u>5</u>	<u>8</u>	<u>24</u>	<u>31</u>	<u>50</u>

9.7	9.7	8.5	7.7	9.4	9.0	9.3	8.8	6.6	7.0	6.5	6.8
<u>50</u>	<u>46</u>	<u>18</u>	<u>14</u>	<u>10</u>		<u>9</u>	<u>11</u>	<u>19</u>	<u>38</u>	<u>23</u>	<u>50</u>

9.8	9.0	9.0	6.9	8.1	7.6	7.9	5.3	4.7	5.8	5.7
<u>50</u>	<u>43</u>	<u>31</u>	<u>14</u>	<u>11</u>	<u>5</u>	<u>10</u>	<u>15</u>	<u>21</u>	<u>32</u>	<u>50</u>

8.8	8.1	8.3	7.1	6.3	7.1	6.4	6.7	4.9	4.9	5.8	4.5
<u>50</u>	<u>46</u>	<u>32</u>	<u>18</u>	<u>14</u>	<u>12</u>	<u>5</u>	<u>9</u>	<u>13</u>	<u>32</u>	<u>27</u>	<u>50</u>

7.9	8.2	7.0	6.2	6.5	5.7	6.0	5.0	5.9	5.0
<u>50</u>	<u>32</u>	<u>18</u>	<u>15</u>	<u>11</u>	<u>5</u>	<u>8</u>	<u>11</u>	<u>21</u>	<u>50</u>

8.7	8.0	5.3	5.0	5.4	6.4	6.0	5.6
<u>50</u>	<u>21</u>	<u>14</u>	<u>5</u>	<u>10</u>	<u>15</u>	<u>17</u>	<u>50</u>

Sta.	+	π	-	Elev.	
		928.73 ✓			
31+50				24.9	
32+0		✓		26.3	✓
T.P.	7.28	935.12	0.89		927.84 ✓
32+50				27.8	
33				29.0	
+50				29.9	
34				30.5	
+50				30.8	
35				31.1	
+50				30.9	
36				30.6	
+30				30.4	
+0	- Approx Inter.	✓		30.4	✓
T.P.	3.75	934.83 ✓	4.04		931.08 ✓

Lt.

Q

Rt.

32

$$\frac{8.0}{50}$$

$$\frac{7.5}{25}$$

$$\frac{3.4}{12}$$

$$\frac{3.8}{-}$$

$$\frac{4.1}{10}$$

$$\frac{5.1}{17}$$

$$\frac{5.1}{50}$$

$$\frac{2.4}{50}$$

$$\frac{4.1}{26}$$

$$\frac{3.8}{17}$$

$$\frac{2.8}{13}$$

$$\frac{3.1}{10}$$

$$\frac{2.5}{9}$$

$$\frac{1.4}{12}$$

$$\frac{2.2}{18}$$

$$\frac{2.4}{40}$$

$$\frac{1.9}{50}$$

$$\frac{7.5}{50}$$

$$\frac{7.2}{18}$$

$$\frac{7.9}{9}$$

$$\frac{7.3}{-}$$

$$\frac{7.6}{10}$$

$$\frac{6.2}{14}$$

$$\frac{7.2}{14}$$

$$\frac{6.0}{25}$$

$$\frac{6.8}{50}$$

$$\frac{5.3}{50}$$

$$\frac{4.8}{27}$$

$$\frac{5.5}{15}$$

$$\frac{6.7}{9}$$

$$\frac{6.1}{-}$$

$$\frac{6.4}{11}$$

$$\frac{5.3}{15}$$

$$\frac{6.8}{23}$$

$$\frac{2.8}{28}$$

$$\frac{4.7}{50}$$

$$\frac{4.8}{50}$$

$$\frac{4.8}{38}$$

$$\frac{5.0}{12}$$

$$\frac{5.7}{9}$$

$$\frac{5.2}{-}$$

$$\frac{5.5}{12}$$

$$\frac{4.4}{15}$$

$$\frac{6.6}{27}$$

$$\frac{4.0}{30}$$

$$\frac{4.0}{50}$$

$$\frac{5.2}{50}$$

$$\frac{4.3}{13}$$

$$\frac{5.1}{8}$$

$$\frac{4.6}{-}$$

$$\frac{5.0}{13}$$

$$\frac{4.4}{15}$$

$$\frac{6.0}{20}$$

$$\frac{3.6}{27}$$

$$\frac{4.5}{50}$$

$$\frac{5.1}{50}$$

$$\frac{5.9}{33}$$

$$\frac{4.3}{14}$$

$$\frac{4.7}{9}$$

$$\frac{4.3}{-}$$

$$\frac{4.8}{11}$$

$$\frac{5.7}{17}$$

$$\frac{3.8}{24}$$

$$\frac{5.3}{50}$$

$$\frac{5.6}{50}$$

$$\frac{4.0}{14}$$

$$\frac{4.0}{-}$$

$$\frac{4.5}{11}$$

$$\frac{4.0}{13}$$

$$\frac{6.0}{19}$$

$$\frac{4.7}{25}$$

$$\frac{5.0}{50}$$

$$\frac{5.1}{50}$$

$$\frac{4.1}{14}$$

$$\frac{4.5}{10}$$

$$\frac{4.2}{-}$$

$$\frac{4.7}{10}$$

$$\frac{3.6}{14}$$

$$\frac{6.7}{22}$$

$$\frac{4.7}{28}$$

$$\frac{5.5}{50}$$

$$\frac{5.7}{50}$$

$$\frac{4.6}{50}$$

$$\frac{4.5}{-}$$

$$\frac{4.7}{9}$$

$$\frac{3.7}{14}$$

$$\frac{4.3}{20}$$

$$\frac{6.5}{25}$$

$$\frac{4.5}{33}$$

$$\frac{6.0}{44}$$

58

$$\frac{5.7}{50}$$

$$\frac{4.5}{14}$$

$$\frac{5.1}{8}$$

$$\frac{4.7}{-}$$

$$\frac{4.9}{9}$$

$$\frac{5.4}{12}$$

$$\frac{4.6}{14}$$

$$\frac{6.6}{27}$$

$$\frac{6.8}{40}$$

$$\frac{5.2}{46}$$

0.1

54.4

50.8

59.2

$$\frac{5.5}{50}$$

$$\frac{4.5}{16}$$

$$\frac{5.3}{11}$$

$$\frac{4.7}{-}$$

$$\frac{5.0}{8}$$

$$\frac{4.9}{20}$$

$$\frac{5.1}{31}$$

$$\frac{6.8}{37}$$

$$\frac{0}{0}$$

hai/in Short Pole Sta. 37 Rt.

Stn. + π ✓ - Elev.

934.83

37+0

30.1

+50

29.9

38

29.9

+50

30.1

39

30.3

+50

30.4

T.P.

4.17

934.60 ✓

440

930.43 ✓

40

30.4

+50

30.2

41+0

29.9

+50

29.4

T.P.

5.50

934.77 ✓

5.33

929.27 ✓

42+0

29.3

+50

29.2

4.

E

Rt

33

$\frac{5.0}{5.0}$	$\frac{5.0}{18}$	$\frac{5.5}{15}$	$\frac{5.2}{10}$	$\frac{4.7}{1}$	$\frac{5.1}{9}$	$\frac{4.7}{17}$	$\frac{4.7}{5.0}$
-------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	-------------------

$\frac{4.7}{5.0}$	$\frac{4.7}{41}$	$\frac{4.7}{17}$	$\frac{4.8}{12}$	$\frac{5.3}{10}$	$\frac{4.9}{1}$	$\frac{5.6}{13}$	$\frac{4.7}{18}$	$\frac{5.2}{30}$	$\frac{5.2}{5.0}$
-------------------	------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	-------------------

$\frac{4.9}{5.0}$	$\frac{4.9}{33}$	$\frac{4.8}{12}$	$\frac{5.3}{10}$	$\frac{4.9}{1}$	$\frac{5.4}{12}$	$\frac{4.6}{18}$	$\frac{4.3}{34}$	$\frac{4.3}{5.0}$
-------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	-------------------

$\frac{4.7}{5.0}$	$\frac{4.2}{23}$	$\frac{4.4}{17}$	$\frac{4.8}{12}$	$\frac{5.3}{11}$	$\frac{4.7}{1}$	$\frac{5.3}{10}$	$\frac{4.3}{16}$	$\frac{4.5}{38}$	$\frac{4.5}{5.0}$
-------------------	------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	-------------------

$\frac{4.3}{5.0}$	$\frac{4.4}{28}$	$\frac{4.8}{12}$	$\frac{5.1}{11}$	$\frac{4.5}{1}$	$\frac{5.0}{12}$	$\frac{4.3}{16}$	$\frac{4.3}{32}$	$\frac{4.4}{5.0}$
-------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	-------------------

$\frac{4.8}{5.0}$	$\frac{4.3}{40}$	$\frac{4.4}{16}$	$\frac{4.9}{11}$	$\frac{4.4}{1}$	$\frac{5.1}{11}$	$\frac{4.3}{16}$	$\frac{4.4}{37}$	$\frac{4.5}{5.0}$
-------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	-------------------

$\frac{4.0}{5.0}$		$\frac{4.1}{14}$	$\frac{4.9}{10}$	$\frac{4.2}{1}$	$\frac{4.4}{11}$	$\frac{4.3}{16}$	$\frac{4.4}{41}$	$\frac{4.4}{5.0}$
-------------------	--	------------------	------------------	-----------------	------------------	------------------	------------------	-------------------

$\frac{4.3}{5.0}$		$\frac{4.1}{16}$	$\frac{4.9}{10}$	$\frac{4.4}{1}$	$\frac{5.0}{12}$	$\frac{4.2}{17}$	$\frac{4.1}{37}$	$\frac{4.0}{5.0}$
-------------------	--	------------------	------------------	-----------------	------------------	------------------	------------------	-------------------

$\frac{4.3}{5.0}$		$\frac{4.3}{18}$	$\frac{5.2}{11}$	$\frac{4.7}{1}$	$\frac{5.3}{11}$	$\frac{4.6}{19}$		$\frac{4.6}{5.0}$
-------------------	--	------------------	------------------	-----------------	------------------	------------------	--	-------------------

$\frac{3.6}{5.0}$	$\frac{4.5}{47}$	$\frac{4.9}{18}$	$\frac{5.0}{14}$	$\frac{5.6}{10}$	$\frac{5.2}{1}$	$\frac{5.8}{10}$	$\frac{5.1}{15}$	$\frac{5.7}{18}$	$\frac{5.4}{5.0}$
-------------------	------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	-------------------

$\frac{3.8}{5.0}$	$\frac{3.6}{40}$	$\frac{4.8}{29}$	$\frac{5.0}{20}$	$\frac{5.2}{14}$	$\frac{5.9}{11}$	$\frac{5.5}{1}$	$\frac{5.9}{9}$	$\frac{4.9}{14}$	$\frac{5.6}{19}$	$\frac{6.6}{34}$	$\frac{6.5}{5.0}$
-------------------	------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------	-------------------

$\frac{6.1}{5.0}$	$\frac{4.5}{27}$	$\frac{4.7}{16}$	$\frac{5.8}{10}$		$\frac{5.6}{1}$	$\frac{6.2}{9}$	$\frac{4.8}{14}$	$\frac{5.4}{14}$	$\frac{6.2}{28}$	$\frac{6.5}{5.0}$
-------------------	------------------	------------------	------------------	--	-----------------	-----------------	------------------	------------------	------------------	-------------------

Sta.	+	Σ	-	Elev.
1340		934.77 ✓		29.5
+50				29.8
44				29.8
+50				29.2
45				28.4
+50				28.2
T.P.	6.73	934.72 ✓	6.78	927.99 ✓
46				28.0
+50				27.9
47				28.0
+50				28.3
48				28.8
+50				29.5

11

12

21

34

$\frac{6.5}{50}$ $\frac{6.4}{39}$ $\frac{5.8}{28}$ $\frac{5.0}{19}$ $\frac{4.8}{13}$ $\frac{5.5}{8}$ 5.3 $\frac{6.0}{9}$ $\frac{4.5}{16}$ $\frac{4.9}{25}$ $\frac{6.5}{31}$ $\frac{6.1}{50}$

$\frac{6.1}{50}$ $\frac{6.1}{31}$ $\frac{4.2}{14}$ $\frac{4.2}{10}$ $\frac{5.2}{6}$ 5.0 $\frac{5.4}{13}$ $\frac{3.3}{20}$ $\frac{4.8}{29}$ $\frac{5.0}{50}$

$\frac{6.2}{50}$ $\frac{5.8}{27}$ $\frac{4.3}{9}$ $\frac{4.7}{6}$ $\frac{5.3}{4}$ 5.0 $\frac{5.2}{15}$ $\frac{3.7}{20}$ $\frac{4.7}{30}$ $\frac{5.1}{50}$

$\frac{6.5}{50}$ $\frac{6.5}{28}$ $\frac{5.2}{17}$ $\frac{5.2}{8}$ $\frac{5.9}{4}$ $\frac{5.6}{5}$ $\frac{5.7}{15}$ $\frac{4.5}{19}$ $\frac{4.7}{22}$ $\frac{5.4}{30}$ $\frac{5.3}{50}$

$\frac{6.6}{50}$ $\frac{6.0}{9}$ $\frac{6.7}{4}$ $\frac{6.4}{5}$ $\frac{6.5}{14}$ $\frac{5.5}{19}$ $\frac{5.6}{31}$ $\frac{5.4}{4}$ $\frac{5.7}{50}$

$\frac{7.5}{50}$ $\frac{6.5}{8}$ $\frac{7.0}{5}$ $\frac{6.6}{5}$ $\frac{6.8}{14}$ $\frac{6.0}{18}$ $\frac{6.6}{27}$ $\frac{6.1}{25}$ $\frac{6.2}{35}$ $\frac{6.0}{50}$

$\frac{7.4}{50}$ $\frac{6.5}{21}$ $\frac{6.7}{10}$ $\frac{7.1}{6}$ $\frac{6.7}{5}$ $\frac{6.9}{14}$ $\frac{6.4}{18}$ $\frac{6.3}{28}$ $\frac{6.3}{50}$

$\frac{7.3}{50}$ $\frac{7.3}{40}$ $\frac{6.7}{10}$ $\frac{7.1}{6}$ $\frac{6.8}{5}$ $\frac{7.0}{13}$ $\frac{6.7}{18}$ $\frac{6.9}{36}$ $\frac{7.0}{50}$

$\frac{6.6}{50}$ $\frac{6.5}{10}$ $\frac{7.0}{6}$ $\frac{6.7}{5}$ $\frac{7.0}{12}$ $\frac{6.6}{16}$ $\frac{6.9}{26}$ $\frac{6.9}{50}$

$\frac{5.6}{50}$ $\frac{5.7}{12}$ $\frac{6.8}{7}$ $\frac{6.4}{5}$ $\frac{6.8}{12}$ $\frac{6.0}{15}$ $\frac{6.3}{28}$ $\frac{6.4}{50}$

$\frac{5.3}{50}$ $\frac{5.3}{34}$ $\frac{5.7}{26}$ $\frac{5.7}{12}$ $\frac{6.2}{8}$ 5.9 $\frac{6.3}{11}$ $\frac{5.6}{13}$ $\frac{5.5}{50}$

$\frac{5.3}{50}$ $\frac{4.9}{14}$ $\frac{5.8}{9}$ $\frac{5.2}{5}$ $\frac{5.5}{10}$ $\frac{4.5}{15}$ $\frac{4.4}{25}$ $\frac{3.7}{50}$

Sta.	+	π ✓	-	Elev.
		934.72		
49+0		✓		30.2
T.P.	5.88	934.54	4.06	✓ 930.66
+50				30.6
50				30.7
+34				30.8
+39				30.9
+44				30.9
+64.67 E Co.				31.1
B.M.	2.83	✓ 935.89	3.48	✓ 933.08
"	4.92	✓ 935.89	4.92	✓ 930.97
50 + 82				31.0
50 + 89				30.9
51 + 0				30.8
+50				30.7

L

L

Rt.

35

$$\begin{array}{r} 5.8 \\ 50 \end{array} \quad \begin{array}{r} 5.3 \\ 29 \end{array} \quad \begin{array}{r} 4.5 \\ 22 \end{array} \quad \begin{array}{r} 4.4 \\ 13 \end{array} \quad \begin{array}{r} 5.1 \\ 9 \end{array} \quad \begin{array}{r} 4.5 \\ - \end{array} \quad \begin{array}{r} 4.9 \\ 9 \end{array} \quad \begin{array}{r} 3.6 \\ 14 \end{array} \quad \begin{array}{r} 4.4 \\ 20 \end{array} \quad \begin{array}{r} 3.1 \\ 28 \end{array} \quad \begin{array}{r} 3.2 \\ 50 \end{array}$$

$$\begin{array}{r} 7.7 \\ 50 \end{array} \quad \begin{array}{r} 7.3 \\ 33 \end{array} \quad \begin{array}{r} 5.8 \\ 23 \end{array} \quad \begin{array}{r} 5.7 \\ 13 \end{array} \quad \begin{array}{r} 6.4 \\ 10 \end{array} \quad \begin{array}{r} 5.9 \\ - \end{array} \quad \begin{array}{r} 6.3 \\ 8 \end{array} \quad \begin{array}{r} 4.8 \\ 14 \end{array} \quad \begin{array}{r} 4.2 \\ 50 \end{array}$$

$$\begin{array}{r} 7.5 \\ 50 \end{array} \quad \begin{array}{r} 6.5 \\ 30 \end{array} \quad \begin{array}{r} 5.7 \\ 23 \end{array} \quad \begin{array}{r} 5.5 \\ 15 \end{array} \quad \begin{array}{r} 6.5 \\ 12 \end{array} \quad \begin{array}{r} 5.8 \\ - \end{array} \quad \begin{array}{r} 6.1 \\ 7 \end{array} \quad \begin{array}{r} 5.0 \\ 12 \end{array} \quad \begin{array}{r} 4.8 \\ 23 \end{array} \quad \begin{array}{r} 5.0 \\ 50 \end{array}$$

$$\begin{array}{r} 7.4 \\ 50 \end{array} \quad \begin{array}{r} 6.3 \\ 29 \end{array} \quad \begin{array}{r} 5.9 \\ 17 \end{array} \quad \begin{array}{r} 6.4 \\ 12 \end{array} \quad \begin{array}{r} 5.7 \\ - \end{array} \quad \begin{array}{r} 6.2 \\ 9 \end{array} \quad \begin{array}{r} 5.7 \\ 13 \end{array} \quad \begin{array}{r} 5.3 \\ 50 \end{array}$$

$$\begin{array}{r} 7.1 \\ 50 \end{array} \quad \begin{array}{r} 6.3 \\ 29 \end{array} \quad \begin{array}{r} 6.8 \\ 18 \end{array} \quad \begin{array}{r} 5.6 \\ - \end{array} \quad \begin{array}{r} 6.4 \\ 12 \end{array} \quad \begin{array}{r} 6.5 \\ 21 \end{array} \quad \begin{array}{r} 7.1 \\ 50 \end{array} = 0.769$$

$$\text{sh/dr.} \quad \begin{array}{r} 6.7 \\ 50 \end{array} \quad \begin{array}{r} 6.4 \\ 20 \end{array} \quad \begin{array}{r} 6.8 \\ 18 \end{array} \quad \begin{array}{r} 5.6 \\ - \end{array} \quad \begin{array}{r} 6.4 \\ 12 \end{array} \quad \begin{array}{r} 5.9 \\ 21 \end{array} \quad \begin{array}{r} 5.5 \\ 50 \end{array}$$

$$\begin{array}{r} 6.1 \\ 50 \end{array} \quad \text{Torvia.} \quad \begin{array}{r} 5.4 \\ - \end{array} = d \quad \begin{array}{r} 5.2 \\ 50 \end{array}$$

Spike Top 18" TW. Stump. South East 'G' & Otter Lake Rd.

Top Stone Mon.

$$\begin{array}{r} 5.8 \\ 50 \end{array} \quad \begin{array}{r} 5.2 \\ 13 \end{array} \quad \begin{array}{r} 4.9 \\ - \end{array} \quad \begin{array}{r} 5.4 \\ 14 \end{array} \quad \begin{array}{r} 4.9 \\ 21 \end{array} \quad \begin{array}{r} 4.9 \\ 50 \end{array}$$

$$\begin{array}{r} 6.3 \\ 50 \end{array} \quad \begin{array}{r} 5.5 \\ 15 \end{array} \quad \begin{array}{r} 5.0 \\ - \end{array} \quad \begin{array}{r} 5.5 \\ 10 \end{array} \quad \begin{array}{r} 6.0 \\ 25 \end{array} \quad \begin{array}{r} 6.6 \\ 50 \end{array}$$

$$\begin{array}{r} 6.2 \\ 50 \end{array} \quad \begin{array}{r} 4.8 \\ 10 \end{array} \quad \begin{array}{r} 5.4 \\ 11 \end{array} \quad \begin{array}{r} 5.1 \\ - \end{array} \quad \begin{array}{r} 5.5 \\ 10 \end{array} \quad \begin{array}{r} 4.4 \\ 13 \end{array} \quad \begin{array}{r} 4.9 \\ 27 \end{array} \quad \begin{array}{r} 4.9 \\ 50 \end{array}$$

$$\begin{array}{r} 6.1 \\ 50 \end{array} \quad \begin{array}{r} 5.8 \\ 31 \end{array} \quad \begin{array}{r} 5.0 \\ 27 \end{array} \quad \begin{array}{r} 4.6 \\ 14 \end{array} \quad \begin{array}{r} 5.6 \\ 12 \end{array} \quad \begin{array}{r} 5.2 \\ - \end{array} \quad \begin{array}{r} 5.5 \\ 8 \end{array} \quad \begin{array}{r} 4.4 \\ 11 \end{array} \quad \begin{array}{r} 4.4 \\ 26 \end{array} \quad \begin{array}{r} 5.1 \\ 50 \end{array}$$

Sta.

+

T

-

Elev.

935.89

52+0

30.6

+50

30.7

53

30.7

+50

30.8

54

30.7

+50

30.2

55

29.0

+50

27.6

56

26.5

+50

25.9

57

24.8

T.P.

1042

925.47

4.

2

81.

36

72
 $\frac{6.3}{50}$ $\frac{5.5}{34}$ $\frac{4.1}{28}$ $\frac{4.6}{22}$ $\frac{4.4}{16}$ $\frac{5.4}{13}$ $\frac{5.3}{-}$ $\frac{5.6}{7}$ $\frac{4.5}{10}$ $\frac{4.0}{23}$ $\frac{4.9}{42}$ $\frac{4.5}{50}$

$\frac{6.8}{50}$ $\frac{5.8}{33}$ $\frac{4.2}{28}$ $\frac{4.6}{16}$ $\frac{5.5}{13}$ $\frac{5.2}{-}$ $\frac{5.5}{7}$ $\frac{4.5}{9}$ $\frac{4.2}{23}$ $\frac{4.5}{50}$

53
 $\frac{7.3}{50}$ $\frac{6.1}{35}$ $\frac{4.5}{28}$ $\frac{4.5}{16}$ $\frac{5.5}{14}$ $\frac{5.2}{-}$ $\frac{5.4}{5}$ $\frac{4.8}{8}$ $\frac{3.8}{26}$ $\frac{4.2}{43}$ $\frac{4.4}{50}$

$\frac{6.9}{50}$ $\frac{5.6}{34}$ $\frac{4.3}{28}$ $\frac{4.4}{17}$ $\frac{5.4}{15}$ $\frac{5.1}{-}$ $\frac{5.2}{6}$ $\frac{3.9}{7}$ $\frac{4.3}{22}$ $\frac{4.0}{50}$

4

74
 $\frac{6.7}{50}$ $\frac{5.7}{32}$ $\frac{4.7}{30}$ $\frac{4.1}{16}$ $\frac{5.4}{15}$ $\frac{5.2}{-}$ $\frac{5.3}{5}$ $\frac{3.9}{8}$ $\frac{3.2}{21}$ $\frac{3.8}{50}$

$\frac{6.9}{50}$ $\frac{5.8}{33}$ $\frac{4.9}{30}$ $\frac{4.6}{17}$ $\frac{5.8}{15}$ $\frac{5.7}{-}$ $\frac{5.8}{5}$ $\frac{4.5}{7}$ $\frac{3.9}{24}$ $\frac{4.3}{50}$

55
 $\frac{8.6}{50}$ $\frac{7.6}{34}$ $\frac{6.2}{29}$ $\frac{6.1}{19}$ $\frac{7.1}{16}$ $\frac{6.7}{6}$ $\frac{6.9}{-}$ $\frac{7.1}{5}$ $\frac{6.0}{6}$ $\frac{4.7}{21}$ $\frac{5.0}{24}$ $\frac{4.8}{50}$

$\frac{10.7}{50}$ $\frac{9.8}{33}$ $\frac{8.8}{29}$ $\frac{8.3}{22}$ $\frac{8.6}{16}$ $\frac{8.1}{7}$ $\frac{8.3}{-}$ $\frac{8.4}{5}$ $\frac{7.6}{6}$ $\frac{7.8}{10}$ $\frac{5.7}{17}$ $\frac{5.3}{28}$ $\frac{6.5}{50}$

56
 $\frac{12.4}{50}$ $\frac{11.4}{33}$ $\frac{10.1}{25}$ $\frac{9.7}{17}$ $\frac{9.0}{7}$ $\frac{9.4}{-}$ $\frac{9.5}{5}$ $\frac{8.9}{8}$ $\frac{9.3}{10}$ $\frac{6.2}{20}$ $\frac{5.5}{29}$ $\frac{6.4}{50}$

$\frac{12.6}{50}$ $\frac{11.4}{32}$ $\frac{10.7}{30}$ $\frac{10.4}{19}$ $\frac{9.7}{8}$ $\frac{10.0}{-}$ $\frac{10.2}{4}$ $\frac{9.3}{8}$ $\frac{6.5}{20}$ $\frac{5.2}{28}$ $\frac{6.4}{28}$ $\frac{6.5}{50}$

61
 $\frac{12.3}{50}$ $\frac{11.6}{32}$ $\frac{10.3}{24}$ $\frac{11.2}{19}$ $\frac{10.6}{7}$ $\frac{11.0}{-}$ $\frac{11.4}{4}$ $\frac{10.5}{5}$ $\frac{8.7}{12}$ $\frac{7.5}{22}$ $\frac{6.1}{27}$ $\frac{5.3}{34}$ $\frac{6.4}{45}$ $\frac{6.8}{50}$

Nail in T.P. 31 ft Sta. 86+30 9x4.47

Stn.	+	T	-	E/cv.
WS Birch Lake 6/29/26	4.46	929.93 ✓	12.97	918.96 ✓ 925.47 Normal 919.5
	5.04	930.51 ✓		925.47
57+44				23.8
58+0				23.1
+50				23.8
T.P.	5.41	930.54 ✓	5.41	925.10 ✓
59				24.9
+50				25.0
60+0				25.2
+50				25.4
61+0				25.7
+50				26.1
62				26.7
	8.91	936.08 ✓	3.31	927.17 ✓

July 1-1936

ERR 6.5 7.1 8.9 8.0 6.5 6.8 7.1 6.5 6.7 6.8 3.8 2.0 0.7 0.5
 88 70 63 41 76 21 17 7 5 12 33 37 50
 54124

54141 6.8 6.2 6.6 6.8 7.4 7.5 6.7 7.1 4.1 3.6 1.6
 52 36 22 8 5 9 16 33 44 50

6.6 6.7 8.9 6.7 6.0 6.0 6.7 7.4 8.0 7.4 5.3 3.9
 50 40 32 25 18 8 7 11 25 42 50

8.2 6.9 7.7 6.6 5.9 5.6 6.1 7.8 7.2 6.0 4.7
 50 42 26 16 8 10 19 32 37 50

8.5 7.1 6.7 7.3 7.7 6.4 5.9 5.5 6.0 7.7 7.1 5.6 4.2
 50 42 35 29 16 12 7 13 19 30 41 50

WE 11.6 10.0 8.6 7.3 6.0 6.9 6.1 5.3 6.0 7.6 6.6 4.0
 104 75 50 45 21 15 13 13 19 28 50

WE 11.6 10.1 7.4 6.0 5.6 5.1 5.1 5.8 8.4 5.8 3.8
 104 75 50 37 22 17 16 11 18 25 50

WE 11.6 9.8 7.1 8.1 8.2 5.2 4.8 5.3 7.0 7.0 5.2 3.0
 104 60 47 29 21 13 11 16 23 28 50

WE 11.6 9.9 8.3 7.5 7.9 4.8 4.4 4.8 6.3 6.0 4.5 2.4
 94 65 50 33 21 13 11 18 23 27 50

WE 11.6 9.3 8.9 7.0 4.2 3.8 4.0 4.9 4.7 4.0 1.3
 94 65 50 22 11 10 13 18 24 50

High R. Stp. RT. 62475

Sta. + π - Elev.

936.08

62+50 27.3

63 28.2

+50 29.2

64 30.1

+50 = approx E Birch Lake Ave. 30.7

B.M. 3.23 936.08 3.23 937.85

65 30.3

+50 29.1

T.P. 3.55 932.25 7.38 928.70

66 28.7

+50 28.3

67 27.9

+50 27.6

68 27.5

Lt.

t

Rt.

38

WE.	$\frac{12.2}{82}$	$\frac{15.5}{60}$	$\frac{12.7}{43}$	$\frac{11.4}{23}$	$\frac{11.4}{17}$	$\frac{9.4}{11}$	$\frac{8.8}{-}$	$\frac{9.2}{11}$	$\frac{10.9}{15}$	$\frac{10.7}{20}$	$\frac{11.1}{30}$	$\frac{5.1}{50}$
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WE.	$\frac{12.2}{80}$	$\frac{15.3}{60}$	$\frac{12.2}{43}$	$\frac{11.5}{26}$	$\frac{10.4}{17}$	$\frac{8.5}{12}$	$\frac{7.9}{-}$	$\frac{8.3}{11}$	$\frac{9.7}{14}$	$\frac{9.7}{20}$	$\frac{6.3}{26}$	$\frac{5.2}{50}$
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WE.	$\frac{12.2}{80}$	$\frac{15.7}{65}$	$\frac{13.8}{50}$	$\frac{11.4}{35}$	$\frac{10.2}{18}$	$\frac{7.5}{12}$	$\frac{6.9}{-}$	$\frac{7.4}{11}$	$\frac{9.1}{14}$	$\frac{8.9}{20}$	$\frac{5.8}{25}$	$\frac{4.8}{50}$
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WE.	$\frac{17.2}{81}$	$\frac{15.5}{60}$	$\frac{12.5}{45}$	$\frac{9.2}{28}$	$\frac{6.6}{11}$	$\frac{6.0}{-}$	$\frac{6.2}{14}$	$\frac{6.2}{17}$	$\frac{5.2}{31}$	$\frac{4.8}{50}$
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WE.	$\frac{17.2}{78}$	$\frac{16.1}{60}$	$\frac{13.3}{50}$	$\frac{10.5}{39}$	$\frac{9.7}{28}$	$\frac{7.5}{15}$	$\frac{6.2}{11}$	$\frac{5.4}{-}$	$\frac{5.2}{10}$	$\frac{5.0}{50}$
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R.R. spike in T.P. 60' Rd. Sdr. 64440

WE.	$\frac{17.2}{70}$	$\frac{14.0}{50}$	$\frac{11.5}{37}$	$\frac{9.1}{23}$	$\frac{6.5}{14}$	$\frac{5.8}{-}$	$\frac{6.5}{16}$	$\frac{6.4}{21}$	$\frac{5.2}{28}$	$\frac{5.0}{50}$
-----	-------------------	-------------------	-------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------

WE.	$\frac{17.2}{73}$	$\frac{15.2}{60}$	$\frac{11.6}{32}$	$\frac{7.2}{16}$	$\frac{7.0}{-}$	$\frac{7.8}{13}$	$\frac{5.8}{17}$	$\frac{5.7}{50}$
-----	-------------------	-------------------	-------------------	------------------	-----------------	------------------	------------------	------------------

WE.	$\frac{13.4}{70}$	$\frac{12.4}{50}$	$\frac{10.1}{38}$	$\frac{7.6}{24}$	$\frac{3.8}{13}$	$\frac{3.6}{-}$	$\frac{4.3}{14}$	$\frac{2.8}{18}$	$\frac{2.5}{34}$	$\frac{2.5}{50}$
-----	-------------------	-------------------	-------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------

WE.	$\frac{13.4}{70}$	$\frac{12.0}{50}$	$\frac{9.7}{36}$	$\frac{7.6}{23}$	$\frac{4.5}{14}$	$\frac{4.0}{-}$	$\frac{4.7}{15}$	$\frac{3.0}{19}$	$\frac{2.5}{35}$	$\frac{2.0}{50}$
-----	-------------------	-------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------

WE.	$\frac{13.4}{71}$	$\frac{11.8}{50}$	$\frac{9.0}{31}$	$\frac{4.8}{20}$	$\frac{4.7}{13}$	$\frac{4.4}{-}$	$\frac{5.1}{17}$	$\frac{2.6}{21}$	$\frac{2.0}{33}$	$\frac{1.6}{50}$
-----	-------------------	-------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------

WE.	$\frac{13.4}{70}$	$\frac{11.8}{50}$	$\frac{10.2}{42}$	$\frac{8.0}{36}$	$\frac{5.1}{19}$	$\frac{4.2}{13}$	$\frac{4.9}{12}$	$\frac{4.7}{-}$	$\frac{5.2}{11}$	$\frac{4.6}{17}$	$\frac{2.1}{21}$	$\frac{2.0}{33}$	$\frac{1.6}{50}$
-----	-------------------	-------------------	-------------------	------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------

WE.	$\frac{13.4}{69}$	$\frac{11.8}{50}$	$\frac{8.8}{42}$	$\frac{7.0}{31}$	$\frac{5.0}{26}$	$\frac{4.3}{15}$	$\frac{5.3}{12}$	$\frac{4.8}{-}$	$\frac{5.1}{12}$	$\frac{2.6}{18}$	$\frac{1.8}{38}$	$\frac{1.4}{50}$
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4.5-4.7
50' 4.7

Sta.	+	π	-	Elev.
		93275		
68+50				27.1
69+0				26.6
T.P.	3.18	929.22 ✓	6.21	226.04 ✓
+50				26.0
70				25.4
+50				25.1
71				25.0
+50				24.7
72				24.4
+75				24.5
+50				24.9
73				25.2
+96				24.97
+55				24.92
B.M.			6.01	923.21 ✓

Lt.

E

Rt.

39

20E / $\frac{13.4}{67}$ $\frac{100}{44}$ $\frac{7.5}{34}$ $\frac{6.0}{24}$ $\frac{4.5}{13}$ $\frac{5.6}{11}$ $\frac{5.2}{10}$ $\frac{5.4}{10}$ $\frac{2.8}{15}$ $\frac{2.1}{24}$ $\frac{1.4}{50}$

20E / $\frac{13.4}{65}$ $\frac{12.4}{50}$ $\frac{7.5}{30}$ $\frac{5.7}{17}$ $\frac{4.8}{11}$ $\frac{6.1}{9}$ $\frac{5.7}{15}$ $\frac{6.0}{15}$ $\frac{2.9}{20}$ $\frac{1.8}{30}$ $\frac{1.4}{50}$

20E / $\frac{10.3}{60}$ $\frac{9.0}{50}$ $\frac{6.8}{36}$ $\frac{4.7}{24}$ $\frac{3.7}{18}$ $\frac{3.3}{11}$ $\frac{3.7}{9}$ $\frac{3.2}{15}$ $\frac{3.6}{15}$ $\frac{1.9}{23}$ $\frac{0.0}{35}$ $\frac{+0.7}{50}$

20E / $\frac{10.3}{55}$ $\frac{9.7}{50}$ $\frac{8.5}{38}$ $\frac{6.2}{26}$ $\frac{5.0}{18}$ $\frac{4.4}{11}$ $\frac{3.8}{17}$ $\frac{4.1}{17}$ $\frac{2.4}{32}$ $\frac{1.6}{50}$

20E / $\frac{10.3}{48}$ $\frac{10.1}{47}$ $\frac{7.9}{26}$ $\frac{6.0}{19}$ $\frac{4.8}{14}$ $\frac{4.1}{13}$ $\frac{4.6}{13}$ $\frac{5.0}{23}$ $\frac{2.5}{50}$

20E / $\frac{10.3}{43}$ $\frac{10.3}{42}$ $\frac{8.8}{27}$ $\frac{7.6}{19}$ $\frac{4.7}{9}$ $\frac{4.1}{13}$ $\frac{4.5}{13}$ $\frac{5.7}{20}$ $\frac{6.4}{36}$ $\frac{6.3}{50}$

July 1-1986 20E / $\frac{10.30}{38}$ $\frac{8.2}{15}$ $\frac{5.2}{10}$ $\frac{4.5}{10}$ $\frac{4.3}{6}$ $\frac{4.8}{18}$ $\frac{6.5}{25}$ $\frac{6.7}{50}$

20E / $\frac{10.3}{36}$ $\frac{8.7}{26}$ $\frac{7.6}{18}$ $\frac{5.7}{12}$ $\frac{4.8}{12}$ $\frac{5.0}{12}$ $\frac{5.7}{17}$ $\frac{6.8}{35}$ $\frac{6.4}{19}$ $\frac{5.4}{68}$ $\frac{7.30}{76}$ = Edge Pass.

20E / $\frac{10.3}{34}$ $\frac{9.0}{27}$ $\frac{7.1}{19}$ $\frac{5.6}{14}$ $\frac{4.7}{23}$ $\frac{4.7}{23}$ $\frac{3.55}{48}$ = Edge Pass.

20E / $\frac{9.80}{20}$ = Fl. 24" CONC. $\frac{7.9}{30}$ $\frac{7.74}{69}$

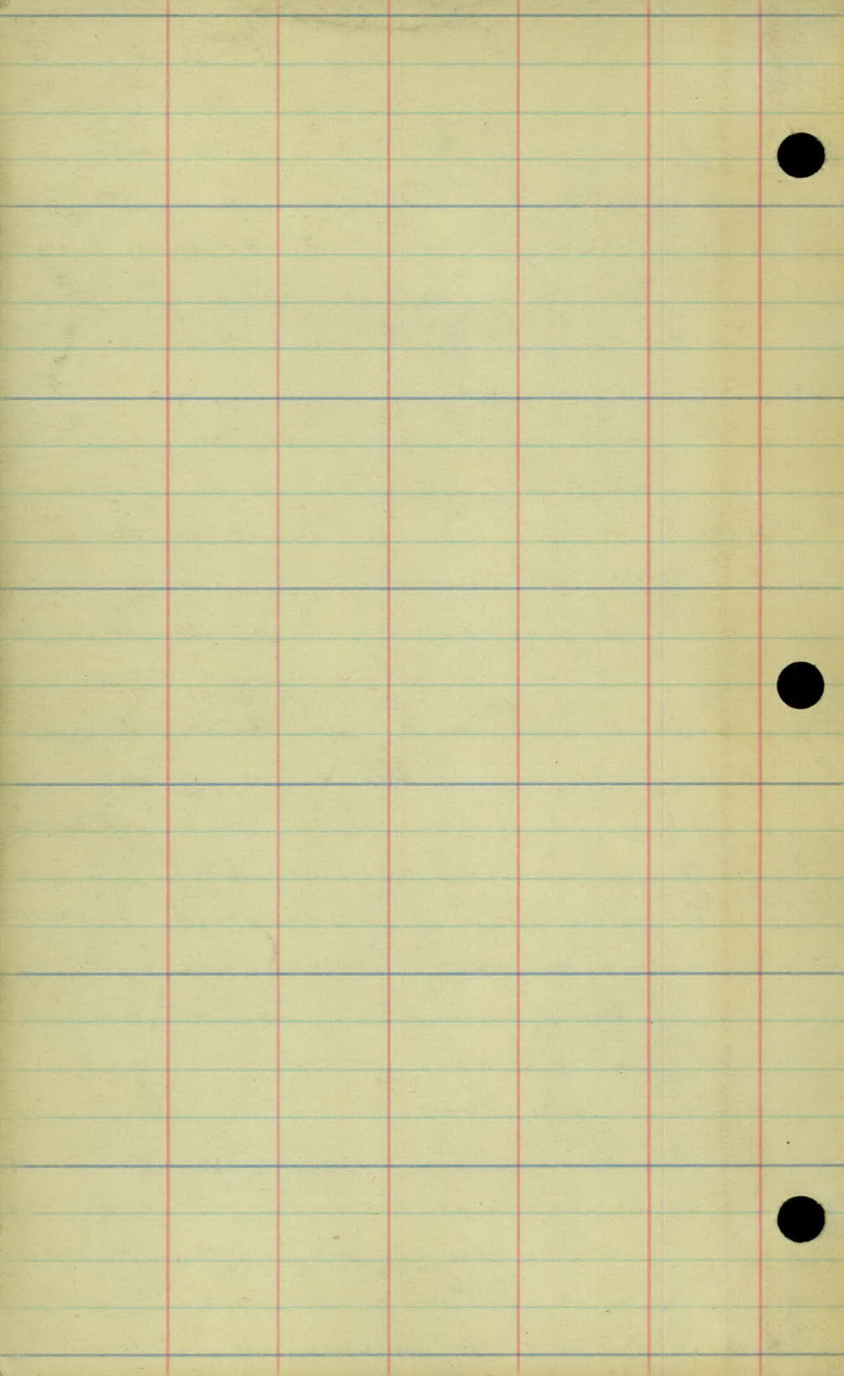
20E / $\frac{10.3}{51}$ $\frac{9.3}{41}$ $\frac{8.5}{31}$ $\frac{7.8}{24}$ $\frac{5.2}{14}$ $\frac{4.3}{24}$ $\frac{3.93}{24}$ = Edge Pass.

20E / $\frac{10.3}{52}$ $\frac{9.0}{38}$ $\frac{4.3}{12}$ $\frac{3.98}{10}$ $\frac{4.60}{10}$ $\frac{4.74}{22}$ = Edge Pass.

20E / $\frac{10.3}{53}$ $\frac{9.3}{37}$ $\frac{8.0}{22}$ $\frac{3.9}{12}$ $\frac{4.04}{8.3}$ $\frac{4.75}{13.8}$ = ✓ ✓

20E / $\frac{10.3}{57}$ $\frac{9.5}{30}$ $\frac{8.6}{23}$ $\frac{4.1}{15}$ $\frac{4.08}{9.2}$ $\frac{4.30}{11.7}$ ✓ ✓

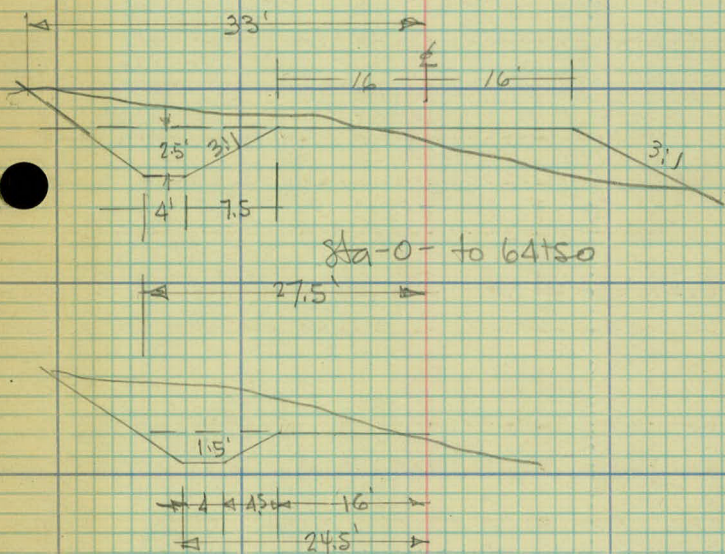
Spike in R.P. @ Pump Ho. Elev. 922.76



Otter Lake Rd.

Schuneman Rd. to Birch Lake Blvd.

Slope stakes



Sta.	+	π	-	Grade
B.M.	4.09	939.92		935.83

-0+25

0+0				933.2
-----	--	--	--	-------

0+30	11.4			33.6
------	------	--	--	------

0+50				33.9
------	--	--	--	------

1+0				34.6
-----	--	--	--	------

+50	⊙			35.3
-----	---	--	--	------

2+0				35.9
-----	--	--	--	------

+50				36.4
-----	--	--	--	------

3				36.7
---	--	--	--	------

+50				36.9
-----	--	--	--	------

T.P.	7.76	943.76	3.42	936.50
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4				36.9
---	--	--	--	------

+20				36.9
-----	--	--	--	------

R.R. spike Top 30' Shump 75' Rt. Sta. - 0+62

6.7

69

$$6.3 \quad 33 \overline{) 15.6} \\ \underline{+0.7}$$

$$\frac{6.4}{-0.1}$$

$$6.0 \quad 33 \overline{) 15.6} \\ \underline{+0.4}$$

$$\frac{6.1}{-0.1}$$

$$5.3 \quad 33 \overline{) 15.2} \\ \underline{+0.1}$$

$$\frac{5.4}{-0.1}$$

$$2.21 / 33$$

$$2.19 / 33$$

$$4.6 \quad 33 \overline{) 15.0} \\ \underline{+2.1}$$

$$\frac{5.1}{-0.5}$$

$$1.8 / 33$$

$$4.0 \quad 33 \overline{) 14.0} \\ \underline{+2.5}$$

$$\frac{5.0}{-1.0}$$

$$2.0 / 33$$

$$3.5 \quad 33 \overline{) 14.2} \\ \underline{+1.8}$$

$$\frac{4.6}{-1.1}$$

$$1.3 / 33$$

$$3.2 \quad 33 \overline{) 12.0} \\ \underline{+1.2}$$

$$\frac{4.1}{-0.9}$$

$$1.2 / 33$$

$$3.0 \quad 33 \overline{) 12.0} \\ \underline{+1.7}$$

$$\frac{3.7}{-0.7}$$

$$1.5 / 33$$

$$6.9 \quad 33 \overline{) 21.6} \\ \underline{+4.3}$$

$$\frac{7.3}{-0.4}$$

$$1.0 / 33$$

$$6.9 \quad 33 \overline{) 21.0} \\ \underline{+1.0}$$

943.76

4+40

36.9

5

36.5

+50

36.1

6

35.5

+50

34.8

938.9

7

33.9

B.M.

5.96

938.87

10.84

932.92

+50

32.9

8

31.8

(+50)

30.7

8+92

29.8

9+08

29.5

9+50

28.7

$$6.9 \quad 330 \overline{) 3.0} \quad \begin{array}{r} 7.2 \\ -0.3 \\ \hline \end{array}$$

$$\frac{8.9}{-2.0} / 22.0$$

$$7.3 \quad 33 \overline{) 4.8} \quad \begin{array}{r} 7.1 \\ -0.4 \\ \hline \end{array}$$

$$\frac{8.3}{-7.0} / 19.0 \quad \frac{7.8}{100.0} / 31$$

$$7.7 \quad 33 \overline{) 7.4} \quad \begin{array}{r} 8.5 \\ -0.8 \\ \hline \end{array}$$

$$\frac{9.2}{-1.5} / 20.5 \quad \frac{10.2}{20.00} / 30$$

$$8.3 \quad \begin{array}{r} 9.2 \\ -0.9 \\ \hline \end{array}$$

$$\frac{9.8}{-1.6} / 20.8 \quad \frac{10.4}{100.4} / 33$$

$$9.0 \quad \begin{array}{r} 9.8 \\ -0.8 \\ \hline \end{array}$$

$$\frac{10.2}{-1.2} / 19.6 \quad \frac{11.0}{100.5} / 33$$

$$5.0 \quad 330 \overline{) 4.1} \quad \begin{array}{r} 6.0 \\ -1.0 \\ \hline \end{array}$$

$$\frac{5.1}{102.4} / 33$$

(932.91) Spike 14" Oak 75' Et. Sta. 7+05

$$6.0 \quad 33 \overline{) 4.9} \quad \begin{array}{r} 7.1 \\ -1.0 \\ \hline \end{array}$$

$$\frac{5.3}{+0.7} / 33$$

$$7.1 \quad 33 \overline{) 3.8} \quad \begin{array}{r} 8.3 \\ -1.2 \\ \hline \end{array}$$

$$\frac{4.3}{+2.8} / 33$$

$$8.2 \quad 33 \overline{) 4.5} \quad \begin{array}{r} 9.4 \\ -1.2 \\ \hline \end{array}$$

$$\frac{4.3}{+0.9} / 33$$

$$9.1 \quad 33 \overline{) 3.7} \quad \begin{array}{r} 10.2 \\ -1.1 \\ \hline \end{array}$$

$$\frac{5.5}{+4.6} / 33$$

$$9.3 \quad \begin{array}{r} 11.8 \\ 33 \overline{) 11.8} \end{array} \quad \begin{array}{r} 11.8 \\ 33 \overline{) 11.8} \end{array} \quad \begin{array}{r} 10.4 \\ -1.1 \\ \hline \end{array}$$

$$\frac{11.8}{-1.8} / 23.5 \quad \frac{11.8}{100.0} / 33$$

$$10.2 \quad \begin{array}{r} 11.6 \\ 33 \overline{) 11.6} \end{array} \quad \begin{array}{r} 10.7 \\ -0.5 \\ \hline \end{array}$$

$$\frac{11.6}{-1.4} / 20.2$$

938.87

1040

28.3

T.P.

7.22

935.56

10.53

928.34

+50

28.2

+

1140

28.6

+14

28.8

+50

29.1

1240

29.4

+80

x

29.5

x

13

29.4

+50

29.2

14

28.7

T.P.

1.10

932.83

3.80

931.73

$$\begin{array}{r}
 106 \\
 19.6 \overline{) 11.8} \\
 \underline{-1.2} \\
 74
 \end{array}
 \qquad
 \begin{array}{r}
 978.7 \\
 106 \\
 \underline{10.4} \\
 70
 \end{array}
 \qquad
 \begin{array}{r}
 106 \\
 \underline{16} \\
 69 \\
 10.5 \overline{) 16}
 \end{array}$$

$$\begin{array}{r}
 7.0 \\
 2.0 \\
 \underline{16} \\
 66 \\
 10.4 \overline{) 7.0} \\
 \underline{8.0} \\
 15
 \end{array}$$

$$\begin{array}{r}
 68 \\
 33 \overline{) 38} \\
 \underline{+20} \\
 65 \\
 10.3 \overline{) 3.0} \\
 \underline{+3.8} \\
 33
 \end{array}$$

$$\begin{array}{r}
 6.5 \\
 33 \overline{) 3.7} \\
 \underline{+2.8} \\
 63 \\
 10.2 \overline{) 2.7} \\
 \underline{+3.8} \\
 33
 \end{array}$$

$$\begin{array}{r}
 6.2 \\
 33 \overline{) 4.2} \\
 \underline{+2.0} \\
 60 \\
 10.2 \overline{) 2.8} \\
 \underline{+3.4} \\
 33
 \end{array}$$

$$\begin{array}{r}
 \times 6.1 \\
 33 \overline{) 4.5} \\
 \underline{+1.6}
 \end{array}$$

$$\begin{array}{r}
 6.2 \\
 33 \overline{) 5.8} \\
 \underline{+2.4} \\
 61 \\
 10.1 \overline{) 4.7} \\
 \underline{+1.5} \\
 33
 \end{array}$$

$$\begin{array}{r}
 6.4 \\
 33 \overline{) 6.6} \\
 \underline{+2.3} \\
 60 \\
 10.4 \overline{) 4.9} \\
 \underline{+1.5} \\
 33
 \end{array}$$

$$\begin{array}{r}
 6.9 \\
 33 \overline{) 7.4} \\
 \underline{+2.0} \\
 65 \\
 10.4 \overline{) 5.3} \\
 \underline{+1.6} \\
 33
 \end{array}$$

Nail in T.R. at Sta. 12+86

932.83

14+50

28.0

15+0

27.2

+50

26.3

16

25.3

3.42

926.91

9.34

977.49

+50

24.5

17

23.6

+50

23.0

18

22.3

+50

21.9

19

21.4

+50

21.1

20

20.9

$$4.8 \overset{7.3}{-}$$

$$33 \overline{) \frac{5.7}{10.6}}$$

$$\frac{4.9}{-0.1}$$

$$\frac{4.1}{+0.7} / 33$$

$$5.6 \overset{9.1}{-}$$

$$33 \overline{) \frac{7.7}{10.4}}$$

$$\frac{6.3}{-0.7}$$

$$\frac{5.6}{-7.5} / 33$$

$$6.5 \overset{9.0}{-}$$

$$33 \overline{) \frac{8.8}{10.2}}$$

$$\frac{7.7}{-1.2}$$

$$\frac{7.0}{-2.0} / 33$$

$$7.5 \overset{10.0}{-}$$

$$33 \overline{) \frac{10.0}{10.0}} \quad 23.2 \overline{) \frac{9.9}{2.4}}$$

$$\frac{8.5}{-1.0}$$

$$\frac{8.4}{-10.6} / 33$$

$$2.4 \overset{4.9}{-}$$

$$33 \overline{) \frac{5.0}{10.0}} \quad 23.2 \overline{) \frac{4.8}{2.4}}$$

$$\frac{3.4}{-1.0}$$

$$\frac{3.9}{-10.0} / 33$$

$$3.3 \overset{5.8}{-}$$

$$33 \overline{) \frac{5.1}{10.7}}$$

$$\frac{4.1}{-0.8}$$

$$\frac{5.3}{-10.5} / 33$$

$$3.9 \overset{6.4}{-}$$

$$33 \overline{) \frac{5.0}{10.4}}$$

$$\frac{4.5}{-0.6}$$

$$\frac{5.1}{-10.3} / 33$$

$$4.6 \overset{7.1}{-}$$

$$33 \overline{) \frac{8.6}{10.5}}$$

$$\frac{4.8}{-0.2}$$

$$\frac{5.1}{-10.2} / 33$$

$$5.0 \overset{7.5}{-}$$

$$33 \overline{) \frac{6.4}{10.1}}$$

$$\frac{5.4}{-0.4}$$

$$\frac{5.6}{-10.9} / 33$$

$$5.5 \overset{8.0}{-}$$

$$33 \overline{) \frac{7.2}{10.8}}$$

$$\frac{6.0}{-0.5}$$

$$\frac{5.6}{-10.4} / 33$$

$$5.8 \overset{8.3}{-}$$

$$33 \overline{) \frac{7.6}{10.7}}$$

$$\frac{6.5}{-0.7}$$

$$\frac{6.2}{-10.1} / 33$$

$$6.0 \overset{8.5}{-}$$

$$33 \overline{) \frac{8.1}{10.4}}$$

$$\frac{7.0}{-1.0}$$

$$\frac{6.8}{-1.7} / 33$$

92691

T.P.

923.43

6.31

920.60

20+50

20.7

21+0

20.5

+50

20.3

22

20.1

B.M.

4.02

92343

+50

19.9

23

19.5

+50

19.1

24

18.6

+50

18.1

25

17.4

+50

16.8

Nor/10 T.P. 20+23

$$2.7 \begin{array}{r} 5.2 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 5.2 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 5.2 \\ 33 \overline{) 1.00} \end{array}$$

$$\begin{array}{r} 38 \\ -1.1 \end{array}$$

$$\begin{array}{r} 4.0 \\ 101.2 \overline{) 299} \end{array} 2:1$$

$$2.9 \begin{array}{r} 5.6 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 5.6 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 5.6 \\ 33 \overline{) 1.00} \end{array}$$

$$\begin{array}{r} 4.1 \\ -1.2 \end{array}$$

$$\begin{array}{r} 4.8 \\ 100.6 \overline{) 787} \end{array} 2:1$$

$$3.1 \begin{array}{r} 5.8 \\ 24 \overline{) 1.00} \end{array} \begin{array}{r} 5.8 \\ 24 \overline{) 1.00} \end{array} \begin{array}{r} 5.8 \\ 24 \overline{) 1.00} \end{array}$$

$$\begin{array}{r} 4.2 \\ -1.1 \end{array}$$

$$\begin{array}{r} 5.2 \\ 100.4 \overline{) 283} \end{array} 2:1$$

$$3.3 \begin{array}{r} 5.5 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 5.5 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 5.5 \\ 33 \overline{) 1.00} \end{array}$$

$$\begin{array}{r} 4.4 \\ -1.1 \end{array}$$

$$\begin{array}{r} 4.9 \\ 100.6 \overline{) 297} \end{array} 2:1$$

(919.41) Spike in 12" Oak 33' Rt. 22+38

$$3.5 \begin{array}{r} 5.4 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 5.4 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 5.4 \\ 33 \overline{) 1.00} \end{array}$$

$$\begin{array}{r} 4.5 \\ -1.0 \end{array}$$

$$\begin{array}{r} 5.5 \\ 100.5 \overline{) 285} \end{array} 2:1$$

$$3.9 \begin{array}{r} 5.6 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 5.6 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 5.6 \\ 33 \overline{) 1.00} \end{array}$$

$$\begin{array}{r} 4.6 \\ -0.7 \end{array}$$

$$\begin{array}{r} 5.1 \\ 101.3 \overline{) 33} \end{array}$$

$$4.3 \begin{array}{r} 5.9 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 5.9 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 5.9 \\ 33 \overline{) 1.00} \end{array}$$

$$\begin{array}{r} 4.8 \\ -0.5 \end{array}$$

$$\begin{array}{r} 5.8 \\ 101.0 \overline{) 33} \end{array}$$

$$4.8 \begin{array}{r} 6.4 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 6.4 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 6.4 \\ 33 \overline{) 1.00} \end{array}$$

$$\begin{array}{r} 5.2 \\ -0.4 \end{array}$$

$$\begin{array}{r} 5.7 \\ 101.6 \overline{) 33} \end{array}$$

$$5.3 \begin{array}{r} 6.9 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 6.9 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 6.9 \\ 33 \overline{) 1.00} \end{array}$$

$$\begin{array}{r} 5.6 \\ -0.3 \end{array}$$

$$\begin{array}{r} 5.9 \\ 101.9 \overline{) 33} \end{array}$$

$$6.0 \begin{array}{r} 7.8 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 7.8 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 7.8 \\ 33 \overline{) 1.00} \end{array}$$

$$\begin{array}{r} 6.2 \\ -0.2 \end{array}$$

$$\begin{array}{r} 6.2 \\ 102.3 \overline{) 33} \end{array}$$

$$6.6 \begin{array}{r} 8.6 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 8.6 \\ 33 \overline{) 1.00} \end{array} \begin{array}{r} 8.6 \\ 33 \overline{) 1.00} \end{array}$$

$$\begin{array}{r} 7.3 \\ -0.7 \end{array}$$

$$\begin{array}{r} 7.4 \\ 101.7 \overline{) 33} \end{array}$$

92343

B.M.

11.99

925.88

9.54

913.89

76.0

16.5

+50

16.4

+64

16.4

+70

16.4

27

16.6

B.M.

+50

17.0

28

17.7

+50

18.6

29

19.8

+50

21.1

30

22.4

+37.36

~~EC~~ 20.17

to 40
to 20
to 10
to 64

23.6

$$9.4 \quad 1.9$$

$$24.1 / -2.7$$

$$105 / -1.1$$

$$-2.5 / 23.5 \quad 11.8 / 20.0 / 33$$

$$9.5 \quad 28.0 / 13.5 / -4.0$$

$$113 / -1.8$$

$$13.5 / 28.0$$

$$9.5$$

$$9.5$$

$$9.3 \quad 29.5 / 13.8 / -4.5$$

$$11.4 / -2.1$$

$$13.7 / -4.4 / 29.2$$

(913.89) Top L. W. H. W. 76 + 60

$$8.9 \quad 28.6 / 13.1 / -4.2$$

$$10.6 / -1.7$$

$$13.1 / -4.2 / 28.6$$

$$8.2 \quad 10.7 \quad 23 / 10.7 \quad 24 / 10.4 / -2.2$$

$$9.3 / -1.1$$

$$10.6 / -2.4 / 23.2 \quad 10.8 / 20.0 / 33$$

$$7.3 \quad 23 / 2.7 / 2.1$$

$$7.3 / 0.0$$

$$6.4 / 2.9 / 33$$

$$6.1 \quad 33 / 6.5 / 2.1$$

$$6.2 / -0.1$$

$$4.4 / 11.7 / 33$$

$$4.8 \quad 33 / 5.9 / 1.4$$

$$4.7 / +0.1$$

$$2.7 / 12.1 / 33$$

$$2.5 \quad 6.0$$

$$33 \quad 5.1 / 16.0.9$$

$$3.5 / 2.0$$

$$2.1 / 11.4 / 33$$

$$2.5 \quad 5.0$$

$$33 \quad 5.1 / 2.4 / 12.1$$

$$2.8 / -0.3$$

$$2.7 / 12.1 / 33$$

	T	π	-	Grade	
Sta.		925.88			
T.P.	9.45	932.50	2.83		923.05
3140		$\begin{smallmatrix} -0.2 & 10.2 \\ \text{of} & 10.5 \end{smallmatrix}$		24.8	
(132.39 P.C. 70)		± 0.4 to 0			
+50		-0.5 to 0.5		25.9	
32		-0.5 to 0.5		26.8	
					Ditch Rd.
+50		-0.5 to 0.5		27.7	7.3
33		-0.5 to 0.5		28.5	6.5
+50		-0.5 to 0.5		29.1	5.9
T.P.	4.98	935.45	2.03		930.47
34		-0.5 to 0.5		29.7	7.4
+50		-0.5 to 0.5		30.2	7.9
35		-0.5 to 0.5		30.6	7.5
Eq. 1 $\begin{smallmatrix} 35+11.79 = \text{PIT} \\ 35+10.66 \end{smallmatrix}$					
+50		-0.2 to 0.2		30.9	7.2
36		-0.0 to 0		31.1	6.9

14.

15.

151.

mai 12 2013 27.26

7.9	7.5	0.8	11.8	87	10.0	9.8
7.7	16.2	27.7	2.9	-11.0	-2.5	20.4/33

7.1	6.1	28.0	11.1	7.7	8.8	8.8
6.6	9.1	-4.0	-11.1	-2.7	24.1	20.3/33

Ditch		6.7	6.7	6.2	5.6	6.1
6.2	5.2	28.5	20.5	16	-0.5	21/33
5.7					-0.4	17.2

5.3	4.3	32.1	5.0	4.7	3.8	3.8
4.8		22.3	10.1	10.1	11.0	33

4.5	3.5	33	2.5	3.5	1.6	1.6
4.0		11.5	10.5	10.5	2.3	33

3.9	2.9	33	2.3	2.5	1.3	1.3
3.4		11.1	10.9	10.9	12.1	33

5.4	4.4	33	4.8	5.0	4.9	4.9
4.9		10.1	0.1	0.1	2.5	33

5.9	4.9	33	5.5	4.7	5.1	5.1
5.4		2.4	10.7	10.7	10.3	33

5.5	4.5	33	5.7	4.4	5.4	5.4
5.0		1.8	10.6	10.6	2.1	33

4.9	4.5	33	5.5	4.5	5.6	5.6
4.7		11.7	10.2	10.2	1.6	33

4.4		33	5.8	4.8	5.2	5.2
		1.1	0.4	0.4	1.7	33

935.45

36 + 30

31.1

69

T.P.

5.44

934.64

6.75

929.20

+ 70

31.1

37

31.2

+ 50

31.1

38

31.1

+ 50

31.1

39

31.0

+ 50

31.0

40

30.9

+ 50

30.9

41

30.8

T.P.

3.70

934.75

4.09

930.55

+ 50

30.7

$\frac{5.1}{4.4}$
 $33 \frac{5.9}{10.0}$
 $\frac{5.1}{-0.7}$
 $\frac{5.8}{10.11/33}$

Top South end Culv. at Sta - 36+35

 $\frac{6.0}{3.5}$
 $33 \frac{4.7}{10.1.3}$
 $\frac{4.3}{-0.8}$
 $\frac{5.9}{3.4}$
 $33 \frac{4.9}{10.1.0}$
 $\frac{4.5}{-1.1}$
 $\frac{5.0}{10.09/33}$
 $\frac{6.0}{3.5}$
 $33 \frac{4.4}{10.1.6}$
 $\frac{4.8}{-1.3}$
 $\frac{4.9}{10.11/33}$
 $\frac{6.0}{3.5}$
 $33 \frac{4.6}{10.1.4}$
 $\frac{4.7}{-1.2}$
 $\frac{4.4}{10.16/33}$
 $\frac{6.0}{3.5}$
 $33 \frac{4.6}{10.1.4}$
 $\frac{4.6}{-1.1}$
 $\frac{4.2}{10.18/33}$
 $\frac{6.1}{3.6}$
 $33 \frac{4.2}{10.1.9}$
 $\frac{4.3}{-0.7}$
 $\frac{4.0}{10.21/33}$
 $\frac{6.1}{3.6}$
 $33 \frac{4.2}{10.1.9}$
 $\frac{4.2}{-0.6}$
 $\frac{4.1}{10.20/33}$
 $\frac{6.2}{3.7}$
 $33 \frac{4.2}{10.2.0}$
 $\frac{4.2}{-0.5}$
 $\frac{4.4}{10.18/33}$
 $\frac{6.2}{3.7}$
 $33 \frac{4.3}{10.1.9}$
 $\frac{4.4}{-0.7}$
 $\frac{4.0}{10.22/33}$
 $\frac{6.3}{3.8}$
 $33 \frac{4.5}{10.1.8}$
 $\frac{4.7}{-0.9}$
 $\frac{4.7}{10.16/33}$

Nail in T.P. Lt. Sta. 41+

 $\frac{6.1}{3.6}$
 $33 \frac{4.4}{10.1.7}$
 $\frac{4.8}{-1.2}$
 $\frac{5.0}{10.11/33}$

Stb. + T - Grade

934.25

42

30.5

ISO

30.5

43

30.3

ISO

30.1

44

29.9

ISO

29.7

45

29.5

ISO

29.4

46

29.3

ISO

29.3

47

29.3

T.P.

7.44

935.43

6.16

927.99

ISO

29.4

4.

2

12.

$$3.8 \overline{) 6.3}$$

$$33 \overline{) \frac{40}{1023}}$$

$$\frac{50}{-1.2}$$

$$\frac{6.0}{1003} / 33'$$

$$3.8 \overline{) 6.3}$$

$$33 \overline{) \frac{48}{1015}}$$

$$\frac{50}{-1.2}$$

$$\frac{5.9}{1004} / 33$$

$$4.0 \overline{) 6.5}$$

$$33 \overline{) \frac{53}{1012}}$$

$$\frac{48}{-0.8}$$

$$\frac{5.1}{1014} / 33'$$

$$4.2 \overline{) 6.7}$$

$$33 \overline{) \frac{53}{1014}}$$

$$\frac{44}{-0.2}$$

$$\frac{4.3}{1024} / 33$$

$$4.4 \overline{) 6.9}$$

$$33 \overline{) \frac{53}{1016}}$$

$$\frac{45}{-0.1}$$

$$\frac{4.2}{10.2} / 33'$$

$$4.6 \overline{) 7.1}$$

$$33 \overline{) \frac{58}{1013}}$$

$$\frac{51}{-0.5}$$

$$\frac{5.0}{102.1} / 33'$$

$$4.8 \overline{) 7.3}$$

$$33 \overline{) \frac{5.8}{101.5}}$$

$$\frac{5.9}{-1.1}$$

$$\frac{5.2}{102.1} / 33'$$

$$4.9 \overline{) 7.4}$$

$$33 \overline{) \frac{6.8}{100.6}}$$

$$\frac{61}{-1.2}$$

$$\frac{5.7}{101.7} / 33'$$

$$5.0 \overline{) 7.5}$$

$$33 \overline{) \frac{6.8}{100.7}}$$

$$\frac{63}{-1.3}$$

$$\frac{61}{101.4} / 33$$

$$5.0 \overline{) 7.5}$$

$$33 \overline{) \frac{6.8}{100.7}}$$

$$\frac{63}{-1.3}$$

$$\frac{65}{101.0} / 33'$$

$$5.0 \overline{) 7.5}$$

$$33 \overline{) \frac{6.4}{101.1}}$$

$$\frac{62}{-1.2}$$

$$\frac{64}{101.1} / 33$$

$$6.0 \overline{) 8.5}$$

$$33 \overline{) \frac{6.5}{102.0}}$$

$$\frac{7.1}{-1.1}$$

$$\frac{6.9}{101.6} / 33'$$

Sta. + Σ - Grade

935.43

48

29.5

+50

29.7

49

29.9

+50

30.1

50

30.3

+70

30.4

2.34

B.M.

2.53

935.59

933.09

933.00

+0.43%

5140¹² R.P.T.

30.7

+50

30.9

L.

P.

Rt.

$$\begin{array}{r} 84 \\ 59 \end{array}$$

$$33 \overline{) 6.1} \\ \underline{66} \\ 2.3$$

$$\begin{array}{r} 66 \\ -07 \end{array}$$

$$65 \overline{) 19} / 33$$

$$\begin{array}{r} 8.2 \\ 57 \end{array}$$

$$33 \overline{) 57} \\ \underline{66} \\ 2.5$$

$$\begin{array}{r} 59 \\ -02 \end{array}$$

$$48 \overline{) 09} / 33$$

$$\begin{array}{r} 8.0 \\ 55 \\ 25 \end{array}$$

$$33 \overline{) 6.0} \\ \underline{66} \\ 2.0$$

$$\begin{array}{r} 52 \\ +03 \end{array}$$

$$37 \overline{) 1.8} / 33$$

$$\begin{array}{r} 7.8 \\ 53 \\ 20 \end{array}$$

$$33 \overline{) 6.0} \\ \underline{66} \\ 1.8$$

$$\begin{array}{r} 47 \\ +06 \end{array}$$

$$30 \overline{) 2.3} / 33$$

$$\begin{array}{r} 7.6 \\ 51 \end{array}$$

$$33 \overline{) 5.6} \\ \underline{66} \\ 2.0$$

$$\begin{array}{r} 47 \\ +04 \end{array}$$

$$37 \overline{) 1.4} / 33$$

$$\begin{array}{r} 7.5 \\ 50 \end{array}$$

$$33 \overline{) 5.8} \\ \underline{66} \\ 1.7$$

$$\begin{array}{r} 46 \\ +04 \end{array}$$

$$41 \overline{) 09} / 33$$

B. Pt.

$$\begin{array}{r} 6.9 \\ 49 \\ 2.0 \end{array}$$

$$33 \overline{) 5.2} \\ \underline{66} \\ 1.7$$

$$49$$

$$4.9 \overline{) 20} / 33$$

$$\begin{array}{r} 7.0 \\ 47 \\ 2.3 \end{array}$$

$$33 \overline{) 5.4} \\ \underline{66} \\ 1.6$$

$$\begin{array}{r} 49 \\ -02 \end{array}$$

$$47 \overline{) 2.3} / 33$$

93559

52

31.1

+50

31.1

53

31.0

+50

30.7

54

30.3

+50

29.7

55

29.0

+50

28.1

6.90

933.77

8.72

976.87

56

27.1

+50

26.2

+80

25.8

57

25.5

$$\begin{array}{r} 4.5 \\ \text{dit- } 7.6 \\ \hline \end{array} \quad \begin{array}{r} 7.1 \\ 33 \overline{) 5.0} \\ \underline{18.1} \end{array} \quad \begin{array}{r} 5.1 \\ -0.6 \\ \hline \end{array} \quad \begin{array}{r} 4.4 \\ +0.1 \\ \hline \end{array} / 33$$

$$\begin{array}{r} 4.5 \\ \text{dit- } 2.7 \\ \hline \end{array} \quad \begin{array}{r} 7.2 \\ 33 \overline{) 5.3} \\ \underline{10.1} \end{array} \quad \begin{array}{r} 4.9 \\ -0.4 \\ \hline \end{array} \quad \begin{array}{r} 4.4 \\ +0.1 \\ \hline \end{array} / 33$$

$$\begin{array}{r} 4.6 \\ \text{dit- } 2.7 \\ \hline \end{array} \quad \begin{array}{r} 7.3 \\ 33 \overline{) 5.5} \\ \underline{10.8} \end{array} \quad \begin{array}{r} 4.9 \\ -0.3 \\ \hline \end{array} \quad \begin{array}{r} 4.0 \\ +0.6 \\ \hline \end{array} / 33$$

$$\begin{array}{r} 4.9 \\ \text{dit- } 7.4 \\ \hline \end{array} \quad \begin{array}{r} 7.4 \\ 33 \overline{) 5.3} \\ \underline{12.1} \end{array} \quad \begin{array}{r} 4.8 \\ \hline \end{array} \quad \begin{array}{r} 5.6 \\ +1.3 \\ \hline \end{array} / 33$$

$$\begin{array}{r} 5.3 \\ \text{dit- } 7.8 \\ \hline \end{array} \quad \begin{array}{r} 7.8 \\ 33 \overline{) 5.3} \\ \underline{12.5} \end{array} \quad \begin{array}{r} 4.8 \\ +0.5 \\ \hline \end{array} \quad \begin{array}{r} 3.6 \\ +1.7 \\ \hline \end{array} / 33$$

$$\begin{array}{r} 5.9 \\ \text{dit- } 8.4 \\ \hline \end{array} \quad \begin{array}{r} 8.4 \\ 33 \overline{) 5.5} \\ \underline{10.4} \end{array} \quad \begin{array}{r} 5.5 \\ +0.4 \\ \hline \end{array} \quad \begin{array}{r} 3.9 \\ +2.0 \\ \hline \end{array} / 33$$

$$\begin{array}{r} 6.6 \\ \hline \end{array} \quad \begin{array}{r} 6.8 \\ 33 \overline{) 6.8} \\ \underline{12.3} \end{array} \quad \begin{array}{r} 6.6 \\ 0.0 \\ \hline \end{array} \quad \begin{array}{r} 5.0 \\ +1.6 \\ \hline \end{array} / 33$$

$$\begin{array}{r} 7.5 \\ \text{dit- } 10.0 \\ \hline \end{array} \quad \begin{array}{r} 10.0 \\ 33 \overline{) 9.3} \\ \underline{100.7} \end{array} \quad \begin{array}{r} 8.1 \\ -0.6 \\ \hline \end{array} \quad \begin{array}{r} 5.9 \\ +2.2 \\ \hline \end{array} / 33$$

$$\begin{array}{r} 6.7 \\ \text{dit- } 9.2 \\ \hline \end{array} \quad \begin{array}{r} 9.2 \\ 33 \overline{) 9.2} \\ \underline{100.0} \end{array} \quad \begin{array}{r} 7.3 \\ -0.6 \\ \hline \end{array} \quad \begin{array}{r} 3.6 \\ +3.4 \\ \hline \end{array} / 33$$

$$\begin{array}{r} 7.6 \\ \text{dit- } 10.1 \\ \hline \end{array} \quad \begin{array}{r} 10.1 \\ 33 \overline{) 9.3} \\ \underline{100.8} \end{array} \quad \begin{array}{r} 7.9 \\ -0.3 \\ \hline \end{array} \quad \begin{array}{r} 3.5 \\ +4.1 \\ \hline \end{array} / 33$$

$$\begin{array}{r} 8.3 \\ \hline \end{array} \quad \begin{array}{r} 9.4 \\ 33 \overline{) 9.4} \\ \underline{11.4} \end{array} \quad \begin{array}{r} 9.0 \\ -0.7 \\ \hline \end{array} \quad \begin{array}{r} 3.2 \\ +5.1 \\ \hline \end{array} / 33$$

933.77

57+44

250

58

24.7

+50

24.6

T.P.

5.76

930.51

9.02

924.75

59

24.7

+50

25.0

60

25.5

+50

26.1

61

26.7

+50

27.3

62

27.9

T.P.

7.98

935.13

3.26

927.15

Windy

$$8.8 \quad \frac{11.3}{-}$$

$$22 \overline{) 109} \\ \underline{104} $$

$$\frac{100}{-1.2}$$

$$\frac{5.1}{+3.7/33}$$

$$9.1$$

$$\frac{106}{-1.8}$$

$$\frac{7.5}{+1.6/33}$$

$$9.2 \quad 11.7$$

$$\frac{100}{-0.8}$$

$$\frac{9.7}{+2.0/33}$$

$$58 \quad 8.3$$

$$33 \overline{) 73} \\ \underline{100} $$

$$\frac{56}{+0.2}$$

$$\frac{7.0}{+1.3/33}$$

$$5.5 \quad 8.0$$

$$33 \overline{) 69} \\ \underline{101} $$

$$\frac{5.5}{+0.0}$$

$$\frac{6.3}{+1.7/33}$$

$$5.0 \quad 7.5$$

$$33 \overline{) 73} \\ \underline{100} $$

$$\frac{5.3}{-0.3}$$

$$\frac{5.8}{+1.7/33}$$

$$4.4 \quad 6.9$$

$$33 \overline{) 84} \\ \underline{100} $$

$$\frac{5.1}{-0.7}$$

$$\frac{5.1}{+1.8/33}$$

$$4.8 \quad 6.3$$

$$22 \overline{) 83} \\ \underline{78} $$

$$\frac{4.8}{-1.0}$$

$$\frac{4.8}{+1.5/33}$$

$$3.7 \quad 2.7$$

$$32 \overline{) 77} \\ \underline{70} $$

$$\frac{4.4}{-1.2}$$

$$\frac{3.8}{+1.9/33}$$

$$2.6$$

$$30 \overline{) 74} \\ \underline{48} $$

$$\frac{3.8}{-1.2}$$

$$\frac{3.8}{+1.8/33}$$

935.13

62+50

28.5

63

29.0

+50

29.4

64

29.7

+50

29.8

B.M.

0.98

932.81

2.30

932.83

65

29.8

+50

29.6

66

29.3

+50

28.9

67

28.4

T.P.

4.23

931.80

6.24

927.57

+65

27.7

d

$$6.6 \quad 51' \begin{array}{r} 11.6 \\ -5.0 \end{array}$$

$$\begin{array}{r} 7.9 \\ -1.2 \end{array}$$

$$\begin{array}{r} 7.4 \\ 101.7/29 \end{array}$$

$$6.1 \quad 78.0 \begin{array}{r} 10.1 \\ -4.0 \end{array}$$

(16)

$$\begin{array}{r} 7.0 \\ -0.9 \end{array}$$

$$\begin{array}{r} 4.8 \\ 11.3/33 \end{array}$$

$$5.7 \quad 34.2 \begin{array}{r} 10.1 \\ -5.4 \end{array}$$

(15)

$$\begin{array}{r} 6.0 \\ -0.3 \end{array}$$

$$\begin{array}{r} 4.2 \\ 11.5/33 \end{array}$$

4.7

4.4 — 5.4

$$34.2 \begin{array}{r} 9.8 \\ -5.4 \end{array}$$

(18)

$$\begin{array}{r} 5.1 \\ 10.3 \end{array}$$

$$\begin{array}{r} 4.3 \\ 11.1/30 \end{array}$$

4.3 5.3

$$31.8 \begin{array}{r} 8.9 \\ -4.6 \end{array}$$

18

$$\begin{array}{r} 4.5 \\ 10.8 \end{array}$$

932.85

Birch Lake Ave.

16'

15

4

5.0 3.0

$$24.0 \begin{array}{r} 7.0 \\ -2.0 \end{array}$$

18

$$\begin{array}{r} 3.5 \\ 10.5 \end{array}$$

$$\begin{array}{r} 3.0 \\ 11.0/33 \end{array}$$

5.2 3.2

$$21.8 \begin{array}{r} 6.5 \\ -1.6 \end{array}$$

17

$$\begin{array}{r} 4.6 \\ -0.4 \end{array}$$

$$\begin{array}{r} 3.6 \\ 10.6/33 \end{array}$$

4.9 4.1

$$35.5 \begin{array}{r} 11.4 \\ -6.5 \end{array}$$

16

$$\begin{array}{r} 5.2 \\ -0.7 \end{array}$$

$$\begin{array}{r} 4.0 \\ 10.1/33 \end{array}$$

4.9

$$34.3 \begin{array}{r} 11.0 \\ -6.1 \end{array}$$

16

$$\begin{array}{r} 5.6 \\ -0.7 \end{array}$$

$$\begin{array}{r} 4.0 \\ 10.9/33 \end{array}$$

5.6 5.4

$$31.6 \begin{array}{r} 10.8 \\ 5.2 \end{array}$$

16

$$\begin{array}{r} 6.0 \\ -0.6 \end{array}$$

$$\begin{array}{r} 3.7 \\ 11.7/33 \end{array}$$

4.8 3.4

$$27.1 \begin{array}{r} 5.7 \\ 2.0 \end{array}$$

17

4.2

$$\begin{array}{r} 4.6 \\ 12.5/33 \end{array}$$

931.80

68

27.4

+50

27.0

69

26.6

+50

26.3

70

25.9

T.P.

4.26 929.31 6.75

925.05

+50

25.7

71

25.5

+50

25.3

72

25.2

+25

25.1

+50

25.0

73

24.8

B.M.^v

6.11

$$\begin{array}{r} 5.2 \\ 4.4 \overline{) 34} \\ 28.3 \end{array} \quad \begin{array}{r} 59 \\ 1000 \end{array}$$

$$\begin{array}{r} 44 \\ 00 \end{array}$$

$$\begin{array}{r} 20 \\ 724 \overline{) 33} \end{array}$$

$$\begin{array}{r} 58 \\ 48 \overline{) 38} \end{array} \quad \begin{array}{r} 30.7 \\ 20.10 \end{array} \quad 16'$$

$$\begin{array}{r} 48 \\ 00 \end{array}$$

$$\begin{array}{r} 1.4 \\ 724 \overline{) 33} \end{array}$$

$$\begin{array}{r} 6.2 \\ 5.2 \overline{) 4.2} \end{array} \quad \begin{array}{r} 78.7 \\ 1000 \end{array} \quad 16'$$

$$\begin{array}{r} 93 \\ 01 \end{array}$$

$$\begin{array}{r} 1.3 \\ 724 \overline{) 33} \end{array}$$

$$\begin{array}{r} 6.5 \\ 5.5 \overline{) 4.5} \end{array} \quad \begin{array}{r} 27.4 \\ 1000 \end{array} \quad 16'$$

$$\begin{array}{r} 58 \\ 03 \end{array}$$

$$\begin{array}{r} 3.2 \\ 724 \overline{) 33} \end{array}$$

$$\begin{array}{r} 6.9 \\ 5.9 \overline{) 4.9} \end{array} \quad \begin{array}{r} 22.5 \\ 1000 \end{array} \quad 18'$$

$$\begin{array}{r} 64 \\ 05 \end{array}$$

$$\begin{array}{r} 4.9 \\ 110 \overline{) 33} \end{array}$$

$$\begin{array}{r} 4.6 \\ 3.6 \overline{) 2.6} \end{array} \quad \begin{array}{r} 31.3 \\ 4.1 \end{array} \quad 19'$$

$$\begin{array}{r} 13 \\ 07 \end{array}$$

$$\begin{array}{r} 4.4 \\ 100.7 \overline{) 33} \end{array}$$

$$\begin{array}{r} 4.8 \\ 3.8 \overline{) 2.8} \end{array} \quad \begin{array}{r} 35.1 \\ 9.8 \end{array} \quad 20$$

$$\begin{array}{r} 42 \\ 04 \end{array}$$

$$\begin{array}{r} 6.2 \\ 3.4 \overline{) 26.2} \end{array}$$

$$\begin{array}{r} 5.0 \\ 4.0 \overline{) 3.0} \end{array} \quad \begin{array}{r} 35.3 \\ 10.1 \end{array} \quad 20$$

$$\begin{array}{r} 47 \\ 07 \end{array}$$

$$\begin{array}{r} 6.6 \\ 3.6 \overline{) 26.8} \end{array}$$

$$\begin{array}{r} 5.1 \\ 4.1 \overline{) 3.1} \end{array} \quad \begin{array}{r} 35.9 \\ 10.5 \end{array} \quad 20$$

$$\begin{array}{r} 5.0 \\ 09 \end{array}$$

$$\begin{array}{r} 6.5 \\ 3.4 \overline{) 26.2} \end{array}$$

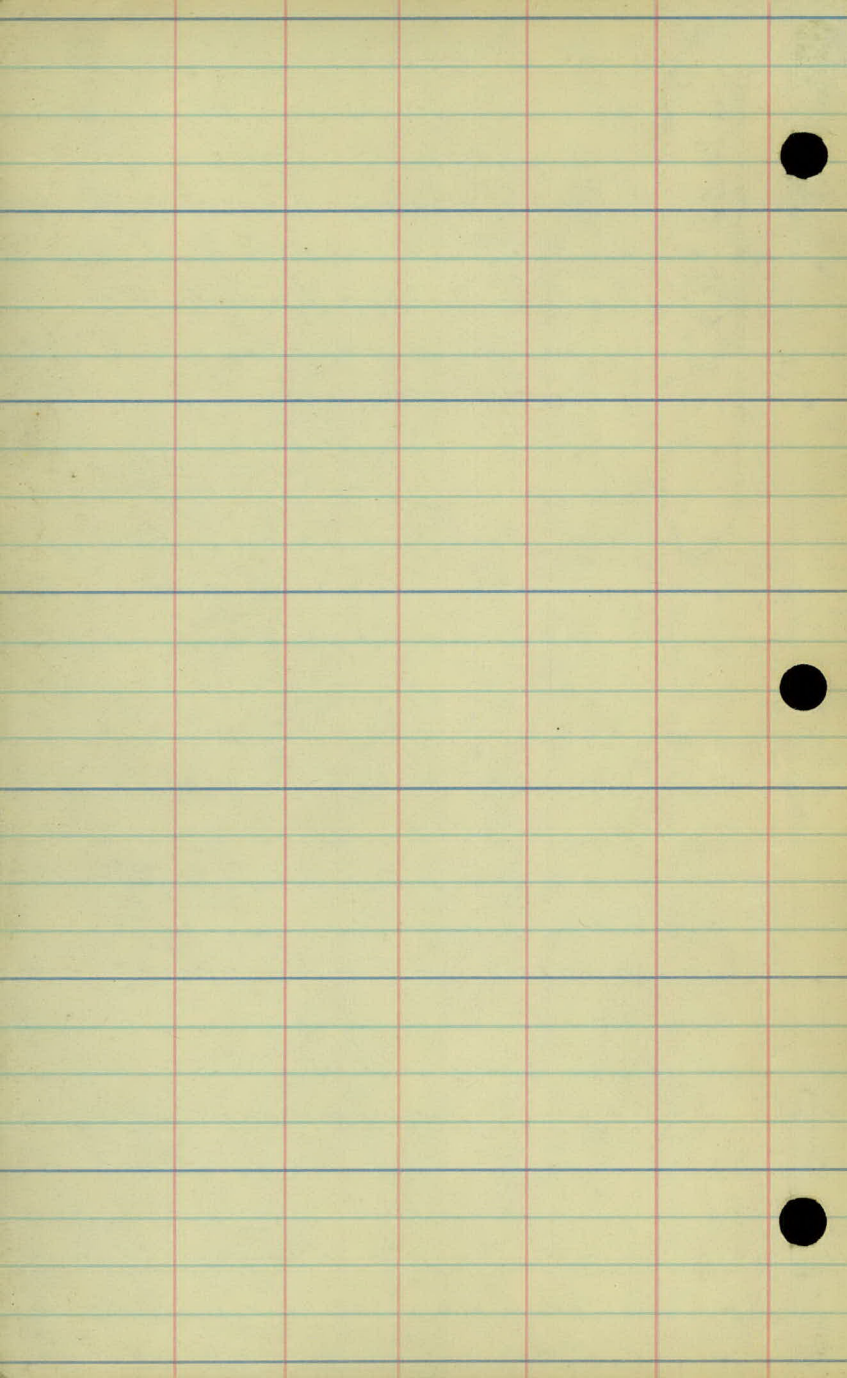
$$\begin{array}{r} 5.2 \\ 4.2 \overline{) 3.2} \end{array} \quad \begin{array}{r} 35.3 \\ 10.3 \end{array} \quad 20$$

$$\begin{array}{r} 48 \\ 06 \end{array}$$

$$\begin{array}{r} 4.3 \\ 3.3 \overline{) 2.3} \end{array} \quad \begin{array}{r} 38.5 \\ 9.3 \end{array} \quad 20$$

$$\begin{array}{r} 44 \\ 01 \end{array}$$

$$\begin{array}{r} 4.5 \\ 3.5 \overline{) 2.5} \end{array} \quad \begin{array}{r} 32.4 \\ 9.9 \end{array}$$



Revised grade

Otter Lake Rd.

Sta. 51- 56

B.M.

722

935.28

933.06

S140

30.7

30.7

+50

30.5

S2

30.3

+50

30.1

S3

29.9

+50

29.7

S4

29.5

+50

29.2

S5

28.7

+50

28.0

S6

27.1

$$4.6 \quad 38 \mid \frac{49}{50.22}$$

$$\frac{45}{101}$$

$$\frac{46}{102.5} / 33'$$

$$4.8 \quad 38 \mid \frac{51}{50.22}$$

$$\frac{45}{103}$$

$$\frac{44}{104} / 33'$$

$$5.0 \quad 38 \mid \frac{46}{104}$$

$$\frac{48}{102}$$

$$\frac{41}{109} / 33'$$

$$5.2 \quad 38 \mid \frac{50}{102}$$

$$\frac{47}{105}$$

$$\frac{39}{113} / 33'$$

$$5.4 \quad 33 \mid \frac{51}{103}$$

$$\frac{47}{107}$$

$$\frac{36}{118} / 33'$$

$$5.6 \quad 33 \mid \frac{50}{106}$$

$$\frac{48}{108}$$

$$\frac{33}{122} / 33'$$

$$5.8 \quad 33 \mid \frac{50}{108}$$

$$\frac{56}{102}$$

$$\frac{33}{125}$$

$$6.1 \quad 37 \mid \frac{51}{110}$$

$$0.0$$

$$\frac{3.6}{125} / 33'$$

$$6.6 \quad 30 \mid \frac{64}{102}$$

$$-0.4$$

$$\frac{49}{117} / 33'$$

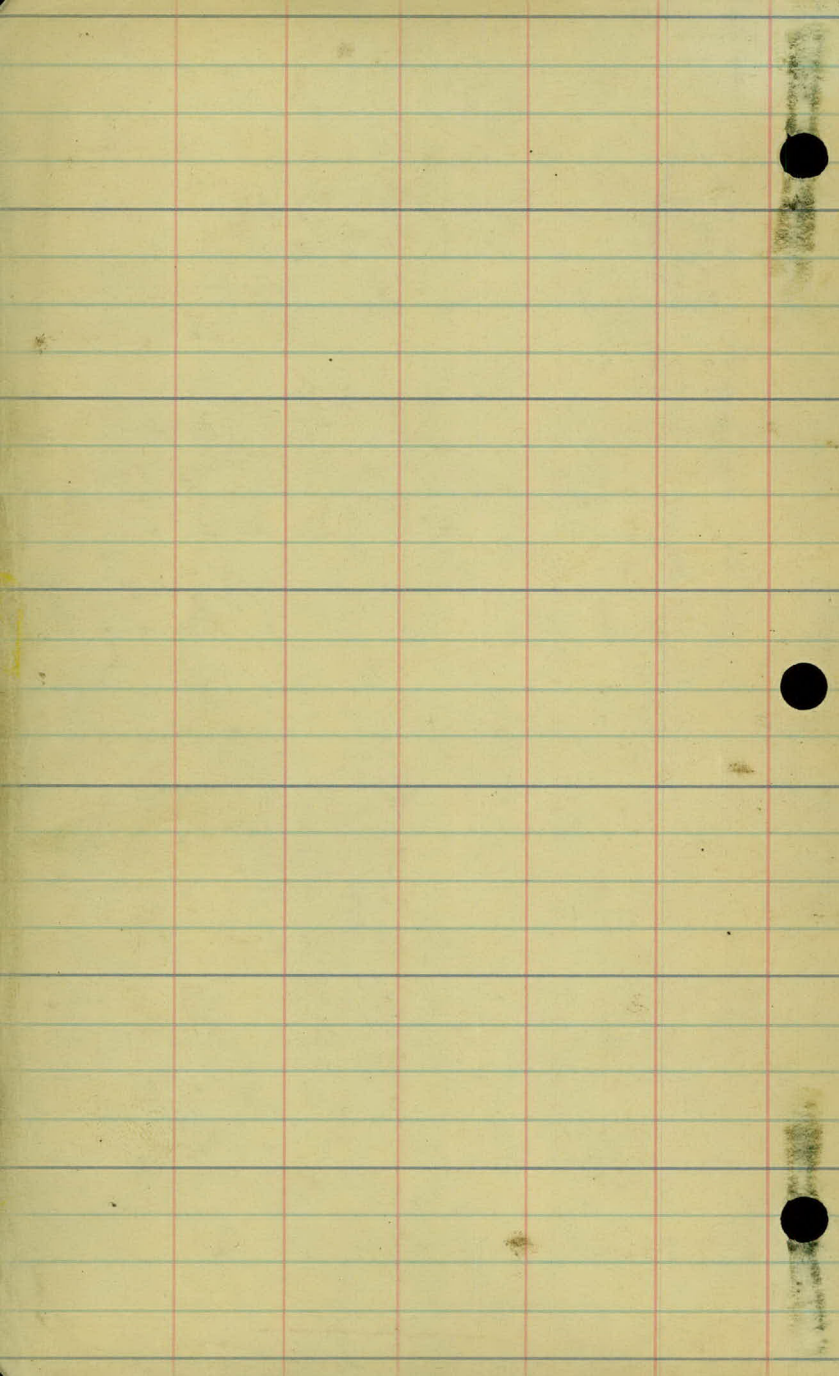
$$7.3 \quad 31 \mid \frac{91}{100.1}$$

$$-0.4$$

$$\frac{54}{119} / 33'$$

$$8.2$$

$$-0.5$$



RG
RJ
DD

Nov. 12, 1974
Overcast, Windy 25°

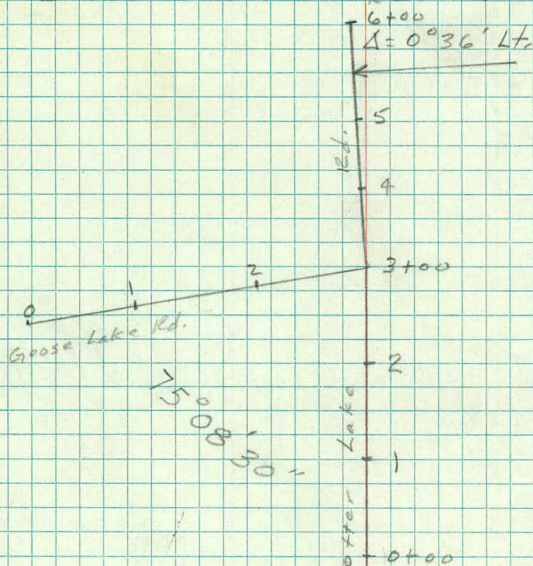
1.

Pavement & Entrance Location

Otter Lake Rd.

&

Goose Lake Rd.



otter Lake Rd

Rt

+50 $\frac{POR}{93}$ Lt

+33 $\frac{POR}{43.5}$

+33 Ent 11' Gravel

2+00

23.7 11.1

+84 $\frac{Iron}{33.00}$

+74 $\frac{74}{13.5}$ Bit.

+50
13.5 11.0

1+00

12.9 11.2

+92 $\frac{Iron}{33.00}$

+80 Ent 10' Gravel

+60 $\frac{Ent 12'}{35}$
Gravel

Rt = +44

0+00

12.8 11.2

+00 $\frac{Iron}{33.00}$

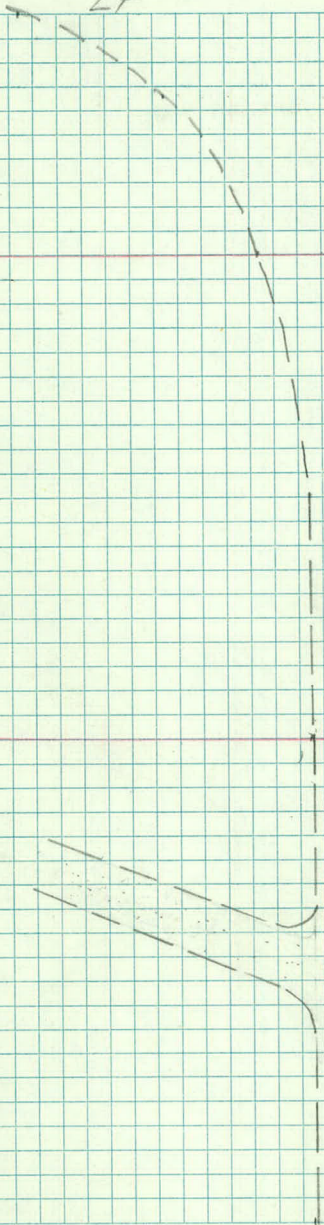
Nov 12, 1974

Lt

E

Rt

2



Otter Lake Rd

O I R & N

O I R & N

O I R & N

otter Lake Rd

5+00

Lt

12.7 11.5

Rt

4+00

12.8 12.0

+30 $\frac{ER}{13}$

+16 $\frac{POR}{26}$

+05 $\frac{BR}{38}$

3+00

10.8

+76 $\frac{1 \text{ RON}}{33.00}$

2+50

+50 $\frac{POR}{73}$

RG
DD

Nov. 13, 1974
Occ. Lt. Snow 25°

Lt

Rt

Rt

3



Older Lake Rd.



OIRON

Lt

Rt

+56 E tracks

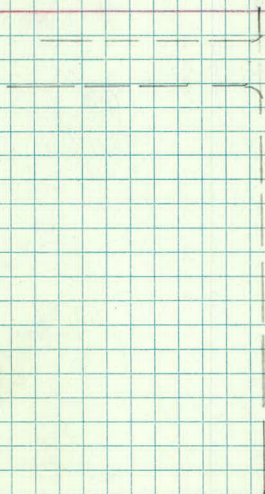
6+00

12.9 11.3

+89 Ent 9' Gravel

5+00

12.7 11.5



Ottar Lake Rd.



Goose Lake Rd

Lt 12.4

Rt

por

por

+50 55

+25

36

Gravel
+12 Ent 8'
(No Garage)

2+00

13.0

Gravel
Ent 8'

+92

29

Rt = 2+11

+75

BR
12

1+00

13.2 10.8

0+00

13.5 10.4

Lt

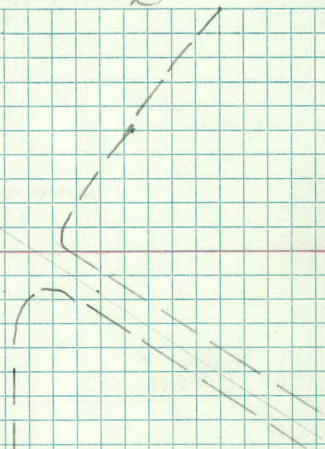
ℓ

Rt

5



Goose Lake Rd.



Goose Lake Rd.

LT

RT

6+28

IRON
33

+93

IRON
33

3+00

Rt = +86 +93 ER
39

BR

+62 13

+75 ER
12

2+50

12.4

+50

POR
55

Nov 13, 1974

L+

R

RT

L



IRON 0

6+28

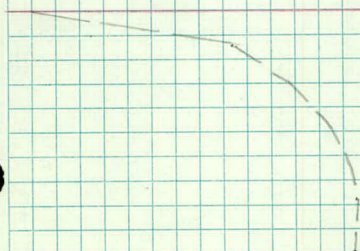
spike

235.90'

IRON 0

3+93

spike



G. H. H.

8.00

5.57

7.50

5.20

7.00

4.70

New G. H. H.

5.17

7.00

5.17

J, A.
LPD
DS

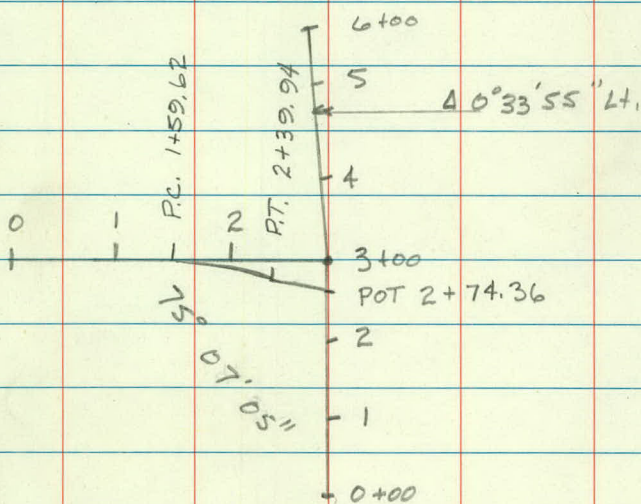
JUNE 15, 1976
P.C. 75°

1

ALIGNMENT

GEOMETRIC REVISIONS AT

GOOSE LAKE Rd & OTTER LAKE Rd



5+A

- 3+62.80

3+00

3+00

3+00

LPD
J.A.
DS
FK

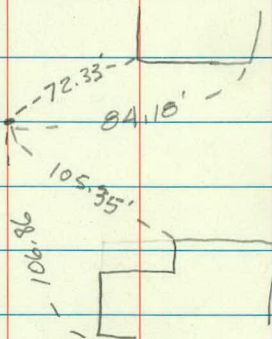
6-11-76

Sunny 95°

2

OTHER LAKE Rd

R/R SPIKE
found

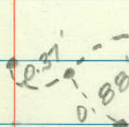


P.K.
0.75'
0.97' P.K.

found 2 SPIKES
in Bit Rdwy

P.K.
0.64'
0.97' P.K.

found 1 SPIKE
in Bit Rdwy



0.05' off E

found 1 SPIKE

Note: Record show that R/R SPIKE is to
BE LOCATED HERE but NONE found.

Sta

3+00

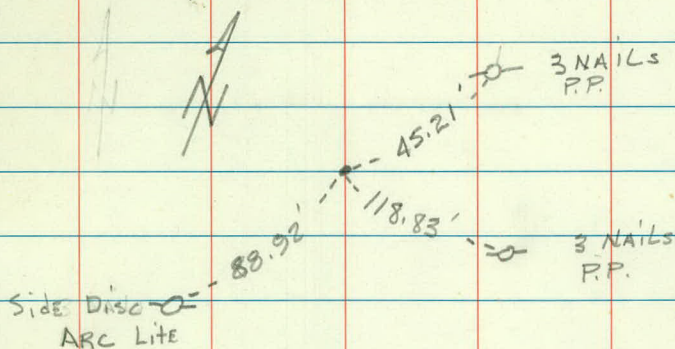
-3+62.5

J, A.
LPD
D.S.

OTHER LAKE RD

JUNE 15, 1976
P.C. 75°

3



STA	Point	Lt	A	Rt	CURVE DATA
2+39.94	P.T.				$7^{\circ}25'45''$
+25					$6^{\circ}02'52'' \Delta = 14^{\circ}51'30''$ $D = 18^{\circ}30''$
2+00	P.I.				$3^{\circ}44'07'' T = 40.38'$ $L = 80.32'$
+75					$1^{\circ}25'22'' R = 309.71'$
1+59.62	P.C.				$0^{\circ}00'00''$

J.A.
LPD
DS
B.W.

JUNE 16, 1974
P.C. 450

4

54A

0+00

5 +21.25

4+60.98

4+82.16

3+63.00

2+70.31

JUNE 18, 1976

5

IRON LOCATIONS

OTTER LAKE Rd

SCHUNEMAN Rd to GOOSE LAKE Rd

6+62.21

6

5

4

3

2

1

0+00

N

$$5 + \Delta$$

$$5 + 21.25$$

$$4 + 60.98$$

$$4 + 32.16$$

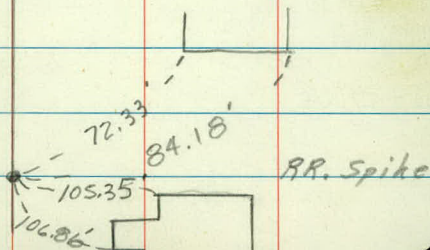
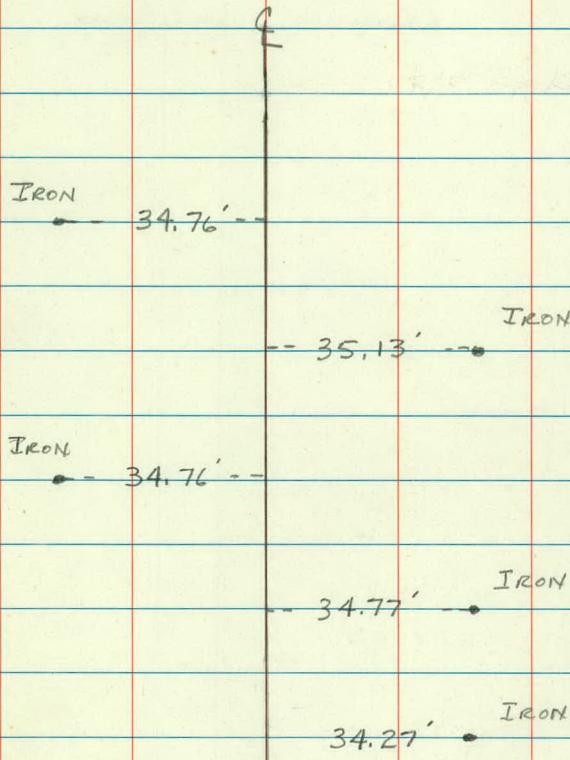
$$3 + 63.01$$

$$2 + 70.31$$

$$0 + 00$$

J.A.
LPD
DS
B.W.

JUNE 18, 1976
CLdy 60° 6



5+A

6+62.21

6+36.81

5+47.82

J.A.
L.P.O.
D.S.
B.W.

JUNE 18, 1976

E

CLdy 60°

7

